

6150 THUNDER ROAD: FLOODPLAIN MAPPING

JULY 2021



Prepared For:

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6150 THUNDER ROAD: FLOODPLAIN MAPPING

In Ottawa, Ontario

JULY 2021

Prepared for:
Avenue 31 Capital Inc.



Prepared by:



Jonathon Burnett, P.Eng
(*J.F. Sabourin and Associates Inc.*)

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ATTACHMENTS:

- Attachment A – Background Documentation
- Attachment B – Hydrologic Model
- Attachment C – Hydraulic Model

1 Introduction

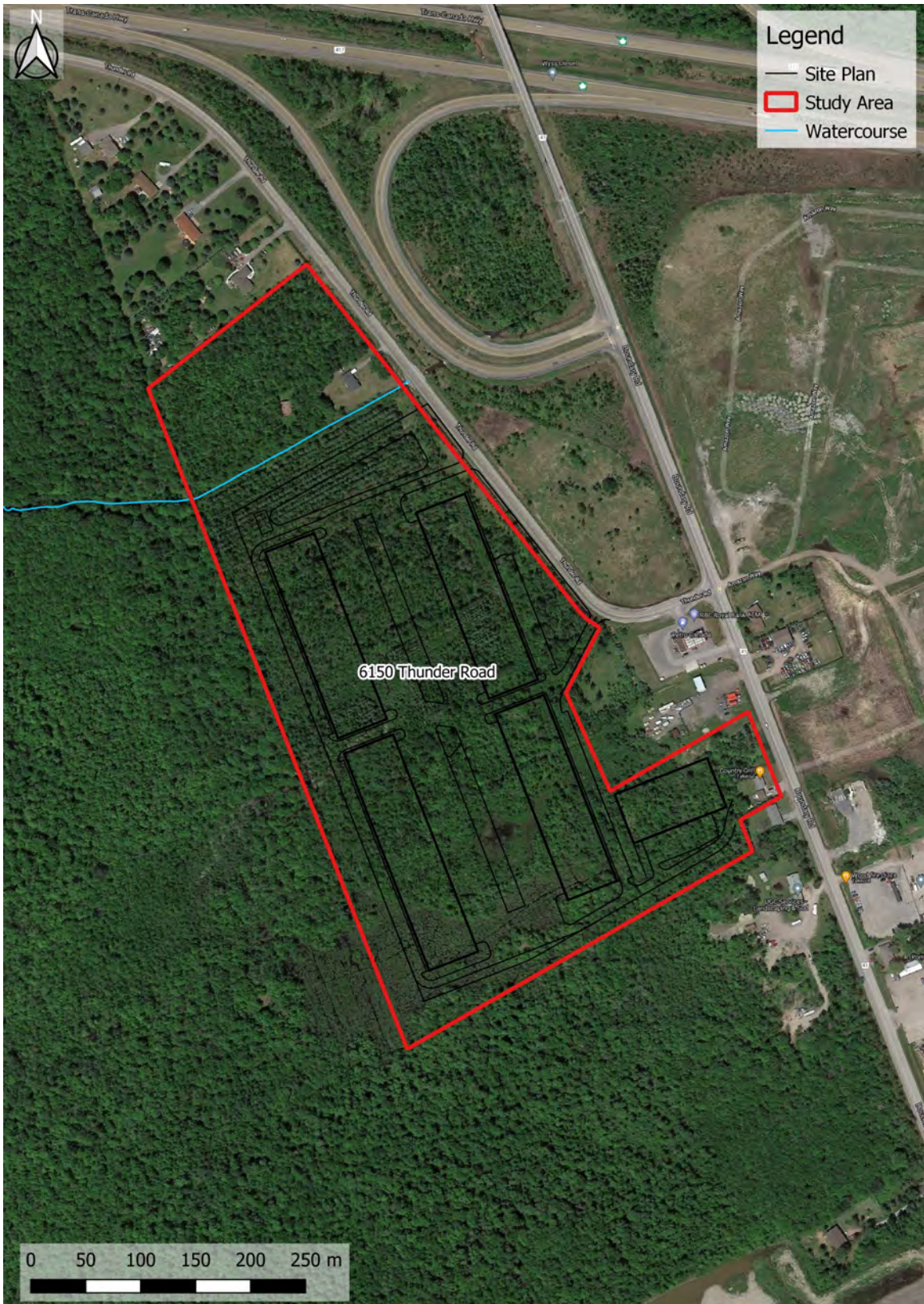
The following report documents and assesses the floodplain extents for the property located at 6150 Thunder Road in Ottawa. The site (16.71 ha) under existing conditions is undeveloped vegetated land, with several small drainage channels and a tributary watercourse running northeast to southwest through the site. This watercourse is a tributary to the Bear Brook and is referred to as the Bear Brook Trib in this report. The site at 6150 Thunder Road will ultimately be a 12.0 ha industrial park, surrounded by natural buffers. Figure 1 below outlines the approximate extent and location of the proposed development along with the location of the existing water feature that runs through the development.

As indicated in correspondence with South Nation Conservation (SNC) dated March 2, 2021, there is currently no official floodplain mapping for this area, although the regulatory floodplain located approximately 108 meters to the west of the site depicts a floodplain elevation of 76.60 m. The study also indicates a floodplain cross-section and elevation on the subject site (cross-section 244700, flood plain elevation 77.26 m). Although an initial analysis conducted by SNC found that a floodplain may exist on the site, the extents are uncertain. As directed by SNC “A floodplain analysis must be completed for the subject site, using updated hydraulic analysis, current land use, and available topographic data such as LiDAR”. See Attachment A for full correspondence.

In light of the lack of certainty with regards to the current floodplain extents within this site and with consideration of SNC’s direction, J.F. Sabourin and Associates Inc (JFSA) was commissioned by Avenue 31 Capital Inc. (Avenue 31) to complete a detailed hydrologic and hydraulic analysis to establish the floodplain extents. An accurately defined floodplain for this location is imperative, as it can greatly affect the amount of developable land within the proposed industrial park, and also controls the elevations of the various proposed infrastructure within the park (SWM pond outlet, storm sewer network and finished floor levels).

The following study includes the development of a detailed existing conditions hydrologic model. The results from this hydrologic study are then applied to a hydraulic model of the existing watercourses to quantify the water level throughout this reach of the Bear Brook Trib watercourse. Additional topographic surveys have been completed to assist in the development of both the hydrologic and hydraulic models. The following report outlines the development of hydrologic and hydraulic models and documents the findings of these analyses.

Figure 1: Site Boundary and Existing Watercourses



1.1 Background Data

The following section outlines the background data and information used to support and supplement this study:

1.1.1 Topographic Survey

A topographic survey of the 6150 Thunder Road site and associated watercourse/drains were completed by Annis O'Sullivan Vollebek Ltd (AOV) in December 2020. This topographic data was used to capture the Bear Brook Trib channel geometry within the site and has been incorporated in the HEC-RAS Hydraulic model. Figures of this survey data have been provided in Attachment A.

1.1.2 LiDAR

LiDAR data flown by the City of Ottawa in 2020 has been acquired for this project. This LiDAR data were merged into a single GIS raster at a resolution of 1.0 m and then used to delineate the drainage areas and topographic condition (Time to Peak – Tp) of the existing lands within the study area, as well as the floodplain topography in the hydraulic model. A figure outlining the extent and elevation data provided by the LiDAR has been presented in Figure B1 in Attachment B.

2 Hydrology

Based on the hydrologic conditions present (primarily undeveloped lands) in conjunction with the information available at the time of the study, SWMHYMO was determined to be the most suitable hydrologic modelling software to assess this area. The following section outlines the input data used to develop the SWMHYMO model.

2.1 Model Development & Parameters

2.1.1 Drainage Areas

As identified above, bare earth LiDAR data was obtained for the study area. This data was imported to GIS software where watershed delineation algorithms were applied. Major known watercourses were taken from the Ontario Integrated Hydrologic data set to ensure any major flow obstructions such as roadways do not affect the delineation of the watersheds. Figure B2 in Attachment B provides a visual overview of the existing drainage areas within the study area, based on this topographic data.

2.1.2 Land Use

Land use data has been taken from Land Information Ontario's (LIO) Land Use Data, and then discretized based on the respective subcatchments. Figure B3 in Attachment B provides a visual overview of the respective land use data for each of the subcatchments within the study area. This land use data was also used to approximate the percent imperviousness for existing developed lands.

2.1.3 Soil/Infiltration Data

Soil data within the study area has been taken from Soil Survey Complex Data available on Land Information Ontario (LIO). Figure B4 in Attachment B provides a visual overview of the respective soil type data for each of the subcatchments within the study area, note that this soils data specifies the SCS hydrologic soil conditions (soil type A-D) for all locations. A full breakdown of the soil data for each drainage area has also been provided in Table B1 in Attachment B.

2.1.4 Curve Number (CN)

Based on the underlying Land Use Type and Soil Classification at each location within a subcatchment, a Curve Number (CN) was calculated, based on applicable values outlined in Tables A2 and A3 in the SWMHYMO Manual. Each Curve Number was then weighted based on the total area within a given subcatchment to determine the weighted CN for that subcatchment. The CN values calculated were then converted to CN*.

Note that the traditional CN procedure assumes that Initial Abstraction (IA) = 0.2S. However, the traditional CN method is subject to errors because of this assumption, particularly for smaller rainfall events. It is recommended instead that a modified CN* and a user-defined IA value be used for SWMHYMO modelling. Modified CN* values have been shown to correlate well with measured flows and perform well in continuous SWMHYMO modelling (as discussed in the July 1989 INTERHYMO / OTTHYMO 89 Manual). The CN values derived were converted to CN* based on the formula provided in the November 2002 Runoff Curve Number Method: Examination of the Initial Abstract Ratio paper and applied to the hydrologic model.

$$CN^* = \frac{100}{1.879 \left[\frac{100}{CN-1} \right]^{1.15} + 1}$$

Note that a substantial portion of the lands within this study area have been identified as “treed swamp” per the land use data from LIO. Based on Design Chart 1.09 of the MTO Drainage Management Manual, Lakes and Wetlands (including swamps) have a CN of 50, regardless of the defined soil type. As such a CN of 50 has been applied to a substantial portion of the study area that has been classified as treed swamp by the LIO data. Table B1 in Appendix B provides a full summary of the CN/CN* calculations for each of the subcatchments.

2.1.5 Time to Peak (T_p)

For natural areas within the study area, the time to peak values for each of the subcatchments has been calculated based on existing topography. Flow paths have been discretized based on the topographic data using GIS tools and the longest major flow path within each subcatchment identified; refer to Figure B5 in Attachment B for the flow paths discretized for each subcatchment. The upstream and downstream topographic elevations and flow lengths were identified for each subcatchment and used in the calculations. For these natural subcatchments, the Federal Aviation Administration (FAA) method was determined to be the most appropriate method to calculate the Time to Peak. Full details of these calculations have been provided in Table B2 in Attachment B, along with other time to peak values using alternative T_p calculation methods.

2.1.6 Channel Routing

To account for channel routing throughout the study area, channel topographic data from the survey completed by AOV has been used where possible. In locations where there was no topographic data, the LiDAR has been used to approximate the channel cross-section and associated flow parameters (length & slope). Figure B5 in Attachment B outlines the major flow paths within the study area, which have been used to account for channel routing and time-to-peak calculations within the subcatchments.

2.2 Proposed Conditions

As a part of this analysis, it has been assumed that the development at 6150 Thunder Road will meet pre-development release rates from the site via an assortment of stormwater management solutions such as a conventional SWM pond, major system storage and grass swales with check dams. The exact details of these features will be documented in forthcoming site plan control reports supporting the development at 6150 Thunder Road. As the development will match pre-development release rates, the proposed development will have no impacts on peak flows within this watercourse and therefore will not affect the hydrologic results determined under existing conditions.

2.3 Hydrologic Results

The following tables outline the peak flow at key locations within the study area based on the SWMHYMO simulations. Note that both the 3 Hour Chicago and 24 Hour SCS design storms were assessed in this study, with the 24 Hour SCS storm determined to be the critical storm for this study area.

Table 1: Critical Peak Flow (m³/s) Summary

Location	Description	2-Year SCS 24Hr	5-Year SCS 24Hr	10-Year SCS 24Hr	25-Year SCS 24Hr	50-Year SCS 24Hr	100-Year SCS 24Hr
J2	Upstream extent at 6150 Thunder Road	0.192	0.339	0.451	0.604	0.731	0.874
J3	Downstream extent at 6150 Thunder Road	0.301	0.530	0.705	0.944	1.143	1.368
J4	600 m Upstream of Thunder Road Crossing	0.336	0.597	0.798	1.076	1.309	1.570
J5	150 m Upstream of Thunder Road Crossing	0.352	0.630	0.846	1.146	1.398	1.683
J6	Upstream side of Thunder Road Crossing	0.369	0.664	0.894	1.211	1.480	1.784
Bear Brook	Confluence with the Bear Brook	0.401	0.724	0.977	1.327	1.625	1.962

As a cursory comparative check, the flows determined by the above analysis at the upstream side of the Thunder Road crossing, downstream of the study area were compared with flows derived by OFAT using both the Index Flood Method and the Primary Multiple Regression. Based on this analysis the flows determined by JFSA at this location compare reasonably well with those derived by OFAT, with the flows determined by JFSA filling in between the two OFAT methods for the larger return periods (100-Year event).

Table 2: Peak Flow Comparison – Thunder Road Crossing (J6)

Return Period	JFSA Analysis (July 2021)	Index Flood Method with EPA	Primary Multiple Regression
2-Year Event	0.369	0.670	0.593
5-Year Event	0.664	0.870	0.939
10-Year Event	0.894	1.030	1.206
20-Year Event	-	1.190	1.479
50-Year Event	1.48	1.440	1.753
100-Year Event	1.784	1.630	2.038

3 Hydraulics

The detailed hydraulic analysis of the Bear Brook Tributary was conducted using the US Army Corps of Engineers HEC- RAS software (version 5.0.7). The purpose of this hydraulic analysis is to determine the regulatory floodplain elevation within the subject site at 6150 Thunder Road, based on the results of the hydrologic analysis outlined above.

3.1 Model Development & Parameters

Detailed topographic survey data was used to develop the hydraulic model cross-sections. Some cross-sections were supplemented with LiDAR data, in locations where the topographic survey was difficult to access or did not extend far enough to capture the full channel over banks. Model cross-sections were taken at locations where detailed topographic cross-sections were recorded, approximately every 50 m, to accurately capture the hydraulic characteristics and flow conveyance of the existing watercourse. Existing hydraulic infrastructure (culverts, bridges and weirs) on the respective watercourses were included in the model based on the details outlined in the topographic surveys.

This HEC-RAS model starts at the downstream side of the existing culvert that passes under Thunder Road near the subject site at 6150 Thunder Road and extends approximately 1.5 km downstream to the confluence with the Bear Brook. The downstream boundary condition at this location has been set as a normal depth with a slope of 0.1%. Given that the site is a considerable distance both vertically (5m) and horizontally (1.5km) from this downstream boundary, any adjustments to this boundary would have negligible impacts on the water level results determined in these simulations.

For all reaches in the models, a Manning's roughness value of 0.035 has been applied for the main channel and a Manning's of 0.08 has been applied for the overbanks. Bank markers were applied based on visual inspection of each cross-section geometry and reviewed with aerial photography. The channel flow lengths were determined based on the flow path distance between each cross-section, with the overbank flow lengths approximated based on the anticipated overbanks center of the flow. Ineffective flow areas and modifications to the expansion-contraction coefficients have also been applied to the two cross-sections upstream and downstream of the structure, with the upstream areas expanding at a rate of 1:1 and the downstream sections expanding at a rate of 1:4. Refer to Figure C1 in Attachment C for an overview of the model extents.

3.2 Results

3.2.1 Water Levels

Peak water levels were extracted from the HEC-RAS model at key locations within the study area. Table 3 below is a summary of peak water level values at these key locations for the various periods assessed in this analysis. Full summary tables have been provided in Attachment C; refer to Figure C1 for the location of the respective cross-sections.

Table 3: Peak Water Levels (m) at Key Locations

Model XS	Location	2-Year SCS 24Hr	5-Year SCS 24Hr	10-Year SCS 24Hr	25-Year SCS 24Hr	50-Year SCS 24Hr	100-Year SCS 24Hr
1578.3	Upstream extent at 6150 Thunder Road	76.06	76.14	76.20	76.27	76.33	76.38
1350	Downstream extent at 6150 Thunder Road	75.87	75.99	76.06	76.15	76.21	76.27
300	Upstream side of Thunder Road Crossing	72.19	72.27	72.32	72.37	72.42	72.47
50	Confluence with the Bear Brook	71.00	71.05	71.09	71.12	71.14	71.17

The table above indicates that the 100-year peak water levels within the proposed development range from 76.27 m - 76.38 m.

3.2.2 Result Tables

Complete typical HEC-RAS hydraulic summary tables of the updated floodplain modelling have been provided in Attachment C.

3.2.3 Long Section & Cross Section Plots

Long and cross-section plots have been extracted from the model and have been provided in Attachment C.

3.2.4 Floodplain Extent Maps

A floodplain extent map has been generated for this study area for the 100-Year event to visually quantify the extent of flooding within this watercourse. Note that these figures have been provided for visual purposes only for this report and should not be used for regulatory flood mapping without approval from the appropriate authorities. Refer to Figure C2 in Attachment C.

3.2.5 Flood Depth Maps

A floodplain depth map has been generated for this study area for the 100-Year event to visually quantify the depth of flooding throughout this watercourse. Note that these figures have been provided for visual purposes only for this report and should not be used as regulatory flood mapping without approval from the appropriate authorities. Refer to Figure C3 in Attachment C.

4 CONCLUSION

As documented above, J.F. Sabourin and Associates Inc (JFSA) has completed a detailed hydrologic and hydraulic analysis of the existing watercourse tributary to the Bear Brook from the crossing near 6150 Thunder Road through to the confluence with the Bear Brook. The results of the detailed hydrologic study were documented and compared with flows derived using OFAT, which showed a good correlation.

A hydraulic model of the watercourse was then developed using site-specific topographic survey data and LiDAR data from 2020, with typical model parameters applied to reflect the hydraulic conditions within this study area. The full suite of flows derived in the hydrologic study was applied to the hydraulic model to determine the peak water level elevations and floodplain extent throughout this reach. A complete summary of peak water levels has been provided and from this analysis, it was found that the 100-Year water level within the 6150 Thunder Road development ranges from an elevation of 76.27 m – 76.38 m. Floodplain extent and depth maps have been generated for this study area for the 100-Year event to visually quantify the extents of flooding related to this watercourse.

5 JFSA STATEMENT OF LIMITATIONS

J.F. Sabourin and Associates Inc. (JFSA) has prepared this report and performed the services described in this report, in a manner consistent with the level of care and skill normally exercised by members of the engineering and science professions currently practicing under similar conditions in the jurisdiction in which the services are provided, subject to the time limits and financial and physical constraints applicable to the services. No other warranty, expressed or implied, is made. This report has been prepared for the exclusive use of the client representative, for the specific site, objective, and purpose described to JFSA by the client. The factual data, interpretations and recommendations pertain to a specific project as described in this report and do not apply to any other project or site location. Any change of site conditions, purpose and/or development plans may alter the validity of the report. The report, which specifically includes all tables, figures and appendices, is based on data and information assembled by JFSA and is based on the conditions at the site and study area at the time of the work and the information provided by others. JFSA has relied in good faith on all information provided and does not accept responsibility for any deficiencies, misstatements, or inaccuracies contained in the report as a result of omissions, misinterpretation, or fraudulent acts of the persons contacted or errors or omissions in the reviewed documentation and data. Any use which a third party makes of this report, or any reliance on, or decisions to be made based on it, are the responsibilities of such third parties. JFSA accepts no responsibility for damages, if any, suffered by any third party as a result of decisions made or actions based on this report.

Attachment A

Background Data

Conservation Partners Partenaires en conservation



March 2, 2021
File: SNC-1666-2021
ROLL No: 061460023012200
061460023012202

Ms. Anissa McAlpine
Planning, Infrastructure and Economic Development Department
City of Ottawa
110 Laurier Avenue West, 4th Floor
Ottawa, ON K1P 1J1

Subject: Official Plan Amendment and Zoning Bylaw Amendment
File No: D01-01-20-0025/D02-02-20-0130
6150 Thunder Road & 5368 Boundary Road
Lot 1, Concession 9 (Gloucester)
Thunder Rd Developments (2019) Inc.

Dear Ms. McAlpine,

The Conservation Partners Planning and Development Review Team has completed a review of the above noted applications, which are to amend the City's Official Plan and Zoning Bylaw to permit industrial, logistics transportation, and warehouse distribution uses on the properties. The proposal would amend the designation from General Rural Area to Rural Employment Area, and the zoning from Rural Countryside (RU) to Rural General Industrial (RG).

The following documents were included in our review:

- i. Planning Rationale. Prepared by Avenue31. Dated December 2020.
- ii. Environmental Impact Statement 6150 Thunder Road, Ottawa. Prepared by Kilgour and Associates Ltd. Dated December 16, 2020.

We have considered the environmental impacts of the proposed amendments, as outlined under Sections 2.1 (Natural Heritage) and 3.1 (Natural Hazards) of the Provincial Policy Statement (May 1, 2020) issued under Section 3 of the *Planning Act*. We offer the following comments on the applications.

Natural Hazards

A flood plain analysis has been completed for the lands to the west of the subject properties:

- i. Bear Brook Floodplain Mapping Study – City of Gloucester. Prepared by SNRCA. Dated December 1997.
- ii. Flood Risk Map Bear Brook (Gloucester). Prepared by The Base Mapping Co. Ltd., SNRCA and J.F Sabourin. Signed, stamped and dated November 23, 1999.

The study delineates the regulatory floodplain to a point approximately 108 meters to the west (cross-section 243800, flood plain elevation 76.60 m). The study also depicts a flood plain cross-section and elevation on the subject site (cross-section 244700, flood plain elevation 77.26 m). An initial analysis conducted by SNC has found that flood plain likely exists on the site, but the extents are uncertain.

1. The floodplain analysis must be completed for the subject site, using updated hydraulic analysis, current land use, and available topographic data such as LiDAR. The new floodplain should be compared to historic flood plain reports and data.
2. Multiple drainage ditches direct water to the main creek bisecting the properties. The current drainage patterns within and adjacent to the properties must be maintained.
3. It must be demonstrated that the development of the properties will have no negative upstream or downstream impacts on neighbouring properties.

Natural Heritage Features

The City of Ottawa's Official Plan Schedule L shows the Natural Heritage System on the adjacent lands to the west, and within the site along the south property boundary. The schedule shows mapped watercourses flowing westward through the property, and a tributary flowing from the south. During the pre-consultation for these applications, the Conservation Partners requested an Environmental Impact Statement (EIS) with an assessment of headwater drainage features. We offer the following comments on the submitted EIS.

1. The EIS must acknowledge whether there is adequate information to assess the significance of the adjacent natural heritage features. In the absence of adequate information, the EIS should provide conservative mitigation recommendations that reflect the uncertainty.
2. The findings of the headwater drainage feature assessment are required within the report. This includes the evaluation rationale and the management recommendations. Without this information, it is not possible to determine whether the EIS recommendations are appropriate. For example, what is the rationale for directing a drainage swale through an on-line pond, and how is this appropriate mitigation or compensation for the headwater features being removed.
3. There is an east-west channel at the south end of the site that is connected to the main R2 features. This channel should be evaluated, discussed as part of the headwater drainage feature assessment, and appropriate mitigation provided.
4. Mitigation recommendations should be provided for a stormwater facility to ensure there are no impacts to downstream water quality and the thermal regime.
5. The 2018 ELC mapping and any supporting soils and groundwater information should be provided within the EIS to fully understand the features and impacts of the proposed development.

Conservation Authority Act

South Nation Conservation (SNC) implements Ontario Regulation 170/06, Development Interference with Wetlands and Alterations to Shorelines and Watercourses, developed under Section 28 of the *Conservation Authorities Act*.

Any future development or site alteration within 15 metres inland of a regulatory floodplain boundary will require a permit from SNC, and restrictions may apply. In addition, any interference with a watercourse may require a permit from SNC and restrictions may apply.

Conclusion

The developability of the subject properties for the proposed uses may be constrained by natural hazards on the site, and by mitigation necessary for the protection of natural heritage features on the adjacent lands. It is recommended that these constraints be established before the applications are approved.

To ensure the safety of the future development and the surrounding properties, a Flood Plain Analysis must be completed. The Environmental Impact Statement should also be finalized to determine the appropriate zoning for the property.

