

ADEQUACY OF PUBLIC SERVICING REPORT 140055-6.04.03

# 1640 – 1660 Carling Avenue

**CITY OF OTTAWA** 



Prepared for Hobin Architecture Inc. by IBI Group December 9, 2022

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## 1 INTRODUCTION

## 1.1 Objective

IBI Group Professional Services (Canada) Inc. (hereinafter referred to as IBI, or IBI Group) has been retained as a subconsultant for Hobin Architecture Inc (HAI). to prepare this Adequacy of Public Services Report in support of a zoning application to the City of Ottawa. Hobin Architecture Inc. has been retained as prime and architectural consultant by RioCan Management Inc (RioCan). This report will provide stakeholders with a conceptual level layout of the proposed development sufficient to support the zoning application for the subject lands.

## 1.2 Location

The subject property is approximately 2.3 Ha in size and is located in the City of Ottawa, at 1640 and 1660 Carling Avenue. The site is bound to the north by Carling Avenue with existing commercials lands; to the east by the Carling Mazda Dealership commercials lands; to the south by future residential lands to be constructed (Claridge Homes – 6 Towers); and bound to the west by Clyde Ave N, with existing commercials lands. Refer to **Figure 1.1** below for key map of site location, and **Appendix A** for a copy of the concept redevelopment plan.



Figure 1.1 – Key Map of Subject Lands

## 1.3 Proposed Development

RioCan is proceeding with the zoning application for redevelopment of it 1640-1660 Carling Avenue site. The proposed development would combine a mix of high density mixed-use residential towers and a park block.

The current concept plan identifies 2 mixed-use buildings, 3 dedicated residential buildings, and 1 seniors living building. Total anticipated units is 1715 along with a public park and a public plaza. Approximately 2.3 Ha in total; a copy of the plan is included in **Appendix A**.

Vehicular access to the subject lands is primarily proposed off Carling Ave and Clyde Ave N and through the construction of a new 20m public right-of-way through the subject lands.

## 1.4 Previous Studies

The following reports have been referenced prior to completing this assessment:

- Site Servicing & Storm Water Management Report Delcan, September 2006. This report provides details on the existing stormwater management, waste water management, water supply and includes drawings of the existing site.
- **1640-1660 Carling Avenue, Amendment to Site Servicing and Stormwater Management Report** - Application for Revision to Site Plan D07-12-10-0138, Restaurant Conversion (Boston Pizza) - Delcan, July 2010. This report provides details of the Boston Pizza parcel on the site.

## 1.5 Pre-Consultation

A pre-consultation meeting was hosted virtually by the City of Ottawa on September 13<sup>th</sup>, 2022. Notes of the meeting were circulated by City staff on September 26<sup>th</sup>, 2022 a copy of the preconsult notes are included in **Appendix A**. To proceed with project development a rezoning for the site is necessary, to change the site from commercial to mixed use/residential zoning. With respect to servicing, there were no specific concerns flagged during the pre-consult.

An informal meeting with the City of Ottawa was held on November 17, 2022, where the city stated their intent to replace and upgrade the sanitary sewer trunk on Carling Avenue flowing eastwards. The City of Ottawa was undertaking a review to confirm if this upgrade would be able to accommodate the increase of sanitary flow proposed from this development. The City has since confirmed that these upgrades will be completed within the next year, and that there are no downstream servicing concerns with the proposed redevelopment plan. Refer to correspondence in **Appendix C**.

## 1.6 Environmental Issues

No environmental issues were identified during the pre-consultation meeting held with the City of Ottawa on September 13<sup>th</sup>, 2022.

There are no identified Municipals Drains or watercourses within the proximity to this subject development.

## 1.7 Geotechnical Considerations

EXP has been retained by RioCan to prepare a Geotechnical investigation. Report is expected in the Spring of 2023 along with Phase 2 ESA and the hydrogeological report.

## 1.8 Existing Infrastructure

Figure 2.1 Conceptual Watermain Layout, Figure 3.1 Conceptual Sanitary Sewer Layout and Figure 4.1 Conceptual Storm Sewer Layout which can all be found in Appendix B, C and D respectively show the existing infrastructure. The existing sanitary and storm sewers on-site will be decommissioned as new infrastructure will be constructed to better accommodate the redevelopment.

## 2 WATER DISTRIBUTION

## 2.1 Existing Conditions

The subject site is located within Pressure Zone 1W of the City of Ottawa's water distribution system. There is an existing 200mm diameter watermain along Carling Avenue and a 200mm diameter watermain along Clyde Avenue North.

## 2.2 Design Criteria

#### 2.2.1 Water Demands

As previously noted, the proposed development will consist of 2 mixed-use buildings, 3 dedicated residential buildings, and 1 seniors living building. Total anticipated units is 1715, for high level analysis purposes a 66-33% split was used to differentiate between 1 bedroom and 2 bedroom units. Based on projected populations taken from Table 4.1 of the City Design Guidelines, a watermain demand calculation sheet was prepared; a copy is included in **Appendix B** and the total water demands are summarized as follows:

Average Day	9.36 l/s
Maximum Day	23.00 l/s
Peak Hour	50.37 l/s
Fire Flow	13,000 l/min (Retirement Building)

#### 2.2.2 System Pressure

The 2010 City of Ottawa Water Distribution Guidelines states that the preferred practice for design of a new distribution system is to have normal operating pressures range between 345 kPa (50 psi) and 552 kPa (80 psi) under maximum daily flow conditions. Other pressure criteria identified in the guidelines are as follows:

Minimum Pressure	Minimum system pressure under peak hour demand conditions shall not be less than 276 kPa (40 psi)
Fire Flow	During the period of maximum day demand, the system pressure shall not be less than 140 kPa (20 psi) during a fire flow event.
Maximum Pressure	Maximum pressure at any point in the distribution system shall not exceed 689 kPa (100 psi). In accordance with the Ontario Building/Plumbing Code, the maximum pressure should not exceed 552 kPa (80 psi). Pressure reduction controls may be required for buildings where it is not possible/feasible to maintain the system pressure below 552 kPa

#### 2.2.3 Boundary Conditions

The boundary condition request has been submitted to the City of Ottawa. Detailed water model analysis and results will be provided in 2<sup>nd</sup> submission. Two watermain connections are

proposed, one connection location along the 200 mm diameter watermain on Carling Avenue and the other to the 200 mm diameter watermain on Clyde Avenue North.

At each location a pressure is provided for the maximum HGL, peak hour and max day plus fire scenarios based on the existing ground elevations.

#### 2.2.4 Watermain Layout

The conceptual watermain layout for this development is shown on **Figure 2.1** in **Appendix B.** A 200 mm diameter main will be extended from Carling Avenue. The 200 mm diameter watermain will continue through the public road in the site and connect to Clyde Avenue North, closing the loop. This watermain will service all 6 proposed residential and mixed-use residential structures, as well as the public park.

A hydraulic model using the InfoWater program will be produced during detailed design that will confirm the watermain sizes. Based on the pressures provided by the boundary conditions it is expected that all the watermain pressure and fire flow requirements will be met for this phase. As the proposed watermain layout is well looped without dead end mains it is expected that all the requirements will be achieved at the detailed design phase.

Each building will have two watermain servicing connections for redundancy due to having more than 50 units.

## 3 WASTEWATER DISPOSAL

## 3.1 Existing Conditions

The existing 1640 - 1660 Carling Ave wastewater system is shown in **Figure 3.1** in **Appendix C.** The existing peak sanitary flow for all buildings was estimated to be 14.1 L/s as shown in the Delcan Design Sheet also provided in **Appendix C.** Serviced by a 200 mm diameter sanitary pipe that outlets into a 300 mm diameter sewer on Carling Avenue.

The existing sanitary main on Carling Avenue is approaching its end-of-life stage and the City of Ottawa already has planned to replace and upgrade the sanitary main to a larger size to accommodate the increased flow from both the 1660 Carling Ave project and the Claridge Homes – 6 Towers project. The City of Ottawa has confirmed that this upgrade is expected in 2023, and that the upgrade will account for the increase density resulting from the rezoning of this parcel. Refer to correspondence provided in **Appendix C**.

## 3.2 Design Criteria

The sanitary flows for the subject lands are determined based on current City of Ottawa design criteria and the population densities established in the MSS, which includes, but is not limited to the following:

#### 3.2.1 Design Flow:

1 Bedroom Unit

Average Residential Flow	-	280 l/cap/day
Average Commercial/Institution Flow	-	28,000 l/Ha/day
Peak Residential Factor	-	Harmon Formula
Peak Commercial/Institution Factor	-	1.0
Infiltration Allowance	-	0.33 l/sec/Ha
<b>3.2.2</b> Population Density per Table 4.1:		
2 Bedroom Unit	-	2.1 person/unit

## 3.3 Proposed Wastewater Disposal System

It is proposed that the subject lands discharge into the existing wastewater disposal system, the 300 mm diameter sanitary sewer along Carling Avenue. The connection point will now be 22 m upstream, to the west of the previous connection point along the Carling Avenue Sanitary main.

1.4 person/unit

The proposed total flow from the subject lands would increase the total peak flow from 14.1 L/s to 28.1 L/s, a net increase of 14.0 L/s. This additional flow may stress the existing sanitary system. Development restrictions <u>may</u> be required to coincide with the timing of the sanitary sewer upgrade.

The proposed Sanitary sewers will consist of 300mm to 200mm diameter sewers, constructed to current City of Ottawa design standards. A conceptual Sanitary Sewer layout is provided on

**Figure 3.1**, and a Sanitary Drainage Area Plan **Figure 3.2**, and a conceptual **Sanitary Sewer Design Sheet** have been prepared for this Adequacy of Public Servicing Report in order to confirm approximate pipes sizes and sewer crossing information that corresponds with the grade raise restriction, unit types and macro grading concept of the proposed redevelopment plan. These documents can be found in **Appendix C.** 

#### 3.3.1 Proposed Population Calculations

As previously noted, the high level analysis concept development plan anticipates 523 two bedroom units, and 1192 single bedroom units, along with 0.67 ha of commercial area. The total anticipated design population is indicated below.

UNIT TYPE	# OF UNITS	POPULATION DENSITY	POPULATION			
2 Bedroom	523	2.1 pp/unit	1098			
1 Bedroom	1192	1.4 pp/unit	1669			
TOTAL	1715	-	2767			

Table 3-1

#### 3.3.2 Design Flows

Design flows for the proposed development lands are determined in the following table.

Table 3-2

Table 3-2							
РОР	280 L/POP/DAY	PEAK FACTOR	PEAK FLOW	AREA	TOTAL FLOW		
2767	280	2.97	27.06 L/s	2.3 ha	28.07 L/s		

Based on the results, peak flows estimated from the proposed draft plan are larger than the existing peak flows from the subject lands. Once the upgrade of the Carling Avenue Sanitary Sewer is completed it will accommodate the discharge and have no negative impact on downstream infrastructure.

## 4 STORMWATER MANAGEMENT

## 4.1 Existing Conditions

The existing 1640 – 1660 Carling Ave stormwater system is shown in Figure 4.1 in **Appendix D**. The existing development plan currently has two discharge locations. The Carling Avenue and Clyde Avenue N stormwater connections both discharge into a 375 mm diameter stormwater main at their respective locations.

The existing development includes an oil and grit separator at each connection, for water quality control. The oil and grit separators include 80% TSS removal.

## 4.2 Synopsis of Previous Studies

The 2006 Site Servicing and Stormwater Management Report from 2006 can be found in **Appendix D**, which highlights the existing conditions noted above in section 4.1.

Additionally, the report identified a total 100-year maximum release rate of 70.25 L/s. This is based on a 5-year restriction with a c-value of 0.50 and a Tc of 20 minutes.

## 4.3 Proposed Stormwater Management Plan

The stormwater management system for the site will incorporate standard urban drainage design and stormwater management features may include:

- a dual drainage concept
- routing of surface runoff
- underground storage
- roof top storage

The stormwater management system will be developed based on the MOE *Stormwater Management Planning and Design Manual* (March 2003) and the *City of Ottawa Sewer Design Guidelines* (October 2012). Additionally, the system has incorporated, wherever possible given the existing trunk sewer inlet capacity restrictions, the new guidelines set forth within the Technical Bulletin ISDTP-2014-1 and PIEDTB-2016-01.

## 4.4 Minor Storm Sewer Design Criteria

The minor storm flow estimates were reviewed by the rational method. A conceptual Storm sewer layout **Figure 4.1**, a conceptual Storm Drainage Area Plan **Figure 4.2**, and a conceptual **Storm Sewer Design Sheet** have been prepared for this adequacy of public servicing report in order to confirm approximate pipes sizes and sewer crossing information that corresponds with the grade raise restriction, unit types and macro grading concept of the proposed phase. These documents can be found in **Appendix D.** Criteria used in the minor storm sewer design include, but are not limited to the following:

- Intensity 2 year curve (local and minor collector roads)
  - Initial Time of Concentration 10 min
- Approximate Average Runoff Coefficients used for this assessment only: Average Subject Area
   0.50
  - Velocities 0.80 m/s to 6.0 m/s

Manning roughness coefficient
Minimal allowable slopes

0.013 (smooth wall pipes) Refer to below table

DIAMETER (MM)	SLOPE (%)			
250	0.432			
300	0.340			
375	0.250			
450	0.195			
525	0.160			

#### Table 4-1 Minimal allowable slopes

• Minimum depth of cover of 2.0 m

The minimum minor system capture of ICDs for 1660 Carling Avenue will be based on the maximum release rate identified above. The subject site will be modelled using DDSWMM and XPSWMM to confirm minor and major system flows. Hydrographs from the site will be downloaded to XPSWMM hydraulic model to confirm hydraulic grade line within the proposed storm sewers. Due to the very restrictive nature of the release rate, it is anticipated that the future public right-of-way will require an underground storm water storage system. This may impact the amount of useable space in the boulevard for public owned street trees. The maximum allowable release rate will be pro-rated by area to each block. It is anticipated that each block, including the public park, will incorporate underground or roof top storage measures.

## 4.5 Major System

Inlet control devices (ICDs) will be proposed to control the surcharge in the minor system downstream of the site during infrequent storm events and maximize the use of available onsite storage. Emergency flow routes have been provided. Freeboard to each building entrance will comply with current City of Ottawa ODSG.

Major flow up to the 100 year event will be retained on-site, flows in excess of the 100 year event will flow along the emergency flow routes as shown on the macro grading plan.

### 4.6 Hydrological Analysis

The dual drainage system will be evaluated during detailed design stage using the DDSWMM hydrological model, while the minor system hydraulic grade line analysis will be evaluated using the XPSWMM dynamic model.

The primary focus of the hydrological analysis will be to evaluate surface flow and ponding conditions during the 100-year storm event in order to satisfy City of Ottawa Sewer Design Guidelines (2012) in terms of velocity x depth.

## 4.7 Conceptual Storm Sewer System

**Figure 4.1** in **Appendix D** illustrates a conceptual layout of the storm sewer network to service the redevelopment plan. The Storm Drainage Area **Figure 4.2** and Storm Sewer Design sheet, also found in **Appendix D**, have been updated to illustrate the existing downstream infrastructure is suitably sized to accommodate the proposed development. The storm sewers for the subject lands will be designed to meet City of Ottawa and MOE requirements. Two branches are proposed with one connecting to Carling Avenue, and the other connecting to Clyde Avenue N, similar to the existing system. The locations will have to move as to accommodate the construction of the new towers.

## 4.8 Storm Water - Water Quality Control

As per the existing conditions identified in section 4.1, on site water quality control is required. Therefore, each of the outlets will require new oil and grit separators sized to provide 80% TSS removal.

## 5 GRADING AND ROADS

## 5.1 Site Grading

The existing grades within portions of the proposed development lands vary due to the existing topography of the site. The final grading plan will require the balancing of various requirements including but not limited to geotechnical constraints, minimum/maximum slopes, overland routing of stormwater, all to ensure the site is graded in accordance with municipal standards.

A conceptual macro grading plan has been prepared to identify the conceptual grading of the proposed development. Refer to Figure 6.1 in Appendix E.

A retaining wall is anticipated along the south and eastern property lines.

