

Environmental Compliance Application 473 Albert Street Ottawa, Ontario October 26, 2020

**Prepared for :** 

**InterRent No. 3 Limited Partnership** 

Submitted to :

**Ontario Ministry of the Environment, Conservation and Parks** 

Parsons Project # 477234



473 ALBERT STREET, OTTAWA, ON

ENVIRONMENTAL COMPLIANCE APPLICATION APPENDICES

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APPENDIX A | PROOF OF LEGAL NAME



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Declaration Form 3 under the Limited Partnerships Act Déclaration Formule 3 aux termes de la Loi sur les sociétés en commandite Page 1 of / de 2

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SCHEDULE - To Form 3, Declaration Under the Limited Partnerships Act
ANNEXE à la Formule 3 - Déclaration Loi sur les sociétés en commandite
Information Regarding General Partners
Renseignements sur le ou les commandités

Page \_\_\_\_\_\_\_ of / de \_\_\_\_\_\_

laration, name change, or signed by at least one ge	<i>le if the limited partnersl renewal. Complete as r neral partner.</i>	hip has more than one nany Schedules as re	e general partner. All genera quired. A change other than	al partners must be lis a name change, wit	ted and must sign a new dec hdrawal or dissolution must be
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#### DECLARATION OF TRUST

### RE: 473 ALBERT STREET, OTTAWA, ONTARIO

The undersigned, Curt Millar, Chief Financial Officer of InterRent Apartments Inc. (the "Corporation"), hereby declares and acknowledges that:

- The Corporation is the registered owner of the property municipally known as 473 Albert Street, Ottawa, Ontario (the "Property") and legally described in PIN 04112-0053 (LT);
- 2. The Corporation holds the Property in trust for InterRent No. 3 Limited Partnership (the "Owner").
- 3. The Corporation shall do all acts and take all actions in respect of the Property upon the instructions of the Owner.

Dated this 24<sup>th</sup> day of April, 2019.

InterRent Apartments Inc.

Per:

Curt Millar - CFO

I have authority to bind the Corporation.

**APPENDIX B | DETAILED PROJECT AND PROCESS DESCRIPTION** 

**Detailed Project and Process Description** 

473 Albert Street, Ottawa, ON

The proposed work includes the conversion of an existing high-rise building from the current office and restaurant use to a residential use. The domestic sewage will be conveyed to the existing City owned 300 mm diameter combined sewer in Albert Street. The existing storm (200mm diameter) and sanitary (200mm diameter) sewer laterals from the building to the combined sewer will be reused. The existing City combined sewer in Albert Street continues west through a local combined sewer until it drains to a collector combined sewer in the LeBreton Flats area.

The City is planning road, sewer and water renewal work for Albert Street that will include sewer separation at which time the sanitary and storm laterals for 473 Albert Street will be connected to the new separated sewers. This work is currently in the design phase and is planned for construction in the next couple of years.

The proposed total allowable release rate to the combined sewer has been reduced to control the 100 year flows (storm and sanitary) to the pre-development 2 year flows.

APPENDIX C | SITE PLAN



- STORM SEWER SYSTEM, ALL GRASSED AREAS MUST BE COMPLETED PRIOR TO THE REMOVAL OF THE FILTER FABRIC IN THE CATCH BASINS. 15. REMOVE FROM SITE ALL EXCESS EXCAVATED MATERIAL UNLESS OTHERWISE DIRECTED FROM THE ENGINEER. EXCAVATE AND REMOVE ALL ORGANIC MATERIAL AND DEBRIS LOCATED WITHIN THE PROPOSED BUILDING. PARKING AND ROADWAY LOCATIONS. ANY CONTAMINATED MATERIAL SHALL BE DISPOSED OF AT A LICENSED LANDFILL FACILITY.
- 16. THE APPROVAL OF THIS PLAN DOES NOT EXEMPT THE CONTRACTOR FROM THE REQUIREMENTS TO OBTAIN THE VARIOUS PERMITS/APPROVALS REQUIRED TO COMPLETE A CONSTRUCTION PROJECT, SUCH AS BUT NOT LIMITED TO; ROAD CUT PERMITS, SEWER PERMITS, WATER PERMIT, ETC.
- 17. AT PROPOSED UTILITY CONNECTION POINTS AND CROSSINGS (I.E. STORM SEWER, SANITARY SEWER, WATER, ETC.) THE CONTRACTOR SHALL DETERMINE THE PRECISE LOCATION AND DEPTH AND SIZE OF EXISTING UTILITIES AND REPORT ANY DISCREPANCIES OR CONFLICTS TO THE ENGINEER BEFORE COMMENCING WORK. PROTECT AND ASSUME RESPONSIBILITY FOR ALL EXISTING UTILITIES.
- 18. REFER TO ARCHITECT AND LANDSCAPE ARCHITECTS DRAWINGS FOR BUILDING, LANDSCAPE, AND HARD SURFACE AREAS AND DIMENSIONS, 19. CONTRACTOR IS RESPONSIBLE TO KEEP THE ROADS FREE AND CLEAN FROM MUD OR DEBRIS.
- INSPECT THEM FREQUENTLY AND CLEAN AND REPAIR OR REPLACE THE DETERIORATED STRUCTURES. AT THE END OF THE CONSTRUCTION PERIOD, THE CONTRACTOR IS RESPONSIBLE FOR REMOVAL OF THE . TEMPORARY STRUCTURES AND RECONDITIONING THE AFFECTED AREAS

- GEOTEXTILE FABRIC TO AVOID FINE PARTICLE TRANSPORT BY WIND AND/OR STREAMING RAIN WATER.
- CONTROL WIND-BLOWN DUST OFF SITE TO ACCEPTABLE LEVELS BY SEEDING TOPSOIL PILES AND OTHER AREAS TEMPORARILY (PROVIDE WATERING AS REQUIRED). FOR DUST CONTROL, CONTRACTOR TO APPLY CALCIUM CHLORIDE (TYPE I - OPSS 2501 AND CAN/CGSB-15-1) AND WATER WITH EQUIPMENT APPROVED BY THE OWNER'S REPRESENTATIVE AT RATE IN ACCORDANCE TO OPSS 506 WHEN DIRECTED BY OWNER'S REPRESENTATIVE.
- ALL EROSION CONTROL STRUCTURE TO REMAIN IN PLACE UNTIL ALL DISTURBED GROUND SURFACES HAVE BEEN DESTABILIZED EITHER BY PAVING OR RESTORATION OF VEGETATIVE GROUND COVER. SEDIMENT CAPTURE SILT SACKS MUST BE MAINTAINED AND CANNOT BE REMOVED UNTIL ALL LANDSCAPING AREAS ARE COMPLETED. NO ALTERNATE METHODS OF EROSION PROTECTION SHALL BE PERMITTED

- FILTER CLOTHS ON CATCH BASINS AND MANHOLE COVERS. INSPECT AND CLEAN CATCH BASIN SUMPS AND STORM SEWERS.

- 20. SUPPLY AND INSTALL ALL WATERMAIN ACCORDANCE WITH MOST CURRENT CITY O
- 21. ALL WATER MAIN TO BE INSTALLED AT MININ
- 23. CONCRETE THRUST BLOCKS AND RESTRA
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APPENDIX D | GEOREFERENCED LOCATION PLAN





SKETCH 1: 473 ALBERT STREET OTTAWA, ON GEO-REFERENCING PLAN

# PROJECT: 477234

APPENDIX E | ZONING MAP





SKETCH 2: 473 ALBERT STREET OTTAWA, ON ZONING MAP

# PROJECT: 477234

**APPENDIX F |** DETAILED DESCRIPTION OF THE PROPOSED WORKS

Detailed Description of the Proposed Works

473 Albert Street, Ottawa, ON

# <u>SEWERS</u>

No proposed sewers. Existing sanitary (200mm diameter) and storm (200mm diameter) laterals will be reused. Both sewer laterals drain to the existing City combined sewer (300mm diameter).

# **STORMWATER**

Four (4) controlled roof drains will provide detention on the roof to restrict the peak release rate during the 1:100 year design storm to 6.1 L/s, discharging to the existing storm service.

The remaining roof drains as well as the surface drain that collects stormwater from the amenity space at ground level behind the building will all drain to a stormwater cistern located within the underground parking garage. The 57.4 m<sup>3</sup> tank will provide detention to restrict the peak release rate during the 1:100 year design storm to 4.9 L/s. The stormwater will be pumped up to the existing gravity storm service.

There is also a narrow area along the west property line that will drain to Albert Street by sheet flow uncontrolled at 2.0 L/s during the 1:100 year design storm.

APPENDIX G | DESIGN BRIEF



# Site Servicing and Stormwater Management Report 473 Albert Street Ottawa, Ontario October 22, 2020

**Prepared for :** 

**InterRent No. 3 Limited Partnership** 

Submitted to :

**City of Ottawa** 

Parsons Project # 477234



delivering a better world

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APPENDIX H   Pre-Development Drainage Plan
APPENDIX I   Storm Sewer Design Sheet
APPENDIX J   Stormwater Management Calculations and Roof Drain Declaration

## **1.0 INTRODUCTION**

#### **1.1** Site Description and Proposed Development

InterRent No. 3 Limited Partnership (InterRent) has retained Parsons Inc. to prepare a Site Servicing and Stormwater *Management Report* in support of the conversion of an existing high-rise office building into a residential rental building at 473 Albert Street. **Figure 1** shows the site location.

There is an existing access driveway from Albert Street at the west side of the property that is covered by the building. The driveway leads to a ramp for the existing two level underground parking garage as well as to a small open area behind the building, historically used as parking. The existing driving access to the surface parking at the back of the building will be converted to pedestrian only access. This open area behind the building will be converted to amenity space including outdoor workout space, bicycle storage, terrace space for residents and a fenced in dog area. The access to the underground parking garage will remain. The parking garage will provide 47 vehicle parking spaces. There will also be at 87 bicycle parking spots divided between interior and exterior spaces. The parking garage extends beyond the building footprint towards the back and side property lines. Therefore the open area at the back of the building at ground level is over the parking garage structure.

The proposed building breakdown is listed in the table below. There will be residential units on floors 1 through 11. There will be amenity space on Floor 12. There are partial floors on Levels 13 and 14 that are mechanical penthouse space.

Table 1: Proposed Building Breakdown

#### 473 ALBERT STREET (12 STOREYS)

Gross Floor Area (Below and Above Grade)	17,711.54 m <sup>2</sup>
Gross Leasable Area (Residential)	9,311.50 m <sup>2</sup>

The existing parcel is roughly 0.17 ha in size with a zoning of Residential Fifth Density Zone. The ground elevation behind the building varies between approximately 74.12 m and 73.20 m and drains west towards a parking drain. The driveway between the ramp and Albert Street drains towards Albert Street.

The 473 Albert Street property is surrounded by the features described below.

- North: High rise buildings (residential apartments and office space) facing Queen Street
- East: Albert at Bay Suite Hotel
- South: low rise residential buildings
- West: The Gardens Condo Development

#### Figure 1: 473 Albert Street, Ottawa Key Plan



#### 1.2 Guidelines and Background Documents

The 473 Albert Street design is in accordance with the documents below.

- Ottawa Design Guidelines Water Distribution, 1st Edition, July 2010 (OWG and technical bulletins)
  - o Technical Bulletin ISD-2010-2, December 15, 2010
  - o Technical Bulletin ISDTB-2014-02, May 27, 2014
  - o Technical Bulletin ISTB-2018-02, March 21, 2018
- Sewer Design Guidelines, City of Ottawa, 2<sup>nd</sup> Edition, October 2012 (OSG and technical bulletins)
  - o Technical Bulletin ISDTB-2012-6, October 31, 2012
  - o Technical Bulletin ISDTB-2014-01, February 5, 2014
  - o Technical Bulletin PIEDTB-2016-01, September 6, 2016
  - Technical Bulletin ISTB-2018-01, March 21, 2018
  - Technical Bulletin ISTB-2019-02, July 8, 2019
- Water Supply for Public Fire Protection, Fire Underwrites Survey, 1999 (FUS)
- City of Ottawa Park and Pathway Development Manual (2017)
- City of Ottawa Accessibility Design Standards (2015)
- Ottawa Standard Tender Documents (2019)
- Ontario Provincial Standards for Roads & Public Works (2019)
- Ontario Building Code (2017)

#### **1.3** Existing Infrastructure

The site is currently developed and serviced by municipal infrastructure. The exiting municipal infrastructure surrounding the property is shown in **Figure 2**.

The existing municipal infrastructure on Albert Street consists of:



- A 152 mm UCI watermain (1933) (abandoned)
- A 203 mm UCI watermain (1933)
- A 300 mm CONC combined sewer (1935)

The building currently has a water service, a storm service and a sanitary service. The storm and sanitary services both drain to the City's combined sewer. The water service is supplied by the 203 mm diameter City watermain.

There is planned road, water and sewer renewal works identified for Slater Street, Albert Street and Bronson Avenue which is currently under design and planned for construction in the next 2 – 4 years. This work will include separation of the existing combined sewer and upgrades to the watermain network.

Figure 2: Existing Municipal Infrastructure Surrounding the Site



#### **1.4 Consultation and Permits**

The City of Ottawa and agencies were consulted for this project. A summary of the consultations is provided below; copies of the correspondences and/or minutes are provided in **Appendix A**.

#### CONSULTATIONS

#### City of Ottawa

The City of Ottawa provided the following criteria for the proposed development:

- The allowable release rate (storm and sanitary) will be the 2-year pre-development rate;
- Runoff coefficient will need to be determined based on existing conditions but be no more than 0.4;
- Time of concentration should be 20 minutes, or can be calculated, but should not be less than 10 minutes;



- Any storm events greater than 2-year, up to 100-year, and including the 100-year storm event must be detained on site;
- Two separate sewer laterals will be required;
- Foundation drains are to be independently connected to the sewer, unless being pumped with appropriate back up power, sufficient sized pump and backflow prevention;
- Roof drains are to be connected downstream of any incorporated ICD within the stormwater system or pumped with the lateral being appropriately sized;
- Surface water to be retained on property and conveyed to ROW, approved on-site storage or directly to City infrastructure;
- A second drinking water service to be provided where the average daily demand exceeds 50 m<sup>3</sup>/day;
- FUS fire flow criteria to be used unless a low-rise building, where OBC requirements may be applicable;
- Above and below ground storage is permitted although uses ½ peak flow rate or is modeled; and
- There must be at least 15 cm of vertical clearance between the spill elevation and the ground elevation at the building envelope that is in proximity of the flow route or ponding area.

#### Rideau Valley Conservation Authority (RVCA)

Parsons contacted the RVCA who indicated that no water quality protections will be required as the site will remain rooftop drainage and the existing surface parking will be converted to open amenity space. The communication with the RVCA is included in **Appendix A**.

#### Ministry of the Environment, Conservation and Parks (MECP)

An Environmental Compliance Approval (ECA) is required for this site as the municipal infrastructure in the area is not fully separated, the two separate building service laterals drain to a combined sewer.

#### PERMITS AND APPROVALS

The City of Ottawa and the various agencies consulted require the approvals and permits listed below. The City of Ottawa Development Servicing Study Checklist is included in **Appendix B**.

City of Ottawa

- Road Cut Permit
- Commence Work Order
- Water permit
- Water Data Card
- Flow Control Roof Drainage Declaration (included in Appendix J)

Ontario Ministry of the Environment, Conservation and Parks

• Environmental Compliance Approval

#### 2.0 WATER SERVICING

#### 2.1 Proposed Water Servicing

The proposed drinking water servicing approach includes providing two 152 mm diameter water services. The existing 152 mm diameter service from the City's 203 mm diameter watermain will be maintained. A second 152 mm diameter water service will be provided to the City's 203 mm diameter watermain. A new 203 mm water valve chamber will be installed on the main line separating the two water services.

Drawing C101, in Appendix C, shows the existing and proposed water distribution network.

#### 2.2 Design Criteria

The proposed water servicing network has been designed in general conformance with OWG as amended by the City of Ottawa by its technical bulletins.

The system pressure criteria under normal and various operating conditions are listed in the table below.

OPERATING CONDITIONS	PRESSURE CRITERIA	
	KPa	psi
Average Daily Demand		
minimum to maximum	276-552	40-80
Desirable range	350-480	50-70
Peak Hourly Demand		
minimum to maximum	276-552	40-80
Desirable range	350-480	50-70
Maximum Daily Demand + Fire Flow		
minimum	140	20

Table 2: Water System Pressure – Criteria

The City of Ottawa provided the watermain boundary conditions for the existing 203 mm diameter watermain, as shown in the table below. A copy of the correspondence is in **Appendix D**. The City noted that the watermains on Bronson, Albert and surrounding streets are planned to be upgraded but the planned sizes are not known yet so boundary conditions for these future conditions are not known at this time.

 Table 3: 203mm Diameter Watermain Boundary Conditions

MINIMUM HGL	MAXIMUM HGL	MAXIMUM DAY + FIRE FLOW
106 m	115.5 m	87.8m
46 psi	60 psi	20 psi
318 KPa	411 KPa	140 KPa

\*The available fire flow = 115 L/s assuming a residual of 20 psi and a ground elevation of 73.5 m.

The boundary conditions provided demonstrate that the available pressure ranges from approximately 46 psi to 60 psi during normal operating conditions but is limited during fire flow conditions.

The fire flow was calculated using the FUS with the following parameters:

Type of construction:	non-combustible construction
Occupancy Type:	limited combustible
Sprinkler Protection:	fully monitored, automatic sprinkler system from standard water supply

The OWG requires that "Service areas with a basic day demand greater than 50 m<sup>3</sup>/day (about 50 homes) shall be connected with a minimum of two watermains, separated by an isolation valve, to avoid the creation of a vulnerable service area. Individual residential facilities with a basic day demand greater than 50 m<sup>3</sup>/day shall be connected with a minimum of two water services, separated by an isolation valve, to avoid the creation of a vulnerable service area." Therefore, a new 152 mm water service will be provided to the building, connected to the existing 203 mm watermain on Albert Street to provide redundancy to the existing 152 mm water service. An isolation valve and chamber will be installed on the City's 203 mm watermain to separate the two services.



The new water service will be installed with a minimum cover of 2.4 m where possible. Should there be less than 2.4 m cover or separation from an open structure, the pipes will be insulated as per City Standard Drawings W22 and W23.

#### 2.3 Calculations and Simulation Results

The table below summarizes the anticipated maximum water demand for the proposed building conversion. Detailed calculations for the water demand and fire flow are in **Appendix E**.

Table 4: Water Demand Rates					
BUILDING	AVERAGE DAY DEMAND (ADD)	MAX DAILY DEMAND (MDD)	PEAK HOURLY DEMAND (PHD)	FIRE FLOW DEMAND (FF)	MDD+FF
	L/s	L/s	L/s	L/s	L/s
473 Albert	1.09	5.08	7.71	182	186.6

High pressure is not an issue on this site as the boundary conditions are below 80 psi. Therefore, pressure reducing valves will not be required.

The required fire flow can be provided by five (5) nearby hydrants at the following locations:

- Two hydrants on Albert Street (within 75 m of the building)
- Two hydrants on Albert Street and one hydrant on Bronson, just north of Albert (within 150 m of the building)

Figure 3: Existing Hydrants



PARSONS

The OBC and Fire Marshal's Office method was used to calculate the fire protection water demand. As per the Office of the Fire Marshal OFT-TG-03-1999, for sprinklered buildings, an adequate fire protection water supply means a reliable water supply providing sufficient water flow for the sprinkler systems in terms of pressure, volume, and duration to limit fire growth until the fire department arrives to suppress the fire. This automatic protection is expected to provide time for the evacuation of buildings, assist the fire department in preventing fire spread to adjacent buildings, limit the environmental impact of fires, and provide significant property protection.

There are 5 fire hydrants within the vicinity of the site, 2 hydrants are within 75m and 3 hydrants within 150m. Due to the age of the watermains, the City completed a multi-hydrant analysis and determined the total available flow from the five hydrants is **215 L/s**. Therefore, the required fire flow per OBC plus max day demand of 187.2 L/s is available within the existing system. Please refer to **Appendix E** for the correspondence from the related correspondence from the City of Ottawa.

#### 2.4 Summary and Conclusions

A second 152 mm water service will be provided from the existing 203 mm watermain on Albert Street.

The water pressures, under average day demand, peak hour demand, are within the allowable pressure range specified by the City of Ottawa.

As per the City's hydrant flow test data, the surrounding hydrants meet the required fire flow demands of the proposed building.

The proposed water service is shown on Drawing C101 in Appendix C.

#### 3.0 SANITARY SERVICING

#### 3.1 Proposed Sanitary Servicing

The existing sanitary service was inspected by Clean Water Works. The internal plumbing was noted to be 150 mm diameter cast iron pipe. The service lateral to the sewer in the road is a 203 mm diameter transite pipe. The pipe was inspected before and after flushing. No deficiencies were noted. Therefore, the existing sanitary service will be maintained. It is likely that this service will be replaced to the property line/building face as part of the City's planned sewer and water upgrades in the next few years. The CCTV reports, including references to pipe materials and sizes, are included in **Appendix F.** It is noted that the interior plumbing is in poor condition and will be completely replaced.