I trust this review is to your satisfaction. If there are any questions or concerns, please feel free to contact our office.

Yours truly,

A handwritten signature in cursive script that reads "James Holland".

James Holland, MSc RPP
Watershed Planner
South Nation Conservation

SKETCH ILLUSTRATING TOPOGRAPHIC INFORMATION AT

6150 THUNDER ROAD
5336 to 5376 Boundary Road
CITY OF OTTAWA

Prepared by Annis, O'Sullivan, Vollebek Ltd.

December 15, 2020.

PROPOSED BORE HOLES (Marked on Site)

POINT NUMBER	NORTHING	EASTING	GROUND ELEVATION
BH No. 1	5023306.75	387472.69	77.22
BH No. 2	5023193.73	387485.63	76.76
BH No. 3	5023212.61	387635.78	76.80
BH No. 4	5023122.95	387602.13	77.32

Scale 1 : 1000



Metric
DISTANCES SHOWN ON THIS PLAN ARE IN METRES AND CAN BE CONVERTED TO FEET BY DIVIDING BY 0.3048

Notes & Legend

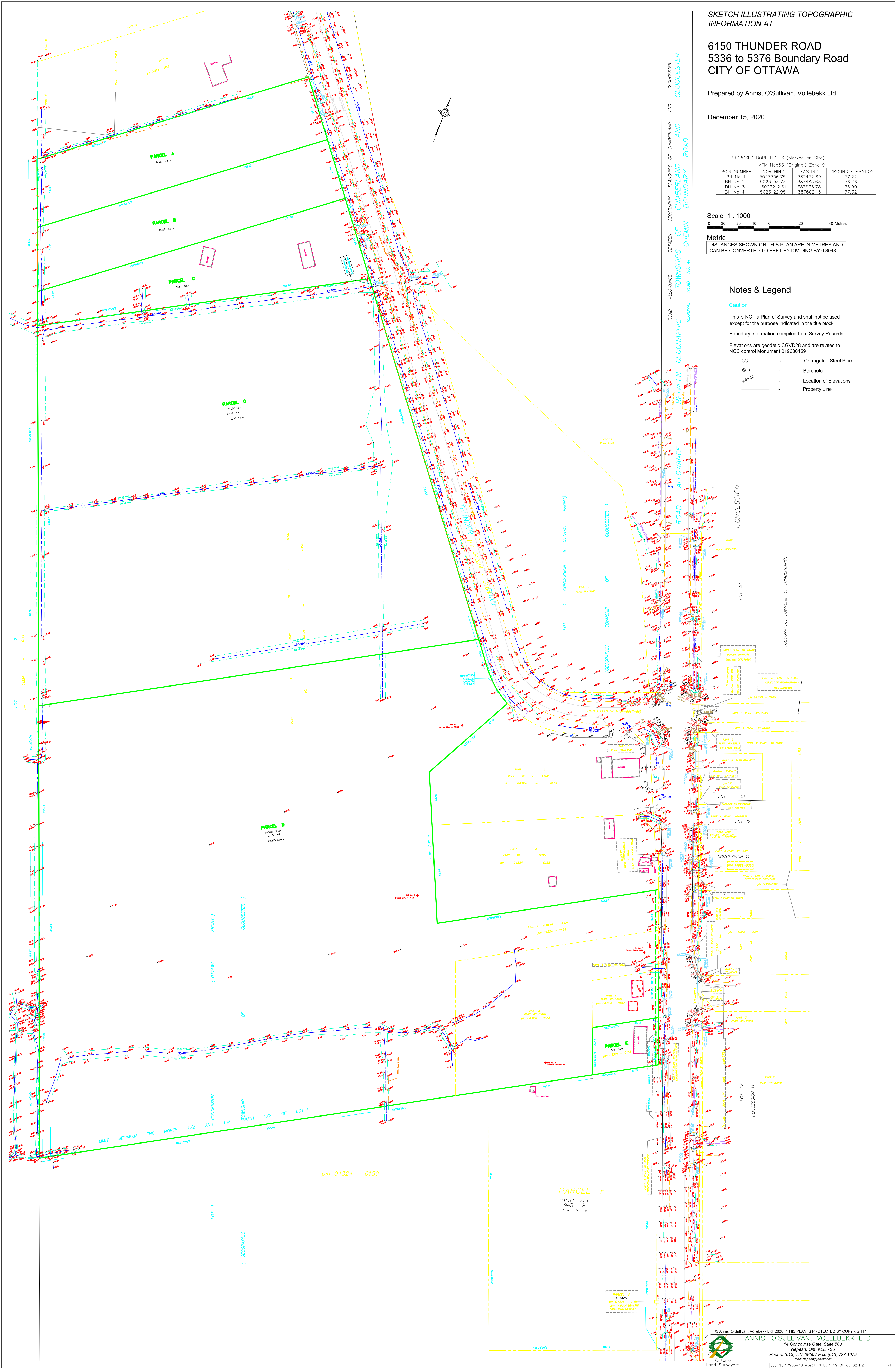
Caution

This is NOT a Plan of Survey and shall not be used except for the purpose indicated in the title block.

Boundary information compiled from Survey Records

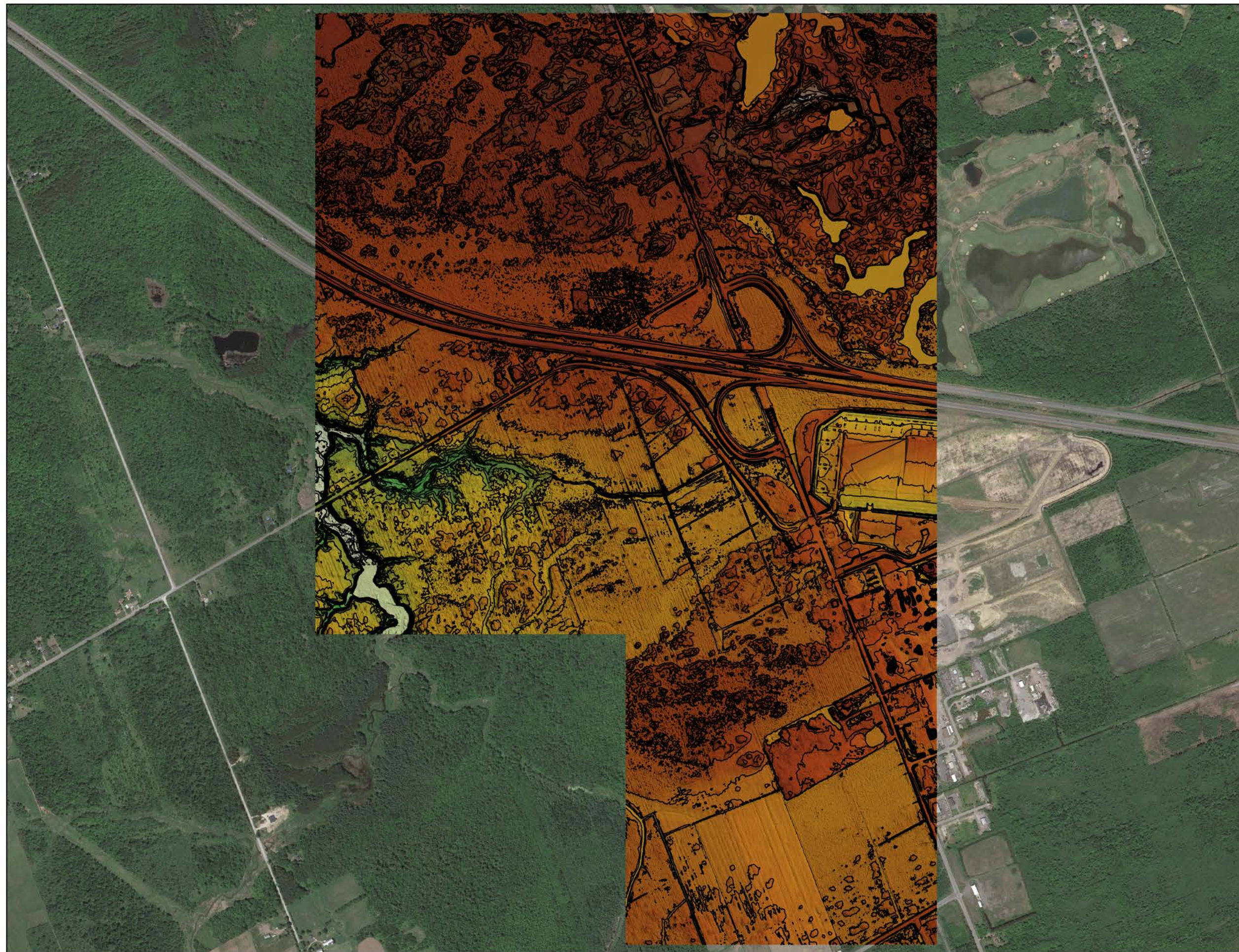
Elevations are geodetic CGVD28 and are related to NCC control Monument 019680159

- CSP - Corrugated Steel Pipe
- BH - Borehole
- +85.00 - Location of Elevations
- - - - - Property Line



Attachment B

Hydrologic Model




Legend

Terrain Elevation (m)



- 70
- 71.5
- 73
- 74.5
- 76
- 77.5
- 79
- 80.5
- 82
- 83.5
- 85

— Contours (0.5m)



SCALE: 1:12000

0 100 200 m

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 WATER RESOURCES AND ENVIRONMENTAL CONSULTANTS
 52 Springbrook Drive
 Ottawa, ON, K2S 1B9

(613) 836-3884
 www.jfsa.com



6150 Thunder Road:
 Floodplain Mapping

Figure B1: Terrain Overview

PROJECT	2120-21
DRAWN	MP
DATE	06-28-2021



Legend

- Model Nodes
- Watercourse
- ▭ Subcatchments:
Area
CN - Tp



SCALE: 1:8000
0 100 200 m

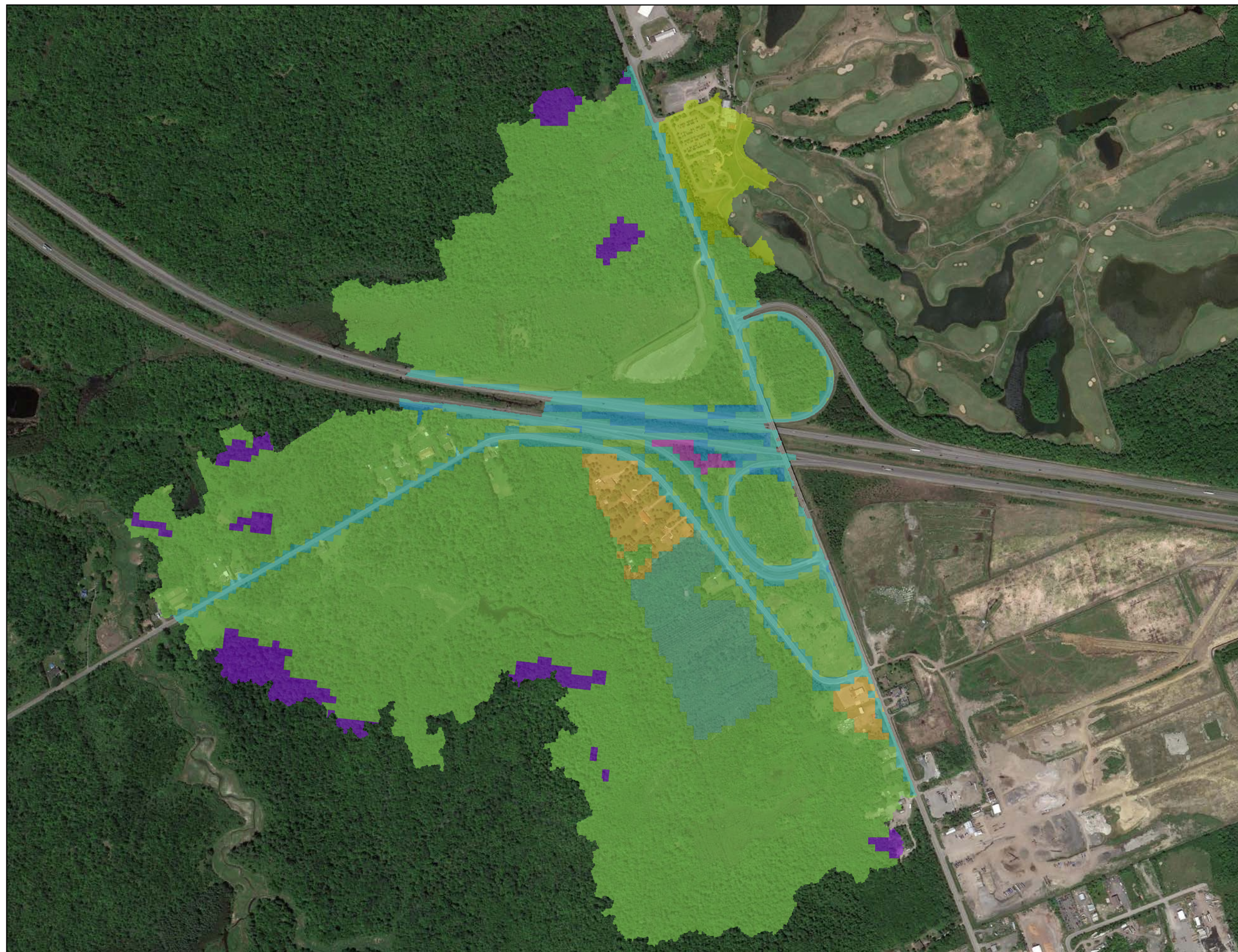
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6150 Thunder Road:
Floodplain Mapping

Figure B2: Subcatchments

PROJECT	2120-21
DRAWN	MP
DATE	06-28-2021



Legend

- Landuse Type
- Built Up Area - Impervious
 - Built Up Area - Pervious
 - Deciduous Forest
 - Forest
 - Plantation
 - Tilled
 - Transportation
 - Treed Swamp

SCALE: 1:8000

0 200 400 m

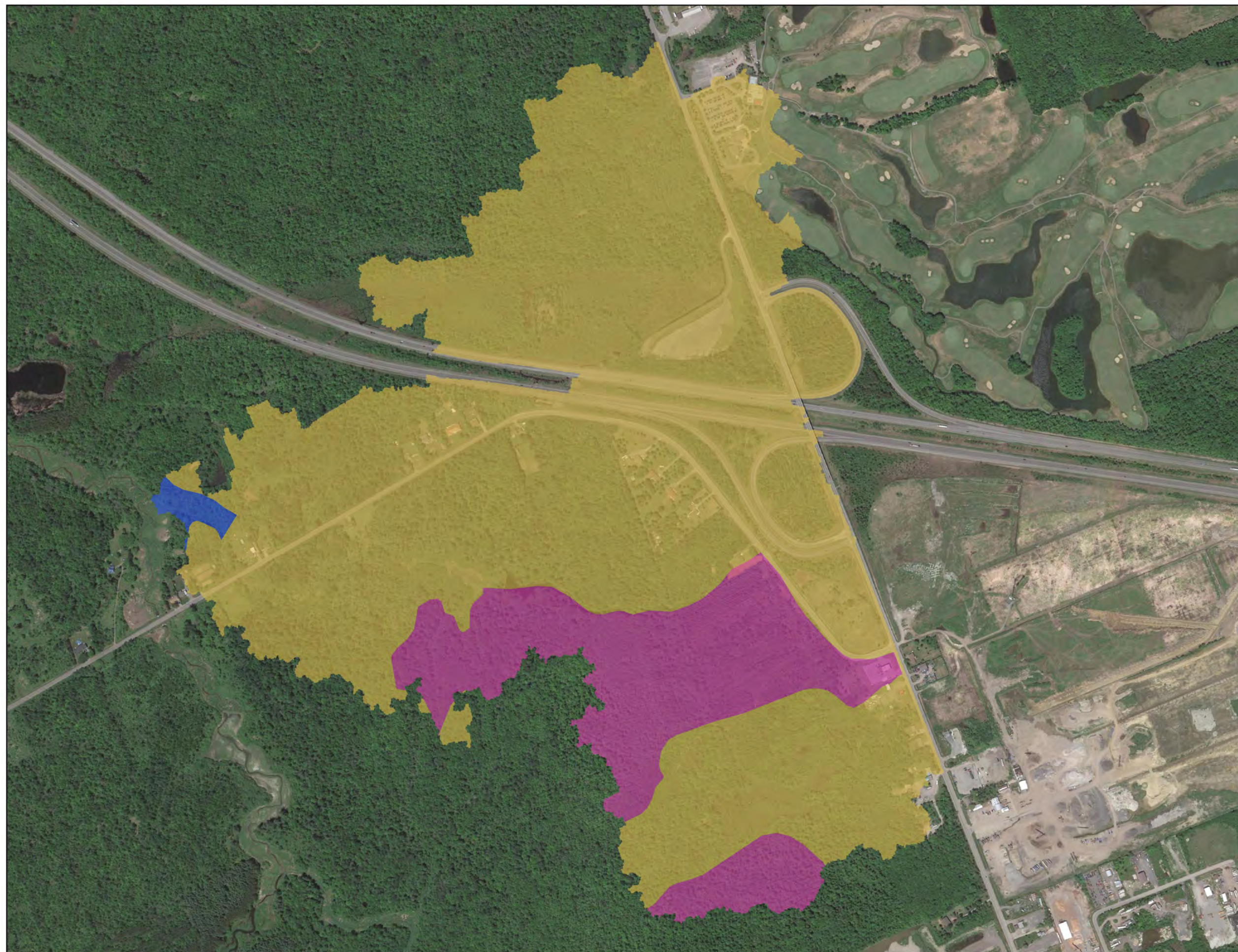
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6150 Thunder Road:
Floodplain Mapping

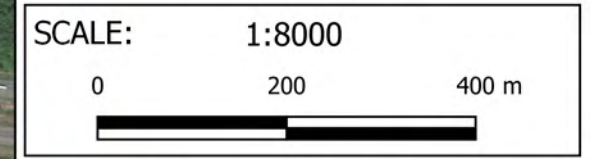
Figure B3: Land Use

PROJECT	2120-21
DRAWN	MP
DATE	06-28-2021



Legend

- Soil Type
- ALLENDALE (C)
 - CHENEY (C)
 - ERODED CHANNEL (N)



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6150 Thunder Road:
 Floodplain Mapping

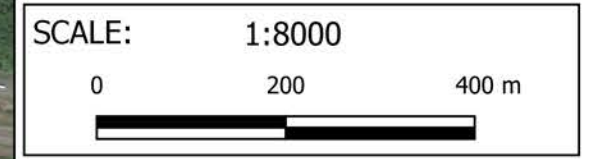
Figure B4: Soil Types

PROJECT	2120-21
DRAWN	MP
DATE	06-28-2021



Legend

- Flow Paths
- Model Nodes
- Streams
- Subcatchments



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6150 Thunder Road:
Floodplain Mapping

Figure B5: Flow Paths

PROJECT	2120-21
DRAWN	MP
DATE	06-28-2021

Table B1: Calculation of SCS Curve Number (CN) and Modified Curve Number (CN*)

A1 (25.946 ha)								
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN	
14.158	Treed Swamp	CHENEY	C	Good	50	54.6%	27.3	
8.311	Treed Swamp	ALLEDALE	C	Good	50	32.0%	16.0	
3.143	Plantation	ALLEDALE	C	Good	70	12.1%	8.5	
0.272	Deciduous Forest	CHENEY	C	Good	70	1.0%	0.7	
0.051	Plantation	CHENEY	C	Good	70	0.2%	0.1	
0.011	Deciduous Forest	ALLEDALE	C	Good	70	0.0%	0.0	
							CN	52.7
							CN*	38

A2 (9.144 ha)								
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN	
3.127	Built Up Area - Impervious	CHENEY	C	Good	98	34.2%	33.5	
2.850	Treed Swamp	CHENEY	C	Good	50	31.2%	15.6	
2.110	Plantation	CHENEY	C	Good	70	23.1%	16.2	
1.033	Transportation	CHENEY	C	Good	98	11.3%	11.1	
0.127	Treed Swamp	ALLEDALE	C	Good	50	1.4%	0.7	
0.013	Plantation	ALLEDALE	C	Good	70	0.1%	0.1	
0.010	Transportation	ALLEDALE	C	Good	98	0.1%	0.1	
							CN	77.2
							CN*	68

A3 (10.53 ha)								
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN	
4.842	Treed Swamp	CHENEY	C	Good	50	46.0%	23.0	
2.096	Treed Swamp	ALLEDALE	C	Good	50	19.9%	10.0	
1.928	Plantation	ALLEDALE	C	Good	70	18.3%	12.8	
0.548	Transportation	CHENEY	C	Good	98	5.2%	5.1	
0.461	Built Up Area - Impervious	ALLEDALE	C	Good	98	4.4%	4.3	
0.426	Built Up Area - Impervious	CHENEY	C	Good	98	4.0%	4.0	
0.229	Transportation	ALLEDALE	C	Good	98	2.2%	2.1	
							CN	61.2
							CN*	47

HWY-1 (2.364 ha)								
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN	
1.225	Transportation	CHENEY	C	Good	98	51.8%	50.8	
1.139	Tilled	CHENEY	C	Good	74	48.2%	35.7	
							CN	86.4
							CN*	82

INT-1 (4.388 ha)								
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN	
2.410	Treed Swamp	CHENEY	C	Good	50	54.9%	27.5	
1.935	Transportation	CHENEY	C	Good	98	44.1%	43.2	
0.035	Tilled	CHENEY	C	Good	74	0.8%	0.6	
0.008	Forest	CHENEY	C	Good	70	0.2%	0.1	
							CN	71.4
							CN*	60

Table B1: Calculation of SCS Curve Number (CN) and Modified Curve Number (CN*)

INT-2 (3.61 ha)							
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
2.755	Treed Swamp	CHENEY	C	Good	50	76.3%	38.2
0.826	Transportation	CHENEY	C	Good	98	22.9%	22.4
0.016	Transportation	ALLENDALE	C	Good	98	0.4%	0.4
0.013	Tilled	CHENEY	C	Good	74	0.4%	0.3
CN							61.3
CN*							47

INT-3 (5.712 ha)							
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
2.874	Treed Swamp	CHENEY	C	Good	50	50.3%	25.2
1.997	Transportation	CHENEY	C	Good	98	35.0%	34.3
0.465	Forest	CHENEY	C	Good	70	8.1%	5.7
0.376	Tilled	CHENEY	C	Good	74	6.6%	4.9
CN							70.0
CN*							58

NORTH-1 (34.701 ha)							
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
31.601	Treed Swamp	CHENEY	C	Good	50	91.1%	45.5
1.699	Transportation	CHENEY	C	Good	98	4.9%	4.8
1.200	Deciduous Forest	CHENEY	C	Good	70	3.5%	2.4
0.201	Tilled	CHENEY	C	Good	74	0.6%	0.4
CN							53.2
CN*							38

NORTH-2 (12.444 ha)							
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
6.154	Treed Swamp	CHENEY	C	Good	50	49.5%	24.7
4.287	Built Up Area - Pervious	CHENEY	C	Good	74	34.5%	25.5
1.898	Transportation	CHENEY	C	Good	98	15.3%	14.9
0.106	Tilled	CHENEY	C	Good	74	0.9%	0.6
CN							65.8
CN*							53

SOUTH-1 (20.21 ha)							
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
9.970	Treed Swamp	ALLENDALE	C	Good	50	49.3%	24.7
9.459	Treed Swamp	CHENEY	C	Good	50	46.8%	23.4
0.001	Built Up Area - Impervious	CHENEY	C	Good	98	0.0%	0.0
0.780	Deciduous Forest	ALLENDALE	C	Good	70	3.9%	2.7
CN							50.8
CN*							36

SOUTH-2 (11.612 ha)							
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
0.450	Transportation	CHENEY	C	Good	98	3.9%	3.8
10.759	Treed Swamp	CHENEY	C	Good	50	92.7%	46.3
0.404	Treed Swamp	ALLENDALE	C	Good	50	3.5%	1.7
CN							51.9
CN*							37

Table B1: Calculation of SCS Curve Number (CN) and Modified Curve Number (CN*)

SOUTH-3 (7.982 ha)								
Area (ha)	Land Type	Soil Name	Soil		CN	% of Catchment	Weighted CN	
			Condition	Soil Group				
0.340	Transportation	CHENEY	C	Good	98	4.3%	4.2	
0.222	Treed Swamp	ALLENDALE	C	Good	50	2.8%	1.4	
5.293	Treed Swamp	CHENEY	C	Good	50	66.3%	33.2	
0.005	Built Up Area - Pervious	CHENEY	C	Good	79	0.1%	0.0	
2.095	Deciduous Forest	CHENEY	C	Good	70	26.2%	18.4	
							CN	57.1
							CN*	43