## 5.2 Road Network

The concept plan delineates the proposed road pattern for the development. The proposed municipal road within the development is to be designed to a 20.0m non-standard local road ROW, with 7.5m wide asphalt at travel lanes, widening to 12.5m where roadside parking is provided.

There are 38 road-side parking spaces along the public road through the development. There are an additional 896 underground parking spaces. The breakdown of the underground parking spaces can be seen in Table 5-1 and a parking concept plan can be seen in **Appendix E**.

Table 5-1 Faiking Spaces					
•	LEVELS	TOTAL SPOTS			
STREET	-	38			
BUILDING 1	3	120			
BUILDING 2	3	160			
BUILDING 3	1	116			
BUILDING 4	3	150			
BUILDING 5&6 (INTERCONNECTED)	4	450			

Table 5-1 Parking Spaces

Noise attenuation features and housing noise provisions will be required for road noise generated by Carling Avenue and Clyde Avenue North. Refer to the Noise Feasibility Study prepared by Gradient Wind.

Sidewalks and pathways will be provided as agreed in the draft conditions of subdivision.

### 5.3 Intersection Improvements

Any intersection improvements will be identified in the Traffic Impact Study.

## 6 SOURCE CONTROLS

## 6.1 General

Oil and grit separators are provided as stormwater treatment prior to connections to existing infrastructure. On site measures may include the following:

- flat site grading where possible
- vegetation planting
- groundwater recharge in landscaped areas

## 6.2 Lot Grading

Where possible, all of the proposed blocks within the development will make use of gentle surface slopes on hard surfaces such as asphalt and concrete. In accordance with local municipal standards, all grading will be between 0.5 and 5.0 percent for hard surfaces and 2.0 and 7.0 percent for all landscaped areas. Significant grade changes will be accomplished through the use of terracing (3:1 max slope), ramps and/or retaining walls. All street and parking lot catchbasins shall be equipped with 3.0m subdrains on opposite sides of a curbside catchbasin running parallel to the curb, and with 3.0m subdrains extending out from all 4 sides of parking lot catchbasins.

## 6.3 Vegetation

As with most subdivision agreements, the developer will be required to complete a vegetation and planting program. Vegetation throughout the development including planting along roadsides and within the individual blocks provides opportunities to re-create lost vegetation.

### 6.4 Groundwater Recharge

Groundwater recharge targets have not been identified for this site. Perforated sub-drain systems will be implemented at capture locations in all vegetated areas. This will promote increased infiltration during low flow events before water is collected by the storm sewer system.

## 7 CONVEYANCE CONTROLS

## 7.1 General

Besides source controls, the development also proposes to use several conveyance control measures to improve runoff quality. These will include:

- vegetated swales; and
- catchbasin sumps and manhole sumps.

## 7.2 Catchbasins and Maintenance Hole Sumps

All catchbasins within the development, either rear yard or street, will be constructed with minimum 600 mm deep sumps. These sumps trap pollutants, sand, grit and debris which can be mechanically removed prior to being flushed into the minor pipe system. Both rear yard and street catchbasins will be to OPSD 705.02. All storm sewer maintenance holes serving local sewers less than 900 mm diameter shall be constructed with a 300 mm sump as per City standards.

## 8 SEDIMENT AND EROSION CONTROL PLAN

## 8.1 General

During construction, existing stream and conveyance systems can be exposed to significant sediment loadings. A conceptual sediment and erosion control will be detailed during the detailed design stages. Although construction is only a temporary situation, it will be proposed to introduce a number of mitigative construction techniques to reduce unnecessary construction sediment loadings. These may include:

- groundwater in trench will be pumped into a filter mechanism prior to release to the environment;
- bulkhead barriers will be installed at the nearest downstream manhole in each sewer which connects to an existing downstream sewer;
- seepage barriers will be constructed in any temporary drainage ditches;
- filter cloths will remain on open surface structure such as manholes and catchbasins until these structures are commissioned and put into use; and
- Silt fence on the site perimeter.

## 8.2 Trench Dewatering

Although little groundwater is expected during construction of municipal services, any trench dewatering using pumps will be discharged into a filter trap made up of geotextile filters and straw bales similar in design to the OPSD 219.240 Dewatering Trap. These will be constructed in a bowl shape with the fabric forming the bottom and the straw bales forming the sides. Any pumped groundwater will be filtered prior to release to the existing surface runoff. The contractor will inspect and maintain the filters as needed including sediment removal and disposal and material replacement as needed.

## 8.3 Bulkhead Barriers

At the first new manhole constructed within the development that is immediately upstream of an existing sewer a temporary ½ diameter bulkhead will be constructed over the lower half of the outletting sewer. This bulkhead will trap any sediment carrying flows thus preventing any construction-related contamination of existing sewers. The bulkheads will be inspected and maintained including periodic sediment removal as needed and removed prior to top course asphalt being laid.

## 8.4 Seepage Barriers

The presence of road side ditches along Fernbank Road necessitate the installation of seepage barriers. These barriers will consist of both the Light Duty Straw Bale Barrier as per OPSD 219.100 or the Light Duty Silt Fence Barrier as per OPSD 219.110. The barriers are typically made of layers of straw bales or geotextile fabric staked in place. All seepage barriers will be inspected and maintained as needed.

## 8.5 Surface Structure Filters

All catchbasins, and to a lesser degree manholes, convey surface water to sewers. However, until the surrounding surface has been completed these structures should be covered in some fashion to prevent sediment from entering the minor storm sewer system. Until landscaped areas are sodded or until streets are asphalted and curbed, catchbasins and manholes will be constructed with geotextile filter bags or a geotextile filter fabric located between the structure frame and cover respectively. These will stay in place and be maintained during construction and build until it is appropriate to remove same.

## 8.6 Stockpile Management

During construction of any development similar to that proposed by the Owner, both imported and native soils are stockpiled. Mitigative measures and proper management to prevent these materials entering the sewer systems is needed. Significant excess material will be generated from the subject lands and will need to be disposed of off-site in a manner consistent with all MOE regulations.

During construction of the deeper municipal services, water, sewers and service connections, imported granular bedding materials are temporarily stockpiled on site. These materials are however quickly used up and generally before any catchbasins are installed.

Contamination of the environment as a result of stockpiling of imported construction materials is generally not a concern provided the above noted seepage barriers are installed. These materials are quickly used and the mitigative measures stated previously, especially the  $\frac{1}{2}$  diameter sewer bulkheads and filter fabric in catchbasins and manholes help to manage these concerns.

The roadway granular materials are not stockpiled on site. They are immediately placed in the roadway and have little opportunity of contamination. Lot grading sometimes generates stockpiles of native materials. However, this is only a temporary event since the materials are quickly moved off site.

To assist in the control of transporting sediment off-site into municipal roads, mud mats will be employed at the construction entrances.

## 9 CONCLUSIONS

Water and stormwater systems required to accommodate the orderly development of the 1640-1660 Carling Avenue Development are available to service the subject site. Wastewater systems will be able to accommodate the development once the City of Ottawa completes upgrades to the sanitary system on the Carling Avenue. Phasing the construction of the towers can be organized to not stress the existing wastewater system until necessary upgrades are completed. The attached figures and supporting conceptual analysis illustrate that the lands can be re-zoned and developed in an orderly and effective manner and in accordance with the City of Ottawa's current level of service requirements.

The use of lot level controls, conveyance controls and end of pipe controls outlined in the report will result in effective treatment of surface stormwater runoff from the site. Adherence to the proposed sediment and erosion control plan during construction will minimize harmful impacts on surface water.

This report outlined a conceptual servicing scheme to support the rezoning application of the proposed development. Detail design of the infrastructure would be completed upon issuance of draft plan approval and would be subject to various governmental approvals prior to construction, including but not limited to the following:

- Certificate of Authorization (C of A) for sewers and SWM: Ministry of Environment;
- Commence Work Order: City of Ottawa;

Report Prepared By:



Demetrius Yannoulopoulos, P. Eng. Director – Office Lead

Row

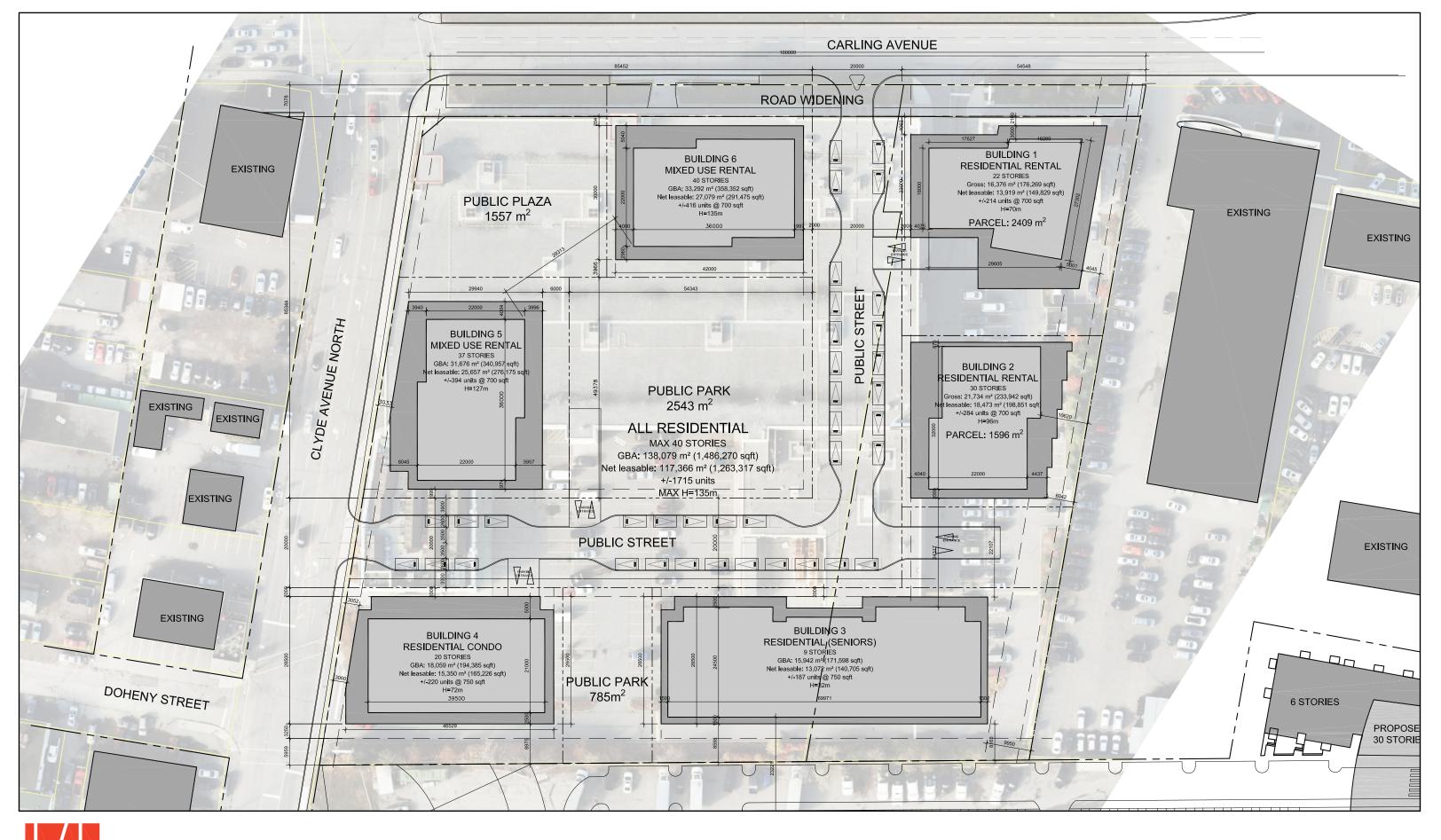
Ryan Magladry, C.E.T. Project Manager

Arthur Beresniewicz, E.I.T. Engineering Intern

\IBI Group\140055 1650-1660 Carling Avenue - Internal Documents\6.0\_Technical\6.04\_Civil\03\_Reports\APSR Submission #1\CTR\_1660 Carling\_APSR\_2022-11-09

## **APPENDIX A**

- Conceptual Site Plan
- Notes of Pre-Consultation Meeting with City of Ottawa
- Existing Conditions Delcan Servicing Plan



<u>1640 - 1660 CARLING AVE</u> Concept Site Plan - Full Build Out

SCALE: 1:750

#### **Pre-Application Consultation Meeting Notes**

Property Address: 1640-1660 Carling Avenue PC2022-0215 September 13, 2022; 2:30 PM – 3:30 PM – Microsoft Teams

#### Attendees:

#### City of Ottawa:

Kersten Nitsche – File Lead, Planner III Masha Wakula Vakula – Planner I Mohammed Fawzi – Infrastructure PM Patrick McMahon – Transportation PM Christopher Moise – Urban Design Mike Russett – Parks Planner Amber Chen – Student Planner

#### Applicants:

Doug Van Den Ham – Hobin Architecture Patrick Bisson – Hobin Architecture Paul Black – Fotenn Consultants Inc. Bipin Dhillon – Fotenn Consultants Inc. Stuart Craig – RioCan REIT Vanessa Leon – RioCan REIT Basel Ansari – Parsons Corporation Ryan Magladry – IBI Group

#### Community Representatives:

N/A

#### **Regrets:**

Mark Richardson - Forester, City of Ottawa

#### Subject: 1640-1660 Carling Avenue

#### Meeting notes:

Opening & attendee introduction

• Introduction of meeting attendees

#### Overview of Proposal

- Zoning By-law Amendment Application
  - Currently not looking for a Site Plan Control Application

- Arterial Mainstreet Zone, Subzone 10 (AM10)
- Redevelopment of the site: highest profile building is put in the corner of Carling and Clyde, transitioning down towards east and south to create a valley of building forms
- Harder landscape, urban plaza is proposed with possible retail and commercial uses
- Internal public street is proposed
- Various public spaces are proposed in the middle of the site
- The 8-storey building is intended for seniors
- Need roughly 900 parking spaces on the site

#### Planning – Kersten Nitsche

- If you move forward with introducing a public road, you will need a Plan of Subdivision application
- Buildings on the south side facing Claridge; what's the intention for those buildings? Will there be access crossing?
- What is your anticipated timing for the zoning application?
  - Answer: Ideally early 2024 for approval
- Do you anticipate/will you be talking to Claridge? It would be ideal to link the public roads with each other
- As noted by Urban Design, we recommend a conceptual context plan be developed to help envision the future context. Please include the site at 861 Clyde as well as any other sites in the immediate vicinity that are undergoing or have the potential for redevelopment.
- Overall, it seems that the tower separation and maximizing the number of buildings has led the site layout. Within the contextual analysis, please ensure that you analyze and consider the public spaces first.

### <u> Urban Design – Christopher Moise</u>

- This proposal runs along one of the City's Design Priority Areas and must attend the City's UDRP. We recommend the proposal attend an Informal visit (prior to a full submission and is not a public meeting), with the City's UDRP to further discuss and evaluate various scenarios of development for the whole site;
- We appreciate the design material submitted for the pre-consultation meeting and have the following comments/questions about the design:
  - Secondary plan: There is no secondary planning document to help direct development for this site, however the property to the south at 861 Clyde developed 'conceptual context framework plans' to help envision the future context around the site on adjacent streets and blocks- (see attached). We recommend this proposal do a similar exercise and use that to guide the discussion with staff and at the UDRP;
  - High-rise guidelines: We recommend the proposal fully considers the guidelines especially with regard to: Floorplate max 750m2; Separation distance 23m between towers; 11.5m to adjacent property lines;
  - **Parks**: We recommend the location and size be considered further, especially considering a shadow study of the built form on and around the site;

• A scoped Design Brief is a required submittal (and separate from any UDRP submission) for all Site Plan/Re-zoning applications. Please see the Design Brief Terms of Reference provided and consult the City's website for details regarding the UDRP schedule.

# • Note. The Design Brief submittal should have a section which addresses these pre-consultation comments;

This is an exciting project in an area full of potential. We look forward to helping you achieve its goals with the highest level of design resolution. We are happy to assist and answer any questions regarding the above. Good luck.

#### Parks Comments – Mike Russett

- Formal comments pending.
- Please review the provisions of Parkland Dedication By-law 2022-280.

