



Site Servicing & Stormwater Management Report

2465070 Ontario Ltd.
2375 St-Laurent Blvd., Ottawa, ON

Prepared for:

Graebeck Construction Ltd.
160 Terence Matthews Crescent,
Kanata, ON
K2M 0B2

Attention: Mr. Evan Cory

LRL File No.: 130828

December 13, 2017



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1 INTRODUCTION

LRL Associates Ltd. (LRL) has been retained by Graebeck Construction Ltd. to prepare a site servicing and stormwater management report in support of their site plan control application for a proposed site development. This report presents the proposed servicing plan for the proposed development in regards to water and sanitary services, as well as stormwater management.

This report has been prepared in consideration of the survey carried out by Annis, O'Sullivan, Vollebekk Ltd. dated August 11th, 2017. Should there be any discrepancies in the existing infrastructure and/or connections to existing services, which may relate to site servicing considerations, LRL should be advised in order to review the report recommendations. This report should be read in conjunction with the Civil plans prepared by LRL.

2 SITE DESCRIPTION

The subject property is located within the suburban boundary of the City of Ottawa; Ward 10 Gloucester-Southgate, within the Greens Creek Study Area. The proposed development will be a motorsports warehouse, located at 2375 St-Laurent Blvd. The total area of the property is approximately 0.659 ha.

The proposed development is located in an industrial area bounded by other light industrial properties and a parks and open space zone to the south. The property is currently a virgin site.

The proposed development will include a two-storey warehouse/garage with office space. The total footprint area of the proposed main building is 930m². There will also be a future building addition of 1000m² which will be built at a later date. The service calculations take into account both the proposed building and the future expansion.

3 SCOPE OF WORK

As per applicable guidelines, the scope of work includes the following:

Water services

- Calculate the expected water supply demand at average and peak conditions.
- Calculate the fire flow as per the Fire Underwriter Survey (FUS) method.
- Describe the proposed water distribution network and connection to the existing system.

Sanitary services

- Describe the existing sanitary sewers available to receive wastewater from the building.
- Calculate peak allowable release flow rate for the subject site.
- Calculate peak actual release flow rate and compare to allowable release.
- Describe the proposed sanitary sewer system.



Stormwater management

- Calculate the allowable stormwater release rate.
- Calculate the anticipated post development stormwater release rates.
- Demonstrate how the target quality and quantity objectives will be achieved.
- Describe the proposed storm sewer system.

4 WATER SUPPLY AND FIRE PROTECTION

4.1 Existing Water Supply Services

An existing 300mm dia. watermain extending along St-Laurent Blvd. is present north of the subject property. From this watermain, a 200mm dia. water service extends into the subject site and is capped off just inside the property line at the northeast corner. There are two existing fire hydrants near the northeast and northwest corners of the property on St-Laurent Blvd. The subject site is located in Pressure Zone 2C. Please refer to Appendix H for the St-Laurent Blvd. As-Built Drawings.

4.2 Water Supply Demand

As per MOE and City of Ottawa Design Guidelines, the average water demand for the subject light industrial development was calculated. A daily and hourly peak factor of **1.5** and **1.8**, respectively were used. The average daily water demand for the site is **0.27L/s**, maximum daily is **0.40L/s**, and maximum hourly is **0.72L/s**. Please refer to Appendix A for the water demand calculation sheet.

The fire flow demand was estimated in accordance with the Fire Underwriters Survey (FUS). This method is based on the floor area of the building to be protected, type and combustibility of the structural frame and the separation distances with adjoining buildings. The fire flow demand was calculated to be **150.0L/s**. Please refer to Appendix A for the fire flow calculation sheet.

The City of Ottawa has provided boundary conditions to LRL Associates for this project. Please refer to Appendix I for boundary conditions. Using the provided HGLs, minimum, maximum and maximum day + fire pressures were calculated at the St-Laurent Blvd. connection. Head losses were then calculated from the connection to the proposed building for the maximum daily demand, maximum hourly demand and maximum daily demand + fire flow. For each of these scenarios, the relevant pressures were determined. Adequate water supply/pressure is available and meets the City of Ottawa standards as per section 4.2.2 of the Ottawa Design Guidelines – Water distribution. For the maximum daily demand, a minimum and maximum pressure of **60.89** and **69.57** psi were calculated; these land within the 50 to 80 psi MOE range.



For the maximum hourly demand, a minimum and maximum pressure of **60.63** and **69.31** psi were calculated; these land within the 40 to 80 psi MOE range. For the maximum daily demand + fire flow, a pressure of **57.33** psi was calculated; this is above the minimum 20 psi MOE requirement. A pressure reducing valve is not required based on the above analysis. Please refer to Appendix A for pressure loss calculations.

Summary Table	
Average Water Demand Rate	23065 L/day
Factors	1.5(max daily) & 1.8(max hourly)
Average Day Demand (L/s)	0.27
Maximum Daily Demand (L/s)	0.40
Peak Hour Demand (L/s)	0.72
FUS Fire Flow Requirement (L/s)	150.0
Max Day+Fire Flow (L/s)	150.4

4.3 Water supply servicing design

The proposed building will be serviced by a new 50mm dia. HDPE “Gold Stripe” water service; to be installed 2.4m below grade. The proposed service will connect to the existing 200mm dia. service stubbed at the property line; located at the northeast corner of the site. One 200mm x 100mm reducer and one 100mm x 50mm reducer will be installed to allow for the proposed water service.

Fire flow protection is to be provided by the existing fire hydrants located near the northeast and northwest corners of the property on St-Laurent Blvd. The existing northwest hydrant is located 40m from the proposed building’s front entrance.

5 SANITARY DRAINAGE

5.1 Existing Sanitary Sewer Services

An existing 300mm dia. sanitary sewer extending along St-Laurent Blvd. is present north of the subject property. Please refer to Appendix H for the St-Laurent Blvd. As-Built Drawings.

5.2 Sanitary Sewer Servicing Design

The new building, including the future addition, will be serviced with a new 150mm dia. sanitary service, which will connect to the existing 300mm dia. sanitary sewer on St-Laurent Blvd. A new monitoring manhole (SAN MH1) is to be installed along the proposed 150mm service; near the property line. The new proposed 150mm PVC sanitary service will be installed at a minimum slope of 1.0%, as per the City of Ottawa Sewer Design Guidelines.

The parameters used to calculate the site's allowable sanitary flows are: Light Industrial average flow demand of 35,000 L/ha/day, an industrial peaking factor of 7.25 (as per Appendix 4-B of the Ottawa Sewer Design Guidelines) and an infiltration rate of 0.28 L/s/ha. Based on these parameters and the total site area of 0.659 ha, the total allowable sanitary flow was estimated to be **2.12 L/s**. Refer to Appendix B for the site's sanitary sewer design sheet.

As per Table 8.2.1.3.B of the Ontario Building Code, the site's anticipated sanitary flow is **3,700 L/day (0.04 L/s)**. The proposed building and future addition will have 2 water closets and 12 loading bays. Under the "Warehouse" item: 2 water closets x 950 L/day = 1900 L/day and 12 loading bays x 150 L/day = 1800 L/day; for a total of 3,700 L/day (0.04 L/s).

The site's anticipated sanitary flow is lower than its allowable flow. The proposed sanitary service has been sized to accommodate the peak allowable flow.

6 STORMWATER MANAGEMENT

6.1 Existing Stormwater Infrastructure

An existing 1200mm dia. storm sewer extending along St-Laurent Blvd. is present north of the subject property. Please refer to Appendix H for the St-Laurent Blvd. As-Built Drawings.

6.2 Stormwater management Concept

The information below should be read in conjunction with LRL drawings C401 and C701, as well as Appendix C (the stormwater management design sheets). The pervious and impervious runoff coefficients have been increased by 25% for the 100yr event; as per the Ottawa Sewer Design Guidelines.

The pre-development 5yr allowable release rate has been calculated using a C coefficient of 0.5 as per the City Pre-Application Consultation Memo, a calculated time of concentration of 36 minutes using the FAA/Rational Method, a calculated intensity of 47.2mm/hr as per City of Ottawa guidelines, and a total site area of 0.659ha. The allowable release rate was calculated to be **29.98L/s**.

The post-development conditions (100 year storm event) were designed using a restricted release flow of **43.22L/s** using Hydrovex Vertical Vortex Flow Regulator model 150VHV-2 to be installed in proposed CBMH5.

The 100year storm runoff from proposed catchment areas CA-01 to CA-06 will be controlled at proposed CBMH5. Runoff above the 100year will back out of all proposed CBMHs and pond around each drainage structure until it flows overland, making its way to St-Laurent Blvd. through the spill out point located at the northeast side of the entrance at the property line. Stormwater will not back up through the system and make its way out of CB1 (located at the bottom of the loading dock area) due to a proposed Armtec flap gate to be installed on the CB's



south inlet. Stormwater from the 5yr storm event will always remain underground; it will never back up/out of the drainage structures and pond overland.

The 100yr storage required for this site is **219.82m³**. The 100yr storage provided is **222.41m³**. This is a combination of the overland ponding storage of 62.78m³ (refer to Appendix J for the Overland Ponding Volume Table), StormTech chambers storage of 133.00m³ (refer to Appendix E for StormTech System Design Sheets) and the underground pipes and drainage structures storage of 26.63m³. This storage capacity will be possible using a Hydrovex Vertical Vortex Flow Regulator model 150VHV-2 to be installed in proposed CBMH5 at an allowable release rate of **43.22L/s**. Refer to Appendix D for Hydrovex Vertical Vortex Flow Regulator Report.

6.3 Design Criteria

Stormwater quantity and quality control measures are taken into account for this site to reduce post development stormwater runoff to allowable levels.

6.3.1 Water Quality

The enhanced 80% TSS removals requirement will be met through the proposed Stormceptor STC 300 oil/grit separator which will provide adequate water quality treatment. Please refer to Appendix F for the Stormceptor Report. An isolator row has been incorporated into the StormTech system as well providing additional on-site quality treatment.

6.3.2 Water Quantity

All storm events up to and including the 100 year event will be controlled to the 5 year pre-development level. The site's major overland flow route has been designed to ensure that storm events beyond the 100 year design storm can be safely conveyed overland towards the St-Laurent Blvd. right of way. The minor system (the on-site storm sewer system) is sized to convey the 5 year storm event flows from the site to the municipal storm sewer on St-Laurent Blvd.

6.4 Method of Analysis

The Rational Method was used to calculate the runoff from the development. The Intensity-Duration-Frequency (IDF) curve formulas of the MacDonald Cartier International Airport, City of Ottawa, were used to calculate the peak storm flows.

6.5 Allowable Release Rate

The pre-development 5yr allowable release rate has been calculated using a C coefficient of 0.5 as per the City Pre-Application Consultation Memo, a calculated time of concentration of 36

minutes using the FAA/Rational Method, a calculated intensity of 47.2mm/hr as per City of Ottawa guidelines, and a total site area of 0.659ha.

7 EROSION AND SEDIMENT CONTROL

During construction, erosion and sediment controls will be provided primarily via a sediment control fence to be erected along the perimeter of the site where runoff has the potential of leaving the site. Inlet sediment control devices are also to be provided in any catchbasin and/or manhole in and around the site that may be impacted by the site construction. Construction and maintenance requirements for erosion and sediment controls are to comply with Ontario Provincial Standard Specification (OPSS) # 577. Refer to LRL drawing C.101 for erosion and sediment control details.

8 CONCLUSIONS

In accordance with the report objectives, the analyses of the proposed development can be summarized as follows:

Water Service

- The anticipated maximum domestic water demand of the site is 0.72L/s.
- The maximum required fire flow was calculated at 150.0L/s using the FUS method.
- There are two existing fire hydrants located near the northeast and northwest corners of the property on St-Laurent Blvd. within a 90m radius. The existing northwest hydrant is located 40m from the proposed building's front entrance.
- The new development will be serviced with by a new 150mm dia. water service connected to the existing 200mm dia. service stubbed at the property line; located at the northeast corner of the site.

Sanitary Service

- The total allowable sanitary flow was estimated to be 2.12 L/s.
- The site's anticipated sanitary flow is 0.04 L/s.
- The proposed building will be serviced by a new 150mm sanitary service which will be connected to the existing 300mm dia. sanitary sewer on St-Laurent Blvd.
- A new monitoring manhole will be installed on the proposed 150mm sanitary service.

Stormwater Management

- The proposed storm system's 100yr post-development release rate of 43.22 L/s will meet the 5yr pre-development allowable release rate of 43.22 L/s.
- Stormwater quantity control objectives will be met through on-site stormwater storage.



- Stormwater quality control objectives will be met on-site through the use of a Stormceptor STC 300 oil/grit separator. An isolator row has been incorporated into the StormTech system as well providing additional on-site quality treatment.

9 LIMITATIONS AND USE OF REPORT

The report conclusions are applicable only to the project described in the report. Any changes require a review by LRL Associates Ltd. to insure compatibility with the recommendations contained in this report. We trust the information presented in this report meets City of Ottawa requirements. Please do not hesitate to contact us should you have any questions or concerns.

Prepared by:

LRL Associates Ltd.



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APPENDIX A

**Water Demand and Fire Flow
Calculations**



Water Service Calculations

LRL File No. : 170721
Project : 2465070 Ontario Ltd
Date : December 13, 2017
Designed by : Guillaume Courtois

Water Demand

Total site area: 0.659 ha

$$Q_{average} = \boxed{35} m^3 / ha \cdot day \quad (\text{As per MOE guidelines})$$

$$Q_{average} = 23.065 m^3 / day$$

$$Q_{average} = 23065 L / day$$

$$Q_{average} = 0.27 L / s$$

Maximum daily peak factor: 1.5

$$\begin{aligned} \text{Maximum daily demand} &= 34598 L / day \\ &= 0.40 L / s \end{aligned}$$

Maximum hour peak factor: 1.8

$$\begin{aligned} \text{Maximum hour demand} &= 62276 L / day \\ &= 0.72 L / s \end{aligned}$$

Water Service Pipe Sizing

$$Q = VA$$

Where: V = velocity

A = area of watermain pipe

Q = water supply flow rate

By deriving the above formula, we can obtain the diameter of the pipe:

Minimum pipe diameter: $d = (4Q/\pi V)^{1/2}$

$$d = 0.023 \text{ m}$$

$$d = 23 \text{ mm}$$

Proposed pipe diameter: 50 mm (I.D. = 41mm)



Fire Flow Calculations

LRL File No. : 170721
Project : 2465070 Ontario Ltd
Date : December 13, 2017
Method : Fire Underwriters Survey (FUS)
Designed by : Guillaume Courtois

Step	Task	Term	Options	Multiplier	Choose:	Value	unit	Fire Flow
Structural Framing Material								
1	Choose frame used for building	Coefficient C related to the type of construction	Wood Frame Ordinary Construction Non-combustible construction Fire resistive construction <2 hrs Fire resistive construction >2 hrs	1.5 1.0 0.8 0.7 0.6	Non-combustible construction	0.8		
Floor Space Area								
2	Choose type of housing	Type of housing	Single family dwelling Townhouse - no. of units Building - no. of units per floor	0 0 1	Building - no. of units per floor	1	unit(s)	
3	Enter area of a unit	Enter floor space area of one unit (excluding basement)		1	1930.0		sq.m.	
4	Obtain fire flow before reductions	Required fire flow	$\text{Fire Flow} = 220 \times C \times \text{Area}^{0.5}$					
Reductions or surcharge due to factors affecting burning								
5	Choose combustibility of contents	Occupancy hazard reduction or surcharge	Non-combustible Limited combustible Combustible Free burning Rapid burning	-0.25 -0.15 0 0.15 0.25	Combustible	0		
6	Choose reduction for sprinklers	Sprinkler reduction	Sprinklers (NFPA13) Water supply is standard for both the system and fire department hose lines Fully supervised system	-0.30 -0.10 -0.10	False	0		
7	Choose separation	Exposure distance between units	North side East side South side West side	Over 45m 10.1 to 20m Over 45m Over 45m	0 0.15 0 0		L/min L/s	8,000 133.3
Net required fire flow								
8	Obtain fire flow, duration, and volume		Minimum required fire flow rate (rounded to nearest 1000)					
			Minimum required fire flow rate					
			Required duration of fire flow					

Note: The above calculations take into account both the current proposed building of 930m² and the future proposed building of 1000m².