SOUTH-4 (14.985 ha)								
Area (ha)	Land Type	Soil Name	Soil		CN	% of Catchment	Weighted CN	
			Condition	Soil Group				
0.129	Tilled	CHENEY	C	Fair	79	0.9%	0.7	
0.179	Deciduous Forest	ERODED CHANNEL	N	Fair	73	1.2%	0.9	
0.714	Deciduous Forest	CHENEY	C	Fair	73	4.8%	3.5	
0.884	Treed Swamp	ERODED CHANNEL	N	Fair	50	5.9%	2.9	
0.884	Transportation	CHENEY	C	Fair	98	5.9%	5.8	
12.194	Treed Swamp	CHENEY	C	Fair	50	81.4%	40.7	
							CN	54.4
							CN*	40

Table A2: Time to Peak Calculations

Parameter	Units	A1	A2	A3	HWY-1	INT-1	INT-2	INT-3	NORTH-1	NORTH-2	SOUTH-1	SOUTH-2	SOUTH-3	SOUTH-4
Area	ha	25.946	9.144	10.530	2.364	4.388	3.610	5.712	34.701	12.444	20.210	11.612	7.982	14.985
CN*	-	38	68	47	82	60	47	58	38	53	36	37	43	40
C	-	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25
Length of Channel	m	1078	563	883	572	1052	384	424	2880	939	806	705	658	1144
	ft	3536	1846	2897	1878	3450	1260	1390	9450	3081	2644	2313	2159	3754
Elevation of Head Water	m	77.41	77.74	77.69	77.71	78.56	77.36	78.12	78.82	80.12	76.77	77.23	76.50	77.46
	ft	254	255	255	255	258	254	256	259	263	252	253	251	254
Elevation of Outlet	m	76.19	76.20	76.21	76.43	76.27	76.37	76.61	76.96	76.44	74.81	72.83	71.89	70.46
	ft	250	250	250	251	250	251	251	253	251	245	239	236	231
Average Slope	m/m	0.11%	0.27%	0.17%	0.22%	0.22%	0.26%	0.36%	0.06%	0.39%	0.24%	0.62%	0.70%	0.61%
	ft/ft	0.11%	0.27%	0.17%	0.22%	0.22%	0.26%	0.36%	0.06%	0.39%	0.24%	0.62%	0.70%	0.61%
Kirpich														
Time of Concentration	mins	57	25	42	27	44	19	18	152	32	34	21	19	31
Time to Peak	min	38	17	28	18	29	13	12	101	21	23	14	13	21
Time to Peak	Hours	0.64	0.28	0.47	0.30	0.49	0.21	0.20	1.69	0.36	0.38	0.24	0.22	0.35
FAA														
Time of Concentration	mins	188	101	150	109	149	85	80	371	116	126	86	80	110
Time to Peak	mins	125	67	100	73	100	57	54	247	77	84	57	53	74
Time to Peak	Hours	2.09	1.12	1.66	1.21	1.66	0.95	0.89	4.12	1.29	1.40	0.96	0.89	1.23
Barnsby Williams														
Time of Concentration	mins	69	34	57	41	71	25	25	201	51	46	35	33	55
Time to Peak	mins	46	22	38	27	47	17	17	134	34	30	23	22	37
Time to Peak	Hours	0.77	0.37	0.64	0.45	0.79	0.28	0.28	2.23	0.56	0.51	0.39	0.37	0.62
SCS														
Time of Concentration	mins	805	138	434	105	314	179	125	2302	257	461	250	190	344
Time to Peak	mins	537	92	289	70	209	119	83	1535	172	307	167	127	229
Time to Peak	Hours	8.94	1.53	4.82	1.17	3.49	1.98	1.38	25.58	2.86	5.12	2.78	2.11	3.82
Selected Method														
FAA														
Time to Peak	min	125	67	100	73	100	57	54	247	77	84	57	53	74
Time to Peak	Hours	2.09	1.12	1.66	1.21	1.66	0.95	0.89	4.12	1.29	1.40	0.96	0.89	1.23

Note:

All methods calculated as per Appendix A of the SWMHYMO manual

Time to Peak calculated as 2/3 Time of concentration

```

1  20    Metric units / ID numbers OFF
2  *#*****
3  *# SWMHYMO / INPUT DATA FILE
4  *#*****
5  *# Project Name: [THUNDER ROAD]    Project Number: [2128]
6  *# Date       : 04-28-2021
7  *# Modeller   : [J.B]
8  *# Company    : JFSAinc.
9  *# License #  : 2549237
10 *#*****
11 * Model Developed to assess the existing hydrologic conditions on the Bear Brook
12 * tributary near 6150 Thunder Road
13 *#*****

15 START           TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[001]
16                  ["25MMC3H.stm"] <--storm filename, one per line for NSTORM time
17 *%-----|-----|
18 READ STORM     STORM_FILENAME=["storm.001"]
19 *%-----|-----|
20 DEFAULT VALUES ICASEdef=[2], read values only
21                  DEFVAL_FILENAME=["Ottawa.val"]
22 *%-----|-----|
23 * DRAINAGE AREAS NORTH OF HIGHWAY
24 *%-----|-----|
25 CALIB NASHYD   NHYD=["NORTH-1"], DT=[1] (min), AREA=[34.701] (ha),
26                  DWF=[0] (cms), CN/C=[38.1], IA=[4.67] (mm), N=[3], TP=[4.12] (hrs),
27                  RAINFALL[ , , -1]
28 *%-----|-----|
29 CALIB NASHYD   NHYD=["NORTH-2"], DT=[1] (min), AREA=[12.444] (ha),
30                  DWF=[0] (cms), CN/C=[53.0], IA=[4.67] (mm), N=[3], TP=[1.29] (hrs),
31                  RAINFALL[ , , -1]
32 *%-----|-----|
33 CALIB NASHYD   NHYD=["HWY-1"], DT=[ 1] (min), AREA=[2.364] (ha),
34                  DWF=[0] (cms), CN/C=[81.7], IA=[4.67] (mm), N=[3], TP=[1.21 ] (hrs),
35                  RAINFALL[ , , -1]
36 *%-----|-----|
37 *ADD AREAS UPSTREAM OF HIGHWAY
38 ADD HYD       NHYDsum=["J1"], NHYDs to add=["NORTH-1"+"NORTH-2"+"HWY-1"]
39 *%-----|-----|
40 * ROUTE UPSTREAM FLOWS TO THUNDER ROAD
41 ROUTE CHANNEL NHYDout=["R1"], NHYDin=["J1"], RDT=[1] (min),
42                  CHLGTH=[ 478 ] (m), CHSLOPE=[0.44] (%), FPSLOPE=[0.44] (%),
43                  SECNUM=[ 1 ], NSEG=[ 3 ]
44                  ( SEGROUGH, SEGDIST (m))=[0.05, 2.49, -0.035, 8.73, 0.05, 26.18]
45                  NSEG times
46                  ( DISTANCE (m), ELEVATION (m))=[0,76.83]
47                  [1.25,76.8]
48                  [2.49,76.64]
49                  [3.74,76.45]
50                  [4.99,76.22]
51                  [6.23,76.3]
52                  [7.48,76.52]
53                  [8.73,76.58]
54                  [9.97,76.61]
55                  [22.44,76.62]
56                  [23.69,76.7]
57                  [24.93,76.75]
58                  [26.18,76.85]
59 *%-----|-----|
60 * DRAINAGE AREAS AROUND HIGHWAY INTERCHANGE
61 *%-----|-----|
62 CALIB NASHYD   NHYD=["INT-1"], DT=[ 1] (min), AREA=[4.388] (ha),
63                  DWF=[0] (cms), CN/C=[60.4 ], IA=[4.67] (mm), N=[3], TP=[1.66 ] (hrs),
64                  RAINFALL[ , , -1]
65 *%-----|-----|
66 CALIB NASHYD   NHYD=["INT-2"], DT=[ 1] (min), AREA=[3.61] (ha),

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66 DWF=[0] (cms), CN/C=[47.4 ], IA=[4.67] (mm), N=[3], TP=[0.95 ] (hrs),
67 RAINFALL[ , , -1]
68 *%-----|-----|
69 CALIB NASHYD NHYD=["A3"], DT=[ 1] (min), AREA=[10.53] (ha),
70 DWF=[0] (cms), CN/C=[47.4 ], IA=[4.67] (mm), N=[3], TP=[1.66 ] (hrs),
71 RAINFALL[ , , -1]
72 *%-----|-----|
73 CALIB NASHYD NHYD=["INT-3"], DT=[ 1] (min), AREA=[5.712] (ha),
74 DWF=[0] (cms), CN/C=[58.5 ], IA=[4.67] (mm), N=[3], TP=[0.89 ] (hrs),
75 RAINFALL[ , , -1]
76 *%-----|-----|
77 ADD HYD NHYDsum=["J2"], NHYDs to add=["R1"+"INT-1"+"INT-2"+"INT-3"+"A3"]
78 *%-----|-----|
79 ROUTE CHANNEL NHYDout=["R2"], NHYDin=["J2"], RDT=[1] (min),
80 CHLGTH=[ 359 ] (m), CHSLOPE=[0.56] (%), FPSLOPE=[0.56] (%),
81 SECNUM=[ 1 ], NSEG=[ 3 ]
82 ( SEGROUGH, SEGDIST (m))=[0.05, 15.18, -0.035, 25.29, 0.05, 30.35]
NSEG times
83 ( DISTANCE (m), ELEVATION (m))=[0,77.2]
84 [1.26,77.14]
85 [2.53,77.09]
86 [6.32,77.02]
87 [7.59,77.01]
88 [8.85,76.99]
89 [11.38,76.96]
90 [13.91,76.92]
91 [15.18,76.86]
92 [16.44,76.63]
93 [17.71,76.28]
94 [18.97,76.24]
95 [20.23,76.23]
96 [21.5,76.33]
97 [22.76,76.62]
98 [24.03,76.73]
99 [25.29,76.8]
100 [27.82,76.8]
101 [29.09,76.81]
102 [30.35,77]
103 [-1,-1]
104 *%-----|-----|
105 * DRAINAGE AREAS DOPWNSTREAM OF THUNDERROAD
106 *%-----|-----|
107 CALIB NASHYD NHYD=["A1"], DT=[ 1] (min), AREA=[25.946] (ha),
108 DWF=[0] (cms), CN/C=[37.6 ], IA=[4.67] (mm), N=[3], TP=[2.09 ] (hrs),
109 RAINFALL[ , , -1]
110 *%-----|-----|
111 CALIB NASHYD NHYD=["A2"], DT=[ 1] (min), AREA=[9.144] (ha),
112 DWF=[0] (cms), CN/C=[68.4 ], IA=[4.67] (mm), N=[3], TP=[1.12 ] (hrs),
113 RAINFALL[ , , -1]
114 *%-----|-----|
115 ADD HYD NHYDsum=["J3"], NHYDs to add=["R2"+"A1"+"A2"]
116 *%-----|-----|
117 ROUTE CHANNEL NHYDout=["R3"], NHYDin=["J3"], RDT=[1] (min),
118 CHLGTH=[ 396 ] (m), CHSLOPE=[0.305] (%), FPSLOPE=[0.305] (%),
119 SECNUM=[ 1 ], NSEG=[ 3 ]
120 ( SEGROUGH, SEGDIST (m))=[0.05, 20.3, -0.035, 25.43, 0.05, 43.65]
NSEG times
121 ( DISTANCE (m), ELEVATION (m))=[0,75.94]
122 [5.08,75.73]
123 [10.15,75.63]
124 [15.23,75.56]
125 [20.3,75.36]
126 [21.32,75.15]
127 [22.33,75.04]
128 [23.35,74.98]
129 [24.36,75.13]

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130                                     [25.38,75.21]
131                                     [30.45,75.36]
132                                     [35.53,75.5]
133                                     [40.61,75.85]
134                                     [43.65,76.04]
135                                     [-1,-1]
136 *%-----|-----|
137 CALIB NASHYD    NHYD=["SOUTH-1"], DT=[1] (min), AREA=[20.21] (ha),
138                   DWF=[0] (cms), CN/C=[35.5 ], IA=[4.67] (mm), N=[3], TP=[1.4 ] (hrs),
139                   RAINFALL[ , , -1]
140 *%-----|-----|
141 ADD HYD        NHYDsum=["J4"], NHYDs to add=["R3"+"SOUTH-1"]
142 *%-----|-----|
143 ROUTE CHANNEL NHYDout=["R4"], NHYDin=["J4"], RDT=[1] (min),
144                   CHLGTH=[ 482 ] (m), CHSLOPE=[0.41] (%), FPSLOPE=[0.41] (%),
145                   SECNUM=[ 1 ], NSEG=[ 3 ]
146                   ( SEGRROUGH, SEGDIST (m))=[0.05, 20.48, -0.035, 24.1, 0.05, 40.97]
147                   NSEG times
148                   ( DISTANCE (m), ELEVATION (m))=[0.00, 75.19]
149                                     [4.82, 75.02]
150                                     [10.84, 74.46]
151                                     [20.48, 73.88]
152                                     [21.69, 73.71]
153                                     [22.89, 73.79]
154                                     [24.1, 74.07]
155                                     [25.3, 74.18]
156                                     [30.12, 74.6]
157                                     [34.94, 74.69]
158                                     [40.97,75.14]
159                                     [-1,-1]
160 *%-----|-----|
161 CALIB NASHYD    NHYD=["SOUTH-2"], DT=[1] (min), AREA=[11.612] (ha),
162                   DWF=[0] (cms), CN/C=[36.7 ], IA=[4.67] (mm), N=[3], TP=[0.96 ] (hrs),
163                   RAINFALL[ , , -1]
164 *%-----|-----|
165 ADD HYD        NHYDsum=["J5"], NHYDs to add=["R4"+"SOUTH-2"]
166 *%-----|-----|
167 ROUTE CHANNEL NHYDout=["R5"], NHYDin=["J5"], RDT=[1] (min),
168                   CHLGTH=[181] (m), CHSLOPE=[0.5] (%), FPSLOPE=[0.5] (%),
169                   SECNUM=[ 1 ], NSEG=[ 3 ]
170                   ( SEGRROUGH, SEGDIST (m))=[0.05, 42.50, -0.035, 47.69, 0.05, 65.31]
171                   NSEG times
172                   ( DISTANCE (m), ELEVATION (m))=[0.000, 75.10]
173                                     [10.37, 74.34]
174                                     [20.73, 73.72]
175                                     [30.06, 73.11]
176                                     [42.50, 72.86]
177                                     [45.61, 72.59]
178                                     [47.69, 72.82]
179                                     [60.13, 73.68]
180                                     [65.31, 74.98]
181                                     [-1,-1]
182 *%-----|-----|
183 CALIB NASHYD    NHYD=["SOUTH-3"], DT=[1] (min), AREA=[7.982] (ha),
184                   DWF=[0] (cms), CN/C=[42.6 ], IA=[4.67] (mm), N=[3], TP=[0.89 ] (hrs),
185                   RAINFALL[ , , -1]
186 *%-----|-----|
187 ADD HYD        NHYDsum=["J6"], NHYDs to add=["R5"+"SOUTH-3"]
188 *%-----|-----|
189 ROUTE CHANNEL NHYDout=["R6"], NHYDin=["J6"], RDT=[1] (min),
190                   CHLGTH=[ 323 ] (m), CHSLOPE=[0.44] (%), FPSLOPE=[0.44] (%),
191                   SECNUM=[ 1 ], NSEG=[ 3 ]
192                   ( SEGRROUGH, SEGDIST (m))=[0.05, 20.48, -0.035, 24.1, 0.05, 40.97]
193                   NSEG times
194                   ( DISTANCE (m), ELEVATION (m))=[0,75.19]
195                                     [4.82,75.02]

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193                                     [10.84,74.46]
194                                     [20.48,73.88]
195                                     [21.69,73.71]
196                                     [22.89,73.79]
197                                     [24.1,74.07]
198                                     [25.3,74.18]
199                                     [30.12,74.6]
200                                     [34.94,74.69]
201                                     [40.97,75.14]
202                                     [-1,-1]
203 *%-----|-----|
204 CALIB NASHYD    NHYD=["SOUTH-4"], DT=[1] (min), AREA=[14.985] (ha),
205                DWF=[0] (cms), CN/C=[39.5 ], IA=[4.67] (mm), N=[3], TP=[1.23 ] (hrs),
206                RAINFALL[ , , -1]
207 *%-----|-----|
208 ADD HYD        NHYDsum=["Total"], NHYDs to add=["R6"+"SOUTH-4"]
209 *%-----|-----|
210 *#=====|=====|
211 *                DESIGN STORMS
212 *#=====|=====|
213 *% 25 mm Storm based on 2-Year, 3-Hour Chicago Storm
214 *START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[001]
215 *                ["25MMC3H.stm"] <--storm filename, one per line for NSTORM time
216 *%-----|-----|
217 *% 2-Year, 3-Hour Chicago Storm
218 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[002]
219                ["002YC3H.stm"] <--storm filename, one per line for NSTORM time
220 *%-----|-----|
221 *% 5-Year, 3-Hour Chicago Storm
222 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[005]
223                ["005YC3H.stm"] <--storm filename, one per line for NSTORM time
224 *%-----|-----|
225 *% 10-Year, 3-Hour Chicago Storm
226 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[010]
227                ["010YC3H.stm"] <--storm filename, one per line for NSTORM time
228 *%-----|-----|
229 *% 25-Year, 3-Hour Chicago Storm
230 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[025]
231                ["025YC3H.stm"] <--storm filename, one per line for NSTORM time
232 *%-----|-----|
233 *% 50-Year, 3-Hour Chicago Storm
234 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[050]
235                ["050YC3H.stm"] <--storm filename, one per line for NSTORM time
236 *%-----|-----|
237 *% 100-Year, 3-Hour Chicago Storm
238 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[099]
239                ["100YC3H.stm"] <--storm filename, one per line for NSTORM time
240 *%-----|-----|
241 *% 2-Year, 24-Hour SCS Storm
242 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[102]
243                ["SC24002x.stm"] <--storm filename, one per line for NSTORM time
244 *%-----|-----|
245 *% 5-Year, 24-Hour SCS Storm
246 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[105]
247                ["SC24005x.stm"] <--storm filename, one per line for NSTORM time
248 *%-----|-----|
249 *% 10-Year, 24-Hour SCS Storm
250 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[110]
251                ["SC24010x.stm"] <--storm filename, one per line for NSTORM time
252 *%-----|-----|
253 *% 25-Year, 24-Hour SCS Storm
254 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[125]
255                ["SC24025x.stm"] <--storm filename, one per line for NSTORM time
256 *%-----|-----|
257 *% 50-Year, 24-Hour SCS Storm
258 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[150]

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259          ["SC24050x.stm"] <--storm filename, one per line for NSTORM time
260  *%-----|-----|
261  *% 100-Year, 24-Hour SCS Storm
262  START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[199]
263          ["SC24100x.stm"] <--storm filename, one per line for NSTORM time
264  *%-----|-----|
265  *% July 1st, 1979 Storm - Ottawa International Airport
266  *START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[979]
267  *              ["19790701.stm"] <--storm filename, one per line for NSTORM time
268  *%-----|-----|
269  *% August 4th, 1988 Storm - Ottawa International Airport
270  *START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[988]
271  *              ["19880804.stm"] <--storm filename, one per line for NSTORM time
272  *%-----|-----|
273  *% August 8th, 1996 Storm - Ottawa International Airport
274  *START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[996]
275  *              ["19960808.stm"] <--storm filename, one per line for NSTORM time
276  *%-----|-----|
277  *% 100-Year, 24-Hour SCS Storm + 20%
278  *START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[998]
279  *              ["SC24100x+.stm"] <--storm filename, one per line for NSTORM time
280  *%-----|-----|
281  *% 100-Year, 3-Hour Chicago Storm + 20%
282  *START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[999]
283  *              ["100YC3H+.stm"] <--storm filename, one per line for NSTORM time
284  *%-----|-----|
285  FINISH
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Object ID	Object Name	Object Type	Object Path	Object Date	Object Size	Object Status	Object Info
00361	R005:C0007	ROUTE CHANNEL	0.01:01:INT-1	34.70	.040	N/A	3127 3.18 n/a .000
00362	ADD HYD	+	1.0:02:R005H-1	12.44	.064	N/A	2145 5.44 n/a .000
00363		+	1.0:02:R005H-2	2.36	.056	N/A	2134 15.12 n/a .000
00364		+	1.0:02:R005H-3	49.51	.118	N/A	2156 4.12 n/a .000
00365		+	1.0:01:INT-1	49.51	.118	N/A	2156 4.12 n/a .000
00366	R005:C0008	ROUTE CHANNEL	0.01:01:INT-1	49.51	.118	N/A	2156 4.12 n/a .000
00367	ROUTE CHANNEL	->	1.0:01:R1	49.51	.115	N/A	3112 4.32 n/a .000
00368							
00369							
00370							
00371	R005:C0009	CALIB NASHYD	1.0:01:INT-1	4.39	.024	N/A	3112 7.01 .165 .000
00372							
00373							
00374	R005:C0010	CALIB NASHYD	1.0:01:INT-1	4.39	.024	N/A	3112 7.01 .165 .000
00375							
00376							
00377	R005:C0011	CALIB NASHYD	1.0:01:INT-2	3.61	.026	N/A	2116 6.35 .124 .000
00378							
00379							
00380	R005:C0012	CALIB NASHYD	1.0:01:INT-3	5.71	.046	N/A	2111 6.37 .155 .000
00381							
00382							
00383	R005:C0013	CALIB NASHYD	1.0:01:INT-3	5.71	.046	N/A	2111 6.37 .155 .000
00384							
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00390	R005:C0014	ROUTE CHANNEL	0.01:01:INT-3	73.75	.225	N/A	3104 4.68 n/a .000
00391							
00392							
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00394							
00395	R005:C0015	CALIB NASHYD	1.0:01:INT-3	73.75	.225	N/A	3104 4.68 n/a .000
00396							
00397							
00398	R005:C0016	CALIB NASHYD	1.0:01:INT-3	73.75	.225	N/A	3104 4.68 n/a .000
00399							
00400							
00401	R005:C0017	CALIB NASHYD	1.0:01:INT-3	73.75	.225	N/A	3104 4.68 n/a .000
00402							
00403							
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00406	R005:C0018	ROUTE CHANNEL	0.01:01:INT-3	108.84	.316	N/A	2128 6.17 n/a .000
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00411	R005:C0019	ROUTE CHANNEL	0.01:01:INT-3	108.84	.316	N/A	2128 6.17 n/a .000
00412							
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00414	R005:C0020	ADD HYD	1.0:02:R005H-1	20.21	.052	N/A	2155 2.87 n/a .000
00415							
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00418	R005:C0021	ADD HYD	1.0:02:R005H-1	20.21	.052	N/A	2155 2.87 n/a .000
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00423	R005:C0022	ADD HYD	1.0:02:R005H-2	11.61	.040	N/A	2118 3.01 n/a .000
00424							
00425							
00426	R005:C0023	ADD HYD	1.0:02:R005H-2	11.61	.040	N/A	2118 3.01 n/a .000
00427							
00428							
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00430	R005:C0024	ROUTE CHANNEL	0.01:01:INT-3	140.66	.418	N/A	3123 4.29 n/a .000
00431							
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00435	R005:C0025	CALIB NASHYD	1.0:01:INT-3	7.98	.037	N/A	2112 3.77 .089 .000
00436							
00437							
00438	R005:C0026	ADD HYD	1.0:02:R005H-3	140.66	.418	N/A	3124 4.26 n/a .000
00439							
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00442	R005:C0027	ROUTE CHANNEL	0.01:01:INT-3	148.64	.439	N/A	3124 4.26 n/a .000
00443							
00444							
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00447	R005:C0028	CALIB NASHYD	1.0:01:INT-4	14.99	.049	N/A	2141 3.35 .079 .000
00448							
00449							
00450	R005:C0029	ADD HYD	1.0:02:R005H-4	148.64	.436	N/A	3133 4.26 n/a .000
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007221 [L/S/n= 323./,440./,035]
007222 [Vmax = 636:Imax= 111]
007223 R005:C00028 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007224 CALIB NASHYD 1.0 01:SOOTH-4 14.99 .096 No_date 2138 6.48 1111 .000
007225 [CM= 38.1: N= 3.00: Tp= 4.12]
007226 R005:C00029 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007227 ADD HYD + 1.0 02:INHT-2 12.44 .152 No_date 2141 12.67 n/a .000
007228 + 1.0 02:INHT-1 34.70 .096 No_date 5135 7.65 n/a .000
007229 + 1.0 02:INHT-4 14.99 .096 No_date 2138 6.48 n/a .000
007230 SIM= 1.0 01:Total 163.63 .928 No_date 3118 7.92 n/a .000
007300 *****
007311 ** END OF RUN : 49
007320 *****
007330 *****
007340 *****
007350 *****
007360 *****
007370 *****
007380 *****
007390 *****
007400 RUN:COMMAND#
007410 R005:C00001
007420 START
007430 [ITER= .00 hrs on 0]
007440 [METRO= 2 (1=Imperial, 2=metric output)]
007450 [INSTORM= 1]
007460 [INUN = 0050]
007470 *****
007480 # SWHYNO / INPUT DATA FILE
007490 *****
007500 # Project Name: [THUNDER ROAD] Project Number: [2128]
007510 # Date : 04-28-2021
007520 # Modeler : [J.B]
007530 # Company : JFSaInc.
007540 # License # : 2549237
007550 *****
007560 *****
007570 R005:C00002
007580 READ STORM
007590 File name = storm.001
007600 Comment = CHICAGO STORM 50 Year, 3 Hours
007610 [SDT=10.00:SDUR= 3.00:PTOT= 64.81]
007620 *****
007630 DEFAULT VALUES
007640 File name = C:\Temp\Design\Ottawa.val
007650 [ICASE= 2 (read values only)]
007660 R005:C00004 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007667 CALIB NASHYD 1.0 01:SOOTH-1 34.70 .096 No_date 5135 7.65 1118 .000
007668 [CM= 38.1: N= 3.00: Tp= 4.12]
007669 R005:C00005 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007670 CALIB NASHYD 1.0 01:INHT-2 12.44 .152 No_date 2141 12.67 n/a .000
007671 [CM= 53.0: N= 3.00: Tp= 1.23]
007672 R005:C00006 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007673 CALIB NASHYD 1.0 01:HW-1 2.36 .088 No_date 2129 36.23 506 .000
007674 [CM= 53.0: N= 3.00: Tp= 1.23]
007675 R005:C00007 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007676 ADD HYD + 1.0 02:INHT-1 34.70 .096 No_date 5135 7.65 n/a .000
007677 + 1.0 02:INHT-2 12.44 .152 No_date 2141 12.67 n/a .000
007678 + 1.0 02:HW-1 2.36 .088 No_date 2129 36.23 n/a .000
007679 SIM= 1.0 01:Total 163.63 .928 No_date 3118 7.92 n/a .000
007680 *****
007681 ROUTE CHANNEL -> 1.0 02:1 49.51 .267 No_date 2153 10.02 n/a .000
007682 [RDT= 1.00] out< 1.0 01:R1 49.51 .264 No_date 3107 10.02 n/a .000
007683 [L/S/n= 478./,440./,035]
007684 [Vmax = 514:Imax= 251]
007685 R005:C00008 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007686 CALIB NASHYD 1.0 01:INHT-1 4.39 .056 No_date 3108 15.95 246 .000
007687 [CM= 60.4: N= 3.00: Tp= 1.66]
007688 R005:C00009 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007689 CALIB NASHYD 1.0 01:INHT-2 3.61 .045 No_date 2114 10.57 163 .000
007690 [CM= 47.4: N= 3.00: Tp= .95]
007691 R005:C00010 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007692 CALIB NASHYD 1.0 01:INHT-3 10.53 .089 No_date 3110 10.37 163 .000
007693 [CM= 47.4: N= 3.00: Tp= 1.66]
007694 R005:C00011 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007695 CALIB NASHYD 1.0 01:INHT-1 4.39 .056 No_date 3108 15.95 246 .000
007696 [CM= 58.5: N= 3.00: Tp= .89]
007697 R005:C00012 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007698 ADD HYD + 1.0 02:R1 49.51 .264 No_date 3107 10.02 n/a .000
007699 + 1.0 02:INHT-1 4.39 .056 No_date 3108 15.95 n/a .000
007700 + 1.0 02:INHT-2 3.61 .045 No_date 2114 10.57 n/a .000
007701 + 1.0 02:INHT-3 10.53 .089 No_date 3110 10.37 n/a .000
007702 + 1.0 02:HW-1 2.36 .088 No_date 2129 36.23 n/a .000
007703 SIM= 1.0 01:Total 163.63 .928 No_date 3118 7.92 n/a .000
007704 *****
007705 ROUTE CHANNEL -> 1.0 02:1 49.51 .267 No_date 2153 10.02 n/a .000
007706 [RDT= 1.00] out< 1.0 01:R1 49.51 .264 No_date 3107 10.02 n/a .000
007707 [L/S/n= 478./,440./,035]
007708 [Vmax = 514:Imax= 251]
007709 R005:C00013 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007710 CALIB NASHYD 1.0 01:INHT-1 4.39 .056 No_date 3108 15.95 246 .000
007711 [CM= 60.4: N= 3.00: Tp= 1.66]
007712 R005:C00014 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007713 CALIB NASHYD 1.0 01:INHT-2 3.61 .045 No_date 2114 10.57 163 .000
007714 [CM= 47.4: N= 3.00: Tp= .95]
007715 R005:C00015 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007716 CALIB NASHYD 1.0 01:INHT-3 10.53 .089 No_date 3110 10.37 163 .000
007717 [CM= 47.4: N= 3.00: Tp= 1.23]
007718 R005:C00016 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007719 ADD HYD + 1.0 02:R1 49.51 .264 No_date 3107 10.02 n/a .000
007720 + 1.0 02:INHT-1 4.39 .056 No_date 3108 15.95 n/a .000
007721 + 1.0 02:INHT-2 3.61 .045 No_date 2114 10.57 n/a .000
007722 + 1.0 02:INHT-3 10.53 .089 No_date 3110 10.37 n/a .000
007723 + 1.0 02:HW-1 2.36 .088 No_date 2129 36.23 n/a .000
007724 SIM= 1.0 01:Total 163.63 .928 No_date 3118 7.92 n/a .000
007725 *****
007726 ROUTE CHANNEL -> 1.0 02:1 49.51 .267 No_date 2153 10.02 n/a .000
007727 [RDT= 1.00] out< 1.0 01:R1 49.51 .264 No_date 3107 10.02 n/a .000
007728 [L/S/n= 396./,305./,035]
007729 [Vmax = 502:Imax= 249]
007730 R005:C00017 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007731 CALIB NASHYD 1.0 01:SOOTH-1 20.21 .155 No_date 2151 8.49 119 .000
007732 [CM= 51.1: N= 3.00: Tp= 1.40]
007733 R005:C00018 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007734 ADD HYD + 1.0 02:INHT-1 20.21 .155 No_date 2151 8.49 n/a .000
007735 + 1.0 02:INHT-2 129.05 .118 No_date 3102 12.43 n/a .000
007736 + 1.0 02:INHT-3 129.05 .118 No_date 3102 12.43 n/a .000
007737 SIM= 1.0 01:Total 258.31 .328 No_date 3154 12.07 n/a .000
007738 *****
007739 ROUTE CHANNEL -> 1.0 02:1 149.64 .127 No_date 3117 12.07 n/a .000
007740 [RDT= 1.00] out< 1.0 01:R1 149.64 .127 No_date 3117 12.07 n/a .000
007741 [L/S/n= 482./,410./,035]
007742 [Vmax = 657:Imax= 427]
007743 R005:C00019 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007744 CALIB NASHYD 1.0 01:SOOTH-2 11.61 .121 No_date 2115 8.89 124 .000
007745 [CM= 52.6: N= 3.00: Tp= 1.40]
007746 R005:C00020 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007747 ADD HYD + 1.0 02:R1 49.51 .264 No_date 3107 10.02 n/a .000
007748 + 1.0 02:INHT-1 4.39 .056 No_date 3108 15.95 n/a .000
007749 + 1.0 02:INHT-2 3.61 .045 No_date 2114 10.57 n/a .000
007750 + 1.0 02:INHT-3 10.53 .089 No_date 3110 10.37 n/a .000
007751 + 1.0 02:HW-1 2.36 .088 No_date 2129 36.23 n/a .000
007752 SIM= 1.0 01:Total 163.63 .928 No_date 3118 7.92 n/a .000
007753 *****
007754 ROUTE CHANNEL -> 1.0 02:1 149.64 .127 No_date 3117 12.07 n/a .000
007755 [RDT= 1.00] out< 1.0 01:R1 149.64 .127 No_date 3117 12.07 n/a .000
007756 [L/S/n= 478./,440./,035]
007757 [Vmax = 639:Imax= 321]
007758 R005:C00021 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007759 CALIB NASHYD 1.0 01:SOOTH-1 20.21 .126 No_date 2151 6.93 107 .000
007760 [CM= 35.8: N= 3.00: Tp= 1.40]
007761 R005:C00022 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007762 ADD HYD + 1.0 02:R1 49.51 .264 No_date 3107 10.02 n/a .000
007763 + 1.0 02:INHT-1 20.21 .126 No_date 2151 6.93 n/a .000
007764 + 1.0 02:INHT-2 129.05 .096 No_date 3104 10.25 n/a .000
007765 + 1.0 02:INHT-3 129.05 .096 No_date 3104 10.25 n/a .000
007766 + 1.0 02:HW-1 2.36 .088 No_date 2129 36.23 n/a .000
007767 SIM= 1.0 01:Total 258.31 .328 No_date 3154 12.07 n/a .000
007768 *****
007769 ROUTE CHANNEL -> 1.0 02:1 149.64 .127 No_date 3117 12.07 n/a .000
007770 [RDT= 1.00] out< 1.0 01:R1 149.64 .127 No_date 3117 12.07 n/a .000
007771 [L/S/n= 482./,410./,035]
007772 [Vmax = 635:Imax= 397]
007773 R005:C00023 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007774 CALIB NASHYD 1.0 01:SOOTH-2 11.61 .099 No_date 2116 7.26 112 .000
007775 [CM= 36.7: N= 3.00: Tp= .96]
007776 R005:C00024 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007777 ADD HYD + 1.0 02:R1 49.51 .264 No_date 3107 10.02 n/a .000
007778 + 1.0 02:INHT-1 20.21 .126 No_date 2151 6.93 n/a .000
007779 + 1.0 02:INHT-2 129.05 .096 No_date 3104 10.25 n/a .000
007780 + 1.0 02:INHT-3 129.05 .096 No_date 3104 10.25 n/a .000
007781 + 1.0 02:HW-1 2.36 .088 No_date 2129 36.23 n/a .000
007782 SIM= 1.0 01:Total 258.31 .328 No_date 3154 12.07 n/a .000
007783 *****
007784 ROUTE CHANNEL -> 1.0 02:1 149.64 .127 No_date 3117 12.07 n/a .000
007785 [RDT= 1.00] out< 1.0 01:R1 149.64 .127 No_date 3117 12.07 n/a .000
007786 [L/S/n= 509./,509./,035]
007787 [Vmax = 643:Imax= 360]
007788 R005:C00025 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007789 CALIB NASHYD 1.0 01:SOOTH-3 7.98 .089 No_date 2110 8.49 139 .000
007790 [CM= 42.6: N= 3.00: Tp= .89]
007791 R005:C00026 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007792 ADD HYD + 1.0 02:R1 49.51 .264 No_date 3107 10.02 n/a .000
007793 + 1.0 02:SOOTH-3 7.98 .089 No_date 2110 8.49 n/a .000
007794 + 1.0 02:SOOTH-4 149.64 .104 No_date 3122 9.85 n/a .000
007795 SIM= 1.0 01:Total 163.63 .928 No_date 3118 7.92 n/a .000
007796 *****
007797 ROUTE CHANNEL -> 1.0 02:1 149.64 .104 No_date 3122 9.85 n/a .000
007798 [RDT= 1.00] out< 1.0 01:R1 149.64 .104 No_date 3122 9.85 n/a .000
007799 [L/S/n= 223./,440./,035]
007800 [Vmax = 669:Imax= 311]
007801 R005:C00027 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007802 CALIB NASHYD 1.0 01:SOOTH-4 14.99 .119 No_date 2137 8.05 124 .000
007803 [CM= 39.5: N= 3.00: Tp= 1.23]
007804 R005:C00028 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007805 ADD HYD + 1.0 02:R1 49.51 .264 No_date 3107 10.02 n/a .000
007806 + 1.0 02:INHT-1 4.39 .056 No_date 3108 15.95 n/a .000
007807 + 1.0 02:INHT-2 3.61 .045 No_date 2114 10.57 n/a .000
007808 + 1.0 02:INHT-3 10.53 .089 No_date 3110 10.37 n/a .000
007809 + 1.0 02:HW-1 2.36 .088 No_date 2129 36.23 n/a .000
007810 SIM= 1.0 01:Total 163.63 .928 No_date 3118 7.92 n/a .000
007811 *****
007812 ROUTE CHANNEL -> 1.0 02:1 149.64 .104 No_date 3122 9.85 n/a .000
007813 [RDT= 1.00] out< 1.0 01:R1 149.64 .104 No_date 3122 9.85 n/a .000
007814 [L/S/n= 223./,440./,035]
007815 [Vmax = 669:Imax= 311]
007816 R005:C00029 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007817 CALIB NASHYD 1.0 01:SOOTH-4 14.99 .119 No_date 2137 8.05 124 .000
007818 [CM= 39.5: N= 3.00: Tp= 1.23]
007819 R005:C00030 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007820 ADD HYD + 1.0 02:R1 49.51 .264 No_date 3107 10.02 n/a .000
007821 + 1.0 02:INHT-1 4.39 .056 No_date 3108 15.95 n/a .000
007822 + 1.0 02:INHT-2 3.61 .045 No_date 2114 10.57 n/a .000
007823 + 1.0 02:INHT-3 10.53 .089 No_date 3110 10.37 n/a .000
007824 + 1.0 02:HW-1 2.36 .088 No_date 2129 36.23 n/a .000
007825 SIM= 1.0 01:Total 163.63 .928 No_date 3118 7.92 n/a .000
007826 *****
007827 ROUTE CHANNEL -> 1.0 02:1 149.64 .104 No_date 3122 9.85 n/a .000
007828 [RDT= 1.00] out< 1.0 01:R1 149.64 .104 No_date 3122 9.85 n/a .000
007829 [L/S/n= 223./,440./,035]
007830 [Vmax = 669:Imax= 311]
007831 R005:C00031 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007832 CALIB NASHYD 1.0 01:SOOTH-4 14.99 .119 No_date 2137 8.05 124 .000
007833 [CM= 39.5: N= 3.00: Tp= 1.23]
007834 R005:C00032 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007835 ADD HYD + 1.0 02:R1 49.51 .264 No_date 3107 10.02 n/a .000
007836 + 1.0 02:INHT-1 4.39 .056 No_date 3108 15.95 n/a .000
007837 + 1.0 02:INHT-2 3.61 .045 No_date 2114 10.57 n/a .000
007838 + 1.0 02:INHT-3 10.53 .089 No_date 3110 10.37 n/a .000
007839 + 1.0 02:HW-1 2.36 .088 No_date 2129 36.23 n/a .000
007840 SIM= 1.0 01:Total 163.63 .928 No_date 3118 7.92 n/a .000
007841 *****
007842 ROUTE CHANNEL -> 1.0 02:1 149.64 .104 No_date 3122 9.85 n/a .000
007843 [RDT= 1.00] out< 1.0 01:R1 149.64 .104 No_date 3122 9.85 n/a .000
007844 [L/S/n= 223./,440./,035]
007845 [Vmax = 669:Imax= 311]
007846 R005:C00033 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007847 CALIB NASHYD 1.0 01:SOOTH-4 14.99 .119 No_date 2137 8.05 124 .000
007848 [CM= 39.5: N= 3.00: Tp= 1.23]
007849 R005:C00034 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007850 ADD HYD + 1.0 02:R1 49.51 .264 No_date 3107 10.02 n/a .000
007851 + 1.0 02:INHT-1 4.39 .056 No_date 3108 15.95 n/a .000
007852 + 1.0 02:INHT-2 3.61 .045 No_date 2114 10.57 n/a .000
007853 + 1.0 02:INHT-3 10.53 .089 No_date 3110 10.37 n/a .000
007854 + 1.0 02:HW-1 2.36 .088 No_date 2129 36.23 n/a .000
007855 SIM= 1.0 01:Total 163.63 .928 No_date 3118 7.92 n/a .000
007856 *****
007857 ROUTE CHANNEL -> 1.0 02:1 149.64 .104 No_date 3122 9.85 n/a .000
007858 [RDT= 1.00] out< 1.0 01:R1 149.64 .104 No_date 3122 9.85 n/a .000
007859 [L/S/n= 223./,440./,035]
007860 [Vmax = 669:Imax= 311]
007861 R005:C00035 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007862 CALIB NASHYD 1.0 01:SOOTH-4 14.99 .119 No_date 2137 8.05 124 .000
007863 [CM= 39.5: N= 3.00: Tp= 1.23]
007864 R005:C00036 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007865 ADD HYD + 1.0 02:R1 49.51 .264 No_date 3107 10.02 n/a .000
007866 + 1.0 02:INHT-1 4.39 .056 No_date 3108 15.95 n/a .000
007867 + 1.0 02:INHT-2 3.61 .045 No_date 2114 10.57 n/a .000
007868 + 1.0 02:INHT-3 10.53 .089 No_date 3110 10.37 n/a .000
007869 + 1.0 02:HW-1 2.36 .088 No_date 2129 36.23 n/a .000
007870 SIM= 1.0 01:Total 163.63 .928 No_date 3118 7.92 n/a .000
007871 *****
007872 ROUTE CHANNEL -> 1.0 02:1 149.64 .104 No_date 3122 9.85 n/a .000
007873 [RDT= 1.00] out< 1.0 01:R1 149.64 .104 No_date 3122 9.85 n/a .000
007874 [L/S/n= 223./,440./,035]
007875 [Vmax = 669:Imax= 311]
007876 R005:C00037 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007877 CALIB NASHYD 1.0 01:SOOTH-4 14.99 .119 No_date 2137 8.05 124 .000
007878 [CM= 39.5: N= 3.00: Tp= 1.23]
007879 R005:C00038 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007880 ADD HYD + 1.0 02:R1 49.51 .264 No_date 3107 10.02 n/a .000
007881 + 1.0 02:INHT-1 4.39 .056 No_date 3108 15.95 n/a .000
007882 + 1.0 02:INHT-2 3.61 .045 No_date 2114 10.57 n/a .000
007883 + 1.0 02:INHT-3 10.53 .089 No_date 3110 10.37 n/a .000
