



Stormwater Management and Servicing Report

Navan Stacked Town Homes
6001-6005 Renaud Road
Orleans, Ontario

Prepared for:

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Attention: Eric Danis

LRL File No.: 210216-02

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1 INTRODUCTION AND SITE DESCRIPTION

LRL Associates Ltd. was retained by Landric Homes Inc. to complete a Stormwater Management Analysis and Servicing Brief for a proposed development of stacked townhomes located at 6001-6005 Renaud Rd, Orleans, Ottawa. The legal description of the property is Part of Lot 7, Concession 3, geographic Township of Gloucester, City of Ottawa.



Figure 1: Aerial View of Proposed Development

The site at 6001-6005 Renaud Road has approximately 76.1 metres of frontage along Renaud Road (south property line), maximum side yard depth of approximately 61.0 metres. The overall lot area is approximately **0.46 ha**. The site is currently zoned DR (Development Reserve Zone) and is occupied by two detached residential dwellings (2-storey and 1.5-storey buildings). Most of the site is landscaped with some paved surfaces.

The proposed works will only take into consideration the area of site allocated to the development of the stacked townhomes and amenities. These works will be located primarily within the south portion of the lot, with the exception of a lane along the east property line (to provide site access to Ziegler). Frontage along Renaud will remain the same, at approximately 76.1m. Side yard lengths will vary; west side yard of 35.5m, east side yard of 61.0m. Rear yard lot line will be split



between the lot line abutting the future semi-detached lots at 68.5m, and abutting Ziegler street at 11.6m. The overall limits of construction area is approximately **0.29 ha**

The development proposes five (5) blocks of 3-storey stacked townhome buildings with walk-out basements, consisting of 20 units to the south of the property and 6 semi-detached houses to the north of the property. However, the 6 semi-detached house will not be considered for site plan application or within the stormwater report. The proposed development will also feature 18 surface parking spaces as well as sheltered garages to accommodate parking demands.

For the purposes of this report & design, the lots allocated to the development of future semi-detached homes will not be considered. The combined area of the future semi-detached lots is approximately 68.5m (frontage along Renaud) by 25.3m (side yard along the west property line).

This report has been prepared in consideration of the terms and conditions noted above and with the civil drawings prepared for the new development. Should there be any changes in the design features, which may relate to the stormwater considerations, LRL Associates Ltd. should be advised to review the report recommendations.

2 EXISTING SITE AND DRAINAGE DESCRIPTION

The subject site measures **0.29 ha** and is gently sloped north from Renaud Road to Ziegler Street. Existing elevations range from 75.65m along south property line fronting Renaud St to 74.34m along north property line fronting Ziegler St.

Sewer and watermain mapping, along with as-built information collected from the City of Ottawa indicate the following existing infrastructure located within the adjacent right-of-way:

Ziegler Street:

- 200mmØ PVC DR-18 watermain
- 250mmØ PVC DR-35 sanitary sewer
- 750, 825 & 975mmØ CL 100-D concrete storm sewer

3 SCOPE OF WORK

As per applicable guidelines, the scope of work includes the following:

Stormwater management

- Calculate the allowable stormwater release rate.
- Calculate the anticipated post-development stormwater release rates.
- Demonstrate how the target quantity objectives will be achieved.

Water services

- Calculate the expected water supply demand at average and peak conditions.



- Calculate the required fire flow as per the Fire Underwriters Survey (FUS) method.
- Confirm the adequacy of water supply and pressure during peak flow and fire flow.
- Describe the proposed water distribution network and connection to the existing system.

Sanitary services

- Describe the existing sanitary sewers available to receive wastewater from the building.
- Calculate peak flow rates from the development.
- Describe the proposed sanitary sewer system.
- Review impact of increased sanitary flow on downstream sanitary sewer.

4 REGULATORY APPROVALS

An MECP Environmental Compliance Approval is not expected to be required for installation of the proposed storm and sanitary sewers within the site. A Permit to Take Water is not anticipated to be required for pumping requirements for sewer installation. The Rideau Valley Conservation Authority will need to be consulted to obtain municipal approval for site development. No other approval requirements from other regulatory agencies are anticipated.

5 WATER SUPPLY AND FIRE PROTECTION

5.1 Existing Water Supply Services and Fire Hydrant Coverage

The subject property lies within the City of Ottawa 2E water distribution network pressure zone. The subject property is located within proximity of an existing 200 mm dia. watermain along Ziegler St. There are currently several existing fire hydrants available to service the subject property. Refer to **Appendix B** for the location of fire hydrants.

5.2 Water Supply Servicing Design

The subject property is proposed to be serviced via a closed loop network of 150 mm diameter watermain connected to the existing 200 mm watermain within Ziegler Street. Refer to Site Servicing Plan C.401 in **Appendix E** for servicing layout.

Table 1 summarizes the City of Ottawa Design Guidelines design parameters employed in the preparation of the water demand estimate.

Table 1: City of Ottawa Design Guidelines Design Parameters

Design Parameter	Value
Residential Townhouse	2.7 P/unit
Average Daily Demand	280 L/d/per
Minimum Depth of Cover	2.4 m from top of watermain to finished grade
Desired operating pressure range during normal operating conditions	350 kPa and 480 kPa
During normal operating conditions pressure must not drop below	275 kPa



During normal operating conditions pressure shall not exceed	552 kPa
During fire flow operating conditions pressure must not drop below	140 kPa
*Table updated to reflect technical Bulletin ISDTB-2018-02	

The interior layout and architectural floor plans have been reviewed, and it was determined that the total proposed residential development will house twenty (20) stacked town units. Based on the City of Ottawa Design guidelines for population projection, this translates to approximately 54.0 residents. Table 2 below summarizes the proposed development as interpreted using table 4.1 of the City of Ottawa Design Guidelines.

Table 2: Development Residential Population Estimate

Proposed Unit type	Persons Per Unit	Number of Units	Population
Townhouse	2.7	20	54.0
Total Residential Population			54.0

The required water supply requirements for the residential units in proposed building have been calculated using the following formula:

Where:

$$Q = (q \times P \times M)$$

q = average water consumption (L/capita/day)

P = design population (capita)

M = Peak factor

Using a calculated Maximum Day Factor and Peak Hour factor of **7.5** and **11.2** respectively as per Table 3-3 in the *MOE Design Guidelines*, anticipated demands were calculated as follows:

- Average daily domestic water demand is **0.18** L/s,
- Maximum daily demand is **1.30** L/s, and
- Maximum hourly is **14.62** L/s.

Refer to **Appendix B** for water demand calculations.

The City of Ottawa was contacted to obtain boundary conditions associated with the estimated water demand, as indicated in the boundary request correspondence included in **Appendix B**. Table 3 below summarizes boundary conditions for the proposed development.



Table 3: Summary of Anticipated Demands and Boundary Conditions

Design Parameter	Anticipated Demand (L/min)	Boundary Conditions @ Renaud Road Head (m) / Pressure (psi)
Average Daily Demand	11	130.7 / 81.2
Max Day + Fire Flow (Block A)	78 + 16,000	115.5 / 59.5
Max Day + Fire Flow (Block B)	78 + 16,000	115.5 / 59.5
Peak Hour	877	126.7 / 75.5
*Assumed Ground elevation at connection point = 73.60 m. Water demand calculation per City of Ottawa Water Design guidelines. See Appendix B for details.		

As indicated in Table 3, Average Daily Demand pressure exceeded the required pressure range (greater than 80 psi) stated in Table 1 as per City of Ottawa Design Guidelines. Pipe Pressure Losses were calculated to factor in the loss in pressure expected. Considering a PVC pipe (roughness coefficient C of 150) of 150mm inner diameter, at a length of 121.5m and an elevation variable of 1.64m, we could calculate a pipe pressure loss of **2.33 psi** within the network, resulting in an adjusted max pressure of **78.90 psi**, now falling within the allowable range.

Refer to **Appendix B** for Boundary Conditions & Pipe Pressure Loss Calculations.

The estimated fire flow for the proposed buildings was calculated in accordance with *ISTB-2018-02*. The following parameters were provided by the Architect, see **Appendix A** for collaborating correspondence:

- Type of construction – Wood Frame Construction;
- Occupancy type – Limited Combustibility; and
- Sprinkler Protection – Non-Sprinklered.

The estimated fire flow demand was estimated to be **16,000 L/min** for Blocks A and **16,000 L/min** for Block B. See **Appendix B** for details.

There are several existing fire hydrants within 300 m to the proposed buildings that are available to meet the required fire flow demands stated above. Refer to **Appendix B** for fire hydrant locations.

Table 4 below summarizes the approximate aggregate fire flow of the contributing hydrants within 300 m to the proposed development based on Table 18.5.4.3 of *ISTB-2018-02*.



Table 4: Fire Protection Summary Table

Building	Fire Flow Demand (L/min)	Fire Hydrants(s) within 75m	Fire Hydrant(s) within 150m	Fire Hydrant(s) within 300m	Approximate Available Combined Fire Flow (L/min)
BLOCK A	16,000	2	6	-	(2 x 5678) + (6 x 3785) = 34,066
BLOCK B	16,000	2	6	-	(2 x 5678) + (6 x 3785) = 34,066

As shown in Table 4, the approximate total available fire flow from contributing hydrants is sufficient to provide adequate fire flow for the proposed buildings.

The proposed water supply design conforms to all relevant City Guidelines and Policies.

6 SANITARY SERVICE

6.1 Existing Sanitary Sewer Services

The subject property is tributary to the Forest valley trunk sewer. There is an existing 250 mm dia. sanitary sewer within Ziegler St. across from the subject site that ultimately conveys flows to the Forest Valley trunk sewer.

The subject property falls within the area contemplated in the *Gloucester East Urban Community Infrastructure Servicing Study Update (Gloucester EUC)*, prepared by Stantec, revision date March 2005. Refer to Drainage Plan extracted from the *Gloucester EUC* in **Appendix C**.

The post development total wet wastewater flow was calculated to be is **0.80 L/s** as a result of proposed residential population and a small portion of infiltration. Refer to **Appendix C** for further information on the calculated sanitary flows.

As per the Urbantech Functional Servicing Report dated December 2020, the 250mm diameter sanitary sewer within Ziegler Street has a full capacity of 38.0 L/s. Maximum design from the current developed subdivision is expected to be 19.97 L/s. Assuming peak design flow should not exceed 85%, the current reserve capacity of the Ziegler sewer is expected to be 12.3 L/s.

The proposed Caivan residential development, directly East of the 6001/6005 Renaud site, is expected to have a peak design flow of 10.5 L/s. This would leave an allowable reserve capacity of **1.8 L/s** for the proposed residential developments at 6001/6005 Renaud Road.

Refer to **Appendix C** for the Caivan Functional Servicing Report referenced.

The current proposed residential developments (Block A, Block B) will require **0.80 L/s** of the sewer capacity. This would leave the sewer with a capacity of **1.00 L/s** for the future semi-detached houses (located along Ziegler Street, refer to site plan). Therefore, it is anticipated that



the existing local sanitary sewer network has sufficient capacity to accommodate the proposed development.

6.2 Sanitary Sewer Servicing Design

The proposed development will be serviced via a 150 mm dia. sanitary sewer network which will connect to the existing 250mm dia. sanitary sewer located within Ziegler Street. Refer to LRL drawing C.401 for the proposed sanitary servicing.

The parameters used to calculate the anticipated sanitary flows are; residential average population per unit of 2.7 persons for townhouse units, a residential daily demand of 280 L/p/day, a residential peaking factor of 4.0 and a total infiltration rate of 0.33 L/s/ha. Based on these parameters and the total site area of 0.29 ha, the total wet wastewater flow was calculated as **0.80 L/s**. Refer to **Appendix C** for the site sanitary sewer design sheet.

7 STORMWATER MANAGEMENT

7.1 Existing Stormwater Infrastructure

Stormwater runoff from the subject property is tributary to the City of Ottawa sewer system as such, approvals for the proposed development within this area are under the approval authority of the City of Ottawa.

In pre-development conditions, the stormwater runoff would flow uncontrolled overland to the towards the Renaud Road right-of-way. There is an existing 750 mm diameter storm sewer within Ziegler Street right-of-way. Refer to **Appendix D** for pre- and post-development watershed information.

7.2 Design Criteria

The stormwater management criteria for this development are based on the criteria stated in the **Gloucester EUC Study**, as well as pre-consultation with City of Ottawa officials, the City of Ottawa Sewer Design Guidelines including City of Ottawa Stormwater Management Design Guidelines, 2012 (City standards), as well as the Ministry of the Environment's Stormwater Planning and Design Manual, 2003 (SWMP Manual).

7.2.1 Water Quality

The subject property lies within the Ottawa River East sub-watershed and is therefore subject to review by the Rideau Valley Conservation Authority (RVCA).

As per the **Gloucester EUC Study**, the subject property falls within the tributary area of SWM Pond 3, refer to Figure 6 as well as the Drainage Plan extracted from the **Gloucester EUC Study** included in **Appendix D**. Therefore, it was determined that no further treatment is required for stormwater runoff from the proposed development. Correspondence with RVCA is included in **Appendix A**.



7.2.2 Water Quantity

Based on **Gloucester EUC Study**, the following stormwater management requirements were identified for the subject site:

- Meet an allowable release of 85 L/s/ha;
- Attenuate all storms up to and including the City of Ottawa 100-year storm event on site; and

The allowable release rate for the subject site was calculated to be **24.77 L/s**. Refer to **Appendix D** for calculations.

7.3 Method of Analysis

The Modified Rational Method has been used to calculate the runoff rate from the site to quantify the detention storage required for quantity control of the development. Refer to **Appendix D** for storage calculations.

7.4 Proposed Stormwater Quantity Controls

The proposed stormwater management quantity control for this development will be accomplished by utilizing an inlet control device to restrict flows to the allowable release rate. Storage required as a result of quantity control will be accomplished through a combination of surface storage and underground stormwater chambers in the parking lot.

The subject site is proposed to be serviced via a network of 300mm diameter storm sewers that outlet to the existing 750 mm diameter storm sewer within Ziegler street. The proposed site storm sewer and stormwater management system are shown on drawing C.401 and detailed calculations, including the design sheet, can be found in **Appendix D**.

The existing site is delineated by catchments EWS-01 which currently drains uncontrolled towards the Renaud Road and Ziegler Street right-of-ways.

The site has been analyzed and post development watersheds have been allocated. Watershed WS-01 (0.058 ha), consisting of landscaping and a paved ramp, will flow uncontrolled. The runoff will be conveyed to the Ziegler Street right-of-way, as per the grading plan C301.

Overland flow within watershed WS-02 (0.233 ha) will be captured by catch basins CB02, CB03 and CB05. A Hydrovex 75VHV-1 vertical flow regulator is proposed at mh01 to restrict collected runoff to a specific release rate. Grading proposed will provide positive overland drainage to the proposed storm water collection and control systems.

Table 5 below summarizes post-development drainage areas. Calculations can be seen in **Appendix D**.



Table 5: Drainage Areas

Drainage Area Name	Area	Weighted Runoff Coefficient	100 Year Weighted Runoff Coefficient (25% increase)
WS-01 (uncontrolled)	0.058	0.50	0.63
WS-02 (controlled)	0.233	0.74	0.92

Table 6 below summarize the release rates and storage volumes required to meet the allowable release rate of **24.77 L/s** for 100-year flow rates.

Table 6: Stormwater Release Rate & Storage Volume Summary (100 Year)

Catchment Area	Drainage Area (ha)	100-year Release Rate (L/s)	100-Year Required Storage (m ³)	Total Available Storage (m ³)
WS-01 (uncontrolled)	0.058	18.15	0	0
WS-02 (controlled)	0.233	6.62	118.35	128.09
TOTAL	0.291	24.77	118.35	128.09

It is estimated that **18.15 L/s** of runoff will flow uncontrolled from WS-01 towards the Ziegler Street right-of-way.

Runoff collected in WS-02 will be attenuated on site and discharged at a specific release rate of 6.62 L/s via a Hydrovex 75-VHV-1 flow control unit located at the invert of MH01, refer to **Appendix D** for additional info on the flow control unit. Considering a halved controlled release rate (to account for variable design head due to the combination of underground and overland storage), it can be calculated that a total **118.35 m³** of storage will be required to attenuate flows to the allowable release rate. The project runoff exceeding the allowable release rate will be stored on-site via surface ponding at the parking lot as well as Stormtech underground chambers Model MC-3500 (or approved equivalent). Total proposed surface ponding provides approx. **16.98 m³** and the proposed underground chambers provide **111.11 m³** to provide a total storage of **128.09 m³**, refer to **Appendix D** for additional info on Stormtech chambers. The 100-year maximum ponding depths can be found on drawing “C601 – Stormwater Management Plan” of **Appendix E**.

8 EROSION AND SEDIMENT CONTROL

During construction, erosion and sediment controls will be provided primarily via a sediment control fence to be erected along the perimeter of the site where runoff has the potential of leaving



the site. Inlet sediment control devices are also to be provided in any catch basin and/or manholes in and around the site that may be impacted by the site construction. Construction and maintenance requirements for erosion and sediment controls are to comply with Ontario Provincial Standard Specification OPSS 577. Refer to LRL Associates drawing C.101 for erosion and sediment control details.

9 CONCLUSION

This Stormwater Management and Servicing Report for the development proposed at 6001/6005 Renaud presents the rationale and details for the servicing requirements for the subject property.

In accordance with the report objectives, the servicing requirements for the development are summarized below:

Water Service

- The maximum required fire flow was calculated at **16,000 L/min** for Block A and **16,000 L/min** for Block B using the FUS method.
- There are at least seven (8) existing fire hydrants within 150m available to service the proposed developments. They will provide a combined fire flow of **34,066 L/min** to the site.
- The new development/expansion will be serviced with a new 150 mm Φ closed loop watermain network to be connected to the existing 200mm Φ watermain within Ziegler Street.
- Boundary conditions received from the City of Ottawa, considering pipe pressure losses, have indicate that sufficient pressure is available to service the proposed site.

Sanitary Service

- The anticipated sanitary flow from the proposed development is **0.80 L/s**.
- The proposed development will be serviced by a 150 mm diameter sanitary sewer network that connects to the existing 250 mm dia. sanitary sewer within Ziegler Street.

Stormwater Management

- The subject property is serviced by existing SWM Pond 3 as per the **Gloucester EUC Study**. Hence additional quality control measures are not proposed.
- The storm water release rates from the proposed development will meet the pre-allocated rate of **85 L/s/ha** stated in the **Gloucester EUC Study**. The target release rate for the site, based on the EUC, was calculated to be **24.77 L/s**. Permitted release rate from the site (considering controlled & uncontrolled catchment areas) was calculated to be **6.62 L/s**.
- Stormwater quantity control objectives will be met through on-site storm water ponding and sub-surface storage in the parking lot.



10 REPORT CONDITIONS AND LIMITATIONS

The report conclusions are applicable only to this specific project described in the preceding pages. Any changes, modifications or additions will require a subsequent review by LRL Associates Ltd. to ensure the compatibility with the recommendations contained in this document. If you have any questions or comments, please contact the undersigned.

Prepared by:
LRL Associates Ltd.

Kyle Herold

Virginia Johnson, P.Eng



APPENDIX A
Pre-consultation / Correspondance



MEMO

Date: July 16, 2021

To /
Destinataire Steve Belan, Planner

From /
Expéditeur Natasha Baird, Senior Engineer, Infrastructure
Approvals

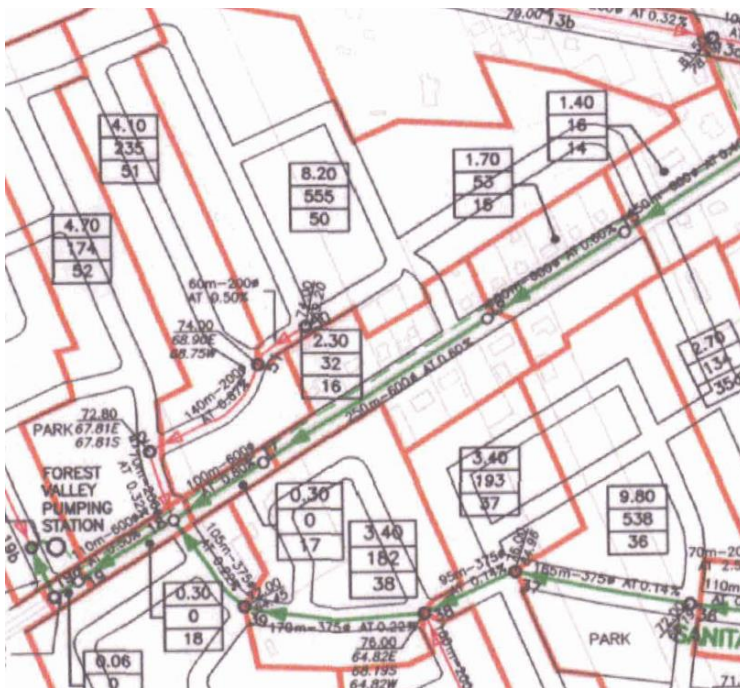
Subject /
Objet **Pre-Application Consultation
6001 and 6007 Renaud Road
Proposed Residential Development.**

File No. PC2020-0295

Please note the following information regarding the engineering design submission for the above noted site:

1. The Servicing Study Guidelines for Development Applications are available at the following address: <http://ottawa.ca/en/development-application-review-process-0/servicing-study-guidelines-development-applications>
2. Servicing and site works shall be in accordance with the following documents:
 - ⇒ Ottawa Sewer Design Guidelines (October 2012)
 - ⇒ Ottawa Design Guidelines – Water Distribution (2010)
 - ⇒ Geotechnical Investigation and Reporting Guidelines for Development Applications in the City of Ottawa (2007)
 - ⇒ City of Ottawa Slope Stability Guidelines for Development Applications (revised 2012)
 - ⇒ City of Ottawa Environmental Noise Control Guidelines (January, 2016)
 - ⇒ City of Ottawa Park and Pathway Development Manual (2012)
 - ⇒ City of Ottawa Accessibility Design Standards (2012)
 - ⇒ Ottawa Standard Tender Documents (latest version)
 - ⇒ Ontario Provincial Standards for Roads & Public Works (2013)

3. Record drawings and utility plans are also available for purchase from the City (Contact the City's Information Centre by email at InformationCentre@ottawa.ca or by phone at (613) 580-2424 x.44455).
4. EUC CDP and Background Studies: The parcels are situated on East Urban Community (EUC) Phase 1 lands, and there is the Phase 1 Community Design Plan (CDP) and associated background studies which accompany this document, such as the 2005 Gloucester EUC Infrastructure Study Update (Stantec) which sets out the infrastructure plan for the CDP area, and the 2004 Geotechnical Considerations: East Urban Community study (Golder), amongst others. Note that a CDP for the Phase 2 lands (bordering Mer Bleue Rd. to the east, Mer Bleue bog to the south, and Renaud Rd. to the North) was finalized in 2013 and the direction of this CDP supersedes the requirements set out in the Phase 1 CDP. These documents are to be consulted accordingly, and the proposed design is to be consistent with these documents.
5. The sanitary servicing criteria is subject to Forest Valley PS and capacity is required. Please refer to the EUC Master Servicing Study from Stantec (dated March 2005).



6. The Stormwater Management Criteria, for the subject site, is to be based on the EUC Master Servicing Study from Stantec (dated March 2005).



7. Servicing: Renaud Road – existing 305mm watermain., existing 1350mm storm sewer, existing 600mm sanitary sewer. There is 30cm reserve at Ziegler Street, where there is existing 205mm watermain, existing 250mm sanitary sewer and 750mm and 825mm storm sewer.
8. Deep Services (Storm, Sanitary & Water Supply)
- i. *Provide existing servicing information and the recommended location for the proposed connections. Services should ideally be grouped in a common trench to minimize the number of road cuts.*
 - ii. *Connections to trunk sewers and easement sewers are typically not permitted.*
 - iii. *Provide information on the monitoring manhole requirements – should be located in an accessible location on private property near the property line (ie. Not in a parking area).*

iv. *Provide information on the type of connection permitted*

Sewer connections to be made above the springline of the sewermain as per:

- a. Std Dwg S11.1 for flexible main sewers – *connections made using approved tee or wye fittings.*
- b. Std Dwg S11 (For rigid main sewers) – *lateral must be less than 50% the diameter of the sewermain,*
- c. Std Dwg S11.2 (for rigid main sewers using bell end insert method) – *for larger diameter laterals where manufactured inserts are not available; lateral must be less than 50% the diameter of the sewermain,*
- d. Connections to manholes permitted when the connection is to rigid main sewers where the lateral exceeds 50% the diameter of the sewermain. – Connect obvert to obvert with the outlet pipe unless pipes are a similar size.
- e. *No submerged outlet connections.*

9. Water Boundary condition requests must include the location of the service and the expected loads required by the proposed development. Please provide the following information:

- i. Location of service
- ii. Type of development and the amount of fire flow required (as per FUS, 1999).
- iii. Average daily demand: ___ l/s.
- iv. Maximum daily demand: ___ l/s.
- v. Maximum hourly daily demand: ___ l/s.

10. MECP ECA Requirements:

An MECP Environmental Compliance Approval (Municipal Sewage Works) will **only be required if multiple parcels** are proposed for this development. This

application will be under the ToR Program. For your information, I have included the email to the Ottawa District office, but you are not required to contact them.

For residential applications: moeccottawaseage@ontario.ca

11. Phase 1 ESAs and Phase 2 ESAs must conform to clause 4.8.4 of the Official Plan that requires that development applications conform to Ontario Regulation 153/04.
12. Provide comments from the conservation authority. It is recommended to consult the office prior to submitting an application. The major overland flow route is susceptible to discharge to the Mud Creek Watershed which is part of the Rideau Valley Conservation Authority. Please contact Jamie Batchelor at the RVCA: <https://www.rvca.ca/contact-us>. Please refer to the Mud Creek Cumulative Impact Study.
13. Development Charges (DC): The site is subject to an Area Specific DC as it falls within Area E-3 of the Gloucester East Urban Centre Stormwater Facilities By-Law 2019-165. Further information regarding DC calculations, exemptions, indexing of rates can be obtained through Gary Baker, DC Program Coordinator (gary.baker@ottawa.ca).
14. Gloucester EUC Cost Sharing Agreement dated February 2008 between participating Owners: Rivard/Monarch, Richcraft, Minto, DCR Phoenix, Claridge, and Ashcroft: The site is subject to an existing EUC Ownership Cost Sharing Agreement which is administered by a Trustee on behalf of the ownership group. It is recommended that the Applicant contact the Trustee to discuss the terms of the agreement as a Non-Participating Owner (an owner of a land shown on the plans attached in Schedule D of the Agreement, and who is not party to this Agreement). The Trustee is Kris Kilborn at Stantec Consulting Ltd. (kris.kilborn@stantec.com).
15. Geotechnical Considerations: East Urban Community study was completed in 2004 by Golder. The study covers the EUC lands and provided findings with respect to the type of development proposed and landform (topography, and the fact that the area predominantly consists of surficial sand and silty sand over sensitive marine clay soils). These can bring some constraints along with them, specifically:
 - a. grade raise restrictions
 - b. slope stability (around the drainage features and the escarpment)
 - c. relatively high groundwater levels.

Geotechnical MSS related to Zone 2A and 3 as per the MSS:



Zone 2

Zone 2 encompasses the area south and west of Navan Road with the exception of Zone 3 and includes the Escarpment lands. The subsurface condition typically consists of discontinuous deposits of surficial sand and silty sand typically 1.5 to 2.0m in depth overlying sensitive weathered silty clay of 2.0 to 3.0m. Surficial sand and silty sand deposits exceed 3.0m in some areas and are absent in others. The soil conditions in Zone 2 are similar to Zone 1 with varying strengths and a thinner weathered crust. The un-drained shear strength of the un-weathered silty clay is in the order of 20 to 25 kPa suggesting it is compressible. Groundwater levels are shallow, ranging in depth from the ground surface to within 1.0 to 1.5m of the ground surface.

The subsurface conditions within the escarpment are similar, with a thicker crust and deeper groundwater levels reflecting better drainage.

Due to the variability in data, making it difficult to establish grade restrictions for all of Zone 2, it was divided into two parts, Zone 2A and Zone 2B. Within Zone 2A, which includes almost all of Zone 2, a maximum grade raise restriction of 0.5m is acceptable, with no grade raise preferred. Conversely, a maximum grade raise of 2.0m is acceptable in Zone 2B.

Zone 2A is not well suited for development of higher-density structures using conventional spread footings. Even with the grade raise, conventional houses may not be feasible through all of Zone 2A, requiring wider footings or shallower foundations consistent with "high ranch" style homes.

Higher density developments on conventional spread footings are possible in Zone 2B provided grade raises are minimized to allow sufficient remaining capacity to support additional structure loads.

Zone 3

Zone 3 covers a portion of the low-lying areas south of Fourth Line Road and consists of glacial till overlain by a thick deposit of weathered silty clay. There is no practical limit to the grade raise permitted in Zone 3 but, for planning purposes, a reasonable limit of 3m was proposed. The area is well suited for mid-rise and possibly high-rise buildings on conventional spread footings.

Table 1
Feasible Building Structures Supported on Spread Footings
within Zones 1, 2, 3 and MUC

Building Structures	Geographical Zones			
	1	2	3	MUC
Up to 2 storey timber frame w or w/o basements and at-grade garage (i.e. conventional suburban housing and/or "high ranch" style homes)		✓ (2A) ¹		
Up to 2 storey timber frame w basements and at-grade garage (i.e. conventional suburban housing)				✓
Up to 3 storey timber frame w or w/o basements (i.e. stacked townhouses)	✓ ²			
Up to 3 storey (possibly 4 storey) timber frame w/o basements (i.e. townhouses or apartment buildings)				✓
Up to 3 storey timber frame w basements, w/o at grade garages or w garage in basement (i.e. stacked townhouses with depressed driveways)				✓
Up to 3 storey (possibly 4 storey) timber frame w concrete framed ground floor and basement level parking garages				✓
Higher density type developments		✓ (2B)	✓	

Note:

¹ Lack of good quality geotechnical information within the area and consequently guideline may be too conservative. Type of housing (conventional suburban versus "high ranch" style homes) depends on the servicing feasibility given the 0-0.5m grade raise restriction.

² Up to 3 storey timber framed w or w/o basements (i.e. stacked townhouses) may only be semi-feasible if supported on spread footings.

Given the grade raise and the building restrictions, please contact a geotechnical engineer to determine what possible development can occur based on the discussion in the MSS report. Further geotechnical investigation will be required to clarify the possible types of development.

Should you have any questions or require additional information, please contact me directly at (613) 580-2424, ext. 27995 or by email at Natasha.baird@ottawa.ca.