Pipe Pressure Losses Calculations

LRL File No. : 170721
Project : 2465070 Ontario Ltd
Date : December 13, 2017
Designed : Guillaume Courtois

Piezometric Head Equation (Derived from Bernoulli's Equation)

$$h = \frac{p}{\gamma} + z$$

Where:

h = HGL (m)	
p = Pressure (Pa)	
γ = Specific weight (N/m ³) =	9810
z = Elevation of centreline of pipe (m) =	80.91

Water Pressure at St-Laurent Blvd. Connection			
HGL (m)	Pressure		
	kPa	psi	
Minimum =	124.5	427.62	62.02
Maximum =	130.6	487.46	70.70
Max. Day + Fire =	124	422.71	61.31

Hazen Williams Equation

$$h_f = \frac{10.67 \times Q^{1.85} \times L}{C^{1.85} \times d^{4.87}}$$

Where:

h_f = Head loss over the length of pipe (m)
 Q = Volumetric flow rate (m³/s)
 L = Length of pipe (m)
 C = Pipe roughness coefficient
 d = Pipe diameter (m)

Scenario 1: maximum daily demand

Q (L/s)	0.40	
C	150	
L (m.)	31.5	
I.D. (mm)	41	
V (m/s)	0.30	
h_f (m)	0.09	
Head Loss (psi)	0.13	
Min. Pressure (psi)	61.89	
Max. Pressure (psi)	70.57	
Service Obv. @ Street Connection (m)	81.10	
Service Obv. @ Building Connection (m)	81.80	
Pressure Adjustment (psi)	-1.00	(due to service elevation difference from street to building)
Adjusted Min. Pressure (psi)	60.89	(must not be less than 50psi)
Adjusted Max. Pressure (psi)	69.57	(must not be more than 80psi)

Scenario 2: maximum hourly demand

Q (L/s)	0.72	
C	150	
L (m.)	31.5	
I.D. (mm)	41	
V (m/s)	0.55	
h_f (m)	0.28	
Head Loss (psi)	0.39	
Min. Pressure (psi)	61.63	
Max. Pressure (psi)	70.31	
Service Obv. @ Street Connection (m)	81.10	
Service Obv. @ Building Connection (m)	81.80	
Pressure Adjustment (psi)	-1.00	(due to service elevation difference from street to building)
Adjusted Min. Pressure (psi)	60.63	(must not be less than 40psi)
Adjusted Max. Pressure (psi)	69.31	(must not be more than 80psi)

Scenario 3: maximum daily demand + fire flow (from street connection to hydrant at northwest of site)

Q (L/s)	150.40	
C	150	
L (m.)	9.3	
I.D. (mm)	155	
V (m/s)	7.97	
h_f (m)	2.47	
Head Loss (psi)	3.51	
Pressure (psi)	57.80	
Service Obv. @ Street Connection (m)	81.12	
Service Obv. @ Hydrant Connection (m)	81.45	
Pressure Adjustment (psi)	-0.47	(due to service elevation difference from street to hydrant)
Adjusted Pressure (psi)	57.33	(must not be less than 20psi)

APPENDIX B
Sanitary Sewer Calculation Sheet



LRL File No. 170721
 Project: 2465070 Ontario Ltd
 Location: 2375 St-Laurent Blvd., Ottawa, ON
 Date: December 13, 2017

Average Daily Flow = 350 L/p/day
 Commercial & Institutional Flow = 50000 L/ha/day
 Light Industrial Flow = 35000 L/ha/day
 Heavy Industrial Flow = 55000 L/ha/day
 Maximum Residential Peak Factor = 4.0
 Commercial & Institutional Peak Factor = 1.5

Sanitary Design Parameters

Industrial Peak Factor = as per Appendix 4-B = 7.25
 Extraneous Flow = 0.28 L/s/gross ha

Pipe Design Parameters

Minimum Velocity = 0.60 m/s
 Manning's n = 0.013

LOCATION			RESIDENTIAL AREA AND POPULATION						COMMERCIAL		INDUSTRIAL		INSTITUTIONAL		C+I+I	INFILTRATION			TOTAL FLOW (l/s)	PIPE				MANHOLE					
CATCHMENT / STREET	FROM MH	TO MH	AREA (Ha)	POP.	CUMMULATIVE		PEAK FACT.	PEAK FLOW (l/s)	AREA (Ha)	ACCU. AREA (Ha)	PEAK FACT.	AREA (Ha)	ACCU. AREA (Ha)	PEAK FLOW (l/s)	TOTAL AREA (Ha)	ACCU. AREA (Ha)	INFILT. FLOW (l/s)	LENGTH (m)	DIA. (mm)	SLOPE (%)	MATERAIL	CAP. (FULL) (l/s)	VEL. (FULL) (m/s)	Ratio (Q/Q _{FULL})	UP INVERT (m)	DOWN INVERT (m)			
					AREA (Ha)	POP.																							
Site	Bldg	MH01	0.000	0.0	0.0	0.0	4.0	0.00	0.000	0.000	0.659	0.659	7.25	0.0	0.0	1.94	0.659	0.659	0.18	2.12	18.3	150	1.00%	PVC	15.23	0.86	0.14		
	MH01	TRUNK	0.000	0.0	0.0	0.0	4.0	0.00	0.000	0.000	0.000	0.659	7.25	0.0	0.0	1.94	0.000	0.659	0.18	2.12	16.8	150	1.00%	PVC	15.23	0.86	0.14		
NOTES															Designed:		PROJECT:										2465070 Ontario Ltd		
Existing invert and slopes are estimated. They are to be confirmed on-site.															Checked:		LOCATION:										2375 St-Laurent Blvd., Ottawa, ON		
															Dwg. Reference:		File Ref.:		Date:		Sheet No.		1 of 1						
															C.401		170721		December 13, 2017										

APPENDIX C
Stormwater Management Design Sheets

LRL Associates Ltd.

Storm Design Sheet



LRL File No. 170721
Project: 2465070 Ontario Ltd
Location: 2375 St-Laurent, Ottawa, ON
Date: 13 Dec 2017
Designed: Guillaume Courtois
Drawing Reference: C701

Post-development Catchments

CATCHMENT	Grass C=0.20	Gravel C=0.80	Bldg. / Asph. / Conc. C=0.90	Total Area (ha)	Combined C
CA-01	0.054	0.000	0.303	0.357	0.79
CA-02	0.000	0.000	0.012	0.012	0.90
CA-03	0.007	0.000	0.097	0.104	0.85
CA-04	0.019	0.000	0.034	0.053	0.65
CA-05	0.021	0.000	0.058	0.079	0.71
CA-06	0.010	0.000	0.044	0.054	0.77



LRL File No. 170721
Project: 2465070 Ontario Ltd
Location: 2375 St-Laurent, Ottawa, ON
Date: 13 Dec 2017
Designed: Guillaume Courtois
Drawing Ref.: C701

**Stormwater Management
Design Sheet**

Allowable Release Rate (5 Year Pre-development)

Time of Concentration:

$$Tc = \frac{G(1.1 - c)L^{0.5}}{(100 \times S)^{1/3}}$$

as per FAA/Rational Method Equation

where: C =	0.5	Runoff Coefficient as per City pre-consultation application memo
G =	3.26	Constant
L =	137.65	Longest watercourse length (in meters) in watershed
S =	0.0025	Average slope of watercourse
Tc =	36	min

Intensity:

$$I_5 = \frac{998.071}{(Tc + 6.053)}^{0.814}$$

as per City of Ottawa Guidelines

where: Tc =	36	Time of Concentration in min.
I₅ =	47.2	mm/hr

Allowable Release:

$$Q = 2.78 \times C \times I \times A$$

where: C =	0.5	Runoff Coefficient as per City pre-consultation application memo
I =	47.2	mm/hr
Tc =	36	min
Total Site Area =	0.659	ha
Q =	43.22	L/s

Catchment Area and Runoff Coeffecient (Post-development)

Individual Watersheds	Total Area (ha)	Grass Area (ha)	Gravel Area (ha)	Bldg. / Asph. / Conc. Area (ha)	$\Sigma C * A$	C weighted (1:5 yr)	C weighted (1:100 yr)	
Controlled	CA-1	0.357	0.054	0.000	0.303	0.284	0.79	0.99
	CA-2	0.012	0.000	0.000	0.012	0.011	0.90	1.00
	CA-3	0.104	0.007	0.000	0.097	0.089	0.85	1.00
	CA-4	0.053	0.019	0.000	0.034	0.034	0.65	0.81
	CA-5	0.079	0.021	0.000	0.058	0.056	0.71	0.89
	CA-6	0.054	0.010	0.000	0.044	0.042	0.77	0.96

					1:5 YEAR	1:100 YEAR
Controlled	Total Site Area =	0.659	ha	$\Sigma C =$	0.78	0.98
	Bldg. / Asph. / Conc. Area =	0.548	ha	C =	0.90	1.00
	Gravel Area =	0.000	ha	C =	0.80	1.00
	Grass Area =	0.111	ha	C =	0.20	0.25
Total Controlled =		0.659	ha	$\Sigma C =$	0.78	0.98



LRL File No. 170721
Project: 2465070 Ontario Ltd
Location: 2375 St-Laurent, Ottawa, ON
Date: 13 Dec 2017
Designed: Guillaume Courtois
Drawing Ref.: C701

**Stormwater Management
Design Sheet**

Post-development Stormwater Management

5 Year Post-development:

$$I_5 = 998.071 / (Tc + 6.053)^{0.814}$$

where: I = intensity in mm/hr
Tc = Time of Concentration

1:5 YEAR STORM EVENT

Time (min)	Intensity (mm/hr)	Peak Flow (L/s)	Release Rate (L/s)	Storage Rate (L/s)	Storage Volume (m³)
10	104.2	149.29	43.22	106.07	63.64
15	83.6	119.72	43.22	76.50	68.85
20	70.3	100.66	43.22	57.43	68.92
25	60.9	87.25	43.22	44.03	66.05
30	53.9	77.27	43.22	34.05	61.28
35	48.5	69.52	43.22	26.29	55.22
40	44.2	63.31	43.22	20.09	48.21
45	40.6	58.21	43.22	14.99	40.48
50	37.7	53.95	43.22	10.73	32.18
55	35.1	50.33	43.22	7.10	23.44
60	32.9	47.20	43.22	3.98	14.33

100 Year Post-development:

Intensity:

$$I_{100} = 1735.688 / (Tc + 6.014)^{0.820}$$

where: I = intensity in mm/hr
Tc = Time of Concentration

1:100 YEAR STORM EVENT

Time (min)	Intensity (mm/hr)	Peak Flow (L/s)	Release Rate (L/s)	Storage Rate (L/s)	Storage Volume (m³)
10	178.6	319.80	43.22	276.58	165.95
15	142.9	255.93	43.22	212.70	191.43
20	120.0	214.83	43.22	171.61	205.93
25	103.8	185.99	43.22	142.77	214.15
30	91.9	164.54	43.22	121.32	218.37
35	82.6	147.90	43.22	104.68	219.82
40	75.1	134.59	43.22	91.36	219.27
45	69.1	123.67	43.22	80.45	217.21
50	64.0	114.54	43.22	71.32	213.96
55	59.6	106.79	43.22	63.57	209.76
60	55.9	100.11	43.22	56.89	204.79

Onsite Stormwater Retention

Total Storage Required = 219.82 m³

Overland Ponding Storage = 62.78 m³ refer to LRL Plan C601

Pipe Storage = 11.61 m³

Drainage Structures Storage = 15.02 m³

Stormtech Chambers Storage = 133.00 m³ refer to LRL Plan C902

Total Available Storage = 222.41 m³

Supplementary Storage Required = 0.00 m³

LRL Associates Ltd.
Storm Design Sheet

Project Information								Storm Design Parameters												Pipe Design Parameters			
 <p>LRL ENGINEERING INGÉNIERIE</p>			LRL File No. 170721 Project: 2465070 Ontario Ltd Location: 2375 St-Laurent, Ottawa, ON Date: 13 Dec 2017 Designed: Guillaume Courtois Drawing Reference: C701		Rational Method $Q = 2.78CIA$ Q = Peak flow in litres per second (L/s) A = Drainage area in hectares (ha) C = Runoff coefficient I = Rainfall intensity (mm/hr)				Runoff Coefficient (C) Grass 0.2 Gravel 0.8 Bldg. / Asph. / Conc. 0.9				IDF Curve Ottawa Macdonald-Cartier International Airport Storm Event 5 years Formula $I = a / (T_c + b)^c$ a = 998.07 b = 6.053 c = 0.814				Minimum velocity = 0.80 m/s Maximum velocity = 3.00 m/s Manning's Coeff. "n" = 0.013						

LOCATION			AREA (ha)			FLOW						STORM SEWER								MANHOLE						WATERSHED		AVAILABLE STORAGE					
CATCHMENT / STREET	From Structure	To Structure	Grass C=0.20	Gravel C=0.80	Bldg./Asph./Conc. C=0.90	Indiv. 2.78AC	Accum. 2.78AC	Time of Conc. (min.)	Rainfall Intensity (mm/hr)	Peak Flow Q (L/s)	ICD Controlled Flow Q (L/s)	Pipe Diameter (mm)	Type	Slope (%)	Length (m)	Capacity Full (L/s)	Spare Capacity (L/s)	Velocity Full (m/s)	Time of Flow (min.)	Ratio (Q/Q _{FULL})	Up Invert (m)	Down Invert (m)	T/G Up Stream (m)	T/G Down Stream (m)	Up Depth obv (m)	Down Depth obv (m)	Up Depth inv (m)	Total Area (ha)	Combined C	Pipe Storage (m ³)	Upstream CB/MH Size (m)	Water Depth (m)	CB/MH Storage (m ³)
CA-01	CBMH1	CBMH2	0.054	0.000	0.303	0.79	0.79	36.43	47.2	37.19		300	PVC	0.34%	45.0	56.39	19.20	0.80	0.94	0.66	80.95	80.80	83.25	83.30	2.00	2.20	2.30	0.357	0.79	3.18	1.20	2.30	2.60
CA-02	CB1	CBMH2	0.000	0.000	0.012	0.03	0.03	36.43	47.2	1.42		200	PVC	1.00%	16.0	32.80	31.38	1.04	0.26	0.04	81.03	80.87	82.93	83.30	1.70	2.23	1.90	0.012	0.90	0.50	0.60	1.90	0.68
CA-03	CBMH2	CBMH5	0.007	0.000	0.097	0.25	1.06	37.37	46.4	49.35		300	PVC	1.19%	28.5	105.49	56.14	1.49	0.32	0.47	80.77	80.43	83.30	83.30	2.23	2.57	2.53	0.104	0.85	2.01	1.20	2.53	2.86
CA-04	CBMH3	CBMH4	0.019	0.000	0.034	0.10	0.10	36.43	47.2	4.51		300	PVC	0.34%	63.2	56.39	51.87	0.80	1.32	0.08	80.95	80.74	83.25	83.30	2.00	2.26	2.30	0.053	0.65	4.47	1.20	2.30	2.60
CA-05	CBMH4	CBMH5	0.021	0.000	0.058	0.16	0.25	37.75	46.0	11.62		300	PVC	1.23%	20.4	107.25	95.63	1.52	0.22	0.11	80.68	80.43	83.30	83.30	2.32	2.57	2.62	0.079	0.71	1.44	1.20	2.62	2.96
CA-06	CBMH5	STC300	0.010	0.000	0.044	0.12	1.43	37.97	45.8	65.67	43.22	300	PVC	4.00%	5.0	193.40	150.18	2.74	0.03	0.22	80.37	80.17	83.30	83.54	2.63	3.07	2.93	0.054	0.77	N/A	1.20	2.93	3.31
	STC300	EX. MH	0.000	0.000	0.000	0.00	1.43	38.00	45.8	65.63	43.22	300	PVC	0.34%	16.3	56.39	13.16	0.80	0.34	0.77	80.10	80.04	83.54	83.37	3.14	3.03	3.44	N/A	N/A	N/A	N/A	N/A	N/A

11.61

15.02

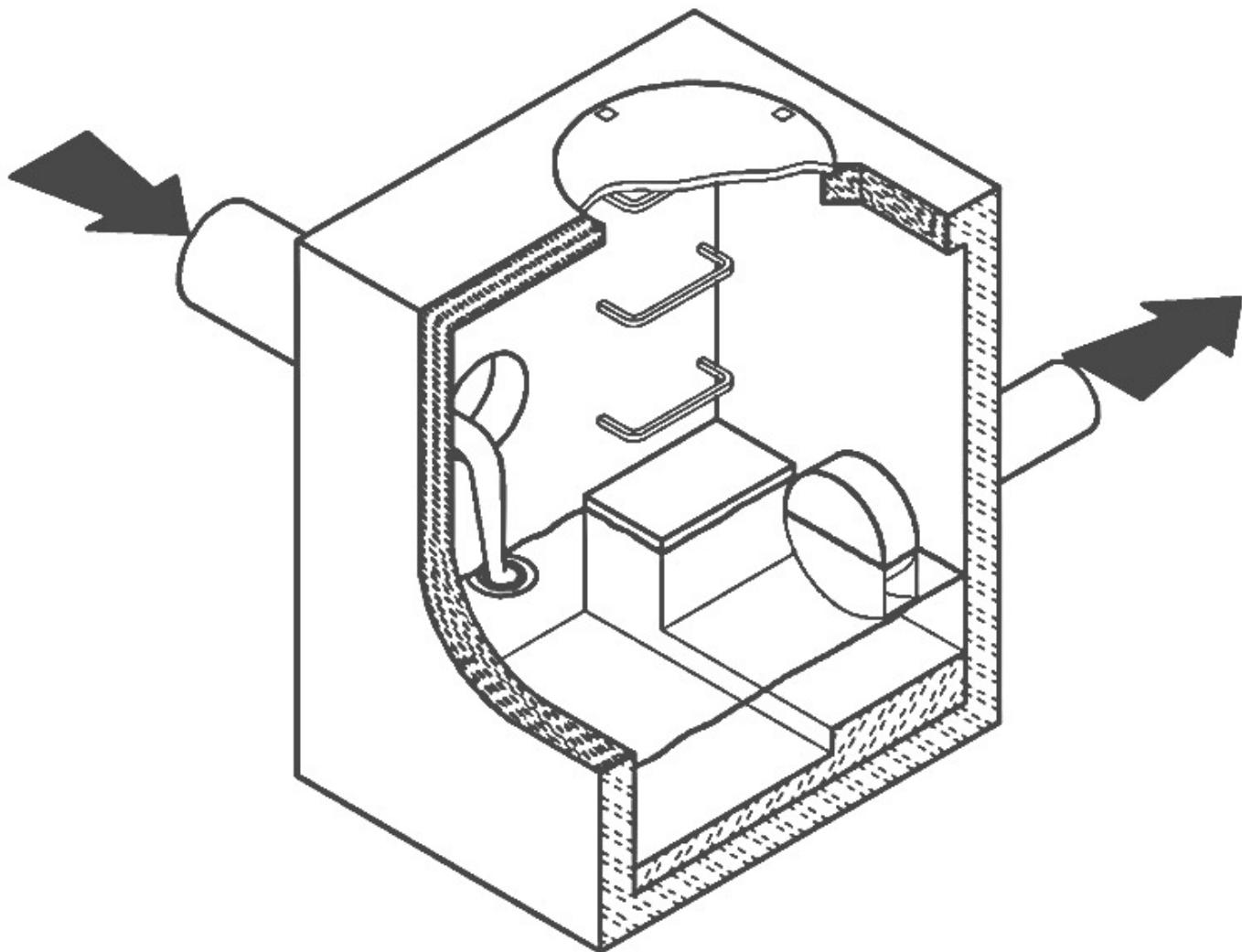
HWL	83.47
Total Storage	26.63

APPENDIX D
Hydrovex Vertical Vortex Flow Regulator Report

CSO/STORMWATER MANAGEMENT



HYDROVEX® VHV / SVHV
Vertical Vortex Flow Regulator



JOHN MEUNIER

HYDROVEX® VHV / SVHV VERTICAL VORTEX FLOW REGULATOR

APPLICATIONS

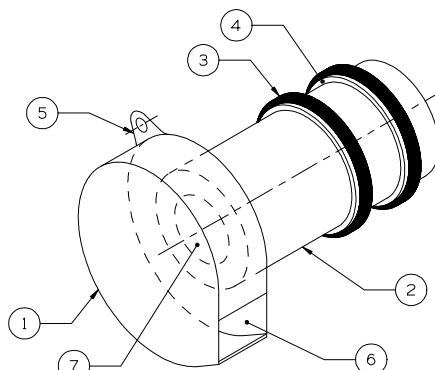
One of the major problems of urban wet weather flow management is the runoff generated after a heavy rainfall. During a storm, uncontrolled flows may overload the drainage system and cause flooding. Due to increased velocities, sewer pipe wear is increased dramatically and results in network deterioration. In a combined sewer system, the wastewater treatment plant may also experience significant increases in flows during storms, thereby losing its treatment efficiency.

