

1-19 Sir John A MacDonald Parkway

Transportation Impact Assessment

Type of Document
Final Report

Project Number
OTT-00245595-A0

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Date Submitted
October 28, 2020







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National Capital Commission

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A handwritten signature in black ink, appearing to read "J. Gowrie".

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1. Screening Form

EXP completed a TIA screening form for the proposed re-zoning request for the property and submitted as part of the original Memorandum submitted to the City of Ottawa on April 26, 2019. A copy of the completed screening form is attached to this report as Appendix A.

The National Capital Commission (NCC) is looking to complete a rezoning request for the property to rezone from 'Open Space and Leisure' to 'Residential First Density (R1)'. The 3.7-hectare site located north of Burnside Avenue between Forward Avenue and Slidell Street, is bounded to the north by Sir John A. MacDonald Parkway (SJAM) and to the south by Burnside Avenue. The site location is shown below in **Figure 1**. For the purposes of this rezoning request, the NCC has prepared a concept plan which divides the land into 6 parcels (see draft concept plan in Appendix B). The proposed concept satisfies the Trip Generation Trigger and the Safety Trigger due to the size of the development and the proximity to an existing intersection and we are proceeding with the Scoping Report.



Figure 1 - Site Area

2. Scoping Report

2.1 Proposed Development

The National Capital Commission (NCC) is proposing the rezoning of the existing 3.7-hectare property described above from 'Open Space and Leisure' to Residential First Density (R1). Diplomatic mission is listed as a permitted use in the R1 zone. The concept plan prepared for the purposes of this rezoning request divides the property into 6 parcels with a pathway along the northern edge of the site (along Sir John A. MacDonald Parkway), two pathway connections through the site and 1,596m² of parkland which has been provided at the eastern edge of the site. The concept shows potential access to the local roadway network, parking and entrances and has a total of 206 parking spaces. The size of the building on each parcel is as follows:

Table 1 - Parcel Building Sizes

| Parcel | Gross Floor Area (m ²) |
|--------------|------------------------------------|
| Parcel 1 | 2,430 |
| Parcel 2 | 2,139 |
| Parcel 3 | 2,123 |
| Parcel 4 | 2,360 |
| Parcel 5 | 2,090 |
| Parcel 6 | 2,147 |
| Total | 13,289 |

As the project moves forward, each parcel will need to follow a site plan approval process which may include the preparation of individual Transportation Impact Assessments (TIAs) discussing potential traffic impacts of each site and how each site would align with the City's transportation objectives through adherence to the Transit-Oriented Development goals of the City.

The NCC is undertaking a comprehensive review of the lands along and including Sir John A. MacDonald Parkway as part of their 'Ottawa River South Shore Riverfront Park Plan' which may have an impact on traffic patterns in the area.

2.2 Existing and Proposed Conditions

2.2.1 Existing Conditions

2.2.1.1 Area Road Network

Sir John A. MacDonald Parkway is an east-west, NCC arterial roadway, which extends from Carling Avenue to the west to Portage Avenue to the east. Sir John A. MacDonald Parkway is a four-lane urban divided controlled access roadway with a traffic control signal at the Slidell Street/River Street intersection and an on/off ramps at Parkdale Avenue. The NCC has posted the following turn restrictions at the Slidell Street/River Street intersection:

- SJAM eastbound, right turn restriction – 7:00 to 9:00, 16:00 to 18:00;
- SJAM westbound, right and left turn restrictions, straight only;
- Slidell Street northbound, right and left turn restrictions, straight only; and
- Onigam Street southbound, left turn restriction.

The posted speed limit is 60 km/hr and no commercial vehicles are permitted on the roadway.

Slidell Street is a north-south, City-owned, collector roadway which extends between SJAM to the north to the Burnside Avenue/Bayview Station Road roundabout to the south. Slidell Street has northbound turning restrictions identified above. The Highway Traffic Act restricts speed to 50 km/hr in unposted urban areas.

Onigam Street is a north-south, City-owned, local roadway which extends between the Lemieux Island Water Purification Plant to the north to SJAM to the south. Onigam Street is a two-lane urban local roadway with the turning restrictions (southbound) identified above. The speed limit is assumed to be 50 km/hr in the unposted area.

Bayview Station Road is a north-south, City-owned, collector roadway which extends from Slidell Road/Burnside Avenue to the north to Wellington Street West to the south. Bayview Station Road is a two-lane, urban collector street with on-street parking and auxiliary turning lanes at major intersections. The speed limit is assumed to be 50 km/hr in the unposted area.

Burnside Avenue is an east-west, City-owned, local roadway which extends from Parkdale Avenue to the west to Slidell Street/Bayview Station Road to the east. Burnside Avenue is a two-lane urban local roadway with a signalized intersection at Parkdale Avenue and unsignalized intersections east of Parkdale. The speed limit is assumed to be 50 km/hr in the unposted area.

Hinchey Avenue is a north-south, City-owned, local roadway which extends from a dead-end north of Burnside Avenue to the north to Armstrong Street to the south. Hinchey Avenue is a two-lane urban local roadway with on-street parking on the west side of the street south of Burnside Avenue and on-street parking on the east side of the street north of Burnside Avenue. Hinchey Avenue has unsignalized intersections throughout and speed limit is posted as 40 km/hr.

Forward Avenue is a north-south, City-owned, local roadway which extends from Emmerson Avenue to the north to a dead-end south of Lyndale Avenue to the south. Forward Avenue is a two-lane urban local roadway with on-street parking on the east side of the street and unsignalized intersections throughout. The speed limit is posted as 40 km/hr.

2.2.1.2 Existing Study Area Intersections

From discussion with the City (Appendix C), the following intersections study area delineates the study area for the Screening and Scoping Report:

Sir John A. MacDonald Parkway & Slidell Street / Onigam Street is a signalized four-way intersection. The eastbound approach consists of two through lanes with no left or right turns permitted between 7:00 and 9:00 and 16:00 and 18:00. The westbound approach consists of two through lanes with no left turns permitted and no right turns permitted between 7:00 to 9:00 and 16:00 to 18:00. The northbound approach consists of one through lane with no left or right turns permitted. The southbound approach consists of one through lane with no left turns permitted.

Slidell Street & Burnside Avenue & Bayview Station Road is a one-lane roundabout with exits at each street and designated pedestrian crossings at each street entry/exit.

Scott Street / Albert St & Bayview Station Road is a signalized four-way intersection. The eastbound approach consists of one through lane and one shared bus lane and right turn lane. The westbound approach consists of one through-lane, one auxiliary left-turn lane and one bus lane which is a shared through lane and right turn lane. The northbound approach consists of one through lane, one auxiliary left turn lane and one right turn lane with a yield sign. The southbound approach consists of one through lane and one auxiliary left turn lane. There are cycle lanes provided along the south side of Scott Street on the eastbound approach.

Parkdale Avenue & Burnside Avenue is a three-way signalized intersection. All approaches at this intersection consist of single full-movement lanes. There are no cycle lanes provided.

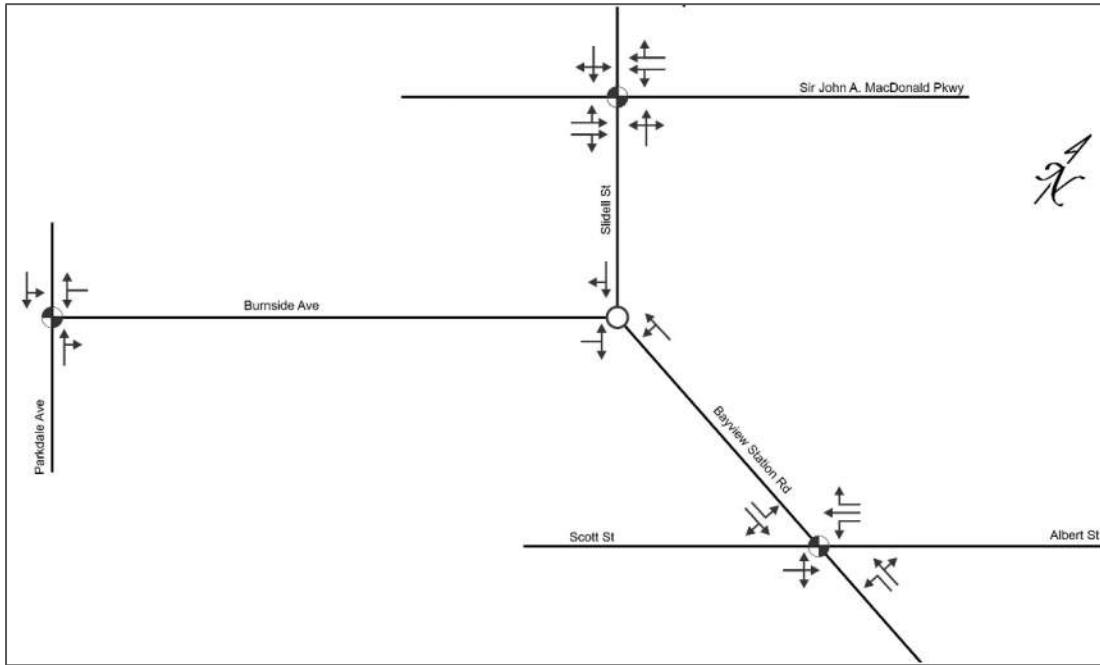


Figure 2 - Study Area Lane Configuration

2.2.1.3 Existing Driveways to Adjacent Developments

There is an existing commercial driveway entrance located approximately 45m to the south of the signalized intersection of SJAM and Slidell Road. This driveway provides access to a large commercial lot for Bayview Yards.

There is an existing apartment driveway/parking lot entrance located on Burnside Avenue approximately 35m west of Stonehurst Avenue. This parking area services the apartment units located between Stonehurst Avenue and Carruthers Avenue on the south side of Burnside Avenue.

There is an existing parking lot and parking lot entrance located approximately 35m to the west of Carruthers Avenue. These parking lots service the surrounding residential properties.

On Burnside Avenue between Hinckley Avenue and Carruthers Avenue there are two driveway accesses to single detached houses, as well as a laneway. On Burnside Avenue between Carruthers Avenue and Stonehurst Avenue there is a driveway access to an apartment building's garage and a laneway.

There is an existing parking garage entrance to the apartment building located at 100 Hinckley Avenue located approximately 50m to the north of Burnside Avenue on Hinckley Avenue.

2.2.1.4 Pedestrian/Cycling Network

With respect to pedestrian traffic, sidewalks in the vicinity of the proposed development will need to be constructed to connect the proposed development to the existing pedestrian walkways.

With respect to cyclists, according to the City of Ottawa Cycling Plan, both SJAM and Scott Street/Albert Street are considered major pathways with Scott Street/Albert Street also classified as a "Spine" cycling route and "Cross-town" cycling route. Slidell Street, Burnside Avenue, Bayview Station Road and Parkdale Avenue north of Burnside Road are considered "local" cycling routes.

The Ottawa River Pathway is a major multi use trail. It runs along the north side of Sir John A MacDonald Parkway and is within the study area. The safest connection point to the pathway is either via the connection on Parkdale Avenue or the crossing at Onigam Street. The pathway is a part of the larger network maintained by the National Capital Commission, as well as a part of the Trans Canada Trail.

A multi-use pathway runs along the north side of Scott Street within the study area. At the intersection of Bayview Station Road and Scott Street/Albert Street, the pathway splits in two and exists on both sides of Albert Street until Bayview Station, where it resumes to follow the north side of Albert Street.

Connections to these pedestrian/cycling networks will need to be examined as part of the pre-consultation process for the individual site plan applications for each parcel.

2.2.1.5 Transit Network

A map of the nearby bus routes and light rail stations is shown in **Figure 3**. The closest bus stop is located at Parkdale Avenue and Burnside Avenue, serviced by a single bus route.

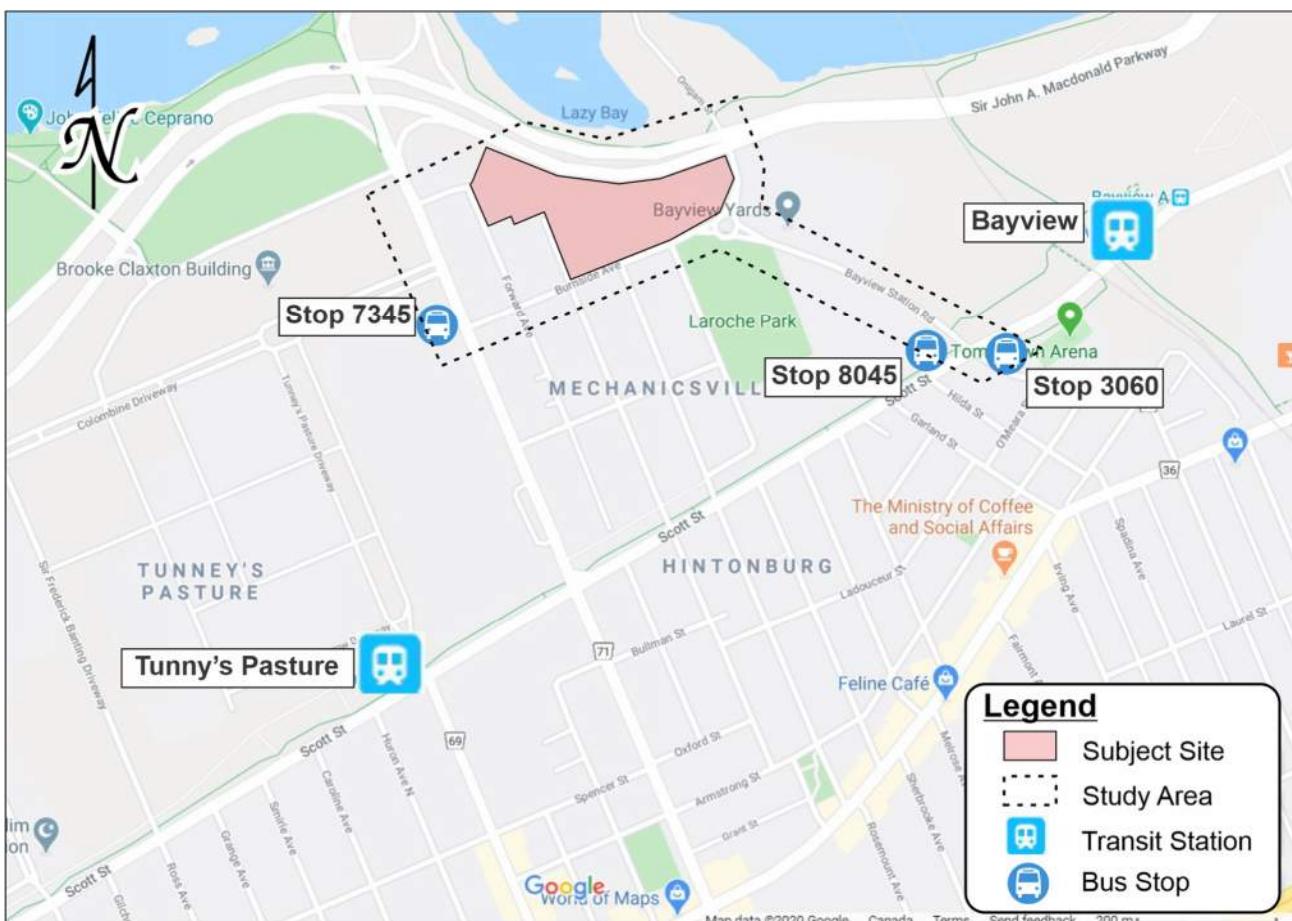


Figure 3 - Transit Network

A description of each transit stop is provided in **Table 2**.

Table 2 Transit Stop Descriptions

| Stop Location | Distance from Subject Site (Approx.) | Amenities | Direction | OC Transpo Route |
|---------------------------------|--------------------------------------|-------------------|-----------------------|------------------|
| Parkdale / Burnside (7345) | 200 m | Bus Shelter Bench | Southbound | 54 |
| Tom Brown Arena (8045) | 450 m | Bus Shelter Bench | Westbound | 16 |
| | | | | 57 |
| | | | | 61 |
| | | | | 75 |
| Bayview B (3060) | 525 m | Bus Shelter | Eastbound | 16 |
| | | | | 57 |
| | | | | 61 |
| | | | | 63 |
| | | | | 66 |
| | | | | 75 |
| Tunney's Pasture Station (3011) | 850 m | Transit Station | Eastbound / Westbound | Route 1 O-Train |
| | | | | 50 Bus Routes |
| Bayview | 650 m | Transit Station | Eastbound / Westbound | Route 1 O-Train |
| | | | | Route 2 O-Train |

An overview of the transit routes within the study area:

Route 1 O-Train Tunney's Pasture – Blair: The O-Train operating in exclusive right-of-way from Tunney's Pasture to Blair Station via Downtown Ottawa with peak headways of approximately 4 minutes and off-peak headways of 5 to 8 minutes and 15 minutes after 23:00. The O-Train operates from 05:00 to 01:00 during the week.

Route 2 O-Train Bayview – Greenboro: The O-Train is currently being served by a bus due to construction but serves all stations along Route 2. This route is currently operating on headways of approximately 12 minutes until 21:00 and then operates on headways of 15 minutes. Route 2 operates from 05:35 to approximately 24:00 during the week.

Route 16 Main – Tunney's Pasture/Westboro: The bus route operates along Scott Street through the study area, between Main Street outside Saint Paul University and Tunney's Pasture transit station. The route extends west of Tunney's Pasture transit station to Westboro at Churchill Avenue and Scott Street between Monday and Saturday. The route has headways of 30 minutes. Route 16 operates from 06:10 to 24:00 during the week.

Route 54 Tunney's Pasture: The bus route operates on Parkdale Avenue and Scott Street through the study area, looping around the adjacent neighborhood clockwise, starting and ending at Tunney's Pasture transit station. The route has headways of 30 minutes, between 07:00 and 22:40 during the week.

Route 57 Tunney's Pasture & N Rideau – Bell's Corners: The bus route operates along Scott Street through the study area. The route operates between Tunney's Pasture transit station and Bell's Corners in western Ottawa. Overnight, the route extends east of Tunney's Pasture to Rideau Station to compensate for the lack of O Train service. The route has headways of 15 minutes and operates between 04:50 and 03:30 during the week.

Route 61 Tunney's Pasture & N Rideau & Gatineau – Stittsville: The bus route operates along Scott Street through the study area. The route operates between Tunney's Pasture transit station and Stittsville in western Ottawa. During peak hours, the route extends north to Gatineau. Overnight, the route extends east of Tunney's Pasture to Rideau Station to compensate for the

lack of O Train service. The route has headways of approximately 9 minutes during peak hours and 15 minutes outside of peak hours. The route operates between 03:50 and 03:30 during the week.

Route 63 Briarbrook – Tunney's Pasture: The bus route operates along Scott Street through the study area. The route operates between Tunney's Pasture transit station and Carp in northwestern Ottawa. During peak hours, the route extends north to Gatineau. The route has headways of approximately 15 minutes during peak hours and 30 minutes outside of peak hours. The route operates between 05:10 and 00:50 during the week.

Route 66 Kanata-Solandt – Tunney's Pasture: The bus route operates along Scott Street through the study area. The route operates between Kanata and Tunney's Pasture with some trips extending to Gatineau. During the morning, the route operates westbound towards Kanata. During the afternoon, the route operates eastbound to Tunney's Pasture and Gatineau. The route has headways of approximately 15 minutes. The route operates between 05:30 and 09:50, 14:20 and 20:00 during the week.

Route 75 Tunney's Pasture & N Rideau & Gatineau – Barrhaven Centre: The bus route operates along Scott Street through the study area. The route operates between Tunney's Pasture transit station and the Minto Recreation Complex in Barrhaven. During peak hours, the route extends north to Gatineau. Overnight, the route extends east of Tunney's Pasture to Rideau Station to compensate for the lack of O Train service. The route has headways of approximately 8 minutes. The route operates a full 24 hours during the week.

2.2.1.6 Existing Area Traffic Management Measures

The existing traffic control measures for each of the boundary streets are as follows:

Sir John A. MacDonald Parkway

- Divided Roadway
- Traffic signal at Slidell Street/Onigam Street
- Turning Movement Restrictions at Slidell Street/Onigam Street
 - EB Vehicles cannot turn left or right in either direction (7:00-9:00, 16:00-18:00).
 - WB Vehicles cannot turn left, or right (7:00-9:00, 16:00-18:00).
- Pedestrian and Cycling pathways nearby and fully separated.

Burnside Avenue

- 40 km/h roadway
- Roundabout with Full Pedestrian Crossings at Slidell Street and Bayview Station Road
- Traffic signal at Parkdale Avenue
- Median flex stakes indicating posted speed
- Speed board between Hincheny Avenue and Carruthers Avenue
- On street parking
- Sidewalk (South)

Slidell Street

- Roundabout with Full Pedestrian Crossings at Burnside Avenue and Bayview Station Road
- Traffic signal at Sir John A. MacDonald Parkway
- Turning Movement Restrictions at Slidell Street/Onigam Street
 - Vehicles cannot turn left or right in either direction on Slidell Street;
 - Vehicles cannot turn left on Onigam Street.
- Sidewalk (West)

Hincheny Avenue

- 40 km/h roadway
- Stop controlled at Burnside Avenue
- On street parking

Sidewalk (West)

Forward Avenue

- 40 km/h roadway
- Stop controlled at Burnside Avenue
- On street parking
- Sidewalk (East and West)

2.2.1.7 Peak Hour Travel Demands

Traffic volumes and signal timings were collected from the City of Ottawa in preparation of the study. The information is provided in **Appendix D**.

As the traffic counts were conducted at different times and in different years, a uniform growth rate was applied to each intersection. An annual growth rate of 2.0% was applied to each intersection not counted within 2020 to grow to a uniform 2020 existing traffic horizon.

Additionally, the Scott Street/Albert Street / Bayview Station Road intersection count was conducted in September 2016 and included bus volumes from the Transitway detour. These buses were removed from the 2020 horizon by reducing the number of heavy vehicles through the intersection.

Typically, the weekday morning and afternoon peak hours on adjacent streets will constitute the “worst case” of the combination of development-generated and background traffic. The time periods for analysis should be confirmed by the City as part of the pre-consultation process for the development of the site plans for each parcel.

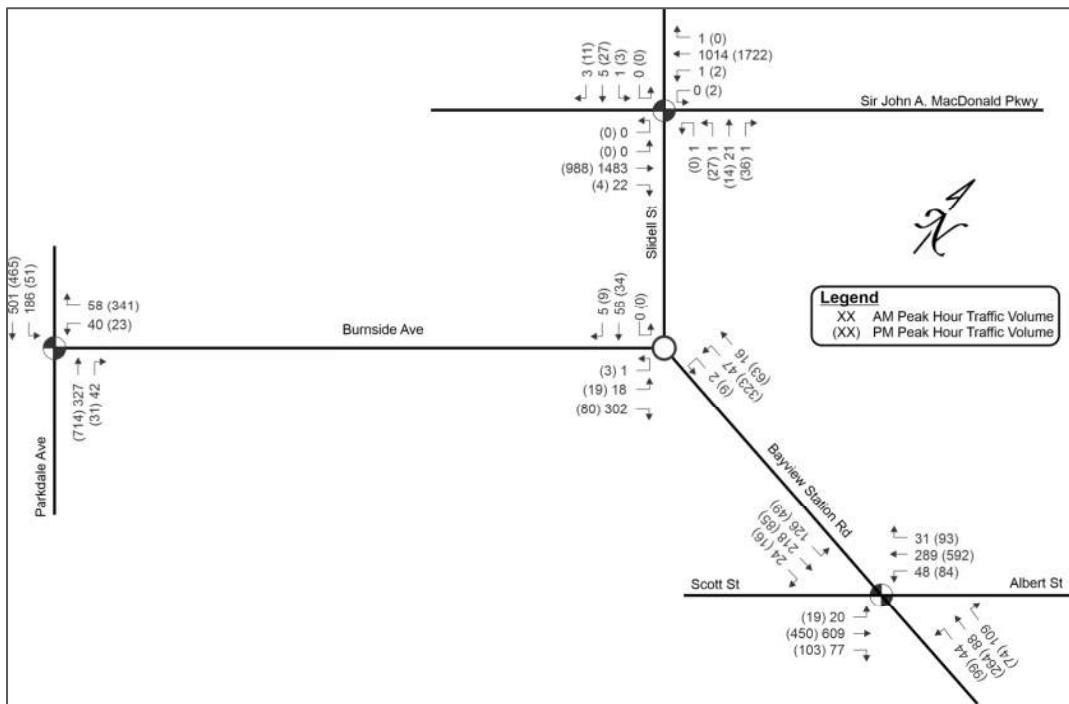


Figure 4 - Existing (2020) Volumes

The existing traffic operations were assessed using Synchro software and the results provided in **Appendix E** summarized in **Table 3**. Critical movements are determined based on the MMLOS Guidelines, wherein movements are deemed critical if the LOS is equal to E or worse. Overall intersection LOS is based on the v/c threshold as per the MMLOS Guidelines.

Table 3 - Existing (2020) Traffic Operations Analysis

| Intersection | Weekday AM Peak (PM Peak) | | | | | |
|---|---------------------------|-------------|----------|-------------|---------------|-------|
| | Critical Movement(s) | | | Overall | | |
| | LoS | v/c | Movement | Delay (s) | v/c | LOS |
| Signalized | | | | | | |
| Parkdale Ave & Burnside Ave | - | - | - | 12.1 (19.2) | 0.68 (0.74) | B (C) |
| Sir John A MacDonald Parkway & Slidell St / Onigam St | - | - | - | 5.7 (9.2) | 0.59 (0.72) | A (C) |
| Scott St / Albert St & Bayview Station Rd | E (E) | 0.88 (0.72) | SBL | 30.5 (26.7) | 0.89 (0.81) | D (D) |
| Unsignalized | | | | | | |
| Burnside Ave & Slidell St & Bayview Station Rd | - | - | - | 3.6 (5.8) | 0.260 (0.335) | A (A) |

2.2.1.8 Existing Road Safety Conditions

Collision history for the study area intersections (2014-2018, inclusive) was obtained from the City of Ottawa. Refer to **Appendix I** for the collision diagrams and details report. The City requires a safety review to be conducted if at least four (4) collisions have occurred for any one movement or of a discernible pattern over a five (5) year period. A review of the boundary streets' historical collision records indicates collisions at the following intersections include:

- **Bayview Road & Scott Street / Albert Street** – a total of twenty-nine (29) collisions were recorded. The impact types were five (5 or 17%) angled, seven (7 or 24%) rear-end, two (2 or 7%) sideswipe, thirteen (13 or 45%) turning movement and two (2 or 7%) single vehicle. Nine (9 or 31%) collisions were classified as non-fatal, all others were property damage only.
- **Bayview Road & Burnside Avenue & Slidell Street** – a total of five (5) collisions were recorded. The impact types were two (2 or 40%) angled, two (2 or 40%) sideswipe, one (1 or 20%) single vehicle. Three (3 or 67%) collisions are classified as non-fatal, all others were property damage only.
- **Sir John A MacDonald Pkwy & Slidell St / Onigam St** – a total of eighteen (18) collisions were recorded. The impact types were six (6 or 33%) angled, nine (9 or 50%) rear end, one (1 or 6%) turning movement and two (2 or 11%) single vehicle. Two collisions (2 or 11%) resulted in a fatal injury, another two resulted in a non-fatal injury and three (3 or 17%) were non-reportable.
- **Parkdale Avenue & Burnside Avenue** – a total of two (2) collisions were recorded. The impact types were one (1 or 50%) rear end and one turning movement. Both collisions were property damage only.

2.2.2 Planning Conditions

2.2.2.1 Planned Study Area Transportation Network

The Ottawa River South Shore Riverfront Park Plan proposes improvements of the at-grade crossing at Slidell Street in addition to the reconfiguration of the Parkdale on-ramp. As these improvements are conceptual, they will need to be re-evaluated as part of the pre-consultation for the site plan applications of the individual parcels.

With the completion of the LRT to Tunney's Pasture, Scott Street and Albert Street will be reconfigured through the study area. The bus lane along Scott Street and Albert Street will be removed and replaced with hatched pavement, provided greater separation between the vehicle and cycling lanes. Functionally, the geometrics of the road will be the same for vehicular traffic.

2.2.2.2 Other Area Development

Several developments have been identified within the surrounding area. The list below outlines their location, purpose, buildout year and number of trips.

- **111, 115, 121 Parkdale Avenue and 51 Burnside Avenue:** A 32-storey residential building, containing 218 condominium units, and 450m² of retail space. Based on the traffic impact assessment prepared by Stantec in 2012, the build-out year is slated for 2020. The TIA added 67 AM vehicular trips and 78 PM vehicular trips to the network.
- **99 Parkdale Avenue:** A 28-storey residential building, containing 238 condominium units. Based on the traffic impact assessment prepared by J.L. Richards & Associates in 2019, the build out year is slated for 2023. The TIA added 36 AM vehicular trips and 29 PM vehicular trips to the network.
- **175 Carruthers Avenue:** A 18-storey residential building containing 187 apartment units, and a 3.5-storey residential building containing 12 units. Based on the traffic impact brief addendum prepared by Parsons in 2017, a build out year has not been provided, but is assumed to be completed by 2023. The traffic impact brief added 59 AM vehicular trips and 69 PM vehicular trips to the network.
- **900 Albert Street:** A mixed use development, containing 1241 residential units, 8124m² of retail space and 37745m² of office space. Based on the traffic impact assessment addendum prepared by Parsons in 2020, the build out year is slated for 2025. The TIA added 398 AM vehicular trips and 613 PM vehicular trips to the network. Trips routed on the north leg of Bayview Station Road at Scott Street/Albert Street are assumed to be assuming the Sir John A MacDonald Parkway, and are routed along Burnside Avenue as well.

2.3 Study Area

The proposed study area is as outlined below, illustrated in **Figure 5** and as highlighted in Section 2.2.1 of this report:

- Sir John A. MacDonald Parkway/Slidell Street;
- Slidell Street/Burnside Avenue/Bayview Station Road (roundabout);
- Scott Street/Bayview Station Road;
- Parkdale Avenue/Burnside Avenue; and
- All boundary streets surrounding the proposed development including Slidell Street, Burnside Avenue, Hinckley Avenue, Forward Avenue and the Sir John A. MacDonald Parkway.



Figure 5 - Study Area

2.4 Time Periods

It is proposed that the residential development will generate peak traffic volumes during the weekday in the AM and PM peak periods.

2.5 Horizon Years

Based upon the anticipated size of the proposed development, it is anticipated both of the horizon periods (full occupancy and 5 years following full occupancy) will be required for analysis. The full occupancy of the development is anticipated for 2023. Therefore, the horizon years are for 2023 and 2028.

2.6 Exemptions Review

Based upon Table 4 in the City of Ottawa TIA Guidelines, the following exemptions apply to the proposed development:

- Modules 4.1.2 'Circulation and Access' – The module is only required for site plans; and
- Modules 4.2 'Parking' – The module is only required for site plans; and

3. Forecasting

3.1 Proposed Development

3.1.1 Development-Generated Travel Demand

Trip generation for the proposed development was derived from ITE Trip Generation Manual 10th Edition. The land use used for is Government Office Building (ITE #730). In occurrence with City of Ottawa standards, person trips were determined by multiplying the ITE trips by 1.28. The breakdown of trip generation is provided in **Table 4**.

Table 4 - Trip Generation

| Land Use | Parcel | Independent Variable | Parameters | AM Peak Hour | | PM Peak Hour | | | | | |
|---------------------------------------|-----------------------|----------------------|------------|------------------------------|-----|------------------------------|-----|--|--|--|--|
| | | | | In | Out | In | Out | | | | |
| Scenario | | | | Peak Hour of Adjacent Street | | Peak Hour of Adjacent Street | | | | | |
| Rate / Eq. | | | | 3.34 | | 1.71 | | | | | |
| Distribution | | | | 75% | 25% | 25% | 75% | | | | |
| Government Office Building (ITE #730) | 1 26156 sq. ft GFA | ITE Trips | | 87 | | 45 | | | | | |
| | | Person Trips (1.28) | | 112 | | 57 | | | | | |
| | | Distributed Trips | | 84 | 28 | 14 | 43 | | | | |
| | 2 23024 sq. ft GFA | ITE Trips | | 77 | | 39 | | | | | |
| | | Person Trips (1.28) | | 98 | | 50 | | | | | |
| | | Distributed Trips | | 74 | 24 | 13 | 38 | | | | |
| | 3 22852 sq. ft GFA | ITE Trips | | 76 | | 39 | | | | | |
| | | Person Trips (1.28) | | 98 | | 50 | | | | | |
| | | Distributed Trips | | 74 | 24 | 13 | 38 | | | | |
| | 4 25403 sq. ft GFA | ITE Trips | | 85 | | 43 | | | | | |
| | | Person Trips (1.28) | | 109 | | 56 | | | | | |
| | | Distributed Trips | | 82 | 27 | 14 | 42 | | | | |
| | 5 22497 sq. ft GFA | ITE Trips | | 75 | | 38 | | | | | |
| | | Person Trips (1.28) | | 96 | | 49 | | | | | |
| | | Distributed Trips | | 72 | 24 | 12 | 37 | | | | |
| | 6 23110 sq. ft GFA | ITE Trips | | 77 | | 40 | | | | | |
| | | Person Trips (1.28) | | 99 | | 51 | | | | | |
| | | Distributed Trips | | 74 | 25 | 13 | 38 | | | | |
| TOTAL NEW PERSON TRIPS | | | | 612 | | 313 | | | | | |
| | | | | 460 | 152 | 79 | 236 | | | | |

The proposed development is expected to generate 612 two-way person trips during the AM peak, and 313 two-way person trips during the PM peak.

3.1.2 Mode Share

The proposed development is located within the Ottawa West neighbourhood and its existing and proposed modal split for the development is provided in **Table 5**. The information source, from the 2011 Origin-Destination Survey by Trans Committee, is included as **Appendix F**.

Table 5 – Existing and Travel Mode Proportions

| Mode | AM Peak Hour | | | | | PM Peak Hour | | |
|----------------|---------------|-----------------|-------|------------|-------------|-----------------|-------|------------|
| | From District | Within District | Total | Proportion | To District | Within District | Total | Proportion |
| Auto Driver | 53530 | 22130 | 75660 | 49% | 53730 | 22130 | 75860 | 50% |
| Auto Passenger | 14560 | 6300 | 20860 | 14% | 14560 | 6300 | 20860 | 14% |
| Transit | 18670 | 2810 | 21480 | 14% | 18820 | 2810 | 21630 | 14% |
| Bicycle | 3120 | 3110 | 6230 | 4% | 3140 | 3110 | 6250 | 4% |
| Walk | 2780 | 21610 | 24390 | 16% | 2750 | 21610 | 24360 | 16% |
| Other | 2340 | 1910 | 4250 | 3% | 2430 | 1910 | 4340 | 3% |

The modal split for the development is expected to change based on the targets in the City's Transportation Master Plan. These modal split targets at associated trip generation are provided in **Table 6**.

Table 6 - Development Trips Targeted Modal Split

| Travel Mode | Proportion | AM Peak Hour | | PM Peak Hour | |
|----------------|------------|--------------|-----|--------------|-----|
| | | In | Out | In | Out |
| Auto Driver | 46% | 211 | 68 | 36 | 109 |
| Auto Passenger | 9% | 41 | 14 | 7 | 21 |
| Transit | 26% | 120 | 40 | 21 | 61 |
| Bicycle | 5% | 23 | 8 | 4 | 12 |
| Walk | 11% | 51 | 17 | 9 | 26 |
| Other | 3% | 14 | 5 | 2 | 7 |

The proposed development will add an estimated 318 new two-way automobile trips during the AM peak, and 164 new two-way automobile trips during the PM peak.

3.1.3 Trip Distribution

Trip distribution was devised by determining the proportions of the original TMC volumes. A uniform proportion was determined by totaling the entries and exits from each study area access point for both peak hours. **Table 7** outlines the proportions for each access point, as well as the total trips entering and exiting.

Table 7 - Trip Distribution

| Access Point | Proportion | AM Peak Hour | | PM Peak Hour | |
|-----------------------------------|------------|--------------|-----|--------------|-----|
| | | In | Out | In | Out |
| West on Sir John A MacDonald Pkwy | 28% | 61 | 18 | 12 | 31 |
| East on Sir John A MacDonald Pkwy | 28% | 58 | 18 | 12 | 31 |
| South on Parkdale | 12% | 24 | 6 | 0 | 12 |
| West on Scott | 12% | 27 | 8 | 6 | 13 |
| East on Scott | 13% | 30 | 12 | 6 | 14 |
| South on Bayview Station | 7% | 14 | 6 | 0 | 6 |

3.1.4 Trip Assignment

Trips were assigned to each of the planned parcel buildings, based on the person trips provided in **Table 4**. Trip distribution was assumed to be uniform across all parcels. **Figure 6** illustrates the trip assignment for the total development. The breakdown of the calculations for determining trip distribution is provided in **Appendix G**.

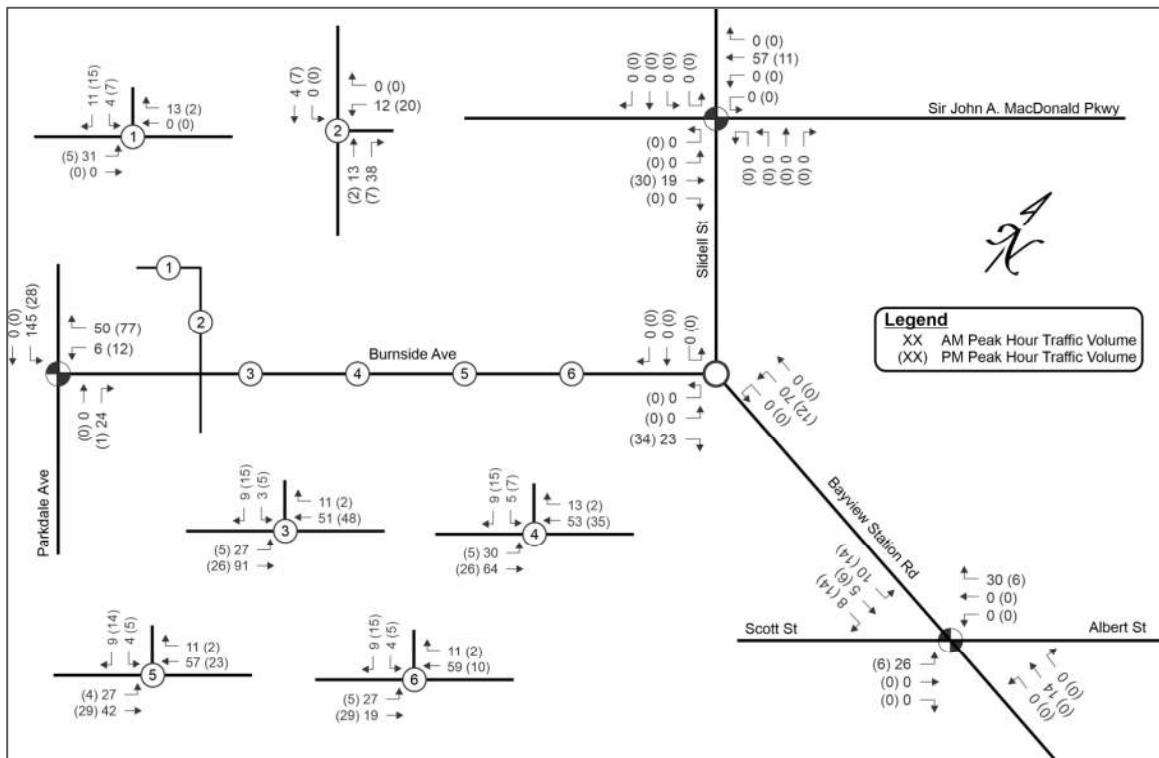


Figure 6 - Site Trip Assignment

3.2 Background Network Travel Demands

3.2.1 Transportation Network Plans

The City of Ottawa Transportation Master Plan consulted to determine the road network changes in the study area. No changes are proposed in the study area within the horizon years.

The Ottawa River South Shore Riverfront Park Plan was also consulted to determine changes to the study area. While improvements to the Parkdale Avenue interchange and Slidell Street intersection on Sir John A MacDonald Parkway are proposed, all plans are currently conceptual, and implementation is likely beyond the study horizon years.

3.2.2 Background Traffic Growth

Background growth was estimated using a 2.0% annual vehicular growth rate.

3.2.3 Other Developments

As outlined in Section 2.2.2.2, four other developments have been identified within the study area.

The trips from 111 Parkdale Avenue, 99 Parkdale Avenue and 175 Carruthers Avenue have been included in both 2023 and 2028 background conditions. The trips from 900 Albert Street have been included in the 2028 background conditions.

3.3 Demand Rationalization

3.3.1 Future Background (2023) Traffic

The future background traffic volumes for 2023 are provided in **Figure 7**.

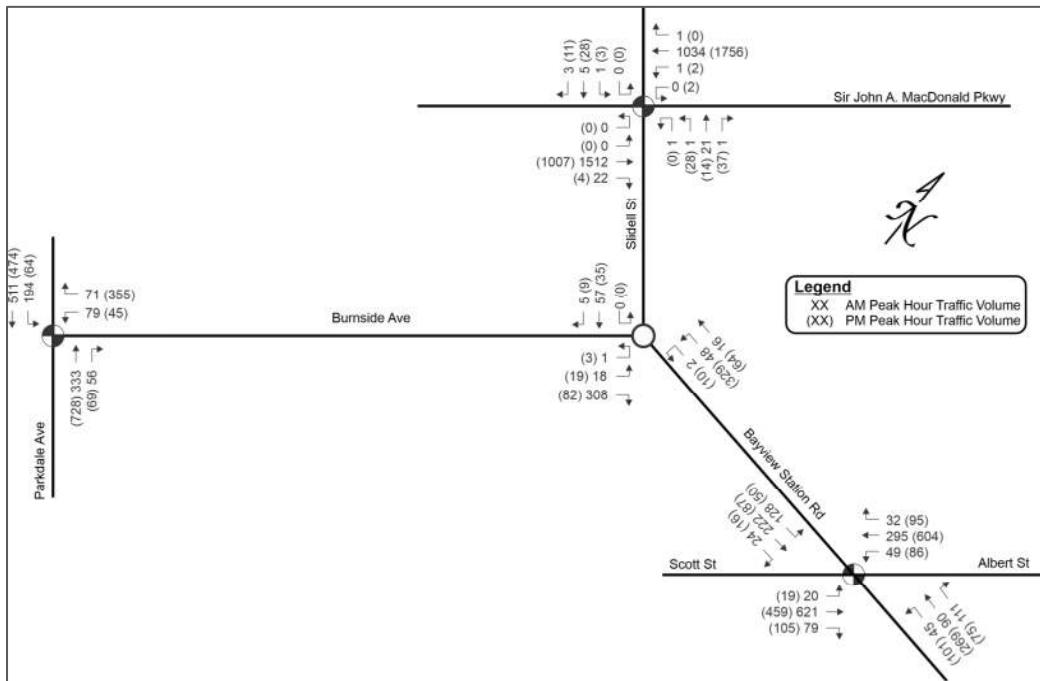


Figure 7 - Future Background (2023) Traffic Volumes

The future background traffic operations analysis for 2023 is provided as **Table 8**. Full outputs are provided in **Appendix H**.

Table 8 - Future Background (2023) Traffic Operations Analysis

| Intersection | Weekday AM Peak (PM Peak) | | | | | |
|---|---------------------------|------|----------|-------------|---------------|-------|
| | Critical Movement(s) | | | Overall | | |
| | LoS | v/c | Movement | Delay (s) | v/c | LOS |
| Signalized | | | | | | |
| Parkdale Ave & Burnside Ave | - | - | - | 11.9 (16.0) | 0.69 (0.67) | B (B) |
| Sir John A MacDonald Parkway & Slidell St / Onigam St | - | - | - | 5.4 (7.8) | 0.56 (0.64) | A (B) |
| Scott St / Albert St & Bayview Station Rd | E | 0.83 | SBL | 27.5 (21.9) | 0.85 (0.70) | D (B) |
| Unsignalized | | | | | | |
| Burnside Ave & Slidell St & Bayview Station Rd | - | - | - | 3.6 (5.9) | 0.276 (0.356) | A (A) |

3.3.2 Future Background (2028) Traffic

The future background traffic volumes for 2028 are provided in **Figure 8**.

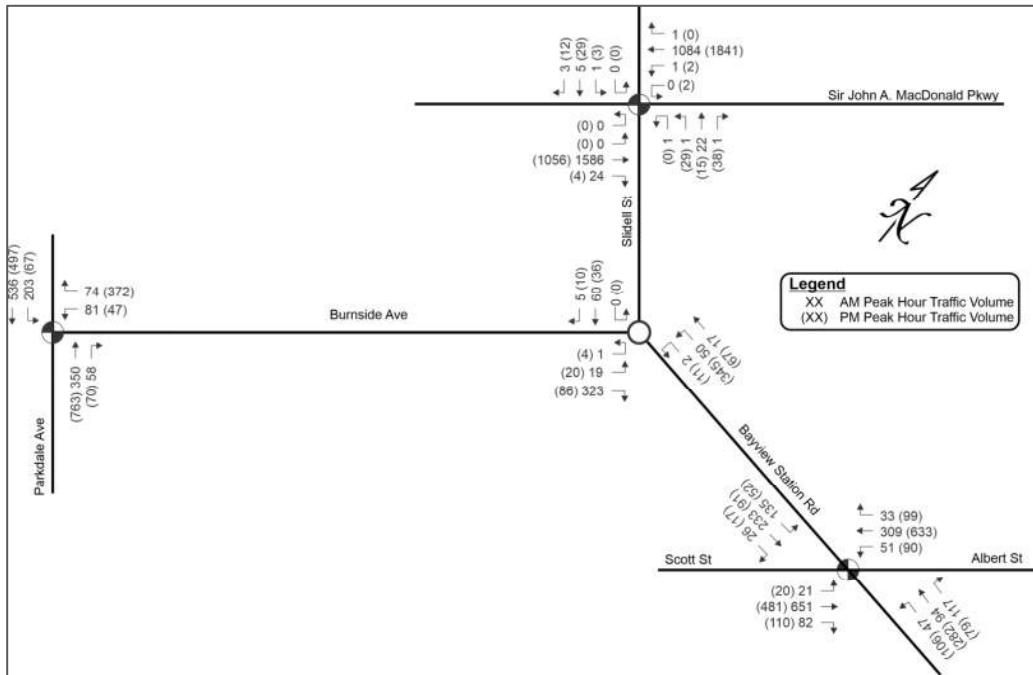


Figure 8 - Future Background (2028) Traffic Volumes

The future background traffic operations analysis for 2028 is provided as **Table 9**. Full outputs are provided in **Appendix H**.

Table 9 - Future Background (2028) Traffic Operations Analysis

| Intersection | Weekday AM Peak (PM Peak) | | | | | |
|---|---------------------------|-------------|----------|--------------|---------------|-------|
| | Critical Movement(s) | | | Overall | | |
| | LoS | v/c | Movement | Delay (s) | v/c | LOS |
| Signalized | | | | | | |
| Parkdale Ave & Burnside Ave | (E) | (0.99) | WBLR | 32.0 (101.5) | 0.86 (1.32) | D (F) |
| | (F) | (1.49) | SBLT | | | |
| Sir John A MacDonald Parkway & Slidell St / Onigam St | - | - | - | 6.1 (10.4) | 0.62 (0.77) | B (C) |
| Scott St / Albert St & Bayview Station Rd | F | 1.15 | EBLTR | 61.8 (50.0) | 1.09 (1.01) | F (F) |
| | (E) | (1.03) | WBT | | | |
| | F (F) | 0.98 (0.99) | SBL | | | |
| Unsignalized | | | | | | |
| Burnside Ave & Slidell St & Bayview Station Rd | - | - | - | 3.6 (5.9) | 0.324 (0.420) | A (A) |

Based on our analysis of future background conditions, there are several critical movements at the Parkdale Avenue & Burnside Avenue, Sir John A MacDonald Parkway & Slidell Street / Onigam Street, and Scott Street / Albert Street & Bayview Station Road intersection, which will require transportation demand rationalization for each site plan application.

4. Analysis

4.1 Development Design

Each parcel will contain a single driveway access point. Parcel 1 will be accessed from a proposed extension of Hinchey Avenue, just east of Forward Avenue where the road extension will connect to. Parcel 2 will be accessed from Hinchey Avenue, along the existing roadway. Parcel 3 will be accessed from Burnside Avenue between Hinchey Avenue and Carruthers Avenue. Parcel 4 will be accessed from Burnside Avenue, offset from the pre-existing intersection with Carruthers Avenue. Parcel 5 will be accessed from Burnside Avenue between Carruthers Avenue and Stonehurst Avenue. Parcel 6 will be accessed from Burnside Avenue between Stonehurst Avenue and Bayview Station Road. No parcels will interconnect.

Site plans for each parcel are still to be developed, however, each parcel will have a direct pedestrian connection to the public road network. Additionally, the developer of each parcel will install a new municipal sidewalk along the frontage of their parcel at the time of construction at the following locations:

- Along the east side of Hinchey Avenue north of Burnside Avenue;
- Along the north side of Burnside Avenue between Hinchey Avenue and;
- Along the west side of Slidell Street between Burnside Avenue / Bayview Road and Sir John A. Macdonald.

Additionally, pedestrian connections are to be provided between Hinchey Avenue and Sir John A. Macdonald Parkway and between Carruthers Avenue and Sir John A. Macdonald Parkway.

The proposed sidewalk location is illustrated in **Figure 9**.



Figure 9 Proposed Sidewalk Locations

4.2 Parking

All parcels will have a separate parking area. According to Schedule 1A in the City of Ottawa Zoning By-Law, the development is situated in "Area Z". This zone designates areas where off-street vehicle parking does not have any provisions. Therefore, no minimum space requirements apply to the development. However, parking will be reviewed for each site at the time of application.

4.3 Boundary Streets

The boundary streets for the development are Parkdale Avenue, Burnside Avenue, Slidell Street and Sir John A MacDonald Parkway. The proposed development will not change the configuration of boundary street roads. The Multimodal Level of Service for the boundary roads segments are summarized in Section 4.9.2. The truck level of service (TkLOS) analysis is included only for Sir John A MacDonald Parkway as it is the only boundary road that is classified as an arterial road. The target levels of service for pedestrians, cyclists, transit and trucks are determined as per the minimum desirable MMLOS targets by the City of Ottawa's Official Plan designation/policy area.

4.4 Access Intersections

Accesses for each parcel will be designed to City of Ottawa standards at the time of site plan application.

4.5 Transportation Demand Management

The proposed development is expected to have a non-auto modal split of 34%, due to the nature of the development and availability of transit and other facilities. The development will coincide with pedestrian improvements to the north side of Burnside Avenue, with the addition of new sidewalks along the developments border. A multi-use path is planned to be implemented along Sir John A MacDonald Parkway along the development. Connections will be established between Parcels 1 and 2 on Hinchey Avenue, and between Parcels 3 and 4 on Burnside Avenue.

4.6 Neighborhood Traffic Management

No road modifications are necessary for existing neighborhood roads to accommodate the development traffic. However, Hinchey Avenue will be connected with Forward Avenue.

Additionally, sidewalks are recommended at the following locations:

- Along the east side of Hinchey Avenue north of Burnside Avenue;
- Along the north side of Burnside Avenue between Hinchey Avenue and;
- Along the west side of Slidell Street between Burnside Avenue / Bayview Road and Sir John A. Macdonald.

4.7 Transit

The development is not expected to necessitate any increase in transit requirements within the area.

4.8 Network Concept

One change to the road network will be implemented as a result of the development – the extension of Hinchey Avenue to connect with Forward Avenue. This road extension is not expected to have a major impact on the rest of the network.

4.9 Network Intersections

4.9.1 Vehicular Level of Service

4.9.1.1 Future Total (2023) Traffic

The future total traffic volumes for 2023 are provided in **Figure 9**.

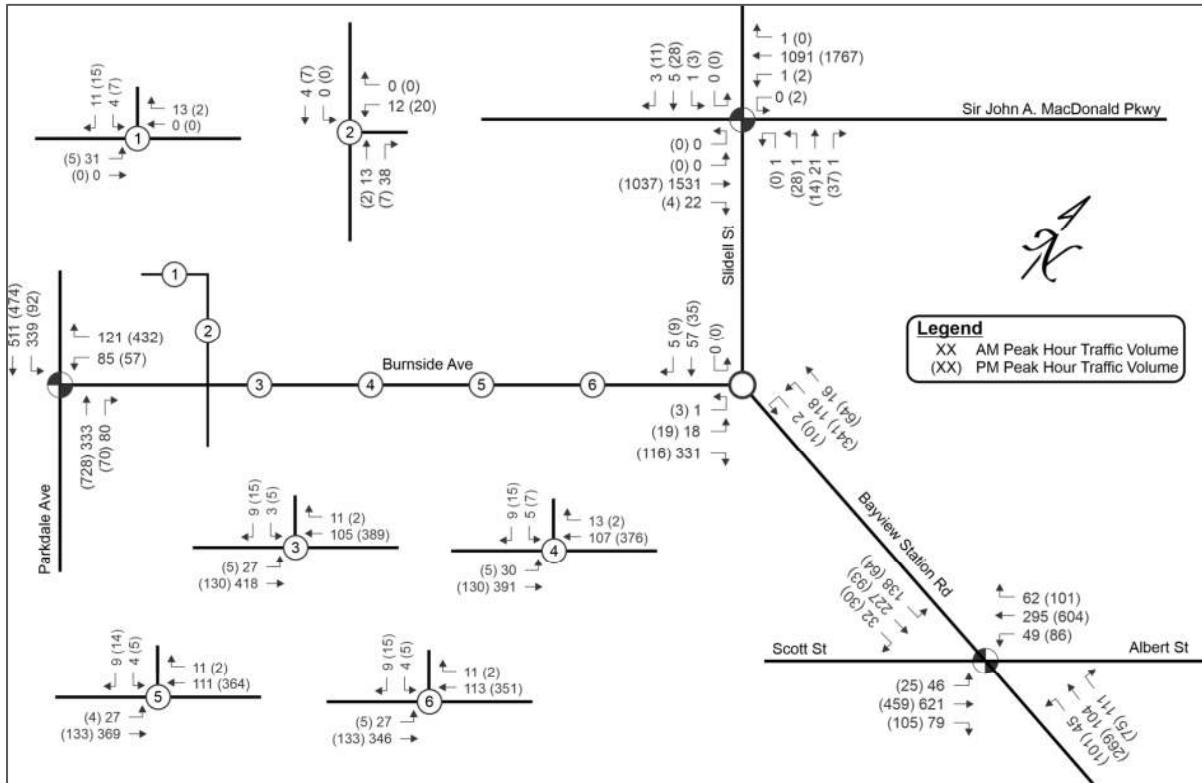


Figure 10- Future Total (2023) Traffic Volumes

The future total traffic operations analysis for 2023 is provided as **Table 9**. Full outputs are provided in **Appendix I**.

Table 10 - Future Total (2023) Traffic Operations Analysis

| Intersection | Weekday AM Peak (PM Peak) | | | | | |
|---|---------------------------|-------------|----------|-------------|-------------|-------|
| | Critical Movement(s) | | | Overall | | |
| | LoS | v/c | Movement | Delay (s) | v/c | LOS |
| Signalized | | | | | | |
| Parkdale Ave & Burnside Ave | E (F) | 1.09 (1.08) | WBLR | 46.1 (56.6) | 0.95 (1.09) | E (F) |
| | (F) | (1.10) | SBLT | | | |
| Sir John A MacDonald Parkway & Slidell St / Onigam St | - | - | - | 5.5 (8.7) | 0.57 (0.70) | A (B) |
| Scott St / Albert St & Bayview Station Rd | E (E) | 0.85 (0.73) | SBL | 31.7 (25.6) | 0.91 (0.79) | E (C) |
| Unsignalized | | | | | | |

| | | | | | | |
|--|---|---|---|-----------|---------------|-------|
| Burnside Ave & Slidell St & Bayview Station Rd | - | - | - | 4.1 (5.7) | 0.303 (0.365) | A (A) |
| Hinchey Ave & Parcel 1 | - | - | - | 5.8 (7.7) | - | A (A) |
| Hinchey Ave & Parcel 2 | - | - | - | 1.5 (4.8) | - | A (A) |
| Burnside Ave & Parcel 3 | - | - | - | 0.6 (0.5) | - | A (A) |
| Burnside Ave & Parcel 4 | - | - | - | 0.7 (0.5) | - | A (A) |
| Burnside Ave & Parcel 5 | - | - | - | 0.6 (0.5) | - | A (A) |
| Burnside Ave & Parcel 6 | - | - | - | 0.6 (0.5) | - | A (A) |

4.9.1.2 Future Total (2028) Traffic

The future total traffic volumes for 2028 are provided in **Figure 10**.

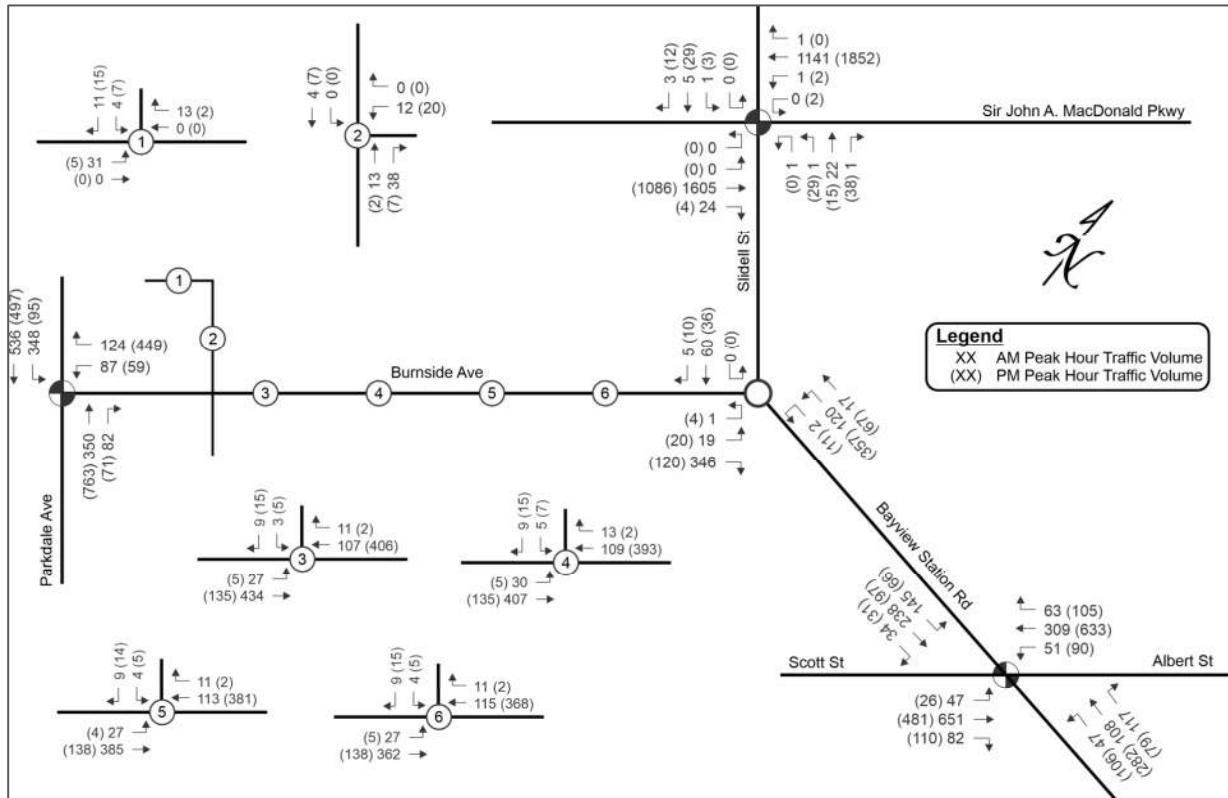


Figure 11 - Future Total (2028) Traffic Volumes

The future total traffic operations analysis for 2028 is provided as **Table 11**. Full outputs are provided in **Appendix I**.

Table 11 - Future Total (2028) Traffic Operations Analysis

| Intersection | Weekday AM Peak (PM Peak) | | | | | |
|---|---------------------------|-------------|----------|--------------|---------------|-------|
| | Critical Movement(s) | | | Overall | | |
| | LoS | v/c | Movement | Delay (s) | v/c | LOS |
| Signalized | | | | | | |
| Parkdale Ave & Burnside Ave | (F) | (1.38) | WBLR | 94.6 (191.0) | 1.11 (1.70) | F (F) |
| | F (F) | 1.30 (1.86) | SBLT | | | |
| Sir John A MacDonald Parkway & Slidell St / Onigam St | - | - | - | 6.2 (10.5) | 0.63 (0.77) | B (C) |
| Scott St / Albert St & Bayview Station Rd | F (E) | 1.21 (1.07) | EBLTR | 75.5 (58.7) | 1.17 (1.10) | F (F) |
| | (E) | (1.03) | WBT | | | |
| | F (F) | 1.10 (1.17) | SBL | | | |
| Unsignalized | | | | | | |
| Burnside Ave & Slidell St & Bayview Station Rd | - | - | - | 4.0 (5.8) | 0.353 (0.430) | A (A) |
| Hinchey Ave & Parcel 1 | - | - | - | 5.8 (7.6) | - | A (A) |
| Hinchey Ave & Parcel 2 | - | - | - | 1.5 (4.7) | - | A (A) |
| Burnside Ave & Parcel 3 | - | - | - | 0.6 (0.4) | - | A (A) |
| Burnside Ave & Parcel 4 | - | - | - | 0.7 (0.4) | - | A (A) |
| Burnside Ave & Parcel 5 | - | - | - | 0.6 (0.4) | - | A (A) |
| Burnside Ave & Parcel 6 | - | - | - | 0.6 (0.4) | - | A (A) |

4.9.2 Multimodal Level of Service

Parkdale Avenue

The existing roadway geometry consists of the following features:

- Approximate 20m R.O.W. road allowance, street width of 11m;
- One (1) vehicular traffic lane in each direction;
- Sidewalk width of 2.0m;
- More than 3,000 annual average daily traffic (AADT);
- Posted speed limit of 50km/h;
- No dedicated transit facilities;
- Dedicated cycling facilities on both sides of the roadway between Colombine Driveway and Sir John A. MacDonald;
- No shoulder of road; and
- No on-street parking between Burnside Avenue and Sir John A. MacDonald.

Table 12 - Parkdale Avenue Projected MMLOS

| Road Segment | Level of Service | | | | | |
|---|-------------------|----------|----------------|----------|----------------|----------|
| | Pedestrian (PLOS) | | Bicycle (BLOS) | | Transit (TLOS) | |
| | PLOS | Target | BLOS | Target | TLOS | Target |
| Parkdale Avenue (between Sir John A MacDonald Parkway & Burnside Avenue) | C | C | C | C | D | D |

Based upon the location of the property in a general urban area, adjacent to an arterial roadway with pedestrian facilities, and dedicated bike facilities with a Level of Traffic Stress (LTS) score of LTS3, the determined level of service for pedestrians is PLOS 'C' and cyclists is BLOS 'C' for the road segment of Parkdale Avenue between Burnside Avenue and Sir John A. MacDonald Parkway. The road currently does not have dedicated transit facilities or transit priority plans; however, there is low friction on the road and the ratio of the average transit travel speed to the posted speed limit is equal to or greater than 80%. Therefore, the determined level of service for transit is TLOS 'D'.

Burnside Avenue

The existing roadway geometry consists of the following features:

- Approximate 18m R.O.W. road allowance, street width of 9m;
- One (1) vehicular traffic lane in each direction;
- Sidewalk width of 1.8m on both sides of the road between Parkdale Avenue and Hincheny Avenue and along the south side of the road between Hincheny Avenue and Slidell Street;
- More than 3,000 annual average daily traffic (AADT);
- Posted speed limit of 40km/h;
- No dedicated transit facilities;
- No dedicated cycling facilities;
- No shoulder of road; and
- On-street parking on the north side of the road between Parkdale Avenue and Stonehurst Avenue.