APPENDIX B
Water Supply Calculations





Water Supply Calculations

LRL File No. 210216-02
 Date June 9, 2023
 Prepared by K. Herold
 Project Location 6001/6005 Renaud

Residential Demand based on the City of Ottawa Design Guidelines-Water Distribution, 2010

Unit Type	Persons Per Unit	Number of Units	Population
Townhouse	2.7	20	54.0
Total		20	54.0

Average Water Consumption Rate	280 L/c/d	
Average Day Demand	15,120 L/d	0.18 L/s
Maximum Day Factor	7.5	(MOE Table 3-3)
Maximum Daily Demand	112,697 L/d	1.30 L/s
Peak Hour Factor	11.2	(MOE Table 3-3)
Maximum Hour Demand	1,263,509 L/d	14.62 L/s

Water Service Pipe Sizing

$$Q = VA$$

Where: V = velocity

A = area of pipe

Q = flow rate

Assuming a maximum velocity of 1.8m/s, the diameter of pipe is calculated as:

$$\begin{aligned} \text{Minimum pipe diameter (d)} &= (4Q/\pi V)^{1/2} \\ &= 0.102 \text{ m} \\ &= 102 \text{ mm} \end{aligned}$$

$$\begin{aligned} \text{Proposed pipe diameter (d)} &= 150 \text{ mm} \\ &= 6 \text{ Inches} \end{aligned}$$



LRJ

**Fire Flow Calculations
6001 / 6005 Renaud - Block A**

LRL File No. 210216-02
 Date June 9, 2023
 Method Fire Underwriters Survey (FUS)
 Prepared by K. Herold

Step	Task	Term	Options	Multiplier	Choose:	Value	Unit	Fire Flow
Structural Framing Material								
1	Choose frame used for building	Coefficient C related to the type of construction	Wood Frame	1.5	Wood Frame	1.5		
			Ordinary Construction	1.0				
			Non-combustible construction	0.8				
			Fire resistive construction <2 hrs	0.7				
			Fire resistive construction >2 hrs	0.6				
Floor Space Area (A)								
2			Total area (building area of 360m ² , 4 stories)			1,440	m ²	
3	Obtain fire flow before reductions	Required fire flow	Fire Flow = 220 x C x A ^{0.5}				L/min	12,523
Reductions or surcharge due to factors affecting burning								
4	Choose combustibility of contents	Occupancy hazard reduction or surcharge	Non-combustible	-25%	Limited combustible	-15%	L/min	10,644
			Limited combustible	-15%				
			Combustible	0%				
			Free burning	15%				
			Rapid burning	25%				
5	Choose reduction for sprinklers	Sprinkler reduction	Full automatic sprinklers	-30%	False	0%	L/min	10,644
			Water supply is standard for both the system and fire department hose lines	-10%	False	0%		
			Fully supervised system	-10%	False	0%		
6	Choose separation	Exposure distance between units	North side	20.1 to 30m	10%	L/min	15,966	
			East side	3.1 to 10m	20%			
			South side	>45m	0%			
			West side	3.1 to 10m	20%			50%
Net required fire flow								
7	Obtain fire flow, duration, and volume					Minimum required fire flow rate (rounded to nearest 1000)	L/min	16,000
						Minimum required fire flow rate	L/s	266.7
						Required duration of fire flow	hr	4.25



LRJ

**Fire Flow Calculations
6001 / 6005 Renaud - Block B**

LRL File No. 210216-02
 Date June 9, 2023
 Method Fire Underwriters Survey (FUS)
 Prepared by K. Herold

Step	Task	Term	Options	Multiplier	Choose:	Value	Unit	Fire Flow
Structural Framing Material								
1	Choose frame used for building	Coefficient C related to the type of construction	Wood Frame	1.5	Wood Frame	1.5		
			Ordinary Construction	1.0				
			Non-combustible construction	0.8				
			Fire resistive construction <2 hrs	0.7				
			Fire resistive construction >2 hrs	0.6				
Floor Space Area (A)								
2			Total area (building area of 360m ² , 4 stories)			1,440	m ²	
3	Obtain fire flow before reductions	Required fire flow	Fire Flow = 220 x C x A ^{0.5}				L/min	12,523
Reductions or surcharge due to factors affecting burning								
4	Choose combustibility of contents	Occupancy hazard reduction or surcharge	Non-combustible	-25%	Limited combustible	-15%	L/min	10,644
			Limited combustible	-15%				
			Combustible	0%				
			Free burning	15%				
			Rapid burning	25%				
5	Choose reduction for sprinklers	Sprinkler reduction	Full automatic sprinklers	-30%	False	0%	L/min	10,644
			Water supply is standard for both the system and fire department hose lines	-10%	False	0%		
			Fully supervised system	-10%	False	0%		
6	Choose separation	Exposure distance between units	North side	20.1 to 30m	10%	L/min	15,966	
			East side	3.1 to 10m	20%			
			South side	>45m	0%			
			West side	3.1 to 10m	20%			50%
Net required fire flow								
7	Obtain fire flow, duration, and volume					Minimum required fire flow rate (rounded to nearest 1000)	L/min	16,000
						Minimum required fire flow rate	L/s	266.7
						Required duration of fire flow	hr	4.25



Pipe Pressure Losses Calculations

LRL File No. 210216-02

Project Navan Stacked Townhomes

Location: 6001/6005 Renaud Road

Date June 9, 2023

Designed: K. Herold

Piezometric Head Equation (Derived from Bernoulli's Equation)

$$h = \frac{p}{\gamma} + z$$

Where:

h = HGL (m)

p = Pressure (Pa)

γ = Specific weight (N/m³) =

9810

z = Elevation of centreline of pipe (m) =

73.6

Water Pressure on Huron Street			
HGL (m)		Pressure	
		kPa	psi
Minimum =	126.7	520.91	75.55
Maximum =	130.7	560.15	81.24
Max. Day + Fire =	115.5	411.04	59.62

Hazen Williams Equation

$$h_f = \frac{10.67 \times Q^{1.85} \times L}{C^{1.85} \times d^{4.87}}$$

Where:

h_f = Head loss over the length of pipe (m)

Q = Volumetric flow rate (m³/s)

L = Length of pipe (m)

C = Pipe roughness coefficient

d = Pipe diameter (m)

Scenario 1: maximum daily demand

Q (L/s)	1.30
C	150
L (m.)	121.5

I.D. (mm)	150	
V (m/s)	0.07	
h_f (m)	0.01	
Head Loss (psi)	0.01	
Min. Pressure (psi)	75.54	
Max. Pressure (psi)	81.23	
Service Obs. @ Street Connection (m)	70.86	
Service Obs. @ Building Connection (m)	72.50	
Pressure Adjustment (psi)	-2.33	(due to service elevation difference from street to building)
Adjusted Min. Pressure (psi)	73.21	(must not be less than 50psi)
Adjusted Max. Pressure (psi)	78.90	(must not be more than 80psi)

Scenario 2: maximum hourly demand

Q (L/s)	14.62	
C	150	
L (m.)	121.5	
I.D. (mm)	150	
V (m/s)	0.83	
h_f (m)	0.51	
Head Loss (psi)	0.72	
Min. Pressure (psi)	74.83	
Max. Pressure (psi)	80.52	
Service Obs. @ Street Connection (m)	70.86	
Service Obs. @ Building Connection (m)	72.50	
Pressure Adjustment (psi)	-2.33	(due to service elevation difference from street to building)
Adjusted Min. Pressure (psi)	72.50	(must not be less than 40psi)
Adjusted Max. Pressure (psi)	78.19	(must not be more than 80psi)

City of Ottawa Boundary Conditions (Multi-Hydrant Analysis)

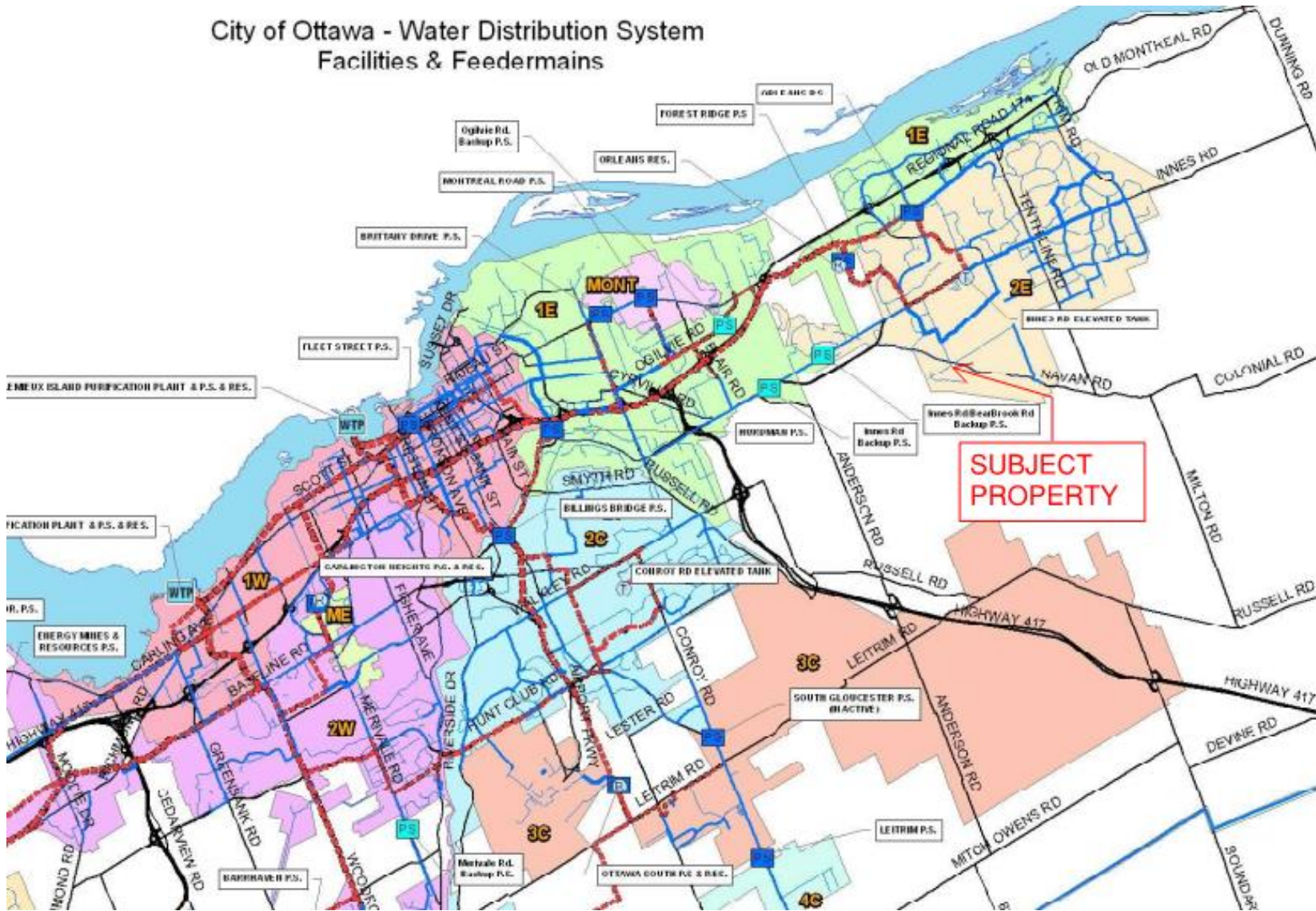
	Quantity	Max Capacity (L/min)*	Available Fire Flow** (L/min)
Fire Hydrant(s) Within 76m	2	5678	11356
Fire Hydrant(s) Within 76m to 152m	6	3785	22710
Fire Hydrant(s) Within 152m to 305m		2839	0
Available Combined Fire Flow (L/min)			34066
Max Day + Fire Flow Demand (L/min)			16000

*as per Table 18.5.4.3. of ISTB-2018-02

**assumed class AA hydrants

***flow provided from all hydrants within 76m is more than adequate to accommodate fire flow requirements, balance of hydrants within 152m and 305m not considered in design

City of Ottawa - Water Distribution System Facilities & Feeder mains



Legend

Water System Structure

- Pump Station
- Backup Pump Station
- Water Treatment Plant
- Well
- Elevated Tank
- Reservoir

WATERMAINS

- Priority, Internal Diameter
- Backbone 1524mm - 1981mm
 - Backbone 1067mm - 1372mm
 - Backbone 610mm - 914mm
 - Backbone 406mm - 508mm
 - Backbone 152mm - 305mm
 - Distribution 1679mm - 1981mm
 - Distribution 1067mm - 1372mm
 - Distribution 610mm - 914mm
 - Distribution 406mm - 508mm
 - Distribution 305mm - 381mm

PRESSURE ZONES

- 1E
- 1W
- 2C
- 2E
- 2W
- 3C
- 3W
- 4C
- 4W
- 5C
- 5W
- 6C
- 6W
- 7C
- 7W
- 8C
- 8W
- 9C
- 9W
- 10C
- 10W

Boundary Conditions 6001-6005 Renaud Road

Provided Information

Scenario	Demand	
	L/min	L/s
Average Daily Demand	11	0.18
Maximum Daily Demand	78	1.30
Peak Hour	877	14.62
Fire Flow Demand #1	16,002	266.70

Location



Results

Connection 1 – Ziegler St.

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	130.7	81.2
Peak Hour	126.7	75.5
Max Day plus Fire Flow	115.5	59.5

¹ Ground Elevation = 73.6 m

Notes

1. As per the Ontario Building Code in areas that may be occupied, the static pressure at any fixture shall not exceed 552 kPa (80 psi.) Pressure control measures to be considered are as follows, in order of preference:

- a. If possible, systems to be designed to residual pressures of 345 to 552 kPa (50 to 80 psi) in all occupied areas outside of the public right-of-way without special pressure control equipment.
- b. Pressure reducing valves to be installed immediately downstream of the isolation valve in the home/ building, located downstream of the meter so it is owner maintained.

Disclaimer

The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation. Fire Flow analysis is a reflection of available flow in the watermain; there may be additional restrictions that occur between the watermain and the hydrant that the model cannot take into account.

**FIRE HYDRANT
LOCATIONS
FIGURE**

LEGEND

SUBJECT SITE

HYDRANTS WITHIN 75 M ●

HYDRANTS WITHIN 150 M ●



Table 18.5.4.3 Maximum Fire Hydrant Fire Flow Capacity

Distance to Building ^a		Maximum Capacity ^b	
(ft)	(m)	(gpm)	(L/min)
≤ 250	≤ 76	1500	5678
> 250 and ≤ 500	> 76 and ≤ 152	1000	3785
> 500 and ≤ 1000	> 152 and ≤ 305	750	2839

^aMeasured in accordance with 18.5.1.4 and 18.5.1.5.
^bMinimum 20 psi (139.9 kPa) residual pressure.

APPENDIX C
Wastewater Collection Calculations
Supporting Documents





LRL File No. 210216-02
Project: Residential Development (20 Stacked TH)
Location: 6001/6005 Renaud Rd
Date: June 9, 2023

Sanitary Design Parameters

Average Daily Flow = 280 L/p/day
 Commercial & Institutional Flow = 50000 L/ha/day
 Light Industrial Flow = 35000 L/ha/day
 Heavy Industrial Flow = 55000 L/ha/day
 Maximum Residential Peak Factor = 4.0
 Commercial & Institutional Peak Factor = 1.5

Industrial Peak Factor = as per Appendix 4-B = 7
 Extraneous Flow = 0.33L/s/gross ha

Pipe Design Parameters

Minimum Velocity = 0.60 m/s
 Manning's n = 0.013

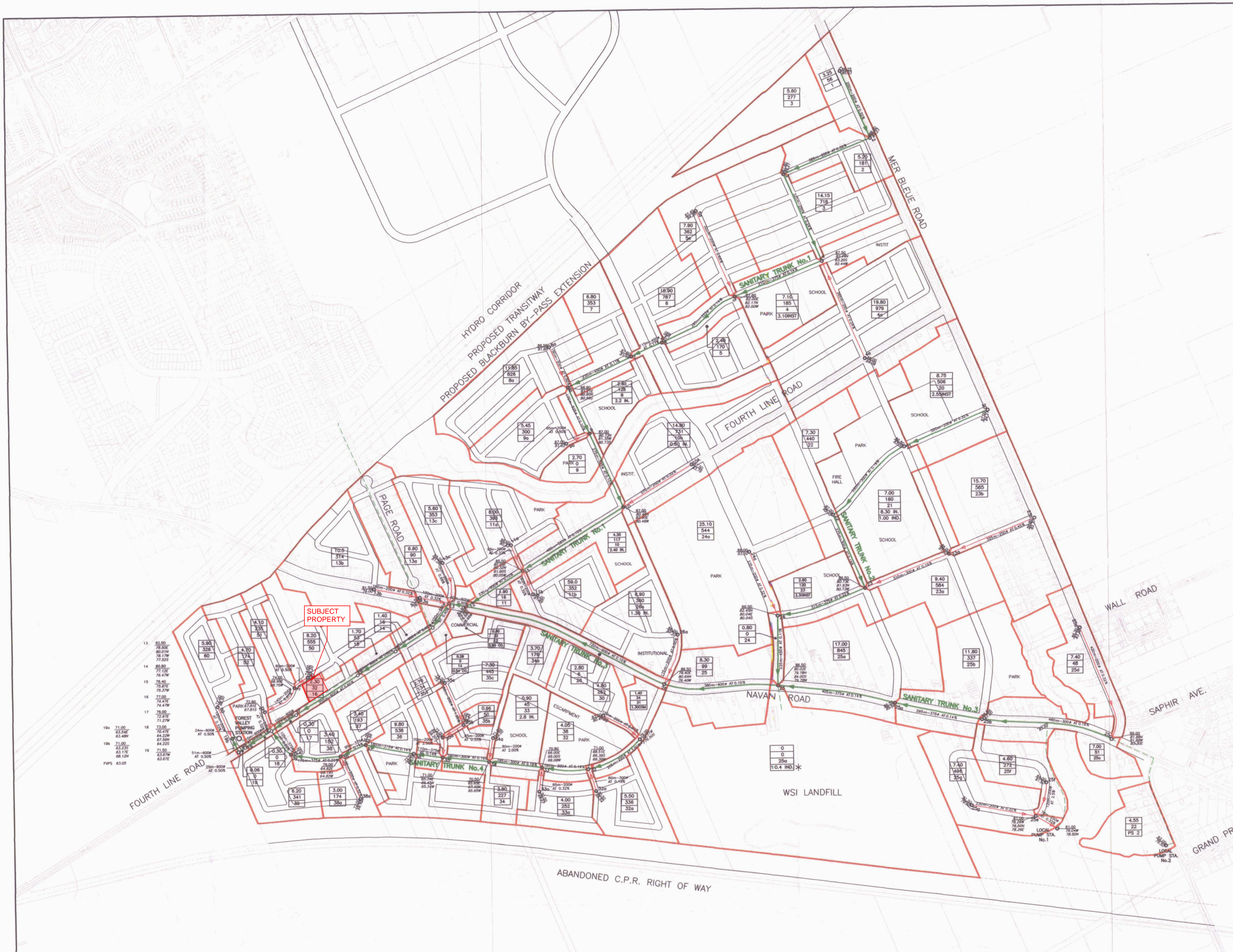
LOCATION			RESIDENTIAL AREA AND POPULATION						COMMERCIAL		INDUSTRIAL			INSTITUTIONAL		C+I+I	INFILTRATION			TOTAL FLOW (l/s)	PIPE					
STREET	FROM MH	TO MH	AREA (Ha)	POP.	CUMMULATIVE		PEAK FACT.	PEAK FLOW (l/s)	AREA (Ha)	ACCU. AREA (Ha)	AREA (Ha)	ACCU. AREA (Ha)	PEAK FACT.	AREA (Ha)	ACCU. AREA (Ha)	PEAK FLOW (l/s)	TOTAL AREA (Ha)	ACCU. AREA (Ha)	INFILT. FLOW (l/s)	TOTAL FLOW (l/s)	LENGTH (m)	DIA. (mm)	SLOPE (%)	MATERIAL	CAP. (FULL) (l/s)	VEL. (FULL) (m/s)
					AREA (Ha)	POP.																				
SITE	MH3	MH2	0.291	54.0	0.29	54.0	4.0	0.70	0.000	0.000	0.00	0.00	7.0	0.0	0.0	0.00	0.291	0.291	0.10	0.80	66.9	150	1.50%	PVC	18.65	1.06
SITE	MH2	MH1						0.70									0.291	0.291	0.10	0.80	24.6	150	1.50%	PVC	18.65	1.06
SITE	MH1	SAN SWR						0.70									0.291	0.291	0.10	0.80	23.7	150	1.50%	PVC	18.65	1.06

NOTES Existing inverts and slopes are estimated. They are to be confirmed on-site.

Designed:	K.H.	PROJECT:	Navan Stacked Townhomes
Checked:	V.J.	LOCATION:	6001/6005 Renaud Rd
Dwg. Reference:	C401	File Ref.:	210216-02
		Date:	June 9 2023
		Sheet No.	1 of 1



- 12a SANITARY SEWER AND MANHOLE
- 12 SANITARY TRUNK SEWER AND MANHOLE
- SANITARY FORCEMAIN
- SANITARY CATCHMENT AREA
- ORIGINAL GROUND OBVERT
- | | |
|------|-------------|
| 3.25 | AREA (ha) |
| 56 | POPULATION |
| 2 | MANHOLE No. |
- | | |
|----------|----------------------|
| 3.25 | AREA (ha) |
| 56 | POPULATION |
| 2 | MANHOLE No. |
| 3.2 INST | INST (INDUSTRIAL) ha |
| 3.2 INST | COM (COMMERCIAL) ha |
- * EQUIVALENT AREA (17.7 1/8 ALLOWABLE PEAK FLOW UNDER C of O SEWER USE AGREEMENT)



SUBJECT PROPERTY

13 82.50
78.50
80.01W
78.17W
77.52S

14 80.80
77.12
76.47W

15 78.40
75.87E
75.37W

16 77.00
74.47E
74.47W

17 76.00
72.97E
71.27W

18 73.00
70.47E
69.50W

19 71.00
68.17E
67.12W

PNP: 63.05

REVISION No.2 MARCH, 2005

CITY OF OTTAWA
GLOUCESTER EUC INFRASTRUCTURE
SERVICING STUDY UPDATE

SANITARY SEWER SYSTEM

Scale: 0 40 80 120 200m

Drawn By: E.C. Date: 04.10.20 Revision: 2

SAN

APPENDIX D
Stormwater Management Calculations
Supporting Documents
Hydrovex ICD
Stormtech Chaber Details



LRL Associates Ltd.
Storm Watershed Summary



LRL File No. 210216-02
Project: Stacked Townhouses
Location: 6001/6005 RENAUD
Date: June 9, 2023
Designed: K. Herold
Drawing Reference: C701/C702

Pre-Development Catchments

WATERSHED	C = 0.2	C = 0.80	C = 0.90	Total Area (m ²)	Total Area (ha)	Combined C
EWS-01	2273.0	0.0	641.4	2914.4	0.291	0.35
TOTAL	2273.0	0.0	641.4	2914.4	0.291	0.35

Post-Development Catchments

WATERSHED	C = 0.20	C = 0.80	C = 0.90	Total Area (m ²)	Total Area (ha)	Combined C
WS-01 (UNCONTROLLED)	275.6	0.0	154.8	430.4	0.043	0.45
WS-02 (UNCONTROLLED)	54.5	0.0	96.9	151.4	0.015	0.65
WS-03 (CONTROLLED)	549.0	0.0	1783.6	2332.6	0.233	0.74
TOTAL	879.1	0.0	2035.3	2914.4	0.291	0.66



LRL File No. 200817
 Project: 8201-0005 RENALD
 Location: Hwy 17 at Old Hwy 17, Rockland
 Date: April 13, 2021
 Designed: Amy Salem
 Drawing Ref.: C.601

Stormwater Management
 100-Year Design Sheet

Runoff Equation

Q = 2.76C₁A (L/s)
 C = Runoff coefficient
 I = Rainfall intensity (mm/hr) = A / (T_c + C)^{0.5}
 A = Area (ha)
 T_c = Time of concentration (min)

Pre-development Stormwater Management

Total Area = 0.291 ha
 Allowable Release Rate: 24.37 L/s *Per pre-allocated release rate of 85L/s/ha as per EUC Master Servicing Study (Stantec 2005)

Post-development Stormwater Management

	Total Site Area =	0.291	ha	Y ₁₀	Y ₁₀₀	Y ₁₀	Y ₁₀₀
Controlled	WS-03	0.233	ha	R _c	R _c	0.74	0.92
	Total Controlled =	0.233	ha	Y ₁₀	Y ₁₀₀	0.74	0.92
Un-controlled	WS-01, 02	0.058	ha	R _u	R _u	0.50	0.63
	Total Un-controlled =	0.058	ha	Y ₁₀	Y ₁₀₀	0.50	0.63

Post-development Stormwater Management (Uncontrolled Catchment WS-01)

100 Year Storm Event:
 $L_{100} = 1735.688 / (T_d + 6.514)^{0.88}$ a = 1735.688 b = 0.820 C = 6.014

Time (min)	Intensity (mm/hr)	Uncontrolled Runoff (L/s)	Controlled Release Rate Constant (L/s)	Total Release Rate (L/s)
10	173.8	11.15	0.00	11.15

Post-development Stormwater Management (WS-02)

100 Year Storm Event:
 $L_{100} = 1735.688 / (T_d + 6.514)^{0.88}$ a = 1735.688 b = 0.820 C = 6.014

Time (min)	Intensity (mm/hr)	Storage Required		Controlled Release Rate Constant (L/s)	Uncontrolled Runoff (L/s)	Total Release Rate (L/s)
		Controlled Runoff (L/s)	Storage Volume (m ³)			
10	173.8	106.62	59.88	6.62	0.00	6.62
15	142.4	85.16	79.89	6.62	0.00	6.62
20	120.0	71.49	77.84	6.62	0.00	6.62
25	103.8	61.89	80.91	6.62	0.00	6.62
30	91.8	54.75	86.64	6.62	0.00	6.62
40	75.1	44.78	91.60	6.62	0.00	6.62
50	64.0	38.12	94.49	6.62	0.00	6.62
60	55.0	33.21	96.01	6.62	0.00	6.62
75	47.3	28.15	96.94	6.62	0.00	6.62
90	41.1	24.50	96.68	6.62	0.00	6.62
100	36.5	21.75	96.30	6.62	0.00	6.62
120	32.0	19.60	95.49	6.62	0.00	6.62
140	28.0	17.87	94.31	6.62	0.00	6.62
160	25.0	16.44	93.57	6.62	0.00	6.62
180	23.0	15.25	93.06	6.62	0.00	6.62
200	22.0	14.19	92.77	6.62	0.00	6.62

Post-development Stormwater Management (WS-03)

Stormwater Storage Calculations: 11.2 release rate for 100 storage & variable design head

100 Year Storm Event:
 $L_{100} = 1735.688 / (T_d + 6.514)^{0.88}$ a = 1735.688 b = 0.820 C = 6.014

Time (min)	Intensity (mm/hr)	Storage Required		Controlled Release Rate Constant (L/s)	Uncontrolled Runoff (L/s)	Total Release Rate (L/s)
		Controlled Runoff (L/s)	Storage Volume (m ³)			
10	173.8	106.42	61.88	3.31	0.00	3.31
15	142.0	85.43	73.67	3.31	0.00	3.31
20	120.0	71.49	81.81	3.31	0.00	3.31
25	103.8	61.89	87.67	3.31	0.00	3.31
30	91.8	54.75	92.09	3.31	0.00	3.31
40	75.1	44.78	95.54	3.31	0.00	3.31
50	64.0	38.12	100.42	3.31	0.00	3.31
60	55.0	33.21	106.01	3.31	0.00	3.31
75	47.3	28.15	111.94	3.31	0.00	3.31
90	41.1	24.50	114.43	3.31	0.00	3.31
100	36.5	21.75	116.19	3.31	0.00	3.31
120	32.0	19.60	117.38	3.31	0.00	3.31
140	28.0	17.87	118.14	3.31	0.00	3.31
160	25.0	16.44	118.75	3.31	0.00	3.31
180	23.0	15.25	119.10	3.31	0.00	3.31
200	22.0	14.19	119.49	3.31	0.00	3.31

Total Storage Required = 118.35 m³ refer to LRL Plan C.601
 Available Storage = 128.00 m³

Summary of release Rates and Storage Volumes

Catchment Area	Drainage Area (ha)	100-year Release Rate (L/s)	100-Year Required Storage (m ³)	Total Available Storage (m ³)
WS-01	0.058	3.63	0	128.00
WS-02	0.233	6.62	118.35	128.00
WS-03	0.291	24.37	118.35	128.00

LRL Associates Ltd.
Storm Design Sheet



LRL File No. 210216-02
Project: 36 Stacked Towns
Location: 6001/6005 RENAUD
Date: June 9, 2023
Designed: K. Herold
Drawing Reference: C401

Storm Design Parameters

Rational Method $Q = 2.78CIA$

Q = Peak flow in litres per second (L/s)
A = Drainage area in hectares (ha)
C = Runoff coefficient
I = Rainfall intensity (mm/hr)

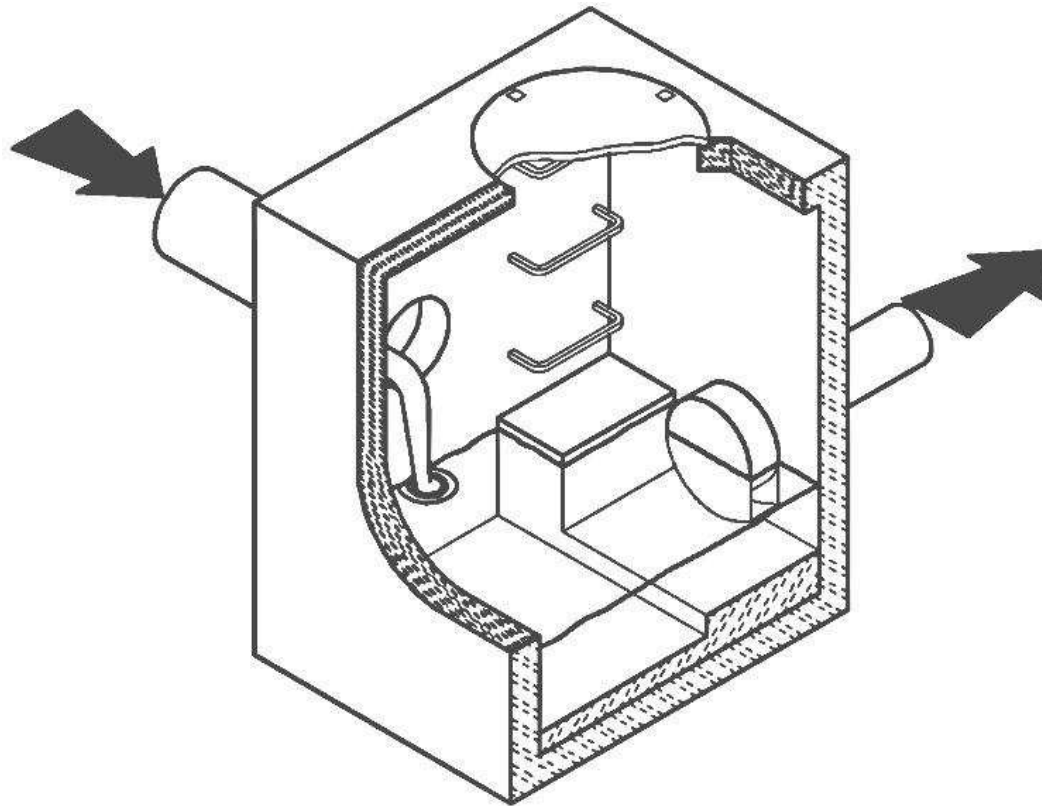
Runoff Coefficient (C)
Grass 0.20
Gravel 0.80
Asphalt / rooftop 0.90

Ottawa Macdonald-Cartier International Airport IDF curve
equation (5 year event, intensity in mm/hr)
 $I = 998.071 / (T_c + 6.053)^{0.814}$
Min. velocity = 0.80 m/s
Manning's "n" = 0.013

LOCATION			AREA (ha)			FLOW						STORM SEWER							
WATERSHED / STREET	From MH	To MH	C = 0.20	C = 0.80	C = 0.90	Indiv. 2.78AC	Accum. 2.78AC	Time of Conc. (min.)	Rainfall Intensity (mm/hr)	Peak Flow Q (L/s)	Controlled Flow Q (L/s)	Pipe Diameter (mm)	Type	Slope (%)	Length (m)	Capacity Full (L/s)	Velocity Full (m/s)	Time of Flow (min.)	Ratio (Q/Q _{FULL})
WS-02	CB06	CBMH05	0.011	0.000	0.003	0.014	0.01	10.00	104.2	1.42		250	PVC	1.00%	16.5	59.5	1.21	0.23	0.02
	CBMH05	CBMH04	0.017	0.000	0.081	0.212	0.23	10.23	103.0	23.25		250	PVC	1.00%	35.5	59.5	1.21	0.49	0.39
	CBMH04	MH03	0.015	0.000	0.079	0.206	0.43	10.72	100.6	43.42		250	PVC	1.00%	17.8	59.5	1.21	0.24	0.73
	MH03	CBMH02	0.012	0.000	0.016	0.047	0.48	10.96	99.4	47.55		250	PVC	1.00%	9.2	59.5	1.21	0.13	0.80
	CBMH02	MH01	0.000	0.000	0.000	0.000	0.48	11.09	98.8	47.26		250	PVC	1.00%	13.3	59.5	1.21	0.18	0.79
	MH01	SEWER	0.000	0.000	0.000	0.000	0.48	11.27	97.9	46.85	6.62	250	PVC	1.00%	21.5	59.5	1.21	0.30	0.79



HYDROVEX[®] VHV / SVHV
Vertical Vortex Flow Regulator



JOHN MEUNIER

HYDROVEX® VHV / SVHV VERTICAL VORTEX FLOW REGULATOR

APPLICATIONS

One of the major problems of urban wet weather flow management is the runoff generated after a heavy rainfall. During a storm, uncontrolled flows may overload the drainage system and cause flooding. Due to increased velocities, sewer pipe wear is increased dramatically and results in network deterioration. In a combined sewer system, the wastewater treatment plant may also experience significant increases in flows during storms, thereby losing its treatment efficiency.

A simple means of controlling excessive water runoff is by controlling excessive flows at their origin (manholes). **John Meunier Inc.** manufactures the **HYDROVEX® VHV / SVHV** line of vortex flow regulators to control stormwater flows in sewer networks, as well as manholes.

The vortex flow regulator design is based on the fluid mechanics principle of the forced vortex. This grants flow regulation without any moving parts, thus reducing maintenance. The operation of the regulator, depending on the upstream head and discharge, switches between orifice flow (gravity flow) and vortex flow. Although the concept is quite simple, over 12 years of research have been carried out in order to get a high performance.

The **HYDROVEX® VHV / SVHV** Vertical Vortex Flow Regulators (**refer to Figure 1**) are manufactured entirely of stainless steel, and consist of a hollow body (1) in which flow control takes place and an outlet orifice (7). Two rubber "O" rings (3) seal and retain the unit inside the outlet pipe. Two stainless steel retaining rings (4) are welded on the outlet sleeve to ensure that there is no shifting of the "O" rings during installation and use.

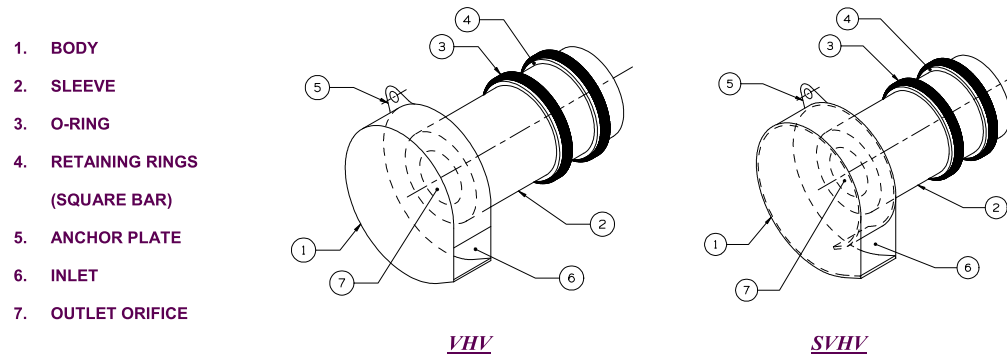


FIGURE 1: HYDROVEX® VHV-SVHV VERTICAL VORTEX FLOW REGULATORS

ADVANTAGES

- The **HYDROVEX® VHV / SVHV** line of flow regulators are manufactured entirely of stainless steel, making them durable and corrosion resistant.
- Having no moving parts, they require minimal maintenance.
- The geometry of the **HYDROVEX® VHV / SVHV** flow regulators allows a control equal to an orifice plate, having a cross section area 4 to 6 times smaller. This decreases the chance of blockage of the regulator, due to sediments and debris found in stormwater flows. **Figure 2** illustrates the comparison between a regulator model 100 SVHV-2 and an equivalent orifice plate. One can see that for the same height of water, the regulator controls a flow approximately four times smaller than an equivalent orifice plate.
- Installation of the **HYDROVEX® VHV / SVHV** flow regulators is quick and straightforward and is performed after all civil works are completed.
- Installation requires no special tools or equipment and may be carried out by any contractor.
- Installation may be carried out in existing structures.

