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ADEQUACY OF SERVICES REPORT

FOR

BARRHAVEN CONSERVANCY DEVELOPMENT CORPORATION

BARRHAVEN CONSERVANCY EAST PHASE 5

CITY OF OTTAWA

PROJECT NO.: 20-1180

DECEMBER 2022 – 1ST SUBMISSION

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**ADEQUACY OF SERVICES REPORT
FOR
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**CITY OF OTTAWA
PROJECT NO: 20-1180**

1.0 INTRODUCTION

David Schaeffer Engineering Limited (DSEL) has been retained to update an Adequacy of Services Report (AES) in support of the Barrhaven Conservancy “Phase 5” development area on behalf of Barrhaven Conservancy Development Corporation (BCDC). This area (being referred to as “Phase 5”) is part of a previously approved draft plan of subdivision within the greater Barrhaven Conservancy development area (City file no. D07-16-20-0021).

The overall Conservancy land area is approximately 139.7 ha (all land use components) and is located within the City of Ottawa urban boundary in the Barrhaven ward. As illustrated in **Figure 1**, the site is located north of the Jock River, east of Highway 416, west of Greenbank Road (and the Kennedy-Burnett Stormwater Facility), and south of both McKenna Casey Drive and Strandherd Drive.

The focus of this report is for the **Conservancy East (Phase 5)** draft plan area consisting of vacant land that is located east of the existing Foster Ditch, which bisects the overall BCDC landholdings, and west of Borrisokane Road. The subject lands are an approximately 19.4 ha irregular parcel including parts of 3288, and 3300 Borrisokane Road. Of this, approximately 13.82 ha in area (including right-of-ways environmental areas and open space) are considered in the servicing review with the proposed updated development draft plan **Figure 2B** provided in the **Drawings** section of this report for reference. Also provided is Figure 2A which illustrates the portion of the prior approved draft plan and the “Phase 5” area being revised. The development area is planned to be developed with a mix of detached single homes, townhomes, park blocks, open spaces and a road network.

The Conservancy East Phase 5 development area is outside of the Jock River 100-year limit as confirmed by the Rideau Valley Conservation Authority (RVCA). Refer to the RVCA confirmation letter in **Appendix D**. The 100-year regulatory flood line is demonstrated in Drawing 1 (Grading) and Drawing 3 (Stormwater) in the **Appendix**.

The objective of this report is to provide sufficient detail to demonstrate that the updated development plan area can be supported by municipal services.

1.1 Existing Conditions

The **Conservancy East (Phase 5)** property is relatively flat with the existing elevations ranging from ~91.5 m in the north to 91 m in the south. All existing flows are either overland to the Jock River or conveyed to the Jock River by way of the Foster Ditch and Borrisokane Road ditches which is adjacent to the subject property. The property is within the Jock River watershed and is under the jurisdiction of the RVCA.

1.2 Summary of Pre-Consultation

The following provides a summary of the pre-consultation:

1.2.1 Ministry of the Environment, Conservation and Parks (MECP)

Prior consultations associated with the Conservancy Phase 2-4 development east of Borrisokane Road were previously undertaken for the approval of those phases of the development area.

A pre-consultation with the local MECP office has not yet been completed for the balance of the Conservancy development area until the functional design details and requirements have been finalized with the City of Ottawa.

1.2.2 Rideau Valley Conservation Authority (RVCA)

Multiple consultations, analysis and submissions were coordinated with the RVCA to establish that the development area is outside of the Jock River 100-year limit. See the RVCA documentation in **Appendix D** for reference.

1.3 Existing Permits / Approvals

Key approvals associated with the advancement of development of the Barrhaven Conservancy area, are presented in the following table. The most relevant approvals are the Environmental Compliance Approval (ECA) for the South Nepean Collector sanitary trunk sewer as well as sanitary sewer ECA for the Conservancy development area east of Borrisokane Road. The documents are provided in **Appendix A** for reference.

Table 1A: Existing Permits / Approvals

Agency	Approval Type	Approval Number	Remarks
Ministry of the Environment, Conservation and Parks (MECP)	Environmental Compliance Approval	# 8129-AB7LDF (June 23, 2016)	South Nepean Collector existing approval (sanitary outlet for development area)
(MECP)	Environmental Compliance Approval	# 4357-CHMQEM (Sept. 1, 2022)	Sanitary and storm sewer approvals for Conservancy lands east of Borrisokane Road
MECP	Permit to take Water	#5633-C2RQPL (May 26, 2021)	Water taking from Building Excavation, Site Servicing, SWMW, In-Water Works, Poned Surface Water
Rideau Valley Conservation Authority (RVCA)	RVCA Letter of Permission under O.Reg. 174/06	RV5-4419	Letter of permission related to placement of fill within a regulated area.

1.4 Required Permits / Approvals

The City of Ottawa must approve detailed engineering design drawings and reports prior to future construction of the municipal infrastructure identified in this report. This will occur as part of the Plan of Subdivision application process and detailed design.

Based on pre-consultation with City staff, the additional approvals and permits listed in the following table are expected to be required prior to construction of the municipal infrastructure detailed herein. Please note that other permits and approvals may be required, as detailed in the other studies to be submitted as part of the Plan of Subdivision application (e.g. *Tree Conservation Report, Environmental Impact Statement, Phase 1 Environmental Site Assessment, Headwater Drainage Feature Assessment, etc.*)

Table 1B: Required Permits/Approvals

Agency	Permit/Approval Required	Trigger	Remarks
MECP	Environmental Compliance Approval	Construction of new sanitary and storm sewers throughout the subdivision.	The MECP will review the sanitary and storm sewer design through the City of Ottawa transfer of review process.
MECP	Environmental Compliance Approval	Implementation of oil-grit separator units and LIDs for quality control.	The MECP will review the stormwater management appurtenance design through the City of Ottawa transfer of review process.

MECP	Permit to Take Water	Construction of proposed land uses (e.g. basements for residential homes) and services.	Pumping of groundwater may be required during construction, given groundwater conditions and proposed land uses and on-site/off-site municipal infrastructure.
City of Ottawa	MECP Form 1 – Record of Watermains Authorized as a Future Alteration.	Construction of watermains throughout the subdivision	The City of Ottawa will review the watermains on behalf of the MECP through the Form 1 – Record of Watermains Authorized as a Future Alteration.
RVCA	Permit under Ontario Regulation 174/06, RVCA's Development, Interference with Wetlands and Alterations to Shorelines and Watercourses Regulation	Grading (proposed development & potential temporary access roads) within the subject lands (i.e. crossing of Fraser-Clarke Watercourse)	Supporting applications and documentation as required through consultation with the RVCA.
RVCA	Outlets to Jock River	In conjunction with issuance of MECP applications	Supporting applications and documentation as required through consultation with the RVCA.
RVCA	Alteration to Watercourses	As necessary through consultation with the RVCA	Supporting applications and documentation as required through consultation with the RVCA.
City of Ottawa	Commence Work Notification (CWN)	Construction of new sanitary and storm sewers throughout the subdivision	The City of Ottawa will issue a commence work notification for construction of the sanitary and storm sewers once an approval is issued by the MECP.

2.0 GUIDELINES, PREVIOUS STUDIES, AND REPORTS

2.1 Existing Studies, Guidelines, and Reports

The following studies were utilized in the preparation of this report.

- Ottawa Sewer Design Guidelines, City of Ottawa, *SDG002*, October 2012 (*City Standards*)

- Technical Bulletin ISDTB-2014-01
City of Ottawa, February 5, 2014
(ITSB-2014-01)
- Technical Bulletin PIEDTB-2016-01
City of Ottawa, September 6, 2016
(PIEDTB-2016-01)
- Technical Bulletin ISTB-2018-01
City of Ottawa, March 21, 2018
(ISTB-2018-01)
- Technical Bulletin ISTB-2018-04
City of Ottawa, June 27, 2018
(ISTB-2018-04)
- Ottawa Design Guidelines – Water Distribution
City of Ottawa, July 2010.
(*Water Supply Guidelines*)
 - Technical Bulletin ISD-2010-2
City of Ottawa, December 15, 2010.
(ISD-2010-2)
 - Technical Bulletin ISDTB-2014-2
City of Ottawa, May 27, 2014.
(ISDTB-2014-2)
 - Technical Bulletin ISTB-2018-02 / ISTB-2019-02
City of Ottawa, March 21, 2018 / July 08, 2019
(ISTB-2018-02 / ISTB-2019-02)
- Design Guidelines for Sewage Works,
Ministry of the Environment, Conservation and Parks, 2008. (formerly MOECC)
(*MECP Design Guidelines*)
- Stormwater Planning and Design Manual,
Ministry of the Environment, March 2003.
(*SWMP Design Manual*)
- City of Ottawa Official Plan,
adopted by Council 2003.
(*Official Plan*)
- City of Ottawa Secondary Plan – Former Nepean – South Nepean Urban Area –
Areas 9 and 10,
Adopted by Council 2003.
(*Secondary Plan*)

- South Nepean Collector: Phase 2 Hydraulics Review / Assessment Technical Memorandum
Novatech, August 2015
(*Novatech SNC Memo*)
- South Nepean Collector: Phase 2 Preliminary Design Report,
Novatech, March 2016
(*Novatech SNC Design Report*)
- Strandherd Drive Widening Project, South Nepean Collector: Phase 3 Sanitary Flow Calculations
Novatech, May 2019
(*2019 Novatech SNC Design Report*)
- Hydraulic Potable Water Assessment for Barrhaven Conservancy Development Corporation, March 2021
(*Stantec Hydraulic Analysis*)
- Jock River Reach One Subwatershed Study
Stantec, 2007
(*Jock River SWS*)
- Geotechnical Investigation, Proposed Residential Development, Conservancy Lands East, Ottawa, Ontario
Paterson Group, September 24, 2019 (Project No. PG5036-1)
(*Geotechnical Report*)
- Environmental Impact Statement for Barrhaven Conservancy East
Kilgour & Associates Ltd., July 29, 2020
(*Kilgour EIS*)
- Barrhaven Conservancy East (Phases 2, 3, 4 & Jock River): Water Distribution System Analysis, Stantec, June 2, 2022
(*Stantec Hydraulic Analysis - East*)
- Adequacy of Services Report for Barrhaven Conservancy Development Corporation, Barrhaven Conservancy East
David Schaeffer Engineering Ltd., July 2021
(*DSEL East FSR*)
- Design Brief for Barrhaven Conservancy East – Phase 2, 3, & Jock River
David Schaeffer Engineering Ltd., June 2022
(*DSEL East Design Brief*)

3.0 WATER SUPPLY SERVICING

3.1 Existing Water Supply Services

The subject property is located adjacent to the City of Ottawa's Pressure Zone (PZ) 3SW (previously known as PZ BARR). PZ SUC services the lands that are east of the subject property, as well as south of the Jock River.

The City of Ottawa has recently reconfigured the pressure zones servicing Barrhaven and the South Urban Community (SUC) in order to improve reliability and efficiency and to increase pumping capacity to accommodate for future growth in the area. Work is ongoing. There are three pumping stations servicing Zone 3SW and Zone SUC as follows: the Fallowfield Road Pumping Station (FRPS), the Barrhaven Pumping Station (BPS) and the Ottawa South Pumping Station (OSPS).

There are future trunk watermains proposed in the vicinity of the subject property (i.e. along Greenbank Road) which will provide water service to development lands to the east and south of Conservancy East. These services will be further extended to provide the requisite water supply to the development area.

3.2 Water Supply Servicing Design

Stantec Consulting Limited was retained to perform a hydraulic assessment for the Conservancy East Lands. The ***Hydraulic Potable Water Assessment for Barrhaven Conservancy Development Corporation (Stantec Hydraulic Analysis)*** prepared by Stantec (March 2021) previously supported the advancement of the Conservancy East lands east of Borrisokane road. Subsequently, as part of the detailed design for the approved phases east of Borrisokane Road, Stantec prepared an updated study "***Barrhaven Conservancy East (Phases 2, 3, 4 & Jock River): Water Distribution System Analysis*** (June 2022 – ***Stantec Hydraulic Analysis - East***) which is enclosed in ***Appendix B*** for reference. Note that phasing references have changed for the development area and the "Phase 4" area referenced in the Stantec study represents the "Phase 5" which is the subject of this updated draft plan – See Figure 1-2 of the ***Stantec Hydraulic Analysis – East*** study for reference. As well, the layout analyzed in the Stantec analysis differs slightly but is not expected to impact the serviceability.

The analysis reviewed the system requirements of the development area on the west and east sides of Borrisokane Road but only the detailed design of the areas east of Borrisokane Road were advanced to detailed design.

The proposed water servicing layout is presented in ***Figure 3***.

The following table summarizes the relevant Water Supply Design Criteria which will be employed in the design of the subject property.

Table 2A: Water Supply Design Criteria

Design Parameter	Value
<i>Extracted from Section 4: Ottawa Design Guidelines, Water Distribution (July 2010)</i>	
Residential – Detached Single	3.4 p/unit
Residential – Townhome/ Semi	2.7 p/unit
Residential – Apartment	1.8 p/unit
Minimum Watermain Size	150 mm diameter
Minimum Depth of Cover	2.4 m from top of watermain to finished grade
During normal operating conditions desired operating pressure is within	350 kPa and 480kPa
During fire flow operating pressure must not drop below	140 kPa
<i>Stantec Hydraulic Analysis, Stantec, July 20, 2017 for Population Exceeding 3000 Persons</i>	
Residential – Detached Single	180 L/cap/day
Residential – Rear Lane Town	198 L/cap/day
Residential – Back-to-Back	198 L/cap/day
Outdoor Water Demand	1049 L/unit/day (single detached)
Basic Day	Population x Demand
Max Day	Basic Day + Outdoor Water Demand

3.2.1 Fire Flow Demand

Fire Flow requirements are established in the boundary condition request found in **Appendix B** as prepared by Stantec. Based on anticipated unit configurations and separations the City’s fire flow cap of 10,000 L/min for single dwellings and traditional townhomes as outlined in *ISDTB-2014-02* does not apply and separation of fire areas with units of ordinary construction, as well as architectural elements, are required to meet target fire flows. The fire flows are calculated in accordance with the Fire Underwriters Survey’s Water Supply for Public Fire Protection Guideline (1999). Detailed FUS calculations can be found in the Stantec reporting.

3.2.2 Boundary Conditions

To support the preparation of a hydraulic analysis for the subdivision, boundary conditions were provided by the City of Ottawa for the anticipated water demands and are summarized in the following table. See **Appendix B** for full details of the boundary condition request submitted.

Table 2B: Boundary Conditions (from *Stantec Hydraulic Analysis – East report*)

HGL (m) - Zone SUC Servicing Conditions			
Demand Scenario	Two Connections ⁽⁵⁾		
	Connection 1 ⁽¹⁾	Connection 2 ⁽²⁾	
AVDY	150.0	150.0	
PKHR	144.2	144.0	
AVDY +FF	138.7	135.1	
MXDY +FF	137.0	133.2	
Demand Scenario	Two Connections with Upgrades ⁽⁴⁾		
	Connection 1 ⁽¹⁾	Connection 2 ⁽²⁾	
AVDY	149.5	149.5	
PKHR	144.1	144.1	
AVDY +FF	138.6	139.8	
MXDY +FF	136.8	138.1	
Demand Scenario	Three Connections ⁽⁵⁾		
	Connection 1 ⁽¹⁾	Connection 2 ⁽²⁾	Connection 3 ⁽³⁾
AVDY	149.5	149.5	149.5
PKHR	144.5	144.4	142.0
AVDY +FF	138.6	135.1	137.4
MXDY +FF	137.1	133.4	134.8

(1) Ground elevation at Connection 1 (Chapman Mills Drive) = 92.80 m
(2) Ground elevation at Connection 2 (Danson Gardens Grv / Darjeeling Ave) 91.80 m
(3) Ground elevation at Connection 3 (Flagstaff Dr) 92.10 m
(4) Upgrades to existing water distribution required to increase HGL at Connection 2; upscale existing 203mm diameter watermain on Danson Gardens Grv to a 305mm watermain
(5) For scenarios where ultimate conditions will include three connections, the boundary conditions for two connections (without upgrades) were used when only connections 1 and 2 are in place (i.e. for modelling Phases 2 and 3.

3.2.3 Water Demand Calculations

A summary of water demands for the subject site is presented in the following table as derived from the criteria above and the *Stantec Hydraulic Analysis* found in **Appendix B**.

Table 2C: Water Demand Estimate

	Unit Count Conservancy East	Pop ⁽¹⁾	AVDY ⁽²⁾ (L/s)	OWD ⁽³⁾ (L/s)	MXDY ⁽⁴⁾ (L/s)	PKHR ⁽⁵⁾ (L/s)
Single Family	782	2,659	8.62	9.49	21.55	47.38
Townhouse	606	1,636	5.30	0	13.25	29.17
Totals	1,388⁽⁶⁾	4,296	13.92	9.49	34.80	76.55

(1) Population per unit is 3.4 for Single Family and 2.7 for Townhomes
(2) AVDY = Average Day
(3) OWD (outdoor water demand) = 1,049 L/unit/day for Singles
(4) MXDY = Maximum Day
(5) PKHR = Peak Hour
(6) Total unit count may vary slightly from final layouts but are estimated to be within +/-2.5%.
(7) See Stantec Hydraulic Analysis in **Appendix B** for details.

3.3 Summary of Hydraulic Modeling Analysis

A watermain analysis has been prepared to confirm that the network is sized adequately, which is the greater of maximum day plus fire and maximum hour. City review comments on the current **Stantec Hydraulic Analysis - East** note that 'Option B' is the preferred system configuration (sizing and layout for three connections) and those results are presented below. For full details of the assessments refer to the **Stantec Hydraulic Analysis - East**, enclosed in **Appendix B**.

System Pressures

The modeling indicates that the development can be adequately serviced by the proposed watermain network. Modeled service pressures for the development are summarized the following table. The detailed pipe and junction tables are contained in the **Stantec Hydraulic Analysis**, enclosed in **Appendix B**.

Table 2D: Summary of Available System Pressures

	AVDY Maximum Pressure		Peak Hour Demand Minimum Pressure	
	kPA	psi	kPA	psi
Option B – 3 Connections	559	81.14 (J55, J60)	482	69.83 (J103)

*Note: See model results in the Appendix D of the **Stantec Hydraulic Analysis** memo (buildout of all phases).*

The generally accepted best practice is to design new water distribution systems to operate between 350 kPa (50 psi) and 480 kPa (70 psi) as outlined in the City of Ottawa Design Guidelines. Where pressures exceed 80psi pressure reducing valves (PRV) shall be implemented as per the Ontario Building Code.

Available Fire Flows

The minimum allowable pressure under fire flow conditions is 140 kPa (20 psi) at the location of the fire. A summary of the available fire flows is presented in the following table. The detailed fire flow reports are found in the **Stantec Hydraulic Analysis - East** enclosed in **Appendix B**.

Table 2E: Summary of Available Fire Flows

	Required Fire Flow (L/s)	Minimum Available Flow (L/s)	Junction ID
Option B – 3 Connections	217	250	J86, J87

*Note: See model results in the Appendix D of the **Stantec Hydraulic Analysis – East** memo (buildout of all phases). Exception is the phase west of Borrisokane Road where the anticipated cul-de-sac fire flow node can be managed by procedures noted in ISDTB-2018-02 (See Section 3.2 of Stantec report)*

As shown in the above table, the model predicts the network will be able to provide all required fire flows. Detailed results are included in the ***Stantec Hydraulic Analysis - East***, enclosed in ***Appendix B***.

System Reliability

Various major watermain failure scenarios were reviewed by Stantec. Some scenarios resulted in potential reliability issues which have been resolved in the updated watermain layout with additional looping in the northwest area of the design. See discussion in Section 3.3 of the ***Stantec Hydraulic Analysis -East***.

3.4 Water Supply Conclusion

The subject lands are have been reviewed by Stantec to confirm that servicing is feasible from the SUC pressure zone. Future watermain extensions from Nepean Town Centre development areas, being constructed as part of Phase 2-4 approvals, will facilitate servicing to the Conservancy East Phase 5 lands via watermain extension along the future Chapman Mills Drive extension and through the Claridge “Burnett Lands” development area. Future modelling at the detailed design stage will confirm phasing of the extensions of trunk watermains and sizing of the local watermain network. The proposed water supply design will conform to all relevant City and MECP Guidelines and Policies.

4.0 WASTEWATER SERVICING

4.1 Existing Wastewater Services

Per the ***South Nepean Collector (SNC) Wastewater Servicing Study and Functional Design Report*** by Dillon in October 2003 (***Dillon SNC Report***), the subject property is tributary to the South Nepean Collector (SNC) sewer as urban development land.

The SNC (previously called the Jock River Collector) sewer operates north of the subject property within Strandherd Drive prior to travelling south down a Chapman Mills Drive (CMD) and then turns eastward within the future CMD right-of-way (ROW).

The ***South Nepean Collector Phase 2: Hydraulics Review / Assessment*** memo was prepared by Novatech Engineering Consultants on August 20, 2015 (***Novatech SNC Memo***) to provide an update to the sanitary design flows for Phase 2 of the South Nepean Collector, as previously documented in the ***South Nepean Collector (SNC) – Functional Design Report and Update*** by Dillon in 2012 (***Dillon SNC Report and Update***).

4.2 South Nepean Collector Phase 3 – Preliminary Design

The 2015 ***Novatech SNC Memo*** contemplated that the Conservancy Phase 1 development area (north of the Fraser-Clarke Watercourse) would be serviced by the 900 mm diameter SNC sewer running adjacent to the property within the future extension of CMD. This is represented by area “A6-E” within the “***Sanitary Drainage Areas and Land Use – Fig.1***” plan within the 2015 Novatech memo (note that the actual tributary area and population varied slightly).

For the Phase 3 extension of the SNC, Novatech has prepared another review of sanitary flows within their technical memorandum titled “***Strandherd Drive Widening Project, South Nepean Collector Phase 3: Sanitary Flow Calculations***” May 30, 2019 (***2019 Novatech SNC Memo***). The memorandum along with the design sheet calculations from the Novatech memo are provided in ***Appendix C*** for reference along with DSEL annotations on key items in the figure and design sheets. The updated “***Sanitary Drainage Areas and Land Use – Fig.1***” (May 2019) plan is essentially reflective of the same tributary information that was provided in the 2015 study (the plan has been marked up to reflect the Conservancy areas as a frame of reference). The associated design sheet also reflects updated City wastewater design criteria that was not accounted for in the 2015 study and is discussed further in the following section.

Report excerpts are provided in ***Appendix C*** for the SNC Phase 2 analysis as well as draft information associated with the Phase 3 extension. The location of the SNC sewer is shown in ***Figure 4***.

4.3 Wastewater Design

The subject property is planned to be serviced by an internal gravity sanitary sewer system that is to generally follow the local road network. The wastewater servicing plan can be seen in **Drawing 4**.

The prior report proposed that the drainage area of the SNC sanitary sewer be expanded to include the entirety of the Conservancy property. The sewer network will connect to the off-site SNC sanitary sewer within the future CMD at existing manhole 'SANMH8' as identified in the Novatech SNC Phase 2 design Drawing No. 20 provided in **Appendix C** for reference (City contract number ISD14-2033). As noted in the prior section, the 2015 **Novatech SNC Memo** was derived flows based on the City guideline parameters of the time (namely 350 L/capita/day, infiltration allowance of 0.28 L/s/ha and commercial properties at 50,000 L/ha/d). The following table summarizes the new City design guidelines and criteria to be applied to the **Conservancy East** sewer design as well for the determination of the projected flows to be tributary to the SNC along the frontage of the Conservancy Phase 1 development area.

Table 3: Wastewater Design Criteria

Design Parameter	Value
Current Design Guidelines	
Residential - Single Family	3.4 p/unit
Residential – Townhome/ Semi	2.7 p/unit
Residential – Apartment	1.8 p/unit
Average Daily Demand	280 L/d/person
Peaking Factor	Harmon's Peaking Factor. Max 4.0, Min 2.0
Commercial / Institutional Flows	28,000 L/ha/day
Commercial / Institutional Peak Factor	1.5
Infiltration and Inflow Allowance	0.33 L/s/ha
Park Flows	28,000 L/ha/d
Park Peaking Factor	1.0
Sanitary sewers are to be sized employing the Manning's Equation	$Q = \frac{1}{n} AR^{2/3} S^{1/2}$
Minimum Sewer Size	200mm diameter
Minimum Manning's 'n'	0.013
Minimum Depth of Cover	2.5m from crown of sewer to grade
Minimum Full Flowing Velocity	0.6m/s
Maximum Full Flowing Velocity	3.0m/s
<i>Extracted from Sections 4 and 6 of the City of Ottawa Sewer Design Guidelines, October 2012, and associated Technical Bulletins.</i>	

The sanitary design sheet for the lands east of Borrisokane Road is provided in **Appendix C** for reference. Within that design sheet the area and flows from the lands west of Borrisokane Road are highlighted where flows enter that development area at the westward stub from MH10A. That design sheet projected a flow of 77.81 L/s. Based on the updated Phase 5 draft plan, and updated concept plans for the

Conservancy West development area (west of the Foster Ditch), the flows shown at the eastern limit of Phase 5 (see Phase 5 design sheet in **Appendix C**) is now ~68.96 L/s at MH 532A. As such, downstream systems are sufficient and no negative impacts given that flows are lower than the previously projected 77.81 L/s.

4.4 Wastewater Servicing Conclusion

The subject property will be serviced by local sanitary sewers, an on-site trunk sanitary sewer, and the off-site SNC sanitary sewer as defined in previous reports. This AES continues to confirm that the expansion of the drainage areas from the **2019 Novatech SNC Memo** to include the entirety of the subject property has no negative impacts. There is residual capacity in the downstream SNC providing sufficient capacity for the peak sanitary flows for the subject property, including external commercial and community park flows.

5.0 STORMWATER CONVEYANCE

5.1 Existing Stormwater Drainage

The subject property is within the Jock River watershed. Per the existing topography characterized in available City of Ottawa base mapping, as well as site specific survey, all flows from the subject property are ultimately conveyed to the Jock River by a series of watercourses, sheet flow and minor ditches. The Foster Ditch, Borrisokane Road roadside ditches, are the main stormwater conveyances within the Conservancy East Phase 5 property that convey stormwater to the Jock River.

5.2 Proposed Stormwater Management Strategy

As documented in the previous AES, various stormwater strategies were discussed within the Master Infrastructure Review (MIR) prepared in parallel with the AES. Alternatives reviewed were:

Alternative 1 – Oil and Grit Separators & Treatment Train to Naturalized Wetlands*

Alternative 2 – Stormwater Management Wetland Facilities in the Floodplain

Alternative 3 – Stormwater Management Wetland Facilities out of the Floodplain

Alternative 4 – Modified Etobicoke filtration System (MEFS)

For the purposes of this AES update for Phase 5 Alternative 1 continues to be advanced as per the evaluation provided in the MIR and per discussions with the City of Ottawa on July 20, 2021. This alternative:

- A storm sewer system designed to capture at least the minimum design capture events in accordance with the amendment to the storm sewer and stormwater management elements of the Ottawa Design Guidelines – Sewer (Technical Bulletin PIEDTB-2016-01). The stormwater runoff will be treated before ultimately being released into the natural heritage features and the Jock River as per the ***Jock River Reach One Subwatershed Study*** prepared by Stantec in 2007 (***Jock River SWS***).
- All proposed units will be equipped with sump pumps due to local constraints;
- A treatment train approach to attain an Enhanced Level of Protection (80% total suspended solids (TSS) removal) per MECP guidelines consisting of:
 - Deep sump catchbasins;
 - The incorporation of infiltration-type LIDs within the right-of-way extending out from catchbasin locations (see ***Figure 5*** in the ***Figures & Drawings*** section). Future detailed grading will allow for the determination of suitable locations in order to yield optimal benefit from this LID. See Section 5.7 for additional LID discussion.

- Multiple oil and grit separators (OGS) units to provide TSS treatment with outlets that are above the 2-year event summer water levels on the Jock River;
- The storm systems will discharge the treated stormwater at multiple outlets located along the southern natural heritage corridor, connecting via channels. Discharge locations are demonstrated in the **Storm Tributary Area** plan in the **Figures & Drawings** section
- An on-site road network designed to maximize the available storage within right-of-ways for the 100-year design event, where possible; and
- An overland flow route designed to safely convey stormwater runoff flows in excess of the on-site road storage.

The design for the site proposes to have stormwater flows conveyed through the development area of the subject property via an underground sewer network. The stormwater runoff will be treated before ultimately being released into the Jock River as per the **Jock River Reach One Subwatershed Study** prepared by Stantec in 2007 (**Jock River SWS**).

The proposed stormwater design layout is shown on **Drawing 3** with the stormwater management design consisting of (similar to prior phases):

- A storm sewer system designed to capture at least the minimum design capture events in accordance with the amendment to the storm sewer and stormwater management elements of the Ottawa Design Guidelines – Sewer (Technical Bulletin PIEDTB-2016-01);
- All proposed units will be equipped with sump pumps due to local constraints;
- A treatment train approach to attain an Enhanced Level of Protection (80% total suspended solids (TSS) removal) per MECP guidelines consisting of:
 - Deep sump catchbasins to reduce catchbasin sump sediment re-suspension and optimize TSS removal;
 - Multiple oil and grit separators (OGS) units to provide TSS treatment with outlets that are above the 2-year event summer water levels of the Jock River;
 - The incorporation of infiltration-type LIDs within the right-of-way extending out from catchbasin locations (see **Figure 5** in the **Figures & Drawings** section). The future detailed grading will allow for the determination of preferred locations in order to yield optimal benefit from this LID. See Section 5.7 for additional LID discussion;

- The storm systems will discharge the treated stormwater at multiple outlets (2) located along the natural heritage corridor, connecting to the Foster Ditch via channels to support hydration of the wetlands and ultimately outletting to the Jock River. Discharge locations are demonstrated in **Drawing 3**;
- An on-site road network designed to maximize the available storage within right-of-ways for the 100-year design event, where possible, with controlled release of stormwater to the minor storm system; and
- An overland flow route designed to safely convey stormwater runoff flows in excess of the on-site road storage.

Although quantity control has not typically been required for this reach of the Jock River, as per the **Jock River SWS**, the quantity of stormwater runoff exiting from the subject property will be minimized by optimizing on-site storage in the sags of the proposed road network, which in turn minimizes the size of downstream storm sewer infrastructure. It is noted that the RVCA is currently reviewing the SWM requirements within the Jock River Reach 1 area. In consideration of this, J.F. Sabourin and Associates (JFSA) has undertaken a review of the existing quantity control recommendations and the existing, and proposed, development conditions for this area. The findings are presented in the JFSA memorandum *Review of Quantity Control Requirement for Jock River Reach 1 (March 2021)* provided in **Appendix D** which concludes that quantity controls will still not be required for this reach of the Jock River.

5.2.1 Post-Development Stormwater Management Targets

Stormwater management requirements for the proposed alternative Stormwater management scheme have been adopted from the **Jock River SWS**, **City Standards**, and the **MECP SWMP Manual**.

Given the general criteria mentioned above, the following specific standards are anticipated for stormwater management within the subject property:

- Enhanced quality treatment will be provided for stormwater runoff from the subject property, corresponding to a long-term average TSS removal efficiency of 80%, as defined by the MECP prescribed treatment levels;
- Downstream receiving watercourses will be assessed for responses to planned stormwater management outflows, and stabilization mitigation measures will be planned as required;
- Storm sewers on local roads are to be designed to provide at least a 2-year level of service without any ponding per the City's latest Technical Bulletin PIEDTB-2016-01;

- Storm sewers on collector roads are to be designed to provide at least a 5-year level of service without any ponding per the City's latest Technical Bulletin PIEDTB-2016-01;
- For less frequent storms (i.e. larger than 2-year or 5-year), the minor system sewer capture will be restricted with the use of inlet control devices to prevent excessive hydraulic surcharges;
- Under full flow conditions, the allowable velocity in storm sewers is to be no less than 0.80 m/s and no greater than 6.0 m/s;
- For the 100-year storm and for all roads, the maximum depth of water (static and/or dynamic) on streets, rear yards, public space and parking areas shall not exceed 0.35 m at the gutter;
- The major system shall be designed with sufficient capacity to allow the excess runoff of a 100-year storm to be conveyed within the public ROW, or adjacent to the ROW, provided the water level does not touch any part of the building envelope; must remain below all building openings during the stress test event (100-year + 20%); and must maintain 15 cm vertical clearance between spill elevation on the street and the ground elevation at the nearest building envelope;
- Flow across road intersections shall not be permitted for minor storms (generally 5-year or less);
- When catchbasins are installed in rear yards, safe overland flow routes are to be provided to allow the release of excess flows from such areas. A minimum of 30 cm of vertical clearance is required between the rear yard spill elevation and the ground elevation at the adjacent building envelope; and
- The product of the maximum flow depths on streets and maximum flow velocity must be less than 0.60 m²/s on all roads.

5.2.2 Quality Control

Per the ***Jock River SWS***, Enhanced quality treatment will be provided for stormwater runoff from the subject property, corresponding to a long-term average TSS removal efficiency of 80%, as described by the MECP prescribed treatment levels. See Section 5.3 for quality control approach and discussion.

5.2.3 Quantity Control

As noted in the ***Jock River SWS***, quantity control is not anticipated to be required for outlets to the Jock River, however, some quantity control may be provided by erosion storage, as erosion thresholds for any watercourses/outlets will be respected where required. As noted in Section 5.2, JFSA has reviewed the current/future development conditions contributing to this reach of the Jock River and concludes that quantity

control will still not be required. See “Review of Quantity Control Requirement for Jock River Reach 1 (JFSA March 2021) provided in **Appendix D**.

5.3 Stormwater Management Design

5.3.1 Treatment Train Approach

JFSA previously (June 2021 memo) prepared a review of various potential stormwater quality treatment options that were investigated for the development. These included options, and combinations of options, as summarized in the following updated table. Each of the options has an expected total suspended sediment (TSS) removal capability, varying from 5% to 88%. This review assessed how the required Enhanced Level of Protection (80% TSS removal) could be achieved when the options are used in a treatment train approach, consistent with the expected requirements of the upcoming MECP Consolidated Linear Infrastructure policy.

<u>Selection and comparison of alternatives</u>									
Method	TSS Removal	Alt. 1	Alt. 2	Alt. 3	Alt. 4	Alt. 5	Alt. 6	Alt. 7	Alt. 8
Street Sweeping (Monthly)	5%								
Street Sweeping (Weekly)	10%								
Street Sweeping (Weekly with Elgin Eagle)*	88%	x							
Curb Cut with Grass Swales	75%			X					
Curb Cut with Infiltration Trenches	80%								
Catchbasin Inserts (CB Shield)*	27%		X			X		X	
Deep Sump Catch Basin	25%				X	X	X		X
Infiltration/ Filtration Trenches**	80%				X	X	X		
Infiltration at CBs, per MOE Table 3.2 (22.5m ³ /ha)	70%								X
OGS*	50%			X					X
JellyFish*	85%							X	
SWM Pond (Wet Pond)	80%		X						
Overall Performance		88.0%	85.4%	87.5%	89.1%	85.4%	85.0%	89.1%	88.8%
Treatment Train Overall Performance = 1 - (1- TSS Removal Rate Method 1) x (1- TSS Removal Rate Method 2) x (1- TSS Removal Rate Method 3 x ...)									
*) TSS Removal as documented by ETV Canada									
**) includes the use of Etobicoke infiltration or filtration systems or other permutations of the same									

The above table provides a summary of the TSS removal for the various methods that were considered. An option of infiltration LID measures located at catchbasin locations has been added as a method, and to Alternative 8 (see further discussion regarding this method below). The options, and combinations of options, have been assessed and shown to meet or exceed the required 80% TSS target.

For the development area, the updated Alternative 8 option demonstrates an estimated TSS removal of 88.8% for that particular treatment train approach which has been discussed with City staff for the approval of prior phases and will be the design being

advanced. For the determination of the TSS removal of 70% for the infiltration LID at catchbasins, the Table 3.2 of the MOECC (now MECP) publication entitled “*Stormwater Management Planning and Design Manual, March 2003*” sets the storage volume requirements for infiltration measures to achieve certain TSS removal rates.

Table 3.2 Water Quality Storage Requirements based on Receiving Waters^{1, 2}

Protection Level	SWMP Type	Storage Volume (m ³ /ha) for Impervious Level			
		35%	55%	70%	85%
<i>Enhanced</i> 80% long-term S.S. removal	Infiltration	25	30	35	40
	Wetlands	80	105	120	140
	Hybrid Wet Pond/Wetland	110	150	175	195
	Wet Pond	140	190	225	250
<i>Normal</i> 70% long-term S.S. removal	Infiltration	20	20	25	30
	Wetlands	60	70	80	90
	Hybrid Wet Pond/Wetland	75	90	105	120
	Wet Pond	90	110	130	150
<i>Basic</i> 60% long-term S.S. removal	Infiltration	20	20	20	20
	Wetlands	60	60	60	60
	Hybrid Wet Pond/Wetland	60	70	75	80
	Wet Pond	60	75	85	95
	Dry Pond (Continuous Flow)	90	150	200	240



¹Table 3.2 does not include every available SWMP type. Any SWMP type that can be demonstrated to the approval agencies to meet the required long-term suspended solids removal for the selected protection levels under the conditions of the site is acceptable for water quality objectives. The sizing for these SWMP types is to be determined based on performance results that have been peer-reviewed. The designer and those who review the design should be fully aware of the assumptions and sampling methodologies used in formulating performance predictions and their implications for the design.

²Hybrid Wet Pond/Wetland systems have 50-60% of their permanent pool volume in deeper portions of the facility (e.g., forebay, wet pond).

The required storage volume of 22.5 m³/ha is determined for the development area prorated from the above table based on an overall imperviousness of ~62.5%. Similar to prior phases it is anticipated that the extent of the site area for Conservancy East Phase 5 can be managed with the proposed LID. For prior phases it is noted that approximately 140 lineal meters of LID per hectare of area to be treated was required. With approximately 9.0 ha of area to be treated (which excludes rear yards similar to the prior phase) this equates to 140x9.0= ~1,260 m extent of LID required. Phase 5 has approximately 1,800 m of roadway to incorporate the LID infrastructure therefore sufficient roadway is available for use.

5.3.2 Oil-Grit Separator Units (OGS)

As shown on **Drawing 3**, two (2) OGS units at locations along the southern boundary of the property, discharging to the Jock River via the existing Foster Ditch. By way of an MECP Certificate of Technology Assessment and manufacturer’s design report, the OGS units will demonstrate compliance with Enhanced Level of Protection requirements, with specific drainage area parameters for each area.

The manufacturer’s reported efficiency of TSS removal of the OGS units is expected to be based on a ‘fine distribution’ particle size distribution in conformance with the following table, unless otherwise approved by the City of Ottawa, RVCA, and MECP. The particle size distribution is the generic particle size distribution accepted by the City of Toronto per the *Wet Weather Flow Management Guidelines* (City of Toronto, 2006) as a typical average stormwater particle size distribution, and is an excerpt from Table 3.3 of the *Stormwater Management Practices Planning and Design Manual* (MOECC, 1994).

**Table 4: Typical Stormwater Particle Size Distribution & Settling Velocities
 (Source: *Stormwater Management Practices Planning and Design Manual*,
 MOECC, 1994)**

Particle Size (microns) (NURP 1983)	% of Particle Mass	Average Settling Velocities (m/s)
< 20	0 - 20	0.00000254
20 - 40	20 - 30	0.00001300
40 - 60	30 - 40	0.00002540
60 - 130	40 - 60	0.00012700
130 - 400	60 - 80	0.00059267
400 - 4000	80 - 100	0.00550333

To allow for flexibility as detailed design advances, it is proposed that any OGS unit can be selected, given that it:

- Meets the requirements set out in the preceding sections;
- Ensures no significant negative impact on the upstream storm sewer system – to be determined via hydraulic modelling at detailed design; and
- Demonstrates suitability for meeting Enhanced water quality targets via a MECP Certificate of Technology Assessment.

The preliminary OGS units proposed in the following table have been sized to treat the stormwater runoff for the tributary areas noted in order to meet MECP Enhanced Level of Protection criteria prior to discharge to the Jock River via naturalized wetlands as

shown on **Drawing 3**. The OGS total suspended removal rates and preliminary OGS unit details have been attached for reference in **Appendix D**.

Table 5: OGS Unit ID and Design Characteristics

Area and Unit ID ⁽¹⁾⁽²⁾	Drainage Area Target (ha)	Estimated Weighted C Value	Unit Treatment Capacity (L/s)	Unit Model ⁽¹⁾
Area 9 – OGS9 ⁽³⁾	7.21	0.72	212	CDS Model 4045-8
Area 10 – OGS10 ⁽³⁾	6.61	0.70	212	CDS Model 4045-8
(1) Providing at minimum 80% TSS removal for a Fine Distribution (2) See Drawing 3 for OGS unit locations (3) NOTE: the OGS numbering of OGS9 and OGS10 have been used to maintain consistency with prior functional servicing reports circulated in relation to this development area.				

The above OGS units will achieve required quality controls within the treatment train and, along with other elements, will have additional beneficial TSS mitigation.

5.3.3 Groundwater

Paterson Group has reviewed the anticipated long term groundwater condition for the development area. Paterson drawing PG5036-10A in **Appendix D** demonstrates the long term groundwater elevation across the Conservancy East Phase 5 development area. The lowest elevation of 88.70 is below the trunk sewer profiles shown in **Drawing No. 5** in the **Drawings** section and would be below any infiltration-type LID proposed within the development area.

5.4 Proposed Minor System

The subject property will be serviced by an internal gravity storm sewer system that will generally follow the local road network and proposed servicing easements as required. The drainage will be conveyed within the underground piped sewer system to headwall outlets located along the natural heritage corridor.

Street catchbasins will collect drainage from the streets and front yards, while rear yard catchbasins will capture drainage from backyards. Perforated catch basin leads will be provided in rear yards, except the last segment where they connect to the right-of-way which will be solid pipe, per City standards.

The rational method design of the minor system captures drainage for storm events up to and including the 2-year (local) and 5-year (collector) event within the subject property. The following table summarizes the standards employed in the detailed

design of the storm sewer network. The preliminary drainage area information can be found in **Drawing 3** and rational method design sheets are provided in **Appendix D**.

Table 6: Storm Sewer Design Criteria

Design Parameter	Value
Minor System Design Return Period	1:2 year (PIEDTB-2016-01) for local roads, without ponding 1:5 year (PIEDTB-2016-01) for collector roads, without ponding 1:100 year (PIEDTB-2016-01) for arterial road, without ponding
Major System Design Return Period	1:100 year
Intensity Duration Frequency Curve (IDF) 2-year storm event: A=732.951 B=6.199 C=0.810 5-year storm event: A = 998.071 B = 6.053 C = 0.814	$i = \frac{A}{(t_c + B)^C}$
Minimum Time of Concentration	10 minutes
Rational Method	$Q = CiA$
Storm sewers are to be sized employing the Manning's Equation	$Q = \frac{1}{n} AR^{2/3} S^{1/2}$
Runoff coefficient for paved and roof areas	0.9
Runoff coefficient for landscaped areas	0.2
Minimum Sewer Size	250 mm diameter
Minimum Manning's 'n' for pipe flow	0.013
Minimum Depth of Cover	1.5 m from crown of sewer to grade
Minimum Full Flowing Velocity	0.8 m/s
Maximum Full Flowing Velocity	6.0 m/s
Clearance from 100-Year Hydraulic Grade Line to Building Opening	0.30 m
Design Parameter	Value
Max. Allowable Flow Depth on Municipal Roads	35 cm above gutter (PIEDTB-2016-01)
Extent of Major System	To be contained within the municipal ROW or adjacent to the ROW provided that the water level must not touch any part of the building envelope and must remain below the lowest building opening during the stress test event (100-year + 20%) and 15cm vertical clearance is maintained between spill elevation on the street and the ground elevation at the nearest building envelope (PIEDTB-2016-01)
Stormwater Management Model	DDSWMM (release 2.1), SWMHYMO (v. 5.02) and XPSWMM (v. 10)

Model Parameters	Fo = 76.2 mm/hr, Fc = 13.2 mm/hr, DCAY = 4.14/hr, D.Stor.Imp. = 1.57 mm, D.Stor.Per. = 4.67 mm
Imperviousness	Based on runoff coefficient (C) where Percent Imperviousness = (C - 0.2) / 0.7 x 100%.
Design Storms	Chicago 3-hour Design Storms and 24-hour SCS Type II Design Storms. Maximum intensity averaged over 10 minutes.
Historical Events	July 1st, 1979, August 4th, 1988 and August 8th, 1996
Climate Change Street Test	20% increase in the 100-year, 3-hour Chicago storm
<i>Extracted from City of Ottawa Sewer Design Guidelines, October 2012, and ISSU, and based on recent residential subdivisions in City of Ottawa.</i>	

The peak design flows are calculated based on an average predicted runoff coefficient (C-value) of 0.67 and 0.80 for the development areas, 0.40 for park areas and 0.25 for grassed areas. As detailed design progresses, the runoff coefficients will be refined to reflect the proposed building envelopes, driveways and other details.

There are several trunk sewers proposed and the peak flows are described for the trunk sewers which correspond to the stormwater management design areas as summarized in the following table:

Table 7: Minor System Trunk Sewer Outlets

Area/Outlet # (from east to west)	Trunk Sewer Outlet Headwall	Peak Flow (L/s)
9 (HW9) ⁽¹⁾	1050 mm diameter @ 0.20%	894
10(HW10) ⁽¹⁾	1050 mm diameter @ 0.11%	739
(1) NOTE: the OGS numbering of OGS9 and OGS10 have been used to maintain consistency with prior functional servicing reports circulated in relation to this development area.		

The storm sewers tributary to the various outlets, and associated peak flows, are detailed in the rational method design sheet, enclosed in **Appendix D**.

The conceptual servicing layout is shown on **Drawing 2** in **Drawings**. As detailed design progresses, alignment and sizing of local storm sewers will be confirmed and additional servicing easements may be required, potentially triggering minor amendments to the proposed lot fabric in the concept plan. The preliminary sanitary and storm trunk plan and profiles are shown on **Drawing 5** in **Drawings**.

5.4.1 Hydraulic Grade Line Analysis

A preliminary hydraulic grade line (HGL) modelling analysis has been completed by JFSA to demonstrate that the HGL will be maintained below the ground surface. See the JFSA memo entitled *BCDC Phase 5 – Preliminary HGL Analysis (December 1, 2022)* in **Appendix D** for details/results. The analysis has been evaluated for various scenarios for the Jock River (as per prior City requirements) in order to assess the appropriate HGL boundary condition:

- 100-year rainfall event on the development and a 5-year spring water level on the Jock River; or
- 5-year rainfall event on the development and a 100-year spring water level on the Jock River (deemed to be the critical event).

The HGL results in JFSA's Table 1 demonstrate that the worst case scenario freeboard to the ground surface ranges from 0.64m to 0.90m for the critical event noted above. The HGL is shown on the profile **Drawing 5** for reference.

An updated HGL analysis will be completed for the proposed system at the detailed design stage, based on the above noted events, including historical design storms and climate change stress test as required. Detailed grading design and storm sewer design will be modified as required to achieve the freeboard requirements (per PIEDTB-2016-01).

5.5 Proposed Major System

Major system conveyance, or overland flow, will be provided to accommodate flows in excess of the minor system capacity. Overland flow is accommodated by generally storing stormwater up to the 100-year design event in road sags then routing additional surface flow along the road network and service easements towards the proposed stormwater outlets, discharging to the Jock River through the natural heritage corridors, as shown on **Drawing 1**. The grading design includes a saw-toothed-road design with 0.10% minimum grade from high point to high point in order to maximize available surface storage for management of flows up to the 100-year design event where possible.

5.6 Foundation Drainage (Sump Pumps)

Due to the grade raise restrictions and the proposed storm and sanitary drainage schemes, the road centerlines do not allow for standard basements with a gravity connection to the storm sewer system. As such, because of the constraints on the subject property, sump pumps are proposed to be installed for all residential blocks and residential lots.

The City of Ottawa issued Technical Bulletin *ISTB-2018-04* and *2019-02* for the amendment of the *Ottawa Design Guidelines – Sewer, Second Edition*, October 2012 with respect to the screening criteria for the use of sump pump systems for foundation drainage in Greenfield developments on sites with clay soils. Similar to the development of Conservancy Phase 1, and Conservancy East (Phase 2-4) this site has also been assessed as meeting the required criteria for the use of sump pumps.

One of the screening criterion is with respect to the hydraulic grade line (HGL) for the development wherein the system should be reviewed to demonstrate that the HGL cannot reasonably be lowered any further due to outlet restrictions. The site grading is constrained by the close proximity of the Jock River, which is the receiver of stormwater outflows, and is also constrained by grade raise restrictions for the property.

For the Barrhaven Conservancy East Phase 5 Lands the grade raise restriction varies between 1.4 m and 1.8 m. Paterson's permissible grade raise plan is contained in **Appendix E** for reference (See Section 6 for discussion). Further investigations on the property and potential surcharging or lightweight fill (LWF) underneath garages could increase the permissible grade raise and will be investigated further as part of the detailed design.

The functional grading plan for the subdivision has been prepared with the grade raise restrictions in mind with grades being kept as low as possible.

The proposed centerline of road grades, and subsequently the house grades, do not allow for standard basements with a gravity connection to the storm sewer system. As such, the subdivision will be serviced entirely by sump pumps due to site constraints imposed by grade raise restrictions, HGL elevations and the proximity to the Jock River stormwater outlet.

5.7 Low Impact Development (LID) - Infiltration

The following general Low Impact Development (LID) techniques could be considered for implementation, where possible, as part of detailed design (noting that they have to be weighed against the objectives of the City's sump pump technical bulletins):

- Rear-yard swales should be designed with minimum grades where possible, to promote infiltration;
- Rear-yard catchbasin leads should be perforated (except for the last segment connecting to the storm sewer within the ROW), to promote infiltration; and,
- Where eavestroughs are provided on residential units, they are to be directed to landscaped surfaces, to promote infiltration.
- Furthermore, the following techniques can be examined as part of detailed landscaping design of the park block; and,
- Micro-grading can be considered to promote infiltration.

Generally, the LID techniques proposed above are most suitable due to the existing clay soils and high groundwater levels. The long term groundwater anticipated is demonstrated on Paterson Drawing *PG5036-10A* in **Appendix D** as previously noted. The proposed LID infiltration measure noted in Section 5.2 will contribute some infiltration benefits as first flush stormwater is conveyed into the filtration trench. The amount of infiltration is dependent upon the surrounding soils, but the proposed design will optimize the potential on the site.

5.8 Existing Watercourses

5.8.1 Foster Ditch

The Foster Ditch borders the western boundary of the Conservancy East Phase 5 development area. It originates south of Fallowfield Road, west of Cedarview Road and flows south until it converges with the Jock River South of McKenna Casey Drive. The ditch is approximately 3200 m long and has been artificially straightened. This non-municipal drain is a fish bearing tributary of the Jock River with approximately 335 ha of catchment area. The surrounding land use is urban and vacant lands. Riparian vegetation is very sparse consisting of mostly grasses with a few shrubs.

As noted in the **Jock River SWS**, to ensure protection of the aquatic habitat north of the Jock River, a development setback should be provided for all of the tributaries. Further studies will determine the development setback, which will be the greater of: 1) regulatory floodplain; 2) meander belt width; and 3) aquatic setback, whichever is greater.

5.9 Floodplain

On November 8th, 2019 the RCVA gave permission to Barrhaven Conservancy Development Corporation to cut and fill on the subject property under permit RV5 44/19 pursuant to review under Section 28 of the Conservation Authorities Act, regulation 174/06. The application and approval by the RVCA was supported by a 2D HEC-RAS model prepared by JFSA. The JFSA model identified the existing and proposed 100-year water levels and permissible extent of fill placement.

The works pursuant to the above-mentioned permit were completed and accepted by the RVCA on May 31st 2020. Options to complete the fill area boundary as set by JFSA included building a structural face of fill (retaining wall) to the limits of the 100-year floodplain boundary, or, building a berm with the toe of slope at the 100-year floodplain boundary. A vertical structural face of fill was not seen as a desirable or practical outcome and a berm was thus constructed. As-builts for the top of berm were subsequently provided and approved by the RVCA, resulting in the May 31st approval noted above and the current 100-year floodplain boundary delineation. The toe of the berm as constructed corresponds to the approved JFSA 100-year floodplain line and the current top of berm corresponds to the as-built top of berm.

5.10 Stormwater Servicing Conclusions

The Phase 5 stormwater runoff is designed to be captured by an internal gravity sewer system that will convey flows to multiple outlet locations equipped with end of line OGS units (two). A proposed treatment train arrangement of 1.0 m deep sump catchbasins, to optimize catchbasin sump retention of solids, as well as select catchbasin locations with connected infiltration-type subdrains will provide the required quality control treatment to achieve the Enhanced Level of protection. Downstream of the storm outlets along the southern development boundary will be channels within the natural heritage corridor where flows will be conveyed to the Foster Ditch prior to discharge to the Jock River. It is anticipated that quantity control is not required for the Jock River. Notwithstanding, some quantity control by means of erosion storage will be included.

A preliminary Hydraulic Grade Line (HGL) modelling analysis has been completed for the Conservancy East (Phase 5) development area at this time and demonstrates that the HGL is maintained below the ground surface with freeboards ranging from 0.64 m to 0.90 m. Further detailed HGL review will be completed for the proposed system at the detailed design stage. Due to the grade raise restrictions, and the proposed storm and sanitary drainage layouts, the road centerlines do not allow for standard basements with a gravity connection to the storm sewer system. As such, because of the constraints on the subject property, sump pumps are proposed to be installed for all residential blocks and residential lots.

The Conservancy East phase 5 development area will be outside of the Jock River's regulatory floodplain area.

Appropriate setbacks from existing watercourse are incorporated into the draft plan based on advancement/finalizing of studies to assess the various determining criteria.

6.0 GRADING

A site grading arrangement has been developed to optimize earthworks and provide major system conveyance to the receiving outlets, and naturalized wetland facilities, which ultimately outlet to the existing Jock River drainage network. The proposed grading can be found in **Drawing 1** in **Drawings**.

The development area is outside of the Jock River regulatory flood plain limits. The site grading will be a minimum of 0.50m above the 100-year regulatory limit event of the Jock River.

6.1 Geotechnical Conditions

Paterson completed a geotechnical investigation for the Conservancy East lands as follows:

- *Geotechnical Investigation – Proposed Residential Development, Conservancy Lands East* (Paterson Group, September 24, 2019);

The existing ground surface across the site is relatively level with approximate ground surface elevation varying between 91.5 m and 91.0 m. The subsurface profile generally consists of an approximate 50 mm to 460 mm thick layer of topsoil underlain by a silty clay deposit.

Due to the presence of a silty clay deposit, permissible grade raise restrictions are recommended for this site. The recommended permissible grade raise varies between 1.4 m in the north area of the phase and 1.8 m in the south. Figure PG5036-2 '*Permissible Grade Raise Plan*' by Paterson is enclosed in **Appendix E** for reference. At the time of detailed design, efforts will be made to mitigate any exceedances and detailed review and signoff by a licensed Geotechnical Engineer will be required. Where grade raises exceed the permissible levels the Engineer will recommend appropriate measures to mitigate where required (i.e. light weight fill or pre-consolidation etc).

The following additional grading criteria and guidelines will be applied to detailed design, per **City of Ottawa Guidelines**:

- Driveway slopes will have a maximum slope of 6%;
- Grading in grassed/landscaped areas to range from 2% to 3:1, with terracing required for slopes larger than 7%;
- Swales are to be 0.15m deep with 3:1 side slopes unless otherwise indicated on the drawings; and,
- Perforated pipe will be required for drainage swales if they are less than 1.5% in slope.

The geotechnical analysis of the site, published under separate cover in support of the development applications, provides additional information about the suitability of the site for the proposed services and grading scheme. At the time of detailed design, detailed review and signoff by a licensed Geotechnical Engineer will be required.

7.0 EROSION AND SEDIMENT CONTROL

Soil erosion occurs naturally and is a function of soil type, climate and topography. The extent of erosion losses is exaggerated during construction where vegetation has been removed and the top layer of soil becomes agitated.

Prior to topsoil stripping, earthworks or underground construction, erosion and sediment controls are implemented and will be maintained throughout any construction phase.

The following specific recommendations to the Contractor will be included in contract documents.

- Limit extent of exposed soils at any given time.
- Re-vegetate exposed areas as soon as possible.
- Minimize the area to be cleared and grubbed.
- Protect exposed slopes with plastic or synthetic mulches.
- Install silt fence to prevent sediment from leaving the site and entering existing watercourses, and clean and maintain throughout construction.
- Install catchbasin inserts during construction to protect from silt entering the storm sewer system.
- Install mud mats in order to prevent mud tracking onto adjacent roadways.
- No refueling or cleaning of equipment near existing watercourses.
- No material stockpiles within 30m of existing watercourses, unless otherwise permitted by RVCA and City of Ottawa.
- Provide sediment traps and basins during dewatering.
- Plan construction at proper time to avoid flooding.
- The Contractor will, at every rainfall, complete inspections to ensure proper performance.
- Erosion and sediment controls will remain in place until the working areas have been stabilized and re-vegetated.

8.0 UTILITIES

Utility services extending to the site may require connections to multiple existing infrastructure points: consultation with Enbridge gas, Hydro Ottawa, Rogers, and Bell is required as part of the development process to confirm the servicing plan for the subject lands.

9.0 CONCLUSION AND RECOMMENDATIONS

This AES provides details on the planned on-site municipal services for the subject property and demonstrates that adequate municipal infrastructure capacity is expected to be available for the planned development area.

- The subject lands are have been reviewed by Stantec to confirm that servicing is feasible from the SUC pressure zone. Future watermain extensions from Nepean Town Centre development areas, being constructed as part of Phase 2-4 approvals, will facilitate servicing to the Conservancy East Phase 5 lands via watermain extensions along the future Chapman Mills Drive extension and through the Claridge “Burnett Lands” development area. Detailed modelling will confirm phasing of the extensions of trunk watermains and verify sizing of the local watermain network.
- The subject property will be serviced by local sanitary sewers, an on-site trunk sanitary sewer, and the off-site SNC sanitary sewer as defined in previous reports. This AES continues to confirm that the expansion of the drainage areas from the **2019 Novatech SNC Memo** to include the entirety of the subject property has no negative impacts. There is residual capacity in the downstream SNC providing sufficient capacity for the peak sanitary flows for the subject property, including external commercial and community park flows.
- Stormwater service is to be provided by capturing stormwater runoff by an internal gravity sewer system that will convey flows to various outlets along the southern boundary to the Foster Ditch which will convey flows to the Jock River. Prior to discharge from the development, any first flush stormwater will have passed through a treatment train of measures in order to provide the appropriate level of Enhanced quality control. The treatment train consists of deep sump catchbasins, LID infiltration trench at catchbasin locations and an end-of-line OGS unit. It is anticipated that quantity control will not be required for discharges to the Jock River.
- A preliminary Hydraulic Grade Line (HGL) modelling analysis has been completed at this time and demonstrates that the HGL is maintained below the ground surface. Another detailed HGL review will be completed for the proposed system at the detailed design level.

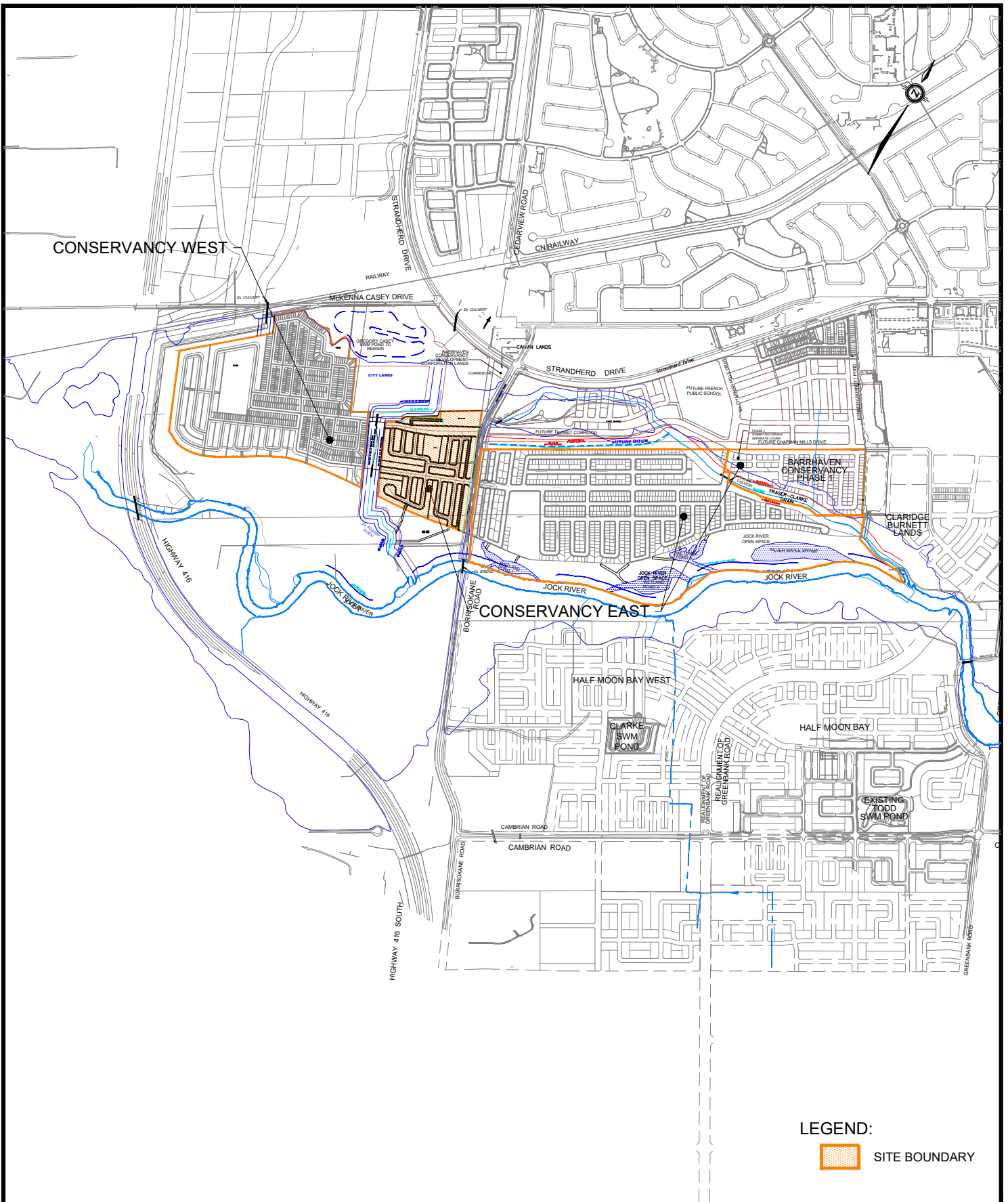
- Sump pumps are proposed to be installed for all units within residential blocks and lots;
- The proposed servicing and grading plans are anticipated to meet all City, RVCA, and MECP requirements as set out in background studies and current standards.
- Prior to detailed design of the infrastructure presented in this report, this AES will require approval under the Planning Act as supporting information for the Plan of Subdivision application. Project-specific approvals are also expected to be required for the infrastructure presented in this report from the City of Ottawa, MECP, and Rideau Valley Conservation Authority, among other agencies.

Prepared by,
David Schaeffer Engineering Ltd.



Per: Kevin L. Murphy, P.Eng.

FIGURES & DRAWINGS



LEGEND:
 SITE BOUNDARY



120 Iber Road, Unit 103
 Stittsville, ON K2S 1E9
 TEL: (613) 836-0856
 FAX: (613) 836-7183
 www.DSEL.ca

**BARRHAVEN CONSERVANCY
 EAST PHASE 5
 KEY PLAN
 CITY OF OTTAWA**

DATE: DECEMBER 2022
 SCALE: 1:20000
 PROJECT No.: 20-1180 A-5
 FIGURE: 1

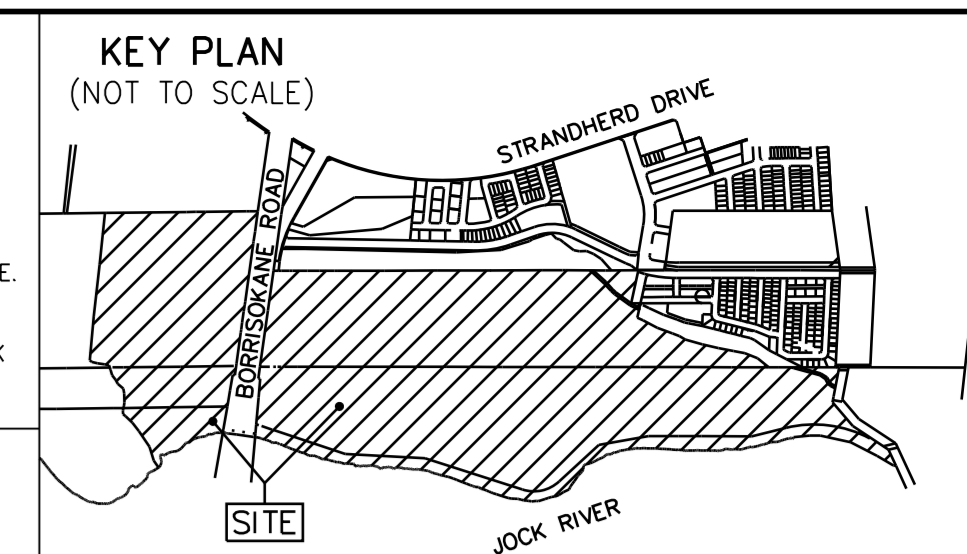
SCHEDULE OF LAND USE		
LAND USE	BLOCK(S)	AREA (Sq. m)
SINGLES (DETACHED)	1 TO 8, (BOTH INCLUSIVE), 20, 21, 24, 25, 41, 43, 45, 47, 48 AND 50 TO 59, (BOTH INCLUSIVE)	219,615.4
TOWNHOME	9 TO 19, (BOTH INCLUSIVE), 22, 23, 26, 27, 31, 32, 35, 42, 44, 46, 49 AND 135	66,745.4
REAR LANE TOWNHOME	100 TO 103, (BOTH INCLUSIVE) AND 106 TO 109, (BOTH INCLUSIVE)	27,698.3
WALKWAYS	104, 105, 110 TO 116, (BOTH INCLUSIVE) AND 134	1,815.1
OPEN SPACE	118, 119 AND 121	4,021.3
BUS LANE	132	8,651.3
FUTURE DEVELOPMENT	120	9,218.2
PARK	117, 122, 123 AND 133	42,832.3
NATURAL HERITAGE SYSTEM	124, 125 AND 126	52,086.5
JOCK RIVER OPEN SPACE	127, 128 AND 129	237,125.6
STREET WIDENING	130 AND 131	5,989.5
STREETS	STREET 'Y' TO STREET '37', (BOTH INCLUSIVE)	176,962.4
LANES	LANE 'Y' TO LANE '3', (BOTH INCLUSIVE)	4,890.3
TOTAL:		857,651.6

SUBJECT TO THE CONDITIONS, IF ANY, SET FORTH IN OUR LETTER DATED _____, THIS DRAFT PLAN IS APPROVED BY THE CITY OF OTTAWA UNDER SECTION 51(17) OF THE PLANNING ACT THIS _____ DAY OF _____, 2021.

SEAN MOORE, MCR, RPP, MANAGER
DEVELOPMENT REVIEW SECTION
PLANNING, INFRASTRUCTURE AND ECONOMIC DEVELOPMENT DEPARTMENT,
CITY OF OTTAWA

ADDITIONAL INFORMATION AS REQUIRED UNDER SECTION 51(17) OF THE PLANNING ACT R.S.O. 2001

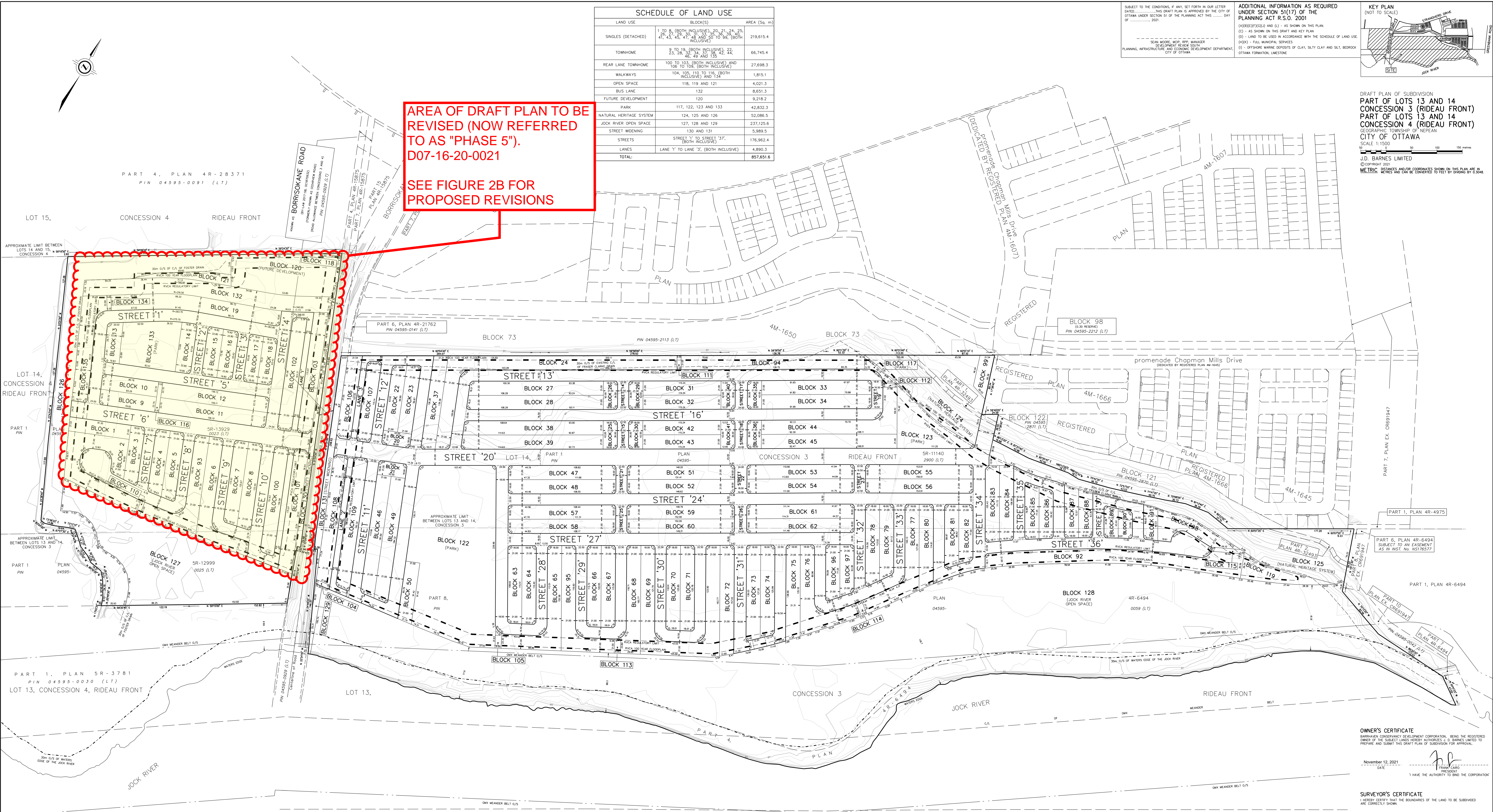
(X) - EXISTING (Y) - AS SHOWN ON THIS PLAN
(O) - AS SHOWN ON THIS DRAFT AND KEY PLAN
(D) - LAND TO BE USED IN ACCORDANCE WITH THE SCHEDULE OF LAND USE
(H) - FULL MUNICIPAL SERVICES
(S) - OFFSHORE MARINE DEPOSITS OF CLAY, SILT, CLAY AND SILT, BEDROCK
OTTAWA FORMATION, LIMESTONE



DRAFT PLAN OF SUBDIVISION
PART OF LOTS 13 AND 14
CONCESSION 3 (RIDEAU FRONT)
PART OF LOTS 13 AND 14
CONCESSION 4 (RIDEAU FRONT)
GEOGRAPHIC TOWNSHIP OF NEPEAN
CITY OF OTTAWA
SCALE 1:1500
J.D. BARNES LIMITED
© COPYRIGHT 2021
DISTANCES AND/OR COORDINATES SHOWN ON THIS PLAN ARE IN METRIC UNITS AND CAN BE CONVERTED TO FEET BY DIVIDING BY 0.3048

AREA OF DRAFT PLAN TO BE REVISED (NOW REFERRED TO AS "PHASE 5").
D07-16-20-0021

SEE FIGURE 2B FOR PROPOSED REVISIONS



LINework COMPILED FROM REGISTERED PLAN 4M-XXXX (STANTEC - GLENVIEW) LINework COMPILED FROM REGISTERED PLAN 4M-1667 LINework COMPILED FROM PLAN 5R-3970

FIGURE 2A
2021 APPROVED DRAFT PLAN

OWNER'S CERTIFICATE
BARRHAVEN CONSERVANCY DEVELOPMENT CORPORATION, BEING THE REGISTERED OWNER OF THE SUBJECT LOTS HEREBY AUTHORIZES J.D. BARNES LIMITED TO PREPARE AND SUBMIT THIS DRAFT PLAN OF SUBDIVISION FOR APPROVAL.

November 12, 2021
DATE
FRANK CARO
PRESIDENT
I HAVE THE AUTHORITY TO SIGN THE CORPORATION

SURVEYOR'S CERTIFICATE
I HEREBY CERTIFY THAT THE BOUNDARIES OF THE LAND TO BE SUBDIVIDED ARE CORRECTLY SHOWN.

NOVEMBER 12th, 2021
DATE
C.M. FOX
ONTARIO LAND SURVEYOR



JOB V.2021.4

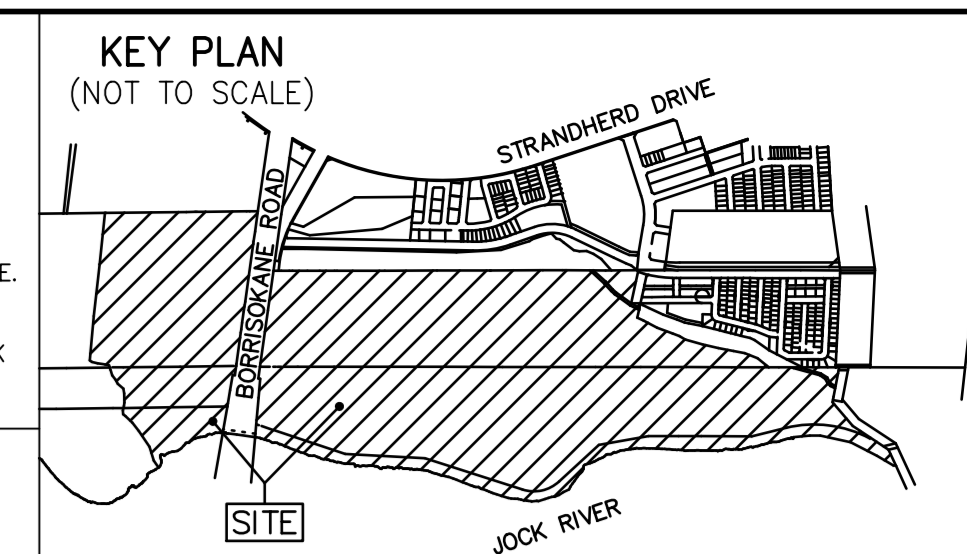
SCHEDULE OF LAND USE		
LAND USE	BLOCK(S)	AREA (Sq. m)
SINGLES (DETACHED)	1 TO 7, (BOTH INCLUSIVE), 20, 21, 24, 25, 26, 27, 28, 29, 30, 31, 32, 33, 34, 35, 36, 37, 38, 39, 40, 41, 42, 43, 44, 45, 46, 47, 48, 49, 50, 51, 52, 53, 54, 55, 56, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 71, 72, 73, 74, 75, 76, 77, 78, 79, 80, 81, 82, 83, 84, 85, 86, 87, 88, 89, 90, 91, 92, 93, 94, 95, 96, 97, 98, 99, 100, 101, 102, 103, 104, 105, 106, 107, 108, 109, 110, 111, 112, 113, 114, 115, 116, 117, 118, 119, 120, 121, 122, 123, 124, 125, 126, 127, 128, 129, 130, 131, 132, 133, 134, 135, 136, 137, 138, 139, 140, 141, 142, 143, 144, 145, 146, 147, 148, 149, 150, 151, 152, 153, 154, 155, 156, 157, 158, 159, 160, 161, 162, 163, 164, 165, 166, 167, 168, 169, 170, 171, 172, 173, 174, 175, 176, 177, 178, 179, 180, 181, 182, 183, 184, 185, 186, 187, 188, 189, 190, 191, 192, 193, 194, 195, 196, 197, 198, 199, 200, 201, 202, 203, 204, 205, 206, 207, 208, 209, 210, 211, 212, 213, 214, 215, 216, 217, 218, 219, 220, 221, 222, 223, 224, 225, 226, 227, 228, 229, 230, 231, 232, 233, 234, 235, 236, 237, 238, 239, 240, 241, 242, 243, 244, 245, 246, 247, 248, 249, 250, 251, 252, 253, 254, 255, 256, 257, 258, 259, 260, 261, 262, 263, 264, 265, 266, 267, 268, 269, 270, 271, 272, 273, 274, 275, 276, 277, 278, 279, 280, 281, 282, 283, 284, 285, 286, 287, 288, 289, 290, 291, 292, 293, 294, 295, 296, 297, 298, 299, 300, 301, 302, 303, 304, 305, 306, 307, 308, 309, 310, 311, 312, 313, 314, 315, 316, 317, 318, 319, 320, 321, 322, 323, 324, 325, 326, 327, 328, 329, 330, 331, 332, 333, 334, 335, 336, 337, 338, 339, 340, 341, 342, 343, 344, 345, 346, 347, 348, 349, 350, 351, 352, 353, 354, 355, 356, 357, 358, 359, 360, 361, 362, 363, 364, 365, 366, 367, 368, 369, 370, 371, 372, 373, 374, 375, 376, 377, 378, 379, 380, 381, 382, 383, 384, 385, 386, 387, 388, 389, 390, 391, 392, 393, 394, 395, 396, 397, 398, 399, 400, 401, 402, 403, 404, 405, 406, 407, 408, 409, 410, 411, 412, 413, 414, 415, 416, 417, 418, 419, 420, 421, 422, 423, 424, 425, 426, 427, 428, 429, 430, 431, 432, 433, 434, 435, 436, 437, 438, 439, 440, 441, 442, 443, 444, 445, 446, 447, 448, 449, 450, 451, 452, 453, 454, 455, 456, 457, 458, 459, 460, 461, 462, 463, 464, 465, 466, 467, 468, 469, 470, 471, 472, 473, 474, 475, 476, 477, 478, 479, 480, 481, 482, 483, 484, 485, 486, 487, 488, 489, 490, 491, 492, 493, 494, 495, 496, 497, 498, 499, 500, 501, 502, 503, 504, 505, 506, 507, 508, 509, 510, 511, 512, 513, 514, 515, 516, 517, 518, 519, 520, 521, 522, 523, 524, 525, 526, 527, 528, 529, 530, 531, 532, 533, 534, 535, 536, 537, 538, 539, 540, 541, 542, 543, 544, 545, 546, 547, 548, 549, 550, 551, 552, 553, 554, 555, 556, 557, 558, 559, 560, 561, 562, 563, 564, 565, 566, 567, 568, 569, 570, 571, 572, 573, 574, 575, 576, 577, 578, 579, 580, 581, 582, 583, 584, 585, 586, 587, 588, 589, 590, 591, 592, 593, 594, 595, 596, 597, 598, 599, 600, 601, 602, 603, 604, 605, 606, 607, 608, 609, 610, 611, 612, 613, 614, 615, 616, 617, 618, 619, 620, 621, 622, 623, 624, 625, 626, 627, 628, 629, 630, 631, 632, 633, 634, 635, 636, 637, 638, 639, 640, 641, 642, 643, 644, 645, 646, 647, 648, 649, 650, 651, 652, 653, 654, 655, 656, 657, 658, 659, 660, 661, 662, 663, 664, 665, 666, 667, 668, 669, 670, 671, 672, 673, 674, 675, 676, 677, 678, 679, 680, 681, 682, 683, 684, 685, 686, 687, 688, 689, 690, 691, 692, 693, 694, 695, 696, 697, 698, 699, 700, 701, 702, 703, 704, 705, 706, 707, 708, 709, 710, 711, 712, 713, 714, 715, 716, 717, 718, 719, 720, 721, 722, 723, 724, 725, 726, 727, 728, 729, 730, 731, 732, 733, 734, 735, 736, 737, 738, 739, 740, 741, 742, 743, 744, 745, 746, 747, 748, 749, 750, 751, 752, 753, 754, 755, 756, 757, 758, 759, 760, 761, 762, 763, 764, 765, 766, 767, 768, 769, 770, 771, 772, 773, 774, 775, 776, 777, 778, 779, 780, 781, 782, 783, 784, 785, 786, 787, 788, 789, 790, 791, 792, 793, 794, 795, 796, 797, 798, 799, 800, 801, 802, 803, 804, 805, 806, 807, 808, 809, 810, 811, 812, 813, 814, 815, 816, 817, 818, 819, 820, 821, 822, 823, 824, 825, 826, 827, 828, 829, 830, 831, 832, 833, 834, 835, 836, 837, 838, 839, 840, 841, 842, 843, 844, 845, 846, 847, 848, 849, 850, 851, 852, 853, 854, 855, 856, 857, 858, 859, 860, 861, 862, 863, 864, 865, 866, 867, 868, 869, 870, 871, 872, 873, 874, 875, 876, 877, 878, 879, 880, 881, 882, 883, 884, 885, 886, 887, 888, 889, 890, 891, 892, 893, 894, 895, 896, 897, 898, 899, 900, 901, 902, 903, 904, 905, 906, 907, 908, 909, 910, 911, 912, 913, 914, 915, 916, 917, 918, 919, 920, 921, 922, 923, 924, 925, 926, 927, 928, 929, 930, 931, 932, 933, 934, 935, 936, 937, 938, 939, 940, 941, 942, 943, 944, 945, 946, 947, 948, 949, 950, 951, 952, 953, 954, 955, 956, 957, 958, 959, 960, 961, 962, 963, 964, 965, 966, 967, 968, 969, 970, 971, 972, 973, 974, 975, 976, 977, 978, 979, 980, 981, 982, 983, 984, 985, 986, 987, 988, 989, 990, 991, 992, 993, 994, 995, 996, 997, 998, 999, 1000	215,112.5
TOWNHOME	8 TO 11, (BOTH INCLUSIVE), 22, 23, 28, 29, 34, 35, 48, 50, 56, 60, 64, 66, AND 110	54,578.7
BACK-TO-BACK TOWNHOME	12 TO 14, (BOTH INCLUSIVE), AND 16	10,524.5
REAR LANE TOWNHOME	15, 100, 101, 102, 103, 106, 107, 108 AND 109	26,421.2
WALKWAYS	17, 77, 104, 105, 111, 112, 113, 129 AND 132	1,510.5
OPEN SPACE	119 AND 130	3,413.8
BUS LANE	18 AND 116	12,894.2
FUTURE DEVELOPMENT	120	8,233.9
PARK	19, 117, 122 AND 123	44,118.1
NATURAL HERITAGE SYSTEM	124, 125 AND 126	56,283.3
JOCK RIVER OPEN SPACE	127 AND 128	236,996.6
STREET WIDENING	110 AND 118	5,989.5
STREETS	'1' TO '39', (BOTH INCLUSIVE)	174,229.7
LANES	'1' TO '5', (BOTH INCLUSIVE)	7,345.1
TOTAL:		857,651.6

SUBJECT TO THE CONDITIONS, IF ANY, SET FORTH IN OUR LETTER DATED... THIS DRAFT PLAN IS APPROVED BY THE CITY OF OTTAWA UNDER SECTION 51 OF THE PLANNING ACT THIS... DAY OF... 2022.

LILY XU, MCRP, RPP, MANAGER DEVELOPMENT REVIEW SOUTH PLANNING, REAL ESTATE AND ECONOMIC DEVELOPMENT DEPARTMENT, CITY OF OTTAWA

ADDITIONAL INFORMATION AS REQUIRED UNDER SECTION 51(17) OF THE PLANNING ACT R.S.O. 2001

(X) - AS SHOWN ON THIS DRAFT AND KEY PLAN
 (O) - AS SHOWN ON THIS DRAFT AND KEY PLAN
 (D) - LAND TO BE USED IN ACCORDANCE WITH THE SCHEDULE OF LAND USE
 (H) - FULL MUNICIPAL SERVICES
 (S) - OFFSHORE MARINE DEPOSITS OF CLAY, SILT, CLAY AND SILT, BEDROCK
 OTTAWA FORMATION, LIMESTONE



"PHASE 5" AREA
 SUBJECT OF PLAN
 REVISIONS.
 DECEMBER 2022

DRAFT PLAN OF SUBDIVISION
 PART OF LOTS 13 AND 14
 CONCESSION 3 (RIDEAU FRONT)
 PART OF LOTS 13 AND 14
 CONCESSION 4 (RIDEAU FRONT)
 GEOGRAPHIC TOWNSHIP OF NEPEAN
 CITY OF OTTAWA
 SCALE 1:1500
 J.D. BARNES LIMITED
 © COPYRIGHT 2022
 DISTANCES AND/OR COORDINATES SHOWN ON THIS PLAN ARE IN METRES AND CAN BE CONVERTED TO FEET BY DIVIDING BY 0.3048

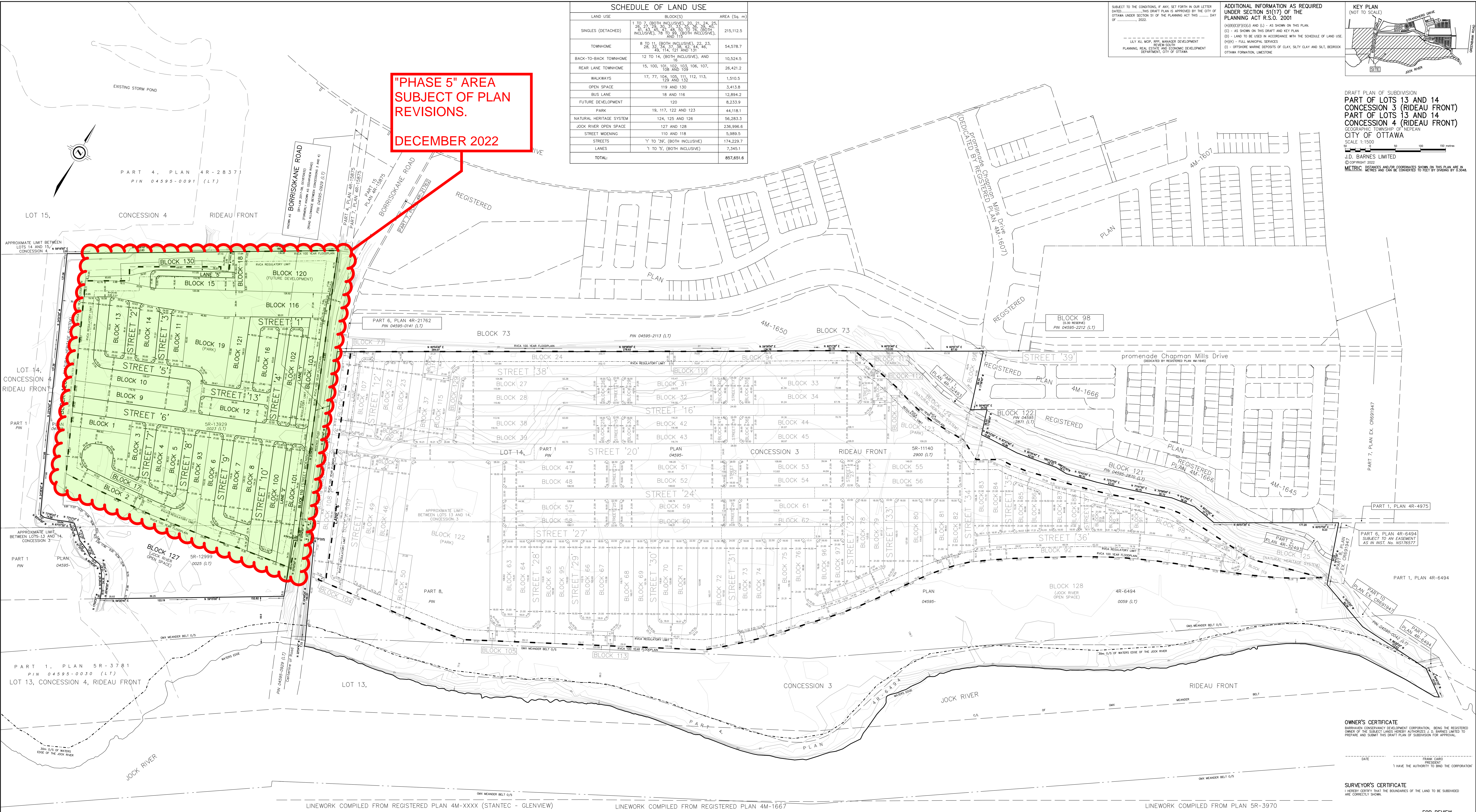


FIGURE 2B
2022 PROPOSED REVISED DRAFT PLAN

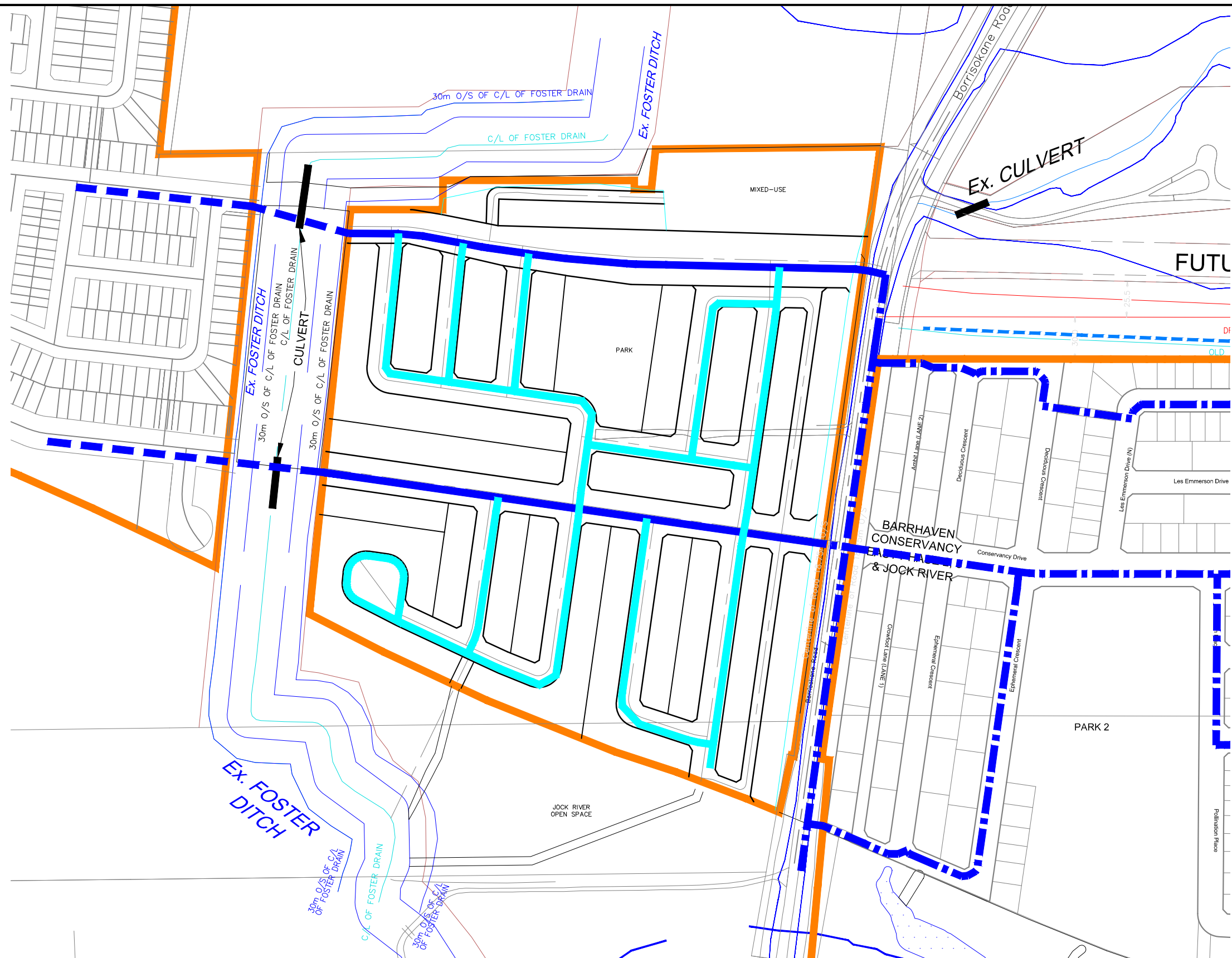
OWNER'S CERTIFICATE
 I HEREBY CERTIFY THAT THE BOUNDARIES OF THE LAND TO BE SUBDIVIDED ARE CORRECTLY SHOWN.

SURVEYOR'S CERTIFICATE
 I HEREBY CERTIFY THAT THE BOUNDARIES OF THE LAND TO BE SUBDIVIDED ARE CORRECTLY SHOWN.

FOR REVIEW
 DATE: _____
 NAME: _____
 TITLE: _____

J.D. BARNES LIMITED
 LAND INFORMATION SPECIALISTS
 455 KENNEDY ROAD, SUITE 101, MARKHAM, ONTARIO L3R 9W7
 T: (905) 751-7584 F: (905) 254-8619 www.jdbarnes.com

DATE: 12/22/2022



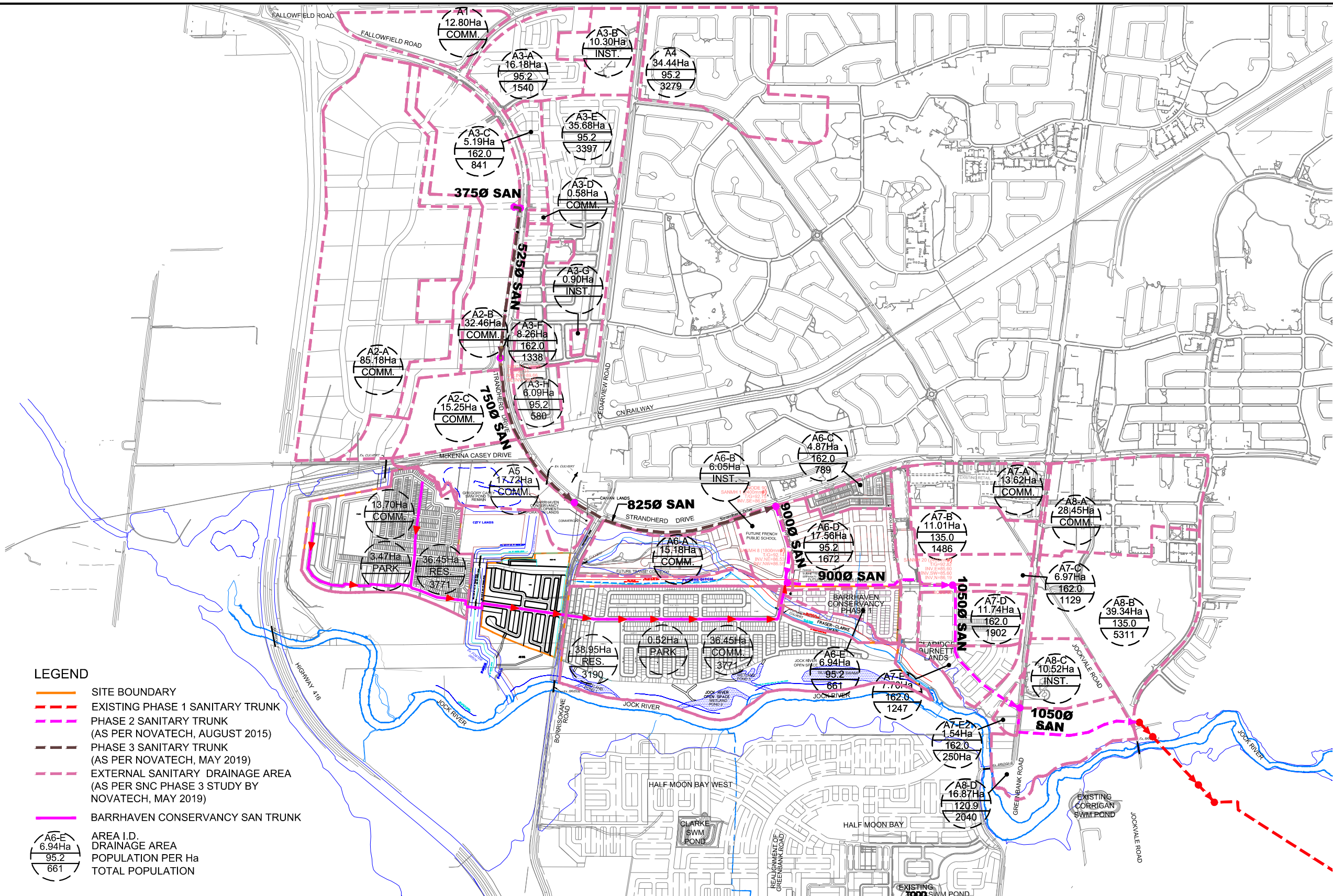
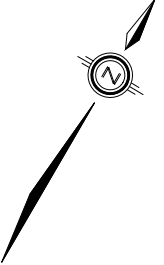
LEGEND	
	SITE BOUNDARY
	PROPOSED 300mm WATERMAIN
	PROPOSED LOCAL WATERMAIN
	EXTERNAL 300mm WATERMAIN
	FUTURE 300mm WATERMAIN



120 Iber Road, Unit 103
 Stittsville, ON K2S 1E9
 TEL: (613) 836-0856
 FAX: (613) 836-7183
 www.DSEL.ca

BARRHAVEN CONSERVANCY EAST PHASE 5
WATERMAIN SERVICING PLAN
 CITY OF OTTAWA

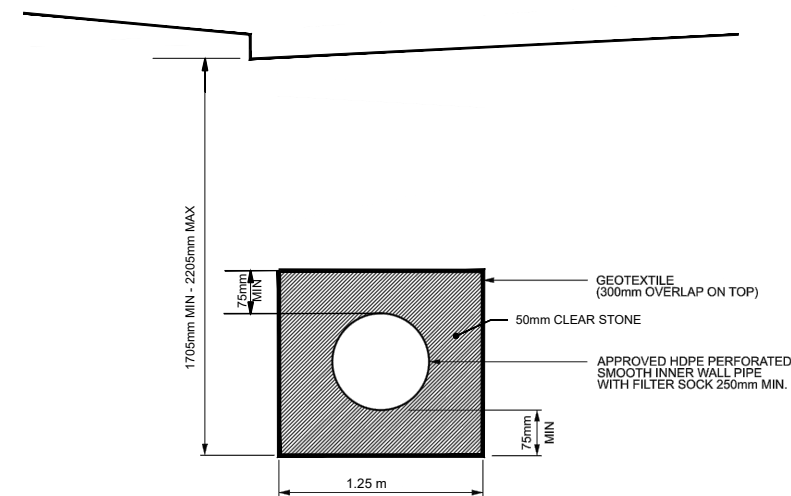
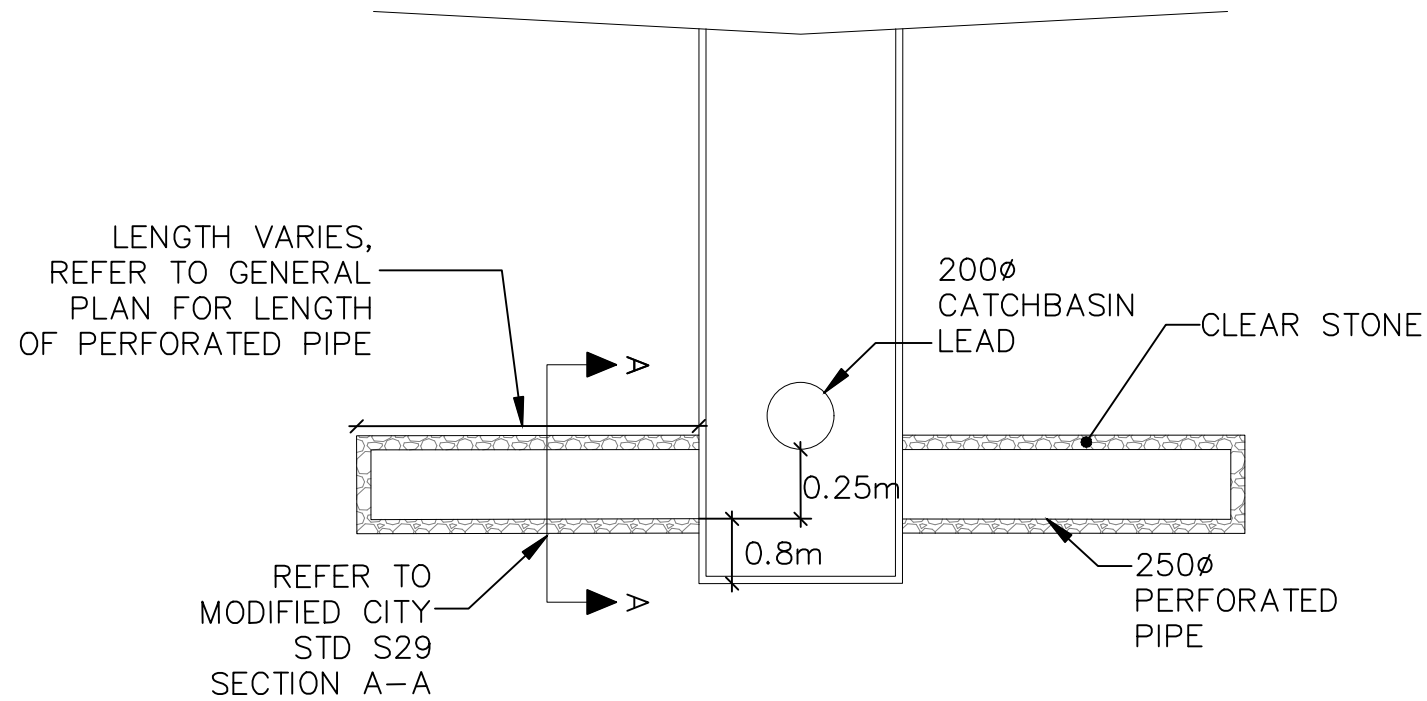
PROJECT No.:	20-1180 A-5
SCALE:	1:3000
DATE:	DECEMBER 2022
FIGURE:	3



120 Iber Road, Unit 103
Stittsville, ON K2S 1E9
TEL: (613) 836-0856
FAX: (613) 836-7183
www.DSEL.ca

**BARRHAVEN CONSERVANCY EAST PHASE 5
EXTERNAL SANITARY SERVICING
CITY OF OTTAWA**

PROJECT No.:	20-1180 A-5
SCALE:	1:18000
DATE:	DECEMBER 2022
FIGURE:	4



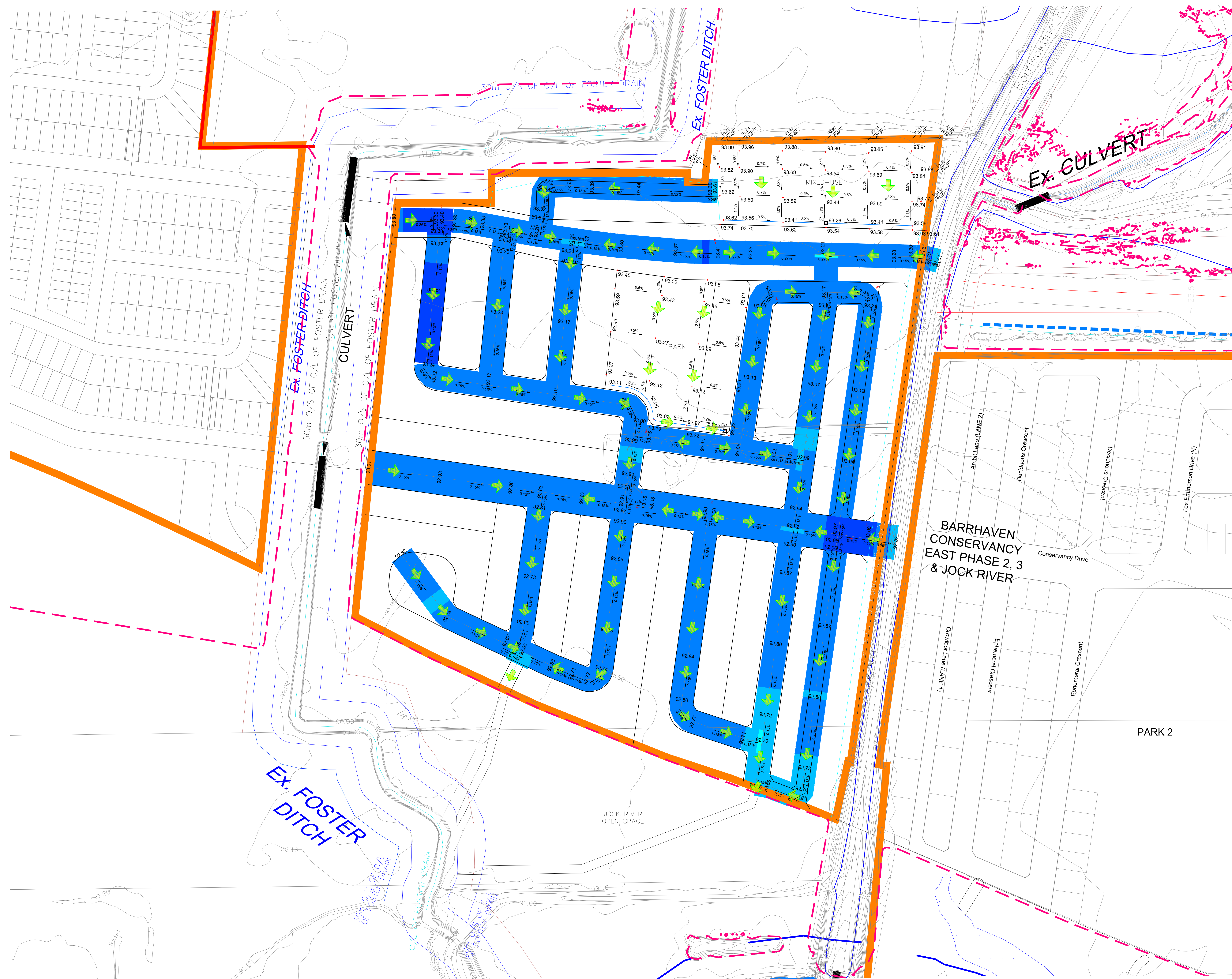
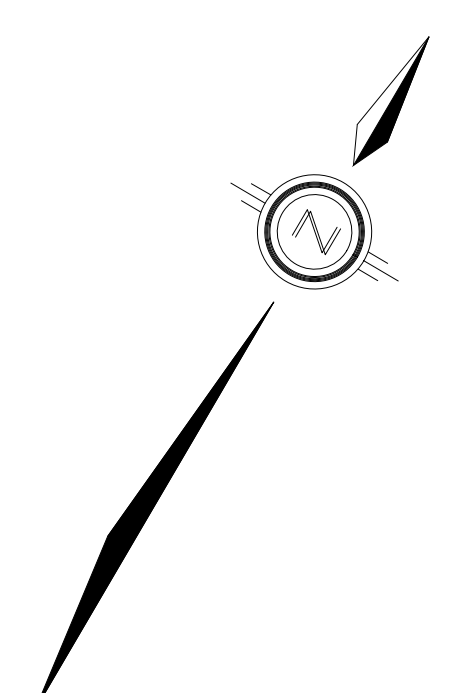
SECTION A-A: MODIFIED CITY STD S29
SCALE: N.T.S.



120 Iber Road, Unit 103
Stittsville, ON K2S 1E9
TEL: (613) 836-0856
FAX: (613) 836-7183
www.DSEL.ca

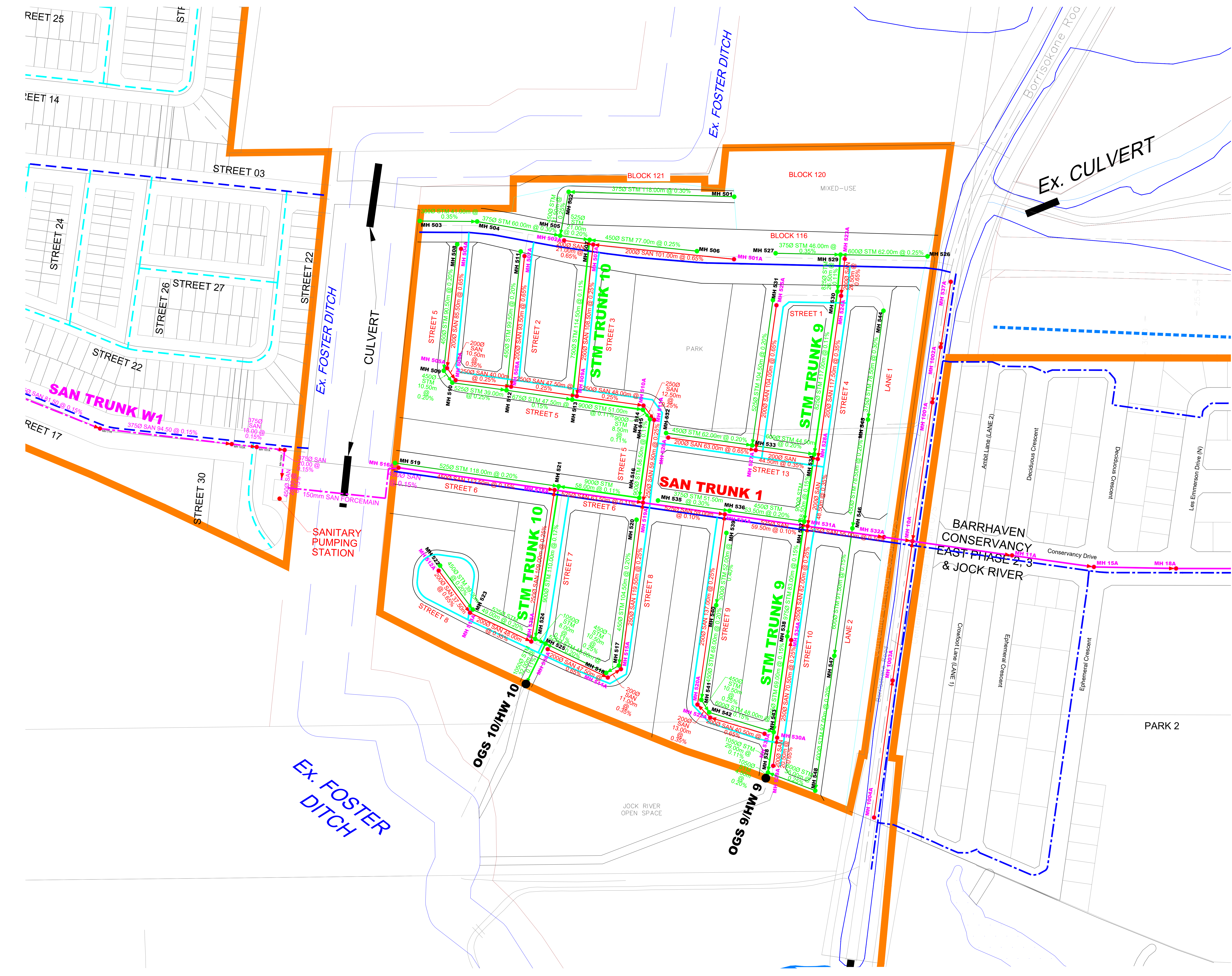
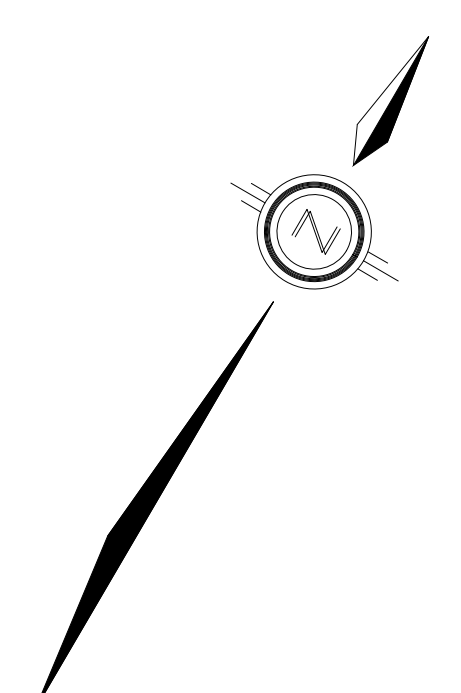
BARRHAVEN CONSERVANCY EAST PHASE 5
FILTRATION SYSTEM DETAILS
CITY OF OTTAWA

PROJECT No.:	20-1180 A-5
SCALE:	NTS
DATE:	DECEMBER 2022
FIGURE:	5

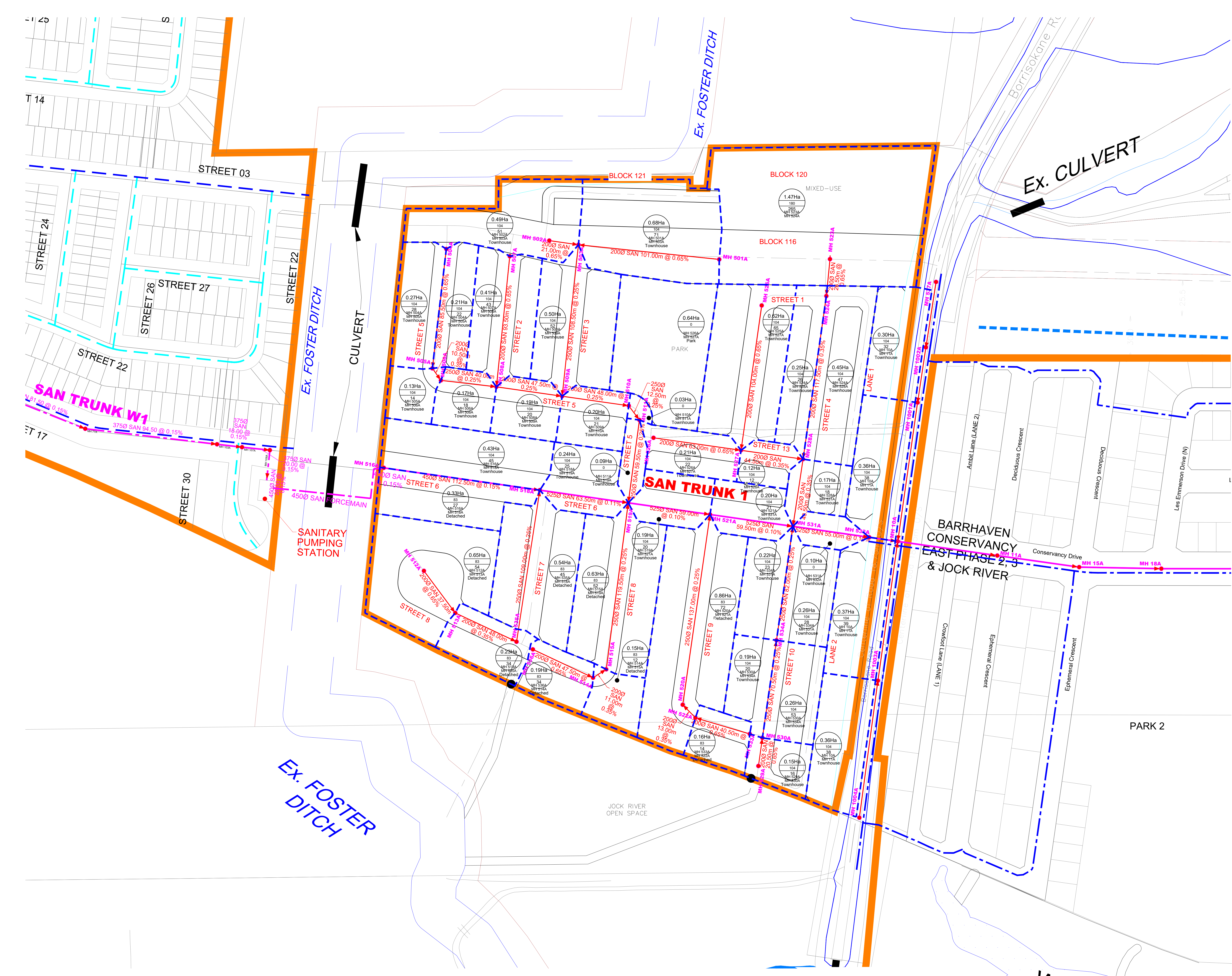
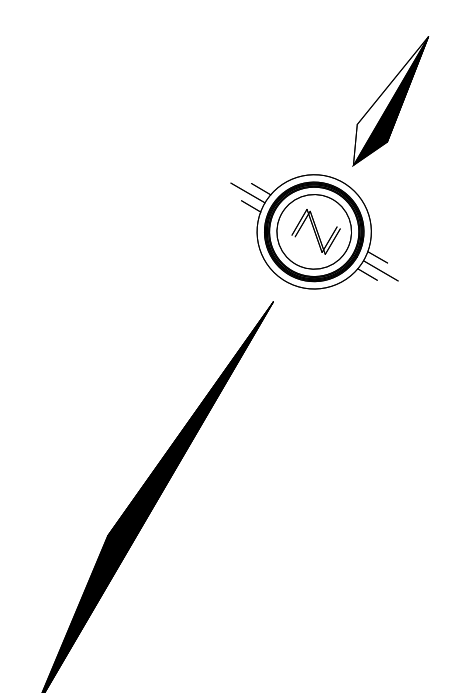


LEGEND

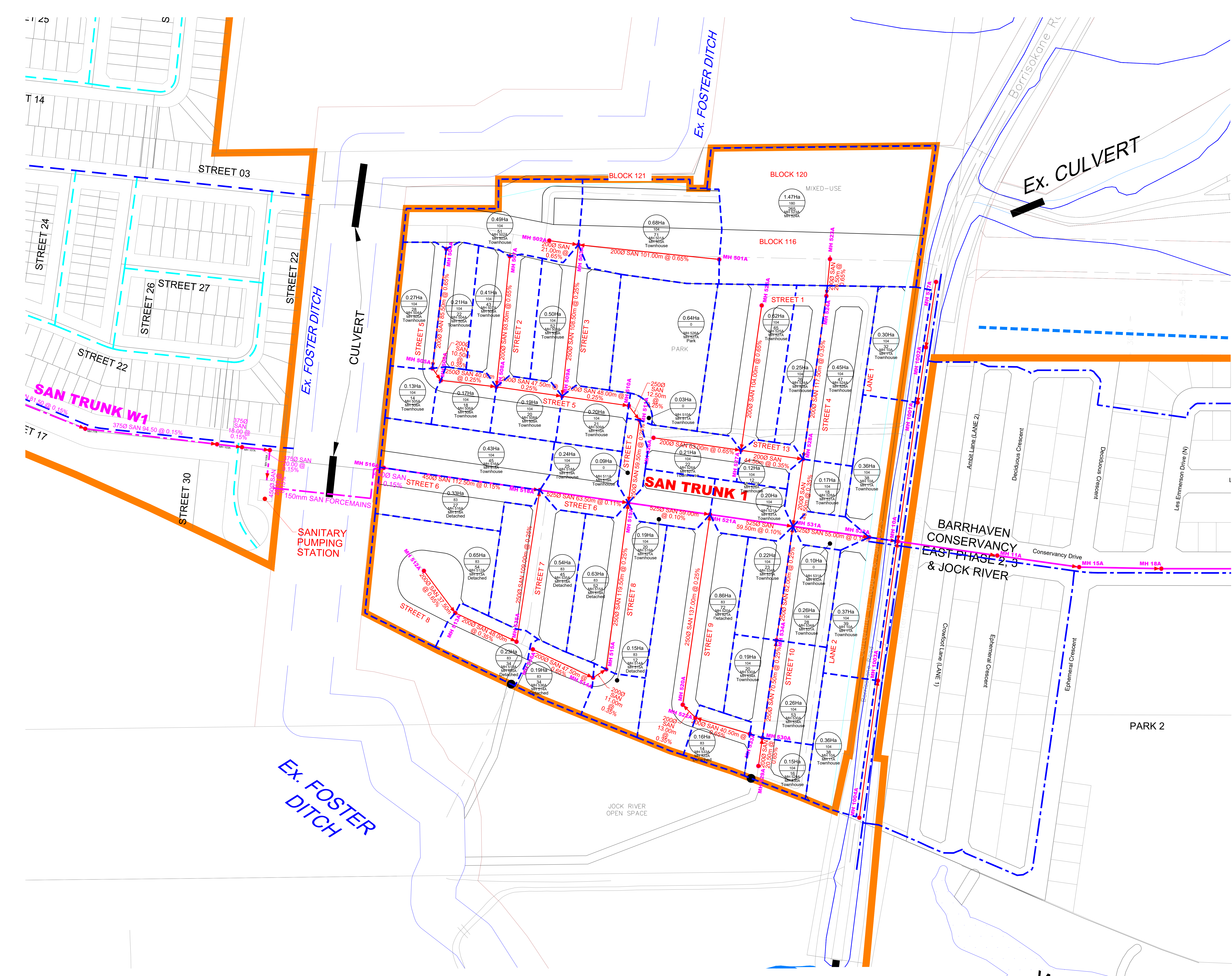
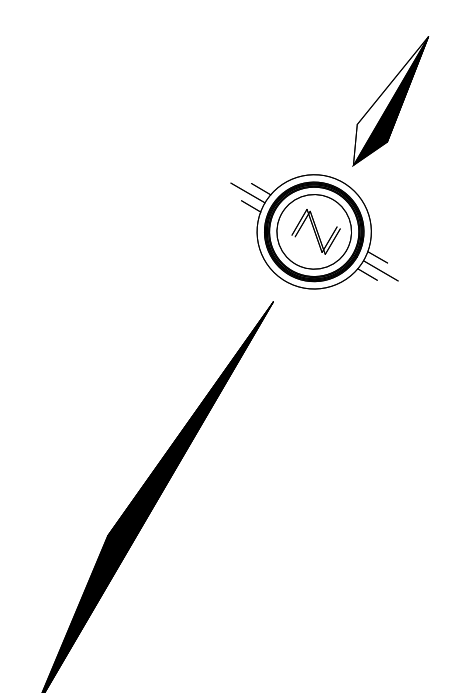
	SITE BOUNDARY		CUT-FILL DEPTH ALONG CENTER LINE:
	STORM OVERLAND FLOW ARROW		CUT DEPTH (m)
	PROPOSED CENTERLINE ELEVATION		FILL DEPTH (m)
	PROPOSED ELEVATION		0.00-0.50:
	EXISTING CONTOUR ELEVATION		0.50-1.00:
	2019 RVCA APPROVED FLOODLINE BOUNDARY		1.00-1.50:
	PROPOSED FLOODLINE PER MARCH 2021 RVCA APPLICATION		1.50-2.00:
			>2.00:



LEGEND	
[Orange line]	SITE BOUNDARY
[Green line]	STORM TRUNK SEWER
[Red line]	STORM LOCAL SEWER
[Blue line]	SANITARY TRUNK SEWER
[Purple line]	SANITARY LOCAL SEWER
[Pink line]	EXTERNAL SANITARY TRUNK SEWER
[Light blue line]	PROPOSED 300mm WATERMAIN
[Dark blue line]	PROPOSED LOCAL WATERMAIN
[Light blue dashed line]	FUTURE 300mm WATERMAIN
[Dark blue dashed line]	EXTERNAL 300mm WATERMAIN
[Green dot]	STORM MANHOLE
[Red dot]	SANITARY MANHOLE

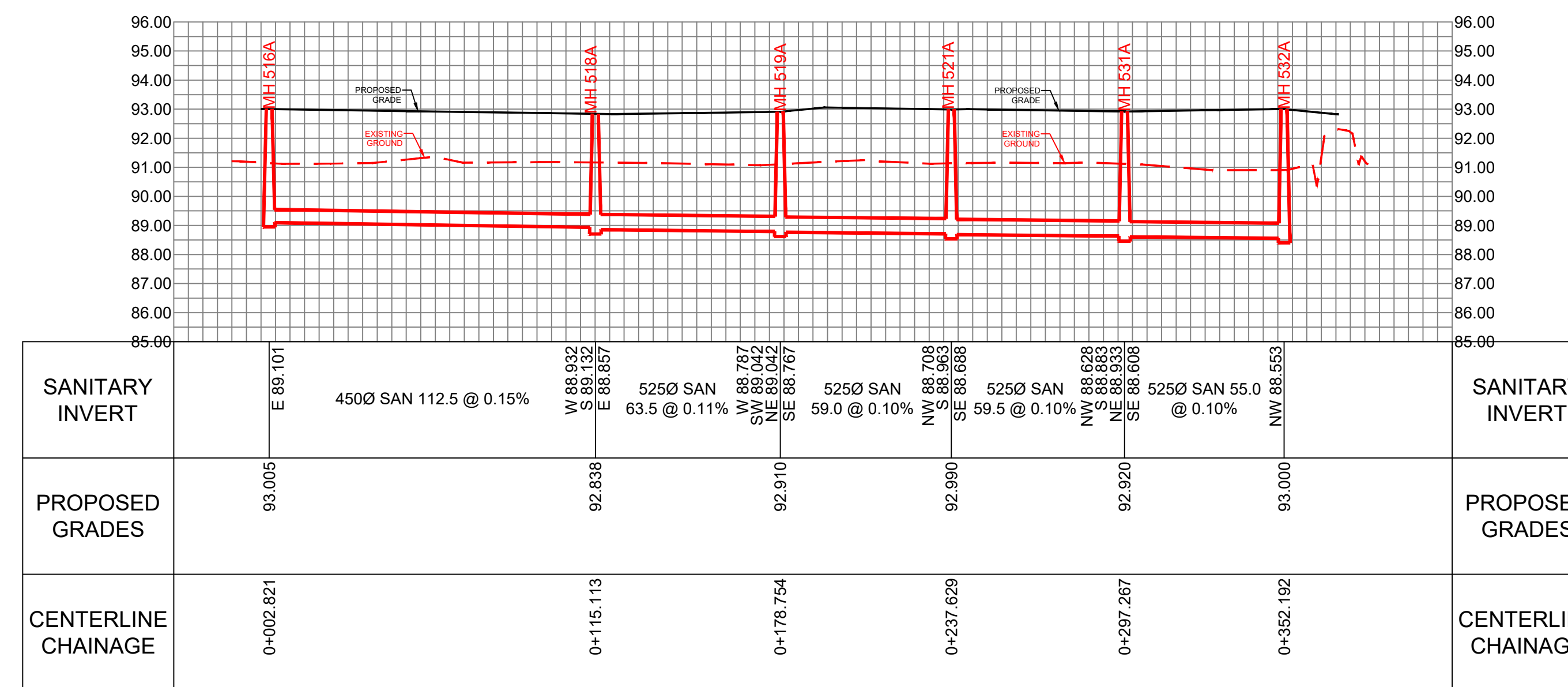


- LEGEND**
- SITE BOUNDARY
 - SANITARY TRUNK SEWER
 - SANITARY LOCAL SEWER
 - EXTERNAL SANITARY TRUNK SEWER
 - SANITARY MANHOLE
 - SANITARY TRIBUTARY AREA
 - AREA IN HECTARES
 - POPULATION PER HECTARE
 - POPULATION
 - AREA TYPE

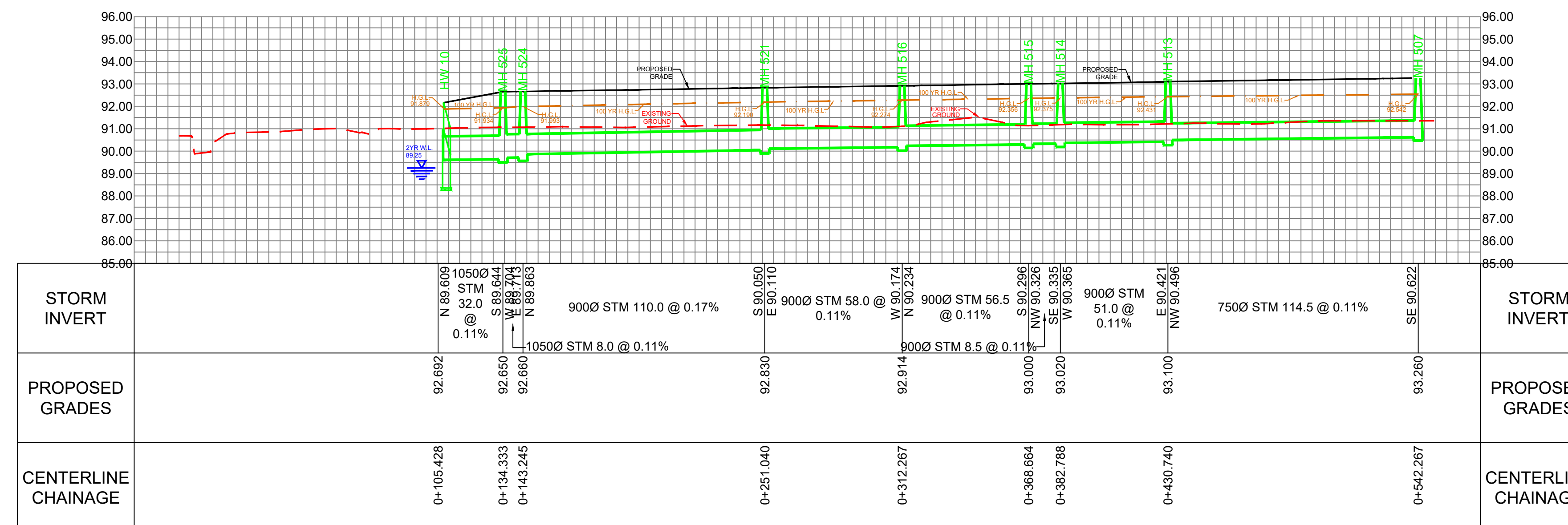


- LEGEND**
- SITE BOUNDARY
 - SANITARY TRUNK SEWER
 - SANITARY LOCAL SEWER
 - EXTERNAL SANITARY TRUNK SEWER
 - SANITARY MANHOLE
 - SANITARY TRIBUTARY AREA
 - AREA IN HECTARES
 - POPULATION PER HECTARE
 - POPULATION
 - AREA TYPE

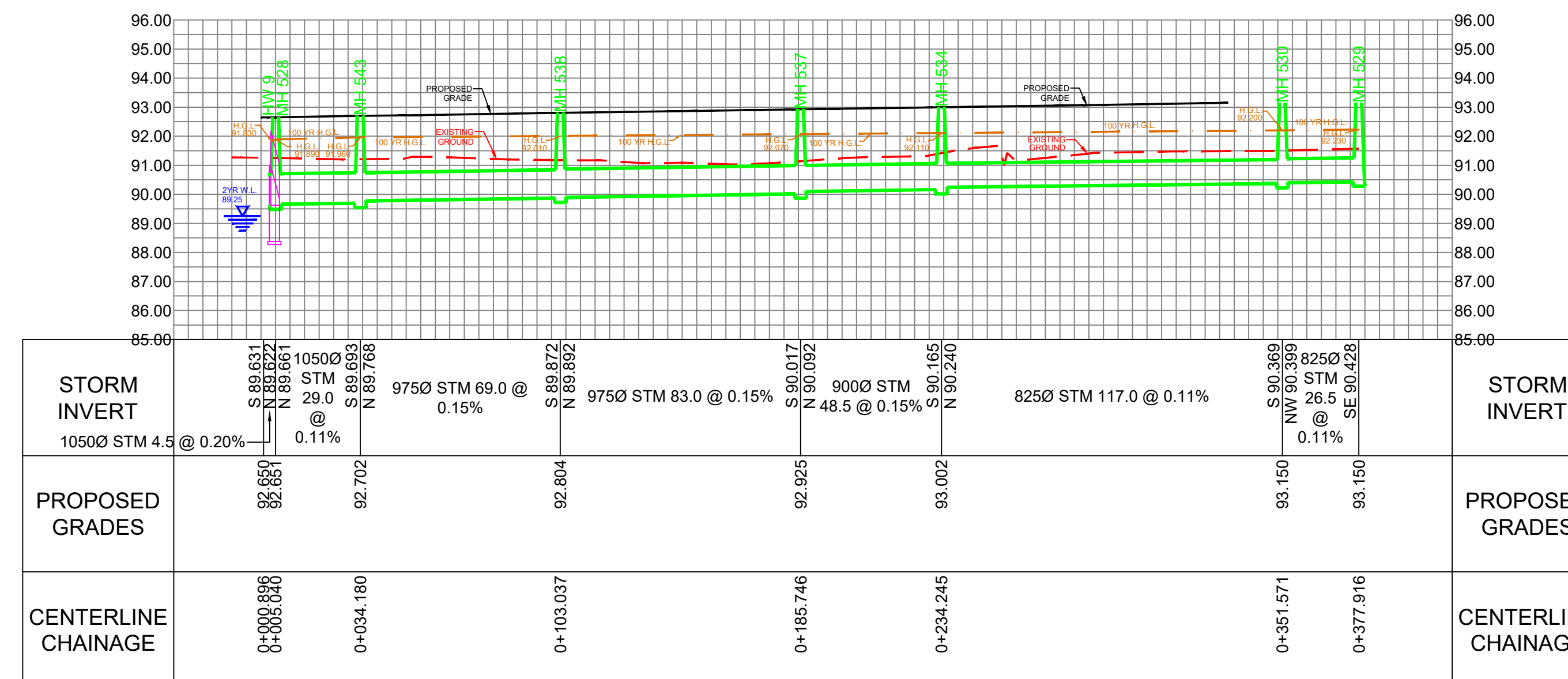
SAN TRUNK 1



STM TRUNK 10



STM TRUNK 9



120 Iber Road, Unit 103
Stittville, ON K2S 1E9
Tel. (613) 836-0856
Fax. (613) 836-7183
www.DSEL.ca

BARRHAVEN CONSERVANCY EAST PHASE 5
SANITARY AND STORM TRUNK PROFILES
CITY OF OTTAWA

PROJECT No. : 20-1180 A-5
SCALE: 1:1500
DATE: DECEMBER 2022
DRAWING No. 5

APPENDIX A

GENERAL

Content Copy Of Original



Ministry of the Environment and Climate Change
Ministère de l'Environnement et de l'Action en matière de changement
climatique

ENVIRONMENTAL COMPLIANCE APPROVAL

NUMBER 8129-AB7LDF

Issue Date: June 23, 2016

City of Ottawa
100 Constellation Crescent West, 6th Floor
Ottawa, Ontario
K2G 6J8

Site Location: Jockvale Road and Strandherd Drive
City of Ottawa, Ontario

You have applied under section 20.2 of Part II.1 of the Environmental Protection Act , R.S.O. 1990, c. E. 19 (Environmental Protection Act) for approval of:

sanitary sewers to be constructed in the City of Ottawa, on various vacant development lands (from Station 0+003 to Station 2+517), Greenbank Road (from Station 1+846 to Station 1+947), and Jockvale Road (from Station 2+430 to Station 2+517);

all in accordance with the application form from the City of Ottawa, dated June 22, 2016, including final plans and specifications prepared by Novatech Engineers, Planners and Landscape Architects.

In accordance with Section 139 of the Environmental Protection Act, you may by written Notice served upon me and the Environmental Review Tribunal within 15 days after receipt of this Notice, require a hearing by the Tribunal. Section 142 of the Environmental Protection Act provides that the Notice requiring the hearing shall state:

1. The portions of the environmental compliance approval or each term or condition in the environmental compliance approval in respect of which the hearing is required, and;
2. The grounds on which you intend to rely at the hearing in relation to each portion appealed.

The Notice should also include:

3. The name of the appellant;
4. The address of the appellant;
5. The environmental compliance approval number;
6. The date of the environmental compliance approval;
7. The name of the Director, and;
8. The municipality or municipalities within which the project is to be engaged in.

And the Notice should be signed and dated by the appellant.

This Notice must be served upon:

The Secretary*
Environmental Review Tribunal
655 Bay Street, Suite 1500

AND

The Director appointed for the
purposes of Part II.1 of the
Environmental Protection Act

Toronto, Ontario
M5G 1E5

Ministry of the Environment and
Climate Change
135 St. Clair Avenue West, 1st
Floor
Toronto, Ontario
M4V 1P5

*** Further information on the Environmental Review Tribunal's requirements for an appeal can be obtained directly from the Tribunal at: Tel: (416) 212-6349, Fax: (416) 326-5370 or www.ert.gov.on.ca**

The above noted activity is approved under s.20.3 of Part II.1 of the Environmental Protection Act.

DATED AT TORONTO this 23rd day of June, 2016

Gregory Zimmer, P.Eng.
Director
appointed for the purposes of Part II.1 of
the *Environmental Protection Act*

AF/
c: District Manager, MOECC Ottawa
Water Supervisor, MOECC, Ottawa
M. Rick O'Connor, City Clerk, City of Ottawa
Luc Marineau, City of Ottawa
Jonathan Knoyle, City of Ottawa
Bob Dowdall, Novatech Engineers, Planners and Landscape Architects
Edson Donnelly, Novatech Engineers, Planners and Landscape Architects

ENVIRONMENTAL COMPLIANCE APPROVAL

NUMBER 4357-CHMQEM
Issue Date: September 1, 2022

Barrhaven Conservancy Development Corporation
2934 Baseline Road, Suite 302
Ottawa, Ontario
K2H 1B2

Site Location: Barrhaven Conservancy East - Phase 2, 3 & Jock River
Part of Lots 13 & 14 (Rideau Front)
City of Ottawa, Ontario

You have applied under section 20.2 of Part II.1 of the Environmental Protection Act, R.S.O. 1990, c. E. 19 (Environmental Protection Act) for approval of:

the establishment of wastewater infrastructure Works located in the City of Ottawa, consisting of the following:

- **sanitary sewers** on Les Emmerson Drive (N)(from Station 0+000.000 to Station 0+720.000), Les Emmerson Drive (S) (from Station 0+000.000 to Station 0+660.000), Conservancy Drive (from Station 0-010.000 to Station 0+973.545), Peninsula Road (from Station 0+010.058 to Station 0+703.797), Sapling Grove (from Station 0+000.000 to Station 0+528.245), Canoe Street (from Station 0+000.000 to Station 0+491.136), Deciduous Crescent (from Station 0+002.000 to Station 0+328.189), Ephemeral Crescent (from Station 0+000.000 to Station 0+492.987), Mineral Street (from Station 0+242.832 to Station 0+000.000), Pollination Place (from Station 0+002.985 to Station 0+433.904), Gallium Crescent (from Station 0+002.728 to Station 0+321.940), Syringa Court (from Station 0+000.000 to Station 0+332.328), Anemone Mews (from Station 0+242.833 to Station 0+059.755), Ainsworth Crescent (from Station 0+002.715 to Station 0+353.228), Ecology Lane (from Station 0+205.411 to Station 0+007.658), Meander Way (from Station 0+002.747 to Station 0+333.559), Elation Heights (from Station 0+000.000 to Station 0+380.000), Jollity Crescent (from Station 0+001.794 to Station 0+221.612), Euphoria Crescent (from Station 0+000.000 to Station 0+170.000), and on Borrisokane Road (from Station 0+168.736 to Station 0+507.126), all discharging to the existing South Nepean Collector sanitary sewer; and

- **storm sewers** on Les Emmerson Drive (N) (from Station 0+002.919 to Station 0+718.915), Les Emmerson Drive (S) (from Station 0-002.269 to Station 0+676.895), Conservancy Drive (from Station 0+020.468 to Station 0+961.195), Peninsula Road (from Station 0-001.986 to Station 0+705.797), Sapling Grove (from Station 0-010.000 to Station 0+526.245), Canoe Street (from Station 0+000.000 to Station 0+493.136), Deciduous Crescent (from Station 0+004.500 to Station 0+324.827), Ephemeral Crescent (from Station 0-002.063 to Station 0+495.738), Mineral Street (from Station 0+244.847 to Station 0+002.015), Pollination Place (from Station 0+000.000 to Station 0+424.262), Gallium Crescent (from Station 0+000.000 to Station 0+325.307), Syringa Court (from Station 0-001.985 to Station 0+334.348), Anemone Mews (from Station 0+244.843 to Station 0+001.982), Ainsworth Crescent (from Station 0+000.000 to Station 0+354.443), Ecology Lane (from Station 0+207.411 to Station 0+006.523), Meander Way (from Station 0+016.643 to Station 0+335.359), Elation Heights (from Station 0+000.000 to Station 0+381.539), Jollity Crescent (from Station 0+003.277 to Station 0+220.000), Euphoria Crescent (from Station 0+003.400 to Station 0+157.175), Lane 1 (Crowfoot Lane) (from Station 0-002.000 to Station 0+201.525), and on Lane 2 (Ambit Lane) (from Station 0+002.000 to Station 0+127.5060), proposed storm sewers collect flows from the subdivision and discharge to the Jock River and the Fraser-Clarke Watercourse which is an existing tributary to the Jock River;

the modification of a section of the Fraser-Clarke Watercourse to accommodate stormwater outflows from Phase 2 of the Barrhaven Conservancy East Subdivision development, for the collection and transmission of stormwater runoff for all storm events up to and including the 100-year storm event, discharging to the Jock River, consisting of the following:

- **approximately 950 metres long modified channel**, located along the northern boundary of the Barrhaven Conservancy East Phase 2, 3 & Jock River, having a channel gradient of 0.09% and 3:1 side slopes, complete with low flow path and riffle-pool sequences and erosion protection structures, including two (2) 2.4 metre by 1.2 metre box culverts under the future Canoe Street crossing, discharging to the Jock River;

the establishment of stormwater management Works to serve the Barrhaven Conservancy East – Phase 2, 3 & Jock River development, located in the City of Ottawa, for the collection, transmission, treatment and disposal of stormwater runoff from a total catchment area of 44.17 hectares, to provide Enhanced Level protection and to provide on-site retention of 22.5 cubic metres per hectare, discharging to proposed storm sewers, consisting of the following:

- **subsurface infiltration trenches (catchment area 41.81 hectares)**, located on-site within proposed roadways, having a total length of 3,514 metres, a width of 1.75 metres, a base area of 6,150 square metres, a maximum allowable storage depth of 0.40 metres and a maximum available storage volume of 1,087 cubic metres, comprised of a 75 millimetre deep clear stone layer overlying a geotextile non-woven filter fabric, complete with a 250 millimetre diameter perforated storm sub-drain installed in the clear stone layer, installed at select street catch basin manhole locations;

the establishment of stormwater management Works to serve Steeves & Rozema Enterprises Limited, located in the City of Sarnia, consisting of the following:

- **oil and grit separator (catchment area 5.52 hectares):** one (1) oil and grit separator (OGS1), CDS Model PMSU4040-8 or Equivalent Equipment, located within the Canoe Street right-of-way, providing a Predicted Net Annual Load Removal Efficiency of 83%, having a sediment storage capacity of 4,270 litres, an oil storage capacity of 1,970 litres, a total storage volume of approximately 10,910 litres, and a maximum treatment rate of 170 litres per second, receiving inflow from the storm sewer located within the Canoe Street right-of-way, discharging via a 975 millimetre diameter outlet pipe to an outlet channel on Block 774 and connecting to the Jock River;
- **oil and grit separator (catchment area 5.59 hectares):** one (1) oil and grit separator (OGS2), CDS Model PMSU4040-8 or Equivalent Equipment, located within Servicing Block 767, providing a Predicted Net Annual Load Removal Efficiency of 82.1%, having a sediment storage capacity of 4,270 litres, an oil storage capacity of 1,970 litres, a total storage volume of approximately 10,910 litres, and a maximum treatment rate of 170 litres per second, receiving inflow from the storm sewer located within the Block 767 and Meander Way right-of-way, discharging via a 975 millimetre diameter outlet pipe to an outlet channel on Block 774 and connecting to the Jock River;
- **oil and grit separator (catchment area 6.77 hectares):** one (1) oil and grit separator (OGS3), CDS Model PMSU4045-8 or Equivalent Equipment, located within the Ainsworth Crescent right-of-way, providing a Predicted Net Annual Load Removal Efficiency of 82.4%, having a sediment storage capacity of 4,270 litres, an oil storage capacity of 2,149 litres, a total storage volume of approximately 11,510 litres, and a maximum treatment rate of 212 litres per second, receiving inflow from the storm sewer located within the Ainsworth Crescent right-of-way, discharging via a 975 millimetre diameter outlet pipe to an outlet channel on Block 774 and connecting to the Jock River;
- **oil and grit separator (catchment area 8.42 hectares):** one (1) oil and grit separator (OGS5), CDS Model PMSU5640-10 or Equivalent Equipment, located within Servicing Block 766, providing a Predicted Net Annual Load Removal Efficiency of 81.7%, having a sediment storage capacity of 6,672 litres, an oil storage capacity of 2,869 litres, a total storage volume of approximately 17,070 litres, and a maximum treatment rate of 255 litres per second, receiving inflow from the storm sewer located within Block 766 and the Gallium Crescent right-of-way, discharging via a 1050 millimetre diameter outlet pipe to an outlet channel on Block 774 and connecting to the Jock River;

- **oil and grit separator (catchment area 5.46 hectares):** one (1) oil and grit separator (OGS6), CDS Model PMSU3035-8 or Equivalent Equipment, located within Servicing Block 765, providing a Predicted Net Annual Load Removal Efficiency of 80.0%, having a sediment storage capacity of 4,270 litres, an oil storage capacity of 1,493 litres, a total storage volume of approximately 10,210 litres, and a maximum treatment rate of 108 litres per second, receiving inflow from the storm sewer located within Block 766 and the Pollination Place right-of-way, discharging via a 900 millimetre diameter outlet pipe to an outlet channel on Block 774 and connecting to the Jock River;
- **oil and grit separator (catchment area 5.05 hectares):** one (1) oil and grit separator (OGS7), CDS Model PMSU4040-8 or Equivalent Equipment, located within the Ephemeral Crescent right-of-way, providing a Predicted Net Annual Load Removal Efficiency of 82.3%, having a sediment storage capacity of 4,270 litres, an oil storage capacity of 1,970 litres, a total storage volume of approximately 10,910 litres, and a maximum treatment rate of 170 litres per second, receiving inflow from the storm sewer located within the Ephemeral Crescent right-of-way, discharging via a 900 millimetre diameter outlet pipe to an outlet channel on Block 774 and connecting to the Jock River;
- **oil and grit separator (catchment area 4.52 hectares):** one (1) oil and grit separator (OGS8), CDS Model PMSU4040-8 or Equivalent Equipment, located within Servicing Block 744, providing a Predicted Net Annual Load Removal Efficiency of 82.1%, having a sediment storage capacity of 4,270 litres, an oil storage capacity of 1,970 litres, a total storage volume of approximately 10,910 litres, and a maximum treatment rate of 170 litres per second, receiving inflow from the storm sewer located within the Borrisokane Road right-of-way, discharging via a 1200 millimetre diameter outlet pipe to an outlet channel on Block 774 and connecting to the Jock River;
- **oil and grit separator (catchment area 1.63 hectares):** one (1) oil and grit separator (OGS12), CDS Model PMSU2025-5 or Equivalent Equipment, located within Servicing Block 317, providing a Predicted Net Annual Load Removal Efficiency of 81.1%, having a sediment storage capacity of 1,668 litres, an oil storage capacity of 439 litres, a total storage volume of approximately 3,330 litres, and a maximum treatment rate of 45 litres per second, receiving inflow from the storm sewer located within the Les Emmerson Drive right-of-way, discharging via a 600 millimetre diameter outlet pipe to an outlet channel connecting to the Fraser-Clarke watercourse;
- **oil and grit separator (catchment area 1.21 hectares):** one (1) oil and grit separator (OGS13), CDS Model PMSU2020-5 or Equivalent Equipment, located within the Deciduous Crescent right-of-way, providing a Predicted Net Annual Load Removal Efficiency of 80.1%, having a sediment storage capacity of 1,668 litres, an oil storage capacity of 376 litres, a total storage volume of approximately 3,150 litres, and a maximum treatment rate of 31 litres per second, receiving inflow from the storm sewer located within the Deciduous Crescent right-of-way, discharging via a 600 millimetre diameter outlet pipe to an outlet channel connecting to the Fraser-Clarke watercourse;

including erosion/sedimentation control measures during construction and all other controls and appurtenances essential for the proper operation of the aforementioned Works;

all in accordance with the submitted application and supporting documents listed in Schedule "A" forming part of this Approval.

For the purpose of this environmental compliance approval, the following definitions apply:

1. "Approval" means this entire document and any schedules attached to it, and the application;
2. "Director" means a person appointed by the Minister pursuant to section 5 of the EPA for the purposes of Part II.1 of the EPA;
3. "District Manager" means the District Manager of the appropriate local District Office of the Ministry, where the Works are geographically located;
4. "EPA" means the *Environmental Protection Act*, R.S.O. 1990, c.E.19, as amended;
5. "Equivalent Equipment" means a substituted equipment or like-for-like equipment that meets the required quality and performance standards of the approved named equipment.
6. "Ministry" means the ministry of the government of Ontario responsible for the EPA and OWRA and includes all officials, employees or other persons acting on its behalf;
7. "Owner" means Barrhaven Conservancy Development Corporation, and includes its successors and assignees;
8. "OWRA" means the *Ontario Water Resources Act*, R.S.O. 1990, c. O.40 , as amended;
9. "Works" means the sewage Works described in the Owner's application, and this Approval.

You are hereby notified that this environmental compliance approval is issued to you subject to the terms and conditions outlined below:

TERMS AND CONDITIONS

1. GENERAL CONDITIONS

1. The Owner shall ensure that any person authorized to carry out work on or operate any aspect of the Works is notified of this Approval and the conditions herein and shall take all reasonable measures to ensure any such person complies with the same.

2. Except as otherwise provided by these Conditions, the Owner shall design, build, install, operate and maintain the Works in accordance with the description given in this Approval, and the application for approval of the Works.
3. Where there is a conflict between a provision of any document in the schedule referred to in this Approval and the conditions of this Approval, the conditions in this Approval shall take precedence, and where there is a conflict between the documents in the schedule, the document bearing the most recent date shall prevail.
4. Where there is a conflict between the documents listed in Schedule "A" and the application, the application shall take precedence unless it is clear that the purpose of the document was to amend the application.
5. The conditions of this Approval are severable. If any condition of this Approval, or the application of any requirement of this Approval to any circumstance, is held invalid or unenforceable, the application of such condition to other circumstances and the remainder of this Approval shall not be affected thereby.

2. EXPIRY OF APPROVAL

1. This Approval will cease to apply to those parts of the Works which have not been constructed within five (5) years of the date of this Approval.
2. In the event that completion and commissioning of any portion of the Works is anticipated to be delayed beyond the specified expiry period, the Owner shall submit an application of extension to the expiry period, at least twelve (12) months prior to the end of the period. The application for extension shall include the reason(s) for the delay, whether there is any design change(s) and a review of whether the standards applicable at the time of Approval of the Works are still applicable at the time of request for extension, to ensure the ongoing protection of the environment.

3. CHANGE OF OWNER

1. The Owner shall notify the District Manager and the Director, in writing, of any of the following changes within thirty (30) days of the change occurring:
 - a. change of Owner;
 - b. change of address of the Owner;
 - c. change of partners where the Owner is or at any time becomes a partnership, and a copy of the most recent declaration filed under the *Business Names Act*, R.S.O. 1990, c.B17 shall be included in the notification to the District Manager; or

- d. change of name of the corporation where the Owner is or at any time becomes a corporation, and a copy of the most current information filed under the *Corporations Information Act*, R.S.O. 1990, c. C39 shall be included in the notification to the District Manager.
2. In the event of any change in ownership of the Works, other than a change to a successor municipality, the Owner shall notify in writing the succeeding owner of the existence of this Approval, and a copy of such notice shall be forwarded to the District Manager and the Director.
3. The Owner shall ensure that all communications made pursuant to this condition refer to the number at the top of this Approval.

4. OPERATION AND MAINTENANCE

1. If applicable, any proposed storm sewers or other stormwater conveyance in this Approval can be constructed but not operated until the proposed stormwater management facilities in this Approval or any other Approval that are designed to service the storm sewers or other stormwater conveyance are in operation.
2. The Owner shall make all necessary investigations, take all necessary steps and obtain all necessary approvals so as to ensure that the physical structure, siting and operations of the Works do not constitute a safety or health hazard to the general public.
3. The Owner shall undertake an inspection of the condition of the Works, at least once a year, and undertake any necessary cleaning and maintenance to ensure that sediment, debris and excessive decaying vegetation are removed from the Works to prevent the excessive build-up of sediment, oil/grit, debris and/or decaying vegetation, to avoid reduction of the capacity and/or permeability of the Works, as applicable. The Owner shall also regularly inspect and clean out the inlet to and outlet from the Works to ensure that these are not obstructed.
4. The Owner shall construct, operate and maintain the Works with the objective that the effluent from the Works is essentially free of floating and settleable solids and does not contain oil or any other substance in amounts sufficient to create a visible film, sheen, foam or discoloration on the receiving waters.
5. The Owner shall maintain a logbook to record the results of these inspections and any cleaning and maintenance operations undertaken, and shall keep the logbook at the Owner's administrative office for inspection by the Ministry. The logbook shall include the following:
 - a. the name of the Works; and
 - b. the date and results of each inspection, maintenance and cleaning, including an estimate of the quantity of any materials removed and method of clean-out of the Works.

6. The Owner shall prepare an operations manual prior to the commencement of operation of the Works that includes, but is not necessarily limited to, the following information:
 - a. operating and maintenance procedures for routine operation of the Works;
 - b. inspection programs, including frequency of inspection, for the Works and the methods or tests employed to detect when maintenance is necessary;
 - c. repair and maintenance programs, including the frequency of repair and maintenance for the Works;
 - d. contingency plans and procedures for dealing with potential spills and any other abnormal situations and for notifying the District Manager; and
 - e. procedures for receiving, responding and recording public complaints, including recording any follow-up actions taken.
7. The Owner shall maintain the operations manual current and retain a copy at the Owner's administrative office for the operational life of the Works. Upon request, the Owner shall make the manual available to Ministry staff.

5. TEMPORARY EROSION AND SEDIMENT CONTROL

1. The Owner shall install and maintain temporary sediment and erosion control measures during construction and conduct inspections once every two (2) weeks and after each significant storm event (a significant storm event is defined as a minimum of 25 mm of rain in any 24 hours period). The inspections and maintenance of the temporary sediment and erosion control measures shall continue until they are no longer required and at which time they shall be removed and all disturbed areas reinstated properly.
2. The Owner shall maintain records of inspections and maintenance which shall be made available for inspection by the Ministry, upon request. The record shall include the name of the inspector, date of inspection, and the remedial measures, if any, undertaken to maintain the temporary sediment and erosion control measures.

6. REPORTING

1. One (1) week prior to the start-up of the operation of the Works, the Owner shall notify the District Manager (in writing) of the pending start-up date.
2. The Owner shall, upon request, make all reports, manuals, plans, records, data, procedures and supporting documentation available to Ministry staff.

3. The Owner shall prepare a performance report within ninety (90) days following the end of the period being reported upon, and submit the report(s) to the District Manager when requested. The first such report shall cover the first annual period following the commencement of operation of the Works and subsequent reports shall be prepared to cover successive annual periods following thereafter. The reports shall contain, but shall not be limited to, the following information:
 - a. a description of any operating problems encountered and corrective actions taken;
 - b. a summary of all maintenance carried out on any major structure, equipment, apparatus, mechanism or thing forming part of the Works, including an estimate of the quantity of any materials removed from the Works;
 - c. a summary of any complaints received during the reporting period and any steps taken to address the complaints;
 - d. a summary of all spill or abnormal discharge events; and
 - e. any other information the District Manager requires from time to time.

7. RECORD KEEPING

1. The Owner shall retain for a minimum of five (5) years from the date of their creation, all records and information related to or resulting from the operation, maintenance and monitoring activities required by this Approval.

Schedule "A"

1. Application for Environmental Compliance Approval, dated August 9, 2022 and received on August 17, 2022, submitted by Barrhaven Conservancy Development Corporation;
2. Transfer of Review Letter of Recommendation, dated August 17, 2022 and signed by Jeff Shillington, P.Eng., Senior Project Manager, Development Review, City of Ottawa , including the following supporting documents:
 - a. Final Plans and Specifications prepared by David Schaeffer Engineering Ltd.
 - b. Pipe Data Form - Watermain, Storm Sewer, Sanitary Sewer, and Forcemain Design Supplement to Application for Approval for Water and Sewage Works.
 - c. Hydraulic Design Sheets prepared by David Schaeffer Engineering Ltd.
 - d. Stormwater Management Report prepared by David Schaeffer Engineering Ltd.
 - e. Design brief, calculations and specifications prepared by David Schaeffer Engineering Ltd.
3. Email received on August 25, 2022 from Jeff Shillington, City of Ottawa.

The reasons for the imposition of these terms and conditions are as follows:

1. Condition 1 is imposed to ensure that the Works are constructed and operated in the manner in which they were described and upon which approval was granted. This condition is also included to emphasize the precedence of conditions in the Approval and the practice that the Approval is based on the most current document, if several conflicting documents are submitted for review.
2. Condition 2 is included to ensure that, when the Works are constructed, the Works will meet the standards that apply at the time of construction to ensure the ongoing protection of the environment.
3. Condition 3 is included to ensure that the Ministry records are kept accurate and current with respect to the approved Works and to ensure that subsequent owners of the Works are made aware of the Approval and continue to operate the Works in compliance with it.
4. Condition 4 is included as regular inspection and necessary removal of sediment and excessive decaying vegetation from the Works are required to mitigate the impact of sediment, debris and/or decaying vegetation on the treatment capacity of the Works. The Condition also ensures that adequate storage is maintained in the Works at all times as required by the design. Furthermore, this Condition is included to ensure that the Works are operated and maintained to function as designed.
5. Condition 5 is included as installation, regular inspection and maintenance of the temporary sediment and erosion control measures is required to mitigate the impact on the downstream receiving watercourse during construction until they are no longer required.
6. Condition 6 is included to provide a performance record for future references, to ensure that the Ministry is made aware of problems as they arise, and to provide a compliance record for all the terms and conditions outlined in this Approval, so that the Ministry can work with the Owner in resolving any problems in a timely manner.
7. Condition 7 is included to require that all records are retained for a sufficient time period to adequately evaluate the long-term operation and maintenance of the Works.

In accordance with Section 139 of the *Environmental Protection Act*, you may by written notice served upon me and the Ontario Land Tribunal within 15 days after receipt of this notice, require a hearing by the Tribunal. Section 142 of the *Environmental Protection Act* provides that the notice requiring the hearing ("the Notice") shall state:

- a. The portions of the environmental compliance approval or each term or condition in the environmental compliance approval in respect of which the hearing is required, and;
- b. The grounds on which you intend to rely at the hearing in relation to each portion appealed.

The Notice should also include:

1. The name of the appellant;
2. The address of the appellant;
3. The environmental compliance approval number;
4. The date of the environmental compliance approval;
5. The name of the Director, and;
6. The municipality or municipalities within which the project is to be engaged in.

And the Notice should be signed and dated by the appellant.

This Notice must be served upon:

Registrar*
Ontario Land Tribunal
655 Bay Street, Suite 1500
Toronto, Ontario
M5G 1E5
OLT.Registrar@ontario.ca

and

The Director appointed for the purposes of
Part II.1 of the *Environmental Protection Act*
Ministry of the Environment,
Conservation and Parks
135 St. Clair Avenue West, 1st Floor
Toronto, Ontario
M4V 1P5

* **Further information on the Ontario Land Tribunal's requirements for an appeal can be obtained directly from the Tribunal at: Tel: (416) 212-6349 or 1 (866) 448-2248, or www.olt.gov.on.ca**

The above noted activity is approved under s.20.3 of Part II.1 of the *Environmental Protection Act*.

DATED AT TORONTO this 1st day of September, 2022



Aziz Ahmed, P.Eng.
Director
appointed for the purposes of Part II.1 of the
Environmental Protection Act

RR/

c: District Manager, MECP Ottawa District Office
Clerk, City of Ottawa (File No. D07-16-20-0021)
Jeff Shillington, P.Eng., Senior Project Manager, Development Review, City of Ottawa
Kevin Murphy, David Shaeffer Engineering Ltd.

APPENDIX B
WATER SUPPLY



**Barrhaven Conservancy East
(Phases 2, 3, 4 & Jock River):
Water Distribution System Analysis**

Final Report

June 2, 2022

Prepared for:

David Schaeffer Engineering Ltd.

Prepared by:

Stantec Consulting Ltd.

Revision	Description	Author		Quality Check		Independent Review	
0	Final	TAW	20211213	JS	20211214	KA	20211216
1	Final	TAW/AMG	20220512	AMG	20220516	AP	20220518
2	Final	TAW/AMG	20220602	AMG	20220602	AP	20220602



BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

This document entitled **Barrhaven Conservancy East (Phases 2, 3, 4 & Jock River): Water Distribution System Analysis** was prepared by Stantec Consulting Ltd. ("Stantec") for the account of David Schaeffer Engineering Ltd. (the "Client"). Any reliance on this document by any third party is strictly prohibited. The material in it reflects Stantec's professional judgment in light of the scope, schedule and other limitations stated in the document and in the contract between Stantec and the Client. The opinions in the document are based on conditions and information existing at the time the document was published and do not take into account any subsequent changes. In preparing the document, Stantec did not verify information supplied to it by others. Any use which a third party makes of this document is the responsibility of such third party. Such third party agrees that Stantec shall not be responsible for costs or damages of any kind, if any, suffered by it or any other third party as a result of decisions made or actions taken based on this document.

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Ana Paerez, P.Eng.



BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

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BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

Introduction
June 2, 2022

1.0 INTRODUCTION

To support David Schaeffer Engineering Ltd (DSEL) with their conceptual design submission for the Barrhaven Conservancy East development lands (Phases 2, 3, 4 and Jock River), Stantec Consulting Ltd (Stantec) was requested to provide engineering services to complete a water distribution system analysis for this proposed development located within the City of Ottawa's (City) South Urban Community (SUC). The purpose of the analysis is to confirm associated watermain sizing and redundancy needs.

For this assignment, Stantec's scope of work included the following tasks:

- 1) Reviewing background information and establishing updated water demands for the Conservancy East development area based on the most current draft plan;
- 2) Preparing and submitting a boundary condition request to the City;
- 3) Preparing a stand-alone hydraulic model of the distribution system within the Conservancy East lands using boundary conditions provided by the City. The backbone watermain planning model used for previous planning-level analyses will be used as a base;
- 4) Assessing Fire Underwriters Survey (FUS) fire flow requirements;
- 5) Setting up and running model simulations for average day (AVDY), peak hour (PKHR), and maximum day (MXDY) plus fire flow demands to identify watermain sizing and redundancy needs required for the water distribution system within the development lands to meet design criteria; and,
- 6) Documenting the approach used, findings and recommendations from the analysis.

1.1 STUDY AREA

The study area, referred to as the Barrhaven Conservancy East development lands, is located in the City's southwestern suburban neighbourhood of Barrhaven. The lands are situated between Strandherd Dr to the north, the Jock River to the south, Fraser-Clark Drain to the east, and bisected by Borrisokane Rd through the western portion. Based on the current site plan provided by DSEL (dated October 13, 2021) and additional sub-phasing information (dated March 9, 2022), the proposed development is to be subdivided into four (4) phases, which are further described in **Section 1.2**. The proposed development will comprise a total of 782 single family home (SFH) units and 606 townhouse (MLT) units (consisting of a combination of rear-lane, back-to-back and standard townhouse units) for a total estimated population of 4,295 persons.

Based on a previously completed serviceability study for these lands (Stantec Consulting Ltd., 2021), this residential community, which is currently situated adjacent to Pressure Zone 3SW (previously known as



BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

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Zone BARR), is ultimately planned to be serviced by the future Zone SUC. In 2015, the City embarked on a large initiative to reconfigure the pressure zones servicing Barrhaven and the southern reaches of Ottawa (i.e., SUC). The City has indicated that the pressure zone reconfiguration is planned to be completed by the second quarter (Q2) of 2024. The purpose of the zone reconfiguration was to improve reliability and efficiencies, and to provide increased pumping capacity for future growth. As such, these development lands are to be serviced by two connections to the existing distribution network, both of which are currently part of Zone 3SW and will ultimately be part of Zone SUC. These include the following locations as shown in **Figure 1-1**:

- 1) The existing 305 mm stub extending from Chapman Mills Dr (east of Kennedy-Burnett Pond); and
- 2) The T-junction on the existing 203 mm watermain at Danson Gardens Grv and Darjeeling Ave.

Both connections would require crossing the Kennedy-Burnett Pond and the Fraser-Clarke Drain.

The City has also suggested that a third connection be considered, which is also illustrated in **Figure 1-1**. This potential third connection is located south of the Jock River, at a future 305 mm stub at the intersection of Flagstaff Dr and Borrisokane Rd, and would require crossing the Jock River to service the proposed development lands. The serviceability of the development lands using this third connection is also analyzed herein.

1.2 PHASING OF BARRHAVEN CONSERVANCY EAST

For the purpose of this assessment, development within Barrhaven Conservancy East, as shown in **Figure 1-2**, is assumed to occur in the following phasing order:

- 1) Phase 2 – Comprising 240 SFH units, 98 MLT units and two park areas. The townhouses in this phase are a combination of rear-lane and standard townhouse units. Phase 2 will consist of three (3) subphases:
 - Phase 2A – Comprising 102 SFH units and one park area.
 - Phase 2B – Comprising 129 SFH units.
 - Phase 2C – Comprising 9 SFH units, 98 MLT units and one park area.
- 2) Phase 3 – Comprising 128 SFH units and 197 MLT units. As with Phase 2, these townhouses are a combination of rear-lane and standard townhouse units. Phase 3 will consist of two (2) subphases:
 - Phase 2D – Comprising 42 SFH units and 47 MLT units.
 - Phase 2E – Comprising 86 SFH units and 150 MLT units.



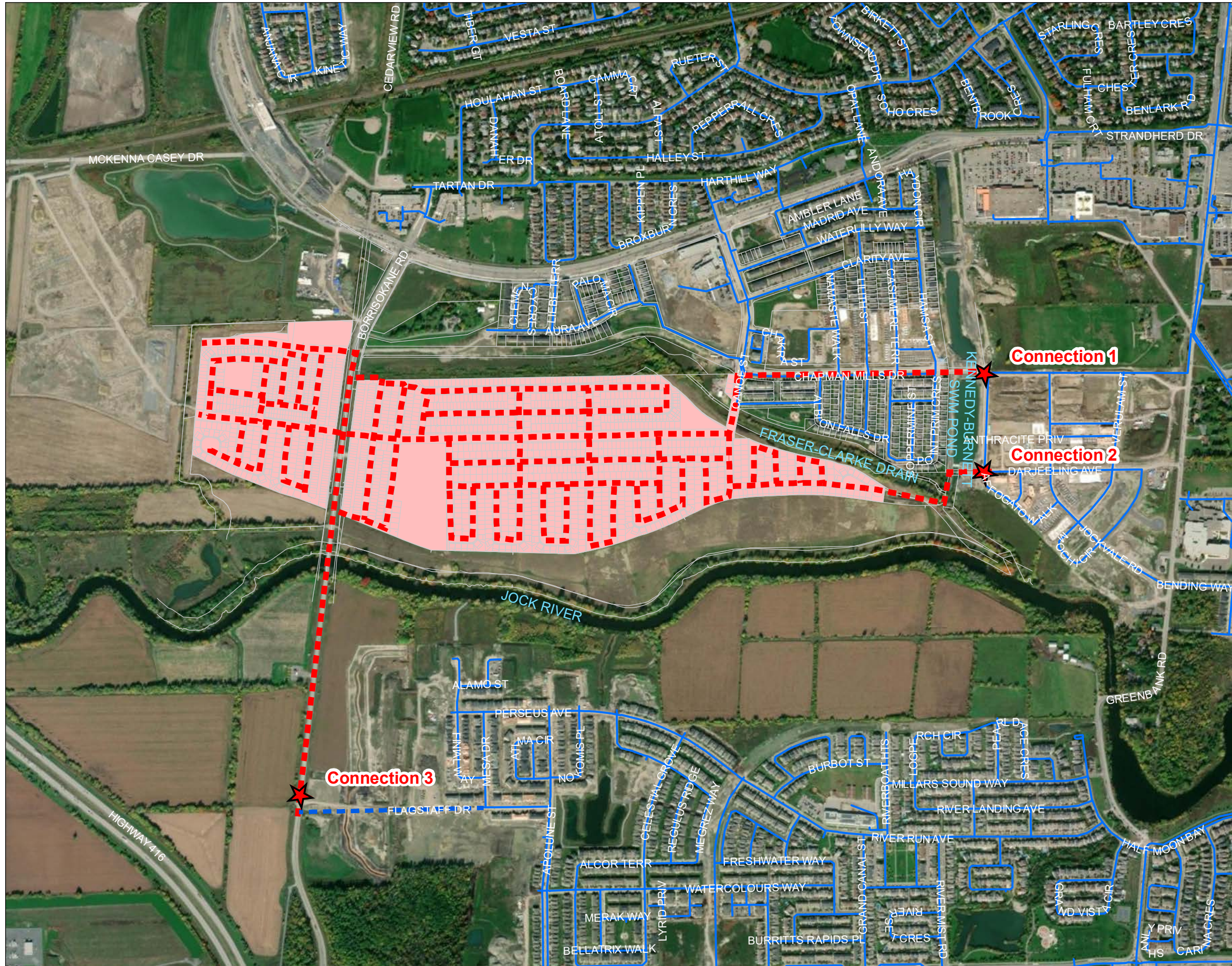
BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

Introduction
June 2, 2022

- 3) Phase 4 - Comprising 86 SFH units, 311 MLT units and one park area. As with Phase 2 and 3, the townhouses in this phase are a combination of rear-lane and standard townhouse units, with additional blocks of back-to-back townhouses; and,
- 4) Jock River – Comprising 328 SFH units.

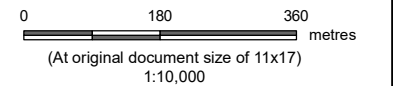
As previously mentioned, the development area will ultimately be serviced by the pressure Zone SUC, once the reconfiguration is complete (planned in Q2 of 2024). As such, the analysis and proposed watermain sizing and layout documented in this report only considers the Zone SUC servicing conditions.



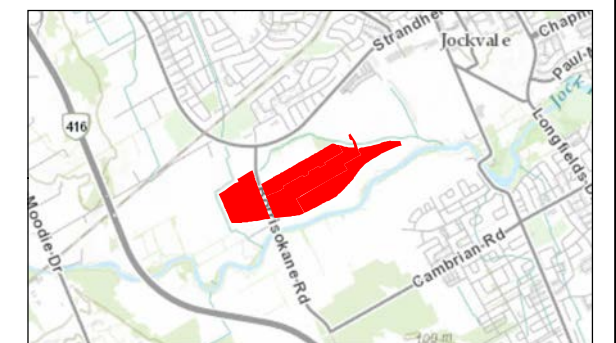


Legend

- Barrhaven Conservancy East Lands
- Property Line
- Existing Distribution Watermain
- Future Distribution Watermain
- Connection Location
- Future Watermain to Service Barrhaven Conservancy East Lands



Notes
 1. Coordinate System: NAD 1983 CSRS MTM 9
 2. Background: Source: Esri, Maxar, GeoEye, Earthstar Geographics, CNES/Airbus DS, USDA, USGS, AeroGRID, IGN, and the GIS User Community
 Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), (c) OpenStreetMap contributors, and the GIS User Community



Project Location
 Ottawa, ON

Client/Project
 David Schaeffer Engineering Ltd
 Barrhaven Conservancy East (Phases 2, 3, 4 & Jock River)
 Water Distribution System Analysis

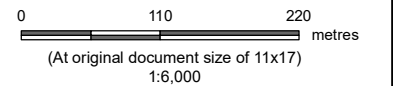
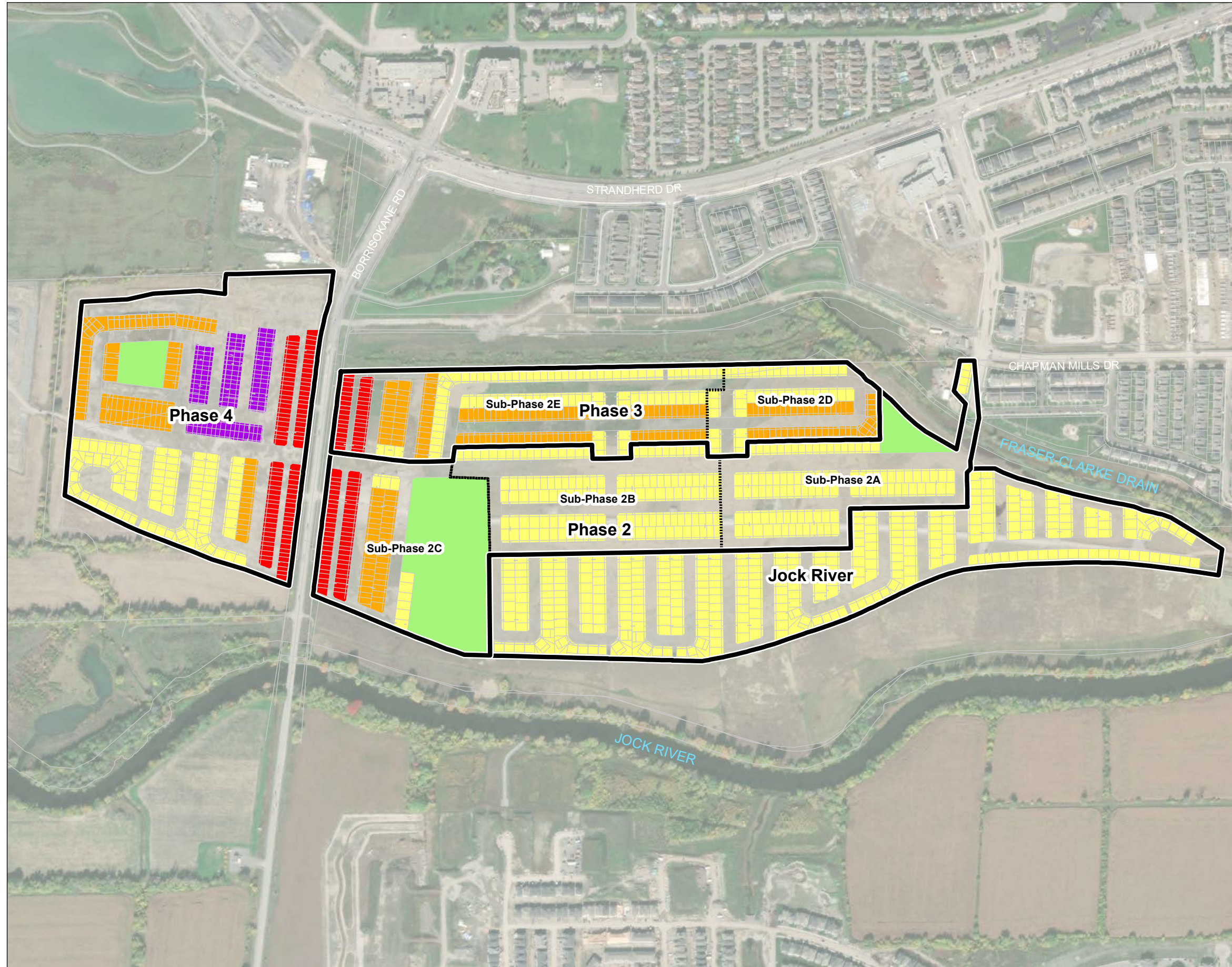
Figure No.

1-1

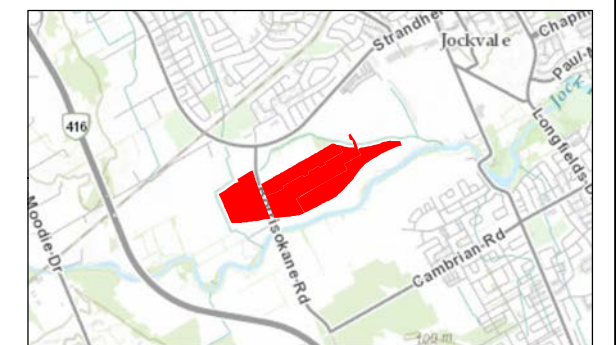
Title
Connections to Existing Water Distribution Network

Legend

- Development Phase Boundary
- Development Sub-Phase Boundary
- Single Family Home (SFH)
- Standard Townhouse (STND TH)
- Rear-Lane Townhouse (RLTH)
- Back-to-Back Townhouse (B2B)
- Park
- Property Line



Notes
 1. Coordinate System: NAD 1983 CSRS MTM 9
 2. Background: Source: Esri, Maxar, GeoEye, Earthstar Geographics, CNES/Airbus DS, USDA, USGS, AeroGRID, IGN, and the GIS User Community
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Project Location
 Ottawa, ON

Client/Project
 David Schaeffer Engineering Ltd
 Barrhaven Conservancy East (Phases 2, 3, 4 & Jock River)
 Water Distribution System Analysis

Figure No.

1-2

Title
Phasing Plan of Barrhaven Conservancy East

BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

Hydraulic Assessment
June 2, 2022

2.0 HYDRAULIC ASSESSMENT

The City of Ottawa Water Design Guidelines (City of Ottawa, 2010) and criteria outlined in the 2013 Water Master Plan (WMP) were used to establish water demands, level of service and pressure objectives during normal and emergency conditions. As per the City's design guidelines and recently issued Technical Bulletin ISTB-2021-03, since this is a new development involving the design of new watermains, the design shall consider a required fire flow established using the calculation method published by the Fire Underwriters Survey (FUS).

2.1 SERVICEABILITY

2.1.1 System Pressures

As per the City's Water Design Guidelines, the desired range of pressure under average day (AVDY), maximum day (MXDY) and peak hour (PKHR) demands is 345 to 552 kPa (50 to 80 psi) and no less than 276 kPa (40 psi) at ground elevation (i.e., at street level). The maximum pressure at any point in the water distribution system should not exceed 552 kPa (80 psi); pressure reducing measures are required to service areas where pressures greater than 552 kPa (80 psi) are anticipated.

Under emergency fire conditions, the system must be able to supply appropriate fire flow while maintaining a residual pressure of 138 kPa (20 psi).

Figure 2-1 shows the elevations of each model junction based on the site's current grading plan. These range from 92.4 m to 93.5 m.

2.1.2 Fire Flows

The City requires a fire flow assessment to be completed to demonstrate that local watermains can provide the objective fire flows. The detailed FUS Guidelines (long method; 1999 Version) was used to calculate the objective fire flows. Based on site plan information provided, the following characteristics were considered in the FUS calculations:

- All townhouse units will be of typical construction (e.g., wood frame, limited combustible building contents); firewalls are to be added where required to meet the study area's target fire flow;
- Single family home units will generally be of typical (wood frame) construction except where a break in fire area is required to meet the study area's target fire flow. At such locations, units will be of ordinary construction as described in the FUS guidelines.
 - With side yard separation distances of < 3.0 m between SFH units, the current site layout would contain several large blocks of contiguous SFH units if all were to be of wood frame construction. It is our understanding that the current rearyard setback for all SFH



BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

Hydraulic Assessment
June 2, 2022

products will be 4.5 m, which in most locations throughout the development area results in rearyard separation distances of less than 10 m. As such, the City's cap of 10,000 L/min, as per Technical Bulletin ISDTB-2018-02, does not apply to these areas and measures such as separating fire areas with units of ordinary construction is required to meet the study area's target fire flow;

- All buildings will have 2 stories above grade (with basements more than 50% below ground level);
- Buildings are not sprinklered; and,
- Setbacks between adjacent units are greater than 3.0 m, with the exception of some proposed SFH units.
 - Per the FUS Guidelines, units with setbacks less than 3.0 m and of wood frame construction will be considered a single fire area.

Based on the latest site plan dated October 2021 and subsequent architectural changes, the required fire flow (RFF) for the governing unit design (rear-lane townhouses, RLTH) was calculated to be 13,000 L/min (217 L/s). This is based on the understanding that, as previously noted, ordinary construction SFH units will be used to separate SFH blocks into fire areas that result in RFFs no greater than 13,000 L/min. Similarly, townhouse blocks will also have firewalls to limit fire areas such that the resulting RFFs will be no greater than 13,000 L/min. The local watermains must therefore be able to provide a minimum fire flow of 13,000 L/min at a residual pressure of 20 psi. The FUS fire flow calculations for the governing unit design and to meet the target fire flow are provided in **Appendix A**.

2.1.3 Water Age

As per the City of Ottawa Design Guidelines, watermains should not be oversized as this may pose water quality degradation, assessed in terms of water age. The Design Guidelines recommend the following:

- A total travel time of 5 days or less during average day demand; and
- A maximum residence time of 8 days.

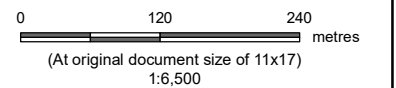
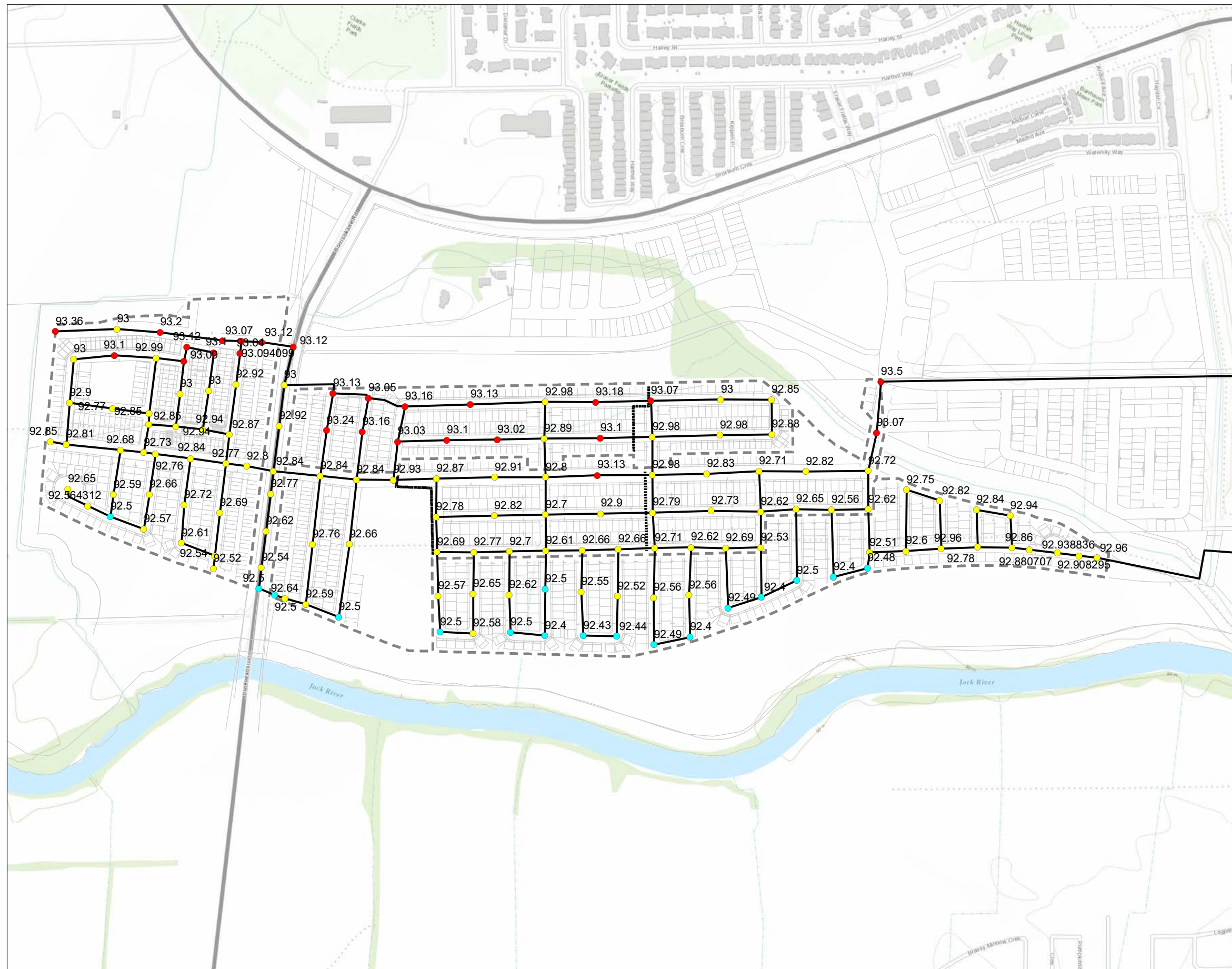


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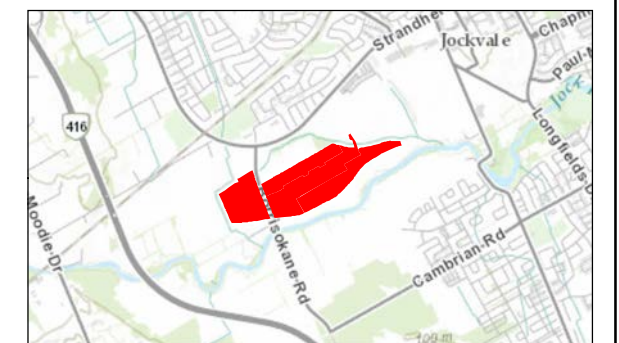
- Development Phase Boundary
- Development Sub-Phase Boundary
- Property Line
- Future Watermain

Ground Elevation (m AD)

- ≤ 92.00
- 92.01 - 92.50
- 92.51 - 93.00
- > 93.00



Notes
 1. Coordinate System: NAD 1983 CSRS MTM 9
 2. Background: Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), (c) OpenStreetMap contributors, and the GIS User Community



Project Location
 Ottawa, ON

Client/Project
 David Schaeffer Engineering Ltd
 Barrhaven Conservancy East (Phases 2, 3, 4 & Jock River)
 Water Distribution System Analysis

Figure No.

2-1

Title

Junction Elevations

BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

Hydraulic Assessment
June 2, 2022

2.2 GROWTH PROJECTIONS

The estimated residential population for Barrhaven Conservancy East was estimated based on projected household sizes as per population densities (or persons per unit, PPU) specified in the City's Water Design Guidelines.

Table 2-1 shows the estimated number of units per phase of these development lands and the projected populations based on the distribution of residential types. The total number of units is estimated to be 1,388 with a residential population of 4,295 persons.

Table 2-1: Estimated Unit Counts and Populations for Barrhaven Conservancy East

Phase	Sub Phase	Unit Types	Units	PPU	Population
2	2A	Singles	102	3.4	347
		Towns	0	2.7	0
	2B	Singles	129	3.4	439
		Towns	0	2.7	0
	2C	Singles	9	3.4	31
		Towns	98	2.7	265
<i>Phase 2 Sub-total</i>			338	-	1,081
3	2D	Singles	42	3.4	143
		Towns	47	2.7	127
	2E	Singles	86	3.4	292
		Towns	150	2.7	405
<i>Phase 3 Sub-total</i>			325	-	967
4		Singles	86	3.4	292
		Towns	311	2.7	840
	<i>Phase 4 Sub-total</i>			397	-
Jock River (JR)		Singles	328	3.4	1,115
		Towns	0	2.7	0
	<i>JR Phase Sub-total</i>			328	-
Total			1,388		4,295



BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

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2.3 DEMAND PROJECTIONS

Due to the size of the service area, the criteria outlined in the City's Water Design Guidelines and recently issued Technical Bulletin ISTB-2021-03 were followed to establish water demands in Barrhaven Conservancy East. As the buildout population of the proposed development is 4,925 (i.e., greater than 3,000), the City's Water Design Guidelines refer to the MECF Guidelines for consumption rates. The MECF Guidelines provide a consumption rate range of 270 L/cap/day to 450 L/cap/day. The City's Water Design Guidelines consumption rates for subdivisions of 501 to 3,000 persons fall within that range and are therefore applicable. The demand rates and peaking factors from the Water Design Guidelines and Technical Bulletin ISTB-2021-03 were applied to the population projections presented in **Table 2-1** based on land-use.

For residential land-use, SFH and MLT units were assigned an average day (AVDY) consumption rate of 280 L/cap/d. To determine maximum day (MXDY) demands, the AVDY demands were multiplied by a residential peaking factor of 2.5. Peak hour (PKHR) demands were established by multiplying MXDY demands by a residential peaking factor of 2.2. The projected AVDY, MXDY and PKHR demands were distributed to the model nodes by phase (and sub-phase) for the corresponding demand scenario.

Estimated AVDY, MXDY and PKHR demand projections are summarized in **Table 2-2**.

Table 2-2: Estimated Demand Projections for Barrhaven Conservancy East

Phase	Sub-Phase	Unit Types	AVDY (L/s)	MXDY (L/s)	PKHR (L/s)
2	2A	Singles	1.12	2.81	6.18
		Towns	0	0	0
	2B	Singles	1.42	3.55	7.82
		Towns	0	0	0
	2C	Singles	0.10	0.25	0.55
		Towns	0.86	2.14	4.72
Phase 2 Sub-total			3.50	8.75	19.26
3	2D	Singles	0.46	1.16	2.55
		Towns	0.41	1.03	2.26
	2E	Singles	0.95	2.37	5.21
		Towns	1.31	3.28	7.22
	Phase 3 Sub-total			3.13	7.84
4	Singles	0.95	2.37	5.21	
	Towns	2.72	6.80	14.97	
	Phase 4 Sub-total			3.67	9.17
Jock River (JR)	Singles	3.61	9.04	19.88	
	Towns	0	0	0	
	JR Phase Sub-total			3.61	9.04
Total			13.92	34.80	76.55



BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

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2.4 MODEL DEVELOPMENT

Innovyze’s InfoWater (Suite 12.4, Update #9) was used to create a stand-alone hydraulic model of the water distribution system within the proposed development area for this analysis. The model was developed to reflect the most current site plan, including proposed watermain layout (based on proposed road alignment) and water demands.

Watermains added to the model were assigned Hazen-Williams coefficients (“C-Factors”) in accordance with the City’s Water Design Guidelines. These factors are listed in **Table 2-3**.

Table 2-3: Hazen-Williams Coefficients by Watermain Size

Watermain Diameter (mm)	Coefficient
152	100
203 - 305	110
350 - 600	120
> 600	130

2.4.1 Boundary Conditions

The proposed subdivision has two connection points to the existing water distribution system; the option to add a third connection point is also assessed (see **Section 1.1**). The boundary conditions provided by the City include hydraulic gradeline (HGL) values for Zone SUC servicing conditions. Values are provided in **Appendix B** and summarized in **Table 2-4**, and have been simulated in the hydraulic model using fixed head reservoirs to which HGLs have been applied for the respective demand scenarios.

Differences in HGL between connections 1 and 2 are observed under higher demand scenarios. While under AVDY and PKHR conditions, these differences are small (0.2 m or less), under MXDY+FF and AVDY+FF conditions, these differences increase to approximately 4 m. This is likely due to the fact that the Connection 1 is connected to a 305 mm diameter along Chapman Mills Dr, whereas Connection 2 is to a 203 mm diameter along Darjeeling Ave, and the two connection points are interconnected by a 203 mm diameter watermain along Danson Gardens Grv.

If the existing watermain along Danson Gardens Grv is upgraded to a 305 mm diameter watermain, the discrepancies in HGL between Connection 1 and Connection 2 decrease. A second set of boundary conditions (two connections with upgrades) reflecting these conditions was provided by the City.

Finally, a third set of boundary conditions was provided by the City, reflecting conditions with three connection points to the existing water distribution system. These boundary conditions do not consider any upgrades between Connection 1 and Connection 2, and as such the HGLs differ by 3.5 to 3.7 m under MXDY+FF and AVDY+FF conditions.



BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

Hydraulic Assessment
June 2, 2022

Table 2-4: HGL Boundary Conditions

HGL (m)			
Zone SUC Servicing Conditions			
Demand Scenario	Two Connections ⁽⁵⁾		
	Connection 1 ⁽¹⁾	Connection 2 ⁽²⁾	
AVDY	150.0	150.0	
PKHR	144.2	144.0	
AVDY +FF	138.7	135.1	
MXDY+FF	137.0	133.2	
Demand Scenario	Two Connections with Upgrades ⁽⁴⁾		
	Connection 1 ⁽¹⁾	Connection 2 ⁽²⁾	
AVDY	149.5	149.5	
PKHR	144.1	144.1	
AVDY +FF	138.6	139.8	
MXDY+FF	136.8	138.1	
Demand Scenario	Three Connections ⁽⁵⁾		
	Connection 1 ⁽¹⁾	Connection 2 ⁽²⁾	Connection 3 ⁽³⁾
AVDY	149.5	149.5	149.5
PKHR	144.5	144.4	142.0
AVDY +FF	138.6	135.1	137.4
MXDY+FF	137.1	133.4	134.8

Notes:

- (1) Ground elevation @ Connection 1 (Chapman Mills Dr) = 92.8 m.
- (2) Ground elevation @ Connection 2 (Danson Gardens Grv / Darjeeling Ave) = 91.8 m.
- (3) Ground elevation @ Connection 3 (Flagstaff Dr) = 92.1 m.
- (4) Upgrades to existing water distribution required to increase HGL at Connection 2; upsize existing 203 mm diameter watermain on Danson Gardens Grv to a 305 mm diameter watermain.
- (5) For scenarios where ultimate conditions will include three connections, the boundary conditions for two connections (without upgrades) were used when only Connections 1 and 2 are in place, i.e., for modelling Phases 2 and 3.



BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

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June 2, 2022

2.4.2 Proposed Watermain Sizing & Layout

Two layouts and sizing of the watermains within the proposed development are presented. The first layout (Option A) is required to service the development if only two connections to the water distribution system (Connection 1 and Connection 2) are made. The second layout (Option B) is required to service the development if a third connection (south of the Jock River) is introduced.

2.4.2.1 Option A: Watermain Sizing & Layout for Two Connections

The layout and sizing of the watermains within the proposed development for a scenario with two ultimate connections to the water distribution system are shown in **Figure 2-2**. The same layout and sizing are required with upgrades to the water distribution system along Danson Gardens Grv.

The network is proposed to consist of 152 mm, 203 mm, 305 mm, and 406 mm diameter watermains, with the 305 mm and 406 mm watermains acting as the hydraulic backbone throughout the development lands. The 406 mm diameter watermains run west from connections 1 and 2, interconnect at the east side of the development lands and continue westward across Borrisokane Rd into the Phase 4 lands. The 406 mm diameter watermains can thus serve as backbone if future developments extend further westward. Additional backbone loops added for reliability will be 305 mm watermains. The remaining local watermains will be 152 mm and 203 mm diameter watermains.

The dead-end watermain in the Phase 4 cul-de-sac is proposed to be 203 mm stepping down to 152 mm. Using the traditional “point load assumption” modelling approach to sizing new watermains, the resulting diameter that would be required to provide a fire flow of 13,000 L/min would be larger than the maximum of 152 mm specified in the City’s design guidelines for dead-end watermains. As such, to optimize sizing of this watermain, the alternative procedure outlined in Appendix I (Guidelines on Coordination of Hydrant Placement with Required Fire Flow) of the City’s Technical Bulletin ISDTB-2018-02 was employed. Additional nodes were added to the model network to represent hydrant locations, to which hydrant flows from Table 1 of Appendix I were applied. To achieve a fire flow of 13,000 L/min, two Class AA hydrants within 75 m (each with an assumed maximum flow capacity of 5,700 L/min) and an additional Class AA hydrant between 75 m and 150 m (with an assumed maximum flow capacity of 3,800 L/min) of the furthest unit along the cul-de-sac would provide a total fire flow of 15,200 L/min (i.e., > the RFF of 13,000 L/min). Other hydrant spacing combinations in accordance with the City’s Technical Bulletin ISDTB-2018-02 can also achieve a total fire flow greater than the RFF of 13,000 L/min.

For reliability, the second backbone feed (305 mm) is redirected north then west (i.e., north of the standard and rear-lane townhouse blocks) across to the Phase 4 lands. This alignment provides reliability of service to the lands west of Borrisokane Rd in the event of a failure at the current intersection of the backbone feeds situated within the Borrisokane Rd ROW. System reliability is further discussed in **Section 3.3**. West of Borrisokane Rd, the 305 mm section of backbone will serve as a service connection to future adjacent development. There are no direct Phase 4 property service connections anticipated



BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

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along this temporary dead-end section of watermain; therefore, it is recommended that this section be isolated until it is required to provide flow to adjacent future lands.

2.4.2.2 Option B: Watermain Sizing & Layout for Three Connections

The layout and sizing of the watermains within the proposed development for a scenario with three ultimate connections to the water distribution system are shown in **Figure 2-3**.

The layout of the watermains is the same as in Option A (with two connections). However, with the third connection, the entire backbone can be reduced to 305 mm diameter watermains at all three connection points and throughout the development lands. The remaining watermain sizes are unchanged from Option A, with local watermains of 152 mm and 203 mm diameter watermains.

Based on the proposed phasing, the implementation of the third connection could be delayed until the development of the Phase 4 lands, west of Borrisokane Rd.

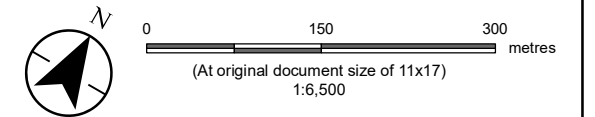


Legend

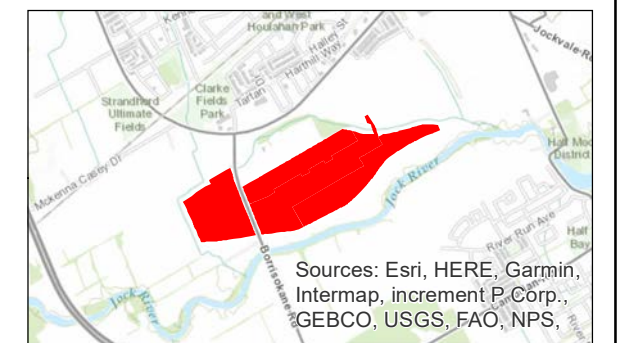
- Development Phase Boundary
- Development Sub-Phase Boundary
- Property Line

Proposed Watermain Diameter (mm)

- 152
- 203
- 305
- 406



Notes
 1. Coordinate System: NAD 1983 CSRS MTM 9NAD 1983 CSRS MTM 9
 2. Background: Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), (c) OpenStreetMap contributors, and the GIS User Community



Project Location
 Ottawa, ON

Client/Project
 David Schaeffer Engineering Ltd
 Barrhaven Conservancy East (Phases 2, 3, 4 & Jock River)
 Water Distribution System Analysis

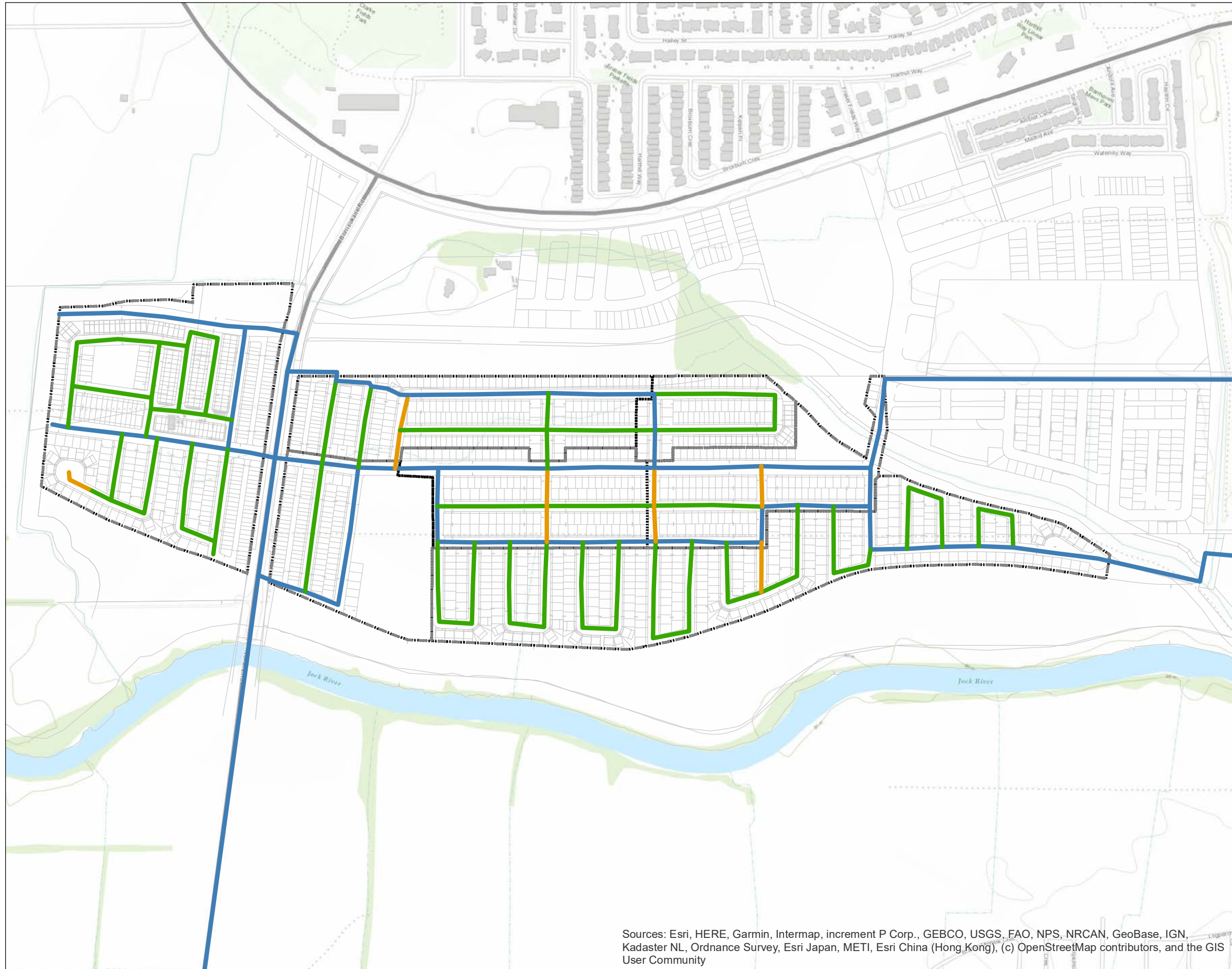
Figure No.

2-2

Title

Proposed Watermain Sizing and Layout - Option A

Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), (c) OpenStreetMap contributors, and the GIS User Community

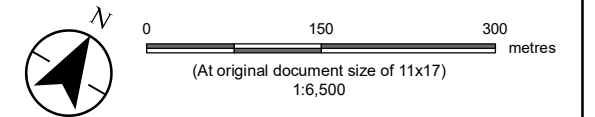


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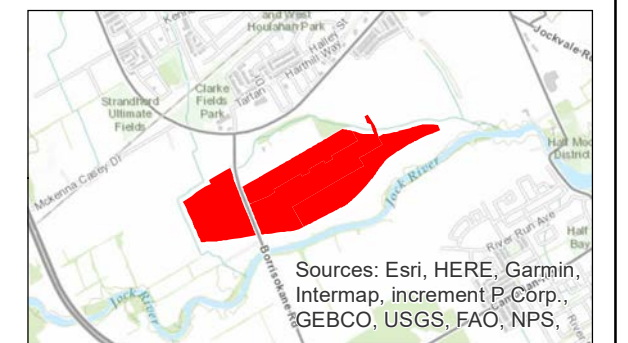
- Development Phase Boundary
- Development Sub-Phase Boundary
- Property Line

Proposed Watermain Diameter (mm)

- 152
- 203
- 305



Notes
 1. Coordinate System: NAD 1983 CSRS MTM 9NAD 1983 CSRS MTM 9
 2. Background: Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), (c) OpenStreetMap contributors, and the GIS User Community



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 Barrhaven Conservancy East (Phases 2, 3, 4 & Jock River)
 Water Distribution System Analysis

Figure No.

2-3

Title

Proposed Watermain Sizing and Layout - Option B

Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), (c) OpenStreetMap contributors, and the GIS User Community

BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

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3.0 HYDRAULIC MODELLING RESULTS

Hydraulic modelling was completed for interim phasing conditions and ultimate buildout conditions of the development lands, under SUC servicing conditions, to verify how the network would respond. The following sub-sections present the modelling results under AVDY, PKHR, and MXDY+FF demands, plus under emergency conditions in the event of a watermain break at key points within the proposed network. Detailed modelling results for all scenarios are provided in **Appendix D**.

3.1 AVERAGE DAY & PEAK HOUR DEMANDS

Under AVDY demands with two connections to the water distribution system, maximum modelled pressures for each interim phase and buildout conditions are 82 psi. With three connections to the water distribution system, maximum modelled pressures for each interim phase and buildout conditions are 81 to 82 psi. These maximum pressures exceed the City's maximum pressure objective of 80 psi. As per the Ontario Building Code (OBC) in areas that may be occupied, the static pressure at any fixture shall not exceed 80 psi. Where pressures do exceed 80 psi, pressure control measures such as pressure reducing valves (PRVs) shall be considered.

Under PKHR demands with two connections to the water distribution system, minimum modelled pressures for each interim phase and buildout conditions are 72 psi. With three connections to the water distribution system, minimum modelled pressures for each interim phase and buildout conditions are also 72 psi. These pressures fall within the desired pressure range of 50 to 80 psi.

3.2 MAXIMUM DAY PLUS FIRE FLOW

MXDY+FF demands were applied for the two connections and the three connections scenarios. Each phase was included sequentially to verify network response as the development phases are constructed and occupied.

With two connections to the water distribution system, available fire flow throughout each interim phase and buildout conditions were above the required 13,000 L/min throughout the network. Likewise, with three connections to the water distribution system, available fire flow throughout each interim phase and buildout conditions were above the required 13,000 L/min throughout the network. To optimize the sizing of the dead-end watermain in the Phase 4 cul-de-sac and to reduce potential water quality issues associated with a large-diameter dead-end watermain, the alternative procedure outlined in Appendix I of ISDTB-2018-02 was employed, as described in **Section 2.4.2**. As such, placing two Class AA hydrants within 75 m of the furthest unit along the cul-de-sac (each with an assumed maximum flow capacity of 5,700 L/min), and two Class AA hydrants between 75 m and 150 m (each with an assumed maximum flow capacity of 3,800 L/min), satisfies the fire flow requirement of 13,000 L/min for units along this cul-de-



BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

Hydraulic Modelling Results
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sac. Other hydrant spacing combinations in accordance with the City's Technical Bulletin ISDTB-2018-02 may be implemented to achieve a total fire flow greater than the RFF of 13,000 L/min.

These results show that the proposed watermain sizing and layout meet serviceability requirements with two connections to the water distribution system without requiring further upstream upgrades along Danson Gardens Grv. Nonetheless, these upgrades would still be beneficial, as they would provide consistent HGLs between the two connection points.

3.3 RELIABILITY

As per the City of Ottawa Design Guidelines, the system must be able to provide average day demand plus fire flow (AVDY+FF) while meeting serviceability requirements during a major failure (i.e., watermain break). To assess reliability and resiliency against major failures, a number of reliability scenarios were completed to confirm sufficient pressure and flow can be achieved during a major failure. These scenarios included the following and are shown in **Figure 3-1** (for Option A, with two connections) and in **Figure 3-2: Reliability Analysis Watermain Break Locations – Option B**

(for Option B, with three connections):

- 1) **Break Scenario 1** – Break in the backbone watermain from Connection 1;
- 2) **Break Scenario 2** – Break in the backbone watermain from Connection 2;
- 3) **Break Scenario 3** – Break in backbone watermain at the northwest edge of the large Phase 2 (Phase 2C) park;
- 4) **Break Scenario 4** – Break along the east-west backbone watermain, immediately west of Borrisokane Rd;
- 5) **Break Scenario 5** – Break in the south backbone watermain through Phase 2 lands, immediately east of Borrisokane Rd;
- 6) **Break Scenario 6** – Break in the north backbone watermain through Phase 2 lands, immediately west of Borrisokane Rd; and,
- 7) **Break Scenario 7** (for Option B only) – Break in the backbone watermain from Connection 3 (crossing the Jock River).

Under break scenario 1, all junctions meet their respective required fire flows, both for Option A (with two connections) and Option B (with three connections).

Under break scenario 2, all junctions meet their respective required fire flows, both for Option A (with two connections) and Option B (with three connections).



BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

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Under break scenario 3, all junctions meet their respective required fire flows, both for Option A (with two connections) and Option B (with three connections). However, under the current phasing plan, a second feed would still be required to service the Phase 2 service area west of the park area (sub-phase 2C; containing more than 50 properties) in the interim until sufficient looping can be provided through the subsequent Phase 3 (sub-phase 2E) if current phasing plans remain unchanged. It is thus recommended that sub-phase 2C be developed after sub-phase 2E, to provide sufficient looping. However, some alternatives could be considered to proceed with sub-phase 2C in accordance with the City's Design Guidelines. First, if the construction of the rear-lane townhouse units (refer to **Figure 1-2**) under sub-phase 2C are delayed until sufficient looping is provided, 55 units will remain as part of sub-phase 2C. As per the City's Design Guidelines, up to 75 units can be serviced on a temporary basis by a dead-end water (or a single feed in this case), given that all pressure and demand objectives are met, and it will be looped by a future phase within 2 years. As such, the 55 units could be serviced from the single feed, given that a second loop is provided in a timely matter (2 years). Alternatively, delaying the construction of 6 other units, in addition to the rear-lane townhouses, to avoid the creation of a vulnerable service area (i.e., less than 50 units under sub-phase 2C until sufficient looping is provided) could be considered.

Under break scenario 4, all junctions meet their respective required fire flows, both for Option A (with two connections) and Option B (with three connections).

Under break scenario 5, all junctions meet their respective required fire flows, both for Option A (with two connections) and Option B (with three connections).

Under break scenario 6, all junctions meet their respective required fire flows, both for Option A (with two connections) and Option B (with three connections).

Under break scenario 7, all junctions meet their respective required fire flows. This break scenario would only occur if Option B (watermain layout with third connection across the Jock River) is selected.

3.4 WATER AGE

Water age is calculated as the total pipe volume divided by the AVDY demand. For sizing Option A (with two connections), water age is highest (1.56 days) when Phase 2 is built. The water age upon buildout is 0.67 days. For sizing Option B (with three connections), water age is highest (1.05 days) when Phase 2 is built. The water age upon buildout is 0.57 days.

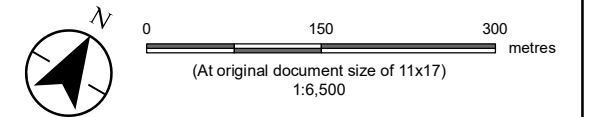
It should be noted that no water age boundary conditions at the connection points were available, therefore the total water age from the source or last point of rechlorination cannot be assessed. Nonetheless, this analysis shows that the residence time of water within the development lands does not exceed the limits per the City's Design Guidelines, and as such water age issues within the development are not anticipated.

Detailed calculations are provided in **Appendix E**.

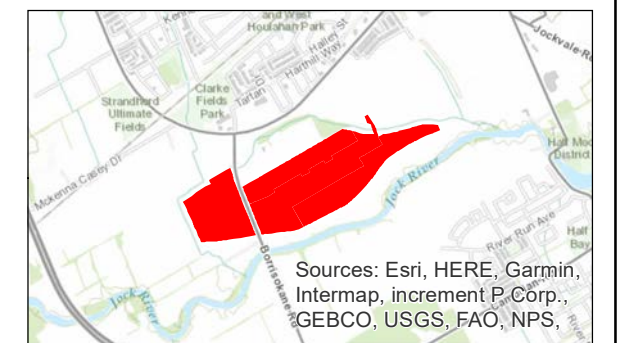


Legend

- Development Phase Boundary
- Development Sub-Phase Boundary
- Property Line
- Proposed Watermain Diameter (mm)**
- 152
- 203
- 305
- 406
- Watermain Break Locations



Notes
 1. Coordinate System: NAD 1983 CSRS MTM 9NAD 1983 CSRS MTM 9
 2. Background: Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), (c) OpenStreetMap contributors, and the GIS User Community



Project Location
 Ottawa, ON

Client/Project
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 Barrhaven Conservancy East (Phases 2, 3, 4 & Jock River)
 Water Distribution System Analysis

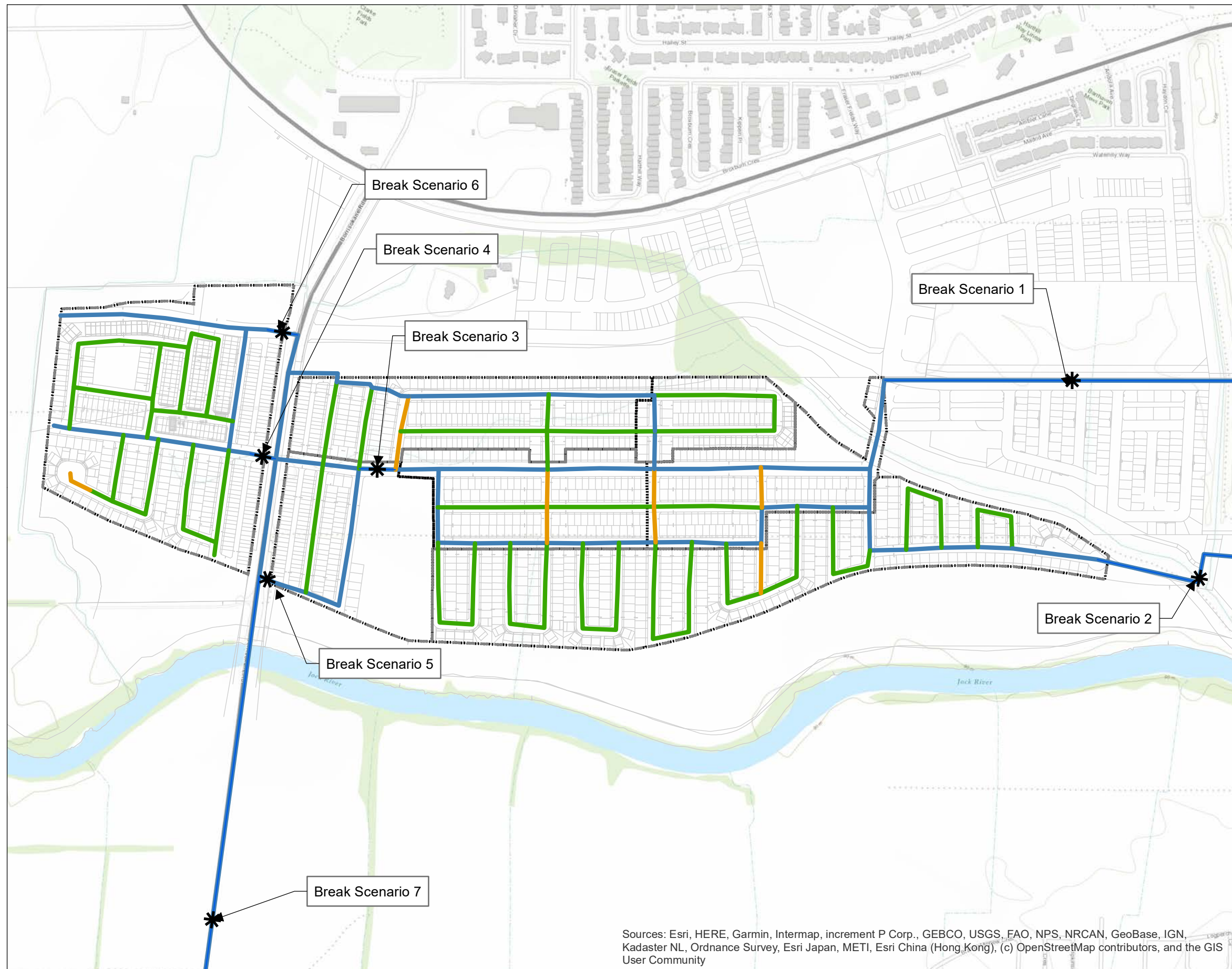
Figure No.

3-1

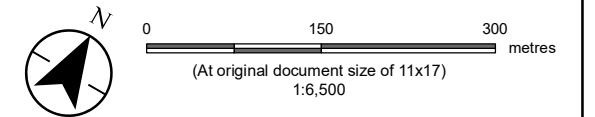
Title

Reliability Analysis Watermain Break Locations - Option A

Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), (c) OpenStreetMap contributors, and the GIS User Community

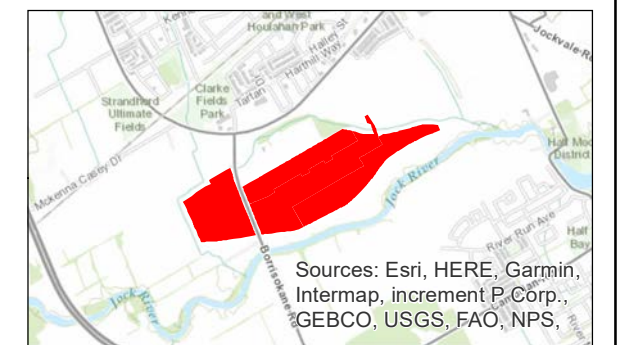


- Legend**
- Development Phase Boundary
 - Development Sub-Phase Boundary
 - Property Line
- Proposed Watermain Diameter (mm)**
- 152
 - 203
 - 305
- Watermain Break Locations



Notes

1. Coordinate System: NAD 1983 CSRS MTM 9NAD 1983 CSRS MTM 9
2. Background: Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), (c) OpenStreetMap contributors, and the GIS User Community



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Water Distribution System Analysis

Figure No.

3-2

Title

Reliability Analysis Watermain Break Locations - Option B

Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), (c) OpenStreetMap contributors, and the GIS User Community

BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

Conclusion and Recommendations
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4.0 CONCLUSION AND RECOMMENDATIONS

A water distribution system hydraulic analysis was completed for the Barrhaven Conservancy East development lands. The purpose of this analysis was to confirm associated watermain sizing and redundancy needs. Based on the hydraulic analysis, the following conclusions and recommendations were made:

- Based on the most current site plan layout, the estimated AVDY, MXDY and PKHR demand projections for the development lands are 13.92 L/s, 34.80 L/s, and 76.55 L/s, respectively.
- The required fire flow for the governing unit design (rear-lane townhouses) was calculated to be 13,000 L/min (217 L/s). This is based on the understanding that ordinary construction single-family housing (SFH) units will be used to separate SFH blocks into fire areas that result in required fire flows (RFFs) no greater than 13,000 L/min. Similarly, townhouse blocks will have firewalls to limit fire areas such that the resulting RFFs will be no greater than 13,000 L/min.
 - As the watermain sizing presented herein is based on an RFF of 13,000 L/min, the final design of the units should meet the requirements for this RFF, per the FUS Guidelines.
- Two watermain layout and sizing are proposed:
 - The first option (Option A) would involve two connections to the water distribution system; the proposed sizing is recommended to include 406 mm diameter watermains from connections 1 and 2 as the hydraulic backbone of the network, with 305 mm diameter watermains for backbone looping. Watermains along local right-of-ways would be 152 mm and 203 mm diameter watermains. The dead-end watermain in the cul-de-sac at the western extent of the development would be 152 mm diameter. The proposed layout and sizing is shown in **Figure 2-2**.
 - The second option (Option B) would involve three connections to the water distribution system, with the third connection requiring crossing the Jock River. The proposed layout within the development is similar to Option A; the proposed sizing is recommended to include 305 mm diameter watermains for the hydraulic backbone of the network. Watermains along local right-of-ways would be 152 mm and 203 mm diameter watermains. The dead-end watermain in the cul-de-sac at the western extent of the development would be 152 mm diameter. The proposed layout and sizing is shown in **Figure 2-3**.
- The serviceability of the development lands was analysed, considering that they would be serviced by the pressure zone SUC.
- As part of the currently proposed watermain layout, the backbone watermain is proposed to extend west along the northern edge of the Phase 4 lands to serve as a service connection to future adjacent development. There are no direct Phase 4 property service connections



BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

Conclusion and Recommendations
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anticipated along this temporary dead-end section of watermain; therefore, it is recommended that this section be isolated until it is required to provide flow to adjacent future lands.

- Under AVDY demand conditions, model results using boundary conditions provided by the City exceed the allowable maximum pressure of 80 psi in accordance with the City of Ottawa Design Guidelines. As per the OBC, the static pressure at any fixture shall not exceed 80 psi, in areas that may be occupied. Where pressures do exceed 80 psi, pressure control measures such as PRVs installed immediately downstream of the isolation valve to the home/building shall be considered.
- Under PKHR demand conditions, the minimum pressures are in accordance with the City's system pressure requirements.
- Under MXDY+FF demand conditions, the target required fire flow of 13,000 L/min can be achieved through the proposed network for all phases when the alternative procedure outlined in the Appendix I of ISDTB-2018-02 is applied to the dead-end watermain in the western extent of the development lands.
- If Option A (servicing with two connections) is selected, watermain upgrades along Danson Gardens Grv are recommended to provide similar HGLs at the two connection points under a fire flow scenario.
- To satisfy and improve system reliability in the event of an emergency break scenario at key points in the network, a second backbone feed was redirected north then west (i.e., north of the standard and rear-lane townhouse blocks) across to the Phase 4 lands. However, under the current phasing plan, a second feed would still be required to service the Phase 2 service area west of the park area (sub-phase 2C, containing more than 50 properties) in the interim until sufficient looping can be provided through the subsequent Phase 3 (sub-phase 2E) if current phasing plans remain unchanged. It is recommended that sub-phase 2C be developed after sub-phase 2E, to provide sufficient looping. However, sub-phase 2C could be serviced on an interim basis, from the single feed, given that the rear-lane townhouses proposed under sub-phase 2C are delayed until sufficient looping is provided. Alternatively, delaying the construction of 6 other units, in addition to the rear-lane townhouses, could be considered for sub-phase 2C, to avoid the creation of a vulnerable service area.
- A water age analysis shows that the residence time of water within the development lands does not exceed the limits per the City's Design Guidelines. No water age boundary conditions at the connection points were available, therefore the total water age from the source or last point of rechlorination cannot be assessed. As such, water age issues within the development are not anticipated.



BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

References
June 2, 2022

5.0 REFERENCES

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BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

June 2, 2022

Appendix A FUS CALCULATION





FUS Fire Flow Calculation

Calculations based on: "Water Supply for Public Fire Protection" by Fire Underwriters' Survey, 1999

Stantec Project #: 163401660
 Project Name: Barrhaven Conservancy
 Date: November 29, 2021
 Data inputted by: Jasmin Sidhu, P.Eng.
 Data reviewed by:

Fire Flow Calculation #: 1
 Building Type/Description/Name: Residential

*Single family house (SFH) block based on draft site plan dated September 20, 2021. Area assumes largest SFH unit size.
 Minimum spatial separation between the backs of adjacent units is <10m (i.e., City's cap of 10,000 L/min as per Technical Bulletin ISDTB-2018-02 does not apply).
 Notes: Assumed wood frame construction.
 Target fire flow = 13,000 L/min. Requires a maximum of 2 adjacent consecutive wood frame construction units.*

Table A: Fire Underwriters Survey Determination of Required Fire Flow - Long Method

Step	Task	Term	Options	Multiplier Associated with Option	Choose:	Value Used	Unit	Total Fire Flow (L/min)	
1	Choose Frame Used for Construction of Unit	Coefficient related to type of construction (C)	Framing Material						
			Wood Frame	1.5	Wood Frame	1.5	m		
			Ordinary construction	1					
			Non-combustible construction	0.8					
			Fire resistive construction (< 2 hrs)	0.7					
Fire resistive construction (> 2 hrs)	0.6								
2	Choose Type of Housing (if TH, Enter Number of Units Per TH Block)	Type of Housing	Floor Space Area						
			Single Family	2	Single Family	2	Units		
			Townhouse - indicate # of units	1					
			Other (Comm, Ind, Apt etc.)	1					
2.2	# of Storeys	Number of Floors/Storeys in the Unit (do not include basement if 50% below grade):						2	2
3	Enter Average Floor Area of Unit or Block of Units	Average Floor Area (A) (non-fire resistive construction):			158	158	Area in Square Meters (m ²)		
					Square Metres (m2)				
3.1	Obtain Total Effective Building Area	Total Effective Building Area (# of Storeys x Average Floor Area of Unit x # of Units):			632	632			
4	Obtain Required Fire Flow without Reductions	Required Fire Flow (without reductions or increases per FUS) (F = 220 * C * √A) Round to nearest 1,000 L/min						8,000	
5	Apply Factors Affecting Burning	Reductions/Increases Due to Factors Affecting Burning							
5.1	Choose Combustibility of Building Contents	Occupancy content hazard reduction or surcharge	Non-combustible	-0.25	Limited combustible	-0.15	N/A	6,800	
			Limited combustible	-0.15					
			Combustible	0					
			Free burning	0.15					
			Rapid burning	0.25					
5.2	Choose Reduction Due to Presence of Sprinklers	Sprinkler reduction	Adequate Sprinkler conforms to NFPA13	-0.3	None	0	N/A	0	
			None	0					
		Water Supply Credit	Water supply is standard for sprinkler and fire dept. hose line	-0.1	Water supply is not standard or N/A	0	N/A	0	
			Water supply is not standard or N/A	0					
		Sprinkler Supervision Credit	Sprinkler system is fully supervised	-0.1	Sprinkler not fully supervised or N/A	0	N/A	0	
			Sprinkler not fully supervised or N/A	0					
5.3	Choose Separation Distance Between Units	Exposure Distance Between Units	Front Yard	20.1 to 30.1m	0.1	0.75	m	5,100	
			Side Yard (Left)	0 to 3.0m	0.25				
			Rear Yard	3.1 to 10.0m	0.2				
			Side Yard (Right)	0 to 3.0m	0.25				
			Total Required Fire Flow, rounded to nearest 1,000 L/min, with max/min limits applied:						
6	Obtain Required Fire Flow, Duration & Volume	Total Required Fire Flow (above) in L/s:						200	
		Required Duration of Fire Flow (hrs)						2.50	
		Required Volume of Fire Flow (m³)						1,800	



FUS Fire Flow Calculation

Calculations based on: "Water Supply for Public Fire Protection" by Fire Underwriters' Survey, 1999

Stantec Project #: 163401660
 Project Name: Barrhaven Conservancy
 Date: November 29, 2021
 Data inputted by: Jasmin Sidhu, P.Eng.
 Data reviewed by:

Fire Flow Calculation #: 2
 Building Type/Description/Name: Residential

*Single family house (SFH) block based on draft site plan dated September 20, 2021. Area assumes largest SFH unit size.
 Notes: Minimum spatial separation between the backs of adjacent units is <10m (i.e., City's cap of 10,000 L/min as per Technical Bulletin ISDTB-2018-02 does not apply).
 Assumed ordinary construction (i.e., more than 2/3 of the buildings' exterior walls are made of brick or masonry veneer).
 Target fire flow = 13,000 L/min. Requires a maximum of 5 adjacent consecutive ordinary construction units.*

Table A: Fire Underwriters Survey Determination of Required Fire Flow - Long Method

Step	Task	Term	Options	Multiplier Associated with Option	Choose:	Value Used	Unit	Total Fire Flow (L/min)	
1	Choose Frame Used for Construction of Unit	Coefficient related to type of construction (C)	Framing Material						
			Wood Frame	1.5	Ordinary construction	1	m		
			Ordinary construction	1					
			Non-combustible construction	0.8					
			Fire resistive construction (< 2 hrs)	0.7					
Fire resistive construction (> 2 hrs)	0.6								
2	Choose Type of Housing (if TH, Enter Number of Units Per TH Block)	Type of Housing	Floor Space Area						
			Single Family	5	Single Family	5	Units		
			Townhouse - indicate # of units	1					
			Other (Comm, Ind, Apt etc.)	1					
2.2	# of Storeys	Number of Floors/Storeys in the Unit (do not include basement if 50% below grade):			2	2	Storeys		
3	Enter Average Floor Area of Unit or Block of Units	Average Floor Area (A) (non-fire resistive construction):			158	158	Area in Square Meters (m ²)		
					Square Metres (m2)				
3.1	Obtain Total Effective Building Area	Total Effective Building Area (# of Storeys x Average Floor Area of Unit x # of Units):			1,580	1,580			
4	Obtain Required Fire Flow without Reductions	Required Fire Flow (without reductions or increases per FUS) (F = 220 * C * √A) Round to nearest 1,000 L/min						9,000	
5	Apply Factors Affecting Burning	Reductions/Increases Due to Factors Affecting Burning							
5.1	Choose Combustibility of Building Contents	Occupancy content hazard reduction or surcharge	Non-combustible	-0.25	Limited combustible	-0.15	N/A	7,650	
			Limited combustible	-0.15					
			Combustible	0					
			Free burning	0.15					
			Rapid burning	0.25					
5.2	Choose Reduction Due to Presence of Sprinklers	Sprinkler reduction	Adequate Sprinkler conforms to NFPA13	-0.3	None	0	N/A	0	
			None	0					
		Water Supply Credit	Water supply is standard for sprinkler and fire dept. hose line	-0.1	Water supply is not standard or N/A	0	N/A	0	
			Water supply is not standard or N/A	0					
		Sprinkler Supervision Credit	Sprinkler system is fully supervised	-0.1	Sprinkler not fully supervised or N/A	0	N/A	0	
			Sprinkler not fully supervised or N/A	0					
5.3	Choose Separation Distance Between Units	Exposure Distance Between Units	Front Yard	20.1 to 30.1m	0.1	0.75	m	5,738	
			Side Yard (Left)	0 to 3.0m	0.25				
			Rear Yard	3.1 to 10.0m	0.2				
			Side Yard (Right)	0 to 3.0m	0.25				
6	Obtain Required Fire Flow, Duration & Volume	Total Required Fire Flow, rounded to nearest 1,000 L/min, with max/min limits applied:						13,000	
		Total Required Fire Flow (above) in L/s:						217	
		Required Duration of Fire Flow (hrs)						2.75	
		Required Volume of Fire Flow (m³)						2,145	



FUS Fire Flow Calculation

Calculations based on: "Water Supply for Public Fire Protection" by Fire Underwriters' Survey, 1999

Stantec Project #: 163401660
 Project Name: Barrhaven Conservancy
 Date: May 10, 2022
 Data inputted by: Christène Razafimaharo
 Data reviewed by: Jasmin Sidhu, P.Eng.

Fire Flow Calculation #: 3
 Building Type/Description/Name: Residential

Notes: Maximum GFA for a STND TH fire area to achieve a required fire flow (RFF) of 13,000 L/min.
 Target fire flow = 13,000 L/min. Fire walls required at the back to achieve RFF.

Table A: Fire Underwriters Survey Determination of Required Fire Flow - Long Method									
Step	Task	Term	Options	Multiplier Associated with Option	Choose:	Value Used	Unit	Total Fire Flow (L/min)	
1	Choose Frame Used for Construction of Unit	Framing Material							
		Coefficient related to type of construction (C)	Wood Frame	1.5	Wood Frame	1.5	m		
			Ordinary construction	1					
			Non-combustible construction	0.8					
			Fire resistive construction (< 2 hrs)	0.7					
Fire resistive construction (> 2 hrs)	0.6								
2	Choose Type of Housing (if TH, Enter Number of Units Per TH Block)	Floor Space Area							
		Type of Housing	Single Family	1	Townhouse - indicate # of units	5	Units		
			Townhouse - indicate # of units	5					
Other (Comm, Ind, Apt etc.)	1								
2.2	# of Storeys	Number of Floors/Storeys in the Unit (do not include basement if 50% below grade):			2	2	Storeys		
3	Enter Average Floor Area of Unit or Block of Units	Average Floor Area (A) (non-fire resistive construction):			82	82	Area in Square Meters (m ²)		
		Square Metres (m2)							
3.1	Obtain Total Effective Building Area	Total Effective Building Area (# of Storeys x Average Floor Area of Unit x # of Units):			820	820			
4	Obtain Required Fire Flow without Reductions	Required Fire Flow (without reductions or increases per FUS) ($F = 220 * C * \sqrt{A}$) Round to nearest 1,000 L/min						9,000	
5	Apply Factors Affecting Burning	Reductions/Increases Due to Factors Affecting Burning							
5.1	Choose Combustibility of Building Contents	Occupancy content hazard reduction or surcharge	Non-combustible	-0.25	Limited combustible	-0.15	N/A	7,650	
			Limited combustible	-0.15					
			Combustible	0					
			Free burning	0.15					
			Rapid burning	0.25					
5.2	Choose Reduction Due to Presence of Sprinklers	Sprinkler reduction	Adequate Sprinkler conforms to NFPA13	-0.3	None	0	N/A	0	
			None	0					
		Water Supply Credit	Water supply is standard for sprinkler and fire dept. hose line	-0.1	Water supply is not standard or N/A	0	N/A	0	
			Water supply is not standard or N/A	0					
		Sprinkler Supervision Credit	Sprinkler system is fully supervised	-0.1	Sprinkler not fully supervised or N/A	0	N/A	0	
			Sprinkler not fully supervised or N/A	0					
5.3	Choose Separation Distance Between Units	Exposure Distance Between Units	Front Yard	20.1 to 30.1m	0.1	0.6	m	4,590	
			Side Yard (Left)	3.1 to 10.0m	0.2				
			Rear Yard	Fire Wall	0.1				
			Side Yard (Right)	3.1 to 10.0m	0.2				
6	Obtain Required Fire Flow, Duration & Volume	Total Required Fire Flow, rounded to nearest 1,000 L/min, with max/min limits applied:						12,000	
		Total Required Fire Flow (above) in L/s:						200	
		Required Duration of Fire Flow (hrs)						2.50	
		Required Volume of Fire Flow (m ³)						1,800	



FUS Fire Flow Calculation

Calculations based on: "Water Supply for Public Fire Protection" by Fire Underwriters' Survey, 1999

Stantec Project #: 163401660
 Project Name: Barrhaven Conservancy
 Date: September 29, 2021
 Data inputted by: Tom Westwood, P.Eng
 Data reviewed by: Jasmin Sidhu, P.Eng.

Fire Flow Calculation #: 4
 Building Type/Description/Name: Residential

Notes: Governing rear lane townhouse (RLTH) block based on draft site plan dated September 20, 2021. Block consists of 5 RLTH units where minimum spatial separation between the backs of adjacent units is <10m and gross floor area of block is > 600m² (i.e., City's cap of 10,000 L/min as per Technical Bulletin ISDTB-2018-02 does not apply).

Table A: Fire Underwriters Survey Determination of Required Fire Flow - Long Method									
Step	Task	Term	Options	Multiplier Associated with Option	Choose:	Value Used	Unit	Total Fire Flow (L/min)	
1	Choose Frame Used for Construction of Unit	Coefficient related to type of construction (C)	Framing Material						
			Wood Frame	1.5	Wood Frame	1.5	m		
			Ordinary construction	1					
			Non-combustible construction	0.8					
			Fire resistive construction (< 2 hrs)	0.7					
Fire resistive construction (> 2 hrs)	0.6								
2	Choose Type of Housing (if TH, Enter Number of Units Per TH Block)	Type of Housing	Floor Space Area						
			Single Family	1	Townhouse - indicate # of units	5	Units		
			Townhouse - indicate # of units	5					
Other (Comm, Ind, Apt etc.)	1								
2.2	# of Storeys	Number of Floors/Storeys in the Unit (do not include basement if 50% below grade):			2	2	Storeys		
3	Enter Average Floor Area of Unit or Block of Units	Average Floor Area (A) (non-fire resistive construction):			78	78	Area in Square Meters (m ²)		
		Square Metres (m2)							
3.1	Obtain Total Effective Building Area	Total Effective Building Area (# of Storeys x Average Floor Area of Unit x # of Units):			780	780			
4	Obtain Required Fire Flow without Reductions	Required Fire Flow (without reductions or increases per FUS) (F = 220 * C * √A) Round to nearest 1,000 L/min						9,000	
5	Apply Factors Affecting Burning	Reductions/Increases Due to Factors Affecting Burning							
5.1	Choose Combustibility of Building Contents	Occupancy content hazard reduction or surcharge	Non-combustible	-0.25	Limited combustible	-0.15	N/A	7,650	
			Limited combustible	-0.15					
			Combustible	0					
			Free burning	0.15					
			Rapid burning	0.25					
5.2	Choose Reduction Due to Presence of Sprinklers	Sprinkler reduction	Adequate Sprinkler conforms to NFPA13	-0.3	None	0	N/A	0	
			None	0					
		Water Supply Credit	Water supply is standard for sprinkler and fire dept. hose line	-0.1	Water supply is not standard or N/A	0	N/A	0	
			Water supply is not standard or N/A	0					
		Sprinkler Supervision Credit	Sprinkler system is fully supervised	-0.1	Sprinkler not fully supervised or N/A	0	N/A	0	
			Sprinkler not fully supervised or N/A	0					
5.3	Choose Separation Distance Between Units	Exposure Distance Between Units	Front Yard	20.1 to 30.1m	0.1	0.7	m	5,355	
			Side Yard (Left)	3.1 to 10.0m	0.2				
			Rear Yard	3.1 to 10.0m	0.2				
			Side Yard (Right)	3.1 to 10.0m	0.2				
6	Obtain Required Fire Flow, Duration & Volume	Total Required Fire Flow, rounded to nearest 1,000 L/min, with max/min limits applied:						13,000	
		Total Required Fire Flow (above) in L/s:						217	
		Required Duration of Fire Flow (hrs)						2.75	
		Required Volume of Fire Flow (m³)						2,145	



FUS Fire Flow Calculation

Calculations based on: "Water Supply for Public Fire Protection" by Fire Underwriters' Survey, 1999

Stantec Project #: 163401660
 Project Name: Barrhaven Conservancy
 Date: September 29, 2021
 Data inputted by: Tom Westwood, P.Eng
 Data reviewed by: Jasmin Sidhu, P.Eng.

Fire Flow Calculation #: 5
 Building Type/Description/Name: Residential

Notes: Governing back-to-back townhouse (B2B TH) block based on draft site plan dated September 20, 2021. Block consists of 10 B2B TH units separated by one fire wall, resulting in a fire area comprising 5 units with no spatial separation between the backs of adjacent units and gross floor area of block is > 600m² (i.e., City's cap of 10,000 L/min as per Technical Bulletin ISDTB-2018-02 does not apply).
 Target Fire Flow = 13,000 L/min. Fire walls required at the back to achieve target fire flow.

Table A: Fire Underwriters Survey Determination of Required Fire Flow - Long Method								
Step	Task	Term	Options	Multiplier Associated with Option	Choose:	Value Used	Unit	Total Fire Flow (L/min)
1	Choose Frame Used for Construction of Unit	Coefficient related to type of construction (C)	Wood Frame	1.5	Wood Frame	1.5	m	
			Ordinary construction	1				
			Non-combustible construction	0.8				
			Fire resistive construction (< 2 hrs)	0.7				
			Fire resistive construction (> 2 hrs)	0.6				
2	Choose Type of Housing (if TH, Enter Number of Units Per TH Block)	Type of Housing	Single Family	1	Townhouse - indicate # of units	5	Units	
			Townhouse - indicate # of units	5				
			Other (Comm, Ind, Apt etc.)	1				
			2.2	# of Storeys				
3	Enter Average Floor Area of Unit or Block of Units	Average Floor Area (A) (non-fire resistive construction):		78	78	78	Area in Square Meters (m ²)	
				Square Metres (m2)				
3.1	Obtain Total Effective Building Area	Total Effective Building Area (# of Storeys x Average Floor Area of Unit x # of Units):		780	780			
4	Obtain Required Fire Flow without Reductions	Required Fire Flow (without reductions or increases per FUS) (F = 220 * C * √A) Round to nearest 1,000 L/min						9,000
5	Apply Factors Affecting Burning	Reductions/Increases Due to Factors Affecting Burning						
5.1	Choose Combustibility of Building Contents	Occupancy content hazard reduction or surcharge	Non-combustible	-0.25	Limited combustible	-0.15	N/A	7,650
			Limited combustible	-0.15				
			Combustible	0				
			Free burning	0.15				
			Rapid burning	0.25				
5.2	Choose Reduction Due to Presence of Sprinklers	Sprinkler reduction	Adequate Sprinkler conforms to NFPA13	-0.3	None	0	N/A	0
			None	0				
		Water Supply Credit	Water supply is standard for sprinkler and fire dept. hose line	-0.1	Water supply is not standard or N/A	0	N/A	0
			Water supply is not standard or N/A	0				
		Sprinkler Supervision Credit	Sprinkler system is fully supervised	-0.1	Sprinkler not fully supervised or N/A	0	N/A	0
			Sprinkler not fully supervised or N/A	0				
5.3	Choose Separation Distance Between Units	Exposure Distance Between Units	Front Yard	3.1 to 10.0m	0.2	0.6	m	4,590
			Side Yard (Left)	20.1 to 30.1m	0.1			
			Rear Yard	3.1 to 10.0m	0.2			
			Side Yard (Right)	20.1 to 30.1m	0.1			
			Total Required Fire Flow, rounded to nearest 1,000 L/min, with max/min limits applied:					
6	Obtain Required Fire Flow, Duration & Volume	Total Required Fire Flow (above) in L/s:						200
		Required Duration of Fire Flow (hrs)						2.50
		Required Volume of Fire Flow (m ³)						1,800

**BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION
SYSTEM ANALYSIS**

June 2, 2022

Appendix B BOUNDARY CONDITIONS

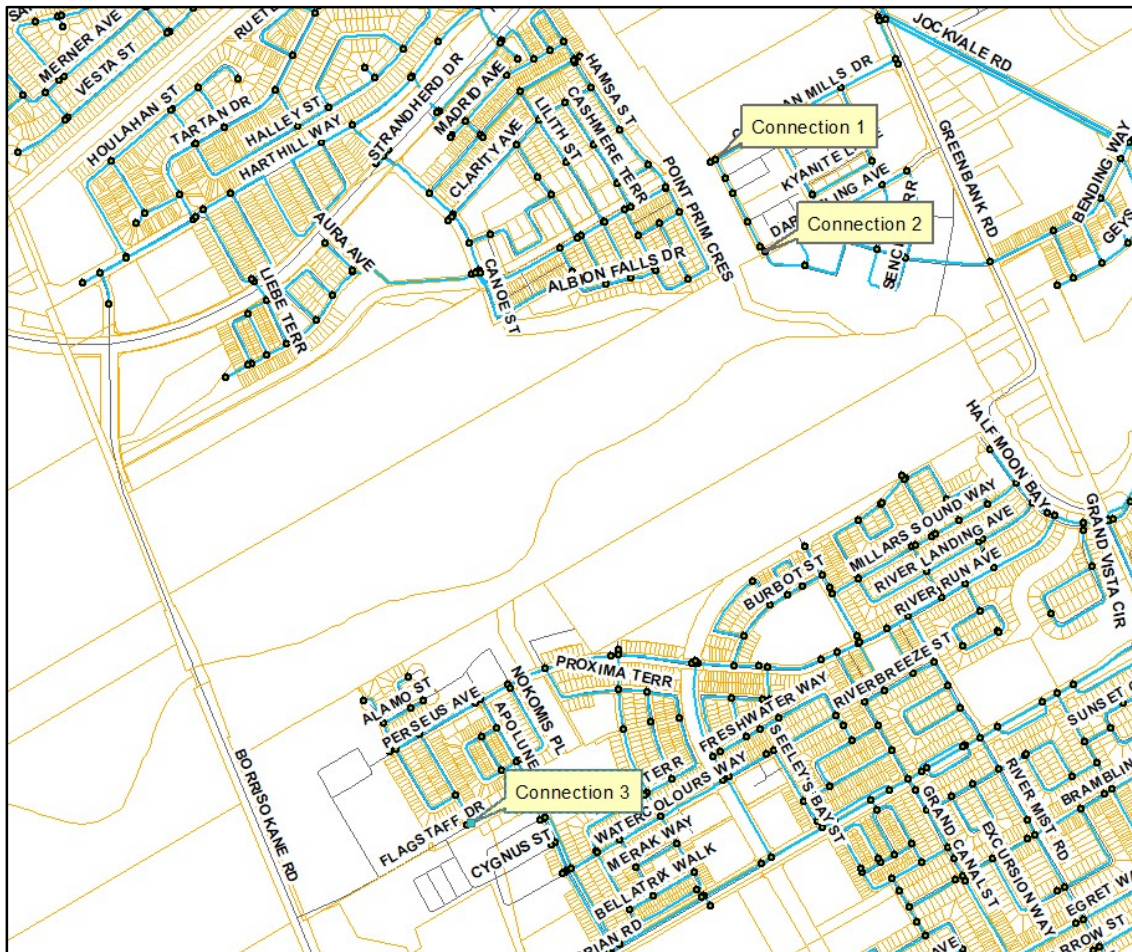


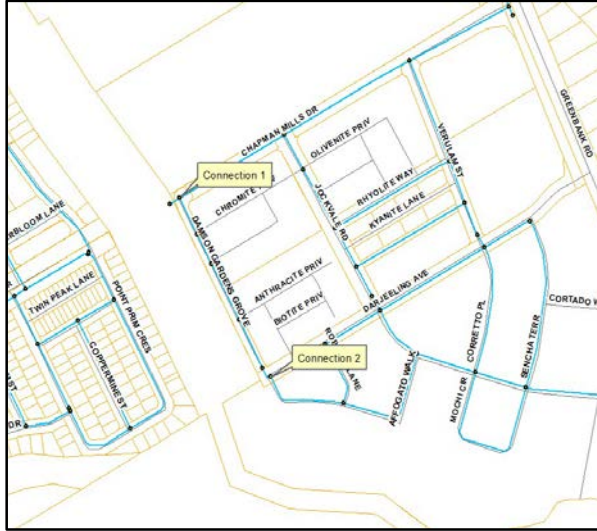
Boundary Conditions Barrhaven Conservancy East

Provided Information

Scenario	Demand	
	L/min	L/s
Average Daily Demand	832	13.87
Maximum Daily Demand	2,080	34.67
Peak Hour	4,576	76.27
Fire Flow Demand #1	13,000	216.67

Location





Results – Existing Conditions BSDY

Connection 1 – Chapman Mills Dr.

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	158.7	93.7
Peak Hour	142.6	70.7
Basic Day plus Fire 1	131.2	54.5

Ground Elevation = 92.8 m

Connection 2 – Danson Gardens Grove / Darjeeling Ave.

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	158.7	95.1
Peak Hour	142.5	72.1
Basic Day plus Fire 1	127.6	50.9

Ground Elevation = 91.8 m

Connection 3 – Flagstaff Dr.

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	158.6	94.5
Peak Hour	142.1	71.1
Basic Day plus Fire 1	129.9	53.7

Ground Elevation = 92.1 m

Results – Existing Conditions MXDY

Connection 1 – Chapman Mills Dr.

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	157.0	91.2
Peak Hour	137.6	63.7
Max Day plus Fire 1	140.1	67.2

Ground Elevation = 92.8 m

Connection 2 – Danson Gardens Grove / Darjeeling Ave.

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	157.0	92.7
Peak Hour	137.6	65.0
Max Day plus Fire 1	136.4	63.4

Ground Elevation = 91.8 m

Connection 3 – Flagstaff Dr.

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	156.8	91.9
Peak Hour	136.9	63.7
Max Day plus Fire 1	137.7	64.8

Ground Elevation = 92.1 m

Results – SUC Zone Reconfiguration BSDY**Connection 1 – Chapman Mills Dr.**

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	149.5	80.7
Peak Hour	147.3	77.5
Basic Day plus Fire 1	138.6	65.1

Ground Elevation = 92.8 m

Connection 2 – Danson Gardens Grove / Darjeeling Ave.

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	149.5	82.1
Peak Hour	147.3	78.9
Basic Day plus Fire 1	135.1	61.5

Ground Elevation = 91.8 m

Connection 3 – Flagstaff Dr.

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	149.5	81.5
Peak Hour	146.9	77.9
Basic Day plus Fire 1	137.4	64.3

Ground Elevation = 92.1 m

Results – SUC Zone Reconfiguration MXDY**Connection 1 – Chapman Mills Dr.**

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	147.9	78.3
Peak Hour	144.5	73.4
Max Day plus Fire 1	137.1	62.9

Ground Elevation = 92.8 m

Connection 2 – Danson Gardens Grove / Darjeeling Ave.

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	147.9	79.7
Peak Hour	144.4	74.7
Max Day plus Fire 1	133.4	59.1

Ground Elevation = 91.8 m

Connection 3 – Flagstaff Dr.

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	147.5	78.8
Peak Hour	142.0	71.0
Max Day plus Fire 1	134.8	60.6

Ground Elevation = 92.1 m

Notes

1. As per the Ontario Building Code in areas that may be occupied, the static pressure at any fixture shall not exceed 552 kPa (80 psi.) Pressure control measures to be considered are as follows, in order of preference:
 - a. If possible, systems to be designed to residual pressures of 345 to 552 kPa (50 to 80 psi) in all occupied areas outside of the public right-of-way without special pressure control equipment.
 - b. Pressure reducing valves to be installed immediately downstream of the isolation valve in the home/ building, located downstream of the meter so it is owner maintained.

Disclaimer

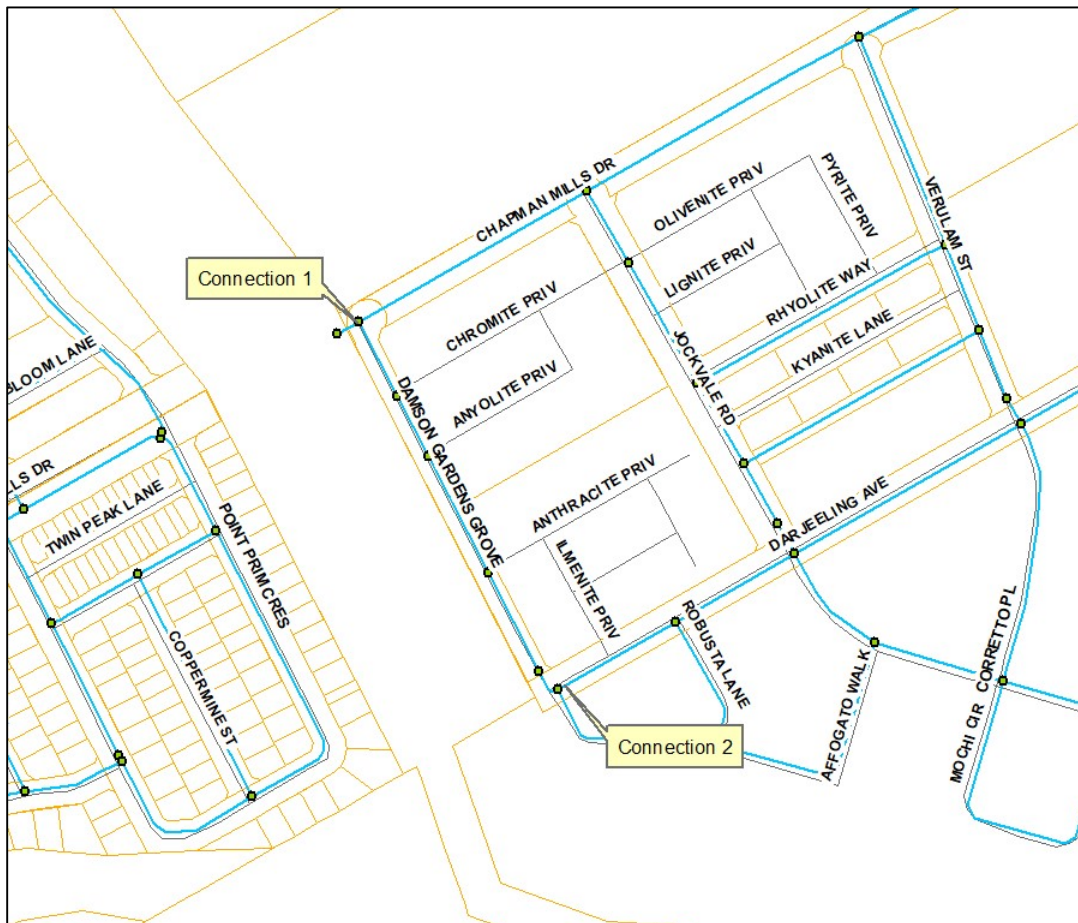
The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation. Fire Flow analysis is a reflection of available flow in the watermain; there may be additional restrictions that occur between the watermain and the hydrant that the model cannot take into account.

Boundary Conditions Barrhaven Conservancy East

Provided Information

Scenario	Demand	
	L/min	L/s
Average Daily Demand	832	13.87
Maximum Daily Demand	2,080	34.67
Peak Hour	4,576	76.27
Fire Flow Demand #1	13,000	216.67

Location



Scenario 1 Results – Existing Conditions BSDY

Connection 1 – Chapman Mills Dr.

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	158.7	93.7
Peak Hour	142.5	70.7
Basic Day plus Fire 1	131.0	54.2

Ground Elevation = 92.8 m

Connection 2 – Danson Gardens Grove / Darjeeling Ave.

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	158.7	95.1
Peak Hour	142.5	72.1
Basic Day plus Fire 1	127.4	50.6

Ground Elevation = 91.8 m

Scenario 1 Results – Existing Conditions MXDY**Connection 1 – Chapman Mills Dr.**

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	157.0	91.2
Peak Hour	137.5	63.5
Max Day plus Fire 1	139.6	66.5

Ground Elevation = 92.8 m

Connection 2 – Danson Gardens Grove / Darjeeling Ave.

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	157.0	92.6
Peak Hour	137.5	64.9
Max Day plus Fire 1	135.8	62.5

Ground Elevation = 91.8 m

Scenario 1 Results – SUC Zone Reconfiguration BSDY**Connection 1 – Chapman Mills Dr.**

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	150.0	81.3
Peak Hour	147.6	77.9
Basic Day plus Fire 1	138.7	65.2

Ground Elevation = 92.8 m

Connection 2 – Danson Gardens Grove / Darjeeling Ave.

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	150.0	82.8
Peak Hour	147.6	79.2
Basic Day plus Fire 1	135.1	61.5

Ground Elevation = 91.8 m

Scenario 1 Results – SUC Zone Reconfiguration MXDY**Connection 1 – Chapman Mills Dr.**

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	148.6	79.3
Peak Hour	144.2	73.0
Max Day plus Fire 1	137.0	62.8

Ground Elevation = 92.8 m

Connection 2 – Danson Gardens Grove / Darjeeling Ave.

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	148.6	80.7
Peak Hour	144.0	74.2
Max Day plus Fire 1	133.2	58.8

Ground Elevation = 91.8 m

Scenario 2 Results – Existing Conditions BSDY**Connection 1 – Chapman Mills Dr.**

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	158.7	93.7
Peak Hour	142.5	70.7
Basic Day plus Fire 1	131.2	54.5

Ground Elevation = 92.8 m

Connection 2 – Danson Gardens Grove / Darjeeling Ave.

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	158.7	93.7
Peak Hour	142.5	70.7
Basic Day plus Fire 1	132.4	57.6

Ground Elevation = 91.8 m

Scenario 2 Results – Existing Conditions MXDY**Connection 1 – Chapman Mills Dr.**

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	157.0	91.2
Peak Hour	137.5	63.6
Max Day plus Fire 1	139.9	66.9

Ground Elevation = 92.8 m

Connection 2 – Danson Gardens Grove / Darjeeling Ave.

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	157.0	92.6
Peak Hour	137.5	65.0
Max Day plus Fire 1	141.1	70.1

Ground Elevation = 91.8 m

Scenario 2 Results – SUC Zone Reconfiguration BSDY**Connection 1 – Chapman Mills Dr.**

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	149.5	80.7
Peak Hour	147.3	77.5
Basic Day plus Fire 1	138.6	65.1

Ground Elevation = 92.8 m

Connection 2 – Danson Gardens Grove / Darjeeling Ave.

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	149.5	80.7
Peak Hour	147.3	77.5
Basic Day plus Fire 1	139.8	68.2

Ground Elevation = 91.8 m

Scenario 2 Results – SUC Zone Reconfiguration MXDY**Connection 1 – Chapman Mills Dr.**

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	147.9	78.3
Peak Hour	144.1	72.9
Max Day plus Fire 1	136.8	62.6

Ground Elevation = 92.8 m

Connection 2 – Danson Gardens Grove / Darjeeling Ave.

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	147.9	79.7
Peak Hour	144.1	74.3
Max Day plus Fire 1	138.1	65.8

Ground Elevation = 91.8 m

Notes

1. The watermain on Darjeeling Ave. was upsized to a 300mm diameter pipe between Danson Gardens Grove and Jockvale Road during Scenario 2 for modelling purposes.
2. As per the Ontario Building Code in areas that may be occupied, the static pressure at any fixture shall not exceed 552 kPa (80 psi.) Pressure control measures to be considered are as follows, in order of preference:
 - a. If possible, systems to be designed to residual pressures of 345 to 552 kPa (50 to 80 psi) in all occupied areas outside of the public right-of-way without special pressure control equipment.
 - b. Pressure reducing valves to be installed immediately downstream of the isolation valve in the home/ building, located downstream of the meter so it is owner maintained.

Disclaimer

The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation. Fire Flow analysis is a reflection of available flow in the watermain; there may be additional restrictions that occur between the watermain and the hydrant that the model cannot take into account.

BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

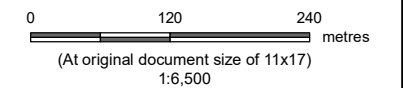
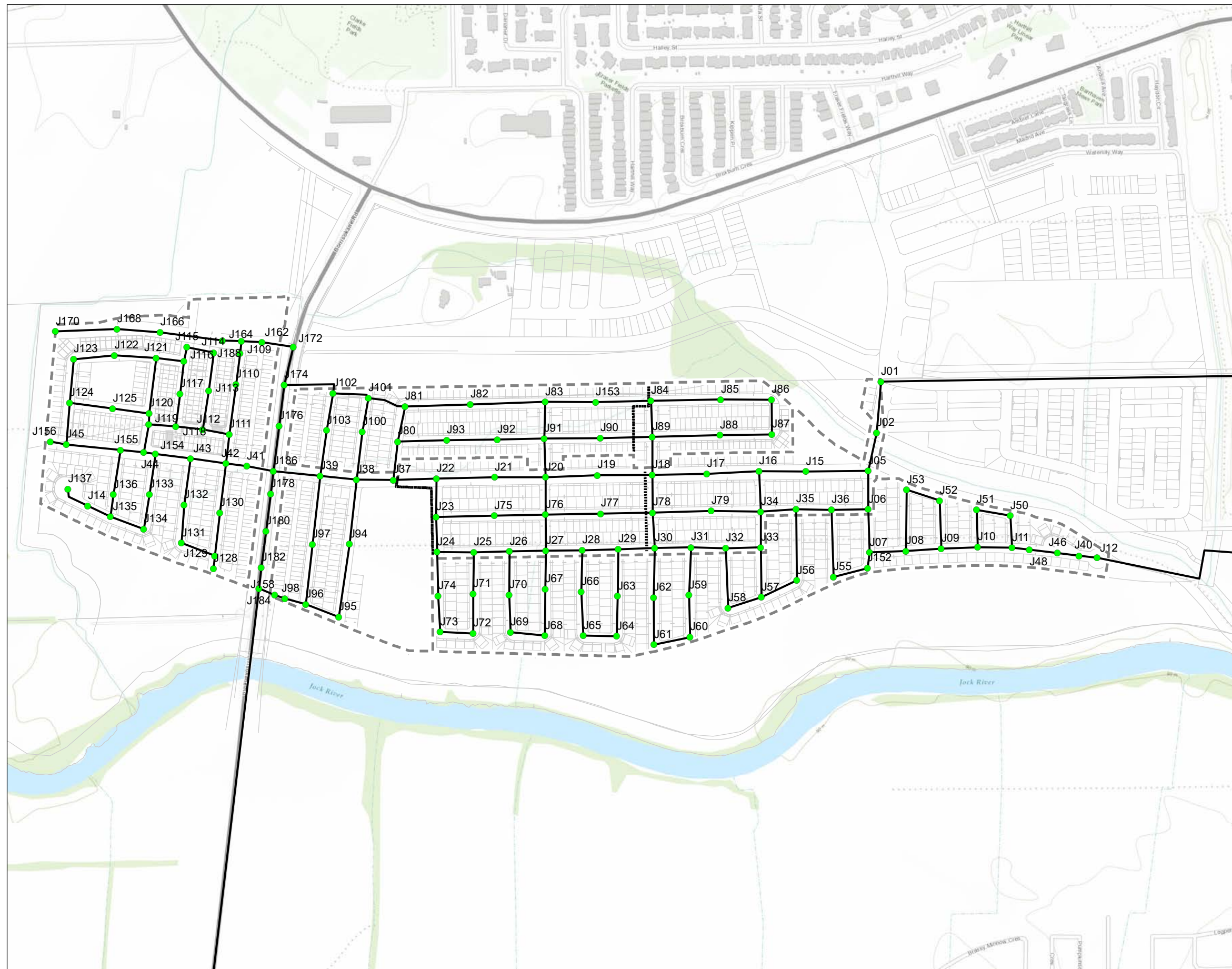
June 2, 2022

Appendix C JUNCTION IDS

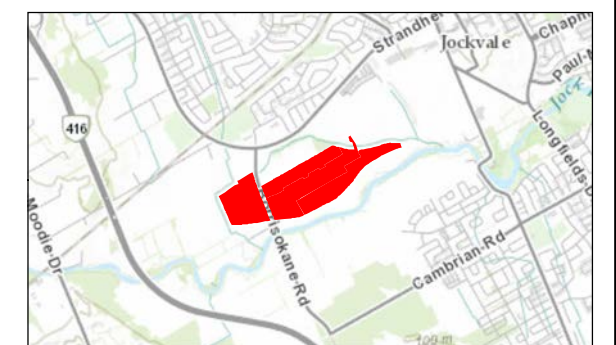


Legend

- Development Phase Boundary
- Development Sub-Phase Boundary
- Property Line
- Future Watermain
- Model Junction



Notes
 1. Coordinate System: NAD 1983 CSRS MTM 9
 2. Background: Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri China (Hong Kong), (c) OpenStreetMap contributors, and the GIS User Community



Project Location
 Ottawa, ON

Client/Project
 David Schaeffer Engineering Ltd
 Barrhaven Conservancy East (Phases 2, 3, 4 & Jock River)
 Water Distribution System Analysis

Figure No.

C1

Title

Junction IDs

BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION SYSTEM ANALYSIS

June 2, 2022

Appendix D MODEL RESULTS



Option A - 2 Connections - Phase 2 (2A, 2B, 2C)				Option A - 2 Connections with Upgrades on Danson Gardens Grv - Phase 2 (2A, 2B, 2C)				Option B - 3 Connections - Phase 2 (2A, 2B, 2C)			
Junction ID	Demand (L/s)	Head (m)	Pressure (psi)	Junction ID	Demand (L/s)	Head (m)	Pressure (psi)	Junction ID	Demand (L/s)	Head (m)	Pressure (psi)
<i>Maximum</i>	0.11	150.00	81.74	<i>Maximum</i>	0.11	149.50	81.23	<i>Maximum</i>	0.11	150.00	81.73
<i>Minimum</i>	0.00	150.00	80.32	<i>Minimum</i>	0.00	149.50	79.61	<i>Minimum</i>	0.00	149.99	80.31
J01	0.07	150.00	80.32	J01	0.07	149.50	79.61	J01	0.07	150.00	80.31
J02	0.00	150.00	80.93	J02	0.00	149.50	80.22	J02	0.00	150.00	80.92
J05	0.07	150.00	81.43	J05	0.07	149.50	80.72	J05	0.07	150.00	81.42
J06	0.07	150.00	81.57	J06	0.07	149.50	80.86	J06	0.07	150.00	81.56
J07	0.11	150.00	81.73	J07	0.11	149.50	81.01	J07	0.11	150.00	81.72
J08	0.11	150.00	81.60	J08	0.11	149.50	80.89	J08	0.11	150.00	81.59
J09	0.11	150.00	81.59	J09	0.11	149.50	80.38	J09	0.11	150.00	81.08
J10	0.11	150.00	81.34	J10	0.11	149.50	80.63	J10	0.11	150.00	81.34
J11	0.11	150.00	81.23	J11	0.11	149.50	80.52	J11	0.11	150.00	81.22
J12	0.11	150.00	81.09	J12	0.11	149.50	80.38	J12	0.11	150.00	81.08
J15	0.07	150.00	81.28	J15	0.07	149.50	80.57	J15	0.07	149.99	81.28
J158	0.00	150.00	81.74	J158	0.00	149.50	81.03	J158	0.00	149.99	81.73
J16	0.07	150.00	81.44	J16	0.07	149.50	80.73	J16	0.07	149.99	81.43
J17	0.07	150.00	81.27	J17	0.07	149.50	80.56	J17	0.07	149.99	81.26
J178	0.08	150.00	81.36	J178	0.08	149.50	80.64	J178	0.08	149.99	81.35
J18	0.07	150.00	81.08	J18	0.07	149.50	80.35	J18	0.07	149.99	81.05
J180	0.08	150.00	81.57	J180	0.08	149.50	80.86	J180	0.08	149.99	81.56
J182	0.08	150.00	81.69	J182	0.08	149.50	80.97	J182	0.08	149.99	81.68
J184	0.08	150.00	81.74	J184	0.08	149.50	81.03	J184	0.08	149.99	81.73
J186	0.08	150.00	81.26	J186	0.08	149.50	80.54	J186	0.08	149.99	81.25
J19	0.10	150.00	80.84	J19	0.10	149.50	80.13	J19	0.10	149.99	80.84
J20	0.10	150.00	81.31	J20	0.10	149.50	80.60	J20	0.10	149.99	81.31
J21	0.10	150.00	81.16	J21	0.10	149.50	80.45	J21	0.10	149.99	81.15
J22	0.10	150.00	81.21	J22	0.10	149.50	80.50	J22	0.10	149.99	81.21
J23	0.10	150.00	81.34	J23	0.10	149.50	80.63	J23	0.10	149.99	81.33
J24	0.10	150.00	81.47	J24	0.10	149.50	80.76	J24	0.10	149.99	81.46
J25	0.10	150.00	81.36	J25	0.10	149.50	80.64	J25	0.10	149.99	81.35
J26	0.10	150.00	81.45	J26	0.10	149.50	80.74	J26	0.10	149.99	81.45
J27	0.10	150.00	81.58	J27	0.10	149.50	80.87	J27	0.10	149.99	81.58
J28	0.10	150.00	81.51	J28	0.10	149.50	80.80	J28	0.10	149.99	81.51
J29	0.10	150.00	81.51	J29	0.10	149.50	80.80	J29	0.10	149.99	81.51
J30	0.07	150.00	81.44	J30	0.07	149.50	80.73	J30	0.07	149.99	81.43
J31	0.07	150.00	81.57	J31	0.07	149.50	80.86	J31	0.07	149.99	81.56
J32	0.07	150.00	81.47	J32	0.07	149.50	80.76	J32	0.07	149.99	81.46
J33	0.07	150.00	81.70	J33	0.07	149.50	80.99	J33	0.07	149.99	81.69
J34	0.07	150.00	81.57	J34	0.07	149.50	80.86	J34	0.07	149.99	81.56
J35	0.07	150.00	81.53	J35	0.07	149.50	80.82	J35	0.07	149.99	81.52
J36	0.07	150.00	81.65	J36	0.07	149.50	80.94	J36	0.07	149.99	81.65
J37	0.08	150.00	81.13	J37	0.08	149.50	80.42	J37	0.08	149.99	81.12
J38	0.08	150.00	81.26	J38	0.08	149.50	80.54	J38	0.08	149.99	81.25
J39	0.08	150.00	81.29	J39	0.08	149.50	80.54	J39	0.08	149.99	81.25
J40	0.11	150.00	81.12	J40	0.11	149.50	80.41	J40	0.11	150.00	81.11
J46	0.11	150.00	81.16	J46	0.11	149.50	80.45	J46	0.11	150.00	81.16
J48	0.11	150.00	81.20	J48	0.11	149.50	80.49	J48	0.11	150.00	81.20
J75	0.10	150.00	81.28	J75	0.10	149.50	80.57	J75	0.10	149.99	81.28
J76	0.10	150.00	81.45	J76	0.10	149.50	80.74	J76	0.10	149.99	81.45
J77	0.10	150.00	81.17	J77	0.10	149.50	80.46	J77	0.10	149.99	81.16
J78	0.07	150.00	81.33	J78	0.07	149.50	80.62	J78	0.07	149.99	81.32
J79	0.07	150.00	81.41	J79	0.07	149.50	80.70	J79	0.07	149.99	81.41
J94	0.08	150.00	81.51	J94	0.08	149.50	80.80	J94	0.08	149.99	81.50
J95	0.08	150.00	81.74	J95	0.08	149.50	81.03	J95	0.08	149.99	81.73
J96	0.08	150.00	81.61	J96	0.08	149.50	80.90	J96	0.08	149.99	81.60
J97	0.08	150.00	81.37	J97	0.08	149.50	80.66	J97	0.08	149.99	81.36
J98	0.00	150.00	81.54	J98	0.00	149.50	80.83	J98	0.00	149.99	81.53

Option A - 2 Connections - Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E)				Option A - 2 Connections with Upgrades on Danson Gardens Grv - Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E)				Option B - 3 Connections - Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E)			
Junction ID	Demand (L/s)	Head (m)	Pressure (psi)	Junction ID	Demand (L/s)	Head (m)	Pressure (psi)	Junction ID	Demand (L/s)	Head (m)	Pressure (psi)
Maximum	0.15	150.00	81.73	Maximum	0.15	149.50	81.62	Maximum	0.15	149.99	81.71
Minimum	0.00	149.99	80.32	Minimum	0.00	149.49	79.61	Minimum	0.00	149.98	80.30
J01	0.07	150.00	80.32	J01	0.07	149.50	79.61	J01	0.07	149.99	80.30
J02	0.00	150.00	80.93	J02	0.00	149.50	80.22	J02	0.00	149.99	80.91
J05	0.07	150.00	81.42	J05	0.07	149.50	80.71	J05	0.07	149.99	81.41
J06	0.07	150.00	81.57	J06	0.07	149.50	80.86	J06	0.07	149.99	81.55
J07	0.11	150.00	81.72	J07	0.11	149.50	81.01	J07	0.11	149.99	81.71
J08	0.11	150.00	81.60	J08	0.11	149.50	80.88	J08	0.11	149.99	81.58
J09	0.11	150.00	81.68	J09	0.11	149.50	80.97	J09	0.11	149.99	81.07
J10	0.11	150.00	81.34	J10	0.11	149.50	80.63	J10	0.11	149.99	81.33
J100	0.15	149.99	80.80	J100	0.15	149.49	80.08	J100	0.15	149.98	80.78
J101	0.15	149.99	80.85	J101	0.15	149.49	80.24	J101	0.15	149.98	80.93
J102	0.15	149.99	80.84	J102	0.15	149.49	80.13	J102	0.15	149.98	80.82
J103	0.15	149.99	80.68	J103	0.15	149.49	79.97	J103	0.15	149.98	80.66
J11	0.11	150.00	81.23	J11	0.11	149.50	80.52	J11	0.11	149.99	81.22
J12	0.11	150.00	81.09	J12	0.11	149.50	80.37	J12	0.11	149.99	81.08
J15	0.07	150.00	81.28	J15	0.07	149.50	80.57	J15	0.07	149.98	81.26
J153	0.15	149.99	80.77	J153	0.15	149.49	80.06	J153	0.15	149.98	80.75
J158	0.00	149.99	81.73	J158	0.00	149.49	81.02	J158	0.00	149.98	81.71
J16	0.07	150.00	81.44	J16	0.07	149.50	80.73	J16	0.07	149.98	81.42
J17	0.07	150.00	81.27	J17	0.07	149.50	80.56	J17	0.07	149.98	81.25
J174	0.15	149.99	81.02	J174	0.15	149.49	80.31	J174	0.15	149.98	81.00
J176	0.15	149.99	81.14	J176	0.15	149.49	80.43	J176	0.15	149.98	81.12
J178	0.08	149.99	81.35	J178	0.08	149.49	80.64	J178	0.08	149.98	81.33
J18	0.07	150.00	81.05	J18	0.07	149.50	80.34	J18	0.07	149.98	81.03
J180	0.08	149.99	81.56	J180	0.08	149.49	80.85	J180	0.08	149.98	81.54
J182	0.08	149.99	81.68	J182	0.08	149.49	80.97	J182	0.08	149.98	81.66
J184	0.08	149.99	81.73	J184	0.08	149.49	81.02	J184	0.08	149.98	81.71
J186	0.08	149.99	81.25	J186	0.08	149.49	80.54	J186	0.08	149.98	81.23
J19	0.10	150.00	80.84	J19	0.10	149.50	80.13	J19	0.10	149.98	80.82
J20	0.10	150.00	81.31	J20	0.10	149.50	80.60	J20	0.10	149.98	81.29
J21	0.10	150.00	81.15	J21	0.10	149.50	80.44	J21	0.10	149.98	81.13
J22	0.10	150.00	81.21	J22	0.10	149.50	80.50	J22	0.10	149.98	81.19
J23	0.10	150.00	81.34	J23	0.10	149.50	80.63	J23	0.10	149.98	81.32
J24	0.10	150.00	81.46	J24	0.10	149.50	80.75	J24	0.10	149.98	81.44
J25	0.10	150.00	81.35	J25	0.10	149.50	80.64	J25	0.10	149.98	81.33
J26	0.10	150.00	81.45	J26	0.10	149.50	80.74	J26	0.10	149.98	81.43
J27	0.10	150.00	81.58	J27	0.10	149.50	80.87	J27	0.10	149.98	81.56
J28	0.10	150.00	81.51	J28	0.10	149.50	80.80	J28	0.10	149.98	81.49
J29	0.10	150.00	81.51	J29	0.10	149.50	80.80	J29	0.10	149.98	81.49
J30	0.07	150.00	81.44	J30	0.07	149.50	80.73	J30	0.07	149.98	81.42
J31	0.07	150.00	81.56	J31	0.07	149.50	80.85	J31	0.07	149.98	81.55
J32	0.07	150.00	81.47	J32	0.07	149.50	80.75	J32	0.07	149.98	81.45
J33	0.07	150.00	81.69	J33	0.07	149.50	80.98	J33	0.07	149.98	81.68
J34	0.07	150.00	81.57	J34	0.07	149.50	80.85	J34	0.07	149.98	81.55
J35	0.07	150.00	81.52	J35	0.07	149.50	80.81	J35	0.07	149.98	81.51
J36	0.07	150.00	81.65	J36	0.07	149.50	80.94	J36	0.07	149.98	81.64
J37	0.08	149.99	81.12	J37	0.08	149.49	80.41	J37	0.08	149.98	81.10
J38	0.08	149.99	81.25	J38	0.08	149.49	80.54	J38	0.08	149.98	81.23
J39	0.08	149.99	81.25	J39	0.08	149.49	80.54	J39	0.08	149.98	81.23
J40	0.11	150.00	81.12	J40	0.11	149.50	80.40	J40	0.11	149.99	81.11
J46	0.11	150.00	81.16	J46	0.11	149.50	80.45	J46	0.11	149.99	81.15
J48	0.11	150.00	81.20	J48	0.11	149.50	80.49	J48	0.11	149.99	81.19
J75	0.10	150.00	81.28	J75	0.10	149.50	80.57	J75	0.10	149.98	81.26
J76	0.10	150.00	81.45	J76	0.10	149.50	80.74	J76	0.10	149.98	81.43
J77	0.10	150.00	81.17	J77	0.10	149.50	80.46	J77	0.10	149.98	81.15
J78	0.07	150.00	81.32	J78	0.07	149.50	80.61	J78	0.07	149.98	81.30
J79	0.07	150.00	81.41	J79	0.07	149.50	80.70	J79	0.07	149.98	81.39
J80	0.15	149.99	80.98	J80	0.15	149.49	80.27	J80	0.15	149.98	80.96
J81	0.15	149.99	80.80	J81	0.15	149.49	80.08	J81	0.15	149.98	80.78
J82	0.15	149.99	80.84	J82	0.15	149.49	80.13	J82	0.15	149.98	80.82
J83	0.15	149.99	81.05	J83	0.15	149.49	80.34	J83	0.15	149.98	81.03
J84	0.15	150.00	80.92	J84	0.15	149.50	80.21	J84	0.15	149.98	80.90
J85	0.15	149.99	81.02	J85	0.15	149.49	80.31	J85	0.15	149.98	81.00
J86	0.15	149.99	81.24	J86	0.15	149.49	80.53	J86	0.15	149.98	81.22
J87	0.15	149.99	81.19	J87	0.15	149.49	80.48	J87	0.15	149.98	81.17
J88	0.15	149.99	81.05	J88	0.15	149.49	80.34	J88	0.15	149.98	81.03
J89	0.15	150.00	81.05	J89	0.15	149.50	80.34	J89	0.15	149.98	81.03
J90	0.15	150.00	80.88	J90	0.15	149.50	80.17	J90	0.15	149.98	80.86
J91	0.15	149.99	81.18	J91	0.15	149.49	80.47	J91	0.15	149.98	81.16
J92	0.15	149.99	80.99	J92	0.15	149.49	80.28	J92	0.15	149.98	80.98
J93	0.15	149.99	80.88	J93	0.15	149.49	80.17	J93	0.15	149.98	80.86
J94	0.08	149.99	81.51	J94	0.08	149.49	80.80	J94	0.08	149.98	81.49
J95	0.08	149.99	81.73	J95	0.08	149.49	81.02	J95	0.08	149.98	81.71
J96	0.08	149.99	81.61	J96	0.08	149.49	80.90	J96	0.08	149.98	81.59
J97	0.08	149.99	81.36	J97	0.08	149.49	80.65	J97	0.08	149.98	81.34
J98	0.00	149.99	81.53	J98	0.00	149.49	80.82	J98	0.00	149.98	81.52

Option A - 2 Connections - Phase 2 (2A, 2B, 2C)				Option A - 2 Connections with Upgrades on Danson Gardens Grv - Phase 2 (2A, 2B, 2C)				Option B - 3 Connections - Phase 2 (2A, 2B, 2C)			
Junction ID	Demand (L/s)	Head (m)	Pressure (psi)	Junction ID	Demand (L/s)	Head (m)	Pressure (psi)	Junction ID	Demand (L/s)	Head (m)	Pressure (psi)
Maximum	0.58	144.12	73.34	Maximum	0.58	144.09	72.31	Maximum	0.58	144.07	72.15
Minimum	0.00	144.09	71.96	Minimum	0.00	144.06	71.90	Minimum	0.00	144.93	71.81
J01	0.39	144.12	71.96	J01	0.39	144.08	71.90	J01	0.39	144.01	71.81
J02	0.00	144.11	72.56	J02	0.00	144.08	72.51	J02	0.00	143.99	72.38
J05	0.39	144.10	73.05	J05	0.39	144.08	73.01	J05	0.39	143.97	72.85
J06	0.39	144.10	73.18	J06	0.39	144.08	73.15	J06	0.39	143.96	72.99
J07	0.58	144.10	73.34	J07	0.58	144.08	73.31	J07	0.58	143.96	73.15
J08	0.58	144.10	73.21	J08	0.58	144.08	73.18	J08	0.58	143.97	73.02
J09	0.58	144.10	72.70	J09	0.58	144.08	72.67	J09	0.58	143.97	72.51
J10	0.58	144.10	72.95	J10	0.58	144.08	72.93	J10	0.58	143.97	72.77
J11	0.58	144.10	72.84	J11	0.58	144.08	72.82	J11	0.58	143.97	72.66
J12	0.58	144.10	72.70	J12	0.58	144.09	72.68	J12	0.58	143.98	72.52
J15	0.39	144.10	72.90	J15	0.39	144.07	72.86	J15	0.39	143.96	72.70
J158	0.00	144.09	73.33	J158	0.00	144.06	73.30	J158	0.00	143.93	73.11
J16	0.39	144.10	73.05	J16	0.39	144.07	73.01	J16	0.39	143.95	72.85
J17	0.39	144.09	72.86	J17	0.39	144.07	72.84	J17	0.39	143.95	72.67
J178	0.44	144.09	72.85	J178	0.44	144.06	72.91	J178	0.44	143.93	72.72
J18	0.39	144.09	72.66	J18	0.39	144.07	72.62	J18	0.39	143.94	72.45
J180	0.44	144.09	73.16	J180	0.44	144.06	73.13	J180	0.44	143.93	72.94
J182	0.44	144.09	73.26	J182	0.44	144.06	73.24	J182	0.44	143.93	73.05
J184	0.44	144.09	73.33	J184	0.44	144.06	73.30	J184	0.44	143.93	73.11
J186	0.44	144.09	72.85	J186	0.44	144.06	72.81	J186	0.44	143.93	72.62
J19	0.56	144.09	72.45	J19	0.56	144.06	72.41	J19	0.56	143.94	72.23
J20	0.56	144.09	72.91	J20	0.56	144.06	72.88	J20	0.56	143.93	72.69
J21	0.56	144.09	72.75	J21	0.56	144.06	72.72	J21	0.56	143.93	72.53
J22	0.56	144.09	72.81	J22	0.56	144.06	72.77	J22	0.56	143.93	72.59
J23	0.56	144.09	72.94	J23	0.56	144.06	72.90	J23	0.56	143.93	72.72
J24	0.56	144.09	73.07	J24	0.56	144.06	73.03	J24	0.56	143.93	72.84
J25	0.56	144.09	72.95	J25	0.56	144.06	72.92	J25	0.56	143.93	72.73
J26	0.56	144.09	73.05	J26	0.56	144.06	73.01	J26	0.56	143.93	72.83
J27	0.56	144.09	73.18	J27	0.56	144.06	73.14	J27	0.56	143.93	72.96
J28	0.56	144.09	73.11	J28	0.56	144.06	73.07	J28	0.56	143.94	72.89
J29	0.56	144.09	73.11	J29	0.56	144.06	73.07	J29	0.56	143.94	72.89
J30	0.39	144.09	73.04	J30	0.39	144.06	73.00	J30	0.39	143.94	72.83
J31	0.39	144.09	73.17	J31	0.39	144.06	73.13	J31	0.39	143.94	72.96
J32	0.39	144.09	73.07	J32	0.39	144.07	73.03	J32	0.39	143.94	72.86
J33	0.39	144.09	73.30	J33	0.39	144.07	73.26	J33	0.39	143.95	73.09
J34	0.39	144.09	73.17	J34	0.39	144.07	73.14	J34	0.39	143.95	72.97
J35	0.39	144.10	73.13	J35	0.39	144.07	73.10	J35	0.39	143.95	72.93
J36	0.39	144.10	73.27	J36	0.39	144.07	73.23	J36	0.39	143.96	73.07
J37	0.44	144.09	72.72	J37	0.44	144.06	72.69	J37	0.44	143.93	72.50
J38	0.44	144.09	72.85	J38	0.44	144.06	72.81	J38	0.44	143.93	72.62
J39	0.44	144.09	72.85	J39	0.44	144.06	72.81	J39	0.44	143.93	72.62
J40	0.58	144.10	72.73	J40	0.58	144.08	72.71	J40	0.58	143.97	72.55
J46	0.58	144.10	72.77	J46	0.58	144.08	72.75	J46	0.58	143.97	72.59
J48	0.58	144.10	72.81	J48	0.58	144.08	72.79	J48	0.58	143.97	72.63
J75	0.56	144.09	72.86	J75	0.56	144.06	72.84	J75	0.56	143.93	72.66
J76	0.56	144.09	73.05	J76	0.56	144.06	73.02	J76	0.56	143.93	72.83
J77	0.56	144.09	72.77	J77	0.56	144.06	72.73	J77	0.56	143.94	72.55
J78	0.39	144.09	72.93	J78	0.39	144.06	72.89	J78	0.39	143.94	72.71
J79	0.39	144.09	73.01	J79	0.39	144.07	72.98	J79	0.39	143.94	72.81
J94	0.44	144.09	73.11	J94	0.44	144.06	73.07	J94	0.44	143.93	72.88
J95	0.44	144.09	73.33	J95	0.44	144.06	73.30	J95	0.44	143.93	73.11
J96	0.44	144.09	73.21	J96	0.44	144.06	73.17	J96	0.44	143.93	72.98
J97	0.44	144.09	72.96	J97	0.44	144.06	72.93	J97	0.44	143.93	72.74
J98	0.00	144.09	73.14	J98	0.00	144.06	73.10	J98	0.00	143.93	72.91

Option A - 2 Connections - Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E)				Option A - 2 Connections with Upgrades on Danson Gardens Grv - Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E)				Option B - 3 Connections - Phase 2 (2A, 2B, 2C) + Phase 3 (2D, 2E)			
Junction ID	Demand (L/s)	Head (m)	Pressure (psi)	Junction ID	Demand (L/s)	Head (m)	Pressure (psi)	Junction ID	Demand (L/s)	Head (m)	Pressure (psi)
Maximum	0.53	144.04	73.12	Maximum	0.53	144.05	72.25	Maximum	0.53	143.88	72.89
Minimum	0.00	143.94	71.84	Minimum	0.00	143.98	71.85	Minimum	0.00	143.64	71.58
J01	0.39	144.04	71.84	J01	0.39	144.04	71.85	J01	0.39	143.85	71.58
J02	0.00	144.01	72.42	J02	0.00	144.04	72.45	J02	0.00	143.81	72.13
J05	0.39	144.00	72.80	J05	0.39	144.03	72.94	J05	0.39	143.77	72.58
J06	0.39	144.00	73.04	J06	0.39	144.03	73.09	J06	0.39	143.77	72.71
J07	0.58	144.00	73.19	J07	0.58	144.04	73.25	J07	0.58	143.78	72.89
J08	0.58	144.00	73.06	J08	0.58	144.04	73.13	J08	0.58	143.80	72.78
J09	0.58	144.00	72.55	J09	0.58	144.04	72.62	J09	0.58	143.81	72.28
J10	0.58	144.00	72.81	J10	0.58	144.05	72.88	J10	0.58	143.82	72.56
J100	0.83	143.94	72.20	J100	0.83	143.98	72.24	J100	0.83	143.65	71.77
J101	0.83	143.94	72.35	J101	0.83	143.98	72.40	J101	0.83	143.65	71.93
J102	0.83	143.94	72.24	J102	0.83	143.98	72.29	J102	0.83	143.64	71.81
J103	0.83	143.94	72.08	J103	0.83	143.98	72.13	J103	0.83	143.64	71.65
J11	0.58	144.00	72.70	J11	0.58	144.05	72.77	J11	0.58	143.84	72.47
J12	0.58	144.00	72.55	J12	0.58	144.06	72.65	J12	0.58	143.86	72.38
J15	0.39	143.99	72.74	J15	0.39	144.02	72.78	J15	0.39	143.74	72.39
J153	0.83	143.95	72.17	J153	0.83	143.98	72.22	J153	0.83	143.65	71.75
J158	0.00	143.95	73.13	J158	0.00	143.98	73.18	J158	0.00	143.64	72.71
J16	0.39	143.98	72.86	J16	0.39	144.01	72.93	J16	0.39	143.72	72.51
J17	0.39	143.97	72.70	J17	0.39	144.00	72.74	J17	0.39	143.69	72.30
J174	0.83	143.94	72.42	J174	0.83	143.98	72.47	J174	0.83	143.64	72.00
J176	0.83	143.95	72.54	J176	0.83	143.98	72.59	J176	0.83	143.64	72.11
J178	0.44	143.95	72.75	J178	0.44	143.98	72.83	J178	0.44	143.64	72.32
J18	0.39	143.96	72.47	J18	0.39	143.99	72.52	J18	0.39	143.67	72.05
J180	0.44	143.95	72.96	J180	0.44	143.98	73.01	J180	0.44	143.64	72.54
J182	0.44	143.95	73.08	J182	0.44	143.98	73.13	J182	0.44	143.64	72.65
J184	0.44	143.95	72.81	J184	0.44	143.98	72.86	J184	0.44	143.64	72.71
J186	0.44	143.95	72.65	J186	0.44	143.98	72.70	J186	0.44	143.64	72.22
J19	0.56	143.95	72.25	J19	0.56	143.99	72.30	J19	0.56	143.66	71.83
J20	0.56	143.95	72.72	J20	0.56	143.99	72.77	J20	0.56	143.66	72.30
J21	0.56	143.95	72.55	J21	0.56	143.98	72.61	J21	0.56	143.66	72.14
J22	0.56	143.95	72.61	J22	0.56	143.98	72.66	J22	0.56	143.65	72.20
J23	0.56	143.95	72.74	J23	0.56	143.98	72.79	J23	0.56	143.66	72.33
J24	0.56	143.95	72.87	J24	0.56	143.98	72.92	J24	0.56	143.66	72.46
J25	0.56	143.95	72.76	J25	0.56	143.98	72.81	J25	0.56	143.66	72.35
J26	0.56	143.95	72.86	J26	0.56	143.99	72.91	J26	0.56	143.66	72.45
J27	0.56	143.95	72.99	J27	0.56	143.99	73.04	J27	0.56	143.67	72.58
J28	0.56	143.95	72.92	J28	0.56	143.99	72.97	J28	0.56	143.67	72.52
J29	0.56	143.96	72.92	J29	0.56	143.99	72.97	J29	0.56	143.68	72.52
J30	0.39	143.96	72.86	J30	0.39	143.99	72.90	J30	0.39	143.68	72.46
J31	0.39	143.96	72.99	J31	0.39	144.00	73.04	J31	0.39	143.69	72.60
J32	0.39	143.97	72.89	J32	0.39	144.00	72.94	J32	0.39	143.70	72.51
J33	0.39	143.97	73.13	J33	0.39	144.00	73.17	J33	0.39	143.71	72.75
J34	0.39	143.97	73.00	J34	0.39	144.01	73.05	J34	0.39	143.72	72.64
J35	0.39	143.98	72.97	J35	0.39	144.02	73.02	J35	0.39	143.73	72.62
J36	0.39	143.99	73.11	J36	0.39	144.02	73.16	J36	0.39	143.75	72.77
J37	0.44	143.95	72.53	J37	0.44	143.98	72.57	J37	0.44	143.65	72.10
J38	0.44	143.95	72.65	J38	0.44	143.98	72.70	J38	0.44	143.65	72.23
J39	0.44	143.95	72.65	J39	0.44	143.98	72.70	J39	0.44	143.65	72.22
J40	0.58	144.00	72.58	J40	0.58	144.06	72.68	J40	0.58	143.87	72.40
J46	0.58	144.00	72.63	J46	0.58	144.06	72.71	J46	0.58	143.86	72.43
J48	0.58	144.00	72.67	J48	0.58	144.05	72.78	J48	0.58	143.84	72.45
J75	0.56	143.95	72.69	J75	0.56	143.98	72.73	J75	0.56	143.66	72.27
J76	0.56	143.95	72.85	J76	0.56	143.99	72.91	J76	0.56	143.66	72.45
J77	0.56	143.95	72.58	J77	0.56	143.99	72.63	J77	0.56	143.67	72.17
J78	0.39	143.96	72.74	J78	0.39	143.99	72.79	J78	0.39	143.68	72.34
J79	0.39	143.97	72.84	J79	0.39	144.00	72.89	J79	0.39	143.70	72.45
J80	0.83	143.94	72.38	J80	0.83	143.98	72.43	J80	0.83	143.65	71.96
J81	0.83	143.95	72.20	J81	0.83	143.98	72.24	J81	0.83	143.65	71.77
J82	0.83	143.95	72.24	J82	0.83	143.98	72.29	J82	0.83	143.65	71.82
J83	0.83	143.95	72.45	J83	0.83	143.98	72.50	J83	0.83	143.65	72.03
J84	0.80	143.95	72.33	J84	0.80	143.98	72.38	J84	0.80	143.65	71.91
J85	0.80	143.95	72.42	J85	0.80	143.98	72.47	J85	0.80	143.65	72.01
J86	0.80	143.95	72.64	J86	0.80	143.98	72.69	J86	0.80	143.65	72.22
J87	0.80	143.95	72.60	J87	0.80	143.98	72.64	J87	0.80	143.65	72.18
J88	0.80	143.95	72.45	J88	0.80	143.98	72.50	J88	0.80	143.65	72.04
J89	0.80	143.95	72.46	J89	0.80	143.99	72.51	J89	0.80	143.66	72.04
J90	0.83	143.95	72.29	J90	0.83	143.98	72.33	J90	0.83	143.65	71.87
J91	0.83	143.95	72.56	J91	0.83	143.98	72.63	J91	0.83	143.65	72.16
J92	0.83	143.95	72.40	J92	0.83	143.98	72.44	J92	0.83	143.65	71.97
J93	0.83	143.94	72.28	J93	0.83	143.98	72.33	J93	0.83	143.65	71.86
J94	0.44	143.95	72.91	J94	0.44	143.98	72.96	J94	0.44	143.65	72.48
J95	0.44	143.95	73.13	J95	0.44	143.98	73.18	J95	0.44	143.64	72.71
J96	0.44	143.95	73.01	J96	0.44	143.98	73.05	J96	0.44	143.64	72.58
J97	0.44	143.95	72.76	J97	0.44	143.98	72.81	J97	0.44	143.64	72.34
J98	0.00	143.95	72.93	J98	0.00	143.98	72.98	J98	0.00	143.64	72.51

Option A - 2 Connections - Phase 2 (2A, 2B, 2C)				
Junction ID	Base Demand (MXDY, L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)
J01	0.18	13,000	59.93	64,000
J02	0.00	13,000	60.51	64,000
J05	0.18	13,000	61.00	64,000
J06	0.18	13,000	61.17	64,000
J07	0.27	13,000	61.40	64,000
J08	0.27	13,000	61.35	65,000
J09	0.27	13,000	60.94	65,000
J10	0.27	13,000	61.31	67,000
J11	0.27	13,000	61.33	68,000
J12	0.27	13,000	61.61	75,000
J15	0.18	13,000	60.14	55,000
J158	0.00	13,000	53.27	29,000
J16	0.18	13,000	59.88	52,000
J17	0.18	13,000	59.23	48,000
J178	0.20	13,000	54.17	31,000
J18	0.18	13,000	58.59	46,000
J180	0.20	13,000	53.53	30,000
J182	0.20	13,000	53.25	29,000
J184	0.20	13,000	53.24	29,000
J186	0.20	13,000	54.90	33,000
J19	0.25	13,000	57.93	43,000
J20	0.25	13,000	58.04	42,000
J21	0.25	13,000	57.50	40,000
J22	0.25	13,000	57.21	39,000
J23	0.25	13,000	56.74	37,000
J24	0.25	13,000	56.19	35,000
J25	0.25	13,000	55.70	34,000
J26	0.25	13,000	55.73	34,000
J27	0.25	13,000	56.06	35,000
J28	0.25	13,000	55.86	34,000
J29	0.25	13,000	55.98	34,000
J30	0.18	13,000	56.30	35,000
J31	0.18	13,000	56.47	36,000
J32	0.18	13,000	56.69	38,000
J33	0.18	13,000	57.55	39,000
J34	0.18	13,000	58.47	43,000
J35	0.18	13,000	58.79	44,000
J36	0.18	13,000	59.70	49,000
J37	0.20	13,000	56.39	37,000
J38	0.20	13,000	55.90	35,000
J39	0.20	13,000	55.42	34,000
J40	0.27	13,000	61.54	73,000
J46	0.27	13,000	61.47	71,000
J48	0.27	13,000	61.38	69,000
J75	0.25	13,000	47.92	23,000
J76	0.25	13,000	52.46	28,000
J77	0.25	13,000	47.31	23,000
J78	0.18	13,000	52.96	29,000
J79	0.18	13,000	49.39	25,000
J94	0.20	13,000	53.82	30,000
J95	0.20	13,000	53.35	29,000
J96	0.20	13,000	53.38	29,000
J97	0.20	13,000	44.98	21,000
J98	0.00	13,000	53.12	29,000

Option A - 2 Connections with Upgrades on Danson Gardens Grv - Phase 2 (2A, 2B, 2C)				
Junction ID	Base Demand (MXDY, L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)
J01	0.18	13,000	62.43	66,000
J02	0.00	13,000	63.01	66,000
J05	0.18	13,000	63.51	66,000
J06	0.18	13,000	63.67	66,000
J07	0.27	13,000	63.90	66,000
J08	0.27	13,000	63.84	67,000
J09	0.27	13,000	63.43	67,000
J10	0.27	13,000	63.80	69,000
J11	0.27	13,000	63.82	70,000
J12	0.27	13,000	64.10	77,000
J15	0.18	13,000	62.64	57,000
J158	0.00	13,000	55.77	30,000
J16	0.18	13,000	62.38	53,000
J17	0.18	13,000	61.73	50,000
J178	0.20	13,000	56.67	32,000
J18	0.18	13,000	61.09	47,000
J180	0.20	13,000	56.03	30,000
J182	0.20	13,000	55.76	30,000
J184	0.20	13,000	55.74	30,000
J186	0.20	13,000	57.40	34,000
J19	0.25	13,000	60.43	45,000
J20	0.25	13,000	60.54	43,000
J21	0.25	13,000	60.00	41,000
J22	0.25	13,000	59.71	40,000
J23	0.25	13,000	59.24	38,000
J24	0.25	13,000	58.69	36,000
J25	0.25	13,000	58.20	35,000
J26	0.25	13,000	58.23	35,000
J27	0.25	13,000	58.56	36,000
J28	0.25	13,000	58.36	35,000
J29	0.25	13,000	58.48	35,000
J30	0.18	13,000	58.80	36,000
J31	0.18	13,000	58.97	37,000
J32	0.18	13,000	59.19	38,000
J33	0.18	13,000	60.05	40,000
J34	0.18	13,000	60.97	44,000
J35	0.18	13,000	61.29	46,000
J36	0.18	13,000	62.20	50,000
J37	0.20	13,000	58.89	38,000
J38	0.20	13,000	58.40	36,000
J39	0.20	13,000	57.92	35,000
J40	0.27	13,000	64.02	75,000
J46	0.27	13,000	63.96	73,000
J48	0.27	13,000	63.86	71,000
J75	0.25	13,000	50.42	24,000
J76	0.25	13,000	54.96	29,000
J77	0.25	13,000	49.81	24,000
J78	0.18	13,000	55.46	30,000
J79	0.18	13,000	51.89	25,000
J94	0.20	13,000	56.32	31,000
J95	0.20	13,000	56.85	30,000
J96	0.20	13,000	55.88	30,000
J97	0.20	13,000	47.48	22,000
J98	0.00	13,000	55.62	30,000

Option B - 3 Connections - Phase 2 (2A, 2B, 2C)				
Junction ID	Base Demand (MXDY, L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)
J01	0.18	13,000	61.23	28,000
J02	0.00	13,000	51.51	28,000
J05	0.18	13,000	51.87	28,000
J06	0.18	13,000	52.01	28,000
J07	0.27	13,000	52.34	28,000
J08	0.27	13,000	52.46	28,000
J09	0.27	13,000	52.27	28,000
J10	0.27	13,000	52.97	29,000
J11	0.27	13,000	53.36	30,000
J12	0.27	13,000	54.89	32,000
J15	0.18	13,000	49.27	25,000
J158	0.00	13,000	33.14	16,000
J16	0.18	13,000	48.40	24,000
J17	0.18	13,000	46.84	23,000
J178	0.20	13,000	33.01	18,000
J18	0.18	13,000	45.74	22,000
J180	0.20	13,000	32.83	16,000
J182	0.20	13,000	32.86	16,000
J184	0.20	13,000	33.00	16,000
J186	0.20	13,000	33.32	16,000
J19	0.25	13,000	44.33	21,000
J20	0.25	13,000	44.19	21,000
J21	0.25	13,000	43.19	20,000
J22	0.25	13,000	42.93	20,000
J23	0.25	13,000	43.28	20,000
J24	0.25	13,000	43.20	20,000
J25	0.25	13,000	43.14	20,000
J26	0.25	13,000	43.53	21,000
J27	0.25	13,000	44.21	21,000
J28	0.25	13,000	44.36	21,000
J29	0.25	13,000	44.80	21,000
J30	0.18	13,000	45.41	22,000
J31	0.18	13,000	45.83	22,000
J32	0.18	13,000	46.25	22,000
J33	0.18	13,000	47.30	23,000
J34	0.18	13,000	48.53	24,000
J35	0.18	13,000	49.22	25,000
J36	0.18	13,000	50.43	26,000
J37	0.20	13,000	39.38	19,000
J38	0.20	13,000	36.58	17,000
J39	0.20	13,000	34.87	17,000
J40	0.27	13,000	54.54	32,000
J46	0.27	13,000	54.12	31,000
J48	0.27	13,000	53.63	30,000
J75	0.25	13,000	35.45	17,000
J76	0.25	13,000	40.42	19,000
J77	0.25	13,000	35.92	17,000
J78	0.18	13,000	42.00	20,000
J79	0.18	13,000	38.99	18,000
J94	0.20	13,000	34.35	17,000
J95	0.20	13,000	33.61	16,000
J96	0.20	13,000	33.46	16,000
J97	0.20	13,000	24.84	14,000
J98	0.00	13,000	33.06	16,000

Option A - 2 Connections with Upgrades on Danson Gardens Grv - Break Scenario 4					Option A - 2 Connections - Break Scenario 4					Option B - 3 Connections - Break Scenario 4				
Junction ID	Base Demand (AVDY; L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)	Junction ID	Base Demand (AVDY; L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)	Junction ID	Base Demand (AVDY; L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)
J01	0.07	13,000	58.88	84,000	J01	0.07	13,000	62.42	67,000	J01	0.07	13,000	54.45	34,000
J02	0.00	13,000	59.33	84,000	J02	0.00	13,000	62.99	66,000	J02	0.00	13,000	55.26	35,000
J05	0.07	13,000	59.72	84,000	J05	0.07	13,000	63.49	66,000	J05	0.07	13,000	56.09	37,000
J06	0.07	13,000	59.80	84,000	J06	0.07	13,000	63.65	66,000	J06	0.07	13,000	56.32	37,000
J07	0.11	13,000	59.91	84,000	J07	0.11	13,000	63.88	67,000	J07	0.11	13,000	55.84	36,000
J08	0.11	13,000	59.74	84,000	J08	0.11	13,000	63.84	67,000	J08	0.11	13,000	55.29	35,000
J09	0.11	13,000	59.21	85,000	J09	0.11	13,000	63.41	68,000	J09	0.11	13,000	54.56	34,000
J10	0.11	13,000	58.45	85,000	J10	0.11	13,000	63.78	69,000	J10	0.11	13,000	54.64	34,000
J100	0.15	13,000	48.98	26,000	J100	0.15	13,000	52.80	27,000	J100	0.15	13,000	46.57	23,000
J101	0.15	13,000	54.27	35,000	J101	0.15	13,000	58.09	36,000	J101	0.15	13,000	51.83	29,000
J102	0.15	13,000	53.96	34,000	J102	0.15	13,000	57.99	35,000	J102	0.15	13,000	51.53	29,000
J103	0.15	13,000	48.46	25,000	J103	0.15	13,000	52.28	26,000	J103	0.15	13,000	45.99	23,000
J109	0.11	13,000	45.11	22,000	J109	0.11	13,000	48.94	23,000	J109	0.11	13,000	42.65	20,000
J11	0.11	13,000	59.34	67,000	J11	0.11	13,000	63.80	71,000	J11	0.11	13,000	54.48	34,000
J110	0.11	13,000	42.73	21,000	J110	0.11	13,000	46.55	22,000	J110	0.11	13,000	40.28	18,000
J111	0.11	13,000	38.74	19,000	J111	0.11	13,000	42.36	19,000	J111	0.11	13,000	36.28	17,000
J112	0.11	13,000	33.38	17,000	J112	0.11	13,000	37.21	17,000	J112	0.11	13,000	30.46	16,000
J113	0.11	13,000	25.38	15,000	J113	0.11	13,000	29.20	15,000	J113	0.11	13,000	22.27	14,000
J114	0.11	13,000	24.19	14,000	J114	0.11	13,000	28.02	15,000	J114	0.11	13,000	21.00	14,000
J115	0.11	13,000	25.76	15,000	J115	0.11	13,000	30.59	16,000	J115	0.11	13,000	23.48	14,000
J116	0.11	13,000	29.56	16,000	J116	0.11	13,000	33.39	16,000	J116	0.11	13,000	26.19	15,000
J117	0.11	13,000	27.87	15,000	J117	0.11	13,000	31.69	16,000	J117	0.11	13,000	24.55	14,000
J118	0.11	13,000	32.38	16,000	J118	0.11	13,000	36.20	17,000	J118	0.11	13,000	22.11	15,000
J119	0.11	13,000	33.73	17,000	J119	0.11	13,000	37.55	17,000	J119	0.11	13,000	30.06	16,000
J12	0.11	13,000	59.27	73,000	J12	0.11	13,000	64.08	77,000	J12	0.11	13,000	54.69	36,000
J120	0.11	13,000	32.38	16,000	J120	0.11	13,000	36.21	17,000	J120	0.11	13,000	28.68	15,000
J121	0.11	13,000	29.65	15,000	J121	0.11	13,000	33.61	16,000	J121	0.11	13,000	26.82	15,000
J122	0.11	13,000	23.34	14,000	J122	0.11	13,000	27.17	15,000	J122	0.11	13,000	19.60	13,000
J123	0.11	13,000	23.56	14,000	J123	0.11	13,000	27.38	15,000	J123	0.11	13,000	19.60	13,000
J124	0.11	13,000	30.36	16,000	J124	0.11	13,000	34.18	16,000	J124	0.11	13,000	26.00	15,000
J125	0.11	13,000	27.43	15,000	J125	0.11	13,000	31.25	16,000	J125	0.11	13,000	23.52	14,000
J128	0.00	6,000	53.07	12,000	J128	0.00	6,000	55.10	13,000	J128	0.00	6,000	51.18	12,000
J129	0.11	13,000	20.88	14,000	J129	0.11	13,000	24.70	14,000	J129	0.11	13,000	18.33	13,000
J130	0.11	13,000	24.37	14,000	J130	0.11	13,000	28.19	15,000	J130	0.11	13,000	21.86	14,000
J131	0.11	13,000	14.07	14,000	J131	0.11	13,000	14.90	14,000	J131	0.11	13,000	18.46	13,000
J132	0.11	13,000	24.67	14,000	J132	0.11	13,000	28.49	15,000	J132	0.11	13,000	21.92	14,000
J133	0.11	13,000	26.02	15,000	J133	0.11	13,000	29.84	15,000	J133	0.11	13,000	21.87	14,000
J134	0.11	13,000	22.97	14,000	J134	0.11	13,000	26.80	15,000	J134	0.11	13,000	18.78	14,000
J135	0.11	13,000	23.47	14,000	J135	0.11	13,000	27.29	15,000	J135	0.11	13,000	19.20	13,000
J136	0.11	13,000	25.46	15,000	J136	0.11	13,000	29.29	15,000	J136	0.11	13,000	21.11	14,000
J137	0.11	6,000	34.45	8,000	J137	0.11	6,000	36.49	8,000	J137	0.11	6,000	32.18	7,000
J14	0.11	6,000	52.07	12,000	J14	0.11	6,000	54.11	13,000	J14	0.11	6,000	48.60	12,000
J15	0.07	13,000	58.83	55,000	J15	0.07	13,000	62.63	57,000	J15	0.07	13,000	54.36	33,000
J152	0.11	13,000	54.93	34,000	J152	0.11	13,000	58.85	36,000	J152	0.11	13,000	51.24	27,000
J153	0.15	13,000	54.09	34,000	J153	0.15	13,000	57.91	36,000	J153	0.15	13,000	51.14	28,000
J154	0.11	13,000	56.19	36,000	J154	0.11	13,000	59.24	38,000	J154	0.11	13,000	53.63	30,000
J155	0.11	13,000	36.45	18,000	J155	0.11	13,000	40.28	18,000	J155	0.11	13,000	31.48	16,000
J156	0.00	13,000	35.33	17,000	J156	0.00	13,000	39.16	18,000	J156	0.00	13,000	27.90	15,000
J158	0.00	13,000	53.43	31,000	J158	0.00	13,000	57.25	33,000	J158	0.00	13,000	52.94	30,000
J16	0.07	13,000	48.57	43,000	J16	0.07	13,000	50.38	44,000	J16	0.07	13,000	44.23	32,000
J162	0.00	13,000	47.64	24,000	J162	0.00	13,000	51.47	25,000	J162	0.00	13,000	45.18	22,000
J164	0.00	13,000	44.56	22,000	J164	0.00	13,000	48.39	23,000	J164	0.00	13,000	42.10	20,000
J166	0.00	13,000	39.45	19,000	J166	0.00	13,000	43.28	20,000	J166	0.00	13,000	36.99	18,000
J168	0.00	13,000	40.33	18,000	J168	0.00	13,000	44.16	19,000	J168	0.00	13,000	38.07	17,000
J17	0.07	13,000	57.93	48,000	J17	0.07	13,000	61.74	50,000	J17	0.07	13,000	53.59	31,000
J170	0.00	13,000	30.96	16,000	J170	0.00	13,000	34.79	17,000	J170	0.00	13,000	28.50	15,000
J172	0.00	13,000	50.22	27,000	J172	0.00	13,000	54.05	28,000	J172	0.00	13,000	47.76	24,000
J174	0.15	13,000	53.56	33,000	J174	0.15	13,000	57.39	34,000	J174	0.15	13,000	51.10	28,000
J176	0.15	13,000	53.99	33,000	J176	0.15	13,000	57.81	35,000	J176	0.15	13,000	51.44	28,000
J178	0.08	13,000	54.49	34,000	J178	0.08	13,000	58.31	36,000	J178	0.08	13,000	52.27	29,000
J18	0.07	13,000	57.30	46,000	J18	0.07	13,000	61.12	48,000	J18	0.07	13,000	53.59	32,000
J180	0.08	13,000	53.78	37,000	J180	0.08	13,000	57.50	39,000	J180	0.08	13,000	51.60	29,000
J182	0.08	13,000	53.46	31,000	J182	0.08	13,000	57.28	33,000	J182	0.08	13,000	52.81	29,000
J184	0.08	13,000	53.42	31,000	J184	0.08	13,000	57.25	32,000	J184	0.08	13,000	53.30	30,000
J186	0.08	13,000	55.31	37,000	J186	0.08	13,000	59.13	38,000	J186	0.08	13,000	53.44	30,000
J188	0.00	13,000	46.02	23,000	J188	0.00	13,000	49.85	24,000	J188	0.00	13,000	43.56	21,000
J19	0.10	13,000	56.72	44,000	J19	0.10	13,000	60.54	45,000	J19	0.10	13,000	52.46	30,000
J20	0.10	13,000	57.02	43,000	J20	0.10	13,000	60.84	45,000	J20	0.10	13,000	53.25	31,000
J21	0.10	13,000	56.61	42,000	J21	0.10	13,000	60.44	44,000	J21	0.10	13,000	52.95	30,000
J22	0.10	13,000	56.53	41,000	J22	0.10	13,000	60.35	43,000	J22	0.10	13,000	53.43	31,000
J23	0.10	13,000	55.93	39,000	J23	0.10	13,000	59.75	40,000	J23	0.10	13,000	52.96	30,000
J24	0.10	13,000	55.37	36,000	J24	0.10	13,000	59.20	38,000	J24	0.10	13,000	52.45	29,000
J25	0.10	13,000	54.97	35,000	J25	0.10	13,000	58.79	37,000	J25	0.10	13,000	51.27	28,000
J26	0.10	13,000	55.00	35,000	J26	0.10	13,000	58.82	37,000	J26	0.10	13,000	52.12	29,000
J27	0.10	13,000	55.29	36,000	J27	0.10	13,000	59.11	37,000	J27	0.10	13,000	52.22	29,000
J28	0.10	13,000	55.12	35,000	J28	0.10	13,000	58.95	37,000	J28	0.10	13,000	52.26	29,000
J29	0.10	13,000	55.25	36,000	J29	0.10	13,000	59.07	37,000	J29	0.10	13,000	52.38	29,000
J30	0.07	13,000	55.60	37,000	J30	0.07	13,000	59.43	39,000	J30	0.07	13,000	52.72	30,000
J31	0.07	13,000	55.84	37,000	J31	0.07	13,000	59.67	39,000	J31	0.07	13,000	52.95	30,000
J32														

Option A - 2 Connections with Upgrades on Danson Gardens Grv - Break Scenario 5					Option A - 2 Connections - Break Scenario 5					Option B - 3 Connections - Break Scenario 5				
Junction ID	Base Demand (AVDY, L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)	Junction ID	Base Demand (AVDY, L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)	Junction ID	Base Demand (AVDY, L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)
J01	0.07	13.000	58.88	64.000	J01	0.07	13.000	62.42	67.000	J01	0.07	13.000	54.31	34.000
J02	0.00	13.000	59.33	64.000	J02	0.00	13.000	62.99	66.000	J02	0.00	13.000	55.09	35.000
J05	0.07	13.000	59.72	64.000	J05	0.07	13.000	63.49	66.000	J05	0.07	13.000	55.90	37.000
J06	0.07	13.000	59.80	64.000	J06	0.07	13.000	63.65	66.000	J06	0.07	13.000	56.82	37.000
J07	0.11	13.000	59.91	64.000	J07	0.11	13.000	63.88	67.000	J07	0.11	13.000	55.68	36.000
J08	0.11	13.000	59.74	64.000	J08	0.11	13.000	63.84	67.000	J08	0.11	13.000	55.15	35.000
J09	0.11	13.000	59.21	65.000	J09	0.11	13.000	63.41	68.000	J09	0.11	13.000	54.43	34.000
J10	0.11	13.000	59.45	66.000	J10	0.11	13.000	63.78	69.000	J10	0.11	13.000	54.83	34.000
J100	0.15	13.000	49.00	26.000	J100	0.15	13.000	52.83	27.000	J100	0.15	13.000	46.25	23.000
J101	0.15	13.000	54.39	35.000	J101	0.15	13.000	58.21	36.000	J101	0.15	13.000	51.70	29.000
J102	0.15	13.000	54.18	35.000	J102	0.15	13.000	58.00	36.000	J102	0.15	13.000	51.58	29.000
J103	0.15	13.000	48.71	25.000	J103	0.15	13.000	52.29	26.000	J103	0.15	13.000	45.80	23.000
J109	0.11	13.000	52.53	31.000	J109	0.11	13.000	56.38	32.000	J109	0.11	13.000	49.58	28.000
J11	0.11	13.000	59.34	67.000	J11	0.11	13.000	63.80	71.000	J11	0.11	13.000	54.38	34.000
J110	0.11	13.000	52.86	31.000	J110	0.11	13.000	56.68	32.000	J110	0.11	13.000	49.72	26.000
J111	0.11	13.000	53.86	33.000	J111	0.11	13.000	57.68	34.000	J111	0.11	13.000	50.27	26.000
J112	0.11	13.000	49.40	26.000	J112	0.11	13.000	53.22	27.000	J112	0.11	13.000	45.11	22.000
J113	0.11	13.000	41.55	20.000	J113	0.11	13.000	45.37	21.000	J113	0.11	13.000	37.03	18.000
J114	0.11	13.000	46.43	19.000	J114	0.11	13.000	46.26	20.000	J114	0.11	13.000	38.89	17.000
J115	0.11	13.000	43.06	21.000	J115	0.11	13.000	46.89	22.000	J115	0.11	13.000	38.32	18.000
J116	0.11	13.000	45.92	23.000	J116	0.11	13.000	48.74	24.000	J116	0.11	13.000	41.07	20.000
J117	0.11	13.000	44.19	21.000	J117	0.11	13.000	48.01	22.000	J117	0.11	13.000	39.41	19.000
J118	0.11	13.000	48.67	25.000	J118	0.11	13.000	52.49	26.000	J118	0.11	13.000	43.95	21.000
J119	0.11	13.000	50.32	27.000	J119	0.11	13.000	54.14	28.000	J119	0.11	13.000	45.10	22.000
J12	0.11	13.000	59.27	73.000	J12	0.11	13.000	64.08	77.000	J12	0.11	13.000	54.62	35.000
J120	0.11	13.000	48.96	25.000	J120	0.11	13.000	52.78	26.000	J120	0.11	13.000	43.71	21.000
J121	0.11	13.000	46.13	23.000	J121	0.11	13.000	49.86	24.000	J121	0.11	13.000	41.03	20.000
J122	0.11	13.000	39.90	19.000	J122	0.11	13.000	43.73	20.000	J122	0.11	13.000	34.22	17.000
J123	0.11	13.000	40.20	19.000	J123	0.11	13.000	44.03	20.000	J123	0.11	13.000	34.67	17.000
J124	0.11	13.000	47.14	24.000	J124	0.11	13.000	50.96	25.000	J124	0.11	13.000	41.15	20.000
J125	0.11	13.000	44.07	21.000	J125	0.11	13.000	47.92	22.000	J125	0.11	13.000	38.69	18.000
J128	0.00	6.000	57.00	16.000	J128	0.00	6.000	59.04	17.000	J128	0.00	6.000	54.73	15.000
J129	0.11	13.000	38.32	18.000	J129	0.11	13.000	42.15	19.000	J129	0.11	13.000	34.28	17.000
J130	0.11	13.000	41.82	20.000	J130	0.11	13.000	45.85	21.000	J130	0.11	13.000	37.86	18.000
J131	0.11	13.000	38.50	18.000	J131	0.11	13.000	42.32	19.000	J131	0.11	13.000	35.63	17.000
J132	0.11	13.000	42.07	20.000	J132	0.11	13.000	45.89	21.000	J132	0.11	13.000	37.76	18.000
J133	0.11	13.000	43.21	21.000	J133	0.11	13.000	47.04	22.000	J133	0.11	13.000	37.27	18.000
J134	0.11	13.000	48.16	19.000	J134	0.11	13.000	43.99	20.000	J134	0.11	13.000	34.21	17.000
J135	0.11	13.000	40.85	19.000	J135	0.11	13.000	44.47	20.000	J135	0.11	13.000	34.57	17.000
J136	0.11	13.000	42.64	20.000	J136	0.11	13.000	46.47	21.000	J136	0.11	13.000	36.47	17.000
J137	0.11	6.000	38.33	8.000	J137	0.11	6.000	40.38	8.000	J137	0.11	6.000	35.60	8.000
J14	0.11	6.000	15.95	6.000	J14	0.11	6.000	15.95	6.000	J14	0.11	6.000	53.23	14.000
J15	0.07	13.000	58.83	55.000	J15	0.07	13.000	62.83	57.000	J15	0.07	13.000	54.15	32.000
J152	0.11	13.000	54.93	34.000	J152	0.11	13.000	58.85	36.000	J152	0.11	13.000	51.06	27.000
J153	0.15	13.000	54.10	34.000	J153	0.15	13.000	57.92	36.000	J153	0.15	13.000	50.88	28.000
J154	0.11	13.000	53.89	33.000	J154	0.11	13.000	57.44	34.000	J154	0.11	13.000	49.75	26.000
J155	0.11	13.000	53.60	32.000	J155	0.11	13.000	57.43	33.000	J155	0.11	13.000	46.80	23.000
J156	0.00	13.000	52.45	30.000	J156	0.00	13.000	56.27	31.000	J156	0.00	13.000	43.18	21.000
J158	0.00	13.000	46.54	23.000	J158	0.00	13.000	50.38	24.000	J158	0.00	13.000	43.48	21.000
J16	0.07	13.000	58.67	62.000	J16	0.07	13.000	64.38	66.000	J16	0.07	13.000	53.97	32.000
J162	0.00	13.000	52.56	31.000	J162	0.00	13.000	56.38	32.000	J162	0.00	13.000	49.74	26.000
J164	0.00	13.000	51.01	28.000	J164	0.00	13.000	54.83	29.000	J164	0.00	13.000	48.11	24.000
J166	0.00	13.000	45.90	23.000	J166	0.00	13.000	49.73	24.000	J166	0.00	13.000	43.00	21.000
J168	0.00	13.000	42.78	21.000	J168	0.00	13.000	46.61	22.000	J168	0.00	13.000	40.85	19.000
J17	0.07	13.000	57.93	48.000	J17	0.07	13.000	61.74	50.000	J17	0.07	13.000	53.34	21.000
J170	0.00	13.000	37.41	18.000	J170	0.00	13.000	41.24	19.000	J170	0.00	13.000	34.51	17.000
J172	0.00	13.000	52.99	32.000	J172	0.00	13.000	56.81	33.000	J172	0.00	13.000	50.29	27.000
J174	0.15	13.000	54.21	34.000	J174	0.15	13.000	60.05	36.000	J174	0.15	13.000	51.64	28.000
J176	0.15	13.000	54.08	34.000	J176	0.15	13.000	57.91	35.000	J176	0.15	13.000	51.52	28.000
J178	0.08	13.000	53.48	32.000	J178	0.08	13.000	57.30	33.000	J178	0.08	13.000	52.30	29.000
J18	0.07	13.000	57.30	46.000	J18	0.07	13.000	61.12	48.000	J18	0.07	13.000	53.31	31.000
J180	0.08	13.000	50.19	27.000	J180	0.08	13.000	53.88	28.000	J180	0.08	13.000	47.85	28.000
J182	0.08	13.000	49.76	27.000	J182	0.08	13.000	51.79	28.000	J182	0.08	13.000	51.62	28.000
J184	0.08	13.000	46.35	23.000	J184	0.08	13.000	50.17	24.000	J184	0.08	13.000	51.46	27.000
J186	0.08	13.000	55.18	36.000	J186	0.08	13.000	59.00	38.000	J186	0.08	13.000	50.99	30.000
J188	0.00	13.000	52.47	31.000	J188	0.00	13.000	56.30	32.000	J188	0.00	13.000	49.57	26.000
J19	0.10	13.000	56.72	44.000	J19	0.10	13.000	60.54	45.000	J19	0.10	13.000	52.16	30.000
J20	0.10	13.000	57.02	43.000	J20	0.10	13.000	60.84	45.000	J20	0.10	13.000	52.93	30.000
J21	0.10	13.000	56.81	42.000	J21	0.10	13.000	60.44	44.000	J21	0.10	13.000	52.03	28.000
J22	0.10	13.000	56.53	41.000	J22	0.10	13.000	60.38	43.000	J22	0.10	13.000	53.06	31.000
J23	0.10	13.000	55.93	39.000	J23	0.10	13.000	59.75	40.000	J23	0.10	13.000	52.62	30.000
J24	0.10	13.000	55.37	36.000	J24	0.10	13.000	59.20	38.000	J24	0.10	13.000	51.13	29.000
J25	0.10	13.000	54.97	35.000	J25	0.10	13.000	58.79	37.000	J25	0.10	13.000	51.75	28.000
J26	0.10	13.000	55.00	35.000	J26	0.10	13.000	58.82	37.000	J26	0.10	13.000	51.23	28.000
J27	0.10	13.000	55.29	36.000	J27	0.10	13.000	59.11	37.000	J27	0.10	13.000	52.18	29.000
J28	0.10	13.000	55.12	35.000	J28	0.10	13.000	58.95	37.000	J28	0.10	13.000	51.98	28.000
J29	0.10	13.000	55.26	36.000	J29	0.10	13.000	59.07	37.000	J29	0.10	13.000	52.13	29.000
J30	0.07	13.000	55.60	37.000	J30	0.07	13.000	59.43	39.000	J30	0.07	13.000	52.46	29.000
J31	0.07	13.000	55.84	37.000	J31	0.07	13.000	59.67	39.000	J31	0.07	13.000	52.69	29.000
J32	0.07	13.000	56.17	39.000	J32	0.07	13.000	60.00						

Option A - 2 Connections with Upgrades on Danson Gardens Grv - Break Scenario 6					Option A - 2 Connections - Break Scenario 6					Option B - 3 Connections - Break Scenario 6				
Junction ID	Base Demand (AVD/Y, L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)	Junction ID	Base Demand (AVD/Y, L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)	Junction ID	Base Demand (AVD/Y, L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)
J01	0.07	13.000	58.88	64.000	J01	0.07	13.000	62.42	67.000	J01	0.07	13.000	54.45	34.000
J02	0.00	13.000	59.33	64.000	J02	0.00	13.000	62.99	66.000	J02	0.00	13.000	55.26	35.000
J05	0.07	13.000	59.72	64.000	J05	0.07	13.000	63.49	66.000	J05	0.07	13.000	56.09	37.000
J06	0.07	13.000	59.80	64.000	J06	0.07	13.000	63.65	66.000	J06	0.07	13.000	56.32	37.000
J07	0.11	13.000	59.91	64.000	J07	0.11	13.000	63.88	67.000	J07	0.11	13.000	55.85	36.000
J08	0.11	13.000	59.74	64.000	J08	0.11	13.000	63.84	67.000	J08	0.11	13.000	55.29	35.000
J09	0.11	13.000	59.21	65.000	J09	0.11	13.000	63.41	68.000	J09	0.11	13.000	54.56	34.000
J10	0.11	13.000	59.45	65.000	J10	0.11	13.000	63.78	69.000	J10	0.11	13.000	54.64	34.000
J100	0.15	13.000	48.99	26.000	J100	0.15	13.000	52.81	27.000	J100	0.15	13.000	46.58	23.000
J101	0.15	13.000	54.29	35.000	J101	0.15	13.000	58.11	36.000	J101	0.15	13.000	51.85	29.000
J102	0.15	13.000	53.99	34.000	J102	0.15	13.000	57.81	35.000	J102	0.15	13.000	51.56	29.000
J103	0.15	13.000	48.47	25.000	J103	0.15	13.000	52.29	26.000	J103	0.15	13.000	46.00	23.000
J109	0.11	13.000	46.16	23.000	J109	0.11	13.000	49.99	24.000	J109	0.11	13.000	40.28	19.000
J11	0.11	13.000	59.34	67.000	J11	0.11	13.000	63.80	71.000	J11	0.11	13.000	54.48	34.000
J110	0.11	13.000	48.81	25.000	J110	0.11	13.000	52.64	26.000	J110	0.11	13.000	42.23	20.000
J111	0.11	13.000	52.84	31.000	J111	0.11	13.000	56.66	32.000	J111	0.11	13.000	46.95	23.000
J112	0.11	13.000	48.94	25.000	J112	0.11	13.000	52.77	27.000	J112	0.11	13.000	42.54	20.000
J113	0.11	13.000	41.16	20.000	J113	0.11	13.000	44.98	21.000	J113	0.11	13.000	34.55	17.000
J114	0.11	13.000	40.08	19.000	J114	0.11	13.000	43.96	20.000	J114	0.11	13.000	33.85	17.000
J115	0.11	13.000	42.73	21.000	J115	0.11	13.000	46.55	22.000	J115	0.11	13.000	35.90	17.000
J116	0.11	13.000	45.60	23.000	J116	0.11	13.000	49.42	24.000	J116	0.11	13.000	38.68	18.000
J117	0.11	13.000	43.86	21.000	J117	0.11	13.000	47.58	22.000	J117	0.11	13.000	37.01	18.000
J118	0.11	13.000	45.33	25.000	J118	0.11	13.000	49.15	26.000	J118	0.11	13.000	41.54	20.000
J119	0.11	13.000	50.06	27.000	J119	0.11	13.000	53.88	28.000	J119	0.11	13.000	42.79	20.000
J12	0.11	13.000	59.27	73.000	J12	0.11	13.000	64.08	77.000	J12	0.11	13.000	54.69	36.000
J120	0.11	13.000	48.70	25.000	J120	0.11	13.000	52.52	26.000	J120	0.11	13.000	41.40	20.000
J121	0.11	13.000	45.85	23.000	J121	0.11	13.000	49.68	24.000	J121	0.11	13.000	38.65	18.000
J122	0.11	13.000	39.64	19.000	J122	0.11	13.000	43.46	20.000	J122	0.11	13.000	32.29	16.000
J123	0.11	13.000	39.96	19.000	J123	0.11	13.000	43.78	20.000	J123	0.11	13.000	32.37	16.000
J124	0.11	13.000	46.92	23.000	J124	0.11	13.000	50.74	24.000	J124	0.11	13.000	38.88	18.000
J125	0.11	13.000	43.83	21.000	J125	0.11	13.000	47.65	22.000	J125	0.11	13.000	37.22	17.000
J128	0.00	6.000	56.96	16.000	J128	0.00	6.000	59.00	16.000	J128	0.00	6.000	54.32	14.000
J129	0.11	13.000	38.15	18.000	J129	0.11	13.000	41.98	19.000	J129	0.11	13.000	32.15	15.000
J130	0.11	13.000	41.66	20.000	J130	0.11	13.000	45.48	21.000	J130	0.11	13.000	35.74	17.000
J131	0.11	13.000	38.31	18.000	J131	0.11	13.000	42.15	19.000	J131	0.11	13.000	32.21	16.000
J132	0.11	13.000	41.89	20.000	J132	0.11	13.000	45.72	21.000	J132	0.11	13.000	35.11	17.000
J133	0.11	13.000	43.03	21.000	J133	0.11	13.000	46.85	21.000	J133	0.11	13.000	35.06	17.000
J134	0.11	13.000	39.98	19.000	J134	0.11	13.000	43.80	20.000	J134	0.11	13.000	31.96	16.000
J135	0.11	13.000	46.47	19.000	J135	0.11	13.000	44.28	20.000	J135	0.11	13.000	32.48	16.000
J136	0.11	13.000	42.46	20.000	J136	0.11	13.000	46.28	21.000	J136	0.11	13.000	34.26	17.000
J137	0.11	6.000	38.28	8.000	J137	0.11	6.000	40.32	8.000	J137	0.11	6.000	35.18	8.000
J14	0.11	15.000	55.81	61.000	J14	0.11	15.000	57.95	61.000	J14	0.11	15.000	52.63	13.000
J15	0.07	13.000	58.83	55.000	J15	0.07	13.000	62.83	57.000	J15	0.07	13.000	54.36	33.000
J152	0.11	13.000	54.93	34.000	J152	0.11	13.000	58.85	36.000	J152	0.11	13.000	51.24	27.000
J153	0.15	13.000	54.09	34.000	J153	0.15	13.000	57.91	36.000	J153	0.15	13.000	51.15	28.000
J154	0.11	13.000	53.70	32.000	J154	0.11	13.000	57.64	34.000	J154	0.11	13.000	45.74	22.000
J155	0.11	13.000	54.22	32.000	J155	0.11	13.000	57.24	33.000	J155	0.11	13.000	44.58	21.000
J156	0.00	13.000	52.26	30.000	J156	0.00	13.000	56.08	31.000	J156	0.00	13.000	40.94	19.000
J158	0.00	13.000	53.42	31.000	J158	0.00	13.000	57.25	32.000	J158	0.00	13.000	52.94	30.000
J159	0.07	13.000	48.57	25.000	J159	0.07	13.000	52.38	26.000	J159	0.07	13.000	45.23	22.000
J162	0.00	13.000	43.49	21.000	J162	0.00	13.000	47.31	22.000	J162	0.00	13.000	37.60	18.000
J164	0.00	13.000	43.67	21.000	J164	0.00	13.000	47.49	22.000	J164	0.00	13.000	37.79	18.000
J166	0.00	13.000	38.56	19.000	J166	0.00	13.000	42.39	19.000	J166	0.00	13.000	32.68	16.000
J168	0.00	13.000	32.44	17.000	J168	0.00	13.000	36.28	18.000	J168	0.00	13.000	25.85	15.000
J169	0.07	13.000	57.93	48.000	J169	0.07	13.000	61.74	50.000	J169	0.07	13.000	53.59	39.000
J170	0.00	13.000	30.07	16.000	J170	0.00	13.000	33.89	16.000	J170	0.00	13.000	24.19	14.000
J172	0.00	13.000	50.38	27.000	J172	0.00	13.000	54.20	29.000	J172	0.00	13.000	47.91	24.000
J174	0.15	13.000	53.82	33.000	J174	0.15	13.000	57.45	34.000	J174	0.15	13.000	51.15	28.000
J176	0.15	13.000	54.02	34.000	J176	0.15	13.000	57.84	35.000	J176	0.15	13.000	51.47	28.000
J178	0.08	13.000	54.48	34.000	J178	0.08	13.000	58.31	36.000	J178	0.08	13.000	52.26	29.000
J18	0.07	13.000	37.30	46.000	J18	0.07	13.000	41.12	48.000	J18	0.07	13.000	33.99	32.000
J180	0.08	13.000	53.78	37.000	J180	0.08	13.000	57.66	39.000	J180	0.08	13.000	52.28	29.000
J182	0.08	13.000	53.45	31.000	J182	0.08	13.000	57.28	33.000	J182	0.08	13.000	52.80	29.000
J184	0.08	13.000	53.42	31.000	J184	0.08	13.000	57.24	32.000	J184	0.08	13.000	53.30	30.000
J186	0.08	13.000	53.00	37.000	J186	0.08	13.000	56.12	38.000	J186	0.08	13.000	52.53	30.000
J188	0.00	13.000	45.13	22.000	J188	0.00	13.000	48.95	23.000	J188	0.00	13.000	40.35	19.000
J19	0.10	13.000	56.72	44.000	J19	0.10	13.000	60.54	45.000	J19	0.10	13.000	52.46	31.000
J20	0.10	13.000	57.02	43.000	J20	0.10	13.000	60.84	45.000	J20	0.10	13.000	53.25	30.000
J21	0.10	13.000	56.61	42.000	J21	0.10	13.000	60.44	44.000	J21	0.10	13.000	52.95	30.000
J22	0.10	13.000	56.53	41.000	J22	0.10	13.000	60.35	43.000	J22	0.10	13.000	53.43	31.000
J23	0.10	13.000	55.93	39.000	J23	0.10	13.000	59.75	40.000	J23	0.10	13.000	52.96	30.000
J24	0.10	13.000	55.37	36.000	J24	0.10	13.000	59.20	38.000	J24	0.10	13.000	52.45	29.000
J25	0.10	13.000	54.87	35.000	J25	0.10	13.000	58.75	37.000	J25	0.10	13.000	51.27	27.000
J26	0.10	13.000	55.00	35.000	J26	0.10	13.000	58.82	37.000	J26	0.10	13.000	52.12	29.000
J27	0.10	13.000	55.29	36.000	J27	0.10	13.000	59.11	37.000	J27	0.10	13.000	52.22	29.000
J28	0.10	13.000	55.12	35.000	J28	0.10	13.000	58.95	37.000	J28	0.10	13.000	52.26	29.000
J29	0.10	13.000	55.25	36.000	J29	0.10	13.000	59.07	37.000	J29	0.10	13.000	52.38	29.000
J30	0.07	13.000	55.60	37.000	J30	0.07	13.000	59.43	39.000	J30	0.07	13.000	52.73	30.000
J31	0.07	13.000	55.84	37.000	J31	0.07	13.000	59.67	39.000	J31	0.07	13.000	52.95	30.000
J32	0.07	13.000	56.17	39.000	J32	0.07	13.000							

Option B - 3 Connections - Break Scenario 7 (Connection 3 Break)				
Junction ID	Base Demand (AVDY; L/s)	Required Fire Flow (L/min)	Residual Pressure (psi)	Available Fire Flow at Residual 20 psi (L/min)
J01	0.07	13,000	50.75	28,000
J02	0.00	13,000	50.85	28,000
J05	0.07	13,000	51.07	28,000
J06	0.07	13,000	51.13	28,000
J07	0.11	13,000	51.35	28,000
J08	0.11	13,000	51.37	28,000
J09	0.11	13,000	51.02	28,000
J10	0.11	13,000	51.58	28,000
J100	0.15	13,000	35.85	17,000
J101	0.15	13,000	41.53	20,000
J102	0.15	13,000	40.97	20,000
J103	0.15	13,000	34.84	17,000
J109	0.11	13,000	38.31	18,000
J11	0.11	13,000	51.74	29,000
J110	0.11	13,000	38.43	18,000
J111	0.11	13,000	38.95	19,000
J112	0.11	13,000	33.79	17,000
J113	0.11	13,000	25.70	15,000
J114	0.11	13,000	24.48	14,000
J115	0.11	13,000	27.00	15,000
J116	0.11	13,000	29.75	16,000
J117	0.11	13,000	28.09	15,000
J118	0.11	13,000	32.53	16,000
J119	0.11	13,000	33.78	17,000
J12	0.11	13,000	52.90	32,000
J120	0.11	13,000	32.39	16,000
J121	0.11	13,000	29.71	16,000
J122	0.11	13,000	23.29	14,000
J123	0.11	13,000	23.35	14,000
J124	0.11	13,000	29.83	16,000
J125	0.11	13,000	27.27	15,000
J128	0.00	6,000	51.65	13,000
J129	0.11	13,000	22.95	14,000
J130	0.11	13,000	26.54	15,000
J131	0.11	13,000	23.03	14,000
J132	0.11	13,000	26.43	15,000
J133	0.11	13,000	25.95	15,000
J134	0.11	13,000	22.85	14,000
J135	0.11	13,000	23.25	14,000
J136	0.11	13,000	25.15	14,000
J137	0.11	6,000	32.53	7,000
J14	0.11	6,000	50.15	12,000
J15	0.07	13,000	49.53	25,000
J152	0.11	13,000	46.54	23,000
J153	0.15	13,000	42.30	20,000
J154	0.11	13,000	38.63	18,000
J155	0.11	13,000	35.48	17,000
J156	0.00	13,000	31.86	16,000
J158	0.00	13,000	39.85	19,000
J16	0.07	13,000	47.76	24,000
J162	0.00	13,000	38.51	19,000
J164	0.00	13,000	36.88	18,000
J166	0.00	13,000	31.75	16,000
J168	0.00	13,000	28.63	15,000
J17	0.07	13,000	46.35	23,000
J170	0.00	13,000	23.26	14,000
J172	0.00	13,000	39.11	19,000
J174	0.15	13,000	40.56	19,000
J176	0.15	13,000	40.26	19,000
J178	0.08	13,000	40.57	19,000
J18	0.07	13,000	45.44	22,000
J180	0.08	13,000	40.03	19,000
J182	0.08	13,000	39.80	19,000
J184	0.08	13,000	39.81	19,000
J186	0.08	13,000	41.19	20,000
J188	0.00	13,000	38.32	18,000
J19	0.10	13,000	43.99	21,000
J20	0.10	13,000	44.59	22,000
J21	0.10	13,000	43.81	21,000
J22	0.10	13,000	44.32	22,000
J23	0.10	13,000	44.26	21,000
J24	0.10	13,000	44.01	21,000
J25	0.10	13,000	43.82	21,000
J26	0.10	13,000	44.10	21,000
J27	0.10	13,000	44.59	22,000
J28	0.10	13,000	44.71	22,000
J29	0.10	13,000	45.04	22,000
J30	0.07	13,000	45.65	22,000
J31	0.07	13,000	46.08	23,000
J32	0.07	13,000	46.61	23,000
J33	0.07	13,000	47.37	24,000
J34	0.07	13,000	46.16	24,000
J35	0.07	13,000	48.80	25,000
J36	0.07	13,000	50.10	26,000
J37	0.08	13,000	43.11	21,000
J38	0.08	13,000	42.37	20,000
J39	0.08	13,000	41.67	20,000
J40	0.11	13,000	52.60	31,000
J41	0.11	13,000	40.06	19,000
J42	0.11	13,000	39.51	19,000
J43	0.11	13,000	37.87	18,000
J44	0.11	13,000	36.34	18,000
J45	0.11	13,000	33.18	17,000
J46	0.11	13,000	52.29	30,000
J48	0.11	13,000	51.93	30,000
J50	0.11	13,000	44.52	22,000
J51	0.11	13,000	44.20	21,000
J52	0.11	13,000	41.04	20,000
J53	0.11	13,000	40.35	19,000
J55	0.11	13,000	42.46	20,000
J56	0.11	13,000	37.12	18,000
J57	0.11	13,000	39.08	19,000
J58	0.11	13,000	37.63	18,000
J59	0.11	13,000	33.31	16,000
J60	0.11	13,000	29.37	15,000
J61	0.11	13,000	28.96	15,000
J62	0.11	13,000	33.01	16,000
J63	0.11	13,000	32.97	16,000
J64	0.11	13,000	29.49	15,000
J65	0.11	13,000	29.56	15,000
J66	0.11	13,000	33.75	17,000
J67	0.11	13,000	33.92	17,000
J68	0.11	13,000	29.43	15,000
J69	0.11	13,000	29.46	15,000
J70	0.11	13,000	32.92	16,000
J71	0.11	13,000	32.99	16,000
J72	0.11	13,000	29.36	15,000
J73	0.11	13,000	29.53	15,000
J74	0.11	13,000	32.78	16,000
J75	0.10	13,000	35.75	17,000
J76	0.10	13,000	40.43	19,000
J77	0.10	13,000	35.66	17,000
J78	0.07	13,000	41.59	20,000
J79	0.07	13,000	38.58	18,000
J80	0.15	13,000	31.52	16,000
J81	0.15	13,000	41.51	20,000
J82	0.15	13,000	41.49	20,000
J83	0.15	13,000	42.73	21,000
J84	0.15	13,000	43.17	21,000
J85	0.15	13,000	26.43	15,000
J86	0.15	13,000	22.78	14,000
J87	0.15	13,000	22.80	14,000
J88	0.15	13,000	26.90	15,000
J89	0.15	13,000	44.16	21,000
J90	0.15	13,000	35.62	17,000
J91	0.15	13,000	42.23	20,000
J92	0.15	13,000	31.56	16,000
J93	0.15	13,000	28.36	15,000
J94	0.08	13,000	40.36	19,000
J95	0.08	13,000	39.95	19,000
J96	0.08	13,000	39.97	19,000
J97	0.08	13,000	31.59	16,000
J98	0.00	13,000	38.70	19,000

**BARRHAVEN CONSERVANCY EAST (PHASES 2, 3, 4 & JOCK RIVER): WATER DISTRIBUTION
SYSTEM ANALYSIS**

June 2, 2022

Appendix E WATER AGE CALCULATIONS



163401660 - Barrhaven Conservancy

Water Age Assessment

Sizing Option A	Pipe Dimensions			Average Day Demand		Water Age		
	Pipe Diameter (mm)	Pipe Length (m)	Pipe Volume (m ³)	(L/s)	(m ³ /s)	(s)	(h)	(d)
2	406	2,609	337.81	3.50	0.004	96,464	26.80	1.12
2	305	1,442	105.38	3.50	0.004	30,091	8.36	0.35
2	203	742	24.00	3.50	0.004	6,853	1.90	0.08
2	152	305	5.54	3.50	0.004	1,581	0.44	0.02
2	Total		472.73	3.50	0.004	134,989	37.50	1.56
3	406	2,609	337.81	6.64	0.007	50,906	14.14	0.59
3	305	2,326	169.96	6.64	0.007	25,612	7.11	0.30
3	203	2,001	64.75	6.64	0.007	9,757	2.71	0.11
3	152	427	7.75	6.64	0.007	1,167	0.32	0.01
3	Total		580.27	6.64	0.007	87,442	24.29	1.01
4	406	2,977	385.42	10.30	0.010	37,402	10.39	0.43
4	305	2,982	217.89	10.30	0.010	21,145	5.87	0.24
4	203	3,747	121.28	10.30	0.010	11,769	3.27	0.14
4	152	474	8.60	10.30	0.010	835	0.23	0.01
4	Total		733.20	10.30	0.010	71,151	19.76	0.82
Ultimate	406	2,977	385.42	13.92	0.014	27,691	7.69	0.32
Ultimate	305	2,982	217.89	13.92	0.014	15,654	4.35	0.18
Ultimate	203	6,024	194.98	13.92	0.014	14,008	3.89	0.16
Ultimate	152	555	10.08	13.92	0.014	724	0.20	0.01
Ultimate	Total		808.38	13.92	0.014	58,078	16.13	0.67

Sizing Option B	Pipe Dimensions			Average Day Demand		Water Age		
	Pipe Diameter (mm)	Pipe Length (m)	Pipe Volume (m ³)	(L/s)	(m ³ /s)	(s)	(h)	(d)
2	406	0	0.00	3.50	0.004	0	0.00	0.00
2	305	3,933	287.37	3.50	0.004	82,059	22.79	0.95
2	203	742	24.00	3.50	0.004	6,853	1.90	0.08
2	152	305	5.54	3.50	0.004	1,581	0.44	0.02
2	Total		316.90	3.50	0.004	90,493	25.14	1.05
3	406	0	0.00	6.64	0.007	0	0.00	0.00
3	305	4,817	351.95	6.64	0.007	53,036	14.73	0.61
3	203	2,001	64.75	6.64	0.007	9,757	2.71	0.11
3	152	427	7.75	6.64	0.007	1,167	0.32	0.01
3	Total		424.45	6.64	0.007	63,960	17.77	0.74
4	406	0	0.00	10.30	0.010	0	0.00	0.00
4	305	5,841	426.75	10.30	0.010	41,413	11.50	0.48
4	203	3,747	121.28	10.30	0.010	11,769	3.27	0.14
4	152	474	8.60	10.30	0.010	835	0.23	0.01
4	Total		556.64	10.30	0.010	54,017	15.00	0.63
Ultimate	406	0	0.00	13.92	0.014	0	0.00	0.00
Ultimate	305	6,619	483.60	13.92	0.014	34,744	9.65	0.40
Ultimate	203	6,024	194.98	13.92	0.014	14,008	3.89	0.16
Ultimate	152	555	10.08	13.92	0.014	724	0.20	0.01
Ultimate	Total		688.66	13.92	0.014	49,477	13.74	0.57

**Kennedy-Burnett Potable
Water Master Servicing Study**



Prepared for:
City of Ottawa
100 Constellation Crescent
Ottawa, ON K2G 6G8

Prepared by:
Stantec Consulting Ltd.
400-1331 Clyde Avenue
Ottawa, ON K2C 3G4

File No. 1634-01221

April 29, 2014

KENNEDY-BURNETT POTABLE WATER MASTER SERVICING STUDY

Hydraulic Assessment
April 29, 2014

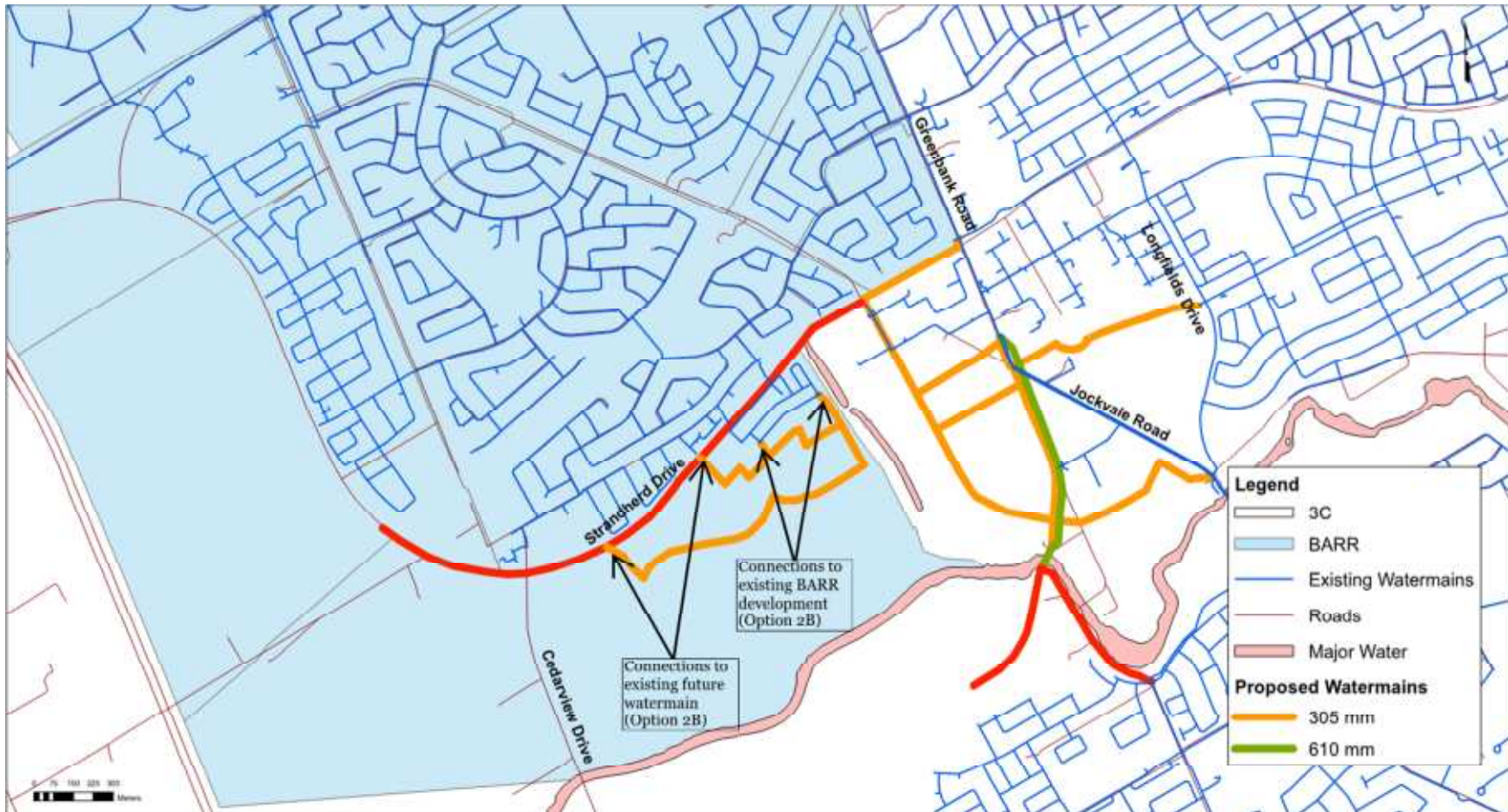


Figure 2-6: Proposed Pipe Layout Post Zone Reconfiguration – Scenario 2B

APPENDIX C

SANITARY

MEMORANDUM

DATE: MAY 30, 2019
TO: JOSÉE VALLEE – CITY OF OTTAWA
FROM: CONRAD STANG – NOVATECH
RE: STRANDHERD DRIVE WIDENING PROJECT
SOUTH NEPEAN COLLECTOR PHASE 3: SANITARY FLOW CALCULATIONS
CC: EDSON DONNELLY – NOVATECH

1.0 PURPOSE

This memorandum provides the sanitary sewer flow calculations and design sheet for Phase 3 of the proposed South Nepean Collector (SNC), as part of the Strandherd Drive Widening Project. Sanitary design flows have been estimated for both current-day operational flows and future development peak design flows. They are based on the latest available planning information for the vacant lands within the SNC sewershed.

