



File: 37923 - 5.2.2

Design Brief Riverside Park 3930 and 3960 Riverside Drive

Development Application File No. **D**__-__-__-__



Prepared for St. Mary's Lands Corporation
by IBI Group
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1 Introduction

1.1 Scope

IBI Group has been retained by St. Mary's Lands Corporation to prepare the necessary engineering plans, specifications and documents to support the proposed concurrent vacant land condominium and re-zoning applications for the subject lands in accordance with the policies set out by the Planning and Development Branch of the City of Ottawa. This Brief will present a detailed servicing scheme to support development of the property, and will include sections on water supply, wastewater management, minor and major stormwater management along with erosion and sediment control.

1.2 Subject Site

Riverside Park (formerly known as the St. Mary's lands) is located at the northwest corner of the Riverside Drive and Hunt Club Road intersection. The Riverside Park development is approximately 6.0 hectares in size and is bounded by Hunt Club Road to the south, Riverside Drive to the east, City of Ottawa Uplands-Riverside park to the north and undeveloped environmental lands, adjacent to the Rideau River, to the west, as shown on Figure 1.

The Riverside Park vacant land condominium will consist of the creation of 4 developable blocks (or "units") along with a common access road. A current concept of the envisioned development is shown on Figure 2; however, as the blocks will be developed independently in the future through the site plan application process the ultimate development may differ from the shown concept.

1.3 Previous Studies

Design of this project has been undertaken in accordance with the following reports:

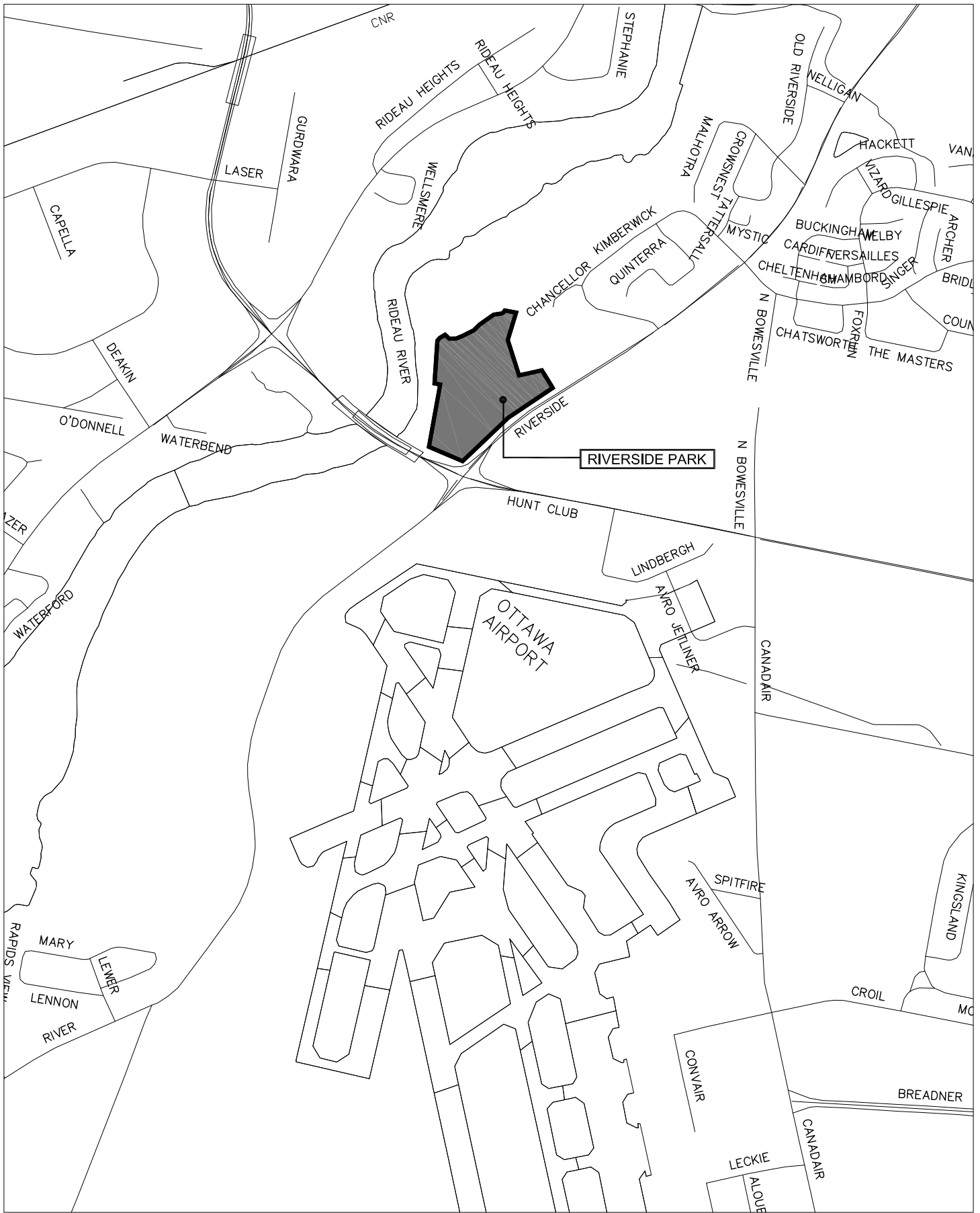
- Riverside Drive Land – Sanitary Sewer Servicing Study prepared by IBI Group, December 2007
- Riverside Drive Area – Brief in Support of Development of Lands Within the Riverside Drive Planning Area prepared by Cumming Cockburn & Associates Limited, May 1986
- Stormwater Management for Riverside Drive Lands prepared by Cumming Cockburn & Associates Limited, April 1987
- Riverwalk Park Stormwater Management Facility Update Stormwater Design Plan prepared by Novatech Engineering, June 1996

1.4 Geotechnical Considerations

The following are the most recent geotechnical investigation reports prepared by Golder Associates:

- Report No. 1670692-1000 March 2018
- Report No. 1670692-2000 March 2018

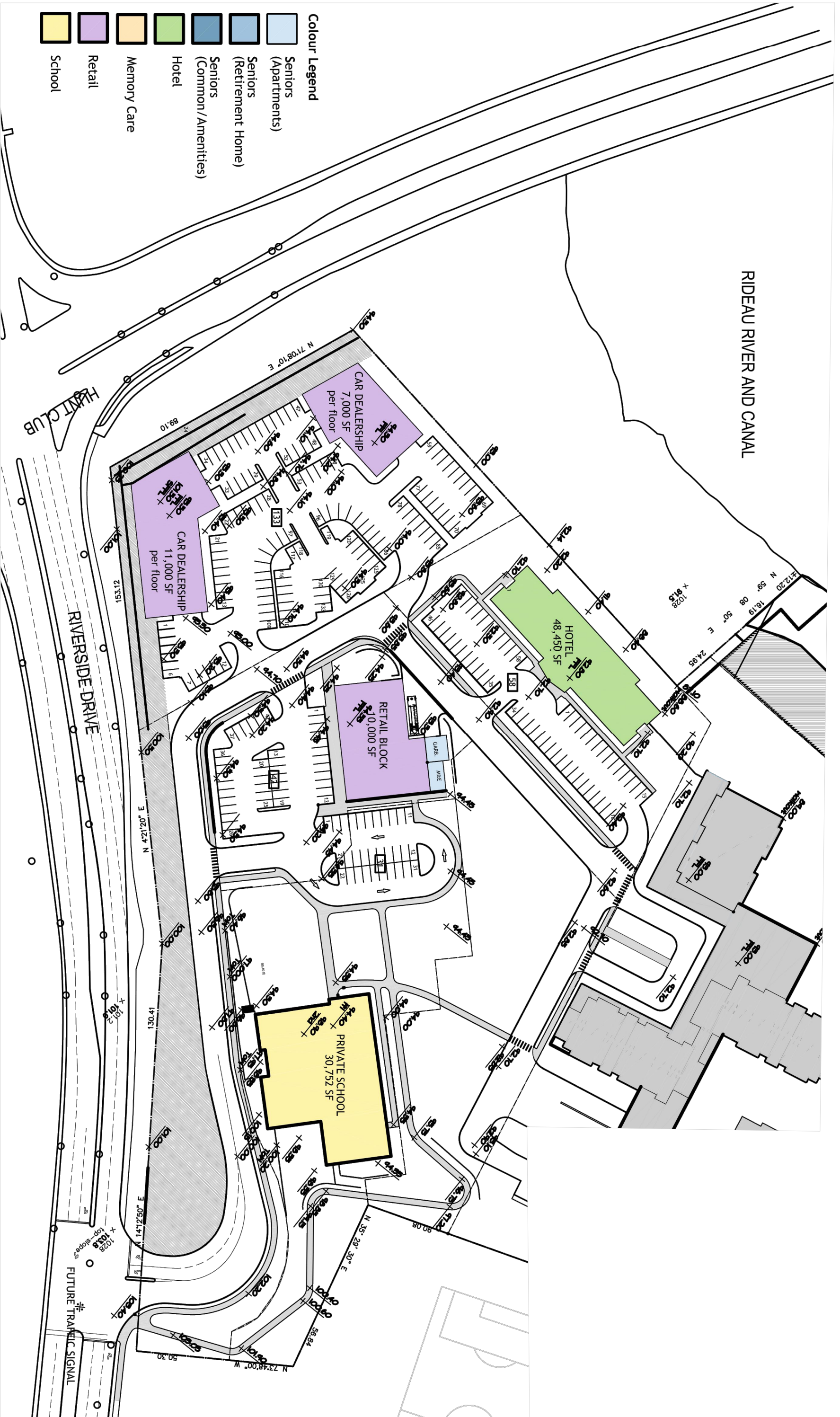
J:\37923-RiversideProperty\5.2 Reports\5.2.2 Civil\5.2.2.1 Sewers\Design Brief\1st Submission\Figures\Figure 1.dwg Layout Name: Layout1



Project Title
RIVERSIDE PARK
TAGGART REALTY MANAGEMENT

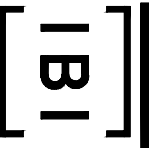
Drawing Title
KEY PLAN

Sheet No.
Fig 1



Colour Legend

Light Blue	Seniors (Apartments)
Medium Blue	Seniors (Retirement Home)
Dark Blue	Seniors (Common/Amenities)
Light Green	Hotel
Orange	Memory Care
Purple	Retail
Yellow	School



N.T.S.
Scale

Project Title
RIVERSIDE PARK
TAGGART REALTY MANAGEMENT

Drawing Title
CURRENT SITE PLAN

Sheet No.
FIG 2

The site slopes generally from Riverside Drive down towards the Rideau River in a rough South-East to North-West direction. The site transitions from an elevation of approximately 100m at the Riverside Drive and Hunt Club Road intersection down to 86m at the North-West limit of the developable lands. The site was previously used as a granular extraction site and has subsequently been filled to reclaim land for development purposes. Generally there is between 10m to 15m of fill across the site.

Among other items, the reports comment on the following:

- Site grading
- Pavement structure
- Infrastructure construction
- Design for earthquakes
- Environmental considerations
- Grade raise considerations

1.5 Pre-consultation

An engineering pre-consultation with the City was held in April 2017 regarding the proposed development. Notes from this meeting may be found in **Appendix E**. A subsequent pre-consult, concerned mainly with planning was then held on October 27, 2017.

It should be noted that pre-consultation with the Ministry of the Environment and Climate Change will be arranged imminently.

2 Water Supply

2.1 Existing Conditions

As previously noted, the six hectare Riverside Park site is located east of Riverside Drive and north of Hunt Club Road. An existing 406mm diameter watermain is located on Riverside Drive in pressure district **Zone 2C** which will provide the water supply to the site.

2.2 Design Criteria

2.2.1 Water Demands

Water demands have been calculated for the full development. Per unit population density and consumption rates are taken from Tables 4.1 and 4.2 at the Ottawa Design Guidelines – Water Distribution and are summarized as follows:

- Single Family 3.4 person per unit
- Townhouse and Semi-Detached 2.7 person per unit
- Average Apartment 1.8 person per unit
- Residential Average Day Demand 350 l/cap/day
- Residential Peak Daily Demand 875 l/cap/day
- Residential Peak Hour Demand 1,925 l/cap/day
- ICI Average Day Demand 28,000 l/gross ha/day
- ICI Peak Daily Demand 42,000 l/gross ha/day
- ICI Peak Hour Demand 75,600 l/gross ha/day

A watermain demand calculation sheet is included in **Appendix A** and the total water demands are summarized as follows:

- Average Day 3.37 l/s
- Maximum Day 7.75 l/s
- Peak Hour 16.65 l/s

2.2.2 System Pressure

The Ottawa Design Guidelines – Water Distribution (WDG001), July 2010, City of Ottawa, Clause 4.2.2 states that the preferred practice for design of a new distribution system is to have normal operating pressures range between 345 kPa (50 psi) and 552 kPa (80 psi) under maximum daily flow conditions. Other pressure criteria identified in Clause 4.2.2 of the guidelines are as follows:

- Minimum Pressure Minimum system pressure under peak hour demand conditions shall not be less than 276 kPa (40 psi)
- Fire Flow During the period of maximum day demand, the system pressure shall not be less than 140 kPa (20 psi) during a fire flow event.
- Maximum Pressure Maximum pressure at any point in the distribution system shall not exceed 689 kPa (100 psi). In accordance with the Ontario Building/Plumbing Code, the maximum pressure should not exceed 552 kPa (80 psi). Pressure reduction controls will be required for buildings where it is not possible/feasible to maintain the system pressure below 552 kPa.

2.2.3 Fire Flow Rates

The current Riverside Park concept contains a senior’s complex, a hotel and a mix of commercial and institutional land uses. Several calculations using the Fire Underwriting Survey (FUS) method were conducted to determine the fire flow requirement for the site. Results of the analysis provides a maximum fire flow rate of 9.000 l/min or 150 l/s is required which is used in the hydraulic analysis. A copy of the FUS calculations is included in **Appendix A**.

2.2.4 Boundary Conditions

The City of Ottawa has provided a hydraulic boundary condition at Riverside Drive where the connection to the site will occur. A copy of the boundary conditions is included in **Appendix A** and summarized as follows:

Table 2.1 Hydraulic Boundary Conditions at Riverside Park

	RIVERSIDE DRIVE.
Max HGL (Basic Day)	134.7 m
Min HGL (Peak Hour)	125.1 m
Max Day + Fire Flow (250 l/s Fire Flow)	126.2 m

2.2.5 Hydraulic Model

A computer model for the subject development has been developed using the H2O MAP Version 6.0 program produced by MWH Soft Inc. The model includes the existing watermain and boundary condition on Riverside Drive.

2.3 Proposed Water Plan

2.3.1 Modeling Results

The hydraulic model was run under basic day, maximum day with fire flows and under peak hour conditions. Water pipes are sized to provide sufficient pressure and to deliver the required fire flows. During the design stage all mains are tested at the minimum 150 mm diameter size, while the pressure criteria is met with the minimum sized mains the fire flow requirement is not achieved at all locations. The main sizes are increased in an iterative process until the fire flow results are sufficient.

Results of the hydraulic model are include in **Appendix A** and summarized as follows:

Scenario

Basic Day (Max HGL) Pressure Range	308.7 to 414.5 kPa
Peak Hour (Min HGL) Pressure Range	214.6 to 319.6 kPa
Max Day + 250 l/s Fire Flow Minimum Flow	170.0 l/s (10,200 l/min)

A comparison of the results and design criteria is summarized as follows:

Maximum Pressure	All nodes have basic day pressures under 552 kPa, therefore pressure reducing control is not required for this development.
Minimum Pressure	Based on the boundary condition provided by the City for minimum pressure, the peak hour pressure at Riverside Drive is less than 276 kPa. As the elevation of the site is lower than Riverside Drive, the minimum required pressure is exceeded at nodes J6 to J9, any connection between nodes J3 and J6 may require a booster pump to meet the minimum requirement.
Fire Flow	The FUS fire demand of 150 l/s is met at all fire nodes.

2.3.2 Watermain Layout

In order to provide additional reliability to the system in case of a watermain break on Riverside Drive, there are two connections proposed to the existing watermain with an isolation valve added between the connections. All watermains are 250mm diameter as required to meet the fire flow criteria.

3 WASTEWATER DISPOSAL

3.1 Existing Conditions

In 1987 the J. Perez Corporation development, known as Riverwalk Park, included a 525 mm diameter sanitary sewer extension to the southern limits of its development and was designed to service the urban area between Riverside Drive and the Rideau River north and south of Hunt Club Road. This sewer currently terminates at the north limit of the existing City of Ottawa Uplands-Riverside Park. For reference, the original Riverwalk Park sanitary sewer design sheet and Drainage Area Plan #3675-501A are included in **Appendix B**. At its current terminus, the existing 525Ø sewer has a spare capacity of at least 108.6 l/s based on now outdated City of Ottawa design guidelines.

Subsequent to the 1987 Riverwalk Park development, the City of Ottawa commissioned a report, completed by IBI Group, to review the sanitary sewer requirements in the Riverside Drive corridor. In November 2007 the Riverside Drive Lands Sanitary Sewer Servicing Study (2007 report) was completed. For reference, excerpts from this 2007 study are also included in **Appendix B**. That study identified a total of 26.45 ha of developable property south of Chancellor Court and west of Riverside Drive. The developable properties and flow estimates from the 2007 report were:

Table 3.1 RIVERSIDE DRIVE LANDS – OWNERSHIP AND AREAS

PROPERTY	AREA (HA)		FLOW (L/S)
	GROSS (HA)	DEVELOPABLE (HA)	
Taggart Realty (St. Mary's Site)	8.58	6.35	7.29
Transport Canada	3.65	0.00	0.00
Dymon Management Ltd.	8.69	6.29	7.22
City of Ottawa/Airport Authority	34.96	13.81	15.85
TOTAL	55.88	26.45	30.36

These estimates are based on now superseded City of Ottawa flow criteria, namely an average commercial flow rate of 50,000 l/s/ha peaked at 1.5 and an infiltration allowance of 0.28l/s/ha. For reference the sanitary sewer spreadsheet from the 2007 report, as well as Figure 5 Sanitary Drainage Area Plan are included in **Appendix B**.

Because the total estimated sanitary flow from tributary areas south of Riverside Park (formerly known as the St. Mary's site) is only 30.36 l/s which is significantly less than the available capacity of 108.6 l/s, the November 2007 report further demonstrated that, theoretically, additional external lands (+/- 65 Ha) upstream of the City of Ottawa/Airport Authority property could also develop as commercial/employment uses and outlet to the study sewer.

3.2 Design Criteria

The sanitary sewers for the subject site will be based on the City of Ottawa design criteria. It should be noted that the sanitary sewer design for this study incorporates the latest City of Ottawa design parameters identified in Technical Bulletin ISTB-2018-01. Some of the key criteria will include the following:

- Commercial/Institutional flow 28,000 l/ha/d
- Residential per capital 280 l/person/d
- Harmon – correction factor $K=0.8$
- Peaking factor 1.5 if ICI in contributing area >20%
1.0 if ICI in contributing area <20%
- Infiltration allowance 0.33 l/s/ha
- Velocities 0.60 m/s min. to 3.0 m/s max.

3.3 Recommended Wastewater Plan

The Riverside Park development calls for the construction of a private road and services that will service 4 blocks. The blocks will ultimately be developed at a later date via individual Site Plan Applications.

Sanitary service for the subject site will be provided via an extension of the sanitary sewer from the City of Ottawa Uplands-Riverside Park. Development of the site must also provide a corridor to accommodate the extension of the 450 mm diameter sanitary sewer to Hunt Club Road, where it can ultimately be extended from the subject site's southern property limit under the Hunt Club bridge to service development lands south of Hunt Club Road. The alignment and associated connection of the proposed sanitary sewer extension is shown on drawing 37923-C-001.

The 2007 City of Ottawa report estimated that the peaked flow from the Riverside Park site would be approximately 7.29 l/s. The current Sanitary Sewer Design Sheet, found in **Appendix B** is based on the current site concept, shown in Figure 2, and includes employment and residential uses with a total flow of 10.16 l/s, calculated using criteria identified in section 3.2.

The flows have been calculated using a conceptual plan, as such we expect that the sanitary flows will be re-calculated at the time of site plan and shall be compared to the remaining residual capacity at the downstream outlet.

Given that there is significant residual capacity at the proposed sanitary connection location, as demonstrated in the 2007 report and identified in section 3.1, and that the recently released sanitary sewer flow criteria for estimating new and existing sanitary sewer flows will result in additional residual capacity both at the proposed connection location and the downstream network, it is our recommendation that the City of Ottawa supersede the flow allocation for the subject lands with the calculated flow identified above, namely 10.16 l/s.

3.4 Sanitary Sewer Easement

The sanitary trunk sewer is proposed to be 450mm dia with inverts similar to the 2007 sanitary sewer servicing study requirements. The easement shown in the proposed plans is 10.0m wide where there are additional private infrastructure items within the easement, and 6.0m wide where the sanitary sewer trunk is the only service within the easement. A series of sections were prepared along the easement to review the ability to access the sewer in the event of future maintenance. The proposed sections include a requirement for a trench boxes and 1:1 side slopes. Profiles of the easement and sanitary sewer have also been provided and show that the approximate depth of the sewer is around 7m throughout the site. The proposed easement widths and sections have been reviewed by a geotechnical engineer and contractor, both of whom are familiar with the site, and deemed acceptable.

It should be noted that secondary manholes at each block have been added to the network to avoid service connections directly to the trunk sewer and excavating down to the deep sewer after construction.

3.5 Hunt Club Road Watermain Crossing

Extending the sanitary sewer under the Hunt Club bridge to service the lands to the south of the subject site will require crossing a City of Ottawa 610mm watermain. Based on City of Ottawa mapping the watermain, which crosses the Rideau River, runs more or less parallel with Hunt Club Road. The watermain crossing will take place +/- 100m south of the proposed sanitary MH107A. The proposed MH107A invert out is 86.60m and assuming a 450mm dia sanitary sewer is specified at 0.20% slope we can expect the sanitary invert to be +/- 86.86m at the crossing.

The City of Ottawa provided design drawings for the watermain in an effort to ensure the watermain can be crossed with the sanitary sewer. We noted the drawings are design only and no as-built elevations were provided; however, in the vicinity of the crossing the watermain appears to be climbing at a slope of +/-24%. It can be said that in a distance of 10m the watermain will change elevations by approximately 2.4m which will certainly allow a crossing to be made.

Based on the watermain design elevations provided and the sanitary crossing inverts referenced above, with the information available we can assume the sanitary sewer will cross over the watermain with 0.50m barrel to barrel clearance beginning at watermain station 1+490 and continuing westward. A crossing under the watermain, again with 0.50m barrel to barrel clearance appears to be possible from watermain station 1+505 and continuing eastward. A crossing does not appear to be feasible, with the required clearance from STA 1+490 to 1+505.

That being said, at the time of designing the sanitary sewer extension southward the designer should obtain a survey of the horizontal location of the watermain and the as-built elevation drawings to ensure the correct alignment and crossing location is chosen.

4 SITE STORMWATER MANAGEMENT

4.1 Background

The Riverside Park site falls within the drainage limits of the existing Riverwalk stormwater facility (henceforth referred to as the City of Ottawa Kimberwick Stormwater Management Facility). The design of that pond was outlined within the report "Stormwater Management for Riverside Drive Lands" completed by CCL in April of 1987. The pond was constructed in the early 1990's to support developments in the area between Riverside Drive and the Rideau River. The drainage area plan (Drawing No. 3625-501) as well as the storm sewer design sheet prepared for the Riverwalk Park development in 1987 is included in Appendix C. The subject site is included south of the Riverwalk Park development in the area identified as St. Mary's Cement with a drainage area of 7.00 ha at a runoff coefficient of 0.70.

Subsequent to that report and the construction of the facility, the stormwater pond was updated as part of the development of adjacent lands by Claridge Homes in 1996. The report "Riverwalk Park Stormwater Management Facility Updated Stormwater Design Plan" was completed by Novatech Engineering (June 1996). That report outlined the strategy to rehabilitate the facility which had fallen into disrepair, operate, maintain and monitor performance up to the point of full assumption of the facility by the City of Ottawa.

4.2 Stormwater Management Plan

In order to provide the Riverwalk Park site with an outlet to the existing pond, a new storm sewer is proposed. The proposed storm sewer will connect to existing storm MH3 (as identified on Drawing 37923-C-002). Storm runoff from the Riverside Park site was included in the design of the existing downstream sewers. The flows are identified on the storm sewer design sheet attached in Appendix C. The existing sewers downstream of the Riverwalk Park site and the Stormwater Management Facility have capacity for the subject site runoff. It should be noted that the ground surface of the inlet works to the Stormwater Management Facility is at or near the 80 meter contour while the lowest part of the upstream Riverwalk Park development is close to the 89 meter contour.

4.3 Objective

The purpose of this section is to present the dual drainage design, including the minor and major system, for the proposed site. The design includes the sizing of inlet control devices, maximum flow on the surface and hydraulic grade line analysis. The evaluation and design takes into consideration the City of Ottawa Sewer Design Guidelines (OSDG) and the June 2012 Technical Bulletin ISDTB-2012-4.

4.4 Overall Stormwater Management Approach

4.4.1 Dual Drainage Design

The site has been designed with dual drainage features, accommodating minor and major system flow. The minor system is tributary to the existing City of Ottawa Kimberwick SWM Facility. Respecting the existing site topography, it is anticipated that major system surface flows from the proposed blocks will be directed to the adjacent Rideau River. Alternatively, major system storage may be provided on these blocks. Ultimately, the blocks will be provided with detailed Site Plan Applications with full stormwater management plans.

The access road through the site is generally on continuous grade, but has been provided with a single low point to facilitate ponding. Inlet control devices (ICDs) are proposed to minimize the

surcharge in the minor system during infrequent storm events and maximize use of available on-site storage. The minor system capture of ICDs along the access road is based on the 2 year flow. The minor system capture for the commercial blocks have been designed with approximately the 5 year flow (limited based on available capacity in downstream receiving storm sewer system).

The dual drainage system has been evaluated using the DDSWMM hydrological model. Further details of the modelling completed for the site are provided in the below sections.

4.4.1.1 Minor System

The storm sewers in the Riverside Park site are sized based on Standards of the City of Ottawa and the MOE. Rational Method Sewer Design Sheet and Drainage Area Plan are provided within Appendix C. Some of the key criteria include the following:

- Runoff Coefficients: Blocks C=0.70-0.80
 11m Access Road C=0.90
- Initial Time of Concentration 10 minutes
- Minimum Velocity 0.80 m/s
- Maximum Velocity 3.00 m/s

Across the site, ICDs are proposed to limit the flow into the minor system during infrequent storm events up to the 100 year event. The minor system capture of ICDs along the access road is based on the 2 year flow. The minor system capture for the commercial blocks have been designed with approximately the 5 year flow (limited based on available capacity in downstream receiving storm sewer system). A summary of the minor system capture across the site is provided within **Table 4.1**.

4.4.1.2 Major System

Respecting the existing site topography, it is anticipated that major system surface flows from the proposed blocks will be directed to the adjacent Rideau River. Alternatively, major system storage may be provided on these sites. Ultimately, the blocks will be provided with detailed Site Plan Applications with full stormwater management plans.

The access road within the site is designed to accommodate on-site storage where possible. Major system storage is based on detailed grading (and volumes are generated from autoCAD) and the storage-outflow characteristics were taken into consideration assuming static conditions.

The hydrological model quantifies the routed surface flows and the resulting major flows along the access road. The primary focus of this analysis was to evaluate surface flow/ponding conditions during the 100 year storm event. The 2 year simulation was performed to assure that runoff is fully captured. Available and conceptual surface storage was accounted in the DDSWMM model and is summarized in **Table 4.1**

4.5 Hydrological Modelling

Hydrological analysis of the proposed dual drainage system of the subject site was conducted using DDSWMM. This technique offers a single storm event flow generation and routing. Land use, selected modeling routines, and input parameters are discussed in the following sections. A drainage area plan is presented in Drawing 37923-500 and model files are included in **Appendix C**. The main hydrological parameters used in the rational method spreadsheet and DDSWMM model are summarized in the following sections.

4.5.1 Hydrological Evaluation

Land use, selected modeling routines, and input parameters for the model are discussed in the following sections.

Land Use

The site will be comprised of commercial blocks with a shared access road.

Storms and Drainage Area Parameters

The main hydrology parameters are summarized below and in **Table 4.1**.

- **Design storms:** The site was evaluated using the following storms:
 - 2 year 3 hour Chicago storm event with a 10 minute time step (for dual drainage evaluation, specifically the minor system);
 - 100 year 3 hour Chicago storm event with a 10 minute time step (for dual drainage evaluation, specifically major flow conveyance); and
 - 100 year 3 hour Chicago storm event + 20% increase in intensity with a 10 minute time step (for a stress test on major flow conveyance as per the City of Ottawa Sewer Design Guidelines).

- **Infiltration:** The selected infiltration losses are consistent with the City of Ottawa Sewer Design Guidelines. The Horton values are as follows: $f_o = 76.2$ mm/h, $f_c = 13.2$ mm/h, $k = 0.00115$ s⁻¹.

- **Area:** The total approximate 6ha, was divided into drainage areas based on the proposed commercial blocks and the storm sewer within the access road.

- **Imperviousness:** Imperviousness ratios are based on the rational method runoff C values as per the Drainage Area Plan (provided within Appendix C).

- **Width:** The catchment width was based on the conveyance route length of the drainage area and multiplied by two. The multiplier of two was only used if the drainage area had runoff contribution from both sides of the drainage area.

- **Slope:** The ground slope was based upon the average slope for both impervious and pervious area. Generally, the slope is approximately 2% (0.02 m/m). This assumes a slope of approximately 1% for impervious or road surfaces and 3% for pervious surfaces (lot grading).

- **Detention storage depth:** Detention storage depths of 1.57 mm and 4.67 mm were used for impervious and pervious areas, respectively.

- **Manning's roughness:** Manning's roughness coefficients of 0.013 and 0.25 were used for impervious and pervious areas, respectively.

- **Major system storage and routing:** The access road is comprised of primarily continuous grade with a single low point. For the drainage area with sawtoothing (low point), available surface storage has been calculated based on the grading plan. Flow is attenuated within low point with potential overflow cascading to the next segment downstream. The total volume at the low point, up to the overflow depth, is the maximum static storage.

For street segments with ponding, cascading overflow from a low point to a downstream segment utilizes the static storage available plus an additional amount of storage equivalent to the depth required for the flow to cascade over the downstream high point. The attenuation in street sags was evaluated to account for static storage and, if overflow occurs, dynamic storage. Within this report it is referred to as double routing.

DDSWMM does not have a direct way of coding double routing since it does not allow the user to code dynamic storage over the high point. For this analysis, the method employed is that recommended in the February 2014 City of Ottawa Technical Bulletin (PIEDTB-2016-01). It accounts for overflow from a street segment (regular static storage at a sag) being conveyed to a downstream dummy segment. In other words, a regular low point segment is provided with a downstream dummy segment for further flow attenuation to account for the dynamic ponding during overflow.

There are no drainage area attributes associated with the dummy segment since it is a segment solely for routing. In addition, there is no inflow to the minor system from these dummy segments. The overflow hydrograph from the upstream catchment is routed in the dummy segment to the next "real" downstream segment. The dummy segments have the following specific characteristics:

- Segment Length: Equivalent to the length of the maximum static storage from the street segment contributing to it.
- Road Type: Equivalent to the right-of-way characteristics from the segment contributing to it, but with a longitudinal slope of 0.01% (0.0001 m/m).

The dummy segments for major system routing have been applied to the analysis of the subject site. The segments are referenced as D1, D2, D3, etc. within the DDSWMM modelling file. The drainage area plan presented in **Drawing 37923-500** does not show the dummy segments, but the DDSWMM output file shows the dummy segments immediately following the corresponding major segment which cascades into that dummy segment.

For street segments with continuous grade, simulations were based on the approach-capture characteristics of the catchbasin with the constraint that during the 100 year design storm the maximum cascading flow does not exceed 350 mm.

For street segments with sawtoothing, simulations were based on the constraint that during the 100 year design storm the maximum depth of ponding (including cascading flow where applicable) does not exceed 350 mm. Where surface storage is available, the storage-outflow characteristics for each low point were taken into consideration. The evaluation was undertaken assuming static ponding conditions.

- **Minor system capture:** The minor system capture for the overall site is limited to the allocated capacity of the existing SWM facility to the 5 year Rational Method flow with runoff value of 0.7. ICDs are incorporated into the design to protect the minor system from surcharge during infrequent storm events and to utilize the available on-site storage. The size of the inlet control devices (ICDs) was optimized using DDSWMM.

The minor system inflow rate was optimized to account for continuous grade. Specifically, the model incorporates the actual flow entering the minor system on continuous grade based on approach-capture curves derived from the 1984 MTO Drainage Manual. Minor system capture was set to 2 year modelled flow for the access road; however, based on the approach-capture curve, the actual capture may be less than this. This results in there being

cascading flow on the surface during both the 2 and 100 year events. Therefore, at receiving low point downstream of on grade CBs, the ICDs have been sized to fully capture the cascading flow from upstream street segments on continuous grade during the 2 year event, while minimizing ponding at the low point.

The main hydrological parameters used in the DDSWMM model are summarized in **Table 4.1**. The corresponding drainage area plan (**Drawing 37923-500**) is provided in **Appendix C**, along with a CD of model files.

Table 4.1 DDSWMM Hydrological Parameters

DRAINAGE AREA ID	AREA (HA)	D/S SEGMENT ID	XPSWMM NODE ID	IMP RATIO [Tp (h)]	Segment Length (m)	Subcatchment WIDTH (M)	AVAILABLE/CONCEPTUAL STATIC PONDING (M ³)
S20A	0.18	S20B	CBMH20	0.50	38	20	n/a
S20B	0.13	S20C	CBMH20	0.43	31	25	n/a
S20C	0.13	S20D	CBMH20	0.43	34	20	n/a
S20D	0.06	S20E	CBMH20	0.43	19	20	n/a
S20E	0.11	S107	107	0.50	39	15	n/a
S107	0.09	S106A	107	0.50	32	15	n/a
S106A	0.02	S106B	106	1.00	18	5	n/a
S106B	0.05	S105A	106	1.00	42	5	n/a
UNIT3	1.12	OUT1	105	0.79	252	126	280*
S105A	0.03	S105B	105	1.00	24	6	n/a
S105B	0.03	S104	105	1.00	23	5	n/a
UNIT1	1.18	S104	104	0.79	265	132	125*
UNIT2	0.52	OUT2	104	0.86	117	58	140*
S104	0.09	REVERA	104	1.00	81	5	6.52
REVERA	2.6	OUT3	104	0.71	585	292	540*

Note: * - conceptual storage

4.5.2 Results of the Hydrological Evaluation

The results of the DDSWMM major system evaluation are summarized in the following sections. Output files are provided within Appendix C for reference.

Table 4.2 DDSWMM Hydrological Model Results for 2 Year Chicago

Segment ID	Total Inflow	U/S Inflow	Catchment Inflow	Max Inlet Capture	Outflow	Max Storage	Storage Duration
	(cms)	(cms)	(cms)	(l/s)	(cms)	(cu.m)	(min)
S20A	0.015	0	0.015	3.34	0.011	0	0
S20B	0.021	0.011	0.01	4.8	0.017	0	0
S20C	0.026	0.017	0.009	5.83	0.02	0	0
S20D	0.025	0.02	0.005	5.58	0.019	0	0
S20E	0.028	0.019	0.009	7.59	0.021	0	0
S107	0.028	0.021	0.007	7.51	0.02	0	0
S106A	0.023	0.02	0.003	6.51	0.017	0	0
S106B	0.024	0.017	0.007	5.98	0.018	0	0
UNIT3	0.135	0	0.135	107.99	0	10.66	20
S105A	0.022	0.018	0.004	22.46	0	0	0
S105B	0.005	0	0.005	1.31	0.003	0	0
UNIT1	0.142	0	0.142	139.84	0	0.01	0
UNIT2	0.067	0	0.067	49.99	0	8.97	30
S104	0.016	0.003	0.013	15.57	0	0	0
D1	0	0	0	0	0	0	0
REVERA	0.287	0	0.287	251.99	0	4.32	10

Table 4.3 DDSWMM Hydrological Model Results for 100 Year Chicago

Segment ID	Total Inflow	U/S Inflow	Catchment Inflow	Max Inlet Capture	Outflow	Max Storage	Storage Duration
	(cms)	(cms)	(cms)	(l/s)	(cms)	(cu.m)	(min)
S20A	0.04	0	0.04	8.95	0.031	0	0
S20B	0.058	0.031	0.027	12	0.046	0	0
S20C	0.073	0.046	0.027	12	0.061	0	0
S20D	0.075	0.061	0.014	12	0.063	0	0
S20E	0.088	0.063	0.025	12	0.076	0	0
S107	0.097	0.076	0.021	12	0.085	0	0
S106A	0.092	0.085	7.00E-03	12	0.08	0	0
S106B	0.098	0.08	0.018	12	0.086	0	0
UNIT3	0.356	0	0.356	108	0	265.35	100
S105A	0.097	0.086	0.011	25	0.072	0	0
S105B	0.083	0.072	0.011	12	0.071	0	0
UNIT1	0.376	0	0.376	197	0	125	50
UNIT2	0.176	0	0.176	50	0	133.5	100
S104	0.1	0.071	0.029	88	0	3.66	10
D1	0	0	0	0	0	0	0
REVERA	0.761	0	0.761	252	0	511.52	90

4.5.2.1 Overland Flow on Street Segments

According to City of Ottawa guidelines, during the 100 year storm event the depth of flow shall not exceed 350 mm and the product of depth and velocity shall not exceed 0.6 m²/s. To determine velocity of the cascading overflow, SWMHYMO was used. The applicable roadway sections were entered into the model with the corresponding longitudinal slopes to obtain the maximum velocity of flow using the Route Channel routine. The resulting depths were also applied for street segments with continuous grade. To determine depth of the cascading overflow for street segments with ponding, the calculation sheet from the February 2014 City of Ottawa Technical Bulletin was employed. The SWMHYMO output files are provided in **Appendix C**.

The major system flow results are summarized in **Table 4.4** and model files are enclosed in **Appendix C**.

Table 4.4 Summary of Cascading Flow during the 100 year 3 hour Chicago Storm (Model files: 37923-3CHI100.OUT and 37923VxD.OUT)

AREA ID (DUMMY SEGMENT IF APPLICABLE)	ROW	LONGITUDINAL SLOPE (%)	OVERFLOW (L/S)	VELOCITY (M/S)	MAX. STATIC PONDING DEPTH (WHERE APPLICABLE) (M)	DYNAMIC DEPTH (DYNAMIC, WHERE APPLICABLE) (M)	MAX. DEPTH (STATIC + DYNAMIC, WHERE APPLICABLE) (M)	VXD (M ² /S)
S20A	11	4.00	31	0.932	n/a	0.031	0.031	0.029
S20B	11	6.00	46	1.200	n/a	0.033	0.033	0.040
S20C	11	4.00	61	1.112	n/a	0.040	0.040	0.045
S20D	11	2.00	63	0.870	n/a	0.046	0.046	0.040
S20E	11	2.00	76	0.909	n/a	0.049	0.049	0.045
S107	11	0.90	85	0.693	n/a	0.060	0.060	0.042
S106A	11	2.99	80	1.077	n/a	0.047	0.047	0.051
S106B	11	4.00	86	1.217	n/a	0.046	0.046	0.056
S105A	11	1.33	72	0.770	n/a	0.052	0.052	0.040
S105B	11	1.00	71	0.690	n/a	0.055	0.055	0.038
S104	11	0.50	0	0.000	0.15	0	0.15	0.000

At each location for the storm event presented, the maximum depth of water on the street is less than the maximum allowable 300 mm, and the d x v product is less than the maximum allowable product of 0.6 m²/s as per the OSDG.