#### Infrastructure Notes and Comments – Mohammed Fawzi

#### Available Infrastructure:

#### Carling Avenue:

- \*Sanitary: 225mm Conc (Install N/A)
- Storm: 375mm Conc (Install N/A)
- Water: 203mm UCI (Install 1958)
- Storm: 225mm Conc (Install 1959)
- \*\*Water: 610mm COO (Install 1955)
- \*Sanitary capacity to be evaluated and confirmed. Please send an email with proposed sanitary flows to determine if constraints are present.
- \*\*No connections to large diameter watermains are permissible. A watermain protection plan may be required during detailed design in the event construction to large watermain is in close proximity.

#### **Clyde Avenue:**

- Sanitary: 225mm Conc (Install 1955)
- Storm: 300mm Conc (Install 1961)
- Water: 203mm UCI (Install 1955)

#### Water Boundary Conditions:

- Will be provided at request of consultant. Requests must include the location of the service and the expected loads required by the proposed development. Please provide the following and <u>submit Fire Flow Calculation Sheet</u> per FUS method with the request:
  - Location of service
  - Type of development and amount of required fire flow (per FUS method <u>include</u> <u>FUS calculation sheet with request</u>)
  - Average Daily Demand (I/s)
  - Maximum Hourly Demand (I/s)
  - Maximum Daily Demand (I/s)
- Water Supply Redundancy Fire Flow:
  - Applicant to ensure that a second service with an inline valve chamber be provided where the average daily demand exceeds 50 m<sup>3</sup> / day (0.5787 l/s per day)
- Water services larger than 19 mm require a Water Data Card. Please complete card and submit.

## Stormwater Management (Quantity Control):

- Coefficient (C) of runoff determined **as per existing conditions** but in no case more than 0.5.
- TC = To be calculated, minimum 10 minutes
- Any storm events greater than 2 year, up to 100 year, and including 100-year storm event must be detained on site.
- Foundation drains are to be independently connected to sewer main unless being pumped with appropriate back up power, sufficient sized pump and back flow prevention.
- Roof drains are to be connected downstream of any incorporated ICD within the SWM system.

### Stormwater Management (Quality Control):

• Rideau Valley Conservation Authority to provide Quality Controls.

### Noise Study:

• Noise study required – due to proximity to existing Arterial Road (Carling Avenue).

### Phase I and Phase II ESA:

- Phase I ESA is required; Phase II ESA may be required depending on the results of the Phase I ESA. Phase I ESA must include an EcoLog ERIS Report.
- Phase I ESA and Phase II ESAs must conform to clause 4.8.4 of the Official Plan that requires that development applications conform to Ontario Regulation 153/04.

### **Required Studies**

- Assessment of Adequacy of Public Services
- Geotechnical Study
- Phase I ESA
- Phase II ESA (depends on outcome of Phase I)
- Noise Study

#### **Required Plans**

• Site Servicing Layout Plan

#### Snow Storage:

 Any portion of the subject property which is intended to be used for permanent or temporary snow storage shall be as shown on the approved site plan and grading plan. Snow storage shall not interfere with approved grading and drainage patters or servicing. Snow storage areas shall be setback from the property lines, foundations, fencing or landscaping a minimum of 1.5m. Snow storage areas shall not occupy driveways, aisles, required parking spaces or any portion of a road allowance. If snow is to be removed from the site please indicate this on the plan(s).

#### **Exterior Site Lighting:**

• Any proposed light fixtures (both pole-mounted and wall mounted) must be part of the approved Site Plan. All external light fixtures must meet the criteria for Full Cut-off Classification as recognized by the Illuminating Engineering Society of North America (IESNA or IES), and must result in minimal light spillage onto adjacent properties (as a guideline, 0.5 fc is normally the maximum allowable spillage). In order to satisfy these criteria, the please provide the City with a Site Lighting Plan, and Certification (Statement) Letter from an acceptable professional engineer stating that the design is compliant.

#### **Relevant information**

- The Servicing Study Guidelines for Development Applications are available at the following address: <u>https://ottawa.ca/en/city-hall/planning-and-development/informationdevelopers/development-application-review-process/development-applicationsubmission/guide-preparing-studies-and-plans#servicing-study-guidelines-developmentapplications
  </u>
- Servicing and site works shall be in accordance with the following documents:
  - Ottawa Sewer Design Guidelines (October 2012)
  - Ottawa Design Guidelines Water Distribution (2010)
  - Geotechnical Investigation and Reporting Guidelines for Development Applications in the City of Ottawa (2007)
  - City of Ottawa Slope Stability Guidelines for Development Applications (revised 2012)
  - City of Ottawa Environmental Noise Control Guidelines (January 2016)
  - City of Ottawa Park and Pathway Development Manual (2012)

- City of Ottawa Accessibility Design Standards (2012)
- Ottawa Standard Tender Documents (latest version)
- Ontario Provincial Standards for Roads & Public Works (2013)
- Record drawings and utility plans are also available for purchase from the City (Contact the City's Information Centre by email at <u>InformationCentre@ottawa.ca</u> or by phone at (613) 580-2424 x.44455).
- Any proposed work in utility easements requires written consent of easement owner.
- Please note that these comments are considered preliminary based on the information available to date and therefore maybe amended as additional details become available and presented to the City. It is the responsibility of the applicant to verify the above information. The applicant may contact me for follow-up questions related to engineering/infrastructure prior to submission of an application if necessary.

#### Transportation – Patrick McMahon

- Follow Traffic Impact Assessment Guidelines
  - Start this process as soon as possible. Applicant advised that their application will not be deemed complete until the submission of the draft step 1-4.
- Traffic calming measures will be evaluated at the time of submission of TIA Step 4 if the public roadway is pursued. Traffic calming measures shall reference best management practices from the Canadian Guide to Neighbourhood Traffic Calming, published by the Transportation Association of Canada, and/or Ontario Traffic Manual, and/or the City of Ottawa's Draft Traffic Calming Design Guidelines.
- Site triangles at the following locations on the final plan will be required:
  - Local at Clyde: 3 metres x 3 metres
  - Local at Carling: 5 metres x 5 metres
- Noise Impact Studies required for the following:
  - Road
  - Stationary (at time of site plan) if there will be any exposed mechanical equipment due to the proximity to neighbouring noise sensitive land uses.
- On site plan:
  - Show all details of the roads abutting the site up to and including the opposite curb; include such items as pavement markings, accesses and/or sidewalks.
  - Turning templates will be required for all accesses showing the largest vehicle to access the site; required for internal movements and at all access (entering and exiting and going in both directions).
  - Show all curb radii measurements; ensure that all curb radii are reduced as much as possible
  - Show lane/aisle widths.
- Show the 44.5m ROW protection for Carling Avenue.
- Minor realignment of the bus pad on Carling may be required, to be confirmed at site plan.
- Providing at least one bicycle parking pace per unit is encouraged rather than the minimum 0.5/unit. With Carling's reduced vehicular capacity, sustainable transportation infrastructure will be increasingly important.
- Consideration should be given to aligning the local through Doheny and through the site.

### Foresting – Mark Richardson

## TCR requirements:

- A Tree Conservation Report (TCR) must be supplied for review along with the suite of other plans/reports required by the City
  - an approved TCR is a requirement of Site Plan approval.
  - The TCR may be combined with the LP provided all information is supplied
- Any removal of privately-owned trees 10cm or larger in diameter, or city-owned trees of any diameter requires a tree permit issued under the Tree Protection Bylaw (Bylaw 2020 – 340); the permit will be based on an approved TCR and made available at or near plan approval.
- The Planning Forester from Planning and Growth Management as well as foresters from Forestry Services will review the submitted TCR
  - If tree removal is required, both municipal and privately-owned trees will be addressed in a single permit issued through the Planning Forester
  - Compensation may be required for city owned trees if so, it will need to be paid prior to the release of the tree permit
- The TCR must contain 2 separate plans:
  - Plan/Map 1 show existing conditions with tree cover information
  - Plan/Map 2 show proposed development with tree cover information
  - Please ensure retained trees are shown on the landscape plan
- the TCR must list all trees on site, as well as off-site trees if the CRZ extends into the developed area, by species, diameter and health condition
- please identify trees by ownership private onsite, private on adjoining site, city owned, co-owned (trees on a property line)
- If trees are to be removed, the TCR must clearly show where they are, and document the reason they cannot be retained
- All retained trees must be shown, and all retained trees within the area impacted by the development process must be protected as per City guidelines available at <u>Tree</u> <u>Protection Specification</u> or by searching Ottawa.ca
  - the location of tree protection fencing must be shown on the plan
  - show the critical root zone of the retained trees
- the City encourages the retention of healthy trees; if possible, please seek opportunities for retention of trees that will contribute to the design/function of the site.
- For more information on the process or help with tree retention options, contact Mark Richardson <u>mark.richardson@ottawa.ca</u> or on <u>City of Ottawa</u>

### LP tree planting requirements:

For additional information on the following please contact tracy.smith@Ottawa.ca

Minimum Setbacks

- Maintain 1.5m from sidewalk or MUP/cycle track or water service laterals.
- Maintain 2.5m from curb
- Coniferous species require a minimum 4.5m setback from curb, sidewalk or MUP/cycle track/pathway.
- Maintain 7.5m between large growing trees, and 4m between small growing trees. Park or open space planting should consider 10m spacing, except where otherwise approved in naturalization / afforestation areas. Adhere to Ottawa Hydro's planting guidelines (species and setbacks) when planting around overhead primary conductors.

Tree specifications

- Minimum stock size: 50mm tree caliper for deciduous, 200cm height for coniferous.
- Maximize the use of large deciduous species wherever possible to maximize future canopy coverage
- Tree planting on city property shall be in accordance with the City of Ottawa's Tree Planting Specification; and include watering and warranty as described in the specification (can be provided by Forestry Services).
- Plant native trees whenever possible
- No root barriers, dead-man anchor systems, or planters are permitted.
- No tree stakes unless necessary (and only 1 on the prevailing winds side of the tree)

Hard surface planting

- Curb style planter is highly recommended
- No grates are to be used and if guards are required, City of Ottawa standard (which can be provided) shall be used.
- Trees are to be planted at grade

#### Soil Volume

• Please document on the LP that adequate soil volumes can be met:

1		
Tree	Single Tree Soil	Multiple Tree Soil
Type/Size	Volume (m3)	Volume (m3/tree)
Ornamental	15	9
Columnar	15	9
Small	20	12
Medium	25	15
Large	30	18
Conifer	25	15

Please note that these soil volumes are not applicable in cases with Sensitive Marine Clay.

Sensitive Marine Clay

• Please follow the City's 2017 Tree Planting in Sensitive Marine Clay guidelines

### **Tree Canopy Cover**

- The landscape plan shall show how the proposed tree planting will replace and increase canopy cover on the site over time, to support the City's 40% urban forest canopy cover target.
- At a site level, efforts shall be made to provide as much canopy cover as possible, through tree planting and tree retention, with an aim of 40% canopy cover at 40 years, as appropriate.
- Indicate on the plan the projected future canopy cover at 40 years for the site.

### City Surveyor

• The determination of property boundaries, minimum setbacks and other regulatory constraints are a critical component of development. An Ontario Land Surveyor (O.L.S.)

needs to be consulted at the outset of a project to ensure properties are properly defined and can be used as the geospatial framework for the development.

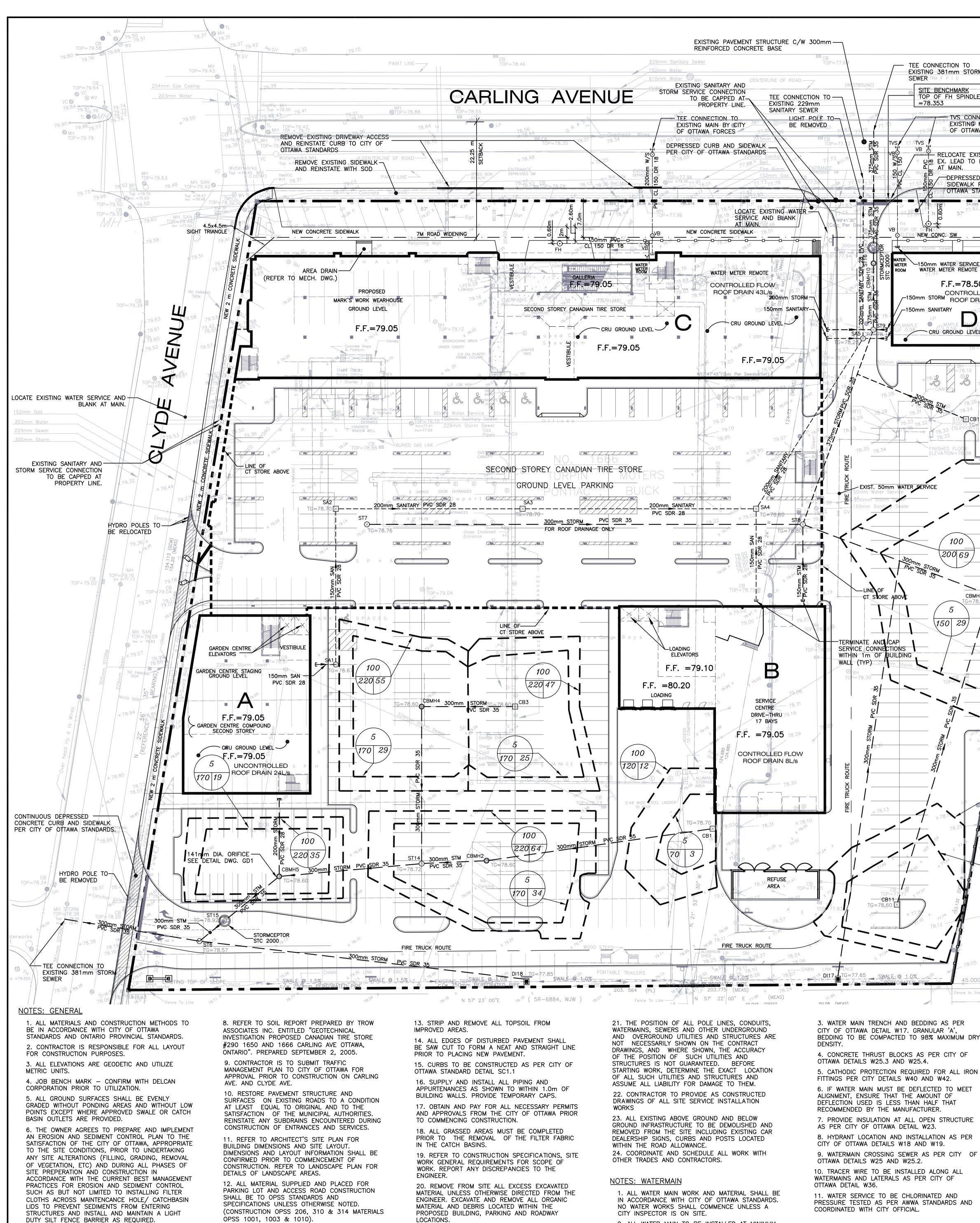
- Topographic details may also be required for a project and should be either carried out by the O.L.S. that has provided the Legal Survey or done in consultation with the O.L.S. to ensure that the project is integrated to the appropriate control network.
- Questions regarding the above requirements can be directed to the City's Surveyor, Bill Harper, at <u>Bill.Harper@ottawa.ca</u>

#### Waste Services

 New multi-unit residential development, defined as containing six (6) or more units, intending to receive City waste collection services will be required, as of June 1, 2022, to participate in the City's Green Bin program in accordance with Council's approval of the <u>multi-residential waste diversion strategy</u>. The development must include adequate facilities for the proper storage of allocated garbage, recycling, and green bin containers and such facilities built in accordance with the approved site design. Questions regarding this change and requirements can be directed to <u>Andre.Laplante@ottawa.ca</u>.

#### Conclusion and Next Steps

- Leading up to Formal Submission if you want to run through some changes, the city staff would be happy to hear reach out.
- If you have questions reach out to Kersten Nitsche.
- Additional information regarding fees related to planning applications can be found <u>here</u>.
- Plans are to be standard A1 size (594 mm x 841 mm) sheets, utilizing an appropriate Metric scale (1:200, 1:250, 1:300, 1:400 or 1:500).
- All PDF submitted documents are to be unlocked and flattened.