Table 13 - Projected MMLOS Burnside Avenue between Parkdale Avenue & Slidell Street (Both Sides of the Roadway)

| Road Segment | Level of Service | | | | | |
|------------------------|-------------------|----------|----------------|----------|----------------|----------|
| | Pedestrian (PLOS) | | Bicycle (BLOS) | | Transit (TLOS) | |
| | PLOS | Target | BLOS | Target | TLOS | Target |
| Burnside Avenue | C | C | B | B | E | D |

Based upon the location of the property in a general urban area, adjacent to a local roadway with pedestrian facilities, and no dedicated bike facilities with a Level of Traffic Stress (LTS) score of LTS3, the determined level of service for pedestrians is PLOS 'C' and cyclists is BLOS 'B' for the road segment of Burnside Avenue between Parkdale Avenue and Slidell Street. The road currently does not have dedicated transit facilities or transit priority plans; however, there is a medium friction on the road and the ratio of the average transit travel speed to the posted speed limit is equal to or greater than 60%. Therefore, the determined level of service for transit is TLOS 'E'.

Slidell Street

The existing roadway geometry consists of the following features:



- Approximate 20m R.O.W. road allowance, street width that transitions from 11m to 8.5m;
- One (1) vehicular traffic lane in each direction;
- Sidewalk width of 1.8m along the east side of the road;
- Less than 3,000 annual average daily traffic (AADT);
- Assumed speed limit of 50km/h as per the Highway Traffic Act;
- No dedicated transit facilities;
- No dedicated cycling facilities;
- No shoulder of road; and
- No on-street parking.

Table 14 - Slidell Street Projected MMLOS

| Road Segment | Level of Service | | | | | |
|---|-------------------|----------|----------------|----------|----------------|----------|
| | Pedestrian (PLOS) | | Bicycle (BLOS) | | Transit (TLOS) | |
| | PLOS | Target | BLOS | Target | TLOS | Target |
| Slidell Street (between Sir John A MacDonald Parkway and Burnside Avenue / Bayview Station Road) | B | C | D | C | D | D |

Based upon the location of the property in a general urban area, adjacent to a collector roadway with pedestrian facilities, and no dedicated bike facilities with a Level of Traffic Stress (LTS) score of LTS3, the determined level of service for pedestrians is PLOS 'B' and cyclists is BLOS 'D' for the road segment of Slidell Street between Burnside Avenue, Bayview Station Road and Sir John A. MacDonald Parkway. The road currently does not have dedicated transit facilities or transit priority plans; however, there is a low friction on the road and the ratio of the average transit travel speed to the posted speed limit is equal to or greater than 80%. Therefore, the determined level of service for transit is TLOS 'D'.

Sir John A. MacDonald Parkway

The existing roadway geometry consists of the following features:

- Approximate 34m R.O.W. road allowance, street width of 26m;
- Two (2) vehicular traffic lanes in each direction;
- No sidewalks on either side of road; 4.0m multi-use pathway on north side of road, grade-separated
- More than 3,000 annual average daily traffic (AADT);'
- A median width of approximately 7.75m;
- Posted speed limit of 60km/h;
- No dedicated transit facilities;
- No cycling facilities;
- No shoulder of road; and
- No on-street parking.

The Multi-Modal Level of Service (MMLOS) analysis for the road segment along Hazeldean Road was thoroughly conducted and is summarized below in **Table 15**. The truck level of service is included in the analysis as Hazeldean Road is classified as an arterial road.

Table 15 –Sir John A MacDonald Parkway Projected MMLOS

| Road Segment | Level of Service | | | | | | | |
|------------------------------|-------------------|--------|----------------|--------|----------------|--------|---------------|--------|
| | Pedestrian (PLOS) | | Bicycle (BLOS) | | Transit (TLOS) | | Truck (TkLOS) | |
| | PLOS | Target | BLOS | Target | TLOS | Target | TkLOS | Target |
| Sir John A MacDonald Parkway | F | C | C | C | N/A | B | A | D |

Based upon the location of the property in a general urban area, adjacent to an arterial roadway with no pedestrian facilities, and dedicated bike facilities with a Level of Traffic Stress (LTS) score of LTS1, the determined level of service for pedestrians is PLOS ‘F’ and cyclists is BLOS ‘C’ for the road segment of Sir John A MacDonald Parkway through the intersection of Slidell Street and Onigam Street. The road currently does not have dedicated transit facilities or transit priority plans; and any transit routes along this road do not make stops, therefore transit level of service is TLOS ‘N/A’. As there are more than two (2) travel lanes and the curb lane width is greater than 3.7m, the determined level of service for trucks is TkLOS ‘A’.

Bayview Station Road

The existing roadway geometry consists of the following features:

- Approximate 30m R.O.W. road allowance, street width of 14m;
- One (1) vehicular traffic lanes in each direction;
- Sidewalk width of 1.8m on both sides of the road;
- More than 3,000 annual average daily traffic (AADT);
- Posted speed limit of 50km/h;
- No dedicated transit facilities;
- No cycling facilities;
- No shoulder of road; and
- On-street parking.

Table 16 – Bayview Station Road Projected MMLOS

| Road Segment | Level of Service | | | | | |
|---|-------------------|--------|----------------|--------|----------------|--------|
| | Pedestrian (PLOS) | | Bicycle (BLOS) | | Transit (TLOS) | |
| | PLOS | Target | BLOS | Target | TLOS | Target |
| Bayview Station Road (between Burnside Ave / Slidell Street and Scott Street / Albert Street) | D | C | D | C | D | D |

Based upon the location of the property in a general urban area, adjacent to a collector roadway with pedestrian facilities, and no dedicated bike facilities with a Level of Traffic Stress (LTS) score of LTS3, the determined level of service for pedestrians is PLOS ‘D’ and cyclists is BLOS ‘D’ for the road segment of Bayview Station Road between Burnside Avenue / Slidell Street and Scott Street / Albert Street. The road currently does not have dedicated transit facilities or transit priority plans; however, there is a low friction on the road and the ratio of the average transit travel speed to the posted speed limit is equal to or greater than 80%. Therefore, the determined level of service for transit is TLOS ‘D’.

Scott Street

The existing roadway geometry consists of the following features:

- Approximate 24m R.O.W. road allowance, street width of 18m;
- One (1) vehicular traffic lanes in each direction;
- Sidewalk width of 1.8m on the south side; Multi-use trail width of 3.2m on the north side.
- More than 3,000 annual average daily traffic (AADT);'
- Posted speed limit of 50km/h;
- Dedicated transit lanes in both directions;
- Dedicated cycling facilities on both sides of the roadway, multi-use trail on the north side, separating cycling lane on the south side;
- No shoulder of road; and
- No on-street parking.

Table 17 – Scott Street Projected MMLOS

| Road Segment | Level of Service | | | | | |
|---|-------------------|--------|----------------|--------|----------------|--------|
| | Pedestrian (PLOS) | | Bicycle (BLOS) | | Transit (TLOS) | |
| | PLOS | Target | BLOS | Target | TLOS | Target |
| Scott Street (between Merton Street and Bayview Station Road) | D | C | A | B | B | B |

Based upon the location of the property in a general urban area, adjacent to a arterial roadway with pedestrian facilities, and no dedicated bike facilities with a Level of Traffic Stress (LTS) score of LTS2, the determined level of service for pedestrians is PLOS 'D' and cyclists is BLOS 'A' for the road segment of Scott Street between Merton Street and Bayview Station Road. The road currently had dedicated bus lanes with limited driveway friction. Therefore, the determined level of service for transit is TLOS 'B'.

Appendix A – TIA Screening Form

City of Ottawa 2017 TIA Guidelines Screening Form

1. Description of Proposed Development

| | |
|------------------------------------|---|
| Municipal Address | 1+19 Sir John A. Macdonald Parkway |
| Description of Location | Naturalized area between SJAMP and Brunside Ave/Hinchey Ave |
| Land Use Classification | Residential (R1) |
| Development Size (units) | To be determined |
| Development Size (m ²) | 6 Parcels - 13,289 sq.m |
| Number of Accesses and Locations | 6 Access - 4 Burnside Avenue, 2 Hinchey Avenue |
| Phase of Development | Conceptual - Rezoning application |
| Buildout Year | To be determined |

If available, please attach a sketch of the development or site plan to this form.

2. Trip Generation Trigger

Considering the Development's Land Use type and Size (as filled out in the previous section), please refer to the Trip Generation Trigger checks below.

| Land Use Type | Minimum Development Size |
|-------------------------------------|--------------------------|
| Single-family homes | 40 units |
| Townhomes or apartments | 90 units |
| Office | 3,500 m ² |
| Industrial | 5,000 m ² |
| Fast-food restaurant or coffee shop | 100 m ² |
| Destination retail | 1,000 m ² |
| Gas station or convenience market | 75 m ² |

* If the development has a land use type other than what is presented in the table above, estimates of person-trip generation may be made based on average trip generation characteristics represented in the current edition of the Institute of Transportation Engineers (ITE) Trip Generation Manual.

If the proposed development size is greater than the sizes identified above, the Trip Generation Trigger is satisfied.

3. Location Triggers

| | Yes | No |
|--|-----|----|
| Does the development propose a new driveway to a boundary street that is designated as part of the City's Transit Priority, Rapid Transit or Spine Bicycle Networks? | | X |
| Is the development in a Design Priority Area (DPA) or Transit-oriented Development (TOD) zone?* | | X |

*DPA and TOD are identified in the City of Ottawa Official Plan (DPA in Section 2.5.1 and Schedules A and B; TOD in Annex 6). See Chapter 4 for a list of City of Ottawa Planning and Engineering documents that support the completion of TIA).

If any of the above questions were answered with 'Yes,' the Location Trigger is satisfied.

4. Safety Triggers

| | Yes | No |
|---|-----|----|
| Are posted speed limits on a boundary street are 80 km/hr or greater? | | X |
| Are there any horizontal/vertical curvatures on a boundary street limits sight lines at a proposed driveway? | | X |
| Is the proposed driveway within the area of influence of an adjacent traffic signal or roundabout (i.e. within 300 m of intersection in rural conditions, or within 150 m of intersection in urban/ suburban conditions)? | X | |
| Is the proposed driveway within auxiliary lanes of an intersection? | | X |
| Does the proposed driveway make use of an existing median break that serves an existing site? | | X |
| Is there is a documented history of traffic operations or safety concerns on the boundary streets within 500 m of the development? | | X |
| Does the development include a drive-thru facility? | | X |

If any of the above questions were answered with 'Yes,' the Safety Trigger is satisfied.

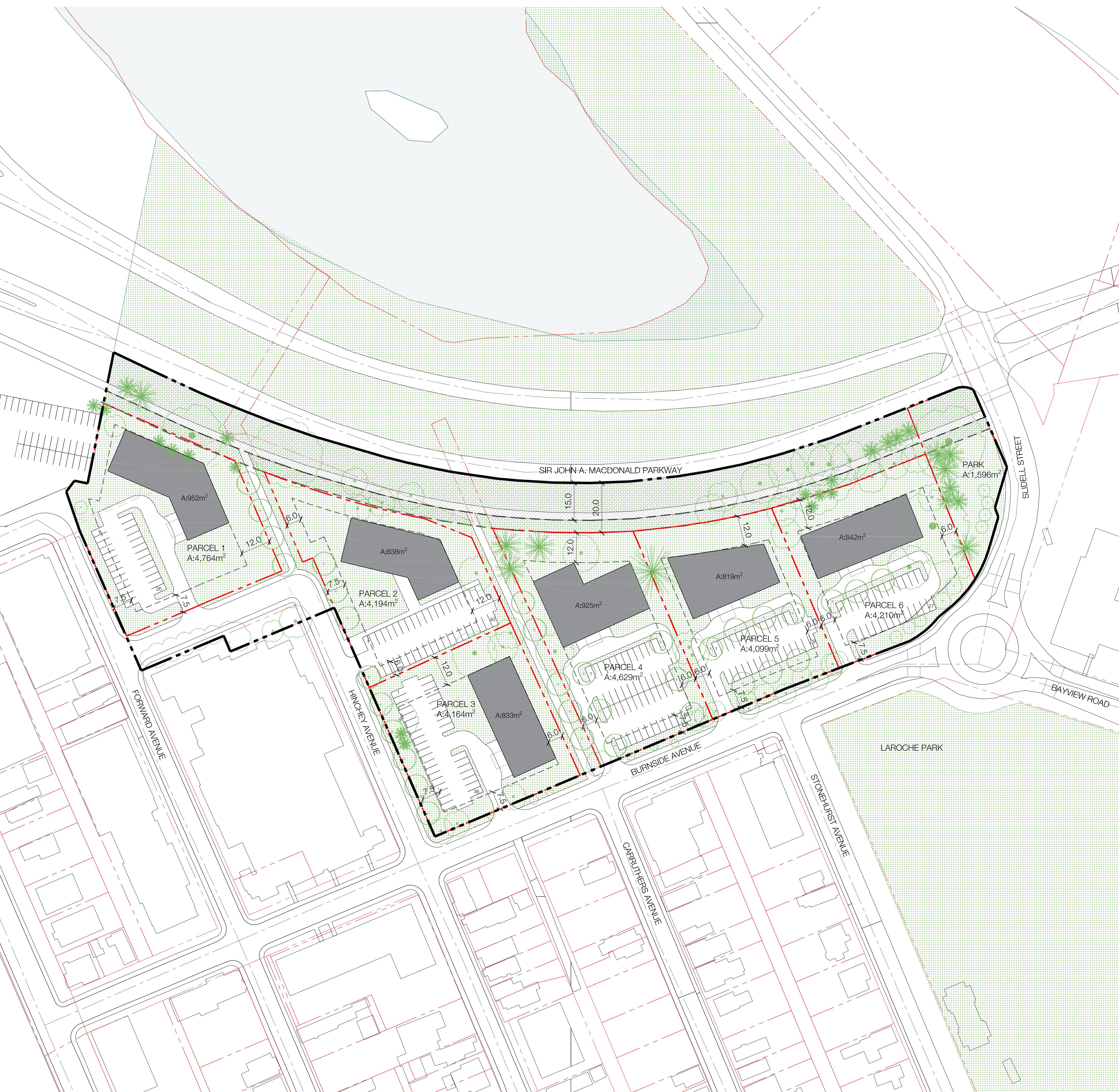
5. Summary

| | Yes | No |
|---|-----|----|
| Does the development satisfy the Trip Generation Trigger? | X | |
| Does the development satisfy the Location Trigger? | | X |
| Does the development satisfy the Safety Trigger? | X | |

If none of the triggers are satisfied, the TIA Study is complete. If one or more of the triggers is satisfied, the TIA Study must continue into the next stage (Screening and Scoping).

Appendix B – Site Plan

1+19 SIR JOHN A MACDONALD PKY CONCEPT PLAN OPTION 1



2 CONCEPT PLANS 2018.07.06 RP
1 BASE PLAN 2018.06.20 RP
No. REVISION DATE BY

CLIENT
NATIONAL CAPITAL COMMISSION National Capital Commission Commission de la capitale nationale

FOTENN
Planning + Design

223 McLeod Street, Ottawa ON K2P 0Z8
613.730.5709 www.fotenn.com

DESIGNED RP
REVIEWED MS
DATE 2018.06.05

P1

Appendix C – Scoping Email with City of Ottawa

Phil Desmarais

From: Dubyk, Wally <Wally.Dubyk@ottawa.ca>
Sent: Wednesday, February 21, 2018 1:03 PM
To: Phil Desmarais
Cc: Nitsche, Kersten; Chantal Miner (chantal.miner@ncc-ccn.ca); Carl Furney (furney@fotenn.com)
Subject: RE: Traffic Impact Study - NCC Embassy OPA & ZBA Burnside, Emmerson, Forward

Phil,

I concur.

Thank you,

Wally Dubyk
Project Manager - Transportation Approvals
Development Review, Central & South Branches
613-580-2424 x13783

From: Phil Desmarais [mailto:Phil.Desmarais@exp.com]
Sent: Wednesday, February 21, 2018 12:25 PM
To: Dubyk, Wally <Wally.Dubyk@ottawa.ca>
Cc: Nitsche, Kersten <Kersten.Nitsche@ottawa.ca>; Chantal Miner (chantal.miner@ncc-ccn.ca) <chantal.miner@ncc-ccn.ca>; Carl Furney (furney@fotenn.com) <furney@fotenn.com>
Subject: Traffic Impact Study - NCC Embassy OPA & ZBA Burnside, Emmerson, Forward

Thanks for taking my call this morning. The NCC has expressed an interest in retaining EXP to complete the required transportation studies to support the NCC's Official Plan Amendment (OPA) and Zoning By-law Amendment (ZBA) for their lands abutting the Sir John A. MacDonald (SJAM) Parkway. The NCC will be developing a framework, and detailed design for each site within the parcel will be advanced at a later date.

From our discussion, we understand that the City will require the preparation of a screening and scoping document per the 2017 City TIA guidelines to support the application. Also, we suggest that the following intersections study area delimit the study area for screening and scoping report:

- SJAM Parkway / Slidell Street
- Slidell Street / Burnside Ave./ Bayview Road
- Scott Street / Bayview Road
- Parkdale Avenue / Burnside Avenue

Following successful completion of the OPA and ZBA process, individual developments will need to undergo a site plan process wherein individual TIA's will be required under site plan approval.



Please confirm that this meets the City's requirements from a transportation perspective.



Phil Desmarais, P.Eng.

EXP | Senior Project Manager

t : +1.613.688.1899 | m : +1.613.790.3295 | e : phil.desmarais@exp.com

2650 Queensview Drive

Suite 100

Ottawa, ON K2B 8H6

CANADA

exp.com | *legal disclaimer*

keep it green, read from the screen

This e-mail originates from the City of Ottawa e-mail system. Any distribution, use or copying of this e-mail or the information it contains by other than the intended recipient(s) is unauthorized. Thank you.

Le présent courriel a été expédié par le système de courriels de la Ville d'Ottawa. Toute distribution, utilisation ou reproduction du courriel ou des renseignements qui s'y trouvent par une personne autre que son destinataire prévu est interdite. Je vous remercie de votre collaboration.

Appendix D – Traffic Data

Traffic Signal Timing

City of Ottawa, Transportation Services Department

Traffic Signal Operations Unit

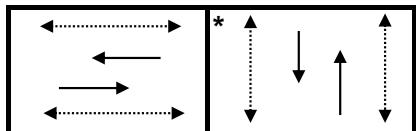
| | | | |
|----------------------|----------------------|--------------|-------------|
| Intersection: | Main: Albert / Scott | Side: | Bayview |
| Controller: | MS 3200 | TSD: | 5613 |
| Author: | Ahmed Abdullah | Date: | 20-Jan-2020 |

Existing Timing Plans†

| Plan | | | | | | | Ped Minimum Time | | |
|---------|----------|----------|---------|-------|---------|---------|------------------|----|---------|
| | Early AM | Off Peak | PM Peak | Night | Weekend | AM Peak | Walk | DW | A+R |
| Cycle | 95 | 65 | 100 | 70 | 65 | 100 | | | |
| Offset | 40 | 54 | 65 | X | 54 | 40 | | | |
| EB Thru | 63 | 33 | 68 | 38 | 33 | 68 | 7 | 19 | 3.3+3.2 |
| WB Thru | 63 | 33 | 68 | 38 | 33 | 68 | 7 | 19 | 3.3+3.2 |
| NB Thru | 32 | 32 | 32 | 32 | 32 | 32 | 7 | 19 | 3.3+3.1 |
| SB Thru | 32 | 32 | 32 | 32 | 32 | 32 | 7 | 19 | 3.3+3.1 |

Phasing Sequence‡

Plan: All



Schedule

| Weekday | |
|---------|------|
| Time | Plan |
| 0:15 | 4 |
| 6:30 | 1 |
| 7:45 | 21 |
| 9:30 | 2 |
| 15:00 | 3 |
| 18:30 | 2 |
| 22:30 | 4 |

| Saturday | |
|----------|------|
| Time | Plan |
| 0:15 | 4 |
| 6:30 | 2 |
| 9:00 | 5 |
| 18:30 | 2 |
| 22:30 | 4 |

| Sunday | |
|--------|------|
| Time | Plan |
| 0:15 | 4 |
| 6:30 | 2 |
| 9:00 | 5 |
| 18:00 | 2 |
| 22:30 | 4 |

Notes

†: Time for each direction includes amber and all red intervals

‡: Start of first phase should be used as reference point for offset

Asterisk (*) Indicates actuated phase

(fp): Fully Protected Left Turn

◀-----→ Pedestrian signal

Cost is \$58.78 (\$52.02 + HST)

Traffic Signal Timing

City of Ottawa, Transportation Services Department

Traffic Signal Operations Unit

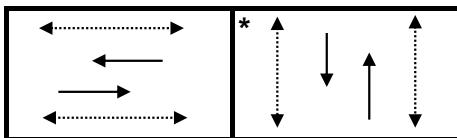
| | | |
|----------------------|-------------------|----------------------|
| Intersection: | <i>Main:</i> SJAM | <i>Side:</i> Slidell |
| Controller: | ATC 3 | TSD: 5890 |
| Author: | Ahmed Abdullah | Date: 20-Jan-2020 |

Existing Timing Plans[†]

| | Plan | | | | Ped Minimum Time | | |
|---------|---------|------------|---------|------------|------------------|----|---------|
| | AM Peak | Off Peak | PM Peak | Night | Walk | DW | A+R |
| Cycle | 95 | Free | 95 | Free | | | |
| Offset | 0 | X | 0 | X | | | |
| EB Thru | 61 | max = 53.5 | 61 | max = 54.5 | 15 | 10 | 3.7+1.8 |
| WB Thru | 61 | max = 53.5 | 61 | max = 54.5 | 15 | 10 | 3.7+1.8 |
| NB Thru | 34 | max = 31.3 | 34 | max = 31.3 | 7 | 20 | 3.3+3.0 |
| SB Thru | 34 | max = 31.3 | 34 | max = 31.3 | 7 | 20 | 3.3+3.0 |

Phasing Sequence[‡]

Plan: All



Notes: 1) Plans 2 & 4, have a max and ped recall on the EW movements

Schedule

| Weekday | |
|---------|------|
| Time | Plan |
| 0:15 | 4 |
| 6:30 | 1 |
| 9:00 | 2 |
| 15:00 | 3 |
| 18:30 | 2 |
| 21:00 | 4 |

| Weekend | |
|---------|------|
| Time | Plan |
| 0:10 | 4 |
| 7:00 | 2 |
| 19:00 | 4 |

Notes

†: Time for each direction includes amber and all red intervals

‡: Start of first phase should be used as reference point for offset

Asterisk (*) Indicates actuated phase

(fp): Fully Protected Left Turn

↔ Pedestrian signal

Cost is \$58.78 (\$52.02 + HST)

Traffic Signal Timing

City of Ottawa, Transportation Services Department

Traffic Signal Operations Unit

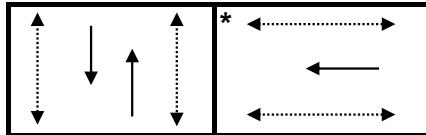
| | | |
|----------------------|-----------------------|--------------------------|
| Intersection: | <i>Main:</i> Parkdale | <i>Side:</i> Burnside |
| Controller: | MS 3200 | TSD: 6108 |
| Author: | Ahmed Abdullah | Date: 20-Jan-2020 |

Existing Timing Plans[†]

| Plan | | | | | | Ped Minimum Time | | |
|---------|---------|----------|---------|-------|---------|------------------|----|---------|
| | AM Peak | Off Peak | PM Peak | Night | Weekend | Walk | DW | A+R |
| Cycle | 60 | 55 | 70 | 50 | 55 | | | |
| Offset | 18 | 18 | 23 | 19 | 18 | | | |
| NB Thru | 40 | 35 | 45 | 30 | 35 | 15 | 6 | 3.3+1.9 |
| SB Thru | 40 | 35 | 45 | 30 | 35 | 15 | 6 | 3.3+1.9 |
| WB Thru | 20 | 20 | 25 | 20 | 20 | 7 | 7 | 3.0+2.4 |

Phasing Sequence[‡]

Plan: All



Schedule

| Time | Plan |
|-------|------|
| 0:15 | 4 |
| 6:30 | 1 |
| 9:30 | 2 |
| 15:00 | 3 |
| 18:30 | 2 |
| 22:30 | 4 |

| Time | Plan |
|-------|------|
| 0:15 | 4 |
| 6:30 | 2 |
| 9:00 | 5 |
| 18:30 | 2 |
| 22:30 | 4 |

| Time | Plan |
|-------|------|
| 0:15 | 4 |
| 6:30 | 2 |
| 9:00 | 5 |
| 18:00 | 2 |
| 22:30 | 4 |

Notes

†: Time for each direction includes amber and all red intervals

‡: Start of first phase should be used as reference point for offset

Asterisk (*) Indicates actuated phase

(fp): Fully Protected Left Turn

◀-----► Pedestrian signal

Cost is \$58.78 (\$52.02 + HST)

Transportation Services - Traffic Services

Turning Movement Count - Study Results

BAYVIEW RD @ SCOTT ST/ALBERT ST

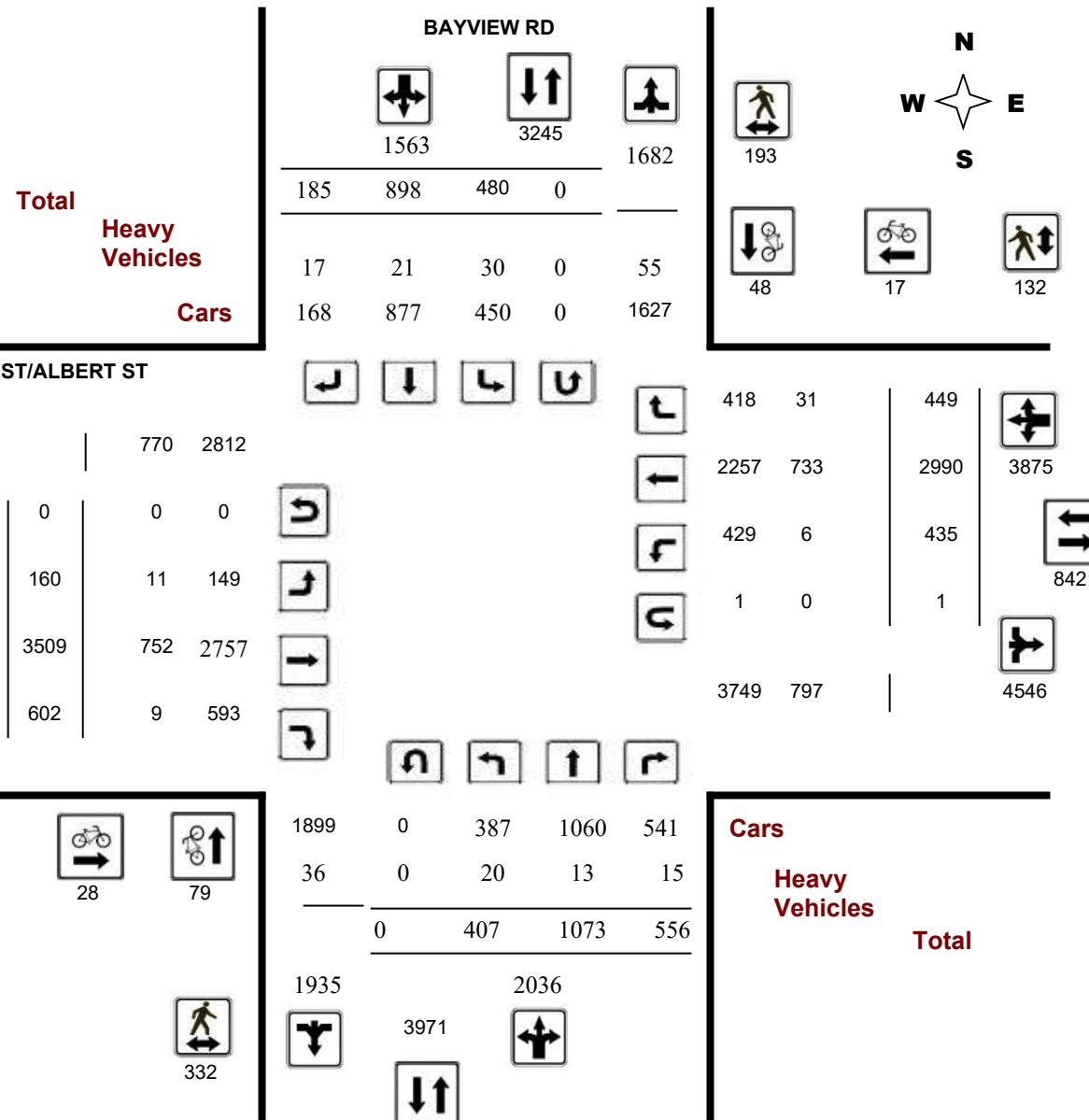
Survey Date: Wednesday, September 07, 2016

WO No: 36277

Start Time: 07:00

Device: Miovision

Full Study Diagram



Transportation Services - Traffic Services

Turning Movement Count - Study Results

BAYVIEW RD @ SCOTT ST/ALBERT ST

Survey Date: Wednesday, September 07, 2016

WO No:

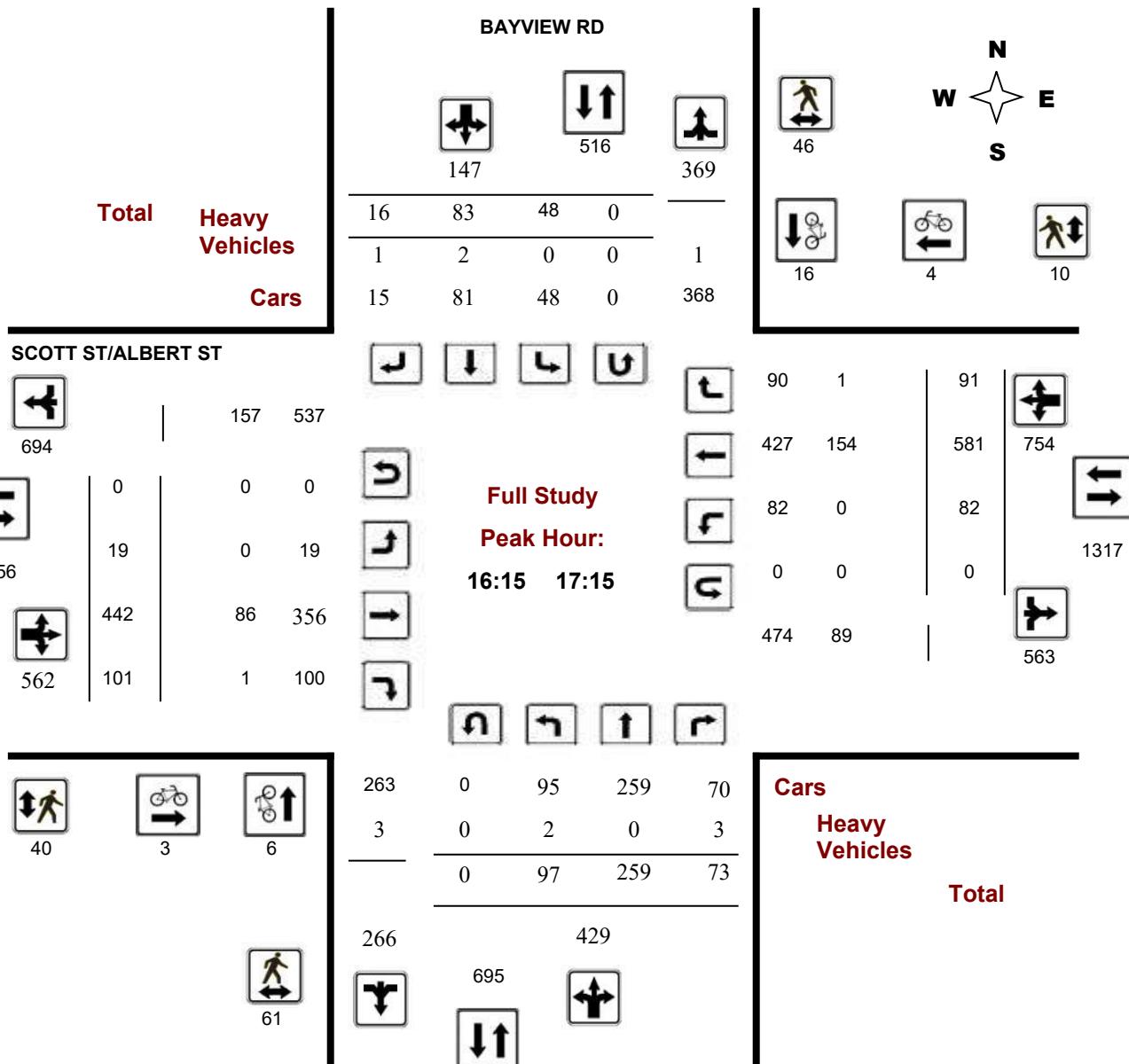
36277

Start Time: 07:00

Device:

Miovision

Full Study Peak Hour Diagram





Transportation Services - Traffic Services

Turning Movement Count - Peak Hour Diagram

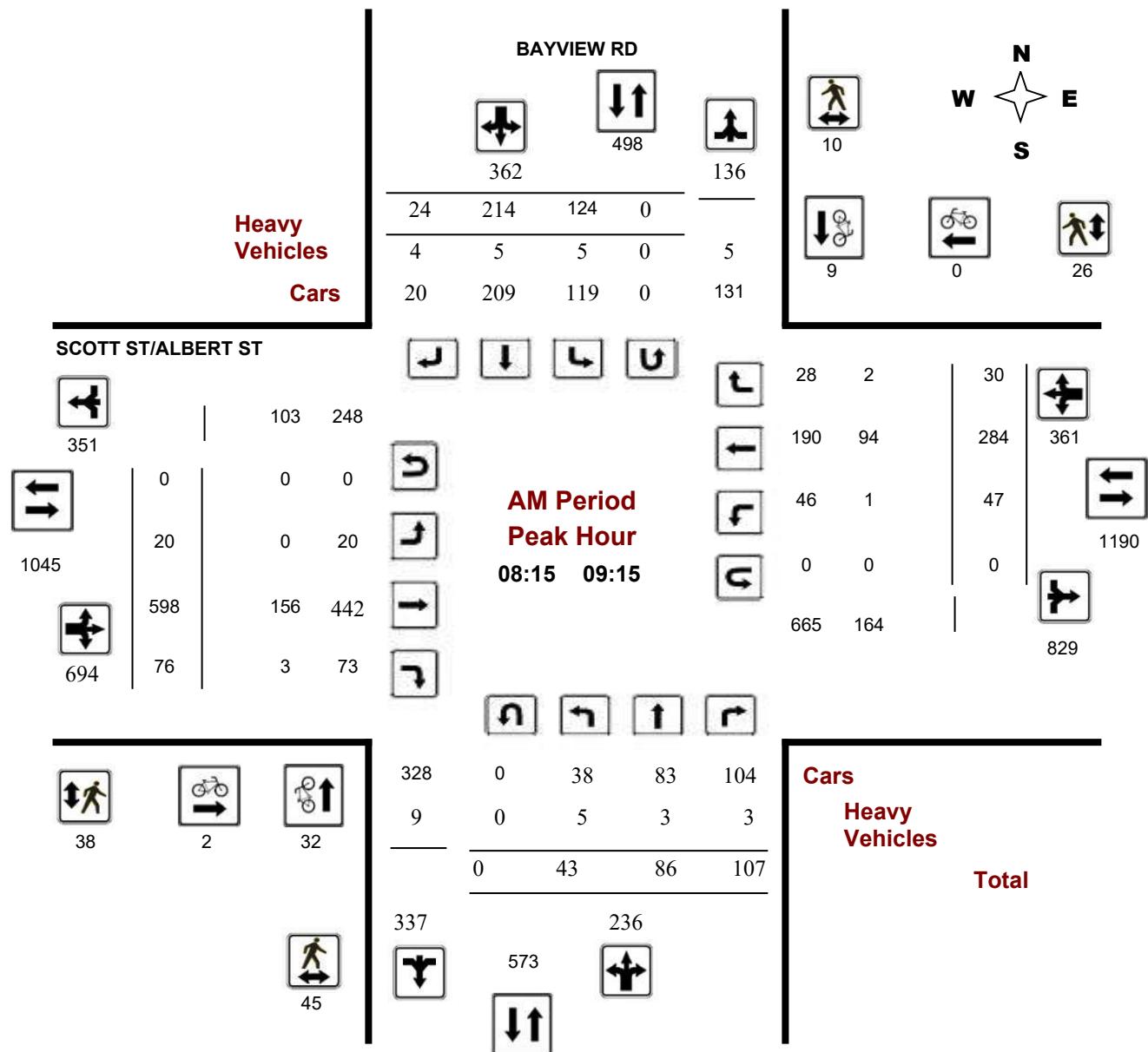
BAYVIEW RD @ SCOTT ST/ALBERT ST

Survey Date: Wednesday, September 07, 2016

Start Time: 07:00

WO No: 36277

Device: Miovision





Transportation Services - Traffic Services

Turning Movement Count - Peak Hour Diagram

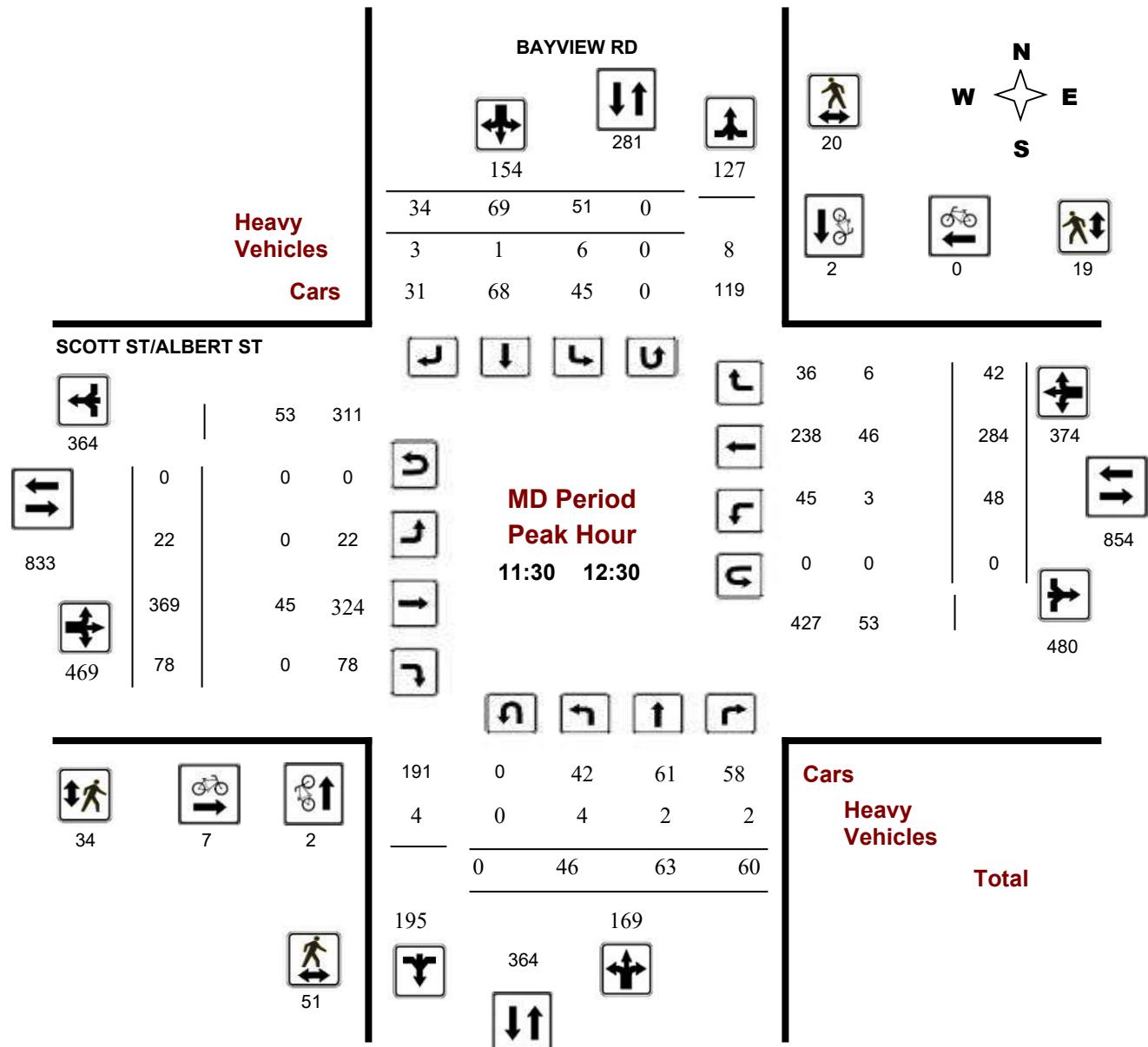
BAYVIEW RD @ SCOTT ST/ALBERT ST

Survey Date: Wednesday, September 07, 2016

Start Time: 07:00

WO No: 36277

Device: Miovision





Transportation Services - Traffic Services

Turning Movement Count - Peak Hour Diagram

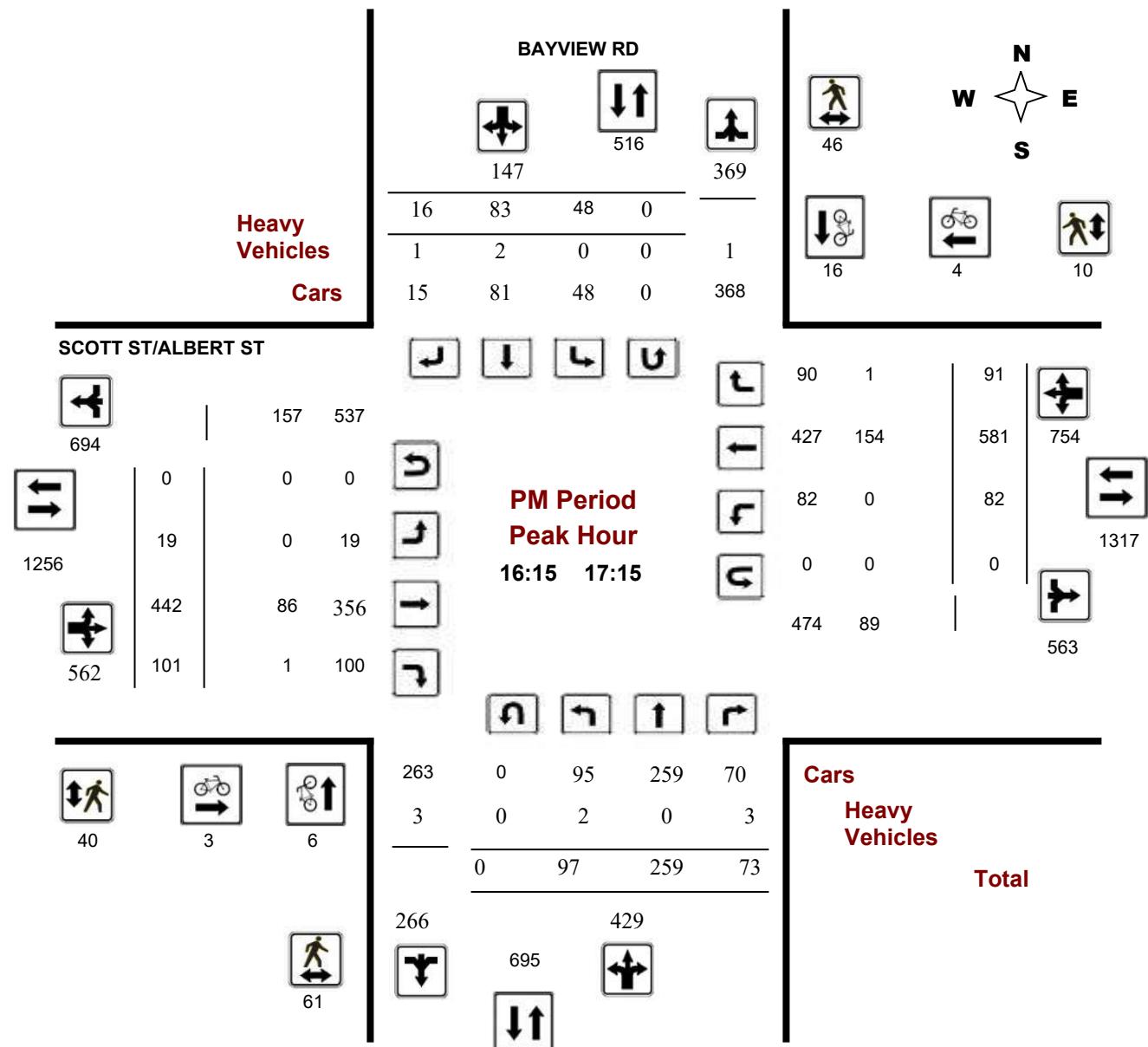
BAYVIEW RD @ SCOTT ST/ALBERT ST

Survey Date: Wednesday, September 07, 2016

Start Time: 07:00

WO No: 36277

Device: Miovision





Transportation Services - Traffic Services

Turning Movement Count - Study Results

BAYVIEW RD @ SCOTT ST/ALBERT ST

Survey Date: Wednesday, September 07, 2016

WO No:

36277

Start Time: 07:00

Device:

Miovision

Full Study Summary (8 HR Standard)

Survey Date: Wednesday, September 07,
2016

Total Observed U-Turns

AADT Factor

| | | | |
|-------------|---|-------------|---|
| Northbound: | 0 | Southbound: | 0 |
| Eastbound: | 0 | Westbound: | 1 |

1.39

BAYVIEW RD

SCOTT ST/ALBERT ST

| Period | Northbound | | | Southbound | | | SB TOT | STR TOT | Eastbound | | | Westbound | | | WB TOT | STR TOT | Grand Total | | |
|------------------|------------|------|-----|-------------|-----|-----|-----------|------------|-----------|-----|------|-----------|----------|-----|-----------|------------|----------------|-------------|--------------|
| | LT | ST | RT | LT | ST | RT | | | LT | ST | RT | EB TOT | LT | ST | RT | | | | |
| 07:00 08:00 | 24 | 49 | 60 | 133 | 71 | 177 | 17 | 265 | 398 | 19 | 453 | 51 | 523 | 40 | 221 | 37 | 298 | 821 | 1219 |
| 08:00 09:00 | 45 | 68 | 116 | 229 | 126 | 207 | 30 | 363 | 592 | 16 | 609 | 76 | 701 | 45 | 276 | 35 | 356 | 1057 | 1649 |
| 09:00 10:00 | 30 | 65 | 49 | 144 | 81 | 134 | 24 | 239 | 383 | 25 | 443 | 72 | 540 | 40 | 282 | 42 | 364 | 904 | 1287 |
| 11:30 12:30 | 46 | 63 | 60 | 169 | 51 | 69 | 34 | 154 | 323 | 22 | 369 | 78 | 469 | 48 | 284 | 42 | 374 | 843 | 1166 |
| 12:30 13:30 | 42 | 84 | 63 | 189 | 33 | 53 | 18 | 104 | 293 | 24 | 320 | 75 | 419 | 42 | 275 | 43 | 360 | 779 | 1072 |
| 15:00 16:00 | 69 | 263 | 67 | 399 | 33 | 99 | 26 | 158 | 557 | 25 | 449 | 64 | 538 | 75 | 490 | 90 | 655 | 1193 | 1750 |
| 16:00 17:00 | 83 | 271 | 68 | 422 | 46 | 87 | 19 | 152 | 574 | 20 | 438 | 95 | 553 | 69 | 580 | 96 | 745 | 1298 | 1872 |
| 17:00 18:00 | 68 | 210 | 73 | 351 | 39 | 72 | 17 | 128 | 479 | 9 | 428 | 91 | 528 | 76 | 582 | 64 | 722 | 1250 | 1729 |
| Sub Total | 407 | 1073 | 556 | 2036 | 480 | 898 | 185 | 1563 | 3599 | 160 | 3509 | 602 | 4271 | 435 | 2990 | 449 | 3874 | 8145 | 11744 |
| U Turns | | | | 0 | | | | 0 | 0 | | | | 0 | | | 1 | 1 | 1 | |
| Total | 407 | 1073 | 556 | 2036 | 480 | 898 | 185 | 1563 | 3599 | 160 | 3509 | 602 | 4271 | 435 | 2990 | 449 | 3875 | 8146 | 11745 |

EQ 12Hr 566 1491 773 **2830** 667 1248 257 2173 5003 222 4878 837 5937 605 4156 624 **5386** 11323 **16326**

Note: These values are calculated by multiplying the totals by the appropriate expansion factor.

1.39

AVG 12Hr 566 1491 773 **2830** 667 1248 257 2173 5003 222 4878 837 5937 605 4156 624 **5386** 11323 **16326**

Note: These volumes are calculated by multiplying the Equivalent 12 hr. totals by the AADT factor.

1

AVG 24Hr 741 1954 1012 **3707** 874 1635 337 2846 6553 291 6390 1096 **7777** 792 5444 818 **7056** 14833 **21386**

Note: These volumes are calculated by multiplying the Average Daily 12 hr. totals by 12 to 24 expansion factor. **1.31**

Note: U-Turns provided for approach totals. Refer to 'U-Turn' Report for specific breakdown.



Transportation Services - Traffic Services

Turning Movement Count - Study Results

BAYVIEW RD @ SCOTT ST/ALBERT ST

Survey Date: Wednesday, September 07, 2016

WO No:

36277

Start Time: 07:00

Device:

Miovision

Full Study Cyclist Volume

BAYVIEW RD

SCOTT ST/ALBERT ST

| Time Period | Northbound | Southbound | Street Total | Eastbound | Westbound | Street Total | Grand Total |
|-------------|------------|------------|--------------|-----------|-----------|--------------|-------------|
| 07:00 | 07:15 | 1 | 1 | 2 | 0 | 0 | 2 |
| 07:15 | 07:30 | 5 | 2 | 7 | 0 | 0 | 7 |
| 07:30 | 07:45 | 6 | 2 | 8 | 0 | 0 | 8 |
| 07:45 | 08:00 | 3 | 1 | 4 | 1 | 1 | 6 |
| 08:00 | 08:15 | 8 | 2 | 10 | 2 | 0 | 12 |
| 08:15 | 08:30 | 11 | 1 | 12 | 0 | 0 | 12 |
| 08:30 | 08:45 | 12 | 0 | 12 | 1 | 0 | 13 |
| 08:45 | 09:00 | 6 | 4 | 10 | 0 | 0 | 10 |
| 09:00 | 09:15 | 3 | 4 | 7 | 1 | 0 | 8 |
| 09:15 | 09:30 | 0 | 0 | 0 | 2 | 1 | 3 |
| 09:30 | 09:45 | 0 | 0 | 0 | 0 | 1 | 1 |
| 09:45 | 10:00 | 1 | 0 | 1 | 0 | 0 | 1 |
| 11:30 | 11:45 | 1 | 0 | 1 | 3 | 0 | 3 |
| 11:45 | 12:00 | 0 | 1 | 1 | 0 | 0 | 1 |
| 12:00 | 12:15 | 0 | 0 | 0 | 1 | 0 | 1 |
| 12:15 | 12:30 | 1 | 1 | 2 | 3 | 0 | 3 |
| 12:30 | 12:45 | 2 | 0 | 2 | 1 | 1 | 4 |
| 12:45 | 13:00 | 0 | 0 | 0 | 2 | 0 | 2 |
| 13:00 | 13:15 | 1 | 0 | 1 | 1 | 0 | 1 |
| 13:15 | 13:30 | 1 | 2 | 3 | 3 | 0 | 6 |
| 15:00 | 15:15 | 0 | 1 | 1 | 0 | 0 | 1 |
| 15:15 | 15:30 | 1 | 3 | 4 | 0 | 4 | 8 |
| 15:30 | 15:45 | 3 | 0 | 3 | 0 | 0 | 3 |
| 15:45 | 16:00 | 4 | 1 | 5 | 1 | 1 | 7 |
| 16:00 | 16:15 | 0 | 0 | 0 | 1 | 0 | 1 |
| 16:15 | 16:30 | 2 | 1 | 3 | 0 | 0 | 3 |
| 16:30 | 16:45 | 0 | 5 | 5 | 0 | 1 | 6 |
| 16:45 | 17:00 | 2 | 8 | 10 | 1 | 0 | 11 |
| 17:00 | 17:15 | 2 | 2 | 4 | 2 | 3 | 9 |
| 17:15 | 17:30 | 1 | 0 | 1 | 0 | 4 | 5 |
| 17:30 | 17:45 | 2 | 4 | 6 | 1 | 0 | 7 |
| 17:45 | 18:00 | 0 | 2 | 2 | 1 | 0 | 3 |
| Total | | 79 | 48 | 127 | 28 | 17 | 172 |



Transportation Services - Traffic Services

Turning Movement Count - Study Results

BAYVIEW RD @ SCOTT ST/ALBERT ST

Survey Date: Wednesday, September 07, 2016

WO No:

36277

Start Time: 07:00

Device:

Miovision

Full Study Pedestrian Volume

BAYVIEW RD

SCOTT ST/ALBERT ST

| Time Period | NB Approach (E or W Crossing) | SB Approach (E or W Crossing) | Total | EB Approach (N or S Crossing) | WB Approach (N or S Crossing) | Total | Grand Total |
|--------------------|----------------------------------|----------------------------------|------------|----------------------------------|----------------------------------|------------|-------------|
| 07:00 07:15 | 12 | 6 | 18 | 5 | 6 | 11 | 29 |
| 07:15 07:30 | 5 | 4 | 9 | 3 | 4 | 7 | 16 |
| 07:30 07:45 | 10 | 11 | 21 | 4 | 1 | 5 | 26 |
| 07:45 08:00 | 7 | 6 | 13 | 9 | 5 | 14 | 27 |
| 08:00 08:15 | 16 | 9 | 25 | 12 | 3 | 15 | 40 |
| 08:15 08:30 | 4 | 3 | 7 | 10 | 12 | 22 | 29 |
| 08:30 08:45 | 10 | 3 | 13 | 8 | 10 | 18 | 31 |
| 08:45 09:00 | 11 | 2 | 13 | 11 | 2 | 13 | 26 |
| 09:00 09:15 | 20 | 2 | 22 | 9 | 2 | 11 | 33 |
| 09:15 09:30 | 6 | 1 | 7 | 4 | 1 | 5 | 12 |
| 09:30 09:45 | 6 | 2 | 8 | 0 | 7 | 7 | 15 |
| 09:45 10:00 | 2 | 1 | 3 | 2 | 2 | 4 | 7 |
| 11:30 11:45 | 17 | 5 | 22 | 4 | 4 | 8 | 30 |
| 11:45 12:00 | 7 | 4 | 11 | 7 | 3 | 10 | 21 |
| 12:00 12:15 | 8 | 1 | 9 | 9 | 3 | 12 | 21 |
| 12:15 12:30 | 19 | 10 | 29 | 14 | 9 | 23 | 52 |
| 12:30 12:45 | 22 | 7 | 29 | 16 | 13 | 29 | 58 |
| 12:45 13:00 | 4 | 1 | 5 | 7 | 2 | 9 | 14 |
| 13:00 13:15 | 10 | 2 | 12 | 2 | 3 | 5 | 17 |
| 13:15 13:30 | 3 | 1 | 4 | 0 | 2 | 2 | 6 |
| 15:00 15:15 | 1 | 6 | 7 | 11 | 2 | 13 | 20 |
| 15:15 15:30 | 5 | 1 | 6 | 4 | 3 | 7 | 13 |
| 15:30 15:45 | 8 | 1 | 9 | 8 | 1 | 9 | 18 |
| 15:45 16:00 | 6 | 3 | 9 | 3 | 2 | 5 | 14 |
| 16:00 16:15 | 7 | 18 | 25 | 5 | 7 | 12 | 37 |
| 16:15 16:30 | 17 | 16 | 33 | 10 | 3 | 13 | 46 |
| 16:30 16:45 | 19 | 9 | 28 | 11 | 0 | 11 | 39 |
| 16:45 17:00 | 8 | 10 | 18 | 6 | 0 | 6 | 24 |
| 17:00 17:15 | 17 | 11 | 28 | 13 | 7 | 20 | 48 |
| 17:15 17:30 | 11 | 16 | 27 | 10 | 6 | 16 | 43 |
| 17:30 17:45 | 14 | 12 | 26 | 18 | 3 | 21 | 47 |
| 17:45 18:00 | 20 | 9 | 29 | 9 | 4 | 13 | 42 |
| Total | 332 | 193 | 525 | 244 | 132 | 376 | 901 |



Transportation Services - Traffic Services

Turning Movement Count - Study Results

BAYVIEW RD @ SCOTT ST/ALBERT ST

Survey Date: Wednesday, September 07, 2016

WO No:

36277

Start Time: 07:00

Device:

Miovision

Full Study Heavy Vehicles

BAYVIEW RD

SCOTT ST/ALBERT ST

| Time Period | Northbound | | | Southbound | | | Eastbound | | | Westbound | | | W TOT | STR TOT | Grand Total | |
|-------------|------------|----|----|------------|----|----|-----------|----------|------------|-----------|----|-----|----------|------------|----------------|-------|
| | LT | ST | RT | N TOT | LT | ST | RT | S TOT | STR TOT | LT | ST | RT | E TOT | | | |
| 07:00 | 07:15 | 0 | 0 | 0 | 0 | 3 | 0 | 2 | 7 | 7 | 2 | 26 | 0 | 45 | 0 | 48 |
| 07:15 | 07:30 | 2 | 0 | 0 | 3 | 0 | 1 | 1 | 2 | 5 | 0 | 31 | 0 | 55 | 0 | 56 |
| 07:30 | 07:45 | 0 | 0 | 2 | 5 | 1 | 2 | 1 | 5 | 10 | 0 | 34 | 1 | 58 | 0 | 64 |
| 07:45 | 08:00 | 0 | 0 | 1 | 3 | 0 | 1 | 1 | 2 | 5 | 0 | 45 | 1 | 72 | 0 | 74 |
| 08:00 | 08:15 | 0 | 0 | 1 | 3 | 2 | 2 | 0 | 7 | 10 | 1 | 49 | 0 | 73 | 0 | 80 |
| 08:15 | 08:30 | 2 | 1 | 1 | 5 | 1 | 1 | 0 | 3 | 8 | 0 | 43 | 0 | 68 | 0 | 72 |
| 08:30 | 08:45 | 2 | 0 | 2 | 6 | 0 | 2 | 2 | 6 | 12 | 0 | 44 | 0 | 69 | 0 | 75 |
| 08:45 | 09:00 | 0 | 1 | 0 | 5 | 3 | 2 | 1 | 7 | 12 | 0 | 36 | 2 | 68 | 0 | 74 |
| 09:00 | 09:15 | 1 | 1 | 0 | 4 | 1 | 0 | 1 | 3 | 7 | 0 | 33 | 1 | 57 | 1 | 60 |
| 09:15 | 09:30 | 0 | 0 | 0 | 2 | 1 | 1 | 1 | 9 | 11 | 3 | 20 | 1 | 47 | 0 | 52 |
| 09:30 | 09:45 | 1 | 2 | 0 | 4 | 0 | 0 | 1 | 9 | 13 | 2 | 21 | 1 | 44 | 0 | 50 |
| 09:45 | 10:00 | 1 | 0 | 0 | 1 | 4 | 0 | 1 | 7 | 8 | 0 | 21 | 0 | 43 | 0 | 49 |
| 11:30 | 11:45 | 1 | 0 | 1 | 2 | 2 | 0 | 0 | 4 | 6 | 0 | 7 | 0 | 19 | 0 | 24 |
| 11:45 | 12:00 | 2 | 1 | 0 | 6 | 1 | 1 | 1 | 4 | 10 | 0 | 15 | 0 | 27 | 2 | 32 |
| 12:00 | 12:15 | 1 | 1 | 1 | 3 | 0 | 0 | 0 | 5 | 8 | 0 | 9 | 0 | 25 | 0 | 31 |
| 12:15 | 12:30 | 0 | 0 | 0 | 1 | 3 | 0 | 2 | 5 | 6 | 0 | 14 | 0 | 27 | 1 | 31 |
| 12:30 | 12:45 | 0 | 1 | 2 | 4 | 1 | 1 | 0 | 7 | 11 | 2 | 13 | 0 | 28 | 0 | 35 |
| 12:45 | 13:00 | 1 | 0 | 0 | 1 | 2 | 0 | 0 | 4 | 5 | 0 | 16 | 0 | 26 | 0 | 30 |
| 13:00 | 13:15 | 0 | 1 | 0 | 2 | 1 | 0 | 0 | 3 | 5 | 0 | 17 | 0 | 29 | 1 | 33 |
| 13:15 | 13:30 | 1 | 0 | 0 | 4 | 1 | 1 | 0 | 6 | 10 | 0 | 16 | 1 | 28 | 1 | 35 |
| 15:00 | 15:15 | 0 | 1 | 0 | 2 | 0 | 1 | 1 | 3 | 5 | 0 | 16 | 0 | 40 | 0 | 42 |
| 15:15 | 15:30 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 2 | 3 | 0 | 14 | 0 | 38 | 0 | 40 |
| 15:30 | 15:45 | 1 | 1 | 0 | 3 | 0 | 1 | 0 | 4 | 7 | 1 | 19 | 0 | 56 | 0 | 59 |
| 15:45 | 16:00 | 1 | 0 | 1 | 2 | 1 | 0 | 0 | 1 | 3 | 0 | 22 | 0 | 48 | 0 | 50 |
| 16:00 | 16:15 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 2 | 0 | 25 | 0 | 56 | 0 | 57 |
| 16:15 | 16:30 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 2 | 0 | 22 | 0 | 57 | 0 | 58 |
| 16:30 | 16:45 | 2 | 0 | 2 | 5 | 0 | 1 | 1 | 3 | 8 | 0 | 17 | 0 | 64 | 0 | 68 |
| 16:45 | 17:00 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 29 | 1 | 64 | 0 | 64 |
| 17:00 | 17:15 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 18 | 0 | 59 | 0 | 60 |
| 17:15 | 17:30 | 0 | 1 | 0 | 2 | 0 | 1 | 0 | 2 | 4 | 0 | 20 | 0 | 51 | 0 | 53 |
| 17:30 | 17:45 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 25 | 0 | 59 | 0 | 60 |
| 17:45 | 18:00 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 15 | 0 | 42 | 0 | 42 |
| Total: | None | 20 | 13 | 15 | 84 | 30 | 21 | 17 | 123 | 207 | 11 | 752 | 9 | 1542 | 6 | 733 |
| | | | | | | | | | | | | | | 3109 | | 1,658 |



