

**TRANSPORTATION NOISE
AND VIBRATION
ASSESSMENT**

93 Norman Street
Ottawa, Ontario

REPORT: 21-011 – Transportation Noise and Vibration



March 1, 2021

PREPARED FOR

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EXECUTIVE SUMMARY

This report describes a transportation noise and vibration assessment in support of a Site Plan Control (SPC) application for the proposed development located at 93 Norman Street in Ottawa, Ontario. The development comprises a residential building which rises to 9 storeys at the west and 5 storeys at the east of the property. The primary sources of transportation noise include Preston Street, Highway 417, and the O-Train Line 2 (Trillium Line) light rail. As the site is in proximity to the O-Train Line 2 Light Rail Transit (LRT) line, a ground vibration impact assessment from the LRT on the proposed development was conducted following the procedures outlined in the Federal Transit Authorities (FTA) protocol. Figure 1 illustrates a complete site plan with the surrounding context.

The assessment is based on (i) theoretical noise prediction methods that conform to the Ministry of the Environment, Conservation and Parks (MECP) and City of Ottawa requirements; (ii) noise level criteria as specified by the City of Ottawa's Environmental Noise Control Guidelines (ENCG); (iii) future vehicular traffic volumes based on the City of Ottawa's Official Plan roadway classifications; (iv) architectural drawings provided by Roderick Lahey Architect Inc. in February 2021; and (v), ground-borne vibration criteria as specified by the Federal Transit Authority (FTA) Protocol.

The results of the current analysis indicate that noise levels will range between 51 and 71 dBA during the daytime period (07:00-23:00) and between 46 and 63 dBA during the nighttime period (23:00-07:00). The highest noise level (71 dBA) occurs at the north façade, which is most exposed to Highway 417. Building components with a higher Sound Transmission Class (STC) rating will be required where exterior noise levels exceed 65 dBA, as indicated in Figure 3.

Results of the calculation also indicate the development will require central air conditioning, or similar mechanical ventilation, which will allow occupants to keep windows closed to maintain a comfortable indoor living environment. A Warning Clause will also be required on all Lease, Purchase and Sale Agreements, as summarized in Section 6.

Noise levels at the Level 6 and rooftop terraces are expected to exceed 55 dBA during the daytime period without a noise barrier. If these areas are to be used as outdoor living areas, noise control measures are required to reduce noise levels as close as possible to 55 dBA where technically and administratively



feasible. Further analysis investigated the noise mitigating impact of raising the perimeter guards from 1.2 m to 2.5 m above the walking surface (see Table 4). Results of the investigation proved that noise levels cannot easily be reduced to 55 dBA. It was determined that a noise barrier over 2.2 meters in height would be required to reduce noise levels to below 60 dBA at both receptors. However, the inclusion of a noise barrier/perimeter guard greater than 1.5 meters in height would negatively impact the space architecturally by blocking views. Therefore, it is not feasible to protect the amenity terraces with a high noise barrier or other control measure. As mitigated noise levels are above 55 dBA, a Warning Clause is required. The guard must be constructed from materials having a minimum surface density of 20 kg/m² (STC rating of 30) and contain no gaps. Design of the guardrail will conform to the requirements outlined in Part 5 of the ENCG and Section 6 of this report.

Estimated vibration levels at the foundation nearest to the O-Train LRT are expected to be 0.07mm/s RMS (69 dBV), based on the FTA protocol and an offset distance of 24 m to the nearest track centerline. Details of the calculation are provided in Appendix A. Since predicted vibration levels do not exceed the criterion of 0.10 mm/s RMS at the foundation, concerns due to vibration impacts on the site are not expected. As vibration levels are acceptable, correspondingly, regenerated noise levels are also expected to be acceptable.

With regard to stationary noise impacts, a stationary noise study is recommended for the site during the detailed design once mechanical plans for the proposed building become available. The stationary noise study would assess impacts of stationary noise from rooftop mechanical units serving the proposed building on surrounding noise-sensitive areas. This study will include recommendations for any noise control measures that may be necessary to ensure noise levels fall below ENCG limits. Noise impacts can generally be minimized by judicious selection and placement of the equipment.

An initial assessment of the area identified several low-rise buildings in the immediate vicinity. As the development's mechanical equipment will primarily reside on the building's high roof in the mechanical penthouse, stationary noise impacts onto the surroundings are not expected to be a concern. Similarly, stationary noise impacts from existing buildings onto the proposed development are expected to be negligible as only a few nearby properties possess standard sized Rooftop Units (RTU) which are positioned several meters away from the development.

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1. INTRODUCTION

Gradient Wind Engineering Inc. (Gradient Wind) was retained by Tamarack (Norman) Corporation to undertake a transportation noise and vibration assessment in support of a Site Plan Control (SPC) application for the proposed development located at 93 Norman Street in Ottawa in Ottawa, Ontario. This report summarizes the methodology, results, and recommendations related to the assessment of exterior and interior noise levels generated by local transportation noise and vibration sources.

Our work is based on theoretical noise calculation methods conforming to the City of Ottawa¹ and Ministry of the Environment, Conservation and Parks (MECP)² guidelines. Noise calculations were based on architectural drawings provided by Roderick Lahey Architect Inc. in February 2021, with future traffic volumes corresponding to the City of Ottawa's Official Plan (OP) roadway classifications.

2. TERMS OF REFERENCE

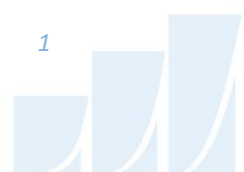
The focus of this transportation noise and vibration assessment is the proposed residential development located at 93 Norman Street in Ottawa, Ontario. The subject site is situated on a rectangular parcel of land bounded by Beech Street to the north, Preston Street to the east, Norman Street to the south, and the O-Train Line 2 (Trillium Line) light rail to the west. The development comprises a residential building which rises to 9 storeys at the west and 5 storeys at the east of the property. The development includes two levels of underground parking.

The ground floor comprises residential space and lobby. Vehicular access to underground parking is provided from Norman Street. The 5-storey podium portion on the eastern part of the building comprises residential suites and an outdoor amenity terrace on the roof (Level 6). The 9-storey massing on the western part of the building comprises residential suites from Levels 1-9. Outdoor amenities are provided at the Mechanical Penthouse Level.

The site is surrounded by a mix of mid and high-rise buildings from the northeast clockwise to the southwest, and mostly low-rise buildings in the remaining compass directions. The primary sources of

¹ City of Ottawa Environmental Noise Control Guidelines, January 2016

² Ontario Ministry of the Environment and Climate Change – Environmental Noise Guidelines, Publication NPC-300, Queens Printer for Ontario, Toronto, 2013



transportation noise include Preston Street, Highway 417, and the O-Train Line 2 (Trillium Line) light rail. The primary source of ground-borne vibration is the O-Train Line 2 light rail line to the west. As per City of Ottawa's Official Plan, the light rail line is situated within 75 m from the nearest property line. As a result, a ground vibration impact assessment from the light rail system on the proposed development was conducted following the procedures outlined in the Federal Transit Authorities (FTA) protocol. Figure 1 illustrates a complete site plan with surrounding context.

With regard to stationary noise impacts, a stationary noise study is recommended for the site during the detailed design once mechanical plans for the proposed building become available. This study would assess impacts of stationary noise from rooftop mechanical units serving the proposed building on surrounding noise-sensitive areas. This study will include recommendations for any noise control measures that may be necessary to ensure noise levels fall below ENCG limits. Noise impacts can generally be minimized by judicious selection and placement of the equipment.

3. OBJECTIVES

The principal objectives of this study are to (i) calculate the future noise levels on the study buildings produced by local road and railway traffic, (ii) predict vibration levels on the study building produced from the light rail system, and (iii) ensure that interior and exterior noise and vibration levels do not exceed the allowable limits specified by the City of Ottawa's Environmental Noise Control Guidelines as outlined in Section 4.2 of this report.

4. METHODOLOGY

4.1 Background

Noise can be defined as any obtrusive sound. It is created at a source, transmitted through a medium, such as air, and intercepted by a receiver. Noise may be characterized in terms of the power of the source or the sound pressure at a specific distance. While the power of a source is characteristic of that particular source, the sound pressure depends on the location of the receiver and the path that the noise takes to reach the receiver. Measurement of noise is based on the decibel unit, dBA, which is a logarithmic ratio referenced to a standard noise level (2×10^{-5} Pascals). The 'A' suffix refers to a weighting scale, which better represents how the noise is perceived by the human ear. With this scale, a doubling of power results in a



3 dBA increase in measured noise levels and is just perceptible to most people. An increase of 10 dBA is often perceived to be twice as loud.

4.2 Roadway Traffic Noise

4.2.1 Criteria for Roadway Traffic Noise

For surface roadway traffic noise, the equivalent sound energy level, L_{eq} , provides a measure of the time-varying noise levels, which is well correlated with the annoyance of sound. It is defined as the continuous sound level, which has the same energy as a time-varying noise level over a period of time. For roadways, the L_{eq} is commonly calculated on the basis of a 16-hour (L_{eq16}) daytime (07:00-23:00) / 8-hour (L_{eq8}) nighttime (23:00-07:00) split to assess its impact on residential buildings. The City of Ottawa’s Environmental Noise Control Guidelines (ENCG) specifies that the recommended indoor noise limit range (that is relevant to this study) is 45 and 40 dBA for living rooms and sleeping quarters respectively for roadway as listed in Table 1. Based on Gradient Wind’s experience, more comfortable indoor noise levels should be targeted, towards 42, and 37 dBA, respectively, to control peak noise and deficiencies in building envelope construction.

TABLE 1: INDOOR SOUND LEVEL CRITERIA (ROAD)³

Type of Space	Time Period	L_{eq} (dBA)
General offices, reception areas, retail stores, etc.	07:00 – 23:00	50
Living/dining/den areas of residences , hospitals, schools, nursing/retirement homes, day-care centres, theatres, places of worship, libraries, individual or semi-private offices, conference rooms, etc.	07:00 – 23:00	45
Sleeping quarters of hotels/motels	23:00 – 07:00	45
Sleeping quarters of residences , hospitals, nursing/retirement homes, etc.	23:00 – 07:00	40

³ Adapted from ENCG 2016 – Tables 2.2b and 2.2c

Predicted noise levels at the plane of window (POW) dictate the action required to achieve the recommended sound levels. An open window is considered to provide a 10 dBA reduction in noise, while a standard closed window is capable of providing a minimum 20 dBA noise reduction⁴. A closed window due to a ventilation requirement will bring noise levels down to achieve an acceptable indoor environment⁵. Therefore, where noise levels exceed 55 dBA daytime and 50 dBA nighttime, the ventilation for the building should consider the need for having windows and doors closed, which triggers the need for forced air heating with provision for central air conditioning. Where noise levels exceed 65 dBA daytime and 60 dBA nighttime, air conditioning will be required and building components will require higher levels of sound attenuation⁶.

The sound level criterion for outdoor living areas (OLA) is 55 dBA, which applies during the daytime (07:00 to 23:00). When noise levels exceed 55 dBA, mitigation should be provided to reduce noise levels where technically and administratively feasible to acceptable levels at or below the criterion. Furthermore, noise levels at the OLA must not exceed 60 dBA if mitigation can be technically and administratively achieved.

4.2.2 Theoretical Roadway Noise Predictions

Noise predictions were performed with the aid of the MECF computerized noise assessment program, STAMSON 5.04, for road analysis. Appendix A includes the STAMSON 5.04 input and output data. Roadway traffic noise calculations were performed by treating each roadway segment as separate line sources of noise. In addition to the traffic volumes summarized in Table 2, theoretical noise predictions were based on the following parameters:

- Truck traffic on all roadways was taken to comprise 5% heavy trucks and 7% medium trucks, as per ENCG requirements for noise level predictions.
- The day/night split for all streets was taken to be 92%/8%, respectively.
- Ground surfaces were taken to be reflective due to the presence of hard (paved) ground. For highway traffic noise, absorptive ground surface was used to account for blockage due to the numerous houses situated between the study site and Highway 417.

⁴ Burberry, P.B. (2014). Mitchell's Environment and Services. Routledge, Page 125

⁵ MOECP, Environmental Noise Guidelines, NPC 300 – Part C, Section 7.8

⁶ MOECP, Environmental Noise Guidelines, NPC 300 – Part C, Section 7.1.3

- Topography was assumed to be a flat/gentle slope surrounding the study building.
- A difference in elevation for Highway 417 and the LRT was measured to be approximately 4 meters above grade and 7 meters below grade, respectively.
- For select sources where appropriate, receptors considered the proposed and/or existing buildings as a barrier partially or fully obstructing exposure to the source as illustrated by exposure angles in Figures 4-7.
- Noise receptors were strategically placed at 9 locations around the study area (see Figure 2).
- Receptor distances and exposure angles are illustrated in Figures 4-7.

4.2.1 Transportation Traffic Volumes

The ENCG dictates that noise calculations should consider future sound levels based on a roadway’s classification at the mature state of development. Therefore, traffic volumes are based on the roadway classifications outlined in the City of Ottawa’s Official Plan (OP) and Transportation Master Plan⁷ which provide additional details on future roadway expansions. Average Annual Daily Traffic (AADT) volumes are then based on data in Table B1 of the ENCG for each roadway classification. Table 2 (below) summarizes the AADT values used for each roadway included in this assessment.

TABLE 2: TRANSPORTATION TRAFFIC DATA

Segment	Roadway Traffic Data	Speed Limit (km/h)	Traffic Volumes
Highway 417	8 Lane Freeway	100	146,664
Preston Street	2-Lane Urban Arterial Undivided	50	15,000
O-Train Line 2	Light Rail Transit	50	192/24*

*Daytime/Nighttime volumes based on the City of Ottawa’s Environmental Assessment for the LRT Project

⁷ City of Ottawa Transportation Master Plan, November 2013



4.3 Indoor Noise Calculations

The difference between outdoor and indoor noise levels is the noise attenuation provided by the building envelope. According to common industry practice, complete walls and individual wall elements are rated according to the Sound Transmission Class (STC). The STC ratings of common residential walls built in conformance with the Ontario Building Code (2012) typically exceed STC 35, depending on exterior cladding, thickness and interior finish details. For example, brick veneer walls can achieve STC 50 or more. Standard commercially sided exterior metal stud walls have around STC 45. Standard good quality double-glazed non-operable windows can have STC ratings ranging from 25 to 40, depending on the window manufacturer, pane thickness and inter-pane spacing. As previously mentioned, the windows are the known weak point in a partition.

As per Section 4.2, when daytime noise levels from road sources at the plane of the window exceed 65 dBA, calculations must be performed to evaluate the sound transmission quality of the building components to ensure acceptable indoor noise levels. The calculation procedure⁸ considers:

- Window type and total area as a percentage of total room floor area
- Exterior wall type and total area as a percentage of the total room floor area
- Acoustic absorption characteristics of the room
- Outdoor noise source type and approach geometry
- Indoor sound level criteria, which varies according to the intended use of a space

Based on published research⁹, exterior walls possess specific sound attenuation characteristics that are used as a basis for calculating the required STC ratings of windows in the same partition. Due to the limited information available at the time of the study, which was prepared for site plan approval, detailed floor layouts and building elevations have not been finalized; therefore, detailed STC calculations could not be performed at this time. As a guideline, the anticipated STC requirements for windows have been estimated based on the overall noise reduction required for each intended use of space (STC = outdoor noise level – targeted indoor noise levels).

⁸ Building Practice Note: Controlling Sound Transmission into Buildings by J.D. Quirt, National Research Council of Canada, September 1985

⁹ CMHC, Road & Rail Noise: Effects on Housing

4.4 Ground Vibration and Ground-borne Noise

Rail systems and heavy vehicles on roadways can produce perceptible levels of ground vibrations, especially when they are in close proximity to residential neighbourhoods or vibration-sensitive buildings. Similar to sound waves in air, vibrations in solids are generated at a source, propagated through a medium, and intercepted by a receiver. In the case of ground vibrations, the medium can be uniform, or more often, a complex layering of soils and rock strata. Also, similar to sound waves in air, ground vibrations produce perceptible motions and regenerated noise known as 'ground-borne noise' when the vibrations encounter a hollow structure such as a building. Ground-borne noise and vibrations are generated when there is excitation of the ground, such as from a train or subway. Repetitive motion of the wheels on the track or rubber tires passing over an uneven surface causes vibration to propagate through the soil. When they encounter a building, vibrations pass along the structure of the building beginning at the foundation and propagating to all floors. Air inside the building excited by the vibrating walls and floors represents regenerated airborne noise. Characteristics of the soil and the building are imparted to the noise, thereby creating a unique noise signature.

Human response to ground vibrations is dependent on the magnitude of the vibrations, which is measured by the root mean square (RMS) of the movement of a particle on a surface. Typical units of ground vibration measures are millimeters per second (mm/s), or inch per second (in/s). Since vibrations can vary over a wide range, it is also convenient to represent them in decibel units, or dBV. In North America, it is common practice to use the reference value of one micro-inch per second ($\mu\text{in/s}$) to represent vibration levels for this purpose. The threshold level of human perception to vibrations is about 0.10 mm/s RMS or about 72 dBV. Although somewhat variable, the threshold of annoyance for continuous vibrations is 0.5 mm/s RMS (or 85 dBV), five times higher than the perception threshold, whereas the threshold for significant structural damage is 10 mm/s RMS (or 112 dBV), at least one hundred times higher than the perception threshold level.

4.4.1 Ground Vibration Criteria

In the United States, the Federal Transportation Authority (FTA) has set vibration criteria for sensitive land uses next to transit corridors. Similar standards have been developed by the MECP. These standards indicate that the appropriate criteria for residences is 0.10 mm/s RMS for vibrations. For main line

railways, a document titled *Guidelines for New Development in Proximity to Railway Operations*¹⁰, indicates that vibration conditions should not exceed 0.14 mm/s RMS averaged over a one second time-period at the first floor and above of the proposed building. The Federal Transportation Authority (FTA) criterion was adopted as the appropriate standard for this study. As the main vibration source is due to the O-Trail LRT which has frequent events, the 0.10 mm/s RMS (72 dBV) vibration criteria and 35 dBA ground-borne noise criteria were adopted for this study.

4.4.2 Theoretical Ground Vibration Prediction Procedure

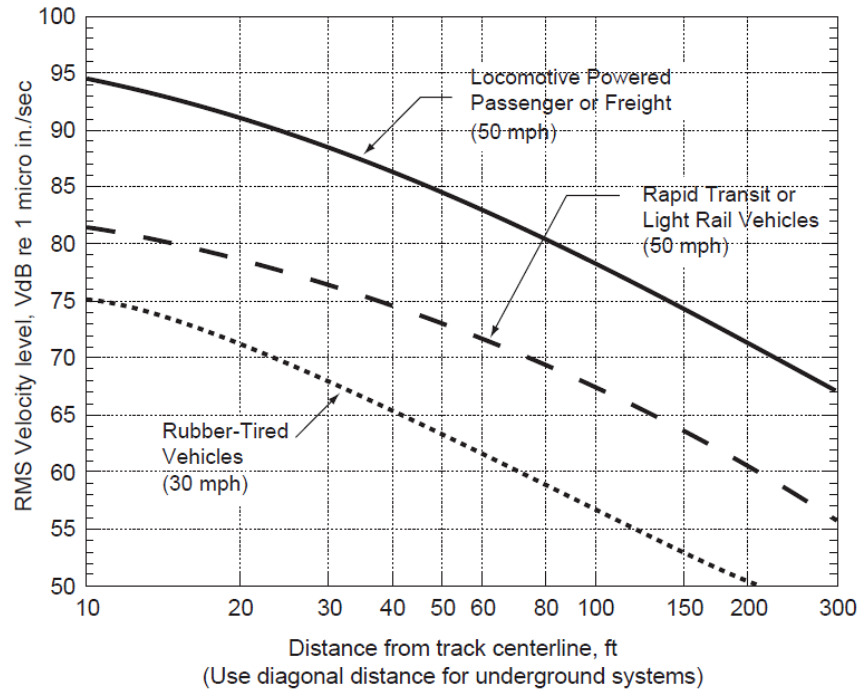
Potential vibration impacts of the trains were predicted using the Federal Transit Authority's (FTA) *Transit Noise and Vibration Impact Assessment*¹¹ protocol. The FTA general vibration assessment is based on an upper bound generic set of curves that show vibration level attenuation with distance. These curves, illustrated in the figure on the following page, are based on ground vibration measurements at various transit systems throughout North America. Vibration levels at points of reception are adjusted by various factors to incorporate known characteristics of the system being analyzed, such as operating speed of vehicle, conditions of the track, construction of the track and geology, as well as the structural type of the impacted building structures. The vibration impact on the building was determined using a set of curves for Rapid Transit at a speed of 50 mph. Adjustment factors were considered based on the following information:

- The maximum operating speed of the LRT is 31 mph (50 km/h) at peak.
- The offset distance between the development and the closest track is 24 m.
- The vehicles are assumed to have soft primary suspensions.
- Tracks are welded and in good condition.
- Soil conditions do not efficiently propagate vibrations.
- Type of transit structure is Open Cut.
- The building's foundation coupling is Foundation in Rock.

