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# Adelaide Apartments Tower Expansion

Stormwater Management and Servicing Brief

# STORMWATER MANAGEMENT AND SERVICING BRIEF

Adelaide Apartments Tower Expansion

Prepared By:

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> January 5<sup>th</sup>, 2016 September 20<sup>th</sup>, 2016 **Revised: January 25<sup>th</sup>, 2019**

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January 25<sup>th</sup>, 2019

City of Ottawa Planning and Growth Management Department Development Review (Urban Services) 110 Laurier Avenue West Ottawa, Ontario K1P 1J1

#### Attention: Mark Fraser

#### **Re: Adelaide Apartments Tower Expansion – Stormwater and Servicing Brief**

Enclosed is a copy of the revised 'Stormwater Management and Servicing Brief' for the proposed development at Preston Square in the City of Ottawa. This brief is submitted in support of the site plan application and demonstrates how the site will be serviced with sanitary, storm, and water infrastructure.

Should you have any questions, please contact me.

#### NOVATECH

Greg MacDonald, P.Eng. Director, Land Development and Public Sector Infrastructure

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### 1.0 INTRODUCTION

The proposed development is located at Preston Square which is a 2.1 hectare (ha) urban mixeduse development located north of Aberdeen Street, between Preston Street and Rochester Street, as shown in **Figure 1 – Key Plan**.

The proposed development will consist of a 30-storey, 228-unit residential tower, located on top of four existing underground parking levels within Preston Square. The proposed tower will connect to the existing 8-storey Adelaide residential building. An additional floor will be added to the existing Adelaide building, which will include 24 units. In addition to the Adelaide building (referred to as Block B), the property also contains three existing commercial towers, referred to as Blocks A, C and D. See **Figure 2 – Existing Conditions** for illustration.

A Stormwater Management and Servicing Brief was previously submitted in support of a Site Plan application for the proposed development in 2016. The concept for the proposed development has since been revised and is presented in this revised report.

#### 1.1 Purpose

This servicing brief addresses the approach to site servicing and stormwater management for the proposed development and is being submitted in support of a site plan control application.

The objective of the site servicing design is to conform to the requirements of the City of Ottawa, to provide suitable sewage outlets and to ensure that a domestic water supply and appropriate fire protection are provided for the proposed development.

Servicing criteria, expected sewage flows and water demands for the proposed development have been established using the City of Ottawa design guidelines for sewer systems and water distribution.

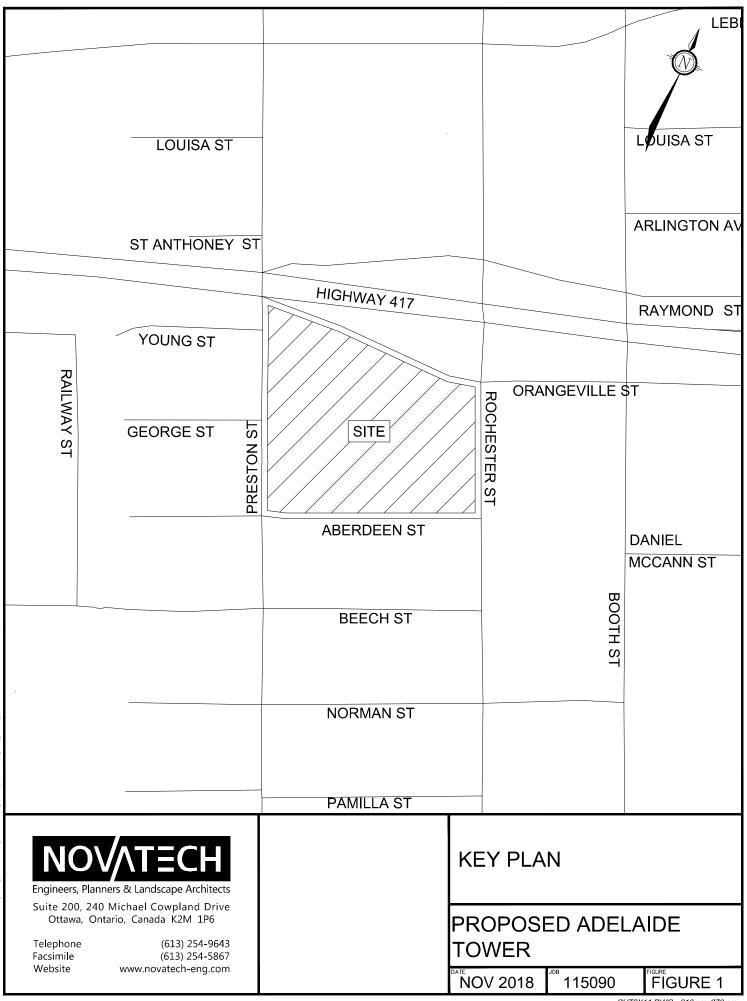
The City of Ottawa Servicing Study Guidelines for Development Applications requires that a Development Servicing Study Checklist be included to confirm that each applicable item is deemed complete and ready for review by City of Ottawa Infrastructure Approvals. A completed checklist in enclosed in **Appendix A**.

#### 2.0 SANITARY SEWER

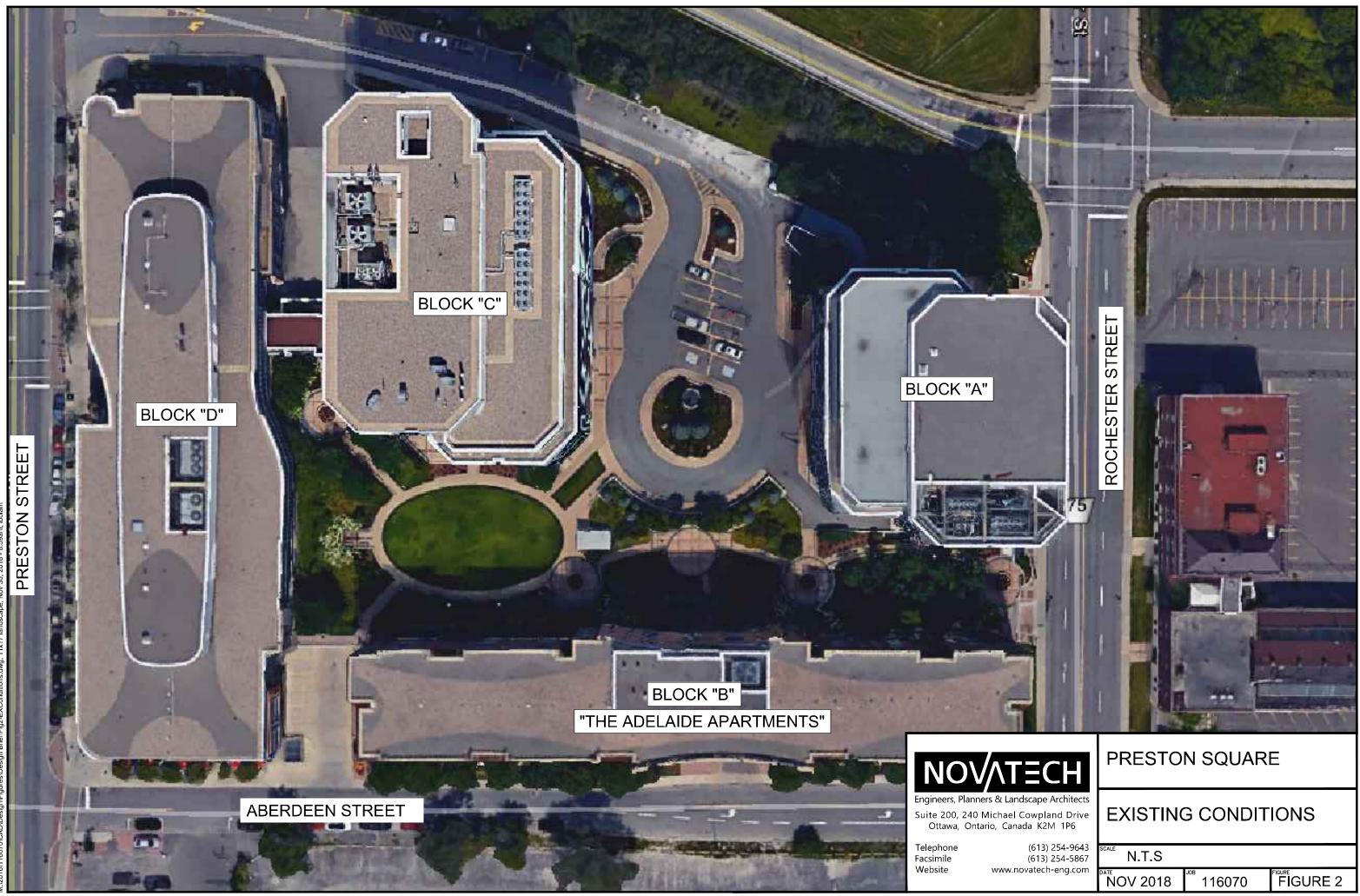
The proposed development will be serviced by a new 200mm dia. sanitary service that will outlet to an existing 1200mm dia. municipal sewer on Aberdeen Street. This sewer flows west on Aberdeen Street before discharging into the existing 1650mm dia. combined trunk sewer on Preston Street which flows north.

#### 2.1 Design Criteria

The City of Ottawa design criteria were used to calculate the theoretical proposed sanitary flows. The following design criteria were taken from Section 4 – 'Sanitary Sewer Systems' of the City of Ottawa Sewer Design Guidelines, incorporating the revisions as per Technical Bulletin ISTB-2018-01.



SHT8X11.DWG - 216mmx279mm



SHT11X17.DWG - 279mmX432mm

Residential Population Densities

- Residential Units (1-bedroom Apartment):
- Residential Units (2-bedroom Apartment):

#### **Residential Flows**

- Average Daily Residential Sewage Flow:
- Residential Peaking Factor:

1.4 people / unit 2.1 people / unit

280 L / person / day Per Harmon Equation (Max. 4.0, Correction Factor=0.8)

<u>Extraneous Flows</u> N/A

The proposed development is located within an existing development as described in Section **1.0** above. The proposed sanitary service is solely dedicated to the new Tower. The proposed development will not increase the extraneous flows currently generated by the site and therefore its value has been omitted from the proposed sanitary flow calculations. Therefore, the following sanitary flow calculations represent the net increase in sanitary flows from the site.

#### 2.2 Proposed Sanitary Flows

Table 2.2 details the sanitary design flows for the proposed development.

Building	Use	Unit Count	Design Population (people)	Average Flow (L/s)	Peak Flow (L/s)
New Tower	Residential	216 x 1-bdrm 12 x 2-bdrm	328	1.06	3.54 <sup>1</sup>
1-storey Addition		22 x 1-bdrm 2 x 2-bdrm	35	0.11	0.38 <sup>1</sup>
Total		252 Units	363	1.17	3.92

 Table 2.2: Theoretical Sanitary Design Flows for Proposed Development

<sup>1</sup> Excluding extraneous flow.

Based on Manning's Equation, a 200mm dia. sanitary gravity service at a minimum slope of 1.0% has a full flow conveyance capacity of approximately 34.2 L/s, which is sufficient to convey the theoretical sanitary design flows calculated above. Refer to the Sanitary Sewer Design Sheet in **Appendix B** for detailed calculations.

#### 3.0 STORMWATER MANAGEMENT

#### 3.1 Existing Site Stormwater Management

Stormwater flows from the Preston Square site are currently split into two drainage areas, as described in the *Stomwater Management Report Tower C and Block D City Gate Corporation*, dated October 2005 (R-2005-116) by Novatech, summarized as follows:

- Drainage Area 1 (northern part of the site): Flows are conveyed to the existing 1650mm dia. combined sewer on Preston Street via an on-site 1200mm diameter super pipe. The on-site super pipe utilizes a 250mm diameter orifice at its outlet to control the flows. Flows from the roofs of Buildings A and C are controlled by roof drains.
- Drainage Area 2 (southern part of the site): Flows are conveyed to the existing 1200mm dia. combined sewer on Aberdeen Street. Flows from the roofs of Buildings B (The Adelaide Apartments) and D are controlled by roof drains.

### 3.2 Stormwater Management Design Criteria and Methodology

The stormwater management criteria and objectives for the site (as per the above referenced 2005 report) are as follows:

- Provide a dual drainage system (i.e. minor and major system flows).
- Control the post-development flows from the site to allowable release rates corresponding to the 5-year and 100-year peak flows using a runoff coefficient of 0.4 and a 20-minute rainfall intensity derived from City of Ottawa IDF curves, as specified by the City of Ottawa. Post-development peak flows will be controlled for storms up to and including the 100-year design event, prior to being released into the municipal combined sewers in Aberdeen Street and Preston Street.
- Provide guidelines to ensure that site preparation and construction is in accordance with the current best management practices for erosion and sediment control.

The stormwater management design for the proposed development is based on the methodology implemented in the above referenced 2005 report.

The Modified Rational Method was used to determine the storage volume(s) required to control the post-development runoff flows to the allowable release rates and to determine the size of the control structure(s).

#### 3.3 Allowable Release Rates

The allowable release rates for the site for the 5-year and the 100-year design events were calculated using the Rational Method and are summarized in **Table 3.3**.

#### Table 3.3: Allowable Release Rates

Area	Allowable Release Rate (L/s)			
Alea	5-year	100-year		
Area 1 (1.304 ha)	101.5 L/s	174.0 L/s		
Area 2 (0.802 ha)	62.4 L/s	107.0 L/s		
Total (Site)	163.9 L/s	281.0 L/s		

Refer to **Appendix C** for detailed calculations.

#### 3.4 Post-Development Site Conditions

The area of the site to be developed will be split between the two drainage areas as shown on attached drawing **116070-STM**. A brief description of the various sub-catchment areas is as follows:

- Drainage Area 1: Runoff from the street-level areas around the exterior of the new Tower will drain uncontrolled via podium drains and catchbasins to the existing 1200mm dia. superpipe. Flows from this superpipe to the combined sewer on Preston Street will continue to be controlled by an orifice at the outlet of the pipe.
- Drainage Area 2: Runoff from the proposed Tower roof (Area B-2) and the new roof on the proposed 9<sup>th</sup> floor addition to the Adelaide Apartment building (Area B-1) will be controlled by roof drains. There will be 10 roof drains on the new roof of the Adelaide Apartment building and 12 roof drains on the roof of the new Tower. These roof drains will outlet to the combined sewer in Aberdeen Street.

The rest of the site is unchanged.

#### 3.4.1 Drainage Area 1

#### Controlled Flow from Block A and C Roofs (Area 1-R)

The flows from the roof areas in Area 1 are attenuated by controlled flow roof drains. There are 14 existing roof drains in Area 1 (6 and 8 roof drains for Blocks A and C respectively). The roof drains on average discharge 1.0 L/s, so flows from the roofs of existing buildings A (Area 1-"A") and C (Area 1-"C") are controlled to approximately 14 L/s for the 5-year and 100-year design events.

Refer to the *Stomwater Management Report Tower C And Block D City Gate Corporation*, (R-2005-116) dated October 2005 by Novatech for details.

#### Controlled Surface Flow (Area 1-A)

The flows from surface areas in Area 1 are currently attenuated by a 250mm dia. orifice plug type ICD installed within the 300mm dia. outlet pipe of MH1. Stormwater runoff from this drainage area is temporarily stored in an underground superpipe prior to being discharged into the municipal storm sewer system. Additional storage is available in the existing catchbasins and manholes. **Table 3.4**-A summarizes the existing available storage volumes for Area 1.

Item	Area (m²)	Depth (m)	Length (m)	Approximate Storage Volume (m³)
1200mm dia. superpipe	1.17	N/A	99.80	116.8
CB 3 (600mmx600mm)	0.36	= 60.35 - 59.37 = 0.98	N/A	0.4
CB 1 (600mmx600mm)	0.36	= 60.35 - 58.98 = 1.37	N/A	0.5
MH1 (2440mm dia.)	4.67	= 60.35 - 58.50 = 1.85	N/A	8.6

Total				130.7 m³
STM 2 (1200mm dia.)	1.13	= 60.35 - 58.65 = 1.70	N/A	1.9
STM 1 (1300mm dia.)	1.32	= 60.35 - 58.46 = 1.89	N/A	2.5

The design release rate for flows from the surface areas of Area 1 was set to meet the allowable release rate for Area 1, taking into account the existing controlled flows from the roof areas. The Modified Rational Method was used to determine the storage volume required for this catchment area.

**Table 3.4-B** summarizes the post-development flows and the required storage volumes for runoff from the surface areas for the 5-year and the 100-year design events for Area 1.

	Roof Areas				
Design Event	Controlled Flow (L/s)	Uncontrolled Flow (L/s)	Design Release Rate (L/s)	Storage Volume Required (m³)	Total Flow for Area 1 (L/s)
5-year	14	135.6	87.5	69 m³	101.5
100-year	14	232.5	160.0	112 m³	174.0

Table 3.4-B: Summary of Area 1 Post-Development Flows and Required Storage Volume

The existing available storage volume is greater than the storage volume required for the 100-year design event, therefore there is adequate existing storage available to meet the required storage volumes for Area 1.

# Inlet Control Device (ICD) Sizing

To achieve the design release rate to the combined sewer on Preston Street, a new orifice will need to be installed. This orifice has been sized using the following orifice equation:

Q = CA(2gh)	^0.5	
Where:	Q C h g A	<ul> <li>= Discharge (m³/s) = 100-year design release rate (0.160 m³/s)</li> <li>= 0.61 (circular hole)</li> <li>= head required (m) = 1.88m (value chosen for no ponding)</li> <li>= 9.81 m/s<sup>2</sup></li> <li>= Area of Orifice (m<sup>2</sup>)</li> </ul>
∴ A =	9 = 0.61* 0.0432 0.234 n	

To achieve the design release rate to the combined sewer, a new Tempest MHF ICD SQ 234mm orifice will be installed at the connection to the 2440mm diameter manhole. Shop drawing has been attached in **Appendix C.** 

### 3.4.2 Drainage Area 2

#### Controlled Flow from Block D (Area 2-"D")

Runoff from the roof of Building D is currently controlled by roof drains. There are 8 existing roof drains on Building D, which will remain. These existing controlled flow roof drains discharge on average 1.0 L/s. Therefore, there is a total controlled flow of approximately 8 L/s for the 5-year and 100-year design events from the roof of Building D.

#### Controlled Flow from Building B and New Tower (Areas 2-"B1" and 2-"B2")

The post-development flows from roof areas 2-"B1" (the Adelaide) and 2-"B2" (the new Tower) will be attenuated by the use of controlled flow roof drains. Watts Adjustable Flow Control Roof Drains set at <sup>1</sup>/<sub>4</sub> weir opening exposed are proposed.

A total of ten (10) roof drains are proposed on the Adelaide building and fourteen (14) roof drains are proposed on the new Tower. The controlled release rate, ponding depth, required and maximum storage volumes for both the 5-year and 100-year design events are summarized in the **Table 3.4**-**C** below.