#### 3.2 Design Criteria

The proposed sanitary sewer flow has been designed in general conformance with the OSG and its technical bulletins.

The sanitary design flow rate is the peak flow plus the peak extraneous flow. The table below presents the values for the average flow, peak factor and peak extraneous flows used in the sanitary servicing calculations for the residential development.

DEVELOPMENT TYPE	AVERAGE Sanitary Flow	UNIT	PEAK FACTOR	PEAK EXTRANEOUS FLOW	
Residential	280	L/c/d	Harmon Equation	0.33 L/s/gross ha	
Amenity Space	5	L/m²/d	1.0		

Table 5	5: Sar	nitarv	Design	Flows	Criteria

#### 3.3 Calculations and Results

The sanitary design flows and sewer pipe design spreadsheets, included in **Appendix G**, shows the flows from the proposed converted building (2.98 L/s) as well as the estimated existing flows (1.56 L/s). The sanitary flows increased due to the proposed residential use of the building. The increase in the sanitary flows will be considered as part of the total allowable



release rate from the site to the combined sewer. The existing sanitary service is sufficient to accommodate the proposed sanitary flows.

There will be additional sanitary flows from the parking garage sump which will collect the drainage collected within the garage from snow melt off cars, etc. The discharge rate from the sump pump is not known at this time but is expected to be negligible compared to the sanitary flows from the domestic use.

#### 3.4 Summary and Conclusions

The existing 203 mm diameter sanitary lateral will be maintained for the proposed development.

#### 4.0 STORM SERVICING AND STORMWATER MANAGEMENT

#### 4.1 Existing Storm Servicing

The existing site has a parking drain at the northwest corner of the site which drains into the underground parking garage and plumbing system. The site generally drains northeast to southwest with the existing driveway access draining towards the City right-of-way. The topography differs with the northeastern parking portion and driveway access being fairly flat with slopes less than 2% and the northwestern parking portion being sloped around 4%. There is also a narrow strip of land between the west side of the building and the west property line. There is no storm infrastructure in this area, it drains through surface flow.

The existing storm service was inspected by Clean Water Works. The internal plumbing was noted to be 100 mm and 152 mm diameter cast iron. The storm service lateral to the City sewer is a 203 mm diameter transite pipe. No deficiencies were noted. Therefore, the existing storm service will be maintained. It is likely that this service will be replaced to the property line/building face as part of the City's planned sewer and water upgrades in the next few years. The CCTV reports, including references to pipe materials and sizes, are included in **Appendix F**. It is noted that the interior plumbing is in poor condition and will be completely replaced.

It is our understanding that the existing building has a foundation drain system that drains to a sump and pump. This configuration will remain.

The site existing drainage area is shown on Figure A: Pre-development Drainage Plan in Appendix H.

#### 4.2 Proposed Storm Servicing

The storm system will maintain the existing parking drain and reuse the existing storm lateral that connects to the 300 mm diameter combined sewer on Albert Street.

The roof drains on Levels 12, 13 and 14 will have a combination of controlled and uncontrolled roof drains. The controlled roof drains will drain directly to the existing storm service. The uncontrolled roof drains and the existing parking drain will drain to a cistern, to be located within the underground parking garage. The narrow area on the west side of the building will continue to flow uncontrolled on the surface. **Drawing C102**, in **Appendix C** depicts the roof drains and their associated catchment areas.

The design approach for the stormwater management is to ensure that the post-development peak flows do not exceed the existing 2-year pre-development release rate flow.

Drawing C101, in Appendix C depicts the boundaries of the post-development drainage areas.

#### 4.3 Design Criteria

The proposed storm sewer system has been designed in general conformance with the OSG and its technical bulletins, plus more specific requirements from the City of Ottawa.

The criteria below were provided in part by the City of Ottawa and RVCA. These agencies correspondence are located in **Appendix A**.



The design criteria for the site includes the following:

- Stormwater management for the site shall be based on the 2-year storm event using the IDF information derived from the Meteorological Services of Canada rainfall data, taken from the MacDonald Cartier Airport, collected 1966 to 1997;
- ii. The pre-development runoff coefficient or a maximum equivalent 'C' of 0.4, whichever is less (8.3.7.3);
- iii. A calculated time of concentration (Cannot be less than 10 minutes);
- iv. Flows to the storm sewer in excess of the 2-year storm release rate, up to and including the 100-year storm event, must be detained on site;
- v. The Rational Method is used to calculate the allowable peak flow to discharge into the receiving combined sewer systems and the runoff volume to be retained on site;
- vi. IDF curve equations used with the Rational formula:
  - a. 2-year =732.951/(Tc+6.199)<sup>0.810</sup>
  - b. 100-year = 1735.688/(Tc+6.014)<sup>0.820</sup>

The Rational Method uses runoff coefficients for various surfaces. The table below shows the runoff coefficients chosen in this study. The runoff coefficient for a 100-year storm event is increased by 25% per the OSG to a maximum of 1.0.

	Table 6:	Rational	Method	Runoff	Coefficients
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SURFACE	5-YEAR COEFFICIENT	100-YEAR COEFFICIENT
Asphalt/Building/Concrete	0.90	1.00

#### 4.4 Allowable Release Rate

The allowable release rate for the 0.17 has ite developed was calculated using the rational method formula based on the 2-year flow and the existing runoff coefficient of 0.4.

where

Q = Flow rate (L/s) C = Runoff coefficient i = Rainfall intensity (mm/hr) A = Area (ha)

The resultant allowable release rate is **14.3 L/s**.

The allowable release rate is a combination of the sanitary and storm flows as the flows are conveyed to a combined sewer. As a result, the allowable release rate for the storm flows is decreased by the equivalent amount of sanitary flows that are additional compared to the flows associated with the existing usage. The existing building usage results in an estimated sanitary flow of 1.56 L/s. The proposed building usage results in an estimated sanitary flow of 2.98 L/s. This represents an increase of 1.42 L/s in the sanitary flows. Therefore, the allowable storm release rate is decreased by 1.42 L/s to a total of 12.9 L/s.

#### 4.5 Storm Sewer Design

Calculations showing the storm sewer design are included in **Appendix I**. The storm sewer design spreadsheet is based on the Rational Method and Manning formula and was used to calculate the design flow and required pipe size. Ottawa IDF information for the 2-year design storm was used to calculate the peak flows.



Drawing C101, in Appendix C shows the drainage areas.

#### 4.6 **Stormwater Management**

The on-site storm water management has been designed to attenuate the 2-year and 100-year post-development flow rates to the allowable post-development flow rates as shown in **Appendix J**.

#### DRAINAGE AREA WS-01 (CONTROLLED ROOF DRAINS)

A portion of the roofs, generally the areas on the east side, will provide stormwater storage through the use of controlled roof drains, Watts Adjustable Accutrol roof drains. The drainage area per roof drain is shown in the table below. The roof drains, including the associated ponding areas, are shown on **Drawing C102**, in **Appendix C**.

Roof Drain	Controlle	Controlled Flow (L/s)		Max Ponding Depth (mm)		Storage Volume (m <sup>3</sup> )	
Number	1:5 Year	1:100 Year	1:5 Year	1:100 Year	1:5 Year	1:100 Year	
CFRD 8	0.95	1.53	76.3	117.4	0.75	2.75	
CFRD 10	0.99	1.51	79.6	121.9	1.03	3.71	
CFRD 11	1.02	1.55	81.9	124.6	1.29	4.55	
CFRD 12	1.02	1.49	81.9	123.3	1.04	3.54	
Total	3.98	6.08					

Table 7: Roof Drain Controlled Flows and Storage

The controlled flow from these sub-catchment areas will be **4.0 L/s** for the 2-year event and **6.1 L/s** for the 100-year event. The controlled roof drains will be connected directly to the storm service, inside the building.

#### DRAINAGE AREA WS-02 (UNCONTROLLED ROOF DRAINS)

The remaining portions of the roofs will drain through uncontrolled roof drains. These flows will be directed to the cistern within the underground parking garage.

#### DRAINAGE AREA WS-03 (GROUND LEVEL AMENITY SPACE BEHIND THE BUILDING)

The post-development flow for this sub-catchment area behind the building will be collected using the existing parking drain. The flows will be directed to the cistern within the underground parking garage.

The flows from drainage areas WS-02 and WS-03 will be directed to the cistern. The stormwater storage tank will be pumped to the existing storm service at a maximum allowable flow rate of **4.9 L/s.** The required storage volume of the storage tank is  $11.6 \text{ m}^3$  and  $44.9 \text{ m}^3$  during the 2-year and 100-year storms respectively. As per the OSG, the storage cistern is being sized to accommodate the 100-year storm + 20% stress test, as a result the required volume is **57.4 m**<sup>3</sup>. No ponding on the surface is planned for the site. All stormwater is being controlled at the roof level or within the cistern in the underground parking garage, including the volumes for the 100 year storm + 20% stress test.

#### DRAINAGE AREA WS-04 (GROUND LEVEL TO THE WEST OF THE BUILDING)

The narrow strip of land between the west side of the building and the west property limit will drain by sheet flow, uncontrolled to Albert Street. The uncontrolled flow from this area is **0.8 L/s** for the 2-year event and **2.0 L/s** for the 100-year event.



#### 4.7 Stormwater Quality

The RVCA has indicated that onsite water quality treatment will not be required as the stormwater is all captured on the roof or in the open space behind and beside the building, there are no surface parking areas and driving isles.

#### 4.8 Major Overland Flow

The major overland flow route generally flows to the southwest with most of the site exiting to the City right-of-way.

#### 4.9 Summary and Conclusions

The existing storm service will be maintained and will convey the flows from the controlled roof drains as well as the pumped flows from the cistern. The narrow area along the west side of the property will continue to flow uncontrolled to Albert Street. The total flow from the site during the 100-year event will be controlled to 12.9 L/s which is equivalent to the predevelopment 2-year event.

#### 5.0 SEDIMENT AND EROSION CONTROL

To mitigate the impacts due to erosion and sedimentation during construction, erosion and sediment control measures shall be installed and maintained throughout the duration of construction. Measures shall only be removed once the construction activities are complete, and the site has stabilized.

The measures will include:

• Siltsack® shall be installed between the frame and cover of existing and new catchbasins and maintenance holes, to minimize sediments entering the storm drainage system. These shall remain in place until construction is complete.

#### 6.0 **CONCLUSIONS**

This report outlines the proposed servicing and stormwater management design for the conversion of the existing building at 473 Albert Street, Ottawa, ON.

The proposed drinking water system will include the use of the existing 152 mm diameter water service as well as the construction of a second 152 mm diameter water service and the installation of a new line valve on the City watermain between these two connections.

The proposed sanitary sewer system will consist of the reuse of the existing sanitary service to convey flows to the existing combined sewer.

Stormwater runoff from the site will include a combination of controlled roof drains as well as uncontrolled roof drains and the ground level amenity space behind and to the west of the building. The uncontrolled flows from the roof and behind the building will be directed to a 57.4 m<sup>3</sup> cistern to be located within the underground parking garage. The flows in the cistern will be pumped to the existing storm service at a maximum allowable rate of 4.9 L/s. The existing narrow area to the west of the building will continue to flow uncontrolled to Albert Street.

#### Prepared by:

ROFESSIONAL ROFESSIONAL M.E. MACSWEEN R 100104372 ROUNCE OF ONT ME Reviewed by:

Mathew Theiner, P.Eng., ing.

Meghan MacSween, M.Eng., P.Eng.

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APPENDIX A | CORRESPONDENCE

# 473 Albert: Preconsultation Meeting

Conversion of existing high-rise office building into a mixed-use building (~126 dwelling units, office and restaurant uses)

# **Christopher Moise (Design) Comments:**

- Consider fenestration / cladding / treatment at grade
- Consider location of loading area
- Re-consider 'dog area' at grade in rear yard
- Building & Façade
  - Clarify 'brutalist' characterization
  - How is the building 'residential' from the exterior
  - Consider balconies (juliette or otherwise)
  - Appropriateness of exposing concrete (especially as an <u>improvement)</u>
- UDRP for DPA not required

# John Bernier (File Lead, Planner)

- Height limit is 37 metres: is 'amenity penthouse' a projection (**if no=Variance**)
- Restaurant terrace (outdoor comm. patio) is prohibited (**MV or Minor ZBA**)
- Minor variances required for existing building setbacks
- Loading space (in ROW) not functional
  - Make reference to 'Downtown Moves'
    - Which considers 2 loading spaces
    - Considers tree plantings
    - 'DM' implementation to be determined
    - J. Bernier to provide timeline for DM
- Encroachment agreement for (new) canopy must be reviewed
- Dog Run is there a more appropriate use for those lands?
- Complex Site Plan Application:
  - Timeline: +4 months
    - o ZBA v. MV different timelines
    - <u>MV only after conclusion of first round of circulation/issue</u> resolution

## E. Johnson (CLV Group)

- Existing encroachment agreement

# Wally Dubyk (Transportation)

- 1.25 metre right-of-way protection to be conveyed
- RE: **TIA Screening:** 2 triggers for step 2 guidelines
- Multimodal service must be analyzed
- Must address reduction of parking spaces on site

- Must review docking/ROW layby
- <u>C. Gordon (Applicants Transportation Consultant, In Response):</u>
  - $\circ$  Initial morning trip generation (ex. Office vs. residential), 200 v. ~80
  - Prefer to avoid full TIA process: proposes Supplement to 'Step 1'
- Dubyk: Supplement to Step 1 as alternate 'works'
- Must submit a Construction Management Plan

## Shawn Wessel (Infrastructure)

- ECA required (combined sewer dates to 1935)
- Services on site, require CCTV Report
- SWM increase, SWM guidelines have changed
  - Rear yard may increase release rate
- Roof Drains: must see existing drain detail
- Wind Study Required
- Record of Site Condition Required
- Enbridge requires new pressure relief valve (to be shown on plans)
- Noise Study Req'd: Height and location of building
  - Must include stationary noise sources
  - Must include amenity areas
  - Fenestration reference FDC Rating
- Road & Sewer & Water Renewal Planned for Albert (likely sewer separation)
- Contact RVCA RE: restrictions
- Existing restaurant: sanitary needs grease trap
- Oil & grit separator: TBD for parking garage
- S.W. to provide **boundary conditions** for SWM Consultant
- Fire hydrant analysis Secondary water service required
- Trees: confirm appropriate species (in ROW) given services
- Must confirm if services in surcharge condition

### Infrastructure:

A 152 mm dia. UCI Watermain (c. 1933) is available on the North side of Albert St.

A 203 mm dia. UCI Watermain (c. 1933) is available on the South side of Albert St.

A 300 mm dia. Conc. Combined Sewer (c. 1935) is available on Albert St., which is conveyed to the Booth St. Trunk and then onto the Interceptor Sewer.

The following apply to this site and any development within a <u>combined sewer</u> area:

- Total (San & Stm) allowable release rate will be 2-year pre-development rate.
- Coefficient (C) of runoff will need to be determined as per existing conditions but in no case more than 0.4
- TC = 20 minutes or can be calculated TC should be not be less than 10 minutes, since IDF curves become unrealistic at less than 10 min.
- Any storm events greater than 2 year, up to 100 year, and including 100-year storm event must be detained on site.
- Two separate sewer laterals (one for sanitary and other for storm) will be required.

### An MECP ECA will be required.

Please have applicant provide one copy of the following for our review: MECP ECA Application Form - Direct Submission tied to SPC Fees - Certified Cheque made out to "Ministry of Finance" Proof of Applicant's Identification (if no Certificate of Incorporation) Certificate of Incorporation (if Applicable) NAICS Code (If Applicable) Plan & Profile Grading and Servicing Plans Survey Plan Pipe Data Form Draft ECA (City of Ottawa Expanded Works Form) Source Protection Policy Screening & Significant Threat Report Sewer Drainage Area Plan SWM Report Services Report Geotechnical Report & any other supportive documentation Correspondence: City of Ottawa including ROW, Water Resources Dept., ISD etc., MNR, Conservation Authority & MECP.

Please note that once the review has been completed and the Sr. Engineer is satisfied and ready to sign off on the application, after the PM recommendations 3 final bound copies
including 3 flash drives will be required to accompany the applications with MECP and for City of Ottawa records.

Footer of ECA Application should have reference #: 8551E (2019/05)

#### Please also note:

Foundation drains are to be independently connected to sewermain (separated or combined) unless being pumped with appropriate back up power, sufficient sized pump and back flow prevention. Water Resources Dept. to comment if connection is to a combined sewer.

Roof drains are to be connected downstream of any incorporated ICD within the SWM system or pumped with the lateral being appropriately sized.

#### RVCA:

Applicant to contact Rideau Valley Conservation Authority (RVCA) for possible restrictions due to quality control. Provide correspondence in Report.

Grease trap required for restaurant if not already installed.

Trees – please ensure proposed trees do not conflict with existing or proposed services. Deep root plantings not permitted. Services to be outside critical root zone (CRZ).

Surface water to be retained on property and conveyed to ROW, approved on-site storage or directly to City infrastructure. Refer to calculated allowable release rate and this sites SWM.

Existing or proposed canopy at front of building: Please provide details on how this canopy will drain and if applicable, connect to City infrastructure. Show DS location on plans and speak to this in the SWM Report.

Provide roof plan showing drain and scupper locations including control information.

Provide all control information including manufacturing specifications in the SWM Report.

Water Supply Redundancy – Fire Flow:

Applicant to ensure that a second service with an inline valve chamber be provided where the average daily demand exceeds 50 m<sup>3</sup> / day (0.5787 l/s per day) FUS Fire Flow Criteria to be used unless a low-rise building, where OBC requirements may be applicable.

Where underground storage (UG) and surface ponding are being considered:

Show all ponding for 5 and 100 year events

Above and below ground storage is permitted although uses ½ Peak Flow Rate or is modeled. Please confirm that this has been accounted for and/or revise.

#### Rationale:

The Modified Rational Method for storage computation in the Sewer Design Guidelines was originally intended to be used for above ground storage (i.e. parking lot) where the change in head over the orifice varied from 1.5 m to 1.2 m (assuming a 1.2 m deep CB and a max ponding depth of 0.3 m). This change in head was small and hence the release rate fluctuated little, therefore there was no need to use an average release rate.

When underground storage is used, the release rate fluctuates from a maximum peak flow based on maximum head down to a release rate of zero. This difference is large and has a significant impact on storage requirements. We therefore require that an average release rate be used to estimate the required volume. Alternatively, the consultant may choose to use a submersible pump in the design to ensure a constant release rate.

In the event that there is a disagreement from the designer regarding the required storage, The City will require that the designer demonstrate their rationale utilizing dynamic modelling, that will then be reviewed by City modellers in the Water Resources Group.

Note that the above will added to upcoming revised Sewer Design Guidelines to account for underground storage, which is now widely used.

Further to above, what will be the actual underground storage provided during the major (100 year) and minor (2 year) storm events?

Please provide information on UG storage pipe. Provide required cover over pipe and details, chart of storage values, capacity etc. How will this pipe be cleaned of sediment and debris?

Note - There must be at least 15cm of vertical clearance between the spill elevation and the ground elevation at the building envelope that is in proximity of the flow route or ponding area. The exception in this case would be at reverse sloped loading dock locations. At these locations, a minimum of 15cm of vertical clearance must be provided below loading dock openings. Ensure to provide discussion in report and ensure grading plan matches if applicable.

Provide information on type of underground storage system including product name and model, number of chambers, chamber configuration, confirm invert of chamber system, top of chamber system, required cover over system and details, interior bottom slope (for self-cleansing), chart of storage values, length, width and height, capacity, entry ports (maintenance) etc.

Provide a cross section of underground chamber system showing invert and obvert/top, major and minor HWLs, top of ground, system volume provided during major and minor events. UG storage to provide actual 2 and 100 year event storage requirements.

In regard to all proposed UG storage, ground water levels (and in particular HGW levels) will need to be reviewed to ensure that the proposed system does not become surcharged and thereby ineffective.

Modeling can be provided to ensure capacity for both storm and sanitary sewers for the proposed development by City's Water Distribution Dept. – Modeling Group, through Infrastructure PM and upon request.

For proposed depressed driveways or developments with private lanes, parking areas or with entrances etc. lower than roadway...





#### Other:

Due to more sensitive use, a Record of Site Condition (RSC) is required. Ensure Phase I, and if applicable, Phase II ESA's speak to required RSC.

Environmental Noise Study is required due to Albert St. and within 100m proximity of Slater and Bronson Avenues.

Stationary Noise Study – consultant to speak to this in their report as per City NCG and NPC 300 Guidelines. Particularly regarding roof top units and amenity spaces.

Shadow Study required for this proposal.

Wind Study is required for this proposal.

Capital Projects:

Road, Water and Sewer renewal projects listed for Slater, Albert and Bronson in the next 3-5 years.

### Environmental Source Information (Re: Phase I ESA):

City of Ottawa - Historical Land Use Inventory (HLUI) - Required

Rationale:

The HLUI database is currently undergoing an update. The updated HLUI will include additional sources beyond those included in the current database, making the inclusion of this record search even more important.