¹⁰ Dialog and J.E. Coulter Associates Limited, prepared for The Federation of Canadian Municipalities and The Railway Association of Canada, May 2013

¹¹ C. E. Hanson; D. A. Towers; and L. D. Meister, Transit Noise and Vibration Impact Assessment, Federal Transit Administration, May 2006





**FTA GENERALIZED CURVES OF VIBRATION LEVELS VERSUS DISTANCE
(ADOPTED FROM FIGURE 10-1, FTA TRANSIT NOISE AND VIBRATION IMPACT
ASSESSMENT)**

5. RESULTS AND DISCUSSION

5.1 Transportation Noise Levels

The results of the transportation noise calculations are summarized in Table 3 below. A complete set of input and output data from all STAMSON 5.04 calculations are available in Appendix A.

TABLE 3: EXTERIOR NOISE LEVELS DUE TO TRANSPORTATION SOURCES

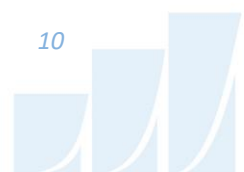
Receptor Number	Receptor Height Above Grade (m)	Receptor Location	STAMSON 5.04 Noise Level (dBA)	
			Day	Night
1	14.8	POW – 5 th Floor – South Façade	56	49
2	14.8	POW – 5 th Floor – East Façade	66	59
3	14.8	POW – 5 th Floor – North Façade	69	61
4	26.8	POW – 9 th Floor – East Façade	69	61
5	26.8	POW – 9 th Floor – South Façade	51	46
6	26.8	POW – 9 th Floor – West Façade	68	60
7	26.8	POW – 9 th Floor – North Façade	71	63
8	17.8	OLA – 6 th Floor Amenity Terrace	70	N/A*
9	29.8	OLA – Rooftop Terrace	68	N/A*

*Noise levels during the nighttime are not considered as per ENCG

The results of the current analysis indicate that noise levels will range between 51 and 71 dBA during the daytime period (07:00-23:00) and between 46 and 63 dBA during the nighttime period (23:00-07:00). The highest noise level (71 dBA) occurs at the north façade, which is most exposed to Highway 417.

5.2 Noise Control Measures

The noise levels predicted due to roadway traffic exceed the criteria listed in Section 4.2 for building components. As discussed in Section 4.3, the anticipated STC requirements for windows have been estimated based on the overall noise reduction required for each intended use of space (STC = outdoor noise level – targeted indoor noise levels). As per city of Ottawa requirements, detailed STC calculations will be required to be completed prior to building permit application for each unit type. The STC



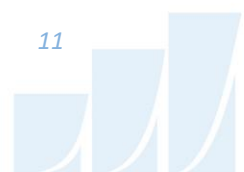
requirements for the windows are summarized below for various units within the development (see Figure 3):

- **Bedroom Windows**
 - (i) Bedroom windows facing east, north, and west will require a minimum STC of 34.
- **Living Room Windows**
 - (i) Living room windows facing east, north, and west will require a minimum STC of 29.
- **Exterior Walls**
 - (i) Exterior wall components on the east, north, and west façades will require a minimum STC of 45, which will be achieved with brick cladding or an acoustical equivalent according to NRC test data¹².

The STC requirements apply to windows, doors, spandrel panels and curtainwall elements. Exterior wall components on these façades are recommended to have a minimum STC of 45, where a window/wall system is used. A review of window supplier literature indicates that the specified STC ratings can be achieved by a variety of window systems having a combination of glass thickness and inter-pane spacing. We have specified an example window configuration, however several manufacturers and various combinations of window components, such as those proposed, will offer the necessary sound attenuation rating. It is the responsibility of the manufacturer to ensure that the specified window achieves the required STC. This can only be assured by using window configurations that have been certified by laboratory testing. The requirements for STC ratings assume that the remaining components of the building are constructed and installed according to the minimum standards of the Ontario Building Code. The specified STC requirements also apply to swinging and/or sliding patio doors.

Results of the calculations also indicate that the development will require central air conditioning, which will allow occupants to keep windows closed and maintain a comfortable living environment. In addition to ventilation requirements, Warning Clauses will also be required in all Lease, Purchase and Sale Agreements, as summarized in Section 6.

¹² J.S. Bradley and J.A. Birta. Laboratory Measurements of the Sound Insulation of Building Façade Elements, National Research Council October 2000.

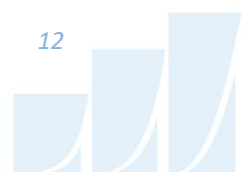


5.3 Noise Barrier Calculation

Noise levels at the Level 6 and rooftop terraces are expected to exceed 55 dBA during the daytime period without a noise barrier. If these areas are to be used as outdoor living areas, noise control measures are required to reduce noise levels as close as possible to 55 dBA where technically and administratively feasible. Further analysis investigated the noise mitigating impact of raising the perimeter guards from 1.2 m to 2.5 m above the walking surface (see Table 4). Results of the investigation proved that noise levels cannot easily be reduced to 55 dBA. It was determined that a noise barrier over 2.2 meters in height would be required to reduce noise levels to below 60 dBA at both receptors. However, the inclusion of a noise barrier greater than 1.5 meters in height would negatively impact the space architecturally by blocking views. Therefore, it is not feasible to protect the amenity terraces with a high noise barrier or other control measure. As mitigated noise levels are above 55 dBA, a Warning Clause is required.

TABLE 4: RESULTS OF NOISE BARRIER INVESTIGATION

Receptor Number	Receptor Height Above Grade (m)	Receptor Location	Daytime L_{eq} Noise Levels (dBA)					
			No Barrier	With 1.2 m Barrier	With 1.5 m Barrier	With 2 m Barrier	With 2.2 m Barrier	With 2.5 m Barrier
8	17.8	OLA – 6 th Floor Amenity Terrace	70	67	66	66	-	65
9	29.8	OLA – Rooftop Terrace	68	63	62	61	60	-



5.4 Ground Vibrations and Ground-Borne Noise Levels

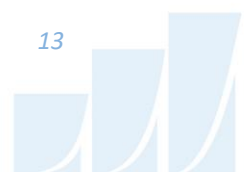
Estimated vibration levels at the foundation nearest to the O-Train LRT are expected to be 0.07mm/s RMS (69 dBV), based on the FTA protocol and an offset distance of 24 m to the nearest track centerline. Details of the calculation are provided in Appendix A. Since predicted vibration levels do not exceed the criterion of 0.10 mm/s RMS at the foundation, concerns due to vibration impacts on the site are not expected. As vibration levels are acceptable, correspondingly, regenerated noise levels are also expected to be acceptable.

6. CONCLUSIONS AND RECOMMENDATIONS

The results of the current analysis indicate that noise levels will range between 51 and 71 dBA during the daytime period (07:00-23:00) and between 46 and 63 dBA during the nighttime period (23:00-07:00). The highest noise level (71 dBA) occurs at the north façade, which is most exposed to Highway 417. Building components with a higher Sound Transmission Class (STC) rating will be required where exterior noise levels exceed 65 dBA, as indicated in Figure 3.

Results of the calculation also indicate the development will require central air conditioning, or similar mechanical ventilation, which will allow occupants to keep windows closed to maintain a comfortable indoor living environment. A Warning Clause will also be required to be placed on all Lease, Purchase and Sale Agreements, as summarized below:

“Purchasers/tenants are advised that despite the inclusion of noise control features in the development and within the building units, sound levels due to increasing roadway traffic may, on occasion, interfere with some activities of the dwelling occupants, as the sound levels exceed the sound level limits of the City and the Ministry of the Environment, Conservation and Parks. To help address the need for sound attenuation, this development includes:



- *STC rated multi-pane glazing elements*
- *STC rated exterior walls*
- *Acoustic barriers*

This dwelling unit has also been designed with air conditioning. Air conditioning will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the sound level limits of the City and the Ministry of the Environment, Conservation and Parks.

To ensure that provincial sound level limits are not exceeded, it is important to maintain these sound attenuation features.”

In addition, the Rail Construction Program Office recommends that the warning clause identified below to be included in all agreements of purchase and sale and lease agreements for the proposed development including those prepared prior to the registration of the Site Plan Agreement:

“The Owner hereby acknowledges and agrees:

- i) The proximity of the proposed development of the lands described in Schedule “A” hereto (the “Lands”) to the City’s existing and future transit operations, may result in noise, vibration, electromagnetic interferences, stray current transmissions, smoke and particulate matter (collectively referred to as “Interferences”) to the development;*
- ii) It has been advised by the City to apply reasonable attenuation measures with respect to the level of the Interferences on and within the Lands and the proposed development; and*
- iii) The Owner acknowledges and agrees all agreements of purchase and sale and lease agreements, and all information on all plans and documents used for marketing purposes, for the whole or any part of the subject lands, shall contain the following clauses which shall also be incorporated in all transfer/deeds and leases from the Owner so that the clauses shall be covenants running with the lands for the benefit of the owner of the adjacent road:*

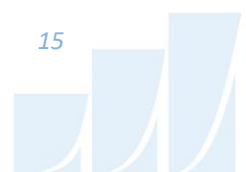


“The Transferee/Lessee for himself, his heirs, executors, administrators, successors and assigns acknowledges being advised that a public transit light-rail rapid transit system (LRT) is proposed to be located in proximity to the subject lands, and the construction, operation and maintenance of the LRT may result in environmental impacts including, but not limited to noise, vibration, electromagnetic interferences, stray current transmissions, smoke and particulate matter (collectively referred to as the Interferences) to the subject lands. The Transferee/Lessee acknowledges and agrees that despite the inclusion of noise control features within the subject lands, Interferences may continue to be of concern, occasionally interfering with some activities of the occupants on the subject lands.

The Transferee covenants with the Transferor and the Lessee covenants with the Lessor that the above clauses verbatim shall be included in all subsequent lease agreements, agreements of purchase and sale and deeds conveying the lands described herein, which covenants shall run with the lands and are for the benefit of the owner of the adjacent road.”

Noise levels at the Level 6 and rooftop terraces are expected to exceed 55 dBA during the daytime period without a noise barrier. If these areas are to be used as outdoor living areas, noise control measures are required to reduce noise levels as close as possible to 55 dBA where technically and administratively feasible. Further analysis investigated the noise mitigating impact of raising the perimeter guards from 1.2 m to 2.5 m above the walking surface (see Table 4). Results of the investigation proved that noise levels cannot easily be reduced to 55 dBA. It was determined that a noise barrier over 2.2 meters in height would be required to reduce noise levels to below 60 dBA at both receptors. However, the inclusion of a noise barrier/perimeter guard greater than 1.5 meters in height would negatively impact the space architecturally by blocking views. Therefore, it is not feasible to protect the amenity terraces with a high noise barrier or other control measure. As mitigated noise levels are above 55 dBA, a Warning Clause is required (see Figure 3).

The guard must be constructed from materials having a minimum surface density of 20 kg/m² (STC rating of 30) and contain no gaps. Design of the guardrail will conform to the requirements outlined in Part 5 of



the ENCG. The following information will be required by the City for review prior to installation of the barrier:

1. Shop drawings, signed and sealed by a qualified Professional Engineer licenced by the Professional Engineers of Ontario, showing the details of the acoustic barrier systems components, including material specifications.
2. Structural drawing(s), signed by a qualified Professional Engineer licenced by the Professional Engineers of Ontario, showing foundation details, and specifying design criteria, climatic design loads, as well as applicable geotechnical data used in the design.
3. Layout plan, and wall elevations, showing proposed colours and patterns.

Estimated vibration levels at the foundation nearest to the O-Train LRT are expected to be 0.07mm/s RMS (69 dBV), based on the FTA protocol and an offset distance of 24 m to the nearest track centerline. Details of the calculation are provided in Appendix A. Since predicted vibration levels do not exceed the criterion of 0.10 mm/s RMS at the foundation, concerns due to vibration impacts on the site are not expected. As vibration levels are acceptable, correspondingly, regenerated noise levels are also expected to be acceptable.

With regard to stationary noise impacts, a stationary noise study is recommended for the site during the detailed design once mechanical plans for the proposed building become available. The stationary noise study would assess impacts of stationary noise from rooftop mechanical units serving the proposed building on surrounding noise-sensitive areas. This study will include recommendations for any noise control measures that may be necessary to ensure noise levels fall below ENCG limits. Noise impacts can generally be minimized by judicious selection and placement of the equipment.

An initial assessment of the area identified several low-rise buildings in the immediate vicinity. As the development's mechanical equipment will primarily reside on the building's high roof in the mechanical penthouse, stationary noise impacts onto the surroundings are not expected to be a concern. Similarly, stationary noise impacts from existing buildings onto the proposed development are expected to be negligible as only a few nearby properties possess standard sized Rooftop Units (RTU) which are positioned several meters away from the development.



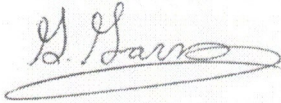
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This concludes our transportation noise and vibration assessment and report. If you have any questions or wish to discuss our findings, please advise us. In the interim, we thank you for the opportunity to be of service.

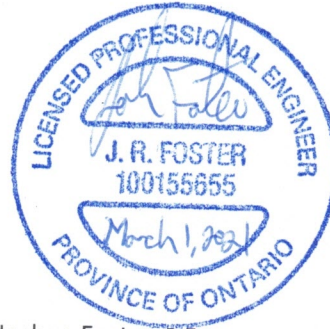
Sincerely,

Gradient Wind Engineering Inc.



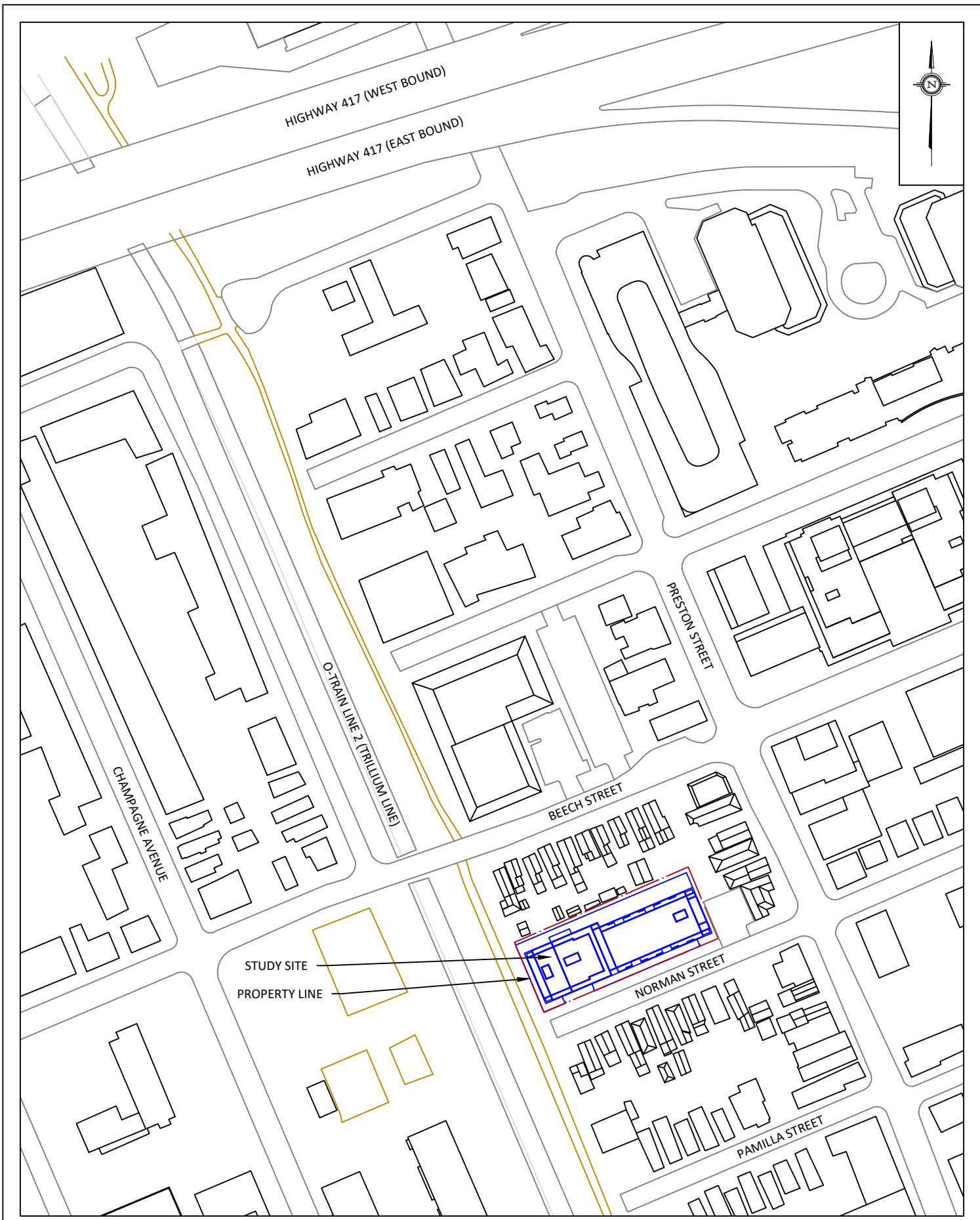
Giuseppe Garro, MASC.
Junior Environmental Scientist

Gradient Wind File #21-011-Transportation Noise and Vibration

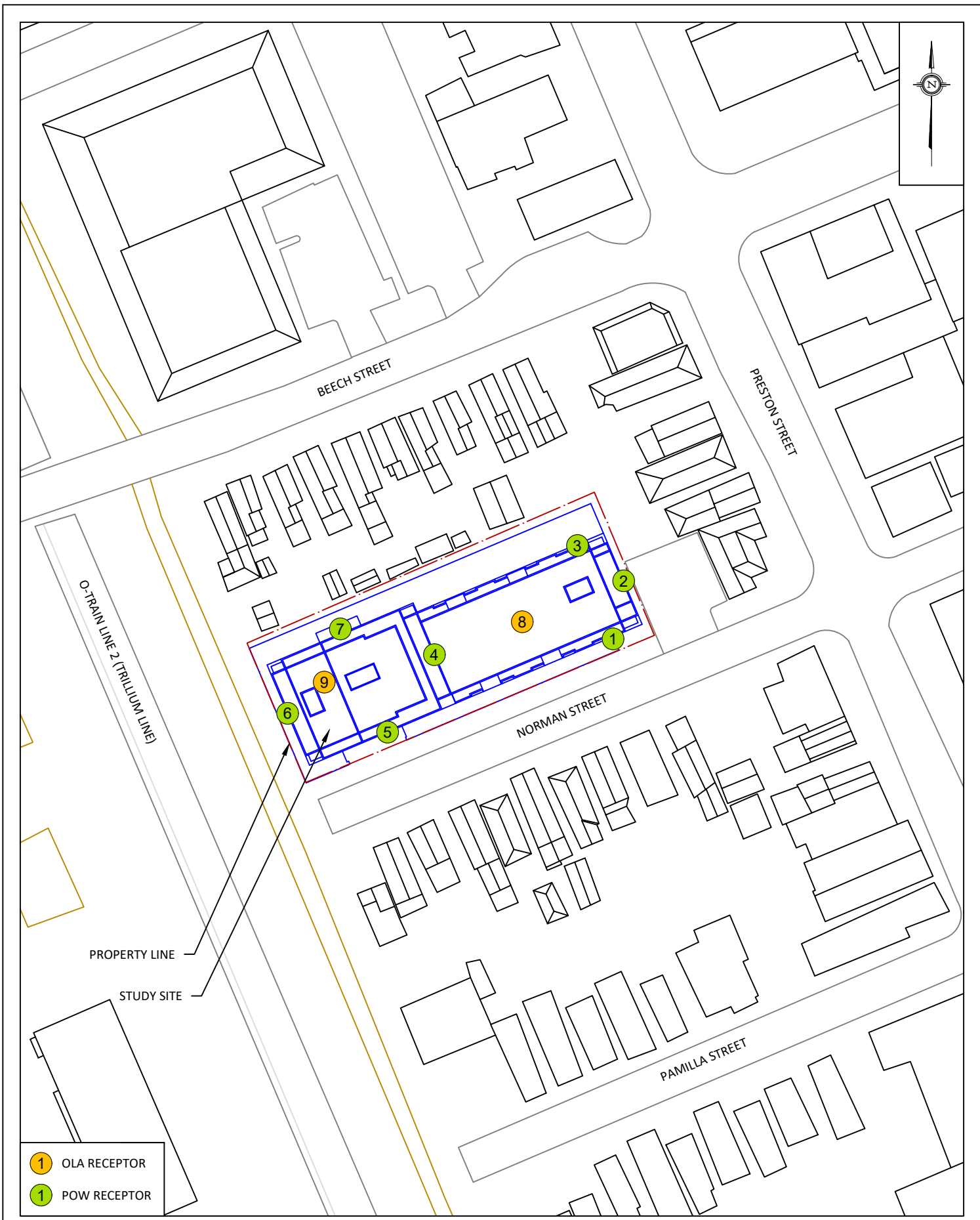


Joshua Foster, P.Eng.
Principal





GRADIENTWIND ENGINEERS & SCIENTISTS 127 WALGREEN ROAD, OTTAWA, ON 613 836 0934 • GRADIENTWIND.COM	PROJECT 93 NORMAN STREET, OTTAWA TRANSPORTATION NOISE ASSESSMENT		DESCRIPTION FIGURE 1: SITE PLAN AND SURROUNDING CONTEXT
	SCALE 1:2000 (APPROX.)	DRAWING NO. 21-011-1	
	DATE FEBRUARY 24, 2021	DRAWN BY O.R.	