2.0 BACKGROUND

In January 1998, the Master Servicing Study for the South Nepean Urban Area provided a conceptual plan for water, wastewater and stormwater infrastructure. The preferred alternative for wastewater servicing was an east/west trunk sewer alignment that was to be completed in several phases. The proposed sanitary trunk sewer was initially called the Jock River Collector, but was renamed the South Nepean Collector during the original functional design study completed in 2003.

Phase 1 of the South Nepean Collector was completed in 2005 and currently terminates at a 2400mm maintenance hole located east of Longfields Drive, north of Bren-Maur Road. Phase 2 was completed in 2016 and currently terminates at a 2400mm maintenance hole located at the intersection of Strandherd Drive and Fraser Fields Way.

Phase 3 will extend the trunk sewer along Strandherd Drive to the intersection of Kennevale Drive. Here it will connect with the existing sanitary trunk sewer that was constructed as part of the 2014 works to improve Strandherd Drive and develop the CitiGate Lands.

The sanitary sewer flows were previously documented in the *South Nepean Collector – Functional Design Report and Update* (Dillon, 2012). Novatech (2016) completed a *Hydraulics Review / Assessment* of the sanitary flows presented in the Dillon Report (attached). This was based on the latest planning information for the vacant lands within the SNC sewershed. The results of the *Hydraulics Review / Assessment* (Novatech, 2016) were similar to the results from the Dillon (2012) analysis.

3.0 DESIGN PARAMETERS AND POPULATION ESTIMATES

3.1 Design Parameters

The sanitary design flow were calculated using the parameters from the City of Ottawa Sewer Design Guidelines (October 2012), revised per Technical Bulletin ISTB-2018-01 (March 2018). These parameters are summarized in **Table 1** and **Table 2**.

Table 1: Peak Design Flow Parameters

Land Use	Average Daily Flow	Peaking Factor	Peak Extraneous Flows
Residential	280 L/cap/day	Harmon Equation, K=0.8 (1.6 min – 3.2 max)	0.33 L/s/ha
Commercial	28,000 L/ha/day	1.0 – 1.5*	
Institutional	28,000 L/ha/day	1.0 – 1.5*	
Other†	0 L/ha/day	N/A	

*Peak Factor = 1.5 if contributing area is >20%; Peak Factor = 1.0 if contributing area is <20%

†Open Space, Arterial ROW, SWM Blocks, etc. with no sanitary flow contribution (extraneous flow only)

Table 2: Operational Design Flow Parameters

Land Use	Average Daily Flow	Peaking Factor	Peak Extraneous Flows
Residential	200 L/cap/day	Harmon Equation, K=0.6 (1.2 min – 2.4 max)	0.30 L/s/ha
Commercial	17,000 L/ha/day	1.0 (non-coincident peak)	
Institutional	17,000 L/ha/day	1.0 (non-coincident peak)	

*There are no industrial areas identified within the tributary area.

$$\text{Harmon Equation} = 1 + \frac{14}{4 + \left(\frac{P}{1000}\right)^{\frac{1}{2}}} \times K$$

Where:

P = Population

K = Correction Factor:

- Peak Flow = 0.8
- Operational = 0.6

3.2 Land Use Designations & Population Estimates

Population densities and unit counts for future residential development are based on the Novatech (2016) Hydraulics Review / Assessment; refer to **Table 3**. They are based on the concept plans provided by the developers of the future residential areas.

Table 3: Residential Land Use Population Densities

Residential Land Use	Units per ha	Persons per Unit	Persons per ha
Low Density (singles and semis)	26 – 28 (28 used)	2.7 – 3.4 (3.4 used)	95.2
Medium Density (row/townhouse)	50 – 60 (60 used)	2.7	162.0
High Density (apartments)	60 – 75 (75 used)	1.8	135.0

The land use designations shown in **Table 4** have been applied for the areas within Phases 2 & 3 of the SNC (Node 70 to 130). The Hydraulics Analysis / Review delineated the sewershed areas and land use designations using aerial photos (existing development) and conceptual site plans (future development).

Table 4: Land Use Designations

Land Use Designation	
Secondary Plan	SNC Design
Residential	Residential (Low / Medium / High Density)
Institutional / Office	Institutional
Commercial	Commercial
Recreational	
Business Park	
Prestige Business Park	
Park/Open Space Area	Other*
Ex. Snow Disposal Facility (future commercial)	
Stormwater Management Facility	
Conservation Lands	
Arterial Right-of-Ways	

* No sanitary flow contribution - extraneous flows (inflow/infiltration) only.

The overall residential population estimate and sewershed area for Phases 2 and 3 of the SNC is provided in **Table 5** below. It is assumed that the snow dump facility at the Stranderd Drive and McKenna Casey Drive will ultimately be re-zoned for commercial development.

Table 5: Population Estimates and Areas

Existing / Future	Estimated Population / Area	Novatech (2015)
Existing	Estimated Population	6,944 persons
	Gross Residential Area	60.09 ha
	Gross Commercial / Institutional Area	64.37 ha
	<i>Total Sewershed Area</i>	124.5 ha
Future (full service)	Estimated Population	27,312 persons
	Gross Residential Area	248.48 ha
	Gross Commercial / Institutional Area	228.82 ha
	<i>Total Sewershed Area</i>	477.3 ha

4.0 SANITARY DESIGN FLOWS

The sanitary flow allocations for Phases 2 and 3 of the SNC are provided in **Table 6**. The corresponding sanitary drainage area plan is provided as **Figure 1**. Sanitary sewer flow calculations for Phases 2 and 3 and detailed sanitary sewer design sheets for Phase 3 are attached to this memorandum.

The estimated sanitary design flows from Phase 3 of the SNC (entering Node 90) are as follows:

- Present-Day Operational Design Flows (Theoretical) = 55.1 L/s
- Future Peak Design Flows = 282.5 L/s

The outlet for Phase 3 of the SNC is the existing 900mm outlet pipe at the 2400mm maintenance hole (Node 90) located at the intersection of Strandherd Drive and Fraser Fields Way. Given a minimum design slope of 0.10%, this 900mm sanitary trunk sewer would have a full flow capacity of 597.2 L/s. Therefore, the downstream sanitary trunk sewer would be at 64% capacity, based on the future peak design flow being 282.5 L/s.

ATTACHMENTS:

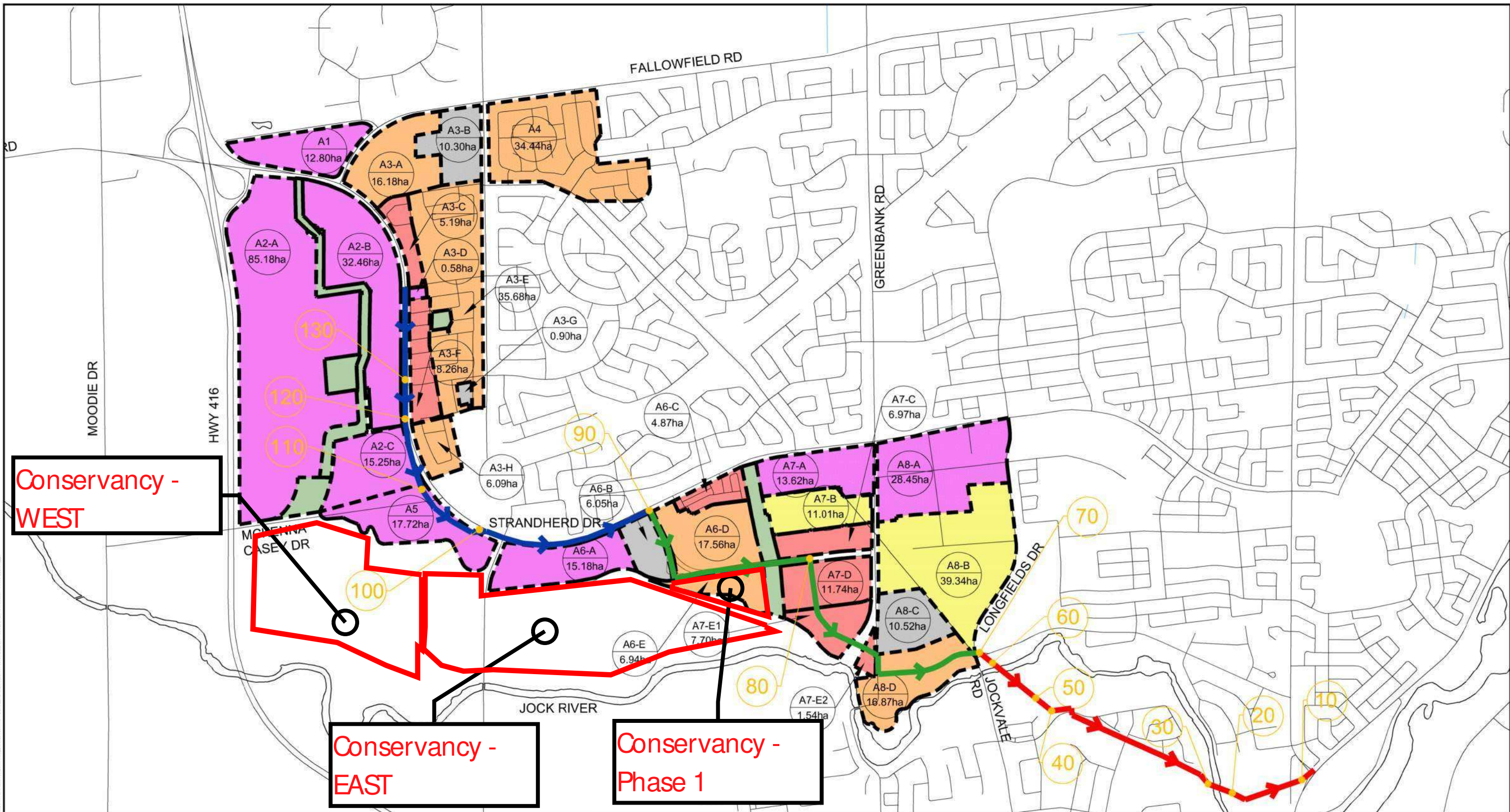
- Figure 1: Sanitary Drainage Areas and Land Use
- Sanitary Sewer Flow Calculations
- Sanitary Sewer Design Sheets (Phase 3)
- South Nepean Collector Phase 2: Hydraulics Review / Assessment (Novatech, 2016)
- Excerpts from Dillion (2012)



Table 6: Updated Allocation of Commercial, Institutional and Residential Demands to Phases 2 & 3 (Nodes 70 – 130) of the SNC by Collection Area

Collection Area	Upstream Node	Existing / Proposed Development	Existing / Proposed Land Use	Area (ha)	Estimated Number of Residential Units	Population Density (persons / ha)	Comment	Reference
A1	130	Proposed	Commercial	12.80	-	-	O'Keefe Court – Conceptual site plan shows proposed commercial.	Conceptual Plans for O'Keefe Court
A2-A	130	Proposed	Commercial	85.18	-	-	CitiGate – Analysis uses same approach as the design for CitiGate.	Detailed Servicing and SWM Report (Phase 1) (Novatech, 2014)
A2-B	130	Proposed	Commercial	32.46	-	-		
A2-C	120	Proposed	Commercial (ex. Snow dump)	15.25	-	-	Existing snow dump facility assumed to be future commercial.	Functional Design Report and Update – SNC Phase 2 and 3 (Dillon, 2012)
A3-A	130	Proposed	Low Density Residential	16.18	461	95.2	Havencrest – Existing single family units.	Havencrest Design Report (IBI, 2013)
A3-B	130	Existing	Institutional	10.30	-	-	Cedarview Middle School and Cedarview Alliance Church.	Aerial Photos / Site Visits
A3-C	130	Existing	Medium Density Residential	5.19	311	162	Existing townhouse units.	
A3-D	130	Existing	Commercial	0.58	-	-	Existing commercial buildings.	
A3-E	130	Existing	Low Density Residential	35.68	999	95.2	Existing single family units.	
A3-F	130	Existing	Medium Density Residential	8.26	496	162.0	Existing townhouse units.	
A3-G	130	Existing	Institutional	0.90	-	-	Ottawa Torah Centre Chibad.	
A3-H	120	Existing	Low Density Residential	6.09	171	95.2	Existing single family units.	
A4	130	Existing	Low Density Residential	34.44	964	95.2	Existing single family units currently serviced by Jockvale pump station; to be redirected to SNC.	
A5	110	Proposed	Commercial	17.72	-	-	Proposed commercial south of McKenna Casey Drive.	Site Visits
A6-A	100	Proposed	Commercial	15.18	-	-	Proposed commercial south of Srandherd Drive; east of Borrisokane Road.	Conceptual Plan for Lands Adjacent the Kennedy-Burnett SWMF provided by Minto (2015)
A6-B	100	Proposed	Institutional	6.05	-	-	Proposed school site on Minto property.	
A6-C	90	Existing	Medium Density Residential	4.87	292	162.0	Existing townhouse units.	Aerial Photos / Site Visits
A6-D	90	Proposed	Low Density Residential	17.56	492	95.2	Proposed single family units on lands owned by Minto / Mion.	Conceptual Plans for Lands Adjacent the Kennedy-Burnett SWMF provided by land owners.
A6-E	90	Proposed	Low Density Residential	6.94	203	95.2	Proposed single family units on lands owned by Pavic / Braovac.	
A7-A	80	Existing	Commercial	13.62	-	-	Existing large retail stores (commercial).	Aerial Photos
A7-B	80	Proposed	High Density Residential	11.01	826	135.0	Proposed high density units on lands owned by Richcraft / Trinity.	Conceptual Plans for Lands Adjacent the Kennedy-Burnett SWMF provided by land owners.
A7-C	80	Proposed	Medium Density Residential	6.97	418	162.0	Proposed Medium density units on lands owned by Mion.	
A7-D	80	Proposed	Medium Density Residential	11.74	704	162.0	Proposed Medium density units on lands owned by Caivan.	
A7-E1/E2	80	Proposed	Medium Density Residential	9.24	554	162.0	Proposed Medium density units on lands owned by Claridge.	
A8-A	80	Existing	Commercial	28.45	-	-	Existing Barrhaven Market Place (commercial).	Aerial Photos / Site Visits
A8-B	80	Proposed	High Density Residential	39.34	2951	135.0	Future development similar to Ampersands development.	Site Visits
A8-C	80	Existing	Institutional	10.52	-	-	Existing St. Joseph High School.	Aerial Photos / Site Visits
A8-D	80	Proposed	Low Density Residential	16.87	1012	162.0	Proposed 600 low density residential units.	Functional Design Report and Update – SNC Phase 2 and 3 (Dillon, 2012)

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LEGEND

- | | | | |
|--|------------------------------------------------|--|--------------------------------------------|
| | EXISTING / PROPOSED HIGH DENSITY RESIDENTIAL | | OTHER LANDS (OPEN SPACE, PARKS, AND SWMFS) |
| | EXISTING / PROPOSED MEDIUM DENSITY RESIDENTIAL | | SOUTH NEPEAN COLLECTOR PHASE 1 |
| | EXISTING / PROPOSED LOW DENSITY RESIDENTIAL | | SOUTH NEPEAN COLLECTOR PHASE 2 |
| | EXISTING / PROPOSED COMMERCIAL | | SOUTH NEPEAN COLLECTOR PHASE 3 |
| | EXISTING / PROPOSED INSTITUTIONAL | | SOUTH NEPEAN COLLECTOR NODE ID |



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SOUTH NEPEAN COLLECTOR SEWER

SANITARY DRAINAGE AREAS AND LAND USE

SCALE 1:20 000

DATE	MAY 2019	JOB	117190	FIGURE	FIG. 1
------	----------	-----	--------	--------	--------

PROJECT #: 117190
 DESIGNED BY: CMS
 CHECKED BY: RJD
 DATE: December 5, 2018

SANITARY SEWER DESIGN SHEET

South Nepean Collector - Phase 2 & 3

Theoretical Current Operational Peak Wastewater Flow



Location			Areas				Population				Individual Design Flows			Cumulative Design Flows				
Area I.D.	Existing Land Use	Upstream Node	Gross Commercial Area (ha)	Gross Institutional Area (ha)	Gross Residential Area (ha)	Total Gross Area (ha)	Residential Population Density (people / ha)	Individual Residential Population	Cumulative Residential Population	Residential Peaking Factor (Harmon Eqn ¹)	Commercial Peak Flow Rate ² (17,000 L/ha/d) (L/s)	Institutional Peak Flow Rate ² (17,000 L/ha/d) (L/s)	Infiltration / Inflow Rate (0.3 L/s/ha) (L/s)	Commercial (L/s)	Institutional (L/s)	Infiltration / Inflow (L/s)	Residential Peak Flow Rate (200 L/cap/d) (L/s)	Cumulative Peak Design Flow (L/s)
A1	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A2-A	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A2-B	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A3-A	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A3-B	Institutional	130		10.30		10.30					0.0	2.0	3.1	0.0	2.0	3.1	0.0	5.1
A3-C	Medium Density Residential	130			5.19	5.19	162.0	841	841	2.40	0.0	0.0	1.6	0.0	2.0	4.6	4.7	11.3
A3-D	Commercial	130	0.58			0.58		841	841	2.40	0.1	0.0	0.2	0.1	2.0	4.8	4.7	11.6
A3-E	Low Density Residential	130			35.68	35.68	95.2	3397	4238	2.39	0.0	0.0	10.7	0.1	2.0	15.5	23.4	41.1
A3-F	Medium Density Residential	130			8.26	8.26	162	1338	5576	2.32	0.0	0.0	2.5	0.1	2.0	18.0	29.9	50.1
A3-G	Institutional	130		0.90		0.90			5576	2.32	0.0	0.2	0.3	0.1	2.2	18.3	29.9	50.5
A4	Low Density Residential*	130				0.00			5576	2.32	0.0	0.0	0.0	0.1	2.2	18.3	29.9	50.5
A2-C	Snow Dump Facility	120				0.00			5576	2.32	0.0	0.0	0.0	0.1	2.2	18.3	29.9	50.5
A3-H	Low Density Residential	120			6.09	6.09	95.2	580	6155	2.30	0.0	0.0	1.8	0.1	2.2	20.1	32.7	55.1
A5	Open Space	110				0.00			6155	2.30	0.0	0.0	0.0	0.1	2.2	20.1	32.7	55.1
A6-A	Open Space	100				0.00			6155	2.30	0.0	0.0	0.0	0.1	2.2	20.1	32.7	55.1
A6-B	Open Space	100				0.00			6155	2.30	0.0	0.0	0.0	0.1	2.2	20.1	32.7	55.1
A6-C	Medium Density Residential	90			4.87	4.87	162.0	789	6944	2.27	0.0	0.0	1.5	0.1	2.2	21.6	36.4	60.3
A6-D	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	0.1	2.2	21.6	36.4	60.3
A6-E	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	0.1	2.2	21.6	36.4	60.3
A7-A	Commercial	90	13.62			13.62			6944	2.27	2.7	0.0	4.1	2.8	2.2	25.6	36.4	67.1
A7-B	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	2.8	2.2	25.6	36.4	67.1
A7-C	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	2.8	2.2	25.6	36.4	67.1
A7-D	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	2.8	2.2	25.6	36.4	67.1
A7-E1/E2	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	2.8	2.2	25.6	36.4	67.1
A8-A	Commercial	80	28.45			28.45			6944	2.27	5.6	0.0	8.5	8.4	2.2	34.2	36.4	81.2
A8-B	Open Space	80				0.00			6944	2.27	0.0	0.0	0.0	8.4	2.2	34.2	36.4	81.2
A8-C	Institutional	80		10.52		10.52			6944	2.27	0.0	2.1	3.2	8.4	4.3	37.3	36.4	86.4
A8-D	Open Space	80				0.00			6944	2.27	0.0	0.0	0.0	8.4	4.3	37.3	36.4	86.4
ROW Along SNC Sewer Alignment	-	80				14.34			6944	2.27	0.0	0.0	4.3	8.4	4.3	41.6	36.4	90.7
TOTAL		80	42.65	21.72	60.09	138.80	-	6944	6944	2.27	8.4	4.3	41.6	8.4	4.3	41.6	36.4	90.7

Residential Land Use	Population Density (Units / ha)	Persons per Unit	Persons per ha
Low Density (singles and semis)	26 – 28 (28 used)	2.7 – 3.4 (3.4 used)	95.2
Medium Density (row/townhouse)	50 – 60 (60 used)	2.7	162.0
High Density (apartments)	60 – 75 (75 used)	1.8	135.0

Notes:

- Harmon Equation = $1 + [14 / (4 + (P/1000)^{1/2})] \times K$
 Where: P = population; K = correction factor = 0.6
- Institutional / Commercial Peaking Factor = 1.0

Reported Design Flows / Assumptions:

- Area A4: Existing single family units currently serviced by Jockvale pump station; currently not directed to SNC

PROJECT #: 117190
 DESIGNED BY: CMS
 CHECKED BY: RJD
 DATE: December 5, 2018

SANITARY SEWER DESIGN SHEET

South Nepean Collector - Phase 2 & 3

Theoretical Future Full Service Peak Wastewater Flow



Location			Areas				Population				Individual Design Flows			Cumulative Design Flows				
Area I.D.	Existing / Proposed Land Use	Upstream Node	Gross Commercial Area (ha)	Gross Institutional Area (ha)	Gross Residential Area (ha)	Total Gross Area (ha)	Residential Population Density (people / ha)	Individual Residential Population	Cumulative Residential Population	Residential Peaking Factor (Harmon Eqn ¹)	Commercial Peak Flow Rate ² (28,000 L/ha/d) (L/s)	Institutional Peak Flow Rate ² (28,000 L/ha/d) (L/s)	Infiltration / Inflow Rate (0.33 L/s/ha) (L/s)	Commercial (L/s)	Institutional (L/s)	Infiltration / Inflow (L/s)	Residential Peak Flow Rate (280 L/cap/d) (L/s)	Cumulative Peak Design Flow (L/s)
A1	Commercial	130	12.80			12.80					6.2	0.0	4.2	6.2	0.0	4.2	0.0	10.4
A2-A	Commercial	130	85.18			85.18					41.4	0.0	28.1	47.6	0.0	32.3	0.0	80.0
A2-B	Commercial	130	32.46			32.46					15.8	0.0	10.7	63.4	0.0	43.0	0.0	106.5
A3-A	Low Density Residential	130			16.18	16.18	95.2	1540	1540	3.14	0.0	0.0	5.3	63.4	0.0	48.4	15.7	127.5
A3-B	Institutional	130		10.30		10.30				3.14	0.0	3.3	3.4	63.4	3.3	51.8	15.7	134.2
A3-C	Medium Density Residential	130			5.19	5.19	162.0	841	2381	3.02	0.0	0.0	1.7	63.4	3.3	53.5	23.3	143.6
A3-D	Commercial	130	0.58			0.58				3.02	0.3	0.0	0.2	63.7	3.3	53.7	23.3	144.0
A3-E	Low Density Residential	130			35.68	35.68	95.2	3397	5778	2.75	0.0	0.0	11.8	63.7	3.3	65.5	51.5	184.0
A3-F	Medium Density Residential	130			8.26	8.26	162	1338	7116	2.68	0.0	0.0	2.7	63.7	3.3	68.2	61.8	197.0
A3-G	Institutional	130		0.90		0.90				2.68	0.0	0.3	0.3	63.7	3.6	68.5	61.8	197.6
A4	Low Density Residential	130			34.44	34.44	95.2	3279	10395	2.55	0.0	0.0	11.4	63.7	3.6	79.9	85.9	233.1
A2-C	Commercial (ex. snow dump)	120	15.25			15.25				2.55	7.4	0.0	5.0	71.1	3.6	84.9	85.9	245.5
A3-H	Low Density Residential	120			6.09	6.09	95.2	580	10974	2.53	0.0	0.0	2.0	71.1	3.6	86.9	90.0	251.7
A5	Commercial	110	17.72			17.72				2.53	8.6	0.0	5.8	79.7	3.6	92.7	90.0	266.1
A6-A	Commercial	100	15.18			15.18				2.53	7.4	0.0	5.0	87.1	3.6	97.7	90.0	278.5
A6-B	Institutional	100		6.05		6.05				2.53	0.0	2.0	2.0	87.1	5.6	99.7	90.0	282.5
A6-C	Medium Density Residential	90			4.87	4.87	162.0	789	11763	2.51	0.0	0.0	1.6	87.1	5.6	101.4	95.6	289.6
A6-D	Low Density Residential	90			17.56	17.56	95.2	1672	13435	2.46	0.0	0.0	5.8	87.1	5.6	107.1	107.2	307.0
A6-E	Low Density Residential	90			6.94	6.94	95.2	661	14096	2.44	0.0	0.0	2.3	87.1	5.6	109.4	111.7	313.8
A7-A	Commercial	90	13.62			13.62				2.44	6.6	0.0	4.5	93.7	5.6	113.9	111.7	324.9
A7-B	High Density Residential	90			11.01	11.01	135.0	1486	15582	2.41	0.0	0.0	3.6	93.7	5.6	117.6	121.7	338.5
A7-C	Medium Density Residential	90			6.97	6.97	162.0	1129	16711	2.38	0.0	0.0	2.3	93.7	5.6	119.9	129.2	348.3
A7-D	Medium Density Residential	90			11.74	11.74	162.0	1902	18613	2.35	0.0	0.0	3.9	93.7	5.6	123.7	141.6	364.6
A7-E1/E2	Medium Density Residential	90			9.24	9.24	162.0	1497	20110	2.32	0.0	0.0	3.0	93.7	5.6	126.8	151.2	377.3
A8-A	Commercial	80	28.45			28.45				2.32	13.8	0.0	9.4	107.5	5.6	136.2	151.2	400.5
A8-B	High Density Residential	80			39.34	39.34	135.0	5311	25421	2.24	0.0	0.0	13.0	107.5	5.6	149.2	184.4	446.7
A8-C	Institutional	80		10.52		10.52				2.24	0.0	3.4	3.5	107.5	9.0	152.6	184.4	453.6
A8-D	Low Density Residential	80			16.87	16.87	120.9	2040	27461	2.21	0.0	0.0	5.6	107.5	9.0	158.2	196.9	471.6
ROW Along SNC Sewer Alignment	-	80				14.34				2.21	0.0	0.0	4.7	107.5	9.0	162.9	196.9	476.3
TOTAL		80	221.24	27.77	230.38	493.73	-	27461	27461	2.21	107.5	9.0	162.9	107.5	9.0	162.9	196.9	476.3

Residential Land Use	Population Density (Units / ha)	Persons per Unit	Persons per ha
Low Density (singles and semis)	26 - 28 (28 used)	2.7 - 3.4 (3.4 used)	95.2
Medium Density (row/townhouse)	50 - 60 (60 used)	2.7	162.0
High Density (apartments)	60 - 75 (75 used)	1.8	135.0

Notes:

- Harmon Equation = $1 + [14 / (4 + (P/1000)^{1/2})] \times K$
 Where: P = population; K = correction factor = 0.8
- Commercial Peaking Factor = 1.5; Institutional Peaking Factor = 1.0

Reported Design Flows / Assumptions:

- Area A4: Existing single family units currently serviced by Jockvale pump station to be redirected to SNC
- Area A8-D: proposed 600 medium density residential units

See Note (2) in the DSEL "Barrhaven Conservancy - Evaluation of SNC Flows" design sheet

THE PRIOR NOVATECH SNC DESIGN SHEET HAD FLOWS AT 423.6 L/s AFTER AREA ID "A6-E". THIS UPDATED NOVATECH 'PHASE 3' EVALUATION HAS A FLOW OF 313.8 L/s. THE DSEL EVALUATION OF SANITARY FLOWS WITH THE NEW CITY DESIGN PARAMETERS AT THIS SAME NODE (WITH CONSERVANCY WEST AND EAST INCLUDED) IS ~401.58 L/s (WHICH IS LESS THAN THE PRIOR 423.6 L/s NOTED ABOVE)

SOUTH NEPEAN COLLECTOR (PHASE 3)
SANITARY SEWER DESIGN SHEET



DECEMBER 5 2018
JOB# 117190

LOCATION			Area				Population		Cumulative Design Flows					PROPOSED SEWER						
From MH	To MH	Upstream Node	Gross Commercial Area (ha)	Gross Institutional Area (ha)	Gross Residential Area (ha)	Total Gross Area (ha)	Cumulative Residential Population	Residential Peaking Factor (Harmon Eqn ¹)	Commercial (L/s)	Institutional (L/s)	Infiltration / Inflow (L/s)	Residential Peak Flow Rate (280 L/cap/d) (L/s)	Cumulative Peak Design Flow (L/s)	Length (m)	Pipe Size (mm)	Type	Slope %	Capacity (L/s)	Full Flow Velocity (m/s)	Ratio (Q/Qfull)
SA 22	SA 21	120	146.27	11.20	105.84	263.31	10974	2.53	71.1	3.6	86.9	90.0	251.7	131.9	750	CONC	0.10	367.3	0.81	69%
SA 21	SA 20	120											251.7	90.6	750	CONC	0.10	367.3	0.81	69%
SA 20	SA 19	120											251.7	90.0	750	CONC	0.10	367.3	0.81	69%
SA 19	SA 18	120											251.7	72.1	750	CONC	0.10	367.3	0.81	69%
SA 18	SA 17	120											251.7	71.9	750	CONC	0.10	367.3	0.81	69%
SA 17	SA 16	120											251.7	71.4	750	CONC	0.10	367.3	0.81	69%
SA 16	SA 15	110	163.99	11.20	105.84	281.03	10974	2.53	79.7	3.6	92.7	90.0	266.1	73.2	750	CONC	0.10	367.3	0.81	72%
SA 15	SA 14	110											266.1	67.5	750	CONC	0.10	367.3	0.81	72%
SA 14	SA 13	110											266.1	56.6	750	CONC	0.10	367.3	0.81	72%
SA 13	SA 12	110											266.1	133.5	750	CONC	0.10	367.3	0.81	72%
SA 12	SA 11	110											266.1	150.0	750	CONC	0.10	367.3	0.81	72%
SA 11	SA 10	100	179.17	17.25	105.84	302.26	10974	2.53	87.1	5.6	99.7	90.0	282.5	97.8	750	CONC	0.10	367.3	0.81	77%
SA 10	SA 9	100											282.5	76.7	750	CONC	0.10	367.3	0.81	77%
SA 9	SA 8	100											282.5	79.7	750	CONC	0.10	367.3	0.81	77%
SA 8	SA 7	100											282.5	75.3	750	CONC	0.10	367.3	0.81	77%
SA 7	SA 6	100											282.5	84.9	750	CONC	0.10	367.3	0.81	77%
SA 6	SA 5	100											282.5	77.1	750	CONC	0.10	367.3	0.81	77%
SA 5	SA 4	100											282.5	78.9	750	CONC	0.10	367.3	0.81	77%
SA 4	SA 3	100											282.5	80.5	750	CONC	0.10	367.3	0.81	77%
SA 3	SA 2	100											282.5	150.0	750	CONC	0.10	367.3	0.81	77%
SA 2	SA 1	100											282.5	114.6	750	CONC	0.10	367.3	0.81	77%
SA 1	EX 80	100											282.5	12.4	750	CONC	0.10	367.3	0.81	77%

Design Parameters:

Residential Land Use	Population Density (Units / ha)	Persons per Unit	Persons per ha
Low Density (singles / semis)	26 – 28 (28 used)	2.7 – 3.4 (3.4 used)	95.2
Medium Density (row / townhouse)	50 – 60 (60 used)	2.7	162.0
High Density (apartments)	60 – 75 (75 used)	1.8	135.0

Notes:

- Harmon Equation = $1 + [14 / (4 + (P/1000)^{1/2})] \times K$
Where: P = population; K = correction factor = 0.8
- Commercial Peaking Factor = 1.5; Institutional Peaking Factor = 1.0

Reported Design Flows / Assumptions:

- Area A4: Existing single family units currently serviced by Jockvale pump station to be redirected to SNC
- Area A8-D: proposed 600 medium density residential units



MEMORANDUM

DATE: MAY 26, 2016
TO: JONATHAN KNOYLE – CITY OF OTTAWA
FROM: CONRAD STANG – NOVATECH
RE: SOUTH NEPEAN COLLECTOR PHASE 2: SANITARY FLOW CALCULATIONS
CC: EDSON DONNELLY – NOVATECH

1.0 PURPOSE

This memorandum provides the sanitary sewer flow calculations and design sheet for Phase 2 of the proposed South Nepean Collector (SNC). Sanitary design flows have been estimated for both current-day operational flows and future development peak design flows, based on the latest available planning information for the vacant lands within the SNC sewershed.

2.0 BACKGROUND

In January 1998, the Master Servicing Study for the South Nepean Urban Area provided a conceptual plan for water, wastewater and stormwater infrastructure. The preferred alternative for wastewater servicing was an east/west trunk sewer alignment that was to be completed in several phases. The proposed sanitary trunk sewer was initially called the Jock River Collector, but was renamed the South Nepean Collector during the original functional design study completed in 2003.

Phase 1 of the South Nepean Collector was completed in 2005 and currently terminates at a 2400mm maintenance hole located east of Longfields Drive, north of Bren-Maur Road. Phase 2 will extend the trunk sewer to Strandherd Drive at the intersection of the proposed transitway along the proposed extension to Chapman Mills Drive. Phase 3 will extend the trunk sewer along Strandherd Drive to the intersection of Maravista Drive.

The sanitary sewer flows were previously documented in the *South Nepean Collector – Functional Design Report and Update* (Dillon, 2012). A review of the sanitary flows provided in the Dillon Report based on the latest planning information for the vacant lands within the SNC sewershed was documented in the technical memorandum titled *South Nepean Collector Phase 2: Hydraulics Review / Assessment* (Novatech, 2015), which is attached to this memorandum. The results of the *Hydraulics Review / Assessment* (Novatech, 2015) were very similar to the results from the Dillon (2012) analysis.

3.0 DESIGN PARAMETERS AND POPULATION ESTIMATES

3.1 Design Parameters

The sanitary design flow were calculated using the parameters from the City of Ottawa Sewer Design Guidelines (October 2012), and are summarized in **Table 1** and **Table 2**.

Table 1: Peak Design Flow Parameters

Land Use	Average Daily Flow	Peaking Factor	Peak Extraneous Flows
Residential	350 L/cap/day	Harmon Equation, K=1 (2.0 min – 4.0 max)	0.28 L/s/ha
Commercial	50,000 L/ha/day	1.5	
Institutional	50,000 L/ha/day	1.5	
Other*	0 L/ha/day	N/A	

*Open Space, Arterial ROW, SWM Blocks, etc. with no sanitary flow contribution (extraneous flow only)

Table 2: Operational Design Flow Parameters

Land Use	Average Daily Flow	Peaking Factor	Peak Extraneous Flows
Residential	300 L/cap/day	Harmon Equation, K=0.6 (1.2 min – 2.4 max)	<u>Dry weather</u> 0.05-0.08 L/s/ha
Commercial	17,000 L/ha/day	1.0 (non-coincident peak)	<u>Wet Weather</u> 0.15 - 0.20 L/s/ha (typical events) 0.28 L/s/ha (large/annual events) 0.30 - 0.50 L/s/ha (extreme events)
Institutional	10,000 L/ha/day	1.0 (non-coincident peak)	

*There are no industrial areas identified within the tributary area.

$$\text{Harmon Equation} = 1 + \frac{14}{4 + \left(\frac{P}{1000}\right)^{\frac{1}{2}}} \times K$$

Where:

P = Population

K = Correction Factor:

- Peak Flow = 1

- Operational = between 0.4 to 0.6 (0.6 used)

3.2 Land Use Designations & Population Estimates

Population densities and unit counts for future residential development are based on the current concept plans for these areas, and are presented in **Table 3**.

Table 3: Residential Land Use Population Densities

Residential Land Use	Units per ha	Persons per Unit	Persons per ha
Low Density (singles and semis)	26 – 28 (28 used)	2.7 – 3.4 (3.4 used)	95.2
Medium Density (row/townhouse)	50 – 60 (60 used)	2.7	162.0
High Density (apartments)	60 – 75 (75 used)	1.8	135.0

The land use designations shown in **Table 4** have been applied for the areas within Phases 2 and 3 of the SNC (Node 70 to 130). The sewershed areas and land use designations were delineated using aerial photos (existing development) and conceptual site plans (future development).

Table 4: Land Use Designations

Land Use Designation	
Secondary Plan	SNC Design
Residential	Residential (Low / Medium / High Density)
Institutional / Office	Institutional
Commercial	Commercial
Recreational	
Business Park	
Prestige Business Park	
Park/Open Space Area	Other*
Ex. Snow Disposal Facility (future commercial)	
Stormwater Management Facility	
Conservation Lands	
Arterial Right-of-Ways	

* No sanitary flow contribution - extraneous flows (inflow/infiltration) only.

The overall residential population estimate and sewershed area for Phases 2 and 3 of the SNC is provided in **Table 5** below. It is assumed that the snow dump facility at the Stranderd Drive and McKenna Casey Drive will ultimately be re-zoned for commercial development.

Table 5: Population Estimates and Areas

Existing / Future	Estimated Population / Area	Novatech (2015)
Existing	Estimated Population	6,944 persons
	Gross Residential Area	60.09 ha
	Gross Commercial / Institutional Area	64.37 ha
	<i>Total Sewershed Area</i>	124.5 ha
Future (full service)	Estimated Population	27,312 persons
	Gross Residential Area	248.48 ha
	Gross Commercial / Institutional Area	228.82 ha
	<i>Total Sewershed Area</i>	477.3 ha

4.0 SANITARY DESIGN FLOWS

The sanitary flow allocations for Phases 2 and 3 of the SNC are provided in **Table 6**. The corresponding sanitary drainage area plan is provided as **Figure 1**. Sanitary sewer flow calculations for Phases 2 and 3 and detailed sanitary sewer design sheets for Phase 2 are attached to this memorandum.

The estimated sanitary design flows from Phases 2 and 3 of the SNC (entering Node 70) are as follows:

- Present-Day Operational Design Flows (Theoretical) = 72.5 L/s
- Future Peak Design Flows = 634.2 L/s

The outlet for Phase 2 of the SNC is the existing 1050mm outlet pipe at the 2400mm maintenance hole (Node 70) located east of Longfields Drive, north of Bren-Maur Road. Given a minimum design slope of 0.10%, this sanitary trunk sewer would have a full flow capacity of 900.5 L/s. Therefore, the downstream sanitary trunk sewer would be at 70% capacity, based on the future peak design flow being 634.2 L/s.

ATTACHMENTS:

- Figure 1: Sanitary Drainage Areas and Land Use
- Sanitary Sewer Flow Calculations
- Sanitary Sewer Design Sheets (Phase 2)
- South Nepean Collector Phase 2: Hydraulics Review / Assessment (Novatech, 2015)

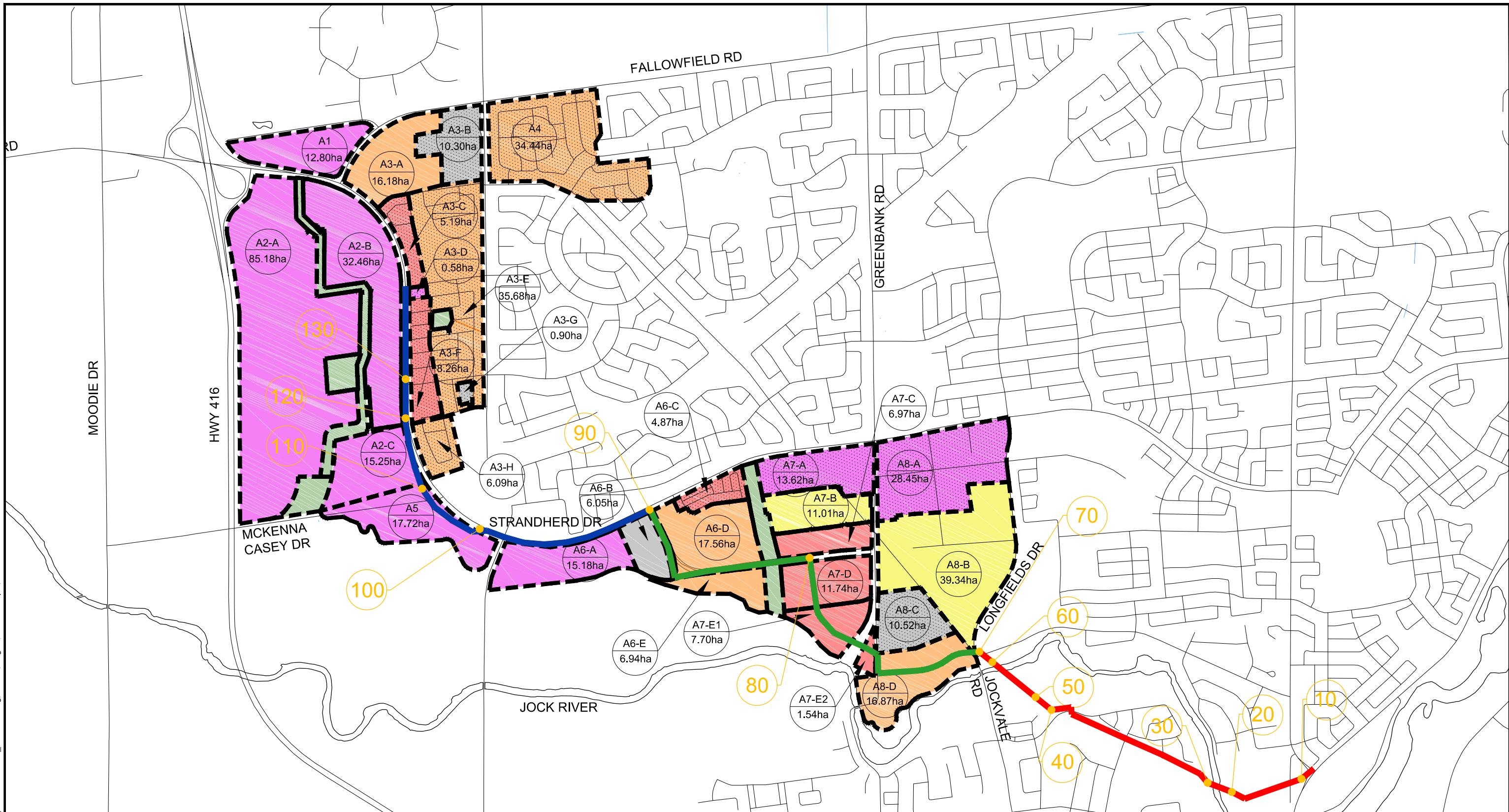


Table 6: Updated Allocation of Commercial, Institutional and Residential Demands to Phases 2 & 3 (Nodes 70 – 130) of the SNC by Collection Area

Collection Area	Upstream Node	Existing / Proposed Development	Existing / Proposed Land Use	Area (ha)	Estimated Number of Residential Units	Population Density (persons / ha)	Comment	Reference
A1	130	Proposed	Commercial	12.80	-	-	O'Keefe Court – Conceptual site plan shows proposed commercial.	Conceptual Plans for O'Keefe Court
A2-A	130	Proposed	Commercial	85.18	-	-	CitiGate – Analysis uses same approach as the design for CitiGate.	Detailed Servicing and SWM Report (Phase 1) (Novatech, 2014)
A2-B	130	Proposed	Commercial	32.46	-	-		
A2-C	120	Proposed	Commercial (ex. Snow dump)	15.25	-	-	Existing snow dump facility assumed to be future commercial.	Functional Design Report and Update – SNC Phase 2 and 3 (Dillon, 2012)
A3-A	130	Proposed	Low Density Residential	16.48	461	95.2	Havencrest – Existing single family units.	Havencrest Design Report (IBI, 2013)
A3-B	130	Existing	Institutional	10.30	-	-	Cedarview Middle School and Cedarview Alliance Church.	Aerial Photos / Site Visits
A3-C	130	Existing	Medium Density Residential	5.19	311	162	Existing townhouse units.	
A3-D	130	Existing	Commercial	0.58	-	-	Existing commercial buildings.	
A3-E	130	Existing	Low Density Residential	35.68	999	95.2	Existing single family units.	
A3-F	130	Existing	Medium Density Residential	8.26	496	162.0	Existing townhouse units.	
A3-G	130	Existing	Institutional	0.90	-	-	Ottawa Torah Centre Chibad.	
A3-H	120	Existing	Low Density Residential	6.09	171	95.2	Existing single family units.	
A4	130	Existing	Low Density Residential	34.44	964	95.2	Existing single family units currently serviced by Jockvale pump station; to be redirected to SNC.	
A5	110	Proposed	Commercial	17.72	-	-	Proposed commercial south of McKenna Casey Drive.	Site Visits
A6-A	100	Proposed	Institutional	20.70	-	-	Proposed school site on Minto property.	Conceptual Plan for Lands Adjacent the Kennedy-Burnett SWMF provided by Minto (2015)
A6-B	90	Existing	Medium Density Residential	4.87	292	162.0	Existing townhouse units.	Aerial Photos / Site Visits
A6-C	90	Proposed	Low Density Residential	10.11	283	95.2	Proposed single family units on lands owned by Minto.	Conceptual Plans for Lands Adjacent the Kennedy-Burnett SWMF provided by land owners.
A6-D	90	Proposed	Low Density Residential	5.59	157	95.2	Proposed single family units on lands owned by Mion.	
A6-E	90	Proposed	Low Density Residential	7.24	203	95.2	Proposed single family units on lands owned by Pavic / Braovac.	
A7-A	80	Existing	Commercial	13.62	-	-	Existing large retail stores (commercial).	Aerial Photos
A7-B	80	Proposed	High Density Residential	11.01	826	135.0	Proposed high density units on lands owned by Richcraft / Trinity.	Conceptual Plans for Lands Adjacent the Kennedy-Burnett SWMF provided by land owners.
A7-C	80	Proposed	Medium Density Residential	6.97	418	162.0	Proposed Medium density units on lands owned by Mion.	
A7-D	80	Proposed	Medium Density Residential	11.74	704	162.0	Proposed Medium density units on lands owned by Caivan.	
A7-E1/E2	80	Proposed	Medium Density Residential	9.24	554	162.0	Proposed Medium density units on lands owned by Claridge.	
A8-A	80	Existing	Commercial	28.45	-	-	Existing Barrhaven Market Place (commercial).	Aerial Photos / Site Visits
A8-B	80	Proposed	High Density Residential	39.34	2951	135.0	Future development similar to Ampersands development.	Site Visits
A8-C	80	Existing	Institutional	10.52	-	-	Existing St. Joseph High School.	Aerial Photos / Site Visits
A8-D	80	Proposed	Low Density Residential	16.87	1012	162.0	Proposed 600 low density residential units.	Functional Design Report and Update – SNC Phase 2 and 3 (Dillon, 2012)

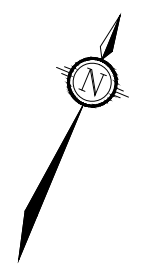
Attachment 1
Sanitary Drainage Areas and Land Use

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LEGEND

- EXISTING / PROPOSED HIGH DENSITY RESIDENTIAL
- EXISTING / PROPOSED MEDIUM DENSITY RESIDENTIAL
- EXISTING / PROPOSED LOW DENSITY RESIDENTIAL
- EXISTING / PROPOSED COMMERCIAL
- EXISTING / PROPOSED INSTITUTIONAL
- OTHER LANDS (OPEN SPACE, PARKS, AND SWMFS)
- SOUTH NEPEAN COLLECTOR PHASE 1
- SOUTH NEPEAN COLLECTOR PHASE 2
- SOUTH NEPEAN COLLECTOR PHASE 3
- SOUTH NEPEAN COLLECTOR NODE ID



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SOUTH NEPEAN COLLECTOR SEWER

SANITARY DRAINAGE AREAS AND LAND USE

SCALE	1:20 000	
DATE	MAY 2016	JOB
		115075
FIGURE	FIG. 1	

Attachment 2
Sewer Flow Calculations

PROJECT #: 115075
 DESIGNED BY: CMS
 CHECKED BY: MJP
 DATE: August 20, 2015

SANITARY SEWER DESIGN SHEET

South Nepean Collector - Phase 2 & 3

Theoretical Current Operational Peak Wastewater Flow



Location			Areas				Population				Individual Design Flows			Cumulative Design Flows				
Area I.D.	Existing Land Use	Upstream Node	Gross Commercial Area (ha)	Gross Institutional Area (ha)	Gross Residential Area (ha)	Total Gross Area (ha)	Residential Population Density (people / ha)	Individual Residential Population	Cumulative Residential Population	Residential Peaking Factor (Harmon Eqn ¹)	Commercial Peak Flow Rate ² (17,000 L/ha/d) (L/s)	Institutional Peak Flow Rate ² (10,000 L/ha/d) (L/s)	Infiltration / Inflow Rate (0.05 L/s/ha) (L/s)	Commercial (L/s)	Institutional (L/s)	Infiltration / Inflow (L/s)	Residential Peak Flow Rate (300 L/cap/d) (L/s)	Cumulative Peak Design Flow (L/s)
A1	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A2-A	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A2-B	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A3-A	Open Space	130				0.00					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A3-B	Institutional	130		10.30		10.30					0.0	1.2	0.5	0.0	1.2	0.5	0.0	1.7
A3-C	Medium Density Residential	130			5.19	5.19	162.0	841	841	2.71	0.0	0.0	0.3	0.0	1.2	0.8	7.9	9.9
A3-D	Commercial	130	0.58			0.58		841	841	2.71	0.1	0.0	0.0	0.1	1.2	0.8	7.9	10.0
A3-E	Low Density Residential	130			35.68	35.68	95.2	3397	4238	2.39	0.0	0.0	1.8	0.1	1.2	2.6	35.1	39.0
A3-F	Medium Density Residential	130			8.26	8.26	162	1338	5576	2.32	0.0	0.0	0.4	0.1	1.2	3.0	44.9	49.2
A3-G	Institutional	130		0.90		0.90			5576	2.32	0.0	0.1	0.0	0.1	1.3	3.0	44.9	49.4
A4	Low Density Residential*	130				0.00			5576	2.32	0.0	0.0	0.0	0.1	1.3	3.0	44.9	49.4
A2-C	Snow Dump Facility	120				0.00			5576	2.32	0.0	0.0	0.0	0.1	1.3	3.0	44.9	49.4
A3-H	Low Density Residential	120			6.09	6.09	95.2	580	6155	2.30	0.0	0.0	0.3	0.1	1.3	3.4	49.1	53.8
A5	Open Space	110				0.00			6155	2.30	0.0	0.0	0.0	0.1	1.3	3.4	49.1	53.8
A6-A	Open Space	100				0.00			6155	2.30	0.0	0.0	0.0	0.1	1.3	3.4	49.1	53.8
A6-B	Open Space	100				0.00			6155	2.30	0.0	0.0	0.0	0.1	1.3	3.4	49.1	53.8
A6-C	Medium Density Residential	90			4.87	4.87	162.0	789	6944	2.27	0.0	0.0	0.2	0.1	1.3	3.6	54.6	59.6
A6-D	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	0.1	1.3	3.6	54.6	59.6
A6-E	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	0.1	1.3	3.6	54.6	59.6
A7-A	Commercial	90	13.62			13.62			6944	2.27	2.7	0.0	0.7	2.8	1.3	4.3	54.6	63.0
A7-B	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	2.8	1.3	4.3	54.6	63.0
A7-C	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	2.8	1.3	4.3	54.6	63.0
A7-D	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	2.8	1.3	4.3	54.6	63.0
A7-E1/E2	Open Space	90				0.00			6944	2.27	0.0	0.0	0.0	2.8	1.3	4.3	54.6	63.0
A8-A	Commercial	80	28.45			28.45			6944	2.27	5.6	0.0	1.4	8.4	1.3	5.7	54.6	70.0
A8-B	Open Space	80				0.00			6944	2.27	0.0	0.0	0.0	8.4	1.3	5.7	54.6	70.0
A8-C	Institutional	80		10.52		10.52			6944	2.27	0.0	1.2	0.5	8.4	2.5	6.2	54.6	71.8
A8-D	Open Space	80				0.00			6944	2.27	0.0	0.0	0.0	8.4	2.5	6.2	54.6	71.8
ROW Along SNC Sewer Alignment	-	80				14.34			6944	2.27	0.0	0.0	0.7	8.4	2.5	6.9	54.6	72.5
TOTAL		80	42.65	21.72	60.09	138.80	-	6944	6944	2.27	8.4	2.5	6.9	8.4	2.5	6.9	54.6	72.5

Residential Land Use	Population Density (Units / ha)	Persons per Unit	Persons per ha
Low Density (singles and semis)	26 - 28 (28 used)	2.7 - 3.4 (3.4 used)	95.2
Medium Density (row/townhouse)	50 - 60 (60 used)	2.7	162.0
High Density (apartments)	60 - 75 (75 used)	1.8	135.0

Notes:

- Harmon Equation = $1 + [14 / (4 + (P/1000)^{1/2})] \times K$
 Where: P = population; K = correction factor = 0.6
- Institutional / Commercial Peaking Factor = 1.0

Reported Design Flows / Assumptions:

- Area A4: Existing single family units currently serviced by Jockvale pump station; currently not directed to SNC

PROJECT #: 115075
 DESIGNED BY: CMS
 CHECKED BY: MJP
 DATE: August 20, 2015

SANITARY SEWER DESIGN SHEET

South Nepean Collector - Phase 2 & 3

Theoretical Future Full Service Peak Wastewater Flow



Location			Areas				Population				Individual Design Flows			Cumulative Design Flows				
Area I.D.	Existing / Proposed Land Use	Upstream Node	Gross Commercial Area (ha)	Gross Institutional Area (ha)	Gross Residential Area (ha)	Total Gross Area (ha)	Residential Population Density (people / ha)	Individual Residential Population	Cumulative Residential Population	Residential Peaking Factor (Harmon Eqn ¹)	Commercial Peak Flow Rate ² (50,000 L/ha/d) (L/s)	Institutional Peak Flow Rate ² (50,000 L/ha/d) (L/s)	Infiltration / Inflow Rate (0.28 L/s/ha) (L/s)	Commercial (L/s)	Institutional (L/s)	Infiltration / Inflow (L/s)	Residential Peak Flow Rate (350 L/cap/d) (L/s)	Cumulative Peak Design Flow (L/s)
A1	Commercial	130	12.80			12.80					11.1	0.0	3.6	11.1	0.0	3.6	0.0	14.7
A2-A	Commercial	130	85.18			85.18					73.9	0.0	23.9	85.1	0.0	27.4	0.0	112.5
A2-B	Commercial	130	32.46			32.46					28.2	0.0	9.1	113.2	0.0	36.5	0.0	149.8
A3-A	Low Density Residential	130			16.18	16.18	95.2	1540	1540	3.67	0.0	0.0	4.5	113.2	0.0	41.1	22.9	177.2
A3-B	Institutional	130		10.30		10.30		1540	1540	3.67	0.0	8.9	2.9	113.2	8.9	43.9	22.9	189.0
A3-C	Medium Density Residential	130			5.19	5.19	162.0	841	2381	3.53	0.0	0.0	1.5	113.2	8.9	45.4	34.0	201.6
A3-D	Commercial	130	0.58			0.58			2381	3.53	0.5	0.0	0.2	113.7	8.9	45.6	34.0	202.2
A3-E	Low Density Residential	130			35.68	35.68	95.2	3397	5778	3.19	0.0	0.0	10.0	113.7	8.9	55.5	74.6	252.8
A3-F	Medium Density Residential	130			8.26	8.26	162	1338	7116	3.10	0.0	0.0	2.3	113.7	8.9	57.9	89.4	269.9
A3-G	Institutional	130		0.90		0.90		1338	7116	3.10	0.0	0.8	0.3	113.7	9.7	58.1	89.4	270.9
A4	Low Density Residential	130			34.44	34.44	95.2	3279	10395	2.94	0.0	0.0	9.6	113.7	9.7	67.8	123.7	314.9
A2-C	Commercial (ex. snow dump)	120	15.25			15.25			10395	2.94	13.2	0.0	4.3	127.0	9.7	72.0	123.7	332.4
A3-H	Low Density Residential	120			6.09	6.09	95.2	580	10974	2.91	0.0	0.0	1.7	127.0	9.7	73.7	129.6	340.0
A5	Commercial	110	17.72			17.72			10974	2.91	15.4	0.0	5.0	142.4	9.7	78.7	129.6	360.3
A6-A	Commercial	100	15.18			15.18			10974	2.91	13.2	0.0	4.3	155.5	9.7	82.9	129.6	377.8
A6-B	Institutional	100		6.05		6.05			10974	2.91	0.0	5.3	1.7	155.5	15.0	84.6	129.6	384.7
A6-C	Medium Density Residential	90			4.87	4.87	162.0	789	11763	2.88	0.0	0.0	1.4	155.5	15.0	86.0	137.4	393.9
A6-D	Low Density Residential	90			17.56	17.56	95.2	1672	13435	2.83	0.0	0.0	4.9	155.5	15.0	90.9	153.8	415.2
A6-E	Low Density Residential	90			6.94	6.94	95.2	661	14096	2.81	0.0	0.0	1.9	155.5	15.0	92.9	160.2	423.6
A7-A	Commercial	90	13.62			13.62			14096	2.81	11.8	0.0	3.8	167.4	15.0	96.7	160.2	439.2
A7-B	High Density Residential	90			11.01	11.01	135.0	1486	15582	2.76	0.0	0.0	3.1	167.4	15.0	99.8	174.3	456.4
A7-C	Medium Density Residential	90			6.97	6.97	162.0	1129	16711	2.73	0.0	0.0	2.0	167.4	15.0	101.7	184.9	468.9
A7-D	Medium Density Residential	90			11.74	11.74	162.0	1902	18613	2.68	0.0	0.0	3.3	167.4	15.0	105.0	202.4	489.7
A7-E1/E2	Medium Density Residential	90			9.24	9.24	162.0	1497	20110	2.65	0.0	0.0	2.6	167.4	15.0	107.6	215.9	505.8
A8-A	Commercial	80	28.45			28.45			20110	2.65	24.7	0.0	8.0	192.0	15.0	115.5	215.9	538.5
A8-B	High Density Residential	80			39.34	39.34	135.0	5311	25421	2.55	0.0	0.0	11.0	192.0	15.0	126.6	262.4	596.0
A8-C	Institutional	80		10.52		10.52			25421	2.55	0.0	9.1	2.9	192.0	24.1	129.5	262.4	608.1
A8-D	Low Density Residential	80			16.87	16.87	120.9	2040	27461	2.52	0.0	0.0	4.7	192.0	24.1	134.2	279.8	630.2
ROW Along SNC Sewer Alignment	-	80				14.34			27461	2.52	0.0	0.0	4.0	192.0	24.1	138.2	279.8	634.2
TOTAL		80	221.24	27.77	230.38	493.73	-	27461	27461	2.52	192.0	24.1	134.2	192.0	24.1	138.2	279.8	634.2

Residential Land Use	Population Density (Units / ha)	Persons per Unit	Persons per ha
Low Density (singles and semis)	26 - 28 (28 used)	2.7 - 3.4 (3.4 used)	95.2
Medium Density (row/townhouse)	50 - 60 (60 used)	2.7	162.0
High Density (apartments)	60 - 75 (75 used)	1.8	135.0

Notes:

- Harmon Equation = $1 + [14 / (4 + (P/1000)^{1/2})] \times K$
 Where: P = population; K = correction factor = 1.0
- Institutional / Commercial Peaking Factor = 1.5

Reported Design Flows / Assumptions:

- Area A4: Existing single family units currently serviced by Jockvale pump station to be redirected to SNC
- Area A8-D: proposed 600 medium density residential units

THIS PRIOR NOVATECH SNC DESIGN SHEET HAD DESIGN FLOWS AT 423.6 L/S AFTER AREA ID "A6-E".

THE DSEL EVALUATION WITH NEW PARAMETERS AT THIS SAME NODE WITH CONSERVANCY WEST AND EAST INCLUDED IS ~401.58 < 423.6 L/S

Attachment 3
Sanitary Sewer Design Sheets (Phase 2)

SOUTH NEPEAN COLLECTOR (PHASE 2)
SANITARY SEWER DESIGN SHEET

MAY 26, 2016
JOB# 115075



LOCATION			Area					Population				Individual Design Flows			Cumulative Design Flows				PROPOSED SEWER							
From MH	To MH	Upstream Node	Gross Commercial Area (ha)	Gross Institutional Area (ha)	Gross Residential Area (ha)	Right-of-Way (ha)	Total Gross Area (ha)	Residential Population Density (people / ha)	Individual Residential Population	Cumulative Residential Population	Residential Peaking Factor (Harmon Eqn ¹)	Commercial Peak Flow Rate ² (50,000 L/ha/d) (L/s)	Institutional Peak Flow Rate ² (50,000 L/ha/d) (L/s)	Infiltration / Inflow Rate (0.28 L/s/ha) (L/s)	Commercial (L/s)	Institutional (L/s)	Infiltration / Inflow (L/s)	Residential Peak Flow Rate (350 L/cap/d) (L/s)	Cumulative Peak Design Flow (L/s)	Length (m)	Pipe Size (mm)	Type	Slope %	Capacity (L/s)	Full Flow Velocity (m/s)	Ratio (Q/Qfull)
MHSA 1	MHSA 2	90	192.79	17.25	174.17	0.00	384.21	1678	20110	20110	2.65	167.352	14.97	107.58	167.4	15.0	107.6	215.9	505.8	57.3	900	CONC	0.10	597.2	0.91	85%
MHSA 2	MHSA 3	90																	505.8	57.3	900	CONC	0.10	597.2	0.91	85%
MHSA 3	MHSA 4	90																	505.8	73.9	900	CONC	0.10	597.2	0.91	85%
MHSA 4	MHSA 5	90																	505.8	34.6	900	CONC	0.10	597.2	0.91	85%
MHSA 5	MHSA 6	90																	505.8	42.8	900	CONC	0.10	597.2	0.91	85%
MHSA 6	MHSA 7	90																	505.8	84.4	900	CONC	0.10	597.2	0.91	85%
MHSA 7	MHSA 8	90																	505.8	16.5	900	CONC	0.10	597.2	0.91	85%
MHSA 8	MHSA 9	90																	505.8	85.4	900	CONC	0.10	597.2	0.91	85%
MHSA 9	MHSA 10	90																	505.8	70.6	900	CONC	0.10	597.2	0.91	85%
MHSA 10	MHSA 11	90																	505.8	70.6	900	CONC	0.10	597.2	0.91	85%
MHSA 11	MHSA 12	90																	505.8	77.8	900	CONC	0.10	597.2	0.91	85%
MHSA 12	MHSA 13	90																	505.8	77.8	900	CONC	0.10	597.2	0.91	85%
MHSA 13	MHSA 14	90																	505.8	77.8	900	CONC	0.10	597.2	0.91	85%
MHSA 14	MHSA 15	90																	505.8	25.4	900	CONC	0.10	597.2	0.91	85%
MHSA 15	MHSA 16	90																	505.8	34.2	900	CONC	0.10	597.2	0.91	85%
MHSA 16	MHSA 17	90																	505.8	86.7	900	CONC	0.10	597.2	0.91	85%
MHSA 17	MHSA 18	90																	505.8	34.3	900	CONC	0.10	597.2	0.91	85%
MHSA 18	MHSA 19	90																	505.8	68.6	900	CONC	0.10	597.2	0.91	85%
MHSA 19	MHSA 20	90																	505.8	65.5	900	CONC	0.10	597.2	0.91	85%
MHSA 20	MHSA 21	80	221.24	27.77	230.38	14.34	493.73	256	7351	27461	2.52	192.049	24.11	138.24	192.0	24.1	138.2	279.8	634.2	18.2	1050	CONC	0.10	900.9	1.01	70%
MHSA 21	MHSA 22	80																	634.2	81.9	1050	CONC	0.10	900.9	1.01	70%
MHSA 22	MHSA 23	80																	634.2	84.7	1050	CONC	0.10	900.9	1.01	70%
MHSA 23	MHSA 24	80																	634.2	77.4	1050	CONC	0.10	900.9	1.01	70%
MHSA 24	MHSA 25	80																	634.2	45.5	1050	CONC	0.10	900.9	1.01	70%
MHSA 25	MHSA 26	80																	634.2	35.8	1050	CONC	0.10	900.9	1.01	70%
MHSA 26	MHSA 27	80																	634.2	83.3	1050	CONC	0.10	900.9	1.01	70%
MHSA 27	MHSA 28	80																	634.2	74.4	1050	CONC	0.10	900.9	1.01	70%
MHSA 28	MHSA 29	80																	634.2	77.3	1050	CONC	0.10	900.9	1.01	70%
MHSA 29	MHSA 30	80																	634.2	83.8	1050	CONC	0.10	900.9	1.01	70%
MHSA 30	MHSA 31	80																	634.2	42.3	1050	CONC	0.10	900.9	1.01	70%
MHSA 31	MHSA 32	80																	634.2	100.6	1050	CONC	0.10	900.9	1.01	70%
MHSA 32	MHSA 33	80																	634.2	13.9	1050	CONC	0.10	900.9	1.01	70%
MHSA 33	MHSA 34	80																	634.2	99.9	1050	CONC	0.10	900.9	1.01	70%
MHSA 34	MHSA 35	80																	634.2	99.9	1050	CONC	0.10	900.9	1.01	70%
MHSA 35	MHSA 36	80																	634.2	88.7	1050	CONC	0.10	900.9	1.01	70%
MHSA 36	MHSA 37	80																	634.2	88.8	1050	CONC	0.10	900.9	1.01	70%
MHSA 37	MHSA 38	80																	634.2	90.3	1050	CONC	0.10	900.9	1.01	70%
MHSA 38	MHSA 39	80																	634.2	87.5	1050	CONC	0.10	900.9	1.01	70%

Design Parameters:

Residential Land Use	Population Density (Units / ha)	Persons per Unit	Persons per ha
Low Density (singles / semis)	26 - 28 (28 used)	2.7 - 3.4 (3.4 used)	95.2
Medium Density (row / townhouse)	50 - 60 (60 used)	2.7	162.0
High Density (apartments)	60 - 75 (75 used)	1.8	135.0

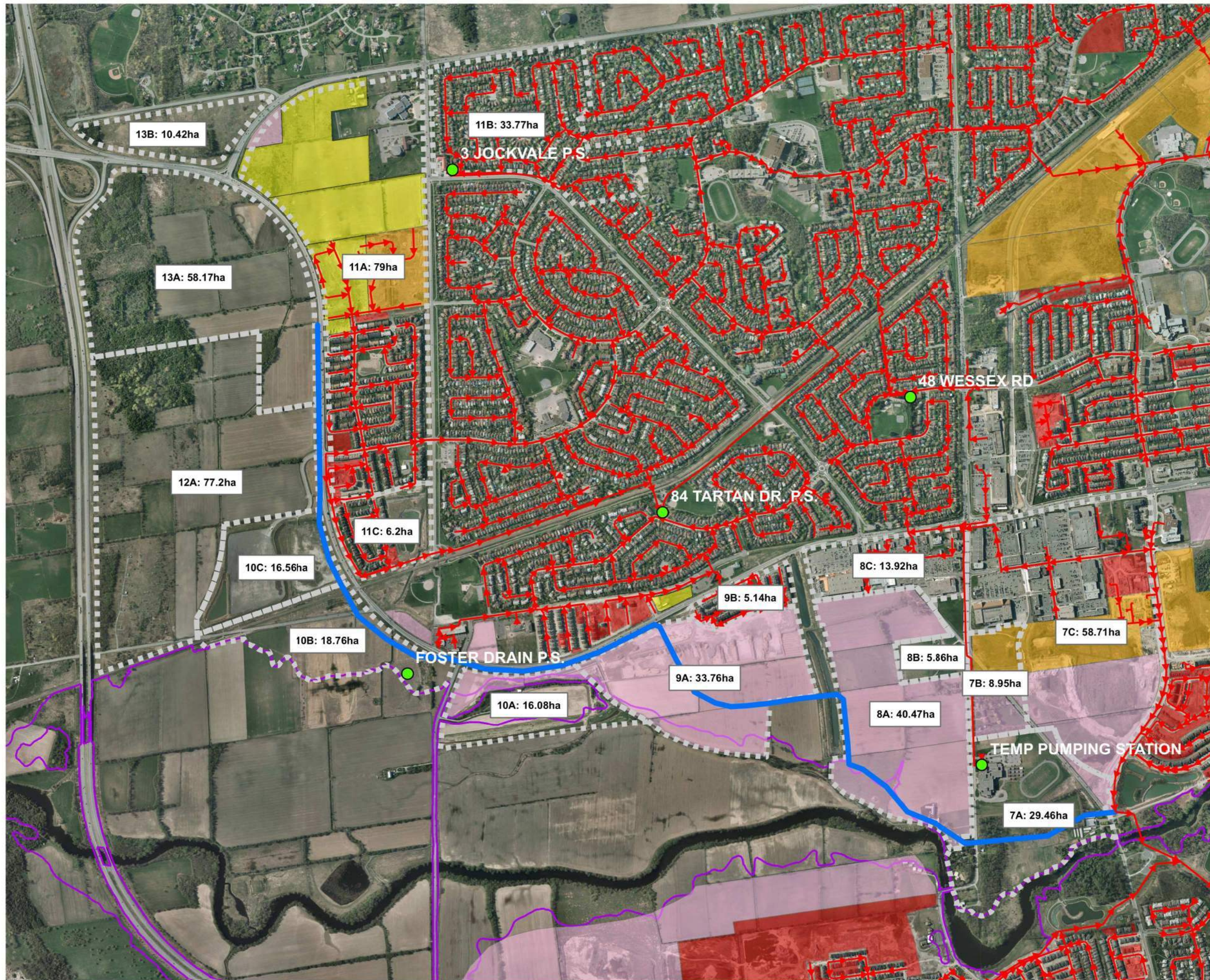
Notes:

- Harmon Equation = $1 + [14 / (4 + (P/1000)^{1/2})] \times K$
Where: P = population; K = correction factor = 1.0
- Institutional / Commercial Peaking Factor = 1.5

Reported Design Flows / Assumptions:

- Area A4: Existing single family units currently serviced by Jockvale pump station to be redirected to SNC
- Area A8-D: proposed 600 medium density residential units

Figure 01
Existing Sanitary Network and Collection Areas



- Pump Station
 - Existing Sanitary Main (With Flow Direction)
 - Proposed Alignment for South Nepean Collector
 - Collection Area
- DEVELOPMENT STATUS**
- Registered
 - Draft Approved
 - Pending
 - No Plan
 - Floodplain

NOT TO SCALE



MAP DRAWING INFORMATION:
DATA PROVIDED BY THE CITY OF OTTAWA

MAP CREATED BY: BC
MAP CHECKED BY: MBM
MAP PROJECTION: NO PROJECTION

FILE LOCATION: \\Dillon.ca\dillon_dfs\Ottawa\Ottawa_GA\CAD\2011\115681\Design_GIS\MXD\Figure01c_ExistingSanitaryNetwork.mxd

Table 5.1: Allocation of Commercial/Institutional and Residential Demands to SNC by Collection Area

Collection Area	Discharging Node	Estimated from GIS			City of Ottawa VURL Data			Other Space ¹ (ha)	Population (PE)	Residential Density (PE/net ha)	Comments	Additional Source(s)
		Gross Institutional/Commercial (ha)	Gross Residential (ha)	Gross Area (ha)	Net Residential (ha)	Units (#)	Unit Density (#/ha)					
7A	70	13.5	7.4	29.5	4.0	605	0.3	9.1	1637	4.25	Flow calculations include St Joseph H.S. Pump Station firm capacity of 7.0 L/s Additional 600 units (TAC)	3.4ppu (TAC)
7B		0.0	9.24	9.24	6.23	1474	136.7	3.0	3321	638.8	Population from split VURL allocated by area. VURL parcel id 323 - inconsistency between net and gross reported area.	2.7ppu (TAC)
8A		0.0	40.0	40.0	24.1	4462	185.1	15.9	12047.4	499.9		2.7ppu (TAC)
8B		5.9	0.0	5.9	0.0	0	0	0.0			Future Commercial area	
8C		13.9	0.0	13.9	0.0	0	0	0.0			Commercial area includes Home Depot	
9A	80	0.0	33.8	33.8	18.6	635	34.1	15.2	2210	116.2		3.4ppu (TAC)
10A	90	0.0	16.1	16.1	9.7	451	28.0	6.4	1533.4	158.0	Assume net population = 60% gross.	3.4ppu (TAC)
10B	100	18.8	0.0	35.3	0.0	0	0	16.5			Allocated as potential future I/C use as directed by TAC	
10C	110	16.6	0.0	35.3	0.0	0	0	18.7			Area includes current Municipal Snow Dump. Flow allowance is made for potential future I/C use	
11C		0.0	6.2	6.2	Note 2			2.5	306	82.7	This area is south of '11 block' in the existing development	From IBI Apr 2010 Report Figure 1
11A	120	12.5	66.5	79.0				26.6	3923	98.3	Institutional includes 4.38ha church site and 6.89 ha institution at northeast corner, as well and Claridge Commercial (0.56ha) and DCR/Phoenix Commercial (0.64ha)	From IBI Apr2010 Report Figure 1
11B		0.0	37.0	37.0				14.8	1550	69.8	Presently serviced by Jockvale pump station; to be redirected to SNC.	Estimated from 2011 Census Block data
12A		77.2	0.0	77.2				0.0			Allow sanitary peak flow 79.0 L/s	Novatech, Employment Lands Report, Revised Jan 2012
13A	130	58.5	0.0	58.5				0.0			Allow sanitary peak flow 62.8 L/s plus Collection Area 13B, total 82.2 L/s	
13B		12.5	0.0	12.5	0.0			Allow sanitary peak flow 19.4 L/s; gravity discharge to Collection Area 13A	IBI/Novatech			

Notes:

1. Other space includes other residential space accounting for the difference between gross area (measured with GIS) and net area (provided in VURL data), such as sidewalks, roads, greenspace, etc.
2. Collection Area 11A and 11B population and land use as identified under Additional Source(s). Other space reported as 60% of gross residential area, consistent with VURL average.

SOUTH NEPEAN COLLECTOR SEWER
SANITARY SEWER DESIGN SHEET - Operational Service (Average Flow Design Parameters)

Sheet 1 of 1

TRIBUTARY AREA	Design Factors	LOCATION		AREA (ha)						INDIVIDUAL		CUMULATIVE		RESIDENTIAL		COMMERCIAL & INSTITUTION			INFL. INFLOW	PEAK DESIGN	FROPOSED SEWER										OPERATIONAL DESIGN											
		FROM	TO	Gross ICI	Net ICI	Other ICI space (Green, Sidewalks, roads)	Gross RESIDENTIAL Area	Net Residential Area	Other Res (Green, Sidewalks, roads)	TOTAL AREA (Gross ICI plus Gross Residential)	POP	DENSITY (po./ha.)	POP	AREA (ha.)	PEAKING FACTOR	RESIDENT. FLOW (L/s)	PEAKING FACTOR	CUM. AREA	I.C.I. FLOW (l/s)	Q(p)	FLOW Q(d)	LENGTH (m)	GROUND ELEVATION (m)	DEPTH OF COVER (m)	PIPE SIZE (m)	INVERT 1 (m)	INVERT 2 (m)	PIPE TYPE	GRADE	CAPACITY (L/s)	Q(d)/Q(c)	VELOCITY at capacity (m/s)	DEPTH (m)	VELOCITY (m/s)								
13A	1			0.0	0.0	0.0	0.0	0.0	0.0	0		0	0.0	4.50	0.00	1.00	0.00	0.00	0.00	0.00																						
13B	1		Node 130	0.0	0.0	0.0	0.0	0.0	0.0	0		0	0.0	4.50	0.00	1.00	0.00	0.00	0.00	0.00																						
12A	1		Node 130	0.0	0.0	0.0	0.0	0.0	0.0	0		0	0.0	4.50	0.00	1.00	0.00	0.00	0.00	0.00																						
11A	1			12.5	9.4	3.1	66.5	8.0	58.5	79.0	1196	148.76	1196	79.0	3.75	15.57	1.00	12.50	2.00	3.95	21.52																					
11B	1		Node 120	0.0	0.0	0.0	37.0	22.2	14.8	37.0	1550	69.82	2746	116.0	3.47	33.13	1.00	12.50	2.00	5.80	40.93	531.89	93.60	4.42	0.750	88.96	88.43	Conc.	0.10%	353.24	0.13	0.80	0.20	0.58								
11C	1		Node 120	0.0	0.0	0.0	6.2	3.7	2.5	6.2	306	82.26	3052	122.2	3.44	36.41	1.00	12.50	2.00	6.11	44.82																					
10C	1		Node 110	16.6	12.5	4.2	0.0	0.0	0.0	16.6	0		0	3052	138.8	3.44	36.41	1.00	29.10	4.66	6.94	497.82	93.44	4.76	0.750	88.43	87.93	Conc.	0.10%	353.24	0.14	0.80	0.20	0.58								
10B	1		Node 110	0.0	0.0	0.0	0.0	0.0	0.0	0		0	3052	138.8	3.44	36.41	1.00	29.10	4.66	6.94	603.17	93.03	4.95	0.750	87.93	87.33	Conc.	0.10%	353.24	0.14	0.80	0.20	0.58									
10A	1		Node 100	0.0	0.0	0.0	0.0	0.0	0.0	0		0	3052	138.8	3.44	36.41	1.00	29.10	4.66	6.94	430.49	93.75	6.03	0.825	87.33	86.90	Conc.	0.10%	455.17	0.11	0.85	0.21	0.61									
9A	1		Node 90	0.0	0.0	0.0	0.0	0.0	0.0	0		0	3052	138.8	3.44	36.41	1.00	29.10	4.66	6.94	1268.65	92.37	5.84	0.900	86.90	85.63	Conc.	0.10%	573.71	0.08	0.90	0.18	0.56									
8A	1		Node 80	0.0	0.0	0.0	0.0	0.0	0.0	0		0	3052	138.8	3.44	36.41	1.00	29.10	4.66	6.94																						
8B	1			5.9	4.4	1.5	0.0	0.0	0.0	5.9	0		0	3052	144.7	3.44	36.41	1.00	35.00	5.60	7.24																					
8C	1			13.9	10.4	3.5	0.0	0.0	0.0	13.9	0		0	3052	188.6	3.44	36.41	1.00	48.90	7.82	7.93																					
7A	1			13.5	10.1	3.4	16.0	1.4	14.6	29.5	17	12.14	3069	188.1	3.43	36.59	1.00	62.40	9.98	9.41																						
7B	1		Node 70	0.0	0.0	0.0	0.0	0.0	0.0	0		0	3069	188.1	3.43	36.59	1.00	62.40	9.98	9.41	1448.98	91.24	6.01	1.050	85.63	84.18	Conc.	0.10%	864.51	0.06	1.00	0.18	0.56									
										188.1																																
										DEFAULTS																																
										q=AVERAGE DAILY FLOW	300	L/CAP.D																														
										l=UNIT OF PEAK EXTR.FLOW	0.050	L/ha.s																														
										Mannings 'n'	0.013																															
										q=AVERAGE COMMERCIAL AND INSTITUTIONAL	0.16	L/ha.s																														
DESIGN		DJG																																								
CHECKED																																										
TODAY:		7/18/2012																																								



Project 11-5681

**SOUTH NEPEAN COLLECTOR SEWER
SANITARY SEWER DESIGN SHEET - Full Service (Peak Flow Design Parameters)**

Sheet 1 of 1

TRIBUTARY AREA	Design Factors	LOCATION		AREA (ha)						INDIVIDUAL		CUMULATIVE		RESIDENTIAL		COMMERCIAL & INSTITUTION			INFL. INFLOW (L/s)	PEAK DESIGN FLOW Q(d) (L/s)	PROPOSED SEWER					PEAK DESIGN											
		FROM	TO	Gross ICI	Net ICI	Other ICI space (Green, Sidewalks, roads)	Gross RESIDENTIAL Area	Net Residential Area	Other Res (Sidewalks, roads)	TOTAL AREA (Gross ICI plus Gross Residential)	POP	DENSITY (pers/net ha.)	POP	Total I/C and Res AREA (ha.)	PEAKING FACTOR	RESIDENT. FLOW (L/s)	PEAKING FACTOR	I/C CUM. AREA			I/C FLOW (l/s)	Q(p) (L/s)	LENGTH (m)	GROUND ELEVATION (m)	DEPTH OF COVER (m)	PIPE SIZE (m)	INVERT 1 (m)	INVERT 2 (m)	PIPE TYPE	GRADE	CAPACITY (L/s)	Q(d)/Q(c)	VELOCITY at capacity (m/s)	DEPTH (m)	VELOCITY (m/s)		
13A	1			58.5	43.9	14.6	0.0	0.0	0.0	58.5	0	0	58.5	4.50	0.00	1.50	58.50	50.90	16.38	67.28																	
13B	1		Node 130	12.5	9.4	3.1	0.0	0.0	0.0	12.5	0	0	71.0	4.50	0.00	1.50	71.00	61.77	19.88	81.65																	
12A	1	Node 130		77.2	57.9	19.3	0.0	0.0	0.0	77.2	0	0	148.2	4.50	0.00	1.50	148.20	128.93	41.50	170.43																	
11A	1			12.5	9.4	3.1	66.5	39.9	26.6	79.0	3923	98.32	3923	227.2	3.34	53.09	1.50	160.70	139.81	63.62	256.52																
11B	1		Node 120	0.0	0.0	0.0	37.0	22.2	14.8	37.0	1550	69.82	5473	264.2	3.21	71.13	1.50	160.70	139.81	73.98	284.92	531.89	93.60	4.42	0.750	88.96	88.43	Conc.	0.10%	353.24	0.81	0.80	0.53	0.90			
11C	1	Node 120		0.0	0.0	0.0	6.2	3.7	2.5	6.2	306	82.26	5779	270.4	3.19	74.59	1.50	160.70	139.81	75.71	290.11																
10C	1		Node 110	16.6	12.5	4.2	0.0	0.0	0.0	16.6	0	0	5779	287.0	3.19	74.59	1.50	177.30	154.25	80.36	309.20	497.82	93.44	4.76	0.750	88.43	87.93	Conc.	0.10%	353.24	0.88	0.80	0.55	0.91			
10B	1	Node 110	Node 100	18.8	14.1	4.7	0.0	0.0	0.0	18.8	0	0	5779	305.8	3.19	74.59	1.50	196.10	170.61	85.62	330.82	603.17	93.03	4.95	0.750	87.93	87.33	Conc.	0.10%	353.24	0.94	0.80	0.58	0.92			
10A	1	Node 100	Node 90	0.0	0.0	0.0	16.1	9.7	6.4	16.1	1533	158.04	7312	321.9	3.09	91.48	1.50	196.10	170.61	90.13	352.22	430.49	93.75	6.03	0.825	87.33	86.90	Conc.	0.10%	455.17	0.77	0.85	0.55	0.95			
9A	1	Node 90	Node 80	0.0	0.0	0.0	33.8	18.6	15.2	33.8	2161	116.18	9473	355.7	2.98	114.28	1.50	196.10	170.61	99.60	384.48	1268.65	92.37	5.84	0.900	86.90	85.63	Conc.	0.10%	573.71	0.67	0.90	0.55	0.97			
8A	1	Node 80		0.0	0.0	0.0	40.0	24.1	15.9	40.0	12047	499.88	21520	395.7	2.62	228.45	1.50	196.10	170.61	110.80	509.85																
8R	1			5.9	4.4	1.5	0.0	0.0	0.0	5.9	0	0	21520	401.6	2.62	228.45	1.50	202.00	175.74	112.45	516.64																
8C	1			13.9	10.4	3.5	0.0	0.0	0.0	13.9	0	0	21520	415.5	2.62	228.45	1.50	215.90	187.83	116.34	532.62																
7A	1			13.5	10.1	3.4	16.5	5.2	11.3	30.0	1637	314.81	23157	445.5	2.59	242.84	1.50	229.40	199.58	124.74	567.6																
7B	1		Node 70	0.0	0.0	0.0				9.2	3980	638.84	27137	454.7	2.52	277.05	1.50	229.40	199.58	127.32	603.94	1448.98	91.24	6.01	1.050	85.63	84.18	Conc.	0.10%	864.51	0.70	1.00	0.64	1.07			
							225.3	129.7		454.7	27,137.0											4,781.0															
DESIGN CHECKED TODAY:		DJG																																			
		7/18/2012																																			

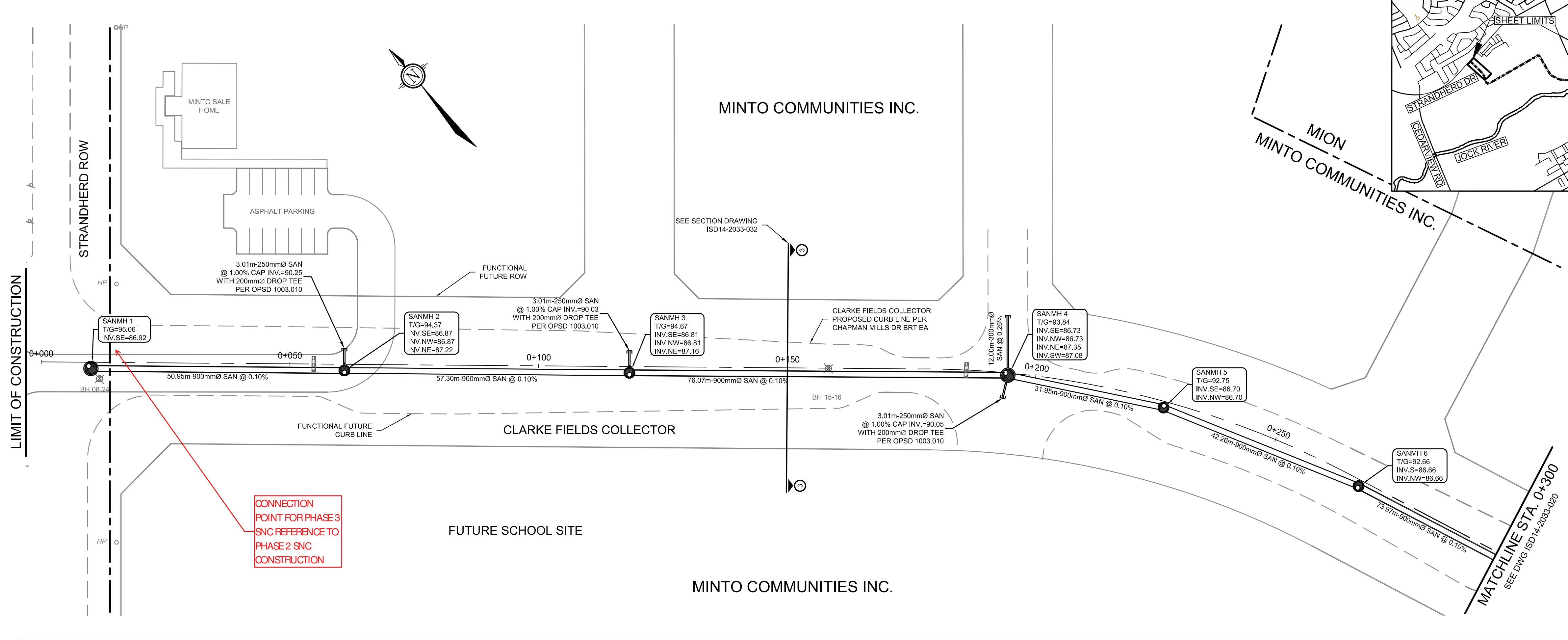
DEFAULTS

q=AVERAGE DAILY FLOW 350 L/CAP.D
I=UNIT OF PEAK EXTR.FLOW 0.280 L/ha.s
Mannings 'n' 0.013

q=AVERAGE COMMERCIAL AND INSTITUTIONAL 0.58 L/ha.s



Project 11-5681



CITY OF OTTAWA
SOUTH NEPEAN COLLECTOR (SNC)
SEWER PHASE 2 - STRANDHERD DRIVE
TO JOCKVALE ROAD

PLAN AND PROFILE
STA. 0+000 TO 0+300

Contract No. **ISD14-2033** Dwg. No. **019**
Sheet 19 of 51

Asset No. _____ Asset Group **ISD**

Wayne Newell, P. Eng. General Manager
Jonathan Knoyle, P. Eng. Senior Engineer

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PROFESSIONAL ENGINEER
M.A. BISSETT
PROVINCE OF ONTARIO

Des. RJD Chk'd. ERD
Dwn. NCS Chk'd. RJD
Utility Circ. No. _____ Index No. _____
Const. Inspector _____

Scale: HORIZONTAL 1:500
VERTICAL 1:100

NOTE: The location of utilities is approximate only, the exact location should be determined by consulting the municipal authorities and utility companies concerned. The contractor shall prove the location of utilities and shall be responsible for adequate protection from damage.

No.	Description	By	Date (dd/mm/yy)
1.	ISSUED FOR PRELIMINARY DESIGN CIRCULATION	ERD	21/12/15
2.	CHANGES TO ORIENTATION ACROSS KB SWM FACILITY	ERD	16/02/16
3.	ISSUED FOR PRELIMINARY DESIGN REPORT	ERD	02/03/16
4.	ISSUED FOR FINAL DESIGN CIRCULATION	ERD	29/04/16
5.	ISSUED FOR MOECC ECA APPLICATION	ERD	26/05/16
6.	ISSUED FOR TENDER	ERD	20/06/16
7.	ISSUED FOR CONSTRUCTION	ERD	30/08/16
8.	SEWER ALIGNMENT SHIFT ON GREENBANK	ERD	16/09/16
9.	REVISED PER MION SERVICING	ERD	08/12/16

LEGEND

EXISTING ITEMS

- WATERMAIN
- WATERMAIN VALVE
- STORM SEWER
- STORM MH
- CATCH BASIN & LEAD
- CULVERT
- STORM STRUCTURE
- SANITARY SEWER
- SANITARY MH

PROPOSED ITEMS

- SANITARY SEWER
- SANITARY MH & LID
- CULVERT
- FUTURE STRUCTURE T/G ADJUSTMENT

- NOTES:**
- CONCRETE PRESSURE PIPE SHALL BE AWWA C301 (L) CL-16. FITTING SHALL BE DESIGNED TO THE SAME CRITERIA AS THE ADJACENT PIPE.
 - CONTRACTOR TO PROVIDE PIPE CLASS CALCULATIONS, AS PER AWWA C304 (DESIGN OF PRESTRESSED CONCRETE CYLINDER PIPE), BY THE PIPE MANUFACTURER, SIGNED AND SEALED BY A PROFESSIONAL ENGINEER LICENSED IN THE PROVINCE OF ONTARIO.
 - PIPE EMBEDMENT SHALL BE AS PER CITY OF OTTAWA DETAIL S6. SAND MAY BE USED AS PIPE COVER MATERIAL ABOVE THE SPRINGLINE.
 - A CLOTH DIAPER APPROVED BY THE PIPE MANUFACTURE SHALL BE PLACED AROUND EACH EXTERIOR JOINT RECESS AND FASTENED IN PLACE WITH EITHER WIRE OR STEEL STRAPPING STITCHED INTO ITS EDGES.
 - THE JOINT SHALL BE FILLED WITH MORTAR IN ONCE CONTINUOUS OPERATION AND PATTED OR MANIPULATED TO SETTLE THE MORTAR AND EXPEL AND ENTRAPPED AIR.
 - INTERIOR JOINTS SHALL BE FILLED WITH MORTAR AFTER BACKFILLING AND FINISHED SMOOTH WITH A TROWEL. CEMENT USED SHALL MEET THE REQUIREMENTS OF TYPE HS CEMENT (HIGH-SULPHATE-RESISTANCE), OR APPROVED EQUIVALENT.
 - THE INTERIOR OF THE JOINTS SHALL BE PROTECTED FROM CORROSION WITH EPOXY AND ZINC COATING APPLIED DURING FABRICATION.
 - THE INTERIOR STRUCTURAL CONCRETE CORE SHALL BE MANUFACTURED WITH TYPE HS CEMENT (HIGH-SULPHATE-RESISTANCE), OR APPROVED EQUIVALENT.
 - SEE MANHOLE DETAIL DRAWINGS ISD14-2033-36 TO ISD14-2033-45 FOR ADDITIONAL DETAILS

MAINTENANCE HOLE DATA

MH ID	STATION	OFFSET	STRUCTURE	COVER	T/G ELEV.	LOW. INV.
1	0+010.00	1.25R	OPSD 701.013	S24/S25	95.06	86.92
2	0+060.95	1.25R	OPSD 701.012	S24/S25	94.37	86.87
3	0+118.25	1.25R	OPSD 701.012	S24/S25	94.67	86.81
4	0+194.38	0.46R	OPSD 701.013	S24/S25	93.84	86.73
5	0+226.51	1.25R	OPSD 701.012	S24/S25	92.75	86.70
6	0+269.14	1.25R	OPSD 701.012	S24/S25	92.66	86.66

SANITARY SEWER PIPE DATA

CONNECTED STRUCTURES & INVERTS	DIA (mm)	LENGTH (m)	MATERIAL
SANMH 1 = 86.92 SANMH 2 = 86.87	900	50.95	AWWA C-301 (L)
SANMH 2 = 86.87 SANMH 3 = 86.81	900	57.30	AWWA C-301 (L)
SANMH 3 = 86.81 SANMH 4 = 86.73	900	76.07	AWWA C-301 (L)
SANMH 4 = 86.73 SANMH 5 = 86.70 SANMH 6 = 86.73	900	31.95	AWWA C-301 (L)
SANMH 5 = 86.70 SANMH 6 = 86.66	900	42.26	AWWA C-301 (L)
SANMH 6 = 86.66 SANMH 7 = 86.59	900	73.97	AWWA C-301 (L)

STATION	EXISTING ELEVATION	CHAINAGE	DESCRIPTION	INVERT ELEVATION	CHAINAGE	EXISTING ELEVATION
0+000	83.47	0+000	SANMH 1 (2400mm \varnothing)	86.92	0+000	83.47
0+010	82.76	0+010	50.95m - 900mm \varnothing SAN	86.87	0+010	82.76
0+020	82.75	0+020	AWWA C-301 (L) @ 0.10%	86.87	0+020	82.75
0+030	82.75	0+030		86.87	0+030	82.75
0+040	82.75	0+040		86.87	0+040	82.75
0+050	82.75	0+050		86.87	0+050	82.75
0+060	82.75	0+060		86.87	0+060	82.75
0+070	82.75	0+070		86.87	0+070	82.75
0+080	82.74	0+080		86.87	0+080	82.74
0+090	82.74	0+090		86.87	0+090	82.74
0+100	82.74	0+100		86.87	0+100	82.74
0+110	82.72	0+110		86.81	0+110	82.72
0+118.25	82.67	0+118.25	SANMH 2 (1800mm \varnothing)	86.81	0+118.25	82.67
0+120	82.62	0+120		86.81	0+120	82.62
0+130	82.59	0+130		86.81	0+130	82.59
0+140	82.59	0+140		86.81	0+140	82.59
0+150	82.59	0+150		86.81	0+150	82.59
0+160	82.55	0+160		86.81	0+160	82.55
0+170	82.51	0+170		86.81	0+170	82.51
0+180	82.50	0+180		86.81	0+180	82.50
0+190	82.49	0+190		86.73	0+190	82.49
0+194.38	82.46	0+194.38	SANMH 3 (1800mm \varnothing)	86.73	0+194.38	82.46
0+200	82.46	0+200		86.73	0+200	82.46
0+210	82.48	0+210		86.73	0+210	82.48
0+220	82.47	0+220		86.70	0+220	82.47
0+226.51	82.45	0+226.51	SANMH 4 (2400mm \varnothing)	86.70	0+226.51	82.45
0+230	82.42	0+230		86.70	0+230	82.42
0+240	82.42	0+240		86.70	0+240	82.42
0+250	82.40	0+250		86.70	0+250	82.40
0+260	82.38	0+260		86.70	0+260	82.38
0+269.14	82.36	0+269.14	SANMH 5 (1800mm \varnothing)	86.66	0+269.14	82.36
0+270	82.34	0+270		86.66	0+270	82.34
0+280	82.34	0+280		86.66	0+280	82.34
0+290	82.32	0+290		86.66	0+290	82.32
0+300	82.29	0+300	SANMH 6 (1800mm \varnothing)	86.66	0+300	82.29

AS-BUILT

THESE AS-BUILT PLANS HAVE BEEN PREPARED BASED ON INFORMATION PROVIDED BY OTHERS. THE DESIGN PROFESSIONAL HAS NOT VERIFIED THE ACCURACY AND/OR THE COMPLETENESS OF THIS INFORMATION AND SHALL NOT BE RESPONSIBLE FOR ANY ERRORS OR OMISSIONS WHICH MAY BE INCORPORATED HEREIN AS A RESULT.



CITY OF OTTAWA
SOUTH NEPEAN COLLECTOR (SNC)
SEWER PHASE 2 - STRANDHERD DRIVE
TO JOCKVALE ROAD

PLAN AND PROFILE
STA. 0+300 TO 0+600

Contract No. **ISD14-2033** Dwg. No. **020**
Sheet **20** of **51**

Asset No. _____
Asset Group **ISD**

Wayne Newell, P.Eng. (General Manager) | Jonathan Knoyle, P.Eng. (Senior Engineer)

NOVATECH
200, 210 Murray Crescent Drive
Kanata, Ontario, Canada, K2M 1P6
Tel: (613) 754-9613 | Fax: (613) 754-9817
www.novatech.ca

Scale: HORIZONTAL 1:500
VERTICAL 1:100

NOTE: The location of utilities is approximate only, the exact location should be determined by consulting the municipal authorities and utility companies concerned. The contractor shall prove the location of utilities and shall be responsible for adequate protection from damage.

No.	Description	By	Date (dd/mm/yyyy)
1	ISSUED FOR PRELIMINARY DESIGN CIRCULATION	FRN	21/12/15
2	CHANGES TO ORIENTATION ACROSS KB SWM FACILITY	ERD	16/02/16
3	ISSUED FOR PRELIMINARY DESIGN REPORT	ERD	02/03/16
4	ISSUED FOR FINAL DESIGN CIRCULATION	ERD	29/04/16
5	ISSUED FOR MOECC ECA APPLICATION	ERD	26/05/16
6	ISSUED FOR TENDER	ERD	20/06/16
7	ISSUED FOR CONSTRUCTION	ERD	30/08/16
8	SEWER ALIGNMENT SHIFT ON GREENBANK	ERD	16/09/16
9	REVISED PER MION SERVICING	ERD	08/12/16
10	MINTO LANDS MANHOLE UPDATE	ERD	24/04/17
11	ISSUED FOR AS-BUILT	ERD	28/09/17

LEGEND

EXISTING ITEMS
WATERMAIN
WATERMAIN VALVE
STORM SEWER
STORM MH
CATCH BASIN & LEAD
CULVERT
STORM STRUCTURE
SANITARY SEWER
SANITARY MH

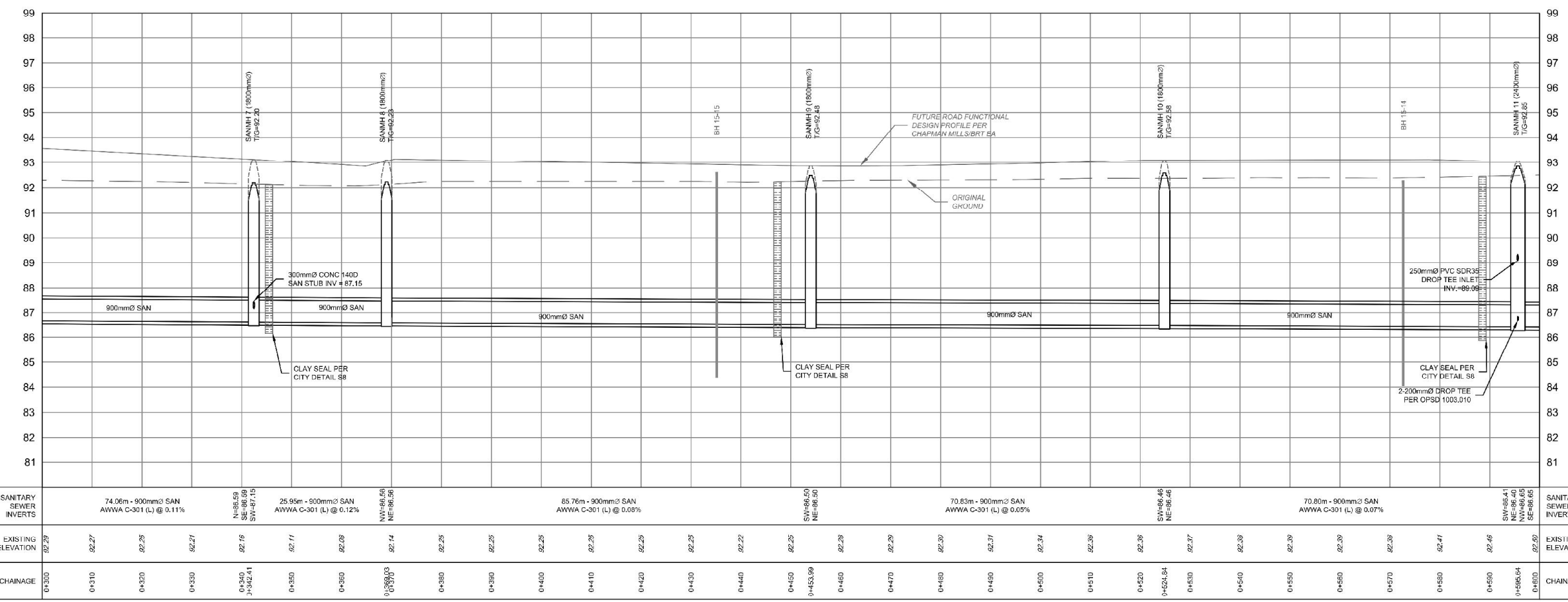
PROPOSED ITEMS
SANITARY SEWER
SANITARY MH & LID
CULVERT
FUTURE STRUCTURE T/G
ADJUSTMENT

- NOTES:**
- CONCRETE PRESSURE PIPE SHALL BE AWWA C301 (L) CL-16. FITTING SHALL BE DESIGNED TO THE SAME CRITERIA AS THE ADJACENT PIPE.
 - CONTRACTOR TO PROVIDE PIPE CLASS CALCULATIONS, AS PER AWWA C304 (DESIGN OF PRESTRESSED CONCRETE CYLINDER PIPE), BY THE PIPE MANUFACTURER. SIGNED AND SEALED BY A PROFESSIONAL ENGINEER LICENSED IN THE PROVINCE OF ONTARIO.
 - PIPE EMBEDMENT SHALL BE AS PER CITY OF OTTAWA DETAIL S6. SAND MAY BE USED AS PIPE COVER MATERIAL ABOVE THE SPRINGLINE.
 - A CLOTH DIAPHRAGM APPROVED BY THE PIPE MANUFACTURER SHALL BE PLACED AROUND EACH EXTERIOR JOINT RECESS AND FASTENED IN PLACE WITH EITHER WIRE OR STEEL STRAPPING STITCHED INTO ITS EDGES.
 - THE JOINT SHALL BE FILLED WITH MORTAR IN ONCE CONTINUOUS OPERATION AND PATTED OR MANIPULATED TO SETTLE THE MORTAR AND EXPEL AND ENTRAPPED AIR.
 - INTERIOR JOINTS SHALL BE FILLED WITH MORTAR AFTER BACKFILLING AND FINISHED SMOOTH WITH A TROWEL. CEMENT USED SHALL MEET THE REQUIREMENTS OF TYPE HS CEMENT (HIGH-SULPHATE-RESISTANCE), OR APPROVED EQUIVALENT.
 - THE INTERIOR OF THE JOINTS SHALL BE PROTECTED FROM CORROSION WITH EPOXY AND ZINC COATING APPLIED DURING FABRICATION.
 - THE INTERIOR STRUCTURAL CONCRETE CORE SHALL BE MANUFACTURED WITH TYPE HS CEMENT (HIGH-SULPHATE-RESISTANCE), OR APPROVED EQUIVALENT.
 - SEE MANHOLE DETAIL DRAWINGS ISD14-2033-36 TO ISD14-2033-45 FOR ADDITIONAL DETAILS

MH ID	STATION	OFFSET	STRUCTURE	COVER	T/G ELEV	LOW. INV.
7	0+342.41	1.41R	OPSD 701.012	S24/S25	92.20	86.59
8	0+369.03	1.50R	OPSD 701.012	S24/S25	92.23	86.56
9	0+453.99	0.07L	OPSD 701.012	S24/S25	92.48	86.50
10	0+524.84	0.04L	OPSD 701.012	S24/S25	92.58	86.46
11	0+595.64	0.41L	OPSD 701.013	S24/S25	92.85	86.40

CONNECTED STRUCTURES & INVERTS	DIA (mm)	LENGTH (m)	MATERIAL
SANMH 6 = 86.68 SANMH 7 = 86.59	900	74.06	AWWA C-301 (L)
SANMH 7 = 86.59 SANMH 8 = 86.56	900	25.95	AWWA C-301 (L)
SANMH 8 = 86.56 SANMH 9 = 86.50	900	85.76	AWWA C-301 (L)
SANMH 10 = 86.46 SANMH 9 = 86.50	900	70.83	AWWA C 301 (L)
SANMH 10 = 86.46 SANMH 11 = 86.41	900	70.80	AWWA C-301 (L)
SANMH 11 = 86.40 SANMH 12 = 86.32	900	78.15	AWWA C-301 (L)

Proposed connection from Conservancy East lands



EXISTING ELEVATION	CHAINAGE	DESCRIPTION	EXISTING ELEVATION	CHAINAGE	DESCRIPTION
82.29	0+300	SANITARY SEWER INVERTS	82.29	0+300	SANITARY SEWER INVERTS
82.27	0+310	74.06m - 900mm \varnothing SAN AWWA C-301 (L) @ 0.11%	82.27	0+310	74.06m - 900mm \varnothing SAN AWWA C-301 (L) @ 0.11%
82.25	0+320		82.25	0+320	
82.21	0+330		82.21	0+330	
82.16	0+340	N=86.59 SE=86.59 SW=87.15	82.16	0+340	N=86.59 SE=86.59 SW=87.15
82.11	0+350	25.95m - 900mm \varnothing SAN AWWA C-301 (L) @ 0.12%	82.11	0+350	25.95m - 900mm \varnothing SAN AWWA C-301 (L) @ 0.12%
82.08	0+360		82.08	0+360	
82.14	0+370	NW=86.56 NE=86.56	82.14	0+370	NW=86.56 NE=86.56
82.25	0+380		82.25	0+380	
82.25	0+390		82.25	0+390	
82.25	0+400		82.25	0+400	
82.25	0+410		82.25	0+410	
82.25	0+420		82.25	0+420	
82.25	0+430		82.25	0+430	
82.22	0+440		82.22	0+440	
82.25	0+450	SW=86.50 NE=86.50	82.25	0+450	SW=86.50 NE=86.50
82.25	0+460		82.25	0+460	
82.29	0+470		82.29	0+470	
82.30	0+480		82.30	0+480	
82.37	0+490		82.37	0+490	
82.37	0+500		82.37	0+500	
82.39	0+510		82.39	0+510	
82.39	0+520		82.39	0+520	
82.37	0+530	SW=86.46 NE=86.46	82.37	0+530	SW=86.46 NE=86.46
82.39	0+540		82.39	0+540	
82.39	0+550		82.39	0+550	
82.39	0+560		82.39	0+560	
82.39	0+570		82.39	0+570	
82.46	0+580		82.46	0+580	
82.46	0+590	SW=86.41 NE=86.40 SE=86.65	82.46	0+590	SW=86.41 NE=86.40 SE=86.65
82.59	0+600	SANITARY SEWER INVERTS	82.59	0+600	SANITARY SEWER INVERTS

SANITARY SEWER CALCULATION SHEET



Manning's n=0.013

STREET	LOCATION		RESIDENTIAL AREA AND POPULATION							PEAK FACT.	PEAK FLOW (l/s)	COMM		INSTIT		PARK		C+H	INFILTRATION				PIPE					VEL.	
	FROM M.H.	TO M.H.	AREA (ha)	UNITS	POP.	AREA (ha)	POP.	CUMULATIVE AREA (ha)	CUMULATIVE POP.			AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)		PEAK FLOW (l/s)	TOTAL AREA (ha)	ACCU. AREA (ha)	INFILT. FLOW (l/s)	TOTAL FLOW (l/s)	DIST (m)	DIA (mm)	SLOPE (%)	CAP. (FULL) (l/s)	RATIO Q act/Q cap	(FULL) (m/s)
Centerline13 - 13																													
	529A	530A	0.15		16	0.15	16	3.7	0.19		0.00	0.00	0.00	0.00	0.00	0.15	0.15	0.04	0.24	20.5	200	0.65	26.44	0.01	0.84	0.26			
			0.19		20	0.34	36			0.00	0.00	0.00	0.00	0.00	0.19	0.34													
	530A	534A	0.26		53	0.60	89	3.6	1.04		0.00	0.00	0.00	0.00	0.26	0.60	0.17	1.21	70.5	250	0.25	29.73	0.04	0.61	0.29				
			0.22		23	0.82	112			0.00	0.00	0.00	0.00	0.00	0.22	0.82													
	534A	531A	0.26		28	1.08	140	3.6	1.62		0.00	0.00	0.00	0.00	0.26	1.08	0.31	1.92	82.0	250	0.25	29.73	0.06	0.61	0.34				
						1.08	140			0.00	0.00	0.00	0.00	0.00		1.08													
Centerline9 - 09																													
	525A	527A	0.62		65	0.62	65	3.6	0.77		0.00	0.00	0.00	0.00	0.62	0.62	0.18	0.94	104.0	200	0.65	26.44	0.04	0.84	0.39				
						0.62	65			0.00	0.00	0.00	0.00	0.00		0.62													
Centerline6 - 06																													
	526A	527A	0.21		22	0.21	22	3.7	0.26		0.00	0.00	0.64	0.64	0.07	0.85	0.85	0.24	0.58	63.0	200	0.65	26.44	0.02	0.84	0.34			
	Contribution From Centerline9 - 09, Pipe 525A - 527A					0.62	65			0.00	0.00	0.00	0.00	0.00	0.62	1.47													
	527A	528A	0.12		12	0.95	99	3.6	1.15		0.00	0.00	0.64	0.07	0.12	1.59	0.45	1.68	44.5	200	0.35	19.40	0.09	0.62	0.37				
						0.95	99			0.00	0.00	0.64				1.59													
Centerline14 - 14																													
	523A	524A				0.00				1.47	1.47	0.00	0.00	0.48	1.47	1.47	0.42	0.90	26.5	200	0.65	26.44	0.03	0.84	0.39				
			0.25		26	0.25	26			1.47	0.00	0.00	0.00	0.00	0.25	1.72													
	524A	528A	0.45		47	0.70	73	3.6	0.86		1.47	0.00	0.00	0.48	0.45	2.17	0.62	1.95	117.5	200	0.35	19.40	0.10	0.62	0.39				
	Contribution From Centerline6 - 06, Pipe 527A - 528A					0.95	99			0.00	0.00	0.64	0.00	0.00	1.59	3.76													
	528A	531A	0.17		18	1.82	190	3.5	2.17		1.47	0.00	0.64	0.55	0.17	3.93	1.12	3.84	48.5	200	0.35	19.40	0.20	0.62	0.48				
						1.82	190			1.47	0.00	0.64				3.93													
Centerline8 - 08																													
	533A	522A	0.16		14	0.16	14	3.7	0.17		0.00	0.00	0.00	0.00	0.16	0.16	0.05	0.21	40.5	200	0.65	26.44	0.01	0.84	0.24				
	522A	520A				0.16	14	3.7	0.17		0.00	0.00	0.00	0.00	0.00	0.16	0.05	0.21	13.0	200	0.35	19.40	0.01	0.62	0.20				
	520A	521A	0.86		72	1.02	86	3.6	1.01		0.00	0.00	0.00	0.00	0.86	1.02	0.29	1.30	137.0	250	0.25	29.73	0.04	0.61	0.30				
						1.02	86			0.00	0.00	0.00	0.00	0.00		1.02													
Centerline15 - 15																													
	501A	503A	0.68		71	0.68	71	3.6	0.83		0.00	0.00	0.00	0.00	0.68	0.68	0.19	1.03	101.0	200	0.65	26.44	0.04	0.84	0.40				
						0.68	71			0.00	0.00	0.00	0.00	0.00		0.68													
	502A	503A	0.49		51	0.49	51	3.7	0.60		0.00	0.00	0.00	0.00	0.49	0.49	0.14	0.74	21.0	200	0.65	26.44	0.03	0.84	0.37				
						0.49	51			0.00	0.00	0.00	0.00	0.00		0.49													
Centerline4 - 04																													
	Contribution From Centerline15 - 15, Pipe 501A - 503A					0.68	71			0.00	0.00	0.00	0.00	0.00	0.68	0.68													
	Contribution From Centerline15 - 15, Pipe 502A - 503A					0.49	51			0.00	0.00	0.00	0.00	0.00	0.49	1.17													
	503A	509A	0.50		52	1.67	174	3.5	1.99		0.00	0.00	0.00	0.00	0.50	1.67	0.48	2.47	108.5	250	0.25	29.73	0.08	0.61	0.36				
						1.67	174			0.00	0.00	0.00	0.00	0.00		1.67													
Centerline2 - 02																													
	507A	508A	0.41		43	0.41	43	3.7	0.51		0.00	0.00	0.00	0.00	0.41	0.41	0.12	0.63	93.5	200	0.65	26.44	0.02	0.84	0.35				
						0.41	43			0.00	0.00	0.00	0.00	0.00		0.41													

Park Flow = 9300 L/ha/da Average Daily Flow = 280 l/p/day Comm/Inst Flow = 28000 L/ha/da Industrial Flow = 35000 L/ha/da Max Res. Peak Factor = 4.00 Commercial/Inst./Park Peak Factor = 1.00 Institutional = 0.32 l/s/ha	DESIGN PARAMETERS 0.10764 l/s/ha Industrial Peak Factor = as per MOE Graph Extraneous Flow = 0.286 L/s/ha Minimum Velocity = 0.600 m/s Manning's n = (Conc) 0.013 (Pvc) 0.013 Townhouse coeff= 2.7 Single house coeff= 3.4										Designed: A.S. Checked: W.L./V.W. Dwg. Reference: Sanitary Drainage Plan, Dwgs. No.	PROJECT: Barrhaven Conservancy East Phase 5 LOCATION: City of Ottawa					File Ref: Date: 01 Dec 2022	Sheet No. 1 of 2
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SANITARY SEWER CALCULATION SHEET

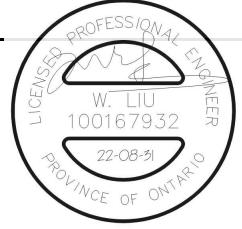


Manning's n=0.013

LOCATION			RESIDENTIAL AREA AND POPULATION								COMM		INSTIT		PARK		C+I	INFILTRATION			PIPE						VEL.			
STREET	FROM M.H.	TO M.H.	AREA (ha)	UNITS	UNITS Singles	UNITS Townhouse	POP.	AREA (ha)	POP.	PEAK FACT.	PEAK FLOW (l/s)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	PEAK FLOW (l/s)	TOTAL AREA (ha)	ACCU. AREA (ha)	INFILT. FLOW (l/s)	TOTAL FLOW (l/s)	DIST (m)	DIA (mm)	SLOPE (%)	CAP. (FULL) (l/s)	RATIO Q act/Q cap	(FULL) (m/s)	(ACT.) (m/s)	
Ainsworth Crescent																														
	80A	81A	0.51	10	10		34	0.51	34	3.68	0.41		0.00		0.00		0.00	0.00	0.51	0.51	0.17	0.57	69.0	200	0.65	26.44	0.02	0.84	0.34	
	81A	82A	0.38	11	11		38	0.89	72	3.62	0.85		0.00		0.00		0.00	0.00	0.38	0.89	0.29	1.14	70.0	250	0.25	29.73	0.04	0.61	0.29	
To Sapling Grove, Pipe 82A - 85A							0.89	72					0.00		0.00		0.00			0.89										
	78A	59A	0.07	1	1		4	0.07	4	3.76	0.05		0.00		0.00		0.00	0.07	0.07	0.02	0.07	13.0	200	0.65	26.44	0.00	0.84	0.17		
	59A	60A	0.45	11	11		38	0.52	42	3.66	0.50		0.00		0.00		0.00	0.45	0.52	0.17	0.67	76.0	250	0.25	29.73	0.02	0.61	0.24		
	60A	61A	0.41	12	12		41	0.93	83	3.61	0.97		0.00		0.00		0.00	0.41	0.93	0.31	1.28	75.0	250	0.25	29.73	0.04	0.61	0.30		
To Sapling Grove, Pipe 61A - 82A							0.93	83					0.00		0.00		0.00			0.93										
Syringa Court																														
	55A	56A	0.14	2	2		7	0.14	7	3.74	0.08		0.00		0.00		0.00	0.14	0.14	0.05	0.13	11.0	200	0.65	26.44	0.00	0.84	0.22		
	56A	57A	0.42	11	11		38	0.56	45	3.66	0.53		0.00		0.00		0.00	0.42	0.56	0.18	0.72	67.0	250	0.65	47.94	0.01	0.98	0.35		
	57A	58A	0.34	10	10		34	0.90	79	3.62	0.93		0.00		0.00		0.00	0.34	0.90	0.30	1.22	67.5	250	0.25	29.73	0.04	0.61	0.29		
To Sapling Grove, Pipe 58A - 61A							0.90	79					0.00		0.00		0.00			0.90										
	55A	53A	0.17	3	3		11	0.17	11	3.73	0.13		0.00		0.00		0.00	0.17	0.17	0.06	0.19	45.5	200	0.65	26.44	0.01	0.84	0.24		
	53A	49A	0.08	1	1		4	0.25	15	3.72	0.18		0.00		0.00		0.00	0.08	0.25	0.08	0.26	9.0	250	0.25	29.73	0.01	0.61	0.18		
	49A	50A	0.44	11	11		38	0.69	53	3.65	0.63		0.00		0.00		0.00	0.44	0.69	0.23	0.85	68.5	250	0.25	29.73	0.03	0.61	0.27		
	50A	51A	0.34	10	10		34	1.03	87	3.61	1.02		0.00		0.00		0.00	0.34	1.03	0.34	1.36	66.5	250	0.25	29.73	0.05	0.61	0.31		
To Sapling Grove, Pipe 51A - 58A							1.03	87					0.00		0.00		0.00			1.03										
Ecology Lane																														
	880A	88A	0.44	10	10		34	0.44	34	3.68	0.41		0.00		0.00		0.00	0.44	0.44	0.15	0.55	76.0	200	0.65	26.44	0.02	0.84	0.33		
Contribution From Sapling Grove, Pipe 85A - 88A							5.48	453					0.00		0.00		0.00		5.48	5.92										
	88A	91A	0.18	4	4		14	6.10	501	3.38	5.49		0.00		0.00		0.00	0.18	6.10	2.01	7.50	60.0	250	0.25	29.73	0.25	0.61	0.50		
Contribution From Peninsula Road, Pipe 90A - 91A							0.78	79					0.00		0.00		0.00		0.78	6.88										
	91A	92A	0.08				0	6.96	580	3.35	6.30		0.00		0.00		0.00	0.08	6.96	2.30	8.60	62.5	250	0.25	29.73	0.29	0.61	0.52		
To Conservancy Drive, Pipe 92A - 93A							6.96	580					0.00		0.00		0.00			6.96										
Anemone Mews																														
			0.09				0	0.09	0				0.00		0.00		0.00	0.09	0.09											
Contribution From Peninsula Road, Pipe 62A - 63A							0.95	90					0.00		0.00		0.00		0.95	1.04										
Contribution From Peninsula Road, Pipe 89A - 63A							0.17	14					0.00		0.00		0.00		0.17	1.21										
	63A	75A	0.09				0	1.30	104	3.59	1.21		0.00		0.00		0.00	0.09	1.30	0.43	1.64	62.5	250	0.25	29.73	0.06	0.61	0.32		
To Conservancy Drive, Pipe 75A - 76A							1.30	104					0.00		0.00		0.00			1.30										
Contribution From Les Emmerson Drive (N), Pipe 70A - 72A							1.09	99					0.00		0.00		0.00		1.09	1.09										
Contribution From Les Emmerson Drive (N), Pipe 71A - 72A							2.25	216					0.00		0.00		0.00		2.25	3.34										
	72A	74A	0.27	6	6		21	3.61	336	3.45	3.75		0.00		0.00		0.00	0.27	3.61	1.19	4.94	58.5	250	0.25	29.73	0.17	0.61	0.45		
Contribution From Les Emmerson Drive (S), Pipe 69A - 74A							1.30	132					0.00		0.00		0.00		1.30	4.91										
Contribution From Les Emmerson Drive (S), Pipe 73A - 74A							0.71	76					0.00		0.00		0.00		0.71	5.62										
	74A	750A	0.26	6	6		21	5.88	565	3.36	6.15		0.00		0.00		0.00	0.26	5.88	1.94	8.09	52.0	250	0.25	29.73	0.27	0.61	0.51		
	750A	75A	0.01				0	5.89	565	3.36	6.15		0.00		0.00		0.00	0.01	5.89	1.94	8.09	10.5	250	0.25	29.73	0.27	0.61	0.51		
To Conservancy Drive, Pipe 75A - 76A							5.89	565					0.00		0.00		0.00			5.89										
Gallium Crescent																														
	30A	31A	0.37	10	10		34	0.37	34	3.68	0.41		0.00		0.00		0.00	0.37	0.37	0.12	0.53	65.0	200	0.65	26.44	0.02	0.84	0.33		

DESIGN PARAMETERS	
Park Flow =	9300 L/ha/da 0.10764 l/s/ha
Average Daily Flow =	280 l/p/day
Comm/Inst Flow =	28000 L/ha/da 0.3241 l/s/ha
Industrial Flow =	35000 L/ha/da 0.40509 l/s/ha
Max Res. Peak Factor =	4.00
Commercial/Inst./Park Peak Factor =	1.50
Institutional =	0.32 l/s/ha
Industrial Peak Factor =	as per MOE Graph
Extraneous Flow =	0.330 L/s/ha
Minimum Velocity =	0.600 m/s
Manning's n = (Conc)	0.013 (Pvc) 0.013
Townhouse coeff=	2.7
Single house coeff=	3.4

Designed:	A.K.	PROJECT:	BARRHAVEN CONCERVANCY EAST PH2, 3, AND JOCK RIVER				
Checked:	W.L.	LOCATION:	City of Ottawa				
Dwg. Reference:	Sanitary Drainage Plan, Dwg. No. 110-112	File Ref:	20-1180	Date:	Aug 2022	Sheet No. of	1 6



SANITARY SEWER CALCULATION SHEET

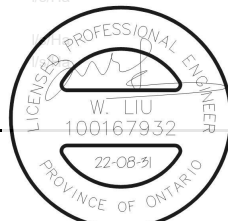


Manning's n=0.013

LOCATION			RESIDENTIAL AREA AND POPULATION							COMM		INSTIT		PARK		C+H+	INFILTRATION			PIPE												
STREET	FROM M.H.	TO M.H.	AREA (ha)	UNITS	UNITS Singles	UNITS Townhouse	POP.	CUMULATIVE		PEAK FLOW (l/s)	PEAK FLOW (l/s)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	PEAK FLOW (l/s)	TOTAL AREA (ha)	ACCU. AREA (ha)	INFILT. FLOW (l/s)	TOTAL FLOW (l/s)	DIST (m)	DIA (mm)	SLOPE (%)	CAP. (FULL) (l/s)	RATIO Q act/Q cap	VEL.				
								AREA (ha)	POP.																			(FULL) (m/s)	(ACT.) (m/s)			
	31A	32A	0.34	9	9		31	0.71	65	3.63	0.77		0.00	0.00		0.00	0.00	0.34	0.71	0.23	1.00	64.0	250	0.25	29.73	0.03	0.61	0.28				
To Sapling Grove, Pipe 32A - 37A								0.71	65			0.00	0.00		0.00	0.00			0.71													
	30A	33A	0.13	2	2		7	0.13	7	3.74	0.08		0.00	0.00		0.00	0.00	0.13	0.13	0.04	0.13	9.5	200	0.65	26.44	0.00	0.84	0.22				
	33A	34A	0.16	3	3		11	0.29	18	3.71	0.22		0.00	0.00		0.00	0.00	0.16	0.29	0.10	0.31	43.5	250	0.25	29.73	0.01	0.61	0.19				
	34A	35A	0.12	1	1		4	0.41	22	3.70	0.26		0.00	0.00		0.00	0.00	0.12	0.41	0.14	0.40	11.5	250	0.25	29.73	0.01	0.61	0.21				
	35A	36A	0.44	11	11		38	0.85	60	3.64	0.71		0.00	0.00		0.00	0.00	0.44	0.85	0.28	0.99	68.5	250	0.25	29.73	0.03	0.61	0.27				
	36A	37A	0.31	9	9		31	1.16	91	3.60	1.06		0.00	0.00		0.00	0.00	0.31	1.16	0.38	1.45	61.5	250	0.25	29.73	0.05	0.61	0.31				
To Mineral Street, Pipe 37A - 39A								1.16	91				0.00	0.00		0.00			1.16													
Pollination Place																																
	250A	26A	0.11	2	2		7	0.11	7	3.74	0.08		0.00	0.00		0.00	0.00	0.11	0.11	0.04	0.12	24.5	200	0.65	26.44	0.00	0.84	0.20				
	26A	27A	0.09	1	1		4	0.20	11	3.73	0.13		0.00	0.00		0.00	0.00	0.09	0.20	0.07	0.20	11.0	200	0.65	26.44	0.01	0.84	0.24				
	27A	28A	0.39	10	10		34	0.59	45	3.66	0.53		0.00	0.00		0.00	0.00	0.39	0.59	0.19	0.73	63.5	250	0.25	29.73	0.02	0.61	0.25				
	28A	29A	0.34	10	10		34	0.93	79	3.62	0.93		0.00	0.00		0.00	0.00	0.34	0.93	0.31	1.23	62.5	250	0.25	29.73	0.04	0.61	0.29				
To Sapling Grove, Pipe 29A - 32A								0.93	79				0.00	0.00		0.00			0.93													
	250A	25A	0.09	2	2		7	0.09	7	3.74	0.08		0.00	0.00		0.00	0.00	0.09	0.09	0.03	0.11	20.5	200	0.65	26.44	0.00	0.84	0.20				
	25A	19A	0.04				0	0.13	7	3.74	0.08		0.00	0.00		0.00	0.00	0.04	0.13	0.04	0.13	8.0	250	0.25	29.73	0.00	0.61	0.15				
	19A	20A	0.28	5	5		17	0.41	24	3.70	0.29		0.00	0.00		0.00	0.00	0.28	0.41	0.14	0.42	71.0	250	0.25	29.73	0.01	0.61	0.21				
	20A	21A	0.19	4	4		14	0.60	38	3.67	0.45		0.00	0.00		0.00	0.00	0.19	0.60	0.20	0.65	54.5	250	0.25	29.73	0.02	0.61	0.24				
To Sapling Grove, Pipe 21A - 29A								0.60	38				0.00	0.00		0.00			0.60													
Sapling Grove																																
Contribution From Pollination Place, Pipe 20A - 21A								0.60	38				0.00	0.00		0.00		0.60	0.60													
	21A	29A	0.23	3	3		11	0.83	49	3.65	0.58		0.00	0.00		0.00	0.00	0.23	0.83	0.27	0.85	59.0	250	0.25	29.73	0.03	0.61	0.27				
Contribution From Pollination Place, Pipe 28A - 29A								0.93	79				0.00	0.00		0.00		0.93	1.76													
	29A	32A	0.25	5	5		17	2.01	145	3.56	1.67		0.00	0.00		0.00	0.00	0.25	2.01	0.66	2.33	58.5	250	0.25	29.73	0.08	0.61	0.36				
Contribution From Gallium Crescent, Pipe 31A - 32A								0.71	65				0.00	0.00		0.00		0.71	2.72													
	32A	37A	0.19	4	4		14	2.91	224	3.50	2.54		0.00	0.00		0.00	0.00	0.19	2.91	0.96	3.50	58.5	250	0.25	29.73	0.12	0.61	0.40				
To Mineral Street, Pipe 37A - 39A								2.91	224				0.00	0.00		0.00			2.91													
Contribution From Syringa Court, Pipe 50A - 51A								1.03	87				0.00	0.00		0.00		1.03	1.21													
	51A	58A	0.25	5	5		17	1.46	115	3.58	1.33		0.00	0.00		0.00	0.00	0.25	1.46	0.48	1.82	58.5	250	0.25	29.73	0.06	0.61	0.33				
Contribution From Syringa Court, Pipe 57A - 58A								0.90	79				0.00	0.00		0.00		0.90	2.36													
	58A	61A	0.19	4	4		14	2.55	208	3.51	2.37		0.00	0.00		0.00	0.00	0.19	2.55	0.84	3.21	58.5	250	0.25	29.73	0.11	0.61	0.39				
Contribution From Ainsworth Crescent, Pipe 60A - 61A								0.93	83				0.00	0.00		0.00		0.93	3.48													
	61A	82A	0.22	4	4		14	3.70	305	3.46	3.42		0.00	0.00		0.00	0.00	0.22	3.70	1.22	4.64	60.0	250	0.25	29.73	0.16	0.61	0.44				
Contribution From Ainsworth Crescent, Pipe 81A - 82A								0.89	72				0.00	0.00		0.00		0.89	4.59													
	82A	85A	0.18	4	4		14	4.77	391	3.42	4.34		0.00	0.00		0.00	0.00	0.18	4.77	1.57	5.91	58.5	250	0.25	29.73	0.20	0.61	0.47				
Contribution From Meander Way, Pipe 84A - 85A								0.50	45				0.00	0.00		0.00		0.50	5.27													
	85A	88A	0.21	5	5		17	5.48	453	3.40	4.99		0.00	0.00		0.00	0.00	0.21	5.48	1.81	6.79	58.5	250	0.25	29.73	0.23	0.61	0.49				
To Ecology Lane, Pipe 88A - 91A								5.48	453				0.00	0.00		0.00			5.48													

DESIGN PARAMETERS

Park Flow =	9300	L/ha/da	0.10764	I/s/ha
Average Daily Flow =	280	l/p/day		
Comm/Inst Flow =	28000	L/ha/da	0.3241	
Industrial Flow =	35000	L/ha/da	0.40509	
Max Res. Peak Factor =	4.00			
Commercial/Inst./Park Peak Factor =	1.50			
Institutional =	0.32	I/s/ha		
Industrial Peak Factor =	as per MOE Graph			
Extraneous Flow =	0.330	L/s/ha		
Minimum Velocity =	0.600	m/s		
Manning's n =	0.013	(Conc) (Pvc)		0.013
Townhouse coeff=	2.7			
Single house coeff=	3.4			



Designed:	A.K.	PROJECT:	BARRHAVEN CONCERVANCY EAST PH2, 3, AND JOCK RIVER		
Checked:	W.L.	LOCATION:	City of Ottawa		
Dwg. Reference:	Sanitary Drainage Plan, Dwgs. No. 110-112	File Ref:	20-1180	Date:	Aug 2022
			Sheet No.	2	of 6

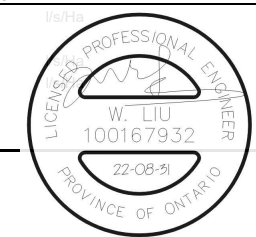
SANITARY SEWER CALCULATION SHEET



Manning's n=0.013

LOCATION		RESIDENTIAL AREA AND POPULATION										COMM		INSTIT		PARK		C+H		INFILTRATION			PIPE						
STREET	FROM M.H.	TO M.H.	AREA	UNITS	UNITS	UNITS	POP.	CUMULATIVE		PEAK	PEAK	AREA	ACCU.	AREA	ACCU.	AREA	ACCU.	PEAK	TOTAL	ACCU.	INFILT.	TOTAL	DIST	DIA	SLOPE	CAP.	RATIO	VEL.	
	(ha)		(ha)		Singles	Townhouse		AREA (ha)	POP.	FACT.	FLOW (l/s)	(ha)	(ha)	(ha)	(ha)	(ha)	(ha)	FLOW (l/s)	AREA (ha)	AREA (ha)	FLOW (l/s)	FLOW (l/s)	(m)	(mm)	(%)	(l/s)	Q act/Q cap	(FULL) (m/s)	(ACT.) (m/s)
Deciduous Crescent																													
	8A	9A	0.44	17		17	46	0.44	46	3.66	0.55		0.00		0.00	0.00	0.00	0.44	0.44	0.15	0.69	62.0	200	0.65	26.44	0.03	0.84	0.36	
	9A	11A	0.26	10		10	27	0.70	73	3.62	0.86		0.00		0.00	0.00	0.00	0.26	0.70	0.23	1.09	66.0	250	0.25	29.73	0.04	0.61	0.29	
To Conservancy Drive, Pipe 11A - 15A								0.70	73				0.00		0.00				0.70										
	12A	13A	0.09	2		2	6	0.09	6	3.75	0.07		0.00		0.00	0.00	0.00	0.09	0.09	0.03	0.10	7.5	200	0.65	26.44	0.00	0.84	0.20	
	13A	14A	0.38	15		15	41	0.47	47	3.66	0.56		0.00		0.00	0.00	0.00	0.38	0.47	0.16	0.71	66.0	250	0.25	29.73	0.02	0.61	0.25	
	14A	15A	0.30	11		11	30	0.77	77	3.62	0.90		0.00		0.00	0.00	0.00	0.30	0.77	0.25	1.16	69.5	250	0.25	29.73	0.04	0.61	0.29	
To Conservancy Drive, Pipe 15A - 18A								0.77	77				0.00		0.00				0.77										
Ephemeral Crescent																													
	2A	3A	0.16	1	1		4	0.16	4	3.76	0.05		0.00		0.00	0.00	0.00	0.16	0.16	0.05	0.10	13.0	200	0.70	27.44	0.00	0.87	0.19	
			0.25	5	5		17	0.41	21				0.00		0.00			0.25	0.41										
	3A	4A	0.31	13		13	36	0.72	57	3.64	0.67		0.00		0.00	0.00	0.00	0.31	0.72	0.24	0.91	107.5	250	0.25	29.73	0.03	0.61	0.27	
	4A	15A	0.35	9		9	25	1.07	82	3.61	0.96		0.00		0.00	0.00	0.00	0.35	1.07	0.35	1.31	112.0	250	0.25	29.73	0.04	0.61	0.30	
To Conservancy Drive, Pipe 15A - 18A								1.07	82				0.00		0.00				1.07										
	5A	500A	0.14	6		6	17	0.14	17	3.71	0.20		0.00		0.00	0.00	0.00	0.14	0.14	0.05	0.25	21.0	200	0.65	26.44	0.01	0.84	0.26	
	500A	6A	0.45	22		22	60	0.59	77	3.62	0.90		0.00		0.00	0.00	0.00	0.45	0.59	0.19	1.10	78.5	250	0.25	29.73	0.04	0.61	0.29	
	6A	11A	0.48	21		21	57	1.07	134	3.57	1.55		0.00		0.00	0.00	0.00	0.48	1.07	0.35	1.90	104.5	250	0.25	29.73	0.06	0.61	0.34	
To Conservancy Drive, Pipe 11A - 15A								1.07	134				0.00		0.00				1.07										
Borrisokane Road																													
	1002A	1001A	0.18	4		4	11	0.18	11	3.73	0.13		0.00		0.00	0.00	0.00	0.18	0.18	0.06	0.19	40.0	200	0.65	26.44	0.01	0.84	0.24	
	1001A	10A	0.40	12		12	33	0.58	44	3.66	0.52		0.00		0.00	0.00	0.00	0.40	0.58	0.19	0.71	100.0	250	0.25	29.73	0.02	0.61	0.25	
To Conservancy Drive, Pipe 10A - 11A								0.58	44				0.00		0.00				0.58										
	1004A	1003A	0.50	14		14	38	0.50	38	3.67	0.45		0.00		0.00	0.00	0.00	0.50	0.50	0.17	0.62	98.5	200	0.65	26.44	0.02	0.84	0.35	
	1003A	10A	0.41	13		13	36	0.91	74	3.62	0.87		0.00		0.00	0.00	0.00	0.41	0.91	0.30	1.17	100.0	250	0.25	29.73	0.04	0.61	0.29	
To Conservancy Drive, Pipe 10A - 11A								0.91	74				0.00		0.00				0.91										
Conservancy Drive																													
			12.88				1182	12.88	1182			4.21	4.21		0.00	0.58	0.58		17.67	17.67									
	PLUG	10A	36.45				3771	49.33	4953	2.80	44.93	13.70	17.91		0.00	3.47	4.05	9.36	53.62	71.29	23.53	77.81	20.5	525	0.10	136.00	0.57	0.63	0.65
Contribution From Borrisokane Road, Pipe 1001A - 10A								0.58	44				0.00		0.00				0.58	71.87									
Contribution From Borrisokane Road, Pipe 1003A - 10A								0.91	74				0.00		0.00				0.91	72.78									
	10A	11A	0.15				0	50.97	5071	2.79	45.87		17.91		0.00	4.05	9.36	0.15	72.93	24.07	79.30	71.5	525	0.10	136.00	0.58	0.63	0.65	
Contribution From Ephemeral Crescent, Pipe 6A - 11A								1.07	134				0.00		0.00				1.07	74.00									
Contribution From Deciduous Crescent, Pipe 9A - 11A								0.70	73				0.00		0.00				0.70	74.70									
	11A	15A	0.30	6	6		21	53.04	5299	2.78	47.69		17.91		0.00	4.05	9.36	0.30	75.00	24.75	81.80	59.0	525	0.10	136.00	0.60	0.63	0.66	
Contribution From Deciduous Crescent, Pipe 14A - 15A								0.77	77				0.00		0.00				0.77	75.77									
Contribution From Ephemeral Crescent, Pipe 4A - 15A								1.07	82				0.00		0.00				1.07	76.84									
	15A	18A	0.12				0	55.00	5458	2.77	48.95		17.91		0.00	4.05	9.36	0.12	76.96	25.40	83.71	58.5	525	0.10	136.00	0.62	0.63	0.66	
Contribution From Les Emmerson Drive (N), Pipe 17A - 18A								0.83	75				0.00		0.00				0.83	77.79									
Contribution From Park (Block 773), Pipe 210A - 18A								0.00	0.00				0.00		0.00				3.22	81.01									
	18A	23A	0.31	5	5		17	56.14	5550	2.76	49.68		17.91		0.00	4.05	9.36	0.31	81.32	26.84	85.88	76.5	525	0.10	136.00	0.63	0.63	0.66	
	23A	24A	0.49	11	11		38	56.63	5588	2.76	49.98		17.91		0.00	4.05	9.36	0.49	81.81	27.00	86.34	71.0	525	0.10	136.00	0.63	0.63	0.66	
	24A	47A	0.61	15	15		51	57.24	5639	2.76	50.38		17.91		0.00	4.05	9.36	0.61	82.42	27.20	86.94	106.0	525	0.10	136.00	0.64	0.63	0.67	

DESIGN PARAMETERS													Designed:			PROJECT:																
Park Flow =	9300	L/ha/da	0.10764																	A.K.		BARRHAVEN CONSERVANCY EAST PH2, 3, AND JOCK RIVER										
Average Daily Flow =	280	l/p/day																				LOCATION:										
Comm/Inst Flow =	28000	L/ha/da	0.3241																	W.L.	City of Ottawa											
Industrial Flow =	35000	L/ha/da	0.40509																													
Max Res. Peak Factor =	4.00																															
Commercial/Inst./Park Peak Factor =	1.50																															
Institutional =	0.32	l/s/ha																														
													Dwg. Reference:			File Ref:			Date:			Sheet No.										
													Sanitary Drainage Plan, Dwg. No. 110-112			20-1180			Aug 2022			4 of 6										



SANITARY SEWER CALCULATION SHEET



Manning's n=0.013

LOCATION			RESIDENTIAL AREA AND POPULATION							COMM		INSTIT		PARK		C+H		INFILTRATION			PIPE					VEL.					
STREET	FROM M.H.	TO M.H.	AREA	UNITS	UNITS Singles	UNITS Townhouse	POP.	AREA (ha)	POP.	PEAK FACT.	PEAK FLOW (l/s)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	PEAK FLOW (l/s)	TOTAL AREA (ha)	ACCU. AREA (ha)	INFILT. FLOW (l/s)	TOTAL FLOW (l/s)	DIST (m)	DIA (mm)	SLOPE (%)	CAP. (FULL) (l/s)	RATIO Q act/Q cap	(FULL) (m/s)	(ACT.) (m/s)		
Contribution From Mineral Street, Pipe 39A - 47A								5.28	398				0.00		0.00		0.00			5.28	87.70										
Contribution From Mineral Street, Pipe 46A - 47A								1.45	137				0.00		0.00		0.00			1.45	89.15										
	47A	48A	0.56	14	14		48	64.53	6222	2.72	54.94		17.91		0.00		4.05	9.36	0.56	89.71	29.60	93.90	99.0	525	0.10	136.00	0.69	0.63	0.68		
	48A	75A	0.42	10	10		34	64.95	6256	2.72	55.20		17.91		0.00		4.05	9.36	0.42	90.13	29.74	94.30	76.5	525	0.10	136.00	0.69	0.63	0.68		
Contribution From Anemone Mews, Pipe 63A - 75A								1.30	104				0.00		0.00		0.00			1.30	91.43										
Contribution From Anemone Mews, Pipe 750A - 75A								5.89	565				0.00		0.00		0.00			5.89	97.32										
	75A	76A	0.31	7	7		24	72.45	6949	2.69	60.53		17.91		0.00		4.05	9.36	0.31	97.63	32.22	102.11	62.0	525	0.10	136.00	0.75	0.63	0.69		
	76A	77A	0.39	11	11		38	72.84	6987	2.69	60.82		17.91		0.00		4.05	9.36	0.39	98.02	32.35	102.52	60.0	525	0.10	136.00	0.75	0.63	0.69		
	77A	92A	0.33	9	9		31	73.17	7018	2.68	61.05		17.91		0.00		4.05	9.36	0.33	98.35	32.46	102.87	53.0	525	0.10	136.00	0.76	0.63	0.69		
Contribution From Ecology Lane, Pipe 91A - 92A								6.96	580				0.00		0.00		0.00			6.96	105.31										
	92A	93A	0.51	12	12		41	80.64	7639	2.66	65.75		17.91		0.00		4.05	9.36	0.51	105.82	34.92	110.03	90.5	525	0.10	136.00	0.81	0.63	0.70		
	93A	119A	0.37	6	6		21	81.01	7660	2.65	65.91		17.91		0.00	0.52	4.57	9.44	0.89	106.71	35.21	110.56	88.0	525	0.10	136.00	0.81	0.63	0.70		
To Canoe Street, Pipe 119A - 120A								81.01	7660				17.91		0.00		4.57				106.71										
Meander Way																															
	84A	85A	0.50	13	13		45	0.50	45	3.66	0.53		0.00		0.00		0.00	0.00	0.50	0.50	0.17	0.70	92.5	200	0.65	26.44	0.03	0.84	0.36		
To Sapling Grove, Pipe 85A - 88A								0.50	45				0.00		0.00		0.00				0.50										
	84A	86A	0.16	1	1		4	0.16	4	3.76	0.05		0.00		0.00		0.00	0.00	0.16	0.16	0.05	0.10	13.0	200	0.65	26.44	0.00	0.84	0.20		
	86A	87A	0.22	4	4		14	0.38	18	3.71	0.22		0.00		0.00		0.00	0.00	0.22	0.38	0.13	0.34	50.5	250	0.65	47.94	0.01	0.98	0.28		
	87A	114A	0.23	5	5		17	0.61	35	3.67	0.42		0.00		0.00		0.00	0.00	0.23	0.61	0.20	0.62	58.0	250	0.25	29.73	0.02	0.61	0.24		
	114A	115A	0.07	1	1		4	0.68	39	3.67	0.46		0.00		0.00		0.00	0.00	0.07	0.68	0.22	0.69	10.0	250	0.25	29.73	0.02	0.61	0.25		
	115A	116A	0.63	17	17		58	1.31	97	3.60	1.13		0.00		0.00		0.00	0.00	0.63	1.31	0.43	1.56	110.5	250	0.25	29.73	0.05	0.61	0.32		
To Peninsula Road, Pipe 116A - 117A								1.31	97				0.00		0.00		0.00				1.31										
Peninsula Road																															
	89A	63A	0.17	4	4		14	0.17	14	3.72	0.17		0.00		0.00		0.00	0.00	0.17	0.17	0.06	0.22	41.0	200	0.65	26.44	0.01	0.84	0.26		
To Anemone Mews, Pipe 63A - 75A								0.17	14				0.00		0.00		0.00				0.17										
	380A	38A	0.45	8	8		28	0.45	28	3.69	0.33		0.00		0.00		0.00	0.00	0.45	0.45	0.15	0.48	57.0	200	0.65	26.44	0.02	0.84	0.32		
	38A	39A	0.60	16	16		55	1.05	83	3.61	0.97		0.00		0.00		0.00	0.00	0.60	1.05	0.35	1.32	108.5	250	0.25	29.73	0.04	0.61	0.30		
To Mineral Street, Pipe 39A - 47A								1.05	83				0.00		0.00		0.00				1.05										
	620A	62A	0.50	13	13		45	0.50	45	3.66	0.53		0.00		0.00		0.00	0.00	0.50	0.50	0.17	0.70	83.0	200	0.65	26.44	0.03	0.84	0.36		
	62A	63A	0.45	13	13		45	0.95	90	3.60	1.05		0.00		0.00		0.00	0.00	0.45	0.95	0.31	1.36	82.0	250	0.25	29.73	0.05	0.61	0.31		
To Anemone Mews, Pipe 63A - 75A								0.95	90				0.00		0.00		0.00				0.95										
	89A	90A	0.41	13	13		45	0.41	45	3.66	0.53		0.00		0.00		0.00	0.00	0.41	0.41	0.14	0.67	67.0	200	0.65	26.44	0.03	0.84	0.35		
	90A	91A	0.37	10	10		34	0.78	79	3.62	0.93		0.00		0.00		0.00	0.00	0.37	0.78	0.26	1.18	68.5	250	0.75	51.50	0.02	1.05	0.42		
To Ecology Lane, Pipe 91A - 92A								0.78	79				0.00		0.00		0.00				0.78										
	91A	116A	0.18	4	4		14	0.18	14	3.72	0.17		0.00		0.00		0.00	0.00	0.18	0.18	0.06	0.23	58.5	200	0.65	26.44	0.01	0.84	0.26		
Contribution From Meander Way, Pipe 115A - 116A								1.31	97				0.00		0.00		0.00				1.31	1.49									
	116A	117A	0.23	6	6		21	1.72	132	3.57	1.53		0.00		0.00		0.00	0.00	0.23	1.72	0.57	2.09	58.5	250	0.25	29.73	0.07	0.61	0.34		
Contribution From Elation Heights, Pipe 109A - 117A								0.74	55				0.00		0.00		0.00				0.74	2.46									
	117A	118A	0.18	3	3		11	2.64	198	3.52	2.26		0.00		0.00		0.00	0.00	0.18	2.64	0.87	3.13	59.0	250	0.25	29.73	0.11	0.61	0.39		
To Canoe Street, Pipe 118A - 1180A								2.64	198				0.00		0.00		0.00				2.64										

DESIGN PARAMETERS

Park Flow = 9300 L/ha/day 0.10764 l/s/ha

Average Daily Flow = 280 l/p/day

Comm/Inst Flow = 28000 L/ha/day 0.3241 l/s/ha

Industrial Flow = 35000 L/ha/day 0.40509 l/s/ha

Max Res. Peak Factor = 4.00

Commercial/Inst./Park Peak Factor = 1.50

Institutional = 0.32 l/s/ha

Industrial Peak Factor = as per MOE Graph

Extraneous Flow = 0.330 L/s/ha

Minimum Velocity = 0.600 m/s

Manning's n = (Conc) 0.013 (Pvc) 0.013

Household coeff= 2.7

Commercial coeff= 3.4



Designed: A.K.

Checked: W.L.

Dwg. Reference: Sanitary Drainage Plan, Dwgs. No. 110-112

PROJECT: **BARRHAVEN CONSERVANCY EAST PH2, 3, AND JOCK RIVER**

LOCATION: **City of Ottawa**

File Ref: 20-1180 Date: Aug 2022

Sheet No. 5 of 6

SANITARY SEWER CALCULATION SHEET



Manning's n=0.013

LOCATION			RESIDENTIAL AREA AND POPULATION							COMM		INSTIT		PARK		C+I		INFILTRATION			PIPE									
STREET	FROM M.H.	TO M.H.	AREA (ha)	UNITS	UNITS Singles	UNITS Townhouse	POP.	AREA (ha)	POP.	PEAK FACT.	PEAK FLOW (l/s)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	PEAK FLOW (l/s)	TOTAL AREA (ha)	ACCU. AREA (ha)	INFILT. FLOW (l/s)	TOTAL FLOW (l/s)	DIST (m)	DIA (mm)	SLOPE (%)	CAP. (FULL) (l/s)	RATIO Q act/Q cap	VEL. (FULL) (m/s)	(ACT.) (m/s)	
Elation Heights																														
To Canoe Street, Pipe 113A - 118A	112A	113A	0.05	1	1		4	0.05	4	3.76	0.05		0.00		0.00		0.00	0.00	0.05	0.05	0.02	0.07	15.5	200	0.65	26.44	0.00	0.84	0.17	
	110A	109A	0.16	1	1		4	0.16	4	3.76	0.05		0.00		0.00		0.00	0.16	0.16	0.05	0.10	13.5	200	0.65	26.44	0.00	0.84	0.20		
To Peninsula Road, Pipe 117A - 118A	109A	117A	0.58	15	15		51	0.74	55	3.64	0.65		0.00		0.00		0.00	0.58	0.74	0.24	0.89	103.0	250	0.25	29.73	0.03	0.61	0.27		
Jollity Crescent																														
To Canoe Street, Pipe 105A - 108A	104A	105A	0.39	10	10		34	0.39	34	3.68	0.41		0.00		0.00		0.00	0.39	0.39	0.13	0.53	69.0	200	0.80	29.34	0.02	0.93	0.35		
	106A	107A	0.15	1	1		4	0.15	4	3.76	0.05		0.00		0.00		0.00	0.15	0.15	0.05	0.10	12.0	200	0.70	27.44	0.00	0.87	0.19		
To Canoe Street, Pipe 108A - 113A	107A	108A	0.48	12	12		41	0.63	45	3.66	0.53		0.00		0.00		0.00	0.48	0.63	0.21	0.74	87.0	250	0.25	29.73	0.02	0.61	0.25		
Euphoria Crescent																														
To Canoe Street, Pipe 102A - 105A	101A	102A	0.36	7	7		24	0.36	24	3.70	0.29		0.00		0.00		0.00	0.36	0.36	0.12	0.41	62.5	250	0.65	47.94	0.01	0.98	0.30		
	98A	99A	0.28	5	5		17	0.28	17	3.71	0.20		0.00		0.00		0.00	0.28	0.28	0.09	0.30	41.5	200	1.20	35.93	0.01	1.14	0.33		
To Canoe Street, Pipe 99A - 102A																														
Canoe Street																														
	94A	95A	0.52	3	3		11	0.52	11	3.73	0.13		0.00		0.00		0.00	0.52	0.52	0.17	0.30	38.5	200	0.65	26.44	0.01	0.84	0.28		
	95A	96A	0.49	9	9		31	1.01	42	3.66	0.50		0.00		0.00		0.00	0.49	1.01	0.33	0.83	83.5	250	0.25	29.73	0.03	0.61	0.26		
	96A	99A	0.10	2	2		7	1.11	49	3.65	0.58		0.00		0.00		0.00	0.10	1.11	0.37	0.95	22.0	250	0.25	29.73	0.03	0.61	0.27		
Contribution From Euphoria Crescent, Pipe 98A - 99A																														
	99A	102A	0.18	3	3		11	0.28	17	3.62	0.90		0.00		0.00		0.00	0.18	1.57	0.52	1.42	58.5	250	0.25	29.73	0.05	0.61	0.31		
Contribution From Euphoria Crescent, Pipe 101A - 102A																														
	102A	105A	0.22	4	4		14	2.15	115	3.58	1.33		0.00		0.00		0.00	0.22	2.15	0.71	2.04	58.5	250	0.25	29.73	0.07	0.61	0.34		
Contribution From Jollity Crescent, Pipe 104A - 105A																														
	105A	108A	0.21	4	4		14	0.39	34	2.75	1.87		0.00		0.00		0.00	0.21	2.75	0.91	2.78	58.5	250	0.25	29.73	0.09	0.61	0.38		
Contribution From Jollity Crescent, Pipe 107A - 108A																														
	108A	113A	0.20	4	4		14	0.63	45	3.58	2.52		0.00		0.00		0.00	0.20	3.58	1.18	3.70	60.0	250	0.25	29.73	0.12	0.61	0.41		
Contribution From Elation Heights, Pipe 112A - 113A																														
	113A	118A	0.43	10	10		34	0.05	4	4.06	2.94		0.00		0.00		0.00	0.05	3.63											
Contribution From Peninsula Road, Pipe 117A - 118A																														
	118A	1180A	0.16	3	3		11	2.64	198	2.64	1.98		0.00		0.00		0.00	2.64	6.70											
	1180A	119A	0.03	0	0		0	6.89	469	3.39	5.15		0.00		0.00		0.00	0.03	6.89	2.27	7.43	20.0	250	0.25	29.73	0.25	0.61	0.50		
Contribution From Conservancy Drive, Pipe 93A - 119A																														
	119A	120A	0.17				0	81.01	7660	17.91	113.60		17.91	0.00	4.57		106.71	113.60												
	120A	121A	0.21	4	4		14	88.07	8129	2.63	69.41		17.91	0.00	4.57		9.44	0.17	113.77	37.54	116.40	75.0	525	0.10	136.00	0.86	0.63	0.71		
	121A	Ex. MH 8						88.28	8143	2.63	69.51		17.91	0.00	4.57		9.44	0.21	113.98	37.61	116.57	87.5	525	0.10	136.00	0.86	0.63	0.71		
								88.28	8143	2.63	69.51		17.91	0.00	4.57		9.44	0.00	113.98	37.61	116.57	10.0	525	0.10	136.00	0.86	0.63	0.71		
Park (Block 773)																														
To Conservancy Drive, Pipe 18A - 23A	210A	18A						0.00					0.00	0.00	3	3.22	0.52	3.22	3.22	1.06	1.58	11.5	200	0.65	26.44	0.06	0.84	0.46		
								0.00	0				0.00	0.00	3.22															

DESIGN PARAMETERS

Park Flow =	9300	L/ha/da	0.10764
Average Daily Flow =	280	l/p/day	
Comm/Inst Flow =	28000	L/ha/da	0.3241
Industrial Flow =	35000	L/ha/da	0.40509
Max Res. Peak Factor =	4.00		
Commercial/Inst./Park Peak Factor =	1.50		
Institutional =	0.32	l/s/ha	



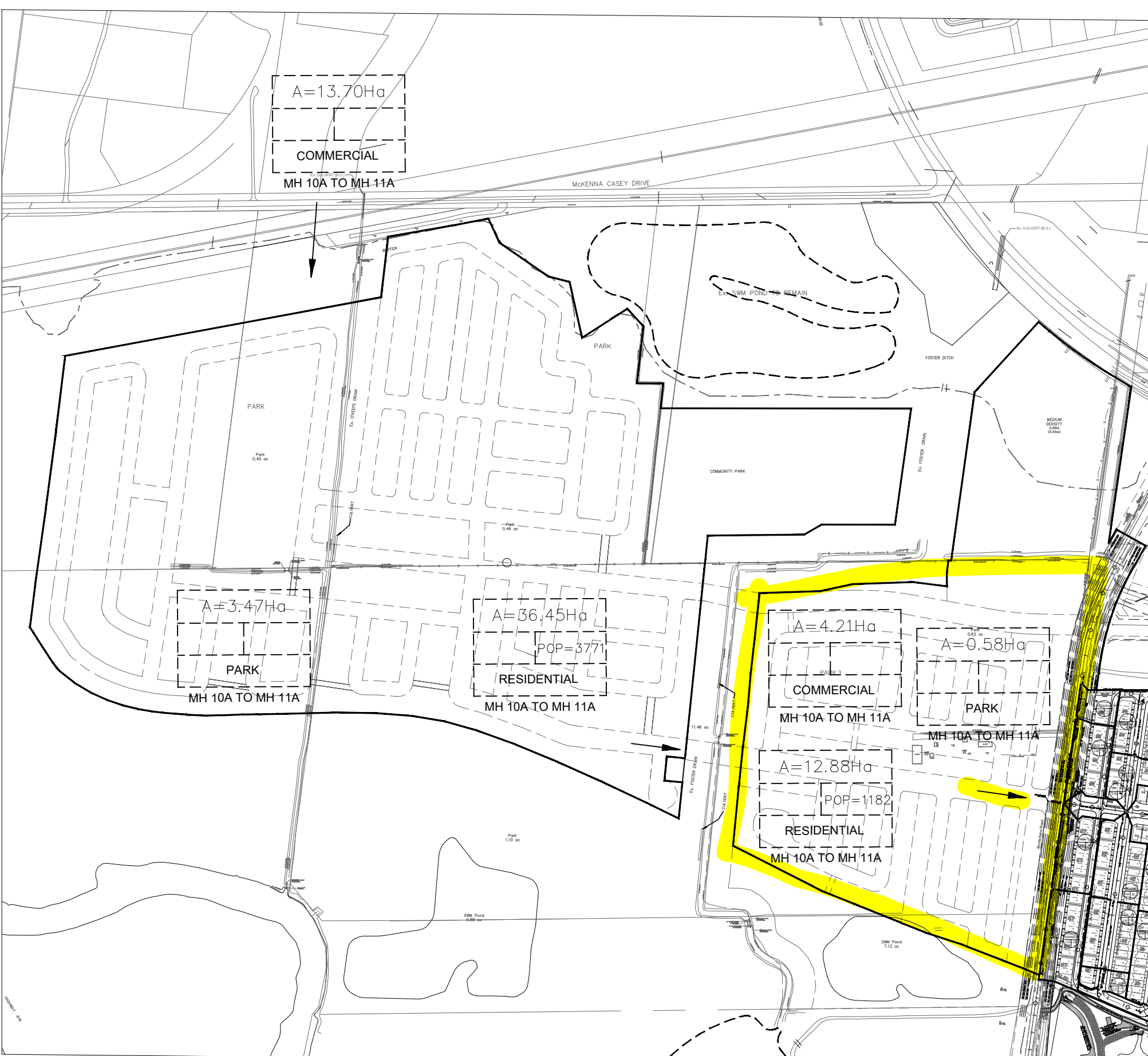
Industrial Peak Factor =	as per MOE Graph		
Extraneous Flow =	0.330	L/s/ha	
Minimum Velocity =	0.600	m/s	
Manning's n =	0.013	(Conc) (Pvc)	0.013
Townhouse coeff=	2.7		
Single house coeff=	3.4		

Designed:

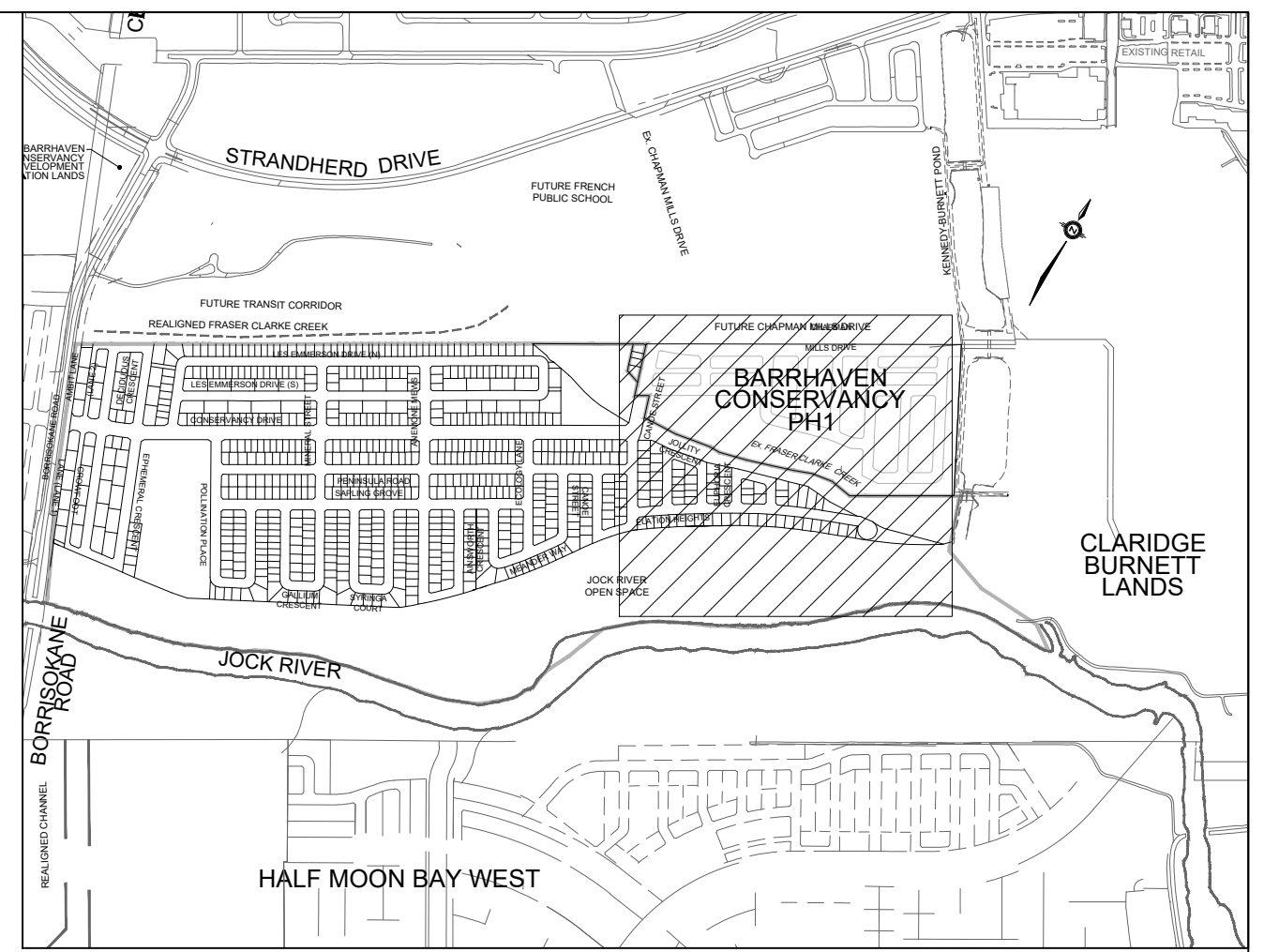
A.K.
Checked:
W.L.
Dwg. Reference:
Sanitary Drainage Plan, Dwgs. No. 110-112

PROJECT:

BARRHAVEN CONCERNVANCY EAST PH2, 3, AND JOCK RIVER			
LOCATION:			
City of Ottawa			
File Ref:	20-1180	Date:	Aug 2022
Sheet No.	6	of	6



EXTERNAL SANITARY DRAINAGE PLAN
SCALE: 1:5000



LEGEND

- SANITARY DRAINAGE BOUNDARY
- SANITARY SUB-DRAINAGE BOUNDARY
- UPSTREAM MH TO DOWNSTREAM MH
AREA IN HECTARES → 43A - 44A
POPULATION → 0.78 61
- UPSTREAM MH TO DOWNSTREAM MH
AREA IN OTHER PHASES IN HECTARES → 43A - 44A
POPULATION → 0.78 61
- EXTERNAL AREA IN HECTARES → A=53.63
EXTERNAL POPULATION → 107 POP=5739
EXTERNAL LAND USE → RESIDENTIAL
- MAINTENANCE HOLE → MH 202A
- CAP
- EXISTING SANITARY MAINTENANCE HOLE

TOPOGRAPHIC INFORMATION
TOPOGRAPHIC INFORMATION PROVIDED BY J.D. BARNES LIMITED, PROJECT NO. 16-10-127-00, SURVEY DATED APRIL 10, 2018.

LEGAL INFORMATION
M-PLAN PROVIDED BY J.D. BARNES, PROJECT NO. 16-10-127-00, RECEIVED ON AUGUST 2, 2022.

NOT FOR CONSTRUCTION

ELEVATION NOTE
ELEVATIONS SHOWN ON THIS PLAN ARE RELATED TO GEODETIC DATUM AND ARE REFERRED TO THE PUBLISHED BENCH MARK NO. D011964U3710
ELEVATION = 71.724m

No.	BY	DATE	DESCRIPTION
7	W.L.	22-09-28	RETAINING WALL UPDATES
6	W.L.	22-09-27	WATERMAIN AND CUP UPDATES
5	W.L.	22-08-31	CITY COMMENTS AND TRANSPORTATION UPDATES
4	W.L.	22-08-10	REVISED STREET NAME & LOT 99 SIGHT TRIANGLE
3	W.L.	22-06-28	3rd SUBMISSION
2	W.L.	22-04-22	2nd SUBMISSION
1	W.L.	21-12-22	1st SUBMISSION

CITY OF OTTAWA

PROJECT No. 20-1180

SANITARY DRAINAGE PLAN

BARRHAVEN CONSERVANCY DEVELOPMENT CORPORATION	BARRHAVEN CONSERVANCY EAST PHASE 2, 3 & JOCK RIVER
-----------------------------------------------	----------------------------------------------------

120 Iber Road, Unit 103
Stittville, ON K2S 1E9
Tel. (613) 836-0856
Fax. (613) 836-7183
www.DSEL.ca

DRAWN BY: A.K./R.A./V.W.	CHECKED BY: W.L.	SHEET NO.
DESIGNED BY: W.L.	CHECKED BY: C.M.	112
SCALE: 1:1000	DATE: DECEMBER 2021	

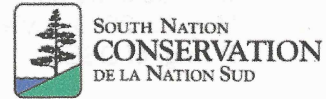
DWG # 111

CITY PLAN No. 18754
CITY FILE No. D07-16-20-0021

APPENDIX D

STORMWATER

Conservation Partners Partenaires en conservation



May 31, 2020

City of Ottawa
110 Laurier Avenue,
Ottawa, ON K1P 1J1

Attention: Doug James

Subject: **Barrhaven Conservancy Development Corporation
Status of As-Built Grading
Related: RVCA Permit # RV5-4419 and RV5-1718)
Vacant land on the north side of the Jock River generally bounded by
Highway 416 and the Fraser Clarke Creek, City of Ottawa**

Dear Mr. James:

The RVCA has reviewed information recently submitted by David Schaeffer Engineering Ltd. including as-built grades in support of works approved by the Rideau Valley Conservation Authority under Section 28 of the Conservation Authorities Act (Permit File Number: RV5-4419 and RV5-1718). The RVCA offers the following comments related to future development proposed for the area within the scope of approved the permits.

The subject lands as identified as part of Lots 11, 12, 13, 14, 15 former geographic Township of Nepean, Concessions 3 & 4, now in the City of Ottawa have been addressed through the general placement of fill and the formal construction of a berm around the perimeter of four blocks within the subject lands. The site specific elevations of the berm have been reviewed by the RVCA and are generally accepted as being appropriate as removing these lands from the floodplain in accordance with the aforementioned approved permits.

The detailed grading plans submitted by David Schaeffer Engineering Ltd. titled "As Constructed plan of Berms and Cut Areas – Barrhaven Conservancy", dated May 27, 2020, prepared by Adam Fobert, P.Eng. of DSEL, DSEL File Number 16891 using the following resources:

- Orthoimagery Survey, dated April 20, 2020, acquired and processed by First Base Solutions a division of JD Barnes Ltd and certified by Chris Fox, O.L.S., A.L.S., P. Eng. of JD Barnes Ltd, file reference number 2037OTTA0001; ·
- Topographic Detail of Part of Lot 13, 14, & 15 Concession 3&4, dated May 6, 2020, certified by Chris Fox, O.L.S., A.L.S., P. Eng. of JD Barnes Ltd, file reference number 16-10-127-00; ·



- Contractor as-built collected by the Tomlinson Group of Companies of Phase 1 dated May 15, 2020, reviewed by Jeremy Chouindard, EIT and certified by Stephen Pichette, P.Eng. of DSEL

The above information indicates that land within the berm have generally been raised to exceed the flood elevation cross sections throughout the project area. However, it is noted that as this is considered an active construction site the presence of lower areas to manage construction, on-site erosion and sediment control show lower elevations. These areas will be addressed through the construction process, as sufficient material is presently stockpiled for this purpose to ensure. For the purposes of the floodplain, these areas are considered removed by virtue of the berm.

Conclusion:

The grade modifications, including construction of the berm and filling behind the berm, as documented in the above noted "as constructed" plans, have been completed in accordance with the plans approved by the RVCA under permits RV5-4419 and RV5-1718.

Please feel free to contact our office with any questions or comments you may have.

Respectfully,

Terry Davidson, P.Eng
Director of Engineering and Regulations
Rideau Valley Conservation Authority
613-692-3571 x1107
terry.davidson@rvca.ca

attach: Technical memorandum by Evelyn Liu, M.Asc., P.Eng. Water Resources
 Engineer, RVCA dated May 29, 2020

STORM SEWER CALCULATION SHEET (RATIONAL METHOD)

Local Roads Return Frequency = 2 years
 Collector Roads Return Frequency = 5 years
 Arterial Roads Return Frequency = 10 years



Manning 0.013

LOCATION			AREA (Ha)																FLOW								SEWER DATA											
			2 YEAR				5 YEAR				10 YEAR				100 YEAR				Time of	Intensity	Intensity	Intensity	Intensity	Peak Flow	DIA. (mm)	DIA. (mm)	TYPE	SLOPE	LENGTH	CAPACITY	VELOCITY	TIME OF	RATIO					
Location	From Node	To Node	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	Conc. (min)	2 Year (mm/h)	5 Year (mm/h)	10 Year (mm/h)	100 Year (mm/h)	Q (l/s)	(actual)	(nominal)	(%)	(m)	(l/s)	(m/s)	LOW (min)	Q/Q full						
Centerline7 - 07																																						
	501	502	0.32	0.67	0.60	0.60			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	46	375	375	PVC	0.30	118.0	96.0323	0.8695	2.2619	0.477					
	502	505	0.02	0.67	0.04	0.63			0.00	0.00			0.00	0.00			0.00	0.00	12.26	69.09	93.59	109.66	160.23	44	450	450	CONC	0.25	31.5	142.5531	0.8963	0.5857	0.307					
To Centerline15 - 15, Pipe 505 - 507					0.63				0.00					0.00				0.00	12.85																			
Centerline4 - 04																																						
Contribution From Centerline15 - 15, Pipe 505 - 507					0.63				0.69					0.00				0.00	13.24																			
Contribution From Centerline15 - 15, Pipe 506 - 507					0.00				0.00					0.85				0.00	11.43																			
			0.22	0.80	0.49	1.12			0.00	0.69			0.00	0.85			0.00	0.00																				
	507	513	0.29	0.67	0.54	1.66			0.00	0.69			0.00	0.85			0.00	0.00	13.24	66.26	89.71	105.08	153.51	261	750	750	CONC	0.11	114.5	369.2322	0.8358	2.2833	0.707					
To Centerline11 - 11, Pipe 513 - 514					1.66				0.69					0.85				0.00	15.52																			
Centerline2 - 02																																						
	511	512	0.42	0.80	0.93	0.93			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	72	450	450	CONC	0.20	99.5	127.5033	0.8017	2.0685	0.563					
To Centerline11 - 11, Pipe 512 - 513					0.93				0.00					0.00				0.00	12.07																			
Centerline11 - 11																																						
	508	509	0.20	0.80	0.44	0.44			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	76	450	450	CONC	0.20	90.5	127.5033	0.8017	1.8814	0.593					
	509	510	0.12	0.67	0.22	1.21			0.00	0.00			0.00	0.00			0.00	0.00	11.88	70.26	95.20	111.56	163.01	85	450	450	CONC	0.20	10.5	127.5033	0.8017	0.2183	0.666					
	510	512	0.16	0.67	0.30	1.51			0.00	0.00			0.00	0.00			0.00	0.00	12.10	69.58	94.27	110.46	161.40	105	525	525	CONC	0.20	39.0	192.3297	0.8885	0.7316	0.545					
Contribution From Centerline2 - 02, Pipe 511 - 512					0.93				0.00				0.00				0.00	12.07																				
	512	513	0.19	0.67	0.35	2.79			0.00	0.00			0.00	0.00			0.00	0.00	12.83	67.41	91.29	106.95	156.24	188	675	675	CONC	0.15	47.5	325.5584	0.9098	0.8702	0.579					
Contribution From Centerline4 - 04, Pipe 507 - 513					1.66				0.69				0.85				0.00	15.52																				
	513	514	0.21	0.67	0.39	4.85			0.00	0.69			0.00	0.85			0.00	0.00	15.52	60.56	81.90	95.90	140.03	431	900	900	CONC	0.11	51.0	600.4123	0.9438	0.9006	0.718					
	514	515	0.03	0.67	0.06	4.90			0.00	0.69			0.00	0.85			0.00	0.00	16.43	58.60	79.22	92.75	135.41	421	900	900	CONC	0.11	8.5	600.4123	0.9438	0.1501	0.700					
	515	516	0.09	0.67	0.17	5.07			0.00	0.69			0.00	0.85			0.00	0.00	16.58	58.28	78.79	92.25	134.67	428	900	900	CONC	0.11	56.5	600.4123	0.9438	0.9978	0.713					
To Centerline1 - 01, Pipe 516 - 521					5.07				0.69				0.85				0.00	17.57																				
Centerline3 - 03																																						
Contribution From Centerline1 - 01, Pipe 516 - 521					5.07				1.15				0.85				0.00	18.60																				
Contribution From Centerline1 - 01, Pipe 519 - 521					0.00				1.40				0.00				0.00	12.21																				
	521	524	0.55	0.67	1.02	6.10			0.00	2.55			0.00	0.85			0.00	0.00	18.60	54.40	73.49	86.01	125.53	592	900	900	CONC	0.17	110.0	746.4104	1.1733	1.5626	0.793					
To Centerline10 - 10, Pipe 524 - 525					6.10				2.55				0.85				0.00	20.16																				
Centerline10 - 10																																						
	520	517	0.62	0.67	1.15	1.15			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	89	450	450	CONC	0.20	104.5	127.5033	0.8017	2.1725	0.696					
	517	518	0.17	0.67	0.32	1.47			0.00	0.00			0.00	0.00			0.00	0.00	12.17	69.36	93.97	110.10	160.87	102	450	450	CONC	0.25	10.5	142.5531	0.8963	0.1952	0.716					
	518	525	0.18	0.67	0.34	1.81			0.00	0.00			0.00	0.00			0.00	0.00	12.37	68.77	93.15	109.14	159.47	124	525	525	CONC	0.20	48.0	192.3297	0.8885	0.9004	0.646					
To Centerline5 - 05, Pipe 525 - HW10					1.81				0.00				0.00				0.00	13.27																				
	522	523	0.65	0.67	1.21	1.21			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	93	450	450	CONC	0.20	39.0	127.5033	0.8017	0.8108	0.729					
	523	524	0.21	0.67	0.39	1.60			0.00	0.00			0.00	0.00			0.00	0.00	10.81	73.83	100.10	117.32	171.47	118	525	525	CONC	0.20	49.0	192.3297	0.8885	0.9192	0.615					
Contribution From Centerline3 - 03, Pipe 521 - 524					6.10				2.55				0.85				0.00	20.16																				
	524	525	0.00	0.67	0.00	7.70			0.00	2.55			0.00	0.85			0.00	0.00	20.16	51.78	69.90	81.80	119.35	646	1050	1050	CONC	0.11	8.0	905.6791	1.0459	0.1275	0.714					
To Centerline5 - 05, Pipe 525 - HW10					7.70				2.55				0.85				0.00	20.29																				
Centerline5 - 05																																						
Contribution From Centerline10 - 10, Pipe 518 - 525					1.81				0.00				0.00				0.00	13.27																				
Contribution From Centerline10 - 10, Pipe 524 - 525					7.70				2.55				0.85				0.00	20.29																				
	525	HW10	0.02	0.67	0.04	9.54			0.00	2.55			0.00	0.85			0.00	0.00	20.29	51.57	69.63	81.48	118.87	739	1050	1050	CONC	0.11	32.0	905.6791	1.0459	0.5099	0.816					
Centerline12 - 12																																						
Contribution From Centerline9 - 09, Pipe 545 - 546					1.38				0.00				0.00				0.00	13.14																				
	546	547	0.36	0.80	0.80	2.18	0.05	0.67	0.09	0.09			0.00	0.00			0.00	0.00	13.14	66.55	90.10	105.55	154.20	153	600	600	CONC	0.15	91.5	237.8056	0.8411	1.8132	0.645					
	547	548	0.45	0.80	1.00	3.18			0.00	0.09			0.00	0.00			0.00	0.00	14.95	61.89	83.72	98.04	143.17	205	600	600	CONC	0.20	97.0	274.5943	0.9712	1.6646	0.745					

Definitions:
 Q = 2.78 AIR, where
 Q = Peak Flow in Litres per second (L/s)
 A = Areas in hectares (ha)
 I = Rainfall Intensity (mm/h)
 R = Runoff Coefficient

Notes:
 1) Ottawa Rainfall-Intensity Curve
 2) Min. Velocity = 0.80 m/s

Designed:	A.S.	PROJECT:	Barrhaven Conservancy East Phase 5	
Checked:	W.L./V.W.	LOCATION:	City of Ottawa	
Dwg. Reference:		File Ref:	Date:	Sheet No.
			01 Dec 2022	SHEET 1 OF 3

STORM SEWER CALCULATION SHEET (RATIONAL METHOD)

Local Roads Return Frequency = 2 years
 Collector Roads Return Frequency = 5 years
 Arterial Roads Return Frequency = 10 years



Manning 0.013

Location	LOCATION		AREA (Ha)																FLOW						SEWER DATA										
			2 YEAR				5 YEAR				10 YEAR				100 YEAR				Time of Conc. (min)	Intensity 2 Year (mm/h)	Intensity 5 Year (mm/h)	Intensity 10 Year (mm/h)	Intensity 100 Year (mm/h)	Peak Flow Q (l/s)	DIA. (mm) (actual)	DIA. (mm) (nominal)	TYPE	SLOPE (%)	LENGTH (m)	CAPACITY (l/s)	VELOCITY (m/s)	TIME OF LOW (min)	RATIO Q/Q full		
			AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC																	
	548	528	0.03	0.67	0.06	3.24					0.00	0.09					0.00	0.00	16.61	58.20	78.68	92.12	134.48	196	600	600	CONC	0.25	36.0	307.0058	1.0858	0.5526	0.637		
	To Centerline13 - 13, Pipe 528 - HW9					3.24						0.09					0.00	0.00	17.17																
	Centerline8 - 08																																		
	539	540	0.32	0.67	0.60	0.60					0.00	0.00					0.00	0.00	10.00	76.81	104.19	122.14	178.56	46	300	300	PVC	0.40	52.0	61.1589	0.8652	1.0017	0.749		
	540	541	0.41	0.67	0.76	1.36					0.00	0.00					0.00	0.00	11.00	73.16	99.18	116.24	169.89	99	450	450	CONC	0.20	68.0	127.5033	0.8017	1.4137	0.780		
	541	542	0.13	0.67	0.24	1.60					0.00	0.00					0.00	0.00	12.42	68.63	92.96	108.91	159.13	110	450	450	CONC	0.25	10.5	142.5531	0.8963	0.1952	0.771		
	542	543	0.17	0.67	0.32	1.92					0.00	0.00					0.00	0.00	12.61	68.05	92.17	107.98	157.76	131	600	600	CONC	0.15	48.0	237.8056	0.8411	0.9512	0.549		
	To Centerline13 - 13, Pipe 543 - 528					1.92						0.00					0.00	0.00	13.56																
	Centerline1 - 01																																		
	519	521			0.00	0.00	0.75	0.67	1.40	1.40							0.00	0.00	10.00	76.81	104.19	122.14	178.56	146	525	525	CONC	0.20	118.0	192.3297	0.8885	2.2136	0.757		
	To Centerline3 - 03, Pipe 521 - 524					0.00			1.40								0.00	0.00	12.21																
	535	536			0.00	0.00	0.21	0.80	0.47	0.47							0.00	0.00	10.00	76.81	104.19	122.14	178.56	49	375	375	PVC	0.30	51.5	96.0323	0.8695	0.9872	0.507		
	536	537			0.00	0.00	0.18	0.80	0.40	0.87							0.00	0.00	10.99	73.21	99.25	116.32	170.01	86	450	450	CONC	0.20	53.5	127.5033	0.8017	1.1122	0.675		
	To Centerline13 - 13, Pipe 537 - 538					0.00			0.87								0.00	0.00	12.10																
	Contribution From Centerline11 - 11, Pipe 515 - 516									5.07							0.00	0.85																	
	516	521			0.00	5.07	0.25	0.67	0.47	1.15							0.00	0.85	17.57	56.29	76.07	89.05	129.98	449	900	900	CONC	0.11	58.0	600.4123	0.9438	1.0242	0.748		
	To Centerline3 - 03, Pipe 521 - 524					5.07				1.15							0.00	0.85	18.60																
	Centerline9 - 09																																		
	531	533	0.25	0.80	0.56	0.56				0.00	0.00					0.00	0.00	10.00	76.81	104.19	122.14	178.56	94	525	525	CONC	0.20	104.5	192.3297	0.8885	1.9603	0.490			
	To Centerline6 - 06, Pipe 533 - 534					1.23				0.00						0.00	0.00	11.96																	
	544	545	0.36	0.80	0.80	0.80				0.00	0.00					0.00	0.00	10.00	76.81	104.19	122.14	178.56	61	375	375	PVC	0.30	78.5	96.0323	0.8695	1.5047	0.640			
	545	546	0.26	0.80	0.58	1.38				0.00	0.00					0.00	0.00	11.50	71.47	96.86	113.51	165.88	99	450	450	CONC	0.20	78.5	127.5033	0.8017	1.6320	0.773			
	To Centerline12 - 12, Pipe 546 - 547					1.38				0.00						0.00	0.00	13.14																	
	Centerline6 - 06																																		
			0.20	0.80	0.44	0.44				0.00	0.00					0.00	0.00	10.00	76.81	104.19	122.14	178.56	89	450	450	CONC	0.20	62.0	127.5033	0.8017	1.2889	0.697			
	532	533	0.64	0.40	0.71	1.16				0.00	0.00					0.00	0.00	10.00	76.81	104.19	122.14	178.56	89	450	450	CONC	0.20	62.0	127.5033	0.8017	1.2889	0.697			
	Contribution From Centerline9 - 09, Pipe 531 - 533									1.23							0.00	0.00	11.96																
	533	534	0.13	0.80	0.29	2.67				0.00	0.00					0.00	0.00	11.96	70.02	94.87	111.16	162.43	187	600	600	CONC	0.20	44.5	274.5943	0.9712	0.7637	0.681			
	To Centerline14 - 14, Pipe 534 - 537					2.67				0.00						0.00	0.00	12.72																	
	Centerline15 - 15																																		
	506	507			0.00	0.00				0.00	0.00	0.36	0.85	0.85	0.85			0.00	0.00	10.00	76.81	104.19	122.14	178.56	104	450	450	CONC	0.25	77.0	142.5531	0.8963	1.4318	0.729	
	To Centerline4 - 04, Pipe 507 - 513					0.00				0.00						0.00	0.00	11.43																	
	526	529	0.93	0.80	2.07	2.07				0.00	0.00	0.23	0.85	0.54	0.54			0.00	0.00	10.00	76.81	104.19	122.14	178.56	225	600	600	CONC	0.25	62.0	307.0058	1.0858	0.9517	0.734	
	To Centerline14 - 14, Pipe 529 - 530					2.07				0.00						0.00	0.00	10.95																	
	527	529			0.00	0.00				0.00	0.00	0.26	0.85	0.61	0.61			0.00	0.00	10.00	76.81	104.19	122.14	178.56	75	375	375	PVC	0.35	46.0	103.7267	0.9392	0.8163	0.723	
	To Centerline14 - 14, Pipe 529 - 530					0.00				0.00						0.00	0.00	10.82																	
	503	504			0.00	0.00	0.10	0.85	0.24	0.24						0.00	0.00	10.00	76.81	104.19	122.14	178.56	25	300	300	PVC	0.35	41.0	57.2089	0.8093	0.8443	0.430			
	504	505			0.00	0.00	0.14	0.85	0.33	0.57						0.00	0.00	10.84	73.71	99.94	117.13	171.19	57	375	375	PVC	0.30	60.0	96.0323	0.8695	1.1501	0.590			
	Contribution From Centerline7 - 07, Pipe 502 - 505									0.63						0.00	0.00	12.85																	
	505	507			0.00	0.63	0.05	0.85	0.12	0.69						0.00	0.00	12.85	67.36	91.22	106.87	156.13	105	525	525	CONC	0.20	21.0	192.3297	0.8885	0.3939	0.547			
	To Centerline4 - 04, Pipe 507 - 513					0.63				0.69						0.00	0.00	13.24																	

Definitions: Q = 2.78 AIR, where Q = Peak Flow in Litres per second (L/s) A = Areas in hectares (ha) I = Rainfall Intensity (mm/h) R = Runoff Coefficient	Notes: 1) Ottawa Rainfall-Intensity Curve 2) Min. Velocity = 0.80 m/s	Designed: A.S.	PROJECT: Barrhaven Conservancy East Phase 5
		Checked: W.L./V.W.	LOCATION: City of Ottawa
		Dwg. Reference:	File Ref: Date: 01 Dec 2022
			Sheet No. SHEET 2 OF 3



**CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION
BASED ON THE RATIONAL RAINFALL METHOD
BASED ON A FINE PARTICLE SIZE DISTRIBUTION**



Project Name: 891 Conservancy East	Engineer: DSEL
Location: Ottawa, ON	Contact: K. Murphy
OGS #: 9	Report Date: 20-Oct-22
Area: 7.21 ha	Rainfall Station #: 215
Weighted C: 0.72	Particle Size Distribution: FINE
CDS Model: 4045 (OFFLINE)	CDS Treatment Capacity: 212 l/s

<u>Rainfall Intensity¹</u> <u>(mm/hr)</u>	<u>Percent Rainfall Volume¹</u>	<u>Cumulative Rainfall Volume</u>	<u>Total Flowrate (l/s)</u>	<u>Treated Flowrate (l/s)</u>	<u>Operating Rate (%)</u>	<u>Removal Efficiency (%)</u>	<u>Incremental Removal (%)</u>
1.0	10.6%	19.8%	14.4	14.4	6.8	96.9	10.3
1.5	9.9%	29.7%	21.6	21.6	10.2	95.9	9.5
2.0	8.4%	38.1%	28.9	28.9	13.6	95.0	8.0
2.5	7.7%	45.8%	36.1	36.1	17.0	94.0	7.2
3.0	5.9%	51.7%	43.3	43.3	20.4	93.0	5.5
3.5	4.4%	56.1%	50.5	50.5	23.8	92.0	4.0
4.0	4.7%	60.7%	57.7	57.7	27.2	91.1	4.2
4.5	3.3%	64.0%	64.9	64.9	30.6	90.1	3.0
5.0	3.0%	67.1%	72.2	72.2	34.0	89.1	2.7
6.0	5.4%	72.4%	86.6	86.6	40.8	87.2	4.7
7.0	4.4%	76.8%	101.0	101.0	47.6	85.2	3.7
8.0	3.5%	80.3%	115.5	115.5	54.4	83.3	2.9
9.0	2.8%	83.2%	129.9	129.9	61.2	81.3	2.3
10.0	2.2%	85.3%	144.3	144.3	67.9	79.4	1.7
15.0	7.0%	92.3%	216.5	212.4	100.0	68.9	4.8
20.0	4.5%	96.9%	288.6	212.4	100.0	51.7	2.3
25.0	1.4%	98.3%	360.8	212.4	100.0	41.3	0.6
30.0	0.7%	99.0%	432.9	212.4	100.0	34.4	0.2
35.0	0.5%	99.5%	505.1	212.4	100.0	29.5	0.1
40.0	0.5%	100.0%	577.3	212.4	100.0	25.8	0.1

87.1

Removal Efficiency Adjustment² = 6.5%
Predicted Net Annual Load Removal Efficiency = 80.6%
Predicted Annual Rainfall Treated = 97.1%

1 - Based on 42 years of hourly rainfall data from Canadian Station 6105976, Ottawa ON
 2 - Reduction due to use of 60-minute data for a site that has a time of concentration less than 30-minutes.
 3 - CDS Efficiency based on testing conducted at the University of Central Florida
 4 - CDS design flowrate and scaling based on standard manufacturer model & product specifications



**CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION
BASED ON THE RATIONAL RAINFALL METHOD
BASED ON A FINE PARTICLE SIZE DISTRIBUTION**



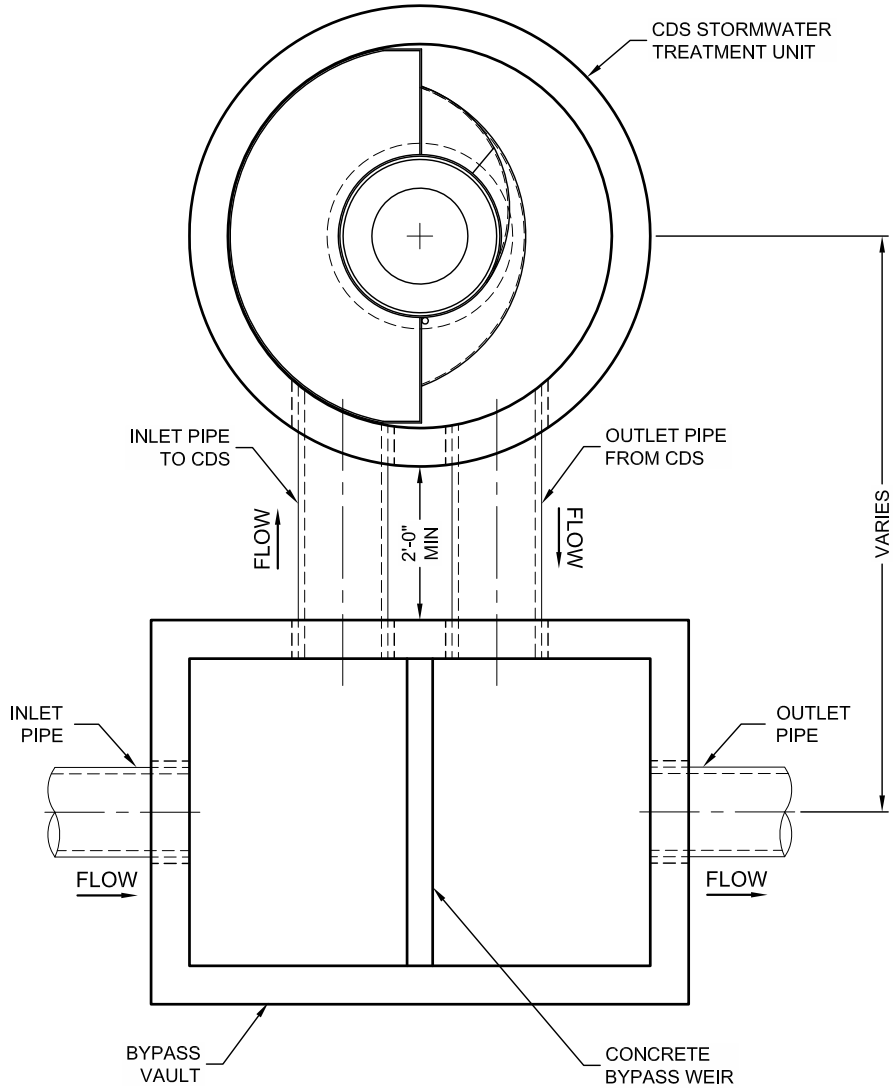
Project Name: 891 Conservancy East	Engineer: DSEL
Location: Ottawa, ON	Contact: K. Murphy
OGS #: 10	Report Date: 20-Oct-22
Area: 6.61 ha	Rainfall Station #: 215
Weighted C: 0.70	Particle Size Distribution: FINE
CDS Model: 4045 (OFFLINE)	CDS Treatment Capacity: 212 l/s

<u>Rainfall Intensity¹</u> <u>(mm/hr)</u>	<u>Percent Rainfall Volume¹</u>	<u>Cumulative Rainfall Volume</u>	<u>Total Flowrate (l/s)</u>	<u>Treated Flowrate (l/s)</u>	<u>Operating Rate (%)</u>	<u>Removal Efficiency (%)</u>	<u>Incremental Removal (%)</u>
1.0	10.6%	19.8%	12.9	12.9	6.1	97.1	10.3
1.5	9.9%	29.7%	19.3	19.3	9.1	96.3	9.5
2.0	8.4%	38.1%	25.7	25.7	12.1	95.4	8.0
2.5	7.7%	45.8%	32.2	32.2	15.1	94.5	7.3
3.0	5.9%	51.7%	38.6	38.6	18.2	93.6	5.6
3.5	4.4%	56.1%	45.0	45.0	21.2	92.8	4.0
4.0	4.7%	60.7%	51.5	51.5	24.2	91.9	4.3
4.5	3.3%	64.0%	57.9	57.9	27.3	91.0	3.0
5.0	3.0%	67.1%	64.3	64.3	30.3	90.2	2.7
6.0	5.4%	72.4%	77.2	77.2	36.3	88.4	4.8
7.0	4.4%	76.8%	90.0	90.0	42.4	86.7	3.8
8.0	3.5%	80.3%	102.9	102.9	48.4	85.0	3.0
9.0	2.8%	83.2%	115.8	115.8	54.5	83.2	2.3
10.0	2.2%	85.3%	128.6	128.6	60.6	81.5	1.8
15.0	7.0%	92.3%	192.9	192.9	90.8	72.8	5.1
20.0	4.5%	96.9%	257.3	212.4	100.0	58.0	2.6
25.0	1.4%	98.3%	321.6	212.4	100.0	46.4	0.7
30.0	0.7%	99.0%	385.9	212.4	100.0	38.6	0.3
35.0	0.5%	99.5%	450.2	212.4	100.0	33.1	0.2
40.0	0.5%	100.0%	514.5	212.4	100.0	29.0	0.2
							88.4

Removal Efficiency Adjustment ² =	6.5%
Predicted Net Annual Load Removal Efficiency =	81.9%
Predicted Annual Rainfall Treated =	97.8%

- 1 - Based on 42 years of hourly rainfall data from Canadian Station 6105976, Ottawa ON
- 2 - Reduction due to use of 60-minute data for a site that has a time of concentration less than 30-minutes.
- 3 - CDS Efficiency based on testing conducted at the University of Central Florida
- 4 - CDS design flowrate and scaling based on standard manufacturer model & product specifications

I:\STORMWATER\COM\WOPS\22 CDS\40 STANDARD DRAWINGS\OFFLINE LAYOUTS DWG\OFFLINE CDS-C LAYOUT BYPASS VAULT STRUCTURED.WG 3/12/2013 3:35 PM



THIS PRODUCT MAY BE PROTECTED BY ONE OR MORE OF THE FOLLOWING U.S. PATENTS: 5,788,848; 6,641,720; 6,511,595; 6,581,783; RELATED FOREIGN PATENTS, OR OTHER PATENTS PENDING.

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CDS STORMWATER TREATMENT SYSTEM
TYPICAL OFFLINE LAYOUT
WITH BYPASS VAULT STRUCTURE

DATE:03/12/13

SCALE: NONE

PROJECT No.: N/A

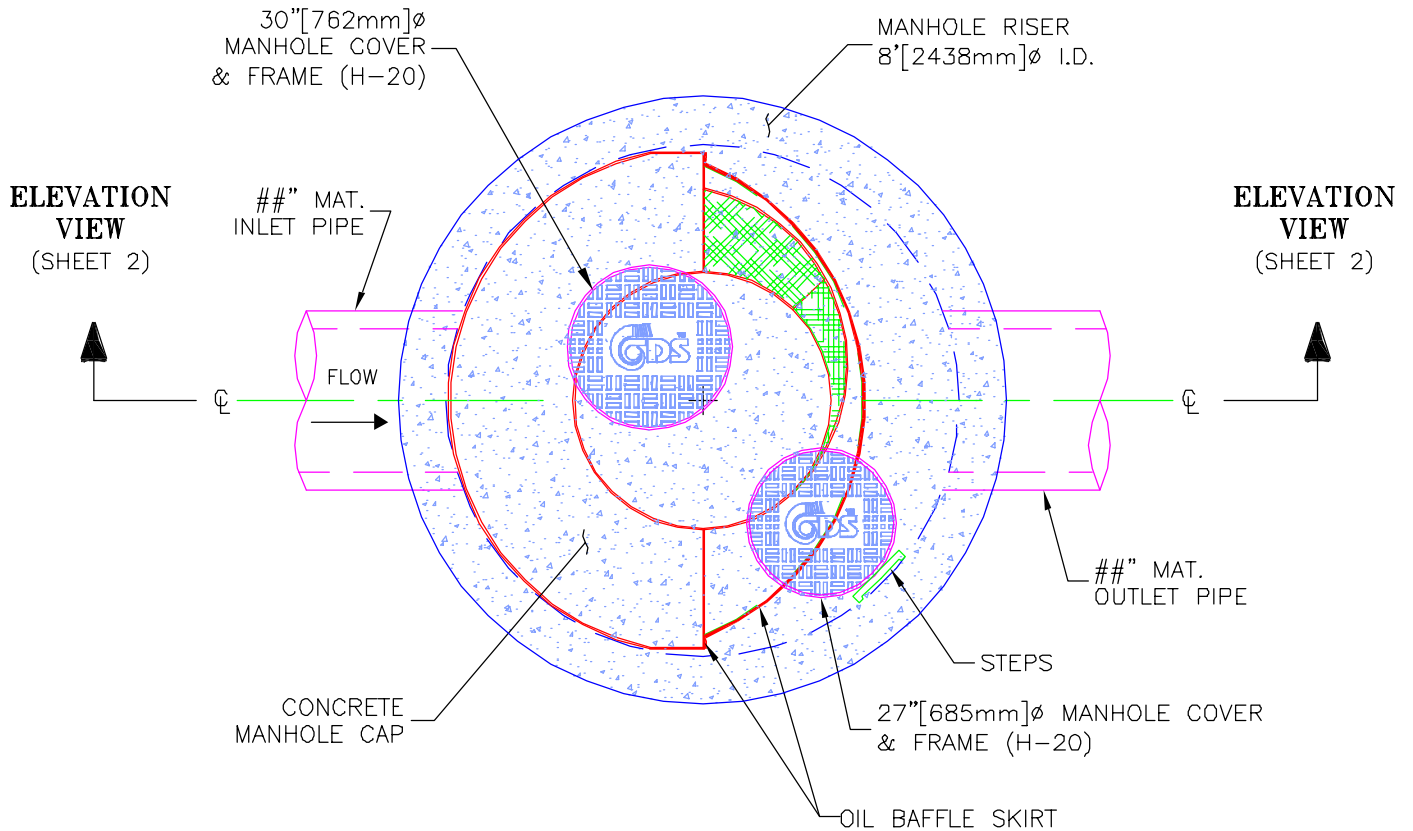
SEQ. No.: N/A

DRAWN: N/A

CHECKED: N/A



PLAN VIEW



CDS MODEL PMSU40_45m, 7.5 CFS TREATMENT CAPACITY STORM WATER TREATMENT UNIT



PROJECT NAME
CITY, STATE

JOB# XX-##-###

DATE ##/##/##

DRAWN INITIALS

APPROV.

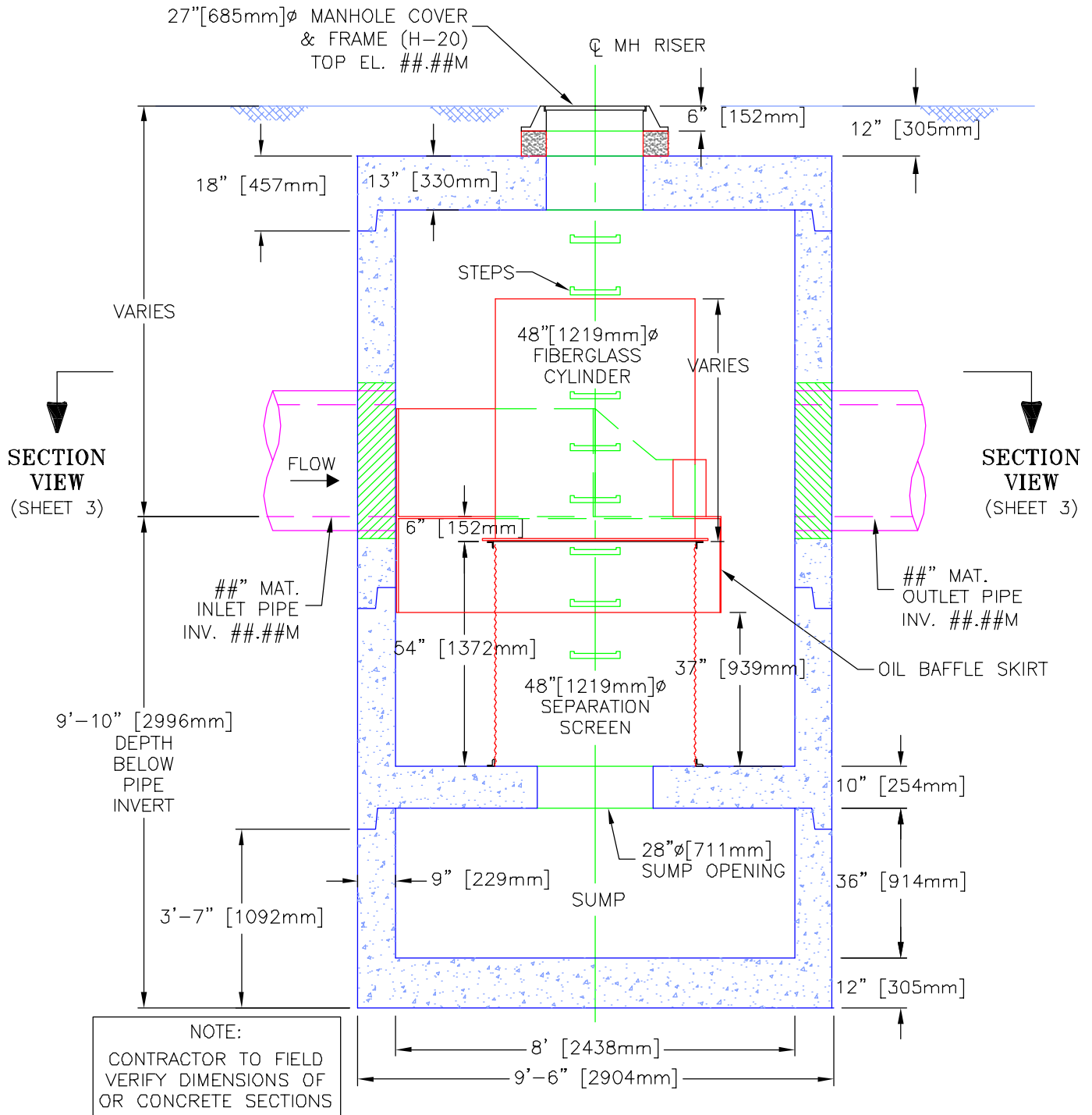
SCALE
1" = 3'

SHEET

1



ELEVATION VIEW

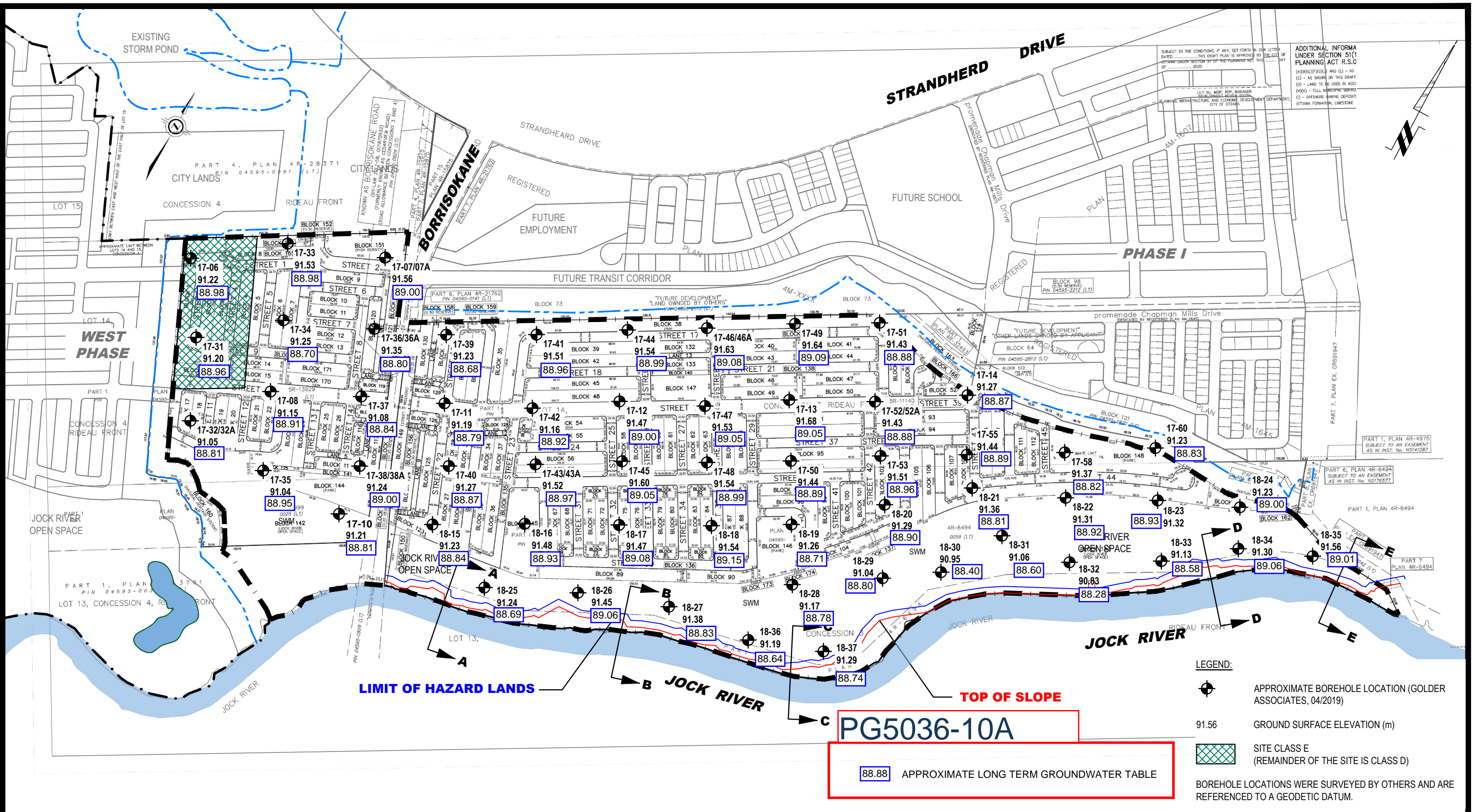


CDS MODEL PMSU40_45m, 7.5 CFS TREATMENT CAPACITY STORM WATER TREATMENT UNIT



PROJECT NAME
CITY, STATE

JOB#	XX-##-###	SCALE 1" = 3'
DATE	##/##/##	SHEET
DRAWN	INITIALS	2
APPROV.		



patersongroup
consulting engineers

154 Colonnade Road South
Ottawa, Ontario K2E 7J5
Tel: (613) 226-7381 Fax: (613) 226-6344

NO.	REVISIONS	DATE	INITIAL
1	CONCEPTUAL PLAN ADDED	09/01/2020	DJG

CAIVAN COMMUNITIES
GEOTECHNICAL INVESTIGATION
PROP. RESIDENTIAL DEVELOPMENT - CONSERVANCY LANDS EAST
OTTAWA, ONTARIO
Title: **TEST HOLE LOCATION PLAN**

Scale:	1:6000	Date:	09/2019
Drawn by:	MPG	Report No.:	PG5036-1
Checked by:	SD	Dwg. No.:	PG5036-1
Approved by:	DJG	Revision No.:	1

December 01, 2022

Project Number: 1474(03)

David Schaeffer Engineering Ltd
120 Iber Road, Unit 103
Ottawa, Ontario
K2S 1E9

Attention: Kevin Murphy, P.Eng

Subject: BCDC Phase 5 – Preliminary HGL Analysis

Introduction

Phase 5 of the Barrhaven Conservancy Development is located in Barrhaven, Ontario, north of the Jock River, east of the Foster Creek and West of Borrisokane Road. The proposed development is approximately **13.17 ha** that will primarily comprise of single and townhouse residential lots along with a **0.64 ha** park. The following outlines the preliminary hydraulic grade line (HGL) assessment for the site, to ensure that the proposed minor system within the development is adequately sized to safely convey flows to the Jock River under various conditions. As such the following memo outlines the approach taken in assessing the development's HGL and summarises the findings of this analysis.

Analysis Approach

Preliminary hydraulic grade line calculations for the proposed BCDC Phase 5 development were completed using PCSWMM modelling software. Pipe data, trunk storm sewer layout and Rational Method flows in the storm sewer are as provided by DSEL. The Rational Method flows were calculated based on the 2-, 5- or 10-year level of service requirements, and the 100-year flows in the hydraulic grade line calculations were estimated as 14% greater than the Rational Method flows, to account for the additional flows captured by catchbasin grates, lead pipes and/or inlet control devices under the higher surface water depths of the 100-year storm.

The 14% increase in flows for the 100-year event is based on the assumption that the head on a lead pipe/ICD will increase by 35 cm (maximum allowable major system ponding depth) during the 100-Year event. Taking a typical 250 mm lead pipe and assuming that the head on the pipe is just below the top of the grate (assumed at 1.38 m) results in a peak flow of 209 L/s, then assuming that the head is increased by 35 cm during the 100-Year (head of 1.730m) the flow through the lead pipe would increase to 234.5 L/s, which results in a 12% increase in peak flows. It is important to note that a 12% increase is observed when the same calculations are applied to the various lead pipe and ICD sizes. An additional 2% is added as a safety factor to allow some flexibility in the design, as it is likely that not all lead pipes will have a head of 1.38 m (just below the top of MH) for the level of service specified.

The proposed storm sewer infrastructure data was extracted from DSEL's drawings and incorporated into a PCSWMM model, and flows derived by DSEL's Rational Method calculations were then applied to each Maintenance Hole (MH) in the model as steady flows (using the baseflow option). Exit losses were applied to all storm sewer pipes in the system based on the angle of the downstream connection.

As in line with all other works completed for the BCDC development phases, the preliminary HGL analysis was completed under two conditions:

- 100-year rainfall event on the development and a 5-year spring water level on the Jock River
- Level of service (2/5/10-year) rainfall event on the development and a 100-year spring water level on the Jock River

Note that the water level along the Jock River through the length of this development varies, and as such the nearest corresponding upstream water surface elevation calculated by RVCA's HEC-RAS floodplain mapping model of the Jock River was applied at each of the respective storm sewer outlets. Also, note that assuming a 5-year spring water level on the Jock River for a 100-year rainfall event on the development is an inherently conservative assumption, as the critical storm for the proposed development is a summer (intense rainfall) event while the critical storm for the Jock River is a spring (snowmelt + rainfall) event. A preliminary Single Station Flood Frequency analysis was completed by JFSA using only summer flows (from May 15 to October 31) based on historical flow data recorded at the Moodie Drive Water Survey Canada gauge. This analysis found that the 100-year summer flow on the Jock River is around **99 m³/s**, while the 5-year spring flow is around **123 m³/s**, therefore the downstream boundary condition applied is conservative.

Within the proposed development Oil and Grit Separators (OGS) units in conjunction with LID measures will be implemented to ensure the site meets quality control requirements. Preliminary OGS units and associated by-pass weir elevations have also been included in the model, based on similar drainage areas and imperviousness seen in BCDC Phase 2.

Trunk Sewer 9 will have a drainage area of **7.21 ha** at **75%** imperviousness, Trunk Sewer 10 has a drainage area of **6.56 ha** at **80%** imperviousness. In a preliminary consultation with the OGS manufacturer, it was suggested that the closest match to the detailed OGS sizing for BCDC Phase 2 is **OGS 3**, which used a **PMSU 4045-8** OGS unit with a weir height of **0.65m**, this unit had a drainage area of **6.77 ha** at **64%** imperviousness.

Results

The maximum HGL obtained at each MH has been extracted from the level of service (2/5/10-year) event / 100-year Jock River water level scenario and the 100-year event / 5-year Jock River water level scenario, with the results from this analysis provided in Tables 1 & 2, respectively. As all proposed units within this development will have sump pumps, the simulated HGL was compared against the top of MH elevation to ensure that all storm sewers infrastructure is sufficiently sized and is not surcharging to the major system during the assessed events.

From this analysis, it was found that the critical scenario for HGL within the development was the level of service development event and 100-year water level on the Jock River scenario. Based on this scenario, no MHs will have an HGL elevation above the top of MH (minimum freeboard of **0.64 m** at **MH-514** to **MH-516** and **MH-521**), with an average freeboard of **0.74 m** from the top of MH throughout the proposed development.

For the 100-year event and 5-year water level on the Jock River, no MHs will have HGL elevations above the top of MH (minimum freeboard of **1.22 m** at **MH-514** and **MH-515**), with an average freeboard of **1.38 m** from the top of MH throughout the proposed development. As such it can be concluded that the proposed storm sewer infrastructure is sufficiently sized, to safely convey minor system flows from the development under various extreme conditions.

Conclusion

A preliminary HGL analysis for Phase 5 of the Barrhaven Conservancy Development was completed using PCSWMM based on storm sewer and flow details provided by DSEL. From this analysis, it was found that the proposed storm sewer infrastructure is sufficiently sized to convey all minor system flows to the Jock River and will not result in any MHs surcharging to the street under extreme events such as 100-year rainfall events on the development and a 5-year spring water level on the Jock River and a level of service (2/5/10 Year) rainfall event on the development and a 100-year spring water level on the Jock River, with the former being the more critical scenario for the HGL within the development.

Yours truly,
J.F Sabourin and Associates Inc.



Jonathon Burnett, P.Eng
Water Resources Engineer



cc: J.F Sabourin, M.Eng, P.Eng
Director of Water Resources Projects

Figures

Figure 1: PCSWMM Model Overview

Tables

Table 1: HGL Result Tables - Level of service (2/5/10-year) BCDC Development & 100-Year Jock River

Table 2: HGL Result Tables - 100-Year BCDC Development & 5-Year Jock River

Attachments

Attachment A: DSEL Rational Method Calculations

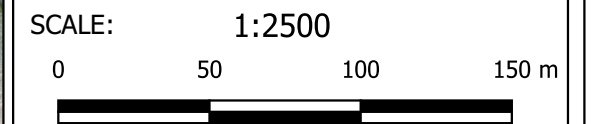
Modelling Files - Provided Electronically

PCSWMM: BCDC-P5_HGL_v01.1-2-5-10-YrDev-100YrJock.inp
BCDC-P5_HGL_v01.1-100-YrDev-5YrJock.inp



Legend

- Junctions
- ▲ Outfalls
- Conduits
- Weirs
- Site Plan



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 Ottawa, ON, K2S 1B9 www.jfsa.com



Barrhaven Conservancy Development
 Phase 5

Figure 1: Preliminary HGL Analysis
 Model Overview

PROJECT	1474(03)-21
DRAWN	JB
DATE	December 2022

Table 1: BCDC Phase 5 - Preliminary HGL Analysis
Level of Service (2/5/10 Year) BCDC Development & 100-Year Jock River

MH-ID	Invert Elevation	Top of MH (m)	Max HGL (m)	Freeboard (m)
MH-507	90.62	93.26	92.54	0.72
MH-513	90.42	93.10	92.43	0.67
MH-514	90.34	93.02	92.38	0.64
MH-515	90.30	93.00	92.36	0.64
MH-516	90.17	92.91	92.27	0.64
MH-521	90.05	92.83	92.19	0.64
MH-524	89.71	92.66	91.99	0.67
MH-525	89.64	92.65	91.93	0.72
MH-525-1	89.63	92.64	91.88	0.76
MH-528	89.63	92.67	91.89	0.78
MH-528-1	89.63	92.67	91.83	0.84
MH-529	90.43	93.01	92.23	0.78
MH-530	90.37	93.01	92.20	0.81
MH-534	90.17	92.99	92.11	0.88
MH-537	90.02	92.91	92.07	0.84
MH-538	89.87	92.91	92.01	0.90
MH-543	89.69	92.65	91.96	0.69
			Min	0.64
			Max	0.90
			Average	0.74

Note: Analysis assumes 100 year spring water level on the Jock River

Model Name:BCDC-P5_HGL_v01.1-2-5-10-YrDev-100YrJock.inp

**Table 2: BCDC Phase 5 - Preliminary HGL Analysis
100-Year BCDC Development & 5-Year Jock River**

MH-ID	Invert Elevation	Top of MH (m)	Max HGL (m)	Freeboard (m)
MH-507	90.62	93.26	92.02	1.24
MH-513	90.42	93.10	91.87	1.23
MH-514	90.34	93.02	91.81	1.22
MH-515	90.30	93.00	91.78	1.22
MH-516	90.17	92.91	91.67	1.24
MH-521	90.05	92.83	91.56	1.27
MH-524	89.71	92.66	91.29	1.37
MH-525	89.64	92.65	91.22	1.43
MH-525-1	89.63	92.64	91.16	1.48
MH-528	89.63	92.67	91.19	1.48
MH-528-1	89.63	92.67	91.12	1.55
MH-529	90.43	93.01	91.63	1.38
MH-530	90.37	93.01	91.59	1.42
MH-534	90.17	92.99	91.47	1.52
MH-537	90.02	92.91	91.42	1.49
MH-538	89.87	92.91	91.34	1.57
MH-543	89.69	92.65	91.27	1.38
			Min	1.22
			Max	1.57
			Average	1.38

Note: Analysis assumes 5 year spring water level on the Jock River

Model Name:BCDC-P5_HGL_v01.1-100-YrDev-5YrJock.inp



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Québec, QC

Attachment A

DSEL Rational Method Calculations

STORM SEWER CALCULATION SHEET (RATIONAL METHOD)

Local Roads Return Frequency = 2 years
 Collector Roads Return Frequency = 5 years
 Arterial Roads Return Frequency = 10 years



Manning 0.013

LOCATION			AREA (Ha)																FLOW						SEWER DATA										
			2 YEAR				5 YEAR				10 YEAR				100 YEAR				Time of	Intensity	Intensity	Intensity	Intensity	Peak Flow	DIA. (mm)	DIA. (mm)	TYPE	SLOPE	LENGTH	CAPACITY	VELOCITY	TIME OF	RATIO		
Location	From Node	To Node	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	Conc. (min)	2 Year (mm/h)	5 Year (mm/h)	10 Year (mm/h)	100 Year (mm/h)	Q (l/s)	(actual)	(nominal)	(%)	(m)	(l/s)	(m/s)	LOW (min)	Q/Q full			
	548	528	0.03	0.67	0.06	3.24			0.00	0.09			0.00	0.00			0.00	0.00	16.61	58.20	78.68	92.12	134.48	196	600	600	CONC	0.25	36.0	307.0058	1.0858	0.5526	0.637		
To Centerline13 - 13, Pipe 528 - HW9						3.24				0.09				0.00				0.00	17.17																
Centerline8 - 08																																			
	539	540	0.32	0.67	0.60	0.60			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	46	300	300	PVC	0.40	52.0	61.1589	0.8652	1.0017	0.749		
	540	541	0.41	0.67	0.76	1.36			0.00	0.00			0.00	0.00			0.00	0.00	11.00	73.16	99.18	116.24	169.89	99	450	450	CONC	0.20	68.0	127.5033	0.8017	1.4137	0.780		
	541	542	0.13	0.67	0.24	1.60			0.00	0.00			0.00	0.00			0.00	0.00	12.42	68.63	92.96	108.91	159.13	110	450	450	CONC	0.25	10.5	142.5531	0.8963	0.1952	0.771		
	542	543	0.17	0.67	0.32	1.92			0.00	0.00			0.00	0.00			0.00	0.00	12.61	68.05	92.17	107.98	157.76	131	600	600	CONC	0.15	48.0	237.8056	0.8411	0.9512	0.549		
To Centerline13 - 13, Pipe 543 - 528						1.92				0.00				0.00				0.00	13.56																
Centerline1 - 01																																			
	519	521			0.00	0.00	0.75	0.67	1.40	1.40			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	146	525	525	CONC	0.20	118.0	192.3297	0.8885	2.2136	0.757		
To Centerline3 - 03, Pipe 521 - 524						0.00			1.40					0.00				0.00	12.21																
	535	536			0.00	0.00	0.21	0.80	0.47	0.47			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	49	375	375	PVC	0.30	51.5	96.0323	0.8695	0.9872	0.507		
	536	537			0.00	0.00	0.18	0.80	0.40	0.87			0.00	0.00			0.00	0.00	10.99	73.21	99.25	116.32	170.01	86	450	450	CONC	0.20	53.5	127.5033	0.8017	1.1122	0.675		
To Centerline13 - 13, Pipe 537 - 538						0.00			0.87					0.00				0.00	12.10																
Contribution From Centerline11 - 11, Pipe 515 - 516						5.07			0.69					0.85				0.00	17.57																
	516	521			0.00	5.07	0.25	0.67	0.47	1.15			0.00	0.85			0.00	0.00	17.57	56.29	76.07	89.05	129.98	449	900	900	CONC	0.11	58.0	600.4123	0.9438	1.0242	0.748		
To Centerline3 - 03, Pipe 521 - 524						5.07			1.15					0.85				0.00	18.60																
Centerline9 - 09																																			
	531	533	0.25	0.80	0.56	0.56			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	94	525	525	CONC	0.20	104.5	192.3297	0.8885	1.9603	0.490		
To Centerline6 - 06, Pipe 533 - 534						1.23			0.00					0.00				0.00	11.96																
	544	545	0.36	0.80	0.80	0.80			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	61	375	375	PVC	0.30	78.5	96.0323	0.8695	1.5047	0.640		
	545	546	0.26	0.80	0.58	1.38			0.00	0.00			0.00	0.00			0.00	0.00	11.50	71.47	96.86	113.51	165.88	99	450	450	CONC	0.20	78.5	127.5033	0.8017	1.6320	0.773		
To Centerline12 - 12, Pipe 546 - 547						1.38			0.00					0.00				0.00	13.14																
Centerline6 - 06																																			
	532	533	0.20	0.80	0.44	0.44			0.00	0.00			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	89	450	450	CONC	0.20	62.0	127.5033	0.8017	1.2889	0.697		
Contribution From Centerline9 - 09, Pipe 531 - 533						1.23			0.00					0.00				0.00	11.96																
	533	534	0.13	0.80	0.29	2.67			0.00	0.00			0.00	0.00			0.00	0.00	11.96	70.02	94.87	111.16	162.43	187	600	600	CONC	0.20	44.5	274.5943	0.9712	0.7637	0.681		
To Centerline14 - 14, Pipe 534 - 537						2.67			0.00					0.00				0.00	12.72																
Centerline15 - 15																																			
	506	507			0.00	0.00			0.00	0.00	0.36	0.85	0.85	0.85			0.00	0.00	10.00	76.81	104.19	122.14	178.56	104	450	450	CONC	0.25	77.0	142.5531	0.8963	1.4318	0.729		
To Centerline4 - 04, Pipe 507 - 513						0.00			0.00					0.85				0.00	11.43																
	526	529	0.93	0.80	2.07	2.07			0.00	0.00	0.23	0.85	0.54	0.54			0.00	0.00	10.00	76.81	104.19	122.14	178.56	225	600	600	CONC	0.25	62.0	307.0058	1.0858	0.9517	0.734		
To Centerline14 - 14, Pipe 529 - 530						2.07			0.00					0.54				0.00	10.95																
	527	529			0.00	0.00			0.00	0.00	0.26	0.85	0.61	0.61			0.00	0.00	10.00	76.81	104.19	122.14	178.56	75	375	375	PVC	0.35	46.0	103.7267	0.9392	0.8163	0.723		
To Centerline14 - 14, Pipe 529 - 530						0.00			0.00					0.61				0.00	10.82																
	503	504			0.00	0.00	0.10	0.85	0.24	0.24			0.00	0.00			0.00	0.00	10.00	76.81	104.19	122.14	178.56	25	300	300	PVC	0.35	41.0	57.2089	0.8093	0.8443	0.430		
	504	505			0.00	0.00	0.14	0.85	0.33	0.57			0.00	0.00			0.00	0.00	10.84	73.71	99.94	117.13	171.19	57	375	375	PVC	0.30	60.0	96.0323	0.8695	1.1501	0.590		
Contribution From Centerline7 - 07, Pipe 502 - 505						0.63			0.00					0.00				0.00	12.85																
	505	507			0.00	0.63	0.05	0.85	0.12	0.69			0.00	0.00			0.00	0.00	12.85	67.36	91.22	106.87	156.13	105	525	525	CONC	0.20	21.0	192.3297	0.8885	0.3939	0.547		
To Centerline4 - 04, Pipe 507 - 513						0.63			0.69					0.00				0.00	13.24																

Definitions:
 Q = 2.78 AIR, where
 Q = Peak Flow in Litres per second (L/s)
 A = Areas in hectares (ha)
 I = Rainfall Intensity (mm/h)
 R = Runoff Coefficient

Notes:
 1) Ottawa Rainfall-Intensity Curve
 2) Min. Velocity = 0.80 m/s

Designed: A.S.	PROJECT: Barrhaven Conservancy East Phase 5		
Checked: W.L./V.W.	LOCATION: City of Ottawa		
Dwg. Reference:	File Ref:	Date: 01 Dec 2022	Sheet No. SHEET 2 OF 3

STORM SEWER CALCULATION SHEET (RATIONAL METHOD)



Local Roads Return Frequency = 2 years
 Collector Roads Return Frequency = 5 years
 Arterial Roads Return Frequency = 10 years

Manning 0.013

LOCATION			AREA (Ha)																FLOW					SEWER DATA												
			2 YEAR				5 YEAR				10 YEAR				100 YEAR				Time of	Intensity	Intensity	Intensity	Intensity	Peak Flow	DIA. (mm)	DIA. (mm)	TYPE	SLOPE	LENGTH	CAPACITY	VELOCITY	TIME OF	RATIO			
Location	From Node	To Node	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	AREA (Ha)	R	Indiv. 2.78 AC	Accum. 2.78 AC	Conc. (min)	2 Year (mm/h)	5 Year (mm/h)	10 Year (mm/h)	100 Year (mm/h)	Q (l/s)	(actual)	(nominal)	(%)	(m)	(l/s)	(m/s)	LOW (min)	Q/Q full				
Centerline14 - 14																																				
Contribution From Centerline15 - 15, Pipe 526 - 529					2.07					0.00					0.54				0.00																	
Contribution From Centerline15 - 15, Pipe 527 - 529					0.00					0.00					0.61				0.00																	
	529	530	0.52	0.80	1.16	3.22			0.00	0.00			0.00	1.16			0.00	0.00	10.95	73.33	99.42	116.52	170.30	371	825	825	CONC	0.11	26.5	476.0801	0.8906	0.4959	0.780			
	530	534			0.00	3.22			0.00	0.00			0.00	1.16			0.00	0.00	11.45	71.66	97.12	113.81	166.33	363	825	825	CONC	0.11	117.0	476.0801	0.8906	2.1895	0.762			
Contribution From Centerline6 - 06, Pipe 533 - 534					2.67					0.00				0.00					0.00																	
	534	537	0.11	0.80	0.24	6.14			0.00	0.00			0.00	1.16			0.00	0.00	13.64	65.18	88.24	103.36	150.97	520	900	900	CONC	0.15	48.5	701.1305	1.1021	0.7334	0.742			
To Centerline13 - 13, Pipe 537 - 538					6.14					0.00				1.16					0.00																	
Centerline13 - 13																																				
Contribution From Centerline14 - 14, Pipe 534 - 537					6.14					0.00				1.16					0.00																	
Contribution From Centerline1 - 01, Pipe 536 - 537					0.00	6.14	0.06	0.67	0.11	0.98			0.00	1.16			0.00	0.00	12.10																	
	537	538	0.28	0.67	0.52	6.66			0.00	0.98			0.00	1.16			0.00	0.00	14.37	63.29	85.65	100.31	146.50	622	975	975	CONC	0.15	83.0	867.9562	1.1625	1.1899	0.716			
	538	543	0.25	0.67	0.47	7.13			0.00	0.98			0.00	1.16			0.00	0.00	15.56	60.48	81.79	95.77	139.84	622	975	975	CONC	0.15	69.0	867.9562	1.1625	0.9892	0.717			
Contribution From Centerline8 - 08, Pipe 542 - 543					1.92					0.00				0.00					0.00																	
	543	528	0.05	0.67	0.09	9.14			0.00	0.98			0.00	1.16			0.00	0.00	16.55	58.34	78.86	92.33	134.80	717	1050	1050	CONC	0.11	29.0	905.6791	1.0459	0.4621	0.792			
Contribution From Centerline12 - 12, Pipe 548 - 528					3.24					0.00				0.00					0.00																	
	528	HW9			0.00	12.38			0.00	1.07			0.00	1.16			0.00	0.00	17.17	57.08	77.15	90.32	131.84	894	1050	1050	CONC	0.20	4.5	1221.2174	1.4103	0.0532	0.732			

Definitions:
 Q = 2.78 AIR, where
 Q = Peak Flow in Litres per second (L/s)
 A = Areas in hectares (ha)
 I = Rainfall Intensity (mm/h)
 R = Runoff Coefficient

Notes:
 1) Ottawa Rainfall-Intensity Curve
 2) Min. Velocity = 0.80 m/s

Designed: A.S.	PROJECT: Barrhaven Conservancy East Phase 5		
Checked: W.L./V.W.	LOCATION: City of Ottawa		
Dwg. Reference:	File Ref:	Date: 01 Dec 2022	Sheet No. SHEET 3 OF 3

March 08, 2021

Project Number: 1474

David Schaeffer Engineering Ltd
120 Iber Road, Unit 103
Ottawa, Ontario
K2S 1E9

Attention: Steve Pichette, P.Eng.

Subject: Review of Quantity Control Requirement for Jock River-Reach One

Introduction

Phase 2 of the Barrhaven Conservancy Development (aka Conservancy East) is located in Barrhaven, Ontario, north of the Jock River, south of the Fraser Clarke Creek and east of the Foster Creek. The proposed development is approximately 59.26 ha that will primarily comprise of single and townhouse residential lots. As a part of the City of Ottawa's review of the proposed development draft plan of Phase 2 of the Barrhaven Conservancy Development, submitted in December 2020, it is proposed that flood quantity control measures will not need to be implemented as a part of this development. This assumption is based on the work completed by Stantec in June 2007 in the "Jock River Reach One Subwatershed Study" which concluded that for future developments within Reach 1 of the Jock River: "No quantity control storage is required for flood control purposes as the hydrograph from the subwatershed will peak before the upstream peak in the Jock River" and that "No erosion control storage is required to maintain the predevelopment in-stream erosion condition". Although this study did not consider the future development of the Barrhaven Conservancy Lands, and as such the modelling completed by Stantec has been updated by JFSA to reflect these changes. The following memo outlines data sources, assessed scenarios, assumptions, and conclusions of this independent Jock River Reach One study.

It is noted that RVCA is currently engaging in a formal update/review of the Jock River Reach One Subwatershed Study, with the findings of this study having the potential to affect the above-noted design criteria. While that study is underway J.F. Sabourin and Associates Inc. (JFSA) has completed an independent Jock River - Reach One study to re-assess/confirm that the assumptions presented in the original 2007 study by Stantec are still valid, as any changes to this conclusion could greatly impact the current BCDC Phase 2 development plan.

Background Data

The following outlines all the model and data sources used in this analysis:

- "Jock River Floodplain Mapping Report", (2005 - PSR Group Ltd. & JFSA)
- "Jock River Reach One Subwatershed Study Final Report", (2007 – Stantec)
- "Corrigan Stormwater Management Facility Stormwater Management Report and Design Brief", (2010 - IBI Group)
- "Citi Gate, Highway 416 Employment Lands, Servicing Study and Stormwater Management Report (O'Keefe SWM)", (2012 – Novatech)
- "Foster Stormwater Management Facility, Environmental Study Report", (2013 - CH2MHill)
- "Todd Pond Model Keeper Analysis (Re-Assessment of Existing System Capacity)", (2015 – JFSA)

- “CitiGate 416 Corporate Campus Detailed Servicing and Stormwater Management Report (Phase 1)”, (2015 – Novatech)
- “Kennedy-Burnett Stormwater Management Facility Retrofit, Detailed Design Report”, (2020 – Novatech)
- “Half Moon Bay South / Addendum to April 2015 Todd Pond Model Keeper Analysis, Re-Assessment of Existing System Capacity Report” (2020 - JFSA).

Model Development/Scenarios

The following section outlines the various hydrologic model scenarios developed as a part of this work, with a brief description of the data sources used for each scenario and how they have been incorporated into the existing Jock River subwatershed hydrologic model.

Model 1 - Jock River Floodplain Model – JFSA, 2005

This hydrologic model was developed as a part of the floodplain mapping study of the Jock River completed in 2005. The hydrologic model of the Jock River was developed by JFSA using SWMHYMO, with independent models developed to simulate both summer and spring events. Both models were calibrated to field measured flows, recorded at the Water Survey Canada Flow Gauge at Moodie Drive. These models function as the basis for which all future models (both by JFSA and others) have been built on. Refer to Figure 1 (JFSA, 2005) for an overview of the subcatchments for reach one in this model, with full SWMHYMO input and summary files provided in Attachment A.

Model 2 – Jock River Reach One Model – Stantec, 2007

The hydrologic analysis completed by Stantec in 2007 built upon the JFSA 2005 floodplain mapping modelling. As a part of the Stantec work, the lower reach of the Jock River (3,176 ha) which was represented as a single subcatchment in the 2005 study was subdivided into thirteen (13) subcatchments to better delineate the drainage areas to the various tributaries (O’Keefe, Fraser, Foster, Todd, Corrigan and Clarke) and to also provide a better representation of the existing development areas (Kennedy Burnett, Chapman Mills, Jockvale and Hearts Desire). The remaining natural/undeveloped areas within the Jock River corridor were subdivided into three smaller (3) sub-catchments. Refer to Figure 2 (Stantec, 2007) for an overview of the subcatchments for reach one in this model, with full SWMHYMO input and summary files provided in Attachment B.

As mentioned above from this study, it was concluded that developments located in the lower reaches of the Jock River do not require any quantity control storage for flood control purposes as the hydrograph from the subwatershed will peak before the upstream peak in the Jock River and that no erosion control storage is required to maintain the pre-development in-stream erosion conditions.

Model 3 – Jock River Reach One Model Update – JFSA, 2021

As a part of the study outlined in this report, the 2007 Stantec SWMHYMO model of the Jock River was updated to reflect (as best as possible with the available information) proposed, approved and potential future developments, since the 2007 study.

At the time of the 2007 study, it was assumed that the floodplain of reach one of the Jock River (from Highway 416 to Greenbank Road) would not be filled and developed. Furthermore, the assumptions that were made in 2007 for the total imperviousness of future developments are not reflective of the actual constructed conditions observed in 2021; for example, the total impervious area for the Todd drainage area was assumed to be 43% in the 2007 study, while based on latest aerial photography it appears that the imperviousness for this area is closer to 58.5%). Additionally, SWM quantity controls were implemented in some tributaries within Reach One (e.g., O'Keefe, Foster and Kennedy-Burnett) to respect the hydraulic capacity of the local watercourses or other existing hydraulic constraints.

As outlined in the Background Data section of this memo, data from various reports and studies were collected and used to update Stantec's 2007 model, to best reflect existing conditions and known approved and planned development projects. As such, the thirteen (13) subcatchments of the 2007 Stantec model have been further discretized into one hundred ten (110) subcatchments, with numerous additional major system storage, SWM Ponds, and channel routing commands added. This updated existing condition model is reflective of current 2021 conditions, which assumes that the lower Jock River floodplain is undeveloped. It should also be noted that only subcatchments downstream of Highway 416 have been updated as a part of this analysis. Updates to other catchments of the Jock River further upstream, such as the Monahan Drain, Hobbs Creek, King Creek, and development areas in Richmond, where additional new information may be available, have not been included in the model updates at this time. Refer to Figure 3 for an overview of the subcatchments for reach one in this model, with full SWMHYMO input and summary files been provided in Attachment C, detailed schematics of the subcatchments updated as a part of this study have been provided in Attachment F.

Note that Novatech's PCSWMM model of the Kennedy-Burnett area was used to create a detailed SWMHYMO model of the same area. In creating this SWMHYMO model it was found that the 100-year peak outflows from the Kennedy Burnett facility were 1.4 times higher than that reported in the Novatech PCSWMM model. While it is expected that different modelling software will produce slightly different results, this difference is significant and should be investigated further; although it is unlikely that this difference is expected to change the fundamental conclusions of this analysis.

Model 4A & 4B – Jock River Reach One Future Conditions (without and with quantity SWM controls) – JFSA, 2021

Two additional models (4A and 4B) were created (which built on model 3) to evaluate the impacts of developing portions of the lower Jock River floodplain (from Highway 416 to Greenbank Road). These lands make up approximately 156 ha and would include BCDC and other properties on the south side of the Jock River. Model 4A assumes that these lands would be developed without any SWM quantity controls and Model 4B assumes that the lands would be developed with SWM Post to Pre-development quantity controls. Refer to Figure 4 for an overview of the subcatchments for reach one in these models, with full SWMHYMO input and summary files for scenarios 4A and 4B provided in Attachment D & E, respectively.

Results

All hydrologic models were run using a 24 hours SCS storm for the 2-to-100-year events. Note that this analysis focuses on this particular rainfall event as for developed areas the summer rainfall events are more critical than the spring rainfall plus snowmelt conditions. Hence, only the summer peak flows have been summarized and compared for the various scenarios below, as the flow contributions from the developments in the lower Jock River under the spring rainfall + snowmelt event are negligible compared to the flows upstream from the greater Jock River. It is further noted that the same design storms were used in all models.

Peak flows at key locations along Reach One of the Jock River have been extracted from the various hydrologic models and provided in the following section. As a part of this analysis, 5 key locations on the Jock River have been selected to compare the simulated peak flows and are as follows: Highway 416, Borrisokane Road, Greenbank Road, Jockvale Road and the Jock River's confluence with the Rideau River. Note that for the older models (JFSA 2005 & Stantec 2007) results have only been provided at some locations, as these original models were not discretized to this higher level of detail. Additionally, the Stantec 2007 model did not assess flows on the Jock River for the 10- and 50-year events at any locations.

Table 1: Comparison of Summer Peak Flows (m³/s) at Highway 416 (52483.00 ha)

Scenario	Return Period					
	2-Year	5- Year	10-Year	25-Year	50-Year	100-Year
Model 1: 2005 Floodplain Study	45.676	66.292	82.076	104.643	122.469	141.415
Model 2: Stantec 2007 Reach One Analysis	45.789	66.413	n/a	104.834	n/a	141.853
Model 3: Updated Model 2 to current/ approved conditions	46.294	67.222	83.235	106.109	124.249	143.580
Model 4A: Model 3 with BCDC & others w/o SWM	46.294	67.222	83.235	106.109	124.249	143.580
Model 4B: Model 3 with BCDC & others with SWM	46.294	67.222	83.235	106.109	124.249	143.580

From Table 1 above it is seen that the peak flows on the Jock River at Highway 416 for Models 3, 4A and 4B are higher than in Models 1 and 2. This is because the computational time step in the updated models was reduced from 5 - 10 minutes to 1 minute. This change was necessary to provide stable results in the various models, especially with the additional ROUTE CHANNEL commands that have been added to the updated models. There were no other changes made to the models upstream of Highway 416.

Table 2: Comparison of Summer Peak Flows (m³/s) at Borrisokane Road (53577.82 ha)

Scenario	Return Period					
	2-Year	5- Year	10-Year	25-Year	50-Year	100-Year
Model 1: 2005 Floodplain Study	n/a	n/a	n/a	n/a	n/a	n/a
Model 2: Stantec 2007 Reach One Analysis	46.817	68.124	n/a	107.402	n/a	144.892
Model 3: Updated Model 2 to current/ approved conditions	47.379	69.117	85.613	108.988	127.740	147.849
Model 4A: Model 3 with BCDC & others w/o SWM	47.426	68.998	85.561	109.064	127.650	147.535
Model 4B: Model 3 with BCDC & others with SWM	47.599	69.319	85.870	109.449	128.055	147.939

From Table 2 it is seen that the peak flows on the Jock River at Borrisokane are generally lower in model 4A (developed without SWM controls) than under existing conditions (Model 3). The inclusion of SWM controls for these future developments results in the peak flows increasing from existing conditions for all return periods at this location. Note that the increase in flows at this location between the Stantec model (model 2) and the JFSA existing conditions model (model 3) again is due to the greater discretization of subcatchments at Borrisokane Road in the JFSA model. For example, in the Stantec model, the subcatchment that represents the currently undeveloped lands along the Jock River is represented as a single subcatchment (S-1). Where the JFSA updated model represents these lands as 14 individual subcatchments, all discharging to their respective locations within the Jock River (e.g. O’Keefe Creek, Foster Creek & Borrisokane Road).

Table 3: Comparison of Summer Peak Flows (m³/s) at Greenbank Road (54717.80 ha)

Scenario	Return Period					
	2-Year	5- Year	10-Year	25-Year	50-Year	100-Year
Model 1: 2005 Floodplain Study	n/a	n/a	n/a	n/a	n/a	n/a
Model 2: Stantec 2007 Reach One Analysis	49.195	71.220	n/a	111.172	n/a	149.236
Model 3: Updated Model 2 to current/ approved conditions	49.055	70.826	86.895	110.282	128.564	147.488
Model 4A: Model 3 with BCDC & others w/o SWM	48.599	69.773	85.389	103.842	126.050	144.531
Model 4B: Model 3 with BCDC & others with SWM	48.982	70.171	85.928	103.651	126.537	144.894

From Table 3 it is seen that peak flows on the Jock River at Greenbank Road are the lowest without SWM controls in place (Model 4A). With SWM controls in place, the peak flows are lower than the existing conditions, but not as low as when SWM controls are not implemented. Note that the JFSA existing conditions model (model 3) is presenting peak flows lower than the Stantec model (model 2) at this location, again this is due to the greater discretization in the JFSA model as discussed above.

Table 4: Comparison of Summer Peak Flows (m³/s) at Jockvale Road (55476.26 ha)

Scenario	Return Period					
	2-Year	5- Year	10-Year	25-Year	50-Year	100-Year
Model 1: 2005 Floodplain Study	n/a	n/a	n/a	n/a	n/a	n/a
Model 2: Stantec 2007 Reach One Analysis	49.870	72.143	n/a	112.074	n/a	150.033
Model 3: Updated Model 2 to current/ approved conditions	49.619	72.224	88.294	111.989	130.865	149.819
Model 4A: Model 3 with BCDC & others w/o SWM	49.482	71.017	86.165	105.082	128.174	146.840
Model 4B: Model 3 with BCDC & others with SWM	49.606	71.408	86.690	104.765	128.229	147.027

From Table 4 is seen that the peak flows at Jockvale Road are generally at their lowest without SWM controls in place, and that either implementing or not implementing SWM controls for future developments results in peak flows at this location being less than existing conditions.

Table 5: Comparison of Summer Peak Flows (m³/s) at Outlet of Jock River (55579.20 ha)

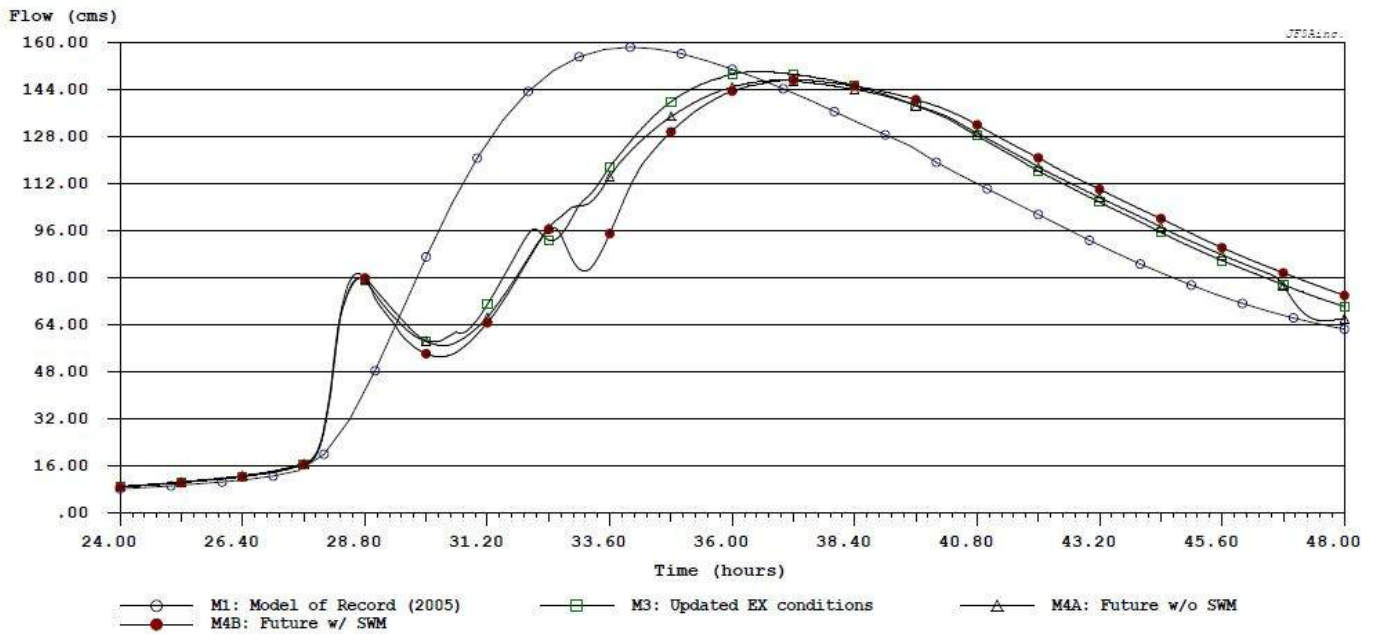
Scenario	Return Period					
	2-Year	5- Year	10-Year	25-Year	50-Year	100-Year
Model 1: 2005 Floodplain Study	49.16	72.08	89.96	115.84	136.46	158.42
Model 2: Stantec 2007 Reach One Analysis	50.78	73.65	n/a	113.97	n/a	157.69
Model 3: Updated Model 2 to current/ approved conditions	49.72	72.36	88.45	112.2	131.12	150.12
Model 4A: Model 3 with BCDC & others w/o SWM	49.58	71.17	86.35	105.27	128.42	147.10
Model 4B: Model 3 with BCDC & others with SWM	49.70	71.54	86.85	104.96	128.45	147.28

From Table 5 it is seen that the peak flows on the Jock River at the confluence with the Rideau River are generally at their lowest without SWM controls in place, and that either implementing or not implementing SWM controls for future developments results in peak flows at this location to be less than existing conditions.

Discussion

Although not initially obvious, the reason that future urban developments within Reach One of the Jock River are decreasing peak flows on the Jock River is because developing land not only affects the peak of the hydrograph but also the overall shape. Figure A below provides a comparison of the simulated hydrographs at the Jock River's confluence with the Rideau River from the various model scenarios. During any rainfall event, the runoff from the existing and future developments within Reach One will have already peaked and decayed before the peak flows arrive at this location from the upstream drainage area. For the 100-Year SCS storm, the peak from the development in Reach One can be seen in the figure below at around 28 hours, while the peak flow on the Jock River from the upstream drainage areas occurs at around 36-37 hours, this is approximately a 9-hour difference in timing. As such, implementing SWM measures for developments in the lower portions of the Jock River will decrease peak flows from the development, but would also prolong the period of time during which they discharge into the Jock River, thus coinciding with flows from the greater Jock River, ultimately resulting in potential increases in peak flows on the Jock River. This is seen in the figure below with the future condition with SWM controls (Model 4B - Red Circles) having a higher flow in the tail than future conditions without SWM controls (Model 4A – Black Triangles). Note that the difference between Model 1 and all other scenarios is simply due to further discretization of subcatchments within Reach One.

Figure A: Comparison of simulated 100 yr Jock River hydrographs at the confluence with the Rideau River



Hydrograph Statistics:

Legend	Filename & Comment	Time Step (min)	Drainage Area (ha)	Peak Flow (cms)	Time to Peak (hrs)	Runoff Volume (mm)	Runoff Volume (cu.m)	Duration of flow (hrs)	Average flow (cms)
○	N1_0100 : M1: Model of Record (2005)	30.00	55659.00	158.420	34.000	14.52	8.082E+06	24.000	93.538
□	SN_N1_0100 : M3: Updated EX conditions	1.00	55579.20	150.120	36.533	14.24	7.914E+06	24.000	91.603
△	SN_N1_0100 : M4A: Future w/o SWM	1.00	55579.20	147.102	36.917	14.12	7.848E+06	24.000	90.831
●	SN_N1_0100 : M4B: Future w/ SWM	1.00	55579.19	147.276	37.250	14.03	7.798E+06	24.000	90.252

Conclusion

The hydrologic model developed as a part of the Jock River Reach One Subwatershed Study (Stantec 2007) has been updated to provide additional refinements in the lower reaches of the Jock River (downstream of Highway 416) and assumes the development of lands that were previously not considered in the 2007 analysis (e.g. Barrhaven Conservancy). Future development condition models were created with and without SWM controls assumed, and the peak flows extracted from these models at key locations along the lower Jock River. From this analysis, it was found that with these additional developments in the lower Jock River peak flows are generally less than existing conditions without SWM controls in place. Implementing SWM controls for these developments has also been found to generally decrease peak flows on the Jock River, but not at all locations and not to the same degree as without SWM controls. Ultimately these findings are consistent with the fundamental conclusions drawn in Stantec's 2007 Jock River Reach One study, which initially determined that for future developments within Reach One of the Jock River "No quantity control storage is required for flood control purposes as the hydrograph from the subwatershed will peak before the upstream peak in the Jock River" and that "No erosion control storage is required to maintain the pre-development in-stream erosion condition". Based on the results of the updated analysis outlined in this memo, it can confirm that the fundamental conclusions drawn in Stantec's 2007 for developments in reach one of the Jock River remain valid.

Yours truly,

J.F Sabourin and Associates Inc.