4.5.3 Hydraulic Evaluation

A static hydraulic grade line analysis has been used to evaluate the proposed storm sewer design. The static HGL calculations are based on the Darcy-Weisbach equation for headloss to calculate friction slope of the storm sewer with manhole losses through the storm sewer network. A summary of the supporting equations for friction slope and manhole losses as well as the calculation sheets for the site are provided within Appendix C for reference. The following table provides summary of the storm hydraulic grade line.

Table 4.5 Storm Hydraulic Grade Line

LOCATION	MH	USF ELEVATION (M)	HGL (M)	FB (M)
Access Road	CBMH20	N/A	98.01	N/A
Access Road	MH107	N/A	92.23	N/A
Access Road	MH106	N/A	91.91	N/A
Access Road	MH105	N/A	90.20	N/A
Access Road	MH104	N/A	90.11	N/A
REVERA	MH103	N/A	89.92	N/A
REVERA	MH102	N/A	89.64	N/A
REVERA	MH101	N/A	88.68	N/A
REVERA	MH100	N/A	81.41	N/A
OFF-SITE	MH99	N/A	78.30	N/A
OFF-SITE	MH98	N/A	78.13	N/A
EXISTING STORM	EXMH3	N/A	78.01	N/A

4.6 Summary of Model Output Files

The following is a reference list of the model output files including file names and storm event evaluated. The files are included on the CD enclosed in Appendix C.

DDSWMM:

- 2 year 3 hour Chicago: 37923-3CHI2.OUT
- 5 year, 3 hour Chicago: 37923-3CHI5.OUT
- 100 year 3 hour Chicago: 37923-3CHI100.OUT
- 100 year 3 hour Chicago +20%: 37923-3CHI120.OUT

SWMHYMO:

- 37923VxD.OUT

5 SEDIMENT AND EROSION CONTROL PLAN

5.1 General

During construction, existing stream and conveyance systems can be exposed to significant sediment loadings. Although construction is only a temporary situation, it is proposed to possibly introduce a number of mitigative construction techniques to reduce unnecessary construction sediment loadings. These may include:

- Until the local storm sewer and storm pond are constructed, groundwater in trenches will be pumped into a filter mechanism prior to release to the environment. bulkhead barriers will be installed at the nearest downstream manhole in each sewer which connects to an existing downstream sewer;
- seepage barriers will be constructed in any temporary drainage ditches (where applicable);
- sediment capture filter socks will remain on open surface structures such as maintenance holes and catchbasins until these structures are commissioned and put into use; and
- silt fence on the site perimeter will be installed.

5.2 Trench Dewatering

Any trench dewatering using pumps will be discharged into a filter trap made up of geotextile filters and straw bales similar in design to the OPSD 219.240 Dewatering Trap. These will be constructed in a bowl shape with the fabric forming the bottom and the straw bales forming the sides. Any pumped groundwater will be filtered prior to release to the existing surface runoff. The contractor will inspect and maintain the filters as needed, including sediment removal and disposal and material replacement as needed. It should be noted that that the contractor will be responsible for the design and management of the trap(s).

5.3 Bulkhead Barriers

Although the storm sewers eventually outlet into a sediment forebay, a ½ diameter bulkhead will be constructed over the lower half of the outletting sewers to reduce sediment loadings during construction. These bulkheads will trap any sediment laden flows, thus preventing any construction-related contamination into existing sewers. The bulkheads will be inspected and maintained including periodic sediment removal as needed.

5.4 Seepage Barriers

In order to further reduce sediment loading to the stormwater management facility, seepage barriers will be installed on any surface water courses at appropriate locations that may become evident during construction. These barriers will be Light Duty Straw Bale Barriers per OPSD 219.100 and Heavy Duty Silt Fence Barriers per OPSD 219.130; locations are shown on the Sediment and Erosion Control Plan included in **Appendix D**. They are typically made of layers of straw bales or geotextile fabric staked in place. All seepage barriers will be inspected and maintained as needed.

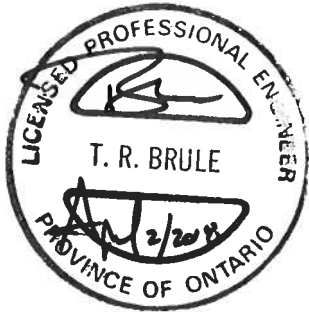
5.5 Surface Structure Filters

All catchbasins, and to a lesser degree, manholes, convey surface water to sewers. Until streets are asphalted and curbed, all catchbasins and manholes will be constructed with sediment capture inserts or equivalent located between the structure frame and cover. These will stay in place and be maintained during construction and build until it is appropriate to remove same.

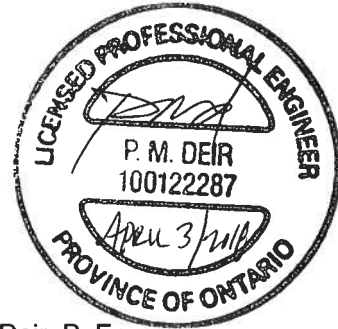
6 CONCLUSION

This report has illustrated that the proposed Riverside Park vacant land condominium can be serviced by extending municipal services. The water network will be extended to provide necessary service. All sanitary and storm sewer designs for this development will be completed in conformance with City of Ottawa standards while acknowledging downstream constraints. By limiting flow into the minor storm sewer system as per the applicable local stormwater management criteria and allowing for excess surface storage on-site, all stormwater management requirements will be met. Adherence to the Sediment and Erosion Control Plan during construction will minimize harmful impacts on surface water.

Based on the information provided within this report, the plans prepared for the subject development can be serviced to meet City of Ottawa requirements.



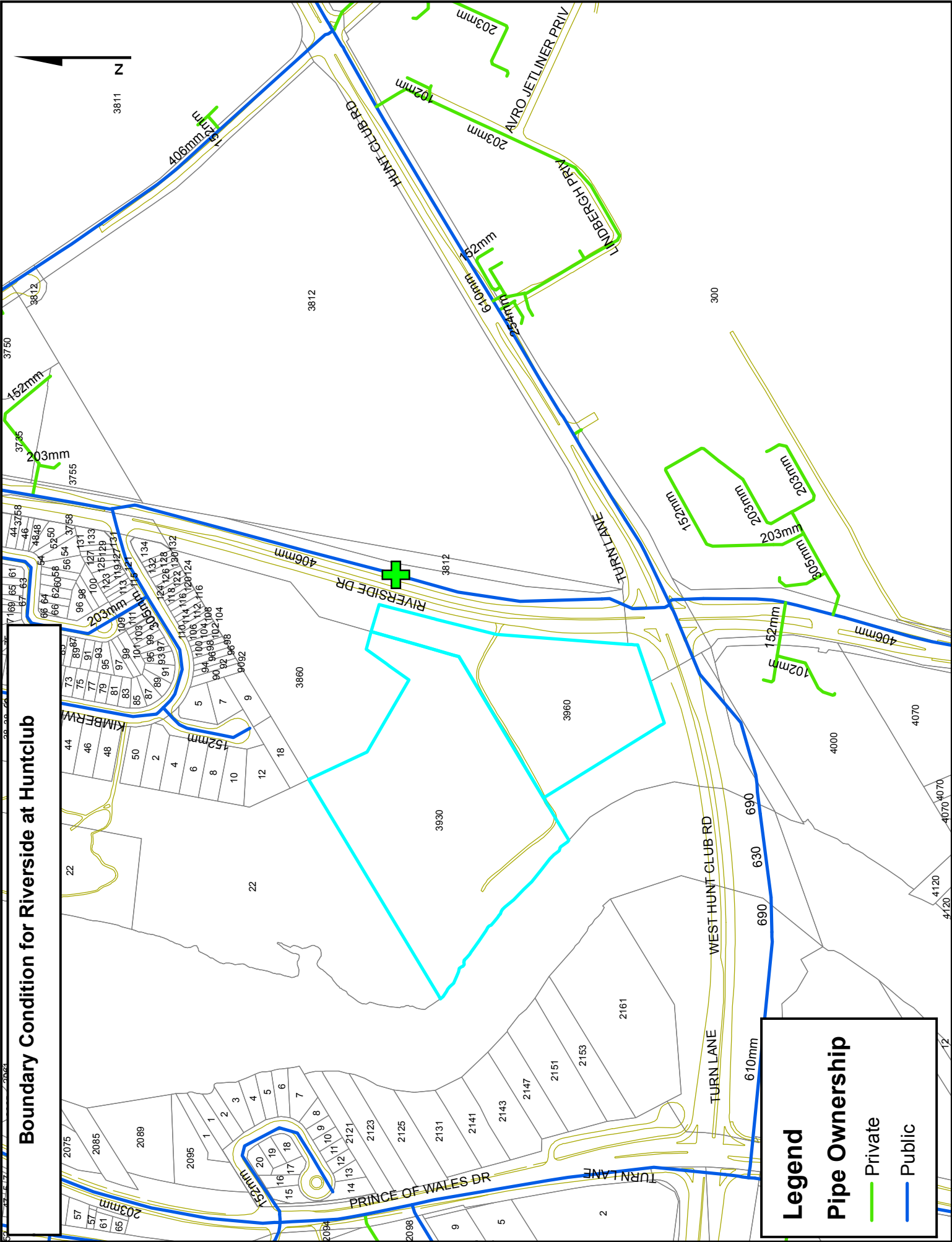
Terry Brule, P. Eng.
Associate



Peter Deir, P. Eng.
Section 4.0

APPENDIX A

Boundary Condition for Riverside at Huntclub



Legend

Pipe Ownership

Private

Public

James Battison

From: Oram, Cody <Cody.Oram@ottawa.ca>
Sent: Wednesday, December 13, 2017 9:28 AM
To: James Battison
Cc: Alex Turner; Terry Brule; Lance Erion
Subject: RE: 37923 - Riverside at Hunt Club - Boundary Condition Request
Attachments: Riverside at Hutn Club Dec 2017.pdf

Hi James,

The following are boundary conditions, HGL, for hydraulic analysis at Riverside at Hunt Club (zone 2C) assumed to be connected to the 406mm on Riverside (see attached PDF for location).

Minimum HGL = 125.1m

Maximum HGL = 134.7m

Max Day + Fire Flow (250 L/s) = 126.2m

These are for current conditions and are based on computer model simulation.

Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation.

Regards,

Cody Oram, P.Eng. Senior Engineer

Development Review, South Services

Planning, Infrastructure and Economic Development Department | Services de planification, d'infrastructure et de développement économique

City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West. Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1

613.580.2424 ext./poste **13422**, fax/télé: 613-580-2576, cody.oram@ottawa.ca



From: James Battison [mailto:James.Battison@ibigroup.com]

Sent: Wednesday, December 06, 2017 2:26 PM

To: Oram, Cody <Cody.Oram@ottawa.ca>

Cc: Alex Turner <aturner@taggart.ca>; Terry Brule <tbrule@IBIGroup.com>; Lance Erion <lerion@IBIGroup.com>

Subject: 37923 - Riverside at Hunt Club - Boundary Condition Request

Hi Cody,

We are initiating our design for a development at the NW corner of Hunt Club and Riverside Drive. A location sketch is attached.

To facilitate our design we are requesting watermain boundary conditions.

The connection location is identified on the sketch referenced above and the proposed water demands can be found on the attached spreadsheet.

Should you need anything else to provide watermain boundary conditions please let us know.

It should also be noted that we will be directing the stormwater to an existing nearby pond, which can be seen on the attached "services-Mark-up" sketch. We may need to have a meeting to discuss the SWM criteria to be used in our design.

Thanks.

James Battison

IBI GROUP

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Ottawa ON K1S 5N4 Canada
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WATERMAIN DEMAND CALCULATION SHEET

PROJECT : Riverside and Huntclub
 LOCATION : Taggart Realty Management

DATE: 2-Apr-18
 DESIGN: LE

NODE	RESIDENTIAL				NON-RESIDENTIAL			AVERAGE DAILY DEMAND (l/s)			MAXIMUM DAILY DEMAND (l/s)			MAXIMUM HOURLY DEMAND (l/s)		
	UNITS				COM (Ha)	IND (Ha)	INST (Ha)	Res.	Non-res.	Total	Res.	Non-res.	Total	Res.	Non-res.	Total
	SF	SD	TH	APT												
J4 (School Block)								0.00	0.25	0.25	0.00	0.37	0.37	0.00	0.67	0.67
J6 (Commercial - South)					0.89			0.00	0.29	0.29	0.00	0.43	0.43	0.00	0.78	0.78
J7 (Commercial - North)					0.41			0.00	0.13	0.13	0.00	0.20	0.20	0.00	0.36	0.36
J8 (Hotel Block)				70		126		0.51	0.00	0.51	1.28	0.00	1.28	2.81	0.00	2.81
J9 (Rivera Block)				300		540		2.19	0.00	2.19	5.47	0.00	5.47	12.03	0.00	12.03

ASSUMPTIONS

RESIDENTIAL DENSITIES	AVERAGE DAILY DEMAND	MAXIMUM DAILY DEMAND	MAXIMUM HOURLY DEMAND
- Single Family (SF)	3.4 p/p/u	350 l/cap/day	- Residential 1.925 l/cap/day
- Semi Detached (SD)	2.7 p/p/u	28,000 l/ha/day	- Commercial 42,000 l/ha/day
- Townhouse (TH)	2.7 p/p/u	35,000 l/ha/day	- Industrial 52,500 l/ha/day
- Apartment (APT)	1.8 p/p/u	28,000 l/student/d	- Institutional 42,000 l/student/d

Fire Flow Requirement from Fire Underwriters Survey

Rivera - Tower B
 Building Floor Area

5,920 m²

Tower footprint = 870m² Podium footprint 1570m²
 Assume 1 floor tower, plus 1 tower floor plus 50% of 8 tower floors

Fire Flow

$F = 220C\sqrt{A}$

C	0.6	C =	1.5 wood frame
A	5,920 m ²		1.0 ordinary
F	10,156 l/min		0.8 non-combustile
use	10,000 l/min		0.6 fire-resistive

Occupancy Adjustment

		-25% non-combustile
		-15% limited combustile
Use	-15%	0% combustile
		+15% free burning
Adjustment	-1500 l/min	+25% rapid burning
Fire flow	8,500 l/min	

Sprinkler Adjustment

		-30% system conforming to NFPA 13
		-50% complete automatic system
Use	-50%	
Adjustment	-4250 l/min	

Exposure Adjustment

Building Face	Separation	Charge	Separation Charge	
			0 to 3m	+25%
			3.1 to 10m	+20%
			10.1 to 20m	+15%
north	0	> 45	20.1 to 30m	+10%
east		> 45	30.1 to 45m	+5%
south	0	> 45		
west		> 45		

Total	50%
Adjustment	4,250 l/min

Required Fire Flow

Total adjustments	-	l/min
Fire flow	8,500	l/min
Use	9,000	l/min
	150.0	l/s

Fire Flow Requirement from Fire Underwriters Survey

Rivera - Tower C
 Building Floor Area 5,555 m²

Tower footprint = 870m² Podium footprint 1205m²
 Assume 1 floor tower, plus 1 tower floor plus 50% of 8 tower floors

Fire Flow

$F = 220C\sqrt{A}$

C	0.6	C =	1.5 wood frame
A	5,555 m ²		1.0 ordinary
			0.8 non-combustile
F	9,838 l/min		0.6 fire-resistive
use	10,000 l/min		

Occupancy Adjustment

		-25% non-combustile
		-15% limited combustile
Use	-15%	0% combustile
		+15% free burning
Adjustment	-1500 l/min	+25% rapid burning
Fire flow	8,500 l/min	

Sprinkler Adjustment

		-30% system conforming to NFPA 13
		-50% complete automatic system
Use	-50%	
Adjustment	-4250 l/min	

Exposure Adjustment

				Separation Charge
				0 to 3m +25%
Building Face	Separation	Charge		3.1 to 10m +20%
north	0	0	25%	10.1 to 20m +15%
east	> 45		0%	20.1 to 30m +10%
south	0		25%	30.1 to 45m +5%
west	> 45		0%	
Total			50%	
Adjustment			4,250 l/min	

Required Fire Flow

Total adjustments	-	l/min
Fire flow	8,500	l/min
Use	9,000	l/min
	150.0	l/s

Fire Flow Requirement from Fire Underwriters Survey

Rivera - Tower D
 Building Floor Area 4,460 m²

Fire Flow

$F = 220C\sqrt{A}$

C	0.6	C =	1.5 wood frame
A	4,460 m ²		1.0 ordinary
F	8,815 l/min		0.8 non-combustile
use	9,000 l/min		0.6 fire-resistive

Occupancy Adjustment

		-25% non-combustile
		-15% limited combustile
Use	-15%	0% combustile
		+15% free burning
Adjustment	-1350 l/min	+25% rapid burning
Fire flow	7,650 l/min	

Sprinkler Adjustment

		-30% system conforming to NFPA 13
		-50% complete automatic system
Use	-50%	
Adjustment	-3825 l/min	

Exposure Adjustment

		Separation Charge	
		0 to 3m	+25%
		3.1 to 10m	+20%
		10.1 to 20m	+15%
		20.1 to 30m	+10%
		30.1 to 45m	+5%
Building Face	Separation	Charge	
north	> 45	0%	
east	> 45	0%	
south	0	25%	
west	> 45	0%	

Total 25%

Adjustment 1,913 l/min

Required Fire Flow

Total adjustments	<u>(1,913) l/min</u>
Fire flow	5,738 l/min
Use	6,000 l/min
	100.0 l/s

Fire Flow Requirement from Fire Underwriters Survey

Rivera - Tower A
 Building Floor Area 4,910 m² Tower footprint = 752m² Podium footprint 1150m²
 Assume 1 floor tower, plus 1 tower floor plus 50% of 8 tower floors

Fire Flow

$F = 220C\sqrt{A}$

C	0.6	C =	1.5 wood frame
A	4,910 m ²		1.0 ordinary
			0.8 non-combustile
F	9,249 l/min		0.6 fire-resistive
use	9,000 l/min		

Occupancy Adjustment

		-25% non-combustile
		-15% limited combustile
Use	-15%	0% combustile
		+15% free burning
Adjustment	-1350 l/min	+25% rapid burning
Fire flow	7,650 l/min	

Sprinkler Adjustment

		-30% system conforming to NFPA 13
		-50% complete automatic system
Use	-50%	
Adjustment	-3825 l/min	

Exposure Adjustment

			Separation Charge	
			0 to 3m	+25%
			3.1 to 10m	+20%
			10.1 to 20m	+15%
			20.1 to 30m	+10%
			30.1 to 45m	+5%
Building Face	Separation	Charge		
north	0	25%		
east	> 45	0%		
south	23	10%		
west	> 45	0%		
Total		35%		

Adjustment 2,678 l/min

Required Fire Flow

Total adjustments	(1,148) l/min
Fire flow	6,503 l/min
Use	7,000 l/min
	116.7 l/s

Fire Flow Requirement from Fire Underwriters Survey

Hotel
 Building Floor Area 3,938 m²

Fire Flow

$F = 220C\sqrt{A}$

C	0.6	C =	1.5 wood frame
A	3,938 m ²		1.0 ordinary
F	8,283 l/min		0.8 non-combustile
use	8,000 l/min		0.6 fire-resistive

Occupancy Adjustment

		-25% non-combustile
		-15% limited combustile
Use	-15%	0% combustile
		+15% free burning
Adjustment	-1200 l/min	+25% rapid burning
Fire flow	6,800 l/min	

Sprinkler Adjustment

		-30% system conforming to NFPA 13
		-50% complete automatic system
Use	-50%	
Adjustment	-3400 l/min	

Exposure Adjustment

		Separation Charge	
Building Face	Separation	Charge	
			0 to 3m +25%
			3.1 to 10m +20%
			10.1 to 20m +15%
north	23	10%	20.1 to 30m +10%
east	37	5%	30.1 to 45m +5%
south	> 45	0%	
west	> 45	0%	

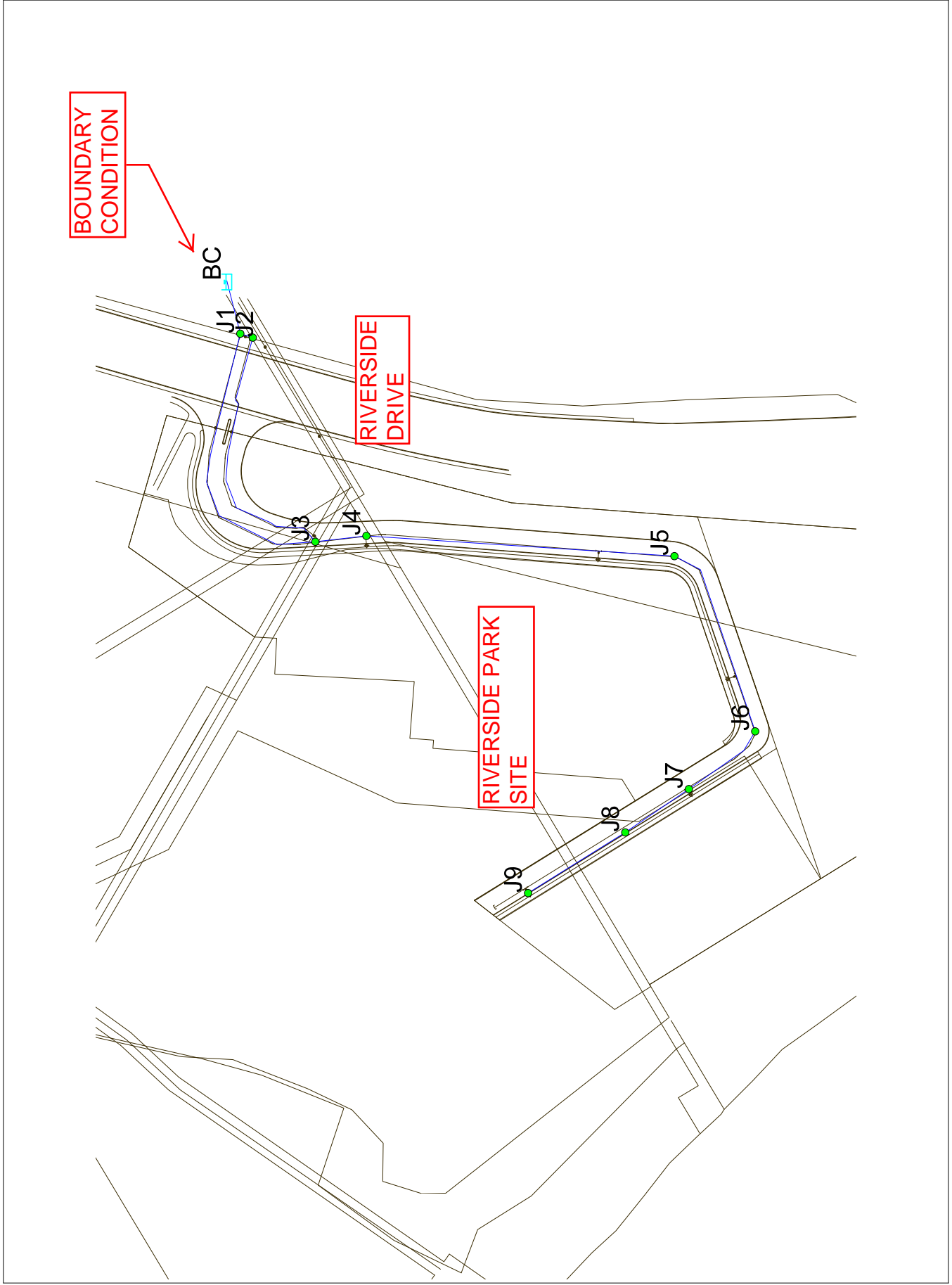
Total 15%

Adjustment 1,020 l/min

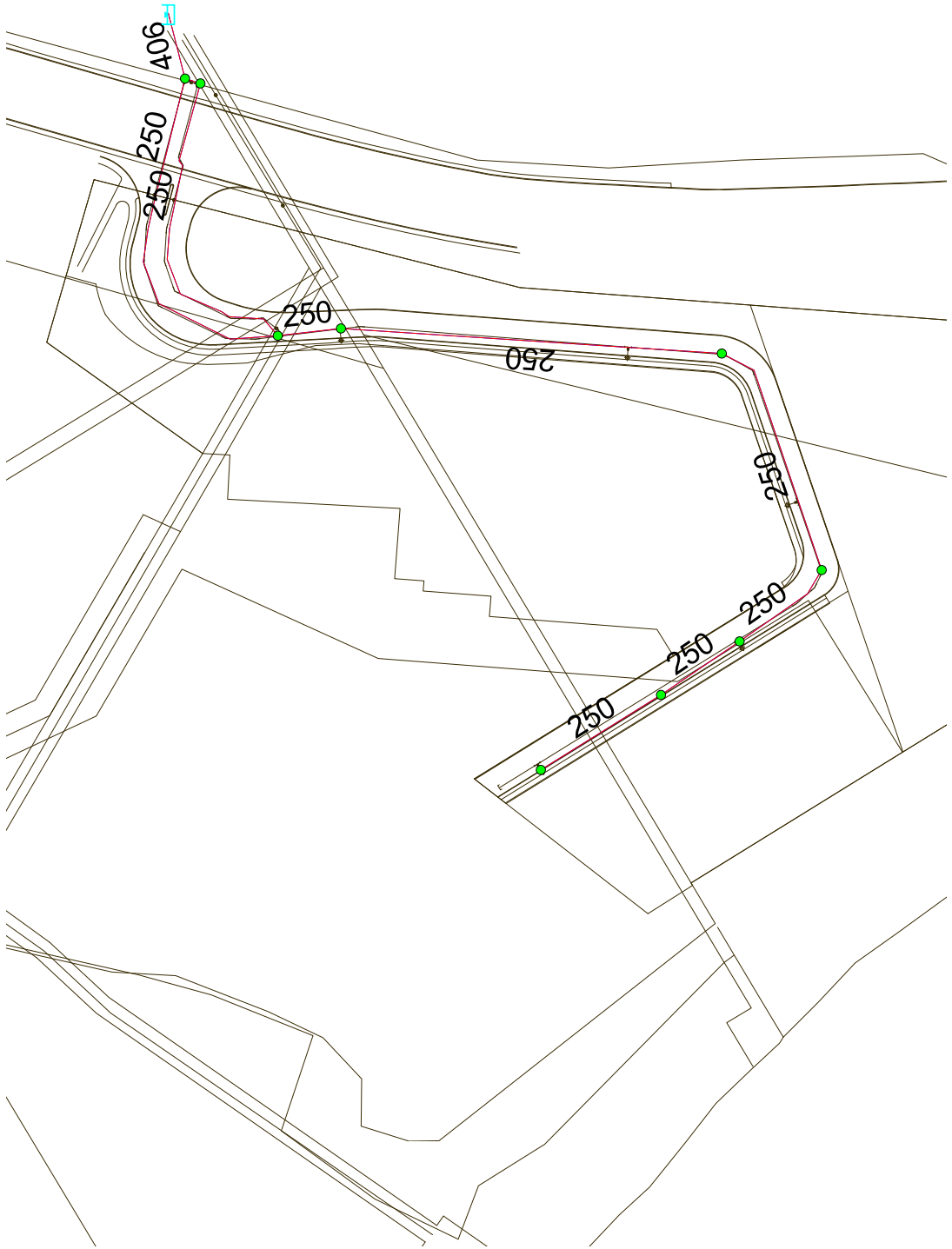
Required Fire Flow

Total adjustments	<u>(2,380) l/min</u>
Fire flow	4,420 l/min
Use	4,000 l/min
	66.7 l/s

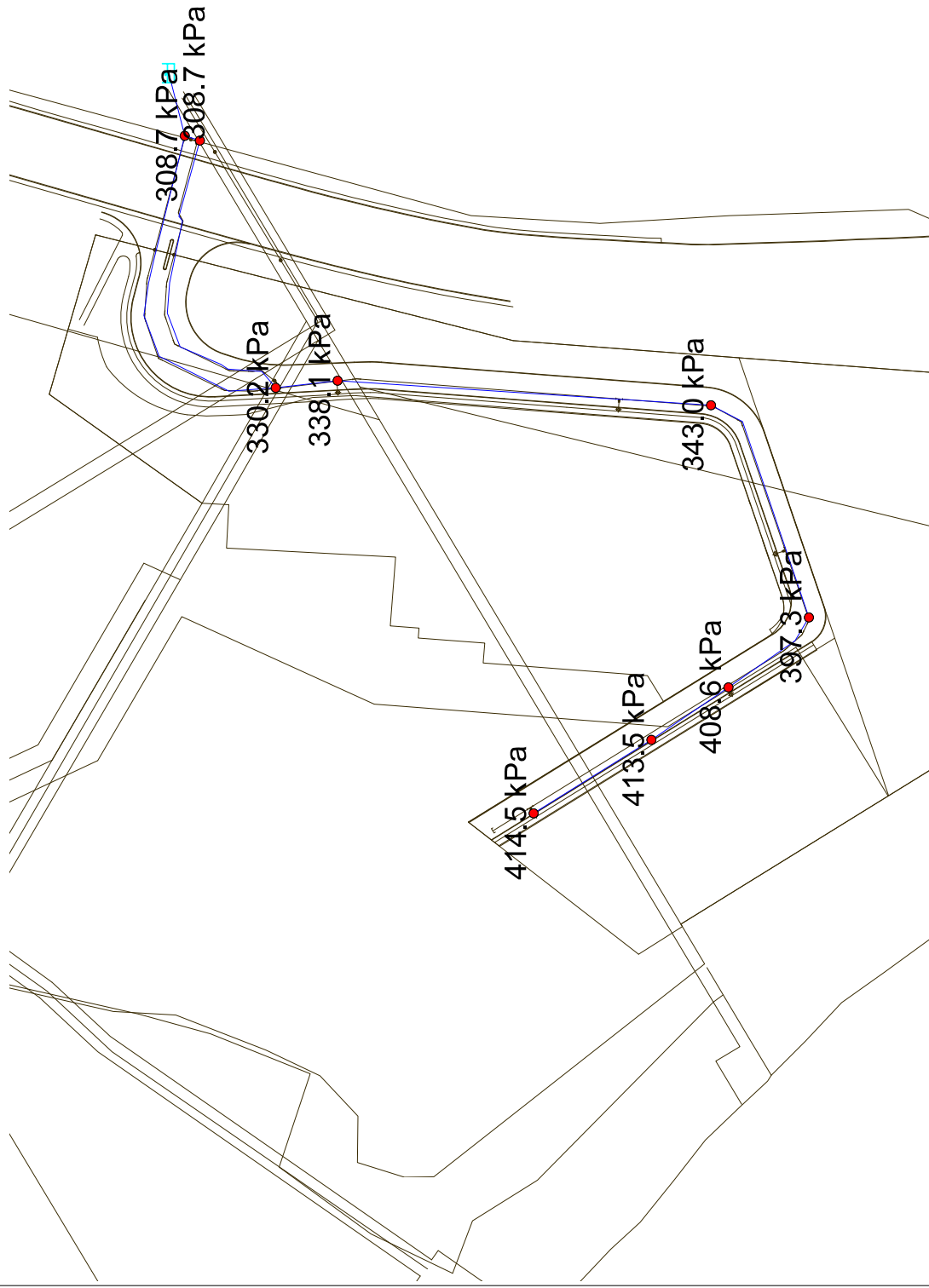
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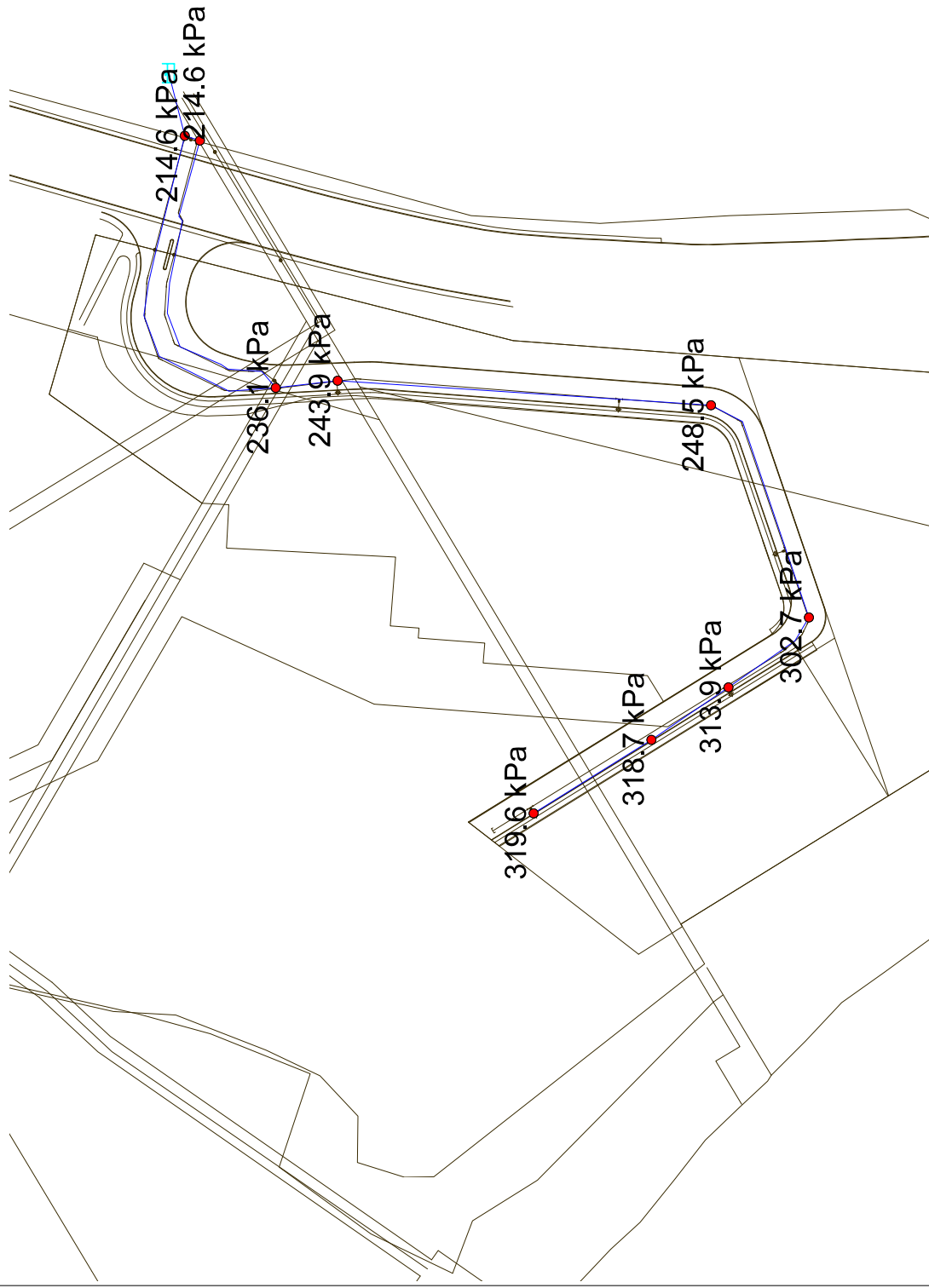
PIPE SIZES



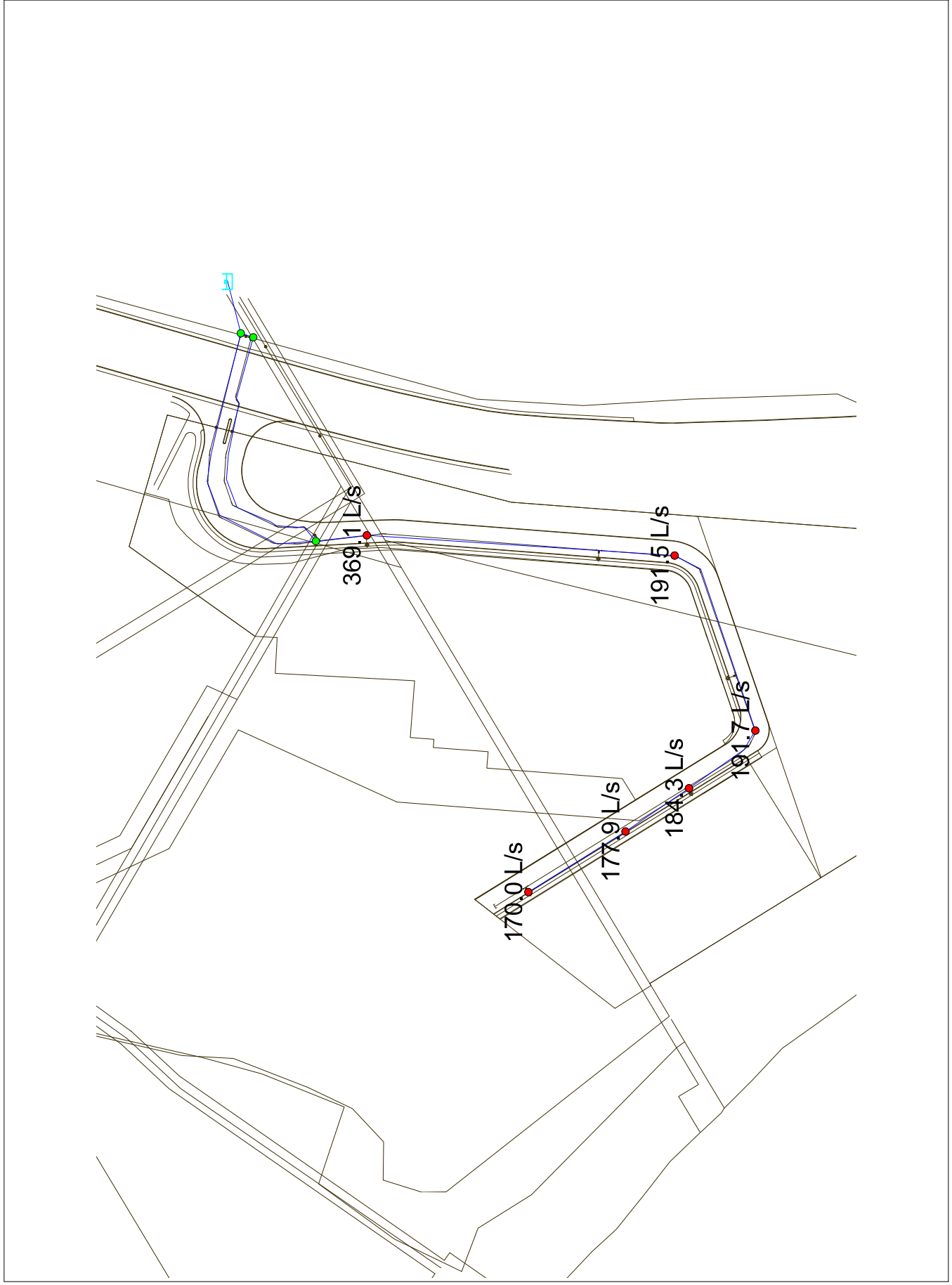
BASIC DAY (MAX HGL) PRESSURES



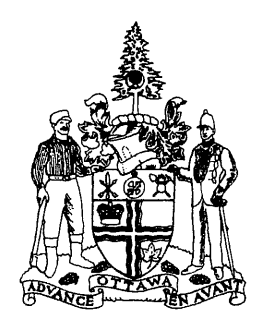
PEAK HOUR PRESSURES



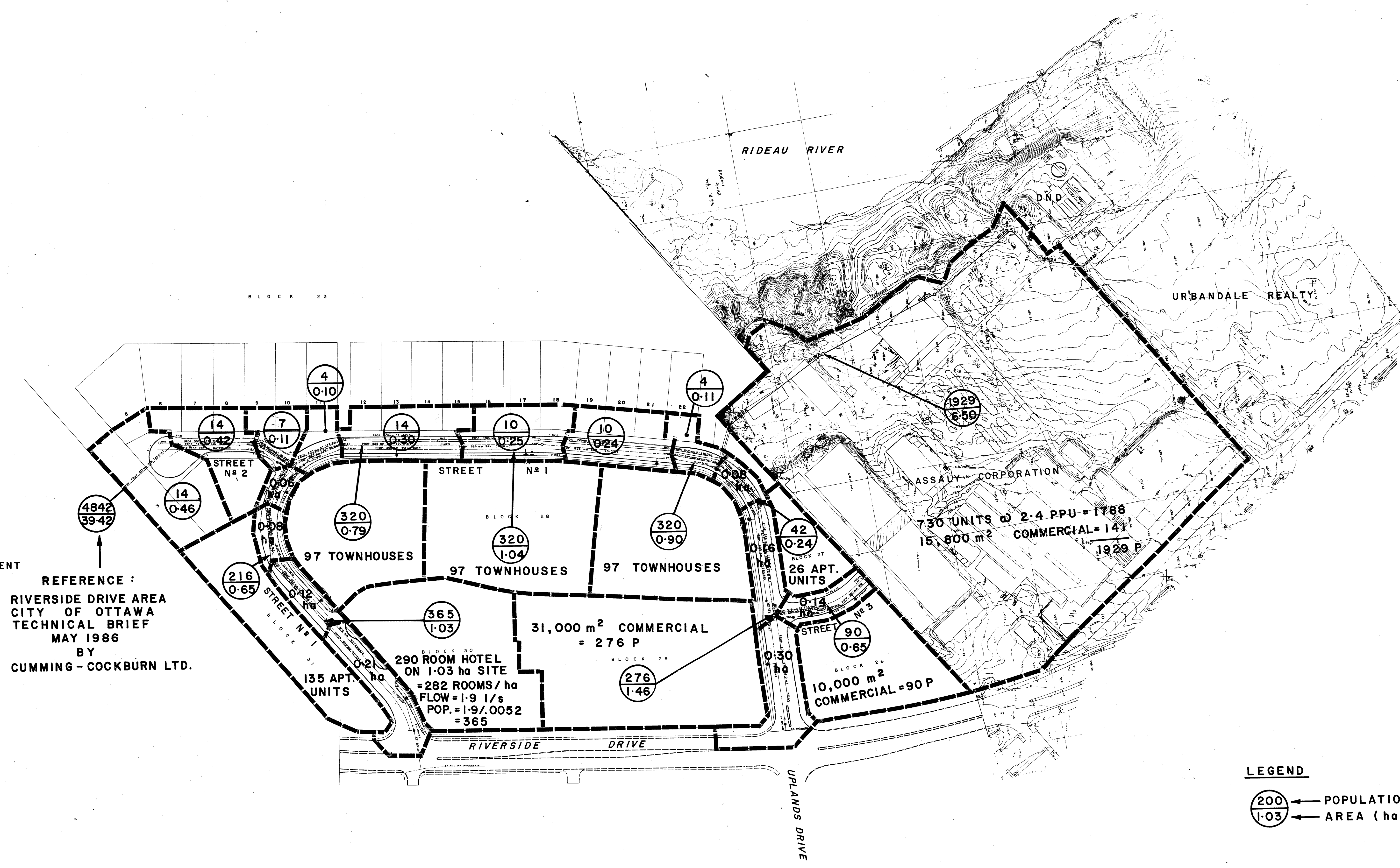
MAX DAY + FIRE FIFEFLOWS



APPENDIX B



City of Ottawa
Department of Physical Environment
Engineering And Surveys Branch



ST. MARY'S CEMENT

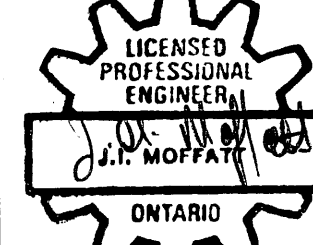
REFERENCE :
RIVERSIDE DRIVE AREA
CITY OF OTTAWA
TECHNICAL BRIEF
MAY 1986
BY
CUMMING - COCKBURN LTD.