Although a municipal historic land use database is not specifically listed as required environmental record in O. Reg 153/04, Schedule D, Part II states the following:

The following are the specific objectives of a records review:

- 1. To obtain and review records that relate to the Phase I (One) property and to the current and past uses of and activities at or affecting the Phase I (One) property in order to determine if an area of potential environmental concern exists and to interpret any area of potential environmental concern.
- 2. To obtain and review records that relate to properties in the Phase I (One) study area other than the Phase I (One) property, in order to determine if an area of potential environmental concern exists and to interpret any area of potential environmental concern.

It is therefore reasonable to request that the HLUI search be included in the Phase I ESA to meet the above objectives. Please submit.

Existing buildings require a CCTV inspection and report to ensure existing services to be reused are in good working order and meet current minimum size requirements. Located services to be placed on site servicing plans.



All existing reports and plans will need to be revised if older than 2 years and must reflect current City Standards, Guidelines, By-laws and Policies.

Please refer to City of Ottawa website portal **for "Guide to preparing Studies and Plans"** at <u>https://ottawa.ca/en/city-hall/planning-and-development/information-</u> <u>developers/development-application-review-process/development-application-</u> <u>submission/guide-preparing-studies-and-plans</u>.

Please ensure you are using the current guidelines, bylaws and standards including materials of construction, disinfection and all relevant reference to OPSS/D and AWWA guidelines - all current and as amended, such as:

<u>City of Ottawa Sewer Design Guidelines</u> (**CoOSDG**) complete with ISTDB 2012-01, 2014-01, 2016-01 & 2018-01 technical bulletin updates as well as current Sewer, Landscape & Road Standard Detail Drawings as well as Material Specifications (MS Docs). Sewer Connection (2003-513) & Sewer Use (2003-514) By-Laws.

<u>City of Ottawa Water Distribution Design Guidelines</u> (**CoOWDDG**) complete with ISTDB 2010-02, 2014-02 & 2018-02 technical bulletin updates as well as current Watermain/ Services Material Specifications (MS Docs) as well as Water and Road Standard Detail Drawings. FUS Fire Flow standards

Water (2018-167) By-Law

Ensure to include version date and add "(as amended)" when referencing all standards, detail drwaings, by-Laws and guidelines.

Please also note:

Regarding provided Information, please be advised that it is the responsibility of the applicant and their representatives/consultants to verify information provided by the City of Ottawa. Please contact City View and Release Info Centre at Ext. 44455

Contact me at 613-580-2424, Ext. # 33017 or e-mail <u>shawn.wessel@ottawa.ca</u> if you have any questions.

Sincerely,

& I

Shawn Wessel, A.Sc.T., rcji Project Manager Development Review, Central Branch



## MacSween, Meghan

From:	Eric Lalande <eric.lalande@rvca.ca></eric.lalande@rvca.ca>
Sent:	Tuesday, November 05, 2019 9:52 AM
То:	MacSween, Meghan
Subject:	[EXTERNAL] RE: 473 Albert Street, Ottawa

Hi Meghan,

The RVCA will not require any additional water quality protections as the site will remain rooftop along with the conversion of parking spaces to open area.

Thank you,

#### Eric Lalande, MCIP, RPP Planner, Rideau Valley Conserva

Planner, Rideau Valley Conservation Authority 613-692-3571 x1137

From: MacSween, Meghan <Meghan.Macsween@parsons.com>
Sent: Tuesday, October 29, 2019 11:29 AM
To: Eric Lalande <eric.lalande@rvca.ca>
Subject: 473 Albert Street, Ottawa

Hi Eric,

We would like to request any RVCA requirements or comments related to proposed work at 473 Albert Street in Ottawa.

We are working for the owner of this building (CLV Group) towards a Site Plan Approval from the City of Ottawa, to convert the existing building from office use to mixed-use (residential, office and restaurant). The existing building footprint will remain the same. As you can see from the existing aerial below, the building covers the majority of the property. Currently there is a driving aisle on the west side of the property, which is covered by the building, see picture below, that allows access to an underground parking garage as well as a small open area at the back of the property that has been used for parking a few cars in the past.



The proposed works include renovations inside the building and reuse of the existing underground parking garage. However, the vehicle access to the back of the property will be eliminated and replaced with pedestrian only access. The ground level at the back of the building will consist of amenity space including a restaurant terrace, bicycle storage and a basketball court – there will be no vehicle parking. I've attached a very preliminary site plan so you can see the building footprint and the amenity space behind the building. There will be a separate sanitary and storm outlet to the existing combined sewer in Albert Street. We are awaiting CCTV results to confirm if we'll be reusing existing service laterals or constructing new ones.

Please feel free to contact me if you have any questions or concerns.

Thanks,

Meghan

## Meghan MacSween, M.Eng., P.Eng.

Municipal Engineer 1223 Michael St. North, Suite 100, Ottawa, ON K1J 7T2 <u>meghan.macsween@parsons.com</u> – P: +1 613.691.1540 M: +1 343.997.3895

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APPENDIX B | SERVICING CHECKLIST

	Development Servicing Study Checklist	
1 Ger	neral Content	Comments
NA	Executive Summary (for larger reports only).	
Y	Date and revision number of the report.	Title page
Y	Location map and plan showing municipal address, boundary, and layout of proposed	Figure 1 and Drawing C101
	development.	
Y	Plan showing the site and location of all existing services.	Drawing C101 and Figure 2
NA	Development statistics, land use, density, adherence to zoning and official plan, and	
	reference to applicable subwatershed and watershed plans that provide context to	
	which individual developments must adhere.	
Γ <u>Υ</u>	Summary of Pre-consultation Meetings with City and other approval agencies.	Section 1.4
NA	Reference and confirm conformance to higher level studies and reports (Master	
	Servicing Studies, Environmental Assessments, Community Design Plans), or in the	
	case where it is not in conformance, the proponent must provide justification and	
	develop a defendable design criteria.	
	Statement of objectives and servicing criteria.	Section 2.2/3.2/4.3
Y	Identification of existing and proposed infrastructure available in the immediate area.	Section 1.3
NA	Identification of Environmentally Significant Areas, watercourses and Municipal	
	Drains potentially impacted by the proposed development (Reference can be made	
	to the Natural Heritage Studies, if available).	
Y	Concept level master grading plan to confirm existing and proposed grades in the	Drawing C101
	development. This is required to confirm the feasibility of proposed storm water	
	management and drainage, soil removal and fill constraints, and potential impacts to	
	neighboring properties. This is also required to confirm that the proposed grading	
	will not impede existing major system flow paths.	
NA	Identification of potential impacts of proposed piped services on private services	
	(such as wells and septic fields on adjacent lands) and mitigation required to address	
	potential impacts.	
Y	Proposed phasing of the development, if applicable	Section 1.1
NA	Reference to geotechnical studies and recommendations concerning servicing.	
	All preliminary and formal site plans submissions should have the following	
	information:	
Y	Metric Scale	Drawings
Y	<ul> <li>North arrow (including construction North)</li> </ul>	Drawings
Y	Key Plan	Drawings
Y	<ul> <li>Name and contact information of applicant and property owner</li> </ul>	Drawings
Y	<ul> <li>Property limits including bearing and dimensions</li> </ul>	Drawings
Y	<ul> <li>Existing and proposed structures and parking areas</li> </ul>	Drawings
Y	<ul> <li>Easement, road widening and right-of-way</li> </ul>	Drawings
Y	Adjacent street names	Drawings
2 De	velopment Servicing Report : Water	Comments
NA	Contirm consistency with Master Servicing Study, if available.	
Υ ···	Availability of public infrastructure to services proposed development.	Section 2.0
⊢ Υ ₩	Identification of system constraints.	Section 2.2
⊢ Y	Identification of boundary conditions.	Section 2.2
⊢ Y	Confirmation of adequate domestic supply and pressure	Section 2.2
Υ	Confirmation of adequate fire flow protection and confirmation that fire flow is	Section 2.2
	calculated as per the Fire Underwriter's Survey. Output should show available fire	
	now at locations throughout the development.	

	Development Servicing Study Checklist	
NA	Provided a check of high pressure. If pressure is found to be high, an assessment is	
NA	required to confirm the application of pressure reducing valves. Definition of phasing constraints. Hydraulic modeling is required to confirm servicing for all defined phases of the project including the ultimate design.	
Y	Address reliability requirements such as appropriate location of shut-off valves.	Section 2.2
NA	Check on the necessity of a pressure zone boundary modification.	
NA	Reference to water supply analysis to show that major infrastructure is capable of delivering sufficient water for the proposed land use. This includes data that shows that expected demands under average day, peak hour and fire flow conditions provide water within the required pressure range.	Section 2.2
Y	Description of the proposed water distribution network, including locations of proposed connections to the existing system, provisions for necessary looping, and appurtenances (valves, pressure reducing valves, valve chambers, and fire hydrants) including special metering provisions.	Section 2.1
NA	Description of off-site required feedermains, booster pumping stations, and other water infrastructure that will be ultimately required to service proposed development, including financing, interim facilities, and timing of implementation.	
Y	Confirmation that water demands are calculated based on the City of Ottawa Design Guidelines.	Section 2.2
Y	Provision of model schematic showing the boundary conditions locations, streets, parcels, and building locations for reference.	Appendix D
3 De	velopment Servicing Report: Wastewater	Comments
Y	Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitoring Flow data from relatively new infrastructure cannot be used to justify capacity requirements for	Section 3.0
Y NA	Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitoring Flow data from relatively new infrastructure cannot be used to justify capacity requirements for Confirm consistency with Master Servicing Study and/or justification for deviations.	Section 3.0
Y NA NA	Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitoring Flow data from relatively new infrastructure cannot be used to justify capacity requirements for Confirm consistency with Master Servicing Study and/or justification for deviations. Consideration of local conditions that may contribute to extraneous flow that are higher than the recommended flow in the guidelines. This includes groundwater and soil conditions, and age and condition of sewers.	Section 3.0
Y NA NA Y	Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitoring Flow data from relatively new infrastructure cannot be used to justify capacity requirements for Confirm consistency with Master Servicing Study and/or justification for deviations. Consideration of local conditions that may contribute to extraneous flow that are higher than the recommended flow in the guidelines. This includes groundwater and soil conditions, and age and condition of sewers. Description of existing sanitary sewer available for discharge of wastewater from proposed development.	Section 3.0 Section 3.1
Y NA NA Y	Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitoring Flow data from relatively new infrastructure cannot be used to justify capacity requirements for Confirm consistency with Master Servicing Study and/or justification for deviations. Consideration of local conditions that may contribute to extraneous flow that are higher than the recommended flow in the guidelines. This includes groundwater and soil conditions, and age and condition of sewers. Description of existing sanitary sewer available for discharge of wastewater from proposed development. Verify available capacity in downstream sanitary sewer and/or identification of upgrades necessary to service the proposed development. (Reference can be made to previously completed Master Servicing Study if applicable).	Section 3.0 Section 3.1
Y NA NA Y NA	Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitoring Flow data from relatively new infrastructure cannot be used to justify capacity requirements for Confirm consistency with Master Servicing Study and/or justification for deviations. Consideration of local conditions that may contribute to extraneous flow that are higher than the recommended flow in the guidelines. This includes groundwater and soil conditions, and age and condition of sewers. Description of existing sanitary sewer available for discharge of wastewater from proposed development. Verify available capacity in downstream sanitary sewer and/or identification of upgrades necessary to service the proposed development. (Reference can be made to previously completed Master Servicing Study if applicable). Calculations related to dry-weather and wet-weather flow rates from the development in standard MOE sanitary sewer design table (Appendix 'C') format.	Section 3.0 Section 3.1 Appendix F
Y NA NA Y NA	Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitoring Flow data from relatively new infrastructure cannot be used to justify capacity requirements for Confirm consistency with Master Servicing Study and/or justification for deviations. Consideration of local conditions that may contribute to extraneous flow that are higher than the recommended flow in the guidelines. This includes groundwater and soil conditions, and age and condition of sewers. Description of existing sanitary sewer available for discharge of wastewater from proposed development. Verify available capacity in downstream sanitary sewer and/or identification of upgrades necessary to service the proposed development. (Reference can be made to previously completed Master Servicing Study if applicable). Calculations related to dry-weather and wet-weather flow rates from the development in standard MOE sanitary sewer design table (Appendix 'C') format. Description of proposed sewer network including sewers, pumping stations, and forcemains.	Section 3.0 Section 3.1 Appendix F
Y NA NA Y NA NA	Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitoring Flow data from relatively new infrastructure cannot be used to justify capacity requirements for Confirm consistency with Master Servicing Study and/or justification for deviations. Consideration of local conditions that may contribute to extraneous flow that are higher than the recommended flow in the guidelines. This includes groundwater and soil conditions, and age and condition of sewers. Description of existing sanitary sewer available for discharge of wastewater from proposed development. Verify available capacity in downstream sanitary sewer and/or identification of upgrades necessary to service the proposed development. (Reference can be made to previously completed Master Servicing Study if applicable). Calculations related to dry-weather and wet-weather flow rates from the development in standard MOE sanitary sewer design table (Appendix 'C') format. Description of proposed sewer network including sewers, pumping stations, and forcemains. Discussion of previously identified environmental constraints and impact on servicing (environmental constraints are related to limitation imposed on the development in order to preserve the physical condition of watercourse, vegetation, soil cover, as	Section 3.0 Section 3.1 Appendix F
Y NA NA Y NA NA NA	Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitoring Flow data from relatively new infrastructure cannot be used to justify capacity requirements for Confirm consistency with Master Servicing Study and/or justification for deviations. Consideration of local conditions that may contribute to extraneous flow that are higher than the recommended flow in the guidelines. This includes groundwater and soil conditions, and age and condition of sewers. Description of existing sanitary sewer available for discharge of wastewater from proposed development. Verify available capacity in downstream sanitary sewer and/or identification of upgrades necessary to service the proposed development. (Reference can be made to previously completed Master Servicing Study if applicable). Calculations related to dry-weather and wet-weather flow rates from the development in standard MOE sanitary sewer design table (Appendix 'C') format. Description of proposed sewer network including sewers, pumping stations, and forcemains. Discussion of previously identified environmental constraints and impact on servicing (environmental constraints are related to limitation imposed on the development in order to preserve the physical condition of watercourse, vegetation, soil cover, as Pumping stations: impacts of proposed development on existing pumping stations or requirements for new pumping station to services development.	Section 3.0 Section 3.1 Appendix F

	Development Servicing Study Checklist	
NA	Identification and implementation of the emergency overflow from sanitary pumping	
	station in relation to the hydraulic grade line to protect against basement flooding.	
NA	Special considerations such as contamination, corrosive environment etc.	-
4 De	velopment Servicing Report: Stormwater Checklist	Comments
Y	Description of drainage outlets and downstream constraints including legality of	Section 4.1
	outlets (i.e. municipal drain, right-of-way, watercourse, or private property)	
<u> </u>	Analysis of available canasity in existing public infrastructure	
	A drawing showing the subject lands, its surroundings, the receiving watercourse	Figure A and Figure B in
'	existing drainage natterns, and proposed drainage natterns	Appendix G
	Water quantity control objective (e.g. controlling post-development, peak flows to	Section 4.2
ľ	mater quality control objective (e.g. controlling post-development peak nows to	Section 4.3
	(dependent on the receiving sewer design) to 100 years return period): if other	
	objectives are being applied, a rationale must be included with reference to	
	hydrologic analyses of the potentially affected subwatershed, taking into account	
	long-term cumulative effects.	
NA	Water Quality control objectives (basic, normal or enhanced level of protection based	
	on the sensitivities of the receiving watercourse) and storage requirements.	
Y	Description of the stormwater management concept with facility locations and	Section 4.6
	descriptions with references and supporting information.	
NA	Set-back from private sewage disposal systems.	
NA	Watercourse and hazard lands setbacks.	
Y	Record of pre-consultation with the Ontario Ministry of Environment and the	Appendix A
-	Conservation Authority that has jurisdiction on the affected watershed.	
	confirm consistency with sub-watersned and Master Servicing Study, if applicable	
	Storage requirements (complete with calculations) and conveyance canacity for	Section 4.6
'	minor events (1.5 years return period) and major events (1.100 years return period)	56000 4.0
NA	Identification of watercourses within the proposed development and how	
	watercourses will be protected, or, if necessary, altered by the proposed	
	development with applicable approvals.	
Y	Calculate pre and post development peak flow rates including a descriptions of	Section 4.6, Appendix I
	existing site conditions and proposed impervious areas and drainage catchments in	
	comparison to existing conditions.	
NA	Any proposed diversion of drainage catchment areas from one outlet to another.	
	Proposed minor and major systems including locations and sizes of stormwater trunk	Drowing C101
ľ	sewers and stormwater management facilities	
ΝΔ	If quantity control is not proposed, demonstration that downstream system has	
	adequate capacity for the post-development flows up to and including the 100-year	
	return period storm event.	
NA	Identification of potential impacts to receiving watercourses.	
NA	Identification of municipal drains and related approvals requirements.	
Y	Descriptions of how the conveyance and storage capacity will be achieved for the	Sections 4.6
	development.	
Y	100 years flood levels and major flow routing to protect proposed development from	Section 4.7
	flooding for establishing minimum building elevations (MBE) and overall grading.	
<u> </u>		
NA	Inclusion of hydraulic analysis including hydraulic grade line elevations.	

	Development Servicing Study Checklist	
Y	Description of approach to erosion and sediment control during construction for the protection of receiving watercourse or drainage corridors.	Section 5.0
NA	Identification of floodplains - proponent to obtain relevant floodplain information from the appropriate Conservation Authority. The proponent may be required to delineate floodplain elevations to the satisfaction of the Conservation Authority if such information is not available or if information does not match current conditions.	
NA	Identification of fill constraints related to floodplain and geotechnical investigation.	
5 Ap	proval and Permit Requirements: Checklist	Comments
NA NA NA	Conservation Authority as the designated approval agency for modification of floodplain, potential impact on fish habitat, proposed works in or adjacent to a watercourse, cut/fill permits and Approvals under Lakes and Rivers Improvements Act. The Conservation Authority is not the approval authority for the Lakes and Rivers Improvements Act. Where there are Conservation Authority regulations in place, approval under the Lakes and Rivers Improvements Act is not required, except in cases of dams as defined in the Act. Application for Certificate of Approvals (CofA) under the Ontario Water Resources Act. Change to Municipal Drains Other permits (National Capital Commission, Parks Capada, Public Works and	
	Government Services Canada, Ministry of Transportation etc.)	
6 Co	nclusion Checklist	Comments
Y	Clearly stated conclusion and recommendations.	Section 6.0
Y	Comments received from review agencies including the City of Ottawa and information on how the comments were addressed. Final sign-off from the responsible reviewing agency.	Appendix A
Y	All draft and final reports shall be signed and stamped by a professional Engineer registered in Ontario.	Report

APPENDIX C | DRAWINGS C101, C102 AND C103



- STORM SEWER SYSTEM, ALL GRASSED AREAS MUST BE COMPLETED PRIOR TO THE REMOVAL OF THE FILTER FABRIC IN THE CATCH BASINS. 15. REMOVE FROM SITE ALL EXCESS EXCAVATED MATERIAL UNLESS OTHERWISE DIRECTED FROM THE ENGINEER. EXCAVATE AND REMOVE ALL ORGANIC MATERIAL AND DEBRIS LOCATED WITHIN THE PROPOSED BUILDING. PARKING AND ROADWAY LOCATIONS. ANY CONTAMINATED MATERIAL SHALL BE DISPOSED OF AT A LICENSED LANDFILL FACILITY.
- 16. THE APPROVAL OF THIS PLAN DOES NOT EXEMPT THE CONTRACTOR FROM THE REQUIREMENTS TO OBTAIN THE VARIOUS PERMITS/APPROVALS REQUIRED TO COMPLETE A CONSTRUCTION PROJECT, SUCH AS BUT NOT LIMITED TO; ROAD CUT PERMITS, SEWER PERMITS, WATER PERMIT, ETC.
- 17. AT PROPOSED UTILITY CONNECTION POINTS AND CROSSINGS (I.E. STORM SEWER, SANITARY SEWER, WATER, ETC.) THE CONTRACTOR SHALL DETERMINE THE PRECISE LOCATION AND DEPTH AND SIZE OF EXISTING UTILITIES AND REPORT ANY DISCREPANCIES OR CONFLICTS TO THE ENGINEER BEFORE COMMENCING WORK. PROTECT AND ASSUME RESPONSIBILITY FOR ALL EXISTING UTILITIES.
- 18. REFER TO ARCHITECT AND LANDSCAPE ARCHITECTS DRAWINGS FOR BUILDING, LANDSCAPE, AND HARD SURFACE AREAS AND DIMENSIONS, 19. CONTRACTOR IS RESPONSIBLE TO KEEP THE ROADS FREE AND CLEAN FROM MUD OR DEBRIS.
- INSPECT THEM FREQUENTLY AND CLEAN AND REPAIR OR REPLACE THE DETERIORATED STRUCTURES. AT THE END OF THE CONSTRUCTION PERIOD, THE CONTRACTOR IS RESPONSIBLE FOR REMOVAL OF THE . TEMPORARY STRUCTURES AND RECONDITIONING THE AFFECTED AREAS

- GEOTEXTILE FABRIC TO AVOID FINE PARTICLE TRANSPORT BY WIND AND/OR STREAMING RAIN WATER.
- CONTROL WIND-BLOWN DUST OFF SITE TO ACCEPTABLE LEVELS BY SEEDING TOPSOIL PILES AND OTHER AREAS TEMPORARILY (PROVIDE WATERING AS REQUIRED). FOR DUST CONTROL, CONTRACTOR TO APPLY CALCIUM CHLORIDE (TYPE I - OPSS 2501 AND CAN/CGSB-15-1) AND WATER WITH EQUIPMENT APPROVED BY THE OWNER'S REPRESENTATIVE AT RATE IN ACCORDANCE TO OPSS 506 WHEN DIRECTED BY OWNER'S REPRESENTATIVE.
- ALL EROSION CONTROL STRUCTURE TO REMAIN IN PLACE UNTIL ALL DISTURBED GROUND SURFACES HAVE BEEN DESTABILIZED EITHER BY PAVING OR RESTORATION OF VEGETATIVE GROUND COVER. SEDIMENT CAPTURE SILT SACKS MUST BE MAINTAINED AND CANNOT BE REMOVED UNTIL ALL LANDSCAPING AREAS ARE COMPLETED. NO ALTERNATE METHODS OF EROSION PROTECTION SHALL BE PERMITTED

- FILTER CLOTHS ON CATCH BASINS AND MANHOLE COVERS. INSPECT AND CLEAN CATCH BASIN SUMPS AND STORM SEWERS.