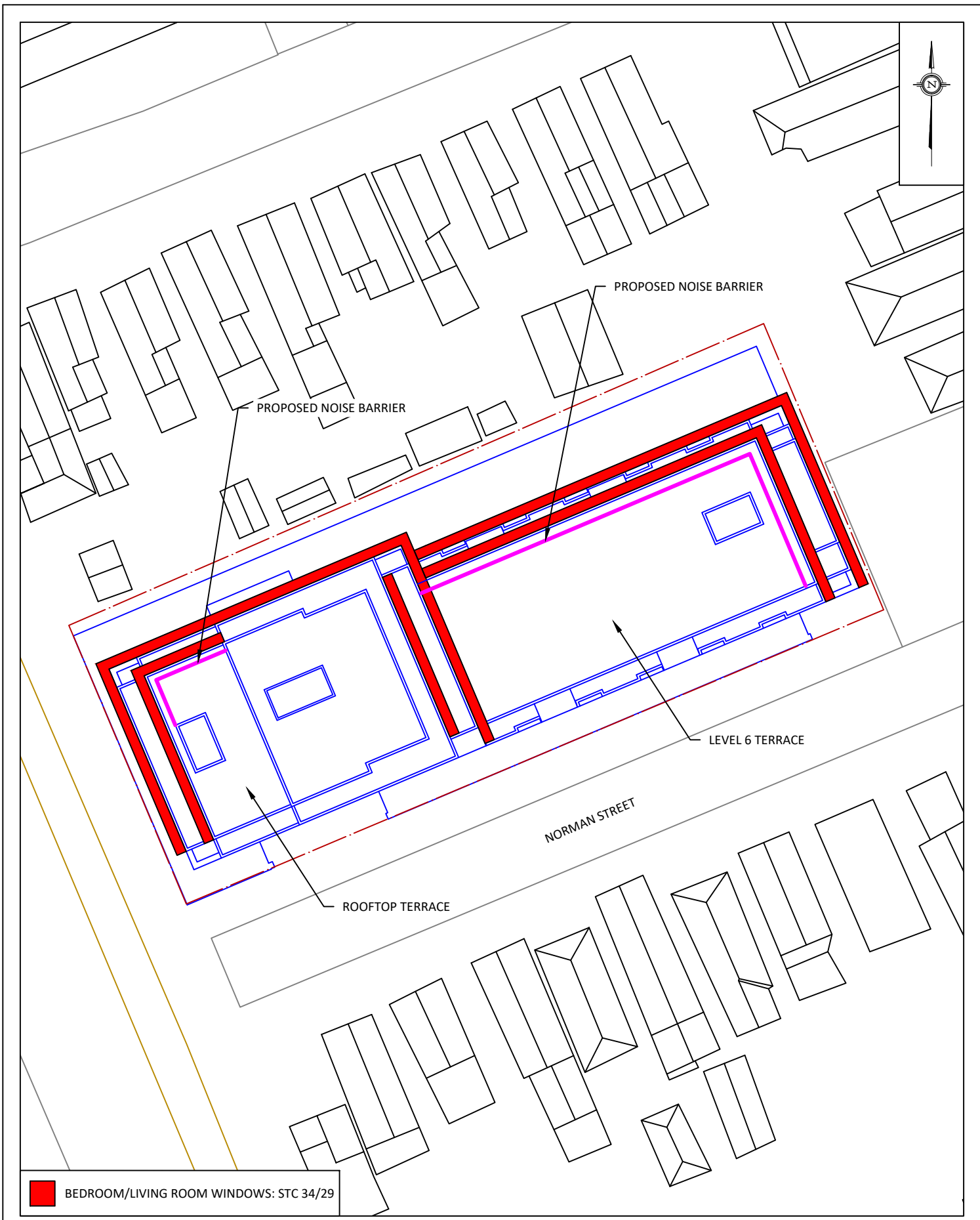


- 1 OLA RECEPTOR
- 1 POW RECEPTOR

PROPERTY LINE

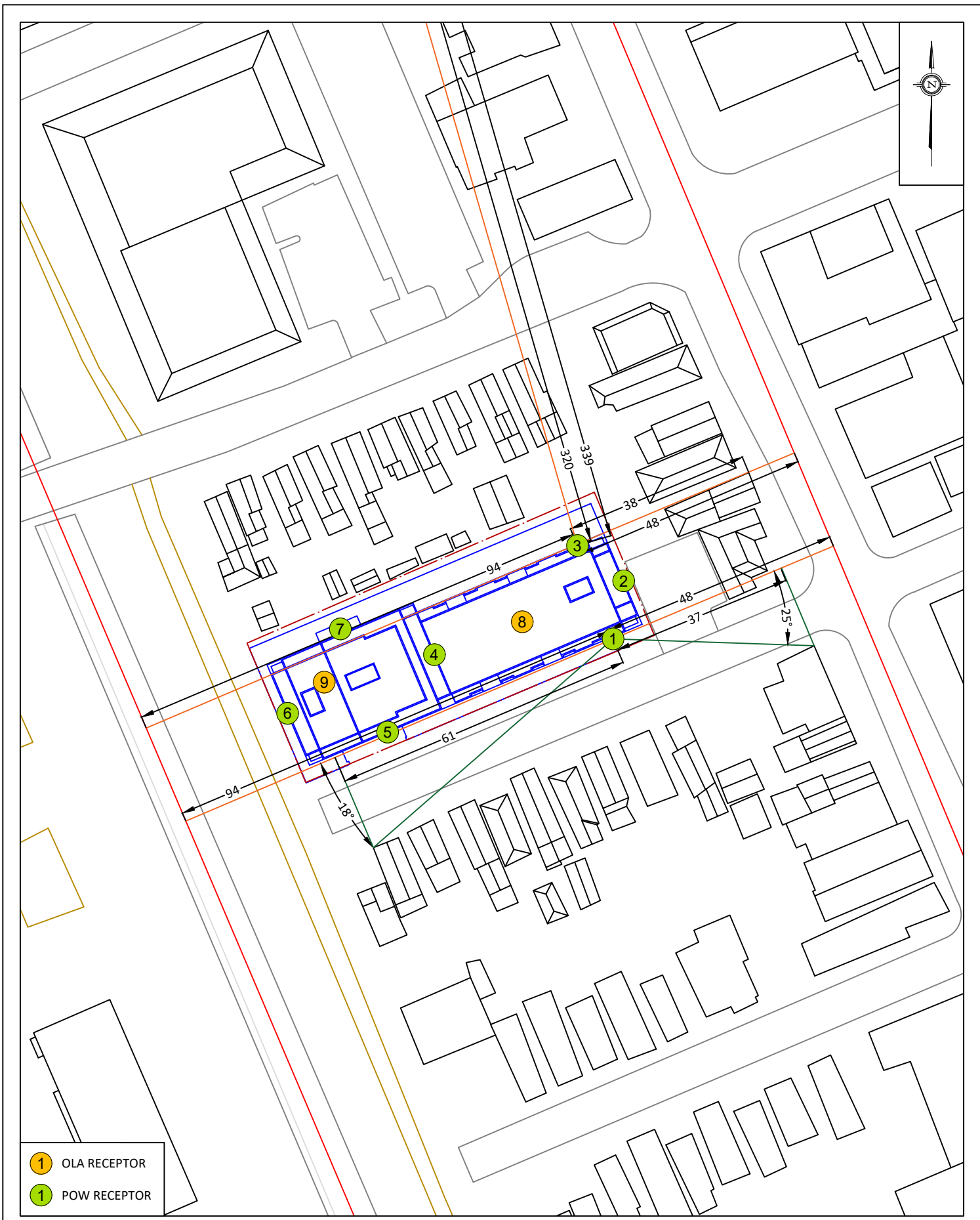
STUDY SITE

GRADIENTWIND ENGINEERS & SCIENTISTS 127 WALGREEN ROAD, OTTAWA, ON 613 836 0934 • GRADIENTWIND.COM	PROJECT 93 NORMAN STREET, OTTAWA TRANSPORTATION NOISE ASSESSMENT		DESCRIPTION FIGURE 2: RECEPTOR LOCATIONS
	SCALE 1:1000 (APPROX.)	DRAWING NO. 21-011-2	
	DATE FEBRUARY 24, 2021	DRAWN BY G.G.	



BEDROOM/LIVING ROOM WINDOWS: STC 34/29

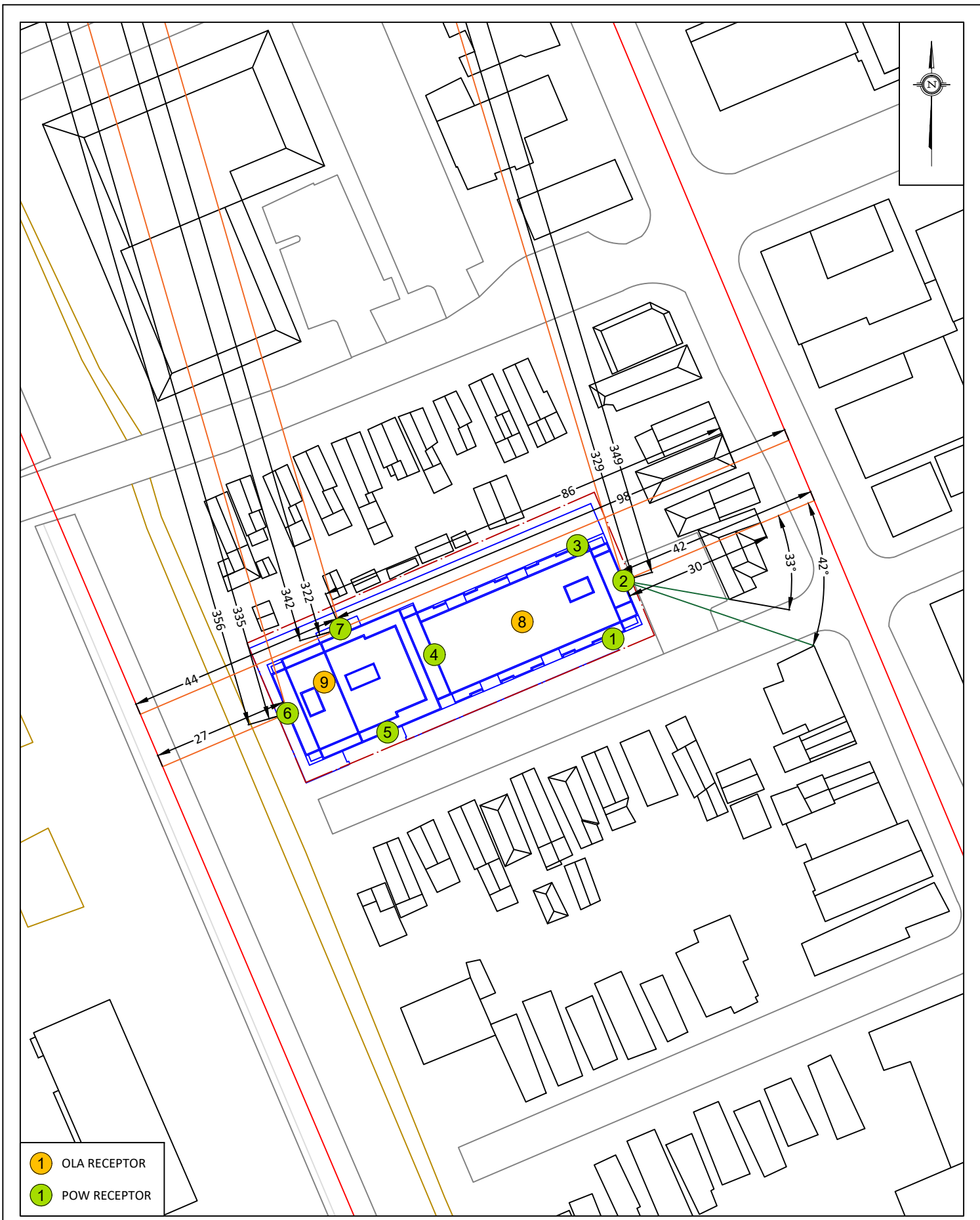
<p>GRADIENTWIND ENGINEERS & SCIENTISTS</p> <p>127 WALGREEN ROAD, OTTAWA, ON 613 836 0934 • GRADIENTWIND.COM</p>	<p>PROJECT: 93 NORMAN STREET, OTTAWA TRANSPORTATION NOISE ASSESSMENT</p>	<p>DESCRIPTION:</p> <p style="text-align: center;">FIGURE 3: WINDOW STC REQUIREMENTS</p>	
	<p>SCALE: 1:500 (APPROX.)</p>	<p>DRAWING NO.: 21-011-3</p>	
	<p>DATE: FEBRUARY 24, 2021</p>	<p>DRAWN BY: G.G.</p>	



- 1 OLA RECEPTOR
- 1 POW RECEPTOR

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	SCALE	1:1000 (APPROX.)	DRAWING NO.
	DATE	FEBRUARY 24, 2021	DRAWN BY

FIGURE 4:
RECEPTOR INPUT PARAMETERS



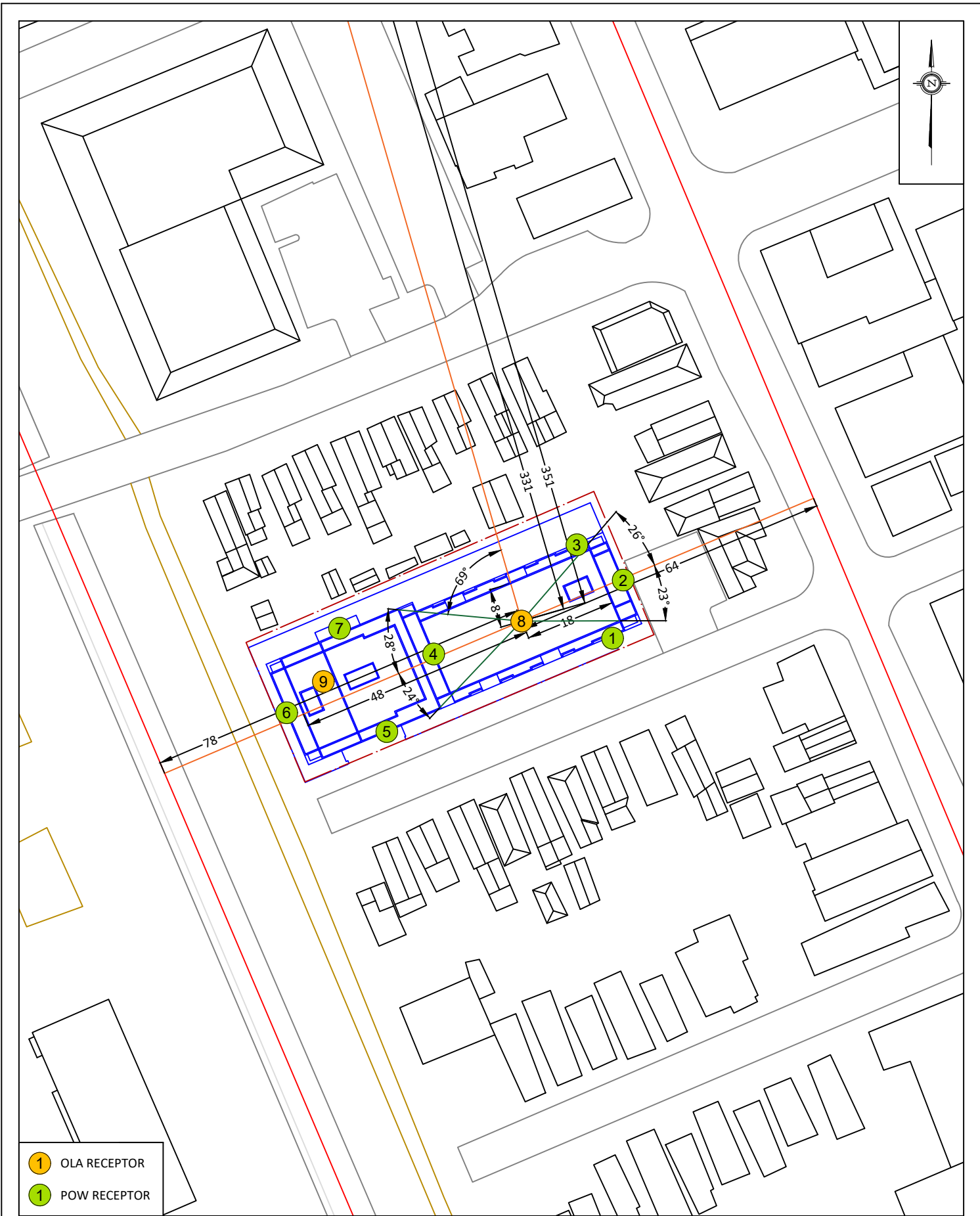
- 1 OLA RECEPTOR
- 1 POW RECEPTOR

GRADIENTWIND ENGINEERS & SCIENTISTS 127 WALGREEN ROAD, OTTAWA, ON 613 836 0934 • GRADIENTWIND.COM	PROJECT: 93 NORMAN STREET, OTTAWA TRANSPORTATION NOISE ASSESSMENT	DESCRIPTION:	
	SCALE: 1:1000 (APPROX.)	DRAWING NO.: 21-011-5	FIGURE 5: RECEPTOR INPUT PARAMETERS
	DATE: FEBRUARY 24, 2021	DRAWN BY: G.G.	



- 1 OLA RECEPTOR
- 1 POW RECEPTOR

GRADIENTWIND ENGINEERS & SCIENTISTS 127 WALGREEN ROAD, OTTAWA, ON 613 836 0934 • GRADIENTWIND.COM	PROJECT: 93 NORMAN STREET, OTTAWA TRANSPORTATION NOISE ASSESSMENT	DESCRIPTION:	
	SCALE: 1:1000 (APPROX.)	DRAWING NO.: 21-011-6	FIGURE 6: RECEPTOR INPUT PARAMETERS
	DATE: FEBRUARY 24, 2021	DRAWN BY: G.G.	



- 1 OLA RECEPTOR
- 1 POW RECEPTOR

GRADIENTWIND ENGINEERS & SCIENTISTS 127 WALGREEN ROAD, OTTAWA, ON 613 836 0934 • GRADIENTWIND.COM	PROJECT: 93 NORMAN STREET, OTTAWA TRANSPORTATION NOISE ASSESSMENT		DESCRIPTION: FIGURE 7: RECEPTOR INPUT PARAMETERS
	SCALE: 1:1000 (APPROX.)	DRAWING NO.: 21-011-7	
	DATE: FEBRUARY 24, 2021	DRAWN BY: G.G.	