Jonathon Burnett, P.Eng
Water Resources Engineer

cc: J.F Sabourin, M.Eng, P.Eng
Director of Water Resources Projects



Figures

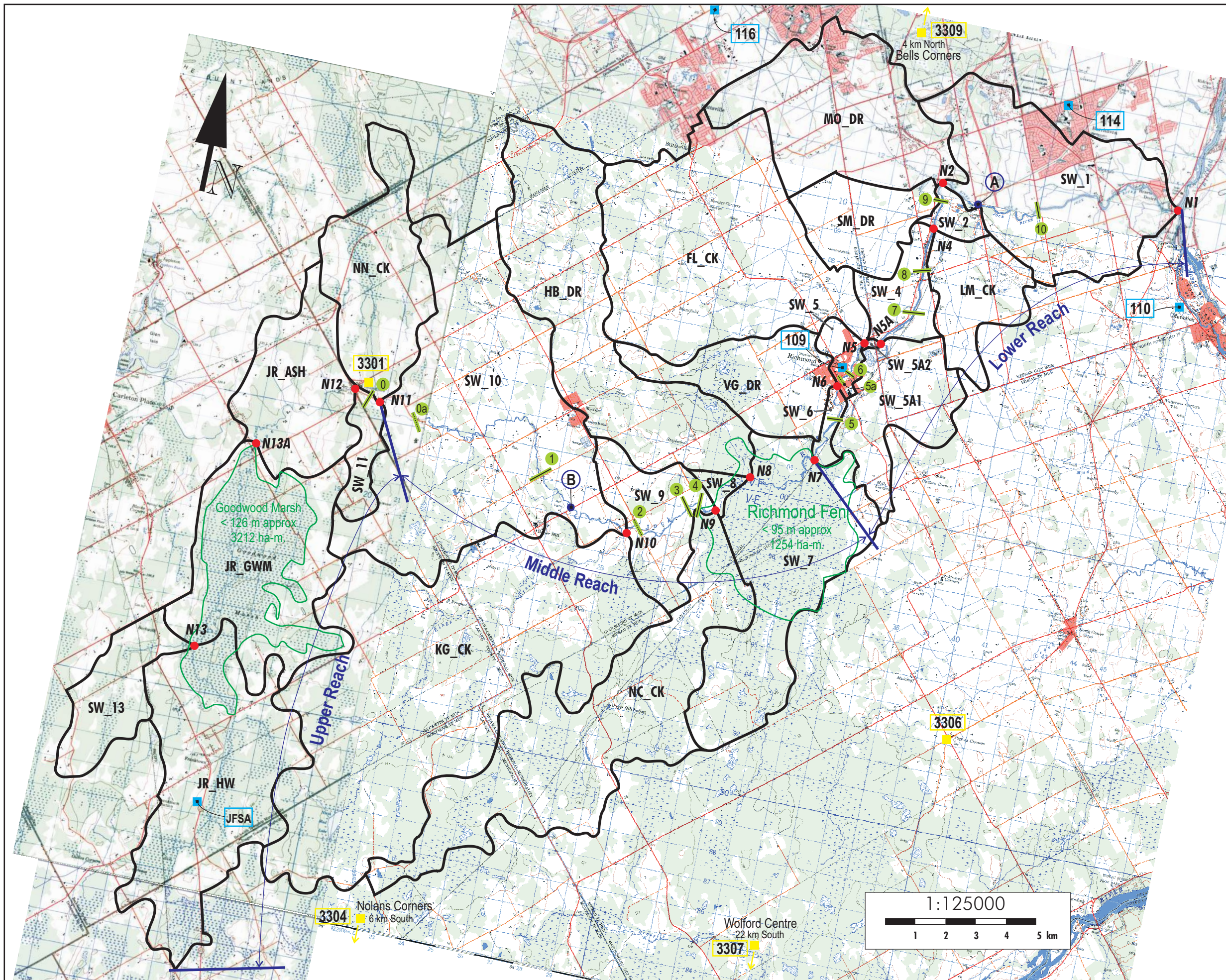
- Figure 1: Model 1 – Jock River Floodplain Model – JFSA, 2005
- Figure 2: Model 2 – Jock River Reach One Model – Stantec, 2007
- Figure 3: Model 3 – Jock River Reach One Model Update - JFSA, 2021
- Figure 4: Model 4A & 4B – Jock River Reach One Future Conditions - JFSA, 2021

Tables

- Table 1: Summer Peak Flows at Highway 416
- Table 2: Summer Peak Flows at Borrisokane Road.
- Table 3: Summer Peak Flows at Greenbank Road
- Table 4: Summer Peak Flows at Jockvale Road
- Table 5: Summer Peak Flows at Outlet of Jock River

Attachments

- Attachment A: Model 1 - SWMHYMO Input & Summary files
- Attachment B: Model 2 - SWMHYMO Input & Summary files
- Attachment C: Model 3 - SWMHYMO Input & Summary files
- Attachment D: Model 4A - SWMHYMO Input & Summary files
- Attachment E: Model 4B - SWMHYMO Input & Summary files
- Attachment F: Updated Subcatchment Schematics & Tables



- Legend:**
- Watershed
 - Bogs (Reservoir)
 - Nodes
 - Flow gauges
 - Rain gauges
 - Snow course stations
 - River Cross-Sections (based on topo. maps)
 - River Cross-Sections adjusted with field data
 - Reaches limits
- Flow gauges ID**
- 02LA007- Jock River near Richmond
 - Jock River at Franktown Rd
- Rain gauges ID**
- Richmond
 - Manotick
 - Barrhaven
 - Maple Grove
 - JFSA Inc, Temporary Rain Gauge 2003
- Snow course stations ID**
- Ashton
 - Nolans Corners
 - Pierces Corners
 - Bells Corners
 - Wolford Centre

Client:

Project:
Jock River Flood Plain Mapping Study

Title:
Watershed Delineation

J.F. Sabourin & Associates Inc.
WATER RESOURCES AND ENVIRONMENTAL CONSULTANTS
OTTAWA (613) 727-5199
GATINEAU (819) 243-6858

Figure 1 Ref. File: Base Map Jock River B.cdr



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Legend

- Existing SWM Facility
- Proposed Stormwater Facility
- Proposed Pond Outlet
- Jock River Tributary (Municipal Drain)
- Jock River Tributary (Non-Municipal Drain)
- Watershed Boundary
- 91.7 Regulatory Flood Level
- W/L 89.50 Normal Water Level
- Woodlot Limits
- Sub-drainage Area Limit
- Desire 24 ha
77 50% hrs
SCS Curve Number
- Application Plans Under Review
- 10 Year Flood Line
- 25 Year Flood Line
- 100 Year Flood Line

1	FINAL REPORT	BCB	N.C.	JUNE 2007
Revision		By	Appd.	YY.MM.DD
File Name:		Own.	Chgd.	Dgn.
Seal				YY.MM.DD

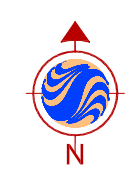
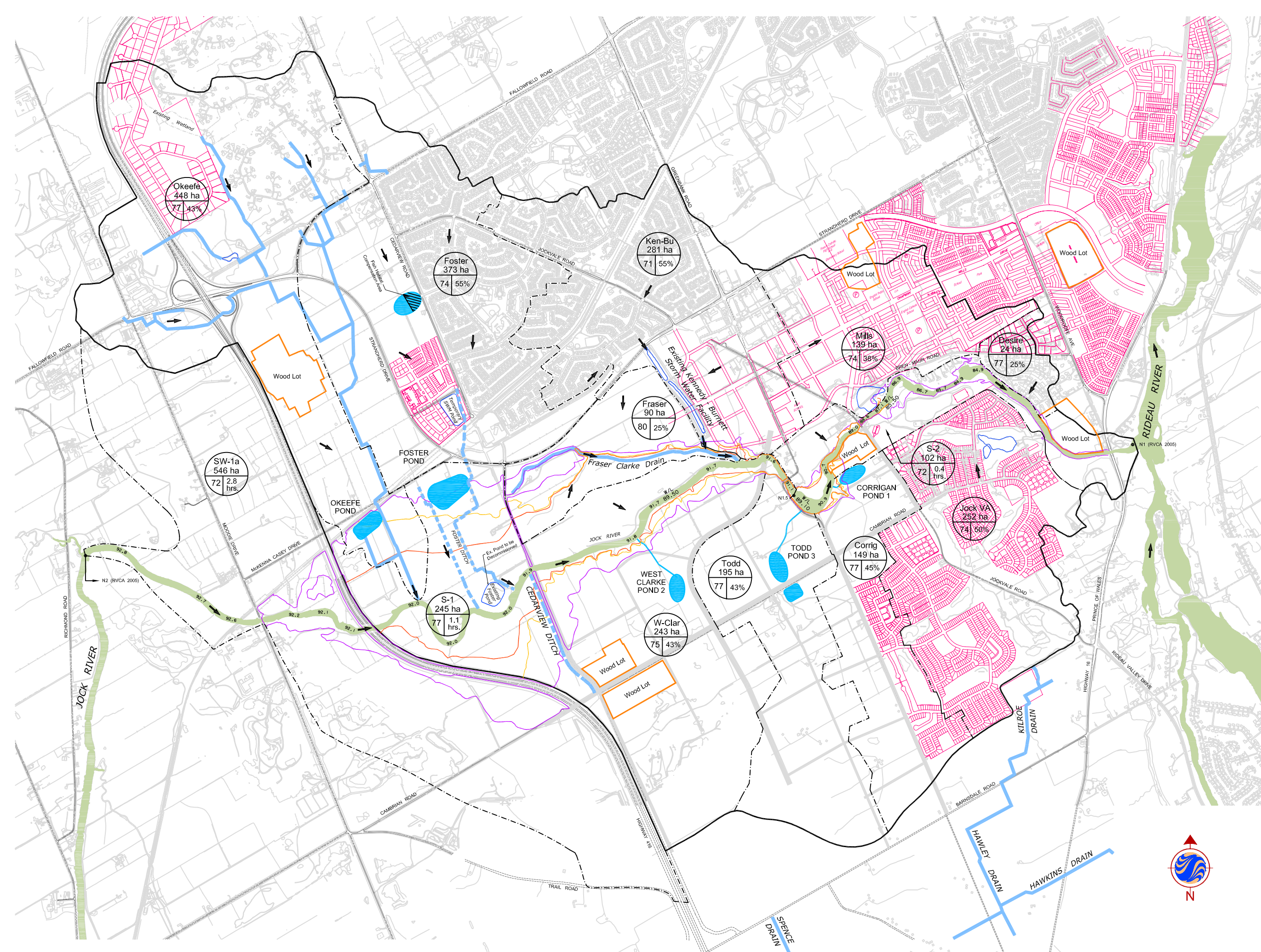
Client/Project

JOCK RIVER REACH ONE
 SUB-WATERSHED STUDY
 Ottawa ON Canada

Title
 PROPOSED CONDITIONS
 HYDROLOGIC MODEL
 DRAINAGE BOUNDARIES

Project No. 60400414 Scale 1:10,000
 Drawing No. _____ Sheet _____ Revision _____

Figure 2 1 of 1 1

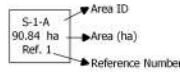




- Legend**
- Channel Cross Sections
 - S-1 Sub-catchments and Fraser Sub-catchments
 - S-1-A
 - S-1-B
 - S-1-D1
 - S-1-D2
 - S-1-D3
 - S-1-D4
 - S-1-D5
 - S-1-D6
 - S-1-D7
 - S-1-D8
 - S-1-FO-D1
 - S-1-FO-D2
 - S-1-FO-F-D
 - S-1-Okeefe
 - FRASER-DRN
 - FRASER-D
- Google Hybrid

File name:
20210304_S-1_Fraser_Schematic-Model4A.pdf

XS 3633 Cross Section at station 3633



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Ottawa, ON, K2S 1B9
(613) 836-3884
www.jfsa.com



PROJECT :
BCDC - Quantity Control Study

TITLE :
S-1 Sub-catchment and Fraser Clarke Sub-catchment Schematic

PROJECT NO. 1474-16

DRAWN: MM

DATE: Mar. 2021

Station	Channel	Area (ha)	Ref.	Flow (m³/s)	Velocity (m/s)	Depth (m)	Width (m)	Material	Notes
3633	FRASER-D	21.67	16	1.5	0.5	0.5	10	Gravel	Channel cross-section at station 3633
3634	S-1-D1	21.67	3	1.5	0.5	0.5	10	Gravel	Channel cross-section at station 3634
3635	S-1-D2	18.67	4	1.5	0.5	0.5	10	Gravel	Channel cross-section at station 3635
3636	S-1-D3	6.79	5	1.5	0.5	0.5	10	Gravel	Channel cross-section at station 3636
3637	S-1-D4	3.28	6	1.5	0.5	0.5	10	Gravel	Channel cross-section at station 3637
3638	S-1-D5	12.84	7	1.5	0.5	0.5	10	Gravel	Channel cross-section at station 3638
3639	S-1-D6	1.75	8	1.5	0.5	0.5	10	Gravel	Channel cross-section at station 3639
3640	S-1-D7	2.03	9	1.5	0.5	0.5	10	Gravel	Channel cross-section at station 3640
3641	S-1-D8	5.27	10	1.5	0.5	0.5	10	Gravel	Channel cross-section at station 3641
3642	S-1-FO-D1	5.11	11	1.5	0.5	0.5	10	Gravel	Channel cross-section at station 3642
3643	S-1-FO-D2	4.94	12	1.5	0.5	0.5	10	Gravel	Channel cross-section at station 3643
3644	S-1-FO-F-D	14.96	13	1.5	0.5	0.5	10	Gravel	Channel cross-section at station 3644
3645	S-1-Okeefe	44.93	14	1.5	0.5	0.5	10	Gravel	Channel cross-section at station 3645
3646	FRASER-DRN	13.65	15	1.5	0.5	0.5	10	Gravel	Channel cross-section at station 3646

SCALE : 0 500 1,000 1,500 m



Legend

- Channel Cross Sections
- S-1 Sub-catchments and Fraser Sub-catchments
- S-1-A
- S-1-B
- S-1-D1
- S-1-D2
- S-1-D3
- S-1-D4
- S-1-D5
- S-1-D6
- S-1-D7
- S-1-D8
- S-1-FO-D1
- S-1-FO-D2
- S-1-FO-F-D
- S-1-Okeefe
- FRASER-DRN
- FRASER-D

Google Hybrid

File name: 20210304_S-1_Fraser_Schematic-Model4B.pdf

XS 3633 Cross Section at station 3633

S-1-A	▼ Area ID
90.84 ha	► Area (ha)
Ref. 1	► Reference Number

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 (613) 836-3884
 www.jfsa.com

DSEL
 david schaeffer engineering ltd

PROJECT :
 BCDC - Quantity Control Study

TITLE :
 S-1 Sub-catchment and Fraser Clarke Sub-catchment Schematic

PROJECT NO. 1474-16

DRAWN: MM

DATE: Mar. 2021



Station	Channel	Area (ha)	Ref.	Notes
3633	S-1-Okeefe	44.93	14	
3633	S-1-FO-D1	5.11	11	
3633	S-1-FO-D2	4.94	12	
3633	S-1-FO-F-D	14.96	13	
3633	S-1-A	75.88	1	
3633	S-1-D2	18.67	4	
3633	S-1-D3	6.79	5	
3633	S-1-D4	3.28	6	
3633	S-1-D5	12.84	7	
3633	S-1-D6	1.75	8	
3633	S-1-D7	2.03	9	
3633	S-1-D8	5.27	10	
3633	S-1-D1	21.67	3	
3633	S-1-B	55.36	2	
3633	FRASER-D	21.61	16	
3633	FRASER-DRN	13.65	15	



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Ottawa, ON
Paris, ON
Gatineau, QC
Montréal, QC
Québec, QC

Attachment A

Model 1 – Jock River Floodplain Model

JFSA, 2005

SWMHYMO Input & Summary files

```

1  20    Metric units / ID numbers OFF
2  *#*****
3  *# SWMHYMO Ver:5.02/Jan 2001 <BETA> / INPUT DATA FILE
4  *#*****
5  *# Project Name: [Jock River]    Project Number: [411-02]
6  *# Date       : 06-06-2003
7  *# Modeller   : [JoF]
8  *# Company    : JFSAinc.
9  *# License #  : 2549237
10 *#*****
11 *# CALIBRATION OF SUMMER MODEL PARAMETERS
12 *# USING CONTINUOUS SIMULATIONS
13 *# Rainfall data from JFSA raingauge installed at site + other gauges by the City
14 *# Use data collected from May 1st to July 14, 2003
15 *
16 * Calibrated parameters for Summer 2003 data:  APII=50, APIK=0.85, CN=varies,
17 *                                               SK=0.01, InterEventTime=12,
18 *                                               GWResk=0.96, VHydCond=0.055
19 *
20 *# -----
21 *
22 *START          TZERO=[2003.0501], METOUT=[2], NSTORM=[1], NRUN=[001]
23 *              ["XAVG0315.STM"] average storm data a 15 minute time step
24 *              The above rainf file is an average of the JFSA gauge data
25 *              with the City of Ottawa rainfall data collected during
26 *              the same period.
27 *% 2 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
28 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[2]
29 *%              ["C24SC002.stm"] <--storm filename, one per line for NSTORM time
30 *%-----|-----|
31 *%-----|-----|
32 READ STORM     STORM_FILENAME=["storm.001"]
33 *%-----|-----|
34 MODIFY STORM   ICASEms=[1], NSHIFT=[96],
35 *              RedFACT=[1],
36 *%-----|-----|
37 COMPUTE API   APII=[50], APIK=[.85]/day
38 *%-----|-----|
39 *%-----|-----|
40 *#
41 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
42 *# of 1.32
43 *%-----|-----|
44 CONTINUOUS NASHYD NHYD=["JR_HW"], DT=[30]min, AREA=[3680] (ha),
45 *              DWF=[0] (cms), CN/C=[64], IA=[2.5] (mm),
46 *              N=[3.0], TP=[7.13]hrs,
47 *              Continuous simulation parameters:
48 *              IaRECper=[4] (hrs),
49 *              SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
50 *              InterEventTime=[12] (hrs)
51 *              Baseflow simulation parameters:
52 *              BaseFlowOption=[1] ,
53 *              InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
54 *              VHydCond=[0.055] (mm/hr), END=-1
55 *%-----|-----|
56 *#
57 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
58 *# of 1.32
59 *%-----|-----|
60 CONTINUOUS NASHYD NHYD=["SW_13"], DT=[30]min, AREA=[971] (ha),
61 *              DWF=[0] (cms), CN/C=[61], IA=[2.5] (mm),
62 *              N=[3.0], TP=[3.76]hrs,
63 *              Continuous simulation parameters:
64 *              IaRECper=[4] (hrs),
65 *              SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
66 *              InterEventTime=[12] (hrs)

```

```

67 Baseflow simulation parameters:
68 BaseFlowOption=[1] ,
69 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
70 VHydCond=[0.055] (mm/hr), END=-1
71 *%-----|-----
72 *#
73 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
74 *# of 1.80
75 *%-----|-----
76 CONTINUOUS NASHYD NHYD=["JR_GWM"], DT=[30]min, AREA=[3074] (ha),
77 DWF=[0] (cms), CN/C=[55], IA=[2.5] (mm),
78 N=[3], TP=[11.33]hrs,
79 Continuous simulation parameters:
80 IaRECper=[4] (hrs),
81 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
82 InterEventTime=[12] (hrs)
83 Baseflow simulation parameters:
84 BaseFlowOption=[1] ,
85 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
86 VHydCond=[0.055] (mm/hr), END=-1
87 *%-----|-----
88 CONTINUOUS NASHYD NHYD=["JR_ASH"], DT=[30]min, AREA=[1781] (ha),
89 DWF=[0] (cms), CN/C=[72], IA=[2.5] (mm),
90 N=[3.0], TP=[3.91]hrs,
91 Continuous simulation parameters:
92 IaRECper=[4] (hrs),
93 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
94 InterEventTime=[12] (hrs)
95 Baseflow simulation parameters:
96 BaseFlowOption=[1] ,
97 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
98 VHydCond=[0.055] (mm/hr), END=-1
99 *%-----|-----
100 CONTINUOUS NASHYD NHYD=["SW_11"], DT=[30]min, AREA=[500] (ha),
101 DWF=[0] (cms), CN/C=[66], IA=[2.5] (mm),
102 N=[3.0], TP=[1.24]hrs,
103 Continuous simulation parameters:
104 IaRECper=[4] (hrs),
105 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
106 InterEventTime=[12] (hrs)
107 Baseflow simulation parameters:
108 BaseFlowOption=[1] ,
109 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
110 VHydCond=[0.055] (mm/hr), END=-1
111 *%-----|-----
112 *#
113 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
114 *# of 1.80
115 *%-----|-----
116 CONTINUOUS NASHYD NHYD=["NN_CK"], DT=[30]min, AREA=[1917] (ha),
117 DWF=[0] (cms), CN/C=[66], IA=[2.5] (mm),
118 N=[3.0], TP=[5.29]hrs,
119 Continuous simulation parameters:
120 IaRECper=[4] (hrs),
121 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
122 InterEventTime=[12] (hrs)
123 Baseflow simulation parameters:
124 BaseFlowOption=[1] ,
125 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
126 VHydCond=[0.055] (mm/hr), END=-1
127 *%-----|-----
128 *#
129 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
130 *# of 1.52
131 *%-----|-----
132 CONTINUOUS NASHYD NHYD=["SW_10"], DT=[30]min, AREA=[5666] (ha),

```

```

133 DWF=[0] (cms), CN/C=[72], IA=[2.5] (mm),
134 N=[3.0], TP=[8.00]hrs,
135 Continuous simulation parameters:
136 IaREcper=[4] (hrs),
137 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
138 InterEventTime=[12] (hrs)
139 Baseflow simulation parameters:
140 BaseFlowOption=[1] ,
141 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
142 VHydCond=[0.055] (mm/hr), END=-1
143 *%-----|-----
144 *#
145 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
146 *# of 1.75
147 *%-----|-----
148 CONTINUOUS NASHYD NHYD=["KG_CK"], DT=[30]min, AREA=[8376] (ha),
149 DWF=[0] (cms), CN/C=[66], IA=[2.5] (mm),
150 N=[3.0], TP=[11.66]hrs,
151 Continuous simulation parameters:
152 IaREcper=[4] (hrs),
153 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
154 InterEventTime=[12] (hrs)
155 Baseflow simulation parameters:
156 BaseFlowOption=[1] ,
157 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
158 VHydCond=[0.055] (mm/hr), END=-1
159 *%-----|-----
160 *#
161 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
162 *# of 1.68
163 *%-----|-----
164 CONTINUOUS NASHYD NHYD=["SW_9"], DT=[30]min, AREA=[1132] (ha),
165 DWF=[0] (cms), CN/C=[70], IA=[2.5] (mm),
166 N=[3.0], TP=[2.51]hrs,
167 Continuous simulation parameters:
168 IaREcper=[4] (hrs),
169 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
170 InterEventTime=[12] (hrs)
171 Baseflow simulation parameters:
172 BaseFlowOption=[1] ,
173 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
174 VHydCond=[0.055] (mm/hr), END=-1
175 *%-----|-----
176 *#
177 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
178 *# of 1.82
179 *%-----|-----
180 CONTINUOUS NASHYD NHYD=["NC_CK"], DT=[30]min, AREA=[4464] (ha),
181 DWF=[0] (cms), CN/C=[62], IA=[2.5] (mm),
182 N=[3.0], TP=[11.32]hrs,
183 Continuous simulation parameters:
184 IaREcper=[4] (hrs),
185 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
186 InterEventTime=[12] (hrs)
187 Baseflow simulation parameters:
188 BaseFlowOption=[1] ,
189 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
190 VHydCond=[0.055] (mm/hr), END=-1
191 *%-----|-----
192 *#
193 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
194 *# of 1.80
195 *%-----|-----
196 CONTINUOUS NASHYD NHYD=["SW_8"], DT=[30]min, AREA=[131] (ha),
197 DWF=[0] (cms), CN/C=[63], IA=[2.5] (mm),
198 N=[3.0], TP=[0.90]hrs,

```

```

199         Continuous simulation parameters:
200         IaREcper=[4] (hrs),
201         SMIN=[-1] (mm),  SMAX=[-1] (mm), SK=[0.010]/(mm),
202         InterEventTime=[12] (hrs)
203         Baseflow simulation parameters:
204         BaseFlowOption=[1] ,
205         InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
206         VHydCond=[0.055] (mm/hr),  END=-1
207     *%-----|-----
208     *#
209     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
210     *# of 1.65
211     *%-----|-----
212     CONTINUOUS NASHYD  NHYD=["HB_DR"], DT=[30]min, AREA=[3854] (ha),
213         DWF=[0] (cms),  CN/C=[66], IA=[2.5] (mm),
214         N=[3.0], TP=[8.42]hrs,
215         Continuous simulation parameters:
216         IaREcper=[4] (hrs),
217         SMIN=[-1] (mm),  SMAX=[-1] (mm), SK=[0.010]/(mm),
218         InterEventTime=[12] (hrs)
219         Baseflow simulation parameters:
220         BaseFlowOption=[1] ,
221         InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
222         VHydCond=[0.055] (mm/hr),  END=-1
223     *%-----|-----
224     *#
225     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
226     *# of 1.82
227     *%-----|-----
228     CONTINUOUS NASHYD  NHYD=["SW_7"], DT=[30]min, AREA=[3197] (ha),
229         DWF=[0] (cms),  CN/C=[57], IA=[2.5] (mm),
230         N=[3.0], TP=[6.65]hrs,
231         Continuous simulation parameters:
232         IaREcper=[4] (hrs),
233         SMIN=[-1] (mm),  SMAX=[-1] (mm), SK=[0.010]/(mm),
234         InterEventTime=[12] (hrs)
235         Baseflow simulation parameters:
236         BaseFlowOption=[1] ,
237         InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
238         VHydCond=[0.055] (mm/hr),  END=-1
239     *%-----|-----
240     *#
241     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
242     *# of 1.75
243     *%-----|-----
244     CONTINUOUS NASHYD  NHYD=["SW_6"], DT=[30]min, AREA=[165] (ha),
245         DWF=[0] (cms),  CN/C=[67], IA=[2.5] (mm),
246         N=[3.0], TP=[4.18]hrs,
247         Continuous simulation parameters:
248         IaREcper=[4] (hrs),
249         SMIN=[-1] (mm),  SMAX=[-1] (mm), SK=[0.010]/(mm),
250         InterEventTime=[12] (hrs)
251         Baseflow simulation parameters:
252         BaseFlowOption=[1] ,
253         InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
254         VHydCond=[0.055] (mm/hr),  END=-1
255     *%-----|-----
256     *#
257     *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
258     *# of 1.67
259     *%-----|-----
260     CONTINUOUS NASHYD  NHYD=["VG_DR"], DT=[30]min, AREA=[1332] (ha),
261         DWF=[0] (cms),  CN/C=[72], IA=[2.5] (mm),
262         N=[3.0], TP=[5.95]hrs,
263         Continuous simulation parameters:
264         IaREcper=[4] (hrs),

```

```

265 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
266 InterEventTime=[12] (hrs)
267 Baseflow simulation parameters:
268 BaseFlowOption=[1] ,
269 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
270 VHydCond=[0.055] (mm/hr), END=-1
271 *%-----|
272 CONTINUOUS NASHYD NHYD=["SW_5"], DT=[30]min, AREA=[224] (ha),
273 DWF=[0] (cms), CN/C=[77], IA=[2.5] (mm),
274 N=[3.0], TP=[0.75]hrs,
275 Continuous simulation parameters:
276 IaRECper=[4] (hrs),
277 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
278 InterEventTime=[12] (hrs)
279 Baseflow simulation parameters:
280 BaseFlowOption=[1] ,
281 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
282 VHydCond=[0.055] (mm/hr), END=-1
283 *%-----|
284 *#
285 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
286 *# of 1.20
287 *%-----|
288 CONTINUOUS NASHYD NHYD=["FL_CK"], DT=[30]min, AREA=[4945] (ha),
289 DWF=[0] (cms), CN/C=[74], IA=[2.5] (mm),
290 N=[3.0], TP=[4.45]hrs,
291 Continuous simulation parameters:
292 IaRECper=[4] (hrs),
293 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
294 InterEventTime=[12] (hrs)
295 Baseflow simulation parameters:
296 BaseFlowOption=[1] ,
297 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
298 VHydCond=[0.055] (mm/hr), END=-1
299 *%-----|
300 CONTINUOUS NASHYD NHYD=["SW_5A2"], DT=[30]min, AREA=[20] (ha),
301 DWF=[0] (cms), CN/C=[81], IA=[2.5] (mm),
302 N=[3.0], TP=[0.62]hrs,
303 Continuous simulation parameters:
304 IaRECper=[4] (hrs),
305 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
306 InterEventTime=[12] (hrs)
307 Baseflow simulation parameters:
308 BaseFlowOption=[1] ,
309 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
310 VHydCond=[0.055] (mm/hr), END=-1
311 *%-----|
312 *#
313 *# The Tp was modified according to a Peak Reduction factor (MTO-Chart B2-4)
314 *# of 1.61
315 *%-----|
316 CONTINUOUS NASHYD NHYD=["SW_5A1"], DT=[30]min, AREA=[1412] (ha),
317 DWF=[0] (cms), CN/C=[75], IA=[2.5] (mm),
318 N=[3.0], TP=[8.00]hrs,
319 Continuous simulation parameters:
320 IaRECper=[4] (hrs),
321 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
322 InterEventTime=[12] (hrs)
323 Baseflow simulation parameters:
324 BaseFlowOption=[1] ,
325 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
326 VHydCond=[0.055] (mm/hr), END=-1
327 *%-----|
328 CONTINUOUS NASHYD NHYD=["SW_4"], DT=[30]min, AREA=[585] (ha),
329 DWF=[0] (cms), CN/C=[81], IA=[2.5] (mm),
330 N=[3.0], TP=[1.75]hrs,

```

```

331 Continuous simulation parameters:
332 IaREcper=[4] (hrs),
333 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
334 InterEventTime=[12] (hrs)
335 Baseflow simulation parameters:
336 BaseFlowOption=[1] ,
337 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
338 VHydCond=[0.055] (mm/hr), END=-1
339 *%-----|
340 CONTINUOUS NASHYD NHYD=["LM_CK"], DT=[30]min, AREA=[1021] (ha),
341 DWF=[0] (cms), CN/C=[80], IA=[2.5] (mm),
342 N=[3.0], TP=[2.46]hrs,
343 Continuous simulation parameters:
344 IaREcper=[4] (hrs),
345 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
346 InterEventTime=[12] (hrs)
347 Baseflow simulation parameters:
348 BaseFlowOption=[1] ,
349 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
350 VHydCond=[0.055] (mm/hr), END=-1
351 *%-----|
352 CONTINUOUS NASHYD NHYD=["SW_2"], DT=[30]min, AREA=[177] (ha),
353 DWF=[0] (cms), CN/C=[77], IA=[2.5] (mm),
354 N=[3.0], TP=[0.75]hrs,
355 Continuous simulation parameters:
356 IaREcper=[4] (hrs),
357 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
358 InterEventTime=[12] (hrs)
359 Baseflow simulation parameters:
360 BaseFlowOption=[1] ,
361 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
362 VHydCond=[0.055] (mm/hr), END=-1
363 *%-----|
364 CONTINUOUS NASHYD NHYD=["SM_DR"], DT=[30]min, AREA=[1122] (ha),
365 DWF=[0] (cms), CN/C=[81], IA=[2.5] (mm),
366 N=[3.0], TP=[3.25]hrs,
367 Continuous simulation parameters:
368 IaREcper=[4] (hrs),
369 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
370 InterEventTime=[12] (hrs)
371 Baseflow simulation parameters:
372 BaseFlowOption=[1] ,
373 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
374 VHydCond=[0.055] (mm/hr), END=-1
375 *%-----|
376 CONTINUOUS NASHYD NHYD=["MO_DR"], DT=[30]min, AREA=[2737] (ha),
377 DWF=[0] (cms), CN/C=[76], IA=[2.5] (mm),
378 N=[3.0], TP=[3.03]hrs,
379 Continuous simulation parameters:
380 IaREcper=[4] (hrs),
381 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
382 InterEventTime=[12] (hrs)
383 Baseflow simulation parameters:
384 BaseFlowOption=[1] ,
385 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
386 VHydCond=[0.055] (mm/hr), END=-1
387 *%-----|
388 CONTINUOUS NASHYD NHYD=["SW_1"], DT=[30]min, AREA=[3176] (ha),
389 DWF=[0] (cms), CN/C=[78], IA=[2.5] (mm),
390 N=[3.0], TP=[3.56]hrs,
391 Continuous simulation parameters:
392 IaREcper=[4] (hrs),
393 SMIN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
394 InterEventTime=[12] (hrs)
395 Baseflow simulation parameters:
396 BaseFlowOption=[1] ,

```



```

397          InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
398          VHydCond=[0.055] (mm/hr),   END=-1
399  *%-----|-----
400  *#
401  *# Routing hydrographs
402  *#
403  *# Starting with the addition of Jock River Headwater and Subwatershed 13
404  *#
405  ADD HYD          NHYDsum=["S_N13"], NHYDs to add=["JR_HW"+"SW_13"]
406  *%-----|-----
407  *#
408  *# Sum of hydrographs from Node 13 routed to Node 13A
409  *# (Approximated cross-section - see cross-section 258)
410  *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
411  *#
412  ROUTE CHANNEL    NHYDout=["N13A"] ,NHYDin=["S_N13"],
413                      RDT=[30] (min),
414                      CHLGTH=[9074] (m),   CHSLOPE=[0.0220] (%),
415                      FPSLOPE=[0.0220] (%),
416                      SECNUM=[1.0],       NSEG=[1]
417                      ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
418                      ( DISTANCE (m), ELEVATION (m))=
419                      [-40, 132.5]
420                      [-30, 132]
421                      [-25, 131.5]
422                      [-13, 130]
423                      [-8, 127.00]
424                      [-7, 126.50]
425                      [-6, 126]
426                      [-5.5, 125.50]
427                      [0, 123.75]
428                      [4.5, 125.50]
429                      [6, 126]
430                      [7.5, 126.5]
431                      [9, 127]
432                      [10, 127.5]
433                      [11.5, 128.0]
434                      [15.5, 129.5]
435  *%-----|-----
436  *#
437  *# Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
438  *#
439  ADD HYD          NHYDsum=["SN13A"], NHYDs to add=["N13A"+"JR_GWM"]
440  *%-----|-----
441  *#
442  *# Insertion of a reservoir to simulate the effects of the Goodwood Marsh
443  *#
444  ROUTE RESERVOIR NHYDout=["RES_GM"] ,NHYDin=["SN13A"],
445                      RDT=[30] (min),
446                      TABLE of ( OUTFLOW-STORAGE ) values
447                      (cms) - (ha-m)
448                      [ 0.0 , 0.0 ]
449                      [1.991, 2.144 ]
450                      [2.693, 39.826 ]
451                      [3.509, 81.697 ]
452                      [4.578, 318.774 ]
453                      [5.647, 594.947 ]
454                      [7.109, 910.219 ]
455                      [8.616, 1264.589 ]
456                      [10.371, 1658.057 ]
457                      [12.402, 2090.622 ]
458                      [22.056, 3462.487 ]
459                      [ -1 , -1 ] (max twenty pts)
460                      NHYDovf=[" " ] ,
461  *%-----|-----
462  *#

```

```

463 SAVE HYD          NHYD=["RES_GM"], # OF PCYCLES=[-1], ICASEsh=[-1]
464                      HYD_FILENAME=["H_RESGM"]
465                      HYD_COMMENT=["Outflow from Res GM"]
466 *%-----|-----
467 *# Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
468 *# (Approximated cross-section - see cross-section 258)
469 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
470 ROUTE CHANNEL    NHYDout=["N12"] ,NHYDin=["RES_GM"] ,
471                      RDT=[30] (min),
472                      CHLGTH=[5926] (m),  CHSLOPE=[0.0759] (%),
473                      FPSLOPE=[0.0759] (%),
474                      SECNUM=[1.0],      NSEG=[1]
475                      ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
476                      ( DISTANCE (m), ELEVATION (m))=
477                        [-40, 132.5]
478                        [-30, 132]
479                        [-25, 131.5]
480                        [-13, 130]
481                        [-8, 127.00]
482                        [-7, 126.50]
483                        [-6, 126]
484                        [-5.5, 125.50]
485                        [0, 123.75]
486                        [4.5, 125.50]
487                        [6, 126]
488                        [7.5, 126.5]
489                        [9, 127]
490                        [10, 127.5]
491                        [11.5, 128.00]
492                        [15.5, 129.5]
493 *%-----|-----
494 *#
495 *# Addition of Subwatershed Jock River at Ashton to Node 12
496 *#
497 ADD HYD          NHYDsum=["S_N12"], NHYDs to add=["N12"+"JR_ASH"]
498 SAVE HYD          NHYD=["S_N12"], # OF PCYCLES=[-1], ICASEsh=[-1]
499                      HYD_FILENAME=["H_SN12"]
500                      HYD_COMMENT=["flow at S_N12 near Ashton"]
501 *%-----|-----
502 *#
503 *# Sum of hydrographs from Node 12 routed to Node 11
504 *# (Approximated cross-section - see cross-section 258)
505 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
506 ROUTE CHANNEL    NHYDout=["N11"] ,NHYDin=["S_N12"] ,
507                      RDT=[30] (min),
508                      CHLGTH=[972] (m),  CHSLOPE=[0.0514] (%),
509                      FPSLOPE=[0.0514] (%),
510                      SECNUM=[1.0],      NSEG=[1]
511                      ( SEGROUGH, SEGDIST (m))=[0.04,15.5] NSEG times
512                      ( DISTANCE (m), ELEVATION (m))=
513                        [-40, 132.5]
514                        [-30, 132]
515                        [-25, 131.5]
516                        [-13, 130]
517                        [-8, 127.00]
518                        [-7, 126.50]
519                        [-6, 126]
520                        [-5.5, 125.50]
521                        [0, 123.75]
522                        [4.5, 125.50]
523                        [6, 126]
524                        [7.5, 126.5]
525                        [9, 127]
526                        [10, 127.5]
527                        [11.5, 128.00]
528                        [15.5, 129.5]

```



```

595  *#
596  *# Addition of Subwatershed 10 to Node 10
597  *#
598  ADD HYD           NHYDsum=["S_N10"], NHYDs to add=["N10"+"SW_10"]
599  *%-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
600  SAVE HYD         NHYD=["S_N10"], # OF PCYCLES=[-1], ICASEsh=[-1]
601                   HYD_FILENAME=["H_SN10"]
602                   HYD_COMMENT=["flow at S_N10: N10 + SW_10"]
603  *%-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
604  *# Addition of Kings Creek to S_N10
605  *#
606  ADD HYD           NHYDsum=["S_N10A"], NHYDs to add=["S_N10"+"KG_CK"]
607  *%-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
608  *#
609  *# Sum of hydrographs from Node 10 routed to Node 9
610  *# Section 2
611  *#
612  ROUTE CHANNEL    NHYDout=["N9"] ,NHYDin=["S_N10A"] ,
613                   RDT=[30] (min),
614                   CHLGTH=[3982] (m),  CHSLOPE=[0.0753] (%),
615                                     FPSLOPE=[0.0753] (%),
616                   SECNUM=[1.0],      NSEG=[4]
617                   ( SEGROUGH, SEGDIST (m))=
618                     [0.04,-30.27
619                      0.05,-18.42
620                      -0.05,18.42
621                      0.04,131.58] NSEG times
622                   ( DISTANCE (m), ELEVATION (m))=
623                     [-446.74, 106.00]
624                     [-415.68, 105.50]
625                     [-285.40, 105.00]
626                     [-173.77, 104.50]
627                     [-144.95, 104.00]
628                     [-111.18, 103.50]
629                     [-94.06, 103.00]
630                     [-71.02, 102.50]
631                     [-30.27, 102.00]
632                     [-19.33, 100.00]
633                     [-18.42, 99.50]
634                     [18.42, 99.50]
635                     [20.77, 100.00]
636                     [27.93, 101.00]
637                     [52.29, 101.00]
638                     [68.80, 101.50]
639                     [79.66, 103.00]
640                     [91.50, 103.50]
641                     [131.58, 104.00]
642  *%-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
643  *#
644  *# Addition of Subwatershed 9 and Nichols Creek to Node 9
645  *#
646  ADD HYD           NHYDsum=["S_N9"], NHYDs to add=["N9"+"SW_9"+"NC_CK"]
647  *%-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
648  *#
649  *# Sum of hydrographs from Node 9 routed to Node 8
650  *# Section 3
651  *#
652  ROUTE CHANNEL    NHYDout=["N8"] ,NHYDin=["S_N9"] ,
653                   RDT=[30] (min),
654                   CHLGTH=[2269] (m),  CHSLOPE=[0.0882] (%),
655                                     FPSLOPE=[0.0882] (%),
656                   SECNUM=[1.0],      NSEG=[3]
657                   ( SEGROUGH, SEGDIST (m))=
658                     [0.1,-17.99
659                      -0.045,17.31
660                      0.1,456.58] NSEG times

```

```

661      ( DISTANCE (m), ELEVATION (m))=
662          [-201.19,100.50]
663          [-135.21, 100.00]
664          [-94.83, 99.50]
665          [-67.05, 99.00]
666          [-17.99, 98.50]
667          [-16.02, 98.00]
668          [-13.95, 97.50]
669          [13.95, 97.50]
670          [15.64, 98.00]
671          [17.31, 98.50]
672          [162.02, 98.50]
673          [172.89 ,99.00]
674          [314.38, 99.00]
675          [343.78, 99.50]
676          [365.67, 100.00]
677          [376.68, 100.00 ]
678          [393.11, 99.50]
679          [404.97, 99.50]
680          [431.70, 100.00]
681          [456.58, 100.50 ]
682  *%-----|-----
683  *#
684  *# Addition of Subwatershed 8 and Hobb's Drain to Node 8
685  *#
686  ADD HYD          NHYDsum=["S_N8"], NHYDs to add=["N8"+"SW_8"+"HB_DR"]
687  *%-----|-----
688  *#
689  *# Sum of hydrographs from Node 8 routed to Node 7
690  *# Section 4
691  *#
692  ROUTE CHANNEL   NHYDout=["N7"] ,NHYDin=["S_N8"],
693                    RDT=[30] (min) ,
694                    CHLGTH=[3750] (m),   CHSLOPE=[0.0533] (%),
695                                          FPSLOPE=[0.0533] (%),
696                    SECNUM=[1.0],       NSEG=[3]
697                    ( SEGROUGH, SEGDIST (m))=
698                      [0.12,-18.11
699                      -0.07,17.22
700                      0.12,590.05] NSEG times
701      ( DISTANCE (m), ELEVATION (m))=
702          [-433.21, 102.00]
703          [-425.34, 101.50]
704          [-377.56, 101.50]
705          [-366.23, 101.00]
706          [-202.60, 100.50]
707          [-96.25, 99.50]
708          [-68.36 99.00]
709          [-18.11, 98.50]
710          [-13.81, 97.50]
711          [13.81, 97.50]
712          [17.22, 98.50]
713          [161.95, 98.50]
714          [173.11, 99.00]
715          [314.05, 99.00]
716          [365.52, 100.00]
717          [404.70, 99.50]
718          [476.74, 100.50]
719          [502.31, 101.00]
720          [584.69, 101.00]
721          [585.79, 101.00]
722          [590.05, 102.00]
723  *%-----|-----
724  *#
725  *# Addition of Subwatershed 7 to Node 7
726  *#

```

```

727 ADD HYD          NHYDsum=["S_N7"], NHYDs to add=["N7"+"SW_7"]
728 *%-----|-----|
729 SAVE HYD         NHYD=["S_N7"], # OF PCYCLES=[-1], ICASEsh=[-1]
730                 HYD_FILENAME=["H_SN7"]
731                 HYD_COMMENT=["flow at S_N7: N7 + SW_7"]
732 *%-----|-----|
733 *# Insertion of a reservoir to simulate the effects of the Richmond Fen.
734 *# Storage area and volumes were estimated from available topo maps.
735 *# Release rate from fen was assumed to be controlled by the downstream
736 *# river cross-section for summer conditions. It is was assumed that for up to
737 *# 0.75 m of water, the main channel of the river provided the storage. Above
738 *# this depth, the wetland starts to signigicantly store water.
739 *#
740 ROUTE RESERVOIR  NHYDout=["RES_RF"] ,NHYDin=["S_N7"] ,
741                 RDT=[30] (min),
742                 TABLE of ( OUTFLOW-STORAGE ) values
743                     (cms) - (ha-m)
744                 TABLE of ( OUTFLOW-STORAGE ) values
745                     (cms) - (ha-m)
746                     [ 0.0 , 0.0 ]
747                     [0.9051, 2.40]
748                     [2.907, 4.13]
749                     [9.744, 9.18]
750                     [20.304, 14.96]
751                     [34.167, 310.21]
752                     [74.993, 605.46]
753                     [104.876, 900.71]
754                     [140.56, 2892.00]
755                     [225.00, 3615.63]
756                     [ -1 , -1 ] (max twenty pts)
757                 NHYDovf=[" " ] ,
758 *%-----|-----|
759 SAVE HYD         NHYD=["RES_RF"], # OF PCYCLES=[-1], ICASEsh=[-1]
760                 HYD_FILENAME=["H_ResRF"]
761                 HYD_COMMENT=["outflow of Richmond Fen"]
762 *%-----|-----|
763 *#
764 *# Sum of hydrographs from Node 7 routed to Node 6
765 *# Section 5
766 *#
767 ROUTE CHANNEL    NHYDout=["N6"] ,NHYDin=["RES_RF"] ,
768                 RDT=[30] (min),
769                 CHLGTH=[3056] (m), CHSLOPE=[0.0818] (%),
770                                     FPSLOPE=[0.0818] (%),
771                 SECNUM=[1.0], NSEG=[5]
772                 ( SEGROUGH, SEGDIST (m))=
773                     [0.025,-70.8
774                     0.1,-23.9
775                     -0.05,23.9
776                     0.06,39.8
777                     0.05,96.3] NSEG times
778                 ( DISTANCE (m), ELEVATION (m))=
779                     [-100.8, 97.00]
780                     [-70.8, 96.50]
781                     [-52.0, 96.00]
782                     [-35.1, 95.50]
783                     [-30.6, 95.00]
784                     [-23.9, 94.54]
785                     [23.9, 94.54]
786                     [39.8, 95.00]
787                     [50.4, 95.50]
788                     [93.5, 96.00]
789                     [94.9, 96.50]
790                     [96.3, 97.00]
791 *%-----|-----|
792 *#

```

```

793  *# Addition of Subwatershed 6 and Van Gaal Drain to Node 6
794  *#
795  ADD HYD              NHYDsum=["S_N6"], NHYDs to add=["N6"+"SW_6"+"VG_DR"]
796  *%-----|-----
797  *#
798  *# Sum of hydrographs from Node 6 routed to Node 5
799  *# Section 6
800  *#
801  ROUTE CHANNEL       NHYDout=["N5"] ,NHYDin=["S_N6"] ,
802                    RDT=[30] (min),
803                    CHLGTH=[1852] (m),  CHSLOPE=[0.0540] (%),
804                    FPSLOPE=[0.0540] (%),
805                    SECNUM=[1.0],      NSEG=[3]
806                    ( SEGROUGH, SEGDIST (m))=
807                    [0.035,-131.59
808                    -0.045,48.96
809                    0.1,239.04] NSEG times
810                    ( DISTANCE (m), ELEVATION (m))=
811                    [-686.30, 94.50]
812                    [-675.70, 94.00]
813                    [-492.52, 93.00]
814                    [-467.28, 94.00]
815                    [-131.59, 94.00]
816                    [-92.79, 92.50]
817                    [-18.06, 91.00]
818                    [18.06, 91.00]
819                    [43.47, 92.50]
820                    [48.96, 94.00]
821                    [177.43, 94.00]
822                    [239.04,94.50]
823  *%-----|-----
824  *#
825  *# Addition of Subwatershed 5 and Flowing Creek to Node 5
826  *#
827  ADD HYD              NHYDsum=["S_N5"], NHYDs to add=["N5"+"SW_5"+"FL_CK"]
828  *%-----|-----
829  *#
830  *# Sum of hydrographs from Node 5 routed to Node 5A
831  *# Section 7
832  *#
833  ROUTE CHANNEL       NHYDout=["N5A"] ,NHYDin=["S_N5"] ,
834                    RDT=[30] (min),
835                    CHLGTH=[556] (m),  CHSLOPE=[0.0900] (%),
836                    FPSLOPE=[0.0900] (%),
837                    SECNUM=[1.0],      NSEG=[4]
838                    ( SEGROUGH, SEGDIST (m))=
839                    [0.04,-41.5
840                    0.1,-14.0
841                    -0.045,14.0
842                    0.1,41.1] NSEG times
843                    ( DISTANCE (m), ELEVATION (m))=
844                    [-275.8, 93.00]
845                    [-248.6, 92.50]
846                    [-237.0, 92.00]
847                    [-219.3, 91.50]
848                    [-202.1, 91.50]
849                    [-186.0, 92.00]
850                    [-129.2, 92.00]
851                    [-117.6, 91.50]
852                    [-100.6, 91.00]
853                    [-41.5, 91.00]
854                    [-20.0, 91.00]
855                    [-14.0, 90.54]
856                    [14.0, 90.54]
857                    [15.3, 91.00]
858                    [17.3, 91.50]

```

```

859                                     [38.4, 92.00]
860                                     [39.8, 92.50]
861                                     [41.1, 93.00]
862 *%-----|-----
863 *#
864 *# Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A
865 *#
866 ADD HYD                NHYDsum=["S_N5A"], NHYDs to add=["N5A"+"SW_5A2"+"SW_5A1"]
867 *%-----|-----
868 *#
869 *# Sum of hydrographs from Node 5A routed to Node 4
870 *# Section 8
871 *#
872 ROUTE CHANNEL        NHYDout=["N4"] ,NHYDin=["S_N5A"] ,
873                          RDT=[30] (min),
874                          CHLGTH=[4630] (m),  CHSLOPE=[0.0432] (%),
875                          FPSLOPE=[0.0432] (%),
876                          SECNUM=[1.0],      NSEG=[3]
877                          ( SEGROUGH, SEGDIST (m))=
878                          [0.05,-28.2
879                          -0.035,28.2
880                          0.05,173.1] NSEG times
881                          ( DISTANCE (m), ELEVATION (m))=
882                                     [-38.9, 92.00]
883                                     [-35.8, 91.50]
884                                     [-33.3, 91.00]
885                                     [-28.2, 90.50]
886                                     [-15.0, 87.48]
887                                     [-5.0, 88.34]
888                                     [5.0, 86.20]
889                                     [15.0, 88.55]
890                                     [28.2, 90.50]
891                                     [29.7, 91.00]
892                                     [46.5, 91.00]
893                                     [127.8, 91.00]
894                                     [148.7, 91.50]
895                                     [173.1, 92.00]
896 *%-----|-----
897 *#
898 *# Addition of Subwatershed 4 and Leamy Creek to Node 4
899 *#
900 ADD HYD                NHYDsum=["S_N4"], NHYDs to add=["N4"+"SW_4"+"LM_CK"]
901 SAVE HYD              NHYD=["S_N4"], # OF PCYCLES=[-1], ICASEsh=[1]
902                          HYD_COMMENT=["flow at S_N4"]
903 *%-----|-----
904 *#
905 *# Sum of hydrographs from Node 4 routed to Node 2
906 *# Section 9
907 *#
908 ROUTE CHANNEL        NHYDout=["N2"] ,NHYDin=["S_N4"] ,
909                          RDT=[30] (min),
910                          CHLGTH=[1667] (m),  CHSLOPE=[0.0600] (%),
911                          FPSLOPE=[0.0600] (%),
912                          SECNUM=[1.0],      NSEG=[4]
913                          ( SEGROUGH, SEGDIST (m))=
914                          [0.1,-28.0
915                          -0.04,28.4
916                          0.06,31.7
917                          0.04,80.2] NSEG times
918                          ( DISTANCE (m), ELEVATION (m))=
919                                     [-36.3, 92.00]
920                                     [-32.6, 91.50]
921                                     [-30.2, 91.00]
922                                     [-28.0, 90.45]
923                                     [-15.0, 87.48]
924                                     [-5.0, 88.34]

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925             [5.0, 86.20]
926             [15.0, 88.55]
927             [28.0, 90.45]
928             [28.4, 90.50]
929             [30.4, 91.00]
930             [31.7, 91.50]
931             [80.2, 92.00]
932 *%-----|-----
933 *#
934 *# Addition of Subwatershed 2 with Monohan Drain and Smith Drain to Node 2
935 *#
936 ADD HYD           NHYDsum=["S_N2"], NHYDs to add=["N2"+"SW_2"+"SM_DR"+"MO_DR"]
937 *%-----|-----
938 SAVE HYD         NHYD=["S_N2"], # OF PCYCLES=[-1], ICASEsh=[-1]
939                   HYD_FILENAME=["H_SN2"]
940                   HYD_COMMENT=["flow at S_N2 Jock River Gauge at Moodie Dr."]
941 *%-----|-----
942 *#
943 *# Sum of hydrographs from Node 2 routed to Node 1
944 *# Section 10
945 *#
946 ROUTE CHANNEL   NHYDout=["N1"] ,NHYDin=["S_N2"] ,
947                   RDТ=[30] (min),
948                   CHLGTH=[10046] (m),  CHSLOPE=[0.0498] (%),
949                                     FPSLOPE=[0.0498] (%),
950                   SECNUM=[1.0],        NSEG=[5]
951                   ( SEGROUGH, SEGDIST (m))=
952                     [0.04,-27.6
953                     0.06,-15.0
954                     -0.045,15.0
955                     0.06,25.4
956                     0.04,122.6] NSEG times
957                   ( DISTANCE (m), ELEVATION (m))=
958                                     [-87.0, 91.50]
959                                     [-32.4, 91.00]
960                                     [-27.6, 90.50]
961                                     [-25.0, 90.00]
962                                     [-22.9, 89.57]
963                                     [-15.0, 86.20]
964                                     [-5.0, 84.83]
965                                     [5.0, 84.83]
966                                     [15.0, 88.11]
967                                     [22.9, 89.57]
968                                     [25.4, 90.00]
969                                     [27.9, 90.50]
970                                     [38.0, 91.00]
971                                     [112.5, 91.00]
972                                     [114.3, 90.50]
973                                     [115.1, 90.26]
974                                     [116.3, 90.50]
975                                     [119.0, 91.00]
976                                     [121.0, 91.50]
977                                     [122.6, 92.00]
978 *%-----|-----
979 *#
980 *# Addition of Subwatershed 1 to Node 1
981 *#
982 ADD HYD           NHYDsum=["N1"], NHYDs to add=["N1"+"SW_1"]
983 SAVE HYD         NHYD=["N1"], # OF PCYCLES=[-1], ICASEsh=[1]
984                   HYD_COMMENT=["total outflow of Jock River"]
985 *%-----|-----
986 *#####
987 *% 5 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
988 START           TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[5]
989 *%               ["C24SC005.stm"] <--storm filename, one per line for NSTORM time
990 *%-----|-----

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991  *% 10 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
992  START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[10]
993  *%              ["C24SC010.stm"] <--storm filename, one per line for NSTORM time
994  *%-----|-----|
995  *% 25 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
996  START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[25]
997  *%              ["C24SC025.stm"] <--storm filename, one per line for NSTORM time
998  *%-----|-----|
999  *% 50 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
1000 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[50]
1001 *%              ["C24SC050.stm"] <--storm filename, one per line for NSTORM time
1002 *%-----|-----|
1003 *% 100 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
1004 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
1005 *%              ["C24SC100.stm"] <--storm filename, one per line for NSTORM time
1006 FINISH
1007
```


003755 + 30.0 02:SW10 5666.00 10.936 No_date 38:00 13.91 n/a .000
003765 ROUTE CHANL -> Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
003775 R0002:CD0043 Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
003785 SAVE HYD -> 30.0 01:SN 17589.00 19.098 No_date 38:30 12.16 n/a .000
003795 # name : H_SND
003800 # remark:flow at S_N0: N0 + SW10
003810 # Addition of Kings Creek to S_N0
003820 #
003830 R0002:CD0044 Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
003840 ADD HYD + 30.0 02:SN 17589.00 19.098 No_date 38:30 12.16 n/a .000
003850 + 30.0 02:SW 8376.00 10.656 No_date 39:30 11.98 n/a .000
003860 SUM 30.0 01:SN 17589.00 19.098 No_date 38:30 12.09 n/a .000
003870 #
003880 # Sum of hydrographs from Node 10 routed to Node 9
003890 # Section 2
003900 #
003910 R0002:CD0045 Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
003920 ROUTE CHANNEL -> 30.0 02:SN 25965.00 29.622 No_date 39:30 12.09 n/a .000
003930 [RFS=30.00] out > 30.0 01:SN 25965.00 29.622 No_date 39:30 12.09 n/a .000
003940 [L/S=3982. / 0751.040]
003950 [Vmax = 591.Dmax= 1.193]
003960 #
003970 # Addition of Subwatershed 9 and Nichols Creek to Node 9
003980 #
003990 R0002:CD0046 Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
004000 ADD HYD + 30.0 02:SN 25965.00 29.622 No_date 39:30 12.09 n/a .000
004010 + 30.0 02:SW 1132.00 4.365 No_date 30:30 13.32 n/a .000
004020 + 30.0 02:NC CK 4464.00 5.212 No_date 39:30 10.96 n/a .000
004030 SUM 30.0 01:SN 31561.00 35.488 No_date 39:30 11.98 n/a .000
004040 #
004050 # Sum of hydrographs from Node 9 routed to Node 8
004060 # Section 3
004070 #
004080 R0002:CD0047 Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
004090 ROUTE CHANNEL -> 30.0 01:SN 31561.00 33.301 No_date 40:00 11.98 n/a .000
004100 [RFS=30.00] out > 30.0 01:SN 31561.00 33.301 No_date 40:00 11.98 n/a .000
004110 [L/S=2269. / 0887.045]
004120 [Vmax = 420.Dmax = 1.290]
004130 #
004140 # Addition of Subwatershed 8 and Hubb's Drain to Node 8
004150 #
004160 R0002:CD0048 Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
004170 ADD HYD + 30.0 02:SN 31561.00 33.301 No_date 40:00 11.98 n/a .000
004180 + 30.0 02:SW 131.00 7.70 No_date 28:30 11.20 n/a .000
004190 + 30.0 02:MR 3854.00 6.083 No_date 38:30 11.85 n/a .000
004200 SUM 30.0 01:SN 35546.00 39.356 No_date 39:30 11.97 n/a .000
004210 #
004220 # Sum of hydrographs from Node 8 routed to Node 7
004230 # Section 4
004240 #
004250 R0002:CD0049 Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
004260 ROUTE CHANNEL -> 30.0 01:SN 35546.00 39.356 No_date 39:30 11.97 n/a .000
004270 [RFS=30.00] out > 30.0 01:SN 35546.00 39.356 No_date 44:00 11.97 n/a .000
004280 [L/S=420.Dmax = 1.290]
004290 [Vmax = 209.Dmax = 1.635]
004300 #
004310 # Addition of Subwatershed 7 to Node 7
004320 #
004330 R0002:CD0050 Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
004340 ADD HYD + 30.0 02:SN 35546.00 39.356 No_date 44:00 11.97 n/a .000
004350 + 30.0 02:SW 3197.00 4.557 No_date 36:30 9.83 n/a .000
004360 + 30.0 01:SN 38743.00 34.345 No_date 43:00 11.79 n/a .000
004370 R0002:CD0051 Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
004380 SAVE HYD -> 30.0 01:SN 38743.00 34.345 No_date 43:00 11.79 n/a .000
004390 # name : H_SND
004400 # remark:flow at S_N7: N7 + SW7
004410 # Insertion of a reservoir to simulate the effects of the Richmond Fen.
004420 # Storage area and volumes were estimated from available topmgs.
004430 # Release rate from fen was assumed to be controlled by the downstream
004440 # river cross-section for summer conditions. It is assumed that for up to
004450 # 0.75 m of water of the river provided the storage. Above
004460 # this depth, the wetland starts to significantly store water.
004470 #
004480 R0002:CD0052 Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
004490 ROUTE RESERVOIR -> 30.0 02:SN 38743.00 34.345 No_date 43:00 11.79 n/a .000
004500 + 30.0 02:RES RF 38743.00 23.075 No_date 54:30 11.79 n/a .000
004510 [MS=0.046E+7399E02]
004520 R0002:CD0053 Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
004530 SAVE HYD -> 30.0 01:RES RF 38743.00 23.075 No_date 54:30 11.79 n/a .000
004540 # name : H_ResRF
004550 # remark:outflow of Richmond Fen
004560 #
004570 # Sum of hydrographs from Node 7 routed to Node 6
004580 # Section 5
004590 #
004600 R0002:CD0054 Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
004610 ROUTE CHANNEL -> 30.0 02:RES RF 38743.00 23.075 No_date 54:30 11.79 n/a .000
004620 [RFS=30.00] out > 30.0 01:RES RF 38743.00 23.075 No_date 56:00 11.79 n/a .000
004630 [L/S=3056. / 0827.025]
004640 [Vmax = 431.Dmax = 0.951]
004650 #
004660 # Addition of Subwatershed 6 and Van Gal Drain to Node 6
004670 #
004680 R0002:CD0055 Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
004690 ADD HYD + 30.0 02:SN 40240.01 23.171 No_date 55:00 11.87 n/a .000
004700 + 30.0 02:SW 165.00 4.075 No_date 33:00 12.21 n/a .000
004710 + 30.0 02:MR 1132.00 2.083 No_date 38:30 11.87 n/a .000
004720 SUM 30.0 01:SN 40405.01 23.225 No_date 39:30 11.87 n/a .000
004730 #
004740 # Sum of hydrographs from Node 6 routed to Node 5
004750 # Section 6
004760 #
004770 R0002:CD0056 Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
004780 ROUTE CHANNEL -> 30.0 01:SN 40405.01 23.171 No_date 55:00 11.87 n/a .000
004790 [RFS=30.00] out > 30.0 01:SN 40405.01 23.171 No_date 55:00 11.87 n/a .000
004800 [L/S=1452. / 0547.035]
004810 [Vmax = 378.Dmax = 0.951]
004820 #
004830 # Addition of Subwatershed 5 and Flowing Creek to Node 5
004840 #
004850 R0002:CD0057 Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
004860 ADD HYD + 30.0 02:SN 40240.01 23.171 No_date 55:00 11.87 n/a .000
004870 + 30.0 02:SW 24.00 2.527 No_date 28:30 15.88 n/a .000
004880 + 30.0 02:MR CK 4945.00 14.54 No_date 39:30 17.76 n/a .000
004890 SUM 30.0 01:SN 52409.01 32.974 No_date 37:00 12.18 n/a .000
004900 #
004910 # Sum of hydrographs from Node 5 routed to Node 5A
004920 # Section 7
004930 #
004940 R0002:CD0058 Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
004950 ROUTE CHANNEL -> 30.0 01:SN 45409.01 32.974 No_date 37:00 12.18 n/a .000
004960 [RFS=30.00] out > 30.0 01:SN 45409.01 32.974 No_date 37:00 12.18 n/a .000
004970 [L/S=556. / 0947.050]
004980 [Vmax = 443.Dmax = 0.951]
004990 #
005000 # Addition of Subwatershed SA1 and Subwatershed SA2 to Node 5A
005010 #
005020 R0002:CD0059 Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
005030 ADD HYD + 30.0 02:SN 45409.01 32.974 No_date 37:00 12.18 n/a .000
005040 + 30.0 02:SW SA2 4612.00 3.007 No_date 38:00 15.19 n/a .000
005050 + 30.0 01:SN SA1 1484.01 35.939 No_date 37:00 12.27 n/a .000
005060 SUM 30.0 01:SN 46841.01 35.939 No_date 37:00 12.27 n/a .000
005070 #
005080 # Sum of hydrographs from Node 5A routed to Node 4
005090 # Section 8
005100 #
005110 R0002:CD0060 Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
005120 ROUTE CHANNEL -> 30.0 01:SN 46841.01 35.966 No_date 39:00 12.27 n/a .000
005130 [RFS=30.00] out > 30.0 01:SN 46841.01 35.966 No_date 39:00 12.27 n/a .000
005140 [L/S=4930. / 0471.035]
005150 [Vmax = 693.Dmax = 2.836]
005160 #
005170 # Addition of Subwatershed 4 and Leamy Creek to Node 4
005180 #
005190 R0002:CD0061 Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
005200 ADD HYD + 30.0 02:SN 46841.01 35.966 No_date 39:00 12.27 n/a .000
005210 + 30.0 02:SW SA 585.00 4.232 No_date 29:00 15.24 n/a .000
005220 + 30.0 02:MR CK 1021.00 5.667 No_date 30:30 17.36 n/a .000
005230 SUM 30.0 01:SN 48447.00 37.399 No_date 38:30 12.44 n/a .000
005240 R0002:CD0062 Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
005250 SAVE HYD -> 30.0 01:SN 48447.00 37.399 No_date 38:30 12.44 n/a .000
005260 # name : S_N002
005270 # remark:flow at S_N
005280 #
005290 # Sum of hydrographs from Node 4 routed to Node 2
005300 # Section 9
005310 #
005320 R0002:CD0063 Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
005330 ROUTE CHANNEL -> 30.0 01:SN 48447.00 37.399 No_date 39:00 12.44 n/a .000
005340 [RFS=30.00] out > 30.0 01:SN 48447.00 37.399 No_date 39:00 12.44 n/a .000
005350 [L/S=1467. / 0647.040]
005360 [Vmax = 714.Dmax = 2.841]
005370 #
005380 # Addition of Subwatershed 2 with Moshan Drain and Smith Drain to Node 2
005390 #
005400 R0002:CD0064 Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
005410 ADD HYD + 30.0 02:SN 48447.00 37.399 No_date 39:00 12.44 n/a .000
005420 + 30.0 02:SW 2 177.00 1.996 No_date 28:30 15.88 n/a .000
005430 + 30.0 02:MR DR 1122.00 5.257 No_date 31:30 17.76 n/a .000
005440 + 30.0 02:MR DR 2737.00 11.338 No_date 31:30 15.83 n/a .000
005450 SUM 30.0 01:SN 52483.00 35.676 No_date 38:30 12.73 n/a .000
005460 R0002:CD0065 Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
005470 SAVE HYD -> 30.0 01:SN 52483.00 35.676 No_date 33:30 12.73 n/a .000
005480 # name : H_SND
005490 # remark:flow at S_N2 Joek River Gauge at Middle Dr.
005500 #
005510 # Sum of hydrographs from Node 2 routed to Node 1
005520 # Section 10
005530 #
005540 R0002:CD0066 Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
005550 ROUTE CHANNEL -> 30.0 02:SN 52483.00 35.676 No_date 33:30 12.73 n/a .000
005560 [RFS=30.00] out > 30.0 01:SN 52483.00 35.676 No_date 39:00 12.73 n/a .000
005570 [L/S=1046. / 0507.040]
005580 [Vmax = 767.Dmax = 2.662]
005590 #
005600 # Addition of Subwatershed 1 to Node 1
005610 #

005620 R0002:CD0067 Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
005630 ADD HYD + 30.0 02:SN 52483.00 35.676 No_date 33:30 12.73 n/a .000
005640 + 30.0 02:SW 1 3176.00 12.490 No_date 32:00 16.23 n/a .000
005650 SUM 30.0 01:SN 52483.00 35.676 No_date 36:30 12.93 n/a .000
005660 R0002:CD0068 Dfm n-1D NND -> AREA-A-QPEAKm-TpeakDte-hh:mm--Rvmm R.C.--DFWcm
005670 SAVE HYD -> 30.0 01:SN 52483.00 35.676 No_date 36:30 12.93 n/a .000
005680 # name : N002
005690 # remark:total outflow of Joek River
005700 # *****
005710 ** END OF RUN : 4
005720 *****
005730 *****
005740 *****
005750 *****
005760 *****
005770 *****
005780 *****
005790 *****
005800 *****
005810 *****
005820 *****
005830 *****
005840 *****
005850 *****
005860 *****
005870 *****
005880 *****
005890 *****
005900 *****
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005970 *****
005980 *****
005990 *****
006000 *****
006010 *****
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006080 *****
006090 *****
006100 *****
006110 *****
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006150 *****
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006980 *****
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007000 *****
007010 *****
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007080 *****
007090 *****
007100 *****
007110 *****
007120 *****
007130 *****
007140 *****
007150 *****
007160 *****
007170 *****
007180 *****
007190 *****
007200 *****
007210 *****
007220 *****
007230 *****
007240 *****
007250 *****
007260 *****
007270 *****
007280 *****
007290 *****
007300 *****
007310 *****
007320 *****
007330 *****
007340 *****
007350 *****
007360 *****
007370 *****
007380 *****
007390 *****
007400 *****
007410 *****
007420 *****
007430 *****
007440 *****
007450 *****
007460 *****
007470 *****
007480 *****

012123 [IARC: 4.0; SMN: 57.05; SMM:380.32; SK: 010]
012124 [InterVtTime= 12.00]
012125 #
012126 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
012127 # of 1.32
012128 R010: C00066.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
012129 CONTI NKS NSHYD 30.01:SW13 971.00 4.293 No,date 32:30 18.81 294
012130 [Cm: 67.0; Nr: 3.00; Tpe: 3.76]
012131 [IARC: 4.0; SMN: 63.46; SMM:430.01; SK: 010]
012132 [InterVtTime= 12.00]
012133 #
012134 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
012135 # of 1.80
012136 R010: C00007.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
012137 CONTI NKS NSHYD 30.01:IR,OM 3074.00 5.604 No,date 39:30 16.19 250
012138 [Cm: 55.0; Nr: 3.00; Tpe: 1.73]
012139 [IARC: 4.0; SMN: 83.24; SMM:554.96; SK: 010]
012140 [InterVtTime= 12.00]
012141 R010: C00038.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
012142 CONTI NKS NSHYD 30.01:IR,ASH 1781.00 10.659 No,date 32:30 24.78 383
012143 [Cm: 72.0; Nr: 3.00; Tpe: 3.91]
012144 [IARC: 4.0; SMN: 39.75; SMM:264.99; SK: 010]
012145 [InterVtTime= 12.00]
012146 R010: C00009.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
012147 CONTI NKS NSHYD 30.01:SW11 500.00 5.516 No,date 29:00 21.17 327
012148 [Cm: 67.0; Nr: 3.00; Tpe: 4.42]
012149 [IARC: 4.0; SMN: 52.62; SMM:350.79; SK: 010]
012150 [InterVtTime= 12.00]
012151 #
012152 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
012153 # of 1.80
012154 R010: C00010.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
012155 CONTI NKS NSHYD 30.01:SN,CK 1917.00 7.737 No,date 34:00 21.17 327
012156 [Cm: 66.0; Nr: 3.00; Tpe: 5.29]
012157 [IARC: 4.0; SMN: 43.44; SMM:350.79; SK: 010]
012158 [InterVtTime= 12.00]
012159 #
012160 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
012161 # of 1.52
012162 R010: C00011.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
012163 CONTI NKS NSHYD 30.01:SW10 5666.00 20.651 No,date 37:30 24.78 383
012164 [Cm: 72.0; Nr: 3.00; Tpe: 3.91]
012165 [IARC: 4.0; SMN: 39.75; SMM:264.99; SK: 010]
012166 [InterVtTime= 12.00]
012167 #
012168 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
012169 # of 1.75
012170 R010: C00012.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
012171 CONTI NKS NSHYD 30.01:NE,CK 8376.00 19.522 No,date 39:30 21.17 327
012172 [Cm: 66.0; Nr: 3.00; Tpe: 4.42]
012173 [IARC: 4.0; SMN: 52.62; SMM:350.79; SK: 010]
012174 [InterVtTime= 12.00]
012175 #
012176 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
012177 # of 1.68
012178 R010: C00013.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
012179 CONTI NKS NSHYD 30.01:NE,CK 8376.00 8.783 No,date 30:30 23.71 366
012180 [Cm: 70.0; Nr: 3.00; Tpe: 2.51]
012181 [IARC: 4.0; SMN: 43.44; SMM:287.10; SK: 010]
012182 [InterVtTime= 12.00]
012183 #
012184 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
012185 # of 1.82
012186 R010: C00014.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
012187 CONTI NKS NSHYD 30.01:NE,CK 4464.00 9.718 No,date 39:30 19.27 298
012188 [Cm: 67.0; Nr: 3.00; Tpe: 4.42]
012189 [IARC: 4.0; SMN: 61.90; SMM:412.66; SK: 010]
012190 [InterVtTime= 12.00]
012191 #
012192 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
012193 # of 1.80
012194 R010: C00015.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
012195 CONTI NKS NSHYD 30.01:NE,CK 131.00 1.610 No,date 28:30 19.73 305
012196 [Cm: 63.0; Nr: 3.00; Tpe: 3.76]
012197 [IARC: 4.0; SMN: 59.42; SMM:396.11; SK: 010]
012198 [InterVtTime= 12.00]
012199 #
012200 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
012201 # of 1.65
012202 R010: C00016.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
012203 CONTI NKS NSHYD 30.01:HB,DR 3854.00 11.473 No,date 38:30 21.17 327
012204 [Cm: 66.0; Nr: 3.00; Tpe: 8.42]
012205 [IARC: 4.0; SMN: 43.44; SMM:350.79; SK: 010]
012206 [InterVtTime= 12.00]
012207 #
012208 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
012209 # of 1.82
012210 R010: C00017.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
012211 CONTI NKS NSHYD 30.01:SW7 3197.00 8.697 No,date 36:00 17.04 263
012212 [Cm: 57.0; Nr: 3.00; Tpe: 4.63]
012213 [IARC: 4.0; SMN: 76.32; SMM:508.81; SK: 010]
012214 [InterVtTime= 12.00]
012215 #
012216 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
012217 # of 1.75
012218 R010: C00018.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
012219 CONTI NKS NSHYD 30.01:NE,CK 165.00 804 No,date 33:00 21.66 335
012220 [Cm: 67.0; Nr: 3.00; Tpe: 4.18]
012221 [IARC: 4.0; SMN: 50.55; SMM:336.97; SK: 010]
012222 [InterVtTime= 12.00]
012223 #
012224 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
012225 # of 1.67
012226 R010: C00019.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
012227 CONTI NKS NSHYD 30.01:VG,IR 1332.00 5.936 No,date 35:00 24.78 383
012228 [Cm: 72.0; Nr: 3.00; Tpe: 5.95]
012229 [IARC: 4.0; SMN: 39.75; SMM:264.99; SK: 010]
012230 [InterVtTime= 12.00]
012231 R010: C00020.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
012232 CONTI NKS NSHYD 30.01:SW5 224.00 5.097 No,date 28:30 28.21 436
012233 [Cm: 72.0; Nr: 3.00; Tpe: 7.57]
012234 [IARC: 4.0; SMN: 31.15; SMM:207.66; SK: 010]
012235 [InterVtTime= 12.00]
012236 #
012237 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
012238 # of 1.20
012239 R010: C00021.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
012240 CONTI NKS NSHYD 30.01:FL,CK 4945.00 28.428 No,date 33:00 25.89 400
012241 [Cm: 74.0; Nr: 3.00; Tpe: 4.40]
012242 [IARC: 4.0; SMN: 36.67; SMM:244.49; SK: 010]
012243 [InterVtTime= 12.00]
012244 R010: C00022.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
012245 CONTI NKS NSHYD 30.01:SW,SA2 20.00 5.69 No,date 28:30 31.34 484
012246 [Cm: 81.0; Nr: 3.00; Tpe: 6.21]
012247 [IARC: 4.0; SMN: 25.21; SMM:168.09; SK: 010]
012248 [InterVtTime= 12.00]
012249 #
012250 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
012251 # of 1.61
012252 R010: C00023.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
012253 CONTI NKS NSHYD 30.01:SW,SA1 1412.00 5.651 No,date 37:30 27.03 418
012254 [Cm: 75.0; Nr: 3.00; Tpe: 8.00]
012255 [IARC: 4.0; SMN: 35.81; SMM:225.43; SK: 010]
012256 [InterVtTime= 12.00]
012257 R010: C00024.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
012258 CONTI NKS NSHYD 30.01:SW,4 585.00 8.289 No,date 29:30 31.34 484
012259 [Cm: 81.0; Nr: 3.00; Tpe: 7.57]
012260 [IARC: 4.0; SMN: 31.15; SMM:207.66; SK: 010]
012261 [InterVtTime= 12.00]
012262 R010: C00025.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
012263 CONTI NKS NSHYD 30.01:LM,CK 1021.00 11.041 No,date 30:30 30.69 474
012264 [Cm: 80.0; Nr: 3.00; Tpe: 2.46]
012265 [IARC: 4.0; SMN: 26.32; SMM:175.50; SK: 010]
012266 [InterVtTime= 12.00]
012267 R010: C00026.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
012268 CONTI NKS NSHYD 30.01:SW,2 177.00 4.027 No,date 28:30 28.21 436
012269 [IARC: 4.0; SMN: 31.15; SMM:207.66; SK: 010]
012270 [InterVtTime= 12.00]
012271 R010: C00027.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
012272 CONTI NKS NSHYD 30.01:SM,DR 1122.00 10.121 No,date 31:30 31.34 484
012273 [Cm: 81.0; Nr: 3.00; Tpe: 4.42]
012274 [IARC: 4.0; SMN: 25.21; SMM:168.09; SK: 010]
012275 [InterVtTime= 12.00]
012276 #
012277 R010: C00028.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
012278 CONTI NKS NSHYD 30.01:MD,DR 2737.00 22.263 No,date 31:30 27.61 427
012279 [Cm: 76.0; Nr: 3.00; Tpe: 3.21]
012280 [IARC: 4.0; SMN: 32.46; SMM:216.39; SK: 010]
012281 [InterVtTime= 12.00]
012282 R010: C00029.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
012283 CONTI NKS NSHYD 30.01:SW,1 3176.00 24.273 No,date 32:00 28.81 445
012284 [Cm: 78.0; Nr: 3.00; Tpe: 3.56]
012285 [IARC: 4.0; SMN: 29.88; SMM:199.22; SK: 010]
012286 [InterVtTime= 12.00]
012287 #
012288 # Routing hydrographs
012289 #
012290 # Starting with the addition of Jock River Headwater and Subwatershed 13
012291 # (Approximated cross-section)
012292 R010: C00030.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
012293 ADD HYD + 30.02:IR,OM 3880.00 11.582 No,date 36:30 20.20 n/a 000
012294 + 30.02:SW13 971.00 4.293 No,date 32:30 18.81 n/a 000
012295 SLM 30.01:SN,3 4651.00 14.791 No,date 35:00 19.91 n/a 000
012296 #
012297 # Sum of hydrographs from Node 13 routed to Node 13A
012298 # (Approximated cross-section)
012299 # Use n=0.04 for summer conditions and n=0.025 for spring conditions
013000 #
013001 R010: C00031.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
013002 ROUTE CHANNEL > 30.02:SN,3 4651.00 14.791 No,date 35:00 19.91 n/a 000
013003 [RFD=30.00] out c. 30.01:SN,3 4651.00 11.868 No,date 39:30 19.91 n/a 000
013004 [L/S/n= 9074 / 0.027/0.040]
013005 [Vmax= 305.Dmax= 3. n/a 000]
013006 #
013007 # Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
013008 #
013009 R010: C00032.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm

013105 ADD HYD + 30.02:SN,3A 4651.00 11.868 No,date 39:30 19.91 n/a 000
013106 + 30.02:IR,OM 3074.00 5.604 No,date 39:30 16.19 n/a 000
013107 SLM 30.01:SN,3A 7725.00 17.472 No,date 39:30 18.43 n/a 000
013108 #
013109 # Insertion of a reservoir to simulate the effects of the Goodwood Marsh
013110 #
013111 R010: C00033.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
013112 ROUTE CHANNEL > 30.02:SN,3A 7725.00 17.472 No,date 39:30 18.43 n/a 000
013113 [RFD=30.00] out c. 30.01:RES,GM 7725.00 3.517 No,date 59:00 18.43 n/a 000
013114 [MStoked= 8337E02 mb]
013115 #
013116 R010: C00034.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
013117 SLM 30.01:RES,GM 7725.00 3.517 No,date 59:00 18.43 n/a 000
013118 #
013119 # Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
013120 # (Approximated cross-section - see cross-section 258)
013121 # Use n=0.04 for summer conditions and n=0.025 for spring conditions
013122 R010: C00035.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
013123 ROUTE CHANNEL > 30.02:RES,GM 7725.00 3.517 No,date 59:00 18.43 n/a 000
013124 [RFD=30.00] out c. 30.02:RES,GM 7725.00 3.517 No,date 63:00 18.43 n/a 000
013125 [L/S/n= 9296 / 0.076/0.040]
013126 [Vmax= 546.Dmax= 1.498]
013127 #
013128 # Addition of Subwatershed Jock River at Ashton to Node 12
013129 #
013130 R010: C00036.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
013131 ADD HYD + 30.02:SN,2 1725.00 3.511 No,date 63:00 18.43 n/a 000
013132 + 30.02:IR,ASH 1781.00 10.659 No,date 32:30 24.78 n/a 000
013133 SLM 30.01:SN,2 9506.00 12.656 No,date 32:30 19.62 n/a 000
013134 R010: C00037.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
013135 SLM 30.01:SN,2 9506.00 12.656 No,date 32:30 19.62 n/a 000
013136 #
013137 # Sum of hydrographs from Node 12 routed to Node 11
013138 # (Approximated cross-section - see cross-section 258)
013139 # Use n=0.04 for summer conditions and n=0.025 for spring conditions
013140 R010: C00038.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
013141 ROUTE CHANNEL > 30.02:SN,2 9506.00 12.656 No,date 32:30 19.62 n/a 000
013142 [RFD=30.00] out c. 30.01:SN,2 9506.00 12.656 No,date 33:00 19.62 n/a 000
013143 [L/S/n= 972 / 0.047/0.040]
013144 [Vmax= 677.Dmax= 2.584]
013145 #
013146 # Addition of Subwatershed 11 and No Name Creek to Node 11
013147 #
013148 R010: C00040.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
013149 ADD HYD + 30.02:Dum,1 9506.00 12.493 No,date 33:00 19.62 n/a 000
013150 + 30.02:SW,11 500.00 5.516 No,date 29:00 21.17 n/a 000
013151 + 30.02:SN,CK 1917.00 7.737 No,date 34:00 21.17 n/a 000
013152 SLM 30.01:SN,1 11923.00 14.261 No,date 33:00 19.93 n/a 000
013153 #
013154 # Sum of hydrographs from Node 11 routed to Node 10
013155 # Section 1
013156 R010: C00041.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
013157 ROUTE CHANNEL > 30.02:SN,1 11923.00 14.261 No,date 33:00 19.93 n/a 000
013158 [RFD=30.00] out c. 30.01:SN,1 11923.00 21.409 No,date 39:30 19.93 n/a 000
013159 [L/S/n= 972 / 0.047/0.040]
013160 [Vmax= 677.Dmax= 2.584]
013161 #
013162 # Addition of Subwatershed 10 to Node 10
013163 #
013164 R010: C00042.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
013165 ADD HYD + 30.02:Dum,1 9506.00 12.493 No,date 33:00 19.62 n/a 000
013166 + 30.02:SW,11 500.00 5.516 No,date 29:00 21.17 n/a 000
013167 + 30.02:SN,CK 1917.00 7.737 No,date 34:00 21.17 n/a 000
013168 SLM 30.01:SN,1 11923.00 14.261 No,date 33:00 19.93 n/a 000
013169 #
013170 # Sum of hydrographs from Node 10 routed to Node 9
013171 # Section 1
013172 R010: C00043.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
013173 ROUTE CHANNEL > 30.02:SN,0 17589.00 35.073 No,date 38:30 21.50 n/a 000
013174 [RFD=30.00] out c. 30.01:SN,0 17589.00 35.073 No,date 38:30 21.50 n/a 000
013175 [L/S/n= 927 / 0.051/0.040]
013176 [Vmax= 451.Dmax= 1.206]
013177 #
013178 # Addition of Subwatershed 9 to Node 9
013179 #
013180 R010: C00044.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
013181 ADD HYD + 30.02:SN,0 17589.00 35.073 No,date 38:30 21.50 n/a 000
013182 + 30.02:SW,10 5666.00 20.651 No,date 37:30 24.78 n/a 000
013183 SLM 30.01:SN,0 17589.00 35.073 No,date 38:30 21.50 n/a 000
013184 #
013185 # Sum of hydrographs from Node 9 routed to Node 8
013186 #
013187 R010: C00045.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
013188 ADD HYD + 30.02:SN,0 17589.00 35.073 No,date 38:30 21.50 n/a 000
013189 + 30.02:SW,9 1132.00 8.783 No,date 38:30 23.71 n/a 000
013190 + 30.02:SN,CK 4464.00 9.718 No,date 39:30 19.27 n/a 000
013191 SLM 30.01:SN,0 31561.00 64.367 No,date 39:30 21.17 n/a 000
013192 #
013193 # Sum of hydrographs from Node 8 routed to Node 7
013194 # Section 3
013195 R010: C00046.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
013196 ADD HYD + 30.02:SN,0 17589.00 35.073 No,date 38:30 21.50 n/a 000
013197 + 30.02:SW,9 1132.00 8.783 No,date 38:30 23.71 n/a 000
013198 + 30.02:SN,CK 4464.00 9.718 No,date 39:30 19.27 n/a 000
013199 SLM 30.01:SN,0 31561.00 64.367 No,date 39:30 21.17 n/a 000
013200 #
013201 # Addition of Subwatershed 8 and Hobb's Drain to Node 8
013202 #
013203 R010: C00048.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
013204 ADD HYD + 30.02:SN,0 17589.00 35.073 No,date 38:30 21.50 n/a 000
013205 + 30.02:SW,8 131.00 1.610 No,date 28:30 19.73 n/a 000
013206 + 30.02:HB,DR 3854.00 11.473 No,date 38:30 21.17 n/a 000
013207 SLM 30.01:SN,8 35548.00 71.021 No,date 38:30 21.17 n/a 000
013208 #
013209 # Sum of hydrographs from Node 8 routed to Node 7
013210 # Section 4
013211 R010: C00049.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
013212 ROUTE CHANNEL > 30.02:SN,8 35548.00 71.021 No,date 39:30 21.17 n/a 000
013213 [RFD=30.00] out c. 30.01:SN,8 35548.00 59.731 No,date 44:30 21.17 n/a 000
013214 [L/S/n= 3750 / 0.037/0.070]
013215 [Vmax= 216.Dmax= 1.966]
013216 #
013217 # Addition of Subwatershed 7 to Node 7
013218 #
013219 R010: C00050.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
013220 ADD HYD + 30.02:SN,7 38743.00 59.731 No,date 44:30 21.17 n/a 000
013221 + 30.02:SW,7 3197.00 8.697 No,date 36:00 17.04 n/a 000
013222 + 30.02:SN,CK 38743.00 64.039 No,date 44:00 20.83 n/a 000
013223 SLM 30.01:SN,7 38743.00 64.039 No,date 44:00 20.83 n/a 000
013224 #
013225 # Insertion of a reservoir to simulate the effects of the Richmond Fen
013226 # Storage area and volumes were estimated from available top maps.
013227 # Release rate for fen was assumed to be controlled by the downstream
013228 # river cross-section for summer conditions. It was assumed that for up to
013229 # 0.75 of water, the main channel of the river provided the storage. Above
013230 # this depth, the wetland starts to significantly store water.
013231 #
013232 R010: C00052.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
013233 ROUTE RESERVOIR > 30.02:SN,7 38743.00 64.039 No,date 44:00 20.83 n/a 000
013234 [RFD=30.00] out c. 30.01:RES,RF 38743.00 31.370 No,date 60:30 20.83 n/a 000
013235 [MStoked= 2507E03 mb]
013236 #
013237 R010: C00053.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
013238 SLM 30.01:RES,RF 38743.00 31.370 No,date 60:30 20.83 n/a 000
013239 #
013240 # Sum of hydrographs from Node 7 routed to Node 6
013241 # Section 5
013242 R010: C00054.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
013243 ROUTE CHANNEL > 30.02:RES,RF 38743.00 31.370 No,date 60:30 20.83 n/a 000
013244 [RFD=30.00] out c. 30.01:SN,6 38743.00 31.314 No,date 62:00 20.83 n/a 000
013245 [L/S/n= 3056 / 0.027/0.025]
013246 [Vmax= 475.Dmax= .953]
013247 #
013248 # Addition of Subwatershed 6 and Van Gal Drain to Node 6
013249 #
013250 R010: C00055.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
013251 ADD HYD + 30.02:SW,6 165.00 804 No,date 35:00 21.66 n/a 000
013252 + 30.02:VG,IR 1332.00 5.936 No,date 35:00 24.78 n/a 000
013253 SLM 30.01:SN,6 40240.00 31.366 No,date 61:00 20.96 n/a 000
013254 #
013255 # Sum of hydrographs from Node 6 routed to Node 5
013256 # Section 6
013257 R010: C00056.....DfIn-ID NND.....AREhA-QPEAGm-TpeakDte,hb,mm---RvmR,C---Dfwm
013258 ROUTE CHANNEL > 30.02:SN,6 40240.00 31.366 No,date 61:00 20.96 n/a 000
013259 [RFD=30.00] out c. 30.02:SN,6 40240.00 31.341 No,date 62:00 20.96 n/a 000
0132


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018173 # 30.0 02: NS,CK 1917.00 10.139 No.date 34.00 26.99 n/a .000
018174 SIM 30.0 02: S,N1 11923.00 27.440 No.date 33.00 25.40 n/a .000
018175 # Sum of hydrographs from Node 11 routed to Node 10
018176 # Section 1
018177 ROUTE2: C00041 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
018178 ROUTE CHANNEL > 30.0 02: S,N1 11923.00 27.440 No.date 33.00 25.40 n/a .000
018179 [RDR-30.00] out > 30.0 01: N1 11923.00 17.756 No.date 40.00 25.40 n/a .000
018180 [L/S=104028 / 1577.040]
018181 [Vmax =.463;Dmax=1.320]
018182 #
018183 # Addition of Subwatershed 10 to Node 10
018184 #
018185 ROUTE2: C00042 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
018186 ADD HYD + 30.0 02: NS,N1 31561.00 44.045 No.date 38.30 27.35 n/a .000
018187 + 30.0 02: SW,IO 5666.00 26.665 No.date 37.30 31.47 n/a .000
018188 SIM 30.0 01: S,N1 17589.00 34.045 No.date 38.30 27.35 n/a .000
018189 ROUTE2: C00043 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
018190 SAVE HYD 30.0 01: S,N1 17589.00 44.045 No.date 38.30 27.35 n/a .000
018191 frame :H,SND
018192 remark:flow at S_N1= SW+IO
018193 # Addition of Kings Creek to S_N1
018194 #
018195 ROUTE2: C00044 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
018196 ADD HYD + 30.0 02: NS,CK 8376.00 25.107 No.date 39.30 26.99 n/a .000
018197 SIM 30.0 01: S,N1 25965.00 68.824 No.date 39.30 27.24 n/a .000
018198 #
018199 # Sum of hydrographs from Node 10 routed to Node 9
019001 # Section 2
019002 #
019003 ROUTE2: C00045 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
019004 ROUTE CHANNEL > 30.0 02: S,N1 25965.00 68.824 No.date 39.30 27.24 n/a .000
019005 [RDR-30.00] out > 30.0 01: N1 25965.00 66.905 No.date 39.30 27.24 n/a .000
019006 [L/S=3982 / 0757.040]
019007 [Vmax =.713;Dmax=1.864]
019008 #
019009 # Addition of Subwatershed 9 and Nichols Creek to Node 9
019010 #
019011 ROUTE2: C00046 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
019012 ADD HYD + 30.0 02: SW,S 31561.00 11.274 No.date 30.30 30.15 n/a .000
019013 + 30.0 02: SW,S 1132.00 11.274 No.date 30.30 30.15 n/a .000
019014 + 30.0 02: NS,CK 4464.00 12.525 No.date 39.30 24.58 n/a .000
019015 SIM 30.0 01: S,N1 31561.00 82.190 No.date 39.30 26.97 n/a .000
019016 #
019017 # Sum of hydrographs from Node 9 routed to Node 8
019018 # Section 3
019019 #
019020 ROUTE2: C00047 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
019021 ROUTE CHANNEL > 30.0 02: S,N1 31561.00 82.190 No.date 39.30 26.97 n/a .000
019022 [RDR-30.00] out > 30.0 01: N1 31561.00 78.196 No.date 40.00 26.97 n/a .000
019023 [L/S=2269 / 0887.045]
019024 [Vmax =.362;Dmax=1.727]
019025 #
019026 # Addition of Subwatershed 8 and Hobbs' Drain to Node 8
019027 #
019028 ROUTE2: C00048 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
019029 ADD HYD + 30.0 02: SW,S 31561.00 17.196 No.date 45.00 26.96 n/a .000
019030 + 30.0 02: SW,S 131.00 2.156 No.date 28.30 25.17 n/a .000
019031 + 30.0 02: NS,CK 38743.00 14.880 No.date 38.30 26.99 n/a .000
019032 SIM 30.0 01: S,N1 35546.00 91.271 No.date 39.30 26.96 n/a .000
019033 #
019034 # Sum of hydrographs from Node 8 routed to Node 7
019035 # Section 4
019036 #
019037 ROUTE2: C00049 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
019038 ROUTE CHANNEL > 30.0 02: S,N1 35546.00 91.271 No.date 39.30 26.96 n/a .000
019039 [RDR-30.00] out > 30.0 01: N1 35546.00 78.196 No.date 45.00 26.96 n/a .000
019040 [L/S=3750 / 0537.070]
019041 [Vmax =.225;Dmax=1.864]
019042 #
019043 # Addition of Subwatershed 7 to Node 7
019044 #
019045 ROUTE2: C00050 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
019046 ADD HYD + 30.0 02: SW,S 35546.00 28.196 No.date 45.00 26.96 n/a .000
019047 + 30.0 02: SW,S 3197.00 11.391 No.date 36.00 21.73 n/a .000
019048 SIM 30.0 01: S,N1 38743.00 84.011 No.date 44.00 26.53 n/a .000
019049 ROUTE2: C00051 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
019050 SAVE HYD 30.0 01: S,N1 38743.00 84.011 No.date 44.00 26.53 n/a .000
019051 frame :H,SNT
019052 remark:flow at S_N1= SW+IO
019053 # Insertion of a reservoir to simulate the effects of the Richmond Fen
019054 # Storage area and volumes were estimated from available top mps.
019055 # Release rate from fen assumed to be controlled by the downstream
019056 # river cross-section for summer conditions. It was assumed that for up
019057 # to 0.75 m of water, the main channel of the river provided the storage. Above
019058 # this depth, the wetland starts to significantly store water.
019059 #
019060 ROUTE2: C00052 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
019061 ROUTE RESERVOIR > 30.0 02: S,N1 38743.00 84.011 No.date 44.00 26.53 n/a .000
019062 [RDR-30.00] out > 30.0 01: RES,RF 38743.00 40.725 No.date 60.30 26.53 n/a .000
019063 [MSI=0.65;S=377E+03]
019064 ROUTE2: C00053 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
019065 SAVE HYD 30.0 01: S,N1 38743.00 40.725 No.date 60.30 26.53 n/a .000
019066 frame :H,RES,RF
019067 remark:outflow of Richmond Fen
019068 #
019069 # Sum of hydrographs from Node 7 routed to Node 6
019070 # Section 5
019071 #
019072 ROUTE2: C00054 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
019073 ROUTE CHANNEL > 30.0 02: RES,RF 38743.00 40.725 No.date 60.30 26.53 n/a .000
019074 [RDR-30.00] out > 30.0 01: N1 38743.00 40.549 No.date 61.30 26.53 n/a .000
019075 [L/S=3056 / 0827.025]
019076 [Vmax =.510;Dmax=1.101]
019077 #
019078 # Addition of Subwatershed 6 and Van Gaal Drain to Node 6
019079 #
019080 ROUTE2: C00055 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
019081 ADD HYD + 30.0 02: SW,S 38743.00 40.549 No.date 61.30 26.53 n/a .000
019082 + 30.0 02: SW,S 165.00 1.056 No.date 33.00 27.61 n/a .000
019083 + 30.0 02: NS,CK 1332.00 7.707 No.date 35.00 31.47 n/a .000
019084 SIM 30.0 01: S,N1 40240.00 61.800 No.date 61.30 26.70 n/a .000
019085 #
019086 # Sum of hydrographs from Node 6 routed to Node 5
019087 # Section 6
019088 #
019089 ROUTE2: C00056 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
019090 ROUTE CHANNEL > 30.0 02: SW,S 40240.00 40.613 No.date 61.30 26.70 n/a .000
019091 [RDR-30.00] out > 30.0 01: N1 40240.00 40.523 No.date 62.30 26.70 n/a .000
019092 [L/S=1852 / 0547.035]
019093 [Vmax =.440;Dmax=1.203]
019094 #
019095 # Addition of Subwatershed 5 and Flowing Creek to Node 5
019096 #
019097 ROUTE2: C00057 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
019098 ADD HYD + 30.0 02: SW,S 40240.00 61.800 No.date 62.30 26.70 n/a .000
019099 + 30.0 02: SW,S 224.00 6.682 No.date 28.30 35.63 n/a .000
020000 [RDR-30.00] out > 30.0 01: SW,S 45409.00 61.906 No.date 34.00 27.41 n/a .000
020001 SIM 30.0 01: S,N1 45409.00 61.906 No.date 34.00 27.41 n/a .000
020002 #
020003 # Sum of hydrographs from Node 5 routed to Node 4
020004 # Section 7
020005 #
020006 ROUTE2: C00058 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
020007 ROUTE CHANNEL > 30.0 02: SW,S 45409.00 61.906 No.date 34.00 27.41 n/a .000
020008 [RDR-30.00] out > 30.0 01: N1 45409.00 61.800 No.date 34.30 27.41 n/a .000
020009 [L/S=556 / 0907.040]
020010 [Vmax =.510;Dmax=1.217]
020011 #
020012 # Addition of Subwatershed 5A and Subwatershed 5A2 to Node 5A
020013 #
020014 ROUTE2: C00059 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
020015 ADD HYD + 30.0 02: SW,S 45409.00 61.800 No.date 34.30 27.41 n/a .000
020016 + 30.0 02: SW,S 20.00 7.739 No.date 28.30 39.33 n/a .000
020017 + 30.0 02: SW,S 1412.00 7.263 No.date 37.30 34.21 n/a .000
020018 SIM 30.0 01: S,NSA 46841.01 68.494 No.date 34.30 27.62 n/a .000
020019 #
020020 # Sum of hydrographs from Node 5A routed to Node 4
020021 # Section 8
020022 #
020023 ROUTE2: C00060 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
020024 ROUTE CHANNEL > 30.0 01: NSA 46841.01 68.494 No.date 34.30 27.62 n/a .000
020025 [RDR-30.00] out > 30.0 01: N1 46841.01 65.794 No.date 36.30 27.62 n/a .000
020026 [L/S=4630 / 0471.015]
020027 [Vmax =.838;Dmax=3.516]
020028 #
020029 # Addition of Subwatershed 4 and Learys Creek to Node 4
020030 #
020031 ROUTE2: C00061 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
020032 ADD HYD + 30.0 02: NS 46841.01 65.794 No.date 36.30 27.62 n/a .000
020033 + 30.0 02: SW,S 585.00 10.733 No.date 29.30 39.33 n/a .000
020034 + 30.0 02: NS,CK 4621.00 14.279 No.date 30.30 38.57 n/a .000
020035 SIM 30.0 01: S,N1 48447.00 73.162 No.date 35.30 27.99 n/a .000
020036 ROUTE2: C00062 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
020037 SAVE HYD 30.0 01: S,N1 48447.00 73.162 No.date 35.30 27.99 n/a .000
020038 frame :S,N1,0025
020039 remark:flow at S_N1
020040 #
020041 # Sum of hydrographs from Node 4 routed to Node 2
020042 # Section 9
020043 #
020044 ROUTE2: C00063 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
020045 ROUTE CHANNEL > 30.0 02: S,N1 48447.00 73.162 No.date 35.30 27.99 n/a .000
020046 [RDR-30.00] out > 30.0 01: N1 48447.00 72.927 No.date 35.30 27.99 n/a .000
020047 [L/S=1867 / 0607.040]
020048 [Vmax =.871;Dmax=3.588]
020049 #
020050 # Addition of Subwatershed 2 with Mnohan Drain and Smith Drain to Node 2
020051 # Section 10
020052 ROUTE2: C00064 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
020053 ADD HYD + 30.0 02: SW,S 177.00 5.280 No.date 28.30 35.63 n/a .000
020054 + 30.0 02: SW,S 177.00 5.280 No.date 28.30 35.63 n/a .000
020055 + 30.0 02: SW,S 1122.00 13.030 No.date 31.30 39.33 n/a .000
020056 + 30.0 02: NS,CK 2737.00 28.975 No.date 31.00 34.91 n/a .000
020057 SIM 30.0 01: S,N1 52483.00 104.643 No.date 33.00 28.62 n/a .000

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020058 ROUTE2: C00065 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
020059 SAVE HYD 30.0 01: S,N1 52483.00 104.643 No.date 33.00 28.62 n/a .000
020060 frame :H,SND
020061 remark:flow at S_N1 Jock River Gauge at Modie Dr.
020062 #
020063 # Sum of hydrographs from Node 2 routed to Node 1
020064 # Section 10
020065 #
020066 ROUTE2: C00066 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
020067 ROUTE CHANNEL > 30.0 02: S,N1 52483.00 104.643 No.date 33.00 28.62 n/a .000
020068 [RDR-30.00] out > 30.0 01: N1 52483.00 92.450 No.date 36.00 28.62 n/a .000
020069 [L/S=10046 / 0507.040]
020070 [Vmax =.998;Dmax=3.955]
020071 #
020072 # Addition of Subwatershed 1 to Node 1
020073 #
020074 ROUTE2: C00067 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
020075 ADD HYD + 30.0 02: NS 52483.00 92.450 No.date 36.00 28.62 n/a .000
020076 + 30.0 02: SW,S 3176.00 31.429 No.date 35.00 36.35 n/a .000
020077 SIM 30.0 01: N1 55659.00 115.838 No.date 34.30 29.06 n/a .000
020078 ROUTE2: C00068 -----DfIn-ID NND -----AREhA-QPEAGm-TpeakDate-hh:mm-----RvM-R.C-----DfWcm
020079 SAVE HYD 30.0 01: N1 55659.00 115.838 No.date 34.30 29.06 n/a .000
020080 frame :N1,0025
020081 remark:total outflow of Jock River
020082 #
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02993 #
02984 # Sum of hydrographs from Node 6 routed to Node 5
02985 # Section 6
02986 #
02997 R0100: C00056..... Dfm n-ID NMYD..... ARE:AbA-QPEAGcm-TpeakDtte_hh:mm..... RVmm R.C..... DWFcm
02998 ROUTE CHANNEL > 30.0 02: S_N 40240.01 60.383 No_date 59:30 36.31 n/a .000
02999 [RDF=30.00] out< 30.0 01: NSA 40240.01 60.383 No_date 60:30 36.31 n/a .000
03000 [L/S/n= 1852. / 054/ 035]
03001 [Vmax= .490; Dmax= 1.346]
03002 #
03003 # Addition of Subwatershed 5 and Flowing Creek to Node 5
03004 #
03005 R0100: C00057..... Dfm n-ID NMYD..... ARE:AbA-QPEAGcm-TpeakDtte_hh:mm..... RVmm R.C..... DWFcm
03006 ADD HYD + 30.0 02: S_N 45409.01 79.891 No_date 34:00 37.22 n/a .000
03007 + 30.0 02: SW_S 224.00 9.294 No_date 28:30 47.59 n/a .000
03008 + 30.0 02: FL_CK 4845.00 51.121 No_date 33:00 44.15 n/a .000
03009 SUM 30.0 01: S_N 45409.01 79.891 No_date 34:00 37.22 n/a .000
03010 #
03011 # Sum of hydrographs from Node 5 routed to Node 5A
03012 # Section 7
03013 #
03014 R0100: C00058..... Dfm n-ID NMYD..... ARE:AbA-QPEAGcm-TpeakDtte_hh:mm..... RVmm R.C..... DWFcm
03015 ROUTE CHANNEL > 30.0 02: S_N 45409.01 79.891 No_date 34:00 37.22 n/a .000
03016 [RDF=30.00] out< 30.0 01: NSA 45409.01 79.815 No_date 34:00 37.22 n/a .000
03017 [L/S/n= 556. / 090/ 040]
03018 [Vmax= .544; Dmax= 1.346]
03019 #
03020 # Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A
03021 #
03022 R0100: C00059..... Dfm n-ID NMYD..... ARE:AbA-QPEAGcm-TpeakDtte_hh:mm..... RVmm R.C..... DWFcm
03023 ADD HYD + 30.0 02: NSA 45409.01 79.815 No_date 34:00 37.22 n/a .000
03024 + 30.0 02: SW_S 20.00 1.014 No_date 28:30 52.03 n/a .000
03025 + 30.0 02: SW_S 1412.00 9.884 No_date 37:30 45.85 n/a .000
03026 SUM 30.0 01: S_N 46841.01 88.619 No_date 34:30 37.48 n/a .000
03027 #
03028 # Sum of hydrographs from Node 5A routed to Node 4
03029 # Section 8
03030 #
03031 R0100: C00060..... Dfm n-ID NMYD..... ARE:AbA-QPEAGcm-TpeakDtte_hh:mm..... RVmm R.C..... DWFcm
03032 ROUTE CHANNEL > 30.0 02: S_N 46841.01 88.619 No_date 34:30 37.48 n/a .000
03033 [RDF=30.00] out< 30.0 01: NI 46841.01 84.955 No_date 36:00 37.48 n/a .000
03034 [L/S/n= 4630. / 043/ 051]
03035 [Vmax= .901; Dmax= 3.849]
03036 #
03037 # Addition of Subwatershed 4 and Leamy Creek to Node 4
03038 #
03039 R0100: C00061..... Dfm n-ID NMYD..... ARE:AbA-QPEAGcm-TpeakDtte_hh:mm..... RVmm R.C..... DWFcm
03040 ADD HYD + 30.0 02: NI 46841.01 84.955 No_date 36:00 37.48 n/a .000
03041 + 30.0 02: SW_C 585.00 14.684 No_date 29:30 52.03 n/a .000
03042 + 30.0 02: FL_CK 1021.00 19.515 No_date 30:30 51.13 n/a .000
03043 SUM 30.0 01: S_N 48447.00 95.694 No_date 34:30 37.95 n/a .000
03044 R0100: C00062..... Dfm n-ID NMYD..... ARE:AbA-QPEAGcm-TpeakDtte_hh:mm..... RVmm R.C..... DWFcm
03045 SAVE HYD + 30.0 01: S_N 48447.00 95.694 No_date 34:30 37.95 n/a .000
03046 fname= S_N1.0100
03047 remark: flow at S_N1
03048 #
03049 # Sum of hydrographs from Node 4 routed to Node 2
03050 # Section 9
03051 #
03052 R0100: C00063..... Dfm n-ID NMYD..... ARE:AbA-QPEAGcm-TpeakDtte_hh:mm..... RVmm R.C..... DWFcm
03053 ROUTE CHANNEL > 30.0 02: S_N 48447.00 95.694 No_date 34:30 37.95 n/a .000
03054 [RDF=30.00] out< 30.0 01: NI 48447.00 95.342 No_date 35:00 37.95 n/a .000
03055 [L/S/n= 1667. / 060/ 040]
03056 [Vmax= .942; Dmax= 3.915]
03057 #
03058 # Addition of Subwatershed 2 with Mnohan Drain and Smith Drain to Node 2
03059 #
03060 R0100: C00064..... Dfm n-ID NMYD..... ARE:AbA-QPEAGcm-TpeakDtte_hh:mm..... RVmm R.C..... DWFcm
03061 ADD HYD + 30.0 02: NI 48447.00 95.342 No_date 35:00 37.95 n/a .000
03062 + 30.0 02: SW_C 177.00 7.344 No_date 28:30 47.59 n/a .000
03063 + 30.0 02: MD_DR 1122.00 17.710 No_date 31:30 52.03 n/a .000
03064 + 30.0 02: MD_DR 2737.00 40.026 No_date 31:00 46.72 n/a .000
03065 SUM 30.0 01: S_N 52483.00 141.415 No_date 32:30 38.74 n/a .000
03066 R0100: C00065..... Dfm n-ID NMYD..... ARE:AbA-QPEAGcm-TpeakDtte_hh:mm..... RVmm R.C..... DWFcm
03067 SAVE HYD + 30.0 01: S_N 52483.00 141.415 No_date 32:30 38.74 n/a .000
03068 fname= S_N2.0100
03069 remark: flow at S_N2 Jock River Gauge at Moudie Dr.
03070 #
03071 # Sum of hydrographs from Node 2 routed to Node 1
03072 # Section 10
03073 #
03074 R0100: C00066..... Dfm n-ID NMYD..... ARE:AbA-QPEAGcm-TpeakDtte_hh:mm..... RVmm R.C..... DWFcm
03075 ROUTE CHANNEL > 30.0 02: S_N 52483.00 141.415 No_date 32:30 38.74 n/a .000
03076 [RDF=30.00] out< 30.0 01: NI 52483.00 124.304 No_date 35:00 38.74 n/a .000
03077 [L/S/n= 1046. / 050/ 040]
03078 [Vmax= 1.091; Dmax= 4.553]
03079 #
03080 # Addition of Subwatershed 1 to Node 1
03081 #
03082 R0100: C00067..... Dfm n-ID NMYD..... ARE:AbA-QPEAGcm-TpeakDtte_hh:mm..... RVmm R.C..... DWFcm
03083 ADD HYD + 30.0 02: NI 52483.00 124.304 No_date 35:00 38.74 n/a .000
03084 + 30.0 02: SW_C 3176.00 43.079 No_date 32:00 48.46 n/a .000
03085 SUM 30.0 01: NI 55659.00 158.420 No_date 34:00 39.29 n/a .000
03086 R0100: C00068..... Dfm n-ID NMYD..... ARE:AbA-QPEAGcm-TpeakDtte_hh:mm..... RVmm R.C..... DWFcm
03087 SAVE HYD + 30.0 01: NI 55659.00 158.420 No_date 34:00 39.29 n/a .000
03088 fname= NI.0100
03089 remark: initial outflow of Jock River
03090 *****
03091 R0100: C0002.....
03092 FLSN1
03093 *****
03094 *****
03095 *****
03096 *****
03097 R0002: C00015 CONTINUES NASHID
03098 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03099 R0002: C00020 CONTINUES NASHID
03100 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03101 R0002: C00022 CONTINUES NASHID
03102 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03103 R0002: C00026 CONTINUES NASHID
03104 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03105 R0005: C00015 CONTINUES NASHID
03106 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03107 R0005: C00020 CONTINUES NASHID
03108 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03109 R0005: C00022 CONTINUES NASHID
03110 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03111 R0005: C00026 CONTINUES NASHID
03112 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03113 R0010: C00015 CONTINUES NASHID
03114 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03115 R0010: C00020 CONTINUES NASHID
03116 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03117 R0010: C00022 CONTINUES NASHID
03118 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03119 R0010: C00026 CONTINUES NASHID
03120 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03121 R0025: C00015 CONTINUES NASHID
03122 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03123 R0025: C00020 CONTINUES NASHID
03124 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03125 R0025: C00022 CONTINUES NASHID
03126 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03127 R0025: C00026 CONTINUES NASHID
03128 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03129 R0050: C00015 CONTINUES NASHID
03130 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03131 R0050: C00020 CONTINUES NASHID
03132 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03133 R0050: C00022 CONTINUES NASHID
03134 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03135 R0050: C00026 CONTINUES NASHID
03136 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03137 R0100: C00015 CONTINUES NASHID
03138 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03139 R0100: C00020 CONTINUES NASHID
03140 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03141 R0100: C00022 CONTINUES NASHID
03142 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03143 R0100: C00026 CONTINUES NASHID
03144 *** WARN NG: Tim step is too large for value of TP. RV may be ok. Peak flow could be off.
03145 Simulation ended on 2021-02-22 at 15:43:22
03146 *****
03147 *****
03148 *****

```

Attachment B

Model 2 – Jock River Reach One Model

Stantec, 2007

SWMHYMO Input & Summary files

```

1 2 Metric units
2 *****
3 *# Project Name: [Jock River Reach 1 SubWatershed Study]Project #: [160400414]
4 *# Date : October 2006
5 *# Mdeller : [Navin Gautam/ Original by Ana M Paerez]
6 *# Company : Stantec.
7 *# License # : 3824306
8 *****
9 START TZERO=[ 0.0], METOUT=[ 2], NSTORM=[ 1], NRUN=[ 002]
10 *% ["C24SC002.stm"] <--storm filename, one per line for NSTORMtime
11 *#-----|-----|
12 READ STORM STORM_FILENAME=[ "st or m 001"]
13 *%-----|-----|
14 MODIFY STORM I CASEms=[ 1], NSHIFT=[ 96],
15 RedFACT=[ 1],
16 *%-----|-----|
17 DEFAULT VALUES I CASEdv=[ 1], read and print values
18 DEFVAL_FILENAME=[ "MODIFIED.VAL"]
19 COMPUTE API API I=[ 50], API K=[. 85]/day
20 *****
21 *#
22 *# JOCK RIVER REACH 1 SUBWATERSHED STUDY DISCRETIZED MODEL
23 *# PROPOSED CONDITIONS DESIGN STORM MODEL (SUMMER)
24 *#
25 *# Version: Draft Final Report, October 2006
26 *# Revision History
27 *# -Draft Interim Condition Report, Nov. 2005
28 *****
29 *# Assumptions
30 *# - All catchments are assumed to be developed except S-1, S-2, and SW1a
31 *# - SWM facilities are modeled
32 *# - Rating curves were estimated based on existing reports and modeling for the
33 *# proposed SWM facilities
34 *# - The rating curve for the existing Kennedy Burnett SWM Facility was obtained from
35 *# the Urban Runoff Treatment in the Kennedy Burnett Settling Pond (URTKBP)- Regional
36 *# Municipality of Ottawa Carleton, March 1983
37 *# - River routing modeled
38 *# - River cross sections obtained from RVCA's HEC-RAS hydraulic model
39 *#-----|-----|
40 *# Parameters
41 *# - Design Storms: 2, 5, 10, 25, 50 & 100yr events: 24hr SCS (DT=10min)-model comparison
42 *# - Impervious area weighted based on: rural subdivision @0% urban @5%
43 *# - NRCS(SCS) CN based on landuse (airphoto) and soil type (base mapping)
44 *# - Time to peak using Uplands Method
45 *#-----|-----|
46 *****
47 *#Read hydrograph upstream of N2 from RVCA Jock R. floodrisk watershed modeling
48 *****
49 READ HYD ID=[ 1 ], NHYD=[ "S_N2" ],
50 HYD_FILENAME=[ "H-S_N2" ]
51 *%-----|-----|
52 *#
53 *# Hydrograph from Node 2 routed to Node 416
54 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 9025
55 *#
56 ROUTE CHANNEL IDout=[ 4], NHYD=[ "N_416" ], IDin=[ 1 ],
57 RDT=[ 10] (min),
58 CHLGTH=[ 2327] (m), CHSLOPE=[ 0.0498] (%),
59 FPSLOPE=[ 0.0498] (%),
60 SECNUM=[ 1.0], NSEG=[ 3]
61 ( SEGROUGH, SEGDIST (m) )=
62 [ 0.075, -23.96
63 -0.055, 23.96
64 0.075, 157.38] NSEG times
65 ( DISTANCE (m), ELEVATION (m) )=
66 [-336.97, 93.5]

```

```

67 [- 318. 85, 93]
68 [- 259, 92. 5]
69 [- 133. 18, 92]
70 [- 33. 17, 92]
71 [- 27. 21, 92]
72 [- 26. 14, 91. 5]
73 [- 24. 99, 91]
74 [- 23. 96, 90. 5]
75 [- 14. 33, 88. 26]
76 [- 0. 68, 88. 12]
77 [14. 33, 88. 26]
78 [23. 96, 90. 5]
79 [32. 12, 91]
80 [43. 74, 91. 5]
81 [57. 09, 92]
82 [73. 53, 92. 5]
83 [108. 27, 93]
84 [125. 88, 93. 5]
85 [144. 81, 94]
86 [157. 38, 94. 5]
87 *%-----|-----|
88 *#*****|
89 *# Catchment SW1a
90 *# - Portion of RVCA catchment SW1 outside of Reach 1 subwatershed
91 *# - Undeveloped agricultural land
92 *#*****|
93 CONTINUOUS NASHYD ID=[ 2], NHYD=[ "SW_1a"], DT=[ 5] mi n, AREA=[ 546] ( ha),
94 DWF=[ 0] ( cms), CN C=[ 72], IA=[ 4. 67] ( mm),
95 N=[ 3], TP=[ 2. 79] hr s,
96 Continuous simulation parameters:
97 IaRECper=[ 4] ( hr s),
98 SM N=[ - 1] ( mm), SMAX=[ - 1] ( mm), SK=[ 0. 010] / ( mm),
99 InterEvent Time=[ 12] ( hr s)
100 Baseflow simulation parameters:
101 BaseFlowOption=[ 1],
102 In it GWRes Vol=[ 50] ( mm), GWRes K=[ 0. 96] ( mm/ day/ mm)
103 VHydCond=[ 0. 055] ( mm/ hr), END=- 1
104 *%-----|-----|
105 ADD HYD IDsum=[ 3 ], NHYD=[ "SN_416"], IDsto add=[ 4, 2]
106 *%-----|-----|
107 SAVE HYD ID=[ 3 ], # OF PCYCLES=[ - 1], ICASEsh=[ 1]
108 HYD_COMMENT=[ "Total Flows at Highway 416"]
109 *%-----|-----|
110 *#
111 *# Hydrograph from Node 416 routed to Node at Okeefe drain
112 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 7245
113 *#
114 ROUTE CHANNEL IDout=[ 1], NHYD=[ "N_OK"], IDin=[ 3],
115 RDT=[ 5] ( mi n),
116 CHLGTH=[ 497] ( m), CHSLOPE=[ 0. 3018] ( %),
117 FPSLOPE=[ 0. 3018] ( %),
118 SECNUM=[ 1. 0], NSEG=[ 3]
119 ( SEGROUGH, SEGDI ST ( m)) =
120 [ 0. 075, - 19. 40
121 - 0. 055, 19. 40
122 0. 075, 377. 02] NSEG times
123 ( DI STANCE ( m), ELEVATI ON ( m)) =
124 [- 1062. 81, 93. 00]
125 [- 1061. 41, 92. 50]
126 [- 945. 91, 92. 00]
127 [- 783. 64, 91. 50]
128 [- 136. 74, 91. 00]
129 [- 134. 06, 91. 00]
130 [- 128. 97, 91. 00]
131 [- 86. 04, 91. 00]
132 [- 20. 86, 91. 00]

```

```

133      [- 20.18, 90.50]
134      [- 19.40, 90.00]
135      [- 11.68, 86.89]
136      [ 0.00, 86.10]
137      [ 12.09, 86.81]
138      [ 19.40, 90.00]
139      [ 34.68, 90.50]
140      [ 60.56, 91.00]
141      [ 170.14, 91.00]
142      [ 175.05, 90.50]
143      [ 180.29, 90.00]
144      [ 193.41, 90.00]
145      [ 195.98, 90.50]
146      [ 377.02, 92.50]
147  *%-----|-----|
148  *#*****|
149  *#      Catchment OKEEFE
150  *#      - To O Keefe drain (north of the Jock)
151  *#      - Developed with assumed 43% imp.
152  *#*****|
153  CONTINUOUS STANDHYD ID=[ 2], NHYD=["OKEEFE"], DT=[ 5](mi n), AREA=[ 448](ha),
154  XI MP=[ 0.43], TI MP=[ 0.43], DWF=[ 0](cms), LOSS=[ 2],
155  SCS curve number CN=[ 77],
156  Pervious surfaces: I A per=[ 4.67](mm), SLPP=[ 0.5](%),
157  LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](mi n),
158  Impervious surfaces: I A i mp=[ 1.57](mm), SLPI=[ 0.5](%),
159  LGI=[ 1728](m), MNI=[ 0.013], SCI=[ 0](mi n),
160  Continuous simulation parameters:
161  I a RE C per=[ 4](hrs), I a RE C i mp=[ 4](hrs),
162  SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
163  Inter Event Ti me=[ 18](hrs), END=- 1
164
165  *#*****|
166  *#      Okeefe Pond
167  *#      - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
168  *#      and a ratio of the catchment area to the West Clarke pond rating curve
169  *#      from the MSS for the next coordinates
170  *#*****|
171  ROUTE RESERVOIR I D out=[ 4], NHYD=["P_OKE"], I D i n=[ 2],
172  RDT=[ 5](mi n),
173  TABLE of ( OUTFLOW STORAGE ) values
174  ( cms ) - ( ha - m)
175  [ 0.0 , 0.0 ]
176  [ 0.20 , 1.72]
177  [ -1 , -1 ] (max twenty pts)
178  I D o v f=[ 9], NHY D o v f=["ok-OVF"]
179
180  *%-----|-----|
181  ADD HYD I D s um=[ 3 ], NHYD=["SN_OK"], I D s t o a dd=[ 1,4,9]
182  *%-----|-----|
183  SAVE HYD I D=[ 3 ], # OF PCYCLES=[ -1], I C A S E s h=[ 1]
184  HYD_COMMENT=["Total Flows at Okeefe Drain"]
185  *%-----|-----|
186  *#
187  *# Hydrograph from Node Okeefe routed to Node at Foster Drain
188  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
189  *#
190  ROUTE CHANNEL I D out=[ 1], NHYD=["N_FO"], I D i n=[ 3 ],
191  RDT=[ 5](mi n),
192  CHLGTH=[ 1183](m), CHSLOPE=[ 0.0761](%),
193  FPSLOPE=[ 0.0761](%),
194  SECNUM=[ 1.0], NSEG=[ 3]
195  ( SEGROUGH, SEGDI ST (m))=
196  [ 0.050, -33.89
197  -0.035, 31.59
198  0.050, 854.54] NSEG times

```

```

199      ( DI STANCE ( m ) , ELEVATI ON ( m ) ) =
200      [ - 1075. 50 , 93. 00 ]
201      [ - 1070. 59 , 92. 50 ]
202      [ - 1003. 21 , 92. 00 ]
203      [ - 1001. 67 , 92. 00 ]
204      [ - 986. 64 , 92. 00 ]
205      [ - 816. 61 , 91. 50 ]
206      [ - 797. 29 , 91. 00 ]
207      [ - 794. 18 , 91. 00 ]
208      [ - 775. 41 , 91. 50 ]
209      [ - 702. 63 , 91. 50 ]
210      [ - 546. 19 , 91. 50 ]
211      [ - 529. 54 , 91. 50 ]
212      [ - 323. 44 , 91. 00 ]
213      [ - 320. 71 , 91. 00 ]
214      [ - 183. 59 , 91. 00 ]
215      [ - 182. 54 , 90. 50 ]
216      [ - 181. 36 , 90. 00 ]
217      [ - 177. 37 , 90. 00 ]
218      [ - 87. 70 , 90. 00 ]
219      [ - 33. 89 , 90. 00 ]
220      [ - 18. 52 , 86. 88 ]
221      [ 0. 00 , 85. 20 ]
222      [ 16. 20 , 86. 83 ]
223      [ 31. 59 , 90. 00 ]
224      [ 33. 03 , 90. 50 ]
225      [ 34. 41 , 91. 00 ]
226      [ 34. 99 , 91. 00 ]
227      [ 72. 19 , 91. 00 ]
228      [ 208. 76 , 91. 50 ]
229      [ 846. 25 , 92. 00 ]
230      [ 854. 54 , 94. 00 ]
231      *%-----|-----|
232      *#*****|
233      *#      Catchment FOSTER
234      *#      - To Foster ditch (north of the Jock)
235      *#      - Partially developed (medium density); remaining agricultural
236      *#*****|
237      CONTINUOUS STANDHYD ID=[ 2 ] , NHYD=[ "FOSTER" ] , DT=[ 5 ] mi n , AREA=[ 373 ] ( ha ) ,
238      XI MP=[ 0. 55 ] , TI MP=[ 0. 55 ] , DWF=[ 0 ] ( cms ) , LOSS=[ 2 ] ,
239      SCS curve number CN=[ 74 ] ,
240      Per vious surfaces: I A per=[ 4. 67 ] ( mm ) , SLPP=[ 0. 5 ] ( % ) ,
241      LGP=[ 40 ] ( m ) , MNP=[ 0. 25 ] , SCP=[ 0 ] ( mi n ) ,
242      Imper vious surfaces: I A i mp=[ 1. 57 ] ( mm ) , SLPI=[ 0. 5 ] ( % ) ,
243      LGI=[ 1577 ] ( m ) , MNI=[ 0. 013 ] , SCI=[ 0 ] ( mi n ) ,
244      Continuous simulation parameters:
245      I a REC per=[ 4 ] ( hr s ) , I a REC i mp=[ 4 ] ( hr s ) ,
246      SM N=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0. 010 ] / ( mm ) ,
247      Inter Event Ti me=[ 18 ] ( hr s ) , END=- 1
248
249      *#*****|
250      *#      Foster Pond
251      *#      - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
252      *#      and a ratio of the catchment area to the West Clarke pond rating curve
253      *#      from the MS for the next coordinates
254      *#*****|
255      ROUTE RESERVOIR I D out =[ 4 ] , NHYD=[ "P_FOS" ] , I D i n =[ 2 ] ,
256      RDT=[ 5 ] ( mi n ) ,
257      TABLE of ( OUTFLOW STORAGE ) values
258      ( cms ) - ( ha - m )
259      [ 0. 0 , 0. 0 ]
260      [ 0. 20 , 1. 72 ]
261      [ - 1 , - 1 ] ( max twenty pts )
262      I D ovf =[ 9 ] , NHYD ovf =[ "FO - OVF" ]
263      *%-----|-----|
264      ADD HYD I D s um =[ 3 ] , NHYD=[ "SN_FO" ] , I D s to add =[ 1 , 4 , 9 ]

```



```

265 *%-----|-----|
266 SAVE HYD          ID=[ 3 ], # OF PCYCLES=[ - 1], I CASEs h=[ 1]
267                  HYD_COMMENT=["Total Flows at Foster Drain"]
268 *%-----|-----|
269 *#
270 *# Hydrograph from Node Foster routed to Node at Cedarview Road
271 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6016
272 *#
273 ROUTE CHANNEL     IDout=[ 1], NHYD=["N_CE"], IDin=[ 3],
274                  RDT=[ 5](min),
275                  CHSLTH=[ 159](m), CHSLOPE=[ 0.0818](%),
276                  FPSLOPE=[ 0.0818](%),
277                  SECNUM=[ 1.0], NSEG=[ 3]
278                  ( SEGROUGH, SEGDI ST (m))=
279                    [ 0.050, -15.46
280                    -0.035, 26.55
281                    0.050, 1299.52] NSEG times
282                  ( DI STANCE (m), ELEVATI ON (m))=
283                    [- 891.38, 93.00]
284                    [- 882.49, 93.00]
285                    [- 880.92, 92.50]
286                    [- 879.37, 92.00]
287                    [- 877.72, 91.50]
288                    [- 876.10, 91.00]
289                    [- 873.23, 91.00]
290                    [- 871.82, 91.50]
291                    [- 870.40, 92.00]
292                    [- 803.44, 92.00]
293                    [- 645.23, 91.50]
294                    [- 391.20, 91.50]
295                    [- 91.00, 91.50]
296                    [- 85.52, 91.50]
297                    [- 15.46, 89.40]
298                    [- 9.79, 89.31]
299                    [- 3.22, 86.24]
300                    [ 3.22, 85.07]
301                    [ 10.96, 85.79]
302                    [ 16.44, 86.49]
303                    [ 26.55, 89.45]
304                    [ 29.03, 90.27]
305                    [ 35.76, 90.67]
306                    [ 36.67, 91.00]
307                    [ 108.08, 91.00]
308                    [ 109.82, 90.50]
309                    [ 112.04, 90.50]
310                    [ 114.62, 91.00]
311                    [ 116.76, 91.50]
312                    [ 118.42, 92.00]
313                    [ 449.53, 92.50]
314                    [ 571.98, 92.50]
315                    [ 1093.81, 93.50]
316                    [ 1150.48, 94.00]
317                    [ 1299.52, 95.00]
318 *%-----|-----|
319 *#*****|*****|
320 *# Catchment S-1
321 *# - To Jock River (north and south of Jock)
322 *# - Primarily agricultural fields; portion of sand quarry
323 *#*****|*****|
324 CONTINUOUS NASHYD ID=[ 2], NHYD=["S-1"], DT=[ 5]min, AREA=[ 245](ha),
325                  DWF=[ 0](cms), CNVC=[ 77], IA=[ 4.67](mm),
326                  N=[ 3], TP=[ 1.10]hrs,
327                  Continuous simulation parameters:
328                  IaRECper=[ 4](hrs),
329                  SMN=[ - 1](mm), SMAX=[ - 1](mm), SK=[ 0.010]/(mm),
330                  InterEventTime=[ 12](hrs)

```

```

331 Baseflow simulation parameters:
332 BaseFlowOption=[ 1] ,
333 InitGWResVol=[ 50] ( mm) , GWResK=[ 0.96] ( mm/ day/ mm)
334 VHydCond=[ 0.055] ( mm/ hr) , END=- 1
335
336 *%-----|-----|
337 ADD HYD IDsum=[ 3 ] , NHYD=[ "SN_CE" ] , IDsto add=[ 1,2]
338 *%-----|-----|
339 SAVE HYD ID=[ 3 ] , # OF PCYCLES=[ -1] , ICASEsh=[ 1]
340 HYD_COMMENT=[ "Total Flows at Cedarview Road" ]
341 *%-----|-----|
342 *#
343 *# Hydrograph from Node Cedarview Road routed to Node at West Clarke Drain
344 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 5002
345 *#
346 ROUTE CHANNEL IDout=[ 1] , NHYD=[ "N_WC" ] , IDin=[ 3] ,
347 RDT=[ 5] ( min) ,
348 CHLGTH=[ 825] ( m) , CHSLOPE=[ 0.01] ( % ) ,
349 FPSLOPE=[ 0.01] ( % ) ,
350 SECNUM=[ 1.0] , NSEG=[ 3]
351 ( SEGROUGH, SEGDI ST ( m) ) =
352 [ 0.050, -37.5
353 -0.035, 37.50
354 0.050, 1367.08] NSEG times
355 ( DI STANCE ( m) , ELEVATI ON ( m) ) =
356 [- 1095.18, 94.00]
357 [- 1091.79, 93.50]
358 [- 1088.95, 93.00]
359 [- 1086.77, 93.00]
360 [- 1069.38, 93.00]
361 [- 1063.14, 93.00]
362 [- 1017.52, 93.00]
363 [- 899.70, 93.00]
364 [- 877.78, 93.00]
365 [- 859.62, 92.50]
366 [- 803.18, 93.00]
367 [- 789.92, 92.00]
368 [- 37.50, 90.00]
369 [- 19.61, 87.04]
370 [ 0.00, 85.70]
371 [ 14.87, 86.93]
372 [ 37.50, 90.00]
373 [ 38.54, 90.50]
374 [ 42.23, 91]
375 [ 157.05, 91.50]
376 [ 161.44, 91.50]
377 [ 236.48, 93.00]
378 [ 385.47, 92.50]
379 [ 390.78, 92.50]
380 [ 863.80, 93.00]
381 [ 866.13, 93.00]
382 [ 990.85, 92.50]
383 [ 991.82, 92.50]
384 [ 993.04, 93.00]
385 [ 994.81, 93.50]
386 [ 1005.36, 93.00]
387 [ 1190.52, 93.00]
388 [ 1267.97, 93.50]
389 [ 1318.99, 94.00]
390 [ 1367.08, 94.50]
391 *%-----|-----|
392 *#*****
393 *# Catchment W_CLAR
394 *# - To West Clarke Drain (south of the Jock)
395 *# - Subdivision with 43% imp. as per Barrhaven South MSS
396 *#*****

```

```

397 CONTINUOUS STANDHYD ID=[ 2], NHYD=["W_CLAR"], DT=[ 5] mi n, AREA=[ 243] (ha),
398 XI MP=[ 0.43], TI MP=[ 0.43], DWF=[ 0] (cms), LOSS=[ 2],
399 SCS curve number CN=[ 75],
400 Pervious surfaces: I A per=[ 4.67] (mm), SLPP=[ 1] (%),
401 LGP=[ 40] (m), MNP=[ 0.25], SCP=[ 0] (mi n),
402 Impervious surfaces: I A i mp=[ 1.57] (mm), SLPI=[ 1] (%),
403 LGI=[ 1273] (m), MNI=[ 0.013], SCI=[ 0] (mi n),
404 Continuous simulation parameters:
405 I a REC per=[ 4] (hr s), I a REC i mp=[ 4] (hr s),
406 SM N=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
407 Inter Event Ti me=[ 18] (hr s), END=- 1
408
409 *%-----|-----|
410 *#*****|
411 *# West Clarke Pond 2
412 *# - Rating curve obtained from Barrhaven South M&S modeling
413 *# - Tributary Drainage Area to M&S Pond 2 = 241 ha
414 *#*****|
415 ROUTE RESERVOIR I D out=[ 8], NHYD=["M&S_P2"], I D i n=[ 2],
416 RDT=[ 5] (mi n),
417 TABLE of ( OUTFLOW STORAGE ) values
418 ( cms ) - ( ha - m)
419 [ 0.0 , 0.0 ]
420 [ 0.11 , 0.96]
421 [ -1 , -1 ] (max twenty pts)
422 I D ovf=[ 9], NHYD ovf=["P2- OVF"]
423 *%-----|-----|
424 ADD HYD I D s um=[ 4 ], NHYD=["SN_WC"], I D s to add=[ 8,9,1]
425 *%-----|-----|
426 SAVE HYD I D=[ 4], # OF PCYCLES=[ -1], I C A S E s h=[ 1]
427 HYD_COMMENT=["Total Flows at West Clarke Pond Outlet"]
428 *%-----|-----|
429 *# Hydrograph from Node West Clarke routed to Node at Kennedy - Burnett Drain
430 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 4534
431 *#
432 ROUTE CHANNEL I D out=[ 1], NHYD=["N_KB"], I D i n=[ 4],
433 RDT=[ 5] (mi n),
434 CHLGTH=[ 1020] (m), CHSLOPE=[ 0.0498] (%),
435 FPSLOPE=[ 0.0498] (%),
436 SECNUM=[ 1.0], NSEG=[ 3]
437 ( SEGROUGH, SEGDI ST (m))=
438 [ 0.050, -23.63
439 -0.035, 23.63
440 0.050, 728.3] NSEG times
441 ( DI STANCE (m), ELEVATI ON (m))=
442 [-1082.01, 94]
443 [-1028.17, 92.5]
444 [-992.3, 93.5]
445 [-279.34, 90]
446 [-23.63, 90]
447 [-13.45, 87.13]
448 [-0.07, 86.24]
449 [10.54, 87.15]
450 [23.63, 90]
451 [24.86, 90.5]
452 [26.72, 91]
453 [45.07, 91.5]
454 [128.17, 91.5]
455 [270.7, 92.5]
456 [728.3, 95]
457
458 *%-----|-----|
459 *#*****|
460 *# Catchment KEN_BU
461 *# - To Kennedy-Burnett SWM Facility
462 *# - Outlets to Fraser-Clarke drain (north of the Jock)

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```

463  *# - Medium density residential subdivision
464  *#*****
465  CONTINUOUS STANDHYD ID=[ 2], NHYD=["KEN_BU"], DT=[ 5] mi n, AREA=[ 281] (ha),
466  XI MP=[ 0.55], TI MP=[ 0.55], DWF=[ 0] (cms), LOSS=[ 2],
467  SCS curve number CN=[ 71],
468  Pervious surfaces: IAper=[ 4.67] (mm), SLPP=[ 1] (%),
469  LGP=[ 40] (m), MNP=[ 0.25], SCP=[ 0] (mi n),
470  Impervious surfaces: IAi mp=[ 1.57] (mm), SLPI =[ 1] (%),
471  LGI =[ 1369] (m), MNI =[ 0.013], SCI =[ 0] (mi n),
472  Continuous simulation parameters:
473  IaRECper=[ 4] (hrs), IaRECI mp=[ 4] (hrs),
474  SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
475  InterEvent Time=[ 18] (hrs), END=- 1
476  *%-----|-----|
477  *#*****
478  *# Existing Kennedy-Burnett SWM Facility
479  *# - Rating curve obtained from URTKBP
480  *# - Tributary Drainage Area to Pond = 160 ha
481  *#*****
482  ROUTE RESERVOIR IDout=[ 5], NHYD=["KEN_P"], IDi n=[ 2],
483  RDT=[ 5] (mi n),
484  TABLE of ( OUTFLOW STORAGE ) values
485  ( cms ) - ( ha-m)
486  [ 0.0 , 0.0 ]
487  [ 0.13 , 0.26]
488  [ 0.43 , 0.56]
489  [ 0.67 , 0.90]
490  [ 0.86 , 1.32]
491  [ 1.01 , 1.79]
492  [ 1.15 , 2.33]
493  [ -1 , -1 ] (max twenty pts)
494  IDovf=[ 6], NHYDovf=["KEN_OV"]
495  *%-----|-----|
496  *#*****
497  *# Catchment FRASER
498  *# - To Fraser-Clarke drain (north of the Jock)
499  *# - Developed land with assumed 43% imp.
500  *#*****
501  CONTINUOUS STANDHYD ID=[ 7], NHYD=["FRASER"], DT=[ 5] mi n, AREA=[ 90] (ha),
502  XI MP=[ 0.25], TI MP=[ 0.25], DWF=[ 0] (cms), LOSS=[ 2],
503  SCS curve number CN=[ 80],
504  Pervious surfaces: IAper=[ 4.67] (mm), SLPP=[ 1] (%),
505  LGP=[ 40] (m), MNP=[ 0.25], SCP=[ 0] (mi n),
506  Impervious surfaces: IAi mp=[ 1.57] (mm), SLPI =[ 1] (%),
507  LGI =[ 775] (m), MNI =[ 0.013], SCI =[ 0] (mi n),
508  Continuous simulation parameters:
509  IaRECper=[ 4] (hrs), IaRECI mp=[ 4] (hrs),
510  SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
511  InterEvent Time=[ 18] (hrs), END=- 1
512
513  *%-----|-----|
514  ROUTE RESERVOIR IDout=[ 8], NHYD=["MS_P2"], IDi n=[ 7],
515  RDT=[ 5] (mi n),
516  TABLE of ( OUTFLOW STORAGE ) values
517  ( cms ) - ( ha-m)
518  [ 0.0 , 0.0 ]
519  [ 0.04 , 0.36]
520  [ -1 , -1 ] (max twenty pts)
521  IDovf=[ 9], NHYDovf=["P2-OVF"]
522  *%-----|-----|
523  ADD HYD IDsum=[ 4 ], NHYD=["SN_KB"], IDst o add=[ 5, 6, 8, 9, 1]
524  *%-----|-----|
525  SAVE HYD ID=[ 4], # OF PCYCLES=[ -1], ICASEsh=[ 1]
526  HYD_COMMENT=["Total Flows at Ken-Burnett Outlet"]
527  *%-----|-----|
528  *# Hydrograph from Node Kennedy - Burnett Drain to Node Todd Drain

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529  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 3633
530  *#
531  ROUTE CHANNEL      I Dout =[ 1], NHYD=[ "N_TO" ] , I D i n=[ 4] ,
532                    RDT=[ 5] ( m i n),
533                    CHLGTH=[ 650] ( m),   CHSLOPE=[ 0. 0498] ( %),
534                    FPSLOPE=[ 0. 0498] ( %),
535                    SECNUM=[ 1. 0],      NSEG=[ 3]
536                    ( SEGROUGH, SEGDI ST ( m) )=
537                      [ 0. 050, - 23. 74
538                      - 0. 035, 23. 74
539                      0. 050, 74. 7] NSEG t i m e s
540                    ( DI STANCE ( m), ELEVATI ON ( m) )=
541                      [- 74. 18, 92. 5]
542                      [- 65. 96, 92]
543                      [- 54. 17, 91. 5]
544                      [- 29. 24, 91]
545                      [- 27. 41, 90. 5]
546                      [- 25. 64, 90]
547                      [- 23. 74, 89. 5]
548                      [- 22, 89. 26]
549                      [- 20, 88. 51]
550                      [- 19, 88. 32]
551                      [- 15, 88. 1]
552                      [- 10, 88. 11]
553                      [- 5, 88. 17]
554                      [ 0, 88. 27]
555                      [ 5, 88. 19]
556                      [ 10, 88. 06]
557                      [ 15, 88. 48]
558                      [ 16, 88. 7]
559                      [ 23. 74, 89. 5]
560                      [ 24. 68, 90]
561                      [ 25. 57, 90. 5]
562                      [ 26. 5, 91]
563                      [ 47. 55, 91]
564                      [ 74. 7, 92. 5]
565  *%-----|-----|
566
567  *#*****
568  *#      Catchment TODD
569  *#      - To Todd Drain (south of the Jock)
570  *#      - Subdivision with 43% imp. as per Barrhaven South M&S
571  *#*****
572  CONTINUOUS STANDHYD I D=[ 3], NHYD=[ "TODD" ], DT=[ 5] m i n, AREA=[ 195] ( ha),
573                    XI MP=[ 0. 43], TI MP=[ 0. 43], DWF=[ 0] ( c m s), LOSS=[ 2],
574                    SCS curve number CN=[ 77],
575                    Pervious surfaces: I A p e r=[ 4. 67] ( m m), SLPP=[ 1] ( %),
576                    LGP=[ 40] ( m), MNP=[ 0. 25], SCP=[ 0] ( m i n),
577                    Impervious surfaces: I A i m p=[ 1. 57] ( m m), SLPI=[ 1] ( %),
578                    LGI=[ 1140] ( m), MNI=[ 0. 013], SCI=[ 0] ( m i n),
579                    Continuous simulation parameters:
580                    I a R E C p e r=[ 4] ( h r s), I a R E C i m p=[ 4] ( h r s),
581                    S M N=[ - 1] ( m m), S M A X=[ - 1] ( m m), S K=[ 0. 010] / ( m m),
582                    I n t e r E v e n t T i m e=[ 18] ( h r s), E N D=- 1
583
584  *#*****
585  *#      Todd Pond 3
586  *#      - Rating curve obtained from Barrhaven South M&S modeling
587  *#      - Tributary Drainage Area to M&S Pond 3 = 193 ha
588  *#*****
589  ROUTE RESERVOIR    I Dout =[ 2], NHYD=[ "M&S_P3" ], I D i n=[ 3],
590                    RDT=[ 5] ( m i n),
591                    TABLE of ( OUTFLOW STORAGE ) values
592                    ( c m s) - ( ha- m)
593                    [ 0. 0 , 0. 0 ]
594                    [ 0. 08 , 0. 78]

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595                                     [ -1 , -1 ] (max twenty pts)
596                               IDovf=[9], NHYDovf=["P3-OVF"]
597 *%-----|-----|
598 ADD HYD                               IDsum=[10], NHYD=["SN_TO"], IDstoadd=[1,2,9]
599 *%-----|-----|
600 SAVE HYD                               ID=[10], # OF PCYCLES=[-1], ICASEsh=[1]
601                               HYD_COMMENT=["Total Flows at Todd Drain"]
602 *%-----|-----|
603 *#
604 *# Hydrograph from Todd Drain routed to Corrigan Drain
605 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
606 *#
607 ROUTE CHANNEL                         IDout=[1], NHYD=["N_TO"], IDin=[10],
608                               RDT=[5] (min),
609                               CHLGTH=[280] (m), CHSLOPE=[0.033] (%),
610                               FPSLOPE=[0.033] (%),
611                               SECNUM=[1.0], NSEG=[3]
612                               ( SEGROUGH, SEGDI ST (m) ) =
613                               [0.075, -17.72
614                               -0.045, 17.72
615                               0.075, 80.62] NSEG times
616                               ( DI STANCE (m), ELEVATI ON (m) ) =
617                               [-83.32, 90.00]
618                               [-81.36, 89.50]
619                               [-79.12, 89.00]
620                               [-76.13, 88.50]
621                               [-20.46, 88.00]
622                               [-19.36, 87.50]
623                               [-18.51, 87.00]
624                               [-17.72, 86.50]
625                               [-11.95, 85.24]
626                               [-0.11, 85.12]
627                               [11.49, 85.20]
628                               [17.72, 86.50]
629                               [19.74, 87.00]
630                               [21.22, 87.50]
631                               [22.68, 88.00]
632                               [24.28, 88.50]
633                               [26.79, 89.00]
634                               [71.98, 90.00]
635                               [80.62, 90.50]
636 *%-----|-----|
637 *#*****|*****|
638 *# Catchment CORRIG
639 *# - To Corrigan Drain (south of the Jock)
640 *# - Primarily Developed (medium density)
641 *#*****|*****|
642 CONTINUOUS STANDHYD ID=[2], NHYD=["CORRIG"], DT=[5] min, AREA=[149] (ha),
643                               XI MP=[0.45], TI MP=[0.45], DWF=[0] (cms), LOSS=[2],
644                               SCS curve number CN=[77],
645                               Pervious surfaces: IAper=[4.67] (mm), SLPP=[1] (%),
646                               LGP=[40] (m), MNP=[0.25], SCP=[0] (min),
647                               Impervious surfaces: IAimp=[1.57] (mm), SLPI=[1] (%),
648                               LGI=[997] (m), MNI=[0.013], SCI=[0] (min),
649                               Continuous simulation parameters:
650                               IaRECper=[4] (hrs), IaRECI mp=[4] (hrs),
651                               SMN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010] / (mm),
652                               InterEvent Time=[18] (hrs), END=-1
653
654 *%-----|-----|
655 *#*****|*****|
656 *# Corrigan Pond 1
657 *# - Rating curve obtained from Barrhaven South MSS modeling
658 *# - Tributary Drainage Area to MSS Pond 1 = 145 ha
659 *#*****|*****|
660 ROUTE RESERVOIR IDout=[5], NHYD=["MS_P1"], IDin=[2],

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661 RDT=[ 5] ( mi n),
662 TABLE of ( OUTFLOW STORAGE ) values
663 ( cms ) - ( ha- m)
664 [ 0. 0 , 0. 0 ]
665 [ 0. 06 , 0. 58]
666 [ -1 , -1 ] (max twenty pts)
667 I Dovf=[ 4], NHYDovf=[" P1- OVF" ]
668 *%-----|-----|
669 ADD HYD I Dsum=[ 3 ], NHYD=[" SN_CO" ], I Ds to add=[ 1, 4, 5]
670 *%-----|-----|
671 SAVE HYD I D=[ 3 ], # OF PCYCLES=[ -1], I CASEsh=[ 1]
672 HYD_COMMENT=[" Total Flows at Corrigan Drain" ]
673 *%-----|-----|
674 *#
675 *# Hydrograph from Corrigan Drain routed to Jockvale Road
676 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
677 *#
678 ROUTE CHANNEL I Dout =[ 1], NHYD=[" N_M" ], I Din =[ 3] ,
679 RDT=[ 5] ( mi n),
680 CHLGTH=[ 580] ( m), CHSLOPE=[ 0. 4448] ( %),
681 FPSLOPE=[ 0. 4448] ( %),
682 SECNUM=[ 1. 0], NSEG=[ 3]
683 ( SEGROUGH, SEGDI ST ( m) ) =
684 [ 0. 075, -17. 72
685 -0. 045, 17. 72
686 0. 075, 80. 62] NSEG times
687 ( DI STANCE ( m), ELEVATI ON ( m) ) =
688 [- 83. 32, 90. 00]
689 [- 81. 36, 89. 50]
690 [- 79. 12, 89. 00]
691 [- 76. 13, 88. 50]
692 [- 20. 46, 88. 00]
693 [- 19. 36, 87. 50]
694 [- 18. 51, 87. 00]
695 [- 17. 72, 86. 50]
696 [- 11. 95, 85. 24]
697 [- 0. 11, 85. 12]
698 [ 11. 49, 85. 20]
699 [ 17. 72, 86. 50]
700 [ 19. 74, 87. 00]
701 [ 21. 22, 87. 50]
702 [ 22. 68, 88. 00]
703 [ 24. 28, 88. 50]
704 [ 26. 79, 89. 00]
705 [ 71. 98, 90. 00]
706 [ 80. 62, 90. 50]
707 *%-----|-----|
708 *#*****|*****|
709 *# Catchment MLLS
710 *# - To SWM Facility north of the Jock
711 *# - Primarily residential development
712 *#*****|*****|
713 CONTINUOUS STANDHYD I D=[ 2], NHYD=[" MLLS" ], DT=[ 5] mi n, AREA=[ 139] ( ha),
714 XI MP=[ 0. 38], TI MP=[ 0. 38], DWF=[ 0] ( cms), LOSS=[ 2],
715 SCS curve number CN=[ 74],
716 Pervious surfaces: I Aper=[ 4. 67] ( mm), SLPP=[ 1] ( %),
717 LGP=[ 40] ( m), MNP=[ 0. 25], SCP=[ 0] ( mi n),
718 Impervious surfaces: I Ai mp=[ 1. 57] ( mm), SLPI=[ 1] ( %),
719 LGI=[ 963] ( m), MNI=[ 0. 013], SCI=[ 0] ( mi n),
720 Continuous simulation parameters:
721 I aRECper=[ 4] ( hrs), I aRECI mp=[ 4] ( hrs),
722 SM N=[ -1] ( mm), SMAX=[ -1] ( mm), SK=[ 0. 010] / ( mm),
723 I nter Event Ti me=[ 18] ( hrs), END=- 1
724
725 *%-----|-----|
726 *#*****|*****|

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727  *#      Chapman Mills SWM Pond
728  *#      - Rating curve obtained from CCL hydraulic modeling
729  *#*****
730  ROUTE RESERVOIR      I Dout =[ 5],      NHYD=[ "M LL_P" ],      I Di n=[ 2],
731                      RDT=[ 5] (mi n),
732                      TABLE of ( OUTFLOW STORAGE ) values
733                      ( cms ) - ( ha- m)
734                      [ 0. 0 , 0. 0 ]
735                      [ 0. 01 , 0. 01]
736                      [ 0. 05 , 0. 06]
737                      [ 0. 09 , 0. 11]
738                      [ 0. 13 , 0. 15]
739                      [ 0. 18 , 0. 19]
740                      [ 0. 28 , 0. 28]
741                      [ 0. 37 , 0. 34]
742                      [ 0. 45 , 0. 40]
743                      [ 0. 51 , 0. 44]
744                      [ 0. 56 , 0. 47]
745                      [ 0. 64 , 0. 52]
746                      [ 0. 76 , 0. 59]
747                      [ 0. 86 , 0. 65]
748                      [ 1. 09 , 0. 78]
749                      [ 1. 44 , 0. 96]
750                      [ 3. 18 , 1. 84]
751                      [ 4. 05 , 2. 31]
752                      [ -1 , -1 ] (max twenty pts)
753                      I Dovf =[ 4],      NHYDovf=[ "M L- OV" ]
754  *%-----|-----|
755  ADD HYD              I Dsum=[ 3 ],      NHYD=[ "SN_M" ],      I Ds to add=[ 1, 4, 5]
756  *%-----|-----|
757  SAVE HYD            I D=[ 3 ],      # OF PCYCLES=[ -1],      I CASEsh=[ 1]
758                      HYD_COMMENT=[ "Tot al Fl ows at Jockvale Road" ]
759  *%-----|-----|
760  *#
761  *# Hydrograph from Jockvale Road routed to Heart's Desire
762  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 689
763  *#
764  ROUTE CHANNEL      I Dout =[ 1],      NHYD=[ "N_DE" ] , I Di n=[ 3] ,
765                      RDT=[ 5] (mi n),
766                      CHLGTH=[ 1962] ( m),      CHSLOPE=[ 0. 2227] ( %),
767                      FPSLOPE=[ 0. 2227] ( %),
768                      SECNUM=[ 1. 0],      NSEG=[ 3]
769                      ( SEGROUGH, SEGDI ST ( m) ) =
770                      [ 0. 075, -17. 56
771                      -0. 045, 18. 27
772                      0. 075, 67. 59] NSEG times
773                      ( DI STANCE ( m), ELEVATI ON ( m) ) =
774                      [ -111. 59, 88. 00]
775                      [ -102. 58, 87. 50]
776                      [ -96. 20, 87. 00]
777                      [ -90. 04, 86. 50]
778                      [ -84. 02, 86. 00]
779                      [ -77. 54, 85. 50]
780                      [ -54. 07, 85. 00]
781                      [ -39. 43, 84. 50]
782                      [ -28. 30, 84. 00]
783                      [ -24. 12, 83. 50]
784                      [ -22. 30, 83. 00]
785                      [ -20. 55, 82. 50]
786                      [ -17. 56, 82. 00]
787                      [ -12. 63, 81. 22]
788                      [ -0. 11, 80. 75]
789                      [ 11. 55, 81. 22]
790                      [ 18. 27, 82. 00]
791                      [ 19. 82, 82. 50]
792                      [ 22. 48, 83. 00]

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793 [27. 90, 83. 50]
794 [29. 31, 84. 00]
795 [30. 81, 84. 50]
796 [32. 51, 85. 00]
797 [34. 24, 85. 50]
798 [36. 34, 86. 00]
799 [41. 65, 86. 50]
800 [62. 64, 87. 00]
801 [65. 14, 87. 50]
802 [67. 59, 88. 00]

803 *%-----|-----|
804 *#*****|

805 *# Catchment DESIRE
806 *# - To Jock River (north of the Jock)
807 *# - Rural-estate subdivision (Heart's Desire Community)
808 *#*****|

809 CONTINUOUS STANDHYD ID=[2], NHYD=["DESIRE"], DT=[5] min, AREA=[24] (ha),
810 XI MP=[0. 25], TI MP=[0. 25], DWF=[0] (cms), LOSS=[2],
811 SCS curve number CN=[77],
812 Pervious surfaces: IAper=[4. 67] (mm), SLPP=[1] (%),
813 LGP=[40] (m), MNP=[0. 25], SCP=[0] (min),
814 Impervious surfaces: IAimp=[1. 57] (mm), SLPI=[1] (%),
815 LGI=[400] (m), MNI=[0. 013], SCI=[0] (min),
816 Continuous simulation parameters:
817 IaRECper=[4] (hrs), IaRECImp=[4] (hrs),
818 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
819 InterEventTime=[18] (hrs), END=- 1

821 *%-----|-----|
822 *#*****|

823 *# Catchment JOCKVA
824 *# - To Jockvale SWM Facility
825 *# - Residential development & golf course
826 *#*****|

827 CONTINUOUS STANDHYD ID=[3], NHYD=["JOCKVA"], DT=[5] min, AREA=[252] (ha),
828 XI MP=[0. 50], TI MP=[0. 50], DWF=[0] (cms), LOSS=[2],
829 SCS curve number CN=[74],
830 Pervious surfaces: IAper=[4. 67] (mm), SLPP=[1] (%),
831 LGP=[40] (m), MNP=[0. 25], SCP=[0] (min),
832 Impervious surfaces: IAimp=[1. 57] (mm), SLPI=[1] (%),
833 LGI=[1296] (m), MNI=[0. 013], SCI=[0] (min),
834 Continuous simulation parameters:
835 IaRECper=[4] (hrs), IaRECImp=[4] (hrs),
836 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
837 InterEventTime=[18] (hrs), END=- 1

839 *%-----|-----|
840 *#*****|

841 *# Jockvale SWM Facility
842 *# - Rating curve obtained from Jockvale Servicing Study (CCL 1999)
843 *#*****|

844 ROUTE RESERVOIR IDout=[5], NHYD=["JOCK_P"], IDin=[3],
845 RDT=[5] (min),
846 TABLE of (OUTFLOW STORAGE) values

847 (cms) - (ha-m)
848 [0. 0 , 0. 0]
849 [0. 27 , 0. 03]
850 [0. 28 , 0. 55]
851 [0. 29 , 1. 14]
852 [0. 30 , 1. 80]
853 [0. 31 , 2. 32]
854 [1. 12 , 2. 87]
855 [2. 92 , 3. 45]
856 [4. 64 , 4. 07]
857 [6. 69 , 4. 72]
858 [9. 02 , 5. 39]

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859             [ 11.62 , 6.10]
860             [ 14.42 , 6.85]
861             [ 17.45 , 7.62]
862             [ 20.69 , 8.44]
863             [ 24.08 , 9.28]
864             [ 27.68 , 10.17]
865             [ -1 , -1 ] (max twenty pts)
866             IDovf=[4], NHYDovf=["JO-OVF"]
867 *%-----|-----|
868 ADD HYD           IDsum=[ 3 ], NHYD=["SN_DE"], IDs to add=[1,2,4,5]
869 *%-----|-----|
870 SAVE HYD         ID=[ 3 ], # OF PCYCLES=[-1], ICASEsh=[1]
871                 HYD_COMMENT=["Total Flows at Heart's Desire"]
872 *%-----|-----|
873 *#
874 *# Hydrograph from Heart's Desire routed to Rideau River
875 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 0
876 *#
877 ROUTE CHANNEL    IDout=[1], NHYD=["NI"], IDin=[3],
878                 RDT=[5](min),
879                 CHLGTH=[563](m), CHSLOPE=[0.9668](%),
880                                     FPSLOPE=[0.9668](%),
881                 SECNUM=[1.0], NSEG=[3]
882                 ( SEGROUGH, SEGDIST (m) )=
883                   [0.075, -30.20
884                   -0.045, 30.20
885                   0.075, 168.81] NSEG times
886                 ( DISTANCE (m), ELEVATION (m) )=
887                 [-170.17, 86.00]
888                 [-164.75, 85.50]
889                 [-158.08, 85.00]
890                 [-113.12, 82.00]
891                 [-98.46, 81.50]
892                 [-92.24, 81.00]
893                 [-86.88, 80.50]
894                 [-81.54, 80.00]
895                 [-74.36, 79.50]
896                 [-63.54, 79.00]
897                 [-39.23, 78.50]
898                 [-34.51, 78.00]
899                 [-33.01, 77.50]
900                 [-30.20, 77.00]
901                 [-13.42, 76.18]
902                 [-1.14, 76.09]
903                 [17.06, 76.18]
904                 [30.20, 77.00]
905                 [32.95, 77.50]
906                 [34.06, 78.00]
907                 [35.11, 78.50]
908                 [36.32, 79.00]
909                 [37.74, 79.50]
910                 [48.48, 81.50]
911                 [49.25, 82.00]
912                 [55.61, 84.50]
913                 [57.09, 85.00]
914                 [59.51, 85.50]
915                 [64.34, 86.00]
916                 [66.30, 86.00]
917                 [76.71, 86.50]
918                 [101.83, 86.50]
919                 [119.73, 87.00]
920                 [142.04, 87.50]
921                 [168.81, 88.00]
922 *%-----|-----|
923 *#*****
924 *# Cat chment S-2

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925 *# - To Jock River (north and south)
926 *# - Undeveloped floodplain and river
927 *#*****
928 CONTINUOUS NASHYD ID=[ 2], NHYD=["S-2"], DT=[ 5] min, AREA=[ 102] (ha),
929 DWF=[ 0] (cms), CNVC=[ 72], IA=[ 4.67] (mm),
930 N=[ 3], TP=[ 0.40] hrs,
931 Continuous simulation parameters:
932 IaRECper=[ 4] (hrs),
933 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010]/(mm),
934 InterEventTime=[ 12] (hrs)
935 Baseflow simulation parameters:
936 BaseFlowOption=[ 1],
937 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/day/mm)
938 VHydCond=[ 0.055] (mm/hr), END=- 1
939
940 *%-----|-----
941 ADD HYD IDsum=[ 3 ], NHYD=["SN_NI"], IDs to add=[ 1,2]
942 *%-----|-----
943 SAVE HYD ID=[ 3 ], # OF PCYCLES=[ -1], ICASEsh=[ 1]
944 HYD_COMMENT=["Total Flows at Rideau River"]
945 *%-----|-----
946 *% 5 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
947 START TZERO=[ 0.0], METOUT=[ 2], NSTORM=[ 1], NRUN=[ 005]
948 *% ["C24SC005.stm"] <--storm filename, one per line for NSTORMtime
949 *%-----|-----
950 *% 10 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
951 *%START TZERO=[ 0.0], METOUT=[ 2], NSTORM=[ 1], NRUN=[ 010]
952 *% ["C24SC010.stm"] <--storm filename, one per line for NSTORMtime
953 *%-----|-----
954 *% 25 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
955 START TZERO=[ 0.0], METOUT=[ 2], NSTORM=[ 1], NRUN=[ 025]
956 *% ["C24SC025.stm"] <--storm filename, one per line for NSTORMtime
957 *%-----|-----
958 *% 50 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
959 *%START TZERO=[ 0.0], METOUT=[ 2], NSTORM=[ 1], NRUN=[ 050]
960 *% ["C24SC050.stm"] <--storm filename, one per line for NSTORMtime
961 *%-----|-----
962 *% 100 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
963 START TZERO=[ 0.0], METOUT=[ 2], NSTORM=[ 1], NRUN=[ 100]
964 *% ["C24SC100.stm"] <--storm filename, one per line for NSTORMtime
965 *%-----|-----
966
967 *#####
968 FINISH
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00749 # 09:04:04P 359.57 18.63 N6_date 28:20 34.02 n/a
00750 # [ID# 5.00] SLM# 03:SN OK 53477.01 68.150 N6_date 34:05 18.44 n/a
00751 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00752 # SVAE IVD .....01:N,P,O 53477.01 68.124 N6_date 34:05 18.44 n/a
00753 # frame :C:\Navit\OCTOBE-1\CONTIN-1\SMR_POSTH-H-SN_OK.005
00754 # remark:Total Flow at Keefer Drain
00755 #
00756 # Hydrograph from Node Keefer routed to Node at Foster Drain
00757 # Channel X-Section obtained from RCVA Hydraulic Model - Station 6215
00758 #
00759 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00760 # ROUTE CHANNEL -> 03:SN OK 53477.01 68.150 N6_date 34:05 18.44 n/a
00761 # [IRD# 5.00] out<: 01:N,P,O 53477.01 68.124 N6_date 34:20 18.44 n/a
00762 # [L/S/m= 1181.07/ 0.01/ 0.05]
00763 # [Vmax= 1.826 Dmax= 0.05]
00764 #
00765 # Catchment FOSTER
00766 # - To Foster ditch (north of the Jack)
00767 # - Partially developed (medium density); remaining agricultural
00768 #
00769 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00770 # CONTINUOUS STANDHDDZ:FOSTER 373.00 20.654 N6_date 28:10 37.71.660
00771 # [L/S/m= 55.71/MP= 55]
00772 # [L/S# 2 - C#n 74.0]
00773 # [Pervious area: IPer= 4.67:SLP= 0.0; LCP= 40.0; MNP= 250; SCP= 0]
00774 # [Impervious area: IImp= 1.57:SLP= 0.0; LCP= 140.0; MNP= 0.13; SCL= 0]
00775 # [IARECmp= 4.00; IAREPer= 4.00]
00776 # [SMN= 36.67; SMM= 244.49; SK= 0.01]
00777 #
00778 # Foster Pond
00779 # - Rating curve obtained assuming 40m/ha in 24 hours for quality control
00780 # and a ratio of the catchment area to the West Clarke pond rating curve
00781 #
00782 #
00783 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00784 # ROUTE RESERVOIR -> 02:FOSTER 373.00 20.654 N6_date 28:10 37.71 n/a
00785 # [IRD# 5.00] out<: 04:P,FB 79.61 200.00 N6_date 26:45 37.71 n/a
00786 # [RTE 5.00] out<: 09:FOF 293.39 20.155 N6_date 28:15 37.71 n/a
00787 # [MS otIed= 1720E+01; Tot Of Vol= 1106E+01; N Of = 2; Tot Dur Of= 14 hrs]
00788 # [L/S/m= 280.7 / 0.03 / 0.45]
00789 # [Vmax= 771 Dmax= 2.8]
00790 #
00791 # ADD IVD .....01:N,P,O 53477.01 68.124 N6_date 34:20 18.44 n/a
00792 # [RD# 5.00] out<: 04:P,FB 79.61 200.00 N6_date 26:45 37.71 n/a
00793 # + 09:FOF 293.39 20.155 N6_date 28:15 37.71 n/a
00794 # [ID# 5.00] SLM# 03:SN FO 53850.01 68.977 N6_date 34:20 18.57 n/a
00795 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00796 # SVAE IVD .....03:SN FO 53850.01 68.977 N6_date 34:20 18.57 n/a
00797 # frame :C:\Navit\OCTOBE-1\CONTIN-1\SMR_POSTH-H-SN_FO.005
00798 # remark:Total Flow at Foster Drain
00799 #
00800 # Hydrograph from Node Foster routed to Node at Cedevard Road
00801 # Channel X-Section obtained from RCVA Hydraulic Model - Station 6016
00802 #
00803 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00804 # CONTINUOUS STANDHDDZ:FOSTER 373.00 20.654 N6_date 28:10 37.71 n/a
00805 # [L/S/m= 159.7 / 0.02 / 0.05]
00806 # [Vmax= 3.197 Dmax= 0.1]
00807 #
00808 # Catchment S 1
00809 # - To Jack River (north and south of Jack)
00810 # - Primarily agricultural fields; portion of sand quarry
00811 #
00812 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00813 # CONTINUOUS STANDHDDZ:S 2.5 245.00 2.163 N6_date 29:10 21.69.380
00814 # [L/S# 7.0 - C#n 3.00]
00815 # [Pervious area: IPer= 4.00:SLP= 0.0; LCP= 40.0; MNP= 250; SCP= 0]
00816 # [Impervious area: IImp= 1.57:SLP= 0.0; LCP= 140.0; MNP= 0.13; SCL= 0]
00817 # [IARECmp= 4.00; IAREPer= 4.00]
00818 # [SMN= 33.81; SMM= 225.45; SK= 0.01]
00819 #
00820 # [ID# 5.00] SLM# 03:SN CE 54095.01 69.514 N6_date 34:15 18.58 n/a
00821 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00822 # SVAE IVD .....03:SN CE 54095.01 69.514 N6_date 34:15 18.58 n/a
00823 # frame :C:\Navit\OCTOBE-1\CONTIN-1\SMR_POSTH-H-SN_CE.005
00824 # remark:Total Flow at Cedarvale Pond
00825 #
00826 # Hydrograph from Node Cedevard Road routed to Node at West Clarke Drain
00827 # Channel X-Section obtained from RCVA Hydraulic Model - Station 5002
00828 #
00829 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00830 # ROUTE CHANNEL -> 03:SN CE 54095.01 69.514 N6_date 34:15 18.58 n/a
00831 # [IRD# 5.00] out<: 01:N,M 54095.01 69.495 N6_date 34:25 18.58 n/a
00832 # [L/S/m= 825.7 / 0.01 / 0.05]
00833 # [Vmax= 2.82 Dmax= 0.01]
00834 #
00835 # Catchment WCLAR
00836 # - To West Clarke Drain (south of the Jack)
00837 # - Subdivision with 43% imp. as per Barhaven South MS
00838 #
00839 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00840 # CONTINUOUS STANDHDDZ:WCLAR 243.00 13.629 N6_date 28:05 33.48.586
00841 # [L/S# 43.71/MP= 43]
00842 # [Pervious area: IPer= 4.67:SLP= 0.0; LCP= 40.0; MNP= 250; SCP= 0]
00843 # [Impervious area: IImp= 1.57:SLP= 0.0; LCP= 140.0; MNP= 0.13; SCL= 0]
00844 # [IARECmp= 4.00; IAREPer= 4.00]
00845 # [SMN= 33.81; SMM= 225.45; SK= 0.01]
00846 #
00847 # [ID# 5.00] SLM# 03:SN WCL 54338.01 70.010 N6_date 34:25 18.65 n/a
00848 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00849 # SVAE IVD .....04:SN WCL 54338.01 70.010 N6_date 34:25 18.65 n/a
00850 # frame :C:\Navit\OCTOBE-1\CONTIN-1\SMR_POSTH-H-SN_WCL.005
00851 # remark:Total Flow at West Clarke Pond Outlet
00852 #
00853 # Hydrograph from Node West Clarke Pond routed to Node at Kennedy - Burnett Drain
00854 # Channel X-Section obtained from RCVA Hydraulic Model - Station 4534
00855 #
00856 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00857 # ROUTE CHANNEL -> 04:SN WCL 54338.01 70.010 N6_date 34:25 18.65 n/a
00858 # [IRD# 5.00] out<: 01:N,M 54338.01 69.990 N6_date 34:30 18.65 n/a
00859 # [L/S/m= 1962.7 / 223 / 0.45]
00860 # [Vmax= 946 Dmax= 2.660]
00861 #
00862 # Catchment KEN_BU
00863 # - To Kennedy-Burnett SWM Facility
00864 # - Outlets to Fraser-Clarke Drain (north of the Jack)
00865 # - Medium density residential
00866 #
00867 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00868 # CONTINUOUS STANDHDDZ:KEN_BU 281.00 18.799 N6_date 28:05 37.13.650
00869 # [L/S# 25.71/MP= 55]
00870 # [L/S# 2 - C#n 71.0]
00871 # [Pervious area: IPer= 4.67:SLP= 0.0; LCP= 40.0; MNP= 250; SCP= 0]
00872 # [Impervious area: IImp= 1.57:SLP= 0.0; LCP= 140.0; MNP= 0.13; SCL= 0]
00873 # [IARECmp= 4.00; IAREPer= 4.00]
00874 # [SMN= 41.38; SMM= 275.84; SK= 0.01]
00875 #
00876 # [ID# 5.00] SLM# 04:SN BU 54709.01 71.220 N6_date 34:10 18.76 n/a
00877 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00878 # SVAE IVD .....05:SN BU 54709.01 71.220 N6_date 34:10 18.76 n/a
00879 # frame :C:\Navit\OCTOBE-1\CONTIN-1\SMR_POSTH-H-SN_BU.005
00880 # remark:Total Flow at Ken Burnett Drain
00881 # Hydrograph from Node Kennedy - Burnett Drain to Node Todd Drain
00882 # Channel X-Section obtained from RCVA Hydraulic Model - Station 3633
00883 #
00884 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00885 # CONTINUOUS STANDHDDZ:FRASER 90.00 4.131 N6_date 28:05 28.74.503
00886 # [L/S# 25.71/MP= 55]
00887 # [L/S# 2 - C#n 80.0]
00888 # [Pervious area: IPer= 4.67:SLP= 0.0; LCP= 40.0; MNP= 250; SCP= 0]
00889 # [Impervious area: IImp= 1.57:SLP= 0.0; LCP= 140.0; MNP= 0.13; SCL= 0]
00890 # [IARECmp= 4.00; IAREPer= 4.00]
00891 # [SMN= 26.32; SMM= 175.84; SK= 0.01]
00892 #
00893 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00894 # ROUTE RESERVOIR -> 07:FRASER 90.00 4.131 N6_date 28:05 28.74 n/a
00895 # [IRD# 5.00] out<: 08:ML,P 20.53 0.00 N6_date 27:45 28.74 n/a
00896 # [RTE 5.00] out<: 09:P,FOF 69.47 4.131 N6_date 28:05 28.74 n/a
00897 # [MS otIed= 3600E+00; Tot Of Vol= 1997E+01; N Of = 2; Tot Dur Of= 13 hrs]
00898 # [L/S/m= 50.7 / 0.01 / 0.05]
00899 # [Vmax= 100.71 Dmax= 0.1]
00900 #
00901 # [ID# 5.00] SLM# 04:SN BU 54709.01 71.220 N6_date 34:10 18.76 n/a
00902 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00903 # SVAE IVD .....05:SN BU 54709.01 71.220 N6_date 34:10 18.76 n/a
00904 # frame :C:\Navit\OCTOBE-1\CONTIN-1\SMR_POSTH-H-SN_BU.005
00905 # remark:Total Flow at Ken Burnett Drain
00906 # Hydrograph from Node Kennedy - Burnett Drain to Node Todd Drain
00907 # Channel X-Section obtained from RCVA Hydraulic Model - Station 3633
00908 #
00909 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00910 # CONTINUOUS STANDHDDZ:FRASER 90.00 4.131 N6_date 28:05 28.74.503
00911 # [L/S# 25.71/MP= 55]
00912 # [L/S# 2 - C#n 80.0]
00913 # [Pervious area: IPer= 4.67:SLP= 0.0; LCP= 40.0; MNP= 250; SCP= 0]
00914 # [Impervious area: IImp= 1.57:SLP= 0.0; LCP= 140.0; MNP= 0.13; SCL= 0]
00915 # [IARECmp= 4.00; IAREPer= 4.00]
00916 # [SMN= 26.32; SMM= 175.84; SK= 0.01]
00917 #
00918 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00919 # ROUTE RESERVOIR -> 07:FRASER 90.00 4.131 N6_date 28:05 28.74 n/a
00920 # [IRD# 5.00] out<: 08:ML,P 20.53 0.00 N6_date 27:45 28.74 n/a
00921 # [RTE 5.00] out<: 09:P,FOF 69.47 4.131 N6_date 28:05 28.74 n/a
00922 # [MS otIed= 3600E+00; Tot Of Vol= 1997E+01; N Of = 2; Tot Dur Of= 13 hrs]
00923 # [L/S/m= 50.7 / 0.01 / 0.05]
00924 # [Vmax= 100.71 Dmax= 0.1]
00925 #
00926 # [ID# 5.00] SLM# 04:SN BU 54709.01 71.220 N6_date 34:10 18.76 n/a
00927 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00928 # SVAE IVD .....05:SN BU 54709.01 71.220 N6_date 34:10 18.76 n/a
00929 # frame :C:\Navit\OCTOBE-1\CONTIN-1\SMR_POSTH-H-SN_BU.005
00930 # remark:Total Flow at Ken Burnett Drain
00931 # Hydrograph from Node Kennedy - Burnett Drain to Node Todd Drain
00932 # Channel X-Section obtained from RCVA Hydraulic Model - Station 3633
00933 #
00934 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00935 # CONTINUOUS STANDHDDZ:FRASER 90.00 4.131 N6_date 28:05 28.74.503
00936 # [L/S# 25.71/MP= 55]
00937 # [L/S# 2 - C#n 80.0]
00938 # [Pervious area: IPer= 4.67:SLP= 0.0; LCP= 40.0; MNP= 250; SCP= 0]
00939 # [Impervious area: IImp= 1.57:SLP= 0.0; LCP= 140.0; MNP= 0.13; SCL= 0]
00940 # [IARECmp= 4.00; IAREPer= 4.00]
00941 # [SMN= 26.32; SMM= 175.84; SK= 0.01]
00942 #
00943 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00944 # ROUTE RESERVOIR -> 07:FRASER 90.00 4.131 N6_date 28:05 28.74 n/a
00945 # [IRD# 5.00] out<: 08:ML,P 20.53 0.00 N6_date 27:45 28.74 n/a
00946 # [RTE 5.00] out<: 09:P,FOF 69.47 4.131 N6_date 28:05 28.74 n/a
00947 # [MS otIed= 3600E+00; Tot Of Vol= 1997E+01; N Of = 2; Tot Dur Of= 13 hrs]
00948 # [L/S/m= 50.7 / 0.01 / 0.05]
00949 # [Vmax= 100.71 Dmax= 0.1]
00950 #
00951 # [ID# 5.00] SLM# 04:SN BU 54709.01 71.220 N6_date 34:10 18.76 n/a
00952 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00953 # SVAE IVD .....05:SN BU 54709.01 71.220 N6_date 34:10 18.76 n/a
00954 # frame :C:\Navit\OCTOBE-1\CONTIN-1\SMR_POSTH-H-SN_BU.005
00955 # remark:Total Flow at Ken Burnett Drain

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00956 # Catchment TODD
00957 # - To Todd Drain (south of the Jack)
00958 # - Subdivision with 43% imp. as per Barhaven South MS
00959 #
00960 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00961 # CONTINUOUS STANDHDDZ:TODD 195.00 11.301 N6_date 28:05 34.02.596
00962 # [L/S# 43.71/MP= 43]
00963 # [Pervious area: IPer= 4.67:SLP= 0.0; LCP= 40.0; MNP= 250; SCP= 0]
00964 # [Impervious area: IImp= 1.57:SLP= 0.0; LCP= 140.0; MNP= 0.13; SCL= 0]
00965 # [IARECmp= 4.00; IAREPer= 4.00]
00966 # [SMN= 31.15; SMM= 207.66; SK= 0.01]
00967 #
00968 # Total Pond 3
00969 # - Rating curve obtained from Barhaven South MS modeling
00970 # - Tributary Drainage Area to MS Pond 3 = 150 ha
00971 #
00972 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00973 # ROUTE RESERVOIR -> 03:TODD 195.00 11.301 N6_date 28:05 34.02 n/a
00974 # [IRD# 5.00] out<: 02:ML,P 37.74 0.00 N6_date 26:50 34.02 n/a
00975 # [RTE 5.00] out<: 09:FOF 157.26 11.301 N6_date 28:10 34.02 n/a
00976 # [MS otIed= 7800E+00; Tot Of Vol= 5350E+01; N Of = 2; Tot Dur Of= 14 hrs]
00977 # [L/S/m= 280.7 / 0.03 / 0.45]
00978 # [Vmax= 771 Dmax= 2.8]
00979 #
00980 # [ID# 5.00] SLM# 01:SN TO 54904.01 70.805 N6_date 35:15 18.76 n/a
00981 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00982 # SVAE IVD .....01:SN TO 54904.01 70.805 N6_date 35:15 18.76 n/a
00983 # frame :C:\Navit\OCTOBE-1\CONTIN-1\SMR_POSTH-H-SN_TO.005
00984 # remark:Total Flow at Todd Drain
00985 #
00986 # Hydrograph from Todd Drain routed to Corrigan Drain
00987 # Channel X-Section obtained from RCVA Hydraulic Model - Station 2462
00988 #
00989 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
00990 # CONTINUOUS STANDHDDZ:CORRIG 149.00 9.766 N6_date 28:05 34.78.609
00991 # [L/S# 45.71/MP= 45]
00992 # [L/S# 2 - C#n 70.0]
00993 # [Pervious area: IPer= 4.67:SLP= 0.0; LCP= 40.0; MNP= 250; SCP= 0]
00994 # [Impervious area: IImp= 1.57:SLP= 0.0; LCP= 140.0; MNP= 0.13; SCL= 0]
00995 # [IARECmp= 4.00; IAREPer= 4.00]
00996 # [SMN= 31.15; SMM= 207.66; SK= 0.01]
00997 #
00998 # Corrigan Pond 1
00999 # - Rating curve obtained from Barhaven South MS modeling
01000 # - Tributary Drainage Area to MS Pond = 145 ha
01001 #
01002 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
01003 # ROUTE RESERVOIR -> 02:CORRIG 149.00 9.766 N6_date 28:05 34.78 n/a
01004 # [IRD# 5.00] out<: 05:ML,P 139.00 2.516 N6_date 28:40 30.98 n/a
01005 # [RTE 5.00] out<: 04:ML,O 121.35 9.684 N6_date 28:05 34.78 n/a
01006 # [MS otIed= 5799E+00; Tot Of Vol= 4220E+01; N Of = 3; Tot Dur Of= 14 hrs]
01007 # [L/S/m= 280.7 / 0.03 / 0.45]
01008 # [Vmax= 771 Dmax= 2.8]
01009 #
01010 # [ID# 5.00] SLM# 01:SN CO 54904.01 71.106 N6_date 35:40 18.82 n/a
01011 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
01012 # SVAE IVD .....01:SN CO 54904.01 71.106 N6_date 35:40 18.82 n/a
01013 # frame :C:\Navit\OCTOBE-1\CONTIN-1\SMR_POSTH-H-SN_CO.005
01014 # remark:Total Flow at Corrigan Drain
01015 #
01016 # Hydrograph from Corrigan Drain routed to Jockvale Road
01017 # Channel X-Section obtained from RCVA Hydraulic Model - Station 2462
01018 #
01019 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
01020 # ROUTE CHANNEL -> 03:SN CO 54904.01 71.106 N6_date 35:40 18.82 n/a
01021 # [IRD# 5.00] out<: 01:N,M 55053.00 71.427 N6_date 35:45 18.86 n/a
01022 # [L/S/m= 580.4 / 0.01 / 0.05]
01023 # [Vmax= 1.654 Dmax= 1.485]
01024 #
01025 # Catchment MLLS
01026 # - To SWM Facility north of the Jack
01027 # - Primarily residential
01028 #
01029 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
01030 # CONTINUOUS STANDHDDZ:MLLS 139.00 7.873 N6_date 28:05 30.98.542
01031 # [L/S# 38.71/MP= 38]
01032 # [L/S# 2 - C#n 74.0]
01033 # [Pervious area: IPer= 4.67:SLP= 0.0; LCP= 40.0; MNP= 250; SCP= 0]
01034 # [Impervious area: IImp= 1.57:SLP= 0.0; LCP= 140.0; MNP= 0.13; SCL= 0]
01035 # [IARECmp= 4.00; IAREPer= 4.00]
01036 # [SMN= 36.67; SMM= 244.49; SK= 0.01]
01037 #
01038 # Chapman Mills SWM Pond
01039 # - Rating curve obtained from CCL hydraulic modeling
01040 # - Tributary Drainage Area to MS Pond = 145 ha
01041 #
01042 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
01043 # ROUTE RESERVOIR -> 02:MLLS 139.00 7.873 N6_date 28:05 30.98 n/a
01044 # [IRD# 5.00] out<: 05:ML,P 139.00 2.516 N6_date 28:40 30.98 n/a
01045 # [RTE 5.00] out<: 04:ML,O 121.35 9.684 N6_date 28:05 34.78 n/a
01046 # [MS otIed= 1500E+00; Tot Of Vol= 0.000E+00; N Of = 0; Tot Dur Of= 0 hrs]
01047 # [L/S/m= 139.00 7.873 N6_date 28:40 30.98 n/a]
01048 # [Vmax= 100.71 Dmax= 0.1]
01049 #
01050 # [ID# 5.00] SLM# 03:SN ML 55192.00 71.786 N6_date 35:45 18.89 n/a
01051 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
01052 # SVAE IVD .....03:SN ML 55192.00 71.786 N6_date 35:45 18.89 n/a
01053 # frame :C:\Navit\OCTOBE-1\CONTIN-1\SMR_POSTH-H-SN_ML.005
01054 # remark:Total Flow at Jockvale Road
01055 #
01056 # Hydrograph from Jockvale Road routed to Heart's Desire
01057 # Channel X-Section obtained from RCVA Hydraulic Model - Station 689
01058 #
01059 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
01060 # CONTINUOUS STANDHDDZ:HEART 252.00 15.852 N6_date 28:05 35.73.626
01061 # [L/S# 50.71/MP= 50]
01062 # [L/S# 2 - C#n 74.0]
01063 # [Pervious area: IPer= 4.67:SLP= 0.0; LCP= 40.0; MNP= 250; SCP= 0]
01064 # [Impervious area: IImp= 1.57:SLP= 0.0; LCP= 140.0; MNP= 0.13; SCL= 0]
01065 # [IARECmp= 4.00; IAREPer= 4.00]
01066 # [SMN= 36.67; SMM= 244.49; SK= 0.01]
01067 #
01068 # Catchment RESER
01069 # - To Jack River (north of the Jack)
01070 # - Rural-estate subdivision (Heart's Desire Community)
01071 #
01072 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
01073 # CONTINUOUS STANDHDDZ:RESER 24.00 1.289 N6_date 28:00 27.22.477
01074 # [L/S# 25.71/MP= 25]
01075 # [L/S# 2 - C#n 73.0]
01076 # [Pervious area: IPer= 4.67:SLP= 0.0; LCP= 40.0; MNP= 250; SCP= 0]
01077 # [Impervious area: IImp= 1.57:SLP= 0.0; LCP= 140.0; MNP= 0.13; SCL= 0]
01078 # [IARECmp= 4.00; IAREPer= 4.00]
01079 # [SMN= 31.15; SMM= 207.66; SK= 0.01]
01080 #
01081 # [ID# 5.00] SLM# 03:SN RE 55468.00 72.143 N6_date 36:15 18.97 n/a
01082 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
01083 # SVAE IVD .....03:SN RE 55468.00 72.143 N6_date 36:15 18.97 n/a
01084 # frame :C:\Navit\OCTOBE-1\CONTIN-1\SMR_POSTH-H-SN_RE.005
01085 # remark:Total Flow at Heart's Desire routed to Riddan River
01086 # Hydrograph from Heart's Desire routed to Riddan River
01087 # Channel X-Section obtained from RCVA Hydraulic Model - Station 0
01088 #
01089 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
01090 # CONTINUOUS STANDHDDZ:JOCKVA 252.00 15.852 N6_date 28:05 35.73.626
01091 # [L/S# 50.71/MP= 50]
01092 # [L/S# 2 - C#n 74.0]
01093 # [Pervious area: IPer= 4.67:SLP= 0.0; LCP= 40.0; MNP= 250; SCP= 0]
01094 # [Impervious area: IImp= 1.57:SLP= 0.0; LCP= 140.0; MNP= 0.13; SCL= 0]
01095 # [IARECmp= 4.00; IAREPer= 4.00]
01096 # [SMN= 36.67; SMM= 244.49; SK= 0.01]
01097 #
01098 # Jockvale SWM Facility
01099 # - Rating curve obtained from Jockvale Servicing Study (CCL 1999)
01100 # - Residential development golf course
01101 #
01102 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
01103 # ROUTE RESERVOIR -> 03:JOCKVA 252.00 15.852 N6_date 28:05 35.73 n/a
01104 # [IRD# 5.00] out<: 05:FOCK,P 252.00 0.00 N6_date 36:20 0.00 n/a
01105 # [RTE 5.00] out<: 04:FO,OF 0.00 0.00 N6_date 0:00 0.00 n/a
01106 # [MS otIed= 3962E+01; Tot Of Vol= 0.000E+00; N Of = 0; Tot Dur Of= 0 hrs]
01107 # [L/S/m= 50.7 / 0.01 / 0.05]
01108 # [Vmax= 100.71 Dmax= 0.1]
01109 #
01110 # [ID# 5.00] SLM# 03:SN JO 55468.00 72.143 N6_date 36:15 18.97 n/a
01111 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
01112 # SVAE IVD .....03:SN JO 55468.00 72.143 N6_date 36:15 18.97 n/a
01113 # frame :C:\Navit\OCTOBE-1\CONTIN-1\SMR_POSTH-H-SN_JO.005
01114 # remark:Total Flow at Heart's Desire routed to Riddan River
01115 # Hydrograph from Heart's Desire routed to Riddan River
01116 # Channel X-Section obtained from RCVA Hydraulic Model - Station 0
01117 #
01118 # 05:00:12:1D NND# .....AREA .....QPEAK TpeaKtite hh:mm .....R.V.R.C.
01119 # CONTINUOUS STANDHDDZ:JOCKVA 252.00 15.852 N6_date 28:05 35.73.626
01120 # [L/S# 50.71/MP= 50]
01121 # [L/S# 2 - C#n 74.0]
01122 # [Pervious area: IPer= 4.67:SLP= 0.0; LCP= 40.0; MNP= 250; SCP= 0]
01123 # [Impervious area: IImp= 1.57:SLP= 0.0; LCP= 140.0; MNP= 0.13; SCL= 0]
01124 # [IARECmp= 4.00; IAREPer= 4.00]
01125 # [SMN= 36.67; SMM= 244.49; SK= 0.01]
01126 #
01127 # [ID# 5.00] SLM# 03:SN JO 55468.00 72.143 N6_date 36:15 18.97 n/a
01128 # 05:0
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014975 # Channel X-Section obtained from RCVA Hydraulic Model - Station 2462
014985 #
015000 025:0042-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
015005 ROUTE CHANNEL -> 03:SN 54904.01 111.061 No.date 28:05 29.29 n/a
015010 [RFD= 5.00] out< 01:N TO 54904.01 110.730 No.date 35:20 29.29 n/a
015020 [L/S=ma 280 / 037.045]
015030 [Vmax 7.17; Dmax 3.38]
015040 *****
015050 # Catchment CORKG
015060 # - To Corrigan Drain (south of the Joek)
015070 # Primarily developed (medium density)
015080 #
015090 025:0043-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
015100 CONTINUOUS STANDHDD2: CORKG 149.00 14.272 No.date 28:05 49.32 .663
015110 [Mx= 45.71; Mz= 45]
015120 [LRS= 2 Cn= 77.0]
015130 [Impervious area: IPer= 4.67; SLP= 0.0; LQ= 4.0; MNP= 250; SCP= 0]
015140 [Impervious area: IPer= 1.57; SLP= 0.0; LQ= 997.0; NN= 013; SCL= 0]
015150 [IARECmp= 4.00; IARECper= 4.00]
015160 [SMN= 31.15; SMM= 207.66; SKE= 010]
015170 [Vmax 2.709; Dmax 0.54]
015180 # Corrigan Pond 1
015190 # - Rating curve obtained from Burhaven South MS modeling
015200 # - Tributary Drainage Area to MS Pond 1 = 145 ha
015210 #
015220 025:0044-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
015230 ROUTE RESERVOIR -> 02: CORKG 149.00 14.272 No.date 28:05 49.32 n/a
015240 [RFD= 5.00] out< 05: M.P. 128.99 14.115 No.date 28:05 49.32 n/a
015250 [MS ovelow ca 04: IO O/P 128.99 14.115 No.date 28:05 49.32 n/a]
015260 [MS ovelow ca 04: P.O.P 128.99 14.115 No.date 28:05 49.32 n/a]
015270 025:0045-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
015280 ADD HDD 01: N TO 54904.01 110.730 No.date 35:20 29.29 n/a
015290 [RFD= 5.00] out< 01: N TO 54904.01 110.730 No.date 35:20 29.29 n/a
015300 [RFD= 5.00] out< 05: M.P. 128.99 14.115 No.date 28:05 49.32 n/a
015310 [RFD= 5.00] SLM 03: SN 55053.01 111.193 No.date 35:20 29.35 n/a
015320 025:0046-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
015330 SAGE H/D 03: SN 55192.01 111.709 No.date 35:20 29.38 n/a
015340 frame: C:\Navis\OCTOBE-1\CONTIN-I\SMR_POSTH.H.SN.CO.025
015350 remark: Total Flow at Corrigan Drain
015360 #
015370 # Hydrograph from Corrigan Drain routed to Joekvale
015380 # Channel X-Section obtained from RCVA Hydraulic Model - Station 2462
015390 #
015400 025:0047-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
015410 ROUTE CHANNEL -> 03: SN 55053.01 111.200 No.date 35:25 29.35 n/a
015420 [RFD= 5.00] out< 01: N TO 55053.01 111.200 No.date 35:25 29.35 n/a
015430 [L/S=ma 1.965; Dmax 1.852]
015440 [Vmax 1.965; Dmax 1.852]
015450 *****
015460 # Catchment MLLS
015470 # - To SWM Facility north of the Joek
015480 # Primarily residential development
015490 #
015500 025:0048-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
015510 CONTINUOUS STANDHDD2: MLLS 139.00 11.666 No.date 28:05 44.62 .600
015520 [Mx= 38.71; Mz= 38]
015530 [LRS= 2 Cn= 74.0]
015540 [Impervious area: IPer= 4.67; SLP= 0.0; LQ= 4.0; MNP= 250; SCP= 0]
015550 [Impervious area: IPer= 1.57; SLP= 0.0; LQ= 963.0; NN= 013; SCL= 0]
015560 [IARECmp= 4.00; IARECper= 4.00]
015570 [SMN= 36.67; SMM= 244.45; SKE= 010]
015580 [Vmax 2.709; Dmax 0.54]
015590 # Chappin Mills SWM Pond
015600 # - Rating curve obtained from CCL hydraulic modeling
015610 #
015620 025:0049-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
015630 ROUTE RESERVOIR -> 02: MLLS 139.00 11.666 No.date 28:05 44.62 n/a
015640 [RFD= 5.00] out< 05: M.L.P 139.00 3.765 No.date 28:40 44.62 n/a
015650 [RFD= 5.00] out< 04: M.L.P 139.00 3.765 No.date 28:40 44.62 n/a]
015660 [MS ovelow ca 04: M.L.P 139.00 3.765 No.date 28:40 44.62 n/a]
015670 025:0050-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
015680 ADD HDD 01: N TO 55053.01 111.200 No.date 35:25 29.35 n/a
015690 [RFD= 5.00] out< 01: N TO 55053.01 111.200 No.date 35:25 29.35 n/a
015700 [RFD= 5.00] out< 05: M.L.P 139.00 3.765 No.date 28:40 44.62 n/a
015710 [RFD= 5.00] SLM 03: SN 55192.01 111.709 No.date 35:25 29.38 n/a
015720 025:0051-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
015730 SAGE H/D 03: SN 55192.01 111.709 No.date 35:25 29.38 n/a
015740 frame: C:\Navis\OCTOBE-1\CONTIN-I\SMR_POSTH.H.SN.CO.025
015750 remark: Total Flow at Joekvale Road
015760 #
015770 # Hydrograph from Joekvale Road routed to Hart's Desire
015780 # Channel X-Section obtained from RCVA Hydraulic Model - Station 689
015790 #
015800 025:0052-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
015810 ROUTE CHANNEL -> 03: SN 55192.01 111.709 No.date 35:25 29.38 n/a
015820 [RFD= 5.00] out< 01: N TO 55192.01 111.156 No.date 36:05 29.38 n/a
015830 [L/S=ma 1.962; Dmax 1.852]
015840 [Vmax 1.962; Dmax 1.852]
015850 *****
015860 # Catchment KEERFE
015870 # - To Joek River (north of the Joek)
015880 # Residential subdivision (Hart's Desire Community)
015890 #
015900 025:0053-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
015910 CONTINUOUS STANDHDD2: KEERFE 242.00 24.912 No.date 28:00 40.77 .548
015920 [Mx= 25.71; Mz= 25]
015930 [LRS= 2 Cn= 77.0]
015940 [Impervious area: IPer= 4.67; SLP= 0.0; LQ= 4.0; MNP= 250; SCP= 0]
015950 [Impervious area: IPer= 1.57; SLP= 0.0; LQ= 400.0; NN= 013; SCL= 0]
015960 [IARECmp= 4.00; IARECper= 4.00]
015970 [SMN= 31.15; SMM= 207.66; SKE= 010]
015980 [Vmax 2.709; Dmax 0.54]
015990 # Catchment JOCKVA
016000 # - To Joekvale SWM Facility
016010 # - Residential development & golf course
016020 #
016030 025:0054-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
016040 CONTINUOUS STANDHDD2: JOCKVA 252.00 22.732 No.date 28:05 50.08 .673
016050 [Mx= 30.88; Mz= 30]
016060 [LRS= 2 Cn= 74.0]
016070 [Impervious area: IPer= 4.67; SLP= 0.0; LQ= 4.0; MNP= 250; SCP= 0]
016080 [Impervious area: IPer= 1.57; SLP= 0.0; LQ= 1296.0; NN= 013; SCL= 0]
016090 [IARECmp= 4.00; IARECper= 4.00]
016100 [SMN= 36.67; SMM= 244.45; SKE= 010]
016110 [Vmax 2.709; Dmax 0.54]
016120 # Joekvale SWM Facility
016130 # - Rating curve obtained from Joekvale Servicing Study (CCL 1999)
016140 #
016150 025:0055-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
016160 ROUTE RESERVOIR -> 03: JOCKVA 252.00 22.732 No.date 28:05 50.08 n/a
016170 [RFD= 5.00] out< 05: JOCK.P 252.00 8.221 No.date 28:40 50.08 n/a]
016180 [RFD= 5.00] out< 04: JO O/P 252.00 8.221 No.date 28:40 50.08 n/a]
016190 [MS ovelow ca 04: JO O/P 252.00 8.221 No.date 28:40 50.08 n/a]
016200 025:0056-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
016210 ADD HDD 01: N TO 55192.01 111.156 No.date 36:05 29.38 n/a
016220 [RFD= 5.00] out< 02: LRS 24.00 2.019 No.date 28:00 40.77 n/a]
016230 [RFD= 5.00] out< 04: JO O/P 252.00 8.221 No.date 28:40 50.08 n/a]
016240 [RFD= 5.00] SLM 05: JOCK.P 252.00 8.221 No.date 28:40 50.08 n/a]
016250 [RFD= 5.00] SLM 03: SN 55468.00 112.074 No.date 36:00 29.48 n/a]
016260 025:0057-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
016270 SAGE H/D 03: SN 55468.00 112.074 No.date 36:00 29.48 n/a
016280 frame: C:\Navis\OCTOBE-1\CONTIN-I\SMR_POSTH.H.SN.CO.025
016290 remark: Total Flow at Hart's Desire
016300 #
016310 # Hydrograph from Hart's Desire routed to Rideoan River
016320 # Channel X-Section obtained from RCVA Hydraulic Model - Station 0
016330 #
016340 025:0058-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
016350 ROUTE CHANNEL -> 03: SN 55468.00 112.074 No.date 36:00 29.48 n/a
016360 [RFD= 5.00] out< 01: N TO 55468.00 112.074 No.date 36:05 29.48 n/a]
016370 [L/S=ma 583 / 967.045]
016380 [Vmax 1.826; Dmax 0.52]
016390 *****
016400 # Catchment S-2
016410 # - To Joek River (north and south)
016420 # - Undeveloped floodplain and river
016430 #
016440 025:0059-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
016450 CONTINUOUS STANDHDD2: S-2 102.00 3.924 No.date 28:20 30.12 .405
016460 [Cn= 72.0; No= 3.00]
016470 [I= 40; DT= 5.00]
016480 [InterEventTime= 12.00]
016490 [InterEventTime= 12.00]
016500 025:0060-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
016510 ADD HDD 01: N TO 55468.00 112.074 No.date 36:05 29.48 n/a
016520 [RFD= 5.00] out< 02: S-2 102.00 3.924 No.date 28:20 30.12 n/a]
016530 [RFD= 5.00] SLM 03: SN 55570.01 112.351 No.date 36:05 29.48 n/a]
016540 025:0061-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
016550 SAGE H/D 03: SN 55570.01 112.351 No.date 36:05 29.48 n/a]
016560 frame: C:\Navis\OCTOBE-1\CONTIN-I\SMR_POSTH.H.SN.CO.025
016570 remark: Total Flow at Rideoan River
016580 # END OF RUN
016590 #
016600 # Hydrograph from Rideoan River routed to Nade at Cedarview
016610 # Channel X-Section obtained from RCVA Hydraulic Model - Station 6016
016620 #
016630 025:0062-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
016640 ROUTE CHANNEL -> 03: SN 55570.01 112.351 No.date 36:05 29.48 n/a
016650 [RFD= 5.00] out< 01: N TO 55570.01 112.351 No.date 36:05 29.48 n/a]
016660 [L/S=ma 183 / 076.052]
016670 [Vmax 1.826; Dmax 0.52]
016680 *****
016690 # Catchment FOSTER
016700 # - To Foster ditch (north of the Joek)
016710 # Partially developed (medium density); remaining agricultural
016720 #
016730 025:0063-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
016740 CONTINUOUS STANDHDD2: FOSTER 373.00 38.921 No.date 28:05 65.13 .735
016750 [Mx= 35.71; Mz= 35]
016760 [LRS= 2 Cn= 74.0]
016770 [Impervious area: IPer= 4.67; SLP= 0.0; LQ= 4.0; MNP= 250; SCP= 0]
016780 [Impervious area: IPer= 1.57; SLP= 0.0; LQ= 1577.0; NN= 013; SCL= 0]
016790 [IARECmp= 4.00; IARECper= 4.00]
016800 [SMN= 36.67; SMM= 244.45; SKE= 010]
016810 [Vmax 2.709; Dmax 0.54]
016820 # Foster Pond
016830 # - Rating curve obtained assuming 40m/h/a in 24 hours for quality control
016840 # and a ratio of the catchment area to the West Clarke pond rating curve
016850 # from the MS for the next coordinates
016860 #
016870 025:0064-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
016880 ROUTE RESERVOIR -> 02: KEERFE 448.00 38.901 No.date 28:15 61.25 n/a
016890 [RFD= 5.00] out< 04: P.O.P 396.62 38.659 No.date 28:15 61.25 n/a]
016900 [RFD= 5.00] out< 09: O.P 396.62 38.659 No.date 28:15 61.25 n/a]
016910 [MS ovelow ca 09: O.P 396.62 38.659 No.date 28:15 61.25 n/a]
016920 [MS ovelow ca 09: O.P 396.62 38.659 No.date 28:15 61.25 n/a]
016930 025:0065-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
016940 ADD HDD 01: N TO 55468.00 112.074 No.date 36:05 29.48 n/a]
016950 [RFD= 5.00] out< 04: P.O.P 396.62 38.659 No.date 28:15 61.25 n/a]
016960 [RFD= 5.00] out< 09: O.P 396.62 38.659 No.date 28:15 61.25 n/a]
016970 [MS ovelow ca 09: O.P 396.62 38.659 No.date 28:15 61.25 n/a]
016980 [MS ovelow ca 09: O.P 396.62 38.659 No.date 28:15 61.25 n/a]
016990 025:0066-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
017000 SAGE H/D 03: SN 55477.02 145.022 No.date 33:30 38.96 n/a]
017010 frame: C:\Navis\OCTOBE-1\CONTIN-I\SMR_POSTH.H.SN.CO.100
017020 remark: Total Flow at Foster Drain
017030 #
017040 # Hydrograph from Nade Foster routed to Nade at Cedarview
017050 # Channel X-Section obtained from RCVA Hydraulic Model - Station 6016
017060 #
017070 025:0067-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
017080 ROUTE CHANNEL -> 03: SN 55477.02 145.022 No.date 33:30 38.96 n/a
017090 [RFD= 5.00] out< 01: N TO 55477.02 144.892 No.date 33:40 38.96 n/a]
017100 [L/S=ma 1183 / 076.052]
017110 [Vmax 1.826; Dmax 0.52]
017120 *****
017130 # Catchment S-1
017140 # - To Joek River (north and south of Joek)
017150 # - Primarily agricultural fields; portion of sandy quarry
017160 #
017170 025:0068-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
017180 ROUTE CHANNEL -> 03: SN 55477.02 145.022 No.date 33:30 38.96 n/a
017190 [RFD= 5.00] out< 01: N TO 55477.02 144.892 No.date 33:40 38.96 n/a]
017200 [L/S=ma 159 / 082.055]
017210 [Vmax 1.826; Dmax 0.52]
017220 *****
017230 # Catchment S-1
017240 # - To Joek River (north and south of Joek)
017250 # - Primarily agricultural fields; portion of sandy quarry
017260 #
017270 025:0069-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
017280 ROUTE CHANNEL -> 03: SN 55477.02 145.022 No.date 33:30 38.96 n/a
017290 [RFD= 5.00] out< 01: N TO 55477.02 144.892 No.date 33:40 38.96 n/a]
017300 [L/S=ma 159 / 082.055]
017310 [Vmax 1.826; Dmax 0.52]
017320 *****
017330 # Catchment S-1
017340 # - To Joek River (north and south of Joek)
017350 # - Primarily agricultural fields; portion of sandy quarry
017360 #
017370 025:0070-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
017380 ROUTE CHANNEL -> 03: SN 55477.02 145.022 No.date 33:30 38.96 n/a
017390 [RFD= 5.00] out< 01: N TO 55477.02 144.892 No.date 33:40 38.96 n/a]
017400 [L/S=ma 159 / 082.055]
017410 [Vmax 1.826; Dmax 0.52]
017420 *****
017430 # Catchment S-1
017440 # - To Joek River (north and south of Joek)
017450 # - Primarily agricultural fields; portion of sandy quarry
017460 #
017470 025:0071-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
017480 ROUTE CHANNEL -> 03: SN 55477.02 145.022 No.date 33:30 38.96 n/a
017490 [RFD= 5.00] out< 01: N TO 55477.02 144.892 No.date 33:40 38.96 n/a]
017500 [L/S=ma 159 / 082.055]
017510 [Vmax 1.826; Dmax 0.52]
017520 *****
017530 # Catchment S-1
017540 # - To Joek River (north and south of Joek)
017550 # - Primarily agricultural fields; portion of sandy quarry
017560 #
017570 025:0072-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
017580 ROUTE CHANNEL -> 03: SN 55477.02 145.022 No.date 33:30 38.96 n/a
017590 [RFD= 5.00] out< 01: N TO 55477.02 144.892 No.date 33:40 38.96 n/a]
017600 [L/S=ma 159 / 082.055]
017610 [Vmax 1.826; Dmax 0.52]
017620 *****
017630 # Catchment S-1
017640 # - To Joek River (north and south of Joek)
017650 # - Primarily agricultural fields; portion of sandy quarry
017660 #
017670 025:0073-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
017680 ROUTE CHANNEL -> 03: SN 55477.02 145.022 No.date 33:30 38.96 n/a
017690 [RFD= 5.00] out< 01: N TO 55477.02 144.892 No.date 33:40 38.96 n/a]
017700 [L/S=ma 159 / 082.055]
017710 [Vmax 1.826; Dmax 0.52]
017720 *****
017730 # Catchment S-1
017740 # - To Joek River (north and south of Joek)
017750 # - Primarily agricultural fields; portion of sandy quarry
017760 #
017770 025:0074-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
017780 ROUTE CHANNEL -> 03: SN 55477.02 145.022 No.date 33:30 38.96 n/a
017790 [RFD= 5.00] out< 01: N TO 55477.02 144.892 No.date 33:40 38.96 n/a]
017800 [L/S=ma 159 / 082.055]
017810 [Vmax 1.826; Dmax 0.52]
017820 *****
017830 # Catchment S-1
017840 # - To Joek River (north and south of Joek)
017850 # - Primarily agricultural fields; portion of sandy quarry
017860 #
017870 025:0075-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
017880 ROUTE CHANNEL -> 03: SN 55477.02 145.022 No.date 33:30 38.96 n/a
017890 [RFD= 5.00] out< 01: N TO 55477.02 144.892 No.date 33:40 38.96 n/a]
017900 [L/S=ma 159 / 082.055]
017910 [Vmax 1.826; Dmax 0.52]
017920 *****
017930 # Catchment S-1
017940 # - To Joek River (north and south of Joek)
017950 # - Primarily agricultural fields; portion of sandy quarry
017960 #
017970 025:0076-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
017980 ROUTE CHANNEL -> 03: SN 55477.02 145.022 No.date 33:30 38.96 n/a
017990 [RFD= 5.00] out< 01: N TO 55477.02 144.892 No.date 33:40 38.96 n/a]
018000 [L/S=ma 159 / 082.055]
018010 [Vmax 1.826; Dmax 0.52]
018020 *****
018030 # Catchment S-1
018040 # - To Joek River (north and south of Joek)
018050 # - Primarily agricultural fields; portion of sandy quarry
018060 #
018070 025:0077-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
018080 ROUTE CHANNEL -> 03: SN 55477.02 145.022 No.date 33:30 38.96 n/a
018090 [RFD= 5.00] out< 01: N TO 55477.02 144.892 No.date 33:40 38.96 n/a]
018100 [L/S=ma 159 / 082.055]
018110 [Vmax 1.826; Dmax 0.52]
018120 *****
018130 # Catchment S-1
018140 # - To Joek River (north and south of Joek)
018150 # - Primarily agricultural fields; portion of sandy quarry
018160 #
018170 025:0078-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
018180 ROUTE CHANNEL -> 03: SN 55477.02 145.022 No.date 33:30 38.96 n/a
018190 [RFD= 5.00] out< 01: N TO 55477.02 144.892 No.date 33:40 38.96 n/a]
018200 [L/S=ma 159 / 082.055]
018210 [Vmax 1.826; Dmax 0.52]
018220 *****
018230 # Catchment S-1
018240 # - To Joek River (north and south of Joek)
018250 # - Primarily agricultural fields; portion of sandy quarry
018260 #
018270 025:0079-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
018280 ROUTE CHANNEL -> 03: SN 55477.02 145.022 No.date 33:30 38.96 n/a
018290 [RFD= 5.00] out< 01: N TO 55477.02 144.892 No.date 33:40 38.96 n/a]
018300 [L/S=ma 159 / 082.055]
018310 [Vmax 1.826; Dmax 0.52]
018320 *****
018330 # Catchment S-1
018340 # - To Joek River (north and south of Joek)
018350 # - Primarily agricultural fields; portion of sandy quarry
018360 #
018370 025:0080-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
018380 ROUTE CHANNEL -> 03: SN 55477.02 145.022 No.date 33:30 38.96 n/a
018390 [RFD= 5.00] out< 01: N TO 55477.02 144.892 No.date 33:40 38.96 n/a]
018400 [L/S=ma 159 / 082.055]
018410 [Vmax 1.826; Dmax 0.52]
018420 *****
018430 # Catchment S-1
018440 # - To Joek River (north and south of Joek)
018450 # - Primarily agricultural fields; portion of sandy quarry
018460 #
018470 025:0081-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
018480 ROUTE CHANNEL -> 03: SN 55477.02 145.022 No.date 33:30 38.96 n/a
018490 [RFD= 5.00] out< 01: N TO 55477.02 144.892 No.date 33:40 38.96 n/a]
018500 [L/S=ma 159 / 082.055]
018510 [Vmax 1.826; Dmax 0.52]
018520 *****
018530 # Catchment S-1
018540 # - To Joek River (north and south of Joek)
018550 # - Primarily agricultural fields; portion of sandy quarry
018560 #
018570 025:0082-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
018580 ROUTE CHANNEL -> 03: SN 55477.02 145.022 No.date 33:30 38.96 n/a
018590 [RFD= 5.00] out< 01: N TO 55477.02 144.892 No.date 33:40 38.96 n/a]
018600 [L/S=ma 159 / 082.055]
018610 [Vmax 1.826; Dmax 0.52]
018620 *****
018630 # Catchment S-1
018640 # - To Joek River (north and south of Joek)
018650 # - Primarily agricultural fields; portion of sandy quarry
018660 #
018670 025:0083-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
018680 ROUTE CHANNEL -> 03: SN 55477.02 145.022 No.date 33:30 38.96 n/a
018690 [RFD= 5.00] out< 01: N TO 55477.02 144.892 No.date 33:40 38.96 n/a]
018700 [L/S=ma 159 / 082.055]
018710 [Vmax 1.826; Dmax 0.52]
018720 *****
018730 # Catchment S-1
018740 # - To Joek River (north and south of Joek)
018750 # - Primarily agricultural fields; portion of sandy quarry
018760 #
018770 025:0084-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
018780 ROUTE CHANNEL -> 03: SN 55477.02 145.022 No.date 33:30 38.96 n/a
018790 [RFD= 5.00] out< 01: N TO 55477.02 144.892 No.date 33:40 38.96 n/a]
018800 [L/S=ma 159 / 082.055]
018810 [Vmax 1.826; Dmax 0.52]
018820 *****
018830 # Catchment S-1
018840 # - To Joek River (north and south of Joek)
018850 # - Primarily agricultural fields; portion of sandy quarry
018860 #
018870 025:0085-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
018880 ROUTE CHANNEL -> 03: SN 55477.02 145.022 No.date 33:30 38.96 n/a
018890 [RFD= 5.00] out< 01: N TO 55477.02 144.892 No.date 33:40 38.96 n/a]
018900 [L/S=ma 159 / 082.055]
018910 [Vmax 1.826; Dmax 0.52]
018920 *****
018930 # Catchment S-1
018940 # - To Joek River (north and south of Joek)
018950 # - Primarily agricultural fields; portion of sandy quarry
018960 #
018970 025:0086-----ID NDD-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.-R.C.
018980 ROUTE CHANNEL -> 03: SN 55477.02 145.022 No.date 33:30 38.96 n/a
018990 [RFD= 5.00] out< 01: N TO 55477.02 144.892 No.date 33:40 38.96 n/a]
019000 [L/S=ma 159 / 082.055]
019010 [Vmax 1.826; Dmax 0.52]
019020 *****
019030 # Catchment S-1

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018173 [AreaC 4.00; SMI_N 31.15; SMMX=207.66; SKE -010]
018174 InterEventTime= 12.000
018175 100:0023-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
018176 ADD HYD + 02:S.P 245.00 27.588 No,date 29:10 45.94 n/a
018177 [DR= 5.00] SIM4 03:SN:CE 54095.02 147.622 No,date 33:35 39.17 n/a
018178 ROUTE CHANNEL -> 02:WCLAR 243.00 27.368 No,date 28:05 60.27 n/a
018179 [RDE= 5.00] out< 01:N.W 28.68 26.785 No,date 28:05 60.27 n/a
018180 SAVED HYD 03:SN:CE 54095.02 147.622 No,date 33:35 39.17 n/a
018181 frame: C:\Navi\OCTOBE-1\CONTI-N\SMR_POST\H-SN_C100
018182 remark:Total Flow at Cedarview Road
018183 # Hydrograph from Node Cedarview Road routed to Node at West Clarke Drain
018184 # Channel X-Section obtained from RCVA Hydraulic Model - Station 5002
018185 100:0025-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
018186 ROUTE CHANNEL -> 03:SN:CE 54095.02 147.622 No,date 33:35 39.17 n/a
018187 [RDE= 5.00] out< 01:N.W 54095.02 147.547 No,date 33:45 39.17 n/a
018188 [L/S=ra= 525 / 050] 035]
018189 [Vmax= 1.282;Dmax= 999]
018190 # Catchment WCLAR
018191 # Subdivision with 43% imp. as per Barhaven South MS
018192 # Catchment TOCD
018193 # Subdivision with 43% imp. as per Barhaven South MS
018194 # Catchment TOCD
018195 100:0026-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
018196 CONTI NUCS STANDHDD2:WCLAR 143.00 27.368 No,date 28:05 60.27 600
018197 [L/S= 43; T1M= 43]
018198 [Pervious area: I=per: 4.67;SLLP=1.00;LQ= 40.;MPP= 250;SCP= 0]
018199 [Imperious area: I=amp: 1.57;SLLP=1.00;LG=1273.;NN= 013;SCL= 0]
018200 [I=RECmp= 4.00; I=RECEper= 4.00]
018201 [SMN= 31.15; SMMX=225.43; SKE -010]
018202 # Total Pond 3
018203 # Rating curve obtained from Barhaven South MS modeling
018204 # Tributary Drainage Area to MS Pond 2 = 241 ha
018205 # Routing curve obtained from Barhaven South MS modeling
018206 100:0027-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
018207 ROUTE RESERVOIR -> 02:WCLAR 243.00 27.368 No,date 28:05 60.27 n/a
018208 [RDE= 5.00] out< 02:WCLAR 243.00 27.368 No,date 28:05 60.27 n/a
018209 overflow< 09:PF:OPF 214.32 26.785 No,date 28:05 60.27 n/a
018210 [MSt=0.626; 96000E+00; TotOfVol= 440E+01; NOf= 2; TotDrOf= 16.1hr]
018211 ADD HYD 08:ME_P2 28.68 26.785 No,date 24:40 60.26 n/a
018212 [DR= 5.00] SIM4 03:SN:CE 54338.02 147.747 No,date 33:45 39.27 n/a
018213 [RDE= 5.00] out< 01:N.W 54095.02 147.547 No,date 33:45 39.17 n/a
018214 [RDE= 5.00] out< 01:N.W 54095.02 147.547 No,date 33:45 39.17 n/a
018215 [MSt=0.626; 96000E+00; TotOfVol= 440E+01; NOf= 2; TotDrOf= 16.1hr]
018216 SAVED HYD 03:SN:CE 54338.02 147.747 No,date 33:45 39.27 n/a
018217 frame: C:\Navi\OCTOBE-1\CONTI-N\SMR_POST\H-SN_U100
018218 remark:Total Flow at West Clarke Pond Outlet
018219 # Hydrograph from Node West Clarke Pond routed to Node at Kennedy - Burnett Drain
018220 # Channel X-Section obtained from RCVA Hydraulic Model - Station 4534
018221 100:0030-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
018222 ROUTE CHANNEL -> 04:SN:KE 54338.02 148.477 No,date 33:45 39.27 n/a
018223 [RDE= 5.00] out< 01:K.NE 55192.02 148.919 No,date 35:05 39.61 n/a
018224 [L/S=ra= 1925 / 050] 035]
018225 [Vmax= 940;Dmax= 152]
018226 # Catchment KEN BU
018227 # To Kennedy-Burnett SWM Facility
018228 # Outlets to Fraser-Clarke drain (north of the Jock)
018229 # Medium density residential development
018230 100:0031-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
018231 CONTI NUCS STANDHDD2:KEN BU 281.00 35.633 No,date 28:05 64.01 723
018232 [L/S= 55; T1M= 55]
018233 [Pervious area: I=per: 4.67;SLLP=1.00;LQ= 40.;MPP= 250;SCP= 0]
018234 [Imperious area: I=amp: 1.57;SLLP=1.00;LG=1369.;NN= 013;SCL= 0]
018235 [I=RECmp= 4.00; I=RECEper= 4.00]
018236 [SMN= 41.38; SMMX=275.84; SKE -010]
018237 # Existing Kennedy-Burnett SWM Facility
018238 # Rating curve obtained from LREQ
018239 # Tributary Drainage Area to Pond = 160 ha
018240 # Routing curve obtained from LREQ
018241 100:0032-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
018242 ROUTE RESERVOIR -> 03:KEN BU 281.00 35.633 No,date 28:05 64.01 n/a
018243 [RDE= 5.00] out< 05:KEN BU 132.84 31.550 No,date 27:45 64.01 n/a
018244 overflow< 06:KEN OV 148.16 34.267 No,date 28:05 64.01 n/a
018245 [MSt=0.626; 23300E+00; TotOfVol= 948E+01; NOf= 0; TotDrOf= 5.1hr]
018246 SAVED HYD 03:SN:KE 281.00 35.633 No,date 28:05 64.01 n/a
018247 frame: C:\Navi\OCTOBE-1\CONTI-N\SMR_POST\H-SN_KB100
018248 remark:Total Flow at Ken Burnett Outlet
018249 # Hydrograph from Node Kennedy - Burnett Drain to Node Todd Drain
018250 # Channel X-Section obtained from RCVA Hydraulic Model - Station 3633
018251 100:0033-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
018252 ROUTE CHANNEL -> 04:SN:KB 54709.01 149.236 No,date 33:55 39.42 n/a
018253 [RDE= 5.00] out< 01:N.W 54709.01 148.001 No,date 33:55 39.42 n/a
018254 [L/S=ra= 650 / 050] 035]
018255 [Vmax= 281;Dmax= 999]
018256 # Catchment TODD
018257 # To Todd Drain (south of the Jock)
018258 # Subdivision with 43% imp. as per Barhaven South MS
018259 # Catchment TODD
018260 # Subdivision with 43% imp. as per Barhaven South MS
018261 100:0034-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
018262 CONTI NUCS STANDHDD2:TODD 90.00 9.664 No,date 28:05 55.76 630
018263 [L/S= 2; C= 77.01]
018264 [Pervious area: I=per: 4.67;SLLP=1.00;LQ= 40.;MPP= 250;SCP= 0]
018265 [Imperious area: I=amp: 1.57;SLLP=1.00;LG= 775.;NN= 013;SCL= 0]
018266 [I=RECmp= 4.00; I=RECEper= 4.00]
018267 [SMN= 26.32; SMMX=175.56; SKE -010]
018268 # Existing TODD
018269 # Rating curve obtained from LREQ
018270 # Tributary Drainage Area to Pond = 160 ha
018271 # Routing curve obtained from LREQ
018272 100:0035-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
018273 ROUTE RESERVOIR -> 07:FRASER 90.00 9.664 No,date 28:05 55.76 n/a
018274 [RDE= 5.00] out< 08:ME_P2 11.04 0.040 No,date 26:20 55.76 n/a
018275 overflow< 09:PF:OPF 78.96 9.261 No,date 28:05 55.76 n/a
018276 [MSt=0.626; 35990E+00; TotOfVol= 440E+01; NOf= 2; TotDrOf= 14.1hr]
018277 ADD HYD 05:KEN_P 132.84 31.550 No,date 27:45 64.01 n/a
018278 [DR= 5.00] SIM4 03:SN:KE 54338.02 147.747 No,date 33:45 39.27 n/a
018279 [RDE= 5.00] out< 01:N.W 54095.02 147.547 No,date 33:45 39.27 n/a
018280 overflow< 09:PF:OPF 173.14 22.231 No,date 28:05 61.22 n/a
018281 [MSt=0.626; 7796E+00; TotOfVol= 1060E+02; NOf= 2; TotDrOf= 16.1hr]
018282 ADD HYD 05:KEN_P 132.84 31.550 No,date 27:45 64.01 n/a
018283 [DR= 5.00] SIM4 03:SN:KE 54709.01 149.236 No,date 33:55 39.42 n/a
018284 [RDE= 5.00] out< 01:N.W 54709.01 148.001 No,date 33:55 39.42 n/a
018285 [L/S=ra= 650 / 050] 035]
018286 [Vmax= 281;Dmax= 999]
018287 # Catchment TODD
018288 # To Todd Drain (south of the Jock)
018289 # Subdivision with 43% imp. as per Barhaven South MS
018290 # Catchment TODD
018291 # Subdivision with 43% imp. as per Barhaven South MS
018292 100:0036-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
018293 CONTI NUCS STANDHDD2:TODD 195.00 22.652 No,date 28:05 61.25 692
018294 [L/S= 43; T1M= 43]
018295 [Pervious area: I=per: 4.67;SLLP=1.00;LQ= 40.;MPP= 250;SCP= 0]
018296 [Imperious area: I=amp: 1.57;SLLP=1.00;LG=1140.;NN= 013;SCL= 0]
018297 [I=RECmp= 4.00; I=RECEper= 4.00]
018298 [SMN= 31.15; SMMX=207.66; SKE -010]
018299 # Total Pond 3
018300 # Rating curve obtained from Barhaven South MS modeling
018301 # Tributary Drainage Area to MS Pond 2 = 191 ha
018302 # Routing curve obtained from Barhaven South MS modeling
018303 100:0039-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
018304 ROUTE CHANNEL -> 10:SN:TO 54904.01 148.757 No,date 35:05 39.50 n/a
018305 [RDE= 5.00] out< 02:ME_P2 21.86 0.080 No,date 24:40 61.25 n/a
018306 overflow< 09:PF:OPF 173.14 22.231 No,date 28:05 61.22 n/a
018307 [MSt=0.626; 5800E+00; TotOfVol= 8259E+01; NOf= 2; TotDrOf= 16.1hr]
018308 ADD HYD 01:N:TO 54904.01 148.481 No,date 35:05 39.50 n/a
018309 [DR= 5.00] SIM4 03:SN:TO 54904.01 148.481 No,date 35:05 39.50 n/a
018310 [RDE= 5.00] out< 01:N:TO 54904.01 148.481 No,date 35:05 39.50 n/a
018311 [L/S=ra= 714;Dmax= 4087]
018312 # Catchment CORRIG
018313 # To Corrig Drain (south of the Jock)
018314 # Primarily Developed (medium density)
018315 100:0043-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
018316 CONTI NUCS STANDHDD2:CORRIG 149.00 19.025 No,date 28:05 62.15 702
018317 [L/S= 45; T1M= 45]
018318 [Pervious area: I=per: 4.67;SLLP=1.00;LQ= 40.;MPP= 250;SCP= 0]
018319 [Imperious area: I=amp: 1.57;SLLP=1.00;LG= 997.;NN= 013;SCL= 0]
018320 [I=RECmp= 4.00; I=RECEper= 4.00]
018321 [SMN= 31.15; SMMX=207.66; SKE -010]
018322 # Corrig Pond 1
018323 # Rating curve obtained from Barhaven South MS modeling
018324 # Tributary Drainage Area to MS Pond = 145 ha
018325 # Routing curve obtained from Barhaven South MS modeling
018326 100:0044-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
018327 ROUTE RESERVOIR -> 02:CORRIG 149.00 19.025 No,date 28:05 62.15 n/a
018328 [RDE= 5.00] out< 05:ME_P1 16.12 0.060 No,date 24:20 62.15 n/a
018329 overflow< 04:PF:OPF 132.88 18.764 No,date 28:05 62.15 n/a
018330 [MSt=0.626; 5800E+00; TotOfVol= 8259E+01; NOf= 2; TotDrOf= 16.1hr]
018331 ADD HYD 01:N:TO 54904.01 148.481 No,date 35:05 39.50 n/a
018332 [DR= 5.00] SIM4 03:SN:TO 54904.01 148.481 No,date 35:05 39.50 n/a
018333 [RDE= 5.00] out< 01:N:TO 54904.01 148.481 No,date 35:05 39.50 n/a
018334 [L/S=ra= 714;Dmax= 4087]
018335 # Catchment CORRIG
018336 # To Corrig Drain (south of the Jock)
018337 # Primarily Developed (medium density)
018338 100:0045-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
018339 CONTI NUCS STANDHDD2:CORRIG 149.00 19.025 No,date 28:05 62.15 702
018340 [L/S= 45; T1M= 45]
018341 [Pervious area: I=per: 4.67;SLLP=1.00;LQ= 40.;MPP= 250;SCP= 0]
018342 [Imperious area: I=amp: 1.57;SLLP=1.00;LG= 997.;NN= 013;SCL= 0]
018343 [I=RECmp= 4.00; I=RECEper= 4.00]
018344 [SMN= 31.15; SMMX=207.66; SKE -010]
018345 # Corrig Pond 1
018346 # Rating curve obtained from Barhaven South MS modeling
018347 # Tributary Drainage Area to MS Pond = 145 ha
018348 # Routing curve obtained from Barhaven South MS modeling
018349 100:0046-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
018350 ROUTE RESERVOIR -> 02:CORRIG 149.00 19.025 No,date 28:05 62.15 n/a
018351 [RDE= 5.00] out< 05:ME_P1 16.12 0.060 No,date 24:20 62.15 n/a
018352 overflow< 04:PF:OPF 132.88 18.764 No,date 28:05 62.15 n/a
018353 [MSt=0.626; 5800E+00; TotOfVol= 8259E+01; NOf= 2; TotDrOf= 16.1hr]
018354 ADD HYD 01:N:TO 54904.01 148.481 No,date 35:05 39.50 n/a
018355 [DR= 5.00] SIM4 03:SN:TO 54904.01 148.481 No,date 35:05 39.50 n/a
018356 [RDE= 5.00] out< 01:N:TO 54904.01 148.481 No,date 35:05 39.50 n/a
018357 [L/S=ra= 714;Dmax= 4087]

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020588 [DR= 5.00] SIM4 03:SN:CE 55053.02 149.062 No,date 35:20 39.56 n/a
020589 SAVED HYD 03:SN:CE 55053.02 149.062 No,date 35:20 39.56 n/a
020600 100:0046-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
020601 [RDE= 5.00] out< 01:N:M 55053.02 149.062 No,date 35:20 39.56 n/a
020602 frame: C:\Navi\OCTOBE-1\CONTI-N\SMR_POST\H-SN_C100
020603 remark:Total Flow at Corrig Drain
020604 # Hydrograph from Corrig Drain routed to Jockvale Road
020605 # Channel X-Section obtained from RCVA Hydraulic Model - Station 2462
020606 100:0047-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
020607 ROUTE CHANNEL -> 03:SN:CO 55053.02 149.062 No,date 35:20 39.56 n/a
020608 [RDE= 5.00] out< 01:N:M 55053.02 149.062 No,date 35:20 39.56 n/a
020609 [L/S=ra= 580 / 445] 045]
020610 [L/S=ra= 2191;Dmax= 2152]
020611 # Catchment MLLS
020612 # To SWM Facility north of the Jock
020613 # Primarily residential development
020614 100:0048-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
020615 CONTI NUCS STANDHDD2:MLLS 139.00 15.807 No,date 28:05 56.87 642
020616 [L/S= 2; C= 74.0]
020617 [Pervious area: I=per: 4.67;SLLP=1.00;LQ= 40.;MPP= 250;SCP= 0]
020618 [Imperious area: I=amp: 1.57;SLLP=1.00;LG= 963.;NN= 013;SCL= 0]
020619 [I=RECmp= 4.00; I=RECEper= 4.00]
020620 [SMN= 36.67; SMMX=244.49; SKE -010]
020621 # Chapman MLLS SWM Pond
020622 # Rating curve obtained from CCL hydraulic modeling
020623 100:0049-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
020624 ROUTE RESERVOIR -> 02:MLLS 139.00 15.807 No,date 28:05 56.87 n/a
020625 [RDE= 5.00] out< 05:MLL 139.00 15.807 No,date 28:05 56.87 n/a
020626 overflow< 04:ML:OV 10.46 7.805 No,date 28:15 56.87 n/a
020627 [MSt=0.626; 2310E+00; TotOfVol= 3940E+01; NOf= 2; TotDrOf= 1.1hr]
020628 ADD HYD 01:N:M 55053.02 149.062 No,date 35:20 39.56 n/a
020629 [RDE= 5.00] out< 04:ML:OV 10.46 7.805 No,date 28:15 56.87 n/a
020630 overflow< 05:MLL 128.54 4.850 No,date 28:15 56.87 n/a
020631 [MSt=0.626; 5500E+00; TotOfVol= 149.062 No,date 35:20 39.61 n/a]
020632 [DR= 5.00] SIM4 03:SN:M 55192.02 148.919 No,date 35:05 39.61 n/a
020633 [RDE= 5.00] out< 01:N:NE 55192.02 148.919 No,date 35:05 39.61 n/a
020634 [L/S=ra= 1962 / 223] 045]
020635 [Vmax= 940;Dmax= 152]
020636 # Hydrograph from Jockvale Road routed to Hart's Desire
020637 # Channel X-Section obtained from RCVA Hydraulic Model - Station 689
020638 100:0052-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
020639 ROUTE CHANNEL -> 03:SN:M 55192.02 148.919 No,date 35:05 39.61 n/a
020640 [RDE= 5.00] out< 01:N:NE 55192.02 148.919 No,date 35:05 39.61 n/a
020641 [L/S=ra= 1962 / 223] 045]
020642 [Vmax= 940;Dmax= 152]
020643 # Catchment DESIRE
020644 # To Jock River (north of the Jock)
020645 # Residential development
020646 100:0053-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
020647 CONTI NUCS STANDHDD2:DESIRE 24.00 2.882 No,date 28:00 53.12 600
020648 [L/S= 25; T1M= 25]
020649 [Pervious area: I=per: 4.67;SLLP=1.00;LQ= 40.;MPP= 250;SCP= 0]
020650 [Imperious area: I=amp: 1.57;SLLP=1.00;LG= 400.;NN= 010;SCL= 0]
020651 [I=RECmp= 4.00; I=RECEper= 4.00]
020652 [SMN= 31.15; SMMX=207.66; SKE -010]
020653 # Catchment JOCKVA
020654 # To Jockvale SWM Facility
020655 # Residential development & golf course
020656 100:0054-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
020657 CONTI NUCS STANDHDD2:JOCKVA 252.00 30.693 No,date 28:05 62.70 708
020658 [L/S= 2; C= 74.0]
020659 [Pervious area: I=per: 4.67;SLLP=1.00;LQ= 40.;MPP= 250;SCP= 0]
020660 [Imperious area: I=amp: 1.57;SLLP=1.00;LG= 1296.;NN= 013;SCL= 0]
020661 [I=RECmp= 4.00; I=RECEper= 4.00]
020662 [SMN= 36.67; SMMX=244.49; SKE -010]
020663 # Jockvale SWM Facility
020664 # Rating curve obtained from Jockvale Servicing Study (CCL 1999)
020665 100:0055-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
020666 ROUTE RESERVOIR -> 03:JOCKVA 252.00 30.693 No,date 28:05 62.70 n/a
020667 [RDE= 5.00] out< 05:JOCK_P 252.00 30.693 No,date 28:35 62.70 n/a
020668 overflow< 04:JO:OV 0.00 0.000 No,date 0:00 0.00 n/a
020669 [MSt=0.626; 320E+00; TotOfVol= 0.000E+00; NOf= 0; TotDrOf= 0.1hr]
020670 ADD HYD 01:N:NE 55468.01 150.033 No,date 36:00 39.72 n/a
020671 [RDE= 5.00] out< 01:N:NE 55468.01 150.033 No,date 36:00 39.72 n/a
020672 overflow< 04:JO:OV 0.00 0.000 No,date 0:00 0.00 n/a
020673 [MSt=0.626; 320E+00; TotOfVol= 0.000E+00; NOf= 0; TotDrOf= 0.1hr]
020674 SAVED HYD 03:SN:NE 55468.01 150.033 No,date 36:00 39.72 n/a
020675 frame: C:\Navi\OCTOBE-1\CONTI-N\SMR_POST\H-SN_NE100
020676 remark:Total Flow at Hart's Desire
020677 # Hydrograph from Hart's Desire routed to Rideau River
020678 # Channel X-Section obtained from RCVA Hydraulic Model - Station 0
020679 100:0058-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
020680 ROUTE CHANNEL -> 03:SN:NE 55468.01 150.033 No,date 36:00 39.72 n/a
020681 [RDE= 5.00] out< 01:N:NE 55468.01 150.033 No,date 36:00 39.72 n/a
020682 [L/S=ra= 563 / 967] 045]
020683 [Vmax= 2709;Dmax= 046]
020684 # Catchment S 2
020685 # To Jock River (north and south)
020686 # Undeveloped floodplain and river
020687 100:0059-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
020688 CONTI NUCS STANDHDD2:S 2 102.00 5.616 No,date 28:15 40.95 462
020689 [L/S= 72.0; C= 3.00]
020690 [Pervious area: I=per: 4.67;SLLP=1.00;LQ= 40.;MPP= 250;SCP= 0]
020691 [Imperious area: I=amp: 1.57;SLLP=1.00;LG= 1020.;NN= 013;SCL= 0]
020692 [I=RECmp= 4.00; I=RECEper= 4.00]
020693 [SMN= 36.67; SMMX=244.49; SKE -010]
020694 [InterEventTime= 12.000]
020695 100:0060-----ID NNDP-----AREA-----QPEAK TpeakDate:hh:mm-----R.V.R.C.
020696 ADD HYD 01:N:NI 55468.01 150.033 No,date 36:05 39.72 n/a
020697 [RDE= 5.00] out< 02:S 2 102.00 5.616 No,date 28:15 40.95 n/a
020698 [DR= 5.00] SIM4 03:SN:NI 55570.01 150.390 No,date 36:05 39.72 n/a
020699 [RDE= 5.00] out< 03:SN:NI 55570.01 150.390 No,date 36:05 39.72 n/a
020700 SAVED HYD 03:SN:NI 55570.01 150.390 No,date 36:05 39.72 n/a
020701 frame: C:\Navi\OCTOBE-1\CONTI-N\SMR_POST\H-SN_N100
020702 remark:Total Flow at Rideau River
020703 #####
020704 # PNI SH
020705 # Warnings / Errors / Notes
020706 002:0037 ROUTE CHANNEL ->
020707 *** WARNING TRAVEL TIME TABLE was exceeded
020708 *** WARNING TRAVEL TIME TABLE was exceeded
020709 *** WARNING TRAVEL TIME TABLE was exceeded
020710 *** WARNING TRAVEL TIME TABLE was exceeded
020711 Simulation ended on 2006-11-15 at 14:33:35
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Attachment C

Model 3 – Jock River Reach One Update

JFSA, 2021

SWMHYMO Input & Summary files

```

1  20      Metric units / ID numbers OFF
2  *****
3  *# SWHYMO Ver: 5.02/Jan 2001 <BETA> / INPUT DATA FILE
4  *****
5  *# Project Name: [Jock River]      Project Number: [1474-16]
6  *# Date       : 04-03-2021
7  *# Modeller   : [M M]
8  *# Company    : JFSA Inc.
9  *# License #  : 2549237
10 *****
11 *# CALIBRATION OF SUMMER MODEL PARAMETERS
12 *# USING CONTINUOUS SIMULATIONS
13 *# Rainfall data from JFSA raingauge installed at site + other gauges by the City
14 *# Use data collected from May 1st to July 14, 2003
15 *# 2020-11-30 change TM STO in COMPUTE DUALHYD (TM STO = 0.1 instead of 0.0001)
16 *# 2020-12-01 correct pond curve values
17 *# 2020-12-01 change W CLAR_BRAZ XIMP to 0.55, SLPI=[0.5](%) (impervious slope), and
18 LGI up to 700m
19 *# 2021-02-19 Change the slope for ROUTE CHANNEL Station 2462 (NHYDout=["N_TO"]
20 , NHYDin=["SN_TO"]) from 0.033 % (as per Stantec Report 2007) to 0.05 % so the model
21 will be more stable and give reasonable results. It is justifiable as ROUTE CHANNELS
22 aren't well suited to really flat slopes.
23 *# 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (NHYDout=["N_WC"]
24 , NHYDin=["SN_CE"]) from 0.01 % (as per Stantec Report 2007) to 0.0255 % so the model
25 will be more stable and give reasonable results. It is justifiable as ROUTE CHANNELS
26 aren't well suited to really flat slopes.
27 *
28 * Calibrated parameters for Summer 2003 data: APII=50, APIK=0.85, CN=varies,
29 *                                               SK=0.01, InterEventTime=12,
30 *                                               GWResk=0.96, VHydCond=0.055
31 *
32 *# -----
33 *
34 *START          TZERO=[2003.0501], METOUT=[2], NSTORM=[1], NRUN=[001]
35 *              ["XAVG0315.STM"] average storm data a 15 minute time step
36 *              The above rainf file is an average of the JFSA gauge data
37 *              with the City of Ottawa rainfall data collected during
38 *              the same period.
39 *% 2 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
40 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[2]
41 ["C24SC002.stm"] <-- storm filename, one per line for NSTORM time
42 *%-----|-----|
43 *%-----|-----|
44 READ STORM     STORM_FILENAME=["storm 001"]
45 *%-----|-----|
46 MODIFY STORM  ICASEms=[1], NSHIFT=[96],
47 RedFACT=[1],
48 *%-----|-----|
49 DEFAULT VALUES ICASEdef=[1], read and print values
50 DEFVAL_FILENAME=["CitiGate.DEF"]
51 *%-----|-----|
52 *%-----|-----|
53 COMPUTE API    APII=[50], APIK=[.85]/day
54 *%-----|-----|
55 *%-----|-----|
56 *#
57 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
58 *# of 1.32
59 *%-----|-----|
60 CONTINUOUS NASHYD NHYD=["JR_HW"], DT=[1]min, AREA=[3680](ha),
61 DWF=[0](cms), CNVC=[64], IA=[2.5](mm),
62 N=[3.0], TP=[7.13]hrs,
63 Continuous simulation parameters:
64 IARECper=[4](hrs),
65 SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
66 InterEventTime=[12](hrs)
67 Baseflow simulation parameters:

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60 BaseFlowOption=[ 1] ,
61 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
62 VHydCond=[ 0.055](mm/hr), END=- 1
63 *%-----|-----
64 *#
65 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
66 *# of 1.32
67 *%-----|-----
68 CONTINUOUS NASHYD NHYD=["SW_13"], DT=[ 1]min, AREA=[ 971](ha),
69 DWF=[ 0](cms), CNVC=[ 61], IA=[ 2.5](mm),
70 N=[ 3.0], TP=[ 3.76]hrs,
71 Continuous simulation parameters:
72 IaRECper=[ 4](hrs),
73 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
74 InterEventTime=[ 12](hrs)
75 Baseflow simulation parameters:
76 BaseFlowOption=[ 1] ,
77 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
78 VHydCond=[ 0.055](mm/hr), END=- 1
79 *%-----|-----
80 *#
81 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
82 *# of 1.80
83 *%-----|-----
84 CONTINUOUS NASHYD NHYD=["JR_GWM"], DT=[ 1]min, AREA=[ 3074](ha),
85 DWF=[ 0](cms), CNVC=[ 55], IA=[ 2.5](mm),
86 N=[ 3], TP=[ 11.33]hrs,
87 Continuous simulation parameters:
88 IaRECper=[ 4](hrs),
89 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
90 InterEventTime=[ 12](hrs)
91 Baseflow simulation parameters:
92 BaseFlowOption=[ 1] ,
93 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
94 VHydCond=[ 0.055](mm/hr), END=- 1
95 *%-----|-----
96 CONTINUOUS NASHYD NHYD=["JR_ASH"], DT=[ 1]min, AREA=[ 1781](ha),
97 DWF=[ 0](cms), CNVC=[ 72], IA=[ 2.5](mm),
98 N=[ 3.0], TP=[ 3.91]hrs,
99 Continuous simulation parameters:
100 IaRECper=[ 4](hrs),
101 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
102 InterEventTime=[ 12](hrs)
103 Baseflow simulation parameters:
104 BaseFlowOption=[ 1] ,
105 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
106 VHydCond=[ 0.055](mm/hr), END=- 1
107 *%-----|-----
108 CONTINUOUS NASHYD NHYD=["SW_11"], DT=[ 1]min, AREA=[ 500](ha),
109 DWF=[ 0](cms), CNVC=[ 66], IA=[ 2.5](mm),
110 N=[ 3.0], TP=[ 1.24]hrs,
111 Continuous simulation parameters:
112 IaRECper=[ 4](hrs),
113 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
114 InterEventTime=[ 12](hrs)
115 Baseflow simulation parameters:
116 BaseFlowOption=[ 1] ,
117 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
118 VHydCond=[ 0.055](mm/hr), END=- 1
119 *%-----|-----
120 *#
121 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
122 *# of 1.80
123 *%-----|-----
124 CONTINUOUS NASHYD NHYD=["NN_CK"], DT=[ 1]min, AREA=[ 1917](ha),
125 DWF=[ 0](cms), CNVC=[ 66], IA=[ 2.5](mm),

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126 N=[ 3. 0], TP=[ 5. 29] hrs,
127 Continuous simulation parameters:
128 IaRECPper=[ 4] (hrs),
129 SMN=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010]/ (mm),
130 InterEventTime=[ 12] (hrs)
131 Baseflow simulation parameters:
132 BaseFlowOption=[ 1] ,
133 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
134 VHydCond=[ 0. 055] (mm/ hr), END=- 1
135 *%-----|-----
136 *#
137 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
138 *# of 1.52
139 *%-----|-----
140 CONTINUOUS NASHYD NHYD=[ "SW_10"], DT=[ 1] min, AREA=[ 5666] (ha),
141 DWF=[ 0] (cms), CNVC=[ 72], IA=[ 2. 5] (mm),
142 N=[ 3. 0], TP=[ 8. 00] hrs,
143 Continuous simulation parameters:
144 IaRECPper=[ 4] (hrs),
145 SMN=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010]/ (mm),
146 InterEventTime=[ 12] (hrs)
147 Baseflow simulation parameters:
148 BaseFlowOption=[ 1] ,
149 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
150 VHydCond=[ 0. 055] (mm/ hr), END=- 1
151 *%-----|-----
152 *#
153 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
154 *# of 1.75
155 *%-----|-----
156 CONTINUOUS NASHYD NHYD=[ "KG_CK"], DT=[ 1] min, AREA=[ 8376] (ha),
157 DWF=[ 0] (cms), CNVC=[ 66], IA=[ 2. 5] (mm),
158 N=[ 3. 0], TP=[ 11. 66] hrs,
159 Continuous simulation parameters:
160 IaRECPper=[ 4] (hrs),
161 SMN=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010]/ (mm),
162 InterEventTime=[ 12] (hrs)
163 Baseflow simulation parameters:
164 BaseFlowOption=[ 1] ,
165 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
166 VHydCond=[ 0. 055] (mm/ hr), END=- 1
167 *%-----|-----
168 *#
169 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
170 *# of 1.68
171 *%-----|-----
172 CONTINUOUS NASHYD NHYD=[ "SW_9"], DT=[ 1] min, AREA=[ 1132] (ha),
173 DWF=[ 0] (cms), CNVC=[ 70], IA=[ 2. 5] (mm),
174 N=[ 3. 0], TP=[ 2. 51] hrs,
175 Continuous simulation parameters:
176 IaRECPper=[ 4] (hrs),
177 SMN=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010]/ (mm),
178 InterEventTime=[ 12] (hrs)
179 Baseflow simulation parameters:
180 BaseFlowOption=[ 1] ,
181 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
182 VHydCond=[ 0. 055] (mm/ hr), END=- 1
183 *%-----|-----
184 *#
185 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
186 *# of 1.82
187 *%-----|-----
188 CONTINUOUS NASHYD NHYD=[ "NC_CK"], DT=[ 1] min, AREA=[ 4464] (ha),
189 DWF=[ 0] (cms), CNVC=[ 62], IA=[ 2. 5] (mm),
190 N=[ 3. 0], TP=[ 11. 32] hrs,
191 Continuous simulation parameters:

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```

192 IaREcper=[ 4] (hr s),
193 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
194 InterEventTime=[ 12] (hr s)
195 Baseflow simulation parameters:
196 BaseFlowOption=[ 1] ,
197 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
198 VHydCond=[ 0. 055] (mm/ hr), END=- 1
199 *%-----|-----
200 *#
201 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
202 *# of 1.80
203 *%-----|-----
204 CONTINUOUS NASHYD NHYD=[ "SW_8" ], DT=[ 1] mi n, AREA=[ 131] (ha),
205 DWF=[ 0] (cms), CN C=[ 63], IA=[ 2. 5] (mm),
206 N=[ 3. 0], TP=[ 0. 90] hr s,
207 Continuous simulation parameters:
208 IaREcper=[ 4] (hr s),
209 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
210 InterEventTime=[ 12] (hr s)
211 Baseflow simulation parameters:
212 BaseFlowOption=[ 1] ,
213 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
214 VHydCond=[ 0. 055] (mm/ hr), END=- 1
215 *%-----|-----
216 *#
217 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
218 *# of 1.65
219 *%-----|-----
220 CONTINUOUS NASHYD NHYD=[ "HB_DR" ], DT=[ 1] mi n, AREA=[ 3854] (ha),
221 DWF=[ 0] (cms), CN C=[ 66], IA=[ 2. 5] (mm),
222 N=[ 3. 0], TP=[ 8. 42] hr s,
223 Continuous simulation parameters:
224 IaREcper=[ 4] (hr s),
225 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
226 InterEventTime=[ 12] (hr s)
227 Baseflow simulation parameters:
228 BaseFlowOption=[ 1] ,
229 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
230 VHydCond=[ 0. 055] (mm/ hr), END=- 1
231 *%-----|-----
232 *#
233 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
234 *# of 1.82
235 *%-----|-----
236 CONTINUOUS NASHYD NHYD=[ "SW_7" ], DT=[ 1] mi n, AREA=[ 3197] (ha),
237 DWF=[ 0] (cms), CN C=[ 57], IA=[ 2. 5] (mm),
238 N=[ 3. 0], TP=[ 6. 65] hr s,
239 Continuous simulation parameters:
240 IaREcper=[ 4] (hr s),
241 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
242 InterEventTime=[ 12] (hr s)
243 Baseflow simulation parameters:
244 BaseFlowOption=[ 1] ,
245 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
246 VHydCond=[ 0. 055] (mm/ hr), END=- 1
247 *%-----|-----
248 *#
249 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
250 *# of 1.75
251 *%-----|-----
252 CONTINUOUS NASHYD NHYD=[ "SW_6" ], DT=[ 1] mi n, AREA=[ 165] (ha),
253 DWF=[ 0] (cms), CN C=[ 67], IA=[ 2. 5] (mm),
254 N=[ 3. 0], TP=[ 4. 18] hr s,
255 Continuous simulation parameters:
256 IaREcper=[ 4] (hr s),
257 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),

```

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258 InterEventTime=[ 12] (hrs)
259 Baseflow simulation parameters:
260 BaseFlowOption=[ 1] ,
261 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/ day/ mm)
262 VHydCond=[ 0.055] (mm/ hr), END=- 1
263 *%-----|-----
264 *#
265 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
266 *# of 1.67
267 *%-----|-----
268 CONTINUOUS NASHYD NHYD=[ "VG_DR" ], DT=[ 1] min, AREA=[ 1332] (ha),
269 DWF=[ 0] (cms), CNVC=[ 72], IA=[ 2.5] (mm),
270 N=[ 3.0], TP=[ 5.95] hrs,
271 Continuous simulation parameters:
272 IaRECper=[ 4] (hrs),
273 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
274 InterEventTime=[ 12] (hrs)
275 Baseflow simulation parameters:
276 BaseFlowOption=[ 1] ,
277 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/ day/ mm)
278 VHydCond=[ 0.055] (mm/ hr), END=- 1
279 *%-----|-----
280 CONTINUOUS NASHYD NHYD=[ "SW_5" ], DT=[ 1] min, AREA=[ 224] (ha),
281 DWF=[ 0] (cms), CNVC=[ 77], IA=[ 2.5] (mm),
282 N=[ 3.0], TP=[ 0.75] hrs,
283 Continuous simulation parameters:
284 IaRECper=[ 4] (hrs),
285 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
286 InterEventTime=[ 12] (hrs)
287 Baseflow simulation parameters:
288 BaseFlowOption=[ 1] ,
289 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/ day/ mm)
290 VHydCond=[ 0.055] (mm/ hr), END=- 1
291 *%-----|-----
292 *#
293 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
294 *# of 1.20
295 *%-----|-----
296 CONTINUOUS NASHYD NHYD=[ "FL_CK" ], DT=[ 1] min, AREA=[ 4945] (ha),
297 DWF=[ 0] (cms), CNVC=[ 74], IA=[ 2.5] (mm),
298 N=[ 3.0], TP=[ 4.45] hrs,
299 Continuous simulation parameters:
300 IaRECper=[ 4] (hrs),
301 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
302 InterEventTime=[ 12] (hrs)
303 Baseflow simulation parameters:
304 BaseFlowOption=[ 1] ,
305 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/ day/ mm)
306 VHydCond=[ 0.055] (mm/ hr), END=- 1
307 *%-----|-----
308 CONTINUOUS NASHYD NHYD=[ "SW_5A2" ], DT=[ 1] min, AREA=[ 20] (ha),
309 DWF=[ 0] (cms), CNVC=[ 81], IA=[ 2.5] (mm),
310 N=[ 3.0], TP=[ 0.62] hrs,
311 Continuous simulation parameters:
312 IaRECper=[ 4] (hrs),
313 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
314 InterEventTime=[ 12] (hrs)
315 Baseflow simulation parameters:
316 BaseFlowOption=[ 1] ,
317 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/ day/ mm)
318 VHydCond=[ 0.055] (mm/ hr), END=- 1
319 *%-----|-----
320 *#
321 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
322 *# of 1.61
323 *%-----|-----

```

324 CONTI NUOUS NASHYD NYHD=["SW_5A1"], DT=[1] mi n, AREA=[1412] (ha),
325 DWF=[0] (cms), CNV C=[75], IA=[2. 5] (mm),
326 N=[3. 0], TP=[8. 00] hr s,
327 Continuous simulation parameters:
328 IaRECper=[4] (hr s),
329 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
330 InterEventTime=[12] (hr s)
331 Baseflow simulation parameters:
332 BaseFlowOpti on=[1] ,
333 In it GWR es Vol = [50] (mm), GWR es K=[0. 96] (mm / day / mm)
334 VHydCond=[0. 055] (mm / hr), END=- 1

*%-----|

336 CONTI NUOUS NASHYD NYHD=["SW_4"], DT=[1] mi n, AREA=[585] (ha),
337 DWF=[0] (cms), CNV C=[81], IA=[2. 5] (mm),
338 N=[3. 0], TP=[1. 75] hr s,
339 Continuous simulation parameters:
340 IaRECper=[4] (hr s),
341 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
342 InterEventTime=[12] (hr s)
343 Baseflow simulation parameters:
344 BaseFlowOpti on=[1] ,
345 In it GWR es Vol = [50] (mm), GWR es K=[0. 96] (mm / day / mm)
346 VHydCond=[0. 055] (mm / hr), END=- 1

*%-----|

348 CONTI NUOUS NASHYD NYHD=["LM_CK"], DT=[1] mi n, AREA=[1021] (ha),
349 DWF=[0] (cms), CNV C=[80], IA=[2. 5] (mm),
350 N=[3. 0], TP=[2. 46] hr s,
351 Continuous simulation parameters:
352 IaRECper=[4] (hr s),
353 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
354 InterEventTime=[12] (hr s)
355 Baseflow simulation parameters:
356 BaseFlowOpti on=[1] ,
357 In it GWR es Vol = [50] (mm), GWR es K=[0. 96] (mm / day / mm)
358 VHydCond=[0. 055] (mm / hr), END=- 1

*%-----|

360 CONTI NUOUS NASHYD NYHD=["SW_2"], DT=[1] mi n, AREA=[177] (ha),
361 DWF=[0] (cms), CNV C=[77], IA=[2. 5] (mm),
362 N=[3. 0], TP=[0. 75] hr s,
363 Continuous simulation parameters:
364 IaRECper=[4] (hr s),
365 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
366 InterEventTime=[12] (hr s)
367 Baseflow simulation parameters:
368 BaseFlowOpti on=[1] ,
369 In it GWR es Vol = [50] (mm), GWR es K=[0. 96] (mm / day / mm)
370 VHydCond=[0. 055] (mm / hr), END=- 1

*%-----|

372 CONTI NUOUS NASHYD NYHD=["SM_DR"], DT=[1] mi n, AREA=[1122] (ha),
373 DWF=[0] (cms), CNV C=[81], IA=[2. 5] (mm),
374 N=[3. 0], TP=[3. 25] hr s,
375 Continuous simulation parameters:
376 IaRECper=[4] (hr s),
377 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
378 InterEventTime=[12] (hr s)
379 Baseflow simulation parameters:
380 BaseFlowOpti on=[1] ,
381 In it GWR es Vol = [50] (mm), GWR es K=[0. 96] (mm / day / mm)
382 VHydCond=[0. 055] (mm / hr), END=- 1

*%-----|

384 CONTI NUOUS NASHYD NYHD=["MO_DR"], DT=[1] mi n, AREA=[2737] (ha),
385 DWF=[0] (cms), CNV C=[76], IA=[2. 5] (mm),
386 N=[3. 0], TP=[3. 03] hr s,
387 Continuous simulation parameters:
388 IaRECper=[4] (hr s),
389 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),


```

390 InterEventTime=[ 12]( hrs)
391 Baseflow simulation parameters:
392 BaseFlowOption=[ 1] ,
393 InitGWResVol=[ 50]( mm) , GWResK=[ 0.96]( mm/ day/ mm)
394 VHydCond=[ 0.055]( mm/ hr) , END=- 1
395 *%-----|-----|
396 * -JFSA 2020 replaced SW_1 with a detailed model from Stantec Report 2007
397 *CONTINUOUS NASHYD NHYD=["SW_1"], DT=[ 1]mi n, AREA=[ 3176]( ha),
398 * DWF=[ 0]( cms) , CN/C=[ 78] , IA=[ 2.5]( mm),
399 * N=[ 3.0] , TP=[ 3.56]hrs,
400 * Continuous simulation parameters:
401 * IaRECper=[ 4]( hrs),
402 * SMN=[ -1]( mm) , SMAX=[ -1]( mm) , SK=[ 0.010]/( mm),
403 * InterEventTime=[ 12]( hrs)
404 * Baseflow simulation parameters:
405 * BaseFlowOption=[ 1] ,
406 * InitGWResVol=[ 50]( mm) , GWResK=[ 0.96]( mm/ day/ mm)
407 * VHydCond=[ 0.055]( mm/ hr) , END=- 1
408 *%-----|-----|
409 *#
410 *# Routing hydrographs
411 *#
412 *# Starting with the addition of Jock River Headwater and Subwatershed 13
413 *#
414 ADD HYD NHYDsum=["S_N13"], NHYDs to add=["JR_HW"+"SW_13"]
415 *%-----|-----|
416 *#
417 *# Sum of hydrographs from Node 13 routed to Node 13A
418 *# (Approximated cross-section - see cross-section 258)
419 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
420 *#
421 ROUTE CHANNEL NHYDout=["N13A"] , NHYDin=["S_N13"],
422 RDT=[ 1]( mi n),
423 CHLGTH=[ 9074]( m) , CHSLOPE=[ 0.0220]( %),
424 FPSLOPE=[ 0.0220]( %),
425 SECNUM=[ 1.0] , NSEG=[ 1]
426 ( SEGROUGH, SEGDI ST ( m))=[ 0.04, 15.5] NSEG times
427 ( DI STANCE ( m) , ELEVATI ON ( m))=
428 [- 40, 132.5]
429 [- 30, 132]
430 [- 25, 131.5]
431 [- 13, 130]
432 [- 8, 127.00]
433 [- 7, 126.50]
434 [- 6, 126]
435 [- 5.5, 125.50]
436 [0, 123.75]
437 [4.5, 125.50]
438 [6, 126]
439 [7.5, 126.5]
440 [9, 127]
441 [10, 127.5]
442 [11.5, 128.0]
443 [15.5, 129.5]
444 *%-----|-----|
445 *#
446 *# Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
447 *#
448 ADD HYD NHYDsum=["SN13A"], NHYDs to add=["N13A"+"JR_GWM"]
449 *%-----|-----|
450 *#
451 *# Insertion of a reservoir to simulate the effects of the Goodwood Marsh
452 *#
453 ROUTE RESERVOIR NHYDout=["RES_GM"] , NHYDin=["SN13A"],
454 RDT=[ 1]( mi n),
455 TABLE of ( OUTFLOW STORAGE ) values

```

```

456 (cms) - (ha-m)
457 [ 0.0 , 0.0 ]
458 [ 1.991, 2.144 ]
459 [ 2.693, 39.826 ]
460 [ 3.509, 81.697 ]
461 [ 4.578, 318.774 ]
462 [ 5.647, 594.947 ]
463 [ 7.109, 910.219 ]
464 [ 8.616, 1264.589 ]
465 [ 10.371, 1658.057 ]
466 [ 12.402, 2090.622 ]
467 [ 22.056, 3462.487 ]
468 [ -1 , -1 ] (max twenty pts)
469
470 NHYDovf=[ " " ] ,
471 *%-----|-----|
472 *#
473 SAVE HYD NHYD=[ "RES_GM" ], # OF PCYCLES=[ -1 ], I CASEs h=[ -1 ]
474 HYD_FILENAMES=[ "H_RESGM" ]
475 HYD_COMMENT=[ "Out flow from Res GM" ]
476 *%-----|-----|
477 *# Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
478 *# (Approximated cross-section - see cross-section 258)
479 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
480 ROUTE CHANNEL NHYDout=[ "N12" ] , NHYDin=[ "RES_GM" ] ,
481 RDT=[ 1 ] (min) ,
482 CHLGTH=[ 5926 ] (m) , CHSLOPE=[ 0.0759 ] ( % ) ,
483 FPSLOPE=[ 0.0759 ] ( % ) ,
484 SECNUM=[ 1.0 ] , NSEG=[ 1 ]
485 ( SEGROUGH, SEGDIST (m) )=[ 0.04, 15.5 ] NSEG times
486 ( DISTANCE (m) , ELEVATION (m) )=
487 [- 40, 132.5]
488 [- 30, 132]
489 [- 25, 131.5]
490 [- 13, 130]
491 [- 8, 127.00]
492 [- 7, 126.50]
493 [- 6, 126]
494 [- 5.5, 125.50]
495 [ 0, 123.75]
496 [ 4.5, 125.50]
497 [ 6, 126]
498 [ 7.5, 126.5]
499 [ 9, 127]
500 [ 10, 127.5]
501 [ 11.5, 128.00]
502 [ 15.5, 129.5]
503 *%-----|-----|
504 *#
505 *# Addition of Subwatershed Jock River at Ashton to Node 12
506 *#
507 ADD HYD NHYDsum=[ "S_N12" ] , NHYDsto add=[ "N12"+"JR_ASH" ]
508 SAVE HYD NHYD=[ "S_N12" ] , # OF PCYCLES=[ -1 ], I CASEs h=[ -1 ]
509 HYD_FILENAMES=[ "H_SN12" ]
510 HYD_COMMENT=[ "flow at S_N12 near Ashton" ]
511 *%-----|-----|
512 *#
513 *# Sum of hydrographs from Node 12 routed to Node 11
514 *# (Approximated cross-section - see cross-section 258)
515 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
516 *ROUTE CHANNEL NHYDout=[ "N11" ] , NHYDin=[ "S_N12" ] ,
517 * RDT=[ 1 ] (min) ,
518 * CHLGTH=[ 972 ] (m) , CHSLOPE=[ 0.0514 ] ( % ) ,
519 * FPSLOPE=[ 0.0514 ] ( % ) ,
520 * SECNUM=[ 1.0 ] , NSEG=[ 1 ]
521 * ( SEGROUGH, SEGDIST (m) )=[ 0.04, 15.5 ] NSEG times
522 * ( DISTANCE (m) , ELEVATION (m) )=

```

```

522 * [- 40, 132.5]
523 * [- 30, 132]
524 * [- 25, 131.5]
525 * [- 13, 130]
526 * [- 8, 127.00]
527 * [- 7, 126.50]
528 * [- 6, 126]
529 * [- 5.5, 125.50]
530 * [0, 123.75]
531 * [4.5, 125.50]
532 * [6, 126]
533 * [7.5, 126.5]
534 * [9, 127]
535 * [10, 127.5]
536 * [11.5, 128.00]
537 * [15.5, 129.5]
538 *%-----|-----
539 *#
540 *# Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
541 *#
542 ROUTE CHANNEL NHYDout=["Duml1"], NHYDin=["S_N12"],
543 RDT=[1](min),
544 CHLGTH=[972](m), CHSLOPE=[0.054](%),
545 FPSLOPE=[0.054](%),
546 SECNUM=[1.0], NSEG=[1]
547 ( SEGROUGH, SEGDIST (m))=[0.04, 15.5] NSEG times
548 ( DISTANCE (m), ELEVATION (m))=
549 [- 40, 132.5]
550 [- 30, 132]
551 [- 25, 131.5]
552 [- 13, 130]
553 [- 8, 127.00]
554 [- 7, 126.50]
555 [- 6, 126]
556 [- 5.5, 125.50]
557 [0, 123.75]
558 [4.5, 125.50]
559 [6, 126]
560 [7.5, 126.5]
561 [9, 127]
562 [10, 127.5]
563 [11.5, 128.00]
564 [15.5, 129.5]
565 *%-----|-----
566 *#
567 *# Addition of Subwatershed 11 and No Name Creek to Node 11
568 *#
569 ADD HYD NHYDsum=["S_N11"], NHYDstoadd=["Duml1"+"SW_11"+"NN_CK"]
570 *%-----|-----
571 *#
572 *# Sum of hydrographs from Node 11 routed to Node 10
573 *# Section 1
574 *#
575 ROUTE CHANNEL NHYDout=["N10"], NHYDin=["S_N11"],
576 RDT=[1](min),
577 CHLGTH=[14028](m), CHSLOPE=[0.1568](%),
578 FPSLOPE=[0.1568](%),
579 SECNUM=[1.0], NSEG=[5]
580 ( SEGROUGH, SEGDIST (m))=
581 [0.04, -52.82
582 0.1, -6.47
583 -0.05, 6.47
584 0.1, 45.36
585 0.04, 423.88] NSEG times
586 ( DISTANCE (m), ELEVATION (m))=
587 [- 226.24 , 112.50]

```

```

588             [- 167. 50 , 111. 50]
589             [- 106. 81 , 111. 00]
590             [- 92. 37 , 110. 00]
591             [- 52. 82 , 109. 00]
592             [- 24. 90, 109. 00]
593             [- 17. 02, 108. 50]
594             [- 6. 47, 108. 00]
595             [ 6. 47, 108. 00]
596             [ 15. 67, 108. 50]
597             [ 18. 95, 109. 00]
598             [ 45. 36, 109. 50]
599             [ 120. 79, 110. 00]
600             [ 145. 72, 111. 00]
601             [ 181. 56, 111. 50]
602             [ 423. 88, 112. 50]
603 *%-----|-----
604 *#
605 *# Addition of Subwatershed 10 to Node 10
606 *#
607 ADD HYD          NHYDs um=["S_N10"], NHYDs to add=["N10"+"SW_10"]
608 *%-----|-----
609 SAVE HYD         NHYD=["S_N10"], # OF PCYCLES=[- 1], I CASEs h=[- 1]
610                 HYD_ FI LENAME=["H_SN10"]
611                 HYD_ COMMENT=["flow at S_N10: N10 + SW_10"]
612 *%-----|-----
613 *# Addition of Kings Creek to S_N10
614 *#
615 ADD HYD          NHYDs um=["S_N10A"], NHYDs to add=["S_N10"+"KG_CK"]
616 *%-----|-----
617 *#
618 *# Sum of hydrographs from Node 10 routed to Node 9
619 *# Section 2
620 *#
621 ROUTE CHANNEL    NHYDout=["N9"] , NHYDin=["S_N10A"] ,
622                 RDT=[ 1] ( mi n) ,
623                 CHLGTH=[ 3982] ( m) ,   CHSLOPE=[ 0. 0753] ( % ) ,
624                                     FPSLOPE=[ 0. 0753] ( % ) ,
625                 SECNUM=[ 1. 0] ,       NSEG=[ 4]
626                 ( SEGROUGH, SEGDI ST ( m) ) =
627                 [ 0. 04, - 30. 27
628                 0. 05, - 18. 42
629                 - 0. 05, 18. 42
630                 0. 04, 131. 58] NSEG t i m e s
631                 ( DI STANCE ( m) , ELEVATI ON ( m) ) =
632                 [- 446. 74, 106. 00]
633                 [- 415. 68, 105. 50]
634                 [- 285. 40, 105. 00]
635                 [- 173. 77, 104. 50]
636                 [- 144. 95, 104. 00]
637                 [- 111. 18, 103. 50]
638                 [- 94. 06, 103. 00]
639                 [- 71. 02, 102. 50]
640                 [- 30. 27, 102. 00]
641                 [- 19. 33, 100. 00]
642                 [- 18. 42, 99. 50]
643                 [ 18. 42, 99. 50]
644                 [ 20. 77, 100. 00]
645                 [ 27. 93, 101. 00]
646                 [ 52. 29, 101. 00]
647                 [ 68. 80, 101. 50]
648                 [ 79. 66, 103. 00]
649                 [ 91. 50, 103. 50]
650                 [ 131. 58, 104. 00]
651 *%-----|-----
652 *#
653 *# Addition of Subwatershed 9 and Nichols Creek to Node 9

```

```

654  *#
655  ADD HYD          NHYDs um=[ "S_N9" ], NHYDs to add=[ "N9"+"SW_9"+"NC_CK" ]
656  *%-----|-----|
657  *#
658  *# Sum of hydrographs from Node 9 routed to Node 8
659  *# Section 3
660  *#
661  ROUTE CHANNEL    NHYDout =["N8" ] , NHYDin=["S_N9" ] ,
662                  RDT=[ 1 ] ( mi n ) ,
663                  CHLGTH=[ 2269 ] ( m ) ,   CHSLOPE=[ 0.0882 ] ( % ) ,
664                                                    FPSLOPE=[ 0.0882 ] ( % ) ,
665                  SECNUM=[ 1.0 ] ,          NSEG=[ 3 ]
666                  ( SEGROUGH, SEGDI ST ( m ) ) =
667                    [ 0.1, -17.99
668                      -0.045, 17.31
669                      0.1, 456.58 ] NSEG t i m e s
670                  ( DI STANCE ( m ) , ELEVATI ON ( m ) ) =
671                    [ -201.19, 100.50 ]
672                    [ -135.21, 100.00 ]
673                    [ -94.83, 99.50 ]
674                    [ -67.05, 99.00 ]
675                    [ -17.99, 98.50 ]
676                    [ -16.02, 98.00 ]
677                    [ -13.95, 97.50 ]
678                    [ 13.95, 97.50 ]
679                    [ 15.64, 98.00 ]
680                    [ 17.31, 98.50 ]
681                    [ 162.02, 98.50 ]
682                    [ 172.89 , 99.00 ]
683                    [ 314.38, 99.00 ]
684                    [ 343.78, 99.50 ]
685                    [ 365.67, 100.00 ]
686                    [ 376.68, 100.00 ]
687                    [ 393.11, 99.50 ]
688                    [ 404.97, 99.50 ]
689                    [ 431.70, 100.00 ]
690                    [ 456.58, 100.50 ]
691  *%-----|-----|
692  *#
693  *# Addition of Subwatershed 8 and Hobb's Drain to Node 8
694  *#
695  ADD HYD          NHYDs um=[ "S_N8" ], NHYDs to add=[ "N8"+"SW_8"+"HB_DR" ]
696  *%-----|-----|
697  *#
698  *# Sum of hydrographs from Node 8 routed to Node 7
699  *# Section 4
700  *#
701  ROUTE CHANNEL    NHYDout =["N7" ] , NHYDin=["S_N8" ] ,
702                  RDT=[ 1 ] ( mi n ) ,
703                  CHLGTH=[ 3750 ] ( m ) ,   CHSLOPE=[ 0.0533 ] ( % ) ,
704                                                    FPSLOPE=[ 0.0533 ] ( % ) ,
705                  SECNUM=[ 1.0 ] ,          NSEG=[ 3 ]
706                  ( SEGROUGH, SEGDI ST ( m ) ) =
707                    [ 0.12, -18.11
708                      -0.07, 17.22
709                      0.12, 590.05 ] NSEG t i m e s
710                  ( DI STANCE ( m ) , ELEVATI ON ( m ) ) =
711                    [ -433.21, 102.00 ]
712                    [ -425.34, 101.50 ]
713                    [ -377.56, 101.50 ]
714                    [ -366.23, 101.00 ]
715                    [ -202.60, 100.50 ]
716                    [ -96.25, 99.50 ]
717                    [ -68.36 99.00 ]
718                    [ -18.11, 98.50 ]
719                    [ -13.81, 97.50 ]

```

```

720 [ 13. 81, 97. 50]
721 [ 17. 22, 98. 50]
722 [ 161. 95, 98. 50]
723 [ 173. 11, 99. 00]
724 [ 314. 05, 99. 00]
725 [ 365. 52, 100. 00]
726 [ 404. 70, 99. 50]
727 [ 476. 74, 100. 50]
728 [ 502. 31, 101. 00]
729 [ 584. 69, 101. 00]
730 [ 585. 79, 101. 00]
731 [ 590. 05, 102. 00]
732 *%-----|-----
733 *#
734 *# Addition of Subwatershed 7 to Node 7
735 *#
736 ADD HYD          NHYDs um=[ "S_N7" ], NHYDs to add=[ "N7"+"SW_7" ]
737 *%-----|-----
738 SAVE HYD         NHYD=[ "S_N7" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ - 1 ]
739                 HYD_FI LENAME=[ "H_SN7" ]
740                 HYD_COMMENT=[ "flow at S_N7: N7 + SW_7" ]
741 *%-----|-----
742 *# Insertion of a reservoir to simulate the effects of the Richmond Fen.
743 *# Storage area and volumes were estimated from available topo maps.
744 *# Release rate from fen was assumed to be controlled by the downstream
745 *# river cross-section for summer conditions. It is was assumed that for up to
746 *# 0.75 m of water, the main channel of the river provided the storage. Above
747 *# this depth, the wetland starts to signigicantly store water.
748 *#
749 ROUTE RESERVOIR NHYDout =[ "RES_RF" ] , NHYDi n=[ "S_N7" ] ,
750                 RDT=[ 1 ] ( mi n ) ,
751                 TABLE of ( OUTFLOW STORAGE ) values
752                         ( cms ) - ( ha- m )
753                 TABLE of ( OUTFLOW STORAGE ) values
754                         ( cms ) - ( ha- m )
755                         [ 0. 0 , 0. 0 ]
756                         [ 0. 9051, 2. 40]
757                         [ 2. 907, 4. 13]
758                         [ 9. 744, 9. 18]
759                         [ 20. 304, 14. 96]
760                         [ 34. 167, 310. 21]
761                         [ 74. 993, 605. 46]
762                         [ 104. 876, 900. 71]
763                         [ 140. 56, 2892. 00]
764                         [ 225. 00, 3615. 63]
765                         [ - 1 , - 1 ] (max t wenty pts)
766                 NHYDovf=[ " " ] ,
767 *%-----|-----
768 SAVE HYD         NHYD=[ "RES_RF" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ - 1 ]
769                 HYD_FI LENAME=[ "H_Res RF" ]
770                 HYD_COMMENT=[ "out flow of Ri chmnd Fen" ]
771 *%-----|-----
772 *#
773 *# Sum of hydrographs from Node 7 routed to Node 6
774 *# Section 5
775 *#
776 ROUTE CHANNEL   NHYDout =[ "N6" ] , NHYDi n=[ "RES_RF" ] ,
777                 RDT=[ 1 ] ( mi n ) ,
778                 CHLGTH=[ 3056 ] ( m ) , CHSLOPE=[ 0. 0818 ] ( % ) ,
779                 FPSLOPE=[ 0. 0818 ] ( % ) ,
780                 SECNUM=[ 1. 0 ] , NSEG=[ 5 ]
781                 ( SEGROUGH, SEGDI ST ( m ) ) =
782                 [ 0. 025, - 70. 8
783                 0. 1, - 23. 9
784                 - 0. 05, 23. 9
785                 0. 06, 39. 8

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```

786           0. 05, 96. 3] NSEG times
787           ( DI STANCE ( m), ELEVATI ON ( m))=
788             [- 100. 8, 97. 00]
789             [- 70. 8, 96. 50]
790             [- 52. 0, 96. 00]
791             [- 35. 1, 95. 50]
792             [- 30. 6, 95. 00]
793             [- 23. 9, 94. 54]
794             [ 23. 9, 94. 54]
795             [ 39. 8, 95. 00]
796             [ 50. 4, 95. 50]
797             [ 93. 5, 96. 00]
798             [ 94. 9, 96. 50]
799             [ 96. 3, 97. 00]
800 *%-----|-----
801 *#
802 *# Addition of Subwatershed 6 and Van Gaal Drain to Node 6
803 *#
804 ADD HYD           NHYDs um=[ "S_N6" ], NHYDs to add=[ "N6"+"SW_6"+"VG_DR" ]
805 *%-----|-----
806 *#
807 *# Sum of hydrographs from Node 6 routed to Node 5
808 *# Section 6
809 *#
810 ROUTE CHANNEL     NHYDout =[ "N5" ] , NHYDin =[ "S_N6" ] ,
811                   RDT=[ 1] ( mi n),
812                   CHLGTH=[ 1852] ( m),   CHSLOPE=[ 0. 0540] ( %),
813                                     FPSLOPE=[ 0. 0540] ( %),
814                   SECNUM=[ 1. 0],       NSEG=[ 3]
815                   ( SEGROUGH, SEGDI ST ( m))=
816                     [ 0. 035, - 131. 59
817                     - 0. 045, 48. 96
818                     0. 1, 239. 04] NSEG times
819                   ( DI STANCE ( m), ELEVATI ON ( m))=
820                     [- 686. 30, 94. 50]
821                     [- 675. 70, 94. 00]
822                     [- 492. 52, 93. 00]
823                     [- 467. 28, 94. 00]
824                     [- 131. 59, 94. 00]
825                     [- 92. 79, 92. 50]
826                     [- 18. 06, 91. 00]
827                     [ 18. 06, 91. 00]
828                     [ 43. 47, 92. 50]
829                     [ 48. 96, 94. 00]
830                     [ 177. 43, 94. 00]
831                     [ 239. 04, 94. 50]
832 *%-----|-----
833 *#
834 *# Addition of Subwatershed 5 and Flowing Creek to Node 5
835 *#
836 ADD HYD           NHYDs um=[ "S_N5" ], NHYDs to add=[ "N5"+"SW_5"+"FL_CK" ]
837 *%-----|-----
838 *#
839 *# Sum of hydrographs from Node 5 routed to Node 5A
840 *# Section 7
841 *#
842 ROUTE CHANNEL     NHYDout =[ "N5A" ] , NHYDin =[ "S_N5" ] ,
843                   RDT=[ 1] ( mi n),
844                   CHLGTH=[ 556] ( m),   CHSLOPE=[ 0. 0900] ( %),
845                                     FPSLOPE=[ 0. 0900] ( %),
846                   SECNUM=[ 1. 0],       NSEG=[ 4]
847                   ( SEGROUGH, SEGDI ST ( m))=
848                     [ 0. 04, - 41. 5
849                     0. 1, - 14. 0
850                     - 0. 045, 14. 0
851                     0. 1, 41. 1] NSEG times

```

```

852          ( DI STANCE ( m) , ELEVATI ON ( m) ) =
853          [- 275. 8, 93. 00]
854          [- 248. 6, 92. 50]
855          [- 237. 0, 92. 00]
856          [- 219. 3, 91. 50]
857          [- 202. 1, 91. 50]
858          [- 186. 0, 92. 00]
859          [- 129. 2, 92. 00]
860          [- 117. 6, 91. 50]
861          [- 100. 6, 91. 00]
862          [- 41. 5, 91. 00]
863          [- 20. 0, 91. 00]
864          [- 14. 0, 90. 54]
865          [ 14. 0, 90. 54]
866          [ 15. 3, 91. 00]
867          [ 17. 3, 91. 50]
868          [ 38. 4, 92. 00]
869          [ 39. 8, 92. 50]
870          [ 41. 1, 93. 00]
871 *%-----|-----
872 *#
873 *# Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A
874 *#
875 ADD HYD          NHYDs um=[ "S_N5A" ] , NHYDs t o add=[ "N5A"+"SW_5A2"+"SW_5A1" ]
876 *%-----|-----
877 *#
878 *# Sum of hydrographs from Node 5A routed to Node 4
879 *# Section 8
880 *#
881 ROUTE CHANNEL    NHYDout =[ "N4" ] , NHYDi n=[ "S_N5A" ] ,
882                  RDT=[ 1 ] ( mi n) ,
883                  CHLGTH=[ 4630 ] ( m) ,   CHSLOPE=[ 0. 0432 ] ( % ) ,
884                                          FPSLOPE=[ 0. 0432 ] ( % ) ,
885                  SECNUM=[ 1. 0 ] ,       NSEG=[ 3 ]
886          ( SEGROUGH, SEGDI ST ( m) ) =
887          [ 0. 05, -28. 2
888          -0. 035, 28. 2
889          0. 05, 173. 1 ] NSEG t i mes
890          ( DI STANCE ( m) , ELEVATI ON ( m) ) =
891          [- 38. 9, 92. 00]
892          [- 35. 8, 91. 50]
893          [- 33. 3, 91. 00]
894          [- 28. 2, 90. 50]
895          [- 15. 0, 87. 48]
896          [- 5. 0, 88. 34]
897          [ 5. 0, 86. 20]
898          [ 15. 0, 88. 55]
899          [ 28. 2, 90. 50]
900          [ 29. 7, 91. 00]
901          [ 46. 5, 91. 00]
902          [ 127. 8, 91. 00]
903          [ 148. 7, 91. 50]
904          [ 173. 1, 92. 00]
905 *%-----|-----
906 *#
907 *# Addition of Subwatershed 4 and Leamy Creek to Node 4
908 *#
909 ADD HYD          NHYDs um=[ "S_N4" ] , NHYDs t o add=[ "N4"+"SW_4"+"LM_CK" ]
910 SAVE HYD        NHYD=[ "S_N4" ] , # OF PCYCLES=[ - 1 ] , I CASEs h=[ 1 ]
911                HYD_COMMENT=[ "f l ow at S_N4" ]
912 *%-----|-----
913 *#
914 *# Sum of hydrographs from Node 4 routed to Node 2
915 *# Section 9
916 *#
917 ROUTE CHANNEL    NHYDout =[ "N2" ] , NHYDi n=[ "S_N4" ] ,

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918 RDT=[ 1] ( mi n),
919 CHLGTH=[ 1667] ( m), CHSLOPE=[ 0. 0600] ( %),
920 FPSLOPE=[ 0. 0600] ( %),
921 SECNUM=[ 1. 0], NSEG=[ 4]
922 ( SEGROUGH, SEGDI ST ( m))=
923 [ 0. 1, - 28. 0
924 - 0. 04, 28. 4
925 0. 06, 31. 7
926 0. 04, 80. 2] NSEG times
927 ( DI STANCE ( m), ELEVATI ON ( m))=
928 [- 36. 3, 92. 00]
929 [- 32. 6, 91. 50]
930 [- 30. 2, 91. 00]
931 [- 28. 0, 90. 45]
932 [- 15. 0, 87. 48]
933 [- 5. 0, 88. 34]
934 [ 5. 0, 86. 20]
935 [ 15. 0, 88. 55]
936 [ 28. 0, 90. 45]
937 [ 28. 4, 90. 50]
938 [ 30. 4, 91. 00]
939 [ 31. 7, 91. 50]
940 [ 80. 2, 92. 00]
941 *%-----|-----|
942 *#
943 *# Addition of Subwatershed 2 with Monohan Drain and Smith Drain to Node 2
944 *#
945 ADD HYD NHYDs um=[ "S_N2" ], NHYDs to add=[ "N2"+"SW_2"+"SM_DR"+"MO_DR" ]
946 *%-----|-----|
947 SAVE HYD NHYD=[ "S_N2" ], # OF PCYCLES=[ - 1], ICASEs h=[ - 1]
948 HYD_FI LENAME=[ "H_SN2" ]
949 HYD_COMMENT=[ "flow at S_N2 Jock River Gauge at Modie Dr." ]
950 *%-----|-----|
951 *#
952 *# Sum of hydrographs from Node 2 routed to Node 1
953 *# Section 10
954 *#
955 *#*****
956 *%READ HYD NHYD=[ "S_N2" ],
957 *% HYD_FI LENAME=[ "H_S_N2" ]
958 *%-----|-----|
959 *#
960 *# Hydrograph from Node 2 routed to Node 416
961 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 9025
962 *#
963 ROUTE CHANNEL NHYDout =["N_416" ] , NHYDin=["S_N2" ] ,
964 RDT=[ 1] ( mi n),
965 CHLGTH=[ 2327] ( m), CHSLOPE=[ 0. 0498] ( %),
966 FPSLOPE=[ 0. 0498] ( %),
967 SECNUM=[ 1. 0], NSEG=[ 3]
968 ( SEGROUGH, SEGDI ST ( m))=
969 [ 0. 075, - 23. 96
970 - 0. 055, 23. 96
971 0. 075, 157. 38] NSEG times
972 ( DI STANCE ( m), ELEVATI ON ( m))=
973 [- 336. 97, 93. 5]
974 [- 318. 85, 93]
975 [- 259, 92. 5]
976 [- 133. 18, 92]
977 [- 33. 17, 92]
978 [- 27. 21, 92]
979 [- 26. 14, 91. 5]
980 [- 24. 99, 91]
981 [- 23. 96, 90. 5]
982 [- 14. 33, 88. 26]
983 [- 0. 68, 88. 12]

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984 [ 14. 33, 88. 26]
985 [ 23. 96, 90. 5]
986 [ 32. 12, 91]
987 [ 43. 74, 91. 5]
988 [ 57. 09, 92]
989 [ 73. 53, 92. 5]
990 [ 108. 27, 93]
991 [ 125. 88, 93. 5]
992 [ 144. 81, 94]
993 [ 157. 38, 94. 5]
994 *%-----|-----|
995 *#*****|
996 *# Catchment SW1a
997 *# - Portion of RVCA catchment SW1 outside of Reach 1 subwatershed
998 *# - Undeveloped agricultural land
999 *#*****|
1000 CONTINUOUS NASHYD NHYD=[ "SW1a" ], DT=[ 1] mi n, AREA=[ 536. 42] ( ha ),
1001 DWF=[ 0] ( cms ), CN C=[ 72], IA=[ 4. 67] ( mm ),
1002 N=[ 3], TP=[ 2. 79] hr s,
1003 Continuous simulation parameters:
1004 IaRECper=[ 4] ( hr s ),
1005 SM N=[ - 1] ( mm ), SMAX=[ - 1] ( mm ), SK=[ 0. 010] / ( mm ),
1006 InterEvent Time=[ 12] ( hr s)
1007 Baseflow simulation parameters:
1008 BaseFlowOption=[ 1] ,
1009 InitGWRes Vol =[ 50] ( mm ), GWRes K=[ 0. 96] ( mm/ day/ mm)
1010 VHydCond=[ 0. 055] ( mm/ hr ), END=- 1
1011 *%-----|-----|
1012 * -JFSA 2021-02-25 "S-1-Okeefe" is a part of S-1 sub-catchment. It is moved to drain
before station 7245 on Jock River
1013 *CONTINUOUS STANDHYD NHYD=[ "S-1-Okeefe" ], DT=[ 1] ( mi n), AREA=[ 44. 93] ( ha ), XI MP=[ 0. 65],
TI MP=[ 0. 65], DWF=[ 0] ( cms ),
1014 * LOSS=[ 2], SCS curve number CN=[ 75], Pervious surfaces:
I Aper =[ 4. 67] ( mm ), SLPP=[ 2. 0] ( % ),
1015 * LGP=[ 40] ( m ), MNP=[ 0. 25], SCP=[ 0] ( mi n), Impervious surfaces:
I Ai mp=[ 1. 57] ( mm ), SLPI =[ 0. 75] ( % ),
1016 * LGI =[ 547. 296] ( m ), MNI =[ 0. 013], SCI =[ 0] ( mi n),
1017 * Continuous simulation parameters:
1018 * IaRECper =[ 4] ( hr s ), IaRECI mp=[ 4] ( hr s),
1019 * SM N=[ - 1] ( mm ), SMAX=[ - 1] ( mm ), SK=[ 0. 010] / ( mm ),
1020 * InterEvent Time =[ 12] ( hr s), END=- 1
1021 *%-----|-----|
1022 CONTINUOUS NASHYD NHYD=[ "S-1-Okeefe" ], DT=[ 1] mi n, AREA=[ 44. 93] ( ha ),
1023 DWF=[ 0] ( cms ), CN C=[ 77], IA=[ 4. 67] ( mm ),
1024 N=[ 3], TP=[ 1. 049] hr s,
1025 Continuous simulation parameters:
1026 IaRECper=[ 4] ( hr s),
1027 SM N=[ - 1] ( mm ), SMAX=[ - 1] ( mm ), SK=[ 0. 010] / ( mm ),
1028 InterEvent Time =[ 12] ( hr s)
1029 Baseflow simulation parameters:
1030 BaseFlowOption=[ 1] ,
1031 InitGWRes Vol =[ 50] ( mm ), GWRes K=[ 0. 96] ( mm/ day/ mm)
1032 VHydCond=[ 0. 055] ( mm/ hr ), END=- 1
1033 *%-----|-----|
1034 *COMPUTE DUALHYD NHYDi n=[ "S-1-Okeefe" ], CI NLET=[ 4. 796] ( cms ), NI NLET=[ 1],
1035 * Mj NHYD=[ "S-1-OkM" ]
1036 * M nNHYD=[ "S-1-OkMN" ]
1037 * TM STO=[ 9999999] ( cu - m)
1038 *%-----|-----|
1039 *ADD HYD NHYDsum=[ "S-1-OkS" ], NHYDs to add=[ "S-1-OkM" +"S-1-OkMN" ]
1040 *%-----|-----|
1041 *ROUTE RESERVOIR NHYDout=[ "S-1-OkSR" ], NHYDi n=[ "S-1-OkS" ],
1042 * RDT=[ 1] ( mi n),
1043 * TABLE of ( OUTFLOW STORAGE ) values
1044 * ( cms ) - ( ha - m)
1045 * [ 0. 0 , 0. 0 ]

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1046 * [ 0.5370, 1.7917 ]
1047 * [ -1 , -1 ] (max twenty pts)
1048 * NHYDovf=["S-1-OkSovf"]
1049 *%-----|-----|
1050 ADD HYD NHYDsum=["SN_416"], NHYDs to add=["N_416"+"SW_1a"+"S-1-Okeefe"]
1051 *%-----|-----|
1052 SAVE HYD NHYD=["SN_416"], # OF PCYCLES=[-1], I CASEs h=[1]
1053 HYD_COMMENT=["Total Flows at Highway 416"]
1054 *%-----|-----|
1055 *#
1056 *# Hydrograph from Node 416 routed to Node at Okeefe drain
1057 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 7245
1058 *#
1059 ROUTE CHANNEL NHYDout=["N_OK"], NHYDin=["SN_416"],
1060 RDT=[1] (min),
1061 CHLGTH=[497] (m), CHSLOPE=[0.3018] (%),
1062 FPSLOPE=[0.3018] (%),
1063 SECNUM=[1.0], NSEG=[3]
1064 ( SEGROUGH, SEGDI ST (m))=
1065 [0.075, -19.40
1066 -0.055, 19.40
1067 0.075, 377.02] NSEG times
1068 ( DI STANCE (m), ELEVATI ON (m))=
1069 [-1061.41, 92.50]
1070 [-945.91, 92.00]
1071 [-783.64, 91.50]
1072 [-136.74, 91.00]
1073 [-86.04, 91.00]
1074 [-20.86, 91.00]
1075 [-20.18, 90.50]
1076 [-19.40, 90.00]
1077 [-11.68, 86.89]
1078 [0.00, 86.10]
1079 [12.09, 86.81]
1080 [19.40, 90.00]
1081 [34.68, 90.50]
1082 [60.56, 91.00]
1083 [170.14, 91.00]
1084 [175.05, 90.50]
1085 [180.29, 90.00]
1086 [193.41, 90.00]
1087 [195.98, 90.50]
1088 [377.02, 92.50]
1089 *%-----|-----|
1090 *#*****
1091 *# Catchment OKEEFE
1092 *# - To O'Keefe drain (north of the Jock)
1093 *# - Developed with assumed 43% imp.
1094 *# - 2020-12-01 add Okeefe model (Area 513.02 HA) instead of current Okeefe (Area
1095 *# - 2020-11-20 Okeefe detailed model was added as per the NOVATECH SWWHYMD model
1096 *# - (Citi-Gate 2014).
1097 *%-----|-----|
1098 *# POST DEVELOPMENT CONDI TIONS
1099 *%-----|-----|
1100 *#*****
1101 CONTINUOUS NASHYD NHYD=["O-1"], DT=[1] min, AREA=[63.72] (ha),
1102 DWF=[0] (cms), CNVC=[61], IA=[6.2] (mm), N=[3], TP=[.9] hrs,
1103 Continuous simulation parameters:
1104 I a RECper=[4] (hrs),
1105 SM N=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
1106 InterEvent Time=[12] (hrs)
1107 Baseflow simulation parameters:
1108 BaseFlowOption=[1],
1109 In it GWRes Vol=[50] (mm), GWRes K=[0.96] (mm/ day/ mm)
1110 VHydCond=[0.055] (mm/ hr), END=-1

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1110  *%-----|-----
1111  *ROUTE FLOW THROUGH AREA 0-2
1112  ROUTE CHANNEL  NHYDout=["O-1R"], NHYDin=["O-1"], RDT=[1](min),
1113                CHLGTH=[960](m), CHSLOPE=[0.63](%), FPSLOPE=[0.63](%),
1114                SECNUM=[1], NSEG=[3]
1115                ( SEGROUGH, SEGDIST (m))=[0.06, 4 - .043, 6 0.06, 10] NSEG times
1116                ( DISTANCE (m), ELEVATION (m))=[0.00, 2.0]
1117                [0.0, 2.0]
1118                [4.0, 0.0]
1119                [6.0, 0.0]
1120                [10.0, 2.0]
1121  *%-----|-----
1122  CONTINUOUS NASHYD  NHYD=["O-2"], DT=[1]min, AREA=[28.61](ha),
1123                DWF=[0](cms), CNVC=[57], IA=[5.2](mm), N=[3], TP=[1.1]hrs,
1124                Continuous simulation parameters:
1125                IARECper=[4](hrs),
1126                SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1127                InterEventTime=[12](hrs)
1128                Baseflow simulation parameters:
1129                BaseFlowOption=[1],
1130                InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1131                VHydCond=[0.055](mm/hr), END=-1
1132  *%-----|-----
1133  CONTINUOUS NASHYD  NHYD=["O-4"], DT=[1]min, AREA=[46.94](ha),
1134                DWF=[0](cms), CNVC=[49], IA=[9.2](mm), N=[3], TP=[0.9]hrs,
1135                Continuous simulation parameters:
1136                IARECper=[4](hrs),
1137                SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1138                InterEventTime=[12](hrs)
1139                Baseflow simulation parameters:
1140                BaseFlowOption=[1],
1141                InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1142                VHydCond=[0.055](mm/hr), END=-1
1143  *%-----|-----
1144  *TOTAL EXTERNAL FLOW NORTH OF O'KEEFE CT. CROSSING
1145  ADD HYD  NHYDsum=["OKF-N"], NHYDstoadd=["O-1R"+"O-2"+"O-4"]
1146  *%-----|-----
1147  *ROUTE FLOW THROUGH AREA 0-6
1148  ROUTE CHANNEL  ROUTE CHANNEL NHYDout=["OKF-NR"], NHYDin=["OKF-N"], RDT=[1](min),
1149                CHLGTH=[210](m), CHSLOPE=[.81](%), FPSLOPE=[.81](%),
1150                SECNUM=[1], NSEG=[3]
1151                ( SEGROUGH, SEGDIST (m))=[0.043, 22.43 - 0.043, 25.07
1152                0.043, 45.54] NSEG times
1153                ( DISTANCE (m), ELEVATION (m))=[0.00, 3.73]
1154                (14.62, 1.56)
1155                (18.41, 1.44)
1156                (22.43, 0.00)
1157                (25.07, 0.70)
1158                (29.10, 1.79)
1159                (33.73, 2.71)
1160                (45.54, 3.58)
1161  *%-----|-----
1162  CONTINUOUS NASHYD  NHYD=["O-6"], DT=[1]min, AREA=[16.46](ha),
1163                DWF=[0](cms), CNVC=[43], IA=[9.2](mm), N=[3], TP=[0.7]hrs,
1164                Continuous simulation parameters:
1165                IARECper=[4](hrs),
1166                SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1167                InterEventTime=[12](hrs)
1168                Baseflow simulation parameters:
1169                BaseFlowOption=[1],
1170                InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1171                VHydCond=[0.055](mm/hr), END=-1
1172  *%-----|-----
1173  CONTINUOUS STANDHYD  NHYD=["O-3"], DT=[1](min), AREA=[39.67](ha), XI MP=[0.15],
                TIMP=[0.30], DWF=[0](cms),

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1174      LOSS=[ 2], SCS curve number CN=[ 50], Pervious surfaces:
1175      IAper=[ 4.67](mm), SLPP=[ 0.32](%),
1176      LGP=[ 440](m), MNP=[ 0.035], SCP=[ 0](min), Impervious surfaces:
1177      IAimp=[ 1.57](mm), SLPI=[ 0.32](%),
1178      LGI=[ 1880](m), MNI=[ 0.013], SCI=[ 0](min),
1179      Continuous simulation parameters:
1180      IARECper=[ 4](hrs), IARECimp=[ 4](hrs),
1181      SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1182      InterEventTime=[ 12](hrs), END=- 1
1183 *%-----|-----|
1184 CONTINUOUS STANDHYD NHYD=["O-5"], DT=[ 1](min), AREA=[ 60.63](ha), XI MP=[ 0.13],
1185 TIMP=[ 0.26], DWF=[ 0](cms),
1186      LOSS=[ 2], SCS curve number CN=[ 61],
1187      Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1.38](%),
1188      LGP=[ 550](m), MNP=[ 0.035], SCP=[ 0](min), Impervious surfaces:
1189      IAimp=[ 1.57](mm), SLPI=[ 1.38](%),
1190      LGI=[ 1450](m), MNI=[ 0.013], SCI=[ 0](min),
1191      Continuous simulation parameters:
1192      IARECper=[ 4](hrs), IARECimp=[ 4](hrs),
1193      SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1194      InterEventTime=[ 12](hrs), END=- 1
1195 *%-----|-----|
1196 *TOTAL EXTERNAL FLOWS WEST OF THE SITE AND NORTH OF O'KEEFE CRT
1197 *%-----|-----|
1198 ADD HYD      NHYDsum=["PT1"], NHYDs to add=["OKF-NR"+"O-3"+"O-5"+"O-6"]
1199 *%-----|-----|
1200 CONTINUOUS NASHYD NHYD=["O-7"], DT=[ 1]min, AREA=[ 5.28](ha),
1201      DWF=[ 0](cms), CN C=[ 54], IA=[ 7.5](mm), N=[ 3], TP=[ 0.6]hrs,
1202      Continuous simulation parameters:
1203      IARECper=[ 4](hrs),
1204      SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1205      InterEventTime=[ 12](hrs)
1206      Baseflow simulation parameters:
1207      BaseFlowOption=[ 1],
1208      InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
1209      VHydCond=[ 0.055](mm/hr), END=- 1
1210 *%-----|-----|
1211 *ANALYSIS POINT 1 - TOTAL FLOW NORTH OF FALLOWFIELD DR. AND O'KEEFE CRT.
1212 ADD HYD      NHYDsum=["FF"], NHYDs to add=["PT1"+"O-7"]
1213 *%-----|-----|
1214 *ROUTE FLOW through O'Keefe Drain 1
1215 ROUTE CHANNEL NHYDout=["DRAIN1"], NHYDin=["FF"], RDT=[ 1](min),
1216      CHLGTH=[ 302](m), CHSLOPE=[ 1.00](%), FPSLOPE=[ 1.00](%),
1217      SECNUM=[ 1], NSEG=[ 3]
1218      ( SEGROUGH, SEGDIST (m))=[ 0.07, 13.45 -0.043, 16.55 0.07, 30.00] NSEG
1219      times
1220      ( DISTANCE (m), ELEVATION (m))=[ 0.00, 1.70]
1221      ( 3.45, 0.60)
1222      ( 13.45, 0.50)
1223      ( 14.45, 0.00)
1224      ( 15.55, 0.00)
1225      ( 16.55, 0.50)
1226      ( 26.55, 0.60)
1227      ( 30.00, 1.70)
1228 *%-----|-----|
1229 CONTINUOUS NASHYD NHYD=["DI"], DT=[ 1]min, AREA=[ 1.17](ha),
1230      DWF=[ 0](cms), CN C=[ 84], IA=[ 9.0](mm), N=[ 3], TP=[ 0.28]hrs,
1231      Continuous simulation parameters:
1232      IARECper=[ 4](hrs),
1233      SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1234      InterEventTime=[ 12](hrs)
1235      Baseflow simulation parameters:
1236      BaseFlowOption=[ 1],
1237      InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
1238      VHydCond=[ 0.055](mm/hr), END=- 1
1239 *%-----|-----|

```

1235 CONTINUOUS STANDHYD NHYD=["A1"], DT=[1] min, AREA=[2.50](ha), XI MP=[0.68], TI MP=[0.85],
DWF=[0](cms), LOSS=[1]:

1236 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),

1237 Pervious areas: I A per=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),

1238 Impervious areas: I A i mp=[1.57](mm), SLPI=[0.5](%),
LGI=[223.607](m), MNI=[0.013], SCI=[0](min),

1239 Continuous simulation parameters:
1240 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=- 1

1241 *%-----|-----|
1242 ROUTE RESERVOIR NHYDout=["A1-STR"], NHYDin=["A1"], RDT=[1](min),
1243 TABLE of (OUTFLOW STORAGE) values
1244 (cms) - (ha-m)
1245 [0.000 , 0.000]
1246 [0.035 , 0.038]
1247 [0.072 , 0.051]
1248 [0.100 , 0.059]
1249 [0.125 , 0.070]
1250 [0.160 , 0.074]
1251 [0.185 , 0.081]
1252 [-1 , -1] (max twenty pts)
1253 NHYDovf=["A1-OVF"]

1254 *%-----|-----|
1255 CONTINUOUS STANDHYD NHYD=["ST-2"], DT=[1] min, AREA=[0.59](ha), XI MP=[0.46],
TI MP=[0.57], DWF=[0](cms), LOSS=[1]:

1256 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),

1257 Pervious areas: I A per=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),

1258 Impervious areas: I A i mp=[1.57](mm), SLPI=[0.5](%),
LGI=[108.628](m), MNI=[0.013], SCI=[0](min),

1259 Continuous simulation parameters:
1260 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=- 1

1261 *%-----|-----|
1262 ROUTE RESERVOIR NHYDout=["ST2STR"], NHYDin=["ST-2"], RDT=[1](min),
1263 TABLE of (OUTFLOW STORAGE) values
1264 (cms) - (ha-m)
1265 [0.000 , 0.0000]
1266 [0.052 , 0.0010]
1267 [0.053 , 0.0080]
1268 [-1 , -1] (max twenty pts)
1269 NHYDovf=["ST2OVF"]

1270 *%-----|-----|
1271 *%-----|-----|
1272 *TOTAL FLOW NORTH OF STRANDHERD DR. (EAST BRANCH) CROSSING
1273 *%-----|-----|
1274 CONTINUOUS NASHYD NHYD=["O-8"], DT=[1] min, AREA=[60.55](ha),
1275 DWF=[0](cms), CNV C=[69], I A=[4.0](mm), N=[3], TP=[1.0]hrs,
1276 Continuous simulation parameters:
1277 I a REC per=[4](hrs),
1278 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1279 I n t e r E v e n t T i m e=[12](hrs)
1280 Baseflow simulation parameters:
1281 BaseFlowOption=[1],
1282 I n i t G W R e s V o l=[50](mm), G W R e s K=[0.96](mm/day/mm)
1283 VHydCond=[0.055](mm/hr), END=- 1

1284 *%-----|-----|
1285 ROUTE PIPE PTYPE=[2]rect, NHYDout=["O8PIPE"], RNUMBER=[1], PW DTH=[1800](mm),
PHEI GHT=[1200](mm), PLNGTH=[335.1](m),
1286 PROUGH=[0.013], PSLOPE=[0.001](m/m), NHYDin=["O-8"], RDT=[1](min)
1287 *%-----|-----|
1288 *%-----|-----|
1289 ADD HYD NHYDs um=["ST2-IN"], NHYDs to

```

add=[ " DRAI N1 " + " D1 " + " A1 - STR" + " A1 - OVF" + " ST2STR" + " ST2OVF" + " O8PI PE" ]
1290 *%-----|-----|
1291 CONTI NUOUS STANDHYD NHYD=[ " A7" ], DT=[ 1 ] mi n, AREA=[ 3. 51 ] ( ha ), XI MP=[ 0. 68 ], TI MP=[ 0. 85 ],
DWF=[ 0 ] ( c ms ), LOSS=[ 1 ] :
1292 Hort on: Fo=[ 76. 20 ] ( mm/ hr ), Fc=[ 13. 20 ] ( mm/ hr ), DCAY=[ 4. 14 ] ( / hr ),
F=[ 0. 00 ] ( mm ),
1293 Per vious areas: I Aper =[ 4. 67 ] ( mm ), SLPP=[ 0. 5 ] ( % ), LGP=[ 50 ] ( m ),
MNP=[ 0. 250 ], SCP=[ 0 ] ( mi n ),
1294 Impervious areas: I Ai mp=[ 1. 57 ] ( mm ), SLPI =[ 0. 5 ] ( % ),
LGI =[ 264. 953 ] ( m ), MNI =[ 0. 013 ], SCI =[ 0 ] ( mi n ),
1295 Continuous simulation parameters:
1296 IaRECper=[ 4 ] ( hr s ), IaRECI mp=[ 4 ] ( hr s ), Int er Event Ti me=[ 12 ] ( hr s ),
END=- 1
1297 *%-----|-----|
1298 ROUTE RESERVOI R NHYDout =[ " A7 - STR" ], NHYDi n=[ " A7" ], RDT=[ 1 ] ( mi n ),
1299 TABLE of ( OUTFLOW STORAGE ) values
1300 ( c ms ) - ( ha - m )
1301 [ 0. 000 , 0. 000 ]
1302 [ 0. 049 , 0. 054 ]
1303 [ 0. 102 , 0. 072 ]
1304 [ 0. 140 , 0. 082 ]
1305 [ 0. 175 , 0. 099 ]
1306 [ 0. 225 , 0. 105 ]
1307 [ 0. 260 , 0. 114 ]
1308 [ - 1 , - 1 ] ( max t went y pt s )
1309 NHYDovf=[ " A7 - OVF" ]
1310 *%-----|-----|
1311 CONTI NUOUS STANDHYD NHYD=[ " ST - 3" ], DT=[ 1 ] mi n, AREA=[ 0. 71 ] ( ha ), XI MP=[ 0. 46 ],
TI MP=[ 0. 57 ], DWF=[ 0 ] ( c ms ), LOSS=[ 1 ] :
1312 Hort on: Fo=[ 76. 20 ] ( mm/ hr ), Fc=[ 13. 20 ] ( mm/ hr ), DCAY=[ 4. 14 ] ( / hr ),
F=[ 0. 00 ] ( mm ),
1313 Per vious areas: I Aper =[ 4. 67 ] ( mm ), SLPP=[ 0. 5 ] ( % ), LGP=[ 50 ] ( m ),
MNP=[ 0. 250 ], SCP=[ 0 ] ( mi n ),
1314 Impervious areas: I Ai mp=[ 1. 57 ] ( mm ), SLPI =[ 0. 5 ] ( % ),
LGI =[ 119. 164 ] ( m ), MNI =[ 0. 013 ], SCI =[ 0 ] ( mi n ),
1315 Continuous simulation parameters:
1316 IaRECper=[ 4 ] ( hr s ), IaRECI mp=[ 4 ] ( hr s ), Int er Event Ti me=[ 12 ] ( hr s ),
END=- 1
1317 *%-----|-----|
1318 ROUTE RESERVOI R NHYDout =[ " ST3STR" ], NHYDi n=[ " ST - 3" ], RDT=[ 1 ] ( mi n ),
1319 TABLE of ( OUTFLOW STORAGE ) values
1320 ( c ms ) - ( ha - m )
1321 [ 0. 000 , 0. 0000 ]
1322 [ 0. 063 , 0. 0010 ]
1323 [ 0. 064 , 0. 0094 ]
1324 [ - 1 , - 1 ] ( max t went y pt s )
1325 NHYDovf=[ " ST3OVF" ]
1326 *%-----|-----|
1327 *ANALYSIS POINT 2 - TOTAL FLOW AT OUTLET OF STREET 2/3 INTERSECTION
1328 *%-----|-----|
1329 ADD HYD NHYDsum=[ " PT2ST3" ], NHYDs to
add=[ " ST2 - I N" + " A7 - STR" + " A7 - OVF" + " ST3STR" + " ST3OVF" ]
1330 *%-----|-----|
1331 *ROUTE FLOW through O Keefe Drain 2
1332 ROUTE CHANNEL NHYDout =[ " DRAI N2" ], NHYDi n=[ " PT2ST3" ], RDT=[ 1 ] ( mi n ),
1333 CHLGTH=[ 592 ] { m }, CHSLOPE=[ . 23 ] ( % ), FPSLOPE=[ . 23 ] ( % ),
1334 SECNUM=[ 1 ], NSEG=[ 3 ]
1335 ( SEGROUGH, SEGDI ST ( m ) )=[ 0. 07, 12. 60 - 0. 043, 17. 40 0. 07, 30. 00 ] NSEG
ti mes
1336 ( DI STANCE ( m ), ELEVATI ON ( m ) )=[ 0. 00, 1. 70 ]
1337 ( 2. 60, 0. 95 )
1338 ( 12. 60, 0. 75 )
1339 ( 14. 10, 0. 00 )
1340 ( 15. 90, 0. 00 )
1341 ( 17. 40, 0. 75 )
1342 ( 27. 40, 0. 95 )

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1343         (30.00, 1.70)
1344 *%-----|-----|
1345 CONTINUOUS NASHYD NHYD=["D2"], DT=[1] min, AREA=[2.28](ha), DWF=[0](cms), CNVC=[84],
IA=[9.0](mm),
1346 N=[3], TP=[0.99] hrs,
1347 Continuous simulation parameters:
1348 IARECper=[4](hrs),
1349 SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1350 InterEventTime=[12](hrs)
1351 Baseflow simulation parameters:
1352 BaseFlowOption=[1],
1353 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1354 VHydCond=[0.055](mm/hr), END=-1
1355 *%-----|-----|
1356 CONTINUOUS STANDHYD NHYD=["A17"], DT=[1] min, AREA=[12.04](ha), XI MP=[0.68],
TI MP=[0.85], DWF=[0](cms), LOSS=[1]:
1357 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1358 PerVIOUS areas: IAPER=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1359 ImperVIOUS areas: IAIMP=[1.57](mm), SLPI=[0.5](%),
LGI=[490.714](m), MNI=[0.013], SCI=[0](min),
1360 Continuous simulation parameters:
1361 IARECper=[4](hrs), IARECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1362 *%-----|-----|
1363 ROUTE RESERVOIR NHYDout=["A17STR"], NHYDin=["A17"], RDT=[1](min),
1364 TABLE of ( OUTFLOW STORAGE ) values
1365 (cms) - (ha-m)
1366 [ 0.000 , 0.000 ]
1367 [ 0.169 , 0.185 ]
1368 [ 0.349 , 0.248 ]
1369 [ 0.482 , 0.283 ]
1370 [ 0.602 , 0.338 ]
1371 [ 0.771 , 0.359 ]
1372 [ 0.891 , 0.391 ]
1373 [ -1 , -1 ] (max twenty pts)
1374 NHYDovf=["A17OVF"]
1375 *%-----|-----|
1376 CONTINUOUS STANDHYD NHYD=["ST-4"], DT=[1] min, AREA=[0.35](ha), XI MP=[0.46],
TI MP=[0.57], DWF=[0](cms), LOSS=[1]:
1377 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1378 PerVIOUS areas: IAPER=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1379 ImperVIOUS areas: IAIMP=[1.57](mm), SLPI=[0.5](%), LGI=[83.666](m),
MNI=[0.013], SCI=[0](min),
1380 Continuous simulation parameters:
1381 IARECper=[4](hrs), IARECimp=[4](hrs), InterEventTime=[12](hrs),
END=-1
1382 *%-----|-----|
1383 ROUTE RESERVOIR NHYDout=["ST4STR"], NHYDin=["ST-4"], RDT=[1](min),
1384 TABLE of ( OUTFLOW STORAGE ) values
1385 (cms) - (ha-m)
1386 [ 0.000 , 0.0000 ]
1387 [ 0.031 , 0.0010 ]
1388 [ 0.032 , 0.0050 ]
1389 [ -1 , -1 ] (max twenty pts)
1390 NHYDovf=["ST4OVF"]
1391 *%-----|-----|
1392 CONTINUOUS STANDHYD NHYD=["A18"], DT=[1] min, AREA=[5.30](ha), XI MP=[0.68], TI MP=[0.85],
DWF=[0](cms), LOSS=[1]:
1393 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1394 PerVIOUS areas: IAPER=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),

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1395      Impervious areas: IAImp=[ 1.57](mm), SLPI=[ 0.5](%),
1396      LGL=[ 325.576](m), MNI=[ 0.013], SCI=[ 0](min),
1397      Continuous simulation parameters:
1397      IARECper=[ 4](hrs), IARECimp=[ 4](hrs), InterEventTime=[ 12](hrs),
1397      END=- 1
1398  *%-----|-----|
1399  ROUTE RESERVOIR  NHYDout=["A18STR"], NHYDin=["A18"], RDT=[ 1](min),
1400                    TABLE of ( OUTFLOW STORAGE ) values
1401                    (cms) - (ha-m)
1402                    [ 0.000 , 0.000 ]
1403                    [ 0.074 , 0.082 ]
1404                    [ 0.154 , 0.109 ]
1405                    [ 0.212 , 0.125 ]
1406                    [ 0.265 , 0.149 ]
1407                    [ 0.339 , 0.158 ]
1408                    [ 0.392 , 0.172 ]
1409                    [ -1 , -1 ] (max twenty pts)
1410                    NHYDovf=["A18OVF"]
1411  *%-----|-----|
1412  *ANALYSIS POINT 3 - TOTAL FLOW AT OUTLET OF STREET 4
1413  *%-----|-----|
1414  ADD HYD           NHYDs um=["PT3ST4"], NHYDs to
1414  add=["DRAIN2"+"D2"+"A17STR"+"A17OVF"+"ST4STR"+"ST4OVF"+"A18STR"+"A18OVF"]
1415  *%-----|-----|
1416  *ROUTE FLOW through O Keefe Drain 3
1417  ROUTE CHANNEL    NHYDout=["DRAIN3"], NHYDin=["PT3ST4"], RDT=[ 1](min),
1418                  CHLGTH=[ 525](m), CHSLOPE=[.23](%), FPSLOPE=[.23](%),
1419                  SECNUM=[ 1], NSEG=[ 3]
1420                  ( SEGROUGH, SEGDIST (m))=[ 0.07, 12.50 -0.043, 17.50 0.07, 30.00] NSEG
1421                  times
1421                  ( DISTANCE (m), ELEVATION (m))=[ 0.00, 1.70]
1422                  ( 2.50, 1.00)
1423                  ( 12.50, 0.80)
1424                  ( 14.10, 0.00)
1425                  ( 15.90, 0.00)
1426                  ( 17.50, 0.80)
1427                  ( 27.50, 1.00)
1428                  ( 30.00, 1.70)
1429  *%-----|-----|
1430  CONTINUOUS NASHYD NHYD=["D3"], DT=[ 1]min, AREA=[ 2.51](ha),
1431                  DWF=[ 0](cms), CNVC=[ 86], IA=[ 8.7](mm), N=[ 3], TP=[ 0.73]hrs,
1432                  Continuous simulation parameters:
1433                  IARECper=[ 4](hrs),
1434                  SMIN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1435                  InterEventTime=[ 12](hrs)
1436                  Baseflow simulation parameters:
1437                  BaseFlowOption=[ 1],
1438                  InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
1439                  VHydCond=[ 0.055](mm/hr), END=- 1
1440  *%-----|-----|
1441  CONTINUOUS STANDHYD NHYD=["C1"], DT=[ 1]min, AREA=[ 3.41](ha), XI MP=[ 0.68], TI MP=[ 0.85],
1441  DWF=[ 0](cms), LOSS=[ 1]:
1442                  Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
1442                  F=[ 0.00](mm),
1443                  Pervious areas: IAPER=[ 4.67](mm), SLPP=[ 0.5](%), LGP=[ 50](m),
1443                  MNP=[ 0.250], SCP=[ 0](min),
1444                  Impervious areas: IAImp=[ 1.57](mm), SLPI=[ 0.5](%),
1444                  LGL=[ 261.151](m), MNI=[ 0.013], SCI=[ 0](min),
1445                  Continuous simulation parameters:
1446                  IARECper=[ 4](hrs), IARECimp=[ 4](hrs), InterEventTime=[ 12](hrs),
1446                  END=- 1
1447  *%-----|-----|
1448  ROUTE RESERVOIR  NHYDout=["C1-STR"], NHYDin=["C1"], RDT=[ 1](min),
1449                    TABLE of ( OUTFLOW STORAGE ) values
1450                    (cms) - (ha-m)
1451                    [ 0.000 , 0.000 ]

```

```

1452         [ 0.048 , 0.052 ]
1453         [ 0.099 , 0.070 ]
1454         [ 0.136 , 0.080 ]
1455         [ 0.170 , 0.096 ]
1456         [ 0.218 , 0.102 ]
1457         [ 0.252 , 0.111 ]
1458         [ -1 , -1 ] (max twenty pts)
1459         NHYDovf=["C1-OVF"]
1460 *%-----|-----|
1461 CONTINUOUS STANDHYD NHYD=["ST-5"], DT=[1] min, AREA=[0.45](ha), XI MP=[0.46],
TI MP=[0.57], DWF=[0](cms), LOSS=[1]:
1462 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1463 Previous areas: I A per=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1464 Impervious areas: I A i mp=[1.57](mm), SLPI=[0.5](%), LGI=[94.868](m),
MNI=[0.013], SCI=[0](min),
1465 Continuous simulation parameters:
1466 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=-1
1467 *%-----|-----|
1468 ROUTE RESERVOIR NHYDout=["ST5STR"], NHYDin=["ST-5"], RDT=[1](min),
1469 TABLE of ( OUTFLOW STORAGE ) values
1470 (cms) - (ha-m)
1471 [ 0.000 , 0.0000 ]
1472 [ 0.040 , 0.0010 ]
1473 [ 0.041 , 0.0062 ]
1474 [ -1 , -1 ] (max twenty pts)
1475 NHYDovf=["ST5OVF"]
1476 *%-----|-----|
1477 ADD HYD NHYDs um=["ST5-E"], NHYDs t o
add=["DRAIN3"+"D3"+"C1-STR"+"C1-OVF"+"ST5STR"+"ST5OVF"]
1478 *%-----|-----|
1479 CONTINUOUS STANDHYD NHYD=["STRAND"], DT=[1](min), AREA=[7.59](ha),
1480 XI MP=[0.64], TI MP=[0.85], DWF=[0](cms), LOSS=[1]:
1481 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1482 Previous areas: I A per=[4.67](mm), SLPP=[0.5](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
1483 Impervious areas: I A i mp=[1.57](mm), SLPI=[0.5](%), LGI=[1230](m),
MNI=[0.013], SCI=[0](min),
1484 Continuous simulation parameters:
1485 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=-1
1486 *%-----|-----|
1487 ROUTE RESERVOIR NHYDout=["S-POND"], NHYDin=["STRAND"], RDT=[1](min),
1488 TABLE of ( OUTFLOW STORAGE ) values
1489 (cms) - (ha-m)
1490 [ 0.000 , 0.000 ]
1491 [ 0.033 , 0.188 ]
1492 [ 0.057 , 0.253 ]
1493 [ 0.104 , 0.287 ]
1494 [ 0.160 , 0.336 ]
1495 [ 0.340 , 0.346 ]
1496 [ 0.471 , 0.360 ]
1497 [ 0.824 , 0.390 ]
1498 [ -1 , -1 ] (max twenty pts)
1499 NHYDovf=["S-OVF"]
1500 *%-----|-----|
1501 ADD HYD NHYDs um=["SSAOUT"], NHYDs t o add=["ST5-E"+"S-POND"+"S-OVF"]
1502 *%-----|-----|
1503 SAVE HYD NHYD=["SSAOUT"], # OF PCYCLES=[5], I CASEs h=[1]
1504 HYD_COMMENT=["SSAOUT"]
1505 *%-----|-----|
1506 CONTINUOUS STANDHYD NHYD=["Area-A"], DT=[1] min, AREA=[66.75](ha), XI MP=[0.64],
TI MP=[0.80], DWF=[0](cms), LOSS=[1]:

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1507      Horton: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14]( / hr),
1508      F=[ 0.00](mm),
1509      Pervious areas: IAper=[ 4.67](mm), SLPP=[ 0.5](%), LGP=[ 50](m),
1510      MNP=[ 0.250], SCP=[ 0](min),
1511      Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 0.5](%),
1512      LGI=[ 1155.422](m), MNI=[ 0.013], SCI=[ 0](min),
1513      Continuous simulation parameters:
1514      IARECper=[ 4](hrs), IARECimp=[ 4](hrs), InterEventTime=[ 12](hrs),
1515      END=- 1
1516  *%-----|-----|
1517  SAVE HYD      NHYD=["Area-A"], # OF PCYCLES=[ 1], ICASEsh=[ 1]
1518  HYD_COMMENT=["SMMF-A Inflow"]
1519  *%-----|-----|
1520  ROUTE RESERVOIR  NHYDout=["SWMF-A"], NHYDin=["Area-A"], RDT=[ 1](min),
1521  TABLE of ( OUTFLOW STORAGE ) values
1522  (cms) - (ha-m)
1523  [ 0.000 , 0.000 ]
1524  [ 0.103 , 1.077 ]
1525  [ 0.128 , 1.749 ]
1526  [ 0.382 , 2.282 ]
1527  [ 0.703 , 2.582 ]
1528  [ 1.256 , 2.978 ]
1529  [ 1.567 , 3.202 ]
1530  [ 1.955 , 3.493 ]
1531  [ 2.100 , 3.600 ]
1532  [ -1 , -1 ] (max twenty pts)
1533  NHYDovf=["SWWAOV"]
1534  *%-----|-----|
1535  SAVE HYD      NHYD=["SWMF-A"], # OF PCYCLES=[ 1], ICASEsh=[ 1]
1536  HYD_COMMENT=["SMMF-A Outflow"]
1537  *%-----|-----|
1538  *ANALYSIS POINT 4 - TOTAL FLOW AT OUTLET OF STREET 5
1539  *%-----|-----|
1540  ADD HYD      NHYDsum=["PT4ST5"], NHYDsto add=["SSAOUT"+"SWMF-A"+"SWWAOV"]
1541  *%-----|-----|
1542  CONTINUOUS STANDHYD NHYD=["C6"], DT=[ 1]min, AREA=[ 1.87](ha), XI MP=[ 0.68], TI MP=[ 0.85],
1543  DWF=[ 0](cms), LOSS=[ 1]:
1544      Horton: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14]( / hr),
1545      F=[ 0.00](mm),
1546      Pervious areas: IAper=[ 4.67](mm), SLPP=[ 0.5](%), LGP=[ 50](m),
1547      MNP=[ 0.250], SCP=[ 0](min),
1548      Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 0.5](%),
1549      LGI=[ 193.391](m), MNI=[ 0.013], SCI=[ 0](min),
1550      Continuous simulation parameters:
1551      IARECper=[ 4](hrs), IARECimp=[ 4](hrs), InterEventTime=[ 12](hrs),
1552      END=- 1
1553  *%-----|-----|
1554  ROUTE RESERVOIR  NHYDout=["C6-STR"], NHYDin=["C6"], RDT=[ 1](min),
1555  TABLE of ( OUTFLOW STORAGE ) values
1556  (cms) - (ha-m)
1557  [ 0.000 , 0.000 ]
1558  [ 0.026 , 0.029 ]
1559  [ 0.054 , 0.038 ]
1560  [ 0.075 , 0.044 ]
1561  [ 0.093 , 0.052 ]
1562  [ 0.120 , 0.056 ]
1563  [ 0.138 , 0.061 ]
1564  [ -1 , -1 ] (max twenty pts)
1565  NHYDovf=["C6-OVF"]
1566  *%-----|-----|
1567  CONTINUOUS STANDHYD NHYD=["C7"], DT=[ 1]min, AREA=[ 1.62](ha), XI MP=[ 0.68], TI MP=[ 0.85],
1568  DWF=[ 0](cms), LOSS=[ 1]:
1569      Horton: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14]( / hr),
1570      F=[ 0.00](mm),
1571      Pervious areas: IAper=[ 4.67](mm), SLPP=[ 0.5](%), LGP=[ 50](m),
1572      MNP=[ 0.250], SCP=[ 0](min),

