



## Site Servicing Report & Stormwater Management Study

The Hindu Heritage Center of Ottawa-Carleton  
4835 Bank Street  
Ottawa, Ontario K1X 1G6

Prepared for:

The Hindu Heritage Center of Ottawa-Carleton  
c/o Lloyd Philips & Associates Ltd.  
1827 Woodward Drive, Suite 109  
Ottawa, Ontario K2C 0P9

Attention: Mr. Harish Gupta

## EXECUTIVE SUMMARY

LRL Associates Ltd. has been mandated by Harish Gupta, of the Hindu Heritage Centre, to prepare a Site Servicing Report and SWM Study for the new assembly hall development at the Hindu Heritage Center of Ottawa-Carleton located at 4835 Bank Street, Ottawa, Ontario.

The analysis concluded that the 1/5 and 1/100-year post-development runoff discharge can be controlled to the 1/5-year pre-development levels or less. We also demonstrated that an enhanced water quality protection level of 80% TSS removal can be achieved for the controlled runoff using a Stormwater Treatment Unit (Jellyfish Filter) prior to discharging stormwater into the existing watercourse.

Furthermore, the proposed water distribution network will be adequate to service the new assembly hall building. The maximum hourly demand is calculated at 8.18 L/s, and the corresponding minimum residual pressure is 61.14 psi. The maximum day demand including total fire flow (for both proposed and existing building) is 174.18 L/s, and the resulting residual minimum pressure is 24.73 psi.

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## 1 INTRODUCTION

LRL Associates Ltd. has been mandated by Lloyd Philips & Associates Ltd. to prepare a Site Servicing Report and Stormwater Management Study for the development of a new assembly hall at the Hindu Heritage Center of Ottawa-Carleton, located at 4835 Bank Street, Ottawa, Ontario. The property is legally described as Part of Lot 22, Concession 5 (Rideau Front), Geographic Township of Gloucester, City of Ottawa. The Key Plan for the proposed site has been included in Appendix A.

The subject property is rectangular in shape, with a frontage of 101.92 m and depth of 401.53 m. The property's total surface area is 4.06 ha. The West portion of the site is currently composed of an existing single storey temple (combined gross floor area of 1062 m<sup>2</sup>, with basement) with landscaped area bordering its North, West and South ends. An existing asphalt parking lot is located adjacent to the East end of the temple. An asphalt roadway (Temple Road) follows the South property line below the landscape area & existing temple, providing access to the existing parking lot. At roughly the center of the property lies an existing creek, running South to North. All property located East of the creek is wooded area.

The proposed addition, the assembly hall, will be a single-story building (with full basement). The proposed development will have a total gross main floor area of approximately 1400 m<sup>2</sup>. The assembly hall will be located East of the existing temple and parking lot, and West of the creek.

Currently, the existing building is serviced by a 150 mmØ water service running West to East along Temple Road. In order to provide water to the proposed development, the service will need to be extended roughly 131m Easterly. The new water service will be designed in order to supply the new domestic and fire flow building demands, as well as the proposed fire hydrant.

As there are no sanitary sewer located along Bank Street, the proposed building will have to be serviced by a septic system. The proposed septic system will be located directly South of the proposed assembly hall. It will be designed to suit the new building sanitary needs as per the Ontario Building Code - Part 8. The Ottawa Septic System Office (OSSO) will be issuing the permit for the new septic system.

As per the City of Ottawa's requirements, all storm runoff will be controlled to pre-development levels for a 5-year storm event. All surplus runoff will be conveyed to, and controlled in a detention area before being treated and discharged to the existing water course. Stormwater quality control will meet the 80% minimum TSS removal requirements, as per the South Nation Conservation Authority (SNCA) requirements.

This report has been prepared in consideration of the terms and conditions noted above. Should there be any changes in the design features, which may relate to the water or sanitary considerations, LRL Associates Ltd. should be advised in order to review the report's recommendations.

## 2 FIELDWORK

The topographic survey of the property was conducted on April 27<sup>th</sup>, 2017 by Annis, Sullivan Vollebeckk Ltd. (Ontario Land Surveyors). A site benchmark was established during the survey for future construction use. The benchmark provided is the top of spindle (elevation 100.17 m) of the existing fire hydrant found between the existing temple and existing access roadway, at the South-West corner of the existing parking lot.

## 3 STORMWATER MANAGEMENT

### 3.1 Existing Stormwater Conditions

In pre-development conditions, all stormwater flows off-site uncontrolled.

The site follows a few overland flow patterns, which will be broken down below.

First, there is the front (West) section of the property, which encompasses the existing Hindu Temple, and surrounding North, West and South landscape. The site was graded down from the Temple building, so naturally, stormwater will flow from the temple to the nearest property line. Stormwater in the North and West landscape areas will flow North / North-West / West to the respective property lines. Stormwater south of the building will flow to the South, and captured & conveyed East by the existing ditch (running along the North end of the existing asphalt driveway)

The second section of the property, the rear (East) end, encompasses the existing parking lot, and surrounding North, East and South landscape. The existing parking lot was developed with a high point running along the center (West to East), with a slight slope towards the East. All stormwater on the North end of the parking lot is conveyed North-West to the North property line. All stormwater on the South end of the parking lot is conveyed South / South-West to the South property line. All stormwater accumulated at the rear end of the property would continue to flow East, until ultimately should reach the existing creek.

The final section of the property is the driveway running along the South property line. All stormwater from this asphalt surface will be conveyed North / North-east to the ditch running along the driveways North end.

Please refer to civil plan C701 – Pre-Development Watershed Plan for greater detail.

### 3.2 Proposed Post-development Watersheds

For stormwater management design purposes, the site was divided into four watershed areas;

WS-01 – Existing building, grass area, ditch & driveway South of the existing building, South existing parking lot & proposed ditch, proposed building and grass area & detention area South of the proposed building

WS-02 – North section of the existing parking lot, including North grass area

WS-03 – Grass area North and South of the existing Temple

WS-04 – Grass area at the South-East corner of the property

The watershed delineations can be seen in Civil Plan C702 – Post-development Watershed Plan.

As per the EIS (Environmental Impact Statement) developed for this site, we could not perform any works, or include any stormwater management structures, within a 20m setback from the existing creek. This 20m setback was delineated as the East boundary of our scope of work.

Watershed 01 is proposed as a control area, where stormwater will be controlled and treated prior to being released at the 20m setback line (and ultimately flowing overland to the existing creek).

Watershed 02 is proposed as an uncontrolled area, where stormwater will flow off the site uncontrolled, as it did in previous conditions. Though no means of flow control will be implemented here, the stormwater in this area will be collected and treated prior to being released.

Watersheds 03 and 04 are proposed as uncontrolled areas. No flow control or treatment are proposed for these areas, stormwater will flow off the site uncontrolled, as it did in previous conditions. As large majority of these watersheds are landscaped/grassed areas, additional treatment isn't an absolute necessity.

### 3.3 Design Criteria

The stormwater management criteria for this development are based on pre-consultation with City of Ottawa officials (which occurred on June 5<sup>th</sup>, 2019), the City of Ottawa Sewer Design Guidelines including City of Ottawa Stormwater Management Design Guidelines, 2012 (City standards), as well as the Ministry of the Environment's Stormwater Management Planning and Design Manual, 2003 (SWMPD Manual).

As discussed during the pre-consultation meeting, all storm events up to and including the 100-year event would be controlled to the 5-year pre-development level, using a smaller of a runoff coefficient (C) of 0.5 or the actual site C, and time of concentration of 10 minutes. The runoff generated from the existing site was calculated using the Rational Method, as follows:

$$Q = 2.78 \times C \times I \times A$$

Where,

*C = the runoff coefficient (C = 0.47)*

*I = the rainfall intensity (mm/hr) (I<sub>5</sub> = 104.2 mm/hr at a T<sub>c</sub> = 10 min)*

*A = Area (2.117 ha)*

$$Q_{\text{allowable 1/5yr (pre-dev)}} = 2.78 \times 0.47 \times 104.2 \text{ mm/hr} \times 2.117 \text{ ha} = 288.68 \text{ L/s}$$

As per the watershed delineation provided in section 3.2, in the 100-year storm event, the maximum uncontrolled runoff was calculated to be 249.13 L/s. With an allowable release rate of 288.68 L/s, this would leave us to have to control the balance of the site to a controlled release rate of 39.55 L/s.

## 4 QUANTITY CONTROL

The area at the South of proposed building is large enough to accommodate a substantial detention area. This proposed detention area, equipped with an inlet control device (ICD) at the outlet, would serve as a primary means of flow control for all controlled stormwater on-site.

To achieve the aforementioned, it was determined that the release rate would have to be controlled to approximately 39.50 L/s for the 100yr storm event, and 28.00 L/s for the 5yr storm

event. The release rate will be controlled by installing an ICD in the outlet maintenance hole (MH01) whereas the excess runoff will be conveyed to and stored in the proposed detention area, upstream of MH01. Please refer to Appendix C for greater details regarding the proposed ICD.

The maximum storage volumes required to contain the 5- and 100-year post-development storm events were calculated to be **177.42 m<sup>3</sup>** and **424.74 m<sup>3</sup>**, respectively. For storage volume calculations, the controlled release rate was taken as half of the discharge rate.

The detailed storage calculations can be found in Appendix N.

All controlled overland flow will be conveyed to the proposed detention area, located near the South-East corner of the proposed assembly hall, by means of the existing grading, as well as the extension of the existing ditch (running West to East along the South property line). The excess runoff will ultimately be stored above ground in the proposed detention area. No ponding will occur on the existing landscaped area, parking lot or pathways during high-level storm events. However, during the 5- and 100-year storm events, some ponding will occur in ditch South-West of the detention area, due to the proposed grading of these elements. The Stormwater Management plan (Civil Plan C601), provided in Appendix F, demonstrates the extent of storage and high-water levels for both the 100- and 5-year storm events.

AutoCAD Civil 3D was used to determine the maximum storage volume and high-water level of the proposed detention area. A Cut/Fill table was generated by the program, which can be seen in Appendix D of the report. The maximum storage volume generated by Civil 3D (428.14 m<sup>3</sup>) was found to be greater than the required storage previously calculated (424.72 m<sup>3</sup>). Therefore, the detention area & ditch will be enough to retain the excess runoff generated by a 100-year major storm event.

## 5 STORM RUNOFF QUALITY REQUIREMENTS

As previously mentioned, the site will be developed so that the post-development controlled runoff will ultimately be discharged at the 20m setback line. As discussed in the pre-consultation meeting with the City of Ottawa, in order to meet the water quality objective, it is required to achieve an enhanced level of protection of 80% total suspended solid (TSS) removal. This can be achieved using a water quality treatment unit.

Considering the post-development watershed area that requires water quality treatment (1.316 ha), (as seen in Appendix B – Post-Development Watershed Plan), it is proposed to install an Jellyfish JF6-4-1 stormwater treatment unit (or approved equivalent). The Jellyfish JF6-4-1 will serve to remove a minimum 80% of the TSS while treating 90% off the annual runoff. Please refer to Appendix E for the selection, type and additional information on the treatment unit.

Stormwater treatment has also been proposed in Watershed WS-02 (consisting of the North half of the existing parking lot). Stormwater in this area will be conveyed to a catchbasin proposed at the North-East corner of the parking lot. The catchbasin will be equipped with a FlexStorm Pure inlet filer. The inlet filter will not provide the full 80% TSS removal, however, it will provide substantial treatment of runoff from the North parking lot. The treated flow from the catchbasin and inlet filter will then be conveyed to a proposed infiltration gallery.

Greater details for the inlet filter can be found in Appendix E and infiltration gallery can be found on Civil Plan C902.

## 6 LOW IMPACT DEVELOPMENT

As per the EIS performed for this site, the proposed development should occur with large focus towards Low Impact Development (LID).

At the rear of the property is located an existing creek. A 20m setback was proposed from the creek as a means of protecting the sensitive resource. This setback was respected in the stormwater management design for the site.

The initial design focused on maintaining as much of the existing grass area and landscape elements (trees) as possible. Any addition to the parking lot was offset by incorporating landscape within the parking lot. The roof drains will also lead flows to either the ditch or detention area, in order to maximize the potential for captured water infiltration.

All controlled runoff is ultimately being treated by the Jellyfish stormwater treatment unit (or approved equivalent). Prior to this, the stormwater will succumb to other means of stormwater treatment. The ditches are low-sloping, and equipped with a subdrain & clear stone, to promote filtration and infiltration. Ditch culvert inverts have been slightly raised at the inlets in order to promote additional ponding and infiltration. The proposed detention area spans a large area; this works increases ground infiltration and treatment of the detained stormwater. The detention area is low sloping, encouraging additional infiltration and decreasing sediment conveyance.

The uncontrolled runoff, specifically the runoff from the North half of the parking lot, will progress through two forms of treatment prior to being released. The stormwater will be captured by a catchbasin installed at the North-East end of the parking lot. The captured runoff will first be treated with a Flexstorm Pure inlet filter. This inlet filter will not provide the full 80% TSS removal, however, it will provide substantial treatment of runoff from the North parking lot, targeting contaminates such as trash, litter, leaves, smaller particles, oil and grease. This treated stormwater will then be conveyed to a proposed infiltration gallery. The infiltration gallery, equipped with a perforated subdrain and clear stone trench, will provide further treatment, and greatly encourage infiltration. The infiltration gallery was designed to retain a volume of stormwater from the first 5mm rainfall over the watershed WS-02. This translates to a storage volume of  $20.55\text{ m}^3$ .

In addition, additional landscaping elements will be incorporated to the site to improve site aesthetic. The detention area will serve to improve the open land use and site development aesthetic.

## 7 WATER SERVICE

### 7.1 Domestic Water Demand

The average domestic water demand, the maximum daily domestic water demand and the maximum hourly domestic water demand were calculated using the number of equivalent plumbing fixtures (as per the OBC) for the proposed new assembly hall building. The plumbing fixtures were determined based on the Architectural Drawings, as seen in Appendix G.

Table 1 included below demonstrates the type, quantity and equivalent number of fixtures units proposed in the new development.

**Table 1 - Number of Equivalent Plumbing Fixtures for Proposed Building**

Fixture Description	Quantity	Hydraulic Load (Public Use)	Fixture Units
Toilet	23	2.2	50.6
Sink	23	1.5	34.5
Shower	2	3	6
Mop service sink	2	2.25	4.5
Urinal	8	3	24
<b>Total</b>			<b>120</b>

The domestic water demand was determined based on the calculated total fixture units for the proposed building. To summarize, a total equivalent fixture unit count of 120 resulted in an average daily water demand of 3.03 L/s (261,648 L/day), a maximum daily demand of 4.54 L/s (392,471 L/day), and a maximum hourly demand of 8.18 L/s (706,448 L/day).

With reference to OBC Table 7.6.3.2.A, calculated total fixture unit for the existing building was calculated to be 55, resulting in an average daily water demand of 1.96 L/s (168,980 L/day), a maximum daily demand of 2.93 L/s (253,471 L/day), and a maximum hourly demand of 5.28 L/s (456,248 L/day).

Detailed calculations can be found in Appendix J.

A new watermain, with dual connection, was proposed on site to service both the existing building, new building, and fire hydrants. The water service connection to the new building was designed and sized to obtain a desired residual pressure range as per Section 4.2.2 of City of Ottawa Design Guidelines – Water Distribution. The new water service layout can be found in the Servicing Plan, included in Appendix H.

## 7.2 Fire Flow Requirements

The minimum fire flow rate required has been calculated using the Fire Underwriters Survey (FUS) method. The fire flow is derived from the proposed building surface area, the type of construction, the combustibility and the separation distances to other adjacent buildings.

Fire flow for both the existing and proposed buildings have been considered for the extent of this report.

The effective building area of the proposed assembly hall building is 1560 square meters, it is to be of non-combustible construction and sprinklered. The required fire flow rate was determined to be 4,000 L/min (66.7 L/s). The effective building area of the existing building on-site assembly hall building is 1062 square meters, of non-combustible construction, and non-sprinklered. The required fire flow rate was determined to be 6,000 L/min (100.0 L/s).

Detailed calculations can be found in Appendix L.

To ensure that the proposed watermain can supply the required fire flow via the proposed new fire hydrant on-site, additional hydraulic analysis have been performed using EPANET (Version 2.2). The modeling results show that the proposed water distribution network is able to meet the required fire flow while the residual pressure, at any point in the distribution network, is greater than 20 psi.

### 7.3 Boundary Conditions

The boundary conditions for this development were obtained from the City of Ottawa on June 16th<sup>th</sup>, 2022, based on the calculated water demands and fire flow. Two sets of boundary conditions were provided for the development: the first for the existing water distribution system and the second for the future SUC zone reconfiguration. Both have been considered for the purposes of this report.

The maximum and minimum water pressure provided for Bank Street for the existing water distribution system are 79.3 psi and 62.7 psi, respectively, and the pressure corresponding to the Max. Day + Fire is 37.4 psi.

The maximum and minimum water pressure provided for Bank Street for the SUC zone reconfiguration water distribution system are 71.2 psi and 65.0 psi, respectively, and the pressure corresponding to the Max. Day + Fire Flow is 59.0 psi.

Refer to Appendix M (City of Ottawa Boundary Conditions) and Appendix K (EPANET Modelling) for additional information.

### 7.4 Water Distribution Network Hydraulic Modeling

To decrease vulnerability of the water distribution system, the subject site is proposed to have two (2) service connections which will be looped inside the property line, refer to Site Servicing Plan C401 for a proposed layout. To study the behavior of the network and obtain operating pressure under different flow scenarios, the proposed network was modeled and analyzed using EPANET software (Version 2.2). The hydraulic model uses two supply reservoirs with HGL provided by City Boundary Conditions at different flow scenarios. The first connection is represented by Reservoir R1 and the second connection is represented by Reservoir R2 at Bank St. Six (6) different flow scenarios were analyzed. The summary of modeling results is summarized in Table 2 below and greater details can be found in Appendix K.

### 7.5 Expected Water Service Pressure

For Scenario 1, the anticipated average day demands are applied to node J14 for the proposed new building and node J16 for the existing building. The residual pressures calculated using EPANET hydraulic analysis are summarized in Table 2. The procedure is repeated for Scenario 2 (Peak Hour). For scenario 3, the calculated fire flow demands are applied to the fire hydrant connection nodes with maximum day domestic demand simultaneously applied to building service entry nodes. For modeling results including pipe pressure, refer to Appendix K.

According to City Guidelines-Water Distribution, the maximum pressure at any point in the distribution system shall not exceed 80 psi. However, for Scenario 1, the calculated pressures of 80.94 and 82.65 psi are greater than 80 psi, therefore a pressure reducing valve is required for both existing building and the proposed new building. Scenario 2 (Peak Hour) and Scenario 3 (Max Day+ Fire Flow) residual pressure exceeds required minimum of 40 and 20 psi respectively, thus appears acceptable.

**Table 2 - Summary of Residual Pressures (psi)**

Scenario	Existing Building		Proposed New Building	
	Existing Conditions	SUC Zone Reconfiguration	Existing Conditions	SUC Zone Reconfiguration
Scenario 1: Avg Day	80.94	72.83	82..65	74.55
Scenario 2: Peak Hour	61.14	63.41	65.81	68.08
Scenario 3: Max Day + Fire Flow	24.73	31.23	27.31	33.81

*Note: The residual pressures correspond to service entry nodes J14 (proposed new building) & J16 (existing building).*

## **8 SANITARY SERVICE**

Based on the existing plans and City of Ottawa resources (geoOttawa), it was apparent that there was no existing municipal sanitary sewer located along Bank Street. Therefore, the development of the new assembly hall will necessitate the design & installation of a new septic system.

The existing building, the Hindu Heritage Center Place of Worship, is currently serviced by two independent sewage systems (septic treatment system and leaching bed), hereby referred to as the north septic and south septic, each having been designed for a capacity of 3750 L/day, or 7500 L/day total. With the current site plan control application, sewage demand was reassessed at 3650 L/day, based on a max occupancy of 250 individuals. Due to the lowered required capacity of the existing building, it is proposed that the north septic be decommissioned, and the south septic system upgraded to become the consolidated septic for the entire Place of Worship. The upgraded septic is proposed to consist of an advanced sewage treatment system (pre-treatment tank, treatment unit, filter vault and shallow bury trench bed).

The proposed building, the Hindu Heritage Center Assembly Hall, due to the lack of municipal sanitary sewer and capacity with the Place of Worship septic system, will require its own independent septic system. The proposed septic system will be constructed on the South side of the proposed building, North of the proposed ditch. Based on the assumption that a maximum 500 individuals will occupy the building, the proposed building is expected to have a daily demand of 4000 L/day. Due to area constraints for the leaching bed, a tertiary septic treatment has been proposed for the Assembly Hall (consisting of a balancing tank, treatment unit and shallow bury trench bed).

The new septic systems have been designed under Part 8 (Sewage System) of the OBC.

Refer to the Site Servicing Plan in Appendix H for the proposed location of the new septic systems. Refer to Appendix P for the septic designs and OSSO approvals.

Greater detail can be found in with reference to the LRL Terrain Analysis and Private Sewage Disposal System Impact Assessment.

## **9 MAINTENANCE**

Monitoring and maintenance are an important component for all types of stormwater management practices. It ensures performance efficiency of the facilities and prevents undesirable consequences such as flooding or contamination to the neighboring properties.

The maintenance of the proposed stormwater treatment unit (Jellyfish Filter) would consist of inspecting the structure (inlet, outlet, cover etc.) on a periodic basis and cleaning them as deemed necessary. The structure should be cleaned (pumped) of its sediments and hydrocarbons content at least once a year, as per the manufacturer recommendations. It is the responsibility of the owner to maintain and clean the treatment unit and keep a log of all the maintenance activities.

## **10 SEDIMENT AND EROSION CONTROL**

Sediment and erosion control measures will be implemented before and during the construction of this project. Typical control measures such as silt fences and sediment straw bail fences are mandatory. For this project, a silt fence will be erected along the perimeter of the development area. A sediment straw bail fence will be constructed downstream of the proposed new ditch, upstream of the proposed detention area. In addition, a mud mat will be installed at the entrance of the proposed development unit. Refer to drawing C101 – Erosion and Sediment Control Plan (Appendix I) for additional details.

## **11 CONCLUSIONS**

The analysis concluded that the 5- and 100-year post-development runoff discharge can be controlled to the 5-year pre-development level. We also demonstrated that an enhanced water quality protection level (80% TSS removal) can be achieved with a stormwater treatment unit prior to discharging controlled treated stormwater into the existing watercourse.

Furthermore, the proposed water distribution network will be adequate to service the new assembly hall building, as well as existing building and fire hydrants.

The sanitary servicing will consist of the construction of a new septic system.

## 12 REPORT CONDITIONS AND LIMITATIONS

The report conclusions are applicable only to this specific project described in the preceding pages. Any changes, modifications or additions will require a subsequent review by LRL Associates Ltd. to ensure the compatibility with the recommendations contained in this document.

If you have any questions or comments, please contact the undersigned.