LEGEND

200 ← POPULATION
1.03 ← AREA (ha)

Revisions:

No	Date	Description	Drawn By	Apprd By


CUMMING - COCKBURN & ASSOCIATES
 CONSULTING MUNICIPAL ENGINEERS
 WATERLOO - TORONTO - OTTAWA

Designed By: J. I. M.	Date: []/[]/[]	Structural Check By: []	Date: []/[]/[]
Survey Detail By: []	Date: []/[]/[]	Checked By: []	Date: []/[]/[]
Drafting By: []	Date: []/[]/[]	Checked By: []	Date: []/[]/[]

Final Measurements:

Construction Type: []	Inspector: []
Work Commenced: []	Instrument Man: []
Work Completed: []	Field Book #: []
Designer: []	Date: []/[]/[]
Drafting Revisions: []	Checked By: []

Design And Construction Division

C. Sim P. Eng.	W. R. Cole P. Eng.
<i>[Signature]</i>	<i>[Signature]</i>

J. PEREZ CORPORATION - RIVERWALK PARK
SANITARY DRAINAGE AREA PLAN

Contract No: 3625	Survey Book: []	Scale: HOR. 1:1250 VERT. []	Plan No: 501 A Sheet 1 of 1
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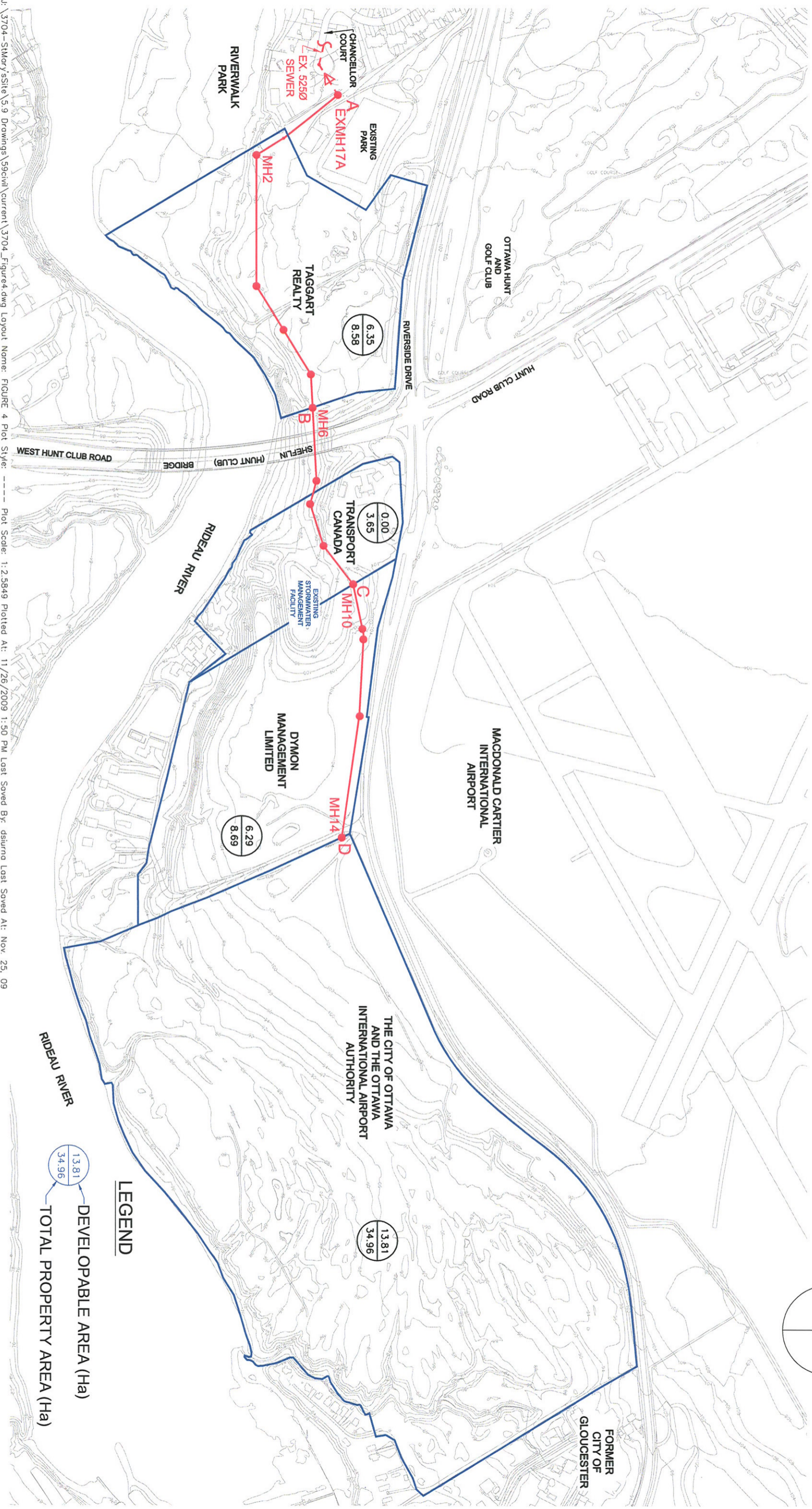
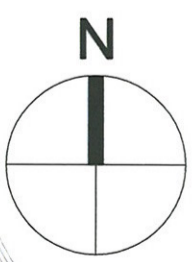
S A N I T A R Y S E W E R D E S I G N S H E E T

Flow Per Person: 450 litres per day, or
0.052 litres per second
0.28 litres per second per hectare
 Infiltration: 3.5 ppu single family
3.3 ppu townhouses
1.6 ppu apartments

DESIGN: J.I.M. PROJECT: Riverwalk Park - SHEET NO.
 CHECKED: W.B. J. Perez Corporation -
 DATE: Oct. 88 City of Ottawa 3625-3 1 of 2

Rev.: March 87 CUMMING-COCKBURN & ASSOCIATES LIMITED
 Consulting Municipal Engineers
 Toronto-Ottawa-Waterloo-London-Brockville

LOCATION	MANHOLE		INCREMENT					CUMULATIVE				INFILTRATION			PROFILE				
	FROM	TO	RES. UNITS	POP.	OTHER AREAS (ha)	AVG. FLOW L/Sec.	POP.	AVG. FLOW L/Sec.	PEAK FACTOR	PEAK FLOW L/Sec.	INCR. OF AREA (ha)	TOTAL AREA	FLOW L/Sec.	TOTAL FLOW L/Sec.	PIPE DIA. (mm)	GRADE (%)	VEL. M/Sec.	CAP. L/Sec.	LENGTH Metres
External (South)		17A		4842	-		4842	25.18	4.00	100.70	39.42	39.42	7.88	108.60	525	0.20	0.896	200.50	-
Street No. 2 (cul-de-sac)	17A	16A	5	18	39.42		4860	25.27	4.00	101.08	0.51	39.93	7.99	109.07	525	0.20	0.896	200.50	49.0
" " "	16A	15A	3	10	39.93		4870	25.32	4.00	101.30	0.37	40.30	8.06	109.40	525	0.20	0.896	200.50	53.0
" " "	15A	5A	2	7	40.30		4877	25.36	4.00	101.40	0.11	40.41	8.08	109.50	525	0.20	0.896	200.50	28.0
Street No. 1	2A	3A	hotel	365	0.21		365	1.90	6.00	11.40	1.15	1.36	0.27	11.65	250	0.50	0.863	43.61	59.5
	3A	4A	135	216	1.36		581	3.02	6.00	18.13	0.73	2.09	0.42	18.54	250	0.50	0.863	43.61	39.5
	4A	5A	-	-	2.09		581	3.02	6.00	18.13	0.06	2.15	0.43	18.55	250	2.80	1.929	97.70	31.0
	5A	6A	1	4	42.56		5462	28.40	4.00	113.60	0.10	42.66	8.53	122.10	525	0.20	0.896	200.50	38.5
	6A	7A	4 97	334	42.66		5796	30.14	4.00	120.60	1.09	43.75	8.75	129.30	525	0.20	0.896	200.50	80.0
	7A	8A	3 97	330	43.75		6126	31.86	4.00	127.40	1.29	45.04	9.01	136.40	525	0.20	0.896	200.50	76.5
	8A	9A	3	10	45.04		6136	31.91	4.00	127.60	0.24	45.28	9.06	136.70	525	0.20	0.896	200.50	74.0
	9A	10A	1 97	324	45.28		6460	33.59	4.00	134.40	1.01	46.29	9.26	143.60	525	0.20	0.896	200.50	31.5



LEGEND

13.81
34.96 — DEVELOPABLE AREA (Ha)

13.81
34.96 — TOTAL PROPERTY AREA (Ha)

J:\3704-StMary'sSite\5.9 Drawings\59civil\current\3704_Figure4.dwg Layout Name: FIGURE 4 Plot Style: --- Plot Scale: 1:2.5849 Plotted At: 11/26/2009 1:50 PM Last Saved By: dsurna Last Saved At: Nov. 25, 09

Scale

Project Title

Drawing Title

Sheet No.



1:5000

ST. MARY'S SITE

SANITARY DRAINAGE AREA PLAN

FIGURE 4



SANITARY SEWER DESIGN SHEET
 RIVERSIDE DRIVE LANDS
 SANITARY SEWER SERVICING STUDY
 CITY OF OTTAWA

JOB #: 15215-5.7.1
 DATE: NOV 07
 DESIGN: JIM

LOCATION			INDIVIDUAL				CUM. RES. FLOW			LIGHT INDUSTRIAL FLOW				INFILTRATION			TOTAL DESIGN FLOW (l/s)	PROPOSED SEWER						
STREET	FROM	TO	RESID. UNITS		RES. AREA (Ha)	POP.	POP.	PEAK FACT.	PEAK FLOW (l/s)	INCR. AREA (Ha)	CUM. AREA (Ha)	PEAK FACT.	PEAK FLOW (l/s)	INCR. AREA (Ha)	CUM. AREA (Ha)	FLOW (l/s)		CAP. l/s	PIPE (mm)	LGTH. (m)	SLOPE (%)	VEL. (full) m/s	AVAIL. CAP. (l/s)	AVAIL. CAP. (%)
			Singles	Towns/ Semis													Condo							
No External Drainage Areas																								
		Point D - MH 14																						
City of Ottawa/Airport Authority	Point D - MH 14	MH 11								13.81	13.81	1.50	11.99	13.81	13.81	3.87	15.85	39.22	250	280.0	0.40	0.77	23.36	60%
Dymon Management Limited	MH 11	Point B - MH 6								6.29	20.10	1.50	17.45	6.29	20.10	5.63	23.08	39.22	250	315.0	0.40	0.77	16.14	41%
Transport Canada/Hunt Club Road																								
	Point B - MH 6	MH 2								0.00	20.10	1.50	17.45	0.00	20.10	5.63	23.08	39.22	250	355.0	0.40	0.77	16.14	41%
Taggart Realty	MH 2	Point A Ex MH 17A								6.35	26.45	1.50	22.96	6.35	26.45	7.41	30.37	55.24	300	130.0	0.30	0.76	24.87	45%
																		200.67	525	0.0	0.20	0.90	200.67	100%
External Drainage Areas																								
Potential External Drainage Contribution		Point D - MH 14								65.00	65.00	1.50	56.42	65.00	65.00	18.20	74.62							
City of Ottawa/Airport Authority	Point D - MH 14	MH 11								13.81	78.81	1.50	68.41	13.81	78.81	22.07	90.48	100.21	375	280.0	0.30	0.88	9.74	10%
Dymon Management Limited	MH 11	Point B - MH 6								6.29	85.10	1.50	73.87	6.29	85.10	23.83	97.70	162.86	450	315.0	0.30	0.99	65.16	40%
Transport Canada/Hunt Club Road																								
	Point B - MH 6	MH 2								0.00	85.10	1.50	73.87	0.00	85.10	23.83	97.70	132.98	450	355.0	0.20	0.81	35.28	27%
Taggart Realty	MH 2	Point A Ex MH 17A								6.35	91.45	1.50	79.38	6.35	91.45	25.61	104.99	132.98	450	130.0	0.20	0.81	27.99	21%
																		200.67	525	0.0	0.20	0.90	200.67	100%

Where Q = average daily per capita flow (350 l/cap.d.) or (0.0041l/sec./cap)

I = Unit of peak extraneous flow (0.28 l/sec/ha)

M = Residential Peaking factor = Harmon Peaking Factor, $M = 1 + (14 / (4 + P^{0.5}))$, where P = population in thousands

Commercial Sanitary Flow Rate = 50,000 litres/hectare/day

Commercial Peaking Factor = 1.50

Revised Dec 03, 2007

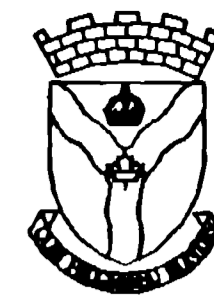


IBI GROUP
 400-333 Preston Street
 Ottawa, Ontario K1S 5N4 Canada
 tel 613 225 1311 fax 613 225 9868
 ibigroup.com

SANITARY SEWER DESIGN SHEET

Riverside Park
 CITY OF OTTAWA
 Taggart Realty Management

STREET	LOCATION			RESIDENTIAL										ICI AREAS						INFILTRATION ALLOWANCE						PROPOSED SEWER DESIGN										
	AREA ID	FROM MH	TO MH	AREA w/Units (Ha)	SF	SD	TH	APT	AREA w/o Units (Ha)	POPULATION IND	POPULATION CUM	PEAK FLOW (L/s)	INSTITUTIONAL IND	INSTITUTIONAL CUM	AREA (Ha) COMMERCIAL IND	AREA (Ha) COMMERCIAL CUM	INDUSTRIAL IND	INDUSTRIAL CUM	PEAK FLOW (L/s)	IND	CUM	AREA (Ha) IND	AREA (Ha) CUM	FLOW (L/s)	IND	CUM	FIXED FLOW (L/s) IND	FIXED FLOW (L/s) CUM	TOTAL FLOW (L/s)	CAPACITY (L/s)	LENGTH (m)	DIA (mm)	SLOPE (%)	VELOCITY (m/s)	AVAILABLE CAPACITY (L/s)	AVAILABLE CAPACITY (%)
		MH107A	MH106A	0.0					0.0	0.0	0.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	133.02	53.52	450	0.20	0.810	133.02	100.00%
		MH106A	MH105A	0.0					0.0	0.0	0.0	3.80	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	133.02	60.75	450	0.20	0.810	133.02	100.00%	
		UNIT 3	MH105A	0.89					0.0	0.0	0.0	3.80	0.00	0.00	0.89	0.89	0.00	0.00	0.43	0.43	0.89	0.89	0.29	0.00	0.00	0.00	0.00	0.73	34.22	12.00	200	1.00	1.055	33.49	97.88%	
		ACCESS ROAD	MH105A	0.80					0.0	0.0	0.0	3.80	0.00	0.00	0.89	0.89	0.00	0.00	0.43	0.80	1.69	0.56	0.00	0.00	0.00	0.00	0.00	0.99	133.02	47.86	450	0.20	0.810	132.03	99.26%	
		UNIT 2	MH104A	0.52					0.0	0.0	0.0	3.57	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.52	0.52	0.17	0.00	0.00	0.00	0.00	0.00	1.63	34.22	14.00	200	1.00	1.055	32.59	95.24%	
		UNIT 1A	MH103A	0.62					0.0	0.0	0.0	3.80	0.00	0.00	0.62	0.62	0.00	0.00	0.30	0.62	0.62	0.20	0.00	0.00	0.00	0.00	0.00	0.51	34.22	6.00	200	1.00	1.055	33.71	98.52%	
		MH104A	MH103A	0.0					0.0	0.0	0.0	3.57	0.00	0.00	0.00	0.00	0.00	0.00	0.73	0.00	2.83	0.93	0.00	0.00	0.00	0.00	0.00	3.13	133.02	85.61	450	0.20	0.810	129.89	97.65%	
		UNIT 1B	MH103A	0.56					0.0	0.0	0.0	3.80	0.00	0.56	0.56	0.00	0.00	0.00	0.27	0.56	0.56	0.18	0.00	0.00	0.00	0.00	0.00	0.46	34.22	22.60	200	1.00	1.055	33.76	98.66%	
		REVERA	MH103A	2.60					0.0	0.0	0.0	3.37	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.60	2.60	0.86	0.00	0.00	0.00	0.00	0.00	6.75	62.04	10.00	250	1.00	1.224	55.29	89.12%	
		MH103A	MH102A	0.0					0.0	0.0	0.0	3.33	0.00	0.56	0.56	0.00	0.00	0.00	1.01	0.00	5.99	1.98	0.00	0.00	0.00	0.00	0.00	10.16	133.02	77.80	450	0.20	0.810	122.86	92.36%	
		MH102A	MH101A	0.0					0.0	0.0	0.0	3.33	0.00	0.56	0.00	0.00	0.00	0.00	1.01	0.00	5.99	1.98	0.00	0.00	0.00	0.00	0.00	10.16	133.02	59.88	450	0.20	0.810	122.86	92.36%	
		MH101A	MH100A	0.0					0.0	0.0	0.0	3.33	0.00	0.56	0.00	0.00	0.00	0.00	1.01	0.00	5.99	1.98	0.00	0.00	0.00	0.00	0.00	10.16	398.60	59.08	450	1.30	2.062	328.44	97.00%	
		MH100A	EX/4/3	0.0					0.0	0.0	0.0	3.33	0.00	0.56	0.00	0.00	0.00	0.00	1.01	0.00	5.99	1.98	0.00	0.00	0.00	0.00	0.00	10.16	148.80	70.89	525	0.11	0.666	138.64	93.17%	
Design Parameters:				Notes:										ICI AREAS						PROPOSED SEWER DESIGN																
Residential				1. Mannings coefficient (n) = 0.013 2. Demand (per capita): 280 L/day 3. Infiltration allowance: 0.33 L/s/ha 4. Residential Peaking Factor: Hamon Formula = $1 + (14 / (4 + (P / 1000)^{0.5}))^{10.8}$ where P = population in thousands										Designed: JEB Checked: TRB Dwg Reference: 37923-501						Revision 1. 2018-03-28 1st City submission																
SF	3.4	pip/u	INST	28,000	L/ha/day	Peak Factor	1.5																													
TH/SD	2.7	pip/u	COM	28,000	L/ha/day	MCE Chart																														
APT	1.8	pip/u	IND	35,000	L/ha/day																															
Other	60	pip/ha		17000	L/ha/day																															
														File Reference: 37923-7.1						Date: 2018-03-28																
														Sheet No: 1 of 1																						

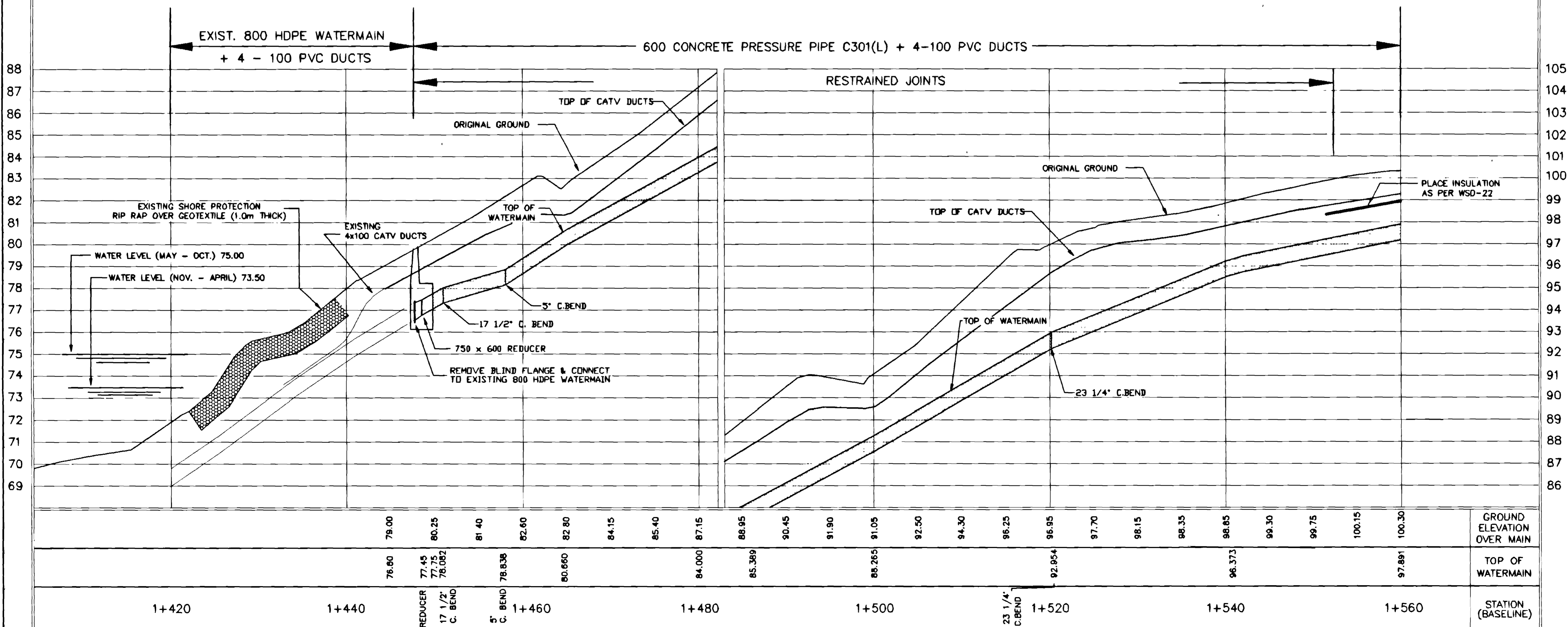
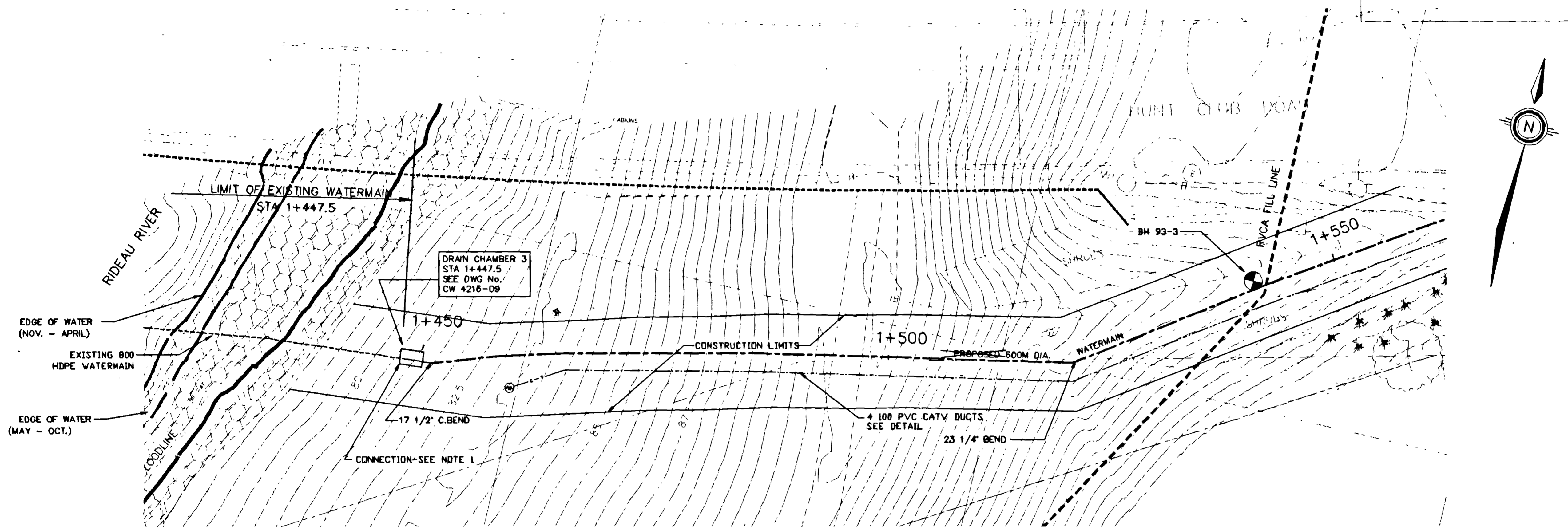


OTTAWA-CARLETON
ENVIRONMENT
and
TRANSPORTATION
DEPARTMENT

M.J.E. SHEFLIN, P.Eng.
ENVIRONMENT AND TRANSPORTATION
COMMISSIONER

CAUTION

THE LOCATION OF UTILITIES IS APPROXIMATE ONLY, AND THE EXACT LOCATION SHOULD BE DETERMINED BY CONSULTING THE MUNICIPAL AUTHORITIES AND UTILITY COMPANIES CONCERNED. THE CONTRACTOR IS RESPONSIBLE TO PROVIDE THE LOCATION AND STATUS OF UTILITIES AND SHALL BE RESPONSIBLE FOR ADEQUATE PROTECTION OF PLANT AND EQUIPMENT FROM DAMAGE.



A Almy Graham and Associates Limited
Consulting Engineers and Planners Others

Design by:	Date
CRG & GP	JUNE /95
Drawn by:	Date
CRG	JUNE /95

- Notes:
1. THE CONTRACTOR SHALL EXPOSE AND VERIFY THE LOCATION AND ELEVATION OF EXISTING WATERMANS AT POINTS OF CONNECTION PRIOR TO PREPARATION OF SHOP DRAWINGS.
 2. THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE DESIGN OF THRUST PROTECTION. SHOP DRAWINGS, SIGNED AND STAMPED BY AN ENGINEER, SHALL BE SUBMITTED FOR ALL THRUST PROTECTION.

SEE "AS BUILT" NOTE AT DWG.No. CW 4216-03

No	Revision	Date
1	AS PER "AS BUILT" INFO. (RMO; Drawn by P.G.)	MAY/96

Scales
HORIZ. 1:250
VERT. 1:100

Project Title
WATERMAIN CROSSING
RIDEAU RIVER
AT HUNT CLUB BRIDGE
PHASE II

4343-5
PLAN AND PROFILE
STA. 1+420 - STA. 1+560

Drawing No.:	Rev. No.:
CW 4216 - 06	1

APPENDIX C

S T O R M S E W E R D E S I G N S H E E T

Q = 2.78 AIC
 WHERE Q = Peak Flow in Litres Per Second (L/S)
 A = Area in Hectares (ha)
 I = Rainfall Intensity in Millimetres Per Hour (MM/HR)
 C = Runoff Coefficient

DESIGN n = .013
 Rev.: March 87
 Sept. 87

CUMMING-COCKBURN & ASSOCIATES LIMITED
 Consulting Municipal Engineers
 Toronto-Ottawa-Waterloo-London-Brockville

DESIGN: J.I.M.
 CHECKED: W.B.
 DATE: Oct. 86

PROJECT: Riverwalk Park -
 J. Perez Corporation -
 City of Ottawa 3625-3

SHEET NO.
 1 of 2

LOCATION		INCR. AREA				ACCUM. 2.78 Ac	CONCENTRATION TIME		RAINFALL INTENSITY I (MM/HR)	PEAK FLOW Q (L/S)	SEWER DATA						
		FROM M.H.	TO M.H.	HECTARE	"C"		2.78 Ac	IN PIPE			TOTAL	TYPE OF PIPE	PIPE SIZE	SLOPE %	LENGTH (M)	CAPACITY (L/S)	VELOCITY (M/S)
Street No. 1	1	2	0.12	0.80	0.27												
			0.20	0.70	0.39	0.66	15.00	0.26	15.26	80.00	52.80	Conc.	300	5.00	47.5	225.7	3.10
	2	3	1.34	0.70	2.61	3.27	15.26	0.43	15.69	79.50	260.00	Conc.	450	1.60	59.5	376.7	2.29
	3	4	0.43	0.70	0.84	4.11	15.69	0.29	15.98	78.00	320.60	Conc.	450	1.60	40.5	376.7	2.29
	4	5	0.06	0.70	0.12	4.23	15.98	0.18	16.16	77.00	325.70	Conc.	450	3.00	33.5	515.4	3.14
Street No. 2	17	15	0.88	0.45	1.10	1.10	15.00	0.95	15.95	80.00	88.00	Conc.	300	1.00	79.0	101.1	1.38
	15	5	0.11	0.45	0.14	1.24	15.95	0.31	16.26	78.00	96.72	Conc.	300	1.00	26.0	101.1	1.38
Street No. 1	5	6	0.10	0.45	0.13	5.60	16.26	0.21	16.47	77.00	431.20	Conc.	450	3.00	39.0	515.4	3.14
Assaly Property (Street No. 3)	-	14	3.41	0.62	5.87						T.C. = 19.87 min.						
Street No. 3	14	12	0.79	0.70	1.54	7.41	19.87	0.46	20.33	67.50	500.20	Conc.	750	0.25	35.0	580.6	1.27
Street No. 1	13	12	0.14	0.80	0.31												
			0.16	0.70	0.31	0.62	12.00	0.37	12.37	92.00	57.04	Conc.	300	4.00	62.0	201.9	2.77
	12	11	1.62	0.70	3.15	11.18	20.33	0.46	20.79	66.70	745.70	Conc.	750	1.20	77.5	1272.0	2.79

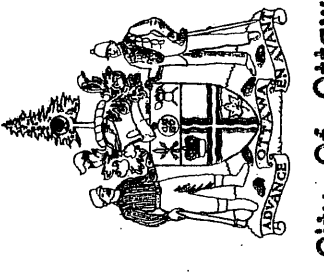
S T O R M S E W E R D E S I G N S H E E T

Q = 2.78 AIC
 WHERE Q = Peak Flow in Litres Per Second (L/S)
 A = Area in Hectares (ha)
 I = Rainfall Intensity in Millimetres Per Hour (MM/HR)
 C = Runoff Coefficient

DESIGN: J.I.M.	PROJECT: Riverwalk Park -	SHEET NO.
CHECKED: W.B.	J. Perez Corporation -	
DATE: Oct. 86	City of Ottawa 3625-3	2 of 2

DESIGN n = .013 Rev.: March 87 CUMMING-COCKBURN & ASSOCIATES LIMITED
 March 31/87 Consulting Municipal Engineers
 Sept. 87 Toronto-Ottawa-Waterloo-London-Brockville

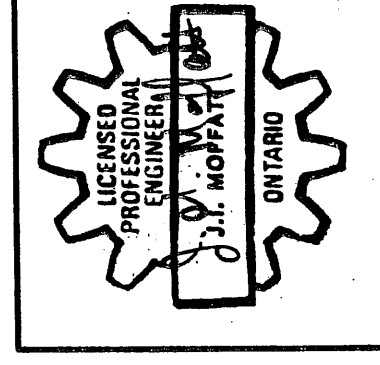
LOCATION				INCR. AREA				CONCENTRATION TIME			RAINFALL INTENSITY	PEAK FLOW	SEWER DATA					
STREET	FROM M.H.	TO M.H.	HECTARE	"C"	2.78 Ac	ACCU. 2.78 Ac	INLET PIPE	IN PIPE	TOTAL	I (MM/HR)	Q (L/S)	TYPE OF PIPE	PIPE SIZE	SLOPE %	LENGTH (M)	CAPACITY (L/S)	VELOCITY (M/S)	
																		INLET PIPE
	11	10	0.32	0.70	0.62	11.80	20.79	0.22	20.01	65.70	775.30	Conc.	750	1.20	37.5	1272.0	2.79	
Assaly Property		North 10 Bulkhead	6.77	0.70	13.17													
Street No. 1	10	8	0.35	0.45	0.44	13.20	23.13	0.28	23.41	61.70	814.40	Conc.	1050	0.20	24.0	1274.0	1.43	
	8	7	0.90	0.70	1.75	26.75	23.41	1.17	24.58	70.80	1894.00	Conc.	1500	0.15	110.0	2857.0	1.57	
			1.04	0.70	2.02	29.08	24.58	0.76	25.34	68.60	1995.00	Conc.	1500	0.15	72.0	2857.0	1.57	
	7	6	0.30	0.45	0.38	29.46	25.34	0.88	26.22	67.40	1986.00	Conc.	1500	0.15	82.5	2857.0	1.57	
	6	28	0.79	0.70	1.54	36.60	26.22	1.52	27.74	66.00	2416.00	Conc.	1500	0.20	165.5	3296.0	1.81	
St. Mary's Cement							T.C. = 15.00 + 300m/1.50m/sec. = 18.33 min.											
	26	28	7.00	0.70	13.62	13.62	18.33	2.08	20.41	71.00	967.00	Conc.	900	0.30	197.5	1034.0	1.58	
	28	outlet	-	-	-	50.22	27.74	0.29	28.03	68.70	3450.00	Conc.	1500	0.25	34.8	3687.0	2.03	



City of Ottawa
 Department of Physical Environment
 Engineering And Surveys Branch

Revisions:

No.	Description	Drawn By	Checked By
1	ISSUE FOR PERMITTING	D.D.	D.D.
2	REVISE ASSALY AREA	M.M.	M.M.
3	REVISE ASSALY AREA	M.M.	M.M.



