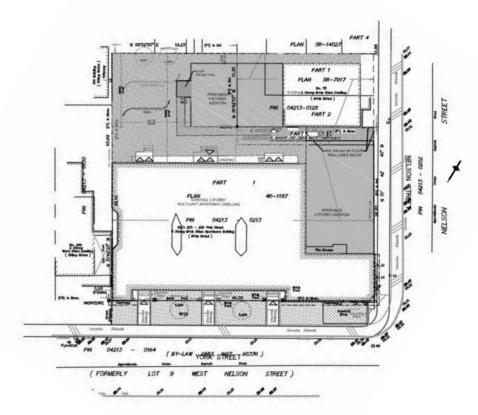
SERVICING & STORMWATER MANAGEMENT REPORT 253 YORK STREET AND 78 & 80 NELSON STREET



Project No.: CCO-22-0938

City File No.: D07-12-21-0135

Prepared for:

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TABLE OF CONTENTS

1.0	PROJECT OVERVIEW	
1.1	Purpose	1
1.2		
1.3	Proposed Development and Statistics	
1.4	Existing Conditions and Infrastructure	
1.5	5 Approvals	3
2.0	BACKROUND STUDIES, STANDARDS AND REFERENCES	4
2.1	Background Reports / Reference Information	4
2.2	Applicable Guidelines and Standards	4
3.0	PRE-CONSULTATION SUMMARY	5
4.0	WATERMAIN	6
4.1	Existing Watermain	6
4	4.1.1 York Street	
4	4.1.2 Nelson Street	6
4.2	Proposed Watermain	6
5.0	SANITARY DESIGN	10
5.1	Existing Sanitary Sewer	10
5.2	Proposed Sanitary Sewer	10
6.0	STORM SEWER & STORMWATER MANAGEMENT DESIGN	13
6.1	Existing Storm Sewers	13
6.2	Proposed Storm Sewers	13
7.0	STORMWATER MANAGEMENT	14
7.1	Design Criteria and Methodology	14
7.2	Quality Control	14
7	7.2.1 Runoff Calculations	14
7.3	Pre-Development Drainage	15
7.4	Post-Development Drainage	15
8.0	EROSION AND SEDIMENT CONTROL	17
8.1	Temporary Measures	17
8.2	Permanent Measures	17
9.0	SUMMARY	18
10.0	RECOMMENDATION	19
11.0	STATEMENT OF LIMITATIONS	20

LIST OF TABLES

Table 1: Water Supply Design Criteria	6
Table 2: Summary of Estimated Water Demand – York Street	7
Table 3: Summary of Estimated Water Demand – Nelson Street	7
Table 4: Boundary Conditions Results	8
Table 5: Fire Protection Confirmation	9
Table 6: Sanitary Design Criteria	10
Table 7: Summary of Estimated Sanitary Flow – York Street	11
Table 8: Summary of Estimated Sanitary Flow – Nelson Street	11
Table 9: Pre-Development Runoff Summary	15
Table 10: Post-Development Runoff Summary	16

APPENDICES

Appendix A: Site Location Plan

Appendix B: City of Ottawa Pre-Consultation Notes

Appendix C: Watermain Calculations

Appendix D: Sanitary Calculations

Appendix E: Pre-Development Drainage Area Plan

Appendix F: Post-Development Drainage Area Plan

Appendix G: Stormwater Management Calculations

1.0 PROJECT OVERVIEW

1.1 Purpose

McIntosh Perry (MP) has been retained by Smart Living Properties to prepare this Servicing and Stormwater Management Report in support of the Site Plan Control (SPC) application process for the proposed development at 253 York Street, 78 Nelson Street, and 80 Nelson Street, within the City of Ottawa.

The main purpose of this report is to present a servicing and stormwater management design for the development in accordance with the recommendations and guidelines provided by the City of Ottawa (City), the Rideau Valley Conservation Authority (RVCA), and the Ministry of the Environment, Conservation and Parks (MECP). This report will address the water, sanitary, and storm sewer servicing for the development, ensuring that existing infrastructure available will adequately service the proposed development.

This report should be read in conjunction with the following drawing:

- CCO-22-0938, C101 Grading, Drainage & Sediment and Erosion Control Plan
- CCO-22-0938, C102 Site Servicing Plan
- CCO-22-0938, C103 Existing Conditions Plan
- CCO-22-0938, PRE Pre Development Drainage Area Plan (Appendix 'E')
- CCO-22-0938, POST Post Development Drainage Area Plan (Appendix 'F')

1.2 Site Description



Figure 1: Site Map

The subject property, herein referred to as the site, is located at 253 York Street, 78 Nelson Street, 80 Nelson Street within the Rideau-Vanier Ward in the City of Ottawa. The site covers approximately **0.15** ha and is located northwest of the York Street and Nelson Street intersection, as shown by **Figure 1** above. The site is zoned for Residential Use (R4UD). Additional details are included on the Site Location Plan included in **Appendix 'A'**.

1.3 Proposed Development and Statistics

The proposed development incorporates a building addition to the existing building within 253 York Street (*B2*) and a building addition to the existing building within 78 & 80 Nelson Street (*B1*). The *Site Plan* proposes an additional 26 bachelor units to the existing 12 bachelor units within *B1*, with street access from Nelson Street. 20 additional residential bachelor units to the existing 31 units are proposed within *B2*, with street access from Nelson Street and York Street. The development is proposed within *0.071 ha* of the site.

1.4 Existing Conditions and Infrastructure

The property is located within the City of Ottawa's Central Sub-Watershed, tributary to the Ottawa River. Two residential buildings exist within the site and are proposed to be retained. The existing building within 253 York Street is serviced via the City's infrastructure within York Street, as designed by Kollaard Associates (Project No. 190502) in January 2020. The existing building within 78 & 80 Nelson Street is serviced via the City's infrastructure within Nelson Street, as designed by W. Elias & Associates (Project No. 2020-42) in September 2020.

Sewer and watermain mapping collected from the City of Ottawa indicate that the following services exist across the property frontages within the adjacent municipal right-of-ways:

♦ York Street

- 152 mm diameter ductile iron watermain;
- 600 mm diameter concrete sanitary sewer, tributary to the King Edward Avenue Trunk; and a
- 600 mm diameter concrete storm sewer, tributary to the Ottawa River approximately 1.5 km downstream.

♦ Nelson Street

- 203 mm diameter ductile iron watermain (within 312 Murray Street);
- 300 mm diameter concrete sanitary sewer, tributary to the King Edward Avenue Trunk; and a
- 300 mm diameter concrete storm Sewer, tributary to the Ottawa River approximately 1.5 km downstream.

1.5 Approvals

The proposed development is subject to the City of Ottawa site plan control approval process. Site plan control requires the City to review, provided concurrence and approve the engineering design package. Permits to construct can be requested once the City has issued a site plan agreement.

An Environmental Compliance Approval (*ECA*) through the Ministry of Environment, Conservation and Parks (*MECP*) is not anticipated to be required for the development since the three parcels of land will be amalgamated into a single parcel. As a result, the stormwater management system meets the exemption requirements under O.Reg 525/90.

2.0 BACKROUND STUDIES, STANDARDS AND REFERENCES

2.1 Background Reports / Reference Information

As-built drawings of existing services, provided by the City of Ottawa Information centre, within the vicinity of the site were reviewed in order to identify infrastructure available to service the proposed development.

A topographic survey (20112-19) of the site was completed by Annis, O'Sullivan, Vollebekk Ltd. dated October 21, 2019.

The Site Plan, SPD-1 was prepared by Ottawa Carleton Construction dated January 2022 (Site Plan).

2.2 Applicable Guidelines and Standards

City of Ottawa:

- Ottawa Sewer Design Guidelines, City of Ottawa, SDG002, October 2012. (Ottawa Sewer Guidelines)
 - Technical Bulletin ISTB-2014-01 City of Ottawa, February 2014. (ISTB-2014-01)
 - Technical Bulletin PIEDTB-2016-01 City of Ottawa, September 2016. (PIEDTB-2016-01)
 - Technical Bulletin ISTB-2018-01 City of Ottawa, January 2018. (ISTB-2018-01)
 - Technical Bulletin ISTB-2018-03 City of Ottawa, March 2018. (ISTB-2018-03)
 - Technical Bulletin ISTB-2019-01 City of Ottawa, January 2019. (ISTB-2019-01)
 - Technical Bulletin ISTB-2019-02 City of Ottawa, February 2019. (ISTB-2019-02)
- Ottawa Design Guidelines Water Distribution City of Ottawa, July 2010. (Ottawa Water Guidelines)
 - Technical Bulletin ISD-2010-2 City of Ottawa, December 15, 2010. (ISD-2010-2)
 - Technical Bulletin ISDTB-2014-02 City of Ottawa, May 2014. (ISDTB-2014-02)
 - Technical Bulletin ISTB-2018-03 City of Ottawa, March 2018. (ISTB-2018-03)

Ministry of Environment, Conservation and Parks:

- ◆ Stormwater Planning and Design Manual, Ministry of the Environment, March 2003.
 (MECP Stormwater Design Manual)
- Design Guidelines for Sewage Works, Ministry of the Environment, 2008. (MECP Sewer Design Guidelines)

3.0 PRE-CONSULTATION SUMMARY

A pre-consultation meeting was conducted on July 31st, 2021, regarding the proposed development at 253 York St, 78 Nelson St, and 80 Nelson St. Specific design parameters to be incorporated within this design are noted by the City of Ottawa pre-consultation found in *Appendix 'B'*.

4.0 WATERMAIN

4.1 Existing Watermain

The subject site is located within the 1W pressure zone, as shown by the Water Distribution figure located in *Appendix 'C'*. The following subsections outline the water infrastructure that exists within York Street and Nelson Street.

4.1.1 *York Street*

There is an existing 152 mm diameter watermain, that runs the entire length of the property along York Street. There is one public hydrant located approximately 25 m west of the site. Based on the Site Servicing Plan for 253 York Street, prepared by Kollaard Associates and dated January 2020, the existing building is currently serviced by a 102 mm diameter water service connected to the infrastructure within the right-of-way.

4.1.2 Nelson Street

There is an existing 203 mm diameter watermain that runs the entire length of the property, within 312 Murray Street. There is one public hydrant located at the north east corner of York Street and Nelson Street, approximately 36 m east of the site. Based on the Site Servicing Plan for 78 & 80 Nelson Street, prepared by W. Elias & Associates and dated September 2020, the existing building is currently serviced by a 25 mm diameter water service connected to the infrastructure within the right-of-way.

4.2 Proposed Watermain

B1 is proposed to be serviced through the existing building at 78 & 80 Nelson Street. **B2** is proposed to be serviced through the existing building at 253 York Street. The building additions will be serviced via a 25 mm and 100 mm diameter services, respectively. Refer to drawing **C102** for a detailed servicing layout.

Table 1, below, summarizes the water supply design criteria obtained from the **Ottawa Water Guidelines** and utilized for the water analysis.

Table 1: Water Supply Design Criteria

Site Area	0.154 ha	
Residential	280 L/day/person	
Residential Bachelor/1 Bedroom	1.4 person/unit	
Max Day Peaking Factor	4.9 x avg. day (B1)	
	9.5 x avg. day (B2)	
Peak Hour Peaking Factor	7.4 x avg. day (B1)	
	14.3 x avg. day (B2)	

The water analysis results for **B2** have been summarized in **Table 2**, below. The fire flow demand accounted for both the existing above-ground floor area and the proposed area within **B2**.

Table 2: Summary of Estimated Water Demand – York Street

Design Parameter	Total Flow (L/s) Existing	Total Flow (L/s) Proposed	Total Flow (L/s) Total
Average Daily Demand	0.4*	0.09	0.49
Max Day Demand	1.0*	0.86	1.86
Max Day + Fire Flow Demand	-	367.53 (FUS) 175.86 (OBC)	-
Peak Hour Demand	2.2*	1.30	2.50

^{*}Per Kollaard Associates Engineers (File No. 190502) Servicing Brief for 253, 255, 257, 259 York Street and dated January 31, 2020 (Rev 1). Analysis based on a peaking factor of 2.5 x avg day and 2.2 x max day for the max day and peak hour demands. Refer to **Appendix 'C'** for relevant excerpt.

The water analysis results for **B1** have been summarized in **Table 3**, below. The fire flow demand accounted for both the existing above-ground floor area and the proposed area within **B1**.

Table 3: Summary of Estimated Water Demand – Nelson Street

Design Parameter	Total Flow (L/s) Existing	Total Flow (L/s) Proposed	Total Flow (L/s) Total
Average Daily Demand	0.05	0.12	0.17
Max Day Demand	0.27	0.58	0.85
Max Day + Fire Flow Demand	-	183.91 (FUS) 45.58 (OBC)	-
Peak Hour Demand	0.40	0.87	1.27

The Fire Underwriters Survey 1999 (FUS) method was utilized to estimate the required fire flow for the site. Fire flow requirements were calculated per City of Ottawa Technical Bulletin ISTB-2018-03.

The following parameters were coordinated with the architect:

- ◆ Type of construction Wood Frame Construction
- ♦ Occupancy type Combustible
- ♦ Sprinkler Protection Standard Sprinkler System

The results of the calculations yielded a required fire flow of 366 L/s (22,000 L/min) for B2 and 183 L/s (11,000 L/min) for B1. OBC calculations yield a required fire flow of 150 L/s (9,000 L/min) for B2 and 45 L/s (2,700 L/min) for B1. The detailed calculations for the FUS and OBC can be found in Appendix 'C'.

The City provided the estimated water pressures at both for the average day scenario, peak hour scenario and the max day plus fire flow scenario for the demands indicated by the correspondence in Appendix C. The resulting pressures for the boundary conditions results are shown in Table 4, below.

Table 4: Boundary Conditions Results

Scenario	Connection 1 - York HGL (m H2O)*/kPa	Connection 1 - Nelson HGL (m H ₂ O)*/kPa	
Average Day Demand	57.3 / 562.0	57.3 / 561.9	
Maximum Daily + Fire Flow Demand	48.8 / 478.6 (OBC)	50.1 / 491.3 (OBC)	
	N/A FUS	46.1 / 452.0 (FUS)	
Peak Hourly Demand	48.1 / 471.8	48.1 / 471.7	
*Adjusted for an estimated ground elevation of 58.1m above the connection point for connection.			

The normal operating pressure range is anticipated to be 472 kPa to 562 kPa and will not be less than 275 kPa (40 psi) or exceed 689 kPa (100 psi). According to the boundary condition results, the infrastructure within York Street can support the estimated OBC fire flow and the infrastructure within Nelson Street can support both the OBC and FUS fire flows. The proposed watermains will meet the minimum required 20 psi (140 kPa) from the Ottawa Water Guidelines at the ground level under maximum day demand and fire flow conditions. A pressure reducing valve (PRV) is anticipated to be required for the site since the pressure is anticipated to exceed 552 kPa (80 psi) in the average day scenario. A pressure test is required during construction to confirm PRV requirements.

To confirm the adequacy of fire flow to protect the proposed development, public fire hydrants within 150 m of the proposed building were accounted for per *ISTB 2018-03 Appendix I*. As demonstrated by *Table 5*, below.

Table 5: Fire Protection Confirmation

Fire Flow Demand	Fire Hydrant(s)	Fire Hydrant(s)	Combined Fire
(L/min.)	within 75m	within 150m	Flow (L/min)
11,000 L/min – B1 22,000 L/min – B2	3 public	2 public	24,300 (405 L/s)

Based on City guidelines the existing hydrants located in the vicinity can provide adequate fire protection to **B1** and **B2**.

5.0 SANITARY DESIGN

5.1 Existing Sanitary Sewer

The subject site lies within the King Edward Collector sewer collection area. There is an existing 600 mm diameter sanitary sewer located within York Street tributary to the King Edward Collector sewer approximately 150 m downstream. In addition, there is an existing 300 mm diameter sanitary sewer within Nelson Street tributary to the King Edward Collector sewer approximately 200 m downstream.

5.2 Proposed Sanitary Sewer

The new building additions are proposed to be serviced through the existing buildings. **B1** is proposed to be serviced by the existing 200 mm diameter sanitary lateral, tributary to the 300 mm diameter sanitary sewer within Nelson Street. **B2** is proposed to be serviced by the existing 150 mm diameter sanitary lateral, tributary to the 600 mm diameter sanitary sewer within York Street. Refer to drawing **C102** for the proposed servicing layout.

Table 6, below, summarizes the wastewater design criteria identified by the **Ottawa Sewer Guidelines**.

Table 6: Sanitary Design Criteria

Design Parameter	Value
Residential 1 Bedroom / Studio Apartment	1.4 persons/unit
Average Daily Demand	280 L/day/person
Extraneous Flow Allowance	0.33 L/s/ha

Table 7 and **Table 8** below, summarizes the estimated wastewater flow from the proposed development. Refer to **Appendix 'D'** for detailed calculations.

Table 7: Summary of Estimated Sanitary Flow – York Street

Design Parameter	Total Flow (L/s) Existing	Total Flow (L/s) Proposed	Total Flow (L/s) Total
Total Estimated Average Dry Weather Flow	0.28*	0.10	0.38
Total Estimated Peak Dry Weather Flow	1.01*	0.35	1.36
Total Estimated Peak Wet Weather Flow	1.05*	0.38	1.43

^{*}Per Kollaard Associates Engineers (File No. 190502) Servicing Brief for 253, 255, 257, 259 York Street and dated January 31, 2020 (Rev 1). Based on a peaking factor of 3.61. Refer to **Appendix 'D'** for relevant excerpt.

Capacity of the Nelson Street and York Street sanitary sewers were reviewed to demonstrate that the receiving system could accommodate development. Per the wastewater analysis included in *Appendix 'D'*, the constraining leg between the subject site and the King Edward Collector sewer (MH1 to MH2) is estimated to be at 1% capacity and can accommodate an additional *495.46 L/s* of wastewater drainage. Therefore, the proposed *0.38 L/s* can be collected by the local sewer within York Street.

As noted above, **B2** is proposed to be serviced by the existing 150 mm diameter sanitary lateral servicing the building at 253 York Street. The full flowing capacity of a 150 mm diameter service at a 1% slope is estimated to be **15.2 L/s**. Per **Table 4**, a combined flow of **1.43 L/s** is proposed to be directed towards the York Street sewer and therefore is sufficient sized. The internal servicing layout is to be reviewed by the mechanical engineer.

Table 8: Summary of Estimated Sanitary Flow – Nelson Street

Design Parameter	Total Flow (L/s) Existing	Total Flow (L/s) Proposed	Total Flow (L/s) Total
Total Estimated Average Dry Weather Flow	0.06	0.12	0.18
Total Estimated Peak Dry Weather Flow	0.21	0.44	0.65
Total Estimated Peak Wet Weather Flow	0.21	0.46	0.67

Capacity of the Nelson Street and Clarence Street sanitary sewers were reviewed to demonstrate that the receiving system could accommodate development. Per the wastewater analysis included in *Appendix 'D'*, the constraining leg between the subject site and the King Edward Collector sewer (MH6 to MH7) is estimated to be at 6.76% capacity and can accommodate an additional *28.22 L/s* of wastewater drainage. Therefore, the proposed *0.46 L/s* can be collected by the local sewer within Nelson Street.

As noted above, **B1** is proposed to be serviced by the existing 200 mm diameter sanitary lateral servicing the building at 78 & 80 Nelson Street. The full flowing capacity of a 200 mm diameter service at a 28% slope is estimated to be **173.6 L/s**. Per **Table 5**, a combined flow of **0.67 L/s** is proposed to be directed towards the Nelson Street sewer and therefore is sufficient sized. The internal servicing layout is to be reviewed by the mechanical engineer.

6.0 STORM SEWER & STORMWATER MANAGEMENT DESIGN

6.1 Existing Storm Sewers

Stormwater runoff from the site is currently tributary to the Ottawa River within the Ottawa Central sub-watershed. There is an existing 600 mm diameter storm sewer within York Street and an existing 300 mm diameter storm sewer within Nelson Street, both tributary to the Ottawa River approximately 1.58 km downstream.

The existing building at 78 & 80 Nelson Street are currently serviced by the Nelson Street storm sewer via a 150 mm diameter service lateral. Refer to W. Elias & Associates Services Plan included in *Appendix 'B'* for further details.

The existing building at 253 York Street are currently serviced by the York Street storm sewer via a 200 mm diameter service lateral. Refer to Kollaard Associates Proposed Servicing Plan included in *Appendix 'B'* for further details.

6.2 Proposed Storm Sewers

A new 250 mm diameter storm service will be extended from the existing 300 mm diameter storm sewer within Nelson Street to collect drainage from building and at-grade common areas within the site.

Foundation drainage is proposed to be connected to the existing building drainage systems, recently designed by W. Elias Associates and Kollaard Associates. The internal servicing layout is to be reviewed by the mechanical engineer.

Runoff collected on the roof of the proposed buildings **B1** and **B2** will be stored and controlled internally using two and three roof drains, respectively. Roof drains will be used to limit the flow from the roof to the specified allowable release rate. For calculation purposes a Watts Accutrol roof drain was used estimate a reasonable roof flow. Other products maybe specified at detailed building design so long as release rates and storage volumes are respected.

Runoff from the at-grade common areas within the site will be directed to two outlets. The first, along the North edge of the property, will convey stormwater overland to Nelson Street via a swale. The second, central in the site, will convey stormwater via a subdrain system to the 300 mm diameter storm sewer within Nelson Street. Storm flows from this will be unattenuated.

See CCO-22-0938 - *POST* include in *Appendix 'F'* of this report for more details. The Stormwater Management design for the subject property will be outlined in *Section 7.0* of this report.