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APPENDIX A

STAMSON 5.04 – INPUT AND OUTPUT DATA

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STAMSON 5.0 NORMAL REPORT Date: 23-02-2021 16:53:39
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r1.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: Preston St (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: Preston St (day/night)

Angle1 Angle2 : 0.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 48.00 / 48.00 m
Receiver height : 14.80 / 14.80 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : 25.00 deg Angle2 : 90.00 deg
Barrier height : 7.00 m
Barrier receiver distance : 37.00 / 37.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Results segment # 1: Preston St (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source ! Receiver ! Barrier ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)



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```

-----+-----+-----+-----
          1.50 !          14.80 !          4.54 !          4.54
ROAD (54.86 + 49.73 + 0.00) = 56.02 dBA
Angle1 Angle2  Alpha RefLeq  P.Adj  D.Adj  F.Adj  W.Adj  H.Adj  B.Adj
SubLeq
-----
--
    0    25    0.00  68.48    0.00  -5.05  -8.57    0.00    0.00    0.00
54.86
-----
--
    25    90    0.00  68.48    0.00  -5.05  -4.42    0.00    0.00   -9.28
49.73
-----
--

```

Segment Leq : 56.02 dBA

Total Leq All Segments: 56.02 dBA

Results segment # 1: Preston St (night)

Source height = 1.50 m

Barrier height for grazing incidence

```

-----+-----+-----+-----
Source      ! Receiver      ! Barrier      ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.50 !          14.80 !          4.54 !          4.54

```

```

ROAD (47.26 + 42.13 + 0.00) = 48.42 dBA
Angle1 Angle2  Alpha RefLeq  P.Adj  D.Adj  F.Adj  W.Adj  H.Adj  B.Adj
SubLeq
-----
--
    0    25    0.00  60.88    0.00  -5.05  -8.57    0.00    0.00    0.00
47.26
-----
--
    25    90    0.00  60.88    0.00  -5.05  -4.42    0.00    0.00   -9.28
42.13
-----
--

```

Segment Leq : 48.42 dBA

Total Leq All Segments: 48.42 dBA



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RT/Custom data, segment # 1: LRT (day/night)

 1 - 4-car SRT:
 Traffic volume : 192/24 veh/TimePeriod
 Speed : 50 km/h

Data for Segment # 1: LRT (day/night)

 Angle1 Angle2 : -90.00 deg 0.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 2 (Reflective ground surface)
 Receiver source distance : 94.00 / 94.00 m
 Receiver height : 14.80 / 14.80 m
 Topography : 3 (Elevated; no barrier)
 Elevation : 7.00 m
 Reference angle : 0.00

Results segment # 1: LRT (day)

 Source height = 0.50 m

RT/Custom (0.00 + 45.04 + 0.00) = 45.04 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	0	0.00	56.02	-7.97	-3.01	0.00	0.00	0.00	45.04

Segment Leq : 45.04 dBA

Total Leq All Segments: 45.04 dBA

Results segment # 1: LRT (night)

 Source height = 0.50 m

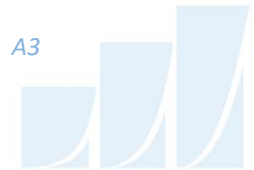
RT/Custom (0.00 + 39.02 + 0.00) = 39.02 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	0	0.00	50.00	-7.97	-3.01	0.00	0.00	0.00	39.02

Segment Leq : 39.02 dBA

Total Leq All Segments: 39.02 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 56.35
 (NIGHT): 48.89



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STAMSON 5.0 NORMAL REPORT Date: 23-02-2021 16:53:47
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r2.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: Preston St1 (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: Preston St1 (day/night)

Angle1 Angle2 : -90.00 deg 33.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 42.00 / 42.00 m
Receiver height : 14.80 / 14.80 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -90.00 deg Angle2 : 33.00 deg
Barrier height : 7.00 m
Barrier receiver distance : 30.00 / 30.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Road data, segment # 2: PRESTON ST2 (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)



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* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: PRESTON ST2 (day/night)

Angle1 Angle2 : 33.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 42.00 / 42.00 m
Receiver height : 14.80 / 14.80 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : 42.00 deg Angle2 : 90.00 deg
Barrier height : 7.00 m
Barrier receiver distance : 30.00 / 30.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Road data, segment # 3: HYW 417 EB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: HYW 417 EB (day/night)

Angle1 Angle2 : 0.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 329.00 / 329.00 m



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```
Receiver height      : 14.80 / 14.80 m
Topography          : 3          (Elevated; no barrier)
Elevation           : 4.00 m
Reference angle     : 0.00
```

Road data, segment # 4: HWY 417 WB (day/night)

```
-----
Car traffic volume  : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411  veh/TimePeriod *
Heavy truck volume  : 3373/293  veh/TimePeriod *
Posted speed limit  : 100 km/h
Road gradient       : 0 %
Road pavement       : 1 (Typical asphalt or concrete)
```

* Refers to calculated road volumes based on the following input:

```
24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth         : 0.00
Number of Years of Growth           : 0.00
Medium Truck % of Total Volume      : 7.00
Heavy Truck % of Total Volume       : 5.00
Day (16 hrs) % of Total Volume      : 92.00
```

Data for Segment # 4: HWY 417 WB (day/night)

```
-----
Angle1  Angle2      : 0.00 deg  90.00 deg
Wood depth      : 0          (No woods.)
No of house rows : 0 / 0
Surface         : 1          (Absorptive ground surface)
Receiver source distance : 349.00 / 349.00 m
Receiver height  : 14.80 / 14.80 m
Topography      : 3          (Elevated; no barrier)
Elevation       : 4.00 m
Reference angle  : 0.00
```

Results segment # 1: Preston St1 (day)

Source height = 1.50 m

Barrier height for grazing incidence

```
-----
Source      ! Receiver      ! Barrier      ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.50 !      14.80 !      5.30 !      5.30
```

ROAD (0.00 + 53.87 + 0.00) = 53.87 dBA

```
Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj
SubLeq
```



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```
-----
--
-90      33      0.00  68.48   0.00  -4.47  -1.65   0.00   0.00  -8.49
53.87
-----
--
```

Segment Leq : 53.87 dBA

Results segment # 2: PRESTON ST2 (day)

Source height = 1.50 m

Barrier height for grazing incidence

```
-----
Source      ! Receiver      ! Barrier      ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.50 !          14.80 !          5.30 !          5.30
-----
```

ROAD (51.00 + 51.10 + 0.00) = 54.06 dBA

```
Angle1 Angle2  Alpha RefLeq  P.Adj  D.Adj  F.Adj  W.Adj  H.Adj  B.Adj
SubLeq
-----
```

```
--
      33      42      0.00  68.48   0.00  -4.47 -13.01   0.00   0.00   0.00
51.00
-----
```

```
--
      42      90      0.00  68.48   0.00  -4.47  -5.74   0.00   0.00  -7.17
51.10
-----
```

```
--
```

Segment Leq : 54.06 dBA

Results segment # 3: HYW 417 EB (day)

Source height = 1.50 m

ROAD (0.00 + 62.69 + 0.00) = 62.69 dBA

```
Angle1 Angle2  Alpha RefLeq  P.Adj  D.Adj  F.Adj  W.Adj  H.Adj  B.Adj
SubLeq
-----
```

```
--
      0      90      0.14  81.40   0.00 -15.30  -3.40   0.00   0.00   0.00
62.69
-----
```

```
--
```



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Segment Leq : 62.69 dBA

Results segment # 4: HWY 417 WB (day)

Source height = 1.50 m

ROAD (0.00 + 62.40 + 0.00) = 62.40 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--									
0	90	0.14	81.40	0.00	-15.60	-3.40	0.00	0.00	0.00
62.40									

Segment Leq : 62.40 dBA

Total Leq All Segments: 66.12 dBA

Results segment # 1: Preston St1 (night)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	14.80	5.30	5.30

ROAD (0.00 + 46.27 + 0.00) = 46.27 dBA

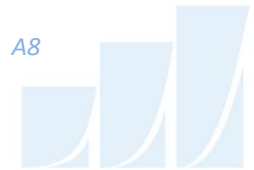
Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--									
-90	33	0.00	60.88	0.00	-4.47	-1.65	0.00	0.00	-8.49
46.27									

Segment Leq : 46.27 dBA

Results segment # 2: PRESTON ST2 (night)

Source height = 1.50 m



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Barrier height for grazing incidence

Source Height (m)	! Receiver Height (m)	! Barrier Height (m)	! Elevation of Barrier Top (m)
1.50	14.80	5.30	5.30

ROAD (43.40 + 43.50 + 0.00) = 46.46 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--	33	42	0.00	60.88	0.00	-4.47	-13.01	0.00	0.00	0.00
	43.40									

--	42	90	0.00	60.88	0.00	-4.47	-5.74	0.00	0.00	-7.17
	43.50									

Segment Leq : 46.46 dBA

Results segment # 3: HYW 417 EB (night)

Source height = 1.49 m

ROAD (0.00 + 55.09 + 0.00) = 55.09 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--	0	90	0.14	73.80	0.00	-15.30	-3.40	0.00	0.00	0.00
	55.09									

Segment Leq : 55.09 dBA

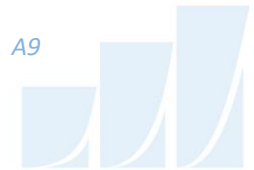
Results segment # 4: HWY 417 WB (night)

Source height = 1.49 m

ROAD (0.00 + 54.80 + 0.00) = 54.80 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--



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0 90 0.14 73.80 0.00 -15.60 -3.40 0.00 0.00 0.00
54.80

--

Segment Leq : 54.80 dBA

Total Leq All Segments: 58.52 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 66.12
(NIGHT): 58.52



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STAMSON 5.0 NORMAL REPORT Date: 23-02-2021 16:53:55
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r3.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: PRESTON ST (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

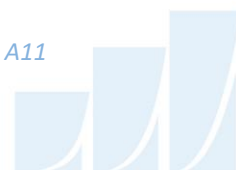
24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: PRESTON ST (day/night)

Angle1 Angle2 : -90.00 deg 0.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 48.00 / 48.00 m
Receiver height : 14.80 / 14.80 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -90.00 deg Angle2 : 0.00 deg
Barrier height : 7.00 m
Barrier receiver distance : 38.00 / 38.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Road data, segment # 2: HWY 417 EB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)



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* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: HWY 417 EB (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 320.00 / 320.00 m
Receiver height : 14.80 / 14.80 m
Topography : 3 (Elevated; no barrier)
Elevation : 4.00 m
Reference angle : 0.00

Road data, segment # 3: HWY 417 WB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: HWY 417 WB (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 339.00 / 339.00 m
Receiver height : 14.80 / 14.80 m
Topography : 3 (Elevated; no barrier)
Elevation : 4.00 m
Reference angle : 0.00



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Results segment # 1: PRESTON ST (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	14.80	4.27	4.27

ROAD (0.00 + 49.71 + 0.00) = 49.71 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	0	0.00	68.48	0.00	-5.05	-3.01	0.00	0.00	-10.71

SubLeq

--

-90 0 0.00 68.48 0.00 -5.05 -3.01 0.00 0.00 -10.71

49.71

--

Segment Leq : 49.71 dBA

Results segment # 2: HWY 417 EB (day)

Source height = 1.50 m

ROAD (0.00 + 65.84 + 0.00) = 65.84 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	90	0.14	81.40	0.00	-15.17	-0.39	0.00	0.00	0.00

SubLeq

--

-90 90 0.14 81.40 0.00 -15.17 -0.39 0.00 0.00 0.00

65.84

--

Segment Leq : 65.84 dBA

Results segment # 3: HWY 417 WB (day)

Source height = 1.50 m

ROAD (0.00 + 65.55 + 0.00) = 65.55 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	90	0.14	81.40	0.00	-15.17	-0.39	0.00	0.00	0.00

SubLeq

--



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```

-90      90      0.14  81.40   0.00 -15.45  -0.39   0.00   0.00   0.00
65.55
-----
--

```

Segment Leq : 65.55 dBA

Total Leq All Segments: 68.76 dBA

Results segment # 1: PRESTON ST (night)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	14.80	4.27	4.27

ROAD (0.00 + 42.11 + 0.00) = 42.11 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	0	0.00	60.88	0.00	-5.05	-3.01	0.00	0.00	-10.71

```

-90      0      0.00  60.88   0.00 -5.05  -3.01   0.00   0.00 -10.71
42.11
-----
--

```

Segment Leq : 42.11 dBA

Results segment # 2: HWY 417 EB (night)

Source height = 1.49 m

ROAD (0.00 + 58.24 + 0.00) = 58.24 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	90	0.14	73.80	0.00	-15.17	-0.39	0.00	0.00	0.00

```

-90      90      0.14  73.80   0.00 -15.17  -0.39   0.00   0.00   0.00
58.24
-----
--

```

Segment Leq : 58.24 dBA



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Results segment # 3: HWY 417 WB (night)

Source height = 1.49 m

ROAD (0.00 + 57.96 + 0.00) = 57.96 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
--------	--------	-------	--------	-------	-------	-------	-------	-------	-------	--------

-90	90	0.14	73.80	0.00	-15.45	-0.39	0.00	0.00	0.00	57.96
-----	----	------	-------	------	--------	-------	------	------	------	-------

Segment Leq : 57.96 dBA

Total Leq All Segments: 61.17 dBA

RT/Custom data, segment # 1: LRT (day/night)

1 - 4-car SRT:

Traffic volume	:	192/24	veh/TimePeriod
Speed	:	50 km/h	

Data for Segment # 1: LRT (day/night)

Angle1	Angle2	:	0.00 deg	90.00 deg
Wood depth	:	0	(No woods.)	
No of house rows	:	0 / 0		
Surface	:	2	(Reflective ground surface)	
Receiver source distance	:	94.00 / 94.00	m	
Receiver height	:	14.80 / 14.80	m	
Topography	:	3	(Elevated; no barrier)	
Elevation	:	7.00	m	
Reference angle	:	0.00		

Results segment # 1: LRT (day)

Source height = 0.50 m

RT/Custom (0.00 + 45.04 + 0.00) = 45.04 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	90	0.00	56.02	-7.97	-3.01	0.00	0.00	0.00	45.04

Segment Leq : 45.04 dBA

Total Leq All Segments: 45.04 dBA



Results segment # 1: LRT (night)

Source height = 0.50 m

RT/Custom (0.00 + 39.02 + 0.00) = 39.02 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	90	0.00	50.00	-7.97	-3.01	0.00	0.00	0.00	39.02

Segment Leq : 39.02 dBA

Total Leq All Segments: 39.02 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 68.78
(NIGHT): 61.19



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STAMSON 5.0 NORMAL REPORT Date: 23-02-2021 16:54:08
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r4.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: PRESTON ST (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: PRESTON ST (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 83.00 / 83.00 m
Receiver height : 26.80 / 26.80 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

Road data, segment # 2: HWY 417 EB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00



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Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: HWY 417 EB (day/night)

Angle1 Angle2 : 0.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 333.00 / 333.00 m
Receiver height : 26.80 / 26.80 m
Topography : 3 (Elevated; no barrier)
Elevation : 4.00 m
Reference angle : 0.00

Road data, segment # 3: HWY 417 WB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: HWY 417 WB (day/night)

Angle1 Angle2 : 0.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 353.00 / 353.00 m
Receiver height : 26.80 / 26.80 m
Topography : 3 (Elevated; no barrier)
Elevation : 4.00 m
Reference angle : 0.00

Results segment # 1: PRESTON ST (day)

Source height = 1.50 m

ROAD (0.00 + 61.05 + 0.00) = 61.05 dBA



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Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

```

-----
--
-90      90      0.00  68.48   0.00  -7.43   0.00   0.00   0.00   0.00
61.05
-----
--

```

Segment Leq : 61.05 dBA

Results segment # 2: HWY 417 EB (day)

Source height = 1.50 m

ROAD (0.00 + 64.92 + 0.00) = 64.92 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

```

-----
--
0        90      0.00  81.40   0.00 -13.46  -3.01   0.00   0.00   0.00
64.92
-----
--

```

Segment Leq : 64.92 dBA

Results segment # 3: HWY 417 WB (day)

Source height = 1.50 m

ROAD (0.00 + 64.67 + 0.00) = 64.67 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

```

-----
--
0        90      0.00  81.40   0.00 -13.72  -3.01   0.00   0.00   0.00
64.67
-----
--

```

Segment Leq : 64.67 dBA

Total Leq All Segments: 68.64 dBA



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Results segment # 1: PRESTON ST (night)

Source height = 1.50 m

ROAD (0.00 + 53.45 + 0.00) = 53.45 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

SubLeq

--									
-90	90	0.00	60.88	0.00	-7.43	0.00	0.00	0.00	0.00
53.45									

Segment Leq : 53.45 dBA

Results segment # 2: HWY 417 EB (night)

Source height = 1.49 m

ROAD (0.00 + 57.33 + 0.00) = 57.33 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

SubLeq

--									
0	90	0.00	73.80	0.00	-13.46	-3.01	0.00	0.00	0.00
57.33									

Segment Leq : 57.33 dBA

Results segment # 3: HWY 417 WB (night)

Source height = 1.49 m

ROAD (0.00 + 57.07 + 0.00) = 57.07 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

SubLeq

--									
0	90	0.00	73.80	0.00	-13.72	-3.01	0.00	0.00	0.00
57.07									

Segment Leq : 57.07 dBA

Total Leq All Segments: 61.04 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 68.64
(NIGHT): 61.04



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STAMSON 5.0 NORMAL REPORT Date: 23-02-2021 16:54:18
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r5.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: Preston St (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: Preston St (day/night)

Angle1 Angle2 : 0.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 97.00 / 97.00 m
Receiver height : 26.80 / 26.80 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : 11.00 deg Angle2 : 90.00 deg
Barrier height : 7.00 m
Barrier receiver distance : 86.00 / 86.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Results segment # 1: Preston St (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source ! Receiver ! Barrier ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)



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```

-----+-----+-----+-----
          1.50 !          26.80 !          4.36 !          4.36
ROAD (48.23 + 47.10 + 0.00) = 50.72 dBA
Angle1 Angle2  Alpha RefLeq  P.Adj  D.Adj  F.Adj  W.Adj  H.Adj  B.Adj
SubLeq
-----
--
    0    11    0.00  68.48    0.00  -8.11 -12.14    0.00    0.00    0.00
48.23
-----
--
    11    90    0.00  68.48    0.00  -8.11  -3.58    0.00    0.00   -9.69
47.10
-----
--

```

Segment Leq : 50.72 dBA

Total Leq All Segments: 50.72 dBA

Results segment # 1: Preston St (night)

Source height = 1.50 m

Barrier height for grazing incidence

```

-----+-----+-----+-----
Source      ! Receiver      ! Barrier      ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.50 !          26.80 !          4.36 !          4.36

```

```

ROAD (40.64 + 39.51 + 0.00) = 43.12 dBA
Angle1 Angle2  Alpha RefLeq  P.Adj  D.Adj  F.Adj  W.Adj  H.Adj  B.Adj
SubLeq
-----
--
    0    11    0.00  60.88    0.00  -8.11 -12.14    0.00    0.00    0.00
40.64
-----
--
    11    90    0.00  60.88    0.00  -8.11  -3.58    0.00    0.00   -9.69
39.51
-----
--

```

Segment Leq : 43.12 dBA

Total Leq All Segments: 43.12 dBA



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RT/Custom data, segment # 1: LRT (day/night)

 1 - 4-car SRT:
 Traffic volume : 192/24 veh/TimePeriod
 Speed : 50 km/h

Data for Segment # 1: LRT (day/night)

 Angle1 Angle2 : -90.00 deg 0.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 2 (Reflective ground surface)
 Receiver source distance : 44.00 / 44.00 m
 Receiver height : 26.80 / 26.80 m
 Topography : 3 (Elevated; no barrier)
 Elevation : 7.00 m
 Reference angle : 0.00

Results segment # 1: LRT (day)

 Source height = 0.50 m

RT/Custom (0.00 + 48.34 + 0.00) = 48.34 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	0	0.00	56.02	-4.67	-3.01	0.00	0.00	0.00	48.34

Segment Leq : 48.34 dBA

Total Leq All Segments: 48.34 dBA

Results segment # 1: LRT (night)

 Source height = 0.50 m

RT/Custom (0.00 + 42.32 + 0.00) = 42.32 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	0	0.00	50.00	-4.67	-3.01	0.00	0.00	0.00	42.32

Segment Leq : 42.32 dBA

Total Leq All Segments: 42.32 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 52.70
 (NIGHT): 45.75



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STAMSON 5.0 NORMAL REPORT Date: 23-02-2021 16:54:27
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r6.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: HWY 417 EB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: HWY 417 EB (day/night)

Angle1 Angle2 : -90.00 deg 0.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 335.00 / 335.00 m
Receiver height : 26.80 / 26.80 m
Topography : 3 (Elevated; no barrier)
Elevation : 4.00 m
Reference angle : 0.00

Road data, segment # 2: HWY 417 WB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00



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Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: HWY 417 WB (day/night)

```
-----
Angle1 Angle2 : -90.00 deg 0.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 356.00 / 356.00 m
Receiver height : 26.80 / 26.80 m
Topography : 3 (Elevated; no barrier)
Elevation : 4.00 m
Reference angle : 0.00
-----
```

Results segment # 1: HWY 417 EB (day)

Source height = 1.50 m

ROAD (0.00 + 64.90 + 0.00) = 64.90 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	0	0.00	81.40	0.00	-13.49	-3.01	0.00	0.00	0.00

```
-----
--
64.90
-----
--
```

Segment Leq : 64.90 dBA

Results segment # 2: HWY 417 WB (day)

Source height = 1.50 m

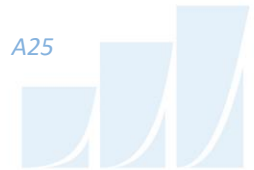
ROAD (0.00 + 64.63 + 0.00) = 64.63 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	0	0.00	81.40	0.00	-13.75	-3.01	0.00	0.00	0.00