Prepared By: J.J.M.
 Checked By: W.R. Cole
 Date: 11/11/03

Scale: 1:750
 Date: 11/11/03

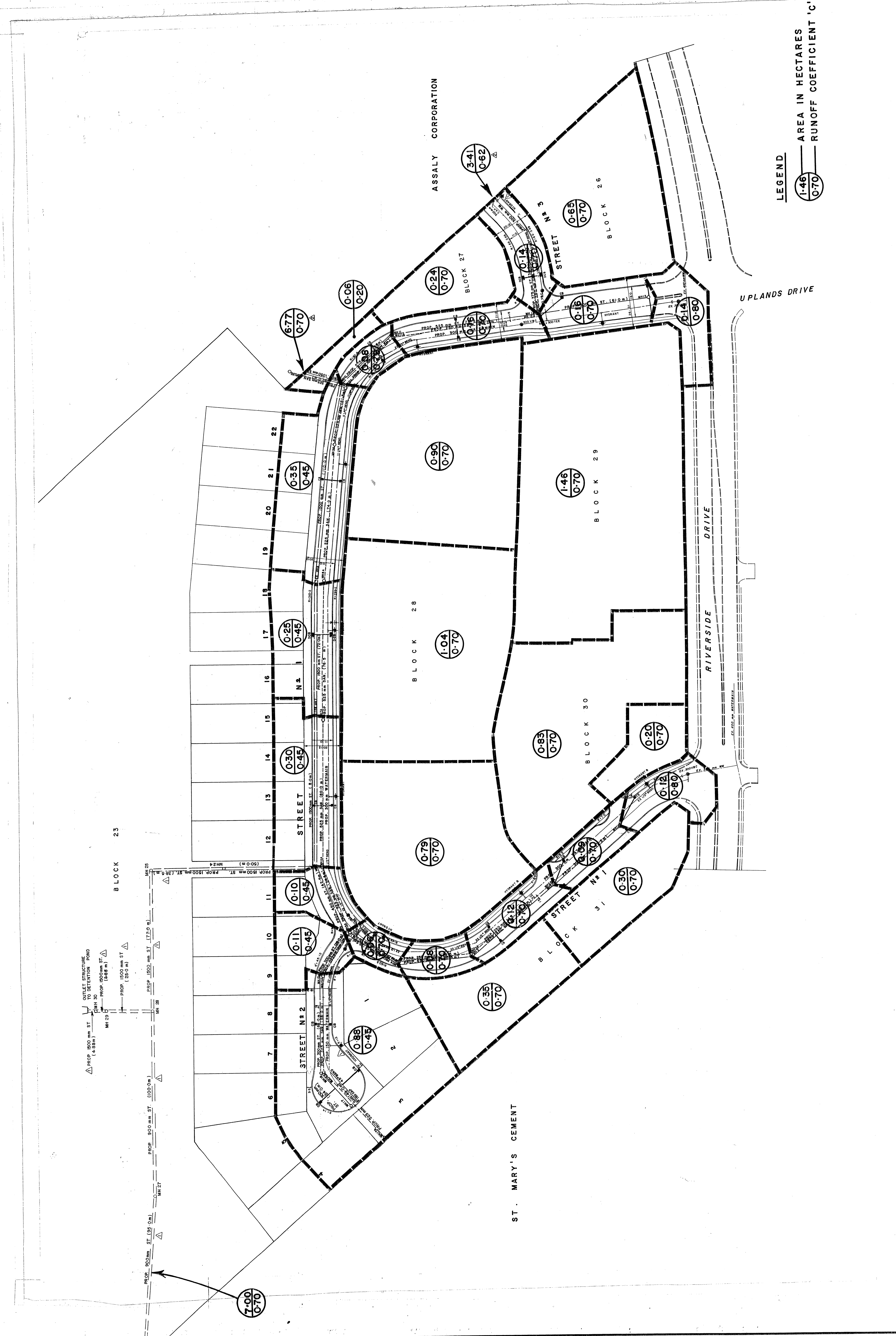
Project Name: STORM DRAINAGE AREA PLAN
 Location: RIVERWALK PARK

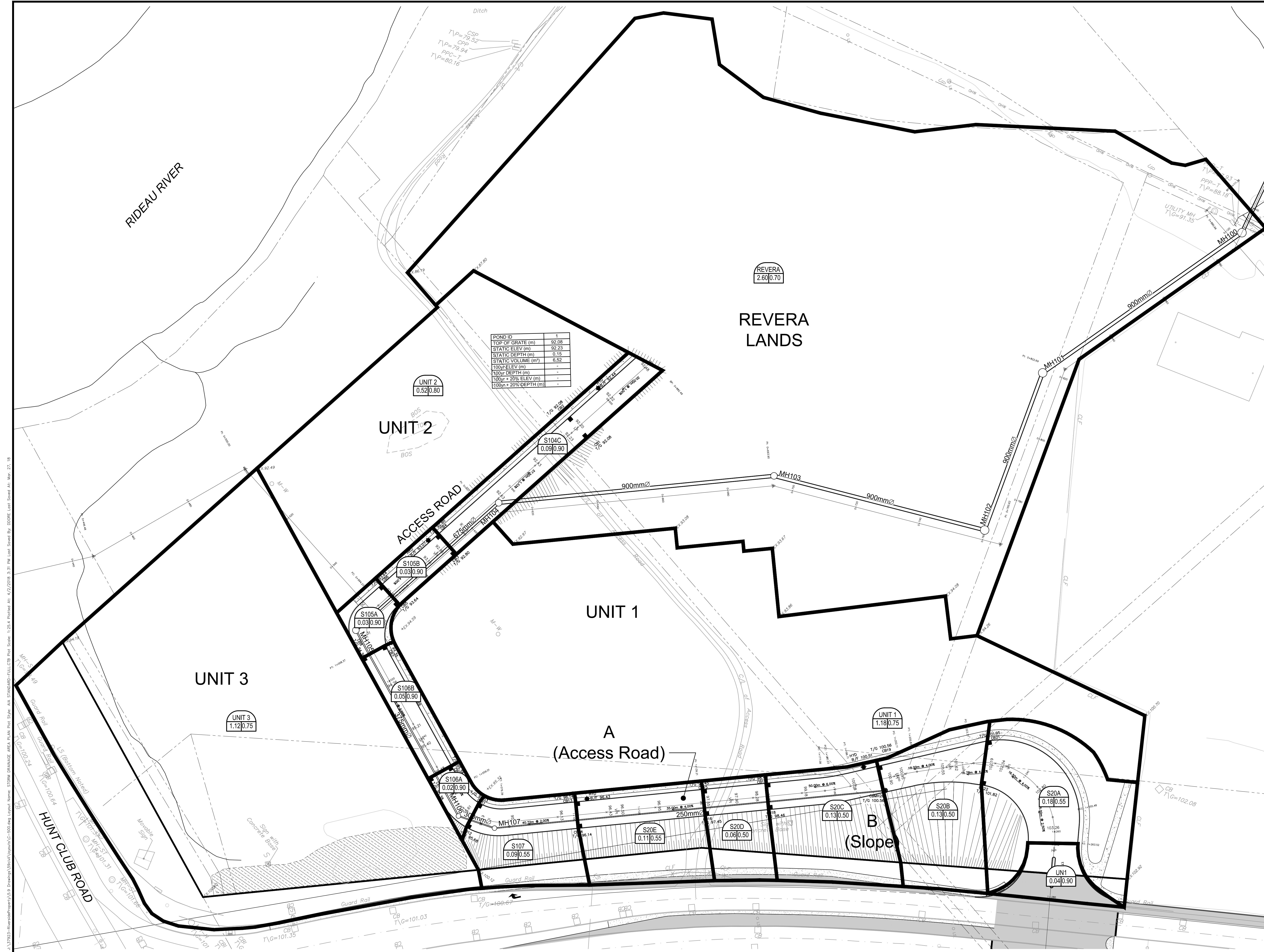
Design And Construction Division

W.R. Cole
 P. Eng.

J. PEREZ CORPORATION - RIVERWALK PARK

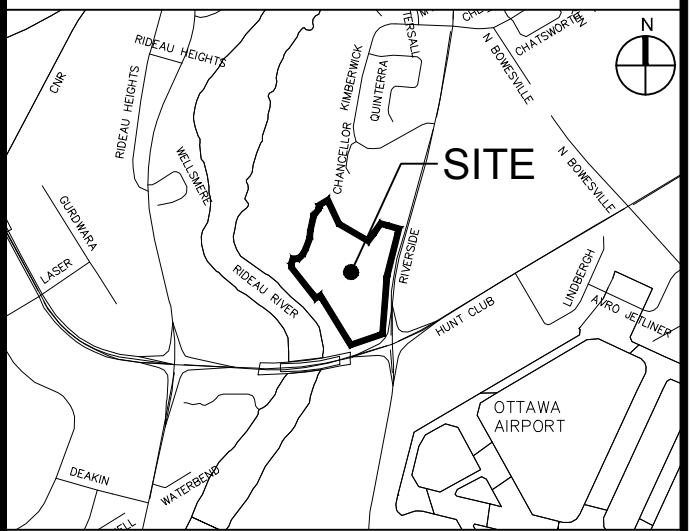
Scale: 1:750
 Date: 11/11/03





LEGEND:

- AREA NUMBER
- RUN OFF COEFFICIENT
- AREA IN HECTARES
- AREA BOUNDARY

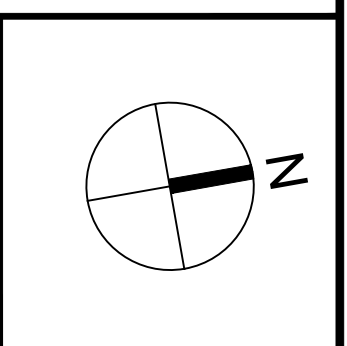
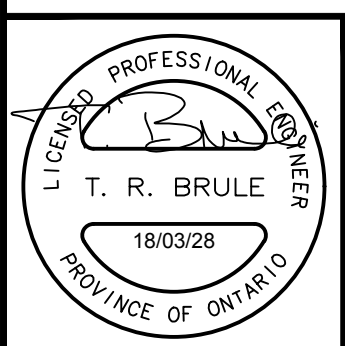


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1	ISSUED FOR CITY APPROVAL	T.R.B.	2018.04.03
No.	REVISIONS	By	Date



IBI GROUP
 400 - 333 Preston Street
 Ottawa ON K1S 5N4 Canada
 tel 613 225 1311 fax 613 225 9868
 ibigroup.com

Project Title
RIVERSIDE PARK
 3930 & 3960 RIVERSIDE DR.



Drawing Title
STORM DRAINAGE
AREA PLAN

Scale
 1 : 500

Design
 J.E.B. Date
 MARCH 2018

Drawn
 D.D. / E.H. Checked
 T.R.B.

Project No.
37923 Drawing No.
C-500

J:\37923-RiversidePark\37923-StormDrainage\37923-StormDrainage-AREA PLAN (Final) - 180328.dwg Date: 18/03/2018 3:31 PM User: J.E.B. Plot Scale: 1:250 Plot Size: 11.00 x 16.00 Plot Date: 18/03/2018 3:31 PM Plot Speed: 100 Plot Style: AIA STANDARD - FULL CTB Plot Source: 1:250.4 Printed At: 4/7/2018 3:31 PM User: J.E.B. Plot Speed: 100 Plot Style: AIA STANDARD - FULL CTB Plot Source: 1:250.4 Printed At: 4/7/2018 3:31 PM User: J.E.B. Plot Speed: 100 Plot Style: AIA STANDARD - FULL CTB Plot Source: 1:250.4 Printed At: 4/7/2018 3:31 PM

CITY PLAN No. ###
 CITY FILE No. ###

STREET	LOCATION			AREA (Ha)										RATIONAL DESIGN FLOW										SEWER DATA										
	AREA ID	FROM	TO	C= 0.20	C= 0.25	C= 0.40	C= 0.55	C= 0.60	C= 0.65	C= 0.70	C= 0.75	C= 0.80	C= 0.90	IND 2.78AC	CUM 2.78AC	INLET (mm)	TIME IN PIPE	TOTAL (min)	I (2) (mm/hr)	I (5) (mm/hr)	I (10) (mm/hr)	I (100) (mm/hr)	2YR PEAK FLOW (L/s)	5YR PEAK FLOW (L/s)	10YR PEAK FLOW (L/s)	100YR PEAK FLOW (L/s)	FIXED FLOW (L/s)	DESIGN FLOW (L/s)	CAPACITY (L/s)	LENGTH (m)	PIPE SIZE (mm)	SLOPE (%)	VELOCITY (m/s)	AVAIL CAP (L/s)
Access Road	S206, S208, S209, S210, S211, S212, S213, S214, S215, S216, S217, S218, S219, S220, S221, S222, S223, S224, S225, S226, S227, S228, S229, S230, S231, S232, S233, S234, S235, S236, S237, S238, S239, S240, S241, S242, S243, S244, S245, S246, S247, S248, S249, S250, S251, S252, S253, S254, S255, S256, S257, S258, S259, S260, S261, S262, S263, S264, S265, S266, S267, S268, S269, S270, S271, S272, S273, S274, S275, S276, S277, S278, S279, S280, S281, S282, S283, S284, S285, S286, S287, S288, S289, S290, S291, S292, S293, S294, S295, S296, S297, S298, S299, S300, S301, S302, S303, S304, S305, S306, S307, S308, S309, S310, S311, S312, S313, S314, S315, S316, S317, S318, S319, S320, S321, S322, S323, S324, S325, S326, S327, S328, S329, S330, S331, S332, S333, S334, S335, S336, S337, S338, S339, S340, S341, S342, S343, S344, S345, S346, S347, S348, S349, S350, S351, S352, S353, S354, S355, S356, S357, S358, S359, S360, S361, S362, S363, S364, S365, S366, S367, S368, S369, S370, 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S2031, S2032, S2033, S2034, S2035, S2036, S2037, S2038, S2039, S2040, S2041, S2042, S2043, S2044, S2045, S2046, S2047, S2048, S2049, S2050, S2051, S2052, S2053, S2054, S2055, S2056, S2057, S2058, S2059, S2060, S2061, S2062, S2063, S2064, S2065, S2066, S2067, S2068, S2069, S2070, S2071, S2072, S2073, S2074, S2075, S2076, S2077, S2078, S2079, S2080, S2081, S2082, S2083, S2084, S2085, S2086, S2087, S2088, S2089, S2090, S2091, S2092, S2093, S2094, S2095, S2096, S2097, S2098, S2099, S2100, S2101, S2102, S2103, S2104, S2105, S2106, S2107, S2108, S2109, S2110, S2111, S2112, S2113, S2114, S2115, S2116, S2117, S2118, S2119, S2120, S2121, S2122, S2123, S2124, S2125, S2126, S2127, S2128, S2129, S2130, S2131, S2132, S2133, S2134, S2135, S2136, S2137, S2138, S2139, S2140, S2141, S2142, S2143, S2144, S2145, S2146, S2147, S2148, S2149, S2150, S2151, S2152, S2153, S2154, S2155, S2156, S2157, S2158, S2159, S2160, S2161, S2162, S2163, S2164, S2165, S2166, S2167, S2168, S2169, S2170, S2171, S2172, S2173, 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37923-3CHI 2. OUT

* D D S W M M (release 2.1) *
* The Dual Drainage Storm Water Management Model *
* Copyright *
* ----- *
* AMK Associates International Ltd. *

August, 2004

IBI Group
Ottawa, Ontario
(S/N DM00691207)

This release of DDSWMM will run with a maximum of

- 500 minor system segments (pipes), including outlets
- 500 major system (street) segments, including outlets
- 500 subcatchments
- 30 storage units for the minor system
- 30 storage units for the major system
- 300 computational time steps
- 300 increments for rainfall hyetograph
- 50 storm inlet types
- 20 points describing the inlet capture curve
- 50 major system segment types
- 5 street segments discharging into a street junction
- 5 pipes discharging into a pipe junction
- 5 subcatchments discharging into a major system segment
- 5 inlet groups discharging into a pipe
- 30 unit area hydrographs

For other program constraints, please refer to the users manual

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

RUN CONTROL PARAMETERS

Measuring units		Metric
Time increment for calculation	10.00	minutes
Number of computational steps	19	
Default limiting capacity of inlets	*****	l/s
Total simulation time	3: 0	(hrs: mins)
Interval between printout	1	

Calculation for the minor system is not included in this simulation

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

10015 RAINFALL DATA

Initial Julian Date

0.00 hours

Initial Time

(mm/hr) Time Rainfall
(hr: min) (mm/hr)

Rainfall intensity

0.46E+02 0.61E+02 0.77E+02

0.00E+00 0.15E+02 0.31E+02

0: 0	0.00	*
0: 10	2.82	**
0: 20	3.50	***
0: 30	4.69	****
0: 40	7.30	*****
0: 50	18.21	*****
1: 0	76.81	*****
1: 10	24.08	*****
1: 20	12.36	*****
1: 30	8.32	*****
1: 40	6.30	*****
1: 50	5.09	****
2: 0	4.29	***
2: 10	3.72	***
2: 20	3.29	***
2: 30	2.95	**
2: 40	2.68	**
2: 50	2.46	**
3: 0	2.28	**

0.46E+02 0.61E+02 0.77E+02

0.00E+00 0.15E+02 0.31E+02

Rainfall duration 3: 10 (hrs: mins.)

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Height of Curb (cm)	Manning (n)	Long. Slope (m/m)	Shoulder Cross Slope (m/m)	Shoulder Roughness (n)
1 35.0	4.00	0.030	15.0	0.0130	0.009	0.030	0.0250

RATING CURVE

Depth (cm)	Flow (cms)	Spread (m)
0.00	0.00	0.00
1.75	0.00	0.58
3.50	0.02	1.17
5.25	0.07	1.75
7.00	0.16	2.33
8.75	0.28	2.92
10.50	0.46	3.50
12.25	0.69	4.00
14.00	0.98	4.00
15.75	1.33	4.25
17.50	1.72	4.83
19.25	2.16	5.42
21.00	2.67	6.00
22.75	3.23	6.58
24.50	3.85	7.17
26.25	4.54	7.75
28.00	5.30	8.33
29.75	6.12	8.92
31.50	7.01	9.50
33.25	7.97	10.08
35.00	9.01	10.67

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Height of Curb (cm)	Manning (n)	Long. Slope (m/m)	Shoulder Cross Slope (m/m)	Shoulder Roughness (n)
2 35.0	4.00	0.030	15.0	0.0130	0.013	0.030	0.0250

RATING CURVE

Depth (cm)	Flow (cms)	Spread (m)
0.00	0.00	0.00
1.75	0.00	0.58
3.50	0.03	1.17
5.25	0.09	1.75
7.00	0.18	2.33
8.75	0.33	2.92
10.50	0.54	3.50
12.25	0.82	4.00
14.00	1.17	4.00
15.75	1.57	4.25
17.50	2.03	4.83
19.25	2.56	5.42
21.00	3.16	6.00
22.75	3.82	6.58
24.50	4.56	7.17
26.25	5.37	7.75
28.00	6.27	8.33
29.75	7.24	8.92
31.50	8.29	9.50
33.25	9.43	10.08
35.00	10.66	10.67

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM RATING CURVE

Type Maximum	Pavement	Pavement	Height	Manning	Long.	Shoulder	Shoulder
-----------------	----------	----------	--------	---------	-------	----------	----------

Flow Depth (cm)	Width (m)	Cross Slope (m/m)	37923-3CHI 2. OUT of Curb (cm)	(n)	Slope (m/m)	Cross Slope (m/m)	Roughness (n)
3 35.0	4.00	0.030	15.0	0.0130	0.020	0.030	0.0250

RATING CURVE

Depth (cm)	Flow (cms)	Spread (m)
0.00	0.00	0.00
1.75	0.01	0.58
3.50	0.04	1.17
5.25	0.11	1.75
7.00	0.23	2.33
8.75	0.41	2.92
10.50	0.67	3.50
12.25	1.01	4.00
14.00	1.43	4.00
15.75	1.92	4.25
17.50	2.49	4.83
19.25	3.14	5.42
21.00	3.87	6.00
22.75	4.69	6.58
24.50	5.59	7.17
26.25	6.59	7.75
28.00	7.68	8.33
29.75	8.88	8.92
31.50	10.17	9.50
33.25	11.57	10.08
35.00	13.07	10.67

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Height of Curb (cm)	Manning (n)	Long. Slope (m/m)	Shoulder Cross Slope (m/m)	Shoulder Roughness (n)
4	4.00	0.030	15.0	0.0130	0.030	0.030	0.0250

35.0

37923-3CHI 2. OUT

RATING CURVE

Depth (cm)	Flow (cms)	Spread (m)
0.00	0.00	0.00
1.75	0.01	0.58
3.50	0.04	1.17
5.25	0.13	1.75
7.00	0.28	2.33
8.75	0.50	2.92
10.50	0.82	3.50
12.25	1.23	4.00
14.00	1.75	4.00
15.75	2.35	4.25
17.50	3.05	4.83
19.25	3.84	5.42
21.00	4.73	6.00
22.75	5.73	6.58
24.50	6.84	7.17
26.25	8.06	7.75
28.00	9.40	8.33
29.75	10.85	8.92
31.50	12.43	9.50
33.25	14.14	10.08
35.00	15.99	10.67

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Height of Curb (cm)	Manning (n)	Long. Slope (m/m)	Shoulder Cross Slope (m/m)	Shoulder Roughness (n)
5 35.0	4.00	0.030	15.0	0.0130	0.040	0.030	0.0250

RATING CURVE

Depth	Flow	Spread
-------	------	--------

37923-3CHI 2. OUT (cm)	(cms)	(m)
0.00	0.00	0.00
1.75	0.01	0.58
3.50	0.05	1.17
5.25	0.15	1.75
7.00	0.32	2.33
8.75	0.58	2.92
10.50	0.94	3.50
12.25	1.42	4.00
14.00	2.02	4.00
15.75	2.72	4.25
17.50	3.53	4.83
19.25	4.44	5.42
21.00	5.48	6.00
22.75	6.63	6.58
24.50	7.91	7.17
26.25	9.32	7.75
28.00	10.87	8.33
29.75	12.55	8.92
31.50	14.38	9.50
33.25	16.36	10.08
35.00	18.49	10.67

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Height of Curb (cm)	Manning (n)	Long. Slope (m/m)	Shoulder Cross Slope (m/m)	Shoulder Roughness (n)
6 35.0	4.00	0.030	15.0	0.0130	0.060	0.030	0.0250

RATING CURVE

Depth (cm)	Flow (cms)	Spread (m)
0.00	0.00	0.00
1.75	0.01	0.58
3.50	0.06	1.17
5.25	0.18	1.75
7.00	0.39	2.33
8.75	0.71	2.92

37923-3CHI 2. OUT		
10.50	1.16	3.50
12.25	1.74	4.00
14.00	2.47	4.00
15.75	3.33	4.25
17.50	4.32	4.83
19.25	5.44	5.42
21.00	6.71	6.00
22.75	8.12	6.58
24.50	9.69	7.17
26.25	11.42	7.75
28.00	13.31	8.33
29.75	15.37	8.92
31.50	17.61	9.50
33.25	20.04	10.08
35.00	22.65	10.67

‡

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Height of Curb (cm)	Manning (n)	Long. Slope (m/m)	Shoulder Cross Slope (m/m)	Shoulder Roughness (n)
7 35.0	4.00	0.030	15.0	0.0130	0.005	0.030	0.0250

RATING CURVE

Depth (cm)	Flow (cms)	Spread (m)
0.00	0.00	0.00
1.75	0.00	0.58
3.50	0.02	1.17
5.25	0.05	1.75
7.00	0.11	2.33
8.75	0.21	2.92
10.50	0.33	3.50
12.25	0.50	4.00
14.00	0.71	4.00
15.75	0.96	4.25
17.50	1.25	4.83
19.25	1.57	5.42
21.00	1.94	6.00
22.75	2.34	6.58

37923-3CHI 2. OUT		
24.50	2.80	7.17
26.25	3.30	7.75
28.00	3.84	8.33
29.75	4.44	8.92
31.50	5.08	9.50
33.25	5.78	10.08
35.00	6.54	10.67

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Height of Curb (cm)	Manning (n)	Long. Slope (m/m)	Shoulder Cross Slope (m/m)	Shoulder Roughness (n)
8 35.0	4.00	0.030	15.0	0.0130	0.000	0.030	0.0250

RATING CURVE

Depth (cm)	Flow (cms)	Spread (m)
0.00	0.00	0.00
1.75	0.00	0.58
3.50	0.00	1.17
5.25	0.01	1.75
7.00	0.02	2.33
8.75	0.03	2.92
10.50	0.05	3.50
12.25	0.07	4.00
14.00	0.10	4.00
15.75	0.14	4.25
17.50	0.18	4.83
19.25	0.22	5.42
21.00	0.27	6.00
22.75	0.33	6.58
24.50	0.40	7.17
26.25	0.47	7.75
28.00	0.54	8.33
29.75	0.63	8.92
31.50	0.72	9.50
33.25	0.82	10.08
35.00	0.92	10.67

♀

Example

DUAL DRAINAGE SIMULATION

STORM INLET DATA

1 Normal Inlet
 Inlet Identification No. 1
 No. of Points on Capture Curve 3

Inlet Capture Relationship

Approach Flow (l/s)	Inlet Flow (l/s)
0.00	0.00
10.00	10.00
99999.00	99999.00

2 Normal Inlet
 Inlet Identification No. 2
 No. of Points on Capture Curve 8

Inlet Capture Relationship

Approach Flow (l/s)	Inlet Flow (l/s)
0.00	0.00
71.00	16.00
104.00	24.00
148.00	31.50
270.00	45.50
470.00	57.00
690.00	67.50
1000.00	67.50

3 Normal Inlet
 Inlet Identification No. 3
 No. of Points on Capture Curve 8

Inlet Capture Relationship

Approach Flow (l/s)	Inlet Flow (l/s)
---------------------	------------------

37923-3CHI 2. OUT

Flow (l/s)	Flow (l/s)
0.00	0.00
78.00	17.50
111.00	24.50
161.00	32.00
296.00	45.00
510.00	57.00
780.00	66.50
1000.00	66.50

4 Normal Inlet

Inlet Identification No. 4

No. of Points on Capture Curve 8

Inlet Capture Relationship

Approach Flow (l/s)	Inlet Flow (l/s)
0.00	0.00
50.00	13.50
71.00	20.00
102.00	26.50
195.00	41.00
330.00	55.00
510.00	65.50
1000.00	65.50

5 Normal Inlet

Inlet Identification No. 5

No. of Points on Capture Curve 8

Inlet Capture Relationship

Approach Flow (l/s)	Inlet Flow (l/s)
0.00	0.00
36.00	10.00
52.00	15.50
74.00	20.50
135.00	34.50
230.00	50.00
350.00	62.00
1000.00	62.00

6 Normal Inlet

Inlet Identification No. 6

No. of Points on Capture Curve 8

Inlet Capture Relationship

37923-3CHI 2. OUT

		Approach Flow (l/s)	Inlet Flow (l/s)
		0.00	0.00
		62.00	15.50
		88.00	23.00
		122.00	30.00
		230.00	44.00
		400.00	57.00
		620.00	67.00
		1000.00	67.00
7	Normal Inlet		
	Inlet Identification No.		7
	No. of Points on Capture Curve		8

Inlet Capture Relationship

		Approach Flow (l/s)	Inlet Flow (l/s)
		0.00	0.00
		36.00	10.00
		52.00	15.50
		74.00	20.50
		135.00	34.50
		230.00	50.00
		350.00	62.00
		1000.00	62.00

8	Storage Inlet		
	Inlet Identification No.		8
	Maximum Storage		280.00 cu. m.
	No. of Points on Storage-Capture Curve		3

Storage-Inlet Capture Relationship

		Storage Volume (cu. m)	Inlet Flow (l/s)
		0.00	0.00
		0.01	107.99
		280.00	108.00

9	Storage Inlet		
	Inlet Identification No.		9

37923-3CHI 2. OUT

Maximum Storage 125.00 cu. m.

No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
0.01	196.99
125.00	197.00

10 Storage Inlet

Inlet Identification No. 10

Maximum Storage 140.00 cu. m.

No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
0.01	49.99
140.00	50.00

11 Storage Inlet

Inlet Identification No. 11

Maximum Storage 6.52 cu. m.

No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
0.01	87.99
6.52	88.00

12 Storage Inlet

Inlet Identification No. 12

37923-3CHI 2. OUT

Maximum Storage 540.00 cu. m.

No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
0.01	251.99
540.00	252.00

‡

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DATA

Flow History	Street Segment	D/S Segment	Length (m)	Type	No. of C. B.	Inlet Type	Limiting Inlet Capture (l/s)	Connecting Pipe/EXTRAN Inlet
(?)								
YES	1 S20A	S20B	38.0	5	2	2 *	6.00	CBMH20
YES	2 S20B	S20C	31.0	5	2	2 *	6.00	CBMH20
YES	3 S20C	S20D	34.0	6	2	3 *	6.00	CBMH20
YES	4 S20D	S20E	19.0	5	2	2 *	6.00	CBMH20
YES	5 S20E	S107	39.0	3	2	4 *	6.00	107
YES	6 S107	S106A	32.0	3	2	4 *	6.00	107
YES	7 S106A	S106B	18.0	1	2	5 *	6.00	106
YES	8 S106B	S105A	42.0	4	2	6 *	6.00	106
YES	9 UNIT3	OUT1	252.0	7	2	8 ***	108.00	105
YES	10 S105A	S105B	24.0	5	2	1 *	12.50	105
YES	11 S105B	S104	23.0	2	2	7 *	6.00	105
YES	12 UNIT1	S104	266.0	7	2	9 ***	197.00	104
YES	13 UNIT2	OUT2	117.0	7	2	10 ***	50.00	104
YES	14 S104	D1	81.0	1	2	11 ***	88.00	104

37923-3CHI 2. OUT

YES	15	D1	REVERA	26.0	8	0	1 *	0.00	PDUM
YES	16	REVERA	OUT3	585.0	7	2	12 ***	252.00	104
YES									

* Normal Inlet.

** Storage Inlet with linear relationship between Storage and Inlet Capture.

*** Storage Inlet with user-specified relationship between Storage and Inlet Capture.

Total Number of Street segments	16	
Total Length of Major System	1627.00	m
Total Number of Inlet C. B.	30	
Average Distance Between Inlets	108.47	m

Outlets From Major System

Outlet I. D.

- OUT1
- OUT2
- OUT3

Total Number of Outlets from Major System = 3

No. of Detention Structures 0

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

SUB-CATCHMENT/SURFACE RUNOFF DATA

Infiltration Parameters

Max. Infiltration Rate	76.20	mm/hr
Min. Infiltration Rate	13.20	mm/hr
Decay Rate	0.001150	1/sec.

Unit Area Hydrograph (UAH) Data

No Unit Area Hydrograph Data

37923-3CHI 2. OUT

SUB-CATCHMENT DATA

No. Dep.	Subarea Storage	Street Flow	Segment	Area (Ha.)	Imp. (%)	Manning (N)	Manning (N)	Slope (m/m)	Width (m)
Imp. (mm)	Perv. (mm)	History (?)				(Imp.)	(Perv.)		
1.500	4.670	NO	S20A	0.18	50.	0.0130	0.2500	0.020	20.
1.500	4.670	NO	S20B	0.13	43.	0.0130	0.2500	0.020	25.
1.500	4.670	NO	S20C	0.13	43.	0.0130	0.2500	0.020	20.
1.500	4.670	NO	S20D	0.06	43.	0.0130	0.2500	0.020	20.
1.500	4.670	NO	S20E	0.11	50.	0.0130	0.2500	0.020	15.
1.500	4.670	NO	S107	0.09	50.	0.0130	0.2500	0.020	15.
1.500	4.670	NO	S106A	0.02	100.	0.0130	0.2500	0.020	5.
1.500	4.670	NO	S106B	0.05	100.	0.0130	0.2500	0.020	5.
1.500	4.670	NO	UNIT3	1.12	79.	0.0130	0.2500	0.020	126.
1.500	4.670	NO	S105A	0.03	100.	0.0130	0.2500	0.020	6.
1.500	4.670	NO	S105B	0.03	100.	0.0130	0.2500	0.020	5.
1.500	4.670	NO	UNIT1	1.18	79.	0.0130	0.2500	0.020	133.
1.500	4.670	NO	UNIT2	0.52	86.	0.0130	0.2500	0.020	58.
1.500	4.670	NO	S104	0.09	100.	0.0130	0.2500	0.020	5.
1.500	4.670	NO	REVERA	2.60	71.	0.0130	0.2500	0.020	292.

* Inflow Hydrograph Input Directly

** Inflow hydrograph Input in terms of flow per unit area

Total Drainage Area 6.34 Hectares

Number of Subcatchments 15

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

Simulation Details - Surface Runoff - 15 Subareas

count Subarea

37923-3CHI 2. OUT

- 1 AS20A
- 2 AS20B
- 3 AS20C
- 4 AS20D
- 5 AS20E
- 6 AS107
- 7 AS106A
- 8 AS106B
- 9 AUNI T3
- 10 AS105A
- 11 AS105B
- 12 AUNI T1
- 13 AUNI T2
- 14 AS104
- 15 AREVERA

†

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

Simulation Details - Major System - 19 Segments/Outlets

count	order	segment	time step (min.)	No. of time steps	Max. flow (cms)	Max. depth (cm)
1	1	S20A	0.56	323	0.01	2.03
2	2	S20B	0.42	427	0.02	2.30
3	3	S20C	0.38	477	0.03	2.30
4	4	S20D	0.25	726	0.02	2.44
5	5	S20E	0.62	293	0.03	3.06
6	6	S107	0.51	355	0.03	3.04
7	7	S106A	0.38	472	0.02	3.41
8	8	S106B	0.61	293	0.02	2.56
9	10	S105A	0.32	560	0.02	2.35
10	12	UNI T1	4.57	40	0.14	7.55
11	11	S105B	0.64	281	0.00	1.76
12	14	S104	2.01	89	0.02	2.74
13	15	D1	2.01	89	0.00	0.00
14	16	REVERA	8.41	22	0.29	9.86
15	13	UNI T2	2.44	74	0.07	5.66
16	9	UNI T3	4.38	41	0.13	7.41

37923-3CHI 2. OUT

17	19	OUT3	0.00
18	18	OUT2	0.00
19	17	OUT1	0.00

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

EXTRAN Interface File Information

Inlet flows are stored at the following 6 inlets (EXTRAN nodes):

CBMH20	107	106	105	104	PDUM
--------	-----	-----	-----	-----	------

DDSWMM-EXTRAN Connectivity

EXTRAN Inlet	DDSWMM Inlets (Major System Segments)				
CBMH20	S20A	S20B	S20C	S20D	
107	S20E	S107			
106	S106A	S106B			
105	UNIT3	S105A	S105B		
104	UNIT1	UNIT2	S104	REVERA	
PDUM	D1				

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment S20A

Time (hr: min)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 40	0.000	0.001	0.001	0.000	0.000	0.2	0.00
0: 50	0.000	0.003	0.003	0.001	0.002	0.7	0.00

37923-3CHI 2. OUT

1: 0	0.000	0.015	0.015	0.003	0.011	2.0	0.00
1: 10	0.000	0.012	0.012	0.003	0.009	1.9	0.00
1: 20	0.000	0.002	0.002	0.001	0.003	0.5	0.00
1: 30	0.000	0.003	0.003	0.001	0.002	0.6	0.00
1: 40	0.000	0.002	0.002	0.000	0.002	0.4	0.00
1: 50	0.000	0.001	0.001	0.000	0.001	0.3	0.00
2: 0	0.000	0.001	0.001	0.000	0.001	0.3	0.00
2: 10	0.000	0.001	0.001	0.000	0.001	0.2	0.00
2: 20	0.000	0.001	0.001	0.000	0.001	0.2	0.00
2: 30	0.000	0.001	0.001	0.000	0.001	0.2	0.00
2: 40	0.000	0.001	0.001	0.000	0.001	0.2	0.00
2: 50	0.000	0.001	0.001	0.000	0.001	0.1	0.00
3: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
Maximum	0.000		0.015	0.003	0.011	2.0	0.00
Time (h: mi n)	0: 0		1: 0	1: 1	1: 1		

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment S20B

Time (hr: mi n)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 40	0.000	0.001	0.001	0.000	0.000	0.2	0.00
0: 50	0.002	0.002	0.005	0.001	0.003	1.0	0.00
1: 0	0.011	0.010	0.021	0.005	0.016	2.3	0.00
1: 10	0.009	0.007	0.016	0.004	0.012	2.1	0.00
1: 20	0.003	0.001	0.004	0.001	0.004	0.9	0.00
1: 30	0.002	0.002	0.004	0.001	0.003	0.8	0.00
1: 40	0.002	0.001	0.002	0.001	0.002	0.5	0.00
1: 50	0.001	0.001	0.002	0.000	0.002	0.5	0.00
2: 0	0.001	0.001	0.002	0.000	0.001	0.4	0.00
2: 10	0.001	0.001	0.001	0.000	0.001	0.3	0.00
2: 20	0.001	0.001	0.001	0.000	0.001	0.3	0.00
2: 30	0.001	0.000	0.001	0.000	0.001	0.3	0.00
2: 40	0.001	0.000	0.001	0.000	0.001	0.2	0.00
2: 50	0.001	0.000	0.001	0.000	0.001	0.2	0.00
3: 0	0.000	0.000	0.000	0.000	0.001	0.1	0.00
Maximum	0.011		0.021	0.005	0.017	2.3	0.00
Time (h: mi n)	1: 1		1: 1	1: 1	1: 1		

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment S20C

Time (hr: min)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 40	0.000	0.001	0.001	0.000	0.000	0.2	0.00
0: 50	0.003	0.002	0.006	0.001	0.004	1.0	0.00
1: 0	0.016	0.010	0.026	0.006	0.019	2.3	0.00
1: 10	0.012	0.007	0.019	0.004	0.015	2.1	0.00
1: 20	0.004	0.001	0.005	0.001	0.005	0.9	0.00
1: 30	0.003	0.002	0.005	0.001	0.004	0.8	0.00
1: 40	0.002	0.001	0.003	0.001	0.003	0.6	0.00
1: 50	0.002	0.001	0.003	0.001	0.002	0.5	0.00
2: 0	0.001	0.001	0.002	0.000	0.002	0.4	0.00
2: 10	0.001	0.001	0.002	0.000	0.001	0.3	0.00
2: 20	0.001	0.001	0.002	0.000	0.001	0.3	0.00
2: 30	0.001	0.000	0.001	0.000	0.001	0.3	0.00
2: 40	0.001	0.000	0.001	0.000	0.001	0.2	0.00
2: 50	0.001	0.000	0.001	0.000	0.001	0.2	0.00
3: 0	0.001	0.000	0.001	0.000	0.001	0.1	0.00
Maximum Time (h: min)	0.017		0.026	0.006	0.020	2.3	0.00
	1: 1		1: 1	1: 1	1: 1		

†

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment S20D

Time (hr: min)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
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37923-3CHI 2. OUT

0: 0	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 40	0.000	0.000	0.001	0.000	0.000	0.000	0.2	0.00
0: 50	0.004	0.001	0.005	0.001	0.004	0.004	1.1	0.00
1: 0	0.019	0.005	0.024	0.005	0.018	0.018	2.4	0.00
1: 10	0.015	0.003	0.018	0.004	0.014	0.014	2.2	0.00
1: 20	0.005	0.000	0.005	0.001	0.004	0.004	1.1	0.00
1: 30	0.004	0.001	0.004	0.001	0.003	0.003	1.0	0.00
1: 40	0.003	0.000	0.003	0.001	0.002	0.002	0.6	0.00
1: 50	0.002	0.000	0.002	0.001	0.002	0.002	0.5	0.00
2: 0	0.002	0.000	0.002	0.000	0.002	0.002	0.4	0.00
2: 10	0.001	0.000	0.002	0.000	0.001	0.001	0.4	0.00
2: 20	0.001	0.000	0.002	0.000	0.001	0.001	0.3	0.00
2: 30	0.001	0.000	0.001	0.000	0.001	0.001	0.3	0.00
2: 40	0.001	0.000	0.001	0.000	0.001	0.001	0.3	0.00
2: 50	0.001	0.000	0.001	0.000	0.001	0.001	0.2	0.00
3: 0	0.001	0.000	0.001	0.000	0.001	0.001	0.2	0.00
Maximum Time (h: mi n)	0.020 1: 1		0.025 1: 1	0.006 1: 2	0.019 1: 2		2.4	0.00