7.0 STORMWATER MANAGEMENT

7.1 Design Criteria and Methodology

Stormwater management for the proposed site will be maintained through two methods. The first will store and control runoff collected on the roof of the proposed buildings. It is estimated that five Watts Accutrol Weirs will be used to control the release rate of the stormwater. The second will control stormwater via a subdrain system and will collect runoff from the at-grade common areas within the site. The flow will be directed to the existing 300 mm storm sewer located within Nelson Street.

The following design criteria will need to be employed to develop the stormwater management design for the site, as directed by the City:

Quality Control

• Due to the distance to the outlet and since no surface parking is proposed, quality controls are not required. Correspondence with the RVCA is included in *Appendix B*.

Quantity Control

- Any storm events greater than 5 year, up to 100 year, and including 100-year storm event must be detained on site.
- Post-development to be restricted to the 5-year storm event, based on a calculated time of concentration greater than 10 minutes and a rational method coefficient of 0.50. Refer to Section 7.2 for further details.

7.2 Quality Control

7.2.1 Runoff Calculations

Runoff calculations presented in this report are derived using the Rational Method, given as:

Q = 2.78CIA (L/s)

Where C = Runoff coefficient

= Rainfall intensity in mm/hr (City of Ottawa IDF curves)

A = Drainage area in hectares

It is recognized that the Rational Method tends to overestimate runoff rates. As a result, the conservative calculation of runoff ensures that any SWM facility sized using this method is expected to function as intended.

The following coefficients were used to develop an average C for each area:

Roofs/Concrete/Asphalt	0.90
Undeveloped and Grass	0.20

As per the *Ottawa Sewer Guidelines*, the 5-year balanced 'C' value must be increased by 25% for a 100-year storm event to a maximum of 1.0.

The time of concentration (Tc) used for pre-development shall be calculated and no less than 10 minutes and post-development flows shall be calculated and no less than 10 minutes.

Based on the criteria listed in *Section 7.2.1*, the development will be required to restrict flow to the 5-year storm event. It is estimated that the target release rate during the 100-year event will be **10.31 L/s** based on the construction limit of **0.071 ha**.

7.3 Pre-Development Drainage

It has been assumed that the existing development contained no stormwater management controls for flow attenuation. The estimated pre-development peak flows for the 2, 5, and 100-year events are summarized below in *Table 9*. See CCO-22-0938 - *PRE* in *Appendix 'E'* and *Appendix 'G'* for calculations.

Table 9: Pre-Development Runoff Summary

Dusiness	A 1100		(L/s)
Drainage Area Area (ha)		5-Year	100-Year
A1	0.071	17.16	32.76

7.4 Post-Development Drainage

To meet the stormwater objectives the development will contain a combination of flow attenuation with rooftop controls.

Based on the criteria listed in *Section 7.2.1*, the development will be required to restrict flow to the 5-year storm event. It is estimated that the target release rate during the 100-year event will be **10.31 L/s** based on the construction limit of **0.071 ha**. See **Appendix 'G'** for calculations.

The proposed site drainage limits are demonstrated on the Post-Development Drainage Area Plan. See CCO-22-0938 - *POST* in *Appendix 'F'* of this report for more details. A summary of the Post-Development Runoff Calculations can be found below.

Table 10: Post-Development Runoff Summary

Drainage Area	Area (ha)	5-year Peak Flow (L/s)	100-year Peak Flow (L/s)	100-year Storage Required (m³)	100-year Storage Available (m³)
B1	0.014	0.64	1.14	4.60	4.89
B2	0.020	1.14	1.89	7.51	7.66
В3	0.017	2.75	5.36	-	-
B4	0.019	3.12	6.08	-	-
Total	0.071	7.66	14.46	12.12	12.55

Runoff for area B1 will be stored on the roof of the proposed building addition (B1) and restricted using two Watts Accutrol roof drains (or equivalent product) to a maximum release rate of 1.14 L/s and will provide up to 4.89 m^3 of storage.

Runoff for area B2 will be stored on the roof of the proposed building addition (B2) and restricted using three Watts Accutrol roof drains (or equivalent product) to a maximum release rate of $1.89 \, \text{L/s}$ and will provide up to $7.66 \, \text{m}^3$ of storage.

Based on direction from City staff, runoff for area B3 will be unrestricted before discharging to the existing storm system within Nelson Street. The unrestricted flow results in a total release rate of **14.46** L/s, **4.15** L/s over the target release rate. As per **Table 9**, above, the predevelopment flow rate was estimated as 32.76 L/s, therefore, there is a 56% reduction from existing conditions.

The flow from Area B4 directed to the City's right of ways without restriction and will be compensated or in areas with attenuation.

8.0 EROSION AND SEDIMENT CONTROL

8.1 Temporary Measures

Before construction begins, temporary silt fence, straw bale or rock flow check dams will be installed at all-natural runoff outlets from the property. It is crucial that these controls be maintained throughout construction and inspection of sediment and erosion control will be facilitated by the Contractor or Contract Administration staff throughout the construction period.

Silt fences will be installed where shown on the final engineering plans, specifically along the downstream property limits. The Contractor, at their discretion or at the instruction of the City, Conservation Authority or the Contract Administrator shall increase the quantity of sediment and erosion controls on-site to ensure that the site is operating as intended and no additional sediment finds its way off site. The rock flow, straw bale & silt fence check dams and barriers shall be inspected weekly and after rainfall events. Care shall be taken to properly remove sediment from the fences and check dams as required. Fibre roll barriers are to be installed at all existing curb inlet catch basins and filter fabric is to be placed under the grates of all existing catch basins and manholes along the frontage of the site and any new structures immediately upon installation. The measures for the existing/proposed structures is to be removed only after all areas have been paved. Care shall be taken at the removal stage to ensure that any silt that has accumulated is properly handled and disposed of. Removal of silt fences without prior removal of the sediments shall not be permitted.

Although not anticipated, work through winter months shall be closely monitored for erosion along sloped areas. Should erosion be noted, the Contractor shall be alerted and shall take all necessary steps to rectify the situation. Should the Contractor's efforts fail at remediating the eroded areas, the Contractor shall contact the City and/or Conservation Authority to review the site conditions and determine the appropriate course of action. As the ground begins to thaw, the Contractor shall place silt fencing at all required locations as soon as ground conditions warrant. Please see the Site Grading, Drainage and Sediment & Erosion Control Plan for additional details regarding the temporary measures to be installed and their appropriate OPSD references.

8.2 Permanent Measures

It is expected that the Contractor will promptly ensure that all disturbed areas receive topsoil and seed/sod and that grass be established as soon as possible. Any areas of excess fill shall be removed or levelled as soon as possible and must be located a sufficient distance from any watercourse to ensure that no sediment is washed out into the watercourse. As the vegetation growth within the site provides a key component to the control of sediment for the site, it must be properly maintained once established. Once the construction is complete, it will be up to

the landowner to maintain the vegetation and ensure that the vegetation is not overgrown or impeded by foreign objects.

9.0 SUMMARY

- The proposed development incorporates a building addition to the existing building within 253 York Street (B2) and a building addition to the existing building within 78 & 80 Nelson Street (B1). The Site Plan proposes an additional 26 bachelor units to the existing 12 units within B1, with street access from Nelson Street. 20 additional bachelor units to the existing 31 units are proposed within B2, with street access from Nelson Street and York Street. The development is proposed within 0.071 ha of the site.
- The FUS method estimated fire flow indicated that 11,000 L/min for B1 and 22,000
 L/min for B2 is required for the proposed development;
- The development is estimated to have a peak wet weather flow of 0.46 L/s for B1 and 0.38 L/s for B2. Based on the sanitary analysis, the receiving sewer system can accommodate the increased wastewater flow from the site;
- Based on City of Ottawa guidelines, the development will be required to attenuate post-development 5 and 100-year flows to the 5-year release rate of 10.31 L/s. This flow rate is based on the limit of work area of 0.071 ha. The unrestricted flow results in a total release rate of 14.46 L/s, 4.15 L/s over the target release rate. As per Table 9, above, the pre-development flow rate was estimated as 32.76 L/s, therefore, there is a 56% reduction from existing conditions;
- To meet the stormwater objectives the development will contain a combination of flow attenuation with rooftop controls. 12.55 m³ of onsite storage will be required to attenuate flow to the established release rate; and
- Quality controls are not required for the site based on coordination with the RVCA.

10.0 RECOMMENDATION

Based on the information presented in this report, we recommend that City of Ottawa approve this Servicing and Stormwater Management report in support of the proposed development at 253 York Street, 78 Nelson Street, and 80 Nelson Street.

This report is respectfully being submitted for approval.

Regards,

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Alison J. Gosling, P.Eng. Project Engineer – Land Development

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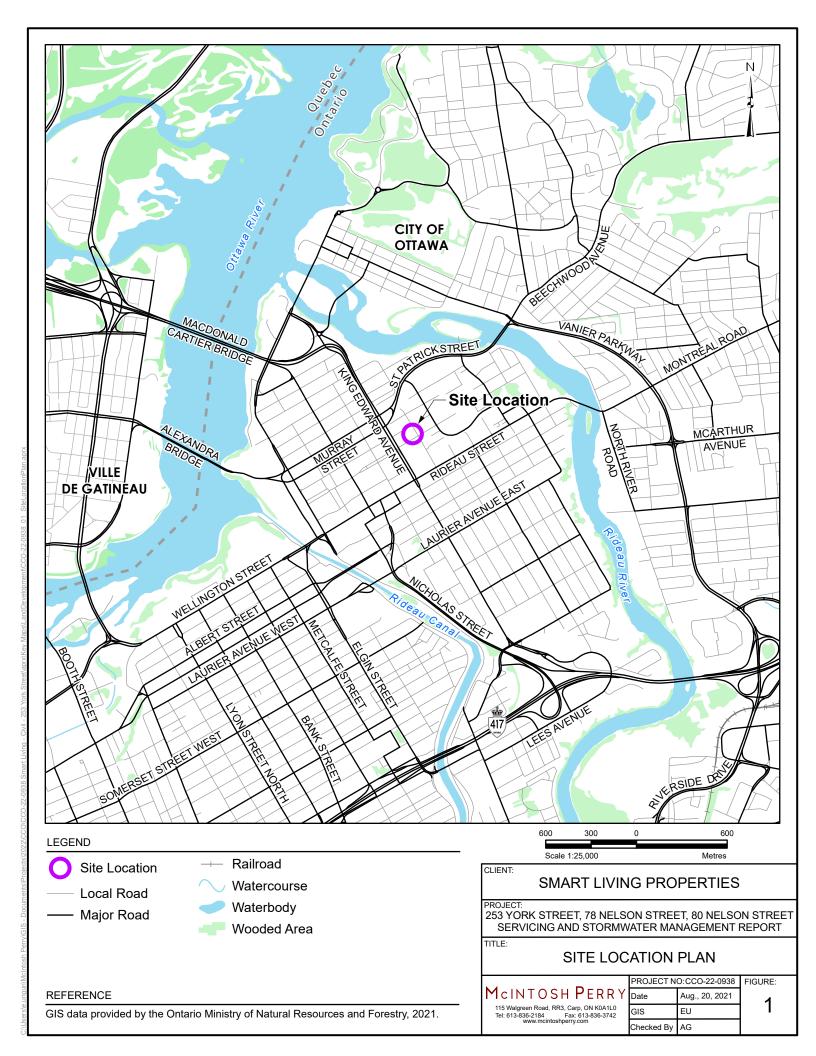
11.0 STATEMENT OF LIMITATIONS

This report was produced for the exclusive use of Smart Living Properties. The purpose of the report is to assess the existing stormwater management system and provide recommendations and designs for the post-construction scenario that are in compliance with the guidelines and standards from the Ministry of the Environment, Parks and Climate Change, City of Ottawa and local approval agencies. McIntosh Perry reviewed the site information and background documents listed in Section 2.0 of this report. While the previous data was reviewed by McIntosh Perry and site visits were performed, no field verification/measures of any information were conducted.

Any use of this review by a third party, or any reliance on decisions made based on it, without a reliance report is the responsibility of such third parties. McIntosh Perry accepts no responsibility for damages, if any, suffered by any third party as a result of decisions or actions made based on this review.

The findings, conclusions and/or recommendations of this report are only valid as of the date of this report. No assurance is made regarding any changes in conditions subsequent to this date. If additional information is discovered or becomes available at a future date, McIntosh Perry should be requested to re-evaluate the conclusions presented in this report, and provide amendments, if required.

APPENDIX A KEY PLAN



APPENDIX B BACKGROUND DOCUMENTS

Alison Gosling

From: Fraser, Mark < Mark.Fraser@ottawa.ca>

Sent: July 31, 2020 9:08 AM

To: Deiaco, Simon

Subject: PC2020-0162_253 York Street

Attachments: 253-255-257 York site plan.pdf; ServicingGuidelines_ final_Dec2009.pdf; Servicing

Report Template Final Version.pdf

Hi Simon,

Please forward the below engineering notes to the applicant regarding a development proposal at **253 York Street**. Note that the information is considered preliminary and the assigned DR Project Manager may modify and/or add additional requirements/conditions upon review of an application or if additional information becomes available.

Comments:

- A deep excavation and dewatering operations have the potential to cause damages to the neighboring adjacent buildings/City infrastructure. Document that construction activities (excavation, dewatering, vibrations associated with construction, etc.) will not have an impact on any adjacent buildings and infrastructure.
- A Record of Site Condition (RSC) in accordance with O.Reg. 153/04 will be required to be <u>filed and</u> <u>acknowledged by the Ministry prior to issuance of a building permit</u> due to a change to a more sensitive property use. O.Reg 153/04 permits the issuance of a building permit for excavation and shoring of excavation but not a construction permit until RSC is acknowledged by the MECP.

Changes of use, s. 168.3.1 (1) (b) of the Act

- **14.** A person shall not change the use of property for the purposes of clause 168.3.1 (1) (b) of the Act in any of the following manners:
- 6. If the property is used for a commercial use as well as any other type or types of property use, a change in the use of part or all of the property used for commercial use to any or all of the following types of property uses:
 - Agricultural or other use.
 - Institutional use.
 - Parkland use.
 - Residential use.
- A singular (1) storm and (1) sanitary service connection to the sewer networks and two (2) water services are permitted for this development if the site is intended to operate under one ownership and remain as single parcel post-development. The additions shall not be serviced independent from the existing building as the City does not want to maintain multiple connections for a single property.
- The sidewalk on Nelson St. fronting the property has a depressed sidewalk for an existing parking lot. This depressed sidewalk shall be removed as part of the site works.
- The condition of the existing services must be verified for reuse to ensure absence of any structural deficiencies and ensure minimum size and materiality requirements are being met. A CCTV scan and accompanying report must be submitted to the City for review to determine if they are acceptable. A comment concerning the CCTV scan and lateral condition must also be included in the servicing report, stating that the existing service laterals for the subject property are absent of any structural defects and are of size and material that adheres to City of Ottawa Guidelines. Located existing services are to be placed on site servicing plan.
- Incorporate permeable pavers into the SWM design to further reduce stormwater runoff however no credit in terms of stormwater management (to be considered and impervious for design purposes).

General:

- It is the consultant /designer's responsibility to verify all the information related to the infrastructures by using as built drawings or field visit and inspection as required.
- It is the sole responsibility of the consultant to investigate the location of existing underground utilities in the proposed servicing area to avoid any conflict with utilities. The location of existing utilities and services shall be documented on an Existing Conditions Plan. Verify all the information related to the infrastructures by using as built drawings or field visit and inspection as required. Include a note on the Servicing and Grading Plan stating the existing utilities in the proposed servicing area have been investigated.
- All underground and above ground building footprints and permanent walls need to be shown on the plans to
 confirm that any permanent structure does not extend either above or below into the existing property lines
 and sight triangles and/or future road widening protection limits.
- Please note that the proposed servicing design and site works shall be in accordance with the following documents:
 - Ottawa Sewer Design Guidelines (October 2012)
 - o Technical Bulletin PIEDTB-2016-01
 - o Technical Bulletins ISTB-2018-01, ISTB-2018-02 and ISTB-2018-03.
 - Ottawa Design Guidelines Water Distribution (2010)
 - o Design Guidelines for Sewage Works, MECP, 2008
 - Stormwater Planning and Design Manual, MECP, March 2003
 - Geotechnical Investigation and Reporting Guidelines for Development Applications in the City of Ottawa (2007)
 - City of Ottawa Slope Stability Guidelines for Development Applications (revised 2012)
 - o City of Ottawa Environmental Noise Control Guidelines (January 2016)
 - City of Ottawa Accessibility Design Standards (November 2015) (City recommends development be in accordance with these standards on private property)
 - Ottawa Standard Tender Documents (latest version)
 - o Ontario Provincial Standards for Roads & Public Works (2013)
 - Record drawings and utility plans are also available for purchase from the City (Contact the City's Information Centre by email at <u>InformationCentre@ottawa.ca</u> or by phone at (613) 580-424 x.44455.
 Include copies in the Appendix of the report as supporting documentation.
- Any proposed work within utility/infrastructure easements requires written consent of the easement owner.



Disclaimer:

The City of Ottawa does not guarantee the accuracy or completeness of the data and information contained on the above image(s) and does not assume any responsibility or liability with respect to any damage or loss arising from the use or interpretation of the image(s) provided. This image is for schematic purposes only.

Stormwater Management Criteria (Quantity and Quality Control) and Servicing Information: SWM Criteria: Discharging into a Separated Sewer System

- Water Quantity Control: Control post-development runoff (for the entire site), up to and including the 100-year storm event, to a 5-year pre-development level. The pre-development runoff coefficient will need to be determined using the <u>smaller of</u> a runoff coefficient of C=0.5 or the actual existing site runoff coefficient. The time of concentration used to determine the pre-development condition will be the larger of 10min. or the calculated time of concentration. [Tc should not be less than 10 min. since IDF curves become unrealistic at less than 10 min; Tc of 10 minutes shall be used for all post-development calculations].
 - o Total allowable release rate will be **5-year pre-development rate**.
 - C Coefficient of runoff will need to be determined as per existing conditions but in no case more than
 0.5
 - o TC =20 minutes or can be calculated,
 - o TC should not be less than 10 minutes, since the IDF curves become unrealistic less than 10min.
 - Any uncontrolled runoff (100-year) is required to be subtracted from the allowable release rate.
- The impact from the receiving system HGL will need to be assessed and considered if proposing underground storage The SWM solution will need to be designed accordingly. The storm connection will need to be above the receiving sewer HGL.
- Any storm events greater than the calculated 5-year allowable release rate, up to and including the 100-year storm event, shall be detained on-site by appropriate SWM measures to avoid impact on the downstream sewer system.
- Water Quality: Please consult with the local conservation authority (RVCA) regarding water quality criteria and onsite requirements prior to submission of an application as the site is located less than 2km from the outlet. It is consultant's responsibility to check with the RVCA regarding water quality control and include this information and discussion within the SWM report. Contact the RVCA for further information regarding requirements for water quality for this project.

- Compare pre-development flows to post-developments flows in the SWM report to document improvement.
- If **rooftop control and storage** is considered as part of the SWM solution for this project sufficient details (Cl. 8.3.8.4) shall be discussed and documented in the report and on the engineering plans. A **roof drainage plan** and detailed roof drain summary table with supporting drain manufacturer information will be required. Any note indicating to be designed by others will not be sufficient for approval. The roof drainage plan will need to document roof drain type, flow rates, emergency scupper locations and spill over elevations and ponding areas. Roof drains are to be connected downstream of any incorporated ICDs within the SWM system and not to the foundation drain system. Provide a **Roof Drain Plan** as part of the engineering submission package.
- Emergency rooftop scuppers and rooftop flow control drains must be shown on the plan if providing roof top storage for stormwater management.
- Provide a memorandum if Rooftop Flow Control drains are used confirming the new roof will be designed to meet the Stormwater Management objectives with flow control drains and roof spill scuppers in accordance with the requirements of clause 7.4.10.4 of the 2012 Ontario Building code.
- Underground Storage: Underground storage volumes are to be based on 50% peak flow rates or use dynamic computer model. The Modified Rational Method for storage computation in the Sewer Design Guidelines was originally intended to be used for above ground storage (i.e. parking lot) where the change in head over the orifice varied from 1.5 m to 1.2 m (assuming a 1.2 m deep CB and a max ponding depth of 0.3 m). This change in head was small and hence the release rate fluctuated little, therefore there was no need to use an average release rate.
 - When underground storage is used, the release rate fluctuates from a maximum peak flow based on maximum head down to a release rate of zero. This difference is large and has a significant impact on storage requirements. We therefore require that an average release rate equal to 50% of the peak allowable rate shall be applied to estimate the required volume. Alternatively, the consultant may choose to use a submersible pump in the design to ensure a constant release rate.
 - In the event that there is a disagreement from the designer regarding the required storage, The City will require that the designer demonstrate their rationale utilizing dynamic modelling, that will then be reviewed by City modellers in the Water Resources Group.
 - Note that the above will added to upcoming revised Sewer Design Guidelines to account for underground storage, which is now widely used.
- If an underground storage tank considered as part of the SWM solution for this project sufficient details and system information will need to be provided in the report and on the plans. A detailed cross-section of such SWM system with sufficient details and information (HWLs, release rate, volume, location, size (dimensions), control device, emergency flow outlet and backflow protection, etc.) will need to be provided. An appropriate emergency overflow location will need to be determined and documented. Backup power supply necessary if pump controlled. Details regarding the proposed on-site stormwater management system are to be provided for review.
- The minimum orifice dia. for a plug style ICD is 83mm and the minimum flow rate from a vortex ICD is 6 L/s in order to reduce the likelihood of plugging otherwise choose to pump the SWM system.
- Please include a Pre-Development Drainage Area Plan to define the pre-development drainage areas/patterns.
 Runoff shall not be directed toward any adjacent properties. Post-development site grading shall match existing property line grades in order to minimize disruption to the adjacent properties.
- Provide a stormwater management summary table within the body of the SWM report to summarize the SWM design for this site.
- Foundation drains are to be <u>independently connected to sewermain (separated or combined) unless being</u> pumped with appropriate back up power, sufficient sized pump and back flow prevention.