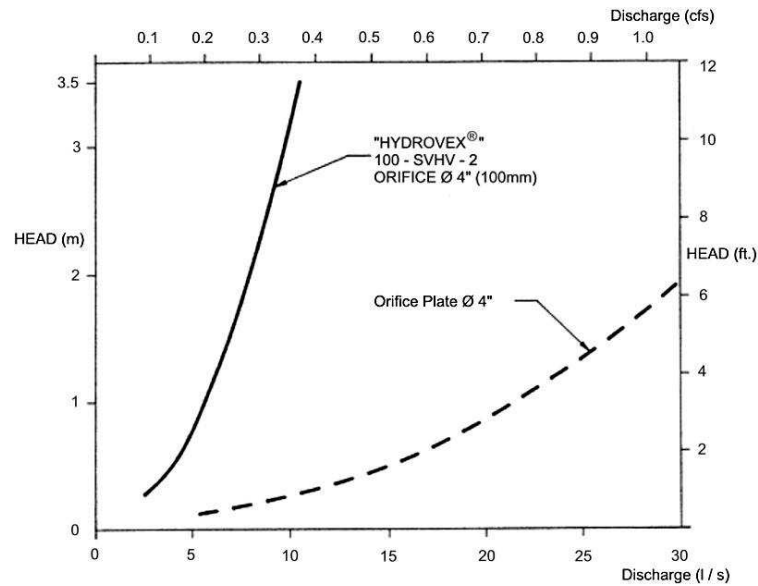


FIGURE 2: DISCHARGE CURVE SHOWING A HYDROVEX® FLOW REGULATOR VS AN ORIFICE PLATE

SELECTION

Selection of a VHV or SVHV regulator can be easily made using the selection charts found at the back of this brochure (see Figure 3). These charts are a graphical representation of the maximum upstream water pressure (head) and the maximum discharge at the manhole outlet. The maximum design head is the difference between the maximum upstream water level and the invert of the outlet pipe. All selections should be verified by John Meunier Inc. personnel prior to fabrication.

Example:

- ✓ Maximum design head 2m (6,56 ft.)
- ✓ Maximum discharge 6 L/s (0.2 cfs)
- ✓ Using Figure 3 - VHV model required is a 75 VHV-1

INSTALLATION REQUIREMENTS

All HYDROVEX® VHV / SVHV flow regulators can be installed in circular or square manholes. Figure 4 gives the various minimum dimensions required for a given regulator. *It is imperative to respect the minimum clearances shown to ensure easy installation and proper functioning of the regulator.*

SPECIFICATIONS

In order to specify a **HYDROVEX**[®] regulator, the following parameters must be defined:

- The model number (ex: 75-VHV-1)
- The diameter and type of outlet pipe (ex: 6" diam. SDR 35)
- The desired discharge (ex: 6 l/s or 0.21 CFS)
- The upstream head (ex: 2 m or 6.56 ft.) *
- The manhole diameter (ex: 36" diam.)
- The minimum clearance "H" (ex: 10 inches)
- The material type (ex: 304 s/s, 11 Ga. standard)

* *Upstream head is defined as the difference in elevation between the maximum upstream water level and the invert of the outlet pipe where the **HYDROVEX**[®] flow regulator is to be installed.*

PLEASE NOTE THAT WHEN REQUESTING A PROPOSAL, WE SIMPLY REQUIRE THAT YOU PROVIDE US WITH THE FOLLOWING:

- *project design flow rate*
- *pressure head*
- *chamber's outlet pipe diameter and type*



Typical VHV model in factory

OPTIONS



VHV-1-O (standard model with odour control inlet)



FV-SVHV (mounted on sliding plate)



FV-VHV-O (mounted on sliding plate with odour control inlet)



VHV with Gooseneck assembly in existing chamber without minimum release at the bottom



VHV with air vent for minimal slopes



VHV Vertical Vortex Flow Regulator

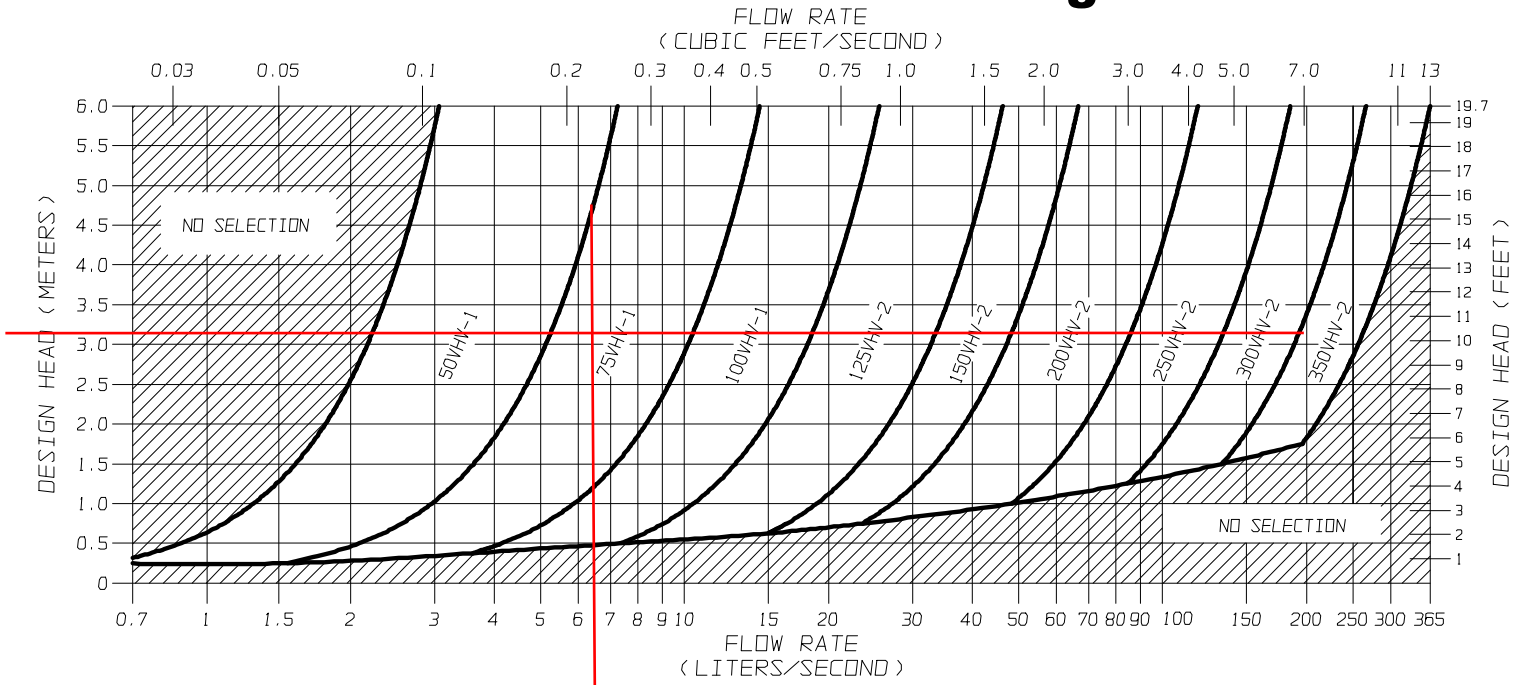


FIGURE 3 - VHV

JOHN MEUNIER



SVHV Vertical Vortex Flow Regulator

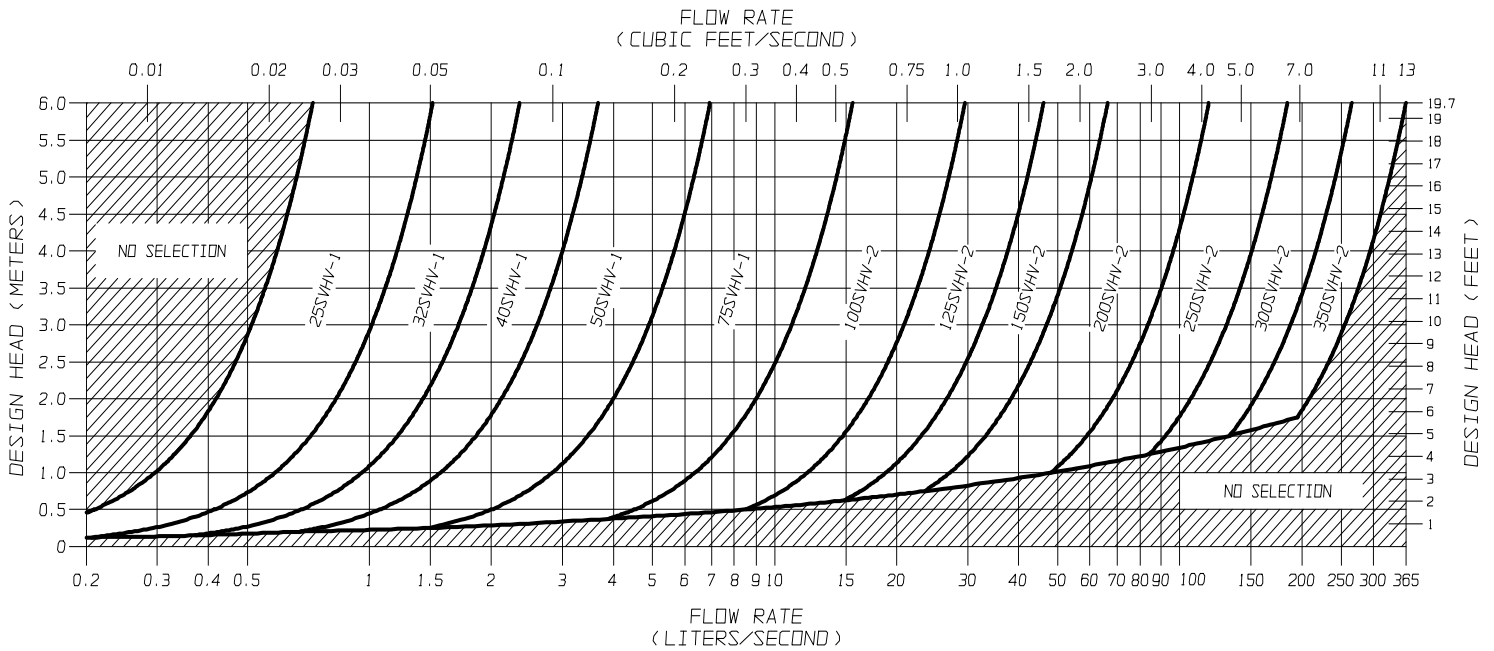
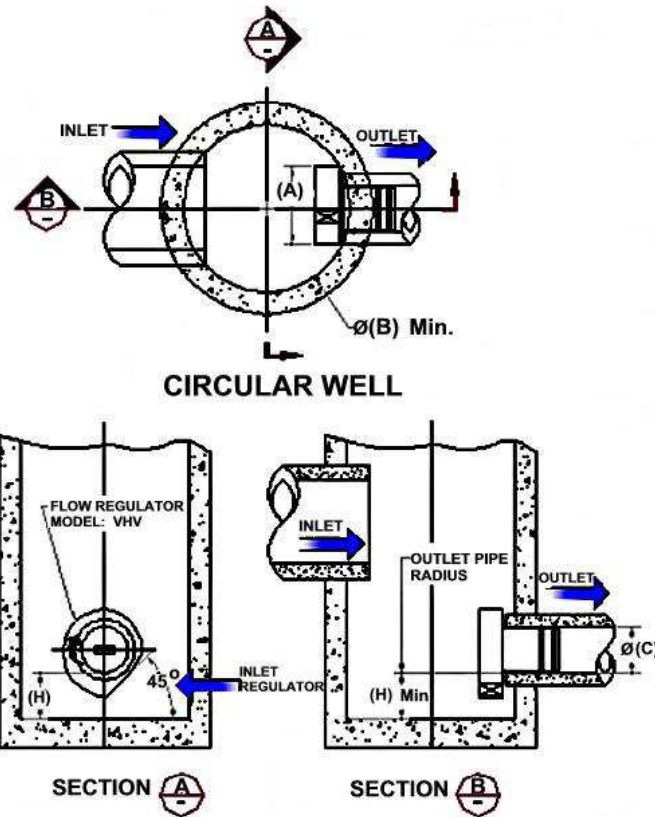


FIGURE 3 - SVHV

JOHN MEUNIER

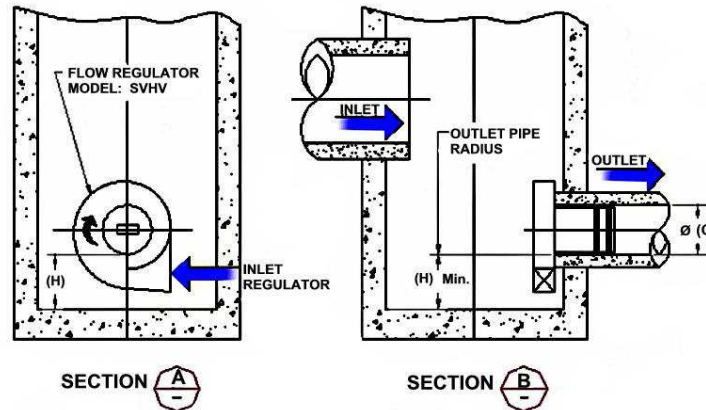
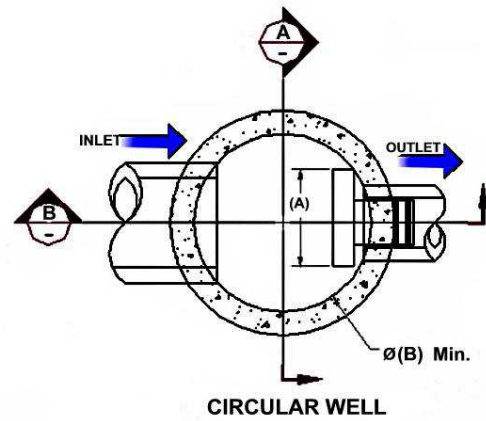
FLOW REGULATOR TYPICAL INSTALLATION IN CIRCULAR MANHOLE
FIGURE 4 (MODEL VHV)

Model Number	Regulator Diameter		Minimum Manhole Diameter		Minimum Outlet Pipe Diameter		Minimum Clearance	
	A (mm)	A (in.)	B (mm)	B (in.)	C (mm)	C (in.)	H (mm)	H (in.)
50VHV-1	150	6	600	24	150	6	150	6
75VHV-1	250	10	600	24	150	6	150	6
100VHV-1	325	13	900	36	150	6	200	8
125VHV-2	275	11	900	36	150	6	200	8
150VHV-2	350	14	900	36	150	6	225	9
200VHV-2	450	18	1200	48	200	8	300	12
250VHV-2	575	23	1200	48	250	10	350	14
300VHV-2	675	27	1600	64	250	10	400	16
350VHV-2	800	32	1800	72	300	12	500	20



**FLOW REGULATOR TYPICAL INSTALLATION IN CIRCULAR MANHOLE
FIGURE 4 (MODEL SVHV)**

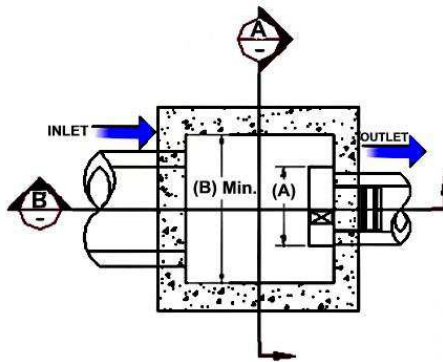
Model Number	Regulator Diameter		Minimum Manhole Diameter		Minimum Outlet Pipe Diameter		Minimum Clearance	
	A (mm)	A (in.)	B (mm)	B (in.)	C (mm)	C (in.)	H (mm)	H (in.)
25 SVHV-1	125	5	600	24	150	6	150	6
32 SVHV-1	150	6	600	24	150	6	150	6
40 SVHV-1	200	8	600	24	150	6	150	6
50 SVHV-1	250	10	600	24	150	6	150	6
75 SVHV-1	375	15	900	36	150	6	275	11
100 SVHV-2	275	11	900	36	150	6	250	10
125 SVHV-2	350	14	900	36	150	6	300	12
150 SVHV-2	425	17	1200	48	150	6	350	14
200 SVHV-2	575	23	1600	64	200	8	450	18
250 SVHV-2	700	28	1800	72	250	10	550	22
300 SVHV-2	850	34	2400	96	250	10	650	26
350 SVHV-2	1000	40	2400	96	250	10	700	28



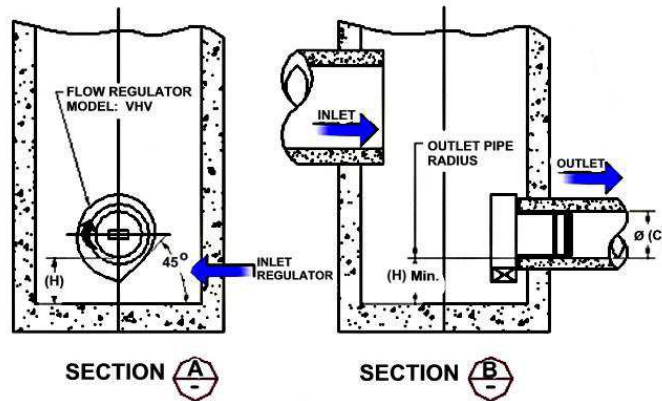
FLOW REGULATOR TYPICAL INSTALLATION IN SQUARE MANHOLE
FIGURE 4 (MODEL VHV)

Model Number	Regulator Diameter		Minimum Chamber Width		Minimum Outlet Pipe Diameter		Minimum Clearance	
	A (mm)	A (in.)	B (mm)	B (in.)	C (mm)	C (in.)	H (mm)	H (in.)
50VHV-1	150	6	600	24	150	6	150	6
75VHV-1	250	10	600	24	150	6	150	6
100VHV-1	325	13	600	24	150	6	200	8
125VHV-2	275	11	600	24	150	6	200	8
150VHV-2	350	14	600	24	150	6	225	9
200VHV-2	450	18	900	36	200	8	300	12
250VHV-2	575	23	900	36	250	10	350	14
300VHV-2	675	27	1200	48	250	10	400	16
350VHV-2	800	32	1200	48	300	12	500	20

NOTE: *In the case of a square manhole, the outlet flow pipe must be centered on the wall to ensure enough clearance for the unit.*



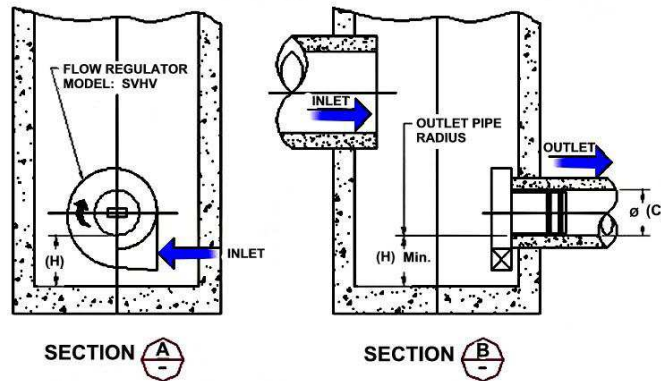
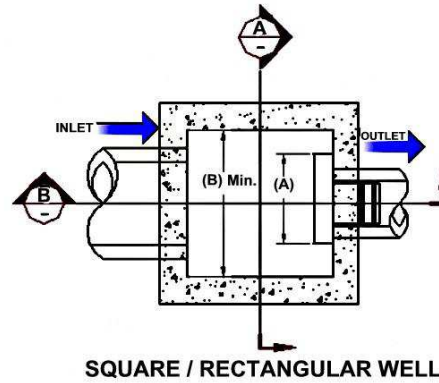
SQUARE / RECTANGULAR WELL



**FLOW REGULATOR TYPICAL INSTALLATION IN SQUARE MANHOLE
FIGURE 4 (MODEL SVHV)**

Model Number	Regulator Diameter		Minimum Chamber Width		Minimum Outlet Pipe Diameter		Minimum Clearance	
	A (mm)	A (in.)	B (mm)	B (in.)	C (mm)	C (in.)	H (mm)	H (in.)
25 SVHV-1	125	5	600	24	150	6	150	6
32 SVHV-1	150	6	600	24	150	6	150	6
40 SVHV-1	200	8	600	24	150	6	150	6
50 SVHV-1	250	10	600	24	150	6	150	6
75 SVHV-1	375	15	600	24	150	6	275	11
100 SVHV-2	275	11	600	24	150	6	250	10
125 SVHV-2	350	14	600	24	150	6	300	12
150 SVHV-2	425	17	600	24 <td 150	6	350	14	
200 SVHV-2	575	23	900	36	200	8	450	18
250 SVHV-2	700	28	900	36	250	10	550	22
300 SVHV-2	850	34	1200	48	250	10	650	26
350 SVHV-2	1000	40	1200	48	250	10	700	28

NOTE: *In the case of a square manhole, the outlet flow pipe must be centered on the wall to ensure enough clearance for the unit.*



INSTALLATION

The installation of a **HYDROVEX**[®] regulator may be undertaken once the manhole and piping is in place. Installation consists of simply fitting the regulator into the outlet pipe of the manhole. **John Meunier Inc.** recommends the use of a lubricant on the outlet pipe, in order to facilitate the insertion and orientation of the flow controller.

MAINTENANCE

HYDROVEX[®] regulators are manufactured in such a way as to be maintenance free; however, a periodic inspection (every 3-6 months) is suggested in order to ensure that neither the inlet nor the outlet has become blocked with debris. The manhole should undergo periodically, particularly after major storms, inspection and cleaning as established by the municipality

GUARANTY

The **HYDROVEX**[®] line of **VHV / SVHV** regulators are guaranteed against both design and manufacturing defects for a period of 5 years. Should a unit be defective, **John Meunier Inc.** is solely responsible for either modification or replacement of the unit.

John Meunier Inc.

ISO 9001 : 2008

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Revised: 2011-05-03

User Inputs

Chamber Model:	MC-3500
Outlet Control Structure:	No
Project Name:	6001/6005 Renaud
Engineer:	N/A
Project Location:	Ontario
Measurement Type:	Metric
Required Storage Volume:	102.01 cubic meters.
Stone Porosity:	40%
Stone Foundation Depth:	229 mm.
Stone Above Chambers:	305 mm.
Average Cover Over Chambers:	458 mm.
Design Constraint Dimensions:	(6.10 m. x 25.00 m.)

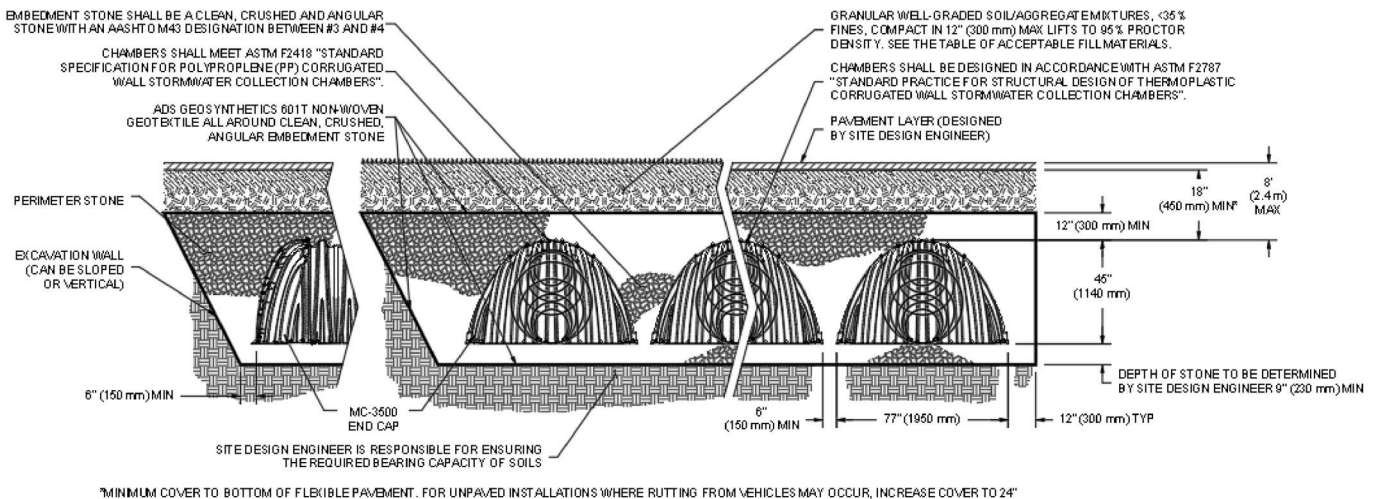
Results

System Volume and Bed Size

Installed Storage Volume:	111.11 cubic meters.
Storage Volume Per Chamber:	3.12 cubic meters.
Number Of Chambers Required:	19
Number Of End Caps Required:	4
Chamber Rows:	2
Maximum Length:	24.80 m.
Maximum Width:	4.68 m.
Approx. Bed Size Required:	111.28 square meters.








System Components

Amount Of Stone Required:	126 cubic meters
Volume Of Excavation (Not Including Fill):	187 cubic meters
Total Non-woven Geotextile Required:	386 square meters
Woven Geotextile Required (excluding Isolator Row):	14 square meters
Woven Geotextile Required (Isolator Row):	74 square meters
Total Woven Geotextile Required:	88 square meters
Impervious Liner Required:	0 square meters





SUBJECT SITE

-  FUTURE ROADS
-  AREAS WHERE FLOW IS DIVERTED TO ADJACENT SUB-WATERSHED
-  DRY POND WHICH REQUIRES EXCAVATION
-  DRY POND USING NATURAL DEPRESSIONS / RAVINES
-  STORMWATER FLOW ROUTE
-  POND TRIBUTARY AREA
-  SUB-WATERSHED BOUNDARY

PLAN IS TAKEN FROM THE CITY OF GLOUCESTER, EAST URBAN COMMUNITY, MASTER DRAINAGE PLAN BY GORE & STORRIE LIMITED, DATED SEPT. 1991.

RECOMMENDED SWM POND LOCATIONS EAST URBAN COMMUNITY City of Ottawa

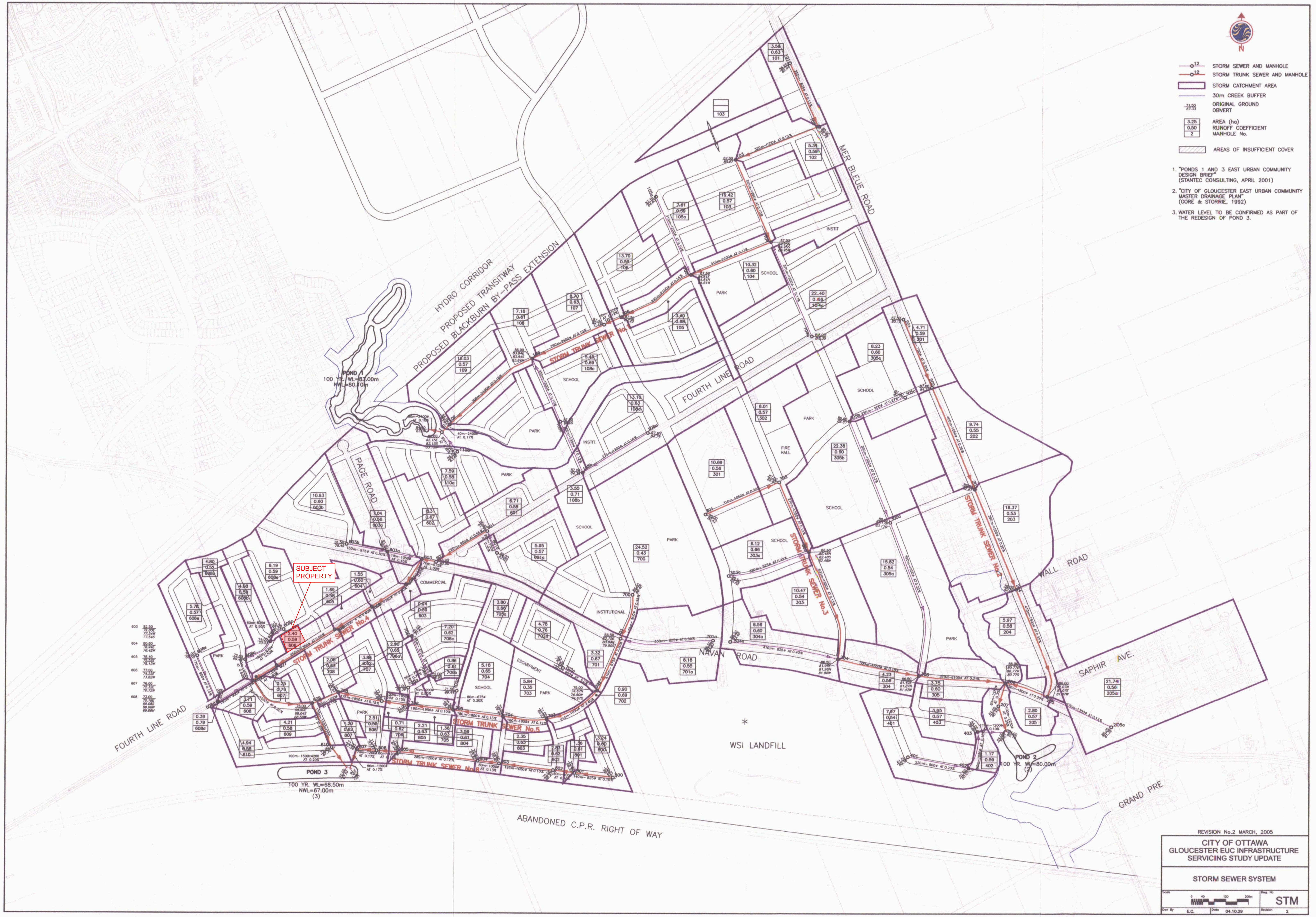


Figure 6



- STORM SEWER AND MANHOLE
- STORM TRUNK SEWER AND MANHOLE
- STORM CATCHMENT AREA
- 30m CREEK BUFFER
- ORIGINAL GROUND OBVERT
- AREA (ha)
RUNOFF COEFFICIENT
MANHOLE No.
- AREAS OF INSUFFICIENT COVER

1. "PONDS 1 AND 3 EAST URBAN COMMUNITY DESIGN BRIEF" (STANTEC CONSULTING, APRIL 2001)
2. "CITY OF GLOUCESTER EAST URBAN COMMUNITY MASTER DRAINAGE PLAN" (GORE & STORRIE, 1992)
3. WATER LEVEL TO BE CONFIRMED AS PART OF THE REDESIGN OF POND 3.



SUBJECT PROPERTY

100 YR. WL=63.00m
NWL=60.10m

100 YR. WL=68.50m
NWL=67.00m
(3)

REVISION No.2 MARCH, 2005

CITY OF OTTAWA
GLOUCESTER EUC INFRASTRUCTURE
SERVICING STUDY UPDATE

STORM SEWER SYSTEM

Scale: 1:1000

Drawn By: E.C. Date: 04.10.29 Revision: 2

STM

APPENDIX E
Civil Engineering Drawings



NAVAN STACKED TOWN HOMES 6001 / 6005 RENAUD ROAD, OTTAWA, ON.

REVISION 02



KEY PLAN (N.T.S.)