Yours truly,  
**LRL Associates Ltd.**



Prepared by:

*Kyle Herold*



Approved by:

*M. Basnet, P. Eng.*

## **APPENDIX A**

### **Key Plan**



PROJECT

PROPOSED ASSEMBLY HALL  
4835 BANK STREET, OTTAWA

**LRJ**

ENGINEERING | INGÉNIERIE

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DRAWING TITLE

KEY PLAN

CLIENT

THE HINDU HERITAGE CENTRE OF OTTAWA-CARLETON

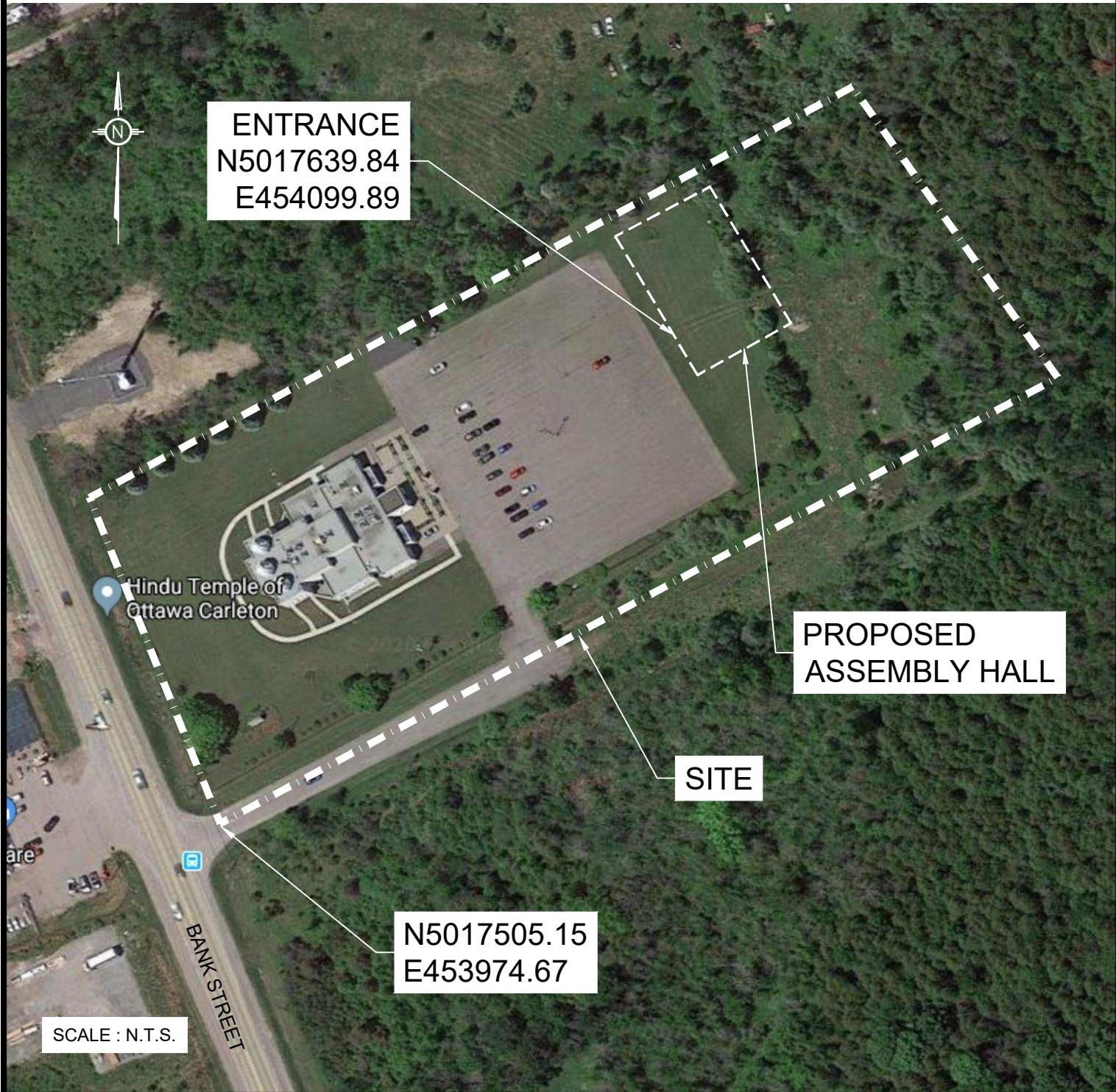
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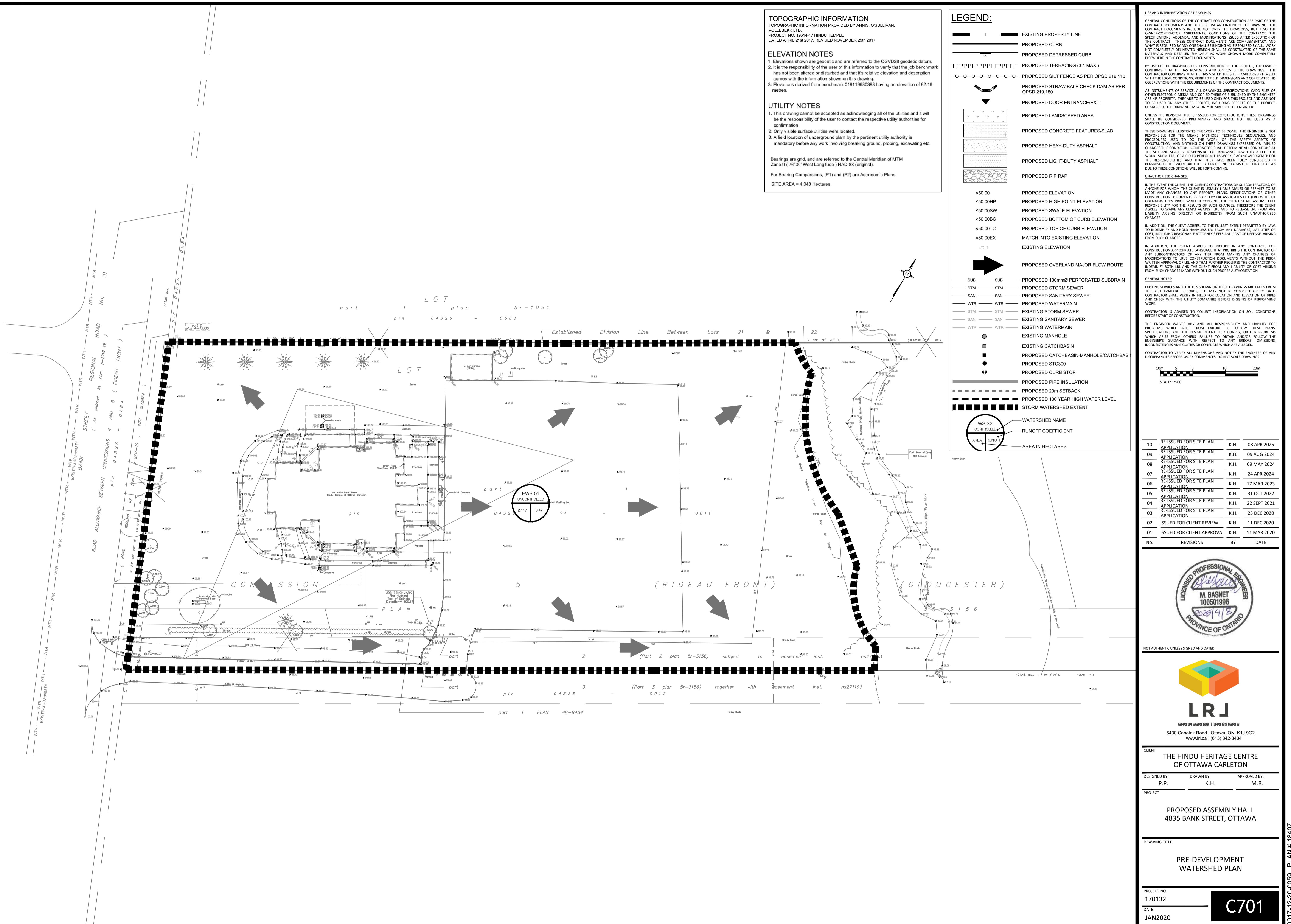
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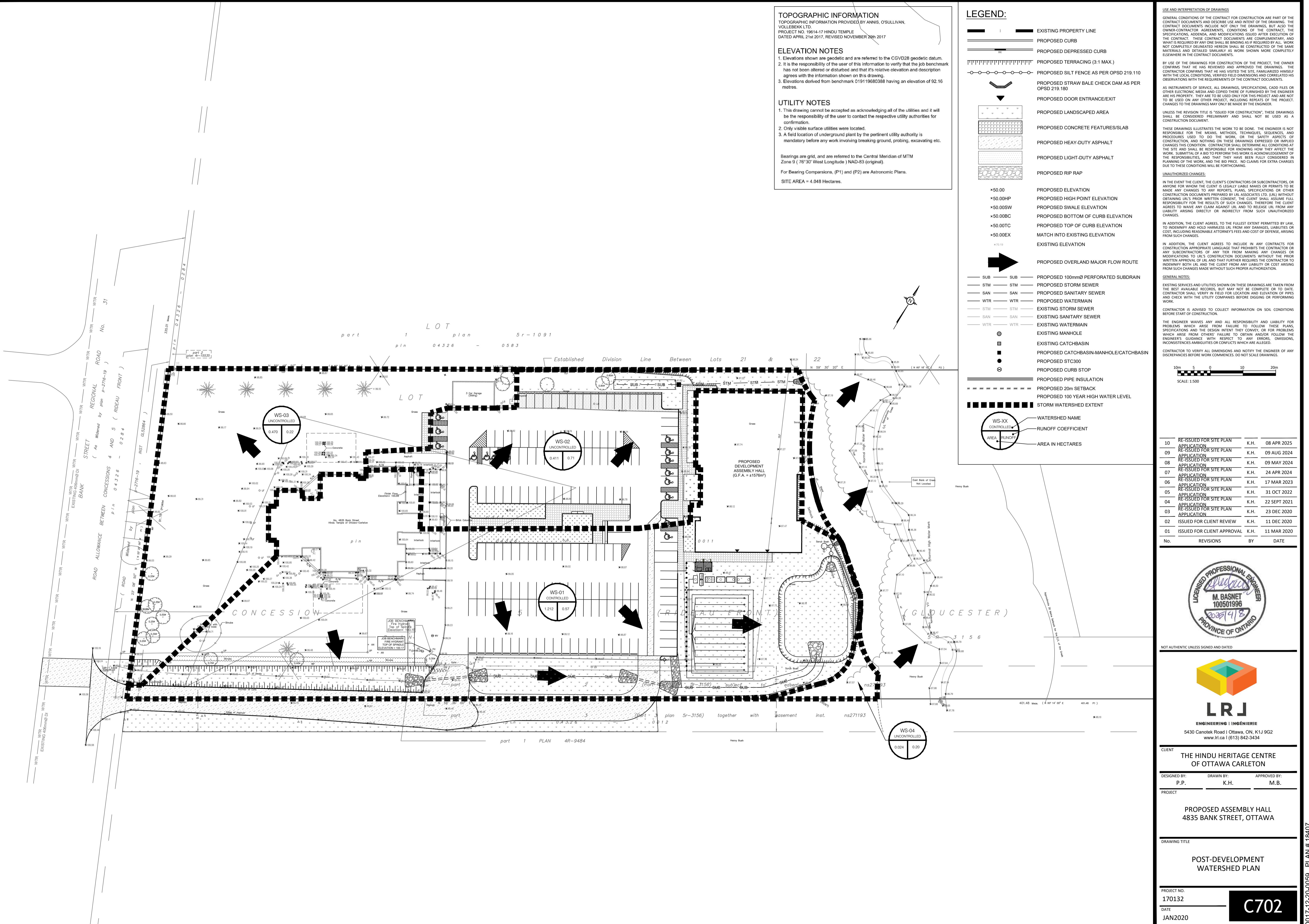
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KP



**APPENDIX B**  
**Pre & Post Watershed Plans**





**APPENDIX C**  
**Flow Restrictor Information**



**LRL File No.** 170132-10  
**Project:** Hindu Heritage Center  
**Location:** 4835 Bank Street, Ottawa  
**Date:** 08-Apr-25  
**Designed:** K. Herold  
**Checked:** M. Basnet  
**Drawing Ref.:** C.401

**Stormwater Management**  
**Design Sheet**

### Orifice Equation

$$Q = 0.61 * A * \sqrt{2 * g * H}$$

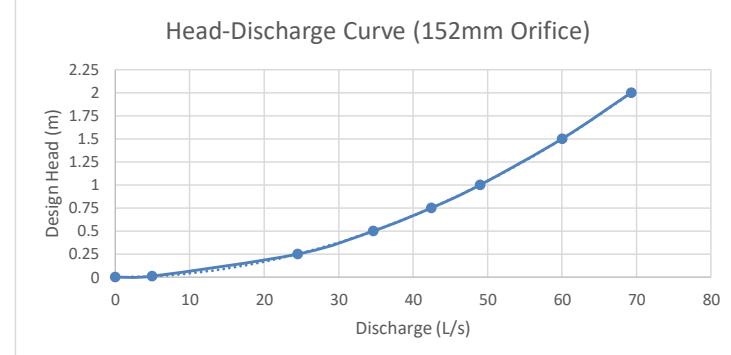
Where;  $Q$  = release rate (in m<sup>3</sup>/s)  
 0.61 = coefficient  
 $A$  = area of the orifice (m<sup>2</sup>)  
 $g$  = gravitational constant (9.81 m/s<sup>2</sup>)  
 $H$  = head (above CL of orifice (m))

### ICD Diameter (based on 100yr design reqt's)

$Q$ (m <sup>3</sup> /s) =	0.0395
$g$ (9.81m/s <sup>2</sup> ) =	9.81
$H$ (m) =	0.65

$A$ (m <sup>2</sup> ) =	0.01813
$D$ (m) =	0.152

Orifice Diameter Required = **152** mm



### Storm - 100 year

Allowable Release Rate = 316.44L/s  
 Controlled Release Rate = 39.50L/s

$Q$ (m <sup>3</sup> /s) =	0.0395
$g$ (9.81m/s <sup>2</sup> ) =	9.81
$A$ (m <sup>2</sup> ) =	0.01813

$H$ (m) =	0.65
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100yr STM Design Head = **0.65** m

### Inlet Control Device Parameters

#### ICD at MH01

##### **Product Orifice Plate**

Design Head =	0.65m
Max. Pond Depth =	0.82m (100y)
100y High Water Level =	98.47
5y High Water Level =	98.15
Outlet Pipe & ICD Inv =	97.72
ICD Dia =	152mm
ICD Head above CL Orifice Inv =	97.80

### Storm - 5 year

Allowable Release Rate = 316.44L/s  
 Controlled Release Rate = 28.00L/s

$Q$ (m <sup>3</sup> /s) =	0.028
$g$ (9.81m/s <sup>2</sup> ) =	9.81
$A$ (m <sup>2</sup> ) =	0.01813

$H$ (m) =	0.33
-----------	------

5yr STM Design Head = **0.33** m

**APPENDIX D**  
**Volume Table Generated by AutoCAD Civil 3D**

# Cut/Fill Report

**Generated:** 2022-10-31 09:11:55

**By user:** KHerold

**Drawing:** W:\FILES 2017\170132\06 CivilDesign\02 Drawings\07  
FinalProductionDrawings\W:\FILES 2017\170132\06 CivilDesign\02  
Drawings\07 FinalProductionDrawings\170132-05.dwg

Volume Summary 5yr							
Name	Type	Cut Factor	Fill Factor	2d Area (hectares)	Cut (Cu. M.)	Fill (Cu. M.)	Net (Cu. M.)
VOL DITCH WEST	full	0.00	1.00	0.05	0.00*	0.00	0.00*
VOL DET AREA	full	0.00	1.00	0.06	0.00*	210.79	210.79*
VOL DITCH EAST	full	0.00	1.00	0.02	0.00*	0.13	0.13*

Totals				
		2d Area (hectares)	Cut (Cu. M.)	Fill (Cu. M.)
Total		0.14	0.00*	210.92
				210.92*

\* Value adjusted by cut or fill factor other than 1.0

# Cut/Fill Report

**Generated:** 2022-10-31 09:15:12

**By user:** KHerold

**Drawing:** W:\FILES 2017\170132\06 CivilDesign\02 Drawings\07  
FinalProductionDrawings\W:\FILES 2017\170132\06 CivilDesign\02  
Drawings\07 FinalProductionDrawings\170132-05.dwg

Volume Summary 100yr							
Name	Type	Cut Factor	Fill Factor	2d Area (hectares)	Cut (Cu. M.)	Fill (Cu. M.)	Net (Cu. M.)
VOL DITCH WEST	full	0.00	1.00	0.05	0.00*	7.85	7.85*
VOL DET AREA	full	0.00	1.00	0.06	0.00*	396.35	396.35*
VOL DITCH EAST	full	0.00	1.00	0.02	0.00*	23.94	23.94*

Totals				
		2d Area (hectares)	Cut (Cu. M.)	Fill (Cu. M.)
Total		0.14	0.00*	428.14
				428.14*

\* Value adjusted by cut or fill factor other than 1.0

**APPENDIX E**  
**Stormwater Treatment Devices**

# DRAWING NOT TO BE USED FOR CONSTRUCTION

## GENERAL NOTES:

1. ALL DIMENSIONS INDICATED ARE IN MILLIMETERS (INCHES) UNLESS OTHERWISE SPECIFIED.
2. JELLYFISH STRUCTURE INLET AND OUTLET PIPE SIZE AND ORIENTATION SHOWN FOR INFORMATIONAL PURPOSES ONLY.
3. UNLESS OTHERWISE NOTED, BYPASS INFRASTRUCTURE, SUCH AS ALL UPSTREAM DIVERSION STRUCTURES, CONNECTING STRUCTURES, OR PIPE CONDUITS CONNECTING TO COMPLETE THE JELLYFISH SYSTEM SHALL BE PROVIDED AND ADDRESSED SEPARATELY.
4. DRAWING FOR INFORMATION PURPOSES ONLY. REFER TO ENGINEER'S SITE/UTILITY PLAN FOR STRUCTURE ORIENTATION.
5. NO PRODUCT SUBSTITUTIONS SHALL BE ACCEPTED UNLESS SUBMITTED 10 DAYS PRIOR TO PROJECTS BID DATE, OR AS DIRECTED BY THE ENGINEER OF RECORD.

## JELLYFISH STRUCTURE & DESIGN NOTES:

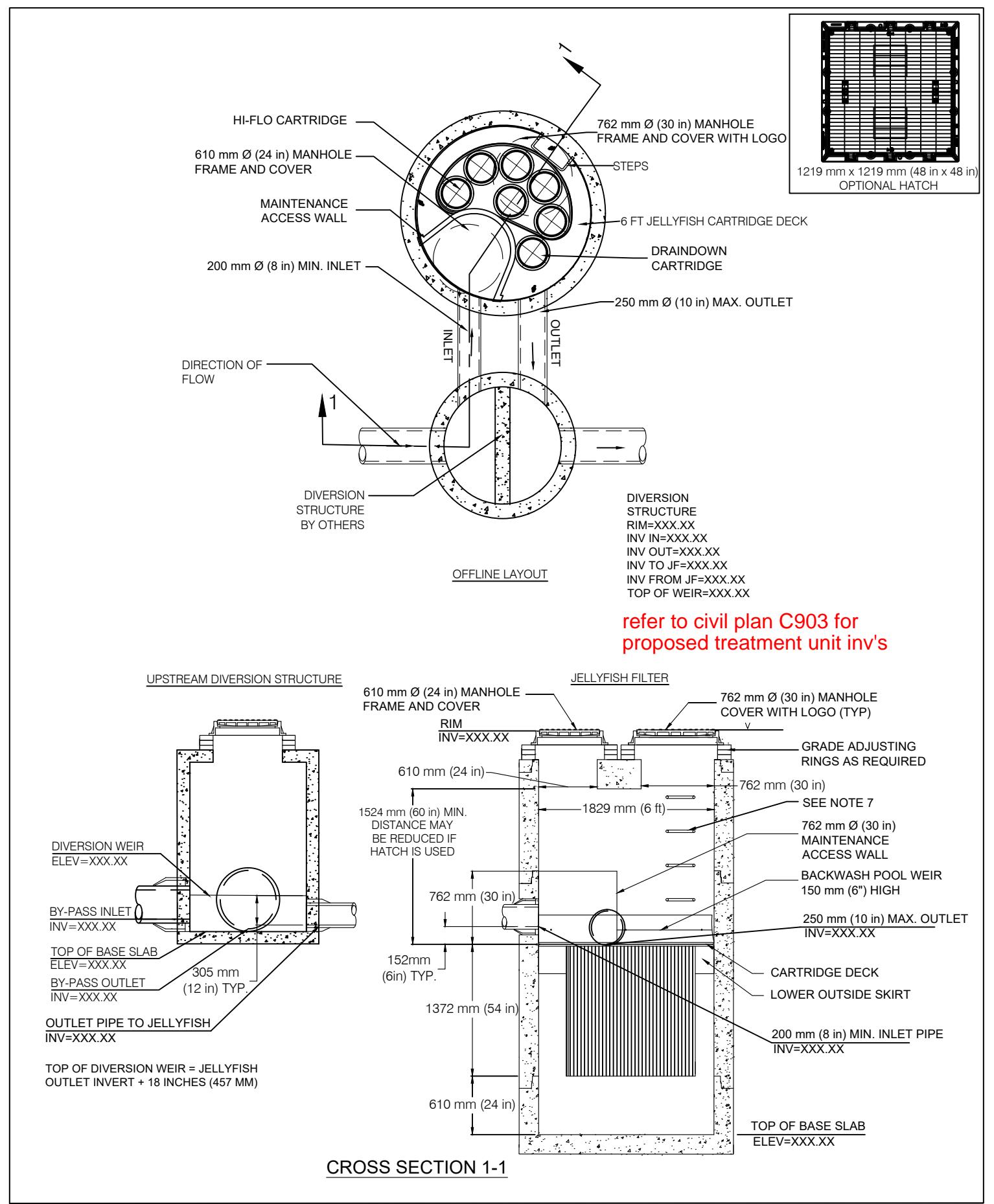
1. 762 MM Ø (30") MAINTENANCE ACCESS WALL TO BE USED FOR CLEANOUT AND ACCESS BELOW CARTRIDGE DECK.
2. CASTINGS OR DOORS OF THE JELLYFISH MANHOLE STRUCTURE TO EXTEND TO DESIGN FINISH GRADE. DEPTHS IN EXCESS OF 3.65 M (12') MAY REQUIRE THE DESIGN AND INSTALLATION OF INTERMEDIATE SAFETY GRATES OR OTHER STRUCTURAL ELEMENTS.
3. CASTINGS AND GRADE RINGS, OR DOORS AND DOOR RISERS, OR BOTH, SHALL BE GROUTED FOR WATERTIGHTNESS. STRUCTURE SHALL MEET AASHTO HS-20, ASSUMING EARTH COVER OF 0' - 3', AND GROUNDWATER ELEVATION AT, OR BELOW, THE OUTLET PIPE INVERT ELEVATION. ENGINEER OF RECORD TO CONFIRM ACTUAL GROUNDWATER ELEVATION. CASTINGS SHALL MEET AASHTO M306 LOAD RATING AND BE CAST WITH THE IMBRIUM LOGO.
4. ALL STRUCTURAL SECTIONS AND PARTS TO MEET OR EXCEED ASTM C-478, ASTM C-443, AND ASTM D-4097 CORRESPONDING TO AASHTO SPECIFICATIONS, AND ANY OTHER SITE OR LOCAL STANDARDS.
5. CONCRETE RISER SECTIONS FROM BOTTOM TO TOP WILL BE ADDED AS REQUIRED INCLUDING TRANSITION PIECES TO SMALLER DIAMETER RISERS FOR SURFACE ACCESSES WHERE WARRANTED BY SERVICING DEPTH.
6. IF MINIMUM DEPTH FROM TOP OF CARTRIDGE DECK TO BOTTOM OF STRUCTURAL TOP SLAB CANNOT BE ACHIEVED DUE TO PIPING INVERT ELEVATIONS OR OTHER SITE CONSTRAINTS. ALTERNATIVE HATCH CONFIGURATIONS MAY BE AVAILABLE. HATCH DOORS SHOULD BE SIZED TO PROVIDE FULL ACCESS ABOVE THE CARTRIDGES TO ACCOMMODATE MAINTENANCE.
7. STEPS TO BE APPROXIMATELY 330 MM (13") APART AND DIMENSIONS MUST MEET LOCAL STANDARDS. STEPS MUST BE INSTALLED AFTER CARTRIDGE DECK IS IN PLACE.
8. CONFIGURATION OF INLET AND OUTLET PIPE CAN VARY TO MEET SITE'S NEEDS.
9. IT IS THE RESPONSIBILITY OF OTHERS TO PROPERLY PROTECT THE TREATMENT DEVICE, AND KEEP THE DEVICE OFFLINE DURING CONSTRUCTION. FILTER CARTRIDGES SHALL NOT BE INSTALLED UNTIL THE PROJECT SITE IS CLEAN AND FREE OF DEBRIS, BY OTHERS. THE PROJECT SITE INCLUDES ANY SURFACE THAT CONTRIBUTES STORM DRAINAGE TO THE TREATMENT DEVICE. CARTRIDGES SHALL BE FURNISHED NEW, AT THE TIME OF FINAL ACCEPTANCE.
10. THIS DRAWING MUST BE VIEWED IN CONJUNCTION WITH THE STANDARD JELLYFISH SPECIFICATION, AND STORMWATER QUALITY FILTER TREATMENT JELLYFISH DOCUMENTS.