Roof Drain ID	Controlled Flow (L/s)		Ponding Depth (m)		Storage Vol. Required (m <sup>3</sup> )		Max. Storage	
	5-year	100-year	5-year	100-year	5-year	100-year	Available (m <sup>3</sup> )	
2-"B1" (RD1 – RD10)	7.9	8.7	0.07-0.11	0.13-0.14	31.7	64.6	74.8	
2-"B2" (RD11-RD24)	9.8	11.1	0.05-0.08	0.10-0.14	2.5	7.4	8.9	

#### Table 3.4-C: Areas 2-"B1" and 2-"B2" Controlled Flow Building Roof Drains

Refer to **Appendix C** for Modified Rational Method calculations and Watts adjustable flow control roof drain information.

#### Uncontrolled Surface Flow (Area 2-A)

The post-development flows from the surface areas of Area 2 will remain uncontrolled. **Table 3.4-D** summarizes the post-development flows for Area 2.

#### Table 3.4-D: Summary of Area 2 Post-Development Flows

Design Event	Roof Areas Controlled Flow (L/s)	Surface Areas Uncontrolled Flow (L/s)	Tota	al Flow for Area 2 (L/s)
5-year	25.7 L/s	33.9 L/s	59.6 L/s	< Allowable Rate of 62.4 L/s
100-year	27.8 L/s	58.1 L/s	85.9	< Allowable Rate of 107.0 L/s

### 3.5 Summary of Site Post-Development Flows

Table 3.5 summarizes the total post-development flows from the site.

Area	Post-Development Flows (L/s)				
Alea	5-year	100-year			
1	101.5	174.0			
2	59.6	85.9			
Total Site	161.1 L/s	259.9 L/s			
	< 163.9 L/s Site Allowable Release Rate	< 281.0 L/s Site Allowable Release Rate			

As the 100-year total site post-development stormwater flow is less than the 100-year site allowable release rate to the municipal combined sewer system, there is remaining capacity for the net increase of approximately 3.9 L/s in peak sanitary flow from the proposed development.

### 3.6 Major Overland Drainage

The site was originally designed to direct major overland drainage flows in excess of the 100-year event flow overland towards Preston and Aberdeen Street. The proposed development will maintain the existing overland flow patterns.

#### 4.0 WATERMAIN

The proposed development will be serviced with twin 150 mm dia. PVC DR 18 services that will connect to the existing 200mm dia. watermain on Aberdeen Street.

#### 4.1 Design Criteria

The City of Ottawa design criteria were used to calculate the theoretical water demands for the proposed development. The following design criteria were taken from Section 4 of the Ottawa Design Guidelines – Water Distribution:

**Residential** 

•	Residential Units (1-bedroom apartment): Residential Units (2-bedroom apartment):	1.4 people / unit 2.1 people / unit
•	Average Day Demand Residential:	350 L / person / day
	Residential Maximum Day Demand: Residential Peak Hour Demand:	2.5 x Avg. Day Demand 2.2 x Max Day Demand

#### 4.2 Average, Maximum Day and Peak Hour Demands

The theoretical water demands for the proposed development are given in **Table 4.2**, based on the design criteria above.

Building	Use	Average Water Demand (L/s)	Maximum Day Demand (L/s)	Peak Hour Demand (L/s)
New Tower	New Tower Residential		3.32	7.31
1-storey Addition	Residential	0.14	0.35	0.78
Total		1.47 L/s	3.68 L/s	8.09 L/s

Refer to **Appendix D** for detailed calculations.

# 4.3 Water Supply for Fire-Fighting

The Fire Underwriters Survey (FUS) was used to estimate fire flow requirements for the proposed Tower. In the absence of detailed architectural information, some assumptions were made regarding the building construction. A fire-resistive construction was assumed due to the large size and type of occupancy for the proposed building. Also, the proposed Tower will be fully sprinklered and supplied with a fire department siamese connection(s), located within 45m of the existing on-site fire hydrant adjacent to Tower A.

The fire flow requirements include both sprinkler system and hose allowances in accordance with the OBC and NFPA 13. The sprinkler system will be designed by the fire protection (sprinkler) contractor at the detailed design stage as this process involves detailed hydraulic calculations based on building layout, pipe runs, head losses, fire pump requirements, etc. Booster pumps will be required to provide adequate service pressure on the upper floors.

It should be noted that fire flow requirements calculated using the FUS method tend to generate higher values when compared to flows being calculated using the OBC and NFPA. In the previous 2016 version of this report, the fire flow required for the proposed Tower was calculated using OBC to be 550 US gpm, or 35 L/s. Since then the building design has been updated.

The calculated fire flow demand for the updated proposed Tower using FUS is 67 L/s (4,000 L/min). Refer to **Appendix D** for detailed FUS calculations.

# 4.4 Boundary Conditions and Summary of Watermain Analysis Results

Preliminary water demands and fire flow requirements for the proposed development were provided to the City of Ottawa in 2016. These values were used to generate the municipal watermain network boundary conditions. **Table 4.4-A** summarizes the boundary conditions provided by the City of Ottawa for the existing municipal watermain network.

Municipal Watermain Boundary Condition	Aberdeen St Watermain
Minimum HGL	106.1 m
Maximum HGL	117.5 m
Max Day + Fire Flow	104.2 m

#### Table 4.4-A: Hydraulic Boundary Condition Provided by the City

Refer to **Appendix D** for a copy of the previous correspondence from the City of Ottawa.

**Table 4.4-B** summarizes the theoretical water demands for the Tower under the various operating conditions and compares the anticipated operating pressures at the watermains to the normal operating pressures outlined in the City of Ottawa Design Guidelines. It is assumed that hydraulic losses in the 150mm water services are negligible. Furthermore, the proposed Tower will be equipped with booster pumps to increase pressure for the upper floors.

Condition	Water Service Connection Location	Total Water Demand (L/s)	Approximate Design Operating Pressures (psi) / Relative Head (m) <sup>1</sup>	Normal Municipal Operating Pressures (psi)
Average Demand		1.33	85 psi (60.05 m)	50-70 psi
Max Day + Fire Flow Demand	Aberdeen Street	70.33	66 psi (46.75 m)	20 psi (Min.)
Peak Hour Demand		7.33	69 psi (48.65 m)	40-70 psi

#### Table 4.4-B: Water Analysis Results Summary

1 - Assuming top of watermain elevation to be 57.45 m

As the approximate design operating pressure for the Average Demand condition is higher than the normal municipal operating pressure range, a pressure check will be completed at completion of construction to determine if pressure control is required.

As indicated in the summary table above, the existing watermain in Aberdeen Street should have sufficient water supply for the proposed Tower.

#### 5.0 Erosion & Sediment Control

To mitigate erosion and to prevent sediment from entering the storm sewer system, temporary erosion and sediment control measures will be implemented on-site during construction in accordance with the Best Management Practices for Erosion and Sediment Control. This includes the following temporary measures:

- Filter bags will be placed under the grates of nearby catchbasins, manholes and will remain in place until construction is completed.
- Silt fencing will be placed per OPSS 577 and OPSD 219.110 along the surrounding construction limits, where applicable.
- Mud mats will be installed at the site entrances.
- Street sweeping and cleaning will be performed, as required, to suppress dust and to provide safe and clean roadways adjacent to the construction site.
- On-site dewatering is to be directed to a sediment trap and/or gravel splash pad and discharged safely to an approved outlet as directed by the engineer.

The temporary erosion and sediment control measures will be implemented prior to construction and will remain in place during all phases of construction. Regular inspection and maintenance of the erosion control measures will be undertaken.

#### 6.0 CONCLUSIONS

This report has been prepared in support of a site plan control application for the proposed development at Preston Square. The proposed development will consist of a new 30-storey residential Tower and the addition of a single storey to the existing 8-storey Adelaide Apartments residential building.

The conclusions are as follows:

- The proposed development will include a total of ±252 residential units.
- The new residential Tower will be serviced by extending new services to the municipal watermain and combined sewer in Aberdeen Street.
- On-site stormwater quantity control will be provided by using controlled roof drains and the existing stormwater management infrastructure, which includes controlled outlets. The existing inlet control device will be adapted. A new 234mm dia. orifice plug type ICD will be installed at the Preston Street stormwater outlet to the combined municipal sewer.
- As total combined stormwater and sanitary flows to the municipal combined sewer system will meet the allowable site flows, the municipal combined sewers in the adjacent streets are estimated to have adequate capacity to accommodate the proposed development.
- The proposed Tower will be sprinklered and supplied with a fire department Siamese connection. The Siamese connection will be located within 45m of an existing private fire hydrant in Preston Square. Based on hydraulic boundary conditions provided by the City of Ottawa, the existing municipal water system has adequate capacity to accommodate the proposed development.
- On-site stormwater quality control is not required, nor being provided.
- Temporary erosion and sediment controls will be provided during construction.

It is recommended that this Stormwater Management and Servicing Brief be approved for implementation.

#### NOVATECH

Prepared by:

Bolam

Lydia Bolam, B.Eng. E.I.T. Reviewed By:



Greg MacDonald, P.Eng. Director, Land Development and Public Sector Infrastructure

# APPENDIX A

4.1 General Content	Addressed (Y/N/NA)	Section	Comments
Executive Summary (for larger reports only).	NA		
Date and revision number of the report.	Y	Cover	
Location map and plan showing municipal address,	Y		Figure 1 & Dwgs.
boundary, and layout of proposed development.	I		Figure 1 & Dwgs.
Plan showing the site and location of all existing services.	Y		Dwg. 116070-GP
Development statistics, land use, density, adherence to			
zoning and official plan, and reference to applicable	Y	1.0	
subwatershed and watershed plans that provide context	T	1.0	
to which individual developments must adhere.			
Summary of Pre-consultation Meetings with City and	N/A		
other approval agencies.	N/A		
Reference and confirm conformance to higher level			
studies and reports (Master Servicing Studies,			
Environmental Assessments, Community Design Plans),	Y	1.1	
or in the case where it is not in conformance, the	T		
proponent must provide justification and develop a			
defendable design criteria.			
Statement of objectives and servicing criteria.	Y	1.1	
Identification of existing and proposed infrastructure	Y	2.0 - 4.0	Dwg. 116070-GP
available in the immediate area.	I	2.0 - 4.0	Dwg. 110070-GF
Identification of Environmentally Significant Areas,			
watercourses and Municipal Drains potentially impacted	N/A		
by the proposed development (Reference can be made	N/A		
to the Natural Heritage Studies, if available).			
Concept level master grading plan to confirm existing and			
proposed grades in the development. This is required to			
confirm the feasibility of proposed stormwater			
management and drainage, soil removal and fill	Y		Dwg. 116070-GR
constraints, and potential impacts to neighboring	T		Dwg. 1100/0-0K
properties. This is also required to confirm that the			
proposed grading will not impede existing major system			
flow paths.			

4.1 General Content	Addressed (Y/N/NA)	Section	Comments
Identification of potential impacts of proposed piped services on private services (such as wells and septic fields on adjacent lands) and mitigation required to address potential impacts.	N/A		
Proposed phasing of the development, if applicable.	N/A		
Reference to geotechnical studies and recommendations concerning servicing.	N/A		
All preliminary and formal site plan submissions should have the following information:	Y		
Metric scale	Y		
North arrow (including construction North)	Y		
Key plan	Y		
Name and contact information of applicant and property owner	Y		
Property limits including bearings and dimensions	Y		
Existing and proposed structures and parking areas	Y		
Easements, road widening and rights-of-way	Y		
Adjacent street names	Y		

4.2 Water	Addressed (Y/N/NA)	Section	Comments
Confirm consistency with Master Servicing Study, if	NI / A		
available.	N/A		
Availability of public infrastructure to service proposed	V		
development.	Y		
Identification of system constraints.	Y	4.0	
Identify boundary conditions.	Y	4.0	
Confirmation of adequate domestic supply and pressure.	Y	4.0	
Confirmation of adequate fire flow protection and			
confirmation that fire flow is calculated as per the Fire	V	4.0	
Underwriter's Survey. Output should show available fire	Y	4.0	
flow at locations throughout the development.			
Provide a check of high pressures. If pressure is found to			
be high, an assessment is required to confirm the	Y	4.0	
application of pressure reducing valves.			
Definition of phasing constraints. Hydraulic modeling is			
required to confirm servicing for all defined phases of the	N/A		
project including the ultimate design.			
Address reliability requirements such as appropriate			
location of shut-off valves.	Ν		Detailed Design Requirement
Check on the necessity of a pressure zone boundary			
modification.	N/A		
Reference to water supply analysis to show that major			
infrastructure is capable of delivering sufficient water for			
the proposed land use. This includes data that shows that			
the expected demands under average day, peak hour and	Ν		Fire Demand Checked Only
fire flow conditions provide water within the required			
pressure range.			
Description of the proposed water distribution network,			
including locations of proposed connections to the			
existing system, provisions for necessary looping, and			
appurtenances (valves, pressure reducing valves, valve	Y	4.0	
chambers, and fire hydrants) including special metering			
provisions.			
Description of off-site required feedermains, booster			
pumping stations, and other water infrastructure that			
will be ultimately required to service proposed	N/A		
development, including financing, interim facilities, and	-		
timing of implementation.			
Confirmation that water demands are calculated based			
on the City of Ottawa Design Guidelines.	Y	4.0	
Provision of a model schematic showing the boundary			
conditions locations, streets, parcels, and building	Ν		
locations for reference.			

4.3 Wastewater	Addressed (Y/N/NA)	Section	Comments
Summary of proposed design criteria (Note: Wet-			
weather flow criteria should not deviate from the City of			
Ottawa Sewer Design Guidelines. Monitored flow data	Y	2.0	
from relatively new infrastructure cannot be used to			
justify capacity requirements for proposed			
Confirm consistency with Master Servicing Study and/or justifications for deviations.	N/A		
Consideration of local conditions that may contribute to			
extraneous flows that are higher than the recommended	N/A		
flows in the guidelines. This includes groundwater and	N/A		
soil conditions, and age and condition of sewers.			
Description of existing sanitary sewer available for	Y	2.0	
discharge of wastewater from proposed development.	ř	2.0	
Verify available capacity in downstream sanitary sewer			
and/or identification of upgrades necessary to service the			
proposed development. (Reference can be made to	Y	2.0	
previously completed Master Servicing Study if			
applicable)			
Calculations related to dry-weather and wet-weather			
flow rates from the development in standard MOE	N/A		
sanitary sewer design table (Appendix 'C') format.			
Description of proposed sewer network including sewers,	Y	2.0	Durg 116070 CD
pumping stations, and forcemains.	T	2.0	Dwg. 116070-GP
Discussion of previously identified environmental			
constraints and impact on servicing (environmental			
constraints are related to limitations imposed on the	NI / A		
development in order to preserve the physical condition	N/A		
of watercourses, vegetation, soil cover, as well as			
protecting against water quantity and quality).			
Pumping stations: impacts of proposed development on			
existing pumping stations or requirements for new	N/A		
pumping station to service development.			
Forcemain capacity in terms of operational redundancy,	NI / A		
surge pressure and maximum flow velocity.	N/A		
Identification and implementation of the emergency			
overflow from sanitary pumping stations in relation to	NI / A		
the hydraulic grade line to protect against basement	N/A		
flooding.			
Special considerations such as contamination, corrosive	NI / A		
environment etc.	N/A		

4.4 Stormwater	Addressed (Y/N/NA)	Section	Comments
Description of drainage outlets and downstream			
constraints including legality of outlet (i.e. municipal	Y	3.0	
drain, right-of-way, watercourse, or private property).			
Analysis of the available capacity in existing public	Y	3.0	
infrastructure.		5.0	
A drawing showing the subject lands, its surroundings,			
the receiving watercourse, existing drainage patterns and	Y		116070-STM
proposed drainage patterns.			
Water quantity control objective (e.g. controlling post-			
development peak flows to pre-development level for			
storm events ranging from the 2 or 5 year event			
(dependent on the receiving sewer design) to 100 year	Y	3.0	
return period); if other objectives are being applied, a	, T	5.0	
rationale must be included with reference to hydrologic			
analyses of the potentially affected subwatersheds,			
taking into account long-term cumulative effects.			
Water Quality control objective (basic, normal or			
enhanced level of protection based on the sensitivities of	Y	3.0	
the receiving watercourse) and storage requirements.			
Description of stormwater management concept with			
facility locations and descriptions with references and	Y	3.0	
supporting information.			
Set-back from private sewage disposal systems.	N/A		
Watercourse and hazard lands setbacks.	N/A		
Record of pre-consultation with the Ontario Ministry of			
Environment and the Conservation Authority that has	N/A		
jurisdiction on the affected watershed.			
Confirm consistency with sub-watershed and Master	N/A		
Servicing Study, if applicable study exists.	N/A		
Storage requirements (complete with calcs) and			
conveyance capacity for minor (5 yr) and major (100 yr)	Y	3.0	
events.			
Identification of watercourse within the proposed			
development and how watercourses will be protected,	N/A		
or, if necessary, altered by the proposed development	,.		
with applicable approvals.			
Calculate pre and post development peak flow rates			
including a description of existing site conditions and	Y	3.0	
proposed impervious areas and drainage catchments in		0.0	
comparison to existing conditions.			
Any proposed diversion of drainage catchment areas	N/A		
from one outlet to another.	,		

Project Name: Adelaide Tower Expansion Project Number: 116070 Date: January 2019

4.4 Stormwater	Addressed (Y/N/NA)	Section	Comments
Proposed minor and major systems including locations and sizes of stormwater trunk sewers, and SWM	Y	3.0	Dwgs. 116070-GP, -GR and - STM
If quantity control is not proposed, demonstration that downstream system has adequate capacity for the post- development flows up to and including the 100-year return period storm event.	Y	3.0	
Identification of potential impacts to receiving watercourses.	N/A		
Identification of municipal drains and related approval requirements.	N/A		
Description of how the conveyance and storage capacity will be achieved for the development.	Y	3.0	
100 year flood levels and major flow routing to protect proposed development from flooding for establishing minimum building elevations (MBE) and overall grading.	Y	3.0	100 Year HGL not available
Inclusion of hydraulic analysis including HGL elevations.	Ν		
Description of approach to erosion and sediment control during construction for the protection of receiving watercourse or drainage corridors.	Y	5.0	
Identification of floodplains – proponent to obtain relevant floodplain information from the appropriate Conservation Authority. The proponent may be required to delineate floodplain elevations to the satisfaction of the Conservation Authority if such information is not available or if information does not match current conditions.	N/A		
Identification of fill constrains related to floodplain and geotechnical investigation.	N/A		