DRAWING INDEX	
TITLE PAGE	
GENERAL NOTES	C001
SEDIMENT AND EROSION CONTROL PLAN	C101
DEMOLITION PLAN	C102
SITE DEVELOPMENT PLAN	C201
GRADING AND DRAINAGE PLAN	C301
SERVICING PLAN	C401
STORMWATER MANAGEMENT PLAN	C601
PRE-DEVELOPMENT WATERSHED PLAN	C701
POST-DEVELOPMENT WATERSHED PLAN	C702
CONSTRUCTION DETAIL PLAN 1/2	C901
CONSTRUCTION DETAIL PLAN 2/2	C902



LRJ

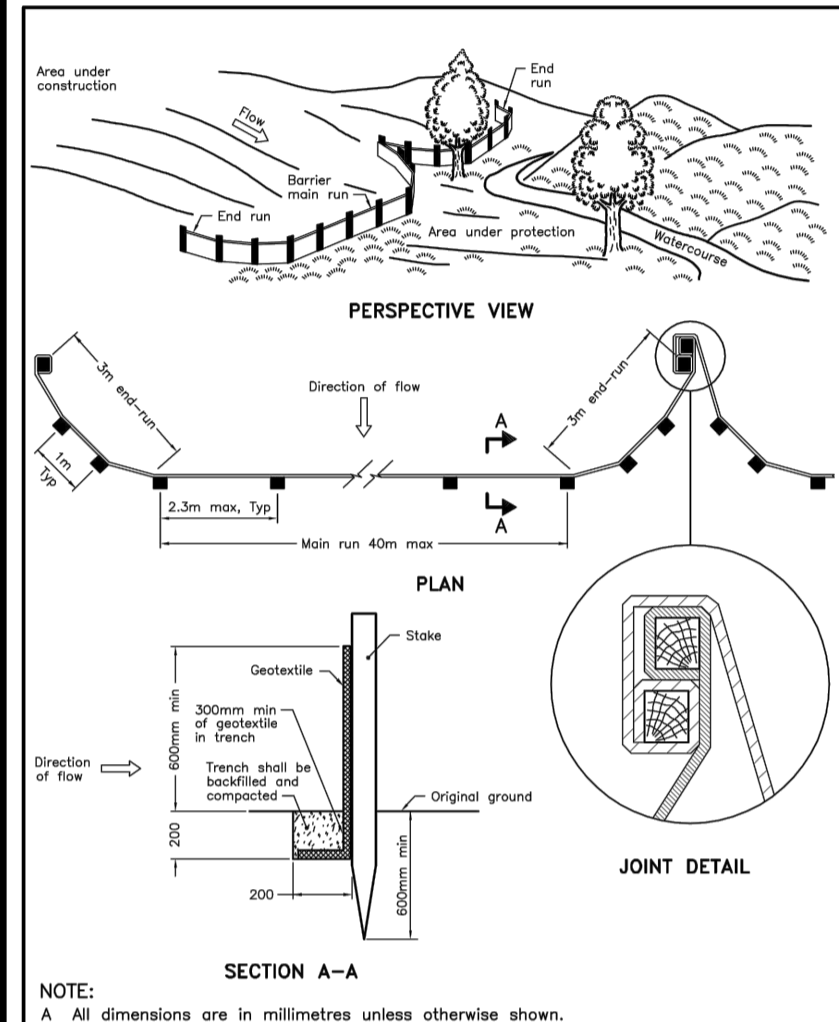
ENGINEERING | INGÉNIERIE

5430 Canotek Road | Ottawa, ON, K1J 9G2
www.lrl.ca | (613) 842-3434

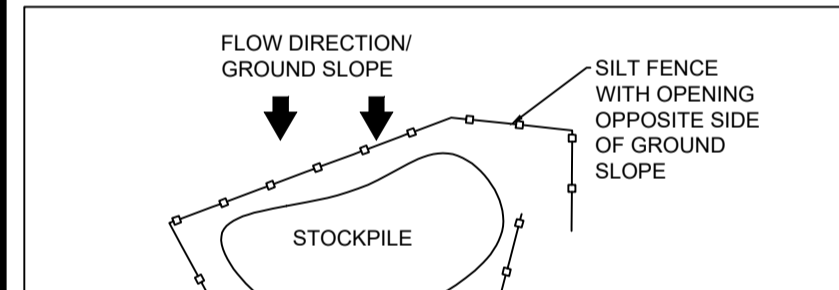
NAVAN STACKED TOWN HOMES
6001/6005 RENAUD ROAD, OTTAWA, ON.
REV.02 - ISSUED FOR CLIENT APPROVAL - JUNE 9, 2023
LRL PROJECT no: 210216-02



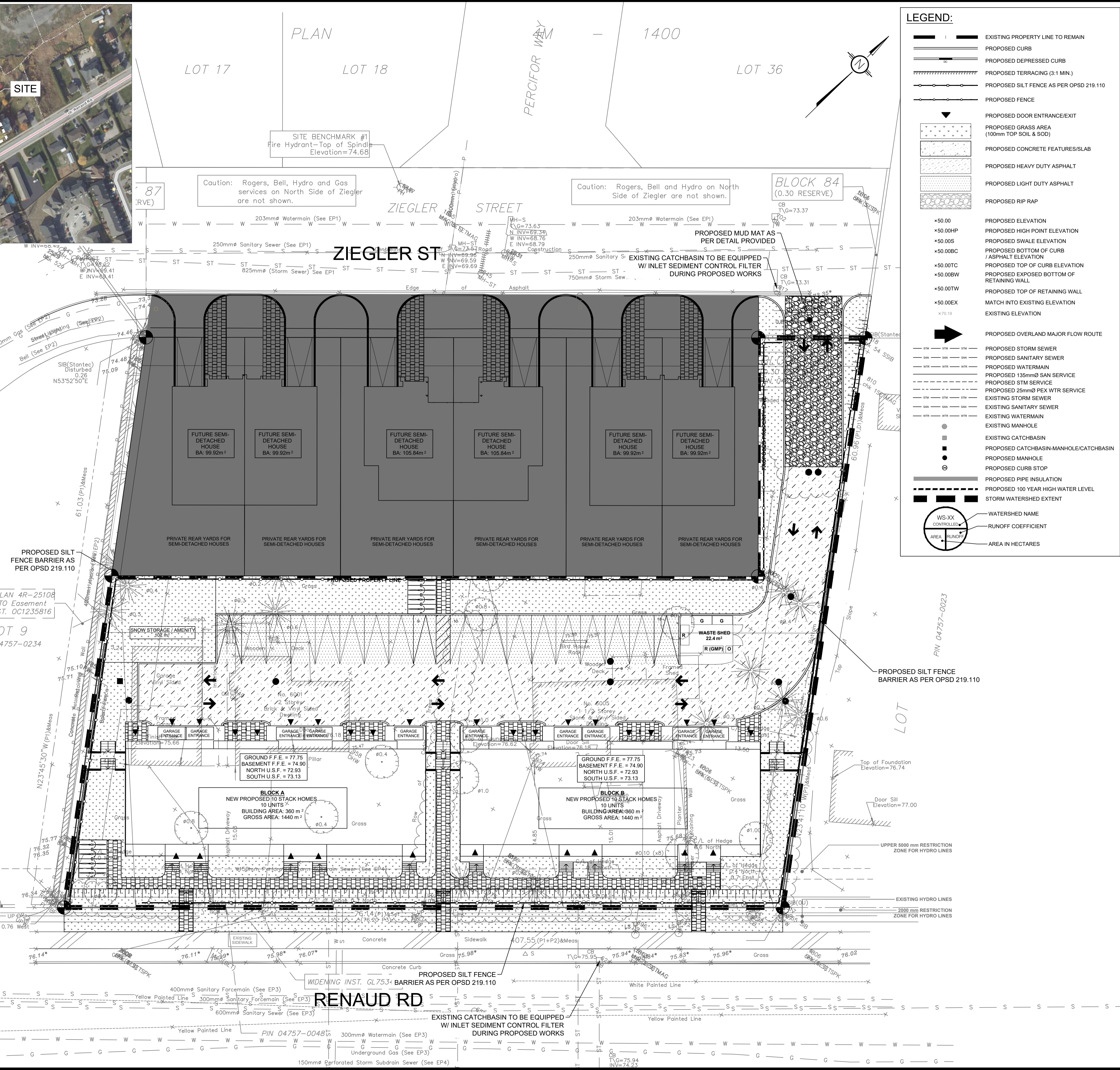
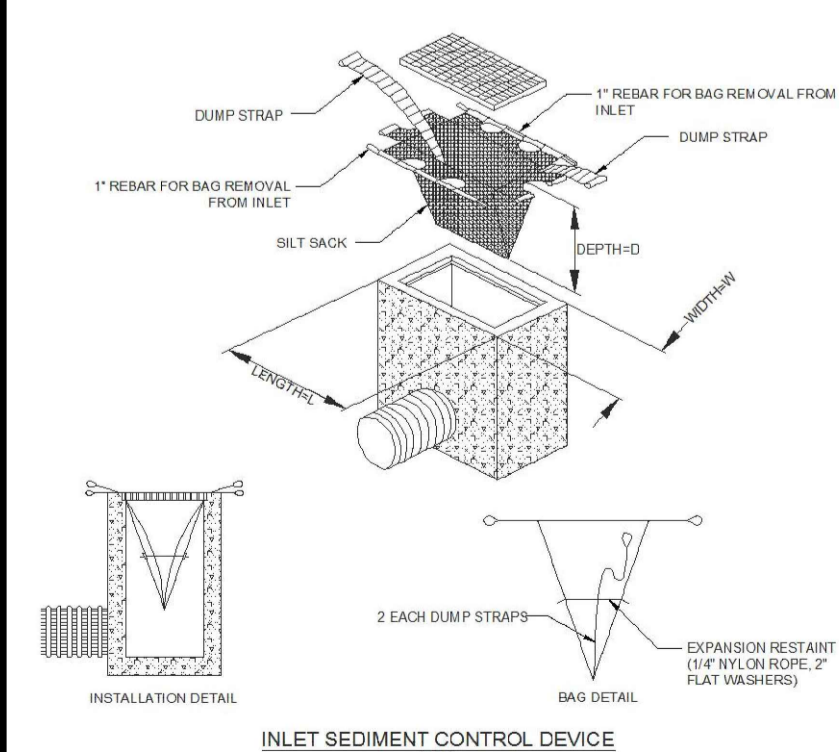
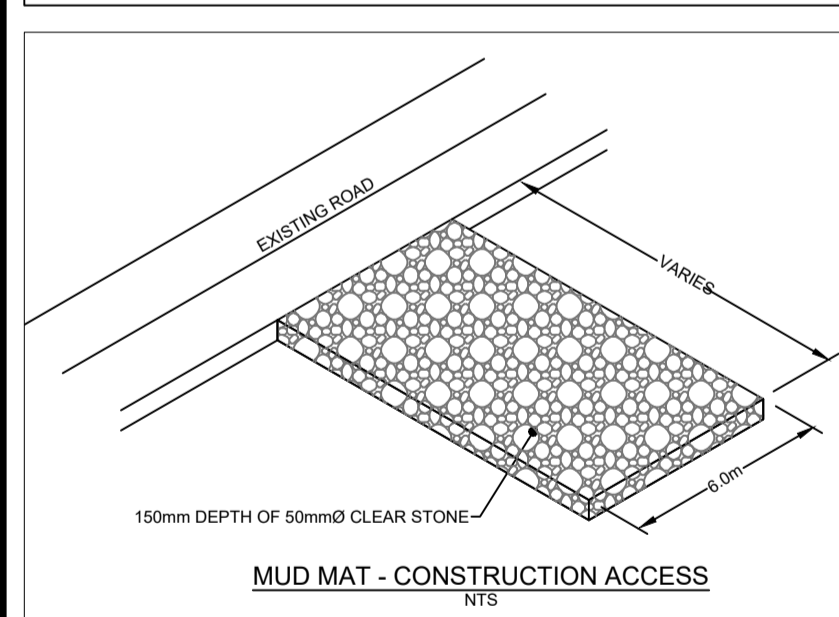
NOT AUTHENTIC UNLESS SIGNED AND DATED



ONTARIO PROVINCIAL STANDARD DRAWING	Nov 2015	Rev 2
LIGHT-DUTY SILT FENCE BARRIER	OPSD 219.110	



STOCKPILE EROSION PROTECTION
N.T.S.



LEGEND:

	EXISTING PROPERTY LINE TO REMAIN
	PROPOSED CURB
	PROPOSED DEPRESSED CURB
	PROPOSED TERRACING (3:1 MIN.)
	PROPOSED SILT FENCE AS PER OPSD 219.110
	PROPOSED FENCE
	PROPOSED DOOR ENTRANCE/EEXIT
	PROPOSED GRASS AREA (100mm TOP SOIL & SOD)
	PROPOSED CONCRETE FEATURES/SLAB
	PROPOSED HEAVY DUTY ASPHALT
	PROPOSED LIGHT DUTY ASPHALT
	PROPOSED RIP RAP
	PROPOSED ELEVATION
	PROPOSED HIGH POINT ELEVATION
	PROPOSED SWALE ELEVATION
	PROPOSED BOTTOM OF CURB / ASPHALT ELEVATION
	PROPOSED TOP OF CURB ELEVATION
	PROPOSED EXPOSED BOTTOM OF RETAINING WALL
	PROPOSED TOP OF RETAINING WALL
	MATCH INTO EXISTING ELEVATION
	EXISTING ELEVATION
	PROPOSED OVERLAND MAJOR FLOW ROUTE
	PROPOSED STORM SEWER
	PROPOSED SANITARY SEWER
	PROPOSED WATERMAIN
	PROPOSED 135mm SAN SERVICE
	PROPOSED STM SERVICE
	PROPOSED 25mm PEX WTR SERVICE
	EXISTING STORM SEWER
	EXISTING SANITARY SEWER
	EXISTING WATERMAIN
	EXISTING MANHOLE
	EXISTING CATCHBASIN
	PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN
	PROPOSED MANHOLE
	PROPOSED CURB STOP
	PROPOSED PIPE INSULATION
	PROPOSED 100 YEAR HIGH WATER LEVEL
	STORM WATERSHED EXTENT
	WATERSHED NAME
	RUNOFF COEFFICIENT
	AREA IN HECTARES

USE AND INTERPRETATION OF DRAWINGS

GENERAL CONDITIONS OF THE CONTRACT FOR CONSTRUCTION ARE PART OF THE CONTRACT DOCUMENTS AND DESCRIBE THE SCOPE AND INTENT OF THE DRAWINGS. THE CONTRACT DOCUMENTS INCLUDE NOT ONLY THE DRAWINGS, BUT ALSO THE OWNER-CONTRACTOR AGREEMENTS, CONDITIONS OF THE CONTRACT, THE SPECIFICATIONS, ADDENDA, AND MODIFICATIONS ISSUED AFTER EXECUTION OF THE CONTRACT. THESE CONTRACT DOCUMENTS ARE COMPLEMENTARY, AND WHAT IS REQUIRED BY ANY ONE SHALL BE BINDING AS REQUIRED BY ALL. WORK NOT COMPLETELY DELINEATED HEREON SHALL BE CONSTRUCTED OF THE SAME MATERIALS AND DETAIL AS SHOWN MORE COMPLETELY ELSEWHERE IN THE CONTRACT DOCUMENTS.

BY USE OF THE DRAWINGS FOR CONSTRUCTION OF THE PROJECT, THE OWNER CONFIRMS THAT HE HAS VISITED THE SITE, FAMILIARIZED HIMSELF WITH THE LOCAL CONDITIONS, VERIFIED FIELD DIMENSIONS AND CORRELATED HIS OBSERVATIONS WITH THE REQUIREMENTS OF THE CONTRACT DOCUMENTS.

AS INSTRUMENTS OF SERVICE, ALL DRAWINGS, SPECIFICATIONS, CAD FILES OR OTHER ELECTRONIC MEDIA AND COPIES THERE OF FURNISHED BY THE ENGINEER ARE HIS PROPERTY. THEY ARE TO BE USED ONLY FOR THE PROJECT AND ARE NOT TO BE USED ON ANY OTHER PROJECT, INCLUDING REPEATS OF THE PROJECT. CHANGES TO THE DRAWINGS MAY ONLY BE MADE BY THE ENGINEER.

UNLESS THE REVISION TITLE IS "ISSUED FOR CONSTRUCTION", THESE DRAWINGS SHALL BE CONSIDERED PRELIMINARY AND SHALL NOT BE USED AS A CONSTRUCTION DOCUMENT.

THESE DRAWINGS ILLUSTRATE THE WORK TO BE DONE. THE ENGINEER IS NOT RESPONSIBLE FOR THE MEANS, METHODS, TECHNIQUES, SEQUENCES AND PROCEDURES USED TO DO THE WORK, OR THE SAFETY ASPECTS OF CONSTRUCTION, AND NOTHING ON THESE DRAWINGS EXPRESSED OR IMPLIED CHANGES THIS CONDITION. CONTRACTOR SHALL DETERMINE ALL CONDITIONS AT THE SITE AND SHALL BE RESPONSIBLE FOR KNOWING HOW THEY AFFECT THE WORK. SUBMITTAL OF A BID TO PERFORM THIS WORK IS ACKNOWLEDGEMENT OF THE RESPONSIBILITIES, AND THAT THEY HAVE BEEN FULLY CONSIDERED IN PLANNING OF THE WORK AND THE BID PRICE. NO CLAIMS FOR EXTRA CHARGES DUE TO THESE CONDITIONS WILL BE FORTHCOMING.

UNAUTHORIZED CHANGES:

IN THE EVENT THE CLIENT, THE CLIENT'S CONTRACTORS OR SUBCONTRACTORS, OR ANYONE FOR WHOM THE CLIENT IS LEGALLY LIABLE MAKES OR PERMITS TO BE MADE ANY CHANGES TO ANY REPORTS, PLANS, SPECIFICATIONS OR OTHER CONSTRUCTION DOCUMENTS PREPARED BY LRI ASSOCIATES LTD. (LRI) WITHOUT OBTAINING LRI'S PRIOR WRITTEN CONSENT, THE CLIENT SHALL ASSUME FULL RESPONSIBILITY FOR THE RESULTS OF SUCH CHANGES. THEREFORE THE CLIENT AGREES TO WAIVE ANY CLAIM AGAINST LRI AND TO RELEASE LRI FROM ANY LIABILITY ARISING, DIRECTLY OR INDIRECTLY, FROM SUCH UNAUTHORIZED CHANGES.

IN ADDITION, THE CLIENT AGREES TO THE FULLEST EXTENT PERMITTED BY LAW, TO INDEMNIFY AND HOLD HARMLESS LRI FROM ANY DAMAGES, LIABILITIES OR COSTS, INCLUDING REASONABLE ATTORNEY'S FEES AND COST OF DEFENSE, ARISING FROM SUCH CHANGES.

IN ADDITION, THE CLIENT AGREES TO INCLUDE IN ANY CONTRACTS FOR CONSTRUCTION APPROPRIATE LANGUAGE THAT PROHIBITS THE CONTRACTOR OR ANY SUBCONTRACTORS, OR ANY TIER FROM MAKING ANY CHANGES OR MODIFICATIONS TO LRI'S CONSTRUCTION DOCUMENTS WITHOUT THE PRIOR WRITTEN APPROVAL OF LRI AND THAT FURTHER REQUIRES THE CONTRACTOR TO INDEMNIFY BOTH LRI AND THE CLIENT FROM ANY LIABILITY OR COST ARISING FROM SUCH CHANGES MADE WITHOUT SUCH PROPER AUTHORIZATION.

GENERAL NOTES:

EXISTING SERVICES AND UTILITIES SHOWN ON THESE DRAWINGS ARE TAKEN FROM THE BEST AVAILABLE RECORDS, BUT MAY NOT BE COMPLETE OR TO DATE. CONTRACTOR SHALL VERIFY IN FIELD FOR LOCATION AND ELEVATION OF PIPES AND CHECK WITH THE UTILITY COMPANIES BEFORE DIGGING OR PERFORMING WORK.

CONTRACTOR IS ADVISED TO COLLECT INFORMATION ON SOIL CONDITIONS BEFORE START OF CONSTRUCTION.

THE ENGINEER WAIVES ANY AND ALL RESPONSIBILITY AND LIABILITY FOR PROBLEMS WHICH ARISE FROM FAILURE TO FOLLOW THESE PLANS, SPECIFICATIONS AND THE DESIGN INTENT THEREIN, CONVEY, OR FOR PROBLEMS WHICH ARISE FROM OTHERS' FAILURE TO OBTAIN AND/OR FOLLOW THE ENGINEER'S GUIDANCE WITH RESPECT TO ANY ERRORS, OMISSIONS, INCONSISTENCIES, AMBIGUITIES OR CONFLICTS WHICH ARE ALLEGED.

CONTRACTOR TO VERIFY ALL DIMENSIONS AND NOTIFY THE ENGINEER OF ANY DISCREPANCIES BEFORE WORK COMMENCES. DO NOT SCALE DRAWINGS.

SCALE: 1:200

5m 2 0 5m

SUBJECT TO APPROVAL

02	ISSUED FOR MUNICIPAL APPROVAL	K.H.	09 JUN 2023
01	ISSUED FOR MUNICIPAL APPROVAL	A.S.	24 DEC 2021
No.	REVISIONS	BY	DATE



NOT AUTHENTIC UNLESS SIGNED AND DATED

LRJ
ENGINEERING | INGENIERIE
5430 Canotek Road | Ottawa, ON, K1J 9G2
www.lri.ca | (613) 842-3434

CLIENT: **LANDRIC HOMES**
1173 CYRILLE RD, SUITE 202,
OTTAWA ON K1J 7S6

DESIGNED BY: K.H. DRAWN BY: K.H. APPROVED BY: J.V.

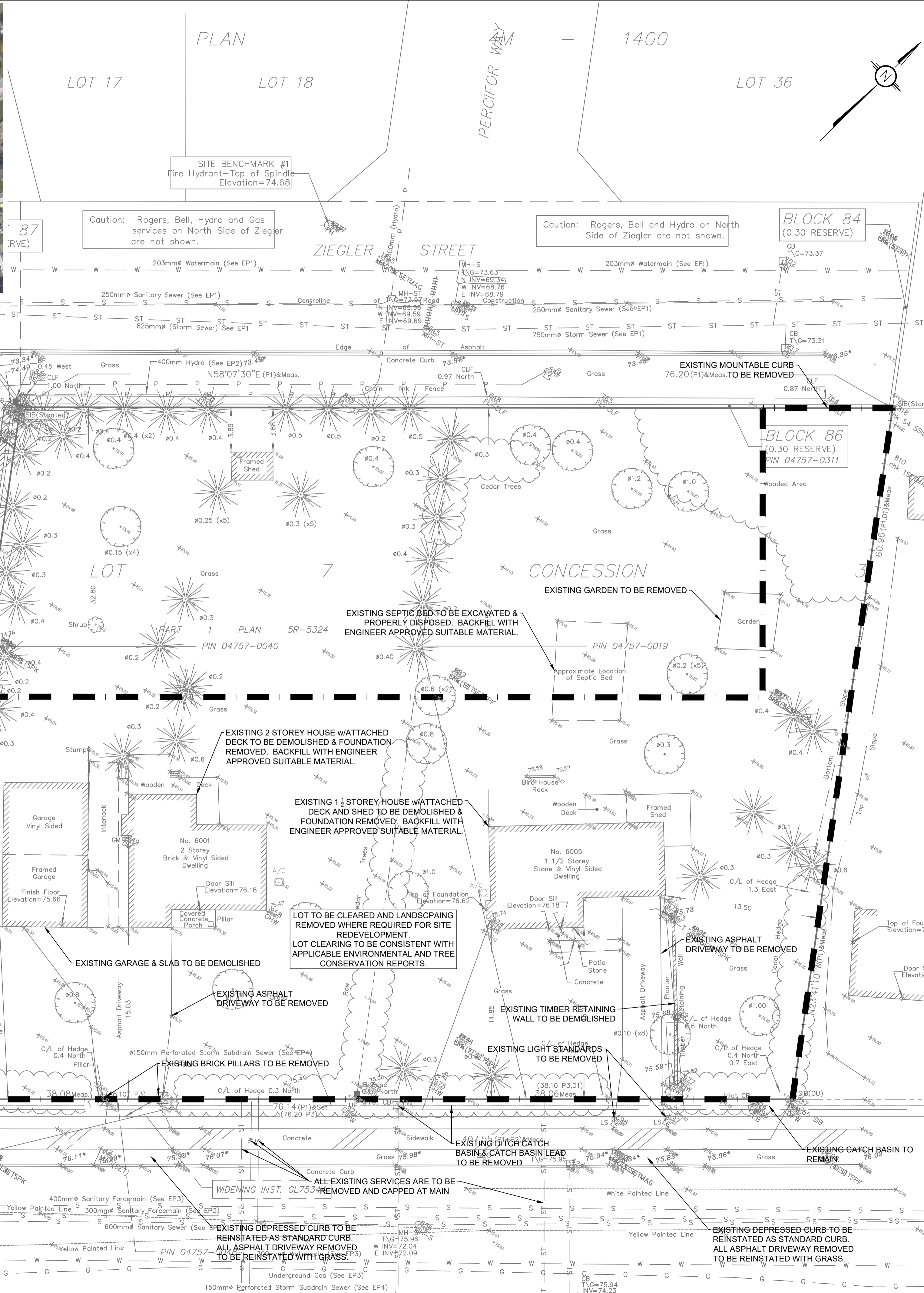
PROJECT: **NAVAN STACKED TOWN HOMES**
6001/6005 RENAUD RD,
OTTAWA, ONTARIO

DRAWING TITLE: **EROSION AND SEDIMENT CONTROL PLAN**

PROJECT NO: 210216
DATE: NOVEMBER 2021

DWG # 18659

CITY FILE # D07-12-21-0239



LEGEND:

- | — EXISTING PROPERTY LINE TO REMAIN
- PROPOSED CURB
- PROPOSED DEPRESSED CURB
- ===== PROPOSED TERRACING (3:1 MIN.)
- | — PROPOSED SILT FENCE AS PER OPSD 219.110
- | — PROPOSED FENCE
- ▼ PROPOSED DOOR ENTRANCE/EXIT
- ▨ PROPOSED GRASS AREA (100mm TOP SOIL & SOD)
- ▨ PROPOSED CONCRETE FEATURES/SLAB
- ▨ PROPOSED HEAVY DUTY ASPHALT
- ▨ PROPOSED LIGHT DUTY ASPHALT
- ▨ PROPOSED RIP RAP
- +50.00P PROPOSED ELEVATION
- +50.00HP PROPOSED HIGH POINT ELEVATION
- +50.00S PROPOSED SWALE ELEVATION
- +50.00BC PROPOSED BOTTOM OF CURB / ASPHALT ELEVATION
- +50.00TC PROPOSED TOP OF CURB ELEVATION
- +50.00BW PROPOSED EXPOSED BOTTOM OF RETAINING WALL
- +50.00TW PROPOSED TOP OF RETAINING WALL
- +50.00EX EXISTING ELEVATION
- PROPOSED OVERLAND MAJOR FLOW ROUTE
- PROPOSED STORM SEWER
- PROPOSED SANITARY SEWER
- PROPOSED WATERMAIN
- PROPOSED 135mm SAN SERVICE
- PROPOSED STM SERVICE
- PROPOSED 25mm PEX WTR SERVICE
- EXISTING STORM SEWER
- EXISTING SANITARY SEWER
- EXISTING WATERMAIN
- EXISTING MANHOLE
- EXISTING CATCHBASIN
- PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN
- PROPOSED MANHOLE
- PROPOSED CURB STOP
- PROPOSED PIPE INSULATION
- PROPOSED 100 YEAR HIGH WATER LEVEL
- STORM WATERSHED EXTENT
- WS-XX WATERSHED NAME
- AREA RUNOFF COEFFICIENT
- AREA IN HECTARES

USE AND INTERPRETATION OF DRAWINGS

GENERAL CONDITIONS OF THE CONTRACT FOR CONSTRUCTION ARE PART OF THE CONTRACT DOCUMENTS AND DESCRIBE USE AND INTENT OF THE DRAWINGS. THE CONTRACT DOCUMENTS INCLUDE NOT ONLY THE DRAWINGS, BUT ALSO THE OWNER-CONTRACTOR AGREEMENTS, CONDITIONS OF THE CONTRACT, THE SPECIFICATIONS, ADDENDA, AND MODIFICATIONS ISSUED AFTER EXECUTION OF THE CONTRACT. THESE CONTRACT DOCUMENTS ARE COMPLEMENTARY, AND WHAT IS REQUIRED BY ANY ONE SHALL BE BINDING AS IF REQUIRED BY ALL. WORK NOT COMPLETELY DELINEATED HEREON SHALL BE CONSTRUCTED OF THE SAME MATERIALS AND DETAILED SIMILARLY AS WORK SHOWN MORE COMPLETELY ELSEWHERE IN THE CONTRACT DOCUMENTS.

BY USE OF THE DRAWINGS FOR CONSTRUCTION OF THE PROJECT, THE OWNER CONFIRMS THAT HE HAS REVIEWED AND APPROVED THE DRAWINGS. THE CONTRACTOR CONFIRMS THAT HE HAS VISITED THE SITE, FAMILIARIZED HIMSELF WITH THE LOCAL CONDITIONS, VERIFIED FIELD DIMENSIONS AND CORRELATED HIS OBSERVATIONS WITH THE REQUIREMENTS OF THE CONTRACT DOCUMENTS.

AS INSTRUMENTS OF SERVICE, ALL DRAWINGS, SPECIFICATIONS, CAD FILES OR OTHER ELECTRONIC MEDIA AND COPIES THERE OF FURNISHED BY THE ENGINEER ARE HIS PROPERTY. THEY ARE TO BE USED ONLY FOR THE PROJECT AND ARE NOT TO BE USED ON ANY OTHER PROJECT, INCLUDING REPEATS OF THE PROJECT. CHANGES TO THE DRAWINGS MAY ONLY BE MADE BY THE ENGINEER.

UNLESS THE REVISION TITLE IS "ISSUED FOR CONSTRUCTION", THESE DRAWINGS SHALL BE CONSIDERED PRELIMINARY AND SHALL NOT BE USED AS A CONSTRUCTION DOCUMENT.

THESE DRAWINGS ILLUSTRATE THE WORK TO BE DONE. THE ENGINEER IS NOT RESPONSIBLE FOR THE MEANS, METHODS, TECHNIQUES, SEQUENCES, AND PROCEDURES USED TO DO THE WORK, OR THE SAFETY ASPECTS OF CONSTRUCTION, AND NOTHING ON THESE DRAWINGS EXPRESSED OR IMPLIED CHANGES THIS CONDITION. CONTRACTOR SHALL DETERMINE ALL CONDITIONS AT THE SITE AND SHALL BE RESPONSIBLE FOR KNOWING HOW THEY AFFECT THE WORK. SUBMITTAL OF A BID TO PERFORM THIS WORK IS ACKNOWLEDGMENT OF THE RESPONSIBILITIES, AND THAT THEY HAVE BEEN FULLY CONSIDERED IN PLANNING OF THE WORK, AND THE BIDDER MAKES NO CLAIMS FOR EXTRA CHARGES DUE TO THESE CONDITIONS WILL BE FORTHCOMING.

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No.	ISSUED FOR MUNICIPAL APPROVAL	REVISIONS	BY	DATE
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01	ISSUED FOR MUNICIPAL APPROVAL		A.S.	24 DEC 2021

NOT AUTHENTIC UNLESS SIGNED AND DATED

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www.lri.ca | (613) 842-3434

CLIENT: **LANDRIC HOMES**
1173 CYRVILLE RD, SUITE 202,
OTTAWA ON K1J 7S6

DESIGNED BY: K.H. DRAWN BY: K.H. APPROVED BY: V.J.

PROJECT: **NAVAN STACKED TOWN HOMES**
6001/6005 RENAUD RD,
OTTAWA, ONTARIO

DRAWING TITLE: **DEMOLITION PLAN**

PROJECT NO: 210216
DATE: NOVEMBER 2021

C102

CITY FILE # D07-12-21-0239



PAVEMENT STRUCTURE

COURSE	MATERIAL	THICKNESS (mm)	
		AUTOMOBILE PARKING	TRUCK ROUTE (HEAVY TRAFFIC)
SURFACE	HL 3 A/C (PG 58-28)	50	40
BINDER	HL 8 A/C (PG 58-28)	-	50
BASECOURSE	OPSS GRANULAR "A"	150	150
SUBBASE	OPSS GRANULAR "B" TYPE II	300	450

NOTE: REFER TO GEOTECHNICAL INVESTIGATION BY PATERSON GROUP DATED APRIL 23, 2021. IN PREPARATION FOR PAVEMENT CONSTRUCTION AT THIS SITE, ANY SURFICIAL OR NEAR SURFACE/SUBGRADE LEVEL TOPSOIL AND ANY SOFT, WET OR DELETERIOUS MATERIALS SHOULD BE REMOVED FROM THE PROPOSED PAVED AREAS. THE EXPOSED SUBGRADE SHOULD BE INSPECTED AND APPROVED BY GEOTECHNICAL PERSONNEL AND ANY SOFT AREAS EVIDENT SHOULD BE SUBEXCAVATED AND REPLACED WITH SUITABLE EARTH BORROW APPROVED BY THE GEOTECHNICAL ENGINEER. THE SUBGRADE SHOULD BE SHAPED AND CROWNED TO PROMOTE DRAINAGE OF THE SITE DRAINAGE STRUCTURES. FOLLOWING APPROVAL OF THE PREPARATION OF THE SUBGRADE, THE PAVEMENT GRANULATES MAY BE PLACED.

