

MEMORANDUM

DATE: NOVEMBER 28, 2019

TO: JULIE CANDOW

FROM: CONRAD STANG / MIKE PETEPIECE

RE: CLARIDGE / UNIFORM DEVELOPMENTS MARCH ROAD STORM SERVICING OPTIONS

CC: JOHN RIDDELL, MARC ST. PIERRE

This memorandum provides an overview of the storm servicing options for the future and existing lands west of March Road based on comments received from the City of Ottawa July 29, 2019 and an email received September 16, 2019.

BACKGROUND:

March Road

Under existing conditions drainage from March Road is conveyed via roadside ditches to Tributary 2 of the Northwest Branch of Shirley's Brook. The western roadside ditch also receives drainage from the residential lots fronting Murphy Court and the undeveloped lands west of March Road. Refer to Figure 1 – Existing / Future Development Areas Included in March Road Storm Servicing Analysis.

The Master Servicing Study (MSS) for the Kanata North Urban Expansion Area (KNUEA) lands identified the future widening of March Road. The ultimate cross-section is a 44.5m right-of-way (ROW) including a central Bus-Rapid Transit corridor. Refer to attached excerpt, Figure No. 24 – March Rod – Ultimate Cross Section. Due to the width of the ROW, storm servicing will be provided by two (2) separate storm sewers for the northbound and southbound lanes:

- The storm sewer for the east side of the ROW (northbound lanes) will outlet to Pond 3.
- The storm sewer for the west side of the ROW (southbound lanes) will outlet to Pond 1.

Pond 1 is part of the CU Developments and Pond 3 is part of the Minto / Valecraft development (by others). Refer to the following attached excerpts for drainage areas tributary to Pond 1 and Pond 3:

- Drawing 112117-STM1: Storm Drainage Area Plan Minor System Drainage
- Drawing 112117-STM2: Storm Drainage Area Plan Major System Drainage

Existing / Future Development Lands

The existing / future development lands consist of residential Block 300, St. Isidore Catholic Church / Cemetery, St. Isidore School, future Claridge lands and residential Block 298. These lands are located between the existing homes on Murphy Court and the proposed Park & Ride. The MSS anticipated the future development of these lands and assumed the proposed land use would consist of commercial or mixed-use residential.

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As identified in the CU Developments Planning Rationale, the lands around St. Isidore Catholic Church and St. Isidore Catholic School have been accounted for in the development of the subject lands and are shown as Blocks on the Plan of Subdivision. No road pattern has been defined as these lands will be included in future development applications. These lands will also be subject to land exchange agreements.

MSS STORM SERVICING OPTIONS:

The MSS identified two (2) storm servicing options for the future development lands and March Road:

- Storm drainage for future development lands conveyed to a storm sewer on Street 1 (preferred). Refer to attached excerpt from the MSS, Figure No. 5.3.2 – Proposed Storm Infrastructure.
- Storm drainage from the future development lands conveyed to a storm sewer on March Road (alternative). Refer to attached excerpt from the MSS, Figure No. 5.3.3 – Storm Drainage – Area NW-2 (St. Isidore Church).

The existing topography slopes from Street 1 to March Road. It is acknowledged that the preferred storm servicing option from the MSS (conveying drainage to Street 1) would result in deep storm sewers and additional rock excavation.

CU DEVELOPMENTS STORM SERVICING OPTIONS:

Both storm servicing options presented in the MSS were based on Pond 1 as a single cell SWM Facility. To reduce rock excavation, Pond 1 is being proposed as a two-cell SWM facility; with the upper cell 2.5m higher than the lower cell. Based on the two-cell design approach for Pond 1, the servicing options from the MSS are no longer applicable and a revised storm sewer layout was developed:

- Storm sewers on Street 1 & Street 12 will be directed to the upper cell.
- March Road and the existing / future development lands will outlet to the lower cell, either by a storm sewer on March Road or a storm sewer through the St. Isidore Church lands, cemetery lands, future Claridge lands, Block 298 and the Park & Ride.

To address serviceability comments provided by the City regarding March Road and the existing / future development lands, Novatech has developed new storm servicing options for these areas based on the two-cell pond layout.

Preferred Storm Servicing Option

The preferred storm servicing option is to keep March Road drainage separate from the CU Developments / future development lands. Refer to the following figures and design sheets for details on the preferred servicing option:

- Figure 2 Preferred Storm Servicing Layout for Future and Existing Lands;
- Design Sheets CU Developments Preferred Option Storm Sewers Through Existing / Future Lands
- Design Sheets March Road Design Sheet, West Side, Ultimate Design Independent Inlet to SWM Pond 1, 10 year

A summary of the preferred storm servicing option is as follows:

• A storm sewer servicing the CU Developments and the existing / future development lands would run through the St. Isidore Church lands, cemetery lands, future Claridge lands, Block 298 and the Park & Ride. The storm sewer would outlet to the forebay within the lower cell of

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Pond 1 and would require inlet controls, as there would be basement connections (residential Blocks 298 and 300). This option is preferred for servicing residential Block 300 as it results in a more direct route to the pond and lowers HGL elevations.

- A storm sewer on March Road would be designed to convey the 10-year storm event based on the ultimate build-out of March Road. This storm sewer could then surcharge during larger storm events and would have sufficient capacity to convey the 100-year peak flows under surcharged conditions. There would be no concerns with the hydraulic grade line (HGL) since there are no basement connections. The March Road storm sewer would outlet into the main lower cell of Pond 1.
- Under existing conditions, a ditch-inlet catchbasin (DICB) would be installed within the western March Road roadside ditch. This DICB would outlet to the main lower cell of Pond 1. Having an independent outlet to Pond 1 for March Road provides additional flexibility as March Road can be widened independent of the proposed CU Developments.

Alternative Storm Servicing Option

The alternative storm servicing option is to provide a storm sewer on March Road that services March Road and the existing / future development lands. This storm sewer would outlet into the forebay within the lower cell of Pond 1. The future Park & Ride and fire hall would connect to this storm sewer immediately upstream Pond 1.

Refer to the following figures and design sheets for details on the alternative servicing option:

- Figure 3 Alternative Storm Servicing Layout for Future and Existing Lands;
- Design Sheets March Road Design Sheet, West Side, Ultimate Design Alternative Option

Due to the low-grades of March Road adjacent the pond this option would require elliptical pipe to provide sufficient cover. The storm sewer on March Road will need to be sized to convey the 100-year storm event. Inlet controls may also be required to maintain HGL elevations. This is due to connecting local storm sewers that have basement connections to an arterial road storm sewer.

A small portion of March Road, between Street 1 and Tributary 2, is lower than the estimated 100year water level in the pond. It is recommended that this area be directed to Pond 3; however, the hydrologic analysis indicates that this area can outlet directly to Tributary 2 without exceeding the pre-development peak flows.

The proposed storm sewer for this alternative has been oversized to provide a 100-year level of service for the existing / future development lands under both existing and full-build out conditions. The full-build out of the existing / future development lands produces the most conservative results.

DISCUSSION:

The following discussion points provide a rationale for the preferred storm servicing option:

- It is preferable to keep the storm sewers servicing the CU Developments lands separate from March Road:
 - The CU Developments storm sewers will service residential units with basement connections (Blocks 298 & 300).
 - If the CU Developments storm sewers were to outlet to March Road, the storm sewer would require inlet controls to prevent surcharging. This would limit the ability of the sewer to convey additional flow during large storm events and the sewer may need to be upsized to manage major system flows in the ROW.

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- If there are no residential connections to the March Road storm sewer, the sewer can be allowed to surcharge during larger storm events, reducing the amount of overland flow in the ROW.
- Independent storm sewers for March Road and the CU Developments lands would also provide better hydraulics (shorter pipe runs / lower HGL).
- An independent storm sewer for March Road, which outlets separately to the lower cell of Pond 1, provides greater flexibility:
 - Allows March Road and proposed developments to be independent.
 - Allows the widening of March Road and the development to proceed in phases.
 - The storm sewer servicing only March Road may be sized for a 10-year storm, which can surcharge during the 100-year storm event as there would be no basement connections.