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1561      Impervious areas: I Aimp=[ 1.57](mm), SLPI=[ 0.5](%),
1562      LGL=[ 180.000](m), MNI=[ 0.013], SCI=[ 0](min),
1563      Continuous simulation parameters:
1564      IARECper=[ 4](hrs), IARECimp=[ 4](hrs), InterEventTime=[ 12](hrs),
1565      END=- 1
1566 *%-----|-----|
1567 ROUTE RESERVOIR NHYDout=["C7-STR"], NHYDin=["C7"], RDT=[ 1](min),
1568      TABLE of ( OUTFLOW STORAGE ) values
1569      (cms) - (ha-m)
1570      [ 0.000 , 0.000 ]
1571      [ 0.023 , 0.025 ]
1572      [ 0.047 , 0.033 ]
1573      [ 0.065 , 0.038 ]
1574      [ 0.081 , 0.045 ]
1575      [ 0.104 , 0.048 ]
1576      [ 0.120 , 0.053 ]
1577      [ -1 , -1 ] (max twenty pts)
1578      NHYDovf=["C7-OVF"]
1579 *%-----|-----|
1580 CONTINUOUS STANDHYD NHYD=["ST-6"], DT=[ 1]min, AREA=[ 0.41](ha), XI MP=[ 0.46], TI MP=[ 0.57],
1581      DWF=[ 0](cms), LOSS=[ 1]:
1582      Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
1583      F=[ 0.00](mm),
1584      Pervious areas: I Aper=[ 4.67](mm), SLPP=[ 0.5](%), LGP=[ 50](m),
1585      MNP=[ 0.250], SCP=[ 0](min),
1586      Impervious areas: I Aimp=[ 1.57](mm), SLPI=[ 0.5](%), LGL=[ 90.554](m),
1587      MNI=[ 0.013], SCI=[ 0](min),
1588      Continuous simulation parameters:
1589      IARECper=[ 4](hrs), IARECimp=[ 4](hrs), InterEventTime=[ 12](hrs),
1590      END=- 1
1591 *%-----|-----|
1592 ROUTE RESERVOIR NHYDout=["ST6STR"], NHYDin=["ST-6"], RDT=[ 1](min),
1593      TABLE of ( OUTFLOW STORAGE ) values
1594      (cms) - (ha-m)
1595      [ 0.000 , 0.0000 ]
1596      [ 0.036 , 0.0010 ]
1597      [ 0.037 , 0.0058 ]
1598      [ -1 , -1 ] (max twenty pts)
1599      NHYDovf=["ST6OVF"]
1600 *%-----|-----|
1601 *ANALYSIS POINT 5 - TOTAL FLOW AT OUTLET OF STREET 6
1602 *%-----|-----|
1603 ADD HYD NHYDs um=["PT5ST6"], NHYDs to
1604      add=["PT4ST5"+"C6-STR"+"C6-OVF"+"C7-STR"+"C7-OVF"+"ST6STR"+"ST6OVF"]
1605 *%-----|-----|
1606 *ROUTE FLOW through O Keefe Drain 4
1607 ROUTE CHANNEL NHYDout=["DRAIN4"], NHYDin=["PT5ST6"], RDT=[ 1](min),
1608      CHLGTH=[ 324]{m}, CHSLOPE=[.10](%), FPSLOPE=[.10](%),
1609      SECNUM=[ 1], NSEG=[ 3]
1610      ( SEGROUGH, SEGDIST (m))=[ 0.07, 12.00 -0.043, 18.00 0.07, 30.00] NSEG
1611      times
1612      ( DISTANCE (m), ELEVATION (m))=[ 0.00, 2.00]
1613      ( 2.00, 1.20)
1614      ( 12.00, 1.00)
1615      ( 14.00, 0.00)
1616      ( 16.00, 0.00)
1617      ( 18.00, 1.00)
1618      ( 28.00, 1.20)
1619      ( 30.00, 2.00)
1620 *%-----|-----|
1621 CONTINUOUS NASHYD NHYD=["D4"], DT=[ 1]min, AREA=[ 1.73](ha), DWF=[ 0](cms), CNVC=[ 88],
1622      IA=[ 8.4](mm),
1623      N=[ 3], TP=[ 0.60]hrs,
1624      Continuous simulation parameters:
1625      IARECper=[ 4](hrs),
1626      SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),

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1617 InterEventTime=[ 12]( hrs)
1618 Baseflow simulation parameters:
1619 BaseFlowOption=[ 1] ,
1620 InitGWResVol=[ 50]( mm) , GWResK=[ 0.96]( mm/ day/ mm)
1621 VHydCond=[ 0.055]( mm/ hr) , END=- 1
1622 *%-----|-----|
1623 CONTINUOUS STANDHYD NHYD=[ "Area- B" ] , DT=[ 1] mi n , AREA=[ 24.04]( ha) , XI MP=[ 0.62] ,
TI MP=[ 0.77] , DWF=[ 0]( cms) , LOSS=[ 1] :
1624 Horton: Fo=[ 76.20]( mm/ hr) , Fc=[ 13.20]( mm/ hr) , DCAY=[ 4.14]( / hr) ,
F=[ 0.00]( mm) ,
1625 Pervious areas: IAper=[ 4.67]( mm) , SLPP=[ 1.4]( %) , LGP=[ 50]( m) ,
MNP=[ 0.250] , SCP=[ 0]( mi n) ,
1626 Impervious areas: IAimp=[ 1.57]( mm) , SLPI=[ 1.4]( %) ,
LGI=[ 693.397]( m) , MNI=[ 0.013] , SCI=[ 0]( mi n) ,
1627 Continuous simulation parameters:
1628 IaRECper=[ 4]( hrs) , IaRECI mp=[ 4]( hrs) , InterEventTime=[ 12]( hrs) ,
END=- 1
1629 *%-----|-----|
1630 ROUTE RESERVOIR NHYDout=[ "SWMF- B" ] , NHYDin=[ "Area- B" ] , RDT=[ 1]( mi n) ,
1631 TABLE of ( OUTFLOW STORAGE ) values
1632 ( cms) - ( ha- m)
1633 [ 0.000 , 0.000 ]
1634 [ 0.025 , 0.090 ]
1635 [ 0.175 , 0.510 ]
1636 [ 0.350 , 0.710 ]
1637 [ 0.495 , 0.820 ]
1638 [ 0.648 , 0.980 ]
1639 [ 0.965 , 1.045 ]
1640 [ 1.072 , 1.140 ]
1641 [ -1 , -1 ] (max twenty pts)
1642 NHYDovf=[ "SWMBOVF" ]
1643 *%-----|-----|
1644 ADD HYD NHYDs um=[ "D4- EX" ] , NHYDs to add=[ "DRAIN4"+"D4"+"SWMF- B"+"SWMBOVF" ]
1645 *%-----|-----|
1646 *ROUTE FLOW THROUGH O'Keefe Drain 5
1647 * JFSA: Nov. 2020, added en points to close X-Section
1648 ROUTE CHANNEL NHYDout=[ "DRAIN5" ] , NHYDin=[ "D4- EX" ] , RDT=[ 1]( mi n) ,
1649 CHLGTH=[ 413.0]( m) , CHSLOPE=[ 0.16]( %) , FPSLOPE=[ 0.16]( %) ,
1650 SECNUM=[ 1] , NSEG=[ 3]
1651 ( SEGROUGH, SEGDIST ( m) )=[ 0.043, 12.29 -0.033, 17.97
1652 0.043, 32.84] NSEG times
1653 ( DISTANCE ( m) , ELEVATION ( m) )=(-0.01, 2.50)
1654 [ 0.00, 1.41]
1655 [ 6.13, 0.97]
1656 [ 12.29, 0.89]
1657 [ 15.71, 0.00]
1658 [ 17.97, 0.39]
1659 [ 23.04, 0.35]
1660 [ 32.83, 0.96]
1661 ( 32.84, 2.50)
1662 *%-----|-----|
1663 CONTINUOUS NASHYD NHYD=[ "D5" ] , DT=[ 1] mi n , AREA=[ 1.90]( ha) ,
1664 DWF=[ 0]( cms) , CNVC=[ 86] , IA=[ 8.7]( mm) , N=[ 3] , TP=[ 0.69] hr s ,
1665 Continuous simulation parameters:
1666 IaRECper=[ 4]( hrs) ,
1667 SMN=[ -1]( mm) , SMAX=[ -1]( mm) , SK=[ 0.010]/( mm) ,
1668 InterEventTime=[ 12]( hrs)
1669 Baseflow simulation parameters:
1670 BaseFlowOption=[ 1] ,
1671 InitGWResVol=[ 50]( mm) , GWResK=[ 0.96]( mm/ day/ mm)
1672 VHydCond=[ 0.055]( mm/ hr) , END=- 1
1673 *%-----|-----|
1674 *EXTERNAL FLOWS SOUTHEAST OF THE SITE NORTH OF McKENNA CASEY DR.
1675 CONTINUOUS NASHYD NHYD=[ "O-13SDF" ] , DT=[ 1] mi n , AREA=[ 9.74]( ha) ,
1676 DWF=[ 0]( cms) , CNVC=[ 81] , IA=[ 4.0]( mm) , N=[ 3] , TP=[ .43] hr s ,
1677 Continuous simulation parameters:

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1678 IaREcper=[ 4] (hrs),
1679 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010]/(mm),
1680 InterEventTime=[ 12] (hrs)
1681 Baseflow simulation parameters:
1682 BaseFlowOption=[ 1] ,
1683 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/day/mm)
1684 VHydCond=[ 0.055] (mm/hr), END=-1
1685 *%-----|-----
1686 *SNOW DISPOSAL FACILITY
1687 *PARAMETERS BASED ON ROBINSON 2006 MODEL
1688 ROUTE RESERVOIR NHYDout=["SDF"], NHYDin=["O-13SDF"], RDT=[ 1] (min),
1689 TABLE of ( OUTFLOW STORAGE ) values
1690 (cms) - (ha-m)
1691 [0.000, 0.000]
1692 [0.150, 0.600]
1693 (0.200, 1.500)
1694 [ -1 , -1 ] (max twenty pts)
1695 NHYDovf=["OVFSDF"]
1696 *%-----|-----
1697 *ANALYSIS POINT 6 - McKenna Casey Dr.
1698 *%-----|-----
1699 ADD HYD NHYDs um=["PT6MC"], NHYDs to add=["DRAIN5"+"D5"+"SDF"]
1700 *%-----|-----
1701 CONTINUOUS NASHYD NHYD=["O-15"], DT=[ 1] min, AREA=[ 10.67] (ha),
1702 DWF=[ 0] (cms), CNVC=[ 82], IA=[ 7.5] (mm), N=[ 3], TP=[ 0.30] hrs,
1703 Continuous simulation parameters:
1704 IaREcper=[ 4] (hrs),
1705 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010]/(mm),
1706 InterEventTime=[ 12] (hrs)
1707 Baseflow simulation parameters:
1708 BaseFlowOption=[ 1] ,
1709 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/day/mm)
1710 VHydCond=[ 0.055] (mm/hr), END=-1
1711 *%-----|-----
1712 *TOTAL FLOW NORTH OF MCKENNA CASEY DR.
1713 ADD HYD NHYDs um=["MC"], NHYDs to add=["PT6MC"+"O-15"]
1714 *%-----|-----
1715 *ROUTE FLOW THROUGH AREA O-14
1716 * JFSA: Nov. 2020, added end points to close X-section
1717 ROUTE CHANNEL NHYDout=["O-14Ch"], NHYDin=["MC"], RDT=[ 1] (min),
1718 CHLGTH=[ 845.3] (m), CHSLOPE=[ 0.10] (%), FPSLOPE=[ 0.10] (%),
1719 SECNUM=[ 1], NSEG=[ 3]
1720 ( SEGROUGH, SEGDIST (m))=[ 0.06, 15.00 -0.033, 18.04 0.06, 31.85] NSEG
times
1721 ( DISTANCE (m), ELEVATION (m))=[ -0.01, 2.5
1722 (0.00, 1.53]
1723 (5.56, 1.47)
1724 (9.21, 1.45)
1725 (12.45, 1.53)
1726 (13.70, 1.50)
1727 (15.00, 0.69)
1728 (15.34, 0.00)
1729 (16.51, 0.05)
1730 (17.30, 0.17)
1731 (18.04, 0.74)
1732 (19.29, 1.32)
1733 (22.73, 1.47)
1734 (31.84, 1.41)
1735 (31.85, 2.50)
1736 *%-----|-----
1737 *% -Change O-14 from NASHYD to STANDHYD, name it "S-1-Okeefe" and add it to S-1
subcatchment based on Project 1474-BCDC, JFSA, Nov. 2020
1738 *% -JFSA 2021-02-16, add detailed subcatchment drainage area for each subcatchment
in Corrigan sub-catchment. After adding part of O-14 to S_1 sub-catchment so O-14
becomes 5 ha instead of 30.02 ha and TP becomes 0.133 (5*0.8/30.02) instead of 0.8
1739 CONTINUOUS NASHYD NHYD=["O-14"], DT=[ 1] min, AREA=[ 5] (ha),

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1740 DWF=[ 0](cms), CN C=[ 82], IA=[ 7.5](mm), N=[ 3], TP=[ 0.133]hrs,
1741 Continuous simulation parameters:
1742 IaRECper=[ 4](hrs),
1743 SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1744 InterEventTime=[ 12](hrs)
1745 Baseflow simulation parameters:
1746 BaseFlowOption=[ 1],
1747 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
1748 VHydCond=[ 0.055](mm/hr), END=- 1
1749 *
1750 *%-----|-----|
1751 *ANALYSIS POINT 7 - JOCK RIVER
1752 * 2020-12-01 To Foster Drain
1753 * 2020-12-01 replace ("PT7JR") by ("OKEEFE")
1754 *%-----|-----|
1755 ADD HYD NHYDsum=[ "OKEEFE"], NHYDs to add=[ "O-14Ch"+"O-14"]
1756 *%-----|-----|
1757 *CONTINUOUS STANDHYD NHYD=[ "OKEEFE"], DT=[ 1](min), AREA=[ 448](ha),
1758 * XI MP=[ 0.65], TI MP=[ 0.65], DWF=[ 0](cms), LOSS=[ 2],
1759 * SCS curve number CN=[ 77],
1760 * Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 0.5](%),
1761 * LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
1762 * Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 0.5](%),
1763 * LGI=[ 1728](m), MNI=[ 0.013], SCI=[ 0](min),
1764 * Continuous simulation parameters:
1765 * IaRECper=[ 4](hrs), IaRECimp=[ 4](hrs),
1766 * SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1767 * InterEventTime=[ 18](hrs), END=- 1
1768 *#*****
1769 *# Okeefe Pond
1770 *# - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
1771 *# and a ratio of the catchment area to the West Clarke pond rating curve
1772 *# from the MS for the next coordinates
1773 *#*****
1774 *ROUTE RESERVOIR NHYDout=[ "P_OKE"], NHYDin=[ "OKEEFE"],
1775 * RDT=[ 1](min),
1776 * TABLE of ( OUTFLOW STORAGE ) values
1777 * (cms) - (ha-m)
1778 * [ 0.0 , 0.0]
1779 * [ 14.13 , 13.0]
1780 * [ -1 , -1 ] (maximum one hundred pairs of points)
1781 * NHYDovf=[ "ok-OVF"],
1782 *%-----|-----|
1783 * -JFSA 2021-02-25 "S-1-D2" and "S-1-D3" are part of S-1 sub-catchment. They are
1784 * moved to drain before station 6215 on Jock River
1785 *CONTINUOUS STANDHYD NHYD=[ "S-1-D2"], DT=[ 1](min), AREA=[ 18.67](ha), XI MP=[ 0.65],
1786 * TI MP=[ 0.65], DWF=[ 0](cms),
1787 * LOSS=[ 2], SCS curve number CN=[ 75], Pervious surfaces:
1788 * IAper=[ 4.67](mm), SLPP=[ 2.0](%),
1789 * LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min), Impervious surfaces:
1790 * IAimp=[ 1.57](mm), SLPI=[ 0.75](%),
1791 * LGI=[ 352.798](m), MNI=[ 0.013], SCI=[ 0](min),
1792 *
1793 * IaRECper=[ 4](hrs), IaRECimp=[ 4](hrs),
1794 * SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1795 * InterEventTime=[ 12](hrs), END=- 1
1796 *%-----|-----|
1797 CONTINUOUS NASHYD NHYD=[ "S-1-D2"], DT=[ 1]min, AREA=[ 18.67](ha),
1798 DWF=[ 0](cms), CN C=[ 77], IA=[ 4.67](mm),
1799 N=[ 3], TP=[ 1.120]hrs,
1800 Continuous simulation parameters:
1801 IaRECper=[ 4](hrs),
1802 SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1803 InterEventTime=[ 12](hrs)
1804 Baseflow simulation parameters:

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1801 BaseFlowOpt ion=[ 1] ,
1802 Ini t GWRes Vol =[ 50] ( mm) , GWRes K=[ 0. 96] ( mm/ day/ mm)
1803 VHydCond=[ 0. 055] ( mm/ hr) , END=- 1
1804 *%-----|-----|
1805 *COMPUTE DUALHYD NHYDi n=[ " S- 1- D2" ] , CI NLET=[ 2. 062] ( cms) , NI NLET=[ 1] ,
1806 * Mj NHYD=[ " S- 1- D2J" ]
1807 * M nNHYD=[ " S- 1- D2N" ]
1808 * TM STO=[ 9999999] ( cu- m)
1809 *%-----|-----|
1810 *ADD HYD NHYDs um=[ " S- 1- D2S" ] , NHYDs t o add=[ " S- 1- D2J" +" S- 1- D2N" ]
1811 *%-----|-----|
1812 *ROUTE RESERVOIR NHYDout =[ " S- 1- D2R" ] , NHYDi n=[ " S- 1- D2S" ] ,
1813 * RDT=[ 1] ( mi n) ,
1814 * TABLE of ( OUTFLOW STORAGE ) values
1815 * ( cms) - ( ha- m)
1816 * [ 0. 0 , 0. 0 ]
1817 * [ 0. 2231, 0. 7445 ]
1818 * [ -1 , -1 ] (max twenty pts)
1819 * NHYDovf=[ " S- 1- D2Rovf" ]
1820 *%-----|-----|
1821 *CONTINUOUS STANDHYD NHYD=[ " S- 1- D3" ] , DT=[ 1] ( mi n) , AREA=[ 6. 79] ( ha) , XI MP=[ 0. 65] ,
1822 * TI MP=[ 0. 65] , DWF=[ 0] ( cms) ,
1823 * LOSS=[ 2] , SCS curve number CN=[ 75] , Pervious surfaces:
1824 * I Aper =[ 4. 67] ( mm) , SLPP=[ 2. 0] ( % ) ,
1825 * LGP=[ 40] ( m) , MNP=[ 0. 25] , SCP=[ 0] ( mi n) , Impervious surfaces:
1826 * I Ai mp=[ 1. 57] ( mm) , SLPI =[ 0. 75] ( % ) ,
1827 * LGI =[ 212. 760] ( m) , MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
1828 * Continuous simulation parameters:
1829 * I aRECper =[ 4] ( hr s) , I aRECI mp=[ 4] ( hr s) ,
1830 * SM N=[ -1] ( mm) , SMAX=[ -1] ( mm) , SK=[ 0. 010] / ( mm) ,
1831 * InterEvent Ti me=[ 12] ( hr s) , END=- 1
1832 *%-----|-----|
1833 CONTINUOUS NASHYD NHYD=[ " S- 1- D3" ] , DT=[ 1] mi n , AREA=[ 6. 79] ( ha) ,
1834 * DWF=[ 0] ( cms) , CN C=[ 77] , I A=[ 4. 67] ( mm) ,
1835 * N=[ 3] , TP=[ 1. 281] hr s ,
1836 * Continuous simulation parameters:
1837 * I aRECper =[ 4] ( hr s) ,
1838 * SM N=[ -1] ( mm) , SMAX=[ -1] ( mm) , SK=[ 0. 010] / ( mm) ,
1839 * InterEvent Ti me=[ 12] ( hr s)
1840 * Baseflow simulation parameters:
1841 * BaseFlowOpt ion=[ 1] ,
1842 * Ini t GWRes Vol =[ 50] ( mm) , GWRes K=[ 0. 96] ( mm/ day/ mm)
1843 * VHydCond=[ 0. 055] ( mm/ hr) , END=- 1
1844 *%-----|-----|
1845 *COMPUTE DUALHYD NHYDi n=[ " S- 1- D3" ] , CI NLET=[ 0. 719] ( cms) , NI NLET=[ 1] ,
1846 * Mj NHYD=[ " S- 1- D3J" ]
1847 * M nNHYD=[ " S- 1- D3N" ]
1848 * TM STO=[ 9999999] ( cu- m)
1849 *%-----|-----|
1850 *ADD HYD NHYDs um=[ " S- 1- D3S" ] , NHYDs t o add=[ " S- 1- D3J" +" S- 1- D3N" ]
1851 *%-----|-----|
1852 *ROUTE RESERVOIR NHYDout =[ " S- 1- D3R" ] , NHYDi n=[ " S- 1- D3S" ] ,
1853 * RDT=[ 1] ( mi n) ,
1854 * TABLE of ( OUTFLOW STORAGE ) values
1855 * ( cms) - ( ha- m)
1856 * [ 0. 0 , 0. 0 ]
1857 * [ 0. 0811, 0. 2708 ]
1858 * [ -1 , -1 ] (max twenty pts)
1859 * NHYDovf=[ " S- 1- D3Rovf" ]
1860 *%-----|-----|
1861 ADD HYD NHYDs um=[ " SN_ OK" ] , NHYDs t o add=[ " N_ OK" +" OKEEFE" +" S- 1- D2" +" S- 1- D3" ]
1862 *%-----|-----|
1863 SAVE HYD NHYD=[ " SN_ OK" ] , # OF PCYCLES=[ -1] , I CASEs h=[ 1]
1864 *%-----|-----|
1865 *# HYD_ COMMENT=[ " Tot al Fl ows at Okeefe Dr ai n" ]

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1864  *# Hydrograph from Node Okeefe routed to Node at Foster Drain
1865  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
1866  *#
1867  ROUTE CHANNEL      NHYDout=[ "N_FO" ] , NHYDin=[ "SN_OK" ] ,
1868                    RDT=[ 1 ] ( min ),
1869                    CHLGTH=[ 1183 ] ( m ) ,    CHSLOPE=[ 0.0761 ] ( % ) ,
1870                                                    FPSLOPE=[ 0.0761 ] ( % ) ,
1871                    SECNUM=[ 1.0 ] ,          NSEG=[ 3 ]
1872                    ( SEGROUGH, SEGDIST ( m ) ) =
1873                    [ 0.050, -33.89
1874                    -0.035, 31.59
1875                    0.050, 34.41 ] NSEG times
1876                    ( DISTANCE ( m ) , ELEVATION ( m ) ) =
1877                    [ -794.18, 91.00 ]
1878                    [ -775.41, 91.50 ]
1879                    [ -702.63, 91.50 ]
1880                    [ -546.19, 91.50 ]
1881                    [ -529.54, 91.50 ]
1882                    [ -323.44, 91.00 ]
1883                    [ -320.71, 91.00 ]
1884                    [ -183.59, 91.00 ]
1885                    [ -182.54, 90.50 ]
1886                    [ -181.36, 90.00 ]
1887                    [ -177.37, 90.00 ]
1888                    [ -87.70, 90.00 ]
1889                    [ -33.89, 90.00 ]
1890                    [ -18.52, 86.88 ]
1891                    [ 0.00, 85.20 ]
1892                    [ 16.20, 86.83 ]
1893                    [ 31.59, 90.00 ]
1894                    [ 33.03, 90.50 ]
1895                    [ 34.41, 91.00 ]
1896  *%-----|-----|
1897  *#*****
1898  *# Catchment FOSTER
1899  *# - To Foster ditch (north of the Jock)
1900  *# - Partially developed (medium density); remaining agricultural
1901  *# - 2020-12-01 JFSA Foster area is 332 as per Foster SWF Environmental Study
1902  *# - 2020-12-01 decrease Foster drainage area from (373 HA) to (307.98 HA) after
1903  *# - 2021-02-12 update Foster area to 325.44 ha as measured from QGIS
1904  *#*****
1905  CONTINUOUS STANDHYD NHYD=[ "FOSTER" ] , DT=[ 1 ] min , AREA=[ 325.44 ] ( ha ) ,
1906                    XI MP=[ 0.55 ] , TI MP=[ 0.55 ] , DWF=[ 0 ] ( cms ) , LOSS=[ 2 ] ,
1907                    SCS curve number CN=[ 74 ] ,
1908                    Pervious surfaces: I A per=[ 4.67 ] ( mm ) , SLPP=[ 0.5 ] ( % ) ,
1909                    LGP=[ 40 ] ( m ) , MNP=[ 0.25 ] , SCP=[ 0 ] ( min ) ,
1910                    Impervious surfaces: I A i mp=[ 1.57 ] ( mm ) , SLPI=[ 0.5 ] ( % ) ,
1911                    LGI=[ 1472.956 ] ( m ) , MNI=[ 0.013 ] , SCI=[ 0 ] ( min ) ,
1912                    Continuous simulation parameters:
1913                    I a REC per=[ 4 ] ( hrs ) , I a REC i mp=[ 4 ] ( hrs ) ,
1914                    SM N=[ -1 ] ( mm ) , SMAX=[ -1 ] ( mm ) , SK=[ 0.010 ] / ( mm ) ,
1915                    Inter Event Time=[ 18 ] ( hrs ) , END=- 1
1916  *#*****
1917  *# Foster Pond
1918  *# - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
1919  *# and a ratio of the catchment area to the West Clarke pond rating curve
1920  *# from the MSS for the next coordinates
1921  *#*****
1922  ROUTE RESERVOIR    NHYDout=[ "P_FOS" ] , NHYDin=[ "FOSTER" ] ,
1923                    RDT=[ 1 ] ( min ) ,
1924                    TABLE of ( OUTFLOW STORAGE ) values
1925                    ( cms ) - ( ha-m )
1926                    [ 0.0 , 0.0 ]

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1927          [ 10.34 , 10]
1928          [ -1 , -1 ] (max twenty pts)
1929          NHYDovf=[ "FO- OVF" ]
1930 *%-----|-----|
1931 ADD HYD          NHYDsum=[ "FOSTER- OUT" ], NHYDs to add=[ "P_FOS"+"FO- OVF" ]
1932 *%-----|-----|
1933 *#*****|
1934 * -Brazeau area from P 1800-19 =[71.751], change to 63.59 ha based on GIS measurements
1935 * -JFSA, 2021-01-19 update "W_CLAR_BRAZ" to 73.29 ha based on GIS measurements
1936 * -JFSA, 2021-01-22 Brazeau ("MS_P10"+"P10-OVF")brazeau pond discharges directly
to the jock river through a road side ditch on the west side of Borrisokane road
(station 6016)
1937 CONTINUOUS STANDHYD NHYD=[ "W_CLAR_BRAZ" ], DT=[ 1]mi n, AREA=[ 73.29](ha),
1938 XI MP=[ 0.6], TI MP=[ 0.65], DWF=[ 0](cms), LOSS=[ 2],
1939 SCS curve number CN=[ 77],
1940 Pervious surfaces: I A per=[ 4.67](mm), SLPP=[ 1](%),
1941 LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](mi n),
1942 Impervious surfaces: I A i mp=[ 1.57](mm), SLPI=[ 0.5](%),
1943 LGI=[ 699.00](m), MNI=[ 0.013], SCI=[ 0](mi n),
1944 Continuous simulation parameters:
1945 I a REC per=[ 4](hr s), I a REC i mp=[ 4](hr s),
1946 SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1947 I nter Event Ti me=[ 18](hr s), END=- 1
1948 *%-----|-----|
1949 * 2020-12-01 correct pond curve values
1950 ROUTE RESERVOIR NHYDout =["MS_P10"], NHYDi n=["W_CLAR_BRAZ"],
1951 RDT=[ 1](mi n),
1952 TABLE of ( OUTFLOW STORAGE ) values
1953 (cms) - (ha-m)
1954 [ 0.0 , 0.0 ]
1955 [ 0.068 , 0.001 ]
1956 [ 0.271 , 0.022 ]
1957 [ 0.379 , 0.051 ]
1958 [ 0.48 , 0.091 ]
1959 [ 0.853 , 0.341 ]
1960 [ 1.005 , 0.61 ]
1961 [ 1.128 , 1.231 ]
1962 [ 1.155 , 1.592 ]
1963 [ 1.194 , 1.876 ]
1964 [ 1.2 , 1.921 ]
1965 [ 1.259 , 2.369 ]
1966 [ 1.3 , 2.665 ]
1967 [ 1.349 , 2.813 ]
1968 [ -1 , -1 ] (max twenty pts)
1969 NHYDovf=[ "P10- OVF" ]
1970 *%-----|-----|
1971 * -JFSA 2021-02-26 "S-1-FO-D2" is a part of S-1 sub-catchment. It is moved to drain
before station 980 on Foster Drain
1972 *CONTINUOUS STANDHYD NHYD=[ "S-1-FO-D2" ], DT=[ 1]mi n, AREA=[ 4.94](ha),
1973 * XI MP=[ 0.55], TI MP=[ 0.55], DWF=[ 0](cms), LOSS=[ 2],
1974 * SCS curve number CN=[ 74],
1975 * Pervious surfaces: I A per=[ 4.67](mm), SLPP=[ 0.5](%),
1976 * LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](mi n),
1977 * Impervious surfaces: I A i mp=[ 1.57](mm), SLPI=[ 0.5](%),
1978 * LGI=[ 181.475](m), MNI=[ 0.013], SCI=[ 0](mi n),
1979 * Continuous simulation parameters:
1980 * I a REC per=[ 4](hr s), I a REC i mp=[ 4](hr s),
1981 * SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1982 * I nter Event Ti me=[ 18](hr s), END=- 1
1983 *%-----|-----|
1984 CONTINUOUS NASHYD NHYD=[ "S-1-FO-D2" ], DT=[ 1]mi n, AREA=[ 4.94](ha),
1985 DWF=[ 0](cms), CN C=[ 77], I A=[ 4.67](mm),
1986 N=[ 3], TP=[ 1.10]hr s,
1987 Continuous simulation parameters:
1988 I a REC per=[ 4](hr s),
1989 SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),

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1990 InterEventTime=[ 12](hrs)
1991 Baseflow simulation parameters:
1992 BaseFlowOption=[ 1] ,
1993 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
1994 VHydCond=[ 0.055](mm/hr), END=- 1
1995 *%-----|-----|
1996 *COMPUTE DUALHYD NHYDin=["S-1-FO-D2"], CINLET=[ 0.508](cms), NINLET=[ 1],
1997 * MjNHYD=["S-1-FO-D2J"]
1998 * MnNHYD=["S-1-FO-D2N"]
1999 * TMSTO=[ 9999999](cu-m)
2000 *%-----|-----|
2001 *ADD HYD NHYDsum=["S-1-FO-D2S"], NHYDsto add=["S-1-FO-D2J"+"S-1-FO-D2N"]
2002 *%-----|-----|
2003 *ROUTE RESERVOIR NHYDout=["S-1-FO-D2R"], NHYDin=["S-1-FO-D2S"],
2004 * RDT=[ 1](min),
2005 * TABLE of ( OUTFLOW STORAGE ) values
2007 * [ 0.0 , 0.0 ]
2008 * [ 0.0590, 0.1970 ]
2009 * [ -1 , -1 ] (max twenty pts)
2010 * NHYDovf=["S-1FOD2ovf"]
2011 *%-----|-----|
2012 ADD HYD NHYDsum=["980"], NHYDsto add=["FOSTER-OUT"+"S-1-FO-D2"]
2013 *%-----|-----|
2014 SAVE HYD NHYD=["980"], # OF PCYCLES=[ -1], ICASEsh=[ 1]
2015 HYD_COMMENT=["Total Flows at Station 980 on Foster Drain"]
2016 *%-----|-----|
2017 *#
2018 *# Hydrograph from Node Foster SWM (Station 980) to Node at station 520
2019 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 980
2020 *#
2021 ROUTE CHANNEL NHYDout=["980-out"], NHYDin=["980"],
2022 RDT=[ 1](min),
2023 CHLGTH=[ 460](m), CHSLOPE=[ 0.04348](%),
2024 FPSLOPE=[ 0.04348](%),
2025 SECNUM=[ 1.0], NSEG=[ 3]
2026 ( SEGROUGH, SEGDI ST (m))=
2027 [ 0.050, 45.90
2028 -0.035, 53.30
2029 0.050, 100] NSEG times
2030 ( DISTANCE (m), ELEVATION (m))=
2031 [ 0, 91.75 ]
2032 [ 42.4, 92.18 ]
2033 [ 43.5, 92.16 ]
2034 [ 44.1, 92.1 ]
2035 [ 44.6, 92 ]
2036 [ 44.8, 91.86 ]
2037 [ 45.9, 91.04 ]
2038 [ 46.4, 90.65 ]
2039 [ 46.8, 90.36 ]
2040 [ 47.9, 90.32 ]
2041 [ 48.7, 90.35 ]
2042 [ 50.7, 90.33 ]
2043 [ 52.2, 90.38 ]
2044 [ 52.5, 90.59 ]
2045 [ 53.3, 91.28 ]
2046 [ 54, 91.83 ]
2047 [ 54.3, 92 ]
2048 [ 54.8, 92.08 ]
2049 [ 55.4, 92.12 ]
2050 [ 100, 91.84 ]
2051 *%-----|-----|
2052 * -JFSA 2021-02-26 "S-1-FO-D1" is a part of S-1 sub-catchment. It is moved to drain
before station 520 on Foster Drain
2053 *CONTINUOUS STANDHYD NHYD=["S-1-FO-D1"], DT=[ 1]min, AREA=[ 5.11](ha),
2054 * XI MP=[ 0.65], TI MP=[ 0.65], DWF=[ 0](cms), LOSS=[ 2],

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2055 *          SCS curve number CN=[ 74],
2056 *          Pervious surfaces: I Aper=[ 4.67] (mm), SLPP=[ 0.5] (%),
2057 *          LGP=[ 40] (m), MNP=[ 0.25], SCP=[ 0] (min),
2058 *          Impervious surfaces: I Aimp=[ 1.57] (mm), SLPI=[ 0.5] (%),
2059 *          LGI=[ 184.572] (m), MNI=[ 0.013], SCI=[ 0] (min),
2060 *          Continuous simulation parameters:
2061 *          I aRECper=[ 4] (hrs), I aRECimp=[ 4] (hrs),
2062 *          SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
2063 *          InterEventTime=[ 18] (hrs), END=- 1
2064 *%-----|-----|
2065 CONTINUOUS NASHYD NHYD=[ "S-1-FO-DI" ], DT=[ 1] min, AREA=[ 5.11] (ha),
2066 DWF=[ 0] (cms), CNC=[ 77], I A=[ 4.67] (mm),
2067 N=[ 3], TP=[ 1.10] hrs,
2068 Continuous simulation parameters:
2069 I aRECper=[ 4] (hrs),
2070 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
2071 InterEventTime=[ 12] (hrs)
2072 Baseflow simulation parameters:
2073 BaseFlowOption=[ 1],
2074 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm3/day/mm)
2075 VHydCond=[ 0.055] (mm/hr), END=- 1
2076 *%-----|-----|
2077 *COMPUTE DUALHYD NHYDin=[ "S-1-FO-DI" ], CINLET=[ 0.605] (cms), NINLET=[ 1],
2078 *          MajNHYD=[ "S-1-FO-DIJ" ]
2079 *          MinNHYD=[ "S-1-FO-DIN" ]
2080 *          TMSTO=[ 9999999] (cu-m)
2081 *%-----|-----|
2082 *ADD HYD NHYDsum=[ "S-1-FO-DIS" ], NHYDto add=[ "S-1-FO-DIN"+"S-1-FO-DIJ" ]
2083 *%-----|-----|
2084 *ROUTE RESERVOIR NHYDout=[ "S-1-FO-DIR" ], NHYDin=[ "S-1-FO-DIS" ],
2085 *          RDT=[ 1] (min),
2086 *          TABLE of ( OUTFLOW STORAGE ) values
2087 *          ( cms ) - ( ha-m)
2088 *          [ 0.0 , 0.0 ]
2089 *          [ 0.0611, 0.2038 ]
2090 *          [ -1 , -1 ] (max twenty pts)
2091 *          NHYDovf=[ "S-1FODlovf" ]
2092 *%-----|-----|
2093 ADD HYD NHYDsum=[ "520" ], NHYDto add=[ "980-out"+"S-1-FO-DI" ]
2094 *%-----|-----|
2095 SAVE HYD NHYD=[ "520" ], # OF PCYCLES=[ -1], ICASEsh=[ 1]
2096 HYD_COMMENT=[ "Total Flows at Sation 520 on Foster Drain" ]
2097 *%-----|-----|
2098 *# Hydrograph from Node at Station 520 (Foster Drain) to Node at station 6016 (Jock
River)
2099 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 520
2100 *#
2101 ROUTE CHANNEL NHYDout=[ "520-out" ], NHYDin=[ "520" ],
2102 RDT=[ 1] (min),
2103 CHLGTH=[ 860] (m), CHSLOPE=[ 0.5872] (%),
2104 FPSLOPE=[ 0.5872] (%),
2105 SECNUM=[ 1.0], NSEG=[ 3]
2106 ( SEGROUGH, SEGDI ST (m))=
2107 [ 0.050, 45.90
2108 -0.035, 54.3
2109 0.050, 100.1097] NSEG times
2110 ( DI STANCE (m), ELEVATI ON (m))=
2111 [ 0, 91.26 ]
2112 [ 44.9, 91.46 ]
2113 [ 45.1, 91.37 ]
2114 [ 45.9, 90.84 ]
2115 [ 47, 90.32 ]
2116 [ 47.5, 90.22 ]
2117 [ 48, 90.17 ]
2118 [ 50.7, 90.19 ]
2119 [ 51.5, 90.17 ]

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2120 [ 52.2, 90.13 ]
2121 [ 52.7, 90.12 ]
2122 [ 53.3, 90.14 ]
2123 [ 53.5, 90.31 ]
2124 [ 53.9, 90.59 ]
2125 [ 54.3, 90.87 ]
2126 [ 54.7, 91.04 ]
2127 [ 55.3, 91.24 ]
2128 [ 55.5, 91.26 ]
2129 [ 63.7, 91.37 ]
2130 [ 100.1097, 91.43 ]
2131 *%-----|-----|
2132 * -JFSA 2021-02-26 "S-1-FO-F-D" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2133 *CONTINUOUS STANDHYD NHYD=["S-1-FO-F-D"], DT=[1]mi n, AREA=[14.96](ha),
2134 * XI MP=[0.65], TI MP=[0.65], DWF=[0](cms), LOSS=[2],
2135 * SCS curve number CN=[74],
2136 * Pervious surfaces: I A per=[4.67](mm), SLPP=[0.5](%),
2137 * LGP=[40](m), MNP=[0.25], SCP=[0](mi n),
2138 * Impervious surfaces: I A i mp=[1.57](mm), SLPI=[0.5](%),
2139 * LGI=[315.806](m), MNI=[0.013], SCI=[0](mi n),
2140 * Continuous simulation parameters:
2141 * I a RE C per=[4](hrs), I a RE C i mp=[4](hrs),
2142 * SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2143 * Inter Event Ti me=[18](hrs), END=-1
2144 *%-----|-----|
2145 CONTINUOUS NASHYD NHYD=["S-1-FO-F-D"], DT=[1]mi n, AREA=[14.96](ha),
2146 DWF=[0](cms), CN C=[77], I A=[4.67](mm),
2147 N=[3], TP=[1.007]hrs,
2148 Continuous simulation parameters:
2149 I a RE C per=[4](hrs),
2150 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2151 Inter Event Ti me=[12](hrs)
2152 Baseflow simulation parameters:
2153 BaseFl owOpt ion=[1],
2154 Ini t GWRes Vol=[50](mm), GWRes K=[0.96](mm/ day/ mm)
2155 VHydCond=[0.055](mm/ hr), END=-1
2156 *%-----|-----|
2157 *COMPUTE DUALHYD NHYD i n=["S-1-FO-F-D"], CI NLET=[1.749](cms), NI NLET=[1],
2158 * M i j NHYD=["S-1FO-F-DJ"]
2159 * M nNHYD=["S-1FO-F-DN"]
2160 * TM I STO=[9999999](cu-m)
2161 *%-----|-----|
2162 *ADD HYD NHYDs um=["S-1FO-F-DS"], NHYDs to add=["S-1FO-F-DJ"+"S-1FO-F-DN"]
2163 *%-----|-----|
2164 *ROUTE RESERVOIR NHYDout=["S-1FO-F-DR"], NHYD i n=["S-1FO-F-DS"],
2165 * RDT=[1](mi n),
2166 * TABLE of ( OUTFLOW STORAGE ) values
2167 * ( cms ) - ( ha-m )
2168 * [ 0.0 , 0.0 ]
2169 * [ 0.1788, 0.5966 ]
2170 * [ -1 , -1 ] (max twenty pts)
2171 * NHYDovf=["S-1FoFDovf"]
2172 *%-----|-----|
2173 * -JFSA 2021-02-26 "S-1-D8" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2174 * -JFSA 2021-03-02 "S-1-D8" is Borriskane Rd. so it will remain STANDHYD in all
scenarios
2175 CONTINUOUS STANDHYD NHYD=["S-1-D8"], DT=[1](mi n), AREA=[5.27](ha), XI MP=[0.65],
TI MP=[0.65], DWF=[0](cms),
2176 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
I A per=[4.67](mm), SLPP=[2.0](%),
2177 LGP=[40](m), MNP=[0.25], SCP=[0](mi n), Impervious surfaces:
I A i mp=[1.57](mm), SLPI=[0.75](%),
2178 LGI=[187.439](m), MNI=[0.013], SCI=[0](mi n),
2179 Continuous simulation parameters:

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2180 IaRECper=[ 4](hr s), IaRECI mp=[ 4](hr s),
2181 SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2182 InterEventTime=[ 12](hr s), END=- 1
2183 *%-----|-----
2184 * This is a road so it is always STANDHYD
2185 *CONTINUOUS NASHYD NHYD=["S-1-D8"], DT=[ 1]mi n, AREA=[ 5.27](ha),
2186 * DWF=[ 0](cms), CNV C=[ 77], IA=[ 4.67](mm),
2187 * N=[ 3], TP=[ 1.10]hr s,
2188 * Continuous simulation parameters:
2189 * IaRECper=[ 4](hr s),
2190 * SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2191 * InterEventTime=[ 12](hr s)
2192 * Baseflow simulation parameters:
2193 * BaseFlowOption=[ 1],
2194 * InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
2195 * VHydCond=[ 0.055](mm/hr), END=- 1
2196 *%-----|-----
2197 *COMPUTE DUALHYD NHYDin=["S-1-D8"], CINLET=[ 2.279](cms), NI NLET=[ 1],
2198 * Mj NHYD=["S-1-D8J"]

2200 * TMJ STO=[ 9999999](cu-m)
2201 *%-----|-----
2202 *ADD HYD NHYDs um=["S-1-D8S"], NHYDs to add=["S-1-D8J"+"S-1-D8N"]
2203 *%-----|-----
2204 *ADD HYD NHYDs um=["S-1-D"], NHYDs to add=["S-1-Okeefe"+"S-1"+"S-1-Fost"]
2205 *%-----|-----
2206 *COMPUTE DUALHYD NHYDin=["S-1-D"], CINLET=[ 11.616](cms), NI NLET=[ 1],
2207 * Mj NHYD=["S-1-D-M"]
2208 * MnNHYD=["S-1-D-MN"]
2209 * TMJ STO=[ 5974](cu-m)
2210 *%-----|-----
2211 *ADD HYD NHYDs um=["S-1-DEV"], NHYDs to add=["S-1-D-M"+"S-1-D-MN"]
2212 *%-----|-----
2213 *ROUTE RESERVOIR NHYDout=["S-1-D8R"], NHYDin=["S-1-D8S"],
2214 * RDT=[ 1](mi n),
2215 * TABLE of ( OUTFLOW STORAGE ) values
2216 * (cms) - (ha-m)
2217 * [ 0.0 , 0.0 ]
2218 * [ 0.0630, 0.2102 ]
2219 * [ -1 , -1 ] (max twenty pts)
2220 * NHYDovf=["S-1-D8Rovf"]
2221 *%-----|-----
2222 * -JFSA 2021-02-26 "S-1-A" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock Ri ver
2223 CONTINUOUS NASHYD NHYD=["S-1-A"], DT=[ 1]mi n, AREA=[ 75.88](ha),
2224 DWF=[ 0](cms), CNV C=[ 77], IA=[ 4.67](mm),
2225 N=[ 3], TP=[ 0.619]hr s,
2226 Continuous simulation parameters:
2227 IaRECper=[ 4](hr s),
2228 SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2229 InterEventTime=[ 12](hr s)
2230 Baseflow simulation parameters:
2231 BaseFlowOption=[ 1],
2232 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
2233 VHydCond=[ 0.055](mm/hr), END=- 1
2234 *%-----|-----
2235 * -JFSA 2021-01-22 "W_CLAR_UNDE" (west of Clarke sub-catchment) discharges
directly to the jock river through a road side ditch on the west side of Borrisokane
road (station 6016)
2236 CONTINUOUS NASHYD NHYD=["W_CLAR_UNDE"], DT=[ 1]mi n, AREA=[ 35.65](ha),
2237 DWF=[ 0](cms), CNV C=[ 77], IA=[ 4.67](mm),
2238 N=[ 3], TP=[ 1.10]hr s,
2239 Continuous simulation parameters:
2240 IaRECper=[ 4](hr s),
2241 SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2242 InterEventTime=[ 12](hr s)

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2243 Baseflow simulation parameters:
2244 BaseFlowOption=[ 1] ,
2245 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/ day/ mm)
2246 VHydCond=[ 0.055] (mm/ hr), END=- 1
2247 *%-----|-----
2248 ADD HYD NHYDsum=[ "SN_FO" ], NHYDs to
add=[ "N_FO"+"520-out"+"MS_P10"+"P10-OVF"+"W_CLAR_UNDE"+"S-1-FO-F-D"+"S-1-D8"+"S-1-A"]
2249 *%-----|-----
2250 SAVE HYD NHYD=[ "SN_FO" ], # OF PCYCLES=[ -1], ICASEsh=[ 1]
2251 HYD_COMMENT=[ "Total Flows at Foster Drain"]
2252 *%-----|-----
2253 *# Hydrograph from Node Foster routed to Node at Cedarview Road
2254 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6016
2255 *#
2256 ROUTE CHANNEL NHYDout=[ "N_CE" ], NHYDin=[ "SN_FO" ],
2257 RDT=[ 1] (min),
2258 CHLGTH=[ 159] (m), CHSLOPE=[ 0.0818] ( %),
2259 FPSLOPE=[ 0.0818] ( %),
2260 SECNUM=[ 1.0], NSEG=[ 3]
2261 ( SEGROUGH, SEGDI ST (m))=
2262 [ 0.050, -15.46
2263 -0.035, 26.55
2264 0.050, 116.76] NSEG times
2265 ( DI STANCE (m), ELEVATI ON (m))=
2266 [- 645.23, 91.50]
2267 [- 391.20, 91.50]
2268 [- 91.00, 91.50]
2269 [- 85.52, 91.50]
2270 [- 15.46, 89.40]
2271 [- 9.79, 89.31]
2272 [- 3.22, 86.24]
2273 [ 3.22, 85.07]
2274 [ 10.96, 85.79]
2275 [ 16.44, 86.49]
2276 [ 26.55, 89.45]
2277 [ 29.03, 90.27]
2278 [ 35.76, 90.67]
2279 [ 36.67, 91.00]
2280 [ 108.08, 91.00]
2281 [ 109.82, 90.50]
2282 [ 112.04, 90.50]
2283 [ 114.62, 91.00]
2284 [ 116.76, 91.50]
2285 *%-----|-----
2286 *#*****
2287 *# Catchment S-1
2288 *# - To Jock River (north and south of Jock)
2289 *# - Primarily agricultural fields; portion of sand quarry
2290 *%-----|-----
2291 *% -2020-12-17 "S-1-Undev" and "S-1-Fost" was a part of Foster drain, they are below
the foster pond. Now they are added to S-1 subcatchment based on Project 1474-BCDC,
JFSA, Nov. 2020
2292 *% -2020-12-17 Change O-14 (it was part of Okeefe drain) to "S-1-Okeefe" and add it
to S-1 subcatchment based on Project 1474-BCDC, JFSA, Nov. 2020
2293 *% -2020-12-17 Add "S-1-BCDC" as NASHYD
2294 *% -2020-12-17 all other S-1 subcatchment as STANDHYD with DUALHYD and ROUTE RESERVOIR
2295 *%-----|-----
2296 *#*****
2297 * -JFSA 2021-02-26 "S-1-A" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2298 *CONTINUOUS NASHYD NHYD=[ "S-1-A" ], DT=[ 1] min, AREA=[ 75.88] (ha),
2299 * DWF=[ 0] (cms), CNVC=[ 77], IA=[ 4.67] (mm),
2300 * N=[ 3], TP=[ 0.619] hrs,
2301 * Continuous simulation parameters:
2302 * IaRECper=[ 4] (hrs),
2303 * SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010]/(mm),

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2304 * InterEventTime=[ 12](hrs)
2305 * Baseflow simulation parameters:
2306 * BaseFlowOption=[ 1] ,
2307 * InitGWResVol =[ 50](mm) , GWResK=[ 0.96](mm/day/mm)
2308 * VHydCond=[ 0.055](mm/hr) , END=- 1
2309 *%-----|
2310 CONTINUOUS NASHYD NHYD=[ "S-1-B" ] , DT=[ 1]min , AREA=[ 55.36](ha) ,
2311 DWF=[ 0](cms) , CNVC=[ 77] , IA=[ 4.67](mm) ,
2312 N=[ 3] , TP=[ 0.451]hrs ,
2313 Continuous simulation parameters:
2314 IaRECper=[ 4](hrs) ,
2315 SMN=[ -1](mm) , SMAX=[ -1](mm) , SK=[ 0.010]/(mm) ,
2316 InterEventTime=[ 12](hrs)
2317 Baseflow simulation parameters:
2318 BaseFlowOption=[ 1] ,
2319 InitGWResVol =[ 50](mm) , GWResK=[ 0.96](mm/day/mm)
2320 VHydCond=[ 0.055](mm/hr) , END=- 1
2321 *%-----|
2322 *# - JFSA 2021-02-24 change the name from S-1-BCDC to S-1-A and S-1-B. Change their
TP values based on the new areas compared to the old ones.
2323 *CONTINUOUS NASHYD NHYD=[ "S-1-BCDC" ] , DT=[ 1]min , AREA=[ 134.9](ha) ,
2324 * DWF=[ 0](cms) , CNVC=[ 77] , IA=[ 4.67](mm) ,
2325 * N=[ 3] , TP=[ 1.10]hrs ,
2326 * Continuous simulation parameters:
2327 * IaRECper=[ 4](hrs) ,
2328 * SMN=[ -1](mm) , SMAX=[ -1](mm) , SK=[ 0.010]/(mm) ,
2329 * InterEventTime=[ 12](hrs)
2330 * Baseflow simulation parameters:
2331 * BaseFlowOption=[ 1] ,
2332 * InitGWResVol =[ 50](mm) , GWResK=[ 0.96](mm/day/mm)
2333 * VHydCond=[ 0.055](mm/hr) , END=- 1
2334 *%-----|
2335 *# - JFSA 2021-02-24 "S-1-BCDC-1" and "S-1-BCDC-2" are not existing anymore.
"S-1-BCDC-1" is part of "S-1-FO-D2" and "S-1-BCDC-2" is part of "S-1-D2" and "S-1-D3"
2336 *CONTINUOUS NASHYD NHYD=[ "S-1-BCDC-1" ] , DT=[ 1]min , AREA=[ 0.3](ha) ,
2337 * DWF=[ 0](cms) , CNVC=[ 77] , IA=[ 4.67](mm) ,
2338 * N=[ 3] , TP=[ 1.10]hrs ,
2339 * Continuous simulation parameters:
2340 * IaRECper=[ 4](hrs) ,
2341 * SMN=[ -1](mm) , SMAX=[ -1](mm) , SK=[ 0.010]/(mm) ,
2342 * InterEventTime=[ 12](hrs)
2343 * Baseflow simulation parameters:
2344 * BaseFlowOption=[ 1] ,
2345 * InitGWResVol =[ 50](mm) , GWResK=[ 0.96](mm/day/mm)
2346 * VHydCond=[ 0.055](mm/hr) , END=- 1
2347 *%-----|
2348 *CONTINUOUS NASHYD NHYD=[ "S-1-BCDC-2" ] , DT=[ 1]min , AREA=[ 1.3](ha) ,
2349 * DWF=[ 0](cms) , CNVC=[ 77] , IA=[ 4.67](mm) ,
2350 * N=[ 3] , TP=[ 1.10]hrs ,
2351 * Continuous simulation parameters:
2352 * IaRECper=[ 4](hrs) ,
2353 * SMN=[ -1](mm) , SMAX=[ -1](mm) , SK=[ 0.010]/(mm) ,
2354 * InterEventTime=[ 12](hrs)
2355 * Baseflow simulation parameters:
2356 * BaseFlowOption=[ 1] ,
2357 * InitGWResVol =[ 50](mm) , GWResK=[ 0.96](mm/day/mm)
2358 * VHydCond=[ 0.055](mm/hr) , END=- 1
2359 *%-----|
2360 *# - JFSA 2021-01-19, after adding Greenbank pond, "S-1-BCDC-3" is not existing
anymore
2361 *CONTINUOUS NASHYD NHYD=[ "S-1-BCDC-3" ] , DT=[ 1]min , AREA=[ 3.9](ha) ,
2362 * DWF=[ 0](cms) , CNVC=[ 77] , IA=[ 4.67](mm) ,
2363 * N=[ 3] , TP=[ 1.10]hrs ,
2364 * Continuous simulation parameters:
2365 * IaRECper=[ 4](hrs) ,
2366 * SMN=[ -1](mm) , SMAX=[ -1](mm) , SK=[ 0.010]/(mm) ,

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2367 * InterEventTime=[ 12](hrs)
2368 * Baseflow simulation parameters:
2369 * BaseFlowOption=[ 1] ,
2370 * InitGWResVol=[ 50](mm) , GWResK=[ 0.96](mm/day/mm)
2371 * VHydCond=[ 0.055](mm/hr) , END=- 1
2372 *%-----|-----
2373 * -JFSA 2021-02-25 "S-1-Okeefe" is a part of S-1 sub-catchment. It is moved to drain
before station 7245 on Jock River
2374 *CONTINUOUS STANDHYD NHYD=["S-1-Okeefe"], DT=[ 1](min) , AREA=[ 44.93](ha) , XI MP=[ 0.65] ,
TI MP=[ 0.65] , DWF=[ 0](cms) ,
2375 * LOSS=[ 2] , SCS curve number CN=[ 75] , Pervious surfaces:
I Aper=[ 4.67](mm) , SLPP=[ 2.0](%) ,
2376 * LGP=[ 40](m) , MNP=[ 0.25] , SCP=[ 0](min) , Impervious surfaces:
I Aimp=[ 1.57](mm) , SLPI=[ 0.75](%) ,
2377 * LGI=[ 547.296](m) , MNI=[ 0.013] , SCI=[ 0](min) ,
2378 * Continuous simulation parameters:
2379 * IaRECper=[ 4](hrs) , IaRECimp=[ 4](hrs) ,
2380 * SMN=[ -1](mm) , SMAX=[ -1](mm) , SK=[ 0.010]/(mm) ,
2381 * InterEventTime=[ 12](hrs) , END=- 1
2382 *%-----|-----
2383 *COMPUTE DUALHYD NHYDin=["S-1-Okeefe"], CINLET=[ 4.796](cms) , NINLET=[ 1] ,
2384 * MajNHYD=["S-1-OkM"]
2385 * MnNHYD=["S-1-OkMN"]
2386 * TMI STO=[ 9999999](cu-m)
2387 *%-----|-----
2388 *ADD HYD NHYDsum=["S-1-OkS"] , NHYDsto add=["S-1-OkM"+"S-1-OkMN"]
2389 *%-----|-----
2390 *ROUTE RESERVOIR NHYDout=["S-1-OkSR"] , NHYDin=["S-1-OkS"] ,
2391 * RDT=[ 1](min) ,
2392 * TABLE of ( OUTFLOW STORAGE ) values
2393 * ( cms ) - ( ha-m)
2394 * [ 0.0 , 0.0 ]
2395 * [ 0.5370, 1.7917 ]
2396 * [ -1 , -1 ] (max twenty pts)
2397 * NHYDovf=["S-1-OkSovf"]
2398 *%-----|-----
2399 *CONTINUOUS NASHYD NHYD=["S-1-Okeefe"], DT=[ 1]min , AREA=[ 44.93](ha) ,
2400 * DWF=[ 0](cms) , CN C=[ 77] , IA=[ 4.67](mm) ,
2401 * N=[ 3] , TP=[ 1.049]hrs ,
2402 * Continuous simulation parameters:
2403 * IaRECper=[ 4](hrs) ,
2404 * SMN=[ -1](mm) , SMAX=[ -1](mm) , SK=[ 0.010]/(mm) ,
2405 * InterEventTime=[ 12](hrs)
2406 * Baseflow simulation parameters:
2407 * BaseFlowOption=[ 1] ,
2408 * InitGWResVol=[ 50](mm) , GWResK=[ 0.96](mm/day/mm)
2409 * VHydCond=[ 0.055](mm/hr) , END=- 1
2410 *%-----|-----
2411 * -JFSA 2021-02-26 "S-1-FO-DI" is a part of S-1 sub-catchment. It is moved to drain
before station 520 on Foster Drain
2412 *CONTINUOUS STANDHYD NHYD=["S-1-FO-DI"] , DT=[ 1]min , AREA=[ 5.11](ha) ,
2413 * XI MP=[ 0.65] , TI MP=[ 0.65] , DWF=[ 0](cms) , LOSS=[ 2] ,
2414 * SCS curve number CN=[ 74] ,
2415 * Pervious surfaces: I Aper=[ 4.67](mm) , SLPP=[ 0.5](%) ,
2416 * LGP=[ 40](m) , MNP=[ 0.25] , SCP=[ 0](min) ,
2417 * Impervious surfaces: I Aimp=[ 1.57](mm) , SLPI=[ 0.5](%) ,
2418 * LGI=[ 184.572](m) , MNI=[ 0.013] , SCI=[ 0](min) ,
2419 * Continuous simulation parameters:
2420 * IaRECper=[ 4](hrs) , IaRECimp=[ 4](hrs) ,
2421 * SMN=[ -1](mm) , SMAX=[ -1](mm) , SK=[ 0.010]/(mm) ,
2422 * InterEventTime=[ 18](hrs) , END=- 1
2423 *%-----|-----
2424 *COMPUTE DUALHYD NHYDin=["S-1-FO-DI"] , CINLET=[ 0.605](cms) , NINLET=[ 1] ,
2425 * MajNHYD=["S-1-FO-DIJ"]
2426 * MnNHYD=["S-1-FO-DIN"]
2427 * TMI STO=[ 9999999](cu-m)

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2428 *%-----|-----|
2429 *ADD HYD          NHYDs um=[ " S- 1- FO- DIS" ], NHYDs to add=[ " S- 1- FO- DIN" +" S- 1- FO- DIJ" ]
2430 *%-----|-----|
2431 *ROUTE RESERVOIR NHYDout=[ " S- 1- FO- DIR" ] , NHYDin=[ " S- 1- FO- DIS" ] ,
2432 *              RDT=[ 1 ] ( mi n ) ,
2433 *              TABLE of ( OUTFLOW STORAGE ) values
2434 *                    ( cms ) - ( ha- m )
2435 *                    [ 0.0      , 0.0 ]
2436 *                    [ 0.0611, 0.2038 ]
2437 *                    [   -1   ,  -1   ] (max twenty pts)
2438 *              NHYDovf=[ " S- 1FOD1ovf" ]
2439 *%-----|-----|
2440 *CONTINUOUS NASHYD NHYD=[ " S- 1- FO- DI" ], DT=[ 1 ] mi n , AREA=[ 5.11 ] ( ha ) ,
2441 *              DWF=[ 0 ] ( cms ) , CN C=[ 77 ] , IA=[ 4.67 ] ( mm ) ,
2442 *              N=[ 3 ] , TP=[ 1.10 ] hr s ,
2443 *              Continuous simulation parameters:
2444 *              IaRECper=[ 4 ] ( hr s ) ,
2445 *              SMN=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0.010 ] / ( mm ) ,
2446 *              InterEventTime=[ 12 ] ( hr s )
2447 *              Baseflow simulation parameters:
2448 *              BaseFlowOption=[ 1 ] ,
2449 *              InitGWResVol=[ 50 ] ( mm ) , GWResK=[ 0.96 ] ( mm/ day/ mm )
2450 *              VHydCond=[ 0.055 ] ( mm/ hr ) , END=- 1
2451 *%-----|-----|
2452 * -JFSA 2021-02-26 " S- 1- FO- D2" is a part of S- 1 sub-catchment. It is moved to drain
before station 980 on Foster Drain
2453 *CONTINUOUS STANDHYD NHYD=[ " S- 1- FO- D2" ], DT=[ 1 ] mi n , AREA=[ 4.94 ] ( ha ) ,
2454 *              XI MP=[ 0.55 ] , TI MP=[ 0.55 ] , DWF=[ 0 ] ( cms ) , LOSS=[ 2 ] ,
2455 *              SCS curve number CN=[ 74 ] ,
2456 *              Pervious surfaces: IAper=[ 4.67 ] ( mm ) , SLPP=[ 0.5 ] ( % ) ,
2457 *              LGP=[ 40 ] ( m ) , MNP=[ 0.25 ] , SCP=[ 0 ] ( mi n ) ,
2458 *              Impervious surfaces: IAimp=[ 1.57 ] ( mm ) , SLPI=[ 0.5 ] ( % ) ,
2459 *              LGI=[ 181.475 ] ( m ) , MNI=[ 0.013 ] , SCI=[ 0 ] ( mi n ) ,
2460 *              Continuous simulation parameters:
2461 *              IaRECper=[ 4 ] ( hr s ) , IaRECImp=[ 4 ] ( hr s ) ,
2462 *              SMN=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0.010 ] / ( mm ) ,
2463 *              InterEventTime=[ 18 ] ( hr s ) , END=- 1
2464 *%-----|-----|
2465 *CONTINUOUS NASHYD NHYD=[ " S- 1- FO- D2" ], DT=[ 1 ] mi n , AREA=[ 4.94 ] ( ha ) ,
2466 *              DWF=[ 0 ] ( cms ) , CN C=[ 77 ] , IA=[ 4.67 ] ( mm ) ,
2467 *              N=[ 3 ] , TP=[ 1.10 ] hr s ,
2468 *              Continuous simulation parameters:
2469 *              IaRECper=[ 4 ] ( hr s ) ,
2470 *              SMN=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0.010 ] / ( mm ) ,
2471 *              InterEventTime=[ 12 ] ( hr s )
2472 *              Baseflow simulation parameters:
2473 *              BaseFlowOption=[ 1 ] ,
2474 *              InitGWResVol=[ 50 ] ( mm ) , GWResK=[ 0.96 ] ( mm/ day/ mm )
2475 *              VHydCond=[ 0.055 ] ( mm/ hr ) , END=- 1
2476 *%-----|-----|
2477 *COMPUTE DUALHYD NHYDin=[ " S- 1- FO- D2" ] , CINLET=[ 0.508 ] ( cms ) , NINLET=[ 1 ] ,
2478 *              Mj NHYD=[ " S- 1- FO- D2J" ]
2479 *              MnNHYD=[ " S- 1- FO- D2N" ]
2480 *              TMSTO=[ 9999999 ] ( cu- m )
2481 *%-----|-----|
2482 *ADD HYD          NHYDs um=[ " S- 1- FO- D2S" ], NHYDs to add=[ " S- 1- FO- D2J" +" S- 1- FO- D2N" ]
2483 *%-----|-----|
2484 *ROUTE RESERVOIR NHYDout=[ " S- 1- FO- D2R" ] , NHYDin=[ " S- 1- FO- D2S" ] ,
2485 *              RDT=[ 1 ] ( mi n ) ,
2486 *              TABLE of ( OUTFLOW STORAGE ) values
2487 *                    ( cms ) - ( ha- m )
2488 *                    [ 0.0      , 0.0 ]
2489 *                    [ 0.0590, 0.1970 ]
2490 *                    [   -1   ,  -1   ] (max twenty pts)
2491 *              NHYDovf=[ " S- 1FOD2ovf" ]
2492 *%-----|-----|

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2493 * -JFSA 2021-02-26 "S-1-FO-F-D" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2494 *CONTINUOUS STANDHYD NHYD=["S-1-FO-F-D"], DT=[1]mi n, AREA=[14.96](ha),
2495 * XI MP=[0.65], TI MP=[0.65], DWF=[0](cms), LOSS=[2],
2496 * SCS curve number CN=[74],
2497 * Pervious surfaces: I A per=[4.67](mm), SLPP=[0.5](%),
2498 * LGP=[40](m), MNP=[0.25], SCP=[0](mi n),
2499 * Imper vious surfaces: I A i mp=[1.57](mm), SLPI =[0.5](%),
2500 * LGI =[315.806](m), MNI =[0.013], SCI =[0](mi n),
2501 * Continuous simulation parameters:
2502 * I a REC per =[4](hrs), I a REC i mp =[4](hrs),
2503 * SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2504 * Inter Event Ti me =[18](hrs), END=-1
2505 *%-----|-----|
2506 *CONTINUOUS NASHYD NHYD=["S-1-FO-F-D"], DT=[1]mi n, AREA=[14.96](ha),
2507 * DWF=[0](cms), CN C=[77], I A=[4.67](mm),
2508 * N=[3], TP=[1.007]hrs,
2509 * Continuous simulation parameters:
2510 * I a REC per =[4](hrs),
2511 * SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2512 * Inter Event Ti me =[12](hrs)
2513 * Baseflow simulation parameters:
2514 * BaseFl owOpt ion=[1],
2515 * Ini t GWRes Vol =[50](mm), GWRes K=[0.96](mm/ day/ mm)
2516 * VHydCond=[0.055](mm/ hr), END=-1
2517 *%-----|-----|
2518 *COMPUTE DUALHYD NHYD i n=["S-1-FO-F-D"], CI NLET=[1.749](cms), NI NLET=[1],
2519 * M a j NHYD=["S-1FO-F-DJ"]
2520 * M nNHYD=["S-1FO-F-DN"]
2521 * TM I STO=[9999999](cu-m)
2522 *%-----|-----|
2523 *ADD HYD NHYDs um=["S-1FO-F-DS"], NHYDs to add=["S-1FO-F-DJ"+"S-1FO-F-DN"]
2524 *%-----|-----|
2525 *ROUTE RESERVOIR NHYDout=["S-1FO-F-DR"], NHYD i n=["S-1FO-F-DS"],
2526 * RDT=[1](mi n),
2527 * TABLE of ( OUTFLOW STORAGE ) values
2528 * ( cms ) - ( ha-m)
2529 * [ 0.0 , 0.0 ]
2530 * [ 0.1788, 0.5966 ]
2531 * [ -1 , -1 ] (max twenty pts)
2532 * NHYDovf=["S-1FoFDovf"]
2533 *%-----|-----|
2534 *CONTINUOUS STANDHYD NHYD=["S-1-DI"], DT=[1](mi n), AREA=[21.67](ha), XI MP=[0.65],
TI MP=[0.65], DWF=[0](cms),
2535 * LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
I A per=[4.67](mm), SLPP=[2.0](%),
2536 * LGP=[40](m), MNP=[0.25], SCP=[0](mi n), Imper vious surfaces:
I A i mp=[1.57](mm), SLPI =[0.75](%),
2537 * LGI =[380.088](m), MNI =[0.013], SCI =[0](mi n),
2538 * Continuous simulation parameters:
2539 * I a REC per =[4](hrs), I a REC i mp =[4](hrs),
2540 * SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2541 * Inter Event Ti me =[12](hrs), END=-1
2542 *%-----|-----|
2543 CONTINUOUS NASHYD NHYD=["S-1-DI"], DT=[1]mi n, AREA=[21.67](ha),
2544 DWF=[0](cms), CN C=[77], I A=[4.67](mm),
2545 N=[3], TP=[1.066]hrs,
2546 Continuous simulation parameters:
2547 I a REC per =[4](hrs),
2548 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2549 Inter Event Ti me =[12](hrs)
2550 Baseflow simulation parameters:
2551 BaseFl owOpt ion=[1],
2552 Ini t GWRes Vol =[50](mm), GWRes K=[0.96](mm/ day/ mm)
2553 VHydCond=[0.055](mm/ hr), END=-1
2554 *%-----|-----|

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2614 * IaRECper=[ 4](hr s), IaRECImp=[ 4](hr s),
2615 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2616 * InterEventTime=[ 12](hr s), END=- 1
2617 *%-----|-----
2618 *CONTINUOUS NASHYD NHYD=["S-1-D3"], DT=[ 1]mi n, AREA=[ 6.79](ha),
2619 * DWF=[ 0](cms), CN C=[ 77], IA=[ 4.67](mm),
2620 * N=[ 3], TP=[ 1.281]hr s,
2621 * Continuous simulation parameters:
2622 * IaRECper=[ 4](hr s),
2623 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2624 * InterEventTime=[ 12](hr s)
2625 * Baseflow simulation parameters:
2626 * BaseFlowOption=[ 1],
2627 * InItGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
2628 * VHydCond=[ 0.055](mm/hr), END=- 1
2629 *%-----|-----
2630 *COMPUTE DUALHYD NHYDin=["S-1-D3"], CINLET=[ 0.719](cms), NINLET=[ 1],
2631 * MjNHYD=["S-1-D3J"]
2632 * MnNHYD=["S-1-D3N"]
2633 * TMI STO=[ 9999999](cu-m)
2634 *%-----|-----
2635 *ADD HYD NHYDsum=["S-1-D3S"], NHYDs to add=["S-1-D3J"+"S-1-D3N"]
2636 *%-----|-----
2637 *ROUTE RESERVOIR NHYDout=["S-1-D3R"], NHYDin=["S-1-D3S"],
2638 * RDT=[ 1](mi n),
2639 * TABLE of ( OUTFLOW STORAGE ) values
2640 * ( cms ) - ( ha-m)
2641 * [ 0.0 , 0.0 ]
2642 * [ 0.0811, 0.2708 ]
2643 * [ -1 , -1 ] (max twenty pts)
2644 * NHYDovf=["S-1-D3Rovf"]
2645 *%-----|-----
2646 *CONTINUOUS STANDHYD NHYD=["S-1-D4"], DT=[ 1](mi n), AREA=[ 3.28](ha), XI MP=[ 0.65],
TI MP=[ 0.65], DWF=[ 0](cms),
2647 * LOSS=[ 2], SCS curve number CN=[ 75], Pervious surfaces:
I Aper=[ 4.67](mm), SLPP=[ 2.0](%),
2648 * LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](mi n), Impervious surfaces:
I Ai mp=[ 1.57](mm), SLPI=[ 0.75](%),
2649 * LGI=[ 147.874](m), MNI=[ 0.013], SCI=[ 0](mi n),
2650 * Continuous simulation parameters:
2651 * IaRECper=[ 4](hr s), IaRECImp=[ 4](hr s),
2652 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2653 * InterEventTime=[ 12](hr s), END=- 1
2654 *%-----|-----
2655 CONTINUOUS NASHYD NHYD=["S-1-D4"], DT=[ 1]mi n, AREA=[ 3.28](ha),
2656 DWF=[ 0](cms), CN C=[ 77], IA=[ 4.67](mm),
2657 N=[ 3], TP=[ 1.10]hr s,
2658 Continuous simulation parameters:
2659 IaRECper=[ 4](hr s),
2660 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2661 InterEventTime=[ 12](hr s)
2662 Baseflow simulation parameters:
2663 BaseFlowOption=[ 1],
2664 InItGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
2665 VHydCond=[ 0.055](mm/hr), END=- 1
2666 *%-----|-----
2667 *COMPUTE DUALHYD NHYDin=["S-1-D4"], CINLET=[ 0.373](cms), NINLET=[ 1],
2668 * MjNHYD=["S-1-D4J"]
2669 * MnNHYD=["S-1-D4N"]
2670 * TMI STO=[ 9999999](cu-m)
2671 *%-----|-----
2672 *ADD HYD NHYDsum=["S-1-D4S"], NHYDs to add=["S-1-D4J"+"S-1-D4N"]
2673 *%-----|-----
2674 *ROUTE RESERVOIR NHYDout=["S-1-D4R"], NHYDin=["S-1-D4S"],
2675 * RDT=[ 1](mi n),
2676 * TABLE of ( OUTFLOW STORAGE ) values

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2677 *                ( cms ) - ( ha - m )
2678 *                [ 0.0      , 0.0 ]
2679 *                [ 0.0392, 0.1308 ]
2680 *                [ -1      , -1      ] (max twenty pts)
2681 *                NHYDovf=[ "S-1-D4Rovf" ]
2682 *%-----|-----|
2683 *CONTINUOUS STANDHYD NHYD=[ "S-1-D5" ], DT=[ 1 ](mi n), AREA=[ 12.84 ](ha), XI MP=[ 0.65 ],
TI MP=[ 0.65 ], DWF=[ 0 ]( cms ),
2685 *                LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](mi n), Impervious surfaces:
I Ai mp=[ 1.57 ](mm), SLPI=[ 0.75 ]( % ),
2686 *                LGI=[ 292.57 ](m), MNI=[ 0.013 ], SCI=[ 0 ](mi n),
2687 *                Continuous simulation parameters:
2688 *                IaRECper=[ 4 ](hrs), IaRECI mp=[ 4 ](hrs),
2689 *                SM N=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2690 *                InterEvent Time=[ 12 ](hrs), END=-1
2691 *%-----|-----|
2692 CONTINUOUS NASHYD NHYD=[ "S-1-D5" ], DT=[ 1 ]mi n, AREA=[ 12.84 ](ha),
2693 DWF=[ 0 ]( cms ), CNV C=[ 77 ], IA=[ 4.67 ](mm),
2694 N=[ 3 ], TP=[ 1.10 ]hrs,
2695 Continuous simulation parameters:
2696 IaRECper=[ 4 ](hrs),
2697 SM N=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2698 InterEvent Time=[ 12 ](hrs)
2699 Baseflow simulation parameters:
2700 BaseFlowOption=[ 1 ],
2701 Ini tGWRes Vol=[ 50 ](mm), GWRes K=[ 0.96 ](mm/ day/ mm)
2702 VHydCond=[ 0.055 ](mm/ hr), END=-1
2703 *%-----|-----|
2704 *COMPUTE DUALHYD NHYDi n=[ "S-1-D5" ], CI NLET=[ 1.395 ]( cms ), NI NLET=[ 1 ],
2705 *                Mi j NHYD=[ "S-1-D5J" ]
2706 *                M nNHYD=[ "S-1-D5N" ]
2707 *                TM I STO=[ 9999999 ](cu - m)
2708 *%-----|-----|
2709 *ADD HYD NHYDs um=[ "S-1-D5S" ], NHYDs to add=[ "S-1-D5J"+"S-1-D5N" ]
2710 *%-----|-----|
2711 *ROUTE RESERVOIR NHYDout=[ "S-1-D5R" ], NHYDi n=[ "S-1-D5S" ],
2712 *                RDT=[ 1 ](mi n),
2713 *                TABLE of ( OUTFLOW STORAGE ) values
2714 *                ( cms ) - ( ha - m )
2715 *                [ 0.0      , 0.0 ]
2717 *                [ -1      , -1      ] (max twenty pts)
2718 *                NHYDovf=[ "S-1-D5Rovf" ]
2719 *%-----|-----|
2720 *CONTINUOUS STANDHYD NHYD=[ "S-1-D6" ], DT=[ 1 ](mi n), AREA=[ 1.75 ](ha), XI MP=[ 0.65 ],
TI MP=[ 0.65 ], DWF=[ 0 ]( cms ),
2721 *                LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
I Aper=[ 4.67 ](mm), SLPP=[ 2.0 ]( % ),
2722 *                LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](mi n), Impervious surfaces:
I Ai mp=[ 1.57 ](mm), SLPI=[ 0.75 ]( % ),
2723 *                LGI=[ 108.01 ](m), MNI=[ 0.013 ], SCI=[ 0 ](mi n),
2724 *                Continuous simulation parameters:
2725 *                IaRECper=[ 4 ](hrs), IaRECI mp=[ 4 ](hrs),
2726 *                SM N=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2727 *                InterEvent Time=[ 12 ](hrs), END=-1
2728 *%-----|-----|
2729 CONTINUOUS NASHYD NHYD=[ "S-1-D6" ], DT=[ 1 ]mi n, AREA=[ 1.75 ](ha),
2730 DWF=[ 0 ]( cms ), CNV C=[ 77 ], IA=[ 4.67 ](mm),
2731 N=[ 3 ], TP=[ 1.10 ]hrs,
2732 Continuous simulation parameters:
2733 IaRECper=[ 4 ](hrs),
2734 SM N=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2735 InterEvent Time=[ 12 ](hrs)
2736 Baseflow simulation parameters:

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2737 BaseFlowOpt ion=[ 1] ,
2738 Ini t GWRes Vol =[ 50] ( mm) , GWRes K=[ 0. 96] ( mm/ day/ mm)
2739 VHydCond=[ 0. 055] ( mm/ hr) , END=- 1
2740 *%-----|-----
2741 *COMPUTE DUALHYD NHYDi n=[ " S- 1- D6" ] , CI NLET=[ 0. 218] ( cms) , NI NLET=[ 1] ,
2742 * Mj NHYD=[ " S- 1- D6J" ]
2743 * M nNHYD=[ " S- 1- D6N" ]
2744 * TM STO=[ 9999999] ( cu- m)
2745 *%-----|-----
2746 *ADD HYD NHYDs um=[ " S- 1- D6S" ] , NHYDs to add=[ " S- 1- D6J" +" S- 1- D6N" ]
2747 *%-----|-----
2748 *ROUTE RESERVOIR NHYDout =[ " S- 1- D6R" ] , NHYDi n=[ " S- 1- D6S" ] ,
2749 * RDT=[ 1] ( mi n) ,
2750 * TABLE of ( OUTFLOW STORAGE ) values
2751 * ( cms) - ( ha- m)
2752 * [ 0. 0 , 0. 0 ]
2753 * [ 0. 0209, 0. 0698 ]
2754 * [ -1 , -1 ] (max twenty pts)
2755 * NHYDovf=[ " S- 1- D6Rovf" ]
2756 *%-----|-----
2757 *CONTINUOUS STANDHYD NHYD=[ " S- 1- D7" ] , DT=[ 1] ( mi n) , AREA=[ 2. 03] ( ha) , XI MP=[ 0. 65] ,
TI MP=[ 0. 65] , DWF=[ 0] ( cms) ,
2758 * LOSS=[ 2] , SCS curve number CN=[ 75] , Pervious surfaces:
IAper=[ 4. 67] ( mm) , SLPP=[ 2. 0] ( % ) ,

2760 * LGI=[ 116. 33] ( m) , MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
2761 * Continuous simulation parameters:
2762 * IaRECper=[ 4] ( hr s) , IaRECI mp=[ 4] ( hr s) ,
2763 * SM N=[ -1] ( mm) , SMAX=[ -1] ( mm) , SK=[ 0. 010] / ( mm) ,
2764 * Inter Event Ti me=[ 12] ( hr s) , END=- 1
2765 *%-----|-----
2766 CONTINUOUS NASHYD NHYD=[ " S- 1- D7" ] , DT=[ 1] mi n , AREA=[ 2. 03] ( ha) ,
2767 DWF=[ 0] ( cms) , CN C=[ 77] , IA=[ 4. 67] ( mm) ,
2768 N=[ 3] , TP=[ 1. 10] hr s ,
2769 Continuous simulation parameters:
2770 IaRECper=[ 4] ( hr s) ,
2771 SM N=[ -1] ( mm) , SMAX=[ -1] ( mm) , SK=[ 0. 010] / ( mm) ,
2772 Inter Event Ti me=[ 12] ( hr s)
2773 Baseflow simulation parameters:
2774 BaseFlowOpt ion=[ 1] ,
2775 Ini t GWRes Vol =[ 50] ( mm) , GWRes K=[ 0. 96] ( mm/ day/ mm)
2776 VHydCond=[ 0. 055] ( mm/ hr) , END=- 1
2777 *%-----|-----
2778 *COMPUTE DUALHYD NHYDi n=[ " S- 1- D7" ] , CI NLET=[ 2. 279] ( cms) , NI NLET=[ 1] ,
2779 * Mj NHYD=[ " S- 1- D7J" ]
2780 * M nNHYD=[ " S- 1- D7N" ]
2781 * TM STO=[ 9999999] ( cu- m)
2782 *%-----|-----
2783 *ADD HYD NHYDs um=[ " S- 1- D7S" ] , NHYDs to add=[ " S- 1- D7J" +" S- 1- D7N" ]
2784 *%-----|-----
2785 *ROUTE RESERVOIR NHYDout =[ " S- 1- D7R" ] , NHYDi n=[ " S- 1- D7S" ] ,
2786 * RDT=[ 1] ( mi n) ,
2787 * TABLE of ( OUTFLOW STORAGE ) values
2788 * ( cms) - ( ha- m)
2789 * [ 0. 0 , 0. 0 ]
2790 * [ 0. 0243, 0. 0810 ]
2791 * [ -1 , -1 ] (max twenty pts)
2792 * NHYDovf=[ " S- 1- D8Rovf" ]
2793 *%-----|-----
2794 * -JFSA 2021-02-26 " S- 1- D8" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2795 *CONTINUOUS STANDHYD NHYD=[ " S- 1- D8" ] , DT=[ 1] ( mi n) , AREA=[ 5. 27] ( ha) , XI MP=[ 0. 65] ,
TI MP=[ 0. 65] , DWF=[ 0] ( cms) ,
2796 * LOSS=[ 2] , SCS curve number CN=[ 75] , Pervious surfaces:
IAper=[ 4. 67] ( mm) , SLPP=[ 2. 0] ( % ) ,

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2797 *                LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min), Impervious surfaces:
I Ai mp=[ 1.57](mm), SLPI=[ 0.75](%),
2798 *                LGI=[ 187.439](m), MNI=[ 0.013], SCI=[ 0](min),
2799 *                Continuous simulation parameters:
2800 *                IaRECPper=[ 4](hrs), IaRECImp=[ 4](hrs),
2801 *                SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2802 *                InterEventTime=[ 12](hrs), END=- 1
2803 *%-----|-----
2804 *CONTINUOUS NASHYD NHYD=[ "S-1-D8"], DT=[ 1]min, AREA=[ 5.27](ha),
2805 *                DWF=[ 0](cms), CN/C=[ 77], IA=[ 4.67](mm),
2806 *                N=[ 3], TP=[ 1.10]hrs,
2807 *                Continuous simulation parameters:
2808 *                IaRECPper=[ 4](hrs),
2809 *                SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2810 *                InterEventTime=[ 12](hrs)
2811 *                Baseflow simulation parameters:
2812 *                BaseFlowOption=[ 1],
2813 *                InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
2814 *                VHydCond=[ 0.055](mm/hr), END=- 1
2815 *%-----|-----
2816 *COMPUTE DUALHYD NHYDin=[ "S-1-D8"], CINLET=[ 2.279](cms), NI NLET=[ 1],
2817 *                Mij NHYD=[ "S-1-D8J"]
2818 *                MnNHYD=[ "S-1-D8N"]
2819 *                TMI STO=[ 9999999](cu-m)
2820 *%-----|-----
2821 *ADD HYD NHYDsum=[ "S-1-D8S"], NHYDs to add=[ "S-1-D8J"+"S-1-D8N"]
2822 *%-----|-----
2823 *ADD HYD NHYDsum=[ "S-1-D"], NHYDs to add=[ "S-1-Okeefe"+"S-1"+"S-1-Fost"]
2824 *%-----|-----
2825 *COMPUTE DUALHYD NHYDin=[ "S-1-D"], CINLET=[ 11.616](cms), NI NLET=[ 1],
2826 *                Mij NHYD=[ "S-1-D-M"]
2827 *                MnNHYD=[ "S-1-D-MN"]
2828 *                TMI STO=[ 5974](cu-m)
2829 *%-----|-----
2830 *ADD HYD NHYDsum=[ "S-1-DEV"], NHYDs to add=[ "S-1-D-M"+"S-1-D-MN"]
2831 *%-----|-----
2832 *ROUTE RESERVOIR NHYDout=[ "S-1-D8R"], NHYDin=[ "S-1-D8S"],
2833 *                RDT=[ 1](min),
2834 *                TABLE of ( OUTFLOW STORAGE ) values
2835 *                (cms) - (ha-m)
2836 *                [ 0.0, 0.0 ]
2837 *                [ 0.0630, 0.2102 ]
2838 *                [ -1, -1 ] (max twenty pts)
2839 *                NHYDovf=[ "S-1-D8Rovf"]
2840 *%-----|-----
2841 *%-----|-----
2842 *                -JFSA 2021-02-08 Clarke (MS_P2 and P2-OVF) and Clarke Undeveloped area
(W_CLAR_UNDE) drain to Jock River at Station 5002 instead of Station 4534
2843 *# Catchment W_CLAR
2844 *# - To West Clarke Drain (south of the Jock)
2845 *# - Subdivision with 43% imp. as per Barrhaven South MS
2846 *# - 2020-11-30 update CLARKE Tributary Drainage Area to = 121 ha based on
P598(04)-11
2847 *# - 2020-11-30 split CLARKE Drainage Area to MAJOR and ALL
2848 *#*****
2849 CONTINUOUS STANDHYD NHYD=[ "W_CLAR_M"], DT=[ 1]min, AREA=[ 1.772](ha),
2850 *                XI MP=[ 0.46], TI MP=[ 0.59], DWF=[ 0](cms), LOSS=[ 2],
2851 *                SCS curve number CN=[ 77],
2852 *                Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
2853 *                LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
2854 *                Impervious surfaces: IAi mp=[ 1.57](mm), SLPI=[ 1](%),
2855 *                LGI=[ 109](m), MNI=[ 0.013], SCI=[ 0](min),
2856 *                Continuous simulation parameters:
2857 *                IaRECPper=[ 4](hrs), IaRECImp=[ 4](hrs),
2858 *                SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2859 *                InterEventTime=[ 18](hrs), END=- 1

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2860 *%-----|-----|
2861 *COMPUTE DUALHYD      NHYDin=["W_CLAR_M"],  CILET=[ 0.213](cms),  NILET=[ 1],
2862 *                      MjNHYD=["W_CLAR_Mj"]
2863 *                      MnNHYD=["W_CLAR_Mn"]
2864 *                      TMSSTO=[ 0.1](cu-m)
2865 *%-----|-----|
2866 *# 5-Year + 12% Capture
2867 ROUTE RESERVOIR      NHYDout=["W_CLAR_Mn"],  NHYDin=["W_CLAR_M"],
2868                      RDT=[ 1](min),
2869                      TABLE of ( OUTFLOW STORAGE ) values
2870                      (cms) - (ha-m)
2871                      [ 0.0      , 0.0 ]
2872                      [ 0.213  , 0.0001 ]
2873                      [      -1  , -1    ] (max twenty pts)
2874                      NHYDovf=["W_CLAR_Mj"],
2875 *%-----|-----|
2876 *      -Clarke_All area from P 598(04)-11 = 120.207 ha, change to 127.298 ha based on
GIS measurements,
2877 *      -JFSA, 2021-01-19 update W_CLAR_ALL to (121.17-1.772=119.398) ha based on GIS
measurements W_CLAR is 121.17 ha and W_CLAR_M is 1.772 ha
2878 CONTINUOUS STANDHYD NHYD=["W_CLAR_ALL"],  DT=[ 1]min,  AREA=[ 119.398](ha),
2879                      XI MP=[ 0.60],  TI MP=[ 0.65],  DWF=[ 0](cms),  LOSS=[ 2],
2880                      SCS curve number CN=[ 77],
2881                      Pervious surfaces: IAper=[ 4.67](mm),  SLPP=[ 1](%),
2882                      LGP=[ 40](m),  MNP=[ 0.25],  SCP=[ 0](min),
2883                      Impervious surfaces: IAimp=[ 1.57](mm),  SLPI=[ 1](%),
2884                      LGI=[ 892.18](m),  MNI=[ 0.013],  SCI=[ 0](min),
2885                      Continuous simulation parameters:
2886                      IaREcper=[ 4](hrs),  IaREcimp=[ 4](hrs),
2887                      SMN=[ -1](mm),  SMAX=[ -1](mm),  SK=[ 0.010]/(mm),
2888                      InterEventTime=[ 18](hrs),  END=-1
2889 *%-----|-----|
2890 ADD HYD              NHYDsum=["W_CLAR"],  NHYDs to add=["W_CLAR_ALL"+"W_CLAR_Mj"]
2891 *%-----|-----|
2892 SAVE HYD             NHYD=["W_CLAR"],  # OF PCYCLES=[ -1],  ICASEsh=[ 1]
2893                      HYD_COMMENT=["Total Flows to West Clarke"]
2894 *#*****
2895 *#      West Clarke Pond 2
2896 *#      - Rating curve obtained from Barrhaven South M&S modeling
2897 *#      - Tributary Drainage Area to M&S Pond 2 = 241 ha
2898 *#*****
2899 ROUTE RESERVOIR      NHYDout=["MS_P2"],  NHYDin=["W_CLAR"],
2900                      RDT=[ 1](min),
2901                      TABLE of ( OUTFLOW STORAGE ) values
2902                      (cms) - (ha-m)
2903                      [ 0.0      , 0.0 ]
2904                      [ 0.128  , 0.161 ]
2905                      [ 0.138  , 0.409 ]
2906                      [ 0.148  , 0.68 ]
2907                      [ 0.227  , 0.931 ]
2908                      [ 0.354  , 1.223 ]
2909                      [ 0.505  , 1.52 ]
2910                      [ 0.666  , 1.821 ]
2911                      [ 0.831  , 2.123 ]
2912                      [ 0.995  , 2.434 ]
2913                      [ 1.069  , 2.583 ]
2914                      [ 1.51   , 2.647 ]
2915                      [ 4.904  , 2.861 ]
2916                      [ 13.048 , 3.188 ]
2917                      [ 23.745 , 3.523 ]
2918                      [ 36.474 , 3.871 ]
2919                      [ 45.938 , 4.127 ]
2920                      [ 61.652 , 4.539 ]
2921                      [      -1  , -1    ] (max twenty pts)
2922                      NHYDovf=["P2-OVF"]
2923 *%-----|-----|

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2924 *#*****
2925 * -JFSA 2021-01-22 "W_CLAR_UNDE" (west of Clarke sub-catchment) discharges
directly to the jock river through a road side ditch on the west side of Borrisokane
road (station 6016)
2926 *CONTINUOUS NASHYD NHYD=["W_CLAR_UNDE"], DT=[1] min, AREA=[35.65](ha),
2927 * DWF=[0](cms), CNVC=[77], IA=[4.67](mm),
2928 * N=[3], TP=[1.10]hrs,
2929 * Continuous simulation parameters:
2930 * IaRECper=[4](hrs),
2931 * SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2932 * InterEventTime=[12](hrs)
2933 * Baseflow simulation parameters:
2934 * BaseFlowOption=[1],
2935 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2936 * VHydCond=[0.055](mm/hr), END=-1
2937 *%-----|-----|
2938 ADD HYD NHYDsum=["SN_CE"], NHYDs to add=["N_CE"+
2939 +"S-1-D4"+"S-1-D5"+"MS_P2"+"P2-OVF"]
2940 *%-----|-----|
2941 SAVE HYD NHYD=["SN_CE"], # OF PCYCLES=[-1], ICASEsh=[1]
2942 HYD_COMMENT=["Total Flows before Station 5737 on Jock River"]
2943 *%-----|-----|
2944 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 5737
2945 *# JFSA 2021-02-25 add station 5737 before station 5002. Station 5737 was extracted
from the HEC-RAS model
T:\PROJ\1474-16\Design\20201026-QuantityControlAnalysis\HEC-RAS\JockLidar2005
2946 *# JFSA 2021-03-02 change the slope to 0.1% instead of 0.0175 to stabilize the model
2947 ROUTE CHANNEL NHYDout=["5737"], NHYDin=["SN_CE"],
2948 RDT=[1](min),
2949 CHLGTH=[270](m), CHSLOPE=[0.0175](%),
2950 FPSLOPE=[0.0175](%),
2951 SECNUM=[1.0], NSEG=[3]
2952 (SEGROUGH, SEGDI ST (m))=
2953 [0.050, -24.04
2954 -0.035, 23.92
2955 0.050, 1130.8] NSEG times
2956 (DISTANCE (m), ELEVATION (m))=
2957 [-1060.52, 94 ]
2958 [-268.6, 91.5 ]
2959 [-259.43, 91.5 ]
2960 [-179.48, 91.5 ]
2961 [-67.9, 91.5 ]
2962 [-59.21, 91.5 ]
2963 [-33.19, 91 ]
2964 [-26.08, 90.5 ]
2965 [-24.04, 90 ]
2966 [-13.14, 86.77 ]
2967 [0, 85 ]
2968 [14.68, 86.74 ]
2969 [23.92, 90 ]
2970 [25.78, 90.5 ]
2971 [31.91, 91 ]
2972 [91.95, 91.5 ]
2973 [772.15, 92 ]
2974 [961.49, 92.5 ]
2975 [1044.69, 93 ]
2976 [1130.8, 95 ]
2977 *%-----|-----|
2978 ADD HYD NHYDsum=["5002"], NHYDs to add=["5737"+
2979 +"S-1-D1"+"S-1-D6"+"S-1-D7"]
2980 *%-----|-----|
2981 SAVE HYD NHYD=["5002"], # OF PCYCLES=[-1], ICASEsh=[1]
2982 HYD_COMMENT=["Total Flows before Station 5002 on Jock River"]
2983 *%-----|-----|
2984 *# Hydrograph from Node Cedarview Road routed to Node at West Clarke Drain
2985 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 5002

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2986 *# JFSA 2021-02-19 Change the slope from 0.01 % (as per Stantec Report 2007) to 0.0255
 % so the model will be more stable and give reasonable results. It is justifiable as
 ROUTE CHANNELs aren't well suited to really flat slopes.

2987 *# JFSA 2021-02-19 Change to three ROUTE CHANNEL with length 275 m each instead of one
 with 825 m length so the model will be more stable

2988 *# JFSA 2021-02-26 change the length of 5002 route channel from 825 m to 736 m That is
 because of adding station 5737 between station 6016 and station 5002. Then the length
 from station 5737 to station 5002 is 736 m Change the slope from 0.0255 % to 0.09511 %

2989 *
 2990 ROUTE CHANNEL NHYDout=["N_WCa"] , NHYDin=["5002"] ,
 2991 RDT=[1] (mi n) ,
 2992 CHLGTH=[245.33333] (m) , CHSLOPE=[0.09511] (%) ,
 2993 FPSLOPE=[0.09511] (%) ,
 2994 SECNUM=[1.0] , NSEG=[3]
 2995 (SEGROUGH, SEGDI ST (m)) =
 2996 [0.050, -37.5
 2997 -0.035, 37.50
 2998 0.050, 157.05] NSEG t i m e s
 2999 (DI STANCE (m) , ELEVATI ON (m)) =
 3000 [-601.81, 91.5]
 3001 [-37.50, 90.00]
 3002 [-19.61, 87.04]
 3003 [0.00, 85.70]
 3004 [14.87, 86.93]
 3005 [37.50, 90.00]
 3006 [38.54, 90.50]
 3007 [42.23, 91]
 3008 [157.05, 91.50]
 3009 * [161.44, 91.50]
 3010 * [236.48, 93.00]
 3011 * [385.47, 92.50]
 3012 * [390.78, 92.50]

3013 *%-----|
 3014 ROUTE CHANNEL NHYDout=["N_WCb"] , NHYDin=["N_WCa"] ,
 3015 RDT=[1] (mi n) ,
 3016 CHLGTH=[245.33333] (m) , CHSLOPE=[0.09511] (%) ,
 3017 FPSLOPE=[0.09511] (%) ,
 3018 SECNUM=[1.0] , NSEG=[3]
 3019 (SEGROUGH, SEGDI ST (m)) =
 3020 [0.050, -37.5
 3021 -0.035, 37.50
 3022 0.050, 157.05] NSEG t i m e s
 3023 (DI STANCE (m) , ELEVATI ON (m)) =
 3024 [-601.81, 91.5]
 3025 [-37.50, 90.00]
 3026 [-19.61, 87.04]
 3027 [0.00, 85.70]
 3028 [14.87, 86.93]
 3029 [37.50, 90.00]
 3030 [38.54, 90.50]
 3031 [42.23, 91]
 3032 [157.05, 91.50]

3033 *%-----|
 3034 ROUTE CHANNEL NHYDout=["N_WC"] , NHYDin=["N_WCb"] ,
 3035 RDT=[1] (mi n) ,
 3036 CHLGTH=[245.33333] (m) , CHSLOPE=[0.09511] (%) ,
 3037 FPSLOPE=[0.09511] (%) ,
 3038 SECNUM=[1.0] , NSEG=[3]
 3039 (SEGROUGH, SEGDI ST (m)) =
 3040 [0.050, -37.5
 3041 -0.035, 37.50
 3042 0.050, 157.05] NSEG t i m e s
 3043 (DI STANCE (m) , ELEVATI ON (m)) =
 3044 [-601.81, 91.5]
 3045 [-37.50, 90.00]
 3046 [-19.61, 87.04]

```

3047 [ 0.00, 85.70]
3048 [ 14.87, 86.93]
3049 [ 37.50, 90.00]
3050 [ 38.54, 90.50]
3051 [ 42.23, 91]
3052 [ 157.05, 91.50]
3053 *#*****
3054 * -JFSA 2021-02-08 Clarke (MS_P2 and P2-OVF) and Clarke Undeveloped area
(W_CLAR_UNDE) drain to Jock River at Station 5002 instead of Station 4534
3055 *ADD HYD NHYDs um=["SN_WC"], NHYDs to
add=["MS_P2"+"P2-OVF"+"N_WC"+"W_CLAR_UNDE"]
3056 *%-----|-----|
3057 *SAVE HYD NHYD=["SN_WC"], # OF PCYCLES=[-1], ICASEsh=[1]
3058 * HYD_COMMENT=["Total Flows at West Clarke Pond Outlet"]
3059 *%-----|-----|
3060 *# Hydrograph from Node West Clarke routed to Node at Kennedy - Burnett Drain
3061 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 4534
3062 *#
3063 ROUTE CHANNEL NHYDout=["N_KB"], NHYDin=["N_WC"],
3064 RDT=[1](min),
3065 CHLGTH=[1020](m), CHSLOPE=[0.0498](%),
3066 FPSLOPE=[0.0498](%),
3067 SECNUM=[1.0], NSEG=[3]
3068 ( SEGROUGH, SEGDI ST (m))=
3069 [0.050, -23.63
3070 -0.035, 23.63
3071 0.050, 728.3] NSEG times
3072 ( DISTANCE (m), ELEVATION (m))=
3073 [-1082.01, 94]
3074 [-1028.17, 92.5]
3075 [-992.3, 93.5]
3076 [-279.34, 90]
3077 [-23.63, 90]
3078 [-13.45, 87.13]
3079 [-0.07, 86.24]
3080 [10.54, 87.15]
3081 [23.63, 90]
3082 [24.86, 90.5]
3083 [26.72, 91]
3084 [45.07, 91.5]
3085 [128.17, 91.5]
3086 [270.7, 92.5]
3087 [728.3, 95]
3088 *%-----|-----|
3089 *#*****
3090 *# Catchment KEN_BU
3091 *# - To Kennedy-Burnett SWM Facility
3092 *# - Outlets to Fraser-Clarke drain (north of the Jock)
3093 *# - Medium density residential subdivision
3094 * - Add Kennedy Burnett model (Convert PCSWMM from NOVATECH June, 2020 to SWWHYMD)
3095 *#*****
3096 *CONTINUOUS STANDHYD NHYD=["KEN_BU"], DT=[1]min, AREA=[281](ha),
3097 * XI MP=[0.55], TI MP=[0.55], DWF=[0](cms), LOSS=[2],
3098 * SCS curve number CN=[71],
3099 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3100 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3101 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3102 * LGI=[1369](m), MNI=[0.013], SCI=[0](min),
3103 * Continuous simulation parameters:
3104 * IaRECper=[4](hrs), IaRECImp=[4](hrs),
3105 * SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3106 * InterEventTime=[18](hrs), END=-1
3107 *%-----|-----|
3108 *#*****
3109 *# Existing Kennedy-Burnett SWM Facility
3110 *# - Rating curve obtained from URTKBP

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3111 *# - Tributary Drainage Area to Pond = 160 ha
3112 *#*****
3113 *ROUTE RESERVOIR NHYDout=[ "KEN_P"], NHYDin=[ "KEN_BU"],
3114 * RDT=[ 1](mi n),
3115 * TABLE of ( OUTFLOW STORAGE ) values
3116 * (cms) - (ha-m)
3117 * [ 0.0 , 0.0 ]
3118 * [ 0.13 , 0.26]
3119 * [ 0.43 , 0.56]
3120 * [ 0.67 , 0.90]
3121 * [ 0.86 , 1.32]
3122 * [ 1.01 , 1.79]
3123 * [ 1.15 , 2.33]
3124 * [ -1 , -1 ] (max twenty pts)
3125 * NHYDovf=[ "KEN_OV"]
3126 *%-----|-----|
3127 * -JFSA, 2021-01-19 update all KEN_BU areas based on GIS measurements
3128 CONTINUOUS STANDHYD NHYD=[ "KB-01A"], DT=[ 1]mi n, AREA=[ 40.82](ha), XI MP=[ 0.097],
3129 T I M P=[ 0.4], DWF=[ 0](cms), LOSS=[ 1]:
3129 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3130 F=[ 0.00](mm),
3130 Pervious areas: I A p e r=[ 4.67](mm), SLPP=[ 0.5](%), LGP=[ 40](m),
3131 MNP=[ 0.250], SCP=[ 0](mi n),
3131 Impervious areas: I A i m p=[ 0.785](mm), SLPI=[ 0.5](%),
3132 L G I=[ 521.664](m), M N I=[ 0.013], S C I=[ 0](mi n),
3132 Continuous simulation parameters:
3133 I a R E C p e r=[ 4](hrs), I a R E C i m p=[ 4](hrs), I n t e r E v e n t T i m e=[ 12](hrs),
3133 E N D=- 1
3134 *%-----|-----|
3135 COMPUTE DUALHYD NHYDin=[ "KB-01A"], CI NLET=[ 3.6](cms), NI NLET=[ 1],
3136 M a j N H Y D=[ "KB-01A-M"]
3137 M n N H Y D=[ "KB-01A-MN"]
3138 T M S T O=[ 4995](cu-m)
3139 *%-----|-----|
3140 ADD HYD NHYDs um=[ "KB-01A-S"], NHYDs t o a d d=[ "KB-01A-M"+"KB-01A-MN"]
3141 *%-----|-----|
3142 CONTINUOUS STANDHYD NHYD=[ "KB-01B"], DT=[ 1]mi n, AREA=[ 31.1](ha), XI MP=[ 0.1875],
3143 T I M P=[ 0.375], DWF=[ 0](cms), LOSS=[ 1]:
3143 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3144 F=[ 0.00](mm),
3144 Pervious areas: I A p e r=[ 4.67](mm), SLPP=[ 0.42](%), LGP=[ 40](m),
3145 MNP=[ 0.250], SCP=[ 0](mi n),
3145 Impervious areas: I A i m p=[ 0.785](mm), SLPI=[ 0.42](%),
3146 L G I=[ 455.339](m), M N I=[ 0.013], S C I=[ 0](mi n),
3146 Continuous simulation parameters:
3147 I a R E C p e r=[ 4](hrs), I a R E C i m p=[ 4](hrs), I n t e r E v e n t T i m e=[ 12](hrs),
3147 E N D=- 1
3148 *%-----|-----|
3149 COMPUTE DUALHYD NHYDin=[ "KB-01B"], CI NLET=[ 1.585](cms), NI NLET=[ 1],
3150 M a j N H Y D=[ "KB-01B-M"]
3151 M n N H Y D=[ "KB-01B-MN"]
3152 T M S T O=[ 6075](cu-m)
3153 *%-----|-----|
3154 ADD HYD NHYDs um=[ "KB-01B-S"], NHYDs t o a d d=[ "KB-01B-M"+"KB-01B-MN"]
3155 *%-----|-----|
3156 CONTINUOUS STANDHYD NHYD=[ "KB-01C"], DT=[ 1]mi n, AREA=[ 13.78](ha), XI MP=[ 0.2045],
3157 T I M P=[ 0.409], DWF=[ 0](cms), LOSS=[ 1]:
3157 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3158 F=[ 0.00](mm),
3158 Pervious areas: I A p e r=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3159 MNP=[ 0.250], SCP=[ 0](mi n),
3159 Impervious areas: I A i m p=[ 0.785](mm), SLPI=[ 0.5](%),
3160 L G I=[ 303.095](m), M N I=[ 0.013], S C I=[ 0](mi n),
3160 Continuous simulation parameters:
3161 I a R E C p e r=[ 4](hrs), I a R E C i m p=[ 4](hrs), I n t e r E v e n t T i m e=[ 12](hrs),
3161 E N D=- 1

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3162 *%-----|-----|
3163 COMPUTE DUALHYD NHYDin=["KB-01C"], CILET=[1.35](cms), NILET=[1],
3164 Maj NHYD=["KB-01C-M"]
3165 MnNHYD=["KB-01C-MN"]
3166 TMSTO=[1880](cu-m)
3167 *%-----|-----|
3168 ADD HYD NHYDsum=["KB-01C-S"], NHYDsto add=["KB-01C-M"+"KB-01C-MN"]
3169 *%-----|-----|
3170 CONTINUOUS STANDHYD NHYD=["KB-03"], DT=[1]min, AREA=[84.78](ha), XI MP=[0.197],
TI MP=[0.394], DWF=[0](cms), LOSS=[1]:
3171 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3172 Pervious areas: I A per=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3173 Impervious areas: I A imp=[0.785](mm), SLPI=[0.63](%),
LGI=[751.798](m), MNI=[0.013], SCI=[0](min),
3174 Continuous simulation parameters:
3175 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=- 1
3176 *%-----|-----|
3177 COMPUTE DUALHYD NHYDin=["KB-03"], CILET=[5.27](cms), NILET=[1],
3178 Maj NHYD=["KB-03-M"]
3179 MnNHYD=["KB-03-MN"]
3180 TMSTO=[15500](cu-m)
3181 *%-----|-----|
3182 ADD HYD NHYDsum=["KB-03-S"], NHYDsto add=["KB-03-M"+"KB-03-MN"]
3183 *%-----|-----|
3184 CONTINUOUS STANDHYD NHYD=["KB-04"], DT=[1]min, AREA=[6.95](ha), XI MP=[0.85],
TI MP=[0.85], DWF=[0](cms), LOSS=[1]:
3185 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3186 Pervious areas: I A per=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3187 Impervious areas: I A imp=[0.942](mm), SLPI=[0.5](%),
LGI=[215.252](m), MNI=[0.013], SCI=[0](min),
3188 Continuous simulation parameters:
3189 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=- 1
3190 *%-----|-----|
3191 COMPUTE DUALHYD NHYDin=["KB-04"], CILET=[0.503](cms), NILET=[1],
3192 Maj NHYD=["KB-04-M"]
3193 MnNHYD=["KB-04-MN"]
3194 TMSTO=[1972](cu-m)
3195 *%-----|-----|
3196 ADD HYD NHYDsum=["KB-04-S"], NHYDsto add=["KB-04-M"+"KB-04-MN"]
3197 *%-----|-----|
3198 CONTINUOUS STANDHYD NHYD=["KB-05"], DT=[1]min, AREA=[5.19](ha), XI MP=[0.93],
TI MP=[0.93], DWF=[0](cms), LOSS=[1]:
3199 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3200 Pervious areas: I A per=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3201 Impervious areas: I A imp=[1.57](mm), SLPI=[0.5](%),
LGI=[186.011](m), MNI=[0.013], SCI=[0](min),
3202 Continuous simulation parameters:
3203 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=- 1
3204 *%-----|-----|
3205 *%-----|-----|
3206 CONTINUOUS STANDHYD NHYD=["KB-06"], DT=[1]min, AREA=[12.93](ha), XI MP=[0.873],
TI MP=[0.873], DWF=[0](cms), LOSS=[1]:
3207 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3208 Pervious areas: I A per=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3209 Impervious areas: I A imp=[0.942](mm), SLPI=[4.75](%),

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3210           LGI=[ 293.598](m), MNI=[ 0.013], SCI=[ 0](min),
3211           Continuous simulation parameters:
3212           IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
           END=- 1
3212 *%-----|-----|
3213 COMPUTE DUALHYD NHYDin=["KB-06"], CINLET=[ 2.262](cms), NINLET=[ 1],
3214           MajNHYD=["KB-06-M"]
3215           MnNHYD=["KB-06-MN"]
3216           TMSTO=[ 1950](cu-m)
3217 *%-----|-----|
3218 ADD HYD NHYDsum=["KB-06-S"], NHYDsto add=["KB-06-M"+"KB-06-MN"]
3219 *%-----|-----|
3220 CONTINUOUS STANDHYD NHYD=["KB-11"], DT=[ 1]min, AREA=[ 4.03](ha), XI MP=[ 0.675],
           TIMP=[ 0.675], DWF=[ 0](cms), LOSS=[ 1]:
3221           Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
           F=[ 0.00](mm),
3222           Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
           MNP=[ 0.250], SCP=[ 0](min),
3223           Impervious areas: IAimp=[ 0.785](mm), SLPI=[ 2.0](%),
           LGI=[ 163.911](m), MNI=[ 0.013], SCI=[ 0](min),
3224           Continuous simulation parameters:
3225           IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
           END=- 1
3226 *%-----|-----|
3227 COMPUTE DUALHYD NHYDin=["KB-11"], CINLET=[ 0.5773](cms), NINLET=[ 1],
3228           MajNHYD=["KB-11-M"]
3229           MnNHYD=["KB-11-MN"]
3230           TMSTO=[ 597](cu-m)
3231 *%-----|-----|
3232 ADD HYD NHYDsum=["KB-11-S"], NHYDsto add=["KB-11-M"+"KB-11-MN"]
3233 *%-----|-----|
3234 CONTINUOUS STANDHYD NHYD=["S1"], DT=[ 1]min, AREA=[ 4.99](ha), XI MP=[ 0.93], TIMP=[ 0.93],
           DWF=[ 0](cms), LOSS=[ 1]:
3235           Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
           F=[ 0.00](mm),
3236           Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
           MNP=[ 0.250], SCP=[ 0](min),
3237           Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 2.0](%),
           LGI=[ 182.392](m), MNI=[ 0.013], SCI=[ 0](min),
3238           Continuous simulation parameters:
3239           IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
           END=- 1
3240 *%-----|-----|
3241 CONTINUOUS STANDHYD NHYD=["KB-15"], DT=[ 1]min, AREA=[ 2.15](ha), XI MP=[ 0.79],
           TIMP=[ 0.79], DWF=[ 0](cms), LOSS=[ 1]:
3242           Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
           F=[ 0.00](mm),
3243           Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
           MNP=[ 0.250], SCP=[ 0](min),
3244           Impervious areas: IAimp=[ 0.157](mm), SLPI=[ 0.3](%),
           LGI=[ 119.722](m), MNI=[ 0.013], SCI=[ 0](min),
3245           Continuous simulation parameters:
3246           IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
           END=- 1
3247 *%-----|-----|
3248 *%-----|-----|
3249 ADD HYD NHYDsum=["KB-P1"], NHYDsto
           add=["KB-01A-S"+"KB-01B-S"+"KB-01C-S"+"KB-03-S"+"KB-04-S"+"KB-05"+"KB-06-S"+"KB-11-S"+"KB
           -15"+"S1"]
3250 *%-----|-----|
3251 ROUTE RESERVOIR NHYDout=["KB-P1R"], NHYDin=["KB-P1"],
3252           RDT=[ 1](min),
3253           TABLE of ( OUTFLOW STORAGE ) values
3254           (cms) - (ha-m)
3255           [ 0.0, 0.0 ]
3256           [ 0.076, 0.003 ]

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3257 [ 0.088, 0.006]
3258 [ 0.136, 0.011]
3259 [ 0.301, 0.017]
3260 [ 0.454, 0.027]
3261 [ 0.631, 0.041]
3262 [ 1.173, 0.068]
3263 [ 1.91, 0.111]
3264 [ 4.847, 0.231]
3265 [ 9.813, 0.436]
3266 [ 12.134, 0.617]
3267 [ 12.438, 0.732]
3268 [ 12.424, 0.811]
3269 [ 12.425, 0.894]
3270 [ -1 , -1 ] (max twenty pts)
3271 NHYDovf=[ "KB- P1ovf" ]
3272 *%-----|-----|
3273 ADD HYD NHYDsum=[ "KB- Pond1" ], NHYDs to add=[ "KB- P1R"+"KB- P1ovf" ]
3274 *%-----|-----|
3275 SAVE HYD NHYD=[ "KB- Pond1" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
3276 HYD_COMMENT=[ "Total Flows at KB first pond" ]
3277 *%-----|-----|
3278 CONTINUOUS STANDHYD NHYD=[ "KB- 07" ], DT=[ 1 ] min, AREA=[ 10.86 ] (ha), XI MP=[ 0.86 ],
TI MP=[ 0.86 ], DWF=[ 0 ] (cms), LOSS=[ 1 ]:
3279 Horton: Fo=[ 76.20 ] (mm/ hr), Fc=[ 13.20 ] (mm/ hr), DCAY=[ 4.14 ] (/ hr),
F=[ 0.00 ] (mm),
3280 Pervious areas: I A per=[ 4.67 ] (mm), SLPP=[ 2.0 ] (%), LGP=[ 40 ] (m),
MNP=[ 0.250 ], SCP=[ 0 ] (min),
3281 Impervious areas: I A i mp=[ 0.785 ] (mm), SLPI=[ 2.0 ] (%),
LGI=[ 269.072 ] (m), MNI=[ 0.013 ], SCI=[ 0 ] (min),
3282 Continuous simulation parameters:
3283 I a REC per=[ 4 ] (hrs), I a REC i mp=[ 4 ] (hrs), I n t e r E v e n t T i m e=[ 12 ] (hrs),
END=- 1
3284 *%-----|-----|
3285 COMPUTE DUALHYD NHYD i n=[ "KB- 07" ], CI NLET=[ 2.094 ] (cms), NI NLET=[ 1 ],
3286 M a j NHYD=[ "KB- 07- M" ]
3287 M i n NHYD=[ "KB- 07- MN" ]
3288 T M S T O=[ 1378 ] (cu- m)
3289 *%-----|-----|
3290 ADD HYD NHYDsum=[ "KB- 07- S" ], NHYDs to add=[ "KB- 07- M"+"KB- 07- MN" ]
3291 *%-----|-----|
3292 CONTINUOUS STANDHYD NHYD=[ "KB- 08" ], DT=[ 1 ] min, AREA=[ 6.61 ] (ha), XI MP=[ 0.64 ],
TI MP=[ 0.64 ], DWF=[ 0 ] (cms), LOSS=[ 1 ]:
3293 Horton: Fo=[ 76.20 ] (mm/ hr), Fc=[ 13.20 ] (mm/ hr), DCAY=[ 4.14 ] (/ hr),
F=[ 0.00 ] (mm),
3294 Pervious areas: I A per=[ 4.67 ] (mm), SLPP=[ 2.0 ] (%), LGP=[ 40 ] (m),
MNP=[ 0.250 ], SCP=[ 0 ] (min),
3295 Impervious areas: I A i mp=[ 0.785 ] (mm), SLPI=[ 2.0 ] (%),
LGI=[ 209.921 ] (m), MNI=[ 0.013 ], SCI=[ 0 ] (min),
3296 Continuous simulation parameters:
3297 I a REC per=[ 4 ] (hrs), I a REC i mp=[ 4 ] (hrs), I n t e r E v e n t T i m e=[ 12 ] (hrs),
END=- 1
3298 *%-----|-----|
3299 COMPUTE DUALHYD NHYD i n=[ "KB- 08" ], CI NLET=[ 1.058 ] (cms), NI NLET=[ 1 ],
3300 M a j NHYD=[ "KB- 08- M" ]
3301 M i n NHYD=[ "KB- 08- MN" ]
3302 T M S T O=[ 787 ] (cu- m)
3303 *%-----|-----|
3304 ADD HYD NHYDsum=[ "KB- 08- S" ], NHYDs to add=[ "KB- 08- M"+"KB- 08- MN" ]
3305 *%-----|-----|
3306 CONTINUOUS STANDHYD NHYD=[ "KB- 09" ], DT=[ 1 ] min, AREA=[ 2.6 ] (ha), XI MP=[ 0.86 ],
TI MP=[ 0.86 ], DWF=[ 0 ] (cms), LOSS=[ 1 ]:
3307 Horton: Fo=[ 76.20 ] (mm/ hr), Fc=[ 13.20 ] (mm/ hr), DCAY=[ 4.14 ] (/ hr),
F=[ 0.00 ] (mm),
3308 Pervious areas: I A per=[ 4.67 ] (mm), SLPP=[ 2.0 ] (%), LGP=[ 40 ] (m),
MNP=[ 0.250 ], SCP=[ 0 ] (min),
3309 Impervious areas: I A i mp=[ 1.57 ] (mm), SLPI=[ 2.0 ] (%),

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3310          LGI=[ 131.656](m), MNI=[ 0.013], SCI=[ 0](min),
3311          Continuous simulation parameters:
3312          IaRECPer=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3313          END=- 1
3314          *%-----|-----|
3315          CONTINUOUS STANDHYD NHYD=["KB- 10_1"], DT=[ 1]min, AREA=[ 2.37](ha), XI MP=[ 0.86],
3316          T I MP=[ 0.86], DWF=[ 0](cms), LOSS=[ 1]:
3317          Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3318          F=[ 0.00](mm),
3319          Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3320          MNP=[ 0.250], SCP=[ 0](min),
3321          Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 2.0](%),
3322          LGI=[ 125.698](m), MNI=[ 0.013], SCI=[ 0](min),
3323          Continuous simulation parameters:
3324          IaRECPer=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3325          END=- 1
3326          *%-----|-----|
3327          CONTINUOUS STANDHYD NHYD=["KB- 10_2"], DT=[ 1]min, AREA=[ 1.14](ha), XI MP=[ 0.86],
3328          T I MP=[ 0.86], DWF=[ 0](cms), LOSS=[ 1]:
3329          Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3330          F=[ 0.00](mm),
3331          Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3332          MNP=[ 0.250], SCP=[ 0](min),
3333          Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 2.0](%), LGI=[ 87.178](m),
3334          MNI=[ 0.013], SCI=[ 0](min),
3335          Continuous simulation parameters:
3336          IaRECPer=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3337          END=- 1
3338          *%-----|-----|
3339          CONTINUOUS STANDHYD NHYD=["KB- 12"], DT=[ 1]min, AREA=[ 4.86](ha), XI MP=[ 0.79],
3340          T I MP=[ 0.79], DWF=[ 0](cms), LOSS=[ 1]:
3341          Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3342          F=[ 0.00](mm),
3343          Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3344          MNP=[ 0.250], SCP=[ 0](min),
3345          Impervious areas: IAimp=[ 1.099](mm), SLPI=[ 2.0](%),
3346          LGI=[ 180.000](m), MNI=[ 0.013], SCI=[ 0](min),
3347          Continuous simulation parameters:
3348          IaRECPer=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3349          END=- 1
3350          *%-----|-----|
3351          COMPUTE DUALHYD NHYDin=["KB- 12"], C I NLET=[ 0.8665](cms), N I NLET=[ 1],
3352          M a j NHYD=["KB- 12- M"]
3353          M n NHYD=["KB- 12- MN"]
3354          T M S T O=[ 632](cu-m)
3355          *%-----|-----|
3356          ADD HYD NHYDs um=["KB- 12- S"], NHYDs t o a d d=["KB- 12- M"+"KB- 12- MN"]
3357          *%-----|-----|
3358          CONTINUOUS STANDHYD NHYD=["KB- 13"], DT=[ 1]min, AREA=[ 10.19](ha), XI MP=[ 0.64],
3359          T I MP=[ 0.64], DWF=[ 0](cms), LOSS=[ 1]:
3360          Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3361          F=[ 0.00](mm),
3362          Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3363          MNP=[ 0.250], SCP=[ 0](min),
3364          Impervious areas: IAimp=[ 0.785](mm), SLPI=[ 2.0](%),
3365          LGI=[ 260.640](m), MNI=[ 0.013], SCI=[ 0](min),
3366          Continuous simulation parameters:
3367          IaRECPer=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3368          END=- 1
3369          *%-----|-----|
3370          COMPUTE DUALHYD NHYDin=["KB- 13"], C I NLET=[ 1.722](cms), N I NLET=[ 1],
3371          M a j NHYD=["KB- 13- M"]
3372          M n NHYD=["KB- 13- MN"]
3373          T M S T O=[ 1077](cu-m)

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3354 *%-----|-----|
3355 ADD HYD          NHYDs um=[ "KB- 13- S" ], NHYDs to add=[ "KB- 13- M" +"KB- 13- MN" ]
3356 *%-----|-----|
3357 CONTINUOUS STANDHYD NHYD=[ "KB- 14" ], DT=[ 1] mi n, AREA=[ 5. 47] ( ha ), XI MP=[ 0. 64 ],
TI MP=[ 0. 64 ], DWF=[ 0] ( cms ), LOSS=[ 1 ] :
3358 Horton: Fo=[ 76. 20] ( mm/ hr ), Fc=[ 13. 20] ( mm/ hr ), DCAY=[ 4. 14] ( / hr ),
F=[ 0. 00] ( mm ),
3359 Pervious areas: IAper=[ 4. 67] ( mm ), SLPP=[ 2. 0] ( % ), LGP=[ 40] ( m ),
MNP=[ 0. 250 ], SCP=[ 0] ( mi n ),
3360 Impervious areas: IAi mp=[ 0. 785] ( mm ), SLPI =[ 2. 0] ( % ),
LGI =[ 190. 962] ( m ), MNI =[ 0. 013 ], SCI =[ 0] ( mi n ),
3361 Continuous simulation parameters:
3362 IaREcper=[ 4] ( hr s ), IaRECi mp=[ 4] ( hr s ), Int er Event Ti me=[ 12] ( hr s ),
END=- 1
3363 *%-----|-----|
3364 COMPUTE DUALHYD   NHYDi n=[ "KB- 14" ], CI NLET=[ 0. 8734] ( cms ), NI NLET=[ 1 ],
3365 M aj NHYD=[ "KB- 14- M" ]
3366 M nNHYD=[ "KB- 14- MN" ]
3367 TM STO=[ 631] ( cu- m )
3368 *%-----|-----|
3369 ADD HYD          NHYDs um=[ "KB- 14- S" ], NHYDs to add=[ "KB- 14- M" +"KB- 14- MN" ]
3370 *%-----|-----|
3371 *%-----|-----|
3372 CONTINUOUS STANDHYD NHYD=[ "KB- 16_2" ], DT=[ 1] mi n, AREA=[ 3. 42] ( ha ), XI MP=[ 0. 71 ],
TI MP=[ 0. 71 ], DWF=[ 0] ( cms ), LOSS=[ 1 ] :
3373 Horton: Fo=[ 76. 20] ( mm/ hr ), Fc=[ 13. 20] ( mm/ hr ), DCAY=[ 4. 14] ( / hr ),
F=[ 0. 00] ( mm ),
3374 Pervious areas: IAper=[ 4. 67] ( mm ), SLPP=[ 2. 0] ( % ), LGP=[ 40] ( m ),
MNP=[ 0. 250 ], SCP=[ 0] ( mi n ),
3375 Impervious areas: IAi mp=[ 0. 157] ( mm ), SLPI =[ 0. 3] ( % ),
LGI =[ 150. 997] ( m ), MNI =[ 0. 013 ], SCI =[ 0] ( mi n ),
3376 Continuous simulation parameters:
3377 IaREcper=[ 4] ( hr s ), IaRECi mp=[ 4] ( hr s ), Int er Event Ti me=[ 12] ( hr s ),
END=- 1
3378 *%-----|-----|
3379 ADD HYD          NHYDs um=[ "KB- P2" ], NHYDs to
add=[ "KB- Pond1" +"KB- 07- S" +"KB- 08- S" +"KB- 09" +"KB- 10_1" +"KB- 10_2" +"KB- 12- S" +"KB- 13- S" +"KB- 1
4- S" +"KB- 16_2" ]
3380 *%-----|-----|
3381 ROUTE RESERVOIR  NHYDout =[ "KB- P2R" ], NHYDi n=[ "KB- P2" ],
3382 RDT=[ 1] ( mi n ),
3383 TABLE of ( OUTFLOW STORAGE ) values
3384 ( cms ) - ( ha- m )
3385 [ 0. 0 , 0. 0 ]
3386 [ 0. 053, 0. 005 ]
3387 [ 0. 132, 0. 009 ]
3388 [ 0. 269, 0. 014 ]
3389 [ 0. 455, 0. 023 ]
3390 [ 0. 699, 0. 037 ]
3391 [ 0. 947, 0. 056 ]
3392 [ 1. 853, 0. 09 ]
3393 [ 2. 712, 0. 146 ]
3394 [ 6. 626, 0. 287 ]
3395 [ 11. 228, 0. 515 ]
3396 [ 14. 885, 0. 738 ]
3397 [ 16. 473, 0. 893 ]
3398 [ 17. 311, 0. 998 ]
3399 [ 17. 633, 1. 063 ]
3400 [ 17. 634, 1. 112 ]
3401 [ - 1 , - 1 ] ( max twenty pts )
3402 NHYDovf=[ "KB- P2ovf" ]
3403 *%-----|-----|
3404 ADD HYD          NHYDs um=[ "KB- Pond2" ], NHYDs to add=[ "KB- P2R" +"KB- P2ovf" ]
3405 *%-----|-----|
3406 SAVE HYD        NHYD=[ "KB- Pond2" ], # OF PCYCLES=[ - 1 ], I CASEsh=[ 1 ]
3407 HYD_COMMENT=[ "Total Flows at KB second pond" ]

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3408 *%-----|-----|
3409 CONTINUOUS STANDHYD NHYD=["KB-16_1"], DT=[1]min, AREA=[2.8](ha), XI MP=[0.75],
TI MP=[0.75], DWF=[0](cms), LOSS=[1]:
3410 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3411 Pervious areas: I A per=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3412 Impervious areas: I A i mp=[0.157](mm), SLPI=[0.3](%),
LGI=[136.626](m), MNI=[0.013], SCI=[0](min),
3413 Continuous simulation parameters:
3414 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=-1
3415 *%-----|-----|
3416 ADD HYD NHYDsum=["KB-P3"], NHYDs to add=["KB-Pond2"+"KB-16_1"]
3417 *%-----|-----|
3418 *%-----|-----|
3419 * One inflow node from pond 3 is added to the model (ROUTE RESERVOIR)
3420 * Another inflow node from right side of pond 3 is not added to the model
3421 ROUTE RESERVOIR NHYDout=["KB-P3R"], NHYDin=["KB-P3"],
3422 RDT=[1](min),
3423 TABLE of ( OUTFLOW STORAGE ) values
3424 (cms) - (ha-m)
3425 [ 0.0 , 0.0 ]
3426 [0.051, 0.002]
3427 [0.048, 0.003]
3428 [0.057, 0.029]
3429 [0.089, 0.045]
3430 [0.133, 0.069]
3431 [0.199, 0.106]
3432 [0.321, 0.172]
3433 [1.029, 0.306]
3434 [4.036, 0.527]
3435 [8.332, 0.761]
3436 [11.727, 0.941]
3437 [14.125, 1.067]
3438 [15.675, 1.149]
3439 [16.555, 1.196]
3440 [16.911, 1.214]
3441 [ -1 , -1 ] (max twenty pts)
3442 NHYDovf=["KB-P3ovf"]
3443 *%-----|-----|
3444 ADD HYD NHYDsum=["KB-Pond3"], NHYDs to add=["KB-P3R"+"KB-P3ovf"]
3445 *%-----|-----|
3446 SAVE HYD NHYD=["KB-Pond3"], # OF PCYCLES=[-1], I CASEs h=[1]
3447 HYD_COMMENT=["Total Flows at KB third pond"]
3448 *%-----|-----|
3449 *#*****
3450 *# EXISTING / PROPOSED Subcatchments (Kennedy-Burnett SWM Facility (118080), SWM
Modeling Approach, NOVATECH Report June, 2020)
3451 *# - TO FRASER-CLARKE DRAIN
3452 *#*****
3453 CONTINUOUS STANDHYD NHYD=["FC-01"], DT=[1]min, AREA=[8.03](ha), XI MP=[0.47],
TI MP=[0.47], DWF=[0](cms), LOSS=[1]:
3454 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3455 Pervious areas: I A per=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3456 Impervious areas: I A i mp=[1.57](mm), SLPI=[1.0](%),
LGI=[231.373](m), MNI=[0.013], SCI=[0](min),
3457 Continuous simulation parameters:
3458 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=-1
3459 *%-----|-----|
3460 COMPUTE DUALHYD NHYDin=["FC-01"], CI NLET=[0.756](cms), NI NLET=[1],
3461 M i j NHYD=["FC-01-M"]
3462 M n NHYD=["FC-01-MN"]

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3463          TMI STO=[ 714] ( cu- m)
3464 *%-----|-----|
3465 ADD HYD      NHYDs um=[ " FC- 01- S" ], NHYDs  to  add=[ " FC- 01- M" +" FC- 01- MN" ]
3466 *%-----|-----|
3467 CONTI NUOUS STANDHYD NHYD=[ " FC- 02" ], DT=[ 1] mi n, AREA=[ 16. 05] ( ha), XI MP=[ 0. 93],
TI MP=[ 0. 93], DWF=[ 0] ( cms), LOSS=[ 1]:
3468          Hort on: Fo=[ 76. 20] ( mm/ hr), Fc=[ 13. 20] ( mm/ hr), DCAY=[ 4. 14] ( / hr),
F=[ 0. 00] ( mm),
3469          Perv ious  areas: IAper=[ 4. 67] ( mm), SLPP=[ 2. 0] ( %), LGP=[ 40] ( m),
MNP=[ 0. 250], SCP=[ 0] ( mi n),
3470          Imperv ious  areas: IAi mp=[ 1. 57] ( mm), SLPI=[ 1. 0] ( %),
LGI=[ 327. 109] ( m), MNI=[ 0. 013], SCI=[ 0] ( mi n),
3471          Continuous simulation parameters:
3472          IaRECper=[ 4] ( hr s), IaRECI mp=[ 4] ( hr s), Int er Event Ti me=[ 12] ( hr s),
END=- 1
3473 *%-----|-----|
3474 COMPUTE DUALHYD  NHYDi n=[ " FC- 02" ], CI NLET=[ 1. 159] ( cms), NI NLET=[ 1],
3475          Mj NHYD=[ " FC- 02- M" ]
3476          MnNHYD=[ " FC- 02- MN" ]
3477          TMI STO=[ 2385] ( cu- m)
3478 *%-----|-----|
3479 ADD HYD      NHYDs um=[ " FC- 02- S" ], NHYDs  to  add=[ " FC- 02- M" +" FC- 02- MN" ]
3480 *%-----|-----|
3481 CONTI NUOUS STANDHYD NHYD=[ " FC- 03" ], DT=[ 1] mi n, AREA=[ 7. 37] ( ha), XI MP=[ 0. 64],
TI MP=[ 0. 64], DWF=[ 0] ( cms), LOSS=[ 1]:
3482          Hort on: Fo=[ 76. 20] ( mm/ hr), Fc=[ 13. 20] ( mm/ hr), DCAY=[ 4. 14] ( / hr),
F=[ 0. 00] ( mm),
3483          Perv ious  areas: IAper=[ 4. 67] ( mm), SLPP=[ 2. 0] ( %), LGP=[ 40] ( m),
MNP=[ 0. 250], SCP=[ 0] ( mi n),
3484          Imperv ious  areas: IAi mp=[ 1. 57] ( mm), SLPI=[ 1. 0] ( %),
LGI=[ 221. 660] ( m), MNI=[ 0. 013], SCI=[ 0] ( mi n),
3485          Continuous simulation parameters:
3486          IaRECper=[ 4] ( hr s), IaRECI mp=[ 4] ( hr s), Int er Event Ti me=[ 12] ( hr s),
END=- 1
3487 *%-----|-----|
3488 COMPUTE DUALHYD  NHYDi n=[ " FC- 03" ], CI NLET=[ 0. 358] ( cms), NI NLET=[ 1],
3489          Mj NHYD=[ " FC- 03- M" ]
3490          MnNHYD=[ " FC- 03- MN" ]
3491          TMI STO=[ 1131] ( cu- m)
3492 *%-----|-----|
3493 ADD HYD      NHYDs um=[ " FC- 03- S" ], NHYDs  to  add=[ " FC- 03- M" +" FC- 03- MN" ]
3494 *%-----|-----|
3495 CONTI NUOUS STANDHYD NHYD=[ " FC- 04" ], DT=[ 1] mi n, AREA=[ 12. 87] ( ha), XI MP=[ 0. 64],
TI MP=[ 0. 64], DWF=[ 0] ( cms), LOSS=[ 1]:
3496          Hort on: Fo=[ 76. 20] ( mm/ hr), Fc=[ 13. 20] ( mm/ hr), DCAY=[ 4. 14] ( / hr),
F=[ 0. 00] ( mm),
3497          Perv ious  areas: IAper=[ 4. 67] ( mm), SLPP=[ 2. 0] ( %), LGP=[ 40] ( m),
MNP=[ 0. 250], SCP=[ 0] ( mi n),
3498          Imperv ious  areas: IAi mp=[ 1. 57] ( mm), SLPI=[ 1. 0] ( %),
LGI=[ 292. 916] ( m), MNI=[ 0. 013], SCI=[ 0] ( mi n),
3499          Continuous simulation parameters:
3500          IaRECper=[ 4] ( hr s), IaRECI mp=[ 4] ( hr s), Int er Event Ti me=[ 12] ( hr s),
END=- 1
3501 *%-----|-----|
3502 COMPUTE DUALHYD  NHYDi n=[ " FC- 04" ], CI NLET=[ 0. 741] ( cms), NI NLET=[ 1],
3503          Mj NHYD=[ " FC- 04- M" ]
3504          MnNHYD=[ " FC- 04- MN" ]
3505          TMI STO=[ 1794] ( cu- m)
3506 *%-----|-----|
3507 ADD HYD      NHYDs um=[ " FC- 04- S" ], NHYDs  to  add=[ " FC- 04- M" +" FC- 04- MN" ]
3508 *%-----|-----|
3509 *#*****
3510 *#      PROPOSED Subcatchments ( Kennedy- Burnett SWM Facility ( 118080), SWM Mdeling
Approach, NOVATECH Report June, 2020)
3511 *#      - TO JOCK RI VER
3512 *#*****

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3513 CONTINUOUS STANDHYD NHYD=["JR-01"], DT=[1] min, AREA=[8.24](ha), XI MP=[0.64],
TI MP=[0.64], DWF=[0](cms), LOSS=[1]:
3514 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3515 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3516 Impervious areas: IAimp=[1.57](mm), SLPI=[1.0](%),
LGI=[234.379](m), MNI=[0.013], SCI=[0](min),
3517 Continuous simulation parameters:
3518 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3519 *%-----|
3520 COMPUTE DUALHYD NHYDin=["JR-01"], CINLET=[0.563](cms), NINLET=[1],
3521 MajNHYD=["JR-01-M"]
3522 MinNHYD=["JR-01-MN"]
3523 TMSSTO=[1040](cu-m)
3524 *%-----|
3525 ADD HYD NHYDsum=["JR-01-S"], NHYDsto add=["JR-01-M"+"JR-01-MN"]
3526 *%-----|
3527 CONTINUOUS STANDHYD NHYD=["JR-02"], DT=[1] min, AREA=[1.59](ha), XI MP=[0.64],
TI MP=[0.64], DWF=[0](cms), LOSS=[1]:
3528 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3529 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3530 Impervious areas: IAimp=[1.57](mm), SLPI=[1.0](%),
LGI=[102.956](m), MNI=[0.013], SCI=[0](min),
3531 Continuous simulation parameters:
3532 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
END=-1
3533 *%-----|
3534 COMPUTE DUALHYD NHYDin=["JR-02"], CINLET=[0.153](cms), NINLET=[1],
3535 MajNHYD=["JR-02-M"]
3536 MinNHYD=["JR-02-MN"]
3537 TMSSTO=[153](cu-m)
3538 *%-----|
3539 ADD HYD NHYDsum=["JR-02-S"], NHYDsto add=["JR-02-M"+"JR-02-MN"]
3540 *%-----|
3541 *#*****
3542 *# Catchment FRASER
3543 *# - To Fraser-Clarke drain (north of the Jock)
3544 *# - Developed land with assumed 43% imp.
3545 *# - 2020-12-17 Change Fraser area to be 35.1 as measured from QGIS
3546 *# - 2020-12-17 All Fraser is undeveloped (Nashyd)
3547 *#*****
3548 CONTINUOUS NASHYD NHYD=["FRASER-DRN"], DT=[1] min, AREA=[13.65](ha),
3549 DWF=[0](cms), CNVC=[77], IA=[4.67](mm),
3550 N=[3], TP=[0.4258]hrs,
3551 Continuous simulation parameters:
3552 IaRECper=[4](hrs),
3553 SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3554 InterEventTime=[12](hrs)
3555 Baseflow simulation parameters:
3556 BaseFlowOption=[1],
3557 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
3558 VHydCond=[0.055](mm/hr), END=-1
3559 *%-----|
3560 *CONTINUOUS STANDHYD NHYD=["FRASER-D"], DT=[1] min, AREA=[21.61](ha),
3561 * XI MP=[0.585], TI MP=[0.585], DWF=[0](cms), LOSS=[2],
3562 * SCS curve number CN=[80],
3563 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3564 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3565 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3566 * LGI=[379.561](m), MNI=[0.013], SCI=[0](min),
3567 * Continuous simulation parameters:
3568 * IaRECper=[4](hrs), IaRECImp=[4](hrs),

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3569 * SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3570 * InterEventTime=[18](hrs), END=-1
3571 */-----|-----|
3572 CONTINUOUS NASHYD NHYD=["FRASER-D"], DT=[1]min, AREA=[21.61](ha),
3573 DWF=[0](cms), CNVC=[77], IA=[4.67](mm),
3574 N=[3], TP=[0.674]hrs,
3575 Continuous simulation parameters:
3576 IaRECper=[4](hrs),
3577 SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3578 InterEventTime=[12](hrs)
3579 Baseflow simulation parameters:
3580 BaseFlowOption=[1],
3581 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
3582 VHydCond=[0.055](mm/hr), END=-1
3583 */-----|-----|
3584 * COMPUTE DUALHYD NHYDin=["FRASER-D"], CINLET=[3.545](cms), NINLET=[1],
3585 * MjNHYD=["FRASER-J"]
3586 * MnNHYD=["FRASER-N"]
3587 * TMSTO=[9999999](cu-m)
3588 */-----|-----|
3589 * ADD HYD NHYDs um=["FRASER-S"], NHYDs to add=["FRASER-J"+"FRASER-N"]
3590 */-----|-----|
3591 * ROUTE RESERVOIR NHYDout=["MS_P20"], NHYDin=["FRASER"],
3592 * RDT=[1](min),
3593 * TABLE of ( OUTFLOW STORAGE ) values
3594 * ( cms ) - ( ha-m )
3595 * [ 0.0 , 0.0 ]
3596 * [ 0.04 , 0.36 ]
3597 * [ -1 , -1 ] (max twenty pts)
3598 * NHYDovf=["P20-OVF"]
3599 */-----|-----|
3600 * ADD HYD NHYDs um=["4241"], NHYDs to
add=["KB-Pond3"+"S-1-B"+"FRASER-DRN"+"FRASER-D"+"N_KB"+"FC-01-S"+"FC-02-S"+"FC-03-S"]
3601 */-----|-----|
3602 * SAVE HYD NHYD=["4241"], # OF PCYCLES=[-1], ICASEsh=[1]
3603 HYD_COMMENT=["Total Flows at Ken-Burnett Outlet"]
3604 */-----|-----|
3605 *# Hydrograph from Node Ken-Burnett to station 3633
3606 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 4241
3607 *#
3608 * ROUTE CHANNEL NHYDout=["4241-out"], NHYDin=["4241"], RDT=[1](min),
3609 CHLGTH=[294](m), CHSLOPE=[0.1088](%), FPSLOPE=[0.1088](%),
3610 SECNUM=[1.0], NSEG=[3]
3611 ( SEGROUGH, SEGDI ST (m))=[0.05, -20.12
3612 -0.035, 45.26
3613 0.05, 403.84] NSEG times
3614 ( DISTANCE (m), ELEVATION (m))=[
3615 [-909.72, 95 ]
3616 [-907.09, 94.5 ]
3617 [-904.65, 94 ]
3618 [-902.26, 93.5 ]
3619 [-44.51, 91.5 ]
3620 [-25.1, 91.5 ]
3621 [-20.98, 91 ]
3622 [-20.61, 90.5 ]
3623 [-20.12, 90 ]
3624 [-6.13, 87.26 ]
3625 [17.51, 86.56 ]
3626 [31.37, 87.2 ]
3627 [45.26, 90 ]
3628 [50.41, 90.5 ]
3629 [63.06, 91 ]
3630 [134.5, 91.5 ]
3631 [190.63, 92 ]
3632 [251.98, 92.5 ]
3633 [321.32, 93.5 ]

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3634 [ 403.84, 95 ]
3635 *%-----|-----
3636 ADD HYD NHYDsum=["SN_KB"], NHYDs to
add=["4241-out"+"FC-04-S"+"JR-01-S"+"JR-02-S"]
3637 *%-----|-----
3638 SAVE HYD NHYD=["SN_KB"], # OF PCYCLES=[-1], ICASEsh=[1]
3639 HYD_COMMENT=["Total Flows before Station 3633"]
3640 *%-----|-----
3641 *# Hydrograph from Station 3633 to Node Todd
3642 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 3633
3643 *# JFSA 2021-02-26 change the channel length (at station 3633) from 650m to 608m and
change the slope from 0.0498% to 0.24671% That is because of adding station 4241
between station 4534 and station 3633
3644 *#
3645 ROUTE CHANNEL NHYDout=["N_TO"], NHYDin=["SN_KB"], RDT=[1](min),
3646 CHLGTH=[608](m), CHSLOPE=[0.24671](%), FPSLOPE=[0.24671](%),
3647 SECNUM=[1.0], NSEG=[3]
3648 (SEGROUGH, SEGDI ST (m))=[0.05, -23.74
3649 -0.035, 23.74
3650 0.05, 26.50] NSEG times
3651 (DISTANCE (m), ELEVATION (m))=[
3652 -29.24, 91.0
3653 -27.41, 90.5
3654 -25.64, 90
3655 -23.74, 89.5
3656 -22, 89.26
3657 -20, 88.51
3658 -19, 88.32
3659 -15, 88.1
3660 -10, 88.11
3661 -5, 88.17
3662 0, 88.27
3663 5, 88.19
3664 10, 88.06
3665 15, 88.48
3666 16, 88.7
3667 23.74, 89.5
3668 24.68, 90
3669 25.57, 90.5
3670 26.50, 91.0
3671 * [-29.24, 91]
3672 * [-27.41, 90.5]
3673 * [-25.64, 90]
3674 * [-23.74, 89.5]
3675 * [-22, 89.26]
3676 * [-20, 88.51]
3677 * [-19, 88.32]
3678 * [-15, 88.1]
3679 * [-10, 88.11]
3680 * [-5, 88.17]
3681 * [0, 88.27]
3682 * [5, 88.19]
3683 * [10, 88.06]
3684 * [15, 88.48]
3685 * [16, 88.7]
3686 * [23.74, 89.5]
3687 * [24.68, 90]
3688 * [25.57, 90.5]
3689 *%-----|-----
3690 *#*****
3691 *# Catchment Greenbank
3692 *# - To Greenbank Drain (south of the Jock)
3693 *# - JFSA 2021-01-18 add Greenbank pond as per JFSA, P598(06)-15, June 2016
3694 *# - JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GIS measurements
3695 *#*****
3696 CONTINUOUS STANDHYD NHYD=["Greenbank"], DT=[1]min, AREA=[36.6](ha),

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3697      XI MP=[ 0. 639], TI MP=[ 0. 682], DWF=[ 0](cms), LOSS=[ 2],
3698      SCS curve number CN=[ 77],
3699      Pervious surfaces: IAper=[ 4. 67](mm), SLPP=[ 1](%),
3700      LGP=[ 40](m), MNP=[ 0. 25], SCP=[ 0](min),
3701      Impervious surfaces: IAimp=[ 1. 57](mm), SLPI=[ 1](%),
3702      LGI=[ 493. 96](m), MNI=[ 0. 013], SCI=[ 0](min),
3703      Continuous simulation parameters:
3704      IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
3705      SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0. 010]/(mm),
3706      InterEventTime=[ 18](hrs), END=- 1
3707  *%-----|-----|
3708  ROUTE RESERVOIR  NHYDout=["GreenB_MN"], NHYDin=["Greenbank"],
3709      RDT=[ 1](min),
3710      TABLE of ( OUTFLOW STORAGE ) values
3711      (cms) - (ha-m)
3712      [ 0. 0 , 0. 0 ]
3713      [ 0. 033 , 0. 084 ]
3714      [ 0. 039 , 0. 201 ]
3715      [ 0. 113 , 0. 292 ]
3716      [ 0. 237 , 0. 386 ]
3717      [ 0. 382 , 0. 484 ]
3718      [ 0. 539 , 0. 585 ]
3719      [ 0. 7 , 0. 692 ]
3720      [ 0. 86 , 0. 804 ]
3721      [ 4. 684 , 0. 922 ]
3722      [ 11. 539 , 1. 052 ]
3723      [ 20. 867 , 1. 168 ]
3724      [ 103. 616 , 1. 974 ]
3725      [ -1 , -1 ] (max twenty pts)
3726      NHYDovf=["GreenB_M"],
3727  *%-----|-----|
3728  *%-----|-----|
3729  ADD HYD          NHYDs um=["GreenB"], NHYDs to add=["N_TO"+"GreenB_M"+"GreenB_MN"]
3730  *%-----|-----|
3731  SAVE HYD        NHYD=["GreenB"], # OF PCYCLES=[ -1], ICASEsh=[ 1]
3732      HYD_COMMENT=["Total Flows at Greenbank Drain"]
3733  *%-----|-----|
3734  *#*****|*****|
3735  *# Catchment TODD
3736  *# - To Todd Drain (south of the Jock)
3737  *# - Subdivision with 43% imp. as per Barrhaven South MSS
3738  *# - 2020-11-30 increase imp. based on P598(04)-11
3739  *# - 2020-11-30 update TODD Tributary Drainage Area to = 146.015 ha based on
3740  P598(04)-11
3741  *# - 2020-11-30 split TODD Drainage Area to MAJOR, MINOR, POND and ALL
3742  *#*****|*****|
3743  *# - JFSA 2021-01-19 add "TODD_MN1" as part of Clarke("W_CLAR_M") and remove it
3744  from Todd
3745  *CONTINUOUS STANDHYD NHYD=["TODD_MN1"], DT=[ 1]min, AREA=[ 1. 772](ha),
3746  *      XI MP=[ 0. 53], TI MP=[ 0. 57], DWF=[ 0](cms), LOSS=[ 2],
3747  *      SCS curve number CN=[ 77],
3748  *      Pervious surfaces: IAper=[ 4. 67](mm), SLPP=[ 1](%),
3749  *      LGP=[ 40](m), MNP=[ 0. 25], SCP=[ 0](min),
3750  *      Impervious surfaces: IAimp=[ 1. 57](mm), SLPI=[ 1](%),
3751  *      LGI=[ 108. 689](m), MNI=[ 0. 013], SCI=[ 0](min),
3752  *      Continuous simulation parameters:
3753  *      IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
3754  *      SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0. 010]/(mm),
3755  *      InterEventTime=[ 18](hrs), END=- 1
3756  *%-----|-----|
3757  CONTINUOUS STANDHYD NHYD=["TODD_MN2"], DT=[ 1]min, AREA=[ 2. 1](ha),
3758  XI MP=[ 0. 53], TI MP=[ 0. 57], DWF=[ 0](cms), LOSS=[ 2],
3759  SCS curve number CN=[ 77],
3760  Pervious surfaces: IAper=[ 4. 67](mm), SLPP=[ 1](%),
3761  LGP=[ 40](m), MNP=[ 0. 25], SCP=[ 0](min),
3762  Impervious surfaces: IAimp=[ 1. 57](mm), SLPI=[ 1](%),

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3761             LGI=[ 118.322](m), MNI=[ 0.013], SCI=[ 0](min),
3762 Continuous simulation parameters:
3763 IaRECPER=[ 4](hrs), IaRECImp=[ 4](hrs),
3764 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
3765 InterEventTime=[ 18](hrs), END=- 1
3766 *%-----|-----|
3767 CONTINUOUS STANDHYD NHYD=["TODD_MN3"], DT=[ 1]min, AREA=[ 0.117](ha),
3768 XI MP=[ 0.53], TI MP=[ 0.57], DWF=[ 0](cms), LOSS=[ 2],
3769 SCS curve number CN=[ 77],
3770 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
3771             LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
3772 Impervious surfaces: IAi mp=[ 1.57](mm), SLPI=[ 1](%),
3773             LGI=[ 27.928](m), MNI=[ 0.013], SCI=[ 0](min),
3774 Continuous simulation parameters:
3775 IaRECPER=[ 4](hrs), IaRECImp=[ 4](hrs),
3776 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
3777 InterEventTime=[ 18](hrs), END=- 1
3778 *%-----|-----|
3779 CONTINUOUS STANDHYD NHYD=["TODD_M"], DT=[ 1]min, AREA=[ 30.230](ha),
3780 XI MP=[ 0.52], TI MP=[ 0.64], DWF=[ 0](cms), LOSS=[ 2],
3781 SCS curve number CN=[ 77],
3782 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
3783             LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
3784 Impervious surfaces: IAi mp=[ 1.57](mm), SLPI=[ 1](%),
3785             LGI=[ 448.925](m), MNI=[ 0.013], SCI=[ 0](min),
3786 Continuous simulation parameters:
3787 IaRECPER=[ 4](hrs), IaRECImp=[ 4](hrs),
3788 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
3789 InterEventTime=[ 18](hrs), END=- 1
3790 *%-----|-----|
3791 * -JFSA, 2021-01-19 update "TODD_ALL" area from 108.741 ha to 112.908 ha based on
GIS measurements (148.41-30.23-0.117-2.1-3.055=112.908 ha)
3792 CONTINUOUS STANDHYD NHYD=["TODD_ALL"], DT=[ 1]min, AREA=[ 112.908](ha),
3793 XI MP=[ 0.52], TI MP=[ 0.57], DWF=[ 0](cms), LOSS=[ 2],
3794 SCS curve number CN=[ 77],
3795 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
3796             LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
3797 Impervious surfaces: IAi mp=[ 1.57](mm), SLPI=[ 1](%),
3798             LGI=[ 867.594](m), MNI=[ 0.013], SCI=[ 0](min),
3799 Continuous simulation parameters:
3800 IaRECPER=[ 4](hrs), IaRECImp=[ 4](hrs),
3801 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
3802 InterEventTime=[ 18](hrs), END=- 1
3803 *%-----|-----|
3804 CONTINUOUS STANDHYD NHYD=["TODD_P"], DT=[ 1]min, AREA=[ 3.055](ha),
3805 XI MP=[ 0.63], TI MP=[ 0.63], DWF=[ 0](cms), LOSS=[ 2],
3806 SCS curve number CN=[ 77],
3807 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
3808             LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
3809 Impervious surfaces: IAi mp=[ 1.57](mm), SLPI=[ 1](%),
3810             LGI=[ 142.712](m), MNI=[ 0.013], SCI=[ 0](min),
3811 Continuous simulation parameters:
3812 IaRECPER=[ 4](hrs), IaRECImp=[ 4](hrs),
3813 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
3814 InterEventTime=[ 18](hrs), END=- 1
3815 *%-----|-----|
3816 *%-----|-----|
3817 * -JFSA 2021-02-23 "TODD_DEVL" is part of the Corrigan sub-catchment because it
drains to Corrigan SWM as per geoOttawa.ca Feb. 2021. "TODD_DEVL" now is called "corr1"
and its parameters remain the same.
3818 *CONTINUOUS STANDHYD NHYD=["TODD_DEVL"], DT=[ 1]min, AREA=[ 15.87](ha),
3819 * XI MP=[ 0.63], TI MP=[ 0.63], DWF=[ 0](cms), LOSS=[ 2],
3820 * SCS curve number CN=[ 77],
3821 * Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
3822 *             LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
3823 * Impervious surfaces: IAi mp=[ 1.57](mm), SLPI=[ 1](%),

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3824 *                LGI=[ 325.27](m), MNI=[ 0.013], SCI=[ 0](min),
3825 *                Continuous simulation parameters:
3826 *                IaRECper=[ 4](hrs), IaRECimp=[ 4](hrs),
3827 *                SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
3828 *                InterEventTime=[ 18](hrs), END=- 1
3829 *%-----|-----|
3830 *                -JFSA 2021-02-23 "TODD_UnD" is part of the Corrigan sub-catchment. "TODD_UnD" now
3831 *                is called "corr2" and its parameters remain the same.
3832 *CONTINUOUS NASHYD  NHYD=[ "TODD_UnD" ], DT=[ 1]min, AREA=[ 12.47](ha),
3833 *                DWF=[ 0](cms), CNVC=[ 77], IA=[ 4.67](mm),
3834 *                N=[ 3], TP=[ 1.10]hrs,
3835 *                Continuous simulation parameters:
3836 *                IaRECper=[ 4](hrs),
3837 *                SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
3838 *                InterEventTime=[ 12](hrs)
3839 *                Baseflow simulation parameters:
3840 *                BaseFlowOption=[ 1],
3841 *                InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
3842 *                VHydCond=[ 0.055](mm/hr), END=- 1
3843 *%-----|-----|
3844 *# 5-Year + 12% Capture
3845 *COMPUTE DUALHYD  NHYDin=[ "TODD_Mj" ], CINLET=[ 3.314](cms), NINLET=[ 1],
3846 *                MjNHYD=[ "TODD_Mj" ]
3847 *                MnNHYD=[ "TODD_Mjn" ]
3848 *                TMSTO=[ 0.1](cu-m)
3849 ROUTE RESERVOIR  NHYDout=[ "TODD_Mjn" ], NHYDin=[ "TODD_Mj" ],
3850 *                RDT=[ 1](min),
3851 *                TABLE of ( OUTFLOW STORAGE ) values
3852 *                ( cms ) - ( ha-m )
3853 *                [ 0.0 , 0.0 ]
3854 *                [ 3.314 , 0.0001 ]
3855 *                [ -1 , -1 ] (max twenty pts)
3856 *                NHYDovf=[ "TODD_Mj" ],
3857 *%-----|-----|
3858 *# 5-Year + 12% Capture
3859 *COMPUTE DUALHYD  NHYDin=[ "TODD_MN1" ], CINLET=[ 0.227](cms), NINLET=[ 1],
3860 *                MjNHYD=[ "TODD_MN1j" ]
3861 *                MnNHYD=[ "TODD_MN1n" ]
3862 *                TMSTO=[ 0.1](cu-m)
3863 ROUTE RESERVOIR  NHYDout=[ "TODD_MN1n" ], NHYDin=[ "TODD_MN1" ],
3864 *                RDT=[ 1](min),
3865 *                TABLE of ( OUTFLOW STORAGE ) values
3866 *                ( cms ) - ( ha-m )
3867 *                [ 0.0 , 0.0 ]
3868 *                [ 0.227 , 0.0001 ]
3869 *                [ -1 , -1 ] (max twenty pts)
3870 *                NHYDovf=[ "TODD_MN1j" ],
3871 *%-----|-----|
3872 *COMPUTE DUALHYD  NHYDin=[ "TODD_MN2" ], CINLET=[ 0.268](cms), NINLET=[ 1],
3873 *                MjNHYD=[ "TODD_MN2j" ]
3874 *                MnNHYD=[ "TODD_MN2n" ]
3875 *                TMSTO=[ 0.1](cu-m)
3876 ROUTE RESERVOIR  NHYDout=[ "TODD_MN2n" ], NHYDin=[ "TODD_MN2" ],
3877 *                RDT=[ 1](min),
3878 *                TABLE of ( OUTFLOW STORAGE ) values
3879 *                ( cms ) - ( ha-m )
3880 *                [ 0.0 , 0.0 ]
3881 *                [ 0.268 , 0.0001 ]
3882 *                [ -1 , -1 ] (max twenty pts)
3883 *                NHYDovf=[ "TODD_MN2j" ],
3884 *%-----|-----|
3885 *COMPUTE DUALHYD  NHYDin=[ "TODD_MN3" ], CINLET=[ 0.016](cms), NINLET=[ 1],
3886 *                MjNHYD=[ "TODD_MN3j" ]
3887 *                MnNHYD=[ "TODD_MN3n" ]
3888 *                TMSTO=[ 0.1](cu-m)
3889 ROUTE RESERVOIR  NHYDout=[ "TODD_MN3n" ], NHYDin=[ "TODD_MN3" ],

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3889          RDT=[ 1 ] ( m i n ) ,
3890          TABLE of ( OUTFLOW STORAGE ) values
3891              ( c m s ) - ( h a - m )
3892              [ 0.0 , 0.0 ]
3893              [ 0.016 , 0.0001 ]
3894              [ -1 , -1 ] ( m a x t w e n t y p t s )
3895          NHYDovf=[ " TODD_MN3j " ] ,
3896 *%-----|-----|
3897 * -JFSA 2021-01-19 move A2 from Corrigan sub-catchment to Todd sub-catchment so the
major system from A2 can be added to Todd
3898 CONTINUOUS STANDHYD NHYD=[ " A2 " ] , DT=[ 1 ] m i n , AREA=[ 25.5 ] ( h a ) ,
3899 XI MP=[ 0.42 ] , TI MP=[ 0.52 ] , DWF=[ 0 ] ( c m s ) , LOSS=[ 2 ] ,
3900 SCS curve number CN=[ 75 ] ,
3901 Pervious surfaces: I A p e r=[ 4.67 ] ( m m ) , SLPP=[ 1 ] ( % ) ,
3902 L G P=[ 40 ] ( m ) , M N P=[ 0.25 ] , S C P=[ 0 ] ( m i n ) ,
3903 I m p e r v i o u s s u r f a c e s : I A i m p=[ 1.57 ] ( m m ) , S L P I=[ 1 ] ( % ) ,
3904 L G I=[ 566 ] ( m ) , M N I=[ 0.013 ] , S C I=[ 0 ] ( m i n ) ,
3905 C o n t i n u o u s s i m u l a t i o n p a r a m e t e r s :
3906 I a R E C p e r=[ 4 ] ( h r s ) , I a R E C i m p=[ 4 ] ( h r s ) ,
3907 S M N=[ -1 ] ( m m ) , S M A X=[ -1 ] ( m m ) , S K=[ 0.010 ] / ( m m ) ,
3908 I n t e r E v e n t T i m e=[ 18 ] ( h r s ) , E N D=-1
3909 *%-----|-----|
3910 COMPUTE DUALHYD NHYD i n=[ " A2 " ] , C I N L E T=[ 1.818 ] ( c m s ) , N I N L E T=[ 1 ] ,
3911 M a j N H Y D=[ " A2 - M " ]
3912 M i n N H Y D=[ " A2 - M N " ]
3913 T M S T O=[ 924 ] ( c u - m )
3914 *%-----|-----|
3915 ADD HYD NHYD s u m=[ " TODD " ] , NHYD s t o
add=[ " TODD_MN2n " + " TODD_MN3n " + " TODD_Mj " + " TODD_P " + " TODD_ALL " + " W_CLAR_Mn " ]
3916 *%-----|-----|
3917 SAVE HYD NHYD=[ " TODD " ] , # O F P C Y C L E S=[ -1 ] , I C A S E s h=[ 1 ]
3918 HYD_COMMENT=[ " T o t a l F l o w s a t T o d d D r a i n " ]
3919 *%-----|-----|
3920 *#*****|*****|
3921 *# Todd Pond 3
3922 *# - Rating curve obtained from Barrhaven South M&S modeling
3923 *# - stantec 2007, Tributary Drainage Area to M&S Pond 3 = 193 ha
3924 *#*****|*****|
3925 ROUTE RESERVOIR NHYDout=[ " M&S_P3 " ] , NHYD i n=[ " TODD " ] ,
3926 RDT=[ 1 ] ( m i n ) ,
3927 TABLE of ( OUTFLOW STORAGE ) values
3928 ( c m s ) - ( h a - m )
3929 [ 0.0 , 0.0 ]
3930 [ 0.014 , 0.155 ]
3931 [ 0.048 , 0.394 ]
3932 [ 0.061 , 0.56 ]
3933 [ 0.08 , 0.909 ]
3934 [ 0.088 , 1.089 ]
3935 [ 0.109 , 1.652 ]
3936 [ 0.118 , 1.952 ]
3937 [ 0.122 , 2.099 ]
3938 [ 1.972 , 2.269 ]
3939 [ 9.135 , 2.598 ]
3940 [ 15.608 , 2.826 ]
3941 [ 19.256 , 2.942 ]
3942 [ 27.282 , 3.181 ]
3943 [ 40.957 , 3.55 ]
3944 [ 56.372 , 3.929 ]
3945 [ 73.349 , 4.317 ]
3946 [ 85.469 , 4.579 ]
3947 [ 104.771 , 4.977 ]
3948 [ -1 , -1 ] ( m a x t w e n t y p t s )
3949 NHYDovf=[ " P3 - O V F " ]
3950 *%-----|-----|
3951 ADD HYD NHYD s u m=[ " SN_TO " ] , NHYD s t o
add=[ " GreenB " + " M&S_P3 " + " P3 - O V F " + " TODD_MN2j " + " A2 - M " ]

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3952 *%-----|-----|
3953 SAVE HYD      NHYD=["SN_TO"], # OF PCYCLES=[-1], ICASEsh=[1]
3954              HYD_COMMENT=["Total Flows at Todd Drain"]
3955 *%-----|-----|
3956 *#
3957 *# Hydrograph from Todd Drain routed to Corrigan Drain
3958 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
3959 *# 2021-02-19 Change the slope from 0.033 % (as per Stantec Report 2007) to 0.05 % so
the model will be more stable and give reasonable results. It is justifiable as ROUTE
CHANNELS aren't well suited to really flat slopes.
*
3960
3961 ROUTE CHANNEL  NHYDout=["N_TO"], NHYDin=["SN_TO"],
3962              RDT=[1](min),
3963              CHLGTH=[280](m), CHSLOPE=[0.05](%),
3964              FPSLOPE=[0.05](%),
3965              SECNUM=[1.0], NSEG=[3]
3966              ( SEGROUGH, SEGDIST (m) )=
3967              [ 0.075, -17.72
3968              -0.045, 17.72
3969              0.075, 80.62] NSEG times
3970              ( DISTANCE (m), ELEVATION (m) )=
3971              [-83.32, 90.00]
3972              [-81.36, 89.50]
3973              [-79.12, 89.00]
3974              [-76.13, 88.50]
3975              [-20.46, 88.00]
3976              [-19.36, 87.50]
3977              [-18.51, 87.00]
3978              [-17.72, 86.50]
3979              [-11.95, 85.24]
3980              [-0.11, 85.12]
3981              [11.49, 85.20]
3982              [17.72, 86.50]
3983              [19.74, 87.00]
3984              [21.22, 87.50]
3985              [22.68, 88.00]
3986              [24.28, 88.50]
3987              [26.79, 89.00]
3988              [71.98, 90.00]
3989              [80.62, 90.50]
3990 *%-----|-----|
3991 SAVE HYD      NHYD=["N_TO"], # OF PCYCLES=[-1], ICASEsh=[1]
3992              HYD_COMMENT=["Total inflows at Station 2462"]
3993 *%-----|-----|
3994 *#*****
3995 *# Catchment CORRIG
3996 *# - To Corrigan Drain (south of the Jock)
3997 *# - Primarily Developed (medium density)
3998 *# - JFSA JAN 2021, add Corrigan subcatchments as per IBI, July 2008
3999 *#*****
4000 *ROUTE RESERVOIR NHYDout=["MS_P1"], NHYDin=["CORRIG"],
4001 *              RDT=[1](min),
4002 *              TABLE of ( OUTFLOW STORAGE ) values
4003 *              (cms) - (ha-m)
4004 *              [ 0.0 , 0.0 ]
4005 *              [ 0.06 , 0.58]
4006 *              [ -1 , -1 ] (max twenty pts)
4007 *              NHYDovf=["P1-OVF"]
4008 *%-----|-----|
4009 *ADD HYD      NHYDsum=["SN_CO"], NHYDs to add=["N_TO"+"P1-OVF"+"MS_P1"]
4010 *%-----|-----|
4011 *SAVE HYD     NHYD=["SN_CO"], # OF PCYCLES=[-1], ICASEsh=[1]
4012 *              HYD_COMMENT=["Total Flows at Corrigan Drain"]
4013 *%-----|-----|
4014 * -JFSA 2021-02-23 "TODD_DEVL" is part of the Corrigan sub-catchment because it
drains to Corrigan SWM as per geoOttawa.ca Feb. 2021. "TODD_DEVL" now is called "corr1"

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and its parameters remain the same.
4015 CONTINUOUS STANDHYD NHYD=["corr1"], DT=[1]min, AREA=[15.87](ha),
4016 XI MP=[0.63], TIMP=[0.63], DWF=[0](cms), LOSS=[2],
4017 SCS curve number CN=[77],
4018 Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
4019 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4020 Impervious surfaces: I A imp=[1.57](mm), SLPI=[1](%),
4021 LGI=[325.27](m), MNI=[0.013], SCI=[0](min),
4022 Continuous simulation parameters:
4023 I a REC per=[4](hrs), I a REC i mp=[4](hrs),
4024 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4025 InterEvent Time=[18](hrs), END=-1
4026 *%-----|-----|
4027 * -JFSA 2021-02-23 add DUALHYD for "corr1". "corr1" DUALHYD Parameters are the
same as A2 DUALHYD Parameters because A2 is the nearest sub-catchment to "corr1".
4028 * At the same time, Corrigan Report, IBI group 2008 has no DUALHYD Parameters for
Al-Corrig
4029 COMPUTE DUALHYD NHYDin=["corr1"], CINLET=[1.818](cms), NINLET=[1],
4030 Mj NHYD=["corr1-M"]
4031 MnNHYD=["corr1-MN"]
4032 TMSTO=[924](cu-m)
4033 *%-----|-----|
4034 * -JFSA 2021-02-23 "TODD_UnD" is part of the Corrigan sub-catchment. "TODD_UnD" now
is called "corr2" and its parameters remain the same.
4035 CONTINUOUS NASHYD NHYD=["corr2"], DT=[1]min, AREA=[12.47](ha),
4036 DWF=[0](cms), CN C=[77], I A=[4.67](mm),
4037 N=[3], TP=[1.10]hrs,
4038 Continuous simulation parameters:
4039 I a REC per=[4](hrs),
4040 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4041 InterEvent Time=[12](hrs)
4042 Baseflow simulation parameters:
4043 BaseFlowOption=[1],
4044 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
4045 VHydCond=[0.055](mm/hr), END=-1
4046 *%-----|-----|
4047 * -JFSA 2021-01-19 change Al-Corrig to be developed as per geottawa website and
apply the parameters of A2, the nearest sub-catchment to Al-Corrig, LGI is calculated
based on Al-Corrig area
4048 * -JFSA 2021-01-19 update all Corrigan areas based on GIS measurements, and keep
LGI as it is from Corrigan Report, IBI Group, 2008 because LGI calculated is less than
LGI from the Corrigan Report
4049 CONTINUOUS STANDHYD NHYD=["Al-Corrig"], DT=[1]min, AREA=[15.75](ha),
4050 XI MP=[0.42], TIMP=[0.52], DWF=[0](cms), LOSS=[2],
4051 SCS curve number CN=[75],
4052 Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
4053 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4054 Impervious surfaces: I A imp=[1.57](mm), SLPI=[1](%),
4055 LGI=[324.037](m), MNI=[0.013], SCI=[0](min),
4056 Continuous simulation parameters:
4057 I a REC per=[4](hrs), I a REC i mp=[4](hrs),
4058 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4059 InterEvent Time=[18](hrs), END=-1
4060 *
4061 * -JFSA 2021-01-25 add DUALHYD for Al-Corrig. Al-Corrig DUALHYD Parameters are the
same as A2 DUALHYD Parameters because A2 is the nearest sub-catchment to Al-Corrig.
4062 * At the same time, Corrigan Report, IBI group 2008 has no DUALHYD Parameters for
Al-Corrig
4063 COMPUTE DUALHYD NHYDin=["Al-Corrig"], CINLET=[1.818](cms), NINLET=[1],
4064 Mj NHYD=["Al-M"]
4065 MnNHYD=["Al-MN"]
4066 TMSTO=[924](cu-m)
4067 *%-----|-----|
4068 *CONTINUOUS NASHYD NHYD=["Al-Corrig"], DT=[1]min, AREA=[15.75](ha),
4069 * DWF=[0](cms), CN C=[66], I A=[2.5](mm),
4070 * N=[3.0], TP=[0.36]hrs,

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4071 *          Continuous simulation parameters:
4072 *          IaRECper=[ 4]( hrs),
4073 *          SMN=[ -1]( mm),   SMAX=[ -1]( mm),   SK=[ 0.010]/( mm),
4074 *          InterEventTime=[ 12]( hrs)
4075 *          Baseflow simulation parameters:
4076 *          BaseFlowOption=[ 1] ,
4077 *          InitGWResVol=[ 50]( mm),   GWResK=[ 0.96]( mm/ day/ mm)
4078 *          VHydCond=[ 0.055]( mm/ hr),   END=- 1
4079 *%-----|-----|
4080 CONTINUOUS NASHYD  NHYD=[ "B1"], DT=[ 1] mi n, AREA=[ 2.77]( ha),
4081 DWF=[ 0]( cms),   CN C=[ 56], IA=[ 2.5]( mm),
4082 N=[ 3.0], TP=[ 0.23] hr s,
4083 Continuous simulation parameters:
4084 IaRECper=[ 4]( hrs),
4085 SMN=[ -1]( mm),   SMAX=[ -1]( mm),   SK=[ 0.010]/( mm),
4086 InterEventTime=[ 12]( hrs)
4087 Baseflow simulation parameters:
4088 BaseFlowOption=[ 1] ,
4089 InitGWResVol=[ 50]( mm),   GWResK=[ 0.96]( mm/ day/ mm)
4090 VHydCond=[ 0.055]( mm/ hr),   END=- 1
4091 *%-----|-----|
4092 CONTINUOUS STANDHYD  NHYD=[ "A4"], DT=[ 1] mi n, AREA=[ 1.27]( ha),
4093 XI MP=[ 0.65], TI MP=[ 0.65], DWF=[ 0]( cms), LOSS=[ 2],
4094 SCS curve number CN=[ 75],
4095 Pervious surfaces: IAper=[ 4.67]( mm), SLPP=[ 1]( %),
4096 LGP=[ 40]( m), MNP=[ 0.25], SCP=[ 0]( mi n),
4097 Impervious surfaces: IAi mp=[ 1.57]( mm), SLPI=[ 1]( %),
4098 LGI=[ 253]( m), MNI =[ 0.013], SCI=[ 0]( mi n),
4099 Continuous simulation parameters:
4100 IaRECper=[ 4]( hrs),   IaRECI mp=[ 4]( hr s),
4101 SMN=[ -1]( mm),   SMAX=[ -1]( mm), SK=[ 0.010]/( mm),
4102 InterEventTime=[ 18]( hr s),   END=- 1
4103 *%-----|-----|
4104 COMPUTE DUALHYD  NHYDin=[ "A4"], CINLET=[ 0.405]( cms), NI NLET=[ 1],
4105 Maj NHYD=[ "A4- M"]
4106 MnNHYD=[ "A4- MN"]
4107 TMI STO=[ 68]( cu- m)
4108 *%-----|-----|
4109 ADD HYD  NHYDsum=[ "MH101"], NHYDs to
add=[ "A1- M" + "A1- MN" + "corr1- M" + "corr1- MN" + "corr2" + "B1" + "A4- MN"]
4110 *%-----|-----|
4111 SAVE HYD  NHYD=[ "MH101"], # OF PCYCLES=[ -1], ICASEsh=[ 1]
4112 HYD_COMMENT=[ "Total Flows at MH101"]
4113 *%-----|-----|
4114 ROUTE PIPE  PTYPE=[ 1] circ, NHYDout=[ "101- 102"], RNUMBER=[ 1.0], PDI AM=[ 1050]( mm),
4115 PLNGTH=[ 368]( m), PROUGH=[ 0.013], PSLOPE=[ 0.0054]( m/ m),
NHYDin=[ "MH101"], RDT=[ 1]
4116 *%-----|-----|
4117 * -JFSA 2021-01-19 move A2 from Corrigan sub-catchment to Todd sub-catchment so the
major system from A2 can be added to Todd
4118 *CONTINUOUS STANDHYD  NHYD=[ "A2"], DT=[ 1] mi n, AREA=[ 25.5]( ha),
4119 * XI MP=[ 0.42], TI MP=[ 0.52], DWF=[ 0]( cms), LOSS=[ 2],
4120 * SCS curve number CN=[ 75],
4121 * Pervious surfaces: IAper=[ 4.67]( mm), SLPP=[ 1]( %),
4122 * LGP=[ 40]( m), MNP=[ 0.25], SCP=[ 0]( mi n),
4123 * Impervious surfaces: IAi mp=[ 1.57]( mm), SLPI=[ 1]( %),
4124 * LGI=[ 566]( m), MNI =[ 0.013], SCI=[ 0]( mi n),
4125 * Continuous simulation parameters:
4126 * IaRECper=[ 4]( hrs),   IaRECI mp=[ 4]( hr s),
4127 * SMN=[ -1]( mm),   SMAX=[ -1]( mm), SK=[ 0.010]/( mm),
4128 * InterEventTime=[ 18]( hr s),   END=- 1
4129 *%-----|-----|
4130 *COMPUTE DUALHYD  NHYDin=[ "A2"], CINLET=[ 1.818]( cms), NI NLET=[ 1],
4131 * Maj NHYD=[ "A2- M"]
4132 * MnNHYD=[ "A2- MN"]
4133 * TMI STO=[ 924]( cu- m)

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4134 *%-----|-----|
4135 ADD HYD          NHYDs um=[ "MH102" ], NHYDs to add=[ "A2-MN"+"101-102" ]
4136 *%-----|-----|
4137 SAVE HYD         NHYD=[ "MH102" ], # OF PCYCLES=[ -1 ], I CASEs h=[ 1 ]
4138 HYD_COMMENT=[ "Total Flows at MH102" ]
4139 *%-----|-----|
4140 CONTINUOUS STANDHYD NHYD=[ "A5" ], DT=[ 1 ] mi n, AREA=[ 1.6 ] (ha),
4141 XI MP=[ 0.71 ], TI MP=[ 0.71 ], DWF=[ 0 ] (cms), LOSS=[ 2 ],
4142 SCS curve number CN=[ 75 ],
4143 Pervious surfaces: I Aper=[ 4.67 ] (mm), SLPP=[ 1 ] ( % ),
4144                    LGP=[ 40 ] (m), MNP=[ 0.25 ], SCP=[ 0 ] (mi n),
4145 ImperVIOUS surfaces: I Ai mp=[ 1.57 ] (mm), SLPI=[ 1 ] ( % ),
4146                    LGI=[ 300 ] (m), MNI=[ 0.013 ], SCI=[ 0 ] (mi n),
4147 Continuous simulation parameters:
4148 I a RE Cper=[ 4 ] (hrs), I a RE Ci mp=[ 4 ] (hrs),
4149 SM N=[ -1 ] (mm), SMAX=[ -1 ] (mm), SK=[ 0.010 ] / (mm),
4150 InterEvent Ti me=[ 18 ] (hrs), END=- 1
4151 *%-----|-----|
4152 ADD HYD          NHYDs um=[ "A5T" ], NHYDs to add=[ "A4-M"+"A5" ]
4153 *%-----|-----|
4154 COMPUTE DUALHYD  NHYDi n=[ "A5T" ], CI NLET=[ 0.357 ] (cms), NI NLET=[ 1 ],
4155 M aj NHYD=[ "A5-M" ]
4156 M nNHYD=[ "A5-MN" ]
4157 TM STO=[ 60 ] (cu-m)
4158 *%-----|-----|
4159 * -JFSA Jan. 2021, A3 is a part of Todd so it is removed
4160 * -JFSA Jan. 2021, "A2-M" added to "Todd"
4161 *CONTINUOUS STANDHYD NHYD=[ "A3" ], DT=[ 1 ] mi n, AREA=[ 18.4 ] (ha),
4162 * XI MP=[ 0.58 ], TI MP=[ 0.65 ], DWF=[ 0 ] (cms), LOSS=[ 2 ],
4163 * SCS curve number CN=[ 75 ],
4164 * Pervious surfaces: I Aper=[ 4.67 ] (mm), SLPP=[ 1 ] ( % ),
4165 *                    LGP=[ 40 ] (m), MNP=[ 0.25 ], SCP=[ 0 ] (mi n),
4166 * ImperVIOUS surfaces: I Ai mp=[ 1.57 ] (mm), SLPI=[ 1 ] ( % ),
4167 *                    LGI=[ 450 ] (m), MNI=[ 0.013 ], SCI=[ 0 ] (mi n),
4168 * Continuous simulation parameters:
4169 * I a RE Cper=[ 4 ] (hrs), I a RE Ci mp=[ 4 ] (hrs),
4170 * SM N=[ -1 ] (mm), SMAX=[ -1 ] (mm), SK=[ 0.010 ] / (mm),
4171 * InterEvent Ti me=[ 18 ] (hrs), END=- 1
4172 *%-----|-----|
4173 *ADD HYD          NHYDs um=[ "A3-A2M" ], NHYDs to add=[ "A2-M"+"A3" ]
4174 *%-----|-----|
4175 *COMPUTE DUALHYD  NHYDi n=[ "A3-A2M" ], CI NLET=[ 2.208 ] (cms), NI NLET=[ 1 ],
4176 * M aj NHYD=[ "A3R-M" ]
4177 * M nNHYD=[ "A3R-MN" ]
4178 * TM STO=[ 908 ] (cu-m)
4179 *%-----|-----|
4180 ROUTE PIPE       PTYPE=[ 1 ] circ, NHYDout=[ "102-103" ], RNUMBER=[ 1.0 ], PDI AM=[ 1500 ] (mm),
4181 PLNGTH=[ 504 ] (m), PROUGH=[ 0.013 ], PSLOPE=[ 0.0028 ] (m/m),
NHYDi n=[ "MH102" ], RDT=[ 1 ]
4182 *%-----|-----|
4183 ADD HYD          NHYDs um=[ "MH103" ], NHYDs to add=[ "102-103"+"A5-MN" ]
4184 *%-----|-----|
4185 SAVE HYD         NHYD=[ "MH103" ], # OF PCYCLES=[ -1 ], I CASEs h=[ 1 ]
4186 HYD_COMMENT=[ "Total Flows at MH103" ]
4187 *%-----|-----|
4188 ROUTE PIPE       PTYPE=[ 1 ] circ, NHYDout=[ "103-104" ], RNUMBER=[ 1.0 ], PDI AM=[ 1650 ] (mm),
4189 PLNGTH=[ 438 ] (m), PROUGH=[ 0.013 ], PSLOPE=[ 0.0046 ] (m/m),
NHYDi n=[ "MH103" ], RDT=[ 1 ]
4190 *%-----|-----|
4191 CONTINUOUS STANDHYD NHYD=[ "A6" ], DT=[ 1 ] mi n, AREA=[ 1.56 ] (ha),
4192 XI MP=[ 0.71 ], TI MP=[ 0.71 ], DWF=[ 0 ] (cms), LOSS=[ 2 ],
4193 SCS curve number CN=[ 75 ],
4194 Pervious surfaces: I Aper=[ 4.67 ] (mm), SLPP=[ 1 ] ( % ),
4195                    LGP=[ 40 ] (m), MNP=[ 0.25 ], SCP=[ 0 ] (mi n),
4196 ImperVIOUS surfaces: I Ai mp=[ 1.57 ] (mm), SLPI=[ 1 ] ( % ),
4197                    LGI=[ 280 ] (m), MNI=[ 0.013 ], SCI=[ 0 ] (mi n),

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4198 Continuous simulation parameters:
4199 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
4200 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4201 InterEventTime=[ 18](hrs), END=- 1
4202 *%-----|
4203 ADD HYD NHYDsum=["A6T"], NHYDs to add=["A5-M"+"A6"]
4204 *%-----|
4205 COMPUTE DUALHYD NHYDin=["A6T"], CINLET=[ 0.357](cms), NINLET=[ 1],
4206 MjNHYD=["A6-M"]
4207 MnNHYD=["A6-MN"]
4208 TMSSTO=[ 60](cu-m)
4209 *%-----|
4210 * -JFSA Jan. 2021, A7-corrig is a part of Todd so it is removed
4211 *CONTINUOUS STANDHYD NHYD=["A7-corrig"], DT=[ 1]min, AREA=[ 11.8](ha),
4212 * XIMP=[ 0.41], TIMP=[ 0.54], DWF=[ 0](cms), LOSS=[ 2],
4213 * SCS curve number CN=[ 75],
4214 * Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
4215 * LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4216 * Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 1](%),
4217 * LGI=[ 438](m), MNI=[ 0.013], SCI=[ 0](min),
4218 * Continuous simulation parameters:
4219 * IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
4220 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4221 * InterEventTime=[ 18](hrs), END=- 1
4222 *%-----|
4223 *ADD HYD NHYDsum=["A7-A3RM"], NHYDs to add=["A3R-M"+"A7-corrig"]
4224 *%-----|
4225 *COMPUTE DUALHYD NHYDin=["A7-A3RM"], CINLET=[ 1.003](cms), NINLET=[ 1],
4226 * MjNHYD=["A7R-M"]
4227 * MnNHYD=["A7R-MN"]
4228 * TMSSTO=[ 496](cu-m)
4229 *%-----|
4230 ADD HYD NHYDsum=["MH104"], NHYDs to add=["A6-MN"+"103-104"+"TODD_Min"]
4231 *%-----|
4232 SAVE HYD NHYD=["MH104"], # OF PCYCLES=[ -1], ICASEsh=[ 1]
4233 HYD_COMMENT=["Total Flows at MH104"]
4234 *%-----|
4235 CONTINUOUS STANDHYD NHYD=["B2"], DT=[ 1]min, AREA=[ 12.31](ha),
4236 XIMP=[ 0.41], TIMP=[ 0.54], DWF=[ 0](cms), LOSS=[ 2],
4237 SCS curve number CN=[ 75],
4238 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
4239 LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4240 Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 1](%),
4241 LGI=[ 417](m), MNI=[ 0.013], SCI=[ 0](min),
4242 Continuous simulation parameters:
4243 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
4244 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4245 InterEventTime=[ 18](hrs), END=- 1
4246 *%-----|
4247 COMPUTE DUALHYD NHYDin=["B2"], CINLET=[ 1.029](cms), NINLET=[ 1],
4248 MjNHYD=["B2-M"]
4249 MnNHYD=["B2-MN"]
4250 TMSSTO=[ 508](cu-m)
4251 *%-----|
4252 ROUTE PIPE PTYPE=[ 1]circ, NHYDout=["315-333"], RNUMBER=[ 1.0], PDIAM=[ 1200](mm),
4253 PLNGTH=[ 254](m), PROUGH=[ 0.013], PSLOPE=[ 0.001](m/m),
NHYDin=["B2-MN"], RDT=[ 1]
4254 *%-----|
4255 CONTINUOUS STANDHYD NHYD=["B3"], DT=[ 1]min, AREA=[ 5.59](ha),
4256 XIMP=[ 0.41], TIMP=[ 0.54], DWF=[ 0](cms), LOSS=[ 2],
4257 SCS curve number CN=[ 75],
4258 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
4259 LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4260 Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 1](%),
4261 LGI=[ 345](m), MNI=[ 0.013], SCI=[ 0](min),
4262 Continuous simulation parameters:

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4263 IaRECper=[ 4](hr s), IaRECImp=[ 4](hr s),
4264 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4265 InterEventTime=[ 18](hr s), END=- 1
4266 *%-----|-----|
4267 COMPUTE DUALHYD NHYDin=[" B3"], CI NLET=[ 0.459](cms), NI NLET=[ 1],
4268 Mj NHYD=[" B3- M"]
4269 MnNHYD=[" B3- MN"]
4270 TMSTO=[ 227](cu- m)
4271 *%-----|-----|
4272 ADD HYD NHYDs um=[" MH333"], NHYDs to add=[" B3- MN"+" 315- 333"]
4273 *%-----|-----|
4274 SAVE HYD NHYD=[" MH333"], # OF PCYCLES=[ -1], I CASEs h=[ 1]
4275 HYD_COMMENT=[" Total Flows at MH333"]
4276 *%-----|-----|
4277 ROUTE PIPE PTYPE=[ 1]circ, NHYDout=[" 333- 335"], RNUMBER=[ 1.0], PDI AM=[ 1200](mm),
4278 PLNGTH=[ 251](m), PROUGH=[ 0.013], PSLOPE=[ 0.001](m/m),
NHYDin=[" MH333"], RDT=[ 1]
4279 *%-----|-----|
4280 ROUTE PIPE PTYPE=[ 1]circ, NHYDout=[" 335- 338"], RNUMBER=[ 1.0], PDI AM=[ 1200](mm),
4281 PLNGTH=[ 185](m), PROUGH=[ 0.013], PSLOPE=[ 0.001](m/m),
NHYDin=[" 333- 335"], RDT=[ 1]
4282 *%-----|-----|
4283 ROUTE PIPE PTYPE=[ 1]circ, NHYDout=[" 338- 340"], RNUMBER=[ 1.0], PDI AM=[ 1350](mm),
4284 PLNGTH=[ 233](m), PROUGH=[ 0.013], PSLOPE=[ 0.001](m/m),
NHYDin=[" 335- 338"], RDT=[ 1]
4285 *%-----|-----|
4286 CONTINUOUS STANDHYD NHYD=[" B4"], DT=[ 1]min, AREA=[ 7.6](ha),
4287 XI MP=[ 0.41], TI MP=[ 0.54], DWF=[ 0](cms), LOSS=[ 2],
4288 SCS curve number CN=[ 75],
4289 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
4290 LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4291 ImperVIOUS surfaces: IAi mp=[ 1.57](mm), SLPI =[ 1](%),
4292 LGI =[ 388](m), MNI =[ 0.013], SCI =[ 0](min),
4293 Continuous simulation parameters:
4294 IaRECper=[ 4](hr s), IaRECImp=[ 4](hr s),
4295 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4296 InterEventTime=[ 18](hr s), END=- 1
4297 *%-----|-----|
4298 COMPUTE DUALHYD NHYDin=[" B4"], CI NLET=[ 0.655](cms), NI NLET=[ 1],
4299 Mj NHYD=[" B4- M"]
4300 MnNHYD=[" B4- MN"]
4301 TMSTO=[ 323](cu- m)
4302 *%-----|-----|
4303 ADD HYD NHYDs um=[" MH340"], NHYDs to add=[" 338- 340"+" B4- MN"]
4304 *%-----|-----|
4305 SAVE HYD NHYD=[" MH340"], # OF PCYCLES=[ -1], I CASEs h=[ 1]
4306 HYD_COMMENT=[" Total Flows at MH340"]
4307 *%-----|-----|
4308 ROUTE PIPE PTYPE=[ 1]circ, NHYDout=[" 340- 104"], RNUMBER=[ 1.0], PDI AM=[ 1650](mm),
4309 PLNGTH=[ 240](m), PROUGH=[ 0.013], PSLOPE=[ 0.0015](m/m),
NHYDin=[" MH340"], RDT=[ 1]
4310 *%-----|-----|
4311 ADD HYD NHYDs um=[" MH104T"], NHYDs to add=[" 340- 104"+" MH104"]
4312 *%-----|-----|
4313 ROUTE PIPE PTYPE=[ 2]rect, NHYDout=[" 104- 105"], RNUMBER=[ 1.0],
4314 PWDTH=[ 2400](mm) by PHEI GHT=[ 2100](mm),
PLNGTH=[ 380](m), PROUGH=[ 0.013], PSLOPE=[ 0.001](m/m),
NHYDin=[" MH104T"], RDT=[ 1]
4315 *%-----|-----|
4316 CONTINUOUS STANDHYD NHYD=[" B5"], DT=[ 1]min, AREA=[ 2.2](ha),
4317 XI MP=[ 0.57], TI MP=[ 0.57], DWF=[ 0](cms), LOSS=[ 2],
4318 SCS curve number CN=[ 75],
4319 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
4320 LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4321 ImperVIOUS surfaces: IAi mp=[ 1.57](mm), SLPI =[ 1](%),

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4322             LGI=[ 187](m), MNI=[ 0.013], SCI=[ 0](min),
4323 Continuous simulation parameters:
4324 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
4325 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4326 InterEventTime=[ 18](hrs), END=- 1
4327 *%-----|
4328 COMPUTE DUALHYD NHYDin=[ "B5" ], CINLET=[ 0.260](cms), NINLET=[ 1],
4329 MijNHYD=[ "B5-M" ]
4330 MnNHYD=[ "B5-MN" ]
4331 TMSSTO=[ 250](cu-m)
4332 *%-----|
4333 CONTINUOUS STANDHYD NHYD=[ "A8" ], DT=[ 1]min, AREA=[ 0.96](ha),
4334 XI MP=[ 0.71], TIMP=[ 0.71], DWF=[ 0](cms), LOSS=[ 2],
4335 SCS curve number CN=[ 75],
4336 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
4337 LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4338 Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 1](%),
4339 LGI=[ 186](m), MNI=[ 0.013], SCI=[ 0](min),
4340 Continuous simulation parameters:
4341 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
4342 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4343 InterEventTime=[ 18](hrs), END=- 1
4344 *%-----|
4345 ADD HYD NHYDs um=[ "A8T" ], NHYDs to add=[ "A6-M" + "A8" ]
4346 *%-----|
4347 COMPUTE DUALHYD NHYDin=[ "A8T" ], CINLET=[ 0.238](cms), NINLET=[ 1],
4348 MijNHYD=[ "A8-M" ]
4349 MnNHYD=[ "A8-MN" ]
4350 TMSSTO=[ 40](cu-m)
4351 *%-----|
4352 ADD HYD NHYDs um=[ "MH105" ], NHYDs to
4353 add=[ "104-105" + "B5-MN" + "A8-MN" + "TODD_MN3j" ]
4354 *%-----|
4355 SAVE HYD NHYD=[ "MH105" ], # OF PCYCLES=[ -1], ICASEsh=[ 1]
4356 HYD_COMMENT=[ "Total Flows at MH105" ]
4357 *%-----|
4358 DI VERT HYD NHYDin=[ "A8-M" ] NIDout=[ 2]max five,
4359 outflow hydrographs (NHYDs)=[ "A8-M-JR" "A8-M-B6" ]
4360 flow distribution table: (modify as necessary)
4361 Note: all flows are in (cms)
4362 QIDi + QIDi = QTOTAL
4363 [ 0 + 0 = 0 ]
4364 [ 50 + 50 = 100 ] end
4365 *%-----|
4366 DI VERT HYD NHYDin=[ "MH105" ] NIDout=[ 2]max five,
4367 outflow hydrographs (NHYDs)=[ "MH105-JR" "MH105-B6" ]
4368 flow distribution table: (modify as necessary)
4369 Note: all flows are in (cms)
4370 QIDi + QIDi = QTOTAL
4371 [ 0 + 0 = 0 ]
4372 [ 0 + 3.0 = 3.0 ]
4373 [ 96.9+ 3.1 = 100 ] end
4374 *%-----|
4375 CONTINUOUS STANDHYD NHYD=[ "B7" ], DT=[ 1]min, AREA=[ 7.19](ha),
4376 XI MP=[ 0.41], TIMP=[ 0.54], DWF=[ 0](cms), LOSS=[ 2],
4377 SCS curve number CN=[ 75],
4378 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
4379 LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4380 Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 1](%),
4381 LGI=[ 211](m), MNI=[ 0.013], SCI=[ 0](min),
4382 Continuous simulation parameters:
4383 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
4384 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4385 InterEventTime=[ 18](hrs), END=- 1

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4385 *%-----|-----|
4386 ADD HYD NHYDs um=[ " B7- B4M " ], NHYDs to add=[ " B4- M " + " B7 " ]
4387 *%-----|-----|
4388 COMPUTE DUALHYD NHYD i n=[ " B7- B4M " ], CI NLET=[ 0. 629 ] ( c ms ), NI NLET=[ 1 ],
4389 M a j NHYD=[ " B7R- M " ]
4390 M n NHYD=[ " B7R- MN " ]
4391 T M S T O=[ 311 ] ( c u- m )
4392 *%-----|-----|
4393 ROUTE PI PE PTYPE=[ 1 ] c i r c, NHYD out=[ " 360- 106A " ], RNUMBER=[ 1. 0 ], PDI AM=[ 1050 ] ( m m ),
4394 PLNGTH=[ 167 ] ( m ), PROUGH=[ 0. 013 ], PSLOPE=[ 0. 001 ] ( m / m ),
NHYD i n=[ " B7R- MN " ], RDT=[ 1 ]
4395 *%-----|-----|
4396 * -JFSA 2021-01-19 change B6 to be developed as per geottawa website and apply the
parameters of A7, the nearest sub-catchment to B6, LGI is calculated based on B6 area
CONTINUOUS STANDHYD NHYD=[ " B6 " ], DT=[ 1 ] m i n, AREA=[ 3. 29 ] ( h a ),
4397 XI MP=[ 0. 41 ], TI MP=[ 0. 54 ], DWF=[ 0 ] ( c ms ), LOSS=[ 2 ],
4398 SCS curve number CN=[ 75 ],
4400 P e r v i o u s s u r f a c e s : I A p e r=[ 4. 67 ] ( m m ), S L P P=[ 1 ] ( % ),
4401 L G P=[ 40 ] ( m ), M N P=[ 0. 25 ], S C P=[ 0 ] ( m i n ),
4402 I m p e r v i o u s s u r f a c e s : I A i m p=[ 1. 57 ] ( m m ), S L P I=[ 1 ] ( % ),
4403 L G I=[ 148. 099 ] ( m ), M N I=[ 0. 013 ], S C I=[ 0 ] ( m i n ),
4404 C o n t i n u o u s s i m u l a t i o n p a r a m e t e r s :
4405 I a R E C p e r=[ 4 ] ( h r s ), I a R E C i m p=[ 4 ] ( h r s ),
4406 S M N=[ - 1 ] ( m m ), S M A X=[ - 1 ] ( m m ), S K=[ 0. 010 ] / ( m m ),
4407 I n t e r E v e n t T i m e=[ 18 ] ( h r s ), E N D=- 1
4408 *%-----|-----|
4409 * -JFSA 2021-01-25 add B1 DUALHYD as per Corrigan Report, IBI Group, 2008
COMPUTE DUALHYD NHYD i n=[ " B6 " ], CI NLET=[ 0. 064 ] ( c ms ), NI NLET=[ 1 ],
4410 M a j NHYD=[ " B6- M " ]
4411 M n NHYD=[ " B6- MN " ]
4412 T M S T O=[ 5484 ] ( c u- m )
4413 *%-----|-----|
4414 *CONTINUOUS NASHYD NHYD=[ " B6 " ], DT=[ 1 ] m i n, AREA=[ 3. 29 ] ( h a ),
4415 DWF=[ 0 ] ( c ms ), C N C=[ 75 ], I A=[ 2. 5 ] ( m m ),
4416 N=[ 3. 0 ], T P=[ 0. 36 ] h r s,
4417 C o n t i n u o u s s i m u l a t i o n p a r a m e t e r s :
4418 I a R E C p e r=[ 4 ] ( h r s ),
4419 S M N=[ - 1 ] ( m m ), S M A X=[ - 1 ] ( m m ), S K=[ 0. 010 ] / ( m m ),
4420 I n t e r E v e n t T i m e=[ 12 ] ( h r s )
4421 B a s e f l o w s i m u l a t i o n p a r a m e t e r s :
4422 B a s e F l o w O p t i o n=[ 1 ],
4423 I n i t G W R e s V o l=[ 50 ] ( m m ), G W R e s K=[ 0. 96 ] ( m m / d a y / m m )
4424 V H y d C o n d=[ 0. 055 ] ( m m / h r ), E N D=- 1
4425 *%-----|-----|
4426 *% -EX-LAND is external land. It is a part of JOCKVA sub-catchment as per Corrigan
Report, IBI Group, 2008
CONTINUOUS STANDHYD NHYD=[ " EX- LAND " ], DT=[ 1 ] m i n, AREA=[ 32. 5 ] ( h a ),
4427 XI MP=[ 0. 50 ], TI MP=[ 0. 50 ], DWF=[ 0 ] ( c ms ), LOSS=[ 2 ],
4428 SCS curve number CN=[ 74 ],
4429 P e r v i o u s s u r f a c e s : I A p e r=[ 4. 67 ] ( m m ), S L P P=[ 1 ] ( % ),
4430 L G P=[ 40 ] ( m ), M N P=[ 0. 25 ], S C P=[ 0 ] ( m i n ),
4431 I m p e r v i o u s s u r f a c e s : I A i m p=[ 1. 57 ] ( m m ), S L P I=[ 1 ] ( % ),
4432 L G I=[ 465. 475 ] ( m ), M N I=[ 0. 013 ], S C I=[ 0 ] ( m i n ),
4433 C o n t i n u o u s s i m u l a t i o n p a r a m e t e r s :
4434 I a R E C p e r=[ 4 ] ( h r s ), I a R E C i m p=[ 4 ] ( h r s ),
4435 S M N=[ - 1 ] ( m m ), S M A X=[ - 1 ] ( m m ), S K=[ 0. 010 ] / ( m m ),
4436 I n t e r E v e n t T i m e=[ 18 ] ( h r s ), E N D=- 1
4437 *%-----|-----|
4438 COMPUTE DUALHYD NHYD i n=[ " EX- LAND " ], CI NLET=[ 2. 275 ] ( c ms ), NI NLET=[ 1 ],
4439 M a j NHYD=[ " EX- LAND- M " ]
4440 M n NHYD=[ " EX- LAND- MN " ]
4441 T M S T O=[ 1365 ] ( c u- m )
4442 *%-----|-----|
4443 ADD HYD NHYDs um=[ " B6- B7ExM " ], NHYDs to
4444 add=[ " B7R- M " + " EX- LAND- M " + " B5- M " + " B6- M " + " B6- MN " + " A8- M - B6 " ]
4445 *%-----|-----|
4446

```

```

4447 COMPUTE DUALHYD      NHYDIn=[ " B6- B7ExM " ], CI NLET=[ 0. 064 ] ( cms ), NI NLET=[ 1 ],
4448                      Mj NHYD=[ " B6R- M " ]
4449                      MnNHYD=[ " B6R- MN " ]
4450                      TM STO=[ 5484 ] ( cu- m )
4451 *%-----|-----|
4452 ROUTE PIPE            PTYPE=[ 1 ] circ, NHYDout=[ " 105- 106A " ], RNUMBER=[ 1. 0 ], PDI AM=[ 1800 ] ( mm ),
4453                      PLNGTH=[ 208 ] ( m ), PROUGH=[ 0. 013 ], PSLOPE=[ 0. 001 ] ( m/ m ),
                      NHYDIn=[ " MHI 05- B6 " ], RDT=[ 1 ]
4454 *%-----|-----|
4455 ADD HYD              NHYDsum=[ " MHI 06A " ], NHYDs to
add=[ " 360- 106A " + " 105- 106A " + " B6R- MN " + " B6R- M " ]
4456 *%-----|-----|
4457 SAVE HYD             NHYD=[ " MHI 06A " ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1 ]
4458                      HYD_COMMENT=[ " Tot al Fl ows at MHI 06A " ]
4459 *%-----|-----|
4460 *%      -JFSA 2021-01-12 THE MANHOLE MHI06 is called MHI17/106 in Corrigan Report, IBI
Group, July 2008
4461 *%
4462 ROUTE PIPE            PTYPE=[ 1 ] circ, NHYDout=[ " 106A- 106 " ], RNUMBER=[ 1. 0 ], PDI AM=[ 1800 ] ( mm ),
4463                      PLNGTH=[ 190 ] ( m ), PROUGH=[ 0. 013 ], PSLOPE=[ 0. 001 ] ( m/ m ),
                      NHYDIn=[ " MHI 06A " ], RDT=[ 1 ]
4464 *%-----|-----|
4465 CONTINUOUS STANDHYD NHYD=[ " A9 " ], DT=[ 1 ] mi n, AREA=[ 2. 44 ] ( ha ),
4466                      XI MP=[ 0. 71 ], TI MP=[ 0. 71 ], DWF=[ 0 ] ( cms ), LOSS=[ 2 ],
4467                      SCS curve number CN=[ 75 ],
4468                      Pervious surfaces: I Aper=[ 4. 67 ] ( mm ), SLPP=[ 1 ] ( % ),
4469                      LGP=[ 40 ] ( m ), MNP=[ 0. 25 ], SCP=[ 0 ] ( mi n ),
4470                      Impervious surfaces: I Ai mp=[ 1. 57 ] ( mm ), SLPI=[ 1 ] ( % ),
4471                      LGI=[ 262 ] ( m ), MNI =[ 0. 013 ], SCI =[ 0 ] ( mi n ),
4472                      Continuous simulation parameters:
4473                      IaRECper=[ 4 ] ( hrs ), IaRECI mp=[ 4 ] ( hrs ),
4474                      SM N=[ - 1 ] ( mm ), SMAX=[ - 1 ] ( mm ), SK=[ 0. 010 ] / ( mm ),
4475                      InterEvent Ti me=[ 18 ] ( hrs ), END=- 1
4476 *%-----|-----|
4477 COMPUTE DUALHYD      NHYDIn=[ " A9 " ], CI NLET=[ 0. 547 ] ( cms ), NI NLET=[ 1 ],
4478                      Mj NHYD=[ " A9- M " ]
4479                      MnNHYD=[ " A9- MN " ]
4480                      TM STO=[ 0 ] ( cu- m )
4481 *%-----|-----|
4482 ADD HYD              NHYDsum=[ " MHI 06 " ], NHYDs to add=[ " 106A- 106 " + " A9- MN " ]
4483 *%-----|-----|
4484 SAVE HYD             NHYD=[ " MHI 06 " ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1 ]
4485                      HYD_COMMENT=[ " Tot al Fl ows at MHI 06 " ]
4486 *%-----|-----|
4487 *%      -JFSA 2021-01-12 THE MANHOLE MHI07 is called MHI18/107 in Corrigan Report, IBI
Group, July 2008
4488 *%
4489 ROUTE PIPE            PTYPE=[ 1 ] circ, NHYDout=[ " 106- 107 " ], RNUMBER=[ 1. 0 ], PDI AM=[ 1800 ] ( mm ),
4490                      PLNGTH=[ 122. 5 ] ( m ), PROUGH=[ 0. 013 ], PSLOPE=[ 0. 001 ] ( m/ m ),
                      NHYDIn=[ " MHI 06 " ], RDT=[ 1 ]
4491 *%-----|-----|
4492 CONTINUOUS STANDHYD NHYD=[ " A10 " ], DT=[ 1 ] mi n, AREA=[ 4. 14 ] ( ha ),
4493                      XI MP=[ 0. 35 ], TI MP=[ 0. 47 ], DWF=[ 0 ] ( cms ), LOSS=[ 2 ],
4494                      SCS curve number CN=[ 75 ],
4495                      Pervious surfaces: I Aper=[ 4. 67 ] ( mm ), SLPP=[ 1 ] ( % ),
4496                      LGP=[ 40 ] ( m ), MNP=[ 0. 25 ], SCP=[ 0 ] ( mi n ),
4497                      Impervious surfaces: I Ai mp=[ 1. 57 ] ( mm ), SLPI=[ 1 ] ( % ),
4498                      LGI=[ 183 ] ( m ), MNI =[ 0. 013 ], SCI =[ 0 ] ( mi n ),
4499                      Continuous simulation parameters:
4500                      IaRECper=[ 4 ] ( hrs ), IaRECI mp=[ 4 ] ( hrs ),
4501                      SM N=[ - 1 ] ( mm ), SMAX=[ - 1 ] ( mm ), SK=[ 0. 010 ] / ( mm ),
4502                      InterEvent Ti me=[ 18 ] ( hrs ), END=- 1
4503 *%-----|-----|
4504 COMPUTE DUALHYD      NHYDIn=[ " A10 " ], CI NLET=[ 0. 310 ] ( cms ), NI NLET=[ 1 ],
4505                      Mj NHYD=[ " A10- M " ]
4506                      MnNHYD=[ " A10- MN " ]

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4507          TMI STO=[ 228] (cu-m)
4508 *%-----|-----|
4509 CONTINUOUS STANDHYD NHYD=["A11"], DT=[1]min, AREA=[10.61](ha),
4510          XI MP=[0.53], TI MP=[0.62], DWF=[0](cms), LOSS=[2],
4511          SCS curve number CN=[75],
4512          Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4513          LGP=[40](m), MNP=[0.25], SCP=[0](min),
4514          Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4515          LGI=[379](m), MNI=[0.013], SCI=[0](min),
4516          Continuous simulation parameters:
4517          IaRECper=[4](hrs), IaRECImp=[4](hrs),
4518          SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4519          InterEventTime=[18](hrs), END=-1
4520 *%-----|-----|
4521 COMPUTE DUALHYD      NHYDin=["A11"], CILET=[0.993](cms), NILET=[1],
4522          MajNHYD=["A11-M"]
4523          MnNHYD=["A11-MN"]
4524          TMI STO=[556](cu-m)
4525 *%-----|-----|
4526 ADD HYD              NHYDsum=["MH107"], NHYDsto add=["106-107"+"A10-MN"+"A11-MN"]
4527 *%-----|-----|
4528 SAVE HYD            NHYD=["MH107"], # OF PCYCLES=[-1], ICASEsh=[1]
4529          HYD_COMMENT=["Total Flows at MH107"]
4530 *%-----|-----|
4531 ROUTE PIPE          PTYPE=[1]circ, NHYDout=["107-119"], RNUMBER=[1.0], PDIAM=[1800](mm),
4532          PLNGTH=[114](m), PROUGH=[0.013], PSLOPE=[0.0012](m/m),
          NHYDin=["MH107"], RDT=[1]
4533 *%-----|-----|
4534 *% -JFSA 2021-01-12 THE MANHOLE MH108 is called MH20/108 in Corrigan Report, IBI
Group, July 2008
4535 *%
4536 ROUTE PIPE          PTYPE=[1]circ, NHYDout=["119-108"], RNUMBER=[1.0], PDIAM=[1800](mm),
4537          PLNGTH=[65.8](m), PROUGH=[0.013], PSLOPE=[0.0012](m/m),
          NHYDin=["107-119"], RDT=[1]
4538 *%-----|-----|
4539 CONTINUOUS STANDHYD NHYD=["A12"], DT=[1]min, AREA=[12.29](ha),
4540          XI MP=[0.41], TI MP=[0.54], DWF=[0](cms), LOSS=[2],
4541          SCS curve number CN=[75],
4542          Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4543          LGP=[40](m), MNP=[0.25], SCP=[0](min),
4544          Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4545          LGI=[183](m), MNI=[0.013], SCI=[0](min),
4546          Continuous simulation parameters:
4547          IaRECper=[4](hrs), IaRECImp=[4](hrs),
4548          SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4549          InterEventTime=[18](hrs), END=-1
4550 *%-----|-----|
4551 COMPUTE DUALHYD      NHYDin=["A12"], CILET=[1.029](cms), NILET=[1],
4552          MajNHYD=["A12-M"]
4553          MnNHYD=["A12-MN"]
4554          TMI STO=[672](cu-m)
4555 *%-----|-----|
4556 CONTINUOUS STANDHYD NHYD=["A13"], DT=[1]min, AREA=[2.59](ha),
4557          XI MP=[0.71], TI MP=[0.71], DWF=[0](cms), LOSS=[2],
4558          SCS curve number CN=[75],
4559          Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4560          LGP=[40](m), MNP=[0.25], SCP=[0](min),
4561          Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4562          LGI=[379](m), MNI=[0.013], SCI=[0](min),
4563          Continuous simulation parameters:
4564          IaRECper=[4](hrs), IaRECImp=[4](hrs),
4565          SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4566          InterEventTime=[18](hrs), END=-1
4567 *%-----|-----|
4568 COMPUTE DUALHYD      NHYDin=["A13"], CILET=[0.571](cms), NILET=[1],
4569          MajNHYD=["A13-M"]

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4570 M nNHYD=[ " A13- MN" ]
4571 TMJ STO=[ 0] ( cu- m)
4572 *%-----|-----
4573 * -JFSA 2021-01-22 add the Corrigan pond area ("Pond-Block")
4574 CONTINUOUS STANDHYD NHYD=[ " Pond- Block" ], DT=[ 1] mi n, AREA=[ 2.94] ( ha),
4575 XI MP=[ 0.415], TI MP=[ 0.415], DWF=[ 0] ( cms), LOSS=[ 2],
4576 SCS curve number CN=[ 75],
4577 Pervious surfaces: I Aper=[ 4.67] ( mm), SLPP=[ 1] ( %),
4578 LGP=[ 40] ( m), MNP=[ 0.25], SCP=[ 0] ( mi n),
4579 Impervious surfaces: I Ai mp=[ 1.57] ( mm), SLPI =[ 1] ( %),
4580 LGI =[ 183] ( m), MNI =[ 0.013], SCI =[ 0] ( mi n),
4581 Continuous simulation parameters:
4582 IaRECper=[ 4] ( hrs), IaRECI mp=[ 4] ( hrs),
4583 SM N=[ -1] ( mm), SMAX=[ -1] ( mm), SK=[ 0.010] / ( mm),
4584 InterEvent Time=[ 18] ( hrs), END=- 1
4585 *%-----|-----
4586 ADD HYD NHYDsum=[ " MHI08" ], NHYDs to add=[ " 119- 108" + " A13- MN" + " A12- MN" ]
4587 *%-----|-----
4588 SAVE HYD NHYD=[ " MHI08" ], # OF PCYCLES=[ -1], ICASEsh=[ 1]
4589 HYD_COMMENT=[ " Total Flows at MHI08" ]
4590 *%-----|-----
4591 ROUTE PIPE PTYPE=[ 1] circ, NHYDout=[ " 108- 116" ], RNUMBER=[ 1.0], PDI AM=[ 1800] ( mm),
4592 PLNGTH=[ 76.6] ( m), PROUGH=[ 0.013], PSLOPE=[ 0.0013] ( m/ m),
4593 NHYDi n=[ " MHI08" ], RDT=[ 1]
4594 *%-----|-----
4595 ROUTE PIPE PTYPE=[ 1] circ, NHYDout=[ " 116- corrig" ], RNUMBER=[ 1.0],
4596 PDI AM=[ 1800] ( mm),
4597 PLNGTH=[ 79.5] ( m), PROUGH=[ 0.013], PSLOPE=[ 0.0013] ( m/ m),
4598 NHYDi n=[ " 108- 116" ], RDT=[ 1]
4599 *%-----|-----
4600 ADD HYD NHYDsum=[ " Corrigan" ], NHYDs to add=[ " 116- corrig" + " Pond- Block" ]
4601 *%-----|-----
4602 SAVE HYD NHYD=[ " Corrigan" ], # OF PCYCLES=[ -1], ICASEsh=[ 1]
4603 HYD_COMMENT=[ " Total Flows at Corrigan Pond" ]
4604 *%-----|-----
4605 ROUTE RESERVOIR NHYDout=[ " Co- P" ], NHYDi n=[ " Corrigan" ],
4606 RDT=[ 1] ( mi n),
4607 TABLE of ( OUTFLOW STORAGE ) values
4608 ( cms ) - ( ha- m)
4609 [ 0.0 , 0.0 ]
4610 [ 0.015 , 0.04118]
4611 [ 0.030 , 0.08297]
4612 [ 0.045 , 0.12537]
4613 [ 0.060 , 0.16837]
4614 [ 0.075 , 0.21199]
4615 [ 0.090 , 0.27545]
4616 [ 0.105 , 0.34650]
4617 [ 0.120 , 0.42049]
4618 [ 0.135 , 0.50188]
4619 [ 0.186 , 0.60307]
4620 [ 2.110 , 0.79083]
4621 [ 5.874 , 1.00271]
4622 [ 11.395 , 1.29643]
4623 [ 18.770 , 1.62054]
4624 [ 28.143 , 1.97516]
4625 [ -1 , -1 ] (max twenty pts)
4626 NHYDovf=[ " Co- P- OVF" ]
4627 *%-----|-----
4628 ADD HYD NHYDsum=[ " corrig" ], NHYDs to
4629 add=[ " Co- P- OVF" + " Co- P" + " N_ TO" + " MHI05- JR" + " A8- M" + " JR" + " A9- M" + " A10- M" + " A11- M" + " A12- M" + " A
4630 13- M" ]
4631 *%-----|-----
4632 SAVE HYD NHYD=[ " corrig" ], # OF PCYCLES=[ -1], ICASEsh=[ 1]
4633 HYD_COMMENT=[ " Total Flows at Corrigan Pond" ]
4634 *%-----|-----
4635 *#*****

```

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4631  *#      Corrigan Pond 1
4632  *#      - Rating curve obtained from Barrhaven South M&S modeling
4633  *#      - Tributary Drainage Area to M&S Pond 1 = 145 ha
4634  *#*****
4635  *ROUTE RESERVOIR      NHYDout=[ "M&S_P1" ],  NHYDin=[ "CORRIG" ],
4636  *                      RDT=[ 1 ] ( mi n ),
4637  *                      TABLE of ( OUTFLOW STORAGE ) values
4638  *                      ( cms ) - ( ha - m )
4639  *                      [ 0.0 , 0.0 ]
4640  *                      [ 0.06 , 0.58 ]
4641  *                      [ -1 , -1 ] (max twenty pts)
4642  *                      NHYDovf=[ "P1-OVF" ]
4643  *%-----|-----|
4644  *ADD HYD              NHYDsum=[ "SN_CO" ], NHYDs to add=[ "N_TO"+"P1-OVF"+"M&S_P1" ]
4645  *%-----|-----|
4646  *SAVE HYD            NHYD=[ "SN_CO" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
4647  *                      HYD_COMMENT=[ "Total Flows at Corrigan Drain" ]
4648  *%-----|-----|
4649  *#
4650  *# Hydrograph from Corrigan Drain routed to Jockvale Road
4651  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
4652  *#
4653  ROUTE CHANNEL      NHYDout=[ "N_M" ] , NHYDin=[ "corrig" ] ,
4654  RDT=[ 1 ] ( mi n ),
4655  CHLGTH=[ 580 ] ( m ),  CHSLOPE=[ 0.4448 ] ( % ),
4656  FPSLOPE=[ 0.4448 ] ( % ),
4657  SECNUM=[ 1.0 ],      NSEG=[ 3 ]
4658  ( SEGROUGH, SEGDI ST ( m ) ) =
4659  [ 0.075, -17.72
4660  -0.045, 17.72
4661  0.075, 80.62 ] NSEG times
4662  ( DI STANCE ( m ), ELEVATI ON ( m ) ) =
4663  [ -83.32, 90.00 ]
4664  [ -81.36, 89.50 ]
4665  [ -79.12, 89.00 ]
4666  [ -76.13, 88.50 ]
4667  [ -20.46, 88.00 ]
4668  [ -19.36, 87.50 ]
4669  [ -18.51, 87.00 ]
4670  [ -17.72, 86.50 ]
4671  [ -11.95, 85.24 ]
4672  [ -0.11, 85.12 ]
4673  [ 11.49, 85.20 ]
4674  [ 17.72, 86.50 ]
4675  [ 19.74, 87.00 ]
4676  [ 21.22, 87.50 ]
4677  [ 22.68, 88.00 ]
4678  [ 24.28, 88.50 ]
4679  [ 26.79, 89.00 ]
4680  [ 71.98, 90.00 ]
4681  [ 80.62, 90.50 ]
4682  *%-----|-----|
4683  *#*****
4684  *#      Catchment MLLS
4685  *#      - To SWM Facility north of the Jock
4686  *#      - Primarily residential development
4687  *#*****
4688  CONTINUOUS STANDHYD NHYD=[ "MLLS" ], DT=[ 1 ] mi n, AREA=[ 175.99 ] ( ha ),
4689  XI MP=[ 0.38 ], TI MP=[ 0.38 ], DWF=[ 0 ] ( cms ), LOSS=[ 2 ],
4690  SCS curve number CN=[ 74 ],
4691  Pervious surfaces: I A per=[ 4.67 ] ( mm ), SLPP=[ 1 ] ( % ),
4692  LGP=[ 40 ] ( m ), MNP=[ 0.25 ], SCP=[ 0 ] ( mi n ),
4693  Impervious surfaces: I A i mp=[ 1.57 ] ( mm ), SLPI=[ 1 ] ( % ),
4694  LGI=[ 1118.123 ] ( m ), MNI=[ 0.013 ], SCI=[ 0 ] ( mi n ),
4695  Continuous simulation parameters:
4696  I a REC per=[ 4 ] ( hr s ), I a REC i mp=[ 4 ] ( hr s ),

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4697 SMN=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0. 010 ] / ( mm ) ,
4698 Inter Event Time=[ 18 ] ( hr s ) , END=- 1
4699 *%-----|-----|
4700 *#*****|
4701 *# Chapman Mills SWM Pond
4702 *# - Rating curve obtained from CCL hydraulic modeling
4703 *#*****|
4704 ROUTE RESERVOIR NHYDout =[ " M LL_P " ] , NHYDin =[ " M LLS " ] ,
4705 RDT=[ 1 ] ( mi n ) ,
4706 TABLE of ( OUTFLOW STORAGE ) values
4707 ( cms ) - ( ha- m)
4708 [ 0. 0 , 0. 0 ]
4709 [ 0. 01 , 0. 01 ]
4710 [ 0. 05 , 0. 06 ]
4711 [ 0. 09 , 0. 11 ]
4712 [ 0. 13 , 0. 15 ]
4713 [ 0. 18 , 0. 19 ]
4714 [ 0. 28 , 0. 28 ]
4715 [ 0. 37 , 0. 34 ]
4716 [ 0. 45 , 0. 40 ]
4717 [ 0. 51 , 0. 44 ]
4718 [ 0. 56 , 0. 47 ]
4719 [ 0. 64 , 0. 52 ]
4720 [ 0. 76 , 0. 59 ]
4721 [ 0. 86 , 0. 65 ]
4722 [ 1. 09 , 0. 78 ]
4723 [ 1. 44 , 0. 96 ]
4724 [ 3. 18 , 1. 84 ]
4725 [ 4. 05 , 2. 31 ]
4726 [ - 1 , - 1 ] ( max t went y pts)
4727 NHYDovf =[ " M L- OV " ]
4728 *%-----|-----|
4729 ADD HYD NHYDs um=[ " SN_M " ] , NHYDs to add=[ " N_M " + " M L- OV " + " M LL_P " ]
4730 *%-----|-----|
4731 SAVE HYD NHYD=[ " SN_M " ] , # OF PCYCLES=[ - 1 ] , I CASEs h=[ 1 ]
4732 HYD_COMMENT=[ " Tot al Fl ows at Jockvale Road " ]
4733 *%-----|-----|
4734 *#
4735 *# Hydrograph from Jockvale Road routed to Heart's Desire
4736 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 689
4737 *#
4738 ROUTE CHANNEL NHYDout =[ " N_DE " ] , NHYDin =[ " SN_M " ] ,
4739 RDT=[ 1 ] ( mi n ) ,
4740 CHLGTH=[ 1962 ] ( m ) , CHSLOPE=[ 0. 2227 ] ( % ) ,
4741 FPSLOPE=[ 0. 2227 ] ( % ) ,
4742 SECNUM=[ 1. 0 ] , NSEG=[ 3 ]
4743 ( SEGROUGH, SEGDI ST ( m ) ) =
4744 [ 0. 075 , - 17. 56
4745 - 0. 045 , 18. 27
4746 0. 075 , 32. 51 ] NSEG t i mes
4747 ( DI STANCE ( m ) , ELEVATI ON ( m ) ) =
4748 [ - 54. 07 , 85. 00 ]
4749 [ - 39. 43 , 84. 50 ]
4750 [ - 28. 30 , 84. 00 ]
4751 [ - 24. 12 , 83. 50 ]
4752 [ - 22. 30 , 83. 00 ]
4753 [ - 20. 55 , 82. 50 ]
4754 [ - 17. 56 , 82. 00 ]
4755 [ - 12. 63 , 81. 22 ]
4756 [ - 0. 11 , 80. 75 ]
4757 [ 11. 55 , 81. 22 ]
4758 [ 18. 27 , 82. 00 ]
4759 [ 19. 82 , 82. 50 ]
4760 [ 22. 48 , 83. 00 ]
4761 [ 27. 90 , 83. 50 ]
4762 [ 29. 31 , 84. 00 ]

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4763 [ 30.81, 84.50]
4764 [ 32.51, 85.00]
4765 *%-----|-----|
4766 *#*****|
4767 *# Catchment DESIRE
4768 *# - To Jock River (north of the Jock)
4769 *# - Rural-estate subdivision (Heart's Desire Community)
4770 *#*****|
4771 CONTINUOUS STANDHYD NHYD=["DESIRE"], DT=[ 1] mi n, AREA=[ 23.78]( ha),
4772 XI MP=[ 0.25], TI MP=[ 0.25], DWF=[ 0]( cms), LOSS=[ 2],
4773 SCS curve number CN=[ 77],
4774 Pervious surfaces: I A per=[ 4.67]( mm), SLPP=[ 1]( %),
4775 LGP=[ 40]( m), MNP=[ 0.25], SCP=[ 0]( mi n),
4776 Impervious surfaces: I A i mp=[ 1.57]( mm), SLPI=[ 1]( %),
4777 LGI=[ 400]( m), MNI=[ 0.013], SCI=[ 0]( mi n),
4778 Continuous simulation parameters:
4779 I a REC per=[ 4]( hrs), I a REC i mp=[ 4]( hrs),
4780 SM N=[ - 1]( mm), SMAX=[ - 1]( mm), SK=[ 0.010]/( mm),
4781 Inter Event Ti me=[ 18]( hrs), END=- 1
4782 *%-----|-----|
4783 *#*****|
4784 *# Catchment JOCKVA
4785 *# - To Jockvale SWM Facility
4786 *# - Residential development & golf course
4787 *# - JFSA 2021-01-11 update JOCKVA after updating CORRIG as per IBI GROUP, July 2008.
4788 *# JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two
areas JOCKVA and EX-LAND 32.5 ha as per IBI GROUP, July 2008.
4789 *#*****|
4790 CONTINUOUS STANDHYD NHYD=["JOCKVA"], DT=[ 1] mi n, AREA=[ 225.13]( ha),
4791 XI MP=[ 0.50], TI MP=[ 0.50], DWF=[ 0]( cms), LOSS=[ 2],
4792 SCS curve number CN=[ 74],
4793 Pervious surfaces: I A per=[ 4.67]( mm), SLPP=[ 1]( %),
4794 LGP=[ 40]( m), MNP=[ 0.25], SCP=[ 0]( mi n),
4795 Impervious surfaces: I A i mp=[ 1.57]( mm), SLPI=[ 1]( %),
4796 LGI=[ 1310.55]( m), MNI=[ 0.013], SCI=[ 0]( mi n),
4797 Continuous simulation parameters:
4798 I a REC per=[ 4]( hrs), I a REC i mp=[ 4]( hrs),
4799 SM N=[ - 1]( mm), SMAX=[ - 1]( mm), SK=[ 0.010]/( mm),
4800 Inter Event Ti me=[ 18]( hrs), END=- 1
4801 *%-----|-----|
4802 ADD HYD NHYDsum=["JOCKVA-TO"], NHYDsto
add=["EX-LAND-MN"+"JOCKVA"+"B2-M"+"B3-M"]
4803 *%-----|-----|
4804 SAVE HYD NHYD=["JOCKVA-TO"], # OF PCYCLES=[ - 1], I CASEsh=[ 1]
4805 HYD_COMMENT=["Total Flows at KB first pond"]
4806 *%-----|-----|
4807 *#*****|
4808 *# Jockvale SWM Facility
4809 *# - Rating curve obtained from Jockvale Servicing Study (CCL 1999)
4810 *#*****|
4811 ROUTE RESERVOIR NHYDout=["JOCK_P"], NHYDin=["JOCKVA-TO"],
4812 RDT=[ 1]( mi n),
4813 TABLE of ( OUTFLOW STORAGE ) values
4814 ( cms ) - ( ha - m)
4815 [ 0.0 , 0.0 ]
4816 [ 0.27 , 0.03]
4817 [ 0.28 , 0.55]
4818 [ 0.29 , 1.14]
4819 [ 0.30 , 1.80]
4820 [ 0.31 , 2.32]
4821 [ 1.12 , 2.87]
4822 [ 2.92 , 3.45]
4823 [ 4.64 , 4.07]
4824 [ 6.69 , 4.72]
4825 [ 9.02 , 5.39]
4826 [ 11.62 , 6.10]

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4827 [ 14.42 , 6.85]
4828 [ 17.45 , 7.62]
4829 [ 20.69 , 8.44]
4830 [ 24.08 , 9.28]
4831 [ 27.68 , 10.17]
4832 [ -1 , -1 ] (max twenty pts)
4833 NHYDovf=["JO-OVF"]
4834 *%-----|-----|
4835 ADD HYD NHYDs um=["SN_DE"], NHYDs to add=["N_DE"+"DESIRE"+"JO-OVF"+"JOCK_P"]
4836 *%-----|-----|
4837 SAVE HYD NHYD=["SN_DE"], # OF PCYCLES=[-1], ICASEsh=[1]
4838 HYD_COMMENT=["Total Flows at Heart's Desire"]
4839 *%-----|-----|
4840 *#
4841 *# Hydrograph from Heart's Desire routed to Rideau River
4842 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 0
4843 *#
4844 ROUTE CHANNEL NHYDout=["NI"], NHYDin=["SN_DE"],
4845 RDT=[1](min),
4846 CHLGTH=[563](m), CHSLOPE=[0.9668](%),
4847 FPSLOPE=[0.9668](%),
4848 SECNUM=[1.0], NSEG=[3]
4849 ( SEGROUGH, SEGDI ST (m))=
4850 [0.075, -30.20
4851 -0.045, 30.20
4852 0.075, 48.48] NSEG times
4853 ( DI STANCE (m), ELEVATI ON (m))=
4854 [-98.46, 81.50]
4855 [-92.24, 81.00]
4856 [-86.88, 80.50]
4857 [-81.54, 80.00]
4858 [-74.36, 79.50]
4859 [-63.54, 79.00]
4860 [-39.23, 78.50]
4861 [-34.51, 78.00]
4862 [-33.01, 77.50]
4863 [-30.20, 77.00]
4864 [-13.42, 76.18]
4865 [-1.14, 76.09]
4866 [17.06, 76.18]
4867 [30.20, 77.00]
4868 [32.95, 77.50]
4869 [34.06, 78.00]
4870 [35.11, 78.50]
4871 [36.32, 79.00]
4872 [37.74, 79.50]
4873 [48.48, 81.50]
4874 *%-----|-----|
4875 *#*****
4876 *# Catchment S-2
4877 *# - To Jock River (north and south)
4878 *# - Undeveloped floodplain and river
4879 *#*****
4880 CONTINUOUS NASHYD NHYD=["S-2"], DT=[1]min, AREA=[102.94](ha),
4881 DWF=[0](cms), CN/C=[72], IA=[4.67](mm),
4882 N=[3], TP=[0.40]hrs,
4883 Continuous simulation parameters:
4884 IaRECper=[4](hrs),
4885 SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4886 InterEventTime=[12](hrs)
4887 Baseflow simulation parameters:
4888 BaseFlowOption=[1],
4889 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
4890 VHydCond=[0.055](mm/hr), END=-1
4891 *%-----|-----|
4892 ADD HYD NHYDs um=["SN_NI"], NHYDs to add=["NI"+"S-2"]

```

```

4893 *%-----|-----|
4894 SAVE HYD          NHYD=["SN_NI"], # OF PCYCLES=[-1], ICASEs h=[1]
4895                  HYD_COMMENT=["Total Flows at Rideau River"]
4896 *%-----|-----|
4897 *#####
4898 *% 5 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4899 START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[5]
4900 *%              ["C24SC005.stm"] <--storm filename, one per line for NSTORMtime
4901 *%-----|-----|
4902 *% 10 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4903 START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[10]
4904 *%              ["C24SC010.stm"] <--storm filename, one per line for NSTORMtime
4905 *%-----|-----|
4906 *% 25 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4907 START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[25]
4908 *%              ["C24SC025.stm"] <--storm filename, one per line for NSTORMtime
4909 *%-----|-----|
4910 *% 50 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4911 START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[50]
4912 *%              ["C24SC050.stm"] <--storm filename, one per line for NSTORMtime
4913 *%-----|-----|
4914 *% 100 yr, 3 hr Chicago storm based on OTTAWA CDA IDF Curves
4915 *START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4916 *%              ["100YC3H.STM"] <--storm filename, one per line for NSTORMtime
4917 *%-----|-----|
4918 *% 100 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4919 START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4920 *%              ["C24SC100.stm"] <--storm filename, one per line for NSTORMtime
4921 *%-----|-----|
4922 *% 100 yr, 3 hr Chicago storm based on OTTAWA CDA IDF Curves
4923 *START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4924 *%              ["C24SC100.stm"] <--storm filename, one per line for NSTORMtime
4925 *START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[101]
4926 *%              ["A24SC100.stm"] <--storm filename, one per line for NSTORMtime
4927 *START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[102]
4928 *%              ["A24SC100_60.stm"] <--storm filename, one per line for NSTORMtime
4929 FINISH
4930

```

```

000011 *****
000012 ***** SWMM0 Ver 5.500 *****
000013 ***** A single event and continuous hydrologic simulation model *****
000014 ***** Based on the principles of HDM and its successors *****
000015 ***** CHTDMS 83 and OTTDMO 89 *****
000016 *****
000017 ***** Distributed by: J.F. Sabourin and Associates Inc. *****
000018 ***** Ottawa, Ontario: (613) 836-3884 *****
000019 ***** Gatineau, Quebec: (819) 243-6858 *****
000020 ***** E-Mail: jsabourin@jfas.com *****
000021 *****
000022 *****
000023 *****
000024 ***** Licensed user: JFSAi *****
000025 ***** Serial#: 2549237 *****
000026 *****
000027 *****
000028 *****
000029 ***** ***** PROGRAM ARRAY DIMENSIONS *****
000030 ***** Maximum value for 1D numbers: 11 *****
000031 ***** Maximum number of rainfall points: 105408 *****
000032 ***** Maximum number of flow points: 105408 *****
000033 *****
000034 *****
000035 ***** S U M M A R Y O U T P U T *****
000036 *****
000037 *****
000038 ***** RIN DATE: 2021-03-04 TIME: 11:49:14 RIN COUNTER: 002082 *****
000039 *****
000040 ***** Input file: T:\PROJ\1474-16\Design\20210304-QuantityControlAnalysis\SWMM0A.SMR.Model\update.d *****
000041 ***** 3\SMR_S-1-Fr-Nash.dat *****
000042 ***** 3\SMR_S-1-Fr-Nash.dat *****
000043 ***** 3\SMR_S-1-Fr-Nash.dat *****
000044 ***** Summary file: T:\PROJ\1474-16\Design\20210304-QuantityControlAnalysis\SWMM0A.SMR.Model\update.d *****
000045 ***** User comment: *****
000046 ***** 1: *****
000047 ***** 2: *****
000048 ***** 3: *****
000049 ***** 4: *****
000050 ***** *****
000051 *****
000052 *****
000053 ***** SWMM0 Ver 5.02/Jan 2001 BETA/ INPUT DATA FILE *****
000054 *****
000055 *****
000056 ***** Project Name: [Jock River] Project Number: [1474-16] *****
000057 ***** Date: [04-03-2021] *****
000058 ***** Modeler: [J.M.] *****
000059 ***** Company: [JFSAi] *****
000060 ***** License #: [2549237] *****
000061 *****
000062 ***** CALIBRATION OF SUMMER MODEL PARAMETERS *****
000063 ***** USING CONTINUOUS SIMULATIONS *****
000064 ***** Rainfall data from JFSAi raingage installed at site + other gauges by the City *****
000065 ***** Use data collected from May 1st to July 14, 2003 *****
000066 ***** 2020-11-30 change TMSD to a COMPLETE POLYD (TMSD=0.1 instead of 0.0001) *****
000067 ***** 2020-12-01 correct pond curve values *****
000068 ***** 2020-12-01 change W.C.LAR, BRG, SLP to 0.55, SLP=[0.5]%(impervious slope), and LGI up to 700m *****
000069 ***** 2021-02-19 Change the slope for ROUTE CHANNEL Station 2462 (NHDOut=[N_TOP], NHDIn=[SN_TOP]) from 0.03 % (as per S *****
000070 ***** 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (NHDOut=[N_TOP], NHDIn=[SN_TOP]) from 0.01 % (as per S *****
000071 ***** *****
000072 ***** ** END OF RIN: *****
000073 *****
000074 *****
000075 *****
000076 *****
000077 *****
000078 *****
000079 *****
000080 ***** RIN: COMAND *****
000081 ***** R0002: C0001 *****
000082 ***** START *****
000083 ***** [TZERO= 0 hrs on 0] *****
000084 ***** [METOUT= 2 (Imperial, 2 metric output)] *****
000085 ***** [EXTOR= 1] *****
000086 ***** [MNS= 0002] *****
000087 *****
000088 ***** SWMM0 Ver 5.02/Jan 2001 BETA/ INPUT DATA FILE *****
000089 *****
000090 *****
000091 ***** Project Name: [Jock River] Project Number: [1474-16] *****
000092 ***** Date: [04-03-2021] *****
000093 ***** Modeler: [J.M.] *****
000094 ***** Company: [JFSAi] *****
000095 ***** License #: [2549237] *****
000096 *****
000097 ***** CALIBRATION OF SUMMER MODEL PARAMETERS *****
000098 ***** USING CONTINUOUS SIMULATIONS *****
000099 ***** Rainfall data from JFSAi raingage installed at site + other gauges by the City *****
000100 ***** Use data collected from May 1st to July 14, 2003 *****
000101 ***** 2020-11-30 change TMSD to a COMPLETE POLYD (TMSD=0.1 instead of 0.0001) *****
000102 ***** 2020-12-01 correct pond curve values *****
000103 ***** 2020-12-01 change W.C.LAR, BRG, SLP to 0.55, SLP=[0.5]%(impervious slope), and LGI up to 700m *****
000104 ***** 2021-02-19 Change the slope for ROUTE CHANNEL Station 2462 (NHDOut=[N_TOP], NHDIn=[SN_TOP]) from 0.03 % (as per S *****
000105 ***** 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (NHDOut=[N_TOP], NHDIn=[SN_TOP]) from 0.01 % (as per S *****
000106 ***** R0002: C0002 *****
000107 ***** READ STORM *****
000108 ***** File name = storm001 *****
000109 ***** [SDF=10.00; SDR= 24.00; PFR= 45.51] *****
000110 *****
000111 ***** MOUFY STORM *****
000112 ***** [RFACT= 1.00; TSHF= 96.00 mm] *****
000113 ***** [SDF=10.00; SDR= 24.00; PFR= 45.51] *****
000114 ***** R0002: C0003 *****
000115 *****
000116 ***** REFLECT VALUES *****
000117 ***** File name = T:\PROJ\1474-16\Design\20210304-QuantityControlAnalysis\SWMM0A.SMR.Model\update.d\G11.Gate_DEF *****
000118 ***** [CNSave= 1 (read and print data) *****
000119 ***** File file comment: [Base onvarious calibration exercises in Onta *****
000120 ***** The FOLLOWING PARAMETERS ARE USED IN THE DESIGN STANDARD COM *****
000121 ***** Horton's infiltration equation on parameters *****
000122 ***** [In= 76.20 mm/hr] [C=13.20 mm/hr] [DCA= 4.14 hr] [P= .00 mm *****
000123 ***** Parameters for PERMANENT *****
000124 ***** [Lager= 4.67 mm] [LPS=50.00 mm] [MNS= 250] *****
000125 ***** Parameters for IMPROVISED surfaces in STANDARD *****
000126 ***** [L= 1.57 mm] [C= 1.50] [DCA= 0.13] *****
000127 ***** Parameters used in NASHID *****
000128 ***** [In= 76.20 mm/hr] *****
000129 ***** Average monthly Pan Evaporation data in (mm) *****
000130 ***** JAN FEB MAR APR MAY JUNE JUL AUG SEP OCT NOV DEC *****
000131 ***** 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *****
000132 ***** Average monthly Potential Evapotranspiration in (mm) *****
000133 ***** JAN FEB MAR APR MAY JUNE JUL AUG SEP OCT NOV DEC *****
000134 ***** 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *****
000135 ***** R0002: C0005 *****
000136 ***** COMPUTE API *****
000137 ***** [API= 50.00; APIKEY= 8500; APIKEY= 0980] *****
000138 ***** [API= 80.12; APIKEY= 56.74; APIKEY= 4.87] *****
000139 *****
000140 ***** The Tp was modified according to a Peak Reduction factor (MO Chart B2-4) *****
000141 ***** # of 1.32 *****
000142 ***** R0002: C0006 *****
000143 ***** CONTINUOUS NASHID 1.0 0.01: SW13 3680.00 6.204 No.date 37.06 11.47 252.00 *****
000144 ***** [Cns: 64.00; No: 3.00; Tps: 1.31] *****
000145 ***** [IaREC= 4.00; SM: 50.42; SMX=30.32; SK= 010] *****
000146 ***** [InterEventTime= 12.00] *****
000147 *****
000148 ***** The Tp was modified according to a Peak Reduction factor (MO Chart B2-4) *****
000149 ***** # of 1.32 *****
000150 ***** R0002: C0007 *****
000151 ***** CONTINUOUS NASHID 1.0 0.01: SW13 971.00 2.187 No.date 32.37 10.75 236.00 *****
000152 ***** [Cns: 64.00; No: 3.00; Tps: 1.31] *****
000153 ***** [IaREC= 4.00; SM: 64.50; SMX=430.01; SK= 010] *****
000154 ***** [InterEventTime= 12.00] *****
000155 *****
000156 ***** The Tp was modified according to a Peak Reduction factor (MO Chart B2-4) *****
000157 ***** # of 1.80 *****
000158 ***** R0002: C0008 *****
000159 ***** CONTINUOUS NASHID 1.0 0.01: SW13 3184.00 6.204 No.date 39.59 9.43 207.00 *****
000160 ***** [Cns: 55.00; No: 3.00; Tps: 1.31] *****
000161 ***** [IaREC= 4.00; SM: 50.42; SMX=554.96; SK= 010] *****
000162 ***** [InterEventTime= 12.00] *****
000163 ***** R0002: C0009 *****
000164 ***** CONTINUOUS NASHID 1.0 0.01: SW13 1781.00 5.504 No.date 32.45 13.94 306.00 *****
000165 ***** [Cns: 72.00; No: 3.00; Tps: 1.91] *****
000166 ***** [IaREC= 4.00; SM: 50.42; SMX=264.99; SK= 010] *****
000167 ***** [InterEventTime= 12.00] *****
000168 ***** R0002: C0010 *****
000169 ***** CONTINUOUS NASHID 1.0 0.01: SW13 500.00 4.042 No.date 34.34 11.98 263.00 *****
000170 ***** [Cns: 66.00; No: 3.00; Tps: 1.31] *****
000171 ***** [IaREC= 4.00; SM: 52.62; SMX=350.79; SK= 010] *****
000172 ***** [InterEventTime= 12.00] *****
000173 *****
000174 ***** The Tp was modified according to a Peak Reduction factor (MO Chart B2-4) *****
000175 ***** # of 1.80 *****
000176 ***** R0002: C0011 *****
000177 ***** CONTINUOUS NASHID 1.0 0.01: SW13 1917.00 4.042 No.date 34.34 11.98 263.00 *****
000178 ***** [Cns: 66.00; No: 3.00; Tps: 1.31] *****
000179 ***** [IaREC= 4.00; SM: 52.62; SMX=350.79; SK= 010] *****
000180 ***** [InterEventTime= 12.00] *****
000181 *****
000182 ***** The Tp was modified according to a Peak Reduction factor (MO Chart B2-4) *****
000183 ***** # of 1.32 *****
000184 ***** R0002: C0012 *****
000185 ***** CONTINUOUS NASHID 1.0 0.01: SW13 5666.00 11.228 No.date 38.07 13.94 306.00 *****
000186 ***** [Cns: 72.00; No: 3.00; Tps: 1.80] *****
000187 ***** [IaREC= 4.00; SM: 39.75; SMX=264.99; SK= 010] *****
000188 *****
000189 ***** [InterEventTime= 12.00] *****
000190 *****
000191 ***** The Tp was modified according to a Peak Reduction factor (MO Chart B2-4) *****
000192 ***** # of 1.32 *****
000193 ***** R0002: C0013 *****
000194 ***** CONTINUOUS NASHID 1.0 0.01: SW9 8376.00 11.072 No.date 39.59 11.98 263.00 *****
000195 ***** [Cns: 66.00; No: 3.00; Tps: 1.31] *****
000196 ***** [IaREC= 4.00; SM: 52.62; SMX=350.79; SK= 010] *****
000197 ***** [InterEventTime= 12.00] *****
000198 *****
000199 ***** The Tp was modified according to a Peak Reduction factor (MO Chart B2-4) *****
000200 ***** # of 1.68 *****
000201 ***** R0002: C0014 *****
000202 ***** CONTINUOUS NASHID 1.0 0.01: SW9 1132.00 4.434 No.date 30.58 13.35 293.00 *****
000203 ***** [Cns: 70.00; No: 3.00; Tps: 2.51] *****
000204 ***** [IaREC= 4.00; SM: 50.42; SMX=287.10; SK= 010] *****
000205 ***** [InterEventTime= 12.00] *****
000206 *****
000207 ***** The Tp was modified according to a Peak Reduction factor (MO Chart B2-4) *****
000208 ***** # of 1.82 *****
000209 ***** R0002: C0015 *****
000210 ***** CONTINUOUS NASHID 1.0 0.01: SW9 4464.00 5.504 No.date 39.59 10.98 241.00 *****
000211 ***** [Cns: 62.00; No: 3.00; Tps: 1.31] *****
000212 ***** [IaREC= 4.00; SM: 61.90; SMX=412.66; SK= 010] *****
000213 ***** [InterEventTime= 12.00] *****
000214 *****
000215 ***** The Tp was modified according to a Peak Reduction factor (MO Chart B2-4) *****
000216 ***** # of 1.50 *****
000217 ***** R0002: C0016 *****
000218 ***** CONTINUOUS NASHID 1.0 0.01: SW8 131.00 .805 No.date 28.57 11.22 247.00 *****
000219 ***** [Cns: 63.00; No: 3.00; Tps: 1.31] *****
000220 ***** [IaREC= 4.00; SM: 59.42; SMX=396.11; SK= 010] *****
000221 ***** [InterEventTime= 12.00] *****
000222 *****
000223 ***** The Tp was modified according to a Peak Reduction factor (MO Chart B2-4) *****
000224 ***** # of 1.65 *****
000225 ***** R0002: C0017 *****
000226 ***** CONTINUOUS NASHID 1.0 0.01: SW8 3854.00 6.242 No.date 38.40 11.98 263.00 *****
000227 ***** [Cns: 66.00; No: 3.00; Tps: 8.42] *****
000228 ***** [IaREC= 4.00; SM: 50.42; SMX=350.79; SK= 010] *****
000229 ***** [InterEventTime= 12.00] *****
000230 *****
000231 ***** The Tp was modified according to a Peak Reduction factor (MO Chart B2-4) *****
000232 ***** # of 1.82 *****
000233 ***** R0002: C0018 *****
000234 ***** CONTINUOUS NASHID 1.0 0.01: SW7 3197.00 4.651 No.date 36.31 9.85 217.00 *****
000235 ***** [Cns: 62.00; No: 3.00; Tps: 1.31] *****
000236 ***** [IaREC= 4.00; SM: 76.32; SMX=508.81; SK= 010] *****
000237 ***** [InterEventTime= 12.00] *****
000238 *****
000239 ***** The Tp was modified according to a Peak Reduction factor (MO Chart B2-4) *****
000240 ***** # of 1.38 *****
000241 ***** R0002: C0019 *****
000242 ***** CONTINUOUS NASHID 1.0 0.01: SW6 165.00 .413 No.date 33.07 12.24 269.00 *****
000243 ***** [Cns: 67.00; No: 3.00; Tps: 4.18] *****
000244 ***** [IaREC= 4.00; SM: 50.42; SMX=396.97; SK= 010] *****
000245 ***** [InterEventTime= 12.00] *****
000246 *****
000247 ***** The Tp was modified according to a Peak Reduction factor (MO Chart B2-4) *****
000248 ***** # of 1.67 *****
000249 ***** R0002: C0020 *****
000250 ***** CONTINUOUS NASHID 1.0 0.01: SW6 1332.00 3.148 No.date 35.23 13.94 306.00 *****
000251 ***** [Cns: 72.00; No: 3.00; Tps: 5.91] *****
000252 ***** [IaREC= 4.00; SM: 39.75; SMX=264.99; SK= 010] *****
000253 ***** [InterEventTime= 12.00] *****
000254 ***** R0002: C0021 *****
000255 ***** CONTINUOUS NASHID 1.0 0.01: SW5 224.00 2.597 No.date 28.45 15.91 350.00 *****
000256 ***** [Cns: 77.00; No: 3.00; Tps: 2.51] *****
000257 ***** [IaREC= 4.00; SM: 31.15; SMX=207.66; SK= 010] *****
000258 ***** [InterEventTime= 12.00] *****
000259 *****
000260 ***** The Tp was modified according to a Peak Reduction factor (MO Chart B2-4) *****
000261 ***** # of 1.32 *****
000262 ***** R0002: C0022 *****
000263 ***** CONTINUOUS NASHID 1.0 0.01: SW5 4945.00 14.839 No.date 33.25 14.57 320.00 *****
000264 ***** [Cns: 74.00; No: 3.00; Tps: 4.21] *****
000265 ***** [IaREC= 4.00; SM: 36.67; SMX=244.49; SK= 010] *****
000266 ***** [InterEventTime= 12.00] *****
000267 ***** R0002: C0023 *****
000268 ***** CONTINUOUS NASHID 1.0 0.01: SW5 20.00 .309 No.date 28.36 17.79 391.00 *****
000269 ***** [Cns: 81.00; No: 3.00; Tps: 6.2] *****
000270 ***** [IaREC= 4.00; SM: 25.21; SMX=168.09; SK= 010] *****
000271 ***** [InterEventTime= 12.00] *****
000272 *****
000273 ***** The Tp was modified according to a Peak Reduction factor (MO Chart B2-4) *****
000274 ***** # of 1.61 *****
000275 ***** R0002: C0024 *****
000276 ***** CONTINUOUS NASHID 1.0 0.01: SW5 1414.00 3.090 No.date 38.04 15.22 374.00 *****
000277 ***** [Cns: 75.00; No: 3.00; Tps: 8.01] *****
000278 ***** [IaREC= 4.00; SM: 33.81; SMX=225.43; SK= 010] *****
000279 ***** [InterEventTime= 12.00] *****
000280 ***** R0002: C0025 *****
000281 ***** CONTINUOUS NASHID 1.0 0.01: SW4 585.00 4.325 No.date 29.58 17.79 391.00 *****
000282 ***** [Cns: 81.00; No: 3.00; Tps: 5.91] *****
000283 ***** [IaREC= 4.00; SM: 25.21; SMX=168.09; SK= 010] *****
000284 ***** [InterEventTime= 12.00] *****
000285 ***** R0002: C0026 *****
000286 ***** CONTINUOUS NASHID 1.0 0.01: SW4 1021.00 5.747 No.date 30.50 17.39 382.00 *****
000287 ***** [Cns: 80.00; No: 3.00; Tps: 1.31] *****
000288 ***** [IaREC= 4.00; SM: 29.32; SMX=175.50; SK= 010] *****
000289 ***** [InterEventTime= 12.00] *****
000290 ***** R0002: C0027 *****
000291 ***** CONTINUOUS NASHID 1.0 0.01: SW2 177.00 2.052 No.date 28.45 15.91 350.00 *****
000292 ***** [Cns: 77.00; No: 3.00; Tps: 2.51] *****
000293 ***** [IaREC= 4.00; SM: 31.15; SMX=207.66; SK= 010] *****
000294 ***** [InterEventTime= 12.00] *****
000295 ***** R0002: C0028 *****
000296 ***** CONTINUOUS NASHID 1.0 0.01: SW1 1122.00 5.337 No.date 31.50 17.79 391.00 *****
000297 ***** [Cns: 81.00; No: 3.00; Tps: 1.31] *****
000298 ***** [IaREC= 4.00; SM: 25.21; SMX=168.09; SK= 010] *****
000299 ***** [InterEventTime= 12.00] *****
000300 ***** R0002: C0029 *****
000301 ***** CONTINUOUS NASHID 1.0 0.01: SW1 2737.00 11.528 No.date 31.35 15.56 342.00 *****
000302 ***** [Cns: 76.00; No: 3.00; Tps: 1.31] *****
000303 ***** [IaREC= 4.00; SM: 32.46; SMX=216.39; SK= 010] *****
000304 ***** [InterEventTime= 12.00] *****
000305 *****
000306 ***** Routing hydrographs *****
000307 ***** Starting with the addition of Jock River Headwater and Subwatershed 13 *****
000308 *****
000309 ***** R0002: C0030 *****
000310 ***** ADD HYD 1.0 0.02: SW1 8680.00 6.204 No.date 37.06 11.47 n/a 0.00 *****
000311 ***** [IaREC= 1.00] out c 1.0 0.02: SW13 971.00 2.187 No.date 32.37 10.75 n/a 0.00 *****
000312 ***** [IaREC= 1.00] out c 1.0 0.01: SW13 4651.00 7.871 No.date 35.37 11.32 n/a 0.00 *****
000313 ***** [IaREC= 1.00] out c 1.0 0.01: SW13 4651.00 6.238 No.date 39.59 11.32 n/a 0.00 *****
000314 ***** [IaREC= 1.00] out c 1.0 0.01: SW13 4651.00 6.238 No.date 39.59 11.32 n/a 0.00 *****
000315 ***** [IaREC= 1.00] out c 1.0 0.01: SW13 4651.00 6.238 No.date 39.59 11.32 n/a 0.00 *****
000316 ***** [IaREC= 1.00] out c 1.0 0.01: SW13 4651.00 6.238 No.date 39.59 11.32 n/a 0.00 *****
000317 ***** [IaREC= 1.00] out c 1.0 0.01: SW13 4651.00 6.238 No.date 39.59 11.32 n/a 0.00 *****
000318 ***** R0002: C0031 *****
000319 ***** ROUTE CHANNEL -> 1.0 0.02: SW13 4651.00 7.871 No.date 35.37 11.32 n/a 0.00 *****
000320 ***** [IaREC= 1.00] out c 1.0 0.01: SW13 4651.00 6.238 No.date 39.59 11.32 n/a 0.00 *****
000321 ***** [IaREC= 1.00] out c 1.0 0.01: SW13 4651.00 6.238 No.date 39.59 11.32 n/a 0.00 *****
000322 ***** [IaREC= 1.00] out c 1.0 0.01: SW13 4651.00 6.238 No.date 39.59 11.32 n/a 0.00 *****
000323 ***** [IaREC= 1.00] out c 1.0 0.01: SW13 4651.00 6.238 No.date 39.59 11.32 n/a 0.00 *****
000324 ***** [IaREC= 1.00] out c 1.0 0.01: SW13 4651.00 6.238 No.date 39.59 11.32 n/a 0.00 *****
000325 ***** [IaREC= 1.00] out c 1.0 0.01: SW13 4651.00 6.238 No.date 39.59 11.32 n/a 0.00 *****
000326 ***** R0002: C0032 *****
000327 ***** ADD HYD 1.0 0.02: SW1 3074.00 3.218 No.date 39.59 9.43 n/a 0.00 *****
000328 ***** [IaREC= 1.00] out c 1.0 0.02: SW1 3074.00 3.218 No.date 39.59 9.43 n/a 0.00 *****
000329 ***** [IaREC= 1.00] out c 1.0 0.01: SW13 7725.00 9.475 No.date 39.59 10.57 n/a 0.00 *****
000330 ***** [IaREC= 1.00] out c 1.0 0.01: SW13 7725.00 9.475 No.date 39.59 10.57 n/a 0.00 *****
000331 ***** [IaREC= 1.00] out c 1.0 0.01: SW1 7725.00 9.475 No.date 39.59 10.57 n/a 0.00 *****
000332 ***** [IaREC= 1.00] out c 1.0 0.01: SW1 7725.00 9.475 No.date 39.59 10.57 n/a 0.00 *****
000333 ***** R0002: C0033 *****
000334 ***** ROUTE RESERVOIR -> 1.0 0.02: SW13 7725.00 9.475 No.date 39.59 10.57 n/a 0.00 *****
000335 ***** [IaREC= 1.00] out c 1.0 0.01: RES. SW1 7725.00 9.475 No.date 39.59 10.57 n/a 0.00 *****
000336 ***** [IaREC= 1.00] out c 1.0 0.01: RES. SW1 7725.00 9.475 No.date 39.59 10.57 n/a 0.00 *****
000337 ***** [IaREC= 1.00] out c 1.0 0.01: RES. SW1 7725.00 9.475 No.date 39.59 10.57 n/a 0.00 *****
000338 ***** R0002: C0034 *****
000339 ***** SAVE HYD 1.0 0.01: RES. SW1 7725.00 9.475 No.date 39.59 10.57 n/a 0.00 *****
000340 ***** name: H.RESUM *****
000341 ***** remark: Outflow from Res. GM *****
000342 ***** Output of Reservoir Goodwood Msh routed from Node 13A to Node 12 *****
000343 ***** [Approximated cross-section - see cross-section 258] *****
000344 ***** Use no.04 for summer conditions and no.025 for spring conditions *****
000345 ***** R0002: C0035 *****
000346 ***** ADD HYD 1.0 0.02: SW1 7725.00 9.475 No.date 39.59 10.57 n/a 0.00 *****
000347 ***** [IaREC= 1.00] out c 1.0 0.01: SW1 7725.00 9.475 No.date 39.59 10.57 n/a 0.00 *****
000348 ***** [IaREC= 1.00] out c 1.0 0.01: SW1 7725.00 9.475 No.date 39.59 10.57 n/a 0.00 *****
000349 ***** [IaREC= 1.00] out c 1.0 0.01: SW1 7725.00 9.475 No.date 39.59 10.57 n/a 0.00 *****
000350 ***** [IaREC= 1.00] out c 1.0 0.01: SW1 7725.00 9.475 No.date 39.59 10.57 n/a 0.00 *****
000351 ***** R0002: C0036 *****
000352 ***** ADD HYD 1.0 0.02: SW1 7725.00 9.475 No.date 39.59 10.57 n/a 0.00 *****
000353 ***** [IaREC= 1.00] out c 1.0 0.01: SW1 7725.00 9.475 No.date 39.59 10.57 n/a 0.00 *****
000354 ***** [IaREC= 1.00] out c 1.0 0.01: SW1 7725.00 9.475 No.date 39.59 10.57 n/a 0.00 *****
000355 ***** [IaREC= 1.00] out c 1.0 0.01: SW1 7725.00 9.475 No.date 39.59 10.57 n/a 0.00 *****
000356 ***** [IaREC= 1.00] out c 1.0 0.01: SW1 7725.00 9.475 No.date 39.59 10.57 n/a 0.00 *****
000357 ***** R0002: C0037 *****
000358 ***** SAVE HYD 1.0 0.01: SW1 9506.00 7.458 No.date 32.50 11.20 n/a 0.00 *****
000359 ***** name: H.SW1 *****
000360 ***** remark: Flow at S_SW1 near Ashton *****
000361 *****
000362 ***** Sum of hydrographs from Node 12 routed to Node 11 *****
000363 ***** [Approximated cross-section - see cross-section 258] *****
000364 ***** Use no.04 for summer conditions and no.025 for spring conditions *****
000365 *****
000366 ***** Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248 *****
000367 *****
000368 ***** R0002: C0038 *****
000369 ***** ROUTE CHANNEL -> 1.0 0.02: SW12 9506.00 7.458 No.date 32.50 11.20 n/a 0.00 *****
000370 ***** [IaREC= 1.00] out c 1.0 0.01: SW12 9506.00 7.458 No.date 32.50 11.20 n/a 0.00 *****
000371 ***** [IaREC= 1.00] out c 1.0 0.01: SW12 9506.00 7.458 No.date 32.50 11.20 n/a 0.00 *****
000372 ***** [IaREC= 1.00] out c 1.0 0.01: SW12 9506.00 7.458 No.date 32.50 11.20 n/a 0.00 *****
000373 ***** [IaREC= 1.00] out c 1.0 0.01: SW12 9506.00 7.458 No.date 32.50 11.20 n/a 0.00 *****
000374 ***** [IaREC= 1.00] out c 1.0 0.01: SW12 9506.00 7.458 No.date 32.50 11.20 n/a 0.00 *****
000375 ***** [IaREC= 1.00] out c 1.0 0.01: SW12 9506.00 7.458 No.date 32.50 11.20 n/a 0.00 *****
000376 ***** [IaREC= 1.00] out c 1.0 0.01: SW12 9506.00 7.458 No.date 32.50 11.20 n/a 0.00 *****
000377 ***** [IaREC= 1.00] out c 1.0 0.01: SW12 9506.00 7.458 No.date 32.50 11.20 n/a 0.00 *****
000378 ***** [IaREC= 1.00] out c 1.0 0.01: SW12 9506.00 7.458 No.date 32.50 11.20 n/a 0.00 *****
000379 ***** [IaREC= 1.00] out c 1.0 0.01: SW12 9506.00 7.458 No.date 32.50 11.20 n/a 0.00 *****
000380 ***** [IaREC= 1.00] out c 1.0 0.01: SW12 9506.00 7.458 No.date 32.50 11.20 n/a 0.00 *****
000381 ***** [IaREC= 1.00] out c 1.0 0.01: SW12 9506.00 7.458 No.date 32.50 11.20 n/a 0.00 *****
000382 ***** [IaREC= 1.00] out c 1.0 0.01: SW12 9506.00 7.458 No.date 32.50 11.20 n/a 0.00 *****
000383 ***** [IaREC= 1.00] out c 1.0 0.01: SW12 9506.00 7.458 No.date 32.50 11.20 n/a 0.00 *****
000384 ***** [IaREC= 1.00] out c 1.0 0.01: SW12 9506.00 7.458 No.date 32.50 11.20 n/a 0.00 *****
000385 ***** [IaREC= 1.00] out c 1.0 0.01: SW12 9506.00 7.458 No.date 32.50 11.20 n/a 0.00 *****
000386 ***** [IaREC= 1.00] out c 1.0 0.01: SW12 9506.00 7.458 No.date 32.50 11.20 n/a 0.00 *****
000387 ***** [IaREC= 1.00] out c
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003755 #
003760 R0002: C00039 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
003770 ADD HYD + 1.0 02: DM1 9506.00 7.379 Ndate 33:12 11.30 n/a 0000
003780 ROUTE CHANNEL -> 1.0 02: S_N1 509.00 2.720 Ndate 29:22 11.98 n/a 0000
003790 + 1.0 02: NC CK 1917.00 4.042 Ndate 34:34 11.98 n/a 0000
003800 SIMM 1.0 01: S_N1 11923.00 12.077 Ndate 33:14 11.36 n/a 0000
003810 #
003820 # Sum of hydrographs from Node 11 routed to Node 10
003830 # Section 3
003840 #
003850 R0002: C00040 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
003860 ROUTE CHANNEL -> 1.0 02: S_N1 11923.00 12.077 Ndate 33:14 11.36 n/a 0000
003870 [RFD=1.00] out c 1.0 01: N10 11923.00 8.276 Ndate 39:46 11.36 n/a 0000
003880 [L/S= 4028.7 / 157.040]
003890 [Vmax =.462; Dmax= .886]
003900 #
003910 # Addition of Subwatershed 10 to Node 10
003920 #
003930 R0002: C00041 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
003940 ADD HYD + 1.0 02: N0 11923.00 8.276 Ndate 39:46 11.36 n/a 0000
003950 + 1.0 02: SW1 509.00 2.720 Ndate 29:22 11.98 n/a 0000
003960 SIMM 1.0 01: S_N0 17589.00 19.451 Ndate 38:31 12.19 n/a 0000
003970 R0002: C00042 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
003980 SAVE HYD 1.0 01: S_N0 17589.00 19.451 Ndate 38:31 12.19 n/a 0000
003990 frame :H_SND0
004000 remark:flow at S_N0: N0 + SW10
004010 # Addition of Kings Creek to S_N10
004020 #
004030 R0002: C00043 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
004040 ADD HYD + 1.0 02: N0 17589.00 19.451 Ndate 38:31 12.19 n/a 0000
004050 + 1.0 02: NC CK 8376.00 11.072 Ndate 39:59 11.98 n/a 0000
004060 SIMM 1.0 01: S_N0A 25965.00 30.328 Ndate 39:58 12.12 n/a 0000
004070 [L/S= 3982.073 / 137.640]
004080 [Vmax =.595; Dmax =1.208]
004090 #
004100 # Addition of Subwatershed 9 and Nchols Creek to Node 9
004110 #
004120 R0002: C00044 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
004130 ROUTE CHANNEL -> 1.0 01: N0 25965.00 29.579 Ndate 39:59 12.12 n/a 0000
004140 [RFD=1.00] out c 1.0 01: N0 25965.00 29.579 Ndate 39:59 12.12 n/a 0000
004150 [L/S= 3982.073 / 137.640]
004160 [Vmax =.595; Dmax =1.208]
004170 #
004180 # Addition of Subwatershed 9 and Nchols Creek to Node 9
004190 #
004200 R0002: C00045 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
004210 ADD HYD + 1.0 02: N0 25965.00 29.579 Ndate 39:59 12.12 n/a 0000
004220 + 1.0 02: SW 1132.00 4.434 Ndate 39:56 13.25 n/a 0000
004230 + 1.0 02: NC CK 4464.00 5.504 Ndate 39:59 10.98 n/a 0000
004240 SIMM 1.0 01: S_N0 31561.00 36.313 Ndate 39:59 12.00 n/a 0000
004250 [L/S= 3156.1 / 109.840]
004260 [Vmax =.418; Dmax =1.281]
004270 #
004280 # Addition of Subwatershed 8 and Hobb's Drain to Node 8
004290 #
004300 R0002: C00046 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
004310 ROUTE CHANNEL -> 1.0 02: S_N0 31561.00 36.313 Ndate 39:59 12.00 n/a 0000
004320 [RFD=1.00] out c 1.0 01: N0 31561.00 36.313 Ndate 39:59 12.00 n/a 0000
004330 [L/S= 2209.087 / 760.000]
004340 [Vmax =.418; Dmax =1.281]
004350 #
004360 # Addition of Subwatershed 8 and Hobb's Drain to Node 8
004370 #
004380 R0002: C00047 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
004390 ADD HYD + 1.0 02: N0 31561.00 36.313 Ndate 39:59 12.00 n/a 0000
004400 + 1.0 02: SW 131.00 0.805 Ndate 39:57 11.82 n/a 0000
004410 + 1.0 02: IB DR 3854.00 6.242 Ndate 38:46 11.98 n/a 0000
004420 SIMM 1.0 01: S_N0 35546.00 40.474 Ndate 39:59 12.00 n/a 0000
004430 [L/S= 3554.6 / 118.320]
004440 [Vmax =.208; Dmax =1.651]
004450 #
004460 # Sum of hydrographs from Node 8 routed to Node 7
004470 # Section 4
004480 #
004490 R0002: C00048 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
004500 ROUTE CHANNEL -> 1.0 02: S_N0 35546.00 40.474 Ndate 39:59 12.00 n/a 0000
004510 [RFD=1.00] out c 1.0 01: N0 35546.00 40.474 Ndate 39:59 12.00 n/a 0000
004520 [L/S= 3750.0 / 1250.000]
004530 [Vmax =.208; Dmax =1.651]
004540 #
004550 # Addition of Subwatershed 7 to Node 7
004560 #
004570 R0002: C00049 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
004580 ADD HYD + 1.0 02: N0 35546.00 40.474 Ndate 39:59 12.00 n/a 0000
004590 + 1.0 02: SW7 3197.00 4.651 Ndate 36:31 9.85 n/a 0000
004600 SIMM 1.0 01: S_N0 38743.00 35.071 Ndate 43:33 11.82 n/a 0000
004610 R0002: C00050 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
004620 SAVE HYD 1.0 01: S_N0 38743.00 35.071 Ndate 43:33 11.82 n/a 0000
004630 frame :H_SNT
004640 remark:flow at S_N0: N0 + SW7
004650 # Insertion of a Reservoir to simulate the effects of the Richmond Fen.
004660 # Storage area and volumes were estimated from available topo maps.
004670 # Release rate from fen was assumed to be controlled by the downstream
004680 # river cross section for various conditions. It is assumed that for up to
004690 # 0.75 m of water, the main channel of the river provided the storage. Above
004700 # this depth, the wetland stores a significantly store water.
004710 #
004720 R0002: C00051 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
004730 ROUTE RESERVOIR + 1.0 02: RES_RF 38743.00 35.071 Ndate 43:33 11.82 n/a 0000
004740 out c 1.0 01: RES_RF 38743.00 23.265 Ndate 55:09 11.82 n/a 0000
004750 [MSStok=4261E+01 mb, TotOfVol=,0000E+00 mb, NOfVol=,0. TotDrOf=,0.0]
004760 #
004770 R0002: C00052 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
004780 SAVE HYD 1.0 01: RES_RF 38743.00 23.265 Ndate 55:09 11.82 n/a 0000
004790 frame :H_RESRF
004800 remark:outflow of Richmond Fen
004810 #
004820 # Sum of hydrographs from Node 7 routed to Node 6
004830 # Section 5
004840 #
004850 R0002: C00053 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
004860 ROUTE CHANNEL -> 1.0 02: S_N0 38743.00 23.265 Ndate 55:09 11.82 n/a 0000
004870 [RFD=1.00] out c 1.0 01: N6 38743.00 23.228 Ndate 56:38 11.82 n/a 0000
004880 [L/S= 182.0 / 60.000]
004890 [Vmax =.432; Dmax =.808]
004900 #
004910 # Addition of Subwatershed 6 and Van Gual Drain to Node 6
004920 #
004930 R0002: C00054 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
004940 ADD HYD + 1.0 02: N6 38743.00 23.228 Ndate 56:38 11.82 n/a 0000
004950 + 1.0 02: SW4 20.00 .309 Ndate 28:36 17.79 n/a 0000
004960 + 1.0 02: NC CK 1332.00 3.148 Ndate 35:23 13.94 n/a 0000
004970 SIMM 1.0 01: S_N0 40240.00 23.318 Ndate 39:59 11.89 n/a 0000
004980 [L/S= 4024.0 / 133.200]
004990 [Vmax =.443; Dmax =.937]
005000 #
005010 # Addition of Subwatershed 5 and Flowing Creek to Node 5
005020 #
005030 R0002: C00055 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
005040 ROUTE CHANNEL -> 1.0 02: S_N0 40240.00 23.318 Ndate 39:59 11.89 n/a 0000
005050 [RFD=1.00] out c 1.0 01: N5A 40240.00 23.288 Ndate 56:09 11.89 n/a 0000
005060 [L/S= 182.0 / 60.000]
005070 [Vmax =.378; Dmax =.917]
005080 #
005090 # Addition of Subwatershed 5 and Flowing Creek to Node 5
005100 #
005110 R0002: C00056 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
005120 ADD HYD + 1.0 02: N5A 40240.00 23.288 Ndate 56:09 11.89 n/a 0000
005130 + 1.0 02: SW4 20.00 .309 Ndate 28:36 17.79 n/a 0000
005140 + 1.0 02: NC CK 1332.00 3.148 Ndate 35:23 13.94 n/a 0000
005150 SIMM 1.0 01: S_N0 40240.00 23.318 Ndate 39:59 11.89 n/a 0000
005160 [L/S= 4024.0 / 133.200]
005170 [Vmax =.443; Dmax =.937]
005180 #
005190 # Addition of Subwatershed 5A and Subwatershed 5A2 to Node 5A
005200 #
005210 R0002: C00057 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
005220 ROUTE CHANNEL -> 1.0 02: S_N0 45409.00 33.166 Ndate 37:08 12.20 n/a 0000
005230 [RFD=1.00] out c 1.0 01: N5A 45409.00 33.158 Ndate 37:20 12.20 n/a 0000
005240 [L/S= 556.0 / 190.040]
005250 [Vmax =.443; Dmax =.937]
005260 #
005270 # Addition of Subwatershed 4 and Leam Creek to Node 4
005280 # Section 8
005290 #
005300 R0002: C00058 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
005310 ADD HYD + 1.0 02: N5A 45409.00 33.158 Ndate 37:20 12.20 n/a 0000
005320 + 1.0 02: SW4 20.00 .309 Ndate 28:36 17.79 n/a 0000
005330 + 1.0 02: NC CK 1021.00 5.747 Ndate 30:50 17.30 n/a 0000
005340 SIMM 1.0 01: S_N0 48447.00 37.581 Ndate 38:13 12.47 n/a 0000
005350 [L/S= 4630.0 / 157.040]
005360 [Vmax =.695; Dmax =2.444]
005370 #
005380 # Addition of Subwatershed 2 with Mbohan Drain and Smith Drain to Node 2
005390 #
005400 R0002: C00059 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
005410 ADD HYD + 1.0 02: N5A 48447.00 37.581 Ndate 38:13 12.47 n/a 0000
005420 + 1.0 02: SW4 20.00 .309 Ndate 28:36 17.79 n/a 0000
005430 + 1.0 02: NC CK 1021.00 5.747 Ndate 30:50 17.30 n/a 0000
005440 SIMM 1.0 01: S_N0 48447.00 37.581 Ndate 38:13 12.47 n/a 0000
005450 [L/S= 4630.0 / 157.040]
005460 [Vmax =.715; Dmax =2.845]
005470 #
005480 # Addition of Subwatershed 2 with Mbohan Drain and Smith Drain to Node 2
005490 #
005500 R0002: C00060 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
005510 ADD HYD + 1.0 02: N5A 48447.00 37.581 Ndate 38:13 12.47 n/a 0000
005520 + 1.0 02: SW4 20.00 .309 Ndate 28:36 17.79 n/a 0000
005530 + 1.0 02: NC CK 1021.00 5.747 Ndate 30:50 17.30 n/a 0000
005540 SIMM 1.0 01: S_N0 48447.00 37.581 Ndate 38:13 12.47 n/a 0000
005550 [L/S= 4630.0 / 157.040]
005560 [Vmax =.715; Dmax =2.845]
005570 #
005580 # Addition of Subwatershed 2 with Mbohan Drain and Smith Drain to Node 2
005590 #
005600 R0002: C00061 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
005610 ADD HYD + 1.0 02: N5A 48447.00 37.581 Ndate 38:13 12.47 n/a 0000
005620 + 1.0 02: SW4 20.00 .309 Ndate 28:36 17.79 n/a 0000
005630 + 1.0 02: NC CK 1021.00 5.747 Ndate 30:50 17.30 n/a 0000
005640 SIMM 1.0 01: S_N0 48447.00 37.581 Ndate 38:13 12.47 n/a 0000
005650 [L/S= 4630.0 / 157.040]
005660 [Vmax =.715; Dmax =2.845]

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005625 + 1.0 02: SW2 177.00 2.052 Ndate 28:45 15.91 n/a 0000
005635 + 1.0 02: SW1R 1122.00 5.337 Ndate 31:50 17.79 n/a 0000
005645 + 1.0 02: MDLR 2737.00 11.528 Ndate 31:35 15.56 n/a 0000
005655 SIMM 52483.00 46.294 Ndate 33:32 12.76 n/a 0000
005665 R0002: C00064 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
005675 SAVE HYD 1.0 01: S_N2 52483.00 46.294 Ndate 33:33 12.76 n/a 0000
005685 frame :H_SND2
005695 remark:flow at S_N2 Lock River Gauge at Modoc Dr.
005700 #
005710 # Sum of hydrographs from Node 2 routed to Node 1
005720 # Section 10
005730 #
005740 #
005750 # Hydrograph from Node 2 routed to Node 416
005760 # Channel X-Section obtained from RVCA Hydraulic Model - Station 9025
005770 #
005780 R0002: C00065 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
005790 ROUTE CHANNEL -> 1.0 02: S_N2 52483.00 46.294 Ndate 33:32 12.76 n/a 0000
005800 [RFD=1.00] out c 1.0 01: N416 52483.00 45.431 Ndate 35:37 12.76 n/a 0000
005810 [L/S= 3227.0 / 1050.050]
005820 [Vmax =.577; Dmax =2.212]
005830 #
005840 # Catchment SW1a
005850 # Portion of RVCA catchment SW1 outside of Reach 1 subwatershed
005860 # Undeveloped agricultural land
005870 #
005880 CONTINUES NASHDD 1.0 01: S_Sw1a 536.42 1.885 Ndate 31:21 13.01 286 0000
005890 [L/REC= 4.00; SM=N=39.75; SMAX=264.99; SK= .010]
005900 [InterEvent Time= 12.00]
005910 #
005920 R0002: C00067 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
005930 ADD HYD + 1.0 02: S_N2 52483.00 45.431 Ndate 35:37 12.76 n/a 0000
005940 + 1.0 02: SW1 536.42 1.885 Ndate 31:21 13.01 n/a 0000
005950 + 1.0 02: S1+Keeffe 44.93 .373 Ndate 29:09 14.83 326 0000
005960 SIMM 53064.36 46.600 Ndate 35:34 12.76 n/a 0000
005970 [L/REC= 4.00; SM=N=31.15; SMAX=207.66; SK= .010]
005980 [InterEvent Time= 12.00]
005990 #
006000 R0002: C00068 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
006010 ADD HYD + 1.0 02: S_N2 52483.00 45.431 Ndate 35:37 12.76 n/a 0000
006020 + 1.0 02: SW1 536.42 1.885 Ndate 31:21 13.01 n/a 0000
006030 + 1.0 02: S1+Keeffe 44.93 .373 Ndate 29:09 14.83 326 0000
006040 SIMM 53064.36 46.600 Ndate 35:34 12.76 n/a 0000
006050 [L/REC= 4.00; SM=N=31.15; SMAX=207.66; SK= .010]
006060 [InterEvent Time= 12.00]
006070 #
006080 R0002: C00069 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
006090 SAVE HYD 1.0 01: S_N2 52483.00 45.431 Ndate 35:37 12.76 n/a 0000
006100 frame :SN_416_0002
006110 remark:Total Flow at Highway 416
006120 # Hydrograph from Node 416 routed to Node at Keeffe drain
006130 # Channel X-Section obtained from RVCA Hydraulic Model - Station 7245
006140 #
006150 R0002: C00070 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
006160 ROUTE CHANNEL -> 1.0 01: NOK 53064.36 46.592 Ndate 35:24 12.76 n/a 0000
006170 [RFD=1.00] out c 1.0 01: NOK 53064.36 46.592 Ndate 35:24 12.76 n/a 0000
006180 [L/S= 407.0 / 302.000]
006190 [Vmax =1.190; Dmax =1.879]
006200 #
006210 # Catchment QKEEFE
006220 # To Q Keeffe drain (north of the Lock)
006230 #
006240 CONTINUES NASHDD 1.0 01: O1 63.72 .305 Ndate 28:59 9.62 n/a 0000
006250 [L/REC= 4.00; SM=N=76.32; SMAX=508.81; SK= .010]
006260 [InterEvent Time= 12.00]
006270 #
006280 R0002: C00071 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
006290 ADD HYD + 1.0 02: S_N2 52483.00 45.431 Ndate 35:37 12.76 n/a 0000
006300 + 1.0 02: SW1 536.42 1.885 Ndate 31:21 13.01 n/a 0000
006310 + 1.0 02: S1+Keeffe 44.93 .373 Ndate 29:09 14.83 326 0000
006320 SIMM 53064.36 46.600 Ndate 35:34 12.76 n/a 0000
006330 [L/REC= 4.00; SM=N=31.15; SMAX=207.66; SK= .010]
006340 [InterEvent Time= 12.00]
006350 #
006360 R0002: C00072 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
006370 ROUTE CHANNEL -> 1.0 02: O1 63.72 .305 Ndate 28:59 9.62 n/a 0000
006380 [RFD=1.00] out c 1.0 01: O1R 63.72 .272 Ndate 29:20 9.62 n/a 0000
006390 [L/S= 960.0 / 630.040]
006400 [Vmax =.589; Dmax =2.121]
006410 #
006420 R0002: C00073 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
006430 CONTINUES NASHDD 1.0 01: O2 28.61 .110 Ndate 29:14 9.11 200 0000
006440 [L/REC= 4.00; SM=N=76.32; SMAX=508.81; SK= .010]
006450 [InterEvent Time= 12.00]
006460 #
006470 R0002: C00074 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
006480 ADD HYD + 1.0 02: O1R 63.72 .272 Ndate 29:20 9.62 n/a 0000
006490 + 1.0 02: O2 28.61 .110 Ndate 29:14 9.11 200 0000
006500 + 1.0 02: O1R 63.72 .272 Ndate 29:20 9.62 n/a 0000
006510 SIMM 46.94 .126 Ndate 29:02 7.06 155 0000
006520 [L/REC= 4.00; SM=N=104.59; SMAX=697.25; SK= .010]
006530 [InterEvent Time= 12.00]
006540 #
006550 R0002: C00075 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
006560 ADD HYD + 1.0 02: O1R 63.72 .272 Ndate 29:20 9.62 n/a 0000
006570 + 1.0 02: O2 28.61 .110 Ndate 29:14 9.11 200 0000
006580 + 1.0 02: O1R 63.72 .272 Ndate 29:20 9.62 n/a 0000
006590 SIMM 46.94 .126 Ndate 29:02 7.06 n/a 0000
006600 [L/REC= 4.00; SM=N=104.59; SMAX=697.25; SK= .010]
006610 [InterEvent Time= 12.00]
006620 #
006630 R0002: C00076 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
006640 ROUTE CHANNEL -> 1.0 02: O1R 63.72 .272 Ndate 29:20 9.62 n/a 0000
006650 [RFD=1.00] out c 1.0 02: O1R 63.72 .272 Ndate 29:20 9.62 n/a 0000
006660 [L/S= 210.0 / 810.040]
006670 [Vmax =.210; Dmax =.810]
006680 #
006690 R0002: C00077 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
006700 CONTINUES NASHDD 1.0 01: O1 63.72 .272 Ndate 29:20 9.62 n/a 0000
006710 [L/REC= 4.00; SM=N=134.47; SMAX=896.47; SK= .010]
006720 [InterEvent Time= 12.00]
006730 #
006740 R0002: C00078 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
006750 ADD HYD + 1.0 02: O1R 63.72 .272 Ndate 29:20 9.62 n/a 0000
006760 + 1.0 02: O2 28.61 .110 Ndate 29:14 9.11 200 0000
006770 + 1.0 02: O1R 63.72 .272 Ndate 29:20 9.62 n/a 0000
006780 SIMM 46.94 .126 Ndate 29:02 7.06 n/a 0000
006790 [L/REC= 4.00; SM=N=104.59; SMAX=697.25; SK= .010]
006800 [InterEvent Time= 12.00]
006810 #
006820 R0002: C00079 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
006830 CONTINUES NASHDD 1.0 01: O1 63.72 .272 Ndate 29:20 9.62 n/a 0000
006840 [L/REC= 4.00; SM=N=134.47; SMAX=896.47; SK= .010]
006850 [InterEvent Time= 12.00]
006860 #
006870 R0002: C00080 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
006880 ADD HYD + 1.0 02: O1R 63.72 .272 Ndate 29:20 9.62 n/a 0000
006890 + 1.0 02: O2 28.61 .110 Ndate 29:14 9.11 200 0000
006900 + 1.0 02: O1R 63.72 .272 Ndate 29:20 9.62 n/a 0000
006910 SIMM 46.94 .126 Ndate 29:02 7.06 n/a 0000
006920 [L/REC= 4.00; SM=N=104.59; SMAX=697.25; SK= .010]
006930 [InterEvent Time= 12.00]
006940 #
006950 R0002: C00081 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
006960 CONTINUES NASHDD 1.0 01: O1 63.72 .272 Ndate 29:20 9.62 n/a 0000
006970 [L/REC= 4.00; SM=N=134.47; SMAX=896.47; SK= .010]
006980 [InterEvent Time= 12.00]
006990 #
007000 R0002: C00082 -> Dfm=1D NDD -> AREA= QPEAKm TpeakDate hh:mm -> Rvmm R C -> Dwfcm
007010 ADD HYD + 1.0 02: O1R 63.72 .272 Ndate 29:20 9.62 n/a 0000
007020 + 1.0 02: O2 28.61 .110 Ndate 29:14 9.11 200 0000
007030 + 1.0 02: O1R 63.72 .272 Ndate 29:20 9.62 n/a 0
```


02993	SUM	1.0 01:5_NDA	25965.00	44.722	No.date	39:35	17.37	n/a	.000
02994	Sum of hydrographs from Node 10 routed to Node 9								
02995	Section 2								
02996	ROUTE CHANNEL ->	1.0 02:5_NDA	25965.00	44.722	No.date	39:35	17.37	n/a	.000
02997	[RFD=1.00] out c.	1.0 01:1_ND	25965.00	43.534	No.date	39:59	17.37	n/a	.000
02998	[L/S= 3982 / 0.71 / 0.01]	1.0 01:1_ND	25965.00	43.534	No.date	39:59	17.37	n/a	.000
03000	[Vmax =.664;Dmax=1.502]								
03003	03004# Addition of Subwatershed 9 and Nichols Creek to Node 9								
03005	ROUTE CHANNEL ->	1.0 02:5_NDA	25965.00	44.722	No.date	39:35	17.37	n/a	.000
03006	ADD HYD +	1.0 02:2_ND	25965.00	43.534	No.date	39:59	17.37	n/a	.000
03008	+ 1.0 02:5_NDA	1132.00	6.963	No.date	30:55	19.24	18.32	n/a	.000
03009	+ 1.0 02:1_ND	4164.00	8.109	No.date	39:59	15.66	n/a	.000	
03010	SUM	1.0 01:5_ND	35546.00	53.366	No.date	39:59	17.20	n/a	.000
03011	Section 3								
03012	ROUTE CHANNEL ->	1.0 02:5_ND	31561.00	53.366	No.date	39:59	17.20	n/a	.000
03013	[RFD=1.00] out c.	1.0 01:1_ND	31561.00	49.404	No.date	39:59	17.20	n/a	.000
03014	[L/S= 2609 / 0.86]	1.0 01:1_ND	31561.00	49.404	No.date	39:59	17.20	n/a	.000
03015	[Vmax =.370;Dmax=1.520]								
03020	03021# Addition of Subwatershed 8 and Hibb's Drain to Node 8								
03022	ROUTE CHANNEL ->	1.0 02:5_ND	31561.00	53.366	No.date	39:59	17.20	n/a	.000
03023	ADD HYD +	1.0 02:2_ND	31561.00	49.404	No.date	39:59	17.20	n/a	.000
03024	+ 1.0 02:5_ND	3197.00	7.027	No.date	36:28	13.89	n/a	.000	
03026	+ 1.0 02:1_ND	3554.00	9.385	No.date	38:41	17.18	n/a	.000	
03027	SUM	1.0 01:5_ND	38546.00	58.845	No.date	39:59	17.18	n/a	.000
03028	Section 4								
03029	ROUTE CHANNEL ->	1.0 02:5_ND	35546.00	58.845	No.date	39:59	17.19	n/a	.000
03030	[RFD=1.00] out c.	1.0 01:1_ND	35546.00	48.127	No.date	45:08	17.19	n/a	.000
03031	[L/S= 3750 / .053 / 0.070]	1.0 01:1_ND	35546.00	48.127	No.date	45:08	17.19	n/a	.000
03032	[Vmax =.208;Dmax=1.855]								
03037	03038# Addition of Subwatershed 7 to Node 7								
03039	ROUTE CHANNEL ->	1.0 02:5_ND	35546.00	58.845	No.date	39:59	17.19	n/a	.000
03040	ADD HYD +	1.0 02:2_ND	35546.00	48.127	No.date	45:08	17.19	n/a	.000
03042	+ 1.0 02:5_ND	3197.00	7.027	No.date	36:28	13.89	n/a	.000	
03043	+ 1.0 01:5_ND	3873.00	51.395	No.date	44:14	16.92	n/a	.000	
03044	SUM	1.0 01:5_ND	38743.00	51.395	No.date	44:14	16.92	n/a	.000
03045	SAVE HYD	1.0 01:5_ND	38743.00	51.395	No.date	44:14	16.92	n/a	.000
03046	name :JRSNT								
03047	remark:flow at S_ND: No SW7								
03048	Insertion of a reservoir to simulate the effects of the Richmond Fen.								
03049	Storage area and volume were estimated from available topographic data.								
03050	Release rate from Fen was assumed to be controlled by the downstream								
03051	river cross section for submerg conditions. It is assumed that for up to								
03052	0.75 m of water, the main channel of the river provided the storage. Above								
03053	this depth, the wetland stands to significantly store water.								
03054	Section 5								
03055	ROUTE CHANNEL ->	1.0 02:5_ND	38743.00	51.395	No.date	39:59	17.19	n/a	.000
03056	ADD HYD +	1.0 02:2_ND	38743.00	48.127	No.date	45:08	17.19	n/a	.000
03057	+ 1.0 02:5_ND	3197.00	7.027	No.date	36:28	13.89	n/a	.000	
03058	+ 1.0 01:5_ND	3873.00	51.395	No.date	44:14	16.92	n/a	.000	
03059	SUM	1.0 01:5_ND	38743.00	51.395	No.date	44:14	16.92	n/a	.000
03060	SAVE HYD	1.0 01:5_ND	38743.00	51.395	No.date	44:14	16.92	n/a	.000
03061	name :JRESRF								
03062	remark:outflow of Richmond Fen								
03063	Section 6								
03064	ROUTE CHANNEL ->	1.0 02:5_ND	38743.00	51.395	No.date	39:59	17.19	n/a	.000
03065	[RFD=1.00] out c.	1.0 01:1_ND	38743.00	27.930	No.date	60:29	16.92	n/a	.000
03066	[L/S= 3056 / .082 / 0.051]	1.0 01:1_ND	38743.00	27.930	No.date	60:29	16.92	n/a	.000
03067	[Vmax =.460;Dmax=.895]								
03072	03073# Addition of Subwatershed 6 and Van Gaal Drain to Node 6								
03074	ROUTE CHANNEL ->	1.0 02:5_ND	38743.00	51.395	No.date	39:59	17.19	n/a	.000
03075	ADD HYD +	1.0 02:2_ND	38743.00	27.930	No.date	60:29	16.92	n/a	.000
03077	+ 1.0 02:5_ND	464.00	4.100	No.date	28:45	22.97	n/a	.000	
03078	+ 1.0 02:1_ND	1432.00	4.803	No.date	35:19	20.12	n/a	.000	
03079	+ 1.0 01:5_ND	1020.00	27.944	No.date	60:06	17.03	n/a	.000	
03080	SUM	1.0 01:5_ND	1020.00	27.944	No.date	60:06	17.03	n/a	.000
03081	Section 7								
03082	ROUTE CHANNEL ->	1.0 02:5_ND	40240.01	27.944	No.date	60:06	17.03	n/a	.000
03083	[RFD=1.00] out c.	1.0 01:1_ND	40240.01	27.944	No.date	60:06	17.03	n/a	.000
03084	[L/S= 1852 / 0.54 / 0.051]	1.0 01:1_ND	40240.01	27.944	No.date	60:06	17.03	n/a	.000
03085	[Vmax =.397;Dmax=1.002]								
03089	03090# Addition of Subwatershed 5 and Flowing Creek to Node 5								
03091	ROUTE CHANNEL ->	1.0 02:5_ND	40240.01	27.944	No.date	60:06	17.03	n/a	.000
03092	ADD HYD +	1.0 02:2_ND	40240.01	27.944	No.date	60:06	17.03	n/a	.000
03093	+ 1.0 02:5_ND	224.00	4.100	No.date	28:45	22.97	n/a	.000	
03095	+ 1.0 02:1_ND	4945.00	22.837	No.date	33:22	21.04	n/a	.000	
03096	+ 1.0 01:5_ND	45409.01	43.566	No.date	35:28	17.49	n/a	.000	
03097	SUM	1.0 01:5_ND	45409.01	43.566	No.date	35:28	17.49	n/a	.000
03098	Section 8								
03099	ROUTE CHANNEL ->	1.0 02:5_ND	45409.01	43.566	No.date	35:28	17.49	n/a	.000
03100	[RFD=1.00] out c.	1.0 01:1_ND	45409.01	43.566	No.date	35:28	17.49	n/a	.000
03101	[L/S= 1607 / .060 / 0.040]	1.0 01:1_ND	45409.01	43.566	No.date	35:28	17.49	n/a	.000
03102	[Vmax =.465;Dmax=1.060]								
03107	03108# Addition of Subwatershed 5A and Subwatershed 5A2 to Node 5A								
03109	ROUTE CHANNEL ->	1.0 02:5_ND	45409.01	43.566	No.date	35:28	17.49	n/a	.000
03110	ADD HYD +	1.0 02:2_ND	45409.01	43.566	No.date	35:28	17.49	n/a	.000
03111	+ 1.0 02:5_ND	20.00	4.83	No.date	28:36	25.62	n/a	.000	
03112	+ 1.0 02:1_ND	1412.00	4.646	No.date	37:58	21.98	n/a	.000	
03113	+ 1.0 01:5_ND	40641.01	47.976	No.date	35:58	17.63	n/a	.000	
03114	SUM	1.0 01:5_ND	40641.01	47.976	No.date	35:58	17.63	n/a	.000
03115	Section 9								
03116	ROUTE CHANNEL ->	1.0 02:5_ND	46484.01	47.976	No.date	37:26	17.63	n/a	.000
03117	[RFD=1.00] out c.	1.0 01:1_ND	46484.01	46.217	No.date	37:26	17.63	n/a	.000
03118	[L/S= 4630 / .041 / 0.051]	1.0 01:1_ND	46484.01	46.217	No.date	37:26	17.63	n/a	.000
03119	[Vmax =.756;Dmax=3.116]								
03123	03124# Addition of Subwatershed 4 and Leamy Creek to Node 4								
03125	ROUTE CHANNEL ->	1.0 02:5_ND	46484.01	47.976	No.date	37:26	17.63	n/a	.000
03126	ADD HYD +	1.0 02:2_ND	46484.01	46.217	No.date	37:26	17.63	n/a	.000
03128	+ 1.0 02:5_ND	585.00	6.888	No.date	29:57	25.62	n/a	.000	
03129	+ 1.0 02:1_ND	1021.00	8.861	No.date	30:48	25.07	n/a	.000	
03130	+ 1.0 01:5_ND	48447.00	50.308	No.date	36:47	17.89	n/a	.000	
03131	SUM	1.0 01:5_ND	48447.00	50.308	No.date	36:47	17.89	n/a	.000
03132	SAVE HYD	1.0 01:5_ND	48447.00	50.308	No.date	36:47	17.89	n/a	.000
03133	name :SFL at N_005								
03134	remark:flow at N_005								
03135	Section 10								
03136	ROUTE CHANNEL ->	1.0 02:5_ND	48447.00	50.308	No.date	36:47	17.89	n/a	.000
03137	[RFD=1.00] out c.	1.0 01:1_ND	48447.00	50.308	No.date	36:47	17.89	n/a	.000
03138	[L/S= 1607 / .060 / 0.040]	1.0 01:1_ND	48447.00	50.308	No.date	36:47	17.89	n/a	.000
03139	[Vmax =.781;Dmax=3.131]								
03144	03145# Addition of Subwatershed 2 with Mhoanah Drain and Smith Drain to Node 2								
03146	ROUTE CHANNEL ->	1.0 02:5_ND	48447.00	50.308	No.date	36:47	17.89	n/a	.000
03147	ADD HYD +	1.0 02:2_ND	48447.00	50.308	No.date	36:47	17.89	n/a	.000
03148	+ 1.0 02:5_ND	177.00	3.240	No.date	28:45	22.97	n/a	.000	
03149	+ 1.0 02:1_ND	1123.00	8.165	No.date	31:48	25.62	n/a	.000	
03150	+ 1.0 01:5_ND	23748.00	17.869	No.date	31:33	17.63	n/a	.000	
03151	SUM	1.0 01:5_ND	24283.00	67.222	No.date	31:37	18.31	n/a	.000
03152	SAVE HYD	1.0 01:5_ND	24283.00	67.222	No.date	31:37	18.31	n/a	.000
03153	name :JRSNT								
03154	remark:flow at S_NJ Jock River Gauge at Montic Dr.								
03155	Section 11								
03156	ROUTE CHANNEL ->	1.0 02:5_ND	52483.00	67.222	No.date	33:17	18.31	n/a	.000
03157	[RFD=1.00] out c.	1.0 01:1_ND	52483.00	65.604					

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03367# R005:CO098.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03368# CNTLNXS STANHD 1.0 01:ST: 12.04 1.279 No.date 28:04 44.03 771 000
03369# [XmPm: 68;TlMm: 85]
03370# [Perivous area: IApr: 4.67;SLPP: 50;LGP: 50;MNP: 250;SCP: 0]
03371# [IAREC: 4.00;SM: 17.43;SMA: 16.21;SK: 010]
03372# [InterEventTime= 12.00]
03373# R005:CO099.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03374# CNTLNXS STANHD 1.0 01:ST: 12.04 1.279 No.date 28:04 44.03 771 000
03375# [XmPm: 68;TlMm: 85]
03376# [Perivous area: IApr: 4.67;SLPP: 50;LGP: 50;MNP: 250;SCP: 0]
03377# [IAREC: 4.00;SM: 17.43;SMA: 16.21;SK: 010]
03378# [InterEventTime= 12.00]
03379# R005:CO100.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03380# ROUTE RESEVIR > 1.0 02:AT: 12.04 353 No.date 28:36 44.03 n/a 000
03381# out < 1.0 01:AT: 12.04 353 No.date 28:36 44.03 n/a 000
03382# overflow < 1.0 03:CF: 0.00 0.00 No.date 0:00 0.00 n/a 000
03383# [MSI:0tda: 2492E+00 mb, TotOfVol: 0.0000E+00 mb, N.Of: 0, TotDurOf: 0 hrs.]
03384# R005:CO101.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03385# CNTLNXS STANHD 1.0 01:ST: 5.30 6.71 No.date 28:02 33.25 582 000
03386# [XmPm: 46;TlMm: 57]
03387# [Perivous area: IApr: 7.20;FC: 13.20;ICAV: 14; Fe: 00]
03388# [Perivous area: IApr: 4.67;SLPP: 50;LGP: 50;MNP: 250;SCP: 0]
03389# [IAREC: 4.00;SM: 17.43;SMA: 16.21;SK: 010]
03390# [InterEventTime= 12.00]
03391# R005:CO102.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03392# ROUTE RESEVIR > 1.0 02:AT: 12.04 353 No.date 28:02 33.25 n/a 000
03393# out < 1.0 01:AT: 12.04 353 No.date 28:02 33.25 n/a 000
03394# overflow < 1.0 03:CF: 0.00 0.00 No.date 0:00 0.00 n/a 000
03395# [MSI:0tda: 1040E+02 mb, TotOfVol: 0.0000E+00 mb, N.Of: 0, TotDurOf: 0 hrs.]
03396# R005:CO103.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03397# CNTLNXS STANHD 1.0 01:ST: 5.30 6.71 No.date 28:02 44.03 771 000
03398# [XmPm: 68;TlMm: 85]
03399# [Perivous area: IApr: 7.20;FC: 13.20;ICAV: 14; Fe: 00]
03400# [Perivous area: IApr: 4.67;SLPP: 50;LGP: 50;MNP: 250;SCP: 0]
03401# [IAREC: 4.00;SM: 17.43;SMA: 16.21;SK: 010]
03402# [InterEventTime= 12.00]
03403# R005:CO104.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03404# ROUTE RESEVIR > 1.0 02:AT: 5.30 6.71 No.date 28:31 44.03 n/a 000
03405# out < 1.0 01:AT: 5.30 6.71 No.date 28:31 44.03 n/a 000
03406# overflow < 1.0 03:CF: 0.00 0.00 No.date 0:00 0.00 n/a 000
03407# [MSI:0tda: 1108E+00 mb, TotOfVol: 0.0000E+00 mb, N.Of: 0, TotDurOf: 0 hrs.]
03408# R005:CO105.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03409# ADD IVD 1.0 02:BR: 330.34 2.842 No.date 29:16 17.68 n/a 000
03410# + 1.0 02: 2.28 0.05 No.date 29:05 23.49 n/a 000
03411# [Perivous area: IApr: 4.67;SLPP: 50;LGP: 50;MNP: 250;SCP: 0]
03412# + 1.0 02:AT: 3.41 45.0 No.date 28:01 44.03 n/a 000
03413# + 1.0 02:AT: 3.41 45.0 No.date 28:01 44.03 n/a 000
03414# + 1.0 02:ST: 4.45 0.04 No.date 28:03 33.25 n/a 000
03415# + 1.0 02:ST: 4.45 0.04 No.date 28:03 33.25 n/a 000
03416# + 1.0 02:ST: 4.45 0.04 No.date 28:03 33.25 n/a 000
03417# + 1.0 02:ST: 4.45 0.04 No.date 28:03 33.25 n/a 000
03418# SIM 1.0 01:PT: 330.31 3.317 No.date 28:57 16.79 n/a 000
03419# R005:CO106.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03420# ROUTE CHANNEL > 1.0 02:PT: 330.31 3.317 No.date 28:57 16.79 n/a 000
03421# [IAREC: 4.00;SM: 17.43;SMA: 16.21;SK: 010]
03422# [L/S= 525 / 2300 / 043]
03423# [Vms: 635;Dm: 79]
03424# R005:CO107.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03425# CNTLNXS NASHD 1.0 01:SI: 2.51 0.55 No.date 28:45 25.92 454 000
03426# [InterEventTime= 12.00]
03427# [IAREC: 4.00;SM: 17.43;SMA: 16.21;SK: 010]
03428# [InterEventTime= 12.00]
03429# R005:CO108.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03430# CNTLNXS STANHD 1.0 01:ST: 3.41 4.50 No.date 28:01 44.03 771 000
03431# [XmPm: 68;TlMm: 85]
03432# [Perivous area: IApr: 7.20;FC: 13.20;ICAV: 14; Fe: 00]
03433# [Perivous area: IApr: 4.67;SLPP: 50;LGP: 50;MNP: 250;SCP: 0]
03434# [IAREC: 4.00;SM: 17.43;SMA: 16.21;SK: 010]
03435# [InterEventTime= 12.00]
03436# R005:CO109.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03437# ROUTE RESEVIR > 1.0 02:AT: 3.41 4.50 No.date 28:01 44.03 n/a 000
03438# out < 1.0 01:AT: 3.41 4.50 No.date 28:01 44.03 n/a 000
03439# overflow < 1.0 03:CF: 0.00 0.00 No.date 0:00 0.00 n/a 000
03440# [MSI:0tda: 1212E+00 mb, TotOfVol: 0.0000E+00 mb, N.Of: 0, TotDurOf: 0 hrs.]
03441# R005:CO110.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03442# CNTLNXS STANHD 1.0 01:ST: 5.30 6.71 No.date 28:00 33.25 582 000
03443# [XmPm: 46;TlMm: 57]
03444# [Perivous area: IApr: 7.20;FC: 13.20;ICAV: 14; Fe: 00]
03445# [Perivous area: IApr: 4.67;SLPP: 50;LGP: 50;MNP: 250;SCP: 0]
03446# [IAREC: 4.00;SM: 17.43;SMA: 16.21;SK: 010]
03447# [InterEventTime= 12.00]
03448# R005:CO111.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03449# ROUTE RESEVIR > 1.0 02:ST: 4.45 0.04 No.date 28:00 33.25 n/a 000
03450# out < 1.0 01:ST: 4.45 0.04 No.date 28:00 33.25 n/a 000
03451# overflow < 1.0 03:ST: 0.00 0.00 No.date 0:00 0.00 n/a 000
03452# [MSI:0tda: 1108E+00 mb, TotOfVol: 0.0000E+00 mb, N.Of: 0, TotDurOf: 0 hrs.]
03453# R005:CO112.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03454# ADD IVD 1.0 02:BR: 330.31 3.191 No.date 29:19 17.68 n/a 000
03455# + 1.0 02: 0.55 0.05 No.date 28:45 25.92 n/a 000
03456# + 1.0 02:CI: 3.41 104 No.date 28:29 44.03 n/a 000
03457# + 1.0 02:CI: 3.41 104 No.date 28:29 44.03 n/a 000
03458# + 1.0 02:ST: 4.45 0.04 No.date 28:03 33.25 n/a 000
03459# + 1.0 02:ST: 4.45 0.04 No.date 28:03 33.25 n/a 000
03460# + 1.0 02:ST: 4.45 0.04 No.date 28:03 33.25 n/a 000
03461# SIM 1.0 01:ST: 330.31 3.317 No.date 29:13 17.14 n/a 000
03462# R005:CO113.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03463# CNTLNXS STANHD 1.0 01:ST: 3.41 4.50 No.date 28:12 42.86 750 000
03464# [XmPm: 64;TlMm: 85]
03465# [Perivous area: IApr: 7.20;FC: 13.20;ICAV: 14; Fe: 00]
03466# [Perivous area: IApr: 4.67;SLPP: 50;LGP: 50;MNP: 250;SCP: 0]
03467# [IAREC: 4.00;SM: 17.43;SMA: 16.21;SK: 010]
03468# [InterEventTime= 12.00]
03469# R005:CO114.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03470# ROUTE RESEVIR > 1.0 02:AT: 7.59 0.48 No.date 29:55 42.86 n/a 000
03471# out < 1.0 01:AT: 7.59 0.48 No.date 29:55 42.86 n/a 000
03472# overflow < 1.0 03:CF: 0.00 0.00 No.date 0:00 0.00 n/a 000
03473# [MSI:0tda: 2288E+00 mb, TotOfVol: 0.0000E+00 mb, N.Of: 0, TotDurOf: 0 hrs.]
03474# R005:CO115.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03475# ADD IVD 1.0 02:ST: 330.31 3.317 No.date 29:13 17.68 n/a 000
03476# + 1.0 02: 7.59 0.48 No.date 29:55 42.86 n/a 000
03477# + 1.0 02: 7.59 0.48 No.date 29:55 42.86 n/a 000
03478# SIM 1.0 01:SS: 364.27 3.358 No.date 29:13 17.68 n/a 000
03479# R005:CO116.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03480# SAVE IVD 1.0 01:SS: 364.27 3.358 No.date 29:13 17.68 n/a 000
03481# [XmPm: 64;TlMm: 85]
03482# [Perivous area: IApr: 7.20;FC: 13.20;ICAV: 14; Fe: 00]
03483# [Perivous area: IApr: 4.67;SLPP: 50;LGP: 50;MNP: 250;SCP: 0]
03484# [IAREC: 4.00;SM: 17.43;SMA: 16.21;SK: 010]
03485# [InterEventTime= 12.00]
03486# R005:CO117.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03487# CNTLNXS STANHD 1.0 01:ST: 66.75 5.433 No.date 28:11 42.06 756 000
03488# [XmPm: 64;TlMm: 80]
03489# [Perivous area: IApr: 7.20;FC: 13.20;ICAV: 14; Fe: 00]
03490# [Perivous area: IApr: 4.67;SLPP: 50;LGP: 50;MNP: 250;SCP: 0]
03491# [IAREC: 4.00;SM: 17.43;SMA: 16.21;SK: 010]
03492# [InterEventTime= 12.00]
03493# R005:CO118.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03494# [Perivous area: IApr: 7.20;FC: 13.20;ICAV: 14; Fe: 00]
03495# [Perivous area: IApr: 4.67;SLPP: 50;LGP: 50;MNP: 250;SCP: 0]
03496# [IAREC: 4.00;SM: 17.43;SMA: 16.21;SK: 010]
03497# [InterEventTime= 12.00]
03498# R005:CO119.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03499# [Perivous area: IApr: 7.20;FC: 13.20;ICAV: 14; Fe: 00]
03500# [Perivous area: IApr: 4.67;SLPP: 50;LGP: 50;MNP: 250;SCP: 0]
03501# [IAREC: 4.00;SM: 17.43;SMA: 16.21;SK: 010]
03502# [InterEventTime= 12.00]
03503# R005:CO120.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03504# ADD IVD 1.0 02:SS: 364.27 3.358 No.date 29:13 17.68 n/a 000
03505# + 1.0 02:SS: 66.75 5.433 No.date 28:11 42.06 n/a 000
03506# + 1.0 02:SS: 66.75 5.433 No.date 28:11 42.06 n/a 000
03507# SIM 1.0 01:PT: 431.02 3.613 No.date 29:19 21.45 n/a 000
03508# R005:CO121.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03509# CNTLNXS STANHD 1.0 01:ST: 1.87 2.60 No.date 28:01 44.03 771 000
03510# [Perivous area: IApr: 7.20;FC: 13.20;ICAV: 14; Fe: 00]
03511# [Perivous area: IApr: 4.67;SLPP: 50;LGP: 50;MNP: 250;SCP: 0]
03512# [IAREC: 4.00;SM: 17.43;SMA: 16.21;SK: 010]
03513# [InterEventTime= 12.00]
03514# R005:CO122.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03515# ROUTE RESEVIR > 1.0 02:CF: 1.87 2.60 No.date 28:01 44.03 n/a 000
03516# out < 1.0 01:CF: 1.87 2.60 No.date 28:01 44.03 n/a 000
03517# overflow < 1.0 03:CF: 0.00 0.00 No.date 0:00 0.00 n/a 000
03518# [MSI:0tda: 3924E+01 mb, TotOfVol: 0.0000E+00 mb, N.Of: 0, TotDurOf: 0 hrs.]
03519# R005:CO123.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03520# CNTLNXS STANHD 1.0 01:CF: 1.62 2.27 No.date 28:01 44.03 771 000
03521# [XmPm: 68;TlMm: 85]
03522# [Perivous area: IApr: 7.20;FC: 13.20;ICAV: 14; Fe: 00]
03523# [Perivous area: IApr: 4.67;SLPP: 50;LGP: 50;MNP: 250;SCP: 0]
03524# [IAREC: 4.00;SM: 17.43;SMA: 16.21;SK: 010]
03525# [InterEventTime= 12.00]
03526# R005:CO124.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03527# ROUTE RESEVIR > 1.0 02:CF: 1.62 2.27 No.date 28:01 44.03 n/a 000
03528# out < 1.0 01:CF: 1.62 2.27 No.date 28:01 44.03 n/a 000
03529# overflow < 1.0 03:CF: 0.00 0.00 No.date 0:00 0.00 n/a 000
03530# [MSI:0tda: 3391E+01 mb, TotOfVol: 0.0000E+00 mb, N.Of: 0, TotDurOf: 0 hrs.]
03531# R005:CO125.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03532# CNTLNXS STANHD 1.0 01:ST: 4.1 0.44 No.date 28:00 33.25 582 000
03533# [Perivous area: IApr: 7.20;FC: 13.20;ICAV: 14; Fe: 00]
03534# [Perivous area: IApr: 4.67;SLPP: 50;LGP: 50;MNP: 250;SCP: 0]
03535# [IAREC: 4.00;SM: 17.43;SMA: 16.21;SK: 010]
03536# [InterEventTime= 12.00]
03537# R005:CO126.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03538# ROUTE RESEVIR > 1.0 02:ST: 4.1 0.44 No.date 28:00 33.25 n/a 000
03539# out < 1.0 01:ST: 4.1 0.44 No.date 28:00 33.25 n/a 000
03540# overflow < 1.0 03:ST: 0.00 0.00 No.date 0:00 0.00 n/a 000
03541# [MSI:0tda: 1092E+02 mb, TotOfVol: 0.0000E+00 mb, N.Of: 0, TotDurOf: 0 hrs.]
03542# R005:CO127.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03543# ADD IVD 1.0 02:PT: 431.02 3.613 No.date 29:19 21.45 n/a 000
03544# + 1.0 02:CF: 0.00 0.00 No.date 0:00 0.00 n/a 000
03545# + 1.0 02:CF: 0.00 0.00 No.date 0:00 0.00 n/a 000
03546# + 1.0 02:CF: 0.00 0.00 No.date 0:00 0.00 n/a 000
03547# + 1.0 02:CF: 0.00 0.00 No.date 0:00 0.00 n/a 000
03548# + 1.0 02:ST: 4.1 0.44 No.date 28:03 33.25 n/a 000
03549# + 1.0 02:ST: 4.1 0.44 No.date 28:03 33.25 n/a 000
03550# SIM 1.0 01:PT: 434.92 3.684 No.date 29:13 21.64 n/a 000
03551# R005:CO128.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03552# ROUTE CHANNEL > 1.0 02:PT: 434.92 3.684 No.date 29:13 21.64 n/a 000
03553# [IAREC: 4.00;SM: 17.43;SMA: 16.21;SK: 010]
03554# [L/S= 460 / 043 / 035]
03555# [Vms: 603;Dm: 127]
03556# R005:CO129.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03557# CNTLNXS NASHD 1.0 01:SI-F: 5.11 0.66 No.date 29:11 21.69 380 000
03558# [InterEventTime= 12.00]
03559# [IAREC: 4.00;SM: 17.43;SMA: 16.21;SK: 010]
03560# [InterEventTime= 12.00]
03561# R005:CO130.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03562# ADD IVD 1.0 02:SS: 330.38 5.238 No.date 29:08 37.71 n/a 000
03563# + 1.0 02:SS: 330.38 5.238 No.date 29:08 37.71 n/a 000
03564# + 1.0 02:SS: 330.38 5.238 No.date 29:08 37.71 n/a 000
03565# SIM 1.0 01:SS: 330.38 5.238 No.date 29:08 37.71 n/a 000
03566# R005:CO131.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03567# SAVE IVD 1.0 01:SS: 330.38 5.238 No.date 29:08 37.71 n/a 000
03568# [XmPm: 68;TlMm: 85]
03569# [Perivous area: IApr: 7.20;FC: 13.20;ICAV: 14; Fe: 00]
03570# [Perivous area: IApr: 4.67;SLPP: 50;LGP: 50;MNP: 250;SCP: 0]
03571# [IAREC: 4.00;SM: 17.43;SMA: 16.21;SK: 010]
03572# [InterEventTime= 12.00]
03573# R005:CO132.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03574# ROUTE RESEVIR > 1.0 02:SS: 330.38 5.238 No.date 29:08 37.71 n/a 000
03575# out < 1.0 01:SS: 330.38 5.238 No.date 29:08 37.71 n/a 000
03576# overflow < 1.0 03:CF: 0.00 0.00 No.date 0:00 0.00 n/a 000
03577# [MSI:0tda: 500E+01 mb, TotOfVol: 0.0000E+00 mb, N.Of: 0, TotDurOf: 0 hrs.]
03578# R005:CO133.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03579# CNTLNXS STANHD 1.0 01:SI-F: 4.94 0.64 No.date 29:11 21.69 380 000
03580# [Perivous area: IApr: 7.20;FC: 13.20;ICAV: 14; Fe: 00]
03581# [Perivous area: IApr: 4.67;SLPP: 50;LGP: 50;MNP: 250;SCP: 0]
03582# [IAREC: 4.00;SM: 17.43;SMA: 16.21;SK: 010]
03583# [InterEventTime= 12.00]
03584# R005:CO134.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03585# ROUTE CHANNEL > 1.0 02:DE: 460.69 3.810 No.date 29:25 22.68 n/a 000
03586# [IAREC: 4.00;SM: 17.43;SMA: 16.21;SK: 010]
03587# [InterEventTime= 12.00]
03588# [L/S= 413 / 160 / 033]
03589# [Vms: 561;Dm: 82]
03590# R005:CO135.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03591# CNTLNXS NASHD 1.0 01:SI: 1.90 0.44 No.date 28:42 25.92 454 000
03592# [InterEventTime= 12.00]
03593# [IAREC: 4.00;SM: 17.43;SMA: 16.21;SK: 010]
03594# [InterEventTime= 12.00]
03595# R005:CO136.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03596# CNTLNXS NASHD 1.0 01:SI-F: 9.74 2.90 No.date 28:22 24.64 431 000
03597# [InterEventTime= 12.00]
03598# [IAREC: 4.00;SM: 17.43;SMA: 16.21;SK: 010]
03599# [InterEventTime= 12.00]
03600# R005:CO137.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03601# ROUTE RESEVIR > 1.0 01:SD: 9.74 0.32 No.date 32:11 24.64 n/a 000
03602# out < 1.0 01:SD: 9.74 0.32 No.date 32:11 24.64 n/a 000
03603# overflow < 1.0 03:CF: 0.00 0.00 No.date 0:00 0.00 n/a 000
03604# [MSI:0tda: 1260E+00 mb, TotOfVol: 0.0000E+00 mb, N.Of: 0, TotDurOf: 0 hrs.]
03605# R005:CO138.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03606# ADD IVD 1.0 02:SI: 4.90 0.44 No.date 28:42 25.92 n/a 000
03607# + 1.0 02:SI: 4.90 0.44 No.date 28:42 25.92 n/a 000
03608# + 1.0 01:PT: 472.33 3.863 No.date 29:44 22.75 n/a 000
03609# SIM 1.0 01:PT: 472.33 3.863 No.date 29:44 22.75 n/a 000
03610# R005:CO139.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03611# CNTLNXS STANHD 1.0 01:SI: 3.85 No.date 28:13 23.43 410 000
03612# [Perivous area: IApr: 7.20;FC: 13.20;ICAV: 14; Fe: 00]
03613# [Perivous area: IApr: 4.67;SLPP: 50;LGP: 50;MNP: 250;SCP: 0]
03614# [IAREC: 4.00;SM: 17.43;SMA: 16.21;SK: 010]
03615# [InterEventTime= 12.00]
03616# [L/S= 845 / 100 / 043]
03617# [Vms: 748;Dm: 430]
03618# R005:CO140.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03619# ADD IVD 1.0 02:SI: 10.67 3.85 No.date 28:13 23.43 n/a 000
03620# + 1.0 02:SI: 10.67 3.85 No.date 28:13 23.43 n/a 000
03621# + 1.0 02:SI: 10.67 3.85 No.date 28:13 23.43 n/a 000
03622# SIM 1.0 01:SI: 10.67 3.85 No.date 28:13 23.43 n/a 000
03623# R005:CO141.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03624# ROUTE CHANNEL > 1.0 02:SI: 483.00 3.921 No.date 29:44 22.75 n/a 000
03625# [IAREC: 4.00;SM: 17.43;SMA: 16.21;SK: 010]
03626# [InterEventTime= 12.00]
03627# [L/S= 1.00] out < 1.0 01:SI: 483.00 3.921 No.date 29:44 22.75 n/a 000
03628# [L/S= 1.00] out < 1.0 01:SI: 483.00 3.921 No.date 29:44 22.75 n/a 000
03629# [Vms: 748;Dm: 430]
03630# R005:CO142.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03631# CNTLNXS NASHD 1.0 01:SI: 5.00 3.00 No.date 28:04 23.43 410 000
03632# [InterEventTime= 12.00]
03633# [IAREC: 4.00;SM: 17.43;SMA: 16.21;SK: 010]
03634# [InterEventTime= 12.00]
03635# R005:CO143.....Dfma 1-D NND.....AREHA-QPEAKm-TpeakDte,hh:mm.....Rvmm R C.....Dfwmc
03636# ROUTE RESEVIR > 1.0 02:SI: 483.00 3.921 No.date 29:44 22.75 n/a 000
03637# out < 1.0 02:SI: 483.00 3.921 No.date 29:44 22.75 n/a 000
03638# overflow < 1.0 03:CF: 0.00 0.00 No.date 0:00 0.00 n/a 000
03639# [MSI:0tda: 153E+00 mb, TotOfVol: 0.0000E+00 mb, N.Of: 0, TotDurOf: 0 hrs.]
03640# R005:CO144
```