7. ABUTTING PROPERTY GRADE TO BE MATCHED.

2. ALL WATER MAIN TO BE INSTALLED AT MINIMUM COVER OF 2.4m.

			WA	TERM	1ain t	-Α
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TOP=77.98 $\otimes$ EH TOP=77.91 77.69 78.27 78.20 77.82 $\Rightarrow$ $\times$ 77.53		CBMH2	STM         78.70           STM         78.60           STM         78.72	77.15 76.99 76.86	– 77.00 76.95(E)	-
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313 =78.20		EX. SEWER	STM         78.57           STM         78.35           STM         78.60	76.61 76.47 77.15	76.64(N) 76.52	÷
78.25 TRANSFORMER (APPROXMATE LOCATION)		СВМН 4	STM         78.60           STM         78.76	77.02	77.08	
		ST8 ST9	STM 78.80 STM 78.19	76.82 76.65	77.02(W) 76.68(S)	
x 78.14		ST16	STM         77.66           STM         77.69           STM         77.82	76.58 76.52 76.33±	76.59 76.55 76.36	
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			STM 78.20 STM 77.65	76.82 77.24	-	
78.10 ×77.66			STM 77.85 STM FF/79.05	76.85 77.55	-	
		BLDG 'B' BLDG 'C'	STM FF/79.05 STM FF/79.05	77.20 76.94	-	
SEE DETAIL DWG. GD1		BLDG 'D'	STM FF/78.50	76.94		
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9 <sup>-1</sup> 8.00 + + 78.34		BLDG 'A' BLDG 'B' BLDG 'C'	SA1 SA4 SA5	SAN.         4           SAN.         19           SAN.         7		
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78.22		CB11 CBMH12	CBMH12 ST8	STM 62 STM 38		
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ine Chain Link Fence 0.131 EAST (5R-6884 & Set)						
12. NEW WATERMAIN SHALL BE CHLORINATED AND FULLY TESTED PRIOR TO CONNECTION TO MUNICIPAL SYSTEM	4. ALL MANHOLES, AND CATCH BASINS TO BE BACKFILLED WITH MIN. 0.3m HORIZ. THICKNESS OF SAND OR APPROVED BACKFILL.		I.C.D. T			
MUNICIPAL SYSTEM. 13. WATER VALVES TO BE OPERATED BY CITY OFFICIAL ONLY.	5. SANITARY SEWER AND STORM SEWER PIPING SHALL BE AS NOTED IN PIPING SCHEDULE ON	MANHOLE NO.		NING m)	I.C.D. TYPE	
14. CONNECTION/TAPPING OF EXISTING WATERMAIN TO BE DONE LIVE; 48 HOURS NOTICE MUST BE PROVIDED TO AFFECTED RESIDENTS PRIOR TO WATER SHUT DOWN.	DWG. SS-1. 6. FRAMES AND COVERS FOR MANHOLES AND CATCH BASINS ARE AS NOTED IN MANHOLE SCHEDULE ON DWG SS-1	СВМН #5	1	41	PLATE	
15. CONNECTION OF WATER SERVICES AND HYDRANT LEADS TO EXISTING MAIN BY CITY	SCHEDULE ON DWG. SS-1. 7. FOR PIPE COVER OF 1.8m AND LESS, INSTALL INSULATION AS PER INSULATION DETAIL ON DRAWING CD1	СВМН #12	1	22	PLATE	
FORCES. EXCAVATION, BACKFILLING AND REINSTATEMENT BY CONTRACTOR. 16. VALVE AND BOX FOR NEW WATER SERVICE CONNECTION TO BE LOCATED 0.30 m FROM	DRAWING GD1. 8. NEW MH/CB/CBMH STRUCTURES SHALL HAVE PREFORMED OPENINGS WITH GASKETED CONNECTIONS AND EXTERNALLY SEALED AND					
PROPERTY LINE BASED ON NEW ROAD WIDENING. NOTES: SEWER	CONNECTIONS AND EXTERNALLY SEALED AND WATERTIGHT. 9. CONTRACTOR TO CONFIRM ELEVATION OF EXISTING STORM AND SANITARY SEWERS AT					
1. MANHOLES AND CATCH BASINS SHALL BE AS NOTED IN MANHOLE SCHEDULE ON DWG. SS—1. STORM MANHOLES TO HAVE 0.3m SUMPS. CATCH BASINS AND CATCH BASIN MANHOLES TO HAVE	EXISTING STORM AND SANITARY SEWERS AT PROPOSED CONNECTION POINTS AND REPORT ANY DISCREPANCIES TO THE ENGINEER BEFORE COMMENCING ANY WORK.					
0.6m SUMPS 2. SEWER TRENCH AS PER CITY OF OTTAWA DETAIL S6. GRANULAR 'A' BEDDING TO BE COMPACTED TO	10. CONNECTION OF SEWERS FROM MAIN TO PROPERTY LINE IS TO BE INSPECTED BY CITY OFFICIAL PRIOR TO BACKFILLING.					
097 MAYIMUM DDY DENSITY						

98% MAXIMUM DRY DENSITY. 3. ALL WORK SHALL BE PERFORMED, AS APPLICABLE IN ACCORDANCE WITH 0.P.S.S. 407,

AND 410.

11. CONTRACTOR TO PROVIDE CCTV INSPECTION OF SANITARY SEWER AND STORM SEWER INSTALLATIONS.

WATE			
	SURFACE ELEV.	TOP OF WM ELEV.	NOTES
<u>B. C</u>	78.17 <u>+</u> 78.00 78.40 79.00	75.60 <u>+</u> 75.60 76.00 76.00	200x200mm CUT—IN TEE EX. 229mm SANITARY SEWER CROSSING INV. 74.4± VALVE AND VALVE BOX CAP WITHIN 1.0m OF BUILDING WALL
	77.66 <u>+</u> 77.58 77.82 77.90	75.20 <u>+</u> 75.10 75.40 75.40	200x150mm TAPPING VALVE AND SLEEVE EX. 229mm SANITARY SEWER CROSSING INV. 74.2± VALVE AND VALVE BOX CAP WITHIN 1.0m OF BUILDING WALL

ITA	TARY AND STORM MAINTENANCE HOLE SCHEDULE										
YPE	T/G	DOWNSTREAM	UPSTREAM	UPSTREAM	UPSTREAM	DETAI	L No.	COMMENT			
		INVERT	INVERT #1	INVERT #2	INVERT #3	STRUCTURE	GRATE				
SAN	78.81	76.46	76.52	-	-	701.010	401.030	OPSD			
SAN	78.70	76.21	76.27	-	_	701.010	S19.1				
SAN	78.70	75.96	75.97	-	-	701.010	S19.1				
SAN	78.60	75.64	75.67	76.20(S)	-	701.010	S19.1				
SAN	78.23	75.36	75.39	75.95(W)	-	701.010	S24	SOLID			
SAN	77.58	74.22(EX.)	74.74	-	75.95	—	_	TEE CONNECTION			
SAN	FF/79.05	76.60	_	_	_	_	_				
SAN	, FF/79.05	76.58	_	-	_	_	_				
SAN	, FF/79.05		_	-	_	_	_				
SAN	FF/78.50		-	-	-	-	_				
STM	78.70	77.15	_	-	_	705.010	S19.1				
STM	78.60	76.99	77.00	_	_	701.010	S19.1				
STM	78.72	76.86	76.95(E)	76.92(N)	_	701.010	S24	PERFORATED			
STM	78.60	76.74	77.40(N)	76.77(E)	_	M4 (M-CON)	S19.1	REFER TO NOTE 1			
STM	78.92	76.67	76.69		-	STC 2000	EMBOSSED	STORMCEPTOR			
STM	78.57	76.61	76.64(N)	76.64(E)	-	701.010	S24	PERFORATED			
STM	78.35	76.47	76.52	_		—	_	TEE CONNECTION			
	78.60	77 15				705.010	S10 1				
STM	78.60	77.15	-	-	_	705.010	S19.1				
STM	78.60	77.02	77.08	_	_	701.010	S19.1				
STM	78.76	77.31	_	-	-	701.010	S24	SOLID			
STM	78.80	76.82	77.02(W)	76.90(E)	77.05(S)	701.010	S24	SOLID			
STM	78.19	76.65	76.68(S)	76.85(W)	76.91(E)	701.010	S24	PERFORATED			
STM	77.66	76.58	76.59	-	-	701.010	S19.1				
STM	77.69	76.52	76.55	-	-	STC 2000	EMBOSSED	STORMCEPTOR			
STM	77.82	76.33±	76.36	-	-			TEE CONNECTION			
STM	78.60	77.30	-	-	_	705.010	S19.1				
STM	78.55	77.03	77.09	-	-	701.010	S19.1				
STM	78.20	76.82	-	-	_	705.010	S19.1				
STM	77.65	77.24	-	-	-	705.030	403.010	GRATE TO MATCH SLOPE			
STM	77.85	76.85	-	-	-	705.030	403.010	GRATE TO MATCH SLOPE			
STM	FF/79.05	77.55	_	-	-	-	-				
STM	FF/79.05	77.20	-	-	-	-	-				
STM	FF/79.05	76.94	-	-	-	-	-				
STM		76.94	-	-	-	-	-				

SANITARY AND STORM PIPING SCHEDULE										
ТО	SEWER TYPE	LENGTH (m)	DIA. (mm)	MATERIAL	CLASS	SLOPE (%)	COMMENT			
SA2 SA3 SA4 SA5	SAN. SAN. SAN. SAN.	30 36 45 38	150 200 200 200	P.V.C. P.V.C. P.V.C. P.V.C.	SDR28 SDR28 SDR28 SDR28	0.65 0.65 0.65 0.65				
EX. SEWER SA1 SA4 SA5 SA5	SAN. SAN. SAN. SAN. SAN.	31 4 19 7 5	200 150 150 150 150	P.V.C. P.V.C. P.V.C. P.V.C. P.V.C.	SDR28 SDR28 SDR28 SDR28 SDR28	2.00 2.00 2.00 2.00 2.00	CAP WITHIN 1.0m OF BUILDING WALL CAP WITHIN 1.0m OF BUILDING WALL CAP WITHIN 1.0m OF BUILDING WALL CAP WITHIN 1.0m OF BUILDING WALL			
CBMH2 ST14 CBMH5 ST15 ST6 EX. SEWER	STM STM STM STM STM STM	43 13 27 13 6 26	300 300 300 300 300 300	P.V.C. P.V.C. P.V.C. P.V.C. P.V.C. P.V.C.	SDR35 SDR35 SDR35 SDR35 SDR35 SDR35 SDR35	0.34 0.34 0.35 0.35 0.35 0.38				
ST6 CBMH4 ST14	STM STM STM	63 18 30	300 300 300	P.V.C. P.V.C. P.V.C.	SDR35 SDR35 SDR35	0.34 0.34 0.34				
ST8 ST9 CBMH10 ST16 EX. SEWER	STM STM STM STM STM	84 39 13 3 22	300 375 375 375 375 375	P.V.C. P.V.C. P.V.C. P.V.C. P.V.C.	SDR35 SDR35 SDR35 SDR35 SDR35 SDR35	0.34 0.36 0.44 0.90 0.75				
CBMH12 ST8	STM STM	62 38	300 300	P.V.C. P.V.C.	SDR35 SDR35	0.34 0.34				
TEE	STM	21	300	P.V.C.	SDR35	0.34				
TEE	STM	81	300	P.V.C.	SDR35	0.34				
CBMH5 ST8 ST9 ST9	STM STM STM STM	15 15 9 3	200 150 200 150	P.V.C. P.V.C. P.V.C. P.V.C.	SDR28 SDR28 SDR28 SDR28	1.00 1.00 1.00 1.00	CAP WITHIN 1.0m OF BUILDING WALL CAP WITHIN 1.0m OF BUILDING WALL CAP WITHIN 1.0m OF BUILDING WALL CAP WITHIN 1.0m OF BUILDING WALL			

SCALE 1:300

JOB No. SO1229EOA

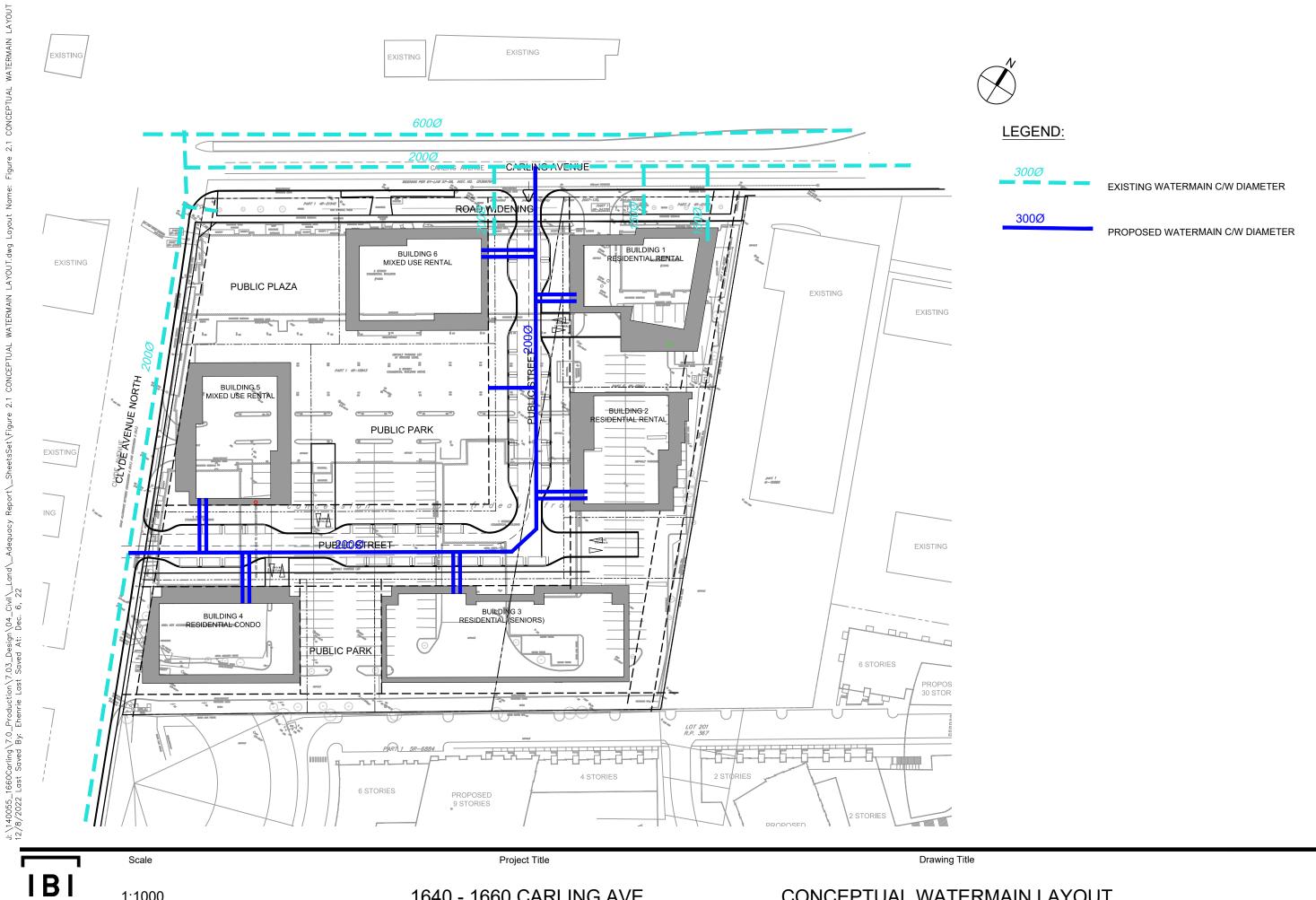
FILE NAME CTC290-AUG-15-2006.DWG PLOT DATE AUGUST-2006