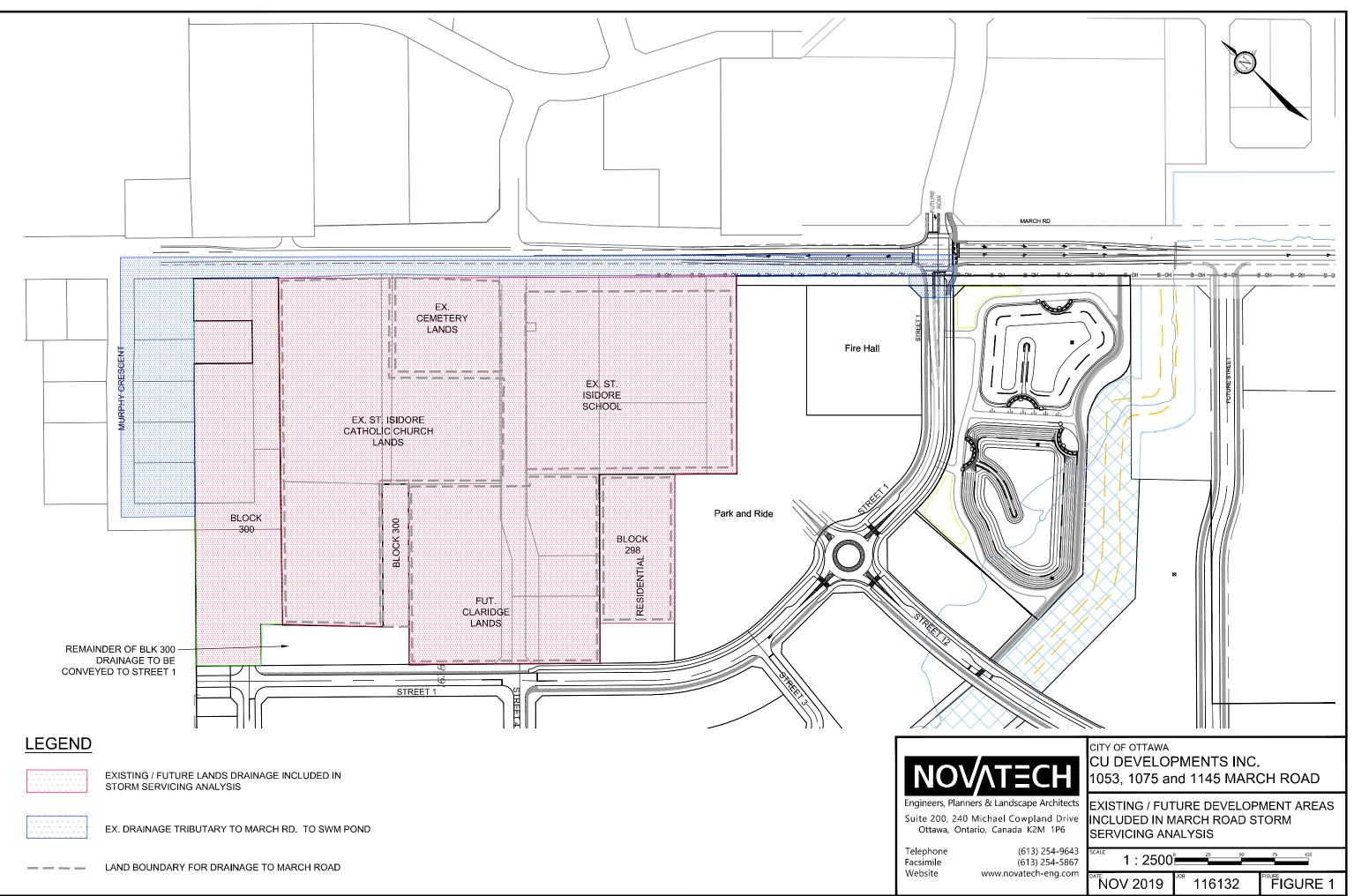
CONCLUSIONS:

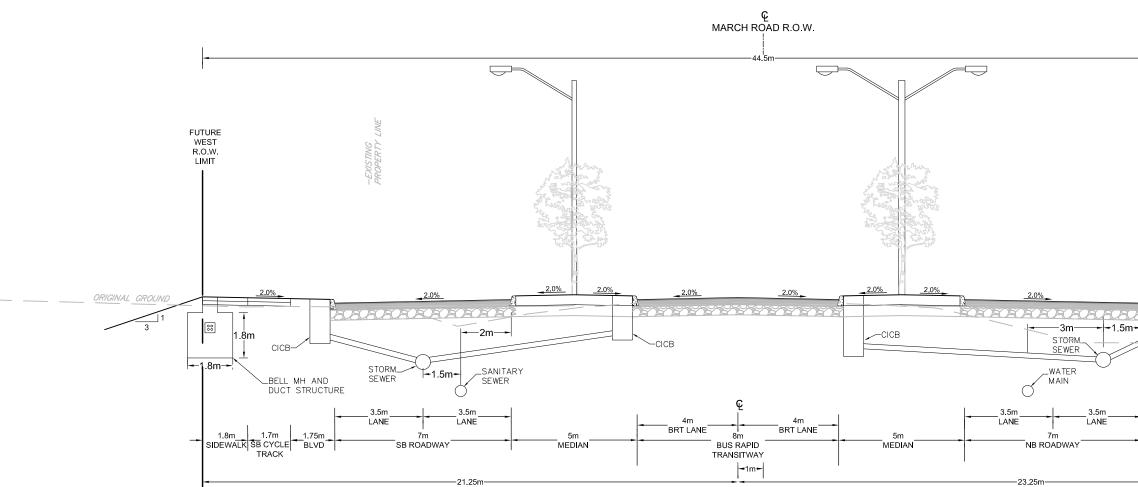
- The preferred drainage option is to provide an independent storm sewer through the existing / future development lands and Park & Ride. This approach will provide greater flexibility in terms of design considerations / constraints and timing.
- The alternative servicing option is to provide a storm sewer on March Road to service the existing / future lands, but this would require larger storm sewers on March Road in areas with limited pipe cover. This option would also require more restrictive inlet controls on March Road to ensure the HGL does not adversely impact basements in the residential areas.

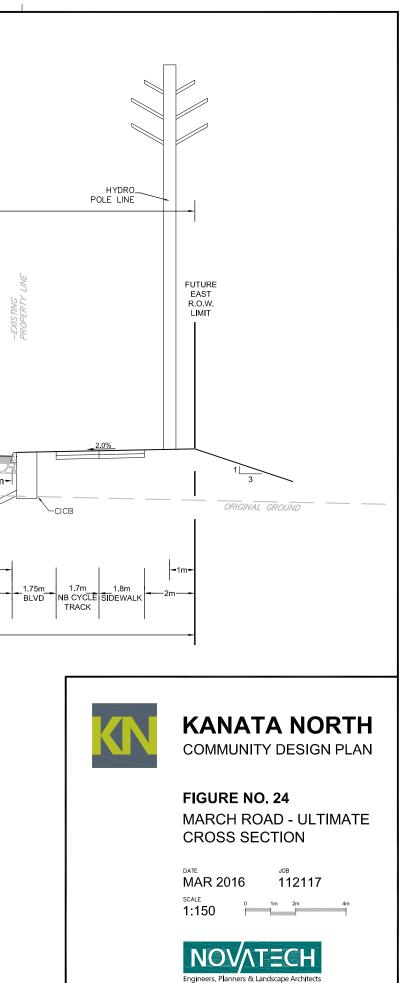
ATTACHMENTS:

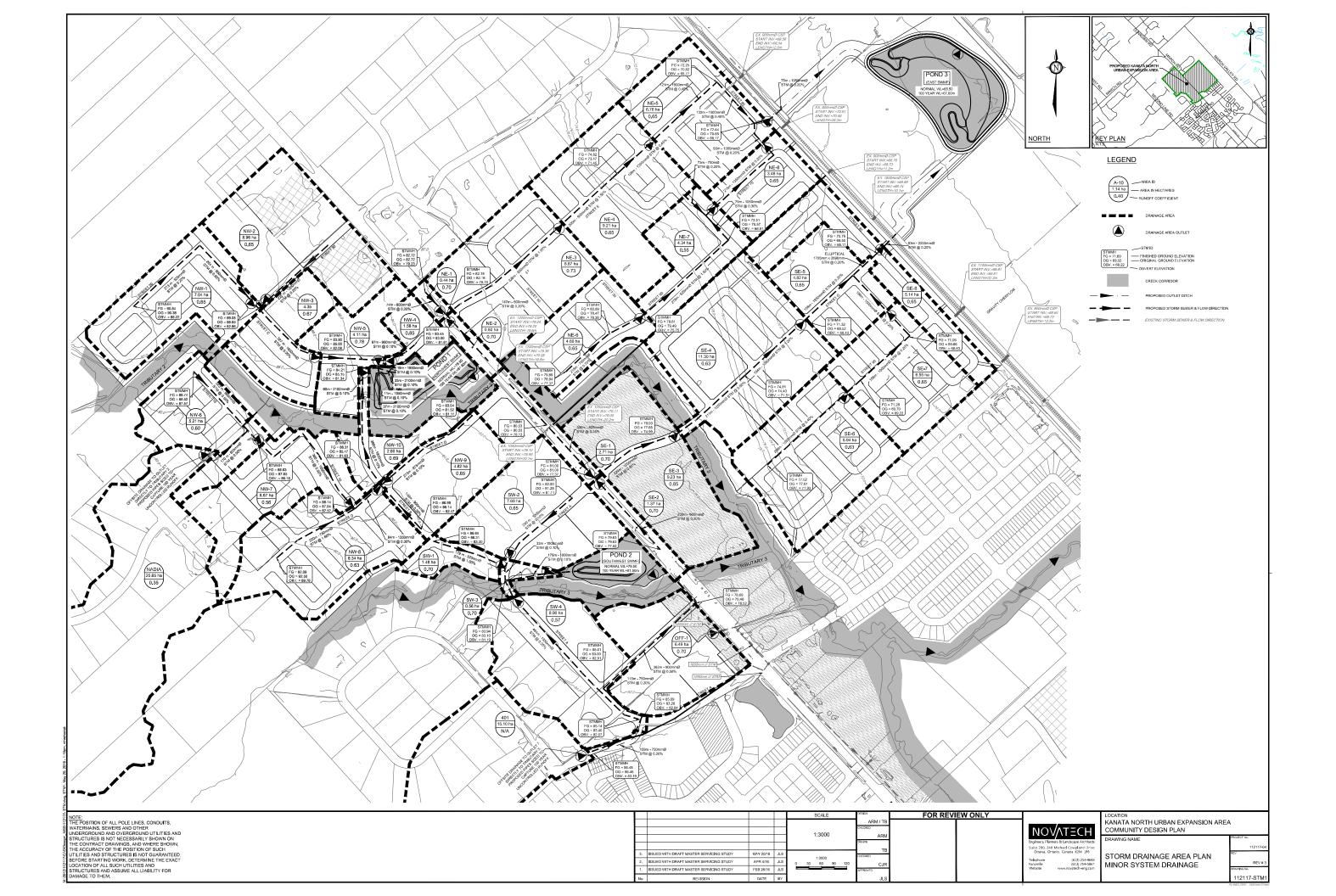
- Figures
 - Figure 1: Areas Included in March Road Storm Servicing Analysis
 - Figure 2: Preferred Storm Servicing Layout for Future and Existing Lands
 - Figure 3: Alternative Storm Servicing Layout for Future and Existing Lands
- Report Excerpts (KNUEA MSS)
 - Figure No. 24: March Road Ultimate Cross-Section
 - Drawing 112117-STM1: Storm Drainage Area Plan Minor System Drainage
 - Drawing 112117-STM2: Storm Drainage Area Plan Major System Drainage
 - Figure No. 5.3.2 Proposed Storm Infrastructure
 - Figure No. 5.3.3 Storm Drainage Area NW-2 (St. Isadore Church)
- Storm Sewer Design Sheets
 - Design Sheets CU Developments Preferred Option Storm Sewers Through Existing / Future Lands
 - Design Sheets March Road Design Sheet, West Side, Ultimate Design Independent Inlet to SWM Pond 1, 10 year
 - Design Sheets March Road Design Sheet, West Side, Ultimate Design Alternative Option