```
-----
--
64.63
-----
--
```

Segment Leq : 64.63 dBA

Total Leq All Segments: 67.78 dBA



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Results segment # 1: HWY 417 EB (night)

Source height = 1.49 m

ROAD (0.00 + 57.30 + 0.00) = 57.30 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

SubLeq

-90	0	0.00	73.80	0.00	-13.49	-3.01	0.00	0.00	0.00
-----	---	------	-------	------	--------	-------	------	------	------

57.30

Segment Leq : 57.30 dBA

Results segment # 2: HWY 417 WB (night)

Source height = 1.49 m

ROAD (0.00 + 57.04 + 0.00) = 57.04 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

SubLeq

-90	0	0.00	73.80	0.00	-13.75	-3.01	0.00	0.00	0.00
-----	---	------	-------	------	--------	-------	------	------	------

57.04

Segment Leq : 57.04 dBA

Total Leq All Segments: 60.18 dBA

RT/Custom data, segment # 1: LRT (day/night)

1 - 4-car SRT:

Traffic volume : 192/24 veh/TimePeriod
Speed : 50 km/h

Data for Segment # 1: LRT (day/night)

Angle1	Angle2	:	-90.00 deg	90.00 deg
Wood depth	:	0	(No woods.)	
No of house rows	:	0 / 0		
Surface	:	2	(Reflective ground surface)	
Receiver source distance	:	27.00 / 27.00	m	
Receiver height	:	26.80 / 26.80	m	
Topography	:	3	(Elevated; no barrier)	



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Elevation : 7.00 m
 Reference angle : 0.00

Results segment # 1: LRT (day)

 Source height = 0.50 m

RT/Custom (0.00 + 53.47 + 0.00) = 53.47 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	90	0.00	56.02	-2.55	0.00	0.00	0.00	0.00	53.47

 Segment Leq : 53.47 dBA

Total Leq All Segments: 53.47 dBA

Results segment # 1: LRT (night)

 Source height = 0.50 m

RT/Custom (0.00 + 47.45 + 0.00) = 47.45 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	90	0.00	50.00	-2.55	0.00	0.00	0.00	0.00	47.45

 Segment Leq : 47.45 dBA

Total Leq All Segments: 47.45 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 67.94
 (NIGHT): 60.41



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STAMSON 5.0 NORMAL REPORT Date: 23-02-2021 16:54:40
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r7.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: PRESTON ST (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: PRESTON ST (day/night)

Angle1 Angle2 : -90.00 deg 0.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 98.00 / 98.00 m
Receiver height : 26.80 / 26.80 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -90.00 deg Angle2 : 0.00 deg
Barrier height : 7.00 m
Barrier receiver distance : 86.00 / 86.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Road data, segment # 2: HWY 417 EB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)



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* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: HWY 417 EB (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 322.00 / 322.00 m
Receiver height : 26.80 / 26.80 m
Topography : 3 (Elevated; no barrier)
Elevation : 4.00 m
Reference angle : 0.00

Road data, segment # 3: HWY 417 WB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: HWY 417 WB (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 342.00 / 342.00 m
Receiver height : 26.80 / 26.80 m
Topography : 3 (Elevated; no barrier)
Elevation : 4.00 m
Reference angle : 0.00



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Results segment # 1: PRESTON ST (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	26.80	4.59	4.59

ROAD (0.00 + 48.00 + 0.00) = 48.00 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	0	0.00	68.48	0.00	-8.15	-3.01	0.00	0.00	-9.31

SubLeq
48.00

Segment Leq : 48.00 dBA

Results segment # 2: HWY 417 EB (day)

Source height = 1.50 m

ROAD (0.00 + 68.08 + 0.00) = 68.08 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	90	0.00	81.40	0.00	-13.32	0.00	0.00	0.00	0.00

SubLeq
68.08

Segment Leq : 68.08 dBA

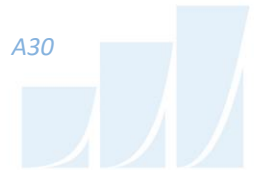
Results segment # 3: HWY 417 WB (day)

Source height = 1.50 m

ROAD (0.00 + 67.82 + 0.00) = 67.82 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	90	0.00	81.40	0.00	-13.32	0.00	0.00	0.00	0.00

SubLeq



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```

-90      90      0.00  81.40   0.00 -13.58   0.00   0.00   0.00   0.00
67.82
-----
--

```

Segment Leq : 67.82 dBA

Total Leq All Segments: 70.98 dBA

Results segment # 1: PRESTON ST (night)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	! Receiver ! Height (m)	! Barrier ! Height (m)	! Elevation of ! Barrier Top (m)
1.50	!	26.80	!
		4.59	!
			4.59

ROAD (0.00 + 40.41 + 0.00) = 40.41 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

```

--
-90      0      0.00  60.88   0.00 -8.15  -3.01   0.00   0.00  -9.31
40.41
-----
--

```

Segment Leq : 40.41 dBA

Results segment # 2: HWY 417 EB (night)

Source height = 1.49 m

ROAD (0.00 + 60.48 + 0.00) = 60.48 dBA

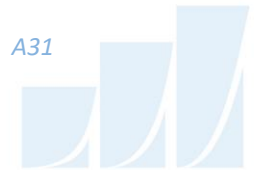
Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

```

--
-90      90      0.00  73.80   0.00 -13.32   0.00   0.00   0.00   0.00
60.48
-----
--

```

Segment Leq : 60.48 dBA



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Results segment # 3: HWY 417 WB (night)

Source height = 1.49 m

ROAD (0.00 + 60.22 + 0.00) = 60.22 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
--------	--------	-------	--------	-------	-------	-------	-------	-------	-------	--------

--										
-90	90	0.00	73.80	0.00	-13.58	0.00	0.00	0.00	0.00	60.22

Segment Leq : 60.22 dBA

Total Leq All Segments: 63.38 dBA

RT/Custom data, segment # 1: LRT (day/night)

1 - 4-car SRT:

Traffic volume	:	192/24	veh/TimePeriod
Speed	:	50 km/h	

Data for Segment # 1: LRT (day/night)

Angle1	Angle2	:	0.00 deg	90.00 deg
Wood depth	:	0	(No woods.)	
No of house rows	:	0 / 0		
Surface	:	2	(Reflective ground surface)	
Receiver source distance	:	44.00 / 44.00	m	
Receiver height	:	26.80 / 26.80	m	
Topography	:	3	(Elevated; no barrier)	
Elevation	:	7.00	m	
Reference angle	:	0.00		

Results segment # 1: LRT (day)

Source height = 0.50 m

RT/Custom (0.00 + 48.34 + 0.00) = 48.34 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	90	0.00	56.02	-4.67	-3.01	0.00	0.00	0.00	48.34

Segment Leq : 48.34 dBA

Total Leq All Segments: 48.34 dBA



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Results segment # 1: LRT (night)

Source height = 0.50 m

RT/Custom (0.00 + 42.32 + 0.00) = 42.32 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	90	0.00	50.00	-4.67	-3.01	0.00	0.00	0.00	42.32

Segment Leq : 42.32 dBA

Total Leq All Segments: 42.32 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 71.01
(NIGHT): 63.42



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STAMSON 5.0 NORMAL REPORT Date: 23-02-2021 16:54:48
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r8.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: PRESTON ST (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: PRESTON ST (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 64.00 / 64.00 m
Receiver height : 17.80 / 17.80 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -26.00 deg Angle2 : 23.00 deg
Barrier height : 16.30 m
Barrier receiver distance : 18.00 / 18.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Road data, segment # 2: HWY 417 EB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)



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* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: HWY 417 EB (day/night)

Angle1 Angle2 : -69.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 331.00 / 331.00 m
Receiver height : 17.80 / 17.80 m
Topography : 4 (Elevated; with barrier)
Barrier angle1 : -69.00 deg Angle2 : 90.00 deg
Barrier height : 16.30 m
Elevation : 4.00 m
Barrier receiver distance : 8.00 / 8.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Road data, segment # 3: HWY 417 WB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: HWY 417 WB (day/night)

Angle1 Angle2 : -69.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)



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Receiver source distance : 351.00 / 351.00 m
Receiver height          : 17.80 / 17.80 m
Topography               : 4 (Elevated; with barrier)
Barrier angle1           : -69.00 deg Angle2 : 90.00 deg
Barrier height           : 16.30 m
Elevation                : 4.00 m
Barrier receiver distance : 8.00 / 8.00 m
Source elevation         : 0.00 m
Receiver elevation       : 0.00 m
Barrier elevation        : 0.00 m
Reference angle          : 0.00
    
```

Results segment # 1: PRESTON ST (day)

Source height = 1.50 m

Barrier height for grazing incidence

```

-----
Source      ! Receiver      ! Barrier      ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.50 !          17.80 !          13.21 !          13.21
    
```

ROAD (57.69 + 43.57 + 57.89) = 60.88 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

```

-----
--
-90    -26    0.00  68.48    0.00  -6.30  -4.49    0.00    0.00    0.00
57.69
    
```

```

-----
--
-26    23     0.00  68.48    0.00  -6.30  -5.65    0.00    0.00  -12.95
43.57
    
```

```

-----
--
 23    90     0.00  68.48    0.00  -6.30  -4.29    0.00    0.00    0.00
57.89
    
```

Segment Leq : 60.88 dBA

Results segment # 2: HWY 417 EB (day)

Source height = 1.50 m

Barrier height for grazing incidence



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Source Height (m)	! Receiver ! Height (m)	! Barrier ! Height (m)	! Elevation of ! Barrier Top (m)
1.50	!	17.80	!
		17.41	!
			17.41

ROAD (0.00 + 66.62 + 0.00) = 66.62 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--	-69	90	0.00	81.40	0.00	-13.44	-0.54	0.00	0.00	-1.09
66.33*	-69	90	0.05	81.40	0.00	-14.12	-0.65	0.00	0.00	0.00
66.62										

* Bright Zone !

Segment Leq : 66.62 dBA

Results segment # 3: HWY 417 WB (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	! Receiver ! Height (m)	! Barrier ! Height (m)	! Elevation of ! Barrier Top (m)
1.50	!	17.80	!
		17.43	!
			17.43

ROAD (0.00 + 66.35 + 0.00) = 66.35 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--	-69	90	0.00	81.40	0.00	-13.69	-0.54	0.00	0.00	-1.01
66.16*	-69	90	0.05	81.40	0.00	-14.39	-0.65	0.00	0.00	0.00
66.35										

* Bright Zone !

Segment Leq : 66.35 dBA

Total Leq All Segments: 70.06 dBA



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Results segment # 1: PRESTON ST (night)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	17.80	13.21	13.21

ROAD (50.09 + 35.98 + 50.29) = 53.28 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

-90	-26	0.00	60.88	0.00	-6.30	-4.49	0.00	0.00	0.00
50.09									

-26	23	0.00	60.88	0.00	-6.30	-5.65	0.00	0.00	-12.95
35.98									

23	90	0.00	60.88	0.00	-6.30	-4.29	0.00	0.00	0.00
50.29									

Segment Leq : 53.28 dBA

Results segment # 2: HWY 417 EB (night)

Source height = 1.49 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.49	17.80	17.41	17.41

ROAD (0.00 + 59.02 + 0.00) = 59.02 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

-69	90	0.00	73.80	0.00	-13.44	-0.54	0.00	0.00	-1.09
58.73*									



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-69 90 0.05 73.80 0.00 -14.12 -0.65 0.00 0.00 0.00
59.02

--

* Bright Zone !

Segment Leq : 59.02 dBA

Results segment # 3: HWY 417 WB (night)

Source height = 1.49 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.49	17.80	17.43	17.43

ROAD (0.00 + 58.76 + 0.00) = 58.76 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--

-69 90 0.00 73.80 0.00 -13.69 -0.54 0.00 0.00 -1.01
58.56*
-69 90 0.05 73.80 0.00 -14.39 -0.65 0.00 0.00 0.00
58.76

--

* Bright Zone !

Segment Leq : 58.76 dBA

Total Leq All Segments: 62.46 dBA

RT/Custom data, segment # 1: LRT 1 (day/night)

1 - 4-car SRT:
Traffic volume : 192/24 veh/TimePeriod
Speed : 50 km/h

Data for Segment # 1: LRT 1 (day/night)

Angle1	Angle2	: -90.00 deg	0.00 deg
Wood depth		: 0	(No woods.)
No of house rows		: 0 / 0	
Surface		: 2	(Reflective ground surface)



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Receiver source distance : 78.00 / 78.00 m
Receiver height          : 17.80 / 17.80 m
Topography               : 4           (Elevated; with barrier)
Barrier angle1           : -24.00 deg   Angle2 : 0.00 deg
Barrier height           : 28.30 m
Elevation                : 7.00 m
Barrier receiver distance : 48.00 / 48.00 m
Source elevation         : 0.00 m
Receiver elevation       : 0.00 m
Barrier elevation        : 0.00 m
Reference angle          : 0.00
  
```

RT/Custom data, segment # 2: LRT 2 (day/night)

```

-----
1 - 4-car SRT:
Traffic volume      : 192/24   veh/TimePeriod
Speed               : 50 km/h
  
```

Data for Segment # 2: LRT 2 (day/night)

```

-----
Angle1  Angle2      : 0.00 deg   90.00 deg
Wood depth      : 0           (No woods.)
No of house rows : 0 / 0
Surface         : 2           (Reflective ground surface)
Receiver source distance : 78.00 / 78.00 m
Receiver height  : 17.80 / 17.80 m
Topography      : 4           (Elevated; with barrier)
Barrier angle1  : 0.00 deg   Angle2 : 28.00 deg
Barrier height   : 28.30 m
Elevation       : 7.00 m
Barrier receiver distance : 48.00 / 48.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle  : 0.00
  
```

Results segment # 1: LRT 1 (day)

Source height = 0.50 m

Barrier height for grazing incidence

```

-----
Source      ! Receiver      ! Barrier      ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          0.50 !      17.80 !      7.15 !      7.15
  
```

RT/Custom (44.51 + 20.11 + 0.00) = 44.52 dBA

```

Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq
-----
  
```



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-90	-24	0.00	56.02	-7.16	-4.36	0.00	0.00	0.00	44.51
-24	0	0.00	56.02	-7.16	-8.75	0.00	0.00	-20.00	20.11

Segment Leq : 44.52 dBA

Results segment # 2: LRT 2 (day)

Source height = 0.50 m

Barrier height for grazing incidence

Source Height (m)	! Receiver Height (m)	! Barrier Height (m)	! Elevation of Barrier Top (m)
0.50	!	17.80	!
		7.15	!
			7.15

RT/Custom (0.00 + 20.78 + 44.24) = 44.25 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	28	0.00	56.02	-7.16	-8.08	0.00	0.00	-20.00	20.78
28	90	0.00	56.02	-7.16	-4.63	0.00	0.00	0.00	44.24

Segment Leq : 44.25 dBA

Total Leq All Segments: 47.40 dBA

Results segment # 1: LRT 1 (night)

Source height = 0.50 m

Barrier height for grazing incidence

Source Height (m)	! Receiver Height (m)	! Barrier Height (m)	! Elevation of Barrier Top (m)
0.50	!	17.80	!
		7.15	!
			7.15

RT/Custom (38.49 + 14.09 + 0.00) = 38.50 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	-24	0.00	50.00	-7.16	-4.36	0.00	0.00	0.00	38.49
-24	0	0.00	50.00	-7.16	-8.75	0.00	0.00	-20.00	14.09



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Segment Leq : 38.50 dBA

Results segment # 2: LRT 2 (night)

Source height = 0.50 m

Barrier height for grazing incidence

Source Height (m)	! Receiver ! Height (m)	! Barrier ! Height (m)	! Elevation of ! Barrier Top (m)
0.50	!	17.80	!
		7.15	!
			7.15

RT/Custom (0.00 + 14.76 + 38.21) = 38.23 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	28	0.00	50.00	-7.16	-8.08	0.00	0.00	-20.00	14.76
28	90	0.00	50.00	-7.16	-4.63	0.00	0.00	0.00	38.21

Segment Leq : 38.23 dBA

Total Leq All Segments: 41.38 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 70.08
(NIGHT): 62.49



GRADIENTWIND

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STAMSON 5.0 NORMAL REPORT Date: 23-02-2021 16:54:57
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r8bl.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: PRESTON ST (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: PRESTON ST (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 64.00 / 64.00 m
Receiver height : 17.80 / 17.80 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -26.00 deg Angle2 : 23.00 deg
Barrier height : 17.50 m
Barrier receiver distance : 18.00 / 18.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Road data, segment # 2: HWY 417 EB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)



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* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: HWY 417 EB (day/night)

Angle1 Angle2 : -69.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 331.00 / 331.00 m
Receiver height : 17.80 / 17.80 m
Topography : 4 (Elevated; with barrier)
Barrier angle1 : -69.00 deg Angle2 : 90.00 deg
Barrier height : 17.50 m
Elevation : 4.00 m
Barrier receiver distance : 8.00 / 8.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Road data, segment # 3: HWY 417 WB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: HWY 417 WB (day/night)

Angle1 Angle2 : -69.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)



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```

Receiver source distance : 351.00 / 351.00 m
Receiver height          : 17.80 / 17.80 m
Topography               : 4 (Elevated; with barrier)
Barrier angle1          : -69.00 deg Angle2 : 90.00 deg
Barrier height          : 17.50 m
Elevation               : 4.00 m
Barrier receiver distance : 8.00 / 8.00 m
Source elevation        : 0.00 m
Receiver elevation      : 0.00 m
Barrier elevation       : 0.00 m
Reference angle         : 0.00
    
```

Results segment # 1: PRESTON ST (day)

Source height = 1.50 m

Barrier height for grazing incidence

```

-----
Source      ! Receiver      ! Barrier      ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.50 !          17.80 !          13.21 !          13.21
    
```

ROAD (57.69 + 40.81 + 57.89) = 60.84 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

```

-----
--
-90   -26   0.00  68.48   0.00  -6.30  -4.49   0.00   0.00   0.00
57.69
    
```

```

-----
--
-26   23   0.00  68.48   0.00  -6.30  -5.65   0.00   0.00 -15.72
40.81
    
```

```

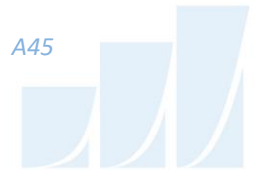
-----
--
 23   90   0.00  68.48   0.00  -6.30  -4.29   0.00   0.00   0.00
57.89
    
```

Segment Leq : 60.84 dBA

Results segment # 2: HWY 417 EB (day)

Source height = 1.50 m

Barrier height for grazing incidence



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Source Height (m)	! Receiver ! Height (m)	! Barrier ! Height (m)	! Elevation of ! Barrier Top (m)
1.50	! 17.80	! 17.41	! 17.41

ROAD (0.00 + 62.40 + 0.00) = 62.40 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--	-69	90	0.00	81.40	0.00	-13.44	-0.54	0.00	0.00	-5.02
62.40										

Segment Leq : 62.40 dBA

Results segment # 3: HWY 417 WB (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	! Receiver ! Height (m)	! Barrier ! Height (m)	! Elevation of ! Barrier Top (m)
1.50	! 17.80	! 17.43	! 17.43

ROAD (0.00 + 62.15 + 0.00) = 62.15 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--	-69	90	0.00	81.40	0.00	-13.69	-0.54	0.00	0.00	-5.01
62.15										

Segment Leq : 62.15 dBA

Total Leq All Segments: 66.62 dBA

Results segment # 1: PRESTON ST (night)

Source height = 1.50 m

Barrier height for grazing incidence

Source	! Receiver	! Barrier	! Elevation of
--------	------------	-----------	----------------



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```

Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.50 !          17.80 !          13.21 !          13.21
  
```

ROAD (50.09 + 33.21 + 50.29) = 53.25 dBA

```

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj
SubLeq
-----
  
```

```

--
-90    -26    0.00  60.88    0.00  -6.30  -4.49    0.00    0.00    0.00
50.09
-----
  
```

```

--
-26    23     0.00  60.88    0.00  -6.30  -5.65    0.00    0.00  -15.72
33.21
-----
  
```

```

--
 23    90     0.00  60.88    0.00  -6.30  -4.29    0.00    0.00    0.00
50.29
-----
  
```

Segment Leq : 53.25 dBA

Results segment # 2: HWY 417 EB (night)

Source height = 1.49 m

Barrier height for grazing incidence

```

Source      ! Receiver      ! Barrier      ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.49 !          17.80 !          17.41 !          17.41
  
```

ROAD (0.00 + 54.80 + 0.00) = 54.80 dBA

```

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj
SubLeq
-----
  