4.5 Approval and Permit Requirements	Addressed (Y/N/NA)	Section	Comments
Conservation Authority as the designated approval agency for modification of floodplain, potential impact on fish habitat, proposed works in or adjacent to a watercourse, cut/fill permits and Approval under Lakes and Rivers Improvement Act. The Conservation Authority is not the approval authority for the Lakes and Rivers Improvement Act. Where there are Conservation Authority regulations in place, approval under the Lakes and Rivers Improvement Act is not required, except in cases of dams as defined in the Act.			
Application for Certificate of Approval (CofA) under the Ontario Water Resources Act.	Ν		
Changes to Municipal Drains.	Ν		
Other permits (National Capital Commission, Parks			
Canada, Public Works and Government Services Canada, Ministry of Transportation etc.)	N/A		

4.6 Conclusion	Addressed (Y/N/NA)	Section	Comments
Clearly stated conclusions and recommendations.	Y	6.0	
Comments received from review agencies including the City of Ottawa and information on how the comments were addressed. Final sign-off from the responsible reviewing agency.	N/A		
All draft and final reports shall be signed and stamped by a professional Engineer registered in Ontario.	Y		

# **APPENDIX B**

# Sanitary Design Sheet

SANITARY SEWER DESIGN SHEET



	LOCATION				RESIDENTI	AL FLOW			EXTRA	NEOUS FLOW		TOTAL FLOW	/S
									Infiltrat	ion Allowance	Average Dry	Peak Dry	Peak Wet
Area ID	Use	Total		of Units	Design	Avg	Peak	Res. Peak	Dry Weather	Wet Weather	Weather	Weather	Weather
/ lica ib	030	Area	1-bdrm	2-bdrm	Population	Flow	Factor	Flow	(l/l dry)	(I/I wet)			Flow (PWWW)
		(ha)	-	-	(persons)	(l/s)	-	(l/s)	(l/s)	(l/s)	(l/s)	(l/s)	(l/s)
THEORETICAL POST-	DEVELOPMENT							-					
Existing Building	Residential	N/A	79	79	277	0.90	3.33	2.99			0.90	2.99	2.99
New 1-storey addition	Residential	N/A	22	2	35	0.11	3.33	0.38			0.11	0.38	0.38
Subtotal			101	81	312	1.01	3.33	3.37			1.01	3.37	3.37
New Tower	Residential	N/A	216	12	328	1.06	3.33	3.54			1.06	3.54	3.54
Total			317	93	640	2.07	3.33	6.91			2.07	6.91	6.91
Residential Population 1-bedroom Apartment 2-bedroom Apartment Average Sanitary Flow Residential	vs	1.40 2.10 280	people / unit people / unit L/c/d										
Peak Extraneous Flow										LGB GJM			
Peaking Factors Residential		Harmon I	Equation, K=0.8	5					Date:	January 16, 2019			

# APPENDIX C

# Stormwater Design Sheets and Roof Drain and ICD Information

2-R

2-A

Surface runoff



			Allowable	Site Flows						Target Allo	wable Flows
	Description	A (ba)	A imp (ha)	A grav (ha)	A perv (ha)	C <sub>5</sub>		Uncontrolle	ed Flows (L/s)	I Flows (L/s) (L	
	Description	A (ha)	C=0.9	C=0.6	C=0.2	05	C <sub>100</sub>	5 year	100 year	5-Yr (L/s)	100-Yr (L/s)
	1 - BUILDINGS A AND C	1.304						N/A	N/A	101.5	174.0
2 - BUILD	INGS B AND D (ADELAIDE), TOWER EXPANSION	0.802						N/A	N/A	62.4	107.0
		2.11							TOTAL	163.9	281.0
										t <sub>e</sub> =20mins	t <sub>c</sub> =20mins
											0
										i=70mm/hr	i=120mm/hr
		Post - I	Development : U	Incontrolled Site	Flows					i=70mm/hr	i=120mm/hr
Aroa	Description		Development: U A imp (ha)	Incontrolled Site	Flows A perv (ha)	C	C	Uncontroll	ed Flow (L/s)	i=70mm/hr	i=120mm/hr
Area	Description	Post - I A (ha)		1		C <sub>5</sub>	C <sub>100</sub>	Uncontroll 5 year	ed Flow (L/s) 100 year	i=70mm/hr	i=120mm/hr
Area 1-R	Description Controlled roof drains - Buildings C and A		A imp (ha)	A grav (ha)	A perv (ha)	<b>C</b> 5 0.90	<b>C</b> <sub>100</sub> 0.90			i=70mm/hr	i=120mm/hr
	·	A (ha)	A imp (ha) C=0.9	A grav (ha)	A perv (ha) C=0.2			5 year	100 year	i=70mm/hr	i=120mm/hr
1-R	Controlled roof drains - Buildings C and A	<b>A (ha)</b> 0.240 1.064	A imp (ha) C=0.9 0.240	A grav (ha)	A perv (ha) C=0.2	0.90	0.90	<b>5 year</b> 42.0	100 year 72.1	i=70mm/hr	i=120mm/hr
1-R	Controlled roof drains - Buildings C and A Surface runoff	<b>A (ha)</b> 0.240 1.064	A imp (ha) C=0.9 0.240 0.692	A grav (ha) C=0.6 0	A perv (ha) C=0.2 0 0.3724	0.90 0.66	0.90	<b>5 year</b> 42.0 135.6	100 year 72.1 232.5	i=70mm/hr	i=120mm/hr
1-R 1-A	Controlled roof drains - Buildings C and A Surface runoff Sub-Total	A (ha) 0.240 1.064 1.304	A imp (ha) C=0.9 0.240 0.692 0.932	A grav (ha) C=0.6 0	A perv (ha) C=0.2 0 0.3724 0.37	0.90 0.66 0.70	0.90 0.66 0.70	<b>5 year</b> 42.0 135.6 <b>177.7</b>	100 year 72.1 232.5 304.6	i=70mm/hr	i=120mm/hr

0

0

0.00

0.90

0.83

1.54

0

0.0225

0.02

0.90

0.83

1.54

0.211 0.802 2.11

0.591

0.591

0.189

1.371

Sub-total: (Area 2 roof areas)

Sub-Total

t<sub>c</sub>=20mins t<sub>c</sub>=20mins *i*=70mm/hr *i*=120mm/hr

177.4

58.1

235.5

103.5

33.9

137.4

Post - Development : Total Flows for Controlled Site								
A	Description	Flo	w (L/s)	Storage Rec	uired (m <sup>3</sup> )	Provided		
Area	Description	5 year	100 year	5 year	100 year	(m <sup>3</sup> )		
1-R	Controlled roof drains - Buildings C and A	14.0	14.0	33.9	74.7	Assume >75		
1-A	Surface runoff	87.5	160.0	68.6	111.6	111.6		
	Sub-Total (Area 1)	101.5	174.0	102.5	186.3	186.6		
2-D	Controlled roof drains - Building D	8.0	8.0	Refer to 'Tower	C and Block D'	SWM Report		
2-B1	Controlled roof drains - Adelaide Building (B1)	7.9	8.7	31.7	64.6	74.8		
2-B2	Controlled roof drains - New Tower (B2)	9.8	11.1	2.5	7.4	8.9		
2-R	Sub-Total (Area 2 roof areas)	25.7	27.8	34.3	71.9	83.7		
2-A	Surface runoff	33.9	58.1	-	-	-		
	Sub-Total (Area 2)	59.6	85.9	34.3	71.9	83.7		
	TOTAL (SITE - AREA 1 + AREA 2)	161.1	259.9	1				

ADELAIDE TOWER EXPANSION					
PROJECT NO: 116070					
REQUIRED ST					
AREA 1-A Cont	rolled Flov	w-Surface A	rea		
OTTAWA IDF C	URVE				_
Area =	1.064	ha	Qallow =	87.5	L/s
C =	0.66		Vol(max) =	68.6	m3
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	141.18	273.52	186.02	55.81	
10	104.19	201.87	114.37	68.62	
15	83.56	161.89	74.39	66.95	
20	70.25	136.11	48.61	58.33	
25	60.90	117.98	30.48	45.72	
30	53.93	104.48	16.98	30.57	
35	48.52	94.00	6.50	13.65	
40	44.18	85.60	-1.90	-4.55	
45	40.63	78.72	-8.78	-23.72	
50	37.65	72.95	-14.55	-43.65	
55	35.12	68.05	-19.45	-64.19	
60	32.94	63.83	-23.67	-85.23	
65	31.04	60.15	-27.35	-106.68	
70	29.37	56.91	-30.59	-128.49	
75	27.89	54.03	-33.47	-150.61	
90	24.29	47.06	-40.44	-218.39	
105	21.58	41.81	-45.69	-287.82	
120	19.47	37.72	-49.78	-358.44	
135	17.76	34.42	-53.08	-429.96	
150	16.36	31.70	-55.80	-502.20	

Structures	Size (mm)	Area (m²)	T/G	Inv IN	Inv OUT
STM MH2	1200	1.13	60.50	58.65	58.65
STM MH1	1300	1.33	60.50	58.46	58.46
MH1	2440	4.68	60.65	58.55	58.50
CB 1	600 x 600	0.36	60.50	58.98	58.98
CB 3	600 x 600	0.36	60.50	59.37	59.37

PI =	3.14159265	
pipe I.D.=	1220	(1200 nominal)
U	G Pipe Volu	
End Area	1.169	(m <sup>2</sup> )
Total Length	99.8	(m)
Pipe Volume	116.7	(m <sup>3</sup> )

U/G Pipe Size	1200MM
Pipe Segment	
Centre-Centre Length	
Inside Structure	1.2
U/G Storage Length	99.8

							Area A	A-1: Storage	Table	
				Un	derground Stor	age			Surface Storage	Total Storage
Elevation (m)	System Head (m)	STM MH2 Volume (m°)	STM MH1 Volume (m°)	MH1 Volume (m°)	CB 1 Volume (m°)	CB 3 Volume (m°)	1200mm dia. Pipe Storage (m <sup>°</sup> )	Total U/G Volume (m°)		Volume (m°)
58.46 58.50 58.65 58.98 59.00 59.37 59.50 59.75 60.00 60.25 60.50	-0.15 0.00 0.33 0.35 0.72 0.85 1.10 1.35 1.60 1.85	0.37 0.40 0.81 0.96 1.24 1.53 1.81 2.09	0.00 0.25 0.69 0.72 1.21 1.38 1.71 2.04 2.38 2.71	0.70 2.24 2.34 4.07 4.68 5.84 7.01 8.18 9.35	0.00 0.01 0.14 0.19 0.28 0.37 0.46 0.55	0.00 0.05 0.14 0.23 0.32 0.41	0.00 26.95 45.91 51.90 59.88 116.66 116.66 116.66 116.66	0.00 27.52 49.08 55.22 66.11 123.92 125.88 127.84 129.81 131.77		0.0 0.0 27.5 48.1 55.2 66.1 123.9 125.9 127.8 129.8 131.8

ELAIDE TOV		NSION			
OJECT NO:					
QUIRED STO	RAGE - 1	:100 YEAR	EVENT		
EA 1-A Cont	rolled Flov	v-Surface A	rea		
TAWA IDF C	URVE				
Area =	1.064	ha	Qallow =	160.0	L/s
C =	0.66		Vol(max) =	111.6	m3
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	242.70	470.22	310.23	93.07	
10	178.56	345.95	185.96	111.57	
15	142.89	276.85	116.86	105.17	
20	119.95	232.40	72.41	86.89	
25	103.85	201.20	41.21	61.81	
30	91.87	177.99	18.00	32.40	
35	82.58	159.99	0.00	0.00	
40	75.15	145.59	-14.40	-34.56	
45	69.05	133.78	-26.21	-70.76	
50	63.95	123.91	-36.08	-108.25	
55	59.62	115.52	-44.47	-146.76	
60	55.89	108.29	-51.70	-186.11	
65	52.65	102.00	-57.99	-226.16	
70	49.79	96.46	-63.53	-266.81	
75	47.26	91.55	-68.44	-307.96	
90	41.11	79.65	-80.34	-433.84	
105	36.50	70.71	-89.28	-562.45	
120	32.89	63.73	-96.26	-693.06	
135 150	30.00 27.61	58.12 53.49	-101.87	-825.17	
			-106.50	-958.46	

Inlet Control Device - Circular Plug						
1:100 Yr						
Flow (L/s) =	160.0					
Head (m) =	1.85					
Elevation (m) =	60.35					
Outlet Pipe Dia.(mm) =	300					
Volume (m3) =	111.6					
1:5 Yr						
Flow (L/s) =	87.5					
Head (m) =	0.55					
Elevation (m) =	59.05					
Outlet Pipe Dia.(mm) =	300					
Volume (m3) =	68.6					
Maximum Ponding Depth	(cm)					
1:100 Yr	0					
1:5 Yr	0					

Orifice S	Size - 1:100 yr Flo	w Check
Q=0.62xAx(2g		
	1:100 yr	Flow Check
Q (m <sup>3</sup> /s) =	0.1600	0.1606
g (m/s <sup>2</sup> ) =	9.81	9.81
h (m) =	1.85	1.85
A (m <sup>2</sup> ) =	0.042831746	0.04301
D (m) =	0.233527457	0.23400
D (mm) =	234	234.0

1:5 yr Flow Check	(
	1:5 yr
Q (m <sup>3</sup> /s) =	0.0876
g (m/s <sup>2</sup> ) =	9.81
h (m) =	0.55
A (m <sup>2</sup> ) =	0.04301
D (m) =	0.234
D (mm) =	234

ADELAIDE	TOWER	EXPANS	SION			
116070						
REQUIRED	STORAGE	E - 1:5 YE	AR EVENT			
AREA 1-R	AREA 1-R Controlled Roof Drains					
OTTAWA ID	F CURVE					
Area =	0.240	ha	Qallow =	14.00	L/s	
C =	0.90		Vol(max) =	33.9	m3	
Time	Intensity	Q	Qnet	Vol		
(min)	(mm/hr)	(L/s)	(L/s)	(m3)		
5	141.18	84.77	70.77	21.23		
10	104.19	62.57	48.57	29.14		
15	83.56	50.17	36.17	32.56		
20	70.25	42.18	28.18	33.82		
25	60.90	36.57	22.57	33.85		
30	53.93	32.38	18.38	33.09		
35	48.52	29.13	15.13	31.78		
40	44.18	26.53	12.53	30.08		
45	40.63	24.40	10.40	28.07		
50	37.65	22.61	8.61	25.83		
55	35.12	21.09	7.09	23.40		
60	32.94	19.78	5.78	20.81		
65	31.04	18.64	4.64	18.10		
70	29.37	17.64	3.64	15.28		
75	27.89	16.75	2.75	12.36		
90	24.29	14.58	0.58	3.16		
105	21.58	12.96	-1.04	-6.55		
120	19.47	11.69	-2.31	-16.63		

ADELAIDE 116070	TOWER	EXPANS	SION		
	0700405		YEAR EVENT	-	
AREA 1-R	STURAGE		led Roof Dra		
		Control	ieu Rooi Dra	ins	
OTTAWA IE			0 1	44.00	
Area =	0.240	ha	Qallow =	14.00	L/s
C =	0.90		Vol(max) =	74.7	m3
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	242.70	145.74	131.74	39.52	
10	178.56	107.22	93.22	55.93	
15	142.89	85.81	71.81	64.62	
20	119.95	72.03	58.03	69.63	
25	103.85	62.36	48.36	72.54	
30	91.87	55.17	41.17	74.10	
35	82.58	49.59	35.59	74.73	
40	75.15	45.12	31.12	74.70	
45	69.05	41.46	27.46	74.15	
50	63.95	38.40	24.40	73.21	
55	59.62	35.80	21.80	71.95	
60	55.89	33.56	19.56	70.43	
65	52.65	31.61	17.61	68.69	
70	49.79	29.90	15.90	66.77	
75	47.26	28.38	14.38	64.69	
90	41.11	24.69	10.69	57.71	
105	36.50	21.92	7.92	49.87	
120	32.89	19.75	5.75	41.42	
			-		

Watts Accutrol Flow Control Roof Drains:			RD-100-A-ADJ	set to 1/4 Exposed	
Design – Flow/Drain (L/s) Total F		Total Flow (L/s)	Ponding	onding Storage (m <sup>3</sup> )	
Event	Event Flow/Drain (L/S)	Total Flow (L/S)	(cm)	Required	Provided
1:5 Year	1.00	14.00	10	33.9	39.0
1:100 Year	1.00	14.00	15	74.7	126.0

Roof Drain Storage Table for AVERAGE RD					
Area RD 1	Total Volume				
m²	m³				
0	0				
17	0.4				
77	2.8				
171	9.0				
	Area RD 1 m <sup>2</sup> 0 17 77				

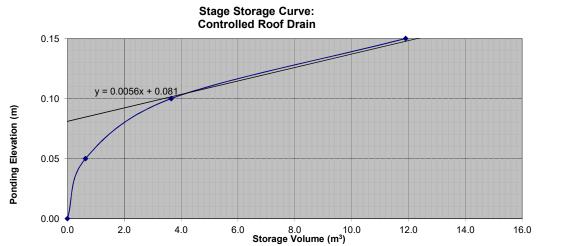
APPROXIMATE ONLY

ADELAIDE	TOWER	EXPANS	SION		
116070					
REQUIRED	STORAGE	E - 1:5 YE	AR EVENT		
AREA 2-R		Co	ntrolled Roof I	Drain	#1
OTTAWA ID	F CURVE				
Area =	0.023	ha	Qallow =	0.80	L/s
C =	0.90		Vol(max) =	4.3	m3
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	141.18	8.29	7.49	2.25	
10	104.19	6.12	5.32	3.19	
15	83.56	4.91	4.11	3.70	
20	70.25	4.13	3.33	3.99	
25	60.90	3.58	2.78	4.16	
30	53.93	3.17	2.37	4.26	
35	48.52	2.85	2.05	4.30	
40	44.18	2.59	1.79	4.31	
45	40.63	2.39	1.59	4.28	
50	37.65	2.21	1.41	4.23	
55	35.12	2.06	1.26	4.17	
60	32.94	1.93	1.13	4.08	
65	31.04	1.82	1.02	3.99	
70	29.37	1.72	0.92	3.88	
75	27.89	1.64	0.84	3.77	
90	24.29	1.43	0.63	3.38	
105	21.58	1.27	0.47	2.94	
120	19.47	1.14	0.34	2.47	

ADELAIDE	TOWER	<b>FXPAN</b>	SION		
116070		-/// / / / / /			
REQUIRED	STORAGE	- 1:100	YEAR EVENT	-	
AREA 2-R			ntrolled Roof		#1
OTTAWA IE	OF CURVE				
Area =	0.023	ha	Qallow =	0.87	L/s
C =	0.90		Vol(max) =	8.7	m3
			( )		
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	242.70	14.25	13.38	4.01	
10	178.56	10.49	9.62	5.77	
15	142.89	8.39	7.52	6.77	
20	119.95	7.04	6.17	7.41	
25	103.85	6.10	5.23	7.84	
30	91.87	5.39	4.52	8.14	
35	82.58	4.85	3.98	8.36	
40	75.15	4.41	3.54	8.50	
45	69.05	4.05	3.18	8.60	
50	63.95	3.76	2.89	8.66	
55	59.62	3.50	2.63	8.68	
60	55.89	3.28	2.41	8.68	
65	52.65	3.09	2.22	8.66	
70	49.79	2.92	2.05	8.63	
75	47.26	2.77	1.90	8.57	
90	41.11	2.41	1.54	8.34	
105	36.50	2.14	1.27	8.02	
120	32.89	1.93	1.06	7.64	