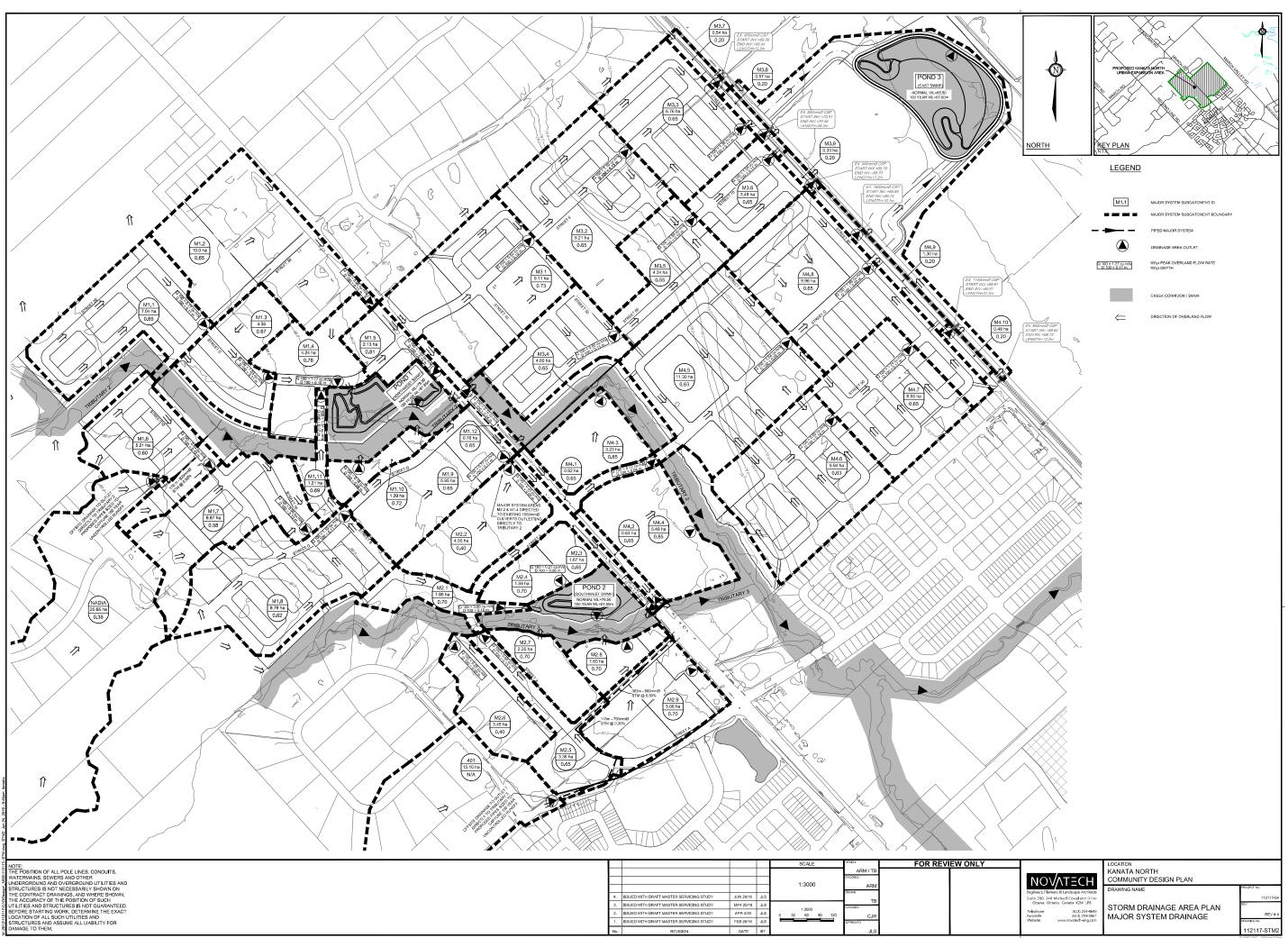
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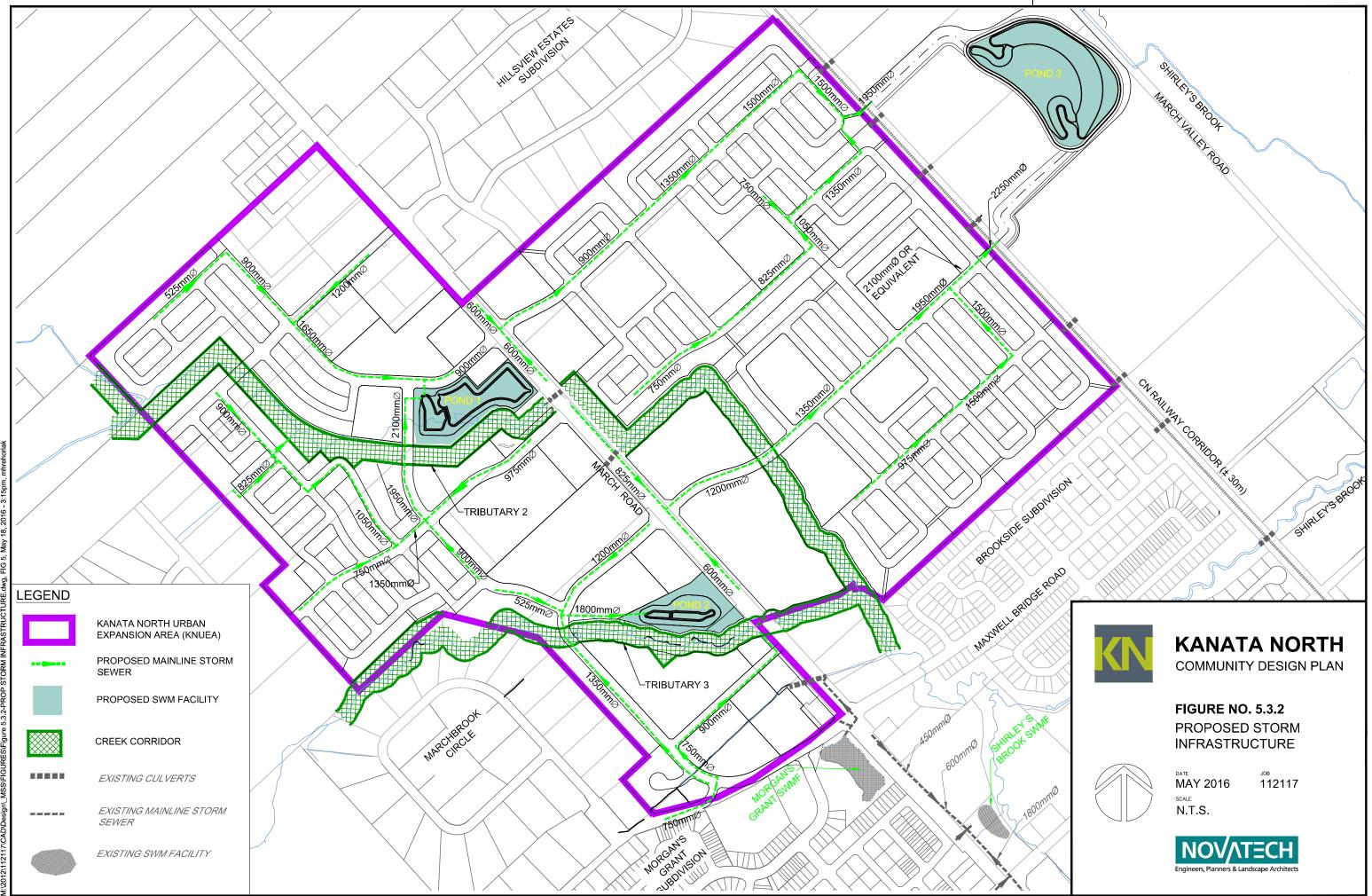