- ### LEGEND:
- EXISTING PROPERTY LINE TO REMAIN
 - PROPOSED CURB
 - PROPOSED DEPRESSED CURB
 - PROPOSED TERRACING (3:1 MIN.)
 - PROPOSED SILT FENCE AS PER OPSD 219.110
 - PROPOSED FENCE
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 - PROPOSED GRASS AREA (100mm TOP SOIL & SOD)
 - PROPOSED CONCRETE FEATURES/SLAB
 - PROPOSED HEAVY DUTY ASPHALT
 - PROPOSED LIGHT DUTY ASPHALT
 - PROPOSED RIP RAP
 - PROPOSED ELEVATION
 - PROPOSED HIGH POINT ELEVATION
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 - PROPOSED STORM SEWER
 - PROPOSED SANITARY SEWER
 - PROPOSED WATERMAIN
 - PROPOSED 150mm SAN SERVICE
 - PROPOSED 250mm PEX WTR SERVICE
 - EXISTING STORM SEWER
 - EXISTING SANITARY SEWER
 - EXISTING WATERMAIN
 - EXISTING MANHOLE
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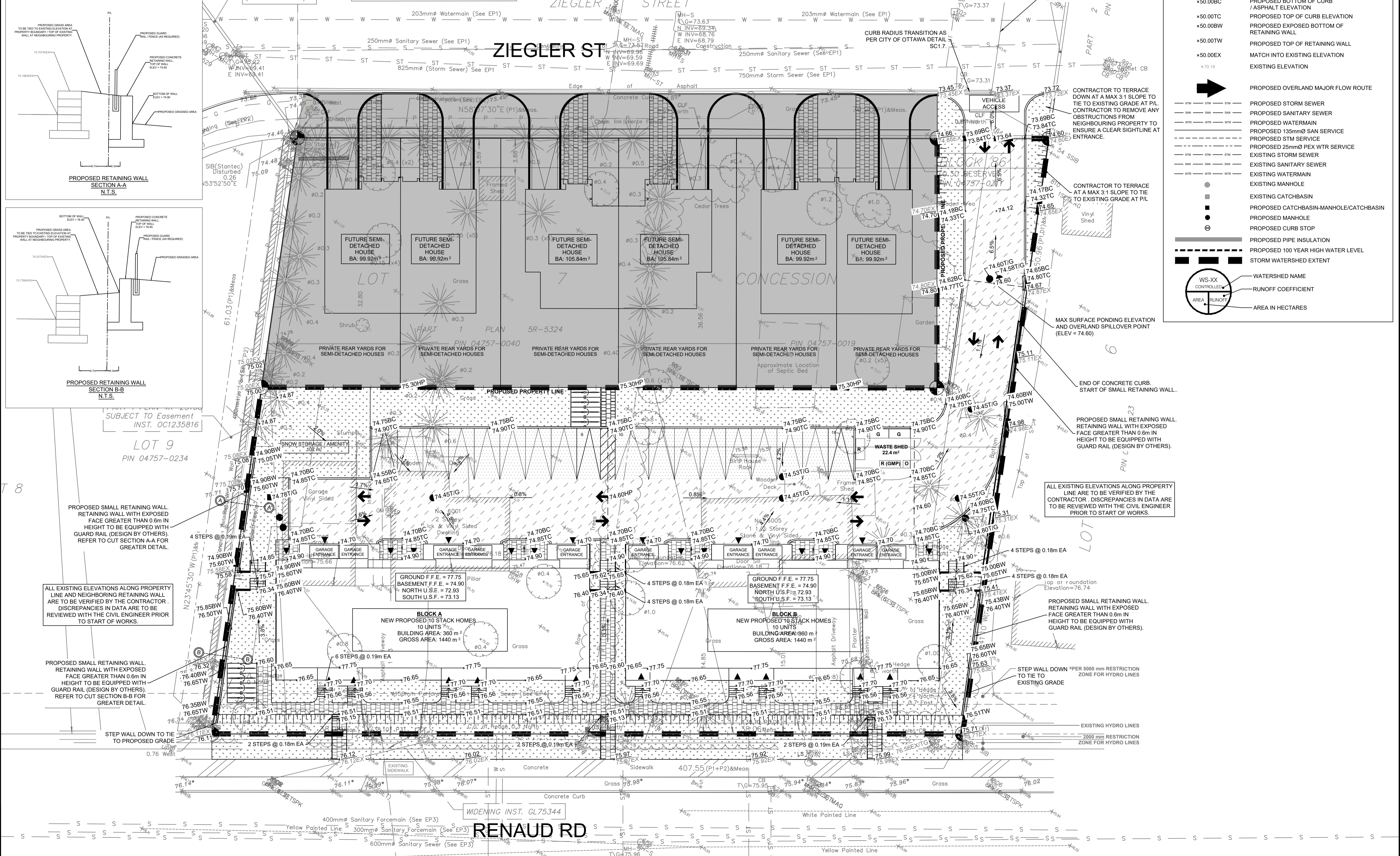
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SUBJECT TO APPROVAL

02	ISSUED FOR MUNICIPAL APPROVAL	K.H.	09 JUN 2023
01	ISSUED FOR MUNICIPAL APPROVAL	A.S.	24 DEC 2021
No.	REVISIONS	BY	DATE

LRJ
ENGINEERING | INGENIERIE
5430 Canotek Road | Ottawa, ON, K1J 9G2
www.lrl.ca | (613) 842-3434

CLIENT	LANDRIC HOMES 1173 CYRVILLE RD, SUITE 202, OTTAWA ON K1J 7S6		
DESIGNED BY:	DRAWN BY:	APPROVED BY:	
K.H.	K.H.	V.J.	
PROJECT			
NAVAN STACKED TOWN HOMES 6001/6005 RENAUD RD, OTTAWA, ONTARIO			
DRAWING TITLE			
GRADING AND DRAINAGE PLAN			
PROJECT NO.			
210216			
DATE			
NOVEMBER 2021			

C301

CITY FILE # D07-12-21-0239



PIPE CROSSING TABLE (+)						
CROSSING ID	PROP. 150mm WTR SERV INV	PROP. 150mm SAN SERV OBV	EX. 250mm SAN SWR OBV	EX. 750mm STM SWR OBV	EX. 750mm STM SWR INV	CLEARANCE (m)
1	70.81		69.18			1.63
2	71.14			70.64		0.50
3		69.22			69.89	0.77

PLAN

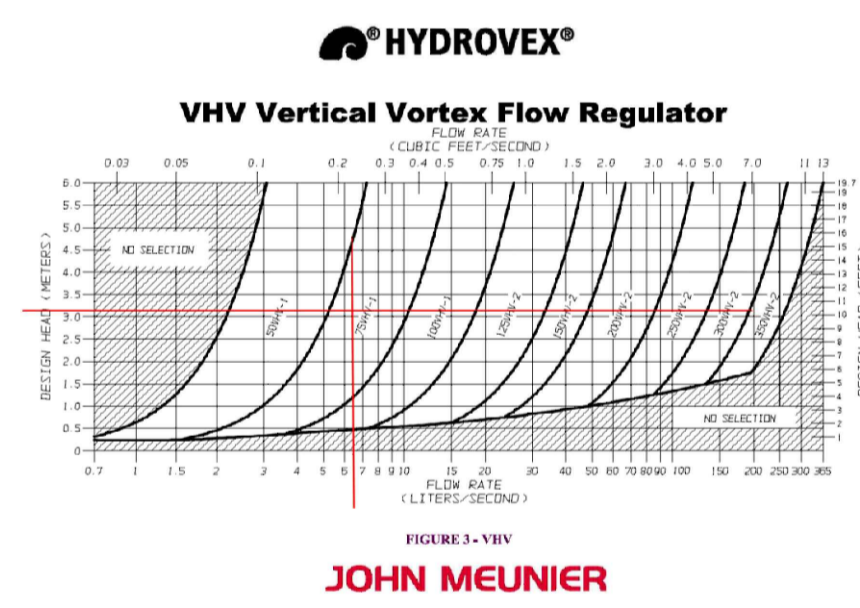
LOT 18

1400

CONTRACTOR TO FIELD VERIFY ALL SEWER / MAIN ELEVATIONS. ANY DISCREPANCIES IN DATA ARE TO BE REVIEWED WITH THE CIVIL ENGINEER PRIOR TO SERVICE INSTALLATION.

LEGEND:

- EXISTING PROPERTY LINE TO REMAIN
- PROPOSED CURB
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USE AND INTERPRETATION OF DRAWINGS

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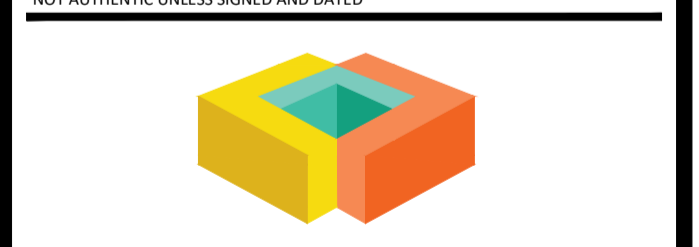
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CLIENT: **LANDRIC HOMES**
1173 CYRVILLE RD, SUITE 202,
OTTAWA ON K1J 756

DESIGNED BY: K.H. DRAWN BY: K.H. APPROVED BY: V.J.

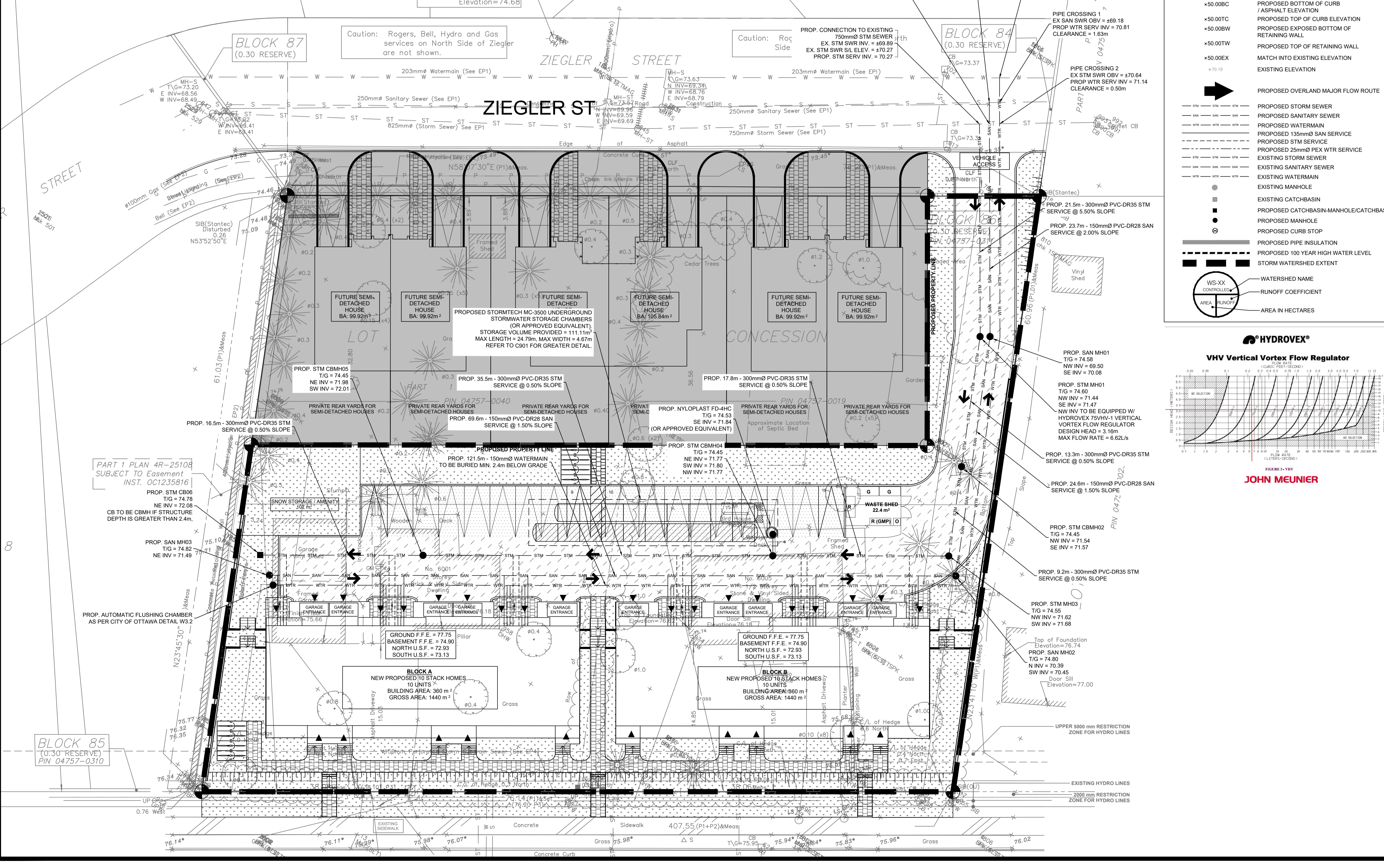
PROJECT: **NAVAN STACKED TOWN HOMES**
6001/6005 RENAUD RD,
OTTAWA, ONTARIO

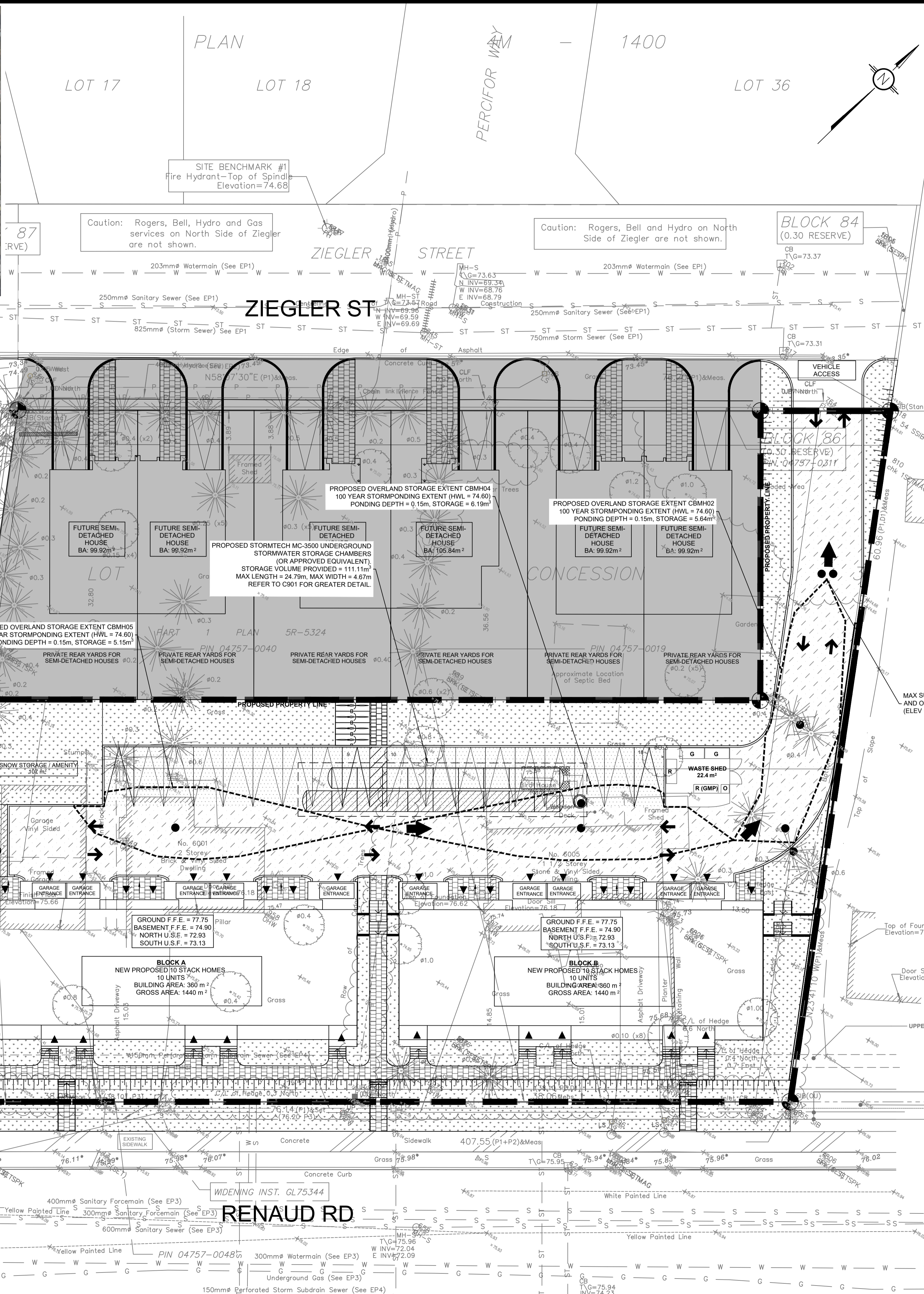
DRAWING TITLE: **SERVICING PLAN**

PROJECT NO: 210216
DATE: NOVEMBER 2021

C401

DWG # 18659





LEGEND:

- EXISTING PROPERTY LINE TO REMAIN
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- PROPOSED 25mm PEX WTR SERVICE
- EXISTING STORM SEWER
- EXISTING SANITARY SEWER
- EXISTING WATERMAIN
- EXISTING MANHOLE
- EXISTING CATCHBASIN
- PROPOSED CATCHBASIN-MANHOLE-CATCHBASIN
- PROPOSED MANHOLE
- PROPOSED CURB STOP
- PROPOSED PIPE INSULATION
- PROPOSED 100 YEAR HIGH WATER LEVEL
- STORM WATERSHED EXTENT
- WATERSHED NAME
- RUNOFF COEFFICIENT
- AREA IN HECTARES

USE AND INTERPRETATION OF DRAWINGS

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IN THE EVENT THE CLIENT, THE CLIENT'S CONTRACTORS OR SUBCONTRACTORS, OR ANYONE FOR WHOM THE CLIENT IS LEGALLY LIABLE MAKES OR PERMITS TO BE MADE ANY CHANGES TO ANY REPORTS, PLANS, SPECIFICATIONS OR OTHER CONSTRUCTION DOCUMENTS PREPARED BY LRL ASSOCIATES LTD. (LRL) WITHOUT OBTAINING LRL'S PRIOR WRITTEN CONSENT, THE CLIENT SHALL ASSUME FULL RESPONSIBILITY FOR THE RESULTS OF SUCH CHANGES. THEREFORE, THE CLIENT AGREES TO WAIVE ANY CLAIM AGAINST LRL AND TO RELEASE LRL FROM ANY LIABILITY ARISING DIRECTLY OR INDIRECTLY FROM SUCH UNAUTHORIZED CHANGES.

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CONTRACTOR TO VERIFY ALL DIMENSIONS AND NOTIFY THE ENGINEER OF ANY DISCREPANCIES BEFORE WORK COMMENCES. DO NOT SCALE DRAWINGS.

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SCALE: 1:200

SUBJECT TO APPROVAL

No.	REVISIONS	BY	DATE
02	ISSUED FOR MUNICIPAL APPROVAL	K.H.	09 JUN 2023
01	ISSUED FOR MUNICIPAL APPROVAL	A.S.	24 DEC 2021

NOT AUTHENTIC UNLESS SIGNED AND DATED

LRJ
ENGINEERING | INGENIERIE
5430 Canotek Road | Ottawa, ON, K1J 9G2
www.lrl.ca | (613) 842-3434

CLIENT: **LANDRIC HOMES**
1173 CYRVILLE RD, SUITE 202,
OTTAWA ON K1J 756

DESIGNED BY: K.H. DRAWN BY: K.H. APPROVED BY: V.J.

PROJECT: **NAVAN STACKED TOWN HOMES**
6001/6005 RENAUD RD,
OTTAWA, ONTARIO

DRAWING TITLE: **STORMWATER MANAGEMENT PLAN**

PROJECT NO: 210216
DATE: NOVEMBER 2021

C601

DWG # 18659

PART 1 PLAN 4R-25108
SUBJECT TO Easement
INST. OC1235816

LOT 9
PIN 04757-0234

LOT 8

LOT 17

LOT 18

LOT 36

LOT 35

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LOT 33

LOT 32

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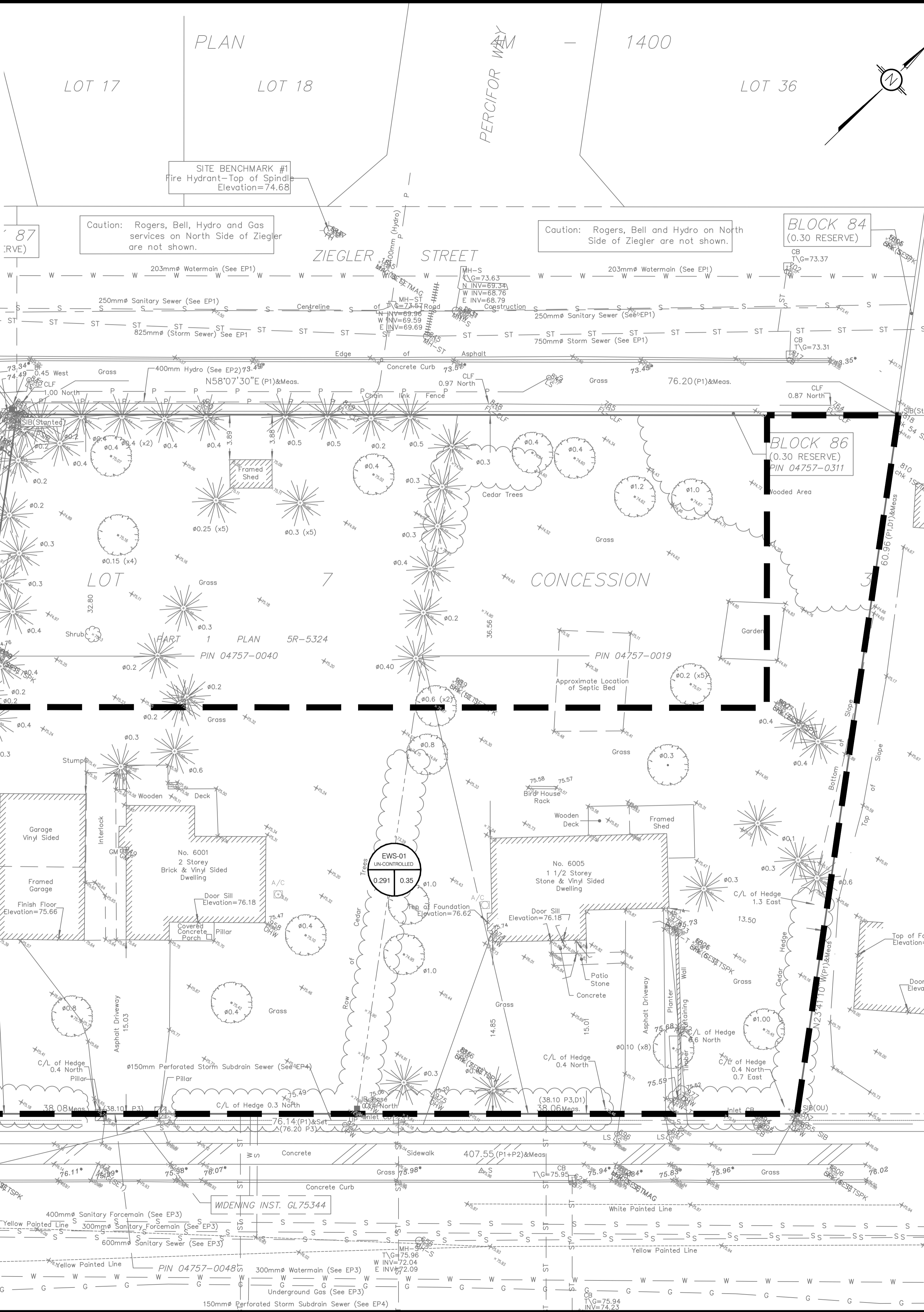
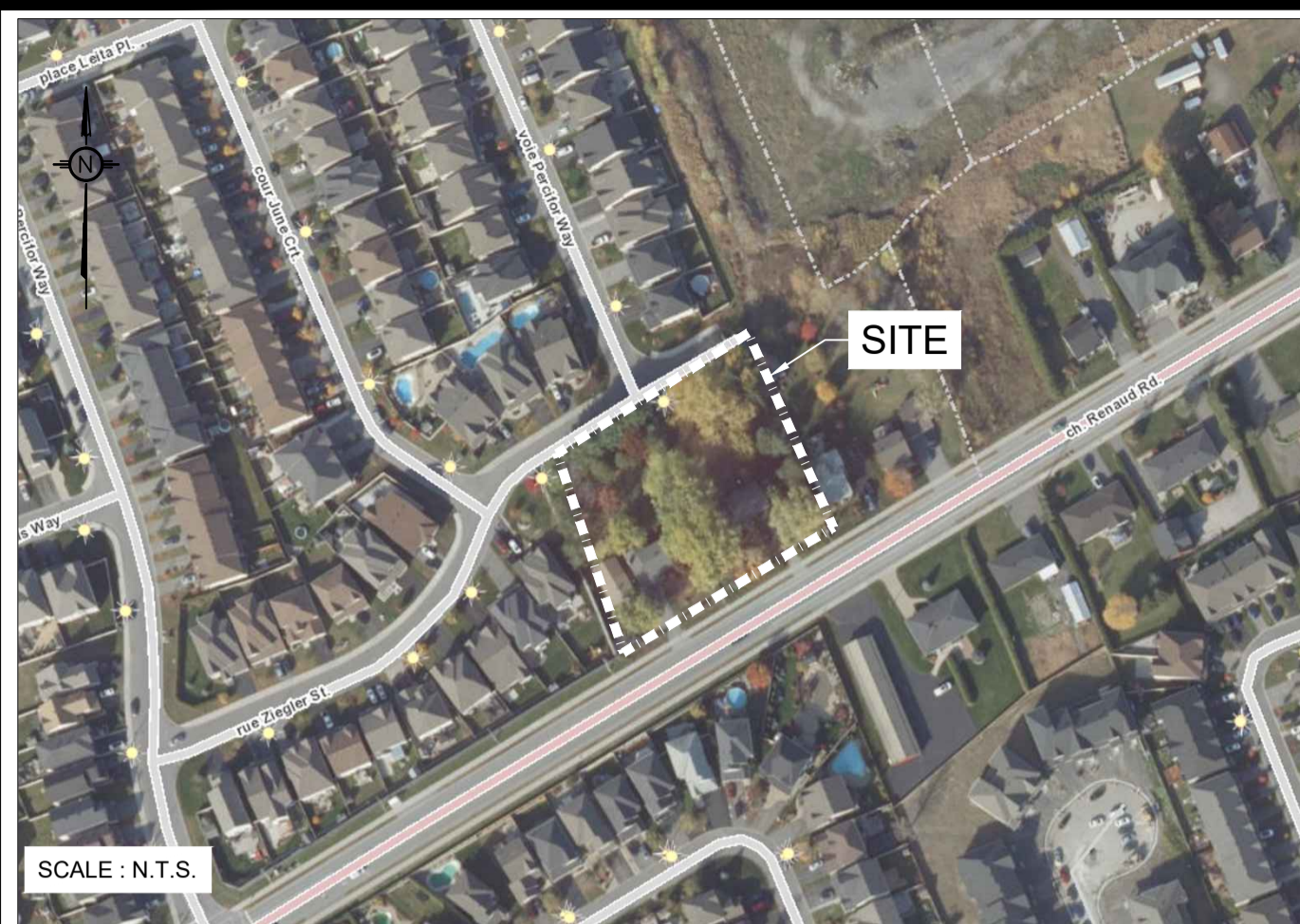
LOT 4

LOT 3

LOT 2

LOT 1

LOT 0



LEGEND:

- EXISTING PROPERTY LINE TO REMAIN
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- PROPOSED DEPRESSED CURB
- PROPOSED TERRACING (3:1 MIN.)
- PROPOSED SILT FENCE AS PER OPSD 219.110
- PROPOSED FENCE
- PROPOSED DOOR ENTRANCE/EXIST
- PROPOSED GRASS AREA (100mm TOP SOIL & SOD)
- PROPOSED CONCRETE FEATURES/SLAB
- PROPOSED HEAVY DUTY ASPHALT
- PROPOSED LIGHT DUTY ASPHALT
- PROPOSED RIP RAP
- PROPOSED ELEVATION
- PROPOSED HIGH POINT ELEVATION
- PROPOSED SWALE ELEVATION
- PROPOSED BOTTOM OF CURB / ASPHALT ELEVATION
- PROPOSED TOP OF CURB ELEVATION
- PROPOSED EXPOSED BOTTOM OF RETAINING WALL
- PROPOSED TOP OF RETAINING WALL
- MATCH INTO EXISTING ELEVATION
- EXISTING ELEVATION
- PROPOSED OVERLAND MAJOR FLOW ROUTE
- PROPOSED STORM SEWER
- PROPOSED SANITARY SEWER
- PROPOSED WATERMAIN
- PROPOSED 135mm SAN SERVICE
- PROPOSED STM SERVICE
- PROPOSED 25mm PEX WTR SERVICE
- EXISTING STORM SEWER
- EXISTING SANITARY SEWER
- EXISTING WATERMAIN
- EXISTING MANHOLE
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SCALE: 1:200

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No.	REVISIONS	BY	DATE



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OTTAWA ON K1J 7S6

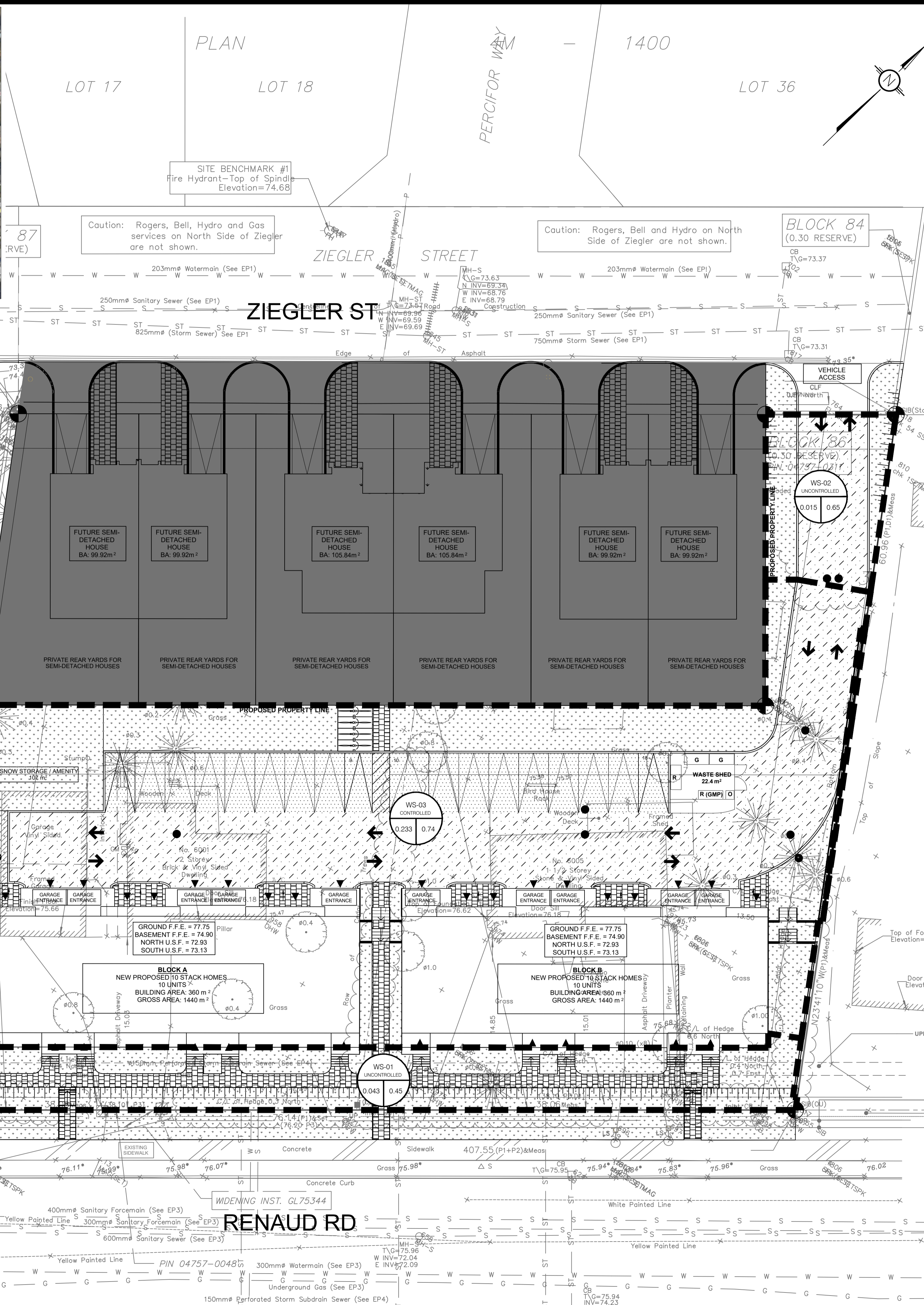
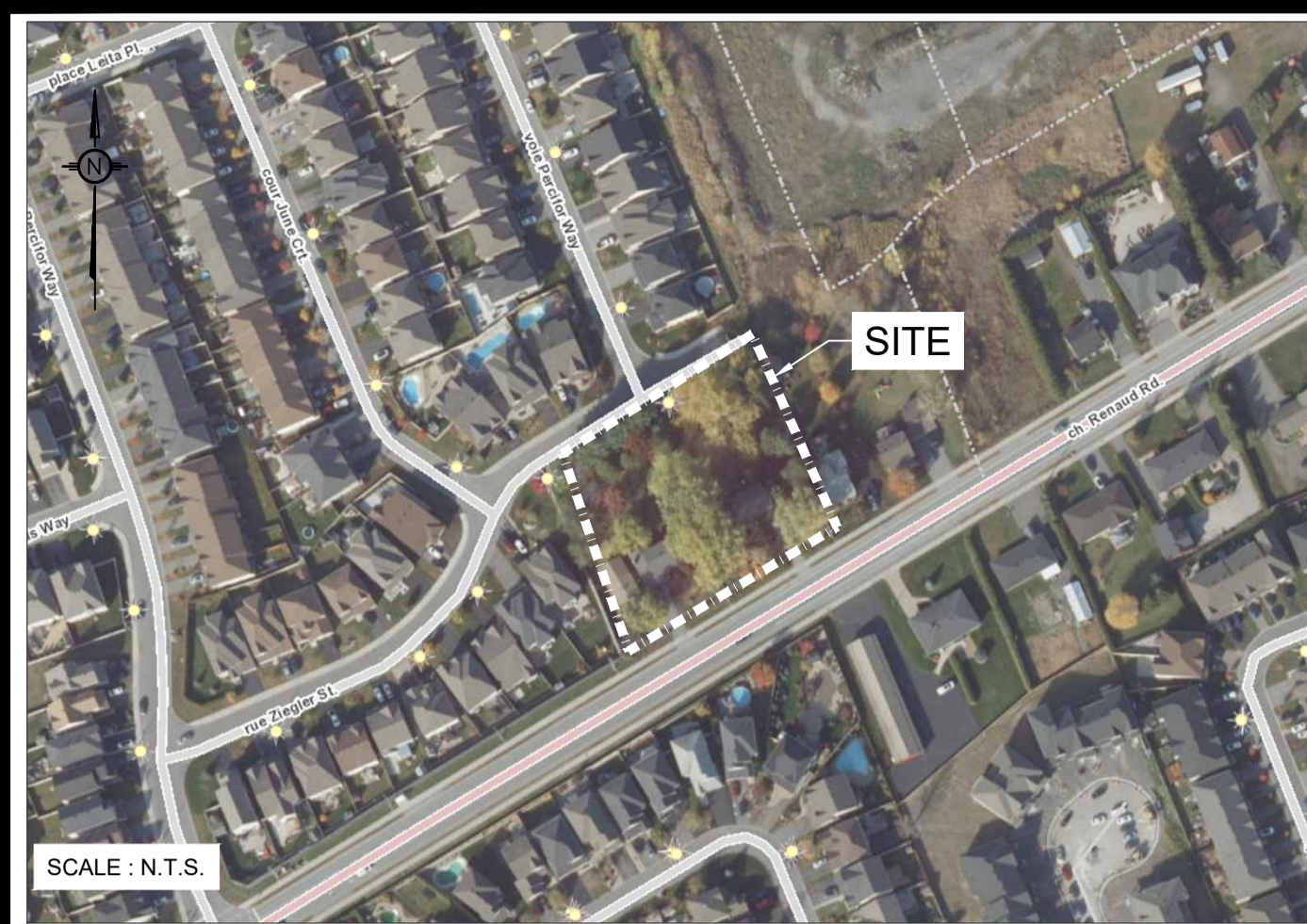
DESIGNED BY: K.H. DRAWN BY: K.H. APPROVED BY: V.J.