I.C.	.D. TABLE	
	OPENING (mm)	I.C.D. TYPE
	141	PLATE
	122	PLATE

	Num In Internet	SWIZER SERV
7]	WELLESLEY CARLING	
		COMMANY
		LAROSE WOODW
		CHATELAIN LEDIGE
	LEGEND PROPOSED SANITARY S PROPOSED STORM SEW PROPOSED WATERMANN	
	PROPOSED WATERMAIN     PROPOSED CURB     PROPOSED SWALE c/w     PERFORATED PIPE	200mm
	PROPOSED DITCH INLE	
	PROPOSED CATCHBASIN MAINTENANCE HOLE     PROPOSED CATCH BAS     PROPOSED SANITARY M	IN
	HOLE FH PROPOSED FIRE HYDRA VB PROPOSED WATER VALV	NT
	VALVE BOX× 78.45PROPOSED ELEVATION78.30PROPOSED TOP OF CO ELEVATION	
	X TG=78.55 PROPOSED TOP OF GR ELEVATION PROPOSED RETAINING Y	
	PROPOSED HANDRAIL    4.0%    OVERLAND FLOW DIRECT    UILDING ENTRANCE	TION
	100 RETURN PERIOD - YI	TARS
	ZIO 62 - VOLUME - m3 MAXIMUM PONDING DEPTH -	mm
	<u>NOTES:</u> 1. INSTALL SLUICE GATE ON NORTH CBMH5. MEDIUM DUTY ARMTEC DELU	
	20–10C; 203mm DIA. WITH EXTEND NON–PROJECTING STEM (GALV. ASTM AND T–WRENCH HANDLE (GALV. AST M–CON TYPE M–4 BOX MH WITH FL	ED   A123) M A123).
	TOP SLAB TO 78.37 MAX. TO ALLOW INSTALLATION OF VALVE OPERATOR. V OPERATOR AS PER OPSD 1101.020.	1
È.		
	Delca	
	SEPT 22 06       4       REVISED PER CITY       COMMENT         AUG 23 06       3       ISSUED FOR 3RD SUBMISSION         JUNE 8 06       2       RE-SUBMISSION	
	DEC 21 05 1 ISSUED FOR SITE PLAN AGE DATE REV. DESCRIPTION REVISION RECORD	REEMENT DRY
	TURNER FLEISC Architects inc.	HER
	67 Lesmill Road Toronto, Ontario M3B 2T8	}
	Tel: 416-425-2222 Fax: 416-425-6717	TEAL
		TFAI
	OTTAWA	
	STORE No.	
	STAMP STAMP	Grégoire
		OF ONTARIO
	CANADIAN TIRE REAL ESTATE	S AND BE
	RESPONSIBLE FOR SAME REPORTING ANY DISCREPANCIE COMMENCING WORK. LATEST APPROVED DRAWING ONLY TO BE USED FOR CO PRINTS ARE NOT TO BE SCALED. PROJECT	ONSTRUCTION,
	1650–1660 CARLING AVE CLYDE AVENUE OTTAWA C	NUE + NTARIO
	drawing title SITE SERVICING	drawing no.

## **APPENDIX B**

- Reserved for Water Model and Boundary Conditions
- Watermain Demand Calculation Sheet
- FUS Fire Flow Requirement Calculation



## 1640 - 1660 CARLING AVE

## CONCEPTUAL WATERMAIN LAYOUT

Sheet No.



## FIGURE 2.1

	IBI GROUP	WATERMA	N DEMAND CALCULATION SHEET		
· _ ·	333 PRESTON STREET			FILE:	140055
IRI	OTTAWA, ON	PROJECT :	1660 Carling Avenue	DATE PRINTED:	08-Dec-22
	K1S 5N4	LOCATION :	CITY OF OTTAWA	DESIGN:	AB
		DEVELOPER :	Hobin Architecture Inc	PAGE :	1 OF 1

	RESIDENTIAL UNITS		NON-RESIDENTIAL				MAXIMUM DAILY DEMAND (I/s)				FIRE						
NODE				POP'N	INDTRL		INST.		DEMAND (I/s)					DEMAND (l/s)			DEMAND
	3 BDRM	2 BDRM	1 BDRM		(ha.)	(ha.)	(ha.)	Res.	Non-res.	Total	Res.	Non-res.	Total	Res.	Non-res.	Total	(l/min)
1660 Carling Ave		523	1192	2,767		0.67		8.97	0.39	9.36	22.42	0.58	23.00	49.32	1.05	50.37	
TOTALS		523	1192	2,767		0.67				9.36			23.00			50.37	

ASSUMPTIONS										
RESIDENTIAL DENSITIES	AVG. DAILY DEMAND		MAX. HOURLY DEMAND							
- 3 Bedroom Unit (BDRM)	3.1 p / p / u - Residential	<u>280</u> I / cap / day	- Residential	<u>1,540</u> I / cap / day						
	- ICI	<u>50,000</u> I / ha / day	- ICI	<u>135,000</u> I / ha / day						
- 2 Bedroom Unit (BDRM)	<u>2.1</u> p/p/u									
			FIRE FLOW							
- 1 Bedroom Unit (BDRM)	<u>1.4</u> p/p/u MAX. DAILY DEMAND		- SF, SD, TH & ST	<u>10,000</u> I / min						
	- Residential	<u>700</u> I / cap / day		l / min						
-Other	<u>66</u> u / p / ha - ICI	<u>75,000</u> I / ha / day	- ICI	<u>13,000</u> I / min						

#### Fire Flow Requirement from Fire Underwriters Survey

### 1660 Carling Avenue - Building 1 (RioCan 209 Units)

Building Floor	<u>Area</u>			
	W	vidth	40.00 m	
	d	lepth	28.21 m	
	S	tories	22	
Т	otal Effectiv	e Area	5,642.0 m <sup>2</sup>	
F = 220C√A				
С	0.8		C =	1.5 wood frame
А	5,642 n	n <sup>2</sup>		1.0 ordinary
				0.8 non-combustile
F	13,220 l/	min		0.6 fire-resistive
use	13,000 l/	min		
Occupancy A	diustment			-25% non-combustile
<u>eccupancy ne</u>	ajaoanona			-15% limited combustile
Use		0%		0% combustile
••••		• • • •		+15% free burning
Adjustment		0	l/min	+25% rapid burning
Fire flow		13,000	l/min	
<u>Sprinkler Adju</u>	<u>istment</u>			
Use		-30%		
Adjustment		-3900	l/min	
-				

#### Exposure Adjustment

Building	Separation	Adjace	Exposure		
Face	(m)	Length	Stories	L*H Factor	Charge *
north	0.00	0.00	0	0	0%
east	24.00	28.21	22	621	4%
south	15.00	36.04	22	793	8%
west	26.00	28.21	1	28	4%
Total					16%
Adjustment			2,080	l/min	
			(1,820)		
Total adjust	ments				
Fire flow			11,180	l/min	
Use			11,000	l/min	
			183.3	l/s	

\* Total Effective Area Calculated with Part 2.2.A From Water Supply For Public Protection in Canada 2020

\*\* Exposure charges from Water Supply For Public Protection in Canada 2020 Techinical Bulletin ISTB 2021-03

#### 1660 Carling Avenue - Building 2 (RioCan 284 units)

Building Floo	r Area				
		width	34	.9 m	
		depth	32	.0 m	
		stories	-	30	
_					
1	otal Effect	ive Area	5,580.	0 m-	
F = 220C√A					
С	0.8		С	=	1.5 wood frame
А	5,580	m <sup>2</sup>			1.0 ordinary
<i>/ / / / / / / / / /</i>	0,000				0.8 non-combustile
F	13,147	l/min			0.6 fire-resistive
-					0.0 me-resistive
use	13,000	i/min			
Occupancy A	djustment				-25% non-combustile
					-15% limited combustile
Use		-15%	)		0% combustile
					+15% free burning
Adjustment		-1950	) I/min		+25% rapid burning
Fire flow		11,050			
The new		11,000	1/11111		
<u>Sprinkler Adj</u>	<u>ustment</u>				
Use		-30%	)		
Adjustment		-3315	5 l/min		

#### Exposure Adjustment

Building	Separation	Adjac	Exposure			
Face	(m)	Length	Charge *			
north	15.0	36.0	22	793	8%	
east	21.4	36.0	1	36	0%	
south	21.3	14.2	9	128	4%	
west	0.0	0.0	0	0	0%	
Total					12%	
Adjustment			1,326	l/min		
Total adjust	ments		(1,989)	l/min		
Fire flow			9,061	l/min		
Use			9,000	l/min		
			150.0	l/s		

\* Total Effective Area Calculated with Part 2.2.A From Water Supply For Public Protection in Canada 2020

#### 1660 Carling Avenue - Building 3 (RioCan 187 units)

Building Floor	Area		
	width	70.0 m	
	depth	28.5 m	
	stories	9	
Т	otal Effective Area	9,970.7 m <sup>2</sup>	2
F = 220C√A			
С	0.8	C =	1.5 wood frame
А	9,971 m <sup>2</sup>		1.0 ordinary
			0.8 non-combustile
F	17,574 l/min		0.6 fire-resistive
use	18,000 l/min		
Occupancy A	<u>djustment</u>		-25% non-combustile
			-15% limited combustile
Use	-1	15%	0% combustile
			+15% free burning
Adjustment		2700 l/min	+25% rapid burning
Fire flow	15,3	300 l/min	
<u>Sprinkler Adju</u>	<u>istment</u>		
Use	-:	30%	
Adjustment	-4	590 l/min	

#### Exposure Adjustment

Building	Separation	Adjac	Exposure		
Face	(m)	Length	Stories	L*H Factor	Charge *
north	21.3	14.2	9	128	4%
east	0.0	0.0	0	0	0%
south	24.3	70.0	9	630	4%
west	24.0	28.5	9	257	4%
Total					12%
Adjustment			1,836	l/min	
Total adjust	ments		(2,754)	l/min	
Fire flow			12,546	l/min	
Use			13,000	l/min	
			216.7	l/s	

\* Total Effective Area Calculated with Part 2.2.A From Water Supply For Public Protection in Canada 2020

#### 1660 Carling Avenue - Building 4 (RioCan 220 units)

Building Floor Area			
	width	46.53 m	
	depth	28.50 m	
	stories	20	
Total F	ffective Area	6,630.5 m <sup>2</sup>	
rotar E		0,000.0	
F = 220C√A			
С	0.8	C =	1.5 wood frame
A 6,0	631 m <sup>2</sup>		1.0 ordinary
			0.8 non-combustile
F 14,5	331 l/min		0.6 fire-resistive
use 14,	000 l/min		
Occupancy Adjustn	nent		-25% non-combustile
			-15% limited combustile
Use	-15%		0% combustile
			+15% free burning
Adjustment	-2100 l/	/min	+25% rapid burning
Fire flow	11,900 l	/min	
Sprinkler Adjustmer	nt		
	_		
Use	-30%		
Adjustment	-3570 l/	/min	

#### Exposure Adjustment

Building	Separation	Adjac	Exposure		
Face	(m)	Length	Charge *		
		_		-	
north	24.00	34.00	20	680	4%
east	24.00	28.50	9	257	4%
south	0.00	0.00	0	0	0%
west	0.00	0.00	0	0	0%
Total					8%
Adjustment			952	l/min	
Total adjust	ments		(2,618)	l/min	
Fire flow			9,282	l/min	
Use			9,000	l/min	
			150.0	l/s	

\* Total Effective Area Calculated with Part 2.2.A From Water Supply For Public Protection in Canada 2020

#### 1660 Carling Avenue - Building 5 (RioCan 394 units)

Building Floor	Area			
-		width	34.00 m	
		depth	42.00 m	
		stories	37	
Т	otal Effect	ive Area	7,140.0 m <sup>2</sup>	
F = 220C√A				
С	0.8		C =	1.5 wood frame
А	7,140	m <sup>2</sup>		1.0 ordinary
	,			0.8 non-combustile
F	14,872	l/min		0.6 fire-resistive
use	15,000	l/min		
Occupancy A	<u>djustment</u>			-25% non-combustile
				-15% limited combustile
Use		0%		0% combustile
				+15% free burning
Adjustment		0	l/min	+25% rapid burning
Fire flow		15,000	l/min	
<u>Sprinkler Adju</u>	<u>ustment</u>			
Use		-30%		
Adjustment		-4500	l/min	

#### Exposure Adjustment

Building	Separation	Adjac	Exposure				
Face	(m)	Length	Charge *				
north	0.00	0.00	0	0	0%		
east	0.00	0.00	0	0	0%		
south	24.00	34.00	20	680	4%		
west	28.24	6.64	2	13	0%		
Total					4%		
Adjustment			600	l/min			
Total adjust	l/min						
Fire flow			11,100	l/min			
Use			11,000	l/min			
			183.3	l/s			

\* Total Effective Area Calculated with Part 2.2.A From Water Supply For Public Protection in Canada 2020

#### 1660 Carling Avenue - Building 6 (RioCan 416 units)

Building Flo	or Area			
		width	40.0 m	
		depth	30.0 m	
		stories	40	
	Total Effect	ive Area	6,000.0 m <sup>2</sup>	
F = 220C√A	L .			
С	0.8		C =	1.5 wood frame
А	6,000	m <sup>2</sup>		1.0 ordinary
				0.8 non-combustile
F	13,633	l/min		0.6 fire-resistive
use	14,000	l/min		
<u>Occupancy</u>	<u>Adjustment</u>			-25% non-combustile
				-15% limited combustile
Use		0%		0% combustile
				+15% free burning
Adjustment			l/min	+25% rapid burning
Fire flow		14,000	l/min	
Sprinkler Ac	ljustment			
Use		-30%		
Adjustment		-4200	l/min	

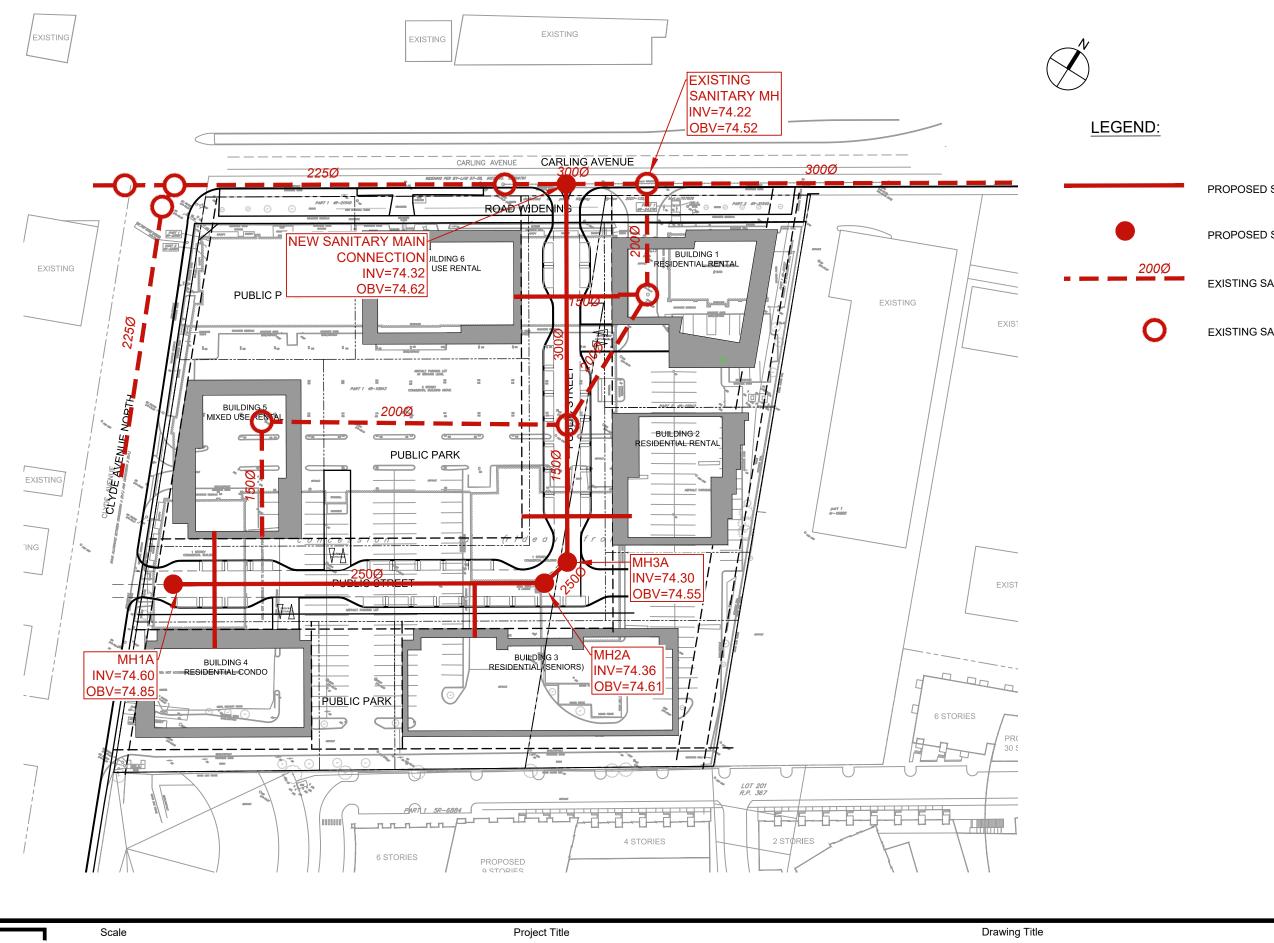
#### Exposure Adjustment

Building	Separation	Adjace	Exposure					
Face	(m)	Length	Charge *					
		-		-				
north	0.0	0.0	0	0	0%			
east	0.0	0.0	0	0	0%			
south	0.0	0.0	0	0	0%			
west	24.0	28.2	22	620	4%			
Total					4%			
Adjustment			560	l/min				
Total adjust	tal adjustments (3,640) I/min							
Fire flow			10,360	l/min				
Use			10,000	l/min				
			166.7	l/s				

\* Total Effective Area Calculated with Part 2.2.A From Water Supply For Public Protection in Canada 2020

# **APPENDIX C**

- Figure 3.1 1660 Carling Ave Sanitary Sewer Layout
- 1660 Carling Ave Sanitary Sewer Design Sheet
- Figure 3.2 1660 Carling Ave Sanitary Drainage Area Plan
- City of Ottawa Correspondence Regarding Offsite capacity
- Excerpt from Delcan Sanitary Sewer Design Sheet



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# 1640 - 1660 CARLING AVE

# CONCEPTUAL SANITARY SEWER LAYOUT

PROPOSED SANITARY SEWERS

PROPOSED SANITARY MANHOLE

EXISTING SANITARY SEWERS

EXISTING SANITARY MANHOLE

Sheet No.