Implementation Considerations:

- Accounting for external overland drainage.
- Use of standard ICDs
- Requirement for ICD/roof drain information on the plans
- Requirement for plans showing 100-year ponding limits
- Provide a foundation drain backwater valve installed as per Std Dwg S14.

Storm Sewer:

- Available Storm Sewers: A 600mm dia. Conc. storm sewer is available within York Street and a 300mm dia. Conc. storm sewer is available within Nelson Street. Stormwater drains to the King Edward collector sewer system and discharged to the Ottawa River.
 - For concrete sewer pipe, maintenance manholes shall be installed when the service is greater than 50% of the diameter of the mainline concrete pipe.
- Only one storm connection to the sewer is permitted for this development. Investigate servicing the additions internally through the existing building utilizing the existing sewer lateral if determined to be suitable for reuse.
 Any new connection is to be discussed with the City. The additions shall not be serviced independent from the existing building.
- A storm sewer monitoring maintenance hole is required to be installed at the property line (on the private side of the property) as per City of Ottawa Sewer-Use By-Law 2003-514 (14) *Monitoring Devices*.
- As-built drawings of the existing services within the vicinity of the site are available and to be reviewed in order to determine proper servicing and SWM plan for the subject site(s).
- Foundation drainage system details are to be discussed in the report and document how the system will be integrated into the servicing design. Please note that foundation drain is to be independently connected to sewermain unless being pumped with appropriate back up power, sufficient sized pump and back flow prevention.
- A backwater valve is required on all service laterals for protection.
- Identify if there is an existing storm lateral that drains the foundation weeping tile, if currently installed. If weeping tile is connected to the sanitary lateral, it must be disconnected and drained via separate lateral to the storm sewer system.

Sanitary Sewer:

- Available Sanitary Sewers: A 600mm dia. Conc. sanitary sewer is located within York Street and 300mm dia. Conc. sanitary sewer within Nelson Street. Wastewater flows to the King Edward Trunk Collector sewer system. For concrete sewer pipe, maintenance manholes shall be installed when the service is greater than 50% of the diameter of the mainline concrete pipe.
- Only one sanitary connection to the sewer is permitted for this development. Investigate servicing the additions
 internally through the existing building utilizing the existing sewer lateral if determined to be suitable for reuse.
 Any new connection is to be discussed with the City. The additions shall not be serviced independent from the
 existing building.
- An analysis and demonstration that there is sufficient/adequate residual capacity to accommodate any increase in wastewater flows in the receiving and downstream wastewater system is required to be provided. It is suggested to calculate the total peak wastewater demand for the proposed development and send it to the City as soon as possible in advance of a submission of an application, as an initial step to determine whether or not there is enough capacity in the city system to accommodate the proposed wastewater flow. Please note that it takes approx. 10 business days to get a response back from the internal circulation.
- Existing and proposed increases in sanitary flow are to be calculated using the methods established in City of Ottawa Sewer Design Guidelines (SDG) 2012, as amended. Refer to Section 4, Appendix 4-A, and Technical Bulletin ISTB-2018-01 for guidance.
- A sanitary sewer monitoring maintenance hole is required to be installed at the property line (on the private side of the property) as per City of Ottawa Sewer-Use By-Law 2003-514 (14) *Monitoring Devices*.
- A backwater valve is required on the sanitary service for protection (mandatory now anyways).
- If the site requires to discharge of remediated groundwater, it will require discharge into the sanitary sewer not into city storm sewer per the Sewer Use By-law and subject to a sewer use agreement. Review the ESA reports.

Watermain:

Available Watermains: A 152mm dia. DI watermain is located within York Street and a 203mm dia. DI watermain
is located within Nelson Street. Any connection to the watermain in Nelson Street will be subject to consent
from the Owners of 312 Murray St. as the watermain is situated on private property.

- Analyze and demonstrate there is adequate fire protection for the buildings per *Technical Bulletin ISTB-2018-02*. Multiple municipal hydrants will be required for fire protection. Adequacy of fire flow must be demonstrated.
- Demonstrate that the pressure requirements, per Section 4.2.2.1, 4.2.2.2, and 4.2.2.3 of the WDG, are met for this building.
- Water Supply Redundancy: Residential buildings with a basic day demand greater than 50m³/day (0.57 L/s) are required to be connected to a minimum of two water services separated by an isolation valve to avoid a vulnerable service area as per the Ottawa Design Guidelines Water Distribution, WDG001, July 2010 Clause 4.3.1 Configuration. This proposed development will require two (2) separate water service connections if the basic day demand for this site exceeds 50m³/day. There shall be a primary water service and a secondary connection. This is a corner lot so we will not support the installation of a new isolation valve on the City watermain to satisfy this requirement.
- Include a **hydrant coverage figure** and **demonstrate there is adequate fire protection** for the building per *Technical Bulletin ISTB-2018-02*. Multiple municipal hydrants will be required for fire protection.
- Boundary conditions, HGL, shall be requested and a hydraulic analysis completed to confirm that the require fire flows can be achieved as well as availability of domestic water pressure. Use <u>Table 3-3 of the MOE Design Guidelines for Drinking-Water System</u> to determine Maximum Day and Maximum Hour peaking factors for 0 to 500 persons and Table 4.2 of the ODG-Water Distribution for 501 to 3,000 persons. Provide the following information to the City of Ottawa via email to request water distribution network boundary conditions for the subject site. Please note that once this information has been provided to the City of Ottawa it <u>takes approximately 5-10 business days</u> to receive boundary conditions.
 - Type of Development and Units
 - Site Address (Street Number and Name)
 - Location of service(s).
 - A plan showing the proposed water service connection locations.
 - Average Daily Demand (L/s)
 - Maximum Daily Demand (L/s)
 - Peak Hour Demand (L/s)
 - Required Fire Flow (L/min) FUS calculations are to be provided with request for boundary conditions.

[Fire flow demand requirements shall be based on Fire Underwriters Survey (FUS) Water Supply for Public Fire Protection

1999 and Technical Bulletin ISTB-2018-02]

Exposure separation distances shall be defined on a figure to support the FUS calculation and required fore flow (RFF).

Fire flow demands will be inputted as point loads at each connection separately unless otherwise noted. A multi-hydrant analysis can be requested if necessary.

- If fire protection is provided by existing municipal hydrants, hydrant capacity shall be assessed to demonstrate the RFF can be achieved. Identify which hydrants are being considered to meet the RFF on a **fire hydrant coverage figure** as part of the boundary conditions request.
- Include a figure showing the location of applicable fire hydrants supplying adequate fire flow. If fire protection is provided by existing municipal hydrants, hydrant capacity shall be assessed to demonstrate the RFF can be achieved. Identify which hydrants are being considered to meet the RFF on a fire hydrant coverage figure as part of the boundary conditions request.
- Hydrant capacity shall be assessed if relying on any public hydrants to provide fire protection particularly if high design fire flows are being proposed to demonstrate the RFF can be achieved. Refer to Table 1: Maximum flow to be considered from a given hydrant in Appendix I of Technical Bulletin ISTB-2018-02. Appropriate fire protection mitigation measures shall be investigated/proposed to lower the RFF for the site to an appropriate level
- The subject site is located within the 1W Pressure Zone.

Snow Storage:

Any portion of the subject property which is intended to be used for permanent or temporary snow storage shall be as shown on the approved site plan and grading plan. Snow storage shall not interfere with approved grading and drainage patters or servicing. Snow storage areas shall be setback from the property lines, foundations, fencing or landscaping a minimum of 1.5m. Snow storage areas shall not occupy driveways, aisles, required parking spaces or any portion of a road allowance. If snow is to be removed from the site please indicate this on the plan(s).

Permits and Approvals:

The consultant shall determine if this project will be subject to an Environmental Compliance Approval (ECA). It shall be determined if the exemptions set out in Ontario Regulation 525/98: *Approval Exemptions* are satisfied. All regulatory approvals shall be documented and discussed in the report. This project will be subject to an ECA application if stormwater works are servicing more than one parcel of land (i.e. 78/80 Nelson Street), regardless of ownership.

Capital Woks:

• No capital works are currently planned in this area.

Sight Triangle and Any Road widening Requirement (By Transportation Project Manager Wally Dubyk)

 The Official Plan does not identify York Street or Nelson Street as a protected road corridor. To be confirmed by the Transportation Project Manager assigned to this project.

Required Engineering Plans and Studies in Support of SPC application:

PLANS:

Design drawings are to be provided at a specified scale (1:200, 1L250, 1:300, 1:400, or 1:500)

- Existing Conditions and Removals Plan
- Site Servicing Plan
- Grade Control and Drainage Plan
- Erosion and Sediment Control Plan
- Pre-Development Drainage Area Plan
- Post-Development Drainage Area Plan
- Roof Drainage Plan w/ Roof Drain Summary Table (if rooftop SWM storage is being considered)
- Stormwater Storage System Detail (Internal Cistern Details from the Mechanical Engineer if being considered)
- Foundation Drainage System Details
- Legal Survey Plan
- Site Lighting Plan, Photometric Plan and Site Lighting Certification Letter

REPORTS:

- Site Servicing and Stormwater Management Report
- Geotechnical Study
- Phase 2 Detailed Noise Study (Transportation Noise Assessment and Stationary Noise Assessment) [due to proximity (within 100m) of King Edward Ave. (Arterial Road Classification)] Stationary noise to be discussed in report as per City NCG and NPC 300 Guidelines]
- Phase I ESA (in accordance with Ontario Regulation 153/04)
- Phase II ESA (depending on results and recommendation of the Phase I-ESA)
- Record of Site Condition (RSC) is anticipated to be required for this property due to change to a more sensitive property use.

Servicing Report Template and Guidelines:

Please find attached the Servicing Report Template & Study Guidelines" and prepare the servicing study accordingly. For capacity issue, please see section 3.2.1 page 3-3 and follow this section. A completed checklist with corresponding references from the servicing study is mandatory for the completeness of the study. Please add a completed checklist in the report. Please ensure you are using current guidelines, by-laws and standards.

- Include development statistics (unit type breakdown), building construction type, site area, building GFA from the Architect.
- Include description of lot topography, surface drainage patterns, and ground cover (grass, hard landscaping, asphalt, etc.)
- Include description of the existing sewer laterals servicing the building, including size and material type, and street location of connection to the City main.
- Reports must be prepared and stamped by a Professional Engineer licensed in the Province of Ontario.

Please refer to the City of Ottawa Guide to Preparing Studies and Plans [Engineering]:

https://ottawa.ca/en/planning-development-and-construction/developing-property/development-application-review-process/development-application-submission/guide-preparing-studies-and-plans

Phase One Environmental Site Assessment (Official Plan Section 4.8.4):

- A Phase I ESA is required to be completed in accordance with Ontario Regulation 153/04 (not per CSA standards) in support of this development proposal to determine the potential for site contamination. A Phase II ESA may be required depending on the results and recommendations of the Phase I-ESA. In accordance with O.Reg. 153/04 TOC requirements.
- The Phase I ESA shall include an RSC statement discussing any requirement to file a RSC with the Ministry. A Record of Site Condition (RSC) in accordance with O.Reg. 153/04 is anticipated to be <u>filed and acknowledged by the Ministry prior to issuance of a building permit</u> due to the change in property use. As per the Official Plan (4.8.4) we do not consider an RSC acknowledged by the Ministry until either it's has been confirmed that it will not be audited or it has passed the Ministry audit.
- Please also note that in the event soil and/or groundwater contamination is identified on this site and the proposal is for a more sensitive land use, the MECP will require approximately 1-1.5 years to review the RSC. PIED will apply appropriate conditions, based on Environmental Protection Act (Section 168.3.1 (1)) and O.Reg. 153/04 (Parts IV and V) regarding requirements for RSC prior to building permit issuance. Dependent on the levels/types of contamination, timelines for building permit issuance may be longer than expected and we recommend applicant speak to Building Code Services, at the earliest convenience, so as to discuss these timelines in more detail, if deemed applicable.
- Environmental Risk Information Services (ERIS) report is required to be included as part of the Phase I ESA to support the findings and recommendations.

https://www.ontario.ca/page/guide-completing-phase-one-environmental-site-assessments-under-ontario-regulation-15304

https://www.ontario.ca/laws/regulation/040153#BK43

Geotechnical Investigation (Official Plan Section 4.8.3):

- A **Geotechnical Study/Investigation** shall be prepared in support of this development proposal.
- Investigate the effect of short-term and long-term lowering of the groundwater level and the impact on the adjacent lands and existing neighboring structures. The impact of groundwater lowering on adjacent properties needs to be discussed and investigated to ensure there will be no short term and long term damages associated with lowering the groundwater in this area.
- A deep excavation and dewatering operations have the potential to cause damages to the neighboring adjacent buildings. Document that construction activities (deep excavation, dewatering, vibrations associated with construction, etc.) will not have an negative impact on any adjacent buildings and infrastructure in proximity to the site.
- Dewatering during construction may be subject to volume restrictions, therefore coordinate with the City of Ottawa Sewer Use Program to discuss discharge details.
- Geotechnical Study shall be consistent with the Geotechnical Investigation and Reporting Guidelines for Development Applications.
 - https://documents.ottawa.ca/sites/default/files/documents/cap137602.pdf

Detailed Noise Study:

- A Transportation Noise Assessment is required as the subject development is located in proximity (within 100m) of King Edward Ave. (Arterial Road Classification)]
- A Stationary Noise Assessment is required in order to assess the noise impact of the proposed sources of stationary noise (mechanical HVAC system/equipment) of the development onto the surrounding residential area to ensure the noise levels do not exceed allowable limits specified in the City Environmental Noise Control Guidelines.
- Noise Study shall be consistent with the City's Environmental Noise Control Guidelines.
 https://documents.ottawa.ca/sites/default/files/documents/enviro_noise_guide_en.pdf

Exterior Site Lighting:

Any proposed light fixtures (both pole-mounted and wall mounted) must be part of the approved Site Plan. All external light fixtures must meet the criteria for Full Cut-off Classification as recognized by the Illuminating Engineering Society of North America (IESNA or IES), and must result in minimal light spillage onto adjacent properties (as a guideline, 0.5 fc is normally the maximum allowable spillage). In order to satisfy these criteria, the please provide the City with a Site Lighting Plan, Photometric Plan and Certification (Statement) Letter from an acceptable professional engineer stating that the design is compliant.

Please note that these comments are considered preliminary based on the information available to date and therefore maybe amended as additional details become available and presented to the City. The above pre-consultation comments are to be considered valid for one year. It is the responsibility of the applicant and their representatives/consultants to verify information provided by the City. The applicant may contact me for any follow-up questions related to engineering/infrastructure prior to submission of an application if necessary.

If you have any questions or require any clarification please let me know.

Regards,

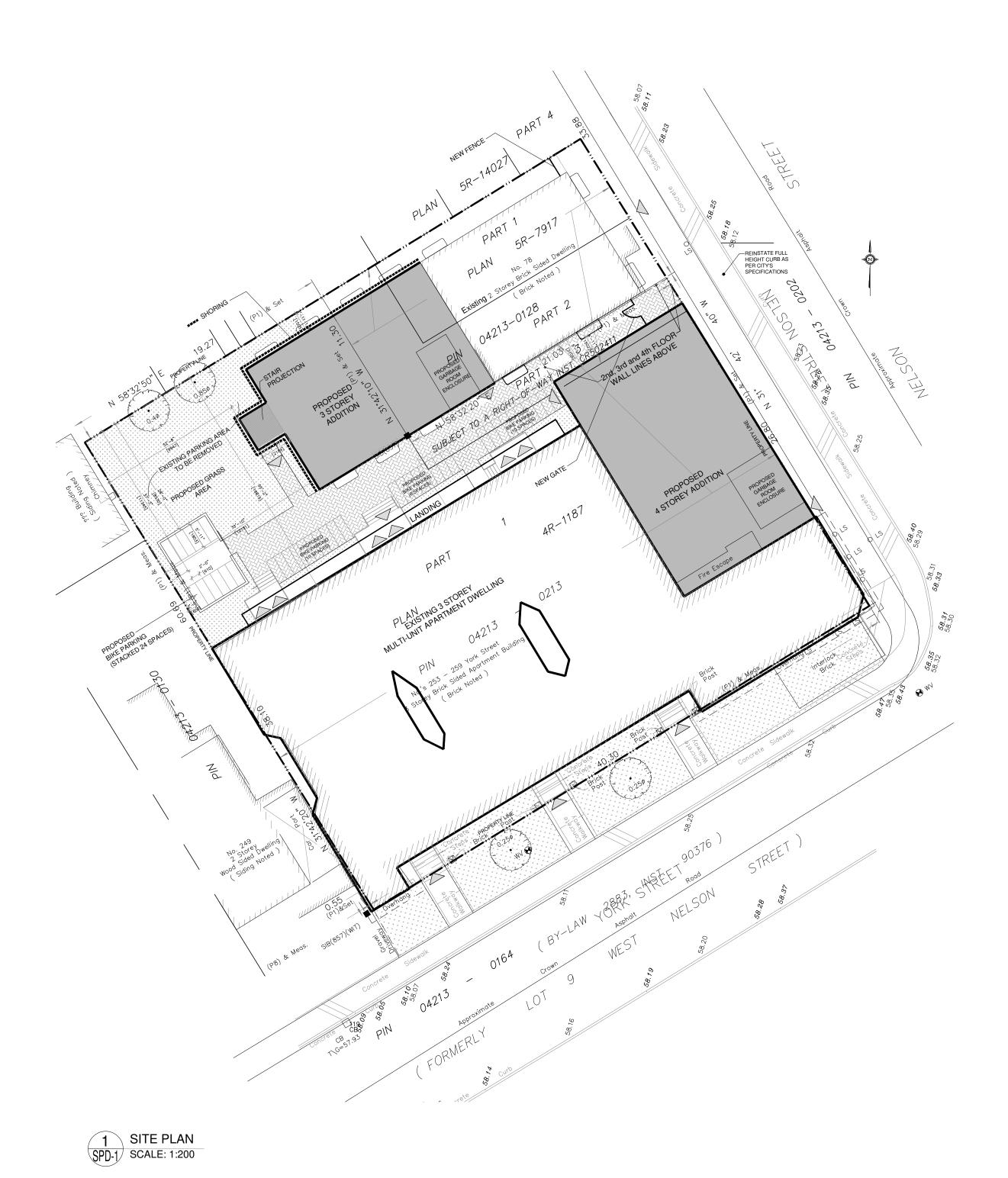
Mark Fraser, P. Eng.
Project Manager, Planning Services
Development Review Central Branch
City of Ottawa | Ville d'Ottawa
Planning, Infrastructure and Economic Development Department
110 Laurier Avenue West. 4th Floor, Ottawa ON, K1P 1J1
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Email: Mark.Fraser@ottawa.ca

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253-255-257 YORK ST. & 78-80 NELSON ST. COMBINED (YORK STREET IS A FRONTAGE)