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037413 # remark Total Flow at Station 520 on Foster Drain
037428 # Hydrogram from Node at Foster Drain to Node at station 6016 (Jock River)
037433 # Channel X-Section obtained from RCHA Hydraulic Model - Station 520
037440 #
037450 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
037460 ROUTE CHANNEL -> 1.0 0:02:SN:FO 335.49 5.129 Ndate 29:14 37.23 n/a .000
037470 # [R/S= 1.00] out < 1.0 0:02:WCLAR 335.49 5.080 Ndate 29:32 37.23 n/a .000
037480 # [L/S= 860 / 587] 0:05]
037490 # [X/M= 1.20] Dmax= 4.0]
037500 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
037510 CONTINUS STANARD 1.0 0:01:1-D 14.96 .206 Ndate 29:05 21.69 380 .000
037520 # [C= 77.0 No. 3.00; Tpa= 1.0]
037530 # [AREC= 4.00; SMN= 31.15; SMM= 207.66; S&= 0.10]
037540 # [InterEvent Time= 12.00]
037550 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
037560 CONTINUS STANARD 1.0 0:01:1-D 5.27 .654 Ndate 28:00 42.00 735 .000
037570 # [X/M= 65; T/MP= 65]
037580 # [L/S= 2; C= 75.0]
037590 # [Impervious area: IApr= 4.67; SLP= 2.0; LG= 40; MPA= 250; SCP= 0]
037600 # [Impervious area: IApr= 1.57; SLP= 75; LG= 187; MN= 0.13; SCI= 0]
037610 # [AREC= 4.00; IAREP= 4.00]
037620 # [SM= 33.81; SMM= 225.43; S&= 0.10]
037630 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
037640 CONTINUS NASIDH 1.0 0:01:1-A 75.88 1.479 Ndate 28:37 21.69 380 .000
037650 # [C= 77.0 No. 3.00; Tpa= 1.0]
037660 # [AREC= 4.00; SMN= 31.15; SMM= 207.66; S&= 0.10]
037670 # [InterEvent Time= 12.00]
037680 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
037690 CONTINUS NASIDH 1.0 0:01:WCLAR 35.65 4.62 Ndate 29:11 21.69 380 .000
037700 # [C= 77.0 No. 3.00; Tpa= 1.0]
037710 # [AREC= 4.00; SMN= 31.15; SMM= 207.66; S&= 0.10]
037720 # [InterEvent Time= 12.00]
037730 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
037740 ADD HYD + 1.0 0:02:PO 5377.82 69.117 Ndate 34:07 18.36 n/a .000
037750 # + 1.0 0:02:WCLAR 5.00 3.22 Ndate 29:32 37.23 n/a .000
037760 # + 1.0 0:02:SR 73.29 1.101 Ndate 28:56 41.22 n/a .000
037770 # + 1.0 0:02:PIV 0.00 0.00 Ndate 0:00 0.00 n/a .000
037780 # + 1.0 0:02:WCLAR 35.65 4.62 Ndate 29:11 21.69 n/a .000
037790 # + 1.0 0:02:1-FO-F-D 14.96 .206 Ndate 29:05 21.69 n/a .000
037800 # + 1.0 0:02:1-D 5.27 .654 Ndate 28:00 42.00 n/a .000
037810 # + 1.0 0:02:1-A 75.88 1.479 Ndate 28:37 21.69 n/a .000
037820 # + 1.0 0:02:SN 54118.36 71.824 Ndate 33:59 18.52 n/a .000
037830 # + 1.0 0:02:SN 54118.36 71.824 Ndate 33:59 18.52 n/a .000
037840 # + 1.0 0:02:SN 54118.36 71.824 Ndate 33:59 18.52 n/a .000
037850 # [L/S= 159 / 082] 0:05]
037860 # [X/M= 1.00] Dmax= 4.0]
037870 #
037880 # remark Total Flow at Foster Drain
037897 # Hydrogram from Node at Foster Drain to Node at Cadwraig Road
037900 # Channel X-Section obtained from RCHA Hydraulic Model - Station 6016
037907 #
037910 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
037920 # ROUTE CHANNEL -> 1.0 0:02:SN:FO 54118.36 71.824 Ndate 33:59 18.52 n/a .000
037930 # [R/S= 1.00] out < 1.0 0:02:WCLAR 54118.36 71.824 Ndate 34:07 18.52 n/a .000
037940 # [L/S= 159 / 082] 0:05]
037950 # [X/M= 1.00] Dmax= 4.0]
037960 #
037970 # Catchment S-1
037980 # To Jock River (north and south of Jock)
037985 # Primarily agricultural fields; portion of sand quarry
037990 #
038000 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
038010 CONTINUS STANARD 1.0 0:01:1-D 55.36 1.342 Ndate 28:24 21.69 380 .000
038020 # [C= 77.0 No. 3.00; Tpa= 4.0]
038030 # [AREC= 4.00; SMN= 31.15; SMM= 207.66; S&= 0.10]
038040 # [InterEvent Time= 12.00]
038050 # # JFSA 2021-02-24 change the name from S-1-BDC3 to S-1-A and S-1-B. Change their TP values based on the new areas
038060 # # JFSA 2021-02-24 change the name from S-1-BDC3 to S-1-B. Change their TP values based on the new areas
038070 # # JFSA 2021-01-19, after adding Greenbank pond, "S-1-BDC3" is not existing anymore
038080 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
038090 CONTINUS STANARD 1.0 0:01:1-D 1.07 1.92 Ndate 28:00 37.26 654 .000
038100 # [C= 77.0 No. 3.00; Tpa= 1.0]
038110 # [AREC= 4.00; SMN= 31.15; SMM= 207.66; S&= 0.10]
038120 # [InterEvent Time= 12.00]
038130 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
038140 CONTINUS NASIDH 1.0 0:01:1-D 3.28 .042 Ndate 29:11 21.69 380 .000
038150 # [C= 77.0 No. 3.00; Tpa= 1.0]
038160 # [AREC= 4.00; SMN= 31.15; SMM= 207.66; S&= 0.10]
038170 # [InterEvent Time= 12.00]
038180 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
038190 CONTINUS NASIDH 1.0 0:01:1-D 12.84 .166 Ndate 29:11 21.69 380 .000
038200 # [C= 77.0 No. 3.00; Tpa= 1.0]
038210 # [AREC= 4.00; SMN= 31.15; SMM= 207.66; S&= 0.10]
038220 # [InterEvent Time= 12.00]
038230 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
038240 CONTINUS NASIDH 1.0 0:01:1-D 1.75 .023 Ndate 29:11 21.69 380 .000
038250 # [C= 77.0 No. 3.00; Tpa= 1.0]
038260 # [AREC= 4.00; SMN= 31.15; SMM= 207.66; S&= 0.10]
038270 # [InterEvent Time= 12.00]
038280 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
038290 CONTINUS NASIDH 1.0 0:01:1-D 2.03 .026 Ndate 29:11 21.69 380 .000
038300 # [C= 77.0 No. 3.00; Tpa= 1.0]
038310 # [AREC= 4.00; SMN= 31.15; SMM= 207.66; S&= 0.10]
038320 # [InterEvent Time= 12.00]
038330 # # Catchment WCLAR
038340 # To West Clarke Drive (south of the Jock)
038350 # Sub-area WCLAR 136.71 ha per Burhewson South MS
038360 # 2020-11-30 update CLARKE Tributary Drainage Area to = 121 ha based on P598(04)-11
038370 # 2020-11-30 update CLARKE Tributary Drainage Area to = 121 ha based on P598(04)-11
038380 #
038390 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
038400 CONTINUS STANARD 1.0 0:01:1-D 1.77 1.92 Ndate 28:00 37.26 654 .000
038410 # [C= 77.0 No. 3.00; Tpa= 1.0]
038420 # [AREC= 4.00; SMN= 31.15; SMM= 207.66; S&= 0.10]
038430 # [InterEvent Time= 12.00]
038440 # [Impervious area: IApr= 4.67; SLP= 2.0; LG= 40; MPA= 250; SCP= 0]
038450 # [Impervious area: IApr= 1.57; SLP= 75; LG= 109; MN= 0.13; SCI= 0]
038460 # [AREC= 4.00; IAREP= 4.00]
038470 # [SM= 33.81; SMM= 225.43; S&= 0.10]
038480 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
038490 ROUTE RESERVOIR -> 1.0 0:02:WCLAR 1.77 1.92 Ndate 28:00 37.26 n/a .000
038500 # out < 1.0 0:02:WCLAR 1.77 1.92 Ndate 28:00 37.26 n/a .000
038510 # [C= 77.0 No. 3.00; Tpa= 1.0]
038520 # [MS oled= 0.16E-04 mb, TotVol= 0.000E+00, No Of= 0, TotDurOf= 0 hrs.]
038530 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
038540 CONTINUS STANARD 1.0 0:01:WCLAR 119.40 10.597 Ndate 28:05 41.22 722 .000
038550 # [X/M= 60; T/MP= 65]
038560 # [L/S= 2; C= 75.0]
038570 # [Impervious area: IApr= 4.67; SLP= 2.0; LG= 40; MPA= 250; SCP= 0]
038580 # [Impervious area: IApr= 1.57; SLP= 75; LG= 892; MN= 0.13; SCI= 0]
038590 # [AREC= 4.00; IAREP= 4.00]
038600 # [SM= 33.81; SMM= 225.43; S&= 0.10]
038610 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
038620 ADD HYD + 1.0 0:02:WCLAR 119.40 10.597 Ndate 28:05 41.22 n/a .000
038630 # + 1.0 0:02:WCLAR 119.40 10.597 Ndate 28:05 41.22 n/a .000
038640 # + 1.0 0:02:WCLAR 119.40 10.597 Ndate 28:05 41.22 n/a .000
038650 # + 1.0 0:02:WCLAR 119.40 10.597 Ndate 28:05 41.22 n/a .000
038660 # + 1.0 0:02:WCLAR 119.40 10.597 Ndate 28:05 41.22 n/a .000
038670 # [name: WCLAR.0005]
038680 # remark Total Flow at West Clarke
038690 # West Clarke Pond 2
038700 # Wet Clark Pond
038710 # Wet Clark Pond obtained from Burhewson South MS modeling
038720 # Tributary Drainage Area to MS Pond = 241 ha
038730 #
038740 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
038750 ROUTE RESERVOIR -> 1.0 0:02:WCLAR 119.40 10.597 Ndate 28:05 41.22 n/a .000
038760 # out < 1.0 0:01:SR 119.40 1.795 Ndate 28:54 41.22 n/a .000
038770 # overflow < 1.0 0:02:PE-DW 0.00 0.00 Ndate 0:00 0.00 n/a .000
038780 # [MS oled= 0.06E+00 mb, TotVol= 0.000E+00, No Of= 0, TotDurOf= 0 hrs.]
038790 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
038800 CONTINUS STANARD 1.0 0:01:1-D 1.07 1.92 Ndate 28:00 37.26 654 .000
038810 # [C= 77.0 No. 3.00; Tpa= 1.0]
038820 # [AREC= 4.00; SMN= 31.15; SMM= 207.66; S&= 0.10]
038830 # [InterEvent Time= 12.00]
038840 # + 1.0 0:02:1-D 12.84 .166 Ndate 29:11 21.69 n/a .000
038850 # + 1.0 0:02:SR 73.29 1.101 Ndate 28:56 41.22 n/a .000
038860 # + 1.0 0:02:PIV 0.00 0.00 Ndate 0:00 0.00 n/a .000
038870 # + 1.0 0:02:SN 54118.36 71.824 Ndate 33:59 18.52 n/a .000
038880 # + 1.0 0:02:SN 54118.36 71.824 Ndate 33:59 18.52 n/a .000
038890 # + 1.0 0:02:SN 54118.36 71.824 Ndate 33:59 18.52 n/a .000
038900 # [L/S= 270 / 018] 0:05]
038910 # [X/M= 68; Dmax= 4.0]
038920 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
038930 ADD HYD + 1.0 0:02:1-D 54253.88 70.229 Ndate 36:14 18.57 n/a .000
038940 # + 1.0 0:02:1-D 2.15 .287 Ndate 29:11 21.69 n/a .000
038950 # + 1.0 0:02:1-D 1.75 .023 Ndate 29:11 21.69 n/a .000
038960 # + 1.0 0:02:1-D 2.03 .026 Ndate 29:11 21.69 n/a .000
038970 # + 1.0 0:02:SN 54279.33 70.280 Ndate 36:12 18.57 n/a .000
038980 # + 1.0 0:02:SN 54279.33 70.280 Ndate 36:14 18.57 n/a .000
038990 # + 1.0 0:02:SN 54279.33 70.280 Ndate 36:14 18.57 n/a .000
039000 # [name: 5002.0005]
039010 # remark Total Flow before Station 5002 on Jock River
039020 # Channel X-Section obtained from RCHA Hydraulic Model - Station 5002
039030 # JFSA 2021-03-02 add the slope to 0.0175 to stabilize the model
039040 # JFSA 2021-03-02 add the slope to 0.0175 to stabilize the model
039050 # JFSA 2021-03-02 add the slope to 0.0175 to stabilize the model
039060 # JFSA 2021-03-02 add the slope to 0.0175 to stabilize the model
039070 # JFSA 2021-03-02 add the slope to 0.0175 to stabilize the model
039080 # JFSA 2021-03-02 add the slope to 0.0175 to stabilize the model
039090 # JFSA 2021-03-02 add the slope to 0.0175 to stabilize the model
039100 # JFSA 2021-03-02 add the slope to 0.0175 to stabilize the model
039110 # JFSA 2021-03-02 add the slope to 0.0175 to stabilize the model
039120 # JFSA 2021-03-02 add the slope to 0.0175 to stabilize the model
039130 # JFSA 2021-03-02 add the slope to 0.0175 to stabilize the model
039140 # JFSA 2021-03-02 add the slope to 0.0175 to stabilize the model
039150 # JFSA 2021-03-02 add the slope to 0.0175 to stabilize the model
039160 # JFSA 2021-03-02 add the slope to 0.0175 to stabilize the model
039170 # JFSA 2021-03-02 add the slope to 0.0175 to stabilize the model
039180 # JFSA 2021-03-02 add the slope to 0.0175 to stabilize the model
039190 # JFSA 2021-03-02 add the slope to 0.0175 to stabilize the model
039200 # JFSA 2021-03-02 add the slope to 0.0175 to stabilize the model
039210 # JFSA 2021-03-02 add the slope to 0.0175 to stabilize the model
039220 # JFSA 2021-03-02 add the slope to 0.0175 to stabilize the model
039230 # JFSA 2021-03-02 add the slope to 0.0175 to stabilize the model
039240 # JFSA 2021-03-02 add the slope to 0.0175 to stabilize the model
039250 # JFSA 2021-03-02 add the slope to 0.0175 to stabilize the model
039260 # JFSA 2021-03-02 add the slope to 0.0175 to stabilize the model
039270 # JFSA 2021-03-02 add the slope to 0.0175 to stabilize the model

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039280 # [X/M= 1.070; Dmax= 2.329]
039290 #
039300 # Hydrogram from Node West Clarke road to Node at Kennedy - Burnett Drain
039310 # Channel X-Section obtained from RCHA Hydraulic Model - Station 4534
039320 #
039330 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
039340 ROUTE CHANNEL -> 1.0 0:02:SN:NC 54279.33 70.433 Ndate 37:41 18.57 n/a .000
039350 # [R/S= 1.00] out < 1.0 0:01:NC 54279.33 70.433 Ndate 37:42 18.57 n/a .000
039360 # [L/S= 1020 / 050] 0:05]
039370 # [X/M= 948; Dmax= 2.868]
039380 #
039390 # Catchment KEN.BU
039400 # To Kennedy-Burnett SWM Facility
039410 # Outlets to Freeway-Clarke drain (north of the Jock)
039420 # Medium density residential subdivision
039430 #
039440 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
039450 COMPUTE DUALHYD 1.0 0:01:KB-01A 40.82 2.624 Ndate 28:14 20.08 n/a .000
039460 # [Impervious area: IApr= 4.67; SLP= 2.0; LG= 40; MPA= 250; SCP= 0]
039470 # [AREC= 4.00; IAREP= 4.00]
039480 # [SM= 33.81; SMM= 225.43; S&= 0.10]
039490 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
039500 COMPUTE DUALHYD 1.0 0:01:KB-01A 40.82 2.624 Ndate 28:14 20.08 n/a .000
039510 # [X/M= 10; T/MP= 40]
039520 # [Horizon parameters: Fw= 76.20; Fc= 13.20; DCAV= 14; F= 0]
039530 # [Previous area: IApr= 4.67; SLP= 2.0; LG= 40; MPA= 250; SCP= 0]
039540 # [AREC= 4.00; IAREP= 4.00]
039550 # [SM= 33.81; SMM= 225.43; S&= 0.10]
039560 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
039570 COMPUTE DUALHYD 1.0 0:01:KB-01C 40.82 2.624 Ndate 28:14 20.08 n/a .000
039580 # [Horizon parameters: Fw= 76.20; Fc= 13.20; DCAV= 14; F= 0]
039590 # [Previous area: IApr= 4.67; SLP= 2.0; LG= 40; MPA= 250; SCP= 0]
039600 # [AREC= 4.00; IAREP= 4.00]
039610 # [SM= 33.81; SMM= 225.43; S&= 0.10]
039620 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
039630 COMPUTE DUALHYD 1.0 0:01:KB-01C 40.82 2.624 Ndate 28:14 20.08 n/a .000
039640 # [Horizon parameters: Fw= 76.20; Fc= 13.20; DCAV= 14; F= 0]
039650 # [Previous area: IApr= 4.67; SLP= 2.0; LG= 40; MPA= 250; SCP= 0]
039660 # [AREC= 4.00; IAREP= 4.00]
039670 # [SM= 33.81; SMM= 225.43; S&= 0.10]
039680 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
039690 COMPUTE DUALHYD 1.0 0:01:KB-01B 31.10 1.779 Ndate 28:08 22.42 393 .000
039700 # [X/M= 19; T/MP= 38]
039710 # [Horizon parameters: Fw= 76.20; Fc= 13.20; DCAV= 14; F= 0]
039720 # [Previous area: IApr= 4.67; SLP= 2.0; LG= 40; MPA= 250; SCP= 0]
039730 # [AREC= 4.00; IAREP= 4.00]
039740 # [SM= 33.81; SMM= 225.43; S&= 0.10]
039750 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
039760 COMPUTE DUALHYD 1.0 0:01:KB-01B 31.10 1.779 Ndate 28:08 22.42 393 .000
039770 # [X/M= 19; T/MP= 38]
039780 # [Horizon parameters: Fw= 76.20; Fc= 13.20; DCAV= 14; F= 0]
039790 # [Previous area: IApr= 4.67; SLP= 2.0; LG= 40; MPA= 250; SCP= 0]
039800 # [AREC= 4.00; IAREP= 4.00]
039810 # [SM= 33.81; SMM= 225.43; S&= 0.10]
039820 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
039830 COMPUTE DUALHYD 1.0 0:01:KB-01C 13.78 1.335 Ndate 28:05 23.43 410 .000
039840 # [X/M= 20; T/MP= 41]
039850 # [Horizon parameters: Fw= 76.20; Fc= 13.20; DCAV= 14; F= 0]
039860 # [Previous area: IApr= 4.67; SLP= 2.0; LG= 40; MPA= 250; SCP= 0]
039870 # [AREC= 4.00; IAREP= 4.00]
039880 # [SM= 33.81; SMM= 225.43; S&= 0.10]
039890 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
039900 COMPUTE DUALHYD 1.0 0:01:KB-01C 13.78 1.335 Ndate 28:05 23.43 410 .000
039910 # [X/M= 20; T/MP= 41]
039920 # [Horizon parameters: Fw= 76.20; Fc= 13.20; DCAV= 14; F= 0]
039930 # [Previous area: IApr= 4.67; SLP= 2.0; LG= 40; MPA= 250; SCP= 0]
039940 # [AREC= 4.00; IAREP= 4.00]
039950 # [SM= 33.81; SMM= 225.43; S&= 0.10]
039960 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
039970 COMPUTE DUALHYD 1.0 0:01:KB-01C 13.78 1.335 Ndate 28:05 23.43 410 .000
039980 # [X/M= 20; T/MP= 41]
039990 # [Horizon parameters: Fw= 76.20; Fc= 13.20; DCAV= 14; F= 0]
040000 # [Previous area: IApr= 4.67; SLP= 2.0; LG= 40; MPA= 250; SCP= 0]
040010 # [AREC= 4.00; IAREP= 4.00]
040020 # [SM= 33.81; SMM= 225.43; S&= 0.10]
040030 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
040040 COMPUTE DUALHYD 1.0 0:01:KB-01C 13.78 1.335 Ndate 28:05 23.43 410 .000
040050 # [X/M= 20; T/MP= 41]
040060 # [Horizon parameters: Fw= 76.20; Fc= 13.20; DCAV= 14; F= 0]
040070 # [Previous area: IApr= 4.67; SLP= 2.0; LG= 40; MPA= 250; SCP= 0]
040080 # [AREC= 4.00; IAREP= 4.00]
040090 # [SM= 33.81; SMM= 225.43; S&= 0.10]
040100 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
040110 COMPUTE DUALHYD 1.0 0:01:KB-01C 13.78 1.335 Ndate 28:05 23.43 410 .000
040120 # [X/M= 20; T/MP= 41]
040130 # [Horizon parameters: Fw= 76.20; Fc= 13.20; DCAV= 14; F= 0]
040140 # [Previous area: IApr= 4.67; SLP= 2.0; LG= 40; MPA= 250; SCP= 0]
040150 # [AREC= 4.00; IAREP= 4.00]
040160 # [SM= 33.81; SMM= 225.43; S&= 0.10]
040170 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
040180 COMPUTE DUALHYD 1.0 0:01:KB-01C 13.78 1.335 Ndate 28:05 23.43 410 .000
040190 # [X/M= 20; T/MP= 41]
040200 # [Horizon parameters: Fw= 76.20; Fc= 13.20; DCAV= 14; F= 0]
040210 # [Previous area: IApr= 4.67; SLP= 2.0; LG= 40; MPA= 250; SCP= 0]
040220 # [AREC= 4.00; IAREP= 4.00]
040230 # [SM= 33.81; SMM= 225.43; S&= 0.10]
040240 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
040250 COMPUTE DUALHYD 1.0 0:01:KB-01C 13.78 1.335 Ndate 28:05 23.43 410 .000
040260 # [X/M= 20; T/MP= 41]
040270 # [Horizon parameters: Fw= 76.20; Fc= 13.20; DCAV= 14; F= 0]
040280 # [Previous area: IApr= 4.67; SLP= 2.0; LG= 40; MPA= 250; SCP= 0]
040290 # [AREC= 4.00; IAREP= 4.00]
040300 # [SM= 33.81; SMM= 225.43; S&= 0.10]
040310 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
040320 COMPUTE DUALHYD 1.0 0:01:KB-01C 13.78 1.335 Ndate 28:05 23.43 410 .000
040330 # [X/M= 20; T/MP= 41]
040340 # [Horizon parameters: Fw= 76.20; Fc= 13.20; DCAV= 14; F= 0]
040350 # [Previous area: IApr= 4.67; SLP= 2.0; LG= 40; MPA= 250; SCP= 0]
040360 # [AREC= 4.00; IAREP= 4.00]
040370 # [SM= 33.81; SMM= 225.43; S&= 0.10]
040380 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
040390 COMPUTE DUALHYD 1.0 0:01:KB-01C 13.78 1.335 Ndate 28:05 23.43 410 .000
040400 # [X/M= 20; T/MP= 41]
040410 # [Horizon parameters: Fw= 76.20; Fc= 13.20; DCAV= 14; F= 0]
040420 # [Previous area: IApr= 4.67; SLP= 2.0; LG= 40; MPA= 250; SCP= 0]
040430 # [AREC= 4.00; IAREP= 4.00]
040440 # [SM= 33.81; SMM= 225.43; S&= 0.10]
040450 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
040460 COMPUTE DUALHYD 1.0 0:01:KB-01C 13.78 1.335 Ndate 28:05 23.43 410 .000
040470 # [X/M= 20; T/MP= 41]
040480 # [Horizon parameters: Fw= 76.20; Fc= 13.20; DCAV= 14; F= 0]
040490 # [Previous area: IApr= 4.67; SLP= 2.0; LG= 40; MPA= 250; SCP= 0]
040500 # [AREC= 4.00; IAREP= 4.00]
040510 # [SM= 33.81; SMM= 225.43; S&= 0.10]
040520 # Dfma-ID NDD .....AREHA-QPEAKm-TpeakDte,hm-mm-Rvmm R.C.-DfWcm
040530 COMPUTE DUALHYD 1.0 0:01:KB-01C 13.78 1.335 Ndate 28:05 23.
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041155	COMPUTE DUAL/D	1.0	01:KB07	10.86	1.770	Ndate	28:00	50.11	n/a	.000
041160	Mjr System	1.0	02:KB-12	4.86	7.77	Ndate	28:00	46.75	n/a	.000
041170	Msr System	1.0	02:KB-13	10.86	1.770	Ndate	28:00	50.11	n/a	.000
041180	Msr System	1.0	02:KB-14	10.86	1.770	Ndate	28:00	50.11	n/a	.000
041190	R0005: C00220	1.0	01:PC-01	8.03	6.65	Ndate	28:01	32.39	567	.000
041200	ADD IVD	1.0	02:KB-07	10.86	1.770	Ndate	28:00	50.11	n/a	.000
041210	Mjr System	1.0	02:KB-12	4.86	7.77	Ndate	28:00	46.75	n/a	.000
041220	Msr System	1.0	02:KB-13	10.86	1.770	Ndate	28:00	50.11	n/a	.000
041230	Msr System	1.0	02:KB-14	10.86	1.770	Ndate	28:00	50.11	n/a	.000
041240	CNTLNKX STAN/D	1.0	01:KB-08	6.61	9.00	Ndate	28:00	40.32	706	.000
041250	[X MPa: 64-TIMP: 64]									
041260	Horton parameters: Fw= 76.20; Fc= 13.20; DCAV4= 14; Fw= 0.00									
041270	[Previous area: IApr= 4.67; SLP2= 0.0; LCP= 40; MNP= 250; SCP= 0]									
041280	[Impervious area: IApr= 7.9; SLP1= 0.0; LCP= 210; MNP= 013; SCL= 0]									
041290	[IAREC mp= 4.00; IAREPR= 4.00]									
041300	R0005: C00221	1.0	01:PC-01	8.03	6.65	Ndate	28:01	32.39	567	.000
041310	COMPUTE DUAL/D	1.0	01:KB-08	6.61	9.00	Ndate	28:00	40.32	706	.000
041320	Mjr System	1.0	02:KB-12	4.86	7.77	Ndate	28:00	46.75	n/a	.000
041330	Msr System	1.0	02:KB-13	10.86	1.770	Ndate	28:00	50.11	n/a	.000
041340	Msr System	1.0	02:KB-14	10.86	1.770	Ndate	28:00	50.11	n/a	.000
041350	[M Syste= 0000E+00; Tot Of Vol= 0000E+00; N Of= 0; Tot Dur Of= 0 hrs]									
041360	ADD IVD	1.0	02:KB-08	6.61	9.00	Ndate	28:00	40.32	706	.000
041370	Mjr System	1.0	02:KB-12	4.86	7.77	Ndate	28:00	46.75	n/a	.000
041380	Msr System	1.0	02:KB-13	10.86	1.770	Ndate	28:00	50.11	n/a	.000
041390	Msr System	1.0	02:KB-14	10.86	1.770	Ndate	28:00	50.11	n/a	.000
041400	CNTLNKX STAN/D	1.0	01:KB-08	6.61	9.00	Ndate	28:00	40.32	706	.000
041410	[X MPa: 86-TIMP: 86]									
041420	Horton parameters: Fw= 76.20; Fc= 13.20; DCAV4= 14; Fw= 0.00									
041430	[Previous area: IApr= 4.67; SLP2= 0.0; LCP= 40; MNP= 250; SCP= 0]									
041440	[Impervious area: IApr= 1.57; SLP1= 0.0; LCP= 132; MNP= 013; SCL= 0]									
041450	[IAREC mp= 4.00; IAREPR= 4.00]									
041460	R0005: C00225	1.0	01:KB-09	2.60	4.48	Ndate	28:00	49.44	865	.000
041470	CNTLNKX STAN/D	1.0	01:KB-09	2.60	4.48	Ndate	28:00	49.44	865	.000
041480	[X MPa: 86-TIMP: 86]									
041490	Horton parameters: Fw= 76.20; Fc= 13.20; DCAV4= 14; Fw= 0.00									
041500	[Previous area: IApr= 4.67; SLP2= 0.0; LCP= 40; MNP= 250; SCP= 0]									
041510	[Impervious area: IApr= 1.57; SLP1= 0.0; LCP= 126; MNP= 013; SCL= 0]									
041520	[IAREC mp= 4.00; IAREPR= 4.00]									
041530	R0005: C00226	1.0	01:KB-09	2.60	4.48	Ndate	28:00	49.44	865	.000
041540	CNTLNKX STAN/D	1.0	01:KB-09	2.60	4.48	Ndate	28:00	49.44	865	.000
041550	[X MPa: 86-TIMP: 86]									
041560	Horton parameters: Fw= 76.20; Fc= 13.20; DCAV4= 14; Fw= 0.00									
041570	[Previous area: IApr= 4.67; SLP2= 0.0; LCP= 40; MNP= 250; SCP= 0]									
041580	[Impervious area: IApr= 1.57; SLP1= 0.0; LCP= 87; MNP= 013; SCL= 0]									
041590	[IAREC mp= 4.00; IAREPR= 4.00]									
041600	R0005: C00227	1.0	01:KB-09	2.60	4.48	Ndate	28:00	49.44	865	.000
041610	CNTLNKX STAN/D	1.0	01:KB-09	2.60	4.48	Ndate	28:00	49.44	865	.000
041620	[X MPa: 79-TIMP: 79]									
041630	Horton parameters: Fw= 76.20; Fc= 13.20; DCAV4= 14; Fw= 0.00									
041640	[Previous area: IApr= 4.67; SLP2= 0.0; LCP= 40; MNP= 250; SCP= 0]									
041650	[Impervious area: IApr= 1.0; SLP1= 0.0; LCP= 180; MNP= 013; SCL= 0]									
041660	[IAREC mp= 4.00; IAREPR= 4.00]									
041670	R0005: C00228	1.0	01:KB-10	4.86	7.77	Ndate	28:00	46.75	n/a	.000
041680	CNTLNKX STAN/D	1.0	01:KB-10	4.86	7.77	Ndate	28:00	46.75	n/a	.000
041690	Mjr System	1.0	02:KB-12	4.86	7.77	Ndate	28:00	46.75	n/a	.000
041700	Msr System	1.0	02:KB-13	10.86	1.770	Ndate	28:00	50.11	n/a	.000
041710	Msr System	1.0	02:KB-14	10.86	1.770	Ndate	28:00	50.11	n/a	.000
041720	R0005: C00229	1.0	01:KB-10	4.86	7.77	Ndate	28:00	46.75	n/a	.000
041730	ADD IVD	1.0	02:KB-12	4.86	7.77	Ndate	28:00	46.75	n/a	.000
041740	Mjr System	1.0	02:KB-12	4.86	7.77	Ndate	28:00	46.75	n/a	.000
041750	Msr System	1.0	02:KB-13	10.86	1.770	Ndate	28:00	50.11	n/a	.000
041760	Msr System	1.0	02:KB-14	10.86	1.770	Ndate	28:00	50.11	n/a	.000
041770	CNTLNKX STAN/D	1.0	01:KB-13	10.86	1.770	Ndate	28:00	50.11	n/a	.000
041780	[X MPa: 86-TIMP: 86]									
041790	Horton parameters: Fw= 76.20; Fc= 13.20; DCAV4= 14; Fw= 0.00									
041800	[Previous area: IApr= 4.67; SLP2= 0.0; LCP= 40; MNP= 250; SCP= 0]									
041810	[Impervious area: IApr= 7.9; SLP1= 0.0; LCP= 261; MNP= 013; SCL= 0]									
041820	[IAREC mp= 4.00; IAREPR= 4.00]									
041830	R0005: C00231	1.0	01:KB-13	10.86	1.770	Ndate	28:00	50.11	n/a	.000
041840	COMPUTE DUAL/D	1.0	01:KB-13	10.86	1.770	Ndate	28:00	50.11	n/a	.000
041850	Mjr System	1.0	02:KB-12	4.86	7.77	Ndate	28:00	46.75	n/a	.000
041860	Msr System	1.0	02:KB-13	10.86	1.770	Ndate	28:00	50.11	n/a	.000
041870	Msr System	1.0	02:KB-14	10.86	1.770	Ndate	28:00	50.11	n/a	.000
041880	R0005: C00232	1.0	01:KB-13	10.86	1.770	Ndate	28:00	50.11	n/a	.000
041890	ADD IVD	1.0	02:KB-13	10.86	1.770	Ndate	28:00	50.11	n/a	.000
041900	Mjr System	1.0	02:KB-12	4.86	7.77	Ndate	28:00	46.75	n/a	.000
041910	Msr System	1.0	02:KB-13	10.86	1.770	Ndate	28:00	50.11	n/a	.000
041920	Msr System	1.0	02:KB-14	10.86	1.770	Ndate	28:00	50.11	n/a	.000
041930	CNTLNKX STAN/D	1.0	01:KB-14	5.47	7.56	Ndate	28:00	40.32	706	.000
041940	[X MPa: 64-TIMP: 64]									
041950	Horton parameters: Fw= 76.20; Fc= 13.20; DCAV4= 14; Fw= 0.00									
041960	[Previous area: IApr= 4.67; SLP2= 0.0; LCP= 40; MNP= 250; SCP= 0]									
041970	[Impervious area: IApr= 7.9; SLP1= 0.0; LCP= 191; MNP= 013; SCL= 0]									
041980	[IAREC mp= 4.00; IAREPR= 4.00]									
041990	R0005: C00234	1.0	01:KB-14	5.47	7.56	Ndate	28:00	40.32	706	.000
042000	COMPUTE DUAL/D	1.0	01:KB-14	5.47	7.56	Ndate	28:00	40.32	706	.000
042010	Mjr System	1.0	02:KB-12	4.86	7.77	Ndate	28:00	46.75	n/a	.000
042020	Msr System	1.0	02:KB-13	10.86	1.770	Ndate	28:00	50.11	n/a	.000
042030	[M Syste= 0000E+00; Tot Of Vol= 0000E+00; N Of= 0; Tot Dur Of= 0 hrs]									
042040	R0005: C00235	1.0	01:KB-14	5.47	7.56	Ndate	28:00	40.32	706	.000
042050	ADD IVD	1.0	02:KB-14	5.47	7.56	Ndate	28:00	40.32	706	.000
042060	Mjr System	1.0	02:KB-12	4.86	7.77	Ndate	28:00	46.75	n/a	.000
042070	Msr System	1.0	02:KB-13	10.86	1.770	Ndate	28:00	50.11	n/a	.000
042080	R0005: C00236	1.0	01:KB-14	5.47	7.56	Ndate	28:00	40.32	706	.000
042090	CNTLNKX STAN/D	1.0	01:KB-14	5.47	7.56	Ndate	28:00	40.32	706	.000
042100	[X MPa: 71-TIMP: 71]									
042110	Horton parameters: Fw= 76.20; Fc= 13.20; DCAV4= 14; Fw= 0.00									
042120	[Previous area: IApr= 4.67; SLP2= 0.0; LCP= 40; MNP= 250; SCP= 0]									
042130	[Impervious area: IApr= 16.0; SLP1= 0.0; LCP= 151; MNP= 013; SCL= 0]									
042140	[IAREC mp= 4.00; IAREPR= 4.00]									
042150	R0005: C00237	1.0	01:KB-15	10.86	1.770	Ndate	28:00	50.11	n/a	.000
042160	ADD IVD	1.0	02:KB-07	10.86	1.770	Ndate	28:00	50.11	n/a	.000
042170	Mjr System	1.0	02:KB-12	4.86	7.77	Ndate	28:00	46.75	n/a	.000
042180	Msr System	1.0	02:KB-13	10.86	1.770	Ndate	28:00	50.11	n/a	.000
042190	Msr System	1.0	02:KB-14	10.86	1.770	Ndate	28:00	50.11	n/a	.000
042200	[M Syste= 0000E+00; Tot Of Vol= 0000E+00; N Of= 0; Tot Dur Of= 0 hrs]									
042210	R0005: C00238	1.0	01:KB-15	10.86	1.770	Ndate	28:00	50.11	n/a	.000
042220	ADD IVD	1.0	02:KB-12	4.86	7.77	Ndate	28:00	46.75	n/a	.000
042230	Mjr System	1.0	02:KB-12	4.86	7.77	Ndate	28:00	46.75	n/a	.000
042240	Msr System	1.0	02:KB-13	10.86	1.770	Ndate	28:00	50.11	n/a	.000

04863#	R005#	C00343	Dfwn-ID NDDND	AREHA-QPEAKM-TpeakDte-hh:mm	Rvmm R C	Dfwm
04864#	VERT	IND	>	1.0 02:18:00	135.9	9.064	28.05	35.39	n/a
04865#	diverted	ca	>	1.0 02:18:05	135.9	9.064	28.05	35.39	n/a
04866#	diverted	ca	>	1.0 02:18:10	135.9	9.064	28.05	35.39	n/a
04867#	R005#	C00344	Dfwn-ID NDDND	AREHA-QPEAKM-TpeakDte-hh:mm	Rvmm R C	Dfwm
04868#	CONTINUOUS STANDBY	1.0 01:01:07	7.19	6.61	28.05	28.01	34.82	61.0	0.00
04869#	[X]Mps: 41.71	SMWX:225.43	SKG: 010						
04870#	[LRS= 2 CN= 75.0]								
04871#	[Previous area: Ipergr 4.67:SLP1+0.0:LG= 40: MNP: 250: SCP= 0]								
04872#	[Impervious area: Ipergr 1.57:SLP1+0.0:LG= 211: MN: 013: SCI= 0]								
04873#	[IAREC mps 4.00: IARECR 4.00]								
04874#	[SMN 33.81: SMWX:225.43: SKG: 010]								
04875#	R005#	C00345	Dfwn-ID NDDND	AREHA-QPEAKM-TpeakDte-hh:mm	Rvmm R C	Dfwm
04876#	ADD HYD	>	1.0 02:07:00	7.19	6.61	28.05	34.82	n/a	0.00
04877#								
04878#								
04879#	R005#	C00346	Dfwn-ID NDDND	AREHA-QPEAKM-TpeakDte-hh:mm	Rvmm R C	Dfwm
04880#	COMPUTE DUALIND	1.0 01:01:00	7.19	6.61	28.05	34.82	n/a	0.00	
04881#	Mjor System	>	1.0 02:18:00	135.9	9.064	28.05	35.39	n/a	0.00
04882#	Mjor System	>	1.0 02:18:05	135.9	9.064	28.05	35.39	n/a	0.00
04883#	Mjor System	>	1.0 02:18:10	135.9	9.064	28.05	35.39	n/a	0.00
04884#	R005#	C00347	Dfwn-ID NDDND	AREHA-QPEAKM-TpeakDte-hh:mm	Rvmm R C	Dfwm
04885#	CONTINUOUS STANDBY	1.0 01:01:07	7.19	6.61	28.05	28.01	34.82	61.0	0.00
04886#	[X]Mps: 41.71	SMWX:225.43	SKG: 010						
04887#	[LRS= 2 CN= 75.0]								
04888#	[Previous area: Ipergr 4.67:SLP1+0.0:LG= 40: MNP: 250: SCP= 0]								
04889#	[Impervious area: Ipergr 1.57:SLP1+0.0:LG= 211: MN: 013: SCI= 0]								
04890#	[IAREC mps 4.00: IARECR 4.00]								
04891#	[SMN 33.81: SMWX:225.43: SKG: 010]								
04892#	R005#	C00348	Dfwn-ID NDDND	AREHA-QPEAKM-TpeakDte-hh:mm	Rvmm R C	Dfwm
04893#	COMPUTE DUALIND	1.0 01:01:00	7.19	6.61	28.05	34.82	n/a	0.00	
04894#	Mjor System	>	1.0 02:18:00	135.9	9.064	28.05	35.39	n/a	0.00
04895#	Mjor System	>	1.0 02:18:05	135.9	9.064	28.05	35.39	n/a	0.00
04896#	Mjor System	>	1.0 02:18:10	135.9	9.064	28.05	35.39	n/a	0.00
04897#	R005#	C00349	Dfwn-ID NDDND	AREHA-QPEAKM-TpeakDte-hh:mm	Rvmm R C	Dfwm
04898#	CONTINUOUS STANDBY	1.0 01:01:07	7.19	6.61	28.05	28.01	34.82	61.0	0.00
04899#	[X]Mps: 41.71	SMWX:225.43	SKG: 010						
04900#	[LRS= 2 CN= 75.0]								
04901#	[Previous area: Ipergr 4.67:SLP1+0.0:LG= 40: MNP: 250: SCP= 0]								
04902#	[Impervious area: Ipergr 1.57:SLP1+0.0:LG= 211: MN: 013: SCI= 0]								
04903#	[IAREC mps 4.00: IARECR 4.00]								
04904#	[SMN 36.67: SMWX:244.45: SKG: 010]								
04905#	R005#	C00350	Dfwn-ID NDDND	AREHA-QPEAKM-TpeakDte-hh:mm	Rvmm R C	Dfwm
04906#	COMPUTE DUALIND	1.0 01:01:00	7.19	6.61	28.05	34.82	n/a	0.00	
04907#	Mjor System	>	1.0 02:18:00	135.9	9.064	28.05	35.39	n/a	0.00
04908#	Mjor System	>	1.0 02:18:05	135.9	9.064	28.05	35.39	n/a	0.00
04909#	Mjor System	>	1.0 02:18:10	135.9	9.064	28.05	35.39	n/a	0.00
04910#	R005#	C00351	Dfwn-ID NDDND	AREHA-QPEAKM-TpeakDte-hh:mm	Rvmm R C	Dfwm
04911#	CONTINUOUS STANDBY	1.0 01:01:07	7.19	6.61	28.05	28.01	34.82	61.0	0.00
04912#	[X]Mps: 41.71	SMWX:225.43	SKG: 010						
04913#	[LRS= 2 CN= 75.0]								
04914#	[Previous area: Ipergr 4.67:SLP1+0.0:LG= 40: MNP: 250: SCP= 0]								
04915#	[Impervious area: Ipergr 1.57:SLP1+0.0:LG= 211: MN: 013: SCI= 0]								
04916#	[IAREC mps 4.00: IARECR 4.00]								
04917#	[SMN 33.81: SMWX:225.43: SKG: 010]								
04918#	R005#	C00352	Dfwn-ID NDDND	AREHA-QPEAKM-TpeakDte-hh:mm	Rvmm R C	Dfwm
04919#	COMPUTE DUALIND	1.0 01:01:00	7.19	6.61	28.05	34.82	n/a	0.00	
04920#	Mjor System	>	1.0 02:18:00	135.9	9.064	28.05	35.39	n/a	0.00
04921#	Mjor System	>	1.0 02:18:05	135.9	9.064	28.05	35.39	n/a	0.00
04922#	Mjor System	>	1.0 02:18:10	135.9	9.064	28.05	35.39	n/a	0.00
04923#	R005#	C00353	Dfwn-ID NDDND	AREHA-QPEAKM-TpeakDte-hh:mm	Rvmm R C	Dfwm
04924#	CONTINUOUS STANDBY	1.0 01:01:07	7.19	6.61	28.05	28.01	34.82	61.0	0.00
04925#	[X]Mps: 41.71	SMWX:225.43	SKG: 010						
04926#	[LRS= 2 CN= 75.0]								
04927#	[Previous area: Ipergr 4.67:SLP1+0.0:LG= 40: MNP: 250: SCP= 0]								
04928#	[Impervious area: Ipergr 1.57:SLP1+0.0:LG= 211: MN: 013: SCI= 0]								
04929#	[IAREC mps 4.00: IARECR 4.00]								
04930#	[SMN 36.67: SMWX:244.45: SKG: 010]								
04931#	R005#	C00354	Dfwn-ID NDDND	AREHA-QPEAKM-TpeakDte-hh:mm	Rvmm R C	Dfwm
04932#	COMPUTE DUALIND	1.0 01:01:00	7.19	6.61	28.05	34.82	n/a	0.00	
04933#	Mjor System	>	1.0 02:18:00	135.9	9.064	28.05	35.39	n/a	0.00
04934#	Mjor System	>	1.0 02:18:05	135.9	9.064	28.05	35.39	n/a	0.00
04935#	Mjor System	>	1.0 02:18:10	135.9	9.064	28.05	35.39	n/a	0.00
04936#	R005#	C00355	Dfwn-ID NDDND	AREHA-QPEAKM-TpeakDte-hh:mm	Rvmm R C	Dfwm
04937#	CONTINUOUS STANDBY	1.0 01:01:07	7.19	6.61	28.05	28.01	34.82	61.0	0.00
04938#	[X]Mps: 41.71	SMWX:225.43	SKG: 010						
04939#	[LRS= 2 CN= 75.0]								
04940#	[Previous area: Ipergr 4.67:SLP1+0.0:LG= 40: MNP: 250: SCP= 0]								
04941#	[Impervious area: Ipergr 1.57:SLP1+0.0:LG= 211: MN: 013: SCI= 0]								
04942#	[IAREC mps 4.00: IARECR 4.00]								
04943#	[SMN 36.67: SMWX:244.45: SKG: 010]								
04944#	R005#	C00356	Dfwn-ID NDDND	AREHA-QPEAKM-TpeakDte-hh:mm	Rvmm R C	Dfwm
04945#	COMPUTE DUALIND	1.0 01:01:00	7.19	6.61	28.05	34.82	n/a	0.00	
04946#	Mjor System	>	1.0 02:18:00	135.9	9.064	28.05	35.39	n/a	0.00
04947#	Mjor System	>	1.0 02:18:05	135.9	9.064	28.05	35.39	n/a	0.00
04948#	Mjor System	>	1.0 02:18:10	135.9	9.064	28.05	35.39	n/a	0.00
04949#	R005#	C00357	Dfwn-ID NDDND	AREHA-QPEAKM-TpeakDte-hh:mm	Rvmm R C	Dfwm
04950#	CONTINUOUS STANDBY	1.0 01:01:07	7.19	6.61	28.05	28.01	34.82	61.0	0.00
04951#	[X]Mps: 41.71	SMWX:225.43	SKG: 010						
04952#	[LRS= 2 CN= 75.0]								
04953#	[Previous area: Ipergr 4.67:SLP1+0.0:LG= 40: MNP: 250: SCP= 0]								
04954#	[Impervious area: Ipergr 1.57:SLP1+0.0:LG= 211: MN: 013: SCI= 0]								
04955#	[IAREC mps 4.00: IARECR 4.00]								
04956#	[SMN 33.81: SMWX:225.43: SKG: 010]								
04957#	R005#	C00358	Dfwn-ID NDDND	AREHA-QPEAKM-TpeakDte-hh:mm	Rvmm R C	Dfwm
04958#	COMPUTE DUALIND	1.0 01:01:00	7.19	6.61	28.05	34.82	n/a	0.00	
04959#	Mjor System	>	1.0 02:18:00	135.9	9.064	28.05	35.39	n/a	0.00
04960#	Mjor System	>	1.0 02:18:05	135.9	9.064	28.05	35.39	n/a	0.00
04961#	Mjor System	>	1.0 02:18:10	135.9	9.064	28.05	35.39	n/a	0.00
04962#	R005#	C00359	Dfwn-ID NDDND	AREHA-QPEAKM-TpeakDte-hh:mm	Rvmm R C	Dfwm
04963#	CONTINUOUS STANDBY	1.0 01:01:07	7.19	6.61	28.05	28.01	34.82	61.0	0.00
04964#	[X]Mps: 41.71	SMWX:225.43	SKG: 010						
04965#	[LRS= 2 CN= 75.0]								
04966#	[Previous area: Ipergr 4.67:SLP1+0.0:LG= 40: MNP: 250: SCP= 0]								
04967#	[Impervious area: Ipergr 1.57:SLP1+0.0:LG= 211: MN: 013: SCI= 0]								
04968#	[IAREC mps 4.00: IARECR 4.00]								
04969#	[SMN 33.81: SMWX:225.43: SKG: 010]								
04970#	R005#	C00360	Dfwn-ID NDDND	AREHA-QPEAKM-TpeakDte-hh:mm	Rvmm R C	Dfwm
04971#	COMPUTE DUALIND	1.0 01:01:00	7.19	6.61	28.05	34.82	n/a	0.00	
04972#	Mjor System	>	1.0 02:18:00	135.9	9.064	28.05	35.39	n/a	0.00
04973#	Mjor System	>	1.0 02:18:05	135.9	9.064	28.05	35.39	n/a	0.00
04974#	Mjor System	>	1.0 02:18:10	135.9	9.064	28.05	35.39	n/a	0.00
04975#	R005#	C00361	Dfwn-ID NDDND	AREHA-QPEAKM-TpeakDte-hh:mm	Rvmm R C	Dfwm
04976#	CONTINUOUS STANDBY	1.0 01:01:07	7.19	6.61	28.05	28.01	34.82	61.0	0.00
04977#	[X]Mps: 41.71	SMWX:225.43	SKG: 010						
04978#	[LRS= 2 CN= 75.0]								
04979#	[Previous area: Ipergr 4.67:SLP1+0.0:LG= 40: MNP: 250: SCP= 0]								
04980#	[Impervious area: Ipergr 1.57:SLP1+0.0:LG= 211: MN: 013: SCI= 0]								
04981#	[IAREC mps 4.00: IARECR 4.00]								
04982#	[SMN 33.81: SMWX:225.								

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052375 R0105: C01040 ..... DfIn=1-D NND ..... AREHA-QPEAKm-TpeakDate_hh:mm ..... RvIm R.C. .... DfWcm
052388 ADD HYD ..... AREHA-QPEAKm-TpeakDate_hh:mm ..... RvIm R.C. .... DfWcm
052390 ..... [Cm= 1.0 0.2: S.2 ..... 102.94 ..... 2.262 No_date ..... 28:20 ..... 19.00 n/a ..... 0.00
052400 ..... SLM ..... 55759.20 ..... 72.356 No_date ..... 36:46 ..... 18.89 n/a ..... 0.00
052411 R0105: C01041 ..... DfIn=1-D NND ..... AREHA-QPEAKm-TpeakDate_hh:mm ..... RvIm R.C. .... DfWcm
052423 SAVE HYD ..... AREHA-QPEAKm-TpeakDate_hh:mm ..... RvIm R.C. .... DfWcm
052433 ..... [Cm= 1.0 0.1: SN_N1 ..... 55579.20 ..... 72.356 No_date ..... 36:46 ..... 18.89 n/a ..... 0.00
052445 ..... remark: Total Flow at Rideau River
052455 *****
052465 *****
052475 *****
052485 *****
052495 *****
052505 *****
052515 *****
052525 *****
052535 *****
052545 *****
052555 R0105: C01001 ..... DfIn=1-D NND ..... AREHA-QPEAKm-TpeakDate_hh:mm ..... RvIm R.C. .... DfWcm
052565 START ..... AREHA-QPEAKm-TpeakDate_hh:mm ..... RvIm R.C. .... DfWcm
052575 [TZERO= 0 hrs on 0] ..... AREHA-QPEAKm-TpeakDate_hh:mm ..... RvIm R.C. .... DfWcm
052585 [MFOUR= 2 (Imperial, 2.0metric output)] ..... AREHA-QPEAKm-TpeakDate_hh:mm ..... RvIm R.C. .... DfWcm
052595 [NSUN= 0.010] ..... AREHA-QPEAKm-TpeakDate_hh:mm ..... RvIm R.C. .... DfWcm
052605 *****
052615 *****
052625 *****
052635 *****
052645 *****
052655 *****
052665 *****
052675 *****
052685 *****
052695 *****
052705 *****
052715 *****
052725 *****
052735 *****
052745 *****
052755 *****
052765 *****
052775 *****
052785 *****
052795 *****
052805 *****
052815 *****
052825 *****
052835 *****
052845 *****
052855 *****
052865 *****
052875 *****
052885 *****
052895 *****
052905 *****
052915 *****
052925 *****
052935 *****
052945 *****
052955 *****
052965 *****
052975 *****
052985 *****
052995 *****
053005 *****
053015 *****
053025 *****
053035 *****
053045 *****
053055 *****
053065 *****
053075 *****
053085 *****
053095 *****
053105 *****
053115 *****
053125 *****
053135 *****
053145 *****
053155 *****
053165 *****
053175 *****
053185 *****
053195 *****
053205 *****
053215 *****
053225 *****
053235 *****
053245 *****
053255 *****
053265 *****
053275 *****
053285 *****
053295 *****
053305 *****
053315 *****
053325 *****
053335 *****
053345 *****
053355 *****
053365 *****
053375 *****
053385 *****
053395 *****
053405 *****
053415 *****
053425 *****
053435 *****
053445 *****
053455 *****
053465 *****
053475 *****
053485 *****
053495 *****
053505 *****
053515 *****
053525 *****
053535 *****
053545 *****
053555 *****
053565 *****
053575 *****
053585 *****
053595 *****
053605 *****
053615 *****
053625 *****
053635 *****
053645 *****
053655 *****
053665 *****
053675 *****
053685 *****
053695 *****
053705 *****
053715 *****
053725 *****
053735 *****
053745 *****
053755 *****
053765 *****
053775 *****
053785 *****
053795 *****
053805 *****
053815 *****
053825 *****
053835 *****
053845 *****
053855 *****
053865 *****
053875 *****
053885 *****
053895 *****
053905 *****
053915 *****
053925 *****
053935 *****
053945 *****
053955 *****
053965 *****
053975 *****
053985 *****
053995 *****
054005 *****
054015 *****
054025 *****
054035 *****
054045 *****
054055 *****
054065 *****
054075 *****
054085 *****
054095 *****
054105 *****
054115 *****
054125 *****
054135 *****
054145 *****
054155 *****
054165 *****
054175 *****
054185 *****
054195 *****
054205 *****
054215 *****
054225 *****
054235 *****

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05611#	ADD HYD	+ 1.0 02: NS	31561.0	61.483 N_date	39:57	21.20	n/a	.000
05612#		+ 1.0 02: SW2	131.0	1.689 N_date	28:57	19.76	n/a	.000
05613#		+ 1.0 02: HB_DR	3854.0	11.811 N_date	38:37	21.19	n/a	.000
05614#	SUM	+ 1.0 01: S_N	35546.0	73.344 N_date	39:57	21.19	n/a	.000
05615#								
05616#	Sum of hydrographs from Node 8 routed to Node 7							
05617#	Section 8							
05618#								
05619#	R0101: C00048	- DfIn - I D NND	AREHA-QPEAKm-TpeakDte-hh-mm-RvMm R.C.-DfCwm					
05620#	ROUTE CHANNEL	> 1.0 02: S_N	35546.0	73.344 N_date	39:57	21.19	n/a	.000
05621#	[RfE: 1.00] out c	+ 1.0 02: SW2	3197.0	8.899 N_date	36:26	17.07	n/a	.000
05622#	[L/S/m: 3750 / 0530 / 070]							
05623#	[Vmax: -218; Dmax: 1.987]							
05624#								
05625#	Addition of Subwatershed 7 to Node 7							
05626#								
05627#	R0101: C00049	- DfIn - I D NND	AREHA-QPEAKm-TpeakDte-hh-mm-RvMm R.C.-DfCwm					
05628#	ADD HYD	+ 1.0 02: NS	35546.0	61.416 N_date	45:01	21.16	n/a	.000
05629#		+ 1.0 02: SW2	3197.0	8.899 N_date	36:26	17.07	n/a	.000
05630#		+ 1.0 02: HB_DR	3854.0	11.811 N_date	38:37	21.19	n/a	.000
05631#	SUM	+ 1.0 01: S_N	3743.0	65.819 N_date	44:06	20.85	n/a	.000
05632#	SAVE HYD	+ 1.0 01: S_N	38740.0	65.819 N_date	44:06	20.85	n/a	.000
05633#	name: H_SNT							
05634#	remark: flow at S_N; No. SW7							
05635#	Insertion of a reservoir to simulate the effects of the Richmond Fen.							
05636#	Storage area and volumes were estimated from available topo maps.							
05637#	Release rate from fen was assumed to be controlled by the downstream							
05638#	river cross-section for summer conditions. It is assumed that for up to							
05639#	0.75 m of water, the main channel of the river provided the storage. Above							
05640#	this depth, the wetland stands to significantly store water.							
05641#								
05642#	R0101: C00051	- DfIn - I D NND	AREHA-QPEAKm-TpeakDte-hh-mm-RvMm R.C.-DfCwm					
05643#	ROUTE RESERVOIR	> 1.0 02: RES_RF	38743.0	65.819 N_date	44:06	20.85	n/a	.000
05644#	out c	+ 1.0 01: RES_RF	38743.0	31.796 N_date	60:32	20.85	n/a	.000
05645#	[MxStoElev: 21000]							
05646#	R0101: C00052	- DfIn - I D NND	AREHA-QPEAKm-TpeakDte-hh-mm-RvMm R.C.-DfCwm					
05647#	SAVE HYD	+ 1.0 01: RES_RF	38743.0	31.796 N_date	60:32	20.85	n/a	.000
05648#	name: H_RESRF							
05649#	remark: outflow of Richmond Fen							
05650#								
05651#	Sum of hydrographs from Node 7 routed to Node 6							
05652#	Section 5							
05653#								
05654#	R0101: C00053	- DfIn - I D NND	AREHA-QPEAKm-TpeakDte-hh-mm-RvMm R.C.-DfCwm					
05655#	ROUTE CHANNEL	> 1.0 02: RES_RF	38743.0	31.737 N_date	62:00	20.85	n/a	.000
05656#	[RfE: 1.00] out c	+ 1.0 01: NS	38743.0	31.737 N_date	62:00	20.85	n/a	.000
05657#	[L/S/m: 3036 / 082 / 025]							
05658#	[Vmax: -477; Dmax: -960]							
05659#								
05660#	Addition of Subwatershed 6 and Van Gaal Drain to Node 6							
05661#								
05662#	R0101: C00054	- DfIn - I D NND	AREHA-QPEAKm-TpeakDte-hh-mm-RvMm R.C.-DfCwm					
05663#	ADD HYD	+ 1.0 02: NS	38743.0	31.737 N_date	62:00	20.85	n/a	.000
05664#		+ 1.0 02: SW2	4549.0	6.669 N_date	33:04	21.69	n/a	.000
05665#		+ 1.0 02: HB_DR	1322.0	6.069 N_date	35:17	24.81	n/a	.000
05666#	SUM	+ 1.0 01: S_N	4040.0	31.737 N_date	62:00	20.99	n/a	.000
05667#								
05668#	Sum of hydrographs from Node 6 routed to Node 5							
05669#	Section 6							
05670#								
05671#	R0101: C00055	- DfIn - I D NND	AREHA-QPEAKm-TpeakDte-hh-mm-RvMm R.C.-DfCwm					
05672#	ROUTE CHANNEL	> 1.0 02: S_N	40240.0	31.737 N_date	62:00	20.99	n/a	.000
05673#	[RfE: 1.00] out c	+ 1.0 01: NS	40240.0	31.737 N_date	62:00	20.99	n/a	.000
05674#	[L/S/m: 482 / 054 / 011]							
05675#	[Vmax: -412; Dmax: 1.069]							
05676#								
05677#	Addition of Subwatershed 5 and Flowing Creek to Node 5							
05678#								
05679#	R0101: C00056	- DfIn - I D NND	AREHA-QPEAKm-TpeakDte-hh-mm-RvMm R.C.-DfCwm					
05680#	ADD HYD	+ 1.0 02: NS	40240.0	31.737 N_date	62:48	20.99	n/a	.000
05681#		+ 1.0 02: SW2	224.0	5.246 N_date	28:45	28.24	n/a	.000
05682#		+ 1.0 02: HB_DR	4549.0	28.945 N_date	33:21	25.91	n/a	.000
05683#	SUM	+ 1.0 01: S_N	4940.0	31.737 N_date	62:48	20.99	n/a	.000
05684#								
05685#	Sum of hydrographs from Node 5 routed to Node 5A							
05686#	Section 7							
05687#								
05688#	R0101: C00057	- DfIn - I D NND	AREHA-QPEAKm-TpeakDte-hh-mm-RvMm R.C.-DfCwm					
05689#	ROUTE CHANNEL	> 1.0 02: S_N	45499.0	31.737 N_date	62:48	20.99	n/a	.000
05690#	[RfE: 1.00] out c	+ 1.0 01: NS	45499.0	31.737 N_date	62:00	20.85	n/a	.000
05691#	[L/S/m: 561 / 090 / 040]							
05692#	[Vmax: -485; Dmax: 1.131]							
05693#								
05694#	Addition of Subwatershed 5A and Subwatershed 5A2 to Node 5A							
05695#								
05696#	R0101: C00058	- DfIn - I D NND	AREHA-QPEAKm-TpeakDte-hh-mm-RvMm R.C.-DfCwm					
05697#	ADD HYD	+ 1.0 02: NS	45499.0	31.737 N_date	62:48	20.99	n/a	.000
05698#		+ 1.0 02: SW2	20.0	6.614 N_date	28:45	28.24	n/a	.000
05699#		+ 1.0 02: HB_DR	4549.0	28.945 N_date	33:21	25.91	n/a	.000
05700#	SUM	+ 1.0 01: S_N	4940.0	31.737 N_date	62:48	20.99	n/a	.000
05701#								
05702#	Sum of hydrographs from Node 5A routed to Node 4							
05703#	Section 8							
05704#								
05705#	R0101: C00059	- DfIn - I D NND	AREHA-QPEAKm-TpeakDte-hh-mm-RvMm R.C.-DfCwm					
05706#	ROUTE CHANNEL	> 1.0 02: NS	46841.0	56.788 N_date	35:22	21.73	n/a	.000
05707#	[RfE: 1.00] out c	+ 1.0 01: NS	46841.0	54.543 N_date	36:56	21.73	n/a	.000
05708#	[L/S/m: 4630 / 043 / 035]							
05709#	[Vmax: -793; Dmax: 3.295]							
05710#								
05711#	Addition of Subwatershed 4 and Leam Creek to Node 4							
05712#								
05713#	R0101: C00060	- DfIn - I D NND	AREHA-QPEAKm-TpeakDte-hh-mm-RvMm R.C.-DfCwm					
05714#	ADD HYD	+ 1.0 02: NS	46841.0	54.543 N_date	36:56	21.73	n/a	.000
05715#		+ 1.0 02: SW2	585.0	8.458 N_date	29:57	31.37	n/a	.000
05716#		+ 1.0 02: HB_DR	1621.0	11.195 N_date	30:48	30.72	n/a	.000
05717#	SUM	+ 1.0 01: S_N	48447.0	59.934 N_date	36:12	22.03	n/a	.000
05718#	R0101: C00061	- DfIn - I D NND	AREHA-QPEAKm-TpeakDte-hh-mm-RvMm R.C.-DfCwm					
05719#	SAVE HYD	+ 1.0 01: S_N	48447.0	59.934 N_date	36:12	22.03	n/a	.000
05720#	name: S_N.0010							
05721#	remark: flow at S_N							
05722#								
05723#	Sum of hydrographs from Node 4 routed to Node 2							
05724#	Section 9							
05725#								
05726#	R0101: C00062	- DfIn - I D NND	AREHA-QPEAKm-TpeakDte-hh-mm-RvMm R.C.-DfCwm					
05727#	ROUTE CHANNEL	> 1.0 02: S_N	48447.0	59.934 N_date	36:12	22.03	n/a	.000
05728#	[RfE: 1.00] out c	+ 1.0 01: NS	48447.0	59.934 N_date	36:56	22.03	n/a	.000
05729#	[L/S/m: 1607 / 060 / 018]							
05730#	[Vmax: -824; Dmax: 3.325]							
05731#								
05732#	Addition of Subwatershed 2 with Mhoan Drain and Smith Drain to Node 2							
05733#								
05734#	R0101: C00063	- DfIn - I D NND	AREHA-QPEAKm-TpeakDte-hh-mm-RvMm R.C.-DfCwm					
05735#	ADD HYD	+ 1.0 02: NS	48447.0	59.934 N_date	36:56	22.03	n/a	.000
05736#		+ 1.0 02: SW2	177.0	4.146 N_date	28:45	28.24	n/a	.000
05737#		+ 1.0 02: HB_DR	1621.0	11.195 N_date	30:48	30.72	n/a	.000
05738#	SUM	+ 1.0 01: S_N	48447.0	59.934 N_date	36:12	22.03	n/a	.000
05739#	R0101: C00064	- DfIn - I D NND	AREHA-QPEAKm-TpeakDte-hh-mm-RvMm R.C.-DfCwm					
05740#	SAVE HYD	+ 1.0 01: S_N	52483.0	83.235 N_date	33:15	22.56	n/a	.000
05741#	name: H_SNT							
05742#	remark: flow at S_N; Jock River Gauge at Modie Dr.							
05743#								
05744#								
05745#	Sum of hydrographs from Node 2 routed to Node 1							
05746#	Section 10							
05747#								
05748#								
05749#	Hydrograph from Node 2 routed to Node 416							
05750#	Channel X Section obtained from RVC Hydraulic Model - Station 9025							
05751#								
05752#								
05753#	R0101: C00065	- DfIn - I D NND	AREHA-QPEAKm-TpeakDte-hh-mm-RvMm R.C.-DfCwm					
05754#	ROUTE CHANNEL	> 1.0 02: S_N	52483.0	83.235 N_date	33:15	22.56	n/a	.000
05755#	[RfE: 1.00] out c	+ 1.0 01: NS	52483.0					

06733# R0100:CO0225-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06734# CNTLNKX STANDRD 1.0 01:FC01 8.3 1.649 Date: 28:01 56.40 872.0000
06735# [XfMps: 86;TfMps: 86]
06736# [Horton parameters: Fw: 76.20; Fc: 13.20; DCAVd: 14; Fa: 00] 0
06737# [Previous area: IArea: 4.67; SLPD: 00; LG: 40; MNF: 250; SCP: 0] 0
06738# [Impervious area: IArea: 1.57; SLPD: 00; LG: 126; MN: 013; SCL: 0] 0
06739# [IARECmp: 4.00; IARECPE: 4.00] 0
06740# R0100:CO0226-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06741# CNTLNKX STANDRD 1.0 01:FC01 8.3 1.649 Date: 28:00 56.40 872.0000
06742# [XfMps: 86;TfMps: 86]
06743# [Horton parameters: Fw: 76.20; Fc: 13.20; DCAVd: 14; Fa: 00] 0
06744# [Previous area: IArea: 4.67; SLPD: 00; LG: 40; MNF: 250; SCP: 0] 0
06745# [Impervious area: IArea: 1.57; SLPD: 00; LG: 87; MN: 013; SCL: 0] 0
06746# [IARECmp: 4.00; IARECPE: 4.00] 0
06747# R0100:CO0227-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06748# CNTLNKX STANDRD 1.0 01:FC01 8.3 1.649 Date: 28:00 53.41 826.0000
06749# [XfMps: 79;TfMps: 79]
06750# [Horton parameters: Fw: 76.20; Fc: 13.20; DCAVd: 14; Fa: 00] 0
06751# [Previous area: IArea: 4.67; SLPD: 00; LG: 40; MNF: 250; SCP: 0] 0
06752# [Impervious area: IArea: 1.57; SLPD: 00; LG: 180; MN: 013; SCL: 0] 0
06753# [IARECmp: 4.00; IARECPE: 4.00] 0
06754# R0100:CO0228-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06755# COMPUTE DUALD 1.0 01:FC01 8.3 1.649 Date: 28:00 53.41 826.0000
06756# Mjr System / 1.0 02:FC02-M 4.86 867 Ndate: 27:58 53.47 n/a 0.000
06757# Mjr System / 1.0 02:FC02-M 4.86 867 Ndate: 27:58 53.47 n/a 0.000
06758# [MfSystm: 2261E+00; TotOfVol: 0.000E+00; NOfv: 0; TotDurOfv: 0 hrs] 0
06759# R0100:CO0229-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06760# ADD IVD 1.0 02:FC02-M 4.86 867 Ndate: 27:58 53.47 n/a 0.000
06761# SIMM + 1.0 02:FC02-M 4.86 867 Ndate: 27:58 53.47 n/a 0.000
06762# SIMM + 1.0 02:FC02-M 4.86 867 Ndate: 27:58 53.47 n/a 0.000
06763# R0100:CO0230-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06764# CNTLNKX STANDRD 1.0 01:FC01 10.19 1.611 Ndate: 28:00 46.33 716.0000
06765# [XfMps: 64;TfMps: 64]
06766# [Horton parameters: Fw: 76.20; Fc: 13.20; DCAVd: 14; Fa: 00] 0
06767# [Previous area: IArea: 4.67; SLPD: 00; LG: 40; MNF: 250; SCP: 0] 0
06768# [Impervious area: IArea: 79; SLPD: 00; LG: 261; MN: 013; SCL: 0] 0
06769# [IARECmp: 4.00; IARECPE: 4.00] 0
06770# R0100:CO0231-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06771# COMPUTE DUALD 1.0 01:FC01 10.19 1.611 Ndate: 28:00 46.33 716.0000
06772# Mjr System / 1.0 02:FC02-M 5.47 873 Ndate: 28:00 46.33 n/a 0.000
06773# Mjr System / 1.0 03:FC03-MN 7.37 358 Ndate: 27:45 45.93 n/a 0.000
06774# [MfSystm: 1663E+00; TotOfVol: 0.000E+00; NOfv: 0; TotDurOfv: 0 hrs] 0
06775# R0100:CO0232-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06776# ADD IVD 1.0 02:FC02-M 5.47 873 Ndate: 28:00 46.33 n/a 0.000
06777# SIMM + 1.0 02:FC02-M 5.47 873 Ndate: 28:00 46.33 n/a 0.000
06778# SIMM + 1.0 02:FC02-M 5.47 873 Ndate: 28:00 46.33 n/a 0.000
06779# R0100:CO0233-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06780# CNTLNKX STANDRD 1.0 01:FC01 5.47 898 Ndate: 28:00 46.33 716.0000
06781# [XfMps: 64;TfMps: 64]
06782# [Horton parameters: Fw: 76.20; Fc: 13.20; DCAVd: 14; Fa: 00] 0
06783# [Previous area: IArea: 4.67; SLPD: 00; LG: 40; MNF: 250; SCP: 0] 0
06784# [Impervious area: IArea: 79; SLPD: 00; LG: 191; MN: 013; SCL: 0] 0
06785# [IARECmp: 4.00; IARECPE: 4.00] 0
06786# R0100:CO0234-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06787# COMPUTE DUALD 1.0 01:FC01 5.47 898 Ndate: 28:00 46.33 716.0000
06788# Mjr System / 1.0 02:FC02-M 5.47 873 Ndate: 28:00 46.33 n/a 0.000
06789# Mjr System / 1.0 03:FC03-MN 5.47 873 Ndate: 27:59 46.40 n/a 0.000
06790# [MfSystm: 1663E+00; TotOfVol: 0.000E+00; NOfv: 0; TotDurOfv: 0 hrs] 0
06791# R0100:CO0235-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06792# ADD IVD 1.0 02:FC02-M 5.47 873 Ndate: 28:00 46.33 n/a 0.000
06793# SIMM + 1.0 02:FC02-M 5.47 873 Ndate: 28:00 46.33 n/a 0.000
06794# SIMM + 1.0 02:FC02-M 5.47 873 Ndate: 27:59 46.40 n/a 0.000
06795# R0100:CO0236-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06796# CNTLNKX STANDRD 1.0 01:FC01 5.47 898 Ndate: 28:01 50.20 776.0000
06797# [XfMps: 71;TfMps: 71]
06798# [Horton parameters: Fw: 76.20; Fc: 13.20; DCAVd: 14; Fa: 00] 0
06799# [Previous area: IArea: 4.67; SLPD: 00; LG: 40; MNF: 250; SCP: 0] 0
06800# [Impervious area: IArea: 16; SLPD: 00; LG: 151; MN: 013; SCL: 0] 0
06801# [IARECmp: 4.00; IARECPE: 4.00] 0
06802# R0100:CO0237-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06803# ADD IVD 1.0 02:FC02-M 10.86 2.042 Ndate: 28:00 57.07 n/a 0.000
06804# SIMM + 1.0 02:FC02-M 10.86 2.042 Ndate: 28:00 57.07 n/a 0.000
06805# SIMM + 1.0 02:FC02-M 10.86 2.042 Ndate: 28:00 57.07 n/a 0.000
06806# + 1.0 02:FC02-M 2.60 5.15 Ndate: 28:00 56.40 n/a 0.000
06807# + 1.0 02:FC02-M 2.37 4.70 Ndate: 28:00 56.40 n/a 0.000
06808# + 1.0 02:FC02-M 1.14 2.29 Ndate: 28:00 56.40 n/a 0.000
06809# + 1.0 02:FC02-M 4.86 867 Ndate: 27:58 53.47 n/a 0.000
06810# + 1.0 02:FC02-M 5.47 873 Ndate: 28:00 46.33 n/a 0.000
06811# + 1.0 02:FC02-M 5.47 873 Ndate: 27:59 46.40 n/a 0.000
06812# + 1.0 02:FC02-M 5.47 873 Ndate: 28:00 46.33 n/a 0.000
06813# SIMM 1.0 01:FC01 25.24 19.235 Ndate: 28:01 35.46 n/a 0.000
06814# R0100:CO0238-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06815# ROUTE RESERVOIR 1.0 01:FC01 25.24 19.235 Ndate: 28:01 35.46 n/a 0.000
06816# out <= 1.0 01:FC01 25.24 19.235 Ndate: 28:01 35.46 n/a 0.000
06817# overflow <= 1.0 01:FC01 25.24 19.235 Ndate: 28:01 35.46 n/a 0.000
06818# [MfSystm: 7575E+00; TotOfVol: 0.000E+00; NOfv: 0; TotDurOfv: 0 hrs] 0
06819# R0100:CO0239-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06820# ADD IVD 1.0 02:FC02-M 15.03 10.983 Ndate: 28:01 35.46 n/a 0.000
06821# SIMM + 1.0 02:FC02-M 0.00 0.00 Ndate: 00:00 0.00 n/a 0.000
06822# SIMM + 1.0 02:FC02-M 284.15 15.294 Ndate: 28:00 35.46 n/a 0.000
06823# R0100:CO0240-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06824# SAVE IVD 1.0 01:FC01 25.24 19.235 Ndate: 28:01 35.46 n/a 0.000
06825# fname: KB-Pond2; 25.24 19.235 Ndate: 28:01 35.46 n/a 0.000
06826# remark: Total Flow at KB second pond
06827# R0100:CO0241-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06828# CNTLNKX STANDRD 1.0 01:FC01 2.80 4.65 Ndate: 28:01 52.17 806.0000
06829# [XfMps: 75;TfMps: 75]
06830# [Horton parameters: Fw: 76.20; Fc: 13.20; DCAVd: 14; Fa: 00] 0
06831# [Previous area: IArea: 4.67; SLPD: 00; LG: 40; MNF: 250; SCP: 0] 0
06832# [Impervious area: IArea: 16; SLPD: 00; LG: 137; MN: 013; SCL: 0] 0
06833# [IARECmp: 4.00; IARECPE: 4.00] 0
06834# R0100:CO0242-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06835# ADD IVD 1.0 02:FC02-M 25.24 15.083 Ndate: 28:01 35.46 n/a 0.000
06836# SIMM + 1.0 02:FC02-M 2.80 4.65 Ndate: 28:01 52.17 n/a 0.000
06837# SIMM + 1.0 02:FC02-M 257.04 15.295 Ndate: 28:08 35.64 n/a 0.000
06838# R0100:CO0243-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06839# ROUTE RESERVOIR 1.0 01:FC01 25.24 15.083 Ndate: 28:01 35.46 n/a 0.000
06840# out <= 1.0 01:FC01 12.26 0.51 Ndate: 17:31 35.64 n/a 0.000
06841# overflow <= 1.0 01:FC01 25.24 15.295 Ndate: 28:09 35.64 n/a 0.000
06842# [MfSystm: 1993E+02; TotOfVol: 8724E+00; NOfv: 2; TotDurOfv: 23 hrs] 0
06843# R0100:CO0244-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06844# ADD IVD 1.0 02:FC02-M 12.26 0.51 Ndate: 17:31 35.64 n/a 0.000
06845# SIMM + 1.0 02:FC02-M 244.78 15.294 Ndate: 28:09 35.64 n/a 0.000
06846# SIMM + 1.0 02:FC02-M 257.04 15.294 Ndate: 28:09 35.64 n/a 0.000
06847# R0100:CO0245-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06848# SAVE IVD 1.0 01:FC01 25.24 15.294 Ndate: 28:09 35.64 n/a 0.000
06849# fname: KB-Pond3; 25.24 15.294 Ndate: 28:09 35.64 n/a 0.000
06850# remark: Total Flow at KB third pond
06851# R0100:CO0246-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06852# ED STING / PROPOSED Subcatchment (Kennedy-Burnett SWM Facility (118080), SWM Modeling Approach, NOVATECH Report Ju
06853# TO FRASER CLARK DRAIN (north of the Jack)
06854# R0100:CO0247-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06855# CNTLNKX STANDRD 1.0 01:FC01 8.03 1.649 Date: 28:01 37.67 582.0000
06856# [XfMps: 47;TfMps: 47]
06857# [Horton parameters: Fw: 76.20; Fc: 13.20; DCAVd: 14; Fa: 00] 0
06858# [Previous area: IArea: 4.67; SLPD: 00; LG: 40; MNF: 250; SCP: 0] 0
06859# [Impervious area: IArea: 1.57; SLPD: 00; LG: 231; MN: 013; SCL: 0] 0
06860# [IARECmp: 4.00; IARECPE: 4.00] 0
06861# R0100:CO0248-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06862# COMPUTE DUALD 1.0 01:FC01 8.03 1.649 Date: 28:01 37.67 582.0000
06863# Mjr System / 1.0 02:FC02-M 0.00 0.00 Ndate: 00:00 0.00 n/a 0.000
06864# Mjr System / 1.0 03:FC03-MN 7.37 358 Ndate: 27:45 45.93 n/a 0.000
06865# [MfSystm: 1270E+00; TotOfVol: 0.000E+00; NOfv: 0; TotDurOfv: 0 hrs] 0
06866# R0100:CO0249-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06867# ADD IVD 1.0 02:FC02-M 0.00 0.00 Ndate: 00:00 0.00 n/a 0.000
06868# SIMM + 1.0 02:FC02-M 8.03 1.756 Ndate: 27:55 37.91 n/a 0.000
06869# SIMM + 1.0 02:FC02-M 8.03 1.756 Ndate: 27:55 37.91 n/a 0.000
06870# R0100:CO0250-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06871# CNTLNKX STANDRD 1.0 01:FC01 16.05 2.930 Ndate: 28:01 59.76 924.0000
06872# [XfMps: 93;TfMps: 93]
06873# [Horton parameters: Fw: 76.20; Fc: 13.20; DCAVd: 14; Fa: 00] 0
06874# [Previous area: IArea: 4.67; SLPD: 00; LG: 40; MNF: 250; SCP: 0] 0
06875# [Impervious area: IArea: 1.57; SLPD: 00; LG: 327; MN: 013; SCL: 0] 0
06876# [IARECmp: 4.00; IARECPE: 4.00] 0
06877# R0100:CO0251-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06878# COMPUTE DUALD 1.0 01:FC01 16.05 2.930 Ndate: 28:01 59.76 924.0000
06879# Mjr System / 1.0 02:FC02-M 16.05 2.930 Ndate: 28:00 59.76 n/a 0.000
06880# Mjr System / 1.0 03:FC03-MN 7.37 358 Ndate: 27:45 45.93 n/a 0.000
06881# [MfSystm: 1407E+04; TotOfVol: 0.000E+00; NOfv: 6; TotDurOfv: 0 hrs] 0
06882# R0100:CO0252-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06883# ADD IVD 1.0 02:FC02-M 16.05 1.159 Ndate: 27:46 59.94 n/a 0.000
06884# SIMM + 1.0 02:FC02-M 0.00 0.00 Ndate: 00:00 0.00 n/a 0.000
06885# SIMM + 1.0 02:FC02-M 16.05 1.159 Ndate: 27:46 59.94 n/a 0.000
06886# R0100:CO0253-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06887# CNTLNKX STANDRD 1.0 01:FC01 7.37 1.130 Ndate: 28:01 45.83 708.0000
06888# [XfMps: 64;TfMps: 64]
06889# [Horton parameters: Fw: 76.20; Fc: 13.20; DCAVd: 14; Fa: 00] 0
06890# [Previous area: IArea: 4.67; SLPD: 00; LG: 40; MNF: 250; SCP: 0] 0
06891# [Impervious area: IArea: 1.57; SLPD: 00; LG: 222; MN: 013; SCL: 0] 0
06892# [IARECmp: 4.00; IARECPE: 4.00] 0
06893# R0100:CO0254-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06894# COMPUTE DUALD 1.0 01:FC01 7.37 1.130 Ndate: 28:01 45.83 708.0000
06895# Mjr System / 1.0 02:FC02-M 7.37 1.130 Ndate: 28:01 45.83 n/a 0.000
06896# Mjr System / 1.0 03:FC03-MN 7.37 358 Ndate: 27:45 45.93 n/a 0.000
06897# [MfSystm: 6706E+00; TotOfVol: 0.000E+00; NOfv: 0; TotDurOfv: 0 hrs] 0
06898# R0100:CO0255-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06899# ADD IVD 1.0 02:FC02-M 7.37 1.130 Ndate: 28:01 45.83 n/a 0.000
06900# SIMM + 1.0 02:FC02-M 7.37 1.130 Ndate: 28:01 45.83 n/a 0.000
06901# SIMM + 1.0 02:FC02-M 7.37 1.130 Ndate: 27:45 45.93 n/a 0.000
06902# R0100:CO0256-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06903# CNTLNKX STANDRD 1.0 01:FC01 12.87 1.906 Ndate: 28:01 45.83 708.0000
06904# [XfMps: 71;TfMps: 71]
06905# [Horton parameters: Fw: 76.20; Fc: 13.20; DCAVd: 14; Fa: 00] 0
06906# [Previous area: IArea: 4.67; SLPD: 00; LG: 40; MNF: 250; SCP: 0] 0
06907# [Impervious area: IArea: 1.57; SLPD: 00; LG: 295; MN: 013; SCL: 0] 0
06908# [IARECmp: 4.00; IARECPE: 4.00] 0
06909# R0100:CO0257-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06910# COMPUTE DUALD 1.0 01:FC01 12.87 1.906 Ndate: 28:01 45.83 708.0000
06911# Mjr System / 1.0 02:FC02-M 12.87 1.906 Ndate: 28:01 45.83 n/a 0.000
06912# Mjr System / 1.0 03:FC03-MN 12.87 741 Ndate: 27:46 45.93 n/a 0.000
06913# [MfSystm: 9380E+00; TotOfVol: 0.000E+00; NOfv: 0; TotDurOfv: 0 hrs] 0
06914# R0100:CO0258-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06915# ADD IVD 1.0 02:FC02-M 12.87 1.906 Ndate: 28:01 45.83 n/a 0.000
06916# SIMM + 1.0 02:FC02-M 12.87 1.906 Ndate: 27:46 45.93 n/a 0.000
06917# SIMM + 1.0 02:FC02-M 12.87 1.906 Ndate: 27:46 45.93 n/a 0.000
06918# R0100:CO0259-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06919# *****

06920# PROPOSED Subcatchment (Kennedy-Burnett SWM Facility (118080), SWM Modeling Approach, NOVATECH Report June, 2020)
06921# TO JACKS RUN
06922# R0100:CO0260-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06923# CNTLNKX STANDRD 1.0 01:FC01 8.24 1.257 Ndate: 28:01 45.83 708.0000
06924# [XfMps: 64;TfMps: 64]
06925# [Horton parameters: Fw: 76.20; Fc: 13.20; DCAVd: 14; Fa: 00] 0
06926# [Previous area: IArea: 4.67; SLPD: 00; LG: 40; MNF: 250; SCP: 0] 0
06927# [Impervious area: IArea: 1.57; SLPD: 00; LG: 234; MN: 013; SCL: 0] 0
06928# [IARECmp: 4.00; IARECPE: 4.00] 0
06929# R0100:CO0261-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06930# COMPUTE DUALD 1.0 01:FC01 8.24 1.257 Ndate: 28:01 45.83 708.0000
06931# Mjr System / 1.0 02:FC02-M 0.00 0.00 Ndate: 00:00 0.00 n/a 0.000
06932# Mjr System / 1.0 03:FC03-MN 8.24 363 Ndate: 28:00 46.14 n/a 0.000
06933# [MfSystm: 4889E+03; TotOfVol: 0.000E+00; NOfv: 0; TotDurOfv: 0 hrs] 0
06934# R0100:CO0262-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06935# ADD IVD 1.0 02:FC02-M 8.24 363 Ndate: 28:00 46.14 n/a 0.000
06936# SIMM + 1.0 02:FC02-M 0.00 0.00 Ndate: 00:00 0.00 n/a 0.000
06937# SIMM + 1.0 02:FC02-M 8.24 363 Ndate: 27:47 46.14 n/a 0.000
06938# SIMM + 1.0 02:FC02-M 8.24 363 Ndate: 27:47 46.14 n/a 0.000
06939# R0100:CO0263-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06940# CNTLNKX STANDRD 1.0 01:FC01 5.59 264 Ndate: 28:00 45.83 708.0000
06941# [XfMps: 64;TfMps: 64]
06942# [Horton parameters: Fw: 76.20; Fc: 13.20; DCAVd: 14; Fa: 00] 0
06943# [Previous area: IArea: 4.67; SLPD: 00; LG: 40; MNF: 250; SCP: 0] 0
06944# [Impervious area: IArea: 1.57; SLPD: 00; LG: 103; MN: 013; SCL: 0] 0
06945# [IARECmp: 4.00; IARECPE: 4.00] 0
06946# R0100:CO0264-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06947# COMPUTE DUALD 1.0 01:FC01 5.59 264 Ndate: 28:00 45.83 708.0000
06948# Mjr System / 1.0 02:FC02-M 0.00 0.00 Ndate: 00:00 0.00 n/a 0.000
06949# Mjr System / 1.0 03:FC03-MN 5.59 153 Ndate: 27:51 46.12 n/a 0.000
06950# [MfSystm: 5453E+02; TotOfVol: 0.000E+00; NOfv: 0; TotDurOfv: 0 hrs] 0
06951# R0100:CO0265-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06952# ADD IVD 1.0 02:FC02-M 1.59 153 Ndate: 27:51 46.12 n/a 0.000
06953# SIMM + 1.0 02:FC02-M 1.59 153 Ndate: 27:51 46.12 n/a 0.000
06954# SIMM + 1.0 02:FC02-M 1.59 153 Ndate: 27:51 46.12 n/a 0.000
06955# Catchment FRASER
06956# To Fraser-Clarke drain (north of the Jack)
06957# Developed land with assumed 43% imp
06958# 2020-12-17 Change Fraser area to be 35.1 as measured from QOS
06959# 2020-12-17 All Fraser is undeveloped (Nashyd)
06960# R0100:CO0266-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06961# CNTLNKX STANDRD 1.0 01:FC01 13.65 1.447 Ndate: 28:22 26.85 415.0000
06962# [XfMps: 27;TfMps: 27]
06963# [Horton parameters: Fw: 76.20; Fc: 13.20; DCAVd: 14; Fa: 00] 0
06964# [Previous area: IArea: 4.67; SLPD: 00; LG: 40; MNF: 250; SCP: 0] 0
06965# [Impervious area: IArea: 1.57; SLPD: 00; LG: 207; MN: 013; SCL: 0] 0
06966# [IARECmp: 4.00; IARECPE: 4.00] 0
06967# R0100:CO0267-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06968# COMPUTE DUALD 1.0 01:FC01 13.65 1.447 Ndate: 28:22 26.85 415.0000
06969# Mjr System / 1.0 02:FC02-M 21.61 514 Ndate: 28:40 26.85 415.0000
06970# Mjr System / 1.0 03:FC03-MN 13.65 447 Ndate: 28:22 26.85 415.0000
06971# [MfSystm: 31; SLMV: 207.66; SK: 0.010] 0
06972# R0100:CO0268-----DfM n-ID NDD-----AREhA-QPEAKm-TpeakTdh-hh-mm-----Rvmm R C-----Dfwm
06973# ADD IVD 1.0 02:FC02-M 21.61 514 Ndate: 28:40 26.85 415.0000
06974# SIMM + 1.0 02:FC02-M 21.61 514 Ndate: 28:40 26.85 415.0000
06975# SIMM + 1.0 02:FC02-M 21.61 514 Ndate: 28:40 26.85 415.0000
06976# R0100:CO

078555 # License # 2549237
078556 *****
078557 # CALIBRATION OF SUMMER MODEL PARAMETERS
078558 # USING CONTINUES SIMULATIONS
078559 # Rainfall data from JFSA rain gauge installed at site + other gauges by the City
078560 # Use data collected from May to July, 2014.
078561 # 2020-12-01 change TMSTO to COMPUTE TROUDED (TMSTO = 0.1 instead of 0.0001)
078562 # 2020-12-01 correct pond curve values
078563 # 2020-12-01 change WCLSR,RROG to WMP to 0.55,SPL(0.51)%(imperial slope), and LGI up to 700m
078564 # 2021-02-19 Change the slope for ROUTE CHANNEL Station 2462 (NRODout="N,T0") ,NND(NML="SN,T0") from 0.03 % (as per S
078565 # 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (NRODout="N,CE") ,NND(NML="SN,CE") from 0.01 % (as per S
078566 #
078567 R0025:C0002.....
078568 # READ STORM
078569 # Filename = storm001
078570 # Comments = Pluic StcS de 24 hrs [1.25 ans pour Ctawm CDA
078571 # [SDI=10.00;SDRW= 24.00;PTOT= 74.39]
078572 R0025:C0003.....
078573 # MEXIPLY STORM
078574 # [RFACT= 1.00;TSHF= 960.00 m]
078575 # [SERIC=10.00;SDRW= 24.00;PTOT= 74.39]
078576 R0025:C0004.....
078577 # DEFLEAT VALUES
078578 # Filename = T.VPROF1474_16[Design]20201026-QuantityControlAnalysis\SWMM64.SMR-ModelUpdated3.C11.G1.Euf.DEF
078579 # [CASH= 1 (read and print data)
078580 # [FILECITE=File comment:] Based onvarious calibration exercises in Onta
078581 # THE FOLLOWING PARAMETERS ARE USED IN THE DESIGN STANDRD COM
078582 # Horton's infiltration equation parameters:
078583 # [Inp= 20.00 m/hr] [Cw=13.20 m/hr] [DCAV= 4.14 ft] [P= .00 mm]
078584 # Parameters for PERKINS surfaces in STANDRD
078585 # [Ave= 4.67 mm] [Lq=50.00 mm] [M= 250]
078586 # Parameters for IMPERVIOUS surfaces in STANDRD
078587 # [Inp= 1.57 mm] [Cw= 1.50] [M= .013]
078588 # Parameters used in NASHID
078589 # [Inp= 1.57 mm] [Cw= 1.50]
078590 # Average monthly Pan Evaporation data in mm
078591 # JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
078592 # 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
078593 # Average monthly Potential Evapotranspiration in (mm)
078594 # JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
078595 # 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
078596 R0025:C0005.....
078597 # COMPUTE API
078598 # [API= 50.00; APIK= 8500; APIKd= .9999]
078599 # [API= 100.76; APIK= 8500; APIKd= 4.87]
079000 #
079001 # The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)
079002 # of 1.32
079003 R0025:C0006..... Dfn=1-D NND AREHA-QPEAKm-TpeakDte,hh:mm...Rvmm R.C...DWfcm
079004 # CONTI NXS NASHID 1.0 0.01:SW,11 500.00 15.500 No,date 36:57 25.80 n/a 000
079005 # [Cw= 6.0; N= 3.00; Tp= 1.31]
079006 # [AREC= 4.00; SMN= 55.05; SMW=300.32; SK= .010]
079007 # [InterEventTime= 12.00]
079008 #
079009 # The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)
079010 # of 1.32
079011 R0025:C0007..... Dfn=1-D NND AREHA-QPEAKm-TpeakDte,hh:mm...Rvmm R.C...DWfcm
079012 # CONTI NXS NASHID 1.0 0.01:SW,13 971.00 5.778 No,date 32:34 24.02 32.33
079013 # [Cw= 6.0; N= 3.00; Tp= 1.32]
079014 # [AREC= 4.00; SMN= 64.50; SMW=430.01; SK= .010]
079015 # [InterEventTime= 12.00]
079016 #
079017 # The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)
079018 # of 1.30
079019 R0025:C0008..... Dfn=1-D NND AREHA-QPEAKm-TpeakDte,hh:mm...Rvmm R.C...DWfcm
079020 # CONTI NXS NASHID 1.0 0.01:SW,10 3074.00 7.521 No,date 39:59 20.65 27.8
079021 # [Cw= 5.5; N= 3.00; Tp= 1.31]
079022 # [AREC= 4.00; SMN= 83.24; SMW=554.96; SK= .010]
079023 # [InterEventTime= 12.00]
079024 R0025:C0009..... Dfn=1-D NND AREHA-QPEAKm-TpeakDte,hh:mm...Rvmm R.C...DWfcm
079025 # CONTI NXS NASHID 1.0 0.01:SW,8 1781.00 14.166 No,date 32:40 31.50 42.3
079026 # [Cw= 7.0; N= 3.00; Tp= 1.31]
079027 # [AREC= 4.00; SMN= 59.75; SMW=264.99; SK= .010]
079028 # [InterEventTime= 12.00]
079029 R0025:C0010..... Dfn=1-D NND AREHA-QPEAKm-TpeakDte,hh:mm...Rvmm R.C...DWfcm
079030 # CONTI NXS NASHID 1.0 0.01:SW,11 500.00 7.521 No,date 29:22 27.01 36.3
079031 # [Cw= 6.0; N= 3.00; Tp= 1.24]
079032 # [AREC= 4.00; SMN= 52.62; SMW=350.79; SK= .010]
079033 # [InterEventTime= 12.00]
079034 #
079035 # The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)
079036 # of 1.30
079037 R0025:C0011..... Dfn=1-D NND AREHA-QPEAKm-TpeakDte,hh:mm...Rvmm R.C...DWfcm
079038 # CONTI NXS NASHID 1.0 0.01:SW,11 1917.00 10.351 No,date 34:27 27.01 36.3
079039 # [Cw= 6.0; N= 3.00; Tp= 1.31]
079040 # [AREC= 4.00; SMN= 52.62; SMW=350.79; SK= .010]
079041 # [InterEventTime= 12.00]
079042 #
079043 # The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)
079044 # of 1.52
079045 R0025:C0012..... Dfn=1-D NND AREHA-QPEAKm-TpeakDte,hh:mm...Rvmm R.C...DWfcm
079046 # CONTI NXS NASHID 1.0 0.01:SW,10 5666.00 27.457 No,date 37:54 31.50 42.3
079047 # [Cw= 7.0; N= 3.00; Tp= 8.00]
079048 # [AREC= 4.00; SMN= 39.75; SMW=264.99; SK= .010]
079049 # [InterEventTime= 12.00]
079050 #
079051 # The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)
079052 # of 1.75
079053 R0025:C0013..... Dfn=1-D NND AREHA-QPEAKm-TpeakDte,hh:mm...Rvmm R.C...DWfcm
079054 # CONTI NXS NASHID 1.0 0.01:SW,11 876.00 16.276 No,date 39:59 27.01 36.3
079055 # [Cw= 6.0; N= 3.00; Tp= 1.66]
079056 # [AREC= 4.00; SMN= 52.62; SMW=350.79; SK= .010]
079057 # [InterEventTime= 12.00]
079058 #
079059 # The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)
079060 # of 1.68
079061 R0025:C0014..... Dfn=1-D NND AREHA-QPEAKm-TpeakDte,hh:mm...Rvmm R.C...DWfcm
079062 # CONTI NXS NASHID 1.0 0.01:SW,9 1132.00 11.752 No,date 30:54 30.18 40.6
079063 # [Cw= 7.0; N= 3.00; Tp= 1.62]
079064 # [AREC= 4.00; SMN= 43.07; SMW=287.10; SK= .010]
079065 # [InterEventTime= 12.00]
079066 #
079067 # The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)
079068 # of 1.82
079069 R0025:C0015..... Dfn=1-D NND AREHA-QPEAKm-TpeakDte,hh:mm...Rvmm R.C...DWfcm
079070 # CONTI NXS NASHID 1.0 0.01:SW,10 4464.00 13.075 No,date 39:59 24.61 33.1
079071 # [Cw= 6.0; N= 3.00; Tp= 1.32]
079072 # [AREC= 4.00; SMN= 61.90; SMW=412.66; SK= .010]
079073 # [InterEventTime= 12.00]
079074 #
079075 # The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)
079076 # of 1.80
079077 R0025:C0016..... Dfn=1-D NND AREHA-QPEAKm-TpeakDte,hh:mm...Rvmm R.C...DWfcm
079078 # CONTI NXS NASHID 1.0 0.01:SW,8 131.00 2.266 No,date 28:57 25.20 33.9
079079 # [Cw= 6.0; N= 3.00; Tp= .90]
079080 # [AREC= 4.00; SMN= 59.42; SMW=396.11; SK= .010]
079081 # [InterEventTime= 12.00]
079082 #
079083 # The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)
079084 # of 1.65
079085 R0025:C0017..... Dfn=1-D NND AREHA-QPEAKm-TpeakDte,hh:mm...Rvmm R.C...DWfcm
079086 # CONTI NXS NASHID 1.0 0.01:SW,9 3854.00 15.333 No,date 38:34 27.01 36.3
079087 # [Cw= 6.0; N= 3.00; Tp= 1.82]
079088 # [AREC= 4.00; SMN= 52.62; SMW=350.79; SK= .010]
079089 # [InterEventTime= 12.00]
079090 #
079091 # The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)
079092 # of 1.82
079093 R0025:C0018..... Dfn=1-D NND AREHA-QPEAKm-TpeakDte,hh:mm...Rvmm R.C...DWfcm
079094 # CONTI NXS NASHID 1.0 0.01:SW,11 3197.00 11.663 No,date 36:24 21.75 29.2
079095 # [Cw= 7.0; N= 3.00; Tp= 6.65]
079096 # [AREC= 4.00; SMN= 75.32; SMW=508.81; SK= .010]
079097 # [InterEventTime= 12.00]
079098 #
079099 # The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)
079100 # of 1.75
080001 R0025:C0019..... Dfn=1-D NND AREHA-QPEAKm-TpeakDte,hh:mm...Rvmm R.C...DWfcm
080002 # CONTI NXS NASHID 1.0 0.01:SW,6 165.00 1.076 No,date 33:03 27.63 37.1
080003 # [AREC= 4.00; SMN= 50.55; SMW=336.97; SK= .010]
080004 # [InterEventTime= 12.00]
080005 #
080006 # The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)
080007 # of 6.7
080008 R0025:C0020..... Dfn=1-D NND AREHA-QPEAKm-TpeakDte,hh:mm...Rvmm R.C...DWfcm
080009 # CONTI NXS NASHID 1.0 0.01:VG,1R 1332.00 7.882 No,date 35:14 31.50 42.3
080010 # [Cw= 7.0; N= 3.00; Tp= 5.81]
080011 # [AREC= 4.00; SMN= 39.75; SMW=264.99; SK= .010]
080012 # [InterEventTime= 12.00]
080013 #
080014 R0025:C0021..... Dfn=1-D NND AREHA-QPEAKm-TpeakDte,hh:mm...Rvmm R.C...DWfcm
080015 # CONTI NXS NASHID 1.0 0.01:SW,8 224.00 6.882 No,date 28:45 35.66 47.9
080016 # [Cw= 7.0; N= 3.00; Tp= .75]
080017 # [AREC= 4.00; SMN= 31.15; SMW=207.66; SK= .010]
080018 # [InterEventTime= 12.00]
080019 #
080020 # The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)
080021 # of 1.20
080022 R0025:C0022..... Dfn=1-D NND AREHA-QPEAKm-TpeakDte,hh:mm...Rvmm R.C...DWfcm
080023 # CONTI NXS NASHID 1.0 0.01:VG,1R 3945.00 37.664 No,date 33:18 52.85 44.2
080024 # [Cw= 7.0; N= 3.00; Tp= 4.45]
080025 # [AREC= 4.00; SMN= 36.24; SMW=244.99; SK= .010]
080026 # [InterEventTime= 12.00]
080027 R0025:C0023..... Dfn=1-D NND AREHA-QPEAKm-TpeakDte,hh:mm...Rvmm R.C...DWfcm
080028 # CONTI NXS NASHID 1.0 0.01:SW,5A 20.00 .798 No,date 28:35 39.36 52.9
080029 # [Cw= 8.1; N= 3.00; Tp= .62]
080030 # [AREC= 4.00; SMN= 25.21; SMW=168.09; SK= .010]
080031 # [InterEventTime= 12.00]
080032 #
080033 # The Tp was modified according to a Peak Reduction factor (MO-Chart B2-4)
080034 # of 6.1
080035 R0025:C0024..... Dfn=1-D NND AREHA-QPEAKm-TpeakDte,hh:mm...Rvmm R.C...DWfcm
080036 # CONTI NXS NASHID 1.0 0.01:SW,SAI 1412.00 7.480 No,date 37:50 34.24 46.0
080037 # [Cw= 7.0; N= 3.00; Tp= 8.45]
080038 # [AREC= 4.00; SMN= 33.81; SMW=225.43; SK= .010]
080039 # [InterEventTime= 12.00]
080040 R0025:C0025..... Dfn=1-D NND AREHA-QPEAKm-TpeakDte,hh:mm...Rvmm R.C...DWfcm
080041 # CONTI NXS NASHID 1.0 0.01:SW,4 585.00 10.942 No,date 29:56 39.36 52.9

Table with multiple columns containing alphanumeric codes (e.g., ROUTE, ADD HYD), coordinates (e.g., 38743.00, 42.032), and numerical values. The table is organized into sections, likely representing different parts of a hydrological model or project.

Table with columns for ID, Description, Parameters, and Values. Contains thousands of entries detailing various models and results for different projects and locations.

Table with multiple columns containing engineering data, including item numbers, descriptions, dimensions, and material specifications. The table lists various components and their properties across many rows.

100999 COMPUTE DUALDID 1.0 01:00:BE-M 3.29 0.64 N_date 27:34 49.75 n/a 0.000
101000 Mjr System / 1.0 02:00:RO-M 3.29 0.64 N_date 27:34 49.75 n/a 0.000
101001 Mnr System / 1.0 02:00:RO-M 3.29 0.64 N_date 27:34 49.75 n/a 0.000
101002 [M SysStn=11960E03, TotOfVol=0.0000E+00, NOf= 0, TotDirOf=0.0 hrs] 0.000
101003 ROUTE PIPE > 1.0 02:MI05-86 100.98 3.008 N_date 28:08 50.23 n/a 0.000
101004 [RDE 1.00] out < 1.0 01:10:106A 100.98 3.008 N_date 28:02 50.23 n/a 0.000
101005 [L/S/m= 208 / 1000/013] 0.000
101006 [Vmax=1.597;Dmax=1.8] 0.000
101007 [Dn=1.80;Dused=1.80] 0.000
101008
101009 ROUTES: C00357 Dfn=1D NDD AREA= QPEAKm= TpeakDte=hh:mm RvM= R.C. Dfcm
101010 ADD HYD + 1.0 02:36:106A 7.19 6.29 N_date 28:21 50.01 n/a 0.000
101011 [Pervious area: IApr= 4.67;SLLP=0.0;LQP= 40.0;MNP= 250;SCP= 0] 0.000
101012 [Impervious area: IApr= 1.57;SLLP=1.0;LQ= 183.0;MNP= 013;SCL= 0] 0.000
101013 [IARCGmp= 4.00; IARCGper= 4.00] 0.000
101014 [SMN= 33.81; SMM=225.43; SK= 010] 0.000
101015 COMPUTE DUALDID 1.0 01:AO-M 2.44 4.33 N_date 28:00 60.02 n/a 0.000
101016 Mjr System / 1.0 02:AO-M 2.44 4.33 N_date 28:00 60.02 n/a 0.000
101017 Mnr System / 1.0 02:AO-M 2.44 4.33 N_date 28:00 60.02 n/a 0.000
101018 [M SysStn=11960E03, TotOfVol=0.0000E+00, NOf= 0, TotDirOf=0.0 hrs] 0.000
101019 ROUTE PIPE > 1.0 02:MI05-86 100.98 3.008 N_date 28:08 50.23 n/a 0.000
101020 [RDE 1.00] out < 1.0 01:10:106A 100.98 3.008 N_date 28:02 50.23 n/a 0.000
101021 [L/S/m= 208 / 1000/013] 0.000
101022 [Vmax=1.597;Dmax=1.8] 0.000
101023 [Dn=1.80;Dused=1.8] 0.000
101024
101025 ROUTES: C00358 Dfn=1D NDD AREA= QPEAKm= TpeakDte=hh:mm RvM= R.C. Dfcm
101026 CONTINUES STANWHD 1.0 01:AO-M 2.44 4.33 N_date 28:00 60.02 807 0.000
101027 [X Mps: 71; TMs: 41] 0.000
101028 [LQES 2. Cn= 75.0] 0.000
101029 [Pervious area: IApr= 4.67;SLLP=0.0;LQP= 40.0;MNP= 250;SCP= 0] 0.000
101030 [Impervious area: IApr= 1.57;SLLP=1.0;LQ= 183.0;MNP= 013;SCL= 0] 0.000
101031 [IARCGmp= 4.00; IARCGper= 4.00] 0.000
101032 [SMN= 33.81; SMM=225.43; SK= 010] 0.000
101033 COMPUTE DUALDID 1.0 01:AO-M 2.44 4.33 N_date 28:00 60.02 n/a 0.000
101034 Mjr System / 1.0 02:AO-M 2.44 4.33 N_date 28:00 60.02 n/a 0.000
101035 Mnr System / 1.0 02:AO-M 2.44 4.33 N_date 28:00 60.02 n/a 0.000
101036 [M SysStn=11960E03, TotOfVol=0.0000E+00, NOf= 0, TotDirOf=0.0 hrs] 0.000
101037 ROUTE PIPE > 1.0 02:MI05-86 100.98 3.008 N_date 28:08 50.23 n/a 0.000
101038 [RDE 1.00] out < 1.0 01:10:106A 100.98 3.008 N_date 28:02 50.23 n/a 0.000
101039 [L/S/m= 208 / 1000/013] 0.000
101040 [Vmax=1.597;Dmax=1.8] 0.000
101041 [Dn=1.80;Dused=1.8] 0.000
101042
101043 ROUTES: C00361 Dfn=1D NDD AREA= QPEAKm= TpeakDte=hh:mm RvM= R.C. Dfcm
101044 SAVE HYD 1.0 01:MI06 113.90 4.900 N_date 28:01 50.41 n/a 0.000
101045 frame: MI06.0025
101046 remark: Total Flow at MI06A
101047 CONTINUES STANWHD 1.0 01:MI06 113.90 4.900 N_date 28:01 50.41 n/a 0.000
101048 ROUTE PIPE > 1.0 02:MI06-107 113.90 4.900 N_date 28:01 50.41 n/a 0.000
101049 [RDE 1.00] out < 1.0 01:10:107 113.90 4.900 N_date 28:03 50.41 n/a 0.000
101050 [L/S/m= 123 / 1000/035] 0.000
101051 [Vmax=1.676;Dmax=1.544] 0.000
101052 [Dn=1.40;Dused=1.4] 0.000
101053 ROUTES: C00362 Dfn=1D NDD AREA= QPEAKm= TpeakDte=hh:mm RvM= R.C. Dfcm
101054 CONTINUES STANWHD 1.0 01:AO-M 4.14 5.26 N_date 28:01 46.81 629 0.000
101055 [X Mps: 53; TMs: 47] 0.000
101056 [LQES 2. Cn= 75.0] 0.000
101057 [Pervious area: IApr= 4.67;SLLP=0.0;LQP= 40.0;MNP= 250;SCP= 0] 0.000
101058 [Impervious area: IApr= 1.57;SLLP=1.0;LQ= 183.0;MNP= 013;SCL= 0] 0.000
101059 [IARCGmp= 4.00; IARCGper= 4.00] 0.000
101060 [SMN= 33.81; SMM=225.43; SK= 010] 0.000
101061 COMPUTE DUALDID 1.0 01:AO-M 4.14 5.26 N_date 28:01 46.81 n/a 0.000
101062 Mjr System / 1.0 02:AO-M 4.14 5.26 N_date 28:01 46.81 n/a 0.000
101063 Mnr System / 1.0 02:AO-M 4.14 5.26 N_date 28:01 46.81 n/a 0.000
101064 [M SysStn=11960E03, TotOfVol=0.0000E+00, NOf= 0, TotDirOf=0.0 hrs] 0.000
101065 ROUTE PIPE > 1.0 02:MI06-107 113.90 4.900 N_date 28:01 50.41 n/a 0.000
101066 [RDE 1.00] out < 1.0 01:10:107 113.90 4.900 N_date 28:03 50.41 n/a 0.000
101067 [L/S/m= 123 / 1000/035] 0.000
101068 [Vmax=1.676;Dmax=1.544] 0.000
101069 [Dn=1.40;Dused=1.4] 0.000
101070
101071 ROUTES: C00366 Dfn=1D NDD AREA= QPEAKm= TpeakDte=hh:mm RvM= R.C. Dfcm
101072 COMPUTE DUALDID 1.0 01:AO-M 10.61 1.911 N_date 28:01 54.09 n/a 0.000
101073 Mjr System / 1.0 02:AO-M 10.61 1.911 N_date 28:03 54.09 n/a 0.000
101074 Mnr System / 1.0 02:AO-M 10.61 1.911 N_date 27:54 54.21 n/a 0.000
101075 [M SysStn=2791E01, TotOfVol=0.0000E+00, NOf= 0, TotDirOf=0.0 hrs] 0.000
101076 ROUTE PIPE > 1.0 02:MI07 128.65 5.370 N_date 28:03 50.61 n/a 0.000
101077 [RDE 1.00] out < 1.0 01:10:107 128.65 5.370 N_date 28:03 50.61 n/a 0.000
101078 [L/S/m= 31.81; SMM=225.43; SK= 010] 0.000
101079 ADD HYD + 1.0 02:36:107 113.90 4.900 N_date 28:03 50.41 n/a 0.000
101080 [Pervious area: IApr= 4.67;SLLP=0.0;LQP= 40.0;MNP= 250;SCP= 0] 0.000
101081 [Impervious area: IApr= 1.57;SLLP=1.0;LQ= 183.0;MNP= 013;SCL= 0] 0.000
101082 [IARCGmp= 4.00; IARCGper= 4.00] 0.000
101083 [SMN= 33.81; SMM=225.43; SK= 010] 0.000
101084 COMPUTE DUALDID 1.0 01:AO-M 10.61 1.911 N_date 28:01 54.09 n/a 0.000
101085 Mjr System / 1.0 02:AO-M 10.61 1.911 N_date 28:03 54.09 n/a 0.000
101086 Mnr System / 1.0 02:AO-M 10.61 1.911 N_date 27:54 54.21 n/a 0.000
101087 [M SysStn=2791E01, TotOfVol=0.0000E+00, NOf= 0, TotDirOf=0.0 hrs] 0.000
101088 ROUTE PIPE > 1.0 02:MI07 128.65 5.370 N_date 28:03 50.61 n/a 0.000
101089 [RDE 1.00] out < 1.0 01:10:107 128.65 5.370 N_date 28:03 50.61 n/a 0.000
101090 [L/S/m= 31.81; SMM=225.43; SK= 010] 0.000
101091 [Vmax=1.922;Dmax=1.633] 0.000
101092 [Dn=1.80;Dused=2.0] 0.000
101093
101094 ROUTES: C00371 Dfn=1D NDD AREA= QPEAKm= TpeakDte=hh:mm RvM= R.C. Dfcm
101095 CONTINUES STANWHD 1.0 01:AO-M 12.29 1.704 N_date 28:01 49.75 669 0.000
101096 [X Mps: 41; TMs: 54] 0.000
101097 [LQES 2. Cn= 75.0] 0.000
101098 [Pervious area: IApr= 4.67;SLLP=0.0;LQP= 40.0;MNP= 250;SCP= 0] 0.000
101099 [Impervious area: IApr= 1.57;SLLP=1.0;LQ= 183.0;MNP= 013;SCL= 0] 0.000
101100 [IARCGmp= 4.00; IARCGper= 4.00] 0.000
101101 [SMN= 33.81; SMM=225.43; SK= 010] 0.000
101102 COMPUTE DUALDID 1.0 01:AO-M 12.29 1.704 N_date 28:01 49.75 n/a 0.000
101103 Mjr System / 1.0 02:AO-M 12.29 1.704 N_date 28:03 49.75 n/a 0.000
101104 Mnr System / 1.0 02:AO-M 12.29 1.704 N_date 27:52 49.91 n/a 0.000
101105 [M SysStn=558E03, TotOfVol=0.0000E+00, NOf= 0, TotDirOf=0.0 hrs] 0.000
101106 ROUTE PIPE > 1.0 02:MI08 143.53 6.791 N_date 28:03 50.72 n/a 0.000
101107 [RDE 1.00] out < 1.0 01:10:108 143.53 6.791 N_date 28:05 50.72 n/a 0.000
101108 [L/S/m= 71 / 1300/013] 0.000
101109 [Vmax=2.100;Dmax=1.778] 0.000
101110 [Dn=1.80;Dused=2.1] 0.000
101111
101112 ROUTES: C00379 Dfn=1D NDD AREA= QPEAKm= TpeakDte=hh:mm RvM= R.C. Dfcm
101113 COMPUTE DUALDID 1.0 01:AO-M 2.59 4.35 N_date 28:01 60.02 807 0.000
101114 Mjr System / 1.0 02:AO-M 2.59 4.35 N_date 28:01 60.02 n/a 0.000
101115 Mnr System / 1.0 02:AO-M 2.59 4.35 N_date 28:01 60.02 n/a 0.000
101116 [M SysStn=558E03, TotOfVol=0.0000E+00, NOf= 0, TotDirOf=0.0 hrs] 0.000
101117 ROUTE PIPE > 1.0 02:MI08 143.53 6.791 N_date 28:03 50.72 n/a 0.000
101118 [RDE 1.00] out < 1.0 01:10:110 143.53 6.791 N_date 28:05 50.72 n/a 0.000
101119 [L/S/m= 71 / 1300/013] 0.000
101120 [Vmax=2.100;Dmax=1.778] 0.000
101121 [Dn=1.80;Dused=2.1] 0.000
101122
101123 ROUTES: C00380 Dfn=1D NDD AREA= QPEAKm= TpeakDte=hh:mm RvM= R.C. Dfcm
101124 CONTINUES STANWHD 1.0 01:AO-M 12.29 1.704 N_date 28:01 49.75 669 0.000
101125 [X Mps: 41; TMs: 54] 0.000
101126 [LQES 2. Cn= 75.0] 0.000
101127 [Pervious area: IApr= 4.67;SLLP=0.0;LQP= 40.0;MNP= 250;SCP= 0] 0.000
101128 [Impervious area: IApr= 1.57;SLLP=1.0;LQ= 183.0;MNP= 013;SCL= 0] 0.000
101129 [IARCGmp= 4.00; IARCGper= 4.00] 0.000
101130 [SMN= 33.81; SMM=225.43; SK= 010] 0.000
101131 COMPUTE DUALDID 1.0 01:AO-M 2.59 4.35 N_date 28:01 60.02 807 0.000
101132 Mjr System / 1.0 02:AO-M 2.59 4.35 N_date 28:01 60.02 n/a 0.000
101133 Mnr System / 1.0 02:AO-M 2.59 4.35 N_date 28:01 60.02 n/a 0.000
101134 [M SysStn=558E03, TotOfVol=0.0000E+00, NOf= 0, TotDirOf=0.0 hrs] 0.000
101135 ROUTE PIPE > 1.0 02:MI08 143.53 6.791 N_date 28:03 50.72 n/a 0.000
101136 [RDE 1.00] out < 1.0 01:10:110 143.53 6.791 N_date 28:05 50.72 n/a 0.000
101137 [L/S/m= 80 / 1300/013] 0.000
101138 [Vmax=2.099;Dmax=1.572] 0.000
101139 [Dn=1.80;Dused=2.1] 0.000
101140
101141 ROUTES: C00394 Dfn=1D NDD AREA= QPEAKm= TpeakDte=hh:mm RvM= R.C. Dfcm
101142 SAVE HYD 1.0 01:MI07 128.65 5.370 N_date 28:03 50.61 n/a 0.000
101143 frame: MI07.0025
101144 remark: Total Flow at MI07
101145 CONTINUES STANWHD 1.0 01:MI07 128.65 5.370 N_date 28:03 50.61 n/a 0.000
101146 ROUTE PIPE > 1.0 02:MI08 143.53 6.791 N_date 28:03 50.72 n/a 0.000
101147 [RDE 1.00] out < 1.0 01:10:111 143.53 6.791 N_date 28:05 50.72 n/a 0.000
101148 [L/S/m= 71 / 1300/013] 0.000
101149 [Vmax=2.100;Dmax=1.778] 0.000
101150 [Dn=1.80;Dused=2.1] 0.000
101151
101152 ROUTES: C00398 Dfn=1D NDD AREA= QPEAKm= TpeakDte=hh:mm RvM= R.C. Dfcm
101153 COMPUTE DUALDID 1.0 01:AO-M 2.59 4.35 N_date 28:01 60.02 807 0.000
101154 Mjr System / 1.0 02:AO-M 2.59 4.35 N_date 28:01 60.02 n/a 0.000
101155 Mnr System / 1.0 02:AO-M 2.59 4.35 N_date 28:01 60.02 n/a 0.000
101156 [M SysStn=558E03, TotOfVol=0.0000E+00, NOf= 0, TotDirOf=0.0 hrs] 0.000
101157 ROUTE PIPE > 1.0 02:MI08 143.53 6.791 N_date 28:03 50.72 n/a 0.000
101158 [RDE 1.00] out < 1.0 01:10:111 143.53 6.791 N_date 28:05 50.72 n/a 0.000
101159 [L/S/m= 80 / 1300/013] 0.000
101160 [Vmax=2.099;Dmax=1.572] 0.000
101161 [Dn=1.80;Dused=2.1] 0.000
101162
101163 ROUTES: C00400 Dfn=1D NDD AREA= QPEAKm= TpeakDte=hh:mm RvM= R.C. Dfcm
101164 CONTINUES STANWHD 1.0 01:AO-M 12.29 1.704 N_date 28:01 49.75 669 0.000
101165 [X Mps: 41; TMs: 54] 0.000
101166 [LQES 2. Cn= 75.0] 0.000
101167 [Pervious area: IApr= 4.67;SLLP=0.0;LQP= 40.0;MNP= 250;SCP= 0] 0.000
101168 [Impervious area: IApr= 1.57;SLLP=1.0;LQ= 183.0;MNP= 013;SCL= 0] 0.000
101169 [IARCGmp= 4.00; IARCGper= 4.00] 0.000
101170 [SMN= 33.81; SMM=225.43; SK= 010] 0.000
101171 COMPUTE DUALDID 1.0 01:AO-M 12.29 1.704 N_date 28:01 49.75 n/a 0.000
101172 Mjr System / 1.0 02:AO-M 12.29 1.704 N_date 28:03 49.75 n/a 0.000
101173 Mnr System / 1.0 02:AO-M 12.29 1.704 N_date 27:52 49.91 n/a 0.000
101174 [M SysStn=558E03, TotOfVol=0.0000E+00, NOf= 0, TotDirOf=0.0 hrs] 0.000
101175 ROUTE PIPE > 1.0 02:MI08 143.53 6.791 N_date 28:03 50.72 n/a 0.000
101176 [RDE 1.00] out < 1.0 01:10:111 143.53 6.791 N_date 28:05 50.72 n/a 0.000
101177 [L/S/m= 77 / 1300/013] 0.000
101178 [Vmax=2.100;Dmax=1.778] 0.000
101179 [Dn=1.80;Dused=2.1] 0.000
101180
101181 ROUTES: C00401 Dfn=1D NDD AREA= QPEAKm= TpeakDte=hh:mm RvM= R.C. Dfcm
101182 COMPUTE DUALDID 1.0 01:AO-M 2.59 4.35 N_date 28:01 60.02 807 0.000
101183 Mjr System / 1.0 02:AO-M 2.59 4.35 N_date 28:01 60.02 n/a 0.000
101184 Mnr System / 1.0 02:AO-M 2.59 4.35 N_date 28:01 60.02 n/a 0.000
101185 [M SysStn=558E03, TotOfVol=0.0000E+00, NOf= 0, TotDirOf=0.0 hrs] 0.000
101186 ROUTE PIPE > 1.0 02:MI08 143.53 6.791 N_date 28:03 50.72 n/a 0.000
101187 [RDE 1.00] out < 1.0 01:10:112 143.53 6.791 N_date 28:05 50.72 n/a 0.000
101188 [L/S/m= 80 / 1300/013] 0.000
101189 [Vmax=2.099;Dmax=1.572] 0.000
101190 [Dn=1.80;Dused=2.1] 0.000
101191
101192 ROUTES: C00402 Dfn=1D NDD AREA= QPEAKm= TpeakDte=hh:mm RvM= R.C. Dfcm
101193 CONTINUES STANWHD 1.0 01:AO-M 12.29 1.704 N_date 28:01 49.75 669 0.000
101194 [X Mps: 41; TMs: 54] 0.000
101195 [LQES 2. Cn= 75.0] 0.000
101196 [Pervious area: IApr= 4.67;SLLP=0.0;LQP= 40.0;MNP= 250;SCP= 0] 0.000
101197 [Impervious area: IApr= 1.57;SLLP=1.0;LQ= 183.0;MNP= 013;SCL= 0] 0.000
101198 [IARCGmp= 4.00; IARCGper= 4.00] 0.000
101199 [SMN= 33.81; SMM=225.43; SK= 010] 0.000
101200 COMPUTE DUALDID 1.0 01:AO-M 12.29 1.704 N_date 28:01 49.75 n/a 0.000
101201 Mjr System / 1.0 02:AO-M 12.29 1.704 N_date 28:03 49.75 n/a 0.000
101202 Mnr System / 1.0 02:AO-M 12.29 1.704 N_date 27:52 49.91 n/a 0.000
101203 [M SysStn=558E03, TotOfVol=0.0000E+00, NOf= 0, TotDirOf=0.0 hrs] 0.000
101204 ROUTE PIPE > 1.0 02:MI08 143.53 6.791 N_date 28:03 50.72 n/a 0.000
101205 [RDE 1.00] out < 1.0 01:10:112 143.53 6.791 N_date 28:05 50.72 n/a 0.000
101206 [L/S/m= 80 / 1300/013] 0.000
101207 [Vmax=2.099;Dmax=1.572] 0.000
101208 [Dn=1.80;Dused=2.1] 0.000
101209
101210 ROUTES: C00403 Dfn=1D NDD AREA= QPEAKm= TpeakDte=hh:mm RvM= R.C. Dfcm
101211 CONTINUES STANWHD 1.0 01:AO-M 12.29 1.704 N_date 28:01 49.75 669 0.000
101212 [X Mps: 41; TMs: 54] 0.000
101213 [LQES 2. Cn= 75.0] 0.000
101214 [Pervious area: IApr= 4.67;SLLP=0.0;LQP= 40.0;MNP= 250;SCP= 0] 0.000
101215 [Impervious area: IApr= 1.57;SLLP=1.0;LQ= 183.0;MNP= 013;SCL= 0] 0.000
101216 [IARCGmp= 4.00; IARCGper= 4.00] 0.000
101217 [SMN= 33.81; SMM=225.43; SK= 010] 0.000
101218 COMPUTE DUALDID 1.0 01:AO-M 12.29 1.704 N_date 28:01 49.75 n/a 0.000
101219 Mjr System / 1.0 02:AO-M 12.29 1.704 N_date 28:03 49.75 n/a 0.000
101220 Mnr System / 1.0 02:AO-M 12.29 1.704 N_date 27:52 49.91 n/a 0.000
101221 [M SysStn=558E03, TotOfVol=0.0000E+00, NOf= 0, TotDirOf=0.0 hrs] 0.000
101222 ROUTE PIPE > 1.0 02:MI08 143.53 6.791 N_date 28:03 50.72 n/a 0.000
101223 [RDE 1.00] out < 1.0 01:10:113 143.53 6.791 N_date 28:05 50.72 n/a 0.000
101224 [L/S/m= 77 / 1300/013] 0.000
101225 [Vmax=2.100;Dmax=1.778] 0.000
101226 [Dn=1.80;Dused=2.1] 0.000
101227
101228 ROUTES: C00404 Dfn=1D NDD AREA= QPEAKm= TpeakDte=hh:mm RvM= R.C. Dfcm
101229 COMPUTE DUALDID 1.0 01:AO-M 2.59 4.35 N_date 28:01 60.02 807 0.000
101230 Mjr System / 1.0 02:AO-M 2.59 4.35 N_date 28:01 60.02 n/a 0.000
101231 Mnr System / 1.0 02:AO-M 2.59 4.35 N_date 28:01 60.02 n/a 0.000
101232 [M SysStn=558E03, TotOfVol=0.0000E+00, NOf= 0, TotDirOf=0.0 hrs] 0.000
101233 ROUTE PIPE > 1.0 02:MI08 143.53 6.791 N_date 28:03 50.72 n/a 0.000
101234 [RDE 1.00] out < 1.0 01:10:113 143.53 6.791 N_date 28:05 50.72 n/a 0.000
101235 [L/S/m= 80 / 1300/013] 0.000
101236 [Vmax=2.099;Dmax=1.572] 0.000
101237 [Dn=1.80;Dused=2.1] 0.000
101238
101239 ROUTES: C00405 Dfn=1D NDD AREA= QPEAKm= TpeakDte=hh:mm RvM= R.C. Dfcm
101240 CONTINUES STANWHD 1.0 01:AO-M 12.29 1.704 N_date 28:01 49.75 669 0.000
101241 [X Mps: 41; TMs: 54] 0.000
101242 [LQES 2. Cn= 75.0] 0.000
101243 [Pervious area: IApr= 4.67;SLLP=0.0;LQP= 40.0;MNP= 250;SCP= 0] 0.000
101244 [Impervious area: IApr= 1.57;SLLP=1.0;LQ= 183.0;MNP= 013;SCL= 0] 0.000
101245 [IARCGmp= 4.00; IARCGper= 4.00] 0.000
101246 [SMN= 33.81; SMM=225.43; SK= 010] 0.000
101247 COMPUTE DUALDID 1.0 01:AO-M 12.29 1.704 N_date 28:01 49.75 n/a 0.000
101248 Mjr System / 1.0 02:AO-M 12.29 1.704 N_date 28:03 49.75 n/a 0.000
101249 Mnr System / 1.0 02:AO-M 12.29 1.704 N_date 27:52 49.91 n/a 0.000
101250 [M SysStn=558E03, TotOfVol=0.0000E+00, NOf= 0, TotDirOf=0.0 hrs] 0.000
101251 ROUTE PIPE > 1.0 02:MI08 143.53 6.791 N_date 28:03 50.72 n/a 0.000
101252 [RDE 1.00] out < 1.0 01:10:114 143.53 6.791 N_date 28:05 50.72 n/a 0.000
101253 [L/S/m= 80 / 1300/013] 0.000
101254 [Vmax=2.099;Dmax=1.572] 0.000
101255 [Dn=1.80;Dused=2.1] 0.000
101256
101257 ROUTES: C00406 Dfn=1D NDD AREA= QPEAKm= TpeakDte=hh:mm RvM= R.C. Dfcm

Table with columns: ID, Description, Node, Elevation, Flow, etc. Contains detailed engineering data for various subwatershed and routing models.

Table with columns: ID, Name, Parameters, Values, Units, and Notes. The table lists numerous hydrological and environmental data points, including flow rates, storage volumes, and model identifiers. It is organized into sections such as CONTINUES STANDBY, ROUTE RESERVOIR, and various hydrograph and channel section descriptions.


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119009 R0505:CD0236.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
119070 CONT NEXS STANDRD 1.0 01:FC02 7.24 18.24 NaDate 28:00 64.30 789 000
119173 [XMap: 75.T1Map: 71]
119172 (Perivus area: Iper: 4.67.SLPP: 00.LGP: 40.MNF: 250.SCP: 0)
119173 (Impervius area: Iimp: 16.SLPI: 30.LGA: 151.MN: 013.SCI: 0)
119175 [IARECmp: 4.00: IARECPE: 4.00]
119176 R0505:CD0237.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
119177 ADD IVD + 1.0 02:FC02-MN 1.00 00.00 NaDate 28:00 0.00 n/a 000
119178 + 1.0 02:KB-Pond3 254.24 22.89 NaDate 28:00 46.87 n/a 000
119179 + 1.0 02:FC02-MN 1.00 00.00 NaDate 28:00 0.00 n/a 000
119180 + 1.0 02:KB-Pond3 254.24 22.89 NaDate 28:00 46.87 n/a 000
119181 + 1.0 02:FC02-MN 1.00 00.00 NaDate 28:00 0.00 n/a 000
119182 + 1.0 02:KB-Pond3 254.24 22.89 NaDate 28:00 46.87 n/a 000
119183 + 1.0 02:FC02-MN 1.00 00.00 NaDate 28:00 0.00 n/a 000
119184 + 1.0 02:KB-Pond3 254.24 22.89 NaDate 28:00 46.87 n/a 000
119185 + 1.0 02:FC02-MN 1.00 00.00 NaDate 28:00 0.00 n/a 000
119186 + 1.0 02:KB-Pond3 254.24 22.89 NaDate 28:00 46.87 n/a 000
119187 + 1.0 02:FC02-MN 1.00 00.00 NaDate 28:00 0.00 n/a 000
119188 R0505:CD0238.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
119189 ROUTE RESERVOIR 1.0 01:FR01 1.14 2.57 NaDate 28:09 46.87 n/a 000
119190 out_cw 1.0 01:KB-PFR 253.10 17.63 NaDate 28:09 46.87 n/a 000
119191 + 1.0 02:FC02-MN 1.00 00.00 NaDate 28:00 0.00 n/a 000
119192 [MSStoEd: 1109E02 mh, TotOfVol: 5.551E-01 mh, N.OfV: 1. TotDurOfV: 0 hrs]
119193 R0505:CD0239.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
119194 ADD IVD + 1.0 02:KB-Pond3 253.10 17.63 NaDate 28:09 46.87 n/a 000
119195 + 1.0 02:KB-Pond3 1.14 2.57 NaDate 28:09 46.87 n/a 000
119196 SIM + 1.0 01:FR02-MN 8.24 5.63 NaDate 28:59 59.28 n/a 000
119197 R0505:CD0240.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
119198 SAVE IVD 1.0 01:FR02-MN 8.24 5.63 NaDate 28:59 59.28 n/a 000
119199 name: KB-Pond3.0050
120001 remark: Total Flow at KB second pond
120002 R0505:CD0241.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120003 CONT NEXS STANDRD 1.0 01:KB-Pond3 2.80 6.24 NaDate 28:00 66.65 818 000
120004 [XMap: 75.T1Map: 71]
120005 (Perivus area: Iper: 4.67.SLPP: 00.LGP: 40.MNF: 250.SCP: 0)
120006 (Impervius area: Iimp: 16.SLPI: 30.LGA: 151.MN: 013.SCI: 0)
120007 [IARECmp: 4.00: IARECPE: 4.00]
120008 R0505:CD0242.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120009 ADD IVD + 1.0 02:KB-Pond3 254.24 22.89 NaDate 28:09 46.87 n/a 000
120010 + 1.0 02:KB-Pond3 254.24 22.89 NaDate 28:09 46.87 n/a 000
120011 SIM + 1.0 01:KB-PF 257.04 23.14 NaDate 28:09 47.08 n/a 000
120012 R0505:CD0243.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120013 ROUTE RESERVOIR 1.0 01:FR01 257.04 13.47 NaDate 28:09 47.08 n/a 000
120014 out_cw 1.0 01:KB-PFR 9.40 0.51 NaDate 17:13 47.07 n/a 000
120015 + 1.0 02:FC02-MN 1.00 00.00 NaDate 28:00 0.00 n/a 000
120016 [MSStoEd: 1988E-02 mh, TotOfVol: 1.166E+02 mh, N.OfV: 1. TotDurOfV: 23 hrs]
120017 R0505:CD0244.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120018 ADD IVD + 1.0 02:KB-Pond3 254.24 22.89 NaDate 28:09 46.87 n/a 000
120019 + 1.0 02:KB-Pond3 247.64 22.26 NaDate 28:10 47.08 n/a 000
120020 SIM + 1.0 02:KB-Pond3 247.64 22.26 NaDate 28:10 47.08 n/a 000
120021 R0505:CD0245.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120022 SAVE IVD 1.0 01:KB-Pond3 257.04 23.14 NaDate 28:10 47.08 n/a 000
120023 name: KB-Pond3.0050
120024 remark: Total Flow at KB third pond
120025 *****
120026 # ESTMGT / PROPOSED Subcatchments (Kennedy-Burnett SWM Facility (118000)), SWM Modeling Approach, NOWATECH Report Ju
120027 # TO FRASER CLARKE
120028 *****
120029 R0505:CD0246.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120030 CONT NEXS STANDRD 1.0 01:FC01 8.03 18.83 NaDate 28:00 49.52 608 000
120031 [XMap: 47.T1Map: 47]
120032 (Perivus area: Iper: 4.67.SLPP: 00.LGP: 40.MNF: 250.SCP: 0)
120033 (Impervius area: Iimp: 16.SLPI: 30.LGA: 151.MN: 013.SCI: 0)
120034 [IARECmp: 4.00: IARECPE: 4.00]
120035 R0505:CD0247.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120036 COMPUTE DUALIND 1.0 01:FC03 7.37 1.54 NaDate 28:00 59.28 n/a 000
120037 Mjur System \ 1.0 03:FC02-MN 0.00 0.00 NaDate 00:00 0.00 n/a 000
120038 Mjur System / 1.0 03:FC02-MN 0.00 0.00 NaDate 00:00 0.00 n/a 000
120039 Mjur System \ 1.0 03:FC03-MN 7.35 358 NaDate 27:42 59.51 n/a 000
120040 [MSystem: 348E+02 mh, TotOfVol: 0.00E+00 mh, N.OfV: 0. TotDurOfV: 0 hrs]
120041 R0505:CD0248.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120042 ADD IVD + 1.0 02:FC01-MN 0.00 0.00 NaDate 00:00 0.00 n/a 000
120043 + 1.0 02:FC02-MN 8.03 756 NaDate 27:51 49.91 n/a 000
120044 SIM + 1.0 01:FR02-MN 8.03 756 NaDate 27:51 49.91 n/a 000
120045 R0505:CD0249.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120046 CONT NEXS STANDRD 1.0 01:FC02 16.05 3.33 NaDate 28:00 75.92 931 000
120047 [XMap: 93.T1Map: 93]
120048 (Perivus area: Iper: 4.67.SLPP: 00.LGP: 40.MNF: 250.SCP: 0)
120049 (Impervius area: Iimp: 16.SLPI: 30.LGA: 151.MN: 013.SCI: 0)
120050 [IARECmp: 4.00: IARECPE: 4.00]
120051 R0505:CD0250.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120052 COMPUTE DUALIND 1.0 01:FC03 16.05 3.33 NaDate 28:00 75.92 n/a 000
120053 Mjur System \ 1.0 03:FC02-MN 0.00 0.00 NaDate 00:00 0.00 n/a 000
120054 Mjur System / 1.0 03:FC02-MN 0.00 0.00 NaDate 00:00 0.00 n/a 000
120055 Mjur System \ 1.0 03:FC03-MN 16.05 1159 NaDate 27:43 59.94 n/a 000
120056 [MSystem: 348E+02 mh, TotOfVol: 0.00E+00 mh, N.OfV: 0. TotDurOfV: 0 hrs]
120057 R0505:CD0251.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120058 ADD IVD + 1.0 02:FC02-MN 16.05 1159 NaDate 27:43 59.94 n/a 000
120059 + 1.0 02:FC02-MN 16.05 1159 NaDate 27:43 59.94 n/a 000
120060 SIM + 1.0 01:FR02-MN 16.05 1159 NaDate 27:43 59.94 n/a 000
120061 R0505:CD0252.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120062 CONT NEXS STANDRD 1.0 01:FC03 7.37 1.54 NaDate 28:00 59.28 727 000
120063 [XMap: 31.T1Map: 64]
120064 (Perivus area: Iper: 4.67.SLPP: 00.LGP: 40.MNF: 250.SCP: 0)
120065 (Impervius area: Iimp: 16.SLPI: 30.LGA: 151.MN: 013.SCI: 0)
120066 [IARECmp: 4.00: IARECPE: 4.00]
120067 R0505:CD0253.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120068 COMPUTE DUALIND 1.0 01:FC03 7.37 1.54 NaDate 28:00 59.28 n/a 000
120069 Mjur System \ 1.0 03:FC02-MN 7.35 358 NaDate 27:42 59.51 n/a 000
120070 Mjur System / 1.0 03:FC02-MN 7.35 358 NaDate 27:42 59.51 n/a 000
120071 Mjur System \ 1.0 03:FC03-MN 7.35 358 NaDate 27:42 59.51 n/a 000
120072 [MSystem: 131E+02 mh, TotOfVol: 0.00E+00 mh, N.OfV: 0. TotDurOfV: 0 hrs]
120073 R0505:CD0254.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120074 ADD IVD + 1.0 02:FC03-MN 0.02 0.92 NaDate 28:14 59.28 n/a 000
120075 + 1.0 02:FC03-MN 7.35 358 NaDate 28:14 59.28 n/a 000
120076 SIM + 1.0 01:FR02-MN 7.35 358 NaDate 28:14 59.28 n/a 000
120077 R0505:CD0255.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120078 CONT NEXS STANDRD 1.0 01:FC04 12.87 2.58 NaDate 28:01 59.28 727 000
120079 [XMap: 64.T1Map: 64]
120080 (Perivus area: Iper: 4.67.SLPP: 00.LGP: 40.MNF: 250.SCP: 0)
120081 (Impervius area: Iimp: 16.SLPI: 30.LGA: 151.MN: 013.SCI: 0)
120082 [IARECmp: 4.00: IARECPE: 4.00]
120083 R0505:CD0256.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120084 COMPUTE DUALIND 1.0 01:FC04 12.87 2.58 NaDate 28:01 59.28 n/a 000
120085 Mjur System \ 1.0 03:FC04-MN 0.00 0.00 NaDate 00:00 0.00 n/a 000
120086 Mjur System / 1.0 03:FC04-MN 0.00 0.00 NaDate 00:00 0.00 n/a 000
120087 Mjur System \ 1.0 03:FR02-MN 12.87 241 NaDate 27:44 59.54 n/a 000
120088 [MSystem: 1729E+02 mh, TotOfVol: 0.00E+00 mh, N.OfV: 0. TotDurOfV: 0 hrs]
120089 R0505:CD0257.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120090 ADD IVD + 1.0 02:FC04-MN 0.00 0.00 NaDate 00:00 0.00 n/a 000
120091 + 1.0 02:FC04-MN 12.87 241 NaDate 27:44 59.54 n/a 000
120092 SIM + 1.0 01:FR02-MN 12.87 241 NaDate 27:44 59.54 n/a 000
120093 R0505:CD0258.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120094 # PROPOSED Subcatchments (Kennedy-Burnett SWM Facility (118000)), SWM Modeling Approach, NOWATECH Report June, 2020)
120095 # TO JACK RIVER
120096 *****
120097 R0505:CD0259.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120098 CONT NEXS STANDRD 1.0 01:FR01 8.24 1.74 NaDate 28:00 59.28 727 000
120099 [XMap: 64.T1Map: 64]
120100 (Perivus area: Iper: 4.67.SLPP: 00.LGP: 40.MNF: 250.SCP: 0)
120101 (Impervius area: Iimp: 16.SLPI: 30.LGA: 151.MN: 013.SCI: 0)
120102 [IARECmp: 4.00: IARECPE: 4.00]
120103 R0505:CD0260.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120104 COMPUTE DUALIND 1.0 01:FR02 0.1 1.59 357 NaDate 28:00 59.28 n/a 000
120105 Mjur System \ 1.0 03:FR02-MN 0.1 1.59 357 NaDate 27:45 59.66 n/a 000
120106 Mjur System / 1.0 03:FR02-MN 0.1 1.59 357 NaDate 27:45 59.66 n/a 000
120107 Mjur System \ 1.0 03:FR03-MN 8.24 5.63 NaDate 28:59 59.28 n/a 000
120108 [MSystem: 964E+03 mh, TotOfVol: 0.00E+00 mh, N.OfV: 0. TotDurOfV: 0 hrs]
120109 R0505:CD0261.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120110 ADD IVD + 1.0 02:FR01-MN 8.24 5.63 NaDate 28:59 59.28 n/a 000
120111 + 1.0 02:FR01-MN 8.24 5.63 NaDate 27:44 59.48 n/a 000
120112 SIM + 1.0 01:FR02-MN 8.24 5.63 NaDate 27:44 59.48 n/a 000
120113 R0505:CD0262.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120114 CONT NEXS STANDRD 1.0 01:FR02 1.59 357 NaDate 28:00 59.28 727 000
120115 [XMap: 64.T1Map: 64]
120116 (Perivus area: Iper: 4.67.SLPP: 00.LGP: 40.MNF: 250.SCP: 0)
120117 (Impervius area: Iimp: 16.SLPI: 30.LGA: 151.MN: 013.SCI: 0)
120118 [IARECmp: 4.00: IARECPE: 4.00]
120119 R0505:CD0263.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120120 COMPUTE DUALIND 1.0 01:FR02 1.59 357 NaDate 28:00 59.28 n/a 000
120121 Mjur System \ 1.0 03:FR02-MN 1.59 153 NaDate 27:45 59.66 n/a 000
120122 Mjur System / 1.0 03:FR02-MN 1.59 153 NaDate 27:45 59.66 n/a 000
120123 Mjur System \ 1.0 03:FR03-MN 8.24 5.63 NaDate 28:59 59.28 n/a 000
120124 [MSystem: 1191E+03 mh, TotOfVol: 0.00E+00 mh, N.OfV: 0. TotDurOfV: 0 hrs]
120125 R0505:CD0264.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120126 ADD IVD + 1.0 02:FR02-MN 0.00 0.00 NaDate 00:00 0.00 n/a 000
120127 + 1.0 02:FR02-MN 1.59 153 NaDate 27:45 59.66 n/a 000
120128 SIM + 1.0 01:FR02-MN 1.59 153 NaDate 27:45 59.66 n/a 000
120129 *****
120130 # Catchment FRASER
120131 # TO FRASER CLARKE drain (north of the Jack)
120132 # Developed land with 13 ha measured from QRS
120133 # 2020-12-17 Change Fraser area to be 15.1 ha measured from QRS
120134 # 2020-12-17 Change Fraser area to be 15.1 ha measured from QRS
120135 *****
120136 R0505:CD0267.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120137 CONT NEXS STANDRD 1.0 01:FRASER-D 21.61 816 NaDate 28:40 39.91 490 000
120138 [IAREC: 4.00: SIM: 31.15: SMM: 207.66: SK: 010]
120139 [InterEventTime: 12.00]
120140 R0505:CD0268.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120141 CONT NEXS STANDRD 1.0 01:FRASER-D 21.61 816 NaDate 28:40 39.91 490 000
120142 [IAREC: 4.00: SIM: 31.15: SMM: 207.66: SK: 010]
120143 [InterEventTime: 12.00]
120144 R0505:CD0269.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
120145 ADD IVD + 1.0 02:KB-Pond3 257.04 23.14 NaDate 28:10 47.08 n/a 000
120146 + 1.0 02:KB-Pond3 254.24 22.89 NaDate 28:00 46.87 n/a 000
120147 + 1.0 02:FRASER-D 21.61 816 NaDate 28:40 39.91 n/a 000
120148 + 1.0 02:FRASER-D 21.61 816 NaDate 28:40 39.91 n/a 000
120149 + 1.0 02:FRASER-D 21.61 816 NaDate 28:40 39.91 n/a 000
120150 + 1.0 02:FRASER-D 21.61 816 NaDate 28:40 39.91 n/a 000
120151 + 1.0 02:FRASER-D 21.61 816 NaDate 28:40 39.91 n/a 000
120152 + 1.0 02:FRASER-D 21.61 816 NaDate 28:40 39.91 n/a 000
120153 + 1.0 02:FRASER-D 21.61 816 NaDate 28:40 39.91 n/a 000
120154 + 1.0 02:FRASER-D 21.61 816 NaDate 28:40 39.91 n/a 000
120155 + 1.0 02:FC03-S 7.37 450 NaDate 28:14 59.51 n/a 000
120156 + 1.0 02:FC03-S 7.37 450 NaDate 28:14 59.51 n/a 000

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121560 R0505:CD0267.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
121561 SAVE IVD 1.0 01:FR01 121.14 17.63 NaDate 28:03 60.06 n/a 000
121562 name: FRASER-D.0050
121563 remark: Total Flow at Kennedy-Burnett Outlet
121564 Channel X Section obtained from RWCA Hydraulic Model - Station 2421
121565 #
121566 R0505:CD0268.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
121567 ROUTE CHANNEL + 1.0 02:FC04-S 12.87 2.58 NaDate 28:01 59.28 n/a 000
121568 [IARECmp: 4.00: IARECPE: 4.00]
121569 [SMM: 31.15: SMM: 207.66: SK: 010]
121570 [Impervius area: Iimp: 16.SLPI: 30.LGA: 151.MN: 013.SCI: 0]
121571 [IARECmp: 4.00: IARECPE: 4.00]
121572 R0505:CD0269.....Dfwn-ID NND.....AREWA-QPEAKm-TpeakTide:hh:mm.....Rvm R C.....Dfwn
121573 ADD IVD + 1.0 02:FC04-S 12.87 2.58 NaDate 28:01 59.28 n/a 000
121574 + 1.0 02:FC04-S 12.87 2.58 NaDate 27:44 59.54 n/a 000
121575 + 1.0 02:FC04-S 12.87 2.58 NaDate 27:44 59.54 n/a 000
121576 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121577 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121578 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121579 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121580 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121581 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121582 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121583 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121584 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121585 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121586 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121587 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121588 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121589 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121590 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121591 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121592 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121593 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121594 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121595 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121596 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121597 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121598 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121599 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121600 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121601 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121602 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121603 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121604 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121605 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121606 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121607 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121608 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121609 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121610 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121611 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121612 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121613 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121614 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121615 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121616 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121617 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121618 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121619 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121620 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121621 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121622 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121623 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121624 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121625 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121626 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121627 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121628 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121629 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121630 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121631 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121632 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121633 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121634 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121635 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121636 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121637 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121638 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121639 + 1.0 02:FR02-S 1.59 153 NaDate 27:45 59.66 n/a 000
121640 +
```


127175 [Impervious area: IArea=1.57; SLP1=0.0; LG=262.0; MN=013; SCI=0]
127176 IARECmp 4.00; IARECmp 4.00
127177 [SMA=33.81; SMA=225.43; SKE=010]
127178 R0050: C00165.....Dfma=1.0;Dfma=1.0
127179 COMPUTE DUALDID Dfma=1.0;01:AO: 2.44 481 NDate 28:00 66.69 n/a 0.00

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13091 # The Tp was modified according to a Peak Reduction factor (MO Chart B2-4)
13092 # of 1.80
13093 #10100:CO0008.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13094 CONTNLMX NASIIDD 1.0 01:SW11 3074.00 10.428 No.date 39:59 28.29 319 .000
13095 [Cm 55.0; No. 3.00; Tp=1.33]
13096 [IAREC 4.00; SMN= 83.24; SMW=554.96; SK= 010]
13097 [InterEventTime= 12.00]
13098 #10100:CO0009.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13099 CONTNLMX NASIIDD 1.0 01:SW11 1781.00 19.695 No.date 32:38 42.49 480 .000
13100 [Cm 72.0; No. 3.00; Tp= 3.91]
13101 [IAREC 4.00; SMN= 264.99; SK= 010]
13102 [InterEventTime= 12.00]
13103 #10100:CO0010.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13104 CONTNLMX NASIIDD 1.0 01:SW11 500.00 10.735 No.date 29:21 36.76 415 .000
13105 [Cm 66.0; No. 3.00; Tp= 1.24]
13106 [IAREC 4.00; SMN= 52.62; SMW=350.79; SK= 010]
13107 [InterEventTime= 12.00]
13108 #
13109 # The Tp was modified according to a Peak Reduction factor (MO Chart B2-4)
13110 # of 1.80
13111 #10100:CO0011.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13112 CONTNLMX NASIIDD 1.0 01:SW11 1917.00 14.496 No.date 34:24 36.76 415 .000
13113 [Cm 66.0; No. 3.00; Tp= 2.97]
13114 [IAREC 4.00; SMN= 52.62; SMW=350.79; SK= 010]
13115 [InterEventTime= 12.00]
13116 #
13117 # The Tp was modified according to a Peak Reduction factor (MO Chart B2-4)
13118 # of 1.52
13119 #10100:CO0012.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13120 CONTNLMX NASIIDD 1.0 01:SW10 5666.00 37.663 No.date 37:48 42.49 480 .000
13121 [Cm 72.0; No. 3.00; Tp= 8.00]
13122 [IAREC 4.00; SMN= 39.75; SMW=264.99; SK= 010]
13123 [InterEventTime= 12.00]
13124 #
13125 # The Tp was modified according to a Peak Reduction factor (MO Chart B2-4)
13126 # of 1.75
13127 #10100:CO0013.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13128 CONTNLMX NASIIDD 1.0 01:SW11 876.00 36.118 No.date 39:59 36.76 415 .000
13129 [Cm 66.0; No. 3.00; Tp=1.66]
13130 [IAREC 4.00; SMN= 52.62; SMW=350.79; SK= 010]
13131 [InterEventTime= 12.00]
13132 #
13133 # The Tp was modified according to a Peak Reduction factor (MO Chart B2-4)
13134 # of 1.68
13135 #10100:CO0014.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13136 CONTNLMX NASIIDD 1.0 01:SW9 1132.00 16.501 No.date 30:52 40.82 461 .000
13137 [Cm 72.0; No. 3.00; Tp= 8.00]
13138 [IAREC 4.00; SMN= 43.07; SMW=287.10; SK= 010]
13139 [InterEventTime= 12.00]
13140 #
13141 # The Tp was modified according to a Peak Reduction factor (MO Chart B2-4)
13142 # of 1.82
13143 #10100:CO0015.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13144 CONTNLMX NASIIDD 1.0 01:SW10 4484.00 18.060 No.date 39:59 33.01 380 .000
13145 [Cm 62.0; No. 3.00; Tp=1.33]
13146 [IAREC 4.00; SMN= 61.90; SMW=412.66; SK= 010]
13147 [InterEventTime= 12.00]
13148 #
13149 # The Tp was modified according to a Peak Reduction factor (MO Chart B2-4)
13150 # of 1.80
13151 #10100:CO0016.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13152 CONTNLMX NASIIDD 1.0 01:SW8 131.00 3.259 No.date 28:57 34.39 388 .000
13153 [Cm 63.0; No. 3.00; Tp= 9.0]
13154 [IAREC 4.00; SMN= 52.62; SMW=396.11; SK= 010]
13155 [InterEventTime= 12.00]
13156 #
13157 # The Tp was modified according to a Peak Reduction factor (MO Chart B2-4)
13158 # of 1.65
13159 #10100:CO0017.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13160 CONTNLMX NASIIDD 1.0 01:HB1R 3854.00 21.218 No.date 38:28 36.76 415 .000
13161 [Cm 60.0; No. 3.00; Tp= 1.51]
13162 [IAREC 4.00; SMN= 52.62; SMW=350.79; SK= 010]
13163 [InterEventTime= 12.00]
13164 #
13165 # The Tp was modified according to a Peak Reduction factor (MO Chart B2-4)
13166 # of 1.82
13167 #10100:CO0018.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13168 CONTNLMX NASIIDD 1.0 01:SW7 3197.00 16.421 No.date 36:21 29.79 336 .000
13169 [Cm 77.0; No. 3.00; Tp= 6.51]
13170 [IAREC 4.00; SMN= 52.62; SMW=508.81; SK= 010]
13171 [InterEventTime= 12.00]
13172 #
13173 # The Tp was modified according to a Peak Reduction factor (MO Chart B2-4)
13174 # of 1.75
13175 #10100:CO0019.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13176 CONTNLMX NASIIDD 1.0 01:SW6 165.00 1.511 No.date 33:01 37.57 424 .000
13177 [Cm 67.0; No. 3.00; Tp= 4.78]
13178 [IAREC 4.00; SMN= 35.42; SMW=336.97; SK= 010]
13179 [InterEventTime= 12.00]
13180 #
13181 # The Tp was modified according to a Peak Reduction factor (MO Chart B2-4)
13182 # of 1.63
13183 #10100:CO0020.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13184 CONTNLMX NASIIDD 1.0 01:VGLR 1332.00 10.882 No.date 35:10 42.49 480 .000
13185 [Cm 72.0; No. 3.00; Tp= 3.91]
13186 [IAREC 4.00; SMN= 39.75; SMW=264.99; SK= 010]
13187 [InterEventTime= 12.00]
13188 #10100:CO0021.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13189 CONTNLMX NASIIDD 1.0 01:SW5 224.00 9.576 No.date 28:44 47.62 538 .000
13190 [Cm 72.0; No. 3.00; Tp= 7.52]
13191 [IAREC 4.00; SMN= 31.15; SMW=207.66; SK= 010]
13192 [InterEventTime= 12.00]
13193 #
13194 # The Tp was modified according to a Peak Reduction factor (MO Chart B2-4)
13195 # of 1.20
13196 #10100:CO0022.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13197 CONTNLMX NASIIDD 1.0 01:FLC 4945.00 52.056 No.date 33:16 44.17 499 .000
13198 [Cm 74.0; No. 3.00; Tp= 4.45]
13199 [IAREC 4.00; SMN= 35.42; SMW=244.49; SK= 010]
13200 [InterEventTime= 12.00]
13201 #10100:CO0023.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13202 CONTNLMX NASIIDD 1.0 01:SW5A2 20.00 1.097 No.date 28:35 52.06 588 .000
13203 [Cm 81.0; No. 3.00; Tp= 6.21]
13204 [IAREC 4.00; SMN= 25.21; SMW=168.09; SK= 010]
13205 [InterEventTime= 12.00]
13206 #
13207 # The Tp was modified according to a Peak Reduction factor (MO Chart B2-4)
13208 # of 1.61
13209 #10100:CO0024.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13210 CONTNLMX NASIIDD 1.0 01:SW5A1 1412.00 10.184 No.date 37:44 45.88 518 .000
13211 [Cm 72.0; No. 3.00; Tp= 1.51]
13212 [IAREC 4.00; SMN= 35.81; SMW=225.43; SK= 010]
13213 [InterEventTime= 12.00]
13214 #10100:CO0025.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13215 CONTNLMX NASIIDD 1.0 01:SW4 585.00 14.953 No.date 29:55 52.06 588 .000
13216 [Cm 81.0; No. 3.00; Tp= 7.52]
13217 [IAREC 4.00; SMN= 25.21; SMW=168.09; SK= 010]
13218 [InterEventTime= 12.00]
13219 #10100:CO0026.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13220 CONTNLMX NASIIDD 1.0 01:SMCK 1021.00 19.782 No.date 30:45 51.16 578 .000
13221 [Cm 80.0; No. 3.00; Tp= 2.46]
13222 [IAREC 4.00; SMN= 26.32; SMW=175.50; SK= 010]
13223 [InterEventTime= 12.00]
13224 #10100:CO0027.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13225 CONTNLMX NASIIDD 1.0 01:SW2 177.00 7.567 No.date 28:44 47.62 538 .000
13226 [Cm 77.0; No. 3.00; Tp= 1.51]
13227 [IAREC 4.00; SMN= 31.15; SMW=207.66; SK= 010]
13228 [InterEventTime= 12.00]
13229 #10100:CO0028.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13230 CONTNLMX NASIIDD 1.0 01:SMCR 1122.00 52.056 No.date 31:42 52.06 588 .000
13231 [Cm 81.0; No. 3.00; Tp= 3.25]
13232 [IAREC 4.00; SMN= 25.21; SMW=168.09; SK= 010]
13233 [InterEventTime= 12.00]
13234 #10100:CO0029.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13235 CONTNLMX NASIIDD 1.0 01:SW3 2977.00 40.710 No.date 31:28 46.75 528 .000
13236 [Cm 76.0; No. 3.00; Tp= 3.01]
13237 [IAREC 4.00; SMN= 35.46; SMW=216.39; SK= 010]
13238 [InterEventTime= 12.00]
13239 #
13240 # Routing hydrographs
13241 #
13242 # Starting with the addition of Jock River Headwater and Subwatershed 13
13243 #
13244 #10100:CO0030.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13245 ADD HYD + 1.0 02:R_HV 3680.00 21.616 No.date 36:52 35.18 n/a .000
13246 [Cm 80.0; No. 3.00; Tp= 8.00] 3074.00 10.428 No.date 39:59 28.29 n/a .000
13247 [IAREC 4.00; SMN= 31.15; SMW=207.66; SK= 010] 4651.00 27.660 No.date 35:21 34.69 n/a .000
13248 #
13249 # Sum of hydrographs from Node 13 routed to Node 13A
13250 # (Approximated cross-section - see cross-section 258)
13251 # Use n=0.04 for summer conditions and n=0.025 for spring conditions
13252 #
13253 #10100:CO0031.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13254 ROUTE CHANNEL > 1.0 02:N3A 4651.00 27.660 No.date 35:21 34.69 n/a .000
13255 [RFE= 1.00] out c. 1.0 01:N3A 4651.00 22.598 No.date 38:56 34.69 n/a .000
13256 [I/S'n= 5926./ 076/ 040]
13257 [Vmax= 598./Dmax= 4.178]
13258 #
13259 # Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
13260 #
13261 #10100:CO0032.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13262 ADD HYD + 1.0 02:N3A 4651.00 27.660 No.date 35:21 34.69 n/a .000
13263 [Cm 80.0; No. 3.00; Tp= 3.01] 3074.00 10.428 No.date 39:59 28.29 n/a .000
13264 [IAREC 4.00; SMN= 35.46; SMW=216.39; SK= 010] 4651.00 27.660 No.date 35:21 34.69 n/a .000
13265 #
13266 # Insertion of a reservoir to simulate the effects of the Goodwood Marsh
13267 #
13268 #10100:CO0033.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13269 ROUTE RESERVOIR > 1.0 02:N3A 7725.00 32.845 No.date 39:44 32.14 n/a .000
13270 [MST 0.00] out c. 1.0 01:RES_GM 7725.00 39.50 No.date 62:26 32.14 n/a .000
13271 [MST 0.00] out c. 1.0 01:RES_GM 7725.00 39.50 No.date 62:26 32.14 n/a .000
13272 #
13273 #10100:CO0034.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13274 SAVE HYD 1.0 01:RES_GM 7725.00 39.50 No.date 62:26 32.14 n/a .000
13275 [IAREC 4.00; SMN= 52.62; SMW=350.79; SK= 010]
13276 [InterEventTime= 12.00]
13277 #
13278 # Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
13279 #
13280 #10100:CO0035.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13281 ADD HYD + 1.0 02:SW6 165.00 1.511 No.date 33:01 37.57 n/a .000
13282 [Cm 72.0; No. 3.00; Tp= 4.78]
13283 [IAREC 4.00; SMN= 35.42; SMW=336.97; SK= 010]
13284 #
13285 #10100:CO0036.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13286 ADD HYD + 1.0 02:SW11 876.00 36.118 No.date 39:59 36.76 n/a .000
13287 [Cm 66.0; No. 3.00; Tp= 1.66]
13288 [IAREC 4.00; SMN= 52.62; SMW=350.79; SK= 010]
13289 #
13290 #10100:CO0037.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13291 ADD HYD + 1.0 02:SW11 500.00 10.735 No.date 29:21 36.76 n/a .000
13292 [Cm 66.0; No. 3.00; Tp= 1.24]
13293 [IAREC 4.00; SMN= 52.62; SMW=350.79; SK= 010]
13294 #
13295 # Addition of Subwatershed Jock River at Ashton to Node 12
13296 #
13297 #10100:CO0038.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13298 ADD HYD + 1.0 02:N2 7725.00 39.50 No.date 62:26 32.14 n/a .000
13299 [Cm 80.0; No. 3.00; Tp= 3.01] 3074.00 10.428 No.date 39:59 28.29 n/a .000
13300 [IAREC 4.00; SMN= 35.46; SMW=216.39; SK= 010] 4651.00 27.660 No.date 35:21 34.69 n/a .000
13301 #
13302 # Sum of hydrographs from Node 12 routed to Node 11
13303 # (Approximated cross-section - see cross-section 258)
13304 # Use n=0.04 for summer conditions and n=0.025 for spring conditions
13305 #
13306 #10100:CO0039.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13307 ROUTE CHANNEL > 1.0 02:S_N2 9506.00 21.745 No.date 32:41 34.08 n/a .000
13308 [RFE= 1.00] out c. 1.0 01:Dan1 9506.00 21.522 No.date 32:57 34.08 n/a .000
13309 [I/S'n= 972./ 054/ 040]
13310 [Vmax= 777./Dmax= 3.194]
13311 #
13312 # Addition of Subwatershed 11 and No Name Creek to Node 11
13313 #
13314 #10100:CO0040.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13315 ADD HYD + 1.0 02:N2 7725.00 39.50 No.date 62:26 32.14 n/a .000
13316 [Cm 80.0; No. 3.00; Tp= 3.01] 3074.00 10.428 No.date 39:59 28.29 n/a .000
13317 [IAREC 4.00; SMN= 35.46; SMW=216.39; SK= 010] 4651.00 27.660 No.date 35:21 34.69 n/a .000
13318 #
13319 # Sum of hydrographs from Node 11 routed to Node 10
13320 #
13321 #10100:CO0041.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13322 ADD HYD + 1.0 02:SW10 5666.00 37.663 No.date 37:48 42.49 n/a .000
13323 [Cm 72.0; No. 3.00; Tp= 8.00]
13324 [IAREC 4.00; SMN= 39.75; SMW=264.99; SK= 010]
13325 #
13326 # Addition of Subwatershed 10 to Node 10
13327 #
13328 #10100:CO0042.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13329 ADD HYD + 1.0 02:SW10 5666.00 37.663 No.date 37:48 42.49 n/a .000
13330 [Cm 72.0; No. 3.00; Tp= 8.00]
13331 [IAREC 4.00; SMN= 39.75; SMW=264.99; SK= 010]
13332 #
13333 #10100:CO0043.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13334 SAVE HYD 1.0 01:S_N0 17589.00 61.058 No.date 38:16 37.16 n/a .000
13335 [IAREC 4.00; SMN= 43.07; SMW=287.10; SK= 010]
13336 #
13337 #10100:CO0044.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13338 ROUTE CHANNEL > 1.0 02:S_N0 17589.00 61.058 No.date 38:16 37.16 n/a .000
13339 [RFE= 1.00] out c. 1.0 02:SG 17589.00 61.058 No.date 38:16 37.16 n/a .000
13340 [I/S'n= 14028./ 157/ 040]
13341 [Vmax= 486./Dmax= 1.492]
13342 #
13343 # Sum of hydrographs from Node 10 routed to Node 9
13344 #
13345 #10100:CO0045.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13346 ADD HYD + 1.0 02:SW9 1132.00 16.501 No.date 30:52 40.82 n/a .000
13347 [Cm 77.0; No. 3.00; Tp= 6.51]
13348 [IAREC 4.00; SMN= 52.62; SMW=508.81; SK= 010]
13349 #
13350 # Addition of Subwatershed 9 and Hobbs' Drain to Node 9
13351 #
13352 #10100:CO0046.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13353 ADD HYD + 1.0 02:SW9 1132.00 16.501 No.date 30:52 40.82 n/a .000
13354 [Cm 77.0; No. 3.00; Tp= 6.51]
13355 [IAREC 4.00; SMN= 52.62; SMW=508.81; SK= 010]
13356 #
13357 #10100:CO0047.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13358 ADD HYD + 1.0 02:SW9 1132.00 16.501 No.date 30:52 40.82 n/a .000
13359 [Cm 77.0; No. 3.00; Tp= 6.51]
13360 [IAREC 4.00; SMN= 52.62; SMW=508.81; SK= 010]
13361 #
13362 # Sum of hydrographs from Node 9 routed to Node 8
13363 #
13364 #10100:CO0048.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13365 ADD HYD + 1.0 02:SW8 131.00 3.259 No.date 28:57 34.39 n/a .000
13366 [Cm 63.0; No. 3.00; Tp= 9.0]
13367 [IAREC 4.00; SMN= 52.62; SMW=396.11; SK= 010]
13368 #
13369 # Addition of Subwatershed 8 and Hobbs' Drain to Node 8
13370 #
13371 #10100:CO0049.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13372 ADD HYD + 1.0 02:SW8 131.00 3.259 No.date 28:57 34.39 n/a .000
13373 [Cm 63.0; No. 3.00; Tp= 9.0]
13374 [IAREC 4.00; SMN= 52.62; SMW=396.11; SK= 010]
13375 #
13376 #10100:CO0050.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13377 SAVE HYD 1.0 01:S_N9 35546.00 130.953 No.date 39:59 36.68 n/a .000
13378 [IAREC 4.00; SMN= 43.07; SMW=287.10; SK= 010]
13379 #
13380 #10100:CO0051.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13381 ROUTE CHANNEL > 1.0 02:S_N9 35546.00 130.953 No.date 39:59 36.68 n/a .000
13382 [RFE= 1.00] out c. 1.0 01:N7 35546.00 111.942 No.date 44:52 36.68 n/a .000
13383 [I/S'n= 3750./ 053/ 070]
13384 [Vmax= 277./Dmax= 2.412]
13385 #
13386 # Addition of Subwatershed 7 to Node 7
13387 #
13388 #10100:CO0052.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13389 ADD HYD + 1.0 02:SW7 1197.00 16.421 No.date 36:21 29.79 n/a .000
13390 [Cm 81.0; No. 3.00; Tp= 6.21]
13391 [IAREC 4.00; SMN= 25.21; SMW=168.09; SK= 010]
13392 #
13393 #10100:CO0053.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13394 SAVE HYD 1.0 01:S_N7 38743.00 120.740 No.date 43:36 36.11 n/a .000
13395 [IAREC 4.00; SMN= 25.21; SMW=168.09; SK= 010]
13396 #
13397 #10100:CO0054.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13398 INSERT HYD + 1.0 02:RS 38743.00 120.740 No.date 43:36 36.11 n/a .000
13399 [Cm 80.0; No. 3.00; Tp= 2.46]
13400 [IAREC 4.00; SMN= 25.21; SMW=168.09; SK= 010]
13401 #
13402 #10100:CO0055.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13403 ROUTE RESERVOIR > 1.0 02:S_N7 38743.00 120.740 No.date 43:36 36.11 n/a .000
13404 [MST 0.00] out c. 1.0 01:RES_RF 38743.00 120.740 No.date 43:36 36.11 n/a .000
13405 [MST 0.00] out c. 1.0 01:RES_RF 38743.00 120.740 No.date 43:36 36.11 n/a .000
13406 [MST 0.00] out c. 1.0 01:RES_RF 38743.00 120.740 No.date 43:36 36.11 n/a .000
13407 [MST 0.00] out c. 1.0 01:RES_RF 38743.00 120.740 No.date 43:36 36.11 n/a .000
13408 #
13409 #10100:CO0056.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13410 ROUTE CHANNEL > 1.0 02:S_N7 38743.00 120.740 No.date 43:36 36.11 n/a .000
13411 [RFE= 1.00] out c. 1.0 01:RS 38743.00 114.000 No.date 44:52 36.68 n/a .000
13412 [I/S'n= 3056./ 052/ 025]
13413 [Vmax= 556./Dmax= 1.373]
13414 #
13415 # Addition of Subwatershed 6 and Van Gal Drain to Node 6
13416 #
13417 #10100:CO0057.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13418 ADD HYD + 1.0 02:SW6 165.00 1.511 No.date 33:01 37.57 n/a .000
13419 [Cm 72.0; No. 3.00; Tp= 4.78]
13420 [IAREC 4.00; SMN= 35.42; SMW=336.97; SK= 010]
13421 #
13422 #10100:CO0058.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13423 ADD HYD + 1.0 02:SW6 165.00 1.511 No.date 33:01 37.57 n/a .000
13424 [Cm 72.0; No. 3.00; Tp= 4.78]
13425 [IAREC 4.00; SMN= 35.42; SMW=336.97; SK= 010]
13426 #
13427 # Sum of hydrographs from Node 6 routed to Node 5
13428 #
13429 #10100:CO0059.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13430 ADD HYD + 1.0 02:SW6 165.00 1.511 No.date 33:01 37.57 n/a .000
13431 [Cm 72.0; No. 3.00; Tp= 4.78]
13432 [IAREC 4.00; SMN= 35.42; SMW=336.97; SK= 010]
13433 #
13434 #10100:CO0060.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13435 ROUTE CHANNEL > 1.0 02:SW6 165.00 1.511 No.date 33:01 37.57 n/a .000
13436 [RFE= 1.00] out c. 1.0 01:S6 165.00 1.511 No.date 33:01 37.57 n/a .000
13437 [I/S'n= 1852./ 054/ 035]
13438 [Vmax= 494./Dmax= 1.468]
13439 #
13440 # Addition of Subwatershed 5 and Flowing Creek to Node 5
13441 #
13442 #10100:CO0061.....DfIn a-ID NDD.....AREhA-QPEAKm-TPeakDate-hh-mm-Rvmm R.C....DfWm
13443 ADD HYD + 1.0 02:SW5 224.00 9.576 No.date 28:44 47.62 n/a .000
13444 [Cm 80.0; No. 3.00; Tp= 2.46]
13445 [IAREC 4.00; SMN= 25.21; SMW=168.09; SK= 010]
13446 #
13447 # Sum of hydrographs from Node 5 routed to Node 5A
13448 #
1344
```



```
157098 *** WARNING: New pipe size used for routing.
157108 R0100: C00370 ROUTE PIPE ->
157118 *** WARNING: New pipe size used for routing.
157128 R0050: C00378 ROUTE PIPE ->
157138 *** WARNING: New pipe size used for routing.
157148 R0050: C00379 ROUTE PIPE ->
157158 *** WARNING: New pipe size used for routing.
157168 R0100: C00303 ROUTE PIPE ->
157178 *** WARNING: New pipe size used for routing.
157188 R0100: C00309 ROUTE PIPE ->
157198 *** WARNING: New pipe size used for routing.
157208 R0100: C00325 ROUTE PIPE ->
157218 *** WARNING: New pipe size used for routing.
157228 R0100: C00326 ROUTE PIPE ->
157238 *** WARNING: New pipe size used for routing.
157248 R0100: C00334 ROUTE PIPE ->
157258 *** WARNING: New pipe size used for routing.
157268 R0100: C00342 INVERT HYD ->
157278 *** NOTE: Inflow hyd. is dry and cannot be diverted.
157288 R0100: C00357 ROUTE PIPE ->
157298 *** WARNING: New pipe size used for routing.
157308 R0100: C00362 ROUTE PIPE ->
157318 *** WARNING: New pipe size used for routing.
157328 R0100: C00369 ROUTE PIPE ->
157338 *** WARNING: New pipe size used for routing.
157348 R0100: C00370 ROUTE PIPE ->
157358 *** WARNING: New pipe size used for routing.
157368 R0100: C00378 ROUTE PIPE ->
157378 *** WARNING: New pipe size used for routing.
157388 R0100: C00379 ROUTE PIPE ->
157398 *** WARNING: New pipe size used for routing.
157408 Simulation ended on 2021-03-04 at 11:53:36
157418 =====
157428
157438
```

Attachment D

Model 4A – Jock River Reach One Future Conditions – Without SWM controls

JFSA, 2021

SWMHYMO Input & Summary files

```

1  20      Metric units / ID numbers OFF
2  *****
3  *# SWHYMO Ver: 5.02/Jan 2001 <BETA> / INPUT DATA FILE
4  *****
5  *# Project Name: [Jock River]      Project Number: [1474-16]
6  *# Date       : 04-03-2021
7  *# Modeller   : [MM]
8  *# Company    : JFSA Inc.
9  *# License #  : 2549237
10 *****
11 *# CALIBRATION OF SUMMER MODEL PARAMETERS
12 *# USING CONTINUOUS SIMULATIONS
13 *# Rainfall data from JFSA raingauge installed at site + other gauges by the City
14 *# Use data collected from May 1st to July 14, 2003
15 *# 2020-11-30 change TMSSTO in COMPUTE DUALHYD (TMSSTO = 0.1 instead of 0.0001)
16 *# 2020-12-01 correct pond curve values
17 *# 2020-12-01 change WCLAR_BRAZ_XIMP to 0.55, SLPI=[0.5](%) (impervious slope), and
    LGI up to 700m
18 *# 2021-02-19 Change the slope for ROUTE CHANNEL Station 2462 (NHYDout=["N_TO"]
    ,NHYDin=["SN_TO"]) from 0.033 % (as per Stantec Report 2007) to 0.05 % so the model
    will be more stable and give reasonable results. It is justifiable as ROUTE CHANNELS
    aren't well suited to really flat slopes.
19 *# 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (NHYDout=["N_WC"]
    ,NHYDin=["SN_CE"]) from 0.01 % (as per Stantec Report 2007) to 0.0255 % so the model
    will be more stable and give reasonable results. It is justifiable as ROUTE CHANNELS
    aren't well suited to really flat slopes.
20 *
21 * Calibrated parameters for Summer 2003 data: APII=50, APIK=0.85, CN=varies,
22 *                                             SK=0.01, InterEventTime=12,
23 *                                             GWResk=0.96, VHydCond=0.055
24 *
25 *# -----
26 *
27 *START          TZERO=[2003.0501], METOUT=[2], NSTORM=[1], NRUN=[001]
28 *              ["XAVG0315.STM"] average storm data a 15 minute time step
29 *              The above rainf file is an average of the JFSA gauge data
30 *              with the City of Ottawa rainfall data collected during
31 *              the same period.
32 *% 2 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
33 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[2]
34              ["C24SC002.stm"] <-- storm filename, one per line for NSTORM time
35 *%-----|-----|
36 *%-----|-----|
37 READ STORM     STORM_FILENAME=["storm 001"]
38 *%-----|-----|
39 MODIFY STORM   ICASEms=[1], NSHIFT=[96],
40              RedFACT=[1],
41 *%-----|-----|
42 DEFAULT VALUES ICASEdef=[1], read and print values
43              DEFVAL_FILENAME=["CitiGate.DEF"]
44 *%-----|-----|
45 COMPUTE API    APII=[50], APIK=[.85]/day
46 *%-----|-----|
47 *%-----|-----|
48 *#
49 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
50 *# of 1.32
51 *%-----|-----|
52 CONTINUOUS NASHYD NHYD=["JR_HW"], DT=[1]min, AREA=[3680](ha),
53              DWF=[0](cms), CNVC=[64], IA=[2.5](mm),
54              N=[3.0], TP=[7.13]hrs,
55              Continuous simulation parameters:
56              IARECper=[4](hrs),
57              SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
58              InterEventTime=[12](hrs)
59              Baseflow simulation parameters:

```



```

60 BaseFlowOption=[ 1] ,
61 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
62 VHydCond=[ 0.055](mm/hr), END=- 1
63 *%-----|-----
64 *#
65 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
66 *# of 1.32
67 *%-----|-----
68 CONTINUOUS NASHYD NHYD=["SW_13"], DT=[ 1]min, AREA=[ 971](ha),
69 DWF=[ 0](cms), CNVC=[ 61], IA=[ 2.5](mm),
70 N=[ 3.0], TP=[ 3.76]hrs,
71 Continuous simulation parameters:
72 IaRECper=[ 4](hrs),
73 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
74 InterEventTime=[ 12](hrs)
75 Baseflow simulation parameters:
76 BaseFlowOption=[ 1] ,
77 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
78 VHydCond=[ 0.055](mm/hr), END=- 1
79 *%-----|-----
80 *#
81 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
82 *# of 1.80
83 *%-----|-----
84 CONTINUOUS NASHYD NHYD=["JR_GWM"], DT=[ 1]min, AREA=[ 3074](ha),
85 DWF=[ 0](cms), CNVC=[ 55], IA=[ 2.5](mm),
86 N=[ 3], TP=[ 11.33]hrs,
87 Continuous simulation parameters:
88 IaRECper=[ 4](hrs),
89 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
90 InterEventTime=[ 12](hrs)
91 Baseflow simulation parameters:
92 BaseFlowOption=[ 1] ,
93 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
94 VHydCond=[ 0.055](mm/hr), END=- 1
95 *%-----|-----
96 CONTINUOUS NASHYD NHYD=["JR_ASH"], DT=[ 1]min, AREA=[ 1781](ha),
97 DWF=[ 0](cms), CNVC=[ 72], IA=[ 2.5](mm),
98 N=[ 3.0], TP=[ 3.91]hrs,
99 Continuous simulation parameters:
100 IaRECper=[ 4](hrs),
101 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
102 InterEventTime=[ 12](hrs)
103 Baseflow simulation parameters:
104 BaseFlowOption=[ 1] ,
105 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
106 VHydCond=[ 0.055](mm/hr), END=- 1
107 *%-----|-----
108 CONTINUOUS NASHYD NHYD=["SW_11"], DT=[ 1]min, AREA=[ 500](ha),
109 DWF=[ 0](cms), CNVC=[ 66], IA=[ 2.5](mm),
110 N=[ 3.0], TP=[ 1.24]hrs,
111 Continuous simulation parameters:
112 IaRECper=[ 4](hrs),
113 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
114 InterEventTime=[ 12](hrs)
115 Baseflow simulation parameters:
116 BaseFlowOption=[ 1] ,
117 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
118 VHydCond=[ 0.055](mm/hr), END=- 1
119 *%-----|-----
120 *#
121 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
122 *# of 1.80
123 *%-----|-----
124 CONTINUOUS NASHYD NHYD=["NN_CK"], DT=[ 1]min, AREA=[ 1917](ha),
125 DWF=[ 0](cms), CNVC=[ 66], IA=[ 2.5](mm),

```

```

126 N=[ 3.0], TP=[ 5.29] hrs,
127 Continuous simulation parameters:
128 IaRECPper=[ 4] (hrs),
129 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010]/(mm),
130 InterEventTime=[ 12] (hrs)
131 Baseflow simulation parameters:
132 BaseFlowOption=[ 1] ,
133 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/ day/ mm)
134 VHydCond=[ 0.055] (mm/ hr), END=- 1
135 *%-----|-----
136 *#
137 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
138 *# of 1.52
139 *%-----|-----
140 CONTINUOUS NASHYD NHYD=[ "SW_10"], DT=[ 1] min, AREA=[ 5666] (ha),
141 DWF=[ 0] (cms), CNVC=[ 72], IA=[ 2.5] (mm),
142 N=[ 3.0], TP=[ 8.00] hrs,
143 Continuous simulation parameters:
144 IaRECPper=[ 4] (hrs),
145 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010]/(mm),
146 InterEventTime=[ 12] (hrs)
147 Baseflow simulation parameters:
148 BaseFlowOption=[ 1] ,
149 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/ day/ mm)
150 VHydCond=[ 0.055] (mm/ hr), END=- 1
151 *%-----|-----
152 *#
153 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
154 *# of 1.75
155 *%-----|-----
156 CONTINUOUS NASHYD NHYD=[ "KG_CK"], DT=[ 1] min, AREA=[ 8376] (ha),
157 DWF=[ 0] (cms), CNVC=[ 66], IA=[ 2.5] (mm),
158 N=[ 3.0], TP=[ 11.66] hrs,
159 Continuous simulation parameters:
160 IaRECPper=[ 4] (hrs),
161 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010]/(mm),
162 InterEventTime=[ 12] (hrs)
163 Baseflow simulation parameters:
164 BaseFlowOption=[ 1] ,
165 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/ day/ mm)
166 VHydCond=[ 0.055] (mm/ hr), END=- 1
167 *%-----|-----
168 *#
169 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
170 *# of 1.68
171 *%-----|-----
172 CONTINUOUS NASHYD NHYD=[ "SW_9"], DT=[ 1] min, AREA=[ 1132] (ha),
173 DWF=[ 0] (cms), CNVC=[ 70], IA=[ 2.5] (mm),
174 N=[ 3.0], TP=[ 2.51] hrs,
175 Continuous simulation parameters:
176 IaRECPper=[ 4] (hrs),
177 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010]/(mm),
178 InterEventTime=[ 12] (hrs)
179 Baseflow simulation parameters:
180 BaseFlowOption=[ 1] ,
181 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/ day/ mm)
182 VHydCond=[ 0.055] (mm/ hr), END=- 1
183 *%-----|-----
184 *#
185 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
186 *# of 1.82
187 *%-----|-----
188 CONTINUOUS NASHYD NHYD=[ "NC_CK"], DT=[ 1] min, AREA=[ 4464] (ha),
189 DWF=[ 0] (cms), CNVC=[ 62], IA=[ 2.5] (mm),
190 N=[ 3.0], TP=[ 11.32] hrs,
191 Continuous simulation parameters:

```

```

192 IaREcper=[ 4] (hr s),
193 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
194 InterEventTime=[ 12] (hr s)
195 Baseflow simulation parameters:
196 BaseFlowOption=[ 1] ,
197 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
198 VHydCond=[ 0. 055] (mm/ hr), END=- 1
199 *%-----|-----
200 *#
201 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
202 *# of 1.80
203 *%-----|-----
204 CONTINUOUS NASHYD NHYD=[ "SW_8" ], DT=[ 1] mi n, AREA=[ 131] (ha),
205 DWF=[ 0] (cms), CN C=[ 63], IA=[ 2. 5] (mm),
206 N=[ 3. 0], TP=[ 0. 90] hr s,
207 Continuous simulation parameters:
208 IaREcper=[ 4] (hr s),
209 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
210 InterEventTime=[ 12] (hr s)
211 Baseflow simulation parameters:
212 BaseFlowOption=[ 1] ,
213 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
214 VHydCond=[ 0. 055] (mm/ hr), END=- 1
215 *%-----|-----
216 *#
217 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
218 *# of 1.65
219 *%-----|-----
220 CONTINUOUS NASHYD NHYD=[ "HB_DR" ], DT=[ 1] mi n, AREA=[ 3854] (ha),
221 DWF=[ 0] (cms), CN C=[ 66], IA=[ 2. 5] (mm),
222 N=[ 3. 0], TP=[ 8. 42] hr s,
223 Continuous simulation parameters:
224 IaREcper=[ 4] (hr s),
225 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
226 InterEventTime=[ 12] (hr s)
227 Baseflow simulation parameters:
228 BaseFlowOption=[ 1] ,
229 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
230 VHydCond=[ 0. 055] (mm/ hr), END=- 1
231 *%-----|-----
232 *#
233 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
234 *# of 1.82
235 *%-----|-----
236 CONTINUOUS NASHYD NHYD=[ "SW_7" ], DT=[ 1] mi n, AREA=[ 3197] (ha),
237 DWF=[ 0] (cms), CN C=[ 57], IA=[ 2. 5] (mm),
238 N=[ 3. 0], TP=[ 6. 65] hr s,
239 Continuous simulation parameters:
240 IaREcper=[ 4] (hr s),
241 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
242 InterEventTime=[ 12] (hr s)
243 Baseflow simulation parameters:
244 BaseFlowOption=[ 1] ,
245 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
246 VHydCond=[ 0. 055] (mm/ hr), END=- 1
247 *%-----|-----
248 *#
249 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
250 *# of 1.75
251 *%-----|-----
252 CONTINUOUS NASHYD NHYD=[ "SW_6" ], DT=[ 1] mi n, AREA=[ 165] (ha),
253 DWF=[ 0] (cms), CN C=[ 67], IA=[ 2. 5] (mm),
254 N=[ 3. 0], TP=[ 4. 18] hr s,
255 Continuous simulation parameters:
256 IaREcper=[ 4] (hr s),
257 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),

```

```

258 InterEventTime=[ 12] (hrs)
259 Baseflow simulation parameters:
260 BaseFlowOption=[ 1] ,
261 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/ day/ mm)
262 VHydCond=[ 0.055] (mm/ hr), END=- 1
263 *%-----|-----
264 *#
265 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
266 *# of 1.67
267 *%-----|-----
268 CONTINUOUS NASHYD NHYD=[ "VG_DR" ], DT=[ 1] min, AREA=[ 1332] (ha),
269 DWF=[ 0] (cms), CNVC=[ 72], IA=[ 2.5] (mm),
270 N=[ 3.0], TP=[ 5.95] hrs,
271 Continuous simulation parameters:
272 IaRECper=[ 4] (hrs),
273 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
274 InterEventTime=[ 12] (hrs)
275 Baseflow simulation parameters:
276 BaseFlowOption=[ 1] ,
277 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/ day/ mm)
278 VHydCond=[ 0.055] (mm/ hr), END=- 1
279 *%-----|-----
280 CONTINUOUS NASHYD NHYD=[ "SW_5" ], DT=[ 1] min, AREA=[ 224] (ha),
281 DWF=[ 0] (cms), CNVC=[ 77], IA=[ 2.5] (mm),
282 N=[ 3.0], TP=[ 0.75] hrs,
283 Continuous simulation parameters:
284 IaRECper=[ 4] (hrs),
285 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
286 InterEventTime=[ 12] (hrs)
287 Baseflow simulation parameters:
288 BaseFlowOption=[ 1] ,
289 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/ day/ mm)
290 VHydCond=[ 0.055] (mm/ hr), END=- 1
291 *%-----|-----
292 *#
293 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
294 *# of 1.20
295 *%-----|-----
296 CONTINUOUS NASHYD NHYD=[ "FL_CK" ], DT=[ 1] min, AREA=[ 4945] (ha),
297 DWF=[ 0] (cms), CNVC=[ 74], IA=[ 2.5] (mm),
298 N=[ 3.0], TP=[ 4.45] hrs,
299 Continuous simulation parameters:
300 IaRECper=[ 4] (hrs),
301 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
302 InterEventTime=[ 12] (hrs)
303 Baseflow simulation parameters:
304 BaseFlowOption=[ 1] ,
305 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/ day/ mm)
306 VHydCond=[ 0.055] (mm/ hr), END=- 1
307 *%-----|-----
308 CONTINUOUS NASHYD NHYD=[ "SW_5A2" ], DT=[ 1] min, AREA=[ 20] (ha),
309 DWF=[ 0] (cms), CNVC=[ 81], IA=[ 2.5] (mm),
310 N=[ 3.0], TP=[ 0.62] hrs,
311 Continuous simulation parameters:
312 IaRECper=[ 4] (hrs),
313 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
314 InterEventTime=[ 12] (hrs)
315 Baseflow simulation parameters:
316 BaseFlowOption=[ 1] ,
317 InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/ day/ mm)
318 VHydCond=[ 0.055] (mm/ hr), END=- 1
319 *%-----|-----
320 *#
321 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
322 *# of 1.61
323 *%-----|-----

```

324 CONTI NUOUS NASHYD NYHD=["SW_5A1"], DT=[1] mi n, AREA=[1412] (ha),
325 DWF=[0] (cms), CNV C=[75], IA=[2. 5] (mm),
326 N=[3. 0], TP=[8. 00] hr s,
327 Continuous simulation parameters:
328 IaRECPper=[4] (hr s),
329 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
330 InterEventTime=[12] (hr s)
331 Baseflow simulation parameters:
332 BaseFlowOpti on=[1] ,
333 In it GWRes Vol = [50] (mm), GWRes K=[0. 96] (mm / day / mm)
334 VHydCond=[0. 055] (mm / hr), END=- 1

*%-----|

336 CONTI NUOUS NASHYD NYHD=["SW_4"], DT=[1] mi n, AREA=[585] (ha),
337 DWF=[0] (cms), CNV C=[81], IA=[2. 5] (mm),
338 N=[3. 0], TP=[1. 75] hr s,
339 Continuous simulation parameters:
340 IaRECPper=[4] (hr s),
341 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
342 InterEventTime=[12] (hr s)
343 Baseflow simulation parameters:
344 BaseFlowOpti on=[1] ,
345 In it GWRes Vol = [50] (mm), GWRes K=[0. 96] (mm / day / mm)
346 VHydCond=[0. 055] (mm / hr), END=- 1

*%-----|

348 CONTI NUOUS NASHYD NYHD=["LM_CK"], DT=[1] mi n, AREA=[1021] (ha),
349 DWF=[0] (cms), CNV C=[80], IA=[2. 5] (mm),
350 N=[3. 0], TP=[2. 46] hr s,
351 Continuous simulation parameters:
352 IaRECPper=[4] (hr s),
353 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
354 InterEventTime=[12] (hr s)
355 Baseflow simulation parameters:
356 BaseFlowOpti on=[1] ,
357 In it GWRes Vol = [50] (mm), GWRes K=[0. 96] (mm / day / mm)
358 VHydCond=[0. 055] (mm / hr), END=- 1

*%-----|

360 CONTI NUOUS NASHYD NYHD=["SW_2"], DT=[1] mi n, AREA=[177] (ha),
361 DWF=[0] (cms), CNV C=[77], IA=[2. 5] (mm),
362 N=[3. 0], TP=[0. 75] hr s,
363 Continuous simulation parameters:
364 IaRECPper=[4] (hr s),
365 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
366 InterEventTime=[12] (hr s)
367 Baseflow simulation parameters:
368 BaseFlowOpti on=[1] ,
369 In it GWRes Vol = [50] (mm), GWRes K=[0. 96] (mm / day / mm)
370 VHydCond=[0. 055] (mm / hr), END=- 1

*%-----|

372 CONTI NUOUS NASHYD NYHD=["SM_DR"], DT=[1] mi n, AREA=[1122] (ha),
373 DWF=[0] (cms), CNV C=[81], IA=[2. 5] (mm),
374 N=[3. 0], TP=[3. 25] hr s,
375 Continuous simulation parameters:
376 IaRECPper=[4] (hr s),
377 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
378 InterEventTime=[12] (hr s)
379 Baseflow simulation parameters:
380 BaseFlowOpti on=[1] ,
381 In it GWRes Vol = [50] (mm), GWRes K=[0. 96] (mm / day / mm)
382 VHydCond=[0. 055] (mm / hr), END=- 1

*%-----|

384 CONTI NUOUS NASHYD NYHD=["MO_DR"], DT=[1] mi n, AREA=[2737] (ha),
385 DWF=[0] (cms), CNV C=[76], IA=[2. 5] (mm),
386 N=[3. 0], TP=[3. 03] hr s,
387 Continuous simulation parameters:
388 IaRECPper=[4] (hr s),
389 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),

```

390 InterEventTime=[ 12]( hrs)
391 Baseflow simulation parameters:
392 BaseFlowOption=[ 1] ,
393 InitGWResVol=[ 50]( mm) , GWResK=[ 0.96]( mm/ day/ mm)
394 VHydCond=[ 0.055]( mm/ hr) , END=- 1
395 *%-----|-----|
396 * -JFSA 2020 replaced SW_1 with a detailed model from Stantec Report 2007
397 *CONTINUOUS NASHYD NHYD=["SW_1"], DT=[ 1]mi n, AREA=[ 3176]( ha),
398 * DWF=[ 0]( cms) , CN/C=[ 78] , IA=[ 2.5]( mm),
399 * N=[ 3.0] , TP=[ 3.56]hrs,
400 * Continuous simulation parameters:
401 * IaRECper=[ 4]( hrs),
402 * SMN=[ -1]( mm) , SMAX=[ -1]( mm) , SK=[ 0.010]/( mm),
403 * InterEventTime=[ 12]( hrs)
404 * Baseflow simulation parameters:
405 * BaseFlowOption=[ 1] ,
406 * InitGWResVol=[ 50]( mm) , GWResK=[ 0.96]( mm/ day/ mm)
407 * VHydCond=[ 0.055]( mm/ hr) , END=- 1
408 *%-----|-----|
409 *#
410 *# Routing hydrographs
411 *#
412 *# Starting with the addition of Jock River Headwater and Subwatershed 13
413 *#
414 ADD HYD NHYDsum=["S_N13"], NHYDs to add=["JR_HW"+"SW_13"]
415 *%-----|-----|
416 *#
417 *# Sum of hydrographs from Node 13 routed to Node 13A
418 *# (Approximated cross-section - see cross-section 258)
419 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
420 *#
421 ROUTE CHANNEL NHYDout=["N13A"] , NHYDin=["S_N13"],
422 RDT=[ 1]( mi n),
423 CHLGTH=[ 9074]( m) , CHSLOPE=[ 0.0220]( %),
424 FPSLOPE=[ 0.0220]( %),
425 SECNUM=[ 1.0] , NSEG=[ 1]
426 ( SEGROUGH, SEGDI ST ( m) )=[ 0.04, 15.5] NSEG times
427 ( DI STANCE ( m) , ELEVATI ON ( m) )=
428 [- 40, 132.5]
429 [- 30, 132]
430 [- 25, 131.5]
431 [- 13, 130]
432 [- 8, 127.00]
433 [- 7, 126.50]
434 [- 6, 126]
435 [- 5.5, 125.50]
436 [0, 123.75]
437 [4.5, 125.50]
438 [6, 126]
439 [7.5, 126.5]
440 [9, 127]
441 [10, 127.5]
442 [11.5, 128.0]
443 [15.5, 129.5]
444 *%-----|-----|
445 *#
446 *# Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
447 *#
448 ADD HYD NHYDsum=["SN13A"], NHYDs to add=["N13A"+"JR_GWM"]
449 *%-----|-----|
450 *#
451 *# Insertion of a reservoir to simulate the effects of the Goodwood Marsh
452 *#
453 ROUTE RESERVOIR NHYDout=["RES_GM"] , NHYDin=["SN13A"],
454 RDT=[ 1]( mi n),
455 TABLE of ( OUTFLOW STORAGE ) values

```

```

456 (cms) - (ha-m)
457 [ 0.0 , 0.0 ]
458 [ 1.991, 2.144 ]
459 [ 2.693, 39.826 ]
460 [ 3.509, 81.697 ]
461 [ 4.578, 318.774 ]
462 [ 5.647, 594.947 ]
463 [ 7.109, 910.219 ]
464 [ 8.616, 1264.589 ]
465 [ 10.371, 1658.057 ]
466 [ 12.402, 2090.622 ]
467 [ 22.056, 3462.487 ]
468 [ -1 , -1 ] (max twenty pts)
469
470 NHYDovf=[ " " ] ,
471 *%-----|-----|
472 *#
473 SAVE HYD NHYD=[ "RES_GM" ], # OF PCYCLES=[ -1 ], I CASEs h=[ -1 ]
474 HYD_FILENAMES=[ "H_RESGM" ]
475 HYD_COMMENT=[ "Out flow from Res GM" ]
476 *%-----|-----|
477 *# Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
478 *# (Approximated cross-section - see cross-section 258)
479 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
480 ROUTE CHANNEL NHYDout=[ "N12" ] , NHYDin=[ "RES_GM" ] ,
481 RDT=[ 1 ] (min) ,
482 CHLGTH=[ 5926 ] (m) , CHSLOPE=[ 0.0759 ] ( % ) ,
483 FPSLOPE=[ 0.0759 ] ( % ) ,
484 SECNUM=[ 1.0 ] , NSEG=[ 1 ]
485 ( SEGROUGH, SEGDIST (m) )=[ 0.04, 15.5 ] NSEG times
486 ( DISTANCE (m) , ELEVATION (m) )=
487 [- 40, 132.5]
488 [- 30, 132]
489 [- 25, 131.5]
490 [- 13, 130]
491 [- 8, 127.00]
492 [- 7, 126.50]
493 [- 6, 126]
494 [- 5.5, 125.50]
495 [ 0, 123.75]
496 [ 4.5, 125.50]
497 [ 6, 126]
498 [ 7.5, 126.5]
499 [ 9, 127]
500 [ 10, 127.5]
501 [ 11.5, 128.00]
502 [ 15.5, 129.5]
503 *%-----|-----|
504 *#
505 *# Addition of Subwatershed Jock River at Ashton to Node 12
506 *#
507 ADD HYD NHYDsum=[ "S_N12" ] , NHYDs to add=[ "N12"+"JR_ASH" ]
508 SAVE HYD NHYD=[ "S_N12" ] , # OF PCYCLES=[ -1 ], I CASEs h=[ -1 ]
509 HYD_FILENAMES=[ "H_SN12" ]
510 HYD_COMMENT=[ "flow at S_N12 near Ashton" ]
511 *%-----|-----|
512 *#
513 *# Sum of hydrographs from Node 12 routed to Node 11
514 *# (Approximated cross-section - see cross-section 258)
515 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
516 *ROUTE CHANNEL NHYDout=[ "N11" ] , NHYDin=[ "S_N12" ] ,
517 * RDT=[ 1 ] (min) ,
518 * CHLGTH=[ 972 ] (m) , CHSLOPE=[ 0.0514 ] ( % ) ,
519 * FPSLOPE=[ 0.0514 ] ( % ) ,
520 * SECNUM=[ 1.0 ] , NSEG=[ 1 ]
521 * ( SEGROUGH, SEGDIST (m) )=[ 0.04, 15.5 ] NSEG times
522 * ( DISTANCE (m) , ELEVATION (m) )=

```

```

522 * [- 40, 132.5]
523 * [- 30, 132]
524 * [- 25, 131.5]
525 * [- 13, 130]
526 * [- 8, 127.00]
527 * [- 7, 126.50]
528 * [- 6, 126]
529 * [- 5.5, 125.50]
530 * [0, 123.75]
531 * [4.5, 125.50]
532 * [6, 126]
533 * [7.5, 126.5]
534 * [9, 127]
535 * [10, 127.5]
536 * [11.5, 128.00]
537 * [15.5, 129.5]
538 *%-----|-----
539 *#
540 *# Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
541 *#
542 ROUTE CHANNEL NHYDout=["Duml1"], NHYDin=["S_N12"],
543 RDT=[1](min),
544 CHLGTH=[972](m), CHSLOPE=[0.054](%),
545 FPSLOPE=[0.054](%),
546 SECNUM=[1.0], NSEG=[1]
547 ( SEGROUGH, SEGDIST (m))=[0.04, 15.5] NSEG times
548 ( DISTANCE (m), ELEVATION (m))=
549 [- 40, 132.5]
550 [- 30, 132]
551 [- 25, 131.5]
552 [- 13, 130]
553 [- 8, 127.00]
554 [- 7, 126.50]
555 [- 6, 126]
556 [- 5.5, 125.50]
557 [0, 123.75]
558 [4.5, 125.50]
559 [6, 126]
560 [7.5, 126.5]
561 [9, 127]
562 [10, 127.5]
563 [11.5, 128.00]
564 [15.5, 129.5]
565 *%-----|-----
566 *#
567 *# Addition of Subwatershed 11 and No Name Creek to Node 11
568 *#
569 ADD HYD NHYDsum=["S_N11"], NHYDstoadd=["Duml1"+"SW_11"+"NN_CK"]
570 *%-----|-----
571 *#
572 *# Sum of hydrographs from Node 11 routed to Node 10
573 *# Section 1
574 *#
575 ROUTE CHANNEL NHYDout=["N10"], NHYDin=["S_N11"],
576 RDT=[1](min),
577 CHLGTH=[14028](m), CHSLOPE=[0.1568](%),
578 FPSLOPE=[0.1568](%),
579 SECNUM=[1.0], NSEG=[5]
580 ( SEGROUGH, SEGDIST (m))=
581 [0.04, -52.82
582 0.1, -6.47
583 -0.05, 6.47
584 0.1, 45.36
585 0.04, 423.88] NSEG times
586 ( DISTANCE (m), ELEVATION (m))=
587 [- 226.24 , 112.50]

```



```

588             [- 167. 50 , 111. 50]
589             [- 106. 81 , 111. 00]
590             [- 92. 37 , 110. 00]
591             [- 52. 82 , 109. 00]
592             [- 24. 90, 109. 00]
593             [- 17. 02, 108. 50]
594             [- 6. 47, 108. 00]
595             [ 6. 47, 108. 00]
596             [ 15. 67, 108. 50]
597             [ 18. 95, 109. 00]
598             [ 45. 36, 109. 50]
599             [ 120. 79, 110. 00]
600             [ 145. 72, 111. 00]
601             [ 181. 56, 111. 50]
602             [ 423. 88, 112. 50]
603 *%-----|-----
604 *#
605 *# Addition of Subwatershed 10 to Node 10
606 *#
607 ADD HYD          NHYDs um=["S_N10"], NHYDs to add=["N10"+"SW_10"]
608 *%-----|-----
609 SAVE HYD         NHYD=["S_N10"], # OF PCYCLES=[- 1], I CASEs h=[- 1]
610                 HYD_FILE NAME=["H_SN10"]
611                 HYD_COMMENT=["flow at S_N10: N10 + SW_10"]
612 *%-----|-----
613 *# Addition of Kings Creek to S_N10
614 *#
615 ADD HYD          NHYDs um=["S_N10A"], NHYDs to add=["S_N10"+"KG_CK"]
616 *%-----|-----
617 *#
618 *# Sum of hydrographs from Node 10 routed to Node 9
619 *# Section 2
620 *#
621 ROUTE CHANNEL    NHYDout=["N9"] , NHYDin=["S_N10A"] ,
622                 RDT=[ 1] ( mi n) ,
623                 CHLGTH=[ 3982] ( m) ,   CHSLOPE=[ 0. 0753] ( % ) ,
624                                     FPSLOPE=[ 0. 0753] ( % ) ,
625                 SECNUM=[ 1. 0] ,       NSEG=[ 4]
626                 ( SEGROUGH, SEGDI ST ( m) ) =
627                 [ 0. 04, - 30. 27
628                 0. 05, - 18. 42
629                 - 0. 05, 18. 42
630                 0. 04, 131. 58] NSEG times
631                 ( DI STANCE ( m) , ELEVATI ON ( m) ) =
632                 [- 446. 74, 106. 00]
633                 [- 415. 68, 105. 50]
634                 [- 285. 40, 105. 00]
635                 [- 173. 77, 104. 50]
636                 [- 144. 95, 104. 00]
637                 [- 111. 18, 103. 50]
638                 [- 94. 06, 103. 00]
639                 [- 71. 02, 102. 50]
640                 [- 30. 27, 102. 00]
641                 [- 19. 33, 100. 00]
642                 [- 18. 42, 99. 50]
643                 [ 18. 42, 99. 50]
644                 [ 20. 77, 100. 00]
645                 [ 27. 93, 101. 00]
646                 [ 52. 29, 101. 00]
647                 [ 68. 80, 101. 50]
648                 [ 79. 66, 103. 00]
649                 [ 91. 50, 103. 50]
650                 [ 131. 58, 104. 00]
651 *%-----|-----
652 *#
653 *# Addition of Subwatershed 9 and Nichols Creek to Node 9

```

```

654  *#
655  ADD HYD          NHYDs um=[ "S_N9" ], NHYDs to add=[ "N9"+"SW_9"+"NC_CK" ]
656  *%-----|-----|
657  *#
658  *# Sum of hydrographs from Node 9 routed to Node 8
659  *# Section 3
660  *#
661  ROUTE CHANNEL    NHYDout =[ "N8" ] , NHYDin =[ "S_N9" ] ,
662                  RDT=[ 1 ] ( mi n ) ,
663                  CHLGTH=[ 2269 ] ( m ) ,   CHSLOPE=[ 0.0882 ] ( % ) ,
664                                                    FPSLOPE=[ 0.0882 ] ( % ) ,
665                  SECNUM=[ 1.0 ] ,          NSEG=[ 3 ]
666                  ( SEGROUGH, SEGDI ST ( m ) ) =
667                    [ 0.1, -17.99
668                    -0.045, 17.31
669                    0.1, 456.58 ] NSEG t i m e s
670                  ( DI STANCE ( m ) , ELEVATI ON ( m ) ) =
671                    [ -201.19, 100.50 ]
672                    [ -135.21, 100.00 ]
673                    [ -94.83, 99.50 ]
674                    [ -67.05, 99.00 ]
675                    [ -17.99, 98.50 ]
676                    [ -16.02, 98.00 ]
677                    [ -13.95, 97.50 ]
678                    [ 13.95, 97.50 ]
679                    [ 15.64, 98.00 ]
680                    [ 17.31, 98.50 ]
681                    [ 162.02, 98.50 ]
682                    [ 172.89 , 99.00 ]
683                    [ 314.38, 99.00 ]
684                    [ 343.78, 99.50 ]
685                    [ 365.67, 100.00 ]
686                    [ 376.68, 100.00 ]
687                    [ 393.11, 99.50 ]
688                    [ 404.97, 99.50 ]
689                    [ 431.70, 100.00 ]
690                    [ 456.58, 100.50 ]
691  *%-----|-----|
692  *#
693  *# Addition of Subwatershed 8 and Hobb's Drain to Node 8
694  *#
695  ADD HYD          NHYDs um=[ "S_N8" ], NHYDs to add=[ "N8"+"SW_8"+"HB_DR" ]
696  *%-----|-----|
697  *#
698  *# Sum of hydrographs from Node 8 routed to Node 7
699  *# Section 4
700  *#
701  ROUTE CHANNEL    NHYDout =[ "N7" ] , NHYDin =[ "S_N8" ] ,
702                  RDT=[ 1 ] ( mi n ) ,
703                  CHLGTH=[ 3750 ] ( m ) ,   CHSLOPE=[ 0.0533 ] ( % ) ,
704                                                    FPSLOPE=[ 0.0533 ] ( % ) ,
705                  SECNUM=[ 1.0 ] ,          NSEG=[ 3 ]
706                  ( SEGROUGH, SEGDI ST ( m ) ) =
707                    [ 0.12, -18.11
708                    -0.07, 17.22
709                    0.12, 590.05 ] NSEG t i m e s
710                  ( DI STANCE ( m ) , ELEVATI ON ( m ) ) =
711                    [ -433.21, 102.00 ]
712                    [ -425.34, 101.50 ]
713                    [ -377.56, 101.50 ]
714                    [ -366.23, 101.00 ]
715                    [ -202.60, 100.50 ]
716                    [ -96.25, 99.50 ]
717                    [ -68.36 99.00 ]
718                    [ -18.11, 98.50 ]
719                    [ -13.81, 97.50 ]

```

```

720 [ 13. 81, 97. 50]
721 [ 17. 22, 98. 50]
722 [ 161. 95, 98. 50]
723 [ 173. 11, 99. 00]
724 [ 314. 05, 99. 00]
725 [ 365. 52, 100. 00]
726 [ 404. 70, 99. 50]
727 [ 476. 74, 100. 50]
728 [ 502. 31, 101. 00]
729 [ 584. 69, 101. 00]
730 [ 585. 79, 101. 00]
731 [ 590. 05, 102. 00]
732 *%-----|-----
733 *#
734 *# Addition of Subwatershed 7 to Node 7
735 *#
736 ADD HYD          NHYDs um=[ "S_N7" ], NHYDs to add=[ "N7"+"SW_7" ]
737 *%-----|-----
738 SAVE HYD         NHYD=[ "S_N7" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ - 1 ]
739                 HYD_FI LENAME=[ "H_SN7" ]
740                 HYD_COMMENT=[ "flow at S_N7: N7 + SW_7" ]
741 *%-----|-----
742 *# Insertion of a reservoir to simulate the effects of the Richmond Fen.
743 *# Storage area and volumes were estimated from available topo maps.
744 *# Release rate from fen was assumed to be controlled by the downstream
745 *# river cross-section for summer conditions. It is was assumed that for up to
746 *# 0.75 m of water, the main channel of the river provided the storage. Above
747 *# this depth, the wetland starts to signigicantly store water.
748 *#
749 ROUTE RESERVOIR NHYDout =[ "RES_RF" ] , NHYDi n=[ "S_N7" ] ,
750                 RDT=[ 1 ] ( mi n ) ,
751                 TABLE of ( OUTFLOW STORAGE ) values
752                         ( cms ) - ( ha- m )
753                 TABLE of ( OUTFLOW STORAGE ) values
754                         ( cms ) - ( ha- m )
755                         [ 0. 0 , 0. 0 ]
756                         [ 0. 9051, 2. 40]
757                         [ 2. 907, 4. 13]
758                         [ 9. 744, 9. 18]
759                         [ 20. 304, 14. 96]
760                         [ 34. 167, 310. 21]
761                         [ 74. 993, 605. 46]
762                         [ 104. 876, 900. 71]
763                         [ 140. 56, 2892. 00]
764                         [ 225. 00, 3615. 63]
765                         [ - 1 , - 1 ] (max t went y pts)
766                 NHYDovf=[ " " ] ,
767 *%-----|-----
768 SAVE HYD         NHYD=[ "RES_RF" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ - 1 ]
769                 HYD_FI LENAME=[ "H_Res RF" ]
770                 HYD_COMMENT=[ "out flow of Ri chmnd Fen" ]
771 *%-----|-----
772 *#
773 *# Sum of hydrographs from Node 7 routed to Node 6
774 *# Section 5
775 *#
776 ROUTE CHANNEL   NHYDout =[ "N6" ] , NHYDi n=[ "RES_RF" ] ,
777                 RDT=[ 1 ] ( mi n ) ,
778                 CHLGTH=[ 3056 ] ( m ) , CHSLOPE=[ 0. 0818 ] ( % ) ,
779                 FPSLOPE=[ 0. 0818 ] ( % ) ,
780                 SECNUM=[ 1. 0 ] , NSEG=[ 5 ]
781                 ( SEGROUGH, SEGDI ST ( m ) ) =
782                 [ 0. 025, - 70. 8
783                 0. 1, - 23. 9
784                 - 0. 05, 23. 9
785                 0. 06, 39. 8

```

```

786           0. 05, 96. 3] NSEG times
787           ( DI STANCE ( m), ELEVATI ON ( m))=
788             [- 100. 8, 97. 00]
789             [- 70. 8, 96. 50]
790             [- 52. 0, 96. 00]
791             [- 35. 1, 95. 50]
792             [- 30. 6, 95. 00]
793             [- 23. 9, 94. 54]
794             [ 23. 9, 94. 54]
795             [ 39. 8, 95. 00]
796             [ 50. 4, 95. 50]
797             [ 93. 5, 96. 00]
798             [ 94. 9, 96. 50]
799             [ 96. 3, 97. 00]
800 *%-----|-----
801 *#
802 *# Addition of Subwatershed 6 and Van Gaal Drain to Node 6
803 *#
804 ADD HYD           NHYDs um=[ "S_N6" ], NHYDs to add=[ "N6"+"SW_6"+"VG_DR" ]
805 *%-----|-----
806 *#
807 *# Sum of hydrographs from Node 6 routed to Node 5
808 *# Section 6
809 *#
810 ROUTE CHANNEL     NHYDout =[ "N5" ] , NHYDin =[ "S_N6" ] ,
811                   RDT=[ 1 ] ( mi n),
812                   CHLGTH=[ 1852 ] ( m),   CHSLOPE=[ 0. 0540 ] ( %),
813                                           FPSLOPE=[ 0. 0540 ] ( %),
814                   SECNUM=[ 1. 0 ],       NSEG=[ 3]
815                   ( SEGROUGH, SEGDI ST ( m))=
816                     [ 0. 035, - 131. 59
817                     - 0. 045, 48. 96
818                     0. 1, 239. 04] NSEG times
819                   ( DI STANCE ( m), ELEVATI ON ( m))=
820                     [- 686. 30, 94. 50]
821                     [- 675. 70, 94. 00]
822                     [- 492. 52, 93. 00]
823                     [- 467. 28, 94. 00]
824                     [- 131. 59, 94. 00]
825                     [- 92. 79, 92. 50]
826                     [- 18. 06, 91. 00]
827                     [ 18. 06, 91. 00]
828                     [ 43. 47, 92. 50]
829                     [ 48. 96, 94. 00]
830                     [ 177. 43, 94. 00]
831                     [ 239. 04, 94. 50]
832 *%-----|-----
833 *#
834 *# Addition of Subwatershed 5 and Flowing Creek to Node 5
835 *#
836 ADD HYD           NHYDs um=[ "S_N5" ], NHYDs to add=[ "N5"+"SW_5"+"FL_CK" ]
837 *%-----|-----
838 *#
839 *# Sum of hydrographs from Node 5 routed to Node 5A
840 *# Section 7
841 *#
842 ROUTE CHANNEL     NHYDout =[ "N5A" ] , NHYDin =[ "S_N5" ] ,
843                   RDT=[ 1 ] ( mi n),
844                   CHLGTH=[ 556 ] ( m),   CHSLOPE=[ 0. 0900 ] ( %),
845                                           FPSLOPE=[ 0. 0900 ] ( %),
846                   SECNUM=[ 1. 0 ],       NSEG=[ 4]
847                   ( SEGROUGH, SEGDI ST ( m))=
848                     [ 0. 04, - 41. 5
849                     0. 1, - 14. 0
850                     - 0. 045, 14. 0
851                     0. 1, 41. 1] NSEG times

```

```

852          ( DI STANCE ( m) , ELEVATI ON ( m) ) =
853          [- 275. 8, 93. 00]
854          [- 248. 6, 92. 50]
855          [- 237. 0, 92. 00]
856          [- 219. 3, 91. 50]
857          [- 202. 1, 91. 50]
858          [- 186. 0, 92. 00]
859          [- 129. 2, 92. 00]
860          [- 117. 6, 91. 50]
861          [- 100. 6, 91. 00]
862          [- 41. 5, 91. 00]
863          [- 20. 0, 91. 00]
864          [- 14. 0, 90. 54]
865          [ 14. 0, 90. 54]
866          [ 15. 3, 91. 00]
867          [ 17. 3, 91. 50]
868          [ 38. 4, 92. 00]
869          [ 39. 8, 92. 50]
870          [ 41. 1, 93. 00]
871 *%-----|-----
872 *#
873 *# Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A
874 *#
875 ADD HYD          NHYDs um=[ "S_N5A" ] , NHYDs t o add=[ "N5A"+"SW_5A2"+"SW_5A1" ]
876 *%-----|-----
877 *#
878 *# Sum of hydrographs from Node 5A routed to Node 4
879 *# Section 8
880 *#
881 ROUTE CHANNEL    NHYDout =[ "N4" ] , NHYDi n=[ "S_N5A" ] ,
882                  RDT=[ 1 ] ( mi n) ,
883                  CHLGTH=[ 4630 ] ( m) ,   CHSLOPE=[ 0. 0432 ] ( % ) ,
884                                          FPSLOPE=[ 0. 0432 ] ( % ) ,
885                  SECNUM=[ 1. 0 ] ,       NSEG=[ 3 ]
886          ( SEGROUGH, SEGDI ST ( m) ) =
887          [ 0. 05, -28. 2
888          -0. 035, 28. 2
889          0. 05, 173. 1 ] NSEG t i mes
890          ( DI STANCE ( m) , ELEVATI ON ( m) ) =
891          [- 38. 9, 92. 00]
892          [- 35. 8, 91. 50]
893          [- 33. 3, 91. 00]
894          [- 28. 2, 90. 50]
895          [- 15. 0, 87. 48]
896          [- 5. 0, 88. 34]
897          [ 5. 0, 86. 20]
898          [ 15. 0, 88. 55]
899          [ 28. 2, 90. 50]
900          [ 29. 7, 91. 00]
901          [ 46. 5, 91. 00]
902          [ 127. 8, 91. 00]
903          [ 148. 7, 91. 50]
904          [ 173. 1, 92. 00]
905 *%-----|-----
906 *#
907 *# Addition of Subwatershed 4 and Leamy Creek to Node 4
908 *#
909 ADD HYD          NHYDs um=[ "S_N4" ] , NHYDs t o add=[ "N4"+"SW_4"+"LM_CK" ]
910 SAVE HYD        NHYD=[ "S_N4" ] , # OF PCYCLES=[ - 1 ] , I CASEs h=[ 1 ]
911                HYD_COMMENT=[ "f l ow at S_N4" ]
912 *%-----|-----
913 *#
914 *# Sum of hydrographs from Node 4 routed to Node 2
915 *# Section 9
916 *#
917 ROUTE CHANNEL    NHYDout =[ "N2" ] , NHYDi n=[ "S_N4" ] ,

```

```

918 RDT=[ 1] ( mi n),
919 CHLGTH=[ 1667] ( m), CHSLOPE=[ 0. 0600] ( %),
920 FPSLOPE=[ 0. 0600] ( %),
921 SECNUM=[ 1. 0], NSEG=[ 4]
922 ( SEGROUGH, SEGDI ST ( m))=
923 [ 0. 1, - 28. 0
924 - 0. 04, 28. 4
925 0. 06, 31. 7
926 0. 04, 80. 2] NSEG t i m e s
927 ( DI STANCE ( m), ELEVATI ON ( m))=
928 [- 36. 3, 92. 00]
929 [- 32. 6, 91. 50]
930 [- 30. 2, 91. 00]
931 [- 28. 0, 90. 45]
932 [- 15. 0, 87. 48]
933 [- 5. 0, 88. 34]
934 [ 5. 0, 86. 20]
935 [ 15. 0, 88. 55]
936 [ 28. 0, 90. 45]
937 [ 28. 4, 90. 50]
938 [ 30. 4, 91. 00]
939 [ 31. 7, 91. 50]
940 [ 80. 2, 92. 00]
941 *%-----|-----|
942 *#
943 *# Addition of Subwatershed 2 with Monohan Drain and Smith Drain to Node 2
944 *#
945 ADD HYD NHYDs um=[ "S_N2"], NHYDs t o add=[ "N2"+"SW_2"+"SM_DR"+"MO_DR"]
946 *%-----|-----|
947 SAVE HYD NHYD=[ "S_N2"], # OF PCYCLES=[ - 1], I CAS E s h=[ - 1]
948 HYD_FI L E N A M E=[ "H_S_N2"]
949 HYD_C O M M E N T=[ "f l o w a t S_N2 J o c k R i v e r G a u g e a t M o d i e D r. "]
950 *%-----|-----|
951 *#
952 *# Sum of hydrographs from Node 2 routed to Node 1
953 *# Section 10
954 *#
955 *#*****
956 *%READ HYD NHYD=[ "S_N2"],
957 *% HYD_FI L E N A M E=[ "H_S_N2"]
958 *%-----|-----|
959 *#
960 *# Hydrograph from Node 2 routed to Node 416
961 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 9025
962 *#
963 ROUTE CHANNEL NHYDout =["N_416"] , NHYDin=["S_N2"] ,
964 RDT=[ 1] ( mi n),
965 CHLGTH=[ 2327] ( m), CHSLOPE=[ 0. 0498] ( %),
966 FPSLOPE=[ 0. 0498] ( %),
967 SECNUM=[ 1. 0], NSEG=[ 3]
968 ( SEGROUGH, SEGDI ST ( m))=
969 [ 0. 075, - 23. 96
970 - 0. 055, 23. 96
971 0. 075, 157. 38] NSEG t i m e s
972 ( DI STANCE ( m), ELEVATI ON ( m))=
973 [- 336. 97, 93. 5]
974 [- 318. 85, 93]
975 [- 259, 92. 5]
976 [- 133. 18, 92]
977 [- 33. 17, 92]
978 [- 27. 21, 92]
979 [- 26. 14, 91. 5]
980 [- 24. 99, 91]
981 [- 23. 96, 90. 5]
982 [- 14. 33, 88. 26]
983 [- 0. 68, 88. 12]

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984 [ 14. 33, 88. 26]
985 [ 23. 96, 90. 5]
986 [ 32. 12, 91]
987 [ 43. 74, 91. 5]
988 [ 57. 09, 92]
989 [ 73. 53, 92. 5]
990 [ 108. 27, 93]
991 [ 125. 88, 93. 5]
992 [ 144. 81, 94]
993 [ 157. 38, 94. 5]
994 *%-----|-----|
995 *#*****|*****|
996 *# Catchment SW1a
997 *# - Portion of RVCA catchment SW1 outside of Reach 1 subwatershed
998 *# - Undeveloped agricultural land
999 *#*****|*****|
1000 CONTINUOUS NASHYD NHYD=[ "SW_1a" ], DT=[ 1] (mi n), AREA=[ 536. 42] ( ha),
1001 DWF=[ 0] ( cms), CN C=[ 72], IA=[ 4. 67] ( mm),
1002 N=[ 3], TP=[ 2. 79] hr s,
1003 Continuous simulation parameters:
1004 IaREcper=[ 4] ( hr s),
1005 SM N=[ - 1] ( mm), SMAX=[ - 1] ( mm), SK=[ 0. 010] / ( mm),
1006 InterEvent Time=[ 12] ( hr s)
1007 Baseflow simulation parameters:
1008 BaseFlowOption=[ 1],
1009 InitGWResVol=[ 50] ( mm), GWResK=[ 0. 96] ( mm/ day/ mm)
1010 VHydCond=[ 0. 055] ( mm/ hr), END=- 1
1011 *%-----|-----|
1012 * -JFSA 2021-02-25 "S-1-Okeefe" is a part of S-1 sub-catchment. It is moved to drain
before station 7245 on Jock River
1013 CONTINUOUS STANDHYD NHYD=[ "S-1-Okeefe" ], DT=[ 1] ( mi n), AREA=[ 44. 93] ( ha), XI MP=[ 0. 65],
TI MP=[ 0. 65], DWF=[ 0] ( cms),
1014 LOSS=[ 2], SCS curve number CN=[ 75], Pervious surfaces:
I Aper=[ 4. 67] ( mm), SLPP=[ 2. 0] ( %),
1015 LGP=[ 40] ( m), MNP=[ 0. 25], SCP=[ 0] ( mi n), Impervious surfaces:
I Ai mp=[ 1. 57] ( mm), SLPI=[ 0. 75] ( %),
1016 LGL=[ 547. 296] ( m), MNI=[ 0. 013], SCI=[ 0] ( mi n),
1017 Continuous simulation parameters:
1018 IaREcper=[ 4] ( hr s), IaRECI mp=[ 4] ( hr s),
1019 SM N=[ - 1] ( mm), SMAX=[ - 1] ( mm), SK=[ 0. 010] / ( mm),
1020 InterEvent Time=[ 12] ( hr s), END=- 1
1021 *%-----|-----|
1022 *COMPUTE DUALHYD NHYDin=[ "S-1-Okeefe" ], CI NLET=[ 4. 796] ( cms), NI NLET=[ 1],
1023 * Mij NHYD=[ "S-1-OkM" ]
1024 * M nNHYD=[ "S-1-OkMN" ]
1025 * TM STO=[ 9999999] ( cu- m)
1026 *%-----|-----|
1027 *ADD HYD NHYDsum=[ "S-1-OkS" ], NHYDs to add=[ "S-1-OkM" +"S-1-OkMN" ]
1028 *%-----|-----|
1029 *ROUTE RESERVOIR NHYDout=[ "S-1-OkSR" ], NHYDin=[ "S-1-OkS" ],
1030 * RDT=[ 1] ( mi n),
1031 * TABLE of ( OUTFLOW STORAGE ) values
1032 * ( cms) - ( ha- m)
1033 * [ 0. 0, 0. 0 ]
1034 * [ 0. 5370, 1. 7917 ]
1035 * [ - 1, - 1 ] ( max twenty pts)
1036 * NHYDovf=[ "S-1-OkSovf" ]
1037 *%-----|-----|
1038 ADD HYD NHYDsum=[ "SN_416" ], NHYDs to add=[ "N_416" +"SW_1a" +"S-1-Okeefe" ]
1039 *%-----|-----|
1040 SAVE HYD NHYD=[ "SN_416" ], # OF PCYCLES=[ - 1], I CASEs h=[ 1]
1041 HYD_COMMENT=[ "Total Flows at Highway 416" ]
1042 *%-----|-----|
1043 *#
1044 *# Hydrograph from Node 416 routed to Node at Okeefe drain
1045 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 7245

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1046 *#
1047 ROUTE CHANNEL      NHYDout=["N_OK"] , NHYDin=["SN_416"] ,
1048                    RDT=[1](min),
1049                    CHLGTH=[497](m),   CHSLOPE=[0.3018](%),
1050                    FPSLOPE=[0.3018](%),
1051                    SECNUM=[1.0],      NSEG=[3]
1052                    ( SEGROUGH, SEGDIST (m))=
1053                    [0.075, -19.40
1054                    -0.055, 19.40
1055                    0.075, 377.02] NSEG times
1056                    ( DISTANCE (m), ELEVATION (m))=
1057                    [-1061.41, 92.50]
1058                    [-945.91, 92.00]
1059                    [-783.64, 91.50]
1060                    [-136.74, 91.00]
1061                    [-86.04, 91.00]
1062                    [-20.86, 91.00]
1063                    [-20.18, 90.50]
1064                    [-19.40, 90.00]
1065                    [-11.68, 86.89]
1066                    [0.00, 86.10]
1067                    [12.09, 86.81]
1068                    [19.40, 90.00]
1069                    [34.68, 90.50]
1070                    [60.56, 91.00]
1071                    [170.14, 91.00]
1072                    [175.05, 90.50]
1073                    [180.29, 90.00]
1074                    [193.41, 90.00]
1075                    [195.98, 90.50]
1076                    [377.02, 92.50]
1077 *%-----|-----|
1078 *#*****|*****|
1079 *#      Catchment OKEEFE
1080 *#      - To O'Keefe drain (north of the Jock)
1081 *#      - Developed with assumed 43% imp.
1082 *#      - 2020-12-01 add Okeefe model (Area 513.02 HA) instead of current Okeefe (Area
1083 *#      - 2020-11-20 Okeefe detailed model was added as per the NOVATECH SWWHYMD model
1084 *#      (Citi-Gate 2014).
1085 *%-----|-----|
1086 *#*****|*****|
1087 *#*****|*****|
1088 CONTINUOUS NASHYD  NHYD=["O-1R"], DT=[1]min, AREA=[63.72](ha),
1089                    DWF=[0](cms), CNVC=[61], IA=[6.2](mm), N=[3], TP=[.9]hrs,
1090                    Continuous simulation parameters:
1091                    IaRECper=[4](hrs),
1092                    SMN=[-1](mm),   SMAX=[-1](mm), SK=[0.010]/(mm),
1093                    InterEventTime=[12](hrs)
1094                    Baseflow simulation parameters:
1095                    BaseFlowOption=[1] ,
1096                    InitGWResVol=[50](mm),   GWResK=[0.96](mm/day/mm)
1097                    VHydCond=[0.055](mm/hr),   END=-1
1098 *%-----|-----|
1099 *%-----|-----|
1100 *ROUTE FLOW THROUGH AREA 0-2
1101 ROUTE CHANNEL      NHYDout=["O-1R"], NHYDin=["O-1"], RDT=[1](min),
1102                    CHLGTH=[960](m),   CHSLOPE=[0.63](%),   FPSLOPE=[0.63](%),
1103                    SECNUM=[1],   NSEG=[3]
1104                    ( SEGROUGH, SEGDIST (m))=[0.06, 4 -.043, 6 0.06, 10] NSEG times
1105                    ( DISTANCE (m), ELEVATION (m))=[0.00, 2.0]
1106                    [0.0, 2.0]
1107                    [4.0, 0.0]
1108                    [6.0, 0.0]
1109                    [10.0, 2.0]

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1109 *%-----|-----|
1110 CONTINUOUS NASHYD NHYD=["O-2"], DT=[1] min, AREA=[28.61] (ha),
1111 DWF=[0] (cms), CN C=[57], IA=[5.2] (mm), N=[3], TP=[1.1] hrs,
1112 Continuous simulation parameters:
1113 IaRECper=[4] (hrs),
1114 SMN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
1115 InterEventTime=[12] (hrs)
1116 Baseflow simulation parameters:
1117 BaseFlowOption=[1],
1118 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
1119 VHydCond=[0.055] (mm/hr), END=-1
1120 *%-----|-----|
1121 CONTINUOUS NASHYD NHYD=["O-4"], DT=[1] min, AREA=[46.94] (ha),
1122 DWF=[0] (cms), CN C=[49], IA=[9.2] (mm), N=[3], TP=[0.9] hrs,
1123 Continuous simulation parameters:
1124 IaRECper=[4] (hrs),
1125 SMN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
1126 InterEventTime=[12] (hrs)
1127 Baseflow simulation parameters:
1128 BaseFlowOption=[1],
1129 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
1130 VHydCond=[0.055] (mm/hr), END=-1
1131 *%-----|-----|
1132 *TOTAL EXTERNAL FLOW NORTH OF O'KEEFE CT. CROSSING
1133 ADD HYD NHYDsum=["OKF-N"], NHYDstoadd=["O-1R"+"O-2"+"O-4"]
1134 *%-----|-----|
1135 *ROUTE FLOW THROUGH AREA O-6
1136 ROUTE CHANNEL ROUTE CHANNEL NHYDout=["OKF-NR"], NHYDin=["OKF-N"], RDT=[1] (min),
1137 CHLGTH=[210] (m), CHSLOPE=[.81] (%), FPSLOPE=[.81] (%),
1138 SECNUM=[1], NSEG=[3]
1139 (SEGROUGH, SEGDIST (m))=[0.043, 22.43 - 0.043, 25.07
1140 0.043, 45.54] NSEG times
1141 (DISTANCE (m), ELEVATION (m))=[0.00, 3.73]
1142 (14.62, 1.56)
1143 (18.41, 1.44)
1144 (22.43, 0.00)
1145 (25.07, 0.70)
1146 (29.10, 1.79)
1147 (33.73, 2.71)
1148 (45.54, 3.58)
1149 *%-----|-----|
1150 CONTINUOUS NASHYD NHYD=["O-6"], DT=[1] min, AREA=[16.46] (ha),
1151 DWF=[0] (cms), CN C=[43], IA=[9.2] (mm), N=[3], TP=[0.7] hrs,
1152 Continuous simulation parameters:
1153 IaRECper=[4] (hrs),
1154 SMN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
1155 InterEventTime=[12] (hrs)
1156 Baseflow simulation parameters:
1157 BaseFlowOption=[1],
1158 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
1159 VHydCond=[0.055] (mm/hr), END=-1
1160 *%-----|-----|
1161 CONTINUOUS STANDHYD NHYD=["O-3"], DT=[1] (min), AREA=[39.67] (ha), XI MP=[0.15],
1162 T I MP=[0.30], DWF=[0] (cms),
1163 LOSS=[2], SCS curve number CN=[50], Pervious surfaces:
1164 IAper=[4.67] (mm), SLPP=[0.32] (%),
1165 LGP=[440] (m), MNP=[0.035], SCP=[0] (min), Impervious surfaces:
1166 IAimp=[1.57] (mm), SLPI=[0.32] (%),
1167 LGI=[1880] (m), MNI=[0.013], SCI=[0] (min),
1168 Continuous simulation parameters:
1169 IaRECper=[4] (hrs), IaRECimp=[4] (hrs),
1170 SMN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
1171 InterEventTime=[12] (hrs), END=-1
1172 *%-----|-----|
1173 CONTINUOUS STANDHYD NHYD=["O-5"], DT=[1] (min), AREA=[60.63] (ha), XI MP=[0.13],
1174 T I MP=[0.26], DWF=[0] (cms),

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1171      LOSS=[ 2], SCS curve number CN=[ 61],
1172      Pervious surfaces: I Aper=[ 4.67] (mm), SLPP=[ 1.38] (%),
1173      LGP=[ 550] (m), MNP=[ 0.035], SCP=[ 0] (min), Impervious surfaces:
      I Aimp=[ 1.57] (mm), SLPI=[ 1.38] (%),
1174      LGI=[ 1450] (m), MNI=[ 0.013], SCI=[ 0] (min),
1175      Continuous simulation parameters:
1176      I aRECper=[ 4] (hrs), I aRECimp=[ 4] (hrs),
1177      SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
1178      Inter Event Time=[ 12] (hrs), END=- 1
1179      *%-----|-----|
1180      *TOTAL EXTERNAL FLOWS WEST OF THE SITE AND NORTH OF O'KEEFE CRT
1181      *%-----|-----|
1182      ADD HYD      NHYDsum=[ "PT1"], NHYDs to add=[ "OKF-NR"+"O-3"+"O-5"+"O-6"]
1183      *%-----|-----|
1184      CONTINUOUS NASHYD      NHYD=[ "O-7"], DT=[ 1] min, AREA=[ 5.28] (ha),
1185      DWF=[ 0] (cms), CNC=[ 54], IA=[ 7.5] (mm), N=[ 3], TP=[ 0.6] hrs,
1186      Continuous simulation parameters:
1187      I aRECper=[ 4] (hrs),
1188      SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
1189      Inter Event Time=[ 12] (hrs)
1190      Baseflow simulation parameters:
1191      BaseFlowOption=[ 1] ,
1192      Init GWRes Vol=[ 50] (mm), GWRes K=[ 0.96] (mm3/day/mm)
1193      VHydCond=[ 0.055] (mm/hr), END=- 1
1194      *%-----|-----|
1195      *ANALYSIS POINT 1 - TOTAL FLOW NORTH OF FALLOWFIELD DR. AND O'KEEFE CRT.
1196      ADD HYD      NHYDsum=[ "FF"], NHYDs to add=[ "PT1"+"O-7"]
1197      *%-----|-----|
1198      *ROUTE FLOW through O'Keefe Drain 1
1199      ROUTE CHANNEL      NHYDout=[ "DRAIN1"], NHYDin=[ "FF"], RDT=[ 1] (min),
1200      CHLGT H=[ 302] {m}, CHSLOPE=[ 1.00] (%), FPSLOPE=[ 1.00] (%),
1201      SECNUM=[ 1], NSEG=[ 3]
1202      ( SEGROUGH, SEGDI ST (m))=[ 0.07, 13.45 -0.043, 16.55 0.07, 30.00] NSEG
      times
1203      ( DI STANCE (m), ELEVATI ON (m))=[ 0.00, 1.70]
1204      ( 3.45, 0.60)
1205      ( 13.45, 0.50)
1206      ( 14.45, 0.00)
1207      ( 15.55, 0.00)
1208      ( 16.55, 0.50)
1209      ( 26.55, 0.60)
1210      ( 30.00, 1.70)
1211      *%-----|-----|
1212      CONTINUOUS NASHYD      NHYD=[ "DI"], DT=[ 1] min, AREA=[ 1.17] (ha),
1213      DWF=[ 0] (cms), CNC=[ 84], IA=[ 9.0] (mm), N=[ 3], TP=[ 0.28] hrs,
1214      Continuous simulation parameters:
1215      I aRECper=[ 4] (hrs),
1216      SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
1217      Inter Event Time=[ 12] (hrs)
1218      Baseflow simulation parameters:
1219      BaseFlowOption=[ 1] ,
1220      Init GWRes Vol=[ 50] (mm), GWRes K=[ 0.96] (mm3/day/mm)
1221      VHydCond=[ 0.055] (mm/hr), END=- 1
1222      *%-----|-----|
1223      CONTINUOUS STANDHYD      NHYD=[ "AI"], DT=[ 1] min, AREA=[ 2.50] (ha), XI MP=[ 0.68], TI MP=[ 0.85],
      DWF=[ 0] (cms), LOSS=[ 1]:
1224      Hort on: Fo=[ 76.20] (mm/hr), Fc=[ 13.20] (mm/hr), DCAY=[ 4.14] (/hr),
      F=[ 0.00] (mm),
1225      Pervious areas: I Aper=[ 4.67] (mm), SLPP=[ 0.5] (%), LGP=[ 50] (m),
      MNP=[ 0.250], SCP=[ 0] (min),
1226      Impervious areas: I Aimp=[ 1.57] (mm), SLPI=[ 0.5] (%),
      LGI=[ 223.607] (m), MNI=[ 0.013], SCI=[ 0] (min),
1227      Continuous simulation parameters:
1228      I aRECper=[ 4] (hrs), I aRECimp=[ 4] (hrs), Inter Event Time=[ 12] (hrs),
      END=- 1
1229      *%-----|-----|

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1230 ROUTE RESERVOIR NHYDout=["A1-STR"], NHYDin=["A1"], RDT=[1](min),
1231 TABLE of (OUTFLOW STORAGE) values
1232 (cms) - (ha-m)
1233 [0.000 , 0.000]
1234 [0.035 , 0.038]
1235 [0.072 , 0.051]
1236 [0.100 , 0.059]
1237 [0.125 , 0.070]
1238 [0.160 , 0.074]
1239 [0.185 , 0.081]
1240 [-1 , -1] (max twenty pts)
1241 NHYDovf=["A1-OVF"]
1242 *%-----|-----|
1243 CONTINUOUS STANDHYD NHYD=["ST-2"], DT=[1]min, AREA=[0.59](ha), XI MP=[0.46],
1244 TIMP=[0.57], DWF=[0](cms), LOSS=[1]:
1245 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1246 F=[0.00](mm),
1247 Pervious areas: I A per=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1248 MNP=[0.250], SCP=[0](min),
1249 ImperVIOUS areas: I Ai mp=[1.57](mm), SLPI=[0.5](%),
1250 LGI=[108.628](m), MNI=[0.013], SCI=[0](min),
1251 Continuous simulation parameters:
1252 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
1253 END=-1
1254 *%-----|-----|
1255 ROUTE RESERVOIR NHYDout=["ST2STR"], NHYDin=["ST-2"], RDT=[1](min),
1256 TABLE of (OUTFLOW STORAGE) values
1257 (cms) - (ha-m)
1258 [0.000 , 0.0000]
1259 [0.052 , 0.0010]
1260 [0.053 , 0.0080]
1261 [-1 , -1] (max twenty pts)
1262 NHYDovf=["ST2OVF"]
1263 *%-----|-----|
1264 *%-----|-----|
1265 *TOTAL FLOW NORTH OF STRANDHERD DR. (EAST BRANCH) CROSSING
1266 *%-----|-----|
1267 CONTINUOUS NASHYD NHYD=["O-8"], DT=[1]min, AREA=[60.55](ha),
1268 DWF=[0](cms), CNV C=[69], I A=[4.0](mm), N=[3], TP=[1.0]hrs,
1269 Continuous simulation parameters:
1270 I a REC per=[4](hrs),
1271 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1272 I n t e r E v e n t T i m e=[12](hrs)
1273 Baseflow simulation parameters:
1274 BaseFlowOption=[1],
1275 I n i t G W R e s V o l=[50](mm), G W R e s K=[0.96](mm/day/mm)
1276 VHydCond=[0.055](mm/hr), END=-1
1277 *%-----|-----|
1278 ROUTE PIPE PTYPE=[2]rect, NHYDout=["O8PIPE"], RNUMBER=[1], PWDTH=[1800](mm),
1279 PHEIGHT=[1200](mm), PLNGTH=[335.1](m),
1280 PROUGH=[0.013], PSLOPE=[0.001](m/m), NHYDin=["O-8"], RDT=[1](min)
1281 *%-----|-----|
1282 *%-----|-----|
1283 ADD HYD NHYDs um=["ST2-IN"], NHYDs to
1284 add=["DRAINI"+"DI"+"A1-STR"+"A1-OVF"+"ST2STR"+"ST2OVF"+"O8PIPE"]
1285 *%-----|-----|
1286 CONTINUOUS STANDHYD NHYD=["A7"], DT=[1]min, AREA=[3.51](ha), XI MP=[0.68], TIMP=[0.85],
1287 DWF=[0](cms), LOSS=[1]:
1288 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1289 F=[0.00](mm),
1290 Pervious areas: I A per=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1291 MNP=[0.250], SCP=[0](min),
1292 ImperVIOUS areas: I Ai mp=[1.57](mm), SLPI=[0.5](%),
1293 LGI=[264.953](m), MNI=[0.013], SCI=[0](min),
1294 Continuous simulation parameters:
1295 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),

END=- 1

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1285 *%-----|-----|
1286 ROUTE RESERVOIR NHYDout=["A7-STR"], NHYDin=["A7"], RDT=[1](min),
1287 TABLE of ( OUTFLOW STORAGE ) values
1288 (cms) - (ha-m)
1289 [ 0.000 , 0.000 ]
1290 [ 0.049 , 0.054 ]
1291 [ 0.102 , 0.072 ]
1292 [ 0.140 , 0.082 ]
1293 [ 0.175 , 0.099 ]
1294 [ 0.225 , 0.105 ]
1295 [ 0.260 , 0.114 ]
1296 [ -1 , -1 ] (max twenty pts)
1297 NHYDovf=["A7-OVF"]
1298 *%-----|-----|
1299 CONTINUOUS STANDHYD NHYD=["ST-3"], DT=[1]min, AREA=[0.71](ha), XI MP=[0.46],
TI MP=[0.57], DWF=[0](cms), LOSS=[1]:
1300 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1301 Pervious areas: IAper=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1302 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
LGI=[119.164](m), MNI=[0.013], SCI=[0](min),
1303 Continuous simulation parameters:
1304 IaRECper=[4](hrs), IaRECimp=[4](hrs), InterEventTime=[12](hrs),
END=- 1
1305 *%-----|-----|
1306 ROUTE RESERVOIR NHYDout=["ST3STR"], NHYDin=["ST-3"], RDT=[1](min),
1307 TABLE of ( OUTFLOW STORAGE ) values
1308 (cms) - (ha-m)
1309 [ 0.000 , 0.0000 ]
1310 [ 0.063 , 0.0010 ]
1311 [ 0.064 , 0.0094 ]
1312 [ -1 , -1 ] (max twenty pts)
1313 NHYDovf=["ST3OVF"]
1314 *%-----|-----|
1315 *ANALYSIS POINT 2 - TOTAL FLOW AT OUTLET OF STREET 2/3 INTERSECTION
1316 *%-----|-----|
1317 ADD HYD NHYDsum=["PT2ST3"], NHYDsto
add=["ST2-IN"+"A7-STR"+"A7-OVF"+"ST3STR"+"ST3OVF"]
1318 *%-----|-----|
1319 *ROUTE FLOW through O Keefe Drain 2
1320 ROUTE CHANNEL NHYDout=["DRAIN2"], NHYDin=["PT2ST3"], RDT=[1](min),
1321 CHLGTH=[592](m), CHSLOPE=[.23](%), FPSLOPE=[.23](%),
1322 SECNUM=[1], NSEG=[3]
1323 ( SEGROUGH, SEGDIST (m))=[0.07, 12.60 -0.043, 17.40 0.07, 30.00] NSEG
times
1324 ( DISTANCE (m), ELEVATION (m))=[0.00, 1.70]
1325 (2.60, 0.95)
1326 (12.60, 0.75)
1327 (14.10, 0.00)
1328 (15.90, 0.00)
1329 (17.40, 0.75)
1330 (27.40, 0.95)
1331 (30.00, 1.70)
1332 *%-----|-----|
1333 CONTINUOUS NASHYD NHYD=["D2"], DT=[1]min, AREA=[2.28](ha), DWF=[0](cms), CNVC=[84],
IA=[9.0](mm),
1334 N=[3], TP=[0.99]hrs,
1335 Continuous simulation parameters:
1336 IaRECper=[4](hrs),
1337 SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1338 InterEventTime=[12](hrs)
1339 Baseflow simulation parameters:
1340 BaseFlowOption=[1],
1341 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
```

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1342          VHydCond=[ 0. 055] ( mm/ hr ) ,      END=- 1
1343 *%-----|-----|
1344 CONTINUOUS STANDHYD NHYD=[ " A17" ] , DT=[ 1] mi n , AREA=[ 12. 04] ( ha) , XI MP=[ 0. 68] ,
TI MP=[ 0. 85] , DWF=[ 0] ( cms) , LOSS=[ 1] :
1345 Horton: Fo=[ 76. 20] ( mm/ hr) , Fc=[ 13. 20] ( mm/ hr) , DCAY=[ 4. 14] ( / hr) ,
F=[ 0. 00] ( mm) ,
1346 Pervious areas: I A per =[ 4. 67] ( mm) , SLPP=[ 0. 5] ( % ) , LGP=[ 50] ( m) ,
MNP=[ 0. 250] , SCP=[ 0] ( mi n) ,
1347 ImperVIOUS areas: I A i mp=[ 1. 57] ( mm) , SLPI =[ 0. 5] ( % ) ,
LGI =[ 490. 714] ( m) , MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
1348 Continuous simulation parameters:
1349 I a REC per =[ 4] ( hr s) , I a REC i mp=[ 4] ( hr s) , I n t e r E v e n t T i m e =[ 12] ( hr s) ,
END=- 1
1350 *%-----|-----|
1351 ROUTE RESERVOIR NHYDout =[ " A17STR" ] , NHYD i n=[ " A17" ] , RDT=[ 1] ( mi n) ,
1352 TABLE of ( OUTFLOW STORAGE ) values
1353 ( cms) - ( ha- m)
1354 [ 0. 000 , 0. 000 ]
1355 [ 0. 169 , 0. 185 ]
1356 [ 0. 349 , 0. 248 ]
1357 [ 0. 482 , 0. 283 ]
1358 [ 0. 602 , 0. 338 ]
1359 [ 0. 771 , 0. 359 ]
1360 [ 0. 891 , 0. 391 ]
1361 [ - 1 , - 1 ] ( m a x t w e n t y p t s)
1362 NHYDovf =[ " A17OVF" ]
1363 *%-----|-----|
1364 CONTINUOUS STANDHYD NHYD=[ " ST- 4" ] , DT=[ 1] mi n , AREA=[ 0. 35] ( ha) , XI MP=[ 0. 46] ,
TI MP=[ 0. 57] , DWF=[ 0] ( cms) , LOSS=[ 1] :
1365 Horton: Fo=[ 76. 20] ( mm/ hr) , Fc=[ 13. 20] ( mm/ hr) , DCAY=[ 4. 14] ( / hr) ,
F=[ 0. 00] ( mm) ,
1366 Pervious areas: I A per =[ 4. 67] ( mm) , SLPP=[ 0. 5] ( % ) , LGP=[ 50] ( m) ,
MNP=[ 0. 250] , SCP=[ 0] ( mi n) ,
1367 ImperVIOUS areas: I A i mp=[ 1. 57] ( mm) , SLPI =[ 0. 5] ( % ) , LGI =[ 83. 666] ( m) ,
MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
1368 Continuous simulation parameters:
1369 I a REC per =[ 4] ( hr s) , I a REC i mp=[ 4] ( hr s) , I n t e r E v e n t T i m e =[ 12] ( hr s) ,
END=- 1
1370 *%-----|-----|
1371 ROUTE RESERVOIR NHYDout =[ " ST4STR" ] , NHYD i n=[ " ST- 4" ] , RDT=[ 1] ( mi n) ,
1372 TABLE of ( OUTFLOW STORAGE ) values
1373 ( cms) - ( ha- m)
1374 [ 0. 000 , 0. 0000 ]
1375 [ 0. 031 , 0. 0010 ]
1376 [ 0. 032 , 0. 0050 ]
1377 [ - 1 , - 1 ] ( m a x t w e n t y p t s)
1378 NHYDovf =[ " ST4OVF" ]
1379 *%-----|-----|
1380 CONTINUOUS STANDHYD NHYD=[ " A18" ] , DT=[ 1] mi n , AREA=[ 5. 30] ( ha) , XI MP=[ 0. 68] , TI MP=[ 0. 85] ,
DWF=[ 0] ( cms) , LOSS=[ 1] :
1381 Horton: Fo=[ 76. 20] ( mm/ hr) , Fc=[ 13. 20] ( mm/ hr) , DCAY=[ 4. 14] ( / hr) ,
F=[ 0. 00] ( mm) ,
1382 Pervious areas: I A per =[ 4. 67] ( mm) , SLPP=[ 0. 5] ( % ) , LGP=[ 50] ( m) ,
MNP=[ 0. 250] , SCP=[ 0] ( mi n) ,
1383 ImperVIOUS areas: I A i mp=[ 1. 57] ( mm) , SLPI =[ 0. 5] ( % ) ,
LGI =[ 325. 576] ( m) , MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
1384 Continuous simulation parameters:
1385 I a REC per =[ 4] ( hr s) , I a REC i mp=[ 4] ( hr s) , I n t e r E v e n t T i m e =[ 12] ( hr s) ,
END=- 1
1386 *%-----|-----|
1387 ROUTE RESERVOIR NHYDout =[ " A18STR" ] , NHYD i n=[ " A18" ] , RDT=[ 1] ( mi n) ,
1388 TABLE of ( OUTFLOW STORAGE ) values
1389 ( cms) - ( ha- m)
1390 [ 0. 000 , 0. 000 ]
1391 [ 0. 074 , 0. 082 ]
1392 [ 0. 154 , 0. 109 ]

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1393         [ 0.212 , 0.125 ]
1394         [ 0.265 , 0.149 ]
1395         [ 0.339 , 0.158 ]
1396         [ 0.392 , 0.172 ]
1397         [ -1 , -1 ] (max twenty pts)
1398         NHYDovf=[ "A18OVF" ]
1399 *%-----|-----|
1400 *ANALYSIS POINT 3 - TOTAL FLOW AT OUTLET OF STREET 4
1401 *%-----|-----|
1402 ADD HYD          NHYDsum=[ "PT3ST4" ], NHYDsto
add=[ "DRAIN2"+"D2"+"A17STR"+"A17OVF"+"ST4STR"+"ST4OVF"+"A18STR"+"A18OVF" ]
1403 *%-----|-----|
1404 *ROUTE FLOW through O Keefe Drain 3
1405 ROUTE CHANNEL   NHYDout=[ "DRAIN3" ], NHYDin=[ "PT3ST4" ], RDT=[ 1 ] (min),
1406                CHLGTH=[ 525 ] (m), CHSLOPE=[ .23 ] (%), FPSLOPE=[ .23 ] (%),
1407                SECNUM=[ 1 ], NSEG=[ 3 ]
1408                ( SEGROUGH, SEGDIST (m) )=[ 0.07, 12.50 -0.043, 17.50 0.07, 30.00 ] NSEG
times
1409                ( DISTANCE (m), ELEVATION (m) )=[ 0.00, 1.70 ]
1410                ( 2.50, 1.00 )
1411                ( 12.50, 0.80 )
1412                ( 14.10, 0.00 )
1413                ( 15.90, 0.00 )
1414                ( 17.50, 0.80 )
1415                ( 27.50, 1.00 )
1416                ( 30.00, 1.70 )
1417 *%-----|-----|
1418 CONTINUOUS NASHYD NHYD=[ "D3" ], DT=[ 1 ] min, AREA=[ 2.51 ] (ha),
1419                DWF=[ 0 ] (cms), CNVC=[ 86 ], IA=[ 8.7 ] (mm), N=[ 3 ], TP=[ 0.73 ] hrs,
1420                Continuous simulation parameters:
1421                IaRECper=[ 4 ] (hrs),
1422                SMN=[ -1 ] (mm), SMAX=[ -1 ] (mm), SK=[ 0.010 ] / (mm),
1423                InterEventTime=[ 12 ] (hrs)
1424                Baseflow simulation parameters:
1425                BaseFlowOption=[ 1 ],
1426                InitGWResVol=[ 50 ] (mm), GWResK=[ 0.96 ] (mm/day/mm)
1427                VHydCond=[ 0.055 ] (mm/hr), END=-1
1428 *%-----|-----|
1429 CONTINUOUS STANDHYD NHYD=[ "C1" ], DT=[ 1 ] min, AREA=[ 3.41 ] (ha), XI MP=[ 0.68 ], TI MP=[ 0.85 ],
DWF=[ 0 ] (cms), LOSS=[ 1 ]:
1430                Horton: Fo=[ 76.20 ] (mm/hr), Fc=[ 13.20 ] (mm/hr), DCAY=[ 4.14 ] (/hr),
F=[ 0.00 ] (mm),
1431                Pervious areas: IAper=[ 4.67 ] (mm), SLPP=[ 0.5 ] (%), LGP=[ 50 ] (m),
MNP=[ 0.250 ], SCP=[ 0 ] (min),
1432                Impervious areas: IAimp=[ 1.57 ] (mm), SLPI=[ 0.5 ] (%),
LGI=[ 261.151 ] (m), MNI=[ 0.013 ], SCI=[ 0 ] (min),
1433                Continuous simulation parameters:
1434                IaRECper=[ 4 ] (hrs), IaRECimp=[ 4 ] (hrs), InterEventTime=[ 12 ] (hrs),
END=-1
1435 *%-----|-----|
1436 ROUTE RESERVOIR NHYDout=[ "C1-STR" ], NHYDin=[ "C1" ], RDT=[ 1 ] (min),
1437                TABLE of ( OUTFLOW STORAGE ) values
1438                ( cms ) - ( ha-m )
1439                [ 0.000 , 0.000 ]
1440                [ 0.048 , 0.052 ]
1441                [ 0.099 , 0.070 ]
1442                [ 0.136 , 0.080 ]
1443                [ 0.170 , 0.096 ]
1444                [ 0.218 , 0.102 ]
1445                [ 0.252 , 0.111 ]
1446                [ -1 , -1 ] (max twenty pts)
1447                NHYDovf=[ "C1-OVF" ]
1448 *%-----|-----|
1449 CONTINUOUS STANDHYD NHYD=[ "ST-5" ], DT=[ 1 ] min, AREA=[ 0.45 ] (ha), XI MP=[ 0.46 ],
TI MP=[ 0.57 ], DWF=[ 0 ] (cms), LOSS=[ 1 ]:
1450                Horton: Fo=[ 76.20 ] (mm/hr), Fc=[ 13.20 ] (mm/hr), DCAY=[ 4.14 ] (/hr),

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1451 F=[ 0. 00] ( mm) ,
      Pervious areas: I A per =[ 4. 67] ( mm) , SLPP=[ 0. 5] ( % ) , LGP=[ 50] ( m) ,
      MNP=[ 0. 250] , SCP=[ 0] ( mi n) ,
1452 Impervious areas: I A i mp =[ 1. 57] ( mm) , SLPI =[ 0. 5] ( % ) , LGI =[ 94. 868] ( m) ,
      MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
1453 Continuous simulation parameters:
1454 I a REC per =[ 4] ( hrs) , I a REC i mp =[ 4] ( hrs) , I nter Event Ti me =[ 12] ( hrs) ,
      END=- 1
1455 *%-----|
1456 ROUTE RESERVOIR NHYDout =[ " ST5STR" ] , NHYDi n =[ " ST- 5" ] , RDT =[ 1] ( mi n) ,
1457 TABLE of ( OUTFLOW STORAGE ) values
1458 ( cms) - ( ha- m)
1459 [ 0. 000 , 0. 0000 ]
1460 [ 0. 040 , 0. 0010 ]
1461 [ 0. 041 , 0. 0062 ]
1462 [ - 1 , - 1 ] ( max t wenty pts)
1463 NHYDovf =[ " ST5OVF" ]
1464 *%-----|
1465 ADD HYD NHYDs um =[ " ST5- E" ] , NHYDs to
      add =[ " DRAI N3" + " D3" + " C1- STR" + " C1- OVF" + " ST5STR" + " ST5OVF" ]
1466 *%-----|
1467 CONTINUOUS STANDHYD NHYD =[ " STRAND" ] , DT =[ 1] ( mi n) , AREA =[ 7. 59] ( ha) ,
1468 XI MP =[ 0. 64] , TI MP =[ 0. 85] , DWF =[ 0] ( cms) , LOSS =[ 1] :
1469 Horton: Fo =[ 76. 20] ( mm/ hr) , Fc =[ 13. 20] ( mm/ hr) , DCAY =[ 4. 14] ( / hr) ,
      F =[ 0. 00] ( mm) ,
1470 Pervious areas: I A per =[ 4. 67] ( mm) , SLPP =[ 0. 5] ( % ) , LGP =[ 40] ( m) ,
      MNP =[ 0. 250] , SCP =[ 0] ( mi n) ,
1471 Impervious areas: I A i mp =[ 1. 57] ( mm) , SLPI =[ 0. 5] ( % ) , LGI =[ 1230] ( m) ,
      MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
1472 Continuous simulation parameters:
1473 I a REC per =[ 4] ( hrs) , I a REC i mp =[ 4] ( hrs) , I nter Event Ti me =[ 12] ( hrs) ,
      END=- 1
1474 *%-----|
1475 ROUTE RESERVOIR NHYDout =[ " S- POND" ] , NHYDi n =[ " STRAND" ] , RDT =[ 1] ( mi n) ,
1476 TABLE of ( OUTFLOW STORAGE ) values
1477 ( cms) - ( ha- m)
1478 [ 0. 000 , 0. 000 ]
1479 [ 0. 033 , 0. 188 ]
1480 [ 0. 057 , 0. 253 ]
1481 [ 0. 104 , 0. 287 ]
1482 [ 0. 160 , 0. 336 ]
1483 [ 0. 340 , 0. 346 ]
1484 [ 0. 471 , 0. 360 ]
1485 [ 0. 824 , 0. 390 ]
1486 [ - 1 , - 1 ] ( max t wenty pts)
1487 NHYDovf =[ " S- OVF" ]
1488 *%-----|
1489 ADD HYD NHYDs um =[ " SSAOUT" ] , NHYDs to add =[ " ST5- E" + " S- POND" + " S- OVF" ]
1490 *%-----|
1491 SAVE HYD NHYD =[ " SSAOUT" ] , # OF PCYCLES =[ 5] , I CASEs h =[ 1]
1492 HYD_ COMMENT =[ " SSAOUT" ]
1493 *%-----|
1494 CONTINUOUS STANDHYD NHYD =[ " Area- A" ] , DT =[ 1] mi n , AREA =[ 66. 75] ( ha) , XI MP =[ 0. 64] ,
      TI MP =[ 0. 80] , DWF =[ 0] ( cms) , LOSS =[ 1] :
1495 Horton: Fo =[ 76. 20] ( mm/ hr) , Fc =[ 13. 20] ( mm/ hr) , DCAY =[ 4. 14] ( / hr) ,
      F =[ 0. 00] ( mm) ,
1496 Pervious areas: I A per =[ 4. 67] ( mm) , SLPP =[ 0. 5] ( % ) , LGP =[ 50] ( m) ,
      MNP =[ 0. 250] , SCP =[ 0] ( mi n) ,
1497 Impervious areas: I A i mp =[ 1. 57] ( mm) , SLPI =[ 0. 5] ( % ) ,
      LGI =[ 1155. 422] ( m) , MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
1498 Continuous simulation parameters:
1499 I a REC per =[ 4] ( hrs) , I a REC i mp =[ 4] ( hrs) , I nter Event Ti me =[ 12] ( hrs) ,
      END=- 1
1500 *%-----|
1501 SAVE HYD NHYD =[ " Area- A" ] , # OF PCYCLES =[ 1] , I CASEs h =[ 1]
1502 HYD_ COMMENT =[ " SMMF- A I nflow" ]

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1503 *%-----|-----|
1504 ROUTE RESERVOIR NHYDout=["SWMF-A"], NHYDin=["Area-A"], RDT=[1](min),
1505 TABLE of ( OUTFLOW STORAGE ) values
1506 (cms) - (ha-m)
1507 [ 0.000 , 0.000 ]
1508 [ 0.103 , 1.077 ]
1509 [ 0.128 , 1.749 ]
1510 [ 0.382 , 2.282 ]
1511 [ 0.703 , 2.582 ]
1512 [ 1.256 , 2.978 ]
1513 [ 1.567 , 3.202 ]
1514 [ 1.955 , 3.493 ]
1515 [ 2.100 , 3.600 ]
1516 [ -1 , -1 ] (max twenty pts)
1517 NHYDovf=["SWVAOV"]
1518 *%-----|-----|
1519 SAVE HYD NHYD=["SWMF-A"], # OF PCYCLES=[1], ICASEsh=[1]
1520 HYD_COMMENT=["SMMF-A Outflow"]
1521 *%-----|-----|
1522 *ANALYSIS POINT 4 - TOTAL FLOW AT OUTLET OF STREET 5
1523 *%-----|-----|
1524 ADD HYD NHYDs um=["PT4ST5"], NHYDs to add=["SSAOUT"+"SWMF-A"+"SWVAOV"]
1525 *%-----|-----|
1526 CONTINUOUS STANDHYD NHYD=["C6"], DT=[1]min, AREA=[1.87](ha), XI MP=[0.68], TI MP=[0.85],
DWF=[0](cms), LOSS=[1]:
1527 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1528 Pervious areas: I A per=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1529 Impervious areas: I A i mp=[1.57](mm), SLPI=[0.5](%),
LGI=[193.391](m), MNI=[0.013], SCI=[0](min),
1530 Continuous simulation parameters:
1531 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=-1
1532 *%-----|-----|
1533 ROUTE RESERVOIR NHYDout=["C6-STR"], NHYDin=["C6"], RDT=[1](min),
1534 TABLE of ( OUTFLOW STORAGE ) values
1535 (cms) - (ha-m)
1536 [ 0.000 , 0.000 ]
1537 [ 0.026 , 0.029 ]
1538 [ 0.054 , 0.038 ]
1539 [ 0.075 , 0.044 ]
1540 [ 0.093 , 0.052 ]
1541 [ 0.120 , 0.056 ]
1542 [ 0.138 , 0.061 ]
1543 [ -1 , -1 ] (max twenty pts)
1544 NHYDovf=["C6-OVF"]
1545 *%-----|-----|
1546 CONTINUOUS STANDHYD NHYD=["C7"], DT=[1]min, AREA=[1.62](ha), XI MP=[0.68], TI MP=[0.85],
DWF=[0](cms), LOSS=[1]:
1547 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1548 Pervious areas: I A per=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1549 Impervious areas: I A i mp=[1.57](mm), SLPI=[0.5](%),
LGI=[180.000](m), MNI=[0.013], SCI=[0](min),
1550 Continuous simulation parameters:
1551 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=-1
1552 *%-----|-----|
1553 ROUTE RESERVOIR NHYDout=["C7-STR"], NHYDin=["C7"], RDT=[1](min),
1554 TABLE of ( OUTFLOW STORAGE ) values
1555 (cms) - (ha-m)
1556 [ 0.000 , 0.000 ]
1557 [ 0.023 , 0.025 ]
1558 [ 0.047 , 0.033 ]

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1559          [ 0.065 , 0.038 ]
1560          [ 0.081 , 0.045 ]
1561          [ 0.104 , 0.048 ]
1562          [ 0.120 , 0.053 ]
1563          [ -1 , -1 ] (max twenty pts)
1564          NHYDovf=["C7-OVF"]
1565 *%-----|-----|
1566 CONTINUOUS STANDHYD NHYD=["ST-6"], DT=[1] min, AREA=[0.41](ha), XI MP=[0.46], TI MP=[0.57],
DWF=[0](cms), LOSS=[1]:
1567 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1568 Pervious areas: I A per=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1569 Impervious areas: I A i mp=[1.57](mm), SLPI=[0.5](%), LGI=[90.554](m),
MNI=[0.013], SCI=[0](min),
1570 Continuous simulation parameters:
1571 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=-1
1572 *%-----|-----|
1573 ROUTE RESERVOIR NHYDout=["ST6STR"], NHYDin=["ST-6"], RDT=[1](min),
1574 TABLE of ( OUTFLOW STORAGE ) values
1575 (cms) - (ha-m)
1576 [ 0.000 , 0.0000 ]
1577 [ 0.036 , 0.0010 ]
1578 [ 0.037 , 0.0058 ]
1579 [ -1 , -1 ] (max twenty pts)
1580          NHYDovf=["ST6OVF"]
1581 *%-----|-----|
1582 *ANALYSIS POINT 5 - TOTAL FLOW AT OUTLET OF STREET 6
1583 *%-----|-----|
1584 ADD HYD NHYDsum=["PT5ST6"], NHYDs to
add=["PT4ST5"+"C6-STR"+"C6-OVF"+"C7-STR"+"C7-OVF"+"ST6STR"+"ST6OVF"]
1585 *%-----|-----|
1586 *ROUTE FLOW through O Keefe Drain 4
1587 ROUTE CHANNEL NHYDout=["DRAIN4"], NHYDin=["PT5ST6"], RDT=[1](min),
1588 CHLGTH=[324](m), CHSLOPE=[.10](%), FPSLOPE=[.10](%),
1589 SECNUM=[1], NSEG=[3]
1590 ( SEGROUGH, SEGDI ST (m))=[0.07, 12.00 -0.043, 18.00 0.07, 30.00] NSEG
t i m e s
1591 ( DI STANCE (m), ELEVATION (m))=[0.00, 2.00]
1592 (2.00, 1.20)
1593 (12.00, 1.00)
1594 (14.00, 0.00)
1595 (16.00, 0.00)
1596 (18.00, 1.00)
1597 (28.00, 1.20)
1598 (30.00, 2.00)
1599 *%-----|-----|
1600 CONTINUOUS NASHYD NHYD=["D4"], DT=[1] min, AREA=[1.73](ha), DWF=[0](cms), CNV C=[88],
I A=[8.4](mm),
1601 N=[3], TP=[0.60] hrs,
1602 Continuous simulation parameters:
1603 I a REC per=[4](hrs),
1604 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1605 I n t e r E v e n t T i m e=[12](hrs)
1606 Baseflow simulation parameters:
1607 BaseFlowOption=[1],
1608 I n i t G W R e s V o l=[50](mm), G W R e s K=[0.96](mm/day/mm)
1609 VHydCond=[0.055](mm/hr), END=-1
1610 *%-----|-----|
1611 CONTINUOUS STANDHYD NHYD=["Area-B"], DT=[1] min, AREA=[24.04](ha), XI MP=[0.62],
TI MP=[0.77], DWF=[0](cms), LOSS=[1]:
1612 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1613 Pervious areas: I A per=[4.67](mm), SLPP=[1.4](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),

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1614      Impervious areas: IAImp=[ 1.57](mm), SLPI=[ 1.4](%),
1615      LGI=[ 693.397](m), MNI=[ 0.013], SCI=[ 0](min),
1616      Continuous simulation parameters:
1617      IARECper=[ 4](hrs), IARECimp=[ 4](hrs), InterEventTime=[ 12](hrs),
1618      END=- 1
1619 *%-----|-----|
1620 ROUTE RESERVOIR      NHYDout=["SWMF- B"], NHYDin=["Area- B"], RDT=[ 1](min),
1621      TABLE of ( OUTFLOW STORAGE ) values
1622      (cms) - (ha-m)
1623      [ 0.000 , 0.000 ]
1624      [ 0.025 , 0.090 ]
1625      [ 0.175 , 0.510 ]
1626      [ 0.350 , 0.710 ]
1627      [ 0.495 , 0.820 ]
1628      [ 0.648 , 0.980 ]
1629      [ 0.965 , 1.045 ]
1630      [ 1.072 , 1.140 ]
1631      [ -1 , -1 ] (max twenty pts)
1632      NHYDovf=["SWMBOVF"]
1633 *%-----|-----|
1634 ADD HYD              NHYDs um=["D4- EX"], NHYDs to add=["DRAIN4"+"D4"+"SWMF- B"+"SWMBOVF"]
1635 *%-----|-----|
1636 *ROUTE FLOW THROUGH O Keefe Drain 5
1637 * JFSA: Nov. 2020, added endpoints to close X-Section
1638 ROUTE CHANNEL      NHYDout=["DRAIN5"], NHYDin=["D4- EX"], RDT=[ 1](min),
1639      CHLGTH=[ 413.0](m), CHSLOPE=[ 0.16](%), FPSLOPE=[ 0.16](%),
1640      SECNUM=[ 1], NSEG=[ 3]
1641      ( SEGROUGH, SEGDIST (m))=[ 0.043, 12.29 -0.033, 17.97
1642      0.043, 32.84] NSEG times
1643      ( DISTANCE (m), ELEVATION (m))=(-0.01, 2.50)
1644      [ 0.00, 1.41]
1645      [ 6.13, 0.97]
1646      [ 12.29, 0.89]
1647      [ 15.71, 0.00]
1648      [ 17.97, 0.39]
1649      [ 23.04, 0.35]
1650      [ 32.83, 0.96]
1651      (32.84, 2.50)
1652 *%-----|-----|
1653 CONTINUOUS NASHYD   NHYD=["D5"], DT=[ 1]min, AREA=[ 1.90](ha),
1654      DWF=[ 0](cms), CNVC=[ 86], IA=[ 8.7](mm), N=[ 3], TP=[ 0.69]hrs,
1655      Continuous simulation parameters:
1656      IARECper=[ 4](hrs),
1657      SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1658      InterEventTime=[ 12](hrs)
1659      Baseflow simulation parameters:
1660      BaseFlowOption=[ 1],
1661      InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
1662      VHydCond=[ 0.055](mm/hr), END=- 1
1663 *%-----|-----|
1664 *EXTERNAL FLOWS SOUTHEAST OF THE SITE NORTH OF McKENNA CASEY DR.
1665 CONTINUOUS NASHYD   NHYD=["O-13SDF"], DT=[ 1]min, AREA=[ 9.74](ha),
1666      DWF=[ 0](cms), CNVC=[ 81], IA=[ 4.0](mm), N=[ 3], TP=[ .43]hrs,
1667      Continuous simulation parameters:
1668      IARECper=[ 4](hrs),
1669      SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1670      InterEventTime=[ 12](hrs)
1671      Baseflow simulation parameters:
1672      BaseFlowOption=[ 1],
1673      InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
1674      VHydCond=[ 0.055](mm/hr), END=- 1
1675 *%-----|-----|
1676 *SNOW DISPOSAL FACILITY
1677 *PARAMETERS BASED ON ROBINSON 2006 MODEL
1678 ROUTE RESERVOIR      NHYDout=["SDF"], NHYDin=["O-13SDF"], RDT=[ 1](min),
1679      TABLE of ( OUTFLOW STORAGE ) values

```

```

1678             ( cms ) - ( ha - m )
1679             [ 0. 000, 0. 000 ]
1680             [ 0. 150, 0. 600 ]
1681             ( 0. 200, 1. 500 )
1682             [ - 1 , - 1 ] ( max t w e n t y p t s )
1683             NHYDovf=[ " OVFSDF " ]
1684 *%-----|-----|
1685 *ANALYSIS POINT 6 - McKenna Casey Dr.
1686 *%-----|-----|
1687 ADD HYD           NHYDsum=[ " PT6MC " ], NHYDs to add=[ " DRAIN5 "+" D5 "+" SDF " ]
1688 *%-----|-----|
1689 CONTINUOUS NASHYD NHYD=[ " O- 15 " ], DT=[ 1 ] mi n , AREA=[ 10. 67 ] ( ha ) ,
1690 DWF=[ 0 ] ( cms ) , CNVC=[ 82 ] , IA=[ 7. 5 ] ( mm ) , N=[ 3 ] , TP=[ 0. 30 ] hr s ,
1691 Continuous simulation parameters:
1692 IaRECper=[ 4 ] ( hr s ) ,
1693 SMN=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0. 010 ] / ( mm ) ,
1694 InterEventTime=[ 12 ] ( hr s )
1695 Baseflow simulation parameters:
1696 BaseFlowOption=[ 1 ] ,
1697 InitGWResVol=[ 50 ] ( mm ) , GWResK=[ 0. 96 ] ( mm / day / mm )
1698 VHydCond=[ 0. 055 ] ( mm / hr ) , END=- 1
1699 *%-----|-----|
1700 *TOTAL FLOW NORTH OF MCKENNA CASEY DR.
1701 ADD HYD           NHYDsum=[ " M C " ], NHYDs to add=[ " PT6MC "+" O- 15 " ]
1702 *%-----|-----|
1703 *ROUTE FLOW THROUGH AREA O- 14
1704 * JFSA: Nov. 2020, added end points to close X-section
1705 ROUTE CHANNEL    NHYDout=[ " O- 14Ch " ], NHYDin=[ " M C " ], RDT=[ 1 ] ( mi n ) ,
1706 CHLGT=[ 845. 3 ] ( m ) , CHSLOPE=[ 0. 10 ] ( % ) , FPSLOPE=[ 0. 10 ] ( % ) ,
1707 SECNUM=[ 1 ] , NSEG=[ 3 ]
1708 ( SEGROUGH, SEGDIST ( m ) )=[ 0. 06, 15. 00 - 0. 033, 18. 04 0. 06, 31. 85 ] NSEG
1709 times
1710 ( DISTANCE ( m ) , ELEVATION ( m ) )=[ - 0. 01, 2. 5
1711 ( 0. 00, 1. 53 ]
1712 ( 5. 56, 1. 47 )
1713 ( 9. 21, 1. 45 )
1714 ( 12. 45, 1. 53 )
1715 ( 13. 70, 1. 50 )
1716 ( 15. 00, 0. 69 )
1717 ( 15. 34, 0. 00 )
1718 ( 16. 51, 0. 05 )
1719 ( 17. 30, 0. 17 )
1720 ( 18. 04, 0. 74 )
1721 ( 19. 29, 1. 32 )
1722 ( 22. 73, 1. 47 )
1723 ( 31. 84, 1. 41 )
1724 ( 31. 85, 2. 50 )
1725 *%-----|-----|
1726 *% -Change O- 14 from NASHYD to STANDHYD, name it "S-1-Okeefe" and add it to S-1
1727 subcatchment based on Project 1474-BCDC, JFSA, Nov. 2020
1728 *% -JFSA 2021-02-16, add detailed subcatchment drainage area for each subcatchment
1729 in Corrigan sub-catchment. After adding part of O- 14 to S_1 sub-catchment so O- 14
1730 becomes 5 ha instead of 30.02 ha and TP becomes 0.133 (5*0.8/30.02) instead of 0.8
1731 CONTINUOUS NASHYD NHYD=[ " O- 14 " ], DT=[ 1 ] mi n , AREA=[ 5 ] ( ha ) ,
1732 DWF=[ 0 ] ( cms ) , CNVC=[ 82 ] , IA=[ 7. 5 ] ( mm ) , N=[ 3 ] , TP=[ 0. 133 ] hr s ,
1733 Continuous simulation parameters:
1734 IaRECper=[ 4 ] ( hr s ) ,
1735 SMN=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0. 010 ] / ( mm ) ,
1736 InterEventTime=[ 12 ] ( hr s )
1737 Baseflow simulation parameters:
1738 BaseFlowOption=[ 1 ] ,
1739 InitGWResVol=[ 50 ] ( mm ) , GWResK=[ 0. 96 ] ( mm / day / mm )
1740 VHydCond=[ 0. 055 ] ( mm / hr ) , END=- 1
1741 *
1742 *%-----|-----|
1743 *ANALYSIS POINT 7 - JOCK RIVER

```

```

1740 * 2020-12-01 To Foster Drain
1741 * 2020-12-01 replace ("PT7JR") by ("OKEEFE")
1742 *%-----|-----|
1743 ADD HYD          NHYDsum=["OKEEFE"], NHYDs to add=["O-14Ch"+"O-14"]
1744 *%-----|-----|
1745 *CONTINUOUS STANDHYD NHYD=["OKEEFE"], DT=[1](min), AREA=[448](ha),
1746 *          XI MP=[0.65], TI MP=[0.65], DWF=[0](cms), LOSS=[2],
1747 *          SCS curve number CN=[77],
1748 *          Pervious surfaces: I A per=[4.67](mm), SLPP=[0.5](%),
1749 *          LGP=[40](m), MNP=[0.25], SCP=[0](min),
1750 *          Impervious surfaces: I A i mp=[1.57](mm), SLPI=[0.5](%),
1751 *          LGI=[1728](m), MNI=[0.013], SCI=[0](min),
1752 *          Continuous simulation parameters:
1753 *          I a REC per=[4](hrs), I a REC i mp=[4](hrs),
1754 *          SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1755 *          Inter Event Ti me=[18](hrs), END=-1
1756 *#*****
1757 *#      Okeefe Pond
1758 *#      - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
1759 *#      and a ratio of the catchment area to the West Clarke pond rating curve
1760 *#      from the M55 for the next coordinates
1761 *#*****
1762 *ROUTE RESERVOIR  NHYDout=["P_OKE"], NHYDin=["OKEEFE"],
1763 *          RDT=[1](min),
1764 *          TABLE of ( OUTFLOW STORAGE ) values
1765 *          ( cms ) - ( ha-m )
1766 *          [ 0.0 , 0.0 ]
1767 *          [ 14.13 , 13.0 ]
1768 *          [ -1 , -1 ] (maximum one hundred pairs of points)
1769 *          NHYDovf=["ok-OVF"],
1770 *%-----|-----|
1771 * -JFSA 2021-02-25 "S-1-D2" and "S-1-D3" are part of S-1 sub-catchment. They are
1772 * moved to drain before station 6215 on Jock River
1773 *CONTINUOUS STANDHYD NHYD=["S-1-D2"], DT=[1](min), AREA=[18.67](ha), XI MP=[0.65],
1774 *          TI MP=[0.65], DWF=[0](cms),
1775 *          LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
1776 *          I A per=[4.67](mm), SLPP=[2.0](%),
1777 *          LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
1778 *          I A i mp=[1.57](mm), SLPI=[0.75](%),
1779 *          LGI=[352.798](m), MNI=[0.013], SCI=[0](min),
1780 *          Continuous simulation parameters:
1781 *          I a REC per=[4](hrs), I a REC i mp=[4](hrs),
1782 *          SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1783 *          Inter Event Ti me=[12](hrs), END=-1
1784 *%-----|-----|
1785 *CONTINUOUS NASHYD  NHYD=["S-1-D2"], DT=[1]min, AREA=[18.67](ha),
1786 *          DWF=[0](cms), CNVC=[77], I A=[4.67](mm),
1787 *          N=[3], TP=[1.120]hrs,
1788 *          Continuous simulation parameters:
1789 *          I a REC per=[4](hrs),
1790 *          SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1791 *          Inter Event Ti me=[12](hrs)
1792 *          Baseflow simulation parameters:
1793 *          BaseFlowOption=[1],
1794 *          I n i t GWR es Vol =[50](mm), GWR es K=[0.96](mm/day/mm)
1795 *          VHydCond=[0.055](mm/hr), END=-1
1796 *%-----|-----|
1797 *COMPUTE DUALHYD  NHYDin=["S-1-D2"], CINLET=[2.062](cms), NINLET=[1],
1798 *          M a j NHYD=["S-1-D2J"]
1799 *          M n NHYD=["S-1-D2N"]
1800 *          T M I STO=[9999999](cu-m)
1801 *%-----|-----|
1802 *ADD HYD          NHYDsum=["S-1-D2S"], NHYDs to add=["S-1-D2J"+"S-1-D2N"]
1803 *%-----|-----|
1804 *ROUTE RESERVOIR  NHYDout=["S-1-D2R"], NHYDin=["S-1-D2S"],

```

```

1801 *          RDT=[ 1 ] ( mi n ) ,
1802 *          TABLE of ( OUTFLOW STORAGE ) values
1803 *                ( cms ) - ( ha - m )
1804 *                [ 0.0      , 0.0 ]
1805 *                [ 0.2231, 0.7445 ]
1806 *                [   -1   ,  -1   ] (max twenty pts)
1807 *          NHYDovf=[ "S- 1- D2Rovf" ]
1808 *%-----|-----|
1809 CONTINUOUS STANDHYD NHYD=[ "S- 1- D3" ] , DT=[ 1 ] ( mi n ) , AREA=[ 6.79 ] ( ha ) , XI MP=[ 0.65 ] ,
TI MP=[ 0.65 ] , DWF=[ 0 ] ( cms ) ,
1810 LOSS=[ 2 ] , SCS curve number CN=[ 75 ] , Pervious surfaces:
1811 IAper=[ 4.67 ] ( mm ) , SLPP=[ 2.0 ] ( % ) ,
LGP=[ 40 ] ( m ) , MNP=[ 0.25 ] , SCP=[ 0 ] ( mi n ) , Impervious surfaces:
1812 IAi mp=[ 1.57 ] ( mm ) , SLPI=[ 0.75 ] ( % ) ,
1813 LGI=[ 212.760 ] ( m ) , MNI=[ 0.013 ] , SCI=[ 0 ] ( mi n ) ,
1814 Continuous simulation parameters:
1815 IaRECPper=[ 4 ] ( hrs ) , IaRECI mp=[ 4 ] ( hrs ) ,
1816 SM N=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0.010 ] / ( mm ) ,
1817 InterEventTime=[ 12 ] ( hrs ) , END=- 1
1818 *%-----|-----|
1819 *CONTINUOUS NASHYD NHYD=[ "S- 1- D3" ] , DT=[ 1 ] mi n , AREA=[ 6.79 ] ( ha ) ,
1820 * DWF=[ 0 ] ( cms ) , CN C=[ 77 ] , IA=[ 4.67 ] ( mm ) ,
1821 * N=[ 3 ] , TP=[ 1.281 ] hrs ,
1822 * Continuous simulation parameters:
1823 * IaRECPper=[ 4 ] ( hrs ) ,
1824 * SM N=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0.010 ] / ( mm ) ,
1825 * InterEventTime=[ 12 ] ( hrs )
1826 * Baseflow simulation parameters:
1827 * BaseFlowOption=[ 1 ] ,
1828 * InitGWResVol=[ 50 ] ( mm ) , GWResK=[ 0.96 ] ( mm / day / mm )
1829 * VHydCond=[ 0.055 ] ( mm / hr ) , END=- 1
1830 *%-----|-----|
1831 *COMPUTE DUALHYD NHYDin=[ "S- 1- D3" ] , CINLET=[ 0.719 ] ( cms ) , NINLET=[ 1 ] ,
1832 * MajNHYD=[ "S- 1- D3J" ]
1833 * MnNHYD=[ "S- 1- D3N" ]
1834 * TMS TO=[ 9999999 ] ( cu - m )
1835 *%-----|-----|
1836 *ADD HYD NHYDsum=[ "S- 1- D3S" ] , NHYDs to add=[ "S- 1- D3J" + "S- 1- D3N" ]
1837 *%-----|-----|
1838 *ROUTE RESERVOIR NHYDout=[ "S- 1- D3R" ] , NHYDin=[ "S- 1- D3S" ] ,
1839 * RDT=[ 1 ] ( mi n ) ,
1840 *          TABLE of ( OUTFLOW STORAGE ) values
1841 *                ( cms ) - ( ha - m )
1842 *                [ 0.0      , 0.0 ]
1843 *                [ 0.0811, 0.2708 ]
1844 *                [   -1   ,  -1   ] (max twenty pts)
1845 *          NHYDovf=[ "S- 1- D3Rovf" ]
1846 *%-----|-----|
1847 *ADD HYD NHYDsum=[ "SN_OK" ] , NHYDs to add=[ "N_OK" + "OKEEFE" + "S- 1- D2" + "S- 1- D3" ]
1848 *%-----|-----|
1849 *SAVE HYD NHYD=[ "SN_OK" ] , # OF PCYCLES=[ - 1 ] , ICASEsh=[ 1 ]
HYD_COMMENT=[ "Total Flows at Okeefe Drain" ]
1850 *%-----|-----|
1851 *#
1852 *# Hydrograph from Node Okeefe routed to Node at Foster Drain
1853 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
1854 *#
1855 *ROUTE CHANNEL NHYDout=[ "N_FO" ] , NHYDin=[ "SN_OK" ] ,
1856 * RDT=[ 1 ] ( mi n ) ,
1857 * CHLGTH=[ 1183 ] ( m ) , CHSLOPE=[ 0.0761 ] ( % ) ,
1858 * FPSLOPE=[ 0.0761 ] ( % ) ,
1859 * SECNUM=[ 1.0 ] , NSEG=[ 3 ]
1860 * ( SEGROUGH, SEGDI ST ( m ) ) =
1861 * [ 0.050, - 33.89
1862 * - 0.035, 31.59
1863 * 0.050, 34.41 ] NSEG times

```

```

1864      ( DI STANCE ( m), ELEVATI ON ( m) ) =
1865      [- 794. 18, 91. 00]
1866      [- 775. 41, 91. 50]
1867      [- 702. 63, 91. 50]
1868      [- 546. 19, 91. 50]
1869      [- 529. 54, 91. 50]
1870      [- 323. 44, 91. 00]
1871      [- 320. 71, 91. 00]
1872      [- 183. 59, 91. 00]
1873      [- 182. 54, 90. 50]
1874      [- 181. 36, 90. 00]
1875      [- 177. 37, 90. 00]
1876      [- 87. 70, 90. 00]
1877      [- 33. 89, 90. 00]
1878      [- 18. 52, 86. 88]
1879      [ 0. 00, 85. 20]
1880      [ 16. 20, 86. 83]
1881      [ 31. 59, 90. 00]
1882      [ 33. 03, 90. 50]
1883      [ 34. 41, 91. 00]
1884      *%-----|-----|
1885      *#*****|
1886      *#      Catchment FOSTER
1887      *#      - To Foster ditch (north of the Jock)
1888      *#      - Partially developed (medium density); remaining agricultural
1889      *#      - 2020-12-01 JFSA Foster area is 332 as per Foster SWF Environmental Study
1890      *#      - 2020-12-01 decrease Foster drainage area from (373 HA) to (307.98 HA) after
1891      *#      - 2021-02-12 update Foster area to 325.44 ha as measured from QGIS
1892      *#*****|
1893      CONTINUOUS STANDHYD NHYD=[ "FOSTER" ], DT=[ 1] mi n, AREA=[ 325. 44] ( ha),
1894      XI MP=[ 0. 55], TI MP=[ 0. 55], DWF=[ 0] ( cms), LOSS=[ 2],
1895      SCS curve number CN=[ 74],
1896      Pervious surfaces: I A per=[ 4. 67] ( mm), SLPP=[ 0. 5] ( %),
1897      LGP=[ 40] ( m), MNP=[ 0. 25], SCP=[ 0] ( mi n),
1898      Impervious surfaces: I A i mp=[ 1. 57] ( mm), SLPI=[ 0. 5] ( %),
1899      LGI=[ 1472. 956] ( m), MNI=[ 0. 013], SCI=[ 0] ( mi n),
1900      Continuous simulation parameters:
1901      I a REC per=[ 4] ( hr s), I a REC i mp=[ 4] ( hr s),
1902      SM N=[ - 1] ( mm), SMAX=[ - 1] ( mm), SK=[ 0. 010] / ( mm),
1903      Inter Event Ti me=[ 18] ( hr s), END=- 1
1904      *#*****|
1905      *#      Foster Pond
1906      *#      - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
1907      *#      and a ratio of the catchment area to the West Clarke pond rating curve
1908      *#      from the MS for the next coordinates
1909      *#*****|
1910      ROUTE RESERVOIR      NHYDout =[" P_FOS" ],      NHYDin=[" FOSTER" ],
1911      RDT=[ 1] ( mi n),
1912      TABLE of ( OUTFLOW STORAGE ) values
1913      ( cms ) - ( ha- m)
1914      [ 0. 0 , 0. 0 ]
1915      [ 10. 34 , 10]
1916      [ - 1 , - 1 ] ( max twenty pts)
1917      NHYDovf=[" FO- OVF" ]
1918      *%-----|-----|
1919      ADD HYD      NHYDsum=[" FOSTER- OUT" ], NHYDs to add=[" P_FOS"+" FO- OVF" ]
1920      *%-----|-----|
1921      *#*****|
1922      *#      -Brazeau area from P 1800-19 =[71.751], change to 63.59 ha based on GIS measurements
1923      *#      -JFSA, 2021-01-19 update "W_CLAR_BRAZ" to 73.29 ha based on GIS measurements
1924      *#      -JFSA, 2021-01-22 Brazeau ("MS_P10"+"P10-OVF")brazeau pond discharges directly
1925      to the jock river through a road side ditch on the west side of Borrisokane road
1926      (station 6016)

```

```

1925 CONTINUOUS STANDHYD NHYD=[ "W_CLAR_BRAZ" ], DT=[ 1 ] mi n, AREA=[ 73.29 ] ( ha ),
1926 XI MP=[ 0.6 ], TI MP=[ 0.65 ], DWF=[ 0 ] ( cms ), LOSS=[ 2 ],
1927 SCS curve number CN=[ 77 ],
1928 Pervious surfaces: I A per=[ 4.67 ] ( mm ), SLPP=[ 1 ] ( % ),
1929 LGP=[ 40 ] ( m ), MNP=[ 0.25 ], SCP=[ 0 ] ( mi n ),
1930 Impervious surfaces: I A i mp=[ 1.57 ] ( mm ), SLPI=[ 0.5 ] ( % ),
1931 LGI=[ 699.00 ] ( m ), MNI=[ 0.013 ], SCI=[ 0 ] ( mi n ),
1932 Continuous simulation parameters:
1933 I a REC per=[ 4 ] ( hr s ), I a REC i mp=[ 4 ] ( hr s ),
1934 SM N=[ -1 ] ( mm ), SMAX=[ -1 ] ( mm ), SK=[ 0.010 ] / ( mm ),
1935 Inter Event Ti me=[ 18 ] ( hr s ), END=- 1
1936 *%-----|-----|
1937 * 2020-12-01 correct pond curve values
1938 ROUTE RESERVOIR NHYDout=[ "MS_P10" ], NHYDin=[ "W_CLAR_BRAZ" ],
1939 RDT=[ 1 ] ( mi n ),
1940 TABLE of ( OUTFLOW STORAGE ) values
1941 ( cms ) - ( ha - m )
1942 [ 0.0 , 0.0 ]
1943 [ 0.068 , 0.001 ]
1944 [ 0.271 , 0.022 ]
1945 [ 0.379 , 0.051 ]
1946 [ 0.48 , 0.091 ]
1947 [ 0.853 , 0.341 ]
1948 [ 1.005 , 0.61 ]
1949 [ 1.128 , 1.231 ]
1950 [ 1.155 , 1.592 ]
1951 [ 1.194 , 1.876 ]
1952 [ 1.2 , 1.921 ]
1953 [ 1.259 , 2.369 ]
1954 [ 1.3 , 2.665 ]
1955 [ 1.349 , 2.813 ]
1956 [ -1 , -1 ] (max twenty pts)
1957 NHYDovf=[ "P10-OVF" ]
1958 *%-----|-----|
1959 * -JFSA 2021-02-26 "S-1-FO-D2" is a part of S-1 sub-catchment. It is moved to drain
before station 980 on Foster Drain
1960 CONTINUOUS STANDHYD NHYD=[ "S-1-FO-D2" ], DT=[ 1 ] mi n, AREA=[ 4.94 ] ( ha ),
1961 XI MP=[ 0.55 ], TI MP=[ 0.55 ], DWF=[ 0 ] ( cms ), LOSS=[ 2 ],
1962 SCS curve number CN=[ 74 ],
1963 Pervious surfaces: I A per=[ 4.67 ] ( mm ), SLPP=[ 0.5 ] ( % ),
1964 LGP=[ 40 ] ( m ), MNP=[ 0.25 ], SCP=[ 0 ] ( mi n ),
1965 Impervious surfaces: I A i mp=[ 1.57 ] ( mm ), SLPI=[ 0.5 ] ( % ),
1966 LGI=[ 181.475 ] ( m ), MNI=[ 0.013 ], SCI=[ 0 ] ( mi n ),
1967 Continuous simulation parameters:
1968 I a REC per=[ 4 ] ( hr s ), I a REC i mp=[ 4 ] ( hr s ),
1969 SM N=[ -1 ] ( mm ), SMAX=[ -1 ] ( mm ), SK=[ 0.010 ] / ( mm ),
1970 Inter Event Ti me=[ 18 ] ( hr s ), END=- 1
1971 *%-----|-----|
1972 *CONTINUOUS NASHYD NHYD=[ "S-1-FO-D2" ], DT=[ 1 ] mi n, AREA=[ 4.94 ] ( ha ),
1973 * DWF=[ 0 ] ( cms ), CNV C=[ 77 ], I A=[ 4.67 ] ( mm ),
1974 * N=[ 3 ], TP=[ 1.10 ] hr s,
1975 * Continuous simulation parameters:
1976 * I a REC per=[ 4 ] ( hr s ),
1977 * SM N=[ -1 ] ( mm ), SMAX=[ -1 ] ( mm ), SK=[ 0.010 ] / ( mm ),
1978 * Inter Event Ti me=[ 12 ] ( hr s )
1979 * Baseflow simulation parameters:
1980 * BaseFl owOpt ion=[ 1 ] ,
1981 * I ni t GWRes Vol =[ 50 ] ( mm ), GWRes K=[ 0.96 ] ( mm / day / mm )
1982 * VHydCond=[ 0.055 ] ( mm / hr ), END=- 1
1983 *%-----|-----|
1984 *COMPUTE DUALHYD NHYDin=[ "S-1-FO-D2" ], CI NLET=[ 0.508 ] ( cms ), NI NLET=[ 1 ],
1985 * M a j NHYD=[ "S-1-FO-D2J" ]
1986 * M nNHYD=[ "S-1-FO-D2N" ]
1987 * TM I STO=[ 9999999 ] ( cu - m )
1988 *%-----|-----|
1989 *ADD HYD NHYDs um=[ "S-1-FO-D2S" ], NHYDs to add=[ "S-1-FO-D2J"+"S-1-FO-D2N" ]

```

```

1990 *%-----|-----|
1991 *ROUTE RESERVOIR      NHYDout=["S-1-FO-D2R"] , NHYDin=["S-1-FO-D2S"] ,
1992 *                      RDT=[1](min),
1993 *                      TABLE of ( OUTFLOW STORAGE ) values
1994 *                      (cms) - (ha-m)
1995 *                      [ 0.0      , 0.0 ]
1996 *                      [ 0.0590, 0.1970 ]
1997 *                      [   -1   ,  -1   ] (max twenty pts)
1998 *                      NHYDovf=["S-1FOD2ovf"]
1999 *%-----|-----|
2000 ADD HYD              NHYDsum=["980"], NHYDsto add=["FOSTER-OUT"+"S-1-FO-D2"]
2001 *%-----|-----|
2002 SAVE HYD            NHYD=["980"], # OF PCYCLES=[-1], ICASEsh=[1]
2003                    HYD_COMMENT=["Total Flows at Station 980 on Foster Drain"]
2004 *%-----|-----|
2005 *#
2006 *# Hydrograph from Node Foster SWM (Station 980) to Node at station 520
2007 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 980
2008 *#
2009 ROUTE CHANNEL      NHYDout=["980-out"] , NHYDin=["980"] ,
2010                    RDT=[1](min),
2011                    CHLGTH=[460](m),  CHSLOPE=[0.04348](%),
2012                    FPSLOPE=[0.04348](%),
2013                    SECNUM=[1.0],    NSEG=[3]
2014                    ( SEGROUGH, SEGDI ST (m))=
2015                    [ 0.050, 45.90
2016                    -0.035, 53.30
2017                    0.050, 100] NSEG times
2018                    ( DISTANCE (m), ELEVATION (m))=
2019                    [ 0, 91.75 ]
2020                    [ 42.4, 92.18 ]
2021                    [ 43.5, 92.16 ]
2022                    [ 44.1, 92.1 ]
2023                    [ 44.6, 92 ]
2024                    [ 44.8, 91.86 ]
2025                    [ 45.9, 91.04 ]
2026                    [ 46.4, 90.65 ]
2027                    [ 46.8, 90.36 ]
2028                    [ 47.9, 90.32 ]
2029                    [ 48.7, 90.35 ]
2030                    [ 50.7, 90.33 ]
2031                    [ 52.2, 90.38 ]
2032                    [ 52.5, 90.59 ]
2033                    [ 53.3, 91.28 ]
2034                    [ 54, 91.83 ]
2035                    [ 54.3, 92 ]
2036                    [ 54.8, 92.08 ]
2037                    [ 55.4, 92.12 ]
2038                    [ 100, 91.84 ]
2039 *%-----|-----|
2040 * -JFSA 2021-02-26 "S-1-FO-DI" is a part of S-1 sub-catchment. It is moved to drain
before station 520 on Foster Drain
2041 CONTINUOUS STANDHYD NHYD=["S-1-FO-DI"], DT=[1]min, AREA=[5.11](ha),
2042                    XI MP=[0.65], TI MP=[0.65], DWF=[0](cms), LOSS=[2],
2043                    SCS curve number CN=[74],
2044                    Pervious surfaces: I A per=[4.67](mm), SLPP=[0.5](%),
2045                    LGP=[40](m), MNP=[0.25], SCP=[0](min),
2046                    Impervious surfaces: I A i mp=[1.57](mm), SLPI=[0.5](%),
2047                    LGI=[184.572](m), MNI=[0.013], SCI=[0](min),
2048                    Continuous simulation parameters:
2049                    I a REC per=[4](hrs), I a REC i mp=[4](hrs),
2050                    SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2051                    Inter Event Time=[18](hrs), END=-1
2052 *%-----|-----|
2053 *COMPUTE DUALHYD    NHYDin=["S-1-FO-DI"], CNILET=[0.605](cms), NI NLET=[1],
2054 *                    Mij NHYD=["S-1-FO-DIJ"]

```



```

2055 * M nNHYD=[ "S- 1- FO- DIN" ]
2056 * TM STO=[ 9999999 ] ( cu- m)
2057 *%-----|-----|
2058 *ADD HYD NHYDsum=[ "S- 1- FO- DIS" ], NHYDs to add=[ "S- 1- FO- DIN" + "S- 1- FO- DIJ" ]
2059 *%-----|-----|
2060 *ROUTE RESERVOIR NHYDout=[ "S- 1- FO- DIR" ] , NHYDin=[ "S- 1- FO- DIS" ] ,
2061 * RDT=[ 1 ] ( mi n) ,
2062 * TABLE of ( OUTFLOW STORAGE ) values
2063 * ( cms ) - ( ha- m)
2064 * [ 0. 0 , 0. 0 ]
2065 * [ 0. 0611, 0. 2038 ]
2066 * [ -1 , -1 ] (max twenty pts)
2067 * NHYDovf=[ "S- 1FODlovf" ]
2068 *%-----|-----|
2069 ADD HYD NHYDsum=[ "520" ], NHYDs to add=[ "980- out " + "S- 1- FO- DI" ]
2070 *%-----|-----|
2071 SAVE HYD NHYD=[ "520" ], # OF PCYCLES=[ - 1 ], ICASEsh=[ 1 ]
2072 HYD_COMMENT=[ "Total Flows at Sation 520 on Foster Drain" ]
2073 *%-----|-----|
2074 *# Hydrograph from Node at Station 520 (Foster Drain) to Node at station 6016 (Jock
River)
2075 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 520
2076 *#
2077 ROUTE CHANNEL NHYDout = [ "520- out " ] , NHYDin = [ "520" ] ,
2078 RDT = [ 1 ] ( mi n) ,
2079 CHLGTH = [ 860 ] ( m) , CHSLOPE = [ 0. 5872 ] ( % ) ,
2080 FPSLOPE = [ 0. 5872 ] ( % ) ,
2081 SECNUM = [ 1. 0 ] , NSEG = [ 3 ]
2082 ( SEGROUGH, SEGDI ST ( m) ) =
2083 [ 0. 050, 45. 90
2084 - 0. 035, 54. 3
2085 0. 050, 100. 1097 ] NSEG times
2086 ( DI STANCE ( m) , ELEVATI ON ( m) ) =
2087 [ 0 , 91. 26 ]
2088 [ 44. 9 , 91. 46 ]
2089 [ 45. 1 , 91. 37 ]
2090 [ 45. 9 , 90. 84 ]
2091 [ 47 , 90. 32 ]
2092 [ 47. 5 , 90. 22 ]
2093 [ 48 , 90. 17 ]
2094 [ 50. 7 , 90. 19 ]
2095 [ 51. 5 , 90. 17 ]
2096 [ 52. 2 , 90. 13 ]
2097 [ 52. 7 , 90. 12 ]
2098 [ 53. 3 , 90. 14 ]
2099 [ 53. 5 , 90. 31 ]
2100 [ 53. 9 , 90. 59 ]
2101 [ 54. 3 , 90. 87 ]
2102 [ 54. 7 , 91. 04 ]
2103 [ 55. 3 , 91. 24 ]
2104 [ 55. 5 , 91. 26 ]
2105 [ 63. 7 , 91. 37 ]
2106 [ 100. 1097 , 91. 43 ]
2107 *%-----|-----|
2108 * -JFSA 2021-02-26 "S- 1- FO- F- D" is a part of S- 1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2109 CONTINUOUS STANDHYD NHYD=[ "S- 1- FO- F- D" ], DT=[ 1 ] mi n, AREA=[ 14. 96 ] ( ha) ,
2110 XI MP=[ 0. 65 ] , TI MP=[ 0. 65 ] , DWF=[ 0 ] ( cms ) , LOSS=[ 2 ] ,
2111 SCS curve number CN=[ 74 ] ,
2112 Pervious surfaces: I A per = [ 4. 67 ] ( mm) , SLPP = [ 0. 5 ] ( % ) ,
2113 LGP = [ 40 ] ( m) , MNP = [ 0. 25 ] , SCP = [ 0 ] ( mi n) ,
2114 Impervious surfaces: I A i mp = [ 1. 57 ] ( mm) , SLPI = [ 0. 5 ] ( % ) ,
2115 LGI = [ 315. 806 ] ( m) , MNI = [ 0. 013 ] , SCI = [ 0 ] ( mi n) ,
2116 Continuous simulation parameters:
2117 I a REC per = [ 4 ] ( hr s) , I a REC i mp = [ 4 ] ( hr s) ,
2118 SM N = [ - 1 ] ( mm) , SMAX = [ - 1 ] ( mm) , SK = [ 0. 010 ] / ( mm) ,