Vatts Accutrol Flow	Control Roof Drain	ıs:	RD-100-A-ADJ	set to 1/4 Exposed	
Design Event	esign Event Flow (L/s)		Ponding	Storage	e (m <sup>3</sup> )
Design Event	FIOW (L/S)	Total Flow (L/s)	(cm)	Required	Provided
1:5 Year	0.80	0.80	10.6	4.3	4.5
1:100 Year	0.87	0.87	13.0	8.7	8.8

<b>Roof Drain Sto</b>	rage Table for RD	#1
Elevation	Area	Total Volume
m	m <sup>2</sup>	m <sup>3</sup>
0.00	0	0
0.05	25.5	0.6
0.10	95.1	3.7
0.15	234.7	11.9

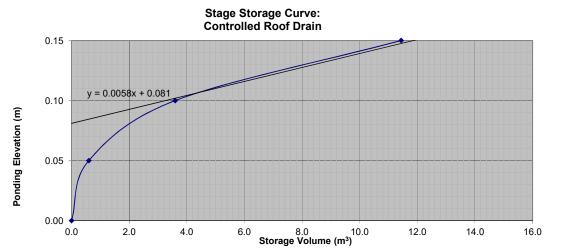


ADELAIDE	TOWER	EXPANS	SION		
116070					
REQUIRED	STORAGE	E - 1:5 YE	AR EVENT		
AREA 2-R		Co	ntrolled Roof I	Drain #	2
OTTAWA ID	F CURVE				
Area =	0.022	ha	Qallow =	0.80	L/s
C =	0.90		Vol(max) =	3.9	m3
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	141.18	7.69	6.89	2.07	
10	104.19	5.68	4.88	2.93	
15	83.56	4.55	3.75	3.38	
20	70.25	3.83	3.03	3.63	
25	60.90	3.32	2.52	3.78	
30	53.93	2.94	2.14	3.85	
35	48.52	2.64	1.84	3.87	
40	44.18	2.41	1.61	3.86	
45	40.63	2.21	1.41	3.82	
50	37.65	2.05	1.25	3.75	
55	35.12	1.91	1.11	3.67	
60	32.94	1.79	0.99	3.58	
65	31.04	1.69	0.89	3.47	
70	29.37	1.60	0.80	3.36	
75	27.89	1.52	0.72	3.24	
90	24.29	1.32	0.52	2.82	
105	21.58	1.18	0.38	2.37	
120	19.47	1.06	0.26	1.87	

	TOWER	EXPAN	SION		
116070					
	STORAGE		YEAR EVENT		2
AREA 2-R Controlled Roof Drain #					
OTTAWA IE					
Area =	0.022	ha	Qallow =	0.87	L/s
C =	0.90		Vol(max) =	7.8	m3
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	242.70	13.22	12.35	3.70	
10	178.56	9.73	8.86	5.31	
15	142.89	7.78	6.91	6.22	
20	119.95	6.53	5.66	6.80	
25	103.85	5.66	4.79	7.18	
30	91.87	5.00	4.13	7.44	
35	82.58	4.50	3.63	7.62	
40	75.15	4.09	3.22	7.74	
45	69.05	3.76	2.89	7.81	
50	63.95	3.48	2.61	7.84	
55	59.62	3.25	2.38	7.85	
60	55.89	3.04	2.17	7.83	
65	52.65	2.87	2.00	7.79	
70	49.79	2.71	1.84	7.74	
75	47.26	2.57	1.70	7.67	
90	41.11	2.24	1.37	7.39	
105	36.50	1.99	1.12	7.04	
120	32.89	1.79	0.92	6.64	

Watts Accutrol Flow Control Roof Drains:			RD-100-A-ADJ	set to 1/4 Exposed	
Design Event	Flow (L/s)	Total Flow (L/s) Ponding Storage (		e (m <sup>3</sup> )	
Design Event	FIOW (L/S)	Total Flow (L/S)	(cm)	Required	Provided
1:5 Year	0.80	0.80	10.6	3.9	4.3
1:100 Year	0.87	0.87	13.0	7.8	8.4

<b>Roof Drain Stor</b>	age Table for RD #	2
Elevation	Area	Total Volume
m	m <sup>2</sup>	m <sup>3</sup>
0.00	0	0
0.05	24	0.6
0.10	95.9	3.6
0.15	217.7	11.4

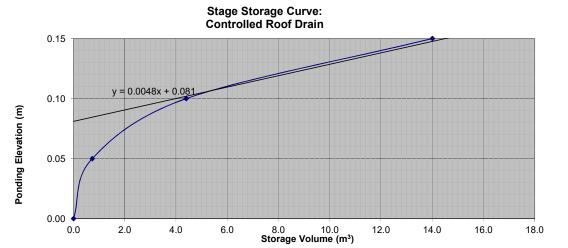


ADELAIDE	TOWER	EXPANS	SION		
116070					
REQUIRED	STORAGE				
AREA 2-R		Co	ntrolled Roof I	Drain #	3
OTTAWA ID	F CURVE				
Area =	0.027	ha	Qallow =	0.80	L/s
C =	0.90		Vol(max) =	5.2	m3
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	141.18	9.43	8.63	2.59	
10	104.19	6.96	6.16	3.70	
15	83.56	5.58	4.78	4.30	
20	70.25	4.69	3.89	4.67	
25	60.90	4.07	3.27	4.90	
30	53.93	3.60	2.80	5.04	
35	48.52	3.24	2.44	5.13	
40	44.18	2.95	2.15	5.16	
45	40.63	2.71	1.91	5.17	
50	37.65	2.52	1.72	5.15	
55	35.12	2.35	1.55	5.10	
60	32.94	2.20	1.40	5.04	
65	31.04	2.07	1.27	4.97	
70	29.37	1.96	1.16	4.88	
75	27.89	1.86	1.06	4.78	
90	24.29	1.62	0.82	4.44	
105	21.58	1.44	0.64	4.04	
120	19.47	1.30	0.50	3.60	

ADELAIDE	TOWER	EXPAN	SION		
116070					
REQUIRED	STORAGE	E - 1:100	YEAR EVENT	-	
AREA 2-R			ntrolled Roof		3
OTTAWA II	OF CURVE				
Area =	0.027	ha	Qallow =	0.88	L/s
C =	0.90		Vol(max) =	10.3	m3
-					
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	242.70	16.21	15.33	4.60	
10	178.56	11.93	11.05	6.63	
15	142.89	9.55	8.67	7.80	
20	119.95	8.01	7.13	8.56	
25	103.85	6.94	6.06	9.09	
30	91.87	6.14	5.26	9.46	
35	82.58	5.52	4.64	9.74	
40	75.15	5.02	4.14	9.94	
45	69.05	4.61	3.73	10.08	
50	63.95	4.27	3.39	10.18	
55	59.62	3.98	3.10	10.24	
60	55.89	3.73	2.85	10.27	
65	52.65	3.52	2.64	10.28	
70	49.79	3.33	2.45	10.27	
75	47.26	3.16	2.28	10.25	
90	41.11	2.75	1.87	10.08	
105	36.50	2.44	1.56	9.82	
120	32.89	2.20	1.32	9.49	

Natts Accutrol Flow	Control Roof Drains:		RD-100-A-ADJ	set to 1/4 Exposed	
Design Event	esign Event Flow (L/s)		Ponding	Storage	e (m <sup>3</sup> )
Design Event		Total Flow (L/s)	(cm)	Provided	
1:5 Year	0.80	0.80	10.6	5.2	5.2
1:100 Year	0.88	0.88	13.1	10.3	10.4

<b>Roof Drain Stor</b>	rage Table for RD #	3
Elevation	Area	Total Volume
m	m <sup>2</sup>	m <sup>3</sup>
0.00	0	0
0.05	29.3	0.7
0.10	117.4	4.4
0.15	267	14.0

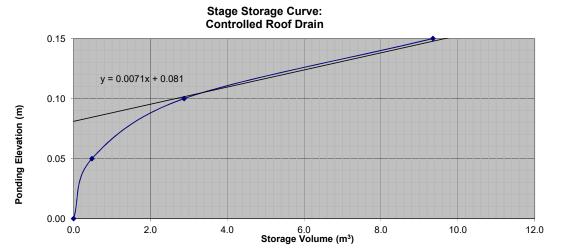


ADELAIDE	TOWER	EXPANS	SION		
116070					
REQUIRED	STORAGE	E - 1:5 YE	AR EVENT		
AREA 2-R		Co	ntrolled Roof I	Drain #	4
OTTAWA ID	F CURVE				
Area =	0.018	ha	Qallow =	0.79	L/s
C =	0.90		Vol(max) =	3.0	m3
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	141.18	6.44	5.65	1.70	
10	104.19	4.76	3.97	2.38	
15	83.56	3.81	3.02	2.72	
20	70.25	3.21	2.42	2.90	
25	60.90	2.78	1.99	2.98	
30	53.93	2.46	1.67	3.01	
35	48.52	2.21	1.42	2.99	
40	44.18	2.02	1.23	2.94	
45	40.63	1.85	1.06	2.87	
50	37.65	1.72	0.93	2.79	
55	35.12	1.60	0.81	2.68	
60	32.94	1.50	0.71	2.57	
65	31.04	1.42	0.63	2.44	
70	29.37	1.34	0.55	2.31	
75	27.89	1.27	0.48	2.17	
90	24.29	1.11	0.32	1.72	
105	21.58	0.98	0.19	1.23	
120	19.47	0.89	0.10	0.71	

ADELAIDE	<b>TOWER</b>	EXPAN	SION		
116070					
REQUIRED	STORAGE	E - 1:100	YEAR EVENT		
AREA 2-R		Co	ntrolled Roof	Drain #	4
OTTAWA II	OF CURVE				
Area =	0.018	ha	Qallow =	0.87	L/s
C =	0.90		Vol(max) =	6.2	m3
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	242.70	11.08	10.21	3.06	
10	178.56	8.15	7.28	4.37	
15	142.89	6.52	5.65	5.09	
20	119.95	5.47	4.60	5.52	
25	103.85	4.74	3.87	5.80	
30	91.87	4.19	3.32	5.98	
35	82.58	3.77	2.90	6.09	
40	75.15	3.43	2.56	6.14	
45	69.05	3.15	2.28	6.16	
50	63.95	2.92	2.05	6.15	
55	59.62	2.72	1.85	6.11	
60	55.89	2.55	1.68	6.05	
65	52.65	2.40	1.53	5.98	
70	49.79	2.27	1.40	5.89	
75	47.26	2.16	1.29	5.79	
90	41.11	1.88	1.01	5.43	
105	36.50	1.67	0.80	5.01	
120	32.89	1.50	0.63	4.54	

Watts Accutrol Flow		RD-100-A-ADJ	set to 1/4 Exposed		
Design Event Flow (L/s)		Total Flow (L/s)	Ponding	Storage (	m <sup>3</sup> )
Design Event	FIOW (L/S)	TOTAL FIOW (L/S)	(cm)	Required	Provided
1:5 Year	0.79	0.79	10.2	3.0	3.0
1:100 Year	0.87	0.87	13.8	6.2	8.0

<b>Roof Drain Sto</b>	rage Table for RD #	4
Elevation	Area	Total Volume
m	m <sup>2</sup>	m <sup>3</sup>
0.00	0	0
0.05	19.2	0.5
0.10	76.7	2.9
0.15	182.4	9.4

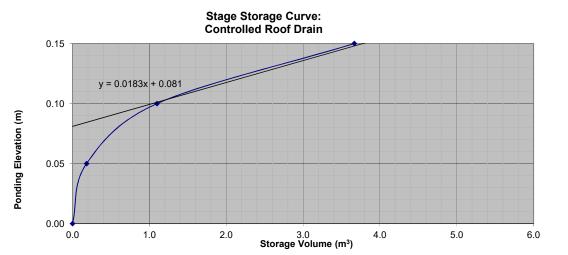


ADELAIDE	TOWER	EXPANS	SION		
116070					
REQUIRED	STORAGE				
AREA 2-R		Co	ntrolled Roof I	Drain #	5
OTTAWA ID	F CURVE				
Area =	0.007	ha	Qallow =	0.79	L/s
C =	0.90		Vol(max) =	0.7	m3
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	141.18	2.59	1.80	0.54	
10	104.19	1.91	1.12	0.67	
15	83.56	1.53	0.74	0.67	
20	70.25	1.29	0.50	0.60	
25	60.90	1.12	0.33	0.49	
30	53.93	0.99	0.20	0.36	
35	48.52	0.89	0.10	0.21	
40	44.18	0.81	0.02	0.05	
45	40.63	0.75	-0.04	-0.12	
50	37.65	0.69	-0.10	-0.30	
55	35.12	0.64	-0.15	-0.48	
60	32.94	0.60	-0.19	-0.67	
65	31.04	0.57	-0.22	-0.86	
70	29.37	0.54	-0.25	-1.06	
75	27.89	0.51	-0.28	-1.25	
90	24.29	0.45	-0.34	-1.86	
105	21.58	0.40	-0.39	-2.48	
120	19.47	0.36	-0.43	-3.12	

ADELAIDE	TOWER	EXPAN	SION		
116070					
	STORAGE		YEAR EVENT		_
AREA 2-R		Co	ntrolled Roof	Drain #	5
OTTAWA IE					
Area =	0.007	ha	Qallow =	0.87	L/s
C =	0.90		Vol(max) =	1.6	m3
		_			
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	242.70	4.45	3.58	1.07	
10	178.56	3.27	2.40	1.44	
15	142.89	2.62	1.75	1.58	
20	119.95	2.20	1.33	1.60	
25	103.85	1.90	1.03	1.55	
30	91.87	1.68	0.81	1.47	
35	82.58	1.51	0.64	1.35	
40	75.15	1.38	0.51	1.22	
45	69.05	1.27	0.40	1.07	
50	63.95	1.17	0.30	0.91	
55	59.62	1.09	0.22	0.74	
60	55.89	1.03	0.16	0.56	
65	52.65	0.97	0.10	0.37	
70	49.79	0.91	0.04	0.18	
75	47.26	0.87	0.00	-0.02	
90	41.11	0.75	-0.12	-0.63	
105	36.50	0.67	-0.20	-1.26	
120	32.89	0.60	-0.27	-1.92	

Natts Accutrol Flow	Control Roof Drains:		RD-100-A-ADJ	set to 1/4 Exposed	
Design Event	Flow (L/s)	Total Flow (L/s)	Ponding	Storage	e (m <sup>3</sup> )
Design Event		Total Flow (L/S)	(cm)	Required	Provided
1:5 Year	0.79	0.79	10.2	0.7	1.1
1:100 Year	0.87	0.87	12.7	1.6	2.5

<b>Roof Drain Stor</b>	rage Table for RD #	5
Elevation	Area	Total Volume
m	m <sup>2</sup>	m³
0.00	0	0
0.05	7.3	0.2
0.10	29.4	1.1
0.15	73.3	3.7

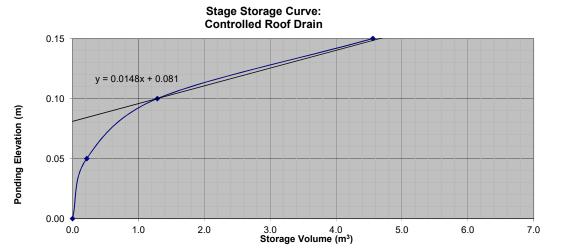


ADELAIDE TOWER EXPANSION					
116070					
REQUIRED	STORAGE	E - 1:5 YE	AR EVENT		
AREA 2-R		Co	ntrolled Roof	Drain #	6
OTTAWA ID	F CURVE				
Area =	0.010	ha	Qallow =	0.79	L/s
C =	0.90		Vol(max) =	1.1	m3
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	141.18	3.41	2.62	0.79	
10	104.19	2.52	1.73	1.04	
15	83.56	2.02	1.23	1.11	
20	70.25	1.70	0.91	1.09	
25	60.90	1.47	0.68	1.02	
30	53.93	1.30	0.51	0.92	
35	48.52	1.17	0.38	0.80	
40	44.18	1.07	0.28	0.67	
45	40.63	0.98	0.19	0.52	
50	37.65	0.91	0.12	0.36	
55	35.12	0.85	0.06	0.19	
60	32.94	0.80	0.01	0.02	
65	31.04	0.75	-0.04	-0.15	
70	29.37	0.71	-0.08	-0.34	
75	27.89	0.67	-0.12	-0.52	
90	24.29	0.59	-0.20	-1.10	
105	21.58	0.52	-0.27	-1.69	
120	19.47	0.47	-0.32	-2.30	

	E TOWER		SION		
116070		EAFAN	3101		
		- 1.100	YEAR EVENT	-	
AREA 2-R	O TONAOL		ntrolled Roof		6
OTTAWA IDF CURVE					
Area =	0.010	ha	Qallow =	0.87	L/s
C =	0.90	Па	Vol(max) =	2.5	m3
0-	0.90		voi(max) –	2.0	1113
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	242.70	5.87	5.00	1.50	
10	178.56	4.32	3.45	2.07	
15	142.89	3.45	2.58	2.33	
20	119.95	2.90	2.03	2.43	
25	103.85	2.51	1.64	2.46	
30	91.87	2.22	1.35	2.43	
35	82.58	2.00	1.13	2.36	
40	75.15	1.82	0.95	2.27	
45	69.05	1.67	0.80	2.16	
50	63.95	1.55	0.68	2.03	
55	59.62	1.44	0.57	1.88	
60	55.89	1.35	0.48	1.73	
65	52.65	1.27	0.40	1.57	
70	49.79	1.20	0.33	1.40	
75	47.26	1.14	0.27	1.22	
90	41.11	0.99	0.12	0.67	
105	36.50	0.88	0.01	0.08	
120	32.89	0.80	-0.07	-0.54	

Watts Accutrol Flow Control Roof Drains:		RD-100-A-ADJ set to 1/4 Exposed				
Design Event Flow (L/s)		Total Flow (L/s)	Ponding	Storage	Storage (m <sup>3</sup> )	
Design Event	FIOW (L/S)	Total Flow (L/S)	(cm)	Required	Provided	
1:5 Year	0.79	0.79	10.2	1.1	1.4	
1:100 Year	0.87	0.87	12.7	2.5	3.1	

<b>Roof Drain Stor</b>	rage Table for RD #	6
Elevation	Area	Total Volume
m	m <sup>2</sup>	m <sup>3</sup>
0.00	0	0
0.05	8.6	0.2
0.10	34.3	1.3
0.15	96.6	4.6