Transportation Services - Traffic Services

Turning Movement Count - Study Results

BAYVIEW RD @ SCOTT ST/ALBERT ST

Survey Date: Wednesday, September 07, 2016

WO No: 36277

Start Time: 07:00

Device: Miovision

Full Study 15 Minute U-Turn Total

BAYVIEW RD SCOTT ST/ALBERT ST

| Time Period | | Northbound U-Turn Total | Southbound U-Turn Total | Eastbound U-Turn Total | Westbound U-Turn Total | Total |
|-------------|-------|----------------------------|----------------------------|---------------------------|---------------------------|-------|
| 07:00 | 07:15 | 0 | 0 | 0 | 0 | 0 |
| 07:15 | 07:30 | 0 | 0 | 0 | 0 | 0 |
| 07:30 | 07:45 | 0 | 0 | 0 | 0 | 0 |
| 07:45 | 08:00 | 0 | 0 | 0 | 1 | 1 |
| 08:00 | 08:15 | 0 | 0 | 0 | 0 | 0 |
| 08:15 | 08:30 | 0 | 0 | 0 | 0 | 0 |
| 08:30 | 08:45 | 0 | 0 | 0 | 0 | 0 |
| 08:45 | 09:00 | 0 | 0 | 0 | 0 | 0 |
| 09:00 | 09:15 | 0 | 0 | 0 | 0 | 0 |
| 09:15 | 09:30 | 0 | 0 | 0 | 0 | 0 |
| 09:30 | 09:45 | 0 | 0 | 0 | 0 | 0 |
| 09:45 | 10:00 | 0 | 0 | 0 | 0 | 0 |
| 11:30 | 11:45 | 0 | 0 | 0 | 0 | 0 |
| 11:45 | 12:00 | 0 | 0 | 0 | 0 | 0 |
| 12:00 | 12:15 | 0 | 0 | 0 | 0 | 0 |
| 12:15 | 12:30 | 0 | 0 | 0 | 0 | 0 |
| 12:30 | 12:45 | 0 | 0 | 0 | 0 | 0 |
| 12:45 | 13:00 | 0 | 0 | 0 | 0 | 0 |
| 13:00 | 13:15 | 0 | 0 | 0 | 0 | 0 |
| 13:15 | 13:30 | 0 | 0 | 0 | 0 | 0 |
| 15:00 | 15:15 | 0 | 0 | 0 | 0 | 0 |
| 15:15 | 15:30 | 0 | 0 | 0 | 0 | 0 |
| 15:30 | 15:45 | 0 | 0 | 0 | 0 | 0 |
| 15:45 | 16:00 | 0 | 0 | 0 | 0 | 0 |
| 16:00 | 16:15 | 0 | 0 | 0 | 0 | 0 |
| 16:15 | 16:30 | 0 | 0 | 0 | 0 | 0 |
| 16:30 | 16:45 | 0 | 0 | 0 | 0 | 0 |
| 16:45 | 17:00 | 0 | 0 | 0 | 0 | 0 |
| 17:00 | 17:15 | 0 | 0 | 0 | 0 | 0 |
| 17:15 | 17:30 | 0 | 0 | 0 | 0 | 0 |
| 17:30 | 17:45 | 0 | 0 | 0 | 0 | 0 |
| 17:45 | 18:00 | 0 | 0 | 0 | 0 | 0 |
| Total | | 0 | 0 | 0 | 1 | 1 |

Transportation Services - Traffic Services

Turning Movement Count - Study Results

BAYVIEW RD/BURNSIDE AVE @ SLIDELL ST

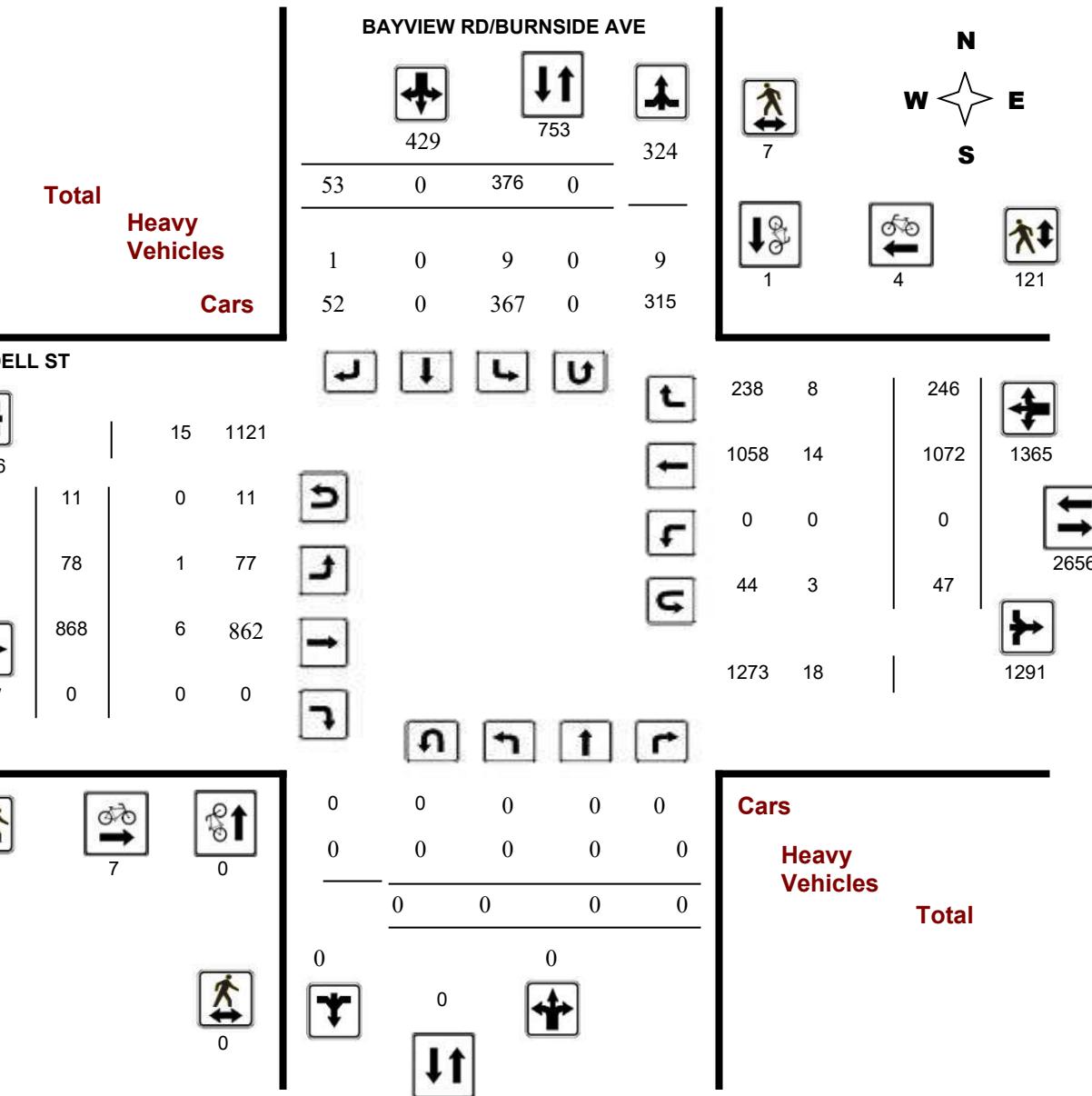
Survey Date: Wednesday, February 26, 2020

WO No: 39631

Start Time: 07:00

Device: Miovision

Full Study Diagram



5478555 - FEB 26 2020 - 8HRS

Transportation Services - Traffic Services

Turning Movement Count - Study Results

BAYVIEW RD/BURNSIDE AVE @ SLIDELL ST

Survey Date: Wednesday, February 26, 2020

Start Time: 07:00

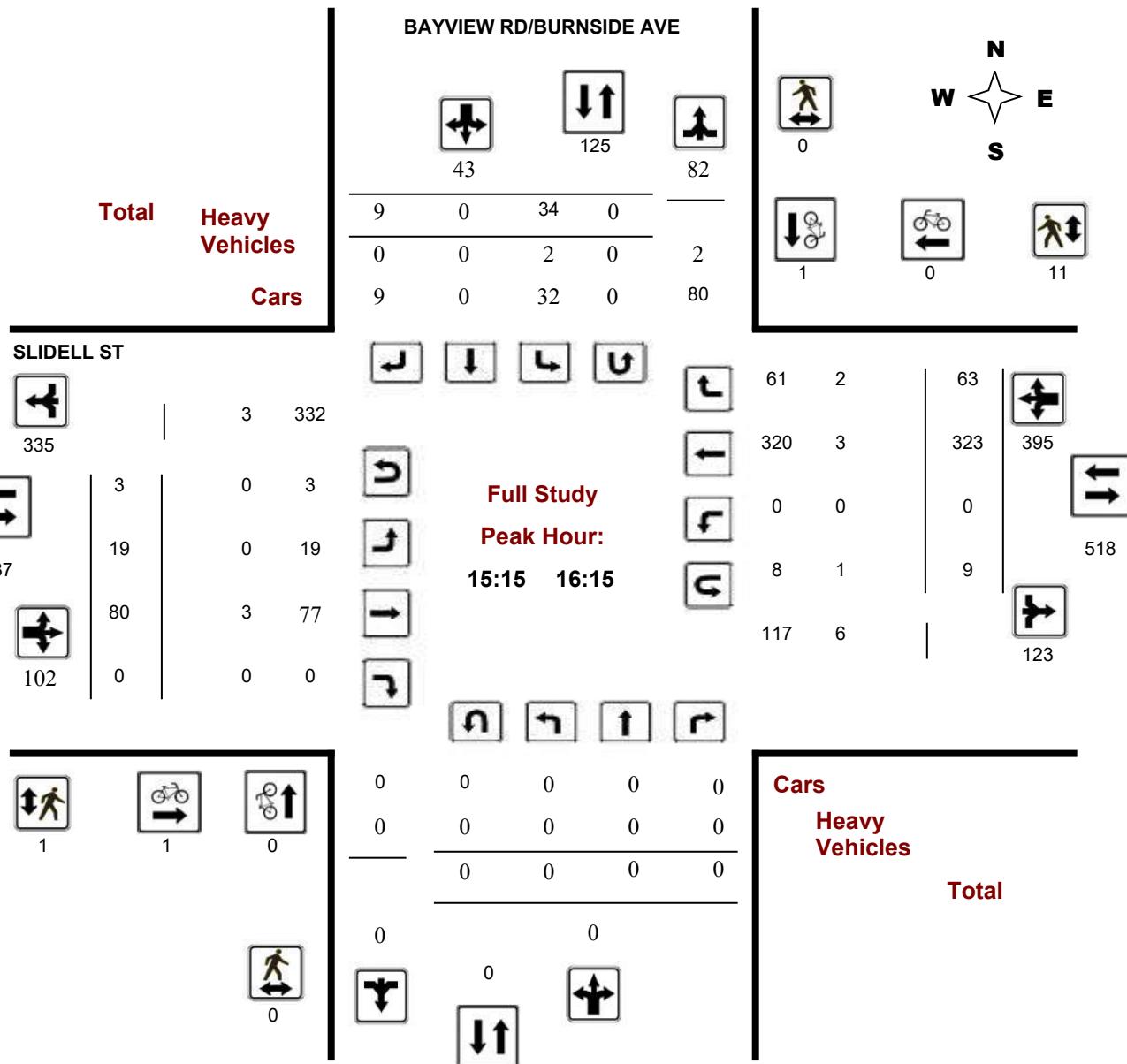
WO No:

39631

Device:

Miovision

Full Study Peak Hour Diagram



5478555 - FEB 26 2020 - 8HRS



Transportation Services - Traffic Services

Turning Movement Count - Peak Hour Diagram

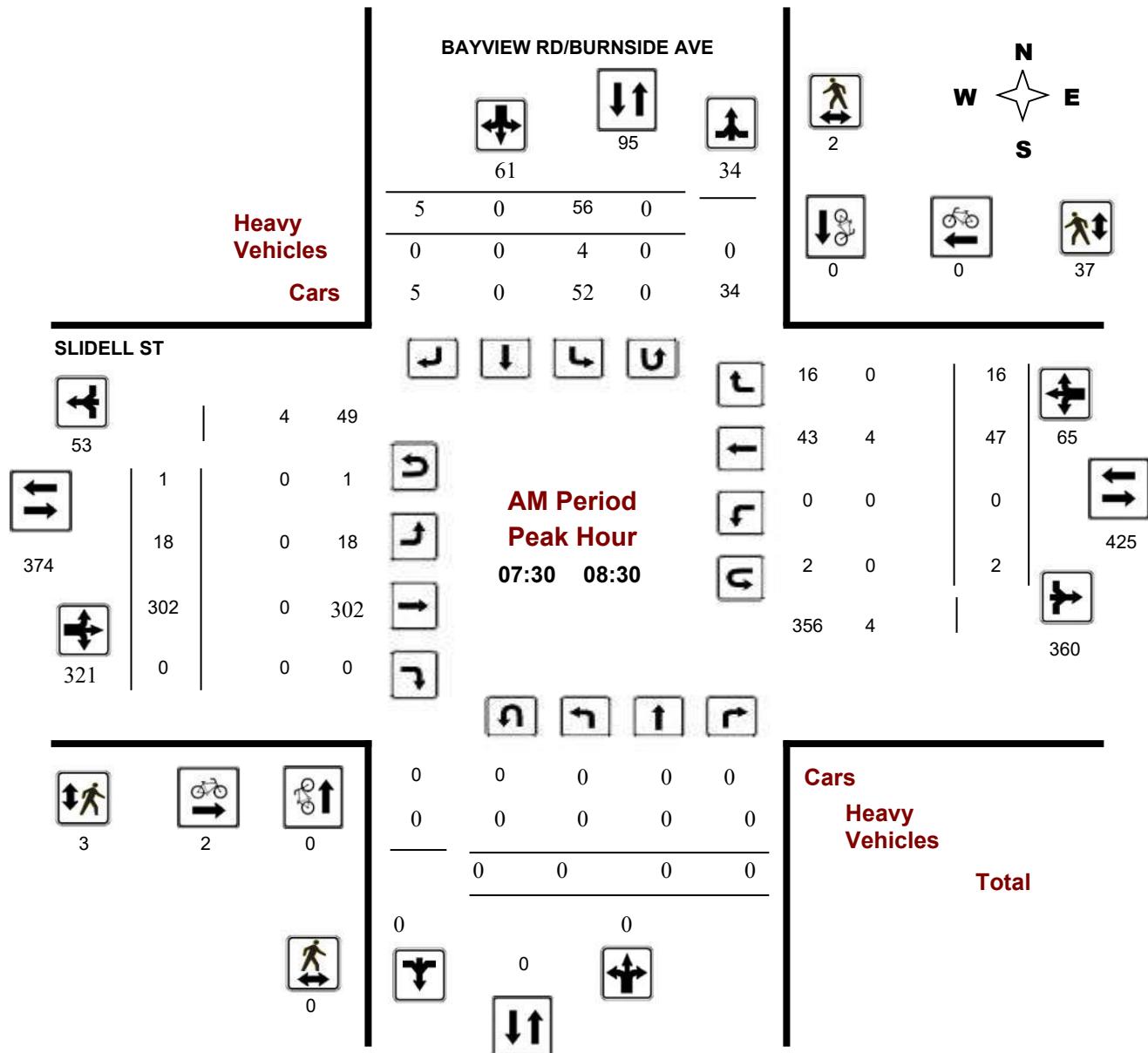
BAYVIEW RD/BURNSIDE AVE @ SLIDELL ST

Survey Date: Wednesday, February 26, 2020

Start Time: 07:00

WO No: 39631

Device: Miovision



Comments 5478555 - FEB 26 2020 - 8HRS



Transportation Services - Traffic Services

Turning Movement Count - Peak Hour Diagram

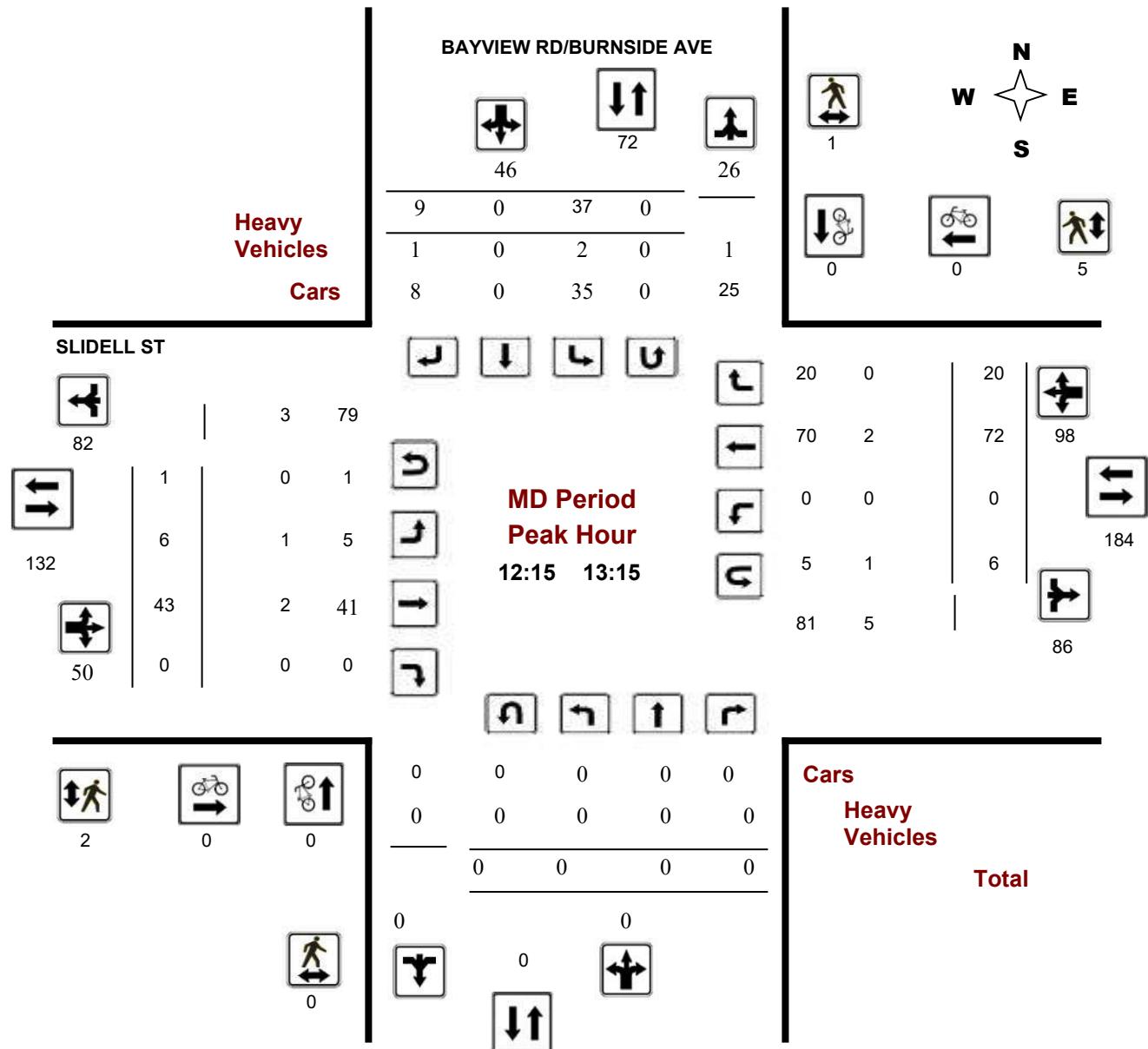
BAYVIEW RD/BURNSIDE AVE @ SLIDELL ST

Survey Date: Wednesday, February 26, 2020

Start Time: 07:00

WO No: 39631

Device: Miovision



Comments 5478555 - FEB 26 2020 - 8HRS

Turning Movement Count - Peak Hour Diagram

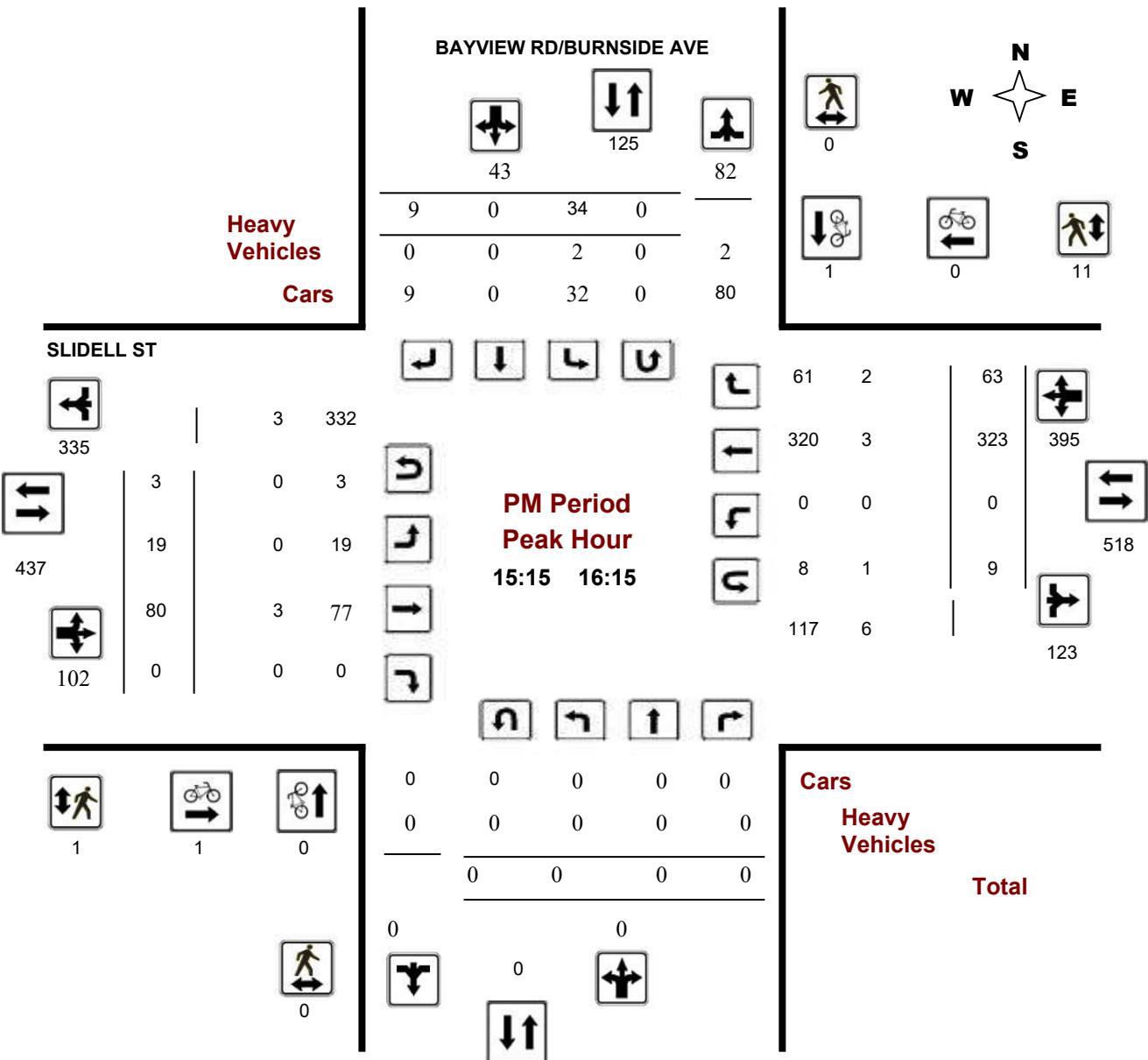
BAYVIEW RD/BURNSIDE AVE @ SLIDELL ST

Survey Date: Wednesday, February 26, 2020

Start Time: 07:00

WO No: 39631

Device: Miovision



Comments 5478555 - FEB 26 2020 - 8HRS



Transportation Services - Traffic Services

Turning Movement Count - Study Results

BAYVIEW RD/BURNSIDE AVE @ SLIDELL ST

Survey Date: Wednesday, February 26, 2020

WO No:

39631

Start Time: 07:00

Device:

Miovision

Full Study Summary (8 HR Standard)

Survey Date: Wednesday, February 26, 2020

Total Observed U-Turns

AADT Factor

| | | | |
|-------------|----|-------------|----|
| Northbound: | 0 | Southbound: | 0 |
| Eastbound: | 11 | Westbound: | 47 |

1.00

BAYVIEW RD/BURNSIDE AVE

SLIDELL ST

| Period | Northbound | | | Southbound | | | SB TOT | STR TOT | Eastbound | | | Westbound | | | WB TOT | STR TOT | Grand Total | | |
|---|------------|----|----|------------|-----|----|-----------|------------|-----------|-----|------|-----------|------|----|-----------|------------|----------------|------|------|
| | LT | ST | RT | NB TOT | LT | ST | RT | | LT | ST | RT | EB TOT | LT | ST | RT | | | | |
| 07:00 08:00 | 0 | 0 | 0 | 0 | 36 | 0 | 6 | 42 | 42 | 16 | 242 | 0 | 258 | 0 | 41 | 8 | 49 | 307 | 349 |
| 08:00 09:00 | 0 | 0 | 0 | 0 | 66 | 0 | 3 | 69 | 69 | 18 | 256 | 0 | 274 | 0 | 54 | 19 | 73 | 347 | 416 |
| 09:00 10:00 | 0 | 0 | 0 | 0 | 110 | 0 | 6 | 116 | 116 | 6 | 62 | 0 | 68 | 0 | 50 | 14 | 64 | 132 | 248 |
| 11:30 12:30 | 0 | 0 | 0 | 0 | 50 | 0 | 9 | 59 | 59 | 6 | 50 | 0 | 56 | 0 | 54 | 18 | 72 | 128 | 187 |
| 12:30 13:30 | 0 | 0 | 0 | 0 | 30 | 0 | 6 | 36 | 36 | 5 | 38 | 0 | 43 | 0 | 76 | 22 | 98 | 141 | 177 |
| 15:00 16:00 | 0 | 0 | 0 | 0 | 39 | 0 | 8 | 47 | 47 | 20 | 72 | 0 | 92 | 0 | 319 | 54 | 373 | 465 | 512 |
| 16:00 17:00 | 0 | 0 | 0 | 0 | 27 | 0 | 8 | 35 | 35 | 4 | 74 | 0 | 78 | 0 | 296 | 73 | 369 | 447 | 482 |
| 17:00 18:00 | 0 | 0 | 0 | 0 | 18 | 0 | 7 | 25 | 25 | 3 | 74 | 0 | 77 | 0 | 182 | 38 | 220 | 297 | 322 |
| Sub Total | 0 | 0 | 0 | 0 | 376 | 0 | 53 | 429 | 429 | 78 | 868 | 0 | 946 | 0 | 1072 | 246 | 1318 | 2264 | 2693 |
| U Turns | | | | 0 | | | | | 0 | | | 11 | | | 47 | | 58 | | |
| Total | 0 | 0 | 0 | 0 | 376 | 0 | 53 | 429 | 429 | 78 | 868 | 0 | 957 | 0 | 1072 | 246 | 1365 | 2322 | 2751 |
| EQ 12Hr | 0 | 0 | 0 | 0 | 523 | 0 | 74 | 596 | 596 | 108 | 1207 | 0 | 1330 | 0 | 1490 | 342 | 1897 | 3228 | 3824 |
| Note: These values are calculated by multiplying the totals by the appropriate expansion factor. | | | | | | | | | | | | | | | 1.39 | | | | |
| Note: These volumes are calculated by multiplying the Equivalent 12 hr. totals by the AADT factor. | | | | | | | | | | | | | | | 1 | | | | |
| AVG 24Hr | 0 | 0 | 0 | 0 | 645 | 0 | 91 | 736 | 736 | 134 | 1490 | 0 | 1642 | 0 | 1840 | 422 | 2342 | 3984 | 4720 |
| Note: These volumes are calculated by multiplying the Average Daily 12 hr. totals by 12 to 24 expansion factor. | | | | | | | | | | | | | | | 1.31 | | | | |
| Note: U-Turns provided for approach totals. Refer to 'U-Turn' Report for specific breakdown. | | | | | | | | | | | | | | | | | | | |



Transportation Services - Traffic Services

Turning Movement Count - Study Results

BAYVIEW RD/BURNSIDE AVE @ SLIDELL ST

Survey Date: Wednesday, February 26, 2020

WO No: 39631

Start Time: 07:00

Device: Miovision

Full Study 15 Minute Increments

BAYVIEW RD/BURNSIDE AVE

SLIDELL ST

Northbound Southbound Eastbound Westbound

| Time Period | LT | ST | RT | N TOT | LT | ST | RT | S TOT | STR TOT | LT | ST | RT | E TOT | LT | ST | RT | W TOT | STR TOT | Grand Total | |
|-------------|-------|----|----|----------|----|-----|----|----------|------------|----|----|-----|----------|-----|----|------|----------|------------|----------------|-------|
| 07:00 | 07:15 | 0 | 0 | 0 | 0 | 8 | 0 | 2 | 10 | 0 | 5 | 31 | 0 | 36 | 0 | 9 | 0 | 10 | 0 | 56 |
| 07:15 | 07:30 | 0 | 0 | 0 | 0 | 3 | 0 | 1 | 4 | 0 | 5 | 56 | 0 | 61 | 0 | 9 | 3 | 13 | 0 | 78 |
| 07:30 | 07:45 | 0 | 0 | 0 | 0 | 12 | 0 | 2 | 14 | 3 | 3 | 73 | 0 | 76 | 0 | 12 | 3 | 15 | 3 | 105 |
| 07:45 | 08:00 | 0 | 0 | 0 | 0 | 13 | 0 | 1 | 14 | 0 | 3 | 82 | 0 | 85 | 0 | 11 | 2 | 14 | 0 | 113 |
| 08:00 | 08:15 | 0 | 0 | 0 | 0 | 10 | 0 | 1 | 11 | 0 | 4 | 73 | 0 | 77 | 0 | 15 | 6 | 21 | 0 | 109 |
| 08:15 | 08:30 | 0 | 0 | 0 | 0 | 21 | 0 | 1 | 22 | 1 | 8 | 74 | 0 | 83 | 0 | 9 | 5 | 15 | 1 | 120 |
| 08:30 | 08:45 | 0 | 0 | 0 | 0 | 10 | 0 | 0 | 10 | 0 | 4 | 64 | 0 | 68 | 0 | 16 | 5 | 22 | 0 | 100 |
| 08:45 | 09:00 | 0 | 0 | 0 | 0 | 25 | 0 | 1 | 26 | 0 | 2 | 45 | 0 | 47 | 0 | 14 | 3 | 20 | 0 | 93 |
| 09:00 | 09:15 | 0 | 0 | 0 | 0 | 44 | 0 | 1 | 45 | 0 | 3 | 19 | 0 | 22 | 0 | 10 | 4 | 18 | 0 | 85 |
| 09:15 | 09:30 | 0 | 0 | 0 | 0 | 23 | 0 | 1 | 24 | 0 | 0 | 19 | 0 | 19 | 0 | 15 | 3 | 19 | 0 | 62 |
| 09:30 | 09:45 | 0 | 0 | 0 | 0 | 28 | 0 | 3 | 31 | 0 | 3 | 12 | 0 | 15 | 0 | 14 | 6 | 21 | 0 | 67 |
| 09:45 | 10:00 | 0 | 0 | 0 | 0 | 15 | 0 | 1 | 16 | 0 | 0 | 12 | 0 | 12 | 0 | 11 | 1 | 13 | 0 | 41 |
| 11:30 | 11:45 | 0 | 0 | 0 | 0 | 11 | 0 | 1 | 12 | 0 | 2 | 13 | 0 | 17 | 0 | 11 | 3 | 16 | 0 | 45 |
| 11:45 | 12:00 | 0 | 0 | 0 | 0 | 16 | 0 | 1 | 17 | 1 | 2 | 18 | 0 | 20 | 0 | 12 | 10 | 23 | 1 | 60 |
| 12:00 | 12:15 | 0 | 0 | 0 | 0 | 12 | 0 | 2 | 14 | 0 | 1 | 6 | 0 | 7 | 0 | 15 | 1 | 17 | 0 | 38 |
| 12:15 | 12:30 | 0 | 0 | 0 | 0 | 11 | 0 | 5 | 16 | 2 | 1 | 13 | 0 | 14 | 0 | 16 | 4 | 21 | 2 | 51 |
| 12:30 | 12:45 | 0 | 0 | 0 | 0 | 10 | 0 | 0 | 10 | 0 | 2 | 13 | 0 | 16 | 0 | 15 | 3 | 18 | 0 | 44 |
| 12:45 | 13:00 | 0 | 0 | 0 | 0 | 8 | 0 | 4 | 12 | 0 | 1 | 8 | 0 | 9 | 0 | 18 | 5 | 27 | 0 | 48 |
| 13:00 | 13:15 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 8 | 1 | 2 | 9 | 0 | 11 | 0 | 23 | 8 | 32 | 1 | 51 |
| 13:15 | 13:30 | 0 | 0 | 0 | 0 | 4 | 0 | 2 | 6 | 0 | 0 | 8 | 0 | 8 | 0 | 20 | 6 | 27 | 0 | 41 |
| 15:00 | 15:15 | 0 | 0 | 0 | 0 | 7 | 0 | 1 | 8 | 0 | 2 | 10 | 0 | 14 | 0 | 74 | 13 | 88 | 0 | 110 |
| 15:15 | 15:30 | 0 | 0 | 0 | 0 | 15 | 0 | 4 | 19 | 1 | 9 | 25 | 0 | 34 | 0 | 80 | 17 | 99 | 1 | 152 |
| 15:30 | 15:45 | 0 | 0 | 0 | 0 | 9 | 0 | 1 | 10 | 0 | 4 | 20 | 0 | 26 | 0 | 67 | 11 | 78 | 0 | 114 |
| 15:45 | 16:00 | 0 | 0 | 0 | 0 | 8 | 0 | 2 | 10 | 1 | 5 | 17 | 0 | 23 | 0 | 98 | 13 | 114 | 1 | 147 |
| 16:00 | 16:15 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 4 | 0 | 1 | 18 | 0 | 19 | 0 | 78 | 22 | 104 | 0 | 127 |
| 16:15 | 16:30 | 0 | 0 | 0 | 0 | 9 | 0 | 3 | 12 | 0 | 2 | 20 | 0 | 22 | 0 | 70 | 24 | 96 | 0 | 130 |
| 16:30 | 16:45 | 0 | 0 | 0 | 0 | 8 | 0 | 1 | 9 | 0 | 1 | 19 | 0 | 20 | 0 | 78 | 18 | 97 | 0 | 126 |
| 16:45 | 17:00 | 0 | 0 | 0 | 0 | 8 | 0 | 2 | 10 | 0 | 0 | 17 | 0 | 18 | 0 | 70 | 9 | 80 | 0 | 108 |
| 17:00 | 17:15 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 4 | 0 | 1 | 24 | 0 | 25 | 0 | 65 | 14 | 81 | 0 | 110 |
| 17:15 | 17:30 | 0 | 0 | 0 | 0 | 3 | 0 | 1 | 4 | 0 | 1 | 23 | 0 | 24 | 0 | 46 | 12 | 60 | 0 | 88 |
| 17:30 | 17:45 | 0 | 0 | 0 | 0 | 6 | 0 | 2 | 8 | 0 | 0 | 16 | 0 | 16 | 0 | 43 | 6 | 49 | 0 | 73 |
| 17:45 | 18:00 | 0 | 0 | 0 | 0 | 7 | 0 | 2 | 9 | 0 | 1 | 11 | 0 | 13 | 0 | 28 | 6 | 37 | 0 | 59 |
| Total: | | 0 | 0 | 0 | 0 | 376 | 0 | 53 | 429 | 10 | 78 | 868 | 0 | 957 | 0 | 1072 | 246 | 1365 | 10 | 2,751 |

Note: U-Turns are included in Totals.



Transportation Services - Traffic Services

Turning Movement Count - Study Results

BAYVIEW RD/BURNSIDE AVE @ SLIDELL ST

Survey Date: Wednesday, February 26, 2020

WO No:

39631

Start Time: 07:00

Device:

Miovision

Full Study Cyclist Volume

BAYVIEW RD/BURNSIDE AVE

SLIDELL ST

| Time Period | Northbound | Southbound | Street Total | Eastbound | Westbound | Street Total | Grand Total |
|-------------|------------|------------|--------------|-----------|-----------|--------------|-------------|
| 07:00 | 07:15 | 0 | 0 | 0 | 1 | 1 | 2 |
| 07:15 | 07:30 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 | 07:45 | 0 | 0 | 0 | 1 | 0 | 1 |
| 07:45 | 08:00 | 0 | 0 | 0 | 1 | 0 | 1 |
| 08:00 | 08:15 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:15 | 08:30 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:30 | 08:45 | 0 | 0 | 0 | 2 | 0 | 2 |
| 08:45 | 09:00 | 0 | 0 | 0 | 1 | 0 | 1 |
| 09:00 | 09:15 | 0 | 0 | 0 | 0 | 0 | 0 |
| 09:15 | 09:30 | 0 | 0 | 0 | 0 | 0 | 0 |
| 09:30 | 09:45 | 0 | 0 | 0 | 0 | 0 | 0 |
| 09:45 | 10:00 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 | 11:45 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 | 12:00 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:00 | 12:15 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:15 | 12:30 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:30 | 12:45 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:45 | 13:00 | 0 | 0 | 0 | 0 | 0 | 0 |
| 13:00 | 13:15 | 0 | 0 | 0 | 0 | 0 | 0 |
| 13:15 | 13:30 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15:00 | 15:15 | 0 | 0 | 0 | 1 | 1 | 1 |
| 15:15 | 15:30 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15:30 | 15:45 | 0 | 0 | 0 | 1 | 0 | 1 |
| 15:45 | 16:00 | 0 | 1 | 1 | 0 | 0 | 1 |
| 16:00 | 16:15 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:15 | 16:30 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:30 | 16:45 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:45 | 17:00 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:00 | 17:15 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:15 | 17:30 | 0 | 0 | 0 | 1 | 1 | 1 |
| 17:30 | 17:45 | 0 | 0 | 0 | 1 | 1 | 1 |
| 17:45 | 18:00 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | | 0 | 1 | 1 | 7 | 4 | 12 |



Transportation Services - Traffic Services

Turning Movement Count - Study Results

BAYVIEW RD/BURNSIDE AVE @ SLIDELL ST

Survey Date: Wednesday, February 26, 2020

WO No:

39631

Start Time: 07:00

Device:

Miovision

Full Study Pedestrian Volume

BAYVIEW RD/BURNSIDE AVE

SLIDELL ST

| Time Period | NB Approach (E or W Crossing) | SB Approach (E or W Crossing) | Total | EB Approach (N or S Crossing) | WB Approach (N or S Crossing) | Total | Grand Total |
|--------------------|----------------------------------|----------------------------------|----------|----------------------------------|----------------------------------|------------|-------------|
| 07:00 07:15 | 0 | 0 | 0 | 0 | 2 | 2 | 2 |
| 07:15 07:30 | 0 | 0 | 0 | 0 | 6 | 6 | 6 |
| 07:30 07:45 | 0 | 0 | 0 | 0 | 5 | 5 | 5 |
| 07:45 08:00 | 0 | 0 | 0 | 1 | 13 | 14 | 14 |
| 08:00 08:15 | 0 | 1 | 1 | 2 | 7 | 9 | 10 |
| 08:15 08:30 | 0 | 1 | 1 | 0 | 12 | 12 | 13 |
| 08:30 08:45 | 0 | 0 | 0 | 0 | 7 | 7 | 7 |
| 08:45 09:00 | 0 | 0 | 0 | 0 | 2 | 2 | 2 |
| 09:00 09:15 | 0 | 0 | 0 | 0 | 3 | 3 | 3 |
| 09:15 09:30 | 0 | 1 | 1 | 0 | 2 | 2 | 3 |
| 09:30 09:45 | 0 | 0 | 0 | 0 | 2 | 2 | 2 |
| 09:45 10:00 | 0 | 0 | 0 | 2 | 2 | 4 | 4 |
| 11:30 11:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 12:00 | 0 | 1 | 1 | 1 | 3 | 4 | 5 |
| 12:00 12:15 | 0 | 0 | 0 | 0 | 1 | 1 | 1 |
| 12:15 12:30 | 0 | 1 | 1 | 2 | 2 | 4 | 5 |
| 12:30 12:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:45 13:00 | 0 | 0 | 0 | 0 | 2 | 2 | 2 |
| 13:00 13:15 | 0 | 0 | 0 | 0 | 1 | 1 | 1 |
| 13:15 13:30 | 0 | 0 | 0 | 0 | 1 | 1 | 1 |
| 15:00 15:15 | 0 | 0 | 0 | 0 | 2 | 2 | 2 |
| 15:15 15:30 | 0 | 0 | 0 | 0 | 2 | 2 | 2 |
| 15:30 15:45 | 0 | 0 | 0 | 0 | 3 | 3 | 3 |
| 15:45 16:00 | 0 | 0 | 0 | 0 | 4 | 4 | 4 |
| 16:00 16:15 | 0 | 0 | 0 | 1 | 2 | 3 | 3 |
| 16:15 16:30 | 0 | 0 | 0 | 2 | 2 | 4 | 4 |
| 16:30 16:45 | 0 | 0 | 0 | 0 | 4 | 4 | 4 |
| 16:45 17:00 | 0 | 0 | 0 | 1 | 7 | 8 | 8 |
| 17:00 17:15 | 0 | 0 | 0 | 0 | 6 | 6 | 6 |
| 17:15 17:30 | 0 | 0 | 0 | 0 | 2 | 2 | 2 |
| 17:30 17:45 | 0 | 0 | 0 | 0 | 9 | 9 | 9 |
| 17:45 18:00 | 0 | 2 | 2 | 3 | 5 | 8 | 10 |
| Total | 0 | 7 | 7 | 15 | 121 | 136 | 143 |

5478555 - FEB 26 2020 - 8HRS



Transportation Services - Traffic Services

Turning Movement Count - Study Results

BAYVIEW RD/BURNSIDE AVE @ SLIDELL ST

Survey Date: Wednesday, February 26, 2020

WO No:

39631

Start Time: 07:00

Device:

Miovision

Full Study Heavy Vehicles

BAYVIEW RD/BURNSIDE AVE

SLIDELL ST

Northbound

Southbound

Eastbound

Westbound

| Time Period | LT | ST | RT | N TOT | LT | ST | RT | S TOT | STR TOT | LT | ST | RT | E TOT | LT | ST | RT | W TOT | STR TOT | Grand Total |
|-------------|-------|----|----|----------|----|----|----|----------|------------|----|----|----|----------|----|----|----|----------|------------|----------------|
| 07:00 | 07:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:15 | 07:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 | 07:45 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 3 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 4 |
| 07:45 | 08:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:00 | 08:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 2 | 2 |
| 08:15 | 08:30 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 2 |
| 08:30 | 08:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:45 | 09:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| 09:00 | 09:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 09:15 | 09:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 09:30 | 09:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 |
| 09:45 | 10:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 | 11:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 2 | 2 |
| 11:45 | 12:00 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 2 |
| 12:00 | 12:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 |
| 12:15 | 12:30 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 2 | 2 | 0 | 1 | 0 | 1 | 0 | 1 | 2 | 4 | |
| 12:30 | 12:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 2 |
| 12:45 | 13:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 |
| 13:00 | 13:15 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 2 |
| 13:15 | 13:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 2 |
| 15:00 | 15:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 2 | 2 |
| 15:15 | 15:30 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 3 | 0 | 3 | 0 | 2 | 2 | 5 | 8 |
| 15:30 | 15:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15:45 | 16:00 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 |
| 16:00 | 16:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:15 | 16:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 2 |
| 16:30 | 16:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:45 | 17:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 |
| 17:00 | 17:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:15 | 17:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:30 | 17:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:45 | 18:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total: None | 0 | 0 | 0 | 0 | 9 | 0 | 1 | 10 | 10 | 1 | 6 | 0 | 7 | 0 | 14 | 8 | 25 | 32 | 42 |



Transportation Services - Traffic Services

Turning Movement Count - Study Results

BAYVIEW RD/BURNSIDE AVE @ SLIDELL ST

Survey Date: Wednesday, February 26, 2020

WO No: 39631

Start Time: 07:00

Device: Miovision

Full Study 15 Minute U-Turn Total

BAYVIEW RD/BURNSIDE AVE

SLIDELL ST

| Time Period | | Northbound U-Turn Total | Southbound U-Turn Total | Eastbound U-Turn Total | Westbound U-Turn Total | Total |
|-------------|-------|----------------------------|----------------------------|---------------------------|---------------------------|-------|
| 07:00 | 07:15 | 0 | 0 | 0 | 1 | 1 |
| 07:15 | 07:30 | 0 | 0 | 0 | 1 | 1 |
| 07:30 | 07:45 | 0 | 0 | 0 | 0 | 0 |
| 07:45 | 08:00 | 0 | 0 | 0 | 1 | 1 |
| 08:00 | 08:15 | 0 | 0 | 0 | 0 | 0 |
| 08:15 | 08:30 | 0 | 0 | 1 | 1 | 2 |
| 08:30 | 08:45 | 0 | 0 | 0 | 1 | 1 |
| 08:45 | 09:00 | 0 | 0 | 0 | 3 | 3 |
| 09:00 | 09:15 | 0 | 0 | 0 | 4 | 4 |
| 09:15 | 09:30 | 0 | 0 | 0 | 1 | 1 |
| 09:30 | 09:45 | 0 | 0 | 0 | 1 | 1 |
| 09:45 | 10:00 | 0 | 0 | 0 | 1 | 1 |
| 11:30 | 11:45 | 0 | 0 | 2 | 2 | 4 |
| 11:45 | 12:00 | 0 | 0 | 0 | 1 | 1 |
| 12:00 | 12:15 | 0 | 0 | 0 | 1 | 1 |
| 12:15 | 12:30 | 0 | 0 | 0 | 1 | 1 |
| 12:30 | 12:45 | 0 | 0 | 1 | 0 | 1 |
| 12:45 | 13:00 | 0 | 0 | 0 | 4 | 4 |
| 13:00 | 13:15 | 0 | 0 | 0 | 1 | 1 |
| 13:15 | 13:30 | 0 | 0 | 0 | 1 | 1 |
| 15:00 | 15:15 | 0 | 0 | 2 | 1 | 3 |
| 15:15 | 15:30 | 0 | 0 | 0 | 2 | 2 |
| 15:30 | 15:45 | 0 | 0 | 2 | 0 | 2 |
| 15:45 | 16:00 | 0 | 0 | 1 | 3 | 4 |
| 16:00 | 16:15 | 0 | 0 | 0 | 4 | 4 |
| 16:15 | 16:30 | 0 | 0 | 0 | 2 | 2 |
| 16:30 | 16:45 | 0 | 0 | 0 | 1 | 1 |
| 16:45 | 17:00 | 0 | 0 | 1 | 1 | 2 |
| 17:00 | 17:15 | 0 | 0 | 0 | 2 | 2 |
| 17:15 | 17:30 | 0 | 0 | 0 | 2 | 2 |
| 17:30 | 17:45 | 0 | 0 | 0 | 0 | 0 |
| 17:45 | 18:00 | 0 | 0 | 1 | 3 | 4 |
| Total | | 0 | 0 | 11 | 47 | 58 |

Transportation Services - Traffic Services

Turning Movement Count - Study Results

OTTAWA RIVER PKWY @ RIVER ST/SLIDELL ST

Survey Date: Tuesday, April 25, 2017

Start Time: 07:00

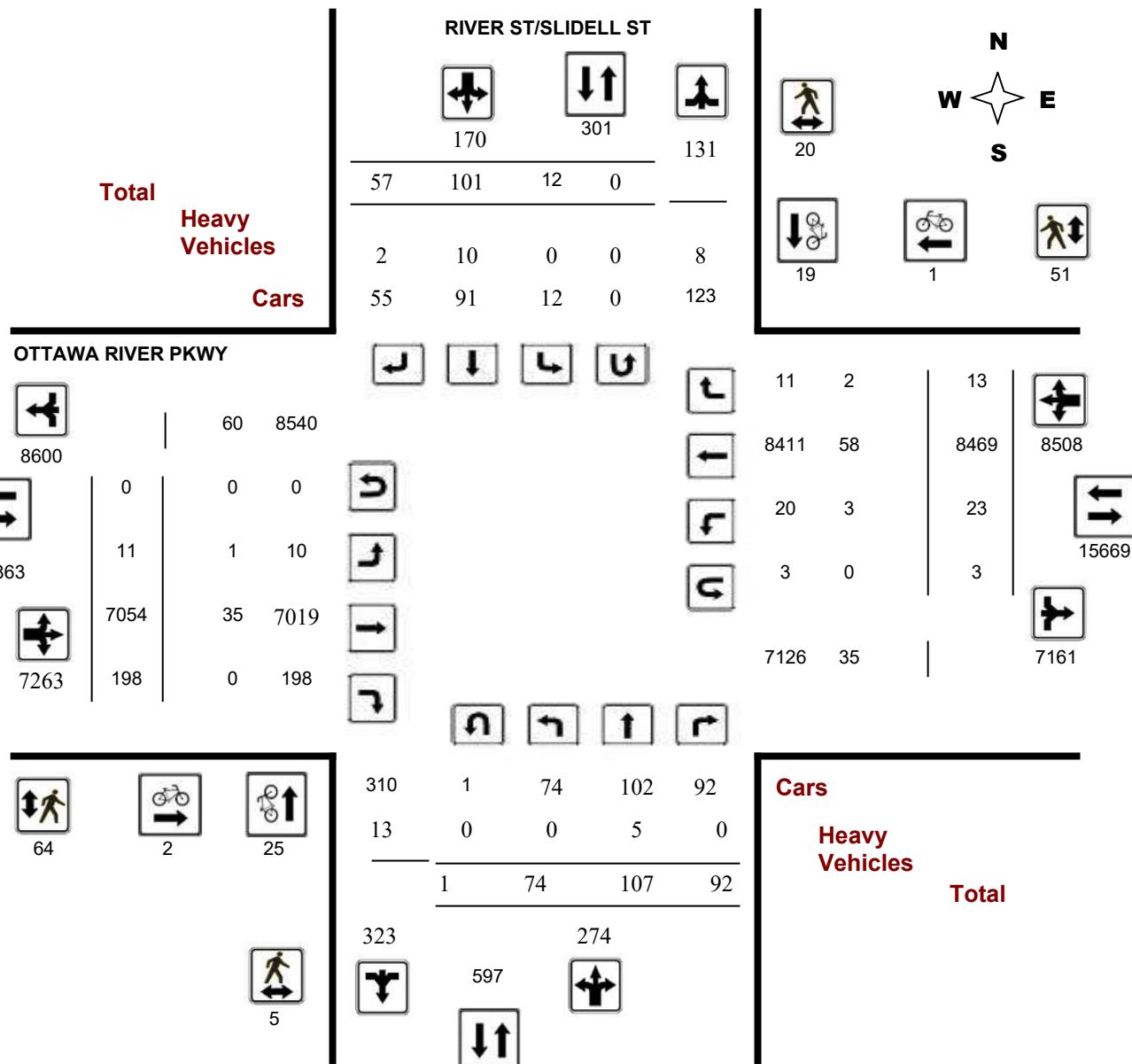
WO No:

36950

Device:

Miovision

Full Study Diagram



Transportation Services - Traffic Services

Turning Movement Count - Study Results

OTTAWA RIVER PKWY @ RIVER ST/SLIDELL ST

Survey Date: Tuesday, April 25, 2017

Start Time: 07:00

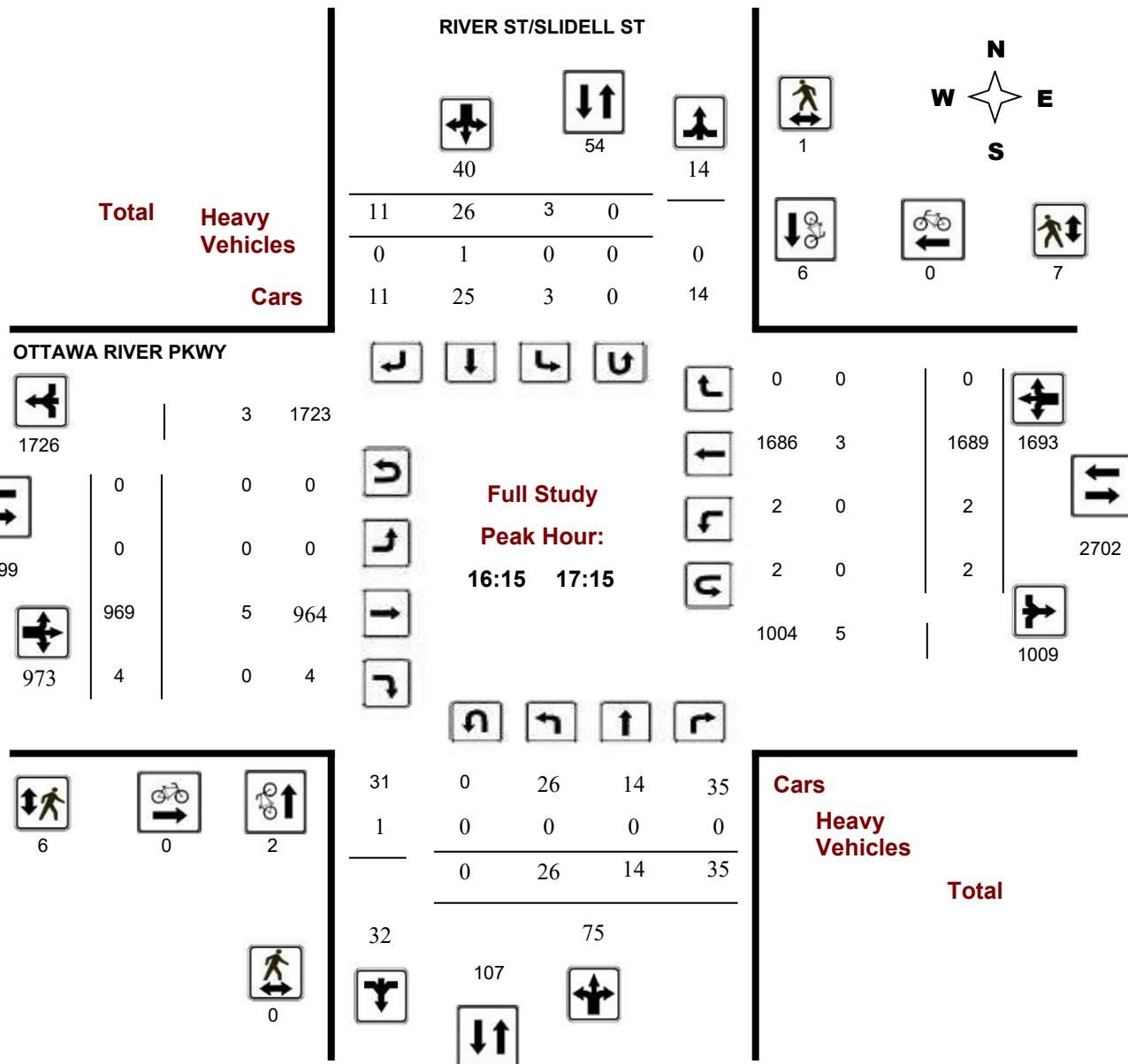
WO No:

36950

Device:

Miovision

Full Study Peak Hour Diagram





Transportation Services - Traffic Services

Turning Movement Count - Peak Hour Diagram

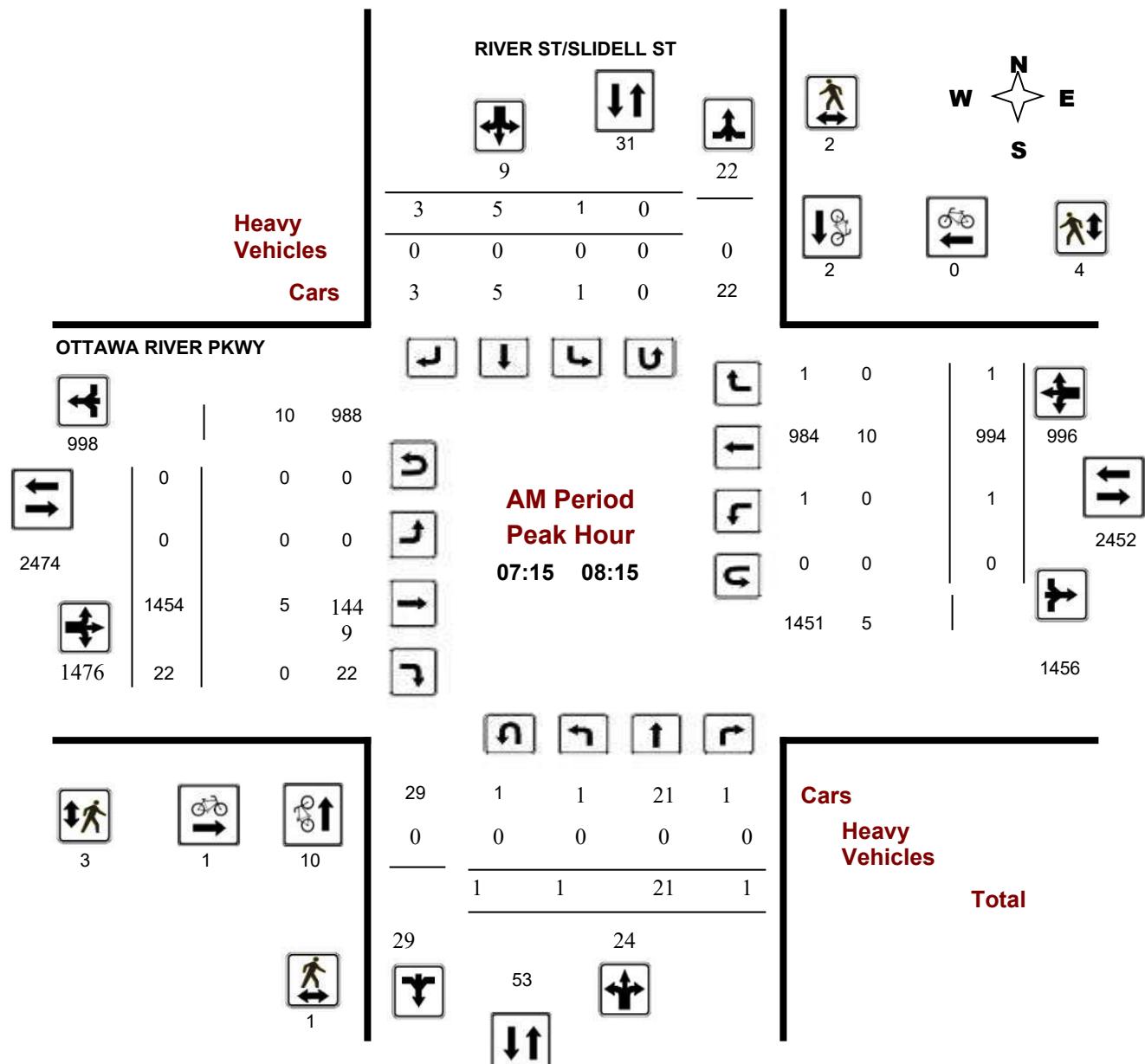
OTTAWA RIVER PKWY @ RIVER ST/SLIDELL ST

Survey Date: Tuesday, April 25, 2017

Start Time: 07:00

WO No: 36950

Device: Miovision





Transportation Services - Traffic Services

Turning Movement Count - Peak Hour Diagram

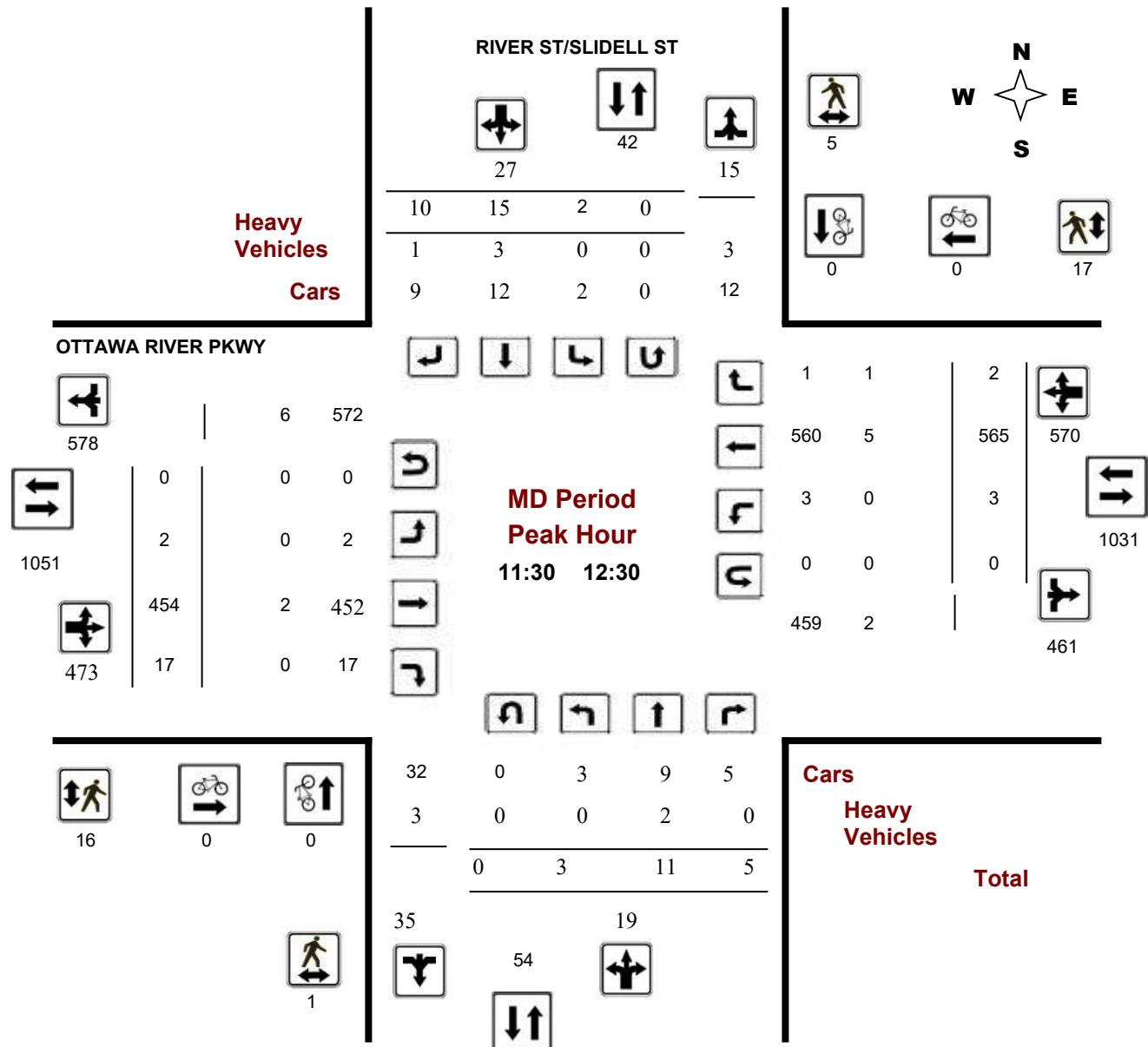
OTTAWA RIVER PKWY @ RIVER ST/SLIDELL ST

Survey Date: Tuesday, April 25, 2017

Start Time: 07:00

WO No: 36950

Device: Miovision





Transportation Services - Traffic Services

Turning Movement Count - Peak Hour Diagram

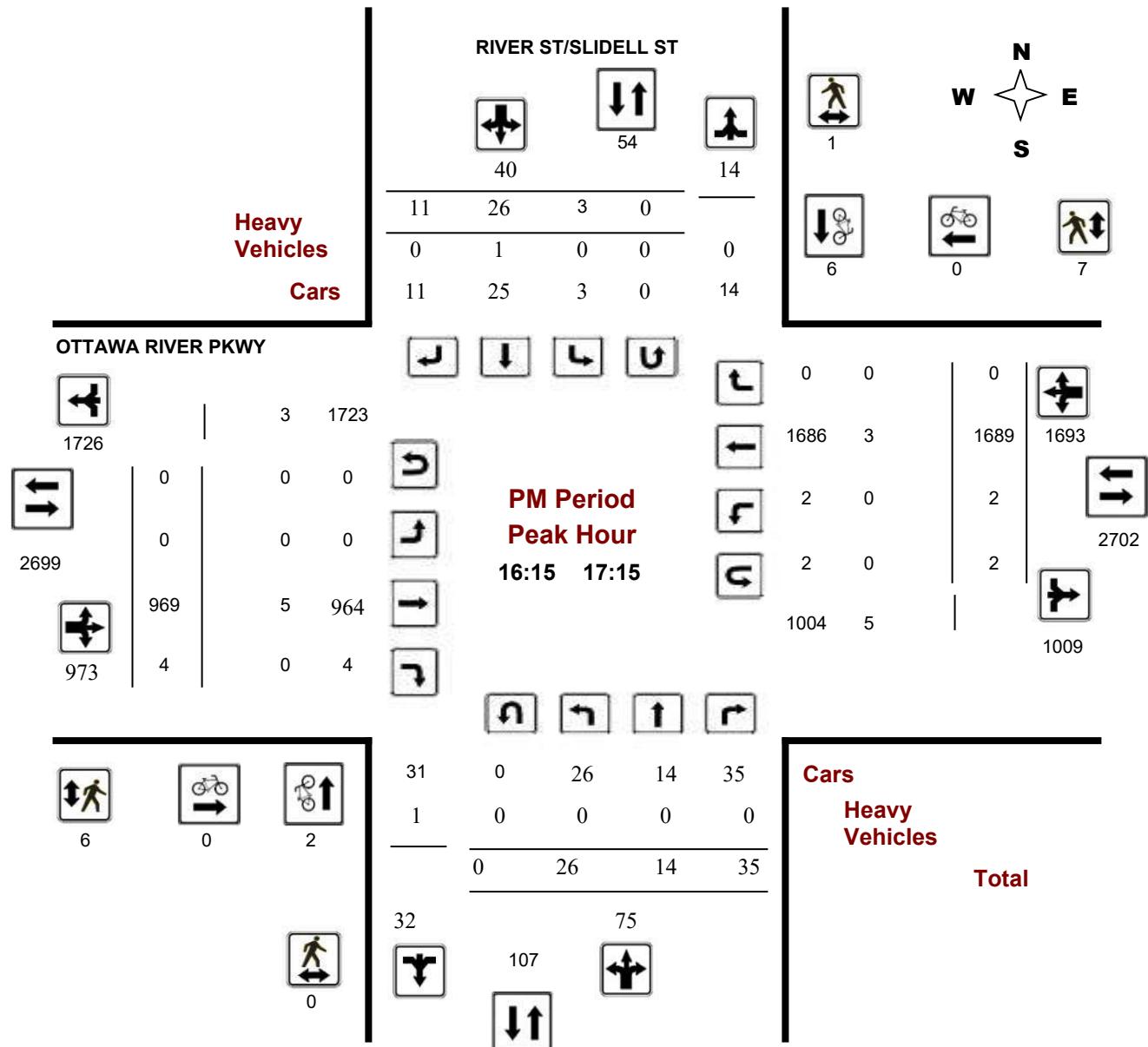
OTTAWA RIVER PKWY @ RIVER ST/SLIDELL ST

Survey Date: Tuesday, April 25, 2017

Start Time: 07:00

WO No: 36950

Device: Miovision





Transportation Services - Traffic Services

Turning Movement Count - Study Results

OTTAWA RIVER PKWY @ RIVER ST/SLIDEELL ST

Survey Date: Tuesday, April 25, 2017

WO No:

36950

Start Time: 07:00

Device:

Miovision

Full Study Summary (8 HR Standard)

Survey Date: Tuesday, April 25, 2017

Total Observed U-Turns

AADT Factor

Northbound: 1 Southbound: 0

1.25

Eastbound: 0 Westbound: 3

RIVER ST/SLIDEELL ST

OTTAWA RIVER PKWY

| Period | Northbound | | | Southbound | | | SB TOT | STR TOT | Eastbound | | | Westbound | | | WB TOT | STR TOT | Grand Total | | |
|------------------|------------|-----|----|------------|----|-----|-----------|------------|-----------|----|------|-----------|------|----|-----------|------------|----------------|-------|-------|
| | LT | ST | RT | NB TOT | LT | ST | RT | | LT | ST | RT | EB TOT | LT | ST | RT | | | | |
| 07:00 08:00 | 1 | 22 | 0 | 23 | 1 | 4 | 2 | 7 | 30 | 0 | 1315 | 21 | 1336 | 0 | 986 | 1 | 987 | 2323 | 2353 |
| 08:00 09:00 | 0 | 28 | 4 | 32 | 0 | 8 | 4 | 12 | 44 | 1 | 1401 | 39 | 1441 | 1 | 909 | 1 | 911 | 2352 | 2396 |
| 09:00 10:00 | 2 | 15 | 2 | 19 | 0 | 14 | 5 | 19 | 38 | 2 | 698 | 80 | 780 | 3 | 693 | 5 | 701 | 1481 | 1519 |
| 11:30 12:30 | 3 | 11 | 5 | 19 | 2 | 15 | 10 | 27 | 46 | 2 | 454 | 17 | 473 | 3 | 565 | 2 | 570 | 1043 | 1089 |
| 12:30 13:30 | 4 | 7 | 7 | 18 | 3 | 11 | 6 | 20 | 38 | 6 | 418 | 20 | 444 | 10 | 529 | 1 | 540 | 984 | 1022 |
| 15:00 16:00 | 10 | 2 | 22 | 34 | 3 | 9 | 10 | 22 | 56 | 0 | 993 | 12 | 1005 | 2 | 1502 | 0 | 1504 | 2509 | 2565 |
| 16:00 17:00 | 27 | 15 | 38 | 80 | 3 | 24 | 11 | 38 | 118 | 0 | 954 | 3 | 957 | 0 | 1684 | 0 | 1684 | 2641 | 2759 |
| 17:00 18:00 | 27 | 7 | 14 | 48 | 0 | 16 | 9 | 25 | 73 | 0 | 821 | 6 | 827 | 4 | 1601 | 3 | 1608 | 2435 | 2508 |
| Sub Total | 74 | 107 | 92 | 273 | 12 | 101 | 57 | 170 | 443 | 11 | 7054 | 198 | 7263 | 23 | 8469 | 13 | 8505 | 15768 | 16211 |
| U Turns | | | | 1 | | | | 0 | 1 | | | | 0 | | | 3 | 3 | 4 | |
| Total | 74 | 107 | 92 | 274 | 12 | 101 | 57 | 170 | 444 | 11 | 7054 | 198 | 7263 | 23 | 8469 | 13 | 8508 | 15771 | 16215 |

EQ 12Hr 103 149 128 381 17 140 79 236 617 15 9805 275 10096 32 11772 18 11826 21922 22539

Note: These values are calculated by multiplying the totals by the appropriate expansion factor.