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2119      InterEventTime=[ 18](hrs),      END=- 1
2120  *%-----|-----|
2121  *CONTINUOUS NASHYD  NHYD=["S-1-FO-F-D"], DT=[ 1]min, AREA=[ 14.96](ha),
2122  *                   DWF=[ 0](cms), CNVC=[ 77], IA=[ 4.67](mm),
2123  *                   N=[ 3], TP=[ 1.007]hrs,
2124  *                   Continuous simulation parameters:
2125  *                   IaRECper=[ 4](hrs),
2126  *                   SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2127  *                   InterEventTime=[ 12](hrs)
2128  *                   Baseflow simulation parameters:
2129  *                   BaseFlowOption=[ 1],
2130  *                   InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
2131  *                   VHydCond=[ 0.055](mm/hr),      END=- 1
2132  *%-----|-----|
2133  *COMPUTE DUALHYD   NHYDin=["S-1-FO-F-D"], CINLET=[ 1.749](cms), NINLET=[ 1],
2134  *                   MajNHYD=["S-1FO-F-DJ"]
2135  *                   MnNHYD=["S-1FO-F-DN"]
2136  *                   TMSSTO=[ 9999999](cu-m)
2137  *%-----|-----|
2138  *ADD HYD           NHYDsum=["S-1FO-F-DS"], NHYDs to add=["S-1FO-F-DJ"+"S-1FO-F-DN"]
2139  *%-----|-----|
2140  *ROUTE RESERVOIR  NHYDout=["S-1FO-F-DR"], NHYDin=["S-1FO-F-DS"],
2141  *                   RDT=[ 1](min),
2142  *                   TABLE of ( OUTFLOW STORAGE ) values
2143  *                   ( cms ) - ( ha-m )
2144  *                   [ 0.0      , 0.0 ]
2145  *                   [ 0.1788, 0.5966 ]
2146  *                   [ -1     , -1     ] (max twenty pts)
2147  *                   NHYDovf=["S-1FoFDovf"]
2148  *%-----|-----|
2149  * -JFSA 2021-02-26 "S-1-D8" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2150  CONTINUOUS STANDHYD NHYD=["S-1-D8"], DT=[ 1]min, AREA=[ 5.27](ha), XI MP=[ 0.325],
TI MP=[ 0.65], DWF=[ 0](cms), LOSS=[ 1]:
2151  Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
F=[ 0.00](mm),
2152  Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
MNP=[ 0.250], SCP=[ 0](min),
2153  Impervious areas: IAimp=[ 0.785](mm), SLPI=[ 0.75](%),
LGI=[ 187.439](m), MNI=[ 0.013], SCI=[ 0](min),
2154  Continuous simulation parameters:
2155  IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
END=- 1
2156  *%-----|-----|
2157  *CONTINUOUS NASHYD  NHYD=["S-1-D8"], DT=[ 1]min, AREA=[ 5.27](ha),
2158  *                   DWF=[ 0](cms), CNVC=[ 77], IA=[ 4.67](mm),
2159  *                   N=[ 3], TP=[ 1.10]hrs,
2160  *                   Continuous simulation parameters:
2161  *                   IaRECper=[ 4](hrs),
2162  *                   SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2163  *                   InterEventTime=[ 12](hrs)
2164  *                   Baseflow simulation parameters:
2165  *                   BaseFlowOption=[ 1],
2166  *                   InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
2167  *                   VHydCond=[ 0.055](mm/hr),      END=- 1
2168  *%-----|-----|
2169  *COMPUTE DUALHYD   NHYDin=["S-1-D8"], CINLET=[ 2.279](cms), NINLET=[ 1],
2170  *                   MajNHYD=["S-1-D8J"]
2171  *                   MnNHYD=["S-1-D8N"]
2172  *                   TMSSTO=[ 9999999](cu-m)
2173  *%-----|-----|
2174  *ADD HYD           NHYDsum=["S-1-D8S"], NHYDs to add=["S-1-D8J"+"S-1-D8N"]
2175  *%-----|-----|
2176  *ADD HYD           NHYDsum=["S-1-D"], NHYDs to add=["S-1-Okeefe"+"S-1"+"S-1-Fost"]
2177  *%-----|-----|
2178  *COMPUTE DUALHYD   NHYDin=["S-1-D"], CINLET=[ 11.616](cms), NINLET=[ 1],

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2179 *           Mj NHYD=[ " S- 1- D- M " ]
2180 *           MnNHYD=[ " S- 1- D- MN" ]
2181 *           TM STO=[ 5974 ] ( cu- m)
2182 *%-----|-----
2183 *ADD HYD           NHYDs um=[ " S- 1- DEV" ] , NHYDs t o add=[ " S- 1- D- M" +" S- 1- D- MN" ]
2184 *%-----|-----
2185 *ROUTE RESERVOIR  NHYDout =[ " S- 1- D8R" ] , NHYDi n=[ " S- 1- D8S" ] ,
2186 *           RDT=[ 1 ] ( mi n) ,
2187 *           TABLE of ( OUTFLOW STORAGE ) values
2188 *                   ( cms ) - ( ha- m)
2189 *                   [ 0. 0      , 0. 0 ]
2190 *                   [ 0. 0630, 0. 2102 ]
2191 *                   [      -1 , -1      ] (max twenty pts)
2192 *           NHYDovf=[ " S- 1- D8Rovf" ]
2193 *%-----|-----
2194 * -JFSA 2021-02-26 "S-1-A" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2195 CONTINUOUS NASHYD NHYD=[ " S- 1- A" ] , DT=[ 1 ] mi n, AREA=[ 75. 88 ] ( ha) ,
2196 DWF=[ 0 ] ( cms ) , CN C=[ 77 ] , IA=[ 4. 67 ] ( mm) ,
2197 N=[ 3 ] , TP=[ 0. 619 ] hr s ,
2198 Continuous simulation parameters:
2199 IaRECper=[ 4 ] ( hr s) ,
2200 SM N=[ - 1 ] ( mm) , SMAX=[ - 1 ] ( mm) , SK=[ 0. 010 ] / ( mm) ,
2201 InterEvent Time=[ 12 ] ( hr s)
2202 Baseflow simulation parameters:
2203 BaseFlowOption=[ 1 ] ,
2204 Init GWRes Vol =[ 50 ] ( mm) , GWRes K=[ 0. 96 ] ( mm/ day/ mm)
2205 VHydCond=[ 0. 055 ] ( mm/ hr) , END=- 1
2206 *%-----|-----
2207 * -JFSA, 2021-01-22 "W_CLAR_UNDE" (west of Clarke sub-catchment) discharges
directly to the jock river through a road side ditch on the west side of Borrisokane
road (station 6016)
2208 CONTINUOUS NASHYD NHYD=[ " W_CLAR_UNDE" ] , DT=[ 1 ] mi n, AREA=[ 35. 65 ] ( ha) ,
2209 DWF=[ 0 ] ( cms ) , CN C=[ 77 ] , IA=[ 4. 67 ] ( mm) ,
2210 N=[ 3 ] , TP=[ 1. 10 ] hr s ,
2211 Continuous simulation parameters:
2212 IaRECper=[ 4 ] ( hr s) ,
2213 SM N=[ - 1 ] ( mm) , SMAX=[ - 1 ] ( mm) , SK=[ 0. 010 ] / ( mm) ,
2214 InterEvent Time=[ 12 ] ( hr s)
2215 Baseflow simulation parameters:
2216 BaseFlowOption=[ 1 ] ,
2217 Init GWRes Vol =[ 50 ] ( mm) , GWRes K=[ 0. 96 ] ( mm/ day/ mm)
2218 VHydCond=[ 0. 055 ] ( mm/ hr) , END=- 1
2219 *%-----|-----
2220 ADD HYD           NHYDs um=[ " SN_FO" ] , NHYDs t o
add=[ " N_FO" +" 520- out " +" MS_P10" +" P10- OVF" +" W_CLAR_UNDE" +" S- 1- FO- F- D" +" S- 1- D8" +" S- 1- A" ]
2221 *%-----|-----
2222 SAVE HYD          NHYD=[ " SN_FO" ] , # OF PCYCLES=[ - 1 ] , I CASEs h=[ 1 ]
2223 HYD_COMMENT=[ " Total Flows at Foster Drain" ]
2224 *%-----|-----
2225 *# Hydrograph from Node Foster routed to Node at Cedarview Road
2226 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6016
2227 *#
2228 ROUTE CHANNEL     NHYDout =[ " N_CE" ] , NHYDi n=[ " SN_FO" ] ,
2229 RDT=[ 1 ] ( mi n) ,
2230 CHLGTH=[ 159 ] ( m) , CHSLOPE=[ 0. 0818 ] ( % ) ,
2231 FPSLOPE=[ 0. 0818 ] ( % ) ,
2232 SECNUM=[ 1. 0 ] , NSEG=[ 3 ]
2233 ( SEGROUGH, SEGDI ST ( m) ) =
2234 [ 0. 050, - 15. 46
2235 - 0. 035, 26. 55
2236 0. 050, 116. 76 ] NSEG times
2237 ( DI STANCE ( m) , ELEVATI ON ( m) ) =
2238 [ - 645. 23, 91. 50 ]
2239 [ - 391. 20, 91. 50 ]
2240 [ - 91. 00, 91. 50 ]

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2241          [- 85.52, 91.50]
2242          [- 15.46, 89.40]
2243          [- 9.79, 89.31]
2244          [- 3.22, 86.24]
2245          [ 3.22, 85.07]
2246          [10.96, 85.79]
2247          [16.44, 86.49]
2248          [26.55, 89.45]
2249          [29.03, 90.27]
2250          [35.76, 90.67]
2251          [36.67, 91.00]
2252          [108.08, 91.00]
2253          [109.82, 90.50]
2254          [112.04, 90.50]
2255          [114.62, 91.00]
2256          [116.76, 91.50]
2257  *%-----|-----|
2258  *#*****|
2259  *#      Catchment S-1
2260  *#      - To Jock River (north and south of Jock)
2261  *#      - Primarily agricultural fields; portion of sand quarry
2262  *%-----|-----|
2263  *%      -2020-12-17 "S-1-Undev" and "S-1-Fost" was a part of Foster drain, they are below
the foster pond. Now they are added to S-1 subcatchment based on Project 1474-BCDC,
JFSA, Nov. 2020
2264  *%      -2020-12-17 Change O-14 (it was part of Okeefe drain) to "S-1-Okeefe" and add it
to S-1 subcatchment based on Project 1474-BCDC, JFSA, Nov. 2020
2265  *%      -2020-12-17 Add "S-1-BCDC" as NASHYD
2266  *%      -2020-12-17 all other S-1 subcatchment as STANDHYD with DUALHYD and ROUTE RESERVOIR
2267  *%-----|-----|
2268  *#*****|
2269  *      -JFSA 2021-02-26 "S-1-A" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2270  *CONTINUOUS NASHYD  NHYD=["S-1-A"], DT=[1]min, AREA=[75.88](ha),
2271  *                    DWF=[0](cms), CNVC=[77], IA=[4.67](mm),
2272  *                    N=[3], TP=[0.619]hrs,
2273  *                    Continuous simulation parameters:
2274  *                    IaRECper=[4](hrs),
2275  *                    SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2276  *                    InterEventTime=[12](hrs)
2277  *                    Baseflow simulation parameters:
2278  *                    BaseFlowOption=[1],
2279  *                    InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2280  *                    VHydCond=[0.055](mm/hr), END=-1
2281  *%-----|-----|
2282  CONTINUOUS NASHYD  NHYD=["S-1-B"], DT=[1]min, AREA=[55.36](ha),
2283  *                    DWF=[0](cms), CNVC=[77], IA=[4.67](mm),
2284  *                    N=[3], TP=[0.451]hrs,
2285  *                    Continuous simulation parameters:
2286  *                    IaRECper=[4](hrs),
2287  *                    SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2288  *                    InterEventTime=[12](hrs)
2289  *                    Baseflow simulation parameters:
2290  *                    BaseFlowOption=[1],
2291  *                    InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2292  *                    VHydCond=[0.055](mm/hr), END=-1
2293  *%-----|-----|
2294  *#      - JFSA 2021-02-24 change the name from S-1-BCDC to S-1-A and S-1-B. Change their
TP values based on the new areas compared to the old ones.
2295  *CONTINUOUS NASHYD  NHYD=["S-1-BCDC"], DT=[1]min, AREA=[134.9](ha),
2296  *                    DWF=[0](cms), CNVC=[77], IA=[4.67](mm),
2297  *                    N=[3], TP=[1.10]hrs,
2298  *                    Continuous simulation parameters:
2299  *                    IaRECper=[4](hrs),
2300  *                    SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2301  *                    InterEventTime=[12](hrs)

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2302 *          Baseflow simulation parameters:
2303 *          BaseFlowOption=[ 1] ,
2304 *          InitGWResVol =[ 50](mm) , GWResK=[ 0.96](mm/day/mm)
2305 *          VHydCond=[ 0.055](mm/hr) ,    END=- 1
2306 *%-----|-----
2307 *# - JFSA 2021-02-24 "S-1-BCDC-1" and "S-1-BCDC-2" are not existing anymore.
      "S-1-BCDC-1" is part of "S-1-FO-D2" and "S-1-BCDC-2" is part of "S-1-D2" and "S-1-D3"
2308 *CONTINUOUS NASHYD  NHYD=["S-1-BCDC-1"], DT=[ 1]min, AREA=[ 0.3](ha),
2309 *          DWF=[ 0](cms) , CN/C=[ 77] , IA=[ 4.67](mm) ,
2310 *          N=[ 3] , TP=[ 1.10]hrs ,
2311 *          Continuous simulation parameters:
2312 *          IaRECper=[ 4](hrs) ,
2313 *          SMN=[ -1](mm) , SMAX=[ -1](mm) , SK=[ 0.010]/(mm) ,
2314 *          InterEventTime=[ 12](hrs)
2315 *          Baseflow simulation parameters:
2316 *          BaseFlowOption=[ 1] ,
2317 *          InitGWResVol =[ 50](mm) , GWResK=[ 0.96](mm/day/mm)
2318 *          VHydCond=[ 0.055](mm/hr) ,    END=- 1
2319 *%-----|-----
2320 *CONTINUOUS NASHYD  NHYD=["S-1-BCDC-2"], DT=[ 1]min, AREA=[ 1.3](ha),
2321 *          DWF=[ 0](cms) , CN/C=[ 77] , IA=[ 4.67](mm) ,
2322 *          N=[ 3] , TP=[ 1.10]hrs ,
2323 *          Continuous simulation parameters:
2324 *          IaRECper=[ 4](hrs) ,
2325 *          SMN=[ -1](mm) , SMAX=[ -1](mm) , SK=[ 0.010]/(mm) ,
2326 *          InterEventTime=[ 12](hrs)
2327 *          Baseflow simulation parameters:
2328 *          BaseFlowOption=[ 1] ,
2329 *          InitGWResVol =[ 50](mm) , GWResK=[ 0.96](mm/day/mm)
2330 *          VHydCond=[ 0.055](mm/hr) ,    END=- 1
2331 *%-----|-----
2332 *# - JFSA 2021-01-19, after adding Greenbank pond, "S-1-BCDC-3" is not existing
      anymore
2333 *CONTINUOUS NASHYD  NHYD=["S-1-BCDC-3"], DT=[ 1]min, AREA=[ 3.9](ha),
2334 *          DWF=[ 0](cms) , CN/C=[ 77] , IA=[ 4.67](mm) ,
2335 *          N=[ 3] , TP=[ 1.10]hrs ,
2336 *          Continuous simulation parameters:
2337 *          IaRECper=[ 4](hrs) ,
2338 *          SMN=[ -1](mm) , SMAX=[ -1](mm) , SK=[ 0.010]/(mm) ,
2339 *          InterEventTime=[ 12](hrs)
2340 *          Baseflow simulation parameters:
2341 *          BaseFlowOption=[ 1] ,
2342 *          InitGWResVol =[ 50](mm) , GWResK=[ 0.96](mm/day/mm)
2343 *          VHydCond=[ 0.055](mm/hr) ,    END=- 1
2344 *%-----|-----
2345 * -JFSA 2021-02-25 "S-1-Okeefe" is a part of S-1 sub-catchment. It is moved to drain
      before station 7245 on Jock River
2346 *CONTINUOUS STANDHYD NHYD=["S-1-Okeefe"], DT=[ 1](min) , AREA=[ 44.93](ha) , XI MP=[ 0.65] ,
      TI MP=[ 0.65] , DWF=[ 0](cms) ,
2347 *          LOSS=[ 2] , SCS curve number CN=[ 75] , Pervious surfaces:
      IAper=[ 4.67](mm) , SLPP=[ 2.0](%) ,
2348 *          LGP=[ 40](m) , MNP=[ 0.25] , SCP=[ 0](min) , Impervious surfaces:
      IAimp=[ 1.57](mm) , SLPI=[ 0.75](%) ,
2349 *          LGI=[ 547.296](m) , MNI=[ 0.013] , SCI=[ 0](min) ,
2350 *          Continuous simulation parameters:
2351 *          IaRECper=[ 4](hrs) , IaRECimp=[ 4](hrs) ,
2352 *          SMN=[ -1](mm) , SMAX=[ -1](mm) , SK=[ 0.010]/(mm) ,
2353 *          InterEventTime=[ 12](hrs) ,    END=- 1
2354 *%-----|-----
2355 *COMPUTE DUALHYD  NHYDin=["S-1-Okeefe"], CINLET=[ 4.796](cms) , NINLET=[ 1] ,
2356 *          MajNHYD=["S-1-OkM"]
2357 *          MnNHYD=["S-1-OkMN"]
2358 *          TMS TO=[ 9999999](cu-m)
2359 *%-----|-----
2360 *ADD HYD          NHYDs um=["S-1-OkS"] , NHYDs to add=["S-1-OkM"+"S-1-OkMN"]
2361 *%-----|-----

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2362 *ROUTE RESERVOIR      NHYDout=[ "S-1-OkSR" ] , NHYDin=[ "S-1-OkS" ] ,
2363 *                      RDT=[ 1 ] (mi n),
2364 *                      TABLE of ( OUTFLOW STORAGE ) values
2365 *                      ( cms ) - ( ha-m)
2366 *                      [ 0.0      , 0.0 ]
2367 *                      [ 0.5370, 1.7917 ]
2368 *                      [ -1      , -1      ] (max twenty pts)
2369 *                      NHYDovf=[ "S-1-OkSovf" ]
2370 *%-----|-----
2371 *CONTINUOUS NASHYD     NHYD=[ "S-1-Okeefe" ], DT=[ 1 ] mi n, AREA=[ 44.93 ] (ha),
2372 *                      DWF=[ 0 ] (cms), CN C=[ 77 ], IA=[ 4.67 ] (mm),
2373 *                      N=[ 3 ], TP=[ 1.049 ] hrs,
2374 *                      Continuous simulation parameters:
2375 *                      IaRECper=[ 4 ] (hrs),
2376 *                      SMN=[ -1 ] (mm), SMAX=[ -1 ] (mm), SK=[ 0.010 ] / (mm),
2377 *                      InterEventTime=[ 12 ] (hrs)
2378 *                      Baseflow simulation parameters:
2379 *                      BaseFlowOption=[ 1 ] ,
2380 *                      InitGWResVol=[ 50 ] (mm), GWResK=[ 0.96 ] (mm/ day/ mm)
2381 *                      VHydCond=[ 0.055 ] (mm/ hr), END=- 1
2382 *%-----|-----
2383 * -JFSA 2021-02-26 "S-1-FO-DI" is a part of S-1 sub-catchment. It is moved to drain
before station 520 on Foster Drain
2384 *CONTINUOUS STANDHYD NHYD=[ "S-1-FO-DI" ], DT=[ 1 ] mi n, AREA=[ 5.11 ] (ha),
2385 *                      XI MP=[ 0.65 ], TI MP=[ 0.65 ], DWF=[ 0 ] (cms), LOSS=[ 2 ],
2386 *                      SCS curve number CN=[ 74 ],
2387 *                      Pervious surfaces: IAper=[ 4.67 ] (mm), SLPP=[ 0.5 ] ( % ),
2388 *                      LGP=[ 40 ] (m), MNP=[ 0.25 ], SCP=[ 0 ] (mi n),
2389 *                      Impervious surfaces: IAimp=[ 1.57 ] (mm), SLPI=[ 0.5 ] ( % ),
2390 *                      LGI=[ 184.572 ] (m), MNI=[ 0.013 ], SCI=[ 0 ] (mi n),
2391 *                      Continuous simulation parameters:
2392 *                      IaRECper=[ 4 ] (hrs), IaRECImp=[ 4 ] (hrs),
2393 *                      SMN=[ -1 ] (mm), SMAX=[ -1 ] (mm), SK=[ 0.010 ] / (mm),
2394 *                      InterEventTime=[ 18 ] (hrs), END=- 1
2395 *%-----|-----
2396 *COMPUTE DUALHYD      NHYDin=[ "S-1-FO-DI" ], CINLET=[ 0.605 ] (cms), NINLET=[ 1 ],
2397 *                      MajNHYD=[ "S-1-FO-DIJ" ]
2398 *                      MnNHYD=[ "S-1-FO-DIN" ]
2399 *                      TMSTO=[ 9999999 ] (cu-m)
2400 *%-----|-----
2401 *ADD HYD               NHYDsum=[ "S-1-FO-DIS" ], NHYDsto add=[ "S-1-FO-DIN"+"S-1-FO-DIJ" ]
2402 *%-----|-----
2403 *ROUTE RESERVOIR      NHYDout=[ "S-1-FO-DIR" ] , NHYDin=[ "S-1-FO-DIS" ] ,
2404 *                      RDT=[ 1 ] (mi n),
2405 *                      TABLE of ( OUTFLOW STORAGE ) values
2406 *                      ( cms ) - ( ha-m)
2407 *                      [ 0.0      , 0.0 ]
2408 *                      [ 0.0611, 0.2038 ]
2409 *                      [ -1      , -1      ] (max twenty pts)
2410 *                      NHYDovf=[ "S-1FODlovf" ]
2411 *%-----|-----
2412 *CONTINUOUS NASHYD     NHYD=[ "S-1-FO-DI" ], DT=[ 1 ] mi n, AREA=[ 5.11 ] (ha),
2413 *                      DWF=[ 0 ] (cms), CN C=[ 77 ], IA=[ 4.67 ] (mm),
2414 *                      N=[ 3 ], TP=[ 1.10 ] hrs,
2415 *                      Continuous simulation parameters:
2416 *                      IaRECper=[ 4 ] (hrs),
2417 *                      SMN=[ -1 ] (mm), SMAX=[ -1 ] (mm), SK=[ 0.010 ] / (mm),
2418 *                      InterEventTime=[ 12 ] (hrs)
2419 *                      Baseflow simulation parameters:
2420 *                      BaseFlowOption=[ 1 ] ,
2421 *                      InitGWResVol=[ 50 ] (mm), GWResK=[ 0.96 ] (mm/ day/ mm)
2422 *                      VHydCond=[ 0.055 ] (mm/ hr), END=- 1
2423 *%-----|-----
2424 * -JFSA 2021-02-26 "S-1-FO-D2" is a part of S-1 sub-catchment. It is moved to drain
before station 980 on Foster Drain
2425 *CONTINUOUS STANDHYD NHYD=[ "S-1-FO-D2" ], DT=[ 1 ] mi n, AREA=[ 4.94 ] (ha),

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2426 * XI MP=[ 0.55], TI MP=[ 0.55], DWF=[ 0](cms), LOSS=[ 2],
2427 * SCS curve number CN=[ 74],
2428 * Previous surfaces: I A per =[ 4.67](mm), SLPP=[ 0.5](%),
2429 * LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
2430 * Impervious surfaces: I A i mp=[ 1.57](mm), SLPI =[ 0.5](%),
2431 * LGI =[ 181.475](m), MNI =[ 0.013], SCI =[ 0](min),
2432 * Continuous simulation parameters:
2433 * I a REC per =[ 4](hrs), I a REC i mp=[ 4](hrs),
2434 * SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2435 * Inter Event Ti me =[ 18](hrs), END=- 1
2436 *%-----|-----
2437 *CONTINUOUS NASHYD NHYD=[ "S-1-FO-D2"], DT=[ 1]mi n, AREA=[ 4.94](ha),
2438 * DWF=[ 0](cms), CN C=[ 77], I A=[ 4.67](mm),
2439 * N=[ 3], TP=[ 1.10]hrs,
2440 * Continuous simulation parameters:
2441 * I a REC per =[ 4](hrs),
2442 * SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2443 * Inter Event Ti me =[ 12](hrs)
2444 * Baseflow simulation parameters:
2445 * BaseFlowOpt ion=[ 1],
2446 * I ni t GWRes Vol =[ 50](mm), GWRes K=[ 0.96](mm/day/mm)
2447 * VHydCond=[ 0.055](mm/hr), END=- 1
2448 *%-----|-----
2449 *COMPUTE DUALHYD NHYD i n=[ "S-1-FO-D2"], CI NLET=[ 0.508](cms), NI NLET=[ 1],
2450 * M a j NHYD=[ "S-1-FO-D2J"]
2451 * M nNHYD=[ "S-1-FO-D2N"]
2452 * TM I STO=[ 9999999](cu-m)
2453 *%-----|-----
2454 *ADD HYD NHYD s um=[ "S-1-FO-D2S"], NHYD s t o a dd=[ "S-1-FO-D2J"+"S-1-FO-D2N"]
2455 *%-----|-----
2456 *ROUTE RESERVOIR NHYD out =[ "S-1-FO-D2R"], NHYD i n=[ "S-1-FO-D2S"],
2457 * RDT=[ 1](mi n),
2458 * TABLE of ( OUTFLOW STORAGE ) values
2459 * (cms) - (ha-m)
2460 * [ 0.0 , 0.0 ]
2461 * [ 0.0590, 0.1970 ]
2462 * [ -1 , -1 ] (max twenty pts)
2463 * NHYD o vf=[ "S-1FOD2ovf"]
2464 *%-----|-----
2465 * -JFSA 2021-02-26 "S-1-FO-F-D" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2466 *CONTINUOUS STANDHYD NHYD=[ "S-1-FO-F-D"], DT=[ 1]mi n, AREA=[ 14.96](ha),
2467 * XI MP=[ 0.65], TI MP=[ 0.65], DWF=[ 0](cms), LOSS=[ 2],
2468 * SCS curve number CN=[ 74],
2469 * Previous surfaces: I A per =[ 4.67](mm), SLPP=[ 0.5](%),
2470 * LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
2471 * Impervious surfaces: I A i mp=[ 1.57](mm), SLPI =[ 0.5](%),
2472 * LGI =[ 315.806](m), MNI =[ 0.013], SCI =[ 0](min),
2473 * Continuous simulation parameters:
2474 * I a REC per =[ 4](hrs), I a REC i mp=[ 4](hrs),
2475 * SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2476 * Inter Event Ti me =[ 18](hrs), END=- 1
2477 *%-----|-----
2478 *CONTINUOUS NASHYD NHYD=[ "S-1-FO-F-D"], DT=[ 1]mi n, AREA=[ 14.96](ha),
2479 * DWF=[ 0](cms), CN C=[ 77], I A=[ 4.67](mm),
2480 * N=[ 3], TP=[ 1.007]hrs,
2481 * Continuous simulation parameters:
2482 * I a REC per =[ 4](hrs),
2483 * SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2484 * Inter Event Ti me =[ 12](hrs)
2485 * Baseflow simulation parameters:
2486 * BaseFlowOpt ion=[ 1],
2487 * I ni t GWRes Vol =[ 50](mm), GWRes K=[ 0.96](mm/day/mm)
2488 * VHydCond=[ 0.055](mm/hr), END=- 1
2489 *%-----|-----
2490 *COMPUTE DUALHYD NHYD i n=[ "S-1-FO-F-D"], CI NLET=[ 1.749](cms), NI NLET=[ 1],

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2491 *           Mj NHYD=[ "S- 1FO- F- DJ" ]
2492 *           MnNHYD=[ "S- 1FO- F- DN" ]
2493 *           TMJ STO=[ 9999999 ] ( cu- m)
2494 *%-----|-----|
2495 *ADD HYD           NHYDs um=[ "S- 1FO- F- DS" ], NHYDs to add=[ "S- 1FO- F- DJ"+"S- 1FO- F- DN" ]
2496 *%-----|-----|
2497 *ROUTE RESERVOIR  NHYDout=[ "S- 1FO- F- DR" ] , NHYDin=[ "S- 1FO- F- DS" ] ,
2498 *           RDT=[ 1 ] ( mi n),
2499 *           TABLE of ( OUTFLOW STORAGE ) values
2500 *                   ( cms ) - ( ha- m)
2501 *                   [ 0.0      , 0.0 ]
2502 *                   [ 0.1788, 0.5966 ]
2503 *                   [   -1   ,  -1   ] (max twenty pts)
2504 *           NHYDovf=[ "S- 1FoFDovf" ]
2505 *%-----|-----|
2506 *CONTINUOUS STANDHYD NHYD=[ "S- 1- D1" ], DT=[ 1 ] ( mi n), AREA=[ 21.67 ] ( ha), XI MP=[ 0.65 ],
TI MP=[ 0.65 ], DWF=[ 0 ] ( cms),
2507 *           LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
I Aper=[ 4.67 ] ( mm), SLPP=[ 2.0 ] ( %),
2508 *           LGP=[ 40 ] ( m), MNP=[ 0.25 ], SCP=[ 0 ] ( mi n), Impervious surfaces:
I Ai mp=[ 1.57 ] ( mm), SLPI=[ 0.75 ] ( %),
2509 *           LGI=[ 380.088 ] ( m), MNI=[ 0.013 ], SCI=[ 0 ] ( mi n),
2510 *           Continuous simulation parameters:
2511 *           IaRECper=[ 4 ] ( hr s), IaRECI mp=[ 4 ] ( hr s),
2512 *           SMN=[ -1 ] ( mm), SMAX=[ -1 ] ( mm), SK=[ 0.010 ] / ( mm),
2513 *           InterEvent Time=[ 12 ] ( hr s), END=- 1
2514 *%-----|-----|
2515 *CONTINUOUS NASHYD  NHYD=[ "S- 1- D1" ], DT=[ 1 ] mi n, AREA=[ 21.67 ] ( ha),
2516 *           DWF=[ 0 ] ( cms), CN C=[ 77 ], IA=[ 4.67 ] ( mm),
2517 *           N=[ 3 ], TP=[ 1.066 ] hr s,
2518 *           Continuous simulation parameters:
2519 *           IaRECper=[ 4 ] ( hr s),
2520 *           SMN=[ -1 ] ( mm), SMAX=[ -1 ] ( mm), SK=[ 0.010 ] / ( mm),
2521 *           InterEvent Time=[ 12 ] ( hr s)
2522 *           Baseflow simulation parameters:
2523 *           BaseFlowOption=[ 1 ] ,
2524 *           InitGWRes Vol=[ 50 ] ( mm), GWRes K=[ 0.96 ] ( mm/ day/ mm)
2525 *           VHydCond=[ 0.055 ] ( mm/ hr), END=- 1
2526 *%-----|-----|
2527 *COMPUTE DUALHYD   NHYDin=[ "S- 1- D1" ], CINLET=[ 2.482 ] ( cms), NI NLET=[ 1 ],
2528 *           Mj NHYD=[ "S- 1- DIJ" ]
2529 *           MnNHYD=[ "S- 1- DIN" ]
2530 *           TMJ STO=[ 9999999 ] ( cu- m)
2531 *%-----|-----|
2532 *ADD HYD           NHYDs um=[ "S- 1- DIS" ], NHYDs to add=[ "S- 1- DIJ"+"S- 1- DIN" ]
2533 *%-----|-----|
2534 *ROUTE RESERVOIR  NHYDout=[ "S- 1- DIR" ] , NHYDin=[ "S- 1- DIS" ] ,
2535 *           RDT=[ 1 ] ( mi n),
2536 *           TABLE of ( OUTFLOW STORAGE ) values
2537 *                   ( cms ) - ( ha- m)
2538 *                   [ 0.0      , 0.0 ]
2539 *                   [ 0.2590, 0.8642 ]
2540 *                   [   -1   ,  -1   ] (max twenty pts)
2541 *           NHYDovf=[ "S- 1- DIRovf" ]
2542 *%-----|-----|
2543 * -JFSA 2021-02-25 "S- 1- D2" and "S- 1- D3" are part of S- 1 sub-catchment. They are
moved to drain before station 6215 on Jock River
2544 *CONTINUOUS STANDHYD NHYD=[ "S- 1- D2" ], DT=[ 1 ] ( mi n), AREA=[ 18.67 ] ( ha), XI MP=[ 0.65 ],
TI MP=[ 0.65 ], DWF=[ 0 ] ( cms),
2545 *           LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
I Aper=[ 4.67 ] ( mm), SLPP=[ 2.0 ] ( %),
2546 *           LGP=[ 40 ] ( m), MNP=[ 0.25 ], SCP=[ 0 ] ( mi n), Impervious surfaces:
I Ai mp=[ 1.57 ] ( mm), SLPI=[ 0.75 ] ( %),
2547 *           LGI=[ 352.798 ] ( m), MNI=[ 0.013 ], SCI=[ 0 ] ( mi n),
2548 *           Continuous simulation parameters:
2549 *           IaRECper=[ 4 ] ( hr s), IaRECI mp=[ 4 ] ( hr s),

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2550 * SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2551 * InterEventTime=[12](hrs), END=-1
2552 *%-----|-----
2553 *CONTINUOUS NASHYD NHYD=["S-1-D2"], DT=[1]min, AREA=[18.67](ha),
2554 * DWF=[0](cms), CNVC=[77], IA=[4.67](mm),
2555 * N=[3], TP=[1.120]hrs,
2556 * Continuous simulation parameters:
2557 * IaRECper=[4](hrs),
2558 * SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2559 * InterEventTime=[12](hrs)
2560 * Baseflow simulation parameters:
2561 * BaseFlowOption=[1],
2562 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2563 * VHydCond=[0.055](mm/hr), END=-1
2564 *%-----|-----
2565 *COMPUTE DUALHYD NHYDin=["S-1-D2"], CINLET=[2.062](cms), NINLET=[1],
2566 * MajNHYD=["S-1-D2J"]
2567 * MnNHYD=["S-1-D2N"]
2568 * TMSSTO=[9999999](cu-m)
2569 *%-----|-----
2570 *ADD HYD NHYDsum=["S-1-D2S"], NHYDsto add=["S-1-D2J"+"S-1-D2N"]
2571 *%-----|-----
2572 *ROUTE RESERVOIR NHYDout=["S-1-D2R"], NHYDin=["S-1-D2S"],
2573 * RDT=[1](min),
2574 * TABLE of ( OUTFLOW STORAGE ) values
2575 * (cms) - (ha-m)
2576 * [ 0.0 , 0.0 ]
2577 * [ 0.2231, 0.7445 ]
2578 * [ -1 , -1 ] (max twenty pts)
2579 * NHYDovf=["S-1-D2Rovf"]
2580 *%-----|-----
2581 *CONTINUOUS STANDHYD NHYD=["S-1-D3"], DT=[1](min), AREA=[6.79](ha), XIIMP=[0.65],
TIIMP=[0.65], DWF=[0](cms),
2582 * LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
IAPER=[4.67](mm), SLPP=[2.0](%),
2583 * LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
IAimp=[1.57](mm), SLPI=[0.75](%),
2584 * LGI=[212.760](m), MNI=[0.013], SCI=[0](min),
2585 * Continuous simulation parameters:
2586 * IaRECper=[4](hrs), IaRECimp=[4](hrs),
2587 * SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2588 * InterEventTime=[12](hrs), END=-1
2589 *%-----|-----
2590 *CONTINUOUS NASHYD NHYD=["S-1-D3"], DT=[1]min, AREA=[6.79](ha),
2591 * DWF=[0](cms), CNVC=[77], IA=[4.67](mm),
2592 * N=[3], TP=[1.281]hrs,
2593 * Continuous simulation parameters:
2594 * IaRECper=[4](hrs),
2595 * SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2596 * InterEventTime=[12](hrs)
2597 * Baseflow simulation parameters:
2598 * BaseFlowOption=[1],
2599 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2600 * VHydCond=[0.055](mm/hr), END=-1
2601 *%-----|-----
2602 *COMPUTE DUALHYD NHYDin=["S-1-D3"], CINLET=[0.719](cms), NINLET=[1],
2603 * MajNHYD=["S-1-D3J"]
2604 * MnNHYD=["S-1-D3N"]
2605 * TMSSTO=[9999999](cu-m)
2606 *%-----|-----
2607 *ADD HYD NHYDsum=["S-1-D3S"], NHYDsto add=["S-1-D3J"+"S-1-D3N"]
2608 *%-----|-----
2609 *ROUTE RESERVOIR NHYDout=["S-1-D3R"], NHYDin=["S-1-D3S"],
2610 * RDT=[1](min),
2611 * TABLE of ( OUTFLOW STORAGE ) values
2612 * (cms) - (ha-m)

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2613 * [ 0.0 , 0.0 ]
2614 * [ 0.0811, 0.2708 ]
2615 * [ -1 , -1 ] (max twenty pts)
2616 * NHYDovf=[ "S-1-D3Rovf" ]
2617 *%-----|-----
2618 CONTINUOUS STANDHYD NHYD=[ "S-1-D4" ], DT=[ 1 ](mi n), AREA=[ 3.28 ](ha), XI MP=[ 0.65 ],
TI MP=[ 0.65 ], DWF=[ 0 ](cms),
2619 LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
I Aper=[ 4.67 ](mm), SLPP=[ 2.0 ]( % ),
2620 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](mi n), Impervious surfaces:
I Ai mp=[ 1.57 ](mm), SLPI=[ 0.75 ]( % ),
2621 LGI=[ 147.874 ](m), MNI=[ 0.013 ], SCI=[ 0 ](mi n),
2622 Continuous simulation parameters:
I aRECper=[ 4 ](hrs), I aRECI mp=[ 4 ](hrs),
2623 SM N=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2624 SM N=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2625 InterEventTime=[ 12 ](hrs), END=- 1
2626 *%-----|-----
2627 *CONTINUOUS NASHYD NHYD=[ "S-1-D4" ], DT=[ 1 ]mi n, AREA=[ 3.28 ](ha),
2628 * DWF=[ 0 ](cms), CN C=[ 77 ], I A=[ 4.67 ](mm),
2629 * N=[ 3 ], TP=[ 1.10 ]hrs,
2630 * Continuous simulation parameters:
2631 * I aRECper=[ 4 ](hrs),
2632 * SM N=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2633 * InterEventTime=[ 12 ](hrs)
2634 * Baseflow simulation parameters:
2635 * BaseFlowOption=[ 1 ],
2636 * I nitGWResVol=[ 50 ](mm), GWResK=[ 0.96 ](mm/day/mm)
2637 * VHydCond=[ 0.055 ](mm/hr), END=- 1
2638 *%-----|-----
2639 *COMPUTE DUALHYD NHYDi n=[ "S-1-D4" ], CI NLET=[ 0.373 ](cms), NI NLET=[ 1 ],
2640 * Mi j NHYD=[ "S-1-D4J" ]
2641 * M nNHYD=[ "S-1-D4N" ]
2642 * TM I STO=[ 9999999 ](cu-m)
2643 *%-----|-----
2644 *ADD HYD NHYDs um=[ "S-1-D4S" ], NHYDs to add=[ "S-1-D4J"+"S-1-D4N" ]
2645 *%-----|-----
2646 *ROUTE RESERVOIR NHYDout=[ "S-1-D4R" ], NHYDi n=[ "S-1-D4S" ],
2647 * RDT=[ 1 ](mi n),
2648 * TABLE of ( OUTFLOW STORAGE ) values
2649 * (cms) - (ha-m)
2650 * [ 0.0 , 0.0 ]
2651 * [ 0.0392, 0.1308 ]
2652 * [ -1 , -1 ] (max twenty pts)
2653 * NHYDovf=[ "S-1-D4Rovf" ]
2654 *%-----|-----
2655 CONTINUOUS STANDHYD NHYD=[ "S-1-D5" ], DT=[ 1 ](mi n), AREA=[ 12.84 ](ha), XI MP=[ 0.65 ],
TI MP=[ 0.65 ], DWF=[ 0 ](cms),
2656 LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
I Aper=[ 4.67 ](mm), SLPP=[ 2.0 ]( % ),
2657 LGP=[ 40 ](m), MNP=[ 0.25 ], SCP=[ 0 ](mi n), Impervious surfaces:
I Ai mp=[ 1.57 ](mm), SLPI=[ 0.75 ]( % ),
2658 LGI=[ 292.57 ](m), MNI=[ 0.013 ], SCI=[ 0 ](mi n),
2659 Continuous simulation parameters:
I aRECper=[ 4 ](hrs), I aRECI mp=[ 4 ](hrs),
2660 SM N=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2661 SM N=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2662 InterEventTime=[ 12 ](hrs), END=- 1
2663 *%-----|-----
2664 *CONTINUOUS NASHYD NHYD=[ "S-1-D5" ], DT=[ 1 ]mi n, AREA=[ 12.84 ](ha),
2665 * DWF=[ 0 ](cms), CN C=[ 77 ], I A=[ 4.67 ](mm),
2666 * N=[ 3 ], TP=[ 1.10 ]hrs,
2667 * Continuous simulation parameters:
2668 * I aRECper=[ 4 ](hrs),
2669 * SM N=[ -1 ](mm), SMAX=[ -1 ](mm), SK=[ 0.010 ]/(mm),
2670 * InterEventTime=[ 12 ](hrs)
2671 * Baseflow simulation parameters:
2672 * BaseFlowOption=[ 1 ],

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2673 *          I n i t G W R e s V o l =[ 50 ] ( m m ) ,   G W R e s K =[ 0. 96 ] ( m m / d a y / m m )
2674 *          V H y d C o n d =[ 0. 055 ] ( m m / h r ) ,   E N D = - 1
2675 *%-----|-----
2676 *COMPUTE DUALHYD  N H Y D i n =[ " S - 1 - D 5 " ] ,   C I N L E T =[ 1. 395 ] ( c m s ) ,   N I N L E T =[ 1 ] ,
2677 *          M a j N H Y D =[ " S - 1 - D 5 J " ]
2678 *          M n N H Y D =[ " S - 1 - D 5 N " ]
2679 *          T M I S T O =[ 9999999 ] ( c u - m )
2680 *%-----|-----
2681 *ADD HYD          N H Y D s u m =[ " S - 1 - D 5 S " ] ,   N H Y D s t o a d d =[ " S - 1 - D 5 J " + " S - 1 - D 5 N " ]
2682 *%-----|-----
2683 *ROUTE RESERVOIR N H Y D o u t =[ " S - 1 - D 5 R " ] ,   N H Y D i n =[ " S - 1 - D 5 S " ] ,
2684 *          R D T =[ 1 ] ( m i n ) ,
2685 *          T A B L E o f ( O U T F L O W S T O R A G E ) v a l u e s
2686 *          ( c m s ) - ( h a - m )
2687 *          [ 0. 0      , 0. 0 ]
2688 *          [ 0. 1535, 0. 5120 ]
2689 *          [ - 1      , - 1      ] ( m a x t w e n t y p t s )
2690 *          N H Y D o v f =[ " S - 1 - D 5 R o v f " ]
2691 *%-----|-----
2692 CONTINUOUS STANDHYD N H Y D =[ " S - 1 - D 6 " ] ,   D T =[ 1 ] ( m i n ) ,   A R E A =[ 1. 75 ] ( h a ) ,   X I M P =[ 0. 65 ] ,
T I M P =[ 0. 65 ] ,   D W F =[ 0 ] ( c m s ) ,
2693 LOSS =[ 2 ] ,   S C S c u r v e n u m b e r C N =[ 75 ] ,   P e r v i o u s s u r f a c e s :
I A p e r =[ 4. 67 ] ( m m ) ,   S L P P =[ 2. 0 ] ( % ) ,
2694 L G P =[ 40 ] ( m ) ,   M N P =[ 0. 25 ] ,   S C P =[ 0 ] ( m i n ) ,   I m p e r v i o u s s u r f a c e s :
I A i m p =[ 1. 57 ] ( m m ) ,   S L P I =[ 0. 75 ] ( % ) ,
2695 L G I =[ 108. 01 ] ( m ) ,   M N I =[ 0. 013 ] ,   S C I =[ 0 ] ( m i n ) ,
2696 C o n t i n u o u s s i m u l a t i o n p a r a m e t e r s :
2697 I a R E C p e r =[ 4 ] ( h r s ) ,   I a R E C i m p =[ 4 ] ( h r s ) ,
2698 S M N =[ - 1 ] ( m m ) ,   S M A X =[ - 1 ] ( m m ) ,   S K =[ 0. 010 ] / ( m m ) ,
2699 I n t e r E v e n t T i m e =[ 12 ] ( h r s ) ,   E N D = - 1
2700 *%-----|-----
2701 *CONTINUOUS NASHYD  N H Y D =[ " S - 1 - D 6 " ] ,   D T =[ 1 ] m i n ,   A R E A =[ 1. 75 ] ( h a ) ,
2702 *          D W F =[ 0 ] ( c m s ) ,   C N C =[ 77 ] ,   I A =[ 4. 67 ] ( m m ) ,
2703 *          N =[ 3 ] ,   T P =[ 1. 10 ] h r s ,
2704 *          C o n t i n u o u s s i m u l a t i o n p a r a m e t e r s :
2705 *          I a R E C p e r =[ 4 ] ( h r s ) ,
2706 *          S M N =[ - 1 ] ( m m ) ,   S M A X =[ - 1 ] ( m m ) ,   S K =[ 0. 010 ] / ( m m ) ,
2707 *          I n t e r E v e n t T i m e =[ 12 ] ( h r s )
2708 *          B a s e f l o w s i m u l a t i o n p a r a m e t e r s :
2709 *          B a s e F l o w O p t i o n =[ 1 ] ,
2710 *          I n i t G W R e s V o l =[ 50 ] ( m m ) ,   G W R e s K =[ 0. 96 ] ( m m / d a y / m m )
2711 *          V H y d C o n d =[ 0. 055 ] ( m m / h r ) ,   E N D = - 1
2712 *%-----|-----
2713 *COMPUTE DUALHYD  N H Y D i n =[ " S - 1 - D 6 " ] ,   C I N L E T =[ 0. 218 ] ( c m s ) ,   N I N L E T =[ 1 ] ,
2714 *          M a j N H Y D =[ " S - 1 - D 6 J " ]
2715 *          M n N H Y D =[ " S - 1 - D 6 N " ]
2716 *          T M I S T O =[ 9999999 ] ( c u - m )
2717 *%-----|-----
2718 *ADD HYD          N H Y D s u m =[ " S - 1 - D 6 S " ] ,   N H Y D s t o a d d =[ " S - 1 - D 6 J " + " S - 1 - D 6 N " ]
2719 *%-----|-----
2720 *ROUTE RESERVOIR N H Y D o u t =[ " S - 1 - D 6 R " ] ,   N H Y D i n =[ " S - 1 - D 6 S " ] ,
2721 *          R D T =[ 1 ] ( m i n ) ,
2722 *          T A B L E o f ( O U T F L O W S T O R A G E ) v a l u e s
2723 *          ( c m s ) - ( h a - m )
2724 *          [ 0. 0      , 0. 0 ]
2725 *          [ 0. 0209, 0. 0698 ]
2726 *          [ - 1      , - 1      ] ( m a x t w e n t y p t s )
2727 *          N H Y D o v f =[ " S - 1 - D 6 R o v f " ]
2728 *%-----|-----
2729 CONTINUOUS STANDHYD N H Y D =[ " S - 1 - D 7 " ] ,   D T =[ 1 ] ( m i n ) ,   A R E A =[ 2. 03 ] ( h a ) ,   X I M P =[ 0. 65 ] ,
T I M P =[ 0. 65 ] ,   D W F =[ 0 ] ( c m s ) ,
2730 LOSS =[ 2 ] ,   S C S c u r v e n u m b e r C N =[ 75 ] ,   P e r v i o u s s u r f a c e s :
I A p e r =[ 4. 67 ] ( m m ) ,   S L P P =[ 2. 0 ] ( % ) ,
2731 L G P =[ 40 ] ( m ) ,   M N P =[ 0. 25 ] ,   S C P =[ 0 ] ( m i n ) ,   I m p e r v i o u s s u r f a c e s :
I A i m p =[ 1. 57 ] ( m m ) ,   S L P I =[ 0. 75 ] ( % ) ,
2732 L G I =[ 116. 33 ] ( m ) ,   M N I =[ 0. 013 ] ,   S C I =[ 0 ] ( m i n ) ,

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2733 Continuous simulation parameters:
2734 IaRECper=[ 4](hr s), IaRECImp=[ 4](hr s),
2735 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2736 InterEventTime=[ 12](hr s), END=- 1
2737 *%-----|-----
2738 *CONTINUOUS NASHYD NHYD=["S-1-D7"], DT=[ 1]min, AREA=[ 2.03](ha),
2739 * DWF=[ 0](cms), CN C=[ 77], IA=[ 4.67](mm),
2740 * N=[ 3], TP=[ 1.10]hr s,
2741 * Continuous simulation parameters:
2742 * IaRECper=[ 4](hr s),
2743 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2744 * InterEventTime=[ 12](hr s)
2745 * Baseflow simulation parameters:
2746 * BaseFlowOption=[ 1],
2747 * InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
2748 * VHydCond=[ 0.055](mm/hr), END=- 1
2749 *%-----|-----
2750 *COMPUTE DUALHYD NHYDin=["S-1-D7"], CINLET=[ 2.279](cms), NINLET=[ 1],
2751 * MjNHYD=["S-1-D7J"]
2752 * MnNHYD=["S-1-D7N"]
2753 * TMS TO=[ 9999999](cu-m)
2754 *%-----|-----
2755 *ADD HYD NHYDsum=["S-1-D7S"], NHYDs to add=["S-1-D7J"+"S-1-D7N"]
2756 *%-----|-----
2757 *ROUTE RESERVOIR NHYDout=["S-1-D7R"], NHYDin=["S-1-D7S"],
2758 * RDT=[ 1](min),
2759 * TABLE of ( OUTFLOW STORAGE ) values
2760 * (cms) - (ha-m)
2761 * [ 0.0, 0.0 ]
2762 * [ 0.0243, 0.0810 ]
2763 * [ -1, -1 ] (max twenty pts)
2764 * NHYDovf=["S-1-D8Rovf"]
2765 *%-----|-----
2766 * -JFSA 2021-02-26 "S-1-D8" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2767 *CONTINUOUS STANDHYD NHYD=["S-1-D8"], DT=[ 1](min), AREA=[ 5.27](ha), XI MP=[ 0.65],
TI MP=[ 0.65], DWF=[ 0](cms),
2768 * LOSS=[ 2], SCS curve number CN=[ 75], Pervious surfaces:
I Aper=[ 4.67](mm), SLPP=[ 2.0](%),
2769 * LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min), Impervious surfaces:
I Ai mp=[ 1.57](mm), SLPI=[ 0.75](%),
2770 * LGI=[ 187.439](m), MNI=[ 0.013], SCI=[ 0](min),
2771 * Continuous simulation parameters:
2772 * IaRECper=[ 4](hr s), IaRECImp=[ 4](hr s),
2773 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2774 * InterEventTime=[ 12](hr s), END=- 1
2775 *%-----|-----
2776 *CONTINUOUS NASHYD NHYD=["S-1-D8"], DT=[ 1]min, AREA=[ 5.27](ha),
2777 * DWF=[ 0](cms), CN C=[ 77], IA=[ 4.67](mm),
2778 * N=[ 3], TP=[ 1.10]hr s,
2779 * Continuous simulation parameters:
2780 * IaRECper=[ 4](hr s),
2781 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2782 * InterEventTime=[ 12](hr s)
2783 * Baseflow simulation parameters:
2784 * BaseFlowOption=[ 1],
2785 * InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
2786 * VHydCond=[ 0.055](mm/hr), END=- 1
2787 *%-----|-----
2788 *COMPUTE DUALHYD NHYDin=["S-1-D8"], CINLET=[ 2.279](cms), NINLET=[ 1],
2789 * MjNHYD=["S-1-D8J"]
2790 * MnNHYD=["S-1-D8N"]
2791 * TMS TO=[ 9999999](cu-m)
2792 *%-----|-----
2793 *ADD HYD NHYDsum=["S-1-D8S"], NHYDs to add=["S-1-D8J"+"S-1-D8N"]
2794 *%-----|-----

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2795 *ADD HYD NHYDs um=[ "S- 1- D" ], NHYDs to add=[ "S- 1- Okeefe"+"S- 1"+"S- 1- Fost" ]
2796 *%-----|-----|
2797 *COMPUTE DUALHYD NHYDi n=[ "S- 1- D" ], CI NLET=[ 11. 616 ] (cms), NI NLET=[ 1 ],
2798 * M j NHYD=[ "S- 1- D- M" ]
2799 * M nNHYD=[ "S- 1- D- MN" ]
2800 * T M STO=[ 5974 ] (cu- m)
2801 *%-----|-----|
2802 *ADD HYD NHYDs um=[ "S- 1- DEV" ], NHYDs to add=[ "S- 1- D- M"+"S- 1- D- MN" ]
2803 *%-----|-----|
2804 *ROUTE RESERVOIR NHYDout=[ "S- 1- D&R" ] , NHYDi n=[ "S- 1- D&S" ] ,
2805 * RDT=[ 1 ] (mi n),
2806 * TABLE of ( OUTFLOW STORAGE ) values
2807 * (cms) - (ha- m)
2808 * [ 0. 0 , 0. 0 ]
2809 * [ 0. 0630, 0. 2102 ]
2810 * [ -1 , -1 ] (max twenty pts)
2811 * NHYDovf=[ "S- 1- D&Rovf" ]
2812 *%-----|-----|
2813 *%-----|-----|
2814 * - JFSA 2021-02-08 Clarke (MS_P2 and P2-OVF) and Clarke Undeveloped area
(W_CLAR_UNDE) drain to Jock River at Station 5002 instead of Station 4534
2815 *# Catchment W_CLAR
2816 *# - To West Clarke Drain (south of the Jock)
2817 *# - Subdivision with 43% imp. as per Barrhaven South MS
2818 *# - 2020-11-30 update CLARKE Tributary Drainage Area to = 121 ha based on
P598(04)-11
2819 *# - 2020-11-30 split CLARKE Drainage Area to MAJOR and ALL
2820 *#*****
2821 CONTINUOUS STANDHYD NHYD=[ "W_CLAR_M" ], DT=[ 1 ] mi n, AREA=[ 1. 772 ] (ha),
2822 XI MP=[ 0. 46 ], TI MP=[ 0. 59 ], DWF=[ 0 ] (cms), LOSS=[ 2 ],
2823 SCS curve number CN=[ 77 ],
2824 Pervious surfaces: I Aper=[ 4. 67 ] (mm), SLPP=[ 1 ] ( % ),
2825 LGP=[ 40 ] (m), MNP=[ 0. 25 ], SCP=[ 0 ] (mi n),
2826 Impervious surfaces: I Ai mp=[ 1. 57 ] (mm), SLPI=[ 1 ] ( % ),
2827 LGI=[ 109 ] (m), MNI=[ 0. 013 ], SCI=[ 0 ] (mi n),
2828 Continuous simulation parameters:
2829 I a RECper=[ 4 ] (hrs), I a RECi mp=[ 4 ] (hrs),
2830 SM N=[ -1 ] (mm), SMAX=[ -1 ] (mm), SK=[ 0. 010 ] / (mm),
2831 Inter Event Ti me=[ 18 ] (hrs), END=- 1
2832 *%-----|-----|
2833 *COMPUTE DUALHYD NHYDi n=[ "W_CLAR_M" ], CI NLET=[ 0. 213 ] (cms), NI NLET=[ 1 ],
2834 * M j NHYD=[ "W_CLAR_M j" ]
2835 * M nNHYD=[ "W_CLAR_M n" ]
2836 * T M STO=[ 0. 1 ] (cu- m)
2837 *%-----|-----|
2838 *# 5- Year + 12% Capture
2839 ROUTE RESERVOIR NHYDout=[ "W_CLAR_M n" ] , NHYDi n=[ "W_CLAR_M" ] ,
2840 * RDT=[ 1 ] (mi n),
2841 * TABLE of ( OUTFLOW STORAGE ) values
2842 * (cms) - (ha- m)
2843 * [ 0. 0 , 0. 0 ]
2844 * [ 0. 213 , 0. 0001 ]
2845 * [ -1 , -1 ] (max twenty pts)
2846 * NHYDovf=[ "W_CLAR_M j" ] ,
2847 *%-----|-----|
2848 * - Clarke_All area from P 598(04)-11 = 120.207 ha, change to 127.298 ha based on
GIS measurements,
2849 * - JFSA 2021-01-19 update W_CLAR_ALL to (121.17-1.772=119.398) ha based on GIS
measurements W_CLAR is 121.17 ha and W_CLAR_M is 1.772 ha
2850 CONTINUOUS STANDHYD NHYD=[ "W_CLAR_ALL" ], DT=[ 1 ] mi n, AREA=[ 119. 398 ] (ha),
2851 XI MP=[ 0. 60 ], TI MP=[ 0. 65 ], DWF=[ 0 ] (cms), LOSS=[ 2 ],
2852 SCS curve number CN=[ 77 ],
2853 Pervious surfaces: I Aper=[ 4. 67 ] (mm), SLPP=[ 1 ] ( % ),
2854 LGP=[ 40 ] (m), MNP=[ 0. 25 ], SCP=[ 0 ] (mi n),
2855 Impervious surfaces: I Ai mp=[ 1. 57 ] (mm), SLPI=[ 1 ] ( % ),
2856 LGI=[ 892. 18 ] (m), MNI=[ 0. 013 ], SCI=[ 0 ] (mi n),

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2857 Continuous simulation parameters:
2858 IaRECper=[ 4](hrs), IaRECimp=[ 4](hrs),
2859 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2860 InterEventTime=[ 18](hrs), END=- 1
2861 *%-----|-----|
2862 ADD HYD NHYDsum=[ "W_CLAR"], NHYDsto add=[ "W_CLAR_ALL"+"W_CLAR_Mj" ]
2863 *%-----|-----|
2864 SAVE HYD NHYD=[ "W_CLAR"], # OF PCYCLES=[ -1], ICASEsh=[ 1]
2865 HYD_COMMENT=[ "Total Flows to West Clarke"]
2866 *#*****
2867 *# West Clarke Pond 2
2868 *# - Rating curve obtained from Barrhaven South M&S modeling
2869 *# - Tributary Drainage Area to M&S Pond 2 = 241 ha
2870 *#*****
2871 ROUTE RESERVOIR NHYDout=[ "MS_P2"], NHYDin=[ "W_CLAR"],
2872 RDT=[ 1](min),
2873 TABLE of ( OUTFLOW STORAGE ) values
2874 (cms) - (ha-m)
2875 [ 0.0 , 0.0 ]
2876 [ 0.128 , 0.161 ]
2877 [ 0.138 , 0.409 ]
2878 [ 0.148 , 0.68 ]
2879 [ 0.227 , 0.931 ]
2880 [ 0.354 , 1.223 ]
2881 [ 0.505 , 1.52 ]
2882 [ 0.666 , 1.821 ]
2883 [ 0.831 , 2.123 ]
2884 [ 0.995 , 2.434 ]
2885 [ 1.069 , 2.583 ]
2886 [ 1.51 , 2.647 ]
2887 [ 4.904 , 2.861 ]
2888 [ 13.048 , 3.188 ]
2889 [ 23.745 , 3.523 ]
2890 [ 36.474 , 3.871 ]
2891 [ 45.938 , 4.127 ]
2892 [ 61.652 , 4.539 ]
2893 [ -1 , -1 ] (max twenty pts)
2894 NHYDovf=[ "P2- OVF" ]
2895 *%-----|-----|
2896 *#*****
2897 * -JFSA, 2021-01-22 "W_CLAR_UNDE" (west of Clarke sub-catchment) discharges
directly to the jock river through a road side ditch on the west side of Borrisokane
road (station 6016)
2898 *CONTINUOUS NASHYD NHYD=[ "W_CLAR_UNDE"], DT=[ 1]min, AREA=[ 35.65](ha),
2899 * DWF=[ 0](cms), CNVC=[ 77], IA=[ 4.67](mm),
2900 * N=[ 3], TP=[ 1.10]hrs,
2901 * Continuous simulation parameters:
2902 * IaRECper=[ 4](hrs),
2903 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2904 * InterEventTime=[ 12](hrs)
2905 * Baseflow simulation parameters:
2906 * BaseFlowOption=[ 1],
2907 * InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
2908 * VHydCond=[ 0.055](mm/hr), END=- 1
2909 *%-----|-----|
2910 ADD HYD NHYDsum=[ "SN_CE"], NHYDsto
add=[ "N_CE"+"S- 1- D4"+"S- 1- D5"+"MS_P2"+"P2- OVF" ]
2911 *%-----|-----|
2912 SAVE HYD NHYD=[ "SN_CE"], # OF PCYCLES=[ -1], ICASEsh=[ 1]
2913 HYD_COMMENT=[ "Total Flows before Station 5737 on Jock River" ]
2914 *%-----|-----|
2915 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 5737
2916 *# 2021-02-25 add station 5737 before station 5002. Station 5737 was extracted from the
HEC-RAS model
T:\PROJ\1474-16\Design\20201026-QuantityControlAnalysis\HEC-RAS\JockLidar2005
2917 *# JFSA 2021-03-02 change the slope to 0.0175% instead of 0.02593 to stabilize the model

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2918 ROUTE CHANNEL      NHYDout =[" 5737" ] , NHYDin=[" SN_CE" ] ,
2919                    RDT=[ 1 ] ( m i n ) ,
2920                    CHLGTH=[ 270 ] ( m ) ,    CHSLOPE=[ 0. 0175 ] ( % ) ,
2921                    FPSLOPE=[ 0. 0175 ] ( % ) ,
2922                    SECNUM=[ 1. 0 ] ,        NSEG=[ 3 ]
2923                    ( SEGROUGH, SEGDI ST ( m ) ) =
2924                    [ 0. 050, - 24. 04
2925                    - 0. 035, 23. 92
2926                    0. 050, 1130. 8 ] NSEG t i m e s
2927                    ( DI STANCE ( m ) , ELEVATI ON ( m ) ) =
2928                    [ - 1060. 52, 94 ]
2929                    [ - 268. 6, 91. 5 ]
2930                    [ - 259. 43, 91. 5 ]
2931                    [ - 179. 48, 91. 5 ]
2932                    [ - 67. 9, 91. 5 ]
2933                    [ - 59. 21, 91. 5 ]
2934                    [ - 33. 19, 91 ]
2935                    [ - 26. 08, 90. 5 ]
2936                    [ - 24. 04, 90 ]
2937                    [ - 13. 14, 86. 77 ]
2938                    [ 0, 85 ]
2939                    [ 14. 68, 86. 74 ]
2940                    [ 23. 92, 90 ]
2941                    [ 25. 78, 90. 5 ]
2942                    [ 31. 91, 91 ]
2943                    [ 91. 95, 91. 5 ]
2944                    [ 772. 15, 92 ]
2945                    [ 961. 49, 92. 5 ]
2946                    [ 1044. 69, 93 ]
2947                    [ 1130. 8, 95 ]
2948 *%-----|-----|
2949 ADD HYD            NHYDs um=[" 5002" ] , NHYDs t o add=[" 5737"+"S- 1- D1"+"S- 1- D6"+"S- 1- D7" ]
2950 *%-----|-----|
2951 SAVE HYD          NHYD=[" 5002" ] ,    # OF PCYCLES=[ - 1 ] ,    I CASEs h=[ 1 ]
2952                    HYD_ COMMENT=[" Total Flows before Station 5002 on Jock Ri ver" ]
2953 *%-----|-----|
2954 *# Hydrograph from Node Cedarview Road routed to Node at West Clarke Drain
2955 *# Channel X- Section obtained from RVCA Hydraulic Model - Station 5002
2956 *# JFSA 2021-02-19 Change the slope from 0.01 % (as per Stantec Report 2007) to 0.0255
% so the model will be more stable and give reasonable results. It is justifiable as
ROUTE CHANNELs aren't well suited to really flat slopes.
2957 *# JFSA 2021-02-19 Change to three ROUTE CHANNEL with length 275 m each instead of one
with 825 m length so the model will be more stable
2958 *# JFSA 2021-02-26 change the length of 5002 route channel from 825 m to 736 m That is
because of adding station 5737 between station 6016 and station 5002. Then the length
from station 5737 to station 5002 is 736 m Change the slope from 0.0255 % to 0.09511 %
2959 *
2960 ROUTE CHANNEL      NHYDout =[" N_ WCa" ] , NHYDin=[" 5002" ] ,
2961                    RDT=[ 1 ] ( m i n ) ,
2962                    CHLGTH=[ 245. 33333 ] ( m ) ,    CHSLOPE=[ 0. 09511 ] ( % ) ,
2963                    FPSLOPE=[ 0. 09511 ] ( % ) ,
2964                    SECNUM=[ 1. 0 ] ,        NSEG=[ 3 ]
2965                    ( SEGROUGH, SEGDI ST ( m ) ) =
2966                    [ 0. 050, - 37. 5
2967                    - 0. 035, 37. 50
2968                    0. 050, 157. 05 ] NSEG t i m e s
2969                    ( DI STANCE ( m ) , ELEVATI ON ( m ) ) =
2970                    [ - 601. 81, 91. 5 ]
2971                    [ - 37. 50, 90. 00 ]
2972                    [ - 19. 61, 87. 04 ]
2973                    [ 0. 00, 85. 70 ]
2974                    [ 14. 87, 86. 93 ]
2975                    [ 37. 50, 90. 00 ]
2976                    [ 38. 54, 90. 50 ]
2977                    [ 42. 23, 91 ]
2978                    [ 157. 05, 91. 50 ]

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2979 * [ 161.44, 91.50]
2980 * [ 236.48, 93.00]
2981 * [ 385.47, 92.50]
2982 * [ 390.78, 92.50]
2983 *%-----|
2984 ROUTE CHANNEL NHYDout=["N_WCb"], NHYDin=["N_WCa"],
2985 RDT=[1](min),
2986 CHLGTH=[245.33333](m), CHSLOPE=[0.09511](%),
2987 FPSLOPE=[0.09511](%),
2988 SECNUM=[1.0], NSEG=[3]
2989 (SEGROUGH, SEGDIST(m))=
2990 [0.050, -37.5
2991 -0.035, 37.50
2992 0.050, 157.05] NSEG times
2993 (DISTANCE(m), ELEVATION(m))=
2994 [-601.81, 91.5]
2995 [-37.50, 90.00]
2996 [-19.61, 87.04]
2997 [0.00, 85.70]
2998 [14.87, 86.93]
2999 [37.50, 90.00]
3000 [38.54, 90.50]
3001 [42.23, 91]
3002 [157.05, 91.50]
3003 *%-----|
3004 ROUTE CHANNEL NHYDout=["N_WC"], NHYDin=["N_WCb"],
3005 RDT=[1](min),
3006 CHLGTH=[245.33333](m), CHSLOPE=[0.09511](%),
3007 FPSLOPE=[0.09511](%),
3008 SECNUM=[1.0], NSEG=[3]
3009 (SEGROUGH, SEGDIST(m))=
3010 [0.050, -37.5
3011 -0.035, 37.50
3012 0.050, 157.05] NSEG times
3013 (DISTANCE(m), ELEVATION(m))=
3014 [-601.81, 91.5]
3015 [-37.50, 90.00]
3016 [-19.61, 87.04]
3017 [0.00, 85.70]
3018 [14.87, 86.93]
3019 [37.50, 90.00]
3020 [38.54, 90.50]
3021 [42.23, 91]
3022 [157.05, 91.50]
3023 ##*****
3024 * -JFSA 2021-02-08 Clarke (MS_P2 and P2-OVF) and Clarke Undeveloped area
(W_CLAR_UNDE) drain to Jock River at Station 5002 instead of Station 4534
3025 *ADD HYD NHYDsum=["SN_WC"], NHYDs to
add=["MS_P2"+"P2-OVF"+"N_WC"+"W_CLAR_UNDE"]
3026 *%-----|
3027 *SAVE HYD NHYD=["SN_WC"], # OF PCYCLES=[-1], I CASESh=[1]
3028 * HYD_COMMENT=["Total Flows at West Clarke Pond Outlet"]
3029 *%-----|
3030 *# Hydrograph from Node West Clarke routed to Node at Kennedy - Burnett Drain
3031 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 4534
3032 *#
3033 ROUTE CHANNEL NHYDout=["N_KB"], NHYDin=["N_WC"],
3034 RDT=[1](min),
3035 CHLGTH=[1020](m), CHSLOPE=[0.0498](%),
3036 FPSLOPE=[0.0498](%),
3037 SECNUM=[1.0], NSEG=[3]
3038 (SEGROUGH, SEGDIST(m))=
3039 [0.050, -23.63
3040 -0.035, 23.63
3041 0.050, 728.3] NSEG times
3042 (DISTANCE(m), ELEVATION(m))=

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3043 [- 1082. 01, 94]
3044 [- 1028. 17, 92. 5]
3045 [- 992. 3, 93. 5]
3046 [- 279. 34, 90]
3047 [- 23. 63, 90]
3048 [- 13. 45, 87. 13]
3049 [- 0. 07, 86. 24]
3050 [ 10. 54, 87. 15]
3051 [ 23. 63, 90]
3052 [ 24. 86, 90. 5]
3053 [ 26. 72, 91]
3054 [ 45. 07, 91. 5]
3055 [ 128. 17, 91. 5]
3056 [ 270. 7, 92. 5]
3057 [ 728. 3, 95]
3058 *%-----|-----|
3059 *#*****|*****|
3060 *# Catchment KEN_BU
3061 *# - To Kennedy-Burnett SWM Facility
3062 *# - Outlets to Fraser-Clarke drain (north of the Jock)
3063 *# - Medium density residential subdivision
3064 * - Add Kennedy Burnett model (Convert PCSWMM from NOVATECH June, 2020 to SWWHYMO)
3065 *#*****|*****|
3066 *CONTINUOUS STANDHYD NHYD=["KEN_BU"], DT=[ 1] mi n, AREA=[ 281] (ha),
3067 * XI MP=[ 0. 55], TI MP=[ 0. 55], DWF=[ 0] (cms), LOSS=[ 2],
3068 * SCS curve number CN=[ 71],
3069 * Pervious surfaces: I A per=[ 4. 67] (mm), SLPP=[ 1] (%),
3070 * LGP=[ 40] (m), MNP=[ 0. 25], SCP=[ 0] (mi n),
3071 * Impervious surfaces: I A i mp=[ 1. 57] (mm), SLPI=[ 1] (%),
3072 * LGI=[ 1369] (m), MNI=[ 0. 013], SCI=[ 0] (mi n),
3073 * Continuous simulation parameters:
3074 * I a REC per=[ 4] (hrs), I a REC i mp=[ 4] (hrs),
3075 * SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
3076 * Int er Event Ti me=[ 18] (hrs), END=- 1
3077 *%-----|-----|
3078 *#*****|*****|
3079 *# Existing Kennedy-Burnett SWM Facility
3080 *# - Rating curve obtained from URTKBP
3081 *# - Tributary Drainage Area to Pond = 160 ha
3082 *#*****|*****|
3083 *ROUTE RESERVOIR NHYDout=["KEN_P"], NHYDin=["KEN_BU"],
3084 * RDT=[ 1] (mi n),
3085 * TABLE of ( OUTFLOW STORAGE ) values
3086 * ( cms ) - ( ha- m)
3087 * [ 0. 0 , 0. 0 ]
3088 * [ 0. 13 , 0. 26]
3089 * [ 0. 43 , 0. 56]
3090 * [ 0. 67 , 0. 90]
3091 * [ 0. 86 , 1. 32]
3092 * [ 1. 01 , 1. 79]
3093 * [ 1. 15 , 2. 33]
3094 * [ - 1 , - 1 ] (max twenty pts)
3095 * NHYDovf=["KEN-OV"]
3096 *%-----|-----|
3097 * -JFSA, 2021-01-19 update all KEN_BU areas based on GIS measurements
3098 CONTINUOUS STANDHYD NHYD=["KB-01A"], DT=[ 1] mi n, AREA=[ 40. 82] (ha), XI MP=[ 0. 097],
3099 TI MP=[ 0. 4], DWF=[ 0] (cms), LOSS=[ 1]:
3099 Horton: Fo=[ 76. 20] (mm/ hr), Fc=[ 13. 20] (mm/ hr), DCAY=[ 4. 14] (/ hr),
3100 F=[ 0. 00] (mm),
3100 Pervious areas: I A per=[ 4. 67] (mm), SLPP=[ 0. 5] (%), LGP=[ 40] (m),
3101 MNP=[ 0. 250], SCP=[ 0] (mi n),
3101 Impervious areas: I A i mp=[ 0. 785] (mm), SLPI=[ 0. 5] (%),
3102 LGI=[ 521. 664] (m), MNI=[ 0. 013], SCI=[ 0] (mi n),
3102 Continuous simulation parameters:
3103 I a REC per=[ 4] (hrs), I a REC i mp=[ 4] (hrs), Int er Event Ti me=[ 12] (hrs),
3103 END=- 1

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3104 *%-----|-----|
3105 COMPUTE DUALHYD NHYDin=[ " KB- 01A" ], CI NLET=[ 3. 6 ] ( cms ), NI NLET=[ 1 ],
3106 Māj NHYD=[ " KB- 01A- M " ]
3107 M nNHYD=[ " KB- 01A- MN" ]
3108 TM STO=[ 4995 ] ( cu- m )
3109 *%-----|-----|
3110 ADD HYD NHYDsum=[ " KB- 01A- S" ], NHYDs to add=[ " KB- 01A- M " + " KB- 01A- MN" ]
3111 *%-----|-----|
3112 CONTINUOUS STANDHYD NHYD=[ " KB- 01B" ], DT=[ 1 ] mi n, AREA=[ 31. 1 ] ( ha ), XI MP=[ 0. 1875 ],
TI MP=[ 0. 375 ], DWF=[ 0 ] ( cms ), LOSS=[ 1 ] :
3113 Horton: Fo=[ 76. 20 ] ( mm/ hr ), Fc=[ 13. 20 ] ( mm/ hr ), DCAY=[ 4. 14 ] ( / hr ),
F=[ 0. 00 ] ( mm ),
3114 Pervious areas: I A per=[ 4. 67 ] ( mm ), SLPP=[ 0. 42 ] ( % ), LGP=[ 40 ] ( m ),
MNP=[ 0. 250 ], SCP=[ 0 ] ( mi n ),
3115 Impervious areas: I A i mp=[ 0. 785 ] ( mm ), SLPI=[ 0. 42 ] ( % ),
LGI=[ 455. 339 ] ( m ), MNI=[ 0. 013 ], SCI=[ 0 ] ( mi n ),
3116 Continuous simulation parameters:
3117 I a REC per=[ 4 ] ( hrs ), I a REC i mp=[ 4 ] ( hrs ), Int er Event Ti me=[ 12 ] ( hrs ),
END=- 1
3118 *%-----|-----|
3119 COMPUTE DUALHYD NHYDin=[ " KB- 01B" ], CI NLET=[ 1. 585 ] ( cms ), NI NLET=[ 1 ],
3120 Māj NHYD=[ " KB- 01B- M " ]
3121 M nNHYD=[ " KB- 01B- MN" ]
3122 TM STO=[ 6075 ] ( cu- m )
3123 *%-----|-----|
3124 ADD HYD NHYDsum=[ " KB- 01B- S" ], NHYDs to add=[ " KB- 01B- M " + " KB- 01B- MN" ]
3125 *%-----|-----|
3126 CONTINUOUS STANDHYD NHYD=[ " KB- 01C" ], DT=[ 1 ] mi n, AREA=[ 13. 78 ] ( ha ), XI MP=[ 0. 2045 ],
TI MP=[ 0. 409 ], DWF=[ 0 ] ( cms ), LOSS=[ 1 ] :
3127 Horton: Fo=[ 76. 20 ] ( mm/ hr ), Fc=[ 13. 20 ] ( mm/ hr ), DCAY=[ 4. 14 ] ( / hr ),
F=[ 0. 00 ] ( mm ),
3128 Pervious areas: I A per=[ 4. 67 ] ( mm ), SLPP=[ 2. 0 ] ( % ), LGP=[ 40 ] ( m ),
MNP=[ 0. 250 ], SCP=[ 0 ] ( mi n ),
3129 Impervious areas: I A i mp=[ 0. 785 ] ( mm ), SLPI=[ 0. 5 ] ( % ),
LGI=[ 303. 095 ] ( m ), MNI=[ 0. 013 ], SCI=[ 0 ] ( mi n ),
3130 Continuous simulation parameters:
3131 I a REC per=[ 4 ] ( hrs ), I a REC i mp=[ 4 ] ( hrs ), Int er Event Ti me=[ 12 ] ( hrs ),
END=- 1
3132 *%-----|-----|
3133 COMPUTE DUALHYD NHYDin=[ " KB- 01C" ], CI NLET=[ 1. 35 ] ( cms ), NI NLET=[ 1 ],
3134 Māj NHYD=[ " KB- 01C- M " ]
3135 M nNHYD=[ " KB- 01C- MN" ]
3136 TM STO=[ 1880 ] ( cu- m )
3137 *%-----|-----|
3138 ADD HYD NHYDsum=[ " KB- 01C- S" ], NHYDs to add=[ " KB- 01C- M " + " KB- 01C- MN" ]
3139 *%-----|-----|
3140 CONTINUOUS STANDHYD NHYD=[ " KB- 03" ], DT=[ 1 ] mi n, AREA=[ 84. 78 ] ( ha ), XI MP=[ 0. 197 ],
TI MP=[ 0. 394 ], DWF=[ 0 ] ( cms ), LOSS=[ 1 ] :
3141 Horton: Fo=[ 76. 20 ] ( mm/ hr ), Fc=[ 13. 20 ] ( mm/ hr ), DCAY=[ 4. 14 ] ( / hr ),
F=[ 0. 00 ] ( mm ),
3142 Pervious areas: I A per=[ 4. 67 ] ( mm ), SLPP=[ 2. 0 ] ( % ), LGP=[ 40 ] ( m ),
MNP=[ 0. 250 ], SCP=[ 0 ] ( mi n ),
3143 Impervious areas: I A i mp=[ 0. 785 ] ( mm ), SLPI=[ 0. 63 ] ( % ),
LGI=[ 751. 798 ] ( m ), MNI=[ 0. 013 ], SCI=[ 0 ] ( mi n ),
3144 Continuous simulation parameters:
3145 I a REC per=[ 4 ] ( hrs ), I a REC i mp=[ 4 ] ( hrs ), Int er Event Ti me=[ 12 ] ( hrs ),
END=- 1
3146 *%-----|-----|
3147 COMPUTE DUALHYD NHYDin=[ " KB- 03" ], CI NLET=[ 5. 27 ] ( cms ), NI NLET=[ 1 ],
3148 Māj NHYD=[ " KB- 03- M " ]
3149 M nNHYD=[ " KB- 03- MN" ]
3150 TM STO=[ 15500 ] ( cu- m )
3151 *%-----|-----|
3152 ADD HYD NHYDsum=[ " KB- 03- S" ], NHYDs to add=[ " KB- 03- M " + " KB- 03- MN" ]
3153 *%-----|-----|
3154 CONTINUOUS STANDHYD NHYD=[ " KB- 04" ], DT=[ 1 ] mi n, AREA=[ 6. 95 ] ( ha ), XI MP=[ 0. 85 ],

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3155 TI MP=[0.85], DWF=[0](cms), LOSS=[1]:
 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
 F=[0.00](mm),
 3156 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
 MNP=[0.250], SCP=[0](min),
 3157 Impervious areas: IAimp=[0.942](mm), SLPI=[0.5](%),
 LGI=[215.252](m), MNI=[0.013], SCI=[0](min),
 3158 Continuous simulation parameters:
 3159 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
 END=- 1
 3160 *%-----|
 3161 COMPUTE DUALHYD NHYDin=["KB- 04"], CINLET=[0.503](cms), NINLET=[1],
 3162 MajNHYD=["KB- 04- M"]
 3163 MnNHYD=["KB- 04- MN"]
 3164 TMSTO=[1972](cu-m)
 3165 *%-----|
 3166 ADD HYD NHYDsum=["KB- 04- S"], NHYDsto add=["KB- 04- M"+"KB- 04- MN"]
 3167 *%-----|
 3168 CONTINUOUS STANDHYD NHYD=["KB- 05"], DT=[1]min, AREA=[5.19](ha), XI MP=[0.93],
 TI MP=[0.93], DWF=[0](cms), LOSS=[1]:
 3169 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
 F=[0.00](mm),
 3170 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
 MNP=[0.250], SCP=[0](min),
 3171 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%),
 LGI=[186.011](m), MNI=[0.013], SCI=[0](min),
 3172 Continuous simulation parameters:
 3173 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
 END=- 1
 3174 *%-----|
 3175 *%-----|
 3176 CONTINUOUS STANDHYD NHYD=["KB- 06"], DT=[1]min, AREA=[12.93](ha), XI MP=[0.873],
 TI MP=[0.873], DWF=[0](cms), LOSS=[1]:
 3177 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
 F=[0.00](mm),
 3178 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
 MNP=[0.250], SCP=[0](min),
 3179 Impervious areas: IAimp=[0.942](mm), SLPI=[4.75](%),
 LGI=[293.598](m), MNI=[0.013], SCI=[0](min),
 3180 Continuous simulation parameters:
 3181 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
 END=- 1
 3182 *%-----|
 3183 COMPUTE DUALHYD NHYDin=["KB- 06"], CINLET=[2.262](cms), NINLET=[1],
 3184 MajNHYD=["KB- 06- M"]
 3185 MnNHYD=["KB- 06- MN"]
 3186 TMSTO=[1950](cu-m)
 3187 *%-----|
 3188 ADD HYD NHYDsum=["KB- 06- S"], NHYDsto add=["KB- 06- M"+"KB- 06- MN"]
 3189 *%-----|
 3190 CONTINUOUS STANDHYD NHYD=["KB- 11"], DT=[1]min, AREA=[4.03](ha), XI MP=[0.675],
 TI MP=[0.675], DWF=[0](cms), LOSS=[1]:
 3191 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
 F=[0.00](mm),
 3192 Pervious areas: IAper=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
 MNP=[0.250], SCP=[0](min),
 3193 Impervious areas: IAimp=[0.785](mm), SLPI=[2.0](%),
 LGI=[163.911](m), MNI=[0.013], SCI=[0](min),
 3194 Continuous simulation parameters:
 3195 IaRECper=[4](hrs), IaRECImp=[4](hrs), InterEventTime=[12](hrs),
 END=- 1
 3196 *%-----|
 3197 COMPUTE DUALHYD NHYDin=["KB- 11"], CINLET=[0.5773](cms), NINLET=[1],
 3198 MajNHYD=["KB- 11- M"]
 3199 MnNHYD=["KB- 11- MN"]
 3200 TMSTO=[597](cu-m)

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3201  *%-----|-----|
3202  ADD HYD      NHYDsum=["KB-11-S"], NHYDs to add=["KB-11-M"+"KB-11-MN"]
3203  *%-----|-----|
3204  CONTINUOUS STANDHYD NHYD=["S1"], DT=[1] min, AREA=[4.99](ha), XI MP=[0.93], TI MP=[0.93],
DWF=[0](cms), LOSS=[1]:
3205  Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3206  Previous areas: I A per=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3207  ImperVIOUS areas: I A i mp=[1.57](mm), SLPI=[2.0](%),
LGI=[182.392](m), MNI=[0.013], SCI=[0](min),
3208  Continuous simulation parameters:
3209  I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=-1
3210  *%-----|-----|
3211  CONTINUOUS STANDHYD NHYD=["KB-15"], DT=[1] min, AREA=[2.15](ha), XI MP=[0.79],
TI MP=[0.79], DWF=[0](cms), LOSS=[1]:
3212  Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3213  Previous areas: I A per=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3214  ImperVIOUS areas: I A i mp=[0.157](mm), SLPI=[0.3](%),
LGI=[119.722](m), MNI=[0.013], SCI=[0](min),
3215  Continuous simulation parameters:
3216  I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=-1
3217  *%-----|-----|
3218  *%-----|-----|
3219  ADD HYD      NHYDsum=["KB-P1"], NHYDs to
add=["KB-01A-S"+"KB-01B-S"+"KB-01C-S"+"KB-03-S"+"KB-04-S"+"KB-05"+"KB-06-S"+"KB-11-S"+"KB
-15"+"S1"]
3220  *%-----|-----|
3221  ROUTE RESERVOIR NHYDout=["KB-P1R"], NHYDin=["KB-P1"],
3222  RDT=[1](min),
3223  TABLE of ( OUTFLOW STORAGE ) values
3224  (cms) - (ha-m)
3225  [ 0.0 , 0.0 ]
3226  [0.076,0.003]
3227  [0.088,0.006]
3228  [0.136,0.011]
3229  [0.301,0.017]
3230  [0.454,0.027]
3231  [0.631,0.041]
3232  [1.173,0.068]
3233  [1.91,0.111]
3234  [4.847,0.231]
3235  [9.813,0.436]
3236  [12.134,0.617]
3237  [12.438,0.732]
3238  [12.424,0.811]
3239  [12.425,0.894]
3240  [ -1 , -1 ] (max twenty pts)
3241  NHYDovf=["KB-P1ovf"]
3242  *%-----|-----|
3243  ADD HYD      NHYDsum=["KB-Pond1"], NHYDs to add=["KB-P1R"+"KB-P1ovf"]
3244  *%-----|-----|
3245  SAVE HYD     NHYD=["KB-Pond1"], # OF PCYCLES=[-1], I CASEs h=[1]
3246  HYD_COMMENT=["Total Flows at KB first pond"]
3247  *%-----|-----|
3248  CONTINUOUS STANDHYD NHYD=["KB-07"], DT=[1] min, AREA=[10.86](ha), XI MP=[0.86],
TI MP=[0.86], DWF=[0](cms), LOSS=[1]:
3249  Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3250  Previous areas: I A per=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3251  ImperVIOUS areas: I A i mp=[0.785](mm), SLPI=[2.0](%),

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3252 LGI=[ 269.072](m), MNI=[ 0.013], SCI=[ 0](min),
3253 Continuous simulation parameters:
3253 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3254 END=- 1
3254 *%-----|
3255 COMPUTE DUALHYD NHYDin=["KB-07"], CINLET=[ 2.094](cms), NINLET=[ 1],
3256 MajNHYD=["KB-07-M"]
3257 MnNHYD=["KB-07-MN"]
3258 TMSTO=[ 1378](cu-m)
3259 *%-----|
3260 ADD HYD NHYDsum=["KB-07-S"], NHYDsto add=["KB-07-M"+"KB-07-MN"]
3261 *%-----|
3262 CONTINUOUS STANDHYD NHYD=["KB-08"], DT=[ 1]min, AREA=[ 6.61](ha), XI MP=[ 0.64],
3263 TIMP=[ 0.64], DWF=[ 0](cms), LOSS=[ 1]:
3263 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3264 F=[ 0.00](mm),
3264 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3265 MNP=[ 0.250], SCP=[ 0](min),
3265 Impervious areas: IAimp=[ 0.785](mm), SLPI=[ 2.0](%),
3266 LGI=[ 209.921](m), MNI=[ 0.013], SCI=[ 0](min),
3266 Continuous simulation parameters:
3267 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3268 END=- 1
3268 *%-----|
3269 COMPUTE DUALHYD NHYDin=["KB-08"], CINLET=[ 1.058](cms), NINLET=[ 1],
3270 MajNHYD=["KB-08-M"]
3271 MnNHYD=["KB-08-MN"]
3272 TMSTO=[ 787](cu-m)
3273 *%-----|
3274 ADD HYD NHYDsum=["KB-08-S"], NHYDsto add=["KB-08-M"+"KB-08-MN"]
3275 *%-----|
3276 CONTINUOUS STANDHYD NHYD=["KB-09"], DT=[ 1]min, AREA=[ 2.6](ha), XI MP=[ 0.86],
3277 TIMP=[ 0.86], DWF=[ 0](cms), LOSS=[ 1]:
3277 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3278 F=[ 0.00](mm),
3278 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3279 MNP=[ 0.250], SCP=[ 0](min),
3279 Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 2.0](%),
3280 LGI=[ 131.656](m), MNI=[ 0.013], SCI=[ 0](min),
3280 Continuous simulation parameters:
3281 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3282 END=- 1
3282 *%-----|
3283 *%-----|
3284 CONTINUOUS STANDHYD NHYD=["KB-10_1"], DT=[ 1]min, AREA=[ 2.37](ha), XI MP=[ 0.86],
3285 TIMP=[ 0.86], DWF=[ 0](cms), LOSS=[ 1]:
3285 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3286 F=[ 0.00](mm),
3286 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3287 MNP=[ 0.250], SCP=[ 0](min),
3287 Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 2.0](%),
3288 LGI=[ 125.698](m), MNI=[ 0.013], SCI=[ 0](min),
3288 Continuous simulation parameters:
3289 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3290 END=- 1
3290 *%-----|
3291 CONTINUOUS STANDHYD NHYD=["KB-10_2"], DT=[ 1]min, AREA=[ 1.14](ha), XI MP=[ 0.86],
3292 TIMP=[ 0.86], DWF=[ 0](cms), LOSS=[ 1]:
3292 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3293 F=[ 0.00](mm),
3293 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3294 MNP=[ 0.250], SCP=[ 0](min),
3294 Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 2.0](%), LGI=[ 87.178](m),
3295 MNI=[ 0.013], SCI=[ 0](min),
3295 Continuous simulation parameters:
3296 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),

```

END=- 1

3297 *%-----|-----|
3298 *%-----|-----|
3299 CONTINUOUS STANDHYD NHYD=[" KB- 12"], DT=[1] mi n, AREA=[4. 86] (ha), XI MP=[0. 79],
TI MP=[0. 79], DWF=[0] (cms), LOSS=[1]:
3300 Horton: Fo=[76. 20] (mm/ hr), Fc=[13. 20] (mm/ hr), DCAY=[4. 14] (/ hr),
F=[0. 00] (mm),
3301 Pervious areas: I A_{per}=[4. 67] (mm), SLPP=[2. 0] (%), LGP=[40] (m),
MNP=[0. 250], SCP=[0] (mi n),
3302 Impervious areas: I A_{imp}=[1. 099] (mm), SLPI=[2. 0] (%),
LGI=[180. 000] (m), MNI=[0. 013], SCI=[0] (mi n),
3303 Continuous simulation parameters:
3304 I aREC_{per}=[4] (hrs), I aREC_{imp}=[4] (hrs), I nter Event Ti me=[12] (hrs),
END=- 1
3305 *%-----|-----|
3306 COMPUTE DUALHYD NHYD_in=[" KB- 12"], CI NLET=[0. 8665] (cms), NI NLET=[1],
3307 M_aj NHYD=[" KB- 12- M"]
3308 M_nNHYD=[" KB- 12- MN"]
3309 TM_{STO}=[632] (cu- m)
3310 *%-----|-----|
3311 ADD HYD NHYD_sum=[" KB- 12- S"], NHYD_s to add=[" KB- 12- M" +" KB- 12- MN"]
3312 *%-----|-----|
3313 CONTINUOUS STANDHYD NHYD=[" KB- 13"], DT=[1] mi n, AREA=[10. 19] (ha), XI MP=[0. 64],
TI MP=[0. 64], DWF=[0] (cms), LOSS=[1]:
3314 Horton: Fo=[76. 20] (mm/ hr), Fc=[13. 20] (mm/ hr), DCAY=[4. 14] (/ hr),
F=[0. 00] (mm),
3315 Pervious areas: I A_{per}=[4. 67] (mm), SLPP=[2. 0] (%), LGP=[40] (m),
MNP=[0. 250], SCP=[0] (mi n),
3316 Impervious areas: I A_{imp}=[0. 785] (mm), SLPI=[2. 0] (%),
LGI=[260. 640] (m), MNI=[0. 013], SCI=[0] (mi n),
3317 Continuous simulation parameters:
3318 I aREC_{per}=[4] (hrs), I aREC_{imp}=[4] (hrs), I nter Event Ti me=[12] (hrs),
END=- 1
3319 *%-----|-----|
3320 COMPUTE DUALHYD NHYD_in=[" KB- 13"], CI NLET=[1. 722] (cms), NI NLET=[1],
3321 M_aj NHYD=[" KB- 13- M"]
3322 M_nNHYD=[" KB- 13- MN"]
3323 TM_{STO}=[1077] (cu- m)
3324 *%-----|-----|
3325 ADD HYD NHYD_sum=[" KB- 13- S"], NHYD_s to add=[" KB- 13- M" +" KB- 13- MN"]
3326 *%-----|-----|
3327 CONTINUOUS STANDHYD NHYD=[" KB- 14"], DT=[1] mi n, AREA=[5. 47] (ha), XI MP=[0. 64],
TI MP=[0. 64], DWF=[0] (cms), LOSS=[1]:
3328 Horton: Fo=[76. 20] (mm/ hr), Fc=[13. 20] (mm/ hr), DCAY=[4. 14] (/ hr),
F=[0. 00] (mm),
3329 Pervious areas: I A_{per}=[4. 67] (mm), SLPP=[2. 0] (%), LGP=[40] (m),
MNP=[0. 250], SCP=[0] (mi n),
3330 Impervious areas: I A_{imp}=[0. 785] (mm), SLPI=[2. 0] (%),
LGI=[190. 962] (m), MNI=[0. 013], SCI=[0] (mi n),
3331 Continuous simulation parameters:
3332 I aREC_{per}=[4] (hrs), I aREC_{imp}=[4] (hrs), I nter Event Ti me=[12] (hrs),
END=- 1
3333 *%-----|-----|
3334 COMPUTE DUALHYD NHYD_in=[" KB- 14"], CI NLET=[0. 8734] (cms), NI NLET=[1],
3335 M_aj NHYD=[" KB- 14- M"]
3336 M_nNHYD=[" KB- 14- MN"]
3337 TM_{STO}=[631] (cu- m)
3338 *%-----|-----|
3339 ADD HYD NHYD_sum=[" KB- 14- S"], NHYD_s to add=[" KB- 14- M" +" KB- 14- MN"]
3340 *%-----|-----|
3341 *%-----|-----|
3342 CONTINUOUS STANDHYD NHYD=[" KB- 16_2"], DT=[1] mi n, AREA=[3. 42] (ha), XI MP=[0. 71],
TI MP=[0. 71], DWF=[0] (cms), LOSS=[1]:
3343 Horton: Fo=[76. 20] (mm/ hr), Fc=[13. 20] (mm/ hr), DCAY=[4. 14] (/ hr),
F=[0. 00] (mm),
3344 Pervious areas: I A_{per}=[4. 67] (mm), SLPP=[2. 0] (%), LGP=[40] (m),

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3345 MNP=[ 0.250], SCP=[ 0]( mi n),
Impervious areas: I A i mp=[ 0.157]( mm), SLPI=[ 0.3]( %),
3346 LGI=[ 150.997]( m), MNI=[ 0.013], SCI=[ 0]( mi n),
3347 Continuous simulation parameters:
I a RE C per=[ 4]( hr s), I a RE C i mp=[ 4]( hr s), I n t e r E v e n t T i m e=[ 12]( hr s),
END=- 1
3348 *%-----|-----|
3349 ADD HYD NHYDs um=[ "KB- P2"], NHYDs t o
add=[ "KB- Pond1"+"KB- 07- S"+"KB- 08- S"+"KB- 09"+"KB- 10_1"+"KB- 10_2"+"KB- 12- S"+"KB- 13- S"+"KB- 1
4- S"+"KB- 16_2"]
3350 *%-----|-----|
3351 ROUTE RESERVOIR NHYDout =[ "KB- P2R"], NHYDi n=[ "KB- P2"],
3352 RDT=[ 1]( mi n),
3353 TABLE of ( OUTFLOW STORAGE ) values
3354 ( cms ) - ( ha- m)
3355 [ 0.0 , 0.0 ]
3356 [ 0.053, 0.005]
3357 [ 0.132, 0.009]
3358 [ 0.269, 0.014]
3359 [ 0.455, 0.023]
3360 [ 0.699, 0.037]
3361 [ 0.947, 0.056]
3362 [ 1.853, 0.09]
3363 [ 2.712, 0.146]
3364 [ 6.626, 0.287]
3365 [ 11.228, 0.515]
3366 [ 14.885, 0.738]
3367 [ 16.473, 0.893]
3368 [ 17.311, 0.998]
3369 [ 17.633, 1.063]
3370 [ 17.634, 1.112]
3371 [ -1 , -1 ] (max t went y pt s)
3372 NHYDovf=[ "KB- P2ovf"]
3373 *%-----|-----|
3374 ADD HYD NHYDs um=[ "KB- Pond2"], NHYDs t o add=[ "KB- P2R"+"KB- P2ovf"]
3375 *%-----|-----|
3376 SAVE HYD NHYD=[ "KB- Pond2"], # OF PCYCLES=[ -1], I CASEs h=[ 1]
3377 HYD_COMMENT=[ "Total Flows at KB second pond"]
3378 *%-----|-----|
3379 CONTINUOUS STANDHYD NHYD=[ "KB- 16_1"], DT=[ 1] mi n, AREA=[ 2.8]( ha), XI MP=[ 0.75],
TI MP=[ 0.75], DWF=[ 0]( cms), LOSS=[ 1]:
3380 Horton: Fo=[ 76.20]( mm/ hr), Fc=[ 13.20]( mm/ hr), DCAY=[ 4.14]( / hr),
F=[ 0.00]( mm),
3381 Pervious areas: I A p e r=[ 4.67]( mm), SLPP=[ 2.0]( %), LGP=[ 40]( m),
MNP=[ 0.250], SCP=[ 0]( mi n),
3382 Impervious areas: I A i mp=[ 0.157]( mm), SLPI=[ 0.3]( %),
LGI=[ 136.626]( m), MNI=[ 0.013], SCI=[ 0]( mi n),
3383 Continuous simulation parameters:
3384 I a RE C per=[ 4]( hr s), I a RE C i mp=[ 4]( hr s), I n t e r E v e n t T i m e=[ 12]( hr s),
END=- 1
3385 *%-----|-----|
3386 ADD HYD NHYDs um=[ "KB- P3"], NHYDs t o add=[ "KB- Pond2"+"KB- 16_1"]
3387 *%-----|-----|
3388 *%-----|-----|
3389 * One inflow node from pond 3 is added to the model (ROUTE RESERVOIR)
3390 * Another inflow node from right side of pond 3 is not added to the model
3391 ROUTE RESERVOIR NHYDout =[ "KB- P3R"], NHYDi n=[ "KB- P3"],
3392 RDT=[ 1]( mi n),
3393 TABLE of ( OUTFLOW STORAGE ) values
3394 ( cms ) - ( ha- m)
3395 [ 0.0 , 0.0 ]
3396 [ 0.051, 0.002]
3397 [ 0.048, 0.003]
3398 [ 0.057, 0.029]
3399 [ 0.089, 0.045]
3400 [ 0.133, 0.069]

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3401 [ 0.199, 0.106]
3402 [ 0.321, 0.172]
3403 [ 1.029, 0.306]
3404 [ 4.036, 0.527]
3405 [ 8.332, 0.761]
3406 [ 11.727, 0.941]
3407 [ 14.125, 1.067]
3408 [ 15.675, 1.149]
3409 [ 16.555, 1.196]
3410 [ 16.911, 1.214]
3411 [ -1 , -1 ] (max twenty pts)
3412 NHYDovf=["KB- P3ovf"]
3413 *%-----|-----|
3414 ADD HYD NHYDsum=["KB- Pond3"], NHYDs to add=["KB- P3R"+"KB- P3ovf"]
3415 *%-----|-----|
3416 SAVE HYD NHYD=["KB- Pond3"], # OF PCYCLES=[ -1], ICASEsh=[ 1]
3417 HYD_COMMENT=["Total Flows at KB third pond"]
3418 *%-----|-----|
3419 *#*****|*****|
3420 *# EXISTING / PROPOSED Subcatchments (Kennedy-Burnett SWM Facility (118080), SWM
3421 Modeling Approach, NOVATECH Report June, 2020)
3422 *# - TO FRASER-CLARKE DRAIN
3423 *#*****|*****|
3424 CONTINUOUS STANDHYD NHYD=["FC- 01"], DT=[ 1]min, AREA=[ 8.03](ha), XI MP=[ 0.47],
3425 T I MP=[ 0.47], DWF=[ 0](cms), LOSS=[ 1]:
3426 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3427 F=[ 0.00](mm),
3428 Pervious areas: I A per=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3429 MNP=[ 0.250], SCP=[ 0](min),
3430 Impervious areas: I A i mp=[ 1.57](mm), SLPI=[ 1.0](%),
3431 LGI=[ 231.373](m), MNI=[ 0.013], SCI=[ 0](min),
3432 Continuous simulation parameters:
3433 I a REC per=[ 4](hrs), I a REC i mp=[ 4](hrs), I n t e r E v e n t T i m e=[ 12](hrs),
3434 E N D=- 1
3435 *%-----|-----|
3436 COMPUTE DUALHYD NHYDin=["FC- 01"], C I N L E T=[ 0.756](cms), N I N L E T=[ 1],
3437 M a j N H Y D=["FC- 01- M"],
3438 M i n N H Y D=["FC- 01- M N"],
3439 T M S T O=[ 714](cu-m)
3440 *%-----|-----|
3441 ADD HYD NHYDsum=["FC- 01- S"], NHYDs to add=["FC- 01- M"+"FC- 01- M N"]
3442 *%-----|-----|
3443 CONTINUOUS STANDHYD NHYD=["FC- 02"], DT=[ 1]min, AREA=[ 16.05](ha), XI MP=[ 0.93],
3444 T I MP=[ 0.93], DWF=[ 0](cms), LOSS=[ 1]:
3445 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3446 F=[ 0.00](mm),
3447 Pervious areas: I A per=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3448 MNP=[ 0.250], SCP=[ 0](min),
3449 Impervious areas: I A i mp=[ 1.57](mm), SLPI=[ 1.0](%),
3450 LGI=[ 327.109](m), MNI=[ 0.013], SCI=[ 0](min),
3451 Continuous simulation parameters:
3452 I a REC per=[ 4](hrs), I a REC i mp=[ 4](hrs), I n t e r E v e n t T i m e=[ 12](hrs),
3453 E N D=- 1
3454 *%-----|-----|
3455 COMPUTE DUALHYD NHYDin=["FC- 02"], C I N L E T=[ 1.159](cms), N I N L E T=[ 1],
3456 M a j N H Y D=["FC- 02- M"],
3457 M i n N H Y D=["FC- 02- M N"],
3458 T M S T O=[ 2385](cu-m)
3459 *%-----|-----|
3460 ADD HYD NHYDsum=["FC- 02- S"], NHYDs to add=["FC- 02- M"+"FC- 02- M N"]
3461 *%-----|-----|
3462 CONTINUOUS STANDHYD NHYD=["FC- 03"], DT=[ 1]min, AREA=[ 7.37](ha), XI MP=[ 0.64],
3463 T I MP=[ 0.64], DWF=[ 0](cms), LOSS=[ 1]:
3464 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3465 F=[ 0.00](mm),
3466 Pervious areas: I A per=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),

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3454 MNP=[ 0.250], SCP=[ 0](mi n),
Impervious areas: IAi mp=[ 1.57](mm), SLPI =[ 1.0](%),
LGI =[ 221.660](m), MNI =[ 0.013], SCI =[ 0](mi n),
3455 Continuous simulation parameters:
3456 IaREcper=[ 4](hrs), IaRECi mp=[ 4](hrs), InterEvent Time=[ 12](hrs),
END=- 1
3457 *%-----|-----|
3458 COMPUTE DUALHYD NHYDin=[ "FC-03"], CINLET=[ 0.358](cms), NINLET=[ 1],
3459 Maj NHYD=[ "FC-03-M"]
3460 MnNHYD=[ "FC-03-MN"]
3461 TMSTO=[ 1131](cu-m)
3462 *%-----|-----|
3463 ADD HYD NHYDsum=[ "FC-03-S"], NHYDs to add=[ "FC-03-M"+"FC-03-MN"]
3464 *%-----|-----|
3465 CONTINUOUS STANDHYD NHYD=[ "FC-04"], DT=[ 1]mi n, AREA=[ 12.87](ha), XI MP=[ 0.64],
TI MP=[ 0.64], DWF=[ 0](cms), LOSS=[ 1]:
3466 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
F=[ 0.00](mm),
3467 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
MNP=[ 0.250], SCP=[ 0](mi n),
3468 Impervious areas: IAi mp=[ 1.57](mm), SLPI =[ 1.0](%),
LGI =[ 292.916](m), MNI =[ 0.013], SCI =[ 0](mi n),
3469 Continuous simulation parameters:
3470 IaREcper=[ 4](hrs), IaRECi mp=[ 4](hrs), InterEvent Time=[ 12](hrs),
END=- 1
3471 *%-----|-----|
3472 COMPUTE DUALHYD NHYDin=[ "FC-04"], CINLET=[ 0.741](cms), NINLET=[ 1],
3473 Maj NHYD=[ "FC-04-M"]
3474 MnNHYD=[ "FC-04-MN"]
3475 TMSTO=[ 1794](cu-m)
3476 *%-----|-----|
3477 ADD HYD NHYDsum=[ "FC-04-S"], NHYDs to add=[ "FC-04-M"+"FC-04-MN"]
3478 *%-----|-----|
3479 *#*****
3480 *# PROPOSED Subcatchments (Kennedy-Burnett SWM Facility (118080), SWM Modeling
Approach, NOVATECH Report June, 2020)
3481 *# - TO JOCK RIVER
3482 *#*****
3483 CONTINUOUS STANDHYD NHYD=[ "JR-01"], DT=[ 1]mi n, AREA=[ 8.24](ha), XI MP=[ 0.64],
TI MP=[ 0.64], DWF=[ 0](cms), LOSS=[ 1]:
3484 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
F=[ 0.00](mm),
3485 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
MNP=[ 0.250], SCP=[ 0](mi n),
3486 Impervious areas: IAi mp=[ 1.57](mm), SLPI =[ 1.0](%),
LGI =[ 234.379](m), MNI =[ 0.013], SCI =[ 0](mi n),
3487 Continuous simulation parameters:
3488 IaREcper=[ 4](hrs), IaRECi mp=[ 4](hrs), InterEvent Time=[ 12](hrs),
END=- 1
3489 *%-----|-----|
3490 COMPUTE DUALHYD NHYDin=[ "JR-01"], CINLET=[ 0.563](cms), NINLET=[ 1],
3491 Maj NHYD=[ "JR-01-M"]
3492 MnNHYD=[ "JR-01-MN"]
3493 TMSTO=[ 1040](cu-m)
3494 *%-----|-----|
3495 ADD HYD NHYDsum=[ "JR-01-S"], NHYDs to add=[ "JR-01-M"+"JR-01-MN"]
3496 *%-----|-----|
3497 CONTINUOUS STANDHYD NHYD=[ "JR-02"], DT=[ 1]mi n, AREA=[ 1.59](ha), XI MP=[ 0.64],
TI MP=[ 0.64], DWF=[ 0](cms), LOSS=[ 1]:
3498 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
F=[ 0.00](mm),
3499 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
MNP=[ 0.250], SCP=[ 0](mi n),
3500 Impervious areas: IAi mp=[ 1.57](mm), SLPI =[ 1.0](%),
LGI =[ 102.956](m), MNI =[ 0.013], SCI =[ 0](mi n),
3501 Continuous simulation parameters:

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3502 IaRECper=[ 4]( hrs), IaRECI mp=[ 4]( hrs), I nterEventTi me=[ 12]( hrs),
END=- 1
3503 *%-----|-----|
3504 COMPUTE DUALHYD NHYDin=["JR-02"], CI NLET=[ 0.153]( cms), NI NLET=[ 1],
3505 Mij NHYD=["JR-02-M"]
3506 MnNHYD=["JR-02-MN"]
3507 TMSTO=[ 153]( cu- m)
3508 *%-----|-----|
3509 ADD HYD NHYDsum=["JR-02-S"], NHYDs to add=["JR-02-M"+"JR-02-MN"]
3510 *%-----|-----|
3511 *#*****|*****|
3512 *# Catchment FRASER
3513 *# - To Fraser-Clarke drain (north of the Jock)
3514 *# - Developed land with assumed 43% imp.
3515 *# - 2020-12-17 Change Fraser area to be 35.1 as measured from QGIS
3516 *# - 2020-12-17 All Fraser is undeveloped (Nashyd)
3517 *#*****|*****|
3518 CONTINUOUS NASHYD NHYD=["FRASER-DRN"], DT=[ 1] mi n, AREA=[ 13.65]( ha),
3519 DWF=[ 0]( cms), CN/C=[ 77], IA=[ 4.67]( mm),
3520 N=[ 3], TP=[ 0.4258] hrs,
3521 Continuous simulation parameters:
3522 IaRECper=[ 4]( hrs),
3523 SMN=[ -1]( mm), SMAX=[ -1]( mm), SK=[ 0.010]/( mm),
3524 InterEventTi me=[ 12]( hrs)
3525 Baseflow simulation parameters:
3526 BaseFlowOption=[ 1],
3527 InitGWResVol=[ 50]( mm), GWResK=[ 0.96]( mm/ day/ mm)
3528 VHydCond=[ 0.055]( mm/ hr), END=- 1
3529 *
3530 CONTINUOUS STANDHYD NHYD=["FRASER-D"], DT=[ 1] mi n, AREA=[ 21.61]( ha),
3531 XI MP=[ 0.585], TI MP=[ 0.585], DWF=[ 0]( cms), LOSS=[ 2],
3532 SCS curve number CN=[ 80],
3533 Pervious surfaces: IAper=[ 4.67]( mm), SLPP=[ 1]( %),
3534 LGP=[ 40]( m), MNP=[ 0.25], SCP=[ 0]( mi n),
3535 Impervious surfaces: IAi mp=[ 1.57]( mm), SLPI=[ 1]( %),
3536 LGI=[ 379.561]( m), MNI=[ 0.013], SCI=[ 0]( mi n),
3537 Continuous simulation parameters:
3538 IaRECper=[ 4]( hrs), IaRECI mp=[ 4]( hrs),
3539 SMN=[ -1]( mm), SMAX=[ -1]( mm), SK=[ 0.010]/( mm),
3540 InterEventTi me=[ 18]( hrs), END=- 1
3541 *%-----|-----|
3542 COMPUTE DUALHYD NHYDin=["FRASER-D"], CI NLET=[ 2.281]( cms), NI NLET=[ 1],
3543 Mij NHYD=["FRASER-J"]
3544 MnNHYD=["FRASER-N"]
3545 TMSTO=[ 9999999]( cu- m)
3546 *%-----|-----|
3547 ADD HYD NHYDsum=["FRASER-S"], NHYDs to add=["FRASER-J"+"FRASER-N"]
3548 *%-----|-----|
3549 *ROUTE RESERVOIR NHYDout=["MS_P20"], NHYDin=["FRASER"],
3550 * RDT=[ 1]( mi n),
3551 * TABLE of ( OUTFLOW STORAGE ) values
3552 * ( cms) - ( ha- m)
3553 * [ 0.0, 0.0 ]
3554 * [ 0.04, 0.36 ]
3555 * [ -1, -1 ] (max twenty pts)
3556 * NHYDovf=["P20-OVF"]
3557 *%-----|-----|
3558 ADD HYD NHYDsum=["4241"], NHYDs to
add=["KB-Pond3"+"S-1-B"+"FRASER-DRN"+"FRASER-S"+"N_KB"+"FC-01-S"+"FC-02-S"+"FC-03-S"]
3559 *%-----|-----|
3560 SAVE HYD NHYD=["4241"], # OF PCYCLES=[ -1], I CASEsh=[ 1]
3561 HYD_COMMENT=["Total Flows at Ken-Burnett Outlet"]
3562 *%-----|-----|
3563 *# Hydrograph from Node Ken-Burnett to station 3633
3564 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 4241
3565 *#

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3566 ROUTE CHANNEL      NHYDout=[" 4241-out "], NHYDin=[" 4241"],   RDT=[ 1](mi n),
3567                   CHLGTH=[ 294](m),   CHSLOPE=[ 0.1088](%), FPSLOPE=[ 0.1088](%),
3568                   SECNUM=[ 1.0],       NSEG=[ 3]
3569                   ( SEGROUGH, SEGDI ST (m))=[ 0.05, -20.12
3570                                     -0.035, 45.26
3571                                     0.05, 403.84] NSEG times
3572                   ( DI STANCE (m), ELEVATI ON (m))=[ ]
3573                   [-909.72, 95 ]
3574                   [-907.09, 94.5 ]
3575                   [-904.65, 94 ]
3576                   [-902.26, 93.5 ]
3577                   [-44.51, 91.5 ]
3578                   [-25.1, 91.5 ]
3579                   [-20.98, 91 ]
3580                   [-20.61, 90.5 ]
3581                   [-20.12, 90 ]
3582                   [-6.13, 87.26 ]
3583                   [17.51, 86.56 ]
3584                   [31.37, 87.2 ]
3585                   [45.26, 90 ]
3586                   [50.41, 90.5 ]
3587                   [63.06, 91 ]
3588                   [134.5, 91.5 ]
3589                   [190.63, 92 ]
3590                   [251.98, 92.5 ]
3591                   [321.32, 93.5 ]
3592                   [403.84, 95 ]
3593 *%-----|-----|
3594 ADD HYD           NHYDsum=["SN_KB"], NHYDs to
add=[" 4241-out "+"FC-04-S"+"JR-01-S"+"JR-02-S"]
3595 *%-----|-----|
3596 SAVE HYD         NHYD=["SN_KB"], # OF PCYCLES=[-1], ICASEsh=[1]
3597 HYD_COMMENT=["Total Flows before Station 3633]
3598 *%-----|-----|
3599 *# Hydrograph from Station 3633 to Node Todd
3600 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 3633
3601 *# JFSA 2021-02-26 change the channel length (at station 3633) from 650m to 608m and
change the slope from 0.0498% to 0.24671% That is because of adding station 4241
between station 4534 and station 3633
*#
3602 ROUTE CHANNEL      NHYDout=["N_TO"], NHYDin=["SN_KB"],   RDT=[ 1](mi n),
3603                   CHLGTH=[ 608](m),   CHSLOPE=[ 0.24671](%), FPSLOPE=[ 0.24671](%),
3604                   SECNUM=[ 1.0],       NSEG=[ 3]
3605                   ( SEGROUGH, SEGDI ST (m))=[ 0.05, -23.74
3606                                     -0.035, 23.74
3607                                     0.05, 26.50] NSEG times
3608                   ( DI STANCE (m), ELEVATI ON (m))=[ ]
3609                   [-29.24, 91.0
3610                   [-27.41, 90.5
3611                   [-25.64, 90
3612                   [-23.74, 89.5
3613                   [-22, 89.26
3614                   [-20, 88.51
3615                   [-19, 88.32
3616                   [-15, 88.1
3617                   [-10, 88.11
3618                   [-5, 88.17
3619                   0, 88.27
3620                   5, 88.19
3621                   10, 88.06
3622                   15, 88.48
3623                   16, 88.7
3624                   23.74, 89.5
3625                   24.68, 90
3626                   25.57, 90.5
3627                   26.50, 91.0

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3629 * [-29.24, 91]
3630 * [-27.41, 90.5]
3631 * [-25.64, 90]
3632 * [-23.74, 89.5]
3633 * [-22, 89.26]
3634 * [-20, 88.51]
3635 * [-19, 88.32]
3636 * [-15, 88.1]
3637 * [-10, 88.11]
3638 * [-5, 88.17]
3639 * [0, 88.27]
3640 * [5, 88.19]
3641 * [10, 88.06]
3642 * [15, 88.48]
3643 * [16, 88.7]
3644 * [23.74, 89.5]
3645 * [24.68, 90]
3646 * [25.57, 90.5]
3647 *%-----|-----|
3648 *#*****|
3649 *# Catchment Greenbank
3650 *# - To Greenbank Drain (south of the Jock)
3651 *# - JFSA 2021-01-18 add Greenbank pond as per JFSA, P598(06)-15, June 2016
3652 *# - JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GIS measurements
3653 *#*****|
3654 CONTINUOUS STANDHYD NHYD=["Greenbank"], DT=[1] min, AREA=[36.6] (ha),
3655 XI MP=[0.639], TI MP=[0.682], DWF=[0] (cms), LOSS=[2],
3656 SCS curve number CN=[77],
3657 Pervious surfaces: I A per=[4.67] (mm), SLPP=[1] (%),
3658 LGP=[40] (m), MNP=[0.25], SCP=[0] (min),
3659 Impervious surfaces: I A i mp=[1.57] (mm), SLPI=[1] (%),
3660 LGI=[493.96] (m), MNI=[0.013], SCI=[0] (min),
3661 Continuous simulation parameters:
3662 I a REC per=[4] (hrs), I a REC i mp=[4] (hrs),
3663 S M N=[-1] (mm), S M A X=[-1] (mm), S K=[0.010] / (mm),
3664 I n t e r E v e n t T i m e=[18] (hrs), E N D=-1
3665 *%-----|-----|
3666 ROUTE RESERVOIR NHYDout=["GreenB_MN"], NHYDin=["Greenbank"],
3667 RDT=[1] (min),
3668 TABLE of ( OUTFLOW STORAGE ) values
3669 ( cms ) - ( ha-m )
3670 [ 0.0 , 0.0 ]
3671 [ 0.033 , 0.084 ]
3672 [ 0.039 , 0.201 ]
3673 [ 0.113 , 0.292 ]
3674 [ 0.237 , 0.386 ]
3675 [ 0.382 , 0.484 ]
3676 [ 0.539 , 0.585 ]
3677 [ 0.7 , 0.692 ]
3678 [ 0.86 , 0.804 ]
3679 [ 4.684 , 0.922 ]
3680 [ 11.539 , 1.052 ]
3681 [ 20.867 , 1.168 ]
3682 [ 103.616 , 1.974 ]
3683 [ -1 , -1 ] (max twenty pts)
3684 NHYDovf=["GreenB_M"],
3685 *%-----|-----|
3686 *%-----|-----|
3687 ADD HYD NHYDsum=["GreenB"], NHYDs to add=["N_TO"+"GreenB_M"+"GreenB_MN"]
3688 *%-----|-----|
3689 SAVE HYD NHYD=["GreenB"], # OF PCYCLES=[-1], I CASEs h=[1]
3690 HYD_COMMENT=["Total Flows at Greenbank Drain"]
3691 *%-----|-----|
3692 *#*****|
3693 *# Catchment TODD
3694 *# - To Todd Drain (south of the Jock)

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3695 *# - Subdivision with 43% imp. as per Barrhaven South M5S
3696 *# - 2020-11-30 increase imp. based on P598(04)-11
3697 *# - 2020-11-30 update TODD Tributary Drainage Area to = 146.015 ha based on
P598(04)-11
3698 *# - 2020-11-30 split TODD Drainage Area to MAJOR, MINOR, POND and ALL
3699 *#*****
3700 *# - JFSA 2021-01-19 add "TODD_MN1" as part of Clarke("W_CLAR_M") and remove it
from Todd
3701 *CONTINUOUS STANDHYD NHYD=["TODD_MN1"], DT=[1] min, AREA=[1.772](ha),
3702 * XI MP=[0.53], TI MP=[0.57], DWF=[0](cms), LOSS=[2],
3703 * SCS curve number CN=[77],
3704 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3705 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3706 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3707 * LGI=[108.689](m), MNI=[0.013], SCI=[0](min),
3708 * Continuous simulation parameters:
3709 * IaRECper=[4](hrs), IaRECImp=[4](hrs),
3710 * SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3711 * InterEventTime=[18](hrs), END=-1
3712 *%-----|-----
3713 CONTINUOUS STANDHYD NHYD=["TODD_MN2"], DT=[1] min, AREA=[2.1](ha),
3714 * XI MP=[0.53], TI MP=[0.57], DWF=[0](cms), LOSS=[2],
3715 * SCS curve number CN=[77],
3716 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3717 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3718 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3719 * LGI=[118.322](m), MNI=[0.013], SCI=[0](min),
3720 * Continuous simulation parameters:
3721 * IaRECper=[4](hrs), IaRECImp=[4](hrs),
3722 * SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3723 * InterEventTime=[18](hrs), END=-1
3724 *%-----|-----
3725 CONTINUOUS STANDHYD NHYD=["TODD_MN3"], DT=[1] min, AREA=[0.117](ha),
3726 * XI MP=[0.53], TI MP=[0.57], DWF=[0](cms), LOSS=[2],
3727 * SCS curve number CN=[77],
3728 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3729 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3730 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3731 * LGI=[27.928](m), MNI=[0.013], SCI=[0](min),
3732 * Continuous simulation parameters:
3733 * IaRECper=[4](hrs), IaRECImp=[4](hrs),
3734 * SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3735 * InterEventTime=[18](hrs), END=-1
3736 *%-----|-----
3737 CONTINUOUS STANDHYD NHYD=["TODD_M"], DT=[1] min, AREA=[30.230](ha),
3738 * XI MP=[0.52], TI MP=[0.64], DWF=[0](cms), LOSS=[2],
3739 * SCS curve number CN=[77],
3740 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3741 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3742 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3743 * LGI=[448.925](m), MNI=[0.013], SCI=[0](min),
3744 * Continuous simulation parameters:
3745 * IaRECper=[4](hrs), IaRECImp=[4](hrs),
3746 * SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3747 * InterEventTime=[18](hrs), END=-1
3748 *%-----|-----
3749 * -JFSA 2021-01-19 update "TODD_ALL" area from 108.741 ha to 112.908 ha based on
GIS measurements (148.41-30.23-0.117-2.1-3.055=112.908 ha)
3750 CONTINUOUS STANDHYD NHYD=["TODD_ALL"], DT=[1] min, AREA=[112.908](ha),
3751 * XI MP=[0.52], TI MP=[0.57], DWF=[0](cms), LOSS=[2],
3752 * SCS curve number CN=[77],
3753 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3754 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3755 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3756 * LGI=[867.594](m), MNI=[0.013], SCI=[0](min),
3757 * Continuous simulation parameters:

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3758 IaREcper=[ 4](hr s), IaREcImp=[ 4](hr s),
3759 SMN=[ - 1](mm), SMAX=[ - 1](mm), SK=[ 0.010]/(mm),
3760 InterEventTime=[ 18](hr s), END=- 1
3761 *%-----|-----
3762 CONTINUOUS STANDHYD NHYD=[" TODD_P"], DT=[ 1]mi n, AREA=[ 3.055](ha),
3763 XI MP=[ 0.63], TI MP=[ 0.63], DWF=[ 0](cms), LOSS=[ 2],
3764 SCS curve number CN=[ 77],
3765 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
3766 LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](mi n),
3767 Impervious surfaces: IAi mp=[ 1.57](mm), SLPI =[ 1](%),
3768 LGI =[ 142.712](m), MNI =[ 0.013], SCI =[ 0](mi n),
3769 Continuous simulation parameters:
3770 IaREcper=[ 4](hr s), IaREcImp=[ 4](hr s),
3771 SMN=[ - 1](mm), SMAX=[ - 1](mm), SK=[ 0.010]/(mm),
3772 InterEventTime=[ 18](hr s), END=- 1
3773 *%-----|-----
3774 *%-----|-----
3775 * -JFSA 2021-02-23 "TODD_DEVL" is part of the Corrigan sub-catchment because it
drains to Corrigan SWM as per geoOttawa.ca Feb. 2021. "TODD_DEVL" now is called "corr1"
and its parameters remain the same.
3776 *CONTINUOUS STANDHYD NHYD=[" TODD_DEVL"], DT=[ 1]mi n, AREA=[ 15.87](ha),
3777 * XI MP=[ 0.63], TI MP=[ 0.63], DWF=[ 0](cms), LOSS=[ 2],
3778 * SCS curve number CN=[ 77],
3779 * Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
3780 * LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](mi n),
3781 * Impervious surfaces: IAi mp=[ 1.57](mm), SLPI =[ 1](%),
3782 * LGI =[ 325.27](m), MNI =[ 0.013], SCI =[ 0](mi n),
3783 * Continuous simulation parameters:
3784 * IaREcper=[ 4](hr s), IaREcImp=[ 4](hr s),
3785 * SMN=[ - 1](mm), SMAX=[ - 1](mm), SK=[ 0.010]/(mm),
3786 * InterEventTime=[ 18](hr s), END=- 1
3787 *%-----|-----
3788 * -JFSA 2021-02-23 "TODD_UnD" is part of the Corrigan sub-catchment. "TODD_UnD" now
is called "corr2" and its parameters remain the same.
3789 *CONTINUOUS NASHYD NHYD=[" TODD_UnD"], DT=[ 1]mi n, AREA=[ 12.47](ha),
3790 * DWF=[ 0](cms), CN C=[ 77], IA=[ 4.67](mm),
3791 * N=[ 3], TP=[ 1.10]hr s,
3792 * Continuous simulation parameters:
3793 * IaREcper=[ 4](hr s),
3794 * SMN=[ - 1](mm), SMAX=[ - 1](mm), SK=[ 0.010]/(mm),
3795 * InterEventTime=[ 12](hr s)
3796 * Baseflow simulation parameters:
3797 * BaseFlowOption=[ 1],
3798 * InitGWResVol =[ 50](mm), GWResK=[ 0.96](mm/ day/ mm)
3799 * VHydCond=[ 0.055](mm/ hr), END=- 1
3800 *%-----|-----
3801 *# 5- Year + 12% Capture
3802 *COMPUTE DUALHYD NHYDin=[" TODD_M"], CINLET=[ 3.314](cms), NINLET=[ 1],
3803 * Mj NHYD=[" TODD_Mj"]
3804 * MnNHYD=[" TODD_Mn"]
3805 * TMSTO=[ 0.1](cu- m)
3806 ROUTE RESERVOIR NHYDout=[" TODD_Mn"], NHYDin=[" TODD_M"],
3807 RDT=[ 1](mi n),
3808 TABLE of ( OUTFLOW STORAGE ) values
3809 ( cms ) - ( ha- m)
3810 [ 0.0 , 0.0 ]
3811 [ 3.314 , 0.0001 ]
3812 [ - 1 , - 1 ] (max twenty pts)
3813 NHYDovf=[" TODD_Mj"],
3814 *%-----|-----
3815 *# 5- Year + 12% Capture
3816 *COMPUTE DUALHYD NHYDin=[" TODD_MN1"], CINLET=[ 0.227](cms), NINLET=[ 1],
3817 * Mj NHYD=[" TODD_MN1j"]
3818 * MnNHYD=[" TODD_MN1n"]
3819 * TMSTO=[ 0.1](cu- m)
3820 *ROUTE RESERVOIR NHYDout=[" TODD_MN1n"], NHYDin=[" TODD_MN1"],

```

```

3821 *          RDT=[ 1](mi n),
3822 *          TABLE of ( OUTFLOW STORAGE ) values
3823 *                ( cms ) - ( ha- m)
3824 *                [ 0.0 , 0.0 ]
3825 *                [ 0.227 , 0.0001 ]
3826 *                [ -1 , -1 ] (max t went y pts)
3827 *          NHYDovf=[ "TODD_MN1j" ] ,
3828 *%-----|-----|
3829 *COMPUTE DUALHYD  NHYDi n=[ "TODD_MN2" ], CI NLET=[ 0.268]( cms ), NI NLET=[ 1],
3830 *                Mj NHYD=[ "TODD_MN2j" ]
3831 *                MnNHYD=[ "TODD_MN2n" ]
3832 *                TM STO=[ 0.1]( cu- m)
3833 ROUTE RESERVOIR NHYDout =[ "TODD_MN2n" ] , NHYDi n=[ "TODD_MN2" ] ,
3834 RDT=[ 1](mi n),
3835          TABLE of ( OUTFLOW STORAGE ) values
3836                ( cms ) - ( ha- m)
3837                [ 0.0 , 0.0 ]
3838                [ 0.268 , 0.0001 ]
3839                [ -1 , -1 ] (max t went y pts)
3840          NHYDovf=[ "TODD_MN2j" ] ,
3841 *%-----|-----|
3842 *COMPUTE DUALHYD  NHYDi n=[ "TODD_MN3" ], CI NLET=[ 0.016]( cms ), NI NLET=[ 1],
3843 *                Mj NHYD=[ "TODD_MN3j" ]
3844 *                MnNHYD=[ "TODD_MN3n" ]
3845 *                TM STO=[ 0.1]( cu- m)
3846 ROUTE RESERVOIR NHYDout =[ "TODD_MN3n" ] , NHYDi n=[ "TODD_MN3" ] ,
3847 RDT=[ 1](mi n),
3848          TABLE of ( OUTFLOW STORAGE ) values
3849                ( cms ) - ( ha- m)
3850                [ 0.0 , 0.0 ]
3851                [ 0.016 , 0.0001 ]
3852                [ -1 , -1 ] (max t went y pts)
3853          NHYDovf=[ "TODD_MN3j" ] ,
3854 *%-----|-----|
3855 *          -JFSA 2021-01-19 move A2 from Corrigan sub-catchment to Todd sub-catchment so the
major system from A2 can be added to Todd
3856 CONTINUOUS STANDHYD NHYD=[ "A2" ], DT=[ 1]mi n, AREA=[ 25.5]( ha),
3857 XI MP=[ 0.42], TI MP=[ 0.52], DWF=[ 0]( cms ), LOSS=[ 2],
3858 SCS curve number CN=[ 75],
3859 Pervious surfaces: I Aper=[ 4.67]( mm), SLPP=[ 1]( %),
3860                LGP=[ 40]( m), MNP=[ 0.25], SCP=[ 0]( mi n),
3861 Imper vious surfaces: I Ai mp=[ 1.57]( mm), SLPI =[ 1]( %),
3862                LGI =[ 566]( m), MNI =[ 0.013], SCI =[ 0]( mi n),
3863 Continuous simulation parameters:
3864 I aRECper=[ 4]( hrs), I aRECI mp=[ 4]( hrs),
3865 SM N=[ -1]( mm), SMAX=[ -1]( mm), SK=[ 0.010]/( mm),
3866 I nterEvent Ti me=[ 18]( hrs), END=- 1
3867 *%-----|-----|
3868 COMPUTE DUALHYD  NHYDi n=[ "A2" ], CI NLET=[ 1.818]( cms ), NI NLET=[ 1],
3869 Mj NHYD=[ "A2- M" ]
3870 MnNHYD=[ "A2- MN" ]
3871 TM STO=[ 924]( cu- m)
3872 *%-----|-----|
3873 ADD HYD          NHYDs um=[ "TODD" ], NHYDs to
add=[ "TODD_MN2n"+"TODD_MN3n"+"TODD_Mj"+"TODD_P"+"TODD_ALL"+"W_CLAR_Mn" ]
3874 *%-----|-----|
3875 SAVE HYD        NHYD=[ "TODD" ], # OF PCYCLES=[ -1], I CASEs h=[ 1]
3876 HYD_COMMENT=[ "Tot al Fl ows at Todd Dr ai n" ]
3877 *%-----|-----|
3878 *#*****|*****|
3879 *# Todd Pond 3
3880 *# - Rating curve obtained from Barrhaven South M5S modeling
3881 *# - stantec 2007, Tributary Drainage Area to M5S Pond 3 = 193 ha
3882 *#*****|*****|
3883 ROUTE RESERVOIR NHYDout =[ "M5_P3" ], NHYDi n=[ "TODD" ],
3884 RDT=[ 1](mi n),

```

3885 TABLE of (OUTFLOW STORAGE) values
 3886 (cms) - (ha - m)
 3887 [0.0 , 0.0]
 3888 [0.014 , 0.155]
 3889 [0.048 , 0.394]
 3890 [0.061 , 0.56]
 3891 [0.08 , 0.909]
 3892 [0.088 , 1.089]
 3893 [0.109 , 1.652]
 3894 [0.118 , 1.952]
 3895 [0.122 , 2.099]
 3896 [1.972 , 2.269]
 3897 [9.135 , 2.598]
 3898 [15.608 , 2.826]
 3899 [19.256 , 2.942]
 3900 [27.282 , 3.181]
 3901 [40.957 , 3.55]
 3902 [56.372 , 3.929]
 3903 [73.349 , 4.317]
 3904 [85.469 , 4.579]
 3905 [104.771 , 4.977]
 3906 [-1 , -1] (max twenty pts)

3907 NHYDovf=["P3- OVF"]

3908 *%-----|-----|

3909 ADD HYD NHYDs um=["SN_TO"], NHYDs to
 add=["GreenB"+"MS_P3"+"P3- OVF"+"TODD_MN2j"+"A2- M"]

3910 *%-----|-----|

3911 SAVE HYD NHYD=["SN_TO"], # OF PCYCLES=[-1], I CASEs h=[1]
 3912 HYD_COMMENT=["Total Flows at Todd Drain"]

3913 *%-----|-----|

3914 *#

3915 *# Hydrograph from Todd Drain routed to Corrigan Drain
 3916 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
 3917 *# 2021-02-19 Change the slope from 0.033 % (as per Stantec Report 2007) to 0.05 % so
 the model will be more stable and give reasonable results. It is justifiable as ROUTE
 CHANNELs aren't well suited to really flat slopes.

3918 *

3919 ROUTE CHANNEL NHYDout=["N_TO"] , NHYDin=["SN_TO"] ,
 3920 RDT=[1] (min),
 3921 CHLGTH=[280] (m), CHSLOPE=[0.05] (%),
 3922 FPSLOPE=[0.05] (%),
 3923 SECNUM=[1.0] , NSEG=[3]
 3924 (SEGROUGH, SEGDI ST (m)) =
 3925 [0.075, -17.72
 3926 -0.045, 17.72
 3927 0.075, 80.62] NSEG times
 3928 (DI STANCE (m), ELEVATI ON (m)) =
 3929 [-83.32, 90.00]
 3930 [-81.36, 89.50]
 3931 [-79.12, 89.00]
 3932 [-76.13, 88.50]
 3933 [-20.46, 88.00]
 3934 [-19.36, 87.50]
 3935 [-18.51, 87.00]
 3936 [-17.72, 86.50]
 3937 [-11.95, 85.24]
 3938 [-0.11, 85.12]
 3939 [11.49, 85.20]
 3940 [17.72, 86.50]
 3941 [19.74, 87.00]
 3942 [21.22, 87.50]
 3943 [22.68, 88.00]
 3944 [24.28, 88.50]
 3945 [26.79, 89.00]
 3946 [71.98, 90.00]
 3947 [80.62, 90.50]


```

3948 *%-----|-----|
3949 SAVE HYD          NHYD=["N_TO"], # OF PCYCLES=[-1], ICASEsh=[1]
3950                  HYD_COMMENT=["Total inflows at Station 2462"]
3951 *%-----|-----|
3952 *#*****|-----|
3953 *#    Catchment CORRIG
3954 *#    - To Corrigan Drain (south of the Jock)
3955 *#    - Primarily Developed (medium density)
3956 *#    - JFSA JAN 2021, add Corrigan subcatchments as per IBI, July 2008
3957 *#*****|-----|
3958 *ROUTE RESERVOIR  NHYDout=["MS_P1"], NHYDin=["CORRIG"],
3959 *                  RDT=[1](min),
3960 *                  TABLE of ( OUTFLOW STORAGE ) values
3961 *                  (cms) - (ha-m)
3962 *                  [ 0.0 , 0.0 ]
3963 *                  [ 0.06 , 0.58]
3964 *                  [ -1 , -1 ] (max twenty pts)
3965 *                  NHYDovf=["P1-OVF"]
3966 *%-----|-----|
3967 *ADD HYD          NHYDsum=["SN_CO"], NHYDs to add=["N_TO"+"P1-OVF"+"MS_P1"]
3968 *%-----|-----|
3969 *SAVE HYD        NHYD=["SN_CO"], # OF PCYCLES=[-1], ICASEsh=[1]
3970 *                  HYD_COMMENT=["Total Flows at Corrigan Drain"]
3971 *%-----|-----|
3972 *    -JFSA 2021-02-23 "TODD_DEVL" is part of the Corrigan sub-catchment because it
drains to Corrigan SWM as per geoOttawa.ca Feb. 2021. "TODD_DEVL" now is called "corr1"
and its parameters remain the same.

3973 CONTINUOUS STANDHYD NHYD=["corr1"], DT=[1]min, AREA=[15.87](ha),
3974 XI MP=[0.63], TI MP=[0.63], DWF=[0](cms), LOSS=[2],
3975 SCS curve number CN=[77],
3976 Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3977 LGP=[40](m), MNP=[0.25], SCP=[0](min),
3978 Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3979 LGI=[325.27](m), MNI=[0.013], SCI=[0](min),
3980 Continuous simulation parameters:
3981 IARECper=[4](hrs), IARECimp=[4](hrs),
3982 SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3983 InterEventTime=[18](hrs), END=-1
3984 *%-----|-----|
3985 *    -JFSA 2021-02-23 add DUALHYD for "corr1". "corr1" DUALHYD Parameters are the
same as A2 DUALHYD Parameters because A2 is the nearest sub-catchment to "corr1".
3986 *    At the same time, Corrigan Report, IBI group 2008 has no DUALHYD Parameters for
Al-Corrig
3987 COMPUTE DUALHYD  NHYDin=["corr1"], CNLET=[1.818](cms), NI NLET=[1],
3988 Maj NHYD=["corr1-M"]
3989 MnNHYD=["corr1-MN"]
3990 TM STO=[924](cu-m)
3991 *%-----|-----|
3992 *    -JFSA 2021-02-23 "TODD_UnD" is part of the Corrigan sub-catchment. "TODD_UnD" now
is called "corr2" and its parameters remain the same.

3993 CONTINUOUS NASHYD  NHYD=["corr2"], DT=[1]min, AREA=[12.47](ha),
3994 DWF=[0](cms), CN C=[77], IA=[4.67](mm),
3995 N=[3], TP=[1.10]hrs,
3996 Continuous simulation parameters:
3997 IARECper=[4](hrs),
3998 SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3999 InterEventTime=[12](hrs)
4000 Baseflow simulation parameters:
4001 BaseFlowOption=[1],
4002 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
4003 VHydCond=[0.055](mm/hr), END=-1
4004 *%-----|-----|
4005 *    -JFSA 2021-01-19 change Al-Corrig to be developed as per geottawa website and
apply the parameters of A2, the nearest sub-catchment to Al-Corrig, LGI is calculated
based on Al-Corrig area
4006 *    -JFSA 2021-01-19 update all Corrigan areas based on GIS measurements, and keep

```

LGI as it is from Corrigan Report, IBI Group, 2008 because LGI calculated is less than LGI from the Corrigan Report

```
4007 CONTINUOUS STANDHYD NHYD=["Al-Corrig"], DT=[1] min, AREA=[15.75](ha),
4008 XI MP=[0.42], TI MP=[0.52], DWF=[0](cms), LOSS=[2],
4009 SCS curve number CN=[75],
4010 Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
4011 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4012 Impervious surfaces: I A i mp=[1.57](mm), SLPI=[1](%),
4013 LGI=[324.037](m), MNI=[0.013], SCI=[0](min),
4014 Continuous simulation parameters:
4015 I a REC per=[4](hrs), I a REC i mp=[4](hrs),
4016 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4017 Inter Event Time=[18](hrs), END=-1
4018 *
4019 * -JFSA 2021-01-25 add DUALHYD for Al-Corrig. Al-Corrig DUALHYD Parameters are the
same as A2 DUALHYD Parameters because A2 is the nearest sub-catchment to Al-Corrig.
4020 * At the same time, Corrigan Report, IBI group 2008 has no DUALHYD Parameters for
Al-Corrig
4021 COMPUTE DUALHYD NHYD i n=["Al-Corrig"], CI NLET=[1.818](cms), NI NLET=[1],
4022 M a j NHYD=["Al-M"]
4023 M n NHYD=["Al-MN"]
4024 TM I STO=[924](cu-m)
4025 *%-----|-----|
4026 *CONTINUOUS NASHYD NHYD=["Al-Corrig"], DT=[1] min, AREA=[15.75](ha),
4027 * DWF=[0](cms), CN C=[66], I A=[2.5](mm),
4028 * N=[3.0], TP=[0.36] hrs,
4029 * Continuous simulation parameters:
4030 * I a REC per=[4](hrs),
4031 * SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4032 * Inter Event Time=[12](hrs)
4033 * Baseflow simulation parameters:
4034 * BaseFl owOpt ion=[1],
4035 * Ini t GWRes Vol =[50](mm), GWRes K=[0.96](mm/day/mm)
4036 * VHydCond=[0.055](mm/hr), END=-1
4037 *%-----|-----|
4038 CONTINUOUS NASHYD NHYD=["B1"], DT=[1] min, AREA=[2.77](ha),
4039 DWF=[0](cms), CN C=[56], I A=[2.5](mm),
4040 N=[3.0], TP=[0.23] hrs,
4041 Continuous simulation parameters:
4042 I a REC per=[4](hrs),
4043 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4044 Inter Event Time=[12](hrs)
4045 Baseflow simulation parameters:
4046 BaseFl owOpt ion=[1],
4047 Ini t GWRes Vol =[50](mm), GWRes K=[0.96](mm/day/mm)
4048 VHydCond=[0.055](mm/hr), END=-1
4049 *%-----|-----|
4050 CONTINUOUS STANDHYD NHYD=["A4"], DT=[1] min, AREA=[1.27](ha),
4051 XI MP=[0.65], TI MP=[0.65], DWF=[0](cms), LOSS=[2],
4052 SCS curve number CN=[75],
4053 Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
4054 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4055 Impervious surfaces: I A i mp=[1.57](mm), SLPI=[1](%),
4056 LGI=[253](m), MNI=[0.013], SCI=[0](min),
4057 Continuous simulation parameters:
4058 I a REC per=[4](hrs), I a REC i mp=[4](hrs),
4059 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4060 Inter Event Time=[18](hrs), END=-1
4061 *%-----|-----|
4062 COMPUTE DUALHYD NHYD i n=["A4"], CI NLET=[0.405](cms), NI NLET=[1],
4063 M a j NHYD=["A4-M"]
4064 M n NHYD=["A4-MN"]
4065 TM I STO=[68](cu-m)
4066 *%-----|-----|
4067 ADD HYD NHYDs um=["MH101"], NHYDs to
add=["Al-M"+"Al-MN"+"corr1-M"+"corr1-MN"+"corr2"+"B1"+"A4-MN"]
```

```

4068 *%-----|-----|
4069 SAVE HYD      NHYD=["MHI01"], # OF PCYCLES=[ - 1], I CASEs h=[ 1]
4070              HYD_COMMENT=["Tot al Fl ows at MHI01"]
4071 *%-----|-----|
4072 ROUTE PIPE    PTYPE=[ 1] circ, NHYDout=[" 101- 102"], RNUMBER=[ 1. 0], PDI AM=[ 1050] ( mm),
4073              PLNGTH=[ 368] ( m), PROUGH=[ 0. 013], PSLOPE=[ 0. 0054] ( m/ m),
              NHYDin=["MHI01"], RDT=[ 1]
4074 *%-----|-----|
4075 *      -JFSA 2021-01-19 move A2 from Corrigan sub-catchment to Todd sub-catchment so the
major system from A2 can be added to Todd
4076 *CONTINUOUS STANDHYD NHYD=["A2"], DT=[ 1] mi n, AREA=[ 25. 5] ( ha),
4077 *              XI MP=[ 0. 42], TI MP=[ 0. 52], DWF=[ 0] ( cms), LOSS=[ 2],
4078 *              SCS curve number CN=[ 75],
4079 *              Pervious surfaces: I A per=[ 4. 67] ( mm), SLPP=[ 1] ( %),
4080 *              LGP=[ 40] ( m), MNP=[ 0. 25], SCP=[ 0] ( mi n),
4081 *              Impervious surfaces: I A i mp=[ 1. 57] ( mm), SLPI =[ 1] ( %),
4082 *              LGI =[ 566] ( m), MNI =[ 0. 013], SCI =[ 0] ( mi n),
4083 *              Continuous simulation parameters:
4084 *              I a REC per=[ 4] ( hr s), I a REC i mp=[ 4] ( hr s),
4085 *              SM N=[ - 1] ( mm), SMAX=[ - 1] ( mm), SK=[ 0. 010] / ( mm),
4086 *              Inter Event Ti me=[ 18] ( hr s), END=- 1
4087 *%-----|-----|
4088 *COMPUTE DUALHYD  NHYDin=["A2"], CI NLET=[ 1. 818] ( cms), NI NLET=[ 1],
4089 *              M a j NHYD=["A2- M"]
4090 *              M nNHYD=["A2- MN"]
4091 *              TM STO=[ 924] ( cu- m)
4092 *%-----|-----|
4093 ADD HYD       NHYDs um=["MHI02"], NHYDs to add=["A2- MN"+"101- 102"]
4094 *%-----|-----|
4095 SAVE HYD      NHYD=["MHI02"], # OF PCYCLES=[ - 1], I CASEs h=[ 1]
4096              HYD_COMMENT=["Tot al Fl ows at MHI02"]
4097 *%-----|-----|
4098 CONTINUOUS STANDHYD NHYD=["A5"], DT=[ 1] mi n, AREA=[ 1. 6] ( ha),
4099 *              XI MP=[ 0. 71], TI MP=[ 0. 71], DWF=[ 0] ( cms), LOSS=[ 2],
4100 *              SCS curve number CN=[ 75],
4101 *              Pervious surfaces: I A per=[ 4. 67] ( mm), SLPP=[ 1] ( %),
4102 *              LGP=[ 40] ( m), MNP=[ 0. 25], SCP=[ 0] ( mi n),
4103 *              Impervious surfaces: I A i mp=[ 1. 57] ( mm), SLPI =[ 1] ( %),
4104 *              LGI =[ 300] ( m), MNI =[ 0. 013], SCI =[ 0] ( mi n),
4105 *              Continuous simulation parameters:
4106 *              I a REC per=[ 4] ( hr s), I a REC i mp=[ 4] ( hr s),
4107 *              SM N=[ - 1] ( mm), SMAX=[ - 1] ( mm), SK=[ 0. 010] / ( mm),
4108 *              Inter Event Ti me=[ 18] ( hr s), END=- 1
4109 *%-----|-----|
4110 ADD HYD       NHYDs um=["A5T"], NHYDs to add=["A4- M"+"A5"]
4111 *%-----|-----|
4112 COMPUTE DUALHYD  NHYDin=["A5T"], CI NLET=[ 0. 357] ( cms), NI NLET=[ 1],
4113 *              M a j NHYD=["A5- M"]
4114 *              M nNHYD=["A5- MN"]
4115 *              TM STO=[ 60] ( cu- m)
4116 *%-----|-----|
4117 *      -JFSA Jan. 2021, A3 is a part of Todd so it is removed
4118 *      -JFSA Jan. 2021, "A2- M" added to "Todd"
4119 *CONTINUOUS STANDHYD NHYD=["A3"], DT=[ 1] mi n, AREA=[ 18. 4] ( ha),
4120 *              XI MP=[ 0. 58], TI MP=[ 0. 65], DWF=[ 0] ( cms), LOSS=[ 2],
4121 *              SCS curve number CN=[ 75],
4122 *              Pervious surfaces: I A per=[ 4. 67] ( mm), SLPP=[ 1] ( %),
4123 *              LGP=[ 40] ( m), MNP=[ 0. 25], SCP=[ 0] ( mi n),
4124 *              Impervious surfaces: I A i mp=[ 1. 57] ( mm), SLPI =[ 1] ( %),
4125 *              LGI =[ 450] ( m), MNI =[ 0. 013], SCI =[ 0] ( mi n),
4126 *              Continuous simulation parameters:
4127 *              I a REC per=[ 4] ( hr s), I a REC i mp=[ 4] ( hr s),
4128 *              SM N=[ - 1] ( mm), SMAX=[ - 1] ( mm), SK=[ 0. 010] / ( mm),
4129 *              Inter Event Ti me=[ 18] ( hr s), END=- 1
4130 *%-----|-----|
4131 *ADD HYD       NHYDs um=["A3- A2M"], NHYDs to add=["A2- M"+"A3"]

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```

4132 *%-----|-----|
4133 *COMPUTE DUALHYD   NHYDin=[" A3- A2M"], CI NLET=[ 2.208](cms), NI NLET=[ 1],
4134 *                   Mj NHYD=[" A3R- M"]
4135 *                   MnNHYD=[" A3R- MN"]
4136 *                   TM STO=[ 908](cu-m)
4137 *%-----|-----|
4138 ROUTE PIPE         PTYPE=[ 1]circ, NHYDout=[" 102- 103"], RNUMBER=[ 1.0], PDI AM=[ 1500](mm),
4139                   PLNGTH=[ 504](m), PROUGH=[ 0.013], PSLOPE=[ 0.0028](m/m),
                   NHYDin=[" MHI02"], RDT=[ 1]
4140 *%-----|-----|
4141 ADD HYD            NHYDsum=[" MHI03"], NHYDs to add=[" 102- 103"+" A5- MN"]
4142 *%-----|-----|
4143 SAVE HYD          NHYD=[" MHI03"], # OF PCYCLES=[ -1], I CASEs h=[ 1]
4144                   HYD_COMMENT=[" Total Flows at MHI03"]
4145 *%-----|-----|
4146 ROUTE PIPE         PTYPE=[ 1]circ, NHYDout=[" 103- 104"], RNUMBER=[ 1.0], PDI AM=[ 1650](mm),
4147                   PLNGTH=[ 438](m), PROUGH=[ 0.013], PSLOPE=[ 0.0046](m/m),
                   NHYDin=[" MHI03"], RDT=[ 1]
4148 *%-----|-----|
4149 CONTINUOUS STANDHYD NHYD=[" A6"], DT=[ 1]min, AREA=[ 1.56](ha),
4150                   XI MP=[ 0.71], TI MP=[ 0.71], DWF=[ 0](cms), LOSS=[ 2],
4151                   SCS curve number CN=[ 75],
4152                   Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
4153                   LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4154                   Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 1](%),
4155                   LGI=[ 280](m), MNI=[ 0.013], SCI=[ 0](min),
4156                   Continuous simulation parameters:
4157                   IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
4158                   SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4159                   InterEventTime=[ 18](hrs), END=- 1
4160 *%-----|-----|
4161 ADD HYD            NHYDsum=[" A6T"], NHYDs to add=[" A5- M"+" A6"]
4162 *%-----|-----|
4163 COMPUTE DUALHYD   NHYDin=[" A6T"], CI NLET=[ 0.357](cms), NI NLET=[ 1],
4164 *                   Mj NHYD=[" A6- M"]
4165 *                   MnNHYD=[" A6- MN"]
4166 *                   TM STO=[ 60](cu-m)
4167 *%-----|-----|
4168 * -JFSA Jan. 2021, A7-corrig is a part of Todd so it is removed
4169 *CONTINUOUS STANDHYD NHYD=[" A7-corrig"], DT=[ 1]min, AREA=[ 11.8](ha),
4170 *                   XI MP=[ 0.41], TI MP=[ 0.54], DWF=[ 0](cms), LOSS=[ 2],
4171 *                   SCS curve number CN=[ 75],
4172 *                   Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
4173 *                   LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4174 *                   Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 1](%),
4175 *                   LGI=[ 438](m), MNI=[ 0.013], SCI=[ 0](min),
4176 *                   Continuous simulation parameters:
4177 *                   IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
4178 *                   SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4179 *                   InterEventTime=[ 18](hrs), END=- 1
4180 *%-----|-----|
4181 *ADD HYD            NHYDsum=[" A7- A3RM"], NHYDs to add=[" A3R- M"+" A7-corrig"]
4182 *%-----|-----|
4183 *COMPUTE DUALHYD   NHYDin=[" A7- A3RM"], CI NLET=[ 1.003](cms), NI NLET=[ 1],
4184 *                   Mj NHYD=[" A7R- M"]
4185 *                   MnNHYD=[" A7R- MN"]
4186 *                   TM STO=[ 496](cu-m)
4187 *%-----|-----|
4188 ADD HYD            NHYDsum=[" MHI04"], NHYDs to add=[" A6- MN"+" 103- 104"+" TODD_Mn"]
4189 *%-----|-----|
4190 SAVE HYD          NHYD=[" MHI04"], # OF PCYCLES=[ -1], I CASEs h=[ 1]
4191                   HYD_COMMENT=[" Total Flows at MHI04"]
4192 *%-----|-----|
4193 CONTINUOUS STANDHYD NHYD=[" B2"], DT=[ 1]min, AREA=[ 12.31](ha),
4194                   XI MP=[ 0.41], TI MP=[ 0.54], DWF=[ 0](cms), LOSS=[ 2],
4195                   SCS curve number CN=[ 75],

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4196          Pervious surfaces: I A per=[ 4.67](mm), SLPP=[ 1](%),
4197          LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4198          Impervious surfaces: I A i mp=[ 1.57](mm), SLPI=[ 1](%),
4199          LGI=[ 417](m), MNI=[ 0.013], SCI=[ 0](min),
4200          Continuous simulation parameters:
4201          I a RE C per=[ 4](hrs), I a RE C i mp=[ 4](hrs),
4202          SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4203          Inter Event Ti me=[ 18](hrs), END=- 1
4204  *%-----|
4205  COMPUTE DUALHYD          NHYD i n=[ "B2"], CI NLET=[ 1.029](cms), NI NLET=[ 1],
4206          M a j NHYD=[ "B2- M "]
4207          M n NHYD=[ "B2- MN"]
4208          TM I STO=[ 508](cu-m)
4209  *%-----|
4210  ROUTE PI PE          PTYPE=[ 1]circ, NHYDout=[ "315-333"], RNUMBER=[ 1.0], PDI AM=[ 1200](mm),
4211          PLNGTH=[ 254](m), PROUGH=[ 0.013], PSLOPE=[ 0.001](m/m),
          NHYD i n=[ "B2- MN"], RDT=[ 1]
4212  *%-----|
4213  CONTINUOUS STANDHYD          NHYD=[ "B3"], DT=[ 1]min, AREA=[ 5.59](ha),
4214          XI MP=[ 0.41], TI MP=[ 0.54], DWF=[ 0](cms), LOSS=[ 2],
4215          SCS curve number CN=[ 75],
4216          Pervious surfaces: I A per=[ 4.67](mm), SLPP=[ 1](%),
4217          LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4218          Impervious surfaces: I A i mp=[ 1.57](mm), SLPI=[ 1](%),
4219          LGI=[ 345](m), MNI=[ 0.013], SCI=[ 0](min),
4220          Continuous simulation parameters:
4221          I a RE C per=[ 4](hrs), I a RE C i mp=[ 4](hrs),
4222          SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4223          Inter Event Ti me=[ 18](hrs), END=- 1
4224  *%-----|
4225  COMPUTE DUALHYD          NHYD i n=[ "B3"], CI NLET=[ 0.459](cms), NI NLET=[ 1],
4226          M a j NHYD=[ "B3- M "]
4227          M n NHYD=[ "B3- MN"]
4228          TM I STO=[ 227](cu-m)
4229  *%-----|
4230  ADD HYD          NHYDs um=[ "MH333"], NHYDs to add=[ "B3- MN"+"315-333"]
4231  *%-----|
4232  SAVE HYD          NHYD=[ "MH333"], # OF PCYCLES=[ -1], I CASEs h=[ 1]
4233          HYD_COMMENT=[ "Total Flows at MH333"]
4234  *%-----|
4235  ROUTE PI PE          PTYPE=[ 1]circ, NHYDout=[ "333-335"], RNUMBER=[ 1.0], PDI AM=[ 1200](mm),
4236          PLNGTH=[ 251](m), PROUGH=[ 0.013], PSLOPE=[ 0.001](m/m),
          NHYD i n=[ "MH333"], RDT=[ 1]
4237  *%-----|
4238  ROUTE PI PE          PTYPE=[ 1]circ, NHYDout=[ "335-338"], RNUMBER=[ 1.0], PDI AM=[ 1200](mm),
4239          PLNGTH=[ 185](m), PROUGH=[ 0.013], PSLOPE=[ 0.001](m/m),
          NHYD i n=[ "333-335"], RDT=[ 1]
4240  *%-----|
4241  ROUTE PI PE          PTYPE=[ 1]circ, NHYDout=[ "338-340"], RNUMBER=[ 1.0], PDI AM=[ 1350](mm),
4242          PLNGTH=[ 233](m), PROUGH=[ 0.013], PSLOPE=[ 0.001](m/m),
          NHYD i n=[ "335-338"], RDT=[ 1]
4243  *%-----|
4244  CONTINUOUS STANDHYD          NHYD=[ "B4"], DT=[ 1]min, AREA=[ 7.6](ha),
4245          XI MP=[ 0.41], TI MP=[ 0.54], DWF=[ 0](cms), LOSS=[ 2],
4246          SCS curve number CN=[ 75],
4247          Pervious surfaces: I A per=[ 4.67](mm), SLPP=[ 1](%),
4248          LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4249          Impervious surfaces: I A i mp=[ 1.57](mm), SLPI=[ 1](%),
4250          LGI=[ 388](m), MNI=[ 0.013], SCI=[ 0](min),
4251          Continuous simulation parameters:
4252          I a RE C per=[ 4](hrs), I a RE C i mp=[ 4](hrs),
4253          SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4254          Inter Event Ti me=[ 18](hrs), END=- 1
4255  *%-----|
4256  COMPUTE DUALHYD          NHYD i n=[ "B4"], CI NLET=[ 0.655](cms), NI NLET=[ 1],
4257          M a j NHYD=[ "B4- M "]

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4258 M nNHYD=[ " B4- MN" ]
4259 TM STO=[ 323] ( cu- m)
4260 *%-----|-----|
4261 ADD HYD NHYDs um=[ " M340" ], NHYDs to add=[ " 338- 340" + " B4- MN" ]
4262 *%-----|-----|
4263 SAVE HYD NHYD=[ " M340" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1 ]
4264 HYD_ COMMENT=[ " Tot al Fl ows at M340" ]
4265 *%-----|-----|
4266 ROUTE PI PE PTYPE=[ 1] circ, NHYDout=[ " 340- 104" ], RNUMBER=[ 1. 0 ], PDI AM=[ 1650] ( mm ),
4267 PLNGTH=[ 240] ( m ), PROUGH=[ 0. 013 ], PSLOPE=[ 0. 0015] ( m/ m ),
NHYDn=[ " M340" ], RDT=[ 1 ]
4268 *%-----|-----|
4269 ADD HYD NHYDs um=[ " M104T" ], NHYDs to add=[ " 340- 104" + " M104" ]
4270 *%-----|-----|
4271 ROUTE PI PE PTYPE=[ 2] rect, NHYDout=[ " 104- 105" ], RNUMBER=[ 1. 0 ],
4272 PW DTH=[ 2400] ( mm ) by PHEI GHT=[ 2100] ( mm ),
PLNGTH=[ 380] ( m ), PROUGH=[ 0. 013 ], PSLOPE=[ 0. 001] ( m/ m ),
NHYDn=[ " M104T" ], RDT=[ 1 ]
4273 *%-----|-----|
4274 CONTINUOUS STANDHYD NHYD=[ " B5" ], DT=[ 1] mi n, AREA=[ 2. 2] ( ha ),
4275 XI MP=[ 0. 57 ], TI MP=[ 0. 57 ], DWF=[ 0] ( cms ), LOSS=[ 2 ],
4276 SCS curve number CN=[ 75 ],
4277 Pervious surfaces: IAper=[ 4. 67] ( mm ), SLPP=[ 1] ( % ),
4278 LGP=[ 40] ( m ), MNP=[ 0. 25 ], SCP=[ 0] ( mi n ),
4279 Impervious surfaces: IAi mp=[ 1. 57] ( mm ), SLPI =[ 1] ( % ),
4280 LGI =[ 187] ( m ), MNI =[ 0. 013 ], SCI =[ 0] ( mi n ),
4281 Continuous simulation parameters:
4282 IaREcper=[ 4] ( hrs ), IaRECi mp=[ 4] ( hrs ),
4283 SM N=[ - 1] ( mm ), SMAX=[ - 1] ( mm ), SK=[ 0. 010] / ( mm ),
4284 InterEvent Ti me=[ 18] ( hrs ), END=- 1
4285 *%-----|-----|
4286 COMPUTE DUALHYD NHYDn=[ " B5" ], CI NLET=[ 0. 260] ( cms ), NI NLET=[ 1 ],
4287 MAj NHYD=[ " B5- M" ]
4288 M nNHYD=[ " B5- MN" ]
4289 TM STO=[ 250] ( cu- m)
4290 *%-----|-----|
4291 CONTINUOUS STANDHYD NHYD=[ " A8" ], DT=[ 1] mi n, AREA=[ 0. 96] ( ha ),
4292 XI MP=[ 0. 71 ], TI MP=[ 0. 71 ], DWF=[ 0] ( cms ), LOSS=[ 2 ],
4293 SCS curve number CN=[ 75 ],
4294 Pervious surfaces: IAper=[ 4. 67] ( mm ), SLPP=[ 1] ( % ),
4295 LGP=[ 40] ( m ), MNP=[ 0. 25 ], SCP=[ 0] ( mi n ),
4296 Impervious surfaces: IAi mp=[ 1. 57] ( mm ), SLPI =[ 1] ( % ),
4297 LGI =[ 186] ( m ), MNI =[ 0. 013 ], SCI =[ 0] ( mi n ),
4298 Continuous simulation parameters:
4299 IaREcper=[ 4] ( hrs ), IaRECi mp=[ 4] ( hrs ),
4300 SM N=[ - 1] ( mm ), SMAX=[ - 1] ( mm ), SK=[ 0. 010] / ( mm ),
4301 InterEvent Ti me=[ 18] ( hrs ), END=- 1
4302 *%-----|-----|
4303 ADD HYD NHYDs um=[ " A8T" ], NHYDs to add=[ " A6- M" + " A8" ]
4304 *%-----|-----|
4305 COMPUTE DUALHYD NHYDn=[ " A8T" ], CI NLET=[ 0. 238] ( cms ), NI NLET=[ 1 ],
4306 MAj NHYD=[ " A8- M" ]
4307 M nNHYD=[ " A8- MN" ]
4308 TM STO=[ 40] ( cu- m)
4309 *%-----|-----|
4310 ADD HYD NHYDs um=[ " M105" ], NHYDs to
4311 add=[ " 104- 105" + " B5- MN" + " A8- MN" + " TODD_ MN3j " ]
4312 *%-----|-----|
4313 SAVE HYD NHYD=[ " M105" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1 ]
4314 HYD_ COMMENT=[ " Tot al Fl ows at M105" ]
4315 *%-----|-----|
4316 DI VERT HYD NHYDn=[ " A8- M" ] NI Dout=[ 2] max five,
4317 outflow hydr ographs ( NHYDs )=[ " A8- M- JR" " A8- M- B6" ]
4318 flow distribution table: ( modify as necessary )
Note: all flows are in ( cms )

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4319          QI Di + QI Di i = QTOTAL
4320          [ 0 + 0 = 0 ]
4321          [ 50 + 50 = 100 ] end
4322  *%-----|-----
|
4323  DI VERT HYD  NHYDin=["MHI05"] NI Dout=[2]max five,
4324              outflow hydrographs (NHYDs)=["MHI05-JR" "MHI05-B6"]
4325              flow distribution table: (modify as necessary)
4326              Note: all flows are in (cms)
4327              QI Di + QI Di i = QTOTAL
4328              [ 0 + 0 = 0 ]
4329              [ 0 + 3.0 = 3.0 ]
4330              [ 96.9+ 3.1 = 100 ] end
4331  *%-----|-----
|
4332  CONTINUOUS STANDHYD  NHYD=["B7"], DT=[1]min, AREA=[7.19](ha),
4333                    XI MP=[0.41], TI MP=[0.54], DWF=[0](cms), LOSS=[2],
4334                    SCS curve number CN=[75],
4335                    Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4336                    LGP=[40](m), MNP=[0.25], SCP=[0](min),
4337                    Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4338                    LGI=[211](m), MNI=[0.013], SCI=[0](min),
4339                    Continuous simulation parameters:
4340                    IaRECper=[4](hrs), IaRECImp=[4](hrs),
4341                    SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4342                    InterEventTime=[18](hrs), END=-1
4343  *%-----|-----
4344  ADD HYD      NHYDsum=["B7-B4M"], NHYDs to add=["B4-M"+"B7"]
4345  *%-----|-----
4346  COMPUTE DUALHYD  NHYDin=["B7-B4M"], CINLET=[0.629](cms), NINLET=[1],
4347                    MajNHYD=["B7R-M"]
4348                    MnNHYD=["B7R-MN"]
4349                    TMSTO=[311](cu-m)
4350  *%-----|-----
4351  ROUTE PIPE   PTYPE=[1]circ, NHYDout=["360-106A"], RNUMBER=[1.0], PDIAM=[1050](mm),
4352                    PLNGTH=[167](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
4353                    NHYDin=["B7R-MN"], RDT=[1]
4354  *%-----|-----
4355  * -JFSA 2021-01-19 change B6 to be developed as per geottawa website and apply the
4356  parameters of A7, the nearest sub-catchment to B6, LGI is calculated based on B6 area
4357  CONTINUOUS STANDHYD  NHYD=["B6"], DT=[1]min, AREA=[3.29](ha),
4358                    XI MP=[0.41], TI MP=[0.54], DWF=[0](cms), LOSS=[2],
4359                    SCS curve number CN=[75],
4360                    Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
4361                    LGP=[40](m), MNP=[0.25], SCP=[0](min),
4362                    Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
4363                    LGI=[148.099](m), MNI=[0.013], SCI=[0](min),
4364                    Continuous simulation parameters:
4365                    IaRECper=[4](hrs), IaRECImp=[4](hrs),
4366                    SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4367                    InterEventTime=[18](hrs), END=-1
4368  *%-----|-----
4369  * -JFSA 2021-01-25 add B1 DUALHYD as per Corrigan Report, IBI Group, 2008
4370  COMPUTE DUALHYD  NHYDin=["B6"], CINLET=[0.064](cms), NINLET=[1],
4371                    MajNHYD=["B6-M"]
4372                    MnNHYD=["B6-MN"]
4373                    TMSTO=[5484](cu-m)
4374  *%-----|-----
4375  *CONTINUOUS NASHHYD  NHYD=["B6"], DT=[1]min, AREA=[3.29](ha),
4376  *                    DWF=[0](cms), CN C=[75], IA=[2.5](mm),
4377  *                    N=[3.0], TP=[0.36]hrs,
4378  *                    Continuous simulation parameters:
4379  *                    IaRECper=[4](hrs),
4380  *                    SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4381  *                    InterEventTime=[12](hrs)
4382  *                    Baseflow simulation parameters:

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4381 * BaseFlowOption=[ 1 ] ,
4382 * InitGWResVol =[ 50 ] ( mm ) , GWResK=[ 0.96 ] ( mm/ day/ mm)
4383 * VHydCond=[ 0.055 ] ( mm/ hr ) , END=- 1
4384 *%-----|-----|
4385 *% -EX-LAND is external land. It is a part of JOCKVA sub-catchment as per Corrigan
Report, IBI Group, 2008
4386 CONTINUOUS STANDHYD NHYD=[ "EX-LAND" ] , DT=[ 1 ] mi n , AREA=[ 32.5 ] ( ha ) ,
4387 XI MP=[ 0.50 ] , TI MP=[ 0.50 ] , DWF=[ 0 ] ( cms ) , LOSS=[ 2 ] ,
4388 SCS curve number CN=[ 74 ] ,
4389 Pervious surfaces: I A per =[ 4.67 ] ( mm ) , SLPP=[ 1 ] ( % ) ,
4390 LGP=[ 40 ] ( m ) , MNP=[ 0.25 ] , SCP=[ 0 ] ( mi n ) ,
4391 Impervious surfaces: I Ai mp =[ 1.57 ] ( mm ) , SLPI =[ 1 ] ( % ) ,
4392 LGI =[ 465.475 ] ( m ) , MNI =[ 0.013 ] , SCI =[ 0 ] ( mi n ) ,
4393 Continuous simulation parameters:
4394 I a REC per =[ 4 ] ( hrs ) , I a REC i mp =[ 4 ] ( hrs ) ,
4395 SM N =[ - 1 ] ( mm ) , SMAX =[ - 1 ] ( mm ) , SK =[ 0.010 ] / ( mm ) ,
4396 InterEventTi me =[ 18 ] ( hrs ) , END=- 1
4397 *%-----|-----|
4398 COMPUTE DUALHYD NHYDi n=[ "EX-LAND" ] , CI NLET=[ 2.275 ] ( cms ) , NI NLET=[ 1 ] ,
4399 M i j NHYD=[ "EX-LAND- M " ]
4400 M nNHYD=[ "EX-LAND- MN" ]
4401 TM STO=[ 1365 ] ( cu- m)
4402 *%-----|-----|
4403 ADD HYD NHYDs um=[ " B6- B7ExM " ] , NHYDs t o
add=[ " B7R- M " + " EX-LAND- M " + " B5- M " + " B6- M " + " B6- MN" + " A8- M - B6 " ]
4404 *%-----|-----|
4405 COMPUTE DUALHYD NHYDi n=[ " B6- B7ExM " ] , CI NLET=[ 0.064 ] ( cms ) , NI NLET=[ 1 ] ,
4406 M i j NHYD=[ " B6R- M " ]
4407 M nNHYD=[ " B6R- MN" ]
4408 TM STO=[ 5484 ] ( cu- m)
4409 *%-----|-----|
4410 ROUTE PI PE PTYPE=[ 1 ] circ , NHYDout =[ " 105- 106A " ] , RNUMBER=[ 1.0 ] , PDI AM=[ 1800 ] ( mm ) ,
4411 PLNGTH=[ 208 ] ( m ) , PROUGH=[ 0.013 ] , PSLOPE=[ 0.001 ] ( m/ m ) ,
NHYDi n=[ " MHI 05- B6 " ] , RDT=[ 1 ]
4412 *%-----|-----|
4413 ADD HYD NHYDs um=[ " MHI 06A " ] , NHYDs t o
add=[ " 360- 106A " + " 105- 106A " + " B6R- MN" + " B6R- M " ]
4414 *%-----|-----|
4415 SAVE HYD NHYD=[ " MHI 06A " ] , # OF PCYCLES=[ - 1 ] , I CASEs h=[ 1 ]
4416 HYD_COMMENT=[ " Total Flows at MHI 06A " ]
4417 *%-----|-----|
4418 *% -JFSA 2021-01-12 THE MANHOLE MHI06 is called MHI17/106 in Corrigan Report, IBI
Group, July 2008
4419 *%
4420 ROUTE PI PE PTYPE=[ 1 ] circ , NHYDout =[ " 106A- 106 " ] , RNUMBER=[ 1.0 ] , PDI AM=[ 1800 ] ( mm ) ,
4421 PLNGTH=[ 190 ] ( m ) , PROUGH=[ 0.013 ] , PSLOPE=[ 0.001 ] ( m/ m ) ,
NHYDi n=[ " MHI 06A " ] , RDT=[ 1 ]
4422 *%-----|-----|
4423 CONTINUOUS STANDHYD NHYD=[ " A9 " ] , DT=[ 1 ] mi n , AREA=[ 2.44 ] ( ha ) ,
4424 XI MP=[ 0.71 ] , TI MP=[ 0.71 ] , DWF=[ 0 ] ( cms ) , LOSS=[ 2 ] ,
4425 SCS curve number CN=[ 75 ] ,
4426 Pervious surfaces: I A per =[ 4.67 ] ( mm ) , SLPP=[ 1 ] ( % ) ,
4427 LGP=[ 40 ] ( m ) , MNP=[ 0.25 ] , SCP=[ 0 ] ( mi n ) ,
4428 Impervious surfaces: I Ai mp =[ 1.57 ] ( mm ) , SLPI =[ 1 ] ( % ) ,
4429 LGI =[ 262 ] ( m ) , MNI =[ 0.013 ] , SCI =[ 0 ] ( mi n ) ,
4430 Continuous simulation parameters:
4431 I a REC per =[ 4 ] ( hrs ) , I a REC i mp =[ 4 ] ( hrs ) ,
4432 SM N =[ - 1 ] ( mm ) , SMAX =[ - 1 ] ( mm ) , SK =[ 0.010 ] / ( mm ) ,
4433 InterEventTi me =[ 18 ] ( hrs ) , END=- 1
4434 *%-----|-----|
4435 COMPUTE DUALHYD NHYDi n=[ " A9 " ] , CI NLET=[ 0.547 ] ( cms ) , NI NLET=[ 1 ] ,
4436 M i j NHYD=[ " A9- M " ]
4437 M nNHYD=[ " A9- MN" ]
4438 TM STO=[ 0 ] ( cu- m)
4439 *%-----|-----|
4440 ADD HYD NHYDs um=[ " MHI 06 " ] , NHYDs t o add=[ " 106A- 106 " + " A9- MN" ]

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4441  *%-----|-----|
4442  SAVE HYD      NHYD=["MHI06"], # OF PCYCLES=[ - 1], I CASEs h=[ 1]
4443              HYD_COMMENT=["Tot al Fl ows at MHI06"]
4444  *%-----|-----|
4445  *%    -JFSA 2021-01-12 THE MANHOLE MHI07 is called MHI18/107 in Corrigan Report, IBI
Group, July 2008
4446  *%
4447  ROUTE PI PE   PTYPE=[ 1]circ, NHYDout=["106-107"], RNUMBER=[ 1.0], PDI AM=[ 1800](mm),
4448              PLNGTH=[ 122.5](m), PROUGH=[ 0.013], PSLOPE=[ 0.001](m/m),
              NHYDin=["MHI06"], RDT=[ 1]
4449  *%-----|-----|
4450  CONTINUOUS STANDHYD NHYD=["A10"], DT=[ 1]mi n, AREA=[ 4.14](ha),
4451              XI MP=[ 0.35], TI MP=[ 0.47], DWF=[ 0](cms), LOSS=[ 2],
4452              SCS curve number CN=[ 75],
4453              Pervious surfaces: I A per=[ 4.67](mm), SLPP=[ 1](%),
4454              LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](mi n),
4455              Impervious surfaces: I Ai mp=[ 1.57](mm), SLPI=[ 1](%),
4456              LGI=[ 183](m), MNI =[ 0.013], SCI =[ 0](mi n),
4457              Continuous simulation parameters:
4458              I a REC per=[ 4](hrs), I a REC i mp=[ 4](hrs),
4459              SM N=[ - 1](mm), SMAX=[ - 1](mm), SK=[ 0.010]/(mm),
4460              Inter Event Ti me=[ 18](hrs), END=- 1
4461  *%-----|-----|
4462  COMPUTE DUALHYD NHYDin=["A10"], CI NLET=[ 0.310](cms), NI NLET=[ 1],
4463              M a j NHYD=["A10- M"]
4464              M nNHYD=["A10- MN"]
4465              TM I STO=[ 228](cu- m)
4466  *%-----|-----|
4467  CONTINUOUS STANDHYD NHYD=["A11"], DT=[ 1]mi n, AREA=[ 10.61](ha),
4468              XI MP=[ 0.53], TI MP=[ 0.62], DWF=[ 0](cms), LOSS=[ 2],
4469              SCS curve number CN=[ 75],
4470              Pervious surfaces: I A per=[ 4.67](mm), SLPP=[ 1](%),
4471              LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](mi n),
4472              Impervious surfaces: I Ai mp=[ 1.57](mm), SLPI=[ 1](%),
4473              LGI=[ 379](m), MNI =[ 0.013], SCI =[ 0](mi n),
4474              Continuous simulation parameters:
4475              I a REC per=[ 4](hrs), I a REC i mp=[ 4](hrs),
4476              SM N=[ - 1](mm), SMAX=[ - 1](mm), SK=[ 0.010]/(mm),
4477              Inter Event Ti me=[ 18](hrs), END=- 1
4478  *%-----|-----|
4479  COMPUTE DUALHYD NHYDin=["A11"], CI NLET=[ 0.993](cms), NI NLET=[ 1],
4480              M a j NHYD=["A11- M"]
4481              M nNHYD=["A11- MN"]
4482              TM I STO=[ 556](cu- m)
4483  *%-----|-----|
4484  ADD HYD       NHYDs um=["MHI07"], NHYDs to add=["106-107"+"A10- MN"+"A11- MN"]
4485  *%-----|-----|
4486  SAVE HYD      NHYD=["MHI07"], # OF PCYCLES=[ - 1], I CASEs h=[ 1]
4487              HYD_COMMENT=["Tot al Fl ows at MHI07"]
4488  *%-----|-----|
4489  ROUTE PI PE   PTYPE=[ 1]circ, NHYDout=["107-119"], RNUMBER=[ 1.0], PDI AM=[ 1800](mm),
4490              PLNGTH=[ 114](m), PROUGH=[ 0.013], PSLOPE=[ 0.0012](m/m),
              NHYDin=["MHI07"], RDT=[ 1]
4491  *%-----|-----|
4492  *%    -JFSA 2021-01-12 THE MANHOLE MHI08 is called MHI20/108 in Corrigan Report, IBI
Group, July 2008
4493  *%
4494  ROUTE PI PE   PTYPE=[ 1]circ, NHYDout=["119-108"], RNUMBER=[ 1.0], PDI AM=[ 1800](mm),
4495              PLNGTH=[ 65.8](m), PROUGH=[ 0.013], PSLOPE=[ 0.0012](m/m),
              NHYDin=["107-119"], RDT=[ 1]
4496  *%-----|-----|
4497  CONTINUOUS STANDHYD NHYD=["A12"], DT=[ 1]mi n, AREA=[ 12.29](ha),
4498              XI MP=[ 0.41], TI MP=[ 0.54], DWF=[ 0](cms), LOSS=[ 2],
4499              SCS curve number CN=[ 75],
4500              Pervious surfaces: I A per=[ 4.67](mm), SLPP=[ 1](%),
4501              LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](mi n),

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4502      Impervious surfaces: I A i mp=[ 1.57](mm), SLPI=[ 1](%),
4503              LGI=[ 183](m), MNI=[ 0.013], SCI=[ 0](mi n),
4504      Continuous simulation parameters:
4505      I a RE C per=[ 4](hrs), I a RE C i mp=[ 4](hrs),
4506      SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4507      Inter Event Ti me=[ 18](hrs), END=- 1
4508  *%-----|
4509  COMPUTE DUALHYD      NHYD i n=[ "A12"], CI NLET=[ 1.029](cms), NI NLET=[ 1],
4510                      M i j NHYD=[ "A12- M "]
4511                      M n NHYD=[ "A12- MN"]
4512                      TM I STO=[ 672](cu- m)
4513  *%-----|
4514  CONTINUOUS STANDHYD      NHYD=[ "A13"], DT=[ 1]mi n, AREA=[ 2.59](ha),
4515                      XI MP=[ 0.71], TI MP=[ 0.71], DWF=[ 0](cms), LOSS=[ 2],
4516                      SCS curve number CN=[ 75],
4517                      Pervious surfaces: I A per=[ 4.67](mm), SLPP=[ 1](%),
4518                      LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](mi n),
4519                      Impervious surfaces: I A i mp=[ 1.57](mm), SLPI=[ 1](%),
4520                      LGI=[ 379](m), MNI=[ 0.013], SCI=[ 0](mi n),
4521                      Continuous simulation parameters:
4522                      I a RE C per=[ 4](hrs), I a RE C i mp=[ 4](hrs),
4523                      SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4524                      Inter Event Ti me=[ 18](hrs), END=- 1
4525  *%-----|
4526  COMPUTE DUALHYD      NHYD i n=[ "A13"], CI NLET=[ 0.571](cms), NI NLET=[ 1],
4527                      M i j NHYD=[ "A13- M "]
4528                      M n NHYD=[ "A13- MN"]
4529                      TM I STO=[ 0](cu- m)
4530  *%-----|
4531  * -JFSA 2021-01-22 add the Corrigan pond area ("Pond-Block")
4532  CONTINUOUS STANDHYD      NHYD=[ "Pond- Bl ock"], DT=[ 1]mi n, AREA=[ 2.94](ha),
4533                      XI MP=[ 0.415], TI MP=[ 0.415], DWF=[ 0](cms), LOSS=[ 2],
4534                      SCS curve number CN=[ 75],
4535                      Pervious surfaces: I A per=[ 4.67](mm), SLPP=[ 1](%),
4536                      LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](mi n),
4537                      Impervious surfaces: I A i mp=[ 1.57](mm), SLPI=[ 1](%),
4538                      LGI=[ 183](m), MNI=[ 0.013], SCI=[ 0](mi n),
4539                      Continuous simulation parameters:
4540                      I a RE C per=[ 4](hrs), I a RE C i mp=[ 4](hrs),
4541                      SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4542                      Inter Event Ti me=[ 18](hrs), END=- 1
4543  *%-----|
4544  ADD HYD      NHYDs um=[ "MH108"], NHYDs to add=[ "119-108"+"A13- MN"+"A12- MN"]
4545  *%-----|
4546  SAVE HYD      NHYD=[ "MH108"], # OF PCYCLES=[ -1], I CASEs h=[ 1]
4547                      HYD_ COMMENT=[ "Tot al Fl ows at MH108"]
4548  *%-----|
4549  ROUTE PI PE      PTYPE=[ 1]circ, NHYDout=[ "108-116"], RNUMBER=[ 1.0], PDI AM=[ 1800](mm),
4550                      PLNGTH=[ 76.6](m), PROUGH=[ 0.013], PSLOPE=[ 0.0013](m/m),
4551                      NHYD i n=[ "MH108"], RDT=[ 1]
4552  *%-----|
4553  ROUTE PI PE      PTYPE=[ 1]circ, NHYDout=[ "116-corrig"], RNUMBER=[ 1.0],
4554                      PDI AM=[ 1800](mm),
4555                      PLNGTH=[ 79.5](m), PROUGH=[ 0.013], PSLOPE=[ 0.0013](m/m),
4556                      NHYD i n=[ "108-116"], RDT=[ 1]
4557  *%-----|
4558  ADD HYD      NHYDs um=[ "Corrigan"], NHYDs to add=[ "116-corrig"+"Pond- Bl ock"]
4559  *%-----|
4560  SAVE HYD      NHYD=[ "Corrigan"], # OF PCYCLES=[ -1], I CASEs h=[ 1]
4561                      HYD_ COMMENT=[ "Tot al Fl ows at Corrigan Pond"]
4562  *%-----|
4563  ROUTE RESERVOIR      NHYDout=[ "Co- P"], NHYD i n=[ "Corrigan"],
4564                      RDT=[ 1](mi n),
4565                      TABLE of ( OUTFLOW STORAGE ) values
4566                      (cms) - (ha- m)
4567                      [ 0.0 , 0.0 ]

```

```

4565 [ 0.015 , 0.04118]
4566 [ 0.030 , 0.08297]
4567 [ 0.045 , 0.12537]
4568 [ 0.060 , 0.16837]
4569 [ 0.075 , 0.21199]
4570 [ 0.090 , 0.27545]
4571 [ 0.105 , 0.34650]
4572 [ 0.120 , 0.42049]
4573 [ 0.135 , 0.50188]
4574 [ 0.186 , 0.60307]
4575 [ 2.110 , 0.79083]
4576 [ 5.874 , 1.00271]
4577 [ 11.395 , 1.29643]
4578 [ 18.770 , 1.62054]
4579 [ 28.143 , 1.97516]
4580 [ -1 , -1 ] (max twenty pts)
4581 NHYDovf=[ "Co- P- OVF" ]
4582 *%-----|-----|
4583 ADD HYD NHYDsum=[ "corrig" ], NHYDs to
add=[ "Co- P- OVF" + "Co- P" + "N_TO" + "M105- JR" + "A8- M- JR" + "A9- M" + "A10- M" + "A11- M" + "A12- M" + "A
13- M" ]
4584 *%-----|-----|
4585 SAVE HYD NHYD=[ "corrig" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1]
4586 HYD_COMMENT=[ "Total Flows at Corrigan Pond" ]
4587 *%-----|-----|
4588 *#*****|
4589 *# Corrigan Pond 1
4590 *# - Rating curve obtained from Barrhaven South M&S modeling
4591 *# - Tributary Drainage Area to M&S Pond 1 = 145 ha
4592 *#*****|
4593 *ROUTE RESERVOIR NHYDout=[ "MS_P1" ], NHYDin=[ "CORRIG" ],
4594 * RDT=[ 1 ] (min),
4595 * TABLE of ( OUTFLOW STORAGE ) values
4596 * (cms) - (ha-m)
4597 * [ 0.0 , 0.0 ]
4598 * [ 0.06 , 0.58]
4599 * [ -1 , -1 ] (max twenty pts)
4600 * NHYDovf=[ "P1- OVF" ]
4601 *%-----|-----|
4602 *ADD HYD NHYDsum=[ "SN_CO" ], NHYDs to add=[ "N_TO" + "P1- OVF" + "MS_P1" ]
4603 *%-----|-----|
4604 *SAVE HYD NHYD=[ "SN_CO" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1]
4605 * HYD_COMMENT=[ "Total Flows at Corrigan Drain" ]
4606 *%-----|-----|
4607 *#
4608 *# Hydrograph from Corrigan Drain routed to Jockvale Road
4609 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
4610 *#
4611 ROUTE CHANNEL NHYDout=[ "N_M" ], NHYDin=[ "corrig" ],
4612 RDT=[ 1 ] (min),
4613 CHLGTH=[ 580 ] (m), CHSLOPE=[ 0.4448 ] ( % ),
4614 FPSLOPE=[ 0.4448 ] ( % ),
4615 SECNUM=[ 1.0 ], NSEG=[ 3]
4616 ( SEGROUGH, SEGDI ST (m) ) =
4617 [ 0.075, -17.72
4618 -0.045, 17.72
4619 0.075, 80.62 ] NSEG times
4620 ( DI STANCE (m), ELEVATI ON (m) ) =
4621 [ -83.32, 90.00]
4622 [ -81.36, 89.50]
4623 [ -79.12, 89.00]
4624 [ -76.13, 88.50]
4625 [ -20.46, 88.00]
4626 [ -19.36, 87.50]
4627 [ -18.51, 87.00]
4628 [ -17.72, 86.50]

```

4629 [- 11.95, 85.24]
 4630 [- 0.11, 85.12]
 4631 [11.49, 85.20]
 4632 [17.72, 86.50]
 4633 [19.74, 87.00]
 4634 [21.22, 87.50]
 4635 [22.68, 88.00]
 4636 [24.28, 88.50]
 4637 [26.79, 89.00]
 4638 [71.98, 90.00]
 4639 [80.62, 90.50]

*%-----|-----|
 *#*****|

*# Catchment MLLS
 *# - To SWM Facility north of the Jock
 *# - Primarily residential development

*#*****|

CONTINUOUS STANDHYD NHYD=["MLLS"], DT=[1]min, AREA=[175.99](ha),
 XI MP=[0.38], TI MP=[0.38], DWF=[0](cms), LOSS=[2],
 SCS curve number CN=[74],
 Per vious surfaces: I A per=[4.67](mm), SLPP=[1](%),
 LGP=[40](m), MNP=[0.25], SCP=[0](min),
 Imper vious surfaces: I A i mp=[1.57](mm), SLPI=[1](%),
 LGI=[1118.123](m), MNI=[0.013], SCI=[0](min),
 Continuous simulation parameters:
 I a REC per=[4](hrs), I a REC i mp=[4](hrs),
 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
 Inter Event Ti me=[18](hrs), END=-1

*%-----|-----|
 *#*****|

*# Chapman Mills SWM Pond
 *# - Rating curve obtained from CCL hydraulic modeling

*#*****|

ROUTE RESERVOIR NHYDout=["MLL_P"], NHYDin=["MLLS"],
 RDT=[1](min),
 TABLE of (OUTFLOW STORAGE) values

	(cms) - (ha - m)
4666	[0.0 , 0.0]
4667	[0.01 , 0.01]
4668	[0.05 , 0.06]
4669	[0.09 , 0.11]
4670	[0.13 , 0.15]
4671	[0.18 , 0.19]
4672	[0.28 , 0.28]
4673	[0.37 , 0.34]
4674	[0.45 , 0.40]
4675	[0.51 , 0.44]
4676	[0.56 , 0.47]
4677	[0.64 , 0.52]
4678	[0.76 , 0.59]
4679	[0.86 , 0.65]
4680	[1.09 , 0.78]
4681	[1.44 , 0.96]
4682	[3.18 , 1.84]
4683	[4.05 , 2.31]
4684	[-1 , -1] (max twenty pts)

NHYDovf=["ML-OV"]

*%-----|-----|

ADD HYD NHYDsum=["SN_M"], NHYDs to add=["N_M"+"ML-OV"+"MLL_P"]

*%-----|-----|

SAVE HYD NHYD=["SN_M"], # OF PCYCLES=[-1], I CASEs h=[1]
 HYD_COMMENT=["Total Flows at Jockvale Road"]

*%-----|-----|

*#
 *# Hydrograph from Jockvale Road routed to Heart's Desire
 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 689

```

4695 *#
4696 ROUTE CHANNEL NHYDout=["N_DE"], NHYDin=["SN_M"],
4697 RDT=[1](min),
4698 CHLGTH=[1962](m), CHSLOPE=[0.2227](%),
4699 FPSLOPE=[0.2227](%),
4700 SECNUM=[1.0], NSEG=[3]
4701 (SEGROUGH, SEGDIST(m))=
4702 [0.075, -17.56
4703 -0.045, 18.27
4704 0.075, 32.51] NSEG times
4705 (DISTANCE(m), ELEVATION(m))=
4706 [-54.07, 85.00]
4707 [-39.43, 84.50]
4708 [-28.30, 84.00]
4709 [-24.12, 83.50]
4710 [-22.30, 83.00]
4711 [-20.55, 82.50]
4712 [-17.56, 82.00]
4713 [-12.63, 81.22]
4714 [-0.11, 80.75]
4715 [11.55, 81.22]
4716 [18.27, 82.00]
4717 [19.82, 82.50]
4718 [22.48, 83.00]
4719 [27.90, 83.50]
4720 [29.31, 84.00]
4721 [30.81, 84.50]
4722 [32.51, 85.00]
4723 *%-----|-----
4724 *#*****
4725 *# Catchment DESIRE
4726 *# - To Jock River (north of the Jock)
4727 *# - Rural-estate subdivision (Heart's Desire Community)
4728 *#*****
4729 CONTINUOUS STANDHYD NHYD=["DESIRE"], DT=[1]min, AREA=[23.78](ha),
4730 XI MP=[0.25], TI MP=[0.25], DWF=[0](cms), LOSS=[2],
4731 SCS curve number CN=[77],
4732 Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
4733 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4734 Impervious surfaces: I A i mp=[1.57](mm), SLPI=[1](%),
4735 LGI=[400](m), MNI=[0.013], SCI=[0](min),
4736 Continuous simulation parameters:
4737 I a REC per=[4](hrs), I a REC i mp=[4](hrs),
4738 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4739 I n t e r E v e n t T i m e=[18](hrs), E N D=-1
4740 *%-----|-----
4741 *#*****
4742 *# Catchment JOCKVA
4743 *# - To Jockvale SWM Facility
4744 *# - Residential development & golf course
4745 *# - JFSA 2021-01-11 update JOCKVA after updating CORRIG as per IBI GROUP, July 2008.
4746 *# JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two
4747 areas JOCKVA and EX-LAND 32.5 ha as per IBI GROUP, July 2008.
4748 *#*****
4749 CONTINUOUS STANDHYD NHYD=["JOCKVA"], DT=[1]min, AREA=[225.13](ha),
4750 XI MP=[0.50], TI MP=[0.50], DWF=[0](cms), LOSS=[2],
4751 SCS curve number CN=[74],
4752 Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
4753 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4754 Impervious surfaces: I A i mp=[1.57](mm), SLPI=[1](%),
4755 LGI=[1310.55](m), MNI=[0.013], SCI=[0](min),
4756 Continuous simulation parameters:
4757 I a REC per=[4](hrs), I a REC i mp=[4](hrs),
4758 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4759 I n t e r E v e n t T i m e=[18](hrs), E N D=-1
4759 *%-----|-----

```

```

4760 ADD HYD          NHYDs um=[" J OCKVA- TO' ], NHYDs t o
add=[" EX- LAND- MN" + " J OCKVA" + " B2- M" + " B3- M" ]
4761 *%-----|-----|
4762 SAVE HYD          NHYD=[" J OCKVA- TO' ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1 ]
4763 HYD_COMMENT=[" Total Flows at KB first pond" ]
4764 *%-----|-----|
4765 *#*****|-----|
4766 *# Jockvale SWM Facility
4767 *# - Rating curve obtained from Jockvale Servicing Study (CCL 1999)
4768 *#*****|-----|
4769 ROUTE RESERVOIR  NHYDout =[" J OCK_P" ], NHYDi n=[" J OCKVA- TO' ],
4770 RDT=[ 1 ] ( mi n ),
4771 TABLE of ( OUTFLOW STORAGE ) values
4772 ( cms ) - ( ha- m )
4773 [ 0.0 , 0.0 ]
4774 [ 0.27 , 0.03 ]
4775 [ 0.28 , 0.55 ]
4776 [ 0.29 , 1.14 ]
4777 [ 0.30 , 1.80 ]
4778 [ 0.31 , 2.32 ]
4779 [ 1.12 , 2.87 ]
4780 [ 2.92 , 3.45 ]
4781 [ 4.64 , 4.07 ]
4782 [ 6.69 , 4.72 ]
4783 [ 9.02 , 5.39 ]
4784 [ 11.62 , 6.10 ]
4785 [ 14.42 , 6.85 ]
4786 [ 17.45 , 7.62 ]
4787 [ 20.69 , 8.44 ]
4788 [ 24.08 , 9.28 ]
4789 [ 27.68 , 10.17 ]
4790 [ -1 , -1 ] (max t went y pts)
4791 NHYDovf=[" J O- OVF" ]
4792 *%-----|-----|
4793 ADD HYD          NHYDs um=[" SN_DE" ], NHYDs t o add=[" N_DE" + " DESI RE" + " J O- OVF" + " J OCK_P" ]
4794 *%-----|-----|
4795 SAVE HYD          NHYD=[" SN_DE" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1 ]
4796 HYD_COMMENT=[" Total Flows at Heart's Desire" ]
4797 *%-----|-----|
4798 *#
4799 *# Hydrograph from Heart's Desire routed to Rideau River
4800 *# Channel X-Section obtained from RVCA Hydraulic Mdel - Station 0
4801 *#
4802 ROUTE CHANNEL    NHYDout =[" NI " ] , NHYDi n=[" SN_DE" ] ,
4803 RDT=[ 1 ] ( mi n ),
4804 CHLGTH=[ 563 ] ( m ), CHSLOPE=[ 0.9668 ] ( % ),
4805 FPSLOPE=[ 0.9668 ] ( % ),
4806 SECNUM=[ 1.0 ], NSEG=[ 3 ]
4807 ( SEGROUGH, SEGDI ST ( m ) ) =
4808 [ 0.075, -30.20
4809 -0.045, 30.20
4810 0.075, 48.48 ] NSEG t i m e s
4811 ( DI STANCE ( m ), ELEVATI ON ( m ) ) =
4812 [ -98.46, 81.50 ]
4813 [ -92.24, 81.00 ]
4814 [ -86.88, 80.50 ]
4815 [ -81.54, 80.00 ]
4816 [ -74.36, 79.50 ]
4817 [ -63.54, 79.00 ]
4818 [ -39.23, 78.50 ]
4819 [ -34.51, 78.00 ]
4820 [ -33.01, 77.50 ]
4821 [ -30.20, 77.00 ]
4822 [ -13.42, 76.18 ]
4823 [ -1.14, 76.09 ]
4824 [ 17.06, 76.18 ]

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```

4825 [ 30.20, 77.00]
4826 [ 32.95, 77.50]
4827 [ 34.06, 78.00]
4828 [ 35.11, 78.50]
4829 [ 36.32, 79.00]
4830 [ 37.74, 79.50]
4831 [ 48.48, 81.50]
4832 *%-----|-----|
4833 *#*****|*****|
4834 *# Catchment S-2
4835 *# - To Jock River (north and south)
4836 *# - Undeveloped floodplain and river
4837 *#*****|*****|
4838 CONTINUOUS NASHYD NHYD=[ "S-2" ], DT=[ 1 ] mi n, AREA=[ 102.94 ] ( ha ),
4839 DWF=[ 0 ] ( cms ), CNVC=[ 72 ], IA=[ 4.67 ] ( mm ),
4840 N=[ 3 ], TP=[ 0.40 ] hrs,
4841 Continuous simulation parameters:
4842 IaRECper=[ 4 ] ( hrs ),
4843 SMN=[ - 1 ] ( mm ), SMAX=[ - 1 ] ( mm ), SK=[ 0.010 ] / ( mm ),
4844 InterEventTime=[ 12 ] ( hrs )
4845 Baseflow simulation parameters:
4846 BaseFlowOption=[ 1 ] ,
4847 InitGWResVol=[ 50 ] ( mm ), GWResK=[ 0.96 ] ( mm/ day/ mm)
4848 VHydCond=[ 0.055 ] ( mm/ hr ), END=- 1
4849 *%-----|-----|
4850 ADD HYD NHYDs um=[ "SN_NI" ], NHYDs to add=[ "NI"+"S-2" ]
4851 *%-----|-----|
4852 SAVE HYD NHYD=[ "SN_NI" ], # OF PCYCLES=[ - 1 ], ICASEsh=[ 1 ]
4853 HYD_COMMENT=[ "Total Flows at Rideau River" ]
4854 *%-----|-----|
4855 *#####|#####|
4856 *% 5 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4857 START TZERO=[ 0.0 ], METOUT=[ 2 ], NSTORM=[ 1 ], NRUN=[ 5 ]
4858 *% ["C24SC005.stm"] <--storm filename, one per line for NSTORMtime
4859 *%-----|-----|
4860 *% 10 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4861 START TZERO=[ 0.0 ], METOUT=[ 2 ], NSTORM=[ 1 ], NRUN=[ 10 ]
4862 *% ["C24SC010.stm"] <--storm filename, one per line for NSTORMtime
4863 *%-----|-----|
4864 *% 25 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4865 START TZERO=[ 0.0 ], METOUT=[ 2 ], NSTORM=[ 1 ], NRUN=[ 25 ]
4866 *% ["C24SC025.stm"] <--storm filename, one per line for NSTORMtime
4867 *%-----|-----|
4868 *% 50 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4869 START TZERO=[ 0.0 ], METOUT=[ 2 ], NSTORM=[ 1 ], NRUN=[ 50 ]
4870 *% ["C24SC050.stm"] <--storm filename, one per line for NSTORMtime
4871 *%-----|-----|
4872 *% 100 yr, 3 hr Chicago storm based on OTTAWA CDA IDF Curves
4873 *START TZERO=[ 0.0 ], METOUT=[ 2 ], NSTORM=[ 1 ], NRUN=[ 100 ]
4874 *% ["100YC3H.STM"] <--storm filename, one per line for NSTORMtime
4875 *%-----|-----|
4876 *% 100 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4877 START TZERO=[ 0.0 ], METOUT=[ 2 ], NSTORM=[ 1 ], NRUN=[ 100 ]
4878 *% ["C24SC100.stm"] <--storm filename, one per line for NSTORMtime
4879 *%-----|-----|
4880 *% 100 yr, 3 hr Chicago storm based on OTTAWA CDA IDF Curves
4881 *START TZERO=[ 0.0 ], METOUT=[ 2 ], NSTORM=[ 1 ], NRUN=[ 100 ]
4882 *% ["C24SC100.stm"] <--storm filename, one per line for NSTORMtime
4883 *START TZERO=[ 0.0 ], METOUT=[ 2 ], NSTORM=[ 1 ], NRUN=[ 101 ]
4884 *% ["A24SC100.stm"] <--storm filename, one per line for NSTORMtime
4885 *START TZERO=[ 0.0 ], METOUT=[ 2 ], NSTORM=[ 1 ], NRUN=[ 102 ]
4886 *% ["A24SC100_60.stm"] <--storm filename, one per line for NSTORMtime
4887 FINISH
4888

```



```

00375# #
00376# R002: C0039# -> Dfm=1D NDD -> AREAh-QPEAKm-TpeakDate-hh:mm--Rvmm-R.C.--Dfwm
00377# ADD HYD + 1.0 02: DM1 9506.00 7.379 No.date 33:12 11.30 n/a 000
00378# + 1.0 02: SW1 509.00 2.720 No.date 29:22 11.98 n/a 000
00379# + 1.0 02: NC_CK 1917.00 4.042 No.date 34:24 11.98 n/a 000
00380# SIMM 1.0 01: S_N1 11923.00 8.276 No.date 39:46 11.36 n/a 000
00381#
00382# # Sum of hydrographs from Node 11 routed to Node 10
00383# # Section 3
00384# #
00385# R002: C0040# -> Dfm=1D NDD -> AREAh-QPEAKm-TpeakDate-hh:mm--Rvmm-R.C.--Dfwm
00386# ROUTE CHANNEL -> 1.0 02: S_N1 11923.00 8.276 No.date 39:46 11.36 n/a 000
00387# [RFE=1.00] out c 1.0 01: N1 11923.00 8.276 No.date 39:46 11.36 n/a 000
00388# [L/S=4.028 / 157.040]
00389# [Vmax=.462; Dmax=.886]
00390# #
00391# # Addition of Subwatershed 10 to Node 10
00392# #
00393# R002: C0041# -> Dfm=1D NDD -> AREAh-QPEAKm-TpeakDate-hh:mm--Rvmm-R.C.--Dfwm
00394# ADD HYD + 1.0 02: N0 11923.00 8.276 No.date 39:46 11.36 n/a 000
00395# + 1.0 02: SW1 509.00 2.720 No.date 29:22 11.98 n/a 000
00396# + 1.0 02: NC_CK 1917.00 4.042 No.date 34:24 11.98 n/a 000
00397# SIMM 1.0 01: S_N0 17589.00 19.451 No.date 38:31 12.19 n/a 000
00398#
00399# SAVE HYD 1.0 01: S_N0 17589.00 19.451 No.date 38:31 12.19 n/a 000
00400# frame_HLSND
00401# remark:flow at S_N0: N0 + SW10
00402# #
00403# R002: C0043# -> Dfm=1D NDD -> AREAh-QPEAKm-TpeakDate-hh:mm--Rvmm-R.C.--Dfwm
00404# ADD HYD + 1.0 02: N0 17589.00 19.451 No.date 38:31 12.19 n/a 000
00405# + 1.0 02: NC_CK 8376.00 11.072 No.date 39:59 11.98 n/a 000
00406# SIMM 1.0 01: S_N0A 25965.00 30.328 No.date 39:58 12.12 n/a 000
00407#
00408# # Sum of hydrographs from Node 10 routed to Node 9
00409# # Section 2
00410# #
00411# R002: C0044# -> Dfm=1D NDD -> AREAh-QPEAKm-TpeakDate-hh:mm--Rvmm-R.C.--Dfwm
00412# ROUTE CHANNEL -> 1.0 02: S_N0A 25965.00 29.579 No.date 39:59 12.12 n/a 000
00413# [RFE=1.00] out c 1.0 01: N0 25965.00 29.579 No.date 39:59 12.12 n/a 000
00414# [L/S=3.982 / 157.040]
00415# [Vmax=.595; Dmax=1.208]
00416# #
00417# # Addition of Subwatershed 9 and Nichols Creek to Node 9
00418# #
00419# R002: C0045# -> Dfm=1D NDD -> AREAh-QPEAKm-TpeakDate-hh:mm--Rvmm-R.C.--Dfwm
00420# ADD HYD + 1.0 02: N0 25965.00 29.579 No.date 39:59 12.12 n/a 000
00421# + 1.0 02: SW 1132.00 4.434 No.date 39:56 13.25 n/a 000
00422# + 1.0 02: NC_CK 4464.00 5.504 No.date 39:59 10.98 n/a 000
00423# SIMM 1.0 01: S_N0 31561.00 36.313 No.date 39:59 12.00 n/a 000
00424#
00425# # Sum of hydrographs from Node 9 routed to Node 8
00426# # Section 3
00427# #
00428# R002: C0046# -> Dfm=1D NDD -> AREAh-QPEAKm-TpeakDate-hh:mm--Rvmm-R.C.--Dfwm
00429# ROUTE CHANNEL -> 1.0 02: S_N0 31561.00 36.313 No.date 39:59 12.00 n/a 000
00430# [RFE=1.00] out c 1.0 01: N0 31561.00 36.313 No.date 39:59 12.00 n/a 000
00431# [L/S=4.028 / 157.040]
00432# [Vmax=.418; Dmax=1.281]
00433# #
00434# # Addition of Subwatershed 8 and Hibbs' Drain to Node 8
00435# #
00436# R002: C0047# -> Dfm=1D NDD -> AREAh-QPEAKm-TpeakDate-hh:mm--Rvmm-R.C.--Dfwm
00437# ADD HYD + 1.0 02: N0 31561.00 36.313 No.date 39:59 12.00 n/a 000
00438# + 1.0 02: SW 131.00 8.052 No.date 38:57 11.22 n/a 000
00439# + 1.0 02: IB_DR 3854.00 6.242 No.date 38:46 11.98 n/a 000
00440# SIMM 1.0 01: S_N0 35546.00 40.474 No.date 39:59 12.00 n/a 000
00441#
00442# # Sum of hydrographs from Node 8 routed to Node 7
00443# # Section 4
00444# #
00445# R002: C0048# -> Dfm=1D NDD -> AREAh-QPEAKm-TpeakDate-hh:mm--Rvmm-R.C.--Dfwm
00446# ROUTE CHANNEL -> 1.0 02: S_N0 35546.00 40.474 No.date 39:59 12.00 n/a 000
00447# [RFE=1.00] out c 1.0 01: N0 35546.00 40.474 No.date 39:59 12.00 n/a 000
00448# [L/S=3.750 / 157.040]
00449# [Vmax=.208; Dmax=1.651]
00450# #
00451# # Addition of Subwatershed 7 to Node 7
00452# # Section 4
00453# R002: C0049# -> Dfm=1D NDD -> AREAh-QPEAKm-TpeakDate-hh:mm--Rvmm-R.C.--Dfwm
00454# ADD HYD + 1.0 02: SW7 3197.00 4.651 No.date 36:31 9.85 n/a 000
00455# SIMM 1.0 01: S_N7 38743.00 35.071 No.date 43:33 11.82 n/a 000
00456#
00457# SAVE HYD 1.0 01: S_N7 38743.00 35.071 No.date 43:33 11.82 n/a 000
00458# frame_HLSND
00459# remark:flow at S_N7: N0 + SW7
00460# #
00461# # Insertion of a Reservoir to simulate the effects of the Richmond Fen.
00462# # Storage area and volumes were estimated from available topography.
00463# # Release rate from fen was assumed to be controlled by the downstream
00464# # river cross section for various conditions. It is assumed that for up to
00465# # 0.75 m of water, the main channel of the river provided the storage. Above
00466# # this depth, the wetland starts to significantly store water.
00467# #
00468# R002: C0051# -> Dfm=1D NDD -> AREAh-QPEAKm-TpeakDate-hh:mm--Rvmm-R.C.--Dfwm
00469# RATE RESERVOIR -> 1.0 02: RES_RF 38743.00 35.071 No.date 43:33 11.82 n/a 000
00470# out c 1.0 01: RES_RF 38743.00 35.071 No.date 43:33 11.82 n/a 000
00471# [MSStoLd=7.00E+03]
00472# R002: C0052# -> Dfm=1D NDD -> AREAh-QPEAKm-TpeakDate-hh:mm--Rvmm-R.C.--Dfwm
00473# SAVE HYD 1.0 01: RES_RF 38743.00 35.071 No.date 43:33 11.82 n/a 000
00474# frame_HLSRF
00475# remark:outflow of Richmond Fen
00476# #
00477# # Sum of hydrographs from Node 7 routed to Node 6
00478# # Section 5
00479# #
00480# R002: C0053# -> Dfm=1D NDD -> AREAh-QPEAKm-TpeakDate-hh:mm--Rvmm-R.C.--Dfwm
00481# ROUTE CHANNEL -> 1.0 02: S_N0 40240.01 23.268 No.date 55:09 11.82 n/a 000
00482# [RFE=1.00] out c 1.0 01: N0 40240.01 23.268 No.date 55:09 11.82 n/a 000
00483# [L/S=1.882 / 157.040]
00484# [Vmax=.432; Dmax=.808]
00485# #
00486# # Addition of Subwatershed 6 and Van Gual Drain to Node 6
00487# #
00488# R002: C0054# -> Dfm=1D NDD -> AREAh-QPEAKm-TpeakDate-hh:mm--Rvmm-R.C.--Dfwm
00489# ADD HYD + 1.0 02: N0 38743.00 23.228 No.date 56:38 11.82 n/a 000
00490# + 1.0 02: SW 413.00 4.133 No.date 38:45 11.94 n/a 000
00491# + 1.0 02: VG_DR 1332.00 3.148 No.date 35:23 13.94 n/a 000
00492# SIMM 1.0 01: S_N0 40240.01 23.218 No.date 55:09 11.82 n/a 000
00493#
00494# # Sum of hydrographs from Node 6 routed to Node 5
00495# # Section 6
00496# #
00497# R002: C0055# -> Dfm=1D NDD -> AREAh-QPEAKm-TpeakDate-hh:mm--Rvmm-R.C.--Dfwm
00498# ROUTE CHANNEL -> 1.0 02: S_N0 40240.01 23.218 No.date 55:09 11.89 n/a 000
00499# [RFE=1.00] out c 1.0 01: N0 40240.01 23.218 No.date 55:09 11.89 n/a 000
00500# [L/S=1.882 / 157.040]
00501# [Vmax=.378; Dmax=.917]
00502# #
00503# # Addition of Subwatershed 5 and Flowing Creek to Node 5
00504# #
00505# R002: C0056# -> Dfm=1D NDD -> AREAh-QPEAKm-TpeakDate-hh:mm--Rvmm-R.C.--Dfwm
00506# ADD HYD + 1.0 02: N0 40240.01 23.285 No.date 56:09 11.89 n/a 000
00507# + 1.0 02: SW 2.597 No.date 29:22 12.20 n/a 000
00508# + 1.0 02: FL_CK 4945.00 14.839 No.date 32:25 14.57 n/a 000
00509# SIMM 1.0 01: S_N0 45099.01 33.166 No.date 37:08 12.20 n/a 000
00510#
00511# # Sum of hydrographs from Node 5 routed to Node 5A
00512# # Section 7
00513# #
00514# R002: C0057# -> Dfm=1D NDD -> AREAh-QPEAKm-TpeakDate-hh:mm--Rvmm-R.C.--Dfwm
00515# ROUTE CHANNEL -> 1.0 02: S_NA 45409.01 33.166 No.date 37:08 12.20 n/a 000
00516# [RFE=1.00] out c 1.0 01: NA 45409.01 33.166 No.date 37:20 12.20 n/a 000
00517# [L/S=556. / 090.040]
00518# [Vmax=.443; Dmax=.937]
00519# #
00520# # Addition of Subwatershed 5A and Subwatershed 5A2 to Node 5A
00521# #
00522# R002: C0058# -> Dfm=1D NDD -> AREAh-QPEAKm-TpeakDate-hh:mm--Rvmm-R.C.--Dfwm
00523# ADD HYD + 1.0 02: N0A 45409.01 33.166 No.date 37:20 12.20 n/a 000
00524# + 1.0 02: SW5A2 20.00 .309 No.date 28:36 17.79 n/a 000
00525# + 1.0 02: SW5A1 1412.00 3.090 No.date 38:04 15.22 n/a 000
00526# SIMM 1.0 01: S_NA 46841.01 36.216 No.date 37:28 12.30 n/a 000
00527#
00528# # Sum of hydrographs from Node 5A routed to Node 4
00529# # Section 8
00530# #
00531# R002: C0059# -> Dfm=1D NDD -> AREAh-QPEAKm-TpeakDate-hh:mm--Rvmm-R.C.--Dfwm
00532# ROUTE CHANNEL -> 1.0 02: S_NA 46841.01 36.216 No.date 37:28 12.30 n/a 000
00533# [RFE=1.00] out c 1.0 01: NA 46841.01 35.288 No.date 39:22 12.30 n/a 000
00534# [L/S=4630. / 043.035]
00535# [Vmax=.695; Dmax=2.444]
00536# #
00537# # Addition of Subwatershed 4 and Leamy Creek to Node 4
00538# #
00539# R002: C0060# -> Dfm=1D NDD -> AREAh-QPEAKm-TpeakDate-hh:mm--Rvmm-R.C.--Dfwm
00540# ADD HYD + 1.0 02: SW4 585.00 4.325 No.date 29:58 17.79 n/a 000
00541# + 1.0 02: LM_CK 1621.00 5.747 No.date 30:50 17.79 n/a 000
00542# + 1.0 01: S_N 48447.00 37.581 No.date 38:13 12.47 n/a 000
00543# SIMM 1.0 01: S_N0 48447.00 37.581 No.date 38:13 12.47 n/a 000
00544#
00545# # Sum of hydrographs from Node 4 routed to Node 2
00546# # Section 9
00547# #
00548# R002: C0061# -> Dfm=1D NDD -> AREAh-QPEAKm-TpeakDate-hh:mm--Rvmm-R.C.--Dfwm
00549# ADD HYD + 1.0 02: N0 48447.00 37.581 No.date 38:13 12.47 n/a 000
00550#
00551# #
00552# R002: C0062# -> Dfm=1D NDD -> AREAh-QPEAKm-TpeakDate-hh:mm--Rvmm-R.C.--Dfwm
00553# ROUTE CHANNEL -> 1.0 02: S_N 48447.00 37.581 No.date 38:13 12.47 n/a 000
00554# [RFE=1.00] out c 1.0 01: N0 48447.00 37.581 No.date 38:13 12.47 n/a 000
00555# [L/S=1667. / 060.040]
00556# [Vmax=.715; Dmax=2.845]
00557# #
00558# # Addition of Subwatershed 2 with Mbohan Drain and Smith Drain to Node 2
00559# #
00560# R002: C0063# -> Dfm=1D NDD -> AREAh-QPEAKm-TpeakDate-hh:mm--Rvmm-R.C.--Dfwm
00561# ADD HYD + 1.0 02: N0 48447.00 37.581 No.date 38:49 12.47 n/a 000

```


02993 # Sum of hydrographs from Node 12 routed to Node 11
02994 # (Approximated cross-section 258)
02995 # like n=0.04 for summer conditions and n=0.025 for spring conditions
02996 #
02997 # Sum of hydrographs from Node 12 routed to Node 11 with Dunny section 248
02998 #
02999 #
03000 #
03001 #
03002 #
03003 #
03004 #
03005 # Addition of Subwatershed 11 and No Name Creek to Node 11
03006 #
03007 #
03008 #
03009 #
03010 #
03011 #
03012 #
03013 # Sum of hydrographs from Node 11 routed to Node 10
03014 # Section 1
03015 #
03016 #
03017 #
03018 #
03019 #
03020 #
03021 #
03022 # Addition of Subwatershed 10 to Node 10
03023 #
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03039 # Sum of hydrographs from Node 10 routed to Node 9
03040 # Section 2
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03042 #
03043 #
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03048 # Addition of Subwatershed 9 and Nichols Creek to Node 9
03049 #
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03056 # Sum of hydrographs from Node 9 routed to Node 8
03057 # Section 3
03058 #
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03062 #
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03064 #
03065 # Addition of Subwatershed 8 and Hobbs' Drain to Node 8
03066 #
03067 #
03068 #
03069 #
03070 #
03071 #
03072 #
03073 # Sum of hydrographs from Node 8 routed to Node 7
03074 # Section 4
03075 #
03076 #
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03081 #
03082 # Addition of Subwatershed 7 to Node 7
03083 #
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03180 # Sum of hydrographs from Node 4 routed to Node 2
03181 # Section 5
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Table with columns for ID, Name, Description, and various numerical values. The table contains a dense list of project entries with associated technical specifications and data points.

Table with columns for component ID, name, parameters (Fow, Frc, F3, F13, F14, Fw, F0), area, and various status indicators (0/1/2/3/4/5). Rows are numbered from 041155 to 045015. Includes detailed component specifications and system modeling information.

052375 SAVE HYD ... 0.01:SN,M ... 55194.85 70.602 No,date 37:03 18.87 n/a ... 0000
052388 remark:Total Flows at Jockvale Road
052389 # Hydrograph from Jockvale Road routed to Heart's Desire
052414 # Channel X-Section obtained from RCVA Hydraulic Model - Station 689
052425 # Dtm=1-D NDD ... AREHA-QPEAKm-TPeakDte,hb,mm ... Rvmm,R,C ... DWfcms
052445 ROUTE CHANNEL ... 1.0:01:SN,IE ... 55194.85 70.452 No,date 37:20 18.87 n/a ... 0000
052446 [RDT=1.00] out ... 1.0:01:N,DE ... 55194.85 70.452 No,date 37:20 18.87 n/a ... 0000
052447 [L/S/a=1062 / 2287.98] ... 1.0:01:RES,DE ... 1.59 No,date 28:03 18.87 n/a ... 0000
052448 [Vmax=1.303;Dmax=1.891]
052489 # Catchment DESIRE
052513 # - To Jock River (north of the Jock)
052529 # Routing file comments: Based on various calibration exercises in Oua
052534 R0005:CO0193 ... Dtm=1-D NDD ... AREHA-QPEAKm-TPeakDte,hb,mm ... Rvmm,R,C ... DWfcms
052555 CONTINUES NASHDD ... 1.0:01:RE,DE ... 3680 11.879 No,date 36:59 20.23 n/a ... 0000
052566 [I=REC=4.00;SM=36.75;SMX=264.99;SK=010]
052567 [I=REC=4.00;SM=36.75;SMX=264.99;SK=010]
052568 [I=REC=4.00;SM=36.75;SMX=264.99;SK=010]
052569 [I=REC=4.00;SM=36.75;SMX=264.99;SK=010]
052570 [I=REC=4.00;SM=36.75;SMX=264.99;SK=010]
052571 [I=REC=4.00;SM=36.75;SMX=264.99;SK=010]
052572 [I=REC=4.00;SM=36.75;SMX=264.99;SK=010]
052573 [I=REC=4.00;SM=36.75;SMX=264.99;SK=010]
052574 [I=REC=4.00;SM=36.75;SMX=264.99;SK=010]
052575 [I=REC=4.00;SM=36.75;SMX=264.99;SK=010]
052576 [I=REC=4.00;SM=36.75;SMX=264.99;SK=010]
052577 [I=REC=4.00;SM=36.75;SMX=264.99;SK=010]
052578 [I=REC=4.00;SM=36.75;SMX=264.99;SK=010]
052579 [I=REC=4.00;SM=36.75;SMX=264.99;SK=010]
052580 [I=REC=4.00;SM=36.75;SMX=264.99;SK=010]
052581 [I=REC=4.00;SM=36.75;SMX=264.99;SK=010]
052582 [I=REC=4.00;SM=36.75;SMX=264.99;SK=010]
052583 [I=REC=4.00;SM=36.75;SMX=264.99;SK=010]
052584 [I=REC=4.00;SM=36.75;SMX=264.99;SK=010]
052685 remark:Total Flows at nd first pond
052875 # Jockvale SWM Facility
052889 # Rating curve obtained from Jockvale Servicing Study (CCL 1999)
052901 R0005:CO0197 ... Dtm=1-D NDD ... AREHA-QPEAKm-TPeakDte,hb,mm ... Rvmm,R,C ... DWfcms
052925 ROUTE RESERVOIR ... 1.0:02:JOCKVA ... 257.63 14.675 No,date 28:09 35.73 n/a ... 0000
052926 [RDT=1.00] out ... 1.0:02:JOCKVA ... 257.63 14.675 No,date 28:09 35.73 n/a ... 0000
052927 [I=REC=4.00;SM=36.67;SMX=264.49;SK=010]
052928 [I=REC=4.00;SM=36.67;SMX=264.49;SK=010]
052929 [I=REC=4.00;SM=36.67;SMX=264.49;SK=010]
052930 [I=REC=4.00;SM=36.67;SMX=264.49;SK=010]
052931 [I=REC=4.00;SM=36.67;SMX=264.49;SK=010]
052932 [I=REC=4.00;SM=36.67;SMX=264.49;SK=010]
052933 [I=REC=4.00;SM=36.67;SMX=264.49;SK=010]
052934 [I=REC=4.00;SM=36.67;SMX=264.49;SK=010]
052935 [I=REC=4.00;SM=36.67;SMX=264.49;SK=010]
052936 [I=REC=4.00;SM=36.67;SMX=264.49;SK=010]
052937 [I=REC=4.00;SM=36.67;SMX=264.49;SK=010]
052938 [I=REC=4.00;SM=36.67;SMX=264.49;SK=010]
052939 [I=REC=4.00;SM=36.67;SMX=264.49;SK=010]
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053100 R0005:CO0400 ... Dtm=1-D NDD ... AREHA-QPEAKm-TPeakDte,hb,mm ... Rvmm,R,C ... DWfcms
053115 ROUTE CHANNEL ... 1.0:02:SN,IE ... 55476.26 71.017 No,date 37:17 18.95 n/a ... 0000
053122 [RDT=1.00] out ... 1.0:02:SN,IE ... 55476.26 71.017 No,date 37:17 18.95 n/a ... 0000
053123 [L/S/a=563 / 967.045]
053144 [Vmax=1.676;Dmax=1.91]
053145 # Catchment S-2
053176 # - To Jock River (north and south)
053189 # Undeveloped floodplain and river
053200 R0005:CO0401 ... Dtm=1-D NDD ... AREHA-QPEAKm-TPeakDte,hb,mm ... Rvmm,R,C ... DWfcms
053225 CONTINUES NASHDD ... 1.0:01:RE,DE ... 102.94 2.262 No,date 28:20 19.00 .333 .000
053232 [I=REC=4.00;SM=36.75;SMX=264.99;SK=010]
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053288 [I=REC=4.00;SM=36.75;SMX=264.99;SK=010]
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053300 R0005:CO0403 ... Dtm=1-D NDD ... AREHA-QPEAKm-TPeakDte,hb,mm ... Rvmm,R,C ... DWfcms
053325 SAVE HYD ... 1.0:01:SN,NI ... 55579.20 71.168 No,date 37:08 18.95 n/a ... 0000
053331 # Save Hydrograph at Riveau River
053332 # Save Hydrograph at Riveau River
053333 # Save Hydrograph at Riveau River
053334 # END OF RUN : 9
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056113 # (Vmax = .546; Dmax = 1.499)
056128 #
056133 # Addition of Subwatershed Jack River at Ashton to Node 12
056143 #
056153 # R010: C00036 ----- DfIn-ID NND ----- AREQA-QPEAKm-TpeakDte-hh:mm ----- Rvmm-R-C- -DfWcm
056160 # ADD HYD + 1.0 02: S_N2 7725.00 3,519.00 date 61:53 18.46 n/a 0.00
056175 # 1.0 02: IR_ASH 1781.00 10,819.00 date 32:42 24.81 n/a 0.00
056188 # SIML 1.0 01: S_N2 9706.00 12,834.00 date 32:45 19.65 n/a 0.00
056199 # R010: C00037 ----- DfIn-ID NND ----- AREQA-QPEAKm-TpeakDte-hh:mm ----- Rvmm-R-C- -DfWcm
056200 # SAVE HYD 1.0 01: S_N2 9506.00 12,834.00 date 32:45 19.65 n/a 0.00
056211 # frame_HLSN2
056222 # remark:flow at 8_N12 near Ashton
056233 #
056243 # Sum of hydrographs from Node 12 routed to Node 11
056253 # (Approximate cross-section - see cross-section 258)
056263 # like n=0.04 for summer conditions and n=0.025 for spring conditions
056273 #
056283 # Sum of hydrographs from Node 12 routed to Node 11 with Dumpy section 248
056293 #
056303 # R010: C00038 ----- DfIn-ID NND ----- AREQA-QPEAKm-TpeakDte-hh:mm ----- Rvmm-R-C- -DfWcm
056313 # ROUTE CHANNEL -> 1.0 02: S_N2 9506.00 55,834.00 date 32:45 19.65 n/a 0.00
056323 # [RfE 1.00] out c 1.0 01: Dm1 9506.00 12,710.00 date 33:02 19.65 n/a 0.00
056333 # [L/S = 972 / 0.50 / 0.40]
056343 # (Vmax = .680; Dmax = 2.598)
056353 #
056363 # Addition of Subwatershed 11 and No Name Creek to Node 11
056373 #
056383 # R010: C00039 ----- DfIn-ID NND ----- AREQA-QPEAKm-TpeakDte-hh:mm ----- Rvmm-R-C- -DfWcm
056393 # ADD HYD + 1.0 02: Dm1 9506.00 12,710.00 date 33:02 19.65 n/a 0.00
056403 # 1.0 02: SW11 500.00 5,639.00 date 29:22 21.19 n/a 0.00
056413 # 1.0 02: NC_CK 1917.00 7,897.00 date 24:28 21.19 n/a 0.00
056423 # SIML 1.0 01: S_N1 11923.00 21,813.00 date 33:05 19.96 n/a 0.00
056433 #
056443 # Sum of hydrographs from Node 11 routed to Node 10
056453 # Section 1
056463 #
056473 # R010: C00040 ----- DfIn-ID NND ----- AREQA-QPEAKm-TpeakDte-hh:mm ----- Rvmm-R-C- -DfWcm
056483 # ROUTE CHANNEL -> 1.0 02: S_N1 11923.00 21,813.00 date 33:05 19.96 n/a 0.00
056493 # [RfE 1.00] out c 1.0 01: N0 11923.00 14,761.00 date 39:58 19.96 n/a 0.00
056503 # [L/S = 44028 / 1.57 / 0.40]
056513 # (Vmax = .452; Dmax = 1.212)
056523 #
056533 # Addition of Subwatershed 10 to Node 10
056543 #
056553 # R010: C00041 ----- DfIn-ID NND ----- AREQA-QPEAKm-TpeakDte-hh:mm ----- Rvmm-R-C- -DfWcm
056563 # ADD HYD + 1.0 02: N0 11923.00 14,761.00 date 39:58 19.96 n/a 0.00
056573 # 1.0 02: SW10 5666.00 21,255.00 date 37:58 24.81 n/a 0.00
056583 # SIML 1.0 01: S_N0 17589.00 35,808.00 date 38:35 21.52 n/a 0.00
056593 # R010: C00042 ----- DfIn-ID NND ----- AREQA-QPEAKm-TpeakDte-hh:mm ----- Rvmm-R-C- -DfWcm
056603 # SAVE HYD 1.0 01: S_N0 17589.00 35,808.00 date 38:35 21.52 n/a 0.00
056613 # frame_HLSN0
056623 # remark:flow at S_N0: N0 + SW10
056633 # Addition of Kings Creek to S_N10
056643 #
056653 # R010: C00043 ----- DfIn-ID NND ----- AREQA-QPEAKm-TpeakDte-hh:mm ----- Rvmm-R-C- -DfWcm
056663 # ADD HYD + 1.0 02: S_N0 17589.00 35,808.00 date 38:35 21.52 n/a 0.00
056673 # 1.0 02: NC_CK 8376.00 20,208.00 date 39:59 21.19 n/a 0.00
056683 # SIML 1.0 01: S_N0A 25965.00 55,807.00 date 39:58 21.41 n/a 0.00
056693 #
056703 # Sum of hydrographs from Node 10 routed to Node 9
056713 # Section 2
056723 #
056733 # R010: C00044 ----- DfIn-ID NND ----- AREQA-QPEAKm-TpeakDte-hh:mm ----- Rvmm-R-C- -DfWcm
056743 # ROUTE CHANNEL -> 1.0 02: S_N1 11923.00 21,813.00 date 33:05 19.96 n/a 0.00
056753 # [RfE 1.00] out c 1.0 01: N0 25965.00 54,076.00 date 39:59 21.41 n/a 0.00
056763 # [L/S = 3982 / 0.70 / 0.50]
056773 # (Vmax = .682; Dmax = 1.695)
056783 #
056793 # Addition of Subwatershed 9 and Nichols Creek to Node 9
056803 #
056813 # R010: C00045 ----- DfIn-ID NND ----- AREQA-QPEAKm-TpeakDte-hh:mm ----- Rvmm-R-C- -DfWcm
056823 # ADD HYD + 1.0 02: N0 25965.00 54,076.00 date 39:59 21.41 n/a 0.00
056833 # 1.0 02: SW9 1132.00 8,921.00 date 30:54 23.73 n/a 0.00
056843 # 1.0 02: NC_CK 4464.00 10,128.00 date 39:59 19.29 n/a 0.00
056853 # SIML 1.0 01: S_N0A 31561.00 66,284.00 date 39:59 21.20 n/a 0.00
056863 #
056873 # Sum of hydrographs from Node 9 routed to Node 8
056883 # Section 3
056893 #
056903 # R010: C00046 ----- DfIn-ID NND ----- AREQA-QPEAKm-TpeakDte-hh:mm ----- Rvmm-R-C- -DfWcm
056913 # ROUTE CHANNEL -> 1.0 02: S_N 31561.00 66,284.00 date 39:59 21.20 n/a 0.00
056923 # [RfE 1.00] out c 1.0 01: N8 31561.00 61,483.00 date 39:57 21.20 n/a 0.00
056933 # [L/S = 2209 / 0.88 / 0.40]
056943 # (Vmax = .363; Dmax = 1.619)
056953 #
056963 # Addition of Subwatershed 8 and Hobbs' Drain to Node 8
056973 #
056983 # R010: C00047 ----- DfIn-ID NND ----- AREQA-QPEAKm-TpeakDte-hh:mm ----- Rvmm-R-C- -DfWcm
056993 # ADD HYD + 1.0 02: N8 31561.00 61,483.00 date 39:57 21.20 n/a 0.00
057003 # 1.0 02: SW8 131.00 8,921.00 date 30:54 23.73 n/a 0.00
057013 # 1.0 02: HB_DR 3854.00 11,811.00 date 38:37 21.19 n/a 0.00
057023 # SIML 1.0 01: S_N 35546.00 73,344.00 date 39:57 21.19 n/a 0.00
057033 #
057043 # Sum of hydrographs from Node 8 routed to Node 7
057053 # Section 4
057063 #
057073 # R010: C00048 ----- DfIn-ID NND ----- AREQA-QPEAKm-TpeakDte-hh:mm ----- Rvmm-R-C- -DfWcm
057083 # ROUTE CHANNEL -> 1.0 02: S_N 35546.00 73,344.00 date 39:57 21.19 n/a 0.00
057093 # [RfE 1.00] out c 1.0 01: N7 35546.00 61,416.00 date 45:01 21.19 n/a 0.00
057103 # [L/S = 2760 / 0.59 / 0.40]
057113 # (Vmax = .218; Dmax = 1.987)
057123 #
057133 # Addition of Subwatershed 7 to Node 7
057143 #
057153 # R010: C00049 ----- DfIn-ID NND ----- AREQA-QPEAKm-TpeakDte-hh:mm ----- Rvmm-R-C- -DfWcm
057163 # ADD HYD + 1.0 02: N7 35546.00 61,416.00 date 45:01 21.19 n/a 0.00
057173 # 1.0 02: SW7 3197.00 8,809.00 date 36:26 17.07 n/a 0.00
057183 # SIML 1.0 01: S_N7 38743.00 65,819.00 date 44:06 20.85 n/a 0.00
057193 # R010: C00050 ----- DfIn-ID NND ----- AREQA-QPEAKm-TpeakDte-hh:mm ----- Rvmm-R-C- -DfWcm
057203 # SAVE HYD 1.0 01: S_N7 38743.00 65,819.00 date 44:06 20.85 n/a 0.00
057213 # frame_HLSN7
057223 # remark:flow at S_N7: N7 + SW7
057233 # Insertion of a reservoir to simulate the effects of the Richmond Fen.
057243 # Storage area and volumes were estimated from available topo maps.
057253 # Release rate from Fen was assumed to be controlled by the downstream
057263 # river cross section for summer conditions. It was assumed that for up to
057273 # 0.75 m of water, the main channel of the river provided the storage. Above
057283 # this depth, the wetland stores to significantly store water.
057293 #
057303 # R010: C00051 ----- DfIn-ID NND ----- AREQA-QPEAKm-TpeakDte-hh:mm ----- Rvmm-R-C- -DfWcm
057313 # ROUTE CHANNEL -> 1.0 01: RES_RF 38743.00 31,796.00 date 60:32 20.85 n/a 0.00
057323 # [RfE 1.00] out c 1.0 01: RES_RF 38743.00 31,796.00 date 60:32 20.85 n/a 0.00
057333 # (M&S St&D= 2597E0)
057343 # R010: C00052 ----- DfIn-ID NND ----- AREQA-QPEAKm-TpeakDte-hh:mm ----- Rvmm-R-C- -DfWcm
057353 # SAVE HYD 1.0 01: RES_RF 38743.00 31,796.00 date 60:32 20.85 n/a 0.00
057363 # frame_HRESRF
057373 # remark:flow of Richmond Fen
057383 #
057393 # Sum of hydrographs from Node 7 routed to Node 6
057403 # Section 5
057413 #
057423 # R010: C00053 ----- DfIn-ID NND ----- AREQA-QPEAKm-TpeakDte-hh:mm ----- Rvmm-R-C- -DfWcm
057433 # ROUTE CHANNEL -> 1.0 02: S_N 38743.00 31,796.00 date 60:32 20.85 n/a 0.00
057443 # [RfE 1.00] out c 1.0 01: N6 38743.00 31,737.00 date 62:00 20.85 n/a 0.00
057453 # [L/S = 3056 / 0.82 / 0.25]
057463 # (Vmax = .477; Dmax = .960)
057473 #
057483 # Addition of Subwatershed 6 and Van Gaal Drain to Node 6
057493 #
057503 # R010: C00054 ----- DfIn-ID NND ----- AREQA-QPEAKm-TpeakDte-hh:mm ----- Rvmm-R-C- -DfWcm
057513 # ADD HYD + 1.0 02: N6 38743.00 31,737.00 date 62:00 20.85 n/a 0.00
057523 # 1.0 02: SW6 165.00 818.00 date 33:04 21.69 n/a 0.00
057533 # 1.0 02: VG_DR 1332.00 6,069.00 date 35:17 24.81 n/a 0.00
057543 # SIML 1.0 01: S_N 40240.01 31,737.00 date 62:00 20.99 n/a 0.00
057553 #
057563 # Sum of hydrographs from Node 6 routed to Node 5
057573 # Section 6
057583 #
057593 # R010: C00055 ----- DfIn-ID NND ----- AREQA-QPEAKm-TpeakDte-hh:mm ----- Rvmm-R-C- -DfWcm
057603 # ROUTE CHANNEL -> 1.0 02: S_N 40240.01 31,737.00 date 62:00 20.99 n/a 0.00
057613 # [RfE 1.00] out c 1.0 01: N5 40240.01 31,713.00 date 62:48 20.99 n/a 0.00
057623 # [L/S = 182 / 0.50 / 0.50]
057633 # (Vmax = .412; Dmax = 1.069)
057643 #
057653 # Addition of Subwatershed 5 and Flowing Creek to Node 5
057663 #
057673 # R010: C00056 ----- DfIn-ID NND ----- AREQA-QPEAKm-TpeakDte-hh:mm ----- Rvmm-R-C- -DfWcm
057683 # ADD HYD + 1.0 02: N5 40240.01 31,713.00 date 62:48 20.99 n/a 0.00
057693 # 1.0 02: FC 4025.00 5,246.00 date 28:26 21.56 n/a 0.00
057703 # 1.0 02: FL_CK 1612.00 49,451.00 date 33:21 25.91 n/a 0.00
057713 # SIML 1.0 01: S_N 45409.01 51,448.00 date 34:54 21.56 n/a 0.00
057723 #
057733 # Sum of hydrographs from Node 5 routed to Node 5A
057743 # Section 7
057753 #
057763 # R010: C00057 ----- DfIn-ID NND ----- AREQA-QPEAKm-TpeakDte-hh:mm ----- Rvmm-R-C- -DfWcm
057773 # ROUTE CHANNEL -> 1.0 02: S_N 45409.01 51,448.00 date 34:54 21.56 n/a 0.00
057783 # [RfE 1.00] out c 1.0 01: N5A 45409.01 51,312.00 date 35:12 21.56 n/a 0.00
057793 # [L/S = 556 / 0.90 / 0.40]
057803 # (Vmax = .485; Dmax = 1.131)
057813 #
057823 # Addition of Subwatershed 5A and Subwatershed 5A2 to Node 5A
057833 #
057843 # R010: C00058 ----- DfIn-ID NND ----- AREQA-QPEAKm-TpeakDte-hh:mm ----- Rvmm-R-C- -DfWcm
057853 # ADD HYD + 1.0 02: N5A 45409.01 51,312.00 date 35:12 21.56 n/a 0.00
057863 # 1.0 02: SW5A 20.00 614.00 date 28:36 31.27 n/a 0.00
057873 # 1.0 02: SW_SAI 1612.00 5,817.00 date 37:54 27.06 n/a 0.00
057883 # SIML 1.0 01: S_N5A 46844.01 56,788.00 date 35:22 21.73 n/a 0.00
057893 #
057903 # Sum of hydrographs from Node 5A routed to Node 4
057913 # Section 8
057923 #
057933 # R010: C00059 ----- DfIn-ID NND ----- AREQA-QPEAKm-TpeakDte-hh:mm ----- Rvmm-R-C- -DfWcm
057943 # ROUTE CHANNEL -> 1.0 02: S_N5A 46844.01 56,788.00 date 35:22 21.73 n/a 0.00
057953 # [RfE 1.00] out c 1.0 01: N4 46844.01 54,543.00 date 36:36 21.73 n/a 0.00
057963 # [L/S = 4630 / 0.40 / 0.50]
057973 # (Vmax = .793; Dmax = 3.295)

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Table with multiple columns containing alphanumeric codes, descriptions of water flow and treatment processes, and numerical data points. Includes headers like 'Flow at MB33', 'Flow at MB03', and various flow rates and dates.

082729 # [MS0105da-1192E03 ml]
082730 #
082731 R0025: C00034 DfIn a-ID NND AREAh-QPEAGcm-TpeakDte,hb-mm Rvmm R.C. DfCwm
082732 SAVE HYD 1.0 01:RES_GM 7725.00 3.678_NDate 60:27 23.52 n/a 000
082733 # name : H_RESGM
082734 # remark : Outflow from Res GM
082735 # Output of Reservoir Groundwater cross-section from Node 13A to Node 12
082736 # (Approximated cross-section - see cross-section 258)

084166 ADD HYD 1.0 02:SA 54509.01 62.487_NDate 34:43 27.43 n/a 000
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089775	#	Catchment FOSTER	091645	CONTINUOUS STANDHID	1.0 0.01: S-1-D	2.03	.369	Ndate	28.00	57.38	771	000
089785	#	to Foster ditch (north of Jack)	091655	[M]P= 65;T[MP]= 65]								
089800	#	to Foster ditch (north of Jack)	091665	[L]SS= 2;C[]= 70.00]								
089810	#	2020-12-01 JFSA Foster area is 332 ac per Foster SWP Environmental Study Report, CH2MHILL, Aug. 2013	091675	[P]ervious area: A[per]= 4.67;S[LP]= 2.00;L[GP]= 40.0;M[DP]= 250;S[CP]= 0]								
089825	#	2020-12-01 decrease Foster drainage area from (373 BA) to (307.98 HA) after increasing Koeffe drainage area to 15	091685	[I]mperVIOUS area: I[AM]= 1.57;S[LP]= 1.00;L[GP]= 45.0;M[DP]= 250;S[CP]= 0]								
089835	#	2020-12-01 update Foster area to 325.45 ac as measured from QDES	091695	[I]R[]C[]= 4.00; I[ARE]R[]= 4.00]								
089845	#	091700	091710	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]								
089855	R0025: C00153	091715	091725	CATCHMENT WCLAR								
089865	#	CNTINUOUS STANDHID	091735	[M]P= 65;T[MP]= 65]								
089875	#	[L]SS= 2;C[]= 70.00]	091745	[P]ervious area: A[per]= 4.67;S[LP]= 2.00;L[GP]= 40.0;M[DP]= 250;S[CP]= 0]								
089885	#	[I]mperVIOUS area: I[AM]= 1.57;S[LP]= 1.00;L[GP]= 45.0;M[DP]= 250;S[CP]= 0]	091755	[I]R[]C[]= 4.00; I[ARE]R[]= 4.00]								
089895	#	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]	091765	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]								
089905	R0025: C00175	091775	091785	CATCHMENT WCLAR								
089915	#	CNTINUOUS STANDHID	091795	[M]P= 65;T[MP]= 65]								
089925	#	[L]SS= 2;C[]= 70.00]	091805	[P]ervious area: A[per]= 4.67;S[LP]= 2.00;L[GP]= 40.0;M[DP]= 250;S[CP]= 0]								
089935	#	[I]mperVIOUS area: I[AM]= 1.57;S[LP]= 1.00;L[GP]= 45.0;M[DP]= 250;S[CP]= 0]	091815	[I]R[]C[]= 4.00; I[ARE]R[]= 4.00]								
089945	#	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]	091825	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]								
089955	R0025: C00185	091835	091845	CATCHMENT WCLAR								
089965	#	CNTINUOUS STANDHID	091855	[M]P= 65;T[MP]= 65]								
089975	#	[L]SS= 2;C[]= 70.00]	091865	[P]ervious area: A[per]= 4.67;S[LP]= 2.00;L[GP]= 40.0;M[DP]= 250;S[CP]= 0]								
089985	#	[I]mperVIOUS area: I[AM]= 1.57;S[LP]= 1.00;L[GP]= 45.0;M[DP]= 250;S[CP]= 0]	091875	[I]R[]C[]= 4.00; I[ARE]R[]= 4.00]								
089995	#	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]	091885	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]								
090005	R0025: C00195	091895	091905	CATCHMENT WCLAR								
090015	#	CNTINUOUS STANDHID	091915	[M]P= 65;T[MP]= 65]								
090025	#	[L]SS= 2;C[]= 70.00]	091925	[P]ervious area: A[per]= 4.67;S[LP]= 2.00;L[GP]= 40.0;M[DP]= 250;S[CP]= 0]								
090035	#	[I]mperVIOUS area: I[AM]= 1.57;S[LP]= 1.00;L[GP]= 45.0;M[DP]= 250;S[CP]= 0]	091935	[I]R[]C[]= 4.00; I[ARE]R[]= 4.00]								
090045	#	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]	091945	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]								
090055	R0025: C00205	091955	091965	CATCHMENT WCLAR								
090065	#	CNTINUOUS STANDHID	091975	[M]P= 65;T[MP]= 65]								
090075	#	[L]SS= 2;C[]= 70.00]	091985	[P]ervious area: A[per]= 4.67;S[LP]= 2.00;L[GP]= 40.0;M[DP]= 250;S[CP]= 0]								
090085	#	[I]mperVIOUS area: I[AM]= 1.57;S[LP]= 1.00;L[GP]= 45.0;M[DP]= 250;S[CP]= 0]	091995	[I]R[]C[]= 4.00; I[ARE]R[]= 4.00]								
090095	#	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]	092005	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]								
090105	R0025: C00215	092015	092025	CATCHMENT WCLAR								
090115	#	CNTINUOUS STANDHID	092035	[M]P= 65;T[MP]= 65]								
090125	#	[L]SS= 2;C[]= 70.00]	092045	[P]ervious area: A[per]= 4.67;S[LP]= 2.00;L[GP]= 40.0;M[DP]= 250;S[CP]= 0]								
090135	#	[I]mperVIOUS area: I[AM]= 1.57;S[LP]= 1.00;L[GP]= 45.0;M[DP]= 250;S[CP]= 0]	092055	[I]R[]C[]= 4.00; I[ARE]R[]= 4.00]								
090145	#	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]	092065	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]								
090155	R0025: C00225	092075	092085	CATCHMENT WCLAR								
090165	#	CNTINUOUS STANDHID	092095	[M]P= 65;T[MP]= 65]								
090175	#	[L]SS= 2;C[]= 70.00]	092105	[P]ervious area: A[per]= 4.67;S[LP]= 2.00;L[GP]= 40.0;M[DP]= 250;S[CP]= 0]								
090185	#	[I]mperVIOUS area: I[AM]= 1.57;S[LP]= 1.00;L[GP]= 45.0;M[DP]= 250;S[CP]= 0]	092115	[I]R[]C[]= 4.00; I[ARE]R[]= 4.00]								
090195	#	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]	092125	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]								
090205	R0025: C00235	092135	092145	CATCHMENT WCLAR								
090215	#	CNTINUOUS STANDHID	092155	[M]P= 65;T[MP]= 65]								
090225	#	[L]SS= 2;C[]= 70.00]	092165	[P]ervious area: A[per]= 4.67;S[LP]= 2.00;L[GP]= 40.0;M[DP]= 250;S[CP]= 0]								
090235	#	[I]mperVIOUS area: I[AM]= 1.57;S[LP]= 1.00;L[GP]= 45.0;M[DP]= 250;S[CP]= 0]	092175	[I]R[]C[]= 4.00; I[ARE]R[]= 4.00]								
090245	#	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]	092185	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]								
090255	R0025: C00245	092195	092205	CATCHMENT WCLAR								
090265	#	CNTINUOUS STANDHID	092215	[M]P= 65;T[MP]= 65]								
090275	#	[L]SS= 2;C[]= 70.00]	092225	[P]ervious area: A[per]= 4.67;S[LP]= 2.00;L[GP]= 40.0;M[DP]= 250;S[CP]= 0]								
090285	#	[I]mperVIOUS area: I[AM]= 1.57;S[LP]= 1.00;L[GP]= 45.0;M[DP]= 250;S[CP]= 0]	092235	[I]R[]C[]= 4.00; I[ARE]R[]= 4.00]								
090295	#	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]	092245	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]								
090305	R0025: C00255	092255	092265	CATCHMENT WCLAR								
090315	#	CNTINUOUS STANDHID	092275	[M]P= 65;T[MP]= 65]								
090325	#	[L]SS= 2;C[]= 70.00]	092285	[P]ervious area: A[per]= 4.67;S[LP]= 2.00;L[GP]= 40.0;M[DP]= 250;S[CP]= 0]								
090335	#	[I]mperVIOUS area: I[AM]= 1.57;S[LP]= 1.00;L[GP]= 45.0;M[DP]= 250;S[CP]= 0]	092295	[I]R[]C[]= 4.00; I[ARE]R[]= 4.00]								
090345	#	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]	092305	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]								
090355	R0025: C00265	092315	092325	CATCHMENT WCLAR								
090365	#	CNTINUOUS STANDHID	092335	[M]P= 65;T[MP]= 65]								
090375	#	[L]SS= 2;C[]= 70.00]	092345	[P]ervious area: A[per]= 4.67;S[LP]= 2.00;L[GP]= 40.0;M[DP]= 250;S[CP]= 0]								
090385	#	[I]mperVIOUS area: I[AM]= 1.57;S[LP]= 1.00;L[GP]= 45.0;M[DP]= 250;S[CP]= 0]	092355	[I]R[]C[]= 4.00; I[ARE]R[]= 4.00]								
090395	#	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]	092365	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]								
090405	R0025: C00275	092375	092385	CATCHMENT WCLAR								
090415	#	CNTINUOUS STANDHID	092395	[M]P= 65;T[MP]= 65]								
090425	#	[L]SS= 2;C[]= 70.00]	092405	[P]ervious area: A[per]= 4.67;S[LP]= 2.00;L[GP]= 40.0;M[DP]= 250;S[CP]= 0]								
090435	#	[I]mperVIOUS area: I[AM]= 1.57;S[LP]= 1.00;L[GP]= 45.0;M[DP]= 250;S[CP]= 0]	092415	[I]R[]C[]= 4.00; I[ARE]R[]= 4.00]								
090445	#	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]	092425	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]								
090455	R0025: C00285	092435	092445	CATCHMENT WCLAR								
090465	#	CNTINUOUS STANDHID	092455	[M]P= 65;T[MP]= 65]								
090475	#	[L]SS= 2;C[]= 70.00]	092465	[P]ervious area: A[per]= 4.67;S[LP]= 2.00;L[GP]= 40.0;M[DP]= 250;S[CP]= 0]								
090485	#	[I]mperVIOUS area: I[AM]= 1.57;S[LP]= 1.00;L[GP]= 45.0;M[DP]= 250;S[CP]= 0]	092475	[I]R[]C[]= 4.00; I[ARE]R[]= 4.00]								
090495	#	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]	092485	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]								
090505	R0025: C00295	092495	092505	CATCHMENT WCLAR								
090515	#	CNTINUOUS STANDHID	092515	[M]P= 65;T[MP]= 65]								
090525	#	[L]SS= 2;C[]= 70.00]	092525	[P]ervious area: A[per]= 4.67;S[LP]= 2.00;L[GP]= 40.0;M[DP]= 250;S[CP]= 0]								
090535	#	[I]mperVIOUS area: I[AM]= 1.57;S[LP]= 1.00;L[GP]= 45.0;M[DP]= 250;S[CP]= 0]	092535	[I]R[]C[]= 4.00; I[ARE]R[]= 4.00]								
090545	#	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]	092545	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]								
090555	R0025: C00305	092555	092565	CATCHMENT WCLAR								
090565	#	CNTINUOUS STANDHID	092575	[M]P= 65;T[MP]= 65]								
090575	#	[L]SS= 2;C[]= 70.00]	092585	[P]ervious area: A[per]= 4.67;S[LP]= 2.00;L[GP]= 40.0;M[DP]= 250;S[CP]= 0]								
090585	#	[I]mperVIOUS area: I[AM]= 1.57;S[LP]= 1.00;L[GP]= 45.0;M[DP]= 250;S[CP]= 0]	092595	[I]R[]C[]= 4.00; I[ARE]R[]= 4.00]								
090595	#	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]	092605	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]								
090605	R0025: C00315	092615	092625	CATCHMENT WCLAR								
090615	#	CNTINUOUS STANDHID	092635	[M]P= 65;T[MP]= 65]								
090625	#	[L]SS= 2;C[]= 70.00]	092645	[P]ervious area: A[per]= 4.67;S[LP]= 2.00;L[GP]= 40.0;M[DP]= 250;S[CP]= 0]								
090635	#	[I]mperVIOUS area: I[AM]= 1.57;S[LP]= 1.00;L[GP]= 45.0;M[DP]= 250;S[CP]= 0]	092655	[I]R[]C[]= 4.00; I[ARE]R[]= 4.00]								
090645	#	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]	092665	[S]M[]= 31.15; S[MW]= 225.45; S[]= 0.010]								
09												


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104735 # - To SWM Facility north of the Jack
10474 # Primary residential development
10475 #*****
10476 #*****
10477 CONTINUES STANDRD 1.0 01:MLLS 175.99 15.275 No.date 28:07 44.62 600 .000
10478 [XMP: 25; TI:MP: 38]
10479 [LGS: 2 (Cm 74.0)]
10480 [Pervious area: IArea 4.67; SLP:4.0; LCP= 40; MNP: 250; SCP= 0]
10481 [Impervious area: IArea 1.57; SLP:4.0; LCP= 1118; MNP: 013; SCP= 0]
10482 [IARECmp: 4.00; LAECP: 4.00]
10483 [SM: No. 67; SMAX: 54.96; SK: 010]
10484 #*****
10485 # Chapman Mills SWM Pond
10486 # Rating curve obtained from CCL hydraulic modeling
10487 #*****
10488 ROUTE RESERVOIR > 1.0 02:MLLS 175.99 15.275 No.date 28:07 44.62 n/a .000
10489 out < 1.0 01:MLL.P 162.60 4.675 No.date 28:16 44.62 n/a .000
10490 overflow < 1.0 01:MLL.OV 13.39 8.160 No.date 28:16 44.62 n/a .000
10491 [M&O: 2310(E)0] sub. Tot(DrVol= 5973(E)0) sub. N(DrV= 2, Tot(DrVol= hrs)]
10492 [M&O: 2310(E)0] sub. Tot(DrVol= 5973(E)0) sub. N(DrV= 2, Tot(DrVol= hrs)]
10493 ADD HYD + 1.0 02: N.M 55194.86 104.478 No.date 38:54 29.33 n/a .000
10494 + 1.0 02: M.D 13.39 8.160 No.date 28:16 44.62 n/a .000
10495 + 1.0 02: M.L.P 162.60 4.675 No.date 28:16 44.62 n/a .000
10496 SLM 1.0 01:SN.M 55194.86 104.675 No.date 38:54 29.33 n/a .000
10497 ROUTE: C030191 -> 1.0 01:SN.D 55194.86 104.675 No.date 38:54 29.33 n/a .000
10498 SAVED HYD 1.0 01:SN.M 55194.86 104.675 No.date 38:54 29.33 n/a .000
10499 #name : SN.M 0025
10500 remark: Total Flow at Jack Road
10501 #*****
10502 # Hydrograph from Jack Road routed to Heart's Desire
10503 # Channel X-Section obtained from RCV Hydraulic Model - Station 689
10504 #*****
10505 ROUTE: C030192 -> 1.0 01:SN.D 55194.86 104.675 No.date 38:54 29.33 n/a .000
10506 ROUTE CHANNEL > 1.0 01:SN.D 55194.86 104.478 No.date 39:12 29.33 n/a .000
10507 [R/S= 1962; / 227; / 045]
10508 [Vmax: 1.484; Dmax: 2.297]
10509 #*****
10510 # Catchment DESIRE
10511 # To Jack River (north of the Jack)
10512 #*****
10513 #*****
10514 #*****
10515 #*****
10516 ROUTE: C030193 -> 1.0 01:SN.D 55194.86 104.675 No.date 38:54 29.33 n/a .000
10517 CONTINUES STANDRD 1.0 01:DESIRE 25.78 2.161 No.date 28:03 40.77 548 .000
10518 [XMP: 25; TI:MP: 25]
10519 [LGS: 2 (Cm 74.0)]
10520 [Pervious area: IArea 4.67; SLP:4.0; LCP= 40; MNP: 250; SCP= 0]
10521 [Impervious area: IArea 1.57; SLP:4.0; LCP= 1118; MNP: 013; SCP= 0]
10522 [IARECmp: 4.00; LAECP: 4.00]
10523 [SM: No. 31.15; SMAX: 207.66; SK: 010]
10524 #*****
10525 # Catchment JOCKVA
10526 # To Jack River SWM Facility
10527 # Residential development & golf course
10528 # JFS: 2021-01-11 update JOCKVA after updating CORR Gas per THE GROUP, July 2008.
10529 # JOCKVA area became 257.63 ha. JOCKVA separated into two areas JOCKVA and EX LAND 32.5 ha as
10530 #*****
10531 ROUTE: C030194 -> 1.0 01:JOCKVA 225.13 21.797 No.date 28:07 50.08 673 .000
10532 CONTINUES STANDRD 1.0 01:JOCKVA 225.13 21.797 No.date 28:07 50.08 673 .000
10533 [XMP: 50; TI:MP: 50]
10534 [LGS: 2 (Cm 74.0)]
10535 [Pervious area: IArea 4.67; SLP:4.0; LCP= 40; MNP: 250; SCP= 0]
10536 [Impervious area: IArea 1.57; SLP:4.0; LCP= 1118; MNP: 013; SCP= 0]
10537 [IARECmp: 4.00; LAECP: 4.00]
10538 [SM: No. 36; SMAX: 287.66; SK: 010]
10539 ROUTE: C030195 -> 1.0 01:JOCKVA 225.13 21.797 No.date 28:07 50.08 673 .000
10540 ADD HYD + 1.0 02: EX.LAND.SM 32.50 2.275 No.date 27:52 50.26 n/a .000
10541 + 1.0 02: JOCKVA.SM 225.13 21.797 No.date 28:07 50.08 n/a .000
10542 + 1.0 02: R.M 0.00 0.00 No.date 0:00 0.00 n/a .000
10543 + 1.0 02: R.M 0.00 0.00 No.date 0:00 0.00 n/a .000
10544 SLM 1.0 01:JOCKVA.TO 257.63 24.072 No.date 28:07 50.10 n/a .000
10545 ROUTE: C030196 -> 1.0 01:JOCKVA 257.63 24.072 No.date 28:07 50.10 n/a .000
10546 SAVED HYD 1.0 01:JOCKVA.TO 257.63 24.072 No.date 28:07 50.10 n/a .000
10547 #name : JOCKVA.TO 0025
10548 remark: Total Flow at KB first pond
10549 #*****
10550 # Jack River SWM Facility
10551 # Rating curve obtained from Jack River Servicing Study (CCL 1999)
10552 #*****
10553 ROUTE: C030197 -> 1.0 01:SN.D 55194.86 104.478 No.date 39:12 29.33 n/a .000
10554 ROUTE RESERVOIR > 1.0 02:JOCKVA 257.63 24.072 No.date 28:07 50.10 n/a .000
10555 overflow < 1.0 01:JOCK.OV 257.63 9.145 No.date 28:37 50.10 n/a .000
10556 [M&O: 2310(E)0] sub. Tot(DrVol= 00000(E)0) sub. N(DrV= 0, Tot(DrVol= 0 hr)]
10557 [M&O: 2310(E)0] sub. Tot(DrVol= 00000(E)0) sub. N(DrV= 0, Tot(DrVol= 0 hr)]
10558 ADD HYD + 1.0 02: N.M 55194.86 104.478 No.date 39:12 29.33 n/a .000
10559 + 1.0 02: M.D 13.39 8.160 No.date 28:03 40.77 n/a .000
10560 + 1.0 02: JOCKVA.SM 225.13 21.797 No.date 28:07 50.08 n/a .000
10561 + 1.0 02: JOCKVA.SM 225.13 21.797 No.date 28:07 50.08 n/a .000
10562 SLM 1.0 01:SN.D 55194.86 104.478 No.date 39:11 29.43 n/a .000
10563 ROUTE: C030198 -> 1.0 01:SN.D 55194.86 104.478 No.date 39:11 29.43 n/a .000
10564 SAVED HYD 1.0 01:SN.D 55194.86 104.478 No.date 39:11 29.43 n/a .000
10565 #name : SN.D 0025
10566 remark: Total Flow at Heart's Desire
10567 #*****
10568 # Hydrograph from Heart's Desire routed to Rideau River
10569 # Channel X-Section obtained from RCV Hydraulic Model - Station 0
10570 #*****
10571 ROUTE: C030199 -> 1.0 01:SN.D 55194.86 104.478 No.date 39:11 29.43 n/a .000
10572 ROUTE CHANNEL > 1.0 02:SN.D 55194.86 104.478 No.date 39:11 29.43 n/a .000
10573 [R/S= 1.944; Dmax: 1.26]
10574 [L/S= 563; / 967; / 045]
10575 [Vmax: 1.944; Dmax: 1.26]
10576 #*****
10577 # Catchment R-2
10578 # To Jack River (north and south)
10579 # Undeveloped floodplain and river
10580 #*****
10581 #*****
10582 ROUTE: C030200 -> 1.0 01:SN.D 55194.86 104.478 No.date 39:11 29.43 n/a .000
10583 CONTINUES STANDRD 1.0 01:R-2 102.94 3.971 No.date 28:20 30.13 405 .000
10584 [Cm 72.0; No. 3.00; Tps= 40]
10585 [IAREC: 4.00; SM: No. 39.75; SMAX: 264.99; SK: 010]
10586 #*****
10587 ROUTE: C030201 -> 1.0 01:SN.D 55194.86 104.478 No.date 39:15 29.43 n/a .000
10588 ADD HYD + 1.0 02: N.M 102.94 3.971 No.date 28:20 30.13 n/a .000
10589 + 1.0 02: M.D 102.94 3.971 No.date 28:20 30.13 n/a .000
10590 SLM 1.0 01:SN.D 55194.86 104.478 No.date 39:15 29.43 n/a .000
10591 ROUTE: C030202 -> 1.0 01:SN.D 55194.86 104.478 No.date 39:15 29.43 n/a .000
10592 SAVED HYD 1.0 01:SN.D 55194.86 104.478 No.date 39:15 29.43 n/a .000
10593 #name : SN.D 0025
10594 remark: Total Flow at Rideau River
10595 #*****
10596 #*****
10597 #*****
10598 #*****
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10660 #*****
10661 #*****
10662 #*****
10663 #*****
10664 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
10665 # of 1.32
10666 #*****
10667 #*****
10668 #*****
10669 #*****
10670 #*****
10671 #*****
10672 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
10673 # of 1.32
10674 ROUTE: C0302007 -> 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10675 CONTINUES STANDRD 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10676 [Cm 61.0; No. 3.00; Tps= 3.76]
10677 [IAREC: 4.00; SM: No. 64.50; SMAX: 430.01; SK: 010]
10678 [IAREC: 4.00; SM: No. 64.50; SMAX: 430.01; SK: 010]
10679 #*****
10680 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
10681 # of 1.80
10682 ROUTE: C0302008 -> 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10683 CONTINUES STANDRD 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10684 [Cm 55.0; No. 3.00; Tps= 1.31]
10685 [IAREC: 4.00; SM: No. 54.74; SMAX: 554.96; SK: 010]
10686 #*****
10687 #*****
10688 #*****
10689 #*****
10690 #*****
10691 #*****
10692 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
10693 # of 1.50
10694 ROUTE: C0302009 -> 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10695 CONTINUES STANDRD 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10696 [Cm 66.0; No. 3.00; Tps= 5.29]
10697 [IAREC: 4.00; SM: No. 52.62; SMAX: 350.79; SK: 010]
10698 #*****
10699 #*****
10700 #*****
10701 #*****
10702 #*****
10703 #*****
10704 #*****
10705 #*****
10706 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
10707 # of 1.52
10708 ROUTE: C0302012 -> 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10709 CONTINUES STANDRD 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10710 [Cm 72.0; No. 3.00; Tps= 8.00]
10711 [IAREC: 4.00; SM: No. 39.75; SMAX: 264.99; SK: 010]
10712 #*****
10713 #*****
10714 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
10715 # of 1.73
10716 ROUTE: C0302013 -> 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10717 CONTINUES STANDRD 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10718 [Cm 66.0; No. 3.00; Tps= 8.42]
10719 [IAREC: 4.00; SM: No. 52.62; SMAX: 350.79; SK: 010]
10720 #*****
10721 #*****
10722 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
10723 # of 1.68
10724 ROUTE: C0302014 -> 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10725 CONTINUES STANDRD 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10726 [Cm 70.0; No. 3.00; Tps= 2.51]
10727 [IAREC: 4.00; SM: No. 53.67; SMAX: 287.10; SK: 010]
10728 #*****
10729 #*****
10730 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
10731 # of 1.82
10732 ROUTE: C0302015 -> 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10733 CONTINUES STANDRD 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10734 [Cm 62.0; No. 3.00; Tps= 1.31]
10735 [IAREC: 4.00; SM: No. 61.50; SMAX: 412.66; SK: 010]
10736 #*****
10737 #*****
10738 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
10739 # of 1.73
10740 ROUTE: C0302016 -> 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10741 CONTINUES STANDRD 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10742 [Cm 63.0; No. 3.00; Tps= 6.65]
10743 [IAREC: 4.00; SM: No. 59.42; SMAX: 396.11; SK: 010]
10744 #*****
10745 #*****
10746 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
10747 # of 1.68
10748 ROUTE: C0302017 -> 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10749 CONTINUES STANDRD 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10750 [Cm 66.0; No. 3.00; Tps= 8.42]
10751 [IAREC: 4.00; SM: No. 52.62; SMAX: 350.79; SK: 010]
10752 #*****
10753 #*****
10754 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
10755 # of 1.82
10756 ROUTE: C0302018 -> 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10757 CONTINUES STANDRD 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10758 [Cm 57.0; No. 3.00; Tps= 6.45]
10759 [IAREC: 4.00; SM: No. 76.32; SMAX: 508.81; SK: 010]
10760 #*****
10761 #*****
10762 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
10763 # of 1.75
10764 ROUTE: C0302019 -> 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10765 CONTINUES STANDRD 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10766 [Cm 67.0; No. 3.00; Tps= 7.1]
10767 [IAREC: 4.00; SM: No. 50.55; SMAX: 336.97; SK: 010]
10768 #*****
10769 #*****
10770 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
10771 # of 1.67
10772 ROUTE: C0302020 -> 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10773 CONTINUES STANDRD 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10774 [Cm 72.0; No. 3.00; Tps= 5.95]
10775 [IAREC: 4.00; SM: No. 39.75; SMAX: 264.99; SK: 010]
10776 #*****
10777 #*****
10778 #*****
10779 #*****
10780 #*****
10781 #*****
10782 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
10783 # of 1.20
10784 ROUTE: C0302022 -> 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10785 CONTINUES STANDRD 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10786 [Cm 74.0; No. 3.00; Tps= 4.43]
10787 [IAREC: 4.00; SM: No. 36.67; SMAX: 244.49; SK: 010]
10788 #*****
10789 #*****
10790 #*****
10791 #*****
10792 #*****
10793 #*****
10794 #*****
10795 #*****
10796 # The Tp was modified according to a Peak Reduction factor (MFO Chart B2-4)
10797 # of 1.61
10798 ROUTE: C0302024 -> 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10799 CONTINUES STANDRD 1.0 01:SN.D 55194.86 104.478 No.date 38:54 29.33 n/a .000
10800 [Cm 75.0; No. 3.00; Tps= 8.00]
10801 [IAREC: 4.00; SM: No. 33.81; SMAX: 225.43; SK: 010]
10802 #*****
10803 #*****
10804 #*****
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10845 #*****
10846 #*****

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108475 #
108480 # Addition of Subwatershed Lock River at Goodwood Marsh to Node 13A
108489 #
108500 RO505: C00032.....Dfai n-ID NND.....AREAH-QPEAKm-TpeakDate-hh:mm--Rvmm R.C---Dfwm
108511 ADD HYD + 1.0 02: N3A 4651.00 19.136 Ndate 39.06 29.90 n/a 000
108522 ROUTE CHANNEL -> 1.0 02: IR_GOM 3074.00 8.912 Ndate 39.59 24.31 n/a 000
108533 SIMM 1.0 01: SNI3A 7725.00 27.939 Ndate 39.54 27.68 n/a 000
108544 #
108555 # Insertion of a reservoir to simulate the effects of the Goodwood Marsh
108560 #
108570 RO505: C00033.....Dfai n-ID NND.....AREAH-QPEAKm-TpeakDate-hh:mm--Rvmm R.C---Dfwm
108588 ROUTE RESERVOIR -> 1.0 02: SNI3A 7725.00 27.939 Ndate 39.54 27.68 n/a 000
108600 (Msk Outflow: 1481E04)
108610 #
108620 RO505: C00034.....Dfai n-ID NND.....AREAH-QPEAKm-TpeakDate-hh:mm--Rvmm R.C---Dfwm
108638 SAVE HYD 1.0 01: RES_GM 7725.00 3.808 Ndate 61.35 27.67 n/a 000
108649 frame :H_RESUM
108659 remark:Outflow from Res GM
108668 # Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
108675 # (Approximated cross-section - see cross-section 258)
108688 # Use n=0.04 for summer conditions and n=0.025 for spring conditions
108690 RO505: C00035.....Dfai n-ID NND.....AREAH-QPEAKm-TpeakDate-hh:mm--Rvmm R.C---Dfwm
108700 ROUTE CHANNEL -> 1.0 02: RES_GM 7725.00 3.808 Ndate 61.35 27.67 n/a 000
108711 (RFD= 1.00) out c 1.0 01: N12 7725.00 3.804 Ndate 64.19 27.68 n/a 000
108722 (L/S n= 522. / 0.76) 0401
108733 (Vmax = .556; Dmax= 1.541)
108744 #
108755 # Addition of Subwatershed Lock River at Ashton to Node 12
108760 #
108770 RO505: C00036.....Dfai n-ID NND.....AREAH-QPEAKm-TpeakDate-hh:mm--Rvmm R.C---Dfwm
108788 ADD HYD + 1.0 02: N12 7725.00 3.804 Ndate 64.19 27.68 n/a 000
108799 + 1.0 02: IR_ASH 1781.00 16.834 Ndate 32.39 36.85 n/a 000
108810 SIMM 1.0 01: S_N12 9506.00 18.867 Ndate 32.42 29.39 n/a 000
108821 (RFD= 1.00) out c 1.0 01: N12 9506.00 18.867 Ndate 32.42 29.39 n/a 000
108832 SAVE HYD 1.0 01: S_N12 9506.00 18.867 Ndate 32.42 29.39 n/a 000
108843 frame :H_SNI2
108853 remark:flow at S_N12 near Ashton
108863 #
108870 # Sum of hydrographs from Node 12 routed to Node 11
108875 # (Approximated cross-section - see cross-section 258)
108888 # Use n=0.04 for summer conditions and n=0.025 for spring conditions
108890 #
108900 # Sum of hydrographs from Node 12 routed to Node 11 with Dump Section 248
108910 #
108920 RO505: C00038.....Dfai n-ID NND.....AREAH-QPEAKm-TpeakDate-hh:mm--Rvmm R.C---Dfwm
108938 ROUTE CHANNEL -> 1.0 02: S_N12 9506.00 18.867 Ndate 32.42 29.39 n/a 000
108949 (RFD= 1.00) out c 1.0 01: Dum1 9506.00 18.867 Ndate 32.59 29.39 n/a 000
108960 (L/S n= 972. / 0.54) 0401
108971 (Vmax = 751; Dmax= 3.029)
108982 #
108990 # Addition of Subwatershed 11 and Noe Creek to Node 11
109000 #
109010 RO505: C00039.....Dfai n-ID NND.....AREAH-QPEAKm-TpeakDate-hh:mm--Rvmm R.C---Dfwm
109028 ADD HYD + 1.0 02: Dum1 9506.00 18.867 Ndate 32.59 29.39 n/a 000
109039 + 1.0 02: SW11 500.00 9.061 Ndate 29.21 31.73 n/a 000
109050 ROUTE CHANNEL -> 1.0 02: S_N11 1917.00 12.342 Ndate 34.26 31.73 n/a 000
109061 SIMM 1.0 01: S_N11 11923.00 32.851 Ndate 33.00 29.87 n/a 000
109072 #
109080 # Sum of hydrographs from Node 11 routed to Node 10
109090 # Section 1
109100 RO505: C00040.....Dfai n-ID NND.....AREAH-QPEAKm-TpeakDate-hh:mm--Rvmm R.C---Dfwm
109118 ROUTE CHANNEL -> 1.0 01: N10 11923.00 20.490 Ndate 40.02 29.87 n/a 000
109129 (L/S n= 822. / 1.57) 0401
109140 (Vmax = 474; Dmax= 1.423)
109151 #
109160 # Addition of Subwatershed 10 to Node 10
109170 RO505: C00041.....Dfai n-ID NND.....AREAH-QPEAKm-TpeakDate-hh:mm--Rvmm R.C---Dfwm
109188 ADD HYD + 1.0 02: N10 11923.00 20.490 Ndate 40.02 29.87 n/a 000
109199 + 1.0 02: SW10 5666.00 22.402 Ndate 37.52 36.85 n/a 000
109210 SIMM 1.0 01: S_N10 17589.00 52.600 Ndate 38.19 32.12 n/a 000
109221 RO505: C00042.....Dfai n-ID NND.....AREAH-QPEAKm-TpeakDate-hh:mm--Rvmm R.C---Dfwm
109232 SAVE HYD 1.0 01: S_N10 17589.00 52.600 Ndate 38.19 32.12 n/a 000
109243 frame :H_SNI0
109254 remark:flow at S_N10: N10 + SW10
109265 #
109270 RO505: C00043.....Dfai n-ID NND.....AREAH-QPEAKm-TpeakDate-hh:mm--Rvmm R.C---Dfwm
109288 ADD HYD + 1.0 02: S_N10 17589.00 52.600 Ndate 38.19 32.12 n/a 000
109299 + 1.0 02: RG_CK 8376.00 31.024 Ndate 39.59 31.73 n/a 000
109310 SIMM 1.0 01: S_N10A 25965.00 82.764 Ndate 39.45 31.99 n/a 000
109321 #
109330 # Sum of hydrographs from Node 10 routed to Node 9
109340 # Section 2
109350 RO505: C00044.....Dfai n-ID NND.....AREAH-QPEAKm-TpeakDate-hh:mm--Rvmm R.C---Dfwm
109368 ROUTE CHANNEL -> 1.0 01: N9A 31561.00 99.424 Ndate 39.59 31.68 n/a 000
109379 (RFD= 1.00) out c 1.0 01: N9 25965.00 80.980 Ndate 39.59 31.99 n/a 000
109390 (L/S n= 3082. / 0.74) 0401
109401 (Vmax = 744; Dmax= 2.015)
109412 #
109420 # Addition of Subwatershed 9 and Nchols Creek to Node 9
109430 RO505: C00045.....Dfai n-ID NND.....AREAH-QPEAKm-TpeakDate-hh:mm--Rvmm R.C---Dfwm
109448 ADD HYD + 1.0 02: N9 25965.00 80.980 Ndate 39.59 31.99 n/a 000
109459 + 1.0 02: SW9 1132.00 14.039 Ndate 30.53 35.35 n/a 000
109470 + 1.0 02: RG_CK 4464.00 15.472 Ndate 39.59 31.73 n/a 000
109481 SIMM 1.0 01: S_N9 31561.00 99.424 Ndate 39.59 31.68 n/a 000
109492 #
109500 # Sum of hydrographs from Node 9 routed to Node 8
109510 # Section 3
109520 RO505: C00046.....Dfai n-ID NND.....AREAH-QPEAKm-TpeakDate-hh:mm--Rvmm R.C---Dfwm
109538 ROUTE CHANNEL -> 1.0 01: N8 31561.00 99.424 Ndate 39.59 31.68 n/a 000
109549 (RFD= 1.00) out c 1.0 01: N8 31561.00 99.665 Ndate 39.59 31.68 n/a 000
109560 (L/S n= 5822. / 0.83) 0401
109571 (Vmax = 367; Dmax= 1.834)
109582 #
109590 # Addition of Subwatershed 8 and Hobbs' Drain to Node 8
109600 RO505: C00047.....Dfai n-ID NND.....AREAH-QPEAKm-TpeakDate-hh:mm--Rvmm R.C---Dfwm
109618 ADD HYD + 1.0 02: N8 31561.00 99.665 Ndate 39.59 31.68 n/a 000
109629 + 1.0 02: SW8 131.00 1.240 Ndate 28.52 39.64 n/a 000
109640 + 1.0 02: HB_DR 3554.00 18.180 Ndate 38.32 31.73 n/a 000
109651 SIMM 1.0 01: S_N8 31561.00 111.843 Ndate 39.59 31.68 n/a 000
109662 #
109670 # Sum of hydrographs from Node 8 routed to Node 7
109680 # Section 4
109690 RO505: C00048.....Dfai n-ID NND.....AREAH-QPEAKm-TpeakDate-hh:mm--Rvmm R.C---Dfwm
109708 ROUTE CHANNEL -> 1.0 02: S_N8 3546.00 111.843 Ndate 39.59 31.68 n/a 000
109719 (RFD= 1.00) out c 1.0 01: N7 3546.00 95.475 Ndate 44.55 31.68 n/a 000
109730 (L/S n= 522. / 0.51) 0401
109741 (Vmax = 231; Dmax= 2.290)
109752 #
109760 # Addition of Subwatershed 7 to Node 7
109770 RO505: C00049.....Dfai n-ID NND.....AREAH-QPEAKm-TpeakDate-hh:mm--Rvmm R.C---Dfwm
109788 ADD HYD + 1.0 02: N7 3546.00 95.475 Ndate 44.55 31.68 n/a 000
109799 + 1.0 02: SW7 3197.00 13.937 Ndate 36.23 35.65 n/a 000
109810 SIMM 1.0 01: S_N7 38743.00 102.892 Ndate 43.46 31.18 n/a 000
109821 RO505: C00050.....Dfai n-ID NND.....AREAH-QPEAKm-TpeakDate-hh:mm--Rvmm R.C---Dfwm
109832 SAVE HYD 1.0 01: S_N7 38743.00 102.892 Ndate 43.46 31.18 n/a 000
109843 frame :H_SNI7
109854 remark:flow at S_N7: N7 + SW7
109865 #
109870 # Insertion of a reservoir to simulate the effects of the Richmond Fen.
109880 # Storage area and volumes were estimated from available topo maps.
109890 # Release rate from fen was assumed to be controlled by the downstream
109900 # river cross-section for summer conditions. It is assumed that for up to
109910 # 0.75 m of water, the main channel of the river provided the storage. Above
109920 # this depth, the wetland starts to significantly store water.
109930 RO505: C00051.....Dfai n-ID NND.....AREAH-QPEAKm-TpeakDate-hh:mm--Rvmm R.C---Dfwm
109948 ROUTE RESERVOIR -> 1.0 02: S_N7 38743.00 102.892 Ndate 43.46 31.18 n/a 000
109959 (Msk Outflow: 4394E04)
109970 #
109980 RO505: C00052.....Dfai n-ID NND.....AREAH-QPEAKm-TpeakDate-hh:mm--Rvmm R.C---Dfwm
109998 SAVE HYD 1.0 01: RES_RF 38743.00 52.029 Ndate 59.07 31.18 n/a 000
110009 frame :H_RES_RF
110020 remark:outflow of Richmond Fen
110030 #
110040 # Sum of hydrographs from Node 7 routed to Node 6
110050 # Section 5
110060 RO505: C00053.....Dfai n-ID NND.....AREAH-QPEAKm-TpeakDate-hh:mm--Rvmm R.C---Dfwm
110078 ROUTE CHANNEL -> 1.0 02: S_N6 38743.00 52.029 Ndate 59.07 31.18 n/a 000
110089 (RFD= 1.00) out c 1.0 01: N6 38743.00 51.784 Ndate 60.27 31.18 n/a 000
110100 (L/S n= 3036. / 0.62) 0401
110111 (Vmax = 538; Dmax= 1.253)
110122 #
110130 # Addition of Subwatershed 6 and Van Gual Drain to Node 6
110140 RO505: C00054.....Dfai n-ID NND.....AREAH-QPEAKm-TpeakDate-hh:mm--Rvmm R.C---Dfwm
110158 ADD HYD + 1.0 02: N6 38743.00 51.784 Ndate 60.27 31.18 n/a 000
110169 + 1.0 02: SW6 185.00 1.285 Ndate 33.02 32.44 n/a 000
110180 + 1.0 02: VG_DR 1332.00 9.332 Ndate 35.12 36.85 n/a 000
110191 SIMM 1.0 01: S_N6 40240.01 51.810 Ndate 60.20 31.47 n/a 000
110202 #
110210 # Sum of hydrographs from Node 6 routed to Node 5
110220 RO505: C00055.....Dfai n-ID NND.....AREAH-QPEAKm-TpeakDate-hh:mm--Rvmm R.C---Dfwm
110238 ROUTE CHANNEL -> 1.0 01: N5 40240.01 51.810 Ndate 60.20 31.47 n/a 000
110249 (RFD= 1.00) out c 1.0 01: N5 40240.01 51.693 Ndate 61.06 31.37 n/a 000
110260 (L/S n= 522. / 0.51) 0401
110271 (Vmax = 469; Dmax= 1.351)
110282 #
110290 # Addition of Subwatershed 5 and Flowing Creek to Node 5
110300 RO505: C00056.....Dfai n-ID NND.....AREAH-QPEAKm-TpeakDate-hh:mm--Rvmm R.C---Dfwm
110318 ADD HYD + 1.0 02: N5 40240.01 51.693 Ndate 61.06 31.37 n/a 000
110329 + 1.0 02: FC_CK 4945.00 44.623 Ndate 33.18 38.37 n/a 000
110340 SIMM 1.0 01: S_N5 45409.01 71.514 Ndate 34.20 32.31 n/a 000

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12343	RO05: C00264	Dfna : 1.01:TD:MD	AREArh: QPEArkm: TpeakDr: bh:mm	Rvkm: R: C: Dwfcm			
12343	CNTLNXS NASVID	1.0	1.01:FRASER:DRN	13.65	711	N_date	28:22	39.91	490	0.00
12343	[Cm: 77.0] out	+	1.01:TO:TD	494	88	N_date	28:02	63.21	34.7	0.00
12343	[LRCM: 4.00] out	+	1.01:TO:TD	494	88	N_date	28:02	63.21	34.7	0.00
12343	[LRS: 2 - Cn: 77.0]
12343	Perivous area:	IAPER: 4.67:SLP:1.0: LEP: 4.0: MNP: 250: SCP: 0]
12343	Imperivous area:	IAPM: 1.57:SLP:1.0: LCG: 388: MN: 013: SCI: 0]
12343	[LRCM: 4.00] out	+	1.01:TO:TD	494	88	N_date	28:02	63.21	34.7	0.00
12343	[LRS: 2 - Cn: 77.0]
12343	Perivous area:	IAPER: 4.67:SLP:1.0: LEP: 4.0: MNP: 250: SCP: 0]
12343	Imperivous area:	IAPM: 1.57:SLP:1.0: LCG: 388: MN: 013: SCI: 0]

Table with multiple columns containing alphanumeric codes and values. Includes headers like 'R0500', 'R0501', etc., and various alphanumeric strings. The table is organized into columns and rows, with some rows containing more detailed information than others.

```
13091# # Tributary Drainage area to MSS Pond = 145 ha
13092# *****
13093#
13094# Hydrograph from Curigan Drain routed to Jockvale Road
13095# Channel X Section obtained from RCPA Hydraulic Model - Station 2462
13096#
13097# R050: CO0387..... Dftm=1-D NDD.....AREAh-QPEAkcm-TpeakDte,hb,mm---Rvm R,C---Dfcm
13098# ROUTE CHANNEL -> 1.0 01: corrig 55019.59 126.926 Ndate 36:27 34.22 n/a 0.000
13099# [RFS=1.00] out_c= 1.0 01: NI,DE 55019.59 126.908 Ndate 36:31 34.22 n/a 0.000
13100# [L/S= 580. / 445/ 045]
13101# [Vmax= 2.065,Dmax= 1.981]
13102# *****
13103# # Catchment MLLS
13104# # To SWM Facility north of the Jock
13105# # Primarily residential development
13106# *****
13107# R050: CO0388..... Dftm=1-D NDD.....AREAh-QPEAkcm-TpeakDte,hb,mm---Rvm R,C---Dfcm
13108# CONTINUS STANDARD 1.0 01: MLLS 175.99 17.756 Ndate 28:06 50.66 6.22 0.000
13109# [X/Mp= 30. Tl/Mp= 34]
13110# [LGS= 2. Cn= 74.0]
13111# [Perivous area: Iperga= 4.67: SLPPI= 0.0: LEP= 4.0: MNP= 250: SCP= 0]
13112# [Impervious area: Iamp= 1.57: SLPPI= 0.0: LG= 1118.: MN= 013: SCL= 0]
13113# [IARECmp= 4.00: IAREP= 4.00]
13114# [SM= 36.67: SMX= 244.49: SKe= 010]
13115# *****
13116# # Chapman Mills SWM Pond
13117# # Rating curve obtained from CCL hydraulic modeling
13118# *****
13119# R050: CO0389..... Dftm=1-D NDD.....AREAh-QPEAkcm-TpeakDte,hb,mm---Rvm R,C---Dfcm
13120# ROUTE RESURVE -> 1.0 02: MLLS 175.99 17.756 Ndate 28:06 50.66 n/a 0.000
13121# out_c= 1.0 01: MLLP,OV 175.99 17.756 Ndate 28:06 50.66 n/a 0.000
13122# overflow sc= 1.0 03: MLLP,OV 22.12 12.440 Ndate 28:11 50.66 n/a 0.000
13123# [MSx0toEdc= 2310E+0] mb, TotOrVol= 1121E+0] mb, Nof= 2, TotOrF= 1hrs]
13124# R050: CO0390..... Dftm=1-D NDD.....AREAh-QPEAkcm-TpeakDte,hb,mm---Rvm R,C---Dfcm
13125# AFD IHD + 1.0 02: IHD 55019.59 126.908 Ndate 36:31 34.22 n/a 0.000
13126# + 1.0 02: MLL,OV 22.12 12.440 Ndate 28:11 50.66 n/a 0.000
13127# + 1.0 02: MLL,OV 153.87 4.650 Ndate 28:11 50.66 n/a 0.000
13128# SIM 55195.58 127.513 Ndate 36:30 34.27 n/a 0.000
13129# R050: CO0391..... Dftm=1-D NDD.....AREAh-QPEAkcm-TpeakDte,hb,mm---Rvm R,C---Dfcm
13130# SAVE IHD 1.0 01: SN,DE 55195.58 127.513 Ndate 36:30 34.27 n/a 0.000
13131# fname= SN,NI 0050
13132# *****
13133# # remark: Total Flow at Jockvale Road
13134#
13135# # Hydrograph from Jockvale Road routed to Heart's Desire
13136# # Channel X Section obtained from RCPA Hydraulic Model - Station 689
13137#
13138# R050: CO0392..... Dftm=1-D NDD.....AREAh-QPEAkcm-TpeakDte,hb,mm---Rvm R,C---Dfcm
13139# ROUTE CHANNEL -> 1.0 02: SN,DE 55195.58 127.513 Ndate 36:30 34.27 n/a 0.000
13140# [RFS=1.00] out_c= 1.0 01: NI,DE 55195.58 127.513 Ndate 36:43 34.27 n/a 0.000
13141# [L/S= 1062. / 2224/ 010]
13142# [Vmax= 1.577,Dmax= 2.490]
13143# *****
13144# # Catchment DESIRE
13145# # To Jock River (north of the Jock)
13146# # Rural estate subdivision (Heart's Desire Community)
13147# *****
13148# R050: CO0393..... Dftm=1-D NDD.....AREAh-QPEAkcm-TpeakDte,hb,mm---Rvm R,C---Dfcm
13149# CONTINUS STANDARD 1.0 01: DESIRE 23.78 2.563 Ndate 28:03 46.85 5.75 0.000
13150# [X/Mp= 25. Tl/Mp= 25]
13151# [LGS= 2. Cn= 77.0]
13152# [Perivous area: Iperga= 4.67: SLPPI= 0.0: LEP= 4.0: MNP= 250: SCP= 0]
13153# [Impervious area: Iamp= 1.57: SLPPI= 0.0: LG= 400.: MN= 013: SCL= 0]
13154# [IARECmp= 4.00: IAREP= 4.00]
13155# [SM= 35.35: SMX= 266.66: SKe= 010]
13156# *****
13157# # # Catchment JOCKVA
13158# # Residential development & golf course
13159# # JFSA 2002-01-11 updated JOCKVA after updating CORRG for IRE GROUP, July 2008.
13160# # JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two areas JOCKVA and EX LAND 32.5 ha as
13161# *****
13162# R050: CO0394..... Dftm=1-D NDD.....AREAh-QPEAkcm-TpeakDte,hb,mm---Rvm R,C---Dfcm
13163# CONTINUS STANDARD 1.0 01: JOCKVA 225.13 25.253 Ndate 28:07 56.33 6.91 0.000
13164# [X/Mp= 50. Tl/Mp= 50]
13165# [LGS= 2. Cn= 74.0]
13166# [Perivous area: Iperga= 4.67: SLPPI= 0.0: LEP= 4.0: MNP= 250: SCP= 0]
13167# [Impervious area: Iamp= 1.57: SLPPI= 0.0: LG= 1311.: MN= 013: SCL= 0]
13168# [IARECmp= 4.00: IAREP= 4.00]
13169# [SM= 36.67: SMX= 244.49: SKe= 010]
13170# *****
13171# R050: CO0395..... Dftm=1-D NDD.....AREAh-QPEAkcm-TpeakDte,hb,mm---Rvm R,C---Dfcm
13172# AFD IHD + 1.0 02: EX-LAND-MN 31.74 2.275 Ndate 27:49 56.55 n/a 0.000
13173# + 1.0 02: JOCKVA 225.13 25.253 Ndate 28:07 56.33 n/a 0.000
13174# + 1.0 02: IHD 55195.58 127.513 Ndate 36:43 34.27 n/a 0.000
13175# + 1.0 02: IHD,OV 02 083 Ndate 28:09 56.26 n/a 0.000
13176# SIM 256.89 10.991 Ndate 28:38 56.36 n/a 0.000
13177# R050: CO0396..... Dftm=1-D NDD.....AREAh-QPEAkcm-TpeakDte,hb,mm---Rvm R,C---Dfcm
13178# SAVE IHD 1.0 01: JOCKVA TO 256.89 10.991 Ndate 28:07 56.36 n/a 0.000
13179# fname= JOCKVA TO 0050
13180# *****
13181# # remark: Total Flow at KH first pond
13182#
13183# # Jockvale SWM Facility
13184# # Rating curve obtained from JOCKVA Servicing Study (CCL 1999)
13185# *****
13186# R050: CO0397..... Dftm=1-D NDD.....AREAh-QPEAkcm-TpeakDte,hb,mm---Rvm R,C---Dfcm
13187# ROUTE CHANNEL -> 1.0 02: JOCKVA TO 256.89 10.991 Ndate 28:38 56.36 n/a 0.000
13188# out_c= 1.0 01: JOCKP,OV 256.89 10.991 Ndate 28:38 56.36 n/a 0.000
13189# overflow sc= 1.0 02: JOCKP,OV 0.00 0.00 Ndate 28:07 56.36 n/a 0.000
13190# [MSx0toEdc= 5928E+0] mb, TotOrVol= 0000E+00 mb, Nof= 0, TotOrF= 0 hrs]
13191# R050: CO0398..... Dftm=1-D NDD.....AREAh-QPEAkcm-TpeakDte,hb,mm---Rvm R,C---Dfcm
13192# AFD IHD + 1.0 02: DESIRE 23.78 2.563 Ndate 28:03 46.85 n/a 0.000
13193# + 1.0 02: JOCKVA TO 256.89 10.991 Ndate 28:38 56.36 n/a 0.000
13194# SIM 55195.58 127.513 Ndate 36:43 34.27 n/a 0.000
13195# R050: CO0399..... Dftm=1-D NDD.....AREAh-QPEAkcm-TpeakDte,hb,mm---Rvm R,C---Dfcm
13196# SAVE IHD 1.0 01: SN,DE 55476.26 128.174 Ndate 36:42 34.38 n/a 0.000
13197# fname= SN,NI 0050
13198# *****
13199# # remark: Total Flow at Heart's Desire
13200#
13201# # Hydrograph from Heart's Desire routed to Rideau River
13202# # Channel X Section obtained from RCPA Hydraulic Model - Station 0
13203#
13204# R050: CO0400..... Dftm=1-D NDD.....AREAh-QPEAkcm-TpeakDte,hb,mm---Rvm R,C---Dfcm
13205# ROUTE CHANNEL -> 1.0 01: NI,DE 55476.26 128.174 Ndate 36:45 34.38 n/a 0.000
13206# [L/S= 963. / 967/ 010]
13207# [Vmax= 2.123,Dmax= 1.248]
13208# *****
13209# # Catchment S 2
13210# # To Jock River (north and south)
13211# # Unimproved floodplain
13212# *****
13213# R050: CO0401..... Dftm=1-D NDD.....AREAh-QPEAkcm-TpeakDte,hb,mm---Rvm R,C---Dfcm
13214# CONTINUS NASIDD 1.0 01: S 2 102.94 4.795 Ndate 28:20 35.39 4.34 0.000
13215# [Cn= 72.0, No 3.00, Tpe= 4.0]
13216# [IAREC= 4.00: SM= 39.75: SMX= 264.99: SKe= 010]
13217# [InterEventTime= 12.00]
13218# *****
13219# R050: CO0402..... Dftm=1-D NDD.....AREAh-QPEAkcm-TpeakDte,hb,mm---Rvm R,C---Dfcm
13220# AFD IHD + 1.0 02: NI 55476.26 128.174 Ndate 36:45 34.38 n/a 0.000
13221# + 1.0 02: IHD 55476.26 128.174 Ndate 36:42 34.38 n/a 0.000
13222# SIM 55579.20 128.417 Ndate 36:44 34.38 n/a 0.000
13223# R050: CO0403..... Dftm=1-D NDD.....AREAh-QPEAkcm-TpeakDte,hb,mm---Rvm R,C---Dfcm
13224# SAVE IHD 1.0 01: SN,DE 55579.20 128.417 Ndate 36:44 34.38 n/a 0.000
13225# fname= SN,NI 0050
13226# *****
13227# # remark: Total Flow at Rideau River
13228# *****
13229# *****
13230# *****
13231# *****
13232# *****
13233# *****
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13500# *****
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Table with multiple columns containing technical data, including node numbers, flow rates, and various engineering parameters. The table is organized into sections and includes detailed annotations for each entry.

Table with columns for ID, description, parameters, and values. Includes entries for ROUTE CHANNEL, CONTINUES STANDBY, and various system parameters.