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment S20E

Time (hr: mi n)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 40	0.000	0.001	0.001	0.000	0.000	0.3	0.00
0: 50	0.004	0.002	0.006	0.001	0.004	1.8	0.00
1: 0	0.018	0.009	0.028	0.007	0.019	3.0	0.00
1: 10	0.014	0.007	0.021	0.006	0.016	2.6	0.00
1: 20	0.004	0.001	0.006	0.002	0.005	1.8	0.00
1: 30	0.003	0.002	0.005	0.001	0.004	1.6	0.00
1: 40	0.002	0.001	0.003	0.001	0.003	1.1	0.00
1: 50	0.002	0.001	0.003	0.001	0.002	0.9	0.00
2: 0	0.002	0.001	0.002	0.001	0.002	0.7	0.00
2: 10	0.001	0.001	0.002	0.001	0.001	0.6	0.00
2: 20	0.001	0.001	0.002	0.000	0.001	0.5	0.00
2: 30	0.001	0.000	0.002	0.000	0.001	0.5	0.00
2: 40	0.001	0.000	0.001	0.000	0.001	0.4	0.00
2: 50	0.001	0.000	0.001	0.000	0.001	0.4	0.00
3: 0	0.001	0.000	0.001	0.000	0.001	0.2	0.00

37923-3CHI 2. OUT

Maximum 0.019 0.028 0.008 0.021 3.1 0.00
 Time (h: mi n) 1: 2 1: 2 1: 2 1: 2

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Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment S107

Time (hr: mi n)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 40	0.000	0.001	0.001	0.000	0.000	0.2	0.00
0: 50	0.004	0.002	0.006	0.001	0.004	1.8	0.00
1: 0	0.019	0.008	0.027	0.007	0.019	3.0	0.00
1: 10	0.016	0.006	0.021	0.006	0.016	2.7	0.00
1: 20	0.005	0.001	0.006	0.002	0.005	1.8	0.00
1: 30	0.004	0.001	0.005	0.001	0.004	1.6	0.00
1: 40	0.003	0.001	0.003	0.001	0.003	1.1	0.00
1: 50	0.002	0.001	0.003	0.001	0.002	0.9	0.00
2: 0	0.002	0.001	0.002	0.001	0.002	0.7	0.00
2: 10	0.001	0.000	0.002	0.001	0.002	0.6	0.00
2: 20	0.001	0.000	0.002	0.000	0.001	0.5	0.00
2: 30	0.001	0.000	0.002	0.000	0.001	0.5	0.00
2: 40	0.001	0.000	0.001	0.000	0.001	0.4	0.00
2: 50	0.001	0.000	0.001	0.000	0.001	0.4	0.00
3: 0	0.001	0.000	0.001	0.000	0.001	0.2	0.00

Maximum 0.021 0.028 0.008 0.020 3.0 0.00
 Time (h: mi n) 1: 2 1: 2 1: 3 1: 3

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Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment S106A

37923-3CHI 2. OUT

Time (hr: min)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 40	0.000	0.000	0.000	0.000	0.000	0.2	0.00
0: 50	0.004	0.001	0.005	0.001	0.003	1.8	0.00
1: 0	0.019	0.003	0.022	0.006	0.016	3.3	0.00
1: 10	0.016	0.003	0.018	0.005	0.013	3.0	0.00
1: 20	0.005	0.001	0.006	0.002	0.005	1.9	0.00
1: 30	0.004	0.001	0.004	0.001	0.003	1.8	0.00
1: 40	0.003	0.000	0.003	0.001	0.002	1.4	0.00
1: 50	0.002	0.000	0.002	0.001	0.002	1.1	0.00
2: 0	0.002	0.000	0.002	0.001	0.001	0.9	0.00
2: 10	0.002	0.000	0.002	0.000	0.001	0.8	0.00
2: 20	0.001	0.000	0.002	0.000	0.001	0.7	0.00
2: 30	0.001	0.000	0.001	0.000	0.001	0.6	0.00
2: 40	0.001	0.000	0.001	0.000	0.001	0.5	0.00
2: 50	0.001	0.000	0.001	0.000	0.001	0.5	0.00
3: 0	0.001	0.000	0.001	0.000	0.001	0.3	0.00
Maximum Time (h: min)	0.020 1: 3		0.023 1: 3	0.007 1: 3	0.017 1: 3	3.4	0.00

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Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment S106B

Time (hr: min)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 40	0.000	0.000	0.000	0.000	0.000	0.1	0.00
0: 50	0.003	0.001	0.005	0.001	0.003	1.2	0.00
1: 0	0.016	0.007	0.023	0.005	0.016	2.5	0.00
1: 10	0.013	0.007	0.021	0.005	0.016	2.4	0.00
1: 20	0.005	0.002	0.007	0.002	0.006	1.7	0.00
1: 30	0.003	0.001	0.005	0.001	0.004	1.2	0.00
1: 40	0.002	0.001	0.003	0.001	0.003	0.9	0.00
1: 50	0.002	0.001	0.003	0.001	0.002	0.7	0.00
2: 0	0.001	0.001	0.002	0.001	0.002	0.6	0.00

37923-3CHI 2. OUT

2: 10	0.001	0.001	0.002	0.000	0.001	0.5	0.00
2: 20	0.001	0.001	0.002	0.000	0.001	0.4	0.00
2: 30	0.001	0.000	0.001	0.000	0.001	0.4	0.00
2: 40	0.001	0.000	0.001	0.000	0.001	0.3	0.00
2: 50	0.001	0.000	0.001	0.000	0.001	0.3	0.00
3: 0	0.001	0.000	0.001	0.000	0.001	0.2	0.00

Maximum	0.017		0.024	0.006	0.018	2.6	0.00
Time (h: mi n)	1: 3		1: 3	1: 4	1: 4		

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Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Examp l e

DUAL DRAI NAGE SI MULATI ON

MAJOR SYSTEM DETAILED SIMULATI ON RESULTS

Major System Segment UNIT3

Time (hr: mi n)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 40	0.000	0.007	0.007	0.000	0.000	2.3	0.00
0: 50	0.000	0.029	0.029	0.010	0.000	4.1	0.00
1: 0	0.000	0.135	0.135	0.080	0.000	7.4	0.01
1: 10	0.000	0.121	0.121	0.108	0.000	7.1	10.66
1: 20	0.000	0.030	0.030	0.108	0.000	4.1	6.74
1: 30	0.000	0.025	0.025	0.021	0.000	3.9	0.00
1: 40	0.000	0.018	0.018	0.033	0.000	3.5	0.00
1: 50	0.000	0.014	0.014	0.008	0.000	3.1	0.00
2: 0	0.000	0.012	0.012	0.024	0.000	2.8	0.00
2: 10	0.000	0.010	0.010	0.002	0.000	2.6	0.00
2: 20	0.000	0.009	0.009	0.020	0.000	2.5	0.00
2: 30	0.000	0.008	0.008	-0.001	0.000	2.3	0.00
2: 40	0.000	0.007	0.007	0.017	0.000	2.3	0.00
2: 50	0.000	0.007	0.007	-0.002	0.000	2.2	0.00
3: 0	0.000	0.000	0.000	0.017	0.000	0.0	0.00

Maximum	0.000		0.135	0.108	0.000	7.4	10.66
Time (h: mi n)	0: 0		1: 0	1: 10	3: 0		

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Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Examp l e

DUAL DRAI NAGE SI MULATI ON

37923-3CHI 2. OUT

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment S105A

Time (hr: min)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 40	0.000	0.000	0.000	0.000	0.000	0.1	0.00
0: 50	0.003	0.001	0.004	0.004	0.000	0.9	0.00
1: 0	0.016	0.005	0.021	0.020	0.000	2.3	0.00
1: 10	0.016	0.004	0.020	0.020	0.000	2.2	0.00
1: 20	0.006	0.001	0.007	0.007	0.000	1.5	0.00
1: 30	0.004	0.001	0.005	0.005	0.000	1.0	0.00
1: 40	0.003	0.001	0.003	0.003	0.000	0.7	0.00
1: 50	0.002	0.000	0.003	0.003	0.000	0.6	0.00
2: 0	0.002	0.000	0.002	0.002	0.000	0.5	0.00
2: 10	0.001	0.000	0.002	0.002	0.000	0.4	0.00
2: 20	0.001	0.000	0.002	0.002	0.000	0.3	0.00
2: 30	0.001	0.000	0.001	0.001	0.000	0.3	0.00
2: 40	0.001	0.000	0.001	0.001	0.000	0.3	0.00
2: 50	0.001	0.000	0.001	0.001	0.000	0.3	0.00
3: 0	0.001	0.000	0.001	0.001	0.000	0.2	0.00
Maximum Time (h: min)	0.018 1: 4		0.022 1: 4	0.022 1: 4	0.000 1: 4	2.3	0.00

♀ Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment S105B

Time (hr: min)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 40	0.000	0.000	0.000	0.000	0.000	0.1	0.00
0: 50	0.000	0.001	0.001	0.000	0.001	0.4	0.00
1: 0	0.000	0.005	0.005	0.001	0.003	1.8	0.00

37923-3CHI 2. OUT

1: 10	0.000	0.004	0.004	0.001	0.003	1.5	0.00
1: 20	0.000	0.001	0.001	0.000	0.001	0.4	0.00
1: 30	0.000	0.001	0.001	0.000	0.001	0.3	0.00
1: 40	0.000	0.001	0.001	0.000	0.001	0.2	0.00
1: 50	0.000	0.000	0.000	0.000	0.000	0.2	0.00
2: 0	0.000	0.000	0.000	0.000	0.000	0.2	0.00
2: 10	0.000	0.000	0.000	0.000	0.000	0.1	0.00
2: 20	0.000	0.000	0.000	0.000	0.000	0.1	0.00
2: 30	0.000	0.000	0.000	0.000	0.000	0.1	0.00
2: 40	0.000	0.000	0.000	0.000	0.000	0.1	0.00
2: 50	0.000	0.000	0.000	0.000	0.000	0.1	0.00
3: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00

Maximum	0.000		0.005	0.001	0.003	1.8	0.00
Time (h: mi n)	2: 20		1: 0	1: 1	1: 1		

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment UNIT1

Time (hr: mi n)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 40	0.000	0.008	0.008	0.000	0.000	2.3	0.00
0: 50	0.000	0.031	0.031	0.009	0.000	4.2	0.00
1: 0	0.000	0.142	0.142	0.081	0.000	7.5	0.00
1: 10	0.000	0.127	0.127	0.134	0.000	7.3	0.01
1: 20	0.000	0.032	0.032	0.082	0.000	4.2	0.00
1: 30	0.000	0.027	0.027	0.032	0.000	3.9	0.00
1: 40	0.000	0.019	0.019	0.025	0.000	3.6	0.00
1: 50	0.000	0.015	0.015	0.018	0.000	3.2	0.00
2: 0	0.000	0.013	0.013	0.015	0.000	2.9	0.00
2: 10	0.000	0.011	0.011	0.012	0.000	2.7	0.00
2: 20	0.000	0.009	0.009	0.011	0.000	2.5	0.00
2: 30	0.000	0.008	0.008	0.009	0.000	2.4	0.00
2: 40	0.000	0.008	0.008	0.008	0.000	2.3	0.00
2: 50	0.000	0.007	0.007	0.008	0.000	2.2	0.00
3: 0	0.000	0.000	0.000	0.008	0.000	0.0	0.00

Maximum	0.000		0.142	0.140	0.000	7.5	0.01
Time (h: mi n)	0: 0		1: 0	1: 5	3: 0		

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment UNIT2

Time (hr: min)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 40	0.000	0.004	0.004	0.001	0.000	1.8	0.00
0: 50	0.000	0.014	0.014	0.010	0.000	3.1	0.00
1: 0	0.000	0.067	0.067	0.050	0.000	5.7	0.93
1: 10	0.000	0.062	0.062	0.050	0.000	5.5	8.97
1: 20	0.000	0.016	0.016	0.050	0.000	3.3	6.72
1: 30	0.000	0.013	0.013	0.016	0.000	2.9	0.00
1: 40	0.000	0.009	0.009	0.009	0.000	2.5	0.00
1: 50	0.000	0.007	0.007	0.010	0.000	2.3	0.00
2: 0	0.000	0.006	0.006	0.005	0.000	2.1	0.00
2: 10	0.000	0.005	0.005	0.008	0.000	2.0	0.00
2: 20	0.000	0.005	0.005	0.003	0.000	2.0	0.00
2: 30	0.000	0.004	0.004	0.006	0.000	1.9	0.00
2: 40	0.000	0.004	0.004	0.002	0.000	1.8	0.00
2: 50	0.000	0.003	0.003	0.006	0.000	1.8	0.00
3: 0	0.000	0.000	0.000	0.001	0.000	0.0	0.00
Maximum Time (h: min)	0.000 0: 0		0.067 1: 0	0.050 1: 10	0.000 3: 0	5.7	8.97

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Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment S104

Time (hr: min)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00

37923-3CHI 2. OUT

0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 40	0.000	0.000	0.000	0.000	0.000	0.2	0.00
0: 50	0.001	0.002	0.002	0.001	0.000	1.1	0.00
1: 0	0.003	0.011	0.014	0.011	0.000	2.6	0.00
1: 10	0.003	0.013	0.016	0.015	0.000	2.7	0.00
1: 20	0.001	0.005	0.006	0.008	0.000	1.9	0.00
1: 30	0.001	0.003	0.004	0.004	0.000	1.7	0.00
1: 40	0.001	0.002	0.003	0.003	0.000	1.2	0.00
1: 50	0.000	0.002	0.002	0.002	0.000	0.9	0.00
2: 0	0.000	0.001	0.002	0.002	0.000	0.8	0.00
2: 10	0.000	0.001	0.001	0.002	0.000	0.6	0.00
2: 20	0.000	0.001	0.001	0.001	0.000	0.6	0.00
2: 30	0.000	0.001	0.001	0.001	0.000	0.5	0.00
2: 40	0.000	0.001	0.001	0.001	0.000	0.4	0.00
2: 50	0.000	0.001	0.001	0.001	0.000	0.4	0.00
3: 0	0.000	0.000	0.000	0.001	0.000	0.1	0.00

Maximum Time (h: mi n)	0.003		0.016	0.016	0.000	2.7	0.00
	1: 1		1: 10	1: 12	3: 0		

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment D1

Time (hr: mi n)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 40	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 50	0.000	0.000	0.000	0.000	0.000	0.0	0.00
1: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
1: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
1: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
1: 30	0.000	0.000	0.000	0.000	0.000	0.0	0.00
1: 40	0.000	0.000	0.000	0.000	0.000	0.0	0.00
1: 50	0.000	0.000	0.000	0.000	0.000	0.0	0.00
2: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
2: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
2: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
2: 30	0.000	0.000	0.000	0.000	0.000	0.0	0.00
2: 40	0.000	0.000	0.000	0.000	0.000	0.0	0.00
2: 50	0.000	0.000	0.000	0.000	0.000	0.0	0.00
3: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00

37923-3CHI 2. OUT

Maximum 0.000 0.000 0.000 0.000 0.0 0.00
 Time (h:mi n) 3: 0 3: 0 0: 0 0: 0

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Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment REVERA

Time (hr:mi n)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 40	0.000	0.016	0.016	0.000	0.000	3.3	0.00
0: 50	0.000	0.063	0.063	0.000	0.000	5.6	0.00
1: 0	0.000	0.287	0.287	0.025	0.000	9.9	0.00
1: 10	0.000	0.249	0.249	0.252	0.000	9.4	4.32
1: 20	0.000	0.060	0.060	0.241	0.000	5.5	0.01
1: 30	0.000	0.053	0.053	0.076	0.000	5.3	0.00
1: 40	0.000	0.038	0.038	0.085	0.000	4.5	0.00
1: 50	0.000	0.030	0.030	0.017	0.000	4.1	0.00
2: 0	0.000	0.025	0.025	0.060	0.000	3.8	0.00
2: 10	0.000	0.021	0.021	0.002	0.000	3.7	0.00
2: 20	0.000	0.018	0.018	0.049	0.000	3.5	0.00
2: 30	0.000	0.016	0.016	-0.006	0.000	3.3	0.00
2: 40	0.000	0.015	0.015	0.044	0.000	3.2	0.00
2: 50	0.000	0.014	0.014	-0.010	0.000	3.0	0.00
3: 0	0.000	0.000	0.000	0.046	0.000	0.0	0.00

Maximum 0.000 0.287 0.252 0.000 9.9 4.32
 Time (h:mi n) 0: 0 1: 0 1: 10 3: 0

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM

SUMMARY OF SIMULATION RESULTS

No. Max.	Segment	Peak Flow	Peak Time	Max. Depth	Max. Capture	Inlet Restriction	D/S Pipe
----------	---------	-----------	-----------	------------	--------------	-------------------	----------

37923-3CHI 2. OUT

Storage

(cu. m.)	(cms)	(hr: mi n.)	(cm)	(l /s)	(?)	
1 S20A 0.00	0.015	1: 0	2.03	3.34	NO	CBMH20
2 S20B 0.00	0.021	1: 1	2.30	4.80	NO	CBMH20
3 S20C 0.00	0.026	1: 1	2.30	5.83	NO	CBMH20
4 S20D 0.00	0.025	1: 1	2.44	5.58	NO	CBMH20
5 S20E 0.00	0.028	1: 2	3.06	7.59	NO	107
6 S107 0.00	0.028	1: 2	3.04	7.51	NO	107
7 S106A 0.00	0.023	1: 3	3.41	6.51	NO	106
8 S106B 0.00	0.024	1: 3	2.56	5.98	NO	106
9 UNI T3 10.66	0.135	1: 0	7.41	107.99	N/A	105
10 S105A 0.00	0.022	1: 4	2.35	22.46	NO	105
11 S105B 0.00	0.005	1: 0	1.76	1.31	NO	105
12 UNI T1 0.01	0.142	1: 0	7.55	139.84	N/A	104
13 UNI T2 8.97	0.067	1: 0	5.66	49.99	N/A	104
14 S104 0.00	0.016	1: 10	2.74	15.57	N/A	104
15 D1 0.00	0.000	3: 0	0.00	0.00	-	PDUM
16 REVERA 4.32	0.287	1: 0	9.86	251.99	N/A	104

*** SIMULATI ON ENDED NORMALLY ***

†

```

*****
*
*   Simulation Starting Date      March   29, 18
*                               Time      13: 25: 50.85
*
*   Simulation Ending   Date      March   29, 18
*                               Time      13: 25: 53.69
*
*   Duration of Simulation          0.05 Minutes
*
*****

```

Data Files

Input Data File Name 37923-3CHI 2. DAT
Output File Name 37923-3CHI 2. OUT
EXTRAN Interface (ASCII) File Name 37923-3CHI 2. TXT

37923-3CHI 100. OUT

* D D S W M M (release 2.1) *
* The Dual Drainage Storm Water Management Model *
* Copyright *
* ----- *
* AMK Associates International Ltd. *

August, 2004

IBI Group
Ottawa, Ontario
(S/N DM00691207)

This release of DDSWMM will run with a maximum of

- 500 minor system segments (pipes), including outlets
- 500 major system (street) segments, including outlets
- 500 subcatchments
- 30 storage units for the minor system
- 30 storage units for the major system
- 300 computational time steps
- 300 increments for rainfall hyetograph
- 50 storm inlet types
- 20 points describing the inlet capture curve
- 50 major system segment types
- 5 street segments discharging into a street junction
- 5 pipes discharging into a pipe junction
- 5 subcatchments discharging into a major system segment
- 5 inlet groups discharging into a pipe
- 30 unit area hydrographs

For other program constraints, please refer to the users manual

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

RUN CONTROL PARAMETERS

Measuring units		Metric
Time increment for calculation	10.00	minutes
Number of computational steps	19	
Default limiting capacity of inlets	*****	l/s
Total simulation time	3: 0	(hrs: mins)
Interval between printout	1	

Calculation for the minor system is not included in this simulation

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

10015 RAINFALL DATA

Initial Julian Date

0.00 hours

Initial Time

(mm/hr) Time Rainfall
(hr: min) (mm/hr)

Rainfall intensity

0.11E+03 0.14E+03 0.18E+03

0.00E+00 0.36E+02 0.71E+02

0: 0	0.00	*
0: 10	6.05	**
0: 20	7.54	***
0: 30	10.16	****
0: 40	15.97	*****
0: 50	40.65	*****
1: 0	178.56	*****
1: 10	54.05	*****
1: 20	27.32	*****
1: 30	18.24	*****
1: 40	13.74	****
1: 50	11.06	****
2: 0	9.28	***
2: 10	8.02	***
2: 20	7.08	**
2: 30	6.35	**
2: 40	5.76	**
2: 50	5.28	**
3: 0	4.88	**

0.11E+03 0.14E+03 0.18E+03

0.00E+00 0.36E+02 0.71E+02

Rainfall duration 3: 10 (hrs: mins.)

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Height of Curb (cm)	Manning (n)	Long. Slope (m/m)	Shoulder Cross Slope (m/m)	Shoulder Roughness (n)
1 35.0	4.00	0.030	15.0	0.0130	0.009	0.030	0.0250

RATING CURVE

Depth (cm)	Flow (cms)	Spread (m)
0.00	0.00	0.00
1.75	0.00	0.58
3.50	0.02	1.17
5.25	0.07	1.75
7.00	0.16	2.33
8.75	0.28	2.92
10.50	0.46	3.50
12.25	0.69	4.00
14.00	0.98	4.00
15.75	1.33	4.25
17.50	1.72	4.83
19.25	2.16	5.42
21.00	2.67	6.00
22.75	3.23	6.58
24.50	3.85	7.17
26.25	4.54	7.75
28.00	5.30	8.33
29.75	6.12	8.92
31.50	7.01	9.50
33.25	7.97	10.08
35.00	9.01	10.67

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Height of Curb (cm)	Manning (n)	Long. Slope (m/m)	Shoulder Cross Slope (m/m)	Shoulder Roughness (n)
2 35.0	4.00	0.030	15.0	0.0130	0.013	0.030	0.0250

RATING CURVE

Depth (cm)	Flow (cms)	Spread (m)
0.00	0.00	0.00
1.75	0.00	0.58
3.50	0.03	1.17
5.25	0.09	1.75
7.00	0.18	2.33
8.75	0.33	2.92
10.50	0.54	3.50
12.25	0.82	4.00
14.00	1.17	4.00
15.75	1.57	4.25
17.50	2.03	4.83
19.25	2.56	5.42
21.00	3.16	6.00
22.75	3.82	6.58
24.50	4.56	7.17
26.25	5.37	7.75
28.00	6.27	8.33
29.75	7.24	8.92
31.50	8.29	9.50
33.25	9.43	10.08
35.00	10.66	10.67

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM RATING CURVE

Type Maximum	Pavement	Pavement	Height	Manning	Long.	Shoulder	Shoulder
-----------------	----------	----------	--------	---------	-------	----------	----------

Flow Depth (cm)	Width (m)	Cross Slope (m/m)	37923-3CHI 100. OUT of Curb (cm)	(n)	Slope (m/m)	Cross Slope (m/m)	Roughness (n)
3 35.0	4.00	0.030	15.0	0.0130	0.020	0.030	0.0250

RATING CURVE

Depth (cm)	Flow (cms)	Spread (m)
0.00	0.00	0.00
1.75	0.01	0.58
3.50	0.04	1.17
5.25	0.11	1.75
7.00	0.23	2.33
8.75	0.41	2.92
10.50	0.67	3.50
12.25	1.01	4.00
14.00	1.43	4.00
15.75	1.92	4.25
17.50	2.49	4.83
19.25	3.14	5.42
21.00	3.87	6.00
22.75	4.69	6.58
24.50	5.59	7.17
26.25	6.59	7.75
28.00	7.68	8.33
29.75	8.88	8.92
31.50	10.17	9.50
33.25	11.57	10.08
35.00	13.07	10.67

†

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Height of Curb (cm)	Manning (n)	Long. Slope (m/m)	Shoulder Cross Slope (m/m)	Shoulder Roughness (n)
4	4.00	0.030	15.0	0.0130	0.030	0.030	0.0250

35.0

37923-3CHI 100. OUT

RATING CURVE

Depth (cm)	Flow (cms)	Spread (m)
0.00	0.00	0.00
1.75	0.01	0.58
3.50	0.04	1.17
5.25	0.13	1.75
7.00	0.28	2.33
8.75	0.50	2.92
10.50	0.82	3.50
12.25	1.23	4.00
14.00	1.75	4.00
15.75	2.35	4.25
17.50	3.05	4.83
19.25	3.84	5.42
21.00	4.73	6.00
22.75	5.73	6.58
24.50	6.84	7.17
26.25	8.06	7.75
28.00	9.40	8.33
29.75	10.85	8.92
31.50	12.43	9.50
33.25	14.14	10.08
35.00	15.99	10.67

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Height of Curb (cm)	Manning (n)	Long. Slope (m/m)	Shoulder Cross Slope (m/m)	Shoulder Roughness (n)
5 35.0	4.00	0.030	15.0	0.0130	0.040	0.030	0.0250

RATING CURVE

Depth	Flow	Spread
-------	------	--------

37923-3CHI 100. OUT		
(cm)	(cms)	(m)
0.00	0.00	0.00
1.75	0.01	0.58
3.50	0.05	1.17
5.25	0.15	1.75
7.00	0.32	2.33
8.75	0.58	2.92
10.50	0.94	3.50
12.25	1.42	4.00
14.00	2.02	4.00
15.75	2.72	4.25
17.50	3.53	4.83
19.25	4.44	5.42
21.00	5.48	6.00
22.75	6.63	6.58
24.50	7.91	7.17
26.25	9.32	7.75
28.00	10.87	8.33
29.75	12.55	8.92
31.50	14.38	9.50
33.25	16.36	10.08
35.00	18.49	10.67

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Height of Curb (cm)	Manning (n)	Long. Slope (m/m)	Shoulder Cross Slope (m/m)	Shoulder Roughness (n)
6 35.0	4.00	0.030	15.0	0.0130	0.060	0.030	0.0250

RATING CURVE

Depth (cm)	Flow (cms)	Spread (m)
0.00	0.00	0.00
1.75	0.01	0.58
3.50	0.06	1.17
5.25	0.18	1.75
7.00	0.39	2.33
8.75	0.71	2.92

37923-3CHI 100. OUT

10.50	1.16	3.50
12.25	1.74	4.00
14.00	2.47	4.00
15.75	3.33	4.25
17.50	4.32	4.83
19.25	5.44	5.42
21.00	6.71	6.00
22.75	8.12	6.58
24.50	9.69	7.17
26.25	11.42	7.75
28.00	13.31	8.33
29.75	15.37	8.92
31.50	17.61	9.50
33.25	20.04	10.08
35.00	22.65	10.67

‡

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Height of Curb (cm)	Manning (n)	Long. Slope (m/m)	Shoulder Cross Slope (m/m)	Shoulder Roughness (n)
7 35.0	4.00	0.030	15.0	0.0130	0.005	0.030	0.0250

RATING CURVE

Depth (cm)	Flow (cms)	Spread (m)
0.00	0.00	0.00
1.75	0.00	0.58
3.50	0.02	1.17
5.25	0.05	1.75
7.00	0.11	2.33
8.75	0.21	2.92
10.50	0.33	3.50
12.25	0.50	4.00
14.00	0.71	4.00
15.75	0.96	4.25
17.50	1.25	4.83
19.25	1.57	5.42
21.00	1.94	6.00
22.75	2.34	6.58

37923-3CHI 100. OUT		
24.50	2.80	7.17
26.25	3.30	7.75
28.00	3.84	8.33
29.75	4.44	8.92
31.50	5.08	9.50
33.25	5.78	10.08
35.00	6.54	10.67

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM RATING CURVE

Type Maximum Flow Depth (cm)	Pavement Width (m)	Pavement Cross Slope (m/m)	Height of Curb (cm)	Manning (n)	Long. Slope (m/m)	Shoulder Cross Slope (m/m)	Shoulder Roughness (n)
8 35.0	4.00	0.030	15.0	0.0130	0.000	0.030	0.0250

RATING CURVE

Depth (cm)	Flow (cms)	Spread (m)
0.00	0.00	0.00
1.75	0.00	0.58
3.50	0.00	1.17
5.25	0.01	1.75
7.00	0.02	2.33
8.75	0.03	2.92
10.50	0.05	3.50
12.25	0.07	4.00
14.00	0.10	4.00
15.75	0.14	4.25
17.50	0.18	4.83
19.25	0.22	5.42
21.00	0.27	6.00
22.75	0.33	6.58
24.50	0.40	7.17
26.25	0.47	7.75
28.00	0.54	8.33
29.75	0.63	8.92
31.50	0.72	9.50
33.25	0.82	10.08
35.00	0.92	10.67

♀

Example

DUAL DRAINAGE SIMULATION

STORM INLET DATA

1 Normal Inlet
 Inlet Identification No. 1
 No. of Points on Capture Curve 3

Inlet Capture Relationship

Approach Flow (l/s)	Inlet Flow (l/s)
0.00	0.00
10.00	10.00
99999.00	99999.00

2 Normal Inlet
 Inlet Identification No. 2
 No. of Points on Capture Curve 8

Inlet Capture Relationship

Approach Flow (l/s)	Inlet Flow (l/s)
0.00	0.00
71.00	16.00
104.00	24.00
148.00	31.50
270.00	45.50
470.00	57.00
690.00	67.50
1000.00	67.50

3 Normal Inlet
 Inlet Identification No. 3
 No. of Points on Capture Curve 8

Inlet Capture Relationship

Approach	Inlet
----------	-------

37923-3CHI 100. OUT

Flow (l/s)	Flow (l/s)
0.00	0.00
78.00	17.50
111.00	24.50
161.00	32.00
296.00	45.00
510.00	57.00
780.00	66.50
1000.00	66.50

4 Normal Inlet

Inlet Identification No. 4

No. of Points on Capture Curve 8

Inlet Capture Relationship

Approach Flow (l/s)	Inlet Flow (l/s)
0.00	0.00
50.00	13.50
71.00	20.00
102.00	26.50
195.00	41.00
330.00	55.00
510.00	65.50
1000.00	65.50

5 Normal Inlet

Inlet Identification No. 5

No. of Points on Capture Curve 8

Inlet Capture Relationship

Approach Flow (l/s)	Inlet Flow (l/s)
0.00	0.00
36.00	10.00
52.00	15.50
74.00	20.50
135.00	34.50
230.00	50.00
350.00	62.00
1000.00	62.00

6 Normal Inlet

Inlet Identification No. 6

No. of Points on Capture Curve 8

Inlet Capture Relationship

37923-3CHI 100. OUT

	Approach Flow (l/s)	Inlet Flow (l/s)
	0.00	0.00
	62.00	15.50
	88.00	23.00
	122.00	30.00
	230.00	44.00
	400.00	57.00
	620.00	67.00
	1000.00	67.00
7	Normal Inlet	
	Inlet Identification No.	7
	No. of Points on Capture Curve	8

Inlet Capture Relationship

	Approach Flow (l/s)	Inlet Flow (l/s)
	0.00	0.00
	36.00	10.00
	52.00	15.50
	74.00	20.50
	135.00	34.50
	230.00	50.00
	350.00	62.00
	1000.00	62.00
8	Storage Inlet	
	Inlet Identification No.	8
	Maximum Storage	280.00 cu. m.
	No. of Points on Storage-Capture Curve	3

Storage-Inlet Capture Relationship

	Storage Volume (cu. m)	Inlet Flow (l/s)
	0.00	0.00
	0.01	107.99
	280.00	108.00
9	Storage Inlet	
	Inlet Identification No.	9

37923-3CHI 100. OUT

Maximum Storage 125.00 cu. m.

No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
0.01	196.99
125.00	197.00

10 Storage Inlet

Inlet Identification No. 10

Maximum Storage 140.00 cu. m.

No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
0.01	49.99
140.00	50.00

11 Storage Inlet

Inlet Identification No. 11

Maximum Storage 6.52 cu. m.

No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
0.01	87.99
6.52	88.00

12 Storage Inlet

Inlet Identification No. 12

37923-3CHI 100. OUT

Maximum Storage 540.00 cu. m.

No. of Points on Storage-Capture Curve 3

Storage-Inlet Capture Relationship

Storage Volume (cu. m)	Inlet Flow (l/s)
0.00	0.00
0.01	251.99
540.00	252.00

‡

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DATA

Flow History	Street Segment	D/S Segment	Length (m)	Type	No. of C. B.	Inlet Type	Limiting Inlet Capture (l/s)	Connecting Pipe/EXTRAN Inlet
(?)								
YES	1 S20A	S20B	38.0	5	2	2 *	6.00	CBMH20
YES	2 S20B	S20C	31.0	5	2	2 *	6.00	CBMH20
YES	3 S20C	S20D	34.0	6	2	3 *	6.00	CBMH20
YES	4 S20D	S20E	19.0	5	2	2 *	6.00	CBMH20
YES	5 S20E	S107	39.0	3	2	4 *	6.00	107
YES	6 S107	S106A	32.0	3	2	4 *	6.00	107
YES	7 S106A	S106B	18.0	1	2	5 *	6.00	106
YES	8 S106B	S105A	42.0	4	2	6 *	6.00	106
YES	9 UNIT3	OUT1	252.0	7	2	8 ***	108.00	105
YES	10 S105A	S105B	24.0	5	2	1 *	12.50	105
YES	11 S105B	S104	23.0	2	2	7 *	6.00	105
YES	12 UNIT1	S104	266.0	7	2	9 ***	197.00	104
YES	13 UNIT2	OUT2	117.0	7	2	10 ***	50.00	104
YES	14 S104	D1	81.0	1	2	11 ***	88.00	104

37923-3CHI 100. OUT

YES	15	D1	REVERA	26.0	8	0	1 *	0.00	PDUM
YES	16	REVERA	OUT3	585.0	7	2	12 ***	252.00	104
YES									

* Normal Inlet.

** Storage Inlet with linear relationship between Storage and Inlet Capture.

*** Storage Inlet with user-specified relationship between Storage and Inlet Capture.

Total Number of Street segments	16	
Total Length of Major System	1627.00	m
Total Number of Inlet C. B.	30	
Average Distance Between Inlets	108.47	m

Outlets From Major System

Outlet I. D.

- OUT1
- OUT2
- OUT3

Total Number of Outlets from Major System = 3

No. of Detention Structures 0

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

SUB-CATCHMENT/SURFACE RUNOFF DATA

Infiltration Parameters

Max. Infiltration Rate	76.20	mm/hr
Min. Infiltration Rate	13.20	mm/hr
Decay Rate	0.001150	1/sec.

Unit Area Hydrograph (UAH) Data

No Unit Area Hydrograph Data

37923-3CHI 100. OUT

SUB-CATCHMENT DATA

No. Dep.	Subarea Storage	Street Flow	Segment	Area (Ha.)	Imp. (%)	Manning (N) (Imp.)	Manning (N) (Perv.)	Slope (m/m)	Width (m)
Imp.	Perv.	History							
(mm)	(mm)	(?)							
1.500	4.670	NO	S20A	0.18	50.	0.0130	0.2500	0.020	20.
1.500	4.670	NO	S20B	0.13	43.	0.0130	0.2500	0.020	25.
1.500	4.670	NO	S20C	0.13	43.	0.0130	0.2500	0.020	20.
1.500	4.670	NO	S20D	0.06	43.	0.0130	0.2500	0.020	20.
1.500	4.670	NO	S20E	0.11	50.	0.0130	0.2500	0.020	15.
1.500	4.670	NO	S107	0.09	50.	0.0130	0.2500	0.020	15.
1.500	4.670	NO	S106A	0.02	100.	0.0130	0.2500	0.020	5.
1.500	4.670	NO	S106B	0.05	100.	0.0130	0.2500	0.020	5.
1.500	4.670	NO	UNIT3	1.12	79.	0.0130	0.2500	0.020	126.
1.500	4.670	NO	S105A	0.03	100.	0.0130	0.2500	0.020	6.
1.500	4.670	NO	S105B	0.03	100.	0.0130	0.2500	0.020	5.
1.500	4.670	NO	UNIT1	1.18	79.	0.0130	0.2500	0.020	133.
1.500	4.670	NO	UNIT2	0.52	86.	0.0130	0.2500	0.020	58.
1.500	4.670	NO	S104	0.09	100.	0.0130	0.2500	0.020	5.
1.500	4.670	NO	REVERA	2.60	71.	0.0130	0.2500	0.020	292.