A simple means of controlling excessive water runoff is by controlling excessive flows at their origin (manholes). **John Meunier Inc.** manufactures the **HYDROVEX® VHV / SVHV** line of vortex flow regulators to control stormwater flows in sewer networks, as well as manholes.

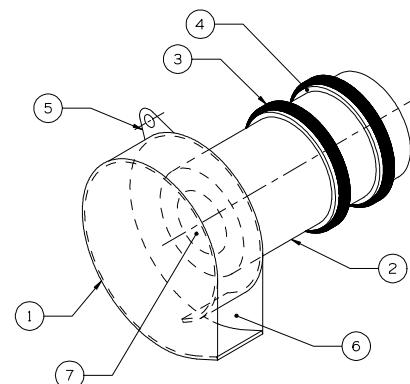
The vortex flow regulator design is based on the fluid mechanics principle of the forced vortex. This grants flow regulation without any moving parts, thus reducing maintenance. The operation of the regulator, depending on the upstream head and discharge, switches between orifice flow (gravity flow) and vortex flow. Although the concept is quite simple, over 12 years of research have been carried out in order to get a high performance.

The **HYDROVEX® VHV / SVHV** Vertical Vortex Flow Regulators (**refer to Figure 1**) are manufactured entirely of stainless steel, and consist of a hollow body (1) (in which flow control takes place) and an outlet orifice (7). Two rubber "O" rings (3) seal and retain the unit inside the outlet pipe. Two stainless steel retaining rings (4) are welded on the outlet sleeve to ensure that there is no shifting of the "O" rings during installation and use.

- 1. BODY
- 2. SLEEVE
- 3. O-RING
- 4. RETAINING RINGS
(SQUARE BAR)
- 5. ANCHOR PLATE
- 6. INLET
- 7. OUTLET ORIFICE



VHV



SVHV

FIGURE 1: HYDROVEX® VHV-SVHV VERTICAL VORTREX FLOW REGULATORS

ADVANTAGES

- The **HYDROVEX® VHV / SVHV** line of flow regulators are manufactured entirely of stainless steel, making them durable and corrosion resistant.
- Having no moving parts, they require minimal maintenance.
- The geometry of the **HYDROVEX® VHV / SVHV** flow regulators allows a control equal to an orifice plate, having a cross section area 4 to 6 times smaller. This decreases the chance of blockage of the regulator, due to sediments and debris found in stormwater flows. **Figure 2** illustrates the comparison between a regulator model 100 SVHV-2 and an equivalent orifice plate. One can see that for the same height of water, the regulator controls a flow approximately four times smaller than an equivalent orifice plate.
- Installation of the **HYDROVEX® VHV / SVHV** flow regulators is quick and straightforward and is performed after all civil works are completed.
- Installation requires no special tools or equipment and may be carried out by any contractor.
- Installation may be carried out in existing structures.

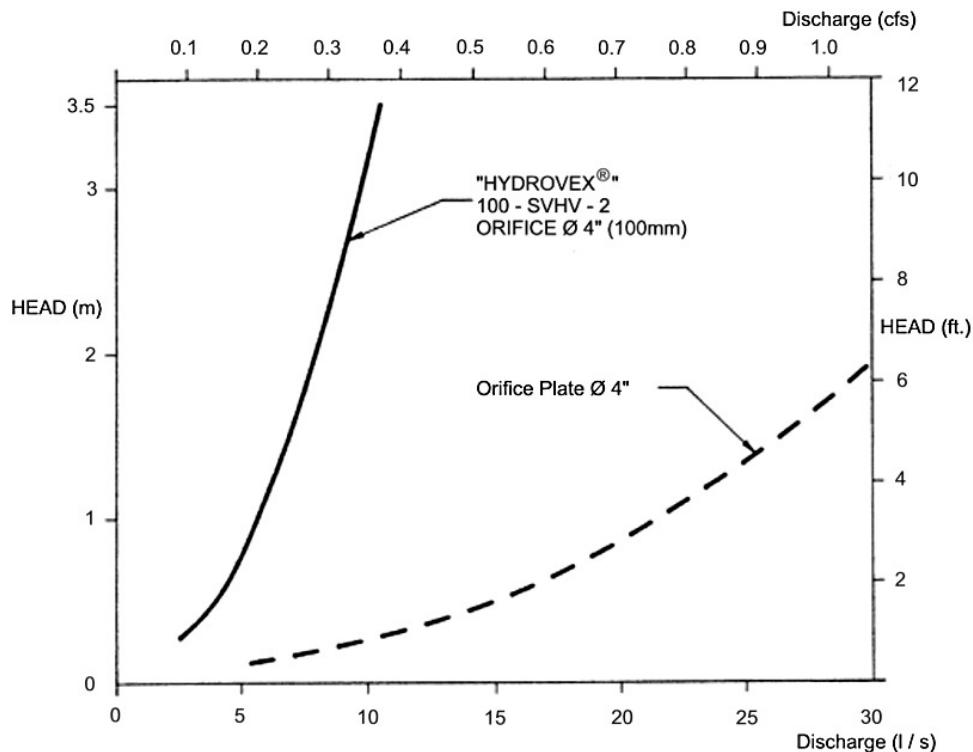


FIGURE 2: DISCHARGE CURVE SHOWING A HYDROVEX® FLOW REGULATOR VS AN ORIFICE PLATE

SELECTION

Selection of a **VHV** or **SVHV** regulator can be easily made using the selection charts found at the back of this brochure (see **Figure 3**). These charts are a graphical representation of the maximum upstream water pressure (head) and the maximum discharge at the manhole outlet. The maximum design head is the difference between the maximum upstream water level and the invert of the outlet pipe. All selections should be verified by John Meunier Inc. personnel prior to fabrication.

Example:

- ✓ Maximum design head 2m (6.56 ft.)
- ✓ Maximum discharge 6 L/s (0.2 cfs)
- ✓ Using **Figure 3 - VHV** model required is a **75 VHV-1**

INSTALLATION REQUIREMENTS

All **HYDROVEX® VHV / SVHV** flow regulators can be installed in circular or square manholes. **Figure 4** gives the various minimum dimensions required for a given regulator. ***It is imperative to respect the minimum clearances shown to ensure easy installation and proper functioning of the regulator.***

SPECIFICATIONS

In order to specify a **HYDROVEX®** regulator, the following parameters must be defined:

- The model number (ex: 75-VHV-1)
- The diameter and type of outlet pipe (ex: 6" diam. SDR 35)
- The desired discharge (ex: 6 l/s or 0.21 CFS)
- The upstream head (ex: 2 m or 6.56 ft.) *
- The manhole diameter (ex: 36" diam.)
- The minimum clearance "H" (ex: 10 inches)
- The material type (ex: 304 s/s, 11 Ga. standard)

* *Upstream head is defined as the difference in elevation between the maximum upstream water level and the invert of the outlet pipe where the HYDROVEX® flow regulator is to be installed.*

PLEASE NOTE THAT WHEN REQUESTING A PROPOSAL, WE SIMPLY REQUIRE THAT YOU PROVIDE US WITH THE FOLLOWING:

- *project design flow rate*
- *pressure head*
- *chamber's outlet pipe diameter and type*



Typical VHV model in factory

OPTIONS



VHV-1-O (standard model with odour control inlet)



FV - SVHV (mounted on sliding plate)



FV - VHV-O (mounted on sliding plate with odour control inlet)



VHV with Gooseneck assembly in existing chamber without minimum release at the bottom



VHV with air vent for minimal slopes



VHV Vertical Vortex Flow Regulator

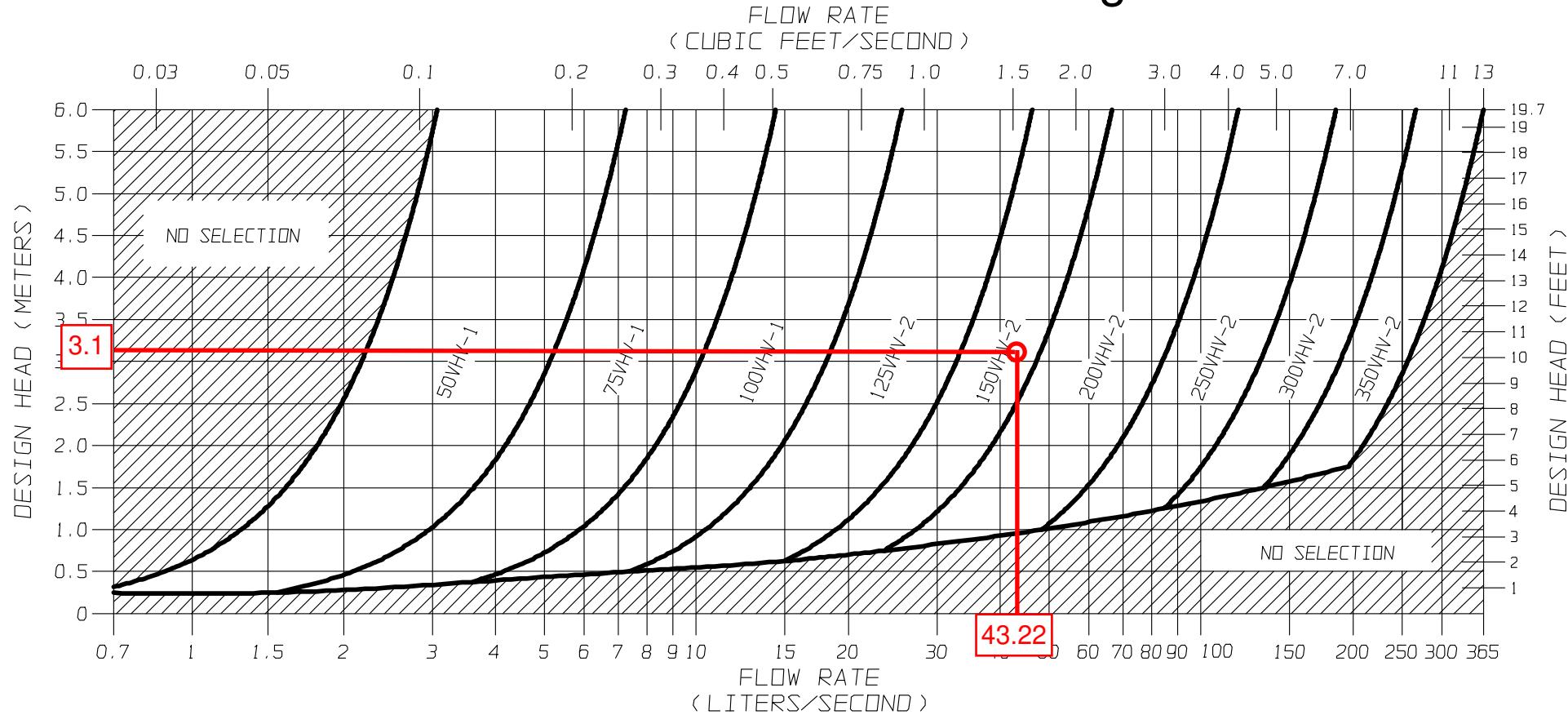
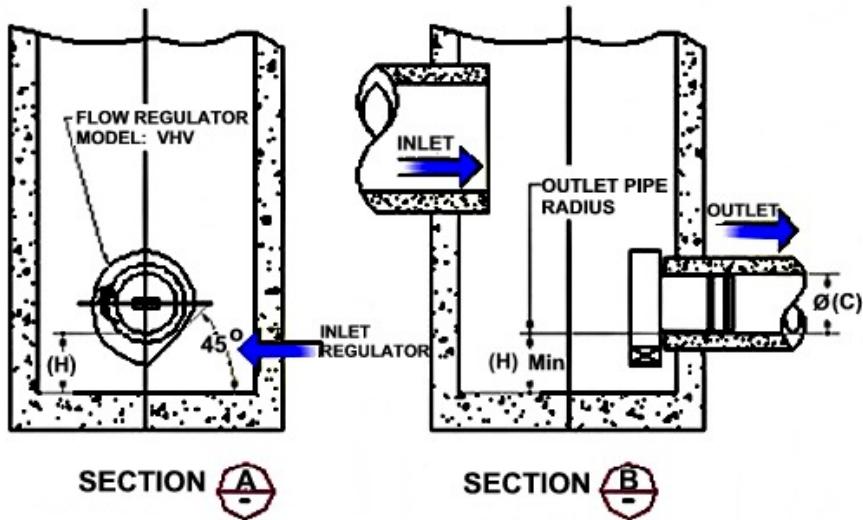
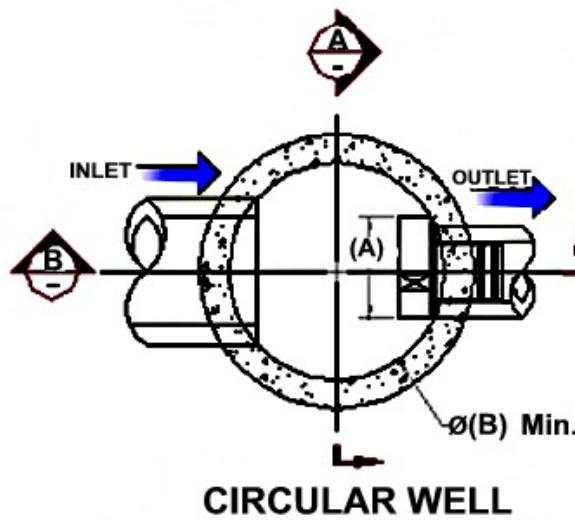


FIGURE 3 - VHV

JOHN MEUNIER

FLOW REGULATOR TYPICAL INSTALLATION IN CIRCULAR MANHOLE
FIGURE 4 (MODEL VHV)

Model Number	Regulator Diameter		Minimum Manhole Diameter		Minimum Outlet Pipe Diameter		Minimum Clearance	
	A (mm)	A (in.)	B (mm)	B (in.)	C (mm)	C (in.)	H (mm)	H (in.)
50VHV-1	150	6	600	24	150	6	150	6
75VHV-1	250	10	600	24	150	6	150	6
100VHV-1	325	13	900	36	150	6	200	8
125VHV-2	275	11	900	36	150	6	200	8
150VHV-2	350	14	900	36	150	6	225	9
200VHV-2	450	18	1200	48	200	8	300	12
250VHV-2	575	23	1200	48	250	10	350	14
300VHV-2	675	27	1600	64	250	10	400	16
350VHV-2	800	32	1800	72	300	12	500	20



INSTALLATION

The installation of a **HYDROVEX®** regulator may be undertaken once the manhole and piping is in place. Installation consists of simply fitting the regulator into the outlet pipe of the manhole. **John Meunier Inc.** recommends the use of a lubricant on the outlet pipe, in order to facilitate the insertion and orientation of the flow controller.

MAINTENANCE

HYDROVEX® regulators are manufactured in such a way as to be maintenance free; however, a periodic inspection (every 3-6 months) is suggested in order to ensure that neither the inlet nor the outlet has become blocked with debris. The manhole should undergo periodically, particularly after major storms, inspection and cleaning as established by the municipality

GUARANTY

The **HYDROVEX®** line of **VHV / SVHV** regulators are guaranteed against both design and manufacturing defects for a period of 5 years. Should a unit be defective, **John Meunier Inc.** is solely responsible for either modification or replacement of the unit.

John Meunier Inc.

ISO 9001 : 2008

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Glenside, PA USA 19038
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Fax: 215-885-4741 asteale@johnmeunier.com



APPENDIX E
StormTech System Design Sheets



ADVANCED DRAINAGE SYSTEMS, INC.



2465070 ONTARIO LTD

2375 ST-LAURENT BLVD., OTTAWA, ON

STORMTECH CHAMBER SPECIFICATIONS

1. CHAMBERS SHALL BE STORMTECH MC-3500 OR APPROVED EQUAL.
2. CHAMBERS SHALL BE MADE FROM VIRGIN, IMPACT-MODIFIED POLYPROPYLENE COPOLYMERS.
3. CHAMBER ROWS SHALL PROVIDE CONTINUOUS, UNOBSTRUCTED INTERNAL SPACE WITH NO INTERNAL SUPPORT PANELS THAT WOULD IMPEDE FLOW OR LIMIT ACCESS FOR INSPECTION.
4. THE STRUCTURAL DESIGN OF THE CHAMBERS, THE STRUCTURAL BACKFILL, AND THE INSTALLATION REQUIREMENTS SHALL ENSURE THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET FOR: 1) LONG-DURATION DEAD LOADS AND 2) SHORT-DURATION LIVE LOADS, BASED ON THE AASHTO DESIGN TRUCK WITH CONSIDERATION FOR IMPACT AND MULTIPLE VEHICLE PRESENCES.
5. CHAMBERS SHALL MEET THE REQUIREMENTS OF ASTM F2418, "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
6. CHAMBERS SHALL BE DESIGNED AND ALLOWABLE LOADS DETERMINED IN ACCORDANCE WITH ASTM F2787, "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
7. ONLY CHAMBERS THAT ARE APPROVED BY THE SITE DESIGN ENGINEER WILL BE ALLOWED. THE CHAMBER MANUFACTURER SHALL SUBMIT THE FOLLOWING UPON REQUEST TO THE SITE DESIGN ENGINEER FOR APPROVAL BEFORE DELIVERING CHAMBERS TO THE PROJECT SITE:
 - a. A STRUCTURAL EVALUATION SEALED BY A REGISTERED PROFESSIONAL ENGINEER THAT DEMONSTRATES THAT THE SAFETY FACTORS ARE GREATER THAN OR EQUAL TO 1.95 FOR DEAD LOAD AND 1.75 FOR LIVE LOAD, THE MINIMUM REQUIRED BY ASTM F2787 AND BY AASHTO FOR THERMOPLASTIC PIPE.
 - b. A STRUCTURAL EVALUATION SEALED BY A REGISTERED PROFESSIONAL ENGINEER THAT DEMONSTRATES THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET. THE 50 YEAR CREEP MODULUS DATA SPECIFIED IN ASTM F2418 MUST BE USED AS PART OF THE AASHTO STRUCTURAL EVALUATION TO VERIFY LONG-TERM PERFORMANCE.
 - c. STRUCTURAL CROSS SECTION DETAIL ON WHICH THE STRUCTURAL EVALUATION IS BASED.
8. CHAMBERS AND END CAPS SHALL BE PRODUCED AT AN ISO 9001 CERTIFIED MANUFACTURING FACILITY.