# FIGURE 3.1



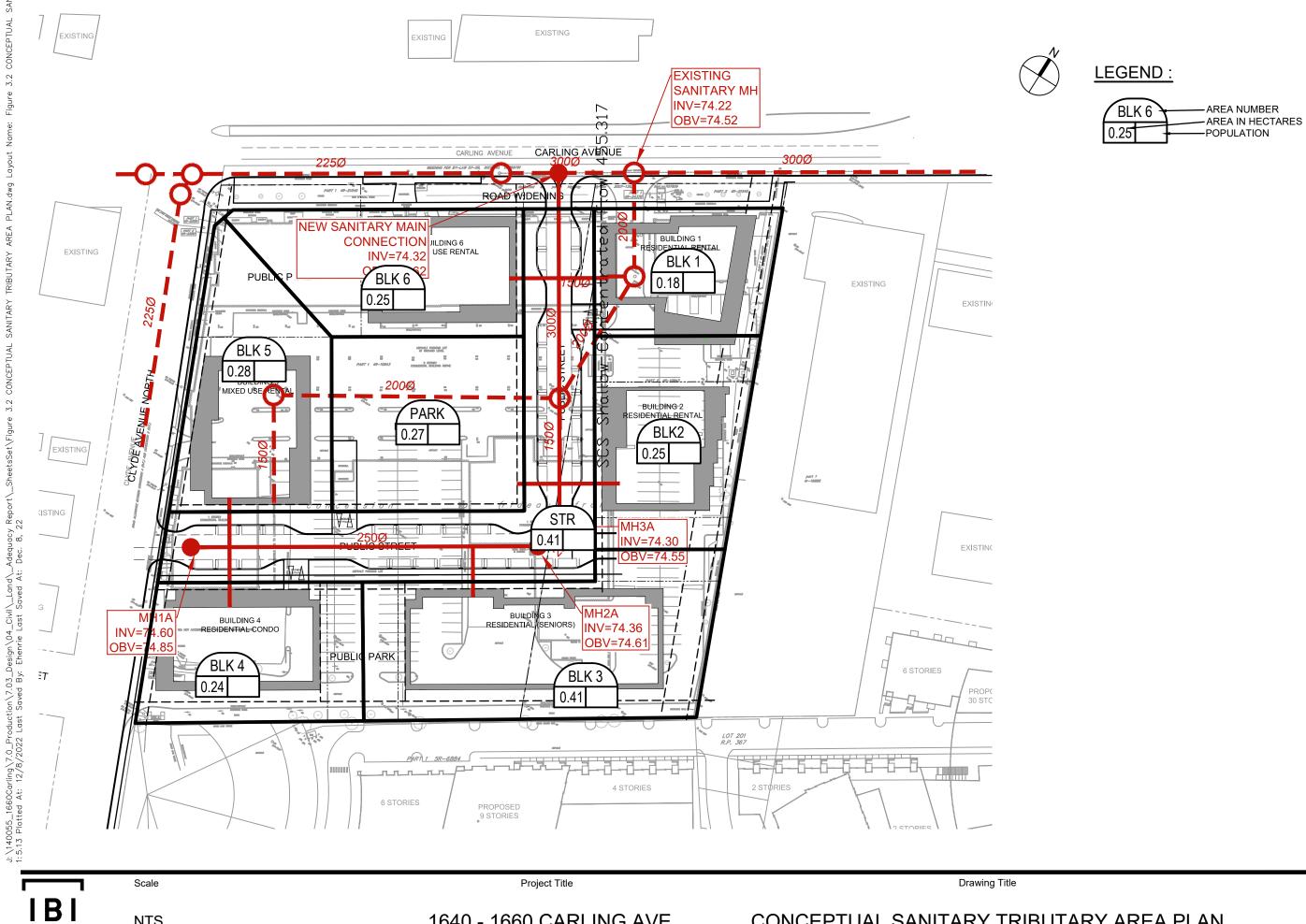
#### IBI GROUP

400-333 Preston Street Ottawa, Ontario K1S 5N4 Canada tel 613 225 1311 fax 613 225 9868 ibigroup.com

	LOCATIO			1				RESIDE	ENTIAL								ICI A	AREAS				INFILTE	RATION ALL	OWANCE			TOTAL			PROPO	SED SEWE	R DESIGN		
	LUCATIO	N		AREA		UNIT	TYPES		AREA	POPU	ILATION	RES	PEAK			ARE	A (Ha)			ICI	PEAK	ARE	A (Ha)	FLOW	FIXED	LOW (L/s)	FLOW	CAPACITY	LENGTH	DIA	SLOPE	VELOCITY	AVA	ILABLE
STREET	AREA ID	FROM	то	w/ Units	SF	TH/SD	1 Bed	2 Bed	w/o Units	1115	0.04	PEAK	FLOW	INSTIT	UTIONAL	COMM	ERCIAL	INDU	STRIAL	PEAK	FLOW		CUM	(1.1-)		CUM	(L/s)	(1.1-)	()	(	(0/)	(full)	CAF	PACITY
SIREEI	AREA ID	мн	МН	(Ha)	5F	TH/SD	APT	APT	(Ha)	IND	CUM	FACTOR	(L/s)	IND	CUM	IND	CUM	IND	CUM	FACTOR	(L/s)	IND	COM	(L/s)	IND	COM	(L/S)	(L/s)	(m)	(mm)	(%)	(m/s)	L/s	(%)
																													0.00	0	0.00			
Carling Avenue																													0.00		0.00			
		212.0.1																									100					0.07/		70.000/
		BLDG 4	1A	0.24			120	100		378.0	378.0	3.43	4.20	0.00	0.0	0.00	0.00	0.00	0.0	1.00	0.00	0.24	0.24	0.08	0.00	0.0	4.28	15.89	15.00	150	1.00	0.871	11.61	73.08%
		BLDG 5	1A	<b>0</b> .44			260	134		645.4	645.4	3.33	6.97	0.00	0.0	0.28	0.28	0.00	0.0	1.50	0.14	0.28	0.28	0.09	0.00	0.0	7.20	34.22	15.00	200	1.00	1.055	27.02	78.97%
		BLDG 3	1A	0.41			187			261.8	261.8	3.48	2.95	0.00	0.0	0.00	0.00	0.00	0.0	1.00	0.00	0.41	0.41	0.14	0.00	0.0	3.09	15.89	15.00	150	1.00	0.871	12.80	80.55%
Street 1		1A	2A						0.41	24.6	1309.8	3.18	13.49	0.00	0.0	0.00	0.28	0.00	0.0	1.50	0.14	0.41	1.34	0.44	0.00	0.0	14.06	31.02	98.20	250	0.25	0.612	16.96	54.66%
Street 1		2A	3A							0.0	1309.8	3.18	13.49	0.00	0.0	0.00	0.28	0.00	0.0	1.50	0.14	0.00	1.34	0.44	0.00	0.0	14.06	31.02	8.25	250	0.25	0.612	16.96	54.66%
		BLDG 2	3A	0.25	-		200	84	-	456.4	456.4	3.40	5.02	0.00	0.0	0.00	0.00	0.00	0.0	1.00	0.00	0.25	0.25	0.08	0.00	0.0	5.10	34.22	15.00	200	1.00	1.055	29.11	85.08%
		BLDG 1	3A	0.18			150	64		344.4	344.4	3.44	3.84	0.00	0.0	0.00	0.00	0.00	0.0	1.00	0.00	0.18	0.18	0.06	0.00	0.0	3.90	15.89	15.00	150	1.00	0.871	11.99	75.45%
		BLDG 6	3A				275	141		681.1	681.1	3.32	7.33	0.00	0.0	0.25	0.25	0.00	0.0		0.12	0.25	0.25	0.08	0.00	0.0	7.53	34.22	15.00	200	1.00	1.055	26.68	77.98%
Street 1		3A	EX. MAIN		-				0.27	16.2	2807.9	2.97	27.06	0.00	0.0	0.00	0.53	0.00	0.0	1.50	0.26	0.27	2.29	0.76	0.00	0.0	28.07	45.12	100.00	300	0.20	0.618	17.05	37.78%
Carling Avenue		EX MAIN	EX MH							0.0	2807.9	2.97	27.06	0.00	0.0	0.00	0.53	0.00	0.0	1.50	0.26	0.00	2.29	0.76	0.00	0.0	28.07	45.12	22.00	300	0.20	0.618	17.05	37.78%
									1																									
Design Parameters:				Notes: 1. Mannings	anofficient	(m) =		0.013				Designed:		RM			No.					Deel		Revision on with City fo	an Demoning							Date 2022-11-15		
Residential		ICI Areas		2. Demand (				0.013 ) L/day	200	L/day							1.					Dial	it - Coordinat	On with City It	or Rezoning							2022-11-15		
SF 3.4 p/p/u		ICI Aleas		3. Infiltration				L/s/Ha	200	L/uay		Checked:		RM																				
TH/SD 2.7 p/p/u	INST 28	,000 L/Ha/day		<ol> <li>4. Residentia</li> </ol>			0.55	L/3/11a				oneckeu.																						
1 Bed 1.4 p/p/u		,000 L/Ha/day					(14/(4+(P/100	00)^0.5))0.8																										
2 Bed 2.1 p/p/u		,000 L/Ha/day	MOE Chart			0.8 Correcti		,,,				Dwg. Refe	rence:	140055			1																	
Other 60 p/p/Ha		000 L/Ha/day					k Factors bas	ed on total	area,								F	ile Referen	e:						Date:							Sheet No:		
		,				0%, otherwi			,			1						140055-6.04							2022-11-1	5						1 of 1		

#### SANITARY SEWER DESIGN SHEET

DRAFT - 1660 Carling Avenue CITY OF OTTAWA Hobin Architecture Inc.



NTS

CEPTUAL

CON

1640 - 1660 CARLING AVE

CONCEPTUAL SANITARY TRIBUTARY AREA PLAN

Sheet No.

# FIGURE 3.2

From:	Tousignant, Eric <eric.tousignant@ottawa.ca></eric.tousignant@ottawa.ca>
Sent:	Monday, December 5, 2022 3:06 PM
То:	Ryan Magladry
Cc:	Arthur Beresniewicz; Fawzi, Mohammed
Subject:	RE: PC2022-0215 - 1640/1660 Carling Avenue - Follow-up

\*\*\* Exercise caution. This is an EXTERNAL email. DO NOT open attachments or click links from unknown senders or unexpected email. \*\*\*

Goof Afternoon Ryan

The Carling sanitary sewer is due for replacement next year. We will be upsizing it to account for future development.

Regards

Eric

From: Ryan Magladry <<u>rmagladry@IBIGroup.com</u>>
Sent: December 05, 2022 1:58 PM
To: Tousignant, Eric <<u>Eric.Tousignant@ottawa.ca</u>>
Cc: Arthur Beresniewicz <<u>arthur.beresniewicz@ibigroup.com</u>>; Tousignant, Eric
<<u>Eric.Tousignant@ottawa.ca</u>>; Fawzi, Mohammed <<u>mohammed.fawzi@ottawa.ca</u>>
Subject: Re: PC2022-0215 - 1640/1660 Carling Avenue - Follow-up

CAUTION: This email originated from an External Sender. Please do not click links or open attachments unless you recognize the source.

ATTENTION : Ce courriel provient d'un expéditeur externe. Ne cliquez sur aucun lien et n'ouvrez pas de pièce jointe, excepté si vous connaissez l'expéditeur.

Good afternoon Eric and Mohammed,

Quickly touching base to see if you were able to confirm that the Carling Avenue sani upgrades are able to accommodate the rezoning of the 1660 Carling Site (Canadian Tire).

Thanks,

Ryan Magladry CET

Project Manager

Suite 500, 333 Preston Street

Ottawa ON K1S 5N4 Canada

tel 1 613 225 1311 cell 1 613 795 5610

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NOTE: Ce courriel peut contenir de l'information privilégiée et confidentielle. Si vous avez recu ce message par erreur, veuillez le mentionner immédiatement à l'expéditeur et effacer ce courriel.

From: Ryan Magladry <rmagladry@IBIGroup.com>
Sent: Thursday, November 17, 2022 10:47 AM
To: Fawzi, Mohammed <mohammed.fawzi@ottawa.ca>
Cc: Arthur Beresniewicz <arthur.beresniewicz@ibigroup.com>; Tousignant, Eric
<Eric.Tousignant@ottawa.ca>
Subject: Re: PC2022-0215 - 1640/1660 Carling Avenue - Follow-up

Hi Mohammed,

Attached is our current storm layout, showing existing and proposed. We would likely add offline potential U/G storage to this sketch prior to wrapping up our report.

The storm sewer on Carling is very shallow. It will likely require insulated pipes between Building 1 & 6, until we can get the grade up to provide adequate cover.

Let us know if there is anything else.

Ryan Magladry CET

**Project Manager** 

Suite 500, 333 Preston Street

Ottawa ON K1S 5N4 Canada

tel 1 613 225 1311 cell 1 613 795 5610



IBI Group is now proudly a part of Arcadis.