```

157099 + 1.0 02:40:M .00 .000 No.date 0.00 .00 n/a .000
157109 + 1.0 02:41:M .09 218 No.date 28.05 59.73 n/a .000
157113 + 1.0 02:41:M .16 564 No.date 28.06 67.38 n/a .000
157123 + 1.0 02:41:M .23 599 No.date 28.05 62.88 n/a .000
157133 + 1.0 02:43:M .00 .000 No.date 0.00 .00 n/a .000
157143 + 1.0 01:corr 55020.08 145.505 No.date 36:37 39.46 n/a .000
157153 R0100:CO0386.....DfM n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm---RvM R.C.....Dfwm
157163 SAVE HYD 1.0 01:corr 55020.08 145.505 No.date 36:37 39.46 n/a .000
157173 fname :corr: 0100
157183 remark:Total Flow at Corrigan Pond
157193 *****
157203 # Corrigan Pond 1
157213 # Rating curve obtained from Barrhaven South MS modeling
157223 # Tributary Drainage at Corrigan Pond 1 - 145 ha
157233 *****
157243 #
157253 # Hydrograph from Corrigan Drain routed to Jockvale Road
157263 # Channel X-Section obtained from RCVA Hydraulic Model - Station 2462
157273 *****
157283 R0100:CO0387.....DfM n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm---RvM R.C.....Dfwm
157293 ROUTE CHANNEL -> 1.0 02:SN,DE 55020.08 145.490 No.date 36:40 39.46 n/a .000
157303 [R/S n= 1.00] out c= 1.0 01:SN,M 55020.08 145.490 No.date 36:40 39.46 n/a .000
157313 [L/S n= 580 / 4457.045]
157323 [Vmax= 2.170,Dmax= 2.124]
157333 *****
157343 # Catchment MLLS
157353 # - To SWM Facility north of the Jock
157363 # Primarily residential development
157373 *****
157383 R0100:CO0388.....DfM n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm---RvM R.C.....Dfwm
157393 CONTINUOUS STANBYD 1.0 01:MLLS 175.99 20.390 No.date 28:06 56.87 642.000
157403 [XfM= 38.71M, 38]
157413 [L/S n= 2 CN= 74.0]
157423 [Previous area: IArea 4.67,SLP=4.00,LD= 40.0;MPP= 250;SCP= 0]
157433 [Impervious area: IArea 1.57,SLP=1.00,LD=1118.0;MN= 013;SC= 0]
157443 [IARECmp= 4.00; IARECPer= 4.00]
157453 [SM N= 36.67; SMM=244.49; SK= 010]
157463 *****
157473 # Chappin Mills SWM Pond
157483 # Rating curve obtained from CCL hydraulic modeling
157493 *****
157503 R0100:CO0389.....DfM n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm---RvM R.C.....Dfwm
157513 ROUTE RESERVOIR -> 1.0 02:MLLS 175.99 20.390 No.date 28:06 56.87 n/a .000
157523 out c= 1.0 01:MLL,P 146.22 4.050 No.date 28:08 56.87 n/a .000
157533 [L/S n= 580 / 4457.045]
157543 [MS oiled= 2310E+01] nb, TotOfVol= 1693E+01] nb, N Of O= 2, TotDurOf= 1,hrs]
157553 *****
157563 ADD HYD + 1.0 02:SN,M 55020.08 145.490 No.date 36:40 39.46 n/a .000
157573 + 1.0 02:MLL,OV 29.77 16.228 No.date 28:08 56.87 n/a .000
157583 + 1.0 02:MLL,OV 146.22 4.050 No.date 28:08 56.87 n/a .000
157593 SUM 1.0 01:SN,M 55196.07 146.161 No.date 36:39 39.51 n/a .000
157603 R0100:CO0391.....DfM n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm---RvM R.C.....Dfwm
157613 SAVE HYD 1.0 01:SN,M 55196.07 146.161 No.date 36:39 39.51 n/a .000
157623 fname :SN,DE 0100
157633 remark:Total Flow at Jockvale Road
157643 #
157653 # Hydrograph from Jockvale Road routed to Heart's Desire
157663 # Channel X-Section obtained from RCVA Hydraulic Model - Station 689
157673 *****
157683 R0100:CO0392.....DfM n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm---RvM R.C.....Dfwm
157693 ROUTE CHANNEL -> 1.0 02:SN,DE 55196.07 146.161 No.date 36:39 39.51 n/a .000
157703 [R/S n= 1.00] out c= 1.0 01:SN,DE 55196.07 146.161 No.date 36:54 39.51 n/a .000
157713 [L/S n= 1642 / 2231.045]
157723 [Vmax= 1.642,Dmax= 2.659]
157733 *****
157743 # Catchment DESIRE
157753 # - To Jock River (north of the Jock)
157763 # Rural estate subdivision (Heart's Desire Community)
157773 *****
157783 R0100:CO0393.....DfM n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm---RvM R.C.....Dfwm
157793 CONTINUOUS STANBYD 1.0 01:DESIRE 23.78 3.004 No.date 28:03 53.11 600.000
157803 [XfM= 25.71M, 25]
157813 [L/S n= 2 CN= 77.0]
157823 [Previous area: IArea 4.67,SLP=4.00,LD= 40.0;MPP= 250;SCP= 0]
157833 [Impervious area: IArea 1.57,SLP=1.00,LD= 400.0;MN= 013;SC= 0]
157843 [IARECmp= 4.00; IARECPer= 4.00]
157853 [SM N= 31.15; SMM=207.66; SK= 010]
157863 *****
157873 # Catchment JOCKVA
157883 # - To Jockvale SWM Facility
157893 # Residential development & golf course
157903 # - JFSA 2021-01-11 update JOCKVA after updating CURRGAS per IBI GROUP, July 2008.
157913 # JOCKVA area increased from 257.62 ha JOCKVA separated into two areas JOCKVA and EX LAND 32.5 ha as
157923 *****
157933 R0100:CO0394.....DfM n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm---RvM R.C.....Dfwm
157943 CONTINUOUS STANBYD 1.0 01:JOCKVA 225.13 28.623 No.date 28:07 62.70 708.000
157953 [XfM= 50.71M, 50]
157963 [L/S n= 2 CN= 74.0]
157973 [Previous area: IArea 4.67,SLP=4.00,LD= 40.0;MPP= 250;SCP= 0]
157983 [Impervious area: IArea 1.57,SLP=1.00,LD=1311.0;MN= 013;SC= 0]
157993 [IARECmp= 4.00; IARECPer= 4.00]
158003 [SM N= 36.67; SMM=244.49; SK= 010]
158013 R0100:CO0395.....DfM n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm---RvM R.C.....Dfwm
158023 ADD HYD + 1.0 02:EV,LOAD,AN 30.73 2.275 No.date 27:48 62.82 n/a .000
158033 + 1.0 02:EV,LOAD,AN 225.13 28.623 No.date 28:07 62.70 n/a .000
158043 + 1.0 02:RD,M 36 820 No.date 28:05 62.88 n/a .000
158053 + 1.0 02:RD,M 19 402 No.date 28:04 62.88 n/a .000
158063 SUM 1.0 01:JOCKVA,TO 256.41 31.850 No.date 28:06 62.71 n/a .000
158073 R0100:CO0396.....DfM n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm---RvM R.C.....Dfwm
158083 SAVE HYD 1.0 01:JOCKVA,TO 256.41 31.850 No.date 28:06 62.71 n/a .000
158093 fname :JOCKVA,TO 0100
158103 remark:Total Flow at KB first pond
158113 *****
158123 # Jockvale SWM Facility
158133 # Rating curve obtained from Jockvale Servicing Study (CCL 1999)
158143 *****
158153 R0100:CO0397.....DfM n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm---RvM R.C.....Dfwm
158163 ROUTE RESERVOIR -> 1.0 02:JOCKVA,TO 256.41 31.850 No.date 28:06 62.71 n/a .000
158173 out c= 1.0 01:JOCKVA,TO 256.41 31.850 No.date 28:15 62.71 n/a .000
158183 overflow c= 1.0 03:JO,OPF 0.00 0.000 No.date 0.00 .00 n/a .000
158193 [MS oiled= 6410E+01] nb, TotOfVol= 0.000E+01] nb, N Of O= 0, TotDurOf= 0,hrs]
158203 R0100:CO0398.....DfM n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm---RvM R.C.....Dfwm
158213 ADD HYD + 1.0 02:DE 55196.07 145.839 No.date 36:54 39.51 n/a .000
158223 + 1.0 02:DESIRE 23.78 3.004 No.date 28:03 53.11 n/a .000
158233 + 1.0 02:JO,OPF 0.00 0.000 No.date 0.00 .00 n/a .000
158243 + 1.0 02:JO,OPF 256.41 12.850 No.date 28:15 62.71 n/a .000
158253 SUM 1.0 01:SN,DE 55476.26 146.840 No.date 36:52 39.63 n/a .000
158263 R0100:CO0399.....DfM n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm---RvM R.C.....Dfwm
158273 SAVE HYD 1.0 01:SN,DE 55476.26 146.840 No.date 36:52 39.63 n/a .000
158283 fname :SN,DE 0100
158293 remark:Total Flow at Heart's Desire
158303 #
158313 # Hydrograph from Heart's Desire routed to Rideau River
158323 # Channel X-Section obtained from RCVA Hydraulic Model - Station 0
158333 *****
158343 R0100:CO0400.....DfM n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm---RvM R.C.....Dfwm
158353 ROUTE CHANNEL -> 1.0 02:SN,DE 55476.26 146.840 No.date 36:52 39.63 n/a .000
158363 [R/S n= 1.00] out c= 1.0 01:SN,DE 55476.26 146.826 No.date 36:55 39.63 n/a .000
158373 [L/S n= 563 / 9677.045]
158383 [Vmax= 2.138,Dmax= 1.328]
158393 *****
158403 # Catchment S-2
158413 # - To Jock River (north and south)
158423 # Undeveloped floodplain and river
158433 *****
158443 R0100:CO0401.....DfM n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm---RvM R.C.....Dfwm
158453 CONTINUOUS STANBYD 1.0 01:S-2 102.94 5.685 No.date 28:20 40.95 462.000
158463 [Cn= 72,Cn= 3.00; Tpe= 40]
158473 [IAREC= 4.00; SM N= 39.75; SMM=264.99; SK= 010]
158483 *****
158493 R0100:CO0402.....DfM n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm---RvM R.C.....Dfwm
158503 ADD HYD + 1.0 02:SN,DE 55476.26 146.826 No.date 36:55 39.63 n/a .000
158513 + 1.0 02:S-2 102.94 5.685 No.date 28:20 40.95 n/a .000
158523 SUM 1.0 01:SN,NO 55579.20 147.102 No.date 36:55 39.63 n/a .000
158533 R0100:CO0403.....DfM n-ID NDD .....AREBA-QPEAGm-TpeakDte,h:mm---RvM R.C.....Dfwm
158543 SAVE HYD 1.0 01:SN,NO 55579.20 147.102 No.date 36:55 39.63 n/a .000
158553 fname :SN,NO 0100
158563 remark:Total Flow at Rideau River
158573 *****
158583 R0100:CO0002.....
158593 FINISH
158603 *****
158613 *****
158623 *****
158633 *****
158643 R0002:CO0283 ROUTE RESERVOIR
158653 *** WARN NG: Inflow peak was not reduced! Check OUTFLOW STORAGE table or reduce DT.
158663 R0002:CO0305 ROUTE PIPE
158673 *** WARN NG: New pipe size used for routing.
158683 R0002:CO0311 ROUTE PIPE
158693 *** WARN NG: New pipe size used for routing.
158703 R0002:CO0344 D VERT HYD
158713 *** NOTE: Inflow hyd. is dry and cannot be diverted.
158723 R0002:CO0364 ROUTE PIPE
158733 *** WARN NG: New pipe size used for routing.
158743 R0002:CO0371 ROUTE PIPE
158753 *** WARN NG: New pipe size used for routing.
158763 R0002:CO0372 ROUTE PIPE
158773 *** WARN NG: New pipe size used for routing.
158783 R0002:CO0380 ROUTE PIPE
158793 *** WARN NG: New pipe size used for routing.
158803 R0002:CO0381 ROUTE PIPE
158813 *** WARN NG: New pipe size used for routing.
158823 R0002:CO0383 ROUTE RESERVOIR
158833 *** WARN NG: Inflow peak was not reduced! Check OUTFLOW STORAGE table or reduce DT.
158843 R0002:CO0385 ROUTE PIPE
158853 *** WARN NG: New pipe size used for routing.
158863 R0002:CO0386 ROUTE PIPE
158873 *** WARN NG: New pipe size used for routing.
158883 R0002:CO0387 ROUTE PIPE
158893 *** WARN NG: New pipe size used for routing.
158903 R0002:CO0388 ROUTE PIPE
158913 *** WARN NG: New pipe size used for routing.
158923 R0002:CO0389 ROUTE PIPE
158933 *** WARN NG: New pipe size used for routing.
158943 R0002:CO0394 D VERT HYD
158953 *** NOTE: Inflow hyd. is dry and cannot be diverted.

```

Attachment E

Model 4B – Jock River Reach One Future Conditions – With SWM controls

JFSA, 2021

SWMHYMO Input & Summary files

```

1  20    Metric units / ID numbers OFF
2  *****
3  *# SWHYMO Ver: 5.02/Jan 2001 <BETA> / INPUT DATA FILE
4  *****
5  *# Project Name: [Jock River]    Project Number: [1474-16]
6  *# Date       : 04-03-2021
7  *# Modeller  : [MM]
8  *# Company   : JFSA Inc.
9  *# License # : 2549237
10 *****
11 *# CALIBRATION OF SUMMER MODEL PARAMETERS
12 *# USING CONTINUOUS SIMULATIONS
13 *# Rainfall data from JFSA raingauge installed at site + other gauges by the City
14 *# Use data collected from May 1st to July 14, 2003
15 *# 2020-11-30 change TMSTO in COMPUTE DUALHYD (TMSTO = 0.1 instead of 0.0001)
16 *# 2020-12-01 correct pond curve values
17 *# 2020-12-01 change WCLAR_BRAZ_XIMP to 0.55, SLPI=[0.5](%) (impervious slope), and
18 LGI up to 700m
19 *# 2021-02-19 Change the slope for ROUTE CHANNEL Station 2462 (NHYDout=["N_TO"]
20 ,NHYDin=["SN_TO"]) from 0.033 % (as per Stantec Report 2007) to 0.05 % so the model
21 will be more stable and give reasonable results. It is justifiable as ROUTE CHANNELS
22 aren't well suited to really flat slopes.
23 *# 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (NHYDout=["N_WC"]
24 ,NHYDin=["SN_CE"]) from 0.01 % (as per Stantec Report 2007) to 0.0255 % so the model
25 will be more stable and give reasonable results. It is justifiable as ROUTE CHANNELS
26 aren't well suited to really flat slopes.
27 *
28 * Calibrated parameters for Summer 2003 data: APII=50, APIK=0.85, CN=varies,
29 SK=0.01, InterEventTime=12,
30 GWResk=0.96, VHydCond=0.055
31 *
32 *# -----
33 *
34 *START          TZERO=[2003.0501], METOUT=[2], NSTORM=[1], NRUN=[001]
35 *              ["XAVG0315.STM"] average storm data a 15 minute time step
36 *              The above rainf file is an average of the JFSA gauge data
37 *              with the City of Ottawa rainfall data collected during
38 *              the same period.
39 *% 2 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
40 START          TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[2]
41 ["C24SC002.stm"] <-- storm filename, one per line for NSTORM time
42 *%-----|-----|
43 *%-----|-----|
44 READ STORM     STORM_FILENAME=["storm 001"]
45 *%-----|-----|
46 MODIFY STORM  ICASEms=[1], NSHIFT=[96],
47 RedFACT=[1],
48 *%-----|-----|
49 DEFAULT VALUES ICASEdef=[1], read and print values
50 DEFVAL_FILENAME=["CitiGate.DEF"]
51 *%-----|-----|
52 *%-----|-----|
53 COMPUTE API    APII=[50], APIK=[.85]/day
54 *%-----|-----|
55 *%-----|-----|
56 *#
57 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
58 *# of 1.32
59 *%-----|-----|
60 CONTINUOUS NASHYD NHYD=["JR_HW"], DT=[1]min, AREA=[3680](ha),
61 DWF=[0](cms), CNVC=[64], IA=[2.5](mm),
62 N=[3.0], TP=[7.13]hrs,
63 Continuous simulation parameters:
64 IARECper=[4](hrs),
65 SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
66 InterEventTime=[12](hrs)
67 Baseflow simulation parameters:

```

```

60 BaseFlowOption=[ 1] ,
61 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
62 VHydCond=[ 0.055](mm/hr), END=- 1
63 *%-----|-----
64 *#
65 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
66 *# of 1.32
67 *%-----|-----
68 CONTINUOUS NASHYD NHYD=[ "SW_13"], DT=[ 1]min, AREA=[ 971](ha),
69 DWF=[ 0](cms), CNVC=[ 61], IA=[ 2.5](mm),
70 N=[ 3.0], TP=[ 3.76]hrs,
71 Continuous simulation parameters:
72 IaRECper=[ 4](hrs),
73 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
74 InterEventTime=[ 12](hrs)
75 Baseflow simulation parameters:
76 BaseFlowOption=[ 1] ,
77 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
78 VHydCond=[ 0.055](mm/hr), END=- 1
79 *%-----|-----
80 *#
81 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
82 *# of 1.80
83 *%-----|-----
84 CONTINUOUS NASHYD NHYD=[ "JR_GWM"], DT=[ 1]min, AREA=[ 3074](ha),
85 DWF=[ 0](cms), CNVC=[ 55], IA=[ 2.5](mm),
86 N=[ 3], TP=[ 11.33]hrs,
87 Continuous simulation parameters:
88 IaRECper=[ 4](hrs),
89 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
90 InterEventTime=[ 12](hrs)
91 Baseflow simulation parameters:
92 BaseFlowOption=[ 1] ,
93 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
94 VHydCond=[ 0.055](mm/hr), END=- 1
95 *%-----|-----
96 CONTINUOUS NASHYD NHYD=[ "JR_ASH"], DT=[ 1]min, AREA=[ 1781](ha),
97 DWF=[ 0](cms), CNVC=[ 72], IA=[ 2.5](mm),
98 N=[ 3.0], TP=[ 3.91]hrs,
99 Continuous simulation parameters:
100 IaRECper=[ 4](hrs),
101 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
102 InterEventTime=[ 12](hrs)
103 Baseflow simulation parameters:
104 BaseFlowOption=[ 1] ,
105 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
106 VHydCond=[ 0.055](mm/hr), END=- 1
107 *%-----|-----
108 CONTINUOUS NASHYD NHYD=[ "SW_11"], DT=[ 1]min, AREA=[ 500](ha),
109 DWF=[ 0](cms), CNVC=[ 66], IA=[ 2.5](mm),
110 N=[ 3.0], TP=[ 1.24]hrs,
111 Continuous simulation parameters:
112 IaRECper=[ 4](hrs),
113 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
114 InterEventTime=[ 12](hrs)
115 Baseflow simulation parameters:
116 BaseFlowOption=[ 1] ,
117 InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
118 VHydCond=[ 0.055](mm/hr), END=- 1
119 *%-----|-----
120 *#
121 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
122 *# of 1.80
123 *%-----|-----
124 CONTINUOUS NASHYD NHYD=[ "NN_CK"], DT=[ 1]min, AREA=[ 1917](ha),
125 DWF=[ 0](cms), CNVC=[ 66], IA=[ 2.5](mm),

```

```

126 N=[ 3. 0], TP=[ 5. 29] hrs,
127 Continuous simulation parameters:
128 IaRECPper=[ 4] (hrs),
129 SMN=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010]/ (mm),
130 InterEventTime=[ 12] (hrs)
131 Baseflow simulation parameters:
132 BaseFlowOption=[ 1] ,
133 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
134 VHydCond=[ 0. 055] (mm/ hr), END=- 1
135 *%-----|-----
136 *#
137 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
138 *# of 1.52
139 *%-----|-----
140 CONTINUOUS NASHYD NHYD=[ "SW_10"], DT=[ 1] min, AREA=[ 5666] (ha),
141 DWF=[ 0] (cms), CNVC=[ 72], IA=[ 2. 5] (mm),
142 N=[ 3. 0], TP=[ 8. 00] hrs,
143 Continuous simulation parameters:
144 IaRECPper=[ 4] (hrs),
145 SMN=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010]/ (mm),
146 InterEventTime=[ 12] (hrs)
147 Baseflow simulation parameters:
148 BaseFlowOption=[ 1] ,
149 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
150 VHydCond=[ 0. 055] (mm/ hr), END=- 1
151 *%-----|-----
152 *#
153 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
154 *# of 1.75
155 *%-----|-----
156 CONTINUOUS NASHYD NHYD=[ "KG_CK"], DT=[ 1] min, AREA=[ 8376] (ha),
157 DWF=[ 0] (cms), CNVC=[ 66], IA=[ 2. 5] (mm),
158 N=[ 3. 0], TP=[ 11. 66] hrs,
159 Continuous simulation parameters:
160 IaRECPper=[ 4] (hrs),
161 SMN=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010]/ (mm),
162 InterEventTime=[ 12] (hrs)
163 Baseflow simulation parameters:
164 BaseFlowOption=[ 1] ,
165 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
166 VHydCond=[ 0. 055] (mm/ hr), END=- 1
167 *%-----|-----
168 *#
169 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
170 *# of 1.68
171 *%-----|-----
172 CONTINUOUS NASHYD NHYD=[ "SW_9"], DT=[ 1] min, AREA=[ 1132] (ha),
173 DWF=[ 0] (cms), CNVC=[ 70], IA=[ 2. 5] (mm),
174 N=[ 3. 0], TP=[ 2. 51] hrs,
175 Continuous simulation parameters:
176 IaRECPper=[ 4] (hrs),
177 SMN=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010]/ (mm),
178 InterEventTime=[ 12] (hrs)
179 Baseflow simulation parameters:
180 BaseFlowOption=[ 1] ,
181 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
182 VHydCond=[ 0. 055] (mm/ hr), END=- 1
183 *%-----|-----
184 *#
185 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
186 *# of 1.82
187 *%-----|-----
188 CONTINUOUS NASHYD NHYD=[ "NC_CK"], DT=[ 1] min, AREA=[ 4464] (ha),
189 DWF=[ 0] (cms), CNVC=[ 62], IA=[ 2. 5] (mm),
190 N=[ 3. 0], TP=[ 11. 32] hrs,
191 Continuous simulation parameters:

```

```

192 IaREcper=[ 4] (hr s),
193 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
194 InterEventTime=[ 12] (hr s)
195 Baseflow simulation parameters:
196 BaseFlowOption=[ 1] ,
197 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
198 VHydCond=[ 0. 055] (mm/ hr), END=- 1
199 *%-----|-----
200 *#
201 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
202 *# of 1.80
203 *%-----|-----
204 CONTINUOUS NASHYD NHYD=[ "SW_8" ], DT=[ 1] mi n, AREA=[ 131] (ha),
205 DWF=[ 0] (cms), CN C=[ 63], IA=[ 2. 5] (mm),
206 N=[ 3. 0], TP=[ 0. 90] hr s,
207 Continuous simulation parameters:
208 IaREcper=[ 4] (hr s),
209 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
210 InterEventTime=[ 12] (hr s)
211 Baseflow simulation parameters:
212 BaseFlowOption=[ 1] ,
213 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
214 VHydCond=[ 0. 055] (mm/ hr), END=- 1
215 *%-----|-----
216 *#
217 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
218 *# of 1.65
219 *%-----|-----
220 CONTINUOUS NASHYD NHYD=[ "HB_DR" ], DT=[ 1] mi n, AREA=[ 3854] (ha),
221 DWF=[ 0] (cms), CN C=[ 66], IA=[ 2. 5] (mm),
222 N=[ 3. 0], TP=[ 8. 42] hr s,
223 Continuous simulation parameters:
224 IaREcper=[ 4] (hr s),
225 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
226 InterEventTime=[ 12] (hr s)
227 Baseflow simulation parameters:
228 BaseFlowOption=[ 1] ,
229 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
230 VHydCond=[ 0. 055] (mm/ hr), END=- 1
231 *%-----|-----
232 *#
233 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
234 *# of 1.82
235 *%-----|-----
236 CONTINUOUS NASHYD NHYD=[ "SW_7" ], DT=[ 1] mi n, AREA=[ 3197] (ha),
237 DWF=[ 0] (cms), CN C=[ 57], IA=[ 2. 5] (mm),
238 N=[ 3. 0], TP=[ 6. 65] hr s,
239 Continuous simulation parameters:
240 IaREcper=[ 4] (hr s),
241 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
242 InterEventTime=[ 12] (hr s)
243 Baseflow simulation parameters:
244 BaseFlowOption=[ 1] ,
245 InitGWResVol=[ 50] (mm), GWResK=[ 0. 96] (mm/ day/ mm)
246 VHydCond=[ 0. 055] (mm/ hr), END=- 1
247 *%-----|-----
248 *#
249 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
250 *# of 1.75
251 *%-----|-----
252 CONTINUOUS NASHYD NHYD=[ "SW_6" ], DT=[ 1] mi n, AREA=[ 165] (ha),
253 DWF=[ 0] (cms), CN C=[ 67], IA=[ 2. 5] (mm),
254 N=[ 3. 0], TP=[ 4. 18] hr s,
255 Continuous simulation parameters:
256 IaREcper=[ 4] (hr s),
257 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),

```

```

258 InterEventTime=[ 12]( hrs)
259 Baseflow simulation parameters:
260 BaseFlowOption=[ 1] ,
261 InitGWResVol =[ 50]( mm) , GWResK=[ 0.96]( mm/ day/ mm)
262 VHydCond=[ 0.055]( mm/ hr) , END=- 1
263 *%-----|-----
264 *#
265 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
266 *# of 1.67
267 *%-----|-----
268 CONTINUOUS NASHYD NHYD=[ "VG_DR" ], DT=[ 1] mi n, AREA=[ 1332]( ha) ,
269 DWF=[ 0]( cms) , CNVC=[ 72] , IA=[ 2.5]( mm) ,
270 N=[ 3.0] , TP=[ 5.95] hr s,
271 Continuous simulation parameters:
272 IaRECper=[ 4]( hr s) ,
273 SMN=[ -1]( mm) , SMAX=[ -1]( mm) , SK=[ 0.010]/ ( mm) ,
274 InterEventTime=[ 12]( hr s)
275 Baseflow simulation parameters:
276 BaseFlowOption=[ 1] ,
277 InitGWResVol =[ 50]( mm) , GWResK=[ 0.96]( mm/ day/ mm)
278 VHydCond=[ 0.055]( mm/ hr) , END=- 1
279 *%-----|-----
280 CONTINUOUS NASHYD NHYD=[ "SW_5" ], DT=[ 1] mi n, AREA=[ 224]( ha) ,
281 DWF=[ 0]( cms) , CNVC=[ 77] , IA=[ 2.5]( mm) ,
282 N=[ 3.0] , TP=[ 0.75] hr s,
283 Continuous simulation parameters:
284 IaRECper=[ 4]( hr s) ,
285 SMN=[ -1]( mm) , SMAX=[ -1]( mm) , SK=[ 0.010]/ ( mm) ,
286 InterEventTime=[ 12]( hr s)
287 Baseflow simulation parameters:
288 BaseFlowOption=[ 1] ,
289 InitGWResVol =[ 50]( mm) , GWResK=[ 0.96]( mm/ day/ mm)
290 VHydCond=[ 0.055]( mm/ hr) , END=- 1
291 *%-----|-----
292 *#
293 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
294 *# of 1.20
295 *%-----|-----
296 CONTINUOUS NASHYD NHYD=[ "FL_CK" ], DT=[ 1] mi n, AREA=[ 4945]( ha) ,
297 DWF=[ 0]( cms) , CNVC=[ 74] , IA=[ 2.5]( mm) ,
298 N=[ 3.0] , TP=[ 4.45] hr s,
299 Continuous simulation parameters:
300 IaRECper=[ 4]( hr s) ,
301 SMN=[ -1]( mm) , SMAX=[ -1]( mm) , SK=[ 0.010]/ ( mm) ,
302 InterEventTime=[ 12]( hr s)
303 Baseflow simulation parameters:
304 BaseFlowOption=[ 1] ,
305 InitGWResVol =[ 50]( mm) , GWResK=[ 0.96]( mm/ day/ mm)
306 VHydCond=[ 0.055]( mm/ hr) , END=- 1
307 *%-----|-----
308 CONTINUOUS NASHYD NHYD=[ "SW_5A2" ], DT=[ 1] mi n, AREA=[ 20]( ha) ,
309 DWF=[ 0]( cms) , CNVC=[ 81] , IA=[ 2.5]( mm) ,
310 N=[ 3.0] , TP=[ 0.62] hr s,
311 Continuous simulation parameters:
312 IaRECper=[ 4]( hr s) ,
313 SMN=[ -1]( mm) , SMAX=[ -1]( mm) , SK=[ 0.010]/ ( mm) ,
314 InterEventTime=[ 12]( hr s)
315 Baseflow simulation parameters:
316 BaseFlowOption=[ 1] ,
317 InitGWResVol =[ 50]( mm) , GWResK=[ 0.96]( mm/ day/ mm)
318 VHydCond=[ 0.055]( mm/ hr) , END=- 1
319 *%-----|-----
320 *#
321 *# The Tp was modified according to a Peak Reduction factor (MFO-Chart B2-4)
322 *# of 1.61
323 *%-----|-----

```


324 CONTI NUOUS NASHYD NYHD=["SW_5A1"], DT=[1] mi n, AREA=[1412] (ha),
325 DWF=[0] (cms), CNV C=[75], IA=[2. 5] (mm),
326 N=[3. 0], TP=[8. 00] hr s,
327 Continuous simulation parameters:
328 IaRECPper=[4] (hr s),
329 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
330 InterEventTime=[12] (hr s)
331 Baseflow simulation parameters:
332 BaseFlowOpti on=[1] ,
333 In it GWR es Vol = [50] (mm), GWR es K=[0. 96] (mm / day / mm)
334 VHydCond=[0. 055] (mm / hr), END=- 1

*%-----|

336 CONTI NUOUS NASHYD NYHD=["SW_4"], DT=[1] mi n, AREA=[585] (ha),
337 DWF=[0] (cms), CNV C=[81], IA=[2. 5] (mm),
338 N=[3. 0], TP=[1. 75] hr s,
339 Continuous simulation parameters:
340 IaRECPper=[4] (hr s),
341 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
342 InterEventTime=[12] (hr s)
343 Baseflow simulation parameters:
344 BaseFlowOpti on=[1] ,
345 In it GWR es Vol = [50] (mm), GWR es K=[0. 96] (mm / day / mm)
346 VHydCond=[0. 055] (mm / hr), END=- 1

*%-----|

348 CONTI NUOUS NASHYD NYHD=["LM_CK"], DT=[1] mi n, AREA=[1021] (ha),
349 DWF=[0] (cms), CNV C=[80], IA=[2. 5] (mm),
350 N=[3. 0], TP=[2. 46] hr s,
351 Continuous simulation parameters:
352 IaRECPper=[4] (hr s),
353 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
354 InterEventTime=[12] (hr s)
355 Baseflow simulation parameters:
356 BaseFlowOpti on=[1] ,
357 In it GWR es Vol = [50] (mm), GWR es K=[0. 96] (mm / day / mm)
358 VHydCond=[0. 055] (mm / hr), END=- 1

*%-----|

360 CONTI NUOUS NASHYD NYHD=["SW_2"], DT=[1] mi n, AREA=[177] (ha),
361 DWF=[0] (cms), CNV C=[77], IA=[2. 5] (mm),
362 N=[3. 0], TP=[0. 75] hr s,
363 Continuous simulation parameters:
364 IaRECPper=[4] (hr s),
365 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
366 InterEventTime=[12] (hr s)
367 Baseflow simulation parameters:
368 BaseFlowOpti on=[1] ,
369 In it GWR es Vol = [50] (mm), GWR es K=[0. 96] (mm / day / mm)
370 VHydCond=[0. 055] (mm / hr), END=- 1

*%-----|

372 CONTI NUOUS NASHYD NYHD=["SM_DR"], DT=[1] mi n, AREA=[1122] (ha),
373 DWF=[0] (cms), CNV C=[81], IA=[2. 5] (mm),
374 N=[3. 0], TP=[3. 25] hr s,
375 Continuous simulation parameters:
376 IaRECPper=[4] (hr s),
377 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),
378 InterEventTime=[12] (hr s)
379 Baseflow simulation parameters:
380 BaseFlowOpti on=[1] ,
381 In it GWR es Vol = [50] (mm), GWR es K=[0. 96] (mm / day / mm)
382 VHydCond=[0. 055] (mm / hr), END=- 1

*%-----|

384 CONTI NUOUS NASHYD NYHD=["MO_DR"], DT=[1] mi n, AREA=[2737] (ha),
385 DWF=[0] (cms), CNV C=[76], IA=[2. 5] (mm),
386 N=[3. 0], TP=[3. 03] hr s,
387 Continuous simulation parameters:
388 IaRECPper=[4] (hr s),
389 SMN=[- 1] (mm), SMAX=[- 1] (mm), SK=[0. 010] / (mm),

```

390 InterEventTime=[ 12]( hrs)
391 Baseflow simulation parameters:
392 BaseFlowOption=[ 1] ,
393 InitGWResVol=[ 50]( mm) , GWResK=[ 0.96]( mm/ day/ mm)
394 VHydCond=[ 0.055]( mm/ hr) , END=- 1
395 *%-----|-----|
396 * -JFSA 2020 replaced SW_1 with a detailed model from Stantec Report 2007
397 *CONTINUOUS NASHYD NHYD=["SW_1"], DT=[ 1]mi n, AREA=[ 3176]( ha),
398 * DWF=[ 0]( cms) , CN/C=[ 78] , IA=[ 2.5]( mm),
399 * N=[ 3.0] , TP=[ 3.56]hrs,
400 * Continuous simulation parameters:
401 * IaRECper=[ 4]( hrs),
402 * SMN=[ -1]( mm) , SMAX=[ -1]( mm) , SK=[ 0.010]/( mm),
403 * InterEventTime=[ 12]( hrs)
404 * Baseflow simulation parameters:
405 * BaseFlowOption=[ 1] ,
406 * InitGWResVol=[ 50]( mm) , GWResK=[ 0.96]( mm/ day/ mm)
407 * VHydCond=[ 0.055]( mm/ hr) , END=- 1
408 *%-----|-----|
409 *#
410 *# Routing hydrographs
411 *#
412 *# Starting with the addition of Jock River Headwater and Subwatershed 13
413 *#
414 ADD HYD NHYDsum=["S_N13"], NHYDs to add=["JR_HW"+"SW_13"]
415 *%-----|-----|
416 *#
417 *# Sum of hydrographs from Node 13 routed to Node 13A
418 *# (Approximated cross-section - see cross-section 258)
419 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
420 *#
421 ROUTE CHANNEL NHYDout=["N13A"] , NHYDin=["S_N13"],
422 RDT=[ 1]( mi n),
423 CHLGTH=[ 9074]( m) , CHSLOPE=[ 0.0220]( %),
424 FPSLOPE=[ 0.0220]( %),
425 SECNUM=[ 1.0] , NSEG=[ 1]
426 ( SEGROUGH, SEGDI ST ( m))=[ 0.04, 15.5] NSEG times
427 ( DI STANCE ( m) , ELEVATI ON ( m))=
428 [- 40, 132.5]
429 [- 30, 132]
430 [- 25, 131.5]
431 [- 13, 130]
432 [- 8, 127.00]
433 [- 7, 126.50]
434 [- 6, 126]
435 [- 5.5, 125.50]
436 [0, 123.75]
437 [4.5, 125.50]
438 [6, 126]
439 [7.5, 126.5]
440 [9, 127]
441 [10, 127.5]
442 [11.5, 128.0]
443 [15.5, 129.5]
444 *%-----|-----|
445 *#
446 *# Addition of Subwatershed Jock River at Goodwood Marsh to Node 13A
447 *#
448 ADD HYD NHYDsum=["SN13A"], NHYDs to add=["N13A"+"JR_GWM"]
449 *%-----|-----|
450 *#
451 *# Insertion of a reservoir to simulate the effects of the Goodwood Marsh
452 *#
453 ROUTE RESERVOIR NHYDout=["RES_GM"] , NHYDin=["SN13A"],
454 RDT=[ 1]( mi n),
455 TABLE of ( OUTFLOW STORAGE ) values

```

```

456 (cms) - (ha-m)
457 [ 0.0 , 0.0 ]
458 [ 1.991, 2.144 ]
459 [ 2.693, 39.826 ]
460 [ 3.509, 81.697 ]
461 [ 4.578, 318.774 ]
462 [ 5.647, 594.947 ]
463 [ 7.109, 910.219 ]
464 [ 8.616, 1264.589 ]
465 [ 10.371, 1658.057 ]
466 [ 12.402, 2090.622 ]
467 [ 22.056, 3462.487 ]
468 [ -1 , -1 ] (max twenty pts)
469
470 NHYDovf=[ " " ] ,
471 *%-----|-----|
472 *#
473 SAVE HYD NHYD=[ "RES_GM" ], # OF PCYCLES=[ -1 ], I CASEs h=[ -1 ]
474 HYD_FILENAMES=[ "H_RESGM" ]
475 HYD_COMMENT=[ "Out flow from Res GM" ]
476 *%-----|-----|
477 *# Output of Reservoir Goodwood Marsh routed from Node 13A to Node 12
478 *# (Approximated cross-section - see cross-section 258)
479 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
480 ROUTE CHANNEL NHYDout=[ "N12" ] , NHYDin=[ "RES_GM" ] ,
481 RDT=[ 1 ] (min) ,
482 CHLGTH=[ 5926 ] (m) , CHSLOPE=[ 0.0759 ] ( % ) ,
483 FPSLOPE=[ 0.0759 ] ( % ) ,
484 SECNUM=[ 1.0 ] , NSEG=[ 1 ]
485 ( SEGROUGH, SEGDIST (m) )=[ 0.04, 15.5 ] NSEG times
486 ( DISTANCE (m) , ELEVATION (m) )=
487 [- 40, 132.5]
488 [- 30, 132]
489 [- 25, 131.5]
490 [- 13, 130]
491 [- 8, 127.00]
492 [- 7, 126.50]
493 [- 6, 126]
494 [- 5.5, 125.50]
495 [ 0, 123.75]
496 [ 4.5, 125.50]
497 [ 6, 126]
498 [ 7.5, 126.5]
499 [ 9, 127]
500 [ 10, 127.5]
501 [ 11.5, 128.00]
502 [ 15.5, 129.5]
503 *%-----|-----|
504 *#
505 *# Addition of Subwatershed Jock River at Ashton to Node 12
506 *#
507 ADD HYD NHYDsum=[ "S_N12" ] , NHYDs to add=[ "N12"+"JR_ASH" ]
508 SAVE HYD NHYD=[ "S_N12" ] , # OF PCYCLES=[ -1 ], I CASEs h=[ -1 ]
509 HYD_FILENAMES=[ "H_SN12" ]
510 HYD_COMMENT=[ "flow at S_N12 near Ashton" ]
511 *%-----|-----|
512 *#
513 *# Sum of hydrographs from Node 12 routed to Node 11
514 *# (Approximated cross-section - see cross-section 258)
515 *# Use n=0.04 for summer conditions and n=0.025 for spring conditions
516 *ROUTE CHANNEL NHYDout=[ "N11" ] , NHYDin=[ "S_N12" ] ,
517 * RDT=[ 1 ] (min) ,
518 * CHLGTH=[ 972 ] (m) , CHSLOPE=[ 0.0514 ] ( % ) ,
519 * FPSLOPE=[ 0.0514 ] ( % ) ,
520 * SECNUM=[ 1.0 ] , NSEG=[ 1 ]
521 * ( SEGROUGH, SEGDIST (m) )=[ 0.04, 15.5 ] NSEG times
522 * ( DISTANCE (m) , ELEVATION (m) )=

```

```

522 * [- 40, 132.5]
523 * [- 30, 132]
524 * [- 25, 131.5]
525 * [- 13, 130]
526 * [- 8, 127.00]
527 * [- 7, 126.50]
528 * [- 6, 126]
529 * [- 5.5, 125.50]
530 * [0, 123.75]
531 * [4.5, 125.50]
532 * [6, 126]
533 * [7.5, 126.5]
534 * [9, 127]
535 * [10, 127.5]
536 * [11.5, 128.00]
537 * [15.5, 129.5]
538 *%-----|-----
539 *#
540 *# Sum of hydrographs from Node 12 routed to Node 11 with Dummy section 248
541 *#
542 ROUTE CHANNEL NHYDout=["Duml1"], NHYDin=["S_N12"],
543 RDT=[1](min),
544 CHLGTH=[972](m), CHSLOPE=[0.054](%),
545 FPSLOPE=[0.054](%),
546 SECNUM=[1.0], NSEG=[1]
547 ( SEGROUGH, SEGDIST (m))=[0.04, 15.5] NSEG times
548 ( DISTANCE (m), ELEVATION (m))=
549 [- 40, 132.5]
550 [- 30, 132]
551 [- 25, 131.5]
552 [- 13, 130]
553 [- 8, 127.00]
554 [- 7, 126.50]
555 [- 6, 126]
556 [- 5.5, 125.50]
557 [0, 123.75]
558 [4.5, 125.50]
559 [6, 126]
560 [7.5, 126.5]
561 [9, 127]
562 [10, 127.5]
563 [11.5, 128.00]
564 [15.5, 129.5]
565 *%-----|-----
566 *#
567 *# Addition of Subwatershed 11 and No Name Creek to Node 11
568 *#
569 ADD HYD NHYDsum=["S_N11"], NHYDstoadd=["Duml1"+"SW_11"+"NN_CK"]
570 *%-----|-----
571 *#
572 *# Sum of hydrographs from Node 11 routed to Node 10
573 *# Section 1
574 *#
575 ROUTE CHANNEL NHYDout=["N10"], NHYDin=["S_N11"],
576 RDT=[1](min),
577 CHLGTH=[14028](m), CHSLOPE=[0.1568](%),
578 FPSLOPE=[0.1568](%),
579 SECNUM=[1.0], NSEG=[5]
580 ( SEGROUGH, SEGDIST (m))=
581 [0.04, -52.82
582 0.1, -6.47
583 -0.05, 6.47
584 0.1, 45.36
585 0.04, 423.88] NSEG times
586 ( DISTANCE (m), ELEVATION (m))=
587 [- 226.24 , 112.50]

```

```

588             [- 167. 50 , 111. 50]
589             [- 106. 81 , 111. 00]
590             [- 92. 37 , 110. 00]
591             [- 52. 82 , 109. 00]
592             [- 24. 90, 109. 00]
593             [- 17. 02, 108. 50]
594             [- 6. 47, 108. 00]
595             [ 6. 47, 108. 00]
596             [ 15. 67, 108. 50]
597             [ 18. 95, 109. 00]
598             [ 45. 36, 109. 50]
599             [ 120. 79, 110. 00]
600             [ 145. 72, 111. 00]
601             [ 181. 56, 111. 50]
602             [ 423. 88, 112. 50]
603 *%-----|-----
604 *#
605 *# Addition of Subwatershed 10 to Node 10
606 *#
607 ADD HYD          NHYDs um=["S_N10"], NHYDs to add=["N10"+"SW_10"]
608 *%-----|-----
609 SAVE HYD        NHYD=["S_N10"], # OF PCYCLES=[- 1], I CASEs h=[- 1]
610                HYD_FILE NAME=["H_SN10"]
611                HYD_COMMENT=["flow at S_N10: N10 + SW_10"]
612 *%-----|-----
613 *# Addition of Kings Creek to S_N10
614 *#
615 ADD HYD          NHYDs um=["S_N10A"], NHYDs to add=["S_N10"+"KG_CK"]
616 *%-----|-----
617 *#
618 *# Sum of hydrographs from Node 10 routed to Node 9
619 *# Section 2
620 *#
621 ROUTE CHANNEL    NHYDout=["N9"] , NHYDin=["S_N10A"] ,
622                RDT=[ 1] ( mi n) ,
623                CHLGTH=[ 3982] ( m) ,    CHSLOPE=[ 0. 0753] ( % ) ,
624                FPSLOPE=[ 0. 0753] ( % ) ,
625                SECNUM=[ 1. 0] ,        NSEG=[ 4]
626                ( SEGROUGH, SEGDI ST ( m) ) =
627                [ 0. 04, - 30. 27
628                0. 05, - 18. 42
629                - 0. 05, 18. 42
630                0. 04, 131. 58] NSEG times
631                ( DI STANCE ( m) , ELEVATI ON ( m) ) =
632                [- 446. 74, 106. 00]
633                [- 415. 68, 105. 50]
634                [- 285. 40, 105. 00]
635                [- 173. 77, 104. 50]
636                [- 144. 95, 104. 00]
637                [- 111. 18, 103. 50]
638                [- 94. 06, 103. 00]
639                [- 71. 02, 102. 50]
640                [- 30. 27, 102. 00]
641                [- 19. 33, 100. 00]
642                [- 18. 42, 99. 50]
643                [ 18. 42, 99. 50]
644                [ 20. 77, 100. 00]
645                [ 27. 93, 101. 00]
646                [ 52. 29, 101. 00]
647                [ 68. 80, 101. 50]
648                [ 79. 66, 103. 00]
649                [ 91. 50, 103. 50]
650                [ 131. 58, 104. 00]
651 *%-----|-----
652 *#
653 *# Addition of Subwatershed 9 and Nichols Creek to Node 9

```

```

654  *#
655  ADD HYD          NHYDs um=[ "S_N9" ], NHYDs  to  add=[ "N9"+"SW_9"+"NC_CK" ]
656  *%-----|-----|
657  *#
658  *# Sum of hydrographs from Node 9 routed to Node 8
659  *# Section 3
660  *#
661  ROUTE CHANNEL    NHYDout =[ "N8" ] , NHYDin =[ "S_N9" ] ,
662                  RDT=[ 1 ] ( mi n ) ,
663                  CHLGTH=[ 2269 ] ( m ) ,   CHSLOPE=[ 0.0882 ] ( % ) ,
664                                                    FPSLOPE=[ 0.0882 ] ( % ) ,
665                  SECNUM=[ 1.0 ] ,          NSEG=[ 3 ]
666                  ( SEGROUGH, SEGDI ST ( m ) ) =
667                    [ 0.1, -17.99
668                      -0.045, 17.31
669                      0.1, 456.58 ] NSEG t i m e s
670                  ( DI STANCE ( m ) , ELEVATI ON ( m ) ) =
671                    [ -201.19, 100.50 ]
672                    [ -135.21, 100.00 ]
673                    [ -94.83, 99.50 ]
674                    [ -67.05, 99.00 ]
675                    [ -17.99, 98.50 ]
676                    [ -16.02, 98.00 ]
677                    [ -13.95, 97.50 ]
678                    [ 13.95, 97.50 ]
679                    [ 15.64, 98.00 ]
680                    [ 17.31, 98.50 ]
681                    [ 162.02, 98.50 ]
682                    [ 172.89 , 99.00 ]
683                    [ 314.38, 99.00 ]
684                    [ 343.78, 99.50 ]
685                    [ 365.67, 100.00 ]
686                    [ 376.68, 100.00 ]
687                    [ 393.11, 99.50 ]
688                    [ 404.97, 99.50 ]
689                    [ 431.70, 100.00 ]
690                    [ 456.58, 100.50 ]
691  *%-----|-----|
692  *#
693  *# Addition of Subwatershed 8 and Hobb's Drain to Node 8
694  *#
695  ADD HYD          NHYDs um=[ "S_N8" ], NHYDs  to  add=[ "N8"+"SW_8"+"HB_DR" ]
696  *%-----|-----|
697  *#
698  *# Sum of hydrographs from Node 8 routed to Node 7
699  *# Section 4
700  *#
701  ROUTE CHANNEL    NHYDout =[ "N7" ] , NHYDin =[ "S_N8" ] ,
702                  RDT=[ 1 ] ( mi n ) ,
703                  CHLGTH=[ 3750 ] ( m ) ,   CHSLOPE=[ 0.0533 ] ( % ) ,
704                                                    FPSLOPE=[ 0.0533 ] ( % ) ,
705                  SECNUM=[ 1.0 ] ,          NSEG=[ 3 ]
706                  ( SEGROUGH, SEGDI ST ( m ) ) =
707                    [ 0.12, -18.11
708                      -0.07, 17.22
709                      0.12, 590.05 ] NSEG t i m e s
710                  ( DI STANCE ( m ) , ELEVATI ON ( m ) ) =
711                    [ -433.21, 102.00 ]
712                    [ -425.34, 101.50 ]
713                    [ -377.56, 101.50 ]
714                    [ -366.23, 101.00 ]
715                    [ -202.60, 100.50 ]
716                    [ -96.25, 99.50 ]
717                    [ -68.36 99.00 ]
718                    [ -18.11, 98.50 ]
719                    [ -13.81, 97.50 ]

```

```

720 [ 13. 81, 97. 50]
721 [ 17. 22, 98. 50]
722 [ 161. 95, 98. 50]
723 [ 173. 11, 99. 00]
724 [ 314. 05, 99. 00]
725 [ 365. 52, 100. 00]
726 [ 404. 70, 99. 50]
727 [ 476. 74, 100. 50]
728 [ 502. 31, 101. 00]
729 [ 584. 69, 101. 00]
730 [ 585. 79, 101. 00]
731 [ 590. 05, 102. 00]
732 *%-----|-----
733 *#
734 *# Addition of Subwatershed 7 to Node 7
735 *#
736 ADD HYD          NHYDs um=[ "S_N7" ], NHYDs to add=[ "N7"+"SW_7" ]
737 *%-----|-----
738 SAVE HYD         NHYD=[ "S_N7" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ - 1 ]
739                 HYD_FI LENAME=[ "H_SN7" ]
740                 HYD_COMMENT=[ "flow at S_N7: N7 + SW_7" ]
741 *%-----|-----
742 *# Insertion of a reservoir to simulate the effects of the Richmond Fen.
743 *# Storage area and volumes were estimated from available topo maps.
744 *# Release rate from fen was assumed to be controlled by the downstream
745 *# river cross-section for summer conditions. It is was assumed that for up to
746 *# 0.75 m of water, the main channel of the river provided the storage. Above
747 *# this depth, the wetland starts to signigicantly store water.
748 *#
749 ROUTE RESERVOIR NHYDout =[ "RES_RF" ] , NHYDi n=[ "S_N7" ] ,
750                 RDT=[ 1 ] ( mi n ) ,
751                 TABLE of ( OUTFLOW STORAGE ) values
752                         ( cms ) - ( ha- m )
753                 TABLE of ( OUTFLOW STORAGE ) values
754                         ( cms ) - ( ha- m )
755                         [ 0. 0 , 0. 0 ]
756                         [ 0. 9051, 2. 40]
757                         [ 2. 907, 4. 13]
758                         [ 9. 744, 9. 18]
759                         [ 20. 304, 14. 96]
760                         [ 34. 167, 310. 21]
761                         [ 74. 993, 605. 46]
762                         [ 104. 876, 900. 71]
763                         [ 140. 56, 2892. 00]
764                         [ 225. 00, 3615. 63]
765                         [ - 1 , - 1 ] (max t wenty pts)
766                 NHYDovf=[ " " ] ,
767 *%-----|-----
768 SAVE HYD         NHYD=[ "RES_RF" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ - 1 ]
769                 HYD_FI LENAME=[ "H_Res RF" ]
770                 HYD_COMMENT=[ "out flow of Ri chmond Fen" ]
771 *%-----|-----
772 *#
773 *# Sum of hydrographs from Node 7 routed to Node 6
774 *# Section 5
775 *#
776 ROUTE CHANNEL   NHYDout =[ "N6" ] , NHYDi n=[ "RES_RF" ] ,
777                 RDT=[ 1 ] ( mi n ) ,
778                 CHLGTH=[ 3056 ] ( m ) , CHSLOPE=[ 0. 0818 ] ( % ) ,
779                 FPSLOPE=[ 0. 0818 ] ( % ) ,
780                 SECNUM=[ 1. 0 ] , NSEG=[ 5 ]
781                 ( SEGROUGH, SEGDI ST ( m ) ) =
782                 [ 0. 025, - 70. 8
783                 0. 1, - 23. 9
784                 - 0. 05, 23. 9
785                 0. 06, 39. 8

```

```

786           0. 05, 96. 3] NSEG times
787           ( DI STANCE ( m), ELEVATI ON ( m))=
788             [- 100. 8, 97. 00]
789             [- 70. 8, 96. 50]
790             [- 52. 0, 96. 00]
791             [- 35. 1, 95. 50]
792             [- 30. 6, 95. 00]
793             [- 23. 9, 94. 54]
794             [ 23. 9, 94. 54]
795             [ 39. 8, 95. 00]
796             [ 50. 4, 95. 50]
797             [ 93. 5, 96. 00]
798             [ 94. 9, 96. 50]
799             [ 96. 3, 97. 00]
800 *%-----|-----
801 *#
802 *# Addition of Subwatershed 6 and Van Gaal Drain to Node 6
803 *#
804 ADD HYD           NHYDs um=[ "S_N6" ], NHYDs to add=[ "N6"+"SW_6"+"VG_DR" ]
805 *%-----|-----
806 *#
807 *# Sum of hydrographs from Node 6 routed to Node 5
808 *# Section 6
809 *#
810 ROUTE CHANNEL     NHYDout =[ "N5" ] , NHYDin =[ "S_N6" ] ,
811                   RDT=[ 1] ( mi n),
812                   CHLGTH=[ 1852] ( m),   CHSLOPE=[ 0. 0540] ( %),
813                                           FPSLOPE=[ 0. 0540] ( %),
814                   SECNUM=[ 1. 0],       NSEG=[ 3]
815                   ( SEGROUGH, SEGDI ST ( m))=
816                     [ 0. 035, - 131. 59
817                     - 0. 045, 48. 96
818                     0. 1, 239. 04] NSEG times
819                   ( DI STANCE ( m), ELEVATI ON ( m))=
820                     [- 686. 30, 94. 50]
821                     [- 675. 70, 94. 00]
822                     [- 492. 52, 93. 00]
823                     [- 467. 28, 94. 00]
824                     [- 131. 59, 94. 00]
825                     [- 92. 79, 92. 50]
826                     [- 18. 06, 91. 00]
827                     [ 18. 06, 91. 00]
828                     [ 43. 47, 92. 50]
829                     [ 48. 96, 94. 00]
830                     [ 177. 43, 94. 00]
831                     [ 239. 04, 94. 50]
832 *%-----|-----
833 *#
834 *# Addition of Subwatershed 5 and Flowing Creek to Node 5
835 *#
836 ADD HYD           NHYDs um=[ "S_N5" ], NHYDs to add=[ "N5"+"SW_5"+"FL_CK" ]
837 *%-----|-----
838 *#
839 *# Sum of hydrographs from Node 5 routed to Node 5A
840 *# Section 7
841 *#
842 ROUTE CHANNEL     NHYDout =[ "N5A" ] , NHYDin =[ "S_N5" ] ,
843                   RDT=[ 1] ( mi n),
844                   CHLGTH=[ 556] ( m),   CHSLOPE=[ 0. 0900] ( %),
845                                           FPSLOPE=[ 0. 0900] ( %),
846                   SECNUM=[ 1. 0],       NSEG=[ 4]
847                   ( SEGROUGH, SEGDI ST ( m))=
848                     [ 0. 04, - 41. 5
849                     0. 1, - 14. 0
850                     - 0. 045, 14. 0
851                     0. 1, 41. 1] NSEG times

```



```

852 ( DI STANCE ( m) , ELEVATI ON ( m) ) =
853 [- 275. 8, 93. 00]
854 [- 248. 6, 92. 50]
855 [- 237. 0, 92. 00]
856 [- 219. 3, 91. 50]
857 [- 202. 1, 91. 50]
858 [- 186. 0, 92. 00]
859 [- 129. 2, 92. 00]
860 [- 117. 6, 91. 50]
861 [- 100. 6, 91. 00]
862 [- 41. 5, 91. 00]
863 [- 20. 0, 91. 00]
864 [- 14. 0, 90. 54]
865 [ 14. 0, 90. 54]
866 [ 15. 3, 91. 00]
867 [ 17. 3, 91. 50]
868 [ 38. 4, 92. 00]
869 [ 39. 8, 92. 50]
870 [ 41. 1, 93. 00]
871 *%-----|-----|
872 *#
873 *# Addition of Subwatershed 5A1 and Subwatershed 5A2 to Node 5A
874 *#
875 ADD HYD NHYDs um=[ "S_N5A" ] , NHYDs t o add=[ "N5A"+"SW_5A2"+"SW_5A1" ]
876 *%-----|-----|
877 *#
878 *# Sum of hydrographs from Node 5A routed to Node 4
879 *# Section 8
880 *#
881 ROUTE CHANNEL NHYDout =[ "N4" ] , NHYDi n=[ "S_N5A" ] ,
882 RDT=[ 1 ] ( mi n) ,
883 CHLGTH=[ 4630 ] ( m) , CHSLOPE=[ 0. 0432 ] ( % ) ,
884 FPSLOPE=[ 0. 0432 ] ( % ) ,
885 SECNUM=[ 1. 0 ] , NSEG=[ 3 ]
886 ( SEGROUGH, SEGDI ST ( m) ) =
887 [ 0. 05, -28. 2
888 -0. 035, 28. 2
889 0. 05, 173. 1 ] NSEG t i mes
890 ( DI STANCE ( m) , ELEVATI ON ( m) ) =
891 [- 38. 9, 92. 00]
892 [- 35. 8, 91. 50]
893 [- 33. 3, 91. 00]
894 [- 28. 2, 90. 50]
895 [- 15. 0, 87. 48]
896 [- 5. 0, 88. 34]
897 [ 5. 0, 86. 20]
898 [ 15. 0, 88. 55]
899 [ 28. 2, 90. 50]
900 [ 29. 7, 91. 00]
901 [ 46. 5, 91. 00]
902 [ 127. 8, 91. 00]
903 [ 148. 7, 91. 50]
904 [ 173. 1, 92. 00]
905 *%-----|-----|
906 *#
907 *# Addition of Subwatershed 4 and Leamy Creek to Node 4
908 *#
909 ADD HYD NHYDs um=[ "S_N4" ] , NHYDs t o add=[ "N4"+"SW_4"+"LM_CK" ]
910 SAVE HYD NHYD=[ "S_N4" ] , # OF PCYCLES=[ - 1 ] , I CASEs h=[ 1 ]
911 HYD_COMMENT=[ "f l ow at S_N4" ]
912 *%-----|-----|
913 *#
914 *# Sum of hydrographs from Node 4 routed to Node 2
915 *# Section 9
916 *#
917 ROUTE CHANNEL NHYDout =[ "N2" ] , NHYDi n=[ "S_N4" ] ,

```

```

918 RDT=[ 1] ( mi n),
919 CHLGTH=[ 1667] ( m), CHSLOPE=[ 0. 0600] ( %),
920 FPSLOPE=[ 0. 0600] ( %),
921 SECNUM=[ 1. 0], NSEG=[ 4]
922 ( SEGROUGH, SEGDI ST ( m))=
923 [ 0. 1, - 28. 0
924 - 0. 04, 28. 4
925 0. 06, 31. 7
926 0. 04, 80. 2] NSEG t i m e s
927 ( DI STANCE ( m), ELEVATI ON ( m))=
928 [- 36. 3, 92. 00]
929 [- 32. 6, 91. 50]
930 [- 30. 2, 91. 00]
931 [- 28. 0, 90. 45]
932 [- 15. 0, 87. 48]
933 [- 5. 0, 88. 34]
934 [ 5. 0, 86. 20]
935 [ 15. 0, 88. 55]
936 [ 28. 0, 90. 45]
937 [ 28. 4, 90. 50]
938 [ 30. 4, 91. 00]
939 [ 31. 7, 91. 50]
940 [ 80. 2, 92. 00]
941 *%-----|-----|
942 *#
943 *# Addition of Subwatershed 2 with Monohan Drain and Smith Drain to Node 2
944 *#
945 ADD HYD NHYDs um=[ "S_N2"], NHYDs t o add=[ "N2"+"SW_2"+"SM_DR"+"MO_DR"]
946 *%-----|-----|
947 SAVE HYD NHYD=[ "S_N2"], # OF PCYCLES=[ - 1], I CAS E s h=[ - 1]
948 HYD_FI L E N A M E=[ "H_S_N2"]
949 HYD_C O M M E N T=[ "f l o w a t S_N2 J o c k R i v e r G a u g e a t M o d i e D r. "]
950 *%-----|-----|
951 *#
952 *# Sum of hydrographs from Node 2 routed to Node 1
953 *# Section 10
954 *#
955 *#*****
956 *%READ HYD NHYD=[ "S_N2"],
957 *% HYD_FI L E N A M E=[ "H_S_N2"]
958 *%-----|-----|
959 *#
960 *# Hydrograph from Node 2 routed to Node 416
961 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 9025
962 *#
963 ROUTE CHANNEL NHYDout =["N_416"] , NHYDin=["S_N2"] ,
964 RDT=[ 1] ( mi n),
965 CHLGTH=[ 2327] ( m), CHSLOPE=[ 0. 0498] ( %),
966 FPSLOPE=[ 0. 0498] ( %),
967 SECNUM=[ 1. 0], NSEG=[ 3]
968 ( SEGROUGH, SEGDI ST ( m))=
969 [ 0. 075, - 23. 96
970 - 0. 055, 23. 96
971 0. 075, 157. 38] NSEG t i m e s
972 ( DI STANCE ( m), ELEVATI ON ( m))=
973 [- 336. 97, 93. 5]
974 [- 318. 85, 93]
975 [- 259, 92. 5]
976 [- 133. 18, 92]
977 [- 33. 17, 92]
978 [- 27. 21, 92]
979 [- 26. 14, 91. 5]
980 [- 24. 99, 91]
981 [- 23. 96, 90. 5]
982 [- 14. 33, 88. 26]
983 [- 0. 68, 88. 12]

```

```

984 [ 14. 33, 88. 26]
985 [ 23. 96, 90. 5]
986 [ 32. 12, 91]
987 [ 43. 74, 91. 5]
988 [ 57. 09, 92]
989 [ 73. 53, 92. 5]
990 [ 108. 27, 93]
991 [ 125. 88, 93. 5]
992 [ 144. 81, 94]
993 [ 157. 38, 94. 5]
994 *%-----|-----|
995 *#*****|*****|
996 *# Catchment SW1a
997 *# - Portion of RVCA catchment SW1 outside of Reach 1 subwatershed
998 *# - Undeveloped agricultural land
999 *#*****|*****|
1000 CONTINUOUS NASHYD NHYD=[ "SW_1a" ], DT=[ 1] mi n, AREA=[ 536. 42] ( ha ),
1001 DWF=[ 0] ( cms ), CN C=[ 72], I A=[ 4. 67] ( mm ),
1002 N=[ 3], TP=[ 2. 79] hr s,
1003 Continuous simulation parameters:
1004 I aRECper=[ 4] ( hr s ),
1005 SM N=[ - 1] ( mm ), SMAX=[ - 1] ( mm ), SK=[ 0. 010] / ( mm ),
1006 I nterEventTi me=[ 12] ( hr s)
1007 Baseflow simulation parameters:
1008 BaseFlowOpt ion=[ 1] ,
1009 I n i t GWR es Vol =[ 50] ( mm ), GWR es K=[ 0. 96] ( mm / day / mm)
1010 VHydCond=[ 0. 055] ( mm / hr ), END=- 1
1011 *%-----|-----|
1012 * -JFSA 2021-02-25 "S-1-Okeefe" is a part of S-1 sub-catchment. It is moved to drain
before station 7245 on Jock River
1013 CONTINUOUS STANDHYD NHYD=[ "S-1-Okeefe" ], DT=[ 1] ( mi n), AREA=[ 44. 93] ( ha ), XI MP=[ 0. 65],
TI MP=[ 0. 65], DWF=[ 0] ( cms ),
1014 LOSS=[ 2], SCS curve number CN=[ 75], Pervious surfaces:
I Aper=[ 4. 67] ( mm ), SLPP=[ 2. 0] ( % ),
1015 LGP=[ 40] ( m ), MNP=[ 0. 25], SCP=[ 0] ( mi n), Impervious surfaces:
I Ai mp=[ 1. 57] ( mm ), SLPI=[ 0. 75] ( % ),
1016 LGI =[ 547. 296] ( m ), MNI =[ 0. 013], SCI =[ 0] ( mi n),
1017 Continuous simulation parameters:
1018 I aRECper=[ 4] ( hr s), I aRECI mp=[ 4] ( hr s),
1019 SM N=[ - 1] ( mm ), SMAX=[ - 1] ( mm ), SK=[ 0. 010] / ( mm ),
1020 I nterEventTi me=[ 12] ( hr s), END=- 1
1021 *%-----|-----|
1022 COMPUTE DUALHYD NHYDin=[ "S-1-Okeefe" ], CI NLET=[ 4. 591] ( cms ), NI NLET=[ 1],
1023 M i j NHYD=[ "S-1-OkM" ]
1024 M nNHYD=[ "S-1-OkMN" ]
1025 TM I STO=[ 9999999] ( cu - m)
1026 *%-----|-----|
1027 ADD HYD NHYDsum=[ "S-1-OkS" ], NHYDs to add=[ "S-1-OkM" +"S-1-OkMN" ]
1028 *%-----|-----|
1029 ROUTE RESERVOIR NHYDout=[ "S-1-OkSR" ], NHYDin=[ "S-1-OkS" ],
1030 RDT=[ 1] ( mi n),
1031 TABLE of ( OUTFLOW STORAGE ) values
1032 ( cms ) - ( ha - m)
1033 [ 0. 0 , 0. 0 ]
1034 [ 0. 5370, 1. 7917 ]
1035 [ - 1 , - 1 ] ( max twenty pts)
1036 NHYDovf=[ "S-1-OkSovf" ]
1037 *%-----|-----|
1038 ADD HYD NHYDsum=[ "SN_416" ], NHYDs to
add=[ "N_416" +"SW_1a" +"S-1-OkSR" +"S-1-OkSovf" ]
1039 *%-----|-----|
1040 SAVE HYD NHYD=[ "SN_416" ], # OF PCYCLES=[ - 1], I CASEsh=[ 1]
1041 HYD_COMMENT=[ "Total Flows at Highway 416 before Station 7245" ]
1042 *%-----|-----|
1043 *#
1044 *# Hydrograph from Node 416 routed to Node at Okeefe drain

```

```

1045 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 7245
1046 *#
1047 ROUTE CHANNEL      NHYDout=["N_OK"], NHYDin=["SN_416"],
1048                    RDT=[1](min),
1049                    CHLGTH=[497](m),  CHSLOPE=[0.3018](%),
1050                    FPSLOPE=[0.3018](%),
1051                    SECNUM=[1.0],      NSEG=[3]
1052                    (SEGROUGH, SEGDIST(m))=
1053                    [0.075, -19.40
1054                    -0.055, 19.40
1055                    0.075, 377.02] NSEG times
1056                    (DISTANCE(m), ELEVATION(m))=
1057                    [-1061.41, 92.50]
1058                    [-945.91, 92.00]
1059                    [-783.64, 91.50]
1060                    [-136.74, 91.00]
1061                    [-86.04, 91.00]
1062                    [-20.86, 91.00]
1063                    [-20.18, 90.50]
1064                    [-19.40, 90.00]
1065                    [-11.68, 86.89]
1066                    [0.00, 86.10]
1067                    [12.09, 86.81]
1068                    [19.40, 90.00]
1069                    [34.68, 90.50]
1070                    [60.56, 91.00]
1071                    [170.14, 91.00]
1072                    [175.05, 90.50]
1073                    [180.29, 90.00]
1074                    [193.41, 90.00]
1075                    [195.98, 90.50]
1076                    [377.02, 92.50]
1077 *%-----|-----|
1078 *#*****|*****|
1079 *# Catchment OKEEFE
1080 *# - To O'Keefe drain (north of the Jock)
1081 *# - Developed with assumed 43% imp.
1082 *# - 2020-12-01 add Okeefe model (Area 513.02 HA) instead of current Okeefe (Area
1083 *# - 2020-11-20 Okeefe detailed model was added as per the NOVATECH SWWHYMD model
1084 *# - (Citi-Gate 2014).
1085 *%-----|-----|
1086 *#*****|*****|
1087 *#*****|*****|
1088 CONTINUOUS NASHYD  NHYD=["O-1R"], DT=[1]min, AREA=[63.72](ha),
1089                    DWF=[0](cms), CNVC=[61], IA=[6.2](mm), N=[3], TP=[.9]hrs,
1090                    Continuous simulation parameters:
1091                    IARECper=[4](hrs),
1092                    SMIN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1093                    InterEventTime=[12](hrs)
1094                    Baseflow simulation parameters:
1095                    BaseFlowOption=[1],
1096                    InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
1097                    VHydCond=[0.055](mm/hr), END=-1
1098 *%-----|-----|
1099 *#*****|*****|
1100 *#*****|*****|
1101 ROUTE CHANNEL      NHYDout=["O-1R"], NHYDin=["O-1R"], RDT=[1](min),
1102                    CHLGTH=[960](m), CHSLOPE=[0.63](%), FPSLOPE=[0.63](%),
1103                    SECNUM=[1], NSEG=[3]
1104                    (SEGROUGH, SEGDIST(m))=[0.06, 4 -.043, 6 0.06, 10] NSEG times
1105                    (DISTANCE(m), ELEVATION(m))=[0.00, 2.0]
1106                    [0.0, 2.0]
1107                    [4.0, 0.0]
1108                    [6.0, 0.0]

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1108 [ 10.0, 2.0]
1109 *%-----|-----|
1110 CONTINUOUS NASHYD NHYD=["O-2"], DT=[1] min, AREA=[28.61] (ha),
1111 DWF=[0] (cms), CN C=[57], IA=[5.2] (mm), N=[3], TP=[1.1] hrs,
1112 Continuous simulation parameters:
1113 IaRECPper=[4] (hrs),
1114 SMN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
1115 InterEventTime=[12] (hrs)
1116 Baseflow simulation parameters:
1117 BaseFlowOption=[1],
1118 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
1119 VHydCond=[0.055] (mm/hr), END=-1
1120 *%-----|-----|
1121 CONTINUOUS NASHYD NHYD=["O-4"], DT=[1] min, AREA=[46.94] (ha),
1122 DWF=[0] (cms), CN C=[49], IA=[9.2] (mm), N=[3], TP=[0.9] hrs,
1123 Continuous simulation parameters:
1124 IaRECPper=[4] (hrs),
1125 SMN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
1126 InterEventTime=[12] (hrs)
1127 Baseflow simulation parameters:
1128 BaseFlowOption=[1],
1129 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
1130 VHydCond=[0.055] (mm/hr), END=-1
1131 *%-----|-----|
1132 *TOTAL EXTERNAL FLOW NORTH OF O'KEEFE CT. CROSSING
1133 ADD HYD NHYDsum=["OKF-N"], NHYDstoadd=["O-1R"+"O-2"+"O-4"]
1134 *%-----|-----|
1135 *ROUTE FLOW THROUGH AREA O-6
1136 ROUTE CHANNEL ROUTE CHANNEL NHYDout=["OKF-NR"], NHYDin=["OKF-N"], RDT=[1] (min),
1137 CHLGTH=[210] (m), CHSLOPE=[.81] (%), FPSLOPE=[.81] (%),
1138 SECNUM=[1], NSEG=[3]
1139 (SEGROUGH, SEGDIST (m))=[0.043, 22.43 - 0.043, 25.07
1140 0.043, 45.54] NSEG times
1141 (DISTANCE (m), ELEVATION (m))=[0.00, 3.73]
1142 (14.62, 1.56)
1143 (18.41, 1.44)
1144 (22.43, 0.00)
1145 (25.07, 0.70)
1146 (29.10, 1.79)
1147 (33.73, 2.71)
1148 (45.54, 3.58)
1149 *%-----|-----|
1150 CONTINUOUS NASHYD NHYD=["O-6"], DT=[1] min, AREA=[16.46] (ha),
1151 DWF=[0] (cms), CN C=[43], IA=[9.2] (mm), N=[3], TP=[0.7] hrs,
1152 Continuous simulation parameters:
1153 IaRECPper=[4] (hrs),
1154 SMN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
1155 InterEventTime=[12] (hrs)
1156 Baseflow simulation parameters:
1157 BaseFlowOption=[1],
1158 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
1159 VHydCond=[0.055] (mm/hr), END=-1
1160 *%-----|-----|
1161 CONTINUOUS STANDHYD NHYD=["O-3"], DT=[1] (min), AREA=[39.67] (ha), XI MP=[0.15],
1162 TI MP=[0.30], DWF=[0] (cms),
1163 LOSS=[2], SCS curve number CN=[50], Pervious surfaces:
1164 IAper=[4.67] (mm), SLPP=[0.32] (%),
1165 LGP=[440] (m), MNP=[0.035], SCP=[0] (min), Impervious surfaces:
1166 IAimp=[1.57] (mm), SLPI=[0.32] (%),
1167 LGI=[1880] (m), MNI=[0.013], SCI=[0] (min),
1168 Continuous simulation parameters:
1169 IaRECPper=[4] (hrs), IaRECImp=[4] (hrs),
1170 SMN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
1171 InterEventTime=[12] (hrs), END=-1
1172 *%-----|-----|
1173 CONTINUOUS STANDHYD NHYD=["O-5"], DT=[1] (min), AREA=[60.63] (ha), XI MP=[0.13],

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1171  T I M P=[ 0. 26] ,  D W F=[ 0] ( c m s ) ,
1172      L O S S=[ 2] ,  S C S  c u r v e  n u m b e r  C N=[ 61] ,
1173      P e r v i o u s  s u r f a c e s :  I A p e r=[ 4. 67] ( m m ) ,  S L P P=[ 1. 38] ( % ) ,
      L G P=[ 550] ( m ) ,  M N P=[ 0. 035] ,  S C P=[ 0] ( m i n ) ,  I m p e r v i o u s  s u r f a c e s :
1174      I A i m p=[ 1. 57] ( m m ) ,  S L P I=[ 1. 38] ( % ) ,
1175      L G I=[ 1450] ( m ) ,  M N I=[ 0. 013] ,  S C I=[ 0] ( m i n ) ,
1176      C o n t i n u o u s  s i m u l a t i o n  p a r a m e t e r s :
1177      I a R E C p e r=[ 4] ( h r s ) ,  I a R E C i m p=[ 4] ( h r s ) ,
1178      S M N=[ - 1] ( m m ) ,  S M A X=[ - 1] ( m m ) ,  S K=[ 0. 010] / ( m m ) ,
1179      I n t e r E v e n t T i m e=[ 12] ( h r s ) ,  E N D=- 1
1180  *%-----|-----|
1181  *TOTAL EXTERNAL FLOWS WEST OF THE SITE AND NORTH OF O'KEEFE CRT
1182  *%-----|-----|
1183  ADD HYD      N H Y D s u m=[ " P T 1 " ] ,  N H Y D s  t o  a d d=[ " O K F - N R " + " O - 3 " + " O - 5 " + " O - 6 " ]
1184  CONTINUOUS NASHYD  N H Y D=[ " O - 7 " ] ,  D T=[ 1] m i n ,  A R E A=[ 5. 28] ( h a ) ,
1185      D W F=[ 0] ( c m s ) ,  C N V C=[ 54] ,  I A=[ 7. 5] ( m m ) ,  N=[ 3] ,  T P=[ 0. 6] h r s ,
1186      C o n t i n u o u s  s i m u l a t i o n  p a r a m e t e r s :
1187      I a R E C p e r=[ 4] ( h r s ) ,
1188      S M N=[ - 1] ( m m ) ,  S M A X=[ - 1] ( m m ) ,  S K=[ 0. 010] / ( m m ) ,
1189      I n t e r E v e n t T i m e=[ 12] ( h r s )
1190      B a s e f l o w  s i m u l a t i o n  p a r a m e t e r s :
1191      B a s e F l o w O p t i o n=[ 1] ,
1192      I n i t G W R e s V o l=[ 50] ( m m ) ,  G W R e s K=[ 0. 96] ( m m / d a y / m m )
1193      V H y d C o n d=[ 0. 055] ( m m / h r ) ,  E N D=- 1
1194  *%-----|-----|
1195  *ANALYSIS POINT 1 - TOTAL FLOW NORTH OF FALLOWFIELD DR. AND O'KEEFE CRT.
1196  ADD HYD      N H Y D s u m=[ " F F " ] ,  N H Y D s  t o  a d d=[ " P T 1 " + " O - 7 " ]
1197  *%-----|-----|
1198  *ROUTE FLOW through O'Keefe Drain 1
1199  ROUTE CHANNEL  N H Y D o u t=[ " D R A I N 1 " ] ,  N H Y D i n=[ " F F " ] ,  R D T=[ 1] ( m i n ) ,
1200      C H L G T H=[ 302] { m } ,  C H S L O P E=[ 1. 00] ( % ) ,  F P S L O P E=[ 1. 00] ( % ) ,
1201      S E C N U M=[ 1] ,  N S E G=[ 3]
1202      ( S E G R O U G H ,  S E G D I S T ( m ) )=[ 0. 07 , 13. 45 - 0. 043 , 16. 55 0. 07 , 30. 00] N S E G
      t i m e s
1203      ( D I S T A N C E ( m ) ,  E L E V A T I O N ( m ) )=[ 0. 00 , 1. 70]
1204      ( 3. 45 , 0. 60)
1205      ( 13. 45 , 0. 50)
1206      ( 14. 45 , 0. 00)
1207      ( 15. 55 , 0. 00)
1208      ( 16. 55 , 0. 50)
1209      ( 26. 55 , 0. 60)
1210      ( 30. 00 , 1. 70)
1211  *%-----|-----|
1212  CONTINUOUS NASHYD  N H Y D=[ " D I " ] ,  D T=[ 1] m i n ,  A R E A=[ 1. 17] ( h a ) ,
1213      D W F=[ 0] ( c m s ) ,  C N V C=[ 84] ,  I A=[ 9. 0] ( m m ) ,  N=[ 3] ,  T P=[ 0. 28] h r s ,
1214      C o n t i n u o u s  s i m u l a t i o n  p a r a m e t e r s :
1215      I a R E C p e r=[ 4] ( h r s ) ,
1216      S M N=[ - 1] ( m m ) ,  S M A X=[ - 1] ( m m ) ,  S K=[ 0. 010] / ( m m ) ,
1217      I n t e r E v e n t T i m e=[ 12] ( h r s )
1218      B a s e f l o w  s i m u l a t i o n  p a r a m e t e r s :
1219      B a s e F l o w O p t i o n=[ 1] ,
1220      I n i t G W R e s V o l=[ 50] ( m m ) ,  G W R e s K=[ 0. 96] ( m m / d a y / m m )
1221      V H y d C o n d=[ 0. 055] ( m m / h r ) ,  E N D=- 1
1222  *%-----|-----|
1223  CONTINUOUS STANDHYD  N H Y D=[ " A I " ] ,  D T=[ 1] m i n ,  A R E A=[ 2. 50] ( h a ) ,  X I M P=[ 0. 68] ,  T I M P=[ 0. 85] ,
1224      D W F=[ 0] ( c m s ) ,  L O S S=[ 1] :
      H o r t o n :  F o=[ 76. 20] ( m m / h r ) ,  F c=[ 13. 20] ( m m / h r ) ,  D C A Y=[ 4. 14] ( / h r ) ,
1225      F=[ 0. 00] ( m m ) ,
      P e r v i o u s  a r e a s :  I A p e r=[ 4. 67] ( m m ) ,  S L P P=[ 0. 5] ( % ) ,  L G P=[ 50] ( m ) ,
1226      M N P=[ 0. 250] ,  S C P=[ 0] ( m i n ) ,
      I m p e r v i o u s  a r e a s :  I A i m p=[ 1. 57] ( m m ) ,  S L P I=[ 0. 5] ( % ) ,
1227      L G I=[ 223. 607] ( m ) ,  M N I=[ 0. 013] ,  S C I=[ 0] ( m i n ) ,
1228      C o n t i n u o u s  s i m u l a t i o n  p a r a m e t e r s :
      I a R E C p e r=[ 4] ( h r s ) ,  I a R E C i m p=[ 4] ( h r s ) ,  I n t e r E v e n t T i m e=[ 12] ( h r s ) ,
      E N D=- 1

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1229 *%-----|-----|
1230 ROUTE RESERVOIR NHYDout=["A1-STR"], NHYDin=["A1"], RDT=[1](min),
1231 TABLE of ( OUTFLOW STORAGE ) values
1232 (cms) - (ha-m)
1233 [ 0.000 , 0.000 ]
1234 [ 0.035 , 0.038 ]
1235 [ 0.072 , 0.051 ]
1236 [ 0.100 , 0.059 ]
1237 [ 0.125 , 0.070 ]
1238 [ 0.160 , 0.074 ]
1239 [ 0.185 , 0.081 ]
1240 [ -1 , -1 ] (max twenty pts)
1241 NHYDovf=["A1-OVF"]
1242 *%-----|-----|
1243 CONTINUOUS STANDHYD NHYD=["ST-2"], DT=[1]min, AREA=[0.59](ha), XI MP=[0.46],
1244 TI MP=[0.57], DWF=[0](cms), LOSS=[1]:
1245 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1246 F=[0.00](mm),
1247 Pervious areas: I A per=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1248 MNP=[0.250], SCP=[0](min),
1249 Impervious areas: I A i mp=[1.57](mm), SLPI=[0.5](%),
1250 LGI=[108.628](m), MNI=[0.013], SCI=[0](min),
1251 Continuous simulation parameters:
1252 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
1253 END=-1
1254 *%-----|-----|
1255 ROUTE RESERVOIR NHYDout=["ST2STR"], NHYDin=["ST-2"], RDT=[1](min),
1256 TABLE of ( OUTFLOW STORAGE ) values
1257 (cms) - (ha-m)
1258 [ 0.000 , 0.0000 ]
1259 [ 0.052 , 0.0010 ]
1260 [ 0.053 , 0.0080 ]
1261 [ -1 , -1 ] (max twenty pts)
1262 NHYDovf=["ST2OVF"]
1263 *%-----|-----|
1264 *%-----|-----|
1265 *TOTAL FLOW NORTH OF STRANDHERD DR. (EAST BRANCH) CROSSING
1266 *%-----|-----|
1267 CONTINUOUS NASHYD NHYD=["O-8"], DT=[1]min, AREA=[60.55](ha),
1268 DWF=[0](cms), CNVC=[69], IA=[4.0](mm), N=[3], TP=[1.0]hrs,
1269 Continuous simulation parameters:
1270 I a REC per=[4](hrs),
1271 SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1272 I n t e r E v e n t T i m e=[12](hrs)
1273 Baseflow simulation parameters:
1274 BaseFlowOption=[1],
1275 I n i t G W R e s V o l=[50](mm), G W R e s K=[0.96](mm/day/mm)
1276 VHydCond=[0.055](mm/hr), END=-1
1277 *%-----|-----|
1278 ROUTE PIPE PTYPE=[2]rect, NHYDout=["O8PIPE"], RNUMBER=[1], PWDTH=[1800](mm),
1279 PHEIGHT=[1200](mm), PLNGTH=[335.1](m),
1280 PROUGH=[0.013], PSLOPE=[0.001](m/m), NHYDin=["O-8"], RDT=[1](min)
1281 *%-----|-----|
1282 *%-----|-----|
1283 ADD HYD NHYDsum=["ST2-IN"], NHYDsto
1284 add=["DRAIN1"+"D1"+"A1-STR"+"A1-OVF"+"ST2STR"+"ST2OVF"+"O8PIPE"]
1285 *%-----|-----|
1286 CONTINUOUS STANDHYD NHYD=["A7"], DT=[1]min, AREA=[3.51](ha), XI MP=[0.68], TI MP=[0.85],
1287 DWF=[0](cms), LOSS=[1]:
1288 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
1289 F=[0.00](mm),
1290 Pervious areas: I A per=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
1291 MNP=[0.250], SCP=[0](min),
1292 Impervious areas: I A i mp=[1.57](mm), SLPI=[0.5](%),
1293 LGI=[264.953](m), MNI=[0.013], SCI=[0](min),
1294 Continuous simulation parameters:

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1284 IaRECPper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
END=- 1
1285 *%-----|-----|
1286 ROUTE RESERVOIR NHYDout=["A7-STR"], NHYDin=["A7"], RDT=[ 1](min),
1287 TABLE of ( OUTFLOW STORAGE ) values
1288 (cms) - (ha-m)
1289 [ 0.000 , 0.000 ]
1290 [ 0.049 , 0.054 ]
1291 [ 0.102 , 0.072 ]
1292 [ 0.140 , 0.082 ]
1293 [ 0.175 , 0.099 ]
1294 [ 0.225 , 0.105 ]
1295 [ 0.260 , 0.114 ]
1296 [ -1 , -1 ] (max twenty pts)
1297 NHYDovf=["A7-OVF"]
1298 *%-----|-----|
1299 CONTINUOUS STANDHYD NHYD=["ST-3"], DT=[ 1]min, AREA=[ 0.71](ha), XI MP=[ 0.46],
TIMP=[ 0.57], DWF=[ 0](cms), LOSS=[ 1]:
1300 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
F=[ 0.00](mm),
1301 Pervious areas: IAper=[ 4.67](mm), SLPP=[ 0.5](%), LGP=[ 50](m),
MNP=[ 0.250], SCP=[ 0](min),
1302 Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 0.5](%),
LGI=[ 119.164](m), MNI=[ 0.013], SCI=[ 0](min),
1303 Continuous simulation parameters:
1304 IaRECPper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
END=- 1
1305 *%-----|-----|
1306 ROUTE RESERVOIR NHYDout=["ST3STR"], NHYDin=["ST-3"], RDT=[ 1](min),
1307 TABLE of ( OUTFLOW STORAGE ) values
1308 (cms) - (ha-m)
1309 [ 0.000 , 0.0000 ]
1310 [ 0.063 , 0.0010 ]
1311 [ 0.064 , 0.0094 ]
1312 [ -1 , -1 ] (max twenty pts)
1313 NHYDovf=["ST3OVF"]
1314 *%-----|-----|
1315 *ANALYSIS POINT 2 - TOTAL FLOW AT OUTLET OF STREET 2/3 INTERSECTION
1316 *%-----|-----|
1317 ADD HYD NHYDsum=["PT2ST3"], NHYDsto
add=["ST2-IN"+"A7-STR"+"A7-OVF"+"ST3STR"+"ST3OVF"]
1318 *%-----|-----|
1319 *ROUTE FLOW through O Keefe Drain 2
1320 ROUTE CHANNEL NHYDout=["DRAIN2"], NHYDin=["PT2ST3"], RDT=[ 1](min),
1321 CHLGTH=[ 592](m), CHSLOPE=[.23](%), FPSLOPE=[.23](%),
1322 SECNUM=[ 1], NSEG=[ 3]
1323 ( SEGROUGH, SEGDIST (m))=[ 0.07, 12.60 -0.043, 17.40 0.07, 30.00] NSEG
times
1324 ( DISTANCE (m), ELEVATION (m))=[ 0.00, 1.70]
1325 ( 2.60, 0.95)
1326 ( 12.60, 0.75)
1327 ( 14.10, 0.00)
1328 ( 15.90, 0.00)
1329 ( 17.40, 0.75)
1330 ( 27.40, 0.95)
1331 ( 30.00, 1.70)
1332 *%-----|-----|
1333 CONTINUOUS NASHYD NHYD=["D2"], DT=[ 1]min, AREA=[ 2.28](ha), DWF=[ 0](cms), CNVC=[ 84],
IA=[ 9.0](mm),
1334 N=[ 3], TP=[ 0.99]hrs,
1335 Continuous simulation parameters:
1336 IaRECPper=[ 4](hrs),
1337 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1338 InterEventTime=[ 12](hrs)
1339 Baseflow simulation parameters:
1340 BaseFlowOption=[ 1],

```



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1341      In i t GWRes Vol =[ 50] ( mm) , GWRes K=[ 0. 96] ( mm/ day/ mm)
1342      VHydCond=[ 0. 055] ( mm/ hr) ,      END=- 1
1343 *%-----|-----|
1344 CONTI NUOUS STANDHYD NHYD=[ " A17" ] , DT=[ 1] mi n , AREA=[ 12. 04] ( ha) , XI MP=[ 0. 68] ,
TI MP=[ 0. 85] , DWF=[ 0] ( cms) , LOSS=[ 1] :
1345      Hort on: Fo=[ 76. 20] ( mm/ hr) , Fc=[ 13. 20] ( mm/ hr) , DCAY=[ 4. 14] (/ hr) ,
F=[ 0. 00] ( mm) ,
1346      Per vious areas: I Aper =[ 4. 67] ( mm) , SLPP=[ 0. 5] ( % ) , LGP=[ 50] ( m) ,
MNP=[ 0. 250] , SCP=[ 0] ( mi n) ,
1347      Impervious areas: I Ai mp=[ 1. 57] ( mm) , SLPI =[ 0. 5] ( % ) ,
LGI =[ 490. 714] ( m) , MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
1348      Conti nuous si mul ati on par ameters:
1349      IaRECper=[ 4] ( hrs) , IaRECI mp=[ 4] ( hrs) , Int er Event Ti me=[ 12] ( hrs) ,
END=- 1
1350 *%-----|-----|
1351 ROUTE RESERVOI R      NHYDout =[ " A17STR" ] , NHYDi n=[ " A17" ] , RDT=[ 1] ( mi n) ,
1352      TABLE of ( OUTFLOW STORAGE ) values
1353      ( cms) - ( ha- m)
1354      [ 0. 000 , 0. 000 ]
1355      [ 0. 169 , 0. 185 ]
1356      [ 0. 349 , 0. 248 ]
1357      [ 0. 482 , 0. 283 ]
1358      [ 0. 602 , 0. 338 ]
1359      [ 0. 771 , 0. 359 ]
1360      [ 0. 891 , 0. 391 ]
1361      [ - 1 , - 1 ] ( max t went y pts)
1362      NHYDovf=[ " A17OVF" ]
1363 *%-----|-----|
1364 CONTI NUOUS STANDHYD NHYD=[ " ST- 4" ] , DT=[ 1] mi n , AREA=[ 0. 35] ( ha) , XI MP=[ 0. 46] ,
TI MP=[ 0. 57] , DWF=[ 0] ( cms) , LOSS=[ 1] :
1365      Hort on: Fo=[ 76. 20] ( mm/ hr) , Fc=[ 13. 20] ( mm/ hr) , DCAY=[ 4. 14] (/ hr) ,
F=[ 0. 00] ( mm) ,
1366      Per vious areas: I Aper =[ 4. 67] ( mm) , SLPP=[ 0. 5] ( % ) , LGP=[ 50] ( m) ,
MNP=[ 0. 250] , SCP=[ 0] ( mi n) ,
1367      Impervious areas: I Ai mp=[ 1. 57] ( mm) , SLPI =[ 0. 5] ( % ) , LGI =[ 83. 666] ( m) ,
MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
1368      Conti nuous si mul ati on par ameters:
1369      IaRECper=[ 4] ( hrs) , IaRECI mp=[ 4] ( hrs) , Int er Event Ti me=[ 12] ( hrs) ,
END=- 1
1370 *%-----|-----|
1371 ROUTE RESERVOI R      NHYDout =[ " ST4STR" ] , NHYDi n=[ " ST- 4" ] , RDT=[ 1] ( mi n) ,
1372      TABLE of ( OUTFLOW STORAGE ) values
1373      ( cms) - ( ha- m)
1374      [ 0. 000 , 0. 0000 ]
1375      [ 0. 031 , 0. 0010 ]
1376      [ 0. 032 , 0. 0050 ]
1377      [ - 1 , - 1 ] ( max t went y pts)
1378      NHYDovf=[ " ST4OVF" ]
1379 *%-----|-----|
1380 CONTI NUOUS STANDHYD NHYD=[ " A18" ] , DT=[ 1] mi n , AREA=[ 5. 30] ( ha) , XI MP=[ 0. 68] , TI MP=[ 0. 85] ,
DWF=[ 0] ( cms) , LOSS=[ 1] :
1381      Hort on: Fo=[ 76. 20] ( mm/ hr) , Fc=[ 13. 20] ( mm/ hr) , DCAY=[ 4. 14] (/ hr) ,
F=[ 0. 00] ( mm) ,
1382      Per vious areas: I Aper =[ 4. 67] ( mm) , SLPP=[ 0. 5] ( % ) , LGP=[ 50] ( m) ,
MNP=[ 0. 250] , SCP=[ 0] ( mi n) ,
1383      Impervious areas: I Ai mp=[ 1. 57] ( mm) , SLPI =[ 0. 5] ( % ) ,
LGI =[ 325. 576] ( m) , MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
1384      Conti nuous si mul ati on par ameters:
1385      IaRECper=[ 4] ( hrs) , IaRECI mp=[ 4] ( hrs) , Int er Event Ti me=[ 12] ( hrs) ,
END=- 1
1386 *%-----|-----|
1387 ROUTE RESERVOI R      NHYDout =[ " A18STR" ] , NHYDi n=[ " A18" ] , RDT=[ 1] ( mi n) ,
1388      TABLE of ( OUTFLOW STORAGE ) values
1389      ( cms) - ( ha- m)
1390      [ 0. 000 , 0. 000 ]
1391      [ 0. 074 , 0. 082 ]

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1392         [ 0.154 , 0.109 ]
1393         [ 0.212 , 0.125 ]
1394         [ 0.265 , 0.149 ]
1395         [ 0.339 , 0.158 ]
1396         [ 0.392 , 0.172 ]
1397         [ -1 , -1 ] (max twenty pts)
1398         NHYDovf=[ "A18OVF" ]
1399 *%-----|-----|
1400 *ANALYSIS POINT 3 - TOTAL FLOW AT OUTLET OF STREET 4
1401 *%-----|-----|
1402 ADD HYD          NHYDs um=[ "PT3ST4" ], NHYDs to
add=[ "DRAIN2"+"D2"+"A17STR"+"A17OVF"+"ST4STR"+"ST4OVF"+"A18STR"+"A18OVF" ]
1403 *%-----|-----|
1404 *ROUTE FLOW through O Keefe Drain 3
1405 ROUTE CHANNEL   NHYDout=[ "DRAIN3" ], NHYDin=[ "PT3ST4" ], RDT=[ 1 ] (min),
1406                CHLGTH=[ 525 ] (m), CHSLOPE=[ .23 ] (%), FPSLOPE=[ .23 ] (%),
1407                SECNUM=[ 1 ], NSEG=[ 3 ]
1408                ( SEGROUGH, SEGDIST (m) )=[ 0.07, 12.50 -0.043, 17.50 0.07, 30.00 ] NSEG
times
1409                ( DISTANCE (m), ELEVATION (m) )=[ 0.00, 1.70 ]
1410                ( 2.50, 1.00 )
1411                ( 12.50, 0.80 )
1412                ( 14.10, 0.00 )
1413                ( 15.90, 0.00 )
1414                ( 17.50, 0.80 )
1415                ( 27.50, 1.00 )
1416                ( 30.00, 1.70 )
1417 *%-----|-----|
1418 CONTINUOUS NASHYD NHYD=[ "D3" ], DT=[ 1 ] min, AREA=[ 2.51 ] (ha),
1419                DWF=[ 0 ] (cms), CNVC=[ 86 ], IA=[ 8.7 ] (mm), N=[ 3 ], TP=[ 0.73 ] hrs,
1420                Continuous simulation parameters:
1421                IaRECper=[ 4 ] (hrs),
1422                SMN=[ -1 ] (mm), SMAX=[ -1 ] (mm), SK=[ 0.010 ] / (mm),
1423                InterEventTime=[ 12 ] (hrs)
1424                Baseflow simulation parameters:
1425                BaseFlowOption=[ 1 ],
1426                InitGWResVol=[ 50 ] (mm), GWResK=[ 0.96 ] (mm/day/mm)
1427                VHydCond=[ 0.055 ] (mm/hr), END=- 1
1428 *%-----|-----|
1429 CONTINUOUS STANDHYD NHYD=[ "C1" ], DT=[ 1 ] min, AREA=[ 3.41 ] (ha), XI MP=[ 0.68 ], TI MP=[ 0.85 ],
DWF=[ 0 ] (cms), LOSS=[ 1 ]:
1430                Horton: Fo=[ 76.20 ] (mm/hr), Fc=[ 13.20 ] (mm/hr), DCAY=[ 4.14 ] (/hr),
1431                F=[ 0.00 ] (mm),
1432                Pervious areas: IAper=[ 4.67 ] (mm), SLPP=[ 0.5 ] (%), LGP=[ 50 ] (m),
1433                MNP=[ 0.250 ], SCP=[ 0 ] (min),
1434                Impervious areas: IAimp=[ 1.57 ] (mm), SLPI=[ 0.5 ] (%),
1435                LGL=[ 261.151 ] (m), MNI=[ 0.013 ], SCI=[ 0 ] (min),
1436                Continuous simulation parameters:
1437                IaRECper=[ 4 ] (hrs), IaRECimp=[ 4 ] (hrs), InterEventTime=[ 12 ] (hrs),
1438                END=- 1
1439 *%-----|-----|
1440 ROUTE RESERVOIR NHYDout=[ "C1-STR" ], NHYDin=[ "C1" ], RDT=[ 1 ] (min),
1441                TABLE of ( OUTFLOW STORAGE ) values
1442                ( cms ) - ( ha-m )
1443                [ 0.000 , 0.000 ]
1444                [ 0.048 , 0.052 ]
1445                [ 0.099 , 0.070 ]
1446                [ 0.136 , 0.080 ]
1447                [ 0.170 , 0.096 ]
1448                [ 0.218 , 0.102 ]
1449                [ 0.252 , 0.111 ]
1450                [ -1 , -1 ] (max twenty pts)
1451                NHYDovf=[ "C1-OVF" ]
1452 *%-----|-----|
1453 CONTINUOUS STANDHYD NHYD=[ "ST-5" ], DT=[ 1 ] min, AREA=[ 0.45 ] (ha), XI MP=[ 0.46 ],
1454                TI MP=[ 0.57 ], DWF=[ 0 ] (cms), LOSS=[ 1 ]:

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1450      Horton: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14](/ hr),
1451      F=[ 0.00](mm),
1452      Pervious areas: IAper=[ 4.67](mm), SLPP=[ 0.5](%), LGP=[ 50](m),
1453      MNP=[ 0.250], SCP=[ 0](min),
1454      Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 0.5](%), LGI=[ 94.868](m),
1455      MNI=[ 0.013], SCI=[ 0](min),
1456      Continuous simulation parameters:
1457      IARECper=[ 4](hrs), IARECimp=[ 4](hrs), InterEventTime=[ 12](hrs),
1458      END=- 1
1459  *%-----|-----|
1460  ROUTE RESERVOIR      NHYDout=[ "ST5STR"], NHYDin=[ "ST-5"], RDT=[ 1](min),
1461      TABLE of ( OUTFLOW STORAGE ) values
1462      (cms) - (ha-m)
1463      [ 0.000 , 0.0000 ]
1464      [ 0.040 , 0.0010 ]
1465      [ 0.041 , 0.0062 ]
1466      [ -1 , -1 ] (max twenty pts)
1467      NHYDovf=[ "ST5OVF"]
1468  *%-----|-----|
1469  ADD HYD              NHYDsum=[ "ST5-E"], NHYDsto
1470  add=[ "DRAIN3"+"D3"+"C1-STR"+"C1-OVF"+"ST5STR"+"ST5OVF"]
1471  *%-----|-----|
1472  CONTINUOUS STANDHYD NHYD=[ "STRAND"], DT=[ 1](min), AREA=[ 7.59](ha),
1473  XI MP=[ 0.64], TI MP=[ 0.85], DWF=[ 0](cms), LOSS=[ 1]:
1474  Horton: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14](/ hr),
1475  F=[ 0.00](mm),
1476  Pervious areas: IAper=[ 4.67](mm), SLPP=[ 0.5](%), LGP=[ 40](m),
1477  MNP=[ 0.250], SCP=[ 0](min),
1478  Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 0.5](%), LGI=[ 1230](m),
1479  MNI=[ 0.013], SCI=[ 0](min),
1480  Continuous simulation parameters:
1481  IARECper=[ 4](hrs), IARECimp=[ 4](hrs), InterEventTime=[ 12](hrs),
1482  END=- 1
1483  *%-----|-----|
1484  ROUTE RESERVOIR      NHYDout=[ "S-POND"], NHYDin=[ "STRAND"], RDT=[ 1](min),
1485      TABLE of ( OUTFLOW STORAGE ) values
1486      (cms) - (ha-m)
1487      [ 0.000 , 0.000 ]
1488      [ 0.033 , 0.188 ]
1489      [ 0.057 , 0.253 ]
1490      [ 0.104 , 0.287 ]
1491      [ 0.160 , 0.336 ]
1492      [ 0.340 , 0.346 ]
1493      [ 0.471 , 0.360 ]
1494      [ 0.824 , 0.390 ]
1495      [ -1 , -1 ] (max twenty pts)
1496      NHYDovf=[ "S-OVF"]
1497  *%-----|-----|
1498  ADD HYD              NHYDsum=[ "SSAOUT"], NHYDsto add=[ "ST5-E"+"S-POND"+"S-OVF"]
1499  *%-----|-----|
1500  SAVE HYD             NHYD=[ "SSAOUT"], # OF PCYCLES=[ 5], ICASEsh=[ 1]
1501      HYD_COMMENT=[ "SSAOUT"]
1502  *%-----|-----|
1503  CONTINUOUS STANDHYD NHYD=[ "Area-A"], DT=[ 1]min, AREA=[ 66.75](ha), XI MP=[ 0.64],
1504  TI MP=[ 0.80], DWF=[ 0](cms), LOSS=[ 1]:
1505  Horton: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14](/ hr),
1506  F=[ 0.00](mm),
1507  Pervious areas: IAper=[ 4.67](mm), SLPP=[ 0.5](%), LGP=[ 50](m),
1508  MNP=[ 0.250], SCP=[ 0](min),
1509  Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 0.5](%),
1510  LGI=[ 1155.422](m), MNI=[ 0.013], SCI=[ 0](min),
1511  Continuous simulation parameters:
1512  IARECper=[ 4](hrs), IARECimp=[ 4](hrs), InterEventTime=[ 12](hrs),
1513  END=- 1
1514  *%-----|-----|
1515  SAVE HYD             NHYD=[ "Area-A"], # OF PCYCLES=[ 1], ICASEsh=[ 1]

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1502 HYD_COMMENT=[ " SMMF- A Inflow" ]
1503 *%-----|-----|
1504 ROUTE RESERVOIR NHYDout=[ " SMMF- A" ], NHYDin=[ " Area- A" ], RDT=[ 1 ] (mi n),
1505 TABLE of ( OUTFLOW STORAGE ) values
1506 ( cms ) - ( ha- m)
1507 [ 0.000 , 0.000 ]
1508 [ 0.103 , 1.077 ]
1509 [ 0.128 , 1.749 ]
1510 [ 0.382 , 2.282 ]
1511 [ 0.703 , 2.582 ]
1512 [ 1.256 , 2.978 ]
1513 [ 1.567 , 3.202 ]
1514 [ 1.955 , 3.493 ]
1515 [ 2.100 , 3.600 ]
1516 [ -1 , -1 ] (max twenty pts)
1517 NHYDovf=[ " SWWAOV" ]
1518 *%-----|-----|
1519 SAVE HYD NHYD=[ " SMMF- A" ], # OF PCYCLES=[ 1 ], ICASEsh=[ 1 ]
1520 HYD_COMMENT=[ " SMMF- A Outflow" ]
1521 *%-----|-----|
1522 *ANALYSIS POINT 4 - TOTAL FLOW AT OUTLET OF STREET 5
1523 *%-----|-----|
1524 ADD HYD NHYDs um=[ " PT4ST5" ], NHYDs to add=[ " SSAOUT" + " SMMF- A" + " SWWAOV" ]
1525 *%-----|-----|
1526 CONTINUOUS STANDHYD NHYD=[ " C6" ], DT=[ 1 ] mi n, AREA=[ 1.87 ] (ha), XI MP=[ 0.68 ], TI MP=[ 0.85 ],
DWF=[ 0 ] (cms), LOSS=[ 1 ]:
1527 Horton: Fo=[ 76.20 ] (mm/ hr), Fc=[ 13.20 ] (mm/ hr), DCAY=[ 4.14 ] (/ hr),
F=[ 0.00 ] (mm),
1528 Pervious areas: IAper=[ 4.67 ] (mm), SLPP=[ 0.5 ] (%), LGP=[ 50 ] (m),
MNP=[ 0.250 ], SCP=[ 0 ] (mi n),
1529 Impervious areas: IAimp=[ 1.57 ] (mm), SLPI=[ 0.5 ] (%),
LGI=[ 193.391 ] (m), MNI=[ 0.013 ], SCI=[ 0 ] (mi n),
1530 Continuous simulation parameters:
1531 IARECper=[ 4 ] (hrs), IARECimp=[ 4 ] (hrs), InterEventTime=[ 12 ] (hrs),
END=- 1
1532 *%-----|-----|
1533 ROUTE RESERVOIR NHYDout=[ " C6- STR" ], NHYDin=[ " C6" ], RDT=[ 1 ] (mi n),
1534 TABLE of ( OUTFLOW STORAGE ) values
1535 ( cms ) - ( ha- m)
1536 [ 0.000 , 0.000 ]
1537 [ 0.026 , 0.029 ]
1538 [ 0.054 , 0.038 ]
1539 [ 0.075 , 0.044 ]
1540 [ 0.093 , 0.052 ]
1541 [ 0.120 , 0.056 ]
1542 [ 0.138 , 0.061 ]
1543 [ -1 , -1 ] (max twenty pts)
1544 NHYDovf=[ " C6- OVf" ]
1545 *%-----|-----|
1546 CONTINUOUS STANDHYD NHYD=[ " C7" ], DT=[ 1 ] mi n, AREA=[ 1.62 ] (ha), XI MP=[ 0.68 ], TI MP=[ 0.85 ],
DWF=[ 0 ] (cms), LOSS=[ 1 ]:
1547 Horton: Fo=[ 76.20 ] (mm/ hr), Fc=[ 13.20 ] (mm/ hr), DCAY=[ 4.14 ] (/ hr),
F=[ 0.00 ] (mm),
1548 Pervious areas: IAper=[ 4.67 ] (mm), SLPP=[ 0.5 ] (%), LGP=[ 50 ] (m),
MNP=[ 0.250 ], SCP=[ 0 ] (mi n),
1549 Impervious areas: IAimp=[ 1.57 ] (mm), SLPI=[ 0.5 ] (%),
LGI=[ 180.000 ] (m), MNI=[ 0.013 ], SCI=[ 0 ] (mi n),
1550 Continuous simulation parameters:
1551 IARECper=[ 4 ] (hrs), IARECimp=[ 4 ] (hrs), InterEventTime=[ 12 ] (hrs),
END=- 1
1552 *%-----|-----|
1553 ROUTE RESERVOIR NHYDout=[ " C7- STR" ], NHYDin=[ " C7" ], RDT=[ 1 ] (mi n),
1554 TABLE of ( OUTFLOW STORAGE ) values
1555 ( cms ) - ( ha- m)
1556 [ 0.000 , 0.000 ]
1557 [ 0.023 , 0.025 ]

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1558         [ 0.047 , 0.033 ]
1559         [ 0.065 , 0.038 ]
1560         [ 0.081 , 0.045 ]
1561         [ 0.104 , 0.048 ]
1562         [ 0.120 , 0.053 ]
1563         [ -1 , -1 ] (max twenty pts)
1564         NHYDovf=["C7-OVF"]
1565 *%-----|-----|
1566 CONTINUOUS STANDHYD NHYD=["ST-6"], DT=[1] min, AREA=[0.41](ha), XI MP=[0.46], TI MP=[0.57],
DWF=[0](cms), LOSS=[1]:
1567 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1568 Pervious areas: I A per=[4.67](mm), SLPP=[0.5](%), LGP=[50](m),
MNP=[0.250], SCP=[0](min),
1569 Impervious areas: I A i mp=[1.57](mm), SLPI=[0.5](%), LGI=[90.554](m),
MNI=[0.013], SCI=[0](min),
1570 Continuous simulation parameters:
1571 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=-1
1572 *%-----|-----|
1573 ROUTE RESERVOIR NHYDout=["ST6STR"], NHYDin=["ST-6"], RDT=[1](min),
1574 TABLE of ( OUTFLOW STORAGE ) values
1575 (cms) - (ha-m)
1576 [ 0.000 , 0.0000 ]
1577 [ 0.036 , 0.0010 ]
1578 [ 0.037 , 0.0058 ]
1579 [ -1 , -1 ] (max twenty pts)
1580 NHYDovf=["ST6OVF"]
1581 *%-----|-----|
1582 *ANALYSIS POINT 5 - TOTAL FLOW AT OUTLET OF STREET 6
1583 *%-----|-----|
1584 ADD HYD NHYDsum=["PT5ST6"], NHYDs to
add=["PT4ST5"+"C6-STR"+"C6-OVF"+"C7-STR"+"C7-OVF"+"ST6STR"+"ST6OVF"]
1585 *%-----|-----|
1586 *ROUTE FLOW through O Keefe Drain 4
1587 ROUTE CHANNEL NHYDout=["DRAI N4"], NHYDin=["PT5ST6"], RDT=[1](min),
1588 CHLGTH=[324](m), CHSLOPE=[.10](%), FPSLOPE=[.10](%),
1589 SECNUM=[1], NSEG=[3]
1590 ( SEGROUGH, SEGDI ST (m))=[0.07, 12.00 -0.043, 18.00 0.07, 30.00] NSEG
t i m e s
1591 ( DI STANCE (m), ELEVATI ON (m))=[0.00, 2.00]
1592 (2.00, 1.20)
1593 (12.00, 1.00)
1594 (14.00, 0.00)
1595 (16.00, 0.00)
1596 (18.00, 1.00)
1597 (28.00, 1.20)
1598 (30.00, 2.00)
1599 *%-----|-----|
1600 CONTINUOUS NASHYD NHYD=["D4"], DT=[1] min, AREA=[1.73](ha), DWF=[0](cms), CNV C=[88],
I A=[8.4](mm),
1601 N=[3], TP=[0.60] hrs,
1602 Continuous simulation parameters:
1603 I a REC per=[4](hrs),
1604 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1605 I n t e r E v e n t T i m e=[12](hrs)
1606 Baseflow simulation parameters:
1607 BaseFl owOpt i on=[1] ,
1608 I n i t GWR es Vol=[50](mm), GWR es K=[0.96](mm/day/mm)
1609 VHydCond=[0.055](mm/hr), END=-1
1610 *%-----|-----|
1611 CONTINUOUS STANDHYD NHYD=["Area-B"], DT=[1] min, AREA=[24.04](ha), XI MP=[0.62],
TI MP=[0.77], DWF=[0](cms), LOSS=[1]:
1612 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
1613 Pervious areas: I A per=[4.67](mm), SLPP=[1.4](%), LGP=[50](m),

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1614 MNP=[ 0.250], SCP=[ 0](mi n),
Impervious areas: I A i mp=[ 1.57](mm), SLPI=[ 1.4](%),
LGI=[ 693.397](m), MNI=[ 0.013], SCI=[ 0](mi n),
1615 Continuous simulation parameters:
1616 I a RE C per=[ 4](hrs), I a RE C i mp=[ 4](hrs), I nter Event Ti me=[ 12](hrs),
END=- 1

1617 *%-----|-----|
1618 ROUTE RESERVOIR NHYDout=["SWMF- B"], NHYDi n=["Area- B"], RDT=[ 1](mi n),
1619 TABLE of ( OUTFLOW STORAGE ) values
1620 (cms) - (ha- m)
1621 [ 0.000 , 0.000 ]
1622 [ 0.025 , 0.090 ]
1623 [ 0.175 , 0.510 ]
1624 [ 0.350 , 0.710 ]
1625 [ 0.495 , 0.820 ]
1626 [ 0.648 , 0.980 ]
1627 [ 0.965 , 1.045 ]
1628 [ 1.072 , 1.140 ]
1629 [ -1 , -1 ] (max twenty pts)
1630 NHYDovf=["SWMBOVF"]

1631 *%-----|-----|
1632 ADD HYD NHYDs um=["D4- EX"], NHYDs to add=["DRAI N4"+"D4"+"SWMF- B"+"SWMBOVF"]
1633 *%-----|-----|
1634 *ROUTE FLOW THROUGH O Keefe Drain 5
1635 * JFSA: Nov. 2020, added en points to close X-Section
1636 ROUTE CHANNEL NHYDout=["DRAI N5"], NHYDi n=["D4- EX"], RDT=[ 1](mi n),
1637 CHLGTH=[ 413.0](m), CHSLOPE=[ 0.16](%), FPSLOPE=[ 0.16](%),
1638 SECNUM=[ 1], NSEG=[ 3]
1639 ( SEGROUGH, SEGDI ST (m))=[ 0.043, 12.29 - 0.033, 17.97
1640 0.043, 32.84] NSEG ti mes
1641 ( DI STANCE (m), ELEVATI ON (m))=(- 0.01, 2.50)
1642 [ 0.00, 1.41]
1643 [ 6.13, 0.97]
1644 [ 12.29, 0.89]
1645 [ 15.71, 0.00]
1646 [ 17.97, 0.39]
1647 [ 23.04, 0.35]
1648 [ 32.83, 0.96]
1649 ( 32.84, 2.50)

1650 *%-----|-----|
1651 CONTINUOUS NASHYD NHYD=["D5"], DT=[ 1]mi n, AREA=[ 1.90](ha),
1652 DWF=[ 0](cms), CN/ C=[ 86], I A=[ 8.7](mm), N=[ 3], TP=[ 0.69]hrs,
1653 Continuous simulation parameters:
1654 I a RE C per=[ 4](hrs),
1655 SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1656 I nter Event Ti me=[ 12](hrs)
1657 Baseflow simulation parameters:
1658 BaseFl owOpt ion=[ 1] ,
1659 I n i t GWRes Vol =[ 50](mm), GWRes K=[ 0.96](mm/ day/ mm)
1660 VHydCond=[ 0.055](mm/ hr), END=- 1

1661 *%-----|-----|
1662 *EXTERNAL FLOWS SOUTHEAST OF THE SITE NORTH OF MCKENNA CASEY DR.
1663 CONTINUOUS NASHYD NHYD=["O- 13SDF"], DT=[ 1]mi n, AREA=[ 9.74](ha),
1664 DWF=[ 0](cms), CN/ C=[ 81], I A=[ 4.0](mm), N=[ 3], TP=[ .43]hrs,
1665 Continuous simulation parameters:
1666 I a RE C per=[ 4](hrs),
1667 SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
1668 I nter Event Ti me=[ 12](hrs)
1669 Baseflow simulation parameters:
1670 BaseFl owOpt ion=[ 1] ,
1671 I n i t GWRes Vol =[ 50](mm), GWRes K=[ 0.96](mm/ day/ mm)
1672 VHydCond=[ 0.055](mm/ hr), END=- 1

1673 *%-----|-----|
1674 *SNOW DISPOSAL FACILITY
1675 *PARAMETERS BASED ON ROBINSON 2006 MODEL
1676 ROUTE RESERVOIR NHYDout=["SDF"], NHYDi n=["O- 13SDF"], RDT=[ 1](mi n),

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```

1677          TABLE of ( OUTFLOW STORAGE ) values
1678                ( cms ) - ( ha-m)
1679                [ 0.000, 0.000]
1680                [ 0.150, 0.600]
1681                ( 0.200, 1.500)
1682                [ -1 , -1 ] (max twenty pts)
1683                NHYDovf=[ "OVFSDF" ]
1684 *%-----|-----|
1685 *ANALYSIS POINT 6 - McKenna Casey Dr.
1686 *%-----|-----|
1687 ADD HYD          NHYDs um=[ "PT6MC" ], NHYDs to add=[ "DRAIN5"+"D5"+"SDF" ]
1688 *%-----|-----|
1689 CONTINUOUS NASHYD NHYD=[ "O-15" ], DT=[ 1] min, AREA=[ 10.67] (ha),
1690                DWF=[ 0] (cms), CNVC=[ 82], IA=[ 7.5] (mm), N=[ 3], TP=[ 0.30] hrs,
1691                Continuous simulation parameters:
1692                IARECper=[ 4] (hrs),
1693                SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
1694                InterEventTime=[ 12] (hrs)
1695                Baseflow simulation parameters:
1696                BaseFlowOption=[ 1] ,
1697                InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/day/mm)
1698                VHydCond=[ 0.055] (mm/hr), END=- 1
1699 *%-----|-----|
1700 *TOTAL FLOW NORTH OF MCKENNA CASEY DR.
1701 ADD HYD          NHYDs um=[ "MC" ], NHYDs to add=[ "PT6MC"+"O-15" ]
1702 *%-----|-----|
1703 *ROUTE FLOW THROUGH AREA O-14
1704 * JFSA: Nov. 2020, added end points to close X-section
1705 ROUTE CHANNEL   NHYDout=[ "O-14Ch" ], NHYDin=[ "MC" ], RDT=[ 1] (min),
1706                CHLGH=[ 845.3] (m), CHSLOPE=[ 0.10] (%), FPSLOPE=[ 0.10] (%),
1707                SECNUM=[ 1], NSEG=[ 3]
1708                ( SEGROUGH, SEGDIST (m) )=[ 0.06, 15.00 -0.033, 18.04 0.06, 31.85] NSEG
1709                times
1710                ( DISTANCE (m), ELEVATION (m) )=[ -0.01, 2.5
1711                ( 0.00, 1.53]
1712                ( 5.56, 1.47)
1713                ( 9.21, 1.45)
1714                ( 12.45, 1.53)
1715                ( 13.70, 1.50)
1716                ( 15.00, 0.69)
1717                ( 15.34, 0.00)
1718                ( 16.51, 0.05)
1719                ( 17.30, 0.17)
1720                ( 18.04, 0.74)
1721                ( 19.29, 1.32)
1722                ( 22.73, 1.47)
1723                ( 31.84, 1.41)
1724                ( 31.85, 2.50)
1725 *%-----|-----|
1726 *% -Change O-14 from NASHYD to STANDHYD, name it "S-1-Okeefe" and add it to S-1
1727 subcatchment based on Project 1474-BCDC, JFSA, Nov. 2020
1728 *% -JFSA 2021-02-16, add detailed subcatchment drainage area for each subcatchment
1729 in Corrigan sub-catchment. After adding part of O-14 to S_1 sub-catchment so O-14
1730 becomes 5 ha instead of 30.02 ha and TP becomes 0.133 (5*0.8/30.02) instead of 0.8
1731 CONTINUOUS NASHYD NHYD=[ "O-14" ], DT=[ 1] min, AREA=[ 5] (ha),
1732                DWF=[ 0] (cms), CNVC=[ 82], IA=[ 7.5] (mm), N=[ 3], TP=[ 0.133] hrs,
1733                Continuous simulation parameters:
1734                IARECper=[ 4] (hrs),
1735                SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010] / (mm),
1736                InterEventTime=[ 12] (hrs)
1737                Baseflow simulation parameters:
1738                BaseFlowOption=[ 1] ,
1739                InitGWResVol=[ 50] (mm), GWResK=[ 0.96] (mm/day/mm)
1740                VHydCond=[ 0.055] (mm/hr), END=- 1
1741 *
1742 *%-----|-----|

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1739 *ANALYSIS POINT 7 - JOCK RIVER
1740 * 2020-12-01 To Foster Drain
1741 * 2020-12-01 replace ("PT7JR") by ("OKEEFE")
1742 *%-----|-----
1743 ADD HYD          NHYDs um=["OKEEFE"], NHYDs to add=["O-14Ch"+"O-14"]
1744 *%-----|-----
1745 *CONTINUOUS STANDHYD NHYD=["OKEEFE"], DT=[1](min), AREA=[448](ha),
1746 *          XI MP=[0.65], TI MP=[0.65], DWF=[0](cms), LOSS=[2],
1747 *          SCS curve number CN=[77],
1748 *          Pervious surfaces: I A per=[4.67](mm), SLPP=[0.5](%),
1749 *          LGP=[40](m), MNP=[0.25], SCP=[0](min),
1750 *          Impervious surfaces: I A i mp=[1.57](mm), SLPI=[0.5](%),
1751 *          LGI=[1728](m), MNI=[0.013], SCI=[0](min),
1752 *          Continuous simulation parameters:
1753 *          I a REC per=[4](hrs), I a REC i mp=[4](hrs),
1754 *          SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1755 *          Inter Event Ti me=[18](hrs), END=-1
1756 *#*****
1757 *#      Okeefe Pond
1758 *#      - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
1759 *#      and a ratio of the catchment area to the West Clarke pond rating curve
1760 *#      from the M55 for the next coordinates
1761 *#*****
1762 *ROUTE RESERVOIR  NHYDout=["P_OKE"], NHYDin=["OKEEFE"],
1763 *          RDT=[1](min),
1764 *          TABLE of ( OUTFLOW STORAGE ) values
1765 *          ( cms ) - ( ha-m )
1766 *          [ 0.0 , 0.0 ]
1767 *          [ 14.13 , 13.0 ]
1768 *          [ -1 , -1 ] (maximum one hundred pairs of points)
1769 *          NHYDovf=["ok-OVF"],
1770 *%-----|-----
1771 * -JFSA 2021-02-25 "S-1-D2" and "S-1-D3" are part of S-1 sub-catchment. They are
1772 * moved to drain before station 6215 on Jock River
1773 *CONTINUOUS STANDHYD NHYD=["S-1-D2"], DT=[1](min), AREA=[18.67](ha), XI MP=[0.65],
1774 *          TI MP=[0.65], DWF=[0](cms),
1775 *          LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
1776 *          I A per=[4.67](mm), SLPP=[2.0](%),
1777 *          LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
1778 *          I A i mp=[1.57](mm), SLPI=[0.75](%),
1779 *          LGI=[352.798](m), MNI=[0.013], SCI=[0](min),
1780 *          Continuous simulation parameters:
1781 *          I a REC per=[4](hrs), I a REC i mp=[4](hrs),
1782 *          SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1783 *          Inter Event Ti me=[12](hrs), END=-1
1784 *%-----|-----
1785 *CONTINUOUS NASHYD  NHYD=["S-1-D2"], DT=[1]min, AREA=[18.67](ha),
1786 *          DWF=[0](cms), CN C=[77], I A=[4.67](mm),
1787 *          N=[3], TP=[1.120]hrs,
1788 *          Continuous simulation parameters:
1789 *          I a REC per=[4](hrs),
1790 *          SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
1791 *          Inter Event Ti me=[12](hrs)
1792 *          Baseflow simulation parameters:
1793 *          BaseFl owOpt ion=[1],
1794 *          I ni t GWRes Vol =[50](mm), GWRes K=[0.96](mm/day/mm)
1795 *          VHydCond=[0.055](mm/hr), END=-1
1796 *%-----|-----
1797 *COMPUTE DUALHYD  NHYDin=["S-1-D2"], CI NLET=[2.097](cms), NI NLET=[1],
1798 *          M a j NHYD=["S-1-D2J"]
1799 *          M n NHYD=["S-1-D2N"]
1800 *          TMJ STO=[9999999](cu-m)
1801 *%-----|-----
1802 *ADD HYD          NHYDs um=["S-1-D2S"], NHYDs to add=["S-1-D2J"+"S-1-D2N"]
1803 *%-----|-----

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1800 ROUTE RESERVOIR      NHYDout =[" S- 1- D2R" ] , NHYDin=[" S- 1- D2S" ] ,
1801                      RDT=[ 1 ] (mi n),
1802                      TABLE of ( OUTFLOW STORAGE ) values
1803                          ( cms ) - ( ha- m)
1804                          [ 0. 0      , 0. 0 ]
1805                          [ 0. 2231, 0. 7445 ]
1806                          [   -1   ,  -1   ] (max twenty pts)
1807                      NHYDovf=[" S- 1- D2Rovf" ]
1808 *%-----|-----|
1809 CONTINUOUS STANDHYD NHYD=[" S- 1- D3" ], DT=[ 1 ] (mi n), AREA=[ 6. 79 ] (ha), XI MP=[ 0. 65 ],
TI MP=[ 0. 65 ], DWF=[ 0 ] (cms),
1810 LOSS=[ 2 ], SCS curve number CN=[ 75 ], Pervious surfaces:
1811 IAper=[ 4. 67 ] (mm), SLPP=[ 2. 0 ] ( %),
LGP=[ 40 ] (m), MNP=[ 0. 25 ], SCP=[ 0 ] (mi n), Impervious surfaces:
1812 IAi mp=[ 1. 57 ] (mm), SLPI=[ 0. 75 ] ( %),
1813 LGI=[ 212. 760 ] (m), MNI=[ 0. 013 ], SCI=[ 0 ] (mi n),
1814 Continuous simulation parameters:
1815 IaREcper=[ 4 ] (hrs), IaRECi mp=[ 4 ] (hrs),
1816 SM N=[ -1 ] (mm), SMAX=[ -1 ] (mm), SK=[ 0. 010 ] / (mm),
1817 InterEvent Time=[ 12 ] (hrs), END=- 1
1818 *%-----|-----|
1819 *CONTINUOUS NASHYD  NHYD=[" S- 1- D3" ], DT=[ 1 ] mi n, AREA=[ 6. 79 ] (ha),
1820 * DWF=[ 0 ] (cms), CN C=[ 77 ], IA=[ 4. 67 ] (mm),
1821 * N=[ 3 ], TP=[ 1. 281 ] hrs,
1822 * Continuous simulation parameters:
1823 * IaREcper=[ 4 ] (hrs),
1824 * SM N=[ -1 ] (mm), SMAX=[ -1 ] (mm), SK=[ 0. 010 ] / (mm),
1825 * InterEvent Time=[ 12 ] (hrs)
1826 * Baseflow simulation parameters:
1827 * BaseFl owOpt ion=[ 1 ] ,
1828 * Ini t GWRes Vol =[ 50 ] (mm), GWRes K=[ 0. 96 ] (mm/ day/ mm)
1829 * VHydCond=[ 0. 055 ] (mm/ hr), END=- 1
1830 *%-----|-----|
1831 COMPUTE DUALHYD      NHYDin=[" S- 1- D3" ], CI NLET=[ 0. 831 ] (cms), NI NLET=[ 1 ],
1832 MAj NHYD=[" S- 1- D3J" ]
1833 M nNHYD=[" S- 1- D3N" ]
1834 TMI STO=[ 9999999 ] (cu- m)
1835 *%-----|-----|
1836 ADD HYD              NHYDsum=[" S- 1- D3S" ], NHYDs to add=[" S- 1- D3J "+" S- 1- D3N" ]
1837 *%-----|-----|
1838 ROUTE RESERVOIR      NHYDout =[" S- 1- D3R" ] , NHYDin=[" S- 1- D3S" ] ,
1839                      RDT=[ 1 ] (mi n),
1840                      TABLE of ( OUTFLOW STORAGE ) values
1841                          ( cms ) - ( ha- m)
1842                          [ 0. 0      , 0. 0 ]
1843                          [ 0. 0811, 0. 2708 ]
1844                          [   -1   ,  -1   ] (max twenty pts)
1845                      NHYDovf=[" S- 1- D3Rovf" ]
1846 *%-----|-----|
1847 ADD HYD              NHYDsum=[" SN_ OK" ], NHYDs to
add=[" "_N_ OK" +" OKEEFE" +" S- 1- D2R" +" S- 1- D3R" +" S- 1- D2Rovf" +" S- 1- D3Rovf" ]
1848 *%-----|-----|
1849 SAVE HYD             NHYD=[" SN_ OK" ], # OF PCYCLES=[ -1 ], I CASEsh=[ 1 ]
1850 HYD_ COMMENT=[" Total Fl ows at Okeefe Dr ai n" ]
1851 *%-----|-----|
1852 *#
1853 *# Hydrograph from Node Okeefe routed to Node at Foster Drain
1854 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6215
1855 *#
1856 ROUTE CHANNEL        NHYDout =[" N_ FO" ] , NHYDin=[" SN_ OK" ] ,
1857                      RDT=[ 1 ] (mi n),
1858                      CHLGTH=[ 1183 ] (m), CHSLOPE=[ 0. 0761 ] ( %),
1859                      FPSLOPE=[ 0. 0761 ] ( %),
1860                      SECNUM=[ 1. 0 ], NSEG=[ 3 ]
( SEGROUGH, SEGDI ST (m) ) =
1861                      [ 0. 050, -33. 89

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1862         - 0.035, 31.59
1863         0.050, 34.41] NSEG times
1864         ( DISTANCE (m), ELEVATION (m))=
1865         [- 794.18, 91.00]
1866         [- 775.41, 91.50]
1867         [- 702.63, 91.50]
1868         [- 546.19, 91.50]
1869         [- 529.54, 91.50]
1870         [- 323.44, 91.00]
1871         [- 320.71, 91.00]
1872         [- 183.59, 91.00]
1873         [- 182.54, 90.50]
1874         [- 181.36, 90.00]
1875         [- 177.37, 90.00]
1876         [- 87.70, 90.00]
1877         [- 33.89, 90.00]
1878         [- 18.52, 86.88]
1879         [0.00, 85.20]
1880         [16.20, 86.83]
1881         [31.59, 90.00]
1882         [33.03, 90.50]
1883         [34.41, 91.00]
1884 *%-----|-----|
1885 *#*****|
1886 *#   Catchment FOSTER
1887 *#   - To Foster ditch (north of the Jock)
1888 *#   - Partially developed (medium density); remaining agricultural
1889 *#   - 2020-12-01 JFSA Foster area is 332 as per Foster SWWF Environmental Study
1890 *#   - 2020-12-01 decrease Foster drainage area from (373 HA) to (307.98 HA) after
1891 *#   - 2021-02-12 update Foster area to 325.44 ha as measured from QGIS
1892 *#*****|
1893 CONTINUOUS STANDHYD NHYD=["FOSTER"], DT=[1] min, AREA=[325.44] (ha),
1894 XI MP=[0.55], TI MP=[0.55], DWF=[0] (cms), LOSS=[2],
1895 SCS curve number CN=[74],
1896 Pervious surfaces: I A per=[4.67] (mm), SLPP=[0.5] (%),
1897 LGP=[40] (m), MNP=[0.25], SCP=[0] (min),
1898 Impervious surfaces: I A i mp=[1.57] (mm), SLPI=[0.5] (%),
1899 LGI=[1472.956] (m), MNI=[0.013], SCI=[0] (min),
1900 Continuous simulation parameters:
1901 I a REC per=[4] (hrs), I a REC i mp=[4] (hrs),
1902 SM N=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
1903 I n t e r E v e n t T i m e=[18] (hrs), E N D=-1
1904 *#*****|
1905 *#   Foster Pond
1906 *#   - Rating curve obtained assuming 40m3/ha in 24 hours for quality control
1907 *#   and a ratio of the catchment area to the West Clarke pond rating curve
1908 *#   from the MS for the next coordinates
1909 *#*****|
1910 ROUTE RESERVOIR NHYDout=["P_FOS"], NHYDin=["FOSTER"],
1911 RDT=[1] (min),
1912 TABLE of ( OUTFLOW STORAGE ) values
1913 ( cms ) - ( ha-m)
1914 [ 0.0 , 0.0 ]
1915 [ 10.34 , 10]
1916 [ -1 , -1 ] (max twenty pts)
1917 NHYDovf=["FO-OVF"]
1918 *%-----|-----|
1919 ADD HYD NHYDsum=["FOSTER-OUT"], NHYDsto add=["P_FOS"+"FO-OVF"]
1920 *%-----|-----|
1921 *#*****|
1922 * -Brazeau area from P 1800-19 =[71.751], change to 63.59 ha based on GIS measurements
1923 * -JFSA, 2021-01-19 update "W_CLAR_BRAZ" to 73.29 ha based on GIS measurements
1924 * -JFSA, 2021-01-22 Brazeau ("MS_P10"+"P10-OVF")brazeau pond discharges directly

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to the jock river through a road side ditch on the west side of Borrisokane road (station 6016)

1925 CONTINUOUS STANDHYD NHYD=["W_CLAR_BRAZ"], DT=[1] min, AREA=[73.29] (ha),
1926 XI MP=[0.6], TI MP=[0.65], DWF=[0] (cms), LOSS=[2],
1927 SCS curve number CN=[77],
1928 Pervious surfaces: I A per=[4.67] (mm), SLPP=[1] (%),
1929 LGP=[40] (m), MNP=[0.25], SCP=[0] (min),
1930 Impervious surfaces: I A i mp=[1.57] (mm), SLPI=[0.5] (%),
1931 LGI=[699.00] (m), MNI=[0.013], SCI=[0] (min),
1932 Continuous simulation parameters:
1933 I a REC per=[4] (hrs), I a REC i mp=[4] (hrs),
1934 SM N=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
1935 Inter Event Time=[18] (hrs), END=-1

*%-----|-----|

* 2020-12-01 correct pond curve values

1938 ROUTE RESERVOIR NHYDout=["MS_P10"], NHYDin=["W_CLAR_BRAZ"],
1939 RDT=[1] (min),

1940 TABLE of (OUTFLOW STORAGE) values
1941 (cms) - (ha - m)
1942 [0.0 , 0.0]
1943 [0.068 , 0.001]
1944 [0.271 , 0.022]
1945 [0.379 , 0.051]
1946 [0.48 , 0.091]
1947 [0.853 , 0.341]
1948 [1.005 , 0.61]
1949 [1.128 , 1.231]
1950 [1.155 , 1.592]
1951 [1.194 , 1.876]
1952 [1.2 , 1.921]
1953 [1.259 , 2.369]
1954 [1.3 , 2.665]
1955 [1.349 , 2.813]
1956 [-1 , -1] (max twenty pts)
1957 NHYDovf=["P10-OVF"]

*%-----|-----|

* -JFSA 2021-02-26 "S-1-FO-D2" is a part of S-1 sub-catchment. It is moved to drain before station 980 on Foster Drain

1960 CONTINUOUS STANDHYD NHYD=["S-1-FO-D2"], DT=[1] min, AREA=[4.94] (ha),
1961 XI MP=[0.55], TI MP=[0.55], DWF=[0] (cms), LOSS=[2],
1962 SCS curve number CN=[74],
1963 Pervious surfaces: I A per=[4.67] (mm), SLPP=[0.5] (%),
1964 LGP=[40] (m), MNP=[0.25], SCP=[0] (min),
1965 Impervious surfaces: I A i mp=[1.57] (mm), SLPI=[0.5] (%),
1966 LGI=[181.475] (m), MNI=[0.013], SCI=[0] (min),
1967 Continuous simulation parameters:
1968 I a REC per=[4] (hrs), I a REC i mp=[4] (hrs),
1969 SM N=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
1970 Inter Event Time=[18] (hrs), END=-1

*%-----|-----|

1972 *CONTINUOUS NASHYD NHYD=["S-1-FO-D2"], DT=[1] min, AREA=[4.94] (ha),
1973 * DWF=[0] (cms), CN/C=[77], I A=[4.67] (mm),
1974 * N=[3], TP=[1.10] hrs,
1975 * Continuous simulation parameters:
1976 * I a REC per=[4] (hrs),
1977 * SM N=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
1978 * Inter Event Time=[12] (hrs)
1979 * Baseflow simulation parameters:
1980 * BaseFlowOption=[1],
1981 * I n i t GWR es Vol =[50] (mm), GWR es K=[0.96] (mm/day/mm)
1982 * VHydCond=[0.055] (mm/hr), END=-1

*%-----|-----|

1984 COMPUTE DUALHYD NHYDin=["S-1-FO-D2"], CI NLET=[0.508] (cms), NI NLET=[1],
1985 M i j NHYD=["S-1-FO-D2J"]
1986 M nNHYD=["S-1-FO-D2N"]
1987 T M I STO=[9999999] (cu-m)

```

1988  *%-----|-----|
1989  ADD HYD      NHYDsum=[ "S- 1- FO- D2S" ], NHYDs to add=[ "S- 1- FO- D2J" +"S- 1- FO- D2N" ]
1990  *%-----|-----|
1991  ROUTE RESERVOIR  NHYDout=[ "S- 1- FO- D2R" ] , NHYDin=[ "S- 1- FO- D2S" ] ,
1992  RDT=[ 1 ] ( mi n ) ,
1993  TABLE of ( OUTFLOW STORAGE ) values
1994  ( cms ) - ( ha- m)
1995  [ 0.0      , 0.0 ]
1996  [ 0.0590, 0.1970 ]
1997  [      -1 , -1      ] (max t went y pts)
1998  NHYDovf=[ "S- 1FOD2ovf" ]
1999  *%-----|-----|
2000  ADD HYD      NHYDsum=[ "980" ], NHYDs to
add=[ "FOSTER- OUT" +"S- 1- FO- D2R" +"S- 1FOD2ovf" ]
2001  *%-----|-----|
2002  SAVE HYD     NHYD=[ "980" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1 ]
2003  HYD_COMMENT=[ "Total Flows at Station 980 on Foster Drain" ]
2004  *%-----|-----|
2005  *#
2006  *# Hydrograph from Node Foster SWM (Station 980) to Node at station 520
2007  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 980
2008  *#
2009  ROUTE CHANNEL  NHYDout=[ "980- out " ] , NHYDin=[ "980" ] ,
2010  RDT=[ 1 ] ( mi n ) ,
2011  CHLGTH=[ 460 ] ( m ) , CHSLOPE=[ 0.04348 ] ( % ) ,
2012  FPSLOPE=[ 0.04348 ] ( % ) ,
2013  SECNUM=[ 1.0 ] , NSEG=[ 3 ]
2014  ( SEGROUGH, SEGDI ST ( m ) ) =
2015  [ 0.050, 45.90
2016  - 0.035, 53.30
2017  0.050, 100 ] NSEG times
2018  ( DI STANCE ( m ) , ELEVATI ON ( m ) ) =
2019  [ 0, 91.75 ]
2020  [ 42.4, 92.18 ]
2021  [ 43.5, 92.16 ]
2022  [ 44.1, 92.1 ]
2023  [ 44.6, 92 ]
2024  [ 44.8, 91.86 ]
2025  [ 45.9, 91.04 ]
2026  [ 46.4, 90.65 ]
2027  [ 46.8, 90.36 ]
2028  [ 47.9, 90.32 ]
2029  [ 48.7, 90.35 ]
2030  [ 50.7, 90.33 ]
2031  [ 52.2, 90.38 ]
2032  [ 52.5, 90.59 ]
2033  [ 53.3, 91.28 ]
2034  [ 54, 91.83 ]
2035  [ 54.3, 92 ]
2036  [ 54.8, 92.08 ]
2037  [ 55.4, 92.12 ]
2038  [ 100, 91.84 ]
2039  *%-----|-----|
2040  * -JFSA 2021-02-26 "S-1-FO-DI" is a part of S-1 sub-catchment. It is moved to drain
before station 520 on Foster Drain
2041  CONTINUOUS STANDHYD  NHYD=[ "S- 1- FO- DI" ], DT=[ 1 ] mi n , AREA=[ 5.11 ] ( ha ) ,
2042  XI MP=[ 0.65 ] , TI MP=[ 0.65 ] , DWF=[ 0 ] ( cms ) , LOSS=[ 2 ] ,
2043  SCS curve number CN=[ 74 ] ,
2044  Pervious surfaces: I A per=[ 4.67 ] ( mm ) , SLPP=[ 0.5 ] ( % ) ,
2045  LGP=[ 40 ] ( m ) , MNP=[ 0.25 ] , SCP=[ 0 ] ( mi n ) ,
2046  Impervious surfaces: I A i mp=[ 1.57 ] ( mm ) , SLPI=[ 0.5 ] ( % ) ,
2047  LGI=[ 184.572 ] ( m ) , MNI=[ 0.013 ] , SCI=[ 0 ] ( mi n ) ,
2048  Continuous simulation parameters:
2049  I a REC per=[ 4 ] ( hr s ) , I a REC i mp=[ 4 ] ( hr s ) ,
2050  SM N=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0.010 ] / ( mm ) ,
2051  Inter Event Ti me=[ 18 ] ( hr s ) , END=- 1

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2052 *%-----|-----|
2053 COMPUTE DUALHYD NHYDin=["S-1-FO-DI"], CINLET=[0.605](cms), NINLET=[1],
2054 MajNHYD=["S-1-FO-DIJ"]
2055 MnNHYD=["S-1-FO-DIN"]
2056 TMSTO=[9999999](cu-m)
2057 *%-----|-----|
2058 ADD HYD NHYDsum=["S-1-FO-DIS"], NHYDs to add=["S-1-FO-DIN"+"S-1-FO-DIJ"]
2059 *%-----|-----|
2060 ROUTE RESERVOIR NHYDout=["S-1-FO-DIR"], NHYDin=["S-1-FO-DIS"],
2061 RDT=[1](min),
2062 TABLE of ( OUTFLOW STORAGE ) values
2063 (cms) - (ha-m)
2064 [ 0.0 , 0.0 ]
2065 [ 0.0611, 0.2038 ]
2066 [ -1 , -1 ] (max twenty pts)
2067 NHYDovf=["S-1FODlovf"]
2068 *%-----|-----|
2069 ADD HYD NHYDsum=["520"], NHYDs to add=["980-out"+"S-1-FO-DIR"+"S-1FODlovf"]
2070 *%-----|-----|
2071 SAVE HYD NHYD=["520"], # OF PCYCLES=[-1], ICASEsh=[1]
2072 HYD_COMMENT=["Total Flows at Sation 520 on Foster Drain"]
2073 *%-----|-----|
2074 *# Hydrograph from Node at Station 520 (Foster Drain) to Node at station 6016 (Jock
River)
2075 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 520
2076 *#
2077 ROUTE CHANNEL NHYDout=["520-out"], NHYDin=["520"],
2078 RDT=[1](min),
2079 CHLGH=[860](m), CHSLOPE=[0.5872](%),
2080 FPSLOPE=[0.5872](%),
2081 SECNUM=[1.0], NSEG=[3]
2082 ( SEGROUGH, SEGDI ST (m))=
2083 [0.050, 45.90
2084 -0.035, 54.3
2085 0.050, 100.1097] NSEG times
2086 ( DI STANCE (m), ELEVATI ON (m))=
2087 [0, 91.26 ]
2088 [44.9, 91.46 ]
2089 [45.1, 91.37 ]
2090 [45.9, 90.84 ]
2091 [47, 90.32 ]
2092 [47.5, 90.22 ]
2093 [48, 90.17 ]
2094 [50.7, 90.19 ]
2095 [51.5, 90.17 ]
2096 [52.2, 90.13 ]
2097 [52.7, 90.12 ]
2098 [53.3, 90.14 ]
2099 [53.5, 90.31 ]
2100 [53.9, 90.59 ]
2101 [54.3, 90.87 ]
2102 [54.7, 91.04 ]
2103 [55.3, 91.24 ]
2104 [55.5, 91.26 ]
2105 [63.7, 91.37 ]
2106 [100.1097, 91.43 ]
2107 *%-----|-----|
2108 * -JFSA 2021-02-26 "S-1-FO-F-D" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2109 CONTINUOUS STANDHYD NHYD=["S-1-FO-F-D"], DT=[1]min, AREA=[14.96](ha),
2110 XI MP=[0.65], TI MP=[0.65], DWF=[0](cms), LOSS=[2],
2111 SCS curve number CN=[74],
2112 Pervious surfaces: I A per=[4.67](mm), SLPP=[0.5](%),
2113 LGP=[40](m), MNP=[0.25], SCP=[0](min),
2114 Imper vious surfaces: I A i mp=[1.57](mm), SLPI=[0.5](%),
2115 LGI=[315.806](m), MNI=[0.013], SCI=[0](min),

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2116 Continuous simulation parameters:
2117 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
2118 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2119 InterEventTime=[ 18](hrs), END=- 1
2120 *%-----|-----|
2121 *CONTINUOUS NASHYD NHYD=["S-1-FO-F-D"], DT=[ 1]min, AREA=[ 14.96](ha),
2122 * DWF=[ 0](cms), CNVC=[ 77], IA=[ 4.67](mm),
2123 * N=[ 3], TP=[ 1.007]hrs,
2124 * Continuous simulation parameters:
2125 * IaRECper=[ 4](hrs),
2126 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2127 * InterEventTime=[ 12](hrs)
2128 * Baseflow simulation parameters:
2129 * BaseFlowOption=[ 1],
2130 * InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
2131 * VHydCond=[ 0.055](mm/hr), END=- 1
2132 *%-----|-----|
2133 COMPUTE DUALHYD NHYDin=["S-1-FO-F-D"], CI NLET=[ 1.615](cms), NI NLET=[ 1],
2134 Maj NHYD=["S-1FO-F-DJ"]
2135 MnNHYD=["S-1FO-F-DN"]
2136 TMI STO=[ 9999999](cu-m)
2137 *%-----|-----|
2138 ADD HYD NHYDsum=["S-1FO-F-DS"], NHYDs to add=["S-1FO-F-DJ"+"S-1FO-F-DN"]
2139 *%-----|-----|
2140 ROUTE RESERVOIR NHYDout=["S-1FO-F-DR"], NHYDin=["S-1FO-F-DS"],
2141 RDT=[ 1](min),
2142 TABLE of ( OUTFLOW STORAGE ) values
2143 (cms) - (ha-m)
2144 [ 0.0 , 0.0 ]
2145 [ 0.1788, 0.5966 ]
2146 [ -1 , -1 ] (max twenty pts)
2147 NHYDovf=["S-1FoFDovf"]
2148 *%-----|-----|
2149 * -JFSA 2021-02-26 "S-1-D8" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2150 CONTINUOUS STANDHYD NHYD=["S-1-D8"], DT=[ 1]min, AREA=[ 5.27](ha), XI MP=[ 0.325],
TI MP=[ 0.65], DWF=[ 0](cms), LOSS=[ 1]:
2151 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
F=[ 0.00](mm),
2152 Previous areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
MNP=[ 0.250], SCP=[ 0](min),
2153 Impervious areas: IAimp=[ 0.785](mm), SLPI=[ 0.75](%),
LGI=[ 187.439](m), MNI=[ 0.013], SCI=[ 0](min),
2154 Continuous simulation parameters:
2155 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
END=- 1
2156 *%-----|-----|
2157 *CONTINUOUS NASHYD NHYD=["S-1-D8"], DT=[ 1]min, AREA=[ 5.27](ha),
2158 * DWF=[ 0](cms), CNVC=[ 77], IA=[ 4.67](mm),
2159 * N=[ 3], TP=[ 1.10]hrs,
2160 * Continuous simulation parameters:
2161 * IaRECper=[ 4](hrs),
2162 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2163 * InterEventTime=[ 12](hrs)
2164 * Baseflow simulation parameters:
2165 * BaseFlowOption=[ 1],
2166 * InitGWResVol=[ 50](mm), GWResK=[ 0.96](mm/day/mm)
2167 * VHydCond=[ 0.055](mm/hr), END=- 1
2168 *%-----|-----|
2169 COMPUTE DUALHYD NHYDin=["S-1-D8"], CI NLET=[ 0.672](cms), NI NLET=[ 1],
2170 Maj NHYD=["S-1-D8J"]
2171 MnNHYD=["S-1-D8N"]
2172 TMI STO=[ 9999999](cu-m)
2173 *%-----|-----|
2174 ADD HYD NHYDsum=["S-1-D8S"], NHYDs to add=["S-1-D8J"+"S-1-D8N"]
2175 *%-----|-----|

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2176 *ADD HYD          NHYDs um=[ "S-1-D" ], NHYDs to add=[ "S-1-Okeefe"+"S-1"+"S-1-Fost" ]
2177 *%-----|-----|
2178 *COMPUTE DUALHYD  NHYDi n=[ "S-1-D" ], CI NLET=[ 11.616 ] (cms), NI NLET=[ 1 ],
2179 *                Maj NHYD=[ "S-1-D-M" ]
2180 *                MnnNHYD=[ "S-1-D-MN" ]
2181 *                TMl STO=[ 5974 ] (cu-m)
2182 *%-----|-----|
2183 *ADD HYD          NHYDs um=[ "S-1-DEV" ], NHYDs to add=[ "S-1-D-M"+"S-1-D-MN" ]
2184 *%-----|-----|
2185 ROUTE RESERVOIR  NHYDout =["S-1-D8R" ] , NHYDi n=["S-1-D8S" ] ,
2186 RDT=[ 1 ] (mi n),
2187                TABLE of ( OUTFLOW STORAGE ) values
2188                ( cms ) - ( ha- m)
2189                [ 0.0      , 0.0 ]
2190                [ 0.0630, 0.2102 ]
2191                [      -1 ,   -1      ] (max twenty pts)
2192                NHYDovf=[ "S-1-D8Rovf" ]
2193 *%-----|-----|
2194 * -JFSA 2021-02-26 "S-1-A" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2195 CONTINUOUS NASHYD NHYD=[ "S-1-A" ], DT=[ 1 ] mi n, AREA=[ 75.88 ] (ha),
2196 DWF=[ 0 ] (cms), CNv C=[ 77 ], I A=[ 4.67 ] (mm),
2197 N=[ 3 ], TP=[ 0.619 ] hr s,
2198 Continuous simulation parameters:
2199 I a RECper=[ 4 ] (hr s),
2200 SM N=[ -1 ] (mm), SMAX=[ -1 ] (mm), SK=[ 0.010 ] / (mm),
2201 InterEvent Time=[ 12 ] (hr s)
2202 Baseflow simulation parameters:
2203 BaseFlowOption=[ 1 ] ,
2204 Ini t GWRes Vol = [ 50 ] (mm), GWRes K=[ 0.96 ] (mm/ day/ mm)
2205 VHydCond=[ 0.055 ] (mm/ hr), END=- 1
2206 *%-----|-----|
2207 * -JFSA, 2021-01-22 "WCLAR_UNDE" (west of Clarke sub-catchment) discharges
directly to the jock river through a road side ditch on the west side of Borrisokane
road (station 6016)
2208 CONTINUOUS NASHYD NHYD=[ "WCLAR_UNDE" ], DT=[ 1 ] mi n, AREA=[ 35.65 ] (ha),
2209 DWF=[ 0 ] (cms), CNv C=[ 77 ], I A=[ 4.67 ] (mm),
2210 N=[ 3 ], TP=[ 1.10 ] hr s,
2211 Continuous simulation parameters:
2212 I a RECper=[ 4 ] (hr s),
2213 SM N=[ -1 ] (mm), SMAX=[ -1 ] (mm), SK=[ 0.010 ] / (mm),
2214 InterEvent Time=[ 12 ] (hr s)
2215 Baseflow simulation parameters:
2216 BaseFlowOption=[ 1 ] ,
2217 Ini t GWRes Vol = [ 50 ] (mm), GWRes K=[ 0.96 ] (mm/ day/ mm)
2218 VHydCond=[ 0.055 ] (mm/ hr), END=- 1
2219 *%-----|-----|
2220 ADD HYD          NHYDs um=[ "SN_FO" ], NHYDs to
add=[ "N_FO"+"520-out"+"MS_P10"+"P10-OVF"+"WCLAR_UNDE"+"S-1FoFDovf"+"S-1FO-F-DR"+"S-1-D8R
ovf"+"S-1-D8R"+"S-1-A" ]
2221 *%-----|-----|
2222 SAVE HYD        NHYD=[ "SN_FO" ], # OF PCYCLES=[ -1 ], I CASEs h=[ 1 ]
2223 HYD_COMMENT=[ "Total Flows at Foster Drain" ]
2224 *%-----|-----|
2225 *# Hydrograph from Node Foster routed to Node at Cedarview Road
2226 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 6016
2227 *#
2228 ROUTE CHANNEL   NHYDout =["NCE" ] , NHYDi n=["SN_FO" ] ,
2229 RDT=[ 1 ] (mi n),
2230 CHLGTH=[ 159 ] (m), CHSLOPE=[ 0.0818 ] ( % ),
2231                FPSLOPE=[ 0.0818 ] ( % ),
2232 SECNUM=[ 1.0 ], NSEG=[ 3 ]
2233 ( SEGROUGH, SEGDI ST (m) )=
2234 [ 0.050, -15.46
2235 -0.035, 26.55
2236 0.050, 116.76 ] NSEG times

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2237 ( DI STANCE ( m), ELEVATI ON ( m)) =
2238 [- 645. 23, 91. 50]
2239 [- 391. 20, 91. 50]
2240 [- 91. 00, 91. 50]
2241 [- 85. 52, 91. 50]
2242 [- 15. 46, 89. 40]
2243 [- 9. 79, 89. 31]
2244 [- 3. 22, 86. 24]
2245 [3. 22, 85. 07]
2246 [10. 96, 85. 79]
2247 [16. 44, 86. 49]
2248 [26. 55, 89. 45]
2249 [29. 03, 90. 27]
2250 [35. 76, 90. 67]
2251 [36. 67, 91. 00]
2252 [108. 08, 91. 00]
2253 [109. 82, 90. 50]
2254 [112. 04, 90. 50]
2255 [114. 62, 91. 00]
2256 [116. 76, 91. 50]
2257 *%-----|-----|
2258 *#*****|
2259 *# Catchment S-1
2260 *# - To Jock River (north and south of Jock)
2261 *# - Primarily agricultural fields; portion of sand quarry
2262 *%-----|-----|
2263 *% -2020-12-17 "S-1-Undev" and "S-1-Fost" was a part of Foster drain, they are below
the foster pond. Now they are added to S-1 subcatchment based on Project 1474-BCDC,
JFSA, Nov. 2020
2264 *% -2020-12-17 Change O-14 (it was part of Okeefe drain) to "S-1-Okeefe" and add it
to S-1 subcatchment based on Project 1474-BCDC, JFSA, Nov. 2020
2265 *% -2020-12-17 Add "S-1-BCDC" as NASHYD
2266 *% -2020-12-17 all other S-1 subcatchment as STANDHYD with DUALHYD and ROUTE RESERVOIR
2267 *%-----|-----|
2268 *#*****|
2269 * -JFSA 2021-02-26 "S-1-A" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2270 *CONTINUOUS NASHYD NHYD=["S-1-A"], DT=[1] min, AREA=[75.88](ha),
2271 * DWF=[0](cms), CNVC=[77], IA=[4.67](mm),
2272 * N=[3], TP=[0.619]hrs,
2273 * Continuous simulation parameters:
2274 * IaRECper=[4](hrs),
2275 * SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2276 * InterEventTime=[12](hrs)
2277 * Baseflow simulation parameters:
2278 * BaseFlowOption=[1],
2279 * InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2280 * VHydCond=[0.055](mm/hr), END=-1
2281 *%-----|-----|
2282 CONTINUOUS NASHYD NHYD=["S-1-B"], DT=[1] min, AREA=[55.36](ha),
2283 DWF=[0](cms), CNVC=[77], IA=[4.67](mm),
2284 N=[3], TP=[0.451]hrs,
2285 Continuous simulation parameters:
2286 IaRECper=[4](hrs),
2287 SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2288 InterEventTime=[12](hrs)
2289 Baseflow simulation parameters:
2290 BaseFlowOption=[1],
2291 InitGWResVol=[50](mm), GWResK=[0.96](mm/day/mm)
2292 VHydCond=[0.055](mm/hr), END=-1
2293 *%-----|-----|
2294 *# - JFSA 2021-02-24 change the name from S-1-BCDC to S-1-A and S-1-B. Change their
TP values based on the new areas compared to the old ones.
2295 *CONTINUOUS NASHYD NHYD=["S-1-BCDC"], DT=[1] min, AREA=[134.9](ha),
2296 * DWF=[0](cms), CNVC=[77], IA=[4.67](mm),
2297 * N=[3], TP=[1.10]hrs,

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2298 * Continuous simulation parameters:
2299 * IaRECper=[ 4]( hrs),
2300 * SMN=[ - 1]( mm), SMAX=[ - 1]( mm), SK=[ 0. 010]/( mm),
2301 * InterEventTime=[ 12]( hrs)
2302 * Baseflow simulation parameters:
2303 * BaseFlowOption=[ 1],
2304 * InitGWResVol=[ 50]( mm), GWResK=[ 0. 96]( mm/ day/ mm)
2305 * VHydCond=[ 0. 055]( mm/ hr), END=- 1
2306 *%-----|-----
2307 *# - JFSA 2021-02-24 "S-1-BCDC-1" and "S-1-BCDC-2" are not existing anymore.
"S-1-BCDC-1" is part of "S-1-FO-D2" and "S-1-BCDC-2" is part of "S-1-D2" and "S-1-D3"
2308 *CONTINUOUS NASHYD NHYD=["S-1-BCDC-1"], DT=[ 1]mi n, AREA=[ 0. 3]( ha),
2309 * DWF=[ 0]( cms), CN C=[ 77], IA=[ 4. 67]( mm),
2310 * N=[ 3], TP=[ 1. 10]hr s,
2311 * Continuous simulation parameters:
2312 * IaRECper=[ 4]( hrs),
2313 * SMN=[ - 1]( mm), SMAX=[ - 1]( mm), SK=[ 0. 010]/( mm),
2314 * InterEventTime=[ 12]( hrs)
2315 * Baseflow simulation parameters:
2316 * BaseFlowOption=[ 1],
2317 * InitGWResVol=[ 50]( mm), GWResK=[ 0. 96]( mm/ day/ mm)
2318 * VHydCond=[ 0. 055]( mm/ hr), END=- 1
2319 *%-----|-----
2320 *CONTINUOUS NASHYD NHYD=["S-1-BCDC-2"], DT=[ 1]mi n, AREA=[ 1. 3]( ha),
2321 * DWF=[ 0]( cms), CN C=[ 77], IA=[ 4. 67]( mm),
2322 * N=[ 3], TP=[ 1. 10]hr s,
2323 * Continuous simulation parameters:
2324 * IaRECper=[ 4]( hrs),
2325 * SMN=[ - 1]( mm), SMAX=[ - 1]( mm), SK=[ 0. 010]/( mm),
2326 * InterEventTime=[ 12]( hrs)
2327 * Baseflow simulation parameters:
2328 * BaseFlowOption=[ 1],
2329 * InitGWResVol=[ 50]( mm), GWResK=[ 0. 96]( mm/ day/ mm)
2330 * VHydCond=[ 0. 055]( mm/ hr), END=- 1
2331 *%-----|-----
2332 *# - JFSA 2021-01-19, after adding Greenbank pond, "S-1-BCDC-3" is not existing
anymore
2333 *CONTINUOUS NASHYD NHYD=["S-1-BCDC-3"], DT=[ 1]mi n, AREA=[ 3. 9]( ha),
2334 * DWF=[ 0]( cms), CN C=[ 77], IA=[ 4. 67]( mm),
2335 * N=[ 3], TP=[ 1. 10]hr s,
2336 * Continuous simulation parameters:
2337 * IaRECper=[ 4]( hrs),
2338 * SMN=[ - 1]( mm), SMAX=[ - 1]( mm), SK=[ 0. 010]/( mm),
2339 * InterEventTime=[ 12]( hrs)
2340 * Baseflow simulation parameters:
2341 * BaseFlowOption=[ 1],
2342 * InitGWResVol=[ 50]( mm), GWResK=[ 0. 96]( mm/ day/ mm)
2343 * VHydCond=[ 0. 055]( mm/ hr), END=- 1
2344 *%-----|-----
2345 * -JFSA 2021-02-25 "S-1-Okeefe" is a part of S-1 sub-catchment. It is moved to drain
before station 7245 on Jock River
2346 *CONTINUOUS STANDHYD NHYD=["S-1-Okeefe"], DT=[ 1]( mi n), AREA=[ 44. 93]( ha), XI MP=[ 0. 65],
TI MP=[ 0. 65], DWF=[ 0]( cms),
2347 * LOSS=[ 2], SCS curve number CN=[ 75], Pervious surfaces:
I Aper=[ 4. 67]( mm), SLPP=[ 2. 0]( %),
2348 * LGP=[ 40]( m), MNP=[ 0. 25], SCP=[ 0]( mi n), Impervious surfaces:
I Ai mp=[ 1. 57]( mm), SLPI=[ 0. 75]( %),
2349 * LGI=[ 547. 296]( m), MNI=[ 0. 013], SCI=[ 0]( mi n),
2350 * Continuous simulation parameters:
2351 * IaRECper=[ 4]( hrs), IaRECI mp=[ 4]( hrs),
2352 * SMN=[ - 1]( mm), SMAX=[ - 1]( mm), SK=[ 0. 010]/( mm),
2353 * InterEventTime=[ 12]( hrs), END=- 1
2354 *%-----|-----
2355 *COMPUTE DUALHYD NHYDin=["S-1-Okeefe"], CI NLET=[ 4. 796]( cms), NI NLET=[ 1],
2356 * Mij NHYD=["S-1-OkM"]
2357 * MnNHYD=["S-1-OkMN"]

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2358 *          TMI STO=[ 9999999 ] ( cu - m)
2359 *%-----|-----
2360 *ADD HYD          NHYDs um=[ " S- 1- OkS" ], NHYDs to add=[ " S- 1- OkM" +" S- 1- OkMN" ]
2361 *%-----|-----
2362 *ROUTE RESERVOIR NHYDout=[ " S- 1- OkSR" ] , NHYDin=[ " S- 1- OkS" ] ,
2363 *          RDT=[ 1 ] ( mi n),
2364 *          TABLE of ( OUTFLOW STORAGE ) values
2365 *                  ( cms ) - ( ha - m)
2366 *                  [ 0.0      , 0.0 ]
2367 *                  [ 0.5370, 1.7917 ]
2368 *                  [   -1   ,  -1   ] (max twenty pts)
2369 *          NHYDovf=[ " S- 1- OkSovf" ]
2370 *%-----|-----
2371 *CONTINUOUS NASHYD NHYD=[ " S- 1- Okeefe" ], DT=[ 1 ] mi n, AREA=[ 44.93 ] ( ha),
2372 *          DWF=[ 0 ] ( cms), CN C=[ 77 ], IA=[ 4.67 ] ( mm),
2373 *          N=[ 3 ], TP=[ 1.049 ] hrs,
2374 *          Continuous simulation parameters:
2375 *          IaRECper=[ 4 ] ( hrs),
2376 *          SMN=[ - 1 ] ( mm), SMAX=[ - 1 ] ( mm), SK=[ 0.010 ] / ( mm),
2377 *          InterEventTime=[ 12 ] ( hrs)
2378 *          Baseflow simulation parameters:
2379 *          BaseFlowOption=[ 1 ] ,
2380 *          InitGWResVol=[ 50 ] ( mm), GWResK=[ 0.96 ] ( mm/ day/ mm)
2381 *          VHydCond=[ 0.055 ] ( mm/ hr), END=- 1
2382 *%-----|-----
2383 * -JFSA 2021-02-26 "S-1-FO-DI" is a part of S-1 sub-catchment. It is moved to drain
before station 520 on Foster Drain
2384 *CONTINUOUS STANDHYD NHYD=[ " S- 1- FO- DI" ], DT=[ 1 ] mi n, AREA=[ 5.11 ] ( ha),
2385 *          XI MP=[ 0.65 ], TI MP=[ 0.65 ], DWF=[ 0 ] ( cms), LOSS=[ 2 ],
2386 *          SCS curve number CN=[ 74 ],
2387 *          Pervious surfaces: IAper=[ 4.67 ] ( mm), SLPP=[ 0.5 ] ( %),
2388 *          LGP=[ 40 ] ( m), MNP=[ 0.25 ], SCP=[ 0 ] ( mi n),
2389 *          Impervious surfaces: IAimp=[ 1.57 ] ( mm), SLPI=[ 0.5 ] ( %),
2390 *          LGI=[ 184.572 ] ( m), MNI=[ 0.013 ], SCI=[ 0 ] ( mi n),
2391 *          Continuous simulation parameters:
2392 *          IaRECper=[ 4 ] ( hrs), IaRECimp=[ 4 ] ( hrs),
2393 *          SMN=[ - 1 ] ( mm), SMAX=[ - 1 ] ( mm), SK=[ 0.010 ] / ( mm),
2394 *          InterEventTime=[ 18 ] ( hrs), END=- 1
2395 *%-----|-----
2396 *COMPUTE DUALHYD NHYDin=[ " S- 1- FO- DI" ], CI NLET=[ 0.605 ] ( cms), NI NLET=[ 1 ],
2397 *          Mi j NHYD=[ " S- 1- FO- DIJ" ]
2398 *          M nNHYD=[ " S- 1- FO- DIN" ]
2399 *          TMI STO=[ 9999999 ] ( cu - m)
2400 *%-----|-----
2401 *ADD HYD          NHYDs um=[ " S- 1- FO- DIS" ], NHYDs to add=[ " S- 1- FO- DIN" +" S- 1- FO- DIJ" ]
2402 *%-----|-----
2403 *ROUTE RESERVOIR NHYDout=[ " S- 1- FO- DIR" ] , NHYDin=[ " S- 1- FO- DIS" ] ,
2404 *          RDT=[ 1 ] ( mi n),
2405 *          TABLE of ( OUTFLOW STORAGE ) values
2406 *                  ( cms ) - ( ha - m)
2407 *                  [ 0.0      , 0.0 ]
2408 *                  [ 0.0611, 0.2038 ]
2409 *                  [   -1   ,  -1   ] (max twenty pts)
2410 *          NHYDovf=[ " S- 1FODlovf" ]
2411 *%-----|-----
2412 *CONTINUOUS NASHYD NHYD=[ " S- 1- FO- DI" ], DT=[ 1 ] mi n, AREA=[ 5.11 ] ( ha),
2413 *          DWF=[ 0 ] ( cms), CN C=[ 77 ], IA=[ 4.67 ] ( mm),
2414 *          N=[ 3 ], TP=[ 1.10 ] hrs,
2415 *          Continuous simulation parameters:
2416 *          IaRECper=[ 4 ] ( hrs),
2417 *          SMN=[ - 1 ] ( mm), SMAX=[ - 1 ] ( mm), SK=[ 0.010 ] / ( mm),
2418 *          InterEventTime=[ 12 ] ( hrs)
2419 *          Baseflow simulation parameters:
2420 *          BaseFlowOption=[ 1 ] ,
2421 *          InitGWResVol=[ 50 ] ( mm), GWResK=[ 0.96 ] ( mm/ day/ mm)
2422 *          VHydCond=[ 0.055 ] ( mm/ hr), END=- 1

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2423 *%-----|-----|
2424 *   -JFSA 2021-02-26 "S-1-FO-D2" is a part of S-1 sub-catchment. It is moved to drain
before station 980 on Foster Drain
2425 *CONTINUOUS STANDHYD NHYD=["S-1-FO-D2"], DT=[1] min, AREA=[4.94](ha),
2426 *   XI MP=[0.55], TI MP=[0.55], DWF=[0](cms), LOSS=[2],
2427 *   SCS curve number CN=[74],
2428 *   Pervious surfaces: I A per=[4.67](mm), SLPP=[0.5](%),
2429 *   LGP=[40](m), MNP=[0.25], SCP=[0](min),
2430 *   Impervious surfaces: I A i mp=[1.57](mm), SLPI=[0.5](%),
2431 *   LGI=[181.475](m), MNI=[0.013], SCI=[0](min),
2432 *   Continuous simulation parameters:
2433 *   I a REC per=[4](hrs), I a REC i mp=[4](hrs),
2434 *   S M N=[-1](mm), S M A X=[-1](mm), S K=[0.010]/(mm),
2435 *   I n t e r E v e n t T i m e=[18](hrs),   E N D=- 1
2436 *%-----|-----|
2437 *CONTINUOUS NASHYD   NHYD=["S-1-FO-D2"], DT=[1] min, AREA=[4.94](ha),
2438 *   DWF=[0](cms), CN C=[77], I A=[4.67](mm),
2439 *   N=[3], TP=[1.10] hrs,
2440 *   Continuous simulation parameters:
2441 *   I a REC per=[4](hrs),
2442 *   S M N=[-1](mm), S M A X=[-1](mm), S K=[0.010]/(mm),
2443 *   I n t e r E v e n t T i m e=[12](hrs)
2444 *   Baseflow simulation parameters:
2445 *   B a s e F l o w O p t i o n=[1] ,
2446 *   I n i t G W R e s V o l=[50](mm), G W R e s K=[0.96](mm/day/mm)
2447 *   V H y d C o n d=[0.055](mm/hr),   E N D=- 1
2448 *%-----|-----|
2449 *COMPUTE DUALHYD    NHYD i n=["S-1-FO-D2"], C I N L E T=[0.508](cms), N I N L E T=[1],
2450 *   M i j N H Y D=["S-1-FO-D2J"]
2451 *   M n N H Y D=["S-1-FO-D2N"]
2452 *   T M I S T O=[9999999](cu-m)
2453 *%-----|-----|
2454 *ADD HYD            NHYD s u m=["S-1-FO-D2S"], NHYD s t o a d d=["S-1-FO-D2J"+"S-1-FO-D2N"]
2455 *%-----|-----|
2456 *ROUTE RESERVOIR   NHYD o u t=["S-1-FO-D2R"], NHYD i n=["S-1-FO-D2S"],
2457 *   R D T=[1](min),
2458 *   TABLE of ( O U T F L O W S T O R A G E ) values
2459 *   (cms) - (ha-m)
2460 *   [ 0.0      , 0.0 ]
2461 *   [ 0.0590, 0.1970 ]
2462 *   [ -1     , -1     ] (max twenty pts)
2463 *   N H Y D o v f=["S-1FOD2ovf"]
2464 *%-----|-----|
2465 *   -JFSA 2021-02-26 "S-1-FO-F-D" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2466 *CONTINUOUS STANDHYD NHYD=["S-1-FO-F-D"], DT=[1] min, AREA=[14.96](ha),
2467 *   XI MP=[0.65], TI MP=[0.65], DWF=[0](cms), LOSS=[2],
2468 *   SCS curve number CN=[74],
2469 *   Pervious surfaces: I A per=[4.67](mm), SLPP=[0.5](%),
2470 *   LGP=[40](m), MNP=[0.25], SCP=[0](min),
2471 *   Impervious surfaces: I A i mp=[1.57](mm), SLPI=[0.5](%),
2472 *   LGI=[315.806](m), MNI=[0.013], SCI=[0](min),
2473 *   Continuous simulation parameters:
2474 *   I a REC per=[4](hrs), I a REC i mp=[4](hrs),
2475 *   S M N=[-1](mm), S M A X=[-1](mm), S K=[0.010]/(mm),
2476 *   I n t e r E v e n t T i m e=[18](hrs),   E N D=- 1
2477 *%-----|-----|
2478 *CONTINUOUS NASHYD   NHYD=["S-1-FO-F-D"], DT=[1] min, AREA=[14.96](ha),
2479 *   DWF=[0](cms), CN C=[77], I A=[4.67](mm),
2480 *   N=[3], TP=[1.007] hrs,
2481 *   Continuous simulation parameters:
2482 *   I a REC per=[4](hrs),
2483 *   S M N=[-1](mm), S M A X=[-1](mm), S K=[0.010]/(mm),
2484 *   I n t e r E v e n t T i m e=[12](hrs)
2485 *   Baseflow simulation parameters:
2486 *   B a s e F l o w O p t i o n=[1] ,

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2487 *          I n i t GWRes Vol =[ 50 ] ( mm ) ,   GWRes K=[ 0. 96 ] ( mm/ day/ mm)
2488 *          VHydCond=[ 0. 055 ] ( mm/ hr ) ,     END=- 1
2489 *%-----|-----|
2490 *COMPUTE DUALHYD  NHYD i n=[ " S- 1- FO- F- D' ] ,   CI NLET=[ 1. 749 ] ( cms ) ,   NI NLET=[ 1 ] ,
2491 *          M a j NHYD=[ " S- 1FO- F- DJ " ]
2492 *          M nNHYD=[ " S- 1FO- F- DN" ]
2493 *          T M I STO=[ 9999999 ] ( cu- m)
2494 *%-----|-----|
2495 *ADD HYD          NHYDs um=[ " S- 1FO- F- DS" ] ,   NHYDs t o add=[ " S- 1FO- F- DJ "+" S- 1FO- F- DN" ]
2496 *%-----|-----|
2497 *ROUTE RESERVOI R  NHYDout =[ " S- 1FO- F- DR" ] ,   NHYD i n=[ " S- 1FO- F- DS" ] ,
2498 *          RDT=[ 1 ] ( mi n ) ,
2499 *          TABLE of ( OUTFLOW STORAGE ) values
2500 *                  ( cms ) - ( ha- m)
2501 *                  [ 0. 0      , 0. 0 ]
2502 *                  [ 0. 1788 , 0. 5966 ]
2503 *                  [      -1 ,  -1      ] ( max t wenty pts)
2504 *          NHYDovf=[ " S- 1FoFDovf " ]
2505 *%-----|-----|
2506 CONTINUOUS STANDHYD NHYD=[ " S- 1- D1 " ] ,   DT=[ 1 ] ( mi n ) ,   AREA=[ 21. 67 ] ( ha ) ,   XI MP=[ 0. 65 ] ,
TI MP=[ 0. 65 ] ,   DWF=[ 0 ] ( cms ) ,
2507 LOSS=[ 2 ] ,   SCS curve number CN=[ 75 ] ,   Pervious surfaces:
I Aper=[ 4. 67 ] ( mm ) ,   SLPP=[ 2. 0 ] ( % ) ,
2508 LGP=[ 40 ] ( m ) ,   MNP=[ 0. 25 ] ,   SCP=[ 0 ] ( mi n ) ,   Impervious surfaces:
I Ai mp=[ 1. 57 ] ( mm ) ,   SLPI=[ 0. 75 ] ( % ) ,
2509 LGI=[ 380. 088 ] ( m ) ,   MNI=[ 0. 013 ] ,   SCI=[ 0 ] ( mi n ) ,
2510 Continuous simulation parameters:
I aRECper=[ 4 ] ( hrs ) ,   I aRECI mp=[ 4 ] ( hrs ) ,
2511 SM N=[ - 1 ] ( mm ) ,   SMAX=[ - 1 ] ( mm ) ,   SK=[ 0. 010 ] / ( mm ) ,
2512 Inter Event Ti me=[ 12 ] ( hrs ) ,   END=- 1
2513
2514 *%-----|-----|
2515 *CONTINUOUS NASHYD  NHYD=[ " S- 1- D1 " ] ,   DT=[ 1 ] mi n ,   AREA=[ 21. 67 ] ( ha ) ,
2516 *          DWF=[ 0 ] ( cms ) ,   CN C=[ 77 ] ,   I A=[ 4. 67 ] ( mm ) ,
2517 *          N=[ 3 ] ,   TP=[ 1. 066 ] hrs ,
2518 *          Continuous simulation parameters:
2519 *          I aRECper=[ 4 ] ( hrs ) ,
2520 *          SM N=[ - 1 ] ( mm ) ,   SMAX=[ - 1 ] ( mm ) ,   SK=[ 0. 010 ] / ( mm ) ,
2521 *          Inter Event Ti me=[ 12 ] ( hrs )
2522 *          Baseflow simulation parameters:
2523 *          BaseFl owOpt ion=[ 1 ] ,
2524 *          I n i t GWRes Vol =[ 50 ] ( mm ) ,   GWRes K=[ 0. 96 ] ( mm/ day/ mm)
2525 *          VHydCond=[ 0. 055 ] ( mm/ hr ) ,     END=- 1
2526 *%-----|-----|
2527 COMPUTE DUALHYD  NHYD i n=[ " S- 1- D1 " ] ,   CI NLET=[ 2. 409 ] ( cms ) ,   NI NLET=[ 1 ] ,
2528 *          M a j NHYD=[ " S- 1- D1 J " ]
2529 *          M nNHYD=[ " S- 1- D1 N" ]
2530 *          T M I STO=[ 9999999 ] ( cu- m)
2531 *%-----|-----|
2532 ADD HYD          NHYDs um=[ " S- 1- D1 S" ] ,   NHYDs t o add=[ " S- 1- D1 J "+" S- 1- D1 N" ]
2533 *%-----|-----|
2534 ROUTE RESERVOI R  NHYDout =[ " S- 1- D1 R" ] ,   NHYD i n=[ " S- 1- D1 S" ] ,
2535 *          RDT=[ 1 ] ( mi n ) ,
2536 *          TABLE of ( OUTFLOW STORAGE ) values
2537 *                  ( cms ) - ( ha- m)
2538 *                  [ 0. 0      , 0. 0 ]
2539 *                  [ 0. 2590 , 0. 8642 ]
2540 *                  [      -1 ,  -1      ] ( max t wenty pts)
2541 *          NHYDovf=[ " S- 1- D1 Rovf " ]
2542 *%-----|-----|
2543 * -JFSA 2021-02-25 " S- 1- D2" and " S- 1- D3" are part of S- 1 sub-catchment. They are
moved to drain before station 6215 on Jock River
2544 *CONTINUOUS STANDHYD NHYD=[ " S- 1- D2 " ] ,   DT=[ 1 ] ( mi n ) ,   AREA=[ 18. 67 ] ( ha ) ,   XI MP=[ 0. 65 ] ,
TI MP=[ 0. 65 ] ,   DWF=[ 0 ] ( cms ) ,
2545 *          LOSS=[ 2 ] ,   SCS curve number CN=[ 75 ] ,   Pervious surfaces:
I Aper=[ 4. 67 ] ( mm ) ,   SLPP=[ 2. 0 ] ( % ) ,
2546 *          LGP=[ 40 ] ( m ) ,   MNP=[ 0. 25 ] ,   SCP=[ 0 ] ( mi n ) ,   Impervious surfaces:

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2547 * I Ai mp=[ 1. 57] ( mm) , SLPI =[ 0. 75] ( %),
2548 * LGI =[ 352. 798] ( m) , MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
2549 * Continuous simulation parameters:
2550 * IaRECper =[ 4] ( hr s) , IaRECI mp =[ 4] ( hr s) ,
2551 * SM N=[ - 1] ( mm) , SMAX=[ - 1] ( mm) , SK=[ 0. 010] / ( mm) ,
2552 * InterEventTime =[ 12] ( hr s) , END=- 1
2553 *%-----|-----
2553 *CONTINUOUS NASHYD NHYD=[ " S- 1- D2" ] , DT=[ 1] mi n , AREA=[ 18. 67] ( ha) ,
2554 * DWF=[ 0] ( cms) , CN C=[ 77] , IA=[ 4. 67] ( mm) ,
2555 * N=[ 3] , TP=[ 1. 120] hr s ,
2556 * Continuous simulation parameters:
2557 * IaRECper =[ 4] ( hr s) ,
2558 * SM N=[ - 1] ( mm) , SMAX=[ - 1] ( mm) , SK=[ 0. 010] / ( mm) ,
2559 * InterEventTime =[ 12] ( hr s)
2560 * Baseflow simulation parameters:
2561 * BaseFlowOption =[ 1] ,
2562 * In it GWRes Vol =[ 50] ( mm) , GWRes K=[ 0. 96] ( mm/ day/ mm)
2563 * VHydCond =[ 0. 055] ( mm/ hr ) , END=- 1
2564 *%-----|-----
2565 *COMPUTE DUALHYD NHYDi n=[ " S- 1- D2" ] , CI NLET=[ 2. 062] ( cms) , NI NLET=[ 1] ,
2566 * M aj NHYD=[ " S- 1- D2J" ]
2567 * M nNHYD=[ " S- 1- D2N" ]
2568 * TM I STO=[ 9999999] ( cu- m)
2569 *%-----|-----
2570 *ADD HYD NHYDs um=[ " S- 1- D2S" ] , NHYDs to add=[ " S- 1- D2J" +" S- 1- D2N" ]
2571 *%-----|-----
2572 *ROUTE RESERVOIR NHYDout =[ " S- 1- D2R" ] , NHYDi n=[ " S- 1- D2S" ] ,
2573 * RDT=[ 1] ( mi n) ,
2574 * TABLE of ( OUTFLOW STORAGE ) values
2575 * ( cms) - ( ha- m)
2576 * [ 0. 0 , 0. 0 ]
2577 * [ 0. 2231, 0. 7445 ]
2578 * [ - 1 , - 1 ] ( max twenty pts)
2579 * NHYDovf =[ " S- 1- D2Rovf" ]
2580 *%-----|-----
2581 *CONTINUOUS STANDHYD NHYD=[ " S- 1- D3" ] , DT=[ 1] ( mi n) , AREA=[ 6. 79] ( ha) , XI MP=[ 0. 65] ,
2582 * TI MP=[ 0. 65] , DWF=[ 0] ( cms) ,
2583 * LOSS=[ 2] , SCS curve number CN=[ 75] , Pervious surfaces:
I Aper =[ 4. 67] ( mm) , SLPP=[ 2. 0] ( %),
2584 * LGP=[ 40] ( m) , MNP=[ 0. 25] , SCP=[ 0] ( mi n) , Impervious surfaces:
I Ai mp=[ 1. 57] ( mm) , SLPI =[ 0. 75] ( %),
2585 * LGI =[ 212. 760] ( m) , MNI =[ 0. 013] , SCI =[ 0] ( mi n) ,
2586 * Continuous simulation parameters:
2587 * IaRECper =[ 4] ( hr s) , IaRECI mp =[ 4] ( hr s) ,
2588 * SM N=[ - 1] ( mm) , SMAX=[ - 1] ( mm) , SK=[ 0. 010] / ( mm) ,
2589 * InterEventTime =[ 12] ( hr s) , END=- 1
2590 *%-----|-----
2590 *CONTINUOUS NASHYD NHYD=[ " S- 1- D3" ] , DT=[ 1] mi n , AREA=[ 6. 79] ( ha) ,
2591 * DWF=[ 0] ( cms) , CN C=[ 77] , IA=[ 4. 67] ( mm) ,
2592 * N=[ 3] , TP=[ 1. 281] hr s ,
2593 * Continuous simulation parameters:
2594 * IaRECper =[ 4] ( hr s) ,
2595 * SM N=[ - 1] ( mm) , SMAX=[ - 1] ( mm) , SK=[ 0. 010] / ( mm) ,
2596 * InterEventTime =[ 12] ( hr s)
2597 * Baseflow simulation parameters:
2598 * BaseFlowOption =[ 1] ,
2599 * In it GWRes Vol =[ 50] ( mm) , GWRes K=[ 0. 96] ( mm/ day/ mm)
2600 * VHydCond =[ 0. 055] ( mm/ hr ) , END=- 1
2601 *%-----|-----
2602 *COMPUTE DUALHYD NHYDi n=[ " S- 1- D3" ] , CI NLET=[ 0. 719] ( cms) , NI NLET=[ 1] ,
2603 * M aj NHYD=[ " S- 1- D3J" ]
2604 * M nNHYD=[ " S- 1- D3N" ]
2605 * TM I STO=[ 9999999] ( cu- m)
2606 *%-----|-----
2607 *ADD HYD NHYDs um=[ " S- 1- D3S" ] , NHYDs to add=[ " S- 1- D3J" +" S- 1- D3N" ]
2608 *%-----|-----

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2609 *ROUTE RESERVOIR      NHYDout=["S-1-D3R"] ,NHYDin=["S-1-D3S"] ,
2610 *                      RDT=[1](min),
2611 *                      TABLE of ( OUTFLOW STORAGE ) values
2612 *                      (cms) - (ha-m)
2613 *                      [ 0.0      , 0.0 ]
2614 *                      [ 0.0811, 0.2708 ]
2615 *                      [ -1      , -1      ] (max twenty pts)
2616 *                      NHYDovf=["S-1-D3Rovf"]
2617 *%-----|-----
2618 CONTINUOUS STANDHYD NHYD=["S-1-D4"], DT=[1](min), AREA=[3.28](ha), XI MP=[0.65],
TI MP=[0.65], DWF=[0](cms),
2619 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
I Aper=[4.67](mm), SLPP=[2.0](%),
2620 LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
I Ai mp=[1.57](mm), SLPI=[0.75](%),
2621 LGI=[147.874](m), MNI=[0.013], SCI=[0](min),
2622 Continuous simulation parameters:
2623 I aRECper=[4](hrs), I aRECI mp=[4](hrs),
2624 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2625 InterEventTime=[12](hrs), END=-1
2626 *%-----|-----
2627 *CONTINUOUS NASHYD   NHYD=["S-1-D4"], DT=[1]min, AREA=[3.28](ha),
2628 *                      DWF=[0](cms), CN C=[77], I A=[4.67](mm),
2629 *                      N=[3], TP=[1.10]hrs,
2630 *                      Continuous simulation parameters:
2631 *                      I aRECper=[4](hrs),
2632 *                      SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2633 *                      InterEventTime=[12](hrs)
2634 *                      Baseflow simulation parameters:
2635 *                      BaseFlowOption=[1] ,
2636 *                      I n i t GWR es Vol =[50](mm), GWR es K=[0.96](mm/day/mm)
2637 *                      VHydCond=[0.055](mm/hr), END=-1
2638 *%-----|-----
2639 COMPUTE DUALHYD      NHYDin=["S-1-D4"], CI NLET=[0.421](cms), NI NLET=[1],
2640 *                      M a j NHYD=["S-1-D4J"]
2641 *                      M i n NHYD=["S-1-D4N"]
2642 *                      TMI STO=[9999999](cu-m)
2643 *%-----|-----
2644 ADD HYD              NHYDsum=["S-1-D4S"], NHYDs to add=["S-1-D4J"+"S-1-D4N"]
2645 *%-----|-----
2646 ROUTE RESERVOIR      NHYDout=["S-1-D4R"] ,NHYDin=["S-1-D4S"] ,
2647 *                      RDT=[1](min),
2648 *                      TABLE of ( OUTFLOW STORAGE ) values
2649 *                      (cms) - (ha-m)
2650 *                      [ 0.0      , 0.0 ]
2651 *                      [ 0.0392, 0.1308 ]
2652 *                      [ -1      , -1      ] (max twenty pts)
2653 *                      NHYDovf=["S-1-D4Rovf"]
2654 *%-----|-----
2655 CONTINUOUS STANDHYD NHYD=["S-1-D5"], DT=[1](min), AREA=[12.84](ha), XI MP=[0.65],
TI MP=[0.65], DWF=[0](cms),
2656 LOSS=[2], SCS curve number CN=[75], Pervious surfaces:
I Aper=[4.67](mm), SLPP=[2.0](%),
2657 LGP=[40](m), MNP=[0.25], SCP=[0](min), Impervious surfaces:
I Ai mp=[1.57](mm), SLPI=[0.75](%),
2658 LGI=[292.57](m), MNI=[0.013], SCI=[0](min),
2659 Continuous simulation parameters:
2660 I aRECper=[4](hrs), I aRECI mp=[4](hrs),
2661 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
2662 InterEventTime=[12](hrs), END=-1
2663 *%-----|-----
2664 *CONTINUOUS NASHYD   NHYD=["S-1-D5"], DT=[1]min, AREA=[12.84](ha),
2665 *                      DWF=[0](cms), CN C=[77], I A=[4.67](mm),
2666 *                      N=[3], TP=[1.10]hrs,
2667 *                      Continuous simulation parameters:
2668 *                      I aRECper=[4](hrs),

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2669 * SMN=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0. 010 ] / ( mm ) ,
2670 * InterEventTime=[ 12 ] ( hr s )
2671 * Baseflow simulation parameters:
2672 * BaseFlowOption=[ 1 ] ,
2673 * InitGWResVol=[ 50 ] ( mm ) , GWResK=[ 0. 96 ] ( mm / day / mm )
2674 * VHydCond=[ 0. 055 ] ( mm / hr ) , END=- 1
2675 *%-----|
2676 COMPUTE DUALHYD NHYDin=[ " S- 1- D5 " ] , CI NLET=[ 1. 5 ] ( cms ) , NI NLET=[ 1 ] ,
2677 Mj NHYD=[ " S- 1- D5J " ]
2678 MnNHYD=[ " S- 1- D5N " ]
2679 TMSTO=[ 9999999 ] ( cu- m )
2680 *%-----|
2681 ADD HYD NHYDsum=[ " S- 1- D5S " ] , NHYDsto add=[ " S- 1- D5J " + " S- 1- D5N " ]
2682 *%-----|
2683 ROUTE RESERVOIR NHYDout=[ " S- 1- D5R " ] , NHYDin=[ " S- 1- D5S " ] ,
2684 RDT=[ 1 ] ( mi n ) ,
2685 TABLE of ( OUTFLOW STORAGE ) values
2686 ( cms ) - ( ha- m )
2687 [ 0. 0 , 0. 0 ]
2688 [ 0. 1535 , 0. 5120 ]
2689 [ - 1 , - 1 ] ( max twenty pts )
2690 NHYDovf=[ " S- 1- D5Rovf " ]
2691 *%-----|
2692 CONTINUOUS STANDHYD NHYD=[ " S- 1- D6 " ] , DT=[ 1 ] ( mi n ) , AREA=[ 1. 75 ] ( ha ) , XI MP=[ 0. 65 ] ,
TI MP=[ 0. 65 ] , DWF=[ 0 ] ( cms ) ,
2693 LOSS=[ 2 ] , SCS curve number CN=[ 75 ] , Pervious surfaces:
I Aper=[ 4. 67 ] ( mm ) , SLPP=[ 2. 0 ] ( % ) ,
2694 LGP=[ 40 ] ( m ) , MNP=[ 0. 25 ] , SCP=[ 0 ] ( mi n ) , Impervious surfaces:
IAi mp=[ 1. 57 ] ( mm ) , SLPI=[ 0. 75 ] ( % ) ,
2695 LGI=[ 108. 01 ] ( m ) , MNI=[ 0. 013 ] , SCI=[ 0 ] ( mi n ) ,
2696 Continuous simulation parameters:
IaRECper=[ 4 ] ( hr s ) , IaRECI mp=[ 4 ] ( hr s ) ,
2697 SMN=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0. 010 ] / ( mm ) ,
2698 InterEventTime=[ 12 ] ( hr s ) , END=- 1
2699 *%-----|
2700 *CONTINUOUS NASHYD NHYD=[ " S- 1- D6 " ] , DT=[ 1 ] mi n , AREA=[ 1. 75 ] ( ha ) ,
2701 DWF=[ 0 ] ( cms ) , CN C=[ 77 ] , IA=[ 4. 67 ] ( mm ) ,
2702 N=[ 3 ] , TP=[ 1. 10 ] hr s ,
2703 Continuous simulation parameters:
2704 IaRECper=[ 4 ] ( hr s ) ,
2705 SMN=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0. 010 ] / ( mm ) ,
2706 InterEventTime=[ 12 ] ( hr s )
2707 Baseflow simulation parameters:
2708 BaseFlowOption=[ 1 ] ,
2709 InitGWResVol=[ 50 ] ( mm ) , GWResK=[ 0. 96 ] ( mm / day / mm )
2710 VHydCond=[ 0. 055 ] ( mm / hr ) , END=- 1
2711 *%-----|
2712 COMPUTE DUALHYD NHYDin=[ " S- 1- D6 " ] , CI NLET=[ 0. 232 ] ( cms ) , NI NLET=[ 1 ] ,
2713 Mj NHYD=[ " S- 1- D6J " ]
2714 MnNHYD=[ " S- 1- D6N " ]
2715 TMSTO=[ 9999999 ] ( cu- m )
2716 *%-----|
2717 ADD HYD NHYDsum=[ " S- 1- D6S " ] , NHYDsto add=[ " S- 1- D6J " + " S- 1- D6N " ]
2718 *%-----|
2719 ROUTE RESERVOIR NHYDout=[ " S- 1- D6R " ] , NHYDin=[ " S- 1- D6S " ] ,
2720 RDT=[ 1 ] ( mi n ) ,
2721 TABLE of ( OUTFLOW STORAGE ) values
2722 ( cms ) - ( ha- m )
2723 [ 0. 0 , 0. 0 ]
2724 [ 0. 0209 , 0. 0698 ]
2725 [ - 1 , - 1 ] ( max twenty pts )
2726 NHYDovf=[ " S- 1- D6Rovf " ]
2727 *%-----|
2728 CONTINUOUS STANDHYD NHYD=[ " S- 1- D7 " ] , DT=[ 1 ] ( mi n ) , AREA=[ 2. 03 ] ( ha ) , XI MP=[ 0. 65 ] ,
2729 TI MP=[ 0. 65 ] , DWF=[ 0 ] ( cms ) ,
2730 LOSS=[ 2 ] , SCS curve number CN=[ 75 ] , Pervious surfaces:

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2731 I Ape r=[ 4. 67] (mm) , SLPP=[ 2. 0] (%) ,
LGP=[ 40] (m) , MNP=[ 0. 25] , SCP=[ 0] (mi n) , I mperv ious surfaces :
2732 I A i mp=[ 1. 57] (mm) , SLPI=[ 0. 75] (%) ,
2733 LGI=[ 116. 33] (m) , MNI=[ 0. 013] , SCI=[ 0] (mi n) ,
2734 C ontinuous simulation parameters :
2735 I aRE Cpe r=[ 4] (hrs) , I aRE Ci mp=[ 4] (hrs) ,
2736 SM N=[ - 1] (mm) , SMAX=[ - 1] (mm) , SK=[ 0. 010] / (mm) ,
2737 I nter Event Ti me=[ 12] (hrs) , EN D=- 1
2737 *%-----|-----|
2738 *CONTI NUOUS NASHYD NHYD=[ "S- 1- D7" ] , DT=[ 1] mi n , AREA=[ 2. 03] (ha) ,
2739 * DWF=[ 0] (cms) , CN C=[ 77] , I A=[ 4. 67] (mm) ,
2740 * N=[ 3] , TP=[ 1. 10] hrs ,
2741 * C ontinuous simulation parameters :
2742 * I aRE Cpe r=[ 4] (hrs) ,
2743 * SM N=[ - 1] (mm) , SMAX=[ - 1] (mm) , SK=[ 0. 010] / (mm) ,
2744 * I nter Event Ti me=[ 12] (hrs)
2745 * B aseflow simulation parameters :
2746 * B aseFl owOpt ion=[ 1] ,
2747 * I n i t GWR es Vol =[ 50] (mm) , GWR es K=[ 0. 96] (mm/ day/ mm)
2748 * VHyd Cond=[ 0. 055] (mm/ hr) , EN D=- 1
2749 *%-----|-----|
2750 COMPUTE DUALHYD NHYD i n=[ "S- 1- D7" ] , CI NLET=[ 0. 265] (cms) , NI NLET=[ 1] ,
2751 M a j NHYD=[ "S- 1- D7J" ]
2752 M nNHYD=[ "S- 1- D7N" ]
2753 TM STO=[ 9999999] (cu- m)
2754 *%-----|-----|
2755 ADD HYD NHYDs um=[ "S- 1- D7S" ] , NHYDs t o add=[ "S- 1- D7J" +"S- 1- D7N" ]
2756 *%-----|-----|
2757 ROUTE RESERVOI R NHYDout =[ "S- 1- D7R" ] , NHYD i n=[ "S- 1- D7S" ] ,
2758 RDT=[ 1] (mi n) ,
2759 TABLE of ( OUTFLOW STORAGE ) values
2760 ( cms ) - ( ha- m)
2761 [ 0. 0 , 0. 0 ]
2762 [ 0. 0243, 0. 0810 ]
2763 [ - 1 , - 1 ] (max twenty pts)
2764 NHYDovf=[ "S- 1- D7Rovf" ]
2765 *%-----|-----|
2766 * -JFSA 2021-02-26 "S-1-D8" is a part of S-1 sub-catchment. It is moved to drain
before station 6016 on Jock River
2767 *CONTI NUOUS STANDHYD NHYD=[ "S- 1- D8" ] , DT=[ 1] (mi n) , AREA=[ 5. 27] (ha) , XI MP=[ 0. 65] ,
TI MP=[ 0. 65] , DWF=[ 0] (cms) ,
2768 * LOSS=[ 2] , SCS curve number CN=[ 75] , Pervious surfaces :
I Ape r=[ 4. 67] (mm) , SLPP=[ 2. 0] (%) ,
2769 * LGP=[ 40] (m) , MNP=[ 0. 25] , SCP=[ 0] (mi n) , I mperv ious surfaces :
I A i mp=[ 1. 57] (mm) , SLPI=[ 0. 75] (%) ,
2770 * LGI=[ 187. 439] (m) , MNI=[ 0. 013] , SCI=[ 0] (mi n) ,
2771 * C ontinuous simulation parameters :
2772 * I aRE Cpe r=[ 4] (hrs) , I aRE Ci mp=[ 4] (hrs) ,
2773 * SM N=[ - 1] (mm) , SMAX=[ - 1] (mm) , SK=[ 0. 010] / (mm) ,
2774 * I nter Event Ti me=[ 12] (hrs) , EN D=- 1
2775 *%-----|-----|
2776 *CONTI NUOUS NASHYD NHYD=[ "S- 1- D8" ] , DT=[ 1] mi n , AREA=[ 5. 27] (ha) ,
2777 * DWF=[ 0] (cms) , CN C=[ 77] , I A=[ 4. 67] (mm) ,
2778 * N=[ 3] , TP=[ 1. 10] hrs ,
2779 * C ontinuous simulation parameters :
2780 * I aRE Cpe r=[ 4] (hrs) ,
2781 * SM N=[ - 1] (mm) , SMAX=[ - 1] (mm) , SK=[ 0. 010] / (mm) ,
2782 * I nter Event Ti me=[ 12] (hrs)
2783 * B aseflow simulation parameters :
2784 * B aseFl owOpt ion=[ 1] ,
2785 * I n i t GWR es Vol =[ 50] (mm) , GWR es K=[ 0. 96] (mm/ day/ mm)
2786 * VHyd Cond=[ 0. 055] (mm/ hr) , EN D=- 1
2787 *%-----|-----|
2788 *COMPUTE DUALHYD NHYD i n=[ "S- 1- D8" ] , CI NLET=[ 2. 279] (cms) , NI NLET=[ 1] ,
2789 * M a j NHYD=[ "S- 1- D8J" ]
2790 * M nNHYD=[ "S- 1- D8N" ]

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2791 *          TMI STO=[ 9999999 ] ( cu- m)
2792 *%-----|-----|
2793 *ADD HYD          NHYDs um=[ " S- 1- D8S" ], NHYDs to add=[ " S- 1- D8J" +" S- 1- D8N" ]
2794 *%-----|-----|
2795 *ADD HYD          NHYDs um=[ " S- 1- D" ], NHYDs to add=[ " S- 1- Okeefe" +" S- 1" +" S- 1- Fost" ]
2796 *%-----|-----|
2797 *COMPUTE DUALHYD  NHYDi n=[ " S- 1- D" ], CI NLET=[ 11. 616 ] ( cms ), NI NLET=[ 1 ],
2798 *          Mj NHYD=[ " S- 1- D- M" ]
2799 *          MnNHYD=[ " S- 1- D- MN" ]
2800 *          TMI STO=[ 5974 ] ( cu- m)
2801 *%-----|-----|
2802 *ADD HYD          NHYDs um=[ " S- 1- DEV" ], NHYDs to add=[ " S- 1- D- M" +" S- 1- D- MN" ]
2803 *%-----|-----|
2804 *ROUTE RESERVOIR NHYDout=[ " S- 1- D8R" ] , NHYDi n=[ " S- 1- D8S" ] ,
2805 *          RDT=[ 1 ] ( mi n),
2806 *          TABLE of ( OUTFLOW STORAGE ) values
2807 *                  ( cms ) - ( ha- m)
2808 *                  [ 0. 0      , 0. 0 ]
2809 *                  [ 0. 0630, 0. 2102 ]
2810 *                  [ - 1      , - 1      ] ( max twenty pts)
2811 *          NHYDovf=[ " S- 1- D8Rovf" ]
2812 *%-----|-----|
2813 *%-----|-----|
2814 *          - JFSA 2021-02-08 Clarke (MS_P2 and P2-OVF) and Clarke Undeveloped area
(W_CLAR_UNDE) drain to Jock River at Station 5002 instead of Station 4534
2815 *#      Catchment W_CLAR
2816 *#      - To West Clarke Drain (south of the Jock)
2817 *#      - Subdivision with 43% imp. as per Barrhaven South MS
2818 *#      - 2020-11-30 update CLARKE Tributary Drainage Area to = 121 ha based on
P598(04)-11
2819 *#      - 2020-11-30 split CLARKE Drainage Area to MAJOR and ALL
2820 *#*****
2821 CONTINUOUS STANDHYD NHYD=[ " W_CLAR_M" ], DT=[ 1 ] mi n, AREA=[ 1. 772 ] ( ha ),
2822 XI MP=[ 0. 46 ], TI MP=[ 0. 59 ], DWF=[ 0 ] ( cms ), LOSS=[ 2 ],
2823 SCS curve number CN=[ 77 ],
2824 Pervious surfaces: I Aper=[ 4. 67 ] ( mm ), SLPP=[ 1 ] ( % ),
2825 LGP=[ 40 ] ( m ), MNP=[ 0. 25 ], SCP=[ 0 ] ( mi n ),
2826 Impervious surfaces: I Ai mp=[ 1. 57 ] ( mm ), SLPI=[ 1 ] ( % ),
2827 LGI=[ 109 ] ( m ), MNI=[ 0. 013 ], SCI=[ 0 ] ( mi n ),
2828 Continuous simulation parameters:
2829 Ia RECper=[ 4 ] ( hr s ), Ia RECI mp=[ 4 ] ( hr s ),
2830 SM N=[ - 1 ] ( mm ), SMAX=[ - 1 ] ( mm ), SK=[ 0. 010 ] / ( mm ),
2831 Inter Event Time=[ 18 ] ( hr s ), END=- 1
2832 *%-----|-----|
2833 *COMPUTE DUALHYD  NHYDi n=[ " W_CLAR_M" ], CI NLET=[ 0. 213 ] ( cms ), NI NLET=[ 1 ],
2834 *          Mj NHYD=[ " W_CLAR_Mj" ]
2835 *          MnNHYD=[ " W_CLAR_Mn" ]
2836 *          TMI STO=[ 0. 1 ] ( cu- m)
2837 *%-----|-----|
2838 *# 5- Year + 12% Capture
2839 ROUTE RESERVOIR NHYDout=[ " W_CLAR_Mn" ] , NHYDi n=[ " W_CLAR_M" ] ,
2840 RDT=[ 1 ] ( mi n),
2841 TABLE of ( OUTFLOW STORAGE ) values
2842 ( cms ) - ( ha- m)
2843 [ 0. 0      , 0. 0 ]
2844 [ 0. 213 , 0. 0001 ]
2845 [ - 1      , - 1      ] ( max twenty pts)
2846 NHYDovf=[ " W_CLAR_Mj" ] ,
2847 *%-----|-----|
2848 *          - Clarke_All area from P 598(04)-11 = 120.207 ha, change to 127.298 ha based on
GIS measurements,
2849 *          - JFSA, 2021-01-19 update W_CLAR_ALL to (121.17-1.772=119.398) ha based on GIS
measurements W_CLAR is 121.17 ha and W_CLAR_M is 1.772 ha
2850 CONTINUOUS STANDHYD NHYD=[ " W_CLAR_ALL" ], DT=[ 1 ] mi n, AREA=[ 119. 398 ] ( ha ),
2851 XI MP=[ 0. 60 ], TI MP=[ 0. 65 ], DWF=[ 0 ] ( cms ), LOSS=[ 2 ],
2852 SCS curve number CN=[ 77 ],

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2853          Pervious surfaces: I A per=[ 4.67](mm), SLPP=[ 1](%),
2854          LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
2855          Impervious surfaces: I A imp=[ 1.57](mm), SLPI=[ 1](%),
2856          LGI=[ 892.18](m), MNI=[ 0.013], SCI=[ 0](min),
2857          Continuous simulation parameters:
2858          I a REC per=[ 4](hrs), I a REC imp=[ 4](hrs),
2859          SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2860          Inter Event Time=[ 18](hrs), END=- 1
2861  *%-----|-----|
2862  ADD HYD          NHYDsum=[ "W_CLAR"], NHYDs to add=[ "W_CLAR_ALL"+"W_CLAR_Mj" ]
2863  *%-----|-----|
2864  SAVE HYD        NHYD=[ "W_CLAR"], # OF PCYCLES=[ -1], I CASEs h=[ 1]
2865                  HYD_COMMENT=[ "Total Flows to West Clarke" ]
2866  *#*****|
2867  *# West Clarke Pond 2
2868  *# - Rating curve obtained from Barrhaven South M&S modeling
2869  *# - Tributary Drainage Area to M&S Pond 2 = 241 ha
2870  *#*****|
2871  ROUTE RESERVOIR NHYDout=[ "MS_P2"], NHYDin=[ "W_CLAR"],
2872                  RDT=[ 1](min),
2873                  TABLE of ( OUTFLOW STORAGE ) values
2874                  (cms) - (ha-m)
2875                  [ 0.0 , 0.0 ]
2876                  [ 0.128 , 0.161 ]
2877                  [ 0.138 , 0.409 ]
2878                  [ 0.148 , 0.68 ]
2879                  [ 0.227 , 0.931 ]
2880                  [ 0.354 , 1.223 ]
2881                  [ 0.505 , 1.52 ]
2882                  [ 0.666 , 1.821 ]
2883                  [ 0.831 , 2.123 ]
2884                  [ 0.995 , 2.434 ]
2885                  [ 1.069 , 2.583 ]
2886                  [ 1.51 , 2.647 ]
2887                  [ 4.904 , 2.861 ]
2888                  [ 13.048 , 3.188 ]
2889                  [ 23.745 , 3.523 ]
2890                  [ 36.474 , 3.871 ]
2891                  [ 45.938 , 4.127 ]
2892                  [ 61.652 , 4.539 ]
2893                  [ -1 , -1 ] (max twenty pts)
2894                  NHYDovf=[ "P2-OVF" ]
2895  *%-----|-----|
2896  *#*****|
2897  * - JFSA, 2021-01-22 "W_CLAR_UNDE" (west of Clarke sub-catchment) discharges
directly to the Jock River through a road side ditch on the west side of Borrisokane
road (station 6016)
2898  *CONTINUOUS NASHYD NHYD=[ "W_CLAR_UNDE"], DT=[ 1]min, AREA=[ 35.65](ha),
2899  * DWF=[ 0](cms), CNVC=[ 77], IA=[ 4.67](mm),
2900  * N=[ 3], TP=[ 1.10]hrs,
2901  * Continuous simulation parameters:
2902  * I a REC per=[ 4](hrs),
2903  * SM N=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
2904  * Inter Event Time=[ 12](hrs)
2905  * Baseflow simulation parameters:
2906  * BaseFlowOption=[ 1],
2907  * I n i t GWR es Vol=[ 50](mm), GWR es K=[ 0.96](mm/day/mm)
2908  * VHydCond=[ 0.055](mm/hr), END=- 1
2909  *%-----|-----|
2910  ADD HYD          NHYDsum=[ "SN_CE"], NHYDs to
add=[ "N_CE"+"S- 1- D4R"+"S- 1- D5R"+"S- 1- D4Rovf"+"S- 1- D5Rovf"+"MS_P2"+"P2-OVF" ]
2911  *%-----|-----|
2912  SAVE HYD        NHYD=[ "SN_CE"], # OF PCYCLES=[ -1], I CASEs h=[ 1]
2913                  HYD_COMMENT=[ "Total Flows before Station 5737 on Jock River" ]
2914  *%-----|-----|
2915  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 5737

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2916  *# 2021-02-25 add station 5737 before station 5002. Station 5737 was extracted from the
      HEC-RAS model
      T:\PROJ\1474-16\Design\20201026-QuantityControlAnalysis\HEC-RAS\JockLi dar 2005
2917  *# JFSA 2021-03-02 change the slope to 0.0175% instead of 0.02593 to stabilize the model
2918  ROUTE CHANNEL      NHYDout=["5737"] , NHYDin=["SN_CE"] ,
2919                      RDT=[1](min),
2920                      CHLGTH=[270](m),   CHSLOPE=[0.0175](%),
2921                      FPSLOPE=[0.0175](%),
2922                      SECNUM=[1.0],      NSEG=[3]
2923                      ( SEGROUGH, SEGDIST (m))=
2924                      [0.050, -24.04
2925                      -0.035, 23.92
2926                      0.050, 1130.8] NSEG times
2927                      ( DISTANCE (m), ELEVATION (m))=
2928                      [-1060.52, 94 ]
2929                      [-268.6, 91.5 ]
2930                      [-259.43, 91.5 ]
2931                      [-179.48, 91.5 ]
2932                      [-67.9, 91.5 ]
2933                      [-59.21, 91.5 ]
2934                      [-33.19, 91 ]
2935                      [-26.08, 90.5 ]
2936                      [-24.04, 90 ]
2937                      [-13.14, 86.77 ]
2938                      [0, 85 ]
2939                      [14.68, 86.74 ]
2940                      [23.92, 90 ]
2941                      [25.78, 90.5 ]
2942                      [31.91, 91 ]
2943                      [91.95, 91.5 ]
2944                      [772.15, 92 ]
2945                      [961.49, 92.5 ]
2946                      [1044.69, 93 ]
2947                      [1130.8, 95 ]
2948  *%-----|-----|
2949  ADD HYD      NHYDsum=["5002"], NHYDs to
      add=["5737"+"S-1-D1R"+"S-1-D6R"+"S-1-D7R"+"S-1-D1Rovf"+"S-1-D6Rovf"+"S-1-D7Rovf"]
2950  *%-----|-----|
2951  SAVE HYD      NHYD=["5002"], # OF PCYCLES=[-1], ICASEsh=[1]
2952                      HYD_COMMENT=["Total Flows before Station 5002 on Jock River"]
2953  *%-----|-----|
2954  *# Hydrograph from Node Cedarview Road routed to Node at West Clarke Drain
2955  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 5002
2956  *# JFSA 2021-02-19 Change the slope from 0.01 % (as per Stantec Report 2007) to 0.0255
      % so the model will be more stable and give reasonable results. It is justifiable as
      ROUTE CHANNELs aren't well suited to really flat slopes.
2957  *# JFSA 2021-02-19 Change to three ROUTE CHANNEL with length 275 m each instead of one
      with 825 m length so the model will be more stable
2958  *# JFSA 2021-02-26 change the length of 5002 route channel from 825 m to 736 m That is
      because of adding station 5737 between station 6016 and station 5002. Then the length
      from station 5737 to station 5002 is 736 m Change the slope from 0.0255 % to 0.09511 %
2959  *
2960  ROUTE CHANNEL      NHYDout=["N_WCa"] , NHYDin=["5002"] ,
2961                      RDT=[1](min),
2962                      CHLGTH=[245.33333](m),   CHSLOPE=[0.09511](%),
2963                      FPSLOPE=[0.09511](%),
2964                      SECNUM=[1.0],      NSEG=[3]
2965                      ( SEGROUGH, SEGDIST (m))=
2966                      [0.050, -37.5
2967                      -0.035, 37.50
2968                      0.050, 157.05] NSEG times
2969                      ( DISTANCE (m), ELEVATION (m))=
2970                      [-601.81, 91.5 ]
2971                      [-37.50, 90.00]
2972                      [-19.61, 87.04]
2973                      [0.00, 85.70]

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2974 [ 14. 87, 86. 93]
2975 [ 37. 50, 90. 00]
2976 [ 38. 54, 90. 50]
2977 [ 42. 23, 91]
2978 [ 157. 05, 91. 50]
2979 * [ 161. 44, 91. 50]
2980 * [ 236. 48, 93. 00]
2981 * [ 385. 47, 92. 50]
2982 * [ 390. 78, 92. 50]
2983 *%-----|
2984 ROUTE CHANNEL NHYDout =["N_WCb" ] , NHYDin=["N_WCa" ] ,
2985 RDT=[ 1]( mi n) ,
2986 CHLGTH=[ 245. 33333]( m) , CHSLOPE=[ 0. 09511]( % ,
2987 FPSLOPE=[ 0. 09511]( % ,
2988 SECNUM=[ 1. 0] , NSEG=[ 3]
2989 ( SEGROUGH, SEGDI ST ( m) ) =
2990 [ 0. 050, - 37. 5
2991 - 0. 035, 37. 50
2992 0. 050, 157. 05] NSEG t i m e s
2993 ( DI STANCE ( m) , ELEVATI ON ( m) ) =
2994 [- 601. 81, 91. 5]
2995 [- 37. 50, 90. 00]
2996 [- 19. 61, 87. 04]
2997 [ 0. 00, 85. 70]
2998 [ 14. 87, 86. 93]
2999 [ 37. 50, 90. 00]
3000 [ 38. 54, 90. 50]
3001 [ 42. 23, 91]
3002 [ 157. 05, 91. 50]
3003 *%-----|
3004 ROUTE CHANNEL NHYDout =["N_WC" ] , NHYDin=["N_WCb" ] ,
3005 RDT=[ 1]( mi n) ,
3006 CHLGTH=[ 245. 33333]( m) , CHSLOPE=[ 0. 09511]( % ,
3007 FPSLOPE=[ 0. 09511]( % ,
3008 SECNUM=[ 1. 0] , NSEG=[ 3]
3009 ( SEGROUGH, SEGDI ST ( m) ) =
3010 [ 0. 050, - 37. 5
3011 - 0. 035, 37. 50
3012 0. 050, 157. 05] NSEG t i m e s
3013 ( DI STANCE ( m) , ELEVATI ON ( m) ) =
3014 [- 601. 81, 91. 5]
3015 [- 37. 50, 90. 00]
3016 [- 19. 61, 87. 04]
3017 [ 0. 00, 85. 70]
3018 [ 14. 87, 86. 93]
3019 [ 37. 50, 90. 00]
3020 [ 38. 54, 90. 50]
3021 [ 42. 23, 91]
3022 [ 157. 05, 91. 50]
3023 *#*****
3024 * - JFSA 2021-02-08 Clarke (MS_P2 and P2-OVF) and Clarke Undeveloped area
(W_CLAR_UNDE) drain to Jock River at Station 5002 instead of Station 4534
3025 *ADD HYD NHYDs um=["SN_WC" ] , NHYDs to
add=["MS_P2"+"P2-OVF"+"N_WC"+"W_CLAR_UNDE" ]
3026 *%-----|
3027 *SAVE HYD NHYD=["SN_WC" ] , # OF PCYCLES=[ - 1] , ICASEsh=[ 1]
3028 * HYD_COMMENT=["Total Flows at West Clarke Pond Outlet" ]
3029 *%-----|
3030 *# Hydrograph from Node West Clarke routed to Node at Kennedy - Burnett Drain
3031 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 4534
3032 *#
3033 ROUTE CHANNEL NHYDout =["N_KB" ] , NHYDin=["N_WC" ] ,
3034 RDT=[ 1]( mi n) ,
3035 CHLGTH=[ 1020]( m) , CHSLOPE=[ 0. 0498]( % ,
3036 FPSLOPE=[ 0. 0498]( % ,
3037 SECNUM=[ 1. 0] , NSEG=[ 3]

```

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3038 ( SEGROUGH, SEGDI ST ( m ) =
3039 [ 0. 050, - 23. 63
3040 - 0. 035, 23. 63
3041 0. 050, 728. 3] NSEG t i m e s
3042 ( DI STANCE ( m ) , ELEVATI ON ( m ) =
3043 [- 1082. 01, 94]
3044 [- 1028. 17, 92. 5]
3045 [- 992. 3, 93. 5]
3046 [- 279. 34, 90]
3047 [- 23. 63, 90]
3048 [- 13. 45, 87. 13]
3049 [- 0. 07, 86. 24]
3050 [ 10. 54, 87. 15]
3051 [ 23. 63, 90]
3052 [ 24. 86, 90. 5]
3053 [ 26. 72, 91]
3054 [ 45. 07, 91. 5]
3055 [ 128. 17, 91. 5]
3056 [ 270. 7, 92. 5]
3057 [ 728. 3, 95]
3058 *%-----|-----|
3059 *#*****|
3060 *# Catchment KEN_BU
3061 *# - To Kennedy-Burnett SWM Facility
3062 *# - Outlets to Fraser-Clarke drain (north of the Jock)
3063 *# - Medium density residential subdivision
3064 * - Add Kennedy Burnett model (Convert PCSWMM from NOVATECH June, 2020 to SWWHYMO)
3065 *#*****|
3066 *CONTINUOUS STANDHYD NHYD=["KEN_BU"], DT=[ 1] mi n, AREA=[ 281]( ha),
3067 * XI MP=[ 0. 55], TI MP=[ 0. 55], DWF=[ 0]( cms), LOSS=[ 2],
3068 * SCS curve number CN=[ 71],
3069 * Per vious surfaces: I A p e r=[ 4. 67]( mm), SLPP=[ 1]( %),
3070 * LGP=[ 40]( m), MNP=[ 0. 25], SCP=[ 0]( mi n),
3071 * I m p e r v i o u s surfaces: I A i m p=[ 1. 57]( mm), SLPI=[ 1]( %),
3072 * LGI=[ 1369]( m), MNI=[ 0. 013], SCI=[ 0]( mi n),
3073 * C o n t i n u o u s simulation parameters:
3074 * I a R E C p e r=[ 4]( h r s), I a R E C i m p=[ 4]( h r s),
3075 * S M N=[ - 1]( mm), S M A X=[ - 1]( mm), S K=[ 0. 010]/( mm),
3076 * I n t e r E v e n t T i m e=[ 18]( h r s), E N D=- 1
3077 *%-----|-----|
3078 *#*****|
3079 *# Existing Kennedy-Burnett SWM Facility
3080 *# - Rating curve obtained from URTKBP
3081 *# - Tributary Drainage Area to Pond = 160 ha
3082 *#*****|
3083 *ROUTE RESERVOIR NHYDout=["KEN_P"], NHYDin=["KEN_BU"],
3084 * RDT=[ 1]( mi n),
3085 * T A B L E of ( O U T F L O W S T O R A G E ) values
3086 * ( cms ) - ( ha - m )
3087 * [ 0. 0 , 0. 0 ]
3088 * [ 0. 13 , 0. 26]
3089 * [ 0. 43 , 0. 56]
3090 * [ 0. 67 , 0. 90]
3091 * [ 0. 86 , 1. 32]
3092 * [ 1. 01 , 1. 79]
3093 * [ 1. 15 , 2. 33]
3094 * [ - 1 , - 1 ] (max twenty pts)
3095 * N H Y D o v f=["KEN_OV"]
3096 *%-----|-----|
3097 * -JFSA, 2021-01-19 update all KEN_BU areas based on GIS measurements
3098 CONTINUOUS STANDHYD NHYD=["KB-01A"], DT=[ 1] mi n, AREA=[ 40. 82]( ha), XI MP=[ 0. 097],
3099 TI MP=[ 0. 4], DWF=[ 0]( cms), LOSS=[ 1]:
3099 Hort on: F o=[ 76. 20]( mm/ hr), F c=[ 13. 20]( mm/ hr), D C A Y=[ 4. 14]( / hr),
3100 F=[ 0. 00]( mm),
3100 P e r v i o u s areas: I A p e r=[ 4. 67]( mm), SLPP=[ 0. 5]( %), LGP=[ 40]( m),
MNP=[ 0. 250], SCP=[ 0]( mi n),

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3101      Impervious areas: I Aimp=[ 0.785](mm), SLPI=[ 0.5](%),
3102      LGI=[ 521.664](m), MNI=[ 0.013], SCI=[ 0](min),
3103      Continuous simulation parameters:
3103      IARECper=[ 4](hrs), IARECimp=[ 4](hrs), InterEventTime=[ 12](hrs),
3103      END=- 1
3104      *%-----|-----|
3105      COMPUTE DUALHYD      NHYDin=[ "KB-01A"], CINLET=[ 3.6](cms), NINLET=[ 1],
3106      MijNHYD=[ "KB-01A-M"]
3107      MnNHYD=[ "KB-01A-MN"]
3108      TMSSTO=[ 4995](cu-m)
3109      *%-----|-----|
3110      ADD HYD              NHYDsum=[ "KB-01A-S"], NHYDs to add=[ "KB-01A-M"+"KB-01A-MN"]
3111      *%-----|-----|
3112      CONTINUOUS STANDHYD NHYD=[ "KB-01B"], DT=[ 1]min, AREA=[ 31.1](ha), XI MP=[ 0.1875],
3112      TIMP=[ 0.375], DWF=[ 0](cms), LOSS=[ 1]:
3113      Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3113      F=[ 0.00](mm),
3114      Pervious areas: I Aper=[ 4.67](mm), SLPP=[ 0.42](%), LGP=[ 40](m),
3114      MNP=[ 0.250], SCP=[ 0](min),
3115      Impervious areas: I Aimp=[ 0.785](mm), SLPI=[ 0.42](%),
3115      LGI=[ 455.339](m), MNI=[ 0.013], SCI=[ 0](min),
3116      Continuous simulation parameters:
3117      IARECper=[ 4](hrs), IARECimp=[ 4](hrs), InterEventTime=[ 12](hrs),
3117      END=- 1
3118      *%-----|-----|
3119      COMPUTE DUALHYD      NHYDin=[ "KB-01B"], CINLET=[ 1.585](cms), NINLET=[ 1],
3120      MijNHYD=[ "KB-01B-M"]
3121      MnNHYD=[ "KB-01B-MN"]
3122      TMSSTO=[ 6075](cu-m)
3123      *%-----|-----|
3124      ADD HYD              NHYDsum=[ "KB-01B-S"], NHYDs to add=[ "KB-01B-M"+"KB-01B-MN"]
3125      *%-----|-----|
3126      CONTINUOUS STANDHYD NHYD=[ "KB-01C"], DT=[ 1]min, AREA=[ 13.78](ha), XI MP=[ 0.2045],
3126      TIMP=[ 0.409], DWF=[ 0](cms), LOSS=[ 1]:
3127      Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3127      F=[ 0.00](mm),
3128      Pervious areas: I Aper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3128      MNP=[ 0.250], SCP=[ 0](min),
3129      Impervious areas: I Aimp=[ 0.785](mm), SLPI=[ 0.5](%),
3129      LGI=[ 303.095](m), MNI=[ 0.013], SCI=[ 0](min),
3130      Continuous simulation parameters:
3131      IARECper=[ 4](hrs), IARECimp=[ 4](hrs), InterEventTime=[ 12](hrs),
3131      END=- 1
3132      *%-----|-----|
3133      COMPUTE DUALHYD      NHYDin=[ "KB-01C"], CINLET=[ 1.35](cms), NINLET=[ 1],
3134      MijNHYD=[ "KB-01C-M"]
3135      MnNHYD=[ "KB-01C-MN"]
3136      TMSSTO=[ 1880](cu-m)
3137      *%-----|-----|
3138      ADD HYD              NHYDsum=[ "KB-01C-S"], NHYDs to add=[ "KB-01C-M"+"KB-01C-MN"]
3139      *%-----|-----|
3140      CONTINUOUS STANDHYD NHYD=[ "KB-03"], DT=[ 1]min, AREA=[ 84.78](ha), XI MP=[ 0.197],
3140      TIMP=[ 0.394], DWF=[ 0](cms), LOSS=[ 1]:
3141      Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
3141      F=[ 0.00](mm),
3142      Pervious areas: I Aper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3142      MNP=[ 0.250], SCP=[ 0](min),
3143      Impervious areas: I Aimp=[ 0.785](mm), SLPI=[ 0.63](%),
3143      LGI=[ 751.798](m), MNI=[ 0.013], SCI=[ 0](min),
3144      Continuous simulation parameters:
3145      IARECper=[ 4](hrs), IARECimp=[ 4](hrs), InterEventTime=[ 12](hrs),
3145      END=- 1
3146      *%-----|-----|
3147      COMPUTE DUALHYD      NHYDin=[ "KB-03"], CINLET=[ 5.27](cms), NINLET=[ 1],
3148      MijNHYD=[ "KB-03-M"]
3149      MnNHYD=[ "KB-03-MN"]

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3150          TMI STO=[ 15500] (cu-m)
3151  *%-----|-----|
3152  ADD HYD      NHYDs um=[ "KB- 03- S"], NHYDs to add=[ "KB- 03- M" +"KB- 03- MN" ]
3153  *%-----|-----|
3154  CONTI NUOUS STANDHYD NHYD=[ "KB- 04"], DT=[ 1] mi n, AREA=[ 6.95] (ha), XI MP=[ 0.85],
TI MP=[ 0.85], DWF=[ 0] (cms), LOSS=[ 1]:
3155          Hort on: Fo=[ 76.20] (mm/ hr), Fc=[ 13.20] (mm/ hr), DCAY=[ 4.14] (/ hr),
F=[ 0.00] (mm),
3156          Perv ious areas: I Aper=[ 4.67] (mm), SLPP=[ 2.0] (%), LGP=[ 40] (m),
MNP=[ 0.250], SCP=[ 0] (mi n),
3157          Imperv ious areas: I Ai mp=[ 0.942] (mm), SLPI =[ 0.5] (%),
LGI =[ 215.252] (m), MNI =[ 0.013], SCI =[ 0] (mi n),
3158          Continuous simulation parameters:
3159          IaRECper=[ 4] (hr s), IaRECI mp=[ 4] (hr s), Int er Event Ti me=[ 12] (hr s),
END=- 1
3160  *%-----|-----|
3161  COMPUTE DUALHYD NHYDi n=[ "KB- 04"], CI NLET=[ 0.503] (cms), NI NLET=[ 1],
3162          M aj NHYD=[ "KB- 04- M" ]
3163          M nNHYD=[ "KB- 04- MN" ]
3164          TMI STO=[ 1972] (cu-m)
3165  *%-----|-----|
3166  ADD HYD      NHYDs um=[ "KB- 04- S"], NHYDs to add=[ "KB- 04- M" +"KB- 04- MN" ]
3167  *%-----|-----|
3168  CONTI NUOUS STANDHYD NHYD=[ "KB- 05"], DT=[ 1] mi n, AREA=[ 5.19] (ha), XI MP=[ 0.93],
TI MP=[ 0.93], DWF=[ 0] (cms), LOSS=[ 1]:
3169          Hort on: Fo=[ 76.20] (mm/ hr), Fc=[ 13.20] (mm/ hr), DCAY=[ 4.14] (/ hr),
F=[ 0.00] (mm),
3170          Perv ious areas: I Aper=[ 4.67] (mm), SLPP=[ 2.0] (%), LGP=[ 40] (m),
MNP=[ 0.250], SCP=[ 0] (mi n),
3171          Imperv ious areas: I Ai mp=[ 1.57] (mm), SLPI =[ 0.5] (%),
LGI =[ 186.011] (m), MNI =[ 0.013], SCI =[ 0] (mi n),
3172          Continuous simulation parameters:
3173          IaRECper=[ 4] (hr s), IaRECI mp=[ 4] (hr s), Int er Event Ti me=[ 12] (hr s),
END=- 1
3174  *%-----|-----|
3175  *%-----|-----|
3176  CONTI NUOUS STANDHYD NHYD=[ "KB- 06"], DT=[ 1] mi n, AREA=[ 12.93] (ha), XI MP=[ 0.873],
TI MP=[ 0.873], DWF=[ 0] (cms), LOSS=[ 1]:
3177          Hort on: Fo=[ 76.20] (mm/ hr), Fc=[ 13.20] (mm/ hr), DCAY=[ 4.14] (/ hr),
F=[ 0.00] (mm),
3178          Perv ious areas: I Aper=[ 4.67] (mm), SLPP=[ 2.0] (%), LGP=[ 40] (m),
MNP=[ 0.250], SCP=[ 0] (mi n),
3179          Imperv ious areas: I Ai mp=[ 0.942] (mm), SLPI =[ 4.75] (%),
LGI =[ 293.598] (m), MNI =[ 0.013], SCI =[ 0] (mi n),
3180          Continuous simulation parameters:
3181          IaRECper=[ 4] (hr s), IaRECI mp=[ 4] (hr s), Int er Event Ti me=[ 12] (hr s),
END=- 1
3182  *%-----|-----|
3183  COMPUTE DUALHYD NHYDi n=[ "KB- 06"], CI NLET=[ 2.262] (cms), NI NLET=[ 1],
3184          M aj NHYD=[ "KB- 06- M" ]
3185          M nNHYD=[ "KB- 06- MN" ]
3186          TMI STO=[ 1950] (cu-m)
3187  *%-----|-----|
3188  ADD HYD      NHYDs um=[ "KB- 06- S"], NHYDs to add=[ "KB- 06- M" +"KB- 06- MN" ]
3189  *%-----|-----|
3190  CONTI NUOUS STANDHYD NHYD=[ "KB- 11"], DT=[ 1] mi n, AREA=[ 4.03] (ha), XI MP=[ 0.675],
TI MP=[ 0.675], DWF=[ 0] (cms), LOSS=[ 1]:
3191          Hort on: Fo=[ 76.20] (mm/ hr), Fc=[ 13.20] (mm/ hr), DCAY=[ 4.14] (/ hr),
F=[ 0.00] (mm),
3192          Perv ious areas: I Aper=[ 4.67] (mm), SLPP=[ 2.0] (%), LGP=[ 40] (m),
MNP=[ 0.250], SCP=[ 0] (mi n),
3193          Imperv ious areas: I Ai mp=[ 0.785] (mm), SLPI =[ 2.0] (%),
LGI =[ 163.911] (m), MNI =[ 0.013], SCI =[ 0] (mi n),
3194          Continuous simulation parameters:
3195          IaRECper=[ 4] (hr s), IaRECI mp=[ 4] (hr s), Int er Event Ti me=[ 12] (hr s),
END=- 1

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3196 *%-----|-----|
3197 COMPUTE DUALHYD NHYDin=["KB-11"], CINLET=[0.5773](cms), NINLET=[1],
3198 MajNHYD=["KB-11-M"]
3199 MnNHYD=["KB-11-MN"]
3200 TMSTO=[597](cu-m)
3201 *%-----|-----|
3202 ADD HYD NHYDsum=["KB-11-S"], NHYDs to add=["KB-11-M"+"KB-11-MN"]
3203 *%-----|-----|
3204 CONTINUOUS STANDHYD NHYD=["S1"], DT=[1]min, AREA=[4.99](ha), XI MP=[0.93], TI MP=[0.93],
DWF=[0](cms), LOSS=[1]:
3205 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3206 Pervious areas: I A per=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3207 Impervious areas: I A i mp=[1.57](mm), SLPI=[2.0](%),
LGI=[182.392](m), MNI=[0.013], SCI=[0](min),
3208 Continuous simulation parameters:
3209 I a RE C per=[4](hrs), I a RE C i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=-1
3210 *%-----|-----|
3211 CONTINUOUS STANDHYD NHYD=["KB-15"], DT=[1]min, AREA=[2.15](ha), XI MP=[0.79],
TI MP=[0.79], DWF=[0](cms), LOSS=[1]:
3212 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3213 Pervious areas: I A per=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3214 Impervious areas: I A i mp=[0.157](mm), SLPI=[0.3](%),
LGI=[119.722](m), MNI=[0.013], SCI=[0](min),
3215 Continuous simulation parameters:
3216 I a RE C per=[4](hrs), I a RE C i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=-1
3217 *%-----|-----|
3218 *%-----|-----|
3219 ADD HYD NHYDsum=["KB-P1"], NHYDs to
add=["KB-01A-S"+"KB-01B-S"+"KB-01C-S"+"KB-03-S"+"KB-04-S"+"KB-05"+"KB-06-S"+"KB-11-S"+"KB
-15"+"S1"]
3220 *%-----|-----|
3221 ROUTE RESERVOIR NHYDout=["KB-P1R"], NHYDin=["KB-P1"],
3222 RDT=[1](min),
3223 TABLE of ( OUTFLOW STORAGE ) values
3224 (cms) - (ha-m)
3225 [ 0.0 , 0.0 ]
3226 [0.076,0.003]
3227 [0.088,0.006]
3228 [0.136,0.011]
3229 [0.301,0.017]
3230 [0.454,0.027]
3231 [0.631,0.041]
3232 [1.173,0.068]
3233 [1.91,0.111]
3234 [4.847,0.231]
3235 [9.813,0.436]
3236 [12.134,0.617]
3237 [12.438,0.732]
3238 [12.424,0.811]
3239 [12.425,0.894]
3240 [ -1 , -1 ] (max twenty pts)
3241 NHYDovf=["KB-P1ovf"]
3242 *%-----|-----|
3243 ADD HYD NHYDsum=["KB-Pond1"], NHYDs to add=["KB-P1R"+"KB-P1ovf"]
3244 *%-----|-----|
3245 SAVE HYD NHYD=["KB-Pond1"], # OF PCYCLES=[-1], I CASEs h=[1]
3246 HYD_COMMENT=["Total Flows at KB first pond"]
3247 *%-----|-----|
3248 CONTINUOUS STANDHYD NHYD=["KB-07"], DT=[1]min, AREA=[10.86](ha), XI MP=[0.86],
TI MP=[0.86], DWF=[0](cms), LOSS=[1]:

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3249      Horton: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14](/ hr),
3250      F=[ 0.00](mm),
3251      Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3252      MNP=[ 0.250], SCP=[ 0](min),
3253      Impervious areas: IAimp=[ 0.785](mm), SLPI=[ 2.0](%),
3254      LGI=[ 269.072](m), MNI=[ 0.013], SCI=[ 0](min),
3255      Continuous simulation parameters:
3256      IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3257      END=- 1
3258
3259      *%-----|-----|
3260      COMPUTE DUALHYD NHYDin=[ "KB-07"], CINLET=[ 2.094](cms), NINLET=[ 1],
3261      MajNHYD=[ "KB-07-M"]
3262      MinNHYD=[ "KB-07-MN"]
3263      TMSSTO=[ 1378](cu-m)
3264
3265      *%-----|-----|
3266      ADD HYD NHYDsum=[ "KB-07-S"], NHYDsto add=[ "KB-07-M"+"KB-07-MN"]
3267      *%-----|-----|
3268      CONTINUOUS STANDHYD NHYD=[ "KB-08"], DT=[ 1]min, AREA=[ 6.61](ha), XI MP=[ 0.64],
3269      TITMP=[ 0.64], DWF=[ 0](cms), LOSS=[ 1]:
3270      Horton: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14](/ hr),
3271      F=[ 0.00](mm),
3272      Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3273      MNP=[ 0.250], SCP=[ 0](min),
3274      Impervious areas: IAimp=[ 0.785](mm), SLPI=[ 2.0](%),
3275      LGI=[ 209.921](m), MNI=[ 0.013], SCI=[ 0](min),
3276      Continuous simulation parameters:
3277      IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3278      END=- 1
3279
3280      *%-----|-----|
3281      COMPUTE DUALHYD NHYDin=[ "KB-08"], CINLET=[ 1.058](cms), NINLET=[ 1],
3282      MajNHYD=[ "KB-08-M"]
3283      MinNHYD=[ "KB-08-MN"]
3284      TMSSTO=[ 787](cu-m)
3285
3286      *%-----|-----|
3287      ADD HYD NHYDsum=[ "KB-08-S"], NHYDsto add=[ "KB-08-M"+"KB-08-MN"]
3288      *%-----|-----|
3289      CONTINUOUS STANDHYD NHYD=[ "KB-09"], DT=[ 1]min, AREA=[ 2.6](ha), XI MP=[ 0.86],
3290      TITMP=[ 0.86], DWF=[ 0](cms), LOSS=[ 1]:
3291      Horton: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14](/ hr),
3292      F=[ 0.00](mm),
3293      Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3294      MNP=[ 0.250], SCP=[ 0](min),
3295      Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 2.0](%),
3296      LGI=[ 131.656](m), MNI=[ 0.013], SCI=[ 0](min),
3297      Continuous simulation parameters:
3298      IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3299      END=- 1
3300
3301      *%-----|-----|
3302      *%-----|-----|
3303      CONTINUOUS STANDHYD NHYD=[ "KB-10_1"], DT=[ 1]min, AREA=[ 2.37](ha), XI MP=[ 0.86],
3304      TITMP=[ 0.86], DWF=[ 0](cms), LOSS=[ 1]:
3305      Horton: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14](/ hr),
3306      F=[ 0.00](mm),
3307      Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
3308      MNP=[ 0.250], SCP=[ 0](min),
3309      Impervious areas: IAimp=[ 1.57](mm), SLPI=[ 2.0](%),
3310      LGI=[ 125.698](m), MNI=[ 0.013], SCI=[ 0](min),
3311      Continuous simulation parameters:
3312      IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs), InterEventTime=[ 12](hrs),
3313      END=- 1
3314
3315      *%-----|-----|
3316      CONTINUOUS STANDHYD NHYD=[ "KB-10_2"], DT=[ 1]min, AREA=[ 1.14](ha), XI MP=[ 0.86],
3317      TITMP=[ 0.86], DWF=[ 0](cms), LOSS=[ 1]:
3318      Horton: Fo=[ 76.20](mm/ hr), Fc=[ 13.20](mm/ hr), DCAY=[ 4.14](/ hr),
3319      F=[ 0.00](mm),
3320      Pervious areas: IAper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),

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3294 MNP=[ 0.250], SCP=[ 0](mi n),
Impervious areas: I Ai mp=[ 1.57](mm), SLPI=[ 2.0](%), LGI=[ 87.178](m),
MNI=[ 0.013], SCI=[ 0](mi n),
3295 Continuous simulation parameters:
3296 IaRECPer=[ 4](hrs), IaRECI mp=[ 4](hrs), Inter Event Ti me=[ 12](hrs),
END=- 1
3297 *%-----|-----|
3298 *%-----|-----|
3299 CONTINUOUS STANDHYD NHYD=["KB- 12"], DT=[ 1]mi n, AREA=[ 4.86](ha), XI MP=[ 0.79],
TIMP=[ 0.79], DWF=[ 0](cms), LOSS=[ 1]:
3300 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
F=[ 0.00](mm),
3301 Pervious areas: I Aper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
MNP=[ 0.250], SCP=[ 0](mi n),
3302 Impervious areas: I Ai mp=[ 1.099](mm), SLPI=[ 2.0](%),
LGI=[ 180.000](m), MNI=[ 0.013], SCI=[ 0](mi n),
3303 Continuous simulation parameters:
3304 IaRECPer=[ 4](hrs), IaRECI mp=[ 4](hrs), Inter Event Ti me=[ 12](hrs),
END=- 1
3305 *%-----|-----|
3306 COMPUTE DUALHYD NHYDin=["KB- 12"], CILET=[ 0.8665](cms), NILET=[ 1],
3307 Maj NHYD=["KB- 12- M"]
3308 MnNHYD=["KB- 12- MN"]
3309 TMS TO=[ 632](cu- m)
3310 *%-----|-----|
3311 ADD HYD NHYDsum=["KB- 12- S"], NHYDs to add=["KB- 12- M"+"KB- 12- MN"]
3312 *%-----|-----|
3313 CONTINUOUS STANDHYD NHYD=["KB- 13"], DT=[ 1]mi n, AREA=[ 10.19](ha), XI MP=[ 0.64],
TIMP=[ 0.64], DWF=[ 0](cms), LOSS=[ 1]:
3314 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
F=[ 0.00](mm),
3315 Pervious areas: I Aper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
MNP=[ 0.250], SCP=[ 0](mi n),
3316 Impervious areas: I Ai mp=[ 0.785](mm), SLPI=[ 2.0](%),
LGI=[ 260.640](m), MNI=[ 0.013], SCI=[ 0](mi n),
3317 Continuous simulation parameters:
3318 IaRECPer=[ 4](hrs), IaRECI mp=[ 4](hrs), Inter Event Ti me=[ 12](hrs),
END=- 1
3319 *%-----|-----|
3320 COMPUTE DUALHYD NHYDin=["KB- 13"], CILET=[ 1.722](cms), NILET=[ 1],
3321 Maj NHYD=["KB- 13- M"]
3322 MnNHYD=["KB- 13- MN"]
3323 TMS TO=[ 1077](cu- m)
3324 *%-----|-----|
3325 ADD HYD NHYDsum=["KB- 13- S"], NHYDs to add=["KB- 13- M"+"KB- 13- MN"]
3326 *%-----|-----|
3327 CONTINUOUS STANDHYD NHYD=["KB- 14"], DT=[ 1]mi n, AREA=[ 5.47](ha), XI MP=[ 0.64],
TIMP=[ 0.64], DWF=[ 0](cms), LOSS=[ 1]:
3328 Horton: Fo=[ 76.20](mm/hr), Fc=[ 13.20](mm/hr), DCAY=[ 4.14](/hr),
F=[ 0.00](mm),
3329 Pervious areas: I Aper=[ 4.67](mm), SLPP=[ 2.0](%), LGP=[ 40](m),
MNP=[ 0.250], SCP=[ 0](mi n),
3330 Impervious areas: I Ai mp=[ 0.785](mm), SLPI=[ 2.0](%),
LGI=[ 190.962](m), MNI=[ 0.013], SCI=[ 0](mi n),
3331 Continuous simulation parameters:
3332 IaRECPer=[ 4](hrs), IaRECI mp=[ 4](hrs), Inter Event Ti me=[ 12](hrs),
END=- 1
3333 *%-----|-----|
3334 COMPUTE DUALHYD NHYDin=["KB- 14"], CILET=[ 0.8734](cms), NILET=[ 1],
3335 Maj NHYD=["KB- 14- M"]
3336 MnNHYD=["KB- 14- MN"]
3337 TMS TO=[ 631](cu- m)
3338 *%-----|-----|
3339 ADD HYD NHYDsum=["KB- 14- S"], NHYDs to add=["KB- 14- M"+"KB- 14- MN"]
3340 *%-----|-----|
3341 *%-----|-----|

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3342 CONTINUOUS STANDHYD NHYD=["KB-16_2"], DT=[1] min, AREA=[3.42](ha), XI MP=[0.71],
TI MP=[0.71], DWF=[0](cms), LOSS=[1]:
3343 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3344 Pervious areas: I A per=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3345 Impervious areas: I A i mp=[0.157](mm), SLPI=[0.3](%),
LGI=[150.997](m), MNI=[0.013], SCI=[0](min),
3346 Continuous simulation parameters:
3347 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=- 1
3348 *%-----|-----|
3349 ADD HYD NHYDsum=["KB-P2"], NHYDs to
add=["KB-Pond1"+"KB-07-S"+"KB-08-S"+"KB-09"+"KB-10_1"+"KB-10_2"+"KB-12-S"+"KB-13-S"+"KB-1
4-S"+"KB-16_2"]
3350 *%-----|-----|
3351 ROUTE RESERVOIR NHYDout=["KB-P2R"], NHYDin=["KB-P2"],
3352 RDT=[1](min),
3353 TABLE of ( OUTFLOW STORAGE ) values
3354 (cms) - (ha-m)
3355 [ 0.0 , 0.0 ]
3356 [ 0.053, 0.005 ]
3357 [ 0.132, 0.009 ]
3358 [ 0.269, 0.014 ]
3359 [ 0.455, 0.023 ]
3360 [ 0.699, 0.037 ]
3361 [ 0.947, 0.056 ]
3362 [ 1.853, 0.09 ]
3363 [ 2.712, 0.146 ]
3364 [ 6.626, 0.287 ]
3365 [ 11.228, 0.515 ]
3366 [ 14.885, 0.738 ]
3367 [ 16.473, 0.893 ]
3368 [ 17.311, 0.998 ]
3369 [ 17.633, 1.063 ]
3370 [ 17.634, 1.112 ]
3371 [ -1 , -1 ] (max twenty pts)
3372 NHYDovf=["KB-P2ovf"]
3373 *%-----|-----|
3374 ADD HYD NHYDsum=["KB-Pond2"], NHYDs to add=["KB-P2R"+"KB-P2ovf"]
3375 *%-----|-----|
3376 SAVE HYD NHYD=["KB-Pond2"], # OF PCYCLES=[-1], I CASEs h=[1]
3377 HYD_COMMENT=["Total Flows at KB second pond"]
3378 *%-----|-----|
3379 CONTINUOUS STANDHYD NHYD=["KB-16_1"], DT=[1] min, AREA=[2.8](ha), XI MP=[0.75],
TI MP=[0.75], DWF=[0](cms), LOSS=[1]:
3380 Horton: Fo=[76.20](mm/hr), Fc=[13.20](mm/hr), DCAY=[4.14](/hr),
F=[0.00](mm),
3381 Pervious areas: I A per=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
MNP=[0.250], SCP=[0](min),
3382 Impervious areas: I A i mp=[0.157](mm), SLPI=[0.3](%),
LGI=[136.626](m), MNI=[0.013], SCI=[0](min),
3383 Continuous simulation parameters:
3384 I a REC per=[4](hrs), I a REC i mp=[4](hrs), I n t e r E v e n t T i m e=[12](hrs),
END=- 1
3385 *%-----|-----|
3386 ADD HYD NHYDsum=["KB-P3"], NHYDs to add=["KB-Pond2"+"KB-16_1"]
3387 *%-----|-----|
3388 *%-----|-----|
3389 * One inflow node from pond 3 is added to the model (ROUTE RESERVOIR)
3390 * Another inflow node from right side of pond 3 is not added to the model
3391 ROUTE RESERVOIR NHYDout=["KB-P3R"], NHYDin=["KB-P3"],
3392 RDT=[1](min),
3393 TABLE of ( OUTFLOW STORAGE ) values
3394 (cms) - (ha-m)
3395 [ 0.0 , 0.0 ]

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3396 [ 0.051, 0.002]
3397 [ 0.048, 0.003]
3398 [ 0.057, 0.029]
3399 [ 0.089, 0.045]
3400 [ 0.133, 0.069]
3401 [ 0.199, 0.106]
3402 [ 0.321, 0.172]
3403 [ 1.029, 0.306]
3404 [ 4.036, 0.527]
3405 [ 8.332, 0.761]
3406 [ 11.727, 0.941]
3407 [ 14.125, 1.067]
3408 [ 15.675, 1.149]
3409 [ 16.555, 1.196]
3410 [ 16.911, 1.214]
3411 [ -1 , -1 ] (max twenty pts)
3412 NHYDovf=["KB- P3ovf"]
3413 *%-----|-----|
3414 ADD HYD NHYDs um=["KB- Pond3"], NHYDs to add=["KB- P3R"+"KB- P3ovf"]
3415 *%-----|-----|
3416 SAVE HYD NHYD=["KB- Pond3"], # OF PCYCLES=[- 1], ICASEsh=[ 1]
3417 HYD_COMMENT=["Total Flows at KB third pond"]
3418 *%-----|-----|
3419 *#*****|
3420 *# EXISTING / PROPOSED Subcatchments (Kennedy-Burnett SWM Facility (118080), SWM
3421 Modeling Approach, NOVATECH Report June, 2020)
3422 *# - TO FRASER- CLARKE DRAIN
3423 *#*****|
3424 CONTINUOUS STANDHYD NHYD=["FC- 01"], DT=[ 1] min, AREA=[ 8.03] (ha), XI MP=[ 0.47],
3425 TI MP=[ 0.47], DWF=[ 0] (cms), LOSS=[ 1]:
3426 Horton: Fo=[ 76.20] (mm/ hr), Fc=[ 13.20] (mm/ hr), DCAY=[ 4.14] (/ hr),
3427 F=[ 0.00] (mm),
3428 Pervious areas: IAper=[ 4.67] (mm), SLPP=[ 2.0] (%), LGP=[ 40] (m),
3429 MNP=[ 0.250], SCP=[ 0] (min),
3430 Impervious areas: IAimp=[ 1.57] (mm), SLPI=[ 1.0] (%),
3431 LGI=[ 231.373] (m), MNI=[ 0.013], SCI=[ 0] (min),
3432 Continuous simulation parameters:
3433 IARECper=[ 4] (hrs), IARECimp=[ 4] (hrs), InterEventTime=[ 12] (hrs),
3434 END=- 1
3435 *%-----|-----|
3436 COMPUTE DUALHYD NHYDin=["FC- 01"], CINLET=[ 0.756] (cms), NINLET=[ 1],
3437 MajNHYD=["FC- 01- M"]
3438 MnNHYD=["FC- 01- MN"]
3439 TMS TO=[ 714] (cu- m)
3440 *%-----|-----|
3441 ADD HYD NHYDs um=["FC- 01- S"], NHYDs to add=["FC- 01- M"+"FC- 01- MN"]
3442 *%-----|-----|
3443 CONTINUOUS STANDHYD NHYD=["FC- 02"], DT=[ 1] min, AREA=[ 16.05] (ha), XI MP=[ 0.93],
3444 TI MP=[ 0.93], DWF=[ 0] (cms), LOSS=[ 1]:
3445 Horton: Fo=[ 76.20] (mm/ hr), Fc=[ 13.20] (mm/ hr), DCAY=[ 4.14] (/ hr),
3446 F=[ 0.00] (mm),
3447 Pervious areas: IAper=[ 4.67] (mm), SLPP=[ 2.0] (%), LGP=[ 40] (m),
3448 MNP=[ 0.250], SCP=[ 0] (min),
3449 Impervious areas: IAimp=[ 1.57] (mm), SLPI=[ 1.0] (%),
3450 LGI=[ 327.109] (m), MNI=[ 0.013], SCI=[ 0] (min),
3451 Continuous simulation parameters:
3452 IARECper=[ 4] (hrs), IARECimp=[ 4] (hrs), InterEventTime=[ 12] (hrs),
3453 END=- 1
3454 *%-----|-----|
3455 COMPUTE DUALHYD NHYDin=["FC- 02"], CINLET=[ 1.159] (cms), NINLET=[ 1],
3456 MajNHYD=["FC- 02- M"]
3457 MnNHYD=["FC- 02- MN"]
3458 TMS TO=[ 2385] (cu- m)
3459 *%-----|-----|
3460 ADD HYD NHYDs um=["FC- 02- S"], NHYDs to add=["FC- 02- M"+"FC- 02- MN"]
3461 *%-----|-----|

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3451 CONTINUOUS STANDHYD NHYD=[ "FC- 03" ], DT=[ 1 ] mi n, AREA=[ 7. 37 ] ( ha ), XI MP=[ 0. 64 ],
TI MP=[ 0. 64 ], DWF=[ 0 ] ( cms ), LOSS=[ 1 ] :
3452 Horton: Fo=[ 76. 20 ] ( mm/ hr ), Fc=[ 13. 20 ] ( mm/ hr ), DCAY=[ 4. 14 ] ( / hr ),
F=[ 0. 00 ] ( mm ),
3453 Pervious areas: IAper=[ 4. 67 ] ( mm ), SLPP=[ 2. 0 ] ( % ), LGP=[ 40 ] ( m ),
MNP=[ 0. 250 ], SCP=[ 0 ] ( mi n ),
3454 Impervious areas: IAi mp=[ 1. 57 ] ( mm ), SLPI =[ 1. 0 ] ( % ),
LGI =[ 221. 660 ] ( m ), MNI =[ 0. 013 ], SCI =[ 0 ] ( mi n ),
3455 Continuous simulation parameters:
3456 IaRECper=[ 4 ] ( hrs ), IaRECI mp=[ 4 ] ( hrs ), Inter Event Time=[ 12 ] ( hrs ),
END=- 1
3457 *%-----|
3458 COMPUTE DUALHYD NHYDi n=[ "FC- 03" ], CI NLET=[ 0. 358 ] ( cms ), NI NLET=[ 1 ],
3459 MAj NHYD=[ "FC- 03- M" ]
3460 M nNHYD=[ "FC- 03- MN" ]
3461 TM STO=[ 1131 ] ( cu- m )
3462 *%-----|
3463 ADD HYD NHYDsum=[ "FC- 03- S" ], NHYDs to add=[ "FC- 03- M" +"FC- 03- MN" ]
3464 *%-----|
3465 CONTINUOUS STANDHYD NHYD=[ "FC- 04" ], DT=[ 1 ] mi n, AREA=[ 12. 87 ] ( ha ), XI MP=[ 0. 64 ],
TI MP=[ 0. 64 ], DWF=[ 0 ] ( cms ), LOSS=[ 1 ] :
3466 Horton: Fo=[ 76. 20 ] ( mm/ hr ), Fc=[ 13. 20 ] ( mm/ hr ), DCAY=[ 4. 14 ] ( / hr ),
F=[ 0. 00 ] ( mm ),
3467 Pervious areas: IAper=[ 4. 67 ] ( mm ), SLPP=[ 2. 0 ] ( % ), LGP=[ 40 ] ( m ),
MNP=[ 0. 250 ], SCP=[ 0 ] ( mi n ),
3468 Impervious areas: IAi mp=[ 1. 57 ] ( mm ), SLPI =[ 1. 0 ] ( % ),
LGI =[ 292. 916 ] ( m ), MNI =[ 0. 013 ], SCI =[ 0 ] ( mi n ),
3469 Continuous simulation parameters:
3470 IaRECper=[ 4 ] ( hrs ), IaRECI mp=[ 4 ] ( hrs ), Inter Event Time=[ 12 ] ( hrs ),
END=- 1
3471 *%-----|
3472 COMPUTE DUALHYD NHYDi n=[ "FC- 04" ], CI NLET=[ 0. 741 ] ( cms ), NI NLET=[ 1 ],
3473 MAj NHYD=[ "FC- 04- M" ]
3474 M nNHYD=[ "FC- 04- MN" ]
3475 TM STO=[ 1794 ] ( cu- m )
3476 *%-----|
3477 ADD HYD NHYDsum=[ "FC- 04- S" ], NHYDs to add=[ "FC- 04- M" +"FC- 04- MN" ]
3478 *%-----|
3479 *#*****
3480 *# PROPOSED Subcatchments ( Kennedy- Burnett SWM Facility ( 118080 ), SWM Mdeling
Approach, NOVATECH Report June, 2020)
3481 *# - TO JOCK RI VER
3482 *#*****
3483 CONTINUOUS STANDHYD NHYD=[ "JR- 01" ], DT=[ 1 ] mi n, AREA=[ 8. 24 ] ( ha ), XI MP=[ 0. 64 ],
TI MP=[ 0. 64 ], DWF=[ 0 ] ( cms ), LOSS=[ 1 ] :
3484 Horton: Fo=[ 76. 20 ] ( mm/ hr ), Fc=[ 13. 20 ] ( mm/ hr ), DCAY=[ 4. 14 ] ( / hr ),
F=[ 0. 00 ] ( mm ),
3485 Pervious areas: IAper=[ 4. 67 ] ( mm ), SLPP=[ 2. 0 ] ( % ), LGP=[ 40 ] ( m ),
MNP=[ 0. 250 ], SCP=[ 0 ] ( mi n ),
3486 Impervious areas: IAi mp=[ 1. 57 ] ( mm ), SLPI =[ 1. 0 ] ( % ),
LGI =[ 234. 379 ] ( m ), MNI =[ 0. 013 ], SCI =[ 0 ] ( mi n ),
3487 Continuous simulation parameters:
3488 IaRECper=[ 4 ] ( hrs ), IaRECI mp=[ 4 ] ( hrs ), Inter Event Time=[ 12 ] ( hrs ),
END=- 1
3489 *%-----|
3490 COMPUTE DUALHYD NHYDi n=[ "JR- 01" ], CI NLET=[ 0. 563 ] ( cms ), NI NLET=[ 1 ],
3491 MAj NHYD=[ "JR- 01- M" ]
3492 M nNHYD=[ "JR- 01- MN" ]
3493 TM STO=[ 1040 ] ( cu- m )
3494 *%-----|
3495 ADD HYD NHYDsum=[ "JR- 01- S" ], NHYDs to add=[ "JR- 01- M" +"JR- 01- MN" ]
3496 *%-----|
3497 CONTINUOUS STANDHYD NHYD=[ "JR- 02" ], DT=[ 1 ] mi n, AREA=[ 1. 59 ] ( ha ), XI MP=[ 0. 64 ],
TI MP=[ 0. 64 ], DWF=[ 0 ] ( cms ), LOSS=[ 1 ] :
3498 Horton: Fo=[ 76. 20 ] ( mm/ hr ), Fc=[ 13. 20 ] ( mm/ hr ), DCAY=[ 4. 14 ] ( / hr ),
F=[ 0. 00 ] ( mm ),

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3499          Pervious areas: I A per=[ 4. 67]( mm), SLPP=[ 2. 0]( %), LGP=[ 40]( m),
3500          MNP=[ 0. 250], SCP=[ 0]( mi n),
3501          Impervious areas: I A imp=[ 1. 57]( mm), SLPI=[ 1. 0]( %),
3502          LGI=[ 102. 956]( m), MNI=[ 0. 013], SCI=[ 0]( mi n),
3503          Continuous simulation parameters:
3504          I a RE C per=[ 4]( hrs), I a RE C imp=[ 4]( hrs), I nter Event Ti me=[ 12]( hrs),
3505          END=- 1
3506
3507 *%-----|-----|
3508 COMPUTE DUALHYD NHYD i n=[ "J R- 02"], CI NLET=[ 0. 153]( c ms), NI NLET=[ 1],
3509          M i j NHYD=[ "J R- 02- M"],
3510          M nNHYD=[ "J R- 02- M N"],
3511          T M S TO=[ 153]( cu- m)
3512
3513 *%-----|-----|
3514 ADD HYD          NHYD s um=[ "J R- 02- S"], NHYD s t o a dd=[ "J R- 02- M"+"J R- 02- M N"]
3515
3516 *%-----|-----|
3517 *#*****|*****|
3518 *# Catchment FRASER
3519 *# - To Fraser-Clarke drain (north of the Jock)
3520 *# - Developed land with assumed 43% imp.
3521 *# - 2020-12-17 Change Fraser area to be 35.1 as measured from QGIS
3522 *# - 2020-12-17 All Fraser is undeveloped (Nashyd)
3523 *#*****|*****|
3524 CONTINUOUS NASHYD NHYD=[ "FRASER- DRN"], DT=[ 1] mi n, AREA=[ 13. 65]( ha),
3525          DWF=[ 0]( c ms), CN C=[ 77], I A=[ 4. 67]( mm),
3526          N=[ 3], TP=[ 0. 4258] hr s,
3527          Continuous simulation parameters:
3528          I a RE C per=[ 4]( hrs),
3529          SM N=[ - 1]( mm), SMAX=[ - 1]( mm), SK=[ 0. 010]/( mm),
3530          I nter Event Ti me=[ 12]( hrs)
3531          Baseflow simulation parameters:
3532          BaseFl owOpt ion=[ 1],
3533          I n i t GWR es Vol=[ 50]( mm), GWR es K=[ 0. 96]( mm/ day/ mm)
3534          VHyd Cond=[ 0. 055]( mm/ hr), END=- 1
3535
3536 *
3537 CONTINUOUS STANDHYD NHYD=[ "FRASER- D"], DT=[ 1] mi n, AREA=[ 21. 61]( ha),
3538          XI MP=[ 0. 585], TI MP=[ 0. 585], DWF=[ 0]( c ms), LOSS=[ 2],
3539          SCS curve number CN=[ 80],
3540          Pervious surfaces: I A per=[ 4. 67]( mm), SLPP=[ 1]( %),
3541          LGP=[ 40]( m), MNP=[ 0. 25], SCP=[ 0]( mi n),
3542          Impervious surfaces: I A imp=[ 1. 57]( mm), SLPI=[ 1]( %),
3543          LGI=[ 379. 561]( m), MNI=[ 0. 013], SCI=[ 0]( mi n),
3544          Continuous simulation parameters:
3545          I a RE C per=[ 4]( hrs), I a RE C imp=[ 4]( hrs),
3546          SM N=[ - 1]( mm), SMAX=[ - 1]( mm), SK=[ 0. 010]/( mm),
3547          I nter Event Ti me=[ 18]( hrs), END=- 1
3548
3549 *%-----|-----|
3550 COMPUTE DUALHYD NHYD i n=[ "FRASER- D"], CI NLET=[ 2. 281]( c ms), NI NLET=[ 1],
3551          M i j NHYD=[ "FRASER- J"],
3552          M nNHYD=[ "FRASER- N"],
3553          T M S TO=[ 9999999]( cu- m)
3554
3555 *%-----|-----|
3556 ADD HYD          NHYD s um=[ "FRASER- S"], NHYD s t o a dd=[ "FRASER- J"+"FRASER- N"]
3557
3558 *%-----|-----|
3559 *ROUTE RESERVOIR NHYDout=[ "MS_P20"], NHYD i n=[ "FRASER"],
3560          *
3561          RDT=[ 1]( mi n),
3562          *
3563          TABLE of ( OUTFLOW STORAGE ) values
3564          *
3565          ( c ms) - ( ha- m)
3566          *
3567          [ 0. 0, 0. 0 ]
3568          *
3569          [ 0. 04, 0. 36]
3570          *
3571          [ - 1, - 1 ] (max twenty pts)
3572          *
3573          NHYDovf=[ "P20- OVF"]
3574
3575 *%-----|-----|
3576 ADD HYD          NHYD s um=[ "4241"], NHYD s t o
3577          add=[ "KB- Pond3"+"S- 1- B"+"FRASER- DRN"+"FRASER- S"+"N_KB"+"FC- 01- S"+"FC- 02- S"+"FC- 03- S"]
3578
3579 *%-----|-----|
3580 SAVE HYD          NHYD=[ "4241"], # OF PCYCLES=[ - 1], I CASEs h=[ 1]

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3561 HYD_COMMENT=[ "Total Flows at Ken-Burnett Outlet" ]
3562 *%-----|-----|
3563 *# Hydrograph from Node Ken-Burnett to station 3633
3564 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 4241
3565 *#
3566 ROUTE CHANNEL NHYDout=[ "4241-out" ], NHYDin=[ "4241" ], RDT=[ 1 ](min),
3567 CHLGTH=[ 294 ](m), CHSLOPE=[ 0.1088 ]( % ), FPSLOPE=[ 0.1088 ]( % ),
3568 SECNUM=[ 1.0 ], NSEG=[ 3 ]
3569 ( SEGROUGH, SEGDI ST (m) )=[ 0.05, -20.12
3570 -0.035, 45.26
3571 0.05, 403.84 ] NSEG times
3572 ( DISTANCE (m), ELEVATION (m) )=[ ]
3573 [-909.72, 95 ]
3574 [-907.09, 94.5 ]
3575 [-904.65, 94 ]
3576 [-902.26, 93.5 ]
3577 [-44.51, 91.5 ]
3578 [-25.1, 91.5 ]
3579 [-20.98, 91 ]
3580 [-20.61, 90.5 ]
3581 [-20.12, 90 ]
3582 [-6.13, 87.26 ]
3583 [17.51, 86.56 ]
3584 [31.37, 87.2 ]
3585 [45.26, 90 ]
3586 [50.41, 90.5 ]
3587 [63.06, 91 ]
3588 [134.5, 91.5 ]
3589 [190.63, 92 ]
3590 [251.98, 92.5 ]
3591 [321.32, 93.5 ]
3592 [403.84, 95 ]
3593 *%-----|-----|
3594 ADD HYD NHYDsum=[ "SN_KB" ], NHYDs to
3595 add=[ "4241-out"+"FC-04-S"+"JR-01-S"+"JR-02-S" ]
3596 *%-----|-----|
3597 SAVE HYD NHYD=[ "SN_KB" ], # OF PCYCLES=[ -1 ], ICASEsh=[ 1 ]
3598 HYD_COMMENT=[ "Total Flows before Station 3633" ]
3599 *%-----|-----|
3600 *# Hydrograph from Station 3633 to Node Todd
3601 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 3633
3602 *# JFSA 2021-02-26 change the channel length (at station 3633) from 650m to 608m and
3603 *# change the slope from 0.0498% to 0.24671% That is because of adding station 4241
3604 *# between station 4534 and station 3633
3605 *#
3606 ROUTE CHANNEL NHYDout=[ "N_TO" ], NHYDin=[ "SN_KB" ], RDT=[ 1 ](min),
3607 CHLGTH=[ 608 ](m), CHSLOPE=[ 0.24671 ]( % ), FPSLOPE=[ 0.24671 ]( % ),
3608 SECNUM=[ 1.0 ], NSEG=[ 3 ]
3609 ( SEGROUGH, SEGDI ST (m) )=[ 0.05, -23.74
3610 -0.035, 23.74
3611 0.05, 26.50 ] NSEG times
3612 ( DISTANCE (m), ELEVATION (m) )=[ ]
3613 [-29.24, 91.0 ]
3614 [-27.41, 90.5 ]
3615 [-25.64, 90 ]
3616 [-23.74, 89.5 ]
3617 [-22, 89.26 ]
3618 [-20, 88.51 ]
3619 [-19, 88.32 ]
3620 [-15, 88.1 ]
3621 [-10, 88.11 ]
3622 [-5, 88.17 ]
3623 0, 88.27 ]
3624 5, 88.19 ]
3625 10, 88.06 ]
3626 15, 88.48 ]

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3624      16, 88.7
3625      23.74, 89.5
3626      24.68, 90
3627      25.57, 90.5
3628      26.50, 91.0
3629      *          [-29.24, 91]
3630      *          [-27.41, 90.5]
3631      *          [-25.64, 90]
3632      *          [-23.74, 89.5]
3633      *          [-22, 89.26]
3634      *          [-20, 88.51]
3635      *          [-19, 88.32]
3636      *          [-15, 88.1]
3637      *          [-10, 88.11]
3638      *          [-5, 88.17]
3639      *          [0, 88.27]
3640      *          [5, 88.19]
3641      *          [10, 88.06]
3642      *          [15, 88.48]
3643      *          [16, 88.7]
3644      *          [23.74, 89.5]
3645      *          [24.68, 90]
3646      *          [25.57, 90.5]
3647      *%-----|-----|
3648      *#*****|*****|
3649      *#      Catchment Greenbank
3650      *#      - To Greenbank Drain (south of the Jock)
3651      *#      - JFSA 2021-01-18 add Greenbank pond as per JFSA, P598(06)-15, June 2016
3652      *#      - JFSA 2021-01-19 update area from 37.479 ha to 36.6 ha based on GIS measurements
3653      *#*****|*****|
3654      CONTINUOUS STANDHYD NHYD=["Greenbank"], DT=[1] min, AREA=[36.6](ha),
3655      XI MP=[0.639], TI MP=[0.682], DWF=[0](cms), LOSS=[2],
3656      SCS curve number CN=[77],
3657      Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
3658      LGP=[40](m), MNP=[0.25], SCP=[0](min),
3659      Impervious surfaces: I A i mp=[1.57](mm), SLPI=[1](%),
3660      LGI=[493.96](m), MNI=[0.013], SCI=[0](min),
3661      Continuous simulation parameters:
3662      I a REC per=[4](hrs), I a REC i mp=[4](hrs),
3663      SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3664      I n t e r E v e n t T i m e=[18](hrs), E N D=-1
3665      *%-----|-----|
3666      ROUTE RESERVOIR NHYDout=["GreenB_MN"], NHYDin=["Greenbank"],
3667      RDT=[1](min),
3668      TABLE of ( OUTFLOW STORAGE ) values
3669      ( cms ) - ( ha - m )
3670      [ 0.0 , 0.0 ]
3671      [ 0.033 , 0.084 ]
3672      [ 0.039 , 0.201 ]
3673      [ 0.113 , 0.292 ]
3674      [ 0.237 , 0.386 ]
3675      [ 0.382 , 0.484 ]
3676      [ 0.539 , 0.585 ]
3677      [ 0.7 , 0.692 ]
3678      [ 0.86 , 0.804 ]
3679      [ 4.684 , 0.922 ]
3680      [ 11.539 , 1.052 ]
3681      [ 20.867 , 1.168 ]
3682      [ 103.616 , 1.974 ]
3683      [ -1 , -1 ] (max twenty pts)
3684      NHYDovf=["GreenB_M"],
3685      *%-----|-----|
3686      *%-----|-----|
3687      ADD HYD NHYDsum=["GreenB"], NHYDs to add=["N_TO"+"GreenB_M"+"GreenB_MN"]
3688      *%-----|-----|
3689      SAVE HYD NHYD=["GreenB"], # OF PCYCLES=[-1], I CASES h=[1]

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3690 HYD_COMMENT=["Total Flows at Greenbank Drain"]
3691 *%-----|-----|
3692 *#*****|
3693 *# Catchment TODD
3694 *# - To Todd Drain (south of the Jock)
3695 *# - Subdivision with 43% imp. as per Barrhaven South M&S
3696 *# - 2020-11-30 increase imp. based on P598(04)-11
3697 *# - 2020-11-30 update TODD Tributary Drainage Area to = 146.015 ha based on
P598(04)-11
3698 *# - 2020-11-30 split TODD Drainage Area to MAJOR, MINOR, POND and ALL
3699 *#*****|
3700 *# - JFSA 2021-01-19 add "TODD_MN1" as part of Clarke("W_CLAR_M") and remove it
from Todd
3701 *CONTINUOUS STANDHYD NHYD=["TODD_MN1"], DT=[1] min, AREA=[1.772](ha),
3702 * XI MP=[0.53], TI MP=[0.57], DWF=[0](cms), LOSS=[2],
3703 * SCS curve number CN=[77],
3704 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3705 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3706 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3707 * LGI=[108.689](m), MNI=[0.013], SCI=[0](min),
3708 * Continuous simulation parameters:
3709 * IaRECper=[4](hrs), IaRECImp=[4](hrs),
3710 * SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3711 * InterEventTime=[18](hrs), END=-1
3712 *%-----|-----|
3713 CONTINUOUS STANDHYD NHYD=["TODD_MN2"], DT=[1] min, AREA=[2.1](ha),
3714 * XI MP=[0.53], TI MP=[0.57], DWF=[0](cms), LOSS=[2],
3715 * SCS curve number CN=[77],
3716 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3717 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3718 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3719 * LGI=[118.322](m), MNI=[0.013], SCI=[0](min),
3720 * Continuous simulation parameters:
3721 * IaRECper=[4](hrs), IaRECImp=[4](hrs),
3722 * SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3723 * InterEventTime=[18](hrs), END=-1
3724 *%-----|-----|
3725 CONTINUOUS STANDHYD NHYD=["TODD_MN3"], DT=[1] min, AREA=[0.117](ha),
3726 * XI MP=[0.53], TI MP=[0.57], DWF=[0](cms), LOSS=[2],
3727 * SCS curve number CN=[77],
3728 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3729 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3730 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3731 * LGI=[27.928](m), MNI=[0.013], SCI=[0](min),
3732 * Continuous simulation parameters:
3733 * IaRECper=[4](hrs), IaRECImp=[4](hrs),
3734 * SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3735 * InterEventTime=[18](hrs), END=-1
3736 *%-----|-----|
3737 CONTINUOUS STANDHYD NHYD=["TODD_M"], DT=[1] min, AREA=[30.230](ha),
3738 * XI MP=[0.52], TI MP=[0.64], DWF=[0](cms), LOSS=[2],
3739 * SCS curve number CN=[77],
3740 * Pervious surfaces: IAper=[4.67](mm), SLPP=[1](%),
3741 * LGP=[40](m), MNP=[0.25], SCP=[0](min),
3742 * Impervious surfaces: IAimp=[1.57](mm), SLPI=[1](%),
3743 * LGI=[448.925](m), MNI=[0.013], SCI=[0](min),
3744 * Continuous simulation parameters:
3745 * IaRECper=[4](hrs), IaRECImp=[4](hrs),
3746 * SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
3747 * InterEventTime=[18](hrs), END=-1
3748 *%-----|-----|
3749 * -JFSA, 2021-01-19 update "TODD_ALL" area from 108.741 ha to 112.908 ha based on
GIS measurements (148.41-30.23-0.117-2.1-3.055=112.908 ha)
3750 CONTINUOUS STANDHYD NHYD=["TODD_ALL"], DT=[1] min, AREA=[112.908](ha),
3751 * XI MP=[0.52], TI MP=[0.57], DWF=[0](cms), LOSS=[2],
3752 * SCS curve number CN=[77],

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3753          Pervious surfaces: I A per=[ 4. 67] (mm), SLPP=[ 1] (%),
3754                    LGP=[ 40] (m), MNP=[ 0. 25], SCP=[ 0] (mi n),
3755          Impervious surfaces: I A i mp=[ 1. 57] (mm), SLPI =[ 1] (%),
3756                    LGI =[ 867. 594] (m), MNI =[ 0. 013], SCI =[ 0] (mi n),
3757          Continuous simulation parameters:
3758          I a REC per=[ 4] (hrs), I a REC i mp=[ 4] (hrs),
3759          SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
3760          Inter Event Ti me=[ 18] (hrs), END=- 1
3761          *%-----|-----|
3762          CONTINUOUS STANDHYD NHYD=[ "TODD_P" ], DT=[ 1] mi n, AREA=[ 3. 055] (ha),
3763          XI MP=[ 0. 63], TI MP=[ 0. 63], DWF=[ 0] (cms), LOSS=[ 2],
3764          SCS curve number CN=[ 77],
3765          Pervious surfaces: I A per=[ 4. 67] (mm), SLPP=[ 1] (%),
3766                    LGP=[ 40] (m), MNP=[ 0. 25], SCP=[ 0] (mi n),
3767          Impervious surfaces: I A i mp=[ 1. 57] (mm), SLPI =[ 1] (%),
3768                    LGI =[ 142. 712] (m), MNI =[ 0. 013], SCI =[ 0] (mi n),
3769          Continuous simulation parameters:
3770          I a REC per=[ 4] (hrs), I a REC i mp=[ 4] (hrs),
3771          SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
3772          Inter Event Ti me=[ 18] (hrs), END=- 1
3773          *%-----|-----|
3774          *%-----|-----|
3775          * -JFSA 2021-02-23 "TODD_DEVL" is part of the Corrigan sub-catchment because it
          drains to Corrigan SWM as per geoOttawa.ca Feb. 2021. "TODD_DEVL" now is called "corr1"
          and its parameters remain the same.
3776          *CONTINUOUS STANDHYD NHYD=[ "TODD_DEVL" ], DT=[ 1] mi n, AREA=[ 15. 87] (ha),
3777          *          XI MP=[ 0. 63], TI MP=[ 0. 63], DWF=[ 0] (cms), LOSS=[ 2],
3778          *          SCS curve number CN=[ 77],
3779          *          Pervious surfaces: I A per=[ 4. 67] (mm), SLPP=[ 1] (%),
3780          *                    LGP=[ 40] (m), MNP=[ 0. 25], SCP=[ 0] (mi n),
3781          *          Impervious surfaces: I A i mp=[ 1. 57] (mm), SLPI =[ 1] (%),
3782          *                    LGI =[ 325. 27] (m), MNI =[ 0. 013], SCI =[ 0] (mi n),
3783          *          Continuous simulation parameters:
3784          *          I a REC per=[ 4] (hrs), I a REC i mp=[ 4] (hrs),
3785          *          SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
3786          *          Inter Event Ti me=[ 18] (hrs), END=- 1
3787          *%-----|-----|
3788          * -JFSA 2021-02-23 "TODD_UnD" is part of the Corrigan sub-catchment. "TODD_UnD" now
          is called "corr2" and its parameters remain the same.
3789          *CONTINUOUS NASHYD NHYD=[ "TODD_UnD" ], DT=[ 1] mi n, AREA=[ 12. 47] (ha),
3790          *          DWF=[ 0] (cms), CN C=[ 77], I A=[ 4. 67] (mm),
3791          *          N=[ 3], TP=[ 1. 10] hrs,
3792          *          Continuous simulation parameters:
3793          *          I a REC per=[ 4] (hrs),
3794          *          SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
3795          *          Inter Event Ti me=[ 12] (hrs)
3796          *          Baseflow simulation parameters:
3797          *          BaseFlowOption=[ 1] ,
3798          *          I n i t GWRes Vol =[ 50] (mm), GWRes K=[ 0. 96] (mm/ day/ mm)
3799          *          VHydCond=[ 0. 055] (mm/ hr), END=- 1
3800          *%-----|-----|
3801          *# 5- Year + 12% Capture
3802          *COMPUTE DUALHYD NHYD i n=[ "TODD_M" ], CI NLET=[ 3. 314] (cms), NI NLET=[ 1],
3803          *          M i j NHYD=[ "TODD_M j " ]
3804          *          M nNHYD=[ "TODD_M n" ]
3805          *          TM I STO=[ 0. 1] (cu- m)
3806          ROUTE RESERVOIR NHYDout =[ "TODD_M n" ], NHYD i n=[ "TODD_M" ] ,
3807          RDT=[ 1] (mi n),
3808          TABLE of ( OUTFLOW STORAGE ) values
3809          ( cms ) - ( ha- m)
3810          [ 0. 0 , 0. 0 ]
3811          [ 3. 314 , 0. 0001 ]
3812          [ - 1 , - 1 ] (max twenty pts)
3813          NHYDovf=[ "TODD_M j " ] ,
3814          *%-----|-----|
3815          *# 5- Year + 12% Capture

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3816 *COMPUTE DUALHYD      NHYDi n=[ " TODD_MN1" ], CI NLET=[ 0. 227 ]( c ms ) , NI NLET=[ 1 ] ,
3817 *                      Mij NHYD=[ " TODD_MN1j " ]
3818 *                      Mn NHYD=[ " TODD_MN1n " ]
3819 *                      TMSTO=[ 0. 1 ]( c u - m )
3820 *ROUTE RESERVOIR      NHYDout =[ " TODD_MN1n " ] , NHYDi n=[ " TODD_MN1 " ] ,
3821 *                      RDT=[ 1 ]( m i n ) ,
3822 *                      TABLE of ( OUTFLOW STORAGE ) values
3823 *                      ( c ms ) - ( ha - m )
3824 *                      [ 0. 0 , 0. 0 ]
3825 *                      [ 0. 227 , 0. 0001 ]
3826 *                      [ -1 , -1 ] (max twenty pts)
3827 *                      NHYDovf=[ " TODD_MN1j " ] ,
3828 *%-----|-----|
3829 *COMPUTE DUALHYD      NHYDi n=[ " TODD_MN2" ], CI NLET=[ 0. 268 ]( c ms ) , NI NLET=[ 1 ] ,
3830 *                      Mij NHYD=[ " TODD_MN2j " ]
3831 *                      Mn NHYD=[ " TODD_MN2n " ]
3832 *                      TMSTO=[ 0. 1 ]( c u - m )
3833 ROUTE RESERVOIR      NHYDout =[ " TODD_MN2n " ] , NHYDi n=[ " TODD_MN2 " ] ,
3834 *                      RDT=[ 1 ]( m i n ) ,
3835 *                      TABLE of ( OUTFLOW STORAGE ) values
3836 *                      ( c ms ) - ( ha - m )
3837 *                      [ 0. 0 , 0. 0 ]
3838 *                      [ 0. 268 , 0. 0001 ]
3839 *                      [ -1 , -1 ] (max twenty pts)
3840 *                      NHYDovf=[ " TODD_MN2j " ] ,
3841 *%-----|-----|
3842 *COMPUTE DUALHYD      NHYDi n=[ " TODD_MN3" ], CI NLET=[ 0. 016 ]( c ms ) , NI NLET=[ 1 ] ,
3843 *                      Mij NHYD=[ " TODD_MN3j " ]
3844 *                      Mn NHYD=[ " TODD_MN3n " ]
3845 *                      TMSTO=[ 0. 1 ]( c u - m )
3846 ROUTE RESERVOIR      NHYDout =[ " TODD_MN3n " ] , NHYDi n=[ " TODD_MN3 " ] ,
3847 *                      RDT=[ 1 ]( m i n ) ,
3848 *                      TABLE of ( OUTFLOW STORAGE ) values
3849 *                      ( c ms ) - ( ha - m )
3850 *                      [ 0. 0 , 0. 0 ]
3851 *                      [ 0. 016 , 0. 0001 ]
3852 *                      [ -1 , -1 ] (max twenty pts)
3853 *                      NHYDovf=[ " TODD_MN3j " ] ,
3854 *%-----|-----|
3855 * -JFSA 2021-01-19 move A2 from Corrigan sub-catchment to Todd sub-catchment so the
major system from A2 can be added to Todd
3856 CONTINUOUS STANDHYD  NHYD=[ " A2 " ], DT=[ 1 ] m i n , AREA=[ 25. 5 ]( ha ) ,
3857 *                      XI MP=[ 0. 42 ] , TI MP=[ 0. 52 ] , DWF=[ 0 ]( c ms ) , LOSS=[ 2 ] ,
3858 *                      SCS curve number CN=[ 75 ] ,
3859 *                      Pervious surfaces: IAper=[ 4. 67 ]( mm ) , SLPP=[ 1 ]( % ) ,
3860 *                      LGP=[ 40 ]( m ) , MNP=[ 0. 25 ] , SCP=[ 0 ]( m i n ) ,
3861 *                      Impervious surfaces: IAi mp=[ 1. 57 ]( mm ) , SLPI=[ 1 ]( % ) ,
3862 *                      LGL=[ 566 ]( m ) , MNI=[ 0. 013 ] , SCI=[ 0 ]( m i n ) ,
3863 *                      Continuous simulation parameters:
3864 *                      IaRECper=[ 4 ]( hr s ) , IaRECI mp=[ 4 ]( hr s ) ,
3865 *                      SMN=[ - 1 ]( mm ) , SMAX=[ - 1 ]( mm ) , SK=[ 0. 010 ] / ( mm ) ,
3866 *                      Inter Event Time=[ 18 ]( hr s ) , END=- 1
3867 *%-----|-----|
3868 COMPUTE DUALHYD      NHYDi n=[ " A2 " ], CI NLET=[ 1. 818 ]( c ms ) , NI NLET=[ 1 ] ,
3869 *                      Mij NHYD=[ " A2 - M " ]
3870 *                      Mn NHYD=[ " A2 - MN " ]
3871 *                      TMSTO=[ 924 ]( c u - m )
3872 *%-----|-----|
3873 ADD HYD              NHYDs um=[ " TODD " ] , NHYDs to
add=[ " TODD_MN2n " + " TODD_MN3n " + " TODD_Mij " + " TODD_P " + " TODD_ALL " + " WCLAR_Mn " ]
3874 *%-----|-----|
3875 SAVE HYD            NHYD=[ " TODD " ] , # OF PCYCLES=[ - 1 ] , I CASEs h=[ 1 ]
3876 *                      HYD_COMMENT=[ " Total Flows at Todd Drain " ]
3877 *%-----|-----|
3878 *#*****
3879 *#      Todd Pond 3

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3880  *# - Rating curve obtained from Barrhaven South M&S modeling
3881  *# - stantec 2007, Tributary Drainage Area to M&S Pond 3 = 193 ha
3882  *#*****
3883  ROUTE RESERVOIR      NHYDout=["MS_P3"],  NHYDIn=["TODD"],
3884                      RDT=[1](min),
3885                      TABLE of ( OUTFLOW STORAGE ) values
3886                      (cms) - (ha-m)
3887                      [ 0.0 , 0.0 ]
3888                      [ 0.014 , 0.155 ]
3889                      [ 0.048 , 0.394 ]
3890                      [ 0.061 , 0.56 ]
3891                      [ 0.08 , 0.909 ]
3892                      [ 0.088 , 1.089 ]
3893                      [ 0.109 , 1.652 ]
3894                      [ 0.118 , 1.952 ]
3895                      [ 0.122 , 2.099 ]
3896                      [ 1.972 , 2.269 ]
3897                      [ 9.135 , 2.598 ]
3898                      [ 15.608 , 2.826 ]
3899                      [ 19.256 , 2.942 ]
3900                      [ 27.282 , 3.181 ]
3901                      [ 40.957 , 3.55 ]
3902                      [ 56.372 , 3.929 ]
3903                      [ 73.349 , 4.317 ]
3904                      [ 85.469 , 4.579 ]
3905                      [ 104.771 , 4.977 ]
3906                      [ -1 , -1 ] (max twenty pts)
3907                      NHYDovf=["P3-OVF"]
3908  *%-----|-----|
3909  ADD HYD              NHYDsum=["SN_TO"], NHYDs to
add=["GreenB"+"MS_P3"+"P3-OVF"+"TODD_MN2j"+"A2-M"]
3910  *%-----|-----|
3911  SAVE HYD            NHYD=["SN_TO"], # OF PCYCLES=[-1], ICASEsh=[1]
3912                      HYD_COMMENT=["Total Flows at Todd Drain"]
3913  *%-----|-----|
3914  *#
3915  *# Hydrograph from Todd Drain routed to Corrigan Drain
3916  *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
3917  *# 2021-02-19 Change the slope from 0.033 % (as per Stantec Report 2007) to 0.05 % so
the model will be more stable and give reasonable results. It is justifiable as ROUTE
CHANNELS aren't well suited to really flat slopes.
3918  *
3919  ROUTE CHANNEL        NHYDout=["N_TO"], NHYDIn=["SN_TO"],
3920                      RDT=[1](min),
3921                      CHLGTH=[280](m),  CHSLOPE=[0.05](%),
3922                      FPSLOPE=[0.05](%),
3923                      SECNUM=[1.0],      NSEG=[3]
3924                      ( SEGROUGH, SEGDIST (m) )=
3925                      [ 0.075, -17.72
3926                      -0.045, 17.72
3927                      0.075, 80.62] NSEG times
3928                      ( DISTANCE (m), ELEVATION (m) )=
3929                      [-83.32, 90.00]
3930                      [-81.36, 89.50]
3931                      [-79.12, 89.00]
3932                      [-76.13, 88.50]
3933                      [-20.46, 88.00]
3934                      [-19.36, 87.50]
3935                      [-18.51, 87.00]
3936                      [-17.72, 86.50]
3937                      [-11.95, 85.24]
3938                      [-0.11, 85.12]
3939                      [11.49, 85.20]
3940                      [17.72, 86.50]
3941                      [19.74, 87.00]
3942                      [21.22, 87.50]

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3943 [ 22. 68,  88. 00]
3944 [ 24. 28,  88. 50]
3945 [ 26. 79,  89. 00]
3946 [ 71. 98,  90. 00]
3947 [ 80. 62,  90. 50]
3948 *%-----|-----|
3949 SAVE HYD      NHYD=[ "N_TO" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1]
3950              HYD_COMMENT=[ "Total inflows at Station 2462" ]
3951 *%-----|-----|
3952 *#*****|*****|
3953 *# Catchment CORRIG
3954 *# - To Corrigan Drain (south of the Jock)
3955 *# - Primarily Developed (medium density)
3956 *# - JFSA JAN 2021, add Corrigan subcatchments as per IBI, July 2008
3957 *#*****|*****|
3958 *ROUTE RESERVOIR NHYDout=[ "MS_P1" ], NHYDin=[ "CORRIG" ],
3959 *              RDT=[ 1 ](min),
3960 *              TABLE of ( OUTFLOW STORAGE ) values
3961 *                  (cms) - (ha-m)
3962 *                  [  0.0 ,  0.0 ]
3963 *                  [  0.06 , 0.58]
3964 *                  [  -1 ,  -1 ] (max twenty pts)
3965 *              NHYDovf=[ "P1-OVF" ]
3966 *%-----|-----|
3967 *ADD HYD      NHYDs um=[ "SN_CO" ], NHYDs to add=[ "N_TO"+"P1-OVF"+"MS_P1" ]
3968 *%-----|-----|
3969 *SAVE HYD      NHYD=[ "SN_CO" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1]
3970 *              HYD_COMMENT=[ "Total Flows at Corrigan Drain" ]
3971 *%-----|-----|
3972 * -JFSA 2021-02-23 "TODD_DEVL" is part of the Corrigan sub-catchment because it
drains to Corrigan SWM as per geoOttawa.ca Feb. 2021. "TODD_DEVL" now is called "corr1"
and its parameters remain the same.
3973 CONTINUOUS STANDHYD NHYD=[ "corr1" ], DT=[ 1 ]min, AREA=[ 15. 87 ](ha),
3974 XI MP=[ 0. 63 ], TI MP=[ 0. 63 ], DWF=[ 0 ](cms), LOSS=[ 2 ],
3975 SCS curve number CN=[ 77 ],
3976 Pervious surfaces: I A per=[ 4. 67 ](mm), SLPP=[ 1 ]( %),
3977 L GP=[ 40 ](m), MNP=[ 0. 25 ], SCP=[ 0 ](min),
3978 Impervious surfaces: I A i mp=[ 1. 57 ](mm), SLPI=[ 1 ]( %),
3979 L GI=[ 325. 27 ](m), MNI=[ 0. 013 ], SCI=[ 0 ](min),
3980 Continuous simulation parameters:
3981 I a REC per=[ 4 ](hrs), I a REC i mp=[ 4 ](hrs),
3982 S M N=[ - 1 ](mm), S M A X=[ - 1 ](mm), S K=[ 0. 010 ]/(mm),
3983 I n t e r E v e n t T i m e=[ 18 ](hrs), E N D=- 1
3984 *%-----|-----|
3985 * -JFSA 2021-02-23 add DUALHYD for "corr1". "corr1" DUALHYD Parameters are the
same as A2 DUALHYD Parameters because A2 is the nearest sub-catchment to "corr1".
3986 * At the same time, Corrigan Report, IBI group 2008 has no DUALHYD Parameters for
Al-Corrig
3987 COMPUTE DUALHYD NHYDin=[ "corr1" ], CI NLET=[ 1. 818 ](cms), NI NLET=[ 1 ],
3988 M a j N H Y D=[ "corr1-M" ]
3989 M n N H Y D=[ "corr1-MN" ]
3990 T M S T O=[ 924 ](cu-m)
3991 *%-----|-----|
3992 * -JFSA 2021-02-23 "TODD_UnD" is part of the Corrigan sub-catchment. "TODD_UnD" now
is called "corr2" and its parameters remain the same.
3993 CONTINUOUS NASHYD NHYD=[ "corr2" ], DT=[ 1 ]min, AREA=[ 12. 47 ](ha),
3994 DWF=[ 0 ](cms), CN C=[ 77 ], I A=[ 4. 67 ](mm),
3995 N=[ 3 ], TP=[ 1. 10 ]hrs,
3996 Continuous simulation parameters:
3997 I a REC per=[ 4 ](hrs),
3998 S M N=[ - 1 ](mm), S M A X=[ - 1 ](mm), S K=[ 0. 010 ]/(mm),
3999 I n t e r E v e n t T i m e=[ 12 ](hrs)
4000 Baseflow simulation parameters:
4001 B a s e F l o w O p t i o n=[ 1 ],
4002 I n i t G W R e s V o l=[ 50 ](mm), G W R e s K=[ 0. 96 ](mm/ day/ mm)
4003 V H y d C o n d=[ 0. 055 ](mm/ hr), E N D=- 1

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4004 *%-----|-----|
4005 * -JFSA 2021-01-19 change Al-Corrig to be developed as per geottawa website and
apply the parameters of A2, the nearest sub-catchment to Al-Corrig, LGI is calculated
based on Al-Corrig area
4006 * -JFSA 2021-01-19 update all Corrigan areas based on GIS measurements, and keep
LGI as it is from Corrigan Report, IBI Group, 2008 because LGI calculated is less than
LGI from the Corrigan Report
4007 CONTINUOUS STANDHYD NHYD=["Al-Corrig"], DT=[1] min, AREA=[15.75](ha),
4008 XI MP=[0.42], TI MP=[0.52], DWF=[0](cms), LOSS=[2],
4009 SCS curve number CN=[75],
4010 Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
4011 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4012 Impervious surfaces: I A i mp=[1.57](mm), SLPI=[1](%),
4013 LGI=[324.037](m), MNI=[0.013], SCI=[0](min),
4014 Continuous simulation parameters:
4015 I a REC per=[4](hrs), I a REC i mp=[4](hrs),
4016 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4017 Inter Event Time=[18](hrs), END=-1
4018 *
4019 * -JFSA 2021-01-25 add DUALHYD for Al-Corrig. Al-Corrig DUALHYD Parameters are the
same as A2 DUALHYD Parameters because A2 is the nearest sub-catchment to Al-Corrig.
4020 * At the same time, Corrigan Report, IBI group 2008 has no DUALHYD Parameters for
Al-Corrig
4021 COMPUTE DUALHYD NHYD i n=["Al-Corrig"], CI NLET=[1.818](cms), NI NLET=[1],
4022 M a j NHYD=["Al-M"]
4023 M n NHYD=["Al-MN"]
4024 TM STO=[924](cu-m)
4025 *%-----|-----|
4026 *CONTINUOUS NASHYD NHYD=["Al-Corrig"], DT=[1] min, AREA=[15.75](ha),
4027 * DWF=[0](cms), CN C=[66], I A=[2.5](mm),
4028 * N=[3.0], TP=[0.36] hrs,
4029 * Continuous simulation parameters:
4030 * I a REC per=[4](hrs),
4031 * SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4032 * Inter Event Time=[12](hrs)
4033 * Baseflow simulation parameters:
4034 * BaseFl owOpt ion=[1],
4035 * I ni t GWRes Vol =[50](mm), GWRes K=[0.96](mm/day/mm)
4036 * VHydCond=[0.055](mm/hr), END=-1
4037 *%-----|-----|
4038 CONTINUOUS NASHYD NHYD=["B1"], DT=[1] min, AREA=[2.77](ha),
4039 DWF=[0](cms), CN C=[56], I A=[2.5](mm),
4040 N=[3.0], TP=[0.23] hrs,
4041 Continuous simulation parameters:
4042 I a REC per=[4](hrs),
4043 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4044 Inter Event Time=[12](hrs)
4045 Baseflow simulation parameters:
4046 BaseFl owOpt ion=[1],
4047 I ni t GWRes Vol =[50](mm), GWRes K=[0.96](mm/day/mm)
4048 VHydCond=[0.055](mm/hr), END=-1
4049 *%-----|-----|
4050 CONTINUOUS STANDHYD NHYD=["A4"], DT=[1] min, AREA=[1.27](ha),
4051 XI MP=[0.65], TI MP=[0.65], DWF=[0](cms), LOSS=[2],
4052 SCS curve number CN=[75],
4053 Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
4054 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4055 Impervious surfaces: I A i mp=[1.57](mm), SLPI=[1](%),
4056 LGI=[253](m), MNI=[0.013], SCI=[0](min),
4057 Continuous simulation parameters:
4058 I a REC per=[4](hrs), I a REC i mp=[4](hrs),
4059 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4060 Inter Event Time=[18](hrs), END=-1
4061 *%-----|-----|
4062 COMPUTE DUALHYD NHYD i n=["A4"], CI NLET=[0.405](cms), NI NLET=[1],
4063 M a j NHYD=["A4-M"]

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4064 MnNHYP=[ " A4- MN" ]
4065 TMI STO=[ 68] ( cu- m)
4066 *%-----|-----|
4067 ADD HYD NHYPsum=[ " MHI 01" ], NHPDs to
add=[ " A1- M" + " A1- MN" + " corr 1- M" + " corr 1- MN" + " corr 2" + " B1" + " A4- MN" ]
4068 *%-----|-----|
4069 SAVE HYD NHPD=[ " MHI 01" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1 ]
4070 HYD_ COMMENT=[ " Tot al Fl ows at MHI 01" ]
4071 *%-----|-----|
4072 ROUTE PI PE PTYPE=[ 1] circ, NHPDout=[ " 101- 102" ], RNUMBER=[ 1. 0 ], PDI AM=[ 1050] ( mm ),
4073 PLNGTH=[ 368] ( m ), PROUGH=[ 0. 013 ], PSLOPE=[ 0. 0054] ( m/ m ),
NHPDin=[ " MHI 01" ], RDT=[ 1 ]
4074 *%-----|-----|
4075 * -JFSA 2021- 01- 19 move A2 from Corrigan sub- catchment to Todd sub- catchment so the
major system from A2 can be added to Todd
4076 *CONTINUOUS STANDHYD NHPD=[ " A2" ], DT=[ 1] mi n, AREA=[ 25. 5] ( ha ),
4077 * XI MP=[ 0. 42 ], TI MP=[ 0. 52 ], DWF=[ 0] ( cms ), LOSS=[ 2 ],
4078 * SCS curve number CN=[ 75 ],
4079 * Pervious surfaces: IAper=[ 4. 67] ( mm ), SLPP=[ 1] ( % ),
4080 * LGP=[ 40] ( m ), MNP=[ 0. 25 ], SCP=[ 0] ( mi n ),
4081 * ImperVIOUS surfaces: IAi mp=[ 1. 57] ( mm ), SLPI =[ 1] ( % ),
4082 * LGI =[ 566] ( m ), MNI =[ 0. 013 ], SCI =[ 0] ( mi n ),
4083 * Continuous simulation parameters:
4084 * IAReCper=[ 4] ( hrs ), IAReCi mp=[ 4] ( hrs ),
4085 * SMN=[ - 1] ( mm ), SMAX=[ - 1] ( mm ), SK=[ 0. 010] / ( mm ),
4086 * InterEvent Time=[ 18] ( hrs ), END=- 1
4087 *%-----|-----|
4088 *COMPUTE DUALHYD NHPDin=[ " A2" ], CINLET=[ 1. 818] ( cms ), NI NLET=[ 1 ],
4089 * Mj NHPD=[ " A2- M" ]
4090 * MnNHPD=[ " A2- MN" ]
4091 * TMI STO=[ 924] ( cu- m)
4092 *%-----|-----|
4093 ADD HYD NHPDsum=[ " MHI 02" ], NHPDs to add=[ " A2- MN" + " 101- 102" ]
4094 *%-----|-----|
4095 SAVE HYD NHPD=[ " MHI 02" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1 ]
4096 HYD_ COMMENT=[ " Tot al Fl ows at MHI 02" ]
4097 *%-----|-----|
4098 CONTINUOUS STANDHYD NHPD=[ " A5" ], DT=[ 1] mi n, AREA=[ 1. 6] ( ha ),
4099 * XI MP=[ 0. 71 ], TI MP=[ 0. 71 ], DWF=[ 0] ( cms ), LOSS=[ 2 ],
4100 * SCS curve number CN=[ 75 ],
4101 * Pervious surfaces: IAper=[ 4. 67] ( mm ), SLPP=[ 1] ( % ),
4102 * LGP=[ 40] ( m ), MNP=[ 0. 25 ], SCP=[ 0] ( mi n ),
4103 * ImperVIOUS surfaces: IAi mp=[ 1. 57] ( mm ), SLPI =[ 1] ( % ),
4104 * LGI =[ 300] ( m ), MNI =[ 0. 013 ], SCI =[ 0] ( mi n ),
4105 * Continuous simulation parameters:
4106 * IAReCper=[ 4] ( hrs ), IAReCi mp=[ 4] ( hrs ),
4107 * SMN=[ - 1] ( mm ), SMAX=[ - 1] ( mm ), SK=[ 0. 010] / ( mm ),
4108 * InterEvent Time=[ 18] ( hrs ), END=- 1
4109 *%-----|-----|
4110 ADD HYD NHPDsum=[ " A5T" ], NHPDs to add=[ " A4- M" + " A5" ]
4111 *%-----|-----|
4112 COMPUTE DUALHYD NHPDin=[ " A5T" ], CINLET=[ 0. 357] ( cms ), NI NLET=[ 1 ],
4113 * Mj NHPD=[ " A5- M" ]
4114 * MnNHPD=[ " A5- MN" ]
4115 * TMI STO=[ 60] ( cu- m)
4116 *%-----|-----|
4117 * -JFSA Jan. 2021, A3 is a part of Todd so it is removed
4118 * -JFSA Jan. 2021, " A2- M" added to " Todd"
4119 *CONTINUOUS STANDHYD NHPD=[ " A3" ], DT=[ 1] mi n, AREA=[ 18. 4] ( ha ),
4120 * XI MP=[ 0. 58 ], TI MP=[ 0. 65 ], DWF=[ 0] ( cms ), LOSS=[ 2 ],
4121 * SCS curve number CN=[ 75 ],
4122 * Pervious surfaces: IAper=[ 4. 67] ( mm ), SLPP=[ 1] ( % ),
4123 * LGP=[ 40] ( m ), MNP=[ 0. 25 ], SCP=[ 0] ( mi n ),
4124 * ImperVIOUS surfaces: IAi mp=[ 1. 57] ( mm ), SLPI =[ 1] ( % ),
4125 * LGI =[ 450] ( m ), MNI =[ 0. 013 ], SCI =[ 0] ( mi n ),
4126 * Continuous simulation parameters:

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4127 * IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
4128 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4129 * InterEventTime=[ 18](hrs), END=- 1
4130 *%-----|-----|
4131 *ADD HYD NHYDsum=[ "A3- A2M"], NHYDs to add=[ "A2- M"+"A3"]
4132 *%-----|-----|
4133 *COMPUTE DUALHYD NHYDin=[ "A3- A2M"], CILET=[ 2.208](cms), NILET=[ 1],
4134 * MjNHYD=[ "A3R- M"]
4135 * MnNHYD=[ "A3R- MN"]
4136 * TMSO=[ 908](cu-m)
4137 *%-----|-----|
4138 ROUTE PIPE PTYPE=[ 1]circ, NHYDout=[ "102- 103"], RNUMBER=[ 1.0], PDIAM=[ 1500](mm),
4139 PLNGTH=[ 504](m), PROUGH=[ 0.013], PSLOPE=[ 0.0028](m/m),
NHYDin=[ "MH102"], RDT=[ 1]
4140 *%-----|-----|
4141 ADD HYD NHYDsum=[ "MH103"], NHYDs to add=[ "102- 103"+"A5- MN"]
4142 *%-----|-----|
4143 SAVE HYD NHYD=[ "MH103"], # OF PCYCLES=[ -1], ICASEsh=[ 1]
4144 HYD_COMMENT=[ "Total Flows at MH103"]
4145 *%-----|-----|
4146 ROUTE PIPE PTYPE=[ 1]circ, NHYDout=[ "103- 104"], RNUMBER=[ 1.0], PDIAM=[ 1650](mm),
4147 PLNGTH=[ 438](m), PROUGH=[ 0.013], PSLOPE=[ 0.0046](m/m),
NHYDin=[ "MH103"], RDT=[ 1]
4148 *%-----|-----|
4149 CONTINUOUS STANDHYD NHYD=[ "A6"], DT=[ 1]min, AREA=[ 1.56](ha),
4150 XI MP=[ 0.71], TI MP=[ 0.71], DWF=[ 0](cms), LOSS=[ 2],
4151 SCS curve number CN=[ 75],
4152 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
4153 LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4154 Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 1](%),
4155 LGI=[ 280](m), MNI=[ 0.013], SCI=[ 0](min),
4156 Continuous simulation parameters:
4157 IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
4158 SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4159 InterEventTime=[ 18](hrs), END=- 1
4160 *%-----|-----|
4161 ADD HYD NHYDsum=[ "A6T"], NHYDs to add=[ "A5- M"+"A6"]
4162 *%-----|-----|
4163 COMPUTE DUALHYD NHYDin=[ "A6T"], CILET=[ 0.357](cms), NILET=[ 1],
4164 MjNHYD=[ "A6- M"]
4165 MnNHYD=[ "A6- MN"]
4166 TMSO=[ 60](cu-m)
4167 *%-----|-----|
4168 * -JFSA Jan. 2021, A7-corrige is a part of Todd so it is removed
4169 *CONTINUOUS STANDHYD NHYD=[ "A7- corrige"], DT=[ 1]min, AREA=[ 11.8](ha),
4170 * XI MP=[ 0.41], TI MP=[ 0.54], DWF=[ 0](cms), LOSS=[ 2],
4171 * SCS curve number CN=[ 75],
4172 * Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
4173 * LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4174 * Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 1](%),
4175 * LGI=[ 438](m), MNI=[ 0.013], SCI=[ 0](min),
4176 * Continuous simulation parameters:
4177 * IaRECper=[ 4](hrs), IaRECImp=[ 4](hrs),
4178 * SMN=[ -1](mm), SMAX=[ -1](mm), SK=[ 0.010]/(mm),
4179 * InterEventTime=[ 18](hrs), END=- 1
4180 *%-----|-----|
4181 *ADD HYD NHYDsum=[ "A7- A3RM"], NHYDs to add=[ "A3R- M"+"A7- corrige"]
4182 *%-----|-----|
4183 *COMPUTE DUALHYD NHYDin=[ "A7- A3RM"], CILET=[ 1.003](cms), NILET=[ 1],
4184 * MjNHYD=[ "A7R- M"]
4185 * MnNHYD=[ "A7R- MN"]
4186 * TMSO=[ 496](cu-m)
4187 *%-----|-----|
4188 ADD HYD NHYDsum=[ "MH104"], NHYDs to add=[ "A6- MN"+"103- 104"+"TODD_Mn"]
4189 *%-----|-----|
4190 SAVE HYD NHYD=[ "MH104"], # OF PCYCLES=[ -1], ICASEsh=[ 1]

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4191 HYD_COMMENT=["Tot al Fl ows at MHI04"]
4192 *%-----|-----|
4193 CONTINUOUS STANDHYD NHYD=[" B2"], DT=[ 1] mi n, AREA=[ 12. 31] (ha),
4194 XI MP=[ 0. 41], TI MP=[ 0. 54], DWF=[ 0] (cms), LOSS=[ 2],
4195 SCS curve number CN=[ 75],
4196 Pervious surfaces: I A per=[ 4. 67] (mm), SLPP=[ 1] (%),
4197 LGP=[ 40] (m), MNP=[ 0. 25], SCP=[ 0] (mi n),
4198 Impervious surfaces: I A i mp=[ 1. 57] (mm), SLPI =[ 1] (%),
4199 LGI =[ 417] (m), MNI =[ 0. 013], SCI =[ 0] (mi n),
4200 Continuous simulation parameters:
4201 I a REC per=[ 4] (hr s), I a REC i mp=[ 4] (hr s),
4202 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
4203 I nter Event Ti me=[ 18] (hr s), END=- 1
4204 *%-----|-----|
4205 COMPUTE DUALHYD NHYD i n=[" B2"], CI NLET=[ 1. 029] (cms), NI NLET=[ 1],
4206 M a j NHYD=[" B2- M "]
4207 M n NHYD=[" B2- MN"]
4208 TM I STO=[ 508] (cu- m)
4209 *%-----|-----|
4210 ROUTE PI PE PTYPE=[ 1] circ, NHYDout=[" 315- 333"], RNUMBER=[ 1. 0], PDI AM=[ 1200] (mm),
4211 PLNGTH=[ 254] (m), PROUGH=[ 0. 013], PSLOPE=[ 0. 001] (m/ m),
NHYD i n=[" B2- MN"], RDT=[ 1]
4212 *%-----|-----|
4213 CONTINUOUS STANDHYD NHYD=[" B3"], DT=[ 1] mi n, AREA=[ 5. 59] (ha),
4214 XI MP=[ 0. 41], TI MP=[ 0. 54], DWF=[ 0] (cms), LOSS=[ 2],
4215 SCS curve number CN=[ 75],
4216 Pervious surfaces: I A per=[ 4. 67] (mm), SLPP=[ 1] (%),
4217 LGP=[ 40] (m), MNP=[ 0. 25], SCP=[ 0] (mi n),
4218 Impervious surfaces: I A i mp=[ 1. 57] (mm), SLPI =[ 1] (%),
4219 LGI =[ 345] (m), MNI =[ 0. 013], SCI =[ 0] (mi n),
4220 Continuous simulation parameters:
4221 I a REC per=[ 4] (hr s), I a REC i mp=[ 4] (hr s),
4222 SM N=[ - 1] (mm), SMAX=[ - 1] (mm), SK=[ 0. 010] / (mm),
4223 I nter Event Ti me=[ 18] (hr s), END=- 1
4224 *%-----|-----|
4225 COMPUTE DUALHYD NHYD i n=[" B3"], CI NLET=[ 0. 459] (cms), NI NLET=[ 1],
4226 M a j NHYD=[" B3- M "]
4227 M n NHYD=[" B3- MN"]
4228 TM I STO=[ 227] (cu- m)
4229 *%-----|-----|
4230 ADD HYD NHYDs um=[" MH333"], NHYDs to add=[" B3- MN" + " 315- 333"]
4231 *%-----|-----|
4232 SAVE HYD NHYD=[" MH333"], # OF PCYCLES=[ - 1], I CASEs h=[ 1]
4233 HYD_COMMENT=["Tot al Fl ows at MH333"]
4234 *%-----|-----|
4235 ROUTE PI PE PTYPE=[ 1] circ, NHYDout=[" 333- 335"], RNUMBER=[ 1. 0], PDI AM=[ 1200] (mm),
4236 PLNGTH=[ 251] (m), PROUGH=[ 0. 013], PSLOPE=[ 0. 001] (m/ m),
NHYD i n=[" MH333"], RDT=[ 1]
4237 *%-----|-----|
4238 ROUTE PI PE PTYPE=[ 1] circ, NHYDout=[" 335- 338"], RNUMBER=[ 1. 0], PDI AM=[ 1200] (mm),
4239 PLNGTH=[ 185] (m), PROUGH=[ 0. 013], PSLOPE=[ 0. 001] (m/ m),
NHYD i n=[" 333- 335"], RDT=[ 1]
4240 *%-----|-----|
4241 ROUTE PI PE PTYPE=[ 1] circ, NHYDout=[" 338- 340"], RNUMBER=[ 1. 0], PDI AM=[ 1350] (mm),
4242 PLNGTH=[ 233] (m), PROUGH=[ 0. 013], PSLOPE=[ 0. 001] (m/ m),
NHYD i n=[" 335- 338"], RDT=[ 1]
4243 *%-----|-----|
4244 CONTINUOUS STANDHYD NHYD=[" B4"], DT=[ 1] mi n, AREA=[ 7. 6] (ha),
4245 XI MP=[ 0. 41], TI MP=[ 0. 54], DWF=[ 0] (cms), LOSS=[ 2],
4246 SCS curve number CN=[ 75],
4247 Pervious surfaces: I A per=[ 4. 67] (mm), SLPP=[ 1] (%),
4248 LGP=[ 40] (m), MNP=[ 0. 25], SCP=[ 0] (mi n),
4249 Impervious surfaces: I A i mp=[ 1. 57] (mm), SLPI =[ 1] (%),
4250 LGI =[ 388] (m), MNI =[ 0. 013], SCI =[ 0] (mi n),
4251 Continuous simulation parameters:
4252 I a REC per=[ 4] (hr s), I a REC i mp=[ 4] (hr s),

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4253 SM N=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0. 010 ] / ( mm ) ,
4254 Inter Event Time=[ 18 ] ( hr s ) , END=- 1
4255 *%-----|-----|
4256 COMPUTE DUALHYD NHYDin=[ " B4 " ] , CI NLET=[ 0. 655 ] ( c ms ) , NI NLET=[ 1 ] ,
4257 Maj NHYD=[ " B4- M " ]
4258 MnNHYD=[ " B4- MN " ]
4259 TMJ STO=[ 323 ] ( cu- m )
4260 *%-----|-----|
4261 ADD HYD NHYDsum=[ " MH340 " ] , NHYDs to add=[ " 338- 340 " + " B4- MN " ]
4262 *%-----|-----|
4263 SAVE HYD NHYD=[ " MH340 " ] , # OF PCYCLES=[ - 1 ] , I CASEs h=[ 1 ]
4264 HYD_COMMENT=[ " Tot al Fl ows at MH340 " ]
4265 *%-----|-----|
4266 ROUTE PI PE PTYPE=[ 1 ] ci rc , NHYDout=[ " 340- 104 " ] , RNUMBER=[ 1. 0 ] , PDI AM=[ 1650 ] ( mm ) ,
4267 PLNGTH=[ 240 ] ( m ) , PROUGH=[ 0. 013 ] , PSLOPE=[ 0. 0015 ] ( m / m ) ,
NHYDin=[ " MH340 " ] , RDT=[ 1 ]
4268 *%-----|-----|
4269 ADD HYD NHYDsum=[ " MH104T " ] , NHYDs to add=[ " 340- 104 " + " MH104 " ]
4270 *%-----|-----|
4271 ROUTE PI PE PTYPE=[ 2 ] re ct , NHYDout=[ " 104- 105 " ] , RNUMBER=[ 1. 0 ] ,
PW DTH=[ 2400 ] ( mm ) by PHEI GHT=[ 2100 ] ( mm ) ,
4272 PLNGTH=[ 380 ] ( m ) , PROUGH=[ 0. 013 ] , PSLOPE=[ 0. 001 ] ( m / m ) ,
NHYDin=[ " MH104T " ] , RDT=[ 1 ]
4273 *%-----|-----|
4274 CONTINUOUS STANDHYD NHYD=[ " B5 " ] , DT=[ 1 ] mi n , AREA=[ 2. 2 ] ( ha ) ,
4275 XI MP=[ 0. 57 ] , TI MP=[ 0. 57 ] , DWF=[ 0 ] ( c ms ) , LOSS=[ 2 ] ,
4276 SCS curve number CN=[ 75 ] ,
4277 Pervious surfaces: IAper=[ 4. 67 ] ( mm ) , SLPP=[ 1 ] ( % ) ,
4278 LGP=[ 40 ] ( m ) , MNP=[ 0. 25 ] , SCP=[ 0 ] ( mi n ) ,
4279 Impervious surfaces: IAi mp=[ 1. 57 ] ( mm ) , SLPI = [ 1 ] ( % ) ,
4280 LGI = [ 187 ] ( m ) , MNI = [ 0. 013 ] , SCI = [ 0 ] ( mi n ) ,
4281 Continuous simulation parameters:
4282 IaRECper=[ 4 ] ( hr s ) , IaRECI mp=[ 4 ] ( hr s ) ,
4283 SM N=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0. 010 ] / ( mm ) ,
4284 Inter Event Time=[ 18 ] ( hr s ) , END=- 1
4285 *%-----|-----|
4286 COMPUTE DUALHYD NHYDin=[ " B5 " ] , CI NLET=[ 0. 260 ] ( c ms ) , NI NLET=[ 1 ] ,
4287 Maj NHYD=[ " B5- M " ]
4288 MnNHYD=[ " B5- MN " ]
4289 TMJ STO=[ 250 ] ( cu- m )
4290 *%-----|-----|
4291 CONTINUOUS STANDHYD NHYD=[ " A8 " ] , DT=[ 1 ] mi n , AREA=[ 0. 96 ] ( ha ) ,
4292 XI MP=[ 0. 71 ] , TI MP=[ 0. 71 ] , DWF=[ 0 ] ( c ms ) , LOSS=[ 2 ] ,
4293 SCS curve number CN=[ 75 ] ,
4294 Pervious surfaces: IAper=[ 4. 67 ] ( mm ) , SLPP=[ 1 ] ( % ) ,
4295 LGP=[ 40 ] ( m ) , MNP=[ 0. 25 ] , SCP=[ 0 ] ( mi n ) ,
4296 Impervious surfaces: IAi mp=[ 1. 57 ] ( mm ) , SLPI = [ 1 ] ( % ) ,
4297 LGI = [ 186 ] ( m ) , MNI = [ 0. 013 ] , SCI = [ 0 ] ( mi n ) ,
4298 Continuous simulation parameters:
4299 IaRECper=[ 4 ] ( hr s ) , IaRECI mp=[ 4 ] ( hr s ) ,
4300 SM N=[ - 1 ] ( mm ) , SMAX=[ - 1 ] ( mm ) , SK=[ 0. 010 ] / ( mm ) ,
4301 Inter Event Time=[ 18 ] ( hr s ) , END=- 1
4302 *%-----|-----|
4303 ADD HYD NHYDsum=[ " A8T " ] , NHYDs to add=[ " A6- M " + " A8 " ]
4304 *%-----|-----|
4305 COMPUTE DUALHYD NHYDin=[ " A8T " ] , CI NLET=[ 0. 238 ] ( c ms ) , NI NLET=[ 1 ] ,
4306 Maj NHYD=[ " A8- M " ]
4307 MnNHYD=[ " A8- MN " ]
4308 TMJ STO=[ 40 ] ( cu- m )
4309 *%-----|-----|
4310 ADD HYD NHYDsum=[ " MH105 " ] , NHYDs to
add=[ " 104- 105 " + " B5- MN " + " A8- MN " + " TODD_MN3j " ]
4311 *%-----|-----|
4312 SAVE HYD NHYD=[ " MH105 " ] , # OF PCYCLES=[ - 1 ] , I CASEs h=[ 1 ]
4313 HYD_COMMENT=[ " Tot al Fl ows at MH105 " ]

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4314 *%-----|
4315 DI VERT HYD      NHYDin=["A8-M"] NIDout=[2]max five,
4316                  outflow hydrographs (NHYDs)=["A8-M-JR" "A8-M-B6"]
4317                  flow distribution table: (modify as necessary)
4318                  Note: all flows are in (cms)
4319                  QIDi + QIDi = QTOTAL
4320                  [ 0 + 0 = 0 ]
4321                  [ 50 + 50 = 100 ] end
4322 *%-----|
4323 DI VERT HYD      NHYDin=["MHI05"] NIDout=[2]max five,
4324                  outflow hydrographs (NHYDs)=["MHI05-JR" "MHI05-B6"]
4325                  flow distribution table: (modify as necessary)
4326                  Note: all flows are in (cms)
4327                  QIDi + QIDi = QTOTAL
4328                  [ 0 + 0 = 0 ]
4329                  [ 0 + 3.0 = 3.0 ]
4330                  [ 96.9+ 3.1 = 100 ] end
4331 *%-----|
4332 CONTINUOUS STANDHYD NHYD=["B7"], DT=[1]min, AREA=[7.19](ha),
4333                  XI MP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4334                  SCS curve number CN=[75],
4335                  Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
4336                  LGP=[40](m), MNP=[0.25], SCP=[0](min),
4337                  Impervious surfaces: I A imp=[1.57](mm), SLPI=[1](%),
4338                  LGI=[211](m), MNI=[0.013], SCI=[0](min),
4339                  Continuous simulation parameters:
4340                  I a REC per=[4](hrs), I a REC imp=[4](hrs),
4341                  SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4342                  InterEvent Time=[18](hrs), END=-1
4343 *%-----|
4344 ADD HYD          NHYDs um=["B7-B4M"], NHYDs to add=["B4-M"+"B7"]
4345 *%-----|
4346 COMPUTE DUALHYD NHYDin=["B7-B4M"], CINLET=[0.629](cms), NINLET=[1],
4347                  Maj NHYD=["B7R-M"]
4348                  MinNHYD=["B7R-MN"]
4349                  TMS TO=[311](cu-m)
4350 *%-----|
4351 ROUTE PIPE      PTYPE=[1]circ, NHYDout=["360-106A"], RNUMBER=[1.0], PDI AM=[1050](mm),
4352                  PLNGTH=[167](m), PROUGH=[0.013], PSLOPE=[0.001](m/m),
4353                  NHYDin=["B7R-MN"], RDT=[1]
4354 *%-----|
4355 * -JFSA 2021-01-19 change B6 to be developed as per geottawa website and apply the
4356 parameters of A7, the nearest sub-catchment to B6, LGI is calculated based on B6 area
4357 CONTINUOUS STANDHYD NHYD=["B6"], DT=[1]min, AREA=[3.29](ha),
4358                  XI MP=[0.41], TIMP=[0.54], DWF=[0](cms), LOSS=[2],
4359                  SCS curve number CN=[75],
4360                  Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
4361                  LGP=[40](m), MNP=[0.25], SCP=[0](min),
4362                  Impervious surfaces: I A imp=[1.57](mm), SLPI=[1](%),
4363                  LGI=[148.099](m), MNI=[0.013], SCI=[0](min),
4364                  Continuous simulation parameters:
4365                  I a REC per=[4](hrs), I a REC imp=[4](hrs),
4366                  SMN=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4367                  InterEvent Time=[18](hrs), END=-1
4368 *%-----|
4369 * -JFSA 2021-01-25 add B1 DUALHYD as per Corrigan Report, IBI Group, 2008
4370 COMPUTE DUALHYD NHYDin=["B6"], CINLET=[0.064](cms), NINLET=[1],
4371                  Maj NHYD=["B6-M"]
4372                  MinNHYD=["B6-MN"]
4373                  TMS TO=[5484](cu-m)
4374 *%-----|
4375 *CONTINUOUS NASHYD NHYD=["B6"], DT=[1]min, AREA=[3.29](ha),
4376                  * DWF=[0](cms), CN/C=[75], IA=[2.5](mm),
4377                  * N=[3.0], TP=[0.36]hrs,

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4376 *          Continuous simulation parameters:
4377 *          IaRECper=[ 4](hrs),
4378 *          SMN=[- 1](mm),  SMAX=[- 1](mm),  SK=[ 0.010]/(mm),
4379 *          InterEventTime=[ 12](hrs)
4380 *          Baseflow simulation parameters:
4381 *          BaseFlowOption=[ 1] ,
4382 *          InitGWResVol=[ 50](mm),  GWResK=[ 0.96](mm/day/mm)
4383 *          VHydCond=[ 0.055](mm/hr),  END=- 1
4384 *%-----|-----
4385 *% -EX-LAND is external land. It is a part of JOCKVA sub-catchment as per Corrigan
Report, IBI Group, 2008
4386 CONTINUOUS STANDHYD NHYD=["EX-LAND"], DT=[ 1]min, AREA=[ 32.5](ha),
4387 XI MP=[ 0.50], TI MP=[ 0.50], DWF=[ 0](cms), LOSS=[ 2],
4388 SCS curve number CN=[ 74],
4389 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
4390 LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4391 Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 1](%),
4392 LGI=[ 465.475](m), MNI=[ 0.013], SCI=[ 0](min),
4393 Continuous simulation parameters:
4394 IaRECper=[ 4](hrs),  IaRECImp=[ 4](hrs),
4395 SMN=[- 1](mm),  SMAX=[- 1](mm),  SK=[ 0.010]/(mm),
4396 InterEventTime=[ 18](hrs),  END=- 1
4397 *%-----|-----
4398 COMPUTE DUALHYD NHYDin=["EX-LAND"], CINLET=[ 2.275](cms), NINLET=[ 1],
4399 MajNHYD=["EX-LAND-M"]
4400 MnNHYD=["EX-LAND-MN"]
4401 TMS TO=[ 1365](cu-m)
4402 *%-----|-----
4403 ADD HYD NHYDsum=["B6-B7ExM"], NHYDsto
add=["B7R-M"+"EX-LAND-M"+"B5-M"+"B6-M"+"B6-MN"+"A8-M-B6"]
4404 *%-----|-----
4405 COMPUTE DUALHYD NHYDin=["B6-B7ExM"], CINLET=[ 0.064](cms), NINLET=[ 1],
4406 MajNHYD=["B6R-M"]
4407 MnNHYD=["B6R-MN"]
4408 TMS TO=[ 5484](cu-m)
4409 *%-----|-----
4410 ROUTE PIPE PTYPE=[ 1]circ, NHYDout=["105-106A"], RNUMBER=[ 1.0], PDIAM=[ 1800](mm),
4411 PLNGTH=[ 208](m), PROUGH=[ 0.013], PSLOPE=[ 0.001](m/m),
NHYDin=["MH105-B6"], RDT=[ 1]
4412 *%-----|-----
4413 ADD HYD NHYDsum=["MH106A"], NHYDsto
add=["360-106A"+"105-106A"+"B6R-MN"+"B6R-M"]
4414 *%-----|-----
4415 SAVE HYD NHYD=["MH106A"], # OF PCYCLES=[- 1], ICASEsh=[ 1]
4416 HYD_COMMENT=["Total Flows at MH106A"]
4417 *%-----|-----
4418 *% -JFSA 2021-01-12 THE MANHOLE MH106 is called MH17/106 in Corrigan Report, IBI
Group, July 2008
4419 *%
4420 ROUTE PIPE PTYPE=[ 1]circ, NHYDout=["106A-106"], RNUMBER=[ 1.0], PDIAM=[ 1800](mm),
4421 PLNGTH=[ 190](m), PROUGH=[ 0.013], PSLOPE=[ 0.001](m/m),
NHYDin=["MH106A"], RDT=[ 1]
4422 *%-----|-----
4423 CONTINUOUS STANDHYD NHYD=["A9"], DT=[ 1]min, AREA=[ 2.44](ha),
4424 XI MP=[ 0.71], TI MP=[ 0.71], DWF=[ 0](cms), LOSS=[ 2],
4425 SCS curve number CN=[ 75],
4426 Pervious surfaces: IAper=[ 4.67](mm), SLPP=[ 1](%),
4427 LGP=[ 40](m), MNP=[ 0.25], SCP=[ 0](min),
4428 Impervious surfaces: IAimp=[ 1.57](mm), SLPI=[ 1](%),
4429 LGI=[ 262](m), MNI=[ 0.013], SCI=[ 0](min),
4430 Continuous simulation parameters:
4431 IaRECper=[ 4](hrs),  IaRECImp=[ 4](hrs),
4432 SMN=[- 1](mm),  SMAX=[- 1](mm),  SK=[ 0.010]/(mm),
4433 InterEventTime=[ 18](hrs),  END=- 1
4434 *%-----|-----
4435 COMPUTE DUALHYD NHYDin=["A9"], CINLET=[ 0.547](cms), NINLET=[ 1],

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4436      Mj NHYD=[ " A9- M " ]
4437      MnNHYD=[ " A9- MN" ]
4438      TM STO=[ 0 ] ( cu- m)
4439  *%-----|-----|
4440  ADD HYD      NHYDs um=[ " MHI06" ], NHYDs to add=[ " 106A- 106" + " A9- MN" ]
4441  *%-----|-----|
4442  SAVE HYD     NHYD=[ " MHI06" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1 ]
4443      HYD_ COMMENT=[ " Tot al Fl ows at MHI06" ]
4444  *%-----|-----|
4445  *%      -JFSA 2021-01-12 THE MANHOLE MHI07 is called MHI18/107 in Corrigan Report, IBI
Group, July 2008
4446  *%
4447  ROUTE PIPE   PTYPE=[ 1 ] circ, NHYDout=[ " 106- 107" ], RNUMBER=[ 1. 0 ], PDI AM=[ 1800 ] ( mm),
4448      PLNGTH=[ 122. 5 ] ( m), PROUGH=[ 0. 013 ], PSLOPE=[ 0. 001 ] ( m/ m),
      NHYDin=[ " MHI06" ], RDT=[ 1 ]
4449  *%-----|-----|
4450  CONTINUOUS STANDHYD NHYD=[ " A10" ], DT=[ 1 ] mi n, AREA=[ 4. 14 ] ( ha),
4451      XI MP=[ 0. 35 ], TI MP=[ 0. 47 ], DWF=[ 0 ] ( cms), LOSS=[ 2 ],
4452      SCS curve number CN=[ 75 ],
4453      Pervious surfaces: IAper=[ 4. 67 ] ( mm), SLPP=[ 1 ] ( %),
4454      LGP=[ 40 ] ( m), MNP=[ 0. 25 ], SCP=[ 0 ] ( mi n),
4455      Impervious surfaces: IAi mp=[ 1. 57 ] ( mm), SLPI=[ 1 ] ( %),
4456      LGI=[ 183 ] ( m), MNI=[ 0. 013 ], SCI=[ 0 ] ( mi n),
4457      Continuous simulation parameters:
4458      IaRECper=[ 4 ] ( hr s), IaRECI mp=[ 4 ] ( hr s),
4459      SMN=[ - 1 ] ( mm), SMAX=[ - 1 ] ( mm), SK=[ 0. 010 ] / ( mm),
4460      InterEvent Time=[ 18 ] ( hr s), END=- 1
4461  *%-----|-----|
4462  COMPUTE DUALHYD NHYDin=[ " A10" ], CI NLET=[ 0. 310 ] ( cms), NI NLET=[ 1 ],
4463      Mj NHYD=[ " A10- M " ]
4464      MnNHYD=[ " A10- MN" ]
4465      TM STO=[ 228 ] ( cu- m)
4466  *%-----|-----|
4467  CONTINUOUS STANDHYD NHYD=[ " A11" ], DT=[ 1 ] mi n, AREA=[ 10. 61 ] ( ha),
4468      XI MP=[ 0. 53 ], TI MP=[ 0. 62 ], DWF=[ 0 ] ( cms), LOSS=[ 2 ],
4469      SCS curve number CN=[ 75 ],
4470      Pervious surfaces: IAper=[ 4. 67 ] ( mm), SLPP=[ 1 ] ( %),
4471      LGP=[ 40 ] ( m), MNP=[ 0. 25 ], SCP=[ 0 ] ( mi n),
4472      Impervious surfaces: IAi mp=[ 1. 57 ] ( mm), SLPI=[ 1 ] ( %),
4473      LGI=[ 379 ] ( m), MNI=[ 0. 013 ], SCI=[ 0 ] ( mi n),
4474      Continuous simulation parameters:
4475      IaRECper=[ 4 ] ( hr s), IaRECI mp=[ 4 ] ( hr s),
4476      SMN=[ - 1 ] ( mm), SMAX=[ - 1 ] ( mm), SK=[ 0. 010 ] / ( mm),
4477      InterEvent Time=[ 18 ] ( hr s), END=- 1
4478  *%-----|-----|
4479  COMPUTE DUALHYD NHYDin=[ " A11" ], CI NLET=[ 0. 993 ] ( cms), NI NLET=[ 1 ],
4480      Mj NHYD=[ " A11- M " ]
4481      MnNHYD=[ " A11- MN" ]
4482      TM STO=[ 556 ] ( cu- m)
4483  *%-----|-----|
4484  ADD HYD      NHYDs um=[ " MHI07" ], NHYDs to add=[ " 106- 107" + " A10- MN" + " A11- MN" ]
4485  *%-----|-----|
4486  SAVE HYD     NHYD=[ " MHI07" ], # OF PCYCLES=[ - 1 ], I CASEs h=[ 1 ]
4487      HYD_ COMMENT=[ " Tot al Fl ows at MHI07" ]
4488  *%-----|-----|
4489  ROUTE PIPE   PTYPE=[ 1 ] circ, NHYDout=[ " 107- 119" ], RNUMBER=[ 1. 0 ], PDI AM=[ 1800 ] ( mm),
4490      PLNGTH=[ 114 ] ( m), PROUGH=[ 0. 013 ], PSLOPE=[ 0. 0012 ] ( m/ m),
      NHYDin=[ " MHI07" ], RDT=[ 1 ]
4491  *%-----|-----|
4492  *%      -JFSA 2021-01-12 THE MANHOLE MHI08 is called MHI20/108 in Corrigan Report, IBI
Group, July 2008
4493  *%
4494  ROUTE PIPE   PTYPE=[ 1 ] circ, NHYDout=[ " 119- 108" ], RNUMBER=[ 1. 0 ], PDI AM=[ 1800 ] ( mm),
4495      PLNGTH=[ 65. 8 ] ( m), PROUGH=[ 0. 013 ], PSLOPE=[ 0. 0012 ] ( m/ m),
      NHYDin=[ " 107- 119" ], RDT=[ 1 ]
4496  *%-----|-----|

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4497 CONTINUOUS STANDHYD NHYD=["A12"], DT=[1] min, AREA=[12.29] (ha),
 4498 XI MP=[0.41], TI MP=[0.54], DWF=[0] (cms), LOSS=[2],
 4499 SCS curve number CN=[75],
 4500 Pervious surfaces: I A per=[4.67] (mm), SLPP=[1] (%),
 4501 LGP=[40] (m), MNP=[0.25], SCP=[0] (min),
 4502 Impervious surfaces: I A i mp=[1.57] (mm), SLPI=[1] (%),
 4503 LGI=[183] (m), MNI=[0.013], SCI=[0] (min),
 4504 Continuous simulation parameters:
 4505 I a REC per=[4] (hrs), I a REC i mp=[4] (hrs),
 4506 SM N=[-1] (mm), SMAX=[-1] (mm), SK=[0.010] / (mm),
 4507 Inter Event Time=[18] (hrs), END=- 1
 4508 *%-----|
 4509 COMPUTE DUALHYD NHYD i n=["A12"], CI NLET=[1.029] (cms), NI NLET=[1],
 4510 M a j NHYD=["A12- M"]
 4511 M n NHYD=["A12- MN"]
 4512 TM STO=[672] (cu-m)
 4513 *%-----|
 4514 CONTINUOUS STANDHYD NHYD=["A13"], DT=[1] min, AREA=[2.59] (ha),
 4515 XI MP=[0.71], TI MP=[0.71], DWF=[0] (cms), LOSS=[2],
 4516 SCS curve number CN=[75],
 4517 Pervious surfaces: I A per=[4.67] (mm), SLPP=[1] (%),
 4518 LGP=[40] (m), MNP=[0.25], SCP=[0] (min),
 4519 Impervious surfaces: I A i mp=[1.57] (mm), SLPI=[1] (%),
 4520 LGI=[379] (m), MNI=[0.013], SCI=[0] (min),
 4521 Continuous simulation parameters:
 4522 I a REC per=[4] (hrs), I a REC i mp=[4] (hrs),
 4523 SM N=[-1] (mm), SMAX=[-1] (mm), SK=[0.010] / (mm),
 4524 Inter Event Time=[18] (hrs), END=- 1
 4525 *%-----|
 4526 COMPUTE DUALHYD NHYD i n=["A13"], CI NLET=[0.571] (cms), NI NLET=[1],
 4527 M a j NHYD=["A13- M"]
 4528 M n NHYD=["A13- MN"]
 4529 TM STO=[0] (cu-m)
 4530 *%-----|
 4531 * -JFSA 2021-01-22 add the Corrigan pond area ("Pond-Block")
 4532 CONTINUOUS STANDHYD NHYD=["Pond-Block"], DT=[1] min, AREA=[2.94] (ha),
 4533 XI MP=[0.415], TI MP=[0.415], DWF=[0] (cms), LOSS=[2],
 4534 SCS curve number CN=[75],
 4535 Pervious surfaces: I A per=[4.67] (mm), SLPP=[1] (%),
 4536 LGP=[40] (m), MNP=[0.25], SCP=[0] (min),
 4537 Impervious surfaces: I A i mp=[1.57] (mm), SLPI=[1] (%),
 4538 LGI=[183] (m), MNI=[0.013], SCI=[0] (min),
 4539 Continuous simulation parameters:
 4540 I a REC per=[4] (hrs), I a REC i mp=[4] (hrs),
 4541 SM N=[-1] (mm), SMAX=[-1] (mm), SK=[0.010] / (mm),
 4542 Inter Event Time=[18] (hrs), END=- 1
 4543 *%-----|
 4544 ADD HYD NHYD s um=["MHI08"], NHYD s t o a dd=["119-108"+"A13-MN"+"A12-MN"]
 4545 *%-----|
 4546 SAVE HYD NHYD=["MHI08"], # OF PCYCLES=[-1], I CASE s h=[1]
 4547 HYD_COMMENT=["Total Flows at MHI08"]
 4548 *%-----|
 4549 ROUTE PIPE PTYPE=[1] circ, NHYD out=["108-116"], RNUMBER=[1.0], PDI AM=[1800] (mm),
 4550 PLNGTH=[76.6] (m), PROUGH=[0.013], PSLOPE=[0.0013] (m/m),
 NHYD i n=["MHI08"], RDT=[1]
 4551 *%-----|
 4552 ROUTE PIPE PTYPE=[1] circ, NHYD out=["116-corrigan"], RNUMBER=[1.0],
 4553 PDI AM=[1800] (mm),
 PLNGTH=[79.5] (m), PROUGH=[0.013], PSLOPE=[0.0013] (m/m),
 NHYD i n=["108-116"], RDT=[1]
 4554 *%-----|
 4555 ADD HYD NHYD s um=["Corrigan"], NHYD s t o a dd=["116-corrigan"+"Pond-Block"]
 4556 *%-----|
 4557 SAVE HYD NHYD=["Corrigan"], # OF PCYCLES=[-1], I CASE s h=[1]
 4558 HYD_COMMENT=["Total Flows at Corrigan Pond"]
 4559 *%-----|

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4560 ROUTE RESERVOIR      NHYDout=["Co-P"],  NHYDin=["Corrigan"],
4561 RDT=[1](min),
4562          TABLE of ( OUTFLOW STORAGE ) values
4563                    (cms) - (ha-m)
4564                    [ 0.0 , 0.0 ]
4565                    [ 0.015 , 0.04118]
4566                    [ 0.030 , 0.08297]
4567                    [ 0.045 , 0.12537]
4568                    [ 0.060 , 0.16837]
4569                    [ 0.075 , 0.21199]
4570                    [ 0.090 , 0.27545]
4571                    [ 0.105 , 0.34650]
4572                    [ 0.120 , 0.42049]
4573                    [ 0.135 , 0.50188]
4574                    [ 0.186 , 0.60307]
4575                    [ 2.110 , 0.79083]
4576                    [ 5.874 , 1.00271]
4577                    [ 11.395 , 1.29643]
4578                    [ 18.770 , 1.62054]
4579                    [ 28.143 , 1.97516]
4580                    [ -1 , -1 ] (max twenty pts)
4581          NHYDovf=["Co-P-OVF"]
4582 *%-----|-----|
4583 ADD HYD          NHYDsum=["corrig"], NHYDs to
add=["Co-P-OVF"+"Co-P"+"N_TO"+"MH105-JR"+"A8-M-JR"+"A9-M-JR"+"A10-M-JR"+"A11-M-JR"+"A12-M-JR"+"A
13-M-JR"]
4584 *%-----|-----|
4585 SAVE HYD        NHYD=["corrig"], # OF PCYCLES=[-1], ICASEsh=[1]
4586          HYD_COMMENT=["Total Flows at Corrigan Pond"]
4587 *%-----|-----|
4588 *#*****|*****|
4589 *#   Corrigan Pond 1
4590 *#   - Rating curve obtained from Barrhaven South M&S modeling
4591 *#   - Tributary Drainage Area to M&S Pond 1 = 145 ha
4592 *#*****|*****|
4593 *ROUTE RESERVOIR  NHYDout=["MS_P1"],  NHYDin=["CORRIG"],
4594 *          RDT=[1](min),
4595 *          TABLE of ( OUTFLOW STORAGE ) values
4596 *                    (cms) - (ha-m)
4597 *                    [ 0.0 , 0.0 ]
4598 *                    [ 0.06 , 0.58]
4599 *                    [ -1 , -1 ] (max twenty pts)
4600 *          NHYDovf=["P1-OVF"]
4601 *%-----|-----|
4602 *ADD HYD          NHYDsum=["SN_CO"], NHYDs to add=["N_TO"+"P1-OVF"+"MS_P1"]
4603 *%-----|-----|
4604 *SAVE HYD        NHYD=["SN_CO"], # OF PCYCLES=[-1], ICASEsh=[1]
4605 *          HYD_COMMENT=["Total Flows at Corrigan Drain"]
4606 *%-----|-----|
4607 *#
4608 *# Hydrograph from Corrigan Drain routed to Jockvale Road
4609 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 2462
4610 *#
4611 ROUTE CHANNEL    NHYDout=["N_M"] , NHYDin=["corrig"] ,
4612 RDT=[1](min),
4613 CHLGTH=[580](m),  CHSLOPE=[0.4448](%),
4614                    FPSLOPE=[0.4448](%),
4615 SECNUM=[1.0],    NSEG=[3]
4616 ( SEGROUGH, SEGDIST (m))=
4617   [0.075, -17.72
4618   -0.045, 17.72
4619   0.075, 80.62] NSEG times
4620 ( DISTANCE (m), ELEVATION (m))=
4621 [-83.32, 90.00]
4622 [-81.36, 89.50]
4623 [-79.12, 89.00]

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4624 [- 76. 13, 88. 50]
4625 [- 20. 46, 88. 00]
4626 [- 19. 36, 87. 50]
4627 [- 18. 51, 87. 00]
4628 [- 17. 72, 86. 50]
4629 [- 11. 95, 85. 24]
4630 [- 0. 11, 85. 12]
4631 [11. 49, 85. 20]
4632 [17. 72, 86. 50]
4633 [19. 74, 87. 00]
4634 [21. 22, 87. 50]
4635 [22. 68, 88. 00]
4636 [24. 28, 88. 50]
4637 [26. 79, 89. 00]
4638 [71. 98, 90. 00]
4639 [80. 62, 90. 50]

4640 *%-----|-----|
4641 *#*****|*****|

4642 *# Catchment MLLS
4643 *# - To SWM Facility north of the Jock
4644 *# - Primarily residential development
4645 *#*****|*****|

4646 CONTINUOUS STANDHYD NHYD=["MLLS"], DT=[1] min, AREA=[175.99] (ha),
4647 XI MP=[0.38], TI MP=[0.38], DWF=[0] (cms), LOSS=[2],
4648 SCS curve number CN=[74],
4649 Pervious surfaces: I A per=[4.67] (mm), SLPP=[1] (%),
4650 LGP=[40] (m), MNP=[0.25], SCP=[0] (min),
4651 Impervious surfaces: I A i mp=[1.57] (mm), SLPI=[1] (%),
4652 LGI=[1118.123] (m), MNI=[0.013], SCI=[0] (min),
4653 Continuous simulation parameters:
4654 I a REC per=[4] (hrs), I a REC i mp=[4] (hrs),
4655 S M N=[-1] (mm), S M A X=[-1] (mm), S K=[0.010] / (mm),
4656 I n t e r E v e n t T i m e=[18] (hrs), E N D=-1

4657 *%-----|-----|
4658 *#*****|*****|

4659 *# Chapman Mills SWM Pond
4660 *# - Rating curve obtained from CCL hydraulic modeling
4661 *#*****|*****|

4662 ROUTE RESERVOIR NHYDout=["MLL_P"], NHYDin=["MLLS"],
4663 RDT=[1] (min),
4664 TABLE of (OUTFLOW STORAGE) values
4665 (cms) - (ha-m)
4666 [0.0 , 0.0]
4667 [0.01 , 0.01]
4668 [0.05 , 0.06]
4669 [0.09 , 0.11]
4670 [0.13 , 0.15]
4671 [0.18 , 0.19]
4672 [0.28 , 0.28]
4673 [0.37 , 0.34]
4674 [0.45 , 0.40]
4675 [0.51 , 0.44]
4676 [0.56 , 0.47]
4677 [0.64 , 0.52]
4678 [0.76 , 0.59]
4679 [0.86 , 0.65]
4680 [1.09 , 0.78]
4681 [1.44 , 0.96]
4682 [3.18 , 1.84]
4683 [4.05 , 2.31]
4684 [-1 , -1] (max twenty pts)
4685 NHYDovf=["ML-OV"]

4686 *%-----|-----|
4687 ADD HYD NHYDsum=["SN_M"], NHYDsto add=["N_M"+"ML-OV"+"MLL_P"]
4688 *%-----|-----|

4689 SAVE HYD NHYD=["SN_M"], # OF PCYCLES=[-1], I CASEs h=[1]


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4690 HYD_COMMENT=["Total Flows at Jockvale Road"]
4691 *%-----|-----|
4692 *#
4693 *# Hydrograph from Jockvale Road routed to Heart's Desire
4694 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 689
4695 *#
4696 ROUTE CHANNEL NHYDout=["N_DE"], NHYDin=["SN_M"],
4697 RDT=[1](min),
4698 CHLGTH=[1962](m), CHSLOPE=[0.2227](%),
4699 FPSLOPE=[0.2227](%),
4700 SECNUM=[1.0], NSEG=[3]
4701 (SEGROUGH, SEGDIST (m))=
4702 [0.075, -17.56
4703 -0.045, 18.27
4704 0.075, 32.51] NSEG times
4705 (DISTANCE (m), ELEVATION (m))=
4706 [-54.07, 85.00]
4707 [-39.43, 84.50]
4708 [-28.30, 84.00]
4709 [-24.12, 83.50]
4710 [-22.30, 83.00]
4711 [-20.55, 82.50]
4712 [-17.56, 82.00]
4713 [-12.63, 81.22]
4714 [-0.11, 80.75]
4715 [11.55, 81.22]
4716 [18.27, 82.00]
4717 [19.82, 82.50]
4718 [22.48, 83.00]
4719 [27.90, 83.50]
4720 [29.31, 84.00]
4721 [30.81, 84.50]
4722 [32.51, 85.00]
4723 *%-----|-----|
4724 *#*****|*****|
4725 *# Catchment DESIRE
4726 *# - To Jock River (north of the Jock)
4727 *# - Rural-estate subdivision (Heart's Desire Community)
4728 *#*****|*****|
4729 CONTINUOUS STANDHYD NHYD=["DESIRE"], DT=[1]min, AREA=[23.78](ha),
4730 XI MP=[0.25], TI MP=[0.25], DWF=[0](cms), LOSS=[2],
4731 SCS curve number CN=[77],
4732 Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
4733 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4734 Impervious surfaces: I A i mp=[1.57](mm), SLPI=[1](%),
4735 LGI=[400](m), MNI=[0.013], SCI=[0](min),
4736 Continuous simulation parameters:
4737 I a RE C per=[4](hrs), I a RE C i mp=[4](hrs),
4738 SM N=[-1](mm), SMAX=[-1](mm), SK=[0.010]/(mm),
4739 Inter Event Time=[18](hrs), END=-1
4740 *%-----|-----|
4741 *#*****|*****|
4742 *# Catchment JOCKVA
4743 *# - To Jockvale SWM Facility
4744 *# - Residential development & golf course
4745 *# - JFSA 2021-01-11 update JOCKVA after updating CORRIG as per IBI GROUP, July 2008.
4746 *# JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two
4747 areas JOCKVA and EX-LAND 32.5 ha as per IBI GROUP, July 2008.
4748 *#*****|*****|
4749 CONTINUOUS STANDHYD NHYD=["JOCKVA"], DT=[1]min, AREA=[225.13](ha),
4750 XI MP=[0.50], TI MP=[0.50], DWF=[0](cms), LOSS=[2],
4751 SCS curve number CN=[74],
4752 Pervious surfaces: I A per=[4.67](mm), SLPP=[1](%),
4753 LGP=[40](m), MNP=[0.25], SCP=[0](min),
4754 Impervious surfaces: I A i mp=[1.57](mm), SLPI=[1](%),
4755 LGI=[1310.55](m), MNI=[0.013], SCI=[0](min),

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4755 Continuous simulation parameters:
4756 IaRECPper=[ 4] (hrs), IaRECImp=[ 4] (hrs),
4757 SMN=[ -1] (mm), SMAX=[ -1] (mm), SK=[ 0.010]/(mm),
4758 InterEventTime=[ 18] (hrs), END=- 1
4759 *%-----|-----|
4760 ADD HYD NHYDsum=["JOCKVA-TO"], NHYDsto
add=["EX-LAND-MN"+"JOCKVA"+"B2-M"+"B3-M"]
4761 *%-----|-----|
4762 SAVE HYD NHYD=["JOCKVA-TO"], # OF PCYCLES=[ -1], ICASEsh=[ 1]
4763 HYD_COMMENT=["Total Flows at KB first pond"]
4764 *%-----|-----|
4765 *#*****|*****|
4766 *# Jockvale SWM Facility
4767 *# - Rating curve obtained from Jockvale Servicing Study (CCL 1999)
4768 *#*****|*****|
4769 ROUTE RESERVOIR NHYDout=["JOCK_P"], NHYDin=["JOCKVA-TO"],
4770 RDT=[ 1] (min),
4771 TABLE of ( OUTFLOW STORAGE ) values
4772 (cms) - (ha-m)
4773 [ 0.0 , 0.0 ]
4774 [ 0.27 , 0.03]
4775 [ 0.28 , 0.55]
4776 [ 0.29 , 1.14]
4777 [ 0.30 , 1.80]
4778 [ 0.31 , 2.32]
4779 [ 1.12 , 2.87]
4780 [ 2.92 , 3.45]
4781 [ 4.64 , 4.07]
4782 [ 6.69 , 4.72]
4783 [ 9.02 , 5.39]
4784 [ 11.62 , 6.10]
4785 [ 14.42 , 6.85]
4786 [ 17.45 , 7.62]
4787 [ 20.69 , 8.44]
4788 [ 24.08 , 9.28]
4789 [ 27.68 , 10.17]
4790 [ -1 , -1 ] (max twenty pts)
4791 NHYDovf=["JO-OVF"]
4792 *%-----|-----|
4793 ADD HYD NHYDsum=["SN_DE"], NHYDsto add=["N_DE"+"DESIRE"+"JO-OVF"+"JOCK_P"]
4794 *%-----|-----|
4795 SAVE HYD NHYD=["SN_DE"], # OF PCYCLES=[ -1], ICASEsh=[ 1]
4796 HYD_COMMENT=["Total Flows at Heart's Desire"]
4797 *%-----|-----|
4798 *#
4799 *# Hydrograph from Heart's Desire routed to Rideau River
4800 *# Channel X-Section obtained from RVCA Hydraulic Model - Station 0
4801 *#
4802 ROUTE CHANNEL NHYDout=["N1"], NHYDin=["SN_DE"],
4803 RDT=[ 1] (min),
4804 CHLGTH=[ 563] (m), CHSLOPE=[ 0.9668] (%),
4805 FPSLOPE=[ 0.9668] (%),
4806 SECNUM=[ 1.0], NSEG=[ 3]
4807 ( SEGROUGH, SEGDIST (m))=
4808 [ 0.075, -30.20
4809 -0.045, 30.20
4810 0.075, 48.48] NSEG times
4811 ( DISTANCE (m), ELEVATION (m))=
4812 [-98.46, 81.50]
4813 [-92.24, 81.00]
4814 [-86.88, 80.50]
4815 [-81.54, 80.00]
4816 [-74.36, 79.50]
4817 [-63.54, 79.00]
4818 [-39.23, 78.50]
4819 [-34.51, 78.00]

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4820 [- 33. 01, 77. 50]
4821 [- 30. 20, 77. 00]
4822 [- 13. 42, 76. 18]
4823 [- 1. 14, 76. 09]
4824 [17. 06, 76. 18]
4825 [30. 20, 77. 00]
4826 [32. 95, 77. 50]
4827 [34. 06, 78. 00]
4828 [35. 11, 78. 50]
4829 [36. 32, 79. 00]
4830 [37. 74, 79. 50]
4831 [48. 48, 81. 50]
4832 *%-----|-----|
4833 *#*****|*****|
4834 *# Catchment S-2
4835 *# - To Jock River (north and south)
4836 *# - Undeveloped floodplain and river
4837 *#*****|*****|
4838 CONTINUOUS NASHYD NHYD=["S-2"], DT=[1] min, AREA=[102.94] (ha),
4839 DWF=[0] (cms), CN/C=[72], IA=[4.67] (mm),
4840 N=[3], TP=[0.40] hrs,
4841 Continuous simulation parameters:
4842 IaRECper=[4] (hrs),
4843 SMN=[-1] (mm), SMAX=[-1] (mm), SK=[0.010]/(mm),
4844 InterEventTime=[12] (hrs)
4845 Baseflow simulation parameters:
4846 BaseFlowOption=[1],
4847 InitGWResVol=[50] (mm), GWResK=[0.96] (mm/day/mm)
4848 VHydCond=[0.055] (mm/hr), END=-1
4849 *%-----|-----|
4850 ADD HYD NHYDs um=["SN_NI"], NHYDs to add=["NI"+"S-2"]
4851 *%-----|-----|
4852 SAVE HYD NHYD=["SN_NI"], # OF PCYCLES=[-1], ICASEsh=[1]
4853 HYD_COMMENT=["Total Flows at Rideau River"]
4854 *%-----|-----|
4855 *#####|#####|
4856 *% 5 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4857 START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[5]
4858 *% ["C24SC005.stm"] <--storm filename, one per line for NSTORMtime
4859 *%-----|-----|
4860 *% 10 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4861 START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[10]
4862 *% ["C24SC010.stm"] <--storm filename, one per line for NSTORMtime
4863 *%-----|-----|
4864 *% 25 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4865 START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[25]
4866 *% ["C24SC025.stm"] <--storm filename, one per line for NSTORMtime
4867 *%-----|-----|
4868 *% 50 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4869 START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[50]
4870 *% ["C24SC050.stm"] <--storm filename, one per line for NSTORMtime
4871 *%-----|-----|
4872 *% 100 yr, 3 hr Chicago storm based on OTTAWA CDA IDF Curves
4873 *START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4874 *% ["100YC3H.STM"] <--storm filename, one per line for NSTORMtime
4875 *%-----|-----|
4876 *% 100 yr, 24 hr SCS storm based on OTTAWA CDA IDF Curves
4877 START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4878 *% ["C24SC100.stm"] <--storm filename, one per line for NSTORMtime
4879 *%-----|-----|
4880 *% 100 yr, 3 hr Chicago storm based on OTTAWA CDA IDF Curves
4881 *START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[100]
4882 *% ["C24SC100.stm"] <--storm filename, one per line for NSTORMtime
4883 *START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[101]
4884 *% ["A24SC100.stm"] <--storm filename, one per line for NSTORMtime
4885 *START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[102]