007884 + 1.0 02:HW-1 2.36 .088 No_date 2129 36.23 n/a .000
007885 SIM= 1.0 01:Total 163.63 .928 No_date 3118 7.92 n/a .000
007886 *****
007887 ROUTE CHANNEL -> 1.0 02:1 149.64 .104 No_date 3122 9.85 n/a .000
007888 [RDT= 1.00] out< 1.0 01:R1 149.64 .104 No_date 3122 9.85 n/a .000
007889 [L/S/n= 223./,440./,035]
007890 [Vmax = 669:Imax= 311]
007891 R005:C00039 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007892 CALIB NASHYD 1.0 01:SOOTH-4 14.99 .119 No_date 2137 8.05 124 .000
007893 [CM= 39.5: N= 3.00: Tp= 1.23]
007894 R005:C00040 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007895 ADD HYD + 1.0 02:R1 49.51 .264 No_date 3107 10.02 n/a .000
007896 + 1.0 02:INHT-1 4.39 .056 No_date 3108 15.95 n/a .000
007897 + 1.0 02:INHT-2 3.61 .045 No_date 2114 10.57 n/a .000
007898 + 1.0 02:INHT-3 10.53 .089 No_date 3110 10.37 n/a .000
007899 + 1.0 02:HW-1 2.36 .088 No_date 2129 36.23 n/a .000
007900 SIM= 1.0 01:Total 163.63 .928 No_date 3118 7.92 n/a .000
007901 *****
007902 ROUTE CHANNEL -> 1.0 02:1 149.64 .104 No_date 3122 9.85 n/a .000
007903 [RDT= 1.00] out< 1.0 01:R1 149.64 .104 No_date 3122 9.85 n/a .000
007904 [L/S/n= 223./,440./,035]
007905 [Vmax = 669:Imax= 311]
007906 R005:C00041 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007907 CALIB NASHYD 1.0 01:SOOTH-4 14.99 .119 No_date 2137 8.05 124 .000
007908 [CM= 39.5: N= 3.00: Tp= 1.23]
007909 R005:C00042 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007910 ADD HYD + 1.0 02:R1 49.51 .264 No_date 3107 10.02 n/a .000
007911 + 1.0 02:INHT-1 4.39 .056 No_date 3108 15.95 n/a .000
007912 + 1.0 02:INHT-2 3.61 .045 No_date 2114 10.57 n/a .000
007913 + 1.0 02:INHT-3 10.53 .089 No_date 3110 10.37 n/a .000
007914 + 1.0 02:HW-1 2.36 .088 No_date 2129 36.23 n/a .000
007915 SIM= 1.0 01:Total 163.63 .928 No_date 3118 7.92 n/a .000
007916 *****
007917 ROUTE CHANNEL -> 1.0 02:1 149.64 .104 No_date 3122 9.85 n/a .000
007918 [RDT= 1.00] out< 1.0 01:R1 149.64 .104 No_date 3122 9.85 n/a .000
007919 [L/S/n= 223./,440./,035]
007920 [Vmax = 669:Imax= 311]
007921 R005:C00043 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007922 CALIB NASHYD 1.0 01:SOOTH-4 14.99 .119 No_date 2137 8.05 124 .000
007923 [CM= 39.5: N= 3.00: Tp= 1.23]
007924 R005:C00044 -----DtmIn-ID:INHYD-----AREAhA-OPeARkms-TPeakDate_hh:mm-----RvM-R-C-----DWfCms
007925 ADD HYD

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01081 ROUTE CHANNEL -> 1.0 0212 73.75 .192 No_date 13134 6.12 n/a .000
01082 (L/S/= 359./,560./,035)
01083 (Vmax=.446;Imax=.141)
01084
01085 R0102/C00015 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01086 CALIB NASHYD 1.0 0112 25.95 .045 No_date 14126 4.12 .085 .000
01087 (CM= 68.4; N= 3.00; Tp= 1.40)
01088 R0102/C00016 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01089 CALIB NASHYD 1.0 0122 9.14 .077 No_date 13111 11.90 .246 .000
01090 (CM= 68.4; N= 3.00; Tp= 1.40)
01091 R0102/C00017 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01092 ADD HYD + 1.0 0212 73.75 .192 No_date 13146 6.12 n/a .000
01093 + 1.0 0211 25.95 .045 No_date 14126 4.12 n/a .000
01094 + 1.0 0212 9.14 .077 No_date 13111 11.90 n/a .000
01095 SIM= 1.0 0112 108.84 .301 No_date 13142 6.13 n/a .000
01096 R0102/C00018 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01097 ROUTE CHANNEL -> 1.0 0213 108.84 .301 No_date 13142 6.13 n/a .000
01098 (RDT= 1.00) out-< 1.0 01183 108.84 .293 No_date 13159 6.13 n/a .000
01099 (L/S/= 396./,305./,035)
01100 (Vmax=.594;Imax=.174)
01101 R0102/C00019 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01102 CALIB NASHYD 1.0 0112 20.21 .044 No_date 13134 3.79 .078 .000
01103 (CM= 35.5; N= 3.00; Tp= 1.40)
01104 R0102/C00020 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01105 ADD HYD + 1.0 0212 108.84 .293 No_date 13159 6.13 n/a .000
01106 + 1.0 0212 20.21 .044 No_date 13134 3.79 n/a .000
01107 SIM= 1.0 0112 129.05 .236 No_date 12156 5.76 n/a .000
01108 R0102/C00021 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01109 ROUTE CHANNEL -> 1.0 0214 129.05 .236 No_date 13156 5.76 n/a .000
01110 (RDT= 1.00) out-< 1.0 01184 129.05 .236 No_date 14111 5.76 n/a .000
01111 (L/S/= 482./,410./,035)
01112 (Vmax=.431;Imax=.138)
01113 R0102/C00022 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01114 CALIB NASHYD 1.0 0112 11.61 .035 No_date 13101 3.98 .082 .000
01115 (CM= 26.1; N= 3.00; Tp= 1.40)
01116 R0102/C00023 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01117 ADD HYD + 1.0 0212 129.05 .236 No_date 14111 5.76 n/a .000
01118 + 1.0 0212 11.61 .035 No_date 13101 3.98 n/a .000
01119 SIM= 1.0 0113 140.66 .352 No_date 14106 5.62 n/a .000
01120 R0102/C00024 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01121 ROUTE CHANNEL -> 1.0 0215 140.66 .352 No_date 14106 5.62 n/a .000
01122 (RDT= 1.00) out-< 1.0 01185 140.66 .351 No_date 14112 5.62 n/a .000
01123 (L/S/= 181./,500./,035)
01124 (Vmax=.493;Imax=.247)
01125 R0102/C00025 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01126 CALIB NASHYD 1.0 0112 7.98 .032 No_date 12156 4.97 .102 .000
01127 (CM= 48.7; N= 3.00; Tp= 1.40)
01128 R0102/C00026 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01129 ADD HYD + 1.0 0212 140.66 .351 No_date 14112 5.62 n/a .000
01130 + 1.0 0212 7.98 .032 No_date 12156 4.97 n/a .000
01131 SIM= 1.0 0112 148.64 .367 No_date 14107 5.58 n/a .000
01132 R0102/C00027 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01133 ROUTE CHANNEL -> 1.0 0216 148.64 .367 No_date 14107 5.58 n/a .000
01134 (RDT= 1.00) out-< 1.0 01186 148.64 .367 No_date 14117 5.58 n/a .000
01135 (L/S/= 323./,440./,035)
01136 (Vmax=.540;Imax=.269)
01137 R0102/C00028 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01138 CALIB NASHYD 1.0 0112 14.99 .042 No_date 13121 4.43 .091 .000
01139 (CM= 39.5; N= 3.00; Tp= 1.23)
01140 R0102/C00029 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01141 ADD HYD + 1.0 0216 148.64 .367 No_date 14117 5.58 n/a .000
01142 + 1.0 0216 14.99 .042 No_date 13121 4.43 n/a .000
01143 SIM= 1.0 0112 163.63 .401 No_date 14112 5.48 n/a .000
01144
01145 ** END OF RUN : 104
01146
01147
01148
01149
01150
01151
01152
01153
01154 RUN#COMMAND#
01155 START
01156 (ITER= .00 hrs on 0)
01157 (METOUT= 2 (1=imperial, 2=metric output))
01158 (MTRM= 1)
01159 (NRUN= 010)
01160 *****
01161 # SWHYD / INPUT DATA FILE
01162 # Project Name: [THUNDER ROAD] Project Number: [2128]
01163 # Date : 04-28-2021
01164 # Modeler : [J.B]
01165 # Company : JFSainc.
01166 # License # : 2549237
01167 *****
01168
01169
01170
01171 R0105/C00002 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01172 READ STORM
01173 File name = storm.01
01174 Comment = 5 years SCS Type 2 Storm 24 Hours step 10 min, City of Ottawa
01175 (RDT= 1.00) out-< 1.0 01187 49.51 .226 No_date 13148 13.03 n/a .000
01176 R0105/C00003 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01177 (RDT= 1.00) out-< 1.0 01181 49.51 .226 No_date 13148 13.03 n/a .000
01178 (L/S/= 478./,440./,035)
01179 (Vmax=.490;Imax=.238)
01180 R0105/C00004 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01181 CALIB NASHYD 1.0 0112 4.39 .048 No_date 13149 20.56 .276 .000
01182 (CM= 60.4; N= 3.00; Tp= 1.66)
01183 R0105/C00005 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01184 CALIB NASHYD 1.0 0112 3.61 .039 No_date 12159 13.81 .186 .000
01185 (CM= 58.5; N= 3.00; Tp= .89)
01186 R0105/C00006 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01187 CALIB NASHYD 1.0 0112 10.53 .075 No_date 13151 13.81 .186 .000
01188 (CM= 44.4; N= 3.00; Tp= .61)
01189 R0105/C00007 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01190 CALIB NASHYD 1.0 0112 4.39 .048 No_date 13149 20.56 n/a .000
01191 (CM= 60.4; N= 3.00; Tp= 1.66)
01192 R0105/C00008 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01193 ADD HYD + 1.0 0211 4.39 .048 No_date 13149 20.56 n/a .000
01194 + 1.0 0211 10.53 .075 No_date 13151 13.81 n/a .000
01195 SIM= 1.0 0112 49.51 .226 No_date 13148 13.03 n/a .000
01196 R0105/C00009 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01197 ROUTE CHANNEL -> 1.0 0213 49.51 .226 No_date 13148 13.03 n/a .000
01198 (RDT= 1.00) out-< 1.0 01182 49.51 .226 No_date 13148 13.03 n/a .000
01199 (L/S/= 359./,560./,035)
01200 (Vmax=.446;Imax=.141)
01201 R0105/C00010 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01202 CALIB NASHYD 1.0 0112 25.95 .045 No_date 14126 4.12 .085 .000
01203 (CM= 68.4; N= 3.00; Tp= 1.40)
01204 R0105/C00011 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01205 ADD HYD + 1.0 0212 73.75 .192 No_date 13146 6.12 n/a .000
01206 + 1.0 0212 25.95 .045 No_date 14126 4.12 n/a .000
01207 SIM= 1.0 0112 108.84 .301 No_date 13142 6.13 n/a .000
01208 R0105/C00012 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01209 ROUTE CHANNEL -> 1.0 0213 108.84 .301 No_date 13142 6.13 n/a .000
01210 (RDT= 1.00) out-< 1.0 01183 108.84 .293 No_date 13159 6.13 n/a .000
01211 (L/S/= 396./,305./,035)
01212 (Vmax=.594;Imax=.174)
01213 R0105/C00013 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01214 CALIB NASHYD 1.0 0112 20.21 .044 No_date 13134 3.79 .078 .000
01215 (CM= 35.5; N= 3.00; Tp= 1.40)
01216 R0105/C00014 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01217 ADD HYD + 1.0 0212 108.84 .293 No_date 13159 6.13 n/a .000
01218 + 1.0 0212 20.21 .044 No_date 13134 3.79 n/a .000
01219 SIM= 1.0 0112 129.05 .236 No_date 12156 5.76 n/a .000
01220 R0105/C00015 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01221 ROUTE CHANNEL -> 1.0 0214 129.05 .236 No_date 13156 5.76 n/a .000
01222 (RDT= 1.00) out-< 1.0 01184 129.05 .236 No_date 14111 5.76 n/a .000
01223 (L/S/= 482./,410./,035)
01224 (Vmax=.431;Imax=.138)
01225 R0105/C00016 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01226 CALIB NASHYD 1.0 0112 11.61 .035 No_date 13101 3.98 .082 .000
01227 (CM= 26.1; N= 3.00; Tp= 1.40)
01228 R0105/C00017 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01229 ADD HYD + 1.0 0212 129.05 .236 No_date 14111 5.76 n/a .000
01230 + 1.0 0212 11.61 .035 No_date 13101 3.98 n/a .000
01231 SIM= 1.0 0113 140.66 .352 No_date 14106 5.62 n/a .000
01232 R0105/C00018 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01233 ROUTE CHANNEL -> 1.0 0215 140.66 .352 No_date 14106 5.62 n/a .000
01234 (RDT= 1.00) out-< 1.0 01185 140.66 .351 No_date 14112 5.62 n/a .000
01235 (L/S/= 181./,500./,035)
01236 (Vmax=.493;Imax=.247)
01237 R0105/C00019 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01238 CALIB NASHYD 1.0 0112 7.98 .032 No_date 12156 4.97 .102 .000
01239 (CM= 48.7; N= 3.00; Tp= 1.40)
01240 R0105/C00020 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01241 ADD HYD + 1.0 0212 140.66 .351 No_date 14112 5.62 n/a .000
01242 + 1.0 0212 7.98 .032 No_date 12156 4.97 n/a .000
01243 SIM= 1.0 0112 148.64 .367 No_date 14107 5.58 n/a .000
01244 R0105/C00021 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01245 ROUTE CHANNEL -> 1.0 0216 148.64 .367 No_date 14107 5.58 n/a .000
01246 (RDT= 1.00) out-< 1.0 01186 148.64 .367 No_date 14117 5.58 n/a .000
01247 (L/S/= 323./,440./,035)
01248 (Vmax=.540;Imax=.269)
01249 R0105/C00022 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01250 CALIB NASHYD 1.0 0112 14.99 .042 No_date 13121 4.43 .091 .000
01251 (CM= 39.5; N= 3.00; Tp= 1.23)
01252 R0105/C00023 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01253 ADD HYD + 1.0 0216 148.64 .367 No_date 14117 5.58 n/a .000
01254 + 1.0 0216 14.99 .042 No_date 13121 4.43 n/a .000
01255 SIM= 1.0 0112 163.63 .401 No_date 14112 5.48 n/a .000
01256 R0105/C00024 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01257 ROUTE CHANNEL -> 1.0 0215 140.66 .352 No_date 14106 5.62 n/a .000
01258 (RDT= 1.00) out-< 1.0 01185 140.66 .351 No_date 14112 5.62 n/a .000
01259 (L/S/= 181./,500./,035)
01260 (Vmax=.493;Imax=.247)
01261 R0105/C00025 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01262 CALIB NASHYD 1.0 0112 7.98 .032 No_date 12156 4.97 .102 .000
01263 (CM= 48.7; N= 3.00; Tp= 1.40)
01264 R0105/C00026 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01265 ADD HYD + 1.0 0212 140.66 .351 No_date 14112 5.62 n/a .000
01266 + 1.0 0212 7.98 .032 No_date 12156 4.97 n/a .000
01267 SIM= 1.0 0112 148.64 .367 No_date 14107 5.58 n/a .000
01268 R0105/C00027 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01269 ROUTE CHANNEL -> 1.0 0216 148.64 .367 No_date 14107 5.58 n/a .000
01270 (RDT= 1.00) out-< 1.0 01186 148.64 .367 No_date 14117 5.58 n/a .000
01271 (L/S/= 323./,440./,035)
01272 (Vmax=.540;Imax=.269)
01273 R0105/C00028 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01274 CALIB NASHYD 1.0 0112 14.99 .042 No_date 13121 4.43 .091 .000
01275 (CM= 39.5; N= 3.00; Tp= 1.23)
01276 R0105/C00029 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01277 ADD HYD + 1.0 0216 148.64 .367 No_date 14117 5.58 n/a .000
01278 + 1.0 0216 14.99 .042 No_date 13121 4.43 n/a .000
01279 SIM= 1.0 0112 163.63 .401 No_date 14112 5.48 n/a .000
01280 R0105/C00030 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01281 ROUTE CHANNEL -> 1.0 0215 140.66 .352 No_date 14106 5.62 n/a .000
01282 (RDT= 1.00) out-< 1.0 01187 140.66 .351 No_date 14112 5.62 n/a .000
01283 (L/S/= 181./,500./,035)
01284 (Vmax=.493;Imax=.247)
01285 R0105/C00031 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01286 CALIB NASHYD 1.0 0112 7.98 .032 No_date 12156 4.97 .102 .000
01287 (CM= 48.7; N= 3.00; Tp= 1.40)
01288 R0105/C00032 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01289 ADD HYD + 1.0 0212 140.66 .351 No_date 14112 5.62 n/a .000
01290 + 1.0 0212 7.98 .032 No_date 12156 4.97 n/a .000
01291 SIM= 1.0 0112 148.64 .367 No_date 14107 5.58 n/a .000
01292 R0105/C00033 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01293 ROUTE CHANNEL -> 1.0 0216 148.64 .367 No_date 14107 5.58 n/a .000
01294 (RDT= 1.00) out-< 1.0 01188 148.64 .367 No_date 14117 5.58 n/a .000
01295 (L/S/= 323./,440./,035)
01296 (Vmax=.540;Imax=.269)
01297 R0105/C00034 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01298 CALIB NASHYD 1.0 0112 14.99 .042 No_date 13121 4.43 .091 .000
01299 (CM= 39.5; N= 3.00; Tp= 1.23)
01300 R0105/C00035 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01301 ADD HYD + 1.0 0216 148.64 .367 No_date 14117 5.58 n/a .000
01302 + 1.0 0216 14.99 .042 No_date 13121 4.43 n/a .000
01303 SIM= 1.0 0112 163.63 .401 No_date 14112 5.48 n/a .000
01304 R0105/C00036 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01305 ROUTE CHANNEL -> 1.0 0215 140.66 .352 No_date 14106 5.62 n/a .000
01306 (RDT= 1.00) out-< 1.0 01189 140.66 .351 No_date 14112 5.62 n/a .000
01307 (L/S/= 181./,500./,035)
01308 (Vmax=.493;Imax=.247)
01309 R0105/C00037 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01310 CALIB NASHYD 1.0 0112 7.98 .032 No_date 12156 4.97 .102 .000
01311 (CM= 48.7; N= 3.00; Tp= 1.40)
01312 R0105/C00038 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01313 ADD HYD + 1.0 0212 140.66 .351 No_date 14112 5.62 n/a .000
01314 + 1.0 0212 7.98 .032 No_date 12156 4.97 n/a .000
01315 SIM= 1.0 0112 148.64 .367 No_date 14107 5.58 n/a .000
01316 R0105/C00039 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01317 ROUTE CHANNEL -> 1.0 0216 148.64 .367 No_date 14107 5.58 n/a .000
01318 (RDT= 1.00) out-< 1.0 01190 148.64 .367 No_date 14117 5.58 n/a .000
01319 (L/S/= 323./,440./,035)
01320 (Vmax=.540;Imax=.269)
01321 R0105/C00040 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01322 CALIB NASHYD 1.0 0112 14.99 .042 No_date 13121 4.43 .091 .000
01323 (CM= 39.5; N= 3.00; Tp= 1.23)
01324 R0105/C00041 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01325 ADD HYD + 1.0 0216 148.64 .367 No_date 14117 5.58 n/a .000
01326 + 1.0 0216 14.99 .042 No_date 13121 4.43 n/a .000
01327 SIM= 1.0 0112 163.63 .401 No_date 14112 5.48 n/a .000
01328 R0105/C00042 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01329 ROUTE CHANNEL -> 1.0 0215 140.66 .352 No_date 14106 5.62 n/a .000
01330 (RDT= 1.00) out-< 1.0 01191 140.66 .351 No_date 14112 5.62 n/a .000
01331 (L/S/= 181./,500./,035)
01332 (Vmax=.493;Imax=.247)
01333 R0105/C00043 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01334 CALIB NASHYD 1.0 0112 7.98 .032 No_date 12156 4.97 .102 .000
01335 (CM= 48.7; N= 3.00; Tp= 1.40)
01336 R0105/C00044 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01337 ADD HYD + 1.0 0212 140.66 .351 No_date 14112 5.62 n/a .000
01338 + 1.0 0212 7.98 .032 No_date 12156 4.97 n/a .000
01339 SIM= 1.0 0112 148.64 .367 No_date 14107 5.58 n/a .000
01340 R0105/C00045 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01341 ROUTE CHANNEL -> 1.0 0216 148.64 .367 No_date 14107 5.58 n/a .000
01342 (RDT= 1.00) out-< 1.0 01192 148.64 .367 No_date 14117 5.58 n/a .000
01343 (L/S/= 323./,440./,035)
01344 (Vmax=.540;Imax=.269)
01345 R0105/C00046 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01346 CALIB NASHYD 1.0 0112 14.99 .042 No_date 13121 4.43 .091 .000
01347 (CM= 39.5; N= 3.00; Tp= 1.23)
01348 R0105/C00047 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01349 ADD HYD + 1.0 0216 148.64 .367 No_date 14117 5.58 n/a .000
01350 + 1.0 0216 14.99 .042 No_date 13121 4.43 n/a .000
01351 SIM= 1.0 0112 163.63 .401 No_date 14112 5.48 n/a .000
01352 R0105/C00048 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01353 ROUTE CHANNEL -> 1.0 0215 140.66 .352 No_date 14106 5.62 n/a .000
01354 (RDT= 1.00) out-< 1.0 01193 140.66 .351 No_date 14112 5.62 n/a .000
01355 (L/S/= 181./,500./,035)
01356 (Vmax=.493;Imax=.247)
01357 R0105/C00049 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01358 CALIB NASHYD 1.0 0112 7.98 .032 No_date 12156 4.97 .102 .000
01359 (CM= 48.7; N= 3.00; Tp= 1.40)
01360 R0105/C00050 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01361 ADD HYD + 1.0 0212 140.66 .351 No_date 14112 5.62 n/a .000
01362 + 1.0 0212 7.98 .032 No_date 12156 4.97 n/a .000
01363 SIM= 1.0 0112 148.64 .367 No_date 14107 5.58 n/a .000
01364 R0105/C00051 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01365 ROUTE CHANNEL -> 1.0 0216 148.64 .367 No_date 14107 5.58 n/a .000
01366 (RDT= 1.00) out-< 1.0 01194 148.64 .367 No_date 14117 5.58 n/a .000
01367 (L/S/= 323./,440./,035)
01368 (Vmax=.540;Imax=.269)
01369 R0105/C00052 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01370 CALIB NASHYD 1.0 0112 14.99 .042 No_date 13121 4.43 .091 .000
01371 (CM= 39.5; N= 3.00; Tp= 1.23)
01372 R0105/C00053 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-RvM-R-C.-DWFCms
01373 ADD HYD + 1.0 0216 148.64 .367 No_date 14117 5.58 n/a .000
01374 + 1.0 0216 14.99 .042 No_date 13121 4.43 n/a .000
01375 SIM= 1.0 0112 163.63 .401 No_date 14112 5.48 n/a .000
01376 R0105/C00054 -> DtmIn-ID:INHYD AREA#-QFEAR#ms-TpeakDate_hh:mm-Rv
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01441: # Date      04-28-2021
01442: # Modeler    JFSaInc.
01443: # Company    JFSaInc.
01444: # License #   254923
01445: *****
01446: *****
01447: *****
01448: READ STORM
01449:   Filename = storm.001
01450:   Comment = 50 years SCS Type 2 Storm 24 hours step 10 min, City of Ottawa
01451:   [SDT=10.0]out< 24.00[PROT= 86.89]
01452: R0125:CO0002-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01453:   DEFAULT VALUES
01454:   Filename = C:\Temp\Design\Ottawa.val
01455:   ICASE5V = 2 (read values only)
01456: R0125:CO0004-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01457:   CALIB MASHYD 1.0 01:INHT-1 34.70 .124 No_date 16:57 13.66 .157 .000
01458:   [CM= 38.1: N= 3.00: Tp= 4.12]
01459: R0125:CO0005-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01460:   CALIB MASHYD 1.0 01:INHT-2 12.44 .174 No_date 13:22 21.99 n/a .000
01461:   [CM= 53.0: N= 3.00: Tp= 1.29]
01462: R0125:CO0006-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01463:   CALIB MASHYD 1.0 01:INHT-1 2.36 .082 No_date 13:13 48.59 .559 .000
01464:   [CM= 81.7: N= 3.00: Tp= 1.21]
01465: R0125:CO0007-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01466:   ADD HYD + 1.0 02:INHT-1 34.70 .124 No_date 16:57 13.66 n/a .000
01467:   + 1.0 02:INHT-2 12.44 .174 No_date 13:22 21.99 n/a .000
01468:   SIM= + 1.0 02:INHT-1 2.36 .082 No_date 13:13 48.59 n/a .000
01469:   + 1.0 02:INHT-2 12.44 .174 No_date 13:22 21.99 n/a .000
01470: R0125:CO0008-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01471:   ROUTE CHANNEL -> 1.0 02:IN1 49.51 .306 No_date 13:33 17.42 n/a .000
01472:   [RDT= 1.00] out< 1.0 01:IN1 49.51 .302 No_date 13:47 17.42 n/a .000
01473:   [L/S= 478. / 440. / 035]
01474:   [Vmax= .533:Imax= .266]
01475: R0125:CO0009-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01476:   CALIB MASHYD 1.0 01:INHT-1 4.39 .064 No_date 13:48 27.17 .313 .000
01477:   [CM= 60.4: N= 3.00: Tp= 1.64]
01478: R0125:CO0010-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01479:   CALIB MASHYD 1.0 01:INHT-2 3.61 .053 No_date 12:58 18.57 .214 .000
01480:   [CM= 47.4: N= 3.00: Tp= 1.95]
01481: R0125:CO0011-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01482:   CALIB MASHYD 1.0 01:INHT-1 10.33 .102 No_date 13:50 18.37 .214 .000
01483:   [CM= 47.4: N= 3.00: Tp= 1.66]
01484: R0125:CO0012-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01485:   CALIB MASHYD 1.0 01:INHT-1 5.71 .124 No_date 13:53 25.76 .296 .000
01486:   [CM= 58.5: N= 3.00: Tp= .89]
01487: R0125:CO0013-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01488:   ADD HYD + 1.0 02:IN1 49.51 .302 No_date 13:47 17.42 n/a .000
01489:   + 1.0 02:INHT-1 4.39 .064 No_date 13:48 27.17 n/a .000
01490:   + 1.0 02:INHT-2 12.44 .174 No_date 13:22 21.99 n/a .000
01491:   + 1.0 02:IN1 49.51 .302 No_date 13:47 17.42 n/a .000
01492:   + 1.0 02:INHT-1 5.71 .124 No_date 13:53 25.76 n/a .000
01493:   + 1.0 02:INHT-2 12.44 .174 No_date 13:22 21.99 n/a .000
01494:   SIM= + 1.0 01:IN1 49.51 .306 No_date 13:33 17.42 n/a .000
01495:   + 1.0 01:IN2 49.51 .302 No_date 13:47 17.42 n/a .000
01496:   ROUTE CHANNEL -> 1.0 01:IN1 49.51 .306 No_date 13:33 17.42 n/a .000
01497:   [RDT= 1.00] out< 1.0 01:IN2 49.51 .302 No_date 13:47 17.42 n/a .000
01498:   [L/S= 478. / 440. / 035]
01499:   [Vmax= .668:Imax= .237]
01500: R0125:CO0015-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01501:   CALIB MASHYD 1.0 01:INHT-1 25.84 .130 No_date 13:54 18.42 .184 .000
01502:   [CM= 37.6: N= 3.00: Tp= 2.09]
01503: R0125:CO0016-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01504:   CALIB MASHYD 1.0 01:INHT-2 9.14 .226 No_date 13:09 33.87 .390 .000
01505:   [CM= 64.1: N= 3.00: Tp= 1.12]
01506: R0125:CO0017-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01507:   ADD HYD + 1.0 02:IN1 73.75 .604 No_date 13:37 18.87 n/a .000
01508:   + 1.0 02:IN2 25.95 .152 No_date 14:22 13.62 n/a .000
01509:   + 1.0 02:IA2 9.14 .226 No_date 13:09 33.87 n/a .000
01510:   SIM= + 1.0 01:IN3 108.84 .944 No_date 13:33 18.83 n/a .000
01511: R0125:CO0018-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01512:   ROUTE CHANNEL -> 1.0 02:IN3 108.84 .944 No_date 13:33 18.83 n/a .000
01513:   [RDT= 1.00] out< 1.0 01:IN3 108.84 .931 No_date 13:45 18.83 n/a .000
01514:   [L/S= 396. / 305. / 035]
01515:   [Vmax= .493:Imax= .403]
01516: R0125:CO0019-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01517:   CALIB MASHYD 1.0 01:INHT-1 20.21 .147 No_date 13:32 12.43 .143 .000
01518:   [CM= 36.7: N= 3.00: Tp= .96]
01519: R0125:CO0020-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01520:   ADD HYD + 1.0 02:IN1 108.84 .931 No_date 13:45 18.83 n/a .000
01521:   + 1.0 02:IN2 25.95 .152 No_date 14:22 13.62 n/a .000
01522:   + 1.0 01:IN3 108.84 .944 No_date 13:33 18.83 n/a .000
01523:   SIM= + 1.0 01:IN4 129.05 1.076 No_date 13:43 17.83 n/a .000
01524: R0125:CO0021-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01525:   ROUTE CHANNEL -> 1.0 02:IN4 129.05 1.076 No_date 13:43 17.83 n/a .000
01526:   [RDT= 1.00] out< 1.0 01:IN4 129.05 1.062 No_date 13:56 17.83 n/a .000
01527:   [L/S= 482. / 419 / 035]
01528: R0125:CO0022-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01529:   CALIB MASHYD 1.0 01:INHT-2 11.61 .117 No_date 13:00 12.99 .150 .000
01530:   [CM= 36.7: N= 3.00: Tp= .96]
01531: R0125:CO0023-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01532:   ADD HYD + 1.0 02:IN4 129.05 1.062 No_date 13:56 17.83 n/a .000
01533:   + 1.0 02:IN1 108.84 .931 No_date 13:45 18.83 n/a .000
01534:   + 1.0 01:IN5 140.66 1.144 No_date 13:56 17.83 n/a .000
01535: R0125:CO0024-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01536:   ROUTE CHANNEL -> 1.0 02:IN5 140.66 1.144 No_date 13:56 17.83 n/a .000
01537:   [RDT= 1.00] out< 1.0 01:IN5 140.66 1.144 No_date 13:56 17.83 n/a .000
01538:   [L/S= 500. / 500. / 035]
01539:   [Vmax= .648:Imax= .373]
01540: R0125:CO0025-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01541:   CALIB MASHYD 1.0 01:INHT-3 7.98 .105 No_date 12:54 15.92 1.82 .000
01542:   [CM= 42.6: N= 3.00: Tp= .89]
01543: R0125:CO0026-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01544:   ADD HYD + 1.0 02:IN5 140.66 1.144 No_date 13:56 17.83 n/a .000
01545:   + 1.0 02:INHT-3 7.98 .105 No_date 12:54 15.92 n/a .000
01546:   + 1.0 02:INHT-2 11.61 .117 No_date 13:00 12.99 n/a .000
01547:   SIM= + 1.0 02:INHT-1 148.64 1.211 No_date 13:52 17.15 n/a .000
01548: R0125:CO0027-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01549:   ROUTE CHANNEL -> 1.0 02:IN5 140.66 1.146 No_date 13:51 17.43 n/a .000
01550:   [RDT= 1.00] out< 1.0 01:IN6 148.64 1.205 No_date 13:59 17.35 n/a .000
01551:   [L/S= 223. / 440. / 035]
01552:   [Vmax= .684:Imax= .431]
01553: R0125:CO0028-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01554:   CALIB MASHYD 1.0 01:INHT-4 14.99 .139 No_date 13:19 14.34 .165 .000
01555:   [CM= 39.5: N= 3.00: Tp= 1.23]
01556: R0125:CO0029-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01557:   ADD HYD + 1.0 02:IN6 148.64 1.205 No_date 13:59 17.15 n/a .000
01558:   + 1.0 02:INHT-4 14.99 .139 No_date 13:19 14.34 n/a .000
01559:   + 1.0 01:TOTAL 163.63 1.229 No_date 13:56 17.07 n/a .000
01560: *****
01561: *****
01562: *****
01563: *****
01564: *****
01565: *****
01566: *****
01567: *****
01568: *****
01569: *****
01570: *****
01571: [ITER= .00 hrs on 0]
01572: [MSTORM= 1]
01573: [MSTORM= 1]
01574: [MSTORM= 1]
01575: *****
01576: # SMMYNO / INPUT DATA FILE
01577: *****
01578: # Project Name: [THUNDER ROAD] Project Number: [2128]
01579: # Date 04-28-2021
01580: # Modeler JFSaInc.
01581: # Company JFSaInc.
01582: # License # 254923
01583: *****
01584: *****
01585: *****
01586: READ STORM
01587:   Filename = storm.001
01588:   Comment = 50 years SCS Type 2 Storm 24 hours step 10 min, City of Ottawa
01589:   [SDT=10.0]out< 24.00[PROT= 86.33]
01590: R0150:CO0003-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01591:   DEFAULT VALUES
01592:   Filename = C:\Temp\Design\Ottawa.val
01593:   ICASE5V = 2 (read values only)
01594: R0150:CO0004-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01595:   CALIB MASHYD 1.0 01:INHT-1 34.70 .124 No_date 16:54 16.54 .190 .000
01596:   [CM= 38.1: N= 3.00: Tp= 4.12]
01597: R0150:CO0005-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01598:   CALIB MASHYD 1.0 01:INHT-2 12.44 .211 No_date 13:22 26.61 .276 .000
01599:   [CM= 53.0: N= 3.00: Tp= 1.29]
01600: R0150:CO0006-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01601:   CALIB MASHYD 1.0 01:INHT-1 2.36 .096 No_date 13:13 56.72 .588 .000
01602:   [CM= 81.7: N= 3.00: Tp= 1.21]
01603: R0150:CO0007-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01604:   ADD HYD + 1.0 02:INHT-1 34.70 .124 No_date 16:56 16.72 n/a .000
01605:   + 1.0 02:INHT-2 12.44 .211 No_date 13:22 26.61 n/a .000
01606:   + 1.0 02:INHT-1 2.36 .096 No_date 13:13 56.72 n/a .000
01607:   + 1.0 02:INHT-2 12.44 .211 No_date 13:22 26.61 n/a .000
01608: R0150:CO0008-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01609:   ROUTE CHANNEL -> 1.0 02:IN1 49.51 .369 No_date 13:33 21.12 n/a .000
01610:   [RDT= 1.00] out< 1.0 01:IN1 49.51 .369 No_date 13:47 21.12 n/a .000
01611:   [L/S= 478. / 440. / 035]
01612:   [Vmax= .478:Imax= .266]
01613: R0150:CO0009-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01614:   CALIB MASHYD 1.0 01:INHT-1 4.39 .077 No_date 13:48 32.65 .398 .000
01615:   [CM= 60.4: N= 3.00: Tp= 1.64]
01616: R0150:CO0010-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01617:   CALIB MASHYD 1.0 01:INHT-2 3.61 .065 No_date 12:58 22.39 .234 .000
01618:   [CM= 47.4: N= 3.00: Tp= .95]
01619: R0150:CO0011-----DtmIn-ID:INHYD-----AREAA-QFEARms-TpeakDate_hh:mm-----RvM-R-C-----DWfms
01620:   CALIB MASHYD 1.0 01:INHT-1 10.33 .124 No_date 13:49 22.58 .234 .000

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01801* [L/S/n= 482./ .410/.035]
01802* [Vmax= .700;Dmax= .484]
01803* R0199:CO0022-----DtnIn-ID:NBHYD-----AREAh-QFEARgms-TpeakDate_hh:mm-----RVm-R.C-----DWFcms
01804* CALIB NASHYD 1.0 01:SOOUTH-2 11.61 .174 No_date 12:59 19.28 .181 .000
01805* [Ck= 26.7; N= 3.00; Tp= .86]
01806* R0199:CO0023-----DtnIn-ID:NBHYD-----AREAh-QFEARgms-TpeakDate_hh:mm-----RVm-R.C-----DWFcms
01807* ADD HYD 1.0 02:R80 129.05 1.554 No_date 13:52 25.35 n/a .000
01808* + 1.0 02:SOOUTH-2 11.61 .174 No_date 12:59 19.28 n/a .000
01809* SIM= 1.0 01:25 140.66 1.683 No_date 13:47 25.35 n/a .000
01810* R0199:CO0024-----DtnIn-ID:NBHYD-----AREAh-QFEARgms-TpeakDate_hh:mm-----RVm-R.C-----DWFcms
01811* ROUTE CHANNEL -> 1.0 02:25 140.66 1.683 No_date 13:47 25.35 n/a .000
01812* [RD= 1.00] out<- 1.0 01:R85 140.66 1.679 No_date 13:52 25.35 n/a .000
01813* [L/S/n= 181./ .500/.035]
01814* [Vmax= .668;Dmax= .420]
01815* R0199:CO0025-----DtnIn-ID:NBHYD-----AREAh-QFEARgms-TpeakDate_hh:mm-----RVm-R.C-----DWFcms
01816* CALIB NASHYD 1.0 01:SOOUTH-3 7.98 .155 No_date 12:54 23.44 .220 .000
01817* [Ck= 42.6; N= 3.00; Tp= .89]
01818* R0199:CO0026-----DtnIn-ID:NBHYD-----AREAh-QFEARgms-TpeakDate_hh:mm-----RVm-R.C-----DWFcms
01819* ADD HYD 1.0 02:R80 140.66 1.679 No_date 13:52 25.35 n/a .000
01820* + 1.0 02:SOOUTH-3 7.98 .155 No_date 12:54 23.44 n/a .000
01821* SIM= 1.0 01:26 148.64 1.784 No_date 13:47 25.25 n/a .000
01822* R0199:CO0027-----DtnIn-ID:NBHYD-----AREAh-QFEARgms-TpeakDate_hh:mm-----RVm-R.C-----DWFcms
01823* ROUTE CHANNEL -> 1.0 02:26 148.64 1.784 No_date 13:47 25.25 n/a .000
01824* [RD= 1.00] out<- 1.0 01:R86 148.64 1.775 No_date 13:54 25.25 n/a .000
01825* [L/S/n= 323./ .440/.035]
01826* [Vmax= .735;Dmax= .500]
01827* R0199:CO0028-----DtnIn-ID:NBHYD-----AREAh-QFEARgms-TpeakDate_hh:mm-----RVm-R.C-----DWFcms
01828* CALIB NASHYD 1.0 01:SOOUTH-4 14.99 .207 No_date 13:18 21.21 .199 .000
01829* [Ck= 39.5; N= 3.00; Tp= 1.23]
01830* R0199:CO0029-----DtnIn-ID:NBHYD-----AREAh-QFEARgms-TpeakDate_hh:mm-----RVm-R.C-----DWFcms
01831* ADD HYD 1.0 02:R86 148.64 1.775 No_date 13:54 25.25 n/a .000
01832* + 1.0 02:SOOUTH-4 14.99 .207 No_date 13:18 21.21 n/a .000
01833* SIM= 1.0 01:Total 163.63 1.862 No_date 13:51 24.88 n/a .000
01834* #-----
01835* #-----
01836* R0199:CO0002-----
01837* FINISH
01838* #-----
01839* #-----
01840* #-----
01841* #-----
01842* #-----
01843* #-----
01844* #-----