- 20. SUPPLY AND INSTALL ALL WATERMAIN ACCORDANCE WITH MOST CURRENT CITY O
- 21. ALL WATER MAIN TO BE INSTALLED AT MININ
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owner   propriétaire	Ottawa, Ontario K2P 1Z2 613-806-7816
Structural engineers   ingénieur structure	D D D 200-580 TERRY FOX DR. KANATA, ON K2L 489 (613) 591-1533
530 - 1600 Carling Avenue Ottawa Onta t 613 230 1186 smithandandersen MEP engineers   ingénieur MEP	n nio K1Z 1G3 .com
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Smith + Andersen 530 - 1600 Carling Avenue Ottawa Ontario t 613 230 1186 smithandandersen.cc	K1Z 1G3
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Adjustable Accutrol Weir Adjustable Flow Control for Roof Drains

For more flexibility in controlling flow with heads deeper than 2", Watts Drainage offers the Adjustable Accutrol. The Adjustable Accutrol Weir is designed with a single parabolic opening that can be covered to restrict flow above 2" of head to less than 5 gpm per inch, up to 6" of head. To adjust the flow rate for depits over 2" of head, set the slot in the adjustable upper cone according to the flow rate required. Reflex to Table 1 below. Note: Flow rates are directly proportional to the amount of weir opening that is exposed.

ADJUSTABLE ACCUTROL (for Large Sump Roof Drains only)



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APPENDIX D | BOUNDARY CONDITIONS

## **Theiner, Mathew**

Wessel, Shawn <shawn.wessel@ottawa.ca></shawn.wessel@ottawa.ca>
Thursday, November 21, 2019 8:52 AM
MacSween, Meghan
Deiaco, Simon; Theiner, Mathew
[EXTERNAL] RE: 473 Albert Street - Boundary Condition Request
473 Albert Nov 2019.pdf

### Good morning Ms. MacSween / Mr. Theiner

As discussed, the existing 152mm on Albert will be abandoned and the existing 203mm will be replaced by a new 203mm PVC in the near future. We can provide boundary conditions for future conditions but we are still waiting to hear back on the planned watermain sizes for Bronson, Albert and surrounding streets.

The following are boundary conditions, HGL, for hydraulic analysis at 473 Albert (zone 1W) assumed to be connected to the 203 mm on Albert (see attached PDF for location).

Minimum HGL = 106.0 m

Maximum HGL = 115.5 m

Available fire flow = 115 L/s assuming a residual of 20 psi and a ground elevation of 73.5 m

These are for current conditions and are based on computer model simulation.

Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation.

If you require additional information or clarification, please do not hesitate to contact me anytime.

Thank you

Regards,

Shawn Wessel, A.Sc.T.,rcji Project Manager - Infrastructure Approvals

### Gestionnaire de projet - Approbation des demandes d'infrastructures

Development Review Central Branch | Direction de l'examen des projets d'aménagement, Centrale Planning, Infrastructure and Economic Development Department | Direction générale de la planification de l'infrastructure et du développement économique City of Ottawa | Ville d'Ottawa 110 Laurier Ave. W. | 110, avenue Laurier Ouest, Ottawa ON K1P 1J1 (613) 580 2424 Ext. | Poste 33017 Int. Mail Code | Code de Courrier Interne 01-14 shawn.wessel@ottawa.ca



Please consider the environment before printing this email

From: MacSween, Meghan < Meghan. Macsween@parsons.com> Sent: November 13, 2019 1:29 PM To: Wessel, Shawn <shawn.wessel@ottawa.ca> Cc: Deiaco, Simon < Simon.Deiaco@ottawa.ca>; Theiner, Mathew < Mathew.Theiner@parsons.com> Subject: RE: 473 Albert Street - Boundary Condition Request

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ATTENTION : Ce courriel provient d'un expéditeur externe. Ne cliquez sur aucun lien et n'ouvrez pas de pièce jointe, excepté si vous connaissez l'expéditeur.

Hi Shawn,

Thanks for the heads up, we'll await confirmation. If the 152mm watermain is out of service we will have to connect to the 203 mm diameter watermain and install a valve to separate the two services.

I am going to be out of the office for the next two weeks, can I ask that you include Mathew Theiner, cc'd, on any communication as he will be taking over in my absence.

Thanks,

Meghan

Meghan MacSween, M.Eng., P.Eng. **Municipal Engineer** 1223 Michael St. North. Suite 100. Ottawa, ON K1J 7T2 meghan.macsween@parsons.com - P: +1 613.691.1540 M: +1 343.997.3895

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From: Wessel, Shawn <<u>shawn.wessel@ottawa.ca</u>>
Sent: Wednesday, November 13, 2019 10:52 AM
To: MacSween, Meghan <<u>Meghan.Macsween@parsons.com</u>>
Cc: Deiaco, Simon <<u>Simon.Deiaco@ottawa.ca</u>>
Subject: [EXTERNAL] 473 Albert Street - Boundary Condition Request

Good morning Ms. Macsween.

Further to your request, the Water Distribution Dept. has sent the following message:

The 152mm watermain on Albert that they're proposing to connect to seems to be out of service according to GIS. I'm just waiting to hear back from Distribution to find out if this is just temporary or permanent.

I will get back to you once I hear from our colleagues regarding this matter.

If you require additional information or clarification, please do not hesitate to contact me anytime.

Thank you

Regards,

ı

## Shawn Wessel, A.Sc.T.,rcji Project Manager - Infrastructure Approvals Gestionnaire de projet – Approbation des demandes d'infrastructures

Development Review Central Branch | Direction de l'examen des projets d'aménagement, Centrale Planning, Infrastructure and Economic Development Department | Direction générale de la planification de l'infrastructure et du développement économique City of Ottawa | Ville d'Ottawa 110 Laurier Ave. W. | 110, avenue Laurier Ouest, Ottawa ON K1P 1J1 (613) 580 2424 Ext. | Poste 33017 Int. Mail Code | Code de Courrier Interne 01-14 shawn.wessel@ottawa.ca

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## Valves / Vannes

- Valve / Vanne ۲
- = TVS, A, D

## Water Fittings / Raccords de conduite d'eau —

- Cap / bouchon
- ÷ Reducer / réducteur
- Hydrants / Bornes-fontaines ÷

- Hydrant Laterals / Branchements de borne-fontaine —
- Water Mains / Conduites d'eau principales
- Private / Branchement privé ----
- Public / Branchement public
- Misc. Water Structures / Structures d'aqueduc divers
- Pumping Station / Station de pompage des eaux **H+**
- Ψ. Well Supply / Alimentation par puits

- Elevated Tank / Château d'eau
- In Ground Tank / Réservoir souterrain
- <del>~+-</del> Water Treatment Plant / Usine d'épuration des eaux



City of Ottawa

APPENDIX E | WATER DEMAND

#### Table1 : Water Demand for 473 Albert Street

			Gross Floor Area	Average Daily Demand (ADD)*	Maximum Daily Demand (MDD)**	Peak Hourly Demand (PHD)**	Fire Flow (FF)	MDD + FF
Building	Units	Population	(m2)		4.9*ADD	7.4*ADD		
Dullung					1.5*ADD (non- residential)	1.8*MDD (non- residential)		
				L/s	L/s	L/s	L/s	L/s
473 Albert Street				1.09	5.08	7.71	182	186.6
Residential	158	251		1.02	4.97	7.51		
Amenity Space (12th floor)			1260	0.07	0.11	0.20		

#### Average Daily Demands

Based on Ottawa Design Guidelines - Water Distribution, 2010 and MOE Design Guidelines for Drinking-Water Systems, 2008

Average Residential Daily Flow =350 L/p/dShopping Centres =2,500 L/(1000m2/d)Restaurant (Ordinary not 24h)125 L/seat/dOffice Daily Flow =75 L/empl/d75 L/empl/d75L/9.3m2/dAmenity Area Flow =5 L/m2/d\*\* Peaking factors as per MOE Guidelines for Drinking-Water Systems Table 3-3 for 0 to 500 persons

# Table 2: Fire Demand Calculation (473 Albert Street)

OBC Division B - Appendix A - A-3.2.5.7

A) Buildings Not Requiring On-Site Water Supply - satisfy Item 3b (flow rates not less than that specified in Table 2)

	Q = KVStot						
	K =	16	water sup	ply coefficie	nt Table 1		
	V =	51660	total build	ing volume i	n m3		
			A =	12	60 m2		
			H =		41 m		
	S tot =	1.6	total of sp	atial coefficio	ent values	s from prop	perty line exposures on all side = 1+(S1+S2+), does not exceed 2
			0m	E		0.5	
			9m	N		0.1	
			16.7m	W		0	
			20.7m	S		0	
	Q = 1,322,	496.00	L				
	Table 2 - if Q is greater than	270,000	DL, Min Wa	ater Supply F	low Rate	is:	
		9000	L/min				
		150	L/s				
B)	Sprinklered Buildings: Sprinkl Sprinkler demand provided by	er syste y Mecha	em plus fire anical Engi	efighting dem neers:	and		

500 gpm 31.5 L/s

Therefore, total demand for 473 Albert Street is 181.5 L/s.

### MacSween, Meghan

From:	Wessel, Shawn <shawn.wessel@ottawa.ca></shawn.wessel@ottawa.ca>
Sent:	Thursday, February 20, 2020 10:42 AM
То:	MacSween, Meghan
Subject:	[EXTERNAL] RE: 473 Albert Street - Hydrant Flow Test Request

Good morning Ms. MacSween.

I have received comments from Water Distribution, based on your SWM and Site Servicing Report review and their discussions with me on the available flows in the nearby FHs within 150 m of the property as well as your email sent yesterday, and their comments are as follows:

The consultant states that the five hydrants within 150m of the building can supply 380 L/s. This is incorrect.

Table 1 in Appendix I of tech bulletin ISTB-2018-02 assumes that the watermains can at minimum deliver the hydrant flow listed in the table . This is true in most cases but not always true on old watermains.

We have performed a multi-hydrant analysis and the total available flow from those five hydrants is 215 L/s assuming existing watermains.

We are looking into the status of the proposed Capital Works Project that would renew sewer and water infrastructure in the area, as mentioned, although this design must take into account the existing aged infrasturture.

If you require additional information or clarification, please do not hesitate to contact me anytime.

Thank you

Regards,

## Shawn Wessel, A.Sc.T.,rcji Project Manager - Infrastructure Approvals Gestionnaire de projet – Approbation des demandes d'infrastructures

Development Review Central Branch | Direction de l'examen des projets d'aménagement, Centrale Planning, Infrastructure and Economic Development Department | Direction générale de la planification de l'infrastructure et du développement économique City of Ottawa | Ville d'Ottawa 110 Laurier Ave. W. | 110, avenue Laurier Ouest, Ottawa ON K1P 1J1 (613) 580 2424 Ext. | Poste 33017 Int. Mail Code | Code de Courrier Interne 01-14 <u>shawn.wessel@ottawa.ca</u>

Please consider the environment before printing this email

From: MacSween, Meghan <Meghan.Macsween@parsons.com>
Sent: February 19, 2020 8:54 AM
To: Wessel, Shawn <shawn.wessel@ottawa.ca>
Subject: 473 Albert Street - Hydrant Flow Test Request

CAUTION: This email originated from an External Sender. Please do not click links or open attachments unless you recognize the source.

ATTENTION : Ce courriel provient d'un expéditeur externe. Ne cliquez sur aucun lien et n'ouvrez pas de pièce jointe, excepté si vous connaissez l'expéditeur.

Hi Shawn,

Thank you for your call yesterday regarding the SPA for 473 Albert Street.

We've calculated the required fire demand using the OBC calculations and determined the demand would be 150 L/s.

We would like to request fire hydrant flow tests for the 5 hydrants within 150m of the building which are shown with red circles on the attached map.

Thanks,

Meghan

Meghan MacSween, M.Eng., P.Eng. Municipal Engineer 1223 Michael St. North, Suite 100, Ottawa, ON K1J 7T2 meghan.macsween@parsons.com P: +1 613.691.1540 M: +1 343.997.3895 Parsons [can01.safelinks.protection.outlook.com] / LinkedIn [can01.safelinks.protection.outlook.com] / Twitter [can01.safelinks.protection.outlook.com] / Facebook [can01.safelinks.protection.outlook.com] / Instagram [can01.safelinks.protection.outlook.com]



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APPENDIX F | CCTV REPORTS

#### **Ottawa (Head Office)**

1800 Bantree Street Ottawa, Ontario K1B 5L6

☎ 613.745.2444 *∰* 613.745.9994

www.cwwcanada.com 1.866.695.0155

Montreal

2700 Sabourin Street St-Laurent, Quebec H4S 1M2

☎ 514.738.2666 *∰* 514.738.9762



INTEGRATED SEWER SOLUTIONS

# **InterRent No.3 Limited Partnership**

473 Albert St. Ottawa, Ontario Job No.: 87892

> **Drain Use** Sanitary

# **Inspection Date**

November 21<sup>st</sup> 2019

# **DRAIN CCTV INSPECTION REPORT**

# THE WAY IS CLEAR<sup>™</sup>

- CIPP Lateral Drain Lining
- Drain Inspection and Locating
- Preventative Maintenance Plumbing
- Frozen Pipe Thawing
- Backwater Valve Devices
- Sewer and Waterline Replacement and Repairs
- High Pressure Blasting
- Drain Cleaning and Flushing
- Plumbing Installation, Renovations and Repairs



# InterRent No. 3 Limited Partnership 473 Albert Street Ottawa, Ontario Job No.: 88792

**Inspection Date** November 21<sup>st</sup> 2019

# **Inspection Notes:**

Water main was verbally confirmed as 6 inch plastic by David Seaman on site with Evan Johnson.



MINI CAMERA CCTV INSPECTION REPORT						
CUSTOMER:	InterRent No. 3 Limited Partnership	START OF INSPECTION:	BASEMENT MECH ROOM			
JOB NO.:	87892	END OF INSPECTION:	CITY MAIN LINE			
		SEWER USE:	SANITARY			
LOCATION:	473 ALBERT STREET	PIPE DIAMETER(S):	150MM / 200MM			
	OTTAWA, ONTARIO	PIPE MATERIAL(S):	CAST IRON / TRANSITE			
		DIRECTION OF FLOW:	DOWNSTREAM			
DATE:	NOVEMBER 21 <sup>ST</sup> 2019	VIDEO FILENAME:	Video #1			
OPERATOR:	DAVID S.	<b>REPORT NUMBER:</b>	1 of 2			

DISTANCE (M)	CODE	INSPECTION COMMENTS	CODE AIF	DESCRIPTION ACTIVE INFILTRATION
0.0	START	START OF INSPECTION – BASEMENT MECH ROOM	BSG	START OF SAG
1.0	LBD	LINE BENDS DOWN	BWV C/O	BACKWATER VALVE CLEANOUT
2.4	LBS	LINE BENDS STRAIGHT	CAL	CALCITE
2.4	DC	DIAMETER CHANGE: 150MM – 200MM	CFL	CULLAPSE CIRCULAR CRACK
3.8	LBR	LINE BENDS RIGHT	DC DEB	DIAMETER CHANGE DEBRIS
3.8	MC	MATERIAL CHANGE: CAST IRON – TRANSITE	DEF	PIPE DEFORMATION
13.4	END	END OF INSPECTION – CITY MAIN LINE	ESG EXG	END OF SAG EXPOSED GASKET
			EXR F/D	EXPOSED REBAR FLOOR DRAIN
			GRS	GREASE
			HOLE LBD	HOLE IN PIPE LINE BENDS DOWN
			LBL	LINE BENDS LEFT
				LINE BENDS RIGHT
			LGC	LONGITUDINAL CRACK
			MAIN	MAIN SEWER IN BUILDING
			MC	MATERIAL CHANGE
			MH	MANHOLE
			OBS	OBSTRUCTION IN PIPE
			OFJ	OFFSET JOINT
			ОРЈ	OPEN JOINT
			PFL	PARTIAL COLLAPSE
			PSC	PROTRUDING CONNECTION
			PUN PTC	PUNCIURE
				SERVICE CONNECTION
			WYE	WYE CONNECTION

COMMENTS:

Before Flushing No deficiencies noted

# Video #1











MINI CAMERA CCTV INSPECTION REPORT						
CUSTOMER:	InterRent No. 3 Limited Partnership	START OF INSPECTION:	BASEMENT MECH ROOM			
JOB NO.:	87892	END OF INSPECTION:	CITY MAIN LINE			
		SEWER USE:	SANITARY			
LOCATION:	473 ALBERT STREET	PIPE DIAMETER(S):	150MM / 200MM			
	OTTAWA, ONTARIO	PIPE MATERIAL(S):	CAST IRON / TRANSITE			
		DIRECTION OF FLOW:	DOWNSTREAM			
DATE:	NOVEMBER 21 <sup>ST</sup> 2019	VIDEO FILENAME:	Video #2			
OPERATOR:	DAVID S.	<b>REPORT NUMBER:</b>	2 of 2			

DISTANCE (M)	CODE	INSPECTION COMMENTS	CODE AIF BK1	DESCRIPTION ACTIVE INFILTRATION BROKEN JOINT
0.0	START	START OF INSPECTION – BASEMENT MECH ROOM	BSG	START OF SAG
1.0	LBD	LINE BENDS DOWN	BWV C/O	BACKWATER VALVE CLEANOUT
2.4	LBS	LINE BENDS STRAIGHT	CAL	
2.4	DC	DIAMETER CHANGE: 150MM – 200MM	CRC	CIRCULAR CRACK
3.8	LBR	LINE BENDS RIGHT	DC DEB	DIAMETER CHANGE DEBRIS
3.8	MC	MATERIAL CHANGE: CAST IRON – TRANSITE	DEF	PIPE DEFORMATION
13.4	END	END OF INSPECTION – CITY MAIN LINE	ESG	END OF SAG EXPOSED GASKET
			EXR F/D FRC	EXPOSED REBAR FLOOR DRAIN FRACTURE
			GRS	GREASE
			HOLE LBD	HOLE IN PIPE LINE BENDS DOWN
			LBL	LINE BENDS LEFT
			LBR	LINE BENDS RIGHT
				LINE BENDS STRAIGHT
			MAIN	MAIN SEWER IN BUILDING
			MC	MATERIAL CHANGE
			МН	MANHOLE
			MSP	MISSING PIPE PIECE
			OBS	OBSTRUCTION IN PIPE
				OPEN JOINT
			PFI	PARTTAL COLLAPSE
			PSC	PROTRUDING CONNECTION
			PUN	PUNCTURE
			RTS	ROOTS
			SC WYE	SERVICE CONNECTION WYE CONNECTION

COMMENTS:

After Flushing No deficiencies noted
## Video #2













### **Ottawa (Head Office)**

1800 Bantree Street Ottawa, Ontario K1B 5L6

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Montreal

2700 Sabourin Street St-Laurent, Quebec H4S 1M2

☎ 514.738.2666 *∰* 514.738.9762



INTEGRATED SEWER SOLUTIONS

# **InterRent No.3 Limited Partnership**

473 Albert St. Ottawa, Ontario Job No.: 87892

> Drain Use Storm

## **Inspection Date**

November 14<sup>th</sup> 2019

# **DRAIN CCTV INSPECTION REPORT**

## THE WAY IS CLEAR<sup>™</sup>

- CIPP Lateral Drain Lining
- Drain Inspection and Locating
- Preventative Maintenance Plumbing
- Frozen Pipe Thawing
- Backwater Valve Devices
- Sewer and Waterline Replacement and Repairs
- High Pressure Blasting
- Drain Cleaning and Flushing
- Plumbing Installation, Renovations and Repairs



	MINI CAMERA CCTV INSPECTION REPORT												
CUSTOMER:	InterRent No. 3 Limited Partnership	START OF INSPECTION:	CLEANOUT										
JOB NO.:	87892	END OF INSPECTION:	MAIN LINE										
		SEWER USE:	STORM										
LOCATION:	473 ALBERT	PIPE DIAMETER(S):	100MM / 150MM / 200MM										
	OTTAWA, ONTARIO	PIPE MATERIAL(S):	CAST IRON / TRANSITE										
		DIRECTION OF FLOW:	DOWNSTREAM										
DATE:	NOVEMBER 14 <sup>TH</sup> 2019	VIDEO FILENAME:	Video #1										
OPERATOR:	TREVOR F.	<b>REPORT NUMBER:</b>	1 of 1										