1.39

AVG 12Hr 93 134 115 343 15 126 71 213 555 14 8825 248 9086 29 10595 16 10644 19730 20285

Note: These volumes are calculated by multiplying the Equivalent 12 hr. totals by the AADT factor.

0.9

AVG 24Hr 121 175 151 449 20 166 93 279 728 18 11560 324 11903 38 13879 21 13943 25846 26574

Note: These volumes are calculated by multiplying the Average Daily 12 hr. totals by 12 to 24 expansion factor.

1.31

Note: U-Turns provided for approach totals. Refer to 'U-Turn' Report for specific breakdown.



Transportation Services - Traffic Services

Turning Movement Count - Study Results

OTTAWA RIVER PKWY @ RIVER ST/SLIDEELL ST

Survey Date: Tuesday, April 25, 2017

WO No: 36950

Start Time: 07:00

Device: Miovision

Full Study 15 Minute Increments

RIVER ST/SLIDEELL ST

OTTAWA RIVER PKWY

| Time Period | Northbound | | | Southbound | | | Eastbound | | | Westbound | | | Grand Total | | | | | | | |
|-------------|------------|----|-----|------------|-----|----|-----------|-------|---------|-----------|-----|------|-------------|------|-----|------|-----|------|-----|--------|
| | LT | ST | RT | N TOT | LT | ST | RT | S TOT | STR TOT | LT | ST | RT | E TOT | | | | | | | |
| 07:00 | 07:15 | 0 | 10 | 0 | 10 | 0 | 0 | 0 | 28 | 0 | 268 | 8 | 276 | 0 | 246 | 28 | 532 | | | |
| 07:15 | 07:30 | 1 | 2 | 0 | 3 | 1 | 0 | 1 | 2 | 11 | 0 | 360 | 3 | 363 | 0 | 234 | 1 | 235 | 11 | 603 |
| 07:30 | 07:45 | 0 | 2 | 0 | 3 | 0 | 1 | 1 | 2 | 17 | 0 | 312 | 8 | 320 | 0 | 271 | 0 | 271 | 17 | 596 |
| 07:45 | 08:00 | 0 | 8 | 0 | 8 | 0 | 3 | 0 | 3 | 24 | 0 | 375 | 2 | 377 | 0 | 235 | 0 | 235 | 24 | 623 |
| 08:00 | 08:15 | 0 | 9 | 1 | 10 | 0 | 1 | 1 | 2 | 32 | 0 | 407 | 9 | 416 | 1 | 254 | 0 | 255 | 32 | 683 |
| 08:15 | 08:30 | 0 | 11 | 1 | 12 | 0 | 3 | 1 | 4 | 38 | 0 | 338 | 8 | 346 | 0 | 221 | 0 | 221 | 38 | 583 |
| 08:30 | 08:45 | 0 | 2 | 0 | 2 | 0 | 2 | 2 | 4 | 19 | 0 | 351 | 9 | 360 | 0 | 193 | 0 | 193 | 19 | 559 |
| 08:45 | 09:00 | 0 | 6 | 2 | 8 | 0 | 2 | 0 | 2 | 33 | 1 | 305 | 13 | 319 | 0 | 241 | 1 | 242 | 33 | 571 |
| 09:00 | 09:15 | 1 | 3 | 1 | 5 | 0 | 4 | 2 | 6 | 47 | 0 | 249 | 27 | 276 | 1 | 241 | 1 | 243 | 47 | 530 |
| 09:15 | 09:30 | 0 | 5 | 0 | 5 | 0 | 2 | 1 | 3 | 43 | 0 | 170 | 24 | 194 | 2 | 171 | 2 | 175 | 43 | 377 |
| 09:30 | 09:45 | 0 | 4 | 1 | 5 | 0 | 4 | 1 | 5 | 36 | 1 | 154 | 17 | 172 | 0 | 135 | 0 | 135 | 36 | 317 |
| 09:45 | 10:00 | 1 | 3 | 0 | 4 | 0 | 4 | 1 | 5 | 31 | 1 | 125 | 12 | 138 | 0 | 146 | 2 | 148 | 31 | 295 |
| 11:30 | 11:45 | 1 | 4 | 2 | 7 | 0 | 4 | 3 | 7 | 28 | 0 | 120 | 5 | 125 | 1 | 126 | 0 | 127 | 28 | 266 |
| 11:45 | 12:00 | 0 | 0 | 0 | 0 | 0 | 3 | 5 | 8 | 16 | 2 | 117 | 3 | 122 | 0 | 138 | 0 | 138 | 16 | 268 |
| 12:00 | 12:15 | 1 | 4 | 1 | 6 | 0 | 6 | 1 | 7 | 32 | 0 | 121 | 5 | 126 | 2 | 149 | 2 | 153 | 32 | 292 |
| 12:15 | 12:30 | 1 | 3 | 2 | 6 | 2 | 2 | 1 | 5 | 20 | 0 | 96 | 4 | 100 | 0 | 152 | 0 | 152 | 20 | 263 |
| 12:30 | 12:45 | 1 | 0 | 2 | 3 | 1 | 1 | 1 | 3 | 19 | 2 | 112 | 7 | 121 | 3 | 132 | 0 | 135 | 19 | 262 |
| 12:45 | 13:00 | 1 | 1 | 0 | 2 | 1 | 8 | 3 | 12 | 33 | 2 | 92 | 6 | 100 | 2 | 130 | 0 | 132 | 33 | 246 |
| 13:00 | 13:15 | 1 | 3 | 2 | 6 | 1 | 2 | 0 | 3 | 20 | 1 | 100 | 4 | 105 | 1 | 137 | 0 | 138 | 20 | 252 |
| 13:15 | 13:30 | 1 | 3 | 3 | 7 | 0 | 0 | 2 | 2 | 21 | 1 | 114 | 3 | 118 | 4 | 130 | 1 | 136 | 21 | 263 |
| 15:00 | 15:15 | 1 | 1 | 4 | 6 | 3 | 3 | 2 | 8 | 24 | 0 | 262 | 5 | 267 | 1 | 309 | 0 | 310 | 24 | 591 |
| 15:15 | 15:30 | 1 | 0 | 8 | 9 | 0 | 5 | 3 | 8 | 23 | 0 | 235 | 1 | 236 | 0 | 424 | 0 | 424 | 23 | 677 |
| 15:30 | 15:45 | 4 | 0 | 6 | 10 | 0 | 1 | 1 | 2 | 16 | 0 | 241 | 3 | 244 | 0 | 370 | 0 | 370 | 16 | 626 |
| 15:45 | 16:00 | 4 | 1 | 4 | 9 | 0 | 0 | 4 | 4 | 18 | 0 | 255 | 3 | 258 | 1 | 399 | 0 | 400 | 18 | 671 |
| 16:00 | 16:15 | 9 | 5 | 9 | 23 | 0 | 1 | 2 | 3 | 32 | 0 | 213 | 0 | 213 | 0 | 450 | 0 | 450 | 32 | 689 |
| 16:15 | 16:30 | 6 | 3 | 9 | 18 | 3 | 6 | 4 | 13 | 42 | 0 | 255 | 2 | 257 | 0 | 412 | 0 | 412 | 42 | 700 |
| 16:30 | 16:45 | 6 | 4 | 13 | 23 | 0 | 12 | 5 | 17 | 56 | 0 | 245 | 0 | 245 | 0 | 432 | 0 | 432 | 56 | 717 |
| 16:45 | 17:00 | 6 | 3 | 7 | 16 | 0 | 5 | 0 | 5 | 30 | 0 | 241 | 1 | 242 | 0 | 390 | 0 | 391 | 30 | 654 |
| 17:00 | 17:15 | 8 | 4 | 6 | 18 | 0 | 3 | 2 | 5 | 33 | 0 | 228 | 1 | 229 | 2 | 455 | 0 | 458 | 33 | 710 |
| 17:15 | 17:30 | 11 | 1 | 4 | 16 | 0 | 8 | 2 | 10 | 41 | 0 | 221 | 4 | 225 | 1 | 388 | 1 | 390 | 41 | 641 |
| 17:30 | 17:45 | 4 | 0 | 1 | 5 | 0 | 4 | 4 | 8 | 18 | 0 | 209 | 0 | 209 | 0 | 420 | 1 | 421 | 18 | 643 |
| 17:45 | 18:00 | 4 | 2 | 3 | 9 | 0 | 1 | 1 | 2 | 17 | 0 | 163 | 1 | 164 | 1 | 338 | 1 | 340 | 17 | 515 |
| Total: | | 74 | 107 | 92 | 274 | 12 | 101 | 57 | 170 | 898 | 11 | 7054 | 198 | 7263 | 23 | 8469 | 13 | 8508 | 898 | 16,215 |

Note: U-Turns are included in Totals.



Transportation Services - Traffic Services

Turning Movement Count - Study Results

OTTAWA RIVER PKWY @ RIVER ST/SLIDEELL ST

Survey Date: Tuesday, April 25, 2017

WO No:

36950

Start Time: 07:00

Device:

Miovision

Full Study Cyclist Volume

RIVER ST/SLIDEELL ST

OTTAWA RIVER PKWY

| Time Period | Northbound | Southbound | Street Total | Eastbound | Westbound | Street Total | Grand Total |
|-------------|------------|------------|--------------|-----------|-----------|--------------|-------------|
| 07:00 | 07:15 | 0 | 1 | 1 | 0 | 0 | 1 |
| 07:15 | 07:30 | 1 | 1 | 2 | 0 | 0 | 2 |
| 07:30 | 07:45 | 2 | 1 | 3 | 1 | 0 | 4 |
| 07:45 | 08:00 | 3 | 0 | 3 | 0 | 0 | 3 |
| 08:00 | 08:15 | 4 | 0 | 4 | 0 | 0 | 4 |
| 08:15 | 08:30 | 1 | 0 | 1 | 0 | 0 | 1 |
| 08:30 | 08:45 | 1 | 0 | 1 | 0 | 0 | 1 |
| 08:45 | 09:00 | 1 | 0 | 1 | 0 | 0 | 1 |
| 09:00 | 09:15 | 0 | 0 | 0 | 0 | 0 | 0 |
| 09:15 | 09:30 | 2 | 0 | 2 | 0 | 0 | 2 |
| 09:30 | 09:45 | 2 | 0 | 2 | 0 | 0 | 2 |
| 09:45 | 10:00 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 | 11:45 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 | 12:00 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:00 | 12:15 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:15 | 12:30 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:30 | 12:45 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:45 | 13:00 | 0 | 0 | 0 | 1 | 0 | 1 |
| 13:00 | 13:15 | 0 | 0 | 0 | 0 | 0 | 0 |
| 13:15 | 13:30 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15:00 | 15:15 | 0 | 2 | 2 | 0 | 0 | 2 |
| 15:15 | 15:30 | 1 | 0 | 1 | 0 | 0 | 1 |
| 15:30 | 15:45 | 0 | 1 | 1 | 0 | 1 | 2 |
| 15:45 | 16:00 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:00 | 16:15 | 1 | 3 | 4 | 0 | 0 | 4 |
| 16:15 | 16:30 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:30 | 16:45 | 0 | 2 | 2 | 0 | 0 | 2 |
| 16:45 | 17:00 | 1 | 3 | 4 | 0 | 0 | 4 |
| 17:00 | 17:15 | 1 | 1 | 2 | 0 | 0 | 2 |
| 17:15 | 17:30 | 1 | 0 | 1 | 0 | 0 | 1 |
| 17:30 | 17:45 | 1 | 1 | 2 | 0 | 0 | 2 |
| 17:45 | 18:00 | 2 | 3 | 5 | 0 | 0 | 5 |
| Total | | 25 | 19 | 44 | 2 | 1 | 47 |



Transportation Services - Traffic Services

Turning Movement Count - Study Results

OTTAWA RIVER PKWY @ RIVER ST/SLIDEELL ST

Survey Date: Tuesday, April 25, 2017

WO No:

36950

Start Time: 07:00

Device:

Miovision

Full Study Pedestrian Volume

RIVER ST/SLIDEELL ST

OTTAWA RIVER PKWY

| Time Period | NB Approach (E or W Crossing) | SB Approach (E or W Crossing) | Total | EB Approach (N or S Crossing) | WB Approach (N or S Crossing) | Total | Grand Total |
|--------------------|----------------------------------|----------------------------------|-----------|----------------------------------|----------------------------------|------------|-------------|
| 07:00 07:15 | 0 | 0 | 0 | 2 | 0 | 2 | 2 |
| 07:15 07:30 | 0 | 0 | 0 | 0 | 2 | 2 | 2 |
| 07:30 07:45 | 0 | 2 | 2 | 2 | 0 | 2 | 4 |
| 07:45 08:00 | 1 | 0 | 1 | 1 | 2 | 3 | 4 |
| 08:00 08:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:15 08:30 | 0 | 1 | 1 | 2 | 1 | 3 | 4 |
| 08:30 08:45 | 0 | 0 | 0 | 3 | 3 | 6 | 6 |
| 08:45 09:00 | 0 | 0 | 0 | 1 | 0 | 1 | 1 |
| 09:00 09:15 | 2 | 0 | 2 | 0 | 2 | 2 | 4 |
| 09:15 09:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 09:30 09:45 | 0 | 0 | 0 | 1 | 1 | 2 | 2 |
| 09:45 10:00 | 0 | 0 | 0 | 0 | 3 | 3 | 3 |
| 11:30 11:45 | 0 | 0 | 0 | 1 | 3 | 4 | 4 |
| 11:45 12:00 | 0 | 2 | 2 | 3 | 4 | 7 | 9 |
| 12:00 12:15 | 1 | 2 | 3 | 3 | 6 | 9 | 12 |
| 12:15 12:30 | 0 | 1 | 1 | 9 | 4 | 13 | 14 |
| 12:30 12:45 | 0 | 4 | 4 | 7 | 4 | 11 | 15 |
| 12:45 13:00 | 0 | 3 | 3 | 9 | 0 | 9 | 12 |
| 13:00 13:15 | 0 | 2 | 2 | 4 | 1 | 5 | 7 |
| 13:15 13:30 | 0 | 1 | 1 | 3 | 0 | 3 | 4 |
| 15:00 15:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15:15 15:30 | 0 | 0 | 0 | 0 | 2 | 2 | 2 |
| 15:30 15:45 | 0 | 0 | 0 | 2 | 1 | 3 | 3 |
| 15:45 16:00 | 0 | 0 | 0 | 0 | 1 | 1 | 1 |
| 16:00 16:15 | 0 | 1 | 1 | 1 | 0 | 1 | 2 |
| 16:15 16:30 | 0 | 0 | 0 | 2 | 2 | 4 | 4 |
| 16:30 16:45 | 0 | 1 | 1 | 1 | 2 | 3 | 4 |
| 16:45 17:00 | 0 | 0 | 0 | 0 | 1 | 1 | 1 |
| 17:00 17:15 | 0 | 0 | 0 | 3 | 2 | 5 | 5 |
| 17:15 17:30 | 0 | 0 | 0 | 2 | 0 | 2 | 2 |
| 17:30 17:45 | 1 | 0 | 1 | 1 | 1 | 2 | 3 |
| 17:45 18:00 | 0 | 0 | 0 | 1 | 3 | 4 | 4 |
| Total | 5 | 20 | 25 | 64 | 51 | 115 | 140 |



Transportation Services - Traffic Services

Turning Movement Count - Study Results

OTTAWA RIVER PKWY @ RIVER ST/SLIDELL ST

Survey Date: Tuesday, April 25, 2017

WO No:

36950

Start Time: 07:00

Device:

Miovision

Full Study Heavy Vehicles

RIVER ST/SLIDELL ST

OTTAWA RIVER PKWY

| Time Period | Northbound | | | Southbound | | | Eastbound | | | Westbound | | | Grand Total | | | | | | | |
|-------------|------------|----|----|------------|----|----|-----------|----------|------------|-----------|----|----|-------------|----|----|----|----------|------------|-----|-----|
| | LT | ST | RT | N TOT | LT | ST | RT | S TOT | STR TOT | LT | ST | RT | E TOT | LT | ST | RT | W TOT | STR TOT | | |
| 07:00 | 07:15 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 3 | 0 | 3 | 0 | 3 | 6 | 4 |
| 07:15 | 07:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 5 | 0 | 2 | 0 | 5 | 10 | 5 |
| 07:30 | 07:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 1 | 0 | 2 | 4 | 2 |
| 07:45 | 08:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 0 | 3 | 6 | 3 |
| 08:00 | 08:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 5 | 0 | 4 | 0 | 5 | 10 | 5 |
| 08:15 | 08:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 5 | 0 | 3 | 0 | 5 | 10 | 5 |
| 08:30 | 08:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 2 | 1 |
| 08:45 | 09:00 | 0 | 1 | 0 | 2 | 0 | 1 | 0 | 3 | 5 | 1 | 3 | 0 | 8 | 0 | 4 | 0 | 7 | 15 | 10 |
| 09:00 | 09:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 7 | 0 | 4 | 0 | 7 | 14 | 7 |
| 09:15 | 09:30 | 0 | 1 | 0 | 2 | 0 | 0 | 0 | 1 | 3 | 0 | 2 | 0 | 4 | 1 | 2 | 0 | 5 | 9 | 6 |
| 09:30 | 09:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 8 | 0 | 3 | 0 | 8 | 16 | 8 |
| 09:45 | 10:00 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 3 | 4 | 0 | 0 | 0 | 7 | 0 | 6 | 1 | 7 | 14 | 9 |
| 11:30 | 11:45 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 2 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 2 | 2 |
| 11:45 | 12:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 4 | 0 | 2 | 0 | 4 | 8 | 4 |
| 12:00 | 12:15 | 0 | 2 | 0 | 4 | 0 | 2 | 0 | 5 | 9 | 0 | 0 | 0 | 2 | 0 | 2 | 1 | 3 | 5 | 7 |
| 12:15 | 12:30 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 |
| 12:30 | 12:45 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 1 | 3 | 0 | 1 | 0 | 3 | 1 | 2 | 0 | 4 | 7 | 5 |
| 12:45 | 13:00 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 2 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 2 | 2 |
| 13:00 | 13:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 2 | 1 |
| 13:15 | 13:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15:00 | 15:15 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 2 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 2 | 2 |
| 15:15 | 15:30 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 2 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 2 | 2 |
| 15:30 | 15:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 6 | 0 | 4 | 0 | 6 | 12 | 6 |
| 15:45 | 16:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 6 | 0 | 4 | 0 | 6 | 12 | 6 |
| 16:00 | 16:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 2 | 1 |
| 16:15 | 16:30 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 2 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 2 | 2 |
| 16:30 | 16:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 2 | 1 |
| 16:45 | 17:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 3 | 0 | 1 | 0 | 3 | 6 | 3 |
| 17:00 | 17:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 3 | 0 | 2 | 0 | 3 | 6 | 3 |
| 17:15 | 17:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 2 | 1 |
| 17:30 | 17:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:45 | 18:00 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 2 | 3 | 2 |
| Total: | None | 0 | 5 | 0 | 18 | 0 | 10 | 2 | 20 | 38 | 1 | 35 | 0 | 96 | 3 | 58 | 2 | 98 | 194 | 116 |



Transportation Services - Traffic Services

Turning Movement Count - Study Results

OTTAWA RIVER PKWY @ RIVER ST/SLIDEELL ST

Survey Date: Tuesday, April 25, 2017

WO No: 36950

Start Time: 07:00

Device: Miovision

Full Study 15 Minute U-Turn Total

RIVER ST/SLIDEELL ST OTTAWA RIVER PKWY

| Time Period | | Northbound U-Turn Total | Southbound U-Turn Total | Eastbound U-Turn Total | Westbound U-Turn Total | Total |
|-------------|-------|----------------------------|----------------------------|---------------------------|---------------------------|-------|
| 07:00 | 07:15 | 0 | 0 | 0 | 0 | 0 |
| 07:15 | 07:30 | 0 | 0 | 0 | 0 | 0 |
| 07:30 | 07:45 | 1 | 0 | 0 | 0 | 1 |
| 07:45 | 08:00 | 0 | 0 | 0 | 0 | 0 |
| 08:00 | 08:15 | 0 | 0 | 0 | 0 | 0 |
| 08:15 | 08:30 | 0 | 0 | 0 | 0 | 0 |
| 08:30 | 08:45 | 0 | 0 | 0 | 0 | 0 |
| 08:45 | 09:00 | 0 | 0 | 0 | 0 | 0 |
| 09:00 | 09:15 | 0 | 0 | 0 | 0 | 0 |
| 09:15 | 09:30 | 0 | 0 | 0 | 0 | 0 |
| 09:30 | 09:45 | 0 | 0 | 0 | 0 | 0 |
| 09:45 | 10:00 | 0 | 0 | 0 | 0 | 0 |
| 11:30 | 11:45 | 0 | 0 | 0 | 0 | 0 |
| 11:45 | 12:00 | 0 | 0 | 0 | 0 | 0 |
| 12:00 | 12:15 | 0 | 0 | 0 | 0 | 0 |
| 12:15 | 12:30 | 0 | 0 | 0 | 0 | 0 |
| 12:30 | 12:45 | 0 | 0 | 0 | 0 | 0 |
| 12:45 | 13:00 | 0 | 0 | 0 | 0 | 0 |
| 13:00 | 13:15 | 0 | 0 | 0 | 0 | 0 |
| 13:15 | 13:30 | 0 | 0 | 0 | 1 | 1 |
| 15:00 | 15:15 | 0 | 0 | 0 | 0 | 0 |
| 15:15 | 15:30 | 0 | 0 | 0 | 0 | 0 |
| 15:30 | 15:45 | 0 | 0 | 0 | 0 | 0 |
| 15:45 | 16:00 | 0 | 0 | 0 | 0 | 0 |
| 16:00 | 16:15 | 0 | 0 | 0 | 0 | 0 |
| 16:15 | 16:30 | 0 | 0 | 0 | 0 | 0 |
| 16:30 | 16:45 | 0 | 0 | 0 | 0 | 0 |
| 16:45 | 17:00 | 0 | 0 | 0 | 1 | 1 |
| 17:00 | 17:15 | 0 | 0 | 0 | 1 | 1 |
| 17:15 | 17:30 | 0 | 0 | 0 | 0 | 0 |
| 17:30 | 17:45 | 0 | 0 | 0 | 0 | 0 |
| 17:45 | 18:00 | 0 | 0 | 0 | 0 | 0 |
| Total | | 1 | 0 | 0 | 3 | 4 |

Transportation Services - Traffic Services

Turning Movement Count - Study Results

PARKDALE AVE @ BURNSIDE AVE

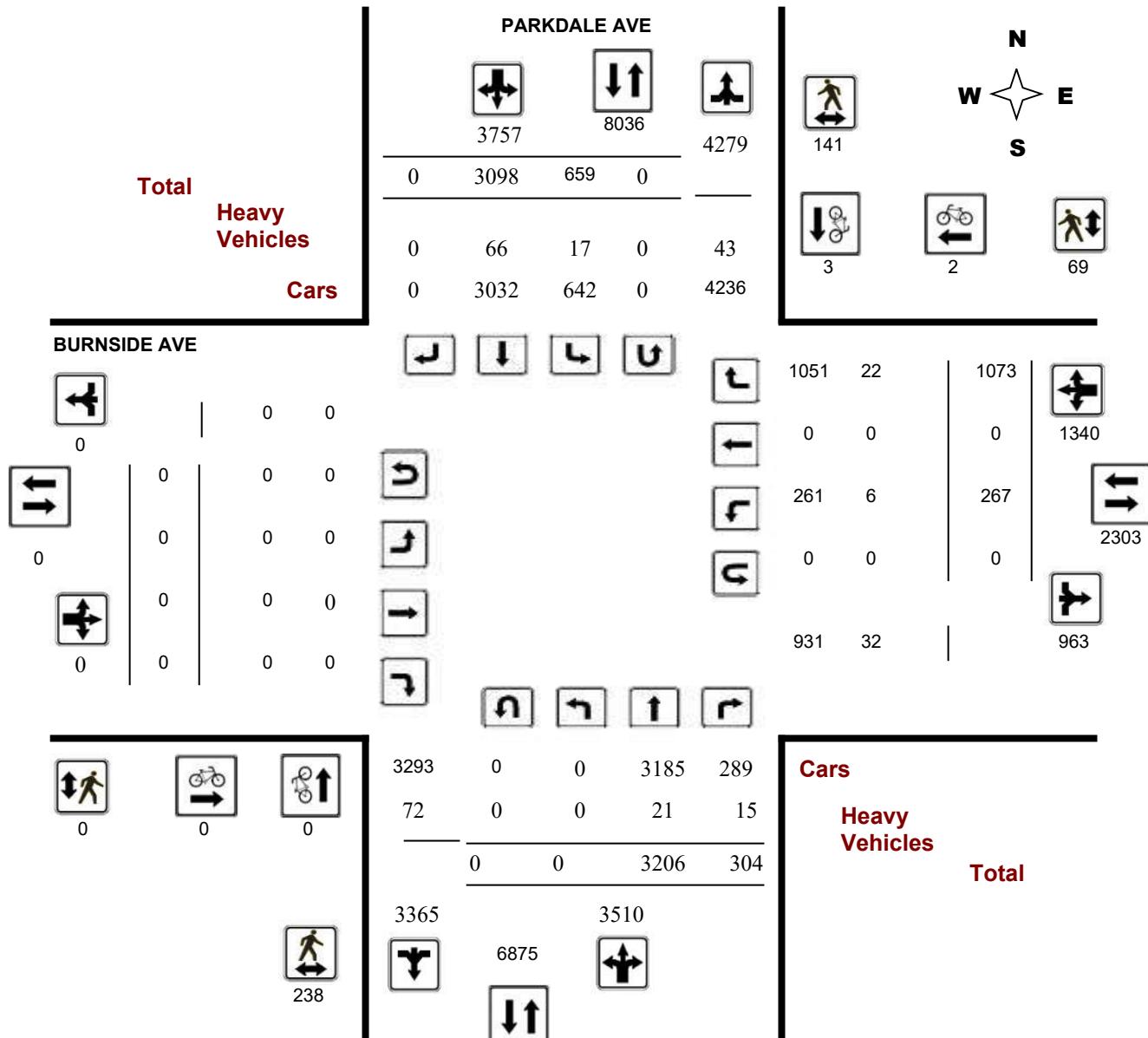
Survey Date: Thursday, February 22, 2018

WO No: 37573

Start Time: 07:00

Device: Miovision

Full Study Diagram



Transportation Services - Traffic Services

Turning Movement Count - Study Results

PARKDALE AVE @ BURNSIDE AVE

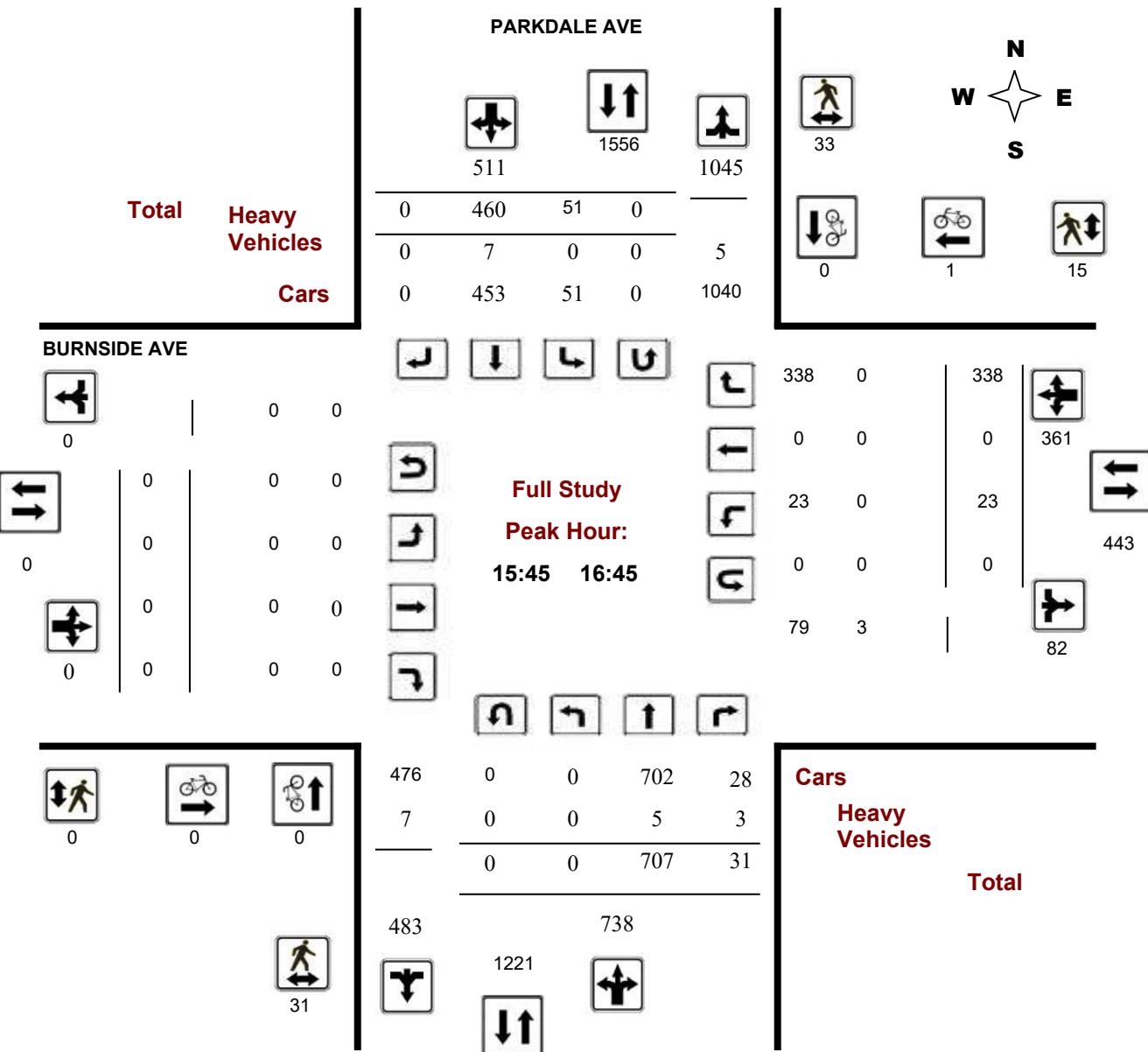
Survey Date: Thursday, February 22, 2018

WO No: 37573

Start Time: 07:00

Device: Miovision

Full Study Peak Hour Diagram



Turning Movement Count - Peak Hour Diagram

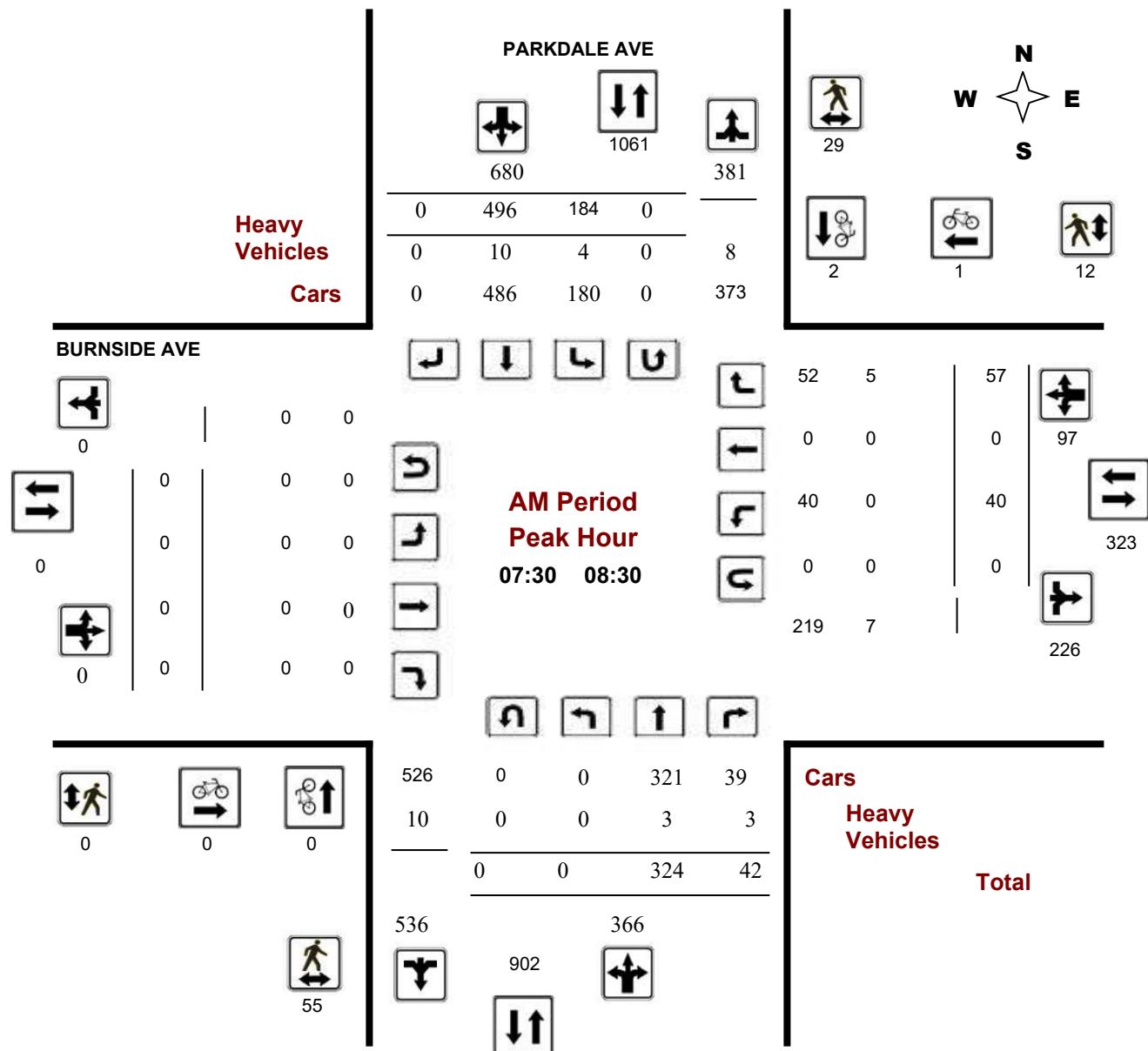
PARKDALE AVE @ BURNSIDE AVE

Survey Date: Thursday, February 22, 2018

Start Time: 07:00

WO No: 37573

Device: Miovision



Turning Movement Count - Peak Hour Diagram

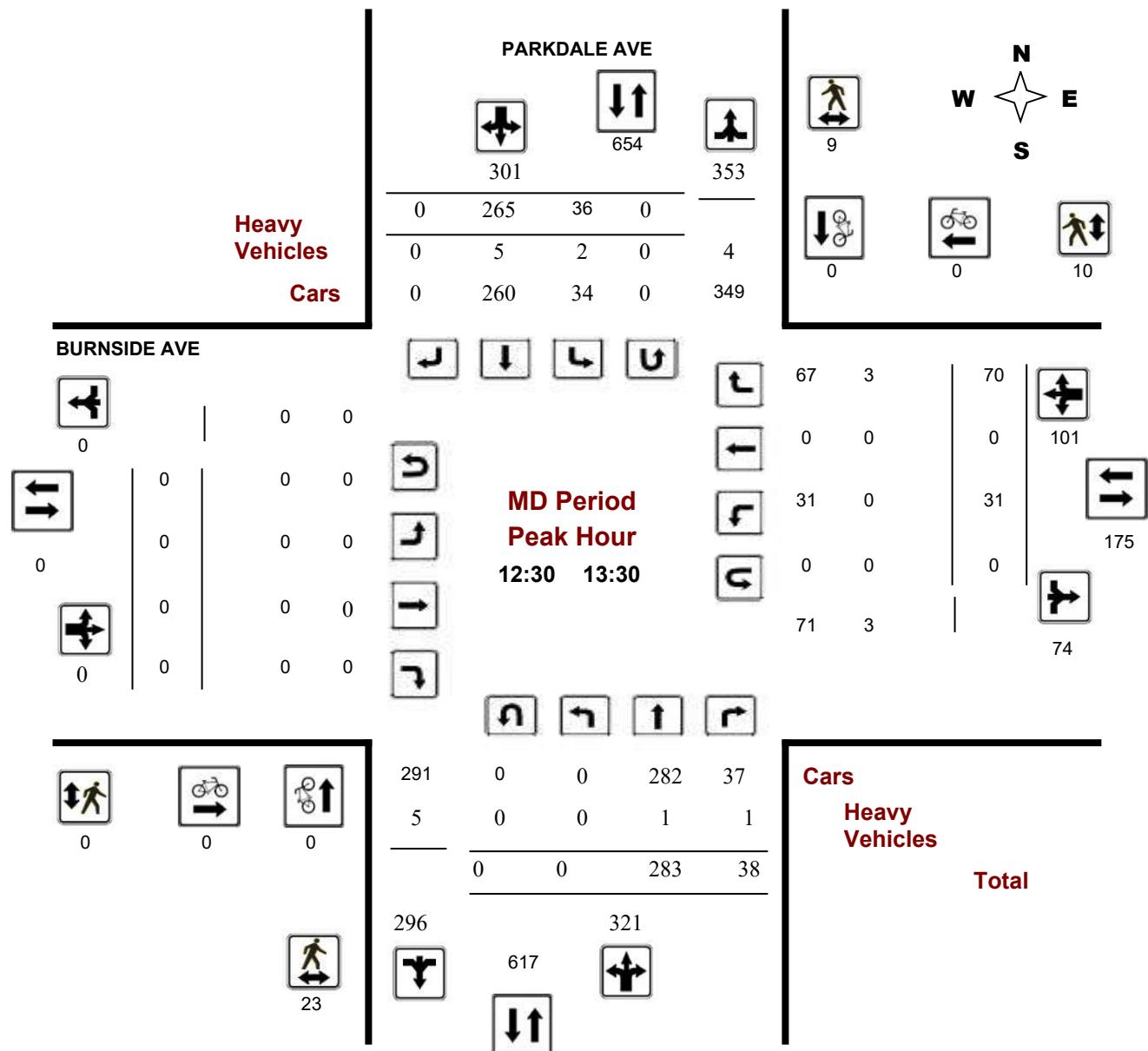
PARKDALE AVE @ BURNSIDE AVE

Survey Date: Thursday, February 22, 2018

Start Time: 07:00

WO No: 37573

Device: Miovision



Turning Movement Count - Peak Hour Diagram

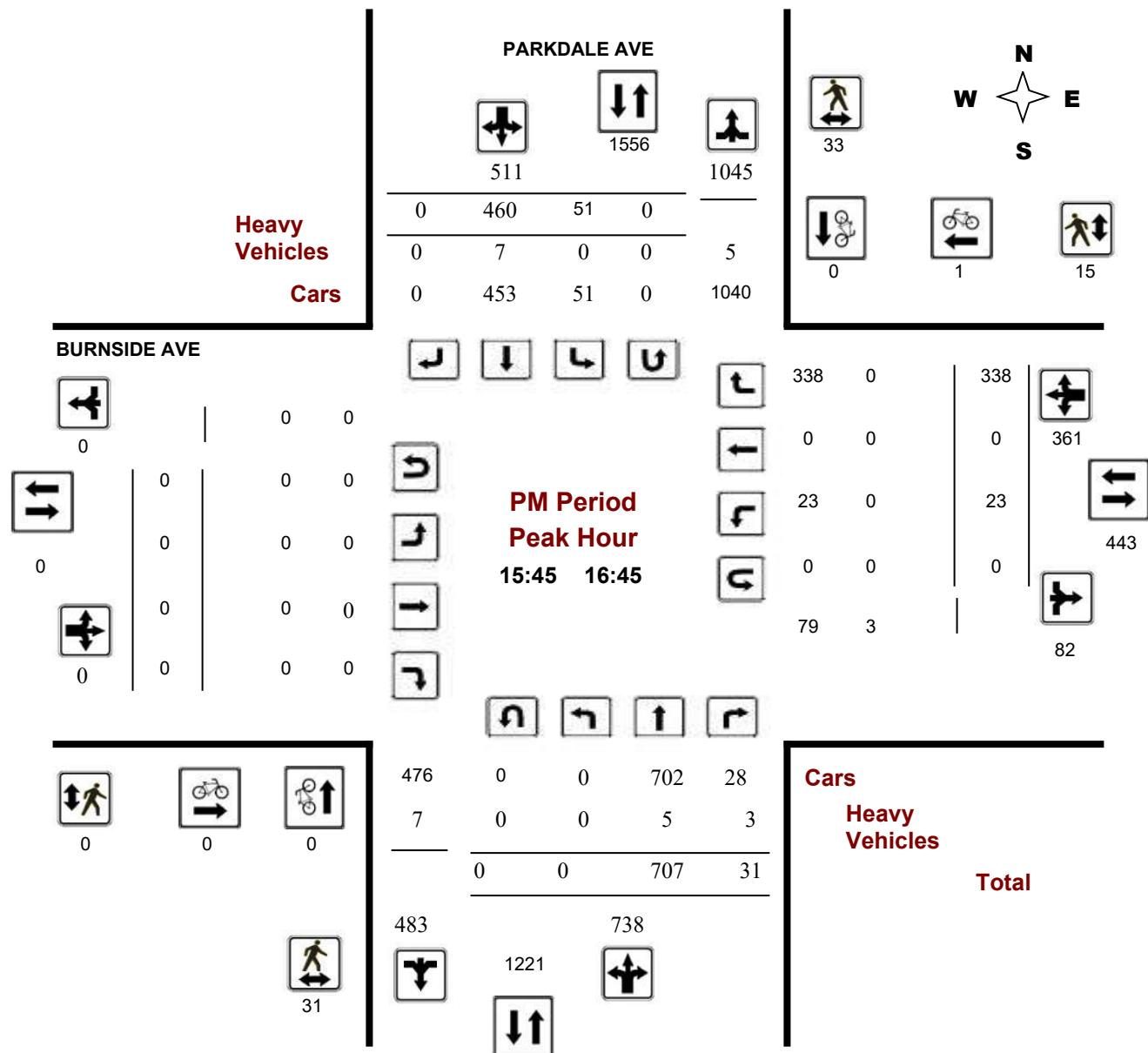
PARKDALE AVE @ BURNSIDE AVE

Survey Date: Thursday, February 22, 2018

Start Time: 07:00

WO No: 37573

Device: Miovision





Transportation Services - Traffic Services

Turning Movement Count - Study Results

PARKDALE AVE @ BURNSIDE AVE

Survey Date: Thursday, February 22, 2018

WO No:

37573

Start Time: 07:00

Device:

Miovision

Full Study Summary (8 HR Standard)

Survey Date: Thursday, February 22, 2018

Total Observed U-Turns

AADT Factor

Northbound: 0 Southbound: 0

1.25

Eastbound: 0 Westbound: 0

PARKDALE AVE

BURNSIDE AVE

| Period | Northbound | | | Southbound | | | SB TOT | STR TOT | Eastbound | | | Westbound | | | WB TOT | STR TOT | Grand Total | | |
|---|------------|------|-----|-------------|------|------|-----------|------------|--------------|----|----|-----------|----|-----|-----------|------------|----------------|-------------|--------------|
| | LT | ST | RT | LT | ST | RT | | | LT | ST | RT | EB TOT | LT | ST | RT | | | | |
| 07:00 08:00 | 0 | 301 | 27 | 328 | 164 | 504 | 0 | 668 | 996 | 0 | 0 | 0 | 0 | 38 | 0 | 39 | 77 | 77 | 1073 |
| 08:00 09:00 | 0 | 308 | 50 | 358 | 189 | 466 | 0 | 655 | 1013 | 0 | 0 | 0 | 0 | 37 | 0 | 65 | 102 | 102 | 1115 |
| 09:00 10:00 | 0 | 204 | 49 | 253 | 70 | 338 | 0 | 408 | 661 | 0 | 0 | 0 | 0 | 33 | 0 | 32 | 65 | 65 | 726 |
| 11:30 12:30 | 0 | 214 | 37 | 251 | 43 | 257 | 0 | 300 | 551 | 0 | 0 | 0 | 0 | 33 | 0 | 59 | 92 | 92 | 643 |
| 12:30 13:30 | 0 | 283 | 38 | 321 | 36 | 265 | 0 | 301 | 622 | 0 | 0 | 0 | 0 | 31 | 0 | 70 | 101 | 101 | 723 |
| 15:00 16:00 | 0 | 718 | 28 | 746 | 42 | 360 | 0 | 402 | 1148 | 0 | 0 | 0 | 0 | 29 | 0 | 274 | 303 | 303 | 1451 |
| 16:00 17:00 | 0 | 659 | 30 | 689 | 61 | 497 | 0 | 558 | 1247 | 0 | 0 | 0 | 0 | 28 | 0 | 326 | 354 | 354 | 1601 |
| 17:00 18:00 | 0 | 519 | 45 | 564 | 54 | 411 | 0 | 465 | 1029 | 0 | 0 | 0 | 0 | 38 | 0 | 208 | 246 | 246 | 1275 |
| Sub Total | 0 | 3206 | 304 | 3510 | 659 | 3098 | 0 | 3757 | 7267 | 0 | 0 | 0 | 0 | 267 | 0 | 1073 | 1340 | 1340 | 8607 |
| U Turns | | | | 0 | | | | 0 | 0 | | | | 0 | | | 0 | 0 | 0 | |
| Total | 0 | 3206 | 304 | 3510 | 659 | 3098 | 0 | 3757 | 7267 | 0 | 0 | 0 | 0 | 267 | 0 | 1073 | 1340 | 1340 | 8607 |
| EQ 12Hr | 0 | 4456 | 423 | 4879 | 916 | 4306 | 0 | 5222 | 10101 | 0 | 0 | 0 | 0 | 371 | 0 | 1491 | 1863 | 1863 | 11964 |
| Note: These values are calculated by multiplying the totals by the appropriate expansion factor. | | | | | | | | | | | | | | | 1.39 | | | | |
| AVG 12Hr | 0 | 4011 | 380 | 4391 | 824 | 3876 | 0 | 4700 | 9091 | 0 | 0 | 0 | 0 | 334 | 0 | 1342 | 1676 | 1677 | 10768 |
| Note: These volumes are calculated by multiplying the Equivalent 12 hr. totals by the AADT factor. | | | | | | | | | | | | | | | 0.9 | | | | |
| AVG 24Hr | 0 | 5254 | 498 | 5752 | 1080 | 5077 | 0 | 6157 | 11909 | 0 | 0 | 0 | 0 | 438 | 0 | 1758 | 2196 | 2196 | 14105 |
| Note: These volumes are calculated by multiplying the Average Daily 12 hr. totals by 12 to 24 expansion factor. | | | | | | | | | | | | | | | 1.31 | | | | |
| Note: U-Turns provided for approach totals. Refer to 'U-Turn' Report for specific breakdown. | | | | | | | | | | | | | | | | | | | |



Transportation Services - Traffic Services

Turning Movement Count - Study Results

PARKDALE AVE @ BURNSIDE AVE

Survey Date: Thursday, February 22, 2018

WO No:

37573

Start Time: 07:00

Device:

Miovision

Full Study 15 Minute Increments

PARKDALE AVE

BURNSIDE AVE

| Time Period | Northbound | | | Southbound | | | Eastbound | | | Westbound | | | Grand Total | | | | | | | |
|-------------|------------|----|------|------------|------|-----|-----------|-------|---------|-----------|----|----|-------------|---|-----|---|------|------|-------|-------|
| | LT | ST | RT | N TOT | LT | ST | RT | S TOT | STR TOT | LT | ST | RT | E TOT | | | | | | | |
| 07:00 | 07:15 | 0 | 75 | 6 | 81 | 39 | 142 | 0 | 181 | 493 | 0 | 0 | 0 | 9 | 0 | 5 | 14 | 493 | 276 | |
| 07:15 | 07:30 | 0 | 67 | 6 | 73 | 45 | 116 | 0 | 161 | 439 | 0 | 0 | 0 | 0 | 11 | 0 | 11 | 22 | 439 | 256 |
| 07:30 | 07:45 | 0 | 80 | 8 | 88 | 42 | 137 | 0 | 179 | 500 | 0 | 0 | 0 | 0 | 8 | 0 | 8 | 16 | 500 | 283 |
| 07:45 | 08:00 | 0 | 79 | 7 | 86 | 38 | 109 | 0 | 147 | 446 | 0 | 0 | 0 | 0 | 10 | 0 | 15 | 25 | 446 | 258 |
| 08:00 | 08:15 | 0 | 80 | 15 | 95 | 58 | 121 | 0 | 179 | 507 | 0 | 0 | 0 | 0 | 14 | 0 | 18 | 32 | 507 | 306 |
| 08:15 | 08:30 | 0 | 85 | 12 | 97 | 46 | 129 | 0 | 175 | 510 | 0 | 0 | 0 | 0 | 8 | 0 | 16 | 24 | 510 | 296 |
| 08:30 | 08:45 | 0 | 67 | 9 | 76 | 46 | 128 | 0 | 174 | 462 | 0 | 0 | 0 | 0 | 4 | 0 | 13 | 17 | 462 | 267 |
| 08:45 | 09:00 | 0 | 76 | 14 | 90 | 39 | 88 | 0 | 127 | 410 | 0 | 0 | 0 | 0 | 11 | 0 | 18 | 29 | 410 | 246 |
| 09:00 | 09:15 | 0 | 62 | 20 | 82 | 21 | 90 | 0 | 111 | 364 | 0 | 0 | 0 | 0 | 9 | 0 | 10 | 19 | 364 | 212 |
| 09:15 | 09:30 | 0 | 48 | 13 | 61 | 23 | 95 | 0 | 118 | 337 | 0 | 0 | 0 | 0 | 5 | 0 | 10 | 15 | 337 | 194 |
| 09:30 | 09:45 | 0 | 49 | 10 | 59 | 16 | 89 | 0 | 105 | 319 | 0 | 0 | 0 | 0 | 10 | 0 | 7 | 17 | 319 | 181 |
| 09:45 | 10:00 | 0 | 45 | 6 | 51 | 10 | 64 | 0 | 74 | 248 | 0 | 0 | 0 | 0 | 9 | 0 | 5 | 14 | 248 | 139 |
| 11:30 | 11:45 | 0 | 53 | 8 | 61 | 10 | 63 | 0 | 73 | 275 | 0 | 0 | 0 | 0 | 11 | 0 | 14 | 25 | 275 | 159 |
| 11:45 | 12:00 | 0 | 48 | 10 | 58 | 12 | 58 | 0 | 70 | 253 | 0 | 0 | 0 | 0 | 5 | 0 | 14 | 19 | 253 | 147 |
| 12:00 | 12:15 | 0 | 62 | 11 | 73 | 15 | 74 | 0 | 89 | 317 | 0 | 0 | 0 | 0 | 8 | 0 | 11 | 19 | 317 | 181 |
| 12:15 | 12:30 | 0 | 51 | 8 | 59 | 6 | 62 | 0 | 68 | 269 | 0 | 0 | 0 | 0 | 9 | 0 | 20 | 29 | 269 | 156 |
| 12:30 | 12:45 | 0 | 74 | 15 | 89 | 7 | 82 | 0 | 89 | 362 | 0 | 0 | 0 | 0 | 9 | 0 | 19 | 28 | 362 | 206 |
| 12:45 | 13:00 | 0 | 64 | 10 | 74 | 13 | 68 | 0 | 81 | 312 | 0 | 0 | 0 | 0 | 5 | 0 | 20 | 25 | 312 | 180 |
| 13:00 | 13:15 | 0 | 78 | 9 | 87 | 9 | 62 | 0 | 71 | 319 | 0 | 0 | 0 | 0 | 10 | 0 | 11 | 21 | 319 | 179 |
| 13:15 | 13:30 | 0 | 67 | 4 | 71 | 7 | 53 | 0 | 60 | 278 | 0 | 0 | 0 | 0 | 7 | 0 | 20 | 27 | 278 | 158 |
| 15:00 | 15:15 | 0 | 168 | 3 | 171 | 12 | 77 | 0 | 89 | 567 | 0 | 0 | 0 | 0 | 8 | 0 | 54 | 62 | 567 | 322 |
| 15:15 | 15:30 | 0 | 183 | 12 | 195 | 12 | 92 | 0 | 104 | 646 | 0 | 0 | 0 | 0 | 5 | 0 | 67 | 72 | 646 | 371 |
| 15:30 | 15:45 | 0 | 179 | 4 | 183 | 12 | 89 | 0 | 101 | 635 | 0 | 0 | 0 | 0 | 11 | 0 | 72 | 83 | 635 | 367 |
| 15:45 | 16:00 | 0 | 188 | 9 | 197 | 6 | 102 | 0 | 108 | 681 | 0 | 0 | 0 | 0 | 5 | 0 | 81 | 86 | 681 | 391 |
| 16:00 | 16:15 | 0 | 166 | 7 | 173 | 17 | 111 | 0 | 128 | 678 | 0 | 0 | 0 | 0 | 6 | 0 | 94 | 100 | 678 | 401 |
| 16:15 | 16:30 | 0 | 175 | 10 | 185 | 9 | 118 | 0 | 127 | 709 | 0 | 0 | 0 | 0 | 8 | 0 | 96 | 104 | 709 | 416 |
| 16:30 | 16:45 | 0 | 178 | 5 | 183 | 19 | 129 | 0 | 148 | 709 | 0 | 0 | 0 | 0 | 4 | 0 | 67 | 71 | 709 | 402 |
| 16:45 | 17:00 | 0 | 140 | 8 | 148 | 16 | 139 | 0 | 155 | 661 | 0 | 0 | 0 | 0 | 10 | 0 | 69 | 79 | 661 | 382 |
| 17:00 | 17:15 | 0 | 147 | 11 | 158 | 16 | 108 | 0 | 124 | 605 | 0 | 0 | 0 | 0 | 14 | 0 | 54 | 68 | 605 | 350 |
| 17:15 | 17:30 | 0 | 134 | 6 | 140 | 18 | 104 | 0 | 122 | 567 | 0 | 0 | 0 | 0 | 6 | 0 | 61 | 67 | 567 | 329 |
| 17:30 | 17:45 | 0 | 130 | 13 | 143 | 14 | 103 | 0 | 117 | 551 | 0 | 0 | 0 | 0 | 9 | 0 | 49 | 58 | 551 | 318 |
| 17:45 | 18:00 | 0 | 108 | 15 | 123 | 6 | 96 | 0 | 102 | 482 | 0 | 0 | 0 | 0 | 9 | 0 | 44 | 53 | 482 | 278 |
| Total: | | 0 | 3206 | 304 | 3510 | 659 | 3098 | 0 | 3757 | 14911 | 0 | 0 | 0 | 0 | 267 | 0 | 1073 | 1340 | 14911 | 8,607 |

Note: U-Turns are included in Totals.