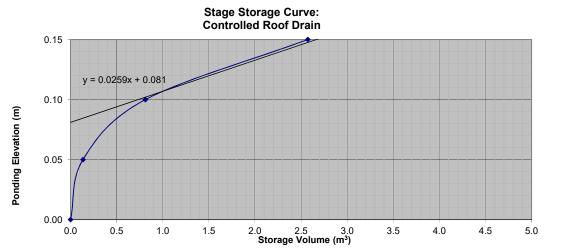


ADELAIDE TOWER EXPANSION					
116070					
REQUIRED	STORAGE				
AREA 2-R		Co	ntrolled Roof	Drain #	7
OTTAWA ID	F CURVE				
Area =	0.005	ha	Qallow =	0.71	L/s
C =	0.90		Vol(max) =	0.3	m3
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	141.18	1.72	1.01	0.30	
10	104.19	1.27	0.56	0.34	
15	83.56	1.02	0.31	0.28	
20	70.25	0.86	0.15	0.18	
25	60.90	0.74	0.03	0.05	
30	53.93	0.66	-0.05	-0.10	
35	48.52	0.59	-0.12	-0.25	
40	44.18	0.54	-0.17	-0.41	
45	40.63	0.50	-0.21	-0.58	
50	37.65	0.46	-0.25	-0.75	
55	35.12	0.43	-0.28	-0.93	
60	32.94	0.40	-0.31	-1.11	
65	31.04	0.38	-0.33	-1.29	
70	29.37	0.36	-0.35	-1.48	
75	27.89	0.34	-0.37	-1.67	
90	24.29	0.30	-0.41	-2.24	
105	21.58	0.26	-0.45	-2.82	
120	19.47	0.24	-0.47	-3.40	

ADELAIDE		EXDVN	SION		
116070		EAFAN	3101		
	STORAGE	- 1.100	YEAR EVENT	-	
AREA 2-R	OTORAGE		ntrolled Roof		7
				Bruit #	•
Area =	0.005	ha	Qallow =	0.87	L/s
C =	0.90	na	Vol(max) =	0.8	m3
0-	0.30		voi(max) –	0.0	mo
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	242.70	2.96	2.09	0.63	
10	178.56	2.18	1.31	0.78	
15	142.89	1.74	0.87	0.78	
20	119.95	1.46	0.59	0.71	
25	103.85	1.27	0.40	0.59	
30	91.87	1.12	0.25	0.45	
35	82.58	1.01	0.14	0.29	
40	75.15	0.92	0.05	0.11	
45	69.05	0.84	-0.03	-0.08	
50	63.95	0.78	-0.09	-0.27	
55	59.62	0.73	-0.14	-0.47	
60	55.89	0.68	-0.19	-0.68	
65	52.65	0.64	-0.23	-0.89	
70	49.79	0.61	-0.26	-1.11	
75	47.26	0.58	-0.29	-1.32	
90	41.11	0.50	-0.37	-1.99	
105	36.50	0.44	-0.43	-2.68	
120	32.89	0.40	-0.47	-3.38	

Watts Accutrol Flow Control Roof Drains:			RD-100-A-ADJ	set to 1/4 Exposed	
Design Event	Flow (L/s)	Total Flow (L/s)	Ponding	Ponding Storage (m <sup>3</sup> )	
Design Event		5) TOTAL FIOW (L/S)	(cm)	Required	Provided
1:5 Year	0.71	0.71	7.6	0.3	0.4
1:100 Year	0.87	0.87	12.7	0.8	1.8

Roof Drain Storage Table for RD # 7						
Elevation	Area	Total Volume				
m	m²	m <sup>3</sup>				
0.00	0	0				
0.05	5.4	0.1				
0.10	21.7	0.8				
0.15	48.7	2.6				

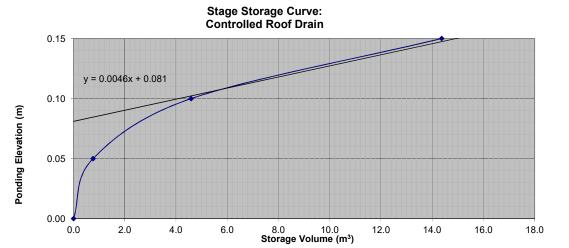


ADELAIDE TOWER EXPANSION					
116070					
REQUIRED	STORAGE				
AREA 2-R		Co	ntrolled Roof I	Drain #	8
OTTAWA ID	F CURVE				
Area =	0.027	ha	Qallow =	0.82	L/s
C =	0.90		Vol(max) =	5.2	m3
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	141.18	9.49	8.67	2.60	
10	104.19	7.01	6.19	3.71	
15	83.56	5.62	4.80	4.32	
20	70.25	4.72	3.90	4.69	
25	60.90	4.10	3.28	4.91	
30	53.93	3.63	2.81	5.05	
35	48.52	3.26	2.44	5.13	
40	44.18	2.97	2.15	5.16	
45	40.63	2.73	1.91	5.16	
50	37.65	2.53	1.71	5.14	
55	35.12	2.36	1.54	5.09	
60	32.94	2.22	1.40	5.02	
65	31.04	2.09	1.27	4.94	
70	29.37	1.98	1.16	4.85	
75	27.89	1.88	1.06	4.75	
90	24.29	1.63	0.81	4.39	
105	21.58	1.45	0.63	3.98	
120	19.47	1.31	0.49	3.52	

ADELAIDE	TOWER	EXPANS	SION		
116070				_	
	STORAGE		YEAR EVENT		
AREA 2-R		Co	ntrolled Roof	Drain #	8
OTTAWA IE					
Area =	0.027	ha	Qallow =	0.87	L/s
C =	0.90		Vol(max) =	10.4	m3
Time	Interneity (	0	Onet	Val	
	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	242.70	16.32	15.45	4.64	
10	178.56	12.01	11.14	6.68	
15	142.89	9.61	8.74	7.87	
20	119.95	8.07	7.20	8.64	
25	103.85	6.98	6.11	9.17	
30	91.87	6.18	5.31	9.56	
35	82.58	5.55	4.68	9.84	
40	75.15	5.05	4.18	10.04	
45	69.05	4.64	3.77	10.19	
50	63.95	4.30	3.43	10.29	
55	59.62	4.01	3.14	10.36	
60	55.89	3.76	2.89	10.40	
65	52.65	3.54	2.67	10.42	
70	49.79	3.35	2.48	10.41	
75	47.26	3.18	2.31	10.39	
90	41.11	2.76	1.89	10.23	
105	36.50	2.45	1.58	9.98	
120	32.89	2.21	1.34	9.66	

Watts Accutrol Flow Control Roof Drains:			RD-100-A-ADJ	set to 1/4 Exposed	
Design Event	Flow (L/s)	Total Flow (L/s)	Ponding	Storage	e (m <sup>3</sup> )
Design Event		Total Flow (L/S)	(cm)	Required	Provided
1:5 Year	0.82	0.82	11.0	5.2	6.3
1:100 Year	0.87	0.87	13.8	10.4	12.3

Roof Drain Storage Table for RD # 8						
Elevation	Area	Total Volume				
m	m <sup>2</sup>	m <sup>3</sup>				
0.00	0	0				
0.05	30.6	0.8				
0.10	122.5	4.6				
0.15	268.8	14.4				

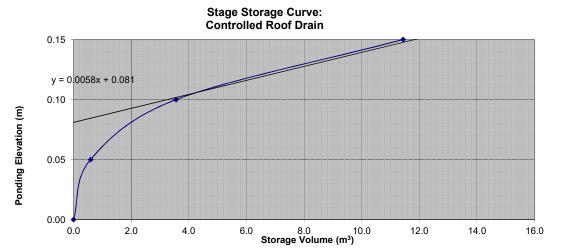


ADELAIDE TOWER EXPANSION					
116070					
REQUIRED	STORAGE				
AREA 2-R		Co	ntrolled Roof I	Drain #	9
OTTAWA ID	F CURVE				
Area =	0.022	ha	Qallow =	0.80	L/s
C =	0.90		Vol(max) =	3.9	m3
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	141.18	7.77	6.97	2.09	
10	104.19	5.74	4.94	2.96	
15	83.56	4.60	3.80	3.42	
20	70.25	3.87	3.07	3.68	
25	60.90	3.35	2.55	3.83	
30	53.93	2.97	2.17	3.91	
35	48.52	2.67	1.87	3.93	
40	44.18	2.43	1.63	3.92	
45	40.63	2.24	1.44	3.88	
50	37.65	2.07	1.27	3.82	
55	35.12	1.93	1.13	3.74	
60	32.94	1.81	1.01	3.65	
65	31.04	1.71	0.91	3.55	
70	29.37	1.62	0.82	3.43	
75	27.89	1.54	0.74	3.31	
90	24.29	1.34	0.54	2.90	
105	21.58	1.19	0.39	2.45	
120	19.47	1.07	0.27	1.96	

ADELAIDE 116070	TOWER	EXPAN	SION		
	STODACE	- 4.400	YEAR EVENT		
REQUIRED	STURAGE				9
AREA 2-R Controlled Roof Drain # 9 OTTAWA IDF CURVE					
Area =	0.022	ha	Qallow =	0.87	L/s
C =	0.022	lla	Vol(max) =	8.0	m3
C =	0.90		voi(max) –	0.0	ms
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	242.70	13.37	12.50	3.75	
10	178.56	9.83	8.96	5.38	
15	142.89	7.87	7.00	6.30	
20	119.95	6.61	5.74	6.88	
25	103.85	5.72	4.85	7.27	
30	91.87	5.06	4.19	7.54	
35	82.58	4.55	3.68	7.72	
40	75.15	4.14	3.27	7.84	
45	69.05	3.80	2.93	7.92	
50	63.95	3.52	2.65	7.96	
55	59.62	3.28	2.41	7.96	
60	55.89	3.08	2.21	7.95	
65	52.65	2.90	2.03	7.91	
70	49.79	2.74	1.87	7.86	
75	47.26	2.60	1.73	7.80	
90	41.11	2.26	1.39	7.53	
105	36.50	2.01	1.14	7.18	
120	32.89	1.81	0.94	6.78	

Watts Accutrol Flow Control Roof Drains:			RD-100-A-ADJ	set to 1/4 Exposed	
Design Event	Flow (L/s)	Total Flow (L/s) Ponding		Storage	(m <sup>3</sup> )
Design Event	Flow (L/S) Flow (L/S)	TOLAI FIOW (L/S)	(cm)	Required	Provided
1:5 Year	0.80	0.80	10.5	3.9	3.9
1:100 Year	0.87	0.87	13.8	8.0	9.7

Roof Drain Storage Table for RD # 9					
Elevation	Area	Total Volume			
m	m <sup>2</sup>	m <sup>3</sup>			
0.00	0	0			
0.05	23.7	0.6			
0.10	95	3.6			
0.15	220.1	11.4			

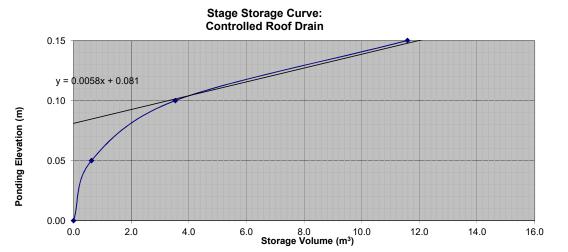


ADELAIDE	ADELAIDE TOWER EXPANSION					
116070						
REQUIRED	STORAGE					
AREA 2-R		Co	ntrolled Roof I	Drain #	10	
OTTAWA ID	F CURVE					
Area =	0.023	ha	Qallow =	0.81	L/s	
C =	0.90		Vol(max) =	4.2	m3	
Time	Intensity	Q	Qnet	Vol		
(min)	(mm/hr)	(L/s)	(L/s)	(m3)		
5	141.18	8.15	7.34	2.20		
10	104.19	6.01	5.20	3.12		
15	83.56	4.82	4.01	3.61		
20	70.25	4.05	3.24	3.89		
25	60.90	3.51	2.70	4.06		
30	53.93	3.11	2.30	4.14		
35	48.52	2.80	1.99	4.18		
40	44.18	2.55	1.74	4.18		
45	40.63	2.35	1.54	4.14		
50	37.65	2.17	1.36	4.09		
55	35.12	2.03	1.22	4.02		
60	32.94	1.90	1.09	3.93		
65	31.04	1.79	0.98	3.83		
70	29.37	1.70	0.89	3.72		
75	27.89	1.61	0.80	3.60		
90	24.29	1.40	0.59	3.20		
105	21.58	1.25	0.44	2.75		
120	19.47	1.12	0.31	2.26		

ADELAIDE					
ADELAIDE 116070	TOWER	CAPAN	51011		
	STORACE	1.100	YEAR EVENT	-	
AREA 2-R	STORAGE		ntrolled Root		10
OTTAWA IE		00	Introlled Root	Dialit #	10
Area =	0.023	ha	Qallow =	0.90	L/s
		na			_, _
C =	0.90		Vol(max) =	8.4	m3
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	242.70	14 01	( <u>∟/s)</u> 13.11	3.93	
10	178.56	10.31	9.41	5.64	
15	142.89	8.25	7.35	6.61	
20	142.69	6.92	6.02	7.23	
20	103.85	0.92 5.99	5.02	7.64	
25 30	91.87	5.30	5.09 4.40	7.92	
30	91.07 82.58	5.30 4.77	4.40 3.87	7.92 8.12	
40 45	75.15 69.05	4.34	3.44	8.25 8.33	
45 50		3.99	3.09		
	63.95	3.69	2.79	8.37	
55	59.62	3.44	2.54	8.39	
60	55.89	3.23	2.33	8.37	
65	52.65	3.04	2.14	8.34	
70	49.79	2.87	1.97	8.29	
75	47.26	2.73	1.83	8.22	
90	41.11	2.37	1.47	7.95	
105	36.50	2.11	1.21	7.60	
120	32.89	1.90	1.00	7.19	

Vatts Accutrol Flow	Control Roof Drains:		RD-100-A-ADJ	set to 1/4 Exposed	
Design Event	Flow (L/s)	Total Flow (L/s)	Ponding	Storage	e (m <sup>3</sup> )
Design Event	FIOW (L/S)	TOTAL FIOW (L/S)	(cm)	Required	Provided
1:5 Year	0.81	0.81	11.0	4.2	4.8
1:100 Year	0.90	0.90	13.8	8.4	9.8

Roof Drain Storage Table for RD # 10				
Elevation	Area	Total Volume		
m	m <sup>2</sup>	m <sup>3</sup>		
0.00	0	0		
0.05	24.9	0.6		
0.10	91.5	3.5		
0.15	230.7	11.6		

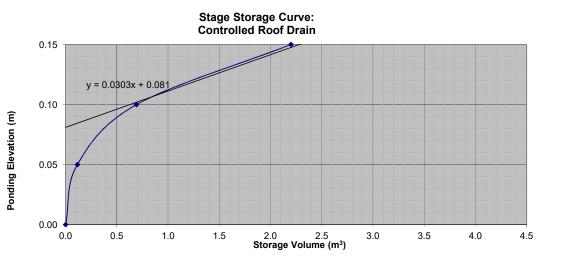


ADELAIDE	ADELAIDE TOWER EXPANSION					
116070						
REQUIRED	STORAGE	E - 1:5 YE	AR EVENT			
AREA 2-R		Co	ntrolled Roof	Drain #	11+12	
OTTAWA ID	F CURVE					
Area =	0.004	ha	Qallow =	0.71	L/s	
C =	0.90		Vol(max) =	0.2	m3	
Time	Intensity	Q	Qnet	Vol		
(min)	(mm/hr)	(L/s)	(L/s)	(m3)		
5	141.18	1.48	0.77	0.23		
10	104.19	1.09	0.38	0.23		
15	83.56	0.87	0.16	0.15		
20	70.25	0.73	0.02	0.03		
25	60.90	0.64	-0.07	-0.11		
30	53.93	0.56	-0.15	-0.26		
35	48.52	0.51	-0.20	-0.43		
40	44.18	0.46	-0.25	-0.59		
45	40.63	0.42	-0.29	-0.77		
50	37.65	0.39	-0.32	-0.95		
55	35.12	0.37	-0.34	-1.13		
60	32.94	0.34	-0.37	-1.32		
65	31.04	0.32	-0.39	-1.50		
70	29.37	0.31	-0.40	-1.69		
75	27.89	0.29	-0.42	-1.88		
90	24.29	0.25	-0.46	-2.46		
105	21.58	0.23	-0.48	-3.05		
120	19.47	0.20	-0.51	-3.65		

ADELAIDE	<b>TOWER</b>	EXPAN	SION		
116070					
REQUIRED	STORAGE	E - 1:100	YEAR EVENT	•	
AREA 2-R		Co	ntrolled Roof	Drain #	11+12
OTTAWA IE	OF CURVE				
Area =	0.004	ha	Qallow =	0.79	L/s
C =	0.90		Vol(max) =	0.6	m3
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	242.70	2.54	1.75	0.52	
10	178.56	1.87	1.08	0.65	
15	142.89	1.49	0.70	0.63	
20	119.95	1.25	0.46	0.56	
25	103.85	1.09	0.30	0.44	
30	91.87	0.96	0.17	0.31	
35	82.58	0.86	0.07	0.15	
40	75.15	0.79	0.00	-0.01	
45	69.05	0.72	-0.07	-0.18	
50	63.95	0.67	-0.12	-0.36	
55	59.62	0.62	-0.17	-0.55	
60	55.89	0.58	-0.21	-0.74	
65	52.65	0.55	-0.24	-0.93	
70	49.79	0.52	-0.27	-1.13	
75	47.26	0.49	-0.30	-1.33	
90	41.11	0.43	-0.36	-1.94	
105	36.50	0.38	-0.41	-2.57	
120	32.89	0.34	-0.45	-3.21	

Watts Accutrol Flo	w Control Roof Drains:		RD-100-A-ADJ	set to 1/4 Exposed	
Design Event	Flow per RD (L/s)	Total Flow (L/s)	Ponding	Storage	• (m <sup>3</sup> )
Design Evenit	Flow per RD (L/S)	TOTAL FIOW (L/S)	(cm)	Required	Provided
1:5 Year	0.71	1.42	7.6	0.7	0.9
1:100 Year	0.79	1.58	10.2	1.9	2.1

<b>Roof Drain Stor</b>	rage Table for RD #	11+12
Elevation	Area	Total Volume
m	m²	m <sup>3</sup>
0.00	0	0
0.05	4.6	0.1
0.10	18.5	0.7
0.15	41.8	2.2