## INSTALLATION NOTES

- A. ANY SUB-BASE, BACKFILL DEPTH, AND/OR ANTI-FLOTATION PROVISIONS ARE SITE-SPECIFIC DESIGN CONSIDERATIONS AND SHALL BE SPECIFIED BY ENGINEER OF RECORD.
- B. CONTRACTOR TO PROVIDE EQUIPMENT WITH SUFFICIENT LIFTING AND REACH CAPACITY TO LIFT AND SET THE STRUCTURE (LIFTING CLUTCHES PROVIDED).
- C. CONTRACTOR WILL INSTALL AND LEVEL THE STRUCTURE, SEALING THE JOINTS, LINE ENTRY AND EXIT POINTS (NON-SHRINK GROUT WITH APPROVED WATERSTOP OR FLEXIBLE BOOT).
- D. CONTRACTOR TO TAKE APPROPRIATE MEASURES TO PROTECT CARTRIDGES FROM CONSTRUCTION-RELATED EROSION RUNOFF.
- E. CARTRIDGE INSTALLATION, BY IMBRIUM, SHALL OCCUR ONLY AFTER SITE HAS BEEN STABILIZED AND THE JELLYFISH UNIT IS CLEAN AND FREE OF DEBRIS. CONTACT IMBRIUM TO COORDINATE CARTRIDGE INSTALLATION WITH SITE STABILIZATION.

STANDARD OFFLINE JELLYFISH RECOMMENDED PIPE DIAMETERS				
MODEL DIAMETER (m)	MINIMUM ANGLE INLET/OUTLET PIPES	MINIMUM INLET PIPE DIAMETER (mm)	MINIMUM OUTLET PIPE DIAMETER (mm)	
1.2	62	150	200	
1.8	59	200	250	
2.4	52	250	300	
3.0	48	300	450	
3.6	40	300	450	
CONTACT IMBRIUM SYSTEMS FOR ALTERNATE PIPE DIAMETERS				

FOR SITE SPECIFIC DRAWINGS PLEASE CONTACT YOUR LOCAL JELLYFISH FILTER REPRESENTATIVE. SITE SPECIFIC DRAWINGS ARE BASED ON THE BEST AVAILABLE INFORMATION AT THE TIME. SOME FIELD REVISIONS TO THE SYSTEM LOCATION OR CONNECTION PIPING MAY BE NECESSARY BASED ON AVAILABLE SPACE OR SITE CONFIGURATION REVISIONS. ELEVATIONS SHOULD BE MAINTAINED EXCEPT WHERE NOTED ON BYPASS STRUCTURE.



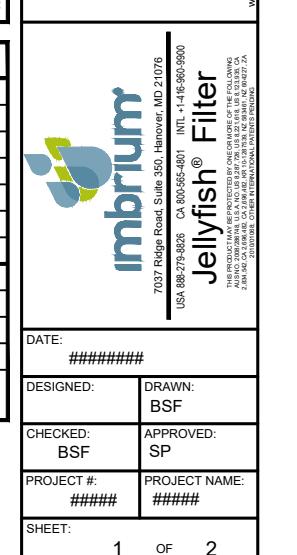
refer to civil plan C903 for proposed treatment unit inv's

## JELLYFISH DESIGN NOTES

JELLYFISH TREATMENT CAPACITY IS A FUNCTION OF THE CARTRIDGE SELECTION AND THE NUMBER OF CARTRIDGES. THE STANDARD MANHOLE STYLE IS SHOWN. Ø1829 mm (72") MANHOLE JELLYFISH PEAK TREATMENT CAPACITY IS 32.8 L/s (1.16 CFS). TREATMENT FLOW RATE IS BASED ON 457 MM (18") OF HEAD PRESSURE.	
CARTRIDGE SELECTION	
CARTRIDGE DEPTH	54"
OUTLET INVERT TO STRUCTURE BASE SLAB	90"
FLOW RATE HIGH-FLO / DRAINDOWN (L/s) (per cart)	5.09 / 2.55
SEDIMENT CAPACITY HIGH-FLO / DRAINDOWN (kg) (per cart)	57 / 28
MAX. CARTS HIGH-FLO/DRAINDOWN	370
MAX. SEDIMENT CAPACITY (kg)	32.8
MAX. TREATMENT (L/s)	

SITE SPECIFIC DATA REQUIREMENTS	
JELLYFISH MODEL	*
STRUCTURE ID	*
WATER QUALITY FLOW RATE (L/s)	*
PEAK FLOW RATE (L/s)	*
RETURN PERIOD OF PEAK FLOW (yrs)	*
# OF CARTRIDGES REQUIRED (HF / DD)	*
CARTRIDGE SIZE (inches)	*
PIPE DATA: I.E.	*
INLET #1	*
INLET #2	*
OUTLET	*

\* PER ENGINEER OF RECORD



**Jellyfish**

JF6 STANDARD

Scale = 1:50

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# STANDARD OFFLINE Jellyfish Filter Sizing Report

## Project Information

Date	Tuesday, November 24, 2020
Project Name	Hindu Heritage Center
Project Number	
Location	Ottawa

## Jellyfish Filter Design Overview

This report provides information for the sizing and specification of the Jellyfish Filter. When designed properly in accordance to the guidelines detailed in the Jellyfish Filter Technical Manual, the Jellyfish Filter will exceed the performance and longevity of conventional horizontal bed and granular media filters.

*Please see [www.ImbriumSystems.com](http://www.ImbriumSystems.com) for more information.*

## Jellyfish Filter System Recommendation

The Jellyfish Filter model JF6-4-1 is recommended to meet the water quality objective by treating a flow of 22.7 L/s, which meets or exceeds 90% of the average annual rainfall runoff volume based on 36 years of OTTAWA MACDONALD-CARTIER INT'L A rainfall data for this site. This model has a sediment capacity of 256 kg, which meets or exceeds the estimated average annual sediment load.

Jellyfish Model	Number of High-Flo Cartridges	Number of Draindown Cartridges	Manhole Diameter (m)	Treatment Flow Rate (L/s)	Sediment Capacity (kg)
JF6-4-1	4	1	1.8	22.7	256

## The Jellyfish Filter System

The patented Jellyfish Filter is an engineered stormwater quality treatment technology featuring unique membrane filtration in a compact stand-alone treatment system that removes a high level and wide variety of stormwater pollutants. Exceptional pollutant removal is achieved at high treatment flow rates with minimal head loss and low maintenance costs. Each lightweight Jellyfish Filter cartridge contains an extraordinarily large amount of membrane surface area, resulting in superior flow capacity and pollutant removal capacity.

## Maintenance

Regular scheduled inspections and maintenance is necessary to assure proper functioning of the Jellyfish Filter. The maintenance interval is designed to be a minimum of 12 months, but this will vary depending on site loading conditions and upstream pretreatment measures. Quarterly inspections and inspections after all storms beyond the 5-year event are recommended until enough historical performance data has been logged to comfortably initiate an alternative inspection interval.

*Please see [www.ImbriumSystems.com](http://www.ImbriumSystems.com) for more information.*

Thank you for the opportunity to present this information to you and your client.

# Jellyfish® Filter

## Performance

Jellyfish efficiently captures a high level of Stormwater pollutants, including:

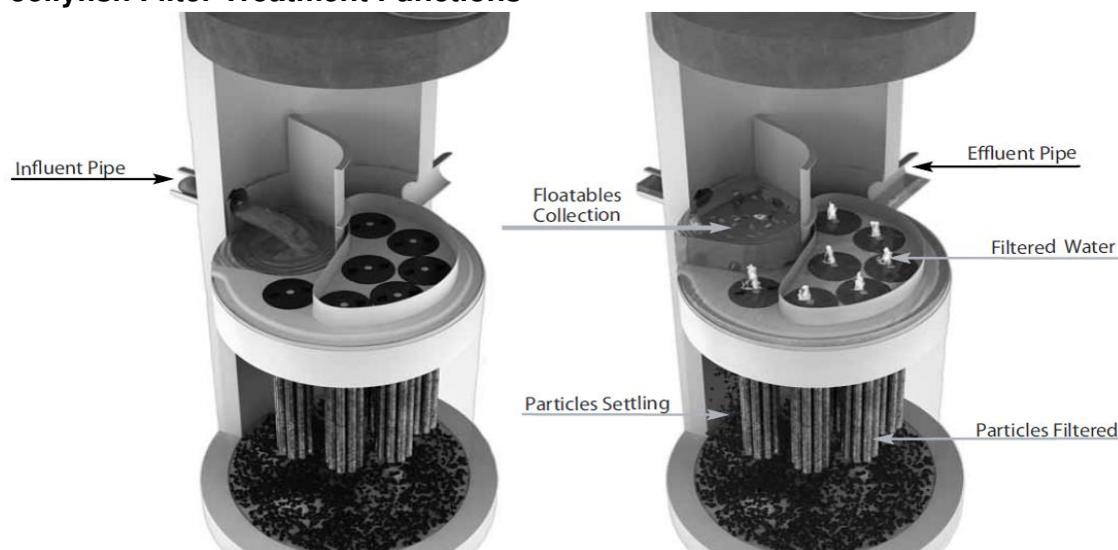
- 89% of the total suspended solids (TSS) load, including particles less than 5 microns
- 59% TP removal & 51% TN removal
- 90% Total Copper, 81% Total Lead, 70% Total Zinc
- Particulate-bound pollutants such as nutrients, toxic metals, hydrocarbons and bacteria
- Free oil, Floatable trash and debris

## Field Proven Performance

The Jellyfish filter has been field-tested on an urban site with 25 TARP qualifying rain events and field monitored according to the TARP field test protocol, demonstrating:

- A median TSS removal efficiency of 89%, and a median SSC removal of 99%;
- The ability to capture fine particles as indicated by an effluent d50 median of 3 microns for all monitored storm events, and a median effluent turbidity of 5 NTUs;
- A median Total Phosphorus removal of 59%, and a median Total Nitrogen removal of 51%.

## Jellyfish Filter Treatment Functions



*Pre-treatment and Membrane Filtration*

## Project Information

Date:	Tuesday, November 24, 2020
Project Name:	Hindu Heritage Center
Project Number:	
Location:	Ottawa

## Designer Information

Company:	LRL Associates Ltd.
Contact:	Kyle Herold
Phone #:	

## Notes

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## Design System Requirements

<b>Flow Loading</b>	90% of the Average Annual Runoff based on 36 years of OTTAWA MACDONALD-CARTIER INT'L A rainfall	<b>17.5 L/s</b>
<b>Sediment Loading</b>	Treating 90% of the average annual runoff volume, 3541 m <sup>3</sup> , with a suspended sediment concentration of 60 mg/L.	<b>212 kg*</b>

\* Indicates that sediment loading is the limiting parameter in the sizing of this Jellyfish system

## Recommendation

The Jellyfish Filter model JF6-4-1 is recommended to meet the water quality objective by treating a flow of 22.7 L/s, which meets or exceeds 90% of the average annual rainfall runoff volume based on 36 years of OTTAWA MACDONALD-CARTIER INT'L A rainfall data for this site. This model has a sediment capacity of 256 kg, which meets or exceeds the estimated average annual sediment load.

Jellyfish Model	Number of High-Flo Cartridges	Number of Draindown Cartridges	Manhole Diameter (m)	Wet Vol Below Deck (L)	Sump Storage (m <sup>3</sup> )	Oil Capacity (L)	Treatment Flow Rate (L/s)	Sediment Capacity (kg)
JF4-1-1	1	1	1.2	2313	0.34	379	7.6	85
JF4-2-1	2	1	1.2	2313	0.34	379	12.6	142
JF6-3-1	3	1	1.8	5205	0.79	848	17.7	199
<b>JF6-4-1</b>	<b>4</b>	<b>1</b>	<b>1.8</b>	<b>5205</b>	<b>0.79</b>	<b>848</b>	<b>22.7</b>	<b>256</b>
JF6-5-1	5	1	1.8	5205	0.79	848	27.8	313
JF6-6-1	6	1	1.8	5205	0.79	848	28.6	370
JF8-6-2	6	2	2.4	9252	1.42	1469	35.3	398
JF8-7-2	7	2	2.4	9252	1.42	1469	40.4	455
JF8-8-2	8	2	2.4	9252	1.42	1469	45.4	512
JF8-9-2	9	2	2.4	9252	1.42	1469	50.5	569
JF8-10-2	10	2	2.4	9252	1.42	1469	50.5	626
JF10-11-3	11	3	3.0	14456	2.21	2302	63.1	711
JF10-12-3	12	3	3.0	14456	2.21	2302	68.2	768
JF10-12-4	12	4	3.0	14456	2.21	2302	70.7	796
JF10-13-4	13	4	3.0	14456	2.21	2302	75.7	853
JF10-14-4	14	4	3.0	14456	2.21	2302	78.9	910
JF10-15-4	15	4	3.0	14456	2.21	2302	78.9	967
JF10-16-4	16	4	3.0	14456	2.21	2302	78.9	1024
JF10-17-4	17	4	3.0	14456	2.21	2302	78.9	1081
JF10-18-4	18	4	3.0	14456	2.21	2302	78.9	1138
JF10-19-4	19	4	3.0	14456	2.21	2302	78.9	1195
JF12-20-5	20	5	3.6	20820	3.2	2771	113.6	1280
JF12-21-5	21	5	3.6	20820	3.2	2771	113.7	1337
JF12-22-5	22	5	3.6	20820	3.2	2771	113.7	1394
JF12-23-5	23	5	3.6	20820	3.2	2771	113.7	1451
JF12-24-5	24	5	3.6	20820	3.2	2771	113.7	1508
JF12-25-5	25	5	3.6	20820	3.2	2771	113.7	1565
JF12-26-5	26	5	3.6	20820	3.2	2771	113.7	1622
JF12-27-5	27	5	3.6	20820	3.2	2771	113.7	1679

## Rainfall

Name:	OTTAWA MACDONALD-CARTIER INT'L A
State:	ON
ID:	6000
Record:	1967 to 2003
Co-ords:	45°19'N, 75°40'W

## Drainage Area

Total Area:	1.316 ha
Runoff Coefficient:	0.59

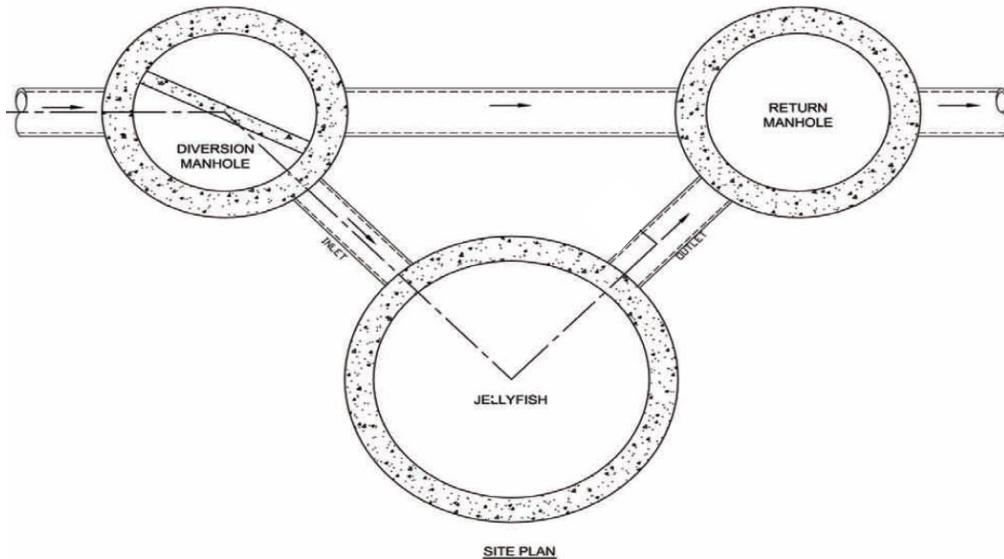
## Upstream Detention

Peak Release Rate:	n/a
Pretreatment Credit:	n/a

# Jellyfish® Filter

## Jellyfish Filter Design Notes

- Typically the Jellyfish Filter is designed in an offline configuration, as all stormwater filter systems will perform for a longer duration between required maintenance services when designed and applied in off-line configurations. Depending on the design parameters, an optional internal bypass may be incorporated into the Jellyfish Filter, however note the inspection and maintenance frequency should be expected to increase above that of an off-line system. Speak to your local representative for more information.



*Jellyfish Filter Typical Layout*

- Typically, 18 inches (457 mm) of driving head is designed into the system, calculated as the difference in elevation between the top of the diversion structure weir and the invert of the Jellyfish Filter outlet pipe. Alternative driving head values can be designed as 12 to 24 inches (305 to 610mm) depending on specific site requirements, requiring additional sizing and design assistance.
- Typically, the Jellyfish Filter is designed with the inlet pipe configured 6 inches (150 mm) above the outlet invert elevation. However, depending on site parameters this can vary to an optional configuration of the inlet pipe entering the unit below the outlet invert elevation.
- The Jellyfish Filter can accommodate multiple inlet pipes within certain restrictions.
- While the optional inlet below deck configuration offers 0 to 360 degree flexibility between the inlet and outlet pipe, typical systems conform to the following:

Model Diameter (m)	Minimum Angle Inlet / Outlet Pipes	Minimum Inlet Pipe Diameter (mm)	Minimum Outlet Pipe Diameter (mm)
1.2	62°	150	200
<b>1.8</b>	<b>59°</b>	<b>200</b>	<b>250</b>
2.4	52°	250	300
3.0	48°	300	450
3.6	40°	300	450

- The Jellyfish Filter can be built at all depths of cover generally associated with conventional stormwater conveyance systems. For sites that require minimal depth of cover for the stormwater infrastructure, the Jellyfish Filter can be applied in a shallow application using a hatch cover. The general minimum depth of cover is 36 inches (915 mm) from top of the underslab to outlet invert.
- If driving head calculations account for water elevation during submerged conditions the Jellyfish Filter will function effectively under submerged conditions.
- Jellyfish Filter systems may incorporate grated inlets depending on system configuration.
- For sites with water quality treatment flow rates or mass loadings that exceed the design flow rate of the largest standard Jellyfish Filter manhole models, systems can be designed that hydraulically connect multiple Jellyfish Filters in series or alternatively Jellyfish Vault units can be designed.

# STANDARD SPECIFICATION STORMWATER QUALITY – MEMBRANE FILTRATION TREATMENT DEVICE

## PART 1 – GENERAL

### 1.1 WORK INCLUDED

Specifies requirements for construction and performance of an underground stormwater quality membrane filtration treatment device that removes pollutants from stormwater runoff through the unit operations of sedimentation, floatation, and membrane filtration.

### 1.2 REFERENCE STANDARDS

ASTM C 891: Specification for Installation of Underground Precast Concrete Utility Structures

ASTM C 478: Specification for Precast Reinforced Concrete Manhole Sections

ASTM C 443: Specification for Joints for Concrete Pipe and Manholes, Using Rubber Gaskets

ASTM D 4101: Specification for Copolymer steps construction

#### CAN/CSA-A257.4-M92

Joints for Circular Concrete Sewer and Culvert Pipe, Manhole Sections and Fittings Using Rubber Gaskets

#### CAN/CSA-A257.4-M92

Precast Reinforced Circular Concrete Manhole Sections, Catch Basins and Fittings

Canadian Highway Bridge Design Code

### 1.3 SHOP DRAWINGS

Shop drawings for the structure and performance are to be submitted with each order to the contractor. Contractor shall forward shop drawing submittal to the consulting engineer for approval. Shop drawings are to detail the structure's precast concrete and call out or note the fiberglass (FRP) internals/components.

### 1.4 PRODUCT SUBSTITUTIONS

No product substitutions shall be accepted unless submitted 10 days prior to project bid date, or as directed by the engineer of record. Submissions for substitutions require review and approval by the Engineer of Record, for hydraulic performance, impact to project designs, equivalent treatment performance, and any required project plan and report (hydrology/hydraulic, water quality, stormwater pollution) modifications that would be required by the approving jurisdictions/agencies. Contractor to coordinate with the Engineer of Record any applicable modifications to the project estimates of cost, bonding amount determinations, plan check fees for changes to approved documents, and/or any other regulatory requirements resulting from the product substitution.

### 1.5 HANDLING AND STORAGE

Prevent damage to materials during storage and handling.

## PART 2 – PRODUCTS

Imbrium Systems  
[www.imbriumsystems.com](http://www.imbriumsystems.com)

Ph 888-279-8826  
Ph 416-960-9900

## 2.1 GENERAL

2.1.1 The device shall be a cylindrical or rectangular, all concrete structure (including risers), constructed from precast concrete riser and slab components or monolithic precast structure(s), installed to conform to ASTM C 891 and to any required state highway, municipal or local specifications; whichever is more stringent. The device shall be watertight.

2.1.2 **Cartridge Deck** The cylindrical concrete device shall include a fiberglass deck. The rectangular concrete device shall include a coated aluminum deck. In either instance, the insert shall be bolted and sealed watertight inside the precast concrete chamber. The deck shall serve as: (a) a horizontal divider between the lower treatment zone and the upper treated effluent zone; (b) a deck for attachment of filter cartridges such that the membrane filter elements of each cartridge extend into the lower treatment zone; (c) a platform for maintenance workers to service the filter cartridges (maximum manned weight = 450 pounds (204 kg)); (d) a conduit for conveyance of treated water to the effluent pipe.