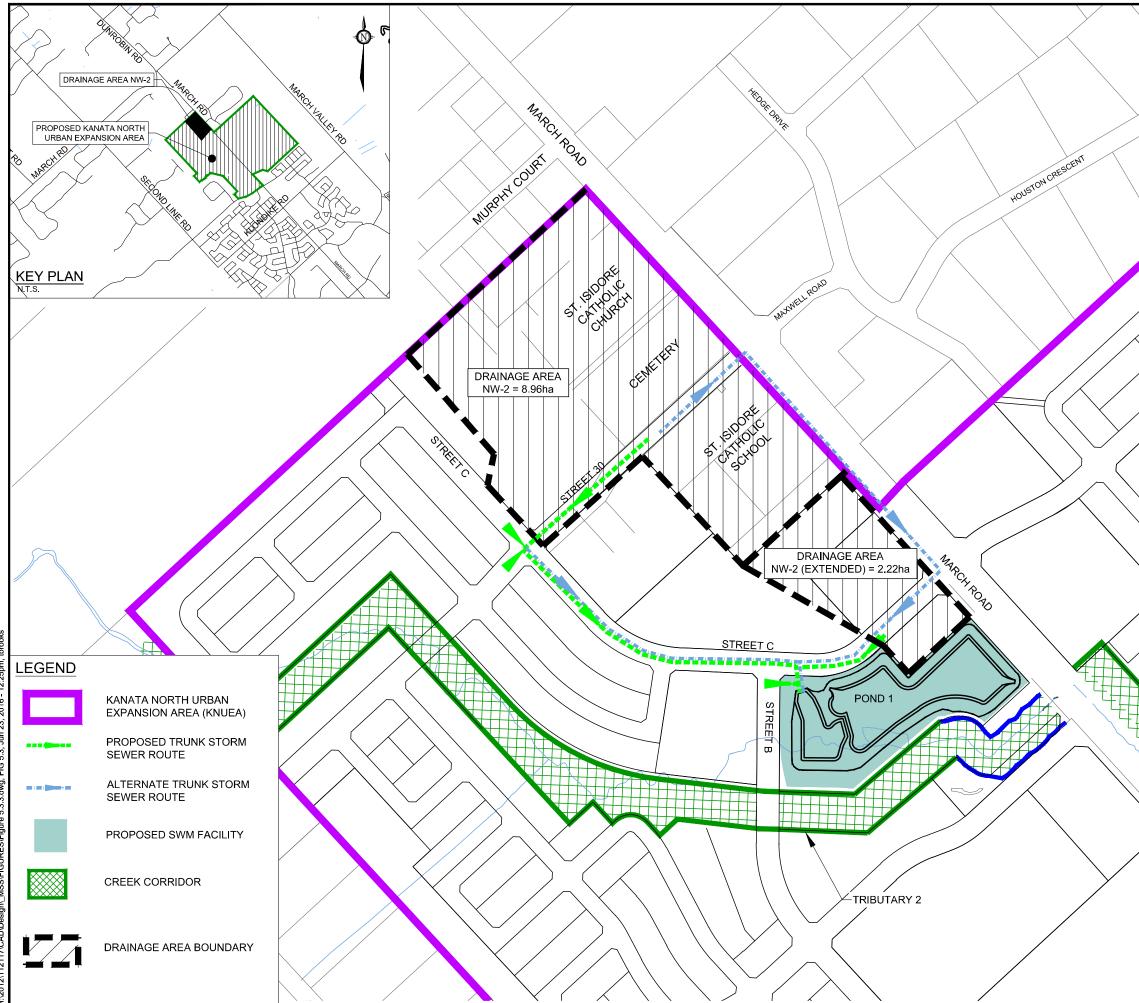


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	112117-STM
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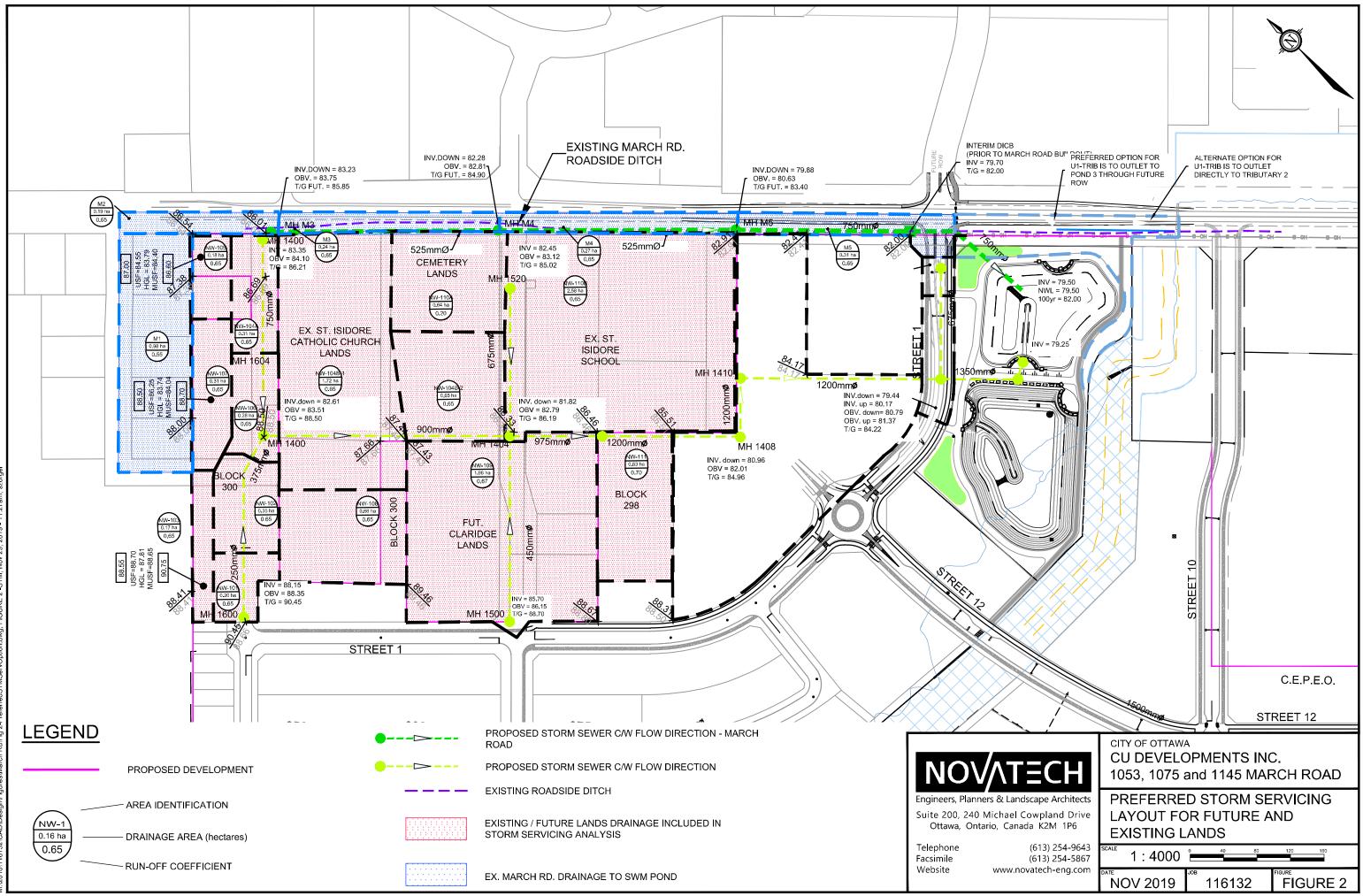
KANATA NORTH

COMMUNITY DESIGN PLAN

FIGURE NO. 5.3.3

STORM DRAINAGE - AREA NW-2 (ST ISADORE CHURCH) DATE JUNE 2016 SCALE N.T.S.





CHT11Y17 NIMC - 970mm YA29mm

STORM SEWER DESIGN SHEET

CU Developments - Preferred Option - Storm Sewers Through Existing / Future Lands FLOW RATES BASED ON RATIONAL METHOD