DISTANCE (M)	CODE	INSPECTION COMMENTS	CODE AIF	DESCRIPTION ACTIVE INFILTRATION BROKEN JOINT
0.0	C/0	START OF INSPECTION – CLEANOUT	BSG	START OF SAG
2.8	LBR	LINE BENDS RIGHT	BWV C/O	BACKWATER VALVE CLEANOUT
2.8	DC	DIAMETER CHANGE: 100MM – 150MM	CAL	
4.8	LBD	LINE BENDS DOWN	CRC	CIRCULAR CRACK
6.0	LBS	LINE BENDS STRAIGHT	DC DEB	DIAMETER CHANGE DEBRIS
7.4	LBR	LINE BENDS RIGHT	DEF	PIPE DEFORMATION
8.2	LBL	LINE BENDS LEFT	ESG	END OF SAG
8.2	DC	DIAMETER CHANGE: 150MM – 200MM	EXG EXR	EXPOSED GASKET EXPOSED REBAR
8.2	МС	MATERIAL CHANGE: CAST IRON – TRANSITE	F/D	FLOOR DRAIN
17.8	END	END OF INSPECTION – MAIN LINE	GRS	GREASE
			HOLE	HOLE IN PIPE
			LBL	LINE BENDS LEFT
			LBR	LINE BENDS RIGHT
			LBS	LINE BENDS STRAIGHT
			MAIN	MAIN SEWER IN BUILDING
			MC	MATERIAL CHANGE
			МН	MANHOLE
			MSP	MISSING PIPE PIECE
			OBS	OBSTRUCTION IN PIPE
			OFJ	OFFSET JOINT
			OPJ	OPEN JOINT
			PFL	PARTIAL COLLAPSE
			RTS	ROOTS
			sc	SERVICE CONNECTION
			WYE	WYE CONNECTION

COMMENTS:

No deficiencies noted

## Video #1













**APPENDIX G** | SANITARY FLOWS AND SEWER DESIGN SHEET

		REST	AURANT				OFFICE			RO	OFTOP AN	MENITY SP	PACE		R	SIDENTIAL		TOTAL	INF	ILTRATION		Total
Area	Restauran Area	t Seats assumed 1 seat	Flow/seat	Peak Factor	Peak Flow	Office Area	Capita	Peak Factor	Peak Flow	Area	Amenity Space	Peak Factor	Peak Flow	Number of units	Capita	Peak Factor	Peak Flow	Peak Flow	Site Areas	Infiltration Allowance	Infilt. Flow	Total Peak Flow
	(m <sup>2</sup> )	per m <sup>2</sup>	L/seat/d		(L/s)	(m <sup>2</sup> )	(1/25m <sup>2</sup> )		(L/s)	(m <sup>2</sup> )	L/m2/d		(L/s)				(L/s)	(L/s)	(ha)	(L/s/ha)	(L/s)	(L/s)
Proposed Building																			0.20	0.33	0.07	0.07
Restaurant																						
Office																						
Residential														158	251	3.5	2.84	2.84				2.84
Amenity Space										1260	5	1.0	0.1					0.07				0.07
																					Total	2.98
Existing Building																			0.20	0.33	0.07	0.07
Office						12,647	506	1.5	0.66									0.66				0.66
Restaurant	3	35 385	125	1.5	0.84													0.84				0.84
																					Total	1.56
	-		•											-				Design:	Benoit Villeneuve	Project:	473 Albert S	st.
																					Ottawa, Ont	ario
Average Daily Demands																		Check :	Meghan MacSwee	Location:	473 Albert S	st.
(Based on City of Ottawa Sewer Desig	ign Guidelines 2012 and M	DE Water Design Gui	delines )																		Ottawa, Ont	ario
Average Residential Daily Flow =	280 L/p/d	Peak Factors																		Project # :	477234	
Institutional Flow =	28,000 L/ha/d	Commercial =		1.5	if commerci	ial contribution	> 20%, otherwise	1.0												Date:	24-Sep-20	)
Commercial Flow =	28,000 L/ha/d	Institutional =		1.5	if institution	al contribution	> 20%, otherwise	1.0												Sheet:	1 of 1	
Light Industrial Flow =	35,000 L/ha/d	Industrial =			per Append	lix 4-B.0 Graph																
Heavy Industrial Flow =	55,000 L/ha/d	Residential :			Harmon Eq	ι 1 + (14/(4+(C	apita/1000) ^ 0.5))	*8														
Hotel Daily Flow =	225 L/bed/d				min =	= 2	max	= 4														
Office/Warehouse Daily Flow =	75 L/empl/d																					
Shanning Control =	2 500 L //4000																					
Amenity Area -	2,500 L/(1000m/d)																					
	J L/11/2	Infiltration allowar	ice (drv weather	)	0.05	l /s/ha																
		Infiltration allowar	ice (wet weather	/ -)	0.28	L/s/ha																
Population Densities			,	,																		
Average suburban residential dev.	60 p/ha	I/I (total)			0.33	L/s/ha																
Single family	3.4 p./unit																					
Semi-detached	2.7 p./unit																					
Duplex	2.3 p./unit																					
Appartment average	2.7 p./unit																					
Bachelor	1.6 p./unit																					
1 Bedroom	1.4 p./unit																					
2 Bedrooms	2.1 p./unit																					
Hotel room, 18 m2	1 p./unit																					
Restaurant, 1 m2	1 p./unit																					
Office	1 p/25m <sup>2</sup>																					

# Table 1: SANITARY DESIGN FLOWS

## Table 2: SANITARY SEWER COMPUTATIONS

			Peak					Se	wer Data					,
Drainage	From	То	Flow	Туре	Pipr	e Dia.	Slope*	Length	Capacity	Vel	ocity	Time of	Q(d) / Q(f)	REMARKS
Area			Q	of	nom.	actual			full	full	actual	Flow		
			(L/sec)	Pipe	(mm)	(mm)	(%)	(m)	(L/sec)	(m/sec)	(m/sec)	(min)		
473 Albert Street	Building	Combined Sewer	2.98	Transite	200	200	1.5	13.4	40.1	1.28	0.68	0.33	0.07	
		1		· · · · ·										
Manning's n =	0.013									Design:	Mathew T	heiner	Project Name	e: 473 Albert St.
*	Min slope for cleans	ing velocities is 0.32%	,							Check:	Meghan N	MacSween 1	Parsons Proj	ect #: 477234
	Estimated invert at !	ouilding wall = 71.4 m								Date:	Sept 24 2	2020	Client:	InterRent

Top of combined sewer at connection point is +/-71.2m

## APPENDIX H | PRE-DEVELOPMENT DRAINAGE PLAN



APPENDIX I | STORM SEWER DESIGN SHEET

## STORM SEWER COMPUTATION FORM

Rational Method       Q = Flow (L/sec)       Ottawa IDF Curve - 2-y         Q = 2.78*A*I*R       A = Area (ha)       I = Rainfall Intensity (mm/h)         R = Ave. Runoff Coefficient       Minimum Time of Conc. Tc = 10				• 10 min	Mar	nning's n =	0.013													
Drainage Area	From	То	Area (ha)	Runoff Coeff. R	Ru Indiv. 2.78AR	noff Parame Accum. 2.78AR	ters Time of Conc. (min)	Rainfall Intensity (mm/br)	Roof Flow Q (L/sec)	Peak Flow Q (L/sec)	Pi nom. (mm)	pe Dia. actual (mm)	Slope (%)	Length (m)	Capacity full (L/sec)	Ve full (m/sec)	ocity actual (m/sec)	Time of Flow (min)	Q(d) / Q(f)	REMARKS
473 Albert Street	Building	Sewer	0.170	0.90	0.43	0.43	10.00	104.19		10.90	200	200	1.12	17.8	34.77	1.11	0.82	0.27	0.31	
Note: Allowable release rate The minimum velocity when flow Estimated invert at builing wall = Top of combined sewer at conne	ring full is 0.80 m/s 71.4m ection point it +/-71.2m	1	-			<u>.</u>		<u>.</u>			Design: Check: Date:	M. Theiner M. MacSwee 24-Sep-20	en )		Project:	473 Alber	t Street			

## **APPENDIX J** | STORMWATER MANAGEMENT CALCULATIONS

### TABLE I - ALLOWABLE RUNOFF CALCULATIONS BASED ON PRE-EXISTING CONDITIONS

			Minor	Storm		Storm = 100 yr					
	Time of Conc,										
Area (ha)	Tc (min)		l <sub>2</sub> (mm/hr)	C <sub>AVG</sub>	Q <sub>ALLOW</sub> (L/s)	l <sub>100</sub> (mm/hr)	C <sub>AVG</sub>	Q <sub>ALLOW</sub> (L/sec)			
0.164	10	Storm = 2 yr	76.81	0.40	14.0	178.56	0.90	73.2			
0.004	10	Storm = 2 yr	76.81	0.40	0.3	178.56	0.90	1.8			
proposed sanitary	flows (2.98L/s-1.5	56L/s=1.42 L/s) dι	e to combined se	ewer	12.9						
	Area (ha) 0.164 0.004 proposed sanitary	Time of Conc,           Area (ha)         Tc (min)           0.164         10           0.004         10           proposed sanitary flows (2.98L/s-1.5)	Time of Conc,           Area (ha)         Tc (min)           0.164         10         Storm = 2 yr           0.004         10         Storm = 2 yr           oroposed sanitary flows (2.98L/s-1.56L/s=1.42 L/s) du         Use 1.42 L/s) du	Area (ha)         Time of Conc, Tc (min)         I₂ (mm/hr)           0.164         10         Storm = 2 yr         76.81           0.004         10         Storm = 2 yr         76.81           oroposed sanitary flows (2.98L/s-1.56L/s=1.42 L/s) due to combined set         Image: Comparison of the set         Image: Comparison of the set	Minor Storm           Time of Conc, Tc (min)         I <sub>2</sub> (mm/hr)         C <sub>AVG</sub> 0.164         10         Storm = 2 yr         76.81         0.40           0.004         10         Storm = 2 yr         76.81         0.40           oroposed sanitary flows (2.98L/s-1.56L/s=1.42 L/s) due to combined sewer         Image: Comparison of the second sec	Area (ha)         Time of Conc, Tc (min)         I <sub>2</sub> (mm/hr)         C <sub>AVG</sub> Q <sub>ALLOW</sub> (L/s)           0.164         10         Storm = 2 yr         76.81         0.40         14.0           0.004         10         Storm = 2 yr         76.81         0.40         0.3           proposed sanitary flows (2.98L/s-1.56L/s=1.42 L/s) due to combined sewer         12.9	Area (ha)         Time of Conc, Tc (min)         I2 (mm/hr)         CAVG         QALLOW (L/s)         I100 (mm/hr)           0.164         10         Storm = 2 yr         76.81         0.40         14.0         178.56           0.004         10         Storm = 2 yr         76.81         0.40         0.3         178.56           0roposed sanitary flows (2.98L/s-1.56L/s=1.42 L/s) due to combined sewer         12.9         12.9         12.9	Area (ha)         Time of Conc, Tc (min)         Minor Storm         Q <sub>ALLOW</sub> (L/s)         I <sub>100</sub> (mm/hr)         C <sub>AVG</sub> 0.164         10         Storm = 2 yr         76.81         0.40         14.0         178.56         0.90           0.004         10         Storm = 2 yr         76.81         0.40         0.3         178.56         0.90           proposed sanitary flows (2.98L/s-1.56L/s=1.42 L/s) due to combined sewer         12.9         12.9         12.9         12.9			

Allowable Capture Rate is based on the 2-year storm at  $T_c$ =10 mins, and a  $C_{avg}$  of 0.40

2-year Storm	C <sub>ASPH/ROOF/CONC</sub> =	0.90	C <sub>GRAVEL</sub> =	0.60	C <sub>GRASS</sub> =	0.20
100-year Storm	C <sub>ASPH/ROOF/CONC</sub> =	<u>1.00</u>	C <sub>GRAVEL</sub> =	<u>0.75</u>	C <sub>GRASS</sub> =	0.25

### TABLE II- POST-DEVELOPMENT AVERAGE RUNOFF COEFFICIENTS

Watershed Area No.	Impervious Areas (m <sup>2</sup> )	A * C <sub>ASPH/ROOF</sub>	Pervious Areas (m <sup>2</sup> )	A * C <sub>GRASS</sub>	Sum AC	Total Area (m <sup>2</sup> )	C <sub>AVG (5yr)</sub>	C <sub>AVG(100yr)</sub>
WS-01*	538.76	485	0.00	0	485	539	0.90	1.00
WS-02**	722.16	650	0.00	0	650	722	0.90	1.00
WS-03***	392.93	354	0.00	0	354	393	0.90	1.00
WS-04	39.62	36	0.00	0	36	40	0.90	1.00
Total	1693		0		1524	1693		
Total Controlled	1654		0		1488	1654		

\* Controlled roof top area

\*\* Uncontrolled roof area directed to cistern

\*\*\* Uncontrolled ground level amenity space directed to cistern

### TABLE III- TOTAL RUNOFF COEFFICIENT FOR CONTROLLED AREAS

### TABLE IV- SUMMARY OF POST-DEVELOPMENT RUNOFF

			Storm	= 2 yr		Storm = 100 yr						
Area No	Area (ha)	l <sub>2</sub> (mm/hr)	C <sub>AVG(2vr)</sub>	Q <sub>GEN</sub> (L/s)	Q <sub>CONT</sub> (L/s)	I <sub>100</sub> (mm/hr)	C <sub>AVG(100yr)</sub>	Q <sub>GEN</sub> (L/s)	Q <sub>CONT</sub> (L/s)			
WS-01*	0.054	76.81	0.90	10.4	4.0	178.56	1.00	26.7	6.1			
WS-02**	0.072	76.81	0.90	13.9	4.0	178.56	1.00	35.8	4.0			
WS-03***	0.039	76.81	0.90	7.6	4.9	178.56	1.00	19.5	4.9			
WS-04	0.004	76.81	0.90	0.8	0.8	178.56	1.00	2.0	2.0			
Total	0.169			32.5	9.6			84.1	12.9			
* Controlled roof to	p area											
** Uncontrolled roo	of area directed to	cistern										
*** Uncontrolled gr	ound level amenit	ty space directed t	o cistern									
l <sub>2</sub> = 732.951 / (Tc -	+ 6.199) <sup>0.810</sup>											
I100 =1735.688 / (T	c + 6.014) <sup>0.820</sup>											
Time of concentrat	tion (min), Tc =		10 mins									

	Table V - Storage Volumes (2-Year and 100-Year Storm Events)											
			;	Storage Red	quirement f	for RD-8						
	C <sub>AVG</sub> =	0.90	(2-year)									
	C <sub>AVG</sub> =	1.00	(100-year)			Watts Adjust	stable Accuti	rol Weir Roo	of Drain			
Tim	ne Interval =	5	(mins)									
Drair	nage Area =	0.011	(hectares)									
		114.52	(sqm)									
	F	Release Rate =	0.95	(L/sec) per	drain	Rele	ease Rate =	1.53	(L/sec) per	drain		
	R	eturn Period =	2	(years)		Retu	urn Period =	100	(years)			
	IDF Pa	arameters, A =	732.951	, B =	0.810	IDF Para	meters, A =	1735.688	, B =	0.820		
		I = A/(	Г <sub>с</sub> +С)В	, C =	6.199		I = A/(Tc	+C)B	, C =	6.014		
	Rainfall			Storage		Rainfall		Release	Storage			
Duration	Intensity, I	Peak Flow	Release	Rate	Storage	Intensity, I	Peak Flow	Rate	Rate	Storage		
(min)	(mm/hr)	(L/sec)	Rate (L/sec)	(L/sec)	(m <sup>3</sup> )	(mm/hr)	(L/sec)	(L/sec)	(L/sec)	(m <sup>3</sup> )		
0	-	-	-	-	-	-	-	-	-	-		
5	103.6	3.0	0.95	2.02	0.607	242.7	7.7	1.53	6.20	1.860		
10	76.8	2.2	0.95	1.25	0.753	178.6	5.7	1.53	4.16	2.494		
15	61.8	1.8	0.95	0.82	0.742	142.9	4.5	1.53	3.02	2.719		
20	52.0	1.5	0.95	0.54	0.654	120.0	3.8	1.53	2.29	2.748		
25	45.2	1.3	0.95	0.35	0.522	103.8	3.3	1.53	1.78	2.666		
30	40.0	1.1	0.95	0.20	0.363	91.9	2.9	1.53	1.40	2.513		
35	36.1	1.0	0.95	0.09	0.183	82.6	2.6	1.53	1.10	2.311		
40	32.9	0.9	0.95	0.00	-0.010	75.1	2.4	1.53	0.86	2.073		
45	30.2	0.9	0.95	-0.08	-0.215	69.1	2.2	1.53	0.67	1.808		
50	28.0	0.8	0.95	-0.14	-0.427	64.0	2.0	1.53	0.51	1.523		
55	26.2	0.7	0.95	-0.20	-0.647	59.6	1.9	1.53	0.37	1.220		
60	24.6	0.7	0.95	-0.24	-0.872	55.9	1.8	1.53	0.25	0.903		
65	23.2	0.7	0.95	-0.28	-1.102	52.6	1.7	1.53	0.15	0.575		
70	21.9	0.6	0.95	-0.32	-1.336	49.8	1.6	1.53	0.06	0.238		
75	20.8	0.6	0.95	-0.35	-1.573	47.3	1.5	1.53	-0.02	-0.108		
80	19.8	0.6	0.95	-0.38	-1.813	45.0	1.4	1.53	-0.10	-0.462		
85	18.9	0.5	0.95	-0.40	-2.056	43.0	1.4	1.53	-0.16	-0.821		
90	18.1	0.5	0.95	-0.43	-2.301	41.1	1.3	1.53	-0.22	-1.186		
95	17.4	0.5	0.95	-0.45	-2.548	39.4	1.3	1.53	-0.27	-1.556		
100	16.7	0.5	0.95	-0.47	-2.797	37.9	1.2	1.53	-0.32	-1.931		
105	16.1	0.5	0.95	-0.48	-3.047	36.5	1.2	1.53	-0.37	-2.309		
110	15.6	0.4	0.95	-0.50	-3.299	35.2	1.1	1.53	-0.41	-2.691		
115	15.0	0.4	0.95	-0.51	-3.552	34.0	1.1	1.53	-0.45	-3.077		
120	14.6	0.4	0.95	-0.53	-3.806	32.9	1.0	1.53	-0.48	-3.465		
Max Storag	le (m <sup>3</sup> )=				0.753					2.748		
Average Po	onding Depth	(mm)			6.6					24.0		
Maximum F	Ponding Dept	th (mm)			76.3					117.4		

1 ) Peak flow is equal to the product of 2.78 x C x I x A

2) Rainfall Intensity, I = A/(Tc/60)<sup>B</sup>

3) Release Rate = LESSER of Min (Release Rate, Peak Flow) - Minus 100 Year Flow Of Uncontroled Areas OR Pipe Outlet Capacity