2.1.3 **Membrane Filter Cartridges** Filter cartridges shall be comprised of reusable cylindrical membrane filter elements connected to a perforated head plate. The number of membrane filter elements per cartridge shall be a minimum of eleven 2.75-inch (70-mm) diameter elements. The length of each filter element shall be a minimum 15 inches (381 mm). Each cartridge shall be fitted into the cartridge deck by insertion into a cartridge receptacle that is permanently mounted into the cartridge deck. Each cartridge shall be secured by a cartridge lid that is threaded onto the receptacle, or similar mechanism to secure the cartridge into the deck. The maximum treatment flow rate of a filter cartridge shall be controlled by an orifice in the cartridge lid, or on the individual cartridge itself, and based on a design flux rate (surface loading rate) determined by the maximum treatment flow rate per unit of filtration membrane surface area. The maximum design flux rate shall be 0.21 gpm/ft<sup>2</sup> (0.142 lps/m<sup>2</sup>).

Each membrane filter cartridge shall allow for manual installation and removal. Each filter cartridge shall have filtration membrane surface area and dry installation weight as follows (if length of filter cartridge is between those listed below, the surface area and weight shall be proportionate to the next length shorter and next length longer as shown below):

Filter Cartridge Length (in / mm)	Minimum Filtration Membrane Surface Area (ft <sup>2</sup> / m <sup>2</sup> )	Maximum Filter Cartridge Dry Weight (lbs / kg)
15	106 / 9.8	10.5 / 4.8
27	190 / 17.7	15.0 / 6.8
40	282 / 26.2	20.5 / 9.3
54	381 / 35.4	25.5 / 11.6

2.1.4 **Backwashing Cartridges** The filter device shall have a weir extending above the cartridge deck, or other mechanism, that encloses the high flow rate filter cartridges when placed in their respective cartridge receptacles within the cartridge deck. The weir, or other mechanism, shall collect a pool of filtered water during inflow events that backwashes the high flow rate cartridges when the inflow

event subsides. All filter cartridges and membranes shall be reusable and allow for the use of filtration membrane rinsing procedures to restore flow capacity and sediment capacity; extending cartridge service life.

- 2.1.5 **Maintenance Access to Captured Pollutants** The filter device shall contain an opening(s) that provides maintenance access for removal of accumulated floatable pollutants and sediment, removal of and replacement of filter cartridges, cleaning of the sump, and rinsing of the deck. Access shall have a minimum clear vertical clear space over all of the filter cartridges. Filter cartridges shall be able to be lifted straight vertically out of the receptacles and deck for the entire length of the cartridge.
- 2.1.6 **Bend Structure** The device shall be able to be used as a bend structure with minimum angles between inlet and outlet pipes of 90-degrees or less in the stormwater conveyance system.
- 2.1.7 **Double-Wall Containment of Hydrocarbons** The cylindrical precast concrete device shall provide double-wall containment for hydrocarbon spill capture by a combined means of an inner wall of fiberglass, to a minimum depth of 12 inches (305 mm) below the cartridge deck, and the precast vessel wall.
- 2.1.8 **Baffle** The filter device shall provide a baffle that extends from the underside of the cartridge deck to a minimum length equal to the length of the membrane filter elements. The baffle shall serve to protect the membrane filter elements from contamination by floatables and coarse sediment. The baffle shall be flexible and continuous in cylindrical configurations, and shall be a straight concrete or aluminum wall in rectangular configurations.
- 2.1.9 **Sump** The device shall include a minimum 24 inches (610 mm) of sump below the bottom of the cartridges for sediment accumulation, unless otherwise specified by the design engineer. Depths less than 24 inches may have an impact on the total performance and/or longevity between cartridge maintenance/replacement of the device.

## 2.2 PRECAST CONCRETE SECTIONS

All precast concrete components shall be manufactured to a minimum live load of HS-20 truck loading or greater based on local regulatory specifications, unless otherwise modified or specified by the design engineer, and shall be watertight.

2.3 **JOINTS** All precast concrete manhole configuration joints shall use nitrile rubber gaskets and shall meet the requirements of ASTM C443, Specification C1619, Class D or engineer approved equal to ensure oil resistance. Mastic sealants or butyl tape are not an acceptable alternative.

2.4 **GASKETS** Only profile neoprene or nitrile rubber gaskets in accordance to CSA A257.3-M92 will be accepted. Mastic sealants, butyl tape or Conseal CS-101 are not acceptable gasket materials.

2.5 **FRAME AND COVER** Frame and covers must be manufactured from cast-iron or other composite material tested to withstand H-20 or greater design loads, and as approved by the

local regulatory body. Frames and covers must be embossed with the name of the device manufacturer or the device brand name.

- 2.6 DOORS AND HATCHES If provided shall meet designated loading requirements or at a minimum for incidental vehicular traffic.
- 2.7 CONCRETE All concrete components shall be manufactured according to local specifications and shall meet the requirements of ASTM C 478.
- 2.8 FIBERGLASS The fiberglass portion of the filter device shall be constructed in accordance with the following standard: ASTM D-4097: Contact Molded Glass Fiber Reinforced Chemical Resistant Tanks.
- 2.9 STEPS Steps shall be constructed according to ASTM D4101 of copolymer polypropylene, and be driven into preformed or pre-drilled holes after the concrete has cured, installed to conform to applicable sections of state, provincial and municipal building codes, highway, municipal or local specifications for the construction of such devices.
- 2.10 INSPECTION All precast concrete sections shall be inspected to ensure that dimensions, appearance and quality of the product meet local municipal specifications and ASTM C 478.

### PART 3 – PERFORMANCE

#### 3.1 GENERAL

- 3.1.1 Verification – The stormwater quality filter must be verified in accordance with ISO 14034:2016 Environmental management – Environmental technology verification (ETV).
- 3.1.2 Function - The stormwater quality filter treatment device shall function to remove pollutants by the following unit treatment processes; sedimentation, floatation, and membrane filtration.
- 3.1.3 Pollutants - The stormwater quality filter treatment device shall remove oil, debris, trash, coarse and fine particulates, particulate-bound pollutants, metals and nutrients from stormwater during runoff events.
- 3.1.4 Bypass - The stormwater quality filter treatment device shall typically utilize an external bypass to divert excessive flows. Internal bypass systems shall be equipped with a floatables baffle, and must avoid passage through the sump and/or cartridge filtration zone.
- 3.1.5 Treatment Flux Rate (Surface Loading Rate) – The stormwater quality filter treatment device shall treat 100% of the required water quality treatment flow based on a maximum design treatment flux rate (surface loading rate) across the membrane filter cartridges of 0.21 gpm/ft<sup>2</sup> (0.142 lps/m<sup>2</sup>).

### 3.2 FIELD TEST PERFORMANCE

At a minimum, the stormwater quality filter device shall have been field tested and verified with a minimum 25 TARP qualifying storm events and field monitoring shall have been conducted according to the TARP 2009 NJDEP TARP field test protocol, and have received NJCAT verification.

- 3.2.1 Suspended Solids Removal - The stormwater quality filter treatment device shall have demonstrated a minimum median TSS removal efficiency of 85% and a minimum median SSC removal efficiency of 95%.
- 3.2.2 Runoff Volume – The stormwater quality filter treatment device shall be engineered, designed, and sized to treat a minimum of 90 percent of the annual runoff volume determined from use of a minimum 15-year rainfall data set.
- 3.2.3 Fine Particle Removal - The stormwater quality filter treatment device shall have demonstrated the ability to capture fine particles as indicated by a minimum median removal efficiency of 75% for the particle fraction less than 25 microns, an effluent  $d_{50}$  of 15 microns or lower for all monitored storm events.
- 3.2.4 Turbidity Reduction - The stormwater quality filter treatment device shall have demonstrated the ability to reduce the turbidity from influent from a range of 5 to 171 NTU to an effluent turbidity of 15 NTU or lower.
- 3.2.5 Nutrient (Total Phosphorus & Total Nitrogen) Removal - The stormwater quality filter treatment device shall have demonstrated a minimum median Total Phosphorus removal of 55%, and a minimum median Total Nitrogen removal of 50%.
- 3.2.6 Metals (Total Zinc & Total Copper) Removal - The stormwater quality filter treatment device shall have demonstrated a minimum median Total Zinc removal of 55%, and a minimum median Total Copper removal of 85%.

### 3.3 INSPECTION and MAINTENANCE

The stormwater quality filter device shall have the following features:

- 3.3.1 Durability of membranes are subject to good handling practices during inspection and maintenance (removal, rinsing, and reinsertion) events, and site specific conditions that may have heavier or lighter loading onto the cartridges, and pollutant variability that may impact the membrane structural integrity. Membrane maintenance and replacement shall be in accordance with manufacturer's recommendations.
- 3.3.2 Inspection which includes trash and floatables collection, sediment depth determination, and visible determination of backwash pool depth shall be easily conducted from grade (outside the structure).
- 3.3.3 Manual rinsing of the reusable filter cartridges shall promote restoration of the flow capacity and sediment capacity of the filter cartridges, extending cartridge service life.

- 3.3.4 The filter device shall have a minimum 12 inches (305 mm) of sediment storage depth, and a minimum of 12 inches between the top of the sediment storage and bottom of the filter cartridge tentacles, unless otherwise specified by the design engineer. Variances may have an impact on the total performance and/or longevity between cartridge maintenance/replacement of the device.
- 3.3.5 Sediment removal from the filter treatment device shall be able to be conducted using a standard maintenance truck and vacuum apparatus, and a minimum one point of entry to the sump that is unobstructed by filter cartridges.
- 3.3.6 Maintenance access shall have a minimum clear height that provides suitable vertical clear space over all of the filter cartridges. Filter cartridges shall be able to be lifted straight vertically out of the receptacles and deck for the entire length of the cartridge.
- 3.3.7 Filter cartridges shall be able to be maintained without the requirement of additional lifting equipment.

## PART 4 – EXECUTION

### 4.1 INSTALLATION

#### 4.1.1 PRECAST DEVICE CONSTRUCTION SEQUENCE

The installation of a watertight precast concrete device should conform to ASTM C 891 and to any state highway, municipal or local specifications for the construction of manholes, whichever is more stringent. Selected sections of a general specification that are applicable are summarized below.

- 4.1.1.1 The watertight precast concrete device is installed in sections in the following sequence:
  - aggregate base
  - base slab
  - treatment chamber and cartridge deck riser section(s)
  - bypass section
  - connect inlet and outlet pipes
  - concrete riser section(s) and/or transition slab (if required)
  - maintenance riser section(s) (if required)
  - frame and access cover
- 4.1.2 The precast base should be placed level at the specified grade. The entire base should be in contact with the underlying compacted granular material. Subsequent sections, complete with joint seals, should be installed in accordance with the precast concrete manufacturer's recommendations.
- 4.1.3 Adjustment of the stormwater quality treatment device can be performed by lifting the upper sections free of the excavated area, re-leveling the base, and re-installing the sections. Damaged sections and gaskets should be repaired or replaced as necessary to restore original condition and watertight seals. Once the stormwater quality treatment device has been constructed, any/all lift holes must be plugged watertight with mortar or non-shrink grout.

4.1.4 Inlet and Outlet Pipes Inlet and outlet pipes should be securely set into the device using approved pipe seals (flexible boot connections, where applicable) so that the structure is watertight, and such that any pipe intrusion into the device does not impact the device functionality.

4.1.5 Frame and Cover Installation Adjustment units (e.g. grade rings) should be installed to set the frame and cover at the required elevation. The adjustment units should be laid in a full bed of mortar with successive units being joined using sealant recommended by the manufacturer. Frames for the cover should be set in a full bed of mortar at the elevation specified.

#### **4.2 MAINTENANCE ACCESS WALL**

In some instances the Maintenance Access Wall, if provided, shall require an extension attachment and sealing to the precast wall and cartridge deck at the job site, rather than at the precast facility. In this instance, installation of these components shall be performed according to instructions provided by the manufacturer.

4.3 FILTER CARTRIDGE INSTALLATION Filter cartridges shall be installed in the cartridge deck only after the construction site is fully stabilized and in accordance with the manufacturer's guidelines and recommendations. Contractor to contact the manufacturer to schedule cartridge delivery and review procedures/requirements to be completed to the device prior to installation of the cartridges and activation of the system.

### **PART 5 – QUALITY ASSURANCE**

5.1 FILTER CARTRIDGE INSTALLATION Manufacturer shall coordinate delivery of filter cartridges and other internal components with contractor. Filter cartridges shall be delivered and installed complete after site is stabilized and unit is ready to accept cartridges. Unit is ready to accept cartridges after it has been cleaned out and any standing water, debris, and other materials have been removed. Contractor shall take appropriate action to protect the filter cartridge receptacles and filter cartridges from damage during construction, and in accordance with the manufacturer's recommendations and guidance. For systems with cartridges installed prior to full site stabilization and prior to system activation, the contractor can plug inlet and outlet pipes to prevent stormwater and other influent from entering the device. Plugs must be removed during the activation process.

#### **5.2 INSPECTION AND MAINTENANCE**

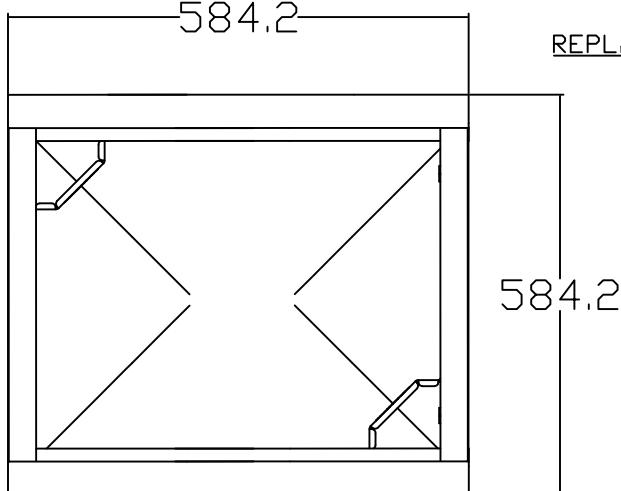
5.2.1 The manufacturer shall provide an Owner's Manual upon request.

5.2.2 After construction and installation, and during operation, the device shall be inspected and cleaned as necessary based on the manufacturer's recommended inspection and maintenance guidelines and the local regulatory agency/body.

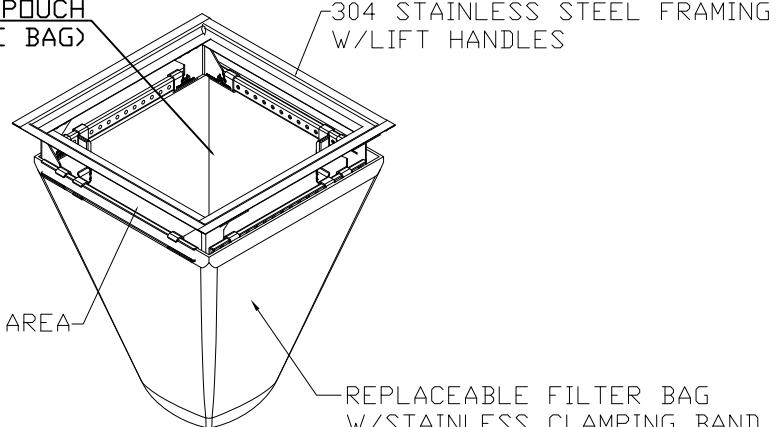
5.3 REPLACEMENT FILTER CARTRIDGES When replacement membrane filter elements and/or other parts are required, only membrane filter elements and parts approved by the manufacturer for use with the stormwater quality filter device shall be installed.

### **END OF SECTION**

4 1 3 2 1 FLEXSTORM INLET FILTER: 62MHDFX FOR ODSPD 400. Std.



REPLACEABLE ACTIVATED CARBON POUCH  
(CLIPPED TO BOTTOM OF THE BAG)

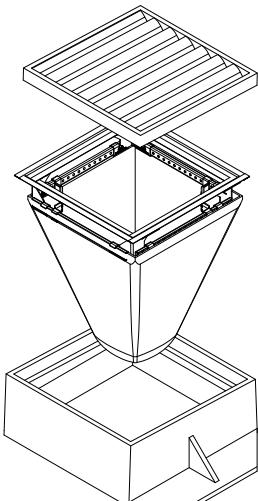


FLEXSTORM PURE INLET FILTERS FOR  
RECTANGULAR OPENINGS WITH GRATES

Product selection for FLEXSTORM PURE Filters (Permanent Inlet Protection)

Standard	Inlet Type	Grate Size	Opening Size	Bag Cap (liters <sup>3</sup> )	Flow Ratings (liters/second)			FX	FX+	PC	PC+
					FX/FX+	PC/PC+	Bypass				
ODSP 400.____	Square/Rect (SQ) tab supports	604 X 604	508 x 508	67.8	53.8	33.9	124.6	62MHDONTFX	62MHDONTFXP	62MHDONTFX	62MHDONTPCP

\*Ratings shown at 50% capacity to accommodate filter bag midway through service life.



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(630) 355-3477 FX  
INFO@INLETFILTERS.COM

SIZE	FRAME TYPE	DWG NO	REV
C			A
SCALE	Drawn		

SHEET 1 OF 1



## **FLEXSTORM™ Inlet Filter Specifications and Work Instructions**

**Product:** **FLEXSTORM Inlet Filters**

**Manufacturer:** **Inlet & Pipe Protection, Inc** [www.inletfilters.com](http://www.inletfilters.com)

***A subsidiary of Advanced Drainage Systems (ADS) [www.ads-pipe.com](http://www.ads-pipe.com)***

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### **1.0 Description of Work:**

- 1.1 The work covered shall consist of supplying, installing, and maintaining/cleaning of the FLEXSTORM Inlet Filter assembly. The purpose of the FLEXSTORM Inlet Filter system is to collect silt and sediment from surface storm water runoff at drainage locations shown on the plans or as directed by the Engineer. FLEXSTORM PURE, permanent filters, are capable of removing small particles, hydrocarbons, and other contaminants from drainage “hot spots”.

### **2.0 Material:**

- 2.1 The FLEXSTORM Inlet Filter system is comprised of a corrosion resistant steel frame and a replaceable geotextile sediment bag attached to the frame with a stainless steel locking band. The sediment bag hangs suspended from the rigid frame at a distance below the grate that shall allow full water flow into the drainage structure if the bag is completely filled with sediment.



- 2.2 The FLEXSTORM Inlet Filter frame includes lifting handles in addition to the standard overflow feature. A FLEXSTORM Removal Tool engages the lifting bars or handles to allow manual removal of the assembly without machine assistance. The frame suspension system on most rectangular designs is adjustable in  $\frac{1}{2}$ " increments up to 5" per side should the casting or drainage structure have imperfections.





2.3 **FLEXSTORM CATCH-IT** Inlet Filters for temporary inlet protection: The FLEXSTORM CATCH-IT framing is galvanized or zinc plated for corrosion resistance. The “FX” Woven Polypropylene filter bag is the design standard, although the “IL” Nonwoven geotextile is also available if preferred by the engineer. These products are typically used for temporary inlet protection lasting 3 months (short term road work) to 5 years (residential developments).



2.4 **FLEXSTORM PURE** Inlet Filters for permanent inlet protection: The FLEXSTORM PURE framing is comprised of 304 stainless steel with a 25 year life rating. Multiple filter bags are available: **FX, FX+, PC, PC+, LL** and others. The Post Construction “**PC+**” is the design standard consisting of the “**FX**” Woven Polypropylene sediment bag lined with Adsorb-it filter fabric, which is made from recycled polyester fibers. The “**PC+**” includes a replaceable hydrocarbon skimmer pouch strapped to the bottom of the bag for advanced TPH removal.



### 3.0 Filter Bag Specifications and Capabilities:

3.1 Material Properties (taken from manufacturers average roll value):

FLEXSTORM FILTER BAGS	(22" depth)	(12" depth)	Clean Water Flow Rate (GPM/SqFt)	Min A.O.S. (US Sieve)
	STD Bag P/N	Short Bag P/N		
<b>FX: Standard Woven Bag</b>	<b>FX</b>	<b>FX-S</b>	200	40
<b>FX+: Woven w/ Oil Skimmer</b>	<b>FXP</b>	<b>FXP-S</b>	200	40
<b>FXO: Woven w/ Oil Boom</b>	<b>FXO</b>	<b>FXO-S</b>	200	40
<b>PC: Post Construction Bag</b>	<b>PC</b>	<b>PC-S</b>	137	140
<b>PC+: PC w/ Oil Skimmer</b>	<b>PCP</b>	<b>PCP-S</b>	137	140
<b>LL: Litter and Leaf Bag</b>	<b>LL</b>	<b>LL-S</b>	High	3.5
<b>IL: IDOT Non-Woven Bag</b>	<b>IL</b>	<b>IL-S</b>	145	70



3.2 Standard Bag Sizes and Capabilities: Bag Sizes are determined by clear opening dimensions of the drainage structure. Once frame design size is confirmed, Small - XL bag ratings can be confirmed to meet design criteria. Ratings below are for standard 22" deep bags.

Standard Bag Size <sup>§</sup>	Solids Storage Capacity (CuFt)	Filtered Flow Rate at 50% Max (CFS)			Oil Retention (Oz)	
		FX	PC	IL	PC*	PCP**
Small	1.6	1.2	0.8	0.9	66	155
Medium	2.1	1.8	1.2	1.3	96	185
Large	3.8	2.2	1.5	1.6	120	209
XL	4.2	3.6	2.4	2.6	192	370

4.0 **Tested Filtration Efficiency and Removal Rates:** Filtration Efficiency, TSS, and TPH testing performed under large scale, real world conditions at accredited third party erosion and sediment control testing laboratory. (See Full Test Reports at [www.inletfilters.com](http://www.inletfilters.com) )



Inside View of  
Hopper Agitator



Hopper With Outlet Pipe  
Leading To Area Inlet



Area Inlet Simulated Showing  
Influent Discharge From Pipe

4.1 **FLEXSTORM "FX" Filtration Efficiency Test Results:** All testing performed in general accordance with the ASTM D 7351, *Standard Test Method For Determination of Sediment Retention Device Effectiveness in Sheet Flow Application*, with flow diverted into an area inlet. Test Soil used as sediment had the following characteristics with a nominal 7% sediment to water concentration mix. This is representative of a heavy sediment load running off of a construction site.

Soil Characteristics	Test Method	Value	Filtration Efficiency of "FX" FLEXSTORM Bag  82%
% Gravel	ASTM D 422	2	
% Sand		60	
% Silt		24	
% Clay		14	
Liquid Limit, %	ASTM D 4318	34	
Plasticity Index, %		9	
Soil Classification	USDA	Sandy Loam	
Soil Classification	USCS	Silty Sand (SM)	



**4.2 FLEXSTORM “PC” and “PC+” Test Results:** TSS measured on effluent samples in accordance with SM 2540D and TPH in accordance with EPA 1664A.