IMPORTANT - NOTES FOR THE BIDDING AND INSTALLATION OF MC-3500 CHAMBER SYSTEM

1. STORMTECH MC-3500 CHAMBERS SHALL NOT BE INSTALLED UNTIL THE MANUFACTURER'S REPRESENTATIVE HAS COMPLETED A PRE-CONSTRUCTION MEETING WITH THE INSTALLERS.
2. STORMTECH MC-3500 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH MC-3500/MC-4500 CONSTRUCTION GUIDE".
3. CHAMBERS ARE NOT TO BE BACKFILLED WITH A DOZER OR AN EXCAVATOR SITUATED OVER THE CHAMBERS.
STORMTECH RECOMMENDS 3 BACKFILL METHODS:
 - STONESHOOTER LOCATED OFF THE CHAMBER BED.
 - BACKFILL AS ROWS ARE BUILT USING AN EXCAVATOR ON THE FOUNDATION STONE OR SUBGRADE.
 - BACKFILL FROM OUTSIDE THE EXCAVATION USING A LONG BOOM HOE OR EXCAVATOR.
4. THE FOUNDATION STONE SHALL BE LEVELED AND COMPACTED PRIOR TO PLACING CHAMBERS.
5. JOINTS BETWEEN CHAMBERS SHALL BE PROPERLY SEATED PRIOR TO PLACING STONE.
6. MAINTAIN MINIMUM - 9" (230 mm) SPACING BETWEEN THE CHAMBER ROWS.
7. INLET AND OUTLET MANIFOLDS MUST BE INSERTED A MINIMUM OF 12" (300 mm) INTO CHAMBER END CAPS.
8. EMBEDMENT STONE SURROUNDING CHAMBERS MUST BE A CLEAN, CRUSHED, ANGULAR STONE 3/4-2" (20-50 mm) MEETING THE AASHTO M43 DESIGNATION OF #3 OR #4.^J
9. STONE MUST BE PLACED ON THE TOP CENTER OF THE CHAMBER TO ANCHOR THE CHAMBERS IN PLACE AND PRESERVE ROW SPACING.^J
10. ADS RECOMMENDS THE USE OF "FLEXSTORM CATCH IT" INSERTS DURING CONSTRUCTION FOR ALL INLETS TO PROTECT THE SUBSURFACE STORMWATER MANAGEMENT SYSTEM FROM CONSTRUCTION SITE RUNOFF.

NOTES FOR CONSTRUCTION EQUIPMENT

1. STORMTECH MC-3500 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH MC-3500/MC-4500 CONSTRUCTION GUIDE".^J
2. THE USE OF EQUIPMENT OVER MC-3500 CHAMBERS IS LIMITED:
 - NO EQUIPMENT IS ALLOWED ON BARE CHAMBERS.
 - NO RUBBER TIRED LOADER, DUMP TRUCK, OR EXCAVATORS ARE ALLOWED UNTIL PROPER FILL DEPTHS ARE REACHED IN ACCORDANCE WITH THE "STORMTECH MC-3500/MC-4500 CONSTRUCTION GUIDE".
 - WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT CAN BE FOUND IN THE "STORMTECH MC-3500/MC-4500 CONSTRUCTION GUIDE".
3. FULL 36" (900 mm) OF STABILIZED COVER MATERIALS OVER THE CHAMBERS IS REQUIRED FOR DUMP TRUCK TRAVEL OR DUMPING.^J
USE OF A DOZER TO PUSH EMBEDMENT STONE BETWEEN THE ROWS OF CHAMBERS MAY CAUSE DAMAGE TO CHAMBERS AND IS NOT AN ACCEPTABLE BACKFILL METHOD. ANY CHAMBERS DAMAGED BY USING THE "DUMP AND PUSH" METHOD ARE NOT COVERED UNDER THE STORMTECH STANDARD WARRANTY.

CONTACT STORMTECH AT 1-888-892-2694 WITH ANY QUESTIONS ON INSTALLATION REQUIREMENTS OR WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT.

CONCEPTUAL LAYOUT

(23) STORMTECH MC-3500 CHAMBERS

(4) STORMTECH MC-3500 END CAPS

INSTALLED WITH 305 mm COVER STONE, 229 mm BASE STONE, 40% STONE VOID

INSTALLED SYSTEM VOLUME: 133 m³

AREA OF SYSTEM: 133 m²

PERIMETER OF SYSTEM: 68 m

PLACE MINIMUM 5.3 m OF ADS GEOSYNTHETICS
315WTK WOVEN GEOTEXTILE OVER BEDDING
STONE AND UNDERNEATH CHAMBER FEET FOR
SCOUR PROTECTION AT ALL CHAMBER INLET
ROWS

300 mm x 300 mm ADS N-12 TOP MANIFOLD, INV
671 mm ABOVE CHAMBER BASE (SIZE TBD BY
ENGINEER / SEE TECH SHEET #7 FOR MANIFOLD
SIZING GUIDANCE)

PROPOSED STRUCTURE W/ELEVATED BYPASS
MANIFOLD (DESIGN BY ENGINEER / PROVIDED BY
OTHERS)

600 mm CORED END CAP PART# MC3500IEPP24BC
TYP OF ALL MC-3500 600 mm CONNECTIONS AND
ISOLATOR ROWS

29,048 m

27,341 m

INSPECTION PORT

ISOLATOR ROW

4,140 m

4,750 m



StormTech®
Retention•Water Quality

70 INWOOD ROAD, SUITE 3 | ROCKY HILL, CT | 06067
860-522-8188 | 888-582-2694 | WWW.STORMTECH.COM

2465070 ONTARIO LTD
2375 ST-LAURENT BLVD., OTTAWA,
ON, K2B 5L2

REV DRW CHK DESCRIPTION

DATE: 12/06/2017 DRAWN: GC

PROJECT #: Tool CHECKED: ---

4640 TRUEMAN BLVD
HILLIARD, OH 43026
1-800-733-7473
ADVANCED DRAINAGE SYSTEMS, INC.

NOT TO SCALE

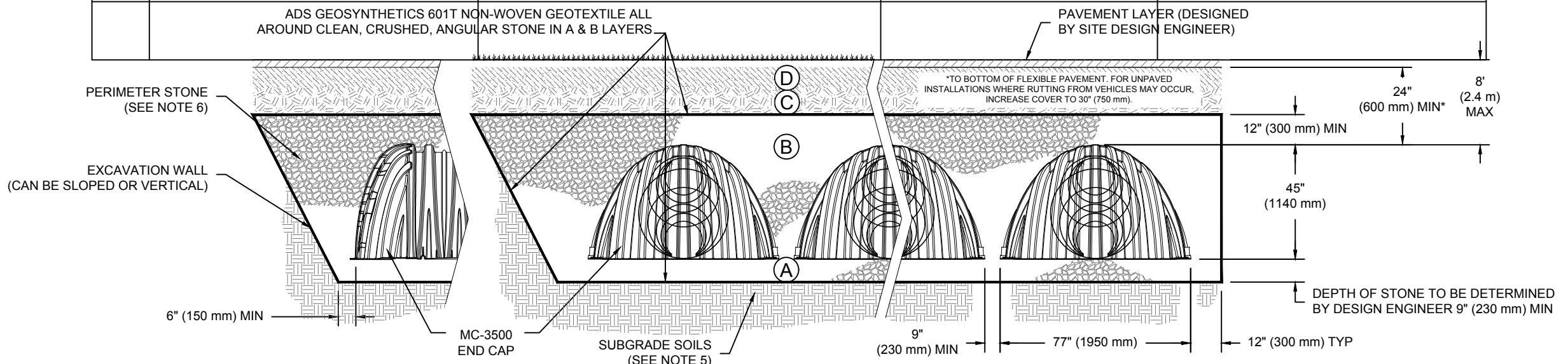
SHEET

2 OF 5

THIS DRAWING HAS BEEN PREPARED BASED ON INFORMATION PROVIDED TO ADS UNDER THE DIRECTION OF THE SITE DESIGN ENGINEER OR OTHER PROJECT REPRESENTATIVE. THE SITE DESIGN ENGINEER SHALL REVIEW THIS DRAWING PRIOR TO CONSTRUCTION. IT IS THE ULTIMATE RESPONSIBILITY OF THE SITE DESIGN ENGINEER TO ENSURE THAT THE PRODUCT(S) DEPICTED AND ALL ASSOCIATED DETAILS MEET ALL APPLICABLE LAWS, REGULATIONS, AND PROJECT REQUIREMENTS.

ACCEPTABLE FILL MATERIALS: STORMTECH MC-3500 CHAMBER SYSTEMS

BEGIN COMPACTIONS AFTER 24" (600 mm) OF MATERIAL OVER THE CHAMBERS IS REACHED. COMPACT ADDITIONAL LAYERS IN 12" (300 mm) MAX LIFTS TO A MIN. 95% PROCTOR DENSITY FOR WELL GRADED MATERIAL AND 95% RELATIVE DENSITY FOR PROCESSED AGGREGATE MATERIALS.		EMBEDMENT STONE: FILL SURROUNDING THE CHAMBERS FROM THE FOUNDATION STONE ('A' LAYER) TO THE 'C' LAYER ABOVE.	CLEAN, CRUSHED, ANGULAR STONE, NOMINAL SIZE DISTRIBUTION BETWEEN 3/4-2 INCH (20-50 mm)	AASHTO M43 ¹ 3, 4
D	A	FOUNDATION STONE: FILL BELOW CHAMBERS FROM THE SUBGRADE UP TO THE FOOT (BOTTOM) OF THE CHAMBER.	CLEAN, CRUSHED, ANGULAR STONE, NOMINAL SIZE DISTRIBUTION BETWEEN 3/4-2 INCH (20-50 mm)	AASHTO M43 ¹ 3, 4 NO COMPACTION REQUIRED.
PLATE COMPACT OR ROLL TO PAVEMENT NOTATION	INITIAL FILL: FILL MATERIAL FOR LAYER 'C' STARTS FROM THE TOP OF THE EMBEDMENT STONE ('B' LAYER) TO 24" (600 mm) ABOVE THE TOP OF THE CHAMBER. NOTE THAT PAVEMENT SUBBASE MAY BE A PART OF THE 'C' LAYER. 1. THE LISTED AASHTO DESIGNATIONS ARE FOR GRADATIONS ONLY. THE STONE MUST ALSO BE CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR NO. 4 (AASHTO M43) STONE". 2. STORMTECH COMPACTION REQUIREMENTS ARE MET FOR 'A' LOCATION MATERIALS WHEN PLACED AND COMPACTED IN 9" (230 mm) (MAX) LIFTS USING TWO FULL COVERS WITH A VIBRATORY COMPACTOR. 3. WHERE INFILTRATION SURFACES MAY BE COMPROMISED BY COMPACTION, FOR STANDARD DESIGN LOAD CONDITIONS EQUIPMENT. FOR SPECIAL LOAD DESIGNS, CONTACT STORMTECH FOR COMPACTION REQUIREMENTS.	GRANULAR WELL-GRADED SOIL/AGGREGATE MIXTURES, <35% FINES OR PROCESSED AGGREGATE. MOST PAVEMENT SUBBASE MATERIALS CAN BE USED IN LIEU OF THIS LAYER.		
	ADS GEOSYNTHETICS 601T NON-WOVEN GEOTEXTILE ALL AROUND CLEAN, CRUSHED, ANGULAR STONE IN A & B LAYERS		PAVEMENT LAYER (DESIGNED BY SITE DESIGN ENGINEER)	



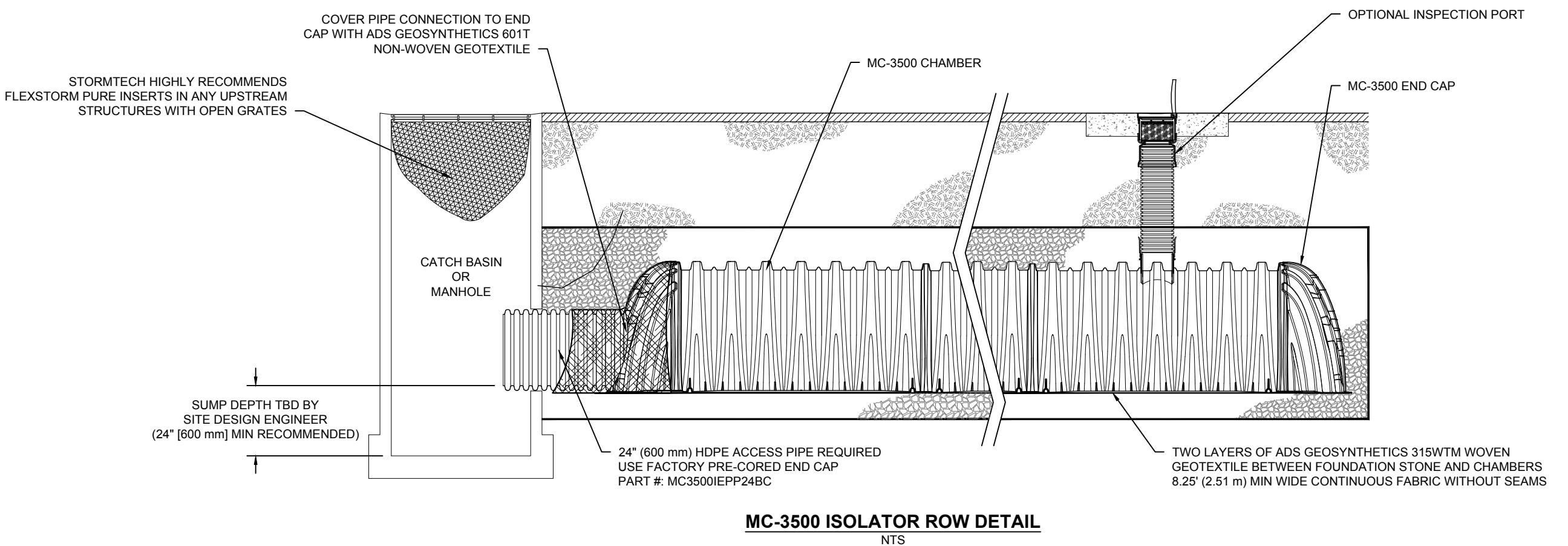
NOTES:

1. MC-3500 CHAMBERS SHALL CONFORM TO THE REQUIREMENTS OF ASTM F2418 "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".^{1J}
2. MC-3500 CHAMBERS SHALL BE DESIGNED IN ACCORDANCE WITH ASTM F2787 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".^{1J}
3. "ACCEPTABLE FILL MATERIALS" TABLE ABOVE PROVIDES MATERIAL LOCATIONS, DESCRIPTIONS, GRADATIONS, AND COMPACTION REQUIREMENTS FOR FOUNDATION, EMBEDMENT, AND FILL MATERIALS.^{1J}
4. THE "SITE DESIGN ENGINEER" REFERS TO THE ENGINEER RESPONSIBLE FOR THE DESIGN AND LAYOUT OF THE STORMTECH CHAMBERS FOR THIS PROJECT.^{1J}
5. THE SITE DESIGN ENGINEER IS RESPONSIBLE FOR ASSESSING THE BEARING RESISTANCE (ALLOWABLE BEARING CAPACITY) OF THE SUBGRADE SOILS AND THE DEPTH OF FOUNDATION STONE WITH CONSIDERATION FOR THE RANGE OF EXPECTED SOIL MOISTURE CONDITIONS.^{1J}
6. PERIMETER STONE MUST BE EXTENDED HORIZONTALLY TO THE EXCAVATION WALL FOR BOTH VERTICAL AND SLOPED EXCAVATION WALLS.
7. ONCE LAYER 'C' IS PLACED, ANY SOIL/MATERIAL CAN BE PLACED IN LAYER 'D' UP TO THE FINISHED GRADE. MOST PAVEMENT SUBBASE SOILS CAN BE USED TO REPLACE THE MATERIAL REQUIREMENTS OF LAYER 'C' OR 'D' AT THE SITE DESIGN ENGINEER'S DISCRETION.