4) Storage Rate = Peak Flow - Release Rate

5) Storage = Duration x Storage Rate

	Table VI - Storage Volumes (2-Year and 100-Year Storm Events)												
	Storage Requirement for RD-10												
	C <sub>AVG</sub> =	0.90	(2-year)										
	C <sub>AVG</sub> =	1.00	(100-year)			Watts Adjust	stable Accuti	rol Weir Roo	of Drain				
Tim	ne Interval =	5	(mins)										
Drair	nage Area =	0.014	(hectares)										
		137.93	(sqm)										
	F	Release Rate =	0.99	(L/sec) per	drain	Rele	ease Rate =	1.51	(L/sec) per	drain			
	R	eturn Period =	2	(years)		Retu	ırn Period =	100	(years)				
	IDF Pa	arameters, A =	732.951	, B =	0.810	IDF Para	meters, A =	1735.688	, B =	0.820			
		I = A/(	Г <sub>с</sub> +С)В	, C =	6.199		I = A/(Tc	+C)B	, C =	6.014			
	Rainfall			Storage		Rainfall		Release	Storage				
Duration	Intensity, I	Peak Flow	Release	Rate	Storage	Intensity, I	Peak Flow	Rate	Rate	Storage			
(min)	(mm/hr)	(L/sec)	Rate (L/sec)	(L/sec)	(m <sup>3</sup> )	(mm/hr)	(L/sec)	(L/sec)	(L/sec)	(m <sup>3</sup> )			
0	-	-	-	-	-	-	-	-	-	-			
5	103.6	3.6	0.99	2.59	0.776	242.7	9.3	1.51	7.79	2.338			
10	76.8	2.7	0.99	1.66	0.998	178.6	6.8	1.51	5.33	3.201			
15	61.8	2.1	0.99	1.14	1.030	142.9	5.5	1.51	3.97	3.570			
20	52.0	1.8	0.99	0.81	0.970	120.0	4.6	1.51	3.09	3.705			
25	45.2	1.6	0.99	0.57	0.858	103.8	4.0	1.51	2.47	3.705			
30	40.0	1.4	0.99	0.39	0.711	91.9	3.5	1.51	2.01	3.619			
35	36.1	1.2	0.99	0.26	0.540	82.6	3.2	1.51	1.65	3.474			
40	32.9	1.1	0.99	0.15	0.353	75.1	2.9	1.51	1.37	3.286			
45	30.2	1.0	0.99	0.06	0.153	69.1	2.6	1.51	1.14	3.066			
50	28.0	1.0	0.99	-0.02	-0.058	64.0	2.5	1.51	0.94	2.820			
55	26.2	0.9	0.99	-0.08	-0.277	59.6	2.3	1.51	0.77	2.554			
60	24.6	0.8	0.99	-0.14	-0.502	55.9	2.1	1.51	0.63	2.272			
65	23.2	0.8	0.99	-0.19	-0.733	52.6	2.0	1.51	0.51	1.975			
70	21.9	0.8	0.99	-0.23	-0.969	49.8	1.9	1.51	0.40	1.667			
75	20.8	0.7	0.99	-0.27	-1.209	47.3	1.8	1.51	0.30	1.349			
80	19.8	0.7	0.99	-0.30	-1.453	45.0	1.7	1.51	0.21	1.022			
85	18.9	0.7	0.99	-0.33	-1.700	43.0	1.6	1.51	0.13	0.688			
90	18.1	0.6	0.99	-0.36	-1.949	41.1	1.6	1.51	0.06	0.346			
95	17.4	0.6	0.99	-0.39	-2.201	39.4	1.5	1.51	0.00	-0.001			
100	16.7	0.6	0.99	-0.41	-2.455	37.9	1.5	1.51	-0.06	-0.353			
105	16.1	0.6	0.99	-0.43	-2.711	36.5	1.4	1.51	-0.11	-0.710			
110	15.6	0.5	0.99	-0.45	-2.968	35.2	1.3	1.51	-0.16	-1.072			
115	15.0	0.5	0.99	-0.47	-3.228	34.0	1.3	1.51	-0.21	-1.437			
120	14.6	0.5	0.99	-0.48	-3.488	32.9	1.3	1.51	-0.25	-1.806			
Max Storag	e (m <sup>3</sup> )=				1.030					3.705			
Average Po	onding Depth	(mm)			7.5					26.9			
Maximum F	Ponding Dept	th (mm)			79.6					121.9			

1 ) Peak flow is equal to the product of 2.78 x C x I x A

2) Rainfall Intensity, I = A/(Tc/60)<sup>B</sup>

3) Release Rate = LESSER of Min (Release Rate, Peak Flow) - Minus 100 Year Flow Of Uncontroled Areas OR Pipe Outlet Capacity

4) Storage Rate = Peak Flow - Release Rate

5) Storage = Duration x Storage Rate

		Table VII -	Storage V	olumes (	2-Year ai	nd 100-Ye	ear Storm	Events)		
			S	Storage Req	uirement f	or RD-11				
	$C_{AVG} = 0.90 \qquad (2-year)$									
	C <sub>AVG</sub> = 1.00 (100-year) Watts Adjustable Accutrol Weir Roof Drain									
Tim	ne Interval =	Interval = 5 (mins)								
Drair	nage Area =	0.016	(hectares)							
		158.67	(sqm)							
	F	Release Rate =	1.02	(L/sec) per	drain	Rele	ease Rate =	1.55	(L/sec) per	drain
	F	leturn Period =	2	(years)		Retu	urn Period =	100	(years)	
	IDF P	arameters, A =	732.951	, B =	0.810	IDF Para	meters, A =	1735.688	, B =	0.820
		I = A/(	Г <sub>с</sub> +С)В	, C =	6.199		I = A/(Tc	+C)B	, C =	6.014
	Rainfall			Storage		Rainfall		Release	Storage	
Duration	Intensity, I	Peak Flow	Release	Rate	Storage	Intensity, I	Peak Flow	Rate	Rate	Storage
(min)	(mm/hr)	(L/sec)	Rate (L/sec)	(L/sec)	(m <sup>3</sup> )	(mm/hr)	(L/sec)	(L/sec)	(L/sec)	(m <sup>3</sup> )
0	-	-	-	-	-	-	-	-	-	-
5	103.6	4.1	1.02	3.10	0.929	242.7	10.7	1.55	9.16	2.748
10	76.8	3.0	1.02	2.03	1.220	178.6	7.9	1.55	6.33	3.798
15	61.8	2.5	1.02	1.44	1.293	142.9	6.3	1.55	4.76	4.282
20	52.0	2.1	1.02	1.05	1.260	120.0	5.3	1.55	3.75	4.494
25	45.2	1.8	1.02	0.78	1.166	103.8	4.6	1.55	3.03	4.552
30	40.0	1.6	1.02	0.57	1.033	91.9	4.1	1.55	2.51	4.512
35	36.1	1.4	1.02	0.42	0.873	82.6	3.6	1.55	2.10	4.403
40	32.9	1.3	1.02	0.29	0.693	75.1	3.3	1.55	1.77	4.245
45	30.2	1.2	1.02	0.18	0.498	69.1	3.0	1.55	1.50	4.050
50	28.0	1.1	1.02	0.10	0.292	64.0	2.8	1.55	1.28	3.826
55	26.2	1.0	1.02	0.02	0.076	59.6	2.6	1.55	1.08	3.578
60	24.6	1.0	1.02	-0.04	-0.148	55.9	2.5	1.55	0.92	3.311
65	23.2	0.9	1.02	-0.10	-0.378	52.6	2.3	1.55	0.78	3.028
70	21.9	0.9	1.02	-0.15	-0.613	49.8	2.2	1.55	0.65	2.732
75	20.8	0.8	1.02	-0.19	-0.854	47.3	2.1	1.55	0.54	2.424
80	19.8	0.8	1.02	-0.23	-1.098	45.0	2.0	1.55	0.44	2.106
85	18.9	0.8	1.02	-0.26	-1.346	43.0	1.9	1.55	0.35	1.780
90	18.1	0.7	1.02	-0.30	-1.597	41.1	1.8	1.55	0.27	1.445
95	17.4	0.7	1.02	-0.32	-1.851	39.4	1.7	1.55	0.19	1.104
100	16.7	0.7	1.02	-0.35	-2.107	37.9	1.7	1.55	0.13	0.757
105	16.1	0.6	1.02	-0.38	-2.366	36.5	1.6	1.55	0.06	0.404
110	15.6	0.6	1.02	-0.40	-2.626	35.2	1.6	1.55	0.01	0.046
115	15.0	0.6	1.02	-0.42	-2.889	34.0	1.5	1.55	-0.05	-0.316
120	14.6	0.6	1.02	-0.44	-3.153	32.9	1.5	1.55	-0.09	-0.683
Max Storag	le (m <sup>3</sup> )=				1.293					4.552
Average Po	onding Depth	(mm)			8.1					28.7
Maximum F	Ponding Dep	th (mm)			81.9					124.6

1 ) Peak flow is equal to the product of 2.78 x C x I x A

2) Rainfall Intensity, I = A/(Tc/60)<sup>B</sup>

3) Release Rate = LESSER of Min (Release Rate, Peak Flow) - Minus 100 Year Flow Of Uncontroled Areas OR Pipe Outlet Capacity

4) Storage Rate = Peak Flow - Release Rate

5) Storage = Duration x Storage Rate

		Table VIII -	Storage V	olumes (	2-Year a	nd 100-Y	ear Storn	n Events)		
			S	Storage Req	uirement f	or RD-12				
	$C_{AVG} = 0.90 \qquad (2-year)$									
	C <sub>AVG</sub> =	1.00 (100-year) Watts Adjustable Accutrol Weir Roof Drain								
Tim	ne Interval =	5	(mins)							
Drair	nage Area =	0.013	(hectares)							
		127.64	(sqm)							
	F	Release Rate =	1.02	(L/sec) per	drain	Rele	ease Rate =	1.53	(L/sec) per	drain
	F	leturn Period =	2	(years)		Retu	urn Period =	100	(years)	
	IDF Pa	arameters, A =	732.951	, B =	0.810	IDF Para	meters, A =	1735.688	, B =	0.820
		I = A/(	Г <sub>с</sub> +С)В	, C =	6.199		I = A/(Tc	+C)B	, C =	6.014
	Rainfall			Storage		Rainfall		Release	Storage	
Duration	Intensity, I	Peak Flow	Release	Rate	Storage	Intensity, I	Peak Flow	Rate	Rate	Storage
(min)	(mm/hr)	(L/sec)	Rate (L/sec)	(L/sec)	(m <sup>3</sup> )	(mm/hr)	(L/sec)	(L/sec)	(L/sec)	(m <sup>3</sup> )
0	-	-	-	-	-	-	-	-	-	-
5	103.6	3.3	0.82	2.49	0.747	242.7	8.6	1.32	7.29	2.186
10	76.8	2.5	0.82	1.64	0.981	178.6	6.3	1.32	5.01	3.007
15	61.8	2.0	0.82	1.15	1.039	142.9	5.1	1.32	3.75	3.371
20	52.0	1.7	0.82	0.84	1.013	120.0	4.3	1.32	2.93	3.518
25	45.2	1.4	0.82	0.62	0.937	103.8	3.7	1.32	2.36	3.540
30	40.0	1.3	0.82	0.46	0.830	91.9	3.3	1.32	1.94	3.483
35	36.1	1.2	0.82	0.33	0.701	82.6	2.9	1.32	1.61	3.372
40	32.9	1.0	0.82	0.23	0.557	75.1	2.7	1.32	1.34	3.221
45	30.2	1.0	0.82	0.15	0.400	69.1	2.5	1.32	1.13	3.039
50	28.0	0.9	0.82	0.08	0.234	64.0	2.3	1.32	0.94	2.834
55	26.2	0.8	0.82	0.02	0.060	59.6	2.1	1.32	0.79	2.611
60	24.6	0.8	0.82	-0.03	-0.120	55.9	2.0	1.32	0.66	2.372
65	23.2	0.7	0.82	-0.08	-0.305	52.6	1.9	1.32	0.54	2.120
70	21.9	0.7	0.82	-0.12	-0.495	49.8	1.8	1.32	0.44	1.857
75	20.8	0.7	0.82	-0.15	-0.688	47.3	1.7	1.32	0.35	1.585
80	19.8	0.6	0.82	-0.18	-0.885	45.0	1.6	1.32	0.27	1.305
85	18.9	0.6	0.82	-0.21	-1.084	43.0	1.5	1.32	0.20	1.018
90	18.1	0.6	0.82	-0.24	-1.286	41.1	1.5	1.32	0.13	0.725
95	17.4	0.6	0.82	-0.26	-1.490	39.4	1.4	1.32	0.07	0.426
100	16.7	0.5	0.82	-0.28	-1.697	37.9	1.3	1.32	0.02	0.122
105	16.1	0.5	0.82	-0.30	-1.905	36.5	1.3	1.32	-0.03	-0.186
110	15.6	0.5	0.82	-0.32	-2.114	35.2	1.2	1.32	-0.08	-0.498
115	15.0	0.5	0.82	-0.34	-2.326	34.0	1.2	1.32	-0.12	-0.813
120	14.6	0.5	0.82	-0.35	-2.538	32.9	1.2	1.32	-0.16	-1.133
Max Storag	e (m°)=				1.039					3.540
Average Po	onding Depth	(mm)			8.1					27.7
Maximum F	Maximum Ponding Depth (mm)         81.9         123.3									

1) Peak flow is equal to the product of 2.78 x C x I x A

2) Rainfall Intensity, I = A/(Tc/60)<sup>B</sup>
 3) Release Rate = LESSER of Min (Release Rate, Peak Flow) - Minus 100 Year Flow Of Uncontroled Areas OR Pipe Outlet Capacity

4) Storage Rate = Peak Flow - Release Rate

5) Storage = Duration x Storage Rate

		Table IX -	Storage V	olumes (	2-Year a	nd 100-Y	ear Storn	n Events)	)	
	Storage Requirement for Uncontrolled Roof Drains and Ground Level Amenity Space Behind Building									
	C <sub>AVG</sub> =	0.90	(2-year)							
	C <sub>AVG</sub> =	1.00	(100-year)							
Tim	ne Interval =	5	(mins)							
Drair	nage Area =	0.112	(hectares)							
	Re	elease Rate =	4.9	(L/sec)		Rele	ease Rate =	4.9	(L/sec)	
	Re	turn Period =	2	(years)		Retu	urn Period =	100	(years)	
	IDF Par	ameters, A =	732.951	, B =	0.810	IDF Para	meters, A =	1735.688	, B =	0.820
		I = A/	/(T <sub>c</sub> +C)B	, C =	6.199		I = A/(Tc	+C)B	, C =	6.014
	Rainfall			Storage	-	Rainfall		Release	Storage	-
Duration	Intensity, I	Peak Flow	Release	Rate	Storage	Intensity, I	Peak Flow	Rate	Rate	Storage
(min)	(mm/hr)	(L/sec)	Rate (L/sec)	(L/sec)	(m³)	(mm/hr)	(L/sec)	(L/sec)	(L/sec)	(m³)
0	-	-	-	-	-	-	-	-	-	-
5	103.6	28.9	4.9	24.0	7.2	242.7	75.2	4.9	70.4	21.1
10	76.8	21.4	4.9	16.6	9.9	178.6	55.4	4.9	50.5	30.3
15	61.8	17.2	4.9	12.4	11.1	142.9	44.3	4.9	39.4	35.5
20	52.0	14.5	4.9	9.6	11.6	120.0	37.2	4.9	32.3	38.8
25	45.2	12.6	4.9	7.7	11.6	103.8	32.2	4.9	27.3	41.0
30	40.0	11.2	4.9	6.3	11.3	91.9	28.5	4.9	23.6	42.5
35	36.1	10.1	4.9	5.2	10.9	82.6	25.6	4.9	20.7	43.5
40	32.9	9.2	4.9	4.3	10.3	75.1	23.3	4.9	18.4	44.2
45	30.2	8.4	4.9	3.6	9.6	69.1	21.4	4.9	16.5	44.7
50	28.0	7.8	4.9	3.0	8.9	64.0	19.8	4.9	15.0	44.9
55	26.2	7.3	4.9	2.4	8.0	59.6	18.5	4.9	13.6	44.9
60	24.6	6.9	4.9	2.0	7.1	55.9	17.3	4.9	12.5	44.9
65	23.2	6.5	4.9	1.6	6.2	52.6	16.3	4.9	11.5	44.7
70	21.9	6.1	4.9	1.2	5.2	49.8	15.4	4.9	10.6	44.4
75	20.8	5.8	4.9	0.9	4.2	47.3	14.6	4.9	9.8	44.0
80	19.8	5.5	4.9	0.7	3.2	45.0	13.9	4.9	9.1	43.6
85	18.9	5.3	4.9	0.4	2.1	43.0	13.3	4.9	8.4	43.1
90	18.1	5.1	4.9	0.2	1.1	41.1	12.7	4.9	7.9	42.5
95	17.4	4.9	4.9	0.0	0.0	39.4	12.2	4.9	7.4	41.9
100	16.7	4.7	4.9	-0.2	-1.2	37.9	11.7	4.9	6.9	41.3
105	16.1	4.5	4.9	-0.4	-2.3	36.5	11.3	4.9	6.4	40.6
110	15.6	4.3	4.9	-0.5	-3.5	35.2	10.9	4.9	6.0	39.9
115	15.0	4.2	4.9	-0.7	-4.6	34.0	10.5	4.9	5.7	39.2
120	14.6	4.1	4.9	-0.8	-5.8	32.9	10.2	4.9	5.3	38.4
Max =					11.6					44.9

1) Peak flow is equal to the product of 2.78 x C x I x A

2) Rainfall Intensity, I = A/(Tc/60)<sup>B</sup>
 3) Release Rate = LESSER of Min (Release Rate, Peak Flow) - Minus 100 Year Flow Of Uncontroled Areas OR Pipe Outlet Capacity

4) Storage Rate = Peak Flow - Release Rate

5) Storage = Duration x Storage Rate

	Table )	K - Storag	e Volumes	(2-Year	and 100-	Year Sto	rm + 20%	Stress E	Events)	
				ieu Rooi Dr	ains and G	rouna Leve	i Amenity 5	расе Беліп	ia bullaing	
	C <sub>AVG</sub> -	0.90	(2-year)							
Tim		1.00	(100-year)							
		D 110	(mins)							
Drair	age Area =	0.112	(neclares)							
	Re	lease Rate =	4.9	(L/sec)		Rele	ease Rate =	4.9	(L/sec)	
	Re	turn Period =	2	(years)		Retu	urn Period =	100	(years)	
	IDF Par	ameters, A =	732.951	, B =	0.810	IDF Para	meters, A =	1735.688	, B =	0.820
		I = A/	(T <sub>c</sub> +C)B	, C =	6.199		I = A/(Tc	+C)B	, C = <u>6.014</u>	
	Rainfall			Storage		Rainfall		Release	Storage	
Duration	Intensity, I	Peak Flow	Release	Rate	Storage	Intensity, I	Peak Flow	Rate	Rate	Storage
(min)	(mm/hr)	(L/sec)	Rate (L/sec)	(L/sec)	(m <sup>3</sup> )	(mm/hr)	(L/sec)	(L/sec)	(L/sec)	(m <sup>3</sup> )
0	-	-	-	-	-	-	-	-	-	-
5	103.6	34.7	4.9	29.8	8.9	242.7	90.3	4.9	85.4	25.6
10	76.8	25.7	4.9	20.8	12.5	178.6	66.4	4.9	61.6	36.9
15	61.8	20.7	4.9	15.8	14.2	142.9	53.2	4.9	48.3	43.5
20	52.0	17.4	4.9	12.6	15.1	120.0	44.6	4.9	39.8	47.7
25	45.2	15.1	4.9	10.3	15.4	103.8	38.6	4.9	33.8	50.6
30	40.0	13.4	4.9	8.5	15.4	91.9	34.2	4.9	29.3	52.8
35	36.1	12.1	4.9	7.2	15.1	82.6	30.7	4.9	25.9	54.3
40	32.9	11.0	4.9	6.1	14.7	75.1	28.0	4.9	23.1	55.4
45	30.2	10.1	4.9	5.3	14.2	69.1	25.7	4.9	20.8	56.2
50	28.0	9.4	4.9	4.5	13.6	64.0	23.8	4.9	18.9	56.8
55	26.2	8.8	4.9	3.9	12.9	59.6	22.2	4.9	17.3	57.1
60	24.6	8.2	4.9	3.4	12.1	55.9	20.8	4.9	15.9	57.3
65	23.2	7.8	4.9	2.9	11.2	52.6	19.6	4.9	14.7	57.4
70	21.9	7.3	4.9	2.5	10.4	49.8	18.5	4.9	13.7	57.4
75	20.8	7.0	4.9	2.1	9.5	47.3	17.6	4.9	12.7	57.2
80	19.8	6.6	4.9	1.8	8.5	45.0	16.7	4.9	11.9	57.0
85	18.9	6.3	4.9	1.5	7.5	43.0	16.0	4.9	11.1	56.7
90	18.1	6.1	4.9	1.2	6.5	41.1	15.3	4.9	10.4	56.3
95	17.4	5.8	4.9	1.0	5.5	39.4	14.7	4.9	9.8	55.9
100	16.7	5.6	4.9	0.7	4.4	37.9	14.1	4.9	9.2	55.4
105	16.1	5.4	4.9	0.5	3.4	36.5	13.6	4.9	8.7	54.9
110	15.6	5.2	4.9	0.3	2.3	35.2	13.1	4.9	8.2	54.3
115	15.0	5.0	4.9	0.2	1.2	34.0	12.6	4.9	7.8	53.7
120	14.6	4.9	4.9	0.0	0.1	32.9	12.2	4.9	7.4	53.1
Max =					15.4					57.4

1) Peak flow is equal to the product of 2.78 x C x I x A

2) Rainfall Intensity, I = A/(Tc/60)<sup>B</sup>
 3) Release Rate = LESSER of Min (Release Rate, Peak Flow) - Minus 100 Year Flow Of Uncontroled Areas OR Pipe Outlet Capacity