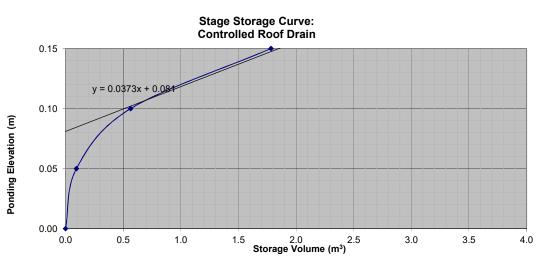


ADELAIDE	TOWER	EXPANS	SION		
116070					
REQUIRED	STORAGE				
AREA 2-R		Col	ntrolled Roof	Drain #	13,15,17
OTTAWA ID	F CURVE				
Area =	0.003	ha	Qallow =	0.71	L/s
C =	0.90		Vol(max) =	0.1	m3
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	141.18	1.19	0.48	0.14	
10	104.19	0.88	0.17	0.10	
15	83.56	0.70	-0.01	0.00	
20	70.25	0.59	-0.12	-0.14	
25	60.90	0.51	-0.20	-0.29	
30	53.93	0.45	-0.26	-0.46	
35	48.52	0.41	-0.30	-0.63	
40	44.18	0.37	-0.34	-0.81	
45	40.63	0.34	-0.37	-0.99	
50	37.65	0.32	-0.39	-1.18	
55	35.12	0.30	-0.41	-1.37	
60	32.94	0.28	-0.43	-1.56	
65	31.04	0.26	-0.45	-1.75	
70	29.37	0.25	-0.46	-1.94	
75	27.89	0.24	-0.47	-2.14	
90	24.29	0.20	-0.51	-2.73	
105	21.58	0.18	-0.53	-3.33	
120	19.47	0.16	-0.55	-3.93	

ADELAIDE TOWER EXPANSION							
116070							
	REQUIRED STORAGE - 1:100 YEAR EVENT						
AREA 2-R		Co	ntrolled Roof	Drain #	13,15,17		
OTTAWA ID							
Area =	0.003	ha	Qallow =	0.79	L/s		
C =	0.90		Vol(max) =	0.4	m3		
Time	Intensity	Q	Qnet	Vol			
(min)	(mm/hr)	(L/s)	(L/s)	(m3)			
5	242.70	2.05	1.26	0.38			
10	178.56	1.51	0.72	0.43			
15	142.89	1.20	0.41	0.37			
20	119.95	1.01	0.22	0.27			
25	103.85	0.88	0.09	0.13			
30	91.87	0.77	-0.02	-0.03			
35	82.58	0.70	-0.09	-0.20			
40	75.15	0.63	-0.16	-0.38			
45	69.05	0.58	-0.21	-0.56			
50	63.95	0.54	-0.25	-0.75			
55	59.62	0.50	-0.29	-0.95			
60	55.89	0.47	-0.32	-1.15			
65	52.65	0.44	-0.35	-1.35			
70	49.79	0.42	-0.37	-1.55			
75	47.26	0.40	-0.39	-1.76			
90	41.11	0.35	-0.44	-2.39			
105	36.50	0.31	-0.48	-3.04			
120	32.89	0.28	-0.51	-3.69			

Watts Accutrol Flow Control Roof Drains:			RD-100-A-ADJ	set to 1/4 Exposed	
Design Event	Design Event Flow (L/s)		Ponding	Storage	(m <sup>3</sup> )
Design Event		Total Flow (L/s)	(cm)	Required	Provided
1:5 Year	0.71	2.13	7.6	0.4	0.8
1:100 Year	0.79	2.37	10.2	1.3	1.7

<b>Roof Drain Stor</b>	13,15,17	
Elevation	Area	Total Volume
m	m²	m <sup>3</sup>
0.00	0	0
0.05	3.8	0.1
0.10	15	0.6
0.15	33.7	1.8

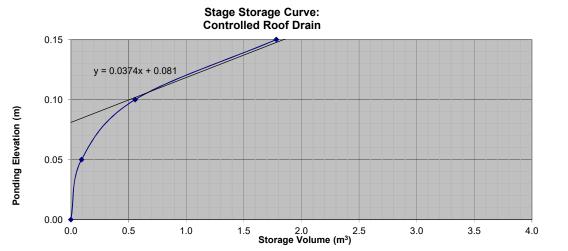


ADELAIDE	TOWER	EXPANS	SION		
116070					
REQUIRED	STORAGE	E - 1:5 YE	AR EVENT		
AREA 2-R		Co	ntrolled Roof	Drain #	14,16,18
OTTAWA ID	F CURVE				
Area =	0.003	ha	Qallow =	0.71	L/s
C =	0.90		Vol(max) =	0.1	m3
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	141.18	1.20	0.49	0.15	
10	104.19	0.89	0.18	0.11	
15	83.56	0.71	0.00	0.00	
20	70.25	0.60	-0.11	-0.13	
25	60.90	0.52	-0.19	-0.29	
30	53.93	0.46	-0.25	-0.45	
35	48.52	0.41	-0.30	-0.62	
40	44.18	0.38	-0.33	-0.80	
45	40.63	0.35	-0.36	-0.98	
50	37.65	0.32	-0.39	-1.17	
55	35.12	0.30	-0.41	-1.35	
60	32.94	0.28	-0.43	-1.54	
65	31.04	0.26	-0.45	-1.74	
70	29.37	0.25	-0.46	-1.93	
75	27.89	0.24	-0.47	-2.12	
90	24.29	0.21	-0.50	-2.71	
105	21.58	0.18	-0.53	-3.31	
120	19.47	0.17	-0.54	-3.92	

ADELAIDE	TOWER	EXPAN	SION		
116070					
REQUIRED	STORAGE	E - 1:100	YEAR EVENT	•	
AREA 2-R		Co	ntrolled Roof	Drain #	14,16,18
OTTAWA ID	OF CURVE				
Area =	0.003	ha	Qallow =	0.79	L/s
C =	0.90		Vol(max) =	0.4	m3
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	242.70	2.07	1.28	0.38	
10	178.56	1.52	0.73	0.44	
15	142.89	1.22	0.43	0.39	
20	119.95	1.02	0.23	0.28	
25	103.85	0.89	0.10	0.14	
30	91.87	0.78	-0.01	-0.01	
35	82.58	0.70	-0.09	-0.18	
40	75.15	0.64	-0.15	-0.36	
45	69.05	0.59	-0.20	-0.54	
50	63.95	0.55	-0.24	-0.73	
55	59.62	0.51	-0.28	-0.93	
60	55.89	0.48	-0.31	-1.13	
65	52.65	0.45	-0.34	-1.33	
70	49.79	0.42	-0.37	-1.53	
75	47.26	0.40	-0.39	-1.74	
90	41.11	0.35	-0.44	-2.37	
105	36.50	0.31	-0.48	-3.02	
120	32.89	0.28	-0.51	-3.67	
<u> </u>					

Watts Accutrol Flow	Control Roof Drains:		RD-100-A-ADJ	set to 1/4 Exposed	
Design Event	Flow (L/s)	Total Flow (L/s)	Ponding	Storage	e (m³)
Design Event Flow		10tal 110w (L/S)	(cm)	Required	Provided
1:5 Year	0.71	2.13	7.6	0.4	0.8
1:100 Year	0.79	2.37	10.2	1.3	1.7

<b>Roof Drain Stor</b>	Roof Drain Storage Table for RD #				
Elevation	Area	Total Volume			
m	m²	m <sup>3</sup>			
0.00	0	0			
0.05	3.7	0.1			
0.10	14.9	0.6			
0.15	34.1	1.8			

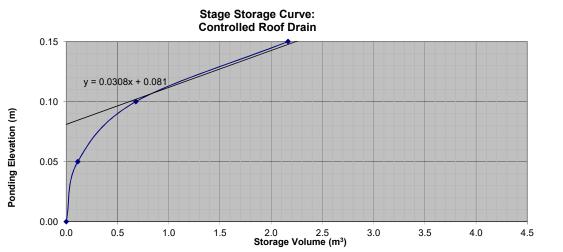


ADELAIDE	TOWER	EXPANS	SION		
116070					
REQUIRED	STORAGE	E - 1:5 YE	AR EVENT		
AREA 2-R		Co	ntrolled Roof	Drain #	19+20
OTTAWA ID	F CURVE				
Area =	0.004	ha	Qallow =	0.71	L/s
C =	0.90		Vol(max) =	0.2	m3
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	141.18	1.46	0.75	0.22	
10	104.19	1.07	0.36	0.22	
15	83.56	0.86	0.15	0.14	
20	70.25	0.72	0.01	0.02	
25	60.90	0.63	-0.08	-0.12	
30	53.93	0.56	-0.15	-0.28	
35	48.52	0.50	-0.21	-0.44	
40	44.18	0.46	-0.25	-0.61	
45	40.63	0.42	-0.29	-0.79	
50	37.65	0.39	-0.32	-0.97	
55	35.12	0.36	-0.35	-1.15	
60	32.94	0.34	-0.37	-1.33	
65	31.04	0.32	-0.39	-1.52	
70	29.37	0.30	-0.41	-1.71	
75	27.89	0.29	-0.42	-1.90	
90	24.29	0.25	-0.46	-2.48	
105	21.58	0.22	-0.49	-3.07	
120	19.47	0.20	-0.51	-3.67	

OTTAWA IDF CURVE	<u>19+20</u> L/s
REQUIRED STORAGE - 1:100 YEAR EVENT AREA 2-R Controlled Roof Drain # OTTAWA IDF CURVE	
AREA 2-R Controlled Roof Drain # OTTAWA IDF CURVE	
OTTAWA IDF CURVE	
	L/s
Area = 0.004 ha Qallow = 0.79	L/s
C = 0.90 Vol(max) = 0.6	m3
Time Intensity Q Qnet Vol	
(min) (mm/hr) (L/s) (L/s) (m3)	
5 242.70 2.50 1.71 0.51	
10 178.56 1.84 1.05 0.63	
15 142.89 1.47 0.68 0.61	
20 119.95 1.24 0.45 0.54	
25 103.85 1.07 0.28 0.42	
30 91.87 0.95 0.16 0.28	
35 82.58 0.85 0.06 0.13	
40 75.15 0.77 -0.02 -0.04	
45 69.05 0.71 -0.08 -0.21	
50 63.95 0.66 -0.13 -0.39	
55 59.62 0.61 -0.18 -0.58	
60 55.89 0.58 -0.21 -0.77	
65 52.65 0.54 -0.25 -0.96	
70 49.79 0.51 -0.28 -1.16	
75 47.26 0.49 -0.30 -1.36	
90 41.11 0.42 -0.37 -1.98	
105 36.50 0.38 -0.41 -2.61	
120 32.89 0.34 -0.45 -3.25	

Watts Accutrol Flow Control Roof Drains:			RD-100-A-ADJ	set to 1/4 Exposed	
Design Event Flow (L/s)		Total Flow (L/s)	Ponding	Storage	e (m³)
Design Event	FIOW (L/S)	Total Flow (L/S)	(cm)	Required	Provided
1:5 Year	0.71	1.42	7.6	0.4	0.6
1:100 Year	0.79	1.58	10.2	1.3	1.4

<b>Roof Drain Stor</b>	Roof Drain Storage Table for RD # 19+20				
Elevation	Area	Total Volume			
m	m²	m <sup>3</sup>			
0.00	0	0			
0.05	4.5	0.1			
0.10	18.2	0.7			
0.15	41.2	2.2			

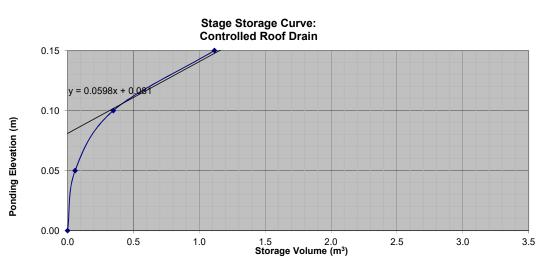


ADELAIDE	TOWER	EXPANS	SION		
116070					
REQUIRED	STORAGE				
AREA 2-R		Co	ntrolled Roof	Drain #	21
OTTAWA ID	F CURVE				
Area =	0.002	ha	Qallow =	0.63	L/s
C =	0.90		Vol(max) =	0.0	m3
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	141.18	0.76	0.13	0.04	
10	104.19	0.56	-0.07	-0.04	
15	83.56	0.45	-0.18	-0.16	
20	70.25	0.38	-0.25	-0.30	
25	60.90	0.33	-0.30	-0.46	
30	53.93	0.29	-0.34	-0.61	
35	48.52	0.26	-0.37	-0.78	
40	44.18	0.24	-0.39	-0.94	
45	40.63	0.22	-0.41	-1.11	
50	37.65	0.20	-0.43	-1.29	
55	35.12	0.19	-0.44	-1.46	
60	32.94	0.18	-0.45	-1.63	
65	31.04	0.17	-0.46	-1.81	
70	29.37	0.16	-0.47	-1.99	
75	27.89	0.15	-0.48	-2.16	
90	24.29	0.13	-0.50	-2.70	
105	21.58	0.12	-0.51	-3.24	
120	19.47	0.10	-0.53	-3.79	

-					
ADELAIDE	TOWER	EXPAN	SION		
116070					
	STORAGE		YEAR EVENT		~
AREA 2-R		Co	ntrolled Roof	Drain #	21
OTTAWA IE					
Area =	0.002	ha	Qallow =	0.79	L/s
C =	0.90		Vol(max) =	0.2	m3
Time	Intonoity	Q	Qnet	Vol	
	Intensity				
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	242.70	1.30	0.51	0.15	
10	178.56	0.96	0.17	0.10	
15	142.89	0.77	-0.02	-0.02	
20	119.95	0.64	-0.15	-0.18	
25	103.85	0.56	-0.23	-0.35	
30	91.87	0.49	-0.30	-0.54	
35	82.58	0.44	-0.35	-0.73	
40	75.15	0.40	-0.39	-0.93	
45	69.05	0.37	-0.42	-1.13	
50	63.95	0.34	-0.45	-1.34	
55	59.62	0.32	-0.47	-1.55	
60	55.89	0.30	-0.49	-1.77	
65	52.65	0.28	-0.51	-1.98	
70	49.79	0.27	-0.52	-2.20	
75	47.26	0.25	-0.54	-2.42	
90	41.11	0.22	-0.57	-3.08	
105	36.50	0.20	-0.59	-3.75	
120	32.89	0.18	-0.61	-4.42	

Watts Accutrol Flow Control Roof Drains:			RD-100-A-ADJ	set to 1/4 Exposed	
Design Event Flow (L/s)		Total Flow (L/s)	Ponding	Storage	e (m <sup>3</sup> )
Design Event		Total Flow (L/S)	(cm)	Required	Provided
1:5 Year	0.63	0.63	5.1	0.04	0.05
1:100 Year	0.79	0.79	10.2	0.2	0.4

Roof Drain Storage Table for RD # 21				
Elevation	Area	Total Volume		
m	m <sup>2</sup>	m³		
0.00	0	0		
0.05	2.3	0.1		
0.10	9.3	0.3		
0.15	21.4	1.1		

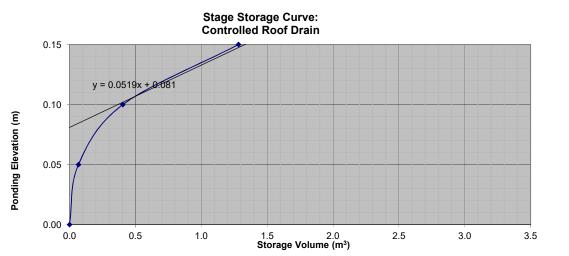


ADELAIDE	TOWER	EXPANS	SION		
116070					
REQUIRED	STORAGE				
AREA 2-R		Co	ntrolled Roof	Drain #	22
OTTAWA ID	F CURVE				
Area =	0.002	ha	Qallow =	0.63	L/s
C =	0.90		Vol(max) =	0.1	m3
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	141.18	0.86	0.23	0.07	
10	104.19	0.63	0.00	0.00	
15	83.56	0.51	-0.12	-0.11	
20	70.25	0.43	-0.20	-0.24	
25	60.90	0.37	-0.26	-0.39	
30	53.93	0.33	-0.30	-0.54	
35	48.52	0.29	-0.34	-0.70	
40	44.18	0.27	-0.36	-0.87	
45	40.63	0.25	-0.38	-1.03	
50	37.65	0.23	-0.40	-1.20	
55	35.12	0.21	-0.42	-1.37	
60	32.94	0.20	-0.43	-1.55	
65	31.04	0.19	-0.44	-1.72	
70	29.37	0.18	-0.45	-1.90	
75	27.89	0.17	-0.46	-2.07	
90	24.29	0.15	-0.48	-2.60	
105	21.58	0.13	-0.50	-3.14	
120	19.47	0.12	-0.51	-3.68	

ADELAIDE	TOWER	EXPAN	SION		
116070					
	STORAGE		YEAR EVENT		
AREA 2-R		Co	ntrolled Roof	Drain #	22
OTTAWA IE					
Area =	0.002	ha	Qallow =	0.79	L/s
C =	0.90		Vol(max) =	0.2	m3
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	242.70	1.48	0.69	0.21	
10	178.56	1.09	0.30	0.18	
15	142.89	0.87	0.08	0.07	
20	119.95	0.73	-0.06	-0.07	
25	103.85	0.63	-0.16	-0.24	
30	91.87	0.56	-0.23	-0.42	
35	82.58	0.50	-0.29	-0.60	
40	75.15	0.46	-0.33	-0.80	
45	69.05	0.42	-0.37	-1.00	
50	63.95	0.39	-0.40	-1.20	
55	59.62	0.36	-0.43	-1.41	
60	55.89	0.34	-0.45	-1.62	
65	52.65	0.32	-0.47	-1.83	
70	49.79	0.30	-0.49	-2.05	
75	47.26	0.29	-0.50	-2.26	
90	41.11	0.25	-0.54	-2.92	
105	36.50	0.22	-0.57	-3.58	
120	32.89	0.20	-0.59	-4.25	

Natts Accutrol Flow	Control Roof Drains:	trol Roof Drains: RD-100-A-ADJ set to 1/4 Exposed						
Design Event Flow (L/s)		Total Flow (L/s)	Ponding Storage (m <sup>3</sup>		e (m <sup>3</sup> )			
Design Event		Total Flow (L/S)	(cm)	Required	uired Provided			
1:5 Year	0.63	0.63	5.1	0.07	0.07			
1:100 Year	0.79	0.79	10.2	0.2	0.4			

<b>Roof Drain Stor</b>	rage Table for RD #	22
Elevation	Area	Total Volume
m	m²	m <sup>3</sup>
0.00	0	0
0.05	2.7	0.1
0.10	10.8	0.4
0.15	24.3	1.3