ADS Advanced Drainage Systems, Inc.
4640 TRUEMAN BLVD
HILLIARD, OH 43026
1-800-733-7473

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Detention/Retention/Water Quality
70 INWOOD ROAD, SUITE 3 | ROCKY HILL, CT | 06067
860-522-8188 | 888-582-2694 | WWW.STORMTECH.COM

REV	DRW	CHK	DESCRIPTION	2465070 ONTARIO LTD
			2315 ST-LAURENT BLVD., OTTAWA,	DATE: 12/06/2017 DRAWN: GC
				PROJECT #: Tool CHECKED: ---



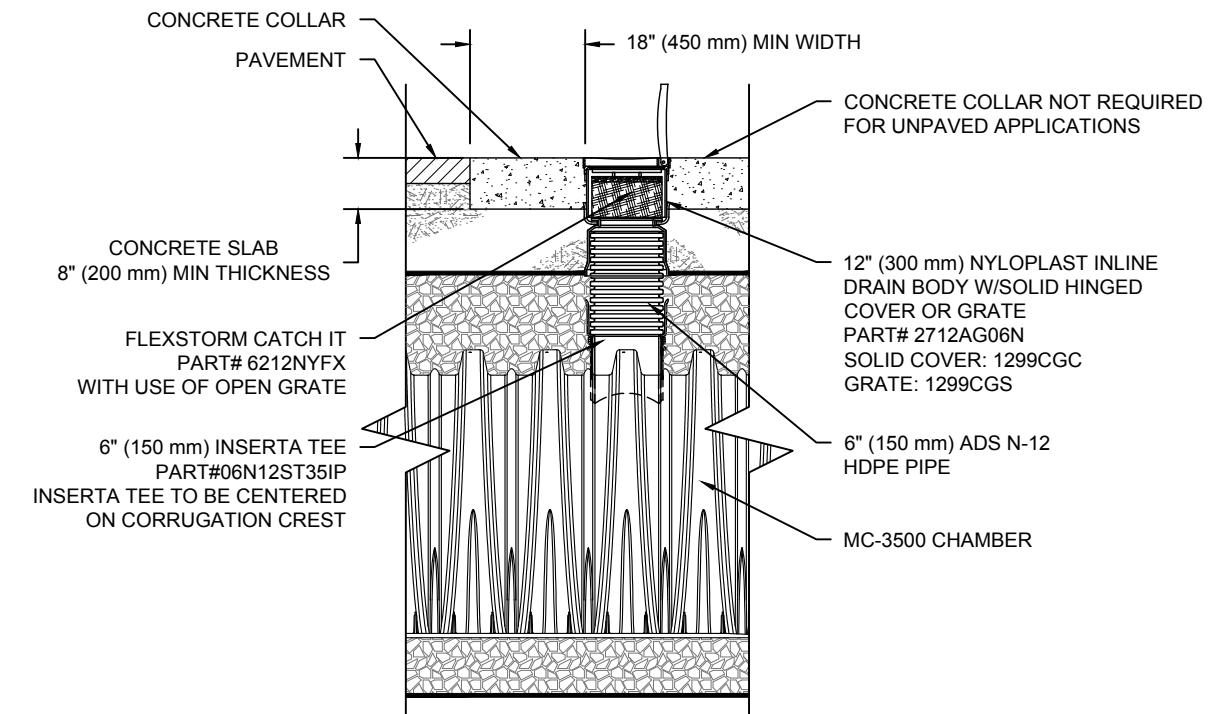
MC-3500 ISOLATOR ROW DETAIL
NTS

INSPECTION & MAINTENANCE

- STEP 1) INSPECT ISOLATOR ROW FOR SEDIMENT
 - A. INSPECTION PORTS (IF PRESENT)
 - A.1. REMOVE/OPEN LID ON NYLOPLAST INLINE DRAIN
 - A.2. REMOVE AND CLEAN FLEXSTORM FILTER IF INSTALLED
 - A.3. USING A FLASHLIGHT AND STADIA ROD, MEASURE DEPTH OF SEDIMENT AND RECORD ON MAINTENANCE LOG
 - A.4. LOWER A CAMERA INTO ISOLATOR ROW FOR VISUAL INSPECTION OF SEDIMENT LEVELS (OPTIONAL)
 - A.5. IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3.
 - B. ALL ISOLATOR ROWS
 - B.1. REMOVE COVER FROM STRUCTURE AT UPSTREAM END OF ISOLATOR ROW
 - B.2. USING A FLASHLIGHT, INSPECT DOWN THE ISOLATOR ROW THROUGH OUTLET PIPE^Ji) MIRRORS ON POLES OR CAMERAS MAY BE USED TO AVOID A CONFINED SPACE ENTRY^Jii) FOLLOW OSHA REGULATIONS FOR CONFINED SPACE ENTRY IF ENTERING MANHOLE
 - B.3. IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3.
- STEP 2) CLEAN OUT ISOLATOR ROW USING THE JETVAC PROCESS
 - A. A FIXED CULVERT CLEANING NOZZLE WITH REAR FACING SPREAD OF 45" (1.1 m) OR MORE IS PREFERRED
 - B. APPLY MULTIPLE PASSES OF JETVAC UNTIL BACKFLUSH WATER IS CLEAN
 - C. VACUUM STRUCTURE SUMP AS REQUIRED
- STEP 3) REPLACE ALL COVERS, GRATES, FILTERS, AND LIDS; RECORD OBSERVATIONS AND ACTIONS.
- STEP 4) INSPECT AND CLEAN BASINS AND MANHOLES UPSTREAM OF THE STORMTECH SYSTEM.

NOTES

1. INSPECT EVERY 6 MONTHS DURING THE FIRST YEAR OF OPERATION. ADJUST THE INSPECTION INTERVAL BASED ON PREVIOUS OBSERVATIONS OF SEDIMENT ACCUMULATION AND HIGH WATER ELEVATIONS.^J
2. CONDUCT JETTING AND VACTORING ANNUALLY OR WHEN INSPECTION SHOWS THAT MAINTENANCE IS NECESSARY.



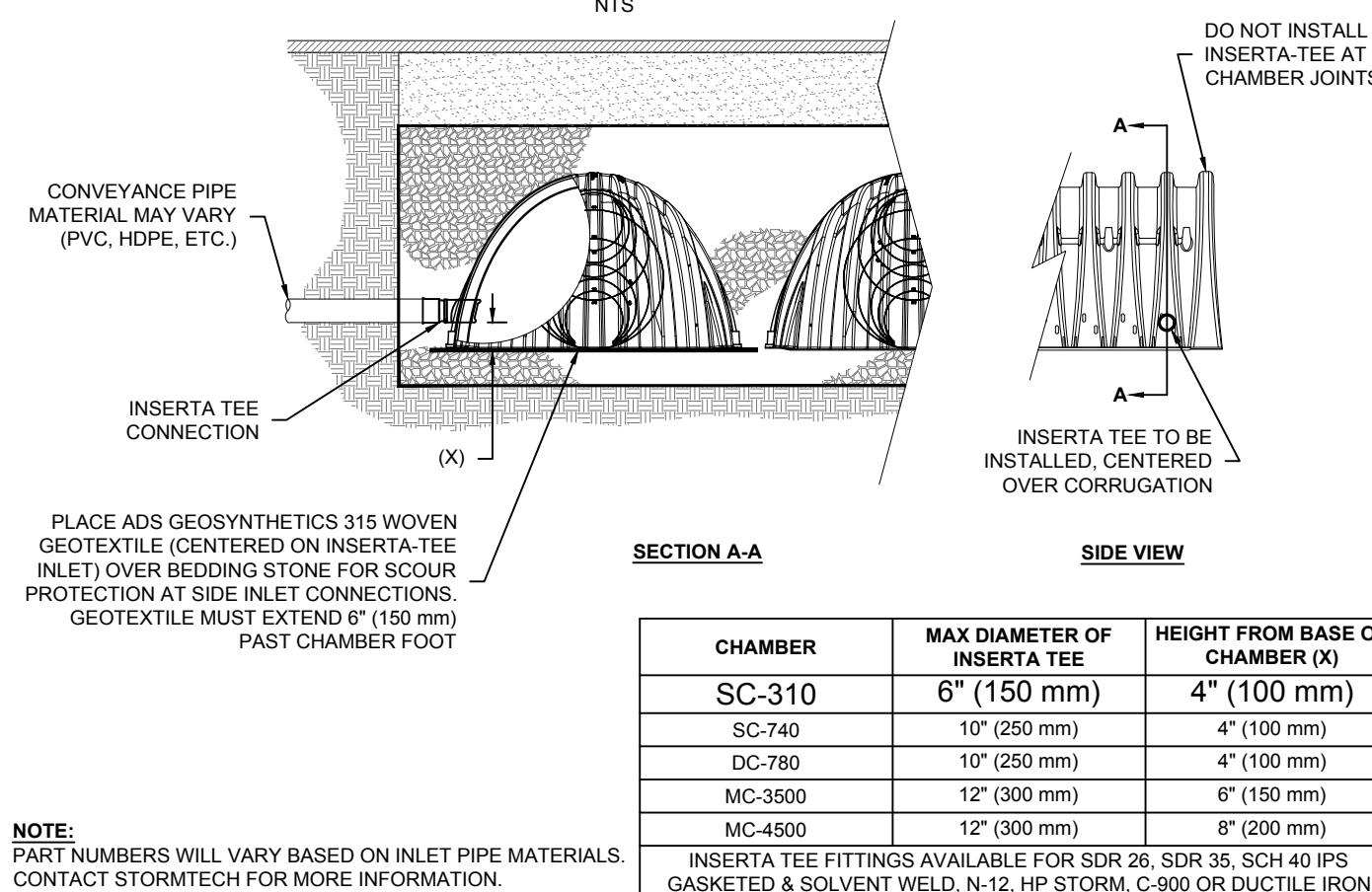
MC-3500 6" INSPECTION PORT DETAIL
NTS

4640 TRUEMAN BLVD HILLIARD, OH 43026 1-800-733-7473	465070 ONTARIO LTD 2375 ST-LAURENT BLVD., OTTAWA, ON K2B 7L2	DATE: 12/06/2017	DRAWN: GC
PROJECT #: Tool	CHECKED: ---	REV	DRW

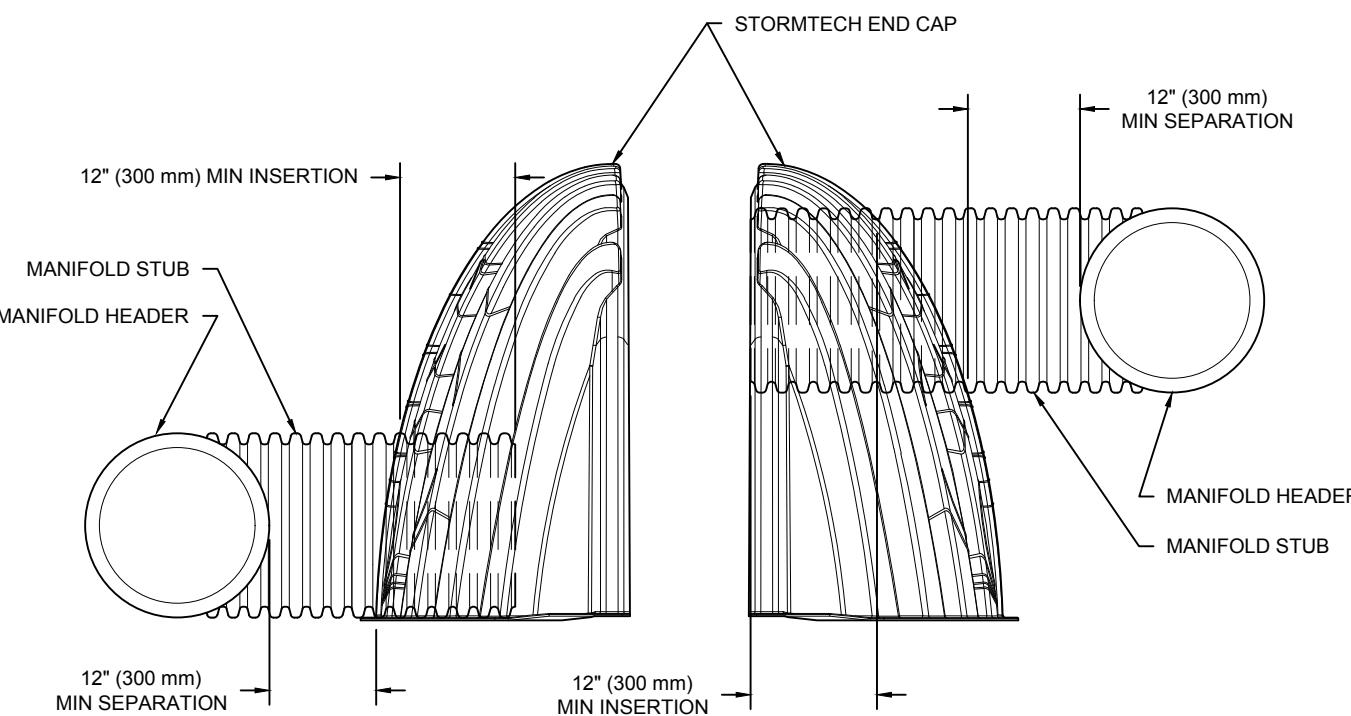
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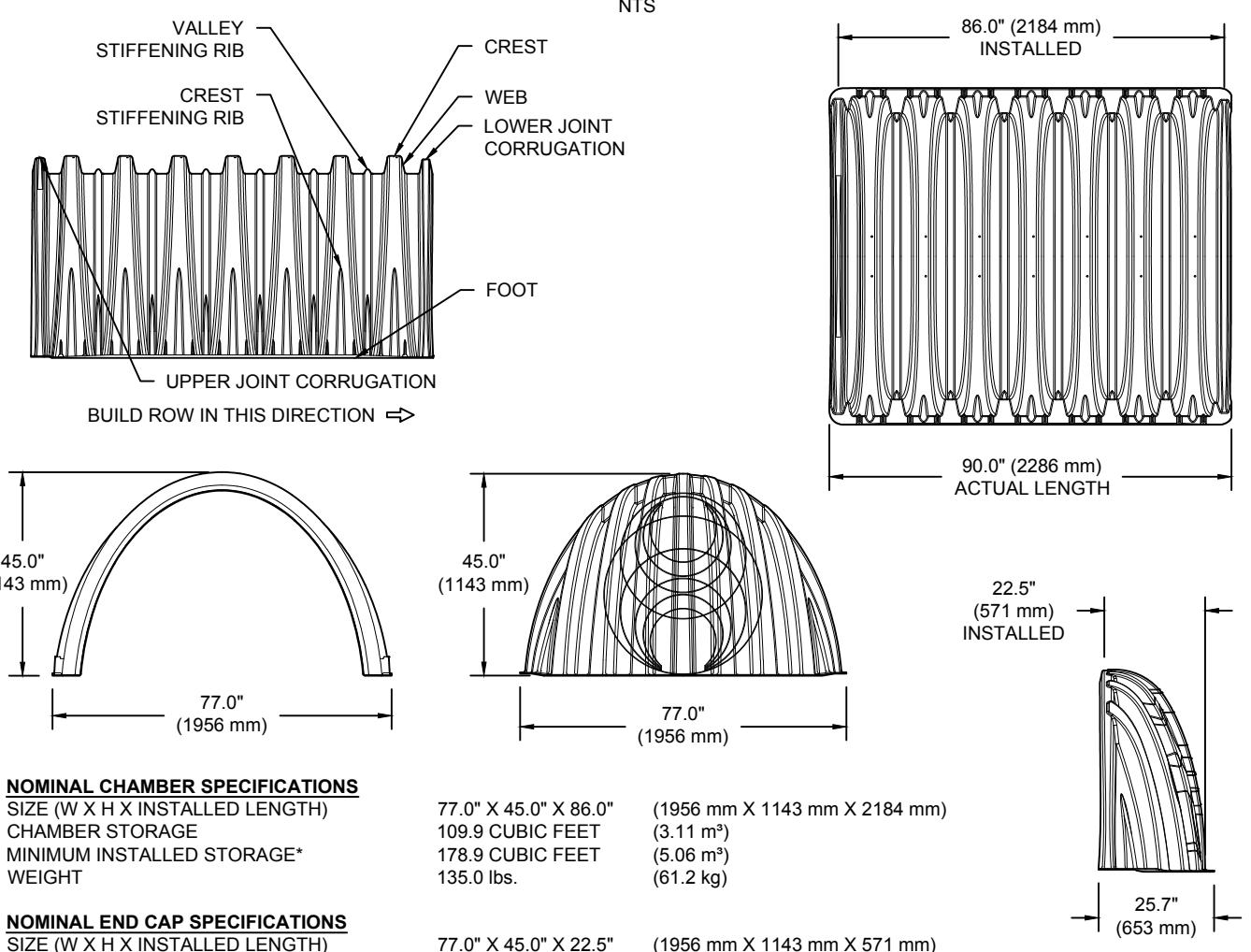
INSERTA TEE DETAIL



MC-SERIES END CAP INSERTION DETAIL



MC-3500 TECHNICAL SPECIFICATION



NOMINAL CHAMBER SPECIFICATIONS

SIZE (W X H X INSTALLED LENGTH)	77.0" X 45.0" X 86.0"	(1956 mm X 1143 mm X 2184 mm)
CHAMBER STORAGE	109.9 CUBIC FEET	(3.11 m ³)
MINIMUM INSTALLED STORAGE*	178.9 CUBIC FEET	(5.06 m ³)
WEIGHT	135.0 lbs.	(61.2 kg)

NOMINAL END CAP SPECIFICATIONS

SIZE (W X H X INSTALLED LENGTH)	77.0" X 45.0" X 22.5"	(1956 mm X 1143 mm X 571 mm)
END CAP STORAGE	14.9 CUBIC FEET	(0.42 m ³)
MINIMUM INSTALLED STORAGE*	46.0 CUBIC FEET	(1.30 m ³)
WEIGHT	50.0 lbs.	(22.7 kg)

*ASSUMES 12" (305 mm) STONE ABOVE, 9" (229 mm) STONE FOUNDATION AND BETWEEN CHAMBERS,
12" (305 mm) STONE PERIMETER IN FRONT OF END CAPS AND 40% STONE POROSITY

STUBS AT BOTTOM OF END CAP FOR PART NUMBERS ENDING WITH "B"
STUBS AT TOP OF END CAP FOR PART NUMBERS ENDING WITH "T"

PART #	STUB	B	C
MC3500IEPP06T	6" (150 mm)	33.21" (844 mm)	---
MC3500IEPP06B		---	0.66" (17 mm)
MC3500IEPP08T	8" (200 mm)	31.16" (791 mm)	---
MC3500IEPP08B		---	0.81" (21 mm)
MC3500IEPP10T	10" (250 mm)	29.04" (738 mm)	---
MC3500IEPP10B		---	0.93" (24 mm)
MC3500IEPP12T	12" (300 mm)	26.36" (670 mm)	---
MC3500IEPP12B		---	1.35" (34 mm)
MC3500IEPP15T	15" (375 mm)	23.39" (594 mm)	---
MC3500IEPP15B		---	1.50" (38 mm)
MC3500IEPP18TC	18" (450 mm)	20.03" (509 mm)	---
MC3500IEPP18BC		---	1.77" (45 mm)
MC3500IEPP24TC	24" (600 mm)	14.48" (368 mm)	---
MC3500IEPP24BC		---	2.06" (52 mm)
MC3500IEPP30BC	30" (750 mm)	---	---

NOTE: ALL DIMENSIONS ARE NOMINAL

CUSTOM PRECORED INVERTS ARE AVAILABLE UPON REQUEST. INVENTORIED MANIFOLDS INCLUDE 12-24" (300-600 mm) SIZE ON SIZE AND 15-48" (375-1200 mm) ECCENTRIC MANIFOLDS.
CUSTOM INVERT LOCATIONS ON THE MC-3500 END CAP CUT IN THE FIELD ARE NOT RECOMMENDED FOR PIPE SIZES GREATER THAN 10" (250 mm)
THE INVERT LOCATION IN COLUMN 'B' ARE THE HIGHEST POSSIBLE FOR THE PIPE SIZE.