Canadian Tire - Carling Ave and Clyde Ave City of Ottawa

Manning's "n" = 0.013

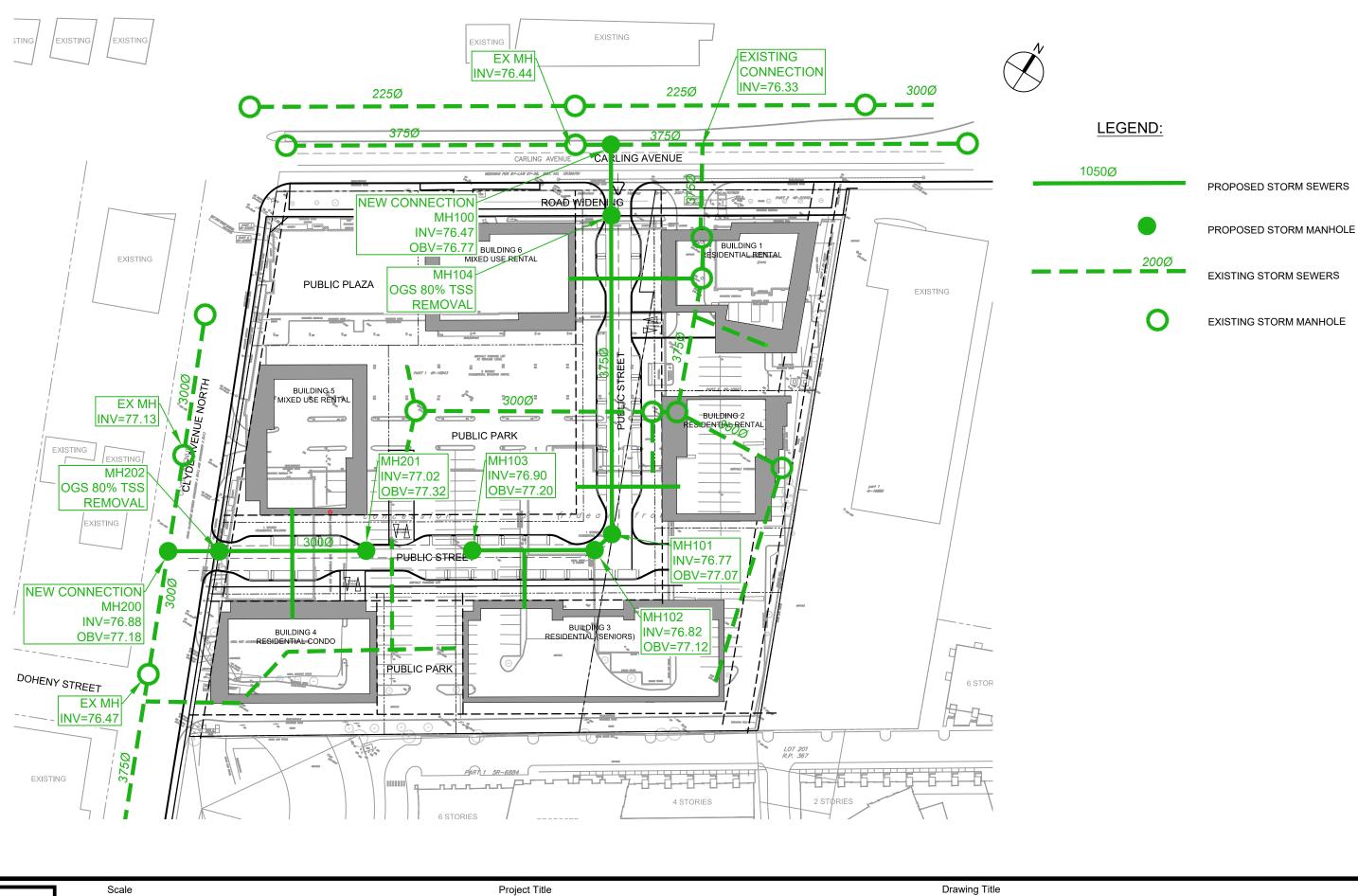
Sanitary Sewer

Junction	Losses
Angle	Drop
Degree	m
0	0.01
45	0.03
90	0.06

Loc	ation	D	esign Flo	w	1	P	ipe Selec	tion	1	Profile										
From	і То	Bidg Incr.	Parking Incr.	Cum	D	So	Capacity	Velocity	Length	Surface U/S	Surface D/S	Invert U/S	Invert D/S	Junctior Angle	Bend Loss	Depth o D/S	of Cover Okay			
MH	MH	L/s	L/s	L/s	mm	%	L/s	m/s	m	m	m	m	m	degree	m	m				
	ng Av		utlet - 22				invert app		2 m	E5 63		52 23	721.022	*1	10110001	a 58	1265			
A	1	2.1		2.1	150	2.00	21.5	1.22	4	78.83	78.81	76.60	76.52	90	0.06	2.14	Yes			
1	2			2.1	200	0.65	26.4	0.84	30	78.81	78.70	76.46	76.27	90	0.06	2.24	Yes			
2	3		0.5	2.6	200	0.65	26.4	0.84	36	78.70	78.70	76.21	75.97	0	0.01	2.53	Yes			
3	4		0.5	3.1	200	0.65	26.4	0.84	45	78.70	78.60	75.96	75.67	45	0.03	2.73	Yes			
4	5	3.4	105727	6.5	200	0.65	26.4	0.84	38	78.60	78.23	75.64	75.39	45	0.03	2.64	Yes			
5	6	7.6		14.1	200	2.00	46.3	1.47	31	78.23	77.58	75.36	74.74	90	0.06	2.64	Yes			

# **APPENDIX D**

- Figure 4.1 1660 Carling Ave Storm Sewer Layout
- 1660 Carling Ave Storm Design Sheet
- Figure 4.2 1660 Carling Ave Storm Drainage Area Plan
- Excerpt from Delcan Stormwater Management Report
- Excerpt from Delcan Storm Sewer Design Sheet



B NTS

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): \140055\_1660Carling\ 2/8/2022 Last Saved

# 1640 - 1660 CARLING AVE

# CONCEPTUAL STORM SEWER LAYOUT

Sheet No.

# FIGURE 4.1

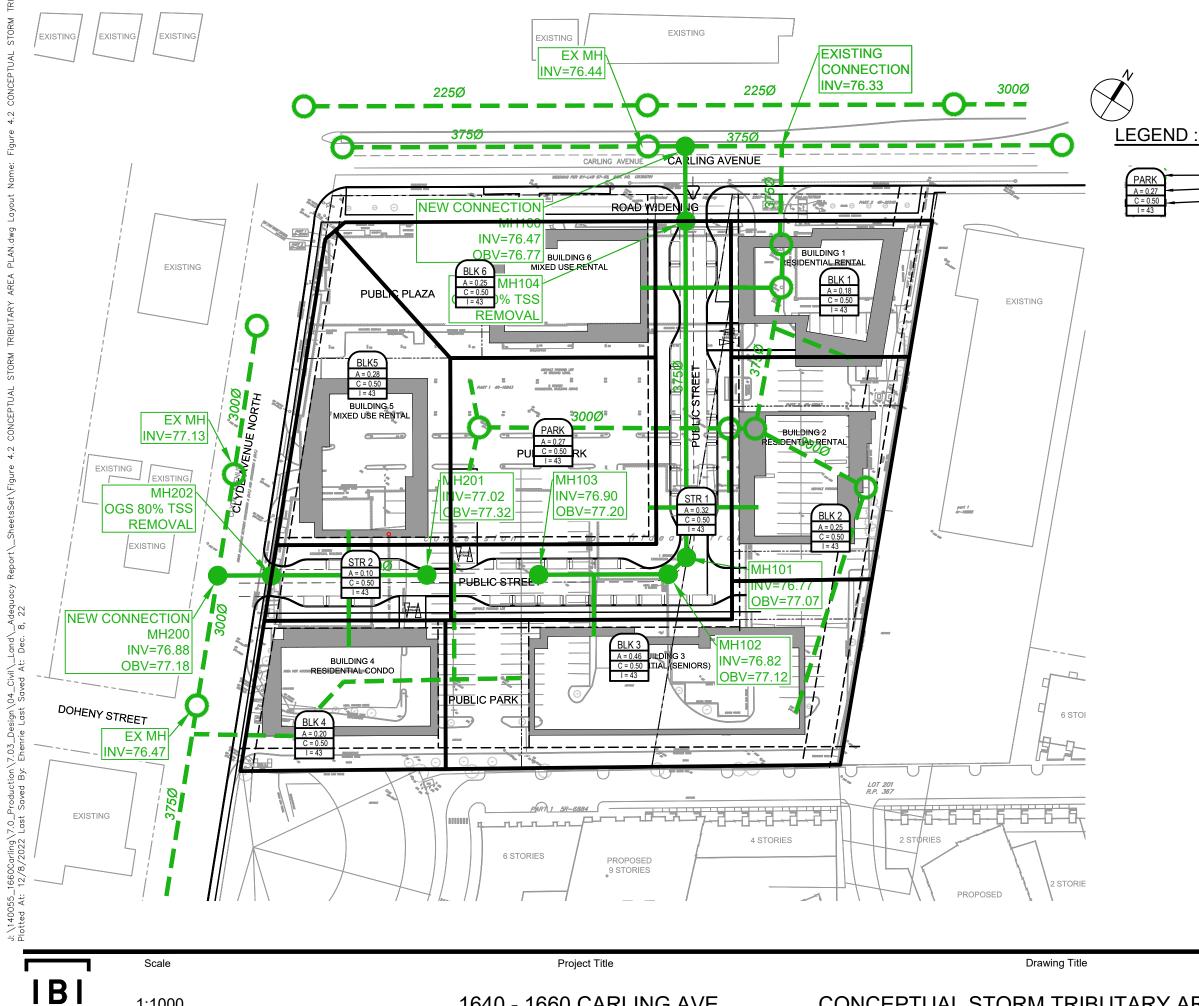
## I B I

IBI GROUP 500-333 Preston Street Ottawa, Ontario K1S 5N4 Canada tel 613 225 1311 fax 613 225 9868 ibigroup.com

LOCATION AREA (Ha) RATIO												NAL DESIG	NELOW							SEWER DATA												
070557	AREA ID		C= C= C=	C= C= C=	- C=	C= C=	C=	IND	CUM I	INLET	TIME	TOTAL	i (2)	i (5)	i (10)			5yr PEAK	10yr PEAK	100yr PEAK	FIXED	FLOW	DESIGN	CAPACITY	LENGTH	1	PIPE SIZE			VELOCITY	AVAIL C	AP (2yr)
STREET	AREA ID	FROM TO	0.20 0.25 0.40	0.50 0.57 0.65	5 0.69	0.70 0.76	0.80	2.78AC	2.78AC	(min)	IN PIPE	(min)			(mm/hr)					) FLÓW (L/s)		CUM	FLOW (L/s)	(L/s)	(m)	DIA	W	Ì Н	(%)	(m/s)	(L/s)	
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Street No. 1 (W) Street No. 1 (W)	Building 4 Building 5	BLDG 4 MAIN 20 BLDG 5 MAIN 20	)	0.20					0.28 0.39		0.47	11.90 12.37	71.75 70.22	97.24 95.14	113.95 111.49			27.03 37.03	31.68 43.39	46.30 63.40	0.00	0.00	19.95 27.33	17.11 17.11					0.25	0.528	-2.84 -10.22	-16.58% -59.75%
	Bulluling 5	BLDG J WIAIN 20		0.20				0.59	0.39	11.90	0.47	12.37	10.22	95.14	111.45	102.91	21.33	37.03	43.39	03.40	0.00	0.00	21.55	17.11	13.00	200			0.25	0.320	-10.22	-39.1370
Street No. 1 (W)		MH 201 MH 200		0.10				0.14	0.81	11.90	1.33	13.23	70.22	95.14	111.49	162.91	56.61	76.71	89.88	131.34	0.00	0.00	56.61	50.44	55.31	300			0.25	0.691	-6.17	-12.23%
Clyde Avenue North		MH 200 EX MH						0.00	0.81	13.23	0.42	13.65	66.29	89.75	105.14	153.59	53.44	72.36	84.76	123.83	0.00	0.00	53.44	100.88	34.85	300			1.00	1.383	47.44	47.02%
							_																							Ļ]		<b>├</b> ────
Street No. 1 (E)	Building 1	BLDG 1 MAIN 10		0.18				0.25	0.25	10.00	0.47	10.47	76.81	104.19	122.14	178.56	19.22	26.07	30.56	44.68	0.00	0.00	19.22	17.11	15.00	200			0.25	0.528	-2.11	-12.32%
Street No. 1 (E)	Building 2	BLDG 1 MAIN 10 BLDG 2 MAIN 10		0.18						10.00	0.47	10.47	75.03	104.19	122.14	176.56	26.07	35.36	41.45	60.58	0.00	0.00	26.07	17.11	15.00	200			0.25	0.528	-2.11	-12.32%
Street No. 1 (E)	Building 3	BLDG 3 MAIN 10		0.46						10.95	0.47	11.42	73.35	99.44	116.54			63.58	74.52	108.91	0.00	0.00	46.90	17.11	15.00				0.25	0.528	-29.79	-174.13%
Street No. 1 (E)	Building 6	BLDG 6 MAIN 10	)	0.25						12.37	0.47	12.84	68.76	93.15	109.14			32.37	37.92	55.41	0.00	0.00	23.90	17.11	15.00	200			0.25	0.528	-6.79	-39.67%
Street No. 1 (E)	Public Park	PARK MAIN 10	)	0.27	_	<u> </u>		0.38	0.38	0.00	0.47	0.47	167.22	230.48	271.61	398.62	62.76	86.50	101.93	149.60	0.00	0.00	62.76	17.11	15.00	200		_	0.25	0.528	-45.65	-266.83%
Street No. 1 (E)		MH 103 MH 102			-	<u>                                      </u>	+	0.00	0.64	13.65	0.71	14.36	65.15	88.19	103.30	150.90	41.66	56.39	66.05	96.48	0.00	0.00	41.66	91.46	34.25	375			0.25	0.802	49.80	54.45%
Street No. 1 (E) Street No. 1 (E)		MH 103 MH 102 MH 102 MH 101			-	+ +	+ 1			14.36	0.71	14.36	63.32	85.68	103.30			56.39	64.16	96.48	0.00	0.00	41.66	91.46		375			0.25	0.802	49.80	54.45%
Street No. 1 (E)		MH 101 MH 100		0.32						14.50	2.26	16.76	62.98	85.22	99.80	145.76		204.92	239.99	350.50	0.00	0.00	151.44	91.46	108.75				0.25	0.802	-59.99	-65.59%
Carling Ave		MH 100 EX MH						0.00	2.40	16.76	0.48	17.23	57.91	78.28	91.64	133.79	139.25	188.24	220.38	321.72	0.00	0.00	139.25	101.84	25.60	375			0.31	0.893	-37.41	-36.74%
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Definitions:			Notes:						De	signed:		AB				No.				-	(1 0 ···	Revi								Date		
Q = 2.78CiA, where: Q = Peak Flow in Litre	s per Second (L/e)		<ol> <li>Mannings coefficier</li> </ol>	lannings coefficient (n) = 0.013												1.				Dra	att - Coordina	ition with Ci	ty for Rezonin	g				+-		2022-11-15		
A = Area in Hectares (									Ch	ecked:		RM																				
i = Rainfall intensity in		(mm/hr)														-												-				
[i = 732.951 / (TC+6	.199)^0.810]	2 YEAR																														
[i = 998.071 / (TC+6		5 YEAR	1						Dw	vg. Referer	nce:	140055										Observiti										
[i = 1174.184 / (TC+ [i = 1735.688 / (TC+		10 YEAR 100 YEAR															File Reference: 140055-6.04.04															
[i - 1/30.000/(1C+	0.014/0.020]	IUU TEAR	L														14005	3-0.04.04	2022-11-15 1						1011							

#### STORM SEWER DESIGN SHEET

DRAFT - 1660 Carling Avenue CITY OF OTTAWA RioCan



# 1640 - 1660 CARLING AVE

# CONCEPTUAL STORM TRIBUTARY AREA PLAN

AREA NUMBER
AREA IN HECTARES
RUNOFF COEFFICIENT

Sheet No.

# FIGURE 4.2

# 3 PROPOSED DEVELOPMENT

The proposed development consists of retail stores fronting Carling Avenue and Clyde Avenue with a vehicle service centre within the property. The building along Carling Avenue has a second storey that extends southward with ground level parking underneath. The overall development has a gross floor area of 13,068 m<sup>2</sup> and a lot coverage of 9,855 m<sup>2</sup>. The layout includes an at grade loading dock adjacent to the vehicle service centre. The rooftop of the buildings along Clyde Avenue will be used for an outdoor garden centre and roof top storage of storm runoff within the garden centre is not appropriate. The remaining buildings will use control flow roof drains with associated ponding/storage during rainfall events.

The non-building areas will be mostly paved parking with a landscape strip along the south and east sides of the site. On the Carling Avenue and Clyde Avenue frontages there are both hard and soft landscaping areas.

The existing grading along Carling Avenue, Clyde Avenue, and the south boundary will be maintained. The area in front of the buildings along Carling Avenue will continue to drain to the street. A swale will be constructed along the south slope and runoff will be captured by ditch inlets that outlet to the site drainage system. A retaining wall with a maximum height of 1.2 m will be constructed along the east property line. This retaining wall essentially replaces the existing retaining wall within the site and facilitates the overall grading and servicing.