PROJECT: **NAVAN STACKED TOWN HOMES**
6001/6005 RENAUD RD,
OTTAWA, ONTARIO

DRAWING TITLE: **PRE-DEVELOPMENT WATERSHED PLAN**

PROJECT NO: 210216
DATE: NOVEMBER 2021

C701



LEGEND:

- EXISTING PROPERTY LINE TO REMAIN
- PROPOSED CURB
- PROPOSED DEPRESSED CURB
- PROPOSED TERRACING (3:1 MIN.)
- PROPOSED SILT FENCE AS PER OPSD 219.110
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- PROPOSED 25mm WTR SERVICE
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SCALE: 1:200

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CLIENT: **LANDRIC HOMES**
1173 CYRVILLE RD, SUITE 202,
OTTAWA ON K1J 7S6

DESIGNED BY: K.H. DRAWN BY: K.H. APPROVED BY: V.J.

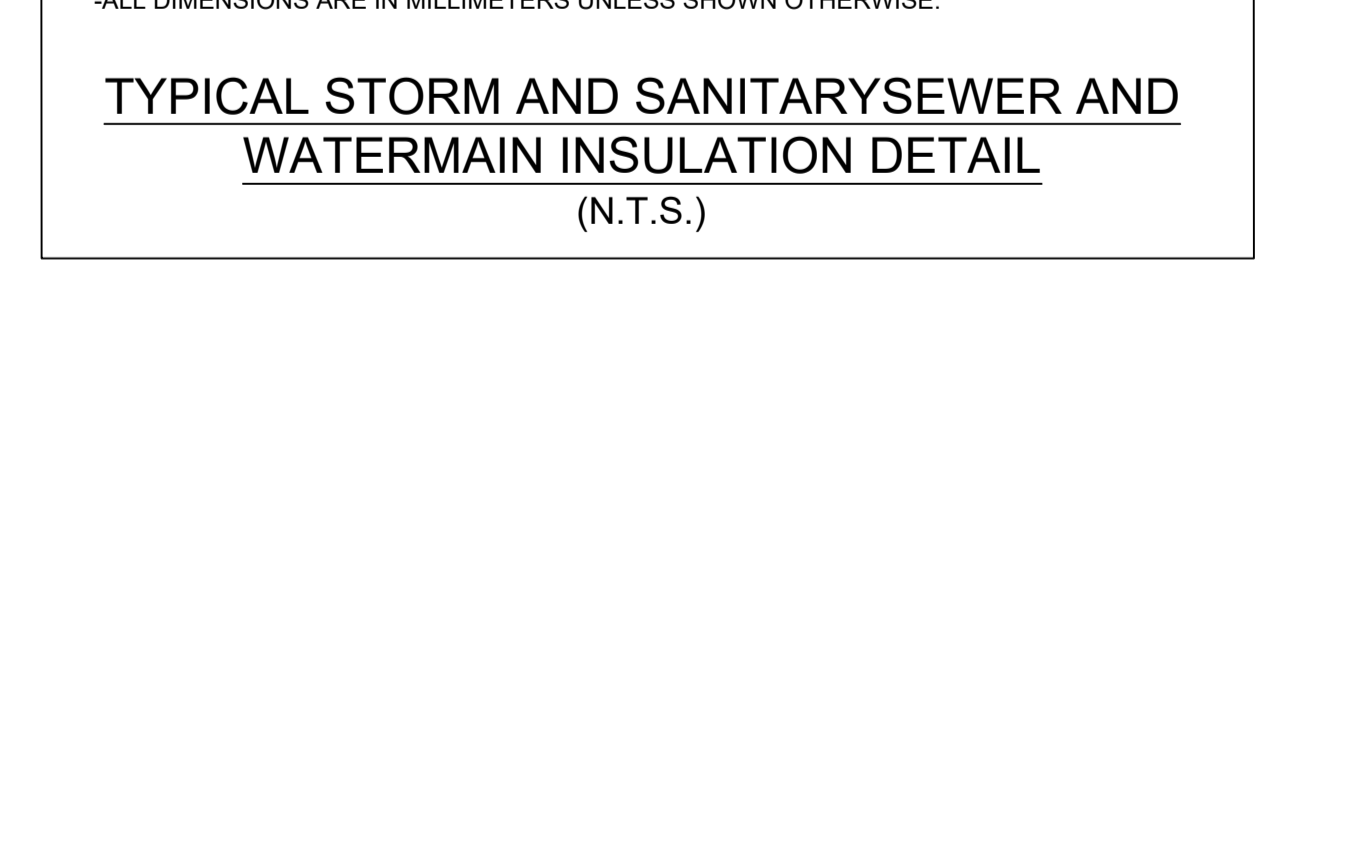
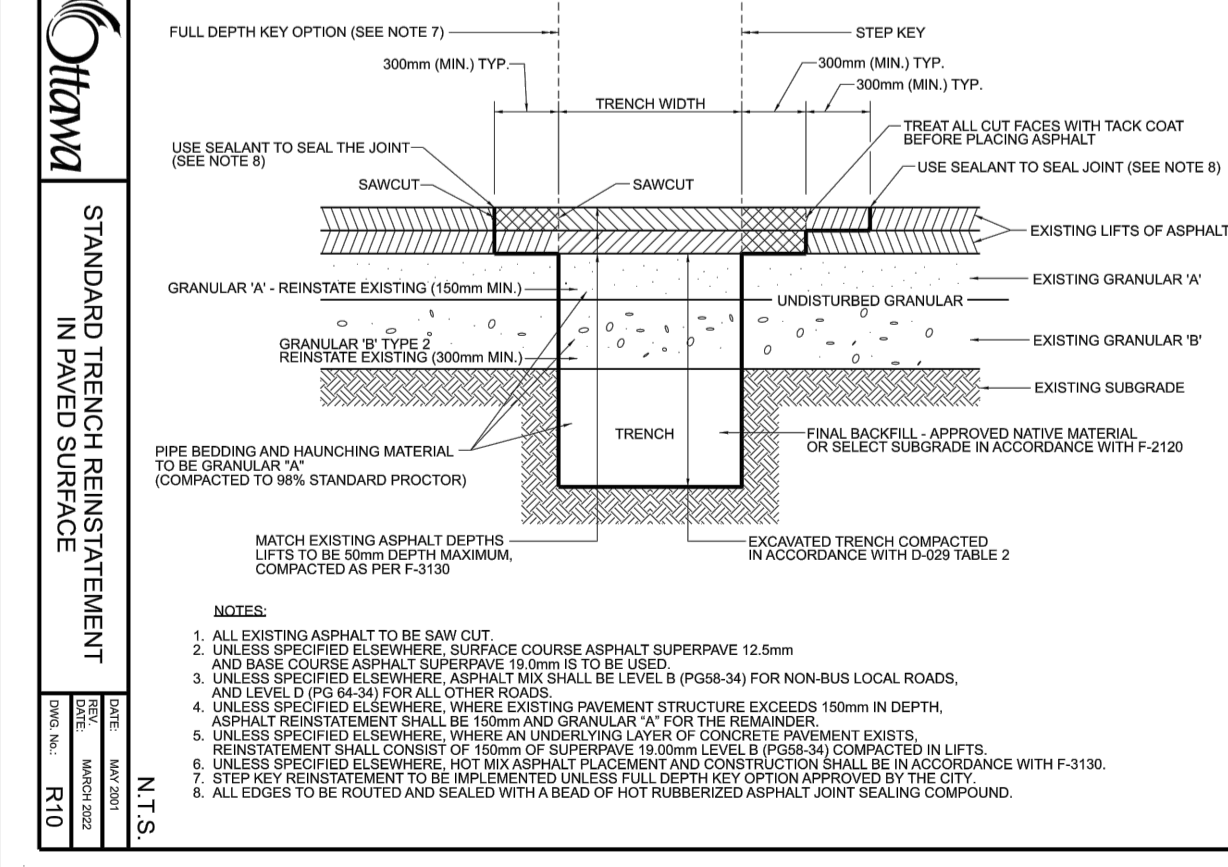
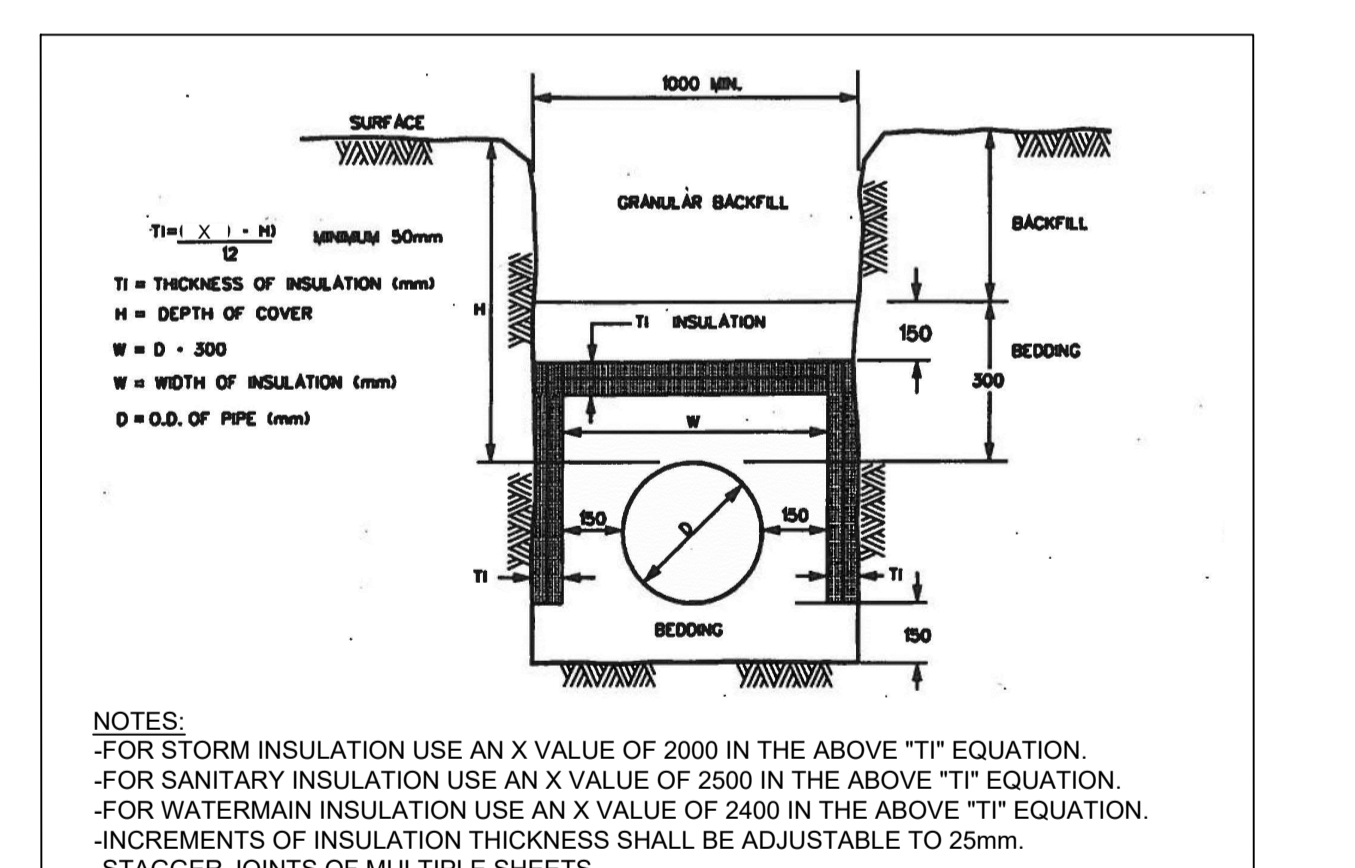
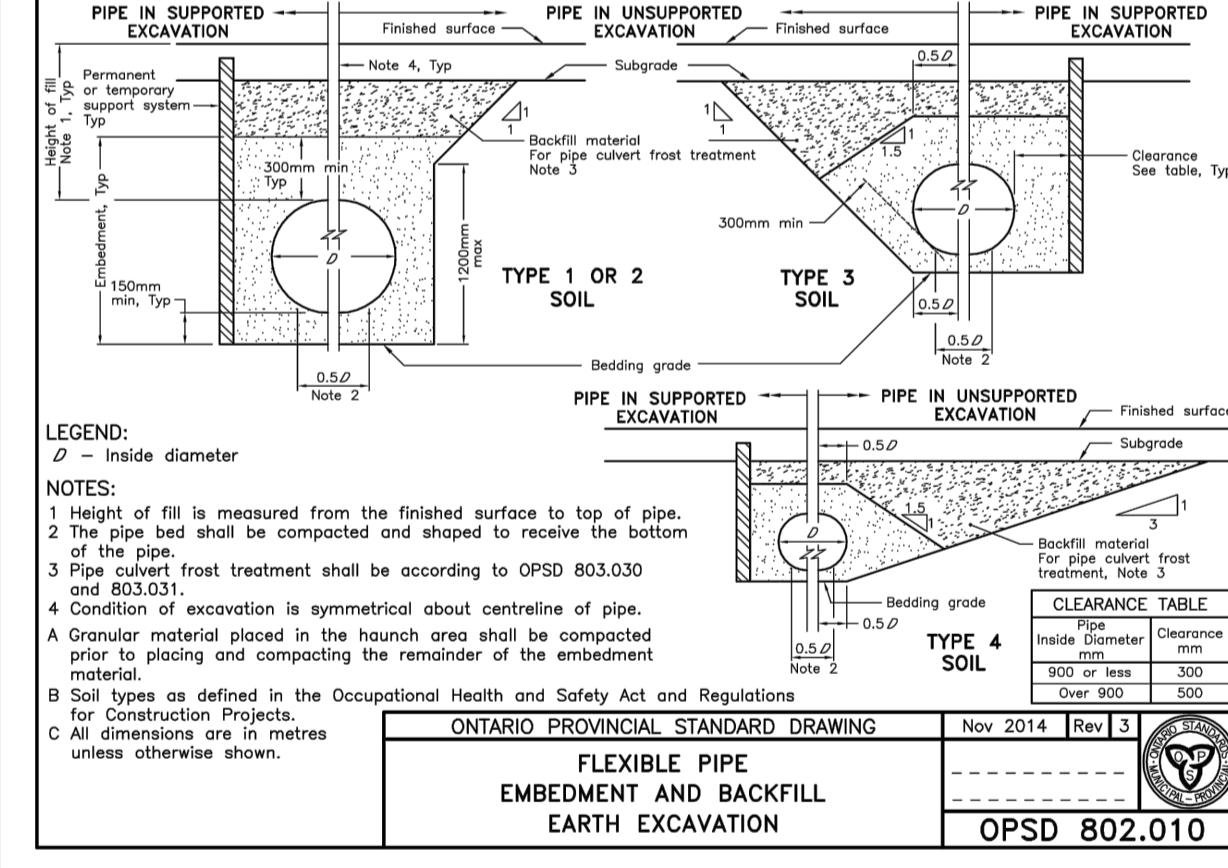
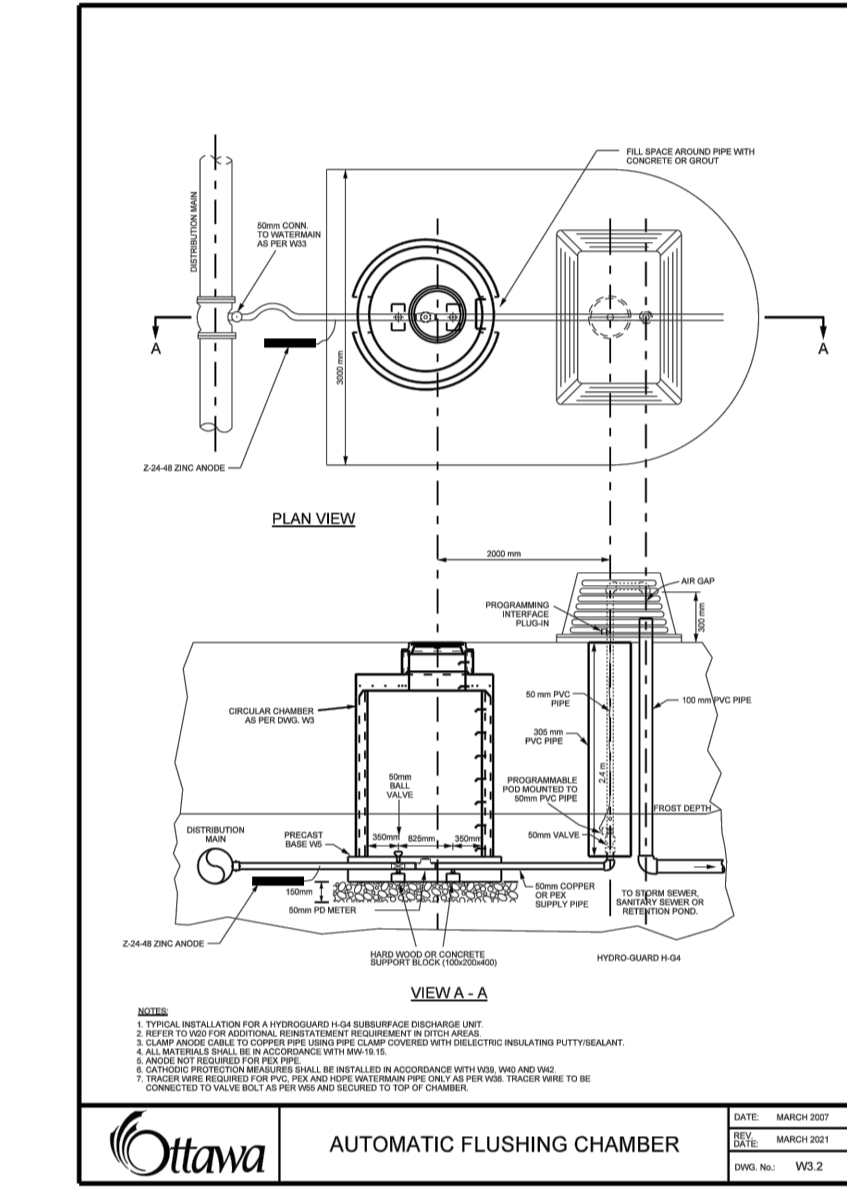
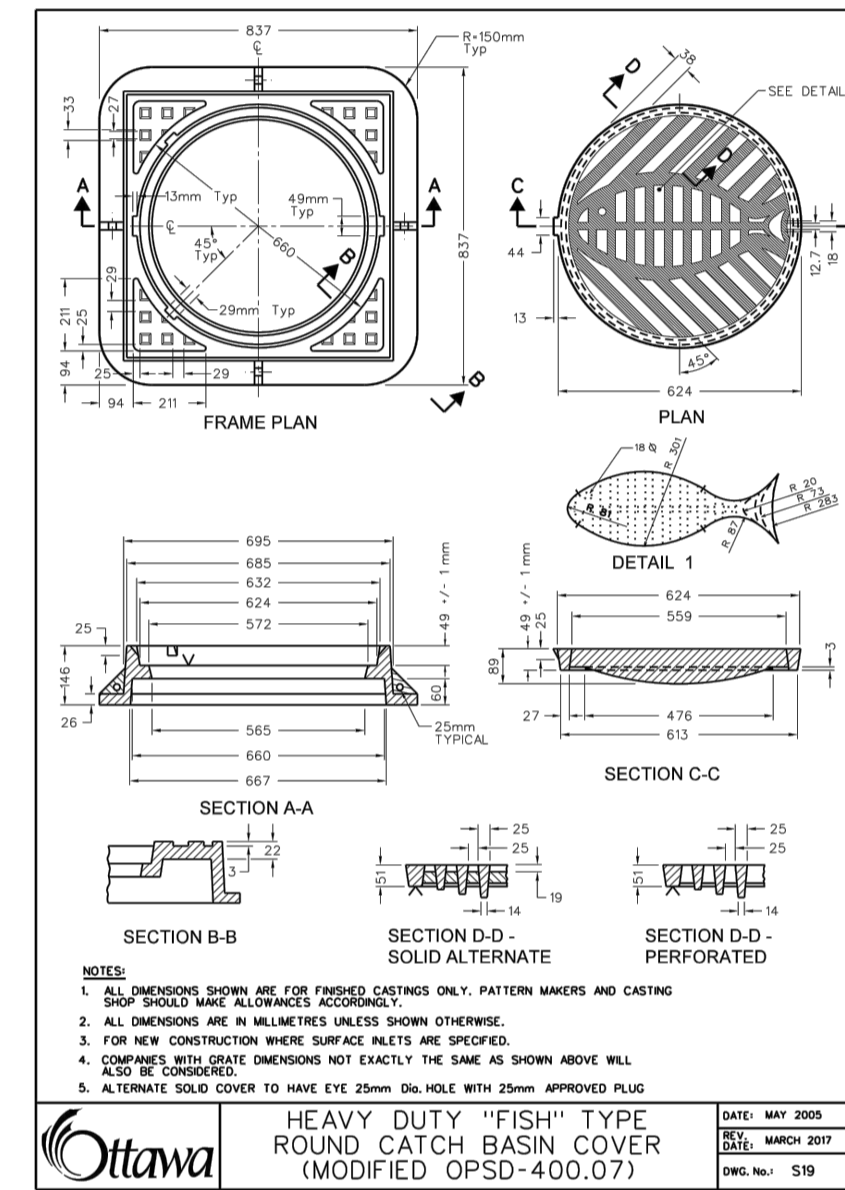
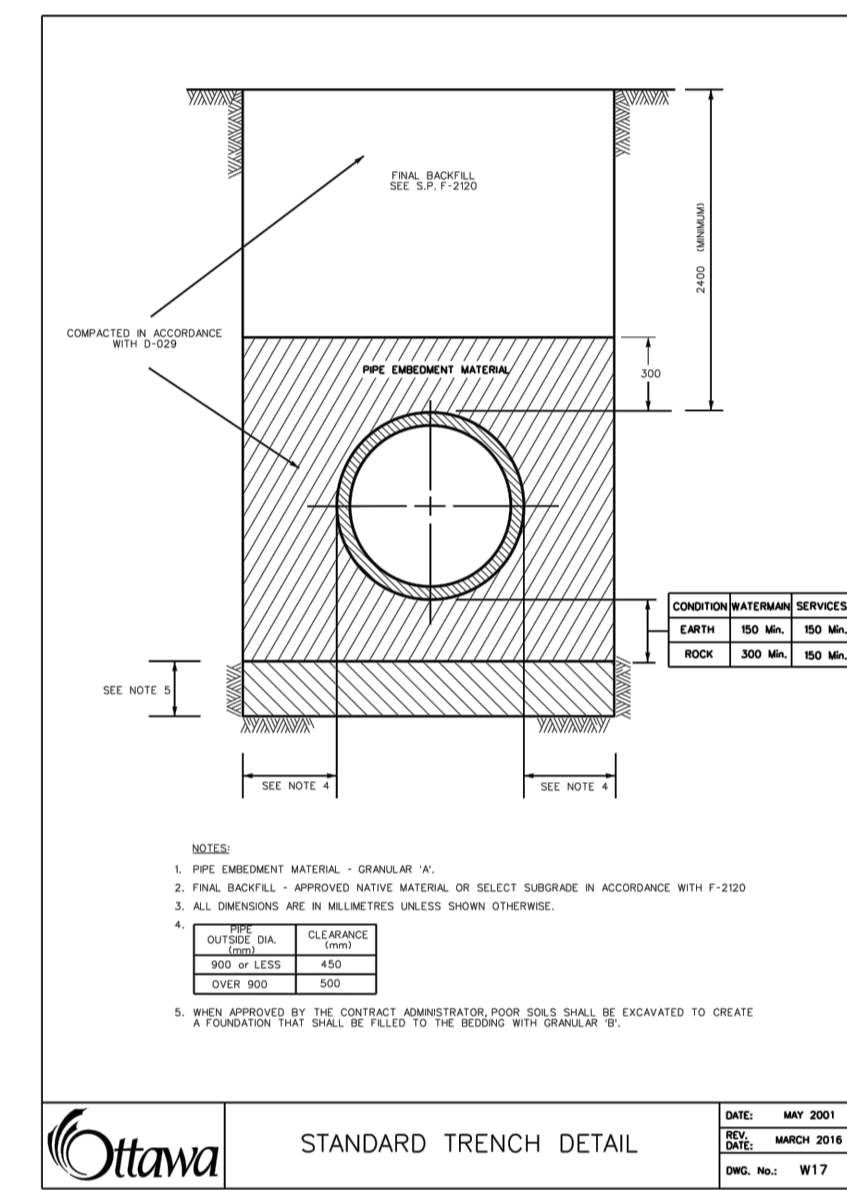
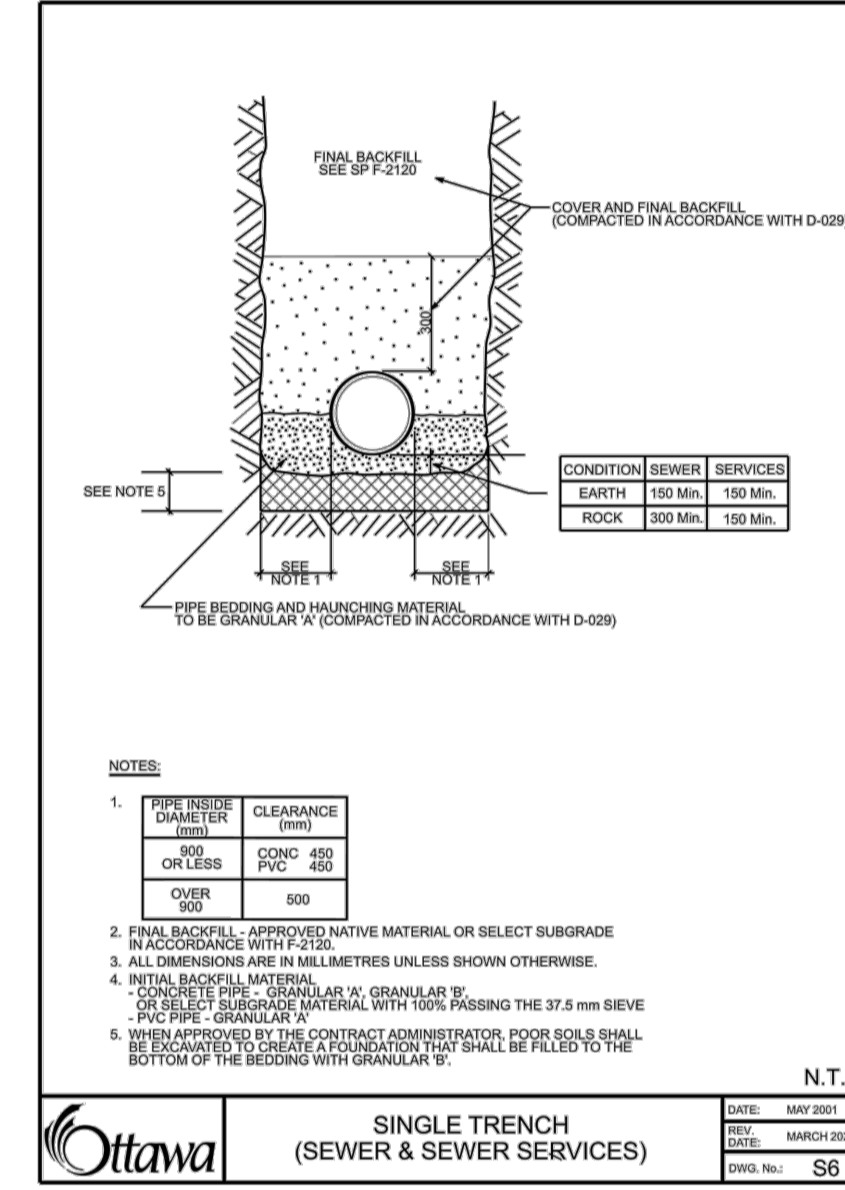
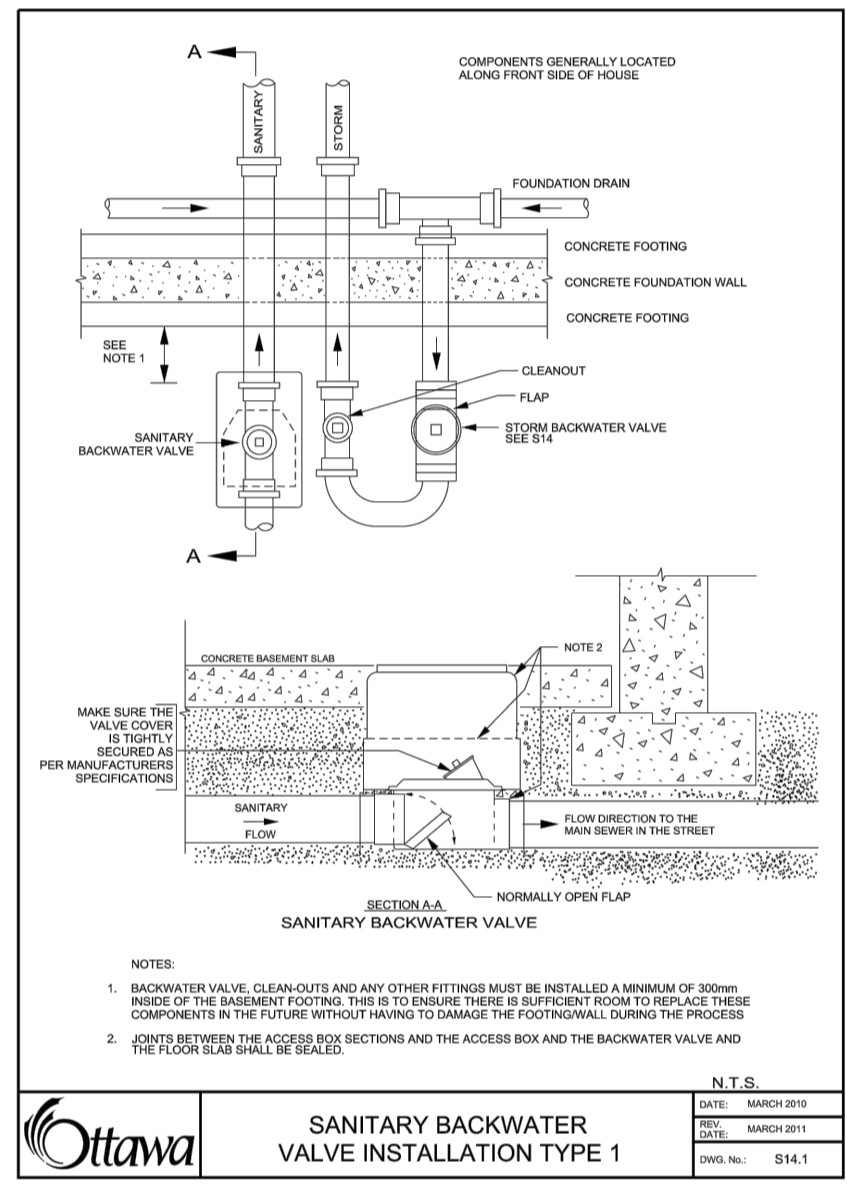
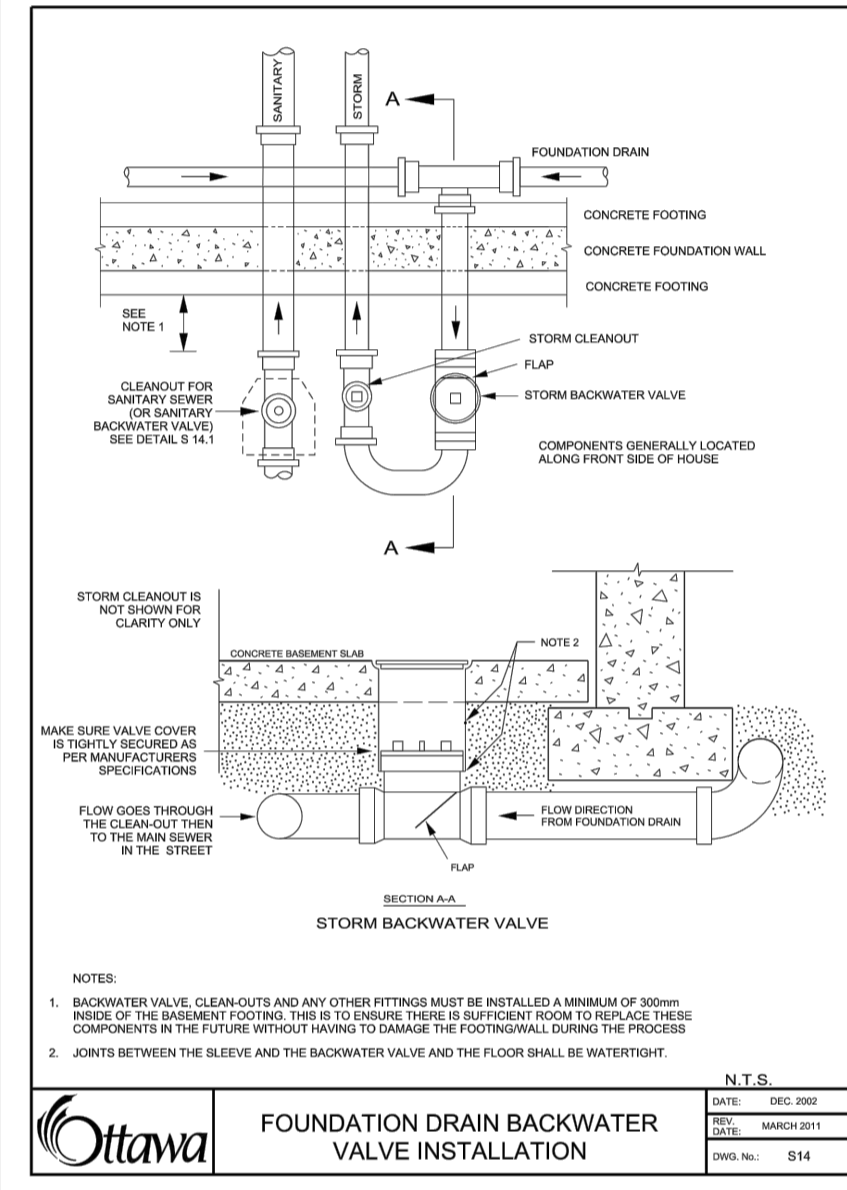
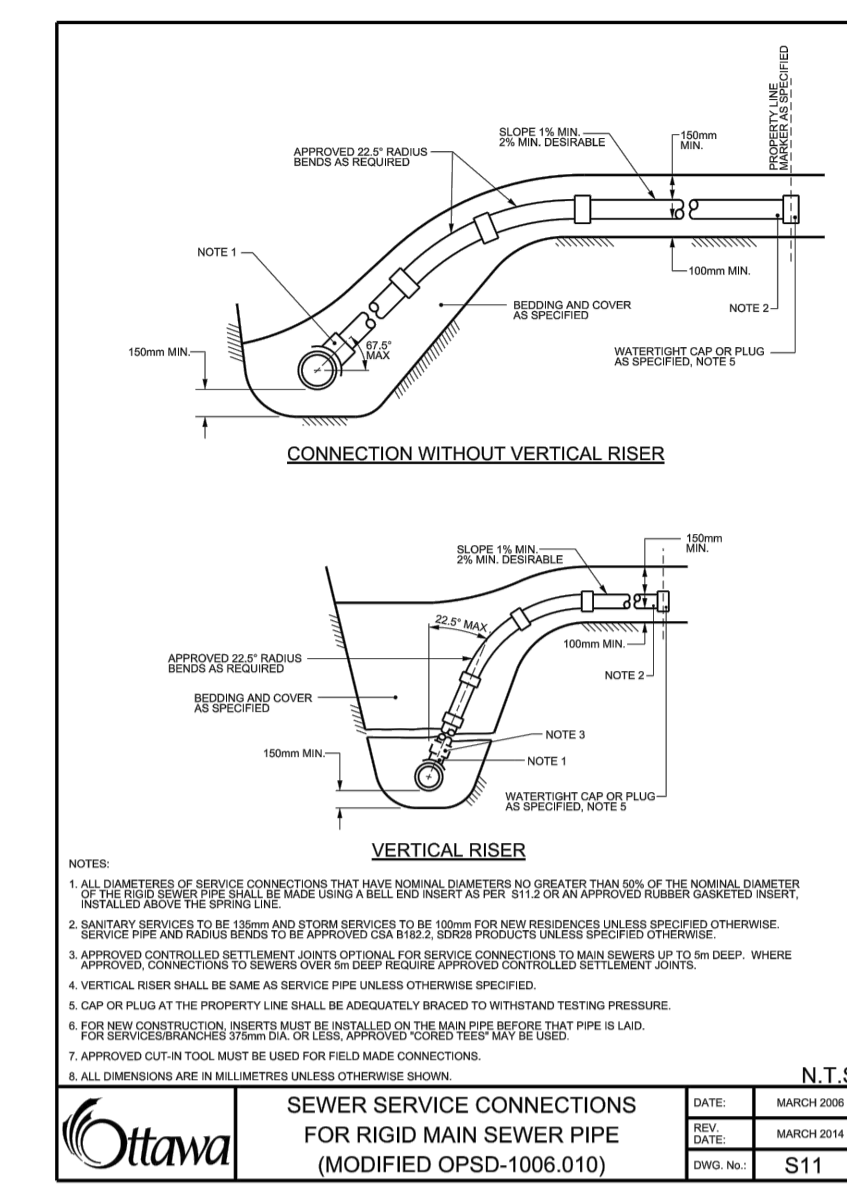
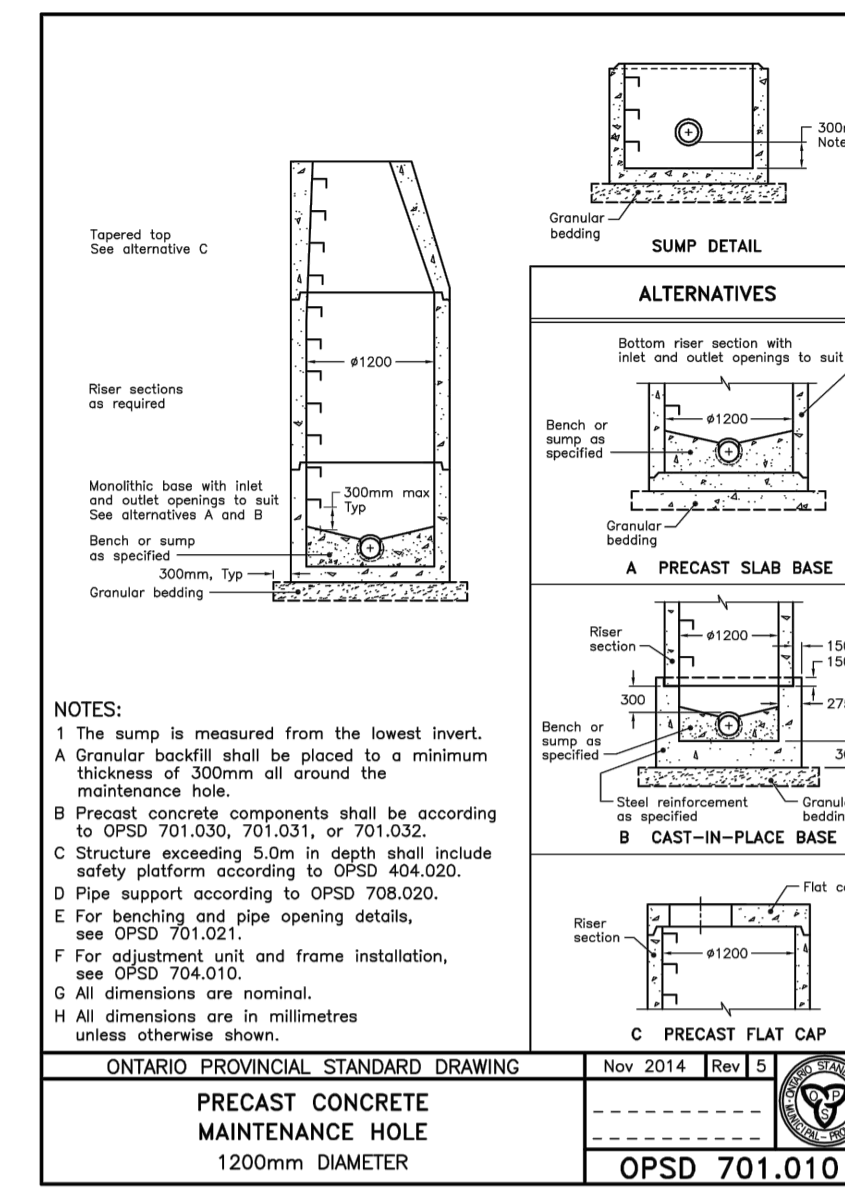
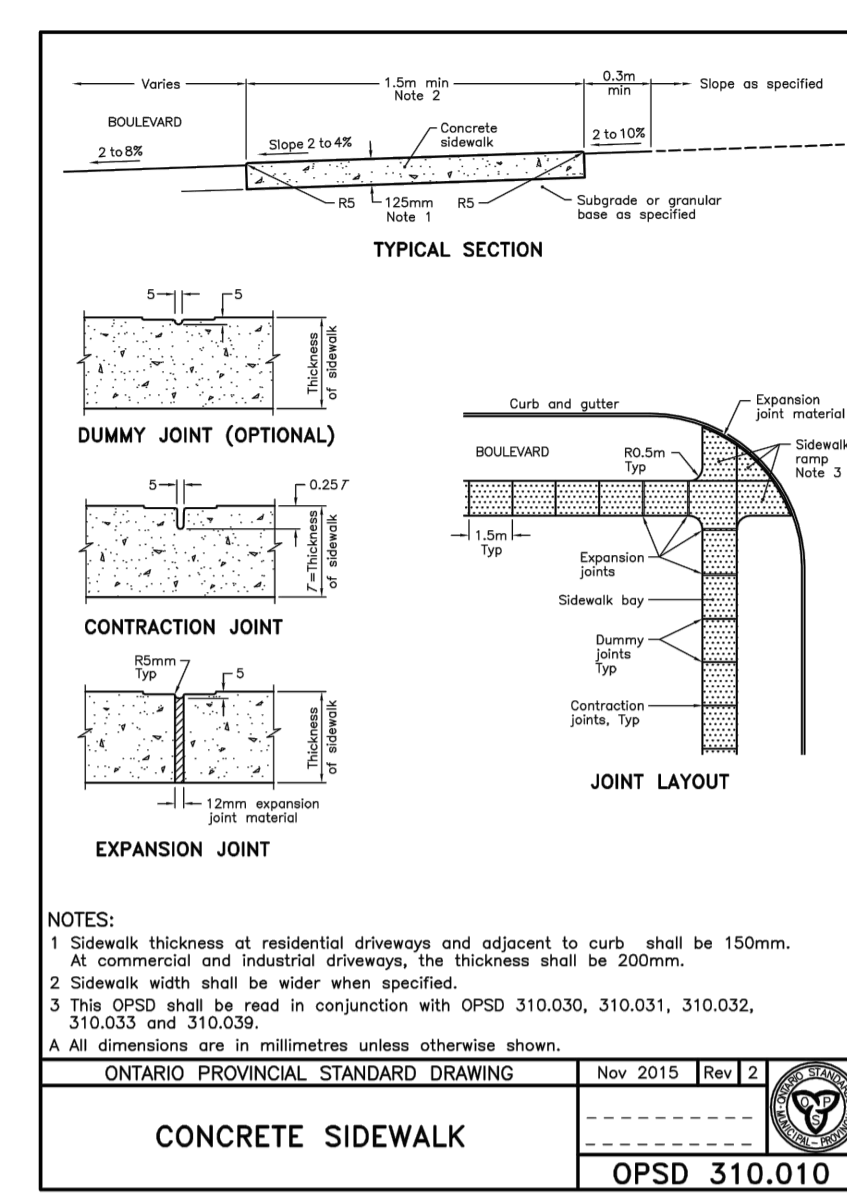
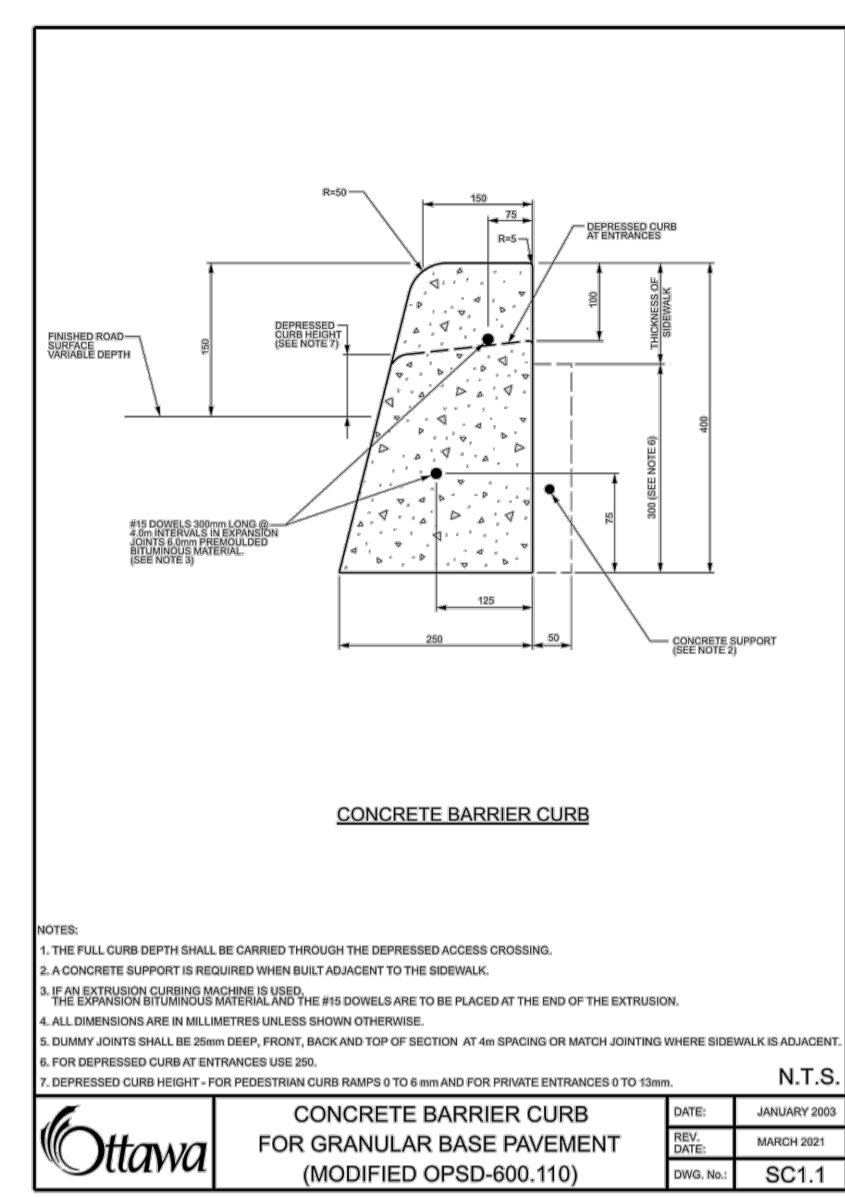
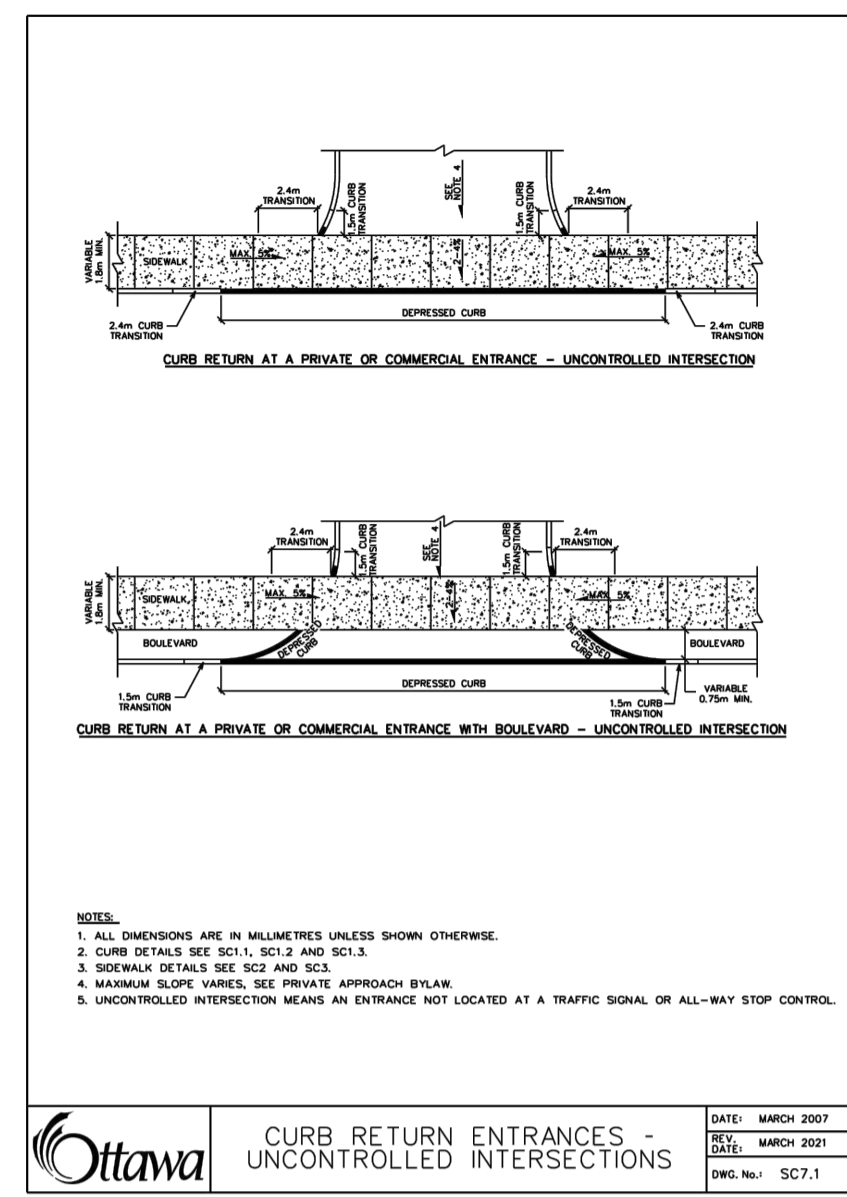
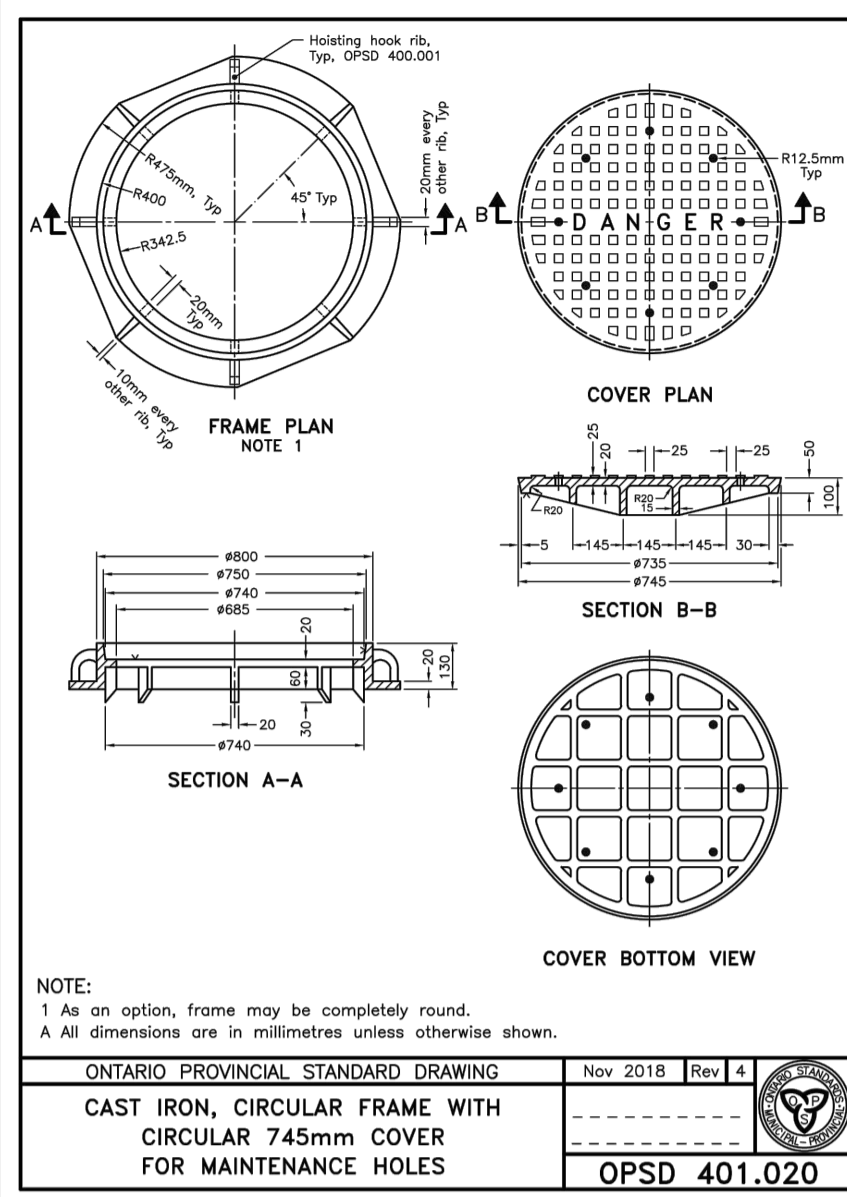
PROJECT: **NAVAN STACKED TOWN HOMES**
6001/6005 RENAUD RD,
OTTAWA, ONTARIO