Transportation Services - Traffic Services

Turning Movement Count - Study Results

PARKDALE AVE @ BURNSIDE AVE

Survey Date: Thursday, February 22, 2018

WO No:

37573

Start Time: 07:00

Device:

Miovision

Full Study Cyclist Volume

PARKDALE AVE

BURNSIDE AVE

| Time Period | Northbound | Southbound | Street Total | Eastbound | Westbound | Street Total | Grand Total |
|-------------|------------|------------|--------------|-----------|-----------|--------------|-------------|
| 07:00 | 07:15 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:15 | 07:30 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 | 07:45 | 0 | 0 | 0 | 1 | 1 | 1 |
| 07:45 | 08:00 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:00 | 08:15 | 0 | 1 | 1 | 0 | 0 | 1 |
| 08:15 | 08:30 | 0 | 1 | 1 | 0 | 0 | 1 |
| 08:30 | 08:45 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:45 | 09:00 | 0 | 0 | 0 | 0 | 0 | 0 |
| 09:00 | 09:15 | 0 | 0 | 0 | 0 | 0 | 0 |
| 09:15 | 09:30 | 0 | 0 | 0 | 0 | 0 | 0 |
| 09:30 | 09:45 | 0 | 1 | 1 | 0 | 0 | 1 |
| 09:45 | 10:00 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 | 11:45 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 | 12:00 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:00 | 12:15 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:15 | 12:30 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:30 | 12:45 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:45 | 13:00 | 0 | 0 | 0 | 0 | 0 | 0 |
| 13:00 | 13:15 | 0 | 0 | 0 | 0 | 0 | 0 |
| 13:15 | 13:30 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15:00 | 15:15 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15:15 | 15:30 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15:30 | 15:45 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15:45 | 16:00 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:00 | 16:15 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:15 | 16:30 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:30 | 16:45 | 0 | 0 | 0 | 1 | 1 | 1 |
| 16:45 | 17:00 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:00 | 17:15 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:15 | 17:30 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:30 | 17:45 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:45 | 18:00 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | | 0 | 3 | 3 | 0 | 2 | 5 |



Transportation Services - Traffic Services

Turning Movement Count - Study Results

PARKDALE AVE @ BURNSIDE AVE

Survey Date: Thursday, February 22, 2018

WO No:

37573

Start Time: 07:00

Device:

Miovision

Full Study Pedestrian Volume

PARKDALE AVE

BURNSIDE AVE

| Time Period | NB Approach (E or W Crossing) | SB Approach (E or W Crossing) | Total | EB Approach (N or S Crossing) | WB Approach (N or S Crossing) | Total | Grand Total |
|--------------------|----------------------------------|----------------------------------|------------|----------------------------------|----------------------------------|-----------|-------------|
| 07:00 07:15 | 10 | 8 | 18 | 0 | 1 | 1 | 19 |
| 07:15 07:30 | 9 | 4 | 13 | 0 | 2 | 2 | 15 |
| 07:30 07:45 | 8 | 4 | 12 | 0 | 4 | 4 | 16 |
| 07:45 08:00 | 18 | 9 | 27 | 0 | 3 | 3 | 30 |
| 08:00 08:15 | 14 | 10 | 24 | 0 | 2 | 2 | 26 |
| 08:15 08:30 | 15 | 6 | 21 | 0 | 3 | 3 | 24 |
| 08:30 08:45 | 13 | 8 | 21 | 0 | 3 | 3 | 24 |
| 08:45 09:00 | 13 | 4 | 17 | 0 | 0 | 0 | 17 |
| 09:00 09:15 | 6 | 5 | 11 | 0 | 1 | 1 | 12 |
| 09:15 09:30 | 5 | 3 | 8 | 0 | 2 | 2 | 10 |
| 09:30 09:45 | 4 | 3 | 7 | 0 | 2 | 2 | 9 |
| 09:45 10:00 | 4 | 1 | 5 | 0 | 0 | 0 | 5 |
| 11:30 11:45 | 1 | 1 | 2 | 0 | 2 | 2 | 4 |
| 11:45 12:00 | 6 | 1 | 7 | 0 | 3 | 3 | 10 |
| 12:00 12:15 | 7 | 2 | 9 | 0 | 2 | 2 | 11 |
| 12:15 12:30 | 1 | 3 | 4 | 0 | 2 | 2 | 6 |
| 12:30 12:45 | 6 | 0 | 6 | 0 | 4 | 4 | 10 |
| 12:45 13:00 | 9 | 3 | 12 | 0 | 0 | 0 | 12 |
| 13:00 13:15 | 6 | 4 | 10 | 0 | 2 | 2 | 12 |
| 13:15 13:30 | 2 | 2 | 4 | 0 | 4 | 4 | 8 |
| 15:00 15:15 | 5 | 7 | 12 | 0 | 1 | 1 | 13 |
| 15:15 15:30 | 4 | 2 | 6 | 0 | 2 | 2 | 8 |
| 15:30 15:45 | 9 | 2 | 11 | 0 | 0 | 0 | 11 |
| 15:45 16:00 | 6 | 3 | 9 | 0 | 4 | 4 | 13 |
| 16:00 16:15 | 8 | 14 | 22 | 0 | 3 | 3 | 25 |
| 16:15 16:30 | 7 | 5 | 12 | 0 | 5 | 5 | 17 |
| 16:30 16:45 | 10 | 11 | 21 | 0 | 3 | 3 | 24 |
| 16:45 17:00 | 7 | 5 | 12 | 0 | 3 | 3 | 15 |
| 17:00 17:15 | 10 | 3 | 13 | 0 | 3 | 3 | 16 |
| 17:15 17:30 | 9 | 2 | 11 | 0 | 2 | 2 | 13 |
| 17:30 17:45 | 4 | 4 | 8 | 0 | 0 | 0 | 8 |
| 17:45 18:00 | 2 | 2 | 4 | 0 | 1 | 1 | 5 |
| Total | 238 | 141 | 379 | 0 | 69 | 69 | 448 |



Transportation Services - Traffic Services

Turning Movement Count - Study Results

PARKDALE AVE @ BURNSIDE AVE

Survey Date: Thursday, February 22, 2018

WO No:

37573

Start Time: 07:00

Device:

Miovision

Full Study Heavy Vehicles

PARKDALE AVE

BURNSIDE AVE

| Time Period | Northbound | | | Southbound | | | Eastbound | | | Westbound | | | Grand Total | | | | | |
|-------------|------------|----|----|------------|-----|----|-----------|----------|------------|-----------|----|----|-------------|----|----|----|----------|------------|
| | LT | ST | RT | N TOT | LT | ST | RT | S TOT | STR TOT | LT | ST | RT | E TOT | LT | ST | RT | W TOT | STR TOT |
| 07:00 | 07:15 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 5 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| 07:15 | 07:30 | 0 | 1 | 0 | 5 | 0 | 3 | 0 | 4 | 9 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| 07:30 | 07:45 | 0 | 1 | 1 | 6 | 1 | 4 | 0 | 8 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 4 |
| 07:45 | 08:00 | 0 | 0 | 0 | 2 | 1 | 2 | 0 | 4 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 |
| 08:00 | 08:15 | 0 | 0 | 2 | 4 | 1 | 2 | 0 | 5 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 5 |
| 08:15 | 08:30 | 0 | 2 | 0 | 4 | 1 | 2 | 0 | 5 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| 08:30 | 08:45 | 0 | 0 | 0 | 3 | 0 | 3 | 0 | 4 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| 08:45 | 09:00 | 0 | 0 | 1 | 8 | 0 | 6 | 0 | 7 | 15 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 3 |
| 09:00 | 09:15 | 0 | 1 | 1 | 8 | 1 | 5 | 0 | 10 | 18 | 0 | 0 | 0 | 0 | 1 | 0 | 3 | 6 |
| 09:15 | 09:30 | 0 | 2 | 2 | 5 | 2 | 1 | 0 | 7 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 6 |
| 09:30 | 09:45 | 0 | 2 | 0 | 6 | 1 | 2 | 0 | 5 | 11 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 3 |
| 09:45 | 10:00 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| 11:30 | 11:45 | 0 | 0 | 0 | 3 | 1 | 2 | 0 | 5 | 8 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 4 |
| 11:45 | 12:00 | 0 | 1 | 1 | 2 | 2 | 0 | 0 | 4 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 |
| 12:00 | 12:15 | 0 | 1 | 1 | 6 | 0 | 4 | 0 | 6 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 |
| 12:15 | 12:30 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| 12:30 | 12:45 | 0 | 1 | 1 | 3 | 0 | 1 | 0 | 2 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 12:45 | 13:00 | 0 | 0 | 0 | 2 | 1 | 2 | 0 | 5 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 3 |
| 13:00 | 13:15 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| 13:15 | 13:30 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| 15:00 | 15:15 | 0 | 0 | 0 | 4 | 1 | 4 | 0 | 7 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 3 |
| 15:15 | 15:30 | 0 | 1 | 1 | 4 | 1 | 2 | 0 | 4 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 15:30 | 15:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15:45 | 16:00 | 0 | 4 | 1 | 7 | 0 | 2 | 0 | 6 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 16:00 | 16:15 | 0 | 0 | 1 | 3 | 0 | 2 | 0 | 2 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| 16:15 | 16:30 | 0 | 1 | 0 | 2 | 0 | 1 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:30 | 16:45 | 0 | 0 | 1 | 3 | 0 | 2 | 0 | 2 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| 16:45 | 17:00 | 0 | 1 | 0 | 3 | 0 | 2 | 0 | 3 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:00 | 17:15 | 0 | 1 | 0 | 3 | 0 | 2 | 0 | 3 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:15 | 17:30 | 0 | 0 | 1 | 2 | 0 | 1 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| 17:30 | 17:45 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 2 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:45 | 18:00 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total: | None | 0 | 21 | 15 | 108 | 17 | 66 | 0 | 126 | 234 | 0 | 0 | 0 | 0 | 6 | 0 | 22 | 60 |
| | | | | | | | | | | | | | | | | | 147 | |



Transportation Services - Traffic Services

Turning Movement Count - Study Results

PARKDALE AVE @ BURNSIDE AVE

Survey Date: Thursday, February 22, 2018

WO No: 37573

Start Time: 07:00

Device: Miovision

Full Study 15 Minute U-Turn Total

| | | PARKDALE AVE | | BURNSIDE AVE | | Total |
|--------------------|-------|--------------------------------|--------------------------------|-------------------------------|-------------------------------|--------------|
| Time Period | | Northbound U-Turn Total | Southbound U-Turn Total | Eastbound U-Turn Total | Westbound U-Turn Total | |
| 07:00 | 07:15 | 0 | 0 | 0 | 0 | 0 |
| 07:15 | 07:30 | 0 | 0 | 0 | 0 | 0 |
| 07:30 | 07:45 | 0 | 0 | 0 | 0 | 0 |
| 07:45 | 08:00 | 0 | 0 | 0 | 0 | 0 |
| 08:00 | 08:15 | 0 | 0 | 0 | 0 | 0 |
| 08:15 | 08:30 | 0 | 0 | 0 | 0 | 0 |
| 08:30 | 08:45 | 0 | 0 | 0 | 0 | 0 |
| 08:45 | 09:00 | 0 | 0 | 0 | 0 | 0 |
| 09:00 | 09:15 | 0 | 0 | 0 | 0 | 0 |
| 09:15 | 09:30 | 0 | 0 | 0 | 0 | 0 |
| 09:30 | 09:45 | 0 | 0 | 0 | 0 | 0 |
| 09:45 | 10:00 | 0 | 0 | 0 | 0 | 0 |
| 11:30 | 11:45 | 0 | 0 | 0 | 0 | 0 |
| 11:45 | 12:00 | 0 | 0 | 0 | 0 | 0 |
| 12:00 | 12:15 | 0 | 0 | 0 | 0 | 0 |
| 12:15 | 12:30 | 0 | 0 | 0 | 0 | 0 |
| 12:30 | 12:45 | 0 | 0 | 0 | 0 | 0 |
| 12:45 | 13:00 | 0 | 0 | 0 | 0 | 0 |
| 13:00 | 13:15 | 0 | 0 | 0 | 0 | 0 |
| 13:15 | 13:30 | 0 | 0 | 0 | 0 | 0 |
| 15:00 | 15:15 | 0 | 0 | 0 | 0 | 0 |
| 15:15 | 15:30 | 0 | 0 | 0 | 0 | 0 |
| 15:30 | 15:45 | 0 | 0 | 0 | 0 | 0 |
| 15:45 | 16:00 | 0 | 0 | 0 | 0 | 0 |
| 16:00 | 16:15 | 0 | 0 | 0 | 0 | 0 |
| 16:15 | 16:30 | 0 | 0 | 0 | 0 | 0 |
| 16:30 | 16:45 | 0 | 0 | 0 | 0 | 0 |
| 16:45 | 17:00 | 0 | 0 | 0 | 0 | 0 |
| 17:00 | 17:15 | 0 | 0 | 0 | 0 | 0 |
| 17:15 | 17:30 | 0 | 0 | 0 | 0 | 0 |
| 17:30 | 17:45 | 0 | 0 | 0 | 0 | 0 |
| 17:45 | 18:00 | 0 | 0 | 0 | 0 | 0 |
| Total | | 0 | 0 | 0 | 0 | 0 |

Appendix E – Existing (2020) Synchro and SIDRA Outputs

MOVEMENT SUMMARY

Site: 1 [Burnside Roundabout - Existing (2020) - AM]

Burnside Roundabout - Existing (2020) - AM

Site Category: (None)

Roundabout

| Movement Performance - Vehicles | | | | | | | | | | | | |
|--|------|--------------------|------------|---------------|-------------------|------------------|--------------------------------|------------------|--------------|---------------------|------------------|--------------------|
| Mov ID | Turn | Demand Total veh/h | Flows HV % | Deg. Satn v/c | Average Delay sec | Level of Service | 95% Back of Queue Vehicles veh | Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Bayview Station Road | | | | | | | | | | | | |
| 21u | U | 2 | 0.0 | 0.066 | 9.2 | LOS A | 0.2 | 1.3 | 0.08 | 0.55 | 0.08 | 47.6 |
| 21 | L2 | 60 | 9.0 | 0.066 | 7.4 | LOS A | 0.2 | 1.3 | 0.08 | 0.55 | 0.08 | 42.8 |
| 23a | R1 | 24 | 0.0 | 0.066 | 2.5 | LOS A | 0.2 | 1.3 | 0.08 | 0.55 | 0.08 | 43.7 |
| Approach | | 86 | 6.3 | 0.066 | 6.1 | LOS A | 0.2 | 1.3 | 0.08 | 0.55 | 0.08 | 43.1 |
| North: Slidell Street | | | | | | | | | | | | |
| 7u | U | 1 | 0.0 | 0.071 | 9.2 | LOS A | 0.2 | 1.4 | 0.11 | 0.55 | 0.11 | 21.4 |
| 7a | L1 | 84 | 7.0 | 0.071 | 6.6 | LOS A | 0.2 | 1.4 | 0.11 | 0.55 | 0.11 | 43.4 |
| 9a | R1 | 8 | 0.0 | 0.071 | 2.6 | LOS A | 0.2 | 1.4 | 0.11 | 0.55 | 0.11 | 38.2 |
| Approach | | 93 | 6.3 | 0.071 | 6.2 | LOS A | 0.2 | 1.4 | 0.11 | 0.55 | 0.11 | 42.6 |
| SouthWest: Burnside Avenue | | | | | | | | | | | | |
| 30u | U | 1 | 0.0 | 0.260 | 7.1 | LOS A | 0.9 | 6.1 | 0.15 | 0.35 | 0.15 | 41.7 |
| 30a | L1 | 32 | 0.0 | 0.260 | 5.0 | LOS A | 0.9 | 6.1 | 0.15 | 0.35 | 0.15 | 25.8 |
| 32 | R2 | 328 | 0.0 | 0.260 | 2.0 | LOS A | 0.9 | 6.1 | 0.15 | 0.35 | 0.15 | 42.3 |
| Approach | | 361 | 0.0 | 0.260 | 2.3 | LOS A | 0.9 | 6.1 | 0.15 | 0.35 | 0.15 | 40.8 |
| All Vehicles | | 540 | 2.1 | 0.260 | 3.6 | LOS A | 0.9 | 6.1 | 0.13 | 0.42 | 0.13 | 41.4 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

MOVEMENT SUMMARY

Site: 1 [Burnside Roundabout - Existing (2020) - PM]

Burnside Roundabout - Existing (2020) - PM

Site Category: (None)

Roundabout

| Movement Performance - Vehicles | | | | | | | | | | | | |
|--|------|--------------------|------------|---------------|-------------------|------------------|--------------------------------|------------------|--------------|---------------------|------------------|--------------------|
| Mov ID | Turn | Demand Total veh/h | Flows HV % | Deg. Satn v/c | Average Delay sec | Level of Service | 95% Back of Queue Vehicles veh | Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Bayview Station Road | | | | | | | | | | | | |
| 21u | U | 10 | 11.0 | 0.335 | 9.3 | LOS A | 1.2 | 8.6 | 0.10 | 0.57 | 0.10 | 46.9 |
| 21 | L2 | 394 | 1.0 | 0.335 | 7.4 | LOS A | 1.2 | 8.6 | 0.10 | 0.57 | 0.10 | 42.5 |
| 23a | R1 | 88 | 3.0 | 0.335 | 2.6 | LOS A | 1.2 | 8.6 | 0.10 | 0.57 | 0.10 | 42.9 |
| Approach | | 492 | 1.6 | 0.335 | 6.6 | LOS A | 1.2 | 8.6 | 0.10 | 0.57 | 0.10 | 42.6 |
| North: Slidell Street | | | | | | | | | | | | |
| 7u | U | 1 | 0.0 | 0.069 | 10.1 | LOS B | 0.2 | 1.7 | 0.33 | 0.60 | 0.33 | 21.1 |
| 7a | L1 | 60 | 6.0 | 0.069 | 7.4 | LOS A | 0.2 | 1.7 | 0.33 | 0.60 | 0.33 | 42.9 |
| 9a | R1 | 16 | 0.0 | 0.069 | 3.5 | LOS A | 0.2 | 1.7 | 0.33 | 0.60 | 0.33 | 37.8 |
| Approach | | 77 | 4.7 | 0.069 | 6.7 | LOS A | 0.2 | 1.7 | 0.33 | 0.60 | 0.33 | 41.4 |
| SouthWest: Burnside Avenue | | | | | | | | | | | | |
| 30u | U | 3 | 0.0 | 0.105 | 7.1 | LOS A | 0.3 | 2.3 | 0.13 | 0.38 | 0.13 | 41.3 |
| 30a | L1 | 36 | 0.0 | 0.105 | 4.9 | LOS A | 0.3 | 2.3 | 0.13 | 0.38 | 0.13 | 27.9 |
| 32 | R2 | 100 | 4.0 | 0.105 | 2.0 | LOS A | 0.3 | 2.3 | 0.13 | 0.38 | 0.13 | 41.9 |
| Approach | | 139 | 2.9 | 0.105 | 2.8 | LOS A | 0.3 | 2.3 | 0.13 | 0.38 | 0.13 | 38.4 |
| All Vehicles | | 708 | 2.2 | 0.335 | 5.8 | LOS A | 1.2 | 8.6 | 0.13 | 0.54 | 0.13 | 41.6 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akcelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

HCM Signalized Intersection Capacity Analysis

1: Parkdale Ave & Burnside Ave

Existing (2020)

AM Peak Hour



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|------------------------|-------|------|------|-------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (vph) | 42 | 59 | 337 | 44 | 191 | 516 |
| Future Volume (vph) | 42 | 59 | 337 | 44 | 191 | 516 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 4.2 | 3.7 | 4.8 | 3.7 | 3.7 | 4.8 |
| Total Lost time (s) | 5.4 | | 5.2 | | | 5.2 |
| Lane Util. Factor | 1.00 | | 1.00 | | | 1.00 |
| Frpb, ped/bikes | 0.95 | | 1.00 | | | 1.00 |
| Flpb, ped/bikes | 1.00 | | 1.00 | | | 1.00 |
| Fr _t | 0.92 | | 0.98 | | | 1.00 |
| Flt Protected | 0.98 | | 1.00 | | | 0.99 |
| Satd. Flow (prot) | 1564 | | 1966 | | | 1968 |
| Flt Permitted | 0.98 | | 1.00 | | | 0.76 |
| Satd. Flow (perm) | 1564 | | 1966 | | | 1511 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 47 | 66 | 374 | 49 | 212 | 573 |
| RTOR Reduction (vph) | 55 | 0 | 7 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 58 | 0 | 416 | 0 | 0 | 785 |
| Confl. Peds. (#/hr) | 57 | 30 | | 12 | 12 | |
| Confl. Bikes (#/hr) | | | 1 | | | |
| Heavy Vehicles (%) | 0% | 9% | 1% | 7% | 2% | 2% |
| Turn Type | pm+pt | | NA | | Perm | NA |
| Protected Phases | 3 | | 2 | | | 6 |
| Permitted Phases | 8 | | | 6 | | |
| Actuated Green, G (s) | 10.4 | | 39.0 | | | 39.0 |
| Effective Green, g (s) | 10.4 | | 39.0 | | | 39.0 |
| Actuated g/C Ratio | 0.17 | | 0.65 | | | 0.65 |
| Clearance Time (s) | 5.4 | | 5.2 | | | 5.2 |
| Vehicle Extension (s) | 3.0 | | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | 271 | | 1277 | | | 982 |
| v/s Ratio Prot | c0.04 | | 0.21 | | | |
| v/s Ratio Perm | | | | c0.52 | | |
| v/c Ratio | 0.22 | | 0.33 | | | 0.80 |
| Uniform Delay, d1 | 21.3 | | 4.7 | | | 7.6 |
| Progression Factor | 1.00 | | 1.00 | | | 1.00 |
| Incremental Delay, d2 | 0.4 | | 0.7 | | | 6.8 |
| Delay (s) | 21.7 | | 5.3 | | | 14.4 |
| Level of Service | C | | A | | | B |
| Approach Delay (s) | 21.7 | | 5.3 | | | 14.4 |
| Approach LOS | C | | A | | | B |

Intersection Summary

| | | | |
|-----------------------------------|-------|---------------------------|------|
| HCM 2000 Control Delay | 12.1 | HCM 2000 Level of Service | B |
| HCM 2000 Volume to Capacity ratio | 0.68 | | |
| Actuated Cycle Length (s) | 60.0 | Sum of lost time (s) | 10.6 |
| Intersection Capacity Utilization | 83.0% | ICU Level of Service | E |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
2: Slidell St/Onigam St & Sir John A MacDonald Pkwy

Existing (2020)
AM Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBL | SBT |
|-----------------------------------|-------|------|------|------|---------------------------|------|------|------|-------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 0 | 1541 | 23 | 1 | 1054 | 1 | 1 | 1 | 22 | 1 | 1 | 5 |
| Future Volume (vph) | 0 | 1541 | 23 | 1 | 1054 | 1 | 1 | 1 | 22 | 1 | 1 | 5 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 3.7 | 3.8 | 3.7 | 3.7 | 3.8 | 3.7 | 3.7 | 3.7 | 3.9 | 3.7 | 3.7 | 4.0 |
| Total Lost time (s) | | 5.5 | | | 5.5 | | | | 6.3 | | | 6.3 |
| Lane Util. Factor | | 0.95 | | | 0.95 | | | | 1.00 | | | 1.00 |
| Frpb, ped/bikes | | 1.00 | | | 1.00 | | | | 1.00 | | | 0.99 |
| Flpb, ped/bikes | | 1.00 | | | 1.00 | | | | 1.00 | | | 1.00 |
| Fr _t | | 1.00 | | | 1.00 | | | | 0.99 | | | 0.96 |
| Flt Protected | | 1.00 | | | 1.00 | | | | 1.00 | | | 1.00 |
| Satd. Flow (prot) | | 3487 | | | 3461 | | | | 1841 | | | 1784 |
| Flt Permitted | | 1.00 | | | 0.95 | | | | 0.98 | | | 0.97 |
| Satd. Flow (perm) | | 3487 | | | 3302 | | | | 1806 | | | 1739 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 0 | 1712 | 26 | 1 | 1171 | 1 | 1 | 1 | 24 | 1 | 1 | 6 |
| RTOR Reduction (vph) | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 3 |
| Lane Group Flow (vph) | 0 | 1737 | 0 | 0 | 1173 | 0 | 0 | 0 | 26 | 0 | 0 | 7 |
| Confl. Peds. (#/hr) | 2 | | 1 | 1 | | 2 | 1 | 3 | | 4 | 4 | |
| Confl. Bikes (#/hr) | | | | 1 | | | | | | 11 | | |
| Heavy Vehicles (%) | 0% | 0% | 0% | 0% | 1% | 0% | 0% | 0% | 0% | 0% | 0% | 0% |
| Turn Type | | NA | | Perm | NA | | Perm | Perm | NA | | Perm | NA |
| Protected Phases | | 2 | | | 6 | | | | 8 | | | 4 |
| Permitted Phases | 2 | | | 6 | | | 8 | 8 | | | 4 | |
| Actuated Green, G (s) | 73.8 | | | 73.8 | | | | | 9.4 | | | 9.4 |
| Effective Green, g (s) | 73.8 | | | 73.8 | | | | | 9.4 | | | 9.4 |
| Actuated g/C Ratio | 0.78 | | | 0.78 | | | | | 0.10 | | | 0.10 |
| Clearance Time (s) | 5.5 | | | 5.5 | | | | | 6.3 | | | 6.3 |
| Vehicle Extension (s) | 3.0 | | | 3.0 | | | | | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | 2708 | | | 2565 | | | | | 178 | | | 172 |
| v/s Ratio Prot | c0.50 | | | | | | | | | | | |
| v/s Ratio Perm | | | | 0.36 | | | | | c0.01 | | | 0.00 |
| v/c Ratio | 0.64 | | | 0.46 | | | | | 0.15 | | | 0.04 |
| Uniform Delay, d1 | 4.7 | | | 3.7 | | | | | 39.1 | | | 38.7 |
| Progression Factor | 1.00 | | | 1.00 | | | | | 1.00 | | | 1.00 |
| Incremental Delay, d2 | 1.2 | | | 0.6 | | | | | 0.4 | | | 0.1 |
| Delay (s) | 5.9 | | | 4.3 | | | | | 39.5 | | | 38.8 |
| Level of Service | A | | | A | | | | | D | | | D |
| Approach Delay (s) | 5.9 | | | 4.3 | | | | | 39.5 | | | 38.8 |
| Approach LOS | A | | | A | | | | | D | | | D |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | 5.7 | | | | HCM 2000 Level of Service | | | | A | | | |
| HCM 2000 Volume to Capacity ratio | 0.59 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 95.0 | | | | Sum of lost time (s) | | | | 11.8 | | | |
| Intersection Capacity Utilization | 65.7% | | | | ICU Level of Service | | | | C | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis
2: Slidell St/Onigam St & Sir John A MacDonald Pkwy

Existing (2020)
AM Peak Hour

| Movement | SBR |
|------------------------|------|
| Lane Configurations | |
| Traffic Volume (vph) | 3 |
| Future Volume (vph) | 3 |
| Ideal Flow (vphpl) | 1800 |
| Lane Width | 3.7 |
| Total Lost time (s) | |
| Lane Util. Factor | |
| Frpb, ped/bikes | |
| Flpb, ped/bikes | |
| Fr | |
| Flt Protected | |
| Satd. Flow (prot) | |
| Flt Permitted | |
| Satd. Flow (perm) | |
| Peak-hour factor, PHF | 0.90 |
| Adj. Flow (vph) | 3 |
| RTOR Reduction (vph) | 0 |
| Lane Group Flow (vph) | 0 |
| Confl. Peds. (#/hr) | 3 |
| Confl. Bikes (#/hr) | 2 |
| Heavy Vehicles (%) | 0% |
| Turn Type | |
| Protected Phases | |
| Permitted Phases | |
| Actuated Green, G (s) | |
| Effective Green, g (s) | |
| Actuated g/C Ratio | |
| Clearance Time (s) | |
| Vehicle Extension (s) | |
| Lane Grp Cap (vph) | |
| v/s Ratio Prot | |
| v/s Ratio Perm | |
| v/c Ratio | |
| Uniform Delay, d1 | |
| Progression Factor | |
| Incremental Delay, d2 | |
| Delay (s) | |
| Level of Service | |
| Approach Delay (s) | |
| Approach LOS | |
| Intersection Summary | |

HCM Signalized Intersection Capacity Analysis

3: Bayview Stn Rd & Scott St/Albert St

Existing (2020)

AM Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|--------|------|------|------|---------------------------|------|------|------|-------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 22 | 636 | 82 | 51 | 297 | 32 | 46 | 93 | 116 | 134 | 231 | 26 |
| Future Volume (vph) | 22 | 636 | 82 | 51 | 297 | 32 | 46 | 93 | 116 | 134 | 231 | 26 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 3.7 | 3.6 | 3.7 | 3.2 | 3.5 | 3.8 | 3.0 | 4.3 | 3.7 | 3.3 | 4.5 | 3.7 |
| Total Lost time (s) | 6.5 | | 6.5 | 6.5 | 6.5 | 6.4 | 6.4 | | 6.4 | 6.4 | | |
| Lane Util. Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | |
| Frpb, ped/bikes | 0.99 | | 1.00 | 1.00 | 0.96 | 1.00 | 0.93 | | 1.00 | 0.99 | | |
| Flpb, ped/bikes | 1.00 | | 0.98 | 1.00 | 1.00 | 0.96 | 1.00 | | 0.96 | 1.00 | | |
| Fr _t | 0.99 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.92 | | 1.00 | 0.98 | | |
| Fl _t Protected | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | |
| Satd. Flow (prot) | 1423 | | 1564 | 1338 | 1402 | 1349 | 1597 | | 1534 | 1862 | | |
| Fl _t Permitted | 0.98 | | 0.33 | 1.00 | 1.00 | 0.37 | 1.00 | | 0.47 | 1.00 | | |
| Satd. Flow (perm) | 1403 | | 540 | 1338 | 1402 | 520 | 1597 | | 763 | 1862 | | |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 24 | 707 | 91 | 57 | 330 | 36 | 51 | 103 | 129 | 149 | 257 | 29 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 | 0 | 13 | 0 | 47 | 0 | 0 | 4 | 0 |
| Lane Group Flow (vph) | 0 | 818 | 0 | 57 | 330 | 23 | 51 | 185 | 0 | 149 | 282 | 0 |
| Confl. Peds. (#/hr) | 11 | | 49 | 49 | | 11 | 41 | | 28 | 28 | | 41 |
| Confl. Bikes (#/hr) | | | 2 | | | | | 35 | | | | 10 |
| Heavy Vehicles (%) | 0% | 26% | 4% | 2% | 33% | 7% | 13% | 4% | 3% | 4% | 2% | 17% |
| Turn Type | Perm | NA | | Perm | NA | Perm | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | 6 | 8 | | | 4 | | |
| Actuated Green, G (s) | 64.9 | | 64.9 | 64.9 | 64.9 | 22.2 | 22.2 | | 22.2 | 22.2 | | |
| Effective Green, g (s) | 64.9 | | 64.9 | 64.9 | 64.9 | 22.2 | 22.2 | | 22.2 | 22.2 | | |
| Actuated g/C Ratio | 0.65 | | 0.65 | 0.65 | 0.65 | 0.22 | 0.22 | | 0.22 | 0.22 | | |
| Clearance Time (s) | 6.5 | | 6.5 | 6.5 | 6.5 | 6.4 | 6.4 | | 6.4 | 6.4 | | |
| Vehicle Extension (s) | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | |
| Lane Grp Cap (vph) | 910 | | 350 | 868 | 909 | 115 | 354 | | 169 | 413 | | |
| v/s Ratio Prot | | | | 0.25 | | | | 0.12 | | | 0.15 | |
| v/s Ratio Perm | c0.58 | | 0.11 | | 0.02 | 0.10 | | | c0.20 | | | |
| v/c Ratio | 0.90 | | 0.16 | 0.38 | 0.03 | 0.44 | 0.52 | | 0.88 | 0.68 | | |
| Uniform Delay, d1 | 14.8 | | 6.9 | 8.2 | 6.3 | 33.6 | 34.2 | | 37.6 | 35.7 | | |
| Progression Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | |
| Incremental Delay, d2 | 13.5 | | 1.0 | 1.3 | 0.1 | 2.7 | 1.4 | | 37.6 | 4.6 | | |
| Delay (s) | 28.3 | | 7.9 | 9.4 | 6.3 | 36.3 | 35.6 | | 75.2 | 40.3 | | |
| Level of Service | C | | A | A | A | D | D | | E | D | | |
| Approach Delay (s) | 28.3 | | | 9.0 | | | 35.7 | | | 52.3 | | |
| Approach LOS | C | | | A | | | D | | | D | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | 30.5 | | | | HCM 2000 Level of Service | | | C | | | | |
| HCM 2000 Volume to Capacity ratio | 0.89 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 100.0 | | | | Sum of lost time (s) | | | 12.9 | | | | |
| Intersection Capacity Utilization | 104.4% | | | | ICU Level of Service | | | G | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

1: Parkdale Ave & Burnside Ave

Existing (2020)

PM Peak Hour



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|--------|------|---------------------------|------|------|------|
| Lane Configurations | WBL | WBR | NBT | NBR | SBL | SBT |
| Traffic Volume (vph) | 24 | 352 | 735 | 32 | 53 | 478 |
| Future Volume (vph) | 24 | 352 | 735 | 32 | 53 | 478 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 4.2 | 3.7 | 4.8 | 3.7 | 3.7 | 4.8 |
| Total Lost time (s) | 5.4 | | 5.2 | | | 5.2 |
| Lane Util. Factor | 1.00 | | 1.00 | | | 1.00 |
| Frpb, ped/bikes | 0.90 | | 1.00 | | | 1.00 |
| Flpb, ped/bikes | 1.00 | | 1.00 | | | 1.00 |
| Fr _t | 0.87 | | 0.99 | | | 1.00 |
| Flt Protected | 1.00 | | 1.00 | | | 1.00 |
| Satd. Flow (prot) | 1508 | | 1997 | | | 1993 |
| Flt Permitted | 1.00 | | 1.00 | | | 0.71 |
| Satd. Flow (perm) | 1508 | | 1997 | | | 1428 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 27 | 391 | 817 | 36 | 59 | 531 |
| RTOR Reduction (vph) | 116 | 0 | 2 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 302 | 0 | 851 | 0 | 0 | 590 |
| Confl. Peds. (#/hr) | 32 | 34 | | 16 | 16 | |
| Confl. Bikes (#/hr) | | | 1 | | | |
| Heavy Vehicles (%) | 0% | 0% | 1% | 10% | 0% | 2% |
| Turn Type | pm+pt | | NA | | Perm | NA |
| Protected Phases | 3 | | 2 | | | 6 |
| Permitted Phases | 8 | | | 6 | | |
| Actuated Green, G (s) | 16.8 | | 42.6 | | | 42.6 |
| Effective Green, g (s) | 16.8 | | 42.6 | | | 42.6 |
| Actuated g/C Ratio | 0.24 | | 0.61 | | | 0.61 |
| Clearance Time (s) | 5.4 | | 5.2 | | | 5.2 |
| Vehicle Extension (s) | 3.0 | | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | 361 | | 1215 | | | 869 |
| v/s Ratio Prot | c0.20 | | c0.43 | | | |
| v/s Ratio Perm | | | | 0.41 | | |
| v/c Ratio | 0.84 | | 0.70 | | | 0.68 |
| Uniform Delay, d1 | 25.3 | | 9.3 | | | 9.1 |
| Progression Factor | 1.00 | | 1.00 | | | 1.00 |
| Incremental Delay, d2 | 15.3 | | 3.4 | | | 4.3 |
| Delay (s) | 40.6 | | 12.7 | | | 13.4 |
| Level of Service | D | | B | | | B |
| Approach Delay (s) | 40.6 | | 12.7 | | | 13.4 |
| Approach LOS | D | | B | | | B |
| Intersection Summary | | | | | | |
| HCM 2000 Control Delay | 19.2 | | HCM 2000 Level of Service | | B | |
| HCM 2000 Volume to Capacity ratio | 0.74 | | | | | |
| Actuated Cycle Length (s) | 70.0 | | Sum of lost time (s) | | 10.6 | |
| Intersection Capacity Utilization | 109.3% | | ICU Level of Service | | H | |
| Analysis Period (min) | 15 | | | | | |
| c Critical Lane Group | | | | | | |

HCM Signalized Intersection Capacity Analysis
2: Slidell St/Onigam St & Sir John A MacDonald Pkwy

Existing (2020)
PM Peak Hour

| Movement | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
|-----------------------------------|-------|------|------|------|------|---------------------------|------|------|-------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 0 | 1027 | 4 | 2 | 2 | 1790 | 0 | 28 | 15 | 37 | 3 | 28 |
| Future Volume (vph) | 0 | 1027 | 4 | 2 | 2 | 1790 | 0 | 28 | 15 | 37 | 3 | 28 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 3.7 | 3.8 | 3.7 | 3.7 | 3.7 | 3.8 | 3.7 | 3.7 | 3.9 | 3.7 | 3.7 | 4.0 |
| Total Lost time (s) | | 5.5 | | | | 5.5 | | | 6.3 | | | 6.3 |
| Lane Util. Factor | 0.95 | | | | | 0.95 | | | 1.00 | | | 1.00 |
| Frpb, ped/bikes | 1.00 | | | | | 1.00 | | | 0.99 | | | 0.99 |
| Flpb, ped/bikes | 1.00 | | | | | 1.00 | | | 1.00 | | | 1.00 |
| Fr _t | 1.00 | | | | | 1.00 | | | 0.94 | | | 0.96 |
| Flt Protected | 1.00 | | | | | 1.00 | | | 0.98 | | | 1.00 |
| Satd. Flow (prot) | 3460 | | | | | 3496 | | | 1693 | | | 1743 |
| Flt Permitted | 1.00 | | | | | 0.95 | | | 0.87 | | | 0.98 |
| Satd. Flow (perm) | 3460 | | | | | 3332 | | | 1491 | | | 1709 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 0 | 1141 | 4 | 2 | 2 | 1989 | 0 | 31 | 17 | 41 | 3 | 31 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 36 | 0 | 0 | 9 |
| Lane Group Flow (vph) | 0 | 1145 | 0 | 0 | 0 | 1993 | 0 | 0 | 53 | 0 | 0 | 38 |
| Confl. Peds. (#/hr) | 1 | | | 7 | | | 1 | 6 | | 7 | 7 | |
| Confl. Bikes (#/hr) | | | | | | | | | 2 | | | |
| Heavy Vehicles (%) | 0% | 1% | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 4% |
| Turn Type | | NA | | Perm | Perm | NA | | Perm | NA | | Perm | NA |
| Protected Phases | | 2 | | | | 6 | | | 8 | | | 4 |
| Permitted Phases | 2 | | 6 | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | 71.8 | | | | | 71.8 | | | 11.4 | | | 11.4 |
| Effective Green, g (s) | 71.8 | | | | | 71.8 | | | 11.4 | | | 11.4 |
| Actuated g/C Ratio | 0.76 | | | | | 0.76 | | | 0.12 | | | 0.12 |
| Clearance Time (s) | 5.5 | | | | | 5.5 | | | 6.3 | | | 6.3 |
| Vehicle Extension (s) | 3.0 | | | | | 3.0 | | | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | 2615 | | | | | 2518 | | | 178 | | | 205 |
| v/s Ratio Prot | 0.33 | | | | | | | | | | | |
| v/s Ratio Perm | | | | | | c0.60 | | | c0.04 | | | 0.02 |
| v/c Ratio | 0.44 | | | | | 0.79 | | | 0.30 | | | 0.19 |
| Uniform Delay, d1 | 4.2 | | | | | 7.1 | | | 38.1 | | | 37.6 |
| Progression Factor | 1.00 | | | | | 1.00 | | | 1.00 | | | 1.00 |
| Incremental Delay, d2 | 0.5 | | | | | 2.6 | | | 0.9 | | | 0.4 |
| Delay (s) | 4.8 | | | | | 9.7 | | | 39.1 | | | 38.1 |
| Level of Service | A | | | | | A | | | D | | | D |
| Approach Delay (s) | 4.8 | | | | | 9.7 | | | 39.1 | | | 38.1 |
| Approach LOS | A | | | | | A | | | D | | | D |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | 9.2 | | | | | HCM 2000 Level of Service | | | A | | | |
| HCM 2000 Volume to Capacity ratio | 0.72 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 95.0 | | | | | Sum of lost time (s) | | | 11.8 | | | |
| Intersection Capacity Utilization | 79.1% | | | | | ICU Level of Service | | | D | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis
2: Slidell St/Onigam St & Sir John A MacDonald Pkwy

Existing (2020)
PM Peak Hour

| Movement | SBR |
|------------------------|------|
| Lane Configurations | |
| Traffic Volume (vph) | 12 |
| Future Volume (vph) | 12 |
| Ideal Flow (vphpl) | 1800 |
| Lane Width | 3.7 |
| Total Lost time (s) | |
| Lane Util. Factor | |
| Frpb, ped/bikes | |
| Flpb, ped/bikes | |
| Fr | |
| Flt Protected | |
| Satd. Flow (prot) | |
| Flt Permitted | |
| Satd. Flow (perm) | |
| Peak-hour factor, PHF | 0.90 |
| Adj. Flow (vph) | 13 |
| RTOR Reduction (vph) | 0 |
| Lane Group Flow (vph) | 0 |
| Confl. Peds. (#/hr) | 6 |
| Confl. Bikes (#/hr) | 6 |
| Heavy Vehicles (%) | 0% |
| Turn Type | |
| Protected Phases | |
| Permitted Phases | |
| Actuated Green, G (s) | |
| Effective Green, g (s) | |
| Actuated g/C Ratio | |
| Clearance Time (s) | |
| Vehicle Extension (s) | |
| Lane Grp Cap (vph) | |
| v/s Ratio Prot | |
| v/s Ratio Perm | |
| v/c Ratio | |
| Uniform Delay, d1 | |
| Progression Factor | |
| Incremental Delay, d2 | |
| Delay (s) | |
| Level of Service | |
| Approach Delay (s) | |
| Approach LOS | |
| Intersection Summary | |

HCM Signalized Intersection Capacity Analysis

3: Bayview Stn Rd & Scott St/Albert St

Existing (2020)

PM Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|-------|------|---------------------------|-------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 21 | 468 | 109 | 89 | 618 | 98 | 105 | 280 | 79 | 52 | 90 | 17 |
| Future Volume (vph) | 21 | 468 | 109 | 89 | 618 | 98 | 105 | 280 | 79 | 52 | 90 | 17 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 3.7 | 3.6 | 3.7 | 3.2 | 3.5 | 3.8 | 3.0 | 4.3 | 3.7 | 3.3 | 4.5 | 3.7 |
| Total Lost time (s) | 6.5 | | 6.5 | 6.5 | 6.5 | 6.4 | 6.4 | | 6.4 | 6.4 | | |
| Lane Util. Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | |
| Frpb, ped/bikes | 0.97 | | 1.00 | 1.00 | 0.88 | 1.00 | 0.99 | | 1.00 | 0.98 | | |
| Flpb, ped/bikes | 1.00 | | 0.96 | 1.00 | 1.00 | 0.93 | 1.00 | | 0.99 | 1.00 | | |
| Fr _t | 0.98 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 | | 1.00 | 0.98 | | |
| Flt Protected | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | |
| Satd. Flow (prot) | 1481 | | 1566 | 1402 | 1368 | 1455 | 1839 | | 1639 | 1845 | | |
| Flt Permitted | 0.97 | | 0.39 | 1.00 | 1.00 | 0.68 | 1.00 | | 0.19 | 1.00 | | |
| Satd. Flow (perm) | 1434 | | 635 | 1402 | 1368 | 1042 | 1839 | | 335 | 1845 | | |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 23 | 520 | 121 | 99 | 687 | 109 | 117 | 311 | 88 | 58 | 100 | 19 |
| RTOR Reduction (vph) | 0 | 8 | 0 | 0 | 0 | 37 | 0 | 11 | 0 | 0 | 7 | 0 |
| Lane Group Flow (vph) | 0 | 656 | 0 | 99 | 687 | 72 | 117 | 388 | 0 | 58 | 112 | 0 |
| Confl. Peds. (#/hr) | 50 | | 66 | 66 | | 50 | 43 | | 11 | 11 | | 43 |
| Confl. Bikes (#/hr) | | | 3 | | | 4 | | | 6 | | | 17 |
| Heavy Vehicles (%) | 0% | 19% | 1% | 0% | 27% | 1% | 2% | 0% | 4% | 0% | 2% | 6% |
| Turn Type | Perm | NA | | Perm | NA | Perm | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | 6 | | 6 | 8 | | | 4 | | | |
| Actuated Green, G (s) | 63.0 | | 63.0 | 63.0 | 63.0 | 24.1 | 24.1 | | 24.1 | 24.1 | | |
| Effective Green, g (s) | 63.0 | | 63.0 | 63.0 | 63.0 | 24.1 | 24.1 | | 24.1 | 24.1 | | |
| Actuated g/C Ratio | 0.63 | | 0.63 | 0.63 | 0.63 | 0.24 | 0.24 | | 0.24 | 0.24 | | |
| Clearance Time (s) | 6.5 | | 6.5 | 6.5 | 6.5 | 6.4 | 6.4 | | 6.4 | 6.4 | | |
| Vehicle Extension (s) | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | |
| Lane Grp Cap (vph) | 903 | | 400 | 883 | 861 | 251 | 443 | | 80 | 444 | | |
| v/s Ratio Prot | | | c0.49 | | | c0.21 | | | | 0.06 | | |
| v/s Ratio Perm | 0.46 | | 0.16 | | 0.05 | 0.11 | | | 0.17 | | | |
| v/c Ratio | 0.73 | | 0.25 | 0.78 | 0.08 | 0.47 | 0.88 | | 0.72 | 0.25 | | |
| Uniform Delay, d1 | 12.6 | | 8.1 | 13.4 | 7.2 | 32.4 | 36.5 | | 34.9 | 30.7 | | |
| Progression Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | |
| Incremental Delay, d2 | 5.1 | | 1.5 | 6.7 | 0.2 | 1.4 | 17.4 | | 27.6 | 0.3 | | |
| Delay (s) | 17.7 | | 9.6 | 20.1 | 7.4 | 33.8 | 53.9 | | 62.5 | 31.0 | | |
| Level of Service | B | | A | C | A | C | D | | E | C | | |
| Approach Delay (s) | 17.7 | | | 17.4 | | | 49.4 | | | 41.3 | | |
| Approach LOS | B | | | B | | | D | | | D | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | 26.7 | | | | HCM 2000 Level of Service | | | | C | | | |
| HCM 2000 Volume to Capacity ratio | 0.81 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 100.0 | | | | Sum of lost time (s) | | | | 12.9 | | | |
| Intersection Capacity Utilization | 97.8% | | | | ICU Level of Service | | | | F | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

Appendix F – Ottawa 2011 O-D Survey, Ottawa West

Ottawa West

Demographic Characteristics

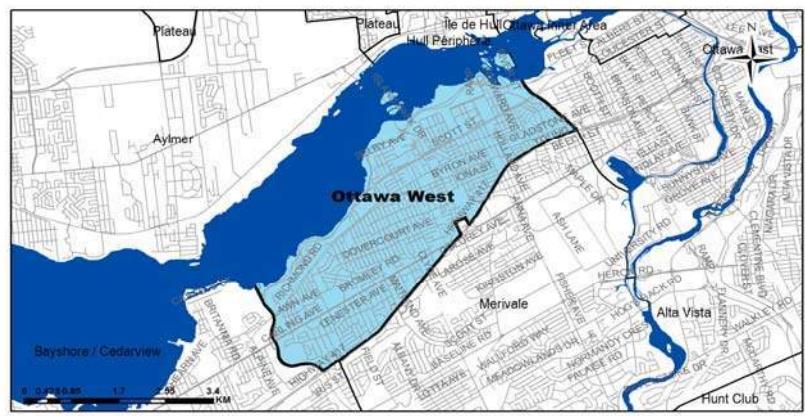
| | | | |
|---------------------|--------|-------------------------|--------|
| Population | 50,410 | Actively Travelled | 40,800 |
| Employed Population | 22,930 | Number of Vehicles | 23,590 |
| Households | 24,070 | Area (km ²) | 18.3 |

| Occupation Status (age 5+) | Male | Female | Total |
|----------------------------|--------|--------|--------|
| Full Time Employed | 10,960 | 9,490 | 20,450 |
| Part Time Employed | 930 | 1,540 | 2,480 |
| Student | 4,680 | 4,690 | 9,370 |
| Retiree | 4,580 | 7,260 | 11,840 |
| Unemployed | 570 | 980 | 1,540 |
| Homemaker | 30 | 990 | 1,020 |
| Other | 670 | 600 | 1,270 |
| Total: | 22,410 | 25,560 | 47,970 |

| Traveller Characteristics | Male | Female | Total |
|---------------------------|--------|--------|---------|
| Transit Pass Holders | 4,120 | 5,780 | 9,900 |
| Licensed Drivers | 17,020 | 17,720 | 34,740 |
| Telecommuters | 140 | 250 | 390 |
| Trips made by residents | 65,610 | 75,080 | 140,690 |

Selected Indicators

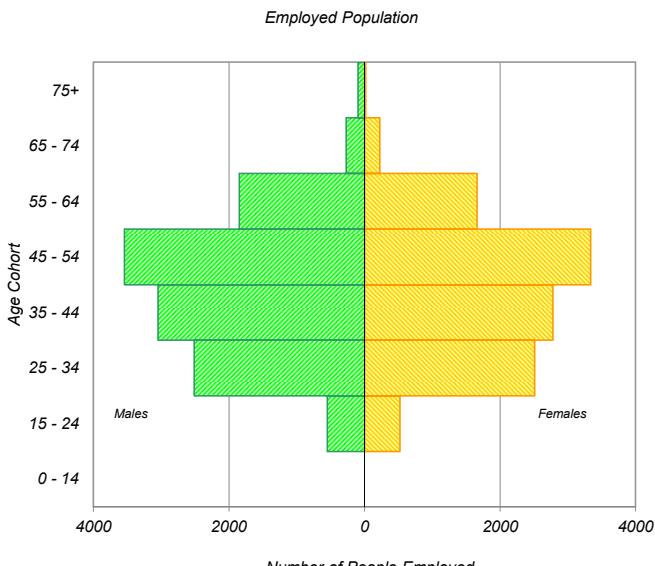
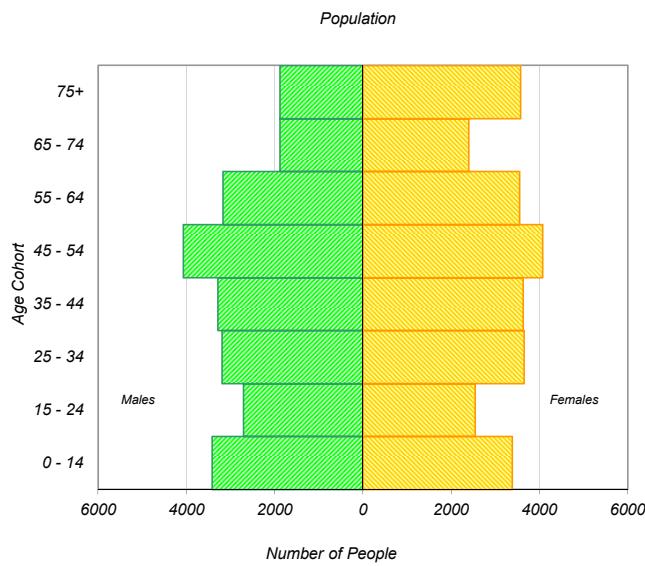
| | |
|---|------|
| Daily Trips per Person (age 5+) | 2.93 |
| Vehicles per Person | 0.47 |
| Number of Persons per Household | 2.09 |
| Daily Trips per Household | 5.85 |
| Vehicles per Household | 0.98 |
| Workers per Household | 0.95 |
| Population Density (Pop/km ²) | 2760 |



| Household Size | | |
|----------------|--------|------|
| 1 person | 10,380 | 43% |
| 2 persons | 7,710 | 32% |
| 3 persons | 2,730 | 11% |
| 4 persons | 2,280 | 9% |
| 5+ persons | 970 | 4% |
| Total: | 24,070 | 100% |

| Households by Vehicle Availability | | |
|------------------------------------|--------|------|
| 0 vehicles | 6,230 | 26% |
| 1 vehicle | 12,950 | 54% |
| 2 vehicles | 4,200 | 17% |
| 3 vehicles | 540 | 2% |
| 4+ vehicles | 140 | 1% |
| Total: | 24,070 | 100% |

| Households by Dwelling Type | | |
|-----------------------------|--------|------|
| Single-detached | 8,320 | 35% |
| Semi-detached | 1,780 | 7% |
| Townhouse | 980 | 4% |
| Apartment/Condo | 13,000 | 54% |
| Total: | 24,070 | 100% |

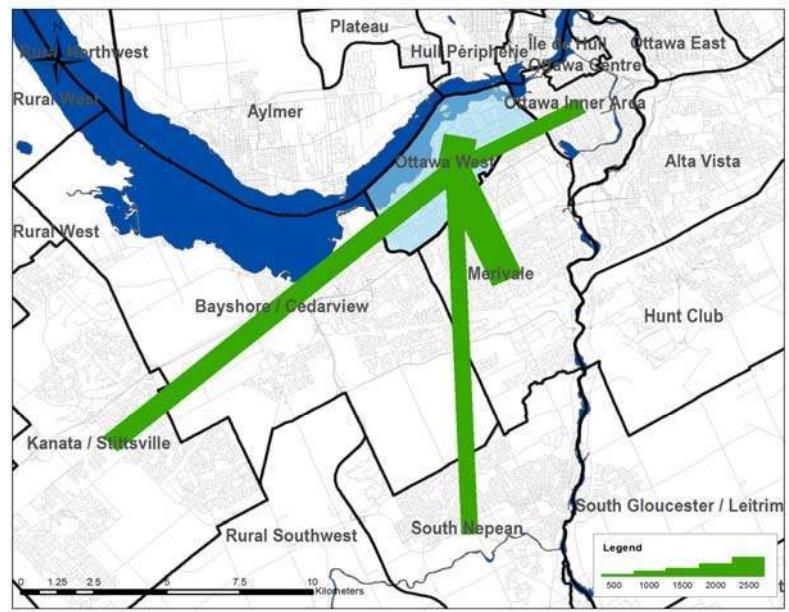


* In 2005 data was only collected for household members aged 11+ therefore these results cannot be compared to the 2011 data.

Travel Patterns

Top Five Origins of Trips to Ottawa West

AM Peak Period



Summary of Trips to and from Ottawa West

| Districts | Trips From District | Destinations of Trips To District | | Origins of Trips To District |
|----------------------------|---------------------|-----------------------------------|---------|------------------------------|
| | | % Total | % Total | |
| Ottawa Centre | 4,270 | 16% | 340 | 1% |
| Ottawa Inner Area | 3,080 | 12% | 1,750 | 5% |
| Ottawa East | 310 | 1% | 460 | 1% |
| Beacon Hill | 150 | 1% | 610 | 2% |
| Alta Vista | 1,550 | 6% | 1,160 | 4% |
| Hunt Club | 360 | 1% | 580 | 2% |
| Merivale | 3,340 | 13% | 4,960 | 15% |
| Ottawa West | 8,280 | 32% | 8,280 | 25% |
| Bayshore / Cedarview | 1,940 | 7% | 4,870 | 15% |
| Orléans | 220 | 1% | 1,460 | 4% |
| Rural East | 40 | 0% | 60 | 0% |
| Rural Southeast | 50 | 0% | 190 | 1% |
| South Gloucester / Leitrim | 0 | 0% | 290 | 1% |
| South Nepean | 160 | 1% | 1,830 | 6% |
| Rural Southwest | 80 | 0% | 400 | 1% |
| Kanata / Stittsville | 840 | 3% | 2,020 | 6% |
| Rural West | 70 | 0% | 170 | 1% |
| Île de Hull | 730 | 3% | 170 | 1% |
| Hull Périphérie | 170 | 1% | 360 | 1% |
| Plateau | 40 | 0% | 760 | 2% |
| Aylmer | 60 | 0% | 770 | 2% |
| Rural Northwest | 20 | 0% | 310 | 1% |
| Pointe Gatineau | 30 | 0% | 450 | 1% |
| Gatineau Est | 70 | 0% | 310 | 1% |
| Rural Northeast | 60 | 0% | 170 | 1% |
| Buckingham / Masson-Angers | 70 | 0% | 140 | 0% |
| Ontario Sub-Total: | 24,740 | 95% | 29,430 | 90% |
| Québec Sub-Total: | 1,250 | 5% | 3,440 | 10% |
| Total: | 25,990 | 100% | 32,870 | 100% |

Trips by Trip Purpose

| 24 Hours | From District | To District | Within District | |
|--------------------------------|----------------------|----------------------|----------------------------|-------------|
| Work or related | 17,850 | 19% | 24,050 | 25% |
| School | 3,820 | 4% | 4,540 | 5% |
| Shopping | 9,960 | 10% | 10,800 | 11% |
| Leisure | 9,570 | 10% | 9,420 | 10% |
| Medical | 2,740 | 3% | 2,190 | 2% |
| Pick-up / drive passenger | 6,010 | 6% | 7,490 | 8% |
| Return Home | 40,560 | 43% | 32,380 | 34% |
| Other | 4,500 | 5% | 4,550 | 5% |
| Total: | 95,010 | 100% | 95,420 | 100% |
| AM Peak (06:30 - 08:59) | From District | To District | Within District | |
| Work or related | 11,500 | 65% | 16,000 | 65% |
| School | 2,450 | 14% | 4,090 | 17% |
| Shopping | 120 | 1% | 250 | 1% |
| Leisure | 720 | 4% | 450 | 2% |
| Medical | 470 | 3% | 330 | 1% |
| Pick-up / drive passenger | 1,110 | 6% | 1,880 | 8% |
| Return Home | 790 | 4% | 530 | 2% |
| Other | 540 | 3% | 1,060 | 4% |
| Total: | 17,700 | 100% | 24,590 | 100% |
| PM Peak (15:30 - 17:59) | From District | To District | Within District | |
| Work or related | 590 | 2% | 550 | 3% |
| School | 180 | 1% | 10 | 0% |
| Shopping | 2,510 | 10% | 2,680 | 12% |
| Leisure | 2,090 | 8% | 2,220 | 10% |
| Medical | 200 | 1% | 270 | 1% |
| Pick-up / drive passenger | 1,970 | 8% | 2,350 | 11% |
| Return Home | 17,330 | 68% | 12,540 | 58% |
| Other | 790 | 3% | 870 | 4% |
| Total: | 25,660 | 100% | 21,490 | 100% |
| Peak Period (%) | Total: | % of 24 Hours | Within District (%) | |
| 24 Hours | 248,320 | | 23% | |
| AM Peak Period | 50,570 | 20% | 16% | |
| PM Peak Period | 61,370 | 25% | 23% | |

Trips by Primary Travel Mode

| 24 Hours | From District | To District | Within District |
|--------------------------------|----------------------|--------------------|------------------------|
| Auto Driver | 53,530 | 56% | 22,130 |
| Auto Passenger | 14,560 | 15% | 6,300 |
| Transit | 18,670 | 20% | 2,810 |
| Bicycle | 3,120 | 3% | 3,110 |
| Walk | 2,780 | 3% | 21,610 |
| Other | 2,340 | 2% | 1,910 |
| Total: | 95,000 | 100% | 57,870 |
| AM Peak (06:30 - 08:59) | From District | To District | Within District |
| Auto Driver | 8,230 | 46% | 2,740 |
| Auto Passenger | 1,910 | 11% | 1,220 |
| Transit | 5,490 | 31% | 370 |
| Bicycle | 1,050 | 6% | 500 |
| Walk | 650 | 4% | 2,770 |
| Other | 370 | 2% | 690 |
| Total: | 17,700 | 100% | 8,290 |
| PM Peak (15:30 - 17:59) | From District | To District | Within District |
| Auto Driver | 14,180 | 55% | 4,550 |
| Auto Passenger | 4,060 | 16% | 1,370 |
| Transit | 5,400 | 21% | 570 |
| Bicycle | 750 | 3% | 1,000 |
| Walk | 690 | 3% | 6,400 |
| Other | 570 | 2% | 320 |
| Total: | 25,650 | 100% | 14,210 |
| Avg Vehicle Occupancy | From District | To District | Within District |
| 24 Hours | 1.27 | 1.27 | 1.28 |
| AM Peak Period | 1.23 | 1.30 | 1.45 |
| PM Peak Period | 1.29 | 1.26 | 1.30 |
| Transit Modal Split | From District | To District | Within District |
| 24 Hours | 22% | 22% | 9% |
| AM Peak Period | 35% | 25% | 9% |
| PM Peak Period | 23% | 26% | 9% |

Appendix G – Trip Assignment Calculations

| Parcel 1 | | | |
|-----------------------------------|-----|--------------|-----|
| AM Peak Hour | | PM Peak Hour | |
| In | Out | In | Out |
| West on Sir John A MacDonald Pkwy | 24% | 11 | 4 |
| East on Sir John A MacDonald Pkwy | 24% | 11 | 4 |
| North on Parkdale | 12% | 5 | 2 |
| South on Parkdale | 10% | 4 | 1 |
| West on Scott | 11% | 5 | 2 |
| East on Scott | 12% | 5 | 2 |
| South on Bayview Station | 6% | 3 | 0 |
| Parcel 2 | | | |
| AM Peak Hour | | PM Peak Hour | |
| In | Out | In | Out |
| West on Sir John A MacDonald Pkwy | 24% | 9 | 3 |
| East on Sir John A MacDonald Pkwy | 24% | 9 | 3 |
| North on Parkdale | 12% | 5 | 2 |
| South on Parkdale | 10% | 4 | 1 |
| West on Scott | 11% | 4 | 1 |
| East on Scott | 12% | 5 | 1 |
| South on Bayview Station | 6% | 2 | 1 |
| Parcel 3 | | | |
| AM Peak Hour | | PM Peak Hour | |
| In | Out | In | Out |
| West on Sir John A MacDonald Pkwy | 24% | 9 | 3 |
| East on Sir John A MacDonald Pkwy | 24% | 9 | 3 |
| North on Parkdale | 12% | 5 | 2 |
| South on Parkdale | 10% | 4 | 1 |
| West on Scott | 11% | 4 | 1 |
| East on Scott | 12% | 5 | 1 |
| South on Bayview Station | 6% | 2 | 1 |
| Parcel 4 | | | |
| AM Peak Hour | | PM Peak Hour | |
| In | Out | In | Out |
| West on Sir John A MacDonald Pkwy | 24% | 11 | 3 |
| East on Sir John A MacDonald Pkwy | 24% | 10 | 3 |
| North on Parkdale | 12% | 5 | 2 |
| South on Parkdale | 10% | 4 | 1 |
| West on Scott | 11% | 5 | 2 |
| East on Scott | 12% | 5 | 2 |
| South on Bayview Station | 6% | 3 | 1 |
| Parcel 5 | | | |
| AM Peak Hour | | PM Peak Hour | |
| In | Out | In | Out |
| West on Sir John A MacDonald Pkwy | 24% | 9 | 3 |
| East on Sir John A MacDonald Pkwy | 24% | 9 | 3 |
| North on Parkdale | 12% | 5 | 2 |
| South on Parkdale | 10% | 4 | 1 |
| West on Scott | 11% | 4 | 1 |
| East on Scott | 12% | 5 | 2 |
| South on Bayview Station | 6% | 2 | 1 |
| Parcel 6 | | | |
| AM Peak Hour | | PM Peak Hour | |
| In | Out | In | Out |
| West on Sir John A MacDonald Pkwy | 24% | 9 | 3 |
| East on Sir John A MacDonald Pkwy | 24% | 9 | 3 |
| North on Parkdale | 12% | 5 | 2 |
| South on Parkdale | 10% | 4 | 1 |
| West on Scott | 11% | 4 | 1 |
| East on Scott | 12% | 5 | 2 |
| South on Bayview Station | 6% | 2 | 1 |

Appendix H – Future Background (2023, 2028) Synchro and SIDRA Outputs

MOVEMENT SUMMARY

Site: 1 [Burnside Roundabout - Background (2023) - AM]

Burnside Roundabout - Background (2023) - AM

Site Category: (None)

Roundabout

| Movement Performance - Vehicles | | | | | | | | | | | | |
|--|------|--------------------|------------|---------------|-------------------|------------------|--------------------------------|------------------|--------------|---------------------|------------------|--------------------|
| Mov ID | Turn | Demand Total veh/h | Flows HV % | Deg. Satn v/c | Average Delay sec | Level of Service | 95% Back of Queue Vehicles veh | Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Bayview Station Road | | | | | | | | | | | | |
| 21u | U | 2 | 0.0 | 0.071 | 9.2 | LOS A | 0.2 | 1.4 | 0.08 | 0.54 | 0.08 | 47.6 |
| 21 | L2 | 64 | 9.0 | 0.071 | 7.4 | LOS A | 0.2 | 1.4 | 0.08 | 0.54 | 0.08 | 42.8 |
| 23a | R1 | 25 | 0.0 | 0.071 | 2.5 | LOS A | 0.2 | 1.4 | 0.08 | 0.54 | 0.08 | 43.7 |
| Approach | | 92 | 6.3 | 0.071 | 6.1 | LOS A | 0.2 | 1.4 | 0.08 | 0.54 | 0.08 | 43.1 |
| North: Slidell Street | | | | | | | | | | | | |
| 7u | U | 1 | 0.0 | 0.075 | 9.2 | LOS A | 0.2 | 1.5 | 0.11 | 0.55 | 0.11 | 21.4 |
| 7a | L1 | 88 | 7.0 | 0.075 | 6.6 | LOS A | 0.2 | 1.5 | 0.11 | 0.55 | 0.11 | 43.3 |
| 9a | R1 | 8 | 0.0 | 0.075 | 2.6 | LOS A | 0.2 | 1.5 | 0.11 | 0.55 | 0.11 | 38.1 |
| Approach | | 97 | 6.4 | 0.075 | 6.3 | LOS A | 0.2 | 1.5 | 0.11 | 0.55 | 0.11 | 42.6 |
| SouthWest: Burnside Avenue | | | | | | | | | | | | |
| 30u | U | 1 | 0.0 | 0.276 | 7.2 | LOS A | 0.9 | 6.6 | 0.16 | 0.36 | 0.16 | 41.7 |
| 30a | L1 | 34 | 0.0 | 0.276 | 5.0 | LOS A | 0.9 | 6.6 | 0.16 | 0.36 | 0.16 | 25.7 |
| 32 | R2 | 348 | 0.0 | 0.276 | 2.0 | LOS A | 0.9 | 6.6 | 0.16 | 0.36 | 0.16 | 42.3 |
| Approach | | 383 | 0.0 | 0.276 | 2.3 | LOS A | 0.9 | 6.6 | 0.16 | 0.36 | 0.16 | 40.7 |
| All Vehicles | | 572 | 2.1 | 0.276 | 3.6 | LOS A | 0.9 | 6.6 | 0.14 | 0.42 | 0.14 | 41.3 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akcelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

MOVEMENT SUMMARY

Site: 1 [Burnside Roundabout - Background (2023) - PM]

Burnside Roundabout - Background (2023) - PM

Site Category: (None)