```

4886 *%
4887 FINISH
4888

["A24SCI00_60.stm"] <-- storm filename, one per line for NSTORMtime

```

000011 *****
000012 ***** SWMM0 Ver 5.500 *****
000013 ***** A single event and continuous hydrologic simulation model *****
000014 ***** Based on the principles of HDM and its successors *****
000015 ***** CHTDMS 83 and OTTDMO 89 *****
000016 *****
000017 ***** Distributed by: J.F. Sabourin and Associates Inc. *****
000018 ***** Ottawa, Ontario: (613) 836-2884 *****
000019 ***** Gatineau, Quebec: (819) 243-6858 *****
000020 ***** E-Mail: swmm@jfsa.com *****
000021 *****
000022 *****
000023 *****
000024 ***** Licensed user: JFSAi *****
000025 ***** Serial#: 2549237 *****
000026 *****
000027 *****
000028 *****
000029 ***** ***** PROGRAM ARRAY DIMENSIONS *****
000030 ***** Maximum value for 1D numbers: 11 *****
000031 ***** Maximum number of rainfall points: 105408 *****
000032 ***** Maximum number of flow points: 105408 *****
000033 *****
000034 *****
000035 ***** S U M M A R Y O U T P U T *****
000036 *****
000037 *****
000038 ***** RIN DATE: 2021-03-04 TIME: 11:57:49 RIN COUNTER: 002084 *****
000039 *****
000040 ***** Input file: T:\PROJ\1474-16\Design\20210304-QuantityControlAnalysis\SWMM0A.SMR.Model\update.d *****
000041 ***** 3\SMR_S_1.SMR.FR.SD.dat *****
000042 ***** 3\SMR_S_1.SMR.FR.SD.out *****
000043 ***** Output file: T:\PROJ\1474-16\Design\20210304-QuantityControlAnalysis\SWMM0A.SMR.Model\update.d *****
000044 ***** Summary file: T:\PROJ\1474-16\Design\20210304-QuantityControlAnalysis\SWMM0A.SMR.Model\update.d *****
000045 ***** User comment: *****
000046 ***** 1: *****
000047 ***** 2: *****
000048 ***** 3: *****
000049 ***** 4: *****
000050 *****
000051 *****
000052 *****
00053 *****
00054 ***** SWMM0 Ver 5.02/Jan 2001 /BETA/ / INPUT DATA FILE *****
00055 *****
00056 ***** Project Name: [Jock River] Project Number: [1474-16] *****
00057 ***** Date: [04-03-2021] *****
00058 ***** Modeler: [JFM] *****
00059 ***** Company: [JFSAi] *****
00060 ***** License #: [2549237] *****
00061 *****
00062 ***** CALIBRATION OF SUMMER MODEL PARAMETERS *****
00063 ***** USING CONTINUOUS SIMULATIONS *****
00064 ***** Rainfall data from JFSA rain gauge installed at site + other gauges by the City *****
00065 ***** Use data collected from May 1st to July 14, 2003 *****
00066 ***** 2020-11-30 change TMSD to a COMPLETE POLYD (TMSD=0.1 instead of 0.0001) *****
00067 ***** 2020-12-01 correct pond curve values *****
00068 ***** 2020-12-01 change W.C.LAR, BRG, SLP to 0.55, SLP1=[0.5] (% (impervious slope), and LGI up to 700m *****
00069 ***** 2021-02-19 Change slope for ROUTE CHANNEL Station 2462 (NHDOut=[N_TOP], NHDIn=[SN_TOP]) from 0.03 % (as per S *****
00070 ***** 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (NHDOut=[N_NC], NHDIn=[SN_NC]) from 0.01 % (as per S *****
00071 ***** *****
00072 ***** ** END OF RUN: *****
00073 *****
00074 *****
00075 *****
00076 *****
00077 *****
00078 *****
00079 *****
00080 ***** RUN: COMAND *****
00081 ***** R0002: C0001 *****
00082 ***** START *****
00083 ***** [TZERO= 0 hrs on 0] *****
00084 ***** [MOUT= 2 (Imperial, 2 metric output)] *****
00085 ***** [NFOR= 1] *****
00086 ***** [NUN= 0002] *****
00087 *****
00088 ***** SWMM0 Ver 5.02/Jan 2001 /BETA/ / INPUT DATA FILE *****
00089 *****
00090 ***** Project Name: [Jock River] Project Number: [1474-16] *****
00091 ***** Date: [04-03-2021] *****
00092 ***** Modeler: [JFM] *****
00093 ***** Company: [JFSAi] *****
00094 ***** License #: [2549237] *****
00095 *****
00096 ***** CALIBRATION OF SUMMER MODEL PARAMETERS *****
00097 ***** USING CONTINUOUS SIMULATIONS *****
00098 ***** Rainfall data from JFSA rain gauge installed at site + other gauges by the City *****
00099 ***** Use data collected from May 1st to July 14, 2003 *****
00100 ***** 2020-11-30 change TMSD to a COMPLETE POLYD (TMSD=0.1 instead of 0.0001) *****
00101 ***** 2020-12-01 correct pond curve values *****
00102 ***** 2020-12-01 change W.C.LAR, BRG, SLP to 0.55, SLP1=[0.5] (% (impervious slope), and LGI up to 700m *****
00103 ***** 2021-02-19 Change the slope for ROUTE CHANNEL Station 2462 (NHDOut=[N_TOP], NHDIn=[SN_TOP]) from 0.03 % (as per S *****
00104 ***** 2021-02-19 Change the slope for ROUTE CHANNEL Station 5002 (NHDOut=[N_NC], NHDIn=[SN_NC]) from 0.01 % (as per S *****
00105 ***** *****
00106 ***** R0002: C0002 *****
00107 ***** READ STORM *****
00108 ***** Filename = storm01 *****
00109 ***** [Area= 6.0 m2; SDR= 24 hrs; 1:2 ans pour; Ours ODA *****
00110 ***** [SD=10.0; SDR= 24.0; PPO= 45.5] *****
00111 *****
00112 ***** MOUFY STORM *****
00113 ***** [RFact= 1.0; TSH= 96.0 mm] *****
00114 ***** [SD= 10.0; SDR= 24.0; PPO= 45.5] *****
00115 ***** R0002: C0003 *****
00116 ***** REFLECT VALUES *****
00117 ***** Filename = T:\PROJ\1474-16\Design\20210304-QuantityControlAnalysis\SWMM0A.SMR.Model\update.d\G1.G1e.DEP *****
00118 ***** [Cshd= 1 (read and print data) *****
00119 ***** File list file comment: [Based onvarious calibration exercises in Ota *****
00120 ***** The FOLLOWING PARAMETERS ARE USED IN THE DESIGN STANDARD COM *****
00121 ***** Horton's infiltration equation parameters *****
00122 ***** [In= 76.20 mm/hr] [C=13.20 mm/hr] [CVA= 1.4 /hr] [F= .00 mm *****
00123 ***** Parameters for PERMANENT *****
00124 ***** [Lager= 4.67 mm] [LPS=50.0 mm] [MNP= .250] *****
00125 ***** Parameters for IMPROVED surfaces in STANDARD *****
00126 ***** [L= 1.57 mm] [C= 1.50] [DK= .013] *****
00127 ***** Parameters used in NASHID *****
00128 ***** [In= 76.20 mm/hr] *****
00129 ***** Average monthly Pan Evaporation data in (mm) *****
00130 ***** JAN FEB MAR APR MAY JEN JUL AUG SEP OCT NOV DEC *****
00131 ***** 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *****
00132 ***** Average monthly Potential Evapotranspiration in (mm) *****
00133 ***** JAN FEB MAR APR MAY JEN JUL AUG SEP OCT NOV DEC *****
00134 ***** 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *****
00135 ***** R0002: C0005 *****
00136 ***** COMPUTE API *****
00137 ***** [API= 50.00; APIKey= 8500; APIKey= 0980] *****
00138 ***** [API= 80.12; APIKey= 56.74; APIKey= 4.87] *****
00139 *****
00140 ***** The Tp was modified according to a Peak Reduction factor (MO Chart B2-4) *****
00141 ***** # of 1.32 *****
00142 ***** R0002: C0006 *****
00143 ***** CONTINUOUS NASHID 1.0 0.01:SR,HW 3680.00 6.204 No.date 37.06 11.47 252.00 *****
00144 ***** [Cn= 64.0; No 3.00; Tp= 1.31] *****
00145 ***** [IaREC= 4.00; SM= 52.62; SMX=30.79; SK= .010] *****
00146 ***** [InterEventTime= 12.00] *****
00147 *****
00148 ***** The Tp was modified according to a Peak Reduction factor (MO Chart B2-4) *****
00149 ***** # of 1.32 *****
00150 ***** R0002: C0007 *****
00151 ***** CONTINUOUS NASHID 1.0 0.01:SR,W 971.00 2.187 No.date 32.37 10.75 236.00 *****
00152 ***** [Cn= 61.0; No 3.00; Tp= 1.31] *****
00153 ***** [IaREC= 4.00; SM= 64.50; SMX=430.01; SK= .010] *****
00154 ***** [InterEventTime= 12.00] *****
00155 *****
00156 ***** The Tp was modified according to a Peak Reduction factor (MO Chart B2-4) *****
00157 ***** # of 1.80 *****
00158 ***** R0002: C0008 *****
00159 ***** CONTINUOUS NASHID 1.0 0.01:SR,HW 3680.00 6.204 No.date 37.06 11.47 252.00 *****
00160 ***** [Cn= 55.0; No 3.00; Tp= 1.31] *****
00161 ***** [IaREC= 4.00; SM= 52.62; SMX=554.96; SK= .010] *****
00162 ***** [InterEventTime= 12.00] *****
00163 ***** R0002: C0009 *****
00164 ***** CONTINUOUS NASHID 1.0 0.01:SR,ASH 1781.00 5.504 No.date 32.45 13.94 306.00 *****
00165 ***** [Cn= 72.0; No 3.00; Tp= 1.91] *****
00166 ***** [IaREC= 4.00; SM= 39.75; SMX=264.99; SK= .010] *****
00167 ***** [InterEventTime= 12.00] *****
00168 ***** R0002: C0010 *****
00169 ***** CONTINUOUS NASHID 1.0 0.01:SR,W 971.00 2.187 No.date 32.37 10.75 236.00 *****
00170 ***** [Cn= 66.0; No 3.00; Tp= 1.34] *****
00171 ***** [IaREC= 4.00; SM= 52.62; SMX=350.79; SK= .010] *****
00172 ***** [InterEventTime= 12.00] *****
00173 *****
00174 ***** The Tp was modified according to a Peak Reduction factor (MO Chart B2-4) *****
00175 ***** # of 1.80 *****
00176 ***** R0002: C0011 *****
00177 ***** CONTINUOUS NASHID 1.0 0.01:SN,CK 1917.00 4.042 No.date 34.34 11.98 263.00 *****
00178 ***** [Cn= 63.0; No 3.00; Tp= 1.80] *****
00179 ***** [IaREC= 4.00; SM= 52.62; SMX=350.79; SK= .010] *****
00180 ***** [InterEventTime= 12.00] *****
00181 *****
00182 ***** The Tp was modified according to a Peak Reduction factor (MO Chart B2-4) *****
00183 ***** # of 1.52 *****
00184 ***** R0002: C0012 *****
00185 ***** CONTINUOUS NASHID 1.0 0.01:SR,W 971.00 2.187 No.date 32.37 10.75 236.00 *****
00186 ***** [Cn= 72.0; No 3.00; Tp= 1.80] *****
00187 ***** [IaREC= 4.00; SM= 39.75; SMX=264.99; SK= .010] *****

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00375# #
00376# R002:CO039 --- Dfm:n-ID NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rv:m R.C. --- Dwfcm
00377# ADD HYD + 1.0 02:DM1 9506.00 7.379 No.date 33:12 11.30 n/a 000
00378# + 1.0 02:SW1 509.00 2.720 No.date 29:22 11.98 n/a 000
00379# + 1.0 02:NC CK 1917.00 4.042 No.date 34:24 11.98 n/a 000
00380# SIMM 1.0 01:S_N1 11923.00 12.077 No.date 33:14 11.36 n/a 000
00381#
00382# Sum of hydrographs from Node 11 routed to Node 10
00383# Section 7
00384#
00385# R002:CO040 --- Dfm:n-ID NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rv:m R.C. --- Dwfcm
00386# ROUTE CHANNEL -> 1.0 02:S_N1 11923.00 12.077 No.date 33:14 11.36 n/a 000
00387# [RFE:1.00] out_c 1.0 01:N1 11923.00 8.276 No.date 39:46 11.36 n/a 000
00388# [L/S:n 4028 / 0.53 / 0.40]
00389# [Vmax :.462;Dmax :.886]
00390#
00391# Addition of Subwatershed 10 to Node 10
00392#
00393# R002:CO041 --- Dfm:n-ID NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rv:m R.C. --- Dwfcm
00394# ADD HYD + 1.0 02:N1 11923.00 8.276 No.date 39:46 11.36 n/a 000
00395# + 1.0 02:SW1 509.00 2.720 No.date 29:22 11.98 n/a 000
00396# SIMM 1.0 01:S_N1 11923.00 12.077 No.date 33:14 11.36 n/a 000
00397# [L/S:n 4028 / 0.53 / 0.40]
00398# [Vmax :.462;Dmax :.886]
00399#
00400# remark:flow at S_N1: N0 + SW10
00401# # Addition of Kings Creek to S_N10
00402#
00403# R002:CO043 --- Dfm:n-ID NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rv:m R.C. --- Dwfcm
00404# ADD HYD + 1.0 02:S_N10 17589.00 19.451 No.date 38:31 12.19 n/a 000
00405# + 1.0 02:NC CK 8376.00 11.072 No.date 39:59 11.98 n/a 000
00406# SIMM 1.0 01:S_N10A 25965.00 30.328 No.date 39:58 12.12 n/a 000
00407#
00408# Sum of hydrographs from Node 10 routed to Node 9
00409# Section 2
00410#
00411# R002:CO044 --- Dfm:n-ID NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rv:m R.C. --- Dwfcm
00412# ROUTE CHANNEL -> 1.0 02:S_N10A 25965.00 29.579 No.date 39:59 12.12 n/a 000
00413# [RFE:1.00] out_c 1.0 01:N1 25965.00 29.579 No.date 39:59 12.12 n/a 000
00414# [L/S:n 3982 / 0.75 / 0.40]
00415# [Vmax :.595;Dmax :1.208]
00416#
00417# Addition of Subwatershed 9 and Nichols Creek to Node 9
00418#
00419# R002:CO045 --- Dfm:n-ID NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rv:m R.C. --- Dwfcm
00420# ADD HYD + 1.0 02:N1 25965.00 29.579 No.date 39:59 12.12 n/a 000
00421# + 1.0 02:SW1 131.00 4.434 No.date 39:56 13.25 n/a 000
00422# + 1.0 02:NC CK 4464.00 5.504 No.date 39:59 10.98 n/a 000
00423# SIMM 1.0 01:S_N1 31561.00 36.313 No.date 39:59 12.00 n/a 000
00424#
00425# Sum of hydrographs from Node 9 routed to Node 8
00426# Section 3
00427#
00428# R002:CO046 --- Dfm:n-ID NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rv:m R.C. --- Dwfcm
00429# ROUTE CHANNEL -> 1.0 02:S_N1 31561.00 36.313 No.date 39:59 12.00 n/a 000
00430# [RFE:1.00] out_c 1.0 01:N1 31561.00 34.173 No.date 39:59 12.00 n/a 000
00431# [L/S:n 3982 / 0.87 / 0.40]
00432# [Vmax :.418;Dmax :1.281]
00433#
00434# Addition of Subwatershed 8 and Hibbs' Drain to Node 8
00435#
00436# R002:CO047 --- Dfm:n-ID NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rv:m R.C. --- Dwfcm
00437# ADD HYD + 1.0 02:N1 31561.00 34.173 No.date 39:59 12.00 n/a 000
00438# + 1.0 02:SW1 131.00 4.434 No.date 39:56 13.25 n/a 000
00439# + 1.0 02:IB DR 3854.00 6.242 No.date 38:46 11.98 n/a 000
00440# SIMM 1.0 01:S_N1 35546.00 40.474 No.date 39:59 12.00 n/a 000
00441#
00442# Sum of hydrographs from Node 8 routed to Node 7
00443# Section 4
00444#
00445# R002:CO048 --- Dfm:n-ID NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rv:m R.C. --- Dwfcm
00446# ROUTE CHANNEL -> 1.0 02:S_N1 35546.00 40.474 No.date 39:59 12.00 n/a 000
00447# [RFE:1.00] out_c 1.0 01:N1 35546.00 32.891 No.date 44:30 12.00 n/a 000
00448# [L/S:n 3750 / 0.53 / 0.70]
00449# [Vmax :.208;Dmax :1.651]
00450#
00451# Addition of Subwatershed 7 to Node 7
00452#
00453# R002:CO049 --- Dfm:n-ID NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rv:m R.C. --- Dwfcm
00454# ADD HYD + 1.0 02:SW1 3197.00 4.651 No.date 36:31 9.85 n/a 000
00455# SIMM 1.0 01:S_N1 38743.00 35.071 No.date 43:33 11.82 n/a 000
00456# [L/S:n 3750 / 0.53 / 0.70]
00457# [Vmax :.208;Dmax :1.651]
00458#
00459# remark:flow at S_N1: N0 + SW7
00460#
00461# Insertion of a Reservoir to simulate the effects of the Richmond Fen.
00462# Storage area and volumes were estimated from available topography.
00463# Release rate from fen was assumed to be controlled by the downstream
00464# river cross section for various conditions. It is assumed that for up to
00465# 0.75 m of water, the main channel of the river provided the storage. Above
00466# this depth, the wetland starts to significantly store water.
00467#
00468# R002:CO051 --- Dfm:n-ID NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rv:m R.C. --- Dwfcm
00469# ROUTE RESERVOIR -> 1.0 01:RES_RF 38743.00 35.071 No.date 43:33 11.82 n/a 000
00470# [RFE:1.00] out_c 1.0 01:RES_RF 38743.00 23.265 No.date 55:09 11.82 n/a 000
00471# [MS:Stable=7.00;Elev=1.0]
00472# R002:CO052 --- Dfm:n-ID NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rv:m R.C. --- Dwfcm
00473# SAVE HYD + 1.0 01:RES_RF 38743.00 23.265 No.date 55:09 11.82 n/a 000
00474# [L/S:n 3750 / 0.53 / 0.70]
00475# remark:outflow of Richmond Fen
00476#
00477# Sum of hydrographs from Node 7 routed to Node 6
00478# Section 5
00479#
00480# R002:CO053 --- Dfm:n-ID NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rv:m R.C. --- Dwfcm
00481# ROUTE CHANNEL -> 1.0 02:RES_RF 38743.00 23.265 No.date 55:09 11.82 n/a 000
00482# [RFE:1.00] out_c 1.0 01:N1 38743.00 23.228 No.date 56:38 11.82 n/a 000
00483# [L/S:n 1007 / 0.83 / 0.40]
00484# [Vmax :.432;Dmax :.808]
00485#
00486# Addition of Subwatershed 6 and Van Gual Drain to Node 6
00487#
00488# R002:CO054 --- Dfm:n-ID NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rv:m R.C. --- Dwfcm
00489# ADD HYD + 1.0 02:N1 38743.00 23.228 No.date 56:38 11.82 n/a 000
00490# + 1.0 02:SW1 131.00 4.434 No.date 39:56 13.25 n/a 000
00491# + 1.0 02:VG DR 1332.00 3.148 No.date 35:23 13.94 n/a 000
00492# SIMM 1.0 01:S_N1 40240.00 23.318 No.date 39:59 11.89 n/a 000
00493#
00494# Sum of hydrographs from Node 6 routed to Node 5
00495# Section 6
00496#
00497# R002:CO055 --- Dfm:n-ID NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rv:m R.C. --- Dwfcm
00498# ROUTE CHANNEL -> 1.0 02:S_N1 40240.00 23.318 No.date 39:59 11.89 n/a 000
00499# [RFE:1.00] out_c 1.0 01:N1 40240.00 23.285 No.date 56:09 11.89 n/a 000
00500# [L/S:n 1067 / 0.54 / 0.40]
00501# [Vmax :.378;Dmax :.917]
00502#
00503# Addition of Subwatershed 5 and Flowing Creek to Node 5
00504#
00505# R002:CO056 --- Dfm:n-ID NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rv:m R.C. --- Dwfcm
00506# ADD HYD + 1.0 02:N1 40240.00 23.285 No.date 56:09 11.89 n/a 000
00507# + 1.0 02:SW1 131.00 4.434 No.date 39:56 13.25 n/a 000
00508# + 1.0 02:FL CK 4945.00 14.839 No.date 32:25 14.57 n/a 000
00509# SIMM 1.0 01:S_N1 45091.00 33.166 No.date 37:08 12.20 n/a 000
00510#
00511# Sum of hydrographs from Node 5 routed to Node 5A
00512# Section 7
00513#
00514# R002:CO057 --- Dfm:n-ID NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rv:m R.C. --- Dwfcm
00515# ROUTE CHANNEL -> 1.0 02:S_N1 45091.00 33.166 No.date 37:08 12.20 n/a 000
00516# [RFE:1.00] out_c 1.0 01:N1 45091.00 33.155 No.date 37:20 12.20 n/a 000
00517# [L/S:n 556 / 0.90 / 0.40]
00518# [Vmax :.443;Dmax :.937]
00519#
00520# Addition of Subwatershed 5A and Subwatershed 5A2 to Node 5A
00521#
00522# R002:CO058 --- Dfm:n-ID NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rv:m R.C. --- Dwfcm
00523# ADD HYD + 1.0 02:SA 45409.01 33.155 No.date 37:23 12.20 n/a 000
00524# + 1.0 02:SWA2 20.00 .309 No.date 28:36 17.79 n/a 000
00525# + 1.0 02:SWSAI 1412.00 3.090 No.date 38:04 15.22 n/a 000
00526# SIMM 1.0 01:S_N1A 46841.01 36.216 No.date 37:28 12.30 n/a 000
00527#
00528# Sum of hydrographs from Node 5A routed to Node 4
00529# Section 8
00530#
00531# R002:CO059 --- Dfm:n-ID NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rv:m R.C. --- Dwfcm
00532# ROUTE CHANNEL -> 1.0 02:S_N1A 46841.01 36.216 No.date 37:28 12.30 n/a 000
00533# [RFE:1.00] out_c 1.0 01:N1 46841.01 35.288 No.date 39:22 12.30 n/a 000
00534# [L/S:n 4630 / 0.43 / 0.35]
00535# [Vmax :.695;Dmax :2.444]
00536#
00537# Addition of Subwatershed 4 and Leary Creek to Node 4
00538#
00539# R002:CO060 --- Dfm:n-ID NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rv:m R.C. --- Dwfcm
00540# ADD HYD + 1.0 02:SA 45409.01 33.155 No.date 37:23 12.20 n/a 000
00541# + 1.0 02:SWA 20.00 .309 No.date 28:36 17.79 n/a 000
00542# + 1.0 02:LM CK 1021.00 5.747 No.date 30:50 17.79 n/a 000
00543# SIMM 1.0 01:S_N1 48447.00 37.581 No.date 38:13 12.47 n/a 000
00544#
00545# R002:CO061 --- Dfm:n-ID NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rv:m R.C. --- Dwfcm
00546# SAVE HYD + 1.0 01:S_N1 48447.00 37.581 No.date 38:13 12.47 n/a 000
00547# [L/S:n 4630 / 0.43 / 0.35]
00548#
00549# Sum of hydrographs from Node 4 routed to Node 2
00550# Section 9
00551#
00552# R002:CO062 --- Dfm:n-ID NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rv:m R.C. --- Dwfcm
00553# ROUTE CHANNEL -> 1.0 02:S_N1 48447.00 37.581 No.date 38:13 12.47 n/a 000
00554# [RFE:1.00] out_c 1.0 01:N1 48447.00 37.455 No.date 38:49 12.47 n/a 000
00555# [L/S:n 1667 / 0.60 / 0.40]
00556# [Vmax :.715;Dmax :2.845]
00557#
00558# Addition of Subwatershed 2 with Mbohan Drain and Smith Drain to Node 2
00559#
00560# R002:CO063 --- Dfm:n-ID NDD --- AREHA-QPEAKm-TpeakDate-hh:mm --- Rv:m R.C. --- Dwfcm
00561# ADD HYD + 1.0 02:N1 48447.00 37.455 No.date 38:49 12.47 n/a 000

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Table with multiple columns containing alphanumeric codes (e.g., 00749, 00750), various parameters (e.g., [RFD: 1.00] out, [Vma: 842.Dmax: 265]), numerical values, and status indicators (e.g., 60.55, .402, N.Date, 29.10, 12.46, n/a, .000).

Table with multiple columns including line numbers, subcatchment identifiers, names, and data fields. The table is organized into sections such as 018775, 018780, 018800, 018850, 018900, 019000, 019100, 019150, 019200, 019250, 019300, 019350, 019400, 019450, 019500, 019550, 019600, 019650, 019700, 019750, 019800, 019850, 019900, 019950, 020000, 020050, 020100, 020150, 020200, 020250, 020300, 020350, 020400, 020450, 020500, 020550, 020600, 020650, 020700, 020750, 020800, 020850, 020900, 020950, 021000, 021050, 021100, 021150, 021200, 021250, 021300, 021350, 021400, 021450, 021500, 021550, 021600, 021650, 021700, 021750, 021800, 021850, 021900, 021950, 022000, 022050, 022100, 022150, 022200, 022250, 022300, 022350, 022400, 022450, 022500, 022550, 022600, 022650, 022700, 022750, 022800, 022850, 022900, 022950, 023000, 023050, 023100, 023150, 023200, 023250, 023300, 023350, 023400, 023450, 023500.

Table with columns for ID, description, and numerical values. The table is organized into columns of approximately 20 entries each, containing technical specifications and data points.

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026199 [Impervious area: 1.00E+04.00] LG= 183.3 MN= 0.13 SCI= 0]
026200 [Irrigated area: 4.00E+00] LG= 4.00 MN= 0.13 SCI= 0]
026201 [SMA= 33.81; SMAV=25.45; SKE= 0.10]
026202 R0002:CO0404.....Dfna-ID NDD.....AREAh-QPEAGm-TPeakDte-hh-mm--Rvmm-R-C--DFWcm
026203 COMPUTE DUALLHD 1.0 0.0:AO-M 4.14 246.26 Date: 28:01 23.49 n/a .000
026204 Mjor System / 1.0 0.2:AO-M 0.00 0.00 Date: 0:00 0.00 n/a .000
026205 Mjor System \ 1.0 0.2:AO-M 4.14 246.26 Date: 28:01 23.49 n/a .000
026206 [M SystSca.0000E+00; TotOfVol=0.000E+00; NOfa= 0; TotDrOfa= 0 hrs]
026207 R0002:CO0405.....Dfna-ID NDD.....AREAh-QPEAGm-TPeakDte-hh-mm--Rvmm-R-C--DFWcm
026208 CONTNIXS STANNHD 1.0 0:AO-M 10.61 781.26 Date: 28:02 29.20 6.42 .000
026209 [X Mps 53.71; TMs 75.0]
026210 [LGs= 2 Cn= 75.0]
026211 [Pervious area: 1.00E+04.00] LG= 4.00 MN= 0.13 SCI= 0]
026212 [Irrigated area: 4.00E+00] LG= 4.00 MN= 0.13 SCI= 0]
026213 [SMA= 33.81; SMAV=25.45; SKE= 0.10]
026214 R0002:CO0406.....Dfna-ID NDD.....AREAh-QPEAGm-TPeakDte-hh-mm--Rvmm-R-C--DFWcm
026215 COMPUTE DUALLHD 1.0 0:AO-M 10.61 781.26 Date: 28:02 29.20 n/a .000
026216 Mjor System / 1.0 0.2:AO-M 0.00 0.00 Date: 0:00 0.00 n/a .000
026217 Mjor System \ 1.0 0.2:AO-M 10.61 781.26 Date: 28:02 29.20 n/a .000
026218 [M SystSca.0000E+00; TotOfVol=0.000E+00; NOfa= 0; TotDrOfa= 0 hrs]
026219 R0002:CO0407.....Dfna-ID NDD.....AREAh-QPEAGm-TPeakDte-hh-mm--Rvmm-R-C--DFWcm
026220 CONTNIXS STANNHD 1.0 0:AO-M 10.61 781.26 Date: 28:02 29.20 n/a .000
026221 [X Mps 53.71; TMs 75.0]
026222 [LGs= 2 Cn= 75.0]
026223 [Pervious area: 1.00E+04.00] LG= 4.00 MN= 0.13 SCI= 0]
026224 [Irrigated area: 4.00E+00] LG= 4.00 MN= 0.13 SCI= 0]
026225 [SMA= 33.81; SMAV=25.45; SKE= 0.10]
026226 R0002:CO0408.....Dfna-ID NDD.....AREAh-QPEAGm-TPeakDte-hh-mm--Rvmm-R-C--DFWcm
026227 ADD HHD 1.0 0:AO-M 10.61 781.26 Date: 28:02 29.20 n/a .000
026228 + 1.0 0:2:AO-M 0.00 0.00 Date: 0:00 0.00 n/a .000
026229 + 1.0 0:2:AO-M 4.14 246.26 Date: 28:01 23.49 n/a .000
026230 + 1.0 0:2:AO-M 10.61 781.26 Date: 28:02 29.20 n/a .000
026231 SIM 1.0 0:2:AO-M 4.14 246.26 Date: 28:02 29.20 n/a .000
026232 R0002:CO0409.....Dfna-ID NDD.....AREAh-QPEAGm-TPeakDte-hh-mm--Rvmm-R-C--DFWcm
026233 SAVE HHD 1.0 0:2:AO-M 4.14 246.26 Date: 28:02 29.20 n/a .000
026234 frame: JCKVA To 0002
026235 remark: Total Flow at RB first pond
026236 *****
026237 JOckvale Sww Facility
026238 Channel %Section obtained from Jockvale Servicing Study (CCL 1999)
026239 *****
026240 R0002:CO0410.....Dfna-ID NDD.....AREAh-QPEAGm-TPeakDte-hh-mm--Rvmm-R-C--DFWcm
026241 ROUTE RESERVOIR > 1.0 0:2:AO-M 257.63 12.234 nDate: 28:07 26.85 n/a .000
026242 [overFlow= 1.0 0:1:OCPK 257.63 2.560 nDate: 29:05 26.85 n/a .000]
026243 [MStoVol=3334E+00; TotOfVol=0.000E+00; NOfa= 0; TotDrOfa= 0 hrs]
026244 R0002:CO0411.....Dfna-ID NDD.....AREAh-QPEAGm-TPeakDte-hh-mm--Rvmm-R-C--DFWcm
026245 ADD HHD 1.0 0:2:AO-M 55194.85 49.260 nDate: 39:17 13.21 n/a .000
026246 + 1.0 0:2:AO-M 257.63 2.560 nDate: 29:05 26.85 n/a .000
026247 + 1.0 0:2:AO-M 55194.85 49.260 nDate: 39:17 13.21 n/a .000
026248 + 1.0 0:2:AO-M 257.63 2.560 nDate: 29:05 26.85 n/a .000
026249 SIM 1.0 0:2:AO-M 55194.85 49.260 nDate: 39:17 13.21 n/a .000
026250 R0002:CO0415.....Dfna-ID NDD.....AREAh-QPEAGm-TPeakDte-hh-mm--Rvmm-R-C--DFWcm
026251 SAVE HHD 1.0 0:2:AO-M 55194.85 49.260 nDate: 39:17 13.21 n/a .000
026252 frame: SN.DE.0002
026253 *****
026254 remark: Total Flow at Heari's Desire
026255 *****
026256 Hydrograph from Heari's Desire routed to Rideau River
026257 Channel %Section obtained from RCVCA Hydraulic Model - Station 0
026258 *****
026259 R0002:CO0416.....Dfna-ID NDD.....AREAh-QPEAGm-TPeakDte-hh-mm--Rvmm-R-C--DFWcm
026260 ROUTE CHANNEL > 1.0 0:2:AO-M 55476.26 49.604 nDate: 39:13 13.27 n/a .000
026261 [overFlow= 1.0 0:1:SN.DE 55476.26 49.604 nDate: 39:13 13.27 n/a .000]
026262 [MStoVol=3334E+00; TotOfVol=0.000E+00; NOfa= 0; TotDrOfa= 0 hrs]
026263 [Vmax= 1.490; Dmax= 1.80]
026264 *****
026265 Catchment S-2
026266 To Jock River (north and south)
026267 Undeveloped floodplain and river
026268 *****
026269 R0002:CO0417.....Dfna-ID NDD.....AREAh-QPEAGm-TPeakDte-hh-mm--Rvmm-R-C--DFWcm
026270 CONTNIXS NASHHD 1.0 0:1:SN.DE 102.94 1.373 nDate: 28:20 13.01 286 .000
026271 [Cn= 61.0; Tp= 3.76]
026272 [REFC= 4.00; SMA= 39.75; SMAV=264.99; SKE= 0.10]
026273 [InterEventTime= 12.00]
026274 R0002:CO0418.....Dfna-ID NDD.....AREAh-QPEAGm-TPeakDte-hh-mm--Rvmm-R-C--DFWcm
026275 ADD HHD 1.0 0:2:AO-M 55476.26 49.604 nDate: 39:13 13.27 n/a .000
026276 + 1.0 0:2:AO-M 102.94 1.373 nDate: 28:20 13.01 286 .000
026277 SIM 1.0 0:2:AO-M 55476.26 49.604 nDate: 39:13 13.27 n/a .000
026278 R0002:CO0419.....Dfna-ID NDD.....AREAh-QPEAGm-TPeakDte-hh-mm--Rvmm-R-C--DFWcm
026279 SAVE HHD 1.0 0:2:AO-M 55476.26 49.604 nDate: 39:13 13.27 n/a .000
026280 frame: SN.NI.0002
026281 remark: Total Flow at Rideau River
026282 *****
026283 Channel %Section obtained from RCVCA Hydraulic Model - Station 2462
026284 *****
026285 *****
026286 *****
026287 *****
026288 *****
026289 *****
026290 R0002:CO0420.....Dfna-ID NDD.....AREAh-QPEAGm-TPeakDte-hh-mm--Rvmm-R-C--DFWcm
026291 RUN COMMAND
026292 *****
026293 *****
026294 [TZDE= 0 hrs on ]
026295 [STOR= 1]
026296 [NTRM= 00]
026297 *****
026298 *****
026299 *****
026300 *****
026301 *****
026302 *****
026303 *****
026304 *****
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026499 *****
026500 *****

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033675	#	(Vmax :.781;Dmax:3.131)	033544	CONTINUES NASBIDD	1.0 01:0:8	60.55	.658	N_date	29.05	18.08	317	000
033688	#		033555	[CNS: 69.0; No. 3.00; Tpa. 1]								
033699	#	Addition of Subwatershed 2 with Mhoanah Drain and Smith Drain to Node 2	033566	[IAREC: 4.00; SMNo: 44.32; SMAX:298.82; Skc: -010]								
033700	#		033577	[InterEventTime: 12.00]								
033710	R0005:CO0063	Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm	033588	R0005:CO0093.....Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm								
033720	ADD HYD	+ 1.0 02:2:ND	033599	ROUTE RESEVOIR >	1.0 02:0:8	60.55	.658	N_date	29.05	18.08	314	000
033730		+ 1.0 02:SMIR	033610	[REF: 1.00] out <	1.0 01:STPE	60.55	.654	N_date	29.05	18.08	314	000
033745		+ 1.0 02:SMIR	033621	[L/S:N= 335. / 1003.13]								
033755		+ 1.0 02:SMIR	033632	[L/S:N= 991.0 / 3068.1]								
033760		+ 1.0 01:SI:CK	033643	[HTS: 1.20;WDB: 1.30]								
033775	R0005:CO0064	Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm	033654	R0005:CO0094.....Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm								
033785	SAVE HYD	+ 1.0 01:SI:CK	033665	ADD HYD	+ 1.0 02:BRANI	261.31	2.298	N_date	28.31	13.87	814	000
033790	frnam :H_SNS		033676		+ 1.0 02:DI	1.17	.044	N_date	28.12	23.49	n/a	000
033800	remark:Total Flows at S_NJock River Gauge at Mondie Dr.		033687		+ 1.0 02:AI:STR	2.50	0.076	N_date	28.28	44.03	n/a	000
033810	#		033698		+ 1.0 02:AI:CFM	.00	.000	N_date	0.00	.00	n/a	000
033820	#	Sum of hydrographs from Node 2 routed to Node 1	033709		+ 1.0 02:STSTW	59.05	0.952	N_date	28.03	33.25	n/a	000
033830	#	Section 10	033720		+ 1.0 02:STZWF	.00	.000	N_date	0.00	.00	n/a	000
033840	#		033731		+ 1.0 02:BRPFI	60.55	.654	N_date	29.09	18.08	n/a	000
033850	#		033742	ROUTE RESEVOIR >	1.0 01:STSTW	326.12	2.907	N_date	28.19	34.05	372	000
033860	#	Hydrograph from Node 2 routed to Node 416	033753	SUM								
033870	#	Channel X Section obtained from RGCA Hydraulic Model - Station 9025	033764	R0005:CO0095.....Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm								
033880	#		033775	[XMP: 68;TIMP: 85]								
033890	R0005:CO0095	Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm	033786	[Hydro parameters: Fw: 76.20;Fcs: 13.20;DCAY:14; Fc: 00]								
033900	ROUTE CHANNEL >	1.0 02:SI:CK	033797	[Previous area: IArea: 4.67;SLLP: 50;LGP: 50;MNF: 250;SCP: 0]								
033920	[RFD: 1.00] out <	1.0 01:SI:CK	033808	[Impervious area: IArea: 1.57;SLIP: 50;LGR: 155;MNF: 013;SCL: 0]								
033930	[L/S:N= 2327. / 0501.055]		033819	[IARECmp: 4.00; IAREBcr: 4.00]								
033945	#		033830	R0005:CO0096.....Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm								
033955	#		033842	out <	1.0 01:A7:STR	3.51	1.08	N_date	28.29	44.03	n/a	000
033965	#		033853	overFlow >	1.0 03:AT:CFM	.00	.000	N_date	0.00	.00	n/a	000
033975	#	Catchment RGCA catchment SWL outside of Reach 1 subwatershed	033864	[MS:otEda: 7240E+01	ml, TotOfVol= 0.0000E+00	ml, NOf= 0, TotDurOf= 0.hrs]						
033985	#	Undeveloped agricultural land	033875	R0005:CO0097.....Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm								
033995	#		033886	CONTINUES STANDIND	1.0 01:ST:3	35	.038	N_date	28.00	33.25	582	000
034000	R0005:CO0096.....Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm		033897	[XMP: 46;TIMP: 57]								
034010	CONTINUES NASBIDD	1.0 01:0:1	033908	[Hydro parameters: Fw: 76.20;Fcs: 13.20;DCAY:14; Fc: 00]								
034020	[CNS: 76.0; No. 3.00; Tpa. 2.9]		033919	[Previous area: IArea: 4.67;SLLP: 50;LGP: 50;MNF: 250;SCP: 0]								
034030	[IAREC: 4.00; SMNo: 39.75; SMAX:264.99; Skc: -010]		033930	[Impervious area: IArea: 1.57;SLIP: 50;LGR: 119;MNF: 013;SCL: 0]								
034040	[InterEventTime: 12.00]		033941	[IARECmp: 4.00; IAREBcr: 4.00]								
034055	R0005:CO0097.....Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm		033952	R0005:CO0098.....Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm								
034060	CONTINUES STANDIND	1.0 01:0:1	033963	ROUTE RESEVOIR >	1.0 01:STSTR	71	.063	N_date	28.03	33.25	n/a	000
034070	[XMP: 65;TIMP: 65]		033974	overFlow >	1.0 02:AI:STR	3.51	1.08	N_date	28.29	44.03	n/a	000
034085	[LGRS: 2;CNS: 76.0; No. 3.00; Tpa. 2.9]		033985	[MS:otEda: 1200E-02	ml, TotOfVol= 0.0000E+00	ml, NOf= 0, TotDurOf= 0.hrs]						
034090	[Previous area: IArea: 4.67;SLLP: 50;LGP: 50;MNF: 250;SCP: 0]		033996	[IARECmp: 4.00; IAREBcr: 4.00]								
034100	[Impervious area: IArea: 1.57;SLIP: 50;LGR: 547;MNF: 013;SCL: 0]		034007	R0005:CO0099.....Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm								
034110	[L/S:N= 4321. / 1011.51]		034018	ADD HYD	+ 1.0 02:A7:STR	3.51	1.08	N_date	28.29	44.03	n/a	000
034120	[XMP: 33.81; SMAX:225.43; Skc: -010]		034029		+ 1.0 02:AI:STR	3.51	1.08	N_date	28.29	44.03	n/a	000
034130	R0005:CO0098.....Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm		034040		+ 1.0 02:STSTR	71	.063	N_date	28.03	33.25	n/a	000
034140	COMPUTE DUADJUD	1.0 01:SI:1;Keefe	034051		+ 1.0 02:STSTR	71	.063	N_date	28.03	33.25	n/a	000
034150	Mjur System /	1.0 02:SI:1;CKM	034062		+ 1.0 02:STSTR	71	.063	N_date	28.03	33.25	n/a	000
034160	Mjur System /	1.0 02:SI:1;CKN	034073		+ 1.0 02:STSTR	71	.063	N_date	28.03	33.25	n/a	000
034170	[MjSystem:0.0000E+00, TotOfVol= 0.0000E+00	NOf= 0, TotDurOf= 0.hrs]	034084	R0005:CO1000.....Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm								
034180	R0005:CO1001.....Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm		034095	ROUTE CHANNEL >	1.0 01:STSTR	330.34	3.026	N_date	28.19	34.05	372	000
034190	ADD HYD	+ 1.0 02:SI:CKM	034106	REF: 1.00] out <	1.0 01:BRANI	330.34	2.842	N_date	29.04	15.30	n/a	000
034200		+ 1.0 02:SI:CKS	034117	[L/S:N= 592. / 2100.374]								
034210		+ 1.0 01:SI:1;CKS	034128	[Vmax: 607;Dmax: 930]								
034220	R0005:CO1002.....Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm		034139	R0005:CO1001.....Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm								
034230	ROUTE RESEVOIR >	1.0 02:SI:1;CKS	034150	[CNS: 84.0; No. 3.00; Tpa: 59]								
034240		+ 1.0 01:SI:1;CKSR	034161	[IAREC: 4.00; SMNo: 171.09; SMAX:140.62; Skc: -010]								
034250	overFlow >	1.0 01:SI:1;CKSR	034172	[InterEventTime: 12.00]								
034260	[MS:otEda: 11330E+01	ml, TotOfVol= 0.0000E+00	034183	CONTINUES STANDIND	1.0 01:0:1	12.04	1.379	N_date	28.04	44.03	771	000
034270	ml, NOf= 0, TotDurOf= 0.hrs]		034194	[XMP: 68;TIMP: 85]								
034280	ADD HYD	+ 1.0 02:SI:1;CKS	034205	[Hydro parameters: Fw: 76.20;Fcs: 13.20;DCAY:14; Fc: 00]								
034290		+ 1.0 02:SMIR	034216	[Previous area: IArea: 4.67;SLLP: 50;LGP: 50;MNF: 250;SCP: 0]								
034300		+ 1.0 02:SMIR	034227	[Impervious area: IArea: 1.57;SLIP: 50;LGR: 326;MNF: 013;SCL: 0]								
034310		+ 1.0 02:SI:1;CKSvF	034238	[IARECmp: 4.00; IAREBcr: 4.00]								
034320	SUM		034249	R0005:CO1002.....Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm								
034330	R0005:CO1002.....Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm		034260	ROUTE RESEVOIR >	1.0 02:AI:STR	3.51	1.08	N_date	28.29	44.03	n/a	000
034340	SAVE HYD	+ 1.0 01:SI:1;CKS	034271	overFlow >	1.0 01:AT:STR	12.04	1.379	N_date	28.04	44.03	n/a	000
034350	frnam :SN_416.0005		034282		+ 1.0 02:AI:STR	12.04	1.379	N_date	28.04	44.03	n/a	000
034360	remark:Total Flows at Hwbay 416 before Station 7245		034293		+ 1.0 01:AT:STR	12.04	1.379	N_date	28.04	44.03	n/a	000
034370	#		034304		+ 1.0 02:AI:STR	12.04	1.379	N_date	28.04	44.03	n/a	000
034380	#	Hydrograph from Node 416 routed to Node at Keefe Drain	034315	[MS:otEda: 2492E+00	ml, TotOfVol= 0.0000E+00	ml, NOf= 0, TotDurOf= 0.hrs]						
034390	#	Channel X Section obtained from RGCA Hydraulic Model - Station 7245	034326	R0005:CO1003.....Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm								
034400	#		034337	CONTINUES STANDIND	1.0 01:ST:4	35	.038	N_date	28.00	33.25	582	000
034410	R0005:CO1003.....Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm		034348	[XMP: 46;TIMP: 57]								
034420	[RFD: 1.00] out <	1.0 01:SI:CK	034359	[Hydro parameters: Fw: 76.20;Fcs: 13.20;DCAY:14; Fc: 00]								
034430	[L/S:N= 497. / 301.055]		034370	[Previous area: IArea: 4.67;SLLP: 50;LGP: 50;MNF: 250;SCP: 0]								
034440	[Vmax: 1.357;Dmax: 2.255]		034381	[Impervious area: IArea: 1.57;SLIP: 50;LGR: 144;MNF: 013;SCL: 0]								
034450	#		034392	[IARECmp: 4.00; IAREBcr: 4.00]								
034460	#	Catchment KEEFE	034403	R0005:CO1004.....Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm								
034470	#	- To O Keefe Drain (north of the Jack)	034414	ROUTE RESEVOIR >	1.0 02:ST:4	35	.038	N_date	28.00	33.25	n/a	000
034480	#	- 2020-10-01 add Keefe model (Area 513.02 HA) instead of current Keefe (Area 513.02 HA)	034425	overFlow >	1.0 01:STSTR	35	.031	N_date	28.03	33.25	n/a	000
034490	#	- 2020-10-01 add Keefe model (Area 513.02 HA) instead of current Keefe (Area 513.02 HA)	034436	[MS:otEda: 1040E+02	ml, TotOfVol= 0.0000E+00	ml, NOf= 0, TotDurOf= 0.hrs]						
034500	#	- 2020-10-01 add detail model was added as per the KEVEEF SIMMED model (GIi-Gee 2014).	034447	R0005:CO1005.....Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm								
034510	#		034458	CONTINUES STANDIND	1.0 01:0:1	3.30	.671	N_date	28.02	44.03	771	000
034520	#		034469	[XMP: 68;TIMP: 85]								
034530	R0005:CO1004.....Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm		034480	[Hydro parameters: Fw: 76.20;Fcs: 13.20;DCAY:14; Fc: 00]								
034540	CONTINUES NASBIDD	1.0 01:0:1	034491	[Previous area: IArea: 4.67;SLLP: 50;LGP: 50;MNF: 250;SCP: 0]								
034550	[CNS: 61.0; No. 3.00; Tpa. 90]		034502	[Impervious area: IArea: 1.57;SLIP: 50;LGR: 326;MNF: 013;SCL: 0]								
034560	[IAREC: 4.00; SMNo: 810.59; SMAX:430.01; Skc: -010]		034513	[IARECmp: 4.00; IAREBcr: 4.00]								
034570	[InterEventTime: 12.00]		034524	R0005:CO1005.....Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm								
034580	R0005:CO1005.....Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm		034535	ROUTE RESEVOIR >	1.0 02:AI:STR	3.51	1.08	N_date	28.29	44.03	n/a	000
034590	ROUTE CHANNEL >	1.0 02:0:1	034546	overFlow >	1.0 01:AI:STR	5.30	1.60	N_date	28.31	44.03	n/a	000
034600	[RFD: 1.00] out <	1.0 01:0:1;R	034557	[MS:otEda: 1109E+00	ml, TotOfVol= 0.0000E+00	ml, NOf= 0, TotDurOf= 0.hrs]						
034610	[L/S:N= 360. / 630.165]		034568	CONTINUES STANDIND	1.0 01:0:1	3.30	.671	N_date	28.02	44.03	771	000
034620	[Vmax: .682;Dmax: .283]		034579	[XMP: 68;TIMP: 85]								
034630	R0005:CO1006.....Dfln=1.D;NIDD.....AREHA-QPEAKm-TpeakDte;hh:mm.....Rvmm.R.C.....DFWcm		034590	[Hydro parameters: Fw: 76.20;Fcs: 13.20;DCAY:14; Fc: 00]								

Table with multiple columns containing technical specifications, numerical values, and alphanumeric codes. Includes entries for ROUTE RESEVER, CONTINUES STAN, ROUTE CHANNEL, and various station identifiers like 03741, 03742, etc.

044889	CNTINUUS STANDBY	1.0 01: KB-11	4.03	584	N_date	28.00	41.88	733	0.000
044890	[X]Mps: 68 [TIMP: 86]								
044891	[Horton parameters: Fw= 76.20; Fc= 13.20; DCAYV: 14; Fc= 00]								
044892	[Major System / 1.0 01: KB-Pond2	25.28	13.528	N_date	28.14	30.40	n/a	0.000	
044893	[Imperious area: IArea= 79.5SLP2+2.00; LG= 164. MN= 013; SCI= 0]								
044894	[IAREG] mps: 4.00; IAREGper: 4.00								
044895	COMPUTE DUAL/D	1.0 01: KB-11	4.03	584	N_date	28.00	41.88	n/a	0.000
044896	[Major System / 1.0 01: KB-11	0.00	0.00	N_date	0.00	n/a	n/a	0.000	
044897	[Minor System / 1.0 01: KB-11	0.00	0.00	N_date	0.00	n/a	n/a	0.000	
044898	[Mjr System / 1.0 01: KB-11	0.00	0.00	N_date	0.00	n/a	n/a	0.000	
044899	[Mj System= 0.0000E+00; TotOfVol= 0.0000E+00; N Of Or= 0; TotDirOf= 0.0]								
044900	R005: CD0222	Dfm: 1D NDD	0.00	0.00	N_date	28.00	41.88	n/a	0.000
044901	ADD HYD	1.0 01: KB-11	0.00	0.00	N_date	0.00	n/a	0.000	
044902	[IAREG] mps: 4.00; IAREGper: 4.00								
045000	R005: CD0227	Dfm: 1D NDD	0.00	0.00	N_date	28.00	41.88	n/a	0.000
045001	ADD HYD	1.0 01: KB-11	0.00	0.00	N_date	0.00	n/a	0.000	
045002	[IAREG] mps: 4.00; IAREGper: 4.00								
045003	SUM	1.0 01: KB-11	0.00	0.00	N_date	28.00	41.88	n/a	0.000
045004	[M]Syst= 0.0000E+00; TotOfVol= 0.0000E+00; N Of Or= 0; TotDirOf= 0.0]								
045005	CNTINUUS STANDBY	1.0 01: KB-11	4.99	892	N_date	28.00	52.49	919	0.000
045006	[X]Mps: 93 [TIMP: 93]								
045007	[Horton parameters: Fw= 76.20; Fc= 13.20; DCAYV: 14; Fc= 00]								
045008	[Imperious area: IArea= 4.67; SLP2+2.00; LG= 40.0; MNP= 250; SCP= 0]								
045009	[Major System / 1.0 01: KB-11	0.00	0.00	N_date	0.00	n/a	n/a	0.000	
045010	[IAREG] mps: 4.00; IAREGper: 4.00								
045111	R005: CD0249	Dfm: 1D NDD	0.00	0.00	N_date	28.00	47.49	831	0.000
045112	CNTINUUS STANDBY	1.0 01: KB-15	2.15	321	N_date	28.00	47.49	831	0.000
045113	[X]Mps: 79 [TIMP: 79]								
045114	[Horton parameters: Fw= 76.20; Fc= 13.20; DCAYV: 14; Fc= 00]								
045115	[Imperious area: IArea= 4.67; SLP2+2.00; LG= 40.0; MNP= 250; SCP= 0]								
045116	[Major System / 1.0 01: KB-15	0.00	0.00	N_date	0.00	n/a	n/a	0.000	
045117	[IAREG] mps: 4.00; IAREGper: 4.00								
045118	R005: CD0250	Dfm: 1D NDD	0.00	0.00	N_date	28.14	20.08	n/a	0.000
045119	ADD HYD	1.0 01: KB-15	41.82	2,624	N_date	28.14	20.08	n/a	0.000
045200	[Major System / 1.0 01: KB-15	0.00	0.00	N_date	0.00	n/a	n/a	0.000	
045201	[Minor System / 1.0 01: KB-15	0.00	0.00	N_date	0.00	n/a	n/a	0.000	
045202	[Mjr System / 1.0 01: KB-15	0.00	0.00	N_date	0.00	n/a	n/a	0.000	
045203	[Mj System= 0.0000E+00; TotOfVol= 0.0000E+00; N Of Or= 0; TotDirOf= 0.0]								
045204	+ 1.0 01: KB-05	5.19	85.70	N_date	28.00	52.49	n/a	0.000	
045205	+ 1.0 01: KB-05	12.93	191.90	N_date	28.00	50.55	n/a	0.000	
045206	+ 1.0 01: KB-05	4.24	71.18	N_date	28.00	41.89	n/a	0.000	
045207	+ 1.0 01: KB-15	2.15	321	N_date	28.00	47.49	n/a	0.000	
045208	[IAREG] mps: 4.00; IAREGper: 4.00								
045209	SUM	1.0 01: KB-15	206.72	14,364	N_date	28.02	27.13	n/a	0.000
045210	[M]Syst= 0.0000E+00; TotOfVol= 0.0000E+00; N Of Or= 0; TotDirOf= 0.0]								
045211	R005: CD0251	Dfm: 1D NDD	206.72	14,364	N_date	28.02	27.13	n/a	0.000
045212	ROUTER RESERVOIR >	1.0 01: KB-P1	206.72	14,364	N_date	28.15	27.13	n/a	0.000
045213	overl	1.0 01: KB-P1	206.72	14,364	N_date	28.15	27.13	n/a	0.000
045214	[M]Syst= 0.0000E+00; TotOfVol= 0.0000E+00; N Of Or= 0; TotDirOf= 0.0]								
045215	R005: CD0252	Dfm: 1D NDD	206.72	14,364	N_date	28.15	27.13	n/a	0.000
045216	ADD HYD	1.0 01: KB-P1	206.72	14,364	N_date	28.15	27.13	n/a	0.000
045217	[IAREG] mps: 4.00; IAREGper: 4.00								
045218	SUM	1.0 01: KB-P1	206.72	14,364	N_date	28.15	27.13	n/a	0.000
045219	R005: CD0253	Dfm: 1D NDD	206.72	14,364	N_date	28.15	27.13	n/a	0.000
045220	SAVE INK Pond1.0005	1.0 01: KB-P1	206.72	14,364	N_date	28.15	27.13	n/a	0.000
045221	remark: Total Flows at KB first pond								
045222	remark: Total Flows at KB third pond								
045223	R005: CD0254	Dfm: 1D NDD	10.86	1,770	N_date	28.00	50.11	877	0.000
045224	CNTINUUS STANDBY	1.0 01: KB-07	10.86	1,770	N_date	28.00	50.11	877	0.000
045225	[X]Mps: 86 [TIMP: 86]								
045226	[Horton parameters: Fw= 76.20; Fc= 13.20; DCAYV: 14; Fc= 00]								
045227	[Imperious area: IArea= 4.67; SLP2+2.00; LG= 40.0; MNP= 250; SCP= 0]								
045228	[Major System / 1.0 01: KB-07	0.00	0.00	N_date	0.00	n/a	n/a	0.000	
045229	[IAREG] mps: 4.00; IAREGper: 4.00								
045230	COMPUTE DUAL/D	1.0 01: KB-07	10.86	1,770	N_date	28.00	50.11	n/a	0.000
045231	[Major System / 1.0 01: KB-07	0.00	0.00	N_date	0.00	n/a	n/a	0.000	
045232	[Minor System / 1.0 01: KB-07	0.00	0.00	N_date	0.00	n/a	n/a	0.000	
045233	[Mjr System= 0.0000E+00; TotOfVol= 0.0000E+00; N Of Or= 0; TotDirOf= 0.0]								
045234	+ 1.0 01: KB-05	5.19	85.70	N_date	28.00	52.49	n/a	0.000	
045235	+ 1.0 01: KB-05	12.93	191.90	N_date	28.00	50.55	n/a	0.000	
045236	+ 1.0 01: KB-05	4.24	71.18	N_date	28.00	41.89	n/a	0.000	
045237	+ 1.0 01: KB-15	2.15	321	N_date	28.00	47.49	n/a	0.000	
045238	[IAREG] mps: 4.00; IAREGper: 4.00								
045239	SUM	1.0 01: KB-P1	206.72	14,364	N_date	28.02	27.13	n/a	0.000
045240	[M]Syst= 0.0000E+00; TotOfVol= 0.0000E+00; N Of Or= 0; TotDirOf= 0.0]								
045241	R005: CD0255	Dfm: 1D NDD	206.72	14,364	N_date	28.02	27.13	n/a	0.000
045242	ROUTER RESERVOIR >	1.0 01: KB-P1	206.72	14,364	N_date	28.02	27.13	n/a	0.000
045243	overl	1.0 01: KB-P1	206.72	14,364	N_date	28.15	27.13	n/a	0.000
045244	[M]Syst= 0.0000E+00; TotOfVol= 0.0000E+00; N Of Or= 0; TotDirOf= 0.0]								
045245	R005: CD0256	Dfm: 1D NDD	206.72	14,364	N_date	28.15	27.13	n/a	0.000
045246	ADD HYD	1.0 01: KB-P1	206.72	14,364	N_date	28.15	27.13	n/a </table	

048863 # fname : SN_RK 0005
048864 remark: Total Flow into before Station 3633
048865 # Hydrograph from Station 3633 to Node Todd
048866 # Channel X Section obtained from RCEA Hydraulic Model Station 3633
048867 # JFSA 2021-02-26 change the channel length (at station 3633) from 650m to 608m and change the slope to 0.0498% to 0.2
048868 #
048869 ROUTES: C00309 ----- Dfma : ID NND ----- AREA: QPEAGm - TpeakDte : hh:mm ----- Rvmm : R.C. ----- Dfcm:
048870 ROUTE CHANNEL > 1.0 0:02:SN BK 54681.13 70.342 NoDate 38:13 18.71 n/a .000
048871 [R/S= 1.00] out c 0.01:TO:TD 54681.13 70.342 NoDate 36:56 18.71 n/a .000
048872 [L/S= 608. / 2477.035]
048873 [D= 1.0]
048874 *****
048875 # Catchment Greenbank
048876 # To Greenbank Drain (south of the Jack)
048877 # - JFSA 2021-01-18 add Greenbank pond as per JFSA P958(04)-15, June 2016
048878 # - JFSA 2021-01-17 update area from 37.479 ha to 36.0 ha based on GIS measurements
048879 #
048880 ROUTES: C00310 ----- Dfma : ID NND ----- AREA: QPEAGm - TpeakDte : hh:mm ----- Rvmm : R.C. ----- Dfcm:
048881 CONTNUS STANNHD 1.0 0:01:TD:MM 3.6 0 3.62 NoDate 28:02 42.39 745 .000
048882 [L/S= 2 Cn= 77.0]
048883 [Previous area: IArea: 4.67:SLP:01.00:LEq: 40. :MNF: 250:SCP: 0]
048884 [Impervious area: IArea: 1.57:SLP:01.00:LEq: 494. :MNF: 013:SCI: 0]
048885 [IARECmp: 4.00: IAREP: 4.00]
048886 [SM N= 31.15: SMW= 207.66: Sk: 010]
048887 *****
048888 ROUTES: C00311 ----- Dfma : ID NND ----- AREA: QPEAGm - TpeakDte : hh:mm ----- Rvmm : R.C. ----- Dfcm:
048889 ROUTE RESERVE R > 1.0 0:02:Greenbank 36.60 3.925 NoDate 28:02 42.59 n/a .000
048890 out c 1.0 0:03:Greenbank 36.60 811 NoDate 28:35 42.58 n/a .000
048891 over flow c 1.0 0:03:Greenbank 36.60 0.00 NoDate 0:00 n/a n/a .000
048892 [MKS:oteds: 769560:04 mb, TotOfVol: 0.0000:00 mb, N.ofA: 0. TotDurOf: 0 hrs]
048893 ROUTES: C00312 ----- Dfma : ID NND ----- AREA: QPEAGm - TpeakDte : hh:mm ----- Rvmm : R.C. ----- Dfcm:
048894 ADD HYD + 1.0 0:02:TD:MN 54681.13 70.342 NoDate 36:56 18.71 n/a .000
048895 + 1.0 0:02:Greenbank 0.00 0.00 NoDate 0:00 n/a n/a .000
048896 + 1.0 0:02:Greenbank 36.60 811 NoDate 28:35 42.58 n/a .000
048897 SIM + 1.0 0:01:SN:TD 54717.73 70.171 NoDate 36:56 18.73 n/a .000
048898 ROUTES: C00313 ----- Dfma : ID NND ----- AREA: QPEAGm - TpeakDte : hh:mm ----- Rvmm : R.C. ----- Dfcm:
048899 SAVE HYD 1.0 0:01:Greenbank 54717.73 70.171 NoDate 36:56 18.73 n/a .000
048900 #
048901 #
048902 #
048903 # Catchment TODD
048904 # - To Todd Drain (south of the Jack)
048905 # - Substn with 436imp: as per Barhaven South MS
048906 # - 2020-11-30 increase imp. based on P958(04)-11
048907 # - 2020-11-30 update area from 146.011 Ha to 146.015 ha based on P958(04)-11
048908 # - 2020-11-30 split TODD Drainage Area to MWLR, MNR, POND and ALL
048909 #
048910 # - JFSA 2021-01-19 add TODD_MNI as part of Clarke(W.C.LAR.M) and remove it from Todd
048911 ROUTES: C00314 ----- Dfma : ID NND ----- AREA: QPEAGm - TpeakDte : hh:mm ----- Rvmm : R.C. ----- Dfcm:
048912 CONTNUS STANNHD 1.0 0:01:TD:MM 12.0 0 12.0 NoDate 28:00 38.41 672 .000
048913 [L/S= 53.73:TM: 57]
048914 [L/S= 2 Cn= 77.0]
048915 [Previous area: IArea: 4.67:SLP:01.00:LEq: 40. :MNF: 250:SCP: 0]
048916 [Impervious area: IArea: 1.57:SLP:01.00:LEq: 118. :MNF: 013:SCI: 0]
048917 [IARECmp: 4.00: IAREP: 4.00]
048918 [SM N= 31.15: SMW= 207.66: Sk: 010]
048919 ROUTES: C00315 ----- Dfma : ID NND ----- AREA: QPEAGm - TpeakDte : hh:mm ----- Rvmm : R.C. ----- Dfcm:
048920 CONTNUS STANNHD 1.0 0:01:TD:MM 12.0 0 12.0 NoDate 28:00 38.39 672 .000
048921 [L/S= 53.73:TM: 57]
048922 [L/S= 2 Cn= 77.0]
048923 [Previous area: IArea: 4.67:SLP:01.00:LEq: 40. :MNF: 250:SCP: 0]
048924 [Impervious area: IArea: 1.57:SLP:01.00:LEq: 28. :MNF: 013:SCI: 0]
048925 [IARECmp: 4.00: IAREP: 4.00]
048926 [SM N= 31.15: SMW= 207.66: Sk: 010]
048927 ROUTES: C00316 ----- Dfma : ID NND ----- AREA: QPEAGm - TpeakDte : hh:mm ----- Rvmm : R.C. ----- Dfcm:
048928 CONTNUS STANNHD 1.0 0:01:TD:MM 30.23 2.959 NoDate 28:02 39.47 691 .000
048929 [L/S= 52:TM: 64]
048930 [L/S= 2 Cn= 77.0]
048931 [Previous area: IArea: 4.67:SLP:01.00:LEq: 40. :MNF: 250:SCP: 0]
048932 [Impervious area: IArea: 1.57:SLP:01.00:LEq: 449. :MNF: 013:SCI: 0]
048933 [IARECmp: 4.00: IAREP: 4.00]
048934 [SM N= 31.15: SMW= 207.66: Sk: 010]
048935 ROUTES: C00317 ----- Dfma : ID NND ----- AREA: QPEAGm - TpeakDte : hh:mm ----- Rvmm : R.C. ----- Dfcm:
048936 CONTNUS STANNHD 1.0 0:01:TD:MM 112.91 9.669 NoDate 28:05 38.19 669 .000
048937 [L/S= 52:TM: 57]
048938 [L/S= 2 Cn= 77.0]
048939 [Previous area: IArea: 4.67:SLP:01.00:LEq: 40. :MNF: 250:SCP: 0]
048940 [Impervious area: IArea: 1.57:SLP:01.00:LEq: 868. :MNF: 013:SCI: 0]
048941 [IARECmp: 4.00: IAREP: 4.00]
048942 [SM N= 31.15: SMW= 207.66: Sk: 010]
048943 ROUTES: C00318 ----- Dfma : ID NND ----- AREA: QPEAGm - TpeakDte : hh:mm ----- Rvmm : R.C. ----- Dfcm:
048944 CONTNUS STANNHD 1.0 0:01:TD:MM 3.06 3.85 NoDate 28:00 41.58 728 .000
048945 [L/S= 53:TM: 63]
048946 [L/S= 2 Cn= 77.0]
048947 [Previous area: IArea: 4.67:SLP:01.00:LEq: 40. :MNF: 250:SCP: 0]
048948 [Impervious area: IArea: 1.57:SLP:01.00:LEq: 143. :MNF: 013:SCI: 0]
048949 [IARECmp: 4.00: IAREP: 4.00]
048950 [SM N= 31.15: SMW= 207.66: Sk: 010]
048951 # 5 Year + 12% Capture
048952 ROUTES: C00319 ----- Dfma : ID NND ----- AREA: QPEAGm - TpeakDte : hh:mm ----- Rvmm : R.C. ----- Dfcm:
048953 ROUTE RESERVE R > 1.0 0:02:TD:MM 30.23 2.959 NoDate 28:02 39.47 n/a .000
048954 + 1.0 0:02:SN BK 30.23 2.959 NoDate 28:02 39.47 n/a .000
048955 over flow c 1.0 0:03:TD:MM 0.00 0.00 NoDate 0:00 n/a n/a .000
048956 [MKS:oteds: 89496:04 mb, TotOfVol: 0.0000:00 mb, N.ofA: 0. TotDurOf: 0 hrs]
048957 # 5 Year + 12% Capture
048958 ROUTES: C00320 ----- Dfma : ID NND ----- AREA: QPEAGm - TpeakDte : hh:mm ----- Rvmm : R.C. ----- Dfcm:
048959 ROUTE RESERVE R > 1.0 0:02:TD:MM 2.10 2.328 NoDate 28:00 38.41 n/a .000
048960 out c 1.0 0:03:TD:MM 2.10 2.328 NoDate 28:00 38.41 n/a .000
048961 over flow c 1.0 0:03:TD:MM 0.00 0.00 NoDate 0:00 n/a n/a .000
048962 [MKS:oteds: 89626:04 mb, TotOfVol: 0.0000:00 mb, N.ofA: 0. TotDurOf: 0 hrs]
048963 ROUTES: C00321 ----- Dfma : ID NND ----- AREA: QPEAGm - TpeakDte : hh:mm ----- Rvmm : R.C. ----- Dfcm:
048964 ROUTE RESERVE R > 1.0 0:02:TD:MM 12.0 0 12.0 NoDate 28:00 38.39 n/a .000
048965 + 1.0 0:02:TD:MM 12.0 0 12.0 NoDate 28:00 38.39 n/a .000
048966 over flow c 1.0 0:03:TD:MM 0.00 0.00 NoDate 0:00 n/a n/a .000
048967 [MKS:oteds: 8651E:04 mb, TotOfVol: 0.0000:00 mb, N.ofA: 0. TotDurOf: 0 hrs]
048968 ROUTES: C00322 ----- Dfma : ID NND ----- AREA: QPEAGm - TpeakDte : hh:mm ----- Rvmm : R.C. ----- Dfcm:
048969 CONTNUS STANNHD 1.0 0:01:TD:MM 25.90 1.991 NoDate 28:03 34.66 607 .000
048970 [L/S= 42:TM: 52]
048971 [L/S= 2 Cn= 77.0]
048972 [Previous area: IArea: 4.67:SLP:01.00:LEq: 40. :MNF: 250:SCP: 0]
048973 [Impervious area: IArea: 1.57:SLP:01.00:LEq: 566. :MNF: 013:SCI: 0]
048974 [IARECmp: 4.00: IAREP: 4.00]
048975 [SM N= 33.81: SMW= 225.43: Sk: 010]
048976 ROUTES: C00323 ----- Dfma : ID NND ----- AREA: QPEAGm - TpeakDte : hh:mm ----- Rvmm : R.C. ----- Dfcm:
048977 COMPUTE DUALHD 1.0 0:01:AD 25.50 1.991 NoDate 28:03 34.66 n/a .000
048978 Mjor System / 1.0 0:02:BM 0.00 0.00 NoDate 0:00 n/a n/a .000
048979 Mjor System \ 1.0 0:03:AD:MN 25.50 1.818 NoDate 28:00 34.70 n/a .000
048980 [M Sys:Tot: 5163:00:00, TotOfVol: 0.0000:00, N.ofA: 0. TotDurOf: 0 hrs]
048981 ROUTES: C00324 ----- Dfma : ID NND ----- AREA: QPEAGm - TpeakDte : hh:mm ----- Rvmm : R.C. ----- Dfcm:
048982 ADD HYD + 1.0 0:02:TD:MM 2.10 2.328 NoDate 28:00 38.41 n/a .000
048983 + 1.0 0:02:TD:MM 2.10 2.328 NoDate 28:00 38.41 n/a .000
048984 + 1.0 0:02:TD:MM 12.0 0 12.0 NoDate 28:00 38.39 n/a .000
048985 + 1.0 0:02:TD:MM 12.0 0 12.0 NoDate 28:00 38.39 n/a .000
048986 + 1.0 0:02:CLAR.MJ 112.91 9.669 NoDate 28:05 38.19 n/a .000
048987 + 1.0 0:02:CLAR.MJ 112.91 9.669 NoDate 28:05 38.19 n/a .000
048988 + 1.0 0:02:CLAR.MJ 112.91 9.669 NoDate 28:05 38.19 n/a .000
048989 ROUTES: C00325 ----- Dfma : ID NND ----- AREA: QPEAGm - TpeakDte : hh:mm ----- Rvmm : R.C. ----- Dfcm:
048990 SAVE HYD 1.0 0:01:SN:TD 54737.09 70.373 NoDate 36:55 18.77 n/a .000
048991 #
048992 #
048993 #
048994 # Todd Pond
048995 # - Rate of capture obtained from Barhaven South MS modelling
048996 # - stantec 2007, Tributary Drainage Area to MESS Pond 3 = 193 ha
048997 #
048998 ROUTES: C00326 ----- Dfma : ID NND ----- AREA: QPEAGm - TpeakDte : hh:mm ----- Rvmm : R.C. ----- Dfcm:
048999 ROUTE RESERVE R > 1.0 0:02:TD:MM 119.95 9.538 NoDate 28:04 38.27 n/a .000
049000 out c 1.0 0:03:PF:DF 119.95 9.538 NoDate 28:04 38.27 n/a .000
049001 over flow c 1.0 0:03:PF:DF 0.00 0.00 NoDate 0:00 n/a n/a .000
049002 [MKS:oteds: 22511:00 mb, TotOfVol: 0.0000:00 mb, N.ofA: 0. TotDurOf: 0 hrs]
049003 ROUTES: C00327 ----- Dfma : ID NND ----- AREA: QPEAGm - TpeakDte : hh:mm ----- Rvmm : R.C. ----- Dfcm:
049004 ADD HYD + 1.0 0:02:SM:PF 54737.09 70.373 NoDate 36:55 18.77 n/a .000
049005 + 1.0 0:02:SM:PF 119.95 9.538 NoDate 28:04 38.27 n/a .000
049006 + 1.0 0:02:PF:DF 0.00 0.00 NoDate 0:00 n/a n/a .000
049007 + 1.0 0:02:TD:MM 0.00 0.00 NoDate 0:00 n/a n/a .000
049008 + 1.0 0:02:AC:M 0.00 0.00 NoDate 0:00 n/a n/a .000
049009 SIM + 1.0 0:01:SN:TD 54837.69 70.373 NoDate 36:55 18.77 n/a .000
049010 ROUTES: C00328 ----- Dfma : ID NND ----- AREA: QPEAGm - TpeakDte : hh:mm ----- Rvmm : R.C. ----- Dfcm:
049011 SAVE HYD 1.0 0:01:SN:TD 54837.69 70.373 NoDate 36:55 18.77 n/a .000
049012 #
049013 #
049014 #
049015 # Hydrograph from Todd Drain routed to Corrigan Drain
049016 # Channel X Section obtained from RCEA Hydraulic Model Station 2462
049017 # 2021-02-19 Change the slope from 0.033 % (as per Stantec Report 2007) to 0.05 % so the model will be more stable and g
049018 ROUTES: C00329 ----- Dfma : ID NND ----- AREA: QPEAGm - TpeakDte : hh:mm ----- Rvmm : R.C. ----- Dfcm:
049019 ROUTE CHANNEL > 1.0 0:02:SN:TD 54837.69 70.373 NoDate 36:55 18.77 n/a .000
049020 + [R/S= 1.00] out c 0.01:TO:TD 54837.69 70.373 NoDate 37:09 18.77 n/a .000
049021 [L/S= 280. / 1050.0]
049022 [D= 1.0]
049023 [Vms: 827:DM: 2.568]
049024 ROUTES: C00330 ----- Dfma : ID NND ----- AREA: QPEAGm - TpeakDte : hh:mm ----- Rvmm : R.C. ----- Dfcm:
049025 CONTNUS STANNHD 1.0 0:01:TD:MM 54837.69 70.373 NoDate 37:09 18.77 n/a .000
049026 SAVE HYD 1.0 0:01:SN:TD 54837.69 70.373 NoDate 37:09 18.77 n/a .000
049027 #
049028 #
049029 #
049030 # Catchment CORRIGAN
049031 # - Primarily Developed (medium density)
049032 # - JFSA JAN 2021 add Corrigan catchments as per I.B. July 2008
049033 ROUTES: C00331 ----- Dfma : ID NND ----- AREA: QPEAGm - TpeakDte : hh:mm ----- Rvmm : R.C. ----- Dfcm:
049034 CONTNUS STANNHD 1.0 0:01:corr1 15.87 1.806 NoDate 28:01 41.58 728 .000
049035 [L/S= 53:TM: 63]
049036 [L/S= 2 Cn= 77.0]
049037 [Previous area: IArea: 4.67:SLP:01.00:LEq: 40. :MNF: 250:SCP: 0]
049038 [Impervious area: IArea: 1.57:SLP:01.00:LEq: 325. :MNF: 013:SCI: 0]
049039 [IARECmp: 4.00: IAREP: 4.00]
049040 [SM N= 31.15: SMW= 207.66: Sk: 010]
049041 ROUTES: C00332 ----- Dfma : ID NND ----- AREA: QPEAGm - TpeakDte : hh:mm ----- Rvmm : R.C. ----- Dfcm:
049042 COMPUTE DUALHD 1.0 0:01:AD 15.87 1.806 NoDate 28:01 41.58 n/a .000
049043 Mjor System / 1.0 0:02:corr1:M 0.00 0.00 NoDate 0:00 n/a n/a .000
049044 Mjor System \ 1.0 0:03:corr1:M 15.87 1.806 NoDate 28:01 41.58 n/a .000
049045 [M Sys:Tot: 0000:00:00, TotOfVol: 0.0000:00, N.ofA: 0. TotDurOf: 0 hrs]
049046 ROUTES: C00333 ----- Dfma : ID NND ----- AREA: QPEAGm - TpeakDte : hh:mm ----- Rvmm : R.C. ----- Dfcm:
049047 CONTNUS STANNHD 1.0 0:01:corr1 12.47 1.61 NoDate 29:11 21.09 380 .000
049048 [Cn= 77.0: No: 3.00: Tp: 10]
049049 [IAREC: 4.00: SM N= 31.15: SMW= 207.66: Sk: 010]

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052375 [SMN= 33.81; SMOX=225.43; SSK= 010] -----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
052388 R0005-CO0187-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
052399 COMPUTE DUALJHD / 1.0 01:41 7.60 638 N_date 28:02 34.82 n/a 0000
052400 Mjr System / 1.0 02:36:MM 7.60 638 N_date 28:02 34.82 n/a 0000
052411 Mnor System / 1.0 03:48:MM 7.60 638 N_date 28:02 34.82 n/a 0000
052423 [M$YSStm=0000E00; TotOfVol=0000E00; NOf= 0; TotDirOf= 0; hrs] -----Rvmm R.C.-Dwfcm
052443 R0005-CO0187-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
052444 ADD IHD / 1.0 02:36:MM 17.90 1183 N_date 28:06 34.84 n/a 0000
052445 Mjr System / 1.0 02:36:MM 7.20 638 N_date 28:02 34.82 n/a 0000
052446 Mnor System / 1.0 01:MM:AO 25.50 1761 N_date 28:05 34.83 n/a 0000
052478 R0005-CO0369-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
052488 SAVE IHD / 1.0 01:MM:AO 25.50 1761 N_date 28:05 34.83 n/a 0000
052490 #fname: MH04.0005
052491 remark: Total Flows at MH04
052511 R0005-CO0370-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
052529 ROUTE PIPE / 1.0 02:36:MM 25.50 1761 N_date 28:05 34.83 n/a 0000
052533 [RDR= 1.00] out < / 1.0 01:340:104 25.50 1.698 N_date 28:06 34.83 n/a 0000
052544 [L/S= 240 / 150] 013]
052555 [Vmax= 1.636; Dmax= 1.1]
052565 [D= 1.65; Dused= 1.65]
052575 R0005-CO0397-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
052588 ADD IHD / 1.0 02:34:104 25.50 1.698 N_date 28:06 34.83 n/a 0000
052590 #fname: MH04.0005
052591 Mjr System / 1.0 01:MM:AO 107.02 623 N_date 28:04 35.37 n/a 0000
052592 Mnor System / 1.0 01:MM:AO 132.52 9.463 N_date 28:04 35.27 n/a 0000
052611 R0005-CO0372-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
052628 ROUTE PIPE / 1.0 02:36:MM 132.92 9.463 N_date 28:04 35.27 n/a 0000
052633 # [RDR= 1.00] out < / 1.0 01:104:105 132.52 8.848 N_date 28:06 35.27 n/a 0000
052644 [L/S= 380 / 100] 013]
052655 [Vmax= 2.012; Dmax= 1.868]
052665 [RDR= 2.20; Dmax= 1.868]
052675 R0005-CO0400-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
052688 CONTINUES STANDBY / 1.0 01:41 2.20 248 N_date 28:00 38.90 681 0000
052699 [L/MS= 7.1; T/MS= 57]
052700 [LRS= 2 / Cn= 75.0]
052711 [Pervious area: IApr= 4.67; SLLP=1.00; LQP= 40; MNP= 250; SCP= 0]
052722 [Impervious area: IApr= 1.57; SLLP=1.00; LQP= 187; MN= 013; SCI= 0]
052733 [IARCCmp= 4.00; IARCCorr= 4.00]
052744 [SMN= 33.81; SMOX=225.43; SSK= 010]
052755 R0005-CO0374-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
052768 COMPUTE DUALJHD / 1.0 01:41 2.20 248 N_date 28:00 38.90 n/a 0000
052779 Mjr System / 1.0 02:36:MM 0.00 000 N_date 00:00 0.00 n/a 0000
052780 Mnor System / 1.0 02:36:MM 0.00 000 N_date 28:00 38.90 n/a 0000
052791 [M$YSStm=0000E00; TotOfVol=0000E00; NOf= 0; TotDirOf= 0; hrs] -----Rvmm R.C.-Dwfcm
052801 R0005-CO0375-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
052811 CONTINUES STANDBY / 1.0 01:41 2.20 248 N_date 28:00 38.90 n/a 0000
052823 [L/MS= 7.1; T/MS= 71]
052833 [LRS= 2 / Cn= 75.0]
052844 [Pervious area: IApr= 4.67; SLLP=1.00; LQP= 40; MNP= 250; SCP= 0]
052855 [Impervious area: IApr= 1.57; SLLP=1.00; LQP= 186; MN= 013; SCI= 0]
052866 [IARCCmp= 4.00; IARCCorr= 4.00]
052877 [SMN= 33.81; SMOX=225.43; SSK= 010]
052888 R0005-CO0380-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
052899 ADD IHD / 1.0 02:36:MM 9.6 130 N_date 28:00 44.32 n/a 0000
052900 #fname: MH04.0005
052901 Mjr System / 1.0 01:MM:AO 9.6 130 N_date 28:00 44.32 n/a 0000
052902 Mnor System / 1.0 01:MM:AO 9.6 130 N_date 28:00 44.32 n/a 0000
052911 R0005-CO0377-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
052928 COMPUTE DUALJHD / 1.0 01:41 2.20 248 N_date 28:00 44.32 n/a 0000
052939 Mjr System / 1.0 02:36:MM 0.00 000 N_date 00:00 0.00 n/a 0000
052940 Mnor System / 1.0 02:36:MM 0.00 000 N_date 28:00 44.32 n/a 0000
052951 [M$YSStm=0000E00; TotOfVol=0000E00; NOf= 0; TotDirOf= 0; hrs] -----Rvmm R.C.-Dwfcm
052961 R0005-CO0378-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
052978 ADD IHD / 1.0 02:34:104 132.52 8.848 N_date 28:06 35.27 n/a 0000
052989 #fname: MH04.0005
052990 Mjr System / 1.0 02:36:MM 2.20 248 N_date 28:00 38.90 n/a 0000
052991 Mnor System / 1.0 02:36:MM 0.00 000 N_date 28:00 44.32 n/a 0000
053001 # [RDR= 1.00] out < / 1.0 02:TRD:MMJ 0.00 000 N_date 00:00 0.00 n/a 0000
053023 [L/S= 100 / 100] 013]
053033 R0005-CO0379-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
053044 SAVE IHD / 1.0 01:MM:AO 135.68 9.064 N_date 28:05 35.39 n/a 0000
053055 #fname: MH05.0005
053066 remark: Total Flows at MH05
053075 R0005-CO0383-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
053088 # DIVERG IHD / 1.0 01:48:MM 0.00 000 N_date 00:00 0.00 n/a 0000
053089 #diverged < / 1.0 02:36:MM 0.00 000 N_date 28:00 44.32 n/a 0000
053100 #diverged < / 1.0 03:48:MM 0.00 000 N_date 00:00 0.00 n/a 0000
053111 R0005-CO0381-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
053122 # DIVERG IHD / 1.0 01:48:MM 0.00 000 N_date 00:00 0.00 n/a 0000
053133 #diverged < / 1.0 02:36:MM 0.00 000 N_date 28:05 35.39 n/a 0000
053144 #diverged < / 1.0 03:48:MM 0.00 000 N_date 28:00 44.32 n/a 0000
053155 R0005-CO0382-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
053166 CONTINUES STANDBY / 1.0 01:41 7.19 661 N_date 28:01 34.82 610 0000
053177 [L/MS= 41; T/MS= 54]
053188 [LRS= 2 / Cn= 75.0]
053199 [Pervious area: IApr= 4.67; SLLP=1.00; LQP= 40; MNP= 250; SCP= 0]
053200 [Impervious area: IApr= 1.57; SLLP=1.00; LQP= 211; MN= 013; SCI= 0]
053211 [IARCCmp= 4.00; IARCCorr= 4.00]
053222 [SMN= 33.81; SMOX=225.43; SSK= 010]
053233 R0005-CO0383-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
053244 ADD IHD / 1.0 02:36:MM 7.19 661 N_date 28:01 34.82 n/a 0000
053255 #fname: MH05.0005
053266 COMPUTE DUALJHD / 1.0 01:41 7.19 661 N_date 28:01 34.82 n/a 0000
053277 Mjr System / 1.0 02:36:MM 7.19 661 N_date 28:01 34.82 n/a 0000
053278 Mnor System / 1.0 02:36:MM 7.19 661 N_date 28:01 34.82 n/a 0000
053289 [M$YSStm=0005E00; TotOfVol=0000E00; NOf= 0; TotDirOf= 0; hrs] -----Rvmm R.C.-Dwfcm
053300 R0005-CO0385-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
053311 ROUTE PIPE / 1.0 02:36:MM 110.61 3.005 N_date 28:05 35.39 n/a 0000
053344 [RDR= 1.00] out < / 1.0 01:360:106A 7.19 615 N_date 28:05 34.89 n/a 0000
053355 [L/S= 187 / 100] 013]
053366 [Vmax= 1.098; Dmax= 1.0]
053377 [D= 1.05; Dused= 1.05]
053388 R0005-CO0386-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
053399 CONTINUES STANDBY / 1.0 01:41 3.29 315 N_date 28:00 34.82 610 0000
053410 [L/MS= 7.1; T/MS= 54]
053421 [LRS= 2 / Cn= 75.0]
053432 [Pervious area: IApr= 4.67; SLLP=1.00; LQP= 40; MNP= 250; SCP= 0]
053443 [Impervious area: IApr= 1.57; SLLP=1.00; LQP= 148; MN= 013; SCI= 0]
053454 [IARCCmp= 4.00; IARCCorr= 4.00]
053465 [SMN= 33.81; SMOX=225.43; SSK= 010]
053476 R0005-CO0387-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
053487 COMPUTE DUALJHD / 1.0 01:41 7.19 661 N_date 28:01 34.82 n/a 0000
053488 Mjr System / 1.0 02:36:MM 0.00 000 N_date 00:00 0.00 n/a 0000
053489 Mnor System / 1.0 03:48:MM 3.29 664 N_date 27:39 34.87 n/a 0000
053490 [M$YSStm=2841E00; TotOfVol=0000E00; NOf= 0; TotDirOf= 0; hrs] -----Rvmm R.C.-Dwfcm
053511 R0005-CO0388-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
053523 CONTINUES STANDBY / 1.0 01:41 32.50 2.843 N_date 28:02 35.73 626 0000
053533 [L/MS= 50; T/MS= 50]
053544 [LRS= 2 / Cn= 75.0]
053555 [Pervious area: IApr= 4.67; SLLP=1.00; LQP= 40; MNP= 250; SCP= 0]
053566 [Impervious area: IApr= 1.57; SLLP=1.00; LQP= 465; MN= 013; SCI= 0]
053577 [IARCCmp= 4.00; IARCCorr= 4.00]
053588 [SMN= 36.67; SMOX=244.49; SSK= 010]
053599 R0005-CO0389-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
053610 COMPUTE DUALJHD / 1.0 01:41 32.50 2.843 N_date 28:02 35.73 n/a 0000
053611 Mjr System / 1.0 02:36:MM 0.00 000 N_date 00:00 0.00 n/a 0000
053612 Mnor System / 1.0 02:36:MM 32.50 2.278 N_date 27:37 35.73 n/a 0000
053623 [M$YSStm=2310E00; TotOfVol=0000E00; NOf= 0; TotDirOf= 0; hrs] -----Rvmm R.C.-Dwfcm
053644 R0005-CO0390-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
053655 ADD IHD / 1.0 02:36:MM 0.00 000 N_date 00:00 0.00 n/a 0000
053666 #fname: MH04.0005
053677 #fname: MH04.0005
053688 #fname: MH04.0005
053699 #fname: MH04.0005
053710 #fname: MH04.0005
053721 R0005-CO0391-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
053732 COMPUTE DUALJHD / 1.0 01:41 32.50 2.843 N_date 27:39 34.87 n/a 0000
053743 Mjr System / 1.0 02:36:MM 0.00 000 N_date 00:00 0.00 n/a 0000
053754 Mnor System / 1.0 03:48:MM 3.29 664 N_date 27:39 34.87 n/a 0000
053765 [M$YSStm=0000E00; TotOfVol=0000E00; NOf= 0; TotDirOf= 0; hrs] -----Rvmm R.C.-Dwfcm
053776 R0005-CO0392-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
053787 ROUTE PIPE / 1.0 02:36:MM 110.61 3.005 N_date 28:05 35.39 n/a 0000
053800 [RDR= 1.00] out < / 1.0 01:105:106A 110.61 3.005 N_date 28:08 35.39 n/a 0000
053811 [L/S= 208 / 100] 013]
053822 [D= 1.80; Dused= 1.80]
053833 R0005-CO0393-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
053844 ADD IHD / 1.0 02:36:106A 7.19 615 N_date 28:05 34.89 n/a 0000
053855 #fname: MH04.0005
053866 #fname: MH04.0005
053877 #fname: MH04.0005
053888 #fname: MH04.0005
053899 R0005-CO0394-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
053910 SAVE IHD / 1.0 01:MM:AO 121.09 3.682 N_date 28:05 35.35 n/a 0000
053921 #fname: MH06A.0005
053922 remark: Total Flows at MH06A
053933 R0005-CO0395-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
053944 ROUTE PIPE / 1.0 02:36:MM 121.09 3.682 N_date 28:05 35.35 n/a 0000
053955 # [RDR= 1.00] out < / 1.0 01:106A:106 121.09 3.682 N_date 28:05 35.35 n/a 0000
053966 [L/S= 190 / 100] 013]
053977 [Vmax= 1.633; Dmax= 1.1]
053988 [D= 1.80; Dused= 1.81]
053999 R0005-CO0396-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
054010 CONTINUES STANDBY / 1.0 01:41 2.44 316 N_date 28:00 44.32 776 0000
054021 [LRS= 2 / Cn= 75.0]
054033 [Pervious area: IApr= 4.67; SLLP=1.00; LQP= 40; MNP= 250; SCP= 0]
054044 [Impervious area: IApr= 1.57; SLLP=1.00; LQP= 262; MN= 013; SCI= 0]
054055 [IARCCmp= 4.00; IARCCorr= 4.00]
054066 [SMN= 33.81; SMOX=225.43; SSK= 010]
054077 R0005-CO0401-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
054088 COMPUTE DUALJHD / 1.0 01:41 2.44 316 N_date 28:00 44.32 n/a 0000
054089 Mjr System / 1.0 02:36:MM 2.44 316 N_date 28:00 44.32 n/a 0000
054090 Mnor System / 1.0 03:48:MM 2.44 316 N_date 28:00 44.32 n/a 0000
054101 #fname: MH06A.0005
054112 R0005-CO0398-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
054123 ADD IHD / 1.0 02:36:MM 2.44 316 N_date 28:00 44.32 n/a 0000
054144 #fname: MH06A.0005
054155 R0005-CO0399-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
054166 SAVE IHD / 1.0 01:MM:AO 123.53 3.896 N_date 28:03 35.52 n/a 0000
054177 #fname: MH06.0005
054188 remark: Total Flows at MH06
054199 R0005-CO0402-----Dfna-ID-NDND-----AREBA-QPEAKm-TpeakDate-hh:mm-----Rvmm R.C.-Dwfcm
054210 ROUTE PIPE / 1.0 02:36:MM 123.53 3.896 N_date 28:03 35.52 n/a 0000
054221 # [RDR= 1.00] out < / 1.0 01:1106:107 123.53 3.814 N_date 28:07 35.52 n/a 0000
054232 [L/S= 123 / 100] 013]
054243 [Vmax= 1.656; Dmax= 1.316]

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056113 # - To Jock River (north of the Jock)
056128 # Rural water substation (Desire Community)
056133 # *****
056149 # *****
056150 # *****
056151 # *****
056160 # *****
056175 # *****
056189 # *****
056199 # *****
056200 # *****
056211 # *****
056225 # *****
056233 # *****
056245 # *****
056255 # *****
056260 # *****
056278 # *****
056289 # *****
056300 # *****
056318 # *****
056323 # *****
056333 # *****
056344 # *****
056355 # *****
056368 # *****
056377 # *****
056388 # *****
056399 # *****
056409 # *****
056411 # *****
056425 # *****
056433 # *****
056444 # *****
056458 # *****
056466 # *****
056478 # *****
056489 # *****
056500 # *****
056511 # *****
056528 # *****
056539 # *****
056549 # *****
056558 # *****
056569 # *****
056579 # *****
056589 # *****
056599 # *****
056601 # *****
056628 # *****
056633 # *****
056644 # *****
056658 # *****
056669 # *****
056679 # *****
056688 # *****
056699 # *****
056700 # *****
056711 # *****
056728 # *****
056733 # *****
056744 # *****
056755 # *****
056766 # *****
056777 # *****
056788 # *****
056799 # *****
056800 # *****
056811 # *****
056828 # *****
056833 # *****
056844 # *****
056855 # *****
056866 # *****
056877 # *****
056888 # *****
056899 # *****
056900 # *****
056911 # *****
056928 # *****
056933 # *****
056944 # *****
056955 # *****
056966 # *****
056977 # *****
056988 # *****
056999 # *****
057000 # *****
057011 # *****
057028 # *****
057033 # *****
057044 # *****
057055 # *****
057066 # *****
057077 # *****
057088 # *****
057099 # *****
057100 # *****
057111 # *****
057128 # *****
057133 # *****
057144 # *****
057155 # *****
057166 # *****
057177 # *****
057188 # *****
057199 # *****
057200 # *****
057211 # *****
057228 # *****
057233 # *****
057244 # *****
057255 # *****
057266 # *****
057277 # *****
057288 # *****
057299 # *****
057300 # *****
057311 # *****
057328 # *****
057333 # *****
057344 # *****
057355 # *****
057366 # *****
057377 # *****
057388 # *****
057399 # *****
057400 # *****
057411 # *****
057428 # *****
057433 # *****
057444 # *****
057455 # *****
057466 # *****
057477 # *****
057488 # *****
057499 # *****
057500 # *****
057511 # *****
057528 # *****
057533 # *****
057544 # *****
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057777 # *****
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057833 # *****
057844 # *****
057855 # *****
057866 # *****
057877 # *****
057888 # *****
057899 # *****
057900 # *****
057911 # *****
057928 # *****
057933 # *****
057944 # *****
057955 # *****
057966 # *****
057977 # *****

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059855 # (Approximated cross-section - see cross-section 258)
059856 # Use method for routing conditions and node 025 for spring conditions
059857 #
059858 # Sum of hydrographs from Node 12 routed to Node 11 with Dumpy section 248
059859 #
059900 R010: C00038 -> DfIn-ID NND -> AREQA-QPEAKm-TPeakDate-hh-mm-RvM-R-C--DFWCm
059901 ROUTE CHANNEL -> 1.0 02: S_N2 9506.00 12.534 NoDate 22:45 19.65 n/a 000
059902 [RDE: 1.00] out-c 1.0 01: N0 9506.00 12.710 NoDate 33:02 19.65 n/a 000
059903 [L/S= 972 / 054/ 040]
059904 [Vmax = 680; Dmax = 2.98]
059905 #
059906 # Addition of Subwatershed 11 and No Name Creek to Node 11
059907 #
059908 R010: C00039 -> DfIn-ID NND -> AREQA-QPEAKm-TPeakDate-hh-mm-RvM-R-C--DFWCm
059909 ADD HYD + 1.0 02: N0 9506.00 12.710 NoDate 33:02 19.65 n/a 000
060000 + 1.0 02: SW10 500.00 5.639 NoDate 29:22 21.19 n/a 000
060001 + 1.0 02: NC_CK 1917.00 7.897 NoDate 34:28 21.19 n/a 000
060002 + 1.0 01: S_N1 11923.00 21.813 NoDate 33:05 19.96 n/a 000
060003 #
060004 # Sum of hydrographs from Node 11 routed to Node 10
060005 # Section 7
060006 R010: C00040 -> DfIn-ID NND -> AREQA-QPEAKm-TPeakDate-hh-mm-RvM-R-C--DFWCm
060007 ROUTE CHANNEL -> 1.0 02: S_N1 11923.00 21.813 NoDate 33:05 19.96 n/a 000
060008 [RDE: 1.00] out-c 1.0 01: N0 11923.00 14.761 NoDate 39:58 19.96 n/a 000
060009 [L/S= 14028 / 157/ 040]
060010 [Vmax = 452; Dmax = 1.212]
060011 #
060012 # Addition of Subwatershed 10 to Node 10
060013 #
060014 R010: C00041 -> DfIn-ID NND -> AREQA-QPEAKm-TPeakDate-hh-mm-RvM-R-C--DFWCm
060015 ADD HYD + 1.0 02: N0 11923.00 14.761 NoDate 39:58 19.96 n/a 000
060016 + 1.0 02: SW10 3066.00 21.255 NoDate 37:58 24.81 n/a 000
060017 + 1.0 02: NC_CK 17589.00 35.808 NoDate 38:35 21.52 n/a 000
060018 + 1.0 01: S_N0 17589.00 35.808 NoDate 38:35 21.52 n/a 000
060019 R010: C00042 -> DfIn-ID NND -> AREQA-QPEAKm-TPeakDate-hh-mm-RvM-R-C--DFWCm
060020 SAVE HYD 1.0 01: S_N0 17589.00 35.808 NoDate 38:35 21.52 n/a 000
060021 frame -H,SNO
060022 remark:flow at S_N0: N0 + SW10
060023 # Addition of Kings Creek to S_N10
060024 #
060025 R010: C00043 -> DfIn-ID NND -> AREQA-QPEAKm-TPeakDate-hh-mm-RvM-R-C--DFWCm
060026 ADD HYD + 1.0 02: N0 17589.00 35.808 NoDate 38:35 21.52 n/a 000
060027 + 1.0 02: NC_CK 8376.00 20.398 NoDate 39:59 21.19 n/a 000
060028 + 1.0 01: N0A 25965.00 55.807 NoDate 39:58 21.41 n/a 000
060029 #
060030 # Sum of hydrographs from Node 10 routed to Node 9
060031 # Section 7
060032 #
060033 R010: C00044 -> DfIn-ID NND -> AREQA-QPEAKm-TPeakDate-hh-mm-RvM-R-C--DFWCm
060034 ROUTE CHANNEL -> 1.0 02: S_N0A 25965.00 55.807 NoDate 39:58 21.41 n/a 000
060035 [RDE: 1.00] out-c 1.0 01: N0 25965.00 54.076 NoDate 39:59 21.41 n/a 000
060036 [L/S= 3082 / 074/ 040]
060037 [Vmax = 682; Dmax = 1.095]
060038 #
060039 # Addition of Subwatershed 9 and Nichols Creek to Node 9
060040 #
060041 R010: C00045 -> DfIn-ID NND -> AREQA-QPEAKm-TPeakDate-hh-mm-RvM-R-C--DFWCm
060042 ADD HYD + 1.0 02: N0 25965.00 54.076 NoDate 39:59 21.41 n/a 000
060043 + 1.0 02: SW10 1132.00 8.921 NoDate 30:54 23.73 n/a 000
060044 + 1.0 02: NC_CK 4464.00 10.128 NoDate 39:59 19.29 n/a 000
060045 + 1.0 01: S_N0 31561.00 66.284 NoDate 39:59 21.20 n/a 000
060046 #
060047 # Sum of hydrographs from Node 9 routed to Node 8
060048 # Section 7
060049 #
060050 R010: C00046 -> DfIn-ID NND -> AREQA-QPEAKm-TPeakDate-hh-mm-RvM-R-C--DFWCm
060051 ROUTE CHANNEL -> 1.0 02: S_N 31561.00 66.284 NoDate 39:59 21.20 n/a 000
060052 [RDE: 1.00] out-c 1.0 01: N0 31561.00 61.483 NoDate 39:57 21.20 n/a 000
060053 [L/S= 2209 / 088/ 045]
060054 [Vmax = 363; Dmax = 1.619]
060055 #
060056 # Addition of Subwatershed 8 and Hobb's Drain to Node 8
060057 #
060058 R010: C00047 -> DfIn-ID NND -> AREQA-QPEAKm-TPeakDate-hh-mm-RvM-R-C--DFWCm
060059 ADD HYD + 1.0 02: N0 31561.00 61.483 NoDate 39:57 21.20 n/a 000
060060 + 1.0 02: SW10 131.00 1.689 NoDate 30:54 23.73 n/a 000
060061 + 1.0 02: HB_DR 3854.00 11.813 NoDate 38:37 21.19 n/a 000
060062 + 1.0 01: S_N 35546.00 73.344 NoDate 39:57 21.19 n/a 000
060063 #
060064 # Sum of hydrographs from Node 8 routed to Node 7
060065 # Section 4
060066 #
060067 R010: C00048 -> DfIn-ID NND -> AREQA-QPEAKm-TPeakDate-hh-mm-RvM-R-C--DFWCm
060068 ROUTE CHANNEL -> 1.0 02: S_N 35546.00 73.344 NoDate 39:57 21.19 n/a 000
060069 [RDE: 1.00] out-c 1.0 01: N0 35546.00 61.416 NoDate 45:01 21.19 n/a 000
060070 [L/S= 3750 / 053/ 070]
060071 [Vmax = 218; Dmax = 1.987]
060072 #
060073 # Addition of Subwatershed 7 to Node 7
060074 #
060075 R010: C00049 -> DfIn-ID NND -> AREQA-QPEAKm-TPeakDate-hh-mm-RvM-R-C--DFWCm
060076 ADD HYD + 1.0 02: N0 35546.00 61.416 NoDate 45:01 21.19 n/a 000
060077 + 1.0 02: SW7 3197.00 8.899 NoDate 36:26 17.07 n/a 000
060078 + 1.0 01: S_N 38743.00 65.819 NoDate 44:06 20.85 n/a 000
060079 R010: C00050 -> DfIn-ID NND -> AREQA-QPEAKm-TPeakDate-hh-mm-RvM-R-C--DFWCm
060080 SAVE HYD 1.0 01: S_N 38743.00 65.819 NoDate 44:06 20.85 n/a 000
060081 frame -H,SNT
060082 remark:flow at S_N: N0 + SW7
060083 # Insertion of a reservoir to simulate the effects of the Richmond Fen
060084 # Storage area and volumes were estimated from available top maps.
060085 # Release rate from Fen was assumed to be controlled by the downstream
060086 # river cross section for summer conditions. It is assumed that for up to
060087 # 0.75 m of water, the main channel of the river provided the storage. Above
060088 # this depth, the wetland starts to significantly store water.
060089 #
060090 R010: C00051 -> DfIn-ID NND -> AREQA-QPEAKm-TPeakDate-hh-mm-RvM-R-C--DFWCm
060091 ROUTE RESERVOIR -> 1.0 02: S_N 38743.00 65.819 NoDate 44:06 20.85 n/a 000
060092 [RDE: 1.00] out-c 1.0 01: RES_RF 38743.00 31.796 NoDate 60:32 20.85 n/a 000
060093 [MS: 0.02m; 25070.00]
060094 R010: C00052 -> DfIn-ID NND -> AREQA-QPEAKm-TPeakDate-hh-mm-RvM-R-C--DFWCm
060095 SAVE HYD 1.0 01: RES_RF 38743.00 31.796 NoDate 60:32 20.85 n/a 000
060096 frame -H,RES_RF
060097 remark:outflow from Richmond Fen
060098 #
060099 # Sum of hydrographs from Node 7 routed to Node 6
060100 # Section 7
060101 #
060102 R010: C00053 -> DfIn-ID NND -> AREQA-QPEAKm-TPeakDate-hh-mm-RvM-R-C--DFWCm
060103 ROUTE CHANNEL -> 1.0 02: S_N 38743.00 31.796 NoDate 60:32 20.85 n/a 000
060104 [RDE: 1.00] out-c 1.0 01: N0 38743.00 31.737 NoDate 62:00 20.85 n/a 000
060105 [L/S= 1852 / 083/ 040]
060106 [Vmax = 477; Dmax = 960]
060107 #
060108 # Addition of Subwatershed 6 and Van Gail Drain to Node 6
060109 #
060110 R010: C00054 -> DfIn-ID NND -> AREQA-QPEAKm-TPeakDate-hh-mm-RvM-R-C--DFWCm
060111 ADD HYD + 1.0 02: N0 38743.00 31.737 NoDate 62:00 20.85 n/a 000
060112 + 1.0 02: SW5 224.00 2.546 NoDate 28:45 28.24 n/a 000
060113 + 1.0 02: ML_CR 1821.00 11.195 NoDate 30:48 20.72 n/a 000
060114 + 1.0 02: PL_CK 4945.00 28.945 NoDate 33:21 25.81 n/a 000
060115 + 1.0 01: S_N 40240.00 31.737 NoDate 62:00 20.99 n/a 000
060116 #
060117 # Sum of hydrographs from Node 6 routed to Node 5
060118 # Section 6
060119 R010: C00055 -> DfIn-ID NND -> AREQA-QPEAKm-TPeakDate-hh-mm-RvM-R-C--DFWCm
060120 ROUTE CHANNEL -> 1.0 02: S_N 40240.00 31.737 NoDate 62:48 20.99 n/a 000
060121 [RDE: 1.00] out-c 1.0 01: N0 40240.00 31.713 NoDate 62:48 20.99 n/a 000
060122 [L/S= 1852 / 054/ 055]
060123 [Vmax = 412; Dmax = 1.069]
060124 #
060125 # Addition of Subwatershed 5 and Flowing Creek to Node 5
060126 #
060127 R010: C00056 -> DfIn-ID NND -> AREQA-QPEAKm-TPeakDate-hh-mm-RvM-R-C--DFWCm
060128 ADD HYD + 1.0 02: N0 40240.00 31.713 NoDate 62:48 20.99 n/a 000
060129 + 1.0 02: SW5 224.00 2.546 NoDate 28:45 28.24 n/a 000
060130 + 1.0 02: PL_CK 4945.00 28.945 NoDate 33:21 25.81 n/a 000
060131 + 1.0 01: S_N 40240.00 31.713 NoDate 62:48 20.99 n/a 000
060132 #
060133 # Sum of hydrographs from Node 5 routed to Node 5A
060134 # Section 7
060135 #
060136 R010: C00057 -> DfIn-ID NND -> AREQA-QPEAKm-TPeakDate-hh-mm-RvM-R-C--DFWCm
060137 ROUTE CHANNEL -> 1.0 02: S_NA 45409.01 51.312 NoDate 35:12 21.56 n/a 000
060138 [RDE: 1.00] out-c 1.0 01: N0A 45409.01 51.312 NoDate 35:12 21.56 n/a 000
060139 [L/S= 556 / 090/ 040]
060140 [Vmax = 485; Dmax = 1.131]
060141 #
060142 # Addition of Subwatershed 5A and Subwatershed 5A2 to Node 5A
060143 #
060144 R010: C00058 -> DfIn-ID NND -> AREQA-QPEAKm-TPeakDate-hh-mm-RvM-R-C--DFWCm
060145 ADD HYD + 1.0 02: N0 45409.01 51.312 NoDate 35:12 21.56 n/a 000
060146 + 1.0 02: SW5A 585.00 8.458 NoDate 29:57 31.37 n/a 000
060147 + 1.0 02: ML_CR 1821.00 11.195 NoDate 30:48 20.72 n/a 000
060148 + 1.0 02: SW_SAI 1412.00 5.817 NoDate 37:54 27.06 n/a 000
060149 + 1.0 01: S_NA 48447.00 59.934 NoDate 36:12 22.03 n/a 000
060150 #
060151 # Sum of hydrographs from Node 5A routed to Node 4
060152 # Section 8
060153 R010: C00059 -> DfIn-ID NND -> AREQA-QPEAKm-TPeakDate-hh-mm-RvM-R-C--DFWCm
060154 ROUTE CHANNEL -> 1.0 02: S_NA 48447.01 59.934 NoDate 36:12 22.03 n/a 000
060155 [RDE: 1.00] out-c 1.0 01: N0A 48447.01 54.543 NoDate 36:56 21.73 n/a 000
060156 [L/S= 4630 / 043/ 055]
060157 [Vmax = 793; Dmax = 3.295]
060158 #
060159 # Addition of Subwatershed 4 and Leamy Creek to Node 4
060160 #
060161 R010: C00060 -> DfIn-ID NND -> AREQA-QPEAKm-TPeakDate-hh-mm-RvM-R-C--DFWCm
060162 ADD HYD + 1.0 02: N0 48447.01 54.543 NoDate 36:56 21.73 n/a 000
060163 + 1.0 02: SW4 585.00 8.458 NoDate 29:57 31.37 n/a 000
060164 + 1.0 02: ML_CR 1821.00 11.195 NoDate 30:48 20.72 n/a 000
060165 + 1.0 02: SW_SAI 1412.00 5.817 NoDate 37:54 27.06 n/a 000
060166 + 1.0 01: S_N 48447.00 59.934 NoDate 36:12 22.03 n/a 000
060167 #
060168 # Iname: S_N, 0010
060169 remark:flow at S_N
060170 #
060171 # Sum of hydrographs from Node 4 routed to Node 2

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Table with multiple columns containing alphanumeric codes, parameters, and numerical values. The table is organized into several vertical sections, with each section containing a similar set of data entries. The entries include various alphanumeric strings and numerical values, possibly representing data points or identifiers in a technical context.

Table with multiple columns containing alphanumeric codes, dates, and numerical values. The table is organized into several vertical sections, each starting with a header line (e.g., '067325 # ...'). Each row contains a series of data points, often separated by '+' signs, representing various parameters and their values. The table ends with a '010608' entry.

074811		1.0	0.02	KB-Pond3	0.00	0.00	Ndate	0.00	0.00	n/a	0.00
074828	SIMM	4.00	1.02	KB-Pond3	254.24	15.083	Ndate	28.10	35.46	n/a	0.00
074833	R0101:CO0276		1.0	0.01:R01-Pond2	254.24	15.083	Ndate	28.10	35.46	n/a	0.00
074848	name: KB-Pond2.0010										
074865	remark: Total Flow at KB second pond										
074870	CNTI NUSK STANDIHD	1.0	0.01:R01-Pond2	254.24	15.083	Ndate	28.10	35.46	n/a	0.00	
074899	[X]M# 75:TIM# 75]										
074900	[Horton parameters: Fw: 76.20; Fc: 13.20; ICAV: 14; Fw: 0.00]										
074911	[Perivous area: IApr: 4.67; SLP: 0.00; LG: 40; MNP: 250; SCP: 0]										
074920	[Impervious area: IApr: 4.67; SLP: 0.00; LG: 137; MNP: 013; SCI: 0]										
074931	[IAREC mpa: 4.00; IARECPR: 4.00]										
074948	ADD HYD	1.0	0.02:KB-Pond3	254.24	15.083	Ndate	28.10	35.46	n/a	0.00	
074960		1.0	0.02:KB-Pond3	254.24	15.083	Ndate	28.10	35.46	n/a	0.00	
074979	SIMM	4.00	1.02:KB-P3	257.04	15.295	Ndate	28.08	35.64	n/a	0.00	
074988	R0101:CO0279		1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00
074999	ROUTE RESERVOIR >		1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00
075000	out >	1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00	
075011	overflow >	1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00	
075020	[MStoUde: 1993E-02; mb; TotOfVol: 8724E+00; N.Of: 2; TotDrOf: 21.8]										
075031	R0101:CO0280		1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00
075040	ADD HYD	1.0	0.02:KB-P3	257.04	15.295	Ndate	28.08	35.64	n/a	0.00	
075050		1.0	0.02:KB-P3	257.04	15.295	Ndate	28.08	35.64	n/a	0.00	
075060	SIMM	4.00	1.02:KB-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00	
075079	R0101:CO0281		1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00
075088	SAVE HYD	1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00	
075099	remark: Total Flow at KB third pond										
075110	[X]M# 31:TIM# 64]										
075120	[Horton parameters: Fw: 76.20; Fc: 13.20; ICAV: 14; Fw: 0.00]										
075131	[Perivous area: IApr: 4.67; SLP: 0.00; LG: 40; MNP: 250; SCP: 0]										
075140	[Impervious area: IApr: 4.67; SLP: 0.00; LG: 137; MNP: 013; SCI: 0]										
075151	[IAREC mpa: 4.00; IARECPR: 4.00]										
075160	ADD HYD	1.0	0.02:KB-P3	257.04	15.295	Ndate	28.08	35.64	n/a	0.00	
075170		1.0	0.02:KB-P3	257.04	15.295	Ndate	28.08	35.64	n/a	0.00	
075180	SIMM	4.00	1.02:KB-P3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00	
075199	R0101:CO0282		1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00
075200	ROUTE RESERVOIR >		1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00
075201	out >	1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00	
075210	overflow >	1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00	
075220	[MStoUde: 1993E-02; mb; TotOfVol: 8724E+00; N.Of: 2; TotDrOf: 21.8]										
075231	R0101:CO0283		1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00
075240	ADD HYD	1.0	0.02:KB-P3	257.04	15.295	Ndate	28.08	35.64	n/a	0.00	
075250		1.0	0.02:KB-P3	257.04	15.295	Ndate	28.08	35.64	n/a	0.00	
075260	SIMM	4.00	1.02:KB-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00	
075279	R0101:CO0284		1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00
075288	SAVE HYD	1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00	
075299	remark: Total Flow at KB third pond										
075310	[X]M# 31:TIM# 64]										
075320	[Horton parameters: Fw: 76.20; Fc: 13.20; ICAV: 14; Fw: 0.00]										
075331	[Perivous area: IApr: 4.67; SLP: 0.00; LG: 40; MNP: 250; SCP: 0]										
075340	[Impervious area: IApr: 4.67; SLP: 0.00; LG: 137; MNP: 013; SCI: 0]										
075351	[IAREC mpa: 4.00; IARECPR: 4.00]										
075360	ADD HYD	1.0	0.02:KB-P3	257.04	15.295	Ndate	28.08	35.64	n/a	0.00	
075370		1.0	0.02:KB-P3	257.04	15.295	Ndate	28.08	35.64	n/a	0.00	
075380	SIMM	4.00	1.02:KB-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00	
075399	R0101:CO0285		1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00
075400	ROUTE RESERVOIR >		1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00
075401	out >	1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00	
075410	overflow >	1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00	
075420	[MStoUde: 1993E-02; mb; TotOfVol: 8724E+00; N.Of: 2; TotDrOf: 21.8]										
075431	R0101:CO0286		1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00
075440	ADD HYD	1.0	0.02:KB-P3	257.04	15.295	Ndate	28.08	35.64	n/a	0.00	
075450		1.0	0.02:KB-P3	257.04	15.295	Ndate	28.08	35.64	n/a	0.00	
075460	SIMM	4.00	1.02:KB-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00	
075479	R0101:CO0287		1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00
075488	SAVE HYD	1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00	
075499	remark: Total Flow at KB third pond										
075510	[X]M# 31:TIM# 64]										
075520	[Horton parameters: Fw: 76.20; Fc: 13.20; ICAV: 14; Fw: 0.00]										
075531	[Perivous area: IApr: 4.67; SLP: 0.00; LG: 40; MNP: 250; SCP: 0]										
075540	[Impervious area: IApr: 4.67; SLP: 0.00; LG: 137; MNP: 013; SCI: 0]										
075551	[IAREC mpa: 4.00; IARECPR: 4.00]										
075560	ADD HYD	1.0	0.02:KB-P3	257.04	15.295	Ndate	28.08	35.64	n/a	0.00	
075570		1.0	0.02:KB-P3	257.04	15.295	Ndate	28.08	35.64	n/a	0.00	
075580	SIMM	4.00	1.02:KB-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00	
075599	R0101:CO0288		1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00
075600	ROUTE RESERVOIR >		1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00
075601	out >	1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00	
075610	overflow >	1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00	
075620	[MStoUde: 1993E-02; mb; TotOfVol: 8724E+00; N.Of: 2; TotDrOf: 21.8]										
075631	R0101:CO0289		1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00
075640	ADD HYD	1.0	0.02:KB-P3	257.04	15.295	Ndate	28.08	35.64	n/a	0.00	
075650		1.0	0.02:KB-P3	257.04	15.295	Ndate	28.08	35.64	n/a	0.00	
075660	SIMM	4.00	1.02:KB-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00	
075679	R0101:CO0290		1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00
075688	SAVE HYD	1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00	
075699	remark: Total Flow at KB third pond										
075710	[X]M# 31:TIM# 64]										
075720	[Horton parameters: Fw: 76.20; Fc: 13.20; ICAV: 14; Fw: 0.00]										
075731	[Perivous area: IApr: 4.67; SLP: 0.00; LG: 40; MNP: 250; SCP: 0]										
075740	[Impervious area: IApr: 4.67; SLP: 0.00; LG: 137; MNP: 013; SCI: 0]										
075751	[IAREC mpa: 4.00; IARECPR: 4.00]										
075760	ADD HYD	1.0	0.02:KB-P3	257.04	15.295	Ndate	28.08	35.64	n/a	0.00	
075770		1.0	0.02:KB-P3	257.04	15.295	Ndate	28.08	35.64	n/a	0.00	
075780	SIMM	4.00	1.02:KB-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00	
075799	R0101:CO0291		1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00
075800	ROUTE RESERVOIR >		1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00
075801	out >	1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00	
075810	overflow >	1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00	
075820	[MStoUde: 1993E-02; mb; TotOfVol: 8724E+00; N.Of: 2; TotDrOf: 21.8]										
075831	R0101:CO0292		1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00
075840	ADD HYD	1.0	0.02:KB-P3	257.04	15.295	Ndate	28.08	35.64	n/a	0.00	
075850		1.0	0.02:KB-P3	257.04	15.295	Ndate	28.08	35.64	n/a	0.00	
075860	SIMM	4.00	1.02:KB-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	0.00	
075879	R0101:CO0293		1.0	0.01:R01-Pond3	257.04	15.295	Ndate	28.09	35.64	n/a	


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04773 # ROUTE CHANNEL -> 1.0 02:4241 54658.48 103.518 No.date 38:57 29.12 n/a .000
04774 # [RFR= 1.0] out c= 1.0 01:2441-out 54658.48 103.664 No.date 38:36 29.12 n/a .000
04775 # [L/S= 294 / 100] 035]
04776 # [X/M= 63 TI= 54]
04777 # ROUTE025:CO0307 -----Df=IN 1-D NND-----ARE/A=QPEAKm-TPeakDt-h-h-m-m-Rvmm-R-C--DfWm
04778 # ADD HYD + 1.0 02:4241-out 54658.48 103.664 No.date 38:57 29.12 n/a .000
04779 # + 1.0 02:4241-out 54658.48 103.664 No.date 38:57 29.12 n/a .000
04800 # 1.0 02:18:01-8 8.24 563.6 No.date 27:45 53.74 n/a .000
04801 # 1.0 02:18:02-5 1.99 153 No.date 27:47 53.69 n/a .000
04802 # SIMM 1.0 01:SN:KB 54681.18 103.700 No.date 38:36 29.13 n/a .000
04803 # ROUTE025:CO0308 -----Df=IN 1-D NND-----ARE/A=QPEAKm-TPeakDt-h-h-m-m-Rvmm-R-C--DfWm
04804 # SAVE HYD + 1.0 01:SN:KB 54681.18 103.700 No.date 38:36 29.13 n/a .000
04805 # fname :SN:KB:0025
04806 # remark:Total Flow at Station 3633
04807 # Hydrograph from Station 3633 to Node Todd
04808 # Channel X-section obtained from RCA Hydraulic Model Station 3633
04809 # JFSA 2021-01-26 change the channel length (at station 3633) from 650m to 608m and change the slope from 0.0489% to 0.2
04810 #
04811 # ROUTE025:CO0309 -----Df=IN 1-D NND-----ARE/A=QPEAKm-TPeakDt-h-h-m-m-Rvmm-R-C--DfWm
04812 # ROUTE CHANNEL -> 1.0 02:SN:KB 54681.18 103.700 No.date 38:36 29.13 n/a .000
04813 # [RFR= 1.0] out c= 1.0 01:SN:TO 54681.18 103.546 No.date 39:00 29.13 n/a .000
04814 # [L/S= 608 / 247] 035]
04815 # [X/M= 608 TI= 54]
04816 # *****
04817 # Catchment Greenbank
04818 # To Greenbank Drain (south of the Jack)
04819 # - JFSA 2021-01-18 add Greenbank pond as per JFSA P958/06-15, June 2016
04820 # - JFSA 2021-10-09 update area from 37.479 ha to 36.9 ha based on GIS measurements
04821 # *****
04822 # ROUTE025:CO0310 -----Df=IN 1-D NND-----ARE/A=QPEAKm-TPeakDt-h-h-m-m-Rvmm-R-C--DfWm
04823 # CONTINUES STANHYD 1.0 01:COR1 15.87 2.535 No.date 28:01 57.01 766 .000
04824 # [X/M= 64 TI= 68]
04825 # [L/S= 2 CN= 77.0]
04826 # [Previous area: IArea= 4.67:SLP=0.00:LEG= 40: MNP= 250:SCP= 0]
04827 # [PERVIOUS area: IArea= 1.57:SLP=1.00:LEG= 494: MNP= 013:SCI= 0]
04828 # [IAREC mps 4.00: IARECPer= 4.00]
04829 # [SM= 31.15: SMM=207.66: SKE= 010]
04830 # ROUTE025:CO0311 -----Df=IN 1-D NND-----ARE/A=QPEAKm-TPeakDt-h-h-m-m-Rvmm-R-C--DfWm
04831 # ROUTE RESERVOIR -> 1.0 02:GREENB 36.60 5.574 No.date 28:02 58.33 n/a .000
04832 # out c= 1.0 01:GREENB 36.60 5.574 No.date 28:02 58.33 n/a .000
04833 # overFlow c= 1.0 03:GREENB 0.00 0.000 No.date 0:00 0.00 n/a .000
04834 # [MS:olcde= 8739:060] Df=IN 1-D NND-----ARE/A=QPEAKm-TPeakDt-h-h-m-m-Rvmm-R-C--DfWm
04835 # ROUTE025:CO0312 -----Df=IN 1-D NND-----ARE/A=QPEAKm-TPeakDt-h-h-m-m-Rvmm-R-C--DfWm
04836 # ADD HYD + 1.0 02:TO 54681.18 103.546 No.date 39:00 29.13 n/a .000
04837 # + 1.0 02:GREENB 36.60 5.574 No.date 28:02 58.33 n/a .000
04838 # + 1.0 02:GREENB 36.60 5.574 No.date 28:02 58.33 n/a .000
04839 # SIMM 54717.78 103.651 No.date 39:00 29.13 n/a .000
04840 # ROUTE025:CO0313 -----Df=IN 1-D NND-----ARE/A=QPEAKm-TPeakDt-h-h-m-m-Rvmm-R-C--DfWm
04841 # SAVE HYD + 1.0 01:GREENB 54717.78 103.651 No.date 39:00 29.13 n/a .000
04842 # fname :GREENB:0025
04843 # remark:Total Flow at Greenbank Drain
04844 # *****
04845 # Catchment TODD
04846 # To Todd Drain (south of the Jack)
04847 # Subdivision with 435/imp as per Barhaven South MS
04848 # - 2020-11-30 increase imp. based on P958/04 (11)
04849 # - 2020-11-30 update TODD Drainage Area to = 146.015 ha based on P958/04 (11)
04850 # - 2020-11-30 split TODD Drainage Area to MW, RR, POND and ALL
04851 # *****
04852 # JFSA 2021-01-19 add TODD MAN as part of Clarke (W.CLAR.M) and remove it from Todd
04853 # ROUTE025:CO0314 -----Df=IN 1-D NND-----ARE/A=QPEAKm-TPeakDt-h-h-m-m-Rvmm-R-C--DfWm
04854 # CONTINUES STANHYD 1.0 01:TODD:M 2.10 2.319 No.date 28:00 53.59 720 .000
04855 # [X/M= 53 TI= 64]
04856 # [L/S= 2 CN= 77.0]
04857 # [Previous area: IArea= 4.67:SLP=0.00:LEG= 40: MNP= 250:SCP= 0]
04858 # [PERVIOUS area: IArea= 1.57:SLP=1.00:LEG= 118: MNP= 013:SCI= 0]
04859 # [IAREC mps 4.00: IARECPer= 4.00]
04860 # [SM= 31.15: SMM=207.66: SKE= 010]
04861 # ROUTE025:CO0315 -----Df=IN 1-D NND-----ARE/A=QPEAKm-TPeakDt-h-h-m-m-Rvmm-R-C--DfWm
04862 # CONTINUES STANHYD 1.0 01:TODD:M 12 0.020 No.date 28:00 53.57 720 .000
04863 # [X/M= 53 TI= 64]
04864 # [L/S= 2 CN= 77.0]
04865 # [Previous area: IArea= 4.67:SLP=0.00:LEG= 40: MNP= 250:SCP= 0]
04866 # [PERVIOUS area: IArea= 1.57:SLP=1.00:LEG= 28: MNP= 013:SCI= 0]
04867 # [IAREC mps 4.00: IARECPer= 4.00]
04868 # [SM= 31.15: SMM=207.66: SKE= 010]
04869 # ROUTE025:CO0316 -----Df=IN 1-D NND-----ARE/A=QPEAKm-TPeakDt-h-h-m-m-Rvmm-R-C--DfWm
04870 # CONTINUES STANHYD 1.0 01:TODD:M 30.23 4.269 No.date 28:02 55.13 741 .000
04871 # [X/M= 52 TI= 64]
04872 # [L/S= 2 CN= 77.0]
04873 # [Previous area: IArea= 4.67:SLP=0.00:LEG= 40: MNP= 250:SCP= 0]
04874 # [PERVIOUS area: IArea= 1.57:SLP=1.00:LEG= 449: MNP= 013:SCI= 0]
04875 # [IAREC mps 4.00: IARECPer= 4.00]
04876 # [SM= 31.15: SMM=207.66: SKE= 010]
04877 # ROUTE025:CO0317 -----Df=IN 1-D NND-----ARE/A=QPEAKm-TPeakDt-h-h-m-m-Rvmm-R-C--DfWm
04878 # CONTINUES STANHYD 1.0 01:TODD:M 112.91 13.132 No.date 28:05 53.38 718 .000
04879 # [X/M= 52 TI= 57]
04880 # [L/S= 2 CN= 77.0]
04881 # [Previous area: IArea= 4.67:SLP=0.00:LEG= 40: MNP= 250:SCP= 0]
04882 # [PERVIOUS area: IArea= 1.57:SLP=1.00:LEG= 868: MNP= 013:SCI= 0]
04883 # [IAREC mps 4.00: IARECPer= 4.00]
04884 # [SM= 31.15: SMM=207.66: SKE= 010]
04885 # ROUTE025:CO0318 -----Df=IN 1-D NND-----ARE/A=QPEAKm-TPeakDt-h-h-m-m-Rvmm-R-C--DfWm
04886 # CONTINUES STANHYD 1.0 01:TODD:P 3.06 5.535 No.date 28:00 57.01 766 .000
04887 # [X/M= 63 TI= 63]
04888 # [L/S= 2 CN= 77.0]
04889 # [Previous area: IArea= 4.67:SLP=0.00:LEG= 40: MNP= 250:SCP= 0]
04890 # [PERVIOUS area: IArea= 1.57:SLP=1.00:LEG= 143: MNP= 013:SCI= 0]
04891 # [IAREC mps 4.00: IARECPer= 4.00]
04892 # [SM= 31.15: SMM=207.66: SKE= 010]
04893 # ROUTE025:CO0319 -----Df=IN 1-D NND-----ARE/A=QPEAKm-TPeakDt-h-h-m-m-Rvmm-R-C--DfWm
04894 # 5% Year + 12% Capture
04895 # ROUTE RESERVOIR -> 1.0 02:TODD:M 30.23 4.269 No.date 28:02 55.13 n/a .000
04896 # + 1.0 02:TODD:M 29.18 4.196 No.date 28:02 55.13 n/a .000
04897 # overFlow c= 1.0 03:TODD:M 7.946 No.date 28:03 55.13 n/a .000
04898 # [MS:olcde= 11756:03 No. TotOfVol= 41536.01 No. N.Of= 1, TotOfDrf= 6 h.rs]
04899 # 5% Year + 12% Capture
04900 # ROUTE025:CO0320 -----Df=IN 1-D NND-----ARE/A=QPEAKm-TPeakDt-h-h-m-m-Rvmm-R-C--DfWm
04901 # ROUTE RESERVOIR -> 1.0 02:TODD:M 2.10 2.319 No.date 28:00 53.59 n/a .000
04902 # + 1.0 01:TODD:M 2.06 2.68 No.date 27:54 53.60 n/a .000
04903 # overFlow c= 1.0 03:TODD:M 3.06 5.535 No.date 28:00 53.59 n/a .000
04904 # [MS:olcde= 845E:04 No. TotOfVol= 22172.02 No. N.Of= 0, TotOfDrf= 0 h.rs]
04905 # ROUTE025:CO0321 -----Df=IN 1-D NND-----ARE/A=QPEAKm-TPeakDt-h-h-m-m-Rvmm-R-C--DfWm
04906 # ROUTE RESERVOIR -> 1.0 02:TODD:M 120 0.020 No.date 28:00 53.58 n/a .000
04907 # + 1.0 01:TODD:M 11 0.016 No.date 27:53 53.58 n/a .000
04908 # overFlow c= 1.0 03:TODD:M 3.06 5.535 No.date 28:00 53.58 n/a .000
04909 # [MS:olcde= 1067E:03 No. TotOfVol= 11926.03 No. N.Of= 1, TotOfDrf= 0 h.rs]
04910 # ROUTE025:CO0322 -----Df=IN 1-D NND-----ARE/A=QPEAKm-TPeakDt-h-h-m-m-Rvmm-R-C--DfWm
04911 # CONTINUES STANHYD 1.0 01:COR1 15.87 2.535 No.date 28:01 57.01 766 .000
04912 # [X/M= 42 TI= 52]
04913 # [L/S= 2 CN= 77.0]
04914 # [Previous area: IArea= 4.67:SLP=0.00:LEG= 40: MNP= 250:SCP= 0]
04915 # [PERVIOUS area: IArea= 1.57:SLP=1.00:LEG= 566: MNP= 013:SCI= 0]
04916 # [IAREC mps 4.00: IARECPer= 4.00]
04917 # [SM= 33.81: SMM=225.43: SKE= 010]
04918 # COMPUTE DUALHYD 1.0 01:BI 25.50 2.974 No.date 28:03 49.44 n/a .000
04919 # Mjr System / 1.0 02:BI:M 25.50 1.874 No.date 28:03 49.44 n/a .000
04920 # Mnor System / 1.0 03:AI:M 25.50 1.874 No.date 27:54 49.44 n/a .000
04921 # [MS:Sto= 3120:0E0] TotOfVol= 0.000E+00, No.Of= 0, TotOfDrf= 0 h.rs]
04922 # ROUTE025:CO0323 -----Df=IN 1-D NND-----ARE/A=QPEAKm-TPeakDt-h-h-m-m-Rvmm-R-C--DfWm
04923 # ADD HYD + 1.0 02:TODD:M 2.06 2.68 No.date 27:54 53.60 n/a .000
04924 # + 1.0 02:TODD:M 11 0.016 No.date 27:53 53.58 n/a .000
04925 # + 1.0 02:TODD:M 7.946 No.date 28:03 55.13 n/a .000
04926 # + 1.0 02:TODD:M 3.06 5.535 No.date 28:00 53.58 n/a .000
04927 # + 1.0 02:TODD:M 112.91 13.132 No.date 28:05 53.38 n/a .000
04928 # + 1.0 02:CLAR:M 1.73 2.13 No.date 27:54 52.78 n/a .000
04929 # SIMM 120 14.962 No.date 28:03 53.48 n/a .000
04930 # ROUTE025:CO0325 -----Df=IN 1-D NND-----ARE/A=QPEAKm-TPeakDt-h-h-m-m-Rvmm-R-C--DfWm
04931 # SAVE HYD + 1.0 01:SN:TO 54838.44 103.908 No.date 39:00 29.21 n/a .000
04932 # fname :TODD:0025
04933 # remark:Total Flow at Todd Drain
04934 # *****
04935 # Todd Pond
04936 # Rating curve obtained from Barhaven South MS modeling
04937 # - stantec 2007, Tributary Drainage Area to MSH Pond 3 = 193 ha
04938 # *****
04939 # ROUTE025:CO0326 -----Df=IN 1-D NND-----ARE/A=QPEAKm-TPeakDt-h-h-m-m-Rvmm-R-C--DfWm
04940 # ROUTE RESERVOIR -> 1.0 02:TODD 120.62 14.962 No.date 28:03 53.48 n/a .000
04941 # + 1.0 01:MS:P 120.62 9.717 No.date 28:14 53.48 n/a .000
04942 # overFlow c= 1.0 03:PF:OW 0.00 0.000 No.date 0:00 0.00 n/a .000
04943 # [MS:olcde= 20:0E0] Df=IN 1-D NND-----ARE/A=QPEAKm-TPeakDt-h-h-m-m-Rvmm-R-C--DfWm
04944 # ROUTE025:CO0327 -----Df=IN 1-D NND-----ARE/A=QPEAKm-TPeakDt-h-h-m-m-Rvmm-R-C--DfWm
04945 # ADD HYD + 1.0 02:TODD:M 54717.78 103.651 No.date 39:00 29.15 n/a .000
04946 # + 1.0 02:MS:P 120.62 9.717 No.date 28:14 53.48 n/a .000
04947 # + 1.0 02:PF:OW 0.00 0.000 No.date 0:00 0.00 n/a .000
04948 # + 1.0 02:TODD:M 94 0.67 No.date 28:00 53.59 n/a .000
04949 # + 1.0 02:AI:M 0.00 0.000 No.date 0:00 0.00 n/a .000
04950 # SIMM 54838.44 103.908 No.date 39:00 29.21 n/a .000
04951 # ROUTE025:CO0328 -----Df=IN 1-D NND-----ARE/A=QPEAKm-TPeakDt-h-h-m-m-Rvmm-R-C--DfWm
04952 # SAVE HYD + 1.0 01:SN:TO 54838.44 103.908 No.date 39:00 29.21 n/a .000
04953 # fname :SN:TO:0025
04954 # remark:Total Flow at Todd Drain
04955 # *****
04956 # Hydrograph from Todd Drain routed to Corigan Drain
04957 # Channel X-section obtained from RCA Hydraulic Model Station 2462
04958 # JFSA 2021-01-19 Change the slope from 0.033 % (as per Stantec Report 2007) to 0.05 % so the model will be more stable and g
04959 # ROUTE025:CO0329 -----Df=IN 1-D NND-----ARE/A=QPEAKm-TPeakDt-h-h-m-m-Rvmm-R-C--DfWm
04960 # ROUTE CHANNEL -> 1.0 02:SN:TO 54838.44 103.908 No.date 39:00 29.21 n/a .000
04961 # [RFR= 1.0] out c= 1.0 01:SN:TO 54838.44 103.688 No.date 39:23 29.21 n/a .000
04962 # [L/S= 200 / 100] 035]
04963 # [X/M= 905 DM= 3.15]
04964 # *****
04965 # ROUTE025:CO0330 -----Df=IN 1-D NND-----ARE/A=QPEAKm-TPeakDt-h-h-m-m-Rvmm-R-C--DfWm
04966 # SAVE HYD + 1.0 01:SN:TO 54838.44 103.688 No.date 39:23 29.21 n/a .000
04967 # fname :N:TO:0025
04968 # remark:Total Flow at Station 2462
04969 # *****
04970 # Catchment CORIGAN
04971 # To Corigan Drain (south of the Jack)
04972 # - Preliminary E-Map (soil density)
04973 # - JFSA (Jan 2021) add C-Map subcatchments as per I.B. July 2008
04974 # *****
04975 # ROUTE025:CO0331 -----Df=IN 1-D NND-----ARE/A=QPEAKm-TPeakDt-h-h-m-m-Rvmm-R-C--DfWm
04976 # CONTINUES STANHYD 1.0 01:COR1 15.87 2.535 No.date 28:01 57.01 766 .000
04977 # [X/M= 63 TI= 63]
04978 # [L/S= 2 CN= 77.0]
04979 # [Previous area: IArea= 4.67:SLP=0.00:LEG= 40: MNP= 250:SCP= 0]

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108477	ROUTE PIPE	>>	1.0	0.02:335-338	17.90	1.490	N_date	28:26	49.83	n/a	0.00																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																						
108478	ROUTE PIPE	>>	1.0	0.02:335-338	17.90	1.456	N_date	28:26	49.83	n/a	0.00																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																						
108479	PERVIOUS	area: I: Aper: 4.67: SLLP=1.0; LCP= 4.0; MNP: 250; SCP= 0] [I: RG: nps: 4.00; I: AR: cper: 4.00] [I: AR: cper: 4.00; I: AR: cper: 4.00] [I: AR: cper: 4.00; I: AR: cper: 4.00]	108479	108480	108481	108482	108483	108484	108485	108486	108487	108488	108489	108490	108491	108492	108493	108494	108495	108496	108497	108498	108499	108500	108501	108502	108503	108504	108505	108506	108507	108508	108509	108510	108511	108512	108513	108514	108515	108516	108517	108518	108519	108520	108521	108522	108523	108524	108525	108526	108527	108528	108529	108530	108531	108532	108533	108534	108535	108536	108537	108538	108539	108540	108541	108542	108543	108544	108545	108546	108547	108548	108549	108550	108551	108552	108553	108554	108555	108556	108557	108558	108559	108560	108561	108562	108563	108564	108565	108566	108567	108568	108569	108570	108571	108572	108573	108574	108575	108576	108577	108578	108579	108580	108581	108582	108583	108584	108585	108586	108587	108588	108589	108590	108591	108592	108593	108594	108595	108596	108597	108598	108599	108600	108601	108602	108603	108604	108605	108606	108607	108608	108609	108610	108611	108612	108613	108614	108615	108616	108617	108618	108619	108620	108621	108622	108623	108624	108625	108626	108627	108628	108629	108630	108631	108632	108633	108634	108635	108636	108637	108638	108639	108640	108641	108642	108643	108644	108645	108646	108647	108648	108649	108650	108651	108652	108653	108654	108655	108656	108657	108658	108659	108660	108661	108662	108663	108664	108665	108666	108667	108668	108669	108670	108671	108672	108673	108674	108675	108676	108677	108678	108679	108680	108681	108682	108683	108684	108685	108686	108687	108688	108689	108690	108691	108692	108693	108694	108695	108696	108697	108698	108699	108700	108701	108702	108703	108704	108705	108706	108707	108708	108709	108710	108711	108712	108713	108714	108715	108716	108717	108718	108719	108720	108721	108722	108723	108724	108725	108726	108727	108728	108729	108730	108731	108732	108733	108734	108735	108736	108737	108738	108739	108740	108741	108742	108743	108744	108745	108746	108747	108748	108749	108750	108751	108752	108753	108754	108755	108756	108757	108758	108759	108760	108761	108762	108763	108764	108765	108766	108767	108768	108769	108770	108771	108772	108773	108774	108775	108776	108777	108778	108779	108780	108781	108782	108783	108784	108785	108786	108787	108788	108789	108790	108791	108792	108793	108794	108795	108796	108797	108798	108799	108800	108801	108802	108803	108804	108805	108806	108807	108808	108809	108810	108811	108812	108813	108814	108815	108816	108817	108818	108819	108820	108821	108822	108823	108824	108825	108826	108827	108828	108829	108830	108831	108832	108833	108834	108835	108836	108837	108838	108839	108840	108841	108842	108843	108844	108845	108846	108847	108848	108849	108850	108851	108852	108853	108854	108855	108856	108857	108858	108859	108860	108861	108862	108863	108864	108865	108866	108867	108868	108869	108870	108871	108872	108873	108874	108875	108876	108877	108878	108879	108880	108881	108882	108883	108884	108885	108886	108887	108888	108889	108890	108891	108892	108893	108894	108895	108896	108897	108898	108899	108900	108901	108902	108903	108904	108905	108906	108907	108908	108909	108910	108911	108912	108913	108914	108915	108916	108917	108918	108919	108920	108921	108922	108923	108924	108925	108926	108927	108928	108929	108930	108931	108932	108933	108934	108935	108936	108937	108938	108939	108940	108941	108942	108943	108944	108945	108946	108947	108948	108949	108950	108951	108952	108953	108954	108955	108956	108957	108958	108959	108960	108961	108962	108963	108964	108965	108966	108967	108968	108969	108970	108971	108972	108973	108974	108975	108976	108977	108978	108979	108980	108981	108982	108983	108984	108985	108986	108987	108988	108989	108990	108991	108992	108993	108994	108995	108996	108997	108998	108999	109000	109001	109002	109003	109004	109005	109006	109007	109008	109009	109010	109011	109012	109013	109014	109015	109016	109017	109018	109019	109020	109021	109022	109023	109024	109025	109026	109027	109028	109029	109030	109031	109032	109033	109034	109035	109036	109037	109038	109039	109040	109041	109042	109043	109044	109045	109046	109047	109048	109049	109050	109051	109052	109053	109054	109055	109056	109057	109058	109059	109060	109061	109062	109063	109064	109065	109066	109067	109068	109069	109070	109071	109072	109073	109074	109075	109076	109077	109078	109079	109080	109081	109082	109083	109084	109085	109086	109087	109088	109089	109090	109091	109092	109093	109094	109095	109096	109097	109098	109099	109100	109101	109102	109103	109104	109105	109106	109107	109108	109109	109110	109111	109112	109113	109114	109115	109116	109117	109118	109119	109120	109121	109122	109123	109124	109125	109126	109127	109128	109129	109130	109131	109132	109133	109134	109135	109136	109137	109138	109139	109140	109141	109142	109143	109144	109145	109146	109147	109148	109149	109150	109151	109152	109153	109154	109155	109156	109157	109158	109159	109160	109161	109162	109163	109164	109165	109166	109167	109168	109169	109170	109171	109172	109173	109174	109175	109176	109177	109178	109179	109180	109181	109182	109183	109184	109185	109186	109187	109188	109189	109190	109191	109192	109193	109194	109195	109196	109197	109198	109199	109200	109201	109202	109203	109204	109205	109206	109207	109208	109209	109210	109211	109212	109213	109214	109215	109216	109217	109218	109219	109220	109221	109222	109223	109224	109225	109226	109227	109228	109229	109230	109231	109232	109233	109234	109235	109236	109237	109238	109239	109240	109241	109242	109243	109244	109245	109246	109247	109248	109249	109250	109251	109252	109253	109254	109255	109256	109257	109258	109259	109260	109261	109262	109263	109264	109265	109266	109267	109268	109269	109270	109271	109272	109273	109274	109275	109276	109277	109278	109279	109280	109281	109282	109283	109284	109285	109286	109287	109288	109289	109290	109291	109292	109293	109294	109295	109296	109297	109298	109299	109300	109301	109302	109303	109304	109305	109306	109307	109308	109309	109310	109311	109312	109313	109314	109315	109316	109317	109318	109319	109320	109321	109322	109323	109324	109325	109326	109327	109328	109329	109330	109331	109332	109333	109334	109335	109336	109337	109338	109339	109340	109341	109342	109343	109344	109345	109346	109347	109348	109349	109350	109351	109352	109353	109354	109355	109356	109357	109358	109359	109360	109361	109362	109363	109364	109365	109366	109367	109368	109369	109370	109371	109372	109373	109374	109375	109376	109377	109378	109379	109380	109381	109382	109383	109384	109385	109386	109387	109388	109389	109390	109391	109392	109393	109394	109395	109396	109397	109398	109399	109400	109401	109402	109403	109404	109405	109406	109407	109408	109409	109410	109411	109412	109413	109414	109415	109416	109417	109418	109419	109420	109421	109422	109423	109424	109425	109426	109427	109428	109429	109430	109431	109432	109433	109434	109435	109436	109437	109438	109439	109440	109441	109442	109443	109444	109445	109446	109447	109448	109449	109450	109451	109452	109453	109454	109455	109456	109457	109458	109459	109460	109461	109462	109463	109464	109465	109466	109467	109468	109469


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11595# # Addition of Subwatershed Lock River at Ashton to Node 12
11596#
11597# RO050: C0003# ----- Dfma-ID NDD ----- AREHA-QPEAGm-TpeakDte-hh:mm----- Rvmm-R-C----- Dfwmc
11598# ADD HYD + 1.0 02: S_N2 9506.0 18.687 N_date 32:42 29.39 n/a 000
11599# ROUTE CHANNEL -> 1.0 02: S_N2 9506.0 18.687 N_date 32:42 29.39 n/a 000
11600# [RfE: 1.00] out c 1.0 01: N2 9506.0 18.687 N_date 32:42 29.39 n/a 000
11601# [L/S: 972 / 054] 040]
11602# [Vmax: .751; Dmax: 3.029]
11603#
11604# remark: flow at S_N2 near Ashton
11605#
11606# Sum of hydrographs from Node 12 routed to Node 11
11607# (Approximated cross section - see cross.section 258)
11608# # Use out.c for summer conditions and out.c025 for spring conditions
11609#
11610# Sum of hydrographs from Node 12 routed to Node 11 with Damsy section 248
11611#
11612# RO050: C0003# ----- Dfma-ID NDD ----- AREHA-QPEAGm-TpeakDte-hh:mm----- Rvmm-R-C----- Dfwmc
11613# ROUTE CHANNEL -> 1.0 02: S_N2 9506.0 18.687 N_date 32:42 29.39 n/a 000
11614# [RfE: 1.00] out c 1.0 01: N2 9506.0 18.687 N_date 32:59 29.39 n/a 000
11615# [L/S: 972 / 054] 040]
11616# [Vmax: .751; Dmax: 3.029]
11617#
11618# Addition of Subwatershed 11 and No Name Creek to Node 11
11619#
11620# RO050: C0003# ----- Dfma-ID NDD ----- AREHA-QPEAGm-TpeakDte-hh:mm----- Rvmm-R-C----- Dfwmc
11621# ADD HYD + 1.0 02: N2 9506.0 18.687 N_date 32:59 29.39 n/a 000
11622# + 1.0 02: SW2 500.0 9.063 N_date 29:21 31.73 n/a 000
11623# + 1.0 02: NC_CK 1917.0 12.342 N_date 34:26 31.73 n/a 000
11624# SIMM 1.0 01: S_N2 11923.0 32.851 N_date 33:00 29.87 n/a 000
11625#
11626# Sum of hydrographs from Node 11 routed to Node 10
11627# Section 1
11628#
11629# RO050: C0040# ----- Dfma-ID NDD ----- AREHA-QPEAGm-TpeakDte-hh:mm----- Rvmm-R-C----- Dfwmc
11630# ROUTE CHANNEL -> 1.0 02: S_N1 11923.0 32.851 N_date 33:00 29.87 n/a 000
11631# [RfE: 1.00] out c 1.0 01: N0 11923.0 20.490 N_date 40:02 29.87 n/a 000
11632# [L/S: 4028 / 157] 040]
11633# [Vmax: .474; Dmax: 1.423]
11634#
11635# Addition of Subwatershed 10 to Node 10
11636#
11637# RO050: C0004# ----- Dfma-ID NDD ----- AREHA-QPEAGm-TpeakDte-hh:mm----- Rvmm-R-C----- Dfwmc
11638# ADD HYD + 1.0 02: N0 11923.0 20.490 N_date 40:02 29.87 n/a 000
11639# + 1.0 02: SW10 8966.0 32.402 N_date 37:52 36.85 n/a 000
11640# SIMM 1.0 01: S_N0 17589.0 52.600 N_date 38:19 32.12 n/a 000
11641#
11642# SAVE HYD 1.0 01: S_N0 17589.0 52.600 N_date 38:19 32.12 n/a 000
11643# frame :H:RSND
11644# remark: flow at S_N0: N10 + SW10
11645#
11646# Addition of Kings Creek to S_N10
11647#
11648# RO050: C0004# ----- Dfma-ID NDD ----- AREHA-QPEAGm-TpeakDte-hh:mm----- Rvmm-R-C----- Dfwmc
11649# ADD HYD + 1.0 02: N0 11923.0 20.490 N_date 38:19 32.12 n/a 000
11650# + 1.0 02: KG_CK 8376.0 31.024 N_date 39:59 31.73 n/a 000
11651# SIMM 1.0 01: S_N0A 25965.0 82.746 N_date 39:45 31.99 n/a 000
11652#
11653# Sum of hydrographs from Node 10 routed to Node 9
11654# Section 2
11655# RO050: C0004# ----- Dfma-ID NDD ----- AREHA-QPEAGm-TpeakDte-hh:mm----- Rvmm-R-C----- Dfwmc
11656# ROUTE CHANNEL -> 1.0 02: S_N0A 25965.0 82.746 N_date 39:45 31.99 n/a 000
11657# [RfE: 1.00] out c 1.0 01: N8 31561.0 80.980 N_date 39:59 31.99 n/a 000
11658# [L/S: 3082 / 074] 040]
11659# [Vmax: .744; Dmax: 2.015]
11660#
11661# Addition of Subwatershed 9 and Nichols Creek to Node 9
11662#
11663# RO050: C0045# ----- Dfma-ID NDD ----- AREHA-QPEAGm-TpeakDte-hh:mm----- Rvmm-R-C----- Dfwmc
11664# ADD HYD + 1.0 02: N0 25965.0 80.980 N_date 39:59 31.99 n/a 000
11665# + 1.0 02: SW10 1432.0 14.039 N_date 30:53 35.35 n/a 000
11666# + 1.0 02: NC_CK 4164.0 15.472 N_date 39:59 28.95 n/a 000
11667# SIMM 1.0 01: S_N2 3486.0 34.664 N_date 39:59 31.68 n/a 000
11668#
11669# Sum of hydrographs from Node 9 routed to Node 8
11670# Section 3
11671# RO050: C0046# ----- Dfma-ID NDD ----- AREHA-QPEAGm-TpeakDte-hh:mm----- Rvmm-R-C----- Dfwmc
11672# ROUTE CHANNEL -> 1.0 02: S_N0 31561.0 99.244 N_date 39:59 31.68 n/a 000
11673# [RfE: 1.00] out c 1.0 01: N8 31561.0 93.665 N_date 39:59 31.68 n/a 000
11674# [L/S: 2209 / 089] 045]
11675# [Vmax: .367; Dmax: 1.834]
11676#
11677# Addition of Subwatershed 8 and Hubb's Drain to Node 8
11678#
11679# RO050: C0047# ----- Dfma-ID NDD ----- AREHA-QPEAGm-TpeakDte-hh:mm----- Rvmm-R-C----- Dfwmc
11680# ADD HYD + 1.0 02: N0 31561.0 93.665 N_date 39:59 31.68 n/a 000
11681# + 1.0 02: HB_D 2740.0 26.400 N_date 30:53 35.35 n/a 000
11682# + 1.0 02: HB_D 3854.0 18.180 N_date 38:32 31.73 n/a 000
11683# SIMM 1.0 01: S_N8 35546.0 111.843 N_date 39:59 31.68 n/a 000
11684#
11685# Sum of hydrographs from Node 8 routed to Node 7
11686# Section 4
11687# RO050: C0048# ----- Dfma-ID NDD ----- AREHA-QPEAGm-TpeakDte-hh:mm----- Rvmm-R-C----- Dfwmc
11688# ROUTE CHANNEL -> 1.0 02: S_N8 35546.0 111.843 N_date 39:59 31.68 n/a 000
11689# [RfE: 1.00] out c 1.0 01: N8 35546.0 95.475 N_date 44:55 31.68 n/a 000
11690# [L/S: 3750 / 053] 070]
11691# [Vmax: .231; Dmax: 2.290]
11692#
11693# Addition of Subwatershed 7 to Node 7
11694#
11695# RO050: C0049# ----- Dfma-ID NDD ----- AREHA-QPEAGm-TpeakDte-hh:mm----- Rvmm-R-C----- Dfwmc
11696# ADD HYD + 1.0 02: S_N7 35546.0 95.475 N_date 43:46 31.18 n/a 000
11697# + 1.0 02: SW7 3197.0 13.937 N_date 36:23 25.61 n/a 000
11698# SIMM 1.0 01: S_N7 38743.0 102.892 N_date 43:46 31.18 n/a 000
11699#
11700# RO050: C0050# ----- Dfma-ID NDD ----- AREHA-QPEAGm-TpeakDte-hh:mm----- Rvmm-R-C----- Dfwmc
11701# SAVE HYD 1.0 01: S_N7 38743.0 102.892 N_date 43:46 31.18 n/a 000
11702# frame :H:RSND
11703# remark: flow at S_N7: N0 + SW7
11704#
11705# Insertion of a reservoir to simulate the effects of the Richmond Fen.
11706# Storage area and volumes were estimated from available top maps.
11707# Release rate from fen was assumed to be controlled by the downstream
11708# river cross-section for summer conditions. It is assumed that for up to
11709# 0.75 m of water, the main channel of the river provided the storage. Above
11710# this depth, the wetland starts to significantly store water.
11711#
11712# RO050: C0051# ----- Dfma-ID NDD ----- AREHA-QPEAGm-TpeakDte-hh:mm----- Rvmm-R-C----- Dfwmc
11713# ROUTE RESERVOIR -> 1.0 02: S_N7 38743.0 102.892 N_date 43:46 31.18 n/a 000
11714# [RfE: 1.00] out c 1.0 01: RES_RF 38743.0 52.029 N_date 59:07 31.18 n/a 000
11715# [MS: 0.64; 4394] 040]
11716#
11717# RO050: C0052# ----- Dfma-ID NDD ----- AREHA-QPEAGm-TpeakDte-hh:mm----- Rvmm-R-C----- Dfwmc
11718# SAVE HYD 1.0 01: RES_RF 38743.0 52.029 N_date 59:07 31.18 n/a 000
11719# frame :H:RES_RF
11720# remark: outflow of Richmond Fen
11721#
11722# Sum of hydrographs from Node 7 routed to Node 6
11723# Section 5
11724# RO050: C0053# ----- Dfma-ID NDD ----- AREHA-QPEAGm-TpeakDte-hh:mm----- Rvmm-R-C----- Dfwmc
11725# ROUTE CHANNEL -> 1.0 02: RES_RF 38743.0 52.029 N_date 59:07 31.18 n/a 000
11726# [RfE: 1.00] out c 1.0 01: N6 38743.0 51.784 N_date 60:27 31.18 n/a 000
11727# [L/S: 1852 / 082] 040]
11728# [Vmax: .538; Dmax: 1.253]
11729#
11730# Addition of Subwatershed 6 and Van Gual Drain to Node 6
11731#
11732# RO050: C0054# ----- Dfma-ID NDD ----- AREHA-QPEAGm-TpeakDte-hh:mm----- Rvmm-R-C----- Dfwmc
11733# ADD HYD + 1.0 02: N6 38743.0 51.784 N_date 60:27 31.18 n/a 000
11734# + 1.0 02: SW6 165.0 1.285 N_date 33:02 32.44 n/a 000
11735# + 1.0 02: VG_DR 1332.0 9.332 N_date 35:12 36.85 n/a 000
11736# SIMM 1.0 01: S_N6 40240.0 51.810 N_date 60:20 31.37 n/a 000
11737#
11738# Sum of hydrographs from Node 6 routed to Node 5
11739# Section 6
11740# RO050: C0055# ----- Dfma-ID NDD ----- AREHA-QPEAGm-TpeakDte-hh:mm----- Rvmm-R-C----- Dfwmc
11741# ROUTE CHANNEL -> 1.0 02: S_N6 40240.0 51.810 N_date 60:20 31.37 n/a 000
11742# [RfE: 1.00] out c 1.0 01: N5 40240.0 51.693 N_date 61:06 31.37 n/a 000
11743# [L/S: 1852 / 082] 040]
11744# [Vmax: .469; Dmax: 1.351]
11745#
11746# Addition of Subwatershed 5 and Flowing Creek to Node 5
11747#
11748# RO050: C0056# ----- Dfma-ID NDD ----- AREHA-QPEAGm-TpeakDte-hh:mm----- Rvmm-R-C----- Dfwmc
11749# ADD HYD + 1.0 02: N5 40240.0 51.693 N_date 61:06 31.37 n/a 000
11750# + 1.0 02: SW5 224.0 8.187 N_date 28:45 41.51 n/a 000
11751# + 1.0 02: FC_CK 4945.0 44.623 N_date 33:18 38.37 n/a 000
11752# SIMM 1.0 01: S_N5 45409.0 71.514 N_date 34:20 32.18 n/a 000
11753#
11754# Sum of hydrographs from Node 5 routed to Node 5A
11755# Section 7
11756# RO050: C0057# ----- Dfma-ID NDD ----- AREHA-QPEAGm-TpeakDte-hh:mm----- Rvmm-R-C----- Dfwmc
11757# ROUTE CHANNEL -> 1.0 02: S_N5A 45409.0 71.514 N_date 34:20 32.18 n/a 000
11758# [RfE: 1.00] out c 1.0 01: N5A 45409.0 71.514 N_date 34:15 32.18 n/a 000
11759# [L/S: 556 / 090] 040]
11760# [Vmax: .530; Dmax: 1.290]
11761#
11762# Addition of Subwatershed 5A and Subwatershed 5A2 to Node 5A
11763#
11764# RO050: C0058# ----- Dfma-ID NDD ----- AREHA-QPEAGm-TpeakDte-hh:mm----- Rvmm-R-C----- Dfwmc
11765# ADD HYD + 1.0 02: S_N5A 45409.0 71.514 N_date 34:15 32.18 n/a 000
11766# + 1.0 02: SW5A2 20.0 943.0 N_date 28:35 45.60 n/a 000
11767# + 1.0 02: SW5A1 1412.0 8.794 N_date 37:48 39.93 n/a 000
11768# SIMM 1.0 01: S_N5 46841.0 71.514 N_date 34:46 32.42 n/a 000
11769#
11770# Sum of hydrographs from Node 5A routed to Node 4
11771# Section 8
11772# RO050: C0059# ----- Dfma-ID NDD ----- AREHA-QPEAGm-TpeakDte-hh:mm----- Rvmm-R-C----- Dfwmc
11773# ROUTE CHANNEL -> 1.0 02: S_N5A 46841.0 79.247 N_date 34:46 32.42 n/a 000
11774# [RfE: 1.00] out c 1.0 01: N4 46841.0 75.833 N_date 36:02 32.42 n/a 000
11775# [L/S: 4630 / 043] 035]
11776# [Vmax: .874; Dmax: 3.702]
11777#
11778# Addition of Subwatershed 4 and Leary Creek to Node 4

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Table containing detailed hydrological data points (e.g., 13091+, 13092+, 13093+, 13094+, 13095+, etc.) and project information. Includes subcatchment names, model parameters, and flow calculations. The table is organized in columns representing various data fields such as ID, description, coordinates, flow rates, and model parameters.

134655	RO050:CO0331	Dfma:ID NDD	AREHA-QPEAKm-TpeakDte,hb,mm	Rvmm R.C.	Dfwm
134656	CNTLNXS STANDBY	1.0 01:COR1	15.87	2.851	Ndate	28:01	63.61	780	000
134657	[XMP: 63.71:TPM:63]								
134658	[LRS: 2 :CN: 77.0]								
134700	[Pervious area: IArea: 4.67:SLP4:00:LG: 40: MNP: 250:SCP: 0]								
134701	[Impervious area: IArea: 1.57:SLP1:00:LG: 324: MNP: 013:SCI: 0]								
134702	[IAREC mps: 4.00: IARECper: 4.00]								
134703	[SM N: 33.81: SMX: 225.43: SKE: 010]								
134704	ADD INVD								
134705	ADD INVD								
134706	ADD INVD								
134707	ADD INVD								
134708	ADD INVD								
134709	ADD INVD								
134710	ADD INVD								
134711	ADD INVD								
134712	ADD INVD								
134713	ADD INVD								
134714	ADD INVD								
134715	ADD INVD								
134716	ADD INVD								
134717	ADD INVD								
134718	ADD INVD								
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134721	ADD INVD								
134722	ADD INVD								
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134727	ADD INVD								
134728	ADD INVD								
134729	ADD INVD								
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134731	ADD INVD								
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134736	ADD INVD								
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134740	ADD INVD								
134741	ADD INVD								
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134743	ADD INVD								
134744	ADD INVD								
134745	ADD INVD								
134746	ADD INVD								
134747	ADD INVD								
134748	ADD INVD								
134749	ADD INVD								
134750	ADD INVD								
134751	ADD INVD								
134752	ADD INVD								
134753	ADD INVD								
134754	ADD INVD								
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134758	ADD INVD								
134759	ADD INVD								
134760	ADD INVD								
134761	ADD INVD								
134762	ADD INVD								
134763	ADD INVD								
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134767	ADD INVD								
134768	ADD INVD								
134769	ADD INVD								
134770	ADD INVD								
134771	ADD INVD								
134772	ADD INVD								
134773	ADD INVD								
134774	ADD INVD								
134775	ADD INVD								
134776	ADD INVD								
134777	ADD INVD								
134778	ADD INVD								
134779	ADD INVD								
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134791	ADD INVD								
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134799	ADD INVD								
134800	ADD INVD								
134801	ADD INVD								
134802	ADD INVD								
134803	ADD INVD								
134804	ADD INVD								
134805	ADD INVD								
134806	ADD INVD								
134807	ADD INVD								
134808	ADD INVD								
134809	ADD INVD								
134810	ADD INVD								
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134814	ADD INVD								
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134836	ADD INVD								
134837	ADD INVD								
134838	ADD INVD								

Table with columns for Node ID, Description, Parameters, and Values. Includes entries for various nodes (e.g., 142131, 142132) and their associated hydrograph data and routing factors.

Table with columns for Node ID, Description, Parameters, and Values. Includes entries for various nodes (e.g., 144009, 144010) and their associated hydrograph data and routing factors.

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145877 ROUTE CHANNEL -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
145878 [RfDf=1.00] out-> 1.0 01:2:NA 4644.01 89.756 Ndate 34:38 37.51 n/a .000
145879 [L/S=na 4630 / 043/055]
145880 [Vmax=.944;Dmax=3.866]
145901 #
145902 # Addition of Subwatershed 4 with Leam Creek to Node 4
145903 #
145904 ROUTE0100:CO0060 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
145905 ADD HYD + 1.0 02:SW2 4644.01 85.943 Ndate 36:10 37.51 n/a .000
145906 + 1.0 02:SW4 585.00 14.953 Ndate 29:55 52.06 n/a .000
145907 + 1.0 02:CLCR 1021.00 19.782 Ndate 30:45 51.16 n/a .000
145908 + 1.0 01:5:NA 4844.00 96.618 Ndate 35:12 37.97 n/a .000
145909 SIMM 1.0 01:5:NA 4844.00 96.618 Ndate 35:12 37.97 n/a .000
145910 ROUTE0100:CO0061 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
145911 SAVE HYD 1.0 01:5:NA 4844.00 96.618 Ndate 35:12 37.97 n/a .000
146000 #
146001 #name :S_N1.010
146002 #remark:Flow at S_N1
146003 #
146004 # Sum of hydrographs from Node 4 routed to Node 2
146005 # Section 9
146006 #
146007 ROUTE0100:CO0062 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
146008 ROUTE CHANNEL -> 1.0 02:5:NA 4844.00 96.618 Ndate 35:12 37.97 n/a .000
146009 [RfDf=1.00] out-> 1.0 01:2:NA 4844.00 96.322 Ndate 35:13 37.97 n/a .000
146010 [L/S=na 1667 / 060/040]
146011 [Vmax=.944;Dmax=3.929]
146012 #
146013 # Addition of Subwatershed 2 with Mhoanah Drain and Smith Drain to Node 2
146014 #
146015 ROUTE0100:CO0063 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
146016 ADD HYD + 1.0 02:NA 4844.00 96.322 Ndate 35:13 37.97 n/a .000
146017 + 1.0 02:SW2 177.00 7.567 Ndate 28:44 47.62 n/a .000
146018 + 1.0 02:SMDR 1122.00 17.981 Ndate 31:42 52.06 n/a .000
146019 [RfDf=2.0] out-> 1.0 01:2:NA 4844.00 40.710 Ndate 31:28 46.75 n/a .000
146020 SIMM 1.0 01:5:NA 52483.00 143.580 Ndate 32:59 38.76 n/a .000
146021 ROUTE0100:CO0064 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
146022 SAVE HYD 1.0 01:5:NA 52483.00 143.580 Ndate 32:59 38.76 n/a .000
146023 #name :H_S2
146024 #remark:Flow at S_N2 Jock River Gauge at Modie Dr.
146025 #
146026 # Sum of hydrographs from Node 2 routed to Node 1
146027 # Section 10
146028 #
146029 #*****
146030 #
146031 # Hydrograph from Node 2 routed to Node 416
146032 # Channel X-Section obtained from RVC/Hydraulic Model - Station 9025
146033 #
146034 ROUTE0100:CO0065 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
146035 ROUTE CHANNEL -> 1.0 02:5:NA 52483.00 143.580 Ndate 32:59 38.76 n/a .000
146036 [RfDf=1.00] out-> 1.0 01:4:16 52483.00 139.298 Ndate 33:45 38.76 n/a .000
146037 [L/S=na 2327 / 050/055]
146038 #
146039 # Catchment SW
146040 #
146041 # - Portion of RVCa catchment SW outside of Reach 1 subwatershed
146042 # - Undeveloped agricultural land
146043 #
146044 ROUTE0100:CO0066 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
146045 CONTINUES STANDARD 1.0 01:2:NA 52483.00 139.298 Ndate 33:45 38.76 n/a .000
146046 [C=72.0; N=3.00; Tm=7.0]
146047 [RfC=4.0; SM=39.75; SMM=264.99; SK=010]
146048 #
146049 ROUTE0100:CO0067 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
146050 CONTINUES STANDARD 1.0 01:2:NA 52483.00 139.298 Ndate 33:45 38.76 n/a .000
146051 [XMP=.65;Tm=.65]
146052 [LRS=2.0;CN=61.0]
146053 #
146054 [Previous area: IArea:4.67;SLPP=.00;LQP=.40;MPP=.250;SCP=.0]
146055 [Impervious area: IArea:1.57;SLPI=.75;LGA=.547;MNI=.013;SCI=.0]
146056 [IAREC=mp 4.00; IAREBep=4.00]
146057 #
146058 ROUTE0100:CO0068 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
146059 COMPUTE DUALID 1.0 01:5:1-CRKE 44.93 4.991 Ndate 27:52 70.65 n/a .000
146060 Mjr Syst=0.0; Tot Of Vol=0.000E+00; N Of Cr=0.0; Tot Dur Of=0. hrs]
146061 #
146062 ADD HYD + 1.0 02:5:NA 44.93 4.991 Ndate 27:52 70.65 n/a .000
146063 + 1.0 02:1-CRAN 44.93 4.991 Ndate 27:52 70.65 n/a .000
146064 SIMM 1.0 01:5:1-CRKS 44.93 4.991 Ndate 27:52 70.65 n/a .000
146065 ROUTE0100:CO0069 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
146066 ROUTE RESERVOIR -> 1.0 02:5:1-CRKS 44.93 4.991 Ndate 27:52 70.65 n/a .000
146067 + 1.0 01:5:1-CRKR 43.17 5.37 Ndate 28:35 70.65 n/a .000
146068 + 1.0 01:5:1-CRKF 41.72 5.94 Ndate 29:17 70.65 n/a .000
146069 overflow out-> 1.0 01:5:1-CRKR 43.17 5.37 Ndate 28:35 70.65 n/a .000
146070 [MSStkEd=1.792E+01; Tot Of Vol=1.240E+00; N Of Cr=2.0; Tot Dur Of=1. hrs]
146071 #
146072 ROUTE0100:CO0070 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
146073 ADD HYD + 1.0 02:NA 52483.00 139.298 Ndate 33:45 38.76 n/a .000
146074 + 1.0 02:SW4 536.42 7.274 Ndate 31:14 40.95 n/a .000
146075 + 1.0 02:1-CRAN 44.93 4.991 Ndate 27:52 70.65 n/a .000
146076 + 1.0 01:5:1-CRKF 1.76 1.172 Ndate 28:35 70.65 n/a .000
146077 + 1.0 01:5:1-CRKS 51064.00 145.256 Ndate 38:31 38.81 n/a .000
146078 ROUTE0100:CO0072 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
146079 SAVE HYD 1.0 01:5:NA;416 53064.36 145.245 Ndate 33:31 38.81 n/a .000
146080 #name :SN_416.010
146081 #remark:Total Flow at Highway 416 before Station 7245
146082 #
146083 # Hydrograph from Node 416 routed to Node at Keeler drain
146084 # Channel X-Section obtained from RVC/Hydraulic Model - Station 7245
146085 #
146086 ROUTE0100:CO0073 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
146087 ROUTE CHANNEL -> 1.0 02:3:NA 53064.36 145.245 Ndate 33:31 38.81 n/a .000
146088 [RfDf=1.00] out-> 1.0 01:2:NA 53064.36 145.101 Ndate 33:45 38.81 n/a .000
146089 [L/S=na 097 / 304/055]
146090 [Vmax=1.729;Dmax=3.269]
146091 #
146092 # Catchment OKEEFIE
146093 # - To O Keefer drain (north of the Jock)
146094 #
146095 # - 2020 12:01 add Okeefe model (Area 513.02 HA) instead of current Okeefe (Area 513.02 HA)
146096 # - 2020 12:01 Okeefe model added as the NEWEST Okeefe model (Citi-Gear 2014).
146097 #*****
146098 ROUTE0100:CO0074 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
146099 CONTINUES STANDARD 1.0 01:0:1A 63.72 1.380 Ndate 28:38 30.74 347.000
146100 [C=61.0; N=3.00; Tm=12.00]
146101 [IAREC=4.00; SM=14.47; SMM=430.01; SK=010]
146102 #
146103 ROUTE0100:CO0075 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
146104 ROUTE CHANNEL -> 1.0 02:0:1R 63.72 1.380 Ndate 28:38 30.74 n/a .000
146105 [RfDf=1.00] out-> 1.0 01:0:1R 63.72 1.380 Ndate 29:13 30.74 n/a .000
146106 [L/S=na 060 / 630/043]
146107 [Vmax=.926;Dmax=0.93]
146108 #
146109 ROUTE0100:CO0076 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
146110 CONTINUES STANDARD 1.0 01:0:1R 28.61 4.85 Ndate 29:13 28.38 320.000
146111 [C=61.0; N=3.00; Tm=12.00]
146112 [IAREC=4.00; SM=76.32; SMM=508.81; SK=010]
146113 #
146114 ROUTE0100:CO0077 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
146115 CONTINUES STANDARD 1.0 01:0:1A 46.94 6.50 Ndate 28:59 21.79 246.000
146116 [C=61.0; N=3.00; Tm=12.00]
146117 #
146118 ROUTE0100:CO0078 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
146119 ADD HYD + 1.0 02:0:1R 63.72 1.380 Ndate 29:13 30.74 n/a .000
146120 + 1.0 02:0:1R 28.61 4.85 Ndate 29:13 28.38 320.000
146121 + 1.0 02:0:1A 46.94 6.50 Ndate 28:59 21.79 n/a .000
146122 SIMM 1.0 01:0:1:PTI 256.03 5.938 Ndate 28:19 30.11 n/a .000
146123 ROUTE0100:CO0079 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
146124 ROUTE CHANNEL -> 1.0 02:0:1R 139.27 2.427 Ndate 29:10 27.24 n/a .000
146125 [RfDf=1.00] out-> 1.0 01:0:1R 139.27 2.427 Ndate 29:12 27.24 n/a .000
146126 [L/S=na 210 / 810/043]
146127 #
146128 ROUTE0100:CO0080 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
146129 CONTINUES STANDARD 1.0 01:0:1A 16.46 .220 Ndate 28:45 18.07 211.000
146130 [C=43.0; N=3.00; Tm=7.00]
146131 [IAREC=4.00; SM=13.47; SMM=896.47; SK=010]
146132 #
146133 ROUTE0100:CO0081 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
146134 CONTINUES STANDARD 1.0 01:0:1A 39.67 1.454 Ndate 28:21 32.90 371.000
146135 [XMP=.15;Tm=.30]
146136 #
146137 [Previous area: IArea:4.67;SLPP=.00;LQP=.40;MPP=.035;SCP=.0]
146138 [Impervious area: IArea:1.57;SLPI=.75;LGA=.1880;MNI=.013;SCI=.0]
146139 [IAREC=mp 4.00; IAREBep=4.00]
146140 #
146141 ROUTE0100:CO0082 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
146142 CONTINUES STANDARD 1.0 01:0:1A 60.63 3.669 Ndate 28:10 38.00 429.000
146143 [XMP=.13;Tm=.26]
146144 [LRS=2.0;CN=61.0]
146145 #
146146 [Previous area: IArea:4.67;SLPP=.00;LQP=.03;LGA=.1880;MNI=.013;SCI=.0]
146147 [Impervious area: IArea:1.57;SLPI=.75;LGA=.1450;MNI=.013;SCI=.0]
146148 [IAREC=mp 4.00; IAREBep=4.00]
146149 #
146150 ROUTE0100:CO0083 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
146151 ADD HYD + 1.0 02:0:1R 139.27 2.423 Ndate 29:12 27.24 n/a .000
146152 + 1.0 02:0:1R 28.61 4.85 Ndate 29:13 28.38 320.000
146153 + 1.0 02:0:1A 46.94 6.50 Ndate 28:59 21.79 n/a .000
146154 + 1.0 02:0:1A 261.31 6.636 Ndate 28:19 30.11 n/a .000
146155 SIMM 1.0 01:0:1:PTI 256.03 5.938 Ndate 28:19 30.11 n/a .000
146156 ROUTE0100:CO0084 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
146157 CONTINUES STANDARD 1.0 01:0:1A 5.28 .117 Ndate 28:37 25.16 284.000
146158 [C=54.0; N=3.00; Tm=6.00]
146159 [IAREC=4.00; SM=8.00; SMM=50.07; SK=010]
146160 #
146161 ROUTE0100:CO0085 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
146162 ADD HYD + 1.0 02:PTI 256.03 5.938 Ndate 28:19 30.11 n/a .000
146163 + 1.0 02:0:1R 5.28 .117 Ndate 28:37 25.16 n/a .000
146164 SIMM 1.0 01:0:1:PTI 261.31 6.636 Ndate 28:19 30.11 n/a .000
146165 ROUTE0100:CO0086 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
146166 ROUTE CHANNEL -> 1.0 02:0:1R 261.31 6.636 Ndate 28:19 30.11 n/a .000
146167 [RfDf=1.00] out-> 1.0 01:0:1R 261.31 5.843 Ndate 28:23 30.01 n/a .000
146168 [L/S=na 302 / 1,000/043]
146169 [Vmax=.853;Dmax=.797]
146170 #
146171 ROUTE0100:CO0087 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm
146172 CONTINUES STANDARD 1.0 01:0:1A 21.00 1.110 Ndate 28:12 50.22 567.000
146173 [C=54.0; N=3.00; Tm=28.1]
146174 [IAREC=4.00; SM=21.00; SMM=140.62; SK=010]
146175 #
146176 ROUTE0100:CO0088 -> DfMn ID NDD -> AREHA-QPEAKm-TPeakDte-hh:mm-RvMn R.C.-DfWm

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Table with columns for ID, description, and numerical data. Includes entries for various systems like ROUTE RESERVOIR, ROUTE CHANNEL, and various flow types (ADD HYD, FLOW, etc.).


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160833 + 1.02:PC01-S 8.03 .756 N_date 27:49 54.46 n/a .000
160834 + 1.02:PC01-S 16.05 2.927 N_date 28:05 82.82 n/a .000
160835 + 1.02:PC03-S 7.37 1.019 N_date 28:06 64.90 n/a .000
160860 SIM 1.02:1241-out 54658.51 144.744 N_date 36:48 39.28 n/a .000
160870 R0100:CO305 ----- Dfn=ID NND -----AREQA-QPEAKm-TpeakDte-hh:mm-----Rvmm R C-----Dfwm
160880 SAVE IHD 1.01:2421 54658.51 144.701 N_date 36:48 39.28 n/a .000
160889 # Name: 2421.0100
160890 remark: Total Flow at Ken Burnett Outlet
160910 # Hydrograph from Node 3633 to Station 3633
160920 # Channel X-Section obtained from RWCA Hydraulic Model - Station 2421
160930 #
160940 R0100:CO306 ----- Dfn=ID NND -----AREQA-QPEAKm-TpeakDte-hh:mm-----Rvmm R C-----Dfwm
160950 ROUTE CHANNEL > 1.02:2421 54658.51 144.701 N_date 36:48 39.28 n/a .000
160960 + [RDE 1.00] out c 1.02:1241-out 54658.51 144.744 N_date 36:44 39.28 n/a .000
160970 [L/S= 294 / 10W/ 035]
160980 # Name: 1396.Dmax=57
160990 R0100:CO307 ----- Dfn=ID NND -----AREQA-QPEAKm-TpeakDte-hh:mm-----Rvmm R C-----Dfwm
161000 ADD IHD + 1.02:2421-out 54658.51 144.744 N_date 36:44 39.28 n/a .000
161010 + 1.02:TOOD.MJ 1.99 .016 N_date 27:52 66.78 n/a .000
161020 + 1.02:TOOD.MN 1.99 .016 N_date 27:52 66.78 n/a .000
161030 + 1.02:TOOD.MJ 1.99 .016 N_date 27:52 66.78 n/a .000
161040 + 1.02:TOOD.MN 1.99 .016 N_date 27:52 66.78 n/a .000
161050 SIM 1.01:TOOD 121.35 20.00 N_date 28:03 66.72 n/a .000
161060 R0100:CO308 ----- Dfn=ID NND -----AREQA-QPEAKm-TpeakDte-hh:mm-----Rvmm R C-----Dfwm
161070 SAVE IHD 1.01:SN:KB 54681.20 144.787 N_date 36:44 39.29 n/a .000
161080 # Name: SN:KB 0100
161090 remark: Total Flow before Station 3633
161100 # Hydrograph from Station 3633 to Node Todd
161110 # Channel X-Section obtained from RWCA Hydraulic Model - Station 3633
161120 # JFSA 2021-01-18 add change the channel length (at station 3633) from 650m to 608m and change the slope from 0.0489% to 0.2
161130 R0100:CO309 ----- Dfn=ID NND -----AREQA-QPEAKm-TpeakDte-hh:mm-----Rvmm R C-----Dfwm
161140 ROUTE CHANNEL > 1.02:SN:KB 54681.20 144.787 N_date 36:44 39.29 n/a .000
161150 + [RDE 1.00] out c 1.02:TOOD 54681.20 144.732 N_date 36:50 39.29 n/a .000
161160 [L/S= 608 / 247/ 035]
161170 # Name: 1906.Dmax=63
161180 #
161190 # Catchment Greenbank
161200 # To Greenbank Drain (south of the Jack)
161210 # JFSA 2021-01-18 add Greenbank pond as per JFSA P598.00-15, June 2016
161220 # JFSA 2021-01-19 update the TODD Drainage Area to be based on QIS measurements
161230 #
161240 R0100:CO310 ----- Dfn=ID NND -----AREQA-QPEAKm-TpeakDte-hh:mm-----Rvmm R C-----Dfwm
161250 CONTINUOUS STANHYD 1.01:Greenbank 36.60 7.069 N_date 28:01 71.80 811 .000
161260 [XMP= 64:TIMP= 68]
161270 [L/S= 2 :CN= 77:0]
161280 [Previous area: Iper= 4.67:SLP=1.00:LG= 40:MP= 250:SCP= 0]
161290 [Impervious area: Iper= 1.57:SLP=1.00:LG= 494:MN= 013:SCI= 0]
161300 [IAREC mp= 4.00: IAREBER= 4.00]
161310 [SM N= 31.15: SMAW=207.66: SK= 010]
161320 R0100:CO311 ----- Dfn=ID NND -----AREQA-QPEAKm-TpeakDte-hh:mm-----Rvmm R C-----Dfwm
161330 ROUTE RESERVOIR > 1.02:Greenbank 36.60 7.069 N_date 28:01 71.80 n/a .000
161340 + 1.02:TOOD.MJ 1.99 .016 N_date 28:01 71.80 n/a .000
161350 + 1.02:TOOD.MN 1.99 .016 N_date 28:01 71.80 n/a .000
161360 [MSk=0.00: 9351:00] TotVol=0.0000E+00, NcOf= 0, TotDur=0.0 h=rs]
161370 R0100:CO312 ----- Dfn=ID NND -----AREQA-QPEAKm-TpeakDte-hh:mm-----Rvmm R C-----Dfwm
161380 ADD IHD + 1.02:TOOD 54681.20 144.732 N_date 36:50 39.29 n/a .000
161390 + 1.02:TOOD.MJ 1.99 .016 N_date 28:01 71.80 n/a .000
161400 + 1.02:TOOD.MN 1.99 .016 N_date 28:01 71.80 n/a .000
161410 + 1.02:TOOD.MJ 1.99 .016 N_date 28:01 71.80 n/a .000
161420 + 1.02:TOOD.MN 1.99 .016 N_date 28:01 71.80 n/a .000
161430 SIM 1.01:TOOD 54717.80 144.894 N_date 36:50 39.32 n/a .000
161440 R0100:CO313 ----- Dfn=ID NND -----AREQA-QPEAKm-TpeakDte-hh:mm-----Rvmm R C-----Dfwm
161450 SAVE IHD 1.01:Greenbank 54717.80 144.894 N_date 36:50 39.32 n/a .000
161460 # Name: Greenb 0100
161470 remark: Total Flow at Greenbank Drain
161480 # To Todd Pond (south of the Jack)
161490 # Subdivison with 435 imp. as per Barhaven South MS
161500 # 2020-11-30 increase imp. based on P598.04-11
161510 # 2020-11-30 update TODD Drainage Area to be 146.015 ha based on P598.04-11
161520 # 2020-11-30 update TODD Drainage Area to be 146.015 ha based on P598.04-11
161530 #
161540 # JFSA 2021-01-19 add TODD.MN as part of Clarker "WCLAR.MN" and remove it from Todd
161550 R0100:CO314 ----- Dfn=ID NND -----AREQA-QPEAKm-TpeakDte-hh:mm-----Rvmm R C-----Dfwm
161560 CONTINUOUS STANHYD 1.01:TOOD.MN 2.10 128.228 N_date 28:00 66.78 754 .000
161570 [XMP= 53:TIMP= 57]
161580 [L/S= 2 :CN= 77:0]
161590 [Previous area: Iper= 4.67:SLP=1.00:LG= 40:MP= 250:SCP= 0]
161600 [Impervious area: Iper= 1.57:SLP=1.00:LG= 118:MN= 013:SCI= 0]
161610 [IAREC mp= 4.00: IAREBER= 4.00]
161620 [SM N= 31.15: SMAW=207.66: SK= 010]
161630 R0100:CO315 ----- Dfn=ID NND -----AREQA-QPEAKm-TpeakDte-hh:mm-----Rvmm R C-----Dfwm
161640 CONTINUOUS STANHYD 1.01:TOOD.MJ 12 .025 N_date 28:00 66.78 754 .000
161650 [XMP= 53:TIMP= 57]
161660 [L/S= 2 :CN= 77:0]
161670 [Previous area: Iper= 4.67:SLP=1.00:LG= 40:MP= 250:SCP= 0]
161680 [Impervious area: Iper= 1.57:SLP=1.00:LG= 28:MN= 013:SCI= 0]
161690 [IAREC mp= 4.00: IAREBER= 4.00]
161700 [SM N= 31.15: SMAW=207.66: SK= 010]
161710 R0100:CO316 ----- Dfn=ID NND -----AREQA-QPEAKm-TpeakDte-hh:mm-----Rvmm R C-----Dfwm
161720 CONTINUOUS STANHYD 1.01:TOOD.MN 30.23 5.210 N_date 28:02 68.65 775 .000
161730 [XMP= 52:TIMP= 64]
161740 [L/S= 2 :CN= 77:0]
161750 [Previous area: Iper= 4.67:SLP=1.00:LG= 40:MP= 250:SCP= 0]
161760 [Impervious area: Iper= 1.57:SLP=1.00:LG= 449:MN= 013:SCI= 0]
161770 [IAREC mp= 4.00: IAREBER= 4.00]
161780 [SM N= 31.15: SMAW=207.66: SK= 010]
161790 R0100:CO317 ----- Dfn=ID NND -----AREQA-QPEAKm-TpeakDte-hh:mm-----Rvmm R C-----Dfwm
161800 CONTINUOUS STANHYD 1.01:TOOD.MJ 112.91 17.286 N_date 28:04 66.60 752 .000
161810 [XMP= 52:TIMP= 57]
161820 [L/S= 2 :CN= 77:0]
161830 [Previous area: Iper= 4.67:SLP=1.00:LG= 40:MP= 250:SCP= 0]
161840 [Impervious area: Iper= 1.57:SLP=1.00:LG= 868:MN= 013:SCI= 0]
161850 [IAREC mp= 4.00: IAREBER= 4.00]
161860 [SM N= 31.15: SMAW=207.66: SK= 010]
161870 R0100:CO318 ----- Dfn=ID NND -----AREQA-QPEAKm-TpeakDte-hh:mm-----Rvmm R C-----Dfwm
161880 CONTINUOUS STANHYD 1.01:TOOD.P 3.06 .669 N_date 28:00 70.28 794 .000
161890 [XMP= 63:TIMP= 63]
161900 [L/S= 2 :CN= 77:0]
161910 [Previous area: Iper= 4.67:SLP=1.00:LG= 40:MP= 250:SCP= 0]
161920 [Impervious area: Iper= 1.57:SLP=1.00:LG= 143:MN= 013:SCI= 0]
161930 [IAREC mp= 4.00: IAREBER= 4.00]
161940 [SM N= 31.15: SMAW=207.66: SK= 010]
161950 # 5 Year + 12% Capture
161960 R0100:CO319 ----- Dfn=ID NND -----AREQA-QPEAKm-TpeakDte-hh:mm-----Rvmm R C-----Dfwm
161970 ROUTE RESERVOIR > 1.02:TOOD.MN 30.23 5.210 N_date 28:02 68.65 n/a .000
161980 + 1.02:TOOD.MJ 1.99 .016 N_date 28:02 68.65 n/a .000
161990 + 1.02:TOOD.MN 1.99 .016 N_date 28:02 68.65 n/a .000
162000 [MSk=0.00: 15212:03] TotVol=1.0944E+00, NcOf= 1, TotDur=0.0 h=rs]
162010 # 5 Year + 12% Capture
162020 R0100:CO320 ----- Dfn=ID NND -----AREQA-QPEAKm-TpeakDte-hh:mm-----Rvmm R C-----Dfwm
162030 ROUTE RESERVOIR > 1.02:TOOD.MN 2.10 .428 N_date 28:00 66.78 n/a .000
162040 + 1.02:TOOD.MJ 1.99 .016 N_date 27:52 66.78 n/a .000
162050 + 1.02:TOOD.MN 1.99 .016 N_date 27:52 66.78 n/a .000
162060 [MSk=0.00: 1204E-03] TotVol=7.282E-02, NcOf= 1, TotDur=0.0 h=rs]
162070 R0100:CO321 ----- Dfn=ID NND -----AREQA-QPEAKm-TpeakDte-hh:mm-----Rvmm R C-----Dfwm
162080 ROUTE RESERVOIR > 1.02:TOOD.MN 1.99 .016 N_date 27:52 66.78 n/a .000
162090 + 1.02:TOOD.MN 1.99 .016 N_date 27:52 66.78 n/a .000
162100 + 1.02:TOOD.MN 1.99 .016 N_date 27:52 66.78 n/a .000
162110 [MSk=0.00: 9808E-04] TotVol=3.933E-03, NcOf= 1, TotDur=0.0 h=rs]
162120 R0100:CO322 ----- Dfn=ID NND -----AREQA-QPEAKm-TpeakDte-hh:mm-----Rvmm R C-----Dfwm
162130 CONTINUOUS STANHYD 1.01:AI 121.35 20.00 N_date 28:03 62.46 705 .000
162140 [XMP= 42:TIMP= 52]
162150 [L/S= 2 :CN= 77:0]
162160 [Previous area: Iper= 4.67:SLP=1.00:LG= 40:MP= 250:SCP= 0]
162170 [Impervious area: Iper= 1.57:SLP=1.00:LG= 566:MN= 013:SCI= 0]
162180 [IAREC mp= 4.00: IAREBER= 4.00]
162190 [SM N= 33.81: SMAW=225.42: SK= 010]
162200 R0100:CO323 ----- Dfn=ID NND -----AREQA-QPEAKm-TpeakDte-hh:mm-----Rvmm R C-----Dfwm
162210 COMPUTE DUALIHD 1.01:AI 25.50 3.884 N_date 28:03 62.46 n/a .000
162220 + 1.02:TOOD.MJ 1.99 .016 N_date 28:03 62.46 n/a .000
162230 + 1.02:TOOD.MN 1.99 .016 N_date 28:03 62.46 n/a .000
162240 [MSk=0.00: 9240E-03] TotVol=0.0000E+00, NcOf= 0, TotDur=0.0 h=rs]
162250 R0100:CO324 ----- Dfn=ID NND -----AREQA-QPEAKm-TpeakDte-hh:mm-----Rvmm R C-----Dfwm
162260 ADD IHD + 1.02:TOOD.MN 1.99 .016 N_date 27:52 66.78 n/a .000
162270 + 1.02:TOOD.MJ 1.99 .016 N_date 27:52 66.78 n/a .000
162280 + 1.02:TOOD.MJ 1.99 .016 N_date 28:02 68.65 n/a .000
162290 + 1.02:TOOD.MN 1.99 .016 N_date 28:02 68.65 n/a .000
162300 + 1.02:TOOD.MN 1.99 .016 N_date 28:02 68.65 n/a .000
162310 + 1.02:TOOD.MN 1.99 .016 N_date 28:02 68.65 n/a .000
162320 + 1.02:TOOD.MN 1.99 .016 N_date 28:02 68.65 n/a .000
162330 SIM 1.01:TOOD 121.35 20.00 N_date 28:03 66.72 n/a .000
162340 R0100:CO325 ----- Dfn=ID NND -----AREQA-QPEAKm-TpeakDte-hh:mm-----Rvmm R C-----Dfwm
162350 SAVE IHD 1.01:TOOD 121.35 20.00 N_date 28:03 66.72 n/a .000
162360 # Name: TODD 0100
162370 remark: Total Flow at Todd Drain
162380 # Todd Pond 3
162390 # Rating curve obtained from Barhaven South MS modeling
162400 # station 2007, Tributary Drainage Area to M33 Pond 3 = 193 ha
162410 #
162420 R0100:CO326 ----- Dfn=ID NND -----AREQA-QPEAKm-TpeakDte-hh:mm-----Rvmm R C-----Dfwm
162430 ROUTE RESERVOIR > 1.02:TOOD.MN 121.35 20.00 N_date 28:03 66.78 n/a .000
162440 + 1.02:TOOD.MN 1.99 .016 N_date 28:03 66.78 n/a .000
162450 + 1.02:TOOD.MN 1.99 .016 N_date 28:03 66.78 n/a .000
162460 + 1.02:TOOD.MN 1.99 .016 N_date 28:03 66.78 n/a .000
162470 + 1.02:TOOD.MN 1.99 .016 N_date 28:03 66.78 n/a .000
162480 + 1.02:TOOD.MN 1.99 .016 N_date 28:03 66.78 n/a .000
162490 + 1.02:TOOD.MN 1.99 .016 N_date 28:03 66.78 n/a .000
162500 + 1.02:TOOD.MN 1.99 .016 N_date 28:03 66.78 n/a .000
162510 + 1.02:TOOD.MN 1.99 .016 N_date 28:03 66.78 n/a .000
162520 + 1.02:TOOD.MN 1.99 .016 N_date 28:03 66.78 n/a .000
162530 SIM 1.01:TOOD 54840.69 145.243 N_date 36:49 39.28 n/a .000
162540 R0100:CO328 ----- Dfn=ID NND -----AREQA-QPEAKm-TpeakDte-hh:mm-----Rvmm R C-----Dfwm
162550 SAVE IHD 1.01:SN:TO 54840.69 145.243 N_date 36:49 39.28 n/a .000
162560 # Name: SN:TO 0100
162570 remark: Total Flow at Todd Drain
162580 #
162590 # Hydrograph from Todd Drain routed to Corrigan Drain
162600 # Channel X-Section obtained from RWCA Hydraulic Model - Station 2462
162610 # 2021-02-19 Change the slope from 0.033 % (as per Station Report 2007) to 0.05 % so the model will be more stable and g
162620 R0100:CO329 ----- Dfn=ID NND -----AREQA-QPEAKm-TpeakDte-hh:mm-----Rvmm R C-----Dfwm
162630 ROUTE CHANNEL > 1.02:AI:M 54840.69 145.243 N_date 36:49 39.28 n/a .000
162640 + [RDE 1.00] out c 1.02:AI:M 54840.69 145.243 N_date 36:58 39.38 n/a .000
162650 [L/S= 200 / 05W/ 045]
162660 # Name: 881.Dmax=3.884
162670 R0100:CO330 ----- Dfn=ID NND -----AREQA-QPEAKm-TpeakDte-hh:mm-----Rvmm R C-----Dfwm
162680 SAVE IHD 1.01:AI:M 54840.69 145.243 N_date 36:58 39.38 n/a .000
162690 # Name: N:TO 0100
162700 #
162710 #
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162740 #
162750 #
162760 #
162770 #
162780 #
162790 #
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164900 #
164910 #
164920 #
164930 #
164940 #
164950 #
164960 #
164970 #
164980 #
164990 #
165000 #

```



```

168313 ROUTE RESERVOIR -> 1.0 02: MLLS 175.99 20.390 No.date 28:06 56.87 n/a .000
168328 out <= 1.0 01: MLLP 146.22 4.050 No.date 28:08 56.87 n/a .000
168333 overflow <= 1.0 03: MLL-OW 20.77 16.228 No.date 28:08 56.87 n/a .000
168349 [MKS]obled: 2.1010E+01 1693540) ab. N.Opt= 2. TotDur=0.4 hrs]
168355 R0100: CO0426 -----Dfm n-1D NMD -----AREba-QPEAgcm-TpeakDtte:hh:mm-----Rvwm R.C-----Dfwm
168360 ADD HYD + 1.0 02: N.M 5520.07 145.768 No.date 36:59 39.46 n/a .000
168375 + 1.0 02: MLL-OW 29.77 16.228 No.date 28:08 56.87 n/a .000
168388 + 1.0 02: MLLP 146.22 4.050 No.date 28:08 56.87 n/a .000
168399 SLM 55196.05 146.399 No.date 36:58 39.51 n/a .000
168400 R1000: CO0427 -----Dfm n-1D NMD -----AREba-QPEAgcm-TpeakDtte:hh:mm-----Rvwm R.C-----Dfwm
168413 SAVE HYD 1.0 01: SN,NI 55196.05 146.399 No.date 36:58 39.51 n/a .000
168425 fnam: SN,M 0100
168433 remark:Total Flow at Jockvale Road
168445 #
168455 # Hydrograph from Jockvale Road routed to Hart's Desire
168460 # Channel X-Section obtained from RVCMA Hydraulic Model - Station 689
168475 #
168480 R1000: CO0428 -----Dfm n-1D NMD -----AREba-QPEAgcm-TpeakDtte:hh:mm-----Rvwm R.C-----Dfwm
168495 ROUTE CHANNEL -> 1.0 02: SN,M 55196.05 146.399 No.date 36:58 39.51 n/a .000
168500 [RDF= 1.00] out <= 1.0 01: NI,DE 55196.05 146.071 No.date 37:13 39.51 n/a .000
168515 [L/S= 1962 / 221.045]
168525 [Vmax= 1.642; Dmax= 2.661]
168535 *****
168545 # Catchment DESIRE
168555 # - To Jock River (north of the Jock)
168560 # Rural estate subdivision (Hart's Desire Community)
168575 #
168580 R1000: CO0429 -----Dfm n-1D NMD -----AREba-QPEAgcm-TpeakDtte:hh:mm-----Rvwm R.C-----Dfwm
168595 CONTINUES STANHPD 1.0 01: DESIRE 23.78 3.004 No.date 28:03 53.11 600 .000
168600 [M P= 25; TSM= 25]
168615 [LRS= 2; C= 77.0]
168625 [Pervious area: IArea 4.67; SLP1= 0; LCP= 40; MPM= 250; SCW= 0]
168635 [Impervious area: IArea 1.57; SLP1= 0; LCP= 400; MN= 013; SC1= 0]
168645 [IARECmp= 4.00; IARECper= 4.00]
168655 [SM N= 31.35; SMAX= 24.45; SKE= 010]
168665 *****
168675 # Catchment JOCKVA
168680 # - To Jockvale SWM Facility
168695 # - Residential development & golf course
168700 # - JESA CO0411 update JOCKVA after updating CORP GIS as per HR GROUP July 2008.
168715 # JOCKVA area became 225.13 ha instead of 257.63 ha. JOCKVA separated into two areas JOCKVA and EX LAND 32.5 ha as
168725 #
168730 R1000: CO0430 -----Dfm n-1D NMD -----AREba-QPEAgcm-TpeakDtte:hh:mm-----Rvwm R.C-----Dfwm
168745 CONTINUES STANHPD 1.0 01: JOCKVA 225.13 28.623 No.date 28:07 62.70 708 .000
168755 [M P= 50; TSM= 50]
168765 [LRS= 2; C= 74.0]
168775 [Pervious area: IArea 4.67; SLP1= 0; LCP= 40; MPM= 250; SCW= 0]
168785 [Impervious area: IArea 1.57; SLP1= 0; LCP= 400; MN= 013; SC1= 0]
168795 [IARECmp= 4.00; IARECper= 4.00]
168805 [SM N= 36.67; SMAX= 24.45; SKE= 010]
168815 R1000: CO0431 -----Dfm n-1D NMD -----AREba-QPEAgcm-TpeakDtte:hh:mm-----Rvwm R.C-----Dfwm
168825 ADD HYD + 1.0 02: JOCKVA 225.13 28.623 No.date 28:07 62.70 n/a .000
168835 + 1.0 02: JOCKVA 225.13 28.623 No.date 28:07 62.70 n/a .000
168845 + 1.0 02: NI 36.820 No.date 28:05 62.88 n/a .000
168855 + 1.0 02: NI 19.402 No.date 28:04 62.88 n/a .000
168865 SLM 1.0 01: JOCKVA-TO 256.41 31.850 No.date 28:06 62.71 n/a .000
168875 R1000: CO0432 -----Dfm n-1D NMD -----AREba-QPEAgcm-TpeakDtte:hh:mm-----Rvwm R.C-----Dfwm
168885 SAVE HYD 1.0 01: JOCKVA-TO 256.41 31.850 No.date 28:06 62.71 n/a .000
168895 fnam: JOCKVA TO 0100
168905 remark:Total Flow at KB first pond
168915 #
168925 # Jockvale SWM Facility
168935 # Rating curve obtained from Jockvale Servicing Study (CC, 1999)
168945 #
168950 R1000: CO0433 -----Dfm n-1D NMD -----AREba-QPEAgcm-TpeakDtte:hh:mm-----Rvwm R.C-----Dfwm
168965 ROUTE RESERVOIR -> 1.0 02: JOCKP 256.41 12.850 No.date 28:35 62.71 n/a .000
168975 out <= 1.0 01: JOCKP 256.41 12.850 No.date 28:35 62.71 n/a .000
168985 overflow <= 1.0 03: JO-OW 0.00 0.00 No.date 0:00 0.00 n/a .000
168995 [MKS]obled: 6.040E+01 0.0000E+00 ab. N.Opt= 0. TotDur=0.0 hrs]
169000 R1000: CO0434 -----Dfm n-1D NMD -----AREba-QPEAgcm-TpeakDtte:hh:mm-----Rvwm R.C-----Dfwm
169015 ADD HYD + 1.0 02: NI,DE 55196.05 146.071 No.date 37:13 39.51 n/a .000
169025 + 1.0 02: DESIRE 23.78 3.004 No.date 28:03 53.11 n/a .000
169035 + 1.0 02: JO-OW 0.00 0.00 No.date 0:00 0.00 n/a .000
169045 + 1.0 02: JOCKP 256.41 12.850 No.date 28:35 62.71 n/a .000
169055 SLM 1.0 01: SN,DE 55476.25 147.027 No.date 37:12 39.63 n/a .000
169065 R1000: CO0435 -----Dfm n-1D NMD -----AREba-QPEAgcm-TpeakDtte:hh:mm-----Rvwm R.C-----Dfwm
169075 SAVE HYD 1.0 01: SN,DE 55476.25 147.027 No.date 37:12 39.63 n/a .000
169085 fnam: SN,DE 0100
169095 remark:Total Flow at Hart's Desire
169105 #
169115 # Hydrograph from Hart's Desire routed to Rideau River
169120 # Channel X-Section obtained from RVCMA Hydraulic Model - Station 0
169135 #
169140 R1000: CO0436 -----Dfm n-1D NMD -----AREba-QPEAgcm-TpeakDtte:hh:mm-----Rvwm R.C-----Dfwm
169155 ROUTE CHANNEL -> 1.0 02: SN,DE 55476.25 147.027 No.date 37:12 39.63 n/a .000
169165 [RDF= 1.00] out <= 1.0 01: NI 55476.25 147.014 No.date 37:15 39.63 n/a .000
169175 [L/S= 563 / 967.045]
169185 [Vmax= 2.19; Dmax= 1.324]
169195 *****
169205 # Catchment S
169215 # - To Jock River (north and south)
169225 # Underlapped floodplain and river
169235 #
169240 R1000: CO0437 -----Dfm n-1D NMD -----AREba-QPEAgcm-TpeakDtte:hh:mm-----Rvwm R.C-----Dfwm
169255 CONTINUES STANHPD 1.0 01: S-2 1.02 94 5.685 No.date 28:20 40.95 142 .000
169265 [C= 72.0; N= 3.00; Tpm= 40]
169275 [IAREC= 4.00; SLM N= 39.75; SMAX= 264.99; SKE= 010]
169285 [InterEventTime= 12.00]
169295 R1000: CO0438 -----Dfm n-1D NMD -----AREba-QPEAgcm-TpeakDtte:hh:mm-----Rvwm R.C-----Dfwm
169305 ADD HYD + 1.0 02: S 55476.25 147.014 No.date 37:15 39.63 n/a .000
169315 + 1.0 02: S-2 102.94 5.685 No.date 28:20 40.95 n/a .000
169325 SLM 1.0 01: SN,NI 55579.19 147.276 No.date 37:15 39.63 n/a .000
169335 R1000: CO0439 -----Dfm n-1D NMD -----AREba-QPEAgcm-TpeakDtte:hh:mm-----Rvwm R.C-----Dfwm
169345 SAVE HYD 1.0 01: SN,NI 55579.19 147.276 No.date 37:15 39.63 n/a .000
169355 fnam: SN,NI 0100
169365 remark:Total Flow at Rideau River
169375 *****
169385 R1000: CO0002 -----Dfm n-1D NMD -----AREba-QPEAgcm-TpeakDtte:hh:mm-----Rvwm R.C-----Dfwm
169395 FIN SH
169405 #
169415 #
169425 #
169435 #
169445 #
169455 #
169465 #
169475 #
169485 #
169495 #
169505 #
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170005 #
170015 #
170025 #
170035 #
170045 #
170055 #
170065 #
170075 #
170085 #
170095 #
170105 #
170115 #
170125 #
170135 #
170145 #
170155 #
170165 #
170175 #

```

```

170185 R0025: CO0364 ROUTE PIPE ->
170195 *** WARNING: New pipe size used for routing.
170205 R0025: CO0372 ROUTE PIPE ->
170215 *** WARNING: New pipe size used for routing.
170225 R0025: CO0380 DI VERT HYD ->
170235 *** NOTE: Inflow hyd. is dry and cannot be diverted.
170245 R0025: CO0385 ROUTE PIPE ->
170255 *** WARNING: New pipe size used for routing.
170265 R0025: CO0400 ROUTE PIPE ->
170275 *** WARNING: New pipe size used for routing.
170285 R0025: CO0407 ROUTE PIPE ->
170295 *** WARNING: New pipe size used for routing.
170305 R0025: CO0408 ROUTE PIPE ->
170315 *** WARNING: New pipe size used for routing.
170325 R0025: CO0416 ROUTE PIPE ->
170335 *** WARNING: New pipe size used for routing.
170345 R0025: CO0417 ROUTE PIPE ->
170355 *** WARNING: New pipe size used for routing.
170365 R0025: CO0431 ROUTE PIPE ->
170375 *** WARNING: New pipe size used for routing.
170385 R0025: CO0447 ROUTE PIPE ->
170395 *** WARNING: New pipe size used for routing.
170405 R0025: CO0363 ROUTE PIPE ->
170415 *** WARNING: New pipe size used for routing.
170425 R0025: CO0364 ROUTE PIPE ->
170435 *** WARNING: New pipe size used for routing.
170445 R0025: CO0372 ROUTE PIPE ->
170455 *** WARNING: New pipe size used for routing.
170465 R0025: CO0380 DI VERT HYD ->
170475 *** NOTE: Inflow hyd. is dry and cannot be diverted.
170485 R0025: CO0385 ROUTE PIPE ->
170495 *** WARNING: New pipe size used for routing.
170505 R0025: CO0400 ROUTE PIPE ->
170515 *** WARNING: New pipe size used for routing.
170525 R0025: CO0407 ROUTE PIPE ->
170535 *** WARNING: New pipe size used for routing.
170545 R0025: CO0408 ROUTE PIPE ->
170555 *** WARNING: New pipe size used for routing.
170565 R0025: CO0416 ROUTE PIPE ->
170575 *** WARNING: New pipe size used for routing.
170585 R0025: CO0417 ROUTE PIPE ->
170595 *** WARNING: New pipe size used for routing.
170605 R1000: CO0341 ROUTE PIPE ->
170615 *** WARNING: New pipe size used for routing.
170625 R1000: CO0347 ROUTE PIPE ->
170635 *** WARNING: New pipe size used for routing.
170645 R0025: CO0363 ROUTE PIPE ->
170655 *** WARNING: New pipe size used for routing.
170665 R1000: CO0364 ROUTE PIPE ->
170675 *** WARNING: New pipe size used for routing.
170685 R1000: CO0372 ROUTE PIPE ->
170695 *** WARNING: New pipe size used for routing.
170705 R1000: CO0380 DI VERT HYD ->
170715 *** NOTE: Inflow hyd. is dry and cannot be diverted.
170725 R1000: CO0385 ROUTE PIPE ->
170735 *** WARNING: New pipe size used for routing.
170745 R1000: CO0400 ROUTE PIPE ->
170755 *** WARNING: New pipe size used for routing.
170765 R1000: CO0407 ROUTE PIPE ->
170775 *** WARNING: New pipe size used for routing.
170785 R1000: CO0408 ROUTE PIPE ->
170795 *** WARNING: New pipe size used for routing.
170805 R1000: CO0416 ROUTE PIPE ->
170815 *** WARNING: New pipe size used for routing.
170825 R1000: CO0417 ROUTE PIPE ->
170835 *** WARNING: New pipe size used for routing.
170845 Simulation ended on 2021-03-04 at 12:01:23
170855 #
170865 #
170875 #

```

Attachment F

Updated Subcatchment Schematics & Tables



- Legend**
- Channel Cross Sections
 - S-1 Sub-catchments and Fraser Sub-catchments
 - S-1 Sub-catchments
 - FRASER-DRN
 - FRASER-D
 - Google Hybrid

File name: Figure 4A - S-1 & Fraser Clarke Sub-catchments.pdf

XS 3633 Cross Section at station 3633

S-1-A	▼ Area ID
90.84 ha	► Area (ha)
Ref. 1	► Reference Number

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PROJECT :
 BCDC - Quantity Control Study

TITLE :
 Figure 4A - S-1 & Fraser Clarke Sub-catchments
 Table 4A - S-1 & Fraser Clarke Sub-catchments

PROJECT NO. 1474-16

DRAWN: MM

DATE: Mar. 2021

Station	Channel	Area (ha)	Reference	Notes
3633	S-1-A	90.84	Ref. 1	
3634	S-1-D1	21.67	Ref. 3	
3635	S-1-D2	18.67	Ref. 4	
3636	S-1-D3	6.79	Ref. 5	
3637	S-1-D4	3.28	Ref. 6	
3638	S-1-D5	12.84	Ref. 7	
3639	S-1-D6	1.75	Ref. 8	
3640	S-1-D7	2.03	Ref. 9	
3641	S-1-D8	5.27	Ref. 10	
3642	S-1-F0-D1	5.11	Ref. 11	
3643	S-1-F0-D2	4.94	Ref. 12	
3644	S-1-F0-F-D	14.96	Ref. 13	
3645	FRASER-D	21.61	Ref. 16	
3646	FRASER-DRN	13.65	Ref. 15	
3647	S-1-Okeefe	44.93	Ref. 14	





- Legend**
- Channel Cross Sections
 - S-1 Sub-catchments and Fraser Sub-catchments
 - S-1 Sub-catchments
 - FRASER-DRN
 - FRASER-D
 - Google Hybrid

File name:
Figure 4B - S-1 & Fraser Clarke Sub-catchments.pdf

XS 3633 Cross Section at station 3633

S-1-A	▼ Area ID
90.84 ha	► Area (ha)
Ref. 1	► Reference Number

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DSEL
david schaeffer engineering ltd

PROJECT :
BCDC - Quantity Control Study

TITLE :
Figure 4B - S-1 & Fraser Clarke Sub-catchments
Table 4B - S-1 & Fraser Clarke Sub-catchments

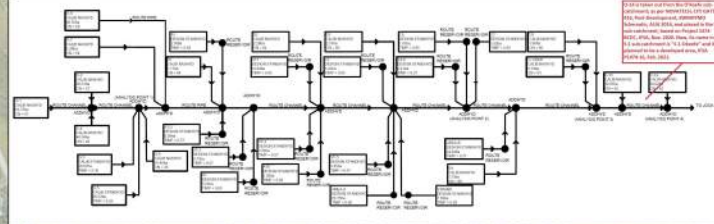
PROJECT NO. 1474-16

DRAWN: MM

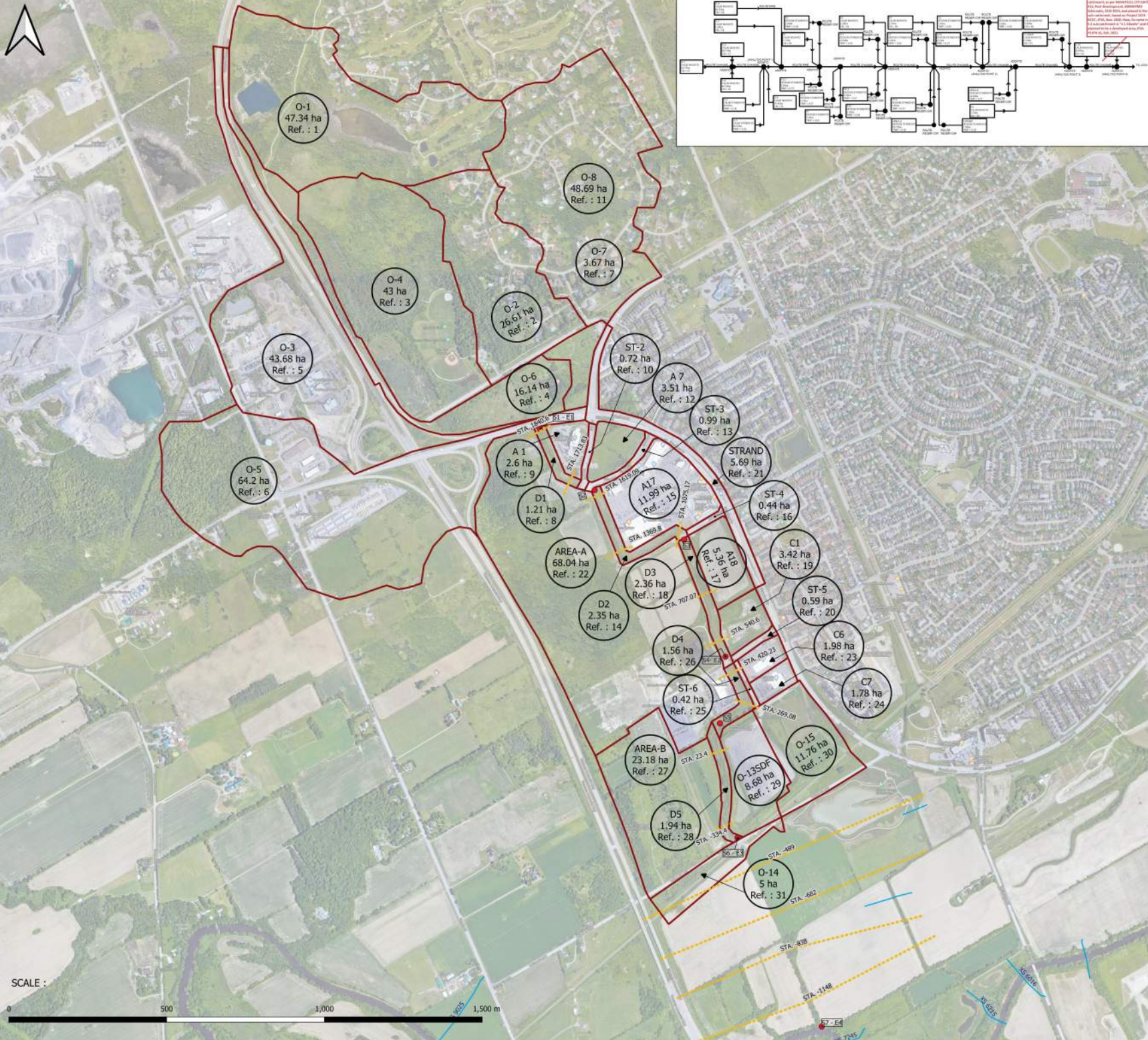
DATE: Mar. 2021

Station	Channel	Area (ha)	Ref.	Notes
3633	S-1-A	90.84	1	
3633	S-1-B	55.36	2	
3633	S-1-D1	21.67	3	
3633	S-1-D2	18.67	4	
3633	S-1-D3	6.79	5	
3633	S-1-D4	3.28	6	
3633	S-1-D5	12.84	7	
3633	S-1-D6	1.75	8	
3633	S-1-D7	2.03	9	
3633	S-1-D8	5.27	10	
3633	S-1-FO-D1	5.11	11	
3633	S-1-FO-D2	4.94	12	
3633	S-1-FO-F-D	14.96	13	
3633	S-1-Okeefe	44.93	14	
3633	FRASER-D	21.61	16	
3633	FRASER-DRN	13.65	15	





Station	Area (ha)	Reference	Notes
O-1	47.34	1	
O-2	26.61	2	
O-3	43.68	5	
O-4	43	3	
O-5	64.2	6	
O-6	16.14	4	
O-7	3.67	7	
O-8	48.69	11	
O-14	5	31	
O-15	11.76	30	
O-13SDP	8.68	29	
A1	2.6	9	
A7	3.51	12	
A17	11.99	15	
A18	5.36	17	
A19	5.36	17	
STRAND	5.69	21	
AREA-A	68.04	22	
AREA-B	23.18	27	
D1	1.21	8	
D2	2.35	14	
D3	2.36	18	
D4	1.56	26	
D5	1.94	28	
ST-1	0.72	10	
ST-2	0.72	10	
ST-3	0.99	13	
ST-4	0.44	16	
ST-5	0.59	20	
ST-6	0.42	25	
C1	3.42	19	
C6	1.98	23	
C7	1.78	24	

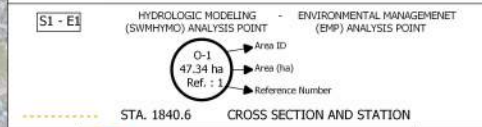


File name:

Figure F1 - O'Keefe Sub-catchments.pdf

Legend

- 20210129-O'Keefe Sub-catchment Boundaries
- O'Keefe Sub-catchment Boundaries
- Google Hybrid
- XS 7245 Cross Section at station 7245



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PROJECT :
 BCDC - Quantity Control Study

TITLE :
 Figure F1 - O'Keefe Sub-catchments
 Table F1 - O'Keefe Sub-catchments
 Schematic F1 - O'Keefe Sub-catchments

PROJECT NO.	1474
DRAWN:	MM
DATE:	Mar. 2021



Ref.	Water ID	Area (ha)	Major System In	Minor System To	I. Imperv.	KIMP	C.N	ICD Length (m) (H2O1) (Area*50000/1)	Slope (%)		NAVDic	NAVDout	RESERVE RESERVOIR				RELEASE CHANNEL (Station (m))				
									S2PW (Paradise)	S1PW (Inapprox)			Outflow (m/s)	Storage (ha-m)	NAVDic	NAVDout	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)	
1	FOSTER	325.44	FOSTER OUT ~ ("F_OST"~"FIO-DIV")		0.55	0.05	74	347.794211	0.5	0.5	FOSTER	F_FOS	FO-OVT	18.34	10	SN_FO (Total Flow at Foster Drain)	N_C8	359	0.0818	445.23	93.5
																			392.2	93.2	
																			-91	91.5	
																			-85.52	91.5	
																			12.48	89.4	
																			-9.79	89.11	
																			-3.22	88.24	
																			1.22	85.07	
																			10.96	82.79	
																			16.44	86.49	
																			35.55	89.45	
																			25.93	90.27	
																			35.76	90.47	
																			34.07	91	
																			188.08	91	
																			189.42	90.5	
																			112.04	90.3	
																			134.42	91	
																			116.78	93.3	



File name: Figure F2 - Foster Sub-catchment.pdf

- Legend**
- Channel Cross Sections
 - SWMF Drains
 - Foster Drain
 - SWMF ponds
 - Foster Pond
 - Foster Sub-catchment
 - FOSTER
 - Google Hybrid

XS 6016 Cross Section at station 6016

FOSTER 325.44 ha Area (ha)
Ref. 1 Reference Number

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DSEL
david schaeffer engineering ltd

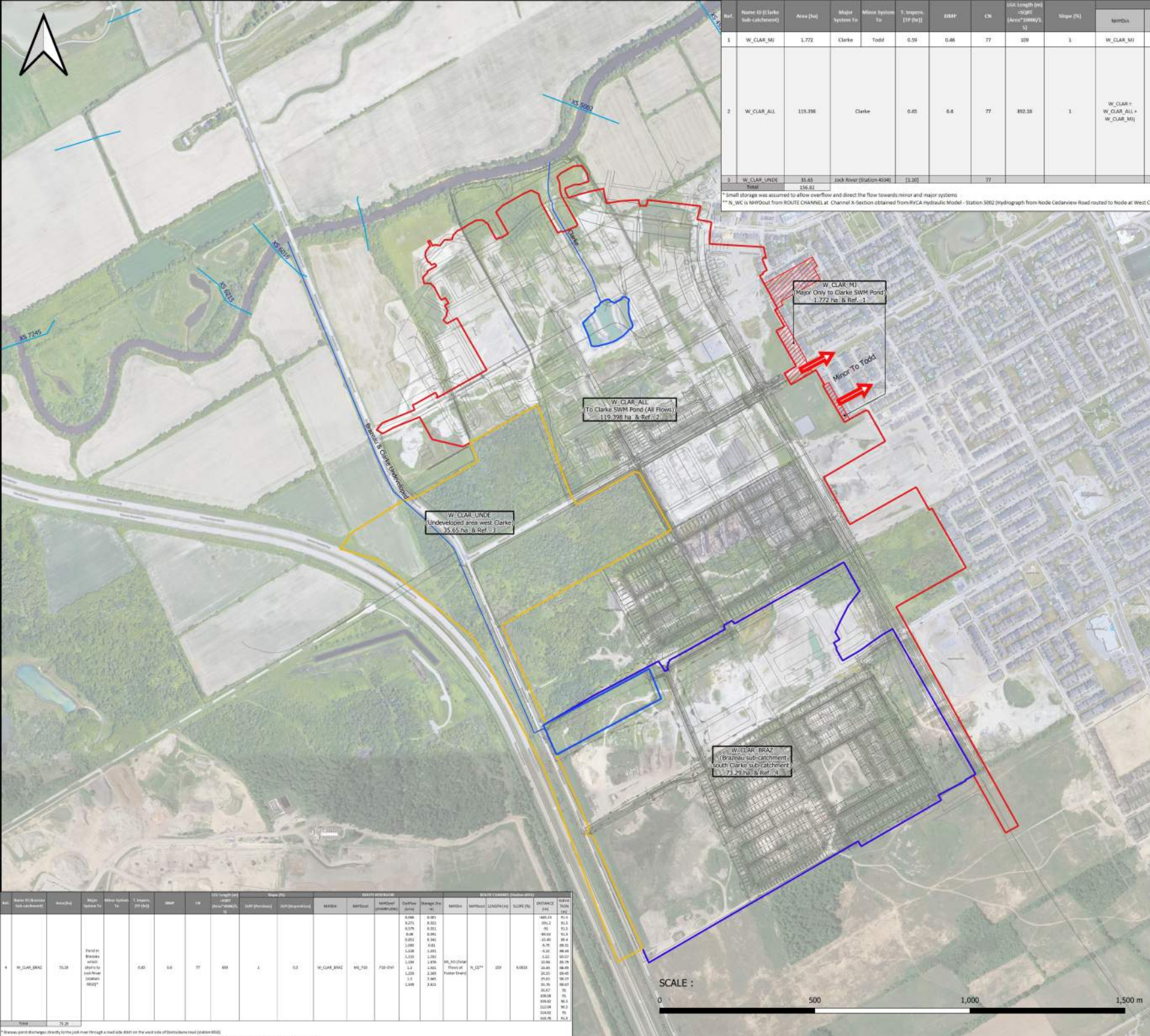
PROJECT : BCDC - Quantity Control Study

TITLE : Figure F2 - Foster Sub-catchment
Table F2 - Foster Sub-catchment

PROJECT NO.	1474-16
DRAWN:	MM
DATE:	Mar. 2021



Ref.	Name ID	Area (ha)	Major System To	Minor System To	T. Imperv.	XIMP	CN	LGI: Length (m) =SQRT (Area*10000/1.5)	Slope (%)		ROUTE RESERVOIR					ROUTE CHANNEL (Station 6016)					
									SLPP (Pervious)	SLPI (Impervious)	NHYDin	NHYDout	NHYDovf (OVERFLOW)	Outflow (cms)	Storage (ha-m)	NHYDin	NHYDout	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)
1	FOSTER	325.44	FOSTER-OUT = ["P_FOS"+"FO-OVF"]		0.55	0.55	74	1472.956211	0.5	0.5	FOSTER	P_FOS	FO-OVF	10.34	10	SN_FO (Total Flows at Foster Drain)	N_CE	159	0.0818	-645.23	91.5
																				-391.2	91.5
																				-91	91.5
																				-85.52	91.5
																				-15.46	89.4
																				-9.79	89.31
																				-3.22	86.24
																				3.22	85.07
																				10.96	85.79
																				16.44	86.49
																				26.55	89.45
																				29.03	90.27
																				35.76	90.67
																				36.67	91
																				108.08	91
																				109.82	90.5
																				112.04	90.5
																				114.62	91
																				116.76	91.5



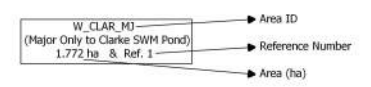
Ref.	Route ID (if applicable sub-catchment)	Area (ha)	Major System To	Minor System To	T. Imperv. FIP (%)	XIMP	CR	Slope (%)	ROUTE RESERVOIR			ROUTE CHANNEL (Station #348)																	
									W/In	W/Out	W/Overflow	W/In	W/Out	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)												
1	W_CLAR_MI	1,772	Clarke	Todd	0.50	0.80	77	109		W_CLAR_MI	W_CLAR_MI	W_CLAR_MI	0.213	0.0001*															
2	W_CLAR_ALL	119,398	Clarke	0.05	0.4	77	892.18	1	W_CLAR = W_CLAR_MI	MS_P2	P2-OVF	0.128	0.351																
												0.148	0.409																
												0.277	0.861																
												0.354	1.223																
												0.505	1.32																
												0.666	1.821																
												0.881	2.125																
												0.995	2.434																
												1.069	2.583																
												1.311	2.647																
												4.884	2.861																
												13.048	3.188																
23.745	3.523																												
36.476	3.871																												
45.919	4.217																												
61.652	4.539																												
3	W_CLAR_UNDE	35.65	Jock River (Station 4534)				77																						
		156.93																											

* Small storage was assumed to allow overflow and direct the flow towards minor and major systems
 ** N_WC is AFFDOUT from ROUTE CHANNEL at Channel X-Section obtained from RIVCA Hydraulic Model - Station 5062 (Hydrograph from Node Cedarview Road routed to Node at West Clarke Drain)

- Legend**
- Channel Cross Sections
 - SWMF Drains
 - Brazeau & Clarke Undeveloped
 - Clarke
 - SWMF ponds
 - West Clarke
 - Brazeau
 - Clarke Sub-catchment & Brazeau Sub-catchment
 - W_CLAR_MI
 - W_CLAR_MJ (Major Only to Clarke SWM Pond)
 - W_CLAR_ALL (Major Only to Clarke SWM Pond)
 - W_CLAR_BRAZ
 - W_CLAR_UNDE
 - Clarke-Brazeau-CAD
 - Google Hybrid

File name: Figure F3 - Clarke & Brazeau Sub-catchments.pdf

XS 4534 Cross Section at station 4534 Minor System



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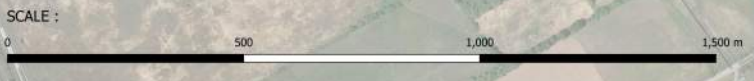


PROJECT : BCDC - Quantity Control Study

TITLE : Figure F3 - Clarke & Brazeau Sub-catchments
 Table F3-1 - Clarke Sub-catchments
 Figure F3-2 - Brazeau Sub-catchment

PROJECT NO. 1474-16
 DRAWN: MM
 DATE: Mar. 2021

Ref.	Route ID (if applicable sub-catchment)	Area (ha)	Major System To	Minor System To	T. Imperv. FIP (%)	XIMP	CR	Slope (%)	ROUTE RESERVOIR			ROUTE CHANNEL (Station #348)																	
									W/In	W/Out	W/Overflow	W/In	W/Out	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)												
4	W_CLAR_BRAZ	73.29	Clarke	Jock River (Station 4534)	0.65	0.8	77	89		W_CLAR_BRAZ	MS_P2	P2-OVF	0.213	0.0001*															
													0.066	0.309															
													0.271	0.583															
													0.576	0.963															
													0.88	0.994															
													0.891	0.941															
													1.266	0.81															
													1.538	1.243															
													1.533	1.587															
													1.134	1.476															
													1.1	1.851															
													1.293	1.269															
													1.1	1.868															
1.388	2.833																												



* Small storage was assumed to allow overflow and direct the flow towards minor and major systems

Ref.	Name ID (Clarke Sub-catchment)	Area (ha)	Major System To	Minor System To	T. Imperv. [TP (hr)]	XIMP	CN	LGI: Length (m) =SQRT (Area*10000/1.5)	Slope (%)	ROUTE RESERVOIR					ROUTE CHANNEL (Station 4534)							
										NHYDin	NHYDout	NHYDovf (OVERFLOW)	Outflow (cms)	Storage (ha-m)	NHYDin	NHYDout	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)		
1	W_CLAR_MJ	1.772	Clarke	Todd	0.59	0.46	77	109	1	W_CLAR_MJ	W_CLAR_MJn	W_CLAR_MJj	0.213	0.0001*								
2	W_CLAR_ALL	119.398	Clarke		0.65	0.6	77	892.18	1	W_CLAR = W_CLAR_ALL + W_CLAR_MJj	MS_P2	P2-OVF	0.128	0.161								
													0.138	0.409								
													0.148	0.68								
													0.227	0.931								
													0.354	1.223								
													0.505	1.52								
													0.666	1.821								
													0.831	2.123								
													0.995	2.434								
													1.069	2.583	N_WC**	N_KB	1020	0.0498				
													1.51	2.647								
													4.904	2.861								
													13.048	3.188								
													23.745	3.523								
36.474	3.871																					
45.938	4.127																					
61.652	4.539																					
3	W_CLAR_UNDE	35.65	Jock River (Station		[1.10]		77															
Total		156.82																				

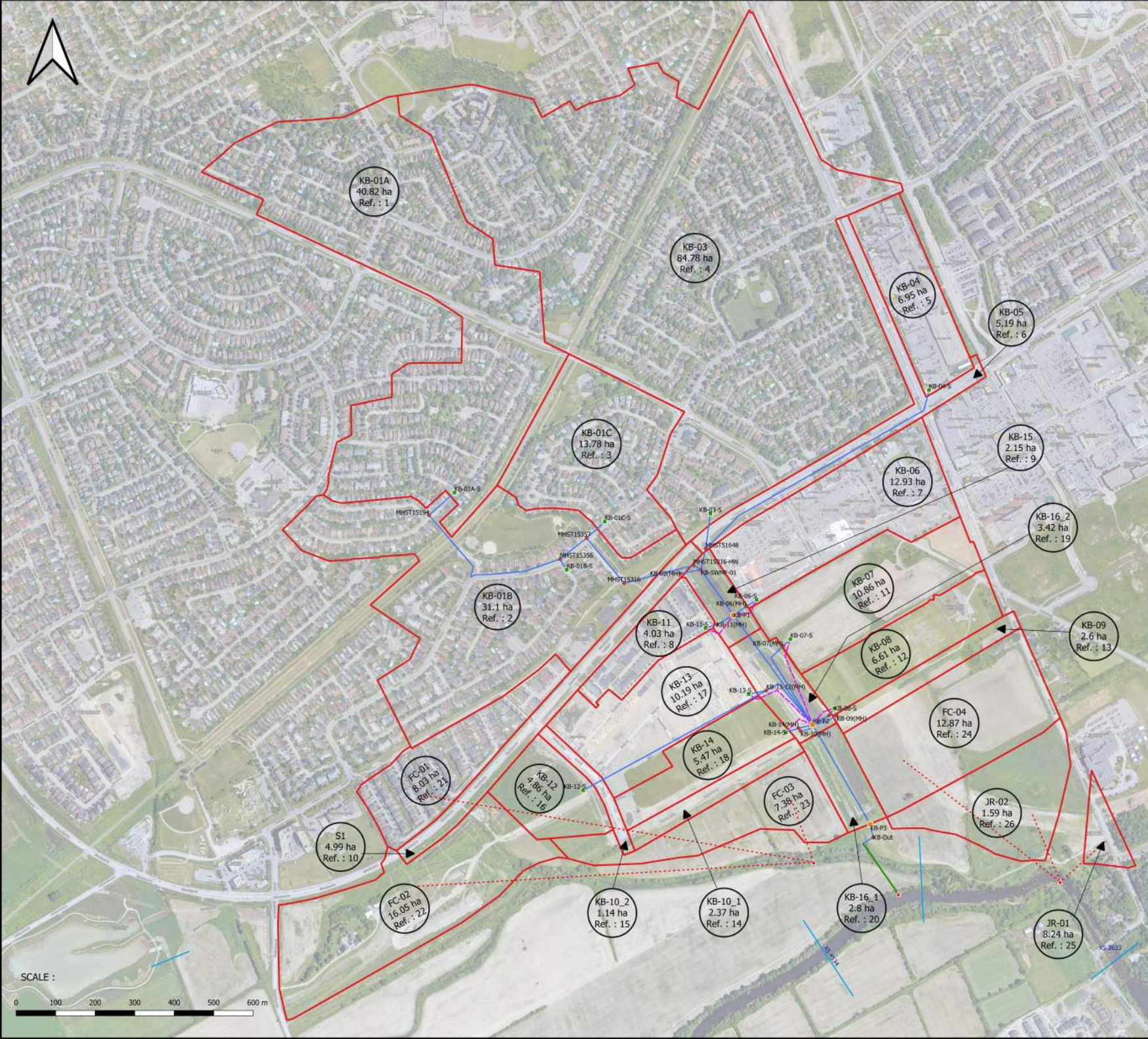
* Small storage was assumed to allow overflow and direct the flow towards minor and major systems

** N_WC is NHYDout from ROUTE CHANNEL at Channel X-Section obtained from RVCA Hydraulic Model - Station 5002 (Hydrograph from Node Cedarview Road routed to Node at West Clarke Drain)

Ref.	ID (Brazeau Sub-catchment)	Area (ha)	Major System To	Minor System To	T. Imperv. [TP (hr)]	XIMP	CN	LGI: Length (m) =SQRT (Area*10000/1.5)	Slope (%)		ROUTE RESERVOIR					ROUTE CHANNEL (Station 6016)					
									SLPP (Pervious)	SLPI (Impervious)	NHYDin	NHYDout	NHYDovf (OVERFLOW)	Outflow (cms)	Storage (ha-m)	NHYDin	NHYDout	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)
4	W_CLAR_BRAZ	73.29	Pond in Brazeau which drains to Jock River (station 6016)*		0.65	0.6	77	699	1	0.5	W_CLAR_BRAZ	MS_P10	P10-OVF	0.068	0.001	SN_FO (Total Flows at Foster Drain)	N_CE**	159	0.0818	-645.23	91.5
														0.271	0.022					-391.2	91.5
														0.379	0.051					-91	91.5
														0.48	0.091					-85.52	91.5
														0.853	0.341					-15.46	89.4
														1.005	0.61					-9.79	89.31
														1.128	1.231					-3.22	86.24
														1.155	1.592					3.22	85.07
														1.194	1.876					10.96	85.79
														1.2	1.921					16.44	86.49
														1.259	2.369					26.55	89.45
														1.3	2.665					29.03	90.27
														1.349	2.813					35.76	90.67
																				36.67	91
																				108.08	91
																				109.82	90.5
		112.04	90.5																		
		114.62	91																		
		116.76	91.5																		
Total		73.29																			

* Brazeau pond discharges directly to the jock river through a road side ditch on the west side of Borrissokane road (station 6016)

** N_CE is NHYDout from ROUTE CHANNEL at Channel X-Section obtained from RVCA Hydraulic Model - Station 6016 (Hydrograph from Node Foster routed to Node at Cedarview Road)



Area ID	Area (ha)	Reference Number
KB-01A	40.82	1
KB-03	84.78	4
KB-04	6.95	5
KB-05	5.19	6
KB-06	12.93	7
KB-07	10.86	11
KB-08	6.61	12
KB-09	2.6	13
KB-10_1	2.37	14
KB-10_2	1.14	15
KB-11	4.03	8
KB-12	4.86	16
KB-13	10.19	17
KB-14	5.47	18
KB-15	2.15	9
KB-16_1	2.8	20
KB-16_2	3.42	19
KB-17	10.19	17
KB-18	5.47	18
KB-19	3.42	19
KB-20	2.8	20
KB-21	8.03	21
KB-22	16.05	22
KB-23	7.36	23
KB-24	12.87	24
KB-25	8.24	25
KB-26	1.59	26

Legend

- Ken-BU storage
- Ken-BU MH
- Ken-BU Pond
- ▲ Ken-BU Outfalls
- Ken-BU Pipe
- Ken-BU Major System
- Ken-BU Channel
- Ken-BU to FC (Fraser Clarke) and JR (Jock River)
- Kennedy Burnett Sub-catchment
- Kennedy Burnett (Ken-BU)
- Google Hybrid

File name: Figure F4 - Kennedy Burnett Sub-catchments.pdf



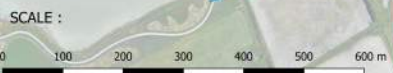
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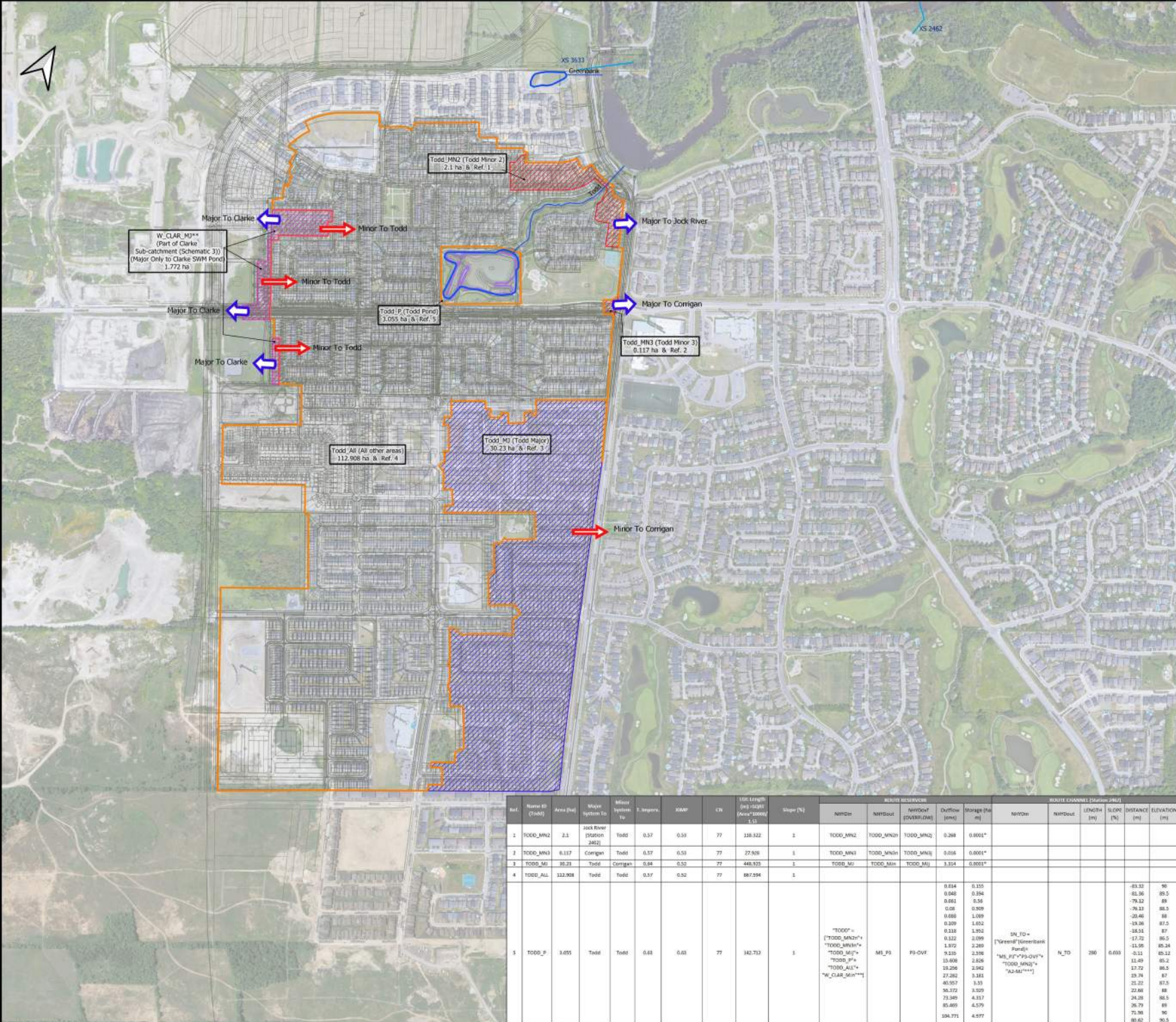


PROJECT :
BCDC - Quantity Control Study

TITLE :
Figure F4 - Kennedy Burnett Sub-catchments
Table F4 - Kennedy Burnett Sub-catchments

PROJECT NO.	1474
DRAWN:	MM
DATE:	Mar. 2021





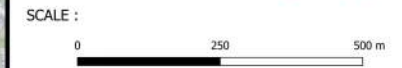
- Legend**
- Channel Cross Sections
 - SWMF Drains
 - SWMF ponds
 - Sub-catchments
 - Todd
 - Todd Minor
 - Todd Major
 - Todd Pond Boundary
 - W_CLAR_Major
 - Todd-Greenbank-CAD
 - Google Hybrid

File name: Figure F5 -Todd Sub-catchments.pdf



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DSEF
 david schaeffer engineering ltd



PROJECT : BCDC - Quantity Control Study

TITLE : Figure F5 -Todd Sub-catchments
 Table F5 -Todd Sub-catchments

PROJECT NO. 1474-16

DRAWN: MM

DATE: Mar. 2021

Ref.	Name ID (Code)	Area (ha)	Major System To	Minor System To	T. Storage	XMP	CN	MFC Length (m) @1% (Area*10000 L/S)	Slope (%)	ROUTER RESERVOIR			ROUTE CHANNEL (Schematic CAD)						
										NRFDIn	NRFDout	NRFDin	NRFDout	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)		
1	TODD_MN2	2.1	Jack River (Station 2462)	Todd	0.57	0.55	77	138.332	1	TODD_MN2	TODD_MN2	TODD_MN2	0.268	0.0501*					
2	TODD_MN3	0.117	Corrigan	Todd	0.57	0.53	77	27.928	1	TODD_MN3	TODD_MN3	TODD_MN3	0.058	0.0501*					
3	TODD_Min	30.23	Todd	Corrigan	0.64	0.52	77	448.925	1	TODD_Min	TODD_Min	TODD_Min	3.314	0.0501*					
4	TODD_All	112.908	Todd	Todd	0.57	0.52	77	667.294	1										
5	TODD_P	3.055	Todd	Todd	0.68	0.63	77	142.713	1	ME_P3	P3-OVF	0.014	0.135						
												0.045	0.384						
												0.061	0.56						
												0.08	0.909						
												0.088	1.089						
												0.109	1.652						
												0.138	1.952						
												0.132	2.089						
												1.872	2.269						
												5.135	2.398						
												13.408	2.636						
												18.296	2.882						
												27.282	3.181						
40.957	3.55																		
56.372	3.929																		
73.949	4.317																		
85.869	4.579																		
104.771	4.977																		
Total											148.41								

* Small storage was assumed to allow overflow and direct the flow towards minor and major systems
 ** "W_CLAR_Min" is the minor system from the major system: area/Area = 1.772 ha & TMP = 0.59 & XMP = 0.46 & CN = 75 & Slope = 1% & Outflow = 0.233 cm/in Clarke sub-catchment (Schematic 3) to Jack River (Station 2462)
 *** "AD_Min" is the major system from A2 area (Area = 25.3 ha & TMP = 0.52 & XMP = 0.42 & CN = 75 & Slope = 1% & Storage = 934 cu-m & Flow rate = 3.833 cms) in Corrigan sub-catchment (Schematic 1) to Todd sub-catchment

Ref.	Name ID (Todd)	Area (ha)	Major System To	Minor System To	T. Imperv.	XIMP	CN	LGI: Length (m) =SQRT (Area*10000/1.5)	Slope (%)	ROUTE RESERVOIR					ROUTE CHANNEL (Station 2462)					
										NHYDin	NHYDout	NHYDovf (OVERFLOW)	Outflow (cms)	Storage (ha-m)	NHYDin	NHYDout	LENGTH (m)	SLOPE (%)	DISTANCE (m)	ELEVATION (m)
1	TODD_MN2	2.1	Jock River (Station 2462)	Todd	0.57	0.53	77	118.322	1	TODD_MN2	TODD_MN2n	TODD_MN2j	0.268	0.0001*						
2	TODD_MN3	0.117	Corrigan	Todd	0.57	0.53	77	27.928	1	TODD_MN3	TODD_MN3n	TODD_MN3j	0.016	0.0001*						
3	TODD_MJ	30.23	Todd	Corrigan	0.64	0.52	77	448.925	1	TODD_MJ	TODD_MJn	TODD_MJj	3.314	0.0001*						
4	TODD_ALL	112.908	Todd	Todd	0.57	0.52	77	867.594	1											
5	TODD_P	3.055	Todd	Todd	0.63	0.63	77	142.712	1	"TODD" = ["TODD_MN2n"+ "TODD_MN3n"+ "TODD_MJj"+ "TODD_P"+ "TODD_ALL"+ "W_CLAR_MJn"***]	MS_P3	P3-OVF	0.014 0.048 0.061 0.08 0.088 0.109 0.118 0.122 1.972 9.135 15.608 19.256 27.282 40.957 56.372 73.349 85.469 104.771	0.155 0.394 0.56 0.909 1.089 1.652 1.952 2.099 2.269 2.598 2.826 2.942 3.181 3.55 3.929 4.317 4.579 4.977	SN_TO = ["GreenB" (Greenbank Pond)+ "MS_P3"+"P3-OVF"+ "TODD_MN2j"+ "A2-MJ"***]	N_TO	280	0.033	-83.32 -81.36 -79.12 -76.13 -20.46 -19.36 -18.51 -17.72 -11.95 -0.11 11.49 17.72 19.74 21.22 22.68 24.28 26.79 71.98 80.62	90 89.5 89 88.5 88 87.5 87 86.5 85.24 85.12 85.2 86.5 87 87.5 88 88.5 89 90 90.5
Total		148.41																		

* Small storage was assumed to allow overflow and direct the flow towards minor and major systems

** "W_CLAR_MJn" is the minor system from the major system area(Area = 1.772 ha & TIMP = 0.59 & XIMP = 0.46 & CN = 75 & Slope = 1% & Outflow = 0.213 cms)in Clarke sub-catchment (Schematic 3) to Jock River (Station 2462)

*** "A2-MJ" is the major system from A2 area (Area = 25.5 ha & TIMP = 0.52 & XIMP = 0.42 & CN = 75 & Slope = 1% & Storage = 924 cu-m & Flow rate = 1.818 cms) in Corrigan sub-catchment (Schematic 1) to Todd sub-catchment



Area ID	Area (ha)	Reference Number	Corrigan-MH	Corrigan-Pipe Line	Corrigan-Drainage Boundaries	Channel Cross Section	Major System	Overflow
A1	15.75	1						
A2	25.5	6						
A3	1.27	5						
A4	1.6	7						
A5	1.56	8						
A6	0.96	13						
A7	2.2	12						
A8	4.14	18						
A9	6.27	19						
A10	12.29	20						
A11	4.34	19						
A12	2.94	22						
A13	2.59	21						
B1	2.77	4						
B2	12.31	9						
B3	5.59	10						
B4	7.6	11						
B5	7.19	14						
B6	3.29	15						
B7	32.25	16						
B8	15.87	2						
B9	12.47	3						
B10	15.75	1						



File name:
Figure F6 - Corrigan Sub-catchments.pdf

- Major System
 Overflow
- Legend**
- Channel Cross Section
 - Corrigan-Pipe Line
 - Corrigan-MH
 - Corrigan Drainage Boundaries
 - Corrigan Drainage Boundaries
- Area ID
 Area (ha)
 Reference Number
- XS 0 Cross Section at station 0

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PROJECT :
BCDC - Quantity Control Study

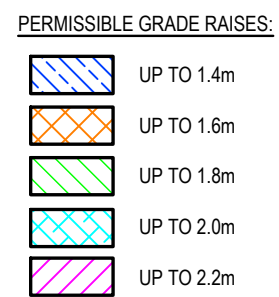
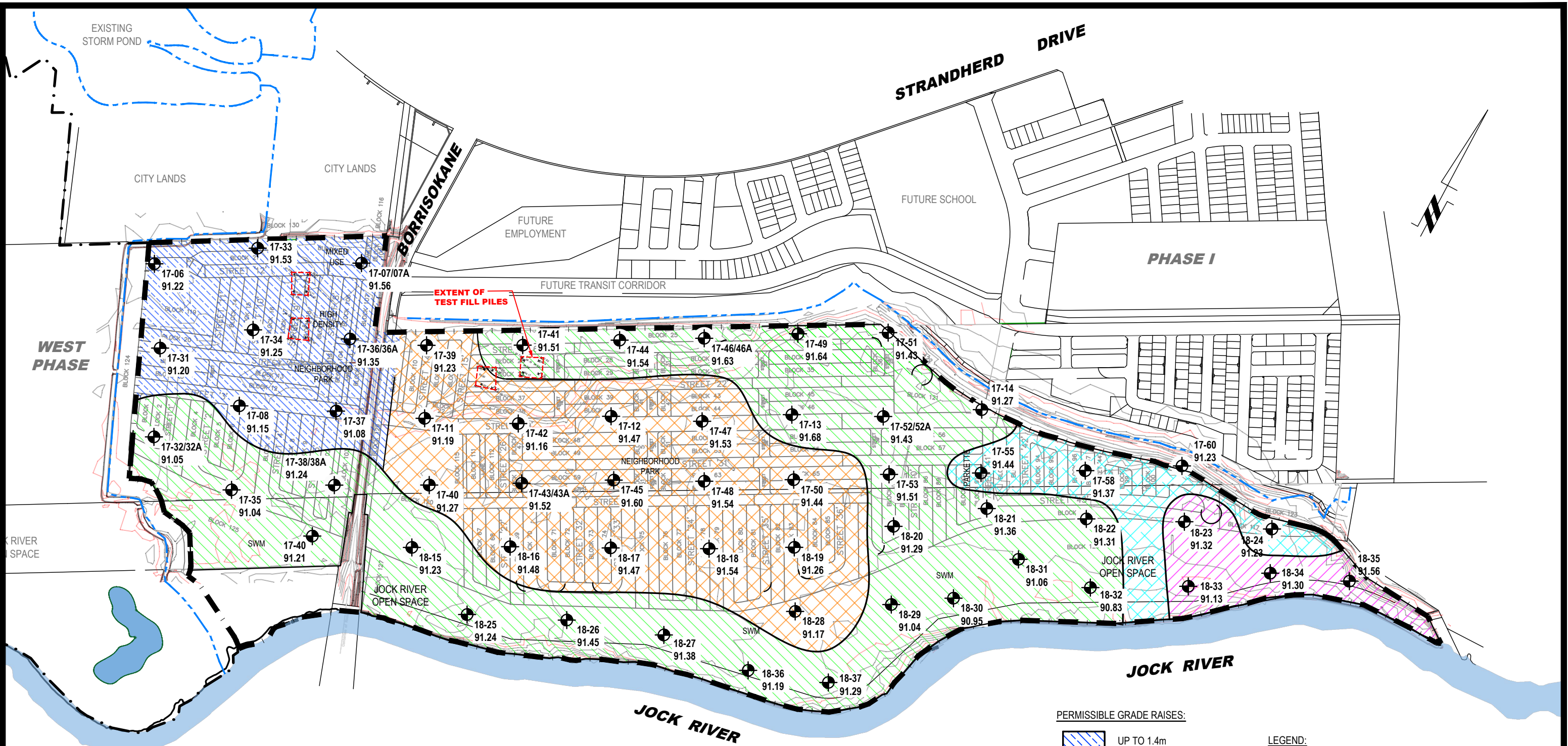
TITLE :
Figure F6 - Corrigan Sub-catchments
Table F6 - Corrigan Sub-catchments

PROJECT NO.	1474
DRAWN:	MM
DATE:	Mar. 2021



APPENDIX E

GEO TECHNICAL



LEGEND:

- ⊙ APPROXIMATE BOREHOLE LOCATION (GOLDER ASSOCIATES, 04/2019)
- 91.56 GROUND SURFACE ELEVATION (m)

BOREHOLE LOCATIONS WERE SURVEYED BY OTHERS AND ARE REFERENCED TO A GEODETIC DATUM.

patersongroup
consulting engineers

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Tel: (613) 226-7381 Fax: (613) 226-6344

NO.	REVISIONS	DATE	INITIAL
2	REVISED CONCEPTUAL PLAN, UPDATED GRADE RAISE RESTRICTIONS	04/02/2021	OC
1	REVISED CONCEPTUAL PLAN, ADDED TEST FILL PILE INFO AND UPDATED GRADE RAISE RESTRICTIONS	14/05/2020	DJG

CAIVAN COMMUNITIES
GEOTECHNICAL INVESTIGATION
PROP. RESIDENTIAL DEVELOPMENT - CONSERVANCY LANDS EAST
OTTAWA, ONTARIO

Title: **PERMISSIBLE GRADE RAISE PLAN**

Scale:	1:6000	Date:	09/2019
Drawn by:	MPG	Report No.:	PG5036-1
Checked by:	OC	PG5036-2	Revision No.: 2
Approved by:	DJG		

re: **Road Grade Exceedance Review**
Proposed Residential Development - Conservancy Lands
Borrisokane Road - Ottawa

to: Caivan Communities - **Mr. Hugo Lalonde** - hugo.lalonde@caivan.com
David Schaeffer Engineering Ltd. - **Mr. Kevin Murphy** - KMurphy@dsel.ca

date: March 8, 2021

file: PG5036-MEMO.10

Paterson Group (Paterson) prepared the following memo to provide a geotechnical review of permissible grade raise exceedances of the proposed roadway grading at various locations throughout the aforementioned development. This memorandum should be read in conjunction with Paterson Group Report PG5036-1 Revision 1 dated February 3, 2021.

The following drawings prepared by David Schaeffer Engineering Ltd. were reviewed from a geotechnical perspective:

- Barrhaven Conservancy - Maximum Grade Raise Exceedance - Project No. 16-891 - Drawing No. 6 and 7 - dated March 2021
- Latest road grading AutoCAD file - 891_Grad_PS_Lowered_Mar5-21

Based on the available drawings, it is understood that minor permissible grade raise exceedances occur within the proposed roadway grades at various locations throughout the subject development.

Geotechnical Review

Based on our detailed review, the grading exceedances are considered acceptable from a geotechnical perspective and lightweight fill will not be required within the City of Ottawa right-of-way(s).

We trust that this information satisfies your immediate requirements.

Paterson Group Inc.



Owen Canton, E.I.T.



David J. Gilbert, P.Eng.

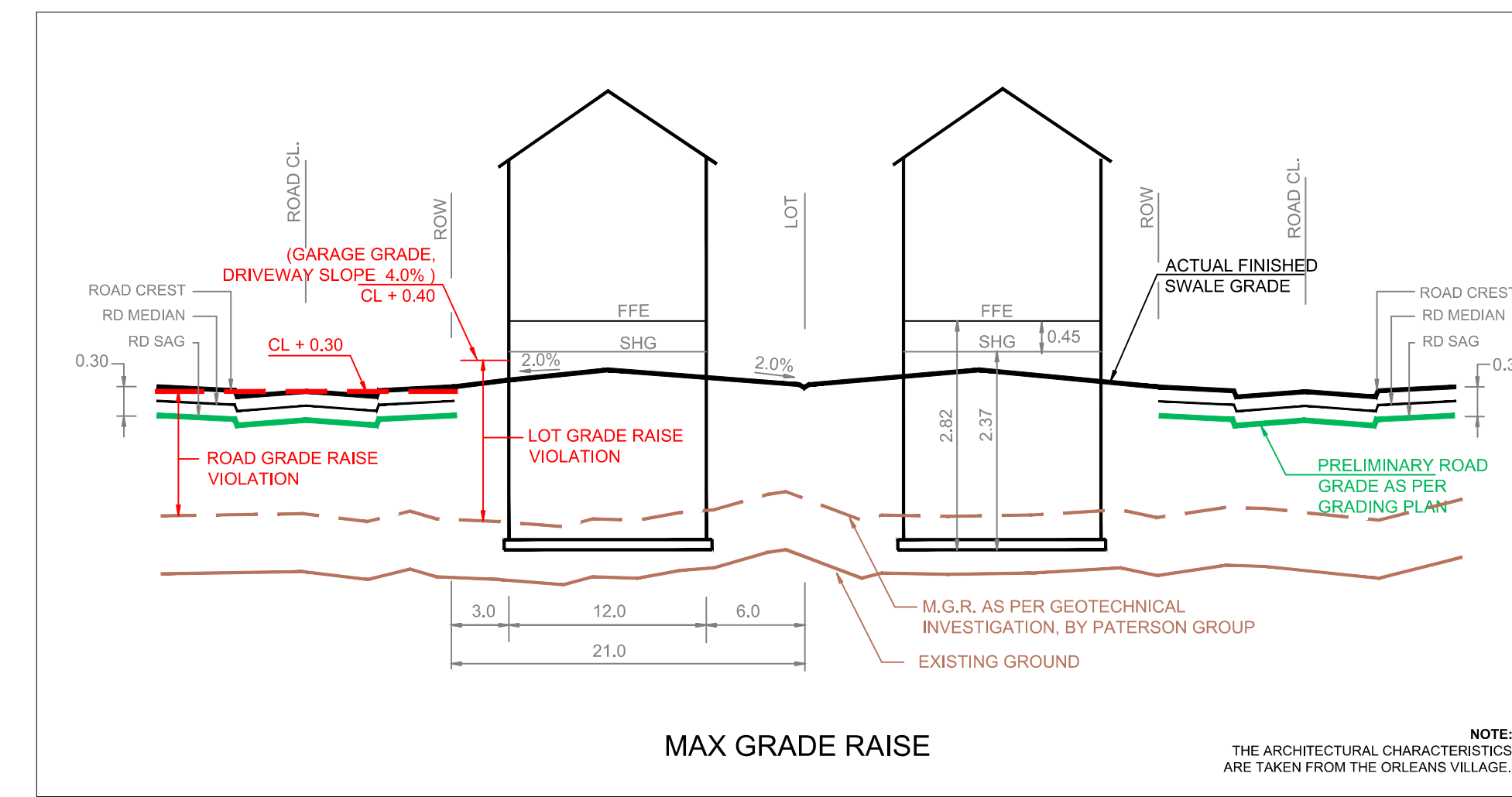
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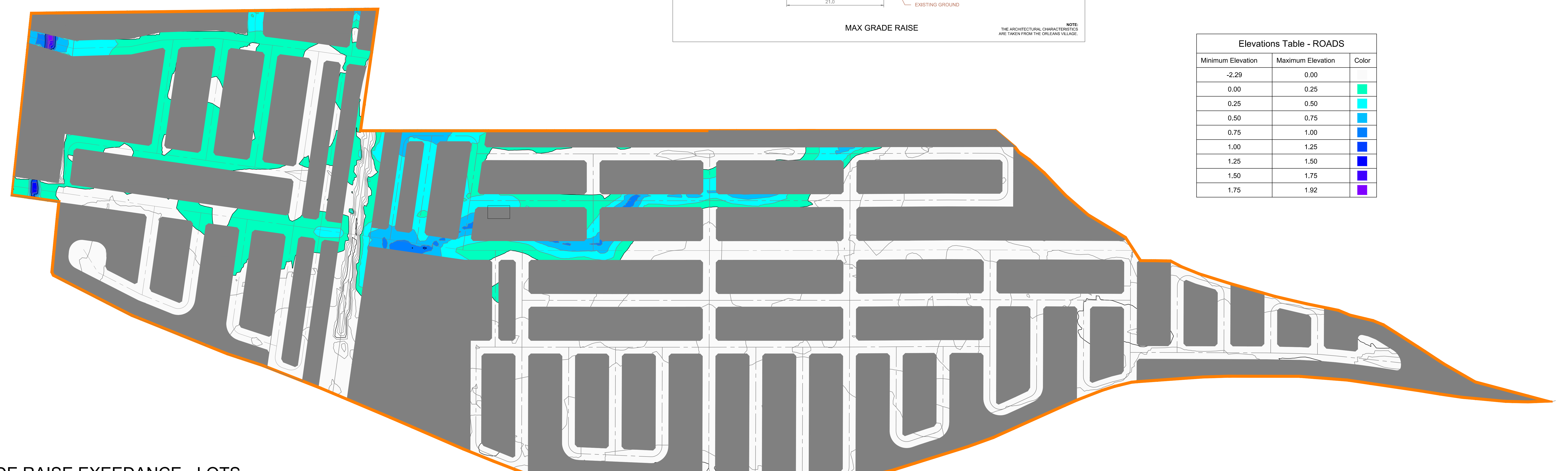
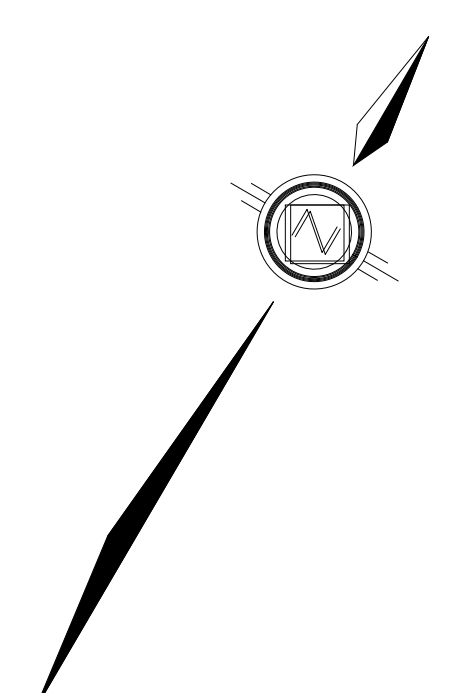
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Kingston - Ontario - K7L 1H3
Tel: (613) 542-7381

MAXIMUM GRADE RAISE EXCEEDANCE - ROADS

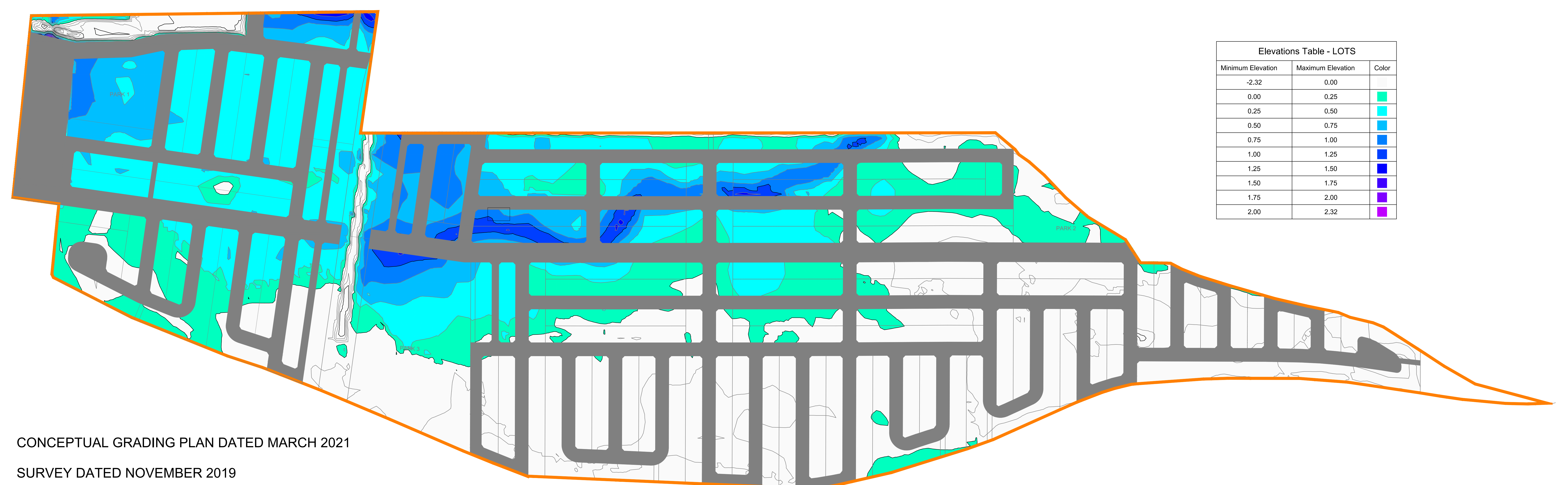


NOTES:
 1. LOW FLOW CHANNEL ELEVATION TO BE VERIFIED IN THE FIELD AT ALL ROAD AND SEWER CROSSING LOCATIONS.
 2. DETAILED DESIGN ROAD GRADES REPRESENT LOW POINTS. ACTUAL DESIGN GRADES WILL RISE AND FALL BY APPROXIMATELY 0.3m ABOVE THE TROUGH/SAG GRADES PRESENTED ON THIS PLAN.
 3. EARTHWORKS VOLUMES ARE BASED ON THE MEDIAN ROAD GRADES, WHICH ARE ESTIMATED TO BE 0.09m HIGHER THAN THE TROUGH/SAG GRADES PRESENTED ON THIS PLAN.
 EARTHWORKS DEPTHS AND VOLUMES ARE APPROXIMATE BASED ON USING ASSUMED MEDIAN VALUES FOR THE MANY VARIABLES THAT AFFECT EARTHWORKS. WHILE THE MEDIAN DEPTH AND VOLUME ARE GENERALLY REFLECTIVE OF THE SITE CHARACTERISTICS, THE ACTUAL DEPTH AND VOLUME AT ANY PRECISE LOCATION WILL VARY (UP OR DOWN) BASED ON THE LOCATION OF HIGH POINTS AND LOW POINTS IN THE ROAD AND ON THE LOTS.
 THE SITE GRADING PLAN HAS BEEN PREPARED IN GENERAL CONFORMANCE WITH CITY OF OTTAWA DESIGN CRITERIA AND HISTORIC PRACTICES. THE GRADING PLAN HAS NOT BEEN REVIEWED BY CITY OF OTTAWA AND IS SUBJECT TO CHANGE FOLLOWING CITY REVIEW. ANY CHANGE IN THE GRADING PLAN WILL HAVE A CORRESPONDING CHANGE IN EARTHWORKS.



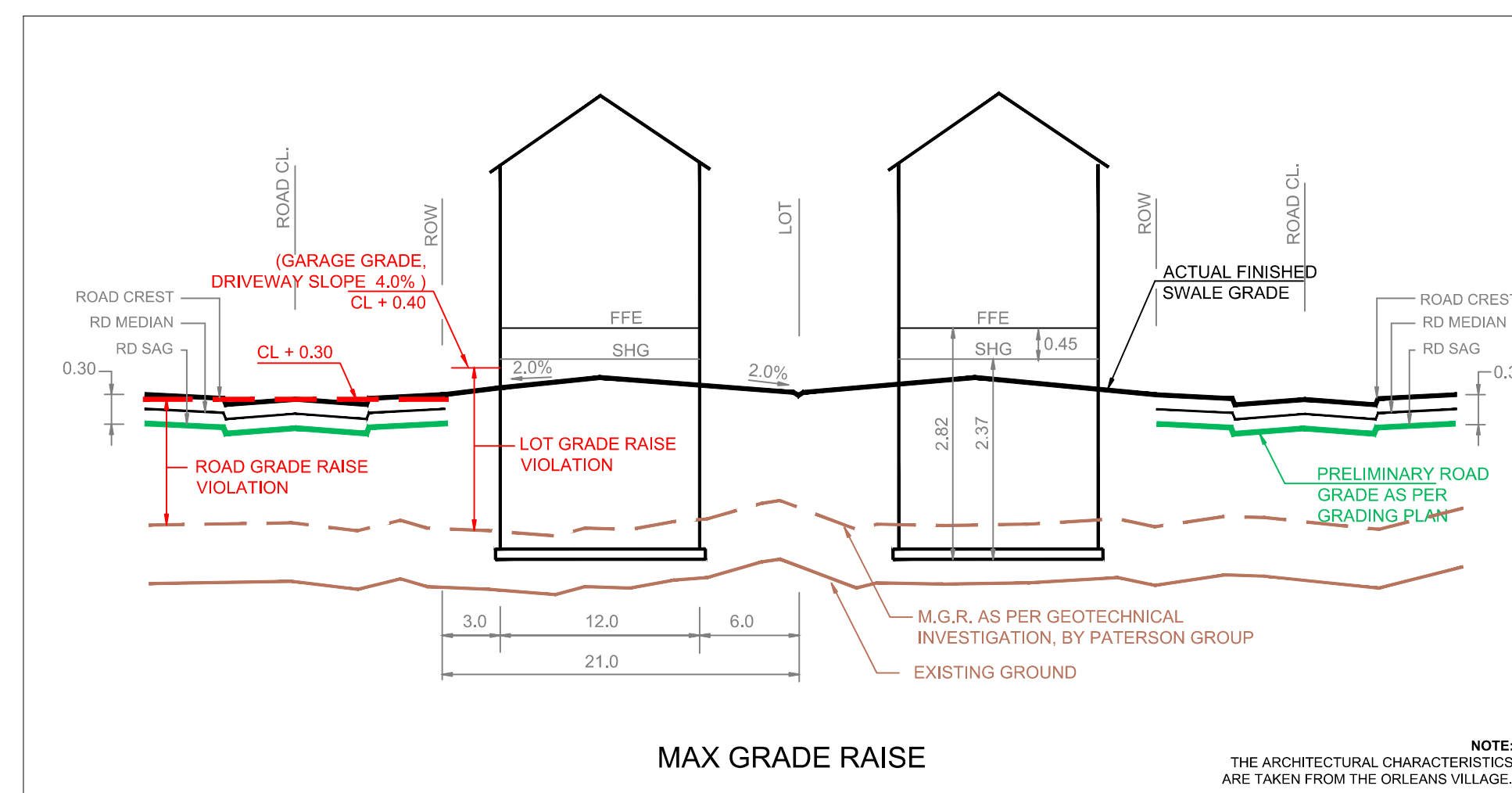
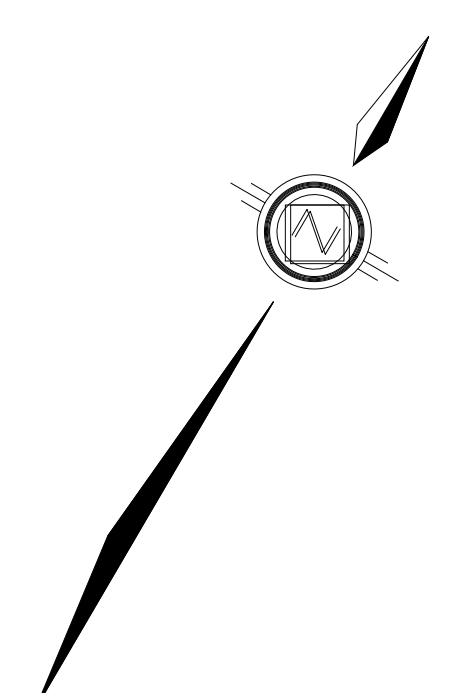
Minimum Elevation	Maximum Elevation	Color
-2.29	0.00	
0.00	0.25	Light Green
0.25	0.50	Light Blue
0.50	0.75	Medium Blue
0.75	1.00	Dark Blue
1.00	1.25	Blue
1.25	1.50	Dark Blue
1.50	1.75	Purple
1.75	1.92	Dark Purple

MAXIMUM GRADE RAISE EXCEEDANCE - LOTS

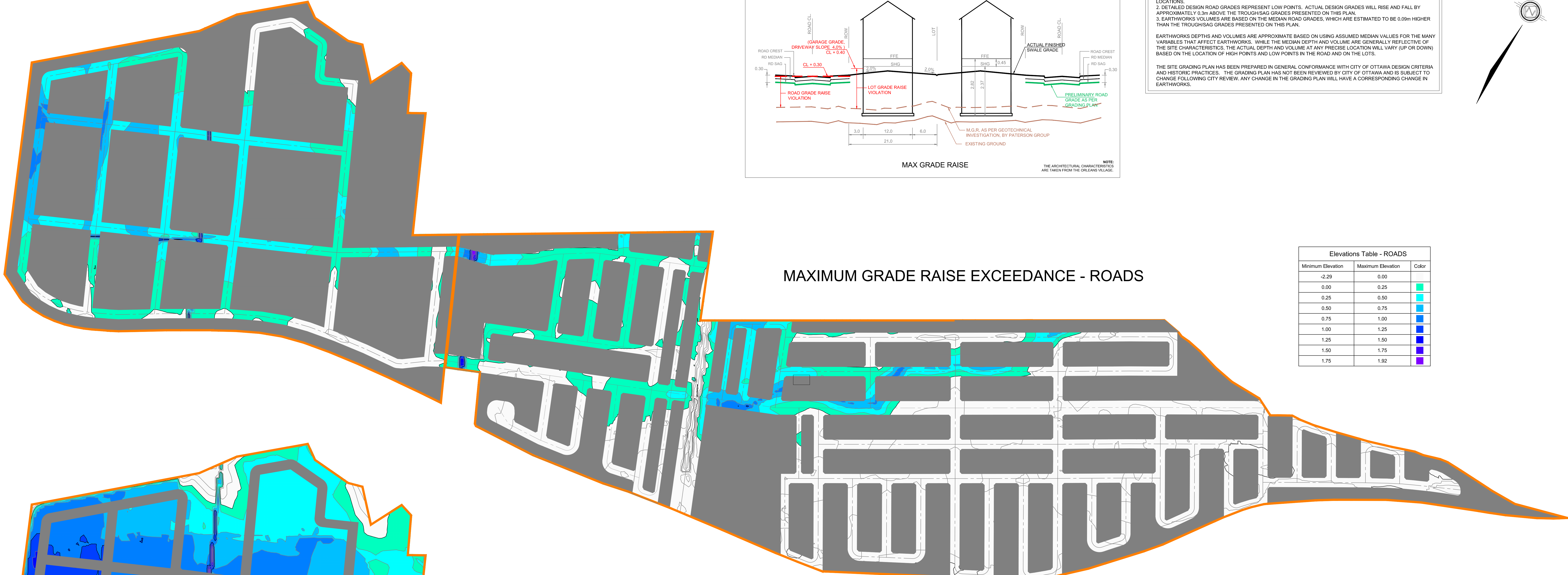


Minimum Elevation	Maximum Elevation	Color
-2.32	0.00	
0.00	0.25	Light Green
0.25	0.50	Light Blue
0.50	0.75	Medium Blue
0.75	1.00	Dark Blue
1.00	1.25	Blue
1.25	1.50	Dark Blue
1.50	1.75	Purple
1.75	2.00	Dark Purple
2.00	2.32	Very Dark Purple

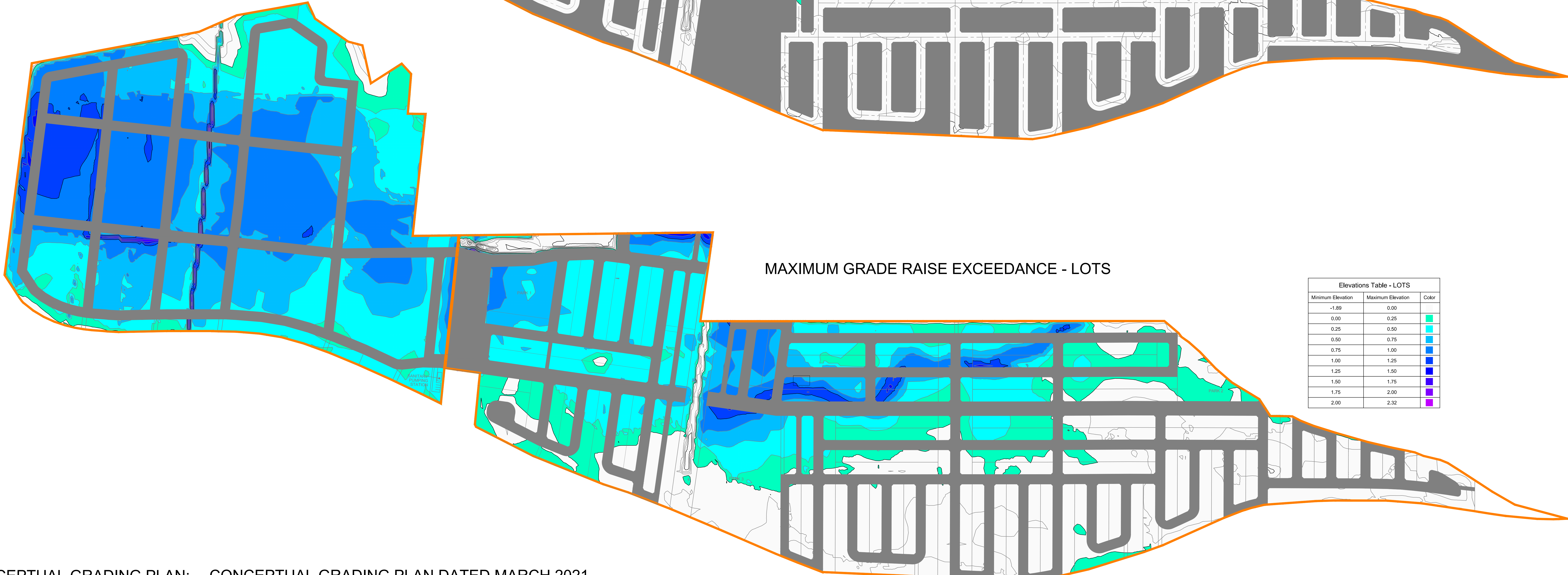
CONCEPTUAL GRADING PLAN: CONCEPTUAL GRADING PLAN DATED MARCH 2021
 ORIGINAL GROUND: SURVEY DATED NOVEMBER 2019
 MAXIMUM GRADE RAISE AS PER : GEOTECHNICAL INVESTIGATION, BY PATERSON GROUP DATED SEPTEMBER 27, 2019 - REVISED MAY 15, 2020



NOTES:
 1. LOW FLOW CHANNEL ELEVATION TO BE VERIFIED IN THE FIELD AT ALL ROAD AND SEWER CROSSING LOCATIONS.
 2. DETAILED DESIGN ROAD GRADES REPRESENT LOW POINTS. ACTUAL DESIGN GRADES WILL RISE AND FALL BY APPROXIMATELY 0.3m ABOVE THE TROUGH/SAG GRADES PRESENTED ON THIS PLAN.
 3. EARTHWORKS VOLUMES ARE BASED ON THE MEDIAN ROAD GRADES, WHICH ARE ESTIMATED TO BE 0.09m HIGHER THAN THE TROUGH/SAG GRADES PRESENTED ON THIS PLAN.
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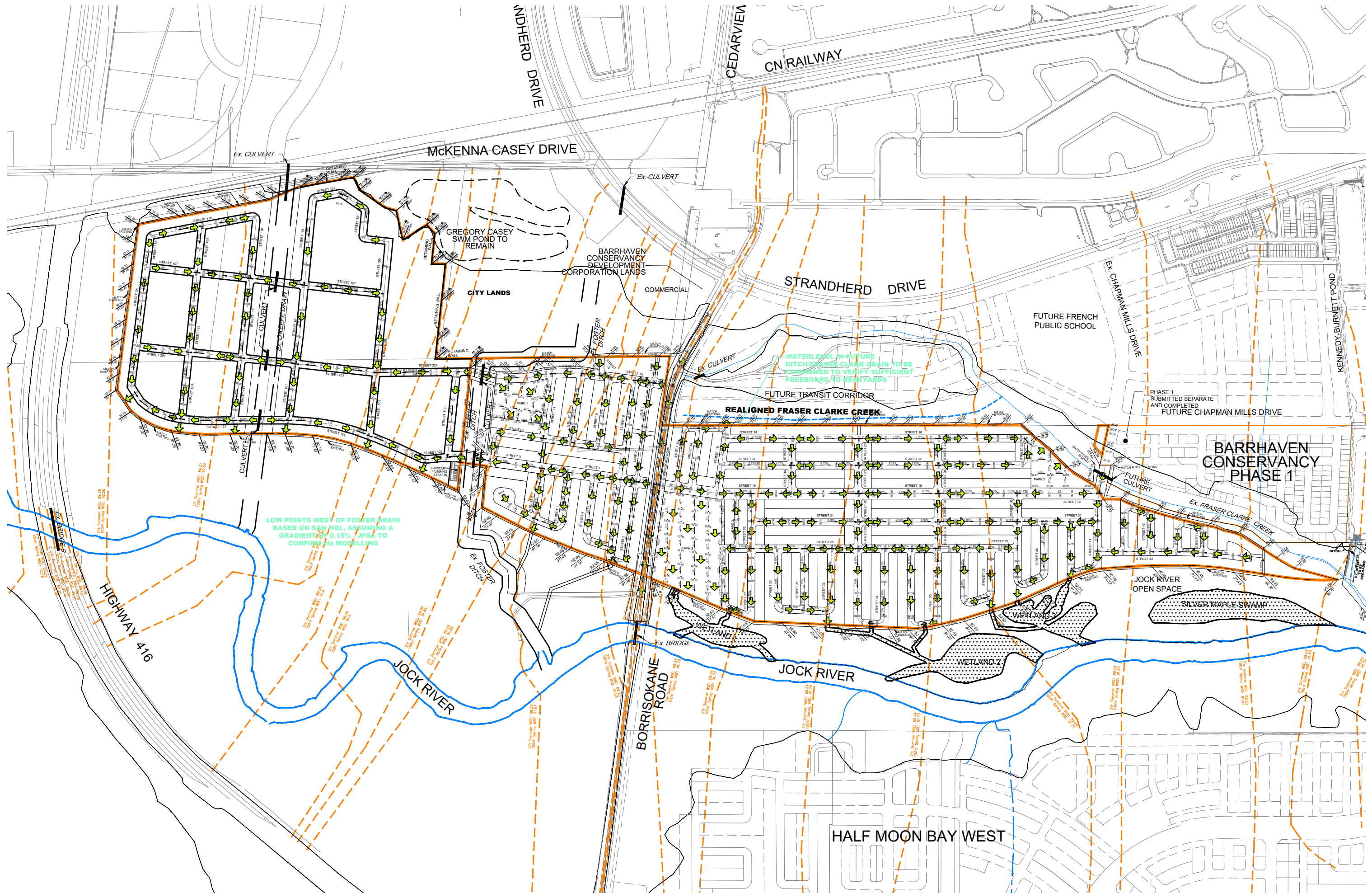


Minimum Elevation	Maximum Elevation	Color
-2.29	0.00	Light Green
0.00	0.25	Green
0.25	0.50	Light Blue
0.50	0.75	Blue
0.75	1.00	Dark Blue
1.00	1.25	Very Dark Blue
1.25	1.50	Dark Purple
1.50	1.75	Medium Purple
1.75	1.92	Dark Purple



Minimum Elevation	Maximum Elevation	Color
-1.89	0.00	Light Green
0.00	0.25	Green
0.25	0.50	Light Blue
0.50	0.75	Blue
0.75	1.00	Dark Blue
1.00	1.25	Very Dark Blue
1.25	1.50	Dark Purple
1.50	1.75	Medium Purple
1.75	2.00	Dark Purple
2.00	2.32	Very Dark Purple

CONCEPTUAL GRADING PLAN: CONCEPTUAL GRADING PLAN DATED MARCH 2021
 ORIGINAL GROUND: SURVEY DATED NOVEMBER 2019
 MAXIMUM GRADE RAISE AS PER : GEOTECHNICAL INVESTIGATION, BY PATERSON GROUP
 DATED SEPTEMBER 27, 2019 - REVISED MAY 15, 2020



McKENNA CASEY DRIVE

STRANDHERD DRIVE

REALIGNED FRASER CLARKE CREEK

BARRHAVEN CONSERVANCY PHASE 1

JOCK RIVER

JOCK RIVER

BORRISOKANE ROAD

HALF MOON BAY WEST

LOW POINTS WEST OF FOSTER DRAIN
BASED ON SAN HGL, ASSUMING A
GRADIENT OF 0.15% - JFSA TO
CONFIRM via MODELLING

WATERLEVEL IN FUTURE
DITCH/FRASER-CLARK DRAIN TO BE
CONFIRMED TO VERIFY SUFFICIENT
FREEBOARD TO REARYARDS

PHASE 1
SUBMITTED SEPARATE
AND COMPLETED
FUTURE CHAPMAN MILLS DRIVE

JOCK RIVER
OPEN SPACE

SILVER MAPLE SWAMP

GREGORY CASEY
SWM POND TO
REMAIN

BARRHAVEN
CONSERVANCY
DEVELOPMENT
CORPORATION LANDS

FUTURE FRENCH
PUBLIC SCHOOL

WETLAND

WETLAND

WETLAND 2

Ex. FOSTER
DITCH

Ex. BRIDGE

Ex. FRASER CLARKE
CREEK

Ex. CHAPMAN MILLS DRIVE

KENNEDY-BURNETT POND

Ex. CULVERT

Ex. CULVERT

Ex. CULVERT

FUTURE CULVERT

HIGHWAY 416

ANDHERD DRIVE

CEDARVIEW

CN RAILWAY