4640 TRUEMAN BLVD HILLIARD, OH 43026 1-800-733-7473	2465070 ONTARIO LTD 2375 ST-LAURENT BLVD., OTTAWA, ONTARIO, CANADA		
ADVANCED DRAINAGE SYSTEMS, INC.	2465070 ONTARIO LTD 2375 ST-LAURENT BLVD., OTTAWA, ONTARIO, CANADA		
REV	DRW	CHK	DESCRIPTION
DATE:	12/06/2017	DRAWN:	GC
PROJECT #:	Tool	CHECKED:	---

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SHEET
5 OF 5

APPENDIX F
Stormceptor Reports

Brief Stormceptor Sizing Report - 2465070 ONTARIO LTD

Project Information & Location			
Project Name	2465070 ONTARIO LTD	Project Number	170721
City	Ottawa	State/ Province	Ontario
Country	Canada	Date	12/7/2017
Designer Information		EOR Information (optional)	
Name	Guillaume Courtois	Name	
Company	LRL Associates Ltd.	Company	
Phone #	613-842-3434	Phone #	
Email	gcourtois@lrl.ca	Email	

Stormwater Treatment Recommendation

The recommended Stormceptor Model(s) which achieve or exceed the user defined water quality objective for each site within the project are listed in the below Sizing Summary table.

Site Name	Proposed Yonaka Warehouse
Target TSS Removal (%)	80
TSS Removal (%) Provided	81
Recommended Stormceptor Model	STC 300

The recommended Stormceptor Model achieves the water quality objectives based on the selected inputs, historical rainfall records and selected particle size distribution.

Stormceptor Sizing Summary	
Stormceptor Model	% TSS Removal Provided
STC 300	81
STC 750	87
STC 1000	88
STC 1500	87
STC 2000	89
STC 3000	90
STC 4000	92
STC 5000	92
STC 6000	93
STC 9000	95
STC 10000	95
STC 14000	96
StormceptorMAX	Custom

Sizing Details			
Drainage Area		Water Quality Objective	
Total Area (ha)	0.659	TSS Removal (%)	80.0
Imperviousness %	83.0	Runoff Volume Capture (%)	
Rainfall			
Station Name	OTTAWA MACDONALD-CARTIER INT'L A	Oil Spill Capture Volume (L)	
State/Province	Ontario	Peak Conveyed Flow Rate (L/s)	
Station ID #	6000	Water Quality Flow Rate (L/s)	
Up Stream Storage			
Years of Records	37	Storage (ha-m)	Discharge (cms)
Latitude	45°19'N	0.000	0.000
Longitude	75°40'W	0.022	0.043
Up Stream Flow Diversion			
		Max. Flow to Stormceptor (cms)	

Particle Size Distribution (PSD) The selected PSD defines TSS removal		
Fine Distribution		
Particle Diameter (microns)	Distribution %	Specific Gravity
20.0	20.0	1.30
60.0	20.0	1.80
150.0	20.0	2.20
400.0	20.0	2.65
2000.0	20.0	2.65

Notes

- Stormceptor performance estimates are based on simulations using PCSWMM for Stormceptor, which uses the EPA Rainfall and Runoff modules.
- Design estimates listed are only representative of specific project requirements based on total suspended solids (TSS) removal defined by the selected PSD, and based on stable site conditions only, after construction is completed.
- For submerged applications or sites specific to spill control, please contact your local Stormceptor representative for further design assistance.

For Stormceptor Specifications and Drawings Please Visit:
<http://www.imbriumsystems.com/technical-specifications>

APPENDIX G
Complete Set of Civil Plans

USE AND INTERPRETATION OF DRAWINGS
GENERAL CONDITIONS OF THE CONTRACT FOR CONSTRUCTION ARE PART OF THE CONTRACT DOCUMENTS AND DESCRIBE USE AND INTENT OF THE DRAWING. THE CONTRACT DOCUMENTS INCLUDE NOT ONLY THE DRAWINGS, BUT ALSO THE CONTRACT CONDITIONS, SPECIFICATIONS, DRAWINGS, AND OTHER DOCUMENTS THAT ARE REFERENCED IN THE CONTRACT DOCUMENTS. THE CONTRACT CONDITIONS, SPECIFICATIONS, ADDENDA, AND MODIFICATIONS ISSUED AFTER EXECUTION OF THE CONTRACT, THESE CONDITIONS, DOCUMENTS, AND OTHER DOCUMENTS ARE COMPLEMENTARY, AND WHERE REFERRED TO, THESE DOCUMENTS SHALL BIND AS IF THEY WERE PART OF THE CONTRACT. THE CONTRACT DOCUMENTS ARE THE SOLE BOUNDING AGREEMENT, AND ANY OTHER DOCUMENTS WHICH ARE NOT PART OF THE CONTRACT DOCUMENTS ARE NOT COMPLETELY DELINEATED HERON SHALL BE CONSTRUCTED OF THE SAME MATERIALS, WORKMANSHIP, AND WORK SHOWN MORE COMPLETELY ELSEWHERE IN THE CONTRACT DOCUMENTS.

BY USE OF THE DRAWINGS FOR CONSTRUCTION OF THE PROJECT, THE OWNER CONFIRMS THAT HE HAS REVIEWED AND APPROVED THE DRAWINGS. THE CONTRACTOR CONVERNS THAT HE HAS REVIEWED AND APPROVED THE DRAWINGS. THE CONTRACTOR AGREES THAT HE HAS READ AND UNDERSTOOD THE DRAWINGS AND THAT HE WILL CONSTRUCT THE WORK IN ACCORDANCE WITH THE DRAWINGS. THE CONTRACTOR AGREES THAT HE WILL CONSTRUCT THE WORK IN ACCORDANCE WITH THE DRAWINGS AND THAT HE WILL CONSTRUCT THE WORK IN ACCORDANCE WITH THE DRAWINGS. THE CONTRACTOR AGREES THAT HE WILL CONSTRUCT THE WORK IN ACCORDANCE WITH THE DRAWINGS AND THAT HE WILL CONSTRUCT THE WORK IN ACCORDANCE WITH THE DRAWINGS.

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IN THE EVENT THE CLIENT, THE CLIENT'S CONTRACTORS OR SUBCONTRACTORS, OR ANY UNAUTHORIZED PERSON USES OR LEAKS IT, LEGALLY LAWS, MARCHES OR TREATIES TO BE MADE ANY CHANGES TO ANY REPORTS, PLANS, SPECIFICATIONS, OR OTHER CONSTRUCTION DOCUMENTS PREPARED BY LRL ASSOCIATES LTD. (LRL) WITHOUT OBTAINING WRITTEN APPROVAL FROM LRL. THE CONTRACTOR AGREES TO BE RESPONSIBLE FOR THE RESULTS OF SUCH CHANGES. THEREFORE THE CLIENT AGREES TO WAIVE ANY CLAIM AGAINST LRL AND TO RELEASE LRL FROM ANY LIABILITY ARISING DIRECTLY OR INDIRECTLY FROM SUCH UNAUTHORIZED CHANGES.

IN ADDITION, THE CLIENT AGREES TO THE FULLEST EXTENT PERMITTED BY LAW, TO INDEMNIFY AND HOLD HARMLESS LRL FROM ANY DAMAGES, LIABILITIES OR COSTS, INCLUDING ATTORNEY'S FEES AND COST OF DEFENSE, ARISING FROM SUCH CHANGES.

IN ADDITION, THE CLIENT AGREES, INCLUDE IN ANY CONTRACTS, FOR CONSTRUCTION APPROPRIATE LANGUAGE THAT PROHIBITS THE CONTRACTOR OR ANY SUBCONTRACTOR OF THE CONTRACTOR FROM MAKING ANY CHANGES TO ANY CONSTRUCTION DOCUMENTS PREPARED BY LRL. THE CONTRACTOR SHALL OBTAIN WRITTEN APPROVAL OF LRL AND THAT FURTHER REQUIRES THE CONTRACTOR TO INDUCE WITH LRL AND THE CLIENT FROM ANY LIABILITY OR COST ARISING FROM SUCH CHANGES MADE WITHOUT SUCH PROPER AUTHORIZATION.

GENERAL NOTES:

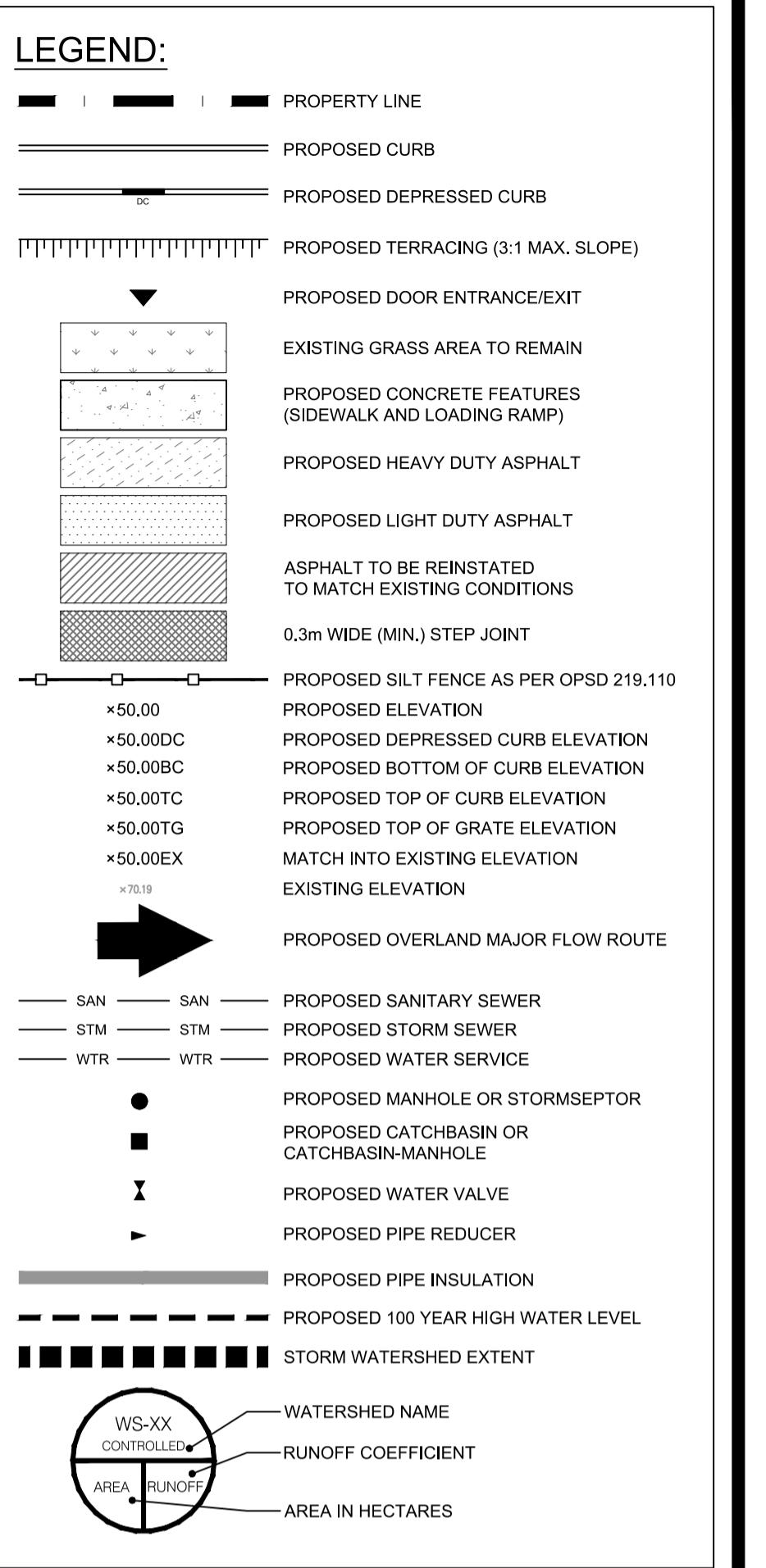
EXISTING SERVICES AND UTILITIES SHOWN ON THESE DRAWINGS ARE TAKEN FROM THE BEST AVAILABLE RECORDS, BUT MAY NOT BE COMPLETE, OR TO DATE. CONTRACTOR SHALL VERIFY IN FIELD FOR LOCATION AND ELEVATION OF PIPES AND CHECK WITH THE UTILITY COMPANIES BEFORE DIGGING OR PERFORMING WORK.

CONTRACTOR IS ADVISED TO COLLECT INFORMATION ON SOIL CONDITIONS BEFORE START OF CONSTRUCTION.

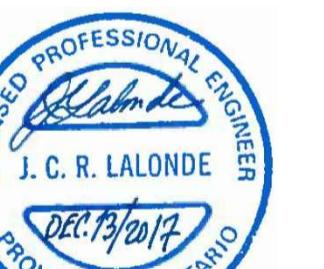
THE ENGINEER WAIVES ANY AND ALL RESPONSIBILITY AND LIABILITY FOR PROBLEMS WHICH ARISE FROM FAILURE TO FOLLOW THESE PLANS, SPECIFICATIONS AND THE DESIGN ELEMENTS THEY CONVEY, OR FOR PROBLEMS WHICH ARISE FROM THE CONTRACTOR'S FAILURE TO FOLLOW THE ENGINEER'S GUIDANCE WITH RESPECT TO ANY ERRORS, OMISSIONS, INCONSISTENCIES, AMBIGUITIES OR CONFLICTS WHICH ARE ALLEGED.

CONTRACTOR TO VERIFY ALL DIMENSIONS AND NOTIFY THE ENGINEER OF ANY DISCREPANCIES BEFORE WORK COMMENCES. DO NOT SCALE DRAWINGS.

SCALE: 1:250



01 ISSUED FOR SPA G.M.C. 13 DEC 2017
No. REVISIONS BY DATE



NOT AUTHENTIC UNLESS SIGNED AND DATED

J. C. R. LALONDE
DEC 13 2017
PROVINCE OF ONTARIO

5430 Canotek Road | Ottawa, ON K1J 9G2
www.lrl.ca | (613) 842-3434

CLIENT GRAEBECK CONSTRUCTION LTD.