	0213 & P.I.N.: 04		NE (SEC. 161-162) CITY OF OT	ΤΛ\Λ/Λ·						PREPARED BY F	FARLEY, SMITH & DENIS SURVEYING LTD.
DWELLING TYF	PE: 4 STOREY 8	3 STOREY F	RESIDENTIAL ADDITIONS TO E	EXISTING	G THREE STOREY L	OW RISE A	PARTM	ENT BUILDING (REI	NTALS)		
ZONING MECH	IANISMS				REQUIREMENT		P	ROVIDED	NOTES		
A) MINIMUM L	OT AREA				450 m²			1535 m²			
B) MINIMUM LO	OT WIDTH				15 m			38.10 m			
C) MINIMUM L	OT DEPTH				NA			40.30 m		+	PROPOSED TREE
D) MINIMUM FF	RONT YARD SE	Г ВАСК	AVERAGE		(0m+4.5 m) / 2	! = 2.25		0 m			
E) MINIMUM IN SIDE YARD SE					1.2 m			1.5 m		(+)	EX. TREE TO BE REMOVED
	ORNER YARD S	ET BACK			4.5 m			0 m			
	REAR YARD AR PROVISION AME LOW)		SEE ZONE PROVISIONS ACCORDING TO OMB ORDER FILE NO. PL1507		30% of 40.30 m x 38.10 m =138.			238 m²			EX. TREE TO REMAIN
G) MINIMUM RI	EAR YARD SET	BACK			1.2 m			0 m		\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	DENOTES SOFT LANDSCAPING (SOD)
I) MAXIMUM BL	JILDING HEIGH				14.5 m			12.34 m			DENOTES ASPHALT
J) AMENITY A					0			194 m² @ REAR			DENOTED ANTINET
K) VEHICULE I	PARKING		0.5 PER UNITS IN EXCESS	OF 12	39 x 0.5 = 19.5			0	MINOR VARIANCE		DENOTES HARD LANDSCAPING
L) BICYCLE PA	ARKING		0.5 PER UNITS		20 x 0.5 = 10	OTAL: 17.75		24 INDOOR & 28 OUTDOOR			
			0.25 PER ROOMING UNIT		31 x 0.25 = 7.75						EXISTING BUILDING TO REMAIN
	O WALL RATIO IN STREET ADD							33.36%			PROPOSED ADDITION
DDODOSED OF	TE DEVELOPME	NT INFO		BI	III DINC ADEAS						
LOT COVERAG	TE DEVELOPME	72.5%		В	JILDING AREAS						
SOFT LANDSC		282 m ²		FL	OOR NAME	EXIS	TING	PROPOSED ADDITION	TOTAL	The state of the s	PROPOSED SHRUB (SEE LANDSCAPE PLAN)
COVERAGE :	-				SEMENT						
HARD LANDSC	APING	54.5 m²		E	BUILDING AREA	789.5	m²	310.43 m²	1099.93 m²		PROPOSED RETAINING WALL
ASPHALT		0 m²			DUND FLOOR BUILDING AREA	790	m²	310.43 m²	1100.43 m²		
REAR YARD SO PERCENTAGE:		78.8%				700		0.10.10.111	1100.10111		TREE PROTECTION FENCING
					OND FLOOR BUILDING AREA	790	m²	333.61 m²	1123.61 m²		PROPOSED/EXISTING ENTRY/EXIT
NUMBER OF U	NITS	EXISTIN	IG NEW & EXISTING		RD FLOOR						
252 255 255 25	NDV ST	37 RESIDE		E	BUILDING AREA	672	m²	333.61 m²	1005.61 m²	•	EX. UTILITY POLE
253-255-257 YC	JKK 51.	1 COMMER			IRTH FLOOR BUILDING AREA	0		188.13 m²	188.13 m²	U.P.	- 5
78 & 80 NELSC	ON ST.	12 ROOMING	UNITS 39 ROOMING UNITS							+	EX. CHAINED LINK/BOARD FENCE
CABBACE	OUIDEMENT		l	TOTA	AL BUILDING AREA	3041	.5 m²	1476.21 m²	4517.71 m²		
GARBAGE REC					ernative Setbacks for			E 2016 Dul 201	E 220\		PROPERTY LINE
	0.231 CUBIC YA		PROVIDED 2- 3 CUBIC YARD & 1- 2 CUBIC	⊢ `	B Order File No: PL15			•	,		
GARBAGE	UNIT: 94x0.231:	21.714	YARD GARBAGE CONTAINER 1- 2 CUBIC YARD FIBRE	S colun		e 162A, the n	ninimum	n required rear yard a	nd interior side yard		
RECYCLING	PROVIDE ONE CART AND ONE BLACK CART	360L BLUE 360L	1- 2 COBIC TARD FIBRE 2- 360L BLUE CART& 2- 360L BLACK CART	metre	columns IX and X of Table 162A, the minimum required rear yard and interior side yard setbacks on a corner lot where the minimum front yard setback is greater than 4.5 metres in Area A on Schedule 342 are as follows: (a) Except for a lot containing a Planned Unit Development, the minimum setback						
"KITCHEN CATCHER" "KITCHE CONTAINER FOR EACH CONTAIN DWELLING UNIT AND ONE DWELLING UNIT			from abutt	any rear lot line or inting both the interior kees, as follows:	terior side lot	line is 1	1.2 metres; however,	a further yard			
	COMMONAL 24				or any lots with a lot d						
SNOW REMOV	AL REQUIREME	ENT .		the lo	ot depth by 30 per cei	nt of the lot w	nath, at	a mınımum. (Subject	то ву-Iaw 2020-289)		
SNOW REMOV	CONTAINER PE	R 50 UNITS							ual to 30 per cent of to By-law 2020-289)		



OTTAWA CARLETON CONSTRUCTION GROUP LTD. - BCIN#: 112782 337 SUNNYSIDE AVE, SUITE 101, OTTAWA, ON K1S 0R9

FERNANDO MATOS - BCIN#: 22431 613-884-4425

QUALIFICATION INFO
SMALL BUILDINGS
The undersigned has reviewed and takes responsibility for this design, and has the qualifications and meets the requirements set out in the Ontario Building Code to be a designer.

RESPONSIBILITIES: DO NOT SCALE DRAWINGS

ALL DESIGN AND CONSTRUCTION TO BE IN ACCORDANCE WITH THE ONTARIO BUILDING CODE 2020

ALL CONTRACTORS MUST WORK IN ACCORDANCE WITH ALL LAWS, REGULATIONS AND BYLAWS HAVING JURISDICTION IT IS THE RESPONSIBILITY OF THE APPROPRIATE CONTRACTOR TO CHECK AND VERIFY ALL DIMENSIONS ON SITE AND REPORT ALL ERRORS AND OMISSIONS TO THE ARCHITECT/DESIGNER

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GENERAL NOTES:

SON RENOVATION NEL -80 257 YORK ST. & 78-8 COMBINED PROPOSED ADDITION AND RE 253-255-257

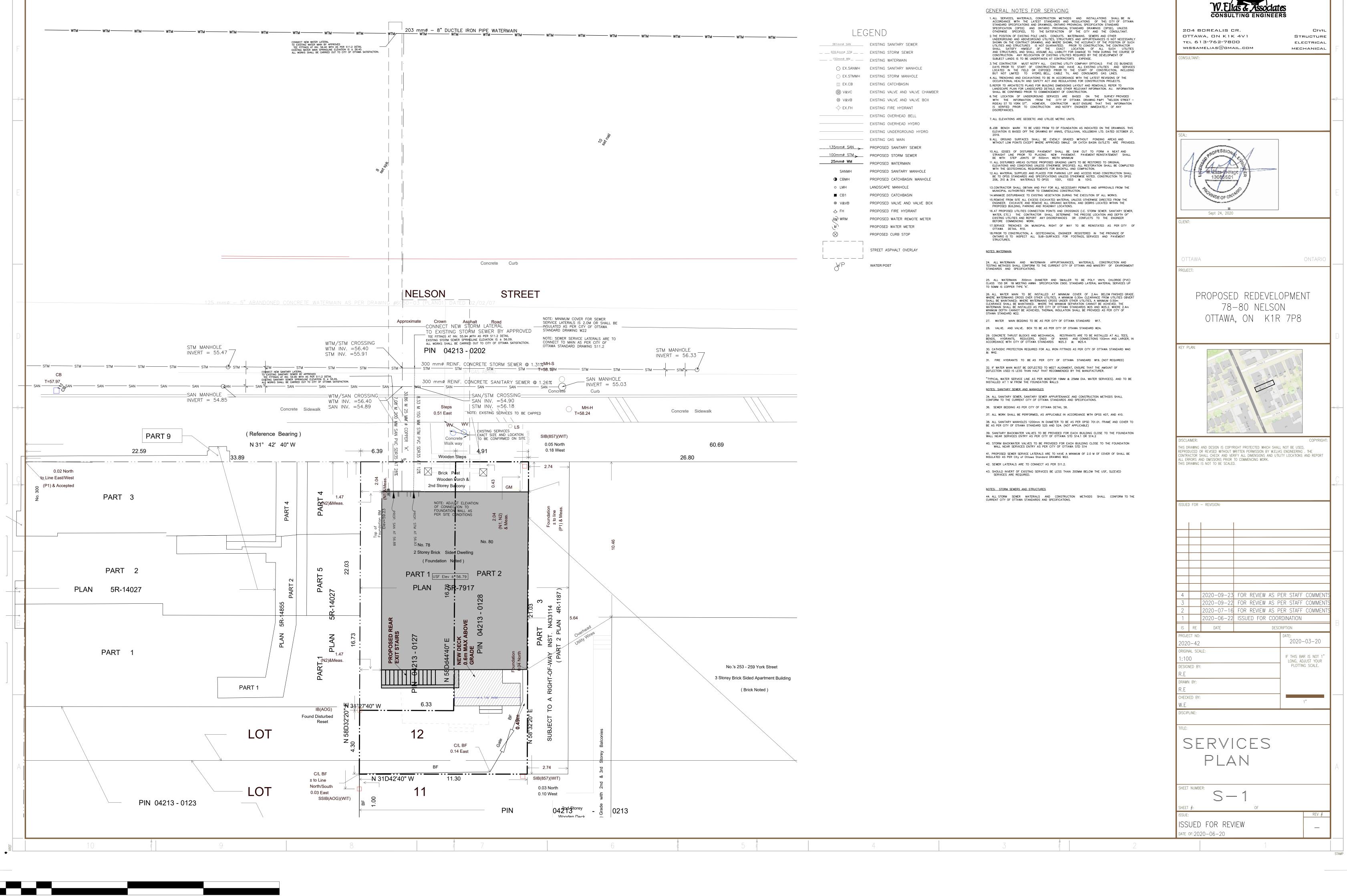
PROJECT: **253-255-257 YORK ST.** & 78-80 NELSON ST.

OTTAWA, ONTARIO K1N 5T9

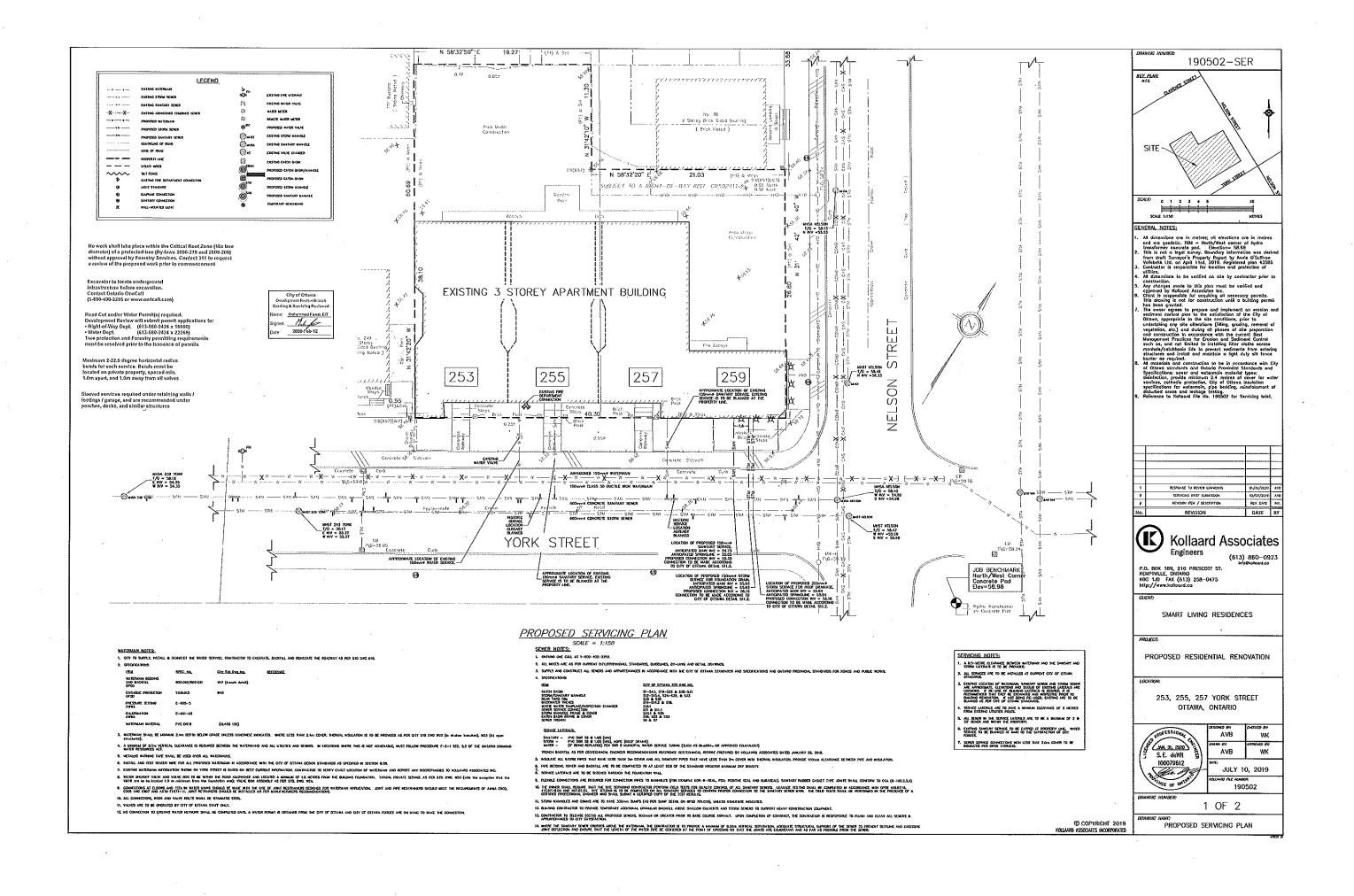
SITE PLAN AND NOTES

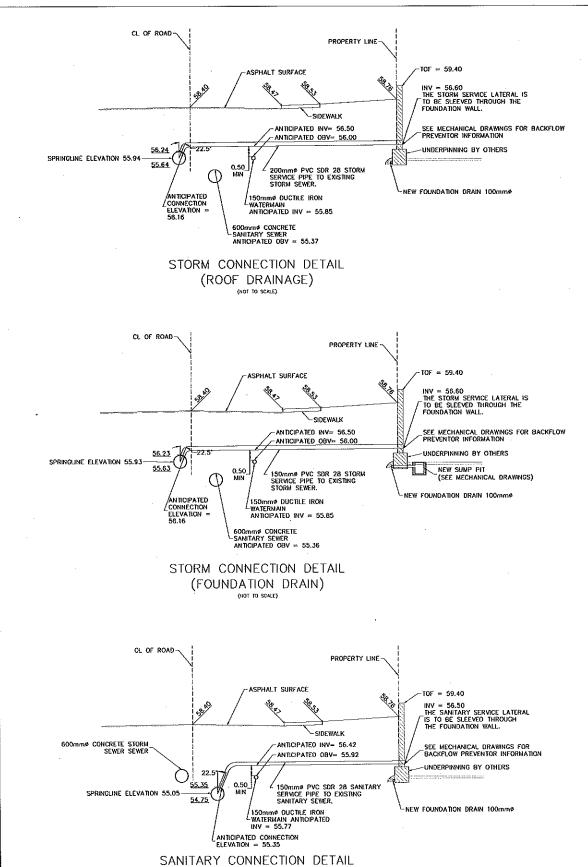
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DATE:MAY, 2021
SCALE: AS NOTED

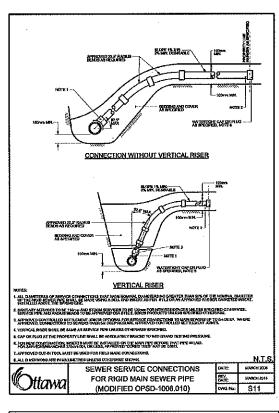


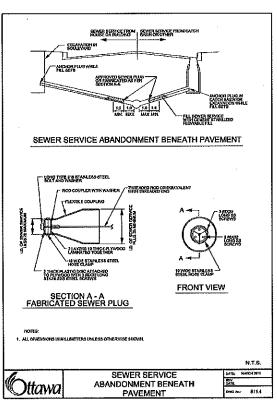
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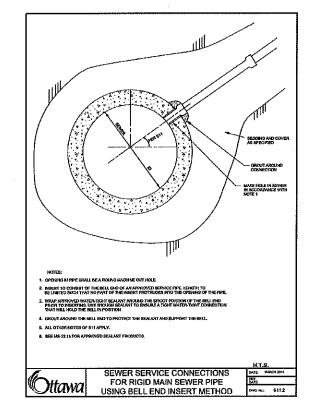


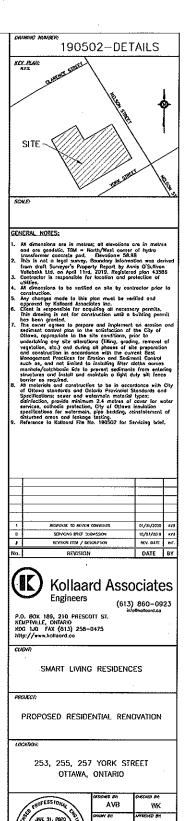


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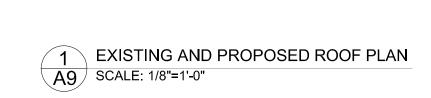






SO W. 31, 2020	AVB	O-ECKED BY:	
S.E. deWit	AVB	. WK	
100079612	JULY 10, 2019		
BOLINEE OF ONTRE	19	0502	

2 OF 2 PROPOSED DETAILS PLAN





OTTAWA CARLETON CONSTRUCTION GROUP LTD. - BCIN#: 112782 337 SUNNYSIDE AVE, SUITE 101, OTTAWA, ON K1S 0R9

Fernando Mates FERNANDO MATOS - BCIN#: 22431 613-884-4425

QUALIFICATION INFO
SMALL BUILDINGS
The undersigned has reviewed and takes
responsibility for this design, and has the
qualifications and meets the requirements
set out in the Ontario Building Code to be a

RESPONSIBILITIES: DO NOT SCALE DRAWINGS

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GENERAL NOTES:

S NEL -80 78 ED YORK 253-255-257

CONSULTANTS: SOMA PRO DESIGNS STRUCTURAL -MECHANICAL -ELECTRICAL -GRADING -

253-255-257 YORK ST. & 78-80 NELSON ST.

OTTAWA, ONTARIO K1N 5T9

EXISTING & PROPOSED ROOF PLAN

DATE:MAY, 2021

SCALE: AS NOTED

 Project:
 COO-22-0938

 Address:
 253 York Street

Re: List of Referenced City Standard Detail Drawings

R10	Standard Trench Reinstatement in Paved Surface
S14	Foundation Drain Backwater Valve Installation
\$24.1	Standard Circular Maintenance Hole Cover
\$25	Standard Circular Frame for Maintenance Holes
\$30	Catch Basin – 'T' For Rear Yard, Ditched Pipe and Landscaping Applications
\$31	Catch Basin – Blow For Rear Yard, Ditched Pipe and Landscaping Applications
SC2	Monolithic Concrete Curb and Sdewalk
SC27	Permeable Paving

Alison Gosling

From: Eric Lalande <eric.lalande@rvca.ca>

Sent: March 10, 2022 2:14 PM

To: Francis Valenti
Cc: Alison Gosling

Subject: RE: 22-0938 - 78-80 Nelson & 253-259 York Street - Quality Control Requirement

Follow Up Flag: Follow up **Flag Status:** Completed

Hi Francis,

Thanks for the site plan, based on the site plan provided the RVCA will not require any additional water quality control requirements, however encourage best management practices, such as outlined in your email.

Thank you,

Eric Lalande, MCIP, RPP

Planner, RVCA 613-692-3571 x1137

From: Francis Valenti < F. Valenti@McIntoshPerry.com >

Sent: Thursday, March 10, 2022 2:02 PM **To:** Eric Lalande <eric.lalande@rvca.ca>

Cc: Alison Gosling <a.gosling@mcintoshperry.com>

Subject: RE: 22-0938 - 78-80 Nelson & 253-259 York Street - Quality Control Requirement

Hi Eric,

Please find attached the site plan for your review. No surface parking is proposed. Permeable paving walkways and landscaping is proposed around the building additions. If you have any other questions please let me know.

Regards,

Francis Valenti, EIT

Engineering Intern, Land Development

T. 613.714.6895 | **C.** 613.808.2123

F.Valenti@McIntoshPerry.com | www.mcintoshperry.com

McINTOSH PERRY

Turning Possibilities Into Reality

From: Eric Lalande <eric.lalande@rvca.ca>

Sent: March 10, 2022 1:50 PM

To: Francis Valenti < F. Valenti@McIntoshPerry.com > **Cc:** Alison Gosling < a.gosling@mcintoshperry.com >

Subject: RE: 22-0938 - 78-80 Nelson & 253-259 York Street - Quality Control Requirement

Hi Francis,

Do you have a site plan I can look at?

I'm interested in how much surface parking will be proposed?

Thanks,

Eric Lalande, MCIP, RPP

Planner, RVCA 613-692-3571 x1137

From: Francis Valenti < F. Valenti@McIntoshPerry.com >

Sent: Thursday, March 10, 2022 1:41 PM **To:** Eric Lalande < <u>eric.lalande@rvca.ca</u>>

Cc: Alison Gosling <a.gosling@mcintoshperry.com>

Subject: 22-0938 - 78-80 Nelson & 253-259 York Street - Quality Control Requirement

Good afternoon,

We wanted to touch base with you regarding the development at 78-80 Nelson Street and 253-259 York Street.

The development will consist of a three story addition to the existing residential building at 78-80 Nelson Street, and a 4-storey addition to the existing residential building at 253-259 York Street. Water from the existing buildings is currently collected and conveyed to the 300mm diameter concrete storm sewer with Nelson Street, and the 600mm diameter concrete storm sewer within York Street, respectively. Stormwater flow from both buildings then enters the 1800mm diameter storm sewer within King Edward, where it travels approximately 1.5km before discharging into the Ottawa River at Outlet#04452. Water from the proposed buildings will maintain existing drainage paths through the existing buildings. Surface water will be collected on site and conveyed to the 300mm diameter concrete storm sewer within Nelson Street, where it will also travel approximately 1.5km before discharging into the Ottawa River at Outlet#04452. A drainage figure is attached showing the storm drainage path for the proposed development.

Due to the distance to the outlet, it is not anticipated that quality controls will be required for the proposed development. Can you please review and confirm?