* Inflow Hydrograph Input Directly

** Inflow hydrograph Input in terms of flow per unit area

Total Drainage Area 6.34 Hectares

Number of Subcatchments 15

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

Simulation Details - Surface Runoff - 15 Subareas

count Subarea

37923-3CHI 100. OUT

- 1 AS20A
- 2 AS20B
- 3 AS20C
- 4 AS20D
- 5 AS20E
- 6 AS107
- 7 AS106A
- 8 AS106B
- 9 AUNI T3
- 10 AS105A
- 11 AS105B
- 12 AUNI T1
- 13 AUNI T2
- 14 AS104
- 15 AREVERA

†

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

Simulation Details - Major System - 19 Segments/Outlets

count	order	segment	time step (min.)	No. of time steps	Max. flow (cms)	Max. depth (cm)
1	1	S20A	0.42	424	0.04	3.06
2	2	S20B	0.31	588	0.06	3.64
3	3	S20C	0.27	659	0.07	3.67
4	4	S20D	0.18	1008	0.07	3.94
5	5	S20E	0.45	398	0.09	4.81
6	6	S107	0.36	500	0.10	5.04
7	7	S106A	0.27	663	0.09	5.67
8	8	S106B	0.41	438	0.10	4.62
9	10	S105A	0.21	849	0.10	4.33
10	12	UNI T1	3.55	50	0.38	10.93
11	11	S105B	0.31	577	0.08	5.16
12	14	S104	1.20	150	0.10	5.82
13	15	D1	1.20	150	0.00	0.00
14	16	REVERA	5.84	31	0.76	14.33
15	13	UNI T2	1.90	95	0.18	8.20
16	9	UNI T3	3.41	53	0.36	10.74

37923-3CHI 100. OUT

17	19	OUT3	0.00
18	18	OUT2	0.00
19	17	OUT1	0.00

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

EXTRAN Interface File Information

Inlet flows are stored at the following 6 inlets (EXTRAN nodes):

CBMH20	107	106	105	104	PDUM
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DDSWMM-EXTRAN Connectivity

EXTRAN Inlet	DDSWMM Inlets (Major System Segments)			
CBMH20	S20A	S20B	S20C	S20D
107	S20E	S107		
106	S106A	S106B		
105	UNIT3	S105A	S105B	
104	UNIT1	UNIT2	S104	REVERA
PDUM	D1			

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment S20A

Time (hr: min)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.000	0.002	0.002	0.000	0.001	0.4	0.00
0: 40	0.000	0.003	0.003	0.001	0.002	0.8	0.00
0: 50	0.000	0.008	0.008	0.002	0.006	1.8	0.00

37923-3CHI 100. OUT

1: 0	0.000	0.040	0.040	0.009	0.030	3.1	0.00
1: 10	0.000	0.037	0.037	0.008	0.029	3.0	0.00
1: 20	0.000	0.013	0.013	0.003	0.011	1.9	0.00
1: 30	0.000	0.011	0.011	0.003	0.009	1.9	0.00
1: 40	0.000	0.007	0.007	0.002	0.005	1.5	0.00
1: 50	0.000	0.005	0.005	0.001	0.004	1.1	0.00
2: 0	0.000	0.004	0.004	0.001	0.003	0.8	0.00
2: 10	0.000	0.003	0.003	0.001	0.002	0.6	0.00
2: 20	0.000	0.002	0.002	0.000	0.002	0.5	0.00
2: 30	0.000	0.002	0.002	0.000	0.001	0.4	0.00
2: 40	0.000	0.002	0.002	0.000	0.001	0.3	0.00
2: 50	0.000	0.001	0.001	0.000	0.001	0.3	0.00
3: 0	0.000	0.000	0.000	0.000	0.001	0.0	0.00

Maximum	0.000		0.040	0.009	0.031	3.1	0.00
Time (h: mi n)	0: 0		1: 0	1: 0	1: 0		

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment S20B

Time (hr: mi n)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.001	0.002	0.003	0.000	0.002	0.6	0.00
0: 40	0.002	0.002	0.005	0.001	0.003	1.0	0.00
0: 50	0.006	0.005	0.011	0.002	0.009	1.9	0.00
1: 0	0.030	0.028	0.057	0.012	0.044	3.6	0.00
1: 10	0.029	0.027	0.056	0.012	0.044	3.6	0.00
1: 20	0.011	0.009	0.020	0.005	0.017	2.3	0.00
1: 30	0.009	0.008	0.017	0.004	0.013	2.1	0.00
1: 40	0.005	0.004	0.009	0.002	0.007	1.8	0.00
1: 50	0.004	0.003	0.007	0.002	0.006	1.6	0.00
2: 0	0.003	0.002	0.005	0.001	0.004	1.1	0.00
2: 10	0.002	0.001	0.004	0.001	0.003	0.8	0.00
2: 20	0.002	0.001	0.003	0.001	0.002	0.6	0.00
2: 30	0.001	0.001	0.002	0.001	0.002	0.5	0.00
2: 40	0.001	0.001	0.002	0.000	0.002	0.5	0.00
2: 50	0.001	0.001	0.002	0.000	0.002	0.4	0.00
3: 0	0.001	0.000	0.001	0.000	0.001	0.2	0.00

Maximum	0.031		0.058	0.012	0.046	3.6	0.00
Time (h: mi n)	1: 0		1: 0	1: 1	1: 1		

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)

IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment S20C

Time (hr: min)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.002	0.001	0.003	0.001	0.002	0.5	0.00
0: 40	0.003	0.002	0.006	0.001	0.004	1.0	0.00
0: 50	0.009	0.005	0.014	0.003	0.010	1.9	0.00
1: 0	0.044	0.027	0.071	0.012	0.057	3.6	0.00
1: 10	0.044	0.026	0.070	0.012	0.058	3.6	0.00
1: 20	0.017	0.009	0.026	0.006	0.022	2.3	0.00
1: 30	0.013	0.008	0.021	0.005	0.017	2.1	0.00
1: 40	0.007	0.004	0.012	0.003	0.009	1.8	0.00
1: 50	0.006	0.003	0.009	0.002	0.007	1.6	0.00
2: 0	0.004	0.002	0.006	0.001	0.005	1.1	0.00
2: 10	0.003	0.002	0.005	0.001	0.004	0.8	0.00
2: 20	0.002	0.001	0.003	0.001	0.003	0.6	0.00
2: 30	0.002	0.001	0.003	0.001	0.002	0.5	0.00
2: 40	0.002	0.001	0.003	0.001	0.002	0.5	0.00
2: 50	0.002	0.001	0.002	0.001	0.002	0.4	0.00
3: 0	0.001	0.000	0.001	0.000	0.001	0.2	0.00
Maximum Time (h: min)	0.046		0.073	0.012	0.061	3.7	0.00
	1: 1		1: 1	1: 1	1: 1		

†

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment S20D

Time (hr: min)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
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37923-3CHI 100. OUT

0: 0	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.002	0.001	0.003	0.001	0.002	0.002	0.6	0.00
0: 40	0.004	0.001	0.005	0.001	0.004	0.004	1.2	0.00
0: 50	0.010	0.003	0.013	0.003	0.010	0.010	2.0	0.00
1: 0	0.057	0.014	0.071	0.012	0.058	0.058	3.9	0.00
1: 10	0.058	0.013	0.071	0.012	0.059	0.059	3.9	0.00
1: 20	0.022	0.004	0.026	0.006	0.021	0.021	2.5	0.00
1: 30	0.017	0.003	0.020	0.005	0.016	0.016	2.2	0.00
1: 40	0.009	0.001	0.011	0.002	0.009	0.009	1.9	0.00
1: 50	0.007	0.001	0.008	0.002	0.006	0.006	1.8	0.00
2: 0	0.005	0.001	0.006	0.001	0.004	0.004	1.2	0.00
2: 10	0.004	0.001	0.004	0.001	0.003	0.003	0.9	0.00
2: 20	0.003	0.001	0.003	0.001	0.003	0.003	0.7	0.00
2: 30	0.002	0.000	0.003	0.001	0.002	0.002	0.6	0.00
2: 40	0.002	0.000	0.002	0.001	0.002	0.002	0.5	0.00
2: 50	0.002	0.000	0.002	0.001	0.002	0.002	0.5	0.00
3: 0	0.001	0.000	0.001	0.000	0.001	0.001	0.2	0.00
Maximum Time (h: mi n)	0.061 1: 1		0.075 1: 1	0.012 1: 1	0.063 1: 1		3.9	0.00

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment S20E

Time (hr: mi n)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.002	0.001	0.003	0.001	0.002	1.0	0.00
0: 40	0.004	0.002	0.006	0.002	0.004	1.8	0.00
0: 50	0.010	0.005	0.015	0.004	0.010	2.3	0.00
1: 0	0.058	0.025	0.083	0.012	0.068	4.7	0.00
1: 10	0.059	0.023	0.083	0.012	0.071	4.7	0.00
1: 20	0.021	0.008	0.028	0.008	0.023	3.1	0.00
1: 30	0.016	0.007	0.022	0.006	0.017	2.7	0.00
1: 40	0.009	0.004	0.012	0.004	0.010	2.1	0.00
1: 50	0.006	0.003	0.009	0.003	0.007	2.0	0.00
2: 0	0.004	0.002	0.006	0.002	0.005	1.8	0.00
2: 10	0.003	0.002	0.005	0.001	0.004	1.5	0.00
2: 20	0.003	0.001	0.004	0.001	0.003	1.2	0.00
2: 30	0.002	0.001	0.003	0.001	0.002	1.0	0.00
2: 40	0.002	0.001	0.003	0.001	0.002	0.9	0.00
2: 50	0.002	0.001	0.003	0.001	0.002	0.8	0.00
3: 0	0.001	0.000	0.001	0.000	0.001	0.3	0.00

37923-3CHI 100. OUT

Maximum 0.063 0.088 0.012 0.076 4.8 0.00
 Time (h: mi n) 1: 1 1: 1 1: 2 1: 2

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment S107

Time (hr: mi n)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.002	0.001	0.003	0.001	0.002	0.9	0.00
0: 40	0.004	0.002	0.006	0.002	0.004	1.8	0.00
0: 50	0.010	0.004	0.015	0.004	0.010	2.3	0.00
1: 0	0.068	0.021	0.089	0.012	0.074	4.8	0.00
1: 10	0.071	0.019	0.090	0.012	0.079	4.9	0.00
1: 20	0.023	0.006	0.029	0.009	0.023	3.1	0.00
1: 30	0.017	0.006	0.022	0.006	0.016	2.7	0.00
1: 40	0.010	0.003	0.012	0.004	0.010	2.1	0.00
1: 50	0.007	0.002	0.009	0.003	0.007	2.0	0.00
2: 0	0.005	0.002	0.006	0.002	0.005	1.8	0.00
2: 10	0.004	0.001	0.005	0.001	0.004	1.5	0.00
2: 20	0.003	0.001	0.004	0.001	0.003	1.2	0.00
2: 30	0.002	0.001	0.003	0.001	0.002	1.0	0.00
2: 40	0.002	0.001	0.003	0.001	0.002	0.9	0.00
2: 50	0.002	0.001	0.003	0.001	0.002	0.8	0.00
3: 0	0.001	0.000	0.001	0.000	0.001	0.4	0.00

Maximum 0.076 0.097 0.012 0.085 5.0 0.00
 Time (h: mi n) 1: 2 1: 2 1: 2 1: 2

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment S106A

37923-3CHI 100. OUT

Time (hr: min)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.002	0.000	0.002	0.001	0.001	1.0	0.00
0: 40	0.004	0.001	0.005	0.001	0.003	1.8	0.00
0: 50	0.010	0.002	0.012	0.003	0.008	2.4	0.00
1: 0	0.074	0.008	0.083	0.012	0.069	5.5	0.00
1: 10	0.079	0.005	0.084	0.012	0.072	5.5	0.00
1: 20	0.023	0.001	0.024	0.007	0.019	3.5	0.00
1: 30	0.016	0.001	0.018	0.005	0.013	2.9	0.00
1: 40	0.010	0.001	0.010	0.003	0.008	2.3	0.00
1: 50	0.007	0.001	0.008	0.002	0.006	2.1	0.00
2: 0	0.005	0.001	0.005	0.002	0.004	1.9	0.00
2: 10	0.004	0.000	0.004	0.001	0.003	1.8	0.00
2: 20	0.003	0.000	0.003	0.001	0.002	1.5	0.00
2: 30	0.002	0.000	0.003	0.001	0.002	1.3	0.00
2: 40	0.002	0.000	0.002	0.001	0.002	1.1	0.00
2: 50	0.002	0.000	0.002	0.001	0.002	1.0	0.00
3: 0	0.001	0.000	0.001	0.000	0.001	0.5	0.00
Maximum Time (h: min)	0.085 1: 2		0.092 1: 2	0.012 1: 2	0.080 1: 2	5.7	0.00

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment S106B

Time (hr: min)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.001	0.001	0.002	0.000	0.001	0.6	0.00
0: 40	0.003	0.002	0.005	0.001	0.004	1.3	0.00
0: 50	0.008	0.004	0.012	0.003	0.009	2.0	0.00
1: 0	0.069	0.018	0.087	0.012	0.072	4.4	0.00
1: 10	0.072	0.015	0.088	0.012	0.076	4.4	0.00
1: 20	0.019	0.003	0.022	0.007	0.020	2.5	0.00
1: 30	0.013	0.003	0.016	0.004	0.012	2.2	0.00
1: 40	0.008	0.002	0.010	0.003	0.008	1.9	0.00
1: 50	0.006	0.002	0.007	0.002	0.006	1.8	0.00
2: 0	0.004	0.001	0.005	0.001	0.004	1.4	0.00

37923-3CHI 100. OUT

2: 10	0.003	0.001	0.004	0.001	0.003	1.1	0.00
2: 20	0.002	0.001	0.003	0.001	0.003	0.9	0.00
2: 30	0.002	0.001	0.003	0.001	0.002	0.8	0.00
2: 40	0.002	0.001	0.003	0.001	0.002	0.7	0.00
2: 50	0.002	0.001	0.002	0.001	0.002	0.6	0.00
3: 0	0.001	0.000	0.001	0.000	0.001	0.2	0.00

Maximum	0.080		0.098	0.012	0.086	4.6	0.00
Time (h: mi n)	1: 2		1: 2	1: 3	1: 3		

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Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Examp l e

DUAL DRAI NAGE SI MULATI ON

MAJOR SYSTEM DETAILED SIMULATI ON RESULTS

Major System Segment UNIT3

Time (hr: mi n)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.3	0.00
0: 30	0.000	0.015	0.015	0.002	0.000	3.2	0.00
0: 40	0.000	0.032	0.032	0.019	0.000	4.2	0.00
0: 50	0.000	0.075	0.075	0.050	0.000	5.9	0.00
1: 0	0.000	0.356	0.356	0.108	0.000	10.7	42.27
1: 10	0.000	0.311	0.311	0.108	0.000	10.2	173.46
1: 20	0.000	0.069	0.069	0.108	0.000	5.7	258.02
1: 30	0.000	0.067	0.067	0.108	0.000	5.7	265.35
1: 40	0.000	0.042	0.042	0.108	0.000	4.7	237.95
1: 50	0.000	0.032	0.032	0.108	0.000	4.2	201.24
2: 0	0.000	0.026	0.026	0.108	0.000	3.9	157.00
2: 10	0.000	0.021	0.021	0.108	0.000	3.7	108.53
2: 20	0.000	0.019	0.019	0.108	0.000	3.5	57.23
2: 30	0.000	0.017	0.017	0.108	0.000	3.4	4.08
2: 40	0.000	0.015	0.015	-0.060	0.000	3.2	0.00
2: 50	0.000	0.014	0.014	0.091	0.000	3.0	0.01
3: 0	0.000	0.000	0.000	-0.063	0.000	0.0	0.00

Maximum	0.000		0.356	0.108	0.000	10.7	265.35
Time (h: mi n)	0: 0		1: 0	1: 30	3: 0		

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Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Examp l e

DUAL DRAI NAGE SI MULATI ON

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment S105A

Time (hr: min)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.001	0.001	0.002	0.001	0.000	0.4	0.00
0: 40	0.004	0.001	0.005	0.005	0.000	1.0	0.00
0: 50	0.009	0.003	0.011	0.011	0.000	1.9	0.00
1: 0	0.072	0.012	0.084	0.025	0.057	4.1	0.00
1: 10	0.076	0.008	0.085	0.025	0.060	4.1	0.00
1: 20	0.020	0.001	0.021	0.023	0.000	2.3	0.00
1: 30	0.012	0.002	0.015	0.015	0.000	2.0	0.00
1: 40	0.008	0.001	0.009	0.009	0.000	1.8	0.00
1: 50	0.006	0.001	0.007	0.007	0.000	1.5	0.00
2: 0	0.004	0.001	0.005	0.005	0.000	1.1	0.00
2: 10	0.003	0.001	0.004	0.004	0.000	0.9	0.00
2: 20	0.003	0.001	0.003	0.003	0.000	0.7	0.00
2: 30	0.002	0.001	0.003	0.003	0.000	0.6	0.00
2: 40	0.002	0.001	0.003	0.003	0.000	0.6	0.00
2: 50	0.002	0.000	0.002	0.002	0.000	0.5	0.00
3: 0	0.001	0.000	0.001	0.001	0.000	0.3	0.00
Maximum Time (h: min)	0.086 1: 3		0.097 1: 3	0.025 1: 3	0.072 1: 3	4.3	0.00

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Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment S105B

Time (hr: min)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.000	0.001	0.001	0.000	0.000	0.2	0.00
0: 40	0.000	0.001	0.001	0.000	0.001	0.4	0.00
0: 50	0.000	0.003	0.003	0.001	0.002	1.0	0.00
1: 0	0.057	0.012	0.069	0.012	0.055	4.7	0.00

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1: 10	0.060	0.009	0.069	0.012	0.057	4.7	0.00
1: 20	0.000	0.002	0.002	0.002	0.005	0.6	0.00
1: 30	0.000	0.002	0.002	0.001	0.001	0.8	0.00
1: 40	0.000	0.001	0.001	0.000	0.001	0.5	0.00
1: 50	0.000	0.001	0.001	0.000	0.001	0.4	0.00
2: 0	0.000	0.001	0.001	0.000	0.001	0.3	0.00
2: 10	0.000	0.001	0.001	0.000	0.001	0.3	0.00
2: 20	0.000	0.001	0.001	0.000	0.000	0.2	0.00
2: 30	0.000	0.001	0.001	0.000	0.000	0.2	0.00
2: 40	0.000	0.001	0.001	0.000	0.000	0.2	0.00
2: 50	0.000	0.000	0.000	0.000	0.000	0.2	0.00
3: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00

Maximum	0.072		0.083	0.012	0.071	5.2	0.00
Time (h: mi n)	1: 3		1: 3	1: 3	1: 3		

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment UNIT1

Time (hr: mi n)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.3	0.00
0: 30	0.000	0.016	0.016	0.002	0.000	3.3	0.00
0: 40	0.000	0.033	0.033	0.019	0.000	4.3	0.00
0: 50	0.000	0.079	0.079	0.050	0.000	6.0	0.00
1: 0	0.000	0.376	0.376	0.197	0.000	10.9	18.00
1: 10	0.000	0.328	0.328	0.197	0.000	10.4	105.50
1: 20	0.000	0.073	0.073	0.197	0.000	5.8	125.00
1: 30	0.000	0.070	0.070	0.197	0.000	5.8	88.11
1: 40	0.000	0.044	0.044	0.197	0.000	4.8	9.71
1: 50	0.000	0.034	0.034	-0.065	0.000	4.3	0.00
2: 0	0.000	0.027	0.027	0.138	0.000	4.0	0.01
2: 10	0.000	0.022	0.022	-0.080	0.000	3.7	0.00
2: 20	0.000	0.020	0.020	0.128	0.000	3.6	0.01
2: 30	0.000	0.018	0.018	-0.087	0.000	3.5	0.00
2: 40	0.000	0.016	0.016	0.123	0.000	3.3	0.01
2: 50	0.000	0.014	0.014	-0.090	0.000	3.1	0.00
3: 0	0.000	0.000	0.000	0.119	0.000	0.0	0.01

Maximum	0.000		0.376	0.197	0.000	10.9	125.00
Time (h: mi n)	0: 0		1: 0	1: 20	3: 0		

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment UNIT2

Time (hr: min)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.1	0.00
0: 30	0.000	0.007	0.007	0.003	0.000	2.3	0.00
0: 40	0.000	0.016	0.016	0.012	0.000	3.3	0.00
0: 50	0.000	0.037	0.037	0.030	0.000	4.5	0.01
1: 0	0.000	0.176	0.176	0.050	0.000	8.2	29.55
1: 10	0.000	0.151	0.151	0.050	0.000	7.7	98.49
1: 20	0.000	0.031	0.031	0.050	0.000	4.2	133.50
1: 30	0.000	0.031	0.031	0.050	0.000	4.2	131.00
1: 40	0.000	0.020	0.020	0.050	0.000	3.6	117.38
1: 50	0.000	0.016	0.016	0.050	0.000	3.3	99.63
2: 0	0.000	0.013	0.013	0.050	0.000	2.9	78.95
2: 10	0.000	0.011	0.011	0.050	0.000	2.7	56.59
2: 20	0.000	0.009	0.009	0.050	0.000	2.5	33.09
2: 30	0.000	0.008	0.008	0.050	0.000	2.4	8.78
2: 40	0.000	0.008	0.008	-0.004	0.000	2.3	0.00
2: 50	0.000	0.007	0.007	0.019	0.000	2.2	0.00
3: 0	0.000	0.000	0.000	-0.007	0.000	0.0	0.00
Maximum	0.000		0.176	0.050	0.000	8.2	133.50
Time (h: min)	0: 0		1: 0	1: 20	3: 0		

♀

Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment S104

Time (hr: min)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00

37923-3CHI 100. OUT

0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.000	0.001	0.001	0.000	0.000	0.5	0.00
0: 40	0.001	0.002	0.003	0.002	0.000	1.4	0.00
0: 50	0.002	0.006	0.008	0.007	0.000	2.1	0.00
1: 0	0.055	0.029	0.084	0.074	0.000	5.5	0.01
1: 10	0.057	0.029	0.086	0.088	0.000	5.5	3.66
1: 20	0.005	0.008	0.013	0.039	0.000	2.5	0.00
1: 30	0.001	0.006	0.007	-0.004	0.000	2.0	0.00
1: 40	0.001	0.004	0.005	0.019	0.000	1.9	0.00
1: 50	0.001	0.003	0.004	-0.009	0.000	1.8	0.00
2: 0	0.001	0.003	0.003	0.017	0.000	1.5	0.00
2: 10	0.001	0.002	0.003	-0.010	0.000	1.3	0.00
2: 20	0.000	0.002	0.003	0.016	0.000	1.1	0.00
2: 30	0.000	0.002	0.002	-0.011	0.000	1.0	0.00
2: 40	0.000	0.002	0.002	0.015	0.000	0.9	0.00
2: 50	0.000	0.001	0.002	-0.011	0.000	0.8	0.00
3: 0	0.000	0.000	0.000	0.015	0.000	0.1	0.00

Maximum	0.071		0.100	0.088	0.000	5.8	3.66
Time (h: mi n)	1: 3		1: 3	1: 10	3: 0		

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Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Examp l e

DUAL DRAI NAGE SIMULATI ON

MAJOR SYSTEM DETAILED SIMULATI ON RESULTS

Major System Segment D1

Time (hr: mi n)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 30	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 40	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 50	0.000	0.000	0.000	0.000	0.000	0.0	0.00
1: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
1: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
1: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
1: 30	0.000	0.000	0.000	0.000	0.000	0.0	0.00
1: 40	0.000	0.000	0.000	0.000	0.000	0.0	0.00
1: 50	0.000	0.000	0.000	0.000	0.000	0.0	0.00
2: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
2: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
2: 20	0.000	0.000	0.000	0.000	0.000	0.0	0.00
2: 30	0.000	0.000	0.000	0.000	0.000	0.0	0.00
2: 40	0.000	0.000	0.000	0.000	0.000	0.0	0.00
2: 50	0.000	0.000	0.000	0.000	0.000	0.0	0.00
3: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00

37923-3CHI 100. OUT

Maximum 0.000 0.000 0.000 0.000 0.0 0.00
 Time (h:mi n) 3: 0 3: 0 0: 0 0: 0

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Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM DETAILED SIMULATION RESULTS

Major System Segment REVERA

Time (hr:mi n)	U/S Inflow (cms)	Catchment Inflow (cms)	Total Inflow (cms)	Inlet Capture (cms)	Outflow (cms)	Depth at Curb (cm)	Storage (cu. m)
0: 0	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 10	0.000	0.000	0.000	0.000	0.000	0.0	0.00
0: 20	0.000	0.001	0.001	0.000	0.000	0.6	0.00
0: 30	0.000	0.034	0.034	0.000	0.000	4.3	0.00
0: 40	0.000	0.067	0.067	0.014	0.000	5.7	0.00
0: 50	0.000	0.158	0.158	0.049	0.000	7.9	0.00
1: 0	0.000	0.761	0.761	0.252	0.000	14.3	15.90
1: 10	0.000	0.677	0.677	0.252	0.000	13.7	228.48
1: 20	0.000	0.169	0.169	0.252	0.000	8.1	447.19
1: 30	0.000	0.157	0.157	0.252	0.000	7.8	511.52
1: 40	0.000	0.096	0.096	0.252	0.000	6.5	468.12
1: 50	0.000	0.073	0.073	0.252	0.000	5.8	394.13
2: 0	0.000	0.056	0.056	0.252	0.000	5.4	297.36
2: 10	0.000	0.045	0.045	0.252	0.000	4.9	187.66
2: 20	0.000	0.039	0.039	0.252	0.000	4.6	69.37
2: 30	0.000	0.035	0.035	0.070	0.000	4.3	0.00
2: 40	0.000	0.031	0.031	0.008	0.000	4.2	0.00
2: 50	0.000	0.029	0.029	0.062	0.000	4.0	0.00
3: 0	0.000	0.000	0.000	0.012	0.000	0.0	0.00

Maximum 0.000 0.761 0.252 0.000 14.3 511.52
 Time (h:mi n) 0: 0 1: 0 1: 30 3: 0

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Dual Drainage Storm Water Management Model (DDSWMM 2.1)
 IBI Group, Ottawa, Ontario

Example

DUAL DRAINAGE SIMULATION

MAJOR SYSTEM

SUMMARY OF SIMULATION RESULTS

No. Max.	Segment	Peak Flow	Peak Time	Max. Depth	Max. Capture	Inlet Restriction	D/S Pipe
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37923-3CHI 100. OUT

Storage (cu. m.)	(cms)	(hr: mi n.)	(cm)	(l /s)	(?)	
1 S20A 0.00	0.040	1: 0	3.06	8.95	NO	CBMH20
2 S20B 0.00	0.058	1: 0	3.64	12.00	YES	CBMH20
3 S20C 0.00	0.073	1: 1	3.67	12.00	YES	CBMH20
4 S20D 0.00	0.075	1: 1	3.94	12.00	YES	CBMH20
5 S20E 0.00	0.088	1: 1	4.81	12.00	YES	107
6 S107 0.00	0.097	1: 2	5.04	12.00	YES	107
7 S106A 0.00	0.092	1: 2	5.67	12.00	YES	106
8 S106B 0.00	0.098	1: 2	4.62	12.00	YES	106
9 UNI T3 265.35	0.356	1: 0	10.74	108.00	N/A	105
10 S105A 0.00	0.097	1: 3	4.33	25.00	YES	105
11 S105B 0.00	0.083	1: 3	5.16	12.00	YES	105
12 UNI T1 125.00	0.376	1: 0	10.93	197.00	N/A	104
13 UNI T2 133.50	0.176	1: 0	8.20	50.00	N/A	104
14 S104 3.66	0.100	1: 3	5.82	88.00	N/A	104
15 D1 0.00	0.000	3: 0	0.00	0.00	-	PDUM
16 REVERA 511.52	0.761	1: 0	14.33	252.00	N/A	104

*** SIMULATI ON ENDED NORMALLY ***

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```

*****
*
*   Simulation Starting Date      March   29, 18
*                               Time      13: 26: 25. 59
*
*   Simulation Ending   Date      March   29, 18
*                               Time      13: 26: 28. 49
*
*   Duration of Simulation          0.05 Mi nutes
*
*****

```

Data Files

Input Data File Name 37923-3CHI 100. DAT
Output File Name 37923-3CHI 100. OUT
EXTRAN Interface (ASCII) File Name 37923-3CHI 100. TXT

```

00001> =====
00002>
00003> SSSSS W W M M H H Y Y M M O O 999 999 =====
00004> S W W M M M H H Y Y M M O O 9 9 9 9
00005> SSSSS W W M M M H H H H Y Y M M O O ## 9 9 9 9 Ver 4.05
00006> S W W M M M H H Y Y M M O O 9999 9999 Sept 2011
00007> SSSSS W W M M H H Y Y M M O O 9 9 9 9 =====
00008> 9 9 9 9 # 3699242
00009> StormWater Management Hydrologic Model 999 999 =====
00010>
00011> *****
00012> ***** SWMHYMO Ver/4.05 *****
00013> ***** A single event and continuous hydrologic simulation model *****
00014> ***** based on the principles of HYMO and its successors *****
00015> ***** OTTHYMO-83 and OTTHYMO-89. *****
00016> *****
00017> ***** Distributed by: J.F. Sabourin and Associates Inc. *****
00018> ***** Ottawa, Ontario: (613) 836-3884 *****
00019> ***** Gatineau, Quebec: (819) 243-6858 *****
00020> ***** E-Mail: swmhyo@jfsa.com *****
00021> *****
00022>
00023> *****
00024> ***** Licensed user: Cumming Cockburn Limited *****
00025> ***** Ottawa SERIAL#:3699242 *****
00026> *****
00027> *****
00028> *****
00029> ***** PROGRAM ARRAY DIMENSIONS *****
00030> ***** Maximum value for ID numbers : 10 *****
00031> ***** Max. number of rainfall points: 105408 *****
00032> ***** Max. number of flow points : 105408 *****
00033> *****
00034> *****
00035> *****
00036> ***** D E T A I L E D O U T P U T *****
00037> *****
00038> * DATE: 2018-03-29 TIME: 12:41:26 RUN COUNTER: 000315 *
00039> *****
00040> * Input filename: C:\SWMHYMO\37923\37923VxD.DAT *
00041> * Output filename: C:\SWMHYMO\37923\37923VxD.out *
00042> * Summary filename: C:\SWMHYMO\37923\37923VxD.sum *
00043> * User comments: *
00044> * 1: *
00045> * 2: *
00046> * 3: *
00047> *****
00048>
00049>
00050> 001:0001
00051> *****
00052> *# Project Name: Example Project Number: [J:\37923-RiversidePropert
00053> *# Date : DUAL DRAINAGE SIMULATION
00054> *# Modeller :
00055> *# Company : P.Deir
00056> *# License # : March 2018
00057> *****
00058> *
00059> *
00060> *# JOB #J:\37923-RiversideProperty\5.7 Calculations\5.7.4 SWM\IS
00061> *****
00062> *#
00063> *#
00064> *****
00065> *
00066> *
00067>
00068> | START | Project dir.: C:\SWMHYMO\37923\
00069> | TZERO = 00 hrs on 0 | Rainfall dir.: C:\SWMHYMO\37923\
00070> | METOUT= 2 (output = METRIC) |
00071> | NRUN = 001 |
00072> | NSTORM= 0 |
00073>
00074>
00075> 001:0002
00076> *
00077> *
00078> *#=====
00079> *# === 100YR DESIGN STORM ===
00080> *# === 3HR CHICAGO (10min TIME STEP) ===
00081> *# === ON-SITE DETENTION ANALYSIS ===
00082> *#=====
00083> *
00084>
00085> | CHICAGO STORM | IDF curve parameters: A=1735.685
00086> | Ptotal= 71.66 mm | B= 6.014
00087> | C= .820
00088> used in: INTENSITY = A / (t + B)^C
00089>
00090> Duration of storm = 3.00 hrs
00091> Storm time step = 10.00 min
00092> Time to peak ratio = .33
00093>
00094> The CORRELATION coefficient is = .9997109
00095>
00096> TIME ENTERED COMPUTED
00097> (min) (mm/hr) (mm/hr)
00098> 5. 242.60 242.70
00099> 10. 179.00 178.56
00100> 15. 146.80 142.89
00101> 30. 91.90 91.87
00102> 60. 53.20 55.89
00103> 120. 31.50 32.89
00104> 360. 14.50 13.72
00105> 720. 8.00 7.83
00106> 1440. 4.30 4.45
00107>
00108> TIME RAIN TIME RAIN TIME RAIN TIME RAIN
00109> hrs mm/hr hrs mm/hr hrs mm/hr hrs mm/hr
00110> .17 6.046 1.00 178.559 1.83 11.059 2.67 5.760
00111> .33 7.542 1.17 5.048 2.00 9.285 2.83 5.280
00112> .50 10.159 1.33 27.319 2.17 8.024 3.00 4.879
00113> .67 15.969 1.50 18.240 2.33 7.080
00114> .83 40.655 1.67 13.737 2.50 6.347
00115>
00116>
00117> 001:0003
00118> *
00119> *
00120> *#=====
00121> *# DUMMY AREA
00122> *#=====
00123> *
00124> *
00125>
00126> | CALIB STANDHYD | Area (ha)= 2.00
00127> | 01:000210 DT= 2.00 | Total Imp(%)= 65.00 Dir. Conn.(%)= 65.00

```

```

00128> -----
00129> IMPERVIOUS PERVIOUS (i)
00130> Surface Area (ha)= 1.30 .70
00131> Dep. Storage (mm)= 4.00 1.50
00132> Average Slope (%)= .50 2.00
00133> Length (m)= 250.00 40.00
00134> Mannings n = .013 .250
00135>
00136> Max.eff.Inten.(mm/hr)= 178.56 71.07
00137> over (min) 4.00 12.00
00138> Storage Coeff. (min)= 4.02 (ii) 12.41 (ii)
00139> Unit Hyd. tpeak (min)= 4.00 12.00
00140> Unit Hyd. peak (cms)= .27 .09
00141>
00142> PEAK FLOW (cms)= .58 .09 *TOTALS*
00143> TIME TO PEAK (hrs)= 1.00 1.17 1.000
00144> RUNOFF VOLUME (mm)= 70.86 33.71 57.861
00145> TOTAL RAINFALL (mm)= 71.66 71.66 71.665
00146> RUNOFF COEFFICIENT = .99 .47 .807
00147> *** ERROR: XIMP cannot be larger than TIMP.
00148> XIMP was forced to equal TIMP.
00149>
00150> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
00151> CN* = 77.0 Ta = Dep. Storage (above)
00152> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
00153> THAN THE STORAGE COEFFICIENT.
00154> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00155>
00156> -----
00157> 001:0004
00158>
00159> *# Area S20A
00160> *#=====2
00161> *# 4.00% Slope
00162> *#=====
00163> *
00164>
00165> ROUTE CHANNEL Routing time step (min) = 1.00
00166> | IN> 01:000210 | Number of SEGMENTS = 3
00167> | OUT< 02:000154 | Slopes (%), CHANNEL=4.0000 FLOODPLAIN=4.0000
00168> | LENGTH = 60.00 (m)
00169>
00170> <----- DATA FOR SECTION ( 1.0) ----->
00171> Distance Elevation Manning
00172> .00 .18 .0250
00173> 1.45 .15 .0250 / .0130 Main Channel
00174> 1.50 .00 .0130 Main Channel
00175> 5.50 .12 .0130 Main Channel
00176> 9.50 .00 .0130 Main Channel
00177> 9.55 .15 .0130 / .0250 Main Channel
00178> 11.00 .18 .0250
00179>
00180> <----- TRAVEL TIME TABLE ----->
00181> DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V
00182> (m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
00183> .009 .009 .178E+00 .347E-03 .001 .425 2.35 .004
00184> .019 .019 .710E+00 .277E-02 .008 .674 1.48 .013
00185> .028 .028 .160E+01 .936E-02 .024 .884 1.13 .025
00186> .038 .038 .284E+01 .222E-01 .051 1.070 .93 .040
00187> .047 .047 .444E+01 .433E-01 .092 1.242 .81 .058
00188> .056 .056 .639E+01 .749E-01 .149 1.403 .71 .079
00189> .066 .066 .870E+01 .119E+00 .225 1.554 .64 .102
00190> .075 .075 .114E+02 .178E+00 .322 1.699 .59 .127
00191> .084 .084 .146E+02 .253E+00 .440 1.838 .54 .155
00192> .094 .094 .178E+02 .347E+00 .583 1.972 .51 .185
00193> .103 .103 .215E+02 .462E+00 .752 2.101 .48 .217
00194> .112 .112 .256E+02 .599E+00 .949 2.226 .45 .250
00195> .122 .122 .300E+02 .762E+00 1.186 2.372 .42 .289
00196> .131 .131 .345E+02 .945E+00 1.498 2.602 .38 .341
00197> .141 .141 .391E+02 1.155E+01 1.838 2.821 .35 .397
00198> .150 .150 .436E+02 1.365E+01 2.205 3.031 .33 .455
00199> .160 .160 .488E+02 .163E+01 2.630 3.234 .31 .517
00200> .170 .170 .545E+02 .193E+01 3.090 3.400 .29 .578
00201> .180 .180 .608E+02 .228E+01 3.586 3.536 .28 .637
00202>
00203> X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
00204> S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
00205>
00206> <---- hydrograph ----> <-pipe / channel->
00207> AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
00208> (ha) (cms) (hrs) (mm) (m) (m/s)
00209> INFLOW : ID= 1:000210 2.00 .622 1.00 57.861 .096 2.000
00210> OUTFLOW: ID= 2:000154 2.00 .615 1.02 57.861 .095 1.992
00211>
00212>
00213>
00214> 001:0005
00215> *
00216> *
00217> *# Area S20B
00218> *#=====2
00219> *# 6.00% Slope
00220> *#=====
00221> *
00222>
00223> ROUTE CHANNEL Routing time step (min) = 1.00
00224> | IN> 01:000210 | Number of SEGMENTS = 3
00225> | OUT< 02:000154 | Slopes (%), CHANNEL=6.0000 FLOODPLAIN=6.0000
00226> | LENGTH = 60.00 (m)
00227>
00228> <----- DATA FOR SECTION ( 1.0) ----->
00229> Distance Elevation Manning
00230> .00 .18 .0250
00231> 1.45 .15 .0250 / .0130 Main Channel
00232> 1.50 .00 .0130 Main Channel
00233> 5.50 .12 .0130 Main Channel
00234> 9.50 .00 .0130 Main Channel
00235> 9.55 .15 .0130 / .0250 Main Channel
00236> 11.00 .18 .0250
00237>
00238> <----- TRAVEL TIME TABLE ----->
00239> DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V
00240> (m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
00241> .009 .009 .178E+00 .231E-03 .002 .520 1.92 .005
00242> .019 .019 .710E+00 .185E-02 .010 .826 1.21 .015
00243> .028 .028 .160E+01 .624E-02 .029 1.082 .92 .030
00244> .038 .038 .284E+01 .148E-01 .062 1.311 .76 .049
00245> .047 .047 .444E+01 .289E-01 .113 1.521 .66 .071
00246> .056 .056 .639E+01 .499E-01 .183 1.718 .58 .097
00247> .066 .066 .870E+01 .793E-01 .276 1.904 .53 .125
00248> .075 .075 .114E+02 .118E+00 .394 2.081 .48 .156
00249> .084 .084 .144E+02 .169E+00 .539 2.251 .44 .190
00250> .094 .094 .178E+02 .231E+00 .714 2.415 .41 .226
00251> .103 .103 .215E+02 .308E+00 .921 2.573 .39 .269
00252> .112 .112 .256E+02 .399E+00 1.162 2.727 .37 .307
00253> .122 .122 .300E+02 .508E+00 1.452 2.905 .34 .354
00254> .131 .131 .345E+02 .630E+00 1.834 3.186 .31 .418

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00255> .141 .141 .391E+02 .764E+00 2.251 3.455 .29 .486
00256> .150 .150 .436E+02 .909E+00 2.701 3.712 .27 .557
00257> .160 .160 .488E+02 .108E+01 3.222 3.961 .25 .634
00258> .170 .170 .545E+02 .129E+01 3.784 4.164 .24 .708
00259> .180 .180 .608E+02 .152E+01 4.392 4.331 .23 .780
00260>

00261> X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
00262> S-VOLUME= Volume that can be stored in channel at specified ELEVATION.