DESIGNED BY: G.M.C. DRAWN BY: G.M.C. APPROVED BY: J.C.L.
PROJECT

2465070 ONTARIO LTD.
2375 ST-LAURENT BLVD., OTTAWA, ON

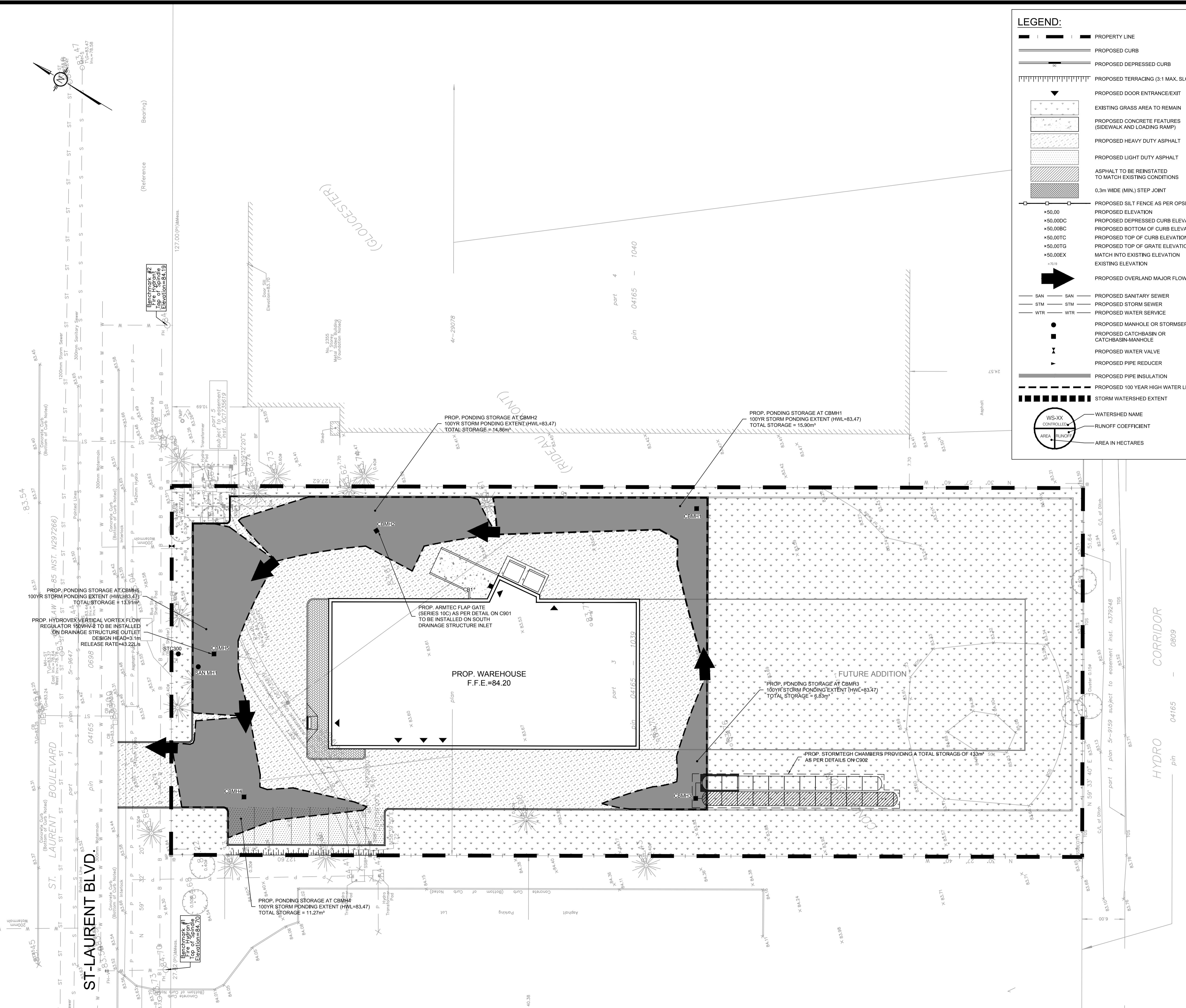
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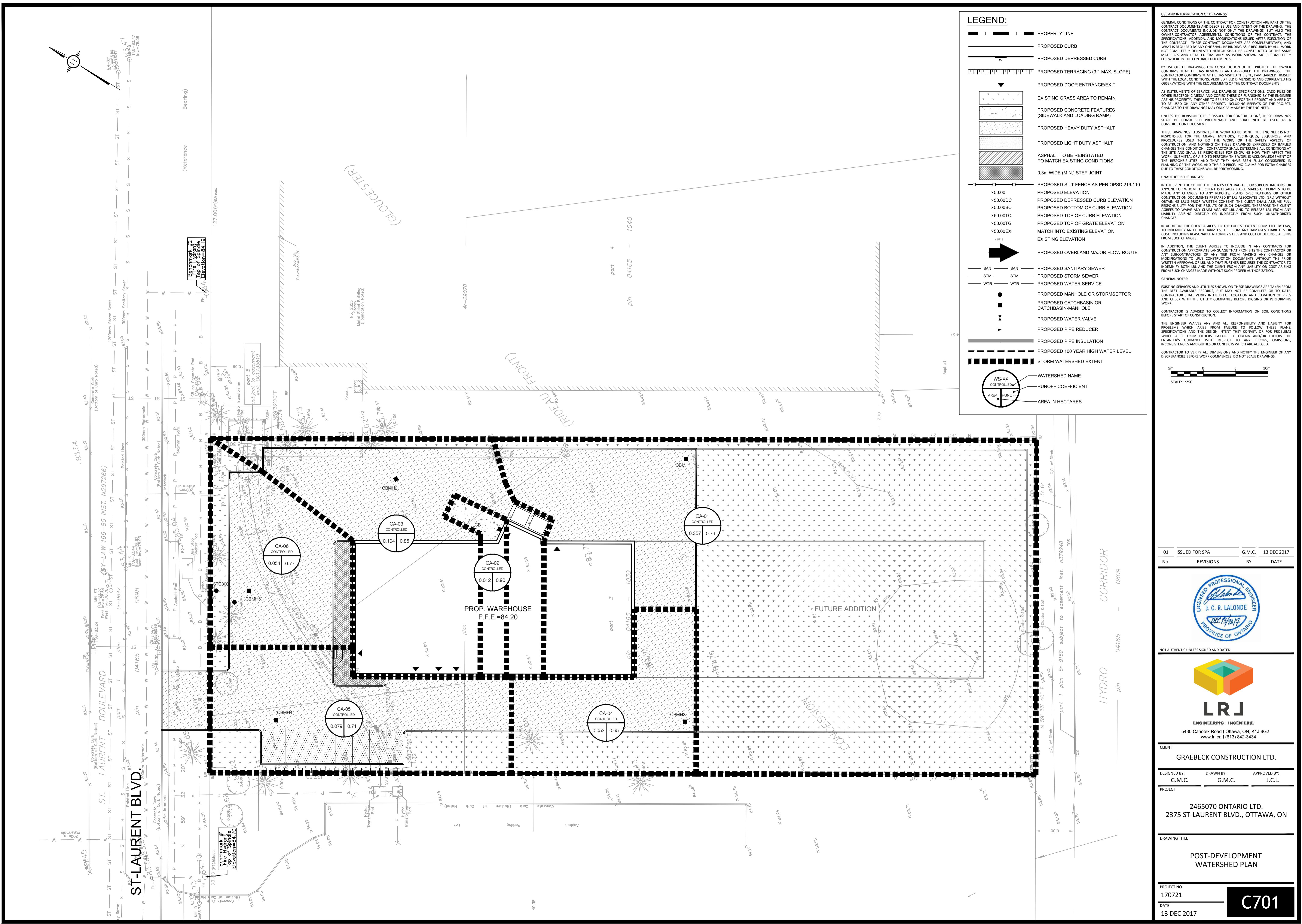
STORMWATER MANAGEMENT PLAN

PROJECT NO. 170721

DATE 13 DEC 2017

C601





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UNAUTHORIZED CHANGES:

IN THE EVENT THE CLIENT, THE CLIENT'S CONTRACTORS OR SUBCONTRACTORS, OR ANY UNAUTHORIZED PERSON, WHETHER LEGALLY LIABLE OR NOT, MAKE OR PERMIT TO MAKE ANY CHANGES TO ANY REPORTS, PLANS, SPECIFICATIONS OR OTHER CONSTRUCTION DOCUMENTS PREPARED BY LRL ASSOCIATES LTD. (LRL) WITHOUT DRAFTING A CORRESPONDING ADDENDUM, THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE COST OF THESE CHANGES. THEREFORE THE CLIENT AGREES TO WAIVE ANY CLAIM AGAINST LRL AND TO RELEASE LRL FROM ANY LIABILITY ARISING DIRECTLY OR INDIRECTLY FROM SUCH UNAUTHORIZED CHANGES.

IN ADDITION, THE CLIENT AGREES TO THE FULLEST EXTENT PERMITTED BY LAW, TO INDEMNIFY AND HOLD HARMLESS LRL FROM ANY DAMAGES, LIABILITIES OR COSTS ARISING OUT OF THE CONTRACTOR'S FAILURE TO FOLLOW THE CONTRACT DOCUMENTS PREPARED BY LRL AND THAT FURTHER REQUIRES THE CONTRACTOR TO INDUCE THE CONTRACTOR TO FOLLOW THE CONTRACT DOCUMENTS PREPARED BY LRL AND THE CLIENT FROM ANY LIABILITY OR COST ARISING FROM SUCH CHANGES MADE WITHOUT SUCH PROPER AUTHORIZATION.

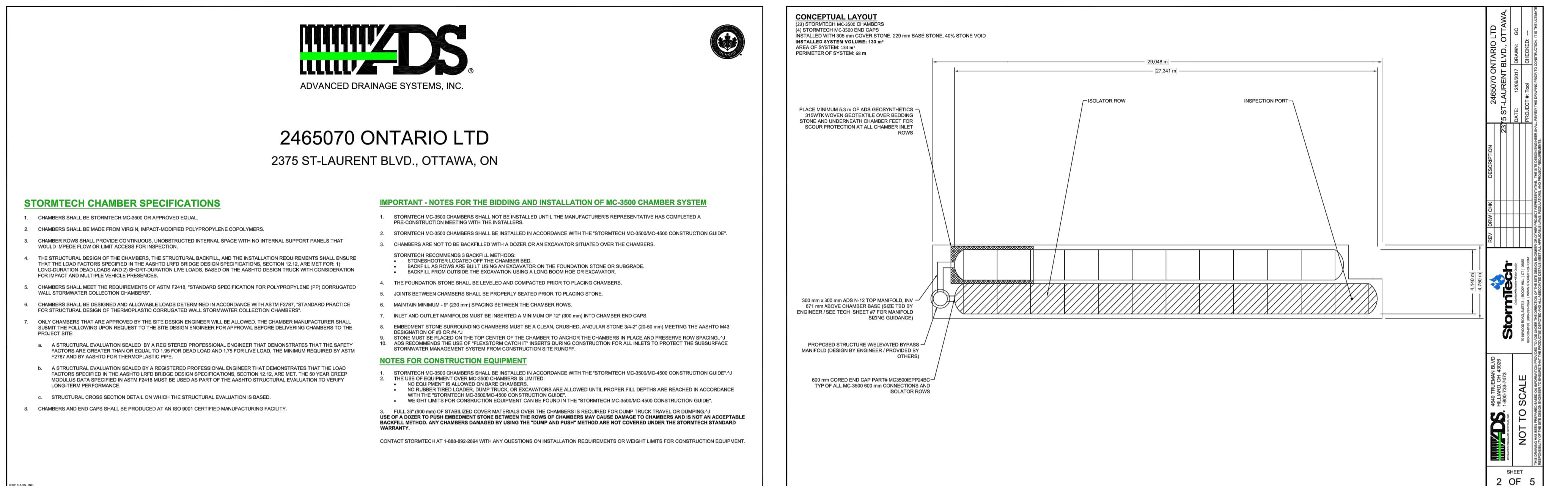
GENERAL NOTES:

EXISTING SERVICES AND UTILITIES SHOWN ON THESE DRAWINGS ARE TAKEN FROM THE BEST AVAILABLE RECORDS, BUT MAY NOT BE COMPLETE OR TO DATE. CONTRACTOR SHALL VERIFY IN FIELD FOR LOCATION AND ELEVATION OF PIPES AND CHECK WITH THE UTILITY COMPANIES BEFORE DIGGING OR PERFORMING WORK.

CONTRACTOR IS ADVISED TO COLLECT INFORMATION ON SOIL CONDITIONS BEFORE START OF CONSTRUCTION.

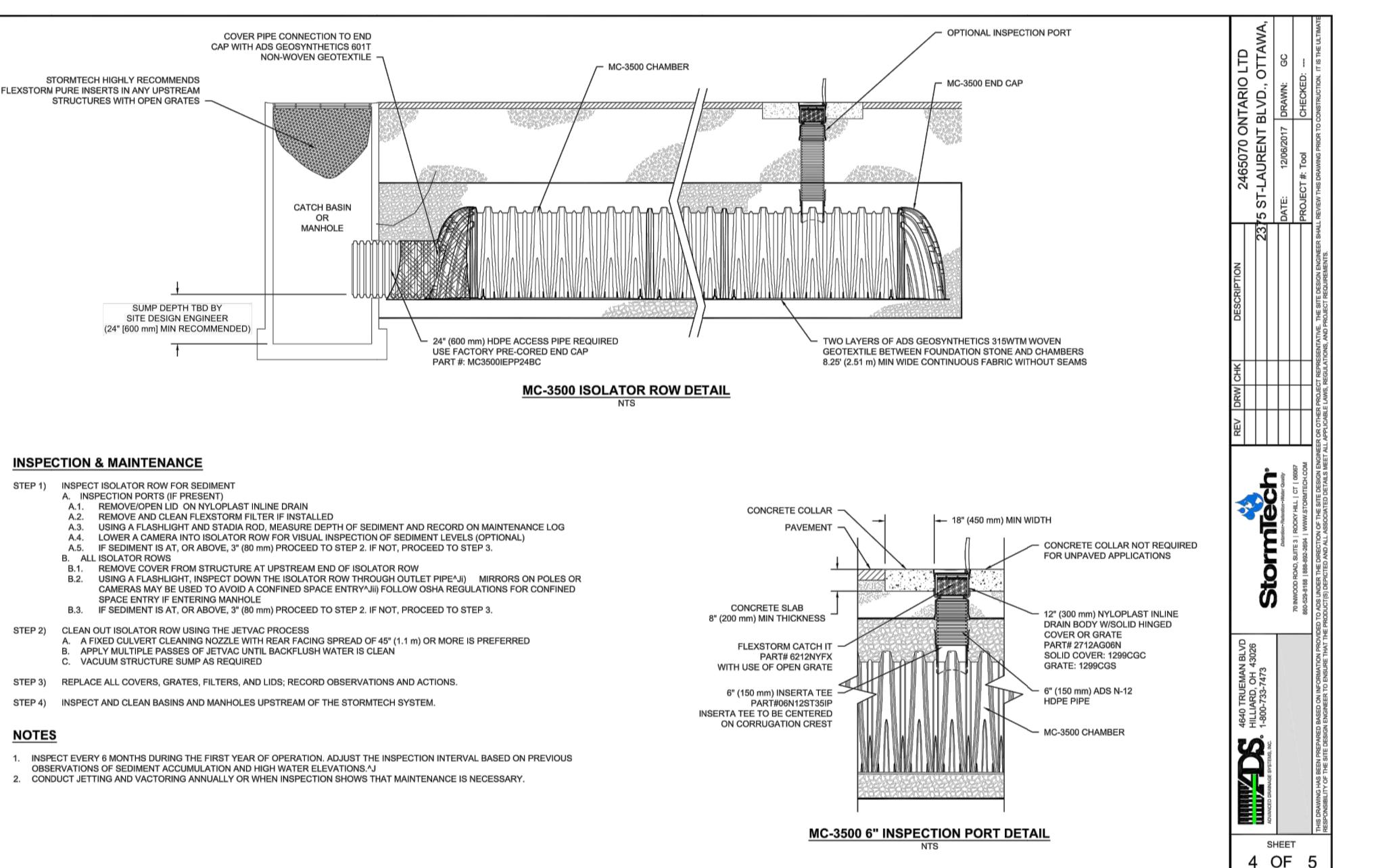
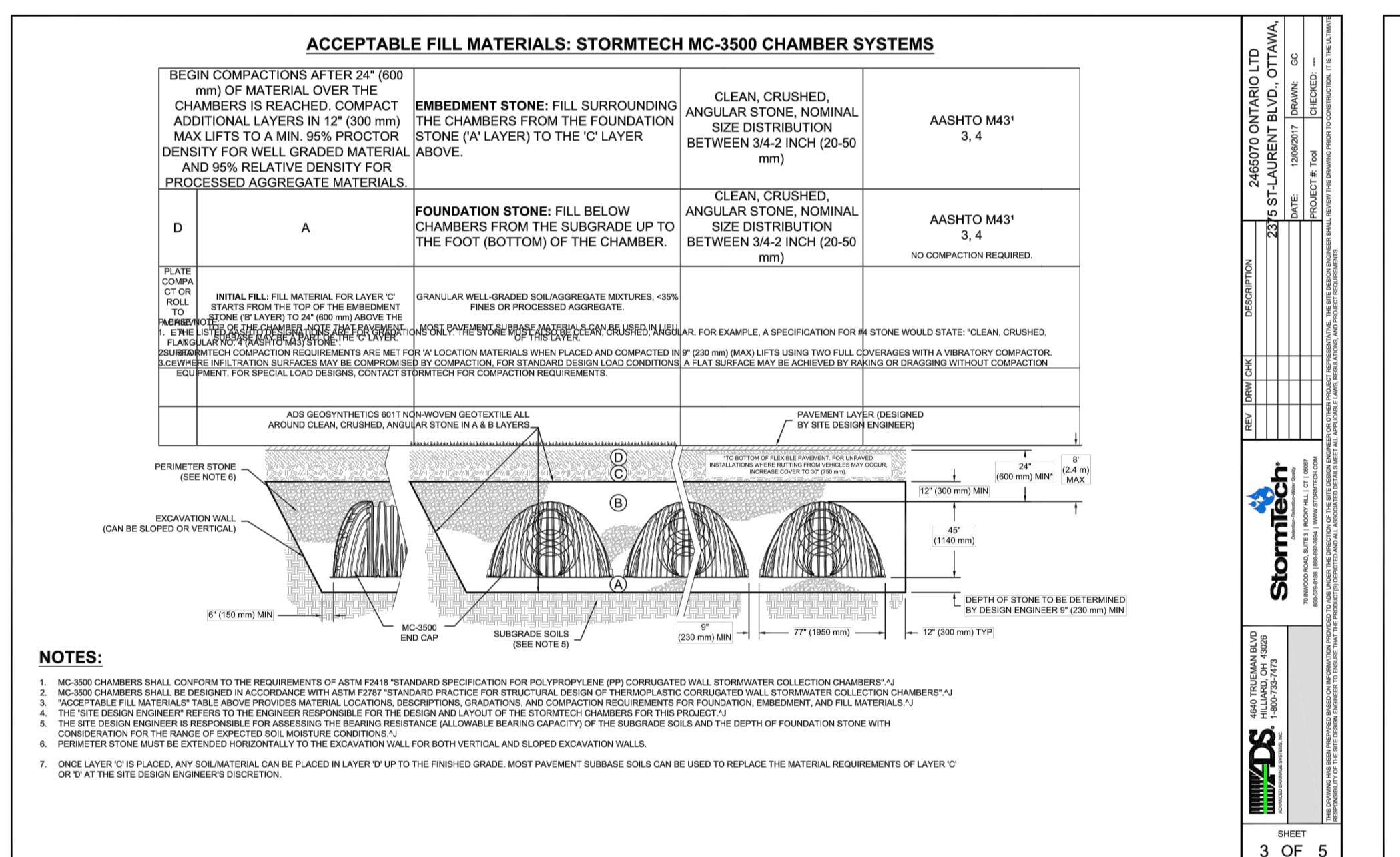
THE ENGINEER WAIVES ANY AND ALL RESPONSIBILITY AND LIABILITY FOR PROBLEMS WHICH ARISE FROM FAILURE TO FOLLOW THESE PLANS, SPECIFICATIONS AND THE DESIGN INTENT THE CONTRACTOR OR FOR ANY UNINTENDED CONSEQUENCES OF THE DESIGN. THE CONTRACTOR AGREES TO FOLLOW THE ENGINEER'S GUIDANCE WITH RESPECT TO ANY ERRORS, OMISSIONS, INCONSISTENCIES AMBIGUITIES OR CONFLICTS WHICH ARE ALLEGED.

CONTRACTOR TO VERIFY ALL DIMENSIONS AND NOTIFY THE ENGINEER OF ANY DISCREPANCIES BEFORE WORK COMMENCES. DO NOT SCALE DRAWINGS.