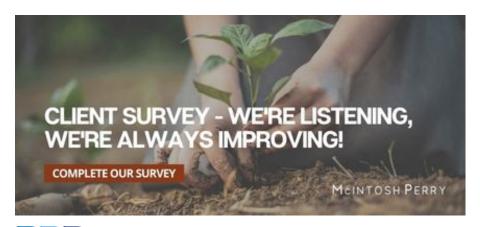
Thanks,

Francis Valenti, EIT

Engineering Intern, Land Development
T. 613.714.6895 | C. 613.808.2123
F.Valenti@McIntoshPerry.com | www.mcintoshperry.com

McINTOSH PERRY

Turning Possibilities Into Reality

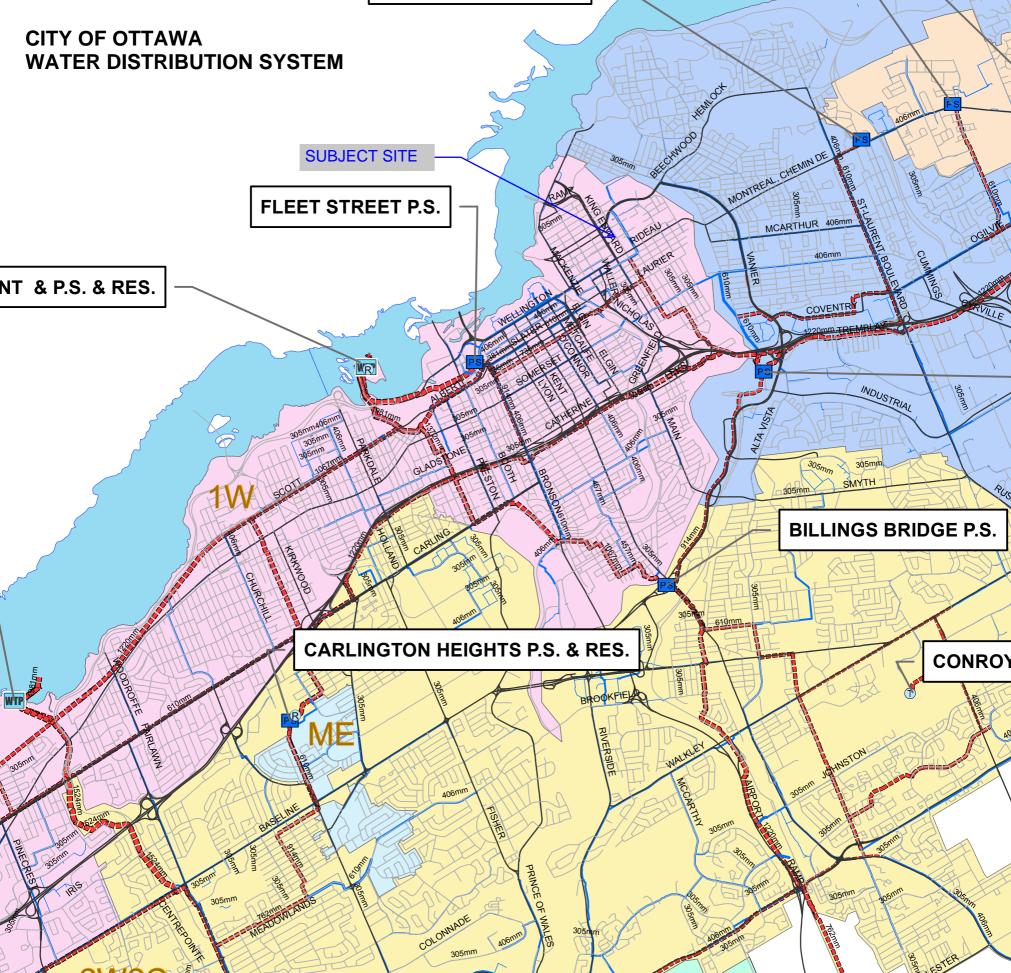




Confidentiality Notice – If this email wasn't intended for you, please return or delete it. Click here to read all of the legal language around this concept.

APPENDIX C WATERMAIN CALCULATIONS

McINTOSH PERRY



CO-22-0938 - 78 & 80 Nelson Street Addition (B1) - Water Demands

Project: 78 & 80 Nelson Street Addition (B1)

 Project No.:
 CO-22-0938

 Designed By:
 AJG

 Checked By:
 RDF

Date: August 23, 2021

 Site Area:
 0.154 gross ha

 Residential
 26 Bachelor
 1.4 Persons per unit

Population 36

AVERAGE DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS	DEMANDS
Residential	280	L/c/d	0.12
Industrial - Light	35,000	L/gross ha/d	0
Industrial - Heavy	55,000	L/gross ha/d	0
Shopping Centres	2,500	L/(1000m ² /d	0
Motels	150	L/(bed-space/d)	0
Hotels	225	L/(bed-space/d)	0
Tourist Commercial	28,000	L/gross ha/d	0
Othe Commercial	28,000	L/gross ha/d	0
AVERAGE DAILY DEMAND	0.12	L/s	
AVERAGE DAILY DEMIAND	7.08	L/min	

MAXIMUM DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS	DEMANDS
Residential	4.9 x avg. day	L/c/d	0.58
Industrial	1.5 x avg. day	L/gross ha/d	
Commercial	1.5 x avg. day	L/gross ha/d	
Institutional	1.5 x avg. day	L/gross ha/d	
MAXIMUM DAILY DEMAND	0.58	L/s	
WAXIMUM DAILY DEMAND	34.68	L/min	

MAXIMUM HOUR DEMAND

DEMAND TYPE	AMOUNT	UNITS	DEMANDS
Residential	7.4 x avg. day	L/c/d	0.87
Industrial	1.8 x max. day	L/gross ha/d	
Commercial	1.8 x max. day	L/gross ha/d	
Institutional	1.8 x max. day	L/gross ha/d	
MAXIMUM HOUR DEMAND	0.87	L/s	
WIAXIIVIOIVI HOOK DEIVIAND	52.38	L/min	

WATER DEMAND DESIGN FLOWS PER UNIT COUNT

CITY OF OTTAWA - WATER DISTRIBUTION GUIDELINES, JULY 2010

CO-22-0938 - 78 & 80 Nelson Street Addition (B1) - Water Demands

Project: 78 & 80 Nelson Street Addition (B1)

 Project No.:
 CO-22-0938

 Designed By:
 AJG

 Checked By:
 RDF

Date: August 23, 2021

 Site Area:
 0.154 gross ha

 Residential
 12 Bachelor
 1.4 Persons per unit

Population 17 *53 persons total

AVERAGE DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS	DEMANDS
Residential	280	L/c/d	0.05
Industrial - Light	35,000	L/gross ha/d	0
Industrial - Heavy	55,000	L/gross ha/d	0
Shopping Centres	2,500	L/(1000m ² /d	0
Motels	150	L/(bed-space/d)	0
Hotels	225	L/(bed-space/d)	0
Tourist Commercial	28,000	L/gross ha/d	0
Othe Commercial	28,000	L/gross ha/d	0
AVERACE DAILY DEMAND	0.05	L/s	
AVERAGE DAILY DEMAND	3.27	L/min	

MAXIMUM DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS	DEMANDS
Residential (Peaking Factor based on total population)	4.9 x avg. day	L/c/d	0.27
Industrial	1.5 x avg. day	L/gross ha/d	
Commercial	1.5 x avg. day	L/gross ha/d	
Institutional	1.5 x avg. day	L/gross ha/d	
MAXIMUM DAILY DEMAND	0.27	L/s	
IVIAXIIVIOIVI DAILY DEIVIAND	16.01	L/min	

MAXIMUM HOUR DEMAND

DEMAND TYPE	AMOUNT	UNITS	DEMANDS
Residential (Peaking Factor based on total population)	7.4 x avg. day	L/c/d	0.40
Industrial	1.8 x max. day	L/gross ha/d	
Commercial	1.8 x max. day	L/gross ha/d	
Institutional	1.8 x max. day	L/gross ha/d	
MAXIMUM HOUR DEMAND	0.40	L/s	
IVIAXIIVIOIVI HOOK DEIVIAND	24.17	L/min	

WATER DEMAND DESIGN FLOWS PER UNIT COUNT

CITY OF OTTAWA - WATER DISTRIBUTION GUIDELINES, JULY 2010

CO-22-0938 - 253 York Street Addition (B2) - Water Demands

Project: 253 York Street Addition (B2)

 Project No.:
 CO-22-0938

 Designed By:
 AJG

 Checked By:
 RDF

Date: August 23, 2021

Site Area: 0.154 gross ha

Residential 20 Bachelor/1 Bedroom 1.4 Persons per unit

Population 28

AVERAGE DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS	DEMANDS
Residential	280	L/c/d	0.09
Industrial - Light	35,000	L/gross ha/d	0
Industrial - Heavy	55,000	L/gross ha/d	0
Shopping Centres	2,500	L/(1000m ² /d	0
Motels	150	L/(bed-space/d)	0
Hotels	225	L/(bed-space/d)	0
Tourist Commercial	28,000	L/gross ha/d	0
Othe Commercial	28,000	L/gross ha/d	0
AVERACE DAILY DEMAND	0.09	L/s	
AVERAGE DAILY DEMAND	5.44	L/min	

MAXIMUM DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS	DEMANDS
Residential	9.5 x avg. day	L/c/d	0.86
Industrial	1.5 x avg. day	L/gross ha/d	
Commercial	1.5 x avg. day	L/gross ha/d	
Institutional	1.5 x avg. day	L/gross ha/d	
MAXIMUM DAILY DEMAND	0.86	L/s	
WIAXIIVIOW DAILY DEWIAND	51.72	L/min	

MAXIMUM HOUR DEMAND

DEMAND TYPE	AMOUNT	UNITS	DEMANDS
Residential	14.3 x avg. day	L/c/d	1.30
Industrial	1.8 x max. day	L/gross ha/d	
Commercial	1.8 x max. day	L/gross ha/d	
Institutional	1.8 x max. day	L/gross ha/d	
MAXIMUM HOUR DEMAND	1.30	L/s	
WAXIWOW HOOK DEWAND	77.86	L/min	

WATER DEMAND DESIGN FLOWS PER UNIT COUNT

CITY OF OTTAWA - WATER DISTRIBUTION GUIDELINES, JULY 2010

CCO-22-0938 - 78 & 80 Nelson Addition - Fire Underwriters Survey (FUS) Fire Calculations

Project: 78 & 80 Nelson (B1)

Project No.: CO-22-0938
Designed By: AJG

Checked By: RDF

Date: August 23, 2021

From the Fire Underwriters Survey (1999)

From Part II – Guide for Determination of Required Fire Flow Copyright I.S.O.:

Updated per City of Ottawa Technical Bulletin ISTB-2018-02

A. BASE REQUIREMENT (Rounded to the nearest 1000 L/min)

 $F = 220 \times C \times VA$ Where: F =Required fire flow in liters per minute

C = Coefficient related to the type of construction.

A = The total floor area in square meters (including all storey's, but excluding basements at least

50 percent below grade) in the building being considered.

Construction Type Wood Frame

C 1.5 A 672.9 m

*Note: Area is the proposed addition + the existing building.

Caluclated Fire Flow 8560.3 L/min 9000.0 L/min

B. REDUCTION FOR OCCUPANCY TYPE (No Rounding)

From note 2, Page 18 of the Fire Underwriter Survey:

Combustible 0%

Fire Flow 9000.0 L/min

C. REDUCTION FOR SPRINKLER TYPE (No Rounding)

Standard Water Supply Sprinklered -40%

Reduction -3600 L/min

D. INCREASE FOR EXPOSURE (No Rounding)

	Separation Distance (m)	Cons.of Exposed Wall	Length Exposed Adjacent Wall (m)	Height (Stories)	Length- Height Factor		
Exposure 1	3.1 to 10	Ordinary (Unprotected)	5	2	10	18%	
Exposure 2	<45	Ordinary (Unprotected)	30	2	60	18%	
Exposure 3	0 to 3	Wood frame	10	4	40	10%	
Exposure 4	10.1 to 20	Wood frame	8	2	16	14%	
					% Increase*	60%	_

Increase* 5400.0 L/min

E. Total Fire Flow (Rounded to the Nearest 1000 L/min)

 Fire Flow
 10800.0 L/min

 Fire Flow Required**
 11000.0 L/min

^{*}In accordance with Part II, Section 4, the Increase for separation distance is not to exceed 75%

^{**}In accordance with Section 4 the Fire flow is not to exceed 45,000 L/min or be less than 2,000 L/min

CCO-22-0938 - 253 York Street Addition (B2) - Fire Underwriters Survey (FUS) Fire Calculations

Project: 253 York Street Addition (B2)

Project No.: CO-22-0938 Designed By: AJG Checked By: RDF

August 23, 2021 Date:

From the Fire Underwriters Survey (1999)

From Part II - Guide for Determination of Required Fire Flow Copyright I.S.O.:

Updated per City of Ottawa Technical Bulletin ISTB-2018-02

A. BASE REQUIREMENT (Rounded to the nearest 1000 L/min)

 $F = 220 \times C \times VA$ Where: **F** = Required fire flow in liters per minute

C = Coefficient related to the type of construction.

A = The total floor area in square meters (including all storey's, but excluding basements at least

50 percent below grade) in the building being considered.

0%

Construction Type Wood Frame

С 1.5 д 2,824.7

*Note: Area is the proposed addition + the existing building.

Caluclated Fire Flow

Reduction

17538.8 L/min 18000.0 L/min

-7200 L/min

B. REDUCTION FOR OCCUPANCY TYPE (No Rounding)

From note 2, Page 18 of the Fire Underwriter Survey: Combustible

Fire Flow 18000.0 L/min

C. REDUCTION FOR SPRINKLER TYPE (No Rounding)

Standard Water Supply Sprinklered

-40%

D. INCREASE FOR EXPOSURE (No Rounding)

	Separation Distance (m)	Cons.of Exposed Wall	Length Exposed Adjacent Wall (m)	Height (Stories)	Length- Height Factor		
Exposure 1	0 to 3	Wood frame	28	3	85	18%	
Exposure 2	30.1 to 45	Wood frame	12	2	24	18%	
Exposure 3	10.1 to 20	Ordinary (Unprotected)	17	3	51	10%	
Exposure 4	0 to 3	Wood frame	8	2	16	14%	
					0/ Ingrasas*	600/	

Increase* 10800.0 L/min

E. Total Fire Flow (Rounded to the Nearest 1000 L/min)

Fire Flow 21600.0 L/min 22000.0 L/min Fire Flow Required**

^{*}In accordance with Part II, Section 4, the Increase for separation distance is not to exceed 75%

^{**}In accordance with Section 4 the Fire flow is not to exceed 45,000 L/min or be less than 2,000 L/min

CO-22-0938 - 78 & 80 Nelson Street - OBC Fire Calculations

 Project:
 78 80 Nelson Street

 Project No.:
 CCO-22-0938

 Designed By:
 AJG

 Checked By:
 AJG

 Date:
 August 26, 2021

Ontario 2006 Building Code Compendium (Div. B - Part 3)

Water Supply for Fire-Fighting - Residential

Building is classified as Group: C

(from table 3.2.2.55)

*approximate distances

Building is of combustible construction. Floor assemblies are fire separations but with no fire-resistance ratings. Roof assemblies, mezzanies, loadbearing walls, columns and arches do not have a fire-resistance rating.

From Div. B A-3.2.5.7. of the Ontario Building Code - 3. Building On-Site Water Supply:

(a) $Q = K \times V \times Stot$

where:

Q = minimum supply of water in litres

K = water supply coefficient from Table 1

V = total building volume in cubic metres

Stot = total of spatial coefficient values from the property line exposures on all sides as obtained from the formula:

Stot = 1.0 + [Sside1+Sside2+Sside3+...etc.]

							From
К	23	(from Table 1 pg A-31) (Worst case occupancy {C} 'K' value used)				Figure 1
V	1,641	(Total building volume in m³.)					(A-32)
Stot	2.0	(From figure 1 pg A-32)		Snorth	1.50	m	0.5
Q =	75,476.77	L		Seast	2.00	m	0.5
				Ssouth	26.80	m	0.0
From Table 2: Required Minim	num Water Supply F	ow Rate (L/s)		Swest	10.00	m	0.0

2700 L/min if Q < 108,000 L 713 gpm

CO-22-0938 - 253 York Street - OBC Fire Calculations

 Project:
 253 York Street

 Project No.:
 CO-22-0938

 Designed By:
 AJG

 Checked By:
 AJG

 Date:
 August 23, 2021

Ontario 2006 Building Code Compendium (Div. B - Part 3)

Water Supply for Fire-Fighting - Residential

Building is classified as Group: C

(from table 3.2.2.55)

From

Building is of combustible construction. Floor assemblies are fire separations but with no fire-resistance ratings. Roof assemblies, mezzanies, loadbearing walls, columns and arches do not have a fire-resistance rating.

From Div. B A-3.2.5.7. of the Ontario Building Code - 3. Building On-Site Water Supply:

(a) $Q = K \times V \times Stot$

where:

Q = minimum supply of water in litres

K = water supply coefficient from Table 1

V = total building volume in cubic metres

Stot = total of spatial coefficient values from the property line exposures on all sides as obtained from the formula:

Stot = 1.0 + [Sside1+Sside2+Sside3+...etc.]

K	23	(from Table 1 pg A-31) (Worst case occupancy {C} 'K' value used)					Figure 1
V	6,888	(Total building volume in m³.)					(A-32)
Stot	2.0	(From figure 1 pg A-32)		Snorth	13.40	m	0.0
Q =	316,836.4	3 L		Seast	0.00	m	0.5
				Ssouth	0.00	m	0.5
From Table 2: Required Mini	mum Water Supply	Flow Rate (L/s)		Swest	0.00	m	0.5
				*app	oroximate d	listan	ces

9000 L/min if Q > 270,000 L 2378 gpm

CO-22-0938 - 253 York Street Addition, 78 & 80 Nelson Street Addition - Boundary Condition Unit Conv

253 York Street Addition, 78 & 80 Nelson Street Addition Project:

Project No.: CO-22-0938 Designed By: AJG

RDF Date: March 10, 2022

Boundary Conditions Unit Conversion

YORK STREET

Checked By:

Scenario	Height (m)	Elevation (m)	m H ₂ O	PSI	kPa
Avg. DD	115.4	58.1	57.3	81.5	562.0
Fire Flow (60 L/s OBC)	106.9	58.1	48.8	69.4	478.6
Peak Hour	106.2	58.1	48.1	68.4	471.8

WATERMAIN DESIGN

When underpinning was completed on the building, part of the existing water lateral was uncovered. The construction manager on site commented that the pipe was of ductile iron material and was in sufficient condition. Correspondence is included in the appendix. The existing 100mm diameter water lateral is to remain.

Fire flow protection requirements were calculated as per the Fire Underwriter's Survey (FUS) Calculations of the fire flow required for the building are provided in Appendix B.

From Appendix B, the maximum fire flow requirement is 14875 L/min or 248 L/sec.

Water Demand 4.1

The water demand for the proposed development was calculated based on the City of Ottawa Water Distribution Design Guidelines (as amended) as follows:

Residential

Total domestic pop:				
One Bedroom units	(14) x 1.4 ppu:	19.6		,
Two Bedroom units	(14) x 2.1 ppu:	29.4		
Three Bedroom	(1) x 3.1 ppu	3.1		
Four Bedroom	(8) x 4.2 ppu	33. <u>6</u>		
Total:		85.7		
Q _{Domestic} = 86 x 350	L/person/day x (1/86,40	00 sec/day)	=	0.35 L/sec

- Average daily demand 0.35 L/s
- Maximum daily demand (factor of 2.5) is $0.35 \text{ L/s} \times 2.5 = 0.87 \text{ L/s}$
- Peak hourly demand (factor of 2.2) = $0.87 \text{ L/s} \times 2.2 = 1.92 \text{ L/s}$

Boundary Conditions

The water demand due to occupancy together with the fire flow requirements were provided to the City of Ottawa in 2019 as follows:

- Average daily water demand 0.4 L/s
- Maximum daily water demand 1.0 L/s
- Peak hourly water demand 2.2 L/s

: FED 11 2020



• Fire Flow required 273 L/s

It is assumed that the water services will be connected to the 150 mm diameter ductile iron (DI) water main along York Street.

The following are the boundary conditions, HGL, for hydraulic analysis that were provided in 2019 for the above indicated peak hourly demand and fire flow demand.

Minimum HGL = 106.5m Maximum HGL = 115.0m

The actual water demand and sanitary was modified from what was submitted for boundary conditions, as the unit count and floor areas were verified. The average daily water demand decreased by 0.06 L/s. It is expected that this minor decrease will have negligible impact on the minimum HGL.

The City of Ottawa Design Guidelines – Water Distribution as amended by technical bulletin ISDTB-2014-02 indicates that if possible water distribution systems are to be designed to provide residual pressures of 345 to 552 kPa in all occupied areas outside of the public right-ofway.

In accordance with MOE Guidelines, the distribution system shall be sized so that under maximum hourly demand conditions the pressures are no less than 276 kPa (40 psi.)

The pressure loss to the third floor of the proposed building was calculated using Bernoulli's Equation in Combination with the Darcy – Weisbach Equation and the Colebrook Equation. The equations are shown below.

$$\begin{split} H_D + Z_1 - Z_2 + \frac{P_1 - P_2}{S} + \frac{V_1^2 - V_2^2}{2g} &= h_f + h_m \quad \text{where:} \\ h_m = K_m \frac{V^2}{2g} \quad \text{Re} = \frac{VD}{V} \quad Q = VA \quad A = \frac{\pi}{4}D^2 \\ \text{Darcy-Weisbach Equation} \quad h_f = f \frac{L}{D} \frac{V^2}{2g} \quad \text{where:} \\ \text{If laminar flow} \left(\text{Re} < 4000 \text{ and any } \frac{e}{D} \right), \quad f = \frac{64}{\text{Re}} \\ \text{If turbulent flow} \left(4000 \le \text{Re} \le 10^8 \text{ and } 0 \le \frac{e}{D} < 0.05 \right), \text{ then} \\ \text{Colebrook Equation:} \quad \frac{1}{\sqrt{f}} = -2.0 \log \left(\frac{e/D}{3.7} + \frac{2.51}{\text{Re}\sqrt{f}} \right) \end{split}$$



Alison Gosling

From: Bakhit, Reza <reza.bakhit@ottawa.ca>

Sent: September 1, 2021 10:36 AM

To: Alison Gosling

Subject: RE: 22-0938 253 York, 78 Nelson, 80 Nelson - Boundary Condition Request

Attachments: 253 York Street August 2021.pdf

Follow Up Flag: Follow up Flag Status: Flagged

Good morning Alison,

The following are boundary conditions, HGL, for hydraulic analysis at 253 York, 78 Nelson and 80 Nelson Street (zone 1W) assumed connected to the 153 mm watermain on York Street and the 203 mm watermain on Nelson Street (see attached PDF for location).