```

Attachment C

Hydraulic Model



Legend

- Cross Section
- Watercourse
- Bank Markers



SCALE: 1:5000

0 100 200 m

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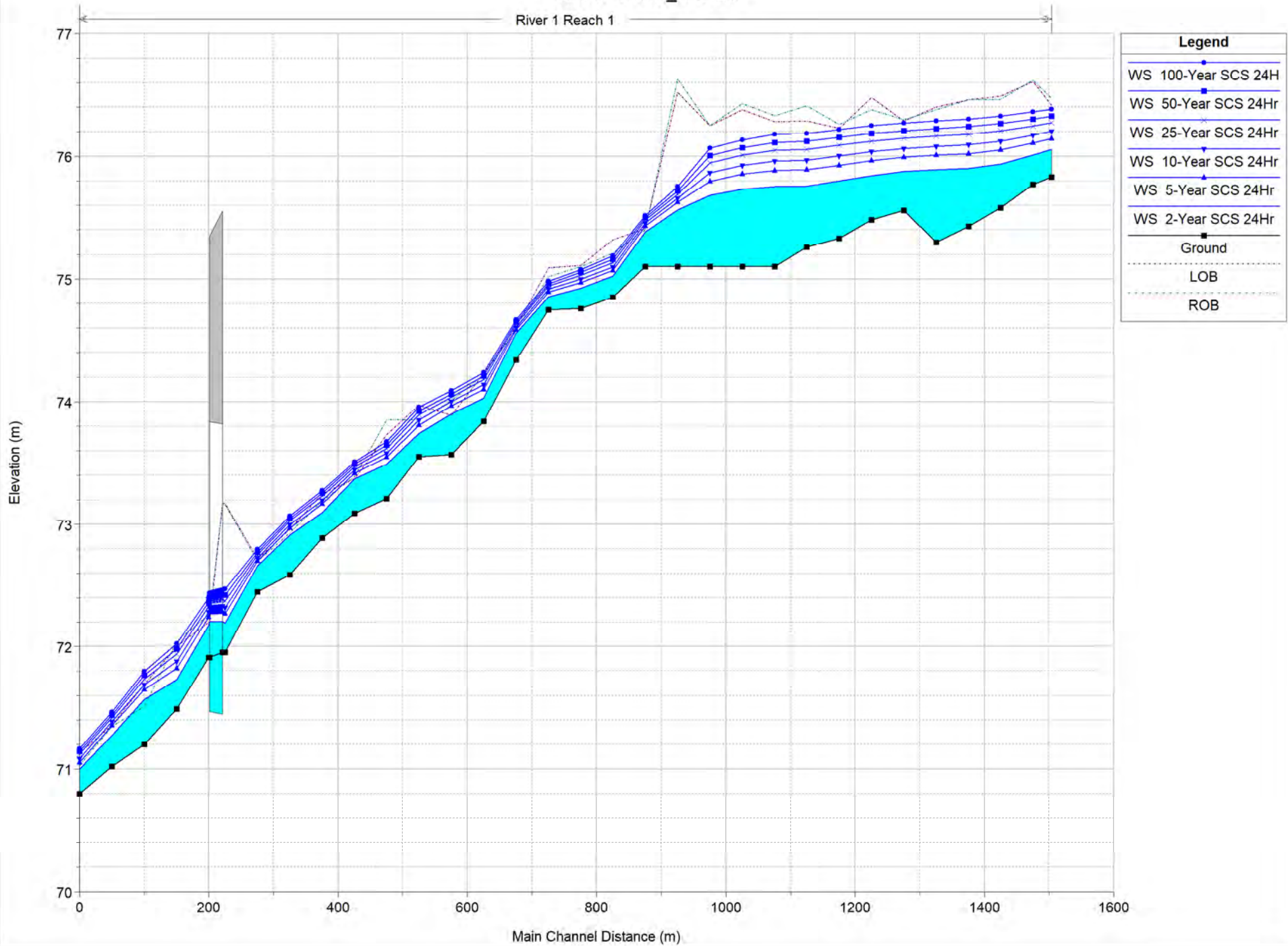
6150 Thunder Road:
Floodplain Mapping

Figure C1: HEC-RAS Model Overview

PROJECT	2120-21
DRAWN	MP
DATE	06-28-2021

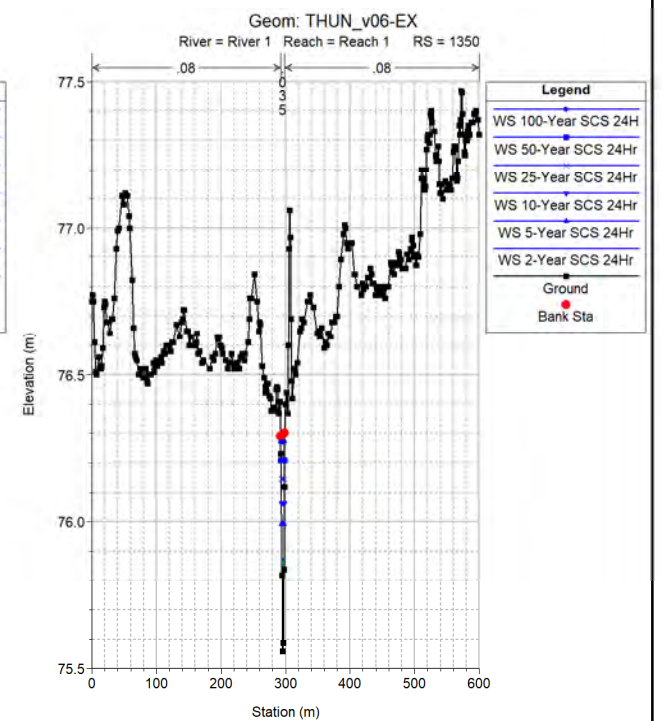
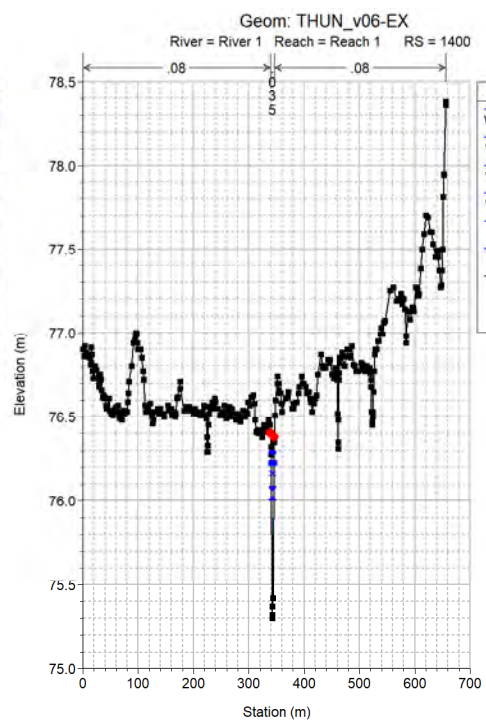
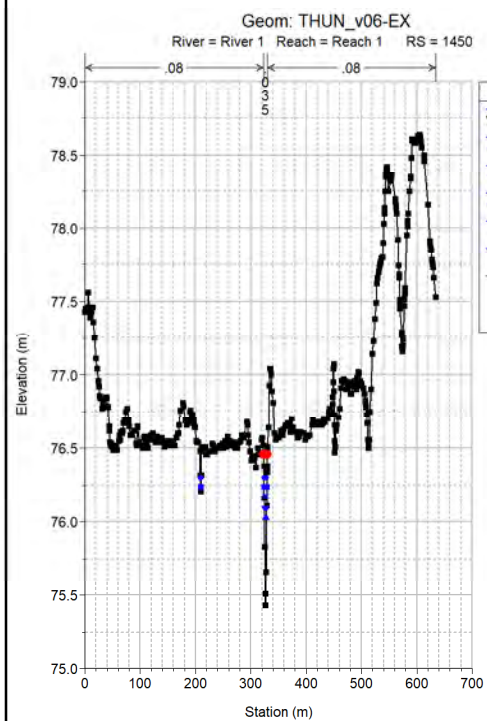
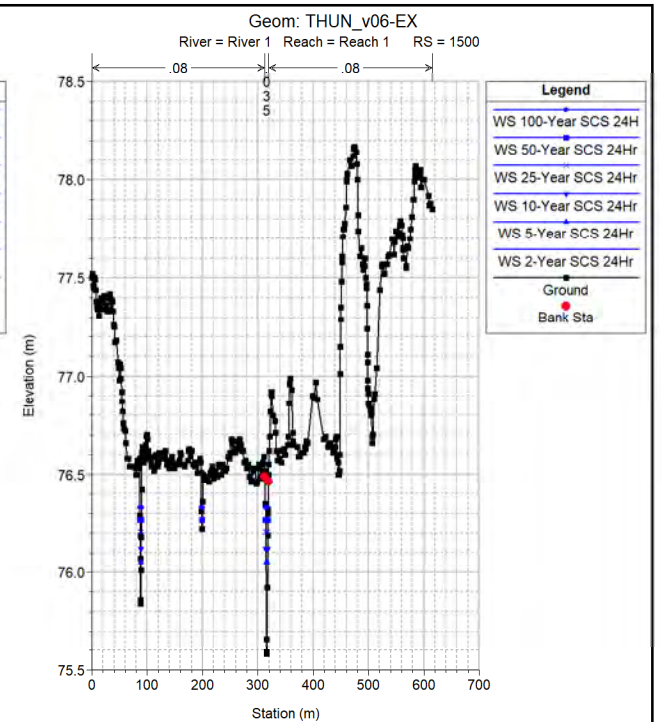
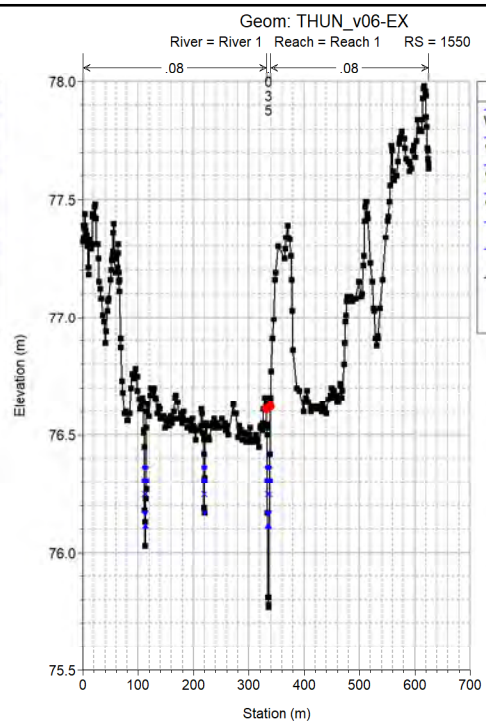
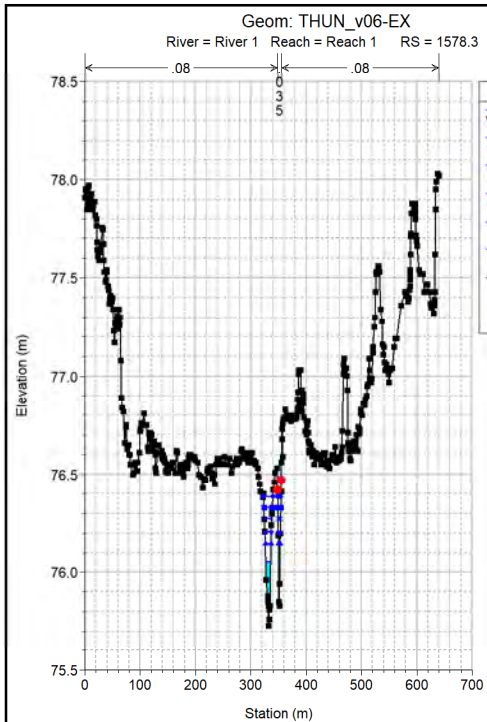
Geom: THUN_v06-EX