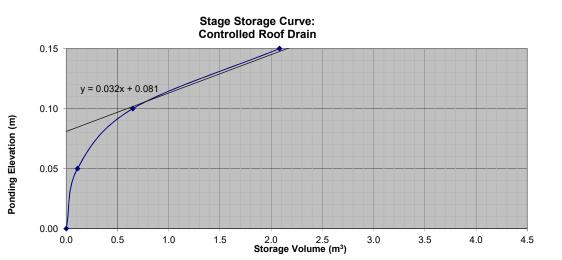


ADELAIDE	ADELAIDE TOWER EXPANSION						
116070							
REQUIRED	STORAGE	E - 1:5 YE	AR EVENT				
AREA 2-R		Co	ntrolled Roof	Drain #	23+24		
OTTAWA ID	F CURVE						
Area =	0.004	ha	Qallow =	0.71	L/s		
C =	0.90		Vol(max) =	0.2	m3		
Time	Intensity	Q	Qnet	Vol			
(min)	(mm/hr)	(L/s)	(L/s)	(m3)			
5	141.18	1.42	0.71	0.21			
10	104.19	1.05	0.34	0.20			
15	83.56	0.84	0.13	0.12			
20	70.25	0.70	-0.01	-0.01			
25	60.90	0.61	-0.10	-0.15			
30	53.93	0.54	-0.17	-0.30			
35	48.52	0.49	-0.22	-0.47			
40	44.18	0.44	-0.27	-0.64			
45	40.63	0.41	-0.30	-0.82			
50	37.65	0.38	-0.33	-1.00			
55	35.12	0.35	-0.36	-1.18			
60	32.94	0.33	-0.38	-1.37			
65	31.04	0.31	-0.40	-1.55			
70	29.37	0.29	-0.42	-1.74			
75	27.89	0.28	-0.43	-1.94			
90	24.29	0.24	-0.47	-2.52			
105	21.58	0.22	-0.49	-3.11			
120	19.47	0.20	-0.51	-3.71			

ADELAIDE		FYPAN	SION		
116070					
	STORAGE	- 1:100	YEAR EVENT	-	
AREA 2-R	0.0.0.0		ntrolled Roof		23+24
OTTAWA II	OF CURVE				-
Area =	0.004	ha	Qallow =	0.79	L/s
C =	0.90		Vol(max) =	0.6	m3
_			( )		
Time	Intensity	Q	Qnet	Vol	
(min)	(mm/hr)	(L/s)	(L/s)	(m3)	
5	242.70	2.44	1.65	0.49	
10	178.56	1.79	1.00	0.60	
15	142.89	1.43	0.64	0.58	
20	119.95	1.20	0.41	0.50	
25	103.85	1.04	0.25	0.38	
30	91.87	0.92	0.13	0.24	
35	82.58	0.83	0.04	0.08	
40	75.15	0.75	-0.04	-0.09	
45	69.05	0.69	-0.10	-0.26	
50	63.95	0.64	-0.15	-0.45	
55	59.62	0.60	-0.19	-0.63	
60	55.89	0.56	-0.23	-0.83	
65	52.65	0.53	-0.26	-1.02	
70	49.79	0.50	-0.29	-1.22	
75	47.26	0.47	-0.32	-1.42	
90	41.11	0.41	-0.38	-2.04	
105	36.50	0.37	-0.42	-2.67	
120	32.89	0.33	-0.46	-3.31	

<b>Watts Accutrol Flow</b>	Control Roof Drains:		RD-100-A-ADJ	set to 1/4 Exposed		
Design Event Flow (L/s)		Total Flow (L/s)	Ponding	Ponding Storage (m <sup>3</sup> )		
Design Lvent		Total Flow (L/S)	(cm)	Required P		
1:5 Year	0.71	1.42	7.6	0.4	0.6	
1:100 Year	0.79	1.58	10.2	1.2	1.3	

<b>Roof Drain Stor</b>	rage Table for RD #	23+24
Elevation	Area	Total Volume
m	m²	m <sup>3</sup>
0.00	0	0
0.05	4.4	0.1
0.10	17.2	0.7
0.15	40.1	2.1



WATTS	Adjustable Accutrol Weir Tag:	Adjustable Flow Control for Roof Drains
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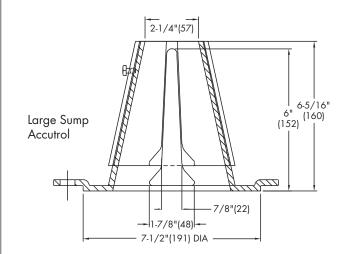
#### ADJUSTABLE ACCUTROL (for Large Sump Roof Drains only)

For more flexibility in controlling flow with heads deeper than 2", Watts Drainage offers the Adjustable Accutrol. The Adjustable Accutrol Weir is designed with a single parabolic opening that can be covered to restrict flow above 2" of head to less than 5 gpm per inch, up to 6" of head. To adjust the flow rate for depths over 2" of head, set the slot in the adjustable upper cone according to the flow rate required. Refer to Table 1 below. Note: Flow rates are directly proportional to the amount of weir opening that is exposed.

### EXAMPLE:

For example, if the adjustable upper cone is set to cover 1/2 of the weir opening, flow rates above 2"of head will be restricted to 2-1/2 gpm per inch of head.

Therefore, at 3" of head, the flow rate through the Accutrol Weir that has 1/2 the slot exposed will be: [5 gpm (per inch of head) x 2 inches of head ] + 2-1/2 gpm (for the third inch of head) = 12-1/2 gpm.



Wair Opening	1"	2"	3"	4"	5"	6"
Weir Opening Exposed	Flow Rate (gallons per minute)					
Fully Exposed	5	10	15	20	25	30
3/4	5	10	13.75	17.5	21.25	25
1/2	5	10	12.5	15	17.5	20
1/4	5	10	11.25	12.5	13.75	15
Closed	5	5	5	5	5	5

Job Name

Job Location

Engineer

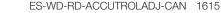
Contractor \_\_\_\_\_

Contractor's P.O. No.

Representative \_\_\_\_

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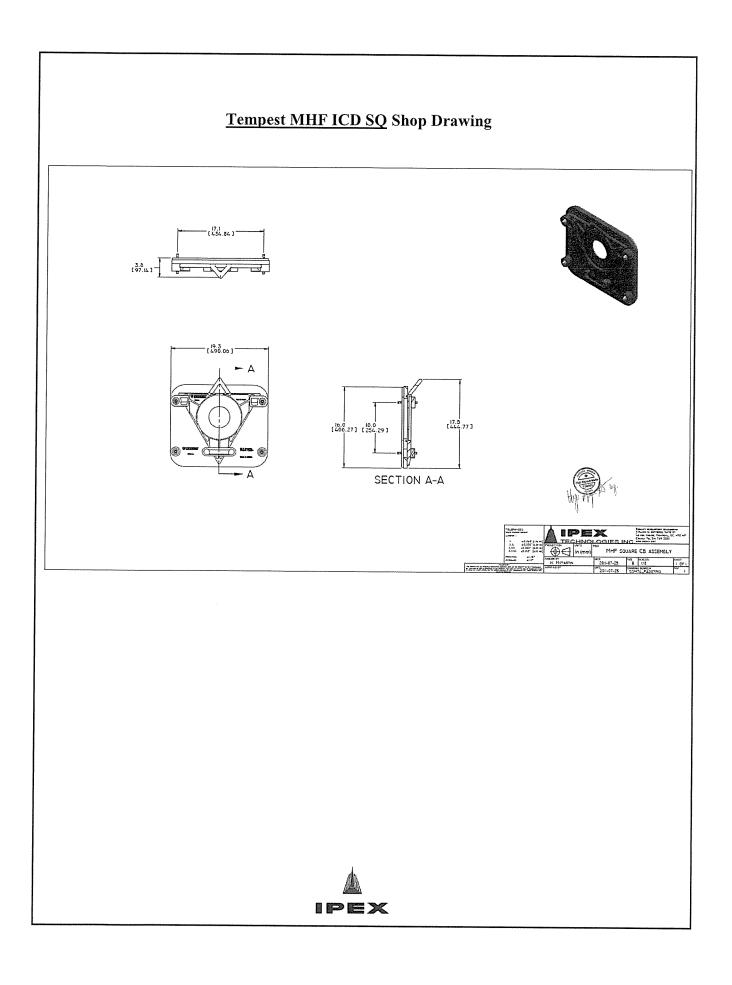
**USA:** Tel: (800) 338-2581 • Fax: (828) 248-3929 • Watts.com **Canada:** Tel: (905) 332-4090 • Fax: (905) 332-7068 • Watts.ca **Latin America:** Tel: (52) 81-1001-8600 • Fax: (52) 81-8000-7091 • Watts.com







A Watts Water Technologies Company



# APPENDIX D

# Water Demands, Boundary Conditions and FUS Calculation



# Adelaide Apartments Tower PRELIMINARY WATER DEMAND CALCULATIONS

Water Demand (Proposed)									
	R	lesidentia	l	Commercial	De	emands (L	_/s)		
Building	Un	nits in the second s		Units		Office Employees	Average	Max.	Peak Hour
	1 Bdrm	2 Bdrm	(pers)	(pers)	Day	Daily	HOUI		
New Addition	216 22	12 2	328 35	0 0	1.33 0.14	3.32 0.35	7.31 0.78		
Total	238	14	363	0	1.47	3.68	8.09		

#### Notes:

Residential Densities (from	n City	<u>/ of Ottawa data):</u>	
- 1 Bedroom Apartment =		1.4	cap/unit
- 2 Bedroom Apartment =		2.1	cap/unit
<u>Avg. Day Demand:</u> - Residential	=	350	L/cap/day
<u>Max. Daily Demand:</u> - Residential	=	2.5	x Avg. Day
<u>Peak Hour Demand:</u> - Residential	=	2.2	x Max. Day

## Greg MacDonald

From:	Fraser, Mark <mark.fraser@ottawa.ca></mark.fraser@ottawa.ca>
Sent:	Friday, August 05, 2016 8:28 AM
То:	Matthew Linton
Cc:	Greg MacDonald
Subject:	RE: Fire Flow Request - Civic Address_333 Preston Street - Closest X-Street_Aberdeen Street
Attachments:	333 Preston Aug 2016.pdf; Fire Flow Calculations-116070.pdf; 116070-GP-toFraser.pdf

#### Hi Matthew,

Please find below water distribution network boundary conditions for hydraulic analysis as requested based on the provided anticipated water demands and fire flow requirement.

### **Proposed Water Demands and Fire Flow Requirement:**

Proposed Development Location: 333 Preston Street [Proposed Adelaide Tower] Average Daily Demand = 1.04 L/s Max Daily Demand = 2.61 L/s Peak Hour Demand = 5.74 L/s Fire Flow = 10,000 L/min

#### **City of Ottawa Boundary Conditions:**

Specified Service Connection Point: Aberdeen Street Minimum HGL = 106.1m Maximum HGL = 117.5 [Please note that the maximum pressure is estimated to be more than 80 psi. A pressure check at completion of construction is recommended to determine if pressure control is required.] MXDY+Fire = 104.2m

Please note that these are for current conditions and are based on computer model simulation.



The above boundary conditions, HGL, for hydraulic analysis at 333 Preston [**Pressure Zone 1W**] assumed to be connected to the 203mm on Aberdeen Street [see attached PDF for connection location].

Please refer to City of Ottawa, *Ottawa Design Guidelines – Water Distribution*, First Edition, July 2010, WDG001 Clause 4.2.2 for watermain pressure and demand objectives. Also, please refer to Guidelines and Technical bulletin ISDTB-2014-02 concerning basic day demands greater than 0.5 L/s

**Disclaimer:** The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation. Fire Flow analysis is a reflection of available flow in the watermain; there may be additional restrictions that occur between the watermain and the hydrant that the model cannot take into account.

Regards,

Mark Fraser Junior Infrastructure Engineer, Suburban Services



City of Ottawa | Ville d'Ottawa Planning and Growth Management Department 110 Laurier Avenue West. 4th Floor, Ottawa ON, K1P 1J1 Tel:613.580.2424 ext. 27791 Fax: 613-580-2576 Mail: Code 01-14 Email: Mark.Fraser@ottawa.ca

\*Please consider your environmental responsibility before printing this e-mail

From: Matthew Linton [mailto:m.linton@novatech-eng.com]
Sent: August 04, 2016 11:44 AM
To: Fraser, Mark
Cc: Greg MacDonald
Subject: RE: Fire Flow Request - Civic Address\_333 Preston Street - Closest X-Street\_Aberdeen Street

Good afternoon Mark,

I am just wondering if there is any update as to when we will receive the boundary conditions.

Thanks,

#### Matthew Linton, CAD Drafting

**NOVATECH** Engineers, Planners & Landscape Architects 240 Michael Cowpland Drive, Suite 200, Ottawa, ON, K2M 1P6 | Tel: 613.254.9643 | Fax: 613.254.5867 The information contained in this email message is confidential and is for exclusive use of the addressee.

From: Adam Lambros
Sent: July-28-16 3:00 PM
To: Fraser, Mark <<u>Mark.Fraser@ottawa.ca</u>>
Cc: Greg MacDonald <<u>g.Macdonald@novatech-eng.com</u>>; Matthew Linton <<u>m.linton@novatech-eng.com</u>>
Subject: RE: Fire Flow Request - Civic Address\_333 Preston Street - Closest X-Street\_Aberdeen Street

#### Hello Mark,

Thanks for the update. My last day at Novatech is tomorrow, please include Greg and Matt (CCed) on your email.

Regards,

### Adam Lambros

From: Fraser, Mark [mailto:Mark.Fraser@ottawa.ca] Sent: July-28-16 2:58 PM To: Adam Lambros <<u>a.lambros@novatech-eng.com</u>> Subject: RE: Fire Flow Request - Civic Address\_333 Preston Street - Closest X-Street\_Aberdeen Street

Hi Adam,

I should have the boundary conditions by tomorrow for you.

Regards,

Mark Fraser Junior Infrastructure Engineer, Suburban Services



City of Ottawa | Ville d'Ottawa Planning and Growth Management Department 110 Laurier Avenue West. 4th Floor, Ottawa ON, K1P 1J1 <u>Tel:613.580.2424</u> ext. 27791 Fax: 613-580-2576 Mail: Code 01-14 Email: <u>Mark.Fraser@ottawa.ca</u>

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From: Fraser, Mark Sent: July 18, 2016 8:46 AM To: 'Adam Lambros' Subject: RE: Fire Flow Request - Civic Address\_333 Preston Street - Closest X-Street\_Aberdeen Street

Hi Adam,

Please accept this email as confirmation that boundary conditions for hydraulic analysis have been requested based on the anticipated water demands for the subject site. Please note that It takes approximately 5 business days to receive boundary conditions.

If you require any additional information I will direct you to a Project Manager in the Development Review Urban Services Unit.

Regards,

## **Mark Fraser**

Junior Infrastructure Engineer, Suburban Services



City of Ottawa | Ville d'Ottawa Planning and Growth Management Department 110 Laurier Avenue West. 4th Floor, Ottawa ON, K1P 1J1 <u>Tel:613.580.2424</u> ext. 27791 Fax: 613-580-2576 Mail: Code 01-14 Email: <u>Mark.Fraser@ottawa.ca</u>

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From: Adam Lambros [mailto:a.lambros@novatech-eng.com] Sent: July 15, 2016 3:14 PM To: Fraser, Mark Cc: Matthew Linton Subject: RE: Fire Flow Request - Civic Address\_333 Preston Street - Closest X-Street\_Aberdeen Street

Hi Mark,

The service connection will be made to Aberdeen street while the fire flows will come off of the hydrant along 200mm WM on-site. So, can the model please be run accordingly, providing boundary conditions at points "1" and "2" as shown on the attached plan and highlighted in yellow?

Requested info is as follows;

Residential Condominium Tower, 184 units. Site Address: 17 Aberdeen St. (Extension of existing building) A plan clearly showing the proposed water service connection location(s): See attached, highlighted in yellow. Anticipated Water Demands:

= 90,160 L/day

= 258 people x 350 L/cap/day

Population Calculation	= 184 units x 1.4 persons per unit
	= 258 people

Proposed Average Residential Flows

	= 1.04 L/sec
Average Day Demand	= 90,160 L/day = 1.04 L/s
Max Daily Demand	= 90,160 L/day x 2.5 = 225,400 L/day
Max Hourly Demand	= 2.61 L/s = 225,400 L/day x 2.2 = 495,880 L/day
Fire Flow	= 5.74 L/s = 10,000 L/min (See attached FUS calc)

Please call I you would like to discuss,

Adam Lambros, P.Eng NOVATECH Engineers, Planners & Landscape Architects 240 Michael Cowpland Drive, Suite 200, Ottawa, ON, K2M 1P6 | Tel: 613.254.9643 x278 | Tel(Direct): 613.254.9839 x278 | Fax: 613.254.5867 The information contained in this email message is confidential and is for exclusive use of the addressee.

From: Fraser, Mark [mailto:Mark.Fraser@ottawa.ca] Sent: July-12-16 3:22 PM To: Adam Lambros <<u>a.lambros@novatech-eng.com</u>> Subject: RE: Fire Flow Request - Civic Address\_333 Preston Street - Closest X-Street\_Aberdeen Street

#### Hi Adam,

To request City of Ottawa water distribution network boundary conditions please provide the City with following information:

- Type of Development
- Site Address
- A plan clearly showing the proposed water service connection location(s)
- Anticipated Water Demands
  - Average Daily Demand (L/s)
  - Maximum Daily Demand (L/s)
  - Peak Hour Demand (L/s)
  - Fire Flow (L/s)

Please provide a PDF copy of the FUS and water demand calculations to support the anticipated demands provided .

- Fire flow demand requirements shall be based on Fire Underwriters Survey (FUS) Water Supply for Public Fire Protection 1999 as per the Ottawa Design Guidelines Water Distribution, First Edition, Document WDG001, July 2010, City of Ottawa Clause 4.2.11.
- The full 50% reduction for sprinklering is only available for monitored systems.
- Reductions, where applied to the fire requirement demand calculation(s), need to be justified.

Once the required information has been provided it will take **approximately five (5) business days** to receive boundary condition results for hydraulic analysis.

If you have any questions please let me know.

Regards,

Mark Fraser Junior Infrastructure Engineer, Suburban Services



City of Ottawa | Ville d'Ottawa Planning and Growth Management Department 110 Laurier Avenue West. 4th Floor, Ottawa ON, K1P 1J1 <u>Tel:613.580.2424</u> ext. 27791 Fax: 613-580-2576 Mail: Code 01-14 Email: <u>Mark.Fraser@ottawa.ca</u>

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From: Adam Lambros [mailto:a.lambros@novatech-eng.com] Sent: July 12, 2016 1:19 PM To: Fraser, Mark Subject: RE: Fire Flow Request - Civic Address\_333 Preston Street - Closest X-Street\_Aberdeen Street

#### Hello Mark,

Can we obtain boundary conditions instead? If so, I'll send over our demands?

Left you a message earlier, please call if you would like to discuss.