Both Connections

Minimum HGL: 106.2 m
Maximum HGL: 115.4 m

York Street

Max Day + FF (60 L/s): 106.9 m Max Day + FF (366.7 L/s): N/A

Nelson Street

Max Day + FF (45 L/s): 108.2 m Max Day + FF (183.3 L/s): 104.2 m

These are for current conditions and are based on computer model simulation.

Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation.

Kind regards,

Reza Bakhit, P.Eng, C.E.T

Project Manager

Planning, Infrastructure and Economic Development Department - Services de la planification, de l'infrastructure et du développement économique

Development Review - Centeral Branch

City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1 613.580.2400 ext./poste 19346, reza.bakhit@ottawa.ca

Please note: Given the current pandemic, I will be working from home until further notice; reaching me by email is the easiest. I will be checking my voicemail, just not as frequently as I normally would be.

From: Alison Gosling <a.gosling@mcintoshperry.com>

Sent: Thursday, August 26, 2021 8:56 AM To: Bakhit, Reza < reza.bakhit@ottawa.ca>

Subject: RE: 22-0938 253 York, 78 Nelson, 80 Nelson - Boundary Condition Request

CAUTION: This email originated from an External Sender. Please do not click links or open attachments unless you recognize the source.

ATTENTION : Ce courriel provient d'un expéditeur externe. Ne cliquez sur aucun lien et n'ouvrez pas de pièce jointe, excepté si vous connaissez l'expéditeur.

Good morning Reza,

OBC calculations for the building additions are attached and summarized below.

Nelson St Addition – 2,700 L/min (45 L/s) York St Addition – 3,600 L/min (60 L/s)

Thank you,

Alison Gosling, P.Eng.

Project Engineer, Land Development
115 Walgreen Road, Carp, ON, K0A 1L0
T. 613.714.4629
a.gosling@mcintoshperry.com | www.mcintoshperry.com

McINTOSH PERRY

From: Bakhit, Reza < reza.bakhit@ottawa.ca>

Sent: August 25, 2021 10:32 AM

To: Alison Gosling < <u>a.gosling@mcintoshperry.com</u>>

Subject: RE: 22-0938 253 York, 78 Nelson, 80 Nelson - Boundary Condition Request

Good morning Alison,

Thanks for the info and the documents.

Could you please include the fire flow based on the OBC as well?

Appreciated,

Reza Bakhit, P.Eng, C.E.T

Project Manager

Planning, Infrastructure and Economic Development Department - Services de la planification, de l'infrastructure et du développement économique

Development Review - Centeral Branch

City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1

613.580.2400 ext./poste 19346, reza.bakhit@ottawa.ca

Please note: Given the current pandemic, I will be working from home until further notice; reaching me by email is the easiest. I will be checking my voicemail, just not as frequently as I normally would be.

From: Alison Gosling <a.gosling@mcintoshperry.com>

Sent: Tuesday, August 24, 2021 4:47 PM **To:** Bakhit, Reza < reza.bakhit@ottawa.ca

Subject: 22-0938 253 York, 78 Nelson, 80 Nelson - Boundary Condition Request

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ATTENTION : Ce courriel provient d'un expéditeur externe. Ne cliquez sur aucun lien et n'ouvrez pas de pièce jointe, excepté si vous connaissez l'expéditeur.

Good afternoon Reza,

We would like to request Boundary Conditions for the proposed site located at 253 York St, 78 Nelson St, and 80 Nelson St. The proposed development consists of a 3-storey building addition with 26 units and a 4-storey building addition with 20 units. The proposed connections will be to the existing 152mm dia. watermain within York Street and to the 203mm dia. watermain within Nelson St.

York Street:

- The estimated fire flow is 22,000 L/min based on the FUS
- Average daily demand: 0.09 L/s OR 0.49 L/s with the existing building
- Maximum daily demand: 0.86 L/s OR 1.86 L/s with the existing building
- Maximum hourly daily demand: 1.30 L/s OR 2.50 L/s with the existing building

Nelson Street:

- The estimated fire flow is 11,000 L/min based on the FUS
- Average daily demand: 0.12 L/s
- Maximum daily demand: 0.58 L/s
- Maximum hourly daily demand: 0.93 L/s

Attached is a map showing the proposed connection location along with the calculations prepared for the demands listed above.

Please let me know if you have any questions.

Thank you,

Alison Gosling, P.Eng.

Project Engineer, Land Development
115 Walgreen Road, Carp, ON, K0A 1L0
T. 613.714.4629
a.gosling@mcintoshperry.com | www.mcintoshperry.com

McINTOSH PERRY

Turning Possibilities Into Reality





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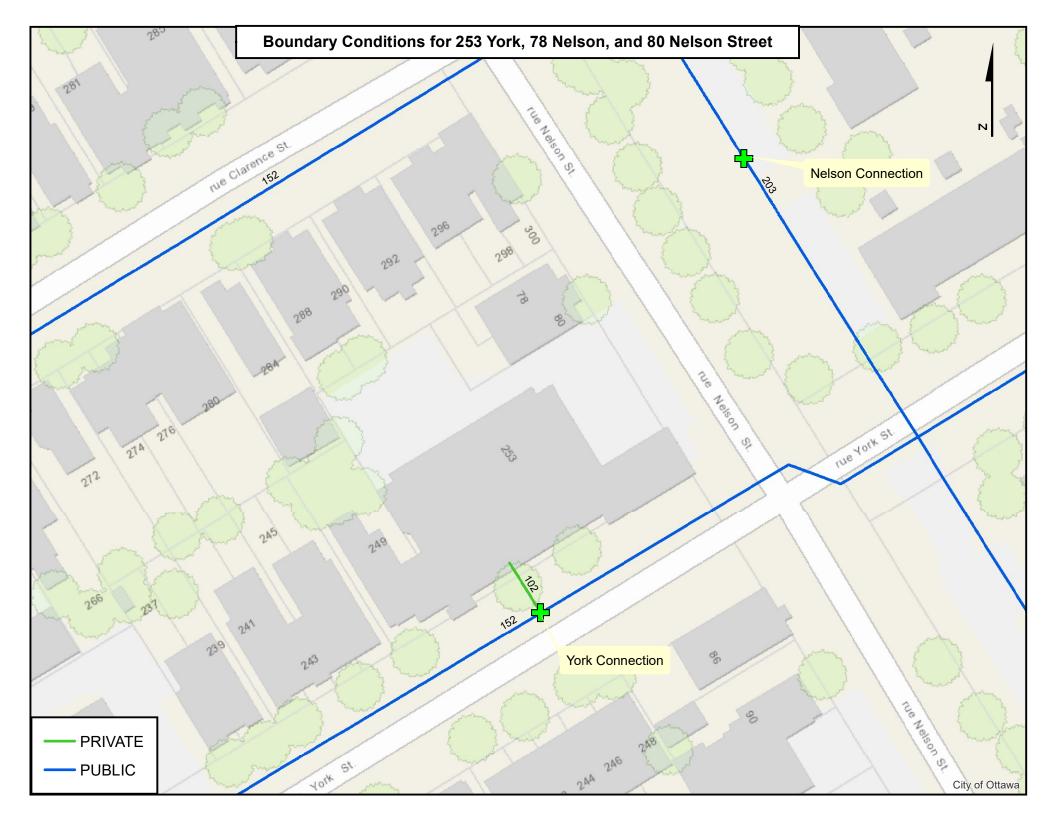
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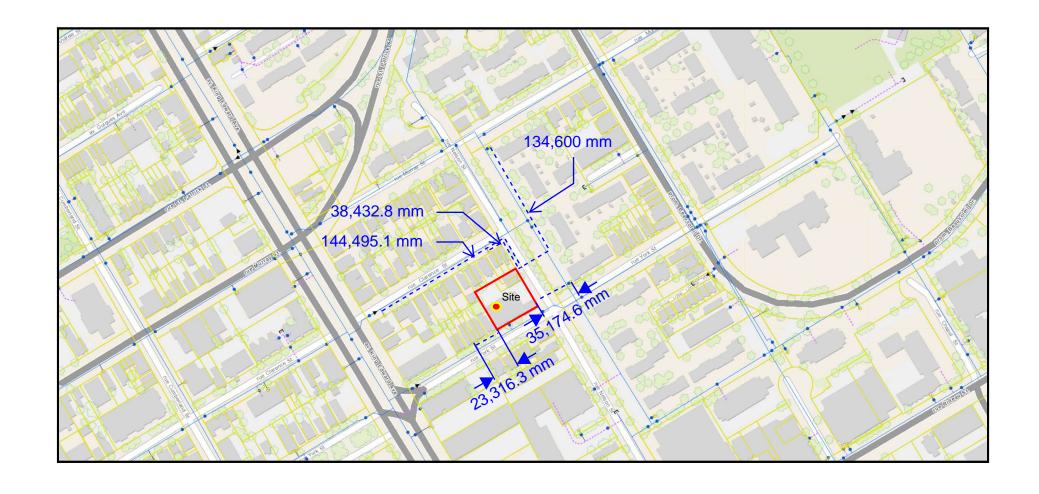
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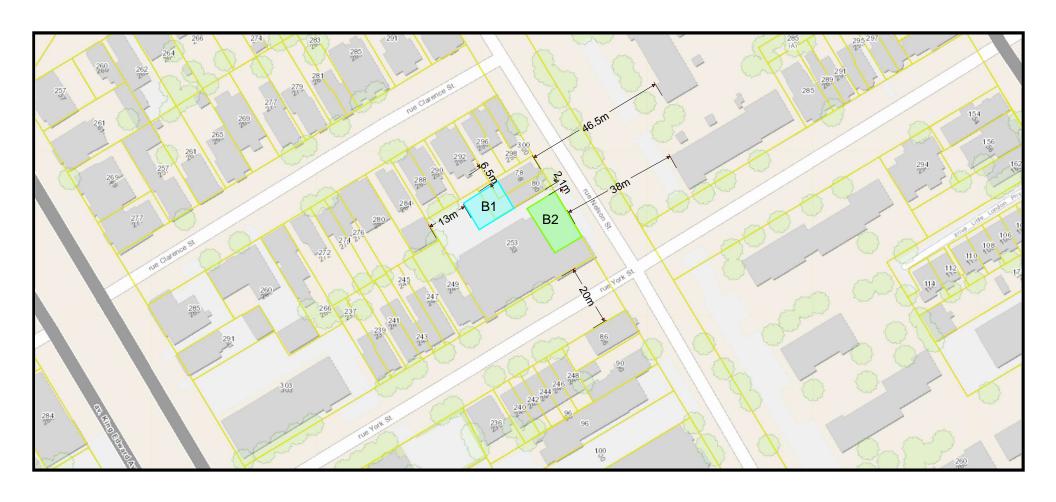
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https://maps.ottawa.ca/geoOttawa/

Exposure Distance Figure



APPENDIX D SANITARY CALCULATIONS

McINTOSH PERRY

CO-22-0938 - Ex. Building at 78 & 80 Nelson St - Sanitary Demands

Project: Ex. Building at 78 & 80 Nelson St

 Project No.:
 CO-22-0938

 Designed By:
 A.J.G.

 Checked By:
 R.D.F.

 Date:
 11/12/2021

Site Area 0.024 Gross ha

Bachelor 12 1.40 Persons per unit

Total Population 17 Persons

DESIGN PARAMETERS

Residential Peaking Factor 3.71 * $Using Harmon Formula = 1+(14/(4+P^0.5))*0.8$

where P = population in thousands, Harmon's Correction Factor = 0.8

Mannings coefficient (n) 0.013

Demand (per capita) 280 L/day Infiltration allowance 0.33 L/s/Ha

EXTRANEOUS FLOW ALLOWANCES

Infiltration / Inflow	Flow (L/s)
Dry	0.001
Wet	0.007
Total	0.008

AVERAGE DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS	POPULATION / AREA	Flow (L/s)
Residential	280	L/c/d	17	0.06
Industrial - Light**	35,000	L/gross ha/d		0
Industrial - Heavy**	55,000	L/gross ha/d		0
Commercial / Amenity	2,800	L/(1000m ² /d)		0
Hospital	900	L/(bed/day)		0
Schools	70	L/(Student/d)		0
Trailer Parks no Hook-Ups	340	L/(space/d)		0
Trailer Park with Hook-Ups	800	L/(space/d)		0
Campgrounds	225	L/(campsite/d)		0
Mobile Home Parks	1,000	L/(Space/d)		0
Motels	150	L/(bed-space/d)		0
Hotels	225	L/(bed-space/d)		0
Office	75	L/7.0m ² /d		0
Tourist Commercial	28,000	L/gross ha/d		0
Other Commercial	28,000	L/gross ha/d		0

AVERAGE RESIDENTIAL FLOW	0.06	L/s
PEAK RESIDENTIAL FLOW	0.20	L/s

TOTAL SANITARY DEMAND

TOTAL ESTIMATED AVERAGE DRY WEATHER FLOW	0.06	L/s
TOTAL ESTIMATED PEAK DRY WEATHER FLOW	0.21	L/s
TOTAL ESTIMATED PEAK WET WEATHER FLOW	0.21	L/s

CO-22-0938 - 78 & 80 Nelson Addition - Sanitary Demands

Project: 78 & 80 Nelson Addition

 Project No.:
 CO-22-0938

 Designed By:
 A.J.G.

 Checked By:
 R.D.F.

 Date:
 11/12/2021

Site Area 0.064 Gross ha

Bachelor 26 1.40 Persons per unit

Total Population 37 Persons

DESIGN PARAMETERS

Residential Peaking Factor 3.67 * Using Harmon Formula = 1+(14/(4+P^0.5))*0.8

where P = population in thousands, Harmon's Correction Factor = 0.8

Mannings coefficient (n) 0.013

Demand (per capita) 280 L/day Infiltration allowance 0.33 L/s/Ha

EXTRANEOUS FLOW ALLOWANCES

Infiltration / Inflow	Flow (L/s)
Dry	0.00
Wet	0.02
Total	0.02

AVERAGE DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS	POPULATION / AREA	Flow (L/s)
Residential	280	L/c/d	37	0.12
Industrial - Light**	35,000	L/gross ha/d		0
Industrial - Heavy**	55,000	L/gross ha/d		0
Commercial / Amenity	2,800	L/(1000m ² /d)		0
Hospital	900	L/(bed/day)		0
Schools	70	L/(Student/d)		0
Trailer Parks no Hook-Ups	340	L/(space/d)		0
Trailer Park with Hook-Ups	800	L/(space/d)		0
Campgrounds	225	L/(campsite/d)		0
Mobile Home Parks	1,000	L/(Space/d)		0
Motels	150	L/(bed-space/d)		0
Hotels	225	L/(bed-space/d)		0
Office	75	L/7.0m ² /d		0
Tourist Commercial	28,000	L/gross ha/d		0
Other Commercial	28,000	L/gross ha/d		0

AVERAGE RESIDENTIAL FLOW	0.12	L/s
PEAK RESIDENTIAL FLOW	0.44	L/s

TOTAL SANITARY DEMAND

TOTAL ESTIMATED AVERAGE DRY WEATHER FLOW	0.12	L/s
TOTAL ESTIMATED PEAK DRY WEATHER FLOW	0.44	L/s
TOTAL ESTIMATED PEAK WET WEATHER FLOW	0.46	L/s

CO-22-0938 - 253 York St Addition - Sanitary Demands

Project: 253 York St Addition Project No.: CO-22-0938 Designed By: A.J.G. Checked By: R.D.F. 11/12/2021 Date: Site Area 0.089 Gross ha Bachelor 17 1.40 Persons per unit 3 1 Bedroom 1.40 Persons per unit **Total Population** 29 Persons

DESIGN PARAMETERS

Residential Peaking Factor 3.69 * Using Harmon Formula = $1+(14/(4+P^0.5))*0.8$

where P = population in thousands, Harmon's Correction Factor = 0.8

Mannings coefficient (n) 0.013

Demand (per capita) 280 L/day Infiltration allowance 0.33 L/s/Ha

EXTRANEOUS FLOW ALLOWANCES

Infiltration / Inflow	Flow (L/s)
Dry	0.00
Wet	0.03
Total	0.03

AVERAGE DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS	POPULATION / AREA	Flow (L/s)
Residential	280	L/c/d	29	0.09
Industrial - Light**	35,000	L/gross ha/d		0
Industrial - Heavy**	55,000	L/gross ha/d		0
Commercial / Amenity	2,800	L/(1000m ² /d)		0
Hospital	900	L/(bed/day)		0
Schools	70	L/(Student/d)		0
Trailer Parks no Hook-Ups	340	L/(space/d)		0
Trailer Park with Hook-Ups	800	L/(space/d)		0
Campgrounds	225	L/(campsite/d)		0
Mobile Home Parks	1,000	L/(Space/d)		0
Motels	150	L/(bed-space/d)		0
Hotels	225	L/(bed-space/d)		0
Office	75	L/7.0m ² /d		0
Tourist Commercial	28,000	L/gross ha/d		0
Other Commercial	28,000	L/gross ha/d		0

AVERAGE RESIDENTIAL FLOW	0.09	L/s
PEAK RESIDENTIAL FLOW	0.35	L/s

TOTAL SANITARY DEMAND

TOTAL ESTIMATED AVERAGE DRY WEATHER FLOW	0.10	L/s
TOTAL ESTIMATED PEAK DRY WEATHER FLOW	0.35	L/s
TOTAL ESTIMATED PEAK WET WEATHER FLOW	0.38	L/s

SANITARY SEWER DESIGN SHEET

PROJECT:

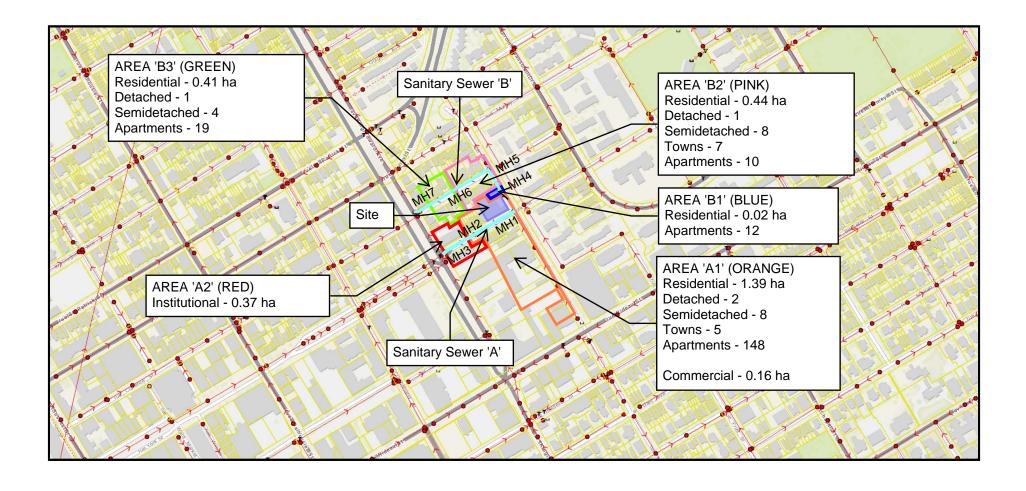
253 York, 80 Nelson, 78 Nelson

LOCATION:

CLIENT: Smart Living Properties

McINTOSH PERRY

	LOCATION			RESIDENTIAL								ICI AREAS								INFILTRATION ALLOWANCE FLOW					SEWER DATA							
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31		
					UNIT	TYPES		AREA	POPU	LATION		PEAK			ARE	A (ha)			PEAK	AREA	A (ha)	FLOW	DESIGN	CAPACITY	LENGTH	DIA	SLOPE	VELOCITY	AVAI	ILABLE		
STREET	AREA ID	FROM	то	SF	SD	ТН	APT	(ha)	IND	сим	PEAK	FLOW	INSTIT	JTIONAL	COMM	IERCIAL	INDU	STRIAL	FLOW	IND	сим	(L/s)	FLOW	(L/s)	(m)	(mm)	(%)	(full)	CAP	PACITY		
		MH	MH	ЭГ	30	In	AFI	(IIa)	IND	COIVI	FACTOR	(L/s)	IND	CUM	IND	CUM	IND	CUM	(L/s)	IND	COIVI	(L/5)	(L/s)	(L/S)	(111)	(111111)	(70)	(m/s)	L/s	(%)		
Nelson Avenue	A-1	MH1	MH2	2	8	5	148	1.39	382.3	382.3	3.43	4.24		0.00	0.16	0.16		0.00	0.08	1.55	1.55	0.51	4.84	500.29	78.00	600	0.61	1.714	495.46	99.03		
York Street	A-2	MH2	MH3					0.00	0.0	382.3	3.43	4.24	0.37	0.37		0.16		0.00	0.26	0.37	1.93	0.64	5.14	597.47	60.00	600	0.87	2.047	592.33	99.14		
Nelson Avenue	B-1	MH4	MH5				12	0.02	27.6	27.6	3.69	0.33		0.00		0.00		0.00	0.00	0.02	0.02	0.01	0.34	113.24	50.00	300	1.26	1.552	112.90	99.70		
Clarence Street	B-2	MH5	MH6	1	8	7	10	0.44	66.9	94.5	3.60	1.10		0.00		0.00		0.00	0.00	0.44	0.47	0.15	1.26	78.79	66.00	300	0.61	1.080	77.53	98.40		
Clarence Street	B-3	MH6	MH7	1	4		19	0.41	57.9	152.4	3.55	1.75		0.00		0.00		0.00	0.00	0.41	0.88	0.29	2.04	30.26	70.00	300	0.09	0.415	28.22	93.24		
Design Parameters:				Notes:							Designed:		AJG			No.					Revision							Date				
					gs coefficien			0.013								1.				City of (Ottawa Subr	nission 1						2021-08-23				
Residential		ICI Areas		2. Demand	d (per capita)):	280) L/day																								
SF 3.4 p/p/u			Peak Factor	Infiltrat	ion allowanc	e:	0.33	B L/s/Ha			Checked:		RDF																			
TH/SD 2.7 p/p/u		00 L/Ha/day	1.5	4. Residen	tial Peaking																											
APT 2.3 p/p/u	COM 28,00	00 L/Ha/day	1.5		Harmon Fo	rmula = 1+(:	14/(4+P^0.5	5)*0.8)																								
Other 60 p/p/Ha	IND 35,00	00 L/Ha/day	MOE Chart		where P = p	oopulation i	n thousands	5			Project No.	:	C0-22-0938	3																		
											I																	Sheet No:				
																												1 of 1				



https://maps.ottawa.ca/geoOttawa/



2 SANITARY SEWER DESIGN

The sanitary service laterals from the proposed development will be connected to the existing 600 mm diameter sanitary sewer along York Street.