	LOCATION			EA (ha						FLOW				TOTAL FLOW				SE	WER DA	ТА		-	
		. .		1	-	La d'ac	A	Time of	Deinfell Interesity		Deinfell le terreiter	Deinfell Internetter			1	Die	T	1	1		Mala alter	Flow	Datia
Catchment ID	From	То	Area	С	AC	Indiv	Accum	Time of	Rainfall Intensity	Rainfall Intensity	Rainfall Intensity	Rainfall Intensity	Peak Flow	Total Peak	Dia. (m)	Dia.	Туре	Siope	Length	Capacity	velocity	Time	Ratio
	Manhole	Manhole	(ha)		(ha)	2.78 AC	2.78 AC	Concentration	2 Year (mm/hr)	5 Year (mm/hr)	10 Year (mm/hr)	100 Year (mm/hr)	(L/s)	Flow, Q (L/s)	Actual	(mm)		(%)	(m)	(L/s)	(m/s)	(min)	Q/Q full
					0.00	0.000	0.000	10.00															
NW-101	1600	1602	0.20	0.65	5 0.13	0.361	0.361	10.00		104.19			38	38	0.254	250	PVC	1.34	107.9	71.7	1.42	1.27	52%
					0.00	0.000	0.000	10.00															!
					0.00	0.000	0.000	11.27															
NW-102			0.35	0.65		0.632	0.994	11.27		97.93			97										
	1602	1400			0.00	0.000	0.000	11.27						127	0.381	375	PVC	2.00	31.5	258.5	2.27	0.23	49%
NW-103			0.17	0.65	5 0.11	0.000	0.000	11.27 11.27		97.93			127										
1444-103			0.17	0.05	0.00	0.000	0.000	11.27		97.93			121										
					0.00	0.000	0.000	11.50															-
					0.00	0.000	0.000	10.00															+
NW-104A			0.31	0.65		0.560	0.560	10.00		104.19			58										
			0.01	0.00	0.00	0.000	0.000	10.00		104.10			00										
					0.00	0.000	0.000	10.00															
NW-104B			2.37	0.65		4.283	4.843	10.00		104.19			505										
	1606	1604			0.00	0.000	0.000	10.00						597	0.762	750	Conc	0.40	76.6	734.1	1.61	0.79	81%
	1000	1004			0.00	0.000	0.000	10.00						597	0.762	750	Conc	0.40	70.0	734.1	1.01	0.79	0170
NW-105			0.18	0.65		0.325	5.168	10.00		104.19			538										
					0.00	0.000	0.000	10.00															
					0.00	0.000	0.000	10.00															
NW-107			0.31	0.65		0.560	5.728	10.00		104.19			597										
					0.00	0.000	0.000	10.00															+
NW-106	1604	1400	0.28	0.65	0.00 5 0.18	0.000	0.000	10.79 10.79		100.18			625	625	0.762	750	Conc	0.40	69.9	734.1	1.61	0.72	85%
1444-100	1004	1400	0.20	0.05	0.00	0.000	0.234	10.79		100.18			025	025	0.702	730	CONC	0.40	03.5	734.1	1.01	0.72	0070
					0.00	0.000	0.000	11.52															
					0.00	0.000	0.000																
NW-108	1400	1402	0.66	0.65	5 0.43	0.000	0.000 8.728	11.52 11.52		96.81			845	845	0.914	900	Conc	0.38	110 1	1,163.6	1.77	1.04	73%
1444-100	1400	1402	0.00	0.00	0.00	0.000	0.000	11.52		30.01			043	0-10	0.314	300	Conc	0.50	110.1	1,105.0	1.77	1.04	1370
					0.00	0.000	0.000	12.55															+
	1402	1404			0.00	0.000	8.728	12.55		92.40			806	806	0.914	900	Conc	0.38	74.0	1,163.6	1.77	0.70	69%
	-	-			0.00	0.000	0.000	12.55												,			
								13.25															
					0.00	0.000	0.000	15.00															1
NW-109	1500	1404	1.98	0.67		3.688	3.688	15.00		83.56			308	308	0.457	450	Conc	1.71	120.0	388.7	2.37	0.84	79%
						0.000	0.000	15.00															
			1					15.84							1								1
					0.00	0.000	0.000	15.00															
NW-110A			0.64	0.20	0.00	0.356	0.356	15.00		83.56			30										
			0.01	0.20	0.00	0.000	0.000	15.00		00.00			00	000	0.000	0			446 -	100.0	4.00		0.404
	1502	1404	 	-†	0.00		0.000	15.00		+		<u> </u>		390	0.686	675	Conc	0.30	110.5	480.0	1.30	1.42	81%
NW-110B			2.58	0.65	5 1.68	4.662	4.662	15.00		83.56			390										
					0.00		0.000	15.00					• •										
	1							16.42							1								1
																							<u>i </u>



STORM SEWER DESIGN SHEET CU Developments - Preferred Option - Storm Sewers Through Existing / Future Lands FLOW RATES BASED ON RATIONAL METHOD

	LOCATION		ARE	A (ha)						FLOW				TOTAL FLOW				SEW	er da	TA			
Ostahasast ID	From	То	Area	С	AC	Indiv	Accum	Time of	Rainfall Intensity	Rainfall Intensity	Rainfall Intensity	Rainfall Intensity	Peak Flow	Total Peak	Dia. (m)	Dia.	Туре	Slope L	ength	Capacity	Velocity	Flow	Ratio
Catchment ID	Manhole	Manhole	(ha)		(ha)	2.78 AC	2.78 AC	Concentration	2 Year (mm/hr)	5 Year (mm/hr)	10 Year (mm/hr)	100 Year (mm/hr)	(L/s)	Flow, Q (L/s)	Actual	(mm)		(%)	(m)	(L/s)	(m/s)	Time (min)	Q/Q full
FUTURE BLOCK / EX						evetem																	
		ACCOUNTED																					-
					0.00	0.000	0.000	16.42															
	1404	1406			0.00	0.000	17.078	16.42		79.24			1,353	1,353	0.991	975	Conc	0.50	69.2	1,652.4	2.14	0.54	82%
					0.00	0.000	0.000	<u>16.42</u> 16.96															
NW-111	1406	1408	0.63	0.70	0.00	1.226	18.304	16.96		77.73			1,423	1,423	1.219	1200	Conc	0.43	103.3	2,666.0	2.28	0.75	53%
	1400	1400	0.00	0.70	0.00	0.000	0.000	16.96		11.15			1,420	1,120	1.210	1200	Cono	0.10	100.0	2,000.0	2.20	0.70	0070
					0.00	0.000	0.000	17.71															
	1408	1410			0.00	0.000	18.304	17.71		75.72			1,386	1,386	1.219	1200	Conc	0.30	43.6	2,226.9	1.91	0.38	62%
					0.00	0.000	0.000	17.71															1
					0.00	0.000	0.000	18.09									_						1
NW-112	1410	1412	2.58	0.85	2.19	6.097	24.400	18.09		74.74			1,824	1,824	1.219	1200	Conc	0.30	75.1	2,226.9	1.91	0.66	82%
					0.00	0.000	0.000	18.09															
	1412	1220			0.00	0.000	0.000	18.75		73.13			1 704	1,784	1.219	1200	Conc	0.30	74.7	2,226.9	1.91	0.65	80%
	1412	1220			0.00	0.000	24.400 0.000	18.75 18.75		13.13			1,784	1,704	1.219	1200	COLC	0.30	14.1	2,220.9	1.91	0.05	00%
					0.00	0.000	0.000																
								19.40															



STORM SEWER DESIGN SHEET

CU Developments - Preferred Option - Storm Sewers Through Existing / Future Lands FLOW RATES BASED ON RATIONAL METHOD

L	OCATION		ARE	EA (ha)						FLOW				TOTAL FLOW				SE	WER DA	TA			
	From	То	Area	С	AC	Indiv	Accum	Time of	Rainfall Intensity	Rainfall Intensity	Rainfall Intensity	Rainfall Intensity	Peak Flow	Total Peak	Dia. (m)	Dia.	Туре	Slope	Length	Capacity	Velocity	Flow	Ratio
Catchment ID	Manhole	Manhole	(ha)		(ha)	2.78 AC	2.78 AC	Concentration	2 Year (mm/hr)	5 Year (mm/hr)	10 Year (mm/hr)	100 Year (mm/hr)	(L/s)	Flow, Q (L/s)	Actual	(mm)		(%)	(m)	(L/s)	(m/s)	Time (min)	Q/Q full
					0.00	0.000	0.000	10.00															
NW-114			0.89	0.85	0.76	2.103	2.103	10.00		104.19			219										
					0.00	0.000	0.000	10.00															
				-++	0.00	0.000	0.000	10.00															
			0.00	0.70	0.00	0.000	0.000	10.00		101.10			000										
NW-115	1222	1220	0.23	0.70	0.16	0.448	2.551 0.000	10.00 10.00		104.19			266	280	0.686	675	Conc	0.15	90.8	339.4	0.92	1.65	82%
					0.00	0.000	0.000	10.00															
					0.00	0.000	0.000	10.00															
			0.07	-	0.05	0.136	2.687	10.00		104.19			280										
NW-116					0.00	0.000	0.000	10.00															
					0.00	0.000	0.000	10.00															
								11.65															
					0.00	0.000	0.000	19.40															
	4000	245			0.00	0.000	27.087	19.40		71.60			1,939	1 0 0 0	4 070	4050	0	0.45	F7 0	0 455 0	1.40	0.00	0.00/
	1220	345			0.00	0.000	0.000	19.40						1,939	1.372	1350	Conc	0.15	57.8	2,155.8	1.46	0.66	90%
					0.00	0.000	0.000	19.40															
					0.00	0.000	0.000	20.06															
	345	INLET 2			0.00	0.000	27.087	20.06		70.12			1,899	1,899	1.372	1350	Conc	0.15	11.3	2,155.8	1.46	0.13	88%
	0.0				0.00	0.000	0.000	20.06						.,			000	00		_,		55	
					0.00	0.000	0.000	20.06															<u> </u>
								20.19															



STORM SEWER DESIGN SHEET CU Developments - Preferred Option - Storm Sewers Through Existing / Future Lands FLOW RATES BASED ON RATIONAL METHOD