Regards,

#### Adam Lambros

 From: Fraser, Mark [mailto:Mark.Fraser@ottawa.ca]

 Sent: July-08-16 3:31 PM

 To: Adam Lambros <a.lambros@novatech-eng.com</td>

 Cc: Greg MacDonald <g.Macdonald@novatech-eng.com</td>

 Subject: RE: Fire Flow Request - Civic Address\_333 Preston Street - Closest X-Street Aberdeen Street

Hi Adam,

Please note that I have been advised by the Environmental Services Department that the City of Ottawa is no longer in a position to provide fire flow/pressure data. Should you wish to schedule a flow test, please visit the website <u>Water</u> <u>Bylaw</u> section 62, and contact <u>Sarah.Ramsey@Ottawa.ca</u> or call the Business Services Branch at 613-580-2424 x22268.

Regards,

Mark Fraser Junior Infrastructure Engineer, Suburban Services



City of Ottawa | Ville d'Ottawa Planning and Growth Management Department 110 Laurier Avenue West. 4th Floor, Ottawa ON, K1P 1J1 <u>Tel:613.580.2424</u> ext. 27791 Fax: 613-580-2576 Mail: Code 01-14 Email: <u>Mark.Fraser@ottawa.ca</u>

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From: Fraser, Mark Sent: July 05, 2016 2:29 PM To: 'hydrantfireflow@ottawa.ca' Cc: 'Adam Lambros'; 'Greg MacDonald'; Matthew Linton Subject: Fire Flow Request - Civic Address\_333 Preston Street - Closest X-Street\_Aberdeen Street

Hydrant Fire Flow,

Please accept this email as a request to obtain City of Ottawa available Fire Hydrant Flow Data:

- A civic address and the closest x-street:
   333 Preston Street Closest x-Street: Aberdeen Street [Adelaide Tower]
- Fire hydrant identification no.(s):
  - Public Fire Hydrant(s): [H312] [H053[ [H054] [H212] [H213]
  - Private Fire Hydrant(s): [HP296] [HP295] if data is available for private fire hydrants
- The nature of the request, development or non-development (development requests are those in which other City permits will be required regardless of the requestor's scope of work): Development Request\_Proposed Site Servicing Study
- General details as to the work being performed (*i.e. purpose for request*):
   Fire hydrant flow data has been requested prior to submission of a Site Plan Control development application for a proposed tower, an extension of the existing Adelaide tower residence, 24 story residential building. Please note that the consultant will be advised to also request boundary conditions to further validate any fire hydrant flow data issued as it is noted that testing remains a point-in-time test, and as such may not reflect the current system conditions and/or hydraulics.
- Required Fire Flow (as per Fire Underwriter's Survey Guidelines):
   Fire Flow Calculations Attached. The floor area in the attached calculations is that of the existing building + the area of the new extension + 25% of floor above + 25% of floor below.



If obsolete or insufficient fire hydrant flow data is only available at this time please notify.

Through this email the consultant has been notified to allow for **10 business days** to receive a reply to this Fire Hydrant Flow Data Request.

To schedule a new test, please contact the Business Services Branch at 613-580-2424 x22268 and visit the website <u>Water</u> <u>Bylaw</u> section **62** for more information.

Regards,

Mark Fraser Junior Infrastructure Engineer, Suburban Services



City of Ottawa | Ville d'Ottawa Planning and Growth Management Department 110 Laurier Avenue West. 4th Floor, Ottawa ON, K1P 1J1 <u>Tel:613.580.2424</u> ext. 27791 Fax: 613-580-2576 Mail: Code 01-14 Email: <u>Mark.Fraser@ottawa.ca</u>

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ിലെ സംപള്ള, സിവികള് ല്യൂര്ഡോന്റെ പ്രതിന്ത് പറിന്ത് പോസ്സ്കോം പ്രതിഷണം പറിന്നും പറ്റും പറിന്നും പറ്റും പ്രതിന്തെ പ്രതിന്റെ മന്ന്റെ ക്ഷിസ്കാന് പ്രതിന്റെ പത്താള് നിന്നും അത്രോഗ്രം കോള് മന്ന്റെ കണ്ട്രിന്നും പറ്റും പോണ് പ്രതിന്നെ

From: Adam Lambros [mailto:a.lambros@novatech-eng.com] Sent: July 04, 2016 2:06 PM To: Fraser, Mark Cc: Greg MacDonald; Matthew Linton Subject: RE: Adelaide Tower

Sorry Mark,

Can we please have HP296 & HP295 as well?

Regards,

Adam Lambros

From: Adam Lambros Sent: July-04-16 2:03 PM To: 'Fraser, Mark' <<u>Mark.Fraser@ottawa.ca</u>> Cc: Greg MacDonald <<u>g.Macdonald@novatech-eng.com</u>>; Matthew Linton <<u>m.linton@novatech-eng.com</u>> Subject: Adelaide Tower

Hello Mark,

Can you please provide hydrant data for the following hydrants on or near Aberdeen St.

H312 H053 H054 H212 H213

Regards,

Adam Lambros, P.Eng

**NOVATECH** Engineers, Planners & Landscape Architects

240 Michael Cowpland Drive, Suite 200, Ottawa, ON, K2M 1P6 | Tel: 613.254.9643 x278 | Tel(Direct): 613.254.9839 x278 | Fax: 613.254.5867

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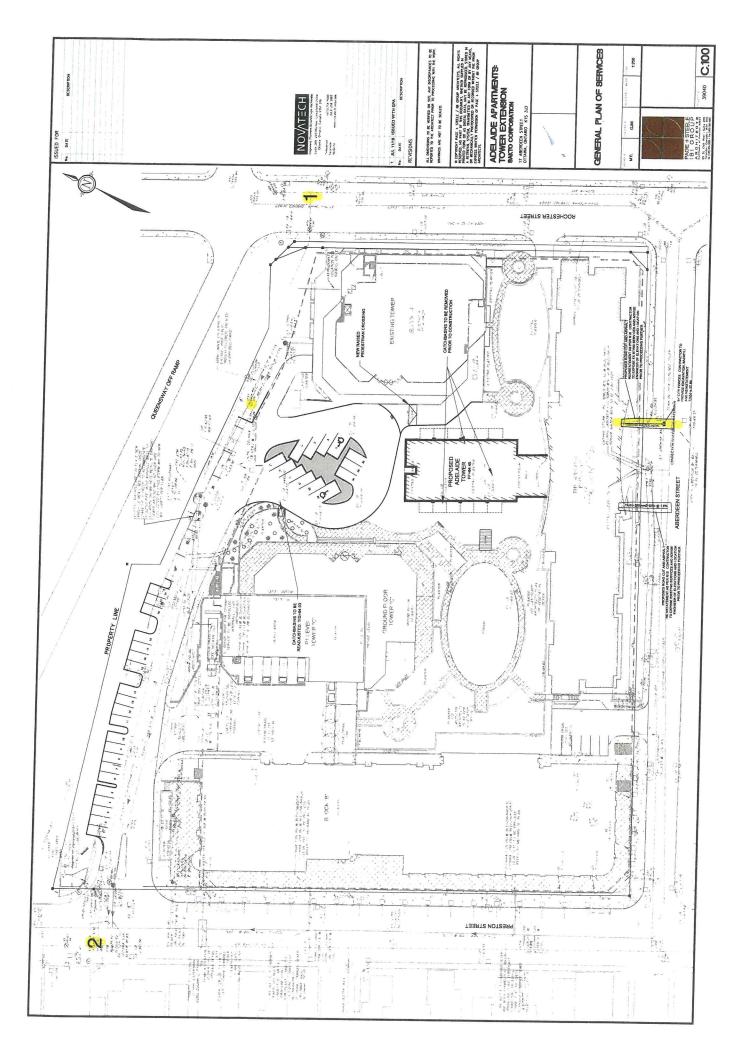
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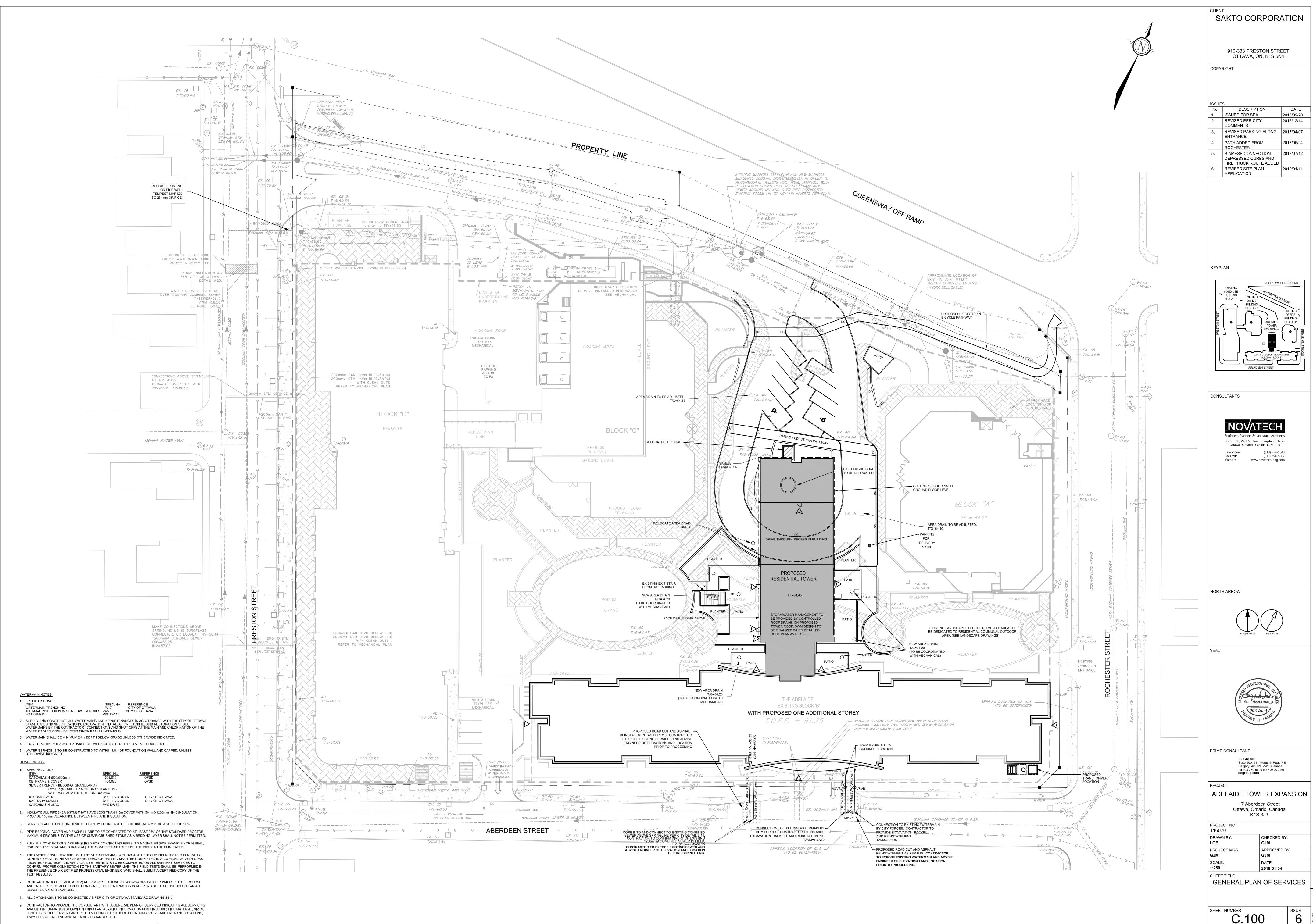
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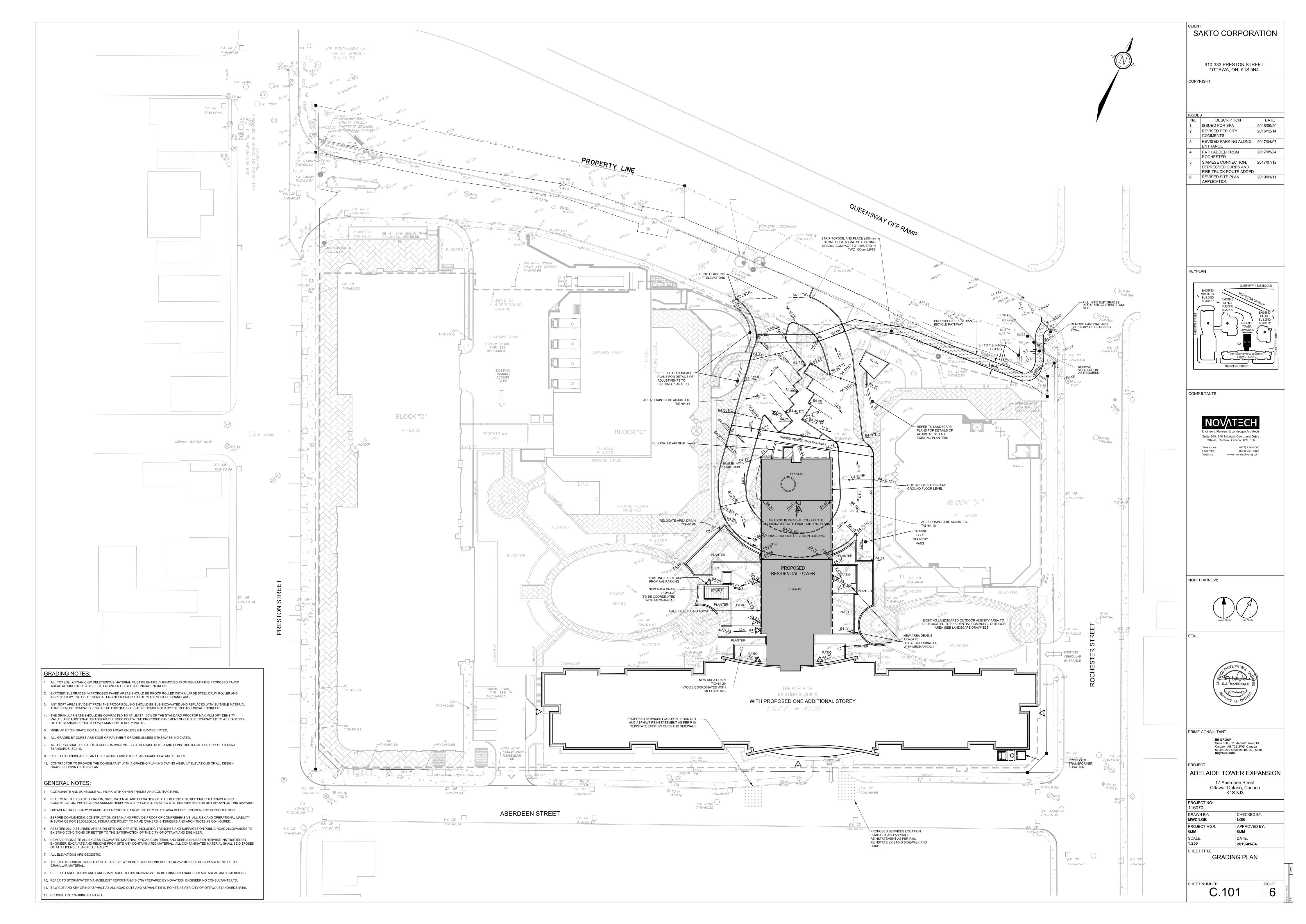


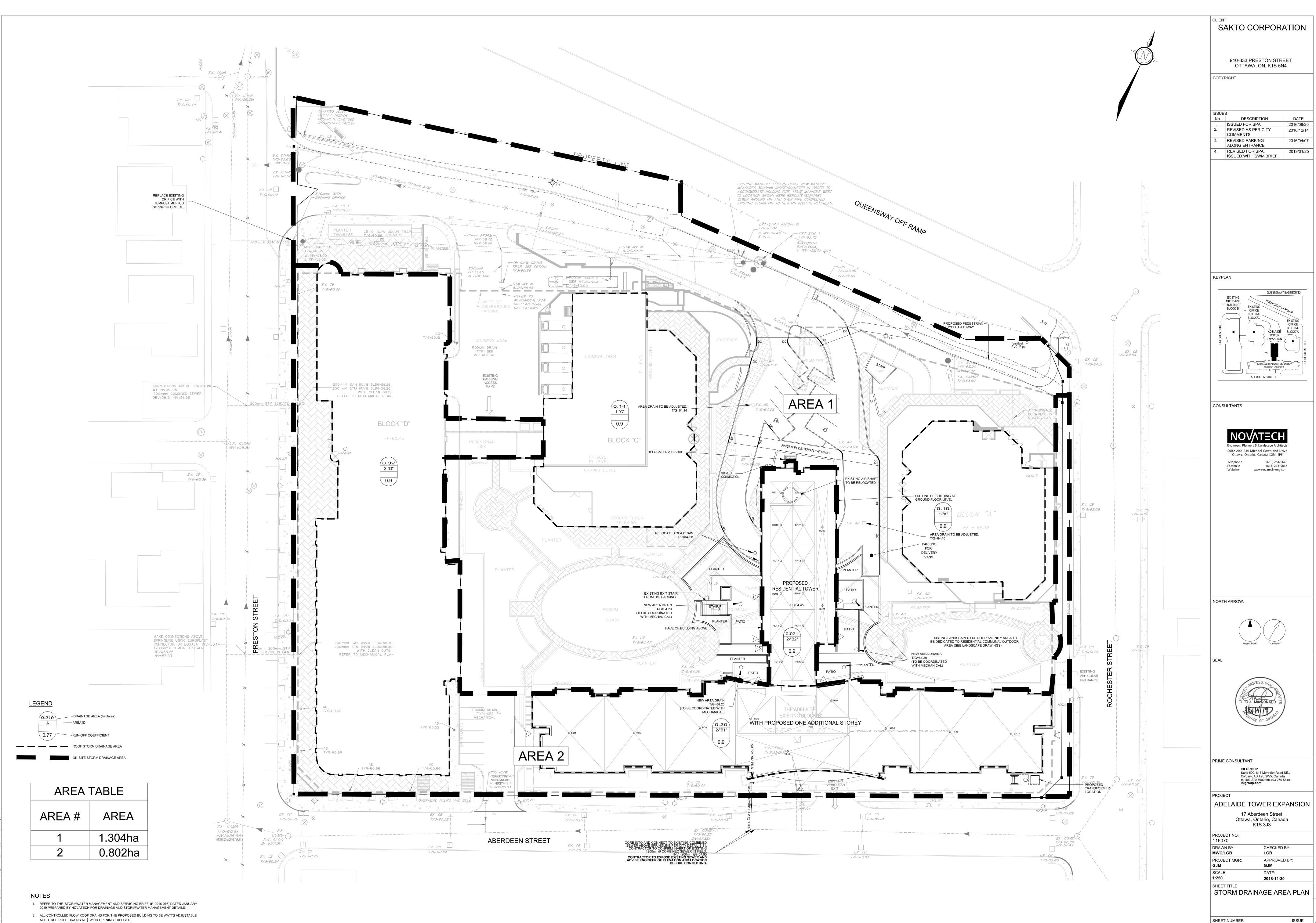


DRAWINGS



10. ROOF DRAINS TO BE WATTS ADJUSTABLE FLOW CONTROL ROOF DRAINS SET AT  $\frac{1}{4}$  WEIR OPENING.





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C.103