Sewage discharges will be domestic in type and in compliance with the City of Ottawa Sewer Use By-law. The anticipated peak sanitary flow will be a total of approximately $1.05\ L/s$.

The sanitary sewage flow for the building was calculated based on the City of Ottawa Sewer Design Guidelines (Section 4.4.1.2).

2.1 Design Flows

The existing building is for residential use with domestic flows. The design flows are calculated based on the population density shown in the Ottawa Water Distribution Guidelines Section 4.2.8.

The peak sanitary design flows are calculated using the Ottawa Sewer Guidelines – Technical Bulletin ISTB-2018-01.

Residential

Total domestic pop:

(14) x 1.4 ppu:	19.6
(14) x 2.1 ppu:	29.4
(1) x 3.1 ppu	3.1
(8) x 4.2 ppu	<i>33.6</i>
·	85.7
	(14) x 2.1 ppu: (1) x 3.1 ppu

 $Q_{Domestic} = 86x 280 L/person/day x (1/86,400 sec/day)$

0.28 L/sec

Peaking Factor =
$$1 + \left(\frac{14}{4 + \left(\frac{P}{1000}\right)}\right) * 0.8$$
 = 3.61 (4 maximum)

$$Q_{Peak Domestic} = 0.28 L/sec \times 3.61 = 1.01 L/sec$$

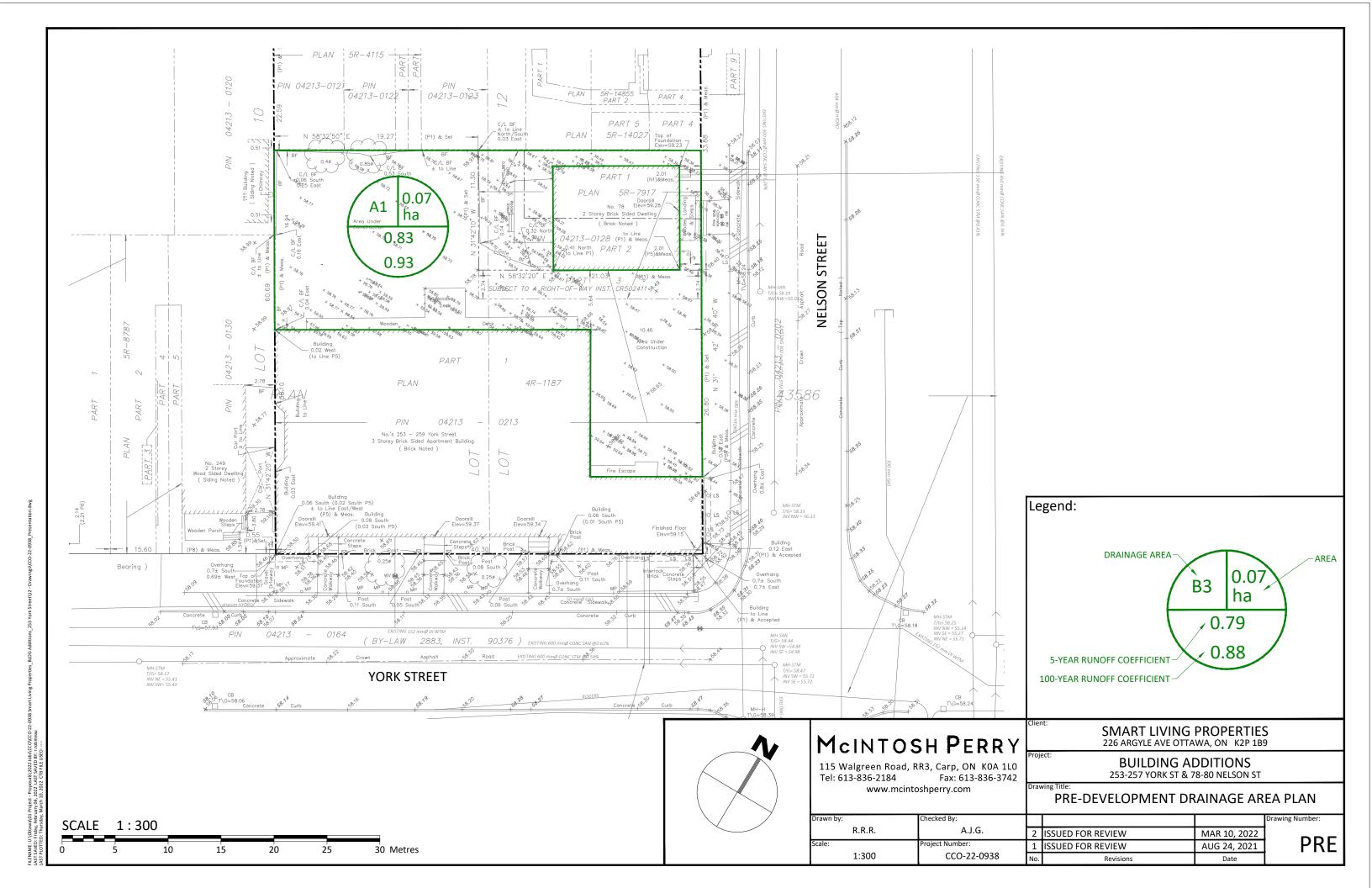
<u>Infiltration</u>

Q $_{Infiltration}$ = 0.33 L/ha/sec x 0.13ha = 0.04L/sec

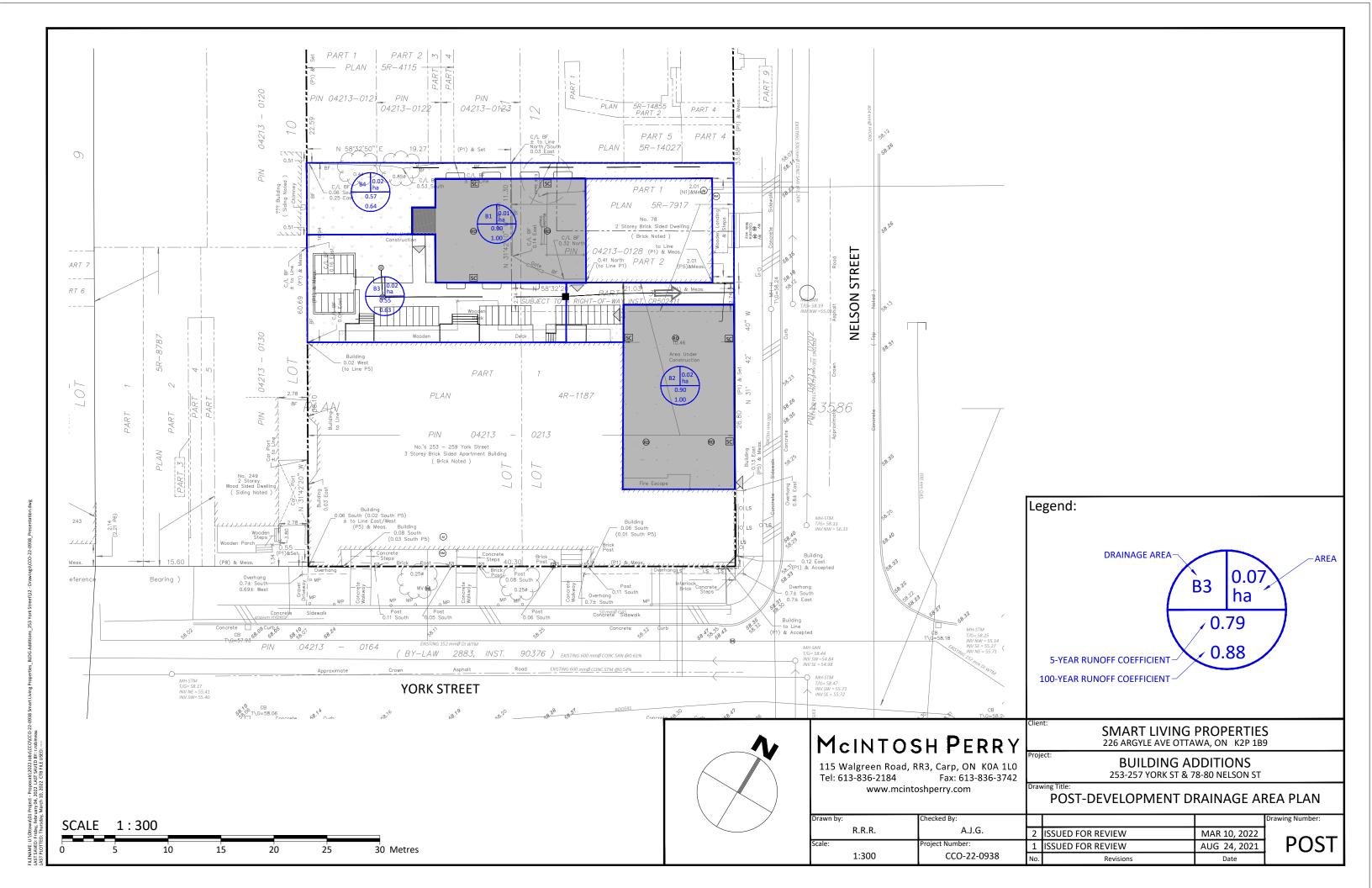
Total Peak Sanitary Flow = 1.01 + 0.04 = 1.05 L/sec



APPENDIX E PRE-DEVELOPMENT DRAINAGE PLAN



APPENDIX F POST-DEVELOPMENT DRAINAGE PLAN



APPENDIX G STORMWATER MANAGEMENT CALCULATIONS

CCO-22-0938 - 253 York Street - Runoff Calculations

1 of 6

Pre-Development Runoff Coefficient

Drainage Area	Area (ha)	Impervious Area (m²)	О	Gravel Area (m²)	O	Pervious Area (m²)	O	C _{AVG} 5-Year	C _{AVG} 100-Year
A1	0.071	642.73	0.90	0.00	0.60	69.00	0.20	0.83	0.93

Pre-Development Runoff Calculations

Drainage Area	Area (ha)	C 5-Year	C 100-Year	Tc (min)	l (mm/hr)			Q / s)
Alea	(IIa)	o- real	100- teal	(111111)	5-Year	100-Year	5-Year	100-Year
A1	0.071	0.83	0.93	10	104.2	178.6	17.16	32.76
Total	0.071		•				17.16	32.76

Post-Development Runoff Coefficient

Drainage Area	Area (ha)	Impervious Area (m²)	С	Gravel Area (m²)	С	Pervious Area (m²)	С	C _{AVG} 5-Year	C _{AVG} 100-Year
B1	0.014	144.80	0.90	0.00	0.60	0.00	0.20	0.90	1.00
B2	0.020	204.40	0.90	0.00	0.60	0.00	0.20	0.90	1.00
B3	0.017	86.58	0.90	0.00	0.60	85.21	0.20	0.55	0.63
B4	0.019	99.60	0.90	0.00	0.60	91.15	0.20	0.57	0.64

Restricted 3 Storey Roof Restricted 4 Storey Roof Unrestricted Area Unrestricted Area

Post-Development Runoff Calculations

Drainage Area	Area (ha)	C 5-Year	C 100-Year	Tc (min)	(mm	l n/hr)		Q / s)
Alea			100-16ai	(111111)	5-Year	100-Year	5-Year	100-Year
B1	0.014	0.90	1.00	10	104.2	178.6	3.77	7.19
B2	0.020	0.90	1.00	10	104.2	178.6	5.33	10.15
B3	0.017	0.55	0.63	10	104.2	178.6	2.75	5.36
B4	0.019	0.57	0.64	10	104.2	178.6	3.12	6.08
Total	0.071						14.98	28.76

Restricted 3 Storey Roof Restricted 4 Storey Roof Unrestricted Area Unrestricted Area

Required Restricted How Per Pre Consultation

Drainage Area	Area (ha)	C 5-Year	Tc (min)	l (mm/hr) 5-Year	Q (L/ s) 5-Year
A1	0.071	0.50	10	104.2	10.31

Post-Development Restricted Runoff Calculations

Drainage Area		cted Flow /s)		ted Flow /s)	_	Required n ³)		Provided n ³)	
Alea	5-Year	100-Year	5-Year	100-Year	5-Year	100-Year	5-Year	100-Year	
B1	3.77	7.19	0.64	1.14	2.36	4.60	2.72	4.89	Restricted
B2	5.33	10.15	1.14	1.89	3.89	7.51	4.60	7.66	Restricted
B3	2.75	5.36	2.75	5.36					Unrestricted
B4	3.12	6.08	3.12	6.08					Unrestricted
Total	11.85	22.69	7.66	14.46	6.25	12.12	7.31	12.55	

CCO-22-0938 - 253 York Street - Runoff Calculations

2 of 6

Storage Requirements for Area B1

5-Year Storm Event

Tc (min)	l (mm/hr)	B1 Runoff (L/s)	Allowable Outflow (L/s)	Runoff to be Stored (L/s)	Storage Required (m³)
10	104.2	3.77	0.64	3.13	1.88
20	70.3	2.55	0.64	1.91	2.29
30	53.9	1.95	0.64	1.31	2.36
40	44.2	1.60	0.64	0.96	2.31
50	37.7	1.36	0.64	0.72	2.17
60	32.9	1.19	0.64	0.55	1.99
70	29.4	1.06	0.64	0.42	1.78
80	26.6	0.96	0.64	0.32	1.55
90	24.3	0.88	0.64	0.24	1.30
100	22.4	0.81	0.64	0.17	1.03

Maximum Storage Required 5-Year (m³) = 2.36

100-Year Storm Event

Tc (min)	l (mm/hr)	B1 Runoff (L/s)	Allowable Outflow (L/s)	Runoff to be Stored (L/s)	Storage Required (m³)
10	178.6	7.19	1.14	6.05	3.63
20	120.0	4.83	1.14	3.69	4.43
30	91.9	3.70	1.14	2.56	4.60
40	75.1	3.02	1.14	1.88	4.52
50	64.0	2.57	1.14	1.43	4.30
60	55.9	2.25	1.14	1.11	4.00
70	49.8	2.00	1.14	0.86	3.63
80	45.0	1.81	1.14	0.67	3.22

Maximum Storage Required 100-Year (m³) = 4.60

Storage Occupied In Area B1

5-Year Storm Event

Roof Storage								
Location	Depth	Volume (m³)						
Roof	108.60	0.025	2.72					
		Total	2.72					

100-Year Storm Event

100-lear donn Event							
Roof Storage							
Location	Area*	Depth	Volume (m³)				
Roof	108.60	0.045	4.89				
		Total	4.89				

^{*}Storage area is 75% of the total roof area

Storage Available (m³) =	2.72
Storage Required (m³) =	2.36

Storage Available (m³) =	4.89
Storage Required (m ³) =	4.60

CCO-22-0938 - 253 York Street - Runoff Calculations

Nelson Street Building Roof Drain How (B1) 3 of 6

Roof Drains Summary				
Type of Control Device	Watts Drianage - Accutrol Weir			
Number of Roof Drains	2			
	5-Year 100-Year			
Rooftop Storage (m ³)	2.72	4.89		
Storage Depth (m)	0.025 0.045			
How (Per Roof Drain) (L/s)	0.32	0.57		
Total How (L/s)	0.64	1.14		

Row Rate Vs. Build-Up (One Weir)		
Depth (mm)	How (L/s)	
15	0.19	
20	0.25	
25	0.32	
30	0.38	
35 0.44		
40	0.50	
45	0.57	
50 0.63		
55 0.69		

^{*} Roof Drain model to be Accutrol Weirs, See attached sheets

CALCULATING ROOF FLOW EXAMPLES

2 roof drains during a 5 year storm elevation of water = 30mm How leaving 2 roof drains = $(2 \times 0.36 \text{ L/s}) = 0.72 \text{ L/s}$

2 roof drains during a 100 year storm elevation of water = 45mm How leaving 2 roof drains = $(2 \times 0.54 \text{ L/s}) = 1.08 \text{ L/s}$

		Roof Drain Flo	W
	How (I/s)	Storage Depth (mm)	Drains Flow (I/s)
	0.19	15	0.38
	0.25	20	0.50
5-Year	0.32	25	0.64
	0.38	30	0.76
	0.44	35	0.88
L	0.50	40	1.00
100-Year	0.57	45	1.14
	0.63	50	1.26
L	0.69	55	1.38
L	0.76	60	1.52
	0.82	65	1.64
	0.88	70	1.76
	0.95	75	1.90
	1.01	80	2.02
	1.07	85	2.14
L	1.13	90	2.26
L	1.20	95	2.40
L	1.26	100	2.52
L	1.32	105	2.64
	1.39	110	2.78
	1.45	115	2.90
	1.51	120	3.02
	1.58	125	3.16
	1.64	130	3.28
	1.70	135	3.40
	1.76	140	3.52
	1.83	145	3.66
	1.89	150	3.78

 $\underline{\text{Note:}}$ The flow leaving through a restricted roof drain is based on flow vs. head information

^{*} Roof Drain Flow information taken from Watts Drainage website

CCO-22-0938 - 253 York Street - Runoff Calculations

4 of 6

Storage Requirements for Area B2

5-Year Storm Event

Tc (min)	l (mm/hr)	B1 Runoff (L/s)	Allowable Outflow (L/s)	Runoff to be Stored (L/s)	Storage Required (m³)
10	104.2	5.33	0.64	4.69	2.81
20	70.3	3.59	0.64	2.95	3.54
30	53.9	2.76	0.64	2.12	3.81
40	44.2	2.26	0.64	1.62	3.89
50	37.7	1.93	0.64	1.29	3.86
60	32.9	1.68	0.64	1.04	3.76
70	29.4	1.50	0.64	0.86	3.62
80	26.6	1.36	0.64	0.72	3.45
90	24.3	1.24	0.64	0.60	3.25
100	22.4	1.15	0.64	0.51	3.04

Maximum Storage Required 5-Year (m³) = 3.89

100-Year Storm Event

Tc (min)	l (mm/hr)	B1 Runoff (L/s)	Allowable Outflow (L/s)	Runoff to be Stored (L/s)	Storage Required (m³)
10	178.6	10.15	1.14	9.01	5.40
20	120.0	6.82	1.14	5.68	6.81
30	91.9	5.22	1.14	4.08	7.34
40	75.1	4.27	1.14	3.13	7.51
50	64.0	3.63	1.14	2.49	7.48
60	55.9	3.18	1.14	2.04	7.33
70	49.8	2.83	1.14	1.69	7.09
80	45.0	2.56	1.14	1.42	6.80

Maximum Storage Required 100-Year (m³) = 7.51

Storage Occupied In Area B2

5-Year Storm Event

Poof Storage				
Location Area* Depth			Volume (m³)	
Roof	153.30	0.030	4.60	
		Total	4.60	

100-Year Storm Event

100- Teal Storm Event				
Poof Storage				
Location	Area*	Depth	Volume (m³)	
Roof	153.30	0.050	7.66	
		Total	7.66	

^{*}Storage area is 75% of the total roof area

Storage Available (m³) =	4.60
Storage Required (m³) =	3.89

Storage Available (m³) =	7.66
Storage Required (m ³) =	7.51

CCO-22-0938 - 253 York Street - Runoff Calculations

York Street Building Roof Drain Flow (B2) 5 of 6

Roof Drains Summary			
Type of Control Device	Watts Drianage - Accutrol Weir		
Number of Roof Drains	3		
	5-Year	100-Year	
Rooftop Storage (m ³)	4.60	7.66	
Storage Depth (m)	0.030	0.050	
How (Per Roof Drain) (L/s)	0.38	0.63	
Total How (L/s)	1.14	1.89	

Row Rate Vs. Build-Up (One Weir)				
Depth (mm)	How (L/s)			
15	0.19			
20	0.25			
25	0.32			
30	0.38			
35	0.44			
40	0.50			
45	0.57			
50	0.63			
55	0.69			

^{*} Roof Drain model to be Accutrol Weirs, See attached sheets

CALCULATING ROOF FLOW EXAMPLES

3 roof drains during a 5 year storm elevation of water = 25mm How leaving 3 roof drains = $(3 \times 0.32 \text{ L/s}) = 0.96 \text{L/s}$