DRAWING TITLE: **POST-DEVELOPMENT WATERSHED PLAN**

PROJECT NO: 210216
DATE: NOVEMBER 2021

C702

CITY FILE # D07-12-21-0239



USE AND INTERPRETATION OF DRAWINGS

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THESE DRAWINGS ILLUSTRATE THE WORK TO BE DONE. THE ENGINEER IS NOT RESPONSIBLE FOR THE MEANS, METHODS, TECHNIQUES, SEQUENCES, AND SCHEDULES USED TO DO THE WORK, OR THE SAFETY ASPECTS OF CONSTRUCTION, AND NOTHING ON THESE DRAWINGS EXPRESSED OR IMPLIED CHANGES THIS CONDITION. CONTRACTOR SHALL DETERMINE ALL CONDITIONS AT THE SITE AND SHALL BE RESPONSIBLE FOR KNOWING HOW THEY AFFECT THE WORK. SUBMITTAL OF A BID TO PERFORM THIS WORK IS AN ACKNOWLEDGEMENT OF THE RESPONSIBILITIES, AND THAT THEY HAVE BEEN FULLY CONSIDERED IN PLANNING OF THE WORK AND THE BID PRICE. NO CLAIMS FOR EXTRA CHARGES DUE TO THESE CONDITIONS WILL BE FORTHCOMING.

UNAUTHORIZED CHANGES:

IN THE EVENT THE CLIENT, THE CLIENT'S CONTRACTORS OR SUBCONTRACTORS, OR ANYONE FOR WHOM THE CLIENT IS LEGALLY LIABLE MAKES OR PERMITS TO BE MADE ANY CHANGES TO ANY REPORTS, PLANS, SPECIFICATIONS OR OTHER CONSTRUCTION DOCUMENTS PREPARED BY LRI ASSOCIATES LTD. (LRI) WITHOUT OBTAINING LRI'S PRIOR WRITTEN CONSENT, THE CLIENT SHALL ASSUME FULL RESPONSIBILITY FOR THE RESULTS OF SUCH CHANGES. THEREFORE THE CLIENT AGREES TO WAIVE ANY CLAIM AGAINST LRI AND TO RELEASE LRI FROM ANY LIABILITY ARISING DIRECTLY OR INDIRECTLY FROM SUCH UNAUTHORIZED CHANGES.

IN ADDITION, THE CLIENT AGREES TO THE FULLEST EXTENT PERMITTED BY LAW, TO INDEMNIFY AND HOLD HARMLESS LRI FROM ANY DAMAGES, LIABILITIES OR COSTS, INCLUDING REASONABLE ATTORNEY'S FEES AND COST OF DEFENSE, ARISING FROM SUCH CHANGES MADE WITHOUT SUCH PROPER AUTHORIZATION.

GENERAL NOTES:

EXISTING SERVICES AND UTILITIES SHOWN ON THESE DRAWINGS ARE TAKEN FROM THE BEST AVAILABLE RECORDS, BUT MAY NOT BE COMPLETE OR TO DATE. CONTRACTOR SHALL VERIFY IN FIELD FOR LOCATION AND ELEVATION OF PIPES AND CHECK WITH THE UTILITY COMPANIES BEFORE DIGGING OR PERFORMING WORK.

CONTRACTOR IS ADVISED TO COLLECT INFORMATION ON SOIL CONDITIONS BEFORE START OF CONSTRUCTION.

THE ENGINEER WAIVES ANY AND ALL RESPONSIBILITY AND LIABILITY FOR PROBLEMS WHICH ARISE FROM FAILURE TO FOLLOW THESE PLANS, SPECIFICATIONS AND THE DRAWINGS INTENT THEY CONVEY, OR FOR PROBLEMS WHICH ARISE FROM OTHER FAILURE TO OBTAIN AND/OR FOLLOW THE ENGINEER'S GUIDANCE WITH RESPECT TO ANY ERRORS, OMISSIONS, INCONSISTENCIES AMBIGUITIES OR CONFLICTS WHICH ARE ALLEGED.

CONTRACTOR TO VERIFY ALL DIMENSIONS AND NOTIFY THE ENGINEER OF ANY DISCREPANCIES BEFORE WORK COMMENCES. DO NOT SCALE DRAWINGS.

SUBJECT TO APPROVAL

02 ISSUED FOR MUNICIPAL APPROVAL K.H. 09 JUN 2023

01 ISSUED FOR MUNICIPAL APPROVAL A.S. 24 DEC 2021

No. REVISIONS BY DATE

Licensed Professional Engineer
 V. JOHNSON
 100510576
 06-09-2023
 PROVINCE OF ONTARIO

NOT AUTHENTIC UNLESS SIGNED AND DATED

LRJ
 ENGINEERING | INGENIERIE
 5430 Canotek Road | Ottawa, ON, K1J 9G2
 www.lri.ca | (613) 842-3434

CLIENT: **LANDRIC HOMES**
 1173 CYRVILLE RD, SUITE 202,
 OTTAWA ON K1J 7S6

DESIGNED BY: K.H. DRAWN BY: K.H. APPROVED BY: V.J.

PROJECT: **NAVAN STACKED TOWN HOMES**
 6001/6005 RENAUD RD,
 OTTAWA, ONTARIO

DRAWING TITLE: **CONSTRUCTION DETAIL PLAN**

PROJECT NO: 210216
 DATE: NOVEMBER 2021

C901



User Inputs

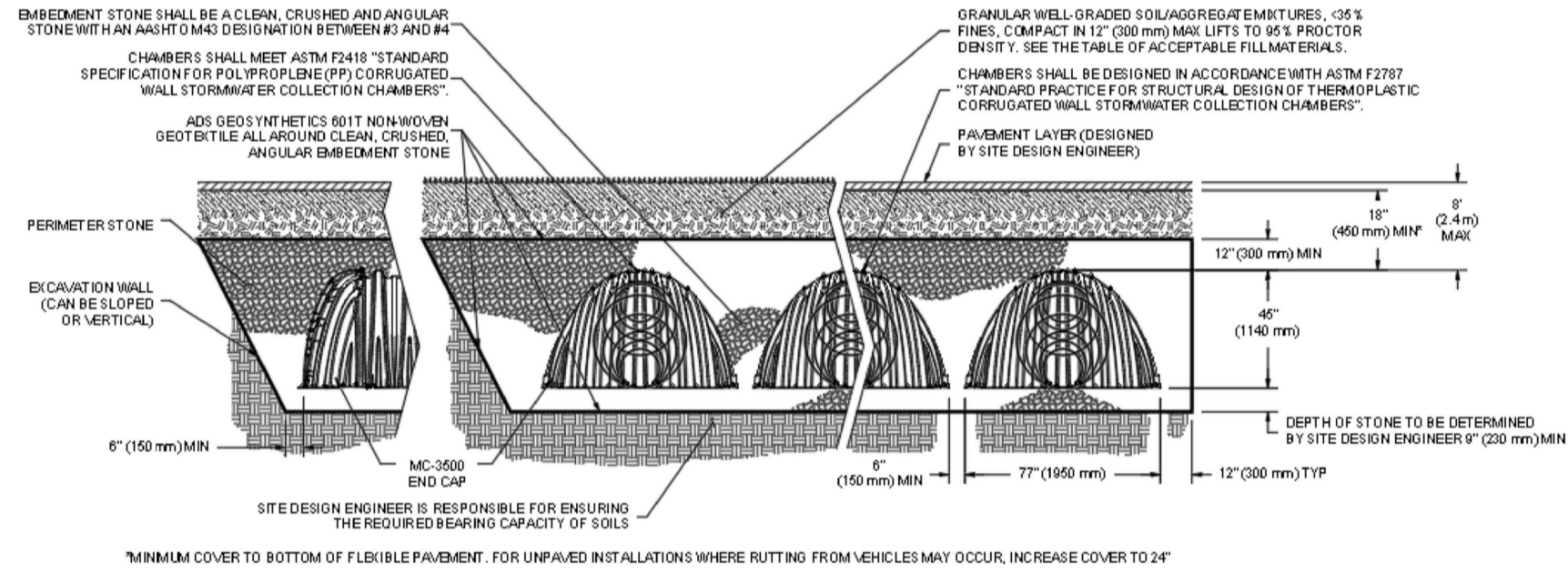
Chamber Model: MC-3500
Outlet Control Structure: No
Project Name: 6001/6005 Renaud
Engineer: N/A
Project Location: Ontario
Measurement Type: Metric
Required Storage Volume: 102.01 cubic meters.
Stone Porosity: 40%
Stone Foundation Depth: 229 mm.
Stone Above Chambers: 305 mm.
Average Cover Over Chambers: 458 mm.
Design Constraint Dimensions: (6.10 m. x 25.00 m.)

Results

System Volume and Bed Size
Installed Storage Volume: 111.11 cubic meters.
Storage Volume Per Chamber: 3.12 cubic meters.
Number Of Chambers Required: 19
Number Of End Caps Required: 4
Chamber Rows: 2
Maximum Length: 24.80 m.
Maximum Width: 4.68 m.
Approx. Bed Size Required: 111.28 square meters.

System Components

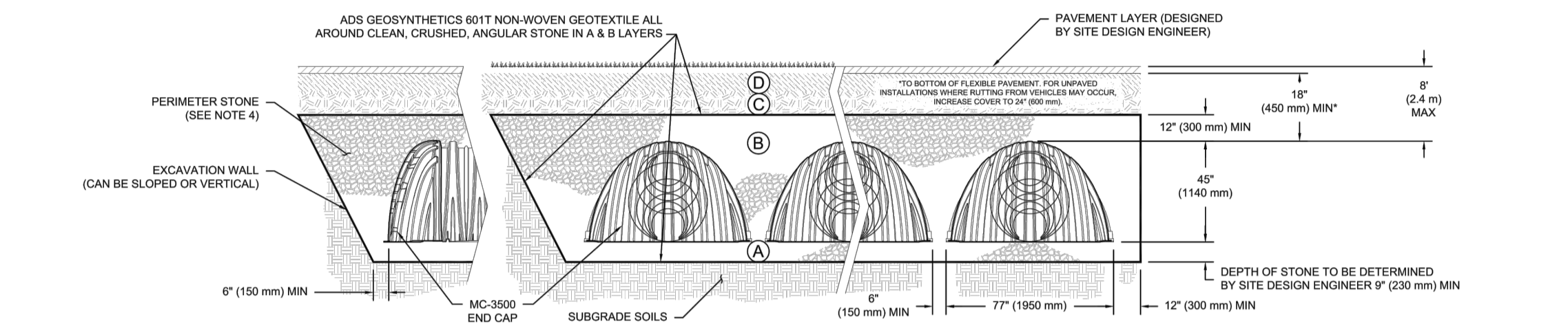
Amount Of Stone Required: 126 cubic meters
Volume Of Excavation (Not Including Fill): 187 cubic meters
Total Non-woven Geotextile Required: 386 square meters
Woven Geotextile Required (excluding Isolator Row): 14 square meters
Woven Geotextile Required (Isolator Row): 74 square meters
Total Woven Geotextile Required: 88 square meters
Impervious Liner Required: 0 square meters



ACCEPTABLE FILL MATERIALS: STORMTECH MC-3500 CHAMBER SYSTEMS

Table with 4 columns: MATERIAL LOCATION, DESCRIPTION, AASHTO MATERIAL CLASSIFICATIONS, COMPACTION / DENSITY REQUIREMENT. Rows A-D describe different layers and materials.

PLEASE NOTE:
1. THE LISTED AASHTO DESIGNATIONS ARE FOR GRADATIONS ONLY...
2. STORMTECH COMPACTION REQUIREMENTS ARE MET FOR ALL LOCATION MATERIALS...
3. WHERE INFILTRATION SURFACES MAY BE COMPROMISED BY COMPACTION...
4. ONCE LAYER 'C' IS PLACED, ANY SOIL MATERIAL CAN BE PLACED IN LAYER 'D' UP TO THE FINISHED GRADE.



- NOTES:
1. CHAMBERS SHALL MEET THE REQUIREMENTS OF ASTM F2418-16a...
2. MC-3500 CHAMBERS SHALL BE DESIGNED IN ACCORDANCE WITH ASTM F2787...
3. THE SITE DESIGN ENGINEER IS RESPONSIBLE FOR ASSESSING THE BEARING RESISTANCE...
4. PERIMETER STONE MUST BE EXTENDED HORIZONTALLY TO THE EXCAVATION WALL...
5. REQUIREMENTS FOR HANDLING AND INSTALLATION:
- TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING...
- TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL...
- TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION...