L	OCATION		AR	EA (ha)						FLOW				TOTAL FLOW				SE	NER DA	TA			
Catchment ID	From	То	Area	С	AC	Indiv	Accum	Time of	Rainfall Intensity	Rainfall Intensity	Rainfall Intensity	Rainfall Intensity	Peak Flow	Total Peak	Dia. (m)	Dia.	Туре	Slope	Length	Capacity	Velocity	Flow Time	Ratio
	Manhole	Manhole	(ha)		(ha)	2.78 AC	2.78 AC	Concentration	2 Year (mm/hr)	5 Year (mm/hr)	10 Year (mm/hr)	100 Year (mm/hr)	(L/s)	Flow, Q (L/s)	Actual	(mm)		(%)	(m)	(L/s)	(m/s)	(min)	Q/Q full
FUTURE BLOCK / EX	ISTING LANDS	ACCOUNTED I	FOR IN STO	ORM SI	EWER	SYSTEM	OUTLETT	ING TO THE S	WM POND THRO	UGH OUTLET #2	2												
					0.00	0.000	0.000	17.01															
	920	351			0.00	0.000	10.621	17.01		77.58			824	998	0.914	900	Conc	0.36	69.5	1,132.6	1.72	0.67	88%
	020			_	0.00	0.000	0.000	17.01							01011			0.00	0010	.,		0.01	0070
				_	0.00	0.000	1.292	17.01				134.92	174										
				-	0.00	0.000	0.000	17.68 17.68		75.79			805										
	351	349		_	0.00	0.000	0.000	17.68		15.15			005	975	0.914	900	Conc	0.36	34.0	1,132.6	1.72	0.33	86%
					0.00	0.000	1.292	17.68				131.80	170										
					0.00	0.000	0.000	18.01															
	349	INLET 2			0.00	0.000	10.621	18.01		74.95			796	964	0.914	900	Conc	0.36	11.2	1,132.6	1.72	0.11	85%
	545				0.00	0.000	0.000	18.01						504	0.314	300	CONC	0.50	11.2	1,102.0	1.72	0.11	0070
				_	0.00	0.000	1.292	18.01				130.34	168										
								18.12															<u> </u>
NADIA LANE			26.11	0.35	9.14	25.405	25.405	132.00				30.53	776	776	0.914	900	Conc	0.35	259.6	1,116.8	1.70	2.54	69%
															1								
Q = 2.78 AIC, where											Consultant:							1	lovatec	h			
Q = Peak Flow in Litre	s per Second (L	/s)									Issued Date:							Nover	nber 28	2019			
A = Area in hectares (I	ha)										Design By:							Ste	eve Zorg	el			
I = Rainfall Intensity (m	nm/hr), 5 year ste	orm									Client:					Dwg	. Referen	ce:			Checke	ed By:	
C = Runoff Coefficient										CU	Developments Inc					I	Figure 2				DD	В	

Legend:

10.00 Storm sewers designed to the 2 year event (without ponding) for local roads

10.00 Storm sewers designed to the 5 year event (without ponding) for collector roads

10.00 Storm sewers designed to the 10 year event (without ponding) for arterial roads

10.00 Storm sewers designed to the 100 year event (without ponding)



STORM SEWER DESIGN SHEET March Road Storm Design Sheet - West Side - Ultimate Design Independent Inlet to SWM Pond 1, 10 Year FLOW RATES BASED ON RATIONAL METHOD

L	LOCATION		ARE	A (ha)						FLOW				TOTAL FLOW				SE	WER DA	TA			
	From	То	Area	C	AC	Indiv	Accum	Time of	Rainfall Intensity	Rainfall Intensity	Rainfall Intensity	Rainfall Intensity	Peak Flow	-	Dia. (m)	Dia.	Туре	Slope	Length	Capacity	Velocity	Flow	Ratio
Catchment ID	Manhole	Manhole	(ha)		(ha)	2.78 AC	2.78 AC	Concentration	2 Year (mm/hr)	5 Year (mm/hr)	10 Year (mm/hr)	100 Year (mm/hr)	(L/s)	Flow, Q (L/s)	Actual			(%)	(m)	(L/s)	(m/s)	Time (min)	Q/Q full
					0.00	0.000	0.000	10.00															
	N44	Mo			0.00	0.000	0.000	10.00						400	0.457	450	0	0.00	100.0	000.0	1 10	0.44	700/
MARCH ROAD	M1	M2	0.98	0.55	0.54	1.498	1.498	10.00			122.14		183	183	0.457	450	Conc	0.60	180.0	230.2	1.40	2.14	79%
					0.00	0.000	0.000	10.00															
					0.00	0.000	0.000	12.14															
MARCH ROAD	M2	M3			0.00	0.000	0.000	12.14						203	0.457	450	Conc	0.60	118.0	230.2	1.40	1.40	88%
MARCHINOAD	1012	1015	0.19	0.65	0.12	0.343	1.842	12.14			110.26		203	200	0.407	400	Conc	0.00	110.0	200.2	1.40	1.40	0070
					0.00	0.000	0.000	12.14															
					0.00	0.000	0.000	13.54															
MARCH ROAD	M3	M4			0.00	0.000	0.000	13.54						236	0.533	525	Conc	0.58	165.0	341.5	1.53	1.80	69%
			0.24	0.65		0.434	2.275	13.54			103.77		236										
					0.00	0.000	0.000	13.54															_
					0.00	0.000	0.000	15.34						-									
MARCH ROAD	M4	M5	0.07	0.05	0.00	0.000	0.000	15.34			00.57		007	267	0.533	525	Conc	1.22	178.0	495.2	2.22	1.34	54%
			0.27	0.65	0.18	0.488	2.763 0.000	15.34 15.34			96.57		267	-									
					0.00	0.000	0.000	16.68															
					0.00	0.000	0.000	16.68						-									
MARCH ROAD	M5	INLET	0.31	0.65	0.00	0.560	3.323	16.68			91.90		305	305	0.762	750	Conc	0.15	232.0	449.6	0.99	3.92	68%
			0.01	0.00	0.20	0.000	0.000	16.68			31.30		505	-									
					0.00	0.000	0.000	20.60															
		i		1	1		I				İ				1			1			<u> </u>		
Q = 2.78 AIC, where											Consultant:							1	Novatec	h			
Q = Peak Flow in Litre	es per Second (L	/s)									Issued Date:							Nover	nber 28,	2019			
A = Area in hectares (I	ha)										Design By:							Ste	eve Zorg	el			
I = Rainfall Intensity (m	nm/hr), 5 year st	orm									Client:					Dwg	. Referenc	ce:			Checke	d By:	
C = Runoff Coefficient										CU	Developments Inc						Figure 2				DD	В	

Q = 2.78 AIC, where	Consultant:	
Q = Peak Flow in Litres per Second (L/s)	Issued Date:	
A = Area in hectares (ha)	Design By:	
I = Rainfall Intensity (mm/hr), 5 year storm	Client:	
C = Runoff Coefficient	CU Developments Inc.	
		i.

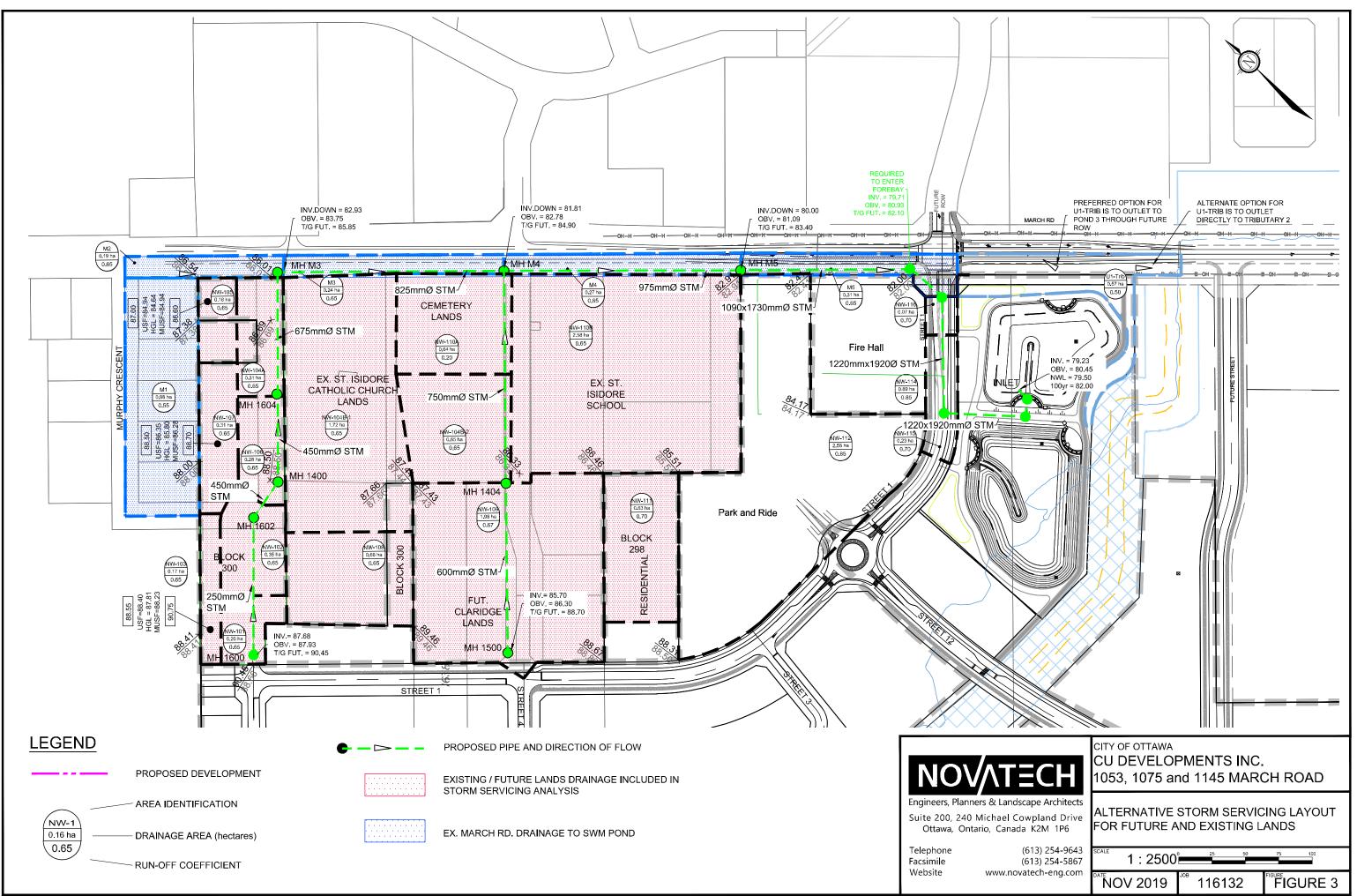
Legend:

Storm sewers designed to the 2 year event (without ponding) for local roads 10.00 10.00

- Storm sewers designed to the 5 year event (without ponding) for collector roads
- Storm sewers designed to the 10 year event (without ponding) for arterial roads 10.00

10.00 Storm sewers designed to the 100 year event (without ponding)

ΝΟΥΛΤΞϹΗ



CHT11V17 DIMC - 270mm YA22mm

STORM SEWER DESIGN SHEET CU Developments & March Road Storm Design Sheet - West Side - Ultimate Design Alternative Option FLOW RATES BASED ON RATIONAL METHOD

	LOCATION		ARE	A (ha)						FLOW			TOTAL FLOW				SEW	/er da	TA			
	From	То	Area	C	AC	Indiv	Accum	Time of	Rainfall Intensity		Rainfall Intensity Rainfall Intensity	Peak Flow	Total Peak	Dia. (m)	Dia.	Туре	1 1	1	Capacity	Velocity	Flow	Ratio
Catchment ID				Ŭ					-	•			Flow, Q (L/s)			Type					Time	
	Manhole	Manhole	(ha)		(ha)	2.78 AC	2.78 AC	Concentration	2 Year (mm/hr)	5 Year (mm/hr)	10 Year (mm/hr) 100 Year (mm/hr)	(L/s)	T 10W, Q (E/3)	Actual	(mm)		(%)	(m)	(L/s)	(m/s)	(min)	Q/Q full
					0.00	0.000	0.000	10.00														
MARCH ROAD	M1	M2			0.00	0.000	0.000	10.00					272	0.533	525	Conc	0.60	180.0	347.3	1.55	1.93	78%
	1011	IVIZ			0.00	0.000	0.000	10.00					212	0.000	020	Conc	0.00	100.0	047.0	1.00	1.00	1070
			0.98	0.55		1.498	1.498	10.00			181.20	272										
					0.00	0.000	0.000	11.93					-									
MARCH ROAD	M2	M3			0.00	0.000	0.000	11.93					304	0.533	525	Conc	0.60	118.0	347.3	1.55	1.27	88%
			0.10	0.65	0.00	0.000	0.000	11.93			165.20	204										
			0.19	0.65	0.12	0.343	1.842	11.93 13.20			105.20	304										-
	1600	1600	0.00	0.05	0.00	0.000		10.00		404.40			20	0.054	250		1 40	107.0	70.0	4 45	1 0 4	E40/
NW-101	1600	1602	0.20	0.65	0.13	0.361	0.361	10.00		104.19		38	38	0.254	250	PVC	1.40	107.9	73.3	1.45	1.24	51%
					0.00	0.000	0.000	10.00 11.24														
NW-102			0.35	0.65		0.632	0.000	11.24		98.06		97										
			0.00	0.05	0.00	0.000	0.000	11.24		30.00		51										
				+	0.00	0.000	0.000	11.24														
NW-108	1602	1400	0.66	0.65	0.43	1.193	2.186	11.24		98.06		214	245	0.457	450	Conc	1.40	31.5	351.7	2.14	0.25	70%
					0.00	0.000	0.000	11.24														
				1	0.00	0.000	0.000	11.24					1									
NW-103			0.17	0.65	0.11	0.307	2.494	11.24		98.06		245										
					0.00	0.000	0.000	11.24														
					0.00	0.000	0.000	11.49								_						
NW-106	1400	1604	0.28	0.65	0.18	0.506	3.000	11.49		96.94		291	291	0.457	450	Conc	1.40	69.9	351.7	2.14	0.54	83%
					0.00	0.000	0.000	11.49														
			0.04	0.05	0.00	0.000	0.000	12.03		04.50		007										
NW-104A			0.31	0.65	0.20	0.560	3.560	12.03		94.56		337										
					0.00	0.000 0.000	0.000	12.03 12.03														
NW-104B-1			1.42	0.65	0.00	2.566	0.000	12.03		94.56		579										
			1.42	0.05	0.92	0.000	0.000	12.03		54.50		575				_						
	1604	M3			0.00	0.000	0.000	12.03					663	0.686	675	Conc	1.40	76.6	1,037.0	2.81	0.45	64%
NW-105			0.18	0.65		0.325	6.451	12.03		94.56		610										
					0.00	0.000	0.000	12.03														
				1	0.00	0.000	0.000	12.03					1									
NW-107			0.31	0.65	0.20	0.560	7.011	12.03		94.56		663]									
					0.00	0.000	0.000	12.03														
								12.49														
					0.00	0.000	0.000	13.20														
MARCH ROAD	M3	M4			0.00	0.000		13.20		89.88		630	986	0.838	825	Conc	0.53	165.0	1,089.6	1.97	1.39	90%
	1010	1117			0.00	0.000		13.20					000	0.000	020	Conc	0.00	100.0	1,000.0	1.51	1.00	5070
			0.24	0.65	0.16	0.434	2.275	13.20			156.30	356										
								14.59														

NOVATECH

STORM SEWER DESIGN SHEET CU Developments & March Road Storm Design Sheet - West Side - Ultimate Design Alternative Option FLOW RATES BASED ON RATIONAL METHOD