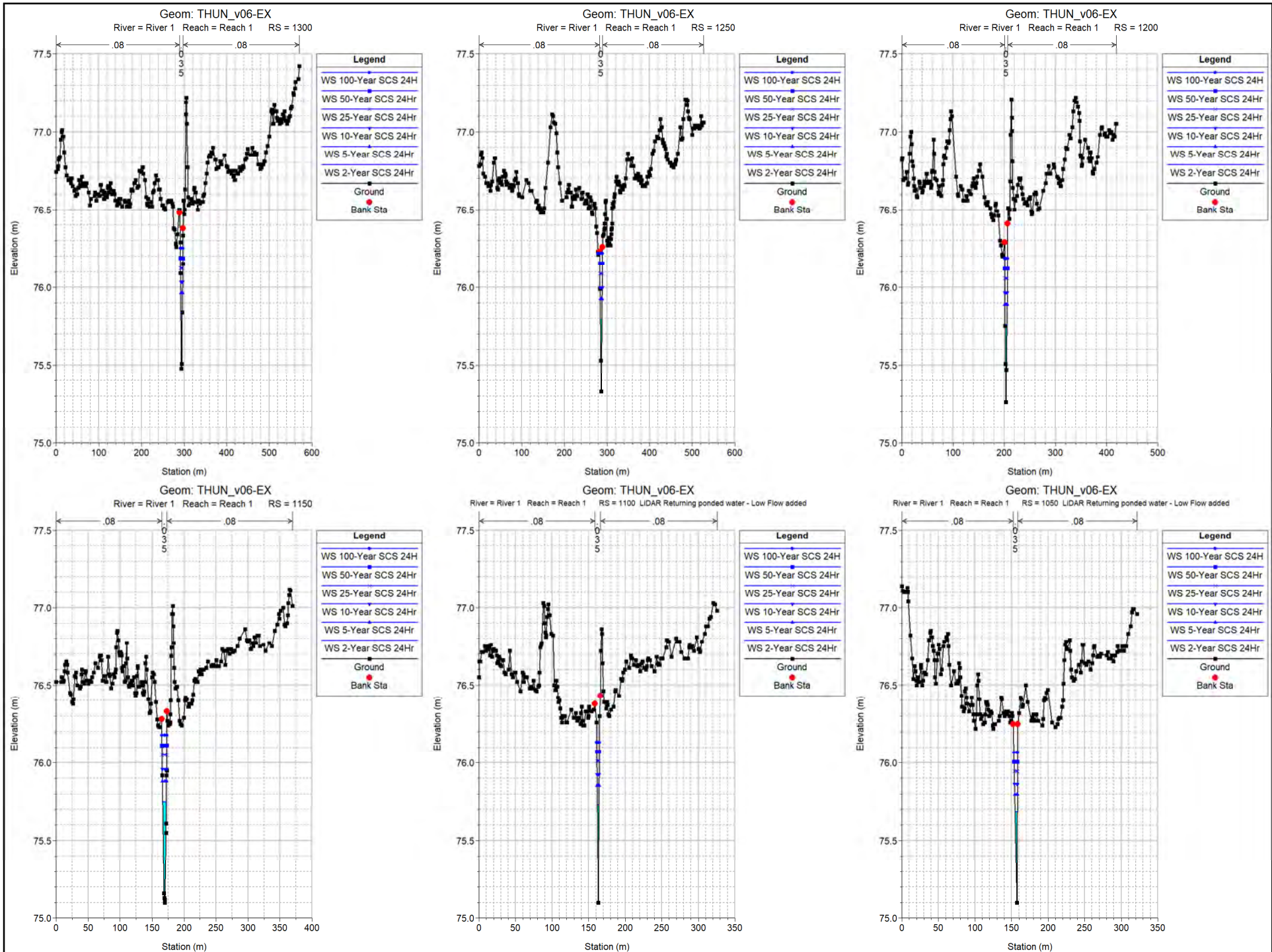
River 1 Reach 1

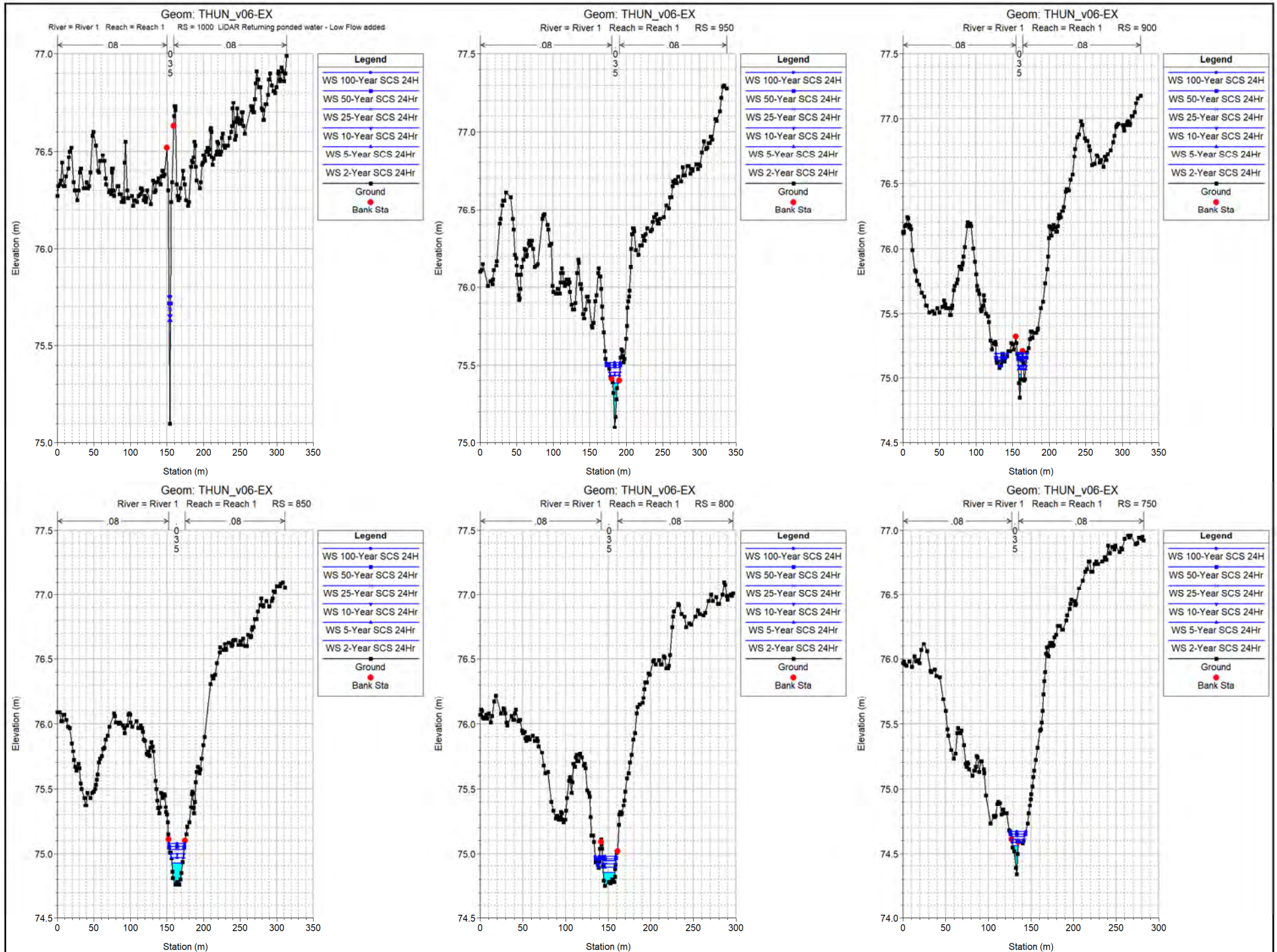


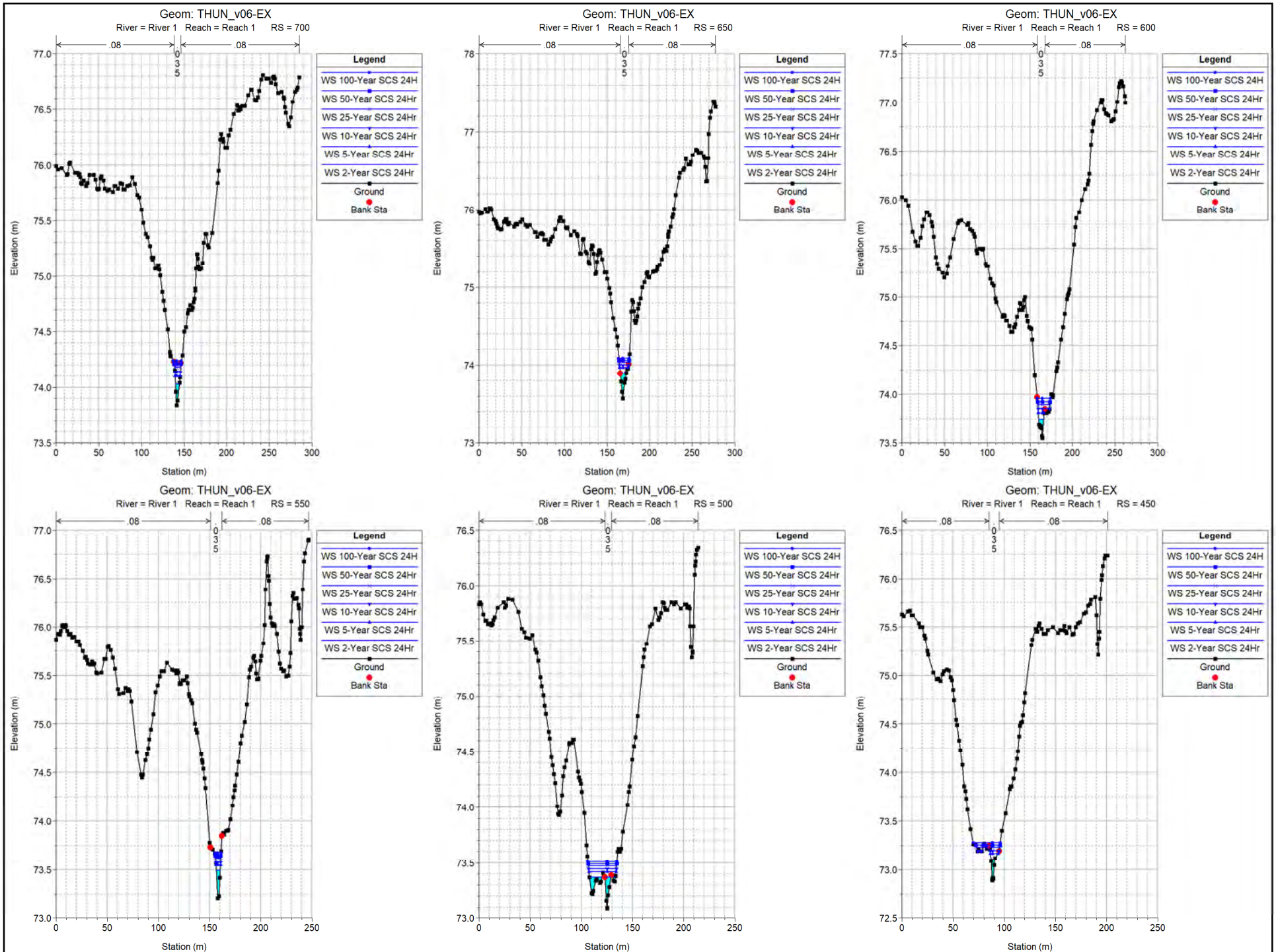
Legend

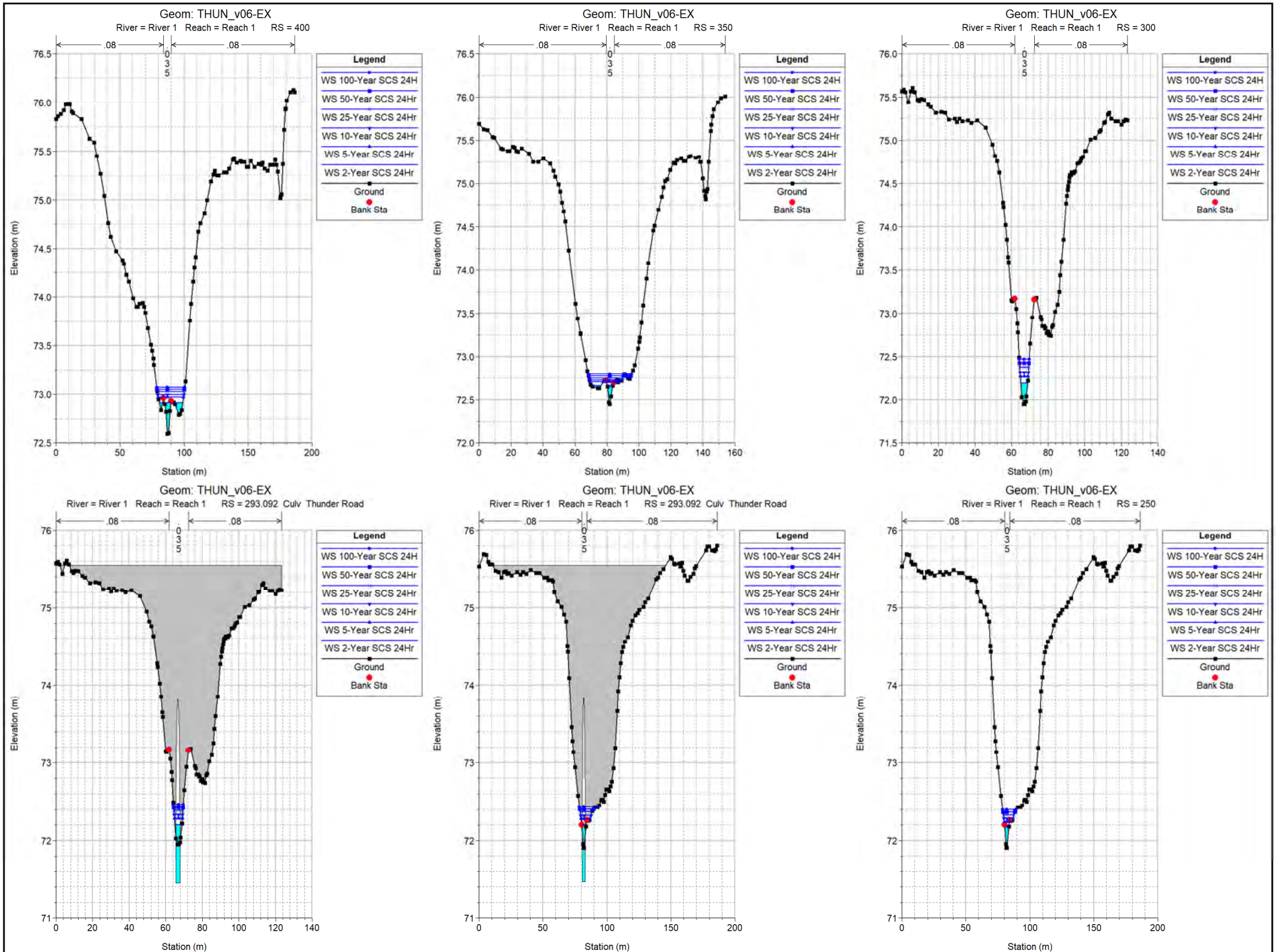
- WS 100-Year SCS 24Hr
- WS 50-Year SCS 24Hr
- WS 25-Year SCS 24Hr
- WS 10-Year SCS 24Hr
- WS 5-Year SCS 24Hr
- WS 2-Year SCS 24Hr
- Ground
- LOB
- ROB

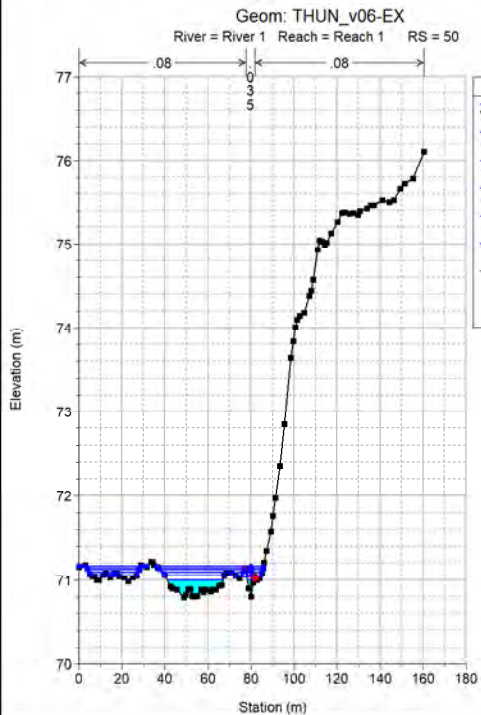
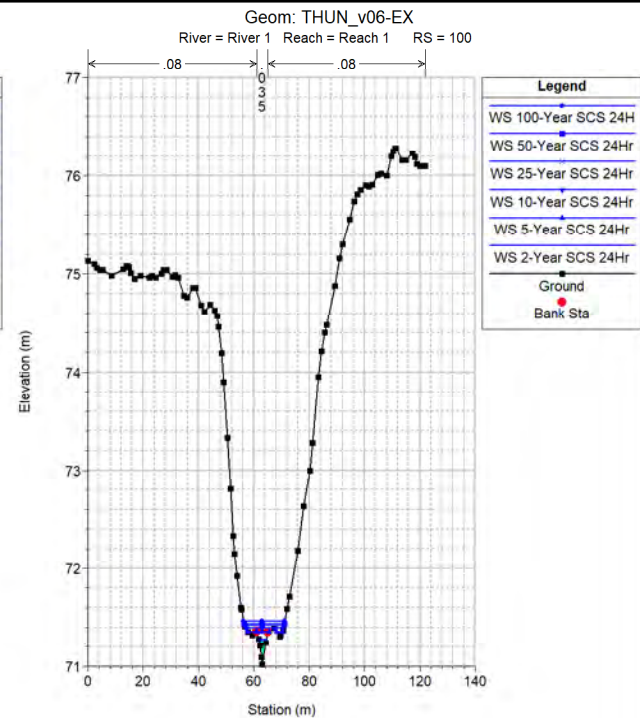
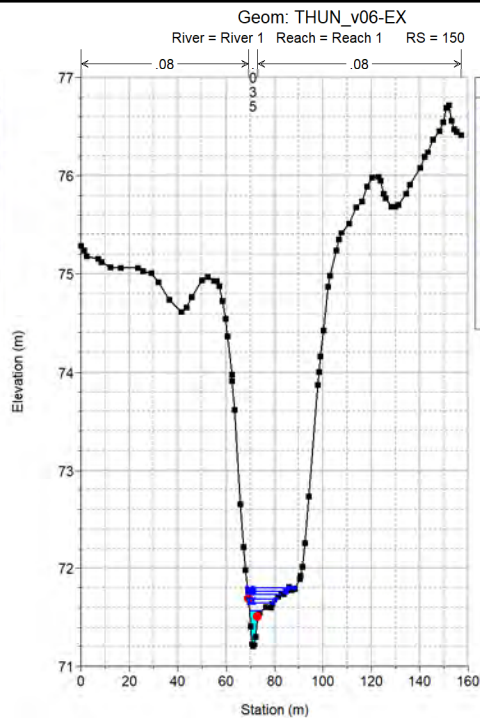
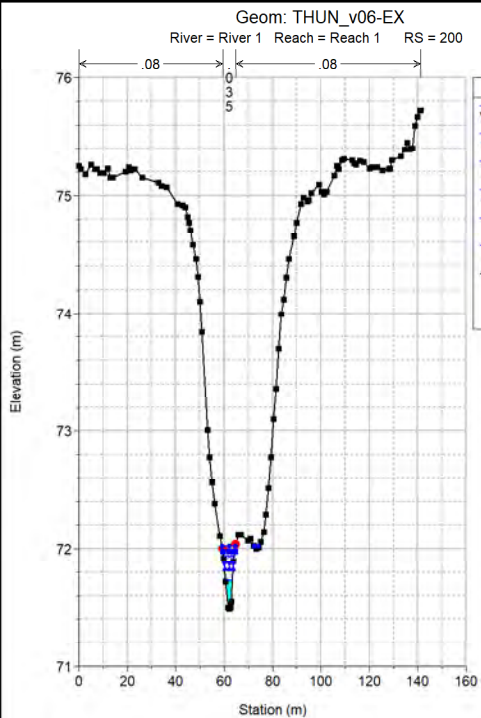












Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
Reach 1	1578.3	2-Year SCS 24Hr	0.19	75.83	76.06		76.06	0.000501	0.16	1.89	11.79	0.14
Reach 1	1578.3	5-Year SCS 24Hr	0.34	75.83	76.14		76.15	0.000390	0.18	3.06	14.26	0.13
Reach 1	1578.3	10-Year SCS 24Hr	0.45	75.83	76.20		76.20	0.000334	0.18	3.95	15.91	0.13
Reach 1	1578.3	25-Year SCS 24Hr	0.60	75.83	76.27		76.28	0.000290	0.19	5.17	18.32	0.12
Reach 1	1578.3	50-Year SCS 24Hr	0.73	75.83	76.33		76.33	0.000264	0.19	6.20	20.47	0.12
Reach 1	1578.3	100-Year SCS 24H	0.87	75.83	76.38		76.39	0.000240	0.19	7.43	23.59	0.11
Reach 1	1550	2-Year SCS 24Hr	0.19	75.77	76.01		76.02	0.003996	0.51	0.38	2.49	0.41
Reach 1	1550	5-Year SCS 24Hr	0.34	75.77	76.11		76.12	0.002633	0.50	0.73	4.56	0.35
Reach 1	1550	10-Year SCS 24Hr	0.45	75.77	76.17		76.18	0.002038	0.49	1.06	5.72	0.32
Reach 1	1550	25-Year SCS 24Hr	0.60	75.77	76.25		76.26	0.001520	0.47	1.57	7.52	0.28
Reach 1	1550	50-Year SCS 24Hr	0.73	75.77	76.30		76.31	0.001253	0.46	2.02	8.47	0.26
Reach 1	1550	100-Year SCS 24H	0.87	75.77	76.36		76.37	0.001049	0.45	2.55	9.40	0.24
Reach 1	1500	2-Year SCS 24Hr	0.19	75.58	75.94		75.94	0.000838	0.30	0.68	3.64	0.20
Reach 1	1500	5-Year SCS 24Hr	0.34	75.58	76.05		76.06	0.000689	0.32	1.18	4.85	0.19
Reach 1	1500	10-Year SCS 24Hr	0.45	75.58	76.12		76.13	0.000629	0.34	1.55	5.51	0.18
Reach 1	1500	25-Year SCS 24Hr	0.60	75.58	76.21		76.21	0.000580	0.35	2.03	6.20	0.18
Reach 1	1500	50-Year SCS 24Hr	0.73	75.58	76.27		76.27	0.000550	0.36	2.45	7.75	0.18
Reach 1	1500	100-Year SCS 24H	0.87	75.58	76.33		76.33	0.000529	0.37	2.98	9.25	0.18
Reach 1	1450	2-Year SCS 24Hr	0.19	75.43	75.90		75.91	0.000567	0.26	0.74	3.03	0.17
Reach 1	1450	5-Year SCS 24Hr	0.34	75.43	76.02		76.03	0.000553	0.29	1.15	3.79	0.17
Reach 1	1450	10-Year SCS 24Hr	0.45	75.43	76.10		76.10	0.000536	0.31	1.45	4.25	0.17
Reach 1	1450	25-Year SCS 24Hr	0.60	75.43	76.18		76.19	0.000508	0.33	1.82	4.70	0.17
Reach 1	1450	50-Year SCS 24Hr	0.73	75.43	76.24		76.25	0.000489	0.34	2.13	5.62	0.17
Reach 1	1450	100-Year SCS 24H	0.87	75.43	76.30		76.31	0.000470	0.36	2.53	7.18	0.17
Reach 1	1400	2-Year SCS 24Hr	0.19	75.30	75.89		75.89	0.000135	0.15	1.24	3.68	0.08
Reach 1	1400	5-Year SCS 24Hr	0.34	75.30	76.01		76.01	0.000177	0.20	1.71	4.30	0.10
Reach 1	1400	10-Year SCS 24Hr	0.45	75.30	76.08		76.08	0.000197	0.22	2.04	4.67	0.11
Reach 1	1400	25-Year SCS 24Hr	0.60	75.30	76.17		76.17	0.000217	0.25	2.45	5.11	0.11
Reach 1	1400	50-Year SCS 24Hr	0.73	75.30	76.23		76.23	0.000228	0.26	2.77	5.43	0.12
Reach 1	1400	100-Year SCS 24H	0.87	75.30	76.29		76.29	0.000237	0.28	3.12	5.75	0.12
Reach 1	1350	2-Year SCS 24Hr	0.19	75.56	75.87		75.88	0.000872	0.28	0.69	3.52	0.20
Reach 1	1350	5-Year SCS 24Hr	0.34	75.56	75.99		76.00	0.000658	0.30	1.15	4.38	0.18
Reach 1	1350	10-Year SCS 24Hr	0.45	75.56	76.06		76.07	0.000578	0.30	1.48	4.91	0.18
Reach 1	1350	25-Year SCS 24Hr	0.60	75.56	76.15		76.15	0.000511	0.31	1.92	5.49	0.17
Reach 1	1350	50-Year SCS 24Hr	0.73	75.56	76.21		76.21	0.000470	0.32	2.27	5.87	0.17
Reach 1	1350	100-Year SCS 24H	0.87	75.56	76.27		76.28	0.000437	0.33	2.65	6.26	0.16
Reach 1	1300	2-Year SCS 24Hr	0.19	75.48	75.84		75.84	0.000582	0.25	0.76	3.28	0.17
Reach 1	1300	5-Year SCS 24Hr	0.34	75.48	75.96		75.97	0.000513	0.28	1.21	4.12	0.16
Reach 1	1300	10-Year SCS 24Hr	0.45	75.48	76.04		76.04	0.000479	0.29	1.54	4.63	0.16
Reach 1	1300	25-Year SCS 24Hr	0.60	75.48	76.12		76.13	0.000447	0.31	1.96	5.21	0.16
Reach 1	1300	50-Year SCS 24Hr	0.73	75.48	76.19		76.19	0.000421	0.32	2.30	5.57	0.16
Reach 1	1300	100-Year SCS 24H	0.87	75.48	76.25		76.26	0.000399	0.33	2.67	5.90	0.16
Reach 1	1250	2-Year SCS 24Hr	0.30	75.33	75.80		75.80	0.001001	0.34	0.89	3.72	0.22
Reach 1	1250	5-Year SCS 24Hr	0.53	75.33	75.92		75.93	0.000874	0.37	1.42	4.70	0.22
Reach 1	1250	10-Year SCS 24Hr	0.71	75.33	76.00		76.01	0.000811	0.39	1.81	5.26	0.21
Reach 1	1250	25-Year SCS 24Hr	0.94	75.33	76.09		76.10	0.000743	0.41	2.29	5.74	0.21
Reach 1	1250	50-Year SCS 24Hr	1.14	75.33	76.15		76.16	0.000709	0.43	2.67	6.09	0.21
Reach 1	1250	100-Year SCS 24H	1.37	75.33	76.22		76.23	0.000684	0.44	3.08	7.68	0.21
Reach 1	1200	2-Year SCS 24Hr	0.30	75.26	75.76		75.76	0.000657	0.29	1.03	3.94	0.18
Reach 1	1200	5-Year SCS 24Hr	0.53	75.26	75.89		75.90	0.000583	0.33	1.58	4.49	0.18
Reach 1	1200	10-Year SCS 24Hr	0.71	75.26	75.97		75.98	0.000573	0.36	1.95	4.81	0.18
Reach 1	1200	25-Year SCS 24Hr	0.94	75.26	76.06		76.07	0.000576	0.39	2.39	5.18	0.19
Reach 1	1200	50-Year SCS 24Hr	1.14	75.26	76.12		76.13	0.000581	0.42	2.74	5.45	0.19
Reach 1	1200	100-Year SCS 24H	1.37	75.26	76.19		76.20	0.000577	0.44	3.10	5.60	0.19
Reach 1	1150	2-Year SCS 24Hr	0.30	75.10	75.75		75.75	0.000083	0.13	2.23	5.80	0.07
Reach 1	1150	5-Year SCS 24Hr	0.53	75.10	75.88		75.88	0.000110	0.17	3.05	6.66	0.08
Reach 1	1150	10-Year SCS 24Hr	0.71	75.10	75.96		75.96	0.000127	0.20	3.59	7.25	0.09
Reach 1	1150	25-Year SCS 24Hr	0.94	75.10	76.05		76.05	0.000136	0.22	4.24	7.41	0.09
Reach 1	1150	50-Year SCS 24Hr	1.14	75.10	76.11		76.12	0.000144	0.24	4.72	7.53	0.10
Reach 1	1150	100-Year SCS 24H	1.37	75.10	76.18		76.18	0.000153	0.26	5.22	7.70	0.10
Reach 1	1100	2-Year SCS 24Hr	0.30	75.10	75.73		75.74	0.001304	0.43	0.69	2.19	0.25
Reach 1	1100	5-Year SCS 24Hr	0.53	75.10	75.85		75.87	0.001563	0.54	0.99	2.62	0.28
Reach 1	1100	10-Year SCS 24Hr	0.71	75.10	75.93		75.94	0.001695	0.59	1.19	2.87	0.29
Reach 1	1100	25-Year SCS 24Hr	0.94	75.10	76.01		76.03	0.001814	0.65	1.44	3.17	0.31
Reach 1	1100	50-Year SCS 24Hr	1.14	75.10	76.07		76.10	0.001883	0.70	1.64	3.38	0.32
Reach 1	1100	100-Year SCS 24H	1.37	75.10	76.13		76.16	0.001947	0.74	1.85	3.59	0.33