StormTech Chamber System logo and contact information. Includes phone number 416-735-5255 and website www.stormtech.com.

USE AND INTERPRETATION OF DRAWINGS

GENERAL CONDITIONS OF THE CONTRACT FOR CONSTRUCTION ARE PART OF THE CONTRACT DOCUMENTS AND DESCRIBE USE AND INTENT OF THE DRAWING. THE CONTRACT DOCUMENTS INCLUDE NOT ONLY THE DRAWINGS, BUT ALSO THE OWNER-CONTRACTOR AGREEMENTS, CONDITIONS OF THE CONTRACT, THE SPECIFICATIONS, ADDENDA, AND MODIFICATIONS ISSUED AFTER EXECUTION OF THE CONTRACT.

BY USE OF THE DRAWINGS FOR CONSTRUCTION OF THE PROJECT, THE OWNER CONFIRMS THAT HE HAS REVIEWED AND APPROVED THE DRAWINGS. THE CONTRACTOR CONFIRMS THAT HE HAS VISITED THE SITE, FAMILIARIZED HIMSELF WITH THE LOCAL CONDITIONS, VERIFIED FIELD DIMENSIONS AND CORRELATED HIS OBSERVATIONS WITH THE REQUIREMENTS OF THE CONTRACT DOCUMENTS.

AS INSTRUMENTS OF SERVICE AND COPIES THEREOF FURNISHED BY THE ENGINEER ARE HIS PROPERTY. THEY ARE TO BE USED ONLY FOR THIS PROJECT AND ARE NOT TO BE USED ON ANY OTHER PROJECT, INCLUDING REPEATS OF THE PROJECT. CHANGES TO THE DRAWINGS MAY BE MADE BY THE ENGINEER.

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IN ADDITION, THE CLIENT AGREES TO THE FULLEST EXTENT PERMITTED BY LAW, TO INDEMNIFY AND HOLD HARMLESS LRL FROM ANY DAMAGES, LIABILITIES OR COST, INCLUDING REASONABLE ATTORNEY'S FEES AND COST OF DEFENSE, ARISING FROM SUCH CHANGES.

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CONTRACTOR TO VERIFY ALL DIMENSIONS AND NOTIFY THE ENGINEER OF ANY DISCREPANCIES BEFORE WORK COMMENCES. DO NOT SCALE DRAWINGS.



Table with 4 columns: No., REVISIONS, BY, DATE. Shows revision 02 issued for municipal approval and revision 01 issued for municipal approval.



NOT AUTHENTIC UNLESS SIGNED AND DATED

LRL logo and contact information: ENGINEERING | INGENIERIE, 5430 Canotek Road | Ottawa, ON, K1J 9G2, www.lrl.ca | (613) 842-3434

CLIENT: LANDRIC HOMES, 1173 CYRVILLE RD, SUITE 202, OTTAWA ON K1J 7S6

DESIGNED BY: K.H. DRAWN BY: K.H. APPROVED BY: V.J.

PROJECT: NAVAN STACKED TOWN HOMES, 6001/6005 RENAUD RD, OTTAWA, ONTARIO

DRAWING TITLE: CONSTRUCTION DETAIL PLAN

PROJECT NO: 210216 DATE: NOVEMBER 2021



DRAWINGS/FIGURES

**Proposed Site Plan
Legal Survey
As-builts**



NOT FOR CONSTRUCTION
PAS POUR CONSTRUCTION

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PROJECT TEAM / ÉQUIPE DU PROJET :

NOTE-A :
• ALL DRAWINGS ARE TO BE READ IN CONJUNCTION WITH ALL OTHER DRAWINGS AND SPECIFICATIONS, INCLUDING OTHER CONSULTANTS DRAWINGS AND SPECIFICATIONS. ANY DISCREPANCIES BETWEEN DRAWINGS WILL BE REPORTED TO THE PROJECT LEAD IMMEDIATELY FOR CLARIFICATION PRIOR TO COMMENCING ANY CONSTRUCTION.

NOTE-B :
• ALL GENERAL SITE INFORMATION AND CONDITIONS HAVE BEEN COMPILED FROM EXISTING PLANS AND SURVEYS.

NOTE-C :
• CONTRACTOR IS RESPONSIBLE TO CHECK AND VERIFY ALL DIMENSIONS ON SITE AND REPORT ALL ERRORS AND / OR OMISSIONS TO THE ARCHITECT.

NOTE-D :
• REFER TO LANDSCAPE PLAN FOR ALL EXTERIOR LANDSCAPING.

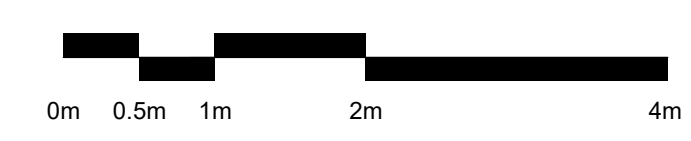
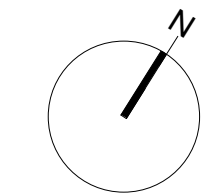
NOTE-E :
• DO NOT SCALE DRAWINGS.

NOTE-F :
• ALL CONTRACTORS MUST COMPLY WITH ALL APPLICABLE CODES AND REGULATIONS.

GENERAL NOTES

SURVEY INFO

TOPOGRAPHIC SURVEY OF :



PROJECT INFORMATION

SITE SUMMARY

ADDRESS	6001-6005 RENAUD, OTTAWA, ON
PROPOSED ZONING	RAZ
SITE AREA	4598.69 m ²
PROPOSED USE	RESIDENTIAL
BUILDING AREA	720.00 m ²

ZONING SUMMARY

	REQUIRED	PROPOSED
LOT AREA	N/A	2913.14 m ²
LOT WIDTH	N/A	76.12 m
MAX. BUILDING HEIGHT	18.00 m	12.02 m
MAX. PARAPET HEIGHT	N/A	N/A
SET BACKS :		
- FRONT YARD	3.00 m	5.39 m
- CORNER SIDE YARD	3.00 m (min.)	N/A
- INTERIOR SIDE YARD	3.00 m / 6.00 m	3.10 m
- REAR YARD	6.00 m	15.88 m
- ADDITIONAL REQ	N/A	N/A
MIN LANDSCAPED AREA	30% OF LOT	35% (1021.6 m ²)

VEHICULAR PARKING

	REQUIRED	PROPOSED
MIN PARKING SPACES	24	24 (10 int)
MIN VISITOR PARKING SPACES	4	4
MIN ACCESSIBLE PRKG SPACES (incl. in count)	1	1

BICYCLE PARKING

	REQUIRED	PROPOSED
MIN PARKING SPACES	5	8

WASTE CONTAINERS

	REQUIRED	PROPOSED
GARBAGE (0.231 y ³ / unit)	5	6
RECYCLING GMP (0.018 y ³ / unit)	2	2
RECYCLING FIBRE (0.062 y ³ / unit)	2	2
ORGANICS (L)	240	240

AMENITY AREA

	REQUIRED	PROPOSED
PRIVATE	60.00 m ²	151.00 m ² BALCONIES
COMMUNAL	60.00 m ²	107.00 m ² EXTERIOR

BUILDING SUMMARY

	UNITS	GFA - GRC
SEMI-BASEMENT	20	420.00 m ²
GROUND		313.00 m ²
LEVEL 2		361.00 m ²
LEVEL 3	20	321.00 m ²

SITE CONTEXT



LEGEND

- PROPOSED GRASS
- RIVERSTONE
- CONCRETE PAVERS
- POURED CONCRETE
- ASPHALT PAVING
- PROPOSED NEW BUILDING
- CONCRETE RETAINING WALL
- EXISTING BUILDING TO BE DEMOLISHED

LINES

- PROPERTY LINE
- SETBACK LINE
- EXISTING FENCE
- NEW FENCE
- OVERHEAD WIRES

VEGETATION

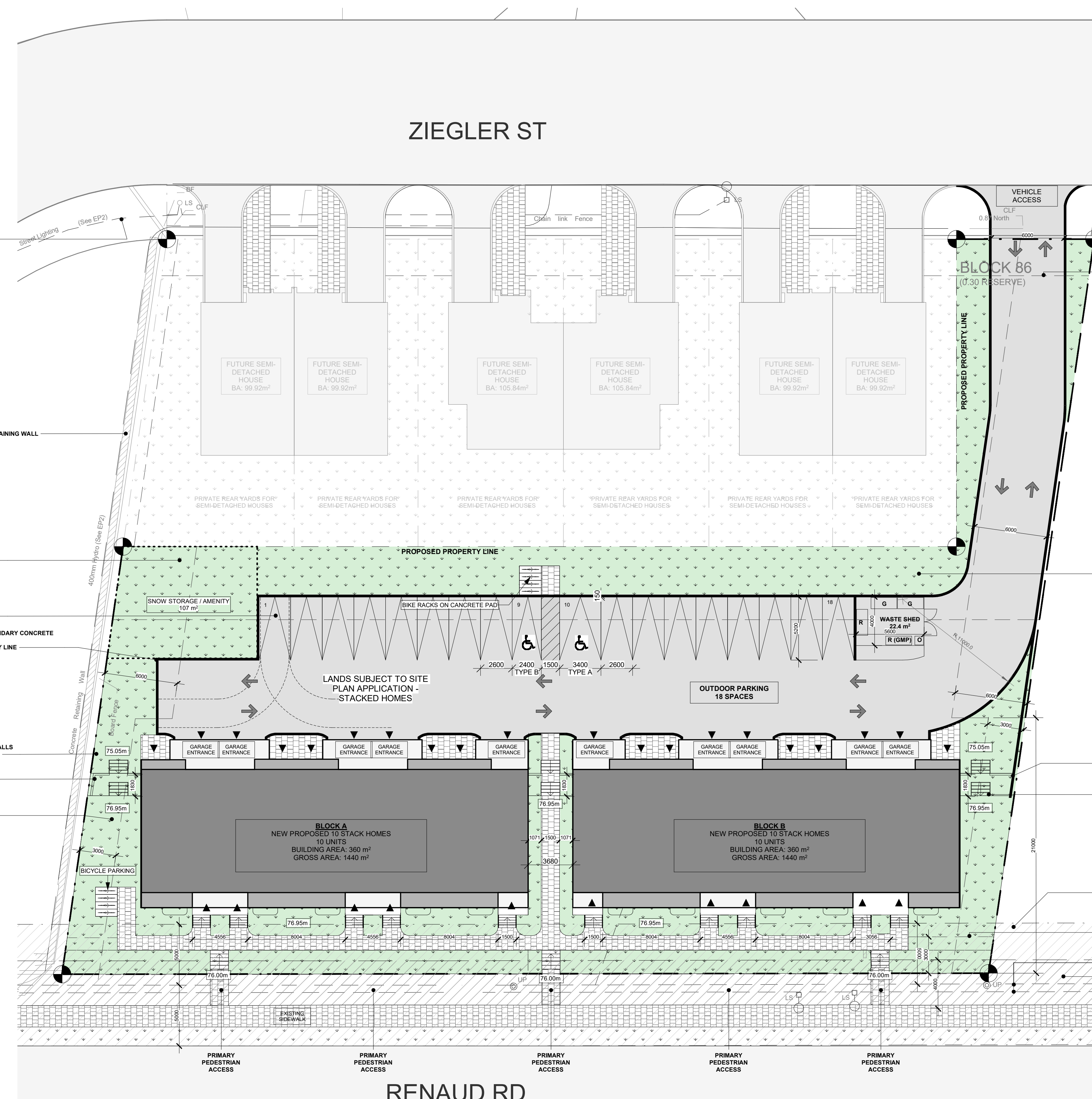
- TREE: EXISTING TO REMAIN
- TREE: EXISTING TO BE REMOVED
- TREE: NEW PROPOSED
- SHRUB: NEW PROPOSED

SYMBOLS

- DIRECTIONAL ARROWS
- BUILDING ACCESS
- BUILDING EGRESS
- SIAMESE CONNECTION
- UTILITY POLE
- FIRE HYDRANT
- CATCH BASIN / MANHOLE
- DEPRESSED CURB
- LANDSCAPE LIGHT
- LIGHT POLE
- WALL MOUNTED LIGHT
- EXISTING GRADE ELEVATION
- PROPOSED GRADE ELEVATION
- LOT CORNERS

PARKING

- BIKE PARKING
- CAR PARKING
- BF PARKING (TYPE A)
- BF PARKING (TYPE B)



1 SITE PLAN
A050 1 : 200

KEY PLAN / PLAN CLÉ :



CLIENT :



1.7	ISSUED FOR SPC	23-04-28
1.6	ISSUED FOR SPC	23-04-05
1.4	ISSUED FOR 66%	23-02-24
1.3	City discussion	22-11-16
1.2	City discussion	22-10-27
1.1	Issued for 33%	22-10-12
1.0	SITE PLAN	22-10-11

PROJECT NAME / NOM DU PROJET :

6001-6005 Renaud

DRAWING NAME / NOM DU DESSIN :

SITE PLAN

DRAWING INFORMATION / INFORMATION DU DESSIN :

PROJECT NO. / NO. DE PROJET :	22170
DATE :	2023-04-28
DRAWN BY / DESSINÉ PAR :	E.T.
REVIEWED BY / VÉRIFIÉ PAR :	L.G.
SCALE / ÉCHELLE :	As indicated
PROJECT PHASE / PHASE DU PROJET :	1
DWG NO. / NO. DESSIN :	A050
REVISION NO. / NO. DE RÉVISION :	1.7

PART OF LOT 7
CONCESSION 3 (OTTAWA FRONT)
(Geographic Township of Gloucester)
CITY OF OTTAWA

Surveyed by Annis, O'Sullivan, Vollebek Ltd.

Scale 1 : 250



Metric
DISTANCES SHOWN ON THIS PLAN ARE IN METRES AND
CAN BE CONVERTED TO FEET BY DIVIDING BY 0.3048

Surveyor's Certificate

I CERTIFY THAT:

- 1. This survey and plan are correct and in accordance with the Surveys Act, the Surveyors Act and the regulations made under them.
- 2. The survey was completed on May 7, 2021.

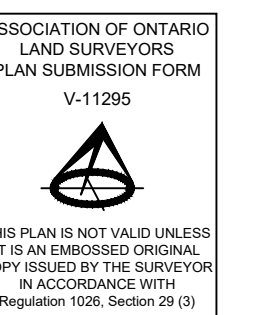
May 14, 2021 Date "Tyler Allison"
Tyler J. Allison
Ontario Land Surveyor

Rev.	Date	Add Pole Conductors and Pole Transformer
1	Oct. 1/21	

ANNIS, O'SULLIVAN, VOLLEBEK LTD. grants to Landis Homes ("The Client"), their solicitors, mortgagees, and other related parties, permission to use original, signed, sealed copies of the Topographical Plan of Survey in transactions involving The Client.

Notes & Legend

- Denotes
- Survey Monument Planted
- Survey Monument Found
- Standard Iron Bar
- Short Standard Iron Bar
- Iron Bar
- Origin Unknown
- N&W Nail & Washer
- Witness
- Measured
- Annis, O'Sullivan, Vollebek Ltd.
- Registered Plan 4M-1400
- Registered Plan 4M-1373
- Plan 5R-5324
- Plan by Slattec Job No. 161650000-109, Ref 4M-1400
- Plan and Profile of Ziegler Street (T.L. Mak Engineer Consultants, Project 805-47) Drawing P-2 Rev. 5
- "As Recorded" 07/22/14
- City of Ottawa U.C.C. Central Registry Data, Sheet J-29-24 Dated August 2015
- Plan and Profile of Renaud Road (Slattec Project 160400704) Drawing PP-2 Rev. 7
- "As Recorded" 11/11/21
- City of Ottawa U.C.C. Central Registry Data, Sheet J-29-30 Dated August 2015
- Inst. CT257733
- Deciduous Tree
- Coniferous Tree
- Fire Hydrant
- Maintenance Hole (Storm Sewer)
- Maintenance Hole (Sanitary)
- Maintenance Hole (Unidentified)
- Catch Basin
- Gas Meter
- Sign
- Chain Link Fence
- Board Fence
- Utility Pole
- Light Standard
- Air Conditioner
- Diameter
- Location of Elevations
- Top of Concrete Curb Elevation
- Top of Retaining Wall Elevation
- Centreline
- Property Line
- Underground Storm Sewer
- Underground Sanitary Sewer
- Underground Water
- Underground Power
- Underground Gas
- Overhead Wires



Bearings are grid, derived from Can-Net 2016 Real Time Network GPS observations and are referenced to Specified Control Points 01919880184 and 019198434761, MTM Zone 9 (76°30' West Longitude) NAD-83 (original).

Coordinate values are to urban accuracy in accordance with O. Reg. 216/10.

01919880184 Northing 5040610.16 Easting 384736.56
019198434761 Northing 5036178.12 Easting 372436.11

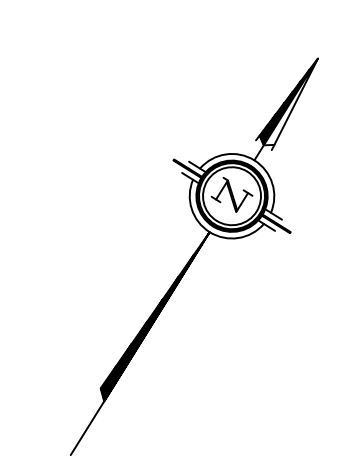
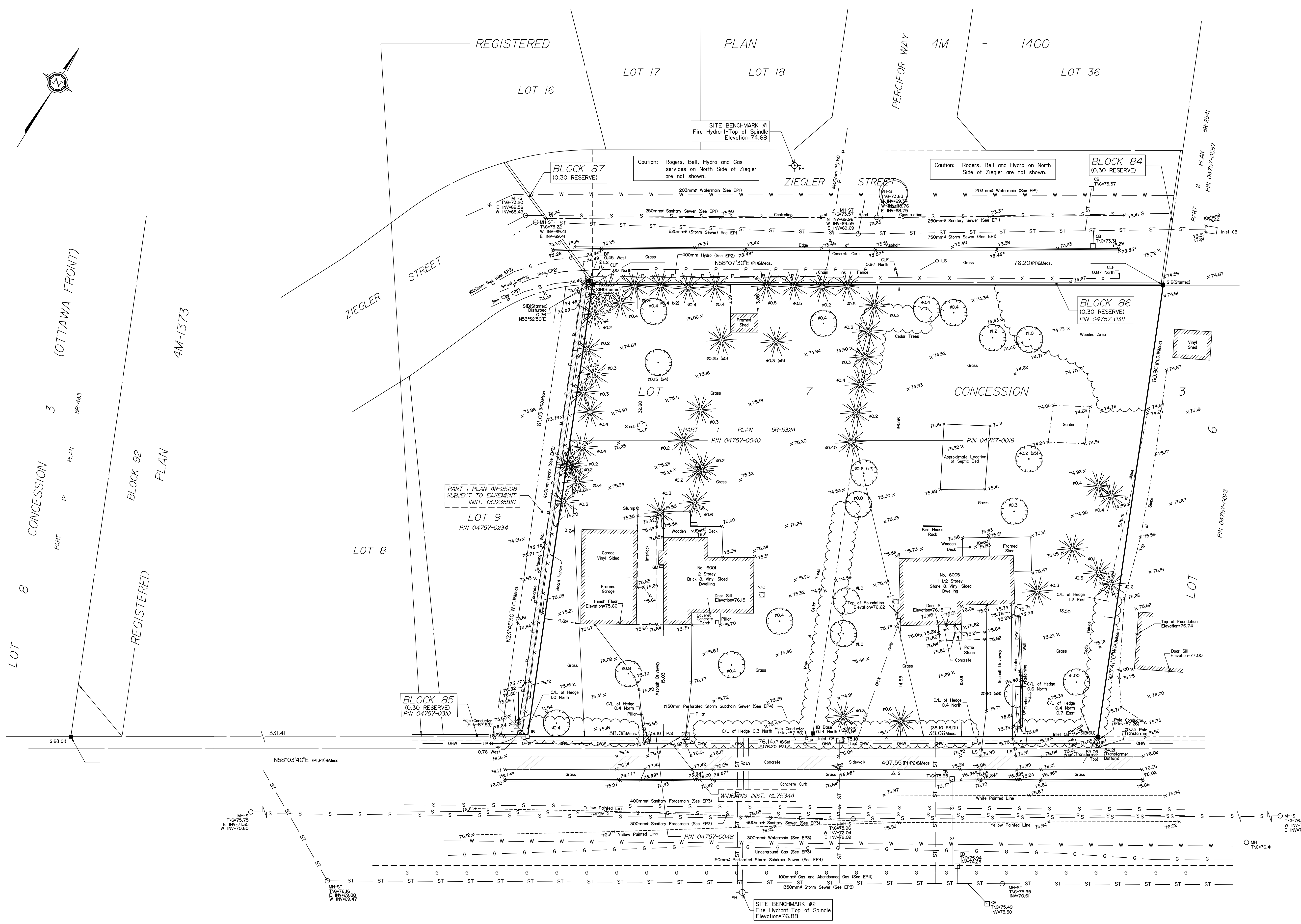
ELEVATION NOTES

- 1. Elevations shown are geoidic and are referred to the CGVD28 geoid datum.
- 2. It is the responsibility of the user of this information to verify that the job benchmark has not been altered or disturbed and that it's relative elevation and description agrees with the information shown on this drawing.

UTILITY NOTES

- 1. This drawing cannot be accepted as acknowledging all of the utilities and it will be the responsibility of the user to contact the respective utility authorities for confirmation.
- 2. Only visible surface utilities were located.
- 3. A field location of underground plant by the pertinent utility authority is mandatory before any work involving breaking ground, probing, excavating etc.
- 4. Underground services (including invert elevations) shown are compiled from EP1, EP2, EP3 and EP4 and are subject to field confirmation.

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ANNIS, O'SULLIVAN, VOLLEBEK LTD.
165 Bay Street
Etobicoke, Ont. M9A 1W1
Phone: (613) 443-3364
Email: annis@annisovl.com
Ontario Land Surveyors
Reg. No. E-1136-2

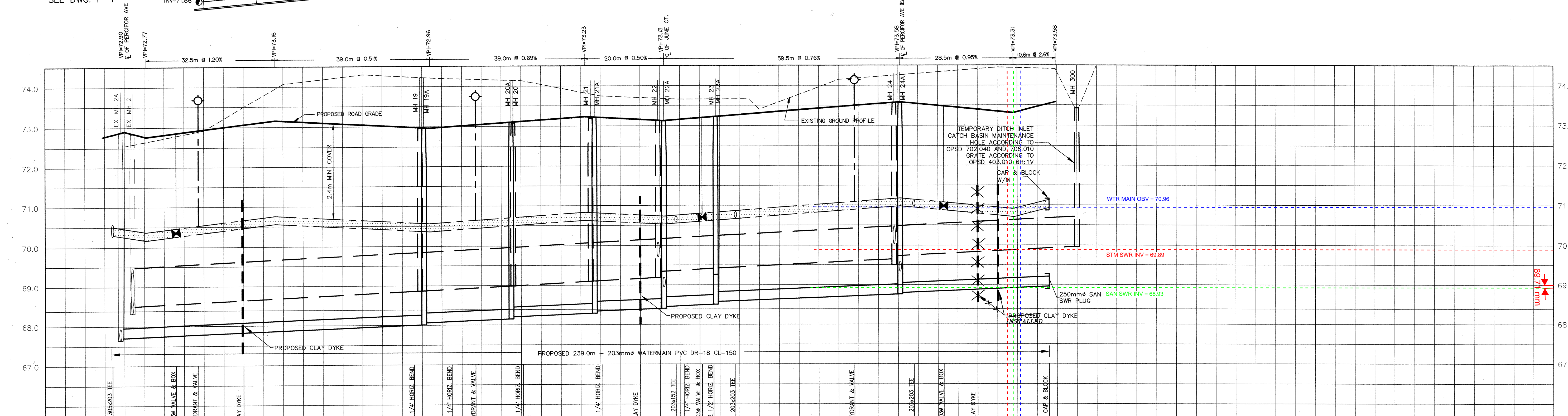
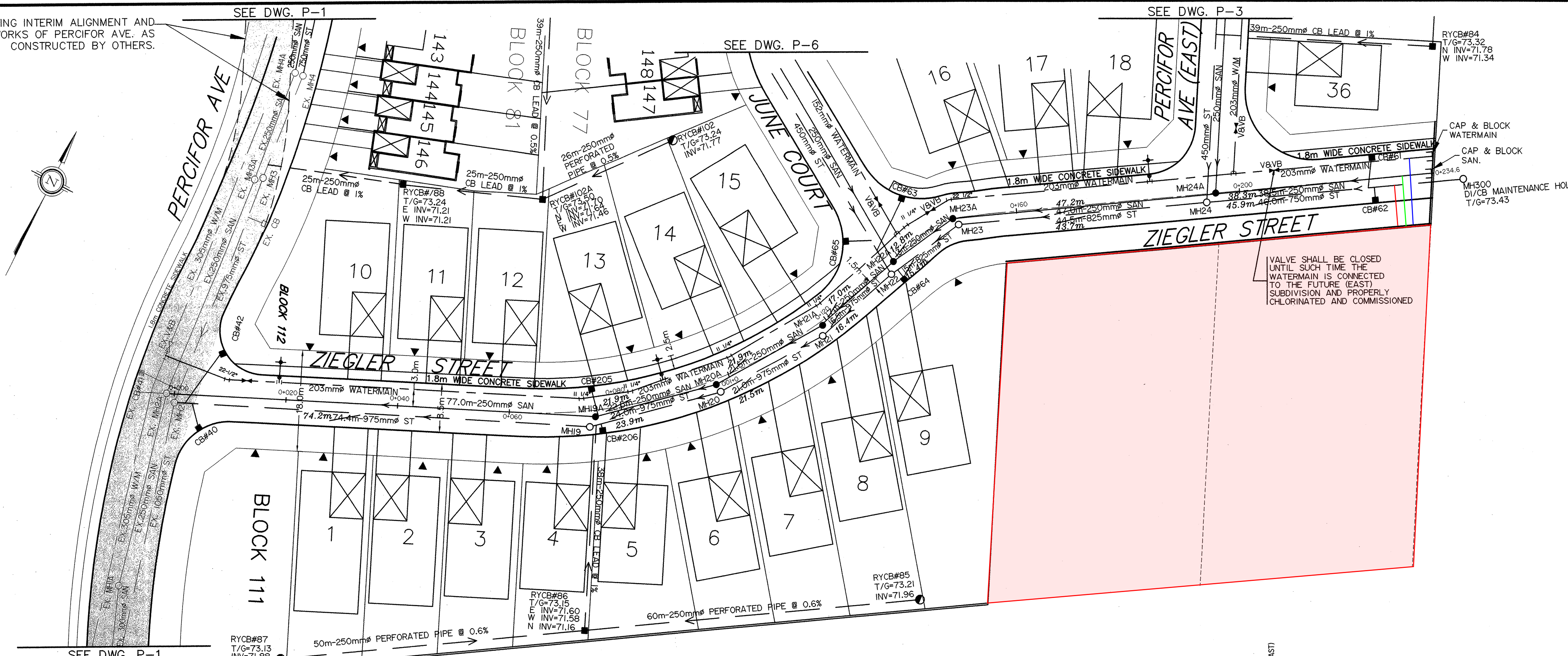


LOT 8
CONCESSION 3
PART 12
PLAN 5R-443
BLOCK 92
PLAN 4M-1373
REGISTERED

ROAD ALLOWANCE BETWEEN CONCESSIONS 3 AND 4 (OTTAWA FRONT) KNOWN AS RENAUD ROAD (FOURTH LINE ROAD)

EXISTING INTERIM ALIGNMENT AND SURFACE WORKS OF PERCIVOR AVE. AS CONSTRUCTED BY OTHERS.

"T.L. MAK ENGINEERING CONSULTANTS LTD. AGREED TO PERFORM A GENERAL REVIEW OF CONSTRUCTION ACTIVITIES DURING THE INSTALLATION OF SANITARY AND STORM SEWERS AND A WATERMAIN FOR THIS PROJECT. IT IS T.L. MAK ENGINEERING CONSULTANTS LTD.'S OPINION, TO THE BEST OF KNOWLEDGE AVAILABLE, THAT THIS WORK HAS BEEN DONE IN GENERAL CONFORMANCE WITH CITY OF OTTAWA STANDARDS ACCORDING TO THE DESIGN AND DRAWINGS THAT HAVE BEEN APPROVED BY THE CITY OF OTTAWA."



PROPOSED CENTER LINE OF ROAD ELEVATIONS	72.90	72.77	72.84	73.16	73.15	73.05	72.96	72.88	73.12	73.13	73.16	73.23	73.21	73.13	73.16	73.31	73.46	73.54	73.35	73.31	73.58
TOP OF WATERMAIN ELEVATIONS	70.95	70.87	70.86	70.85	70.76	70.67	70.72	70.72	70.72	70.72	70.72	70.72	70.72	70.72	70.72	70.72	70.72	70.72	70.72	70.72	70.72
STORM SEWER INVERTS	67.64	67.52	67.49	67.49	67.49	67.49	67.49	67.49	67.49	67.49	67.49	67.49	67.49	67.49	67.49	67.49	67.49	67.49	67.49	67.49	67.49
SANITARY SEWER INVERTS	67.64	67.52	67.49	67.49	67.49	67.49	67.49	67.49	67.49	67.49	67.49	67.49	67.49	67.49	67.49	67.49	67.49	67.49	67.49	67.49	67.49
EXISTING ELEVATION	74.30	74.30	74.30	74.30	74.30	74.30	74.30	74.30	74.30	74.30	74.30	74.30	74.30	74.30	74.30	74.30	74.30	74.30	74.30	74.30	74.30
CHAINAGE	0+003	0+003	0+005	0+005	0+005	0+005	0+005	0+005	0+005	0+005	0+005	0+005	0+005	0+005	0+005	0+005	0+005	0+005	0+005	0+005	0+005

- NOTES:
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 - ANY SURFACE OR SUBSURFACE INFORMATION AND DATA FURNISHED TO THE CONTRACTOR IN RELATION TO THE CONTRACT AS INDICATED ON THE DRAWINGS OR BY REPORT, IS NOT INTENDED AS A REPRESENTATION OF WARRANTY, BUT IS FURNISHED IN ORDER THAT THE CONTRACTOR MAY HAVE ACCESS TO THE SAME INFORMATION WHICH IS AVAILABLE TO THE OWNER AND ENGINEERS WILL NOT BE RESPONSIBLE FOR THE ACCURACY THEREOF OR ANY DEDUCTION, INTERPRETATION OR CONCLUSION DRAWN THEREFROM BY THE CONTRACTOR.
 - CONTRACTOR IS ADVISED TO COLLECT INFORMATION ON SOIL CONDITIONS AS DEEMED NECESSARY.
 - CONSTRUCT CLAY DYKE AS SHOWN ON THE LOCATION OF THIS DRAWING AND REFER TO DWG. NO. CD-1 FOR DETAILS.
 - ROADWAY CATCH BASIN LEAD SHALL BE 200mm PVC AT SLOPE OF 1% UNLESS OTHERWISE NOTED.
 - REFER TO STATNEX CONSULTING'S SIRM REPORT INLET CONTROL DATA TABLE FOR DETAILS OF CB LEAD INVERT ELEVATION AND INLET CONTROL DEVICE (ICD) INSERTS.
 - SEWER BEDDING SHALL BE CLASS "B" UNLESS OTHERWISE NOTED.
 - CONSTRUCT ALL STORM AND SANITARY SEWER SYSTEMS IN ACCORDANCE WITH CITY OF OTTAWA'S LATEST REVISED STANDARDS OTHERWISE AS PER OPSS REQUIREMENTS AND DONE TO THE SATISFACTION OF THE ENGINEERS AND THE CITY.
 - ALL WATERWORKS TO BE CONSTRUCTED TO THE CITY OF OTTAWA'S LATEST REVISED STANDARDS AND REQUIREMENTS.
 - CATHODIC PROTECTION FOR PVC PRESSURE PIPE WATERMAIN SYSTEM AS PER CITY'S WS-40 DETAILS.
 - MAXIMUM ALLOWABLE DEFLECTION IS 1% PER PIPE FOR 150mm AND 200mm DIAMETER WATERMAIN.

NO.	REVISION	DATE	BY
5	AS RECORDED	07/22/14	TLM
4	ADDED 1.8m SIDEWALK ON ZIEGLER ST. AND ADJUSTED HYDRANT LOCATION	04/01/09	TLM
3	REVISED REF. NO. OF LOTS & TOWNS PER SUBDIVISION 4M-PLAN AND PER CITY'S COMMENTS OF 10/09/08	02/23/09	TLM
2	REVISIONS AS PER CITY'S COMMENTS OF AUG.14/08	09/12/08	TLM
1	REVISIONS AS PER CITY'S COMMENTS OF FEB./08	06/10/08	TLM

RECORD DRAWING
DATE July 22/14

SCALE	DESIGN	T.L.M.
1:500 HORIZONTAL	CHECKED	T.L.M.
1:50 VERTICAL	CHECKED	T.L.M.
	APPROVED	T.L.M.

PROJECT LOCATION
PART OF LOT 7, CONCESSION 3 (OF)
GEOGRAPHIC TOWNSHIP OF GLOUCESTER
CITY OF OTTAWA
FORMERLY IN THE CITY OF GLOUCESTER

PROJECT
**JEAN GUY RIVARD SUBDIVISION
BRADLEY ESTATES NORTH
PLAN AND PROFILE
ZIEGLER STREET (STA. 0+003 TO 0+240)**

T.L. MAK ENGINEERING CONSULTANTS LTD.
CONSULTING ENGINEERS

PROJECT No. 805-47 DATE FEBRUARY 2007 DRAWING No. P-2

14962

D07-16-07-009