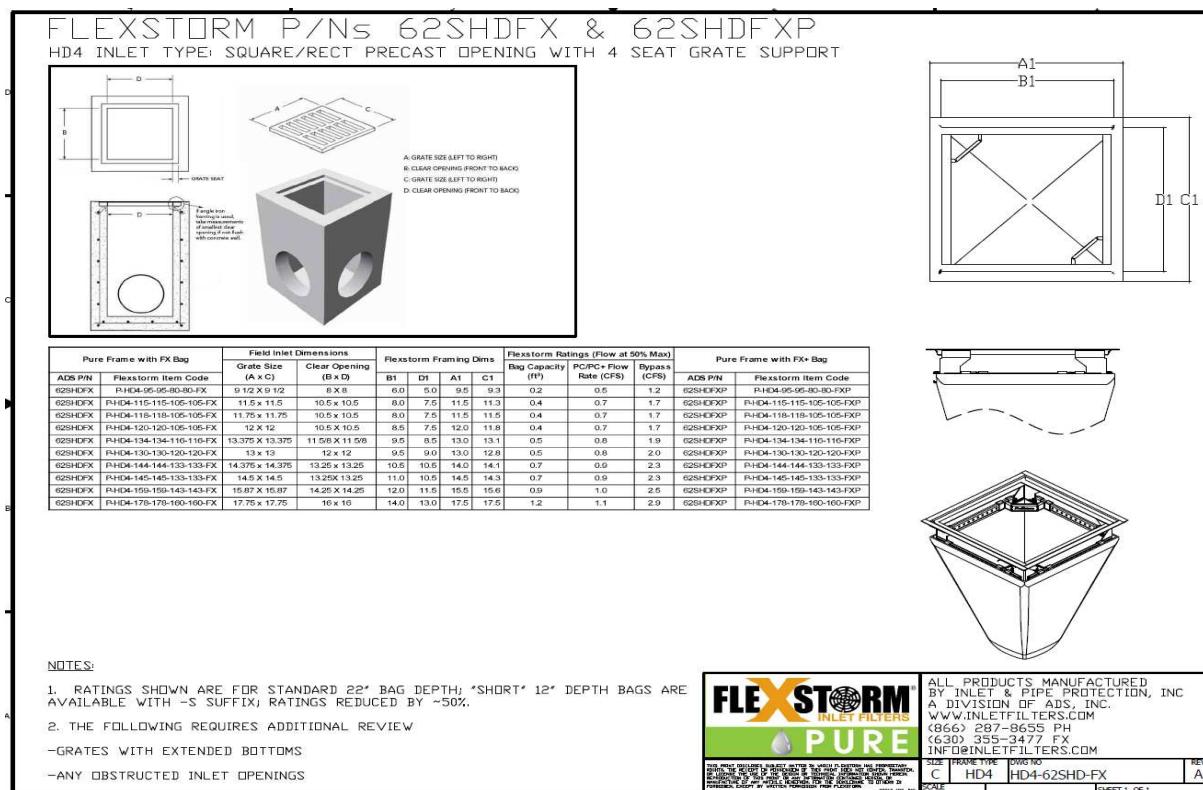
Product Tested	110 micron Sediment Load	Ave Flow Rate GPM	% TSS Removal	Soil Retention Efficiency
<b>FLEXSTORM PC Sediment Bag</b>	1750 mg/L using OK-110 Silica Sand and Clean Water	23	<b>99.28%</b>	98.96%
		48	<b>99.32%</b>	99.25%
		70	<b>98.89%</b>	98.80%

Product Tested	Street Sweep Sediment Load	Particle Size of Sediment Load	% TSS Removal	Soil Retention Efficiency
<b>FLEXSTORM PC Sediment Bag</b>	2.5% = 100 lbs Sed / 4000 lbs water	.001 mm – 10.0 mm (median 200 micron)	<b>99.68%</b>	95.61%

Product Tested	Hydrocarbon Load	Ave Flow Rate GPM	% TPH Removal	Oil Retention Efficiency
<b>FLEXSTORM PC+</b>	243 mg/L using 750 mL (1.45 lb) used motor oil + lube oil and clean water	19	<b>99.04%</b>	97.22%
<b>FLEXSTORM PC</b>		20	<b>97.67%</b>	91.61%
<b>FLEXSTORM PC+</b>		92	<b>96.88%</b>	99.11%

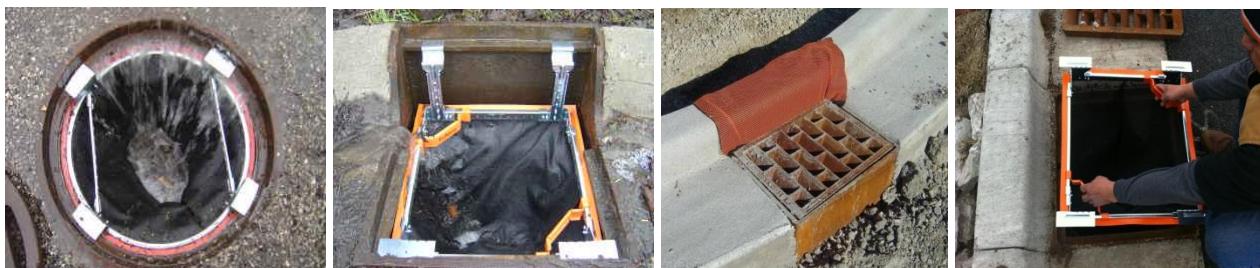
## **5.0 Identification of Drainage Structures to Determine FLEXSTORM Item Codes:**

5.1 The Installer (Contactor) shall inspect the plans and/or worksite to determine the quantity of each drainage structure casting type. The foundry casting number or the exact grate size and clear opening size will provide the information necessary to identify the required FLEXSTORM Inlet Filter part number. Inlet Filters are supplied to the field pre-configured to fit the specified drainage structure. Item Codes can be built using the FLEXSTORM Product Configurator at [www.inletfilters.com](http://www.inletfilters.com). Detailed Submittal / Specification drawings are linked to each Item Code and available for download by engineers and contractors to include on plans and/or verify field inlet requirements. An example of a typical drawing is shown below.



## 6.0 Installation Into Standard Grated Drainage Structures:

6.1 Remove the grate from the casting or concrete drainage structure. Clean the ledge (lip) of the casting frame or drainage structure to ensure it is free of stone and dirt. Drop in the FLEXSTORM Inlet Filter through the clear opening and be sure the suspension hangers rest firmly on the inside ledge (lip) of the casting. Replace the grate and confirm it is elevated no more than 1/8", which is the thickness of the steel hangers. For Curb Box Inlet Filters: Insert FLEXSTORM CATCH IT Inlet Filter as described above, pull the rear curb guard flap up and over the open curb box until tight, align magnets to ensure firm attachment to the top portion of the curb box casting. If the curb back opening is not magnetic, slide a typical rock sack or 2 x 4 through the 2-ply rear curb box flap to create a dam which will direct runoff into the sediment bag.





**7.0 Maintenance Guidelines:** The frequency of maintenance will vary depending on the application (during construction, post construction, or industrial use), the area of installation (relative to grade and runoff exposure), and the time of year relative to the geographic location (infrequent rain, year round rain, rain and snow conditions). The FLEXSTORM Operation & Maintenance Plan (as shown in 7.5) or other maintenance log should be kept on file.

**7.1 Frequency of Inspections:** Construction site inspection should occur following each  $\frac{1}{2}$ " or more rain event. Post Construction inspections should occur three times per year (every four months) in areas with year round rainfall and three times per year (every three months) in areas with rainy seasons before and after snowfall season. Industrial application site inspections (loading ramps, wash racks, maintenance facilities) should occur on a regularly scheduled basis no less than three times per year.

**7.2 General Maintenance for standard sediment bags:** Upon inspection, the FLEXSTORM Inlet Filter should be emptied if the sediment bag is more than half filled with sediment and debris, or as directed by the Engineer. Remove the grate, engage the lifting bars or handles with the FLEXSTORM Removal Tool, and lift the FLEXSTORM Inlet Filter from the drainage structure. Machine assistance is not required. Dispose of the sediment or debris as directed by the Engineer. As an alternative, an industrial vacuum may be used to collect the accumulated sediment if available. Remove any caked on silt from the sediment bag and reverse flush the bag for optimal filtration. Replace the bag if the geotextile is torn or punctured to  $\frac{1}{2}$ " diameter or greater on the lower half of the bag. If properly maintained, the Woven sediment bag will last a minimum of 4 years in the field.

**7.3 Inspection and Handling of the FLEXSTORM PC / PC+ post construction sediment bag:** The PC+ sediment bags will collect oil until saturated. Both the Adsorb-it filter liner and the skimmer pouch will retain oil. The volume of oils retained will depend on sediment bag size. Unlike other passive oil sorbent products, Adsorb-it filter fabric has the ability to remove hydrocarbons at high flow rates while retaining 10- 20 times its weight in oil (weight of fabric is 12.8 oz / sq yd). The average 2' x 2' PC Bag contains approx .8 sq yds, or 10 oz of fabric. At 50% saturation, the average Adsorb-it lined PC filter will retain approximately 75 oz (4.2 lbs) of oil. Once the bag has become saturated with oils, it can be centrifuged or passed through a wringer to recover the oils, and the fabric reused with 85% to 90% efficacy. If it is determined, per Maintenance Contracts or Engineering Instructions, that the saturated PC sediment bags will be completely replaced, it is the responsibility of the service technician to place the filter medium and associated debris in an approved container and dispose of in accordance with EPA regulations. Spent Adsorb-it can be recycled for its fuel value through waste to energy incineration with a higher BTU per pound value than coal. The oil skimmers start white in color and will gradually turn brown/black as they become saturated, indicating time for replacement. The average skimmer pouch will absorb approximately 62 oz (4 lbs) of oil before requiring replacement. To remove the pouch simply unclip it from the swivel strap sewn to the bottom of the bag. Dispose of all oil contaminated products in accordance to EPA guidelines. The ClearTec Rubberizer media used in the pouch, since a solidifier, will not leach under pressure and can be disposed of in most landfills, recycled for industrial applications, or burned as fuel.



7.4 Sediment Bag Replacement: When replacing a Sediment Bag, remove the bag by loosening or cutting off the clamping band. Take the new sediment bag, which is equipped with a stainless steel worm drive clamping band, and use a drill or screw driver to tighten the bag around the frame channel. Ensure the bag is secure and that there is no slack around the perimeter of the band. For Oil absorbent boom bags, simply replace the oil boom or pouch when saturated by sliding it through the mesh support sleeve.





7.5 Operation & Maintenance Plan. (Download at [www.inletfilters.com](http://www.inletfilters.com) or [www.ads-pipe.com](http://www.ads-pipe.com) )

# FLEXSTORM® PURE PERMANENT INLET PROTECTION

## SPECIFY WITH CONFIDENCE

State DOTs and municipalities across the country now have a universal structural BMP to address the issue of storm sewer inlet protection: FLEXSTORM PURE Inlet Filters.

The FLEXSTORM PURE system is the preferred choice for permanent inlet protection and storm water runoff control. Constructed of versatile stainless steel, FLEXSTORM PURE Inlet Filters will fit any drainage structure and are available with site-specific filter bags providing various levels of filtration. Whether you're the specifier or the user, it's clear to see how FLEXSTORM PURE Inlet Filters outperform the competition.

## APPLICATIONS:

Car Washes	Gas Stations
Commercial	Parking Lots
Loading Ramps	Dock Drains
Industrial	Maintenance

## FEATURES:

- Stainless Steel filter framing is custom configured to fit perfectly into any drainage structure, whether a standard design or obstructed inlet opening
- Filtered Flow Rates and Ultimate Bypass Rates are designed to meet your specific inlet requirements
- Multiple Filter Bags are available targeting site specific removal of trash, litter, leaves, or small particles, oil and grease
- Filters work below grade with an ultimate bypass allowing inlet area to drain with a full bag
- Units install in seconds and are easily maintained with the FLEXSTORM Universal Removal Tool (no heavy machinery required)

**ADS Service:** ADS representatives are committed to providing you with the answers to all your questions, including selecting the proper filter, specifications, installation and more. Also try the **ADS FLEXSTORM Online Product Configurator** at [www.inletfilters.com](http://www.inletfilters.com)

## FEATURES:

- Receive payback on your investment: durable stainless steel framing provides extended service life while replaceable filter bags handle loads with a safety factor of 5
- Meets stringent removal requirements:
  - FX filter bags are rated for >80% removal efficiency of street sweep-size particles
  - PC/PC+ filter bags have been tested to 99% TSS removal of OK-110 US Silica Sand and 97% TPH (total petroleum hydrocarbon) removal
- Help prevent fines: FLEXSTORM Inlet Filters comply with EPA NPDES initiatives as a temporary or permanent BMP
- If not in stock, orders up to 100 pieces can ship within 48 hours



## FLEXSTORM PURE INLET FILTERS SPECIFICATION

### IDENTIFICATION

The installer shall inspect the plans and/or worksite to determine the quantity of each drainage structure casting type. The foundry casting number, exact grate size and clear opening size, or other information will be necessary to finalize the FLEXSTORM part number and dimensions. The units are shipped to the field configured precisely to fit the identified drainage structure.

### MATERIAL AND PERFORMANCE

The FLEXSTORM Inlet Filter system is comprised of a corrosion resistant steel frame and a replaceable geotextile filter bag attached to the frame with a stainless steel locking band. The filter bag hangs suspended at a distance below the grate that shall allow full water flow into the drainage structure if the bag is completely filled with sediment. The standard Woven Polypropylene FX filter bags are rated for 200 gpm/sqft with a removal efficiency of 82% when filtering a USDA Sandy Loam sediment load. The Post Construction PC filter bags are rated for 137 gpm/sqft and have been 3rd party tested at 99% TSS removal to 110 micron and 97% TPH removal of used motor oil hydrocarbon mix.

### INSTALLATION

Remove the grate from the casting or concrete drainage structure. Clean the ledge (lip) of the casting frame or drainage structure to ensure it is free of stone and dirt. Drop in the FLEXSTORM Inlet Filter through the clear opening and be sure the suspension hangers rest firmly on the inside ledge (lip) of the casting. Replace the grate and confirm it is elevated no more than 1/8", which is the thickness of the steel hangers. For wall mount units, follow instructions for attaching the stainless steel mounting brackets using the provided concrete fasteners.

### INSPECTION FREQUENCY

Construction site inspection should occur following each 1/2" or more rain event. Post Construction inspections should occur three times per year (every four months) in areas with mild year round rainfall and four times per year (every three months Feb–Nov) in areas with summer rains and before and after the winter snowfall season. Industrial application site inspections (loading ramps, wash racks, maintenance facilities) should occur on a regularly scheduled basis no less than three times per year.

### MAINTENANCE GUIDELINES

Empty the filter bag if more than half filled with sediment and debris, or as directed by the engineer. Remove the grate, engage the lifting bars or handles with the FLEXSTORM Removal Tool, and lift from the drainage structure. Dispose of the sediment or debris as directed by the engineer or maintenance contract in accordance with EPA guidelines.

As an alternative, an industrial vacuum may be used to collect the accumulated sediment. Remove any caked-on silt from the sediment bag and reverse flush the bag with medium spray for optimal filtration. Replace the bag if torn or punctured to 1/2" diameter or greater on the lower half of the bag. Post Construction PC/PC+ Bags should be maintained prior to 50% oil saturation. The average 2' x 2' PC filter bag will retain approx. 96 oz (5.4 lbs) of oil at which time it should be serviced or replaced. It can be centrifuged or passed through a wringer to recover the oils, and the fabric reused with 85% to 90% efficacy. It may also be recycled for its fuel value through waste to energy incineration. When utilizing the Cleartec Rubberizer Pouches in the + bags, note that these oil skimmers will gradually turn brown and solidify as they become saturated, indicating time for replacement. Each pouch will absorb approximately 62 oz (4 lbs) of oil before requiring replacement. The spent media may also be recycled for its fuel value through waste to energy incineration. Dispose of all oil contaminated products in accordance with EPA guidelines.

### FILTER BAG REPLACEMENT

Remove the bag by loosening or cutting off the clamping band. Take the new filter bag, which is equipped with a stainless steel worm drive clamping band, and use a screw driver to tighten the bag around the frame channel. Ensure the bag is secure and that there is no slack around the perimeter of the band.

**Lift Handles** ease installation and maintenance

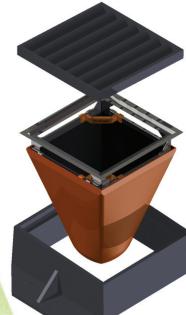


Replaceable Sediment Bag

1/8" thick steel hangers & channels; precision stampings **configured to fit each individual casting**



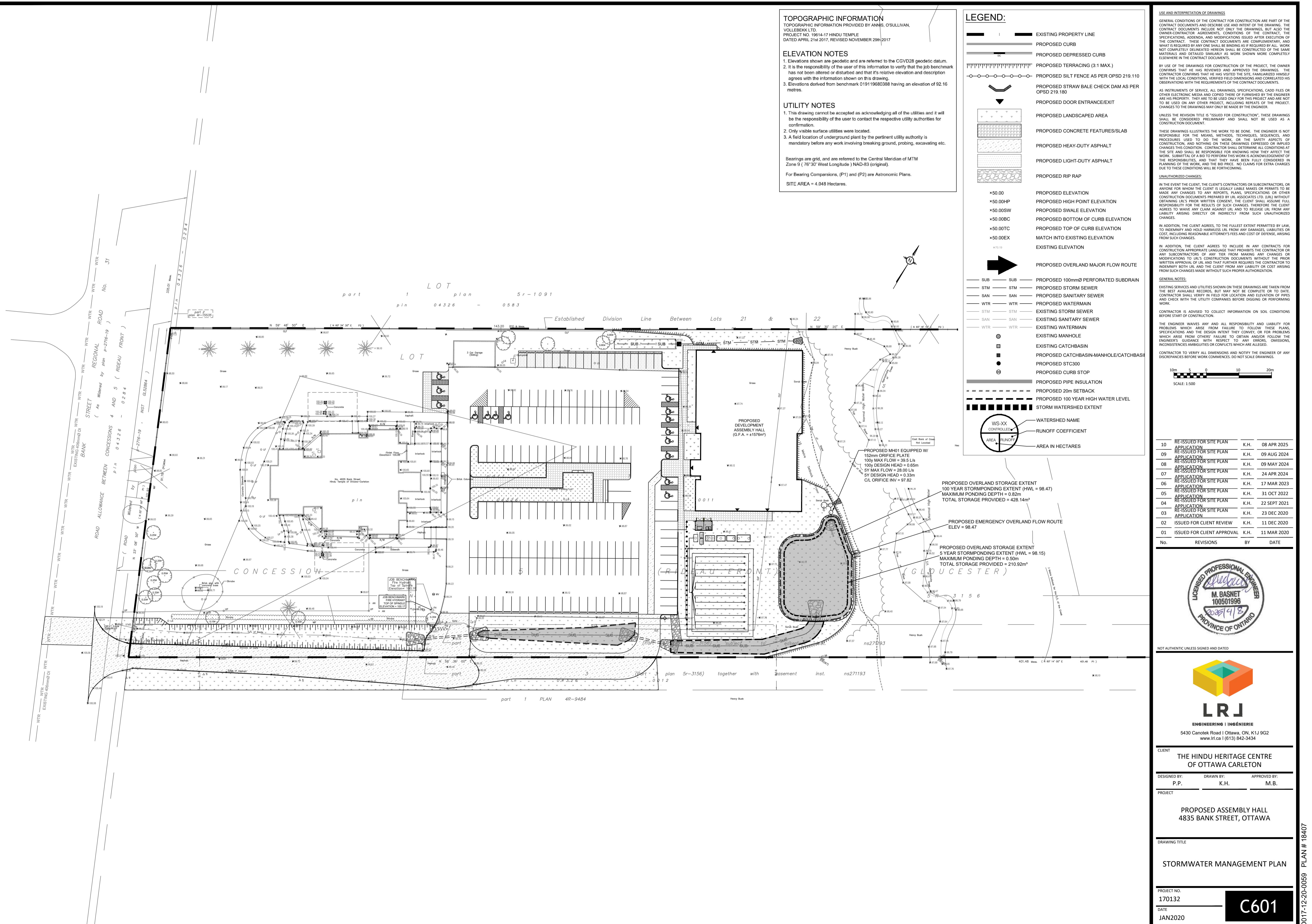
CAD drawings, work instructions and test reports on website: [www.inletfilters.com](http://www.inletfilters.com)



For more information on FLEXSTORM Inlet Filters and other ADS products, please contact our Customer Service Representatives at 1-800-821-6710  
Try the **ADS FLEXSTORM Online Product Configurator** at [www.inletfilters.com](http://www.inletfilters.com).