Roundabout

| Movement Performance - Vehicles | | | | | | | | | | | | |
|--|------|--------------------|------------|---------------|-------------------|------------------|--------------------------------|------------------|--------------|---------------------|------------------|--------------------|
| Mov ID | Turn | Demand Total veh/h | Flows HV % | Deg. Satn v/c | Average Delay sec | Level of Service | 95% Back of Queue Vehicles veh | Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Bayview Station Road | | | | | | | | | | | | |
| 21u | U | 11 | 11.0 | 0.356 | 9.3 | LOS A | 1.3 | 9.4 | 0.11 | 0.57 | 0.11 | 46.8 |
| 21 | L2 | 417 | 1.0 | 0.356 | 7.4 | LOS A | 1.3 | 9.4 | 0.11 | 0.57 | 0.11 | 42.5 |
| 23a | R1 | 93 | 3.0 | 0.356 | 2.6 | LOS A | 1.3 | 9.4 | 0.11 | 0.57 | 0.11 | 42.9 |
| Approach | | 521 | 1.6 | 0.356 | 6.6 | LOS A | 1.3 | 9.4 | 0.11 | 0.57 | 0.11 | 42.6 |
| North: Slidell Street | | | | | | | | | | | | |
| 7u | U | 1 | 0.0 | 0.074 | 10.2 | LOS B | 0.3 | 1.8 | 0.35 | 0.61 | 0.35 | 21.1 |
| 7a | L1 | 63 | 6.0 | 0.074 | 7.5 | LOS A | 0.3 | 1.8 | 0.35 | 0.61 | 0.35 | 42.9 |
| 9a | R1 | 18 | 0.0 | 0.074 | 3.6 | LOS A | 0.3 | 1.8 | 0.35 | 0.61 | 0.35 | 37.8 |
| Approach | | 82 | 4.6 | 0.074 | 6.7 | LOS A | 0.3 | 1.8 | 0.35 | 0.61 | 0.35 | 41.4 |
| SouthWest: Burnside Avenue | | | | | | | | | | | | |
| 30u | U | 3 | 0.0 | 0.112 | 7.1 | LOS A | 0.3 | 2.5 | 0.14 | 0.39 | 0.14 | 41.3 |
| 30a | L1 | 38 | 0.0 | 0.112 | 4.9 | LOS A | 0.3 | 2.5 | 0.14 | 0.39 | 0.14 | 27.9 |
| 32 | R2 | 106 | 4.0 | 0.112 | 2.0 | LOS A | 0.3 | 2.5 | 0.14 | 0.39 | 0.14 | 41.9 |
| Approach | | 147 | 2.9 | 0.112 | 2.8 | LOS A | 0.3 | 2.5 | 0.14 | 0.39 | 0.14 | 38.4 |
| All Vehicles | | 751 | 2.2 | 0.356 | 5.9 | LOS A | 1.3 | 9.4 | 0.14 | 0.54 | 0.14 | 41.6 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

MOVEMENT SUMMARY

Site: 1 [Burnside Roundabout - Background (2028) - AM]

Burnside Roundabout - Background (2028) - AM

Site Category: (None)

Roundabout

| Movement Performance - Vehicles | | | | | | | | | | | | |
|--|------|--------------------|------------|---------------|-------------------|------------------|--------------------------------|------------------|--------------|---------------------|------------------|--------------------|
| Mov ID | Turn | Demand Total veh/h | Flows HV % | Deg. Satn v/c | Average Delay sec | Level of Service | 95% Back of Queue Vehicles veh | Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Bayview Station Road | | | | | | | | | | | | |
| 21u | U | 2 | 0.0 | 0.085 | 9.2 | LOS A | 0.2 | 1.8 | 0.09 | 0.55 | 0.09 | 47.5 |
| 21 | L2 | 79 | 9.0 | 0.085 | 7.4 | LOS A | 0.2 | 1.8 | 0.09 | 0.55 | 0.09 | 42.8 |
| 23a | R1 | 28 | 0.0 | 0.085 | 2.5 | LOS A | 0.2 | 1.8 | 0.09 | 0.55 | 0.09 | 43.6 |
| Approach | | 110 | 6.5 | 0.085 | 6.2 | LOS A | 0.2 | 1.8 | 0.09 | 0.55 | 0.09 | 43.0 |
| North: Slidell Street | | | | | | | | | | | | |
| 7u | U | 1 | 0.0 | 0.085 | 9.3 | LOS A | 0.2 | 1.7 | 0.13 | 0.55 | 0.13 | 21.4 |
| 7a | L1 | 99 | 7.0 | 0.085 | 6.6 | LOS A | 0.2 | 1.7 | 0.13 | 0.55 | 0.13 | 43.3 |
| 9a | R1 | 10 | 0.0 | 0.085 | 2.6 | LOS A | 0.2 | 1.7 | 0.13 | 0.55 | 0.13 | 38.1 |
| Approach | | 109 | 6.3 | 0.085 | 6.3 | LOS A | 0.2 | 1.7 | 0.13 | 0.55 | 0.13 | 42.6 |
| SouthWest: Burnside Avenue | | | | | | | | | | | | |
| 30u | U | 1 | 0.0 | 0.324 | 7.2 | LOS A | 1.2 | 8.3 | 0.18 | 0.36 | 0.18 | 41.6 |
| 30a | L1 | 38 | 0.0 | 0.324 | 5.0 | LOS A | 1.2 | 8.3 | 0.18 | 0.36 | 0.18 | 25.7 |
| 32 | R2 | 410 | 0.0 | 0.324 | 2.1 | LOS A | 1.2 | 8.3 | 0.18 | 0.36 | 0.18 | 42.2 |
| Approach | | 448 | 0.0 | 0.324 | 2.3 | LOS A | 1.2 | 8.3 | 0.18 | 0.36 | 0.18 | 40.8 |
| All Vehicles | | 667 | 2.1 | 0.324 | 3.6 | LOS A | 1.2 | 8.3 | 0.16 | 0.42 | 0.16 | 41.3 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akcelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

MOVEMENT SUMMARY

Site: 1 [Burnside Roundabout - Background (2028) - PM]

Burnside Roundabout - Background (2028) - PM

Site Category: (None)

Roundabout

| Movement Performance - Vehicles | | | | | | | | | | | | |
|--|------|--------------------|------------|---------------|-------------------|------------------|--------------------------------|------------------|--------------|---------------------|------------------|--------------------|
| Mov ID | Turn | Demand Total veh/h | Flows HV % | Deg. Satn v/c | Average Delay sec | Level of Service | 95% Back of Queue Vehicles veh | Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Bayview Station Road | | | | | | | | | | | | |
| 21u | U | 12 | 11.0 | 0.420 | 9.3 | LOS A | 1.7 | 12.2 | 0.13 | 0.57 | 0.13 | 46.7 |
| 21 | L2 | 501 | 1.0 | 0.420 | 7.4 | LOS A | 1.7 | 12.2 | 0.13 | 0.57 | 0.13 | 42.4 |
| 23a | R1 | 103 | 3.0 | 0.420 | 2.6 | LOS A | 1.7 | 12.2 | 0.13 | 0.57 | 0.13 | 42.8 |
| Approach | | 616 | 1.5 | 0.420 | 6.6 | LOS A | 1.7 | 12.2 | 0.13 | 0.57 | 0.13 | 42.5 |
| North: Slidell Street | | | | | | | | | | | | |
| 7u | U | 1 | 0.0 | 0.086 | 10.5 | LOS B | 0.3 | 2.3 | 0.40 | 0.63 | 0.40 | 20.9 |
| 7a | L1 | 70 | 6.0 | 0.086 | 7.9 | LOS A | 0.3 | 2.3 | 0.40 | 0.63 | 0.40 | 42.6 |
| 9a | R1 | 20 | 0.0 | 0.086 | 3.9 | LOS A | 0.3 | 2.3 | 0.40 | 0.63 | 0.40 | 37.6 |
| Approach | | 91 | 4.6 | 0.086 | 7.0 | LOS A | 0.3 | 2.3 | 0.40 | 0.63 | 0.40 | 41.2 |
| SouthWest: Burnside Avenue | | | | | | | | | | | | |
| 30u | U | 4 | 0.0 | 0.138 | 7.1 | LOS A | 0.5 | 3.3 | 0.15 | 0.38 | 0.15 | 41.3 |
| 30a | L1 | 42 | 0.0 | 0.138 | 4.9 | LOS A | 0.5 | 3.3 | 0.15 | 0.38 | 0.15 | 27.9 |
| 32 | R2 | 136 | 4.0 | 0.138 | 2.0 | LOS A | 0.5 | 3.3 | 0.15 | 0.38 | 0.15 | 41.9 |
| Approach | | 182 | 3.0 | 0.138 | 2.8 | LOS A | 0.5 | 3.3 | 0.15 | 0.38 | 0.15 | 38.8 |
| All Vehicles | | 890 | 2.1 | 0.420 | 5.9 | LOS A | 1.7 | 12.2 | 0.16 | 0.54 | 0.16 | 41.6 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akcelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

HCM Signalized Intersection Capacity Analysis

1: Parkdale Ave & Burnside Ave

Future Background (2023)

AM Peak Hour



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|------------------------|-------|------|------|-------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (vph) | 91 | 91 | 357 | 63 | 206 | 547 |
| Future Volume (vph) | 91 | 91 | 357 | 63 | 206 | 547 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 4.2 | 3.7 | 4.8 | 3.7 | 3.7 | 4.8 |
| Total Lost time (s) | 5.4 | | 5.2 | | | 5.2 |
| Lane Util. Factor | 1.00 | | 1.00 | | | 1.00 |
| Frpb, ped/bikes | 0.96 | | 0.99 | | | 1.00 |
| Flpb, ped/bikes | 1.00 | | 1.00 | | | 1.00 |
| Fr _t | 0.93 | | 0.98 | | | 1.00 |
| Flt Protected | 0.98 | | 1.00 | | | 0.99 |
| Satd. Flow (prot) | 1597 | | 1950 | | | 1968 |
| Flt Permitted | 0.98 | | 1.00 | | | 0.76 |
| Satd. Flow (perm) | 1597 | | 1950 | | | 1521 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 91 | 91 | 357 | 63 | 206 | 547 |
| RTOR Reduction (vph) | 65 | 0 | 9 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 117 | 0 | 411 | 0 | 0 | 753 |
| Confl. Peds. (#/hr) | 60 | 32 | | 13 | 13 | |
| Confl. Bikes (#/hr) | | 1 | | 2 | | |
| Heavy Vehicles (%) | 0% | 9% | 1% | 7% | 2% | 2% |
| Turn Type | pm+pt | | NA | | Perm | NA |
| Protected Phases | 3 | | 2 | | | 6 |
| Permitted Phases | 8 | | | 6 | | |
| Actuated Green, G (s) | 10.4 | | 39.0 | | | 39.0 |
| Effective Green, g (s) | 10.4 | | 39.0 | | | 39.0 |
| Actuated g/C Ratio | 0.17 | | 0.65 | | | 0.65 |
| Clearance Time (s) | 5.4 | | 5.2 | | | 5.2 |
| Vehicle Extension (s) | 3.0 | | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | 276 | | 1267 | | | 988 |
| v/s Ratio Prot | c0.07 | | 0.21 | | | |
| v/s Ratio Perm | | | | c0.50 | | |
| v/c Ratio | 0.42 | | 0.32 | | | 0.76 |
| Uniform Delay, d1 | 22.1 | | 4.7 | | | 7.3 |
| Progression Factor | 1.00 | | 1.00 | | | 1.00 |
| Incremental Delay, d2 | 1.0 | | 0.7 | | | 5.5 |
| Delay (s) | 23.2 | | 5.3 | | | 12.8 |
| Level of Service | C | | A | | | B |
| Approach Delay (s) | 23.2 | | 5.3 | | | 12.8 |
| Approach LOS | C | | A | | | B |

Intersection Summary

| | | | |
|-----------------------------------|-------|---------------------------|------|
| HCM 2000 Control Delay | 11.9 | HCM 2000 Level of Service | B |
| HCM 2000 Volume to Capacity ratio | 0.69 | | |
| Actuated Cycle Length (s) | 60.0 | Sum of lost time (s) | 10.6 |
| Intersection Capacity Utilization | 92.3% | ICU Level of Service | F |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
2: Slidell St/Onigam St & Sir John A MacDonald Pkwy

Future Background (2023)
AM Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBL | SBT |
|-----------------------------------|-------|------|------|------|---------------------------|------|------|-------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 0 | 1647 | 24 | 1 | 1119 | 1 | 1 | 1 | 23 | 1 | 1 | 5 |
| Future Volume (vph) | 0 | 1647 | 24 | 1 | 1119 | 1 | 1 | 1 | 23 | 1 | 1 | 5 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 3.7 | 3.8 | 3.7 | 3.7 | 3.8 | 3.7 | 3.7 | 3.7 | 3.9 | 3.7 | 3.7 | 4.0 |
| Total Lost time (s) | | 5.5 | | | 5.5 | | | | 6.3 | | | 6.3 |
| Lane Util. Factor | 0.95 | | | | 0.95 | | | | 1.00 | | | 1.00 |
| Frpb, ped/bikes | 1.00 | | | | 1.00 | | | | 1.00 | | | 0.99 |
| Flpb, ped/bikes | 1.00 | | | | 1.00 | | | | 1.00 | | | 1.00 |
| Fr _t | 1.00 | | | | 1.00 | | | | 0.99 | | | 0.95 |
| Flt Protected | 1.00 | | | | 1.00 | | | | 1.00 | | | 0.99 |
| Satd. Flow (prot) | 3487 | | | | 3461 | | | | 1840 | | | 1773 |
| Flt Permitted | 1.00 | | | | 0.95 | | | | 0.98 | | | 0.97 |
| Satd. Flow (perm) | 3487 | | | | 3302 | | | | 1804 | | | 1724 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 0 | 1647 | 24 | 1 | 1119 | 1 | 1 | 1 | 23 | 1 | 1 | 5 |
| RTOR Reduction (vph) | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 3 |
| Lane Group Flow (vph) | 0 | 1670 | 0 | 0 | 1121 | 0 | 0 | 0 | 25 | 0 | 0 | 6 |
| Confl. Peds. (#/hr) | 2 | | 1 | 1 | | 2 | 1 | 3 | | 4 | 4 | |
| Confl. Bikes (#/hr) | | | 1 | | | | | | 12 | | | |
| Heavy Vehicles (%) | 0% | 0% | 0% | 0% | 1% | 0% | 0% | 0% | 0% | 0% | 0% | 0% |
| Turn Type | | NA | | Perm | NA | | Perm | Perm | NA | | Perm | NA |
| Protected Phases | | 2 | | | 6 | | | | 8 | | | 4 |
| Permitted Phases | 2 | | 6 | | | 8 | 8 | | | 4 | | |
| Actuated Green, G (s) | 73.8 | | | 73.8 | | | | 9.4 | | | | 9.4 |
| Effective Green, g (s) | 73.8 | | | 73.8 | | | | 9.4 | | | | 9.4 |
| Actuated g/C Ratio | 0.78 | | | 0.78 | | | | 0.10 | | | | 0.10 |
| Clearance Time (s) | 5.5 | | | 5.5 | | | | 6.3 | | | | 6.3 |
| Vehicle Extension (s) | 3.0 | | | 3.0 | | | | 3.0 | | | | 3.0 |
| Lane Grp Cap (vph) | 2708 | | | 2565 | | | | 178 | | | | 170 |
| v/s Ratio Prot | c0.48 | | | | | | | | | | | |
| v/s Ratio Perm | | | | 0.34 | | | | c0.01 | | | | 0.00 |
| v/c Ratio | 0.62 | | | 0.44 | | | | 0.14 | | | | 0.04 |
| Uniform Delay, d1 | 4.5 | | | 3.6 | | | | 39.1 | | | | 38.7 |
| Progression Factor | 1.00 | | | 1.00 | | | | 1.00 | | | | 1.00 |
| Incremental Delay, d2 | 1.1 | | | 0.5 | | | | 0.4 | | | | 0.1 |
| Delay (s) | 5.6 | | | 4.1 | | | | 39.5 | | | | 38.8 |
| Level of Service | A | | | A | | | | D | | | | D |
| Approach Delay (s) | 5.6 | | | 4.1 | | | | 39.5 | | | | 38.8 |
| Approach LOS | A | | | A | | | | D | | | | D |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | 5.4 | | | | HCM 2000 Level of Service | | | A | | | | |
| HCM 2000 Volume to Capacity ratio | 0.56 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 95.0 | | | | Sum of lost time (s) | | | 11.8 | | | | |
| Intersection Capacity Utilization | 68.8% | | | | ICU Level of Service | | | C | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| Movement | SBR |
|------------------------|------|
| Lane Configurations | |
| Traffic Volume (vph) | 3 |
| Future Volume (vph) | 3 |
| Ideal Flow (vphpl) | 1800 |
| Lane Width | 3.7 |
| Total Lost time (s) | |
| Lane Util. Factor | |
| Frpb, ped/bikes | |
| Flpb, ped/bikes | |
| Fr | |
| Flt Protected | |
| Satd. Flow (prot) | |
| Flt Permitted | |
| Satd. Flow (perm) | |
| Peak-hour factor, PHF | 1.00 |
| Adj. Flow (vph) | 3 |
| RTOR Reduction (vph) | 0 |
| Lane Group Flow (vph) | 0 |
| Confl. Peds. (#/hr) | 3 |
| Confl. Bikes (#/hr) | 2 |
| Heavy Vehicles (%) | 0% |
| Turn Type | |
| Protected Phases | |
| Permitted Phases | |
| Actuated Green, G (s) | |
| Effective Green, g (s) | |
| Actuated g/C Ratio | |
| Clearance Time (s) | |
| Vehicle Extension (s) | |
| Lane Grp Cap (vph) | |
| v/s Ratio Prot | |
| v/s Ratio Perm | |
| v/c Ratio | |
| Uniform Delay, d1 | |
| Progression Factor | |
| Incremental Delay, d2 | |
| Delay (s) | |
| Level of Service | |
| Approach Delay (s) | |
| Approach LOS | |
| Intersection Summary | |

HCM Signalized Intersection Capacity Analysis

3: Bayview Stn Rd & Scott St/Albert St

Future Background (2023)

AM Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|--------|------|------|------|---------------------------|------|------|------|-------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 23 | 674 | 87 | 54 | 326 | 34 | 49 | 99 | 123 | 142 | 245 | 28 |
| Future Volume (vph) | 23 | 674 | 87 | 54 | 326 | 34 | 49 | 99 | 123 | 142 | 245 | 28 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 3.7 | 3.6 | 3.7 | 3.2 | 3.5 | 3.8 | 3.0 | 4.3 | 3.7 | 3.3 | 4.5 | 3.7 |
| Total Lost time (s) | 6.5 | | 6.5 | 6.5 | 6.5 | 6.4 | 6.4 | | 6.4 | 6.4 | | |
| Lane Util. Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | |
| Frpb, ped/bikes | 0.99 | | 1.00 | 1.00 | 0.96 | 1.00 | 0.92 | | 1.00 | 0.99 | | |
| Flpb, ped/bikes | 1.00 | | 0.97 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.96 | 1.00 | | |
| Fr _t | 0.99 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.92 | | 1.00 | 0.98 | | |
| Flt Protected | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | |
| Satd. Flow (prot) | 1422 | | 1559 | 1338 | 1399 | 1344 | 1590 | | 1528 | 1860 | | |
| Flt Permitted | 0.98 | | 0.34 | 1.00 | 1.00 | 0.39 | 1.00 | | 0.49 | 1.00 | | |
| Satd. Flow (perm) | 1402 | | 563 | 1338 | 1399 | 546 | 1590 | | 786 | 1860 | | |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 23 | 674 | 87 | 54 | 326 | 34 | 49 | 99 | 123 | 142 | 245 | 28 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 | 0 | 12 | 0 | 47 | 0 | 0 | 5 | 0 |
| Lane Group Flow (vph) | 0 | 780 | 0 | 54 | 326 | 22 | 49 | 175 | 0 | 142 | 268 | 0 |
| Confl. Peds. (#/hr) | 12 | | 52 | 52 | | 12 | 43 | | 30 | 30 | | 43 |
| Confl. Bikes (#/hr) | | | 2 | | | | | | 37 | | | 11 |
| Heavy Vehicles (%) | 0% | 26% | 4% | 2% | 33% | 7% | 13% | 4% | 3% | 4% | 2% | 17% |
| Turn Type | Perm | NA | | Perm | NA | Perm | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | 6 | 8 | | | 4 | | |
| Actuated Green, G (s) | 65.3 | | 65.3 | 65.3 | 65.3 | 21.8 | 21.8 | | 21.8 | 21.8 | | |
| Effective Green, g (s) | 65.3 | | 65.3 | 65.3 | 65.3 | 21.8 | 21.8 | | 21.8 | 21.8 | | |
| Actuated g/C Ratio | 0.65 | | 0.65 | 0.65 | 0.65 | 0.22 | 0.22 | | 0.22 | 0.22 | | |
| Clearance Time (s) | 6.5 | | 6.5 | 6.5 | 6.5 | 6.4 | 6.4 | | 6.4 | 6.4 | | |
| Vehicle Extension (s) | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | |
| Lane Grp Cap (vph) | 915 | | 367 | 873 | 913 | 119 | 346 | | 171 | 405 | | |
| v/s Ratio Prot | | | | 0.24 | | | | 0.11 | | | 0.14 | |
| v/s Ratio Perm | c0.56 | | 0.10 | | 0.02 | 0.09 | | | c0.18 | | | |
| v/c Ratio | 0.85 | | 0.15 | 0.37 | 0.02 | 0.41 | 0.51 | | 0.83 | 0.66 | | |
| Uniform Delay, d1 | 13.6 | | 6.7 | 8.0 | 6.1 | 33.6 | 34.4 | | 37.3 | 35.7 | | |
| Progression Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | |
| Incremental Delay, d2 | 9.9 | | 0.8 | 1.2 | 0.0 | 2.3 | 1.2 | | 27.6 | 4.0 | | |
| Delay (s) | 23.5 | | 7.5 | 9.2 | 6.2 | 35.9 | 35.5 | | 64.9 | 39.8 | | |
| Level of Service | C | | A | A | A | D | D | | E | D | | |
| Approach Delay (s) | 23.5 | | | 8.7 | | | 35.6 | | | 48.4 | | |
| Approach LOS | C | | | A | | | D | | | D | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | 27.5 | | | | HCM 2000 Level of Service | | | | C | | | |
| HCM 2000 Volume to Capacity ratio | 0.85 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 100.0 | | | | Sum of lost time (s) | | | | 12.9 | | | |
| Intersection Capacity Utilization | 108.0% | | | | ICU Level of Service | | | | G | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

1: Parkdale Ave & Burnside Ave

Future Background (2023)

PM Peak Hour



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|--------|------|---------------------------|------|------|------|
| Lane Configurations | WBL | WBR | NBT | NBR | SBL | SBT |
| Traffic Volume (vph) | 45 | 355 | 728 | 69 | 64 | 474 |
| Future Volume (vph) | 45 | 355 | 728 | 69 | 64 | 474 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 4.2 | 3.7 | 4.8 | 3.7 | 3.7 | 4.8 |
| Total Lost time (s) | 5.4 | | 5.2 | | | 5.2 |
| Lane Util. Factor | 1.00 | | 1.00 | | | 1.00 |
| Frpb, ped/bikes | 0.90 | | 1.00 | | | 1.00 |
| Flpb, ped/bikes | 1.00 | | 1.00 | | | 1.00 |
| Fr _t | 0.88 | | 0.99 | | | 1.00 |
| Flt Protected | 0.99 | | 1.00 | | | 0.99 |
| Satd. Flow (prot) | 1517 | | 1973 | | | 1991 |
| Flt Permitted | 0.99 | | 1.00 | | | 0.77 |
| Satd. Flow (perm) | 1517 | | 1973 | | | 1543 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 45 | 355 | 728 | 69 | 64 | 474 |
| RTOR Reduction (vph) | 146 | 0 | 4 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 254 | 0 | 793 | 0 | 0 | 538 |
| Confl. Peds. (#/hr) | 34 | 36 | | 17 | 17 | |
| Confl. Bikes (#/hr) | | | 1 | | | |
| Heavy Vehicles (%) | 0% | 0% | 1% | 10% | 0% | 2% |
| Turn Type | pm+pt | | NA | | Perm | NA |
| Protected Phases | 3 | | 2 | | | 6 |
| Permitted Phases | 8 | | | 6 | | |
| Actuated Green, G (s) | 15.6 | | 43.8 | | | 43.8 |
| Effective Green, g (s) | 15.6 | | 43.8 | | | 43.8 |
| Actuated g/C Ratio | 0.22 | | 0.63 | | | 0.63 |
| Clearance Time (s) | 5.4 | | 5.2 | | | 5.2 |
| Vehicle Extension (s) | 3.0 | | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | 338 | | 1234 | | | 965 |
| v/s Ratio Prot | c0.17 | | c0.40 | | | |
| v/s Ratio Perm | | | | 0.35 | | |
| v/c Ratio | 0.75 | | 0.64 | | | 0.56 |
| Uniform Delay, d1 | 25.4 | | 8.2 | | | 7.5 |
| Progression Factor | 1.00 | | 1.00 | | | 1.00 |
| Incremental Delay, d2 | 9.1 | | 2.6 | | | 2.3 |
| Delay (s) | 34.5 | | 10.8 | | | 9.9 |
| Level of Service | C | | B | | | A |
| Approach Delay (s) | 34.5 | | 10.8 | | | 9.9 |
| Approach LOS | C | | B | | | A |
| Intersection Summary | | | | | | |
| HCM 2000 Control Delay | 16.0 | | HCM 2000 Level of Service | | B | |
| HCM 2000 Volume to Capacity ratio | 0.67 | | | | | |
| Actuated Cycle Length (s) | 70.0 | | Sum of lost time (s) | | 10.6 | |
| Intersection Capacity Utilization | 116.8% | | ICU Level of Service | | H | |
| Analysis Period (min) | 15 | | | | | |
| c Critical Lane Group | | | | | | |

HCM Signalized Intersection Capacity Analysis
2: Slidell St/Onigam St & Sir John A MacDonald Pkwy

Future Background (2023)
PM Peak Hour

| Movement | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
|-----------------------------------|-------|------|------|------|------|---------------------------|------|------|-------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 0 | 1007 | 4 | 2 | 2 | 1756 | 0 | 28 | 14 | 37 | 3 | 28 |
| Future Volume (vph) | 0 | 1007 | 4 | 2 | 2 | 1756 | 0 | 28 | 14 | 37 | 3 | 28 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 3.7 | 3.8 | 3.7 | 3.7 | 3.7 | 3.8 | 3.7 | 3.7 | 3.9 | 3.7 | 3.7 | 4.0 |
| Total Lost time (s) | | 5.5 | | | | 5.5 | | | 6.3 | | | 6.3 |
| Lane Util. Factor | 0.95 | | | | | 0.95 | | | 1.00 | | | 1.00 |
| Frpb, ped/bikes | 1.00 | | | | | 1.00 | | | 0.99 | | | 0.99 |
| Flpb, ped/bikes | 1.00 | | | | | 1.00 | | | 1.00 | | | 1.00 |
| Fr _t | 1.00 | | | | | 1.00 | | | 0.94 | | | 0.96 |
| Flt Protected | 1.00 | | | | | 1.00 | | | 0.98 | | | 1.00 |
| Satd. Flow (prot) | 3459 | | | | | 3496 | | | 1690 | | | 1746 |
| Flt Permitted | 1.00 | | | | | 0.95 | | | 0.87 | | | 0.98 |
| Satd. Flow (perm) | 3459 | | | | | 3333 | | | 1489 | | | 1709 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 0 | 1007 | 4 | 2 | 2 | 1756 | 0 | 28 | 14 | 37 | 3 | 28 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 33 | 0 | 0 | 10 |
| Lane Group Flow (vph) | 0 | 1011 | 0 | 0 | 0 | 1760 | 0 | 0 | 46 | 0 | 0 | 32 |
| Confl. Peds. (#/hr) | 1 | | | 7 | | | 1 | 6 | | 7 | 7 | |
| Confl. Bikes (#/hr) | | | | | | | | | 2 | | | |
| Heavy Vehicles (%) | 0% | 1% | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 4% |
| Turn Type | | NA | | Perm | Perm | NA | | Perm | NA | | Perm | NA |
| Protected Phases | | 2 | | | | 6 | | | 8 | | | 4 |
| Permitted Phases | 2 | | 6 | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | 71.8 | | | | | 71.8 | | | 11.4 | | | 11.4 |
| Effective Green, g (s) | 71.8 | | | | | 71.8 | | | 11.4 | | | 11.4 |
| Actuated g/C Ratio | 0.76 | | | | | 0.76 | | | 0.12 | | | 0.12 |
| Clearance Time (s) | 5.5 | | | | | 5.5 | | | 6.3 | | | 6.3 |
| Vehicle Extension (s) | 3.0 | | | | | 3.0 | | | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | 2614 | | | | | 2519 | | | 178 | | | 205 |
| v/s Ratio Prot | 0.29 | | | | | | | | | | | |
| v/s Ratio Perm | | | | | | c0.53 | | | c0.03 | | | 0.02 |
| v/c Ratio | 0.39 | | | | | 0.70 | | | 0.26 | | | 0.16 |
| Uniform Delay, d1 | 4.0 | | | | | 6.0 | | | 38.0 | | | 37.5 |
| Progression Factor | 1.00 | | | | | 1.00 | | | 1.00 | | | 1.00 |
| Incremental Delay, d2 | 0.4 | | | | | 1.6 | | | 0.8 | | | 0.4 |
| Delay (s) | 4.4 | | | | | 7.6 | | | 38.8 | | | 37.9 |
| Level of Service | A | | | | | A | | | D | | | D |
| Approach Delay (s) | 4.4 | | | | | 7.6 | | | 38.8 | | | 37.9 |
| Approach LOS | A | | | | | A | | | D | | | D |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | 7.8 | | | | | HCM 2000 Level of Service | | | A | | | |
| HCM 2000 Volume to Capacity ratio | 0.64 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 95.0 | | | | | Sum of lost time (s) | | | 11.8 | | | |
| Intersection Capacity Utilization | 78.0% | | | | | ICU Level of Service | | | D | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| Movement | SBR |
|------------------------|------|
| Lane Configurations | |
| Traffic Volume (vph) | 11 |
| Future Volume (vph) | 11 |
| Ideal Flow (vphpl) | 1800 |
| Lane Width | 3.7 |
| Total Lost time (s) | |
| Lane Util. Factor | |
| Frpb, ped/bikes | |
| Flpb, ped/bikes | |
| Fr | |
| Flt Protected | |
| Satd. Flow (prot) | |
| Flt Permitted | |
| Satd. Flow (perm) | |
| Peak-hour factor, PHF | 1.00 |
| Adj. Flow (vph) | 11 |
| RTOR Reduction (vph) | 0 |
| Lane Group Flow (vph) | 0 |
| Confl. Peds. (#/hr) | 6 |
| Confl. Bikes (#/hr) | 6 |
| Heavy Vehicles (%) | 0% |
| Turn Type | |
| Protected Phases | |
| Permitted Phases | |
| Actuated Green, G (s) | |
| Effective Green, g (s) | |
| Actuated g/C Ratio | |
| Clearance Time (s) | |
| Vehicle Extension (s) | |
| Lane Grp Cap (vph) | |
| v/s Ratio Prot | |
| v/s Ratio Perm | |
| v/c Ratio | |
| Uniform Delay, d1 | |
| Progression Factor | |
| Incremental Delay, d2 | |
| Delay (s) | |
| Level of Service | |
| Approach Delay (s) | |
| Approach LOS | |
| Intersection Summary | |

HCM Signalized Intersection Capacity Analysis

3: Bayview Stn Rd & Scott St/Albert St

Future Background (2023)

PM Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|-------|------|---------------------------|-------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 19 | 459 | 105 | 86 | 604 | 95 | 101 | 269 | 75 | 50 | 87 | 16 |
| Future Volume (vph) | 19 | 459 | 105 | 86 | 604 | 95 | 101 | 269 | 75 | 50 | 87 | 16 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 3.7 | 3.6 | 3.7 | 3.2 | 3.5 | 3.8 | 3.0 | 4.3 | 3.7 | 3.3 | 4.5 | 3.7 |
| Total Lost time (s) | 6.5 | | 6.5 | 6.5 | 6.5 | 6.4 | 6.4 | | 6.4 | 6.4 | | |
| Lane Util. Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | |
| Frpb, ped/bikes | 0.97 | | 1.00 | 1.00 | 0.88 | 1.00 | 0.99 | | 1.00 | 0.98 | | |
| Flpb, ped/bikes | 1.00 | | 0.95 | 1.00 | 1.00 | 0.92 | 1.00 | | 0.99 | 1.00 | | |
| Fr _t | 0.98 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 | | 1.00 | 0.98 | | |
| Flt Protected | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | |
| Satd. Flow (prot) | 1479 | | 1550 | 1402 | 1360 | 1445 | 1839 | | 1635 | 1845 | | |
| Flt Permitted | 0.97 | | 0.43 | 1.00 | 1.00 | 0.69 | 1.00 | | 0.26 | 1.00 | | |
| Satd. Flow (perm) | 1443 | | 696 | 1402 | 1360 | 1050 | 1839 | | 455 | 1845 | | |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 19 | 459 | 105 | 86 | 604 | 95 | 101 | 269 | 75 | 50 | 87 | 16 |
| RTOR Reduction (vph) | 0 | 7 | 0 | 0 | 0 | 34 | 0 | 11 | 0 | 0 | 7 | 0 |
| Lane Group Flow (vph) | 0 | 576 | 0 | 86 | 604 | 61 | 101 | 333 | 0 | 50 | 96 | 0 |
| Confl. Peds. (#/hr) | 53 | | 70 | 70 | | 53 | 46 | | 12 | 12 | | 46 |
| Confl. Bikes (#/hr) | | | 3 | | | 4 | | | 6 | | | 18 |
| Heavy Vehicles (%) | 0% | 19% | 1% | 0% | 27% | 1% | 2% | 0% | 4% | 0% | 2% | 6% |
| Turn Type | Perm | NA | | Perm | NA | Perm | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | 6 | | 6 | 8 | | | 4 | | | |
| Actuated Green, G (s) | 64.4 | | 64.4 | 64.4 | 64.4 | 22.7 | 22.7 | | 22.7 | 22.7 | | |
| Effective Green, g (s) | 64.4 | | 64.4 | 64.4 | 64.4 | 22.7 | 22.7 | | 22.7 | 22.7 | | |
| Actuated g/C Ratio | 0.64 | | 0.64 | 0.64 | 0.64 | 0.23 | 0.23 | | 0.23 | 0.23 | | |
| Clearance Time (s) | 6.5 | | 6.5 | 6.5 | 6.5 | 6.4 | 6.4 | | 6.4 | 6.4 | | |
| Vehicle Extension (s) | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | |
| Lane Grp Cap (vph) | 929 | | 448 | 902 | 875 | 238 | 417 | | 103 | 418 | | |
| v/s Ratio Prot | | | c0.43 | | | c0.18 | | | | 0.05 | | |
| v/s Ratio Perm | 0.40 | | 0.12 | | 0.04 | 0.10 | | | 0.11 | | | |
| v/c Ratio | 0.62 | | 0.19 | 0.67 | 0.07 | 0.42 | 0.80 | | 0.49 | 0.23 | | |
| Uniform Delay, d1 | 10.5 | | 7.2 | 11.1 | 6.6 | 33.1 | 36.5 | | 33.6 | 31.5 | | |
| Progression Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | |
| Incremental Delay, d2 | 3.1 | | 1.0 | 3.9 | 0.2 | 1.2 | 10.3 | | 3.6 | 0.3 | | |
| Delay (s) | 13.7 | | 8.2 | 15.1 | 6.8 | 34.3 | 46.8 | | 37.1 | 31.8 | | |
| Level of Service | B | | A | B | A | C | D | | D | C | | |
| Approach Delay (s) | 13.7 | | | 13.3 | | | 43.9 | | | 33.5 | | |
| Approach LOS | B | | | B | | | D | | | C | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | 21.9 | | | | HCM 2000 Level of Service | | | | C | | | |
| HCM 2000 Volume to Capacity ratio | 0.70 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 100.0 | | | | Sum of lost time (s) | | | | 12.9 | | | |
| Intersection Capacity Utilization | 95.7% | | | | ICU Level of Service | | | | F | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

1: Parkdale Ave & Burnside Ave

Future Background (2028)

AM Peak Hour



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|--------|------|---------------------------|-------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (vph) | 95 | 104 | 394 | 67 | 251 | 604 |
| Future Volume (vph) | 95 | 104 | 394 | 67 | 251 | 604 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 4.2 | 3.7 | 4.8 | 3.7 | 3.7 | 4.8 |
| Total Lost time (s) | 5.4 | | 5.2 | | | 5.2 |
| Lane Util. Factor | 1.00 | | 1.00 | | | 1.00 |
| Frpb, ped/bikes | 0.95 | | 0.99 | | | 1.00 |
| Flpb, ped/bikes | 1.00 | | 1.00 | | | 1.00 |
| Fr _t | 0.93 | | 0.98 | | | 1.00 |
| Flt Protected | 0.98 | | 1.00 | | | 0.99 |
| Satd. Flow (prot) | 1582 | | 1952 | | | 1965 |
| Flt Permitted | 0.98 | | 1.00 | | | 0.68 |
| Satd. Flow (perm) | 1582 | | 1952 | | | 1361 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 95 | 104 | 394 | 67 | 251 | 604 |
| RTOR Reduction (vph) | 69 | 0 | 9 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 130 | 0 | 452 | 0 | 0 | 855 |
| Confl. Peds. (#/hr) | 67 | 35 | | 14 | 14 | |
| Confl. Bikes (#/hr) | | | 1 | | | |
| Heavy Vehicles (%) | 0% | 9% | 1% | 7% | 2% | 2% |
| Turn Type | pm+pt | | NA | | Perm | NA |
| Protected Phases | 3 | | 2 | | | 6 |
| Permitted Phases | 8 | | | 6 | | |
| Actuated Green, G (s) | 12.5 | | 36.9 | | | 36.9 |
| Effective Green, g (s) | 12.5 | | 36.9 | | | 36.9 |
| Actuated g/C Ratio | 0.21 | | 0.61 | | | 0.61 |
| Clearance Time (s) | 5.4 | | 5.2 | | | 5.2 |
| Vehicle Extension (s) | 3.0 | | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | 329 | | 1200 | | | 837 |
| v/s Ratio Prot | c0.08 | | 0.23 | | | |
| v/s Ratio Perm | | | | c0.63 | | |
| v/c Ratio | 0.40 | | 0.38 | | | 1.02 |
| Uniform Delay, d1 | 20.5 | | 5.8 | | | 11.6 |
| Progression Factor | 1.00 | | 1.00 | | | 1.00 |
| Incremental Delay, d2 | 0.8 | | 0.9 | | | 36.7 |
| Delay (s) | 21.3 | | 6.7 | | | 48.2 |
| Level of Service | C | | A | | | D |
| Approach Delay (s) | 21.3 | | 6.7 | | | 48.2 |
| Approach LOS | C | | A | | | D |
| Intersection Summary | | | | | | |
| HCM 2000 Control Delay | 32.0 | | HCM 2000 Level of Service | | C | |
| HCM 2000 Volume to Capacity ratio | 0.86 | | | | | |
| Actuated Cycle Length (s) | 60.0 | | Sum of lost time (s) | | 10.6 | |
| Intersection Capacity Utilization | 101.6% | | ICU Level of Service | | G | |
| Analysis Period (min) | 15 | | | | | |
| c Critical Lane Group | | | | | | |

HCM Signalized Intersection Capacity Analysis
2: Slidell St/Onigam St & Sir John A MacDonald Pkwy

Future Background (2028)
AM Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBL | SBT |
|-----------------------------------|-------|------|------|------|---------------------------|------|------|------|-------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 0 | 1824 | 27 | 1 | 1259 | 1 | 1 | 1 | 26 | 1 | 1 | 6 |
| Future Volume (vph) | 0 | 1824 | 27 | 1 | 1259 | 1 | 1 | 1 | 26 | 1 | 1 | 6 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 3.7 | 3.8 | 3.7 | 3.7 | 3.8 | 3.7 | 3.7 | 3.7 | 3.9 | 3.7 | 3.7 | 4.0 |
| Total Lost time (s) | | 5.5 | | | 5.5 | | | | 6.3 | | | 6.3 |
| Lane Util. Factor | | 0.95 | | | 0.95 | | | | 1.00 | | | 1.00 |
| Frpb, ped/bikes | | 1.00 | | | 1.00 | | | | 1.00 | | | 0.99 |
| Flpb, ped/bikes | | 1.00 | | | 1.00 | | | | 1.00 | | | 1.00 |
| Fr _t | | 1.00 | | | 1.00 | | | | 1.00 | | | 0.95 |
| Flt Protected | | 1.00 | | | 1.00 | | | | 1.00 | | | 1.00 |
| Satd. Flow (prot) | | 3487 | | | 3461 | | | | 1841 | | | 1765 |
| Flt Permitted | | 1.00 | | | 0.95 | | | | 0.98 | | | 0.97 |
| Satd. Flow (perm) | | 3487 | | | 3302 | | | | 1809 | | | 1724 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 0 | 1824 | 27 | 1 | 1259 | 1 | 1 | 1 | 26 | 1 | 1 | 6 |
| RTOR Reduction (vph) | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 4 |
| Lane Group Flow (vph) | 0 | 1850 | 0 | 0 | 1261 | 0 | 0 | 0 | 28 | 0 | 0 | 7 |
| Confl. Peds. (#/hr) | 2 | | 1 | 1 | | 2 | 1 | 4 | | 5 | 5 | |
| Confl. Bikes (#/hr) | | | 1 | | | | | | | 13 | | |
| Heavy Vehicles (%) | 0% | 0% | 0% | 0% | 1% | 0% | 0% | 0% | 0% | 0% | 0% | 0% |
| Turn Type | | NA | | Perm | NA | | Perm | Perm | NA | | Perm | NA |
| Protected Phases | | 2 | | | 6 | | | | 8 | | | 4 |
| Permitted Phases | 2 | | | 6 | | | 8 | 8 | | | 4 | |
| Actuated Green, G (s) | 73.8 | | | 73.8 | | | | | 9.4 | | | 9.4 |
| Effective Green, g (s) | 73.8 | | | 73.8 | | | | | 9.4 | | | 9.4 |
| Actuated g/C Ratio | 0.78 | | | 0.78 | | | | | 0.10 | | | 0.10 |
| Clearance Time (s) | 5.5 | | | 5.5 | | | | | 6.3 | | | 6.3 |
| Vehicle Extension (s) | 3.0 | | | 3.0 | | | | | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | 2708 | | | 2565 | | | | | 178 | | | 170 |
| v/s Ratio Prot | c0.53 | | | | | | | | | | | |
| v/s Ratio Perm | | | | 0.38 | | | | | c0.02 | | | 0.00 |
| v/c Ratio | 0.68 | | | 0.49 | | | | | 0.16 | | | 0.04 |
| Uniform Delay, d1 | 5.0 | | | 3.8 | | | | | 39.2 | | | 38.7 |
| Progression Factor | 1.00 | | | 1.00 | | | | | 1.00 | | | 1.00 |
| Incremental Delay, d2 | 1.4 | | | 0.7 | | | | | 0.4 | | | 0.1 |
| Delay (s) | 6.5 | | | 4.5 | | | | | 39.6 | | | 38.8 |
| Level of Service | A | | | A | | | | | D | | | D |
| Approach Delay (s) | 6.5 | | | 4.5 | | | | | 39.6 | | | 38.8 |
| Approach LOS | A | | | A | | | | | D | | | D |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | 6.1 | | | | HCM 2000 Level of Service | | | | A | | | |
| HCM 2000 Volume to Capacity ratio | 0.62 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 95.0 | | | | Sum of lost time (s) | | | | 11.8 | | | |
| Intersection Capacity Utilization | 74.5% | | | | ICU Level of Service | | | | D | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| Movement | SBR |
|------------------------|------|
| Lane Configurations | |
| Traffic Volume (vph) | 4 |
| Future Volume (vph) | 4 |
| Ideal Flow (vphpl) | 1800 |
| Lane Width | 3.7 |
| Total Lost time (s) | |
| Lane Util. Factor | |
| Frpb, ped/bikes | |
| Flpb, ped/bikes | |
| Fr | |
| Flt Protected | |
| Satd. Flow (prot) | |
| Flt Permitted | |
| Satd. Flow (perm) | |
| Peak-hour factor, PHF | 1.00 |
| Adj. Flow (vph) | 4 |
| RTOR Reduction (vph) | 0 |
| Lane Group Flow (vph) | 0 |
| Confl. Peds. (#/hr) | 4 |
| Confl. Bikes (#/hr) | 2 |
| Heavy Vehicles (%) | 0% |
| Turn Type | |
| Protected Phases | |
| Permitted Phases | |
| Actuated Green, G (s) | |
| Effective Green, g (s) | |
| Actuated g/C Ratio | |
| Clearance Time (s) | |
| Vehicle Extension (s) | |
| Lane Grp Cap (vph) | |
| v/s Ratio Prot | |
| v/s Ratio Perm | |
| v/c Ratio | |
| Uniform Delay, d1 | |
| Progression Factor | |
| Incremental Delay, d2 | |
| Delay (s) | |
| Level of Service | |
| Approach Delay (s) | |
| Approach LOS | |
| Intersection Summary | |

HCM Signalized Intersection Capacity Analysis

3: Bayview Stn Rd & Scott St/Albert St

Future Background (2028)

AM Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|--------|------|------|------|---------------------------|------|------|------|-------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 26 | 861 | 96 | 67 | 389 | 44 | 54 | 109 | 160 | 181 | 270 | 30 |
| Future Volume (vph) | 26 | 861 | 96 | 67 | 389 | 44 | 54 | 109 | 160 | 181 | 270 | 30 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 3.7 | 3.6 | 3.7 | 3.2 | 3.5 | 3.8 | 3.0 | 4.3 | 3.7 | 3.3 | 4.5 | 3.7 |
| Total Lost time (s) | 6.5 | | | 6.5 | 6.5 | 6.4 | 6.4 | | | 6.4 | 6.4 | |
| Lane Util. Factor | 1.00 | | | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | 1.00 | |
| Frpb, ped/bikes | 0.99 | | | 1.00 | 1.00 | 0.96 | 1.00 | 0.92 | | 1.00 | 0.99 | |
| Flpb, ped/bikes | 1.00 | | | 0.98 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.96 | 1.00 | |
| Fr _t | 0.99 | | | 1.00 | 1.00 | 0.85 | 1.00 | 0.91 | | 1.00 | 0.98 | |
| Flt Protected | 1.00 | | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1422 | | | 1571 | 1338 | 1397 | 1340 | 1570 | | 1529 | 1861 | |
| Flt Permitted | 0.98 | | | 0.26 | 1.00 | 1.00 | 0.39 | 1.00 | | 0.44 | 1.00 | |
| Satd. Flow (perm) | 1400 | | | 432 | 1338 | 1397 | 551 | 1570 | | 713 | 1861 | |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 26 | 861 | 96 | 67 | 389 | 44 | 54 | 109 | 160 | 181 | 270 | 30 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 | 0 | 17 | 0 | 53 | 0 | 0 | 4 | 0 |
| Lane Group Flow (vph) | 0 | 979 | 0 | 67 | 389 | 27 | 54 | 216 | 0 | 181 | 296 | 0 |
| Confl. Peds. (#/hr) | 13 | | 57 | 57 | | 13 | 48 | | 33 | 33 | | 48 |
| Confl. Bikes (#/hr) | | | 2 | | | | | | 41 | | | 12 |
| Heavy Vehicles (%) | 0% | 26% | 4% | 2% | 33% | 7% | 13% | 4% | 3% | 4% | 2% | 17% |
| Turn Type | Perm | NA | | Perm | NA | Perm | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | 6 | 8 | | | 4 | | |
| Actuated Green, G (s) | 61.1 | | 61.1 | 61.1 | 61.1 | 26.0 | 26.0 | | 26.0 | 26.0 | | |
| Effective Green, g (s) | 61.1 | | 61.1 | 61.1 | 61.1 | 26.0 | 26.0 | | 26.0 | 26.0 | | |
| Actuated g/C Ratio | 0.61 | | 0.61 | 0.61 | 0.61 | 0.26 | 0.26 | | 0.26 | 0.26 | | |
| Clearance Time (s) | 6.5 | | 6.5 | 6.5 | 6.5 | 6.4 | 6.4 | | 6.4 | 6.4 | | |
| Vehicle Extension (s) | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | |
| Lane Grp Cap (vph) | 855 | | 263 | 817 | 853 | 143 | 408 | | 185 | 483 | | |
| v/s Ratio Prot | | | | 0.29 | | | | 0.14 | | | 0.16 | |
| v/s Ratio Perm | c0.70 | | 0.15 | | 0.02 | 0.10 | | | c0.25 | | | |
| v/c Ratio | 1.15 | | 0.25 | 0.48 | 0.03 | 0.38 | 0.53 | | 0.98 | 0.61 | | |
| Uniform Delay, d1 | 19.4 | | 9.0 | 10.7 | 7.7 | 30.4 | 31.8 | | 36.7 | 32.6 | | |
| Progression Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | |
| Incremental Delay, d2 | 79.0 | | 2.3 | 2.0 | 0.1 | 1.7 | 1.3 | | 59.2 | 2.3 | | |
| Delay (s) | 98.5 | | 11.3 | 12.7 | 7.8 | 32.0 | 33.1 | | 95.9 | 34.9 | | |
| Level of Service | F | | B | B | A | C | C | | F | C | | |
| Approach Delay (s) | 98.5 | | | 12.0 | | | 32.9 | | | 57.8 | | |
| Approach LOS | F | | | B | | | C | | | E | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | 61.8 | | | | HCM 2000 Level of Service | | | | E | | | |
| HCM 2000 Volume to Capacity ratio | 1.09 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 100.0 | | | | Sum of lost time (s) | | | 12.9 | | | | |
| Intersection Capacity Utilization | 124.0% | | | | ICU Level of Service | | | H | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

1: Parkdale Ave & Burnside Ave

Future Background (2028)

PM Peak Hour



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|------------------------|-------|------|------|-------|------|-------|
| Lane Configurations | WBL | WBR | NBT | NBR | SBL | SBT |
| Traffic Volume (vph) | 54 | 459 | 860 | 86 | 89 | 559 |
| Future Volume (vph) | 54 | 459 | 860 | 86 | 89 | 559 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 4.2 | 3.7 | 4.8 | 3.7 | 3.7 | 4.8 |
| Total Lost time (s) | 5.4 | | 5.2 | | | 5.2 |
| Lane Util. Factor | 1.00 | | 1.00 | | | 1.00 |
| Frpb, ped/bikes | 0.89 | | 1.00 | | | 1.00 |
| Flpb, ped/bikes | 1.00 | | 1.00 | | | 1.00 |
| Fr _t | 0.88 | | 0.99 | | | 1.00 |
| Flt Protected | 0.99 | | 1.00 | | | 0.99 |
| Satd. Flow (prot) | 1500 | | 1970 | | | 1992 |
| Flt Permitted | 0.99 | | 1.00 | | | 0.38 |
| Satd. Flow (perm) | 1500 | | 1970 | | | 765 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 54 | 459 | 860 | 86 | 89 | 559 |
| RTOR Reduction (vph) | 98 | 0 | 5 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 415 | 0 | 941 | 0 | 0 | 648 |
| Confl. Peds. (#/hr) | 37 | 40 | | 19 | 19 | |
| Confl. Bikes (#/hr) | | | 1 | | | |
| Heavy Vehicles (%) | 0% | 0% | 1% | 10% | 0% | 2% |
| Turn Type | pm+pt | | NA | | Perm | NA |
| Protected Phases | 3 | | 2 | | | 6 |
| Permitted Phases | 8 | | | 6 | | |
| Actuated Green, G (s) | 19.6 | | 39.8 | | | 39.8 |
| Effective Green, g (s) | 19.6 | | 39.8 | | | 39.8 |
| Actuated g/C Ratio | 0.28 | | 0.57 | | | 0.57 |
| Clearance Time (s) | 5.4 | | 5.2 | | | 5.2 |
| Vehicle Extension (s) | 3.0 | | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | 420 | | 1120 | | | 434 |
| v/s Ratio Prot | c0.28 | | 0.48 | | | |
| v/s Ratio Perm | | | | c0.85 | | |
| v/c Ratio | 0.99 | | 0.84 | | | 1.49 |
| Uniform Delay, d1 | 25.1 | | 12.5 | | | 15.1 |
| Progression Factor | 1.00 | | 1.00 | | | 1.00 |
| Incremental Delay, d2 | 40.4 | | 7.6 | | | 233.8 |
| Delay (s) | 65.5 | | 20.1 | | | 248.9 |
| Level of Service | E | | C | | | F |
| Approach Delay (s) | 65.5 | | 20.1 | | | 248.9 |
| Approach LOS | E | | C | | | F |

Intersection Summary

| | | | |
|-----------------------------------|--------|---------------------------|------|
| HCM 2000 Control Delay | 101.5 | HCM 2000 Level of Service | F |
| HCM 2000 Volume to Capacity ratio | 1.32 | | |
| Actuated Cycle Length (s) | 70.0 | Sum of lost time (s) | 10.6 |
| Intersection Capacity Utilization | 139.0% | ICU Level of Service | H |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
2: Slidell St/Onigam St & Sir John A MacDonald Pkwy

Future Background (2028)
PM Peak Hour

| Movement | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
|-----------------------------------|-------|------|------|------|------|---------------------------|------|------|-------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 0 | 1242 | 5 | 2 | 2 | 2115 | 0 | 33 | 18 | 43 | 4 | 33 |
| Future Volume (vph) | 0 | 1242 | 5 | 2 | 2 | 2115 | 0 | 33 | 18 | 43 | 4 | 33 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 3.7 | 3.8 | 3.7 | 3.7 | 3.7 | 3.8 | 3.7 | 3.7 | 3.9 | 3.7 | 3.7 | 4.0 |
| Total Lost time (s) | | 5.5 | | | | 5.5 | | | 6.3 | | | 6.3 |
| Lane Util. Factor | 0.95 | | | | | 0.95 | | | 1.00 | | | 1.00 |
| Frpb, ped/bikes | 1.00 | | | | | 1.00 | | | 0.99 | | | 0.99 |
| Flpb, ped/bikes | 1.00 | | | | | 1.00 | | | 1.00 | | | 1.00 |
| Fr _t | 1.00 | | | | | 1.00 | | | 0.94 | | | 0.96 |
| Flt Protected | 1.00 | | | | | 1.00 | | | 0.98 | | | 1.00 |
| Satd. Flow (prot) | 3459 | | | | | 3496 | | | 1692 | | | 1741 |
| Flt Permitted | 1.00 | | | | | 0.95 | | | 0.86 | | | 0.97 |
| Satd. Flow (perm) | 3459 | | | | | 3332 | | | 1486 | | | 1698 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 0 | 1242 | 5 | 2 | 2 | 2115 | 0 | 33 | 18 | 43 | 4 | 33 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 38 | 0 | 0 | 6 |
| Lane Group Flow (vph) | 0 | 1247 | 0 | 0 | 0 | 2119 | 0 | 0 | 56 | 0 | 0 | 45 |
| Confl. Peds. (#/hr) | 1 | | | 8 | | | 1 | 7 | | 8 | 8 | |
| Confl. Bikes (#/hr) | | | | | | | | | 2 | | | |
| Heavy Vehicles (%) | 0% | 1% | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 4% |
| Turn Type | | NA | | Perm | Perm | NA | | Perm | NA | | Perm | NA |
| Protected Phases | | 2 | | | | 6 | | | 8 | | | 4 |
| Permitted Phases | 2 | | 6 | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | 71.7 | | | | | 71.7 | | | 11.5 | | | 11.5 |
| Effective Green, g (s) | 71.7 | | | | | 71.7 | | | 11.5 | | | 11.5 |
| Actuated g/C Ratio | 0.75 | | | | | 0.75 | | | 0.12 | | | 0.12 |
| Clearance Time (s) | 5.5 | | | | | 5.5 | | | 6.3 | | | 6.3 |
| Vehicle Extension (s) | 3.0 | | | | | 3.0 | | | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | 2610 | | | | | 2514 | | | 179 | | | 205 |
| v/s Ratio Prot | 0.36 | | | | | | | | | | | |
| v/s Ratio Perm | | | | | | c0.64 | | | c0.04 | | | 0.03 |
| v/c Ratio | 0.48 | | | | | 0.84 | | | 0.31 | | | 0.22 |
| Uniform Delay, d1 | 4.5 | | | | | 7.9 | | | 38.1 | | | 37.7 |
| Progression Factor | 1.00 | | | | | 1.00 | | | 1.00 | | | 1.00 |
| Incremental Delay, d2 | 0.6 | | | | | 3.7 | | | 1.0 | | | 0.5 |
| Delay (s) | 5.1 | | | | | 11.5 | | | 39.2 | | | 38.2 |
| Level of Service | A | | | | | B | | | D | | | D |
| Approach Delay (s) | 5.1 | | | | | 11.5 | | | 39.2 | | | 38.2 |
| Approach LOS | A | | | | | B | | | D | | | D |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | 10.4 | | | | | HCM 2000 Level of Service | | | B | | | |
| HCM 2000 Volume to Capacity ratio | 0.77 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 95.0 | | | | | Sum of lost time (s) | | | 11.8 | | | |
| Intersection Capacity Utilization | 89.5% | | | | | ICU Level of Service | | | E | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |

c Critical Lane Group

| Movement | SBR |
|------------------------|------|
| Lane Configurations | |
| Traffic Volume (vph) | 14 |
| Future Volume (vph) | 14 |
| Ideal Flow (vphpl) | 1800 |
| Lane Width | 3.7 |
| Total Lost time (s) | |
| Lane Util. Factor | |
| Frpb, ped/bikes | |
| Flpb, ped/bikes | |
| Fr | |
| Flt Protected | |
| Satd. Flow (prot) | |
| Flt Permitted | |
| Satd. Flow (perm) | |
| Peak-hour factor, PHF | 1.00 |
| Adj. Flow (vph) | 14 |
| RTOR Reduction (vph) | 0 |
| Lane Group Flow (vph) | 0 |
| Confl. Peds. (#/hr) | 7 |
| Confl. Bikes (#/hr) | 7 |
| Heavy Vehicles (%) | 0% |
| Turn Type | |
| Protected Phases | |
| Permitted Phases | |
| Actuated Green, G (s) | |
| Effective Green, g (s) | |
| Actuated g/C Ratio | |
| Clearance Time (s) | |
| Vehicle Extension (s) | |
| Lane Grp Cap (vph) | |
| v/s Ratio Prot | |
| v/s Ratio Perm | |
| v/c Ratio | |
| Uniform Delay, d1 | |
| Progression Factor | |
| Incremental Delay, d2 | |
| Delay (s) | |
| Level of Service | |
| Approach Delay (s) | |
| Approach LOS | |
| Intersection Summary | |

HCM Signalized Intersection Capacity Analysis

3: Bayview Stn Rd & Scott St/Albert St

Future Background (2028)

PM Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|--------|------|-------|------|---------------------------|------|------|------|-------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 25 | 632 | 128 | 137 | 880 | 148 | 123 | 328 | 107 | 76 | 105 | 20 |
| Future Volume (vph) | 25 | 632 | 128 | 137 | 880 | 148 | 123 | 328 | 107 | 76 | 105 | 20 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 3.7 | 3.6 | 3.7 | 3.2 | 3.5 | 3.8 | 3.0 | 4.3 | 3.7 | 3.3 | 4.5 | 3.7 |
| Total Lost time (s) | 6.5 | | 6.5 | 6.5 | 6.5 | 6.4 | 6.4 | | 6.4 | 6.4 | | |
| Lane Util. Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | |
| Frpb, ped/bikes | 0.97 | | 1.00 | 1.00 | 0.87 | 1.00 | 0.99 | | 1.00 | 0.98 | | |
| Flpb, ped/bikes | 1.00 | | 0.96 | 1.00 | 1.00 | 0.92 | 1.00 | | 0.99 | 1.00 | | |
| Fr _t | 0.98 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.96 | | 1.00 | 0.98 | | |
| Flt Protected | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | |
| Satd. Flow (prot) | 1481 | | 1572 | 1402 | 1341 | 1438 | 1826 | | 1638 | 1841 | | |
| Flt Permitted | 0.86 | | 0.33 | 1.00 | 1.00 | 0.68 | 1.00 | | 0.17 | 1.00 | | |
| Satd. Flow (perm) | 1278 | | 544 | 1402 | 1341 | 1025 | 1826 | | 298 | 1841 | | |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 25 | 632 | 128 | 137 | 880 | 148 | 123 | 328 | 107 | 76 | 105 | 20 |
| RTOR Reduction (vph) | 0 | 7 | 0 | 0 | 0 | 41 | 0 | 12 | 0 | 0 | 7 | 0 |
| Lane Group Flow (vph) | 0 | 778 | 0 | 137 | 880 | 107 | 123 | 423 | 0 | 76 | 118 | 0 |
| Confl. Peds. (#/hr) | 59 | | 77 | 77 | | 59 | 50 | | 13 | 13 | | 50 |
| Confl. Bikes (#/hr) | | | 4 | | | 5 | | | 7 | | | 20 |
| Heavy Vehicles (%) | 0% | 19% | 1% | 0% | 27% | 1% | 2% | 0% | 4% | 0% | 2% | 6% |
| Turn Type | Perm | NA | | Perm | NA | Perm | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | 6 | | 6 | 8 | | | 4 | | | |
| Actuated Green, G (s) | 61.1 | | 61.1 | 61.1 | 61.1 | 26.0 | 26.0 | | 26.0 | 26.0 | | |
| Effective Green, g (s) | 61.1 | | 61.1 | 61.1 | 61.1 | 26.0 | 26.0 | | 26.0 | 26.0 | | |
| Actuated g/C Ratio | 0.61 | | 0.61 | 0.61 | 0.61 | 0.26 | 0.26 | | 0.26 | 0.26 | | |
| Clearance Time (s) | 6.5 | | 6.5 | 6.5 | 6.5 | 6.4 | 6.4 | | 6.4 | 6.4 | | |
| Vehicle Extension (s) | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | |
| Lane Grp Cap (vph) | 780 | | 332 | 856 | 819 | 266 | 474 | | 77 | 478 | | |
| v/s Ratio Prot | | | c0.63 | | | | 0.23 | | | 0.06 | | |
| v/s Ratio Perm | 0.61 | | 0.25 | | 0.08 | 0.12 | | | c0.25 | | | |
| v/c Ratio | 1.00 | | 0.41 | 1.03 | 0.13 | 0.46 | 0.89 | | 0.99 | 0.25 | | |
| Uniform Delay, d1 | 19.4 | | 10.1 | 19.4 | 8.2 | 31.1 | 35.7 | | 36.8 | 29.3 | | |
| Progression Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | |
| Incremental Delay, d2 | 31.6 | | 3.8 | 38.1 | 0.3 | 1.3 | 18.8 | | 97.4 | 0.3 | | |
| Delay (s) | 51.0 | | 13.9 | 57.6 | 8.6 | 32.4 | 54.4 | | 134.2 | 29.5 | | |
| Level of Service | D | B | E | A | C | D | | F | | C | | |
| Approach Delay (s) | 51.0 | | | 46.2 | | | 49.6 | | | 69.1 | | |
| Approach LOS | D | | | D | | | D | | | E | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | 50.0 | | | | HCM 2000 Level of Service | | | D | | | | |
| HCM 2000 Volume to Capacity ratio | 1.01 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 100.0 | | | | Sum of lost time (s) | | | 12.9 | | | | |
| Intersection Capacity Utilization | 131.2% | | | | ICU Level of Service | | | H | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

Appendix I – Future Total (2023, 2028) Synchro and SIDRA Outputs

MOVEMENT SUMMARY

Site: 1 [Burnside Roundabout - Total (2023) - AM]