Calcimant III From Mannel Too Mannel Area C Accom Time dr Reinfall Intensity Reinfall	L	OCATION		ARE	A (ha)						FLOW				TOTAL FLOW				SE	WER DA	TA			
Lether Hill Markade	I		То			1	Indiv	Acoum	Time of	Painfall Intensity				Dook Flow		Ĩ.	Die	Turne	1	1		Volocity	Flow	Ratio
Nethole Nethole <t< th=""><th>Catchment ID</th><th>FIOIN</th><th>10</th><th>Area</th><th>C</th><th>AC</th><th>indiv</th><th>Accum</th><th>Time of</th><th>Ramai mensity</th><th>Rainiali Intensity</th><th>Rainiali intensity</th><th>Ramai mensity</th><th>Peak Flow</th><th></th><th></th><th>Dia.</th><th>туре</th><th>Siope</th><th>Length</th><th>Capacity</th><th>velocity</th><th>Time</th><th></th></t<>	Catchment ID	FIOIN	10	Area	C	AC	indiv	Accum	Time of	Ramai mensity	Rainiali Intensity	Rainiali intensity	Ramai mensity	Peak Flow			Dia.	туре	Siope	Length	Capacity	velocity	Time	
NN-109 100<		Manhole	Manhole	(ha)		(ha)	2.78 AC	2.78 AC	Concentration	2 Year (mm/hr)	5 Year (mm/hr)	10 Year (mm/hr)	100 Year (mm/hr)	(L/s)	Flow, Q (L/s)	Actual	(mm)		(%)	(m)	(L/s)	(m/s)	(min)	Q/Q full
NN-109 190<						0.00	0.000	0.000	10.00							Ī								
NN-10 1600 1600 1600 0.00 </th <th>NW-109</th> <th></th> <th></th> <th>1.98</th> <th>0.67</th> <th>1.33</th> <th></th> <th></th> <th></th> <th></th> <th>104.19</th> <th></th> <th></th> <th>384</th> <th></th>	NW-109			1.98	0.67	1.33					104.19			384										
NH-111 0.83 0.70 0.00 <		1500	1404			0.00	0.000	0.000							510	0.610	600	Cono	4 4 7	100.0	600.4	2.27	0.94	74%
NW-108-2 NU-108-2		1500	1404			0.00	0.000	0.000	10.00						512	0.610	600	Conc	1.17	120.0	092.4	2.37	0.64	74%
NW-108-2 NW-108-2 NW-108-2 NW-107 6.31 0.84 0.90 0.000	NW-111			0.63	0.70	0.44	1.226	4.914	10.00		104.19			512										
NW-1048-2 NB-1048-2 1404 1405 0.80 0.00 0.000							0.000		10.00															
NN-110A 1404 A 0.00 0.000 10.084						0.00	0.000	0.000	10.84															
NW-110A 1404 MA 0.00 0.000 10.04 0.04 0.05 0.064 0.06 0.007 0.084 0.06 0.007 0.084 0.06 0.007 0.084 0.06 0.007 0.084 0.06 0.007 0.084 0.06 0.007 0.084 0.06 0.007 0.084 0.06 0.007 0.084 0.06 0.007 0.084 0.06 0.007 0.084 0.06 0.007 0.084 0.06 0.007 0.084 0.06 0.007 0.07	NW-104B-2			0.95	0.65	0.62	1.717				99.94			663										
NW-110A 1404 M4 0.64 0.20 0.13 0.356 6.386 10.84 90.94 608 1.164 0.762 750 Conc 1.17 1600 1.255 2.75 0.87 NW-110B																								
NW-1108 Image: mark state						0.00																		
NW-1108 Image: book book book book book book book boo	NW-110A	1404	M4	0.64	0.20						99.94			698	1,164	0.762	750	Conc	1.17	160.0	1,255.6	2.75	0.97	93%
NW-1108 2.58 0.66 1.84 0.02 10.84 90.94 1.164 1.164 1.8																								
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$																								
Image: biole	NW-110B			2.58	0.65						99.94			1,164										
MARCH ROAD M4 M5 0.00 0.000 1.459 0.00 0.000 1.584 1.984 1.984 1.984 1.992 0.91 975 Con 1.00 178.0 2.385.9 3.03 0.98 MARCH ROAD M5 INLET 0.00 0.000 0.000 1.557 0 0 1.984 1.998 1.372 1.980 0.37 0.00 0.000 0.000 0.000 1.577 0 1.528 1.998 1.372 1.372 1.370 0.01 0.00 0.000 1.000 0.000 1.660 1.459 0 1.459 0 1.998 1.372 1.370 0.00 0.000 0.000 1.000 0.000 1.000 1.46 2.68 MARCH ROAD M5 INLET 0.00 0.000 1.557 81.77 1.528 1.998 1.372 1.370 0.01 1.320 1.46 2.68 NW-112 1410 1412 2.00 0.000 0.00						0.00	0.000	0.000																'
MARCH ROAD M4 M5 0.00 0.000 0.000 14.59 84.91 1.92 0.99 975 Conc 1.00 780 2.38.9 3.03 0.98 MARCH ROAD M5 INLET 0.05 0.060 0.000 16.57 0 147.66 408 MARCH ROAD M5 INLET 0.05 0.060 0.860 15.57 81.77 1.02 1.998 1.37 150 Conc 0.15 22.05 2.155.8 1.46 2.65 MARCH ROAD M5 0.00 0.60 0.800 15.57 0 142.20 473 1.998 1.372 1350 Conc 0.15 23.20 2.155.8 1.46 2.55 NW-112 1410 1412 0.00 0.000 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 <th< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>11.81</th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>'</th></th<>									11.81															'
MARCH ROLD M4 M5 0.00 0.000 14.59 1 <th1< th=""> <th1< th=""></th1<></th1<>						0.00	0.000		14.59															
Image: book of the second se		M4	M5								84.91			1,584	1 992	0 991	975	Conc	1.00	178.0	2 336 9	3.03	0.98	85%
MARCH ROAD M5 INLET 0.00 0.000 15.57 81.77 1.526 1.998 1.372 1350 Conc 0.15 23.20 2.155.8 1.46 2.65 0.01 0.000 0.000 18.600 15.57 81.77 1.526 1.998 1.372 1350 Conc 0.15 23.20 2.155.8 1.46 2.65 0.01 0.020 0.000 0.000 10.000 15.57 0 142.20 473 0 </th <th></th> <td>111-1</td> <td>MO</td> <td></td> <td>1,002</td> <td>0.001</td> <td>010</td> <td>Cono</td> <td>1.00</td> <td>170.0</td> <td>2,000.0</td> <td>0.00</td> <td>0.00</td> <td>0070</td>		111-1	MO												1,002	0.001	010	Cono	1.00	170.0	2,000.0	0.00	0.00	0070
MARCH ROAD M5 INLET 0.00 0.000 15.57 0 1.57 0 1.526 1.988 1.372 1350 Conc 0.15 232.0 2.15.8 1.46 2.65 0.00 0.000 0.000 15.57 0 142.20 473 0 0 0.00				0.27	0.65	0.18	0.488	2.763	14.59				147.66	408										'
MARCH ROAD M5 INLET 0.00 0.000 15.57 0 1.57 0 1.526 1.988 1.372 1350 Conc 0.15 232.0 2.15.8 1.46 2.65 0.00 0.000 0.000 15.57 0 142.20 473 0 0 0.00						0.00	0.000	0.000	15.57															
MARCH RAD MS INSET 0.00 0.000 15.57 1 1 1 1 1 1 1 2 2 2 2 1 3 2 1 3 0.00 0.00 0.00 1 5.57 1 1 1 1 1 1 2 0.00 0.00 1 <th></th> <td>NAC</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>81.77</td> <td></td> <td></td> <td>1,526</td> <td>1 009</td> <td>1 070</td> <td>1250</td> <td>Cono</td> <td>0.15</td> <td>222.0</td> <td>0 155 0</td> <td>1.40</td> <td>2.65</td> <td>0.20/</td>		NAC									81.77			1,526	1 009	1 070	1250	Cono	0.15	222.0	0 155 0	1.40	2.65	0.20/
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	MARCH ROAD	IVI5	INLET												1,998	1.372	1350	Conc	0.15	232.0	2,155.8	1.40	2.65	93%
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$				0.31	0.65	0.20	0.560	3.323	15.57				142.20	473										
NW-112 1410 1412 2.58 0.85 2.19 6.097 10.00 100.0 104.19 635 635 0.762 750 Conc 0.41 75.1 74.33 1.63 0.77 1412 1220 0.00 0.000 10.07 0.00 10.03 0.00 10.07 0.00 0.00 1.63 0.76 750 Conc 0.41 75.1 74.33 1.63 0.77 1412 1220 0.00 0.000 6.097 10.77 100.30 0.612 612 0.76 750 Conc 0.39 74.7 724.9 1.59 0.76 0.00 0.000 0.000 18.22 74.42 1.999 0.60 0.000 18.22 74.42 1.999 1.59 0.60 0.000 18.22 1.24 1.29.43 430 1.54 1.59 0.66 0.66 0.00 0.00 1.82.9 1.54 1.54 1.50 Conc 0.15 2.855.2 <									18.22															
NW-112 1410 1412 2.58 0.85 2.19 6.097 10.00 100.0 104.19 635 635 0.762 750 Conc 0.41 75.1 74.33 1.63 0.77 1412 1220 0.00 0.000 10.07 0.00 10.030 0.00 6.012 612 612 0.62 750 Conc 0.39 74.7 724.9 1.59 0.78 1412 1220 0.00 0.000 10.77 100.30 0.00 6.612 612 0.76 750 Conc 0.39 74.7 724.9 1.59 0.78 1412 1220 0.00 0.000 18.22 0.00 0.000 18.22 74.42 1.999 74.7 724.9 74.7 74.9 74.7 74.9 74.7 74.9 74.7 74.9 74.7 74.9 74.7 74.9 74.7 74.9 74.7 74.9 74.7 74.9 74.7 74.9 74.7						0.00	0.000	0.000	10.00															
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	NW-112	1410	1412	2.58	0.85						104.19			635	635	0.762	750	Conc	0.41	75.1	743.3	1.63	0.77	85%
1412 1200 1 0.00 0.000 10.77 100.30 100.30 612 0.76 750 Conc 0.39 74.7 724.9 1.59 0.78 1 1 0.00 0.000 0.000 10.77 0 0 0 0.00 0.00 10.77 0 0 0 0 0.00 0.00 10.77 0 0 0 0 0 0.00 10.77 0				2.00	0.00														-	_			-	
1412 1220 0.00 0.00 6.00 10.77 100.30 612 612 0.72 750 Conc 0.39 74.7 724.9 1.59 0.78 Image: Conc 0.00 0.000 0.000 10.77 0																								
NW-114 1222 1220 0.00 0.000 0.000 18.22 74.42 129.43 430 NW-116 0.00 0.000 18.22 74.42 2.02 2.473 1.524 1.50 1.57		1412	1220								100.30			612	612	0.762	750	Conc	0.39	74.7	724.9	1.59	0.78	84%
Image: NW-114 Image: NW-115 Image: NW-116 Image: N																								
NW-114 0.00 0.00 0.000 18.22 74.42 1.999 NW-115 0.89 0.85 0.76 2.103 26.859 18.22 74.42 1.999 NW-115 1222 1220 0.00 0.000 18.22 1220 1220 0.00 0.000 18.22 1220 129.43 430 NW-116 1220 0.000 0.000 18.22 74.42 2.032 2,032 2,473 1.524 1500 Conc 0.15 20.0 2,855.2 1.57 2.13 NW-116 0.00 0.000 0.000 18.22 74.42 2.042 2,042 2,473 1.524 1500 Conc 0.15 20.0 2,855.2 1.57 2.13 NW-116 0.00 0.000 0.000 18.22 74.42 2.042 2.042 1500 Conc 0.15 20.0 2,855.2 1.57 2.13															-							1		
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STORM SEWER DESIGN SHEET CU Developments & March Road Storm Design Sheet - West Side - Ultimate Design Alternative Option FLOW RATES BASED ON RATIONAL METHOD

L	OCATION		ARE	A (ha)						FLOW				TOTAL FLOW			SE	EWER DA	TA		
Catchment ID	From Manhole	To Manhole	Area (ha)	С	AC		Accum		-	-	-	Rainfall Intensity 100 Year (mm/hr)		Total Peak Flow, Q (L/s)	Dia. (m)		e Slope		Capacity (L/s)	ר `	Flow Ratio Fime min) Q/Q full
	Wannole	Manhole	(iid)		(na)	2.13 AU	2.13 40	Concentration					(Ľ/3)			(,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	(70)	(11)		(11/3) (
Q = 2.78 AIC, where											Consultant:							Novatec	h		
Q = Peak Flow in Litre	s per Second (L/	s)									Issued Date:						Nove	ember 28,	2019		
A = Area in hectares (h	na)										Design By:						S	teve Zorg	el		
I = Rainfall Intensity (m	nm/hr), 5 year sto	orm									Client:					Dwg. Refer	ence:			Checked	By:
C = Runoff Coefficient										CU	Developments Inc	2.				Figure	3			DDB	

Legend:

10.00 Storm sewers designed to the 2 year event (without ponding) for local roads

- 10.00 Storm sewers designed to the 5 year event (without ponding) for collector roads
- 10.00 Storm sewers designed to the 10 year event (without ponding) for arterial roads
- 10.00 Storm sewers designed to the 100 year event (without ponding)