ADS "Terms and Conditions of Sale" are available on the ADS website, [www.ads-pipe.com](http://www.ads-pipe.com)  
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**APPENDIX F**  
**Stormwater Management Plan**



**APPENDIX G**  
**Architectural Drawings**



**APPENDIX H**  
**Servicing Plan**



**APPENDIX I**  
**Erosion and Sediment Control Plan**

**EROSION AND SEDIMENT CONTROL MEASURES:**

\*\* CONTRACTOR IS RESPONSIBLE FOR ALL INSTALLATION, MONITORING, REPAIR AND REMOVAL OF ALL EROSION AND SEDIMENT CONTROL FEATURES \*\*

\*\* THE SEDIMENT AND EROSION CONTROL MEASURES MAY BE MODIFIED IN THE FIELD AT THE DISCRETION OF THE CITY OF OTTAWA SITE INSPECTOR OR CONSERVATION AUTHORITY\*\*

1. PRIOR TO START OF CONSTRUCTION:

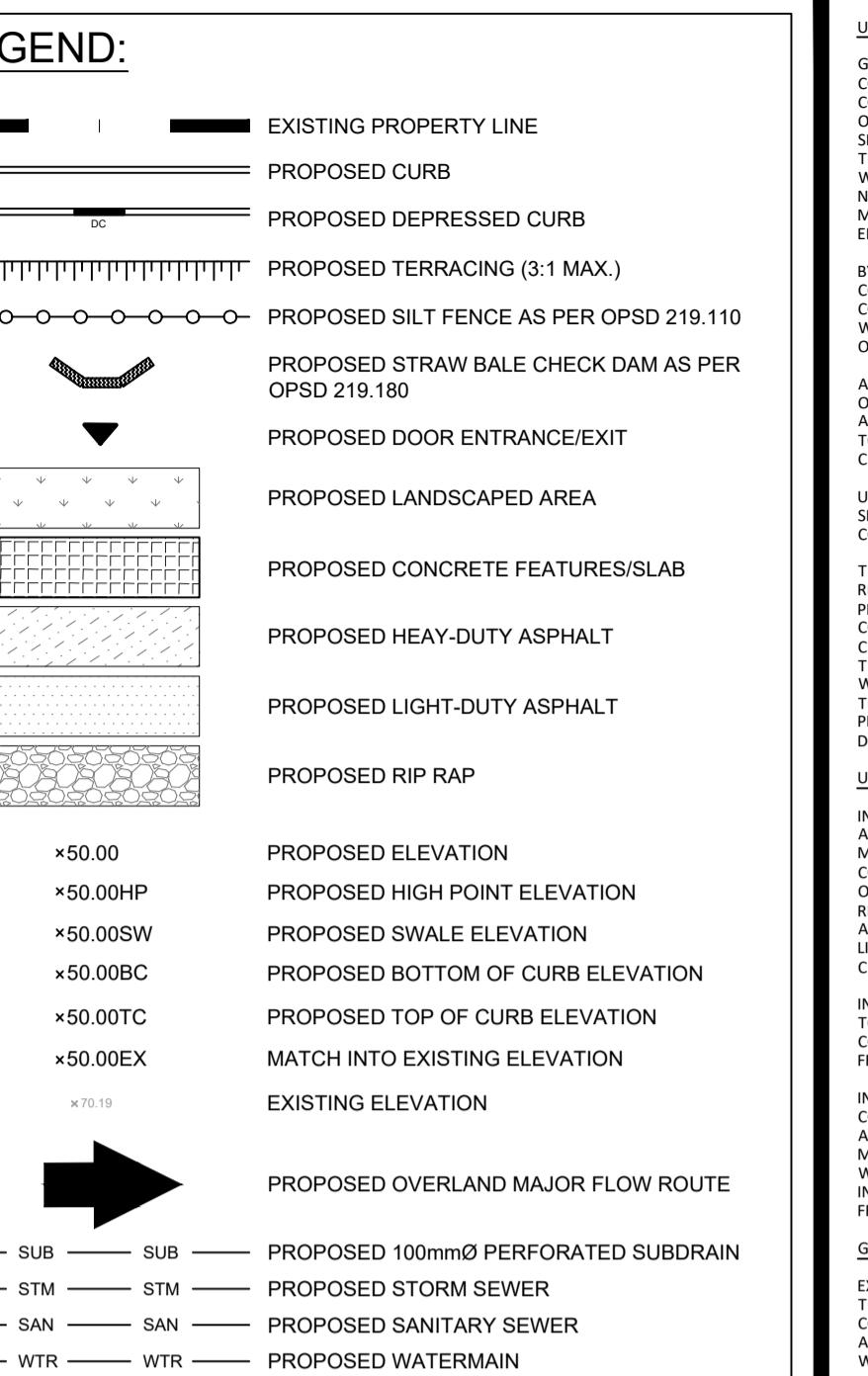
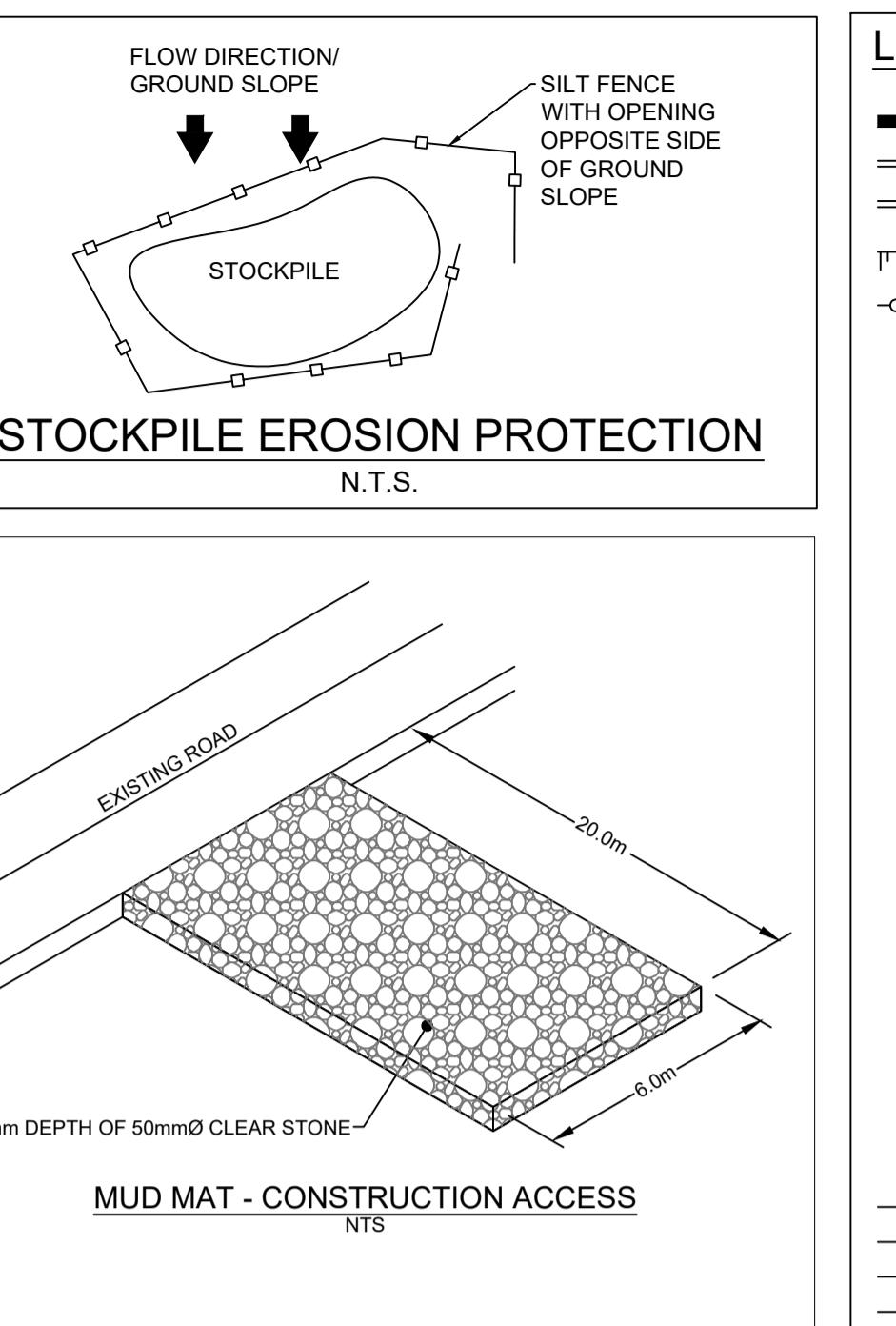
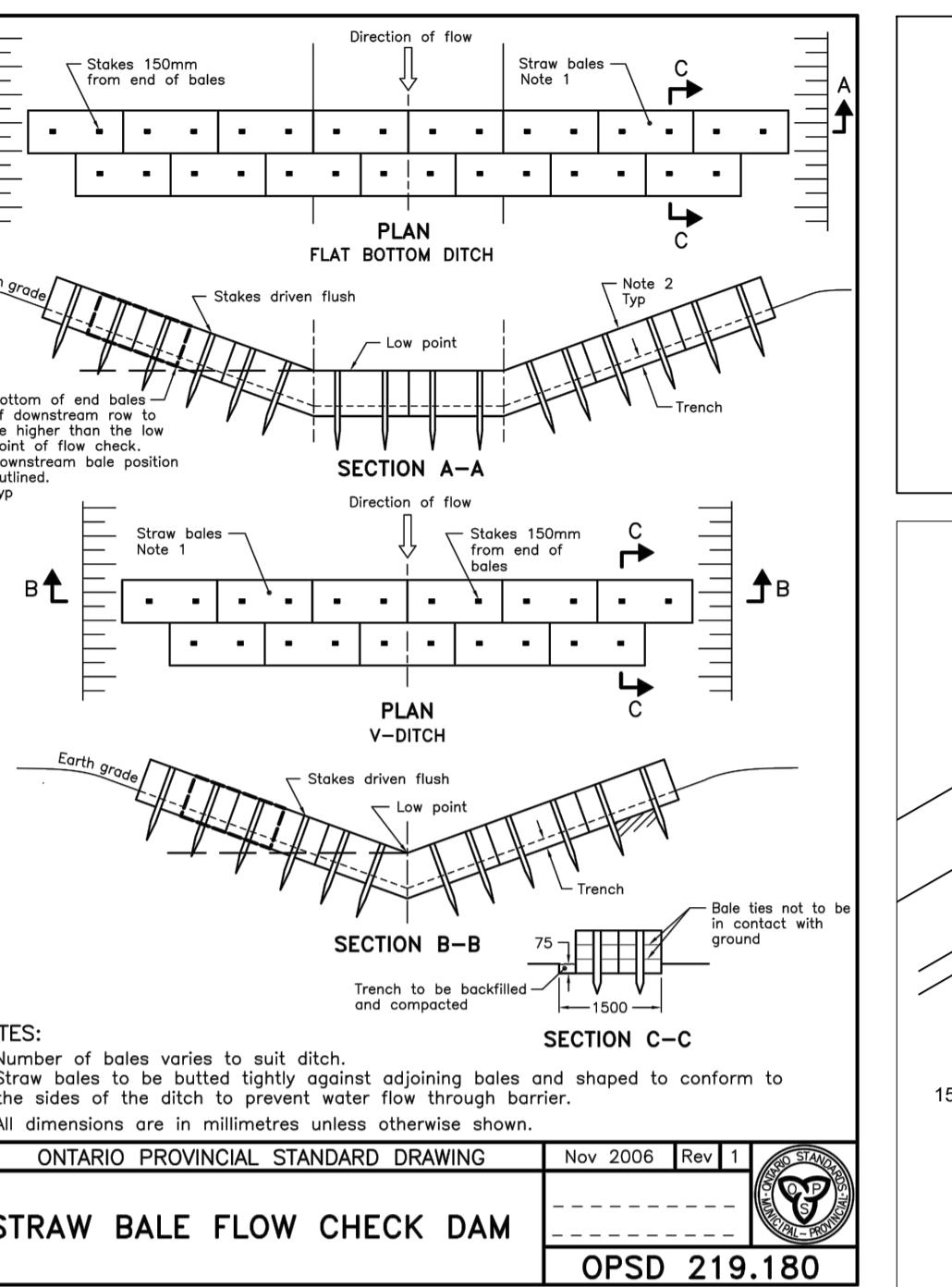
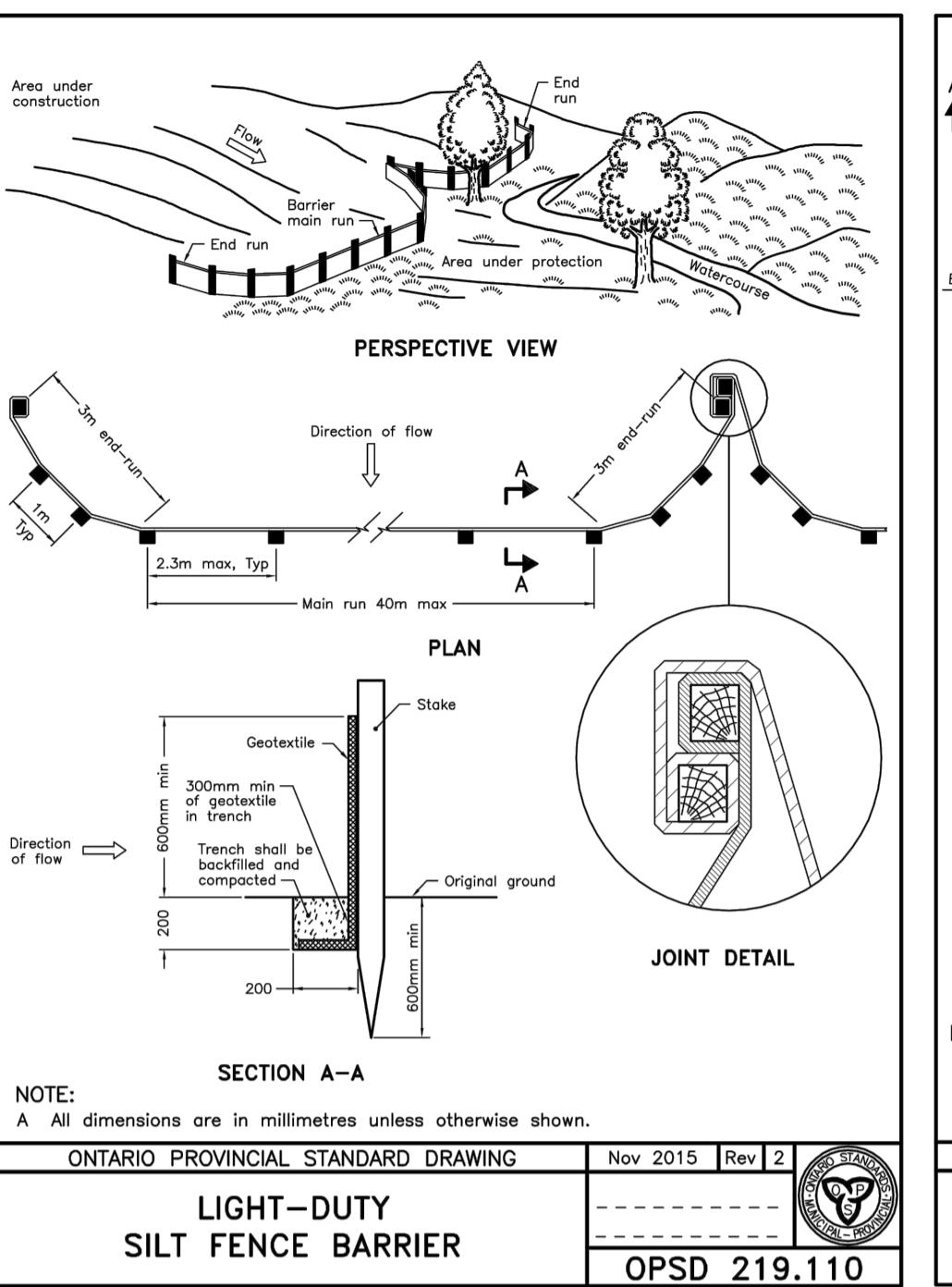
- PRIOR TO THE REMOVAL OF ANY VEGETATIVE COVER, MOVING OF SOIL AND CONSTRUCTION:
- INSTALL SILT FENCE IMMEDIATELY DOWNSTREAM FROM AREAS TO BE DISTURBED (SEE PLAN FOR LOCATION).
- INSTALL GEOTEXTILE INSERTS WITH AN OVERLAY OF 10MM DOWNSLOPE CATCH BASINS AND MANHOLES
- INSTALL SILTBACK FILTERS IN ALL CONCRETE CATCH BASINS STRUCTURES
- INSPECT MEASURES IMMEDIATELY AFTER INSTALLATION.

2. DURING CONSTRUCTION:

- WORK TO BE DONE IN THE VICINITY OF MAJOR WATERWAYS TO BE CARRIED OUT FROM JULY TO SEPTEMBER ONLY.
- MINIMIZE THE EXTENT OF DISTURBED AREAS AND THE DURATION OF EXPOSURE.
- PROTECT DISTURBED AREAS FROM RUNOFF.
- PROVIDE TEMPORARY COVER SUCH AS SEEDING OR MULCHING IF DISTURBED AREA WILL NOT BE REHABILITATED WITHIN 30 DAYS.
- INSPECT SILT FENCES, FILTER CLOTHS AND CATCH BASIN SUMPS WEEKLY AND AFTER EVERY MAJOR STORM EVENT.
- ENSURE SILT FENCE IS TIGHTLY BUTTED TO THE TRENCH.
- DO NOT ALLOW TOPSOIL PILES AND EXCAVATION MATERIAL CLOSER THAN 2.5m FROM ANY PAVED SURFACE, OR ONE WHICH IS TO BE PAVED BEFORE THE PILE IS REMOVED. ALL TOPSOIL PILES ARE TO BE SEEDED IF THEY ARE TO REMAIN ON SITE LONG ENOUGH FOR SEEDS TO GROW (LONGER THAN 30 DAYS).
- CONTROL WIND BLOWN DUST CLOUDS TO AGRICULTURAL LEVELS BY SEEDING TOPSOIL PILES AND OTHER AREAS DEMANDING AGRICULTURAL PRACTICES AS REQUIRED.
- ALL EROSION CONTROL STRUCTURE TO REMAIN IN PLACE UNTIL ALL DISTURBED GROUND SURFACES HAVE BEEN STABILIZED EITHER BY PAVING OR RESTORATION OF VEGETATIVE GROUND COVER.
- ALL EROSION CONTROL STRUCTURE TO REMAIN IN PLACE UNTIL ALL DISTURBED GROUND SURFACES HAVE BEEN STABILIZED EITHER BY PAVING OR RESTORATION OF VEGETATIVE GROUND COVER.
- NO ALTERNATE METHODS OF EROSION PROTECTION SHALL BE PERMITTED UNLESS APPROVED BY THIS CONSULTING ENGINEER AND THE CITY DEPARTMENT OF PUBLIC WORKS.
- CONTRACTOR RESPONSIBLE FOR CITY ROADWAY AND SIDEWALK TO BE CLEANED OF ALL SEDIMENT FROM VEHICULAR TRACKING ETHERS OF EACH VEHICLE.
- PROVIDE GRAVEL ENTRANCE TO AGRICULTURAL EQUIPMENT LEAVES THE SITE TO PREVENT MUD TRACKING ONTO PAVED SURFACES. GRAVEL BED SHALL BE A MINIMUM OF 15m LONG, 4m WIDE AND 0.3m DEEP AND SHALL CONSIST OF COARSE (50mm CRUSHED-ROCK LIMESTONE) MATERIAL. MAINTAIN GRAVEL ENTRANCE IN CLEAN CONDITION.
- DURING WET CONDITIONS, TIRES OF ALL VEHICLES/EQUIPMENT LEAVING THE SITE ARE TO BE SCRAPED.
- ANY MUD/MATERIAL TRACKED ONTO THE ROAD SHALL BE REMOVED IMMEDIATELY BY HAND OR RUBBER TIRE LOADER.
- TAKE ALL NECESSARY STEPS TO PREVENT BUILDING MATERIAL, CONSTRUCTION DEBRIS OR WASTE BEING SPILLED OR TRACKED ONTO ADJACENT PROPERTIES OR PUBLIC STREETS DURING CONSTRUCTION AND PROCEED IMMEDIATELY TO CLEAN UP ANY AREAS SO AFFECTED.

3. AFTER CONSTRUCTION:

- PROVIDE PERMANENT COVER CONSISTING OF TOPSOIL AND SEED TO DISTURBED AREAS.
- REMOVE STRAW BALE FLOW CHECK DAMS, SILT FENCES AND FILTER CLOTHS ON CATCH BASINS AND MANHOLE COVERS AFTER DISTURBED AREAS HAVE BEEN REHABILITATED AND STABILIZED.
- INSPECT AND CLEAN CATCH BASIN SUMPS AND STORM SEWERS.



**LEGEND:**

— Existing Property Line  
— Proposed Curb  
— Proposed Depressed Curb  
— Proposed Terracing (3:1 Max.)  
— Proposed Silt Fence As Per OPSD 219.110  
— Proposed Straw Bale Check Dam As Per OPSD 219.180  
— Proposed Door Entrance/Exit  
— Proposed Landscaped Area  
— Proposed Concrete Features/Slab  
— Proposed Heavy-Duty Asphalt  
— Proposed Light-Duty Asphalt  
— Proposed Rip Rap  
— Proposed Elevation  
— Proposed High Point Elevation  
— Proposed Swale Elevation  
— Proposed Bottom of Curb Elevation  
— Proposed Top of Curb Elevation  
— Match Into Existing Elevation  
— Existing Elevation  
— Proposed Overland Major Flow Route  
— Sub — Proposed 100mm Ø Perforated Subdrain  
— STM — Proposed Storm Sewer  
— SAN — Proposed Sanitary Sewer  
— WTR — Proposed Watermain  
— STM — Existing Storm Sewer  
— SAN — Existing Sanitary Sewer  
— WTR — Existing Watermain  
— Existing Manhole  
— Existing Catchbasin  
— Proposed Catchbasin-Manhole/Catchbasin  
— Proposed STC300  
— Proposed Curb Stop  
— Proposed Pipe Insulation  
— Proposed 20m Setback  
— Proposed 100 Year High Water Level  
— Storm Watershed Extent  
— Watershed Name  
— Runoff Coefficient  
— Area in Hectares

**GENERAL CONDITIONS OF THE CONTRACT FOR CONSTRUCTION** ARE PART OF THE CONTRACT DOCUMENTS AND DESCRIBE USE AND INTENT OF THE DRAWING. THE CONTRACT DOCUMENTS INCLUDE NOT ONLY THE DRAWINGS, BUT ALSO THE GENERAL CONDITIONS, CONTRACT DOCUMENTS, CONTRACT CONDITIONS, CONTRACT SPECIFICATIONS, ADDENDA, AND MODIFICATIONS ISSUED AFTER EXECUTION OF THE CONTRACT. THESE CONTRACT DOCUMENTS ARE COMPLEMENTARY, AND UNLESS OTHERWISE PROVIDED, ARE TO BE READ AND CONSTRUED AS ONE. ANY PART OF THE CONTRACT WHICH IS NOT COMPLETED OR WHICH IS NOT COMPLETELY DELINEATED HEREIN SHALL BE CONSTRUED AS THE SAME MATERIALS AND DETAILED SIMILARLY AS THE WORK SHOWN MORE COMPLETELY ELSEWHERE.

BY USE OF THE DRAWINGS FOR CONSTRUCTION OF THE PROJECT, THE OWNER CONFIRMS THAT HE HAS REVIEWED AND APPROVED THE DRAWINGS. THE CONTRACTOR CONFIRMS THAT HE HAS VISITED THE SITE, FAMILIARIZED HIMSELF WITH THE CONDITIONS OF THE SITE, AND HAS MADE HIS OBSERVATIONS WITH THE REQUIREMENTS OF THE CONTRACT DOCUMENTS.

AS INSTRUMENTS OF SERVICE, ALL DRAWINGS, SPECIFICATIONS, CAD FILES OR OTHER ELECTRONIC MEDIA AND COPIES THEREOF FURNISHED BY THE ENGINEER ARE THE PROPERTY OF THE ENGINEER. THEY ARE TO BE USED ONLY FOR THE PROJECT FOR WHICH THEY WERE FURNISHED. THEY ARE NOT TO BE USED ON ANY OTHER PROJECT, INCLUDING REWORK OR ON THE PROJECT CHANGES TO THE DRAWINGS MAY ONLY BE MADE BY THE ENGINEER.

UNLESS THE REVISION TITLE IS 'ISSUED FOR CONSTRUCTION', THESE DRAWINGS SHALL BE CONSIDERED PRELIMINARY AND SHALL NOT BE USED AS A CONSTRUCTION DOCUMENT.

THESE DRAWINGS ILLUSTRATE THE WORK TO BE DONE. THE ENGINEER IS NOT RESPONSIBLE FOR THE MEANS, METHODS, TECHNIQUES, SECURITIES, AND PROCEDURES USED TO DO THE WORK OR THE SAFETY ASPECTS OF CONSTRUCTION, AND NOTHING ON THESE DRAWINGS SHALL BE CONSTRUED AS A CONTRACT FOR THE WORK. THE CONTRACTOR SHALL DETERMINE ALL CONDITIONS AT THE SITE AND SHALL BE RESPONSIBLE FOR KNOWING HOW THEY AFFECT THE WORK AND FOR THE METHODS AND PROCEDURES USED TO DO THE WORK. THE RESPONSIBILITY AND THE COSTS THEREOF SHALL BE BORN BY THE CONTRACTOR. THE CONTRACTOR AGREES THAT ANY CHANGES MADE TO THE DRAWINGS SHALL BE MADE IN WRITING AND APPROVED BY THE ENGINEER. THE CONTRACTOR AGREES TO WAIVE ANY CLAIM AGAINST LRL AND TO RELEASE LRL FROM ANY LIABILITY ARISING DIRECTLY OR INDIRECTLY FROM SUCH UNAUTHORIZED CHANGES.

IN THE EVENT THE CLIENT, THE CLIENT'S CONTRACTORS OR SUBCONTRACTORS, OR THE ENGINEER MAKE ANY CHANGES TO THE DRAWINGS, THE CONTRACTOR SHALL NOTIFY THE CONTRACTOR OF THE CHANGES AND THE CONTRACTOR SHALL INDEMNIFY AND HOLD HARMLESS LRL FROM ANY DAMAGES, LIABILITIES OR COSTS, INCLUDING REASONABLE ATTORNEY'S FEES AND COST OF DEFENSE, ARISING FROM SUCH CHANGES.