3 roof drains during a 100 year storm elevation of water = 50mm How leaving 3 roof drains = $(3 \times 0.54 \text{ L/s}) = 1.89 \text{L/s}$

		Roof Drain Flo	W
	How (I/s)	Storage Depth (mm)	Drains How (I/s)
	0.19	15	0.57
	0.25	20	0.75
	0.32	25	0.96
5-Year	0.38	30	1.14
	0.44	35	1.32
	0.50	40	1.50
	0.57	45	1.71
100-Year	0.63	50	1.89
	0.69	55	2.07
	0.76	60	2.28
	0.82	65	2.46
	0.88	70	2.64
	0.95	75	2.85
	1.01	80	3.03
	1.07	85	3.21
	1.13	90	3.39
	1.20	95	3.60
	1.26	100	3.78
	1.32	105	3.96
	1.39	110	4.17
	1.45	115	4.35
	1.51	120	4.53
	1.58	125	4.74
ľ	1.64	130	4.92
ľ	1.70	135	5.10
ľ	1.76	140	5.28
ľ	1.83	145	5.49
	1.89	150	5.67

 $\underline{\text{Note:}}$ The flow leaving through a restricted roof drain is based on flow vs. head information

^{*} Roof Drain Flow information taken from Watts Drainage website

CCO-22-0938 - 253 York Street - Runoff Calculations

6 of 6

Time of Concentration Pre-Development

Drainage Area	Sheet Flow	Sope of	Tc (min)	Tc (min)
ID	Distance (m)	Land (%)	(5-Year)	(100-Year)
A1	39	0.76	6	4

* Therefore, a Tc of 10 can be used

 $Tc = (3.26(1.1-c)L^0.5/S^0.33)$

c= Balanced Runoff Coefficient
 L= Length of Drainage Area
 S= Average Sope of Watershed

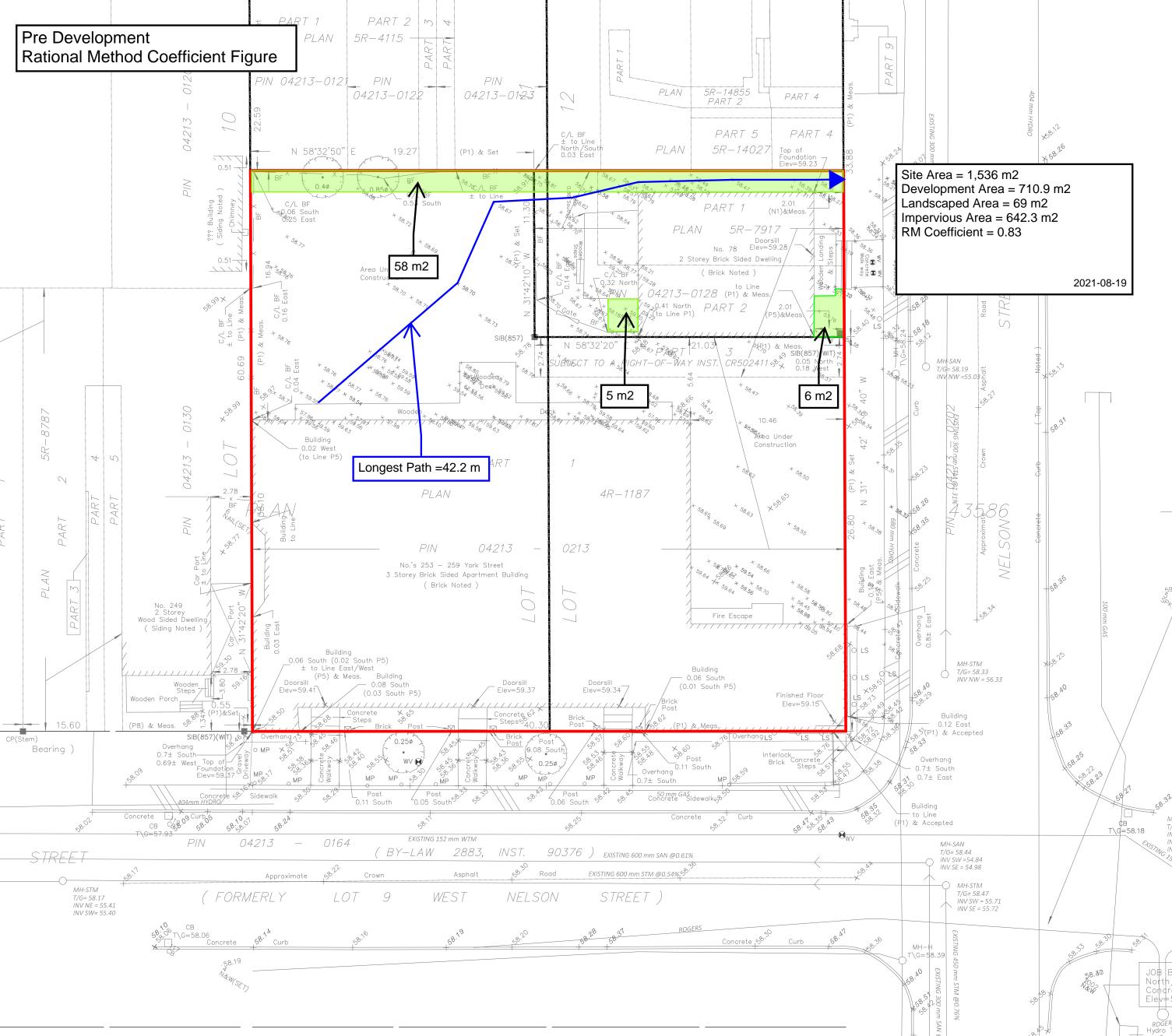
STORM SEWER DESIGN SHEET

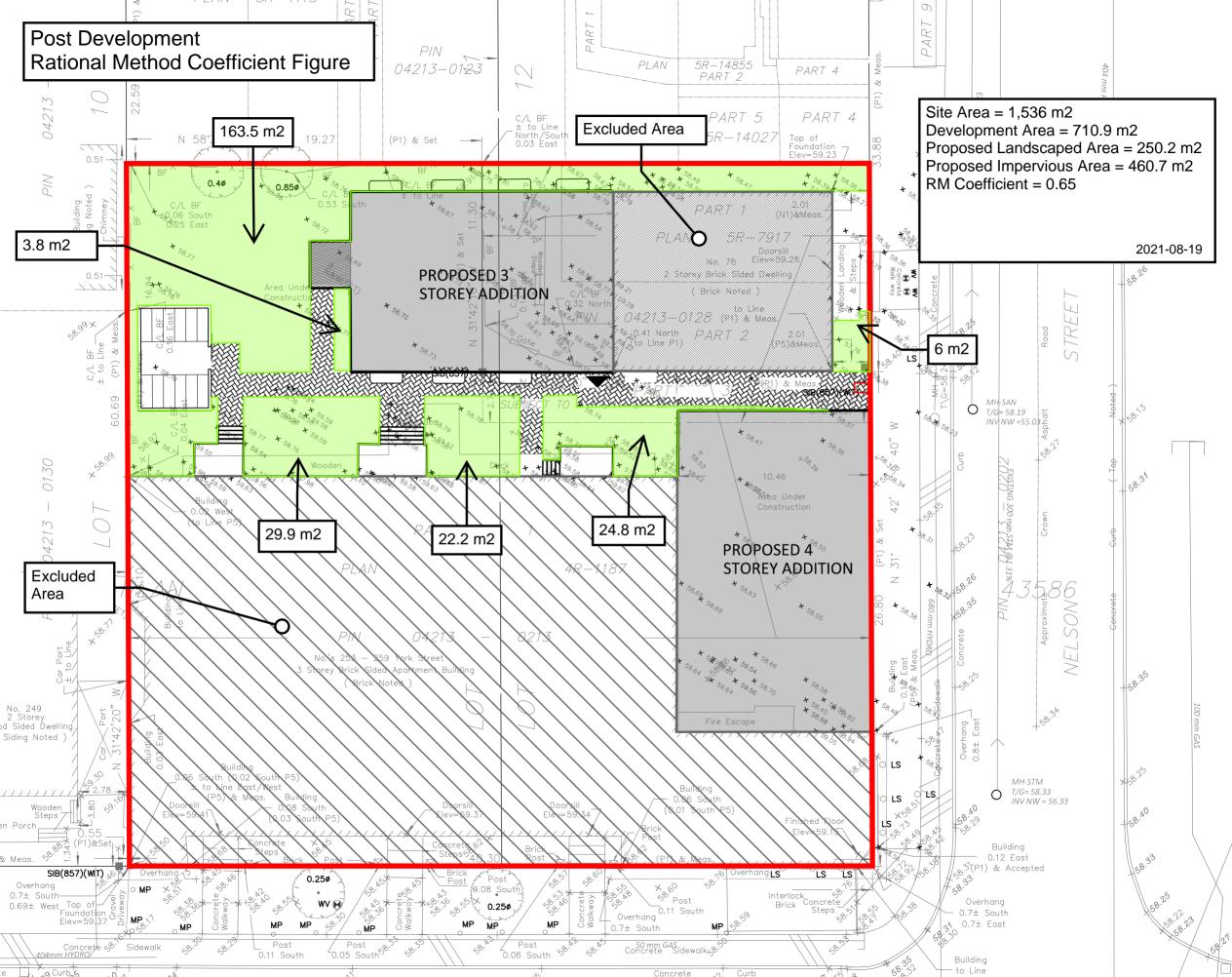
PROJECT: Building Additions

LOCATION: 253 York Street

CLIENT: Smart Living Properties

	LOCATION				CONTRIBUTING AREA (ha)							RATIO	ONAL DESIGN	FLOW				1					SEWER DATA				
1	2	3	4	5	6	7	8		10		12	13	14	15			18	19				23	24	25	26	27	28
STREET	AREA ID	FROM	TO	C-VALUE	AREA	INDIV	CUMUL	INLET	TIME	TOTAL	i (5)	i (10)	i (100)	5yr PEAK	10yr PEAK		FIXED		CAPACITY	LENGTH		PIPE SIZE (mm		SLOPE	VELOCITY	AVAILO	
		МН	MH			AC	AC	(min)	IN PIPE	(min)	(mm/hr)	(mm/hr)	(mm/ hr)	HLOW (L/s)	HLOW (L/s)	FLOW (L/s) R	LOW (L/s)	FLOW (L/s)	(L/s)	(m)	DIA	W	Н	(%)	(m/s)	(L/s)	(%)
	B3	CB4	TEE	0.55	0.02	0.01	0.01	10.00	0.02	10.02	104.19	122.14	178.56	2.71				2.71	62.04	1.30	250			1.00	1.224	59.33	95.63%
Nelson Street	B1	BLDG	TEE	0.90	0.01	0.01	0.01	10.00	0.02	10.02	104.19	122.14	178.56	2.61				2.61	62.04	1.23	250			1.00	1.224	59.43	95.80%
		TEE	MH1			0.00	0.02	10.02	0.29	10.31	104.10	122.04	178.41	5.31				5.31	62.04	21.23	250			1.00	1.224	56.73	91.44%
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efinitions:				Notes:		•	•	Designed:		•			No.					Revision							Date		
Q = 2.78QA, where:				1. Mannings coefficient (n	1) =		0.013		RRR				1.				ISS	UED FOR REVIE	W						2022-03-10		
= Peak Flow in Litres p								<u> </u>																			
A = Area in Hectares (ha)		n/hr\						Checked:	A 10																		
= Hainfall intensity in m [i = 998.071 / (TC+6.05	nillimeters per hour (mn 53)^0 8141	n/hr) 5 YEAR							AJG					-													
[i = 1174.184 / (TC+6.0		10 YEAR						Project No.:					 														
		100 YEAR							000-22-0938								Da	te:							Sheet No:		
[i = 1735.688 / (TC+6.0)]	014)^0.820	TOU TEAN																							areet No.		





APPENDIX H CITY OF OTTAWA DESIGN CHECKLIST

City of Ottawa

4. Development Servicing Study Checklist

The following section describes the checklist of the required content of servicing studies. It is expected that the proponent will address each one of the following items for the study to be deemed complete and ready for review by City of Ottawa Infrastructure Approvals staff.

The level of required detail in the Servicing Study will increase depending on the type of application. For example, for Official Plan amendments and re-zoning applications, the main issues will be to determine the capacity requirements for the proposed change in land use and confirm this against the existing capacity constraint, and to define the solutions, phasing of works and the financing of works to address the capacity constraint. For subdivisions and site plans, the above will be required with additional detailed information supporting the servicing within the development boundary.

4.1 General Content

Criteria	Location (if applicable)
Executive Summary (for larger reports only).	N/A
Date and revision number of the report.	On Cover
Location map and plan showing municipal address, boundary, and layout of proposed development.	Appendix A
☐ Plan showing the site and location of all existing services.	Site Servicing Plan (C101)
 Development statistics, land use, density, adherence to zoning and official plan, and reference to applicable subwatershed and watershed plans that provide context to which individual developments must adhere. 	1.1 Purpose 1.2 Site Description
developments must adhere.	6.0 Stormwater Management
☐ Summary of pre-consultation meetings with City and other approval agencies.	Appendix B
Reference and confirm conformance to higher level studies and reports (Master Servicing Studies, Environmental Assessments, Community Design Plans), or in the case where it is not in	1.1 Purpose 1.2 Site Description
conformance, the proponent must provide justification and develop a defendable design criteria.	6.0 Stormwater Management
\square Statement of objectives and servicing criteria.	3.0 Pre-Consultation Summary



$\hfill \square$ Identification of existing and proposed infrastructure available in the immediate area.	N/A
☐ Identification of Environmentally Significant Areas, watercourses and Municipal Drains potentially impacted by the proposed development (Reference can be made to the Natural Heritage Studies, if available).	Site Grading, Drainage, Sediment & Erosion Control Plan (C101)
☐ Concept level master grading plan to confirm existing and proposed grades in the development. This is required to confirm the feasibility of proposed stormwater management and drainage, soil removal and fill constraints, and potential impacts to neighbouring properties. This is also required to confirm that the proposed grading will not impede existing major system flow paths.	Site Grading, Drainage, Sediment & Erosion Control Plan (C101)
☐ Identification of potential impacts of proposed piped services on private services (such as wells and septic fields on adjacent lands) and mitigation required to address potential impacts.	N/A
☐ Proposed phasing of the development, if applicable.	N/A
☐ Reference to geotechnical studies and recommendations concerning servicing.	Section 2.0 Background Studies, Standards and References
 All preliminary and formal site plan submissions should have the following information: Metric scale North arrow (including construction North) Key plan Name and contact information of applicant and property owner Property limits including bearings and dimensions Existing and proposed structures and parking areas Easements, road widening and rights-of-way Adjacent street names 	Site Grading, Drainage, Sediment & Erosion Control Plan (C101)

4.2 Development Servicing Report: Water

Criteria	Location (if applicable)
☐ Confirm consistency with Master Servicing Study, if available	N/A
Availability of public infrastructure to service proposed development	N/A
☐ Identification of system constraints	N/A
☐ Identify boundary conditions	Unavailable at time of submission
☐ Confirmation of adequate domestic supply and pressure	N/A
 Confirmation of adequate fire flow protection and confirmation that fire flow is calculated as per the Fire Underwriter's Survey. Output should show available fire flow at locations throughout the development. 	Appendix C
 Provide a check of high pressures. If pressure is found to be high, an assessment is required to confirm the application of pressure reducing valves. 	N/A
 Definition of phasing constraints. Hydraulic modeling is required to confirm servicing for all defined phases of the project including the ultimate design 	N/A
☐ Address reliability requirements such as appropriate location of shut-off valves	N/A
☐ Check on the necessity of a pressure zone boundary modification.	N/A
Reference to water supply analysis to show that major infrastructure is capable of delivering sufficient water for the proposed land use. This includes data that shows that the expected demands under average day, peak hour and fire flow conditions provide water within the required pressure range	Appendix C

 Description of the proposed water distribution network, including locations of proposed connections to the existing system, provisions for necessary looping, and appurtenances (valves, pressure reducing valves, valve chambers, and fire hydrants) including special metering provisions. 	Site Servicing Plan (C101)
 Description of off-site required feedermains, booster pumping stations, and other water infrastructure that will be ultimately required to service proposed development, including financing, interim facilities, and timing of implementation. 	N/A
☐ Confirmation that water demands are calculated based on the City of Ottawa Design Guidelines.	Appendix C
 Provision of a model schematic showing the boundary conditions locations, streets, parcels, and building locations for reference. 	N/A

4.3 Development Servicing Report: Wastewater

Criteria	Location (if applicable)
☐ Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitored flow data from relatively new infrastructure cannot be used to justify capacity requirements for proposed infrastructure).	N/A
☐ Confirm consistency with Master Servicing Study and/or justifications for deviations.	N/A
☐ Consideration of local conditions that may contribute to extraneous flows that are higher than the recommended flows in the guidelines. This includes groundwater and soil conditions, and age and condition of sewers.	N/A
Description of existing sanitary sewer available for discharge of wastewater from proposed development.	Section 5.1

☐ Verify available capacity in downstream sanitary sewer and/or identification of upgrades necessary to service the proposed development. (Reference can be made to previously completed Master Servicing Study if applicable)	Section 5.2 Proposed Sanitary Design
☐ Calculations related to dry-weather and wet-weather flow rates from the development in standard MOE sanitary sewer design table (Appendix 'C') format.	Appendix C
 Description of proposed sewer network including sewers, pumping stations, and forcemains. 	Section 5.2 Proposed Sanitary Sewer
Discussion of previously identified environmental constraints and impact on servicing (environmental constraints are related to limitations imposed on the development in order to preserve the physical condition of watercourses, vegetation, soil cover, as well as protecting against water quantity and quality).	N/A
 Pumping stations: impacts of proposed development on existing pumping stations or requirements for new pumping station to service development. 	N/A
☐ Forcemain capacity in terms of operational redundancy, surge pressure and maximum flow velocity.	N/A
☐ Identification and implementation of the emergency overflow from sanitary pumping stations in relation to the hydraulic grade line to protect against basement flooding.	N/A
☐ Special considerations such as contamination, corrosive environment etc.	N/A

4.4 Development Servicing Report: Stormwater Checklist

Criteria	Location (if applicable)
 Description of drainage outlets and downstream constraints including legality of outlets (i.e. municipal drain, right-of-way, watercourse, or private property) 	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
Analysis of available capacity in existing public infrastructure.	N/A
 A drawing showing the subject lands, its surroundings, the receiving watercourse, existing drainage patterns, and proposed drainage pattern. 	Pre & Post-Development Plans
☐ Water quantity control objective (e.g. controlling post-development peak flows to pre-development level for storm events ranging from the 2 or 5-year event (dependent on the receiving sewer design) to 100-year return period); if other objectives are being applied, a rationale must be included with reference to hydrologic analyses of the potentially affected subwatersheds, taking into account long-term cumulative effects.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
☐ Water Quality control objective (basic, normal or enhanced level of protection based on the sensitivities of the receiving watercourse) and storage requirements.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
 Description of the stormwater management concept with facility locations and descriptions with references and supporting information. 	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
Set-back from private sewage disposal systems.	N/A
☐ Watercourse and hazard lands setbacks.	N/A
Record of pre-consultation with the Ontario Ministry of Environment and the Conservation Authority that has jurisdiction on the affected watershed.	N/A
Confirm consistency with sub-watershed and Master Servicing Study, if applicable study exists.	N/A
Storage requirements (complete with calculations) and conveyance capacity for minor events (1:5-year return period) and major events (1:100-year return period).	Appendix G

☐ Identification of watercourses within the proposed development and how watercourses will be protected, or, if necessary, altered by the proposed development with applicable approvals.	Site Grading, Drainage, Sediment & Erosion Control Plan
☐ Calculate pre-and post development peak flow rates including a description of existing site conditions and proposed impervious areas and drainage catchments in comparison to existing conditions.	Section 7.0 Proposed Stormwater Management Appendix G
☐ Any proposed diversion of drainage catchment areas from one outlet to another.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
 Proposed minor and major systems including locations and sizes of stormwater trunk sewers, and stormwater management facilities. 	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
☐ If quantity control is not proposed, demonstration that downstream system has adequate capacity for the post-development flows up to and including the 100-year return period storm event.	N/A
☐ Identification of potential impacts to receiving watercourses	N/A
Identification of municipal drains and related approval requirements.	N/A
Descriptions of how the conveyance and storage capacity will be achieved for the development.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
100-year flood levels and major flow routing to protect proposed development from flooding for establishing minimum building elevations (MBE) and overall grading.	Site Grading, Drainage, Sediment & Erosion Control Plan (C101)
☐ Inclusion of hydraulic analysis including hydraulic grade line elevations.	N/A

 Description of approach to erosion and sediment control during construction for the protection of receiving watercourse or drainage corridors. 	Section 8.0 Sediment & Erosion Control
Identification of floodplains – proponent to obtain relevant floodplain information from the appropriate Conservation Authority. The proponent may be required to delineate floodplain elevations to the satisfaction of the Conservation Authority if such information is not available or if information does not match current conditions.	N/A
☐ Identification of fill constraints related to floodplain and geotechnical investigation.	N/A

4.5 Conclusion Checklist

Criteria	Location (if applicable)
Clearly stated conclusions and recommendations	Section 9.0 Summary
	Section 10.0 Recommendations
☐ Comments received from review agencies including the City of Ottawa and information on how the comments were addressed. Final sign-off from the responsible reviewing agency.	All are stamped
All draft and final reports shall be signed and stamped by a professional Engineer registered in Ontario	All are stamped