Burnside Roundabout - Total (2023) - AM

Site Category: (None)

Roundabout

| Movement Performance - Vehicles | | | | | | | | | | | | |
|--|------|--------------------|------------|---------------|-------------------|------------------|--------------------------------|------------------|--------------|---------------------|------------------|--------------------|
| Mov ID | Turn | Demand Total veh/h | Flows HV % | Deg. Satn v/c | Average Delay sec | Level of Service | 95% Back of Queue Vehicles veh | Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Bayview Station Road | | | | | | | | | | | | |
| 21u | U | 2 | 0.0 | 0.136 | 9.2 | LOS A | 0.4 | 3.0 | 0.08 | 0.57 | 0.08 | 47.0 |
| 21 | L2 | 155 | 9.0 | 0.136 | 7.4 | LOS A | 0.4 | 3.0 | 0.08 | 0.57 | 0.08 | 42.4 |
| 23a | R1 | 25 | 0.0 | 0.136 | 2.5 | LOS A | 0.4 | 3.0 | 0.08 | 0.57 | 0.08 | 43.0 |
| Approach | | 183 | 7.6 | 0.136 | 6.8 | LOS A | 0.4 | 3.0 | 0.08 | 0.57 | 0.08 | 42.5 |
| North: Slidell Street | | | | | | | | | | | | |
| 7u | U | 1 | 0.0 | 0.079 | 9.4 | LOS A | 0.2 | 1.7 | 0.19 | 0.57 | 0.19 | 21.2 |
| 7a | L1 | 88 | 7.0 | 0.079 | 6.8 | LOS A | 0.2 | 1.7 | 0.19 | 0.57 | 0.19 | 43.0 |
| 9a | R1 | 8 | 0.0 | 0.079 | 2.8 | LOS A | 0.2 | 1.7 | 0.19 | 0.57 | 0.19 | 37.9 |
| Approach | | 97 | 6.4 | 0.079 | 6.5 | LOS A | 0.2 | 1.7 | 0.19 | 0.57 | 0.19 | 42.3 |
| SouthWest: Burnside Avenue | | | | | | | | | | | | |
| 30u | U | 1 | 0.0 | 0.303 | 7.2 | LOS A | 1.1 | 7.5 | 0.17 | 0.36 | 0.17 | 41.7 |
| 30a | L1 | 34 | 0.0 | 0.303 | 5.0 | LOS A | 1.1 | 7.5 | 0.17 | 0.36 | 0.17 | 25.7 |
| 32 | R2 | 376 | 0.0 | 0.303 | 2.0 | LOS A | 1.1 | 7.5 | 0.17 | 0.36 | 0.17 | 42.3 |
| Approach | | 411 | 0.0 | 0.303 | 2.3 | LOS A | 1.1 | 7.5 | 0.17 | 0.36 | 0.17 | 40.8 |
| All Vehicles | | 691 | 2.9 | 0.303 | 4.1 | LOS A | 1.1 | 7.5 | 0.15 | 0.44 | 0.15 | 41.4 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akcelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

MOVEMENT SUMMARY

Site: 1 [Burnside Roundabout - Total (2023) - PM]

Burnside Roundabout - Total (2023) - PM

Site Category: (None)

Roundabout

| Movement Performance - Vehicles | | | | | | | | | | | | |
|--|------|--------------------|------------|---------------|-------------------|------------------|--------------------------------|------------------|--------------|---------------------|------------------|--------------------|
| Mov ID | Turn | Demand Total veh/h | Flows HV % | Deg. Satn v/c | Average Delay sec | Level of Service | 95% Back of Queue Vehicles veh | Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Bayview Station Road | | | | | | | | | | | | |
| 21u | U | 11 | 11.0 | 0.365 | 9.3 | LOS A | 1.4 | 9.8 | 0.11 | 0.57 | 0.11 | 46.8 |
| 21 | L2 | 432 | 1.0 | 0.365 | 7.4 | LOS A | 1.4 | 9.8 | 0.11 | 0.57 | 0.11 | 42.4 |
| 23a | R1 | 93 | 3.0 | 0.365 | 2.6 | LOS A | 1.4 | 9.8 | 0.11 | 0.57 | 0.11 | 42.9 |
| Approach | | 536 | 1.6 | 0.365 | 6.6 | LOS A | 1.4 | 9.8 | 0.11 | 0.57 | 0.11 | 42.6 |
| North: Slidell Street | | | | | | | | | | | | |
| 7u | U | 1 | 0.0 | 0.075 | 10.2 | LOS B | 0.3 | 1.9 | 0.35 | 0.61 | 0.35 | 21.0 |
| 7a | L1 | 63 | 6.0 | 0.075 | 7.6 | LOS A | 0.3 | 1.9 | 0.35 | 0.61 | 0.35 | 42.8 |
| 9a | R1 | 18 | 0.0 | 0.075 | 3.6 | LOS A | 0.3 | 1.9 | 0.35 | 0.61 | 0.35 | 37.7 |
| Approach | | 82 | 4.6 | 0.075 | 6.8 | LOS A | 0.3 | 1.9 | 0.35 | 0.61 | 0.35 | 41.3 |
| SouthWest: Burnside Avenue | | | | | | | | | | | | |
| 30u | U | 3 | 0.0 | 0.142 | 7.1 | LOS A | 0.5 | 3.3 | 0.14 | 0.37 | 0.14 | 41.4 |
| 30a | L1 | 38 | 0.0 | 0.142 | 4.9 | LOS A | 0.5 | 3.3 | 0.14 | 0.37 | 0.14 | 27.9 |
| 32 | R2 | 148 | 4.0 | 0.142 | 2.0 | LOS A | 0.5 | 3.3 | 0.14 | 0.37 | 0.14 | 42.0 |
| Approach | | 189 | 3.1 | 0.142 | 2.7 | LOS A | 0.5 | 3.3 | 0.14 | 0.37 | 0.14 | 39.3 |
| All Vehicles | | 807 | 2.2 | 0.365 | 5.7 | LOS A | 1.4 | 9.8 | 0.14 | 0.53 | 0.14 | 41.7 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akcelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

MOVEMENT SUMMARY

Site: 1 [Burnside Roundabout - Total (2028) - AM]

Burnside Roundabout - Total (2028) - AM

Site Category: (None)

Roundabout

| Movement Performance - Vehicles | | | | | | | | | | | | |
|--|------|--------------------|------------|---------------|-------------------|------------------|--------------------------------|------------------|--------------|---------------------|------------------|--------------------|
| Mov ID | Turn | Demand Total veh/h | Flows HV % | Deg. Satn v/c | Average Delay sec | Level of Service | 95% Back of Queue Vehicles veh | Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Bayview Station Road | | | | | | | | | | | | |
| 21u | U | 2 | 0.0 | 0.150 | 9.2 | LOS A | 0.5 | 3.4 | 0.09 | 0.57 | 0.09 | 47.0 |
| 21 | L2 | 171 | 9.0 | 0.150 | 7.4 | LOS A | 0.5 | 3.4 | 0.09 | 0.57 | 0.09 | 42.4 |
| 23a | R1 | 28 | 0.0 | 0.150 | 2.6 | LOS A | 0.5 | 3.4 | 0.09 | 0.57 | 0.09 | 43.0 |
| Approach | | 201 | 7.6 | 0.150 | 6.8 | LOS A | 0.5 | 3.4 | 0.09 | 0.57 | 0.09 | 42.5 |
| North: Slidell Street | | | | | | | | | | | | |
| 7u | U | 1 | 0.0 | 0.089 | 9.5 | LOS A | 0.3 | 1.9 | 0.20 | 0.57 | 0.20 | 21.2 |
| 7a | L1 | 99 | 7.0 | 0.089 | 6.8 | LOS A | 0.3 | 1.9 | 0.20 | 0.57 | 0.20 | 42.9 |
| 9a | R1 | 10 | 0.0 | 0.089 | 2.9 | LOS A | 0.3 | 1.9 | 0.20 | 0.57 | 0.20 | 37.9 |
| Approach | | 109 | 6.3 | 0.089 | 6.5 | LOS A | 0.3 | 1.9 | 0.20 | 0.57 | 0.20 | 42.2 |
| SouthWest: Burnside Avenue | | | | | | | | | | | | |
| 30u | U | 1 | 0.0 | 0.353 | 7.2 | LOS A | 1.3 | 9.4 | 0.19 | 0.36 | 0.19 | 41.6 |
| 30a | L1 | 38 | 0.0 | 0.353 | 5.0 | LOS A | 1.3 | 9.4 | 0.19 | 0.36 | 0.19 | 25.7 |
| 32 | R2 | 438 | 0.0 | 0.353 | 2.1 | LOS A | 1.3 | 9.4 | 0.19 | 0.36 | 0.19 | 42.2 |
| Approach | | 477 | 0.0 | 0.353 | 2.3 | LOS A | 1.3 | 9.4 | 0.19 | 0.36 | 0.19 | 40.9 |
| All Vehicles | | 787 | 2.8 | 0.353 | 4.0 | LOS A | 1.3 | 9.4 | 0.17 | 0.45 | 0.17 | 41.4 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akcelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

MOVEMENT SUMMARY

Site: 1 [Burnside Roundabout - Total (2028) - PM]

Burnside Roundabout - Total (2028) - PM

Site Category: (None)

Roundabout

| Movement Performance - Vehicles | | | | | | | | | | | | |
|--|------|--------------------|------------|---------------|-------------------|------------------|--------------------------------|------------------|--------------|---------------------|------------------|--------------------|
| Mov ID | Turn | Demand Total veh/h | Flows HV % | Deg. Satn v/c | Average Delay sec | Level of Service | 95% Back of Queue Vehicles veh | Queue Distance m | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed km/h |
| SouthEast: Bayview Station Road | | | | | | | | | | | | |
| 21u | U | 12 | 11.0 | 0.430 | 9.3 | LOS A | 1.8 | 12.7 | 0.13 | 0.57 | 0.13 | 46.7 |
| 21 | L2 | 516 | 1.0 | 0.430 | 7.4 | LOS A | 1.8 | 12.7 | 0.13 | 0.57 | 0.13 | 42.4 |
| 23a | R1 | 103 | 3.0 | 0.430 | 2.6 | LOS A | 1.8 | 12.7 | 0.13 | 0.57 | 0.13 | 42.7 |
| Approach | | 631 | 1.5 | 0.430 | 6.7 | LOS A | 1.8 | 12.7 | 0.13 | 0.57 | 0.13 | 42.5 |
| North: Slidell Street | | | | | | | | | | | | |
| 7u | U | 1 | 0.0 | 0.086 | 10.6 | LOS B | 0.3 | 2.3 | 0.41 | 0.64 | 0.41 | 20.9 |
| 7a | L1 | 70 | 6.0 | 0.086 | 7.9 | LOS A | 0.3 | 2.3 | 0.41 | 0.64 | 0.41 | 42.6 |
| 9a | R1 | 20 | 0.0 | 0.086 | 3.9 | LOS A | 0.3 | 2.3 | 0.41 | 0.64 | 0.41 | 37.6 |
| Approach | | 91 | 4.6 | 0.086 | 7.1 | LOS A | 0.3 | 2.3 | 0.41 | 0.64 | 0.41 | 41.1 |
| SouthWest: Burnside Avenue | | | | | | | | | | | | |
| 30u | U | 4 | 0.0 | 0.169 | 7.1 | LOS A | 0.6 | 4.1 | 0.16 | 0.38 | 0.16 | 41.4 |
| 30a | L1 | 42 | 0.0 | 0.169 | 4.9 | LOS A | 0.6 | 4.1 | 0.16 | 0.38 | 0.16 | 27.9 |
| 32 | R2 | 178 | 4.0 | 0.169 | 2.0 | LOS A | 0.6 | 4.1 | 0.16 | 0.38 | 0.16 | 42.0 |
| Approach | | 224 | 3.2 | 0.169 | 2.7 | LOS A | 0.6 | 4.1 | 0.16 | 0.38 | 0.16 | 39.4 |
| All Vehicles | | 945 | 2.2 | 0.430 | 5.8 | LOS A | 1.8 | 12.7 | 0.16 | 0.53 | 0.16 | 41.6 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).

Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Roundabout Capacity Model: SIDRA Standard.

SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.

Gap-Acceptance Capacity: SIDRA Standard (Akcelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

HCM Signalized Intersection Capacity Analysis

1: Parkdale Ave & Burnside Ave

Future Total (2023)

AM Peak Hour



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|--------|------|---------------------------|-------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (vph) | 97 | 127 | 357 | 87 | 325 | 547 |
| Future Volume (vph) | 97 | 127 | 357 | 87 | 325 | 547 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 4.2 | 3.7 | 4.8 | 3.7 | 3.7 | 4.8 |
| Total Lost time (s) | 5.4 | | 5.2 | | | 5.2 |
| Lane Util. Factor | 1.00 | | 1.00 | | | 1.00 |
| Frpb, ped/bikes | 0.81 | | 0.99 | | | 1.00 |
| Flpb, ped/bikes | 1.00 | | 1.00 | | | 1.00 |
| Fr _t | 0.92 | | 0.97 | | | 1.00 |
| Flt Protected | 0.98 | | 1.00 | | | 0.98 |
| Satd. Flow (prot) | 1330 | | 1928 | | | 1956 |
| Flt Permitted | 0.98 | | 1.00 | | | 0.65 |
| Satd. Flow (perm) | 1330 | | 1928 | | | 1297 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 97 | 127 | 357 | 87 | 325 | 547 |
| RTOR Reduction (vph) | 82 | 0 | 13 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 142 | 0 | 431 | 0 | 0 | 872 |
| Confl. Peds. (#/hr) | 60 | 151 | | 13 | 13 | |
| Confl. Bikes (#/hr) | | 5 | | 6 | | |
| Heavy Vehicles (%) | 0% | 9% | 1% | 7% | 2% | 2% |
| Turn Type | pm+pt | | NA | | Perm | NA |
| Protected Phases | 3 | | 2 | | | 6 |
| Permitted Phases | 8 | | | 6 | | |
| Actuated Green, G (s) | 12.5 | | 36.9 | | | 36.9 |
| Effective Green, g (s) | 12.5 | | 36.9 | | | 36.9 |
| Actuated g/C Ratio | 0.21 | | 0.61 | | | 0.61 |
| Clearance Time (s) | 5.4 | | 5.2 | | | 5.2 |
| Vehicle Extension (s) | 3.0 | | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | 277 | | 1185 | | | 797 |
| v/s Ratio Prot | c0.11 | | 0.22 | | | |
| v/s Ratio Perm | | | | c0.67 | | |
| v/c Ratio | 0.51 | | 0.36 | | | 1.09 |
| Uniform Delay, d1 | 21.0 | | 5.7 | | | 11.6 |
| Progression Factor | 1.00 | | 1.00 | | | 1.00 |
| Incremental Delay, d2 | 1.6 | | 0.9 | | | 60.7 |
| Delay (s) | 22.6 | | 6.6 | | | 72.2 |
| Level of Service | C | | A | | | E |
| Approach Delay (s) | 22.6 | | 6.6 | | | 72.2 |
| Approach LOS | C | | A | | | E |
| Intersection Summary | | | | | | |
| HCM 2000 Control Delay | 46.1 | | HCM 2000 Level of Service | | D | |
| HCM 2000 Volume to Capacity ratio | 0.95 | | | | | |
| Actuated Cycle Length (s) | 60.0 | | Sum of lost time (s) | | 10.6 | |
| Intersection Capacity Utilization | 106.1% | | ICU Level of Service | | G | |
| Analysis Period (min) | 15 | | | | | |
| c Critical Lane Group | | | | | | |

HCM Signalized Intersection Capacity Analysis
2: Slidell St/Onigam St & Sir John A MacDonald Pkwy

Future Total (2023)

AM Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBL | SBT |
|-----------------------------------|-------|------|------|------|---------------------------|------|------|------|-------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 0 | 1665 | 24 | 1 | 1177 | 1 | 1 | 1 | 23 | 1 | 1 | 5 |
| Future Volume (vph) | 0 | 1665 | 24 | 1 | 1177 | 1 | 1 | 1 | 23 | 1 | 1 | 5 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 3.7 | 3.8 | 3.7 | 3.7 | 3.8 | 3.7 | 3.7 | 3.7 | 3.9 | 3.7 | 3.7 | 4.0 |
| Total Lost time (s) | | 5.5 | | | 5.5 | | | | 6.3 | | | 6.3 |
| Lane Util. Factor | | 0.95 | | | 0.95 | | | | 1.00 | | | 1.00 |
| Frpb, ped/bikes | | 1.00 | | | 1.00 | | | | 1.00 | | | 0.99 |
| Flpb, ped/bikes | | 1.00 | | | 1.00 | | | | 1.00 | | | 1.00 |
| Fr _t | | 1.00 | | | 1.00 | | | | 0.99 | | | 0.95 |
| Flt Protected | | 1.00 | | | 1.00 | | | | 1.00 | | | 0.99 |
| Satd. Flow (prot) | | 3487 | | | 3461 | | | | 1839 | | | 1765 |
| Flt Permitted | | 1.00 | | | 0.95 | | | | 0.98 | | | 0.97 |
| Satd. Flow (perm) | | 3487 | | | 3302 | | | | 1804 | | | 1716 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 0 | 1665 | 24 | 1 | 1177 | 1 | 1 | 1 | 23 | 1 | 1 | 5 |
| RTOR Reduction (vph) | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 3 |
| Lane Group Flow (vph) | 0 | 1688 | 0 | 0 | 1179 | 0 | 0 | 0 | 25 | 0 | 0 | 6 |
| Confl. Peds. (#/hr) | 2 | | 1 | 1 | | 2 | 1 | 3 | | 4 | 4 | |
| Confl. Bikes (#/hr) | | | | 1 | | | | | | 14 | | |
| Heavy Vehicles (%) | 0% | 0% | 0% | 0% | 1% | 0% | 0% | 0% | 0% | 0% | 0% | 0% |
| Turn Type | | NA | | Perm | NA | | Perm | Perm | NA | | Perm | NA |
| Protected Phases | | 2 | | | 6 | | | | 8 | | | 4 |
| Permitted Phases | 2 | | | 6 | | | 8 | 8 | | | 4 | |
| Actuated Green, G (s) | 73.8 | | | 73.8 | | | | | 9.4 | | | 9.4 |
| Effective Green, g (s) | 73.8 | | | 73.8 | | | | | 9.4 | | | 9.4 |
| Actuated g/C Ratio | 0.78 | | | 0.78 | | | | | 0.10 | | | 0.10 |
| Clearance Time (s) | 5.5 | | | 5.5 | | | | | 6.3 | | | 6.3 |
| Vehicle Extension (s) | 3.0 | | | 3.0 | | | | | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | 2708 | | | 2565 | | | | | 178 | | | 169 |
| v/s Ratio Prot | c0.48 | | | | | | | | | | | |
| v/s Ratio Perm | | | | 0.36 | | | | | c0.01 | | | 0.00 |
| v/c Ratio | 0.62 | | | 0.46 | | | | | 0.14 | | | 0.04 |
| Uniform Delay, d1 | 4.6 | | | 3.7 | | | | | 39.1 | | | 38.7 |
| Progression Factor | 1.00 | | | 1.00 | | | | | 1.00 | | | 1.00 |
| Incremental Delay, d2 | 1.1 | | | 0.6 | | | | | 0.4 | | | 0.1 |
| Delay (s) | 5.7 | | | 4.3 | | | | | 39.5 | | | 38.8 |
| Level of Service | A | | | A | | | | | D | | | D |
| Approach Delay (s) | 5.7 | | | 4.3 | | | | | 39.5 | | | 38.8 |
| Approach LOS | A | | | A | | | | | D | | | D |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | 5.5 | | | | HCM 2000 Level of Service | | | | A | | | |
| HCM 2000 Volume to Capacity ratio | 0.57 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 95.0 | | | | Sum of lost time (s) | | | | 11.8 | | | |
| Intersection Capacity Utilization | 69.3% | | | | ICU Level of Service | | | | C | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis
2: Slidell St/Onigam St & Sir John A MacDonald Pkwy

Future Total (2023)
AM Peak Hour

| Movement | SBR |
|------------------------|------|
| Lane Configurations | |
| Traffic Volume (vph) | 3 |
| Future Volume (vph) | 3 |
| Ideal Flow (vphpl) | 1800 |
| Lane Width | 3.7 |
| Total Lost time (s) | |
| Lane Util. Factor | |
| Frpb, ped/bikes | |
| Flpb, ped/bikes | |
| Fr | |
| Flt Protected | |
| Satd. Flow (prot) | |
| Flt Permitted | |
| Satd. Flow (perm) | |
| Peak-hour factor, PHF | 1.00 |
| Adj. Flow (vph) | 3 |
| RTOR Reduction (vph) | 0 |
| Lane Group Flow (vph) | 0 |
| Confl. Peds. (#/hr) | 3 |
| Confl. Bikes (#/hr) | 8 |
| Heavy Vehicles (%) | 0% |
| Turn Type | |
| Protected Phases | |
| Permitted Phases | |
| Actuated Green, G (s) | |
| Effective Green, g (s) | |
| Actuated g/C Ratio | |
| Clearance Time (s) | |
| Vehicle Extension (s) | |
| Lane Grp Cap (vph) | |
| v/s Ratio Prot | |
| v/s Ratio Perm | |
| v/c Ratio | |
| Uniform Delay, d1 | |
| Progression Factor | |
| Incremental Delay, d2 | |
| Delay (s) | |
| Level of Service | |
| Approach Delay (s) | |
| Approach LOS | |
| Intersection Summary | |

HCM Signalized Intersection Capacity Analysis

3: Bayview Stn Rd & Scott St/Albert St

Future Total (2023)

AM Peak Hour

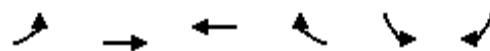
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|--------|------|------|------|---------------------------|------|------|------|------|-------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 50 | 674 | 87 | 54 | 326 | 64 | 49 | 113 | 123 | 154 | 251 | 36 |
| Future Volume (vph) | 50 | 674 | 87 | 54 | 326 | 64 | 49 | 113 | 123 | 154 | 251 | 36 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 3.7 | 3.6 | 3.7 | 3.2 | 3.5 | 3.8 | 3.0 | 4.3 | 3.7 | 3.3 | 4.5 | 3.7 |
| Total Lost time (s) | 6.5 | | 6.5 | 6.5 | 6.5 | 6.4 | 6.4 | 6.4 | | 6.4 | 6.4 | |
| Lane Util. Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frpb, ped/bikes | 0.99 | | 1.00 | 1.00 | 0.78 | 1.00 | 0.93 | | | 1.00 | 0.98 | |
| Flpb, ped/bikes | 0.99 | | 0.97 | 1.00 | 1.00 | 0.94 | 1.00 | | | 0.96 | 1.00 | |
| Fr _t | 0.99 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.92 | | | 1.00 | 0.98 | |
| Flt Protected | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1419 | | 1562 | 1338 | 1136 | 1322 | 1607 | | | 1530 | 1835 | |
| Flt Permitted | 0.96 | | 0.33 | 1.00 | 1.00 | 0.38 | 1.00 | | | 0.48 | 1.00 | |
| Satd. Flow (perm) | 1365 | | 542 | 1338 | 1136 | 534 | 1607 | | | 771 | 1835 | |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 50 | 674 | 87 | 54 | 326 | 64 | 49 | 113 | 123 | 154 | 251 | 36 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 | 0 | 23 | 0 | 40 | 0 | 0 | 5 | 0 |
| Lane Group Flow (vph) | 0 | 807 | 0 | 54 | 326 | 41 | 49 | 196 | 0 | 154 | 282 | 0 |
| Confl. Peds. (#/hr) | 107 | | 52 | 52 | | 107 | 59 | | 30 | 30 | | 59 |
| Confl. Bikes (#/hr) | | | 2 | | | 3 | | | 39 | | | 12 |
| Heavy Vehicles (%) | 0% | 26% | 4% | 2% | 33% | 7% | 13% | 4% | 3% | 4% | 2% | 17% |
| Turn Type | Perm | NA | | Perm | NA | Perm | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | 6 | 8 | | | 4 | | |
| Actuated Green, G (s) | 63.5 | | 63.5 | 63.5 | 63.5 | 23.6 | 23.6 | | | 23.6 | 23.6 | |
| Effective Green, g (s) | 63.5 | | 63.5 | 63.5 | 63.5 | 23.6 | 23.6 | | | 23.6 | 23.6 | |
| Actuated g/C Ratio | 0.64 | | 0.64 | 0.64 | 0.64 | 0.24 | 0.24 | | | 0.24 | 0.24 | |
| Clearance Time (s) | 6.5 | | 6.5 | 6.5 | 6.5 | 6.4 | 6.4 | | | 6.4 | 6.4 | |
| Vehicle Extension (s) | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 866 | | 344 | 849 | 721 | 126 | 379 | | | 181 | 433 | |
| v/s Ratio Prot | | | | 0.24 | | | | 0.12 | | | 0.15 | |
| v/s Ratio Perm | c0.59 | | 0.10 | | 0.04 | 0.09 | | | | c0.20 | | |
| v/c Ratio | 0.93 | | 0.16 | 0.38 | 0.06 | 0.39 | 0.52 | | | 0.85 | 0.65 | |
| Uniform Delay, d1 | 16.3 | | 7.4 | 8.8 | 6.9 | 32.1 | 33.2 | | | 36.5 | 34.5 | |
| Progression Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 17.9 | | 1.0 | 1.3 | 0.1 | 2.0 | 1.2 | | | 29.8 | 3.5 | |
| Delay (s) | 34.2 | | 8.4 | 10.1 | 7.1 | 34.1 | 34.4 | | | 66.4 | 38.0 | |
| Level of Service | C | | A | B | A | C | C | | | E | D | |
| Approach Delay (s) | 34.2 | | | 9.5 | | | 34.4 | | | | 47.9 | |
| Approach LOS | C | | | A | | | C | | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | 31.7 | | | | HCM 2000 Level of Service | | | | C | | | |
| HCM 2000 Volume to Capacity ratio | 0.91 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 100.0 | | | | Sum of lost time (s) | | | 12.9 | | | | |
| Intersection Capacity Utilization | 118.9% | | | | ICU Level of Service | | | H | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Unsignalized Intersection Capacity Analysis

5: Hinchey Ave & Parcel 1

Future Total (2023)

AM Peak Hour



| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|------|-------|------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 26 | 0 | 0 | 12 | 5 | 7 |
| Future Volume (Veh/h) | 26 | 0 | 0 | 12 | 5 | 7 |
| Sign Control | Free | Free | | Stop | | |
| Grade | 0% | 0% | | 0% | | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 26 | 0 | 0 | 12 | 5 | 7 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | None | | | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 12 | | | 58 | 6 | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 12 | | | 58 | 6 | |
| tC, single (s) | 4.1 | | | 6.4 | 6.2 | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 2.2 | | | 3.5 | 3.3 | |
| p0 queue free % | 98 | | | 99 | 99 | |
| cM capacity (veh/h) | 1607 | | | 934 | 1077 | |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total | 26 | 12 | 12 | | | |
| Volume Left | 26 | 0 | 5 | | | |
| Volume Right | 0 | 12 | 7 | | | |
| cSH | 1607 | 1700 | 1012 | | | |
| Volume to Capacity | 0.02 | 0.01 | 0.01 | | | |
| Queue Length 95th (m) | 0.3 | 0.0 | 0.3 | | | |
| Control Delay (s) | 7.3 | 0.0 | 8.6 | | | |
| Lane LOS | A | | A | | | |
| Approach Delay (s) | 7.3 | 0.0 | 8.6 | | | |
| Approach LOS | | | A | | | |
| Intersection Summary | | | | | | |
| Average Delay | | 5.8 | | | | |
| Intersection Capacity Utilization | | 18.2% | | ICU Level of Service | | A |
| Analysis Period (min) | | 15 | | | | |

HCM Unsignalized Intersection Capacity Analysis
6: Hinckley Ave & Parcel 2

Future Total (2023)
AM Peak Hour

| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|------|-------|------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 11 | 0 | 12 | 35 | 0 | 5 |
| Future Volume (Veh/h) | 11 | 0 | 12 | 35 | 0 | 5 |
| Sign Control | Stop | | Free | | | Free |
| Grade | 0% | | 0% | | | 0% |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 11 | 0 | 12 | 35 | 0 | 5 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | | | None | | | None |
| Median storage veh) | | | | | | |
| Upstream signal (m) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 34 | 30 | | | 47 | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 34 | 30 | | | 47 | |
| tC, single (s) | 6.4 | 6.2 | | | 4.1 | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 3.5 | 3.3 | | | 2.2 | |
| p0 queue free % | 99 | 100 | | | 100 | |
| cM capacity (veh/h) | 979 | 1045 | | | 1560 | |
| Direction, Lane # | WB 1 | NB 1 | SB 1 | | | |
| Volume Total | 11 | 47 | 5 | | | |
| Volume Left | 11 | 0 | 0 | | | |
| Volume Right | 0 | 35 | 0 | | | |
| cSH | 979 | 1700 | 1560 | | | |
| Volume to Capacity | 0.01 | 0.03 | 0.00 | | | |
| Queue Length 95th (m) | 0.2 | 0.0 | 0.0 | | | |
| Control Delay (s) | 8.7 | 0.0 | 0.0 | | | |
| Lane LOS | A | | | | | |
| Approach Delay (s) | 8.7 | 0.0 | 0.0 | | | |
| Approach LOS | A | | | | | |
| Intersection Summary | | | | | | |
| Average Delay | | 1.5 | | | | |
| Intersection Capacity Utilization | | 13.3% | | ICU Level of Service | | A |
| Analysis Period (min) | | 15 | | | | |

HCM Unsignalized Intersection Capacity Analysis
7: Burnside Ave & Parcel 3

Future Total (2023)
AM Peak Hour

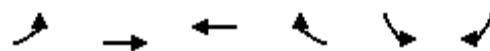
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|------|-------|------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 23 | 420 | 101 | 12 | 4 | 7 |
| Future Volume (Veh/h) | 23 | 420 | 101 | 12 | 4 | 7 |
| Sign Control | | Free | Free | | Stop | |
| Grade | | 0% | 0% | | 0% | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 23 | 420 | 101 | 12 | 4 | 7 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | | None | None | | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | | 201 | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 113 | | | 573 | 107 | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 113 | | | 573 | 107 | |
| tC, single (s) | 4.1 | | | 6.4 | 6.2 | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 2.2 | | | 3.5 | 3.3 | |
| p0 queue free % | 98 | | | 99 | 99 | |
| cM capacity (veh/h) | 1476 | | | 474 | 947 | |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total | 443 | 113 | 11 | | | |
| Volume Left | 23 | 0 | 4 | | | |
| Volume Right | 0 | 12 | 7 | | | |
| cSH | 1476 | 1700 | 694 | | | |
| Volume to Capacity | 0.02 | 0.07 | 0.02 | | | |
| Queue Length 95th (m) | 0.3 | 0.0 | 0.3 | | | |
| Control Delay (s) | 0.5 | 0.0 | 10.3 | | | |
| Lane LOS | A | B | | | | |
| Approach Delay (s) | 0.5 | 0.0 | 10.3 | | | |
| Approach LOS | | B | | | | |
| Intersection Summary | | | | | | |
| Average Delay | | 0.6 | | | | |
| Intersection Capacity Utilization | | 41.3% | | ICU Level of Service | | A |
| Analysis Period (min) | | 15 | | | | |

HCM Unsignalized Intersection Capacity Analysis

8: Burnside Ave & Parcel 4

Future Total (2023)

AM Peak Hour



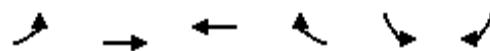
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|------|-------|------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 26 | 398 | 106 | 12 | 5 | 7 |
| Future Volume (Veh/h) | 26 | 398 | 106 | 12 | 5 | 7 |
| Sign Control | Free | Free | | Stop | | |
| Grade | 0% | 0% | | 0% | | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 26 | 398 | 106 | 12 | 5 | 7 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | None | | | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | | 256 | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 118 | | | 562 | 112 | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 118 | | | 562 | 112 | |
| tC, single (s) | 4.1 | | | 6.4 | 6.2 | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 2.2 | | | 3.5 | 3.3 | |
| p0 queue free % | 98 | | | 99 | 99 | |
| cM capacity (veh/h) | 1470 | | | 480 | 941 | |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total | 424 | 118 | 12 | | | |
| Volume Left | 26 | 0 | 5 | | | |
| Volume Right | 0 | 12 | 7 | | | |
| cSH | 1470 | 1700 | 672 | | | |
| Volume to Capacity | 0.02 | 0.07 | 0.02 | | | |
| Queue Length 95th (m) | 0.4 | 0.0 | 0.4 | | | |
| Control Delay (s) | 0.6 | 0.0 | 10.5 | | | |
| Lane LOS | A | | B | | | |
| Approach Delay (s) | 0.6 | 0.0 | 10.5 | | | |
| Approach LOS | | | B | | | |
| Intersection Summary | | | | | | |
| Average Delay | | 0.7 | | | | |
| Intersection Capacity Utilization | | 40.3% | | ICU Level of Service | | A |
| Analysis Period (min) | | 15 | | | | |

HCM Unsignalized Intersection Capacity Analysis

9: Burnside Ave & Parcel 5

Future Total (2023)

AM Peak Hour



| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|------|-------|------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 22 | 381 | 111 | 11 | 4 | 7 |
| Future Volume (Veh/h) | 22 | 381 | 111 | 11 | 4 | 7 |
| Sign Control | Free | Free | | Stop | | |
| Grade | 0% | 0% | | 0% | | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 22 | 381 | 111 | 11 | 4 | 7 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | | None | None | | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | | 298 | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 122 | | | 542 | 116 | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 122 | | | 542 | 116 | |
| tC, single (s) | 4.1 | | | 6.4 | 6.2 | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 2.2 | | | 3.5 | 3.3 | |
| p0 queue free % | 98 | | | 99 | 99 | |
| cM capacity (veh/h) | 1465 | | | 494 | 936 | |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total | 403 | 122 | 11 | | | |
| Volume Left | 22 | 0 | 4 | | | |
| Volume Right | 0 | 11 | 7 | | | |
| cSH | 1465 | 1700 | 706 | | | |
| Volume to Capacity | 0.02 | 0.07 | 0.02 | | | |
| Queue Length 95th (m) | 0.3 | 0.0 | 0.3 | | | |
| Control Delay (s) | 0.5 | 0.0 | 10.2 | | | |
| Lane LOS | A | | B | | | |
| Approach Delay (s) | 0.5 | 0.0 | 10.2 | | | |
| Approach LOS | | | B | | | |
| Intersection Summary | | | | | | |
| Average Delay | | 0.6 | | | | |
| Intersection Capacity Utilization | | 42.7% | | ICU Level of Service | | A |
| Analysis Period (min) | | 15 | | | | |

HCM Unsignalized Intersection Capacity Analysis
10: Burnside Ave & Parcel 6

Future Total (2023)
AM Peak Hour

| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|------|-------|------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 23 | 362 | 115 | 12 | 4 | 7 |
| Future Volume (Veh/h) | 23 | 362 | 115 | 12 | 4 | 7 |
| Sign Control | Free | Free | | Stop | | |
| Grade | 0% | 0% | | 0% | | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 23 | 362 | 115 | 12 | 4 | 7 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | None | | | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | 344 | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 127 | | | 529 | 121 | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 127 | | | 529 | 121 | |
| tC, single (s) | 4.1 | | | 6.4 | 6.2 | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 2.2 | | | 3.5 | 3.3 | |
| p0 queue free % | 98 | | | 99 | 99 | |
| cM capacity (veh/h) | 1459 | | | 502 | 930 | |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total | 385 | 127 | 11 | | | |
| Volume Left | 23 | 0 | 4 | | | |
| Volume Right | 0 | 12 | 7 | | | |
| cSH | 1459 | 1700 | 710 | | | |
| Volume to Capacity | 0.02 | 0.07 | 0.02 | | | |
| Queue Length 95th (m) | 0.3 | 0.0 | 0.3 | | | |
| Control Delay (s) | 0.6 | 0.0 | 10.1 | | | |
| Lane LOS | A | | B | | | |
| Approach Delay (s) | 0.6 | 0.0 | 10.1 | | | |
| Approach LOS | | | B | | | |
| Intersection Summary | | | | | | |
| Average Delay | | 0.6 | | | | |
| Intersection Capacity Utilization | | 41.9% | | ICU Level of Service | | A |
| Analysis Period (min) | | 15 | | | | |

HCM Signalized Intersection Capacity Analysis

1: Parkdale Ave & Burnside Ave

Future Total (2023)

PM Peak Hour



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|------------------------|-------|------|------|-------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (vph) | 35 | 425 | 728 | 33 | 80 | 474 |
| Future Volume (vph) | 35 | 425 | 728 | 33 | 80 | 474 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 4.2 | 3.7 | 4.8 | 3.7 | 3.7 | 4.8 |
| Total Lost time (s) | 5.4 | | 5.2 | | | 5.2 |
| Lane Util. Factor | 1.00 | | 1.00 | | | 1.00 |
| Frpb, ped/bikes | 0.90 | | 1.00 | | | 1.00 |
| Flpb, ped/bikes | 1.00 | | 1.00 | | | 1.00 |
| Fr _t | 0.88 | | 0.99 | | | 1.00 |
| Flt Protected | 1.00 | | 1.00 | | | 0.99 |
| Satd. Flow (prot) | 1512 | | 1996 | | | 1990 |
| Flt Permitted | 1.00 | | 1.00 | | | 0.70 |
| Satd. Flow (perm) | 1512 | | 1996 | | | 1397 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 35 | 425 | 728 | 33 | 80 | 474 |
| RTOR Reduction (vph) | 143 | 0 | 2 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 317 | 0 | 759 | 0 | 0 | 554 |
| Confl. Peds. (#/hr) | 32 | 34 | | 15 | 15 | |
| Confl. Bikes (#/hr) | | | 1 | | | |
| Heavy Vehicles (%) | 0% | 0% | 1% | 10% | 0% | 2% |
| Turn Type | Prot | | NA | | Perm | NA |
| Protected Phases | 8 | | 2 | | | 6 |
| Permitted Phases | | | | 6 | | |
| Actuated Green, G (s) | 17.2 | | 42.2 | | | 42.2 |
| Effective Green, g (s) | 17.2 | | 42.2 | | | 42.2 |
| Actuated g/C Ratio | 0.25 | | 0.60 | | | 0.60 |
| Clearance Time (s) | 5.4 | | 5.2 | | | 5.2 |
| Vehicle Extension (s) | 3.0 | | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | 371 | | 1203 | | | 842 |
| v/s Ratio Prot | c0.21 | | 0.38 | | | |
| v/s Ratio Perm | | | | c0.40 | | |
| v/c Ratio | 0.85 | | 0.63 | | | 0.66 |
| Uniform Delay, d1 | 25.2 | | 8.9 | | | 9.1 |
| Progression Factor | 1.00 | | 1.00 | | | 1.00 |
| Incremental Delay, d2 | 17.1 | | 2.5 | | | 4.0 |
| Delay (s) | 42.3 | | 11.4 | | | 13.2 |
| Level of Service | D | | B | | | B |
| Approach Delay (s) | 42.3 | | 11.4 | | | 13.2 |
| Approach LOS | D | | B | | | B |

Intersection Summary

| | | | |
|-----------------------------------|--------|---------------------------|------|
| HCM 2000 Control Delay | 20.0 | HCM 2000 Level of Service | B |
| HCM 2000 Volume to Capacity ratio | 0.71 | | |
| Actuated Cycle Length (s) | 70.0 | Sum of lost time (s) | 10.6 |
| Intersection Capacity Utilization | 119.3% | ICU Level of Service | H |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
2: Slidell St/Onigam St & Sir John A MacDonald Pkwy

Future Total (2023)
PM Peak Hour

| Movement | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
|-----------------------------------|-------|------|------|------|------|---------------------------|------|------|-------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 0 | 1037 | 4 | 2 | 2 | 1767 | 0 | 28 | 14 | 37 | 3 | 28 |
| Future Volume (vph) | 0 | 1037 | 4 | 2 | 2 | 1767 | 0 | 28 | 14 | 37 | 3 | 28 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 3.7 | 3.8 | 3.7 | 3.7 | 3.7 | 3.8 | 3.7 | 3.7 | 3.9 | 3.7 | 3.7 | 4.0 |
| Total Lost time (s) | | 5.5 | | | | 5.5 | | | 6.3 | | | 6.3 |
| Lane Util. Factor | 0.95 | | | | | 0.95 | | | 1.00 | | | 1.00 |
| Frpb, ped/bikes | 1.00 | | | | | 1.00 | | | 0.99 | | | 0.99 |
| Flpb, ped/bikes | 1.00 | | | | | 1.00 | | | 1.00 | | | 1.00 |
| Fr _t | 1.00 | | | | | 1.00 | | | 0.94 | | | 0.96 |
| Flt Protected | 1.00 | | | | | 1.00 | | | 0.98 | | | 1.00 |
| Satd. Flow (prot) | 3460 | | | | | 3496 | | | 1689 | | | 1744 |
| Flt Permitted | 1.00 | | | | | 0.95 | | | 0.87 | | | 0.98 |
| Satd. Flow (perm) | 3460 | | | | | 3333 | | | 1488 | | | 1708 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 0 | 1037 | 4 | 2 | 2 | 1767 | 0 | 28 | 14 | 37 | 3 | 28 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 34 | 0 | 0 | 10 |
| Lane Group Flow (vph) | 0 | 1041 | 0 | 0 | 0 | 1771 | 0 | 0 | 45 | 0 | 0 | 32 |
| Confl. Peds. (#/hr) | 1 | | | 7 | | | 1 | 6 | | 7 | 7 | |
| Confl. Bikes (#/hr) | | | | | | | | | 2 | | | |
| Heavy Vehicles (%) | 0% | 1% | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 4% |
| Turn Type | | NA | | Perm | Perm | NA | | Perm | NA | | Perm | NA |
| Protected Phases | | 2 | | | | 6 | | | 8 | | | 4 |
| Permitted Phases | 2 | | 6 | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | 74.7 | | | | | 74.7 | | | 8.5 | | | 8.5 |
| Effective Green, g (s) | 74.7 | | | | | 74.7 | | | 8.5 | | | 8.5 |
| Actuated g/C Ratio | 0.79 | | | | | 0.79 | | | 0.09 | | | 0.09 |
| Clearance Time (s) | 5.5 | | | | | 5.5 | | | 6.3 | | | 6.3 |
| Vehicle Extension (s) | 3.0 | | | | | 3.0 | | | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | 2720 | | | | | 2620 | | | 133 | | | 152 |
| v/s Ratio Prot | 0.30 | | | | | | | | | | | |
| v/s Ratio Perm | | | | | | c0.53 | | | c0.03 | | | 0.02 |
| v/c Ratio | 0.38 | | | | | 0.68 | | | 0.34 | | | 0.21 |
| Uniform Delay, d1 | 3.1 | | | | | 4.6 | | | 40.6 | | | 40.1 |
| Progression Factor | 1.00 | | | | | 1.00 | | | 1.00 | | | 1.00 |
| Incremental Delay, d2 | 0.4 | | | | | 1.4 | | | 1.5 | | | 0.7 |
| Delay (s) | 3.5 | | | | | 6.0 | | | 42.1 | | | 40.8 |
| Level of Service | A | | | | | A | | | D | | | D |
| Approach Delay (s) | 3.5 | | | | | 6.0 | | | 42.1 | | | 40.8 |
| Approach LOS | A | | | | | A | | | D | | | D |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | 6.6 | | | | | HCM 2000 Level of Service | | | A | | | |
| HCM 2000 Volume to Capacity ratio | 0.64 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 95.0 | | | | | Sum of lost time (s) | | | 11.8 | | | |
| Intersection Capacity Utilization | 78.4% | | | | | ICU Level of Service | | | D | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis
2: Slidell St/Onigam St & Sir John A MacDonald Pkwy

Future Total (2023)
PM Peak Hour

| Movement | SBR |
|------------------------|------|
| Lane Configurations | |
| Traffic Volume (vph) | 11 |
| Future Volume (vph) | 11 |
| Ideal Flow (vphpl) | 1800 |
| Lane Width | 3.7 |
| Total Lost time (s) | |
| Lane Util. Factor | |
| Frpb, ped/bikes | |
| Fpb, ped/bikes | |
| Fr | |
| Flt Protected | |
| Satd. Flow (prot) | |
| Flt Permitted | |
| Satd. Flow (perm) | |
| Peak-hour factor, PHF | 1.00 |
| Adj. Flow (vph) | 11 |
| RTOR Reduction (vph) | 0 |
| Lane Group Flow (vph) | 0 |
| Confl. Peds. (#/hr) | 6 |
| Confl. Bikes (#/hr) | 6 |
| Heavy Vehicles (%) | 0% |
| Turn Type | |
| Protected Phases | |
| Permitted Phases | |
| Actuated Green, G (s) | |
| Effective Green, g (s) | |
| Actuated g/C Ratio | |
| Clearance Time (s) | |
| Vehicle Extension (s) | |
| Lane Grp Cap (vph) | |
| v/s Ratio Prot | |
| v/s Ratio Perm | |
| v/c Ratio | |
| Uniform Delay, d1 | |
| Progression Factor | |
| Incremental Delay, d2 | |
| Delay (s) | |
| Level of Service | |
| Approach Delay (s) | |
| Approach LOS | |
| Intersection Summary | |

HCM Signalized Intersection Capacity Analysis

3: Bayview Stn Rd & Scott St/Albert St

Future Total (2023)

PM Peak Hour

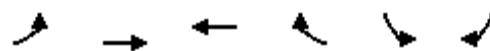
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|------|-------|---------------------------|------|------|-------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 25 | 459 | 105 | 86 | 604 | 101 | 101 | 269 | 75 | 64 | 93 | 30 |
| Future Volume (vph) | 25 | 459 | 105 | 86 | 604 | 101 | 101 | 269 | 75 | 64 | 93 | 30 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 3.7 | 3.6 | 3.7 | 3.2 | 3.5 | 3.8 | 3.0 | 4.3 | 3.7 | 3.3 | 4.5 | 3.7 |
| Total Lost time (s) | 6.5 | | | 6.5 | 6.5 | 6.4 | 6.4 | | | 6.4 | 6.4 | |
| Lane Util. Factor | 1.00 | | | 1.00 | 1.00 | 1.00 | 1.00 | | | 1.00 | 1.00 | |
| Frpb, ped/bikes | 0.98 | | | 1.00 | 1.00 | 0.89 | 1.00 | 0.99 | | 1.00 | 0.97 | |
| Flpb, ped/bikes | 1.00 | | | 0.95 | 1.00 | 1.00 | 0.93 | 1.00 | | 0.99 | 1.00 | |
| Fr _t | 0.98 | | | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 | | 1.00 | 0.96 | |
| Flt Protected | 1.00 | | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1484 | | | 1559 | 1402 | 1374 | 1458 | 1841 | | 1638 | 1797 | |
| Flt Permitted | 0.96 | | | 0.43 | 1.00 | 1.00 | 0.68 | 1.00 | | 0.25 | 1.00 | |
| Satd. Flow (perm) | 1433 | | | 699 | 1402 | 1374 | 1041 | 1841 | | 436 | 1797 | |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 25 | 459 | 105 | 86 | 604 | 101 | 101 | 269 | 75 | 64 | 93 | 30 |
| RTOR Reduction (vph) | 0 | 7 | 0 | 0 | 0 | 35 | 0 | 11 | 0 | 0 | 12 | 0 |
| Lane Group Flow (vph) | 0 | 582 | 0 | 86 | 604 | 66 | 101 | 333 | 0 | 64 | 111 | 0 |
| Confl. Peds. (#/hr) | 48 | | 63 | 63 | | 48 | 42 | | 10 | 10 | | 42 |
| Confl. Bikes (#/hr) | | | 3 | | | 4 | | | 6 | | | 16 |
| Heavy Vehicles (%) | 0% | 19% | 1% | 0% | 27% | 1% | 2% | 0% | 4% | 0% | 2% | 6% |
| Turn Type | Perm | NA | | Perm | NA | Perm | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | 6 | 8 | | | 4 | | |
| Actuated Green, G (s) | 65.0 | | 65.0 | 65.0 | 65.0 | 22.1 | 22.1 | | 22.1 | 22.1 | | |
| Effective Green, g (s) | 65.0 | | 65.0 | 65.0 | 65.0 | 22.1 | 22.1 | | 22.1 | 22.1 | | |
| Actuated g/C Ratio | 0.65 | | 0.65 | 0.65 | 0.65 | 0.22 | 0.22 | | 0.22 | 0.22 | | |
| Clearance Time (s) | 6.5 | | 6.5 | 6.5 | 6.5 | 6.4 | 6.4 | | 6.4 | 6.4 | | |
| Vehicle Extension (s) | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | |
| Lane Grp Cap (vph) | 931 | | 454 | 911 | 893 | 230 | 406 | | 96 | 397 | | |
| v/s Ratio Prot | | | | c0.43 | | | | c0.18 | | | 0.06 | |
| v/s Ratio Perm | 0.41 | | 0.12 | | 0.05 | 0.10 | | | 0.15 | | | |
| v/c Ratio | 0.63 | | 0.19 | 0.66 | 0.07 | 0.44 | 0.82 | | 0.67 | 0.28 | | |
| Uniform Delay, d1 | 10.3 | | 7.0 | 10.8 | 6.4 | 33.6 | 37.1 | | 35.6 | 32.3 | | |
| Progression Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | |
| Incremental Delay, d2 | 3.2 | | 0.9 | 3.8 | 0.2 | 1.3 | 12.5 | | 16.1 | 0.4 | | |
| Delay (s) | 13.5 | | 7.9 | 14.6 | 6.6 | 34.9 | 49.6 | | 51.7 | 32.7 | | |
| Level of Service | B | | A | B | A | C | D | | D | C | | |
| Approach Delay (s) | 13.5 | | | | 12.8 | | | 46.2 | | | 39.2 | |
| Approach LOS | B | | | | B | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | 22.9 | | | | HCM 2000 Level of Service | | | C | | | | |
| HCM 2000 Volume to Capacity ratio | 0.70 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 100.0 | | | | Sum of lost time (s) | | | 12.9 | | | | |
| Intersection Capacity Utilization | 99.9% | | | | ICU Level of Service | | | F | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Unsignalized Intersection Capacity Analysis

5: Hinchey Ave & Parcel 1

Future Total (2023)

PM Peak Hour



| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|------|-------|------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 5 | 0 | 0 | 2 | 7 | 15 |
| Future Volume (Veh/h) | 5 | 0 | 0 | 2 | 7 | 15 |
| Sign Control | Free | Free | | Stop | | |
| Grade | 0% | 0% | | 0% | | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 5 | 0 | 0 | 2 | 7 | 15 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | None | | | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 2 | | | 11 | 1 | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 2 | | | 11 | 1 | |
| tC, single (s) | 4.1 | | | 6.4 | 6.2 | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 2.2 | | | 3.5 | 3.3 | |
| p0 queue free % | 100 | | | 99 | 99 | |
| cM capacity (veh/h) | 1620 | | | 1006 | 1084 | |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total | 5 | 2 | 22 | | | |
| Volume Left | 5 | 0 | 7 | | | |
| Volume Right | 0 | 2 | 15 | | | |
| cSH | 1620 | 1700 | 1058 | | | |
| Volume to Capacity | 0.00 | 0.00 | 0.02 | | | |
| Queue Length 95th (m) | 0.1 | 0.0 | 0.4 | | | |
| Control Delay (s) | 7.2 | 0.0 | 8.5 | | | |
| Lane LOS | A | | A | | | |
| Approach Delay (s) | 7.2 | 0.0 | 8.5 | | | |
| Approach LOS | | | A | | | |
| Intersection Summary | | | | | | |
| Average Delay | | 7.7 | | | | |
| Intersection Capacity Utilization | | 14.4% | | ICU Level of Service | | A |
| Analysis Period (min) | | 15 | | | | |

HCM Unsignalized Intersection Capacity Analysis
6: Hinckley Ave & Parcel 2

Future Total (2023)
PM Peak Hour

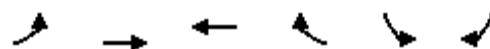
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|------|-------|------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 20 | 0 | 2 | 7 | 0 | 7 |
| Future Volume (Veh/h) | 20 | 0 | 2 | 7 | 0 | 7 |
| Sign Control | Stop | | Free | | | Free |
| Grade | 0% | | 0% | | | 0% |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 20 | 0 | 2 | 7 | 0 | 7 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | | | None | | | None |
| Median storage veh) | | | | | | |
| Upstream signal (m) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 12 | 6 | | | 9 | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 12 | 6 | | | 9 | |
| tC, single (s) | 6.4 | 6.2 | | | 4.1 | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 3.5 | 3.3 | | | 2.2 | |
| p0 queue free % | 98 | 100 | | | 100 | |
| cM capacity (veh/h) | 1007 | 1077 | | | 1611 | |
| Direction, Lane # | WB 1 | NB 1 | SB 1 | | | |
| Volume Total | 20 | 9 | 7 | | | |
| Volume Left | 20 | 0 | 0 | | | |
| Volume Right | 0 | 7 | 0 | | | |
| cSH | 1007 | 1700 | 1611 | | | |
| Volume to Capacity | 0.02 | 0.01 | 0.00 | | | |
| Queue Length 95th (m) | 0.4 | 0.0 | 0.0 | | | |
| Control Delay (s) | 8.6 | 0.0 | 0.0 | | | |
| Lane LOS | A | | | | | |
| Approach Delay (s) | 8.6 | 0.0 | 0.0 | | | |
| Approach LOS | A | | | | | |
| Intersection Summary | | | | | | |
| Average Delay | | 4.8 | | | | |
| Intersection Capacity Utilization | | 13.3% | | ICU Level of Service | | A |
| Analysis Period (min) | | 15 | | | | |

HCM Unsignalized Intersection Capacity Analysis

7: Burnside Ave & Parcel 3

Future Total (2023)

PM Peak Hour



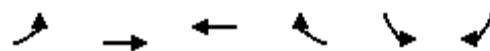
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|------|-------|------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 5 | 130 | 389 | 2 | 5 | 15 |
| Future Volume (Veh/h) | 5 | 130 | 389 | 2 | 5 | 15 |
| Sign Control | Free | Free | | Stop | | |
| Grade | 0% | 0% | | 0% | | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 5 | 130 | 389 | 2 | 5 | 15 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | None | | | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | | 201 | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 391 | | | 530 | 390 | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 391 | | | 530 | 390 | |
| tC, single (s) | 4.1 | | | 6.4 | 6.2 | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 2.2 | | | 3.5 | 3.3 | |
| p0 queue free % | 100 | | | 99 | 98 | |
| cM capacity (veh/h) | 1168 | | | 507 | 658 | |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total | 135 | 391 | 20 | | | |
| Volume Left | 5 | 0 | 5 | | | |
| Volume Right | 0 | 2 | 15 | | | |
| cSH | 1168 | 1700 | 613 | | | |
| Volume to Capacity | 0.00 | 0.23 | 0.03 | | | |
| Queue Length 95th (m) | 0.1 | 0.0 | 0.7 | | | |
| Control Delay (s) | 0.3 | 0.0 | 11.1 | | | |
| Lane LOS | A | | B | | | |
| Approach Delay (s) | 0.3 | 0.0 | 11.1 | | | |
| Approach LOS | | | B | | | |
| Intersection Summary | | | | | | |
| Average Delay | | 0.5 | | | | |
| Intersection Capacity Utilization | | 31.7% | | ICU Level of Service | | A |
| Analysis Period (min) | | 15 | | | | |

HCM Unsignalized Intersection Capacity Analysis

8: Burnside Ave & Parcel 4

Future Total (2023)

PM Peak Hour



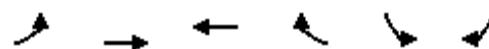
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|------|-------|------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 5 | 130 | 376 | 2 | 7 | 15 |
| Future Volume (Veh/h) | 5 | 130 | 376 | 2 | 7 | 15 |
| Sign Control | Free | Free | | Stop | | |
| Grade | 0% | 0% | | 0% | | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 5 | 130 | 376 | 2 | 7 | 15 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | None | | | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | | 256 | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 378 | | | 517 | 377 | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 378 | | | 517 | 377 | |
| tC, single (s) | 4.1 | | | 6.4 | 6.2 | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 2.2 | | | 3.5 | 3.3 | |
| p0 queue free % | 100 | | | 99 | 98 | |
| cM capacity (veh/h) | 1180 | | | 516 | 670 | |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total | 135 | 378 | 22 | | | |
| Volume Left | 5 | 0 | 7 | | | |
| Volume Right | 0 | 2 | 15 | | | |
| cSH | 1180 | 1700 | 612 | | | |
| Volume to Capacity | 0.00 | 0.22 | 0.04 | | | |
| Queue Length 95th (m) | 0.1 | 0.0 | 0.8 | | | |
| Control Delay (s) | 0.3 | 0.0 | 11.1 | | | |
| Lane LOS | A | | B | | | |
| Approach Delay (s) | 0.3 | 0.0 | 11.1 | | | |
| Approach LOS | | | B | | | |
| Intersection Summary | | | | | | |
| Average Delay | | 0.5 | | | | |
| Intersection Capacity Utilization | | 31.0% | | ICU Level of Service | | A |
| Analysis Period (min) | | 15 | | | | |

HCM Unsignalized Intersection Capacity Analysis

9: Burnside Ave & Parcel 5

Future Total (2023)

PM Peak Hour



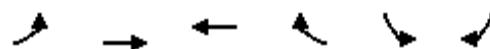
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|------|-------|------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 4 | 133 | 364 | 2 | 5 | 14 |
| Future Volume (Veh/h) | 4 | 133 | 364 | 2 | 5 | 14 |
| Sign Control | Free | Free | | Stop | | |
| Grade | 0% | 0% | | 0% | | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 4 | 133 | 364 | 2 | 5 | 14 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | | None | None | | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | | 298 | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 366 | | | 506 | 365 | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 366 | | | 506 | 365 | |
| tC, single (s) | 4.1 | | | 6.4 | 6.2 | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 2.2 | | | 3.5 | 3.3 | |
| p0 queue free % | 100 | | | 99 | 98 | |
| cM capacity (veh/h) | 1193 | | | 524 | 680 | |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total | 137 | 366 | 19 | | | |
| Volume Left | 4 | 0 | 5 | | | |
| Volume Right | 0 | 2 | 14 | | | |
| cSH | 1193 | 1700 | 631 | | | |
| Volume to Capacity | 0.00 | 0.22 | 0.03 | | | |
| Queue Length 95th (m) | 0.1 | 0.0 | 0.7 | | | |
| Control Delay (s) | 0.3 | 0.0 | 10.9 | | | |
| Lane LOS | A | B | | | | |
| Approach Delay (s) | 0.3 | 0.0 | 10.9 | | | |
| Approach LOS | | B | | | | |
| Intersection Summary | | | | | | |
| Average Delay | | 0.5 | | | | |
| Intersection Capacity Utilization | | 30.4% | | ICU Level of Service | | A |
| Analysis Period (min) | | 15 | | | | |

HCM Unsignalized Intersection Capacity Analysis

10: Burnside Ave & Parcel 6

Future Total (2023)

PM Peak Hour



| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|------|-------|----------------------|------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 5 | 133 | 351 | 2 | 5 | 15 |
| Future Volume (Veh/h) | 5 | 133 | 351 | 2 | 5 | 15 |
| Sign Control | Free | Free | | Stop | | |
| Grade | 0% | 0% | | 0% | | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 5 | 133 | 351 | 2 | 5 | 15 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | None | | | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | | 344 | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 353 | | | 495 | 352 | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 353 | | | 495 | 352 | |
| tC, single (s) | 4.1 | | | 6.4 | 6.2 | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 2.2 | | | 3.5 | 3.3 | |
| p0 queue free % | 100 | | | 99 | 98 | |
| cM capacity (veh/h) | 1206 | | | 532 | 692 | |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total | 138 | 353 | 20 | | | |
| Volume Left | 5 | 0 | 5 | | | |
| Volume Right | 0 | 2 | 15 | | | |
| cSH | 1206 | 1700 | 643 | | | |
| Volume to Capacity | 0.00 | 0.21 | 0.03 | | | |
| Queue Length 95th (m) | 0.1 | 0.0 | 0.7 | | | |
| Control Delay (s) | 0.3 | 0.0 | 10.8 | | | |
| Lane LOS | A | B | | | | |
| Approach Delay (s) | 0.3 | 0.0 | 10.8 | | | |
| Approach LOS | | B | | | | |
| Intersection Summary | | | | | | |
| Average Delay | | 0.5 | | | | |
| Intersection Capacity Utilization | | 29.6% | ICU Level of Service | | A | |
| Analysis Period (min) | | 15 | | | | |

HCM Signalized Intersection Capacity Analysis

1: Parkdale Ave & Burnside Ave

Future Total (2028)

AM Peak Hour



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|------------------------|-------|------|------|-------|------|-------|
| Lane Configurations | | | | | | |
| Traffic Volume (vph) | 101 | 140 | 394 | 91 | 370 | 604 |
| Future Volume (vph) | 101 | 140 | 394 | 91 | 370 | 604 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 4.2 | 3.7 | 4.8 | 3.7 | 3.7 | 4.8 |
| Total Lost time (s) | 5.4 | | 5.2 | | | 5.2 |
| Lane Util. Factor | 1.00 | | 1.00 | | | 1.00 |
| Frpb, ped/bikes | 0.80 | | 0.99 | | | 1.00 |
| Flpb, ped/bikes | 1.00 | | 1.00 | | | 1.00 |
| Fr _t | 0.92 | | 0.97 | | | 1.00 |
| Flt Protected | 0.98 | | 1.00 | | | 0.98 |
| Satd. Flow (prot) | 1313 | | 1931 | | | 1956 |
| Flt Permitted | 0.98 | | 1.00 | | | 0.61 |
| Satd. Flow (perm) | 1313 | | 1931 | | | 1223 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 101 | 140 | 394 | 91 | 370 | 604 |
| RTOR Reduction (vph) | 87 | 0 | 13 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 154 | 0 | 472 | 0 | 0 | 974 |
| Confl. Peds. (#/hr) | 67 | 154 | | 14 | 14 | |
| Confl. Bikes (#/hr) | | 5 | | 6 | | |
| Heavy Vehicles (%) | 0% | 9% | 1% | 7% | 2% | 2% |
| Turn Type | pm+pt | | NA | | Perm | NA |
| Protected Phases | 3 | | 2 | | | 6 |
| Permitted Phases | 8 | | | 6 | | |
| Actuated Green, G (s) | 12.6 | | 36.8 | | | 36.8 |
| Effective Green, g (s) | 12.6 | | 36.8 | | | 36.8 |
| Actuated g/C Ratio | 0.21 | | 0.61 | | | 0.61 |
| Clearance Time (s) | 5.4 | | 5.2 | | | 5.2 |
| Vehicle Extension (s) | 3.0 | | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | 275 | | 1184 | | | 750 |
| v/s Ratio Prot | c0.12 | | 0.24 | | | |
| v/s Ratio Perm | | | | c0.80 | | |
| v/c Ratio | 0.56 | | 0.40 | | | 1.30 |
| Uniform Delay, d1 | 21.2 | | 5.9 | | | 11.6 |
| Progression Factor | 1.00 | | 1.00 | | | 1.00 |
| Incremental Delay, d2 | 2.6 | | 1.0 | | | 144.1 |
| Delay (s) | 23.8 | | 6.9 | | | 155.7 |
| Level of Service | C | | A | | | F |
| Approach Delay (s) | 23.8 | | 6.9 | | | 155.7 |
| Approach LOS | C | | A | | | F |

Intersection Summary

| | | | |
|-----------------------------------|--------|---------------------------|------|
| HCM 2000 Control Delay | 94.6 | HCM 2000 Level of Service | F |
| HCM 2000 Volume to Capacity ratio | 1.11 | | |
| Actuated Cycle Length (s) | 60.0 | Sum of lost time (s) | 10.6 |
| Intersection Capacity Utilization | 115.5% | ICU Level of Service | H |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
2: Slidell St/Onigam St & Sir John A MacDonald Pkwy