4) Storage Rate = Peak Flow - Release Rate

5) Storage = Duration x Storage Rate

## FLOW CONTROL ROOF DRAINAGE DECLARATION

THIS FORM TO BE COMPLETED BY THE MECHANICAL AND STRUCTURAL ENGINEERS RESPONSIBLE FOR DESIGN

		Permit Application No.
Project Name:	473 Albert, Proposed Mixed Use Renovatio	n
Building Location	n:	Municipality:
	473 Albert, Ottawa, Ontario	City of Ottawa
The roof draina	ge system has been designed in accordance with	the following criteria: (please check one of the following).
M1. 🗖	Conventionally drained roof (no flow control ro	of drains used).
M2. 🛛	Flow control roof drains meeting the following	conditions have been incorporated in this design:
	<ul> <li>(a) the maximum drain down time does</li> <li>(b) one or more scuppers are installed s cannot exceed 150mm,</li> <li>(c) drains are located not more than 15r adjacent drains, and</li> <li>(d) there is at least one drain for each 9</li> </ul>	not exceed 24h, o that the maximum depth of water on the roof n from the edge of roof and not more than 30m from 0 sq.m.
M3. 🗖	A flow control drainage system that does not r M2 has been incorporated in this design.	PROFESSIONAL
PROFESSIONAL	L SEAL APPLIED BY:	\$ 2020. 63. 35%
Practitioner's Nar	ne: Elaine Guenette	E.J.GUENETTA ZA
Firm:	Smith and Andersen	19372.002
Phone#:	613-552-8335	LINCE OF ONTA
City: Ottawa	Province: Ontario	Mechanical Engineer's Seal
S1. 🕱	The design parameters incorporated into the or the Mechanical Engineer in M2. Loads due to per Sentence 4.1.7.3 (3) OBC.	verall structural design are consistent with the information provided by ain are not considered to act simultaneously with loads due to snow as
S2. 🗖	The structure has been designed incorporating snow load. The design parameters are consist engineer.	the additional structural loading due to rain acting simultaneously with the ont with the control flow drainage system designed by the mechanical
PROFESSIONAL	SEAL APPLIED BY:	PROFESSIONAL
Practitioner's Nan	<sup>ne:</sup> Colin Davies, P.Eng.	& Claude
Firm: Clelan	d Jardine Engineering Ltd	Apr 6, 2020
Phone#: 613	-591-1533	BUNCE OF ONTARIO
City: Ottaw	a Province: Ontario	Structural Engineer's Seal

**APPENDIX H** | ENGINEERING DRAWINGS AND SPECIFICATIONS



- STORM SEWER SYSTEM, ALL GRASSED AREAS MUST BE COMPLETED PRIOR TO THE REMOVAL OF THE FILTER FABRIC IN THE CATCH BASINS. 15. REMOVE FROM SITE ALL EXCESS EXCAVATED MATERIAL UNLESS OTHERWISE DIRECTED FROM THE ENGINEER. EXCAVATE AND REMOVE ALL ORGANIC MATERIAL AND DEBRIS LOCATED WITHIN THE PROPOSED BUILDING. PARKING AND ROADWAY LOCATIONS. ANY CONTAMINATED MATERIAL SHALL BE DISPOSED OF AT A LICENSED LANDFILL FACILITY.
- 16. THE APPROVAL OF THIS PLAN DOES NOT EXEMPT THE CONTRACTOR FROM THE REQUIREMENTS TO OBTAIN THE VARIOUS PERMITS/APPROVALS REQUIRED TO COMPLETE A CONSTRUCTION PROJECT, SUCH AS BUT NOT LIMITED TO; ROAD CUT PERMITS, SEWER PERMITS, WATER PERMIT, ETC.
- 17. AT PROPOSED UTILITY CONNECTION POINTS AND CROSSINGS (I.E. STORM SEWER, SANITARY SEWER, WATER, ETC.) THE CONTRACTOR SHALL DETERMINE THE PRECISE LOCATION AND DEPTH AND SIZE OF EXISTING UTILITIES AND REPORT ANY DISCREPANCIES OR CONFLICTS TO THE ENGINEER BEFORE COMMENCING WORK. PROTECT AND ASSUME RESPONSIBILITY FOR ALL EXISTING UTILITIES.
- 18. REFER TO ARCHITECT AND LANDSCAPE ARCHITECTS DRAWINGS FOR BUILDING, LANDSCAPE, AND HARD SURFACE AREAS AND DIMENSIONS, 19. CONTRACTOR IS RESPONSIBLE TO KEEP THE ROADS FREE AND CLEAN FROM MUD OR DEBRIS.
- INSPECT THEM FREQUENTLY AND CLEAN AND REPAIR OR REPLACE THE DETERIORATED STRUCTURES. AT THE END OF THE CONSTRUCTION PERIOD, THE CONTRACTOR IS RESPONSIBLE FOR REMOVAL OF THE . TEMPORARY STRUCTURES AND RECONDITIONING THE AFFECTED AREAS

- GEOTEXTILE FABRIC TO AVOID FINE PARTICLE TRANSPORT BY WIND AND/OR STREAMING RAIN WATER.
- CONTROL WIND-BLOWN DUST OFF SITE TO ACCEPTABLE LEVELS BY SEEDING TOPSOIL PILES AND OTHER AREAS TEMPORARILY (PROVIDE WATERING AS REQUIRED). FOR DUST CONTROL, CONTRACTOR TO APPLY CALCIUM CHLORIDE (TYPE I - OPSS 2501 AND CAN/CGSB-15-1) AND WATER WITH EQUIPMENT APPROVED BY THE OWNER'S REPRESENTATIVE AT RATE IN ACCORDANCE TO OPSS 506 WHEN DIRECTED BY OWNER'S REPRESENTATIVE.
- ALL EROSION CONTROL STRUCTURE TO REMAIN IN PLACE UNTIL ALL DISTURBED GROUND SURFACES HAVE BEEN DESTABILIZED EITHER BY PAVING OR RESTORATION OF VEGETATIVE GROUND COVER. SEDIMENT CAPTURE SILT SACKS MUST BE MAINTAINED AND CANNOT BE REMOVED UNTIL ALL LANDSCAPING AREAS ARE COMPLETED. NO ALTERNATE METHODS OF EROSION PROTECTION SHALL BE PERMITTED

- FILTER CLOTHS ON CATCH BASINS AND MANHOLE COVERS. INSPECT AND CLEAN CATCH BASIN SUMPS AND STORM SEWERS.

- 20. SUPPLY AND INSTALL ALL WATERMAIN ACCORDANCE WITH MOST CURRENT CITY O
- 21. ALL WATER MAIN TO BE INSTALLED AT MININ
- 23. CONCRETE THRUST BLOCKS AND RESTRA
- THAT THE AMOUNT OF DEFLECTION USED
- CONNECTIONS AND SHUT-OFFS AT THE MAIN

![](_page_93_Figure_28.jpeg)

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Image: Construction of the second s	$\begin{array}{c c} \mathbf{TRUCTION} & \mathbf{B} & \underline{\mathbf{B}} \\ - & \mathbf{B} & \underline{\mathbf{B}} & \underline{\mathbf{B}} & \mathbf{B} \\ - & \mathbf{B} & \mathbf{B} & \mathbf{B} & \mathbf{B} \\ - & \mathbf{B} & \mathbf{B} & \mathbf{B} & \mathbf{B} \end{array}$	
Match         Match <th< td=""><td>0<sup>1/57</sup> <u>172.</u>24 </td><td></td></th<>	0 <sup>1/57</sup> <u>172.</u> 24 	
<b>73.84</b> 73.84 73.87 74.07 0 ABN W ABN W ABN W ABN W	Concrete Curb	
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T CURRENT CITY OF OTTAWA STANDARDS AND		
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DEFLECTION USED IS LESS THAN HALF THAT MANUFACTURER. ATION, AND BACKFILL BY CONTRACTOR. -OFFS AT THE MAIN BY CITY.		
<u>D:</u>		
EXISTING PROPERTY LINE	COMB	EXISTING COMBINED SEWER AND MANHOLE
PROPOSED CONCRETE CURB - PROPOSED DEPRESSED CURB -	S S ● ST ST	PROPOSED SANITARY SEWER AND MANHOLE EXISTING STORM SEWER
- PROPOSED BUILDING OR STRUCTURE	ST ST	PROPOSED STORM SEWER AND MANHOLE PROPOSED CATCH BASIN
EXISTING WATERMAIN EXISTING ABANDONED WATERMAIN	113.45 <sup>×</sup> 114.40 <sup>×</sup>	EXISTING GRADE PROPOSED GRADE
EXISTING V&VB EXISTING CURBSTOP	<u>0.7%</u>	PROPOSED SLOPE SILT SACKS IN CATCH BASIN GRATE PER DETAIL D1
EXISTING FIRE HYDRANT PROPOSED WATERMAIN PROPOSED V&VB		PROPOSED MAXIMUM PONDING LIMIT PRIOR TO OVERFLOW
PROPOSED FIRE HYDRANT EXISTING UNDERGROUND GAS		PROPOSED MAJOR OVERLAND FLOW PROPOSED WATERSHED BOUNDARY
EXISTING UNDERGROUND BELL EXISTING UNDERGROUND POWER	WS-03	
EXISTING UVERHEAD WIRES EXISTING UNDERGROUND COMMUNICATIONS	0.039 0.90	- AREA (IN HECTARES)

owner   propriétaire	Ottawa, Ontario K2P 1Z2 613-806-7816
Structural engineers   ingénieur structure	D D D 200-580 TERRY FOX DR. KANATA, ON K2L 489 (613) 591-1533
530 - 1600 Carling Avenue Ottawa Onta t 613 230 1186 smithandandersen MEP engineers   ingénieur MEP	n nio K1Z 1G3 .com
DARSON 1223 MICHAEL STREET, SUITE 100, OTTAWA, ONT Tel: 613-738-4160 Fax: 613-739-7105	ARIO K1J 7T2
general notes   note générale 1. CONTRACTOR SHALL CHECK AND VERIFY ALL DIM REPORT ALL ERRORS AND OMISSIONS TO THE ARCI 2. DO NOT SCALE THE DRAWINGS. 3. NOT FOR CONSTRUCTION UNTIL SIGNED BY THE AR	ENSIONS AND HITECT. CHITECT.
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CLELANI JARDIN ENGINEERING Structural engineers   ingénieur structure	DEBC 200-580 TERRY FOX DR. KANATA, ON K21, 489 (613) 591-1533
Smith + Andersen 530 - 1600 Carling Avenue Ottawa Ontario t 613 230 1186 smithandandersen.cc	K1Z 1G3
MEP engineers   ingénieur MEP PARSON 1223 MICHAEL STREET, SUITE 100, OTTAWA, ONTARI Tel: 613-738-4160 Fax: 613-739-7105	0 K1J 7T2
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![](_page_95_Figure_0.jpeg)

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DEPRESSED CUR

Adjustable Accutrol Weir Adjustable Flow Control for Roof Drains

For more flexibility in controlling flow with heads deeper than 2", Watts Drainage offers the Adjustable Accutrol. The Adjustable Accutrol Weir is designed with a single parabolic opening that can be covered to restrict flow above 2" of head to less than 5 gpm per inch, up to 6" of head. To adjust the flow rate for depits over 2" of head, set the slot in the adjustable upper cone according to the flow rate required. Reflex to Table 1 below. Note: Flow rates are directly proportional to the amount of weir opening that is exposed.

ADJUSTABLE ACCUTROL (for Large Sump Roof Drains only)

![](_page_95_Figure_4.jpeg)

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-	10	)0mm	N/A	3	6	8	10	14
	11	50mm	N/A	N/A	4	6	9	13
-	20	0mm	N/A	N/A	N/A	3	6	11
	25	50mm	N/A	N/A	N/A	N/A	4	9
1	30	)0mm	N/A	N/A	N/A	N/A	N/A	7
68	40	)0mm	N/A	N/A	N/A	N/A	N/A	N/A
DE	AD ENDS, CA	PS, PLUGS, VALVES	100mm	150mm	200mm	250mm	300mm	400mr
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-	VERTI	CAL BENDS						
-	LENGTH H	GH SIDE - LHS	3	4	5	6	7	9
_	LENGTH L	DW SIDE - LLS	1.5	2	2.5	3	3.5	4.5
		TEES						
6	LENGTH ALON	G THE BRANCH - L	1	1	1	1	1	1
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485 Bank Street, Suite 200 613-806-7816 613-806-7816
CLELAND JARDINE ENGINEERING LTD
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APPENDIX I | PIPE DATA FORM

![](_page_97_Picture_0.jpeg)

Ministry of the Environment and Climate Change

Pipe Data Form - Watermain, Storm Sewer, Sanitary Sewer, and Forcemain Design Supplement to Application for Approval for Water and Sewage Works

### General

Information requested in this form is collected under the authority of the *Ontario Water Resources Act*, R.S.O. 1990 (OWRA), the *Safe Drinking Water Act* (SDWA), the Drinking-Water Systems Regulation (O. Reg. 170.03) and the Environmental Bill of Rights, c. 28, Statutes of Ontario 1993 (EBR). This information will be used to evaluate applications for approval of municipal and private sewage works as required by Section 53 (OWRA) and to evaluate applications for approval of municipal and non- municipal drinking-water systems as required by Sections 31, 36, 38, 52 and 60 of the SDWA.

### Instructions

- This form should accompany all Applications for a Water and Sewage Works. It does not replace the Application form for a Certificate of Approval and is required in addition to the supporting technical information described in the Guide for Applying for Municipal and Private Water and Sewage Works. All designs are expected to be in accordance with MOECC design guidelines and the 10 State Standards.
- 2. The information contained in this form and the required supporting stamped engineering drawings are the minimum information requirements used to process the application for a Certificate of Approval. All sections MUST be filled out and incomplete forms will be RETURNED to the applicant. If the design does not meet the MOECC design guidelines and the 10 State Standards, please explain why and how the issue will be addressed. Additional information may be requested during the review process.
- 3. Application forms and supporting documentation are available from the Client Services and Permissions Branch (CSPB) toll free at 1-800-461-6290 (locally at 416-314-8001), from your local District Office of the Ministry of the Environment and Climate Change, and in the "Publications" section of the Ministry of the Environment and Climate Change website at <a href="https://www.ontario.ca/page/water-and-sewage-works-approvals-sample-applications-guides-and-resources">https://www.ontario.ca/page/water-and-sewage-works-approvals-sample-applications-guides-and-resources</a>
- 4. Questions regarding completion and submission of this data form should be directed to the Client Services and Permissions Branch (CSPB), 135 St. Clair Avenue West, 1<sup>st</sup> Floor, Toronto, Ontario, M4V 1P5, 1-800-461-6290 or (416) 314-8001, or to your local District Office of the Ministry of the Environment and Climate Change.

## Information for Proponents Applying for a ECA for Water and Sewage Works

Section 53 of the *Ontario Water Resources Act* R.S.O. 1990 and Part V of the *Safe Drinking Water Act* require that anyone who establishes, alters, extends or replaces new or existing water or sewage works do so only in accordance with approval granted by the Director. As a result, any plans to change watermains, storm sewers, sanitary sewers, or combined sewers must first be granted a Certificate of Approval (works which are exempt from Certificate of Approval requirements are detailed in Ontario Regulation 525/98). Detailed information on approval requirements and procedures are contained in separate documents entitled "Guide for Applying for Approval of Municipal and Private Water and Sewage Works (Section 53 *Ontario Water Resources Act* R.S.O. 1990)" and "Guide For Applying For Approvals Related To Municipal And Nun-Municipal Drinking-Water-Systems – Parts V and VI of the *Safe Drinking Water Act* and Drinking-Water Systems Regulation" These documents are available on the Ministry of the Environment and Climate Change's website (<u>https://www.ontario.ca/page/water-and-sewage-works-approvals-sample-applications-guides-and-resources</u>) or can be obtained by contacting a client services representative at (413) 314-8001.

## Criteria for Approval - Water and Sewage Works

The anticipated environmental impacts of water and sewage works are land and water contamination, or overflow causing physical damage, or resulting in adverse effects. Generally, these impacts can be minimized by the appropriate design installation, operating and maintenance of the water and sewage pipes. There are a number of guideline assessment criteria, which will be explained in this data form, and which can be read in greater detail in the following guidelines:

- · Guidelines for the design of water distribution systems, Ministry of the Environment, 1985
- Guidelines for the design of sanitary sewage systems, Ministry of the Environment, 1985
- · Interim guidelines for the design of storm sewer systems, Ministry of the Environment, 1985
- Procedure for the Determination of Treatment Requirements for Municipal and Private Combined and Partially Separated Sewer Systems (Procedure F-5-5)
- Procedures to govern separation of sewers and watermains (Procedure F-6-1)

1.0 General Project Information
1.1 Site Name
473 Albert Street
1.2 Municipality
City of Ottawa
Client (if different from Municipality)
12 Time of Media Data (17)
1.3 Type of vvorks Project (Please check all that apply)
Watermain Please complete Sections 1.0 to 5.0 of this form
Storm Sewer Please complete Sections 1.0 to 4.0, 6.0 and Appendix A of this form
Sanitary Sewer Please complete Sections 1.0 to 4.0, 7.0 and Appendix B of this form
Forcemain Please complete Sections 1.0 to 4.0, 8.0 and Appendix C of this form
1.4 (a) Project Purpose (Please check all that apply)
Replacement
Increased demand
Connecting existing lines
New development
Other (specify) Reusing existing storm and sanitary services to a combined sewer
2.0 Environmental Assessment Act Requirements
2.1 Is this a private sector project?
Yes No If 'No', please complete 2.2 and 2.3
2.2 (a) Choose applicable Municipal sector Class EA Schedule
Schedule A
Schedule B
Schedule C
(b) From the appropriate Schedule identified in 2.2(a), please identify Project Type and associated Schedule/Paragraph No. which applies to the proposed project
Water Project
Wastewater Project Schedule Number
For 'Schedule B' please complete 2.3(a),(b) For 'Schedule C', please complete 2.3(a) (b) (c)
2.3 (a) Has a Notice of Completion been submitted along with this application?
(b) Were any Part II Orders (ie "Bump-up" requests) received for this project?
Yes No If 'Yes' please provide details:
(c) Has an Environmental Study Report (ESR) been completed?
Yes If 'Yes', please include ESR Cover page with this submission
3.0 Drawings
Note: All drawings must include an accurate scale and be stamped by a Professional engineer. If the drawing is of a large scale where small separation distances cannot be easily measured, these distances must be marked on the drawing or noted as a trained engineer.
Have the following details been included with this submission?
✓ Site Plan, including
✓ Proposed works
✓ Existing works (as appropriate)
✓ Property lines/Municipal boundaries

🗌 Any	water bodies in proximity to the works
🖌 Plan and	Profile of all Pipes
Horiz	zontal distance between watermains and sewers
🗸 Verti	ical distance between watermains and sewers
Lenç	pth, diameter and slope of each pipe segment
🖌 Loca	ations of valves, valve chambers if > 300mm diametre, pressure reducers, tees, etc.
Loca	ation of manholes (and their respective IDs)
Storm Dra	ainage Area
 ✓ Indic	ate all areas which drain into the proposed works
V Phys	sical area in hectares
✓ Runc	off Coefficient for each drainage area
🖌 Storn	n water drainage path
Sanitary D	Drainage Area
Indica	ate all areas which drain into the proposed works
🗌 Physi	ical area in hectares
Popu	lation for each drainage area
Sanita	ary Sewer drainage path
Other Deta	ails
Typic:	al separations, where not easily measured from pipe drawings
Apper	rtunances
Munic	cipal drains
4.0 Addition	nal Information
4.1 Are the pr	roposed works laid below the frost penetration depth for the area at all points?
Yes	✓ No
4.2 (a) Are all sewer:	l existing and proposed watermains separated by at least 2.5 m of clear horizontal distance from all existing and proposed s and storm water conveyance systems (ie. ditches)?
Ves Yes	No
(b) Are all e sewers	existing and proposed watermains separated by at least 0.5 m of clear vertical distance higher than all existing and proposed and storm water conveyance systems (ie. ditches)?
✓ Yes	No
(c) Are all e potable	existing and proposed sewers, including all drains and similar sources of contamination, separated by at least 15 metres from water reservoirs below normal ground surface and well supplies?
🖌 Yes	No No
If 'No' to an be met	by part of Question 4.0, please refer to Procedure F-6-1 for solutions to prevent contamination when separation distances cannot
50 Waterm:	ains

5.2 Description of Existing Works (in proximity to proposed works)

5.3	For each watermain,	please provide the following details in the chart below (or equivalent)
	and a second	provide the following details in the chart below (of equivalent)