00263>
00264> <---- hydrograph ----> <-pipe / channel->
00265> AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
00266> (ha) (cms) (hrs) (mm) (m) (m/s)
00267> INFLOW : ID= 1:000210 2.00 .622 1.00 57.861 .089 2.325
00268> OUTFLOW : ID= 2:000154 2.00 .615 1.02 57.861 .088 2.317
00269>

00270>
00271>
00272> 001:0006-----
00273> *
00274> *
00275> *# Area S20C
00276> *#-----
00277> *# 4.00% Slope
00278> *#-----
00279> *

00280>
00281> ROUTE CHANNEL Routing time step (min) = 1.00
00282> IN> 01:000210 Number of SEGMENTS = 3
00283> OUT< 02:000154 Slopes (%), CHANNEL=4.0000 FLOODPLAIN=4.0000
00284> LENGTH = 60.00 (m)
00285>

00286> <----- DATA FOR SECTION (1.0) ----->
00287> Distance Elevation Manning
00288> .00 .18 .0250
00289> 1.45 .15 .0250 / .0130 Main Channel
00290> 1.50 .00 .0130 Main Channel
00291> 5.50 .12 .0130 Main Channel
00292> 9.50 .00 .0130 Main Channel
00293> 9.55 .15 .0130 / .0250 Main Channel
00294> 11.00 .18 .0250
00295>

00296> <----- TRAVEL TIME TABLE ----->
00297> DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V
00298> (m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
00299> .009 .009 .178E+00 .347E-03 .001 .425 2.35 .004
00300> .019 .019 .710E+00 .277E-02 .008 .674 1.48 .013
00301> .028 .028 .160E+01 .936E-02 .024 .884 1.13 .025
00302> .038 .038 .284E+01 .222E-01 .051 1.070 .93 .040
00303> .047 .047 .444E+01 .443E-01 .092 1.242 .81 .058
00304> .056 .056 .639E+01 .749E-01 .149 1.403 .71 .079
00305> .066 .066 .870E+01 .119E+00 .225 1.554 .64 .102
00306> .075 .075 .114E+02 .178E+00 .322 1.699 .59 .127
00307> .084 .084 .144E+02 .253E+00 .440 1.838 .54 .155
00308> .094 .094 .178E+02 .347E+00 .583 1.972 .51 .185
00309> .103 .103 .215E+02 .462E+00 .752 2.101 .48 .217
00310> .112 .112 .256E+02 .599E+00 .949 2.226 .45 .250
00311> .122 .122 .300E+02 .762E+00 1.186 2.372 .42 .289
00312> .131 .131 .345E+02 .945E+00 1.498 2.602 .38 .341
00313> .141 .141 .391E+02 .115E+01 1.838 2.821 .35 .397
00314> .150 .150 .436E+02 .136E+01 2.205 3.031 .33 .455
00315> .160 .160 .488E+02 .163E+01 2.630 3.234 .31 .517
00316> .170 .170 .545E+02 .193E+01 3.090 3.400 .29 .578
00317> .180 .180 .608E+02 .228E+01 3.586 3.536 .28 .637
00318>

00319> X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
00320> S-VOLUME= Volume that can be stored in channel at specified ELEVATION.

00321>
00322>
00323> <---- hydrograph ----> <-pipe / channel->
00324> AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
00325> (ha) (cms) (hrs) (mm) (m) (m/s)
00326> INFLOW : ID= 1:000210 2.00 .622 1.00 57.861 .095 1.992
00327> OUTFLOW : ID= 2:000154 2.00 .615 1.02 57.861 .095 1.992
00328>

00329>
00330> 001:0007-----
00331> *
00332> *
00333> *# Area S20D
00334> *#-----
00335> *# 2.00% Slope
00336> *#-----
00337> *

00338>
00339> ROUTE CHANNEL Routing time step (min) = 1.00
00340> IN> 01:000210 Number of SEGMENTS = 3
00341> OUT< 02:000154 Slopes (%), CHANNEL=2.0000 FLOODPLAIN=2.0000
00342> LENGTH = 60.00 (m)
00343>

00344> <----- DATA FOR SECTION (1.0) ----->
00345> Distance Elevation Manning
00346> .00 .18 .0250
00347> 1.45 .15 .0250 / .0130 Main Channel
00348> 1.50 .00 .0130 Main Channel
00349> 5.50 .12 .0130 Main Channel
00350> 9.50 .00 .0130 Main Channel
00351> 9.55 .15 .0130 / .0250 Main Channel
00352> 11.00 .18 .0250
00353>

00354> <----- TRAVEL TIME TABLE ----->
00355> DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V
00356> (m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
00357> .009 .009 .178E+00 .694E-03 .001 .300 3.33 .003
00358> .019 .019 .710E+00 .555E-02 .006 4.77 2.10 .009
00359> .028 .028 .160E+01 .187E-01 .017 .625 1.60 .018
00360> .038 .038 .284E+01 .144E-01 .036 .757 1.32 .028
00361> .047 .047 .444E+01 .867E-01 .065 .878 1.14 .041
00362> .056 .056 .639E+01 .150E+00 .106 .992 1.01 .056
00363> .066 .066 .870E+01 .238E+00 .159 1.099 .91 .072
00364> .075 .075 .114E+02 .345E+00 .228 1.201 .83 .090
00365> .084 .084 .144E+02 .506E+00 .311 1.300 .77 .110
00366> .094 .094 .178E+02 .694E+00 .413 1.394 .72 .131
00367> .103 .103 .215E+02 .923E+00 .532 1.486 .67 .153
00368> .112 .112 .256E+02 .120E+01 .671 1.574 .64 .177
00369> .122 .122 .300E+02 .152E+01 .838 1.677 .60 .204
00370> .131 .131 .345E+02 .189E+01 1.059 1.840 .54 .241
00371> .141 .141 .391E+02 .229E+01 1.300 1.995 .50 .280
00372> .150 .150 .436E+02 .273E+01 1.559 2.143 .47 .321
00373> .160 .160 .488E+02 .325E+01 1.860 2.287 .44 .366
00374> .170 .170 .545E+02 .386E+01 2.185 2.404 .42 .409
00375> .180 .180 .608E+02 .456E+01 2.536 2.501 .40 .450
00376>

00377> X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
00378> S-VOLUME= Volume that can be stored in channel at specified ELEVATION.

00379>
00380> <---- hydrograph ----> <-pipe / channel->
00381> AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL

00382> (ha) (cms) (hrs) (mm) (m) (m/s)
00383> INFLOW : ID= 1:000210 2.00 .622 1.00 57.861 .109 1.542
00384> OUTFLOW : ID= 2:000154 2.00 .615 1.02 57.861 .109 1.537
00385>
00386>
00387>
00388> 001:0008-----
00389> *
00390> *
00391> *# Area S20E
00392> *#-----
00393> *# 2.00% Slope
00394> *#-----
00395> *

00396>
00397> ROUTE CHANNEL Routing time step (min) = 1.00
00398> IN> 01:000210 Number of SEGMENTS = 3
00399> OUT< 02:000154 Slopes (%), CHANNEL=2.0000 FLOODPLAIN=2.0000
00400> LENGTH = 60.00 (m)
00401>

00402> <----- DATA FOR SECTION (1.0) ----->
00403> Distance Elevation Manning
00404> .00 .18 .0250
00405> 1.45 .15 .0250 / .0130 Main Channel
00406> 1.50 .00 .0130 Main Channel
00407> 5.50 .12 .0130 Main Channel
00408> 9.50 .00 .0130 Main Channel
00409> 9.55 .15 .0130 / .0250 Main Channel
00410> 11.00 .18 .0250
00411>

00412> <----- TRAVEL TIME TABLE ----->
00413> DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V
00414> (m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
00415> .009 .009 .178E+00 .694E-03 .001 .300 3.33 .003
00416> .019 .019 .710E+00 .555E-02 .006 .477 2.10 .009
00417> .028 .028 .160E+01 .187E-01 .017 .625 1.60 .018
00418> .038 .038 .284E+01 .144E-01 .036 .757 1.32 .028
00419> .047 .047 .444E+01 .867E-01 .065 .878 1.14 .041
00420> .056 .056 .639E+01 .150E+00 .106 .992 1.01 .056
00421> .066 .066 .870E+01 .238E+00 .159 1.099 .91 .072
00422> .075 .075 .114E+02 .345E+00 .228 1.201 .83 .090
00423> .084 .084 .144E+02 .506E+00 .311 1.300 .77 .110
00424> .094 .094 .178E+02 .694E+00 .413 1.394 .72 .131
00425> .103 .103 .215E+02 .923E+00 .532 1.486 .67 .153
00426> .112 .112 .256E+02 .120E+01 .671 1.574 .64 .177
00427> .122 .122 .300E+02 .152E+01 .838 1.677 .60 .204
00428> .131 .131 .345E+02 .189E+01 1.059 1.840 .54 .241
00429> .141 .141 .391E+02 .229E+01 1.300 1.995 .50 .280
00430> .150 .150 .436E+02 .273E+01 1.559 2.143 .47 .321
00431> .160 .160 .488E+02 .325E+01 1.860 2.287 .44 .366
00432> .170 .170 .545E+02 .386E+01 2.185 2.404 .42 .409
00433> .180 .180 .608E+02 .456E+01 2.536 2.501 .40 .450
00434>

00435> X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
00436> S-VOLUME= Volume that can be stored in channel at specified ELEVATION.

00437>
00438> <---- hydrograph ----> <-pipe / channel->
00439> AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
00440> (ha) (cms) (hrs) (mm) (m) (m/s)
00441> INFLOW : ID= 1:000210 2.00 .622 1.00 57.861 .109 1.542
00442> OUTFLOW : ID= 2:000154 2.00 .615 1.02 57.861 .109 1.537
00443>

00444>
00445>
00446> 001:0009-----
00447> *
00448> *
00449> *# Area S107
00450> *#-----
00451> *# 0.90% Slope
00452> *#-----
00453> *

00454>
00455> ROUTE CHANNEL Routing time step (min) = 1.00
00456> IN> 01:000210 Number of SEGMENTS = 3
00457> OUT< 02:000154 Slopes (%), CHANNEL=.9000 FLOODPLAIN=.9000
00458> LENGTH = 60.00 (m)
00459>

00460> <----- DATA FOR SECTION (1.0) ----->
00461> Distance Elevation Manning
00462> .00 .18 .0250
00463> 1.45 .15 .0250 / .0130 Main Channel
00464> 1.50 .00 .0130 Main Channel
00465> 5.50 .12 .0130 Main Channel
00466> 9.50 .00 .0130 Main Channel
00467> 9.55 .15 .0130 / .0250 Main Channel
00468> 11.00 .18 .0250
00469>

00470> <----- TRAVEL TIME TABLE ----->
00471> DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V
00472> (m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
00473> .009 .009 .178E+00 .154E-02 .001 .201 4.96 .002
00474> .019 .019 .710E+00 .123E-01 .004 .320 3.13 .006
00475> .028 .028 .160E+01 .416E-01 .011 .419 2.39 .012
00476> .038 .038 .284E+01 .986E-01 .024 .508 1.97 .019
00477> .047 .047 .444E+01 .193E+00 .044 .589 1.70 .028
00478> .056 .056 .639E+01 .333E+00 .071 .665 1.50 .037
00479> .066 .066 .870E+01 .529E+00 .107 .737 1.36 .048
00480> .075 .075 .114E+02 .789E+00 .153 .806 1.24 .060
00481> .084 .084 .144E+02 .112E+01 .209 .872 1.15 .074
00482> .094 .094 .178E+02 .154E+01 .277 .935 1.07 .088
00483> .103 .103 .215E+02 .205E+01 .357 .997 1.00 .103
00484> .112 .112 .256E+02 .266E+01 .450 1.056 .95 .119
00485> .122 .122 .300E+02 .339E+01 .562 1.125 .89 .137
00486> .131 .131 .345E+02 .420E+01 .710 1.234 .81 .162
00487> .141 .141 .391E+02 .509E+01 .872 1.338 .75 .188
00488> .150 .150 .436E+02 .606E+01 1.046 1.438 .70 .216
00489> .160 .160 .488E+02 .723E+01 1.248 1.534 .65 .245
00490> .170 .170 .545E+02 .858E+01 1.466 1.613 .62 .274
00491> .180 .180 .608E+02 .101E+02 1.701 1.677 .60 .302
00492>

00493> X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
00494> S-VOLUME= Volume that can be stored in channel at specified ELEVATION.

00495>
00496> <---- hydrograph ----> <-pipe / channel->
00497> AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
00498> (ha) (cms) (hrs) (mm) (m) (m/s)
00499> INFLOW : ID= 1:000210 2.00 .622 1.00 57.861 .126 1.167
00500> OUTFLOW : ID= 2:000154 2.00 .615 1.02 57.861 .125 1.161
00501>