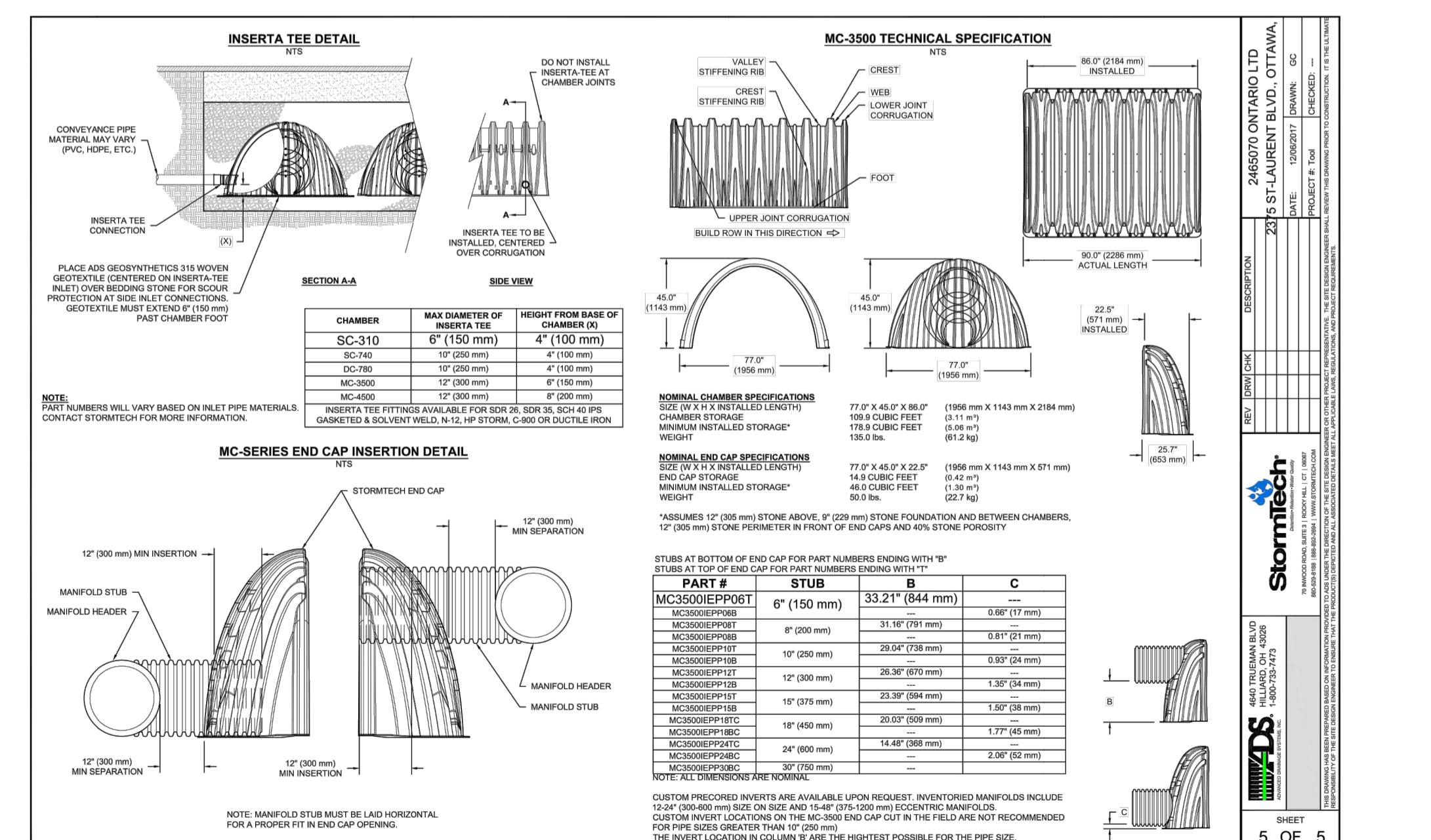


NOT TO SCALE

2 OF 5



4 OF 5



5 OF 5

NOT AUTHENTIC UNLESS SIGNED AND DATED



J.C.R. LALONDE
PROVINCE OF ONTARIO
DEC 13 2017

L.R.J.
ENGINEERING | INGENIERIE

5430 Canotek Road | Ottawa, ON, K1J 9G2
www.lrl.ca | (613) 842-3434

CLIENT
GRAEBECK CONSTRUCTION LTD.

DESIGNED BY: G.M.C. DRAWN BY: G.M.C. APPROVED BY: J.C.L.

PROJECT

2465070 ONTARIO LTD.
2375 ST-LAURENT BLVD., OTTAWA, ON

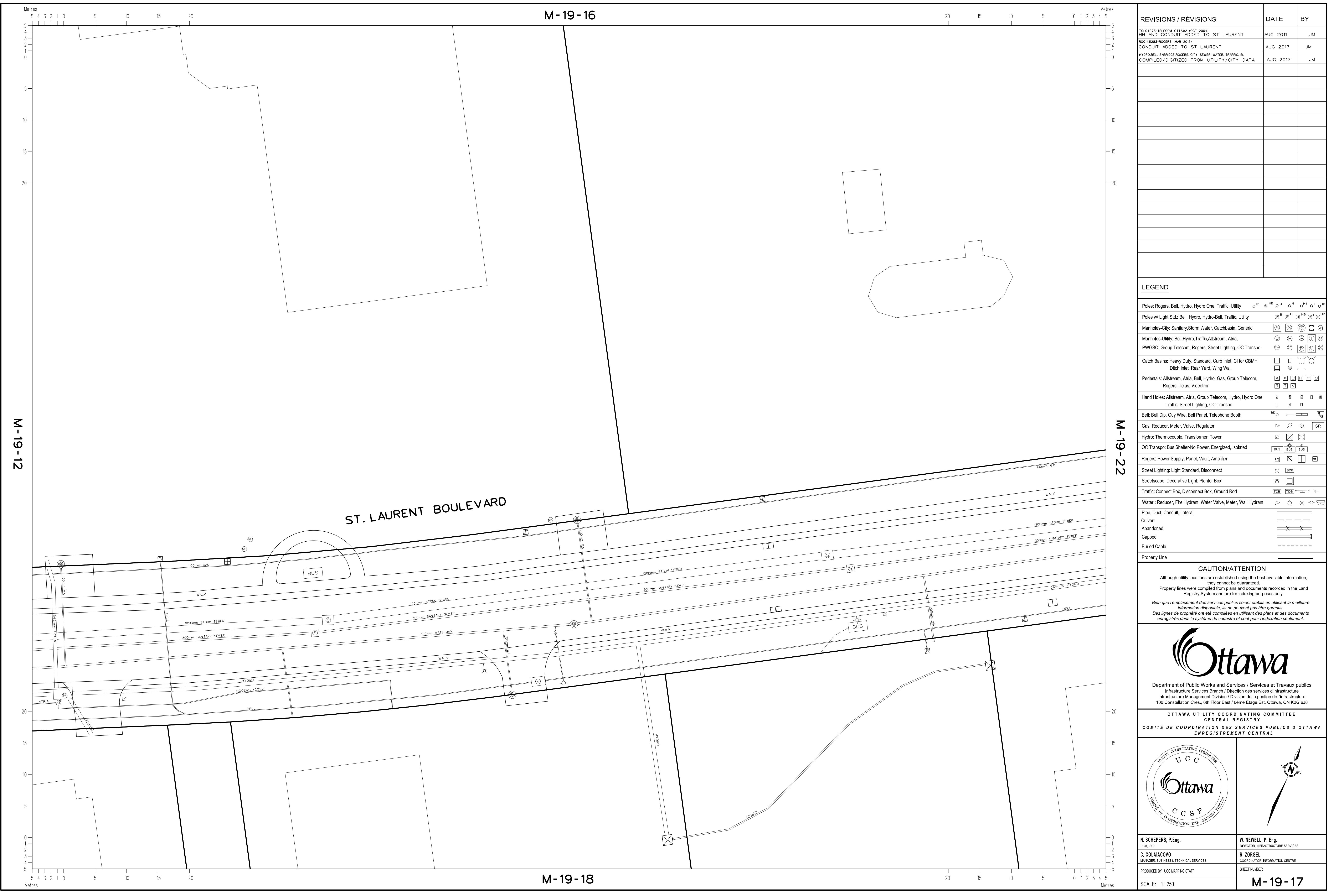
DRAWING TITLE

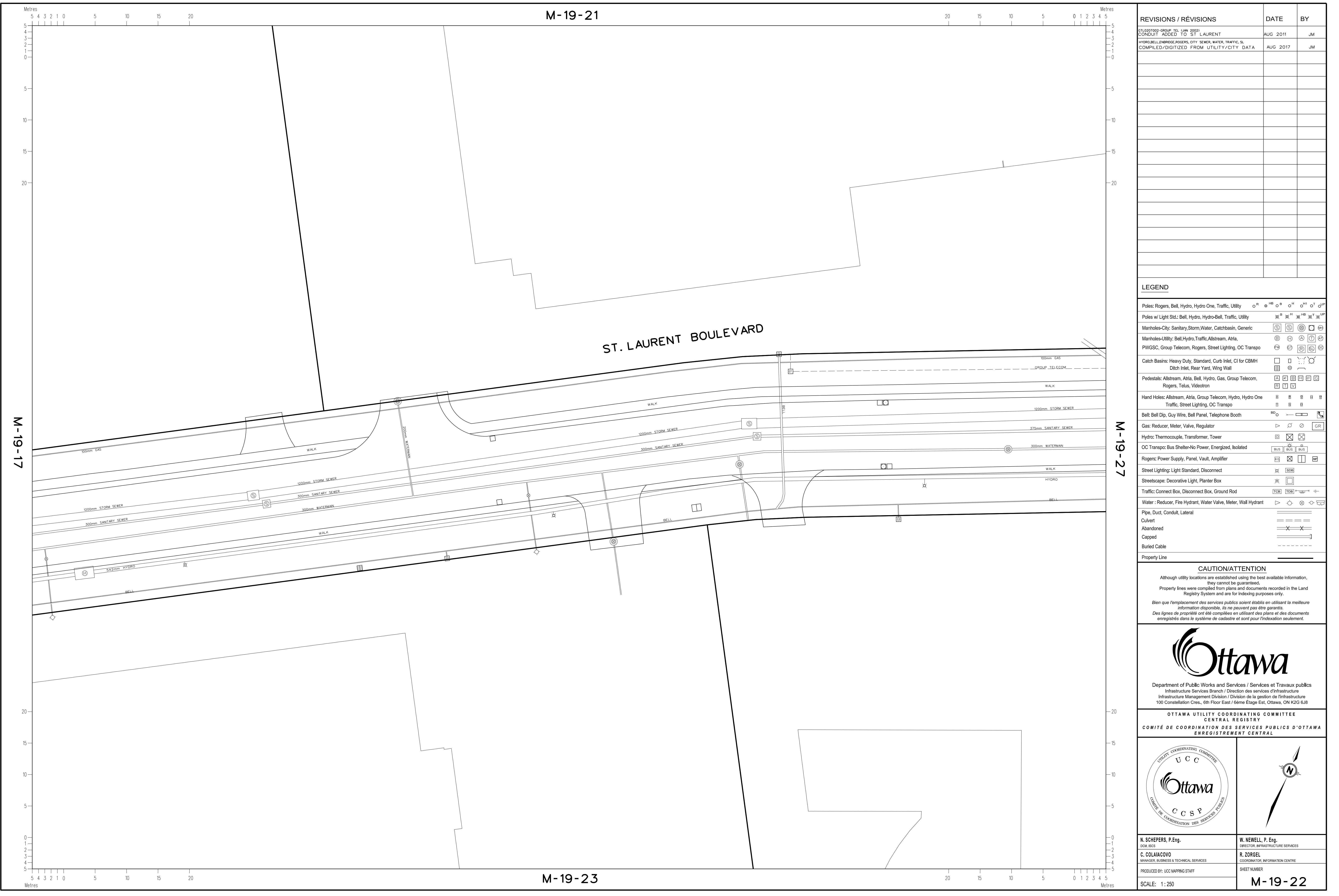
CONSTRUCTION DETAIL PLAN

PROJECT NO. 170721
DATE 13 DEC 2017

C902

APPENDIX H
St-Laurent Blvd. As-Built Drawings





APPENDIX I

Boundary Conditions

Guillaume Courtois

From: Baker, Adam <adam.baker@ottawa.ca>
Sent: December-13-17 9:18 AM
To: Guillaume Courtois
Cc: Oram, Cody
Subject: 2375 St-Laurent - Water Boundary Conditions
Attachments: 2375 St-Laurent Dec 2017.pdf

Follow Up Flag: Follow up
Flag Status: Flagged

Hi Guillaume,

Please find attached the boundary conditions requested for 2375 St-Laurent Blvd:

The following are boundary conditions, HGL, for hydraulic analysis at 2375 St-Laurent (zone 2C) assumed to be connected to the 305mm on St-Laurent (see attached PDF for location).

Minimum HGL = 124.5m

Maximum HGL = 130.6m

Max Day + Fire Flow (150 L/s) = 124.0m

These are for current conditions and are based on computer model simulation.

Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation.

If you have any questions, let me know.

Thanks,

Adam Baker, E.I.T.

Engineering Intern

Planning, Infrastructure and Economic Development Department - Services de la planification, de l'infrastructure et du développement économique

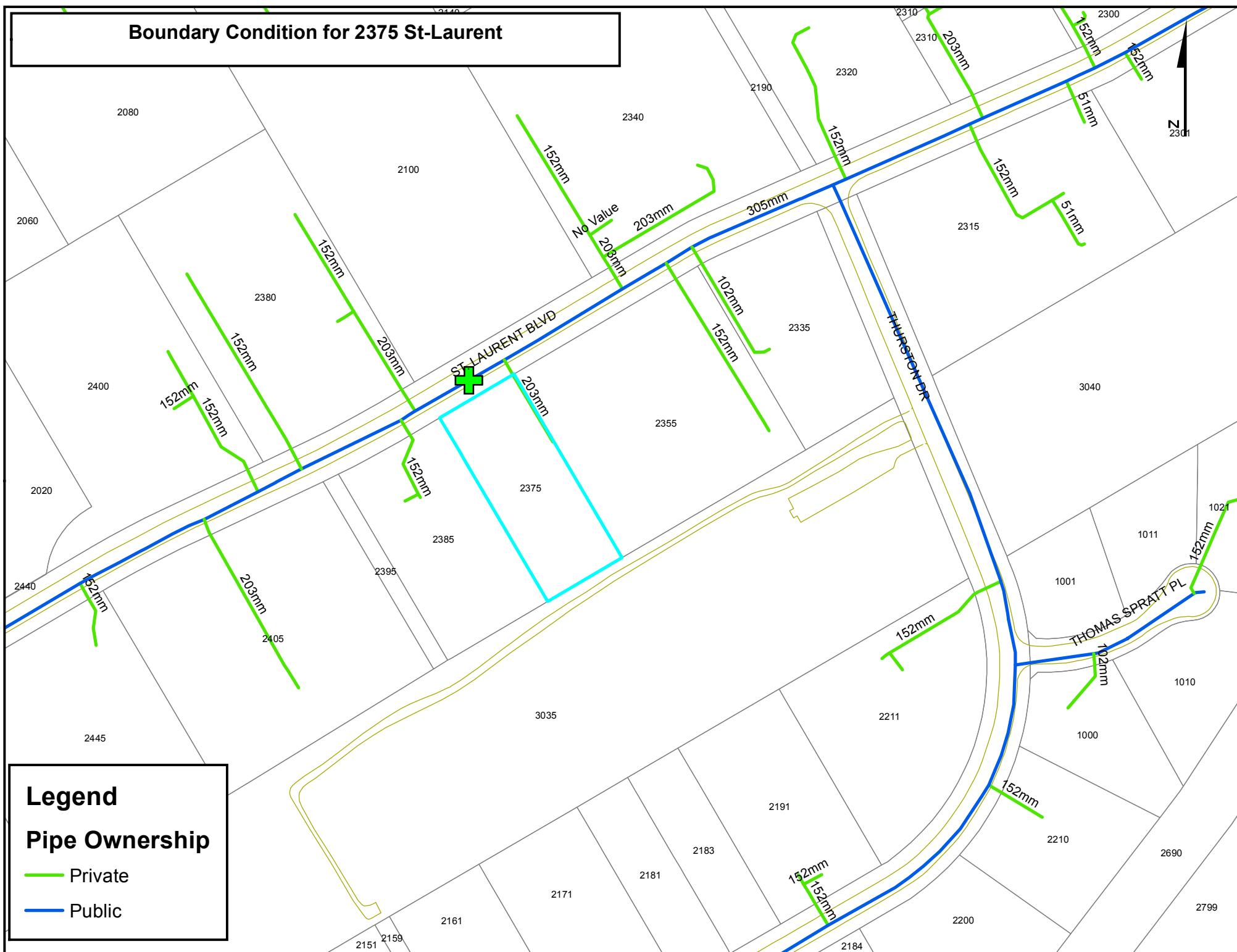
Development Review - South Branch

City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1

613.580.2424 ext./poste 26552, Adam.Baker@ottawa.ca

Boundary Condition for 2375 St-Laurent



APPENDIX J
Overland Ponding Volume Table

Overland Ponding Volume Report

Generated: 2017-12-07 14:40:49
By user: gcourtois
Drawing: W:\FILES 2017\170721\06 CivilDesign\Drawings\LRL Civil Plans\W:\FILES 2017\170721\06 CivilDesign\Drawings\LRL Civil Plans\170721-02.dwg

Volume Summary							
Name	Type	Cut Factor	Fill Factor	2d Area (hectares)	Cut (Cu. M.)	Fill (Cu. M.)	Net (Cu. M.)
CBMH1 PONDING VOLUME HWL83.47	full	1.00	1.00	0.02	0.00	15.90	15.90<Fill>
CBMH2 PONDING VOLUME HWL83.47	full	1.00	1.00	0.02	0.00	14.87	14.86<Fill>
CBMH3 PONDING VOLUME HWL83.47	full	1.00	1.00	0.01	0.00	6.83	6.83<Fill>
CBMH4 PONDING VOLUME HWL83.47	full	1.00	1.00	0.02	0.00	11.27	11.27<Fill>
CBMH5 PONDING VOLUME HWL83.47	full	1.00	1.00	0.02	0.00	13.91	13.91<Fill>

Totals				
		2d Area (hectares)	Cut (Cu. M.)	Fill (Cu. M.)
Total		0.09	0.01	62.78

* Value adjusted by cut or fill factor other than 1.0