Future Total (2028)
AM Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBL | SBT |
|-----------------------------------|-------|------|------|------|---------------------------|------|------|------|-------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 0 | 1842 | 27 | 1 | 1317 | 1 | 1 | 1 | 26 | 1 | 1 | 6 |
| Future Volume (vph) | 0 | 1842 | 27 | 1 | 1317 | 1 | 1 | 1 | 26 | 1 | 1 | 6 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 3.7 | 3.8 | 3.7 | 3.7 | 3.8 | 3.7 | 3.7 | 3.7 | 3.9 | 3.7 | 3.7 | 4.0 |
| Total Lost time (s) | | 5.5 | | | 5.5 | | | | 6.3 | | | 6.3 |
| Lane Util. Factor | 0.95 | | | | 0.95 | | | | 1.00 | | | 1.00 |
| Frpb, ped/bikes | 1.00 | | | | 1.00 | | | | 1.00 | | | 0.99 |
| Flpb, ped/bikes | 1.00 | | | | 1.00 | | | | 1.00 | | | 1.00 |
| Fr _t | 1.00 | | | | 1.00 | | | | 1.00 | | | 0.95 |
| Flt Protected | 1.00 | | | | 1.00 | | | | 1.00 | | | 1.00 |
| Satd. Flow (prot) | 3487 | | | | 3461 | | | | 1841 | | | 1757 |
| Flt Permitted | 1.00 | | | | 0.95 | | | | 0.98 | | | 0.97 |
| Satd. Flow (perm) | 3487 | | | | 3302 | | | | 1809 | | | 1716 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 0 | 1842 | 27 | 1 | 1317 | 1 | 1 | 1 | 26 | 1 | 1 | 6 |
| RTOR Reduction (vph) | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 4 |
| Lane Group Flow (vph) | 0 | 1868 | 0 | 0 | 1319 | 0 | 0 | 0 | 28 | 0 | 0 | 7 |
| Confl. Peds. (#/hr) | 2 | | 1 | 1 | | 2 | 1 | 4 | | 5 | 5 | |
| Confl. Bikes (#/hr) | | | 1 | | | | | | | 15 | | |
| Heavy Vehicles (%) | 0% | 0% | 0% | 0% | 1% | 0% | 0% | 0% | 0% | 0% | 0% | 0% |
| Turn Type | | NA | | Perm | NA | | Perm | Perm | NA | | Perm | NA |
| Protected Phases | | 2 | | | 6 | | | | 8 | | | 4 |
| Permitted Phases | 2 | | | 6 | | | 8 | 8 | | | 4 | |
| Actuated Green, G (s) | 73.8 | | | 73.8 | | | | | 9.4 | | | 9.4 |
| Effective Green, g (s) | 73.8 | | | 73.8 | | | | | 9.4 | | | 9.4 |
| Actuated g/C Ratio | 0.78 | | | 0.78 | | | | | 0.10 | | | 0.10 |
| Clearance Time (s) | 5.5 | | | 5.5 | | | | | 6.3 | | | 6.3 |
| Vehicle Extension (s) | 3.0 | | | 3.0 | | | | | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | 2708 | | | 2565 | | | | | 178 | | | 169 |
| v/s Ratio Prot | c0.54 | | | | | | | | | | | |
| v/s Ratio Perm | | | | 0.40 | | | | | c0.02 | | | 0.00 |
| v/c Ratio | 0.69 | | | 0.51 | | | | | 0.16 | | | 0.04 |
| Uniform Delay, d1 | 5.1 | | | 3.9 | | | | | 39.2 | | | 38.7 |
| Progression Factor | 1.00 | | | 1.00 | | | | | 1.00 | | | 1.00 |
| Incremental Delay, d2 | 1.5 | | | 0.7 | | | | | 0.4 | | | 0.1 |
| Delay (s) | 6.6 | | | 4.7 | | | | | 39.6 | | | 38.8 |
| Level of Service | A | | | A | | | | | D | | | D |
| Approach Delay (s) | 6.6 | | | 4.7 | | | | | 39.6 | | | 38.8 |
| Approach LOS | A | | | A | | | | | D | | | D |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | 6.2 | | | | HCM 2000 Level of Service | | | | A | | | |
| HCM 2000 Volume to Capacity ratio | 0.63 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 95.0 | | | | Sum of lost time (s) | | | | 11.8 | | | |
| Intersection Capacity Utilization | 75.0% | | | | ICU Level of Service | | | | D | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis
2: Slidell St/Onigam St & Sir John A MacDonald Pkwy

Future Total (2028)
AM Peak Hour

| Movement | SBR |
|------------------------|------|
| Lane Configurations | |
| Traffic Volume (vph) | 4 |
| Future Volume (vph) | 4 |
| Ideal Flow (vphpl) | 1800 |
| Lane Width | 3.7 |
| Total Lost time (s) | |
| Lane Util. Factor | |
| Frpb, ped/bikes | |
| Flpb, ped/bikes | |
| Fr | |
| Flt Protected | |
| Satd. Flow (prot) | |
| Flt Permitted | |
| Satd. Flow (perm) | |
| Peak-hour factor, PHF | 1.00 |
| Adj. Flow (vph) | 4 |
| RTOR Reduction (vph) | 0 |
| Lane Group Flow (vph) | 0 |
| Confl. Peds. (#/hr) | 4 |
| Confl. Bikes (#/hr) | 8 |
| Heavy Vehicles (%) | 0% |
| Turn Type | |
| Protected Phases | |
| Permitted Phases | |
| Actuated Green, G (s) | |
| Effective Green, g (s) | |
| Actuated g/C Ratio | |
| Clearance Time (s) | |
| Vehicle Extension (s) | |
| Lane Grp Cap (vph) | |
| v/s Ratio Prot | |
| v/s Ratio Perm | |
| v/c Ratio | |
| Uniform Delay, d1 | |
| Progression Factor | |
| Incremental Delay, d2 | |
| Delay (s) | |
| Level of Service | |
| Approach Delay (s) | |
| Approach LOS | |
| Intersection Summary | |

HCM Signalized Intersection Capacity Analysis

3: Bayview Stn Rd & Scott St/Albert St

Future Total (2028)

AM Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|--------|------|------|------|---------------------------|------|------|------|-------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 53 | 861 | 96 | 67 | 389 | 74 | 54 | 123 | 160 | 193 | 276 | 38 |
| Future Volume (vph) | 53 | 861 | 96 | 67 | 389 | 74 | 54 | 123 | 160 | 193 | 276 | 38 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 3.7 | 3.6 | 3.7 | 3.2 | 3.5 | 3.8 | 3.0 | 4.3 | 3.7 | 3.3 | 4.5 | 3.7 |
| Total Lost time (s) | 6.5 | | 6.5 | 6.5 | 6.5 | 6.4 | 6.4 | | 6.4 | 6.4 | | |
| Lane Util. Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | |
| Frpb, ped/bikes | 0.99 | | 1.00 | 1.00 | 0.78 | 1.00 | 0.92 | | 1.00 | 0.98 | | |
| Flpb, ped/bikes | 0.99 | | 0.98 | 1.00 | 1.00 | 0.93 | 1.00 | | 0.96 | 1.00 | | |
| Fr _t | 0.99 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.92 | | 1.00 | 0.98 | | |
| Fl _t Protected | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | |
| Satd. Flow (prot) | 1420 | | 1573 | 1338 | 1133 | 1320 | 1581 | | 1531 | 1837 | | |
| Fl _t Permitted | 0.96 | | 0.26 | 1.00 | 1.00 | 0.37 | 1.00 | | 0.42 | 1.00 | | |
| Satd. Flow (perm) | 1366 | | 426 | 1338 | 1133 | 510 | 1581 | | 676 | 1837 | | |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 53 | 861 | 96 | 67 | 389 | 74 | 54 | 123 | 160 | 193 | 276 | 38 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 | 0 | 29 | 0 | 47 | 0 | 0 | 5 | 0 |
| Lane Group Flow (vph) | 0 | 1006 | 0 | 67 | 389 | 45 | 54 | 236 | 0 | 193 | 309 | 0 |
| Confl. Peds. (#/hr) | 108 | | 57 | 57 | | 108 | 64 | | 33 | 33 | | 64 |
| Confl. Bikes (#/hr) | | | 2 | | | 3 | | | 43 | | | 13 |
| Heavy Vehicles (%) | 0% | 26% | 4% | 2% | 33% | 7% | 13% | 4% | 3% | 4% | 2% | 17% |
| Turn Type | Perm | NA | | Perm | NA | Perm | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | 6 | 8 | | | 4 | | |
| Actuated Green, G (s) | 61.1 | | 61.1 | 61.1 | 61.1 | 26.0 | 26.0 | | 26.0 | 26.0 | | |
| Effective Green, g (s) | 61.1 | | 61.1 | 61.1 | 61.1 | 26.0 | 26.0 | | 26.0 | 26.0 | | |
| Actuated g/C Ratio | 0.61 | | 0.61 | 0.61 | 0.61 | 0.26 | 0.26 | | 0.26 | 0.26 | | |
| Clearance Time (s) | 6.5 | | 6.5 | 6.5 | 6.5 | 6.4 | 6.4 | | 6.4 | 6.4 | | |
| Vehicle Extension (s) | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | |
| Lane Grp Cap (vph) | 834 | | 260 | 817 | 692 | 132 | 411 | | 175 | 477 | | |
| v/s Ratio Prot | | | | 0.29 | | | | 0.15 | | | 0.17 | |
| v/s Ratio Perm | c0.74 | | 0.16 | | 0.04 | 0.11 | | | c0.29 | | | |
| v/c Ratio | 1.21 | | 0.26 | 0.48 | 0.07 | 0.41 | 0.58 | | 1.10 | 0.65 | | |
| Uniform Delay, d1 | 19.4 | | 9.0 | 10.7 | 7.9 | 30.6 | 32.2 | | 37.0 | 32.9 | | |
| Progression Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | |
| Incremental Delay, d2 | 104.1 | | 2.4 | 2.0 | 0.2 | 2.1 | 1.9 | | 98.2 | 3.0 | | |
| Delay (s) | 123.6 | | 11.4 | 12.7 | 8.1 | 32.7 | 34.1 | | 135.2 | 35.9 | | |
| Level of Service | F | | B | B | A | C | C | | F | D | | |
| Approach Delay (s) | 123.6 | | | | 11.9 | | | 33.9 | | | 73.7 | |
| Approach LOS | F | | | | B | | | C | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | 75.5 | | | | HCM 2000 Level of Service | | | E | | | | |
| HCM 2000 Volume to Capacity ratio | 1.17 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 100.0 | | | | Sum of lost time (s) | | | 12.9 | | | | |
| Intersection Capacity Utilization | 132.7% | | | | ICU Level of Service | | | H | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Unsignalized Intersection Capacity Analysis
4: Bayview Stn Rd/Slidell St & Burnside Ave

Future Total (2028)
AM Peak Hour

| Movement | EBU | EBL | EBC | NBU | NBL | NBT | SBT | SBR | | | | | |
|-----------------------------------|-------|------|----------------------|------|------|------|------|------|--|--|--|--|--|
| Right Turn Channelized | | | | | | | | | | | | | |
| Traffic Volume (veh/h) | 1 | 21 | 403 | 2 | 133 | 19 | 66 | 6 | | | | | |
| Future Volume (veh/h) | 1 | 21 | 403 | 2 | 133 | 19 | 66 | 6 | | | | | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | | |
| Hourly flow rate (vph) | 1 | 21 | 403 | 2 | 133 | 19 | 66 | 6 | | | | | |
| Approach Volume (veh/h) | 425 | | | 154 | | 72 | | | | | | | |
| Crossing Volume (veh/h) | 68 | | | 22 | | 136 | | | | | | | |
| High Capacity (veh/h) | 1313 | | | 1361 | | 1245 | | | | | | | |
| High v/c (veh/h) | 0.32 | | | 0.11 | | 0.06 | | | | | | | |
| Low Capacity (veh/h) | 1096 | | | 1140 | | 1034 | | | | | | | |
| Low v/c (veh/h) | 0.39 | | | 0.14 | | 0.07 | | | | | | | |
| Intersection Summary | | | | | | | | | | | | | |
| Maximum v/c High | 0.32 | | | | | | | | | | | | |
| Maximum v/c Low | 0.39 | | | | | | | | | | | | |
| Intersection Capacity Utilization | 53.2% | | ICU Level of Service | | | A | | | | | | | |

HCM Unsignalized Intersection Capacity Analysis
5: Hinckley Ave & Parcel 1

Future Total (2028)
AM Peak Hour

| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|------|-------|------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 26 | 0 | 0 | 12 | 5 | 7 |
| Future Volume (Veh/h) | 26 | 0 | 0 | 12 | 5 | 7 |
| Sign Control | | Free | Free | | Stop | |
| Grade | | 0% | 0% | | 0% | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 26 | 0 | 0 | 12 | 5 | 7 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | | None | None | | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 12 | | | 58 | 6 | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 12 | | | 58 | 6 | |
| tC, single (s) | 4.1 | | | 6.4 | 6.2 | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 2.2 | | | 3.5 | 3.3 | |
| p0 queue free % | 98 | | | 99 | 99 | |
| cM capacity (veh/h) | 1607 | | | 934 | 1077 | |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total | 26 | 12 | 12 | | | |
| Volume Left | 26 | 0 | 5 | | | |
| Volume Right | 0 | 12 | 7 | | | |
| cSH | 1607 | 1700 | 1012 | | | |
| Volume to Capacity | 0.02 | 0.01 | 0.01 | | | |
| Queue Length 95th (m) | 0.3 | 0.0 | 0.3 | | | |
| Control Delay (s) | 7.3 | 0.0 | 8.6 | | | |
| Lane LOS | A | | A | | | |
| Approach Delay (s) | 7.3 | 0.0 | 8.6 | | | |
| Approach LOS | | | A | | | |
| Intersection Summary | | | | | | |
| Average Delay | | 5.8 | | | | |
| Intersection Capacity Utilization | | 18.2% | | ICU Level of Service | | A |
| Analysis Period (min) | | 15 | | | | |

HCM Unsignalized Intersection Capacity Analysis
6: Hinckley Ave & Parcel 2

Future Total (2028)
AM Peak Hour

| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|------|-------|------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 11 | 0 | 12 | 35 | 0 | 5 |
| Future Volume (Veh/h) | 11 | 0 | 12 | 35 | 0 | 5 |
| Sign Control | Stop | | Free | | | Free |
| Grade | 0% | | 0% | | | 0% |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 11 | 0 | 12 | 35 | 0 | 5 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | | | None | | | None |
| Median storage veh) | | | | | | |
| Upstream signal (m) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 34 | 30 | | | 47 | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 34 | 30 | | | 47 | |
| tC, single (s) | 6.4 | 6.2 | | | 4.1 | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 3.5 | 3.3 | | | 2.2 | |
| p0 queue free % | 99 | 100 | | | 100 | |
| cM capacity (veh/h) | 979 | 1045 | | | 1560 | |
| Direction, Lane # | WB 1 | NB 1 | SB 1 | | | |
| Volume Total | 11 | 47 | 5 | | | |
| Volume Left | 11 | 0 | 0 | | | |
| Volume Right | 0 | 35 | 0 | | | |
| cSH | 979 | 1700 | 1560 | | | |
| Volume to Capacity | 0.01 | 0.03 | 0.00 | | | |
| Queue Length 95th (m) | 0.2 | 0.0 | 0.0 | | | |
| Control Delay (s) | 8.7 | 0.0 | 0.0 | | | |
| Lane LOS | A | | | | | |
| Approach Delay (s) | 8.7 | 0.0 | 0.0 | | | |
| Approach LOS | A | | | | | |
| Intersection Summary | | | | | | |
| Average Delay | | 1.5 | | | | |
| Intersection Capacity Utilization | | 13.3% | | ICU Level of Service | | A |
| Analysis Period (min) | | 15 | | | | |

HCM Unsignalized Intersection Capacity Analysis
7: Burnside Ave & Parcel 3

Future Total (2028)
AM Peak Hour

| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|------|-------|------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 23 | 479 | 114 | 12 | 4 | 7 |
| Future Volume (Veh/h) | 23 | 479 | 114 | 12 | 4 | 7 |
| Sign Control | | Free | Free | | Stop | |
| Grade | | 0% | 0% | | 0% | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 23 | 479 | 114 | 12 | 4 | 7 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | | None | None | | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | | 201 | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 126 | | | 645 | 120 | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 126 | | | 645 | 120 | |
| tC, single (s) | 4.1 | | | 6.4 | 6.2 | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 2.2 | | | 3.5 | 3.3 | |
| p0 queue free % | 98 | | | 99 | 99 | |
| cM capacity (veh/h) | 1460 | | | 430 | 931 | |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total | 502 | 126 | 11 | | | |
| Volume Left | 23 | 0 | 4 | | | |
| Volume Right | 0 | 12 | 7 | | | |
| cSH | 1460 | 1700 | 654 | | | |
| Volume to Capacity | 0.02 | 0.07 | 0.02 | | | |
| Queue Length 95th (m) | 0.3 | 0.0 | 0.4 | | | |
| Control Delay (s) | 0.5 | 0.0 | 10.6 | | | |
| Lane LOS | A | | B | | | |
| Approach Delay (s) | 0.5 | 0.0 | 10.6 | | | |
| Approach LOS | | | B | | | |
| Intersection Summary | | | | | | |
| Average Delay | | 0.6 | | | | |
| Intersection Capacity Utilization | | 48.4% | | ICU Level of Service | | A |
| Analysis Period (min) | | 15 | | | | |

HCM Unsignalized Intersection Capacity Analysis
8: Burnside Ave & Parcel 4

Future Total (2028)
AM Peak Hour

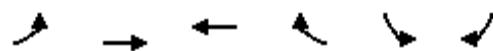
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|------|-------|------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 26 | 457 | 119 | 12 | 5 | 7 |
| Future Volume (Veh/h) | 26 | 457 | 119 | 12 | 5 | 7 |
| Sign Control | | Free | Free | | Stop | |
| Grade | | 0% | 0% | | 0% | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 26 | 457 | 119 | 12 | 5 | 7 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | | None | None | | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | | 256 | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 131 | | | 634 | 125 | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 131 | | | 634 | 125 | |
| tC, single (s) | 4.1 | | | 6.4 | 6.2 | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 2.2 | | | 3.5 | 3.3 | |
| p0 queue free % | 98 | | | 99 | 99 | |
| cM capacity (veh/h) | 1454 | | | 435 | 926 | |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total | 483 | 131 | 12 | | | |
| Volume Left | 26 | 0 | 5 | | | |
| Volume Right | 0 | 12 | 7 | | | |
| cSH | 1454 | 1700 | 630 | | | |
| Volume to Capacity | 0.02 | 0.08 | 0.02 | | | |
| Queue Length 95th (m) | 0.4 | 0.0 | 0.4 | | | |
| Control Delay (s) | 0.6 | 0.0 | 10.8 | | | |
| Lane LOS | A | B | | | | |
| Approach Delay (s) | 0.6 | 0.0 | 10.8 | | | |
| Approach LOS | | B | | | | |
| Intersection Summary | | | | | | |
| Average Delay | | 0.7 | | | | |
| Intersection Capacity Utilization | | 47.6% | | ICU Level of Service | | A |
| Analysis Period (min) | | 15 | | | | |

HCM Unsignalized Intersection Capacity Analysis

9: Burnside Ave & Parcel 5

Future Total (2028)

AM Peak Hour



| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|------|-------|------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 22 | 440 | 124 | 11 | 4 | 7 |
| Future Volume (Veh/h) | 22 | 440 | 124 | 11 | 4 | 7 |
| Sign Control | Free | Free | | Stop | | |
| Grade | 0% | 0% | | 0% | | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 22 | 440 | 124 | 11 | 4 | 7 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | | None | None | | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | | 298 | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 135 | | | 614 | 130 | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 135 | | | 614 | 130 | |
| tC, single (s) | 4.1 | | | 6.4 | 6.2 | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 2.2 | | | 3.5 | 3.3 | |
| p0 queue free % | 98 | | | 99 | 99 | |
| cM capacity (veh/h) | 1449 | | | 449 | 920 | |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total | 462 | 135 | 11 | | | |
| Volume Left | 22 | 0 | 4 | | | |
| Volume Right | 0 | 11 | 7 | | | |
| cSH | 1449 | 1700 | 666 | | | |
| Volume to Capacity | 0.02 | 0.08 | 0.02 | | | |
| Queue Length 95th (m) | 0.3 | 0.0 | 0.4 | | | |
| Control Delay (s) | 0.5 | 0.0 | 10.5 | | | |
| Lane LOS | A | | B | | | |
| Approach Delay (s) | 0.5 | 0.0 | 10.5 | | | |
| Approach LOS | | | B | | | |
| Intersection Summary | | | | | | |
| Average Delay | | 0.6 | | | | |
| Intersection Capacity Utilization | | 46.7% | | ICU Level of Service | | A |
| Analysis Period (min) | | 15 | | | | |

HCM Unsignalized Intersection Capacity Analysis
10: Burnside Ave & Parcel 6

Future Total (2028)
AM Peak Hour

| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|------|-------|------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 23 | 421 | 128 | 12 | 4 | 7 |
| Future Volume (Veh/h) | 23 | 421 | 128 | 12 | 4 | 7 |
| Sign Control | Free | Free | | Stop | | |
| Grade | 0% | 0% | | 0% | | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 23 | 421 | 128 | 12 | 4 | 7 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | None | | | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | 344 | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 140 | | | 601 | 134 | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 140 | | | 601 | 134 | |
| tC, single (s) | 4.1 | | | 6.4 | 6.2 | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 2.2 | | | 3.5 | 3.3 | |
| p0 queue free % | 98 | | | 99 | 99 | |
| cM capacity (veh/h) | 1443 | | | 456 | 915 | |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total | 444 | 140 | 11 | | | |
| Volume Left | 23 | 0 | 4 | | | |
| Volume Right | 0 | 12 | 7 | | | |
| cSH | 1443 | 1700 | 670 | | | |
| Volume to Capacity | 0.02 | 0.08 | 0.02 | | | |
| Queue Length 95th (m) | 0.3 | 0.0 | 0.4 | | | |
| Control Delay (s) | 0.5 | 0.0 | 10.5 | | | |
| Lane LOS | A | | B | | | |
| Approach Delay (s) | 0.5 | 0.0 | 10.5 | | | |
| Approach LOS | | | B | | | |
| Intersection Summary | | | | | | |
| Average Delay | | 0.6 | | | | |
| Intersection Capacity Utilization | | 45.9% | | ICU Level of Service | | A |
| Analysis Period (min) | | 15 | | | | |

HCM Unsignalized Intersection Capacity Analysis
11: Forward Ave & Hinckley Ave

Future Total (2028)
AM Peak Hour

| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|------|-------|------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 7 | 0 | 0 | 26 | 0 | 0 |
| Future Volume (Veh/h) | 7 | 0 | 0 | 26 | 0 | 0 |
| Sign Control | Stop | | Free | | | Free |
| Grade | 0% | | 0% | | | 0% |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 7 | 0 | 0 | 26 | 0 | 0 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | | | None | | | None |
| Median storage veh) | | | | | | |
| Upstream signal (m) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 13 | 13 | | | 26 | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 13 | 13 | | | 26 | |
| tC, single (s) | 6.4 | 6.2 | | | 4.1 | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 3.5 | 3.3 | | | 2.2 | |
| p0 queue free % | 99 | 100 | | | 100 | |
| cM capacity (veh/h) | 1006 | 1067 | | | 1588 | |
| Direction, Lane # | WB 1 | NB 1 | SB 1 | | | |
| Volume Total | 7 | 26 | 0 | | | |
| Volume Left | 7 | 0 | 0 | | | |
| Volume Right | 0 | 26 | 0 | | | |
| cSH | 1006 | 1700 | 1700 | | | |
| Volume to Capacity | 0.01 | 0.02 | 0.00 | | | |
| Queue Length 95th (m) | 0.1 | 0.0 | 0.0 | | | |
| Control Delay (s) | 8.6 | 0.0 | 0.0 | | | |
| Lane LOS | A | | | | | |
| Approach Delay (s) | 8.6 | 0.0 | 0.0 | | | |
| Approach LOS | A | | | | | |
| Intersection Summary | | | | | | |
| Average Delay | | 1.8 | | | | |
| Intersection Capacity Utilization | | 13.3% | | ICU Level of Service | | A |
| Analysis Period (min) | | 15 | | | | |

HCM Unsignalized Intersection Capacity Analysis

12: Forward Ave & Burnside Ave

Future Total (2028)

AM Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|------|----------------------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (veh/h) | 26 | 435 | 0 | 0 | 234 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| Future Volume (Veh/h) | 26 | 435 | 0 | 0 | 234 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| Sign Control | Free | | | | Free | | | Stop | | | Stop | |
| Grade | 0% | | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 26 | 435 | 0 | 0 | 234 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (m) | | | | | | | | | | | | |
| Walking Speed (m/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | | | | |
| Median type | | None | | | | None | | | | | | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (m) | | 81 | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 234 | | | 435 | | | 728 | 721 | 435 | 721 | 721 | 234 |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 234 | | | 435 | | | 728 | 721 | 435 | 721 | 721 | 234 |
| tC, single (s) | 4.1 | | | 4.1 | | | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 2.2 | | | 2.2 | | | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free % | 98 | | | 100 | | | 100 | 100 | 100 | 100 | 100 | 99 |
| cM capacity (veh/h) | 1333 | | | 1125 | | | 331 | 347 | 621 | 337 | 347 | 805 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | SB 1 | | | | | | | | |
| Volume Total | 461 | 234 | 0 | 7 | | | | | | | | |
| Volume Left | 26 | 0 | 0 | 0 | | | | | | | | |
| Volume Right | 0 | 0 | 0 | 7 | | | | | | | | |
| cSH | 1333 | 1125 | 1700 | 805 | | | | | | | | |
| Volume to Capacity | 0.02 | 0.00 | 0.00 | 0.01 | | | | | | | | |
| Queue Length 95th (m) | 0.4 | 0.0 | 0.0 | 0.2 | | | | | | | | |
| Control Delay (s) | 0.6 | 0.0 | 0.0 | 9.5 | | | | | | | | |
| Lane LOS | A | | A | A | | | | | | | | |
| Approach Delay (s) | 0.6 | 0.0 | 0.0 | 9.5 | | | | | | | | |
| Approach LOS | | | A | A | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | 0.5 | | | | | | | | | | |
| Intersection Capacity Utilization | | 52.0% | | | ICU Level of Service | | | | | A | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |

HCM Unsignalized Intersection Capacity Analysis

13: Hinckley Ave & Burnside Ave

Future Total (2028)

AM Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|------|----------------------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (veh/h) | 23 | 493 | 0 | 0 | 97 | 24 | 0 | 0 | 0 | 9 | 0 | 7 |
| Future Volume (Veh/h) | 23 | 493 | 0 | 0 | 97 | 24 | 0 | 0 | 0 | 9 | 0 | 7 |
| Sign Control | Free | | | | Free | | | Stop | | | Stop | |
| Grade | 0% | | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 23 | 493 | 0 | 0 | 97 | 24 | 0 | 0 | 0 | 9 | 0 | 7 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (m) | | | | | | | | | | | | |
| Walking Speed (m/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | | | | |
| Median type | | None | | | | None | | | | | | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (m) | | 159 | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 121 | | | 493 | | | 655 | 660 | 493 | 648 | 648 | 109 |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 121 | | | 493 | | | 655 | 660 | 493 | 648 | 648 | 109 |
| tC, single (s) | 4.1 | | | 4.1 | | | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 2.2 | | | 2.2 | | | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free % | 98 | | | 100 | | | 100 | 100 | 100 | 98 | 100 | 99 |
| cM capacity (veh/h) | 1467 | | | 1071 | | | 372 | 377 | 576 | 379 | 383 | 945 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | SB 1 | | | | | | | | |
| Volume Total | 516 | 121 | 0 | 16 | | | | | | | | |
| Volume Left | 23 | 0 | 0 | 9 | | | | | | | | |
| Volume Right | 0 | 24 | 0 | 7 | | | | | | | | |
| cSH | 1467 | 1071 | 1700 | 513 | | | | | | | | |
| Volume to Capacity | 0.02 | 0.00 | 0.00 | 0.03 | | | | | | | | |
| Queue Length 95th (m) | 0.3 | 0.0 | 0.0 | 0.7 | | | | | | | | |
| Control Delay (s) | 0.5 | 0.0 | 0.0 | 12.2 | | | | | | | | |
| Lane LOS | A | | A | B | | | | | | | | |
| Approach Delay (s) | 0.5 | 0.0 | 0.0 | 12.2 | | | | | | | | |
| Approach LOS | | | A | B | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 0.7 | | | | | | | | | |
| Intersection Capacity Utilization | | 49.0% | | | ICU Level of Service | | | | A | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

1: Parkdale Ave & Burnside Ave

Future Total (2028)

PM Peak Hour



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|--------|------|---------------------------|-------|------|-------|
| Lane Configurations | | | | | | |
| Traffic Volume (vph) | 66 | 521 | 860 | 86 | 113 | 559 |
| Future Volume (vph) | 66 | 521 | 860 | 86 | 113 | 559 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 4.2 | 3.7 | 4.8 | 3.7 | 3.7 | 4.8 |
| Total Lost time (s) | 5.4 | | 5.2 | | | 5.2 |
| Lane Util. Factor | 1.00 | | 1.00 | | | 1.00 |
| Frpb, ped/bikes | 0.76 | | 1.00 | | | 1.00 |
| Flpb, ped/bikes | 1.00 | | 1.00 | | | 1.00 |
| Fr _t | 0.88 | | 0.99 | | | 1.00 |
| Flt Protected | 0.99 | | 1.00 | | | 0.99 |
| Satd. Flow (prot) | 1271 | | 1970 | | | 1990 |
| Flt Permitted | 0.99 | | 1.00 | | | 0.32 |
| Satd. Flow (perm) | 1271 | | 1970 | | | 635 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 66 | 521 | 860 | 86 | 113 | 559 |
| RTOR Reduction (vph) | 98 | 0 | 5 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 489 | 0 | 941 | 0 | 0 | 672 |
| Confl. Peds. (#/hr) | 37 | 101 | | 19 | 19 | |
| Confl. Bikes (#/hr) | | 7 | | 1 | | |
| Heavy Vehicles (%) | 0% | 0% | 1% | 10% | 0% | 2% |
| Turn Type | pm+pt | | NA | | Perm | NA |
| Protected Phases | 3 | | 2 | | | 6 |
| Permitted Phases | 8 | | | 6 | | |
| Actuated Green, G (s) | 19.6 | | 39.8 | | | 39.8 |
| Effective Green, g (s) | 19.6 | | 39.8 | | | 39.8 |
| Actuated g/C Ratio | 0.28 | | 0.57 | | | 0.57 |
| Clearance Time (s) | 5.4 | | 5.2 | | | 5.2 |
| Vehicle Extension (s) | 3.0 | | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | 355 | | 1120 | | | 361 |
| v/s Ratio Prot | c0.38 | | 0.48 | | | |
| v/s Ratio Perm | | | | c1.06 | | |
| v/c Ratio | 1.38 | | 0.84 | | | 1.86 |
| Uniform Delay, d1 | 25.2 | | 12.5 | | | 15.1 |
| Progression Factor | 1.00 | | 1.00 | | | 1.00 |
| Incremental Delay, d2 | 186.8 | | 7.6 | | | 398.2 |
| Delay (s) | 212.0 | | 20.1 | | | 413.3 |
| Level of Service | F | | C | | | F |
| Approach Delay (s) | 212.0 | | 20.1 | | | 413.3 |
| Approach LOS | F | | C | | | F |
| Intersection Summary | | | | | | |
| HCM 2000 Control Delay | 191.0 | | HCM 2000 Level of Service | | F | |
| HCM 2000 Volume to Capacity ratio | 1.70 | | | | | |
| Actuated Cycle Length (s) | 70.0 | | Sum of lost time (s) | | 10.6 | |
| Intersection Capacity Utilization | 147.4% | | ICU Level of Service | | H | |
| Analysis Period (min) | 15 | | | | | |
| c Critical Lane Group | | | | | | |

HCM Signalized Intersection Capacity Analysis
2: Slidell St/Onigam St & Sir John A MacDonald Pkwy

Future Total (2028)
PM Peak Hour

| Movement | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
|-----------------------------------|-------|------|------|------|------|---------------------------|------|------|-------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 0 | 1273 | 5 | 2 | 2 | 2127 | 0 | 33 | 18 | 43 | 4 | 33 |
| Future Volume (vph) | 0 | 1273 | 5 | 2 | 2 | 2127 | 0 | 33 | 18 | 43 | 4 | 33 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 3.7 | 3.8 | 3.7 | 3.7 | 3.7 | 3.8 | 3.7 | 3.7 | 3.9 | 3.7 | 3.7 | 4.0 |
| Total Lost time (s) | | 5.5 | | | | 5.5 | | | 6.3 | | | 6.3 |
| Lane Util. Factor | 0.95 | | | | | 0.95 | | | 1.00 | | | 1.00 |
| Frpb, ped/bikes | 1.00 | | | | | 1.00 | | | 0.99 | | | 0.99 |
| Flpb, ped/bikes | 1.00 | | | | | 1.00 | | | 1.00 | | | 1.00 |
| Fr _t | 1.00 | | | | | 1.00 | | | 0.94 | | | 0.96 |
| Flt Protected | 1.00 | | | | | 1.00 | | | 0.98 | | | 1.00 |
| Satd. Flow (prot) | 3459 | | | | | 3496 | | | 1688 | | | 1741 |
| Flt Permitted | 1.00 | | | | | 0.95 | | | 0.86 | | | 0.97 |
| Satd. Flow (perm) | 3459 | | | | | 3332 | | | 1482 | | | 1697 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 0 | 1273 | 5 | 2 | 2 | 2127 | 0 | 33 | 18 | 43 | 4 | 33 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 38 | 0 | 0 | 6 |
| Lane Group Flow (vph) | 0 | 1278 | 0 | 0 | 0 | 2131 | 0 | 0 | 56 | 0 | 0 | 45 |
| Confl. Peds. (#/hr) | 1 | | | 8 | | | 1 | 7 | | 8 | 8 | |
| Confl. Bikes (#/hr) | | | | | | | | | 5 | | | |
| Heavy Vehicles (%) | 0% | 1% | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 4% |
| Turn Type | | NA | | Perm | Perm | NA | | Perm | NA | | Perm | NA |
| Protected Phases | | 2 | | | | 6 | | | 8 | | | 4 |
| Permitted Phases | 2 | | 6 | 6 | | | 8 | | | 4 | | |
| Actuated Green, G (s) | 71.7 | | | | | 71.7 | | | 11.5 | | | 11.5 |
| Effective Green, g (s) | 71.7 | | | | | 71.7 | | | 11.5 | | | 11.5 |
| Actuated g/C Ratio | 0.75 | | | | | 0.75 | | | 0.12 | | | 0.12 |
| Clearance Time (s) | 5.5 | | | | | 5.5 | | | 6.3 | | | 6.3 |
| Vehicle Extension (s) | 3.0 | | | | | 3.0 | | | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | 2610 | | | | | 2514 | | | 179 | | | 205 |
| v/s Ratio Prot | 0.37 | | | | | | | | | | | |
| v/s Ratio Perm | | | | | | c0.64 | | | c0.04 | | | 0.03 |
| v/c Ratio | 0.49 | | | | | 0.85 | | | 0.31 | | | 0.22 |
| Uniform Delay, d1 | 4.5 | | | | | 7.9 | | | 38.1 | | | 37.7 |
| Progression Factor | 1.00 | | | | | 1.00 | | | 1.00 | | | 1.00 |
| Incremental Delay, d2 | 0.7 | | | | | 3.8 | | | 1.0 | | | 0.5 |
| Delay (s) | 5.2 | | | | | 11.7 | | | 39.2 | | | 38.2 |
| Level of Service | A | | | | | B | | | D | | | D |
| Approach Delay (s) | 5.2 | | | | | 11.7 | | | 39.2 | | | 38.2 |
| Approach LOS | A | | | | | B | | | D | | | D |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | 10.5 | | | | | HCM 2000 Level of Service | | | B | | | |
| HCM 2000 Volume to Capacity ratio | 0.77 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 95.0 | | | | | Sum of lost time (s) | | | 11.8 | | | |
| Intersection Capacity Utilization | 89.9% | | | | | ICU Level of Service | | | E | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis
2: Slidell St/Onigam St & Sir John A MacDonald Pkwy

Future Total (2028)
PM Peak Hour

| Movement | SBR |
|------------------------|------|
| Lane Configurations | |
| Traffic Volume (vph) | 14 |
| Future Volume (vph) | 14 |
| Ideal Flow (vphpl) | 1800 |
| Lane Width | 3.7 |
| Total Lost time (s) | |
| Lane Util. Factor | |
| Frpb, ped/bikes | |
| Flpb, ped/bikes | |
| Fr | |
| Flt Protected | |
| Satd. Flow (prot) | |
| Flt Permitted | |
| Satd. Flow (perm) | |
| Peak-hour factor, PHF | 1.00 |
| Adj. Flow (vph) | 14 |
| RTOR Reduction (vph) | 0 |
| Lane Group Flow (vph) | 0 |
| Confl. Peds. (#/hr) | 7 |
| Confl. Bikes (#/hr) | 8 |
| Heavy Vehicles (%) | 0% |
| Turn Type | |
| Protected Phases | |
| Permitted Phases | |
| Actuated Green, G (s) | |
| Effective Green, g (s) | |
| Actuated g/C Ratio | |
| Clearance Time (s) | |
| Vehicle Extension (s) | |
| Lane Grp Cap (vph) | |
| v/s Ratio Prot | |
| v/s Ratio Perm | |
| v/c Ratio | |
| Uniform Delay, d1 | |
| Progression Factor | |
| Incremental Delay, d2 | |
| Delay (s) | |
| Level of Service | |
| Approach Delay (s) | |
| Approach LOS | |
| Intersection Summary | |

HCM Signalized Intersection Capacity Analysis

3: Bayview Stn Rd & Scott St/Albert St

Future Total (2028)

PM Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|--------|------|------|------|---------------------------|------|------|------|-------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 31 | 632 | 128 | 137 | 880 | 154 | 123 | 328 | 107 | 90 | 111 | 33 |
| Future Volume (vph) | 31 | 632 | 128 | 137 | 880 | 154 | 123 | 328 | 107 | 90 | 111 | 33 |
| Ideal Flow (vphpl) | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 | 1800 |
| Lane Width | 3.7 | 3.6 | 3.7 | 3.2 | 3.5 | 3.8 | 3.0 | 4.3 | 3.7 | 3.3 | 4.5 | 3.7 |
| Total Lost time (s) | 6.5 | | 6.5 | 6.5 | 6.5 | 6.4 | 6.4 | | 6.4 | 6.4 | | |
| Lane Util. Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | |
| Frpb, ped/bikes | 0.97 | | 1.00 | 1.00 | 0.78 | 1.00 | 0.99 | | 1.00 | 0.96 | | |
| Flpb, ped/bikes | 1.00 | | 0.96 | 1.00 | 1.00 | 0.91 | 1.00 | | 0.99 | 1.00 | | |
| Fr _t | 0.98 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.96 | | 1.00 | 0.97 | | |
| Flt Protected | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | |
| Satd. Flow (prot) | 1482 | | 1573 | 1402 | 1201 | 1422 | 1826 | | 1638 | 1791 | | |
| Flt Permitted | 0.81 | | 0.33 | 1.00 | 1.00 | 0.66 | 1.00 | | 0.17 | 1.00 | | |
| Satd. Flow (perm) | 1198 | | 542 | 1402 | 1201 | 994 | 1826 | | 298 | 1791 | | |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 31 | 632 | 128 | 137 | 880 | 154 | 123 | 328 | 107 | 90 | 111 | 33 |
| RTOR Reduction (vph) | 0 | 7 | 0 | 0 | 0 | 42 | 0 | 12 | 0 | 0 | 10 | 0 |
| Lane Group Flow (vph) | 0 | 784 | 0 | 137 | 880 | 112 | 123 | 423 | 0 | 90 | 134 | 0 |
| Confl. Peds. (#/hr) | 107 | | 77 | 77 | | 107 | 58 | | 13 | 13 | | 58 |
| Confl. Bikes (#/hr) | | | 4 | | | 6 | | | 7 | | | 21 |
| Heavy Vehicles (%) | 0% | 19% | 1% | 0% | 27% | 1% | 2% | 0% | 4% | 0% | 2% | 6% |
| Turn Type | Perm | NA | | Perm | NA | Perm | Perm | NA | | Perm | NA | |
| Protected Phases | | 2 | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | 6 | | 6 | 8 | | | 4 | | | |
| Actuated Green, G (s) | 61.1 | | 61.1 | 61.1 | 61.1 | 26.0 | 26.0 | | 26.0 | 26.0 | | |
| Effective Green, g (s) | 61.1 | | 61.1 | 61.1 | 61.1 | 26.0 | 26.0 | | 26.0 | 26.0 | | |
| Actuated g/C Ratio | 0.61 | | 0.61 | 0.61 | 0.61 | 0.26 | 0.26 | | 0.26 | 0.26 | | |
| Clearance Time (s) | 6.5 | | 6.5 | 6.5 | 6.5 | 6.4 | 6.4 | | 6.4 | 6.4 | | |
| Vehicle Extension (s) | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | |
| Lane Grp Cap (vph) | 731 | | 331 | 856 | 733 | 258 | 474 | | 77 | 465 | | |
| v/s Ratio Prot | | | | 0.63 | | | | 0.23 | | | 0.07 | |
| v/s Ratio Perm | c0.65 | | 0.25 | | 0.09 | 0.12 | | | c0.30 | | | |
| v/c Ratio | 1.07 | | 0.41 | 1.03 | 0.15 | 0.48 | 0.89 | | 1.17 | 0.29 | | |
| Uniform Delay, d1 | 19.4 | | 10.1 | 19.4 | 8.3 | 31.3 | 35.7 | | 37.0 | 29.6 | | |
| Progression Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | |
| Incremental Delay, d2 | 54.5 | | 3.8 | 38.1 | 0.4 | 1.4 | 18.8 | | 155.2 | 0.3 | | |
| Delay (s) | 73.9 | | 13.9 | 57.6 | 8.8 | 32.6 | 54.4 | | 192.2 | 29.9 | | |
| Level of Service | E | | B | E | A | C | D | | F | C | | |
| Approach Delay (s) | 73.9 | | | 46.1 | | | 49.6 | | | 92.3 | | |
| Approach LOS | E | | | D | | | D | | | F | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | 58.7 | | | | HCM 2000 Level of Service | | | | E | | | |
| HCM 2000 Volume to Capacity ratio | 1.10 | | | | | | | | | | | |
| Actuated Cycle Length (s) | 100.0 | | | | Sum of lost time (s) | | | | 12.9 | | | |
| Intersection Capacity Utilization | 125.5% | | | | ICU Level of Service | | | | H | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Unsignalized Intersection Capacity Analysis
4: Bayview Stn Rd/Slidell St & Burnside Ave

Future Total (2028)
PM Peak Hour

| Movement | EBU | EBL | EBR | NBU | NBL | NBT | SBT | SBR | | | | | |
|-----------------------------------|-------|------|----------------------|------|------|------|------|------|--|--|--|--|--|
| Right Turn Channelized | | | | | | | | | | | | | |
| Traffic Volume (veh/h) | 4 | 22 | 142 | 11 | 423 | 74 | 40 | 11 | | | | | |
| Future Volume (veh/h) | 4 | 22 | 142 | 11 | 423 | 74 | 40 | 11 | | | | | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | | |
| Hourly flow rate (vph) | 4 | 22 | 142 | 11 | 423 | 74 | 40 | 11 | | | | | |
| Approach Volume (veh/h) | 168 | | | 508 | | | 51 | | | | | | |
| Crossing Volume (veh/h) | 51 | | | 26 | | | 438 | | | | | | |
| High Capacity (veh/h) | 1331 | | | 1357 | | | 981 | | | | | | |
| High v/c (veh/h) | 0.13 | | | 0.37 | | | 0.05 | | | | | | |
| Low Capacity (veh/h) | 1112 | | | 1136 | | | 797 | | | | | | |
| Low v/c (veh/h) | 0.15 | | | 0.45 | | | 0.06 | | | | | | |
| Intersection Summary | | | | | | | | | | | | | |
| Maximum v/c High | 0.37 | | | | | | | | | | | | |
| Maximum v/c Low | 0.45 | | | | | | | | | | | | |
| Intersection Capacity Utilization | 55.2% | | ICU Level of Service | | | | B | | | | | | |

HCM Unsignalized Intersection Capacity Analysis
5: Hinckley Ave & Parcel 1

Future Total (2028)
PM Peak Hour

| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|------|-------|------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 4 | 0 | 0 | 2 | 6 | 14 |
| Future Volume (Veh/h) | 4 | 0 | 0 | 2 | 6 | 14 |
| Sign Control | Free | Free | | Stop | | |
| Grade | 0% | 0% | | 0% | | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 4 | 0 | 0 | 2 | 6 | 14 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | None | | | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 2 | | | 9 | 1 | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 2 | | | 9 | 1 | |
| tC, single (s) | 4.1 | | | 6.4 | 6.2 | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 2.2 | | | 3.5 | 3.3 | |
| p0 queue free % | 100 | | | 99 | 99 | |
| cM capacity (veh/h) | 1620 | | | 1009 | 1084 | |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total | 4 | 2 | 20 | | | |
| Volume Left | 4 | 0 | 6 | | | |
| Volume Right | 0 | 2 | 14 | | | |
| cSH | 1620 | 1700 | 1060 | | | |
| Volume to Capacity | 0.00 | 0.00 | 0.02 | | | |
| Queue Length 95th (m) | 0.1 | 0.0 | 0.4 | | | |
| Control Delay (s) | 7.2 | 0.0 | 8.5 | | | |
| Lane LOS | A | | A | | | |
| Approach Delay (s) | 7.2 | 0.0 | 8.5 | | | |
| Approach LOS | | | A | | | |
| Intersection Summary | | | | | | |
| Average Delay | | 7.6 | | | | |
| Intersection Capacity Utilization | | 13.5% | | ICU Level of Service | | A |
| Analysis Period (min) | | 15 | | | | |

HCM Unsignalized Intersection Capacity Analysis
6: Hinckley Ave & Parcel 2

Future Total (2028)
PM Peak Hour

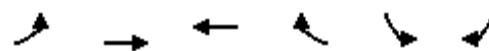
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|------|-------|------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 17 | 0 | 2 | 6 | 0 | 6 |
| Future Volume (Veh/h) | 17 | 0 | 2 | 6 | 0 | 6 |
| Sign Control | Stop | | Free | | | Free |
| Grade | 0% | | 0% | | | 0% |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 17 | 0 | 2 | 6 | 0 | 6 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | | | None | | | None |
| Median storage veh) | | | | | | |
| Upstream signal (m) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 11 | 5 | | | 8 | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 11 | 5 | | | 8 | |
| tC, single (s) | 6.4 | 6.2 | | | 4.1 | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 3.5 | 3.3 | | | 2.2 | |
| p0 queue free % | 98 | 100 | | | 100 | |
| cM capacity (veh/h) | 1009 | 1078 | | | 1612 | |
| Direction, Lane # | WB 1 | NB 1 | SB 1 | | | |
| Volume Total | 17 | 8 | 6 | | | |
| Volume Left | 17 | 0 | 0 | | | |
| Volume Right | 0 | 6 | 0 | | | |
| cSH | 1009 | 1700 | 1612 | | | |
| Volume to Capacity | 0.02 | 0.00 | 0.00 | | | |
| Queue Length 95th (m) | 0.4 | 0.0 | 0.0 | | | |
| Control Delay (s) | 8.6 | 0.0 | 0.0 | | | |
| Lane LOS | A | | | | | |
| Approach Delay (s) | 8.6 | 0.0 | 0.0 | | | |
| Approach LOS | A | | | | | |
| Intersection Summary | | | | | | |
| Average Delay | | 4.7 | | | | |
| Intersection Capacity Utilization | | 13.3% | | ICU Level of Service | | A |
| Analysis Period (min) | | 15 | | | | |

HCM Unsignalized Intersection Capacity Analysis

7: Burnside Ave & Parcel 3

Future Total (2028)

PM Peak Hour



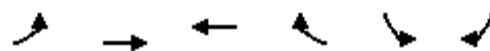
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|------|-------|----------------------|------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 4 | 158 | 466 | 2 | 5 | 12 |
| Future Volume (Veh/h) | 4 | 158 | 466 | 2 | 5 | 12 |
| Sign Control | Free | Free | | Stop | | |
| Grade | 0% | 0% | | 0% | | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 4 | 158 | 466 | 2 | 5 | 12 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | None | | | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | | 201 | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 468 | | | 633 | 467 | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 468 | | | 633 | 467 | |
| tC, single (s) | 4.1 | | | 6.4 | 6.2 | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 2.2 | | | 3.5 | 3.3 | |
| p0 queue free % | 100 | | | 99 | 98 | |
| cM capacity (veh/h) | 1094 | | | 442 | 596 | |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total | 162 | 468 | 17 | | | |
| Volume Left | 4 | 0 | 5 | | | |
| Volume Right | 0 | 2 | 12 | | | |
| cSH | 1094 | 1700 | 541 | | | |
| Volume to Capacity | 0.00 | 0.28 | 0.03 | | | |
| Queue Length 95th (m) | 0.1 | 0.0 | 0.7 | | | |
| Control Delay (s) | 0.2 | 0.0 | 11.9 | | | |
| Lane LOS | A | B | | | | |
| Approach Delay (s) | 0.2 | 0.0 | 11.9 | | | |
| Approach LOS | | B | | | | |
| Intersection Summary | | | | | | |
| Average Delay | | 0.4 | | | | |
| Intersection Capacity Utilization | | 36.0% | ICU Level of Service | | A | |
| Analysis Period (min) | | 15 | | | | |

HCM Unsignalized Intersection Capacity Analysis

8: Burnside Ave & Parcel 4

Future Total (2028)

PM Peak Hour



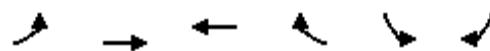
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|------|-------|----------------------|------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 4 | 159 | 456 | 2 | 7 | 12 |
| Future Volume (Veh/h) | 4 | 159 | 456 | 2 | 7 | 12 |
| Sign Control | Free | Free | | Stop | | |
| Grade | 0% | 0% | | 0% | | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 4 | 159 | 456 | 2 | 7 | 12 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | None | | | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | | 256 | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 458 | | | 624 | 457 | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 458 | | | 624 | 457 | |
| tC, single (s) | 4.1 | | | 6.4 | 6.2 | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 2.2 | | | 3.5 | 3.3 | |
| p0 queue free % | 100 | | | 98 | 98 | |
| cM capacity (veh/h) | 1103 | | | 448 | 604 | |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total | 163 | 458 | 19 | | | |
| Volume Left | 4 | 0 | 7 | | | |
| Volume Right | 0 | 2 | 12 | | | |
| cSH | 1103 | 1700 | 535 | | | |
| Volume to Capacity | 0.00 | 0.27 | 0.04 | | | |
| Queue Length 95th (m) | 0.1 | 0.0 | 0.8 | | | |
| Control Delay (s) | 0.2 | 0.0 | 12.0 | | | |
| Lane LOS | A | B | | | | |
| Approach Delay (s) | 0.2 | 0.0 | 12.0 | | | |
| Approach LOS | | B | | | | |
| Intersection Summary | | | | | | |
| Average Delay | | 0.4 | | | | |
| Intersection Capacity Utilization | | 35.5% | ICU Level of Service | | A | |
| Analysis Period (min) | | 15 | | | | |

HCM Unsignalized Intersection Capacity Analysis

9: Burnside Ave & Parcel 5

Future Total (2028)

PM Peak Hour



| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|------|-------|------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 4 | 162 | 446 | 2 | 5 | 12 |
| Future Volume (Veh/h) | 4 | 162 | 446 | 2 | 5 | 12 |
| Sign Control | Free | Free | | Stop | | |
| Grade | 0% | 0% | | 0% | | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 4 | 162 | 446 | 2 | 5 | 12 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | | None | None | | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | | 298 | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 448 | | | 617 | 447 | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 448 | | | 617 | 447 | |
| tC, single (s) | 4.1 | | | 6.4 | 6.2 | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 2.2 | | | 3.5 | 3.3 | |
| p0 queue free % | 100 | | | 99 | 98 | |
| cM capacity (veh/h) | 1112 | | | 452 | 612 | |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total | 166 | 448 | 17 | | | |
| Volume Left | 4 | 0 | 5 | | | |
| Volume Right | 0 | 2 | 12 | | | |
| cSH | 1112 | 1700 | 554 | | | |
| Volume to Capacity | 0.00 | 0.26 | 0.03 | | | |
| Queue Length 95th (m) | 0.1 | 0.0 | 0.7 | | | |
| Control Delay (s) | 0.2 | 0.0 | 11.7 | | | |
| Lane LOS | A | | B | | | |
| Approach Delay (s) | 0.2 | 0.0 | 11.7 | | | |
| Approach LOS | | | B | | | |
| Intersection Summary | | | | | | |
| Average Delay | | 0.4 | | | | |
| Intersection Capacity Utilization | | 34.9% | | ICU Level of Service | | A |
| Analysis Period (min) | | 15 | | | | |

HCM Unsignalized Intersection Capacity Analysis
10: Burnside Ave & Parcel 6

Future Total (2028)
PM Peak Hour

| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|------|-------|------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 4 | 163 | 436 | 2 | 5 | 12 |
| Future Volume (Veh/h) | 4 | 163 | 436 | 2 | 5 | 12 |
| Sign Control | Free | Free | | Stop | | |
| Grade | 0% | 0% | | 0% | | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 4 | 163 | 436 | 2 | 5 | 12 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | None | None | | | | |
| Median storage veh) | | | | | | |
| Upstream signal (m) | 344 | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 438 | | | 608 | 437 | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 438 | | | 608 | 437 | |
| tC, single (s) | 4.1 | | | 6.4 | 6.2 | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 2.2 | | | 3.5 | 3.3 | |
| p0 queue free % | 100 | | | 99 | 98 | |
| cM capacity (veh/h) | 1122 | | | 457 | 620 | |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total | 167 | 438 | 17 | | | |
| Volume Left | 4 | 0 | 5 | | | |
| Volume Right | 0 | 2 | 12 | | | |
| cSH | 1122 | 1700 | 561 | | | |
| Volume to Capacity | 0.00 | 0.26 | 0.03 | | | |
| Queue Length 95th (m) | 0.1 | 0.0 | 0.7 | | | |
| Control Delay (s) | 0.2 | 0.0 | 11.6 | | | |
| Lane LOS | A | B | | | | |
| Approach Delay (s) | 0.2 | 0.0 | 11.6 | | | |
| Approach LOS | | B | | | | |
| Intersection Summary | | | | | | |
| Average Delay | | 0.4 | | | | |
| Intersection Capacity Utilization | | 34.4% | | ICU Level of Service | | A |
| Analysis Period (min) | | 15 | | | | |

HCM Unsignalized Intersection Capacity Analysis
11: Forward Ave & Hinckley Ave

Future Total (2028)
PM Peak Hour

| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|------|-------|------|----------------------|------|------|
| Lane Configurations | | | | | | |
| Traffic Volume (veh/h) | 14 | 0 | 0 | 4 | 0 | 0 |
| Future Volume (Veh/h) | 14 | 0 | 0 | 4 | 0 | 0 |
| Sign Control | Stop | | Free | | | Free |
| Grade | 0% | | 0% | | | 0% |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 14 | 0 | 0 | 4 | 0 | 0 |
| Pedestrians | | | | | | |
| Lane Width (m) | | | | | | |
| Walking Speed (m/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | | | None | | | None |
| Median storage veh) | | | | | | |
| Upstream signal (m) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 2 | 2 | | | 4 | |
| vC1, stage 1 conf vol | | | | | | |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 2 | 2 | | | 4 | |
| tC, single (s) | 6.4 | 6.2 | | | 4.1 | |
| tC, 2 stage (s) | | | | | | |
| tF (s) | 3.5 | 3.3 | | | 2.2 | |
| p0 queue free % | 99 | 100 | | | 100 | |
| cM capacity (veh/h) | 1021 | 1082 | | | 1618 | |
| Direction, Lane # | WB 1 | NB 1 | SB 1 | | | |
| Volume Total | 14 | 4 | 0 | | | |
| Volume Left | 14 | 0 | 0 | | | |
| Volume Right | 0 | 4 | 0 | | | |
| cSH | 1021 | 1700 | 1700 | | | |
| Volume to Capacity | 0.01 | 0.00 | 0.00 | | | |
| Queue Length 95th (m) | 0.3 | 0.0 | 0.0 | | | |
| Control Delay (s) | 8.6 | 0.0 | 0.0 | | | |
| Lane LOS | A | | | | | |
| Approach Delay (s) | 8.6 | 0.0 | 0.0 | | | |
| Approach LOS | A | | | | | |
| Intersection Summary | | | | | | |
| Average Delay | | 6.7 | | | | |
| Intersection Capacity Utilization | | 13.3% | | ICU Level of Service | | A |
| Analysis Period (min) | | 15 | | | | |

HCM Unsignalized Intersection Capacity Analysis

12: Forward Ave & Burnside Ave

Future Total (2028)

PM Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|------|----------------------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (veh/h) | 4 | 195 | 0 | 0 | 573 | 0 | 0 | 0 | 0 | 0 | 0 | 14 |
| Future Volume (Veh/h) | 4 | 195 | 0 | 0 | 573 | 0 | 0 | 0 | 0 | 0 | 0 | 14 |
| Sign Control | Free | | | | Free | | | Stop | | | Stop | |
| Grade | 0% | | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 4 | 195 | 0 | 0 | 573 | 0 | 0 | 0 | 0 | 0 | 0 | 14 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (m) | | | | | | | | | | | | |
| Walking Speed (m/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | | | | |
| Median type | | None | | | | None | | | | | | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (m) | | 81 | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 573 | | | 195 | | | 790 | 776 | 195 | 776 | 776 | 573 |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 573 | | | 195 | | | 790 | 776 | 195 | 776 | 776 | 573 |
| tC, single (s) | 4.1 | | | 4.1 | | | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 2.2 | | | 2.2 | | | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free % | 100 | | | 100 | | | 100 | 100 | 100 | 100 | 100 | 97 |
| cM capacity (veh/h) | 1000 | | | 1378 | | | 299 | 327 | 846 | 314 | 327 | 519 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | SB 1 | | | | | | | | |
| Volume Total | 199 | 573 | 0 | 14 | | | | | | | | |
| Volume Left | 4 | 0 | 0 | 0 | | | | | | | | |
| Volume Right | 0 | 0 | 0 | 14 | | | | | | | | |
| cSH | 1000 | 1378 | 1700 | 519 | | | | | | | | |
| Volume to Capacity | 0.00 | 0.00 | 0.00 | 0.03 | | | | | | | | |
| Queue Length 95th (m) | 0.1 | 0.0 | 0.0 | 0.6 | | | | | | | | |
| Control Delay (s) | 0.2 | 0.0 | 0.0 | 12.1 | | | | | | | | |
| Lane LOS | A | | A | B | | | | | | | | |
| Approach Delay (s) | 0.2 | 0.0 | 0.0 | 12.1 | | | | | | | | |
| Approach LOS | | | A | B | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | 0.3 | | | | | | | | | | |
| Intersection Capacity Utilization | | 41.8% | | | ICU Level of Service | | | | | A | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

HCM Unsignalized Intersection Capacity Analysis

13: Hinckley Ave & Burnside Ave

Future Total (2028)

PM Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|------|----------------------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (veh/h) | 4 | 151 | 0 | 0 | 474 | 4 | 0 | 0 | 0 | 11 | 0 | 12 |
| Future Volume (Veh/h) | 4 | 151 | 0 | 0 | 474 | 4 | 0 | 0 | 0 | 11 | 0 | 12 |
| Sign Control | Free | | | | Free | | | Stop | | | Stop | |
| Grade | 0% | | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 4 | 151 | 0 | 0 | 474 | 4 | 0 | 0 | 0 | 11 | 0 | 12 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (m) | | | | | | | | | | | | |
| Walking Speed (m/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | | | | |
| Median type | None | | | | None | | | | | | | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (m) | 159 | | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 478 | | | 151 | | | 647 | 637 | 151 | 635 | 635 | 476 |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 478 | | | 151 | | | 647 | 637 | 151 | 635 | 635 | 476 |
| tC, single (s) | 4.1 | | | 4.1 | | | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 2.2 | | | 2.2 | | | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free % | 100 | | | 100 | | | 100 | 100 | 100 | 97 | 100 | 98 |
| cM capacity (veh/h) | 1084 | | | 1430 | | | 375 | 393 | 895 | 390 | 395 | 589 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | SB 1 | | | | | | | | |
| Volume Total | 155 | 478 | 0 | 23 | | | | | | | | |
| Volume Left | 4 | 0 | 0 | 11 | | | | | | | | |
| Volume Right | 0 | 4 | 0 | 12 | | | | | | | | |
| cSH | 1084 | 1430 | 1700 | 473 | | | | | | | | |
| Volume to Capacity | 0.00 | 0.00 | 0.00 | 0.05 | | | | | | | | |
| Queue Length 95th (m) | 0.1 | 0.0 | 0.0 | 1.1 | | | | | | | | |
| Control Delay (s) | 0.2 | 0.0 | 0.0 | 13.0 | | | | | | | | |
| Lane LOS | A | | A | B | | | | | | | | |
| Approach Delay (s) | 0.2 | 0.0 | 0.0 | 13.0 | | | | | | | | |
| Approach LOS | | | A | B | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | 0.5 | | | | | | | | | | |
| Intersection Capacity Utilization | 36.6% | | ICU Level of Service | | | | | | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |

Appendix J – Certification Form



TIA Plan Reports

On 14 June 2017, the Council of the City of Ottawa adopted new Transportation Impact Assessment (TIA) Guidelines. In adopting the guidelines, Council established a requirement for those preparing and delivering transportation impact assessments and reports to sign a letter of certification.

Individuals submitting TIA reports will be responsible for all aspects of development-related transportation assessment and reporting, and undertaking such work, in accordance and compliance with the City of Ottawa's Official Plan, the Transportation Master Plan and the Transportation Impact Assessment (2017) Guidelines.

By submitting the attached TIA report (and any associated documents) and signing this document, the individual acknowledges that s/he meets the four criteria listed below.

CERTIFICATION

1. I have reviewed and have a sound understanding of the objectives, needs and requirements of the City of Ottawa's Official Plan, Transportation Master Plan and the Transportation Impact Assessment (2017) Guidelines;
2. I have a sound knowledge of industry standard practice with respect to the preparation of transportation impact assessment reports, including multi modal level of service review;
3. I have substantial experience (more than 5 years) in undertaking and delivering transportation impact studies (analysis, reporting and geometric design) with strong background knowledge in transportation planning, engineering or traffic operations; and
4. I am either a licensed¹ or registered² professional in good standing, whose field of expertise [check ✓ appropriate field(s)] is either transportation engineering ☑ or transportation planning □.

^{1,2} License of registration body that oversees the profession is required to have a code of conduct and ethics guidelines that will ensure appropriate conduct and representation for transportation planning and/or transportation engineering works.



Dated at Ottawa this 28th day of October, 2020.
(City)

Name: Louis P. Desmarais, P. Eng.
(Please Print)

Professional Title: Senior Project Manager

Signature of Individual certifier that s/he meets the above four criteria

| |
|---|
| Office Contact Information (Please Print) |
| Address: 100 - 2650 Queensview Road |
| City / Postal Code: Ottawa, ON K2B 8H6 |
| Telephone / Extension: 613 688 1899 extension 3248 |
| E-Mail Address: phil.desmarais@exp.com |

Stamp