HEC-RAS Plan: THUN_v06-EX-Normal River: River 1 Reach: Reach 1 (Continued)

Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
Reach 1	1050	2-Year SCS 24Hr	0.30	75.10	75.68		75.69	0.000849	0.34	0.88	3.03	0.20
Reach 1	1050	5-Year SCS 24Hr	0.53	75.10	75.80		75.81	0.001010	0.42	1.26	3.63	0.23
Reach 1	1050	10-Year SCS 24Hr	0.71	75.10	75.86		75.88	0.001082	0.46	1.53	3.99	0.24
Reach 1	1050	25-Year SCS 24Hr	0.94	75.10	75.95		75.96	0.001130	0.51	1.87	4.42	0.25
Reach 1	1050	50-Year SCS 24Hr	1.14	75.10	76.01		76.02	0.001150	0.53	2.14	4.73	0.25
Reach 1	1050	100-Year SCS 24H	1.37	75.10	76.07		76.08	0.001166	0.56	2.44	5.04	0.26
Reach 1	1000	2-Year SCS 24Hr	0.30	75.10	75.56		75.59	0.006456	0.79	0.38	1.66	0.52
Reach 1	1000	5-Year SCS 24Hr	0.53	75.10	75.63		75.68	0.009734	1.06	0.50	1.90	0.66
Reach 1	1000	10-Year SCS 24Hr	0.71	75.10	75.66		75.74	0.012751	1.26	0.56	2.01	0.76
Reach 1	1000	25-Year SCS 24Hr	0.94	75.10	75.69	75.66	75.81	0.016905	1.51	0.63	2.12	0.88
Reach 1	1000	50-Year SCS 24Hr	1.14	75.10	75.72	75.70	75.86	0.019355	1.68	0.69	2.22	0.95
Reach 1	1000	100-Year SCS 24H	1.37	75.10	75.75	75.75	75.92	0.020954	1.79	0.76	2.34	1.00
Reach 1	950	2-Year SCS 24Hr	0.30	75.10	75.38		75.39	0.002647	0.34	0.89	8.11	0.32
Reach 1	950	5-Year SCS 24Hr	0.53	75.10	75.43	75.32	75.44	0.002665	0.38	1.42	12.89	0.34
Reach 1	950	10-Year SCS 24Hr	0.71	75.10	75.46	75.34	75.46	0.002704	0.43	1.73	13.69	0.35
Reach 1	950	25-Year SCS 24Hr	0.94	75.10	75.48	75.38	75.50	0.002768	0.49	2.12	14.67	0.36
Reach 1	950	50-Year SCS 24Hr	1.14	75.10	75.50	75.40	75.51	0.002982	0.54	2.38	15.61	0.38
Reach 1	950	100-Year SCS 24H	1.37	75.10	75.52		75.53	0.003310	0.59	2.66	19.37	0.41
Reach 1	900	2-Year SCS 24Hr	0.34	74.85	75.03	75.03	75.07	0.024526	0.93	0.41	5.56	0.96
Reach 1	900	5-Year SCS 24Hr	0.60	74.85	75.07	75.07	75.12	0.022290	1.05	0.69	7.05	0.96
Reach 1	900	10-Year SCS 24Hr	0.80	74.85	75.10	75.10	75.15	0.020424	1.10	0.93	11.16	0.94
Reach 1	900	25-Year SCS 24Hr	1.08	74.85	75.13	75.13	75.19	0.018154	1.13	1.38	16.59	0.90
Reach 1	900	50-Year SCS 24Hr	1.31	74.85	75.16	75.16	75.21	0.015717	1.08	1.93	21.33	0.85
Reach 1	900	100-Year SCS 24H	1.57	74.85	75.19	75.18	75.23	0.013463	1.00	2.66	27.61	0.78
Reach 1	850	2-Year SCS 24Hr	0.34	74.76	74.93		74.93	0.000687	0.18	1.82	14.90	0.17
Reach 1	850	5-Year SCS 24Hr	0.60	74.76	74.97		74.97	0.000833	0.24	2.52	16.35	0.19
Reach 1	850	10-Year SCS 24Hr	0.80	74.76	75.00		75.00	0.000917	0.27	2.99	17.48	0.21
Reach 1	850	25-Year SCS 24Hr	1.08	74.76	75.03		75.04	0.001043	0.30	3.63	19.86	0.22
Reach 1	850	50-Year SCS 24Hr	1.31	74.76	75.05		75.06	0.001102	0.32	4.09	20.84	0.23
Reach 1	850	100-Year SCS 24H	1.57	74.76	75.08		75.08	0.001143	0.34	4.58	21.60	0.24
Reach 1	800	2-Year SCS 24Hr	0.34	74.75	74.85		74.86	0.003912	0.32	1.06	14.05	0.37
Reach 1	800	5-Year SCS 24Hr	0.60	74.75	74.89		74.90	0.003188	0.37	1.61	14.86	0.36
Reach 1	800	10-Year SCS 24Hr	0.80	74.75	74.92		74.93	0.003012	0.40	2.00	17.26	0.36
Reach 1	800	25-Year SCS 24Hr	1.08	74.75	74.94		74.95	0.003150	0.45	2.46	19.71	0.37
Reach 1	800	50-Year SCS 24Hr	1.31	74.75	74.96		74.97	0.003158	0.49	2.84	20.42	0.38
Reach 1	800	100-Year SCS 24H	1.57	74.75	74.98		74.99	0.003193	0.52	3.25	21.25	0.39
Reach 1	750	2-Year SCS 24Hr	0.34	74.34	74.56		74.58	0.009113	0.55	0.61	6.83	0.58
Reach 1	750	5-Year SCS 24Hr	0.60	74.34	74.59	74.56	74.61	0.012899	0.73	0.83	11.85	0.71
Reach 1	750	10-Year SCS 24Hr	0.80	74.34	74.61	74.59	74.64	0.013823	0.82	1.08	14.17	0.75
Reach 1	750	25-Year SCS 24Hr	1.08	74.34	74.63	74.61	74.67	0.012654	0.89	1.46	15.95	0.74
Reach 1	750	50-Year SCS 24Hr	1.31	74.34	74.65	74.63	74.69	0.011955	0.93	1.77	17.32	0.74
Reach 1	750	100-Year SCS 24H	1.57	74.34	74.67	74.65	74.71	0.011632	0.99	2.09	18.64	0.74
Reach 1	700	2-Year SCS 24Hr	0.34	73.84	74.03		74.06	0.011968	0.69	0.49	4.63	0.68
Reach 1	700	5-Year SCS 24Hr	0.60	73.84	74.10		74.13	0.007675	0.70	0.86	5.84	0.58
Reach 1	700	10-Year SCS 24Hr	0.80	73.84	74.14		74.17	0.006825	0.73	1.09	6.34	0.56
Reach 1	700	25-Year SCS 24Hr	1.08	73.84	74.18		74.21	0.006863	0.79	1.37	7.09	0.57
Reach 1	700	50-Year SCS 24Hr	1.31	73.84	74.21		74.25	0.006912	0.83	1.58	7.68	0.58
Reach 1	700	100-Year SCS 24H	1.57	73.84	74.24		74.28	0.006844	0.87	1.81	9.14	0.59
Reach 1	650	2-Year SCS 24Hr	0.34	73.57	73.90		73.90	0.001266	0.30	1.12	7.08	0.24
Reach 1	650	5-Year SCS 24Hr	0.60	73.57	73.97		73.97	0.001559	0.36	1.67	9.59	0.27
Reach 1	650	10-Year SCS 24Hr	0.80	73.57	74.00		74.01	0.001694	0.40	2.02	10.73	0.29
Reach 1	650	25-Year SCS 24Hr	1.08	73.57	74.04		74.05	0.001824	0.46	2.41	11.43	0.30
Reach 1	650	50-Year SCS 24Hr	1.31	73.57	74.06		74.07	0.001918	0.50	2.70	11.83	0.32
Reach 1	650	100-Year SCS 24H	1.57	73.57	74.09		74.10	0.001954	0.54	3.03	12.27	0.33
Reach 1	600	2-Year SCS 24Hr	0.34	73.55	73.74		73.76	0.011563	0.62	0.54	5.95	0.66
Reach 1	600	5-Year SCS 24Hr	0.60	73.55	73.81		73.83	0.006732	0.62	0.96	6.96	0.54
Reach 1	600	10-Year SCS 24Hr	0.80	73.55	73.85		73.87	0.005389	0.61	1.42	13.43	0.49
Reach 1	600	25-Year SCS 24Hr	1.08	73.55	73.89		73.91	0.004411	0.63	1.99	14.20	0.46
Reach 1	600	50-Year SCS 24Hr	1.31	73.55	73.92		73.94	0.003903	0.64	2.44	14.80	0.44
Reach 1	600	100-Year SCS 24H	1.57	73.55	73.96		73.98	0.003520	0.66	2.93	15.52	0.43
Reach 1	550	2-Year SCS 24Hr	0.34	73.21	73.49		73.50	0.002883	0.48	0.70	3.94	0.36
Reach 1	550	5-Year SCS 24Hr	0.60	73.21	73.55		73.57	0.004145	0.64	0.93	4.45	0.45
Reach 1	550	10-Year SCS 24Hr	0.80	73.21	73.58		73.61	0.005036	0.74	1.08	4.78	0.50
Reach 1	550	25-Year SCS 24Hr	1.08	73.21	73.62		73.65	0.006029	0.85	1.27	5.31	0.55
Reach 1	550	50-Year SCS 24Hr	1.31	73.21	73.65		73.69	0.006738	0.92	1.42	5.69	0.59

HEC-RAS Plan: THUN_v06-EX-Normal River: River 1 Reach: Reach 1 (Continued)

Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
Reach 1	550	100-Year SCS 24H	1.57	73.21	73.67		73.72	0.007525	0.98	1.59	6.28	0.62
Reach 1	500	2-Year SCS 24Hr	0.34	73.09	73.37		73.37	0.002287	0.35	1.58	20.54	0.31
Reach 1	500	5-Year SCS 24Hr	0.60	73.09	73.42		73.42	0.002040	0.39	2.74	26.50	0.31
Reach 1	500	10-Year SCS 24Hr	0.80	73.09	73.44		73.45	0.002009	0.43	3.42	27.02	0.31
Reach 1	500	25-Year SCS 24Hr	1.08	73.09	73.47		73.48	0.002112	0.48	4.17	27.59	0.32
Reach 1	500	50-Year SCS 24Hr	1.31	73.09	73.49		73.50	0.002236	0.52	4.70	27.98	0.34
Reach 1	500	100-Year SCS 24H	1.57	73.09	73.51		73.52	0.002353	0.56	5.24	28.38	0.35
Reach 1	450	2-Year SCS 24Hr	0.35	72.89	73.10		73.13	0.015107	0.83	0.42	3.65	0.78
Reach 1	450	5-Year SCS 24Hr	0.63	72.89	73.17		73.20	0.015754	0.81	0.78	7.25	0.79
Reach 1	450	10-Year SCS 24Hr	0.85	72.89	73.20		73.23	0.014907	0.82	1.03	10.53	0.78
Reach 1	450	25-Year SCS 24Hr	1.15	72.89	73.23	73.20	73.27	0.012266	0.85	1.50	16.87	0.73
Reach 1	450	50-Year SCS 24Hr	1.40	72.89	73.25	73.22	73.29	0.010661	0.85	1.97	21.50	0.69
Reach 1	450	100-Year SCS 24H	1.68	72.89	73.28	73.24	73.31	0.009243	0.87	2.55	26.52	0.66
Reach 1	400	2 Year SCS 24Hr	0.35	72.59	72.91		72.92	0.001877	0.37	1.37	14.05	0.29
Reach 1	400	5-Year SCS 24Hr	0.63	72.59	72.97		72.98	0.002010	0.42	2.39	19.65	0.31
Reach 1	400	10-Year SCS 24Hr	0.85	72.59	73.00		73.01	0.002095	0.47	2.95	20.28	0.32
Reach 1	400	25-Year SCS 24Hr	1.15	72.59	73.03		73.04	0.002299	0.54	3.57	20.96	0.34
Reach 1	400	50-Year SCS 24Hr	1.40	72.59	73.05		73.06	0.002502	0.59	4.01	21.36	0.36
Reach 1	400	100-Year SCS 24H	1.68	72.59	73.07		73.08	0.002727	0.65	4.45	21.75	0.39
Reach 1	350	2-Year SCS 24Hr	0.35	72.45	72.66	72.66	72.70	0.018168	0.88	0.51	9.43	0.85
Reach 1	350	5-Year SCS 24Hr	0.63	72.45	72.70	72.70	72.74	0.021074	0.95	0.97	13.55	0.91
Reach 1	350	10-Year SCS 24Hr	0.85	72.45	72.73	72.73	72.77	0.018929	1.00	1.36	19.98	0.89
Reach 1	350	25-Year SCS 24Hr	1.15	72.45	72.75	72.75	72.79	0.016479	1.05	1.88	22.47	0.85
Reach 1	350	50-Year SCS 24Hr	1.40	72.45	72.77	72.76	72.81	0.014039	1.06	2.39	24.63	0.81
Reach 1	350	100-Year SCS 24H	1.68	72.45	72.80	72.78	72.84	0.011854	1.06	3.00	27.00	0.76
Reach 1	300	2-Year SCS 24Hr	0.37	71.95	72.19	72.10	72.21	0.004232	0.57	0.65	3.82	0.44
Reach 1	300	5-Year SCS 24Hr	0.66	71.95	72.27	72.16	72.29	0.004257	0.68	0.97	4.31	0.46
Reach 1	300	10-Year SCS 24Hr	0.89	71.95	72.32	72.20	72.35	0.004315	0.75	1.19	4.58	0.47
Reach 1	300	25-Year SCS 24Hr	1.21	71.95	72.37	72.24	72.41	0.004368	0.83	1.46	4.91	0.49
Reach 1	300	50-Year SCS 24Hr	1.48	71.95	72.42	72.27	72.46	0.004197	0.87	1.71	5.18	0.48
Reach 1	300	100-Year SCS 24H	1.78	71.95	72.47	72.30	72.51	0.004096	0.91	1.96	5.45	0.48
Reach 1	293.092		Culvert									
Reach 1	250	2-Year SCS 24Hr	0.37	71.91	72.17		72.20	0.008738	0.76	0.49	3.16	0.62
Reach 1	250	5-Year SCS 24Hr	0.66	71.91	72.24		72.28	0.009565	0.92	0.73	4.06	0.67
Reach 1	250	10-Year SCS 24Hr	0.89	71.91	72.28	72.23	72.33	0.009542	1.01	0.97	7.15	0.69
Reach 1	250	25-Year SCS 24Hr	1.21	71.91	72.33	72.28	72.39	0.008535	1.09	1.34	8.41	0.67
Reach 1	250	50-Year SCS 24Hr	1.48	71.91	72.37	72.31	72.43	0.008052	1.14	1.65	9.33	0.66
Reach 1	250	100-Year SCS 24H	1.78	71.91	72.40	72.34	72.47	0.007812	1.21	1.99	10.74	0.67
Reach 1	200	2-Year SCS 24Hr	0.37	71.49	71.73		71.76	0.008870	0.80	0.46	2.82	0.63
Reach 1	200	5-Year SCS 24Hr	0.66	71.49	71.82		71.86	0.007551	0.89	0.75	3.43	0.60
Reach 1	200	10-Year SCS 24Hr	0.89	71.49	71.88		71.92	0.007181	0.94	0.95	3.79	0.60
Reach 1	200	25-Year SCS 24Hr	1.21	71.49	71.94		71.99	0.007495	1.02	1.19	4.39	0.62
Reach 1	200	50-Year SCS 24Hr	1.48	71.49	71.98		72.04	0.007628	1.06	1.40	4.91	0.64
Reach 1	200	100-Year SCS 24H	1.78	71.49	72.02		72.08	0.007655	1.11	1.63	7.47	0.64
Reach 1	150	2-Year SCS 24Hr	0.37	71.20	71.57		71.58	0.001901	0.47	0.82	4.85	0.31
Reach 1	150	5-Year SCS 24Hr	0.66	71.20	71.65		71.67	0.002230	0.59	1.44	9.95	0.35
Reach 1	150	10-Year SCS 24Hr	0.89	71.20	71.69		71.71	0.002542	0.67	1.86	11.37	0.37
Reach 1	150	25-Year SCS 24Hr	1.21	71.20	71.73	71.58	71.76	0.002764	0.76	2.42	13.33	0.40
Reach 1	150	50-Year SCS 24Hr	1.48	71.20	71.77	71.63	71.80	0.002924	0.83	2.91	15.67	0.42
Reach 1	150	100-Year SCS 24H	1.78	71.20	71.80	71.66	71.83	0.003124	0.90	3.41	18.50	0.44
Reach 1	100	2-Year SCS 24Hr	0.37	71.02	71.27	71.27	71.34	0.025388	1.12	0.33	2.62	1.02
Reach 1	100	5-Year SCS 24Hr	0.66	71.02	71.36	71.36	71.41	0.018432	1.09	0.71	9.48	0.89
Reach 1	100	10-Year SCS 24Hr	0.89	71.02	71.39	71.39	71.45	0.015307	1.13	1.10	13.49	0.84
Reach 1	100	25-Year SCS 24Hr	1.21	71.02	71.42	71.42	71.49	0.015066	1.24	1.51	14.19	0.86
Reach 1	100	50-Year SCS 24Hr	1.48	71.02	71.44	71.44	71.51	0.015071	1.31	1.80	14.48	0.87
Reach 1	100	100-Year SCS 24H	1.78	71.02	71.46	71.46	71.54	0.014170	1.36	2.17	14.83	0.86
Reach 1	50	2-Year SCS 24Hr	0.40	70.80	71.00	70.87	71.00	0.001000	0.20	3.69	30.53	0.20
Reach 1	50	5-Year SCS 24Hr	0.72	70.80	71.05	70.91	71.05	0.001001	0.23	5.84	52.18	0.20
Reach 1	50	10-Year SCS 24Hr	0.98	70.80	71.09	70.92	71.09	0.001002	0.26	7.77	65.12	0.21
Reach 1	50	25-Year SCS 24Hr	1.33	70.80	71.12	70.93	71.12	0.001001	0.30	10.29	70.92	0.22
Reach 1	50	50-Year SCS 24Hr	1.63	70.80	71.14	70.94	71.15	0.001001	0.32	11.88	73.08	0.22
Reach 1	50	100-Year SCS 24H	1.96	70.80	71.17	70.96	71.17	0.001002	0.34	13.56	77.60	0.22

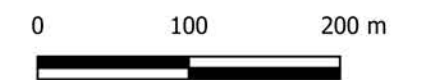


Legend

100-Year Flood Extents



SCALE: 1:5000



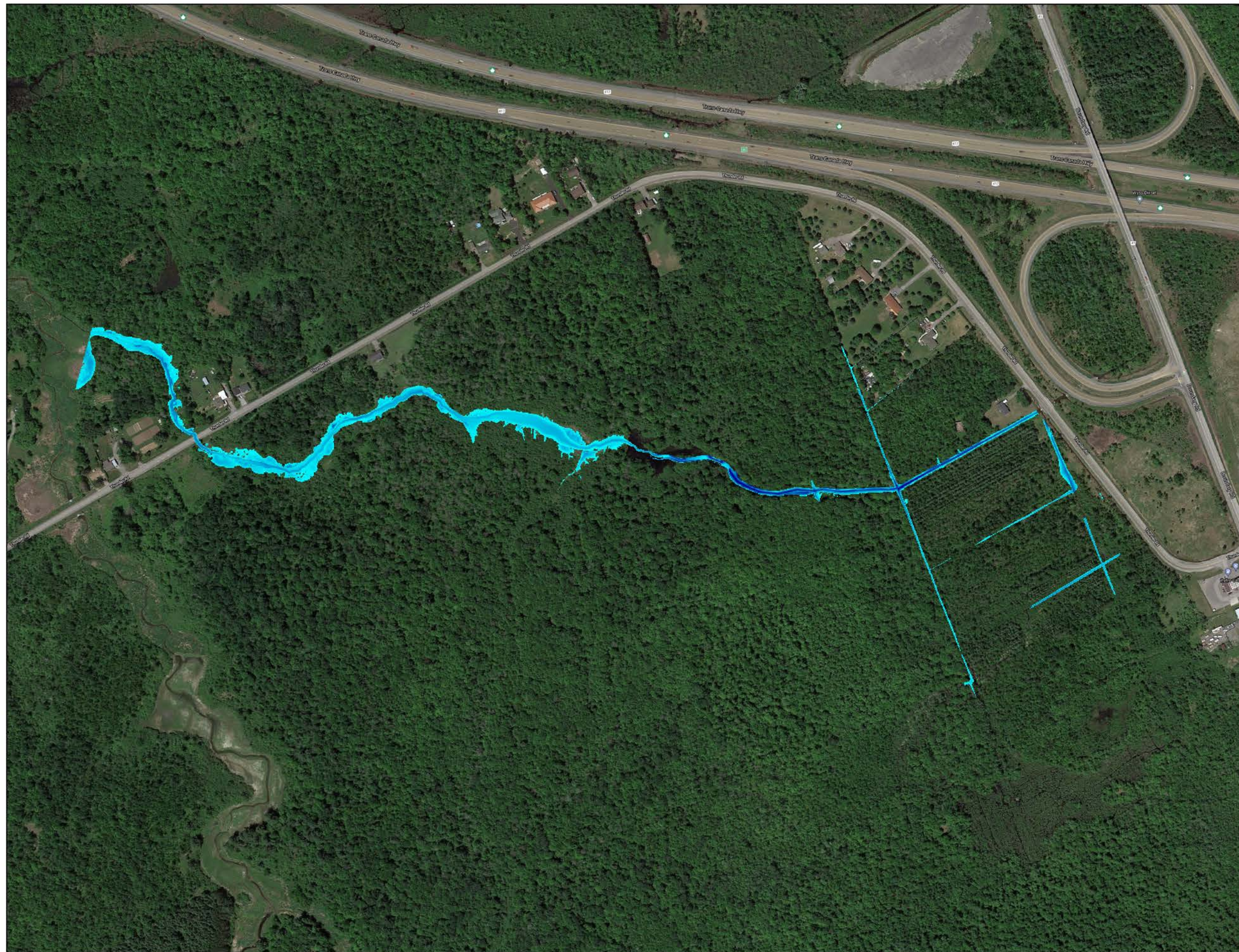
J.F. Sabourin and Associates Inc.
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 52 Springbrook Drive (613) 836-3884
 Ottawa, ON, K2S 1B9 www.jfsa.com



6150 Thunder Road:
 Floodplain Mapping

Figure C2: 100 Year Flood Extents

PROJECT	2120-21
DRAWN	MP
DATE	06-28-2021



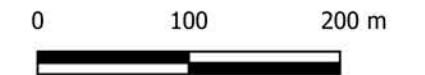
Legend

100 Year Flood Depth (m)

- 0
- 0.25
- 0.5
- 0.75
- 1 >



SCALE: 1:5000



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6150 Thunder Road:
 Floodplain Mapping

Figure C3: 100 Year Flood Depth

PROJECT	2120-21
DRAWN	MP
DATE	06-28-2021