The site will be serviced by a new storm sewer system, sanitary sewer and watermain. The proposed servicing and grading of the site are illustrated on Drawings SS-1 and GD-1. Copies of these drawings are appended to this report.

## 4 STORM WATER MANAGEMENT AND DRAINAGE

## 4.1 DESIGN CRITERIA

The storm water management requirements are identified in the City of Ottawa Sewer Design Guidelines as follows:

- allowable peak flow to the City storm sewer based on a 5 year event; Tc = 20 min; C = 0.5
- 100 year runoff to be stored on site and discharge at allowable peak flow
- 5 year rainfall intensity: i = 998 / (t + 6.053)<sup>0.814</sup>
- 100 year rainfall intensity: i = 1736 / (t + 6.014)<sup>0.820</sup>

## 4.2 ALLOWABLE DISCHARGE

The Rational method was used to calculate the allowable discharge from the site:

- Area = 2.41 ha
- Runoff coefficient = 0.5
- Tc = 20 min
- 5 year rainfall intensity = 70.2 mm/h
- Allowable discharge = 235 L/s

## 4.3 STORM DRAINAGE SYSTEM

A storm sewer system has been designed to provide drainage for the proposed development. Due to the size and depth of the existing municipal sewers it is not possible to outlet the entire site to the existing storm sewer on Carling Avenue or Clyde Avenue. The storm drainage system has been designed with two outlets – one to Clyde Avenue at the southwest corner of the site and one to Carling Avenue near the northeast corner of the site. The Clyde Avenue outlet drains the southwest portion of the site and the garden centre located on the roof of the building along Clyde Avenue.



	Canadian Tire - Carling Ave and Clyde Ave City of Ottawa Event - yr a b c																									
Maa									vent - yr		b	C												Junction	Losses	
wan	ning's	u ≔		0.013		=	a/(Td +	b)^c	5	998	6.05	0.814												Angle	Drop	
																								Degree	m	
Stor		wer Des	ion Cal	loulatio																				0	0.01	
Ever		Nel Des	ign cai 5	Year	JAS																			45	0.03	
2001			5	1941																				90	0.06	
Loc	Location Drainage Area Runoff Contolled Runoff											Ĩ		Pine	Selectio	n .		i i			Pro	filo				
From	To I	ID	Area	C	AC	Cum	Тс	1	Q	СВ	Roof	Cum	D	So	Capacity			Travel	Surface	Surface	Invert	Invert	Junction	Bend	Depth (	of Cover
	0.00					AC				Incr.	Incr.		-			, electri	Longai	Time	U/S	D/S	U/S	D/S	Angle	Loss	D/S	Okay
MH	MH		ha				mīn.	mm/h	m³/s	m³/s	m³/s	m³/s	mm	%	m³/s	m/s	m	mîn	m	m	m	m	degree	m	m	0,10,7
Carl	ing Av	venue ou	itlet - 3	81 mm	etorm	COWOT	invert	200503	76 22	l_																
0.000					storm	30401	I	appioz	. 70.00	Ë –			1													
7	8	C1	0.00	0.00	0.00	0.00	20.00	70.3	0.000	0.000	0.028	0.028	304	0.34	0.058	0.80	84	1.74	78.76	78.80	77.31	77.02	45	0.03	1.48	Yes
																0.00	01		10.10	10.00	11.01	11.02	40	0.00	1.40	103
11	12	11	0.18	0.86	0.15	0.15	20.00	70.3	0.030	0.020		0.020	304	0.34	0.058	0.80	62	1.29	78.60	78.55	77.30	77.09	90	0.06	1.16	Yes
												20														
17	Tee	9	0.03	0.20	0.01	0.01	20.00	70.3	0.001	0.001		0.001	304	0.34	0.058	0.80	81	1.68	77.65	78.67	77.24	76.96	90	0.06	1.40	Yes
12	8	12	0.20	0.81	0.16	0,32	21.29	67.6	0.060	0.020		0.041	304	0.34	0.058	0.80	38	0.79	78.55	78.80	77.03	76.90	90	0.06	1.60	Yes
10	-	10																								
13	Tee	13	0.10	0.71	0.07	0.07				0.013		0.013	304	0.34	0.058	0.80	21	0.44	78.20	78.46	76.82	76.75	90	0.06	1.41	Yes
8	9	В	0.00	0.00	0.00	0.39		66.0	0.071			0.090		0.36	0.110	0.96	39	0.68	78.80	78.19	76.82	76.68	45	0.03	1.13	Yes
9	10	C2 & D	0.00	0.00	0.00		22.75		0,070		0.018	0.108	381	0.44	0.121	1.06	13	0.20	78.19	77.66	76.65	76.59	0	0.01	0.69	No
10	16 Too	10		0.90	0.04				0.076			0.116		0.90	0.173	1.52	3	0.03	77.66	77.69	76.58	76.55	45	0.03	0.75	No

0.116 381 0.75 0.158 1.39 22

0.26 77.69 77.82 76.52 76.36

90

0.06

1.08 Yes

0.542 0.062 0.054 Note: C1 is 65% and C2 is 35% respectively of the the total controlled flow from Building C.

16 Tee --- 0.00 0.00 0.00 0.43 22.99 64.3 0.076

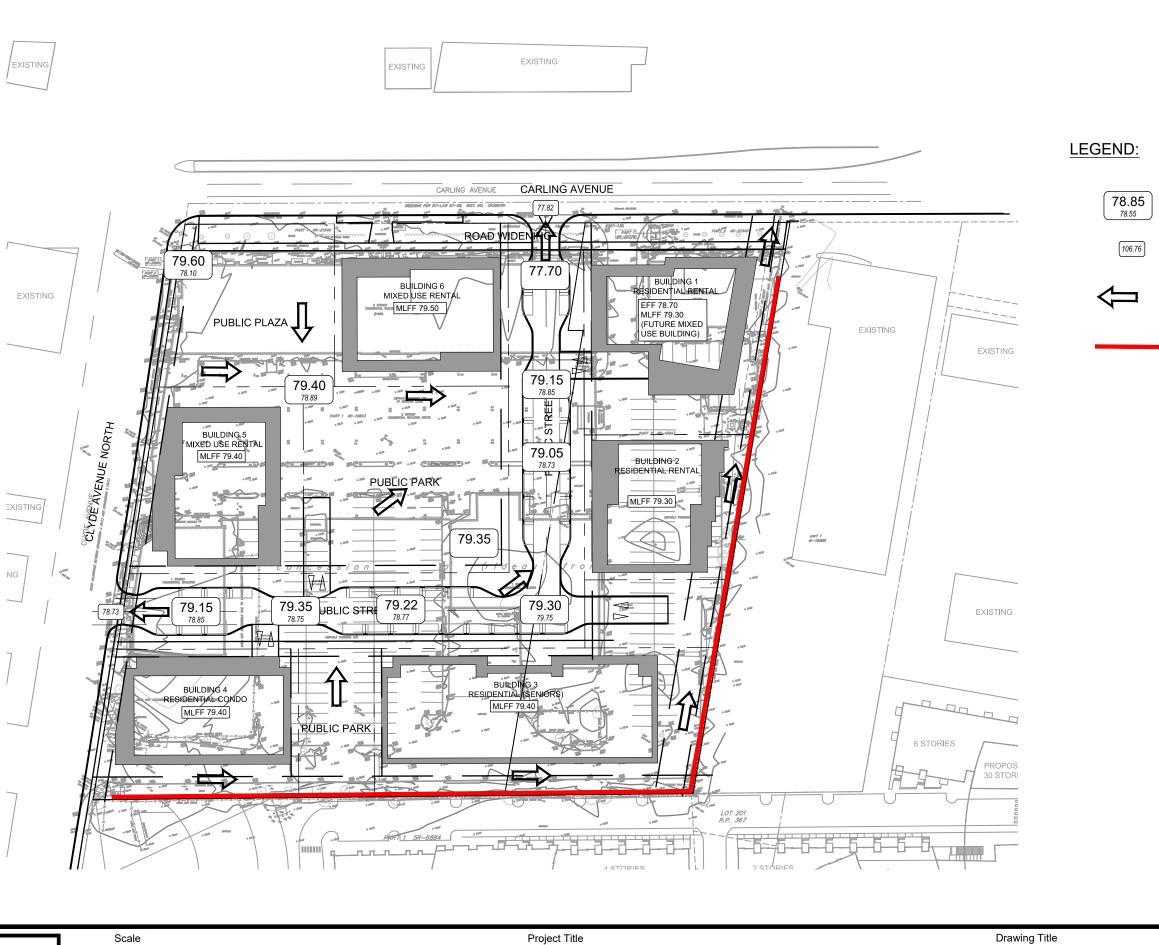
							Runof	ff	Cont	olled R	unoff	Ĩ.		Pipe	Selectio	n		Profile									
From	To	ID	Area	С	AC	Cum	Tc	1	Q	CB	Roof	Cum	D	So	Capacity	Velocity	Length	Travel	Surface	Surface	Invert	Invert	Junction	Bend	Depth o	of Cover	
						AC				Incr.	Incr.						0	Time	U/S	D/S	U/S	D/S	Angle	Loss	D/S	Okay	
MH	MH		ha				min.	mm/h	m³/s	m³/s	m³/s	m³/s	mm	%	m³/s	m/s	т	min	m	m	m	m	degree	m	m	,	
										0													3				
Clyde Avenue outlet - 381 mm storm sewer; inv							nvert approx. 76.47 m																				
1	2	1	0.12	0.90	0.11	0.11	20.00	70.3	0.021	0.007		0.007	304	0.34	0.058	0.80	43	0.89	78.70	78.60	77.15	77.00	0	0.01	1.30	Yes	
2	14	2	0.16	0.90	0.14	0.25	20.89	68.4	0.047	0.007		0.014	304	0.34	0.058	0,80	13	0.27	78.60	78.72	76.99	76.95	0	0.01	1.47	Yes	
_																											
3	4	3	0.11	0.90	0.10	0.10	20.00	70.3	0.019	0.007		0.007	304	0.34	0.058	0.80	18	0.37	78.60	78.60	77.15	77.08	90	0.06	1.21	Yes	
4	14	4	0.12	0.90	0.10	0.20	20.37	69.4	0.039	0.007		0.014	304	0.34	0.058	0.80	30	0.62	78.60	78.72	77.02	76.92	90	0.06	1.49	Yes	
14	5		0.00	0.00	0.00	0.45	21.16	67.8	0.085			0.028	304	0.34	0.058	0.80	27	0.56	78.72	78.60	76.86	76.77	45	0.03	1.53	Yes	
5	15	5&A	0.08	0.90	0.07	0.52	21.72	66.7	0.097	0.007	0.014	0.049	304	0.35	0.059	0.82	13	0.27	78.60	78.92	76.74	76.70	45	0.03	1.92	Yes	
15	6	3.000	0.00	0.00	0.00	0.52	21,99	66.2	0.096			0.049	304	0.35	0.059	0.82	6	0.12	78.92	78.57	76.67	76.64	45	0.03	1.62	Yes	
18	6	16	0.04	0.20	0.01		20.00			0.002		0.002	304	0.34	0.058	0.80	63	1.31	77.85	78.57	76.85	76.64	90	0.06	1.63	Yes	
6	Tee	1.000	0.00	0.00	0.00	0.52	22.11	65.9	0.096			0.051	304	0.38	0.062	0.85	26	0.51	78.57	78.35	76.61	76.52	90	0.06	1.53	Yes	

0.62

0.037 0.014

# **APPENDIX E**

- Figure 6.1 Macro Grading
- Figure 6.2 Erosion and Sediment Control Plan



Scale

ЯG

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# 1640 - 1660 CARLING AVE

# CONCEPTUAL MACRO GRADING



PROPOSED GRADE AND EXISTING GRADE

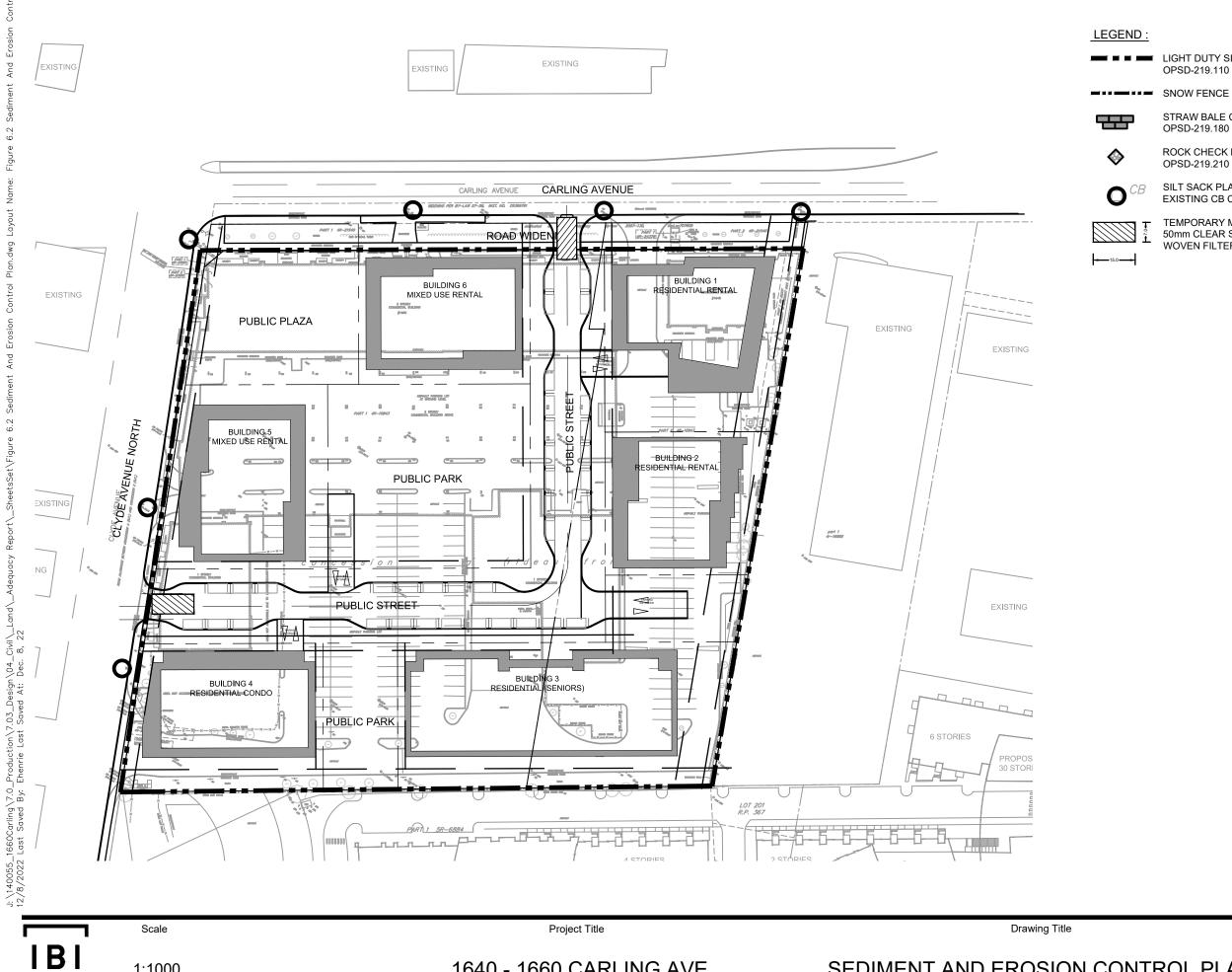
EXISTING EXISTING GRADE

PROPOSED MAJOR OVERLAND FLOW ROUTE

ANTICIPATED RETAINING WALL

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# FIGURE 6.1



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# 1640 - 1660 CARLING AVE

# SEDIMENT AND EROSION CONTROL PLAN

LIGHT DUTY SILT FENCE AS PER OPSD-219.110

STRAW BALE CHECK DAM AS PER OPSD-219.180

ROCK CHECK DAM AS PER OPSD-219.210

SILT SACK PLACED UNDER EXISTING CB COVER

TEMPORARY MUD MAT 0.15m THICK 50mm CLEAR STONE ON NON WOVEN FILTER CLOTH



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# FIGURE 6.2