```

```

--
-69    90     0.00  73.80    0.00 -13.44  -0.54    0.00    0.00  -5.02
54.80
-----
  
```

Segment Leq : 54.80 dBA



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Results segment # 3: HWY 417 WB (night)

Source height = 1.49 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.49	17.80	17.43	17.43

ROAD (0.00 + 54.56 + 0.00) = 54.56 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-69	90	0.00	73.80	0.00	-13.69	-0.54	0.00	0.00	-5.01

SubLeq
54.56

Segment Leq : 54.56 dBA

Total Leq All Segments: 59.03 dBA

RT/Custom data, segment # 1: LRT 1 (day/night)

1 - 4-car SRT:

Traffic volume : 192/24 veh/TimePeriod
Speed : 50 km/h

Data for Segment # 1: LRT 1 (day/night)

Angle1	Angle2	: -90.00 deg	0.00 deg
Wood depth		: 0	(No woods.)
No of house rows		: 0 / 0	
Surface		: 2	(Reflective ground surface)
Receiver source distance		: 78.00 / 78.00 m	
Receiver height		: 17.80 / 17.80 m	
Topography		: 4	(Elevated; with barrier)
Barrier angle1		: -24.00 deg	Angle2 : 0.00 deg
Barrier height		: 28.30 m	
Elevation		: 7.00 m	
Barrier receiver distance		: 48.00 / 48.00 m	
Source elevation		: 0.00 m	
Receiver elevation		: 0.00 m	
Barrier elevation		: 0.00 m	
Reference angle		: 0.00	



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RT/Custom data, segment # 2: LRT 2 (day/night)

 1 - 4-car SRT:
 Traffic volume : 192/24 veh/TimePeriod
 Speed : 50 km/h

Data for Segment # 2: LRT 2 (day/night)

 Angle1 Angle2 : 0.00 deg 90.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 2 (Reflective ground surface)
 Receiver source distance : 78.00 / 78.00 m
 Receiver height : 17.80 / 17.80 m
 Topography : 4 (Elevated; with barrier)
 Barrier angle1 : 0.00 deg Angle2 : 28.00 deg
 Barrier height : 28.30 m
 Elevation : 7.00 m
 Barrier receiver distance : 48.00 / 48.00 m
 Source elevation : 0.00 m
 Receiver elevation : 0.00 m
 Barrier elevation : 0.00 m
 Reference angle : 0.00

Results segment # 1: LRT 1 (day)

 Source height = 0.50 m

Barrier height for grazing incidence

Source Height (m)	! Receiver Height (m)	! Barrier Height (m)	! Elevation of Barrier Top (m)
0.50	!	17.80	!
		7.15	!
			7.15

RT/Custom (44.51 + 20.11 + 0.00) = 44.52 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	-24	0.00	56.02	-7.16	-4.36	0.00	0.00	0.00	44.51
-24	0	0.00	56.02	-7.16	-8.75	0.00	0.00	-20.00	20.11

 Segment Leq : 44.52 dBA



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Results segment # 2: LRT 2 (day)

Source height = 0.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
0.50	17.80	7.15	7.15

RT/Custom (0.00 + 20.78 + 44.24) = 44.25 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	28	0.00	56.02	-7.16	-8.08	0.00	0.00	-20.00	20.78
28	90	0.00	56.02	-7.16	-4.63	0.00	0.00	0.00	44.24

Segment Leq : 44.25 dBA

Total Leq All Segments: 47.40 dBA

Results segment # 1: LRT 1 (night)

Source height = 0.50 m

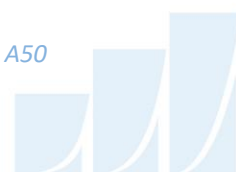
Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
0.50	17.80	7.15	7.15

RT/Custom (38.49 + 14.09 + 0.00) = 38.50 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	-24	0.00	50.00	-7.16	-4.36	0.00	0.00	0.00	38.49
-24	0	0.00	50.00	-7.16	-8.75	0.00	0.00	-20.00	14.09

Segment Leq : 38.50 dBA



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Results segment # 2: LRT 2 (night)

 Source height = 0.50 m

Barrier height for grazing incidence

Source Height (m)	! Receiver ! Height (m)	! Barrier ! Height (m)	! Elevation of ! Barrier Top (m)
0.50	!	17.80	!
		7.15	!
			7.15

RT/Custom (0.00 + 14.76 + 38.21) = 38.23 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	28	0.00	50.00	-7.16	-8.08	0.00	0.00	-20.00	14.76
28	90	0.00	50.00	-7.16	-4.63	0.00	0.00	0.00	38.21

Segment Leq : 38.23 dBA

Total Leq All Segments: 41.38 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 66.67
 (NIGHT): 59.10



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STAMSON 5.0 NORMAL REPORT Date: 23-02-2021 16:55:05
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r8b2.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: PRESTON ST (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: PRESTON ST (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 64.00 / 64.00 m
Receiver height : 17.80 / 17.80 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -26.00 deg Angle2 : 23.00 deg
Barrier height : 17.80 m
Barrier receiver distance : 18.00 / 18.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Road data, segment # 2: HWY 417 EB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)



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* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: HWY 417 EB (day/night)

Angle1 Angle2 : -69.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 331.00 / 331.00 m
Receiver height : 17.80 / 17.80 m
Topography : 4 (Elevated; with barrier)
Barrier angle1 : -69.00 deg Angle2 : 90.00 deg
Barrier height : 17.80 m
Elevation : 4.00 m
Barrier receiver distance : 8.00 / 8.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Road data, segment # 3: HWY 417 WB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: HWY 417 WB (day/night)

Angle1 Angle2 : -69.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)



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```

Receiver source distance : 351.00 / 351.00 m
Receiver height          : 17.80 / 17.80 m
Topography               : 4 (Elevated; with barrier)
Barrier angle1           : -69.00 deg Angle2 : 90.00 deg
Barrier height           : 17.80 m
Elevation                : 4.00 m
Barrier receiver distance : 8.00 / 8.00 m
Source elevation         : 0.00 m
Receiver elevation       : 0.00 m
Barrier elevation        : 0.00 m
Reference angle          : 0.00
    
```

Results segment # 1: PRESTON ST (day)

Source height = 1.50 m

Barrier height for grazing incidence

```

-----
Source      ! Receiver      ! Barrier      ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.50 !          17.80 !          13.21 !          13.21
    
```

ROAD (57.69 + 40.22 + 57.89) = 60.84 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

```

-----
--
-90   -26   0.00  68.48   0.00  -6.30  -4.49   0.00   0.00   0.00
57.69
    
```

```

-----
--
-26   23   0.00  68.48   0.00  -6.30  -5.65   0.00   0.00 -16.31
40.22
    
```

```

-----
--
 23   90   0.00  68.48   0.00  -6.30  -4.29   0.00   0.00   0.00
57.89
    
```

Segment Leq : 60.84 dBA

Results segment # 2: HWY 417 EB (day)

Source height = 1.50 m

Barrier height for grazing incidence



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Source Height (m)	! Receiver Height (m)	! Barrier Height (m)	! Elevation of Barrier Top (m)
1.50	!	17.80	!
		17.41	!
			17.41

ROAD (0.00 + 62.07 + 0.00) = 62.07 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-69	90	0.00	81.40	0.00	-13.44	-0.54	0.00	0.00	-5.35

SubLeq

--
62.07

--

Segment Leq : 62.07 dBA

Results segment # 3: HWY 417 WB (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	! Receiver Height (m)	! Barrier Height (m)	! Elevation of Barrier Top (m)
1.50	!	17.80	!
		17.43	!
			17.43

ROAD (0.00 + 61.85 + 0.00) = 61.85 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-69	90	0.00	81.40	0.00	-13.69	-0.54	0.00	0.00	-5.31

SubLeq

--
61.85

--

Segment Leq : 61.85 dBA

Total Leq All Segments: 66.39 dBA

Results segment # 1: PRESTON ST (night)

Source height = 1.50 m

Barrier height for grazing incidence

Source	! Receiver	! Barrier	! Elevation of
--------	------------	-----------	----------------



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```

Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.50 !          17.80 !          13.21 !          13.21
  
```

ROAD (50.09 + 32.62 + 50.29) = 53.24 dBA

```

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj
SubLeq
-----
  
```

```

--
-90    -26    0.00  60.88    0.00  -6.30  -4.49    0.00    0.00    0.00
50.09
-----
  
```

```

--
-26    23     0.00  60.88    0.00  -6.30  -5.65    0.00    0.00  -16.31
32.62
-----
  
```

```

--
 23    90     0.00  60.88    0.00  -6.30  -4.29    0.00    0.00    0.00
50.29
-----
  
```

Segment Leq : 53.24 dBA

Results segment # 2: HWY 417 EB (night)

Source height = 1.49 m

Barrier height for grazing incidence

```

Source      ! Receiver      ! Barrier      ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.49 !          17.80 !          17.41 !          17.41
  
```

ROAD (0.00 + 54.47 + 0.00) = 54.47 dBA

```

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj
SubLeq
-----
  
```

```

--
-69    90     0.00  73.80    0.00 -13.44  -0.54    0.00    0.00  -5.35
54.47
-----
  
```

Segment Leq : 54.47 dBA



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Results segment # 3: HWY 417 WB (night)

 Source height = 1.49 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.49	17.80	17.43	17.43

ROAD (0.00 + 54.25 + 0.00) = 54.25 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

 --
 -69 90 0.00 73.80 0.00 -13.69 -0.54 0.00 0.00 -5.31
 54.25

 --

Segment Leq : 54.25 dBA

Total Leq All Segments: 58.79 dBA

RT/Custom data, segment # 1: LRT 1 (day/night)

 1 - 4-car SRT:
 Traffic volume : 192/24 veh/TimePeriod
 Speed : 50 km/h

Data for Segment # 1: LRT 1 (day/night)

 Angle1 Angle2 : -90.00 deg 0.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 2 (Reflective ground surface)
 Receiver source distance : 78.00 / 78.00 m
 Receiver height : 17.80 / 17.80 m
 Topography : 4 (Elevated; with barrier)
 Barrier angle1 : -24.00 deg Angle2 : 0.00 deg
 Barrier height : 28.30 m
 Elevation : 7.00 m
 Barrier receiver distance : 48.00 / 48.00 m
 Source elevation : 0.00 m
 Receiver elevation : 0.00 m
 Barrier elevation : 0.00 m
 Reference angle : 0.00



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RT/Custom data, segment # 2: LRT 2 (day/night)

1 - 4-car SRT:
 Traffic volume : 192/24 veh/TimePeriod
 Speed : 50 km/h

Data for Segment # 2: LRT 2 (day/night)

 Angle1 Angle2 : 0.00 deg 90.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 2 (Reflective ground surface)
 Receiver source distance : 78.00 / 78.00 m
 Receiver height : 17.80 / 17.80 m
 Topography : 4 (Elevated; with barrier)
 Barrier angle1 : 0.00 deg Angle2 : 28.00 deg
 Barrier height : 28.30 m
 Elevation : 7.00 m
 Barrier receiver distance : 48.00 / 48.00 m
 Source elevation : 0.00 m
 Receiver elevation : 0.00 m
 Barrier elevation : 0.00 m
 Reference angle : 0.00

Results segment # 1: LRT 1 (day)

 Source height = 0.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
0.50	17.80	7.15	7.15

RT/Custom (44.51 + 20.11 + 0.00) = 44.52 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	-24	0.00	56.02	-7.16	-4.36	0.00	0.00	0.00	44.51
-24	0	0.00	56.02	-7.16	-8.75	0.00	0.00	-20.00	20.11

Segment Leq : 44.52 dBA



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Results segment # 2: LRT 2 (day)

Source height = 0.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
0.50	17.80	7.15	7.15

RT/Custom (0.00 + 20.78 + 44.24) = 44.25 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	28	0.00	56.02	-7.16	-8.08	0.00	0.00	-20.00	20.78
28	90	0.00	56.02	-7.16	-4.63	0.00	0.00	0.00	44.24

Segment Leq : 44.25 dBA

Total Leq All Segments: 47.40 dBA

Results segment # 1: LRT 1 (night)

Source height = 0.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
0.50	17.80	7.15	7.15

RT/Custom (38.49 + 14.09 + 0.00) = 38.50 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	-24	0.00	50.00	-7.16	-4.36	0.00	0.00	0.00	38.49
-24	0	0.00	50.00	-7.16	-8.75	0.00	0.00	-20.00	14.09

Segment Leq : 38.50 dBA



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Results segment # 2: LRT 2 (night)

Source height = 0.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
0.50	17.80	7.15	7.15

RT/Custom (0.00 + 14.76 + 38.21) = 38.23 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	28	0.00	50.00	-7.16	-8.08	0.00	0.00	-20.00	14.76
28	90	0.00	50.00	-7.16	-4.63	0.00	0.00	0.00	38.21

Segment Leq : 38.23 dBA

Total Leq All Segments: 41.38 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 66.44
(NIGHT): 58.87



GRADIENTWIND

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STAMSON 5.0 NORMAL REPORT Date: 23-02-2021 16:55:13
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r8b3.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: PRESTON ST (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: PRESTON ST (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 64.00 / 64.00 m
Receiver height : 17.80 / 17.80 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -26.00 deg Angle2 : 23.00 deg
Barrier height : 18.30 m
Barrier receiver distance : 18.00 / 18.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Road data, segment # 2: HWY 417 EB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)



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* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: HWY 417 EB (day/night)

Angle1 Angle2 : -69.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 331.00 / 331.00 m
Receiver height : 17.80 / 17.80 m
Topography : 4 (Elevated; with barrier)
Barrier angle1 : -69.00 deg Angle2 : 90.00 deg
Barrier height : 18.30 m
Elevation : 4.00 m
Barrier receiver distance : 8.00 / 8.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Road data, segment # 3: HWY 417 WB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: HWY 417 WB (day/night)

Angle1 Angle2 : -69.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)



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```

Receiver source distance : 351.00 / 351.00 m
Receiver height          : 17.80 / 17.80 m
Topography               : 4 (Elevated; with barrier)
Barrier angle1          : -69.00 deg Angle2 : 90.00 deg
Barrier height          : 18.30 m
Elevation                : 4.00 m
Barrier receiver distance : 8.00 / 8.00 m
Source elevation         : 0.00 m
Receiver elevation      : 0.00 m
Barrier elevation        : 0.00 m
Reference angle          : 0.00
    
```

Results segment # 1: PRESTON ST (day)

Source height = 1.50 m

Barrier height for grazing incidence

```

-----
Source      ! Receiver      ! Barrier      ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.50 !          17.80 !          13.21 !          13.21
    
```

ROAD (57.69 + 39.32 + 57.89) = 60.83 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

```

-----
--
-90  -26  0.00  68.48  0.00  -6.30  -4.49  0.00  0.00  0.00
57.69
-----

```

```

-----
--
-26  23  0.00  68.48  0.00  -6.30  -5.65  0.00  0.00 -17.21
39.32
-----

```

```

-----
--
 23  90  0.00  68.48  0.00  -6.30  -4.29  0.00  0.00  0.00
57.89
-----

```

Segment Leq : 60.83 dBA

Results segment # 2: HWY 417 EB (day)

Source height = 1.50 m

Barrier height for grazing incidence



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Source Height (m)	! Receiver ! Height (m)	! Barrier ! Height (m)	! Elevation of ! Barrier Top (m)
1.50	! 17.80	! 17.41	! 17.41

ROAD (0.00 + 60.85 + 0.00) = 60.85 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--	-69	90	0.00	81.40	0.00	-13.44	-0.54	0.00	0.00	-6.58
60.85										

Segment Leq : 60.85 dBA

Results segment # 3: HWY 417 WB (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	! Receiver ! Height (m)	! Barrier ! Height (m)	! Elevation of ! Barrier Top (m)
1.50	! 17.80	! 17.43	! 17.43

ROAD (0.00 + 60.66 + 0.00) = 60.66 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--	-69	90	0.00	81.40	0.00	-13.69	-0.54	0.00	0.00	-6.51
60.66										

Segment Leq : 60.66 dBA

Total Leq All Segments: 65.55 dBA

Results segment # 1: PRESTON ST (night)

Source height = 1.50 m

Barrier height for grazing incidence

Source	! Receiver	! Barrier	! Elevation of
--------	------------	-----------	----------------



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```

Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.50 !          17.80 !          13.21 !          13.21
  
```

ROAD (50.09 + 31.72 + 50.29) = 53.23 dBA

```

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj
SubLeq
  
```

```

--
-90    -26    0.00  60.88    0.00  -6.30  -4.49    0.00    0.00    0.00
50.09
  
```

```

--
-26    23     0.00  60.88    0.00  -6.30  -5.65    0.00    0.00  -17.21
31.72
  
```

```

--
23     90     0.00  60.88    0.00  -6.30  -4.29    0.00    0.00    0.00
50.29
  
```

Segment Leq : 53.23 dBA

Results segment # 2: HWY 417 EB (night)

Source height = 1.49 m

Barrier height for grazing incidence

```

Source      ! Receiver      ! Barrier      ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.49 !          17.80 !          17.41 !          17.41
  
```

ROAD (0.00 + 53.25 + 0.00) = 53.25 dBA

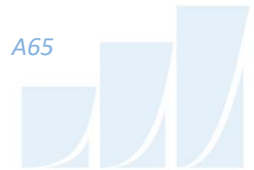
```

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj
SubLeq
  
```

```

--
-69    90     0.00  73.80    0.00 -13.44  -0.54    0.00    0.00  -6.57
53.25
  
```

Segment Leq : 53.25 dBA



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Results segment # 3: HWY 417 WB (night)

Source height = 1.49 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.49	17.80	17.43	17.43

ROAD (0.00 + 53.06 + 0.00) = 53.06 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

-69	90	0.00	73.80	0.00	-13.69	-0.54	0.00	0.00	-6.51
53.06									

Segment Leq : 53.06 dBA

Total Leq All Segments: 57.95 dBA

RT/Custom data, segment # 1: LRT 1 (day/night)

1 - 4-car SRT:

Traffic volume : 192/24 veh/TimePeriod
 Speed : 50 km/h

Data for Segment # 1: LRT 1 (day/night)

Angle1	Angle2	: -90.00 deg	0.00 deg
Wood depth		: 0	(No woods.)
No of house rows		: 0 / 0	
Surface		: 2	(Reflective ground surface)
Receiver source distance		: 78.00 / 78.00 m	
Receiver height		: 17.80 / 17.80 m	
Topography		: 4	(Elevated; with barrier)
Barrier angle1		: -24.00 deg	Angle2 : 0.00 deg
Barrier height		: 28.30 m	
Elevation		: 7.00 m	
Barrier receiver distance		: 48.00 / 48.00 m	
Source elevation		: 0.00 m	
Receiver elevation		: 0.00 m	
Barrier elevation		: 0.00 m	
Reference angle		: 0.00	



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RT/Custom data, segment # 2: LRT 2 (day/night)

1 - 4-car SRT:
 Traffic volume : 192/24 veh/TimePeriod
 Speed : 50 km/h

Data for Segment # 2: LRT 2 (day/night)

 Angle1 Angle2 : 0.00 deg 90.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 2 (Reflective ground surface)
 Receiver source distance : 78.00 / 78.00 m
 Receiver height : 17.80 / 17.80 m
 Topography : 4 (Elevated; with barrier)
 Barrier angle1 : 0.00 deg Angle2 : 28.00 deg
 Barrier height : 28.30 m
 Elevation : 7.00 m
 Barrier receiver distance : 48.00 / 48.00 m
 Source elevation : 0.00 m
 Receiver elevation : 0.00 m
 Barrier elevation : 0.00 m
 Reference angle : 0.00

Results segment # 1: LRT 1 (day)

 Source height = 0.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
0.50	17.80	7.15	7.15

RT/Custom (44.51 + 20.11 + 0.00) = 44.52 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	-24	0.00	56.02	-7.16	-4.36	0.00	0.00	0.00	44.51
-24	0	0.00	56.02	-7.16	-8.75	0.00	0.00	-20.00	20.11

Segment Leq : 44.52 dBA



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Results segment # 2: LRT 2 (day)

Source height = 0.50 m

Barrier height for grazing incidence

Source Height (m)	! Receiver ! Height (m)	! Barrier ! Height (m)	! Elevation of ! Barrier Top (m)
0.50	!	17.80	!
		7.15	!
			7.15

RT/Custom (0.00 + 20.78 + 44.24) = 44.25 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	28	0.00	56.02	-7.16	-8.08	0.00	0.00	-20.00	20.78
28	90	0.00	56.02	-7.16	-4.63	0.00	0.00	0.00	44.24

Segment Leq : 44.25 dBA

Total Leq All Segments: 47.40 dBA

Results segment # 1: LRT 1 (night)