00502>
00503>
00504> 001:0010-----
00505> *
00506> *
00507> *# Area S106A
00508> *#-----

```

00509> *# 2.99% Slope
00510> *#-----
00511> *
00512> *
00513> ROUTE CHANNEL Routing time step (min) = 1.00
00514> IN> 01:000210 Number of SEGMENTS = 3
00515> OUT< 02:000154 Slopes (%), CHANNEL=2.9900 FLOODPLAIN=2.9900
00516> LENGTH = 60.00 (m)
00517>
00518> <----- DATA FOR SECTION ( 1.0) ----->
00519> Distance Elevation Manning
00520> .00 .18 .0250
00521> 1.45 .15 .0250 / .0130 Main Channel
00522> 1.50 .00 .0130 Main Channel
00523> 5.50 .12 .0130 Main Channel
00524> 9.50 .00 .0130 Main Channel
00525> 9.55 .15 .0130 / .0250 Main Channel
00526> 11.00 .18 .0250
00527>
00528> <----- TRAVEL TIME TABLE ----->
00529> DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V
00530> (m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
00531> .009 .009 .178E+00 .464E-03 .001 .367 2.72 .003
00532> .019 .019 .710E+00 .272E-02 .007 .583 1.72 .011
00533> .028 .028 .160E+01 .125E-01 .020 .764 1.31 .021
00534> .038 .038 .284E+01 .297E-01 .044 .925 1.08 .035
00535> .047 .047 .444E+01 .580E-01 .079 1.074 .93 .050
00536> .056 .056 .639E+01 .100E+00 .129 1.213 .82 .068
00537> .066 .066 .870E+01 .159E+00 .195 1.344 .74 .088
00538> .075 .075 .114E+02 .230E+00 .278 1.469 .68 .110
00539> .084 .084 .144E+02 .330E+00 .394 1.589 .63 .134
00540> .094 .094 .178E+02 .464E+00 .504 1.705 .59 .160
00541> .103 .103 .215E+02 .617E+00 .650 1.816 .55 .187
00542> .112 .112 .256E+02 .802E+00 .820 1.925 .52 .217
00543> .122 .122 .300E+02 .102E+01 1.025 2.051 .49 .250
00544> .131 .131 .345E+02 .126E+01 1.295 2.249 .44 .295
00545> .141 .141 .391E+02 .153E+01 1.589 2.439 .41 .343
00546> .150 .150 .436E+02 .182E+01 1.906 2.621 .38 .393
00547> .160 .160 .488E+02 .218E+01 2.274 2.796 .36 .447
00548> .170 .170 .545E+02 .258E+01 2.722 2.940 .34 .500
00549> .180 .180 .608E+02 .305E+01 3.100 3.057 .33 .550
00550>
00551> X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
00552> S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
00553> *
00554> <---- hydrograph ----> <-pipe / channel->
00555> AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
00556> (ha) (cms) (hrs) (mm) (m) (m/s)
00557> INFLOW : ID= 1:000210 2.00 .622 1.00 57.861 .101 1.794
00558> OUTFLOW : ID= 2:000154 2.00 .615 1.02 57.861 .101 1.784
00559> *
00560> *
00561> *
00562> 001:0011-----
00563> *
00564> *
00565> *# Area S105B
00566> *#-----
00567> *# 4.00% Slope
00568> *#-----
00569> *
00570> *
00571> ROUTE CHANNEL Routing time step (min) = 1.00
00572> IN> 01:000210 Number of SEGMENTS = 3
00573> OUT< 02:000154 Slopes (%), CHANNEL=4.0000 FLOODPLAIN=4.0000
00574> LENGTH = 60.00 (m)
00575>
00576> <----- DATA FOR SECTION ( 1.0) ----->
00577> Distance Elevation Manning
00578> .00 .18 .0250
00579> 1.45 .15 .0250 / .0130 Main Channel
00580> 1.50 .00 .0130 Main Channel
00581> 5.50 .12 .0130 Main Channel
00582> 9.50 .00 .0130 Main Channel
00583> 9.55 .15 .0130 / .0250 Main Channel
00584> 11.00 .18 .0250
00585>
00586> <----- TRAVEL TIME TABLE ----->
00587> DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V
00588> (m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
00589> .009 .009 .178E+00 .347E-03 .001 .425 2.35 .004
00590> .019 .019 .710E+00 .277E-02 .008 .674 1.48 .013
00591> .028 .028 .160E+01 .936E-02 .024 .884 1.13 .025
00592> .038 .038 .284E+01 .222E-01 .051 1.070 .93 .040
00593> .047 .047 .444E+01 .433E-01 .092 1.242 .81 .058
00594> .056 .056 .639E+01 .749E-01 .149 1.403 .71 .079
00595> .066 .066 .870E+01 .119E+00 .225 1.554 .64 .102
00596> .075 .075 .114E+02 .178E+00 .322 1.699 .59 .127
00597> .084 .084 .144E+02 .253E+00 .440 1.838 .54 .155
00598> .094 .094 .178E+02 .347E+00 .583 1.972 .51 .185
00599> .103 .103 .215E+02 .462E+00 .752 2.101 .48 .217
00600> .112 .112 .256E+02 .599E+00 .949 2.226 .45 .250
00601> .122 .122 .300E+02 .762E+00 1.186 2.372 .42 .289
00602> .131 .131 .345E+02 .945E+00 1.498 2.602 .38 .341
00603> .141 .141 .391E+02 .115E+01 1.838 2.821 .35 .397
00604> .150 .150 .436E+02 .136E+01 2.205 3.031 .33 .455
00605> .160 .160 .488E+02 .163E+01 2.630 3.234 .31 .517
00606> .170 .170 .545E+02 .193E+01 3.090 3.400 .29 .578
00607> .180 .180 .608E+02 .228E+01 3.586 3.536 .28 .637
00608>
00609> X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
00610> S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
00611> *
00612> <---- hydrograph ----> <-pipe / channel->
00613> AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
00614> (ha) (cms) (hrs) (mm) (m) (m/s)
00615> INFLOW : ID= 1:000210 2.00 .622 1.00 57.861 .096 2.000
00616> OUTFLOW : ID= 2:000154 2.00 .615 1.02 57.861 .095 1.992
00617> *
00618> *
00619> *
00620> 001:0012-----
00621> *
00622> *
00623> *# Area S105A
00624> *#-----
00625> *# 1.33% Slope
00626> *#-----
00627> *
00628> *
00629> ROUTE CHANNEL Routing time step (min) = 1.00
00630> IN> 01:000210 Number of SEGMENTS = 3
00631> OUT< 02:000154 Slopes (%), CHANNEL=1.3300 FLOODPLAIN=1.3300
00632> LENGTH = 60.00 (m)
00633>
00634> <----- DATA FOR SECTION ( 1.0) ----->
00635> Distance Elevation Manning

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00636> .00 .18 .0250
00637> 1.45 .15 .0250 / .0130 Main Channel
00638> 1.50 .00 .0130 Main Channel
00639> 5.50 .12 .0130 Main Channel
00640> 9.50 .00 .0130 Main Channel
00641> 9.55 .15 .0130 / .0250 Main Channel
00642> 11.00 .18 .0250
00643>
00644> <----- TRAVEL TIME TABLE ----->
00645> DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V
00646> (m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
00647> .009 .009 .178E+00 .104E-02 .001 .245 4.08 .002
00648> .019 .019 .710E+00 .834E-02 .005 .389 2.57 .007
00649> .028 .028 .160E+01 .282E-01 .014 .509 1.96 .014
00650> .038 .038 .284E+01 .667E-01 .029 .617 1.62 .023
00651> .047 .047 .444E+01 .130E+00 .053 .716 1.40 .034
00652> .056 .056 .639E+01 .225E+00 .086 .809 1.24 .045
00653> .066 .066 .870E+01 .358E+00 .130 .896 1.12 .059
00654> .075 .075 .114E+02 .534E+00 .186 .980 1.02 .073
00655> .084 .084 .144E+02 .760E+00 .254 1.060 .94 .089
00656> .094 .094 .178E+02 .104E+01 .336 1.137 .88 .107
00657> .103 .103 .215E+02 .139E+01 .434 1.211 .83 .125
00658> .112 .112 .256E+02 .180E+01 .547 1.284 .78 .144
00659> .122 .122 .300E+02 .229E+01 .684 1.368 .73 .167
00660> .131 .131 .345E+02 .284E+01 .864 1.500 .67 .197
00661> .141 .141 .391E+02 .344E+01 1.060 1.627 .61 .229
00662> .150 .150 .436E+02 .410E+01 1.272 1.748 .57 .262
00663> .160 .160 .488E+02 .489E+01 1.517 1.865 .54 .298
00664> .170 .170 .545E+02 .581E+01 1.782 1.960 .51 .333
00665> .180 .180 .608E+02 .686E+01 2.068 2.039 .49 .367
00666> X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
00667> S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
00668> *
00669> <---- hydrograph ----> <-pipe / channel->
00670> AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
00671> (ha) (cms) (hrs) (mm) (m) (m/s)
00672> INFLOW : ID= 1:000210 2.00 .622 1.00 57.861 .118 1.328
00673> OUTFLOW : ID= 2:000154 2.00 .615 1.02 57.861 .117 1.324
00674> *
00675> *
00676> *
00677> *
00678> 001:0013-----
00679> *
00680> *
00681> *# Area S105B
00682> *#-----
00683> *# 1.00% Slope
00684> *#-----
00685> *
00686> *
00687> ROUTE CHANNEL Routing time step (min) = 1.00
00688> IN> 01:000210 Number of SEGMENTS = 3
00689> OUT< 02:000154 Slopes (%), CHANNEL=1.0000 FLOODPLAIN=1.0000
00690> LENGTH = 60.00 (m)
00691>
00692> <----- DATA FOR SECTION ( 1.0) ----->
00693> Distance Elevation Manning
00694> .00 .18 .0250
00695> 1.45 .15 .0250 / .0130 Main Channel
00696> 1.50 .00 .0130 Main Channel
00697> 5.50 .12 .0130 Main Channel
00698> 9.50 .00 .0130 Main Channel
00699> 9.55 .15 .0130 / .0250 Main Channel
00700> 11.00 .18 .0250
00701>
00702> <----- TRAVEL TIME TABLE ----->
00703> DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V
00704> (m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
00705> .009 .009 .178E+00 .139E-02 .001 .212 4.71 .002
00706> .019 .019 .710E+00 .111E-01 .004 .337 2.97 .006
00707> .028 .028 .160E+01 .374E-01 .012 .442 2.26 .012
00708> .038 .038 .284E+01 .888E-01 .025 .535 1.87 .020
00709> .047 .047 .444E+01 .173E+00 .046 .621 1.61 .029
00710> .056 .056 .639E+01 .300E+00 .075 .701 1.43 .039
00711> .066 .066 .870E+01 .476E+00 .113 .777 1.29 .051
00712> .075 .075 .114E+02 .710E+00 .161 .850 1.18 .064
00713> .084 .084 .144E+02 .101E+01 .220 .919 1.09 .078
00714> .094 .094 .178E+02 .139E+01 .292 .986 1.01 .092
00715> .103 .103 .215E+02 .185E+01 .376 1.050 .95 .108
00716> .112 .112 .256E+02 .240E+01 .474 1.113 .90 .125
00717> .122 .122 .300E+02 .305E+01 .593 1.186 .84 .145
00718> .131 .131 .345E+02 .378E+01 .749 1.301 .77 .171
00719> .141 .141 .391E+02 .458E+01 .919 1.410 .71 .198
00720> .150 .150 .436E+02 .546E+01 1.103 1.516 .66 .227
00721> .160 .160 .488E+02 .651E+01 1.315 1.617 .62 .259
00722> .170 .170 .545E+02 .773E+01 1.545 1.700 .59 .289
00723> .180 .180 .608E+02 .913E+01 1.793 1.768 .57 .318
00724>
00725> X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
00726> S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
00727> *
00728> <---- hydrograph ----> <-pipe / channel->
00729> AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
00730> (ha) (cms) (hrs) (mm) (m) (m/s)
00731> INFLOW : ID= 1:000210 2.00 .622 1.00 57.861 .124 1.206
00732> OUTFLOW : ID= 2:000154 2.00 .615 1.02 57.861 .123 1.200
00733> *
00734> *
00735> *
00736> 001:0014-----
00737> *
00738> *
00739> *# Area U1N1
00740> *#-----
00741> *# 1.00% Slope
00742> *#-----
00743> *
00744> *
00745> ROUTE CHANNEL Routing time step (min) = 1.00
00746> IN> 01:000210 Number of SEGMENTS = 3
00747> OUT< 02:000154 Slopes (%), CHANNEL=1.0000 FLOODPLAIN=1.0000
00748> LENGTH = 60.00 (m)
00749>
00750> <----- DATA FOR SECTION ( 1.0) ----->
00751> Distance Elevation Manning
00752> .00 .18 .0250
00753> 1.45 .15 .0250 / .0130 Main Channel
00754> 1.50 .00 .0130 Main Channel
00755> 5.50 .12 .0130 Main Channel
00756> 9.50 .00 .0130 Main Channel
00757> 9.55 .15 .0130 / .0250 Main Channel
00758> 11.00 .18 .0250
00759>
00760> <----- TRAVEL TIME TABLE ----->
00761> DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V
00762> (m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)

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00763> .009 .009 .178E+00 .139E-02 .001 .212 4.71 .002
00764> .019 .019 .710E+00 .111E-01 .004 .337 2.97 .006
00765> .028 .028 .160E+01 .374E-01 .012 .442 2.26 .012
00766> .038 .038 .284E+01 .898E-01 .025 .535 1.87 .020
00767> .047 .047 .444E+01 .173E+00 .046 .621 1.61 .029
00768> .056 .056 .639E+01 .300E+00 .075 .701 1.43 .039
00769> .066 .066 .870E+01 .476E+00 .113 .777 1.29 .051
00770> .075 .075 .114E+02 .710E+00 .161 .850 1.18 .064
00771> .084 .084 .144E+02 .101E+01 .220 .919 1.09 .078
00772> .094 .094 .178E+02 .139E+01 .292 .986 1.01 .092
00773> .103 .103 .215E+02 .185E+01 .376 1.050 .95 .108
00774> .112 .112 .256E+02 .240E+01 .474 1.113 .90 .125
00775> .122 .122 .300E+02 .305E+01 .593 1.186 .84 .145
00776> .131 .131 .345E+02 .378E+01 .749 1.301 .77 .171
00777> .141 .141 .391E+02 .458E+01 .919 1.410 .71 .198
00778> .150 .150 .436E+02 .546E+01 1.103 1.516 .66 .227
00779> .160 .160 .488E+02 .651E+01 1.315 1.617 .62 .259
00780> .170 .170 .545E+02 .773E+01 1.545 1.700 .59 .289
00781> .180 .180 .608E+02 .913E+01 1.793 1.768 .57 .318
00782>
00783> X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
00784> S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
00785>
00786>
00787> <---- hydrograph ----> <-pipe / channel->
00788> AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
00789> (ha) (cms) (hrs) (mm) (m) (m/s)
00789> INFLOW : ID= 1:000210 2.00 .622 1.00 57.861 .124 1.206
00790> OUTFLOW : ID= 2:000154 2.00 .615 1.02 57.861 .123 1.200
00791>
00792>
00793>
00794> 001:0015-----
00795> *
00796> *
00797> *
00798> *# Area S104
00799> *#####2
00800> *# 0.50% Slope
00801> *#####
00802> *
00803>
00804> ROUTE CHANNEL Routing time step (min) = 1.00
00805> IN= 01:000210 Number of SEGMENTS = 3
00806> OUF= 02:000154 Slopes (%), CHANNEL= .5000 FLOODPLAIN= .5000
00807> LENGTH = 60.00 (m)
00808>
00809> <----- DATA FOR SECTION ( 1.0) ----->
00810> Distance Elevation Manning
00811> .00 .18 .0250
00812> 1.45 .15 .0250 / .0130 Main Channel
00813> 1.50 .00 .0130 Main Channel
00814> 5.50 .12 .0130 Main Channel
00815> 9.50 .00 .0130 Main Channel
00816> 9.55 .15 .0130 / .0250 Main Channel
00817> 11.00 .18 .0250
00818>
00819> <----- TRAVEL TIME TABLE ----->
00820> DEPTH ELEV X-VOLUME S-VOLUME FLOW RATE VELOCITY TRAV.TIME D x V
00821> (m) (m) (cu.m.) (cu.m.) (cms) (m/s) (min) (m2/s)
00822> .009 .009 .178E+00 .277E-02 .000 .150 6.66 .001
00823> .019 .019 .710E+00 .222E-01 .003 .238 4.19 .004
00824> .028 .028 .160E+01 .749E-01 .008 .312 3.20 .009
00825> .038 .038 .284E+01 .178E+00 .018 .378 2.64 .014
00826> .047 .047 .444E+01 .347E+00 .032 .439 2.28 .021
00827> .056 .056 .639E+01 .599E+00 .053 .496 2.02 .028
00828> .066 .066 .870E+01 .951E+00 .080 .550 1.82 .036
00829> .075 .075 .114E+02 .142E+01 .114 .601 1.66 .045
00830> .084 .084 .144E+02 .202E+01 .156 .650 1.54 .055
00831> .094 .094 .178E+02 .277E+01 .206 .697 1.43 .065
00832> .103 .103 .215E+02 .369E+01 .266 .743 1.35 .077
00833> .112 .112 .256E+02 .479E+01 .335 .787 1.27 .089
00834> .122 .122 .300E+02 .609E+01 .419 .839 1.19 .102
00835> .131 .131 .345E+02 .756E+01 .530 .920 1.09 .121
00836> .141 .141 .391E+02 .916E+01 .650 .997 1.00 .140
00837> .150 .150 .436E+02 .109E+02 .780 1.072 .93 .161
00838> .160 .160 .488E+02 .130E+02 .930 1.143 .87 .183
00839> .170 .170 .545E+02 .155E+02 1.092 1.202 .83 .204
00840> .180 .180 .608E+02 .183E+02 1.268 1.250 .80 .225
00841>
00842> X-VOLUME= Total X-Section volume over given CHANNEL LENGTH at specified DEPTH.
00843> S-VOLUME= Volume that can be stored in channel at specified ELEVATION.
00844>
00845>
00846> AREA <---- hydrograph ----> <-pipe / channel->
00847> (ha) (cms) (hrs) (mm) (m) (m/s)
00848> INFLOW : ID= 1:000210 2.00 .622 1.00 57.861 .138 .978
00849> OUTFLOW : ID= 2:000154 2.00 .614 1.02 57.861 .138 .972
00850>
00851>
00852>
00853> 001:0016-----
00854> *
00855> *
00856> FINISH
00857>
00858> *****
00859> WARNINGS / ERRORS / NOTES
00860>
00861> 001:0003 CALIB STANDHYD
00862> *** ERROR: XIMP cannot be larger than TIMP.
00863> XIMP was forced to equal TIMP.
00864> Simulation ended on 2018-03-29 at 12:41:27
00865> =====
00866>

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STORM HYDRAULIC GRADE LINE CALCULATION SHEET
 RIVERSIDE PARK
 CITY OF OTTAWA
 TAGGART REALTY MANAGEMENT

JOB #: 37923 5.7
 DATE: MARCH 2018
 DESIGN: PD
 FILE: CCS_storm_2018-03-26.xls
 REV #:

FROM EXMH 3 TO CBMH20				MANNING FORMULA - FLOWING FULL						
FRICITION LOSS	FROM MH	TO MH	PIPE ID	DIA (m)	Area (m2)	Perim. (m)	Slope (%)	Hyd.R. (m)	Vel. (m/s)	Q (l/s)
	EXMH3	MH98		0.9750	0.75	3.06	0.080	0.24	1.34	1001.721396
INVERT ELEVATION (m)	77.039	77.183		HYDRAULIC SLOPE = 0.16 %						
OBVERT ELEVATION (m)	78.014	78.158		DESIGN FLOW TO FULL FLOW RATIO (= 0.725						
DIAMETER (mm)				DESIGN FLOW DEPTH = 0.614						
LENGTH (m)				975						
FLOW (l/s)				71.78						
HGL (m) ***	78.014	78.089	0.075							
MANHOLE COEF K= 0.75	LOSS (m)	0.036								
TOTAL HGL (m)				Head loss in manhole simplified method p. 71 (MWDWM) fig1.7.1, Kratio = 0.75 for 45 bends $K_L=0.75$ Velocity = Flow / Area = 0.97 m/s $HL = K_L * V^2 / 2g$						
MAX. SURCHARGE (mm)				-32						

FROM EXMH 3 TO CBMH20				MANNING FORMULA - FLOWING FULL						
FRICITION LOSS	FROM MH	TO MH	PIPE ID	DIA (m)	Area (m2)	Perim. (m)	Slope (%)	Hyd.R. (m)	Vel. (m/s)	Q (l/s)
	98	99		0.9750	0.75	3.06	0.130	0.24	1.34	1001.721396
INVERT ELEVATION (m)	77.183	77.420		HYDRAULIC SLOPE = 0.12 %						
OBVERT ELEVATION (m)	78.158	78.395		DESIGN FLOW TO FULL FLOW RATIO (= 0.764						
DIAMETER (mm)				DESIGN FLOW DEPTH = 0.634						
LENGTH (m)				118.68						
FLOW (l/s)				766						
HGL (m) ***	78.158	78.296	0.139							
MANHOLE COEF K= 0.05	LOSS (m)	0.003								
TOTAL HGL (m)				Head loss in manhole simplified method p. 71 (MWDWM) straight through $K_L=0.05$ Velocity = Flow / Area = 1.03 m/s $HL = K_L * V^2 / 2g$						
MAX. SURCHARGE (mm)				-96						

FROM EXMH 3 TO CBMH20				MANNING FORMULA - FLOWING FULL						
FRICITION LOSS	FROM MH	TO MH	PIPE ID	DIA (m)	Area (m2)	Perim. (m)	Slope (%)	Hyd.R. (m)	Vel. (m/s)	Q (l/s)
	99	100		0.9000	0.64	2.83	0.100	0.23	5.94	3773.789142
INVERT ELEVATION (m)	78.695	81.137		HYDRAULIC SLOPE = 3.23 %						
OBVERT ELEVATION (m)	79.595	82.037		DESIGN FLOW TO FULL FLOW RATIO (= 0.204						
DIAMETER (mm)				DESIGN FLOW DEPTH = 0.270						
LENGTH (m)				900						
FLOW (l/s)				56.15						
HGL (m) ***	79.595	79.697	0.102							
MANHOLE COEF K= 1.50	LOSS (m)	0.112								
TOTAL HGL (m)				Head loss in manhole simplified method p. 71 (MWDWM) flow at 90, assume cons. K_L 1.50 Velocity = Flow / Area = 1.21 m/s $HL = K_L * V^2 / 2g$						
MAX. SURCHARGE (mm)				-630						

FROM EXMH 3 TO CBMH20				MANNING FORMULA - FLOWING FULL						
FRICITION LOSS	FROM MH	TO MH	PIPE ID	DIA (m)	Area (m2)	Perim. (m)	Slope (%)	Hyd.R. (m)	Vel. (m/s)	Q (l/s)
	100	101		0.9000	0.64	2.83	0.200	0.23	1.56	991.0358306
INVERT ELEVATION (m)	87.577	87.801		HYDRAULIC SLOPE = 0.27 %						
OBVERT ELEVATION (m)	88.477	88.701		DESIGN FLOW TO FULL FLOW RATIO (= 0.801						
DIAMETER (mm)				DESIGN FLOW DEPTH = 0.603						
LENGTH (m)				900						
FLOW (l/s)				74.5						
HGL (m) ***	88.477	88.621	0.143							
MANHOLE COEF K= 0.75	LOSS (m)	0.060								
TOTAL HGL (m)				Head loss in manhole simplified method p. 71 (MWDWM) fig1.7.1, Kratio = 0.75 for 45 bends $K_L=0.75$ Velocity = Flow / Area = 1.25 m/s $HL = K_L * V^2 / 2g$						
MAX. SURCHARGE (mm)				-20						



STORM HYDRAULIC GRADE LINE CALCULATION SHEET
RIVERSIDE PARK
CITY OF OTTAWA
TAGGART REALTY MANAGEMENT

JOB #: 37923 5.7
 DATE: MARCH 2018
 DESIGN: PD
 FILE: CCS_storm_2018-03-26.xls

FRICTION LOSS	FROM MH	TO MH	PIPE ID	MANNING FORMULA - FLOWING FULL							
				DIA (m)	Area (m ²)	Perim. (m)	Slope (%)	Hyd.R. (m)	Vel. (m/s)	Q (l/s)	
	101	102									
INVERT ELEVATION (m)	88.576	88.730		0.9000	0.64	2.83	0.160	0.23	1.56	991.07	
OBVERT ELEVATION (m)	89.476	89.630		HYDRAULIC SLOPE = 0.32 %							
DIAMETER (mm)	900			DESIGN FLOW TO FULL FLOW RATIO (= 0.819							
LENGTH (m)	51.24			DESIGN FLOW DEPTH = 0.612							
FLOW (l/s)	812			<div style="border: 1px solid black; padding: 5px;"> Head loss in manhole simplified method p. 71 (MWDM) fig1.7.1, Kratio = 0.75 for 45 bends K_L=0.75 Velocity = Flow / Area = 1.28 m/s HL = K_L * V²/ 2g </div>							
HGL (m) ***	89.476	89.579	0.103								
MANHOLE COEF K= 0.75	LOSS (m)	0.062									
TOTAL HGL (m)		89.641									
MAX. SURCHARGE (mm)		12									

FRICTION LOSS	FROM MH	TO MH	PIPE ID	MANNING FORMULA - FLOWING FULL						
				DIA (m)	Area (m ²)	Perim. (m)	Slope (%)	Hyd.R. (m)	Vel. (m/s)	Q (l/s)
	102	103								
INVERT ELEVATION (m)	88.730	88.929		0.9000	0.64	2.83	0.120	0.23	1.56	991.04
OBVERT ELEVATION (m)	89.630	89.829		HYDRAULIC SLOPE = 0.41 %						
DIAMETER (mm)	900			DESIGN FLOW TO FULL FLOW RATIO (= 0.843						
LENGTH (m)	66.48			DESIGN FLOW DEPTH = 0.630						
FLOW (l/s)	835			<div style="border: 1px solid black; padding: 5px;"> Head loss in manhole simplified method p. 71 (MWDM) flow at 90, assume cons. K_L 1.50 Velocity = Flow / Area = 1.31 m/s HL = K_L * V²/ 2g </div>						
HGL (m) ***	89.641	89.783	0.142							
MANHOLE COEF K= 1.50	LOSS (m)	0.132								
TOTAL HGL (m)		89.915								
MAX. SURCHARGE (mm)		86								

FRICTION LOSS	FROM MH	TO MH	PIPE ID	MANNING FORMULA - FLOWING FULL						
				DIA (m)	Area (m ²)	Perim. (m)	Slope (%)	Hyd.R. (m)	Vel. (m/s)	Q (l/s)
	103	104								
INVERT ELEVATION (m)	88.929	89.183		0.9000	0.64	2.83	0.100	0.23	1.56	991.05
OBVERT ELEVATION (m)	89.829	90.083		HYDRAULIC SLOPE = 0.24 %						
DIAMETER (mm)	900			DESIGN FLOW TO FULL FLOW RATIO (= 0.876						
LENGTH (m)	84.57			DESIGN FLOW DEPTH = 0.648						
FLOW (l/s)	868			<div style="border: 1px solid black; padding: 5px;"> Head loss in manhole simplified method p. 71 (MWDM) straight through K_L=0.05 Velocity = Flow / Area = 1.37 m/s HL = K_L * V²/ 2g </div>						
HGL (m) ***	89.915	90.109	0.195							
MANHOLE COEF K= 0.05	LOSS (m)	0.005								
TOTAL HGL (m)		90.114								
MAX. SURCHARGE (mm)		31								

FRICTION LOSS	FROM MH	TO MH	PIPE ID	MANNING FORMULA - FLOWING FULL						
				DIA (m)	Area (m ²)	Perim. (m)	Slope (%)	Hyd.R. (m)	Vel. (m/s)	Q (l/s)
ACCESS ROAD	104	105								
INVERT ELEVATION (m)	89.408	89.525		0.6750	0.36	2.12	0.100	0.17	1.05	375.73
OBVERT ELEVATION (m)	90.083	90.200		HYDRAULIC SLOPE = 0.15 %						
DIAMETER (mm)	675			DESIGN FLOW TO FULL FLOW RATIO (= 0.743						
LENGTH (m)	58.51			DESIGN FLOW DEPTH = 0.432						
FLOW (l/s)	279			<div style="border: 1px solid black; padding: 5px;"> Head loss in manhole simplified method p. 71 (MWDM) fig1.7.1, Kratio = 0.75 for 45 bends K_L=0.75 Velocity = Flow / Area = 0.78 m/s HL = K_L * V²/ 2g </div>						
HGL (m) ***	90.114	90.179	0.065							
MANHOLE COEF K= 0.75	LOSS (m)	0.023								
TOTAL HGL (m)		90.202								
MAX. SURCHARGE (mm)		2								



STORM HYDRAULIC GRADE LINE CALCULATION SHEET
 RIVERSIDE PARK
 CITY OF OTTAWA
 TAGGART REALTY MANAGEMENT

JOB #: 37923 5.7
 DATE: MARCH 2018
 DESIGN: PD
 FILE: CCS_storm_2018-03-26.xls

FRICTION LOSS		FROM MH	TO MH	PIPE ID	MANNING FORMULA - FLOWING FULL						
ACCESS ROAD		105	106		DIA (m)	Area (m ²)	Perim. (m)	Slope (%)	Hyd.R. (m)	Vel. (m/s)	Q (l/s)
INVERT ELEVATION (m)		90.459	91.756		0.3750	0.11	1.18	0.650	0.09	2.25	247.83
OBVERT ELEVATION (m)		90.834	92.131		HYDRAULIC SLOPE = 1.65 %						
DIAMETER (mm)				375	DESIGN FLOW TO FULL FLOW RATIO () = 0.346						
LENGTH (m)				64.88	DESIGN FLOW DEPTH = 0.150						
FLOW (l/s)				86	Head loss in manhole simplified method p. 71 (MWDM) flow at 90, assume cons. KL = 1.50 Velocity = Flow / Area = 0.78 m/s HL = KL * V ² / 2g						
HGL (m) ***		90.834	90.990	0.156							
MANHOLE COEF K= 1.50		LOSS (m)	0.046								
TOTAL HGL (m)			91.906								
MAX. SURCHARGE (mm)			-225								

FRICTION LOSS		FROM MH	TO MH	PIPE ID	MANNING FORMULA - FLOWING FULL						
ACCESS ROAD		106	107		DIA (m)	Area (m ²)	Perim. (m)	Slope (%)	Hyd.R. (m)	Vel. (m/s)	Q (l/s)
INVERT ELEVATION (m)		91.831	92.064		0.3000	0.07	0.94	0.200	0.08	1.93	136.69
OBVERT ELEVATION (m)		92.131	92.364		HYDRAULIC SLOPE = 0.87 %						
DIAMETER (mm)				300	DESIGN FLOW TO FULL FLOW RATIO () = 0.604						
LENGTH (m)				11.64	DESIGN FLOW DEPTH = 0.168						
FLOW (l/s)				83	Head loss in manhole simplified method p. 71 (MWDM) fig1.7.1, Kratio = 0.75 for 45 bends KL=0.75 Velocity = Flow / Area = 1.17 m/s HL = KL * V ² / 2g						
HGL (m) ***		92.131	92.216	0.085							
MANHOLE COEF K= 0.75		LOSS (m)	0.000								
TOTAL HGL (m)			92.232								
MAX. SURCHARGE (mm)			-132								

FRICTION LOSS		FROM MH	TO MH	PIPE ID	MANNING FORMULA - FLOWING FULL						
ACCESS ROAD		107	CBMH20		DIA (m)	Area (m ²)	Perim. (m)	Slope (%)	Hyd.R. (m)	Vel. (m/s)	Q (l/s)
INVERT ELEVATION (m)		92.114	97.874		0.2500	0.05	0.79	0.650	0.06	2.65	130.22
OBVERT ELEVATION (m)		92.364	98.124		HYDRAULIC SLOPE = 4.70 %						
DIAMETER (mm)				250	DESIGN FLOW TO FULL FLOW RATIO () = 0.576						
LENGTH (m)				120	DESIGN FLOW DEPTH = 0.135						
FLOW (l/s)				75	Head loss in manhole simplified method p. 71 (MWDM) Figure 1.7.:Qu 75 83 0.909098 0.32 Velocity = Flow / Area = 1.53 m/s HL = KL * V ² / 2g						
HGL (m) ***		92.364	94.277	1.913							
MANHOLE COEF K= 0.37		LOSS (m)	0.044								
TOTAL HGL (m)			98.009								
MAX. SURCHARGE (mm)			-115								



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Environment

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de
l'Environnement

RECEIVED
FEB 13 2002

AMÉNDMENT TO CERTIFICATE OF APPROVAL
MUNICIPAL AND PRIVATE SEWAGE WORKS
NUMBER 3-0842-87-006
Notice No. 1

Claridge Homes (Briar Ridge) Inc.
210 Gladstone Avenue, No. 201
Ottawa, Ontario
K4B 1H9

Site Location: Riverwalk Park Subdivision
Kimberwick Crescent
Ottawa City,

You are hereby notified that I have amended Certificate of Approval No. 3-0842-87-006 issued on December 28, 1988 for construction of stormwater management facilities consisting of a primary settling pond and secondary marsh treatment pond, as follows:

modification to raise the height of the overflow weir to an elevation of approximately 76.75 metres;

all in accordance with the application for approval dated December 12, 2001, and supporting information and documentation prepared by Novatech Engineering Ltd., Consulting Engineers and Planners.

This Notice shall constitute part of the approval issued under Certificate of Approval No. 3-0842-87-006 dated December 28, 1988

In accordance with Section 100 of the Ontario Water Resources Act, R.S.O. 1990, Chapter 0.40, as amended, you may by written notice served upon me and the Environmental Review Tribunal within 15 days after receipt of this Notice, require a hearing by the Tribunal. Section 101 of the Ontario Water Resources Act, R.S.O. 1990, Chapter 0.40, provides that the Notice requiring the hearing shall state:

1. The portions of the approval or each term or condition in the approval in respect of which the hearing is required, and;
2. The grounds on which you intend to rely at the hearing in relation to each portion appealed.

The Notice should also include:

3. The name of the appellant;
4. The address of the appellant;
5. The Certificate of Approval number;
6. The date of the Certificate of Approval;
7. The name of the Director;
8. The municipality within which the works are located;

And the Notice should be signed and dated by the appellant.

This Notice must be served upon:

The Secretary*
Environmental Review Tribunal
2300 Yonge St., 12th Floor
P.O. Box 2382
Toronto, Ontario
M4P 1E4

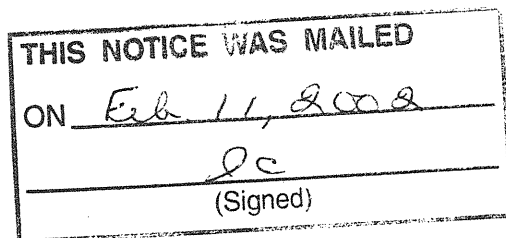
AND

The Director
Section 53, *Ontario Water Resources Act*
Ministry of the Environment
2 St. Clair Avenue West, Floor 12A
Toronto, Ontario
M4V 1L5

* Further information on the Environmental Review Tribunal's requirements for an appeal can be obtained directly from the Tribunal at: Tel: (416) 314-4600, Fax: (416) 314-4506 or www.ert.gov.on.ca

The above noted sewage works are approved under Section 53 of the Ontario Water Resources Act.

DATED AT TORONTO this 7th day of February, 2002



Mohamed Dhalla, P.Eng.
Director
Section 53, *Ontario Water Resources Act*

AM/

c: District Manager, MOE Ottawa
Greg MacDonald, Novatech Engineering Consultants Ltd. ✓

2072 P

AS-BUILT FINAL

- NOTES: GENERAL**
1. ALL WORK TO BE COMPLETED IN ACCORDANCE WITH CITY OF OTTAWA STANDARDS AND OPS DRAWINGS AND SPECIFICATIONS, UNLESS OTHERWISE NOTED.
 2. CONTRACTOR IS TO PROCURE COPIES OF THE STANDARDS AND KEEP ON SITE.
 3. DIMENSIONS AND LAYOUT INFORMATION SHALL BE CONFIRMED PRIOR TO COMMENCEMENT OF CONSTRUCTION.
 4. THE ORIGINAL TOPOGRAPHY AND GROUND ELEVATIONS, SURVEYING AND SURVEY INFORMATION SHOWN ON THIS PLAN ARE SUPPLIED FOR INFORMATION PURPOSES ONLY. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO VERIFY THE ACCURACY OF ALL INFORMATION OBTAINED FROM THIS PLAN.
 5. COORDINATE AND SCHEDULE ALL WORK WITH OTHER TRADES AND CONTRACTORS.
 6. BEFORE COMMENCING CONSTRUCTION, PROVIDE PROOF OF COMPREHENSIVE ALL RISK AND OPERATIONAL LIABILITY INSURANCE INCLUDING BLASTING INSURANCE POLICY TO NAME THE OWNER, ENGINEER, MUNICIPALITY AND THE COUNTY AS CO-INSURED. AMOUNT OF INSURANCE TO BE SPECIFIED BY OWNER'S AGENT.
 7. PRIOR TO ANY ROCK EXCAVATION, CONTRACTOR IS REQUIRED TO COMPLETE A PRE-CONSTRUCTION SURVEY.
 8. DETERMINE THE EXACT LOCATION, SIZE, MATERIAL AND ELEVATION OF ALL EXISTING UTILITIES PRIOR TO COMMENCING CONSTRUCTION. PROTECT AND ASSUME ALL RESPONSIBILITY FOR ALL EXISTING UTILITIES WHETHER OR NOT SHOWN ON THESE DRAWINGS.
 9. OBTAIN AND PAY FOR ALL NECESSARY PERMITS AND APPROVALS FROM THE CITY OF OTTAWA BEFORE COMMENCING CONSTRUCTION.
 10. RESTORE ALL SURFACE FEATURES TO EXISTING CONDITIONS OR BETTER AND TO THE SATISFACTION OF THE CITY OF OTTAWA.
 11. ALL ELEVATIONS ARE GEODETIC AND UTILIZE METRIC UNITS.
 12. SIDE SLOPES FOR ALL EXCAVATIONS ARE TO BE IN ACCORDANCE WITH THE OCCUPATIONAL HEALTH AND SAFETY ACT (ONTARIO REGULATION 213/91).
 13. THE OWNER AGREES TO PREPARE AND IMPLEMENT AN EROSION AND SEDIMENT CONTROL PLAN TO THE SATISFACTION OF THE CITY OF OTTAWA, APPROPRIATE TO THE SITE CONDITIONS, PRIOR TO UNDERTAKING ANY SITE ALTERATIONS AND DURING ALL PHASES OF THE SITE PREPARATION AND CONSTRUCTION IN ACCORDANCE WITH THE CURRENT BEST MANAGEMENT PRACTICES FOR EROSION AND SEDIMENT CONTROL, SUCH AS BUT NOT LIMITED TO INSTALLING FILTER CLOTHS ACROSS VM & CBS TO PREVENT SEDIMENT FROM ENTERING STRUCTURES AND INSTALL AND MAINTAIN A LIGHT DUTY SILT FENCE BARRIER AS REQUIRED.

- NOTES: GRADING**
1. REMOVE FROM SITE ALL EXCESS EXCAVATED MATERIAL UNLESS OTHERWISE INSTRUCTED BY THE ENGINEER.
 2. GRADE AND/OR FILL WHERE REQUIRED.
 3. MATCH EXISTING ELEVATIONS UNLESS OTHERWISE NOTED.
 4. ENSURE POSITIVE DRAINAGE FROM SHORELINE AND BERM INTO STORMWATER POND WHETHER INDICATED OR NOT.
 5. MINIMUM OF 0.5% AND MAXIMUM OF 8% GRADE FOR ALL GRASS AREAS UNLESS OTHERWISE NOTED.
 6. MAXIMUM TERRACING GRADE IS 3:1.

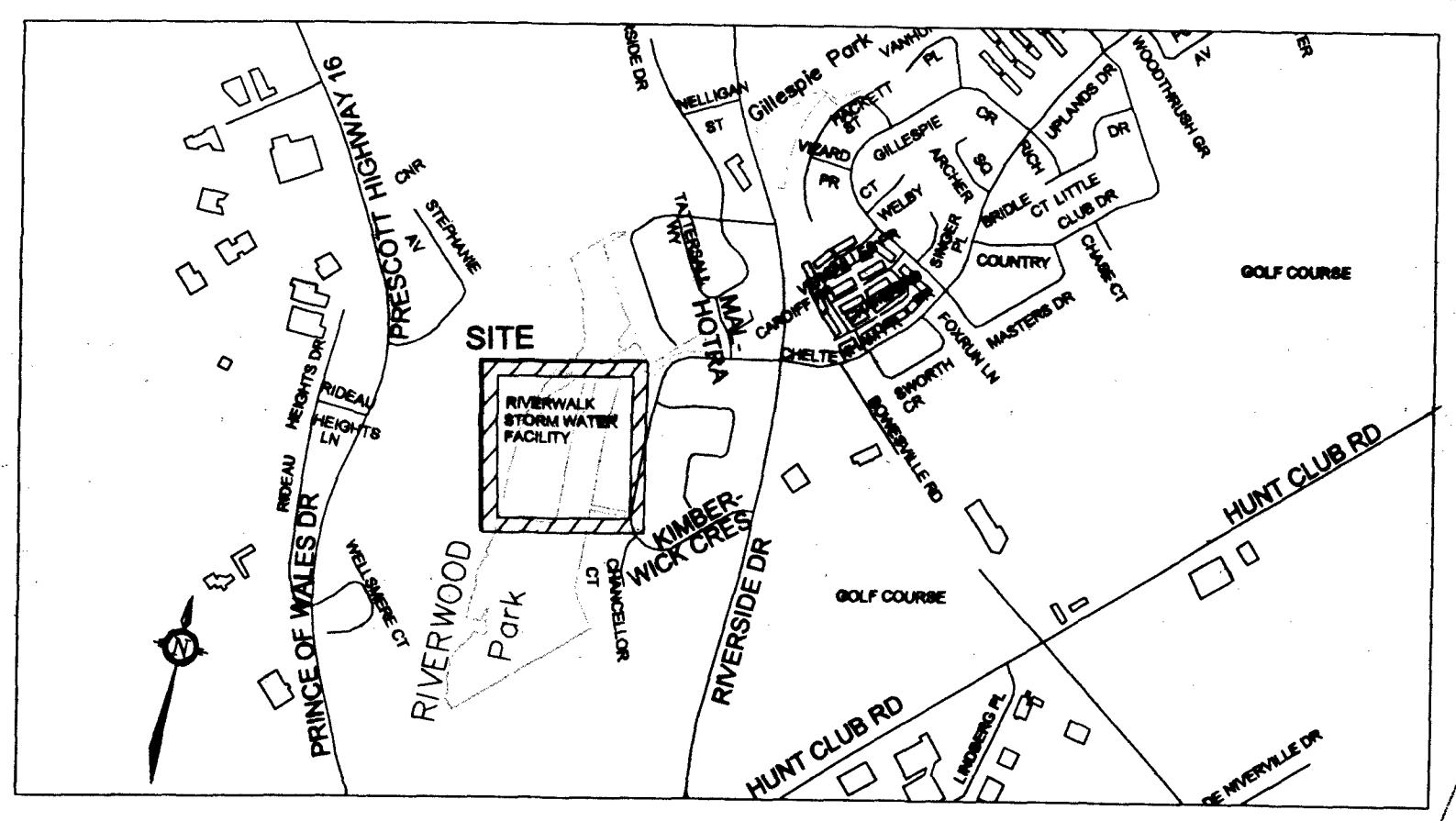
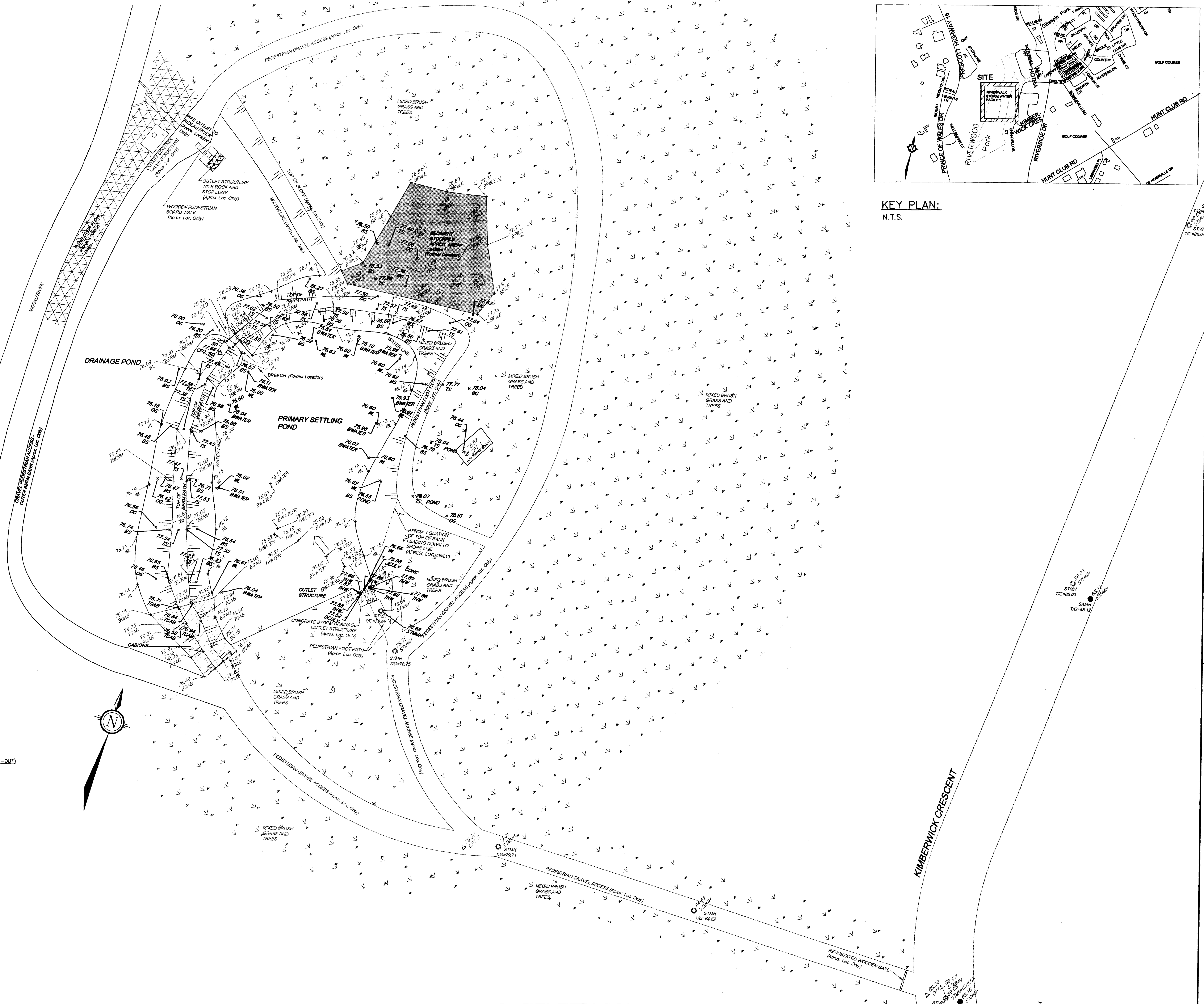
- NOTES: SOIL ANALYSIS**
1. SOIL MATRIX INVESTIGATION - RIVERWALK STORM WATER FACILITY KIMBERWICK CRESCENT, OTTAWA, ONTARIO
 - ACCUTEST: REP.# 2709961, MAY, 2007.

SITE BENCHMARK:
EXISTING FIRE HYDRANT - TOP OF FLANGE, EAST SIDE OF MALHOTRA CRESCENT, SIX HOUSES NORTH OF CUL-DE-SAC.

DERIVED FROM:
NOVATECH ENGINEERING AS-BUILTS
PLAN #9023 P2, RIVERWOOD
LANDINGS (STA 1+400 TO 1+803.93)

- LEGEND**
- ④ BREACH AND DIRECTION OF FLOW
 - GENERAL POND FLOW DIRECTION
 - EXISTING CONCRETE HEADWALL
 - EXISTING STORM MANHOLE
 - EXISTING SANITARY MANHOLE
 - △ SLOPES
 - GABIONS
- SURVEY - NOVEMBER 2007 (POST POND CLEAN-OUT)**
- 76.81' EXISTING TOP OF SLOPE/BERM
 - 75' EXISTING ORIGINAL GROUND
 - 76.81' EXISTING BOTTOM OF SLOPE
 - 76.81' EXISTING WATER LINE
 - 76.81' EXISTING BOTTOM OF WATER
 - 76.81' EXISTING TOP OF HEAD WALL
 - 76.81' EXISTING CONCRETE CULVERT
 - 76.81' EXISTING OVERLAY OF CONCRETE CULVERT
 - 76.81' EXISTING POND TOP OF SLOPE
- SURVEY - MAY 2007**
- 76.81' EXISTING TOP OF BERM ELEVATION
 - 76.14' EXISTING POND WATER LINE
 - 76.82' EXISTING CENTRE LINE OF BREACH
 - 76.93' EXISTING CENTRE LINE OF CONCRETE FLOOR OF HEAD WALL
 - 77.57' EXISTING TOP OF SEDIMENT STOCK PILE
 - 77.57' EXISTING BOTTOM OF SEDIMENT STOCK PILE
 - 76.21' EXISTING WATER LEVEL - TOP
 - 76.82' EXISTING WATER LEVEL - BOTTOM
 - 77.87' EXISTING TOP OF HEAD WALL
 - 78.87' SURVEY CONTROL POINT

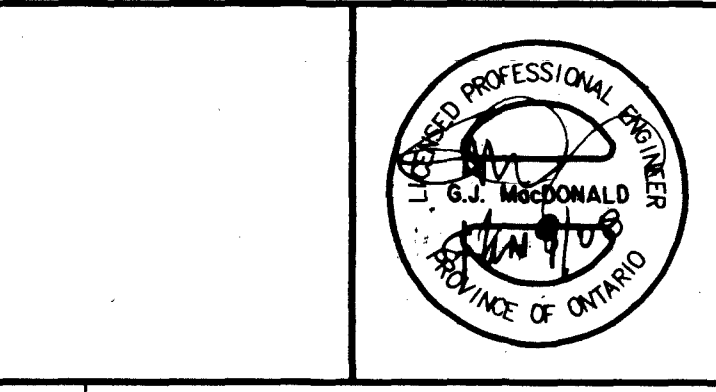
NOTE: THE POSITION OF ALL POLE LINES, CONDUITS, WATERMANS, SEWERS AND OTHER UNDERGROUND AND OVERGROUND UTILITIES AND STRUCTURES IS NOT NECESSARILY SHOWN ON THE CONTRACT DRAWINGS, AND WHERE SHOWN, THE ACCURACY OF THE POSITION OF SUCH UTILITIES AND STRUCTURES IS NOT GUARANTEED. BEFORE STARTING WORK, DETERMINE THE EXACT LOCATION OF ALL SUCH UTILITIES AND STRUCTURES AND ASSUME ALL LIABILITY FOR DAMAGE TO THEM.



KEY PLAN:
N.T.S.

Drawing: 13851550231 2007RiverwalkStormWaterFacility.dwg, Updated: NOV 7, 2007 at 9:28am by mcconnally

No.	REVISION	DATE	BY
1	ISSUED FOR FINAL APPROVAL AND TAKE OVER BY CITY	JAN, 08	GMacD
2	ISSUED FOR SWF TAKE OVER BY CITY	JUN, 07	GMacD



NOVATECH ENGINEERING CONSULTANTS LTD.
ENGINEERS & PLANNERS
Suite 200, 240 Michael Campbell Drive
Ottawa, Ontario, Canada
Telephone: (613) 254-6643
Facsimile: (613) 254-5867
Email: novatech@novatech-eng.com

DESIGN	SCALE
GMacD	1 : 300
GMacD	
MWC	
GMacD	
GMacD	

CITY OF OTTAWA
RIVER WALK STORM WATER - FACILITY (Kimberwick Cres.)
GRADING AND SERVICING PLAN: CLEAN OUT AND BERM REPAIRS, 2007

PROJECT NO. 95023SWF
DATE: MAY, 2007
DRAWING NO. 95023SWF-GS
PLANNING - 95023SWF070

2072 P

APPENDIX D

APPENDIX E

From: Oram, Cody [<mailto:Cody.Oram@ottawa.ca>]
Sent: Monday, May 02, 2016 10:55 AM
To: O'Connor, Ann
Subject: 3860/3930 Riverside Dr_Pre-Consult_Engineering follow up

Hi Ann,

I've summarized the engineering submission requirements below;

1. Servicing and SWM

Water – See attached Water.PNG for approximate location of existing public infrastructure adjacent to the site. Water frontage fee's apply to Riverside Dr. The current watermain frontage rate is \$190/m, for the entire length of the property that will front onto Riverside Drive.

Storm – The City of Ottawa Kimberwick SWF (SWF 1612) is located north of the site, west of Quinterra subdivision. The Kimberwick SWF was designed to receive runoff from 6.0 ha of the site at a runoff coefficient $C=0.7$. See attached the Certificate of Approval for the Storm Pond, Storm Pond Design Report, design and as-built plans of the pond. The site will need to control the 100 year storm event to a 5 year event using a $C=0.7$. The City is not aware of the storm pipe leading south towards the site. The pipe may have been proposed and not actually built; this will need to be verified in the field.

Sanitary – The development is to be serviced by extending the existing 525mm dia. sanitary sewer from north of the site (Chancellor Crt.), see attached Sanitary.PNG for approximate location of sanitary sewer. The sanitary sewer is to be extended through the site to the south property line and designed to service approximately 47.3 hectares of land south of the Hunt Club Rd. The Servicing Study will need to clearly demonstrate that the sanitary sewer is capable of servicing the subject site as well as the land's south of Hunt Club Rd. The previous report submitted in 2008, prepared by IBI Group did not include information on the 610 mm watermain crossing at Hunt Club. Hunt Club watermain plans will be forwarded under a separate email to the civil consultant. The functional design plan and profile of the sanitary sewer to be extended south of the property will need to be revised to include the watermain and submitted for review.

2. Geotechnical Investigation and Slope Stability Study

- Discussion on sanitary sewer easement width and location to be included.

3. Noise Study

4. Phase I Environmental Site Assessment, Phase II ESA if required.

5. Plans required;

- a. Site Servicing Plan (Plan and Profile's for all services requiring MOE ECA)
- b. Grade Control and Drainage Plan
- c. Erosion and Sediment Control Plan

Additional Information;

- The Servicing Study Guidelines for Development Applications are available at the following address: <http://ottawa.ca/en/development-application-review-process-0/servicing-study-guidelines-development-applications>
- Servicing and site works shall be in accordance with the following documents:
 - ⇒ Ottawa Sewer Design Guidelines (October 2012)
 - ⇒ Ottawa Design Guidelines – Water Distribution (2010)

- ⇒ Geotechnical Investigation and Reporting Guidelines for Development Applications in the City of Ottawa (2007)
- ⇒ City of Ottawa Slope Stability Guidelines for Development Applications (revised 2012)
- ⇒ City of Ottawa Environmental Noise Control Guidelines (January, 2016)
- ⇒ City of Ottawa Park and Pathway Development Manual (2012)
- ⇒ City of Ottawa Accessibility Design Standards (2012)
- ⇒ Ottawa Standard Tender Documents (latest version)
- ⇒ Ontario Provincial Standards for Roads & Public Works (2013)
- Record drawings and utility plans are also available for purchase from the City (Contact the City's Information Centre by email at InformationCentre@ottawa.ca or by phone at (613) 580-2424 x.44455).
- Water Boundary condition requests must include the location of the service and the expected loads required by the proposed development. Please provide the following information:
 - i. Location of service
 - ii. Type of development and the amount of fire flow required (as per FUS, 1999).
 - iii. Average daily demand: ___ l/s.
 - iv. Maximum daily demand: ___ l/s.
 - v. Maximum hourly daily demand: ___ l/s.
- An MOECC Environmental Compliance Approval (Private Sewage Works) will be required for the proposed development. Please contact Ontario Ministry of the Environment and Climate Change, Ottawa District Office to arrange a pre-submission consultation:
 - For residential applications: Charlie Primeau, (613) 521-3450, ext. 251, Charlie.Primeau@ontario.ca
 - For I/C/I applications: Emily Diamond, (613) 521-3450, ext. 238, Emily.Diamond@ontario.ca

If you have any questions please don't hesitate to call or email.

Regards,

Cody

Cody Oram, P.Eng.

Project Manager, Development Review

(Urban Services) Outer

Gestionnaire de projets

(Secteur urbain) Extérieur

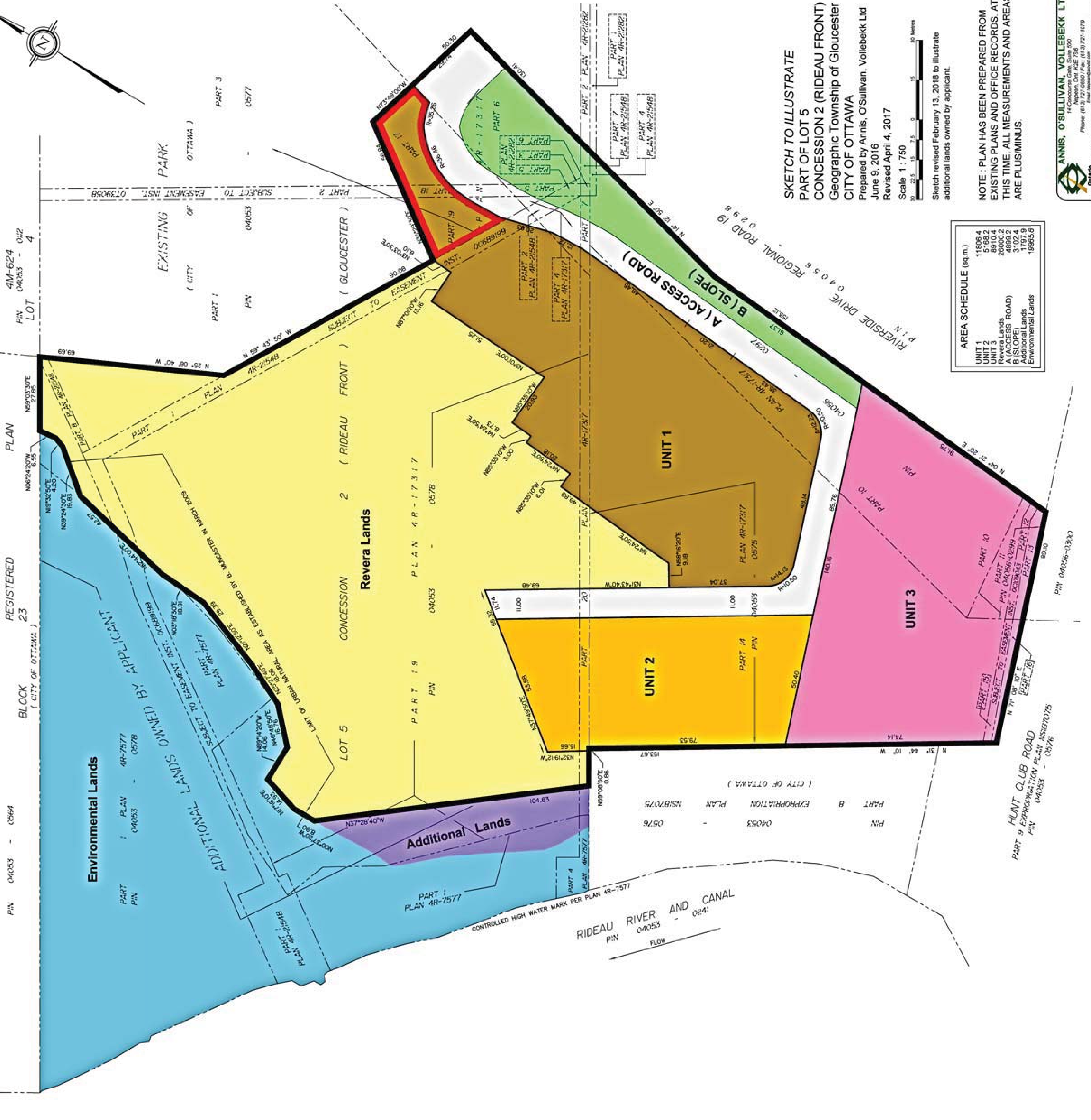
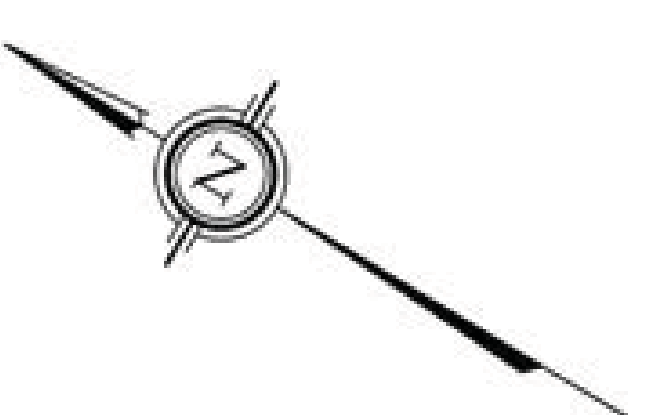


City of Ottawa | ville d'Ottawa

☎ 613.580.2424 ext/poste 13422

Please consider the environment before printing this e-mail.

APPENDIX F



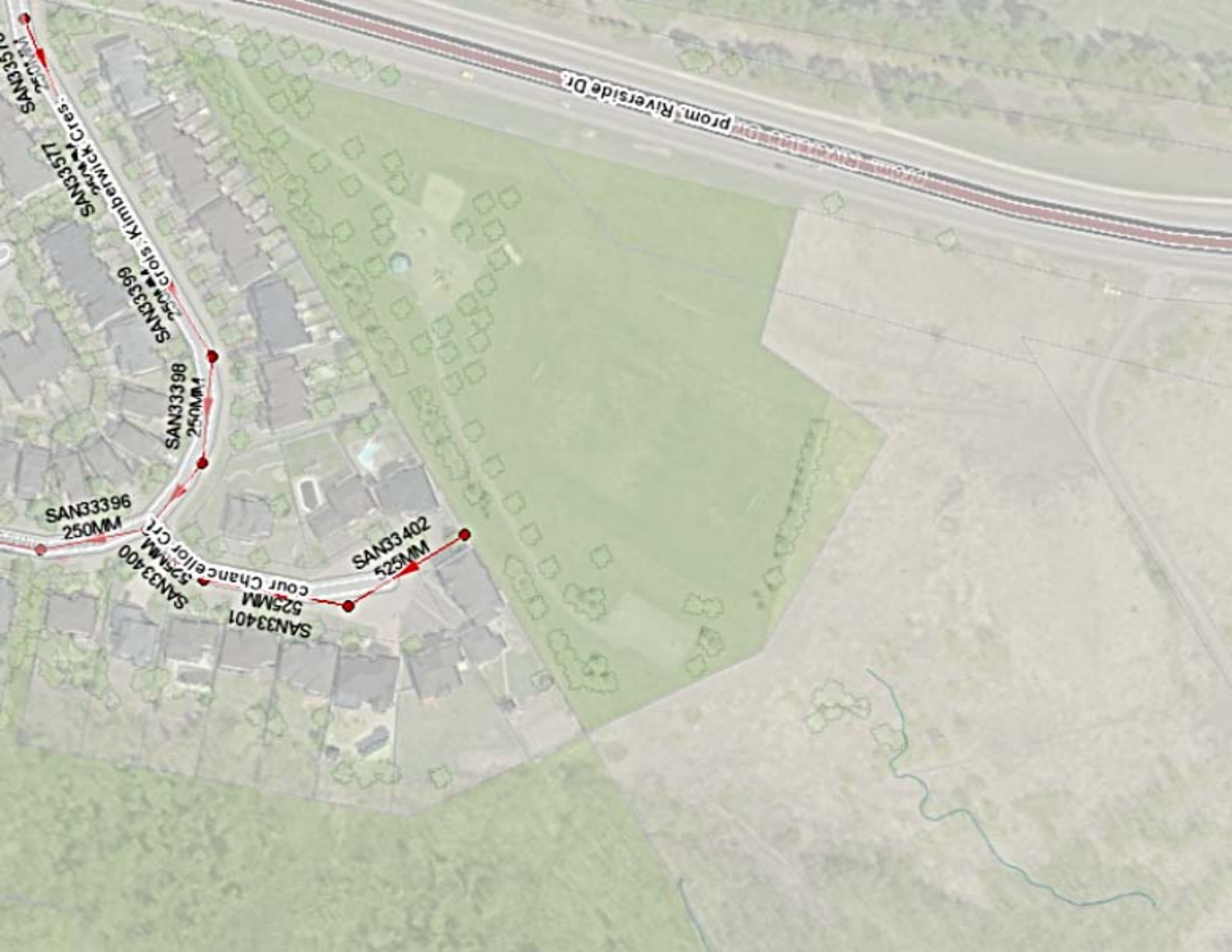
**SKETCH TO ILLUSTRATE
PART OF LOT 5
CONCESSION 2 (RIDEAU FRONT)
Geographic Township of Gloucester
CITY OF OTTAWA**
Prepared by Annis, O'Sullivan, Vollebek Ltd
June 9, 2016
Revised April 4, 2017
Scale 1 : 750

Sketch revised February 13, 2018 to illustrate additional lands owned by applicant.

AREA SCHEDULE (sq. m.)	
UNIT 1	11806.4
UNIT 2	8910.4
UNIT 3	28000.2
Revera Lands	48892.2
A (ACCESS ROAD)	3102.4
B (SLOPE)	1707.9
Additional Lands	19865.6
Environmental Lands	19865.6

NOTE : PLAN HAS BEEN PREPARED FROM EXISTING PLANS AND OFFICE RECORDS. AT THIS TIME, ALL MEASUREMENTS AND AREAS ARE PLUS/MINUS.





Prom. Riverside Dr.

SAN33395
250MM

SAN33377
Kimberwick Cres.

SAN33399
Crais Kimberwick Cres.

SAN33398
250MM

SAN33396
250MM

SAN33400
525MM
Chancellor Crt

SAN33401
525MM

SAN33402
525MM