Street	From (street/manhole)	To (street/manhole)	Diameter (mm)	Rouahness
.4 Are all of the waterma	ins a minimum of 150 mm in diame	ter?		
Yes No				
5.5 What is the expected	operating pressure range for this wa	atermain under maximum da	ay demand?	
	to		(please indicate uni	ts)
5.6 (a) Will the watermain	pressure drop below 275 kPa (40 p	si)?		
Yes No				
If 'Yes', please provide	an explanation for this situation an	d future plans to address th	e problem	
(b) Is there sufficient an	(1001.00			
(b) Is there sufficient pro	essure (138 kPA or 20 psi) reserved	for fire flow/protection?		
(b) Is there sufficient pro	essure (138 kPA or 20 psi) reserved	for fire flow/protection?		
<ul> <li>(b) Is there sufficient pre</li> <li>Yes No</li> <li>.7 If this is a feedermain of been considered?</li> </ul>	essure (138 kPA or 20 psi) reserved or a pipe dedicated to transporting p	for fire flow/protection?	g no service connections)	, have hydraulic transie
(b) Is there sufficient provide the sufficient provides the	essure (138 kPA or 20 psi) reserved	d for fire flow/protection?	g no service connections)	, have hydraulic transie
(b) Is there sufficient pro- Yes No If this is a feedermain of been considered? Yes No If 'Yes', please describe	essure (138 kPA or 20 psi) reserved or a pipe dedicated to transporting p e the results	for fire flow/protection?	g no service connections)	, have hydraulic transie
<ul> <li>(b) Is there sufficient present the present of the presen</li></ul>	essure (138 kPA or 20 psi) reserved or a pipe dedicated to transporting p e the results	d for fire flow/protection?	g no service connections)	, have hydraulic transie
(b) Is there sufficient pro	essure (138 kPA or 20 psi) reserved or a pipe dedicated to transporting p e the results	d for fire flow/protection?	g no service connections)	, have hydraulic transie
<ul> <li>(b) Is there sufficient pre</li> <li>Yes No</li> <li>If this is a feedermain of been considered?</li> <li>Yes No</li> <li>If 'Yes', please described</li> </ul>	essure (138 kPA or 20 psi) reserved or a pipe dedicated to transporting p e the results	d for fire flow/protection?	g no service connections)	, have hydraulic transie
<ul> <li>(b) Is there sufficient products</li> <li>Yes No</li> <li>If this is a feedermain of been considered?</li> <li>Yes No</li> <li>If 'Yes', please describe</li> </ul>	essure (138 kPA or 20 psi) reserved or a pipe dedicated to transporting p e the results	d for fire flow/protection?	g no service connections)	, have hydraulic transie
<ul> <li>(b) Is there sufficient products</li> <li>Yes No</li> <li>If this is a feedermain of been considered?</li> <li>Yes No</li> <li>If 'Yes', please describe</li> </ul> 8 (a) Are there any dead	essure (138 kPA or 20 psi) reserved or a pipe dedicated to transporting p e the results end points in the system?	d for fire flow/protection?	g no service connections)	, have hydraulic transie
<ul> <li>(b) Is there sufficient president of the sufficient present of the second sec</li></ul>	essure (138 kPA or 20 psi) reserved or a pipe dedicated to transporting p e the results end points in the system? ''Yes', then please complete 5.8(b)	d for fire flow/protection?	g no service connections)	, have hydraulic transie
<ul> <li>(b) Is there sufficient products</li> <li>Yes No</li> <li>If this is a feedermain of been considered?</li> <li>Yes No</li> <li>If 'Yes', please described</li> </ul> 8 (a) Are there any dead <ul> <li>Yes No</li> <li>If 'Yes' No</li> <li>If 'Yes' No</li> </ul>	essure (138 kPA or 20 psi) reserved or a pipe dedicated to transporting p e the results end points in the system? 'Yes', then please complete 5.8(b) ation be addressed?	d for fire flow/protection?	g no service connections)	, have hydraulic transie
<ul> <li>(b) Is there sufficient preside the preside the presentation of the presentat</li></ul>	essure (138 kPA or 20 psi) reserved or a pipe dedicated to transporting p e the results end points in the system? "Yes', then please complete 5.8(b) ation be addressed? Blow-off point Other (Specify)	d for fire flow/protection?	g no service connections)	, have hydraulic transie
<ul> <li>(b) Is there sufficient products of the sufficient product of the sufficient product of the sufficient product of the sufficient of the sufficient</li></ul>	essure (138 kPA or 20 psi) reserved or a pipe dedicated to transporting p e the results end points in the system? "Yes', then please complete 5.8(b) ation be addressed? Blow-off point Other (Specify) r cross-connections?	d for fire flow/protection?	g no service connections)	, have hydraulic transie
<ul> <li>(b) Is there sufficient products of the sufficient products of the</li></ul>	essure (138 kPA or 20 psi) reserved or a pipe dedicated to transporting p e the results end points in the system? 'Yes', then please complete 5.8(b) ation be addressed? Blow-off point Other (Specify) r cross-connections? 'Yes', then please complete 5.9(b)	d for fire flow/protection?	g no service connections)	, have hydraulic transie
<ul> <li>(b) Is there sufficient products of the sufficient of the</li></ul>	essure (138 kPA or 20 psi) reserved or a pipe dedicated to transporting p e the results end points in the system? "Yes', then please complete 5.8(b) ation be addressed? Blow-off point	d for fire flow/protection?	g no service connections)	, have hydraulic transic
<ul> <li>(b) Is there sufficient properties a feedermain of been considered?</li> <li>Yes No</li> <li>Yes No</li> <li>Yes', please described</li> <li>Yes', please described</li> <li>8 (a) Are there any dead</li> <li>Yes No</li> <li>No</li> <li>If 'Yes' No</li> <li>If (b) How will water stagnate of the stagnate of the</li></ul>	essure (138 kPA or 20 psi) reserved or a pipe dedicated to transporting p e the results end points in the system? "Yes', then please complete 5.8(b) ation be addressed? Blow-off point Other (Specify) r cross-connections? "Yes', then please complete 5.9(b) (2) shut-off valves at each tee-con	d for fire flow/protection? Potable water only (ie. having	g no service connections)	, have hydraulic transic

## 6.0 Storm Sewers

For Questions 6.1 to 6.3, please attach an additional sheet if necessary

6.1 Description of Proposed Storm Sewer(s) (including service area/development) See Design Brief.

6.2 Is this application for approval a part of a larger and/or phased development?

Yes 🖌 No If 'Yes', please provide full details on any existing developments including all Certificates of Approval that have been approved or application that are currently under review. Clearly indicate in all stamped engineering drawings and reports which developments belong to which phase and whether they are existing, for current development, or for future development

6.3 Description of Existing Works (in proximity to proposed works) See Design Brief.

6.4 For each storm sewer, please provide the following details in the chart below (or equivalent)

Street	From (street/manhole)	To (street/manhole)	Diameter (mm)	Roughness
473 Albert Street (existing)	Building	Sewer	200	0.013

## 6.5 Has the Storm Sewer Hydraulic Design Sheet (or equivalent) been included with this submission? (refer to the Guidance Document in Appendix A)

1	Yes	No

## 6.6 Please indicate which land use surface types are included in the drainage area and list the runoff coefficient(s) used for each type

	Surface Type	Recommended	Used
1	Asphalt, concrete, roof areas	0.90 - 1.00	0.9
	Gravel	0.80 - 0.85	
	Grassed areas, parkland	0.15 - 0.35	
	Commercial	0.75 - 0.85	
	Industrial	0.65 - 0.75	
	Single family dwelling	0.40 - 0.45	
	Semi-detached	0.45 - 0.60	
	Row housing, Townhousing	0.50 - 0.70	
	Apartments	0.60 - 0.75	
	Institutional	0.40 - 0.75	
	Other		
16110			

If USED runoff coefficient does not fall within the RECOMMENDED range, please provide rationale below:

to 1.11

6.7 (a) What is the full flow velocity range for all storm sewers in the proposed works?

1.11

m/s

(b) If the full flow velocity is outside of the range of 0.8 m/s to 6.0 m/s, what measures will be employed to reduce sediment build up and/or erosion in the pipe?

6.8 (a) V	Vhat is the municip	ality's requirement	for the minor	design storm ever	nt?			
$\checkmark$ 2	2 year 🗌 5 year	10 year [	Other					
(b) W	hat storm event ha	s been used for th	e design of th	e proposed works	?			
✓ 2	2 year 🗌 5 year	🗌 10 year 🛛	Other					
(c) Ar	e there any inlet co	ntrol devices (ICD	s) proposed in	n the catch basins	?			
Y	′es 🖌 No							
6.9 Pleas	se indicate the first	destination/location	on that will be	receiving the storr	n water:			
Natura	al Water Body							
N	ame							
	Has the Cons	ervation Authority ] No	granted appro	oval to discharge t	o this wa	ter body?		
Storm	Water Managemer	nt (SWM) Facility						
Na	me	1999						
	Certificate of Ap	proval Number (if	applicable)			1. Constanting of the second	an a	OR
	Application Refe	erence Number (if	submitted)					
	Has the Opera	ating Authority (of	the SWM facil	ity) granted appro	al to dis	charge to this facility?		
<b>—</b>	Yes	No						
	pal Drain							
Existing	g Sewers							
7.0 Sani	tary Sewers							
7.1 Descri	ption of Proposed S	se attach an addit Sanitary Sewer(s)	ional sheet if r (including ser	necessary vice area/developr	nent)			
See Desi	gn Brief				,			
7.2 Descri	ption of Existing W	orks (in proximity t	o proposed w	orks)				
73 For or								
	ch sewer, please p	Founde the following	ng details in th	e chart below (or e	equivaler	it)	1	
	Street	From (street	/manhole)	To (street/ma	nhole)	Diameter (mm)	Roughness	
473 Alber	rt Street	Building		Sewer		200	0.013	
(existing)		<u></u>						
7.4 Has th	e Sanitary Sewer [	Desian Sheet (or e	quivalent) bee	n included with th		ninn? (refer to Ouill		
Ve Ye	s 🗌 No		quivalenty bee			sion? (refer to Guidan	ce Document in Appendix B	)
7.5 Please	indicate which sev	vage types are apr	licable in the	drainage area and	lict the d	oily design flours		
	Sewage Type	<u> </u>	Recommend	ed	Used	any design nows used	In the pipe design for each t	уре.
1	Domestic		225 - 450 L/c	ap/day	280 L/	p/d		
	Hospitals		900 - 1800 L/	/bed/day				
	Schools		70 - 140 L/stu	udent/day				
	Trailer Parks		340 - 800 L/s	pace/day				
	Infiltration		0.1 - 0.28 L/h	a/s				
	Industrial		35 - 55 m3/h	a/dav				
	Shopping Centres	1	2500 - 5000 1	/1000 m2/day				
	Hotels/Motels		150 - 225 L/h	ed space/day				
 	Other			ou space/udy				
hand	and the second sec							

If USED sewage daily design flow does not fall within the RECOMMENDED range, please provide rationale below

1 00	toroonly range for an samilary ser	wers in the proposed works?	?	
.20	to 1.28		m/s	
(b) If the full flow veloci erosion in the pipe?	ity is outside of the range of 0.6 m	n/s to 3.0 m/s, what measure	es will be employed to red	uce sewage build up and/or
7.7 It is recommended that the depth of any basen	sanitary sewers be laid at sufficionents in the area?	ent depth to receive gravity	flow from basements. Are	any sanitary sewers above
[√] Yes [] No If 'Yes', what methods will be backwater valve	e employed to prevent sewage ba	ackup into basements?		
8.0 Forcemains				
For Questions 8.1 to 8.3, ple	ase attach an additional sheet if i	necessary		
3.1 Description of Proposed	Forcemain(s) (including service	area/development)		
2 Departmention of Eviction 1				
5.2 Description of Existing V	Vorks (in proximity to proposed w	orks)		
3.3 For each forcemain, ple	ase provide the following details	in the chart below (or equive	alont)	
Street	From (street/manhole)	To (street/manhole)	Diameter (mm)	Roughness
.4 (a) Is there an existing E	ECA for the pumping station asso	ciated with this forcemain?		
<ul> <li>8.4 (a) Is there an existing E</li> <li>Yes No</li> <li>If 'Yes', please provide t</li> <li>If 'No', please complete</li> <li>(b) Please provide the puincluded with this sub</li> <li>Yes No</li> <li>S If this system is not a grident of the provide the provide the provide the provided with this sub</li> </ul>	ECA for the pumping station associate the Certificate of Approval Numbe 8.4(b) Imping station design elements by mission? Inder pump system, is the minimu	ciated with this forcemain? r: y completing Tables 1, 2, an m pipe size at least 100 mm	d 3 in Appendix C. Have to allow for the passage n the pipe	Tables 1, 2, and 3 been of small solids?
<ul> <li>4 (a) Is there an existing E</li> <li>Yes No</li> <li>If 'Yes', please provide t</li> <li>If 'No', please complete</li> <li>(b) Please provide the puincluded with this sub</li> <li>Yes No</li> <li>S If this system is not a grident of the s</li></ul>	ECA for the pumping station associate the Certificate of Approval Numbe 8.4(b) unping station design elements by mission? Inder pump system, is the minimu elow which methods will be emplo	ciated with this forcemain? r: y completing Tables 1, 2, an m pipe size at least 100 mm byed to prevent a blockage in Dosed works?	d 3 in Appendix C. Have to allow for the passage n the pipe	Tables 1, 2, and 3 been of small solids?
<ul> <li>a.4 (a) Is there an existing E</li> <li>Yes No</li> <li>If 'Yes', please provide t</li> <li>If 'No', please complete</li> <li>(b) Please provide the puincluded with this sub</li> <li>Yes No</li> <li>S If this system is not a grident of the provide t</li></ul>	ECA for the pumping station associate the Certificate of Approval Number 8.4(b) imping station design elements by mission? nder pump system, is the minimu elow which methods will be employ ange for all forcemains in the prop to	ciated with this forcemain? r: y completing Tables 1, 2, an m pipe size at least 100 mm byed to prevent a blockage in boosed works?	d 3 in Appendix C. Have	Tables 1, 2, and 3 been of small solids?
<ul> <li>3.4 (a) Is there an existing E</li> <li>Yes No</li> <li>If 'Yes', please provide t</li> <li>If 'No', please complete</li> <li>(b) Please provide the puincluded with this sub</li> <li>Yes No</li> <li>S If this system is not a grident of the provide the provide the provide the provide the provided with this sub</li> <li>Yes No</li> <li>If this system is not a grident of the provided the provided with this sub</li> <li>Yes No</li> <li>If 'No', please indicate be</li> <li>6 (a) What is the velocity rates of the provided the provided the provided with this sub</li> <li>If the velocity falls out of the provided the provided the provided the provided with the provided th</li></ul>	ECA for the pumping station associate of Approval Number 8.4(b) umping station design elements by mission? Inder pump system, is the minimute elow which methods will be emploted ange for all forcemains in the proprotect to	ciated with this forcemain? r:	d 3 in Appendix C. Have to allow for the passage n the pipe m/s e employed to reduce sev	Tables 1, 2, and 3 been of small solids? /age build up and/or
<ul> <li>3.4 (a) Is there an existing E</li> <li>Yes No</li> <li>If 'Yes', please provide t</li> <li>If 'No', please complete</li> <li>(b) Please provide the puincluded with this sub</li> <li>Yes No</li> <li>S If this system is not a grident of the system o</li></ul>	ECA for the pumping station associated for the pumping station associated for the certificate of Approval Number 8.4(b) amping station design elements by mission? The minimulation of the methods will be emplored for all forcemains in the property to the transient been considered?	ciated with this forcemain? r:	d 3 in Appendix C. Have to allow for the passage n the pipe m/s e employed to reduce sew	Tables 1, 2, and 3 been of small solids? /age build up and/or
<ul> <li>4 (a) Is there an existing E</li> <li>Yes No</li> <li>If 'Yes', please provide t</li> <li>If 'No', please complete</li> <li>(b) Please provide the puincluded with this sub</li> <li>Yes No</li> <li>If this system is not a grident of the system of the system is not a grident of the system of the system is not a grident of the system of the system</li></ul>	ECA for the pumping station associated for the pumping station associated for the certificate of Approval Number 8.4(b) supping station design elements by mission? Inder pump system, is the minimulation of the methods will be employed angle for all forcemains in the property to to the range of 0.8 m/s to 2.4 still be and the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 still be angle for the range of 0.8 m/s to 2.4 sti	ciated with this forcemain? r:	d 3 in Appendix C. Have to allow for the passage n the pipe m/s e employed to reduce sev	Tables 1, 2, and 3 been of small solids? /age build up and/or

	in fir in an	aunic Desig	n sheet													
Site local	tion (City)	D							<u> </u>				0	recking Da	ate (yyyy/mi	m/dd)
Ref#							Review	/er	_							
Design S	torm: The		Year Sto	Im Event			_									
Rational I Where: ( E: A	Formula: Q 2: peak flov 2: runoff co 7: rainfall int 4: area (ha)	= 2.78*CIA v (L/s) efficient ensity (mm/ł	Ē		Concentrati Where: ti: ir tf: t tf =	on time: tc ilet time be ime of flow L/(60V) (m	= ti + tf (mir fore pipe (m in pipe (mir inute)	nute) iinute) nute)	ж а с с с с с с	anning Equ cap. = (D/1 pipe size ( slope (grad roughness	Jation: 000)^2.667 <sup>∞</sup> (mm) de) of pipe ( coefficient	'(S/100)^0. %)	5/(3.211*n)*	1000 (L/s)		
						Runoff							Pipe			
street lame	From (MH/CB)	To (MH/CB)	Area (A) (ha)	Runoff Coefficient (C)	Section (AC) (ha)	Accum. (AC) (ha)	Concentra tion time (tc) (min.)	Rainfall Intensity (I) (mm/ hr)	Peak Flow (Q) (L/s)	Length (L) (m)	Slope (S) (%)	N. D. (D) (mm)	Qcap. (full) (L/s)	V (full) (m/s)	Time of flow in pipe (min ) (ff)	(Q) /Qcap
		-														

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Ref#									<u> </u>	н			<u> </u>	Checking D	ate (yyy/m	(pp/m
							Revier	ver								
Residential	Unit average	le daily fl	:(b) wo			cap.d (225	~450 L/cap	.d) Unit	extraneous	flow (E):				L/s/ha	(0.1-0.281	(et s
q = average I = Unit of pr Q(p) = peak Q(l) = peak Q(d) = peak	daily per ca eak extranei population extraneous design flow	apita flov eous flow flow (L/s flow (L/s / (L/s)	v (L/cap.d) (L/s/ha) )		Peaking F <sub>i</sub> M =1+14/( Q(p) = (P/1 Q(l) =IA (L Q(d) = Q(p	actor: 4+(P/1000)^ 000)qM/86. (s); where A ) + Q(l) (L/s	0.5) 4 (L/s) = Area in ł	iectares	Ξ ἀ ̈́̈́̈́́ ̈́́́́́́́́́́́́́́́́́́́́́́́́́́́	anning Equ cap. = (D/1( pipe size ( slope (grac roughness	lation: 200)^22.667 mm) fe) of pipe coefficient	**(S/100)^0. (%)	.5/(3.211*n)	*1000 (L/s)		
						Inlet	Flow						۵.	ipe		
Ĺ	ocation		Indiv	vidual	Accun	Julative	Peaking	Pop.	Extran.	Design	Length	Size	Slope	Capacity	Velocity	
Street F <sub>I</sub> Name (N	rom Tc AH) (M	(HI	P (person)	) Area (ha)	P (person)	Area (ha)	Factor (M)	Q(p) (L/s)	Q(e) (L/s)	Q(d) (L/s)	r (m)	D (mm)	S (%)	Qcap. (L/s)	V (m/s)	Q(d)/Qcap

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## Table 1 (H-1 of APPENDIX H)

## Sewage Pumping Station Design – Table 1 Municipality

## Pumping Station

Designed by

Designed by						Date (yyyy/mm/dd)
Desigr	n Subject	Unit	Initial Period	10 Year Period	20 Year Period	Ultimate Period
	A) Residential	ha				
Tributary	B) Commercial	ha				
	C) Industrial	ha				
Population	Density	Pers/ha				
	A) Residential	No.				
Population or Equivalent	B) Commercial	No.				
	C) Industrial	No.				
Per Cap	ita Flow	L/cap.d				
Average	Flow	L/s				
Peak Flor	w Factor*					
Peak Dome	estic Flow	L/s				
Infiltration	Rate	L/ha.s				
Infiltration	Flow	L/s				
Design Pea	ak Flow	L/s				
Pump	os	No.				
Pump Dis	scharge	L/s				
Force Main	Diameter	mm				
Veloc	ity	m/s				

Note: \* The peak flow factor is: 1+14/(4+P^0.5), where P is designed population, in thousand.

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## Table 2 (H-2 of APPENDIX H)

## Sewage Pumping Station Design – Table 2

Municipality

## **Pumping Station**

Designed by

Date (yyyy/mm/dd) **Design Subject** Unit C=120 C=130 C=140 Pump Design Flow L/s Forcemain Diam. mm Velocity m/s Forcemain Length m Forcemain Head Loss m Suction Line Head Loss m **Discharge Line Head Loss** m **Total Head Loss** m Low Water Level Wet Well m High Water Level Wet Well m Forcemain End Elevation m Static Head Max. m Static Head Min. m Total Danamic Head Max. m Total Danamic Head Min. m
Table 3 (Abstracted from Appendix I)	
Information Required for Sewage Pumping Stations Applications	
Standby Power Supply	
Is standby power required?	
If yes, what kind of standby power is available for this pumping station?	
a) Standby Generator b) Portable Generator c) Additional hydro feed line	
Receiving Watercourse	
Will sewage be overflow/bypass any receiving watercourse?	
Yes No	
If yes, then:	
a) It will be necessary to know in detail the route by which overflow/bypass flow would gain access to the watercourse?	
b) The flow in the receiving watercourse at the point of overflow/bypass from the pumping station is as follows:	
flow in dry weather (m <sup>3</sup> /s)	
flow in wet weather (m <sup>3</sup> /s)	
c) The nearest water intake is located on the receiving watercourse within	
metres of the point of entry of the overflow.	
Sewage Pumping Station	
a) The operating authority responsible for maintenance and operation of this pumping station is	
b) The high level alarm is set up to relay a signal to	
b) Between the time of activation of the high level alarm and the overflow/basement flooding, there are:	
m <sup>3</sup> of storage capacity available in the sewers;	
m <sup>3</sup> of storage capacity available in the pumping station.	
I) This storage will provide:	
minutes retention before overflow/basement flooding occurs at the average daily design flow of	L/or
ind minutes retention before overflow/basement flooding occurs at the peak design flow of	L/S,
) It is possible to bypass or pump around the pumping station with portable equipment by utilizing the following procedure	L/S;