Source height = 0.50 m

Barrier height for grazing incidence

Source Height (m)	! Receiver ! Height (m)	! Barrier ! Height (m)	! Elevation of ! Barrier Top (m)
0.50	!	17.80	!
		7.15	!
			7.15

RT/Custom (38.49 + 14.09 + 0.00) = 38.50 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	-24	0.00	50.00	-7.16	-4.36	0.00	0.00	0.00	38.49
-24	0	0.00	50.00	-7.16	-8.75	0.00	0.00	-20.00	14.09

Segment Leq : 38.50 dBA



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Results segment # 2: LRT 2 (night)

Source height = 0.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
0.50	17.80	7.15	7.15

RT/Custom (0.00 + 14.76 + 38.21) = 38.23 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	28	0.00	50.00	-7.16	-8.08	0.00	0.00	-20.00	14.76
28	90	0.00	50.00	-7.16	-4.63	0.00	0.00	0.00	38.21

Segment Leq : 38.23 dBA

Total Leq All Segments: 41.38 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 65.62
(NIGHT): 58.05



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STAMSON 5.0 NORMAL REPORT Date: 23-02-2021 16:55:23
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r8b4.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: PRESTON ST (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: PRESTON ST (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 64.00 / 64.00 m
Receiver height : 17.80 / 17.80 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -26.00 deg Angle2 : 23.00 deg
Barrier height : 18.80 m
Barrier receiver distance : 18.00 / 18.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Road data, segment # 2: HWY 417 EB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)



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* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: HWY 417 EB (day/night)

Angle1 Angle2 : -69.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 331.00 / 331.00 m
Receiver height : 17.80 / 17.80 m
Topography : 4 (Elevated; with barrier)
Barrier angle1 : -69.00 deg Angle2 : 90.00 deg
Barrier height : 18.80 m
Elevation : 4.00 m
Barrier receiver distance : 8.00 / 8.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Road data, segment # 3: HWY 417 WB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: HWY 417 WB (day/night)

Angle1 Angle2 : -69.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)



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```

Receiver source distance : 351.00 / 351.00 m
Receiver height          : 17.80 / 17.80 m
Topography               : 4 (Elevated; with barrier)
Barrier angle1           : -69.00 deg Angle2 : 90.00 deg
Barrier height           : 18.80 m
Elevation                : 4.00 m
Barrier receiver distance : 8.00 / 8.00 m
Source elevation         : 0.00 m
Receiver elevation       : 0.00 m
Barrier elevation        : 0.00 m
Reference angle          : 0.00
    
```

Results segment # 1: PRESTON ST (day)

Source height = 1.50 m

Barrier height for grazing incidence

```

-----
Source      ! Receiver      ! Barrier      ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.50 !       17.80 !       13.21 !       13.21
    
```

ROAD (57.69 + 38.50 + 57.89) = 60.82 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

```

-----
--
-90  -26  0.00  68.48  0.00  -6.30  -4.49  0.00  0.00  0.00
57.69
-----

```

```

-----
--
-26  23  0.00  68.48  0.00  -6.30  -5.65  0.00  0.00 -18.03
38.50
-----

```

```

-----
--
 23  90  0.00  68.48  0.00  -6.30  -4.29  0.00  0.00  0.00
57.89
-----

```

Segment Leq : 60.82 dBA

Results segment # 2: HWY 417 EB (day)

Source height = 1.50 m

Barrier height for grazing incidence



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Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	17.80	17.41	17.41

ROAD (0.00 + 59.28 + 0.00) = 59.28 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-69	90	0.00	81.40	0.00	-13.44	-0.54	0.00	0.00	-8.14

SubLeq
59.28

Segment Leq : 59.28 dBA

Results segment # 3: HWY 417 WB (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	17.80	17.43	17.43

ROAD (0.00 + 59.10 + 0.00) = 59.10 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-69	90	0.00	81.40	0.00	-13.69	-0.54	0.00	0.00	-8.07

SubLeq
59.10

Segment Leq : 59.10 dBA

Total Leq All Segments: 64.58 dBA

Results segment # 1: PRESTON ST (night)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	17.80	17.43	17.43



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```

Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.50 !          17.80 !          13.21 !          13.21
  
```

ROAD (50.09 + 30.91 + 50.29) = 53.23 dBA

```

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj
SubLeq
-----
  
```

```

--
-90    -26    0.00  60.88    0.00  -6.30  -4.49    0.00    0.00    0.00
50.09
-----
  
```

```

--
-26    23     0.00  60.88    0.00  -6.30  -5.65    0.00    0.00  -18.03
30.91
-----
  
```

```

--
 23    90     0.00  60.88    0.00  -6.30  -4.29    0.00    0.00    0.00
50.29
-----
  
```

Segment Leq : 53.23 dBA

Results segment # 2: HWY 417 EB (night)

Source height = 1.49 m

Barrier height for grazing incidence

```

Source      ! Receiver      ! Barrier      ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.49 !          17.80 !          17.41 !          17.41
  
```

ROAD (0.00 + 51.68 + 0.00) = 51.68 dBA

```

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj
SubLeq
-----
  
```

```

--
-69    90     0.00  73.80    0.00 -13.44  -0.54    0.00    0.00  -8.14
51.68
-----
  
```

Segment Leq : 51.68 dBA



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Results segment # 3: HWY 417 WB (night)

Source height = 1.49 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.49	17.80	17.43	17.43

ROAD (0.00 + 51.50 + 0.00) = 51.50 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

-69	90	0.00	73.80	0.00	-13.69	-0.54	0.00	0.00	-8.07
51.50									

Segment Leq : 51.50 dBA

Total Leq All Segments: 56.98 dBA

RT/Custom data, segment # 1: LRT 1 (day/night)

1 - 4-car SRT:

Traffic volume : 192/24 veh/TimePeriod
 Speed : 50 km/h

Data for Segment # 1: LRT 1 (day/night)

Angle1	Angle2	: -90.00 deg	0.00 deg
Wood depth		: 0	(No woods.)
No of house rows		: 0 / 0	
Surface		: 2	(Reflective ground surface)
Receiver source distance		: 78.00 / 78.00 m	
Receiver height		: 17.80 / 17.80 m	
Topography		: 4	(Elevated; with barrier)
Barrier angle1		: -24.00 deg	Angle2 : 0.00 deg
Barrier height		: 28.30 m	
Elevation		: 7.00 m	
Barrier receiver distance		: 48.00 / 48.00 m	
Source elevation		: 0.00 m	
Receiver elevation		: 0.00 m	
Barrier elevation		: 0.00 m	
Reference angle		: 0.00	



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RT/Custom data, segment # 2: LRT 2 (day/night)

 1 - 4-car SRT:
 Traffic volume : 192/24 veh/TimePeriod
 Speed : 50 km/h

Data for Segment # 2: LRT 2 (day/night)

 Angle1 Angle2 : 0.00 deg 90.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 2 (Reflective ground surface)
 Receiver source distance : 78.00 / 78.00 m
 Receiver height : 17.80 / 17.80 m
 Topography : 4 (Elevated; with barrier)
 Barrier angle1 : 0.00 deg Angle2 : 28.00 deg
 Barrier height : 28.30 m
 Elevation : 7.00 m
 Barrier receiver distance : 48.00 / 48.00 m
 Source elevation : 0.00 m
 Receiver elevation : 0.00 m
 Barrier elevation : 0.00 m
 Reference angle : 0.00

Results segment # 1: LRT 1 (day)

 Source height = 0.50 m

Barrier height for grazing incidence

Source Height (m)	! Receiver ! Height (m)	! Barrier ! Height (m)	! Elevation of ! Barrier Top (m)
0.50	!	17.80	!
	!	7.15	!
			7.15

RT/Custom (44.51 + 20.11 + 0.00) = 44.52 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	-24	0.00	56.02	-7.16	-4.36	0.00	0.00	0.00	44.51
-24	0	0.00	56.02	-7.16	-8.75	0.00	0.00	-20.00	20.11

 Segment Leq : 44.52 dBA



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Results segment # 2: LRT 2 (day)

Source height = 0.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
0.50	17.80	7.15	7.15

RT/Custom (0.00 + 20.78 + 44.24) = 44.25 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	28	0.00	56.02	-7.16	-8.08	0.00	0.00	-20.00	20.78
28	90	0.00	56.02	-7.16	-4.63	0.00	0.00	0.00	44.24

Segment Leq : 44.25 dBA

Total Leq All Segments: 47.40 dBA

Results segment # 1: LRT 1 (night)

Source height = 0.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
0.50	17.80	7.15	7.15

RT/Custom (38.49 + 14.09 + 0.00) = 38.50 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	-24	0.00	50.00	-7.16	-4.36	0.00	0.00	0.00	38.49
-24	0	0.00	50.00	-7.16	-8.75	0.00	0.00	-20.00	14.09

Segment Leq : 38.50 dBA



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Results segment # 2: LRT 2 (night)

 Source height = 0.50 m

Barrier height for grazing incidence

Source Height (m)	! Receiver ! Height (m)	! Barrier ! Height (m)	! Elevation of ! Barrier Top (m)
0.50	!	17.80	!
		7.15	!
			7.15

RT/Custom (0.00 + 14.76 + 38.21) = 38.23 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	28	0.00	50.00	-7.16	-8.08	0.00	0.00	-20.00	14.76
28	90	0.00	50.00	-7.16	-4.63	0.00	0.00	0.00	38.21

Segment Leq : 38.23 dBA

Total Leq All Segments: 41.38 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 64.66
 (NIGHT): 57.10



GRADIENTWIND

ENGINEERS & SCIENTISTS

STAMSON 5.0 NORMAL REPORT Date: 23-02-2021 16:55:32
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r9.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: HWY 417 EB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: HWY 417 EB (day/night)

Angle1 Angle2 : -90.00 deg 0.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 332.00 / 332.00 m
Receiver height : 29.80 / 29.80 m
Topography : 4 (Elevated; with barrier)
Barrier angle1 : -90.00 deg Angle2 : 0.00 deg
Barrier height : 28.30 m
Elevation : 4.00 m
Barrier receiver distance : 5.00 / 5.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Road data, segment # 2: HWY 417 WB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)



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* Refers to calculated road volumes based on the following input:

```

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth      : 0.00
Number of Years of Growth       : 0.00
Medium Truck % of Total Volume  : 7.00
Heavy Truck % of Total Volume   : 5.00
Day (16 hrs) % of Total Volume  : 92.00
    
```

Data for Segment # 2: HWY 417 WB (day/night)

```

-----
Angle1  Angle2      : -90.00 deg   0.00 deg
Wood depth      :      0      (No woods.)
No of house rows :      0 / 0
Surface         :      1      (Absorptive ground surface)
Receiver source distance : 352.00 / 352.00 m
Receiver height  : 29.80 / 29.80 m
Topography      :      4      (Elevated; with barrier)
Barrier angle1   : -90.00 deg   Angle2 : 0.00 deg
Barrier height   : 28.30 m
Elevation       : 4.00 m
Barrier receiver distance : 5.00 / 5.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle  : 0.00
    
```

Results segment # 1: HWY 417 EB (day)

Source height = 1.50 m

Barrier height for grazing incidence

```

-----
Source      ! Receiver      ! Barrier      ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.50 !      29.80 !      29.37 !      29.37
    
```

ROAD (0.00 + 64.94 + 0.00) = 64.94 dBA

```

Angle1 Angle2  Alpha RefLeq  P.Adj  D.Adj  F.Adj  W.Adj  H.Adj  B.Adj
SubLeq
-----
--
    
```

```

--
-90      0      0.00  81.40  0.00 -13.45 -3.01  0.00  0.00 -0.82
64.11*
-90      0      0.00  81.40  0.00 -13.45 -3.01  0.00  0.00  0.00
64.94
-----
--
    
```



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* Bright Zone !

Segment Leq : 64.94 dBA

Results segment # 2: HWY 417 WB (day)

 Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	29.80	29.40	29.40

ROAD (0.00 + 64.68 + 0.00) = 64.68 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--									
-90	0	0.00	81.40	0.00	-13.70	-3.01	0.00	0.00	-0.78
63.90*									
-90	0	0.00	81.40	0.00	-13.70	-3.01	0.00	0.00	0.00
64.68									

 * Bright Zone !

Segment Leq : 64.68 dBA

Total Leq All Segments: 67.82 dBA

Results segment # 1: HWY 417 EB (night)

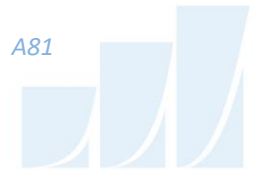
 Source height = 1.49 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.49	29.80	29.37	29.37

ROAD (0.00 + 57.34 + 0.00) = 57.34 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									



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```

-----
--
-90      0    0.00  73.80   0.00 -13.45  -3.01   0.00   0.00  -0.82
56.51*
-90      0    0.00  73.80   0.00 -13.45  -3.01   0.00   0.00   0.00
57.34
-----

```

* Bright Zone !

Segment Leq : 57.34 dBA

Results segment # 2: HWY 417 WB (night)

Source height = 1.49 m

Barrier height for grazing incidence

```

-----
Source      ! Receiver      ! Barrier      ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.49 !       29.80 !       29.40 !       29.40
-----

```

ROAD (0.00 + 57.08 + 0.00) = 57.08 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj
SubLeq

```

-----
--
-90      0    0.00  73.80   0.00 -13.70  -3.01   0.00   0.00  -0.78
56.30*
-90      0    0.00  73.80   0.00 -13.70  -3.01   0.00   0.00   0.00
57.08
-----

```

* Bright Zone !

Segment Leq : 57.08 dBA

Total Leq All Segments: 60.22 dBA

RT/Custom data, segment # 1: LRT (day/night)

```

-----
1 - 4-car SRT:
Traffic volume      :    192/24    veh/TimePeriod
Speed                :    50 km/h
-----

```

Data for Segment # 1: LRT (day/night)



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```

Angle1   Angle2           :   0.00 deg   90.00 deg
Wood depth      :           0       (No woods.)
No of house rows :           0 / 0
Surface         :           2       (Reflective ground surface)
Receiver source distance : 37.00 / 37.00 m
Receiver height : 29.80 / 29.80 m
Topography      :           4       (Elevated; with barrier)
Barrier angle1  :   0.00 deg   Angle2 : 90.00 deg
Barrier height  : 28.30 m
Elevation       :   7.00 m
Barrier receiver distance : 6.00 / 6.00 m
Source elevation :   0.00 m
Receiver elevation :   0.00 m
Barrier elevation :   0.00 m
Reference angle :   0.00
  
```

Results segment # 1: LRT (day)

Source height = 0.50 m

Barrier height for grazing incidence

```

-----
Source      ! Receiver      ! Barrier      ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          0.50 !      29.80 !      25.05 !      25.05
  
```

RT/Custom (0.00 + 37.02 + 0.00) = 37.02 dBA

```

-----
Angle1 Angle2  Alpha RefLeq  D.Adj  F.Adj  W.Adj  H.Adj  B.Adj  SubLeq
-----+-----+-----+-----+-----+-----+-----+-----+-----
      0    90   0.00  56.02  -3.92  -3.01   0.00   0.00 -12.07  37.02
-----
  
```

Segment Leq : 37.02 dBA

Total Leq All Segments: 37.02 dBA

Results segment # 1: LRT (night)

Source height = 0.50 m

Barrier height for grazing incidence

```

-----
Source      ! Receiver      ! Barrier      ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          0.50 !      29.80 !      25.05 !      25.05
  
```

RT/Custom (0.00 + 31.00 + 0.00) = 31.00 dBA



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Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	90	0.00	50.00	-3.92	-3.01	0.00	0.00	-12.07	31.00

Segment Leq : 31.00 dBA

Total Leq All Segments: 31.00 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 67.83
(NIGHT): 60.23



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STAMSON 5.0 NORMAL REPORT Date: 23-02-2021 16:55:40
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r9b1.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: HWY 417 EB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: HWY 417 EB (day/night)

Angle1 Angle2 : -90.00 deg 0.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 332.00 / 332.00 m
Receiver height : 29.80 / 29.80 m
Topography : 4 (Elevated; with barrier)
Barrier angle1 : -90.00 deg Angle2 : 0.00 deg
Barrier height : 29.50 m
Elevation : 4.00 m
Barrier receiver distance : 5.00 / 5.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Road data, segment # 2: HWY 417 WB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)



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* Refers to calculated road volumes based on the following input:

```

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth       : 0.00
Number of Years of Growth        : 0.00
Medium Truck % of Total Volume   : 7.00
Heavy Truck % of Total Volume    : 5.00
Day (16 hrs) % of Total Volume   : 92.00
    
```

Data for Segment # 2: HWY 417 WB (day/night)

```

-----
Angle1   Angle2       : -90.00 deg   0.00 deg
Wood depth      : 0 (No woods.)
No of house rows : 0 / 0
Surface        : 1 (Absorptive ground surface)
Receiver source distance : 352.00 / 352.00 m
Receiver height : 29.80 / 29.80 m
Topography     : 4 (Elevated; with barrier)
Barrier angle1 : -90.00 deg   Angle2 : 0.00 deg
Barrier height  : 29.50 m
Elevation      : 4.00 m
Barrier receiver distance : 5.00 / 5.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00
    
```

Results segment # 1: HWY 417 EB (day)

Source height = 1.50 m

Barrier height for grazing incidence

```

-----
Source      ! Receiver      ! Barrier      ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.50 !      29.80 !      29.37 !      29.37
    
```

ROAD (0.00 + 59.88 + 0.00) = 59.88 dBA

```

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj
SubLeq
-----
--
-90     0     0.00 81.40 0.00 -13.45 -3.01 0.00 0.00 -5.05
59.88
-----
--
    
```

Segment Leq : 59.88 dBA



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Results segment # 2: HWY 417 WB (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	29.80	29.40	29.40

ROAD (0.00 + 59.65 + 0.00) = 59.65 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	0	0.00	81.40	0.00	-13.70	-3.01	0.00	0.00	-5.04

SubLeq

Segment Leq : 59.65 dBA

Total Leq All Segments: 62.78 dBA

Results segment # 1: HWY 417 EB (night)

Source height = 1.49 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.49	29.80	29.37	29.37

ROAD (0.00 + 52.28 + 0.00) = 52.28 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	0	0.00	73.80	0.00	-13.45	-3.01	0.00	0.00	-5.05

SubLeq

Segment Leq : 52.28 dBA



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Results segment # 2: HWY 417 WB (night)

 Source height = 1.49 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.49	29.80	29.40	29.40

ROAD (0.00 + 52.05 + 0.00) = 52.05 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

 --
 -90 0 0.00 73.80 0.00 -13.70 -3.01 0.00 0.00 -5.04
 52.05

 --

Segment Leq : 52.05 dBA

Total Leq All Segments: 55.18 dBA

RT/Custom data, segment # 1: LRT (day/night)

 1 - 4-car SRT:
 Traffic volume : 192/24 veh/TimePeriod
 Speed : 50 km/h

Data for Segment # 1: LRT (day/night)

 Angle1 Angle2 : 0.00 deg 90.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 2 (Reflective ground surface)
 Receiver source distance : 37.00 / 37.00 m
 Receiver height : 29.80 / 29.80 m
 Topography : 4 (Elevated; with barrier)
 Barrier angle1 : 0.00 deg Angle2 : 90.00 deg
 Barrier height : 29.50 m
 Elevation : 7.00 m
 Barrier receiver distance : 6.00 / 6.00 m
 Source elevation : 0.00 m
 Receiver elevation : 0.00 m
 Barrier elevation : 0.00 m
 Reference angle : 0.00



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Results segment # 1: LRT (day)

Source height = 0.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
0.50	29.80	25.05	25.05

RT/Custom (0.00 + 34.77 + 0.00) = 34.77 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	90	0.00	56.02	-3.92	-3.01	0.00	0.00	-14.32	34.77

Segment Leq : 34.77 dBA

Total Leq All Segments: 34.77 dBA

Results segment # 1: LRT (night)

Source height = 0.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
0.50	29.80	25.05	25.05

RT/Custom (0.00 + 28.75 + 0.00) = 28.75 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	90	0.00	50.00	-3.92	-3.01	0.00	0.00	-14.32	28.75

Segment Leq : 28.75 dBA

Total Leq All Segments: 28.75 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 62.78
(NIGHT): 55.19



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STAMSON 5.0 NORMAL REPORT Date: 23-02-2021 16:55:52
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r9b2.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: HWY 417 EB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: HWY 417 EB (day/night)

Angle1 Angle2 : -90.00 deg 0.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 332.00 / 332.00 m
Receiver height : 29.80 / 29.80 m
Topography : 4 (Elevated; with barrier)
Barrier angle1 : -90.00 deg Angle2 : 0.00 deg
Barrier height : 29.80 m
Elevation : 4.00 m
Barrier receiver distance : 5.00 / 5.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Road data, segment # 2: HWY 417 WB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)



GRADIENTWIND

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* Refers to calculated road volumes based on the following input:

```

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth      : 0.00
Number of Years of Growth       : 0.00
Medium Truck % of Total Volume  : 7.00
Heavy Truck % of Total Volume   : 5.00
Day (16 hrs) % of Total Volume  : 92.00
    
```

Data for Segment # 2: HWY 417 WB (day/night)

```

-----
Angle1   Angle2      : -90.00 deg   0.00 deg
Wood depth      :      0      (No woods.)
No of house rows :      0 / 0
Surface        :      1      (Absorptive ground surface)
Receiver source distance : 352.00 / 352.00 m
Receiver height : 29.80 / 29.80 m
Topography     :      4      (Elevated; with barrier)
Barrier angle1 : -90.00 deg   Angle2 : 0.00 deg
Barrier height  : 29.80 m
Elevation      : 4.00 m
Barrier receiver distance : 5.00 / 5.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00
    
```

Results segment # 1: HWY 417 EB (day)

Source height = 1.50 m

Barrier height for grazing incidence

```

-----
Source      ! Receiver      ! Barrier      ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.50 !      29.80 !      29.37 !      29.37
    
```

ROAD (0.00 + 59.36 + 0.00) = 59.36 dBA

```

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj
SubLeq
    
```

```

-----
--
-90      0      0.00  81.40  0.00 -13.45 -3.01  0.00  0.00 -5.58
59.36
-----
--
    
```

Segment Leq : 59.36 dBA



GRADIENTWIND

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Results segment # 2: HWY 417 WB (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	29.80	29.40	29.40

ROAD (0.00 + 59.17 + 0.00) = 59.17 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	0	0.00	81.40	0.00	-13.70	-3.01	0.00	0.00	-5.52

SubLeq

59.17

Segment Leq : 59.17 dBA

Total Leq All Segments: 62.28 dBA

Results segment # 1: HWY 417 EB (night)

Source height = 1.49 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.49	29.80	29.37	29.37

ROAD (0.00 + 51.76 + 0.00) = 51.76 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	0	0.00	73.80	0.00	-13.45	-3.01	0.00	0.00	-5.58

SubLeq

51.76

Segment Leq : 51.76 dBA



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Results segment # 2: HWY 417 WB (night)

Source height = 1.49 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.49	29.80	29.40	29.40

ROAD (0.00 + 51.57 + 0.00) = 51.57 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	0	0.00	73.80	0.00	-13.70	-3.01	0.00	0.00	-5.52

SubLeq
51.57

Segment Leq : 51.57 dBA

Total Leq All Segments: 54.68 dBA

RT/Custom data, segment # 1: LRT (day/night)

1 - 4-car SRT:

Traffic volume : 192/24 veh/TimePeriod
Speed : 50 km/h

Data for Segment # 1: LRT (day/night)

Angle1	Angle2	: 0.00 deg	90.00 deg
Wood depth		: 0	(No woods.)
No of house rows		: 0 / 0	
Surface		: 2	(Reflective ground surface)
Receiver source distance		: 37.00 / 37.00 m	
Receiver height		: 29.80 / 29.80 m	
Topography		: 4	(Elevated; with barrier)
Barrier angle1		: 0.00 deg	Angle2 : 90.00 deg
Barrier height		: 29.80 m	
Elevation		: 7.00 m	
Barrier receiver distance		: 6.00 / 6.00 m	
Source elevation		: 0.00 m	
Receiver elevation		: 0.00 m	
Barrier elevation		: 0.00 m	
Reference angle		: 0.00	



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Results segment # 1: LRT (day)

Source height = 0.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
0.50	29.80	25.05	25.05

RT/Custom (0.00 + 34.28 + 0.00) = 34.28 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	90	0.00	56.02	-3.92	-3.01	0.00	0.00	-14.81	34.28

Segment Leq : 34.28 dBA

Total Leq All Segments: 34.28 dBA

Results segment # 1: LRT (night)

Source height = 0.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
0.50	29.80	25.05	25.05

RT/Custom (0.00 + 28.26 + 0.00) = 28.26 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	90	0.00	50.00	-3.92	-3.01	0.00	0.00	-14.81	28.26

Segment Leq : 28.26 dBA

Total Leq All Segments: 28.26 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 62.28
(NIGHT): 54.69



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ENGINEERS & SCIENTISTS

STAMSON 5.0 NORMAL REPORT Date: 23-02-2021 16:56:16
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r9b3.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: HWY 417 EB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: HWY 417 EB (day/night)

Angle1 Angle2 : -90.00 deg 0.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 332.00 / 332.00 m
Receiver height : 29.80 / 29.80 m
Topography : 4 (Elevated; with barrier)
Barrier angle1 : -90.00 deg Angle2 : 0.00 deg
Barrier height : 30.30 m
Elevation : 4.00 m
Barrier receiver distance : 5.00 / 5.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Road data, segment # 2: HWY 417 WB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)



GRADIENTWIND

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* Refers to calculated road volumes based on the following input:

```

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth       : 0.00
Number of Years of Growth        : 0.00
Medium Truck % of Total Volume   : 7.00
Heavy Truck % of Total Volume    : 5.00
Day (16 hrs) % of Total Volume   : 92.00
    
```

Data for Segment # 2: HWY 417 WB (day/night)

```

-----
Angle1   Angle2       : -90.00 deg   0.00 deg
Wood depth      :           0       (No woods.)
No of house rows :           0 / 0
Surface        :           1       (Absorptive ground surface)
Receiver source distance : 352.00 / 352.00 m
Receiver height  : 29.80 / 29.80 m
Topography     :           4       (Elevated; with barrier)
Barrier angle1  : -90.00 deg   Angle2 : 0.00 deg
Barrier height  : 30.30 m
Elevation      : 4.00 m
Barrier receiver distance : 5.00 / 5.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00
    
```

Results segment # 1: HWY 417 EB (day)

Source height = 1.50 m

Barrier height for grazing incidence

```

-----
Source      ! Receiver      ! Barrier      ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.50 !       29.80 !       29.37 !       29.37
    
```

ROAD (0.00 + 57.75 + 0.00) = 57.75 dBA

```

Angle1 Angle2  Alpha RefLeq  P.Adj  D.Adj  F.Adj  W.Adj  H.Adj  B.Adj
SubLeq
    
```

```

-----
--
-90      0      0.00  81.40   0.00 -13.45  -3.01   0.00   0.00  -7.18
57.75
-----
--
    
```

Segment Leq : 57.75 dBA



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Results segment # 2: HWY 417 WB (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	29.80	29.40	29.40

ROAD (0.00 + 57.59 + 0.00) = 57.59 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	0	0.00	81.40	0.00	-13.70	-3.01	0.00	0.00	-7.09

SubLeq

Segment Leq : 57.59 dBA

Total Leq All Segments: 60.68 dBA

Results segment # 1: HWY 417 EB (night)

Source height = 1.49 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.49	29.80	29.37	29.37

ROAD (0.00 + 50.16 + 0.00) = 50.16 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	0	0.00	73.80	0.00	-13.45	-3.01	0.00	0.00	-7.18

SubLeq

Segment Leq : 50.16 dBA



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Results segment # 2: HWY 417 WB (night)

Source height = 1.49 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.49	29.80	29.40	29.40

ROAD (0.00 + 49.99 + 0.00) = 49.99 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

-90	0	0.00	73.80	0.00	-13.70	-3.01	0.00	0.00	-7.09
49.99									

Segment Leq : 49.99 dBA

Total Leq All Segments: 53.09 dBA

RT/Custom data, segment # 1: LRT (day/night)

1 - 4-car SRT:

Traffic volume : 192/24 veh/TimePeriod
 Speed : 50 km/h

Data for Segment # 1: LRT (day/night)

Angle1	Angle2	: 0.00 deg	90.00 deg
Wood depth		: 0	(No woods.)
No of house rows		: 0 / 0	
Surface		: 2	(Reflective ground surface)
Receiver source distance		: 37.00 / 37.00 m	
Receiver height		: 29.80 / 29.80 m	
Topography		: 4	(Elevated; with barrier)
Barrier angle1		: 0.00 deg	Angle2 : 90.00 deg
Barrier height		: 30.30 m	
Elevation		: 7.00 m	
Barrier receiver distance		: 6.00 / 6.00 m	
Source elevation		: 0.00 m	
Receiver elevation		: 0.00 m	
Barrier elevation		: 0.00 m	
Reference angle		: 0.00	



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Results segment # 1: LRT (day)

Source height = 0.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
0.50	29.80	25.05	25.05

RT/Custom (0.00 + 33.54 + 0.00) = 33.54 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	90	0.00	56.02	-3.92	-3.01	0.00	0.00	-15.55	33.54

Segment Leq : 33.54 dBA

Total Leq All Segments: 33.54 dBA

Results segment # 1: LRT (night)

Source height = 0.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
0.50	29.80	25.05	25.05

RT/Custom (0.00 + 27.52 + 0.00) = 27.52 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	90	0.00	50.00	-3.92	-3.01	0.00	0.00	-15.55	27.52

Segment Leq : 27.52 dBA

Total Leq All Segments: 27.52 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 60.69
(NIGHT): 53.10



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STAMSON 5.0 NORMAL REPORT Date: 23-02-2021 16:56:25
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r9b4.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: HWY 417 EB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: HWY 417 EB (day/night)

Angle1 Angle2 : -90.00 deg 0.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 332.00 / 332.00 m
Receiver height : 29.80 / 29.80 m
Topography : 4 (Elevated; with barrier)
Barrier angle1 : -90.00 deg Angle2 : 0.00 deg
Barrier height : 30.50 m
Elevation : 4.00 m
Barrier receiver distance : 5.00 / 5.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Road data, segment # 2: HWY 417 WB (day/night)

Car traffic volume : 59370/5163 veh/TimePeriod *
Medium truck volume : 4723/411 veh/TimePeriod *
Heavy truck volume : 3373/293 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)



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* Refers to calculated road volumes based on the following input:

```

24 hr Traffic Volume (AADT or SADT): 73332
Percentage of Annual Growth      : 0.00
Number of Years of Growth       : 0.00
Medium Truck % of Total Volume  : 7.00
Heavy Truck % of Total Volume   : 5.00
Day (16 hrs) % of Total Volume  : 92.00
    
```

Data for Segment # 2: HWY 417 WB (day/night)

```

-----
Angle1  Angle2      : -90.00 deg   0.00 deg
Wood depth      :      0      (No woods.)
No of house rows :      0 / 0
Surface         :      1      (Absorptive ground surface)
Receiver source distance : 352.00 / 352.00 m
Receiver height  : 29.80 / 29.80 m
Topography      :      4      (Elevated; with barrier)
Barrier angle1  : -90.00 deg   Angle2 : 0.00 deg
Barrier height   : 30.50 m
Elevation       : 4.00 m
Barrier receiver distance : 5.00 / 5.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle  : 0.00
    
```

Results segment # 1: HWY 417 EB (day)

Source height = 1.50 m

Barrier height for grazing incidence

```

-----
Source      ! Receiver      ! Barrier      ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.50 !      29.80 !      29.37 !      29.37
    
```

ROAD (0.00 + 57.04 + 0.00) = 57.04 dBA

```

Angle1 Angle2  Alpha RefLeq  P.Adj  D.Adj  F.Adj  W.Adj  H.Adj  B.Adj
SubLeq
-----
--
-90     0     0.00  81.40   0.00 -13.45  -3.01   0.00   0.00  -7.90
57.04
-----
--
    
```

Segment Leq : 57.04 dBA



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Results segment # 2: HWY 417 WB (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	29.80	29.40	29.40

ROAD (0.00 + 56.87 + 0.00) = 56.87 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	0	0.00	81.40	0.00	-13.70	-3.01	0.00	0.00	-7.81

SubLeq

Segment Leq : 56.87 dBA

Total Leq All Segments: 59.97 dBA

Results segment # 1: HWY 417 EB (night)

Source height = 1.49 m

Barrier height for grazing incidence

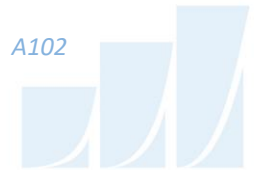
Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.49	29.80	29.37	29.37

ROAD (0.00 + 49.44 + 0.00) = 49.44 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	0	0.00	73.80	0.00	-13.45	-3.01	0.00	0.00	-7.90

SubLeq

Segment Leq : 49.44 dBA



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Results segment # 2: HWY 417 WB (night)

Source height = 1.49 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.49	29.80	29.40	29.40

ROAD (0.00 + 49.27 + 0.00) = 49.27 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	0	0.00	73.80	0.00	-13.70	-3.01	0.00	0.00	-7.81

SubLeq

Segment Leq : 49.27 dBA

Total Leq All Segments: 52.37 dBA

RT/Custom data, segment # 1: LRT (day/night)

1 - 4-car SRT:

Traffic volume : 192/24 veh/TimePeriod
 Speed : 50 km/h

Data for Segment # 1: LRT (day/night)

Angle1	Angle2	: 0.00 deg	90.00 deg
Wood depth		: 0	(No woods.)
No of house rows		: 0 / 0	
Surface		: 2	(Reflective ground surface)
Receiver source distance		: 37.00 / 37.00 m	
Receiver height		: 29.80 / 29.80 m	
Topography		: 4	(Elevated; with barrier)
Barrier angle1		: 0.00 deg	Angle2 : 90.00 deg
Barrier height		: 30.50 m	
Elevation		: 7.00 m	
Barrier receiver distance		: 6.00 / 6.00 m	
Source elevation		: 0.00 m	
Receiver elevation		: 0.00 m	
Barrier elevation		: 0.00 m	
Reference angle		: 0.00	



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Results segment # 1: LRT (day)

Source height = 0.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
0.50	29.80	25.05	25.05

RT/Custom (0.00 + 33.29 + 0.00) = 33.29 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	90	0.00	56.02	-3.92	-3.01	0.00	0.00	-15.80	33.29

Segment Leq : 33.29 dBA

Total Leq All Segments: 33.29 dBA

Results segment # 1: LRT (night)

Source height = 0.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
0.50	29.80	25.05	25.05

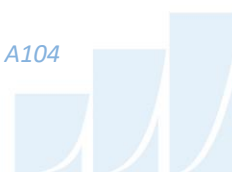
RT/Custom (0.00 + 27.27 + 0.00) = 27.27 dBA

Angle1	Angle2	Alpha	RefLeq	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
0	90	0.00	50.00	-3.92	-3.01	0.00	0.00	-15.80	27.27

Segment Leq : 27.27 dBA

Total Leq All Segments: 27.27 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 59.98
(NIGHT): 52.38



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APPENDIX B

FTA VIBRATION CALCULATIONS

**Possible Vibration Impacts
Predicted using FTA General Assesment**

Train Speed	50 km/h	31 mph
	Distance from C/L	
	(m)	(ft)
LRT	24.0	78.7

Vibration

From FTA Manual Fig 10-1

Vibration Levels at distance from track 69 dBV re 1 micro in/sec

Adjustment Factors FTA Table 10-1

Speed reference 50 mph	-4.15	Speed Limit of 50 km/h (54.7 mph)
Vehicle Parameters	0	Assume Soft primary suspension, Wheels run true
Track Condition	0	None
Track Treatments	0	None
Type of Transit Structure	0	Open Cut
Efficient vibration Propagation	0	Propagation through rock
Vibration Levels at Fdn	65	
Coupling to Building Foundation	0	Foundation in rock
Floor to Floor Attenuation	-2.0	Ground Floor Occupied
Amplification of Floor and Walls	6	
Total Vibration Level	68.85	dBV or 0.070 mm/s
Noise Level in dBA	33.85	dBa



**Table 10-1. Adjustment Factors for Generalized Predictions of
Ground-Borne Vibration and Noise**

<i>Factors Affecting Vibration Source</i>				
Source Factor	Adjustment to Propagation Curve		Comment	
Speed	Reference Speed		Vibration level is approximately proportional to $20 \cdot \log(\text{speed}/\text{speed}_{\text{ref}})$. Sometimes the variation with speed has been observed to be as low as 10 to 15 $\log(\text{speed}/\text{speed}_{\text{ref}})$.	
	Vehicle Speed			
		50 mph		30 mph
	60 mph	+1.6 dB		+6.0 dB
	50 mph	0.0 dB		+4.4 dB
	40 mph	-1.9 dB		+2.5 dB
30 mph	-4.4 dB	0.0 dB		
20 mph	-8.0 dB	-3.5 dB		
Vehicle Parameters (not additive, apply greatest value only)				
Vehicle with stiff primary suspension	+8 dB		Transit vehicles with stiff primary suspensions have been shown to create high vibration levels. Include this adjustment when the primary suspension has a vertical resonance frequency greater than 15 Hz.	
Resilient Wheels	0 dB		Resilient wheels do not generally affect ground-borne vibration except at frequencies greater than about 80 Hz.	
Worn Wheels or Wheels with Flats	+10 dB		Wheel flats or wheels that are unevenly worn can cause high vibration levels. This can be prevented with wheel truing and slip-slide detectors to prevent the wheels from sliding on the track.	
Track Conditions (not additive, apply greatest value only)				
Worn or Corrugated Track	+10 dB		If both the wheels and the track are worn, only one adjustment should be used. Corrugated track is a common problem. Mill scale on new rail can cause higher vibration levels until the rail has been in use for some time.	
Special Trackwork	+10 dB		Wheel impacts at special trackwork will significantly increase vibration levels. The increase will be less at greater distances from the track.	
Jointed Track or Uneven Road Surfaces	+5 dB		Jointed track can cause higher vibration levels than welded track. Rough roads or expansion joints are sources of increased vibration for rubber-tire transit.	
Track Treatments (not additive, apply greatest value only)				
Floating Slab Trackbed	-15 dB		The reduction achieved with a floating slab trackbed is strongly dependent on the frequency characteristics of the vibration.	
Ballast Mats	-10 dB		Actual reduction is strongly dependent on frequency of vibration.	
High-Resilience Fasteners	-5 dB		Slab track with track fasteners that are very compliant in the vertical direction can reduce vibration at frequencies greater than 40 Hz.	



Table 10-1. Adjustment Factors for Generalized Predictions of Ground-Borne Vibration and Noise (Continued)

<i>Factors Affecting Vibration Path</i>				
Path Factor	Adjustment to Propagation Curve		Comment	
Resiliently Supported Ties	-10 dB		Resiliently supported tie systems have been found to provide very effective control of low-frequency vibration.	
<i>Track Configuration (not additive, apply greatest value only)</i>				
Type of Transit Structure	Relative to at-grade tie & ballast:		The general rule is the heavier the structure, the lower the vibration levels. Putting the track in cut may reduce the vibration levels slightly. Rock-based subways generate higher-frequency vibration.	
	Elevated structure	-10 dB		
	Open cut	0 dB		
	Relative to bored subway tunnel in soil:			
	Station	-5 dB		
	Cut and cover	-3 dB		
	Rock-based	-15 dB		
<i>Ground-borne Propagation Effects</i>				
Geologic conditions that promote efficient vibration propagation	Efficient propagation in soil		+10 dB	Refer to the text for guidance on identifying areas where efficient propagation is possible.
	Propagation in rock layer	<u>Dist.</u>	<u>Adjust.</u>	
		50 ft	+2 dB	
		100 ft	+4 dB	
150 ft	+6 dB			
	200 ft	+9 dB		
Coupling to building foundation	Wood Frame Houses		-5 dB	The general rule is the heavier the building construction, the greater the coupling loss.
	1-2 Story Masonry		-7 dB	
	3-4 Story Masonry		-10 dB	
	Large Masonry on Piles		-10 dB	
	Large Masonry on Spread Footings		-13 dB	
	Foundation in Rock		0 dB	
<i>Factors Affecting Vibration Receiver</i>				
Receiver Factor	Adjustment to Propagation Curve		Comment	
Floor-to-floor attenuation	1 to 5 floors above grade:		-2 dB/floor	This factor accounts for dispersion and attenuation of the vibration energy as it propagates through a building.
	5 to 10 floors above grade:		-1 dB/floor	
Amplification due to resonances of floors, walls, and ceilings			+6 dB	The actual amplification will vary greatly depending on the type of construction. The amplification is lower near the wall/floor and wall/ceiling intersections.
<i>Conversion to Ground-borne Noise</i>				
Noise Level in dBA	Peak frequency of ground vibration:		Use these adjustments to estimate the A-weighted sound level given the average vibration velocity level of the room surfaces. See text for guidelines for selecting low, typical or high frequency characteristics. Use the high-frequency adjustment for subway tunnels in rock or if the dominant frequencies of the vibration spectrum are known to be 60 Hz or greater.	
	Low frequency (<30 Hz):			-50 dB
	Typical (peak 30 to 60 Hz):			-35 dB
	High frequency (>60 Hz):			-20 dB