IN ADDITION, THE CLIENT AGREES, TO THE FULLEST EXTENT PERMITTED BY LAW, TO INDEMNIFY AND HOLD HARMLESS LRL FROM ANY DAMAGES, LIABILITIES OR COSTS, INCLUDING REASONABLE ATTORNEY'S FEES AND COST OF DEFENSE, ARISING FROM ANY CHANGES MADE TO THE DRAWINGS.

THE CONTRACTOR AGREES TO INCLUDE IN THE CONTRACTS FOR SUBCONTRACTORS THE SAME PROVISIONS AS ARE CONTAINED IN THIS CONTRACT.

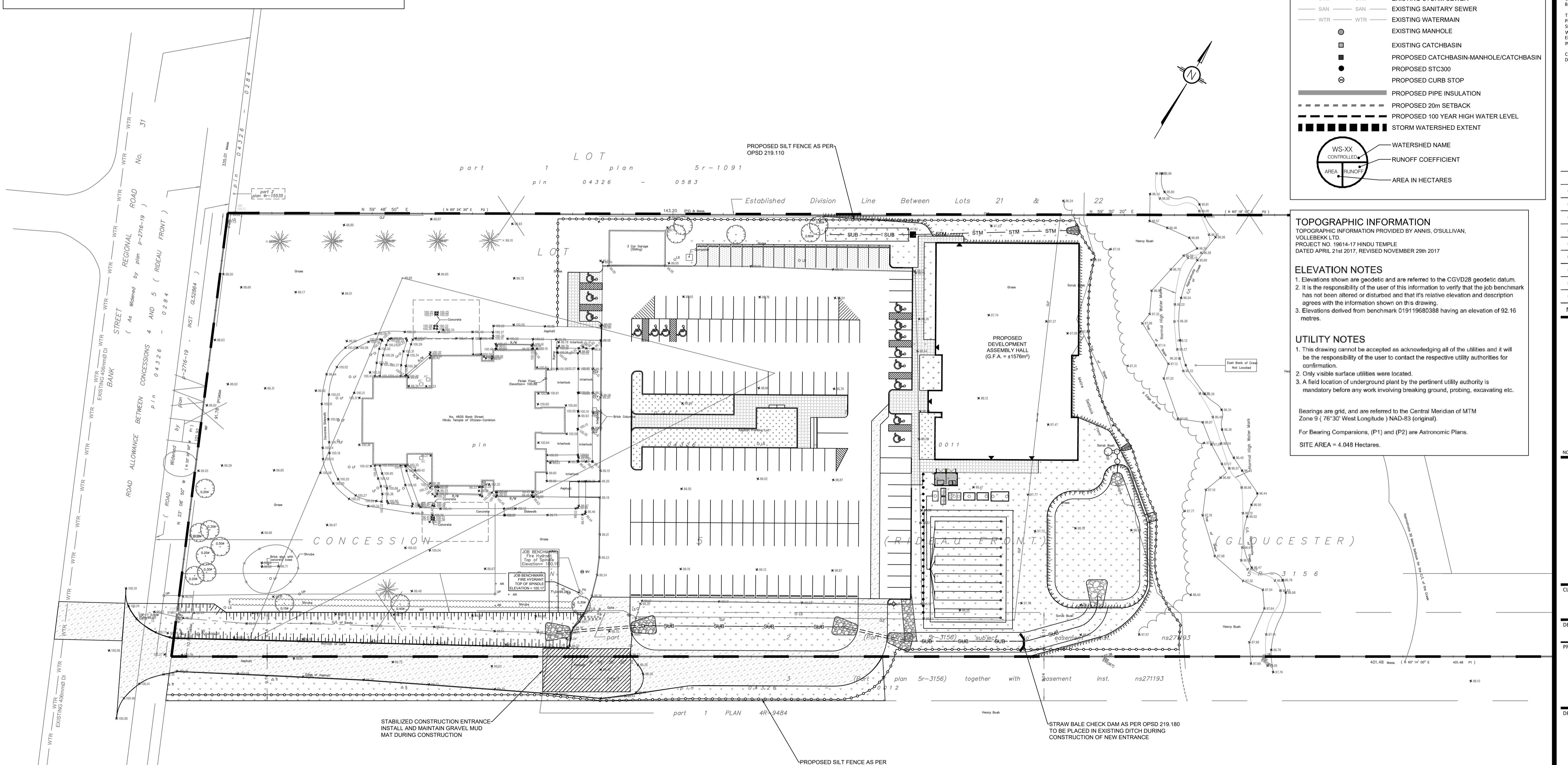
THE CONTRACTOR SHALL VERIFY IN FIELD FOR LOCATION AND ELEVATION OF PIPES AND CHECK WITH THE UTILITY COMPANIES BEFORE DIGGING OR PERFORMING WORK.

CONTRACTOR IS ADVISED TO COLLECT INFORMATION ON SOIL CONDITIONS BEFORE START OF CONSTRUCTION.

THE ENGINEER WAIVES ANY AND ALL RESPONSIBILITY AND LIABILITY FOR PROBLEMS WHICH ARISE FROM FAILURE TO FOLLOW THESE PLANS, SPECIFICATIONS OR THE DESIGN INTENT THEY CONVEY, FOR PROBLEMS WHICH ARE CAUSED BY THE CONTRACTOR'S OWN DESIGN, CONSTRUCTION, OR OPERATION OF THE WORK. THE CONTRACTOR IS ADVISED TO FOLLOW THE ENGINEER'S GUIDANCE WITH RESPECT TO ANY ERRORS, OMISSIONS, INCONSISTENCIES, AMBIGUITIES OR CONFLICTS WHICH ARE ALLEGED.

CONTRACTOR TO VERIFY ALL DIMENSIONS AND NOTIFY THE ENGINEER OF ANY DISCREPANCIES BEFORE WORK COMMENCES. DO NOT SCALE DRAWINGS.

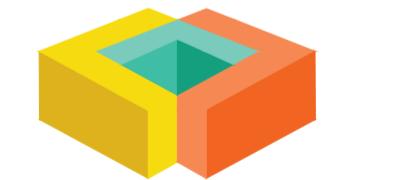
SCALE: 1:500



10	RE-ISSUED FOR SITE PLAN	K.H.	08 APR 2025
09	APPLICATION FOR SITE PLAN	K.H.	09 AUG 2024
08	RE-ISSUED FOR SITE PLAN	K.H.	09 MAY 2024
07	APPLICATION FOR SITE PLAN	K.H.	24 APR 2024
06	RE-ISSUED FOR SITE PLAN	K.H.	17 MAR 2023
05	APPLICATION FOR SITE PLAN	K.H.	31 OCT 2022
04	APPLICATION FOR SITE PLAN	K.H.	22 SEPT 2021
03	RE-ISSUED FOR SITE PLAN APPLICATION	K.H.	23 DEC 2020
02	ISSUED FOR CLIENT REVIEW	K.H.	11 DEC 2020
01	ISSUED FOR CLIENT APPROVAL	K.H.	11 MAR 2020
	REVISIONS	BY	DATE



NOT AUTHENTIC UNLESS SIGNED AND DATED



Engineering Ingénierie  
5430 Canotek Road | Ottawa, ON, K1J 9G2  
www.lrl.ca (613) 842-3434

CLIENT THE HINDU HERITAGE CENTRE OF OTTAWA CARLETON

DESIGNED BY: P.P. DRAWN BY: K.H. APPROVED BY: M.B.

PROJECT PROPOSED ASSEMBLY HALL 4835 BANK STREET, OTTAWA

DRAWING TITLE

EROSION AND SEDIMENT CONTROL PLAN

PROJECT NO. 170132

DATE JAN 2020

**APPENDIX J**  
**Domestic Water Demand Calculations**



## Water Service Calculations

**LRL File No. :** 170132  
**Project :** Hindu Heritage Centre  
**Date :** October 31, 2022  
**Designed by :** Kyle Herold

### Water Demand - Proposed Development

**Total fixture units:**  (as per OBC Table 7.6.3.2.A)

**Conversion of fixture units to equivalent gpm:**  gpm (as per PS&D)

**Average water demand** = 261647.52 L / day  
= 3.03 L/s

**Maximum daily peak factor:** 1.5

**Maximum daily demand** = 392471 L / day  
= 4.54 L / s

**Maximum hour peak factor:** 1.8

**Maximum hour demand** = 706448 L / day  
= 8.18 L / s

### Water Demand - Existing Building

**Total fixture units:**  (as per OBC Table 7.6.3.2.A)

**Conversion of fixture units to equivalent gpm:**  gpm (as per PS&D)

**Average water demand** = 168980.69 L / day  
= 1.96 L/s

**Maximum daily peak factor:** 1.5

**Maximum daily demand** = 253471 L / day  
= 2.93 L / s

**Maximum hour peak factor:** 1.8

**Maximum hour demand** = 456248 L / day  
= 5.28 L / s

### Total Water Demand

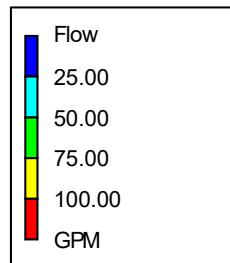
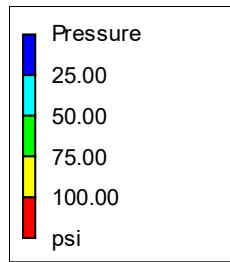
**Avg water demand** = 430628.21 L / day  
= 4.98 L / s

**Max daily demand** = 645942.3 L / day

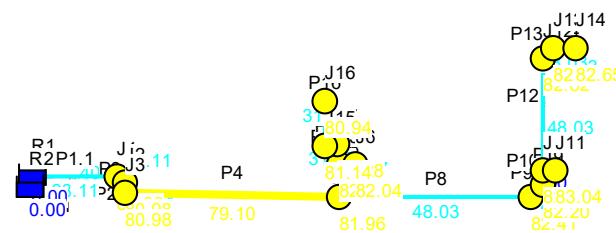
$$= 7.48 \text{ L/s}$$

**Max hour demand** = 1162696.2 L/day  
= 13.46 L/s

**Appendix K**  
**EPANET**  
**Hydraulic Analysis**



## Day 1, 1



## Scenario 1: Avg Day (Existing Conditions)

```
*****
*          E P A N E T
*          Hydraulic and Water Quality
*          Analysis for Pipe Networks
*          Version 2.2
*****
```

Input File: Scenario 1-Avg Day.net

Link - Node Table:

Link ID	Start Node	End Node	Length ft	Diameter in
P1	R2	J3	113.16	8
P2	J1	J2	8.2	8
P3	J2	J3	8.2	8
P4	J3	J4	252.6	8
P5	J4	J5	37.06	6
P6	J5	J6	16.4	6
P7	J5	J7	24.93	6
P8	J4	J8	227.96	8
P9	J8	J9	18.04	8
P10	J9	J10	20.34	8
P11	J10	J11	14.1	6
P12	J10	J12	155.47	6
P13	J12	J13	16.07	6
P14	J13	J14	28.21	6
P1.1	R1	J1	113.16	8
P15	J7	J15	16.73	2
P16	J15	J16	52.81	2

Node Results:

Node ID	Demand GPM	Head ft	Pressure psi	Quality
J1	0.00	507.08	80.98	0.00
J2	0.00	507.08	80.98	0.00
J3	0.00	507.08	80.98	0.00
J4	0.00	507.05	81.96	0.00
J5	0.00	507.05	82.04	0.00
J6	0.00	507.05	82.04	0.00
J7	0.00	507.05	81.28	0.00
J8	0.00	507.04	82.41	0.00
J9	0.00	507.04	82.20	0.00
J10	0.00	507.04	82.69	0.00
J11	0.00	507.04	83.04	0.00
J12	0.00	507.01	82.82	0.00
J13	0.00	507.00	82.89	0.00
J14	48.03	507.00	82.65	0.00

Page 2

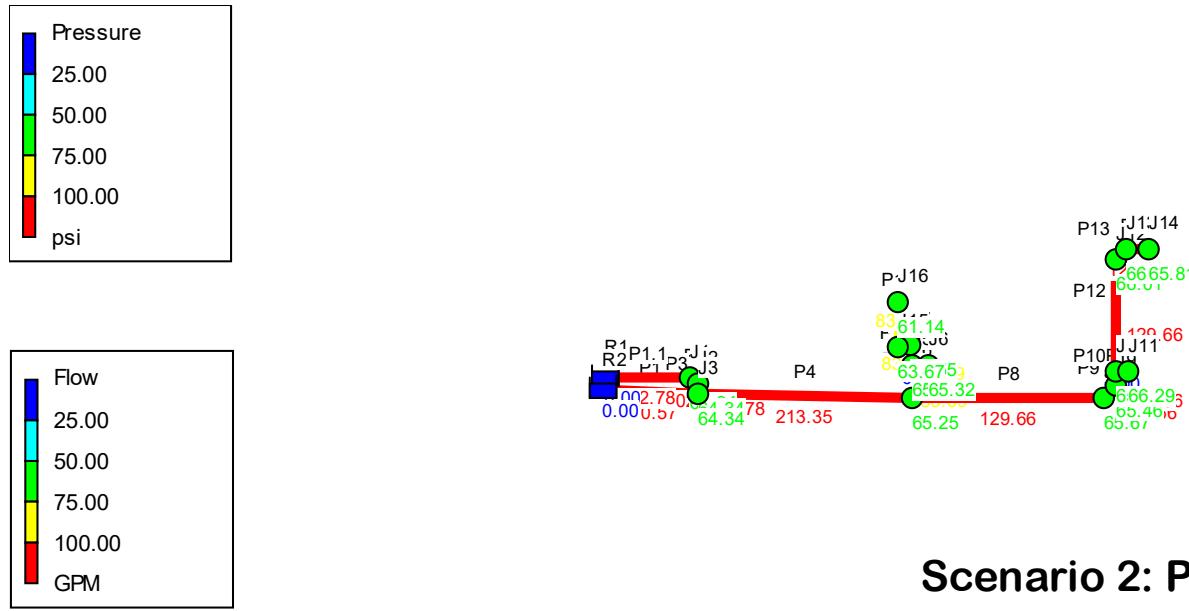
Node Results: (continued)

Node ID	Demand GPM	Head ft	Pressure psi	Quality
J15	0.00	506.72	81.14	0.00
J16	31.07	505.70	80.94	0.00
R1	-38.11	507.09	0.00	0.00 Reservoir
R2	-40.99	507.09	0.00	0.00 Reservoir

Link Results:

Link ID	Flow GPM	Velocity fps	Unit Headloss ft/Kft	Status
P1	40.99	0.26	0.04	Open
P2	38.11	0.24	0.03	Open
P3	38.11	0.24	0.03	Open
P4	79.10	0.50	0.13	Open
P5	31.07	0.35	0.09	Open
P6	0.00	0.00	0.00	Open
P7	31.07	0.35	0.09	Open
P8	48.03	0.31	0.05	Open
P9	48.03	0.31	0.05	Open
P10	48.03	0.31	0.05	Open
P11	0.00	0.00	0.00	Open
P12	48.03	0.55	0.21	Open
P13	48.03	0.55	0.21	Open
P14	48.03	0.55	0.21	Open
P1.1	38.11	0.24	0.03	Open
P15	31.07	3.17	19.36	Open
P16	31.07	3.17	19.36	Open

Day 1, 1



## Scenario 2: Peak Hour (Existing Conditions)

```
*****
*          E P A N E T
*          Hydraulic and Water Quality
*          Analysis for Pipe Networks
*          Version 2.2
*****
```

Input File: Scenario 2-Peak Hour.net

Link - Node Table:

Link ID	Start Node	End Node	Length ft	Diameter in
P1	R2	J3	113.16	8
P2	J1	J2	8.2	8
P3	J2	J3	8.2	8
P4	J3	J4	252.6	8
P5	J4	J5	37.06	6
P6	J5	J6	16.4	6
P7	J5	J7	24.93	6
P8	J4	J8	227.96	8
P9	J8	J9	18.04	8
P10	J9	J10	20.34	8
P11	J10	J11	14.1	6
P12	J10	J12	155.47	6
P13	J12	J13	16.07	6
P14	J13	J14	28.21	6
P1.1	R1	J1	113.16	8
P15	J7	J15	16.73	2
P16	J15	J16	52.81	2

Node Results:

Node ID	Demand GPM	Head ft	Pressure psi	Quality
J1	0.00	468.69	64.34	0.00
J2	0.00	468.69	64.34	0.00
J3	0.00	468.69	64.34	0.00
J4	0.00	468.48	65.25	0.00
J5	0.00	468.46	65.32	0.00
J6	0.00	468.46	65.32	0.00
J7	0.00	468.45	64.55	0.00
J8	0.00	468.41	65.67	0.00
J9	0.00	468.40	65.46	0.00
J10	0.00	468.40	65.95	0.00
J11	0.00	468.40	66.29	0.00
J12	0.00	468.20	66.01	0.00
J13	0.00	468.18	66.07	0.00
J14	129.66	468.14	65.81	0.00

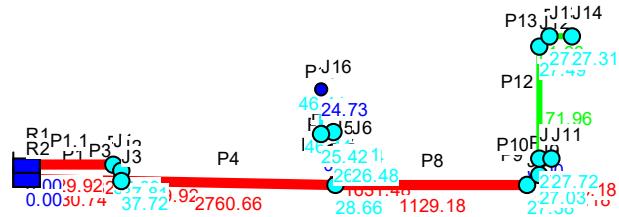
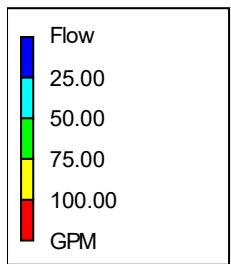
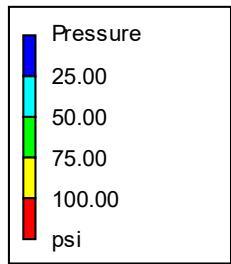
Page 2

Node Results: (continued)

Node ID	Demand GPM	Head ft	Pressure psi	Quality
J15	0.00	466.42	63.67	0.00
J16	83.69	460.01	61.14	0.00
R1	-102.78	468.71	0.00	0.00 Reservoir
R2	-110.57	468.71	0.00	0.00 Reservoir

Link Results:

Link ID	Flow GPM	Velocity fps	Unit Headloss ft/Kft	Status
P1	110.57	0.71	0.24	Open
P2	102.78	0.66	0.21	Open
P3	102.78	0.66	0.20	Open
P4	213.35	1.36	0.80	Open
P5	83.69	0.95	0.58	Open
P6	0.00	0.00	0.00	Open
P7	83.69	0.95	0.58	Open
P8	129.66	0.83	0.32	Open
P9	129.66	0.83	0.32	Open
P10	129.66	0.83	0.32	Open
P11	0.00	0.00	0.00	Open
P12	129.66	1.47	1.29	Open
P13	129.66	1.47	1.30	Open
P14	129.66	1.47	1.29	Open
P1.1	102.78	0.66	0.21	Open
P15	83.69	8.55	121.33	Open
P16	83.69	8.55	121.33	Open



Day 1, 1

### Scenario 3: Max Day + Fire Flow (Existing Conditions)

```
*****
*          E P A N E T
*          Hydraulic and Water Quality
*          Analysis for Pipe Networks
*          Version 2.2
*****
```

Input File: Scenario 3-Avg Day+Fire.net

Link - Node Table:

Link ID	Start Node	End Node	Length ft	Diameter in
P1	R2	J3	113.16	8
P2	J1	J2	8.2	8
P3	J2	J3	8.2	8
P4	J3	J4	252.6	8
P5	J4	J5	37.06	6
P6	J5	J6	16.4	6
P7	J5	J7	24.93	6
P8	J4	J8	227.96	8
P9	J8	J9	18.04	8
P10	J9	J10	20.34	8
P11	J10	J11	14.1	6
P12	J10	J12	155.47	6
P13	J12	J13	16.07	6
P14	J13	J14	28.21	6
P1.1	R1	J1	113.16	8
P15	J7	J15	16.73	2
P16	J15	J16	52.81	2

Node Results:

Node ID	Demand GPM	Head ft	Pressure psi	Quality
J1	0.00	407.64	37.89	0.00
J2	0.00	407.45	37.81	0.00
J3	0.00	407.25	37.72	0.00
J4	0.00	384.04	28.66	0.00
J5	1585.04	378.82	26.48	0.00
J6	0.00	378.82	26.48	0.00
J7	0.00	378.81	25.71	0.00
J8	0.00	380.04	27.38	0.00
J9	0.00	379.72	27.03	0.00
J10	1057.22	379.36	27.37	0.00
J11	0.00	379.36	27.72	0.00
J12	0.00	379.30	27.49	0.00
J13	0.00	379.29	27.55	0.00
J14	71.96	379.28	27.31	0.00

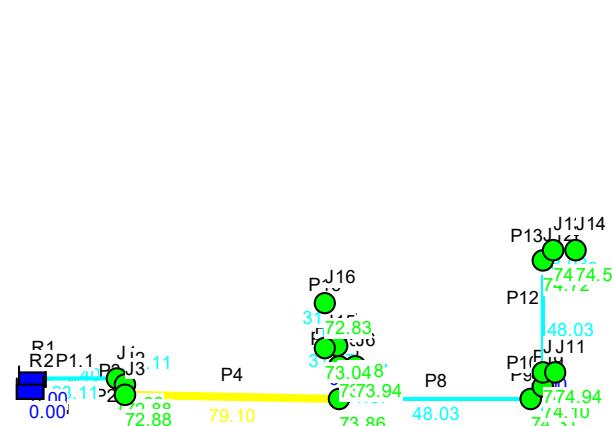
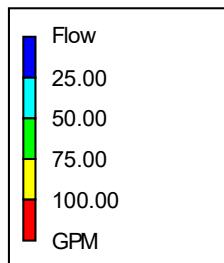
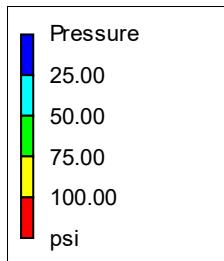
Page 2

Node Results: (continued)

Node ID	Demand GPM	Head ft	Pressure psi	Quality
J15	0.00	378.13	25.42	0.00
J16	46.44	375.98	24.73	0.00
R1	-1329.92	410.33	0.00	0.00 Reservoir
R2	-1430.74	410.33	0.00	0.00 Reservoir

Link Results:

Link ID	Flow GPM	Velocity fps	Unit Headloss ft/Kft	Status
P1	1430.74	9.13	27.20	Open
P2	1329.92	8.49	23.76	Open
P3	1329.92	8.49	23.76	Open
P4	2760.66	17.62	91.90	Open
P5	1631.48	18.51	140.87	Open
P6	0.00	0.00	0.00	Open
P7	46.44	0.53	0.19	Open
P8	1129.18	7.21	17.55	Open
P9	1129.18	7.21	17.55	Open
P10	1129.18	7.21	17.55	Open
P11	0.00	0.00	0.00	Open
P12	71.96	0.82	0.43	Open
P13	71.96	0.82	0.43	Open
P14	71.96	0.82	0.43	Open
P1.1	1329.92	8.49	23.76	Open
P15	46.44	4.74	40.76	Open
P16	46.44	4.74	40.76	Open



## Scenario 1: Avg Day (SUC Zone Reconfiguration)

```
*****
*          E P A N E T
*          Hydraulic and Water Quality
*          Analysis for Pipe Networks
*          Version 2.2
*****
```

Input File: Scenario 1-Avg Day\_SUC.net

Link - Node Table:

Link ID	Start Node	End Node	Length ft	Diameter in
P1	R2	J3	113.16	8
P2	J1	J2	8.2	8
P3	J2	J3	8.2	8
P4	J3	J4	252.6	8
P5	J4	J5	37.06	6
P6	J5	J6	16.4	6
P7	J5	J7	24.93	6
P8	J4	J8	227.96	8
P9	J8	J9	18.04	8
P10	J9	J10	20.34	8
P11	J10	J11	14.1	6
P12	J10	J12	155.47	6
P13	J12	J13	16.07	6
P14	J13	J14	28.21	6
P1.1	R1	J1	113.16	8
P15	J7	J15	16.73	2
P16	J15	J16	52.81	2

Node Results:

Node ID	Demand GPM	Head ft	Pressure psi	Quality
J1	0.00	488.39	72.88	0.00
J2	0.00	488.39	72.88	0.00
J3	0.00	488.39	72.88	0.00
J4	0.00	488.36	73.86	0.00
J5	0.00	488.35	73.94	0.00
J6	0.00	488.35	73.94	0.00
J7	0.00	488.35	73.18	0.00
J8	0.00	488.34	74.31	0.00
J9	0.00	488.34	74.10	0.00
J10	0.00	488.34	74.59	0.00
J11	0.00	488.34	74.94	0.00
J12	0.00	488.31	74.72	0.00
J13	0.00	488.31	74.79	0.00
J14	48.03	488.30	74.55	0.00

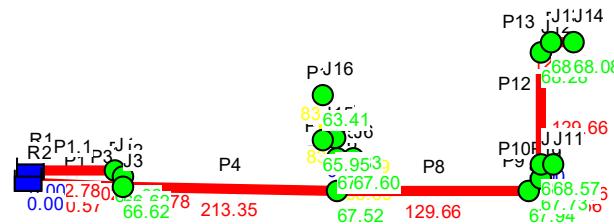
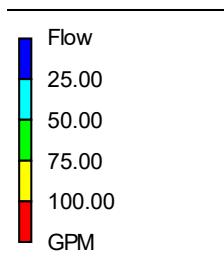
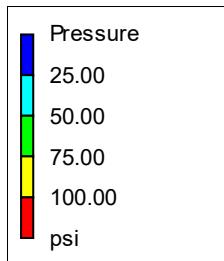
Page 2

Node Results: (continued)

Node ID	Demand GPM	Head ft	Pressure psi	Quality
J15	0.00	488.03	73.04	0.00
J16	31.07	487.00	72.83	0.00
R1	-38.11	488.39	0.00	0.00 Reservoir
R2	-40.99	488.39	0.00	0.00 Reservoir

Link Results:

Link ID	Flow GPM	Velocity fps	Unit Headloss ft/Kft	Status
P1	40.99	0.26	0.04	Open
P2	38.11	0.24	0.03	Open
P3	38.11	0.24	0.03	Open
P4	79.10	0.50	0.13	Open
P5	31.07	0.35	0.09	Open
P6	0.00	0.00	0.00	Open
P7	31.07	0.35	0.09	Open
P8	48.03	0.31	0.05	Open
P9	48.03	0.31	0.05	Open
P10	48.03	0.31	0.05	Open
P11	0.00	0.00	0.00	Open
P12	48.03	0.55	0.21	Open
P13	48.03	0.55	0.21	Open
P14	48.03	0.55	0.21	Open
P1.1	38.11	0.24	0.03	Open
P15	31.07	3.17	19.36	Open
P16	31.07	3.17	19.36	Open



## Scenario 2: Peak Hour (SUC Zone Reconfiguration)

```
*****
*          E P A N E T
*          Hydraulic and Water Quality
*          Analysis for Pipe Networks
*          Version 2.2
*****
```

Input File: Scenario 2-Peak Hour\_SUC.net

Link - Node Table:

Link ID	Start Node	End Node	Length ft	Diameter in
P1	R2	J3	113.16	8
P2	J1	J2	8.2	8
P3	J2	J3	8.2	8
P4	J3	J4	252.6	8
P5	J4	J5	37.06	6
P6	J5	J6	16.4	6
P7	J5	J7	24.93	6
P8	J4	J8	227.96	8
P9	J8	J9	18.04	8
P10	J9	J10	20.34	8
P11	J10	J11	14.1	6
P12	J10	J12	155.47	6
P13	J12	J13	16.07	6
P14	J13	J14	28.21	6
P1.1	R1	J1	113.16	8
P15	J7	J15	16.73	2
P16	J15	J16	52.81	2

Node Results:

Node ID	Demand GPM	Head ft	Pressure psi	Quality
J1	0.00	473.94	66.62	0.00
J2	0.00	473.93	66.62	0.00
J3	0.00	473.93	66.62	0.00
J4	0.00	473.73	67.52	0.00
J5	0.00	473.71	67.60	0.00
J6	0.00	473.71	67.60	0.00
J7	0.00	473.69	66.83	0.00
J8	0.00	473.66	67.94	0.00
J9	0.00	473.65	67.73	0.00
J10	0.00	473.65	68.23	0.00
J11	0.00	473.65	68.57	0.00
J12	0.00	473.44	68.28	0.00
J13	0.00	473.42	68.34	0.00
J14	129.66	473.39	68.08	0.00

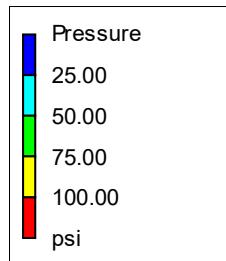
Page 2

Node Results: (continued)

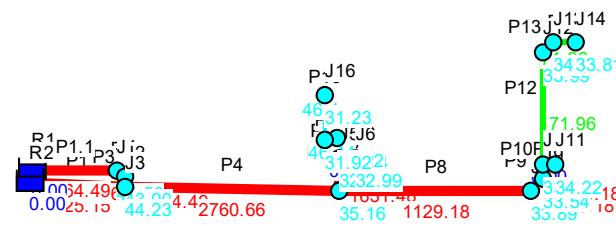
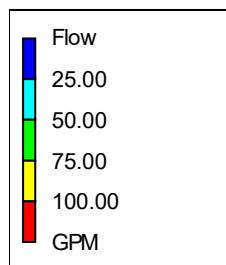
Node ID	Demand GPM	Head ft	Pressure psi	Quality
J15	0.00	471.67	65.95	0.00
J16	83.69	465.26	63.41	0.00
R1	-102.78	473.96	0.00	0.00 Reservoir
R2	-110.57	473.96	0.00	0.00 Reservoir

Link Results:

Link ID	Flow GPM	Velocity fps	Unit Headloss ft/Kft	Status
P1	110.57	0.71	0.24	Open
P2	102.78	0.66	0.21	Open
P3	102.78	0.66	0.21	Open
P4	213.35	1.36	0.80	Open
P5	83.69	0.95	0.58	Open
P6	0.00	0.00	0.00	Open
P7	83.69	0.95	0.58	Open
P8	129.66	0.83	0.32	Open
P9	129.66	0.83	0.32	Open
P10	129.66	0.83	0.32	Open
P11	0.00	0.00	0.00	Open
P12	129.66	1.47	1.29	Open
P13	129.66	1.47	1.29	Open
P14	129.66	1.47	1.29	Open
P1.1	102.78	0.66	0.21	Open
P15	83.69	8.55	121.33	Open
P16	83.69	8.55	121.33	Open



Day 1, 1



## Scenario 3: Max Day + Fire Flow (SUC Zone Reconfiguration)

```
*****
*          E P A N E T
*          Hydraulic and Water Quality
*          Analysis for Pipe Networks
*          Version 2.2
*****
```

Input File: Scenario 3-Max Day+Fire\_SUC Zone.net

Link - Node Table:

Link ID	Start Node	End Node	Length ft	Diameter in
P1	R2	J3	113.16	8
P2	J1	J2	8.2	8
P3	J2	J3	8.2	8
P4	J3	J4	252.6	8
P5	J4	J5	37.06	6
P6	J5	J6	16.4	6
P7	J5	J7	24.93	6
P8	J4	J8	227.96	8
P9	J8	J9	18.04	8
P10	J9	J10	20.34	8
P11	J10	J11	14.1	6
P12	J10	J12	155.47	6
P13	J12	J13	16.07	6
P14	J13	J14	28.21	6
P1.1	R1	J1	113.16	8
P15	J7	J15	16.73	2
P16	J15	J16	52.81	2

Node Results:

Node ID	Demand GPM	Head ft	Pressure psi	Quality
J1	0.00	420.76	43.58	0.00
J2	0.00	421.51	43.90	0.00
J3	0.00	422.27	44.23	0.00
J4	0.00	399.05	35.16	0.00
J5	1585.04	393.83	32.99	0.00
J6	0.00	393.83	32.99	0.00
J7	0.00	393.83	32.22	0.00
J8	0.00	395.05	33.89	0.00
J9	0.00	394.74	33.54	0.00
J10	1057.22	394.38	33.88	0.00
J11	0.00	394.38	34.22	0.00
J12	0.00	394.31	33.99	0.00
J13	0.00	394.30	34.06	0.00
J14	71.96	394.29	33.81	0.00

Page 2

Node Results: (continued)

Node ID	Demand GPM	Head ft	Pressure psi	Quality
J15	0.00	393.15	31.92	0.00
J16	46.44	390.99	31.23	0.00
R1	2764.49	410.33	0.00	0.00 Reservoir
R2	-5525.15	459.86	0.00	0.00 Reservoir

Link Results:

Link ID	Flow GPM	Velocity fps	Unit Headloss ft/Kft	Status
P1	5525.15	35.27	332.18	Open
P2	-2764.49	17.65	92.14	Open
P3	-2764.49	17.65	92.13	Open
P4	2760.66	17.62	91.90	Open
P5	1631.48	18.51	140.87	Open
P6	0.00	0.00	0.00	Open
P7	46.44	0.53	0.19	Open
P8	1129.18	7.21	17.55	Open
P9	1129.18	7.21	17.55	Open
P10	1129.18	7.21	17.55	Open
P11	0.00	0.00	0.00	Open
P12	71.96	0.82	0.43	Open
P13	71.96	0.82	0.43	Open
P14	71.96	0.82	0.43	Open
P1.1	-2764.49	17.65	92.13	Open
P15	46.44	4.74	40.76	Open
P16	46.44	4.74	40.76	Open

**APPENDIX L**  
**FUS Fire Flow Calculations**



## Fire Flow Calculations - Proposed Building

LRL File No. 170132  
 Project Hindu Heritage Centre  
 Date October 31, 2022  
 Method Fire Underwriters Survey (FUS)  
 Designed by Philippe Paquette, C.E.T.

Step	Task	Term	Options	Multiplier	Choose:	Value	unit	Fire Flow
<b>Structural Framing Material</b>								
1	Choose frame used for building	Coefficient C related to the type of construction	Wood Frame	1.5	Non-combustible construction	0.8		
			Ordinary Construction	1.0				
			Non-combustible construction	0.8				
			Fire resistive construction <2 hrs	0.7				
			Fire resistive construction >2 hrs	0.6				
<b>Floor Space Area</b>								
2	Choose type of housing	Type of housing	Single family dwelling	0	Building - no. of units per floor	1	unit(s)	
			Townhouse - no. of units	0				
			Building - no. of units per floor	1				
3	Enter area of a unit	Enter floor space area of one unit (excluding basement)		1	1576.0		sq.m.	
4	Obtain fire flow before reductions	Required fire flow	$Fire Flow = 220 \times C \times Area^{0.5}$					L/min 7,000
								L/s 116.7
<b>Reductions or surcharge due to factors affecting burning</b>								
5	Choose combustibility of contents	Occupancy hazard reduction or surcharge	Non-combustible	-0.25	Combustible	0		
			Limited combustible	-0.15				
			Combustible	0				
			Free burning	0.15			L/min 7,000	
			Rapid burning	0.25				
6	Choose reduction for sprinklers	Sprinkler reduction	Sprinklers (NFPA13)	-0.30	True	-0.3		
			Water supply is standard for both the system and fire department hose lines	-0.10	True	-0.1	L/min 3,500	
			Fully supervised system	-0.10	True	-0.1	L/s 58.3	
7	Choose separation	Exposure distance between units	North side	Over 45m	0			
			East side	Over 45m	0			
			South side	Over 45m	0		L/min 4,000	
			West side	Over 45m	0	0	L/s 66.7	
<b>Net required fire flow</b>								
8	Obtain fire flow, duration, and volume							Minimum required fire flow rate (rounded to nearest 1000) L/min 4,000
								Minimum required fire flow rate L/s 66.7
								Required duration of fire flow hr 1.5



## Fire Flow Calculations - Existing Building

LRL File No. 170132  
 Project Hindu Heritage Centre  
 Date October 31, 2022  
 Method Fire Underwriters Survey (FUS)  
 Designed by Philippe Paquette, C.E.T.

Step	Task	Term	Options	Multiplier	Choose:	Value	unit	Fire Flow
<b>Structural Framing Material</b>								
1	Choose frame used for building	Coefficient C related to the type of construction	Wood Frame	1.5	Non-combustible construction	0.8		
			Ordinary Construction	1.0				
			Non-combustible construction	0.8				
			Fire resistive construction <2 hrs	0.7				
			Fire resistive construction >2 hrs	0.6				
<b>Floor Space Area</b>								
2	Choose type of housing	Type of housing	Single family dwelling	0	Building - no. of units per floor	1	unit(s)	
			Townhouse - no. of units	0				
			Building - no. of units per floor	1				
3	Enter area of a unit	Enter floor space area of one unit (excluding basement)		1	1062.0		sq.m.	
4	Obtain fire flow before reductions	Required fire flow	$Fire\ Flow = 220 \times C \times Area^{0.5}$					L/min <b>6,000</b>
								L/s <b>100.0</b>
<b>Reductions or surcharge due to factors affecting burning</b>								
5	Choose combustibility of contents	Occupancy hazard reduction or surcharge	Non-combustible	-0.25	Limited combustible	-0.15		
			Limited combustible	-0.15				
			Combustible	0				
			Free burning	0.15				
			Rapid burning	0.25				
6	Choose reduction for sprinklers	Sprinkler reduction	Sprinklers (NFPA13)	-0.30	False	0		
			Water supply is standard for both the system and fire department hose lines	-0.10	False	0	L/min	<b>6,000</b>
			Fully supervised system	-0.10	False	0	L/s	100.0
7	Choose separation	Exposure distance between units	North side	Over 45m	0			
			East side	Over 45m	0			
			South side	Over 45m	0		L/min	<b>6,000</b>
			West side	Over 45m	0	0	L/s	100.0
<b>Net required fire flow</b>								
8	Obtain fire flow, duration, and volume							Minimum required fire flow rate (rounded to nearest 1000) L/min <b>6,000</b>
								Minimum required fire flow rate L/s <b>100.0</b>
								Required duration of fire flow hr <b>2.0</b>

**APPENDIX M**  
**City of Ottawa Boundary Calculations**

## Boundary Conditions 4835 Bank Street

### Provided Information

Scenario	Demand	
	L/min	L/s
Average Daily Demand	299	4.98
Maximum Daily Demand	449	7.48
Peak Hour	808	13.46
Fire Flow Demand #1	10,000	166.67

### Location



### Results – Existing Conditions

#### Connection 1 – Bank St.

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	154.6	79.3
Peak Hour	142.9	62.7
Max Day plus Fire 1	125.1	37.4

Ground Elevation = 98.8 m

## **Results – SUC Zone Reconfiguration**

### **Connection 1 – Bank St.**

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	148.9	71.2
Peak Hour	144.5	65.0
Max Day plus Fire 1	140.2	59.0

Ground Elevation = 98.8 m

### **Notes**

1. A second connection to the watermain, separated by an isolation valve, is required to decrease vulnerability of the water system in case of breaks.

### **Disclaimer**

*The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation. Fire Flow analysis is a reflection of available flow in the watermain; there may be additional restrictions that occur between the watermain and the hydrant that the model cannot take into account.*

**APPENDIX N**  
**1/5 Year & 1/100 Year SWM Storage Tables**

LR Associates Ltd.  
Storm Watershed Summary



**LRL File No.** 170132-10  
**Project:** Hindu Heritage Centre  
**Location:** 4835 Bank Street, Ottawa  
**Date:** April 8, 2025  
**Designed:** K. Herold  
**Checked:** M. Basnet  
**Drawing Reference:** C.701, C.702

**Pre-Development Catchments**

WATERSHED	C = 0.20	C = 0.8	C = 0.90	Total Area (ha)	Combined C
EWS-01	1.298	0.000	0.819	2.117	0.47
<b>TOTAL</b>	<b>1.298</b>	<b>0.000</b>	<b>0.819</b>	<b>2.117</b>	<b>0.47</b>

**Post-Development Catchments**

WATERSHED	C = 0.20	C = 0.8	C = 0.90	Total Area (ha)	Combined C
WS-01 (CONTROLLED)	0.571	0.023	0.618	1.212	0.57
<b>TOTAL CONTROL</b>	<b>0.571</b>	<b>0.023</b>	<b>0.618</b>	<b>1.212</b>	<b>0.57</b>
WS-02 (UNCONTROLLED)	0.112	0.000	0.299	0.411	0.71
WS-03 (UNCONTROLLED)	0.454	0.000	0.016	0.470	0.22
WS-04 (UNCONTROLLED)	0.024	0.000	0.000	0.024	0.20
<b>TOTAL UNCONTROLLED</b>	<b>0.590</b>	<b>0.000</b>	<b>0.315</b>	<b>0.905</b>	<b>0.44</b>
<b>TOTAL</b>	<b>1.161</b>	<b>0.023</b>	<b>0.933</b>	<b>2.117</b>	<b>0.52</b>



**LRL File No.** 170132-10  
**Project:** Hindu Heritage Centre  
**Location:** 4835 Bank Street, Ottawa  
**Date:** April 8, 2025  
**Designed:** K. Herold  
**Checked:** M. Basnet  
**Drawing Ref.:** C.401

Stormwater Management  
Design Sheet

**STORM - 100 YEAR**

**Runoff Equation**

$Q = 2.78CIA$  (L/s)  
 $C$  = Runoff coefficient  
 $I$  = Rainfall intensity (mm/hr) =  $A / (Td + C)^B$   
 $A$  = Area (ha)  
 $T_c$  = Time of concentration (min)

**Pre-Development Catchments within Development Area**

	Total Area =	2.117	ha	$\Sigma R_5$ =	0.47
Un-Controlled	EWS-01	2.117	ha	$\Sigma R_5$ =	0.47
	Total Uncontrolled =	2.117	ha	$\Sigma R_5$ =	0.47

**Allowable Release Rate (Max C=0.5, 5-year Pre-Dev FR)**

5 Year Pre-Development Flow Rate

$$I_5 = 998.071 / (Td + 6.053)^{0.814} \quad a = 998.071 \quad b = 0.814 \quad C = 6.053$$

$C = 0.47$  the smaller of 0.5 or the actual existing as per the City of Ottawa  
 $I = 104.2$  mm/hr  
 $T_c = 10$  min  
 $Total = 2.117$  ha  
**Allowable Release Rate=** 288.68 L/s  
**Controlled Release Rate=** 39.50 L/s

**Post-development Stormwater Management**

			$\Sigma R_5$	$\Sigma R_{100}$
	Total Site Area =	2.117	ha	$\Sigma R_5$ = 0.52 0.64
Controlled	Total Controlled =	1.212	ha	$\Sigma R_5$ = 0.57 0.71
Un-controlled	Total Un-Controlled =	0.905	ha	$\Sigma R_5$ = 0.44 0.55

**Post-development Stormwater Management**

$$I_{100} = 1735.688 / (Td + 6.014)^{0.820} \quad a = 1735.688 \quad b = 0.82 \quad C = 6.014$$

Time (min)	Intensity (mm/hr)	Controlled Runoff** (L/s)	Storage Volume* (m <sup>3</sup> )	Controlled Release Rate (L/s)	Halved Controlled Release Rate (L/s)	Uncontrolled Runoff (L/s)	Total Release Rate (L/s)
10	178.6	427.40	244.59	39.50	19.75	249.13	288.63
15	142.9	342.03	290.05	39.50	19.75	199.37	238.87
20	120.0	287.11	320.83	39.50	19.75	167.36	206.86
30	91.9	219.89	360.26	39.50	19.75	128.18	167.68
45	69.1	165.28	392.92	39.50	19.75	96.34	135.84
60	55.9	133.79	410.54	39.50	19.75	77.98	117.48
75	47.3	113.11	420.12	39.50	19.75	65.93	105.43
90	41.1	98.40	424.72	39.50	19.75	57.36	96.86
120	32.9	78.74	424.70	39.50	19.75	45.90	85.40
150	27.6	66.09	417.05	39.50	19.75	38.52	78.02
180	23.9	57.21	404.60	39.50	19.75	33.35	72.85

\* for volume calculation, controlled release rate taken as half of the discharge rate of 39.50L/s



**LRL File No.** 170132-10  
**Project:** Hindu Heritage Centre  
**Location:** 4835 Bank Street, Ottawa  
**Date:** April 8, 2025  
**Designed:** K. Herold  
**Checked:** M. Basnet  
**Drawing Ref.:** C.401

Stormwater Management  
Design Sheet

**STORM - 100 YEAR**

**Onsite Stormwater Retention**

<b>Total Storage Required =</b>	<b>424.72 m<sup>3</sup></b>
Pipe Storage =	0.00 m <sup>3</sup>
CB/MH Storage =	0.00 m <sup>3</sup>
Underground Storage =	0.00 m <sup>3</sup>
Surface/Detention Area Storage =	428.14 m <sup>3</sup>
<b>Total Available Storage =</b>	<b>428.14 m<sup>3</sup></b>

refer to LRL Plans C301 & C601



LRL File No. 170132-10  
 Project: Hindu Heritage Centre  
 Location: 4835 Bank Street, Ottawa  
 Date: April 8, 2025  
 Designed: K. Herold  
 Checked: M. Basnet  
 Drawing Ref.: C.401

Stormwater Management  
Design Sheet

#### STORM - 5 YEAR

##### Runoff Equation

$$Q = 2.78CIA \text{ (L/s)}$$

C = Runoff coefficient

$$I = \text{Rainfall intensity (mm/hr)} = A / (Td + C)^B$$

A = Area (ha)

T<sub>c</sub> = Time of concentration (min)

##### Pre-Development Catchments within Development Area

	Total Area =	2.117	ha	$\Sigma R_5 =$	0.47
Un-Controlled	EWS-01	2.117	ha	$R_5 =$	0.47
	Total Uncontrolled =	2.117	ha	$\Sigma R_{100} =$	0.47

##### Allowable Release Rate (Max C=0.5, 5-year Pre-Dev FR)

5 Year Pre-Development Flow Rate

$$I_5 = 998.071 / (Td + 6.053)^{0.814}$$

a = 998.071

b = 0.814

C = 6.053

C =	0.47	the smaller of 0.5 or the actual existing as per the City of Ottawa
I =	104.2	mm/hr
T <sub>c</sub> =	10	min
Total =	2.117	ha
Allowable Release Rates =	288.68	L/s
Controlled Release Rate =	28.00	L/s

##### Post-Development Stormwater Management (Storage Calculations)

	Total Site Area =	2.117	ha	$\Sigma R_5 =$	0.52	$\Sigma R_{100} =$
Controlled	Total Controlled =	1.212	ha	$\Sigma R_5 =$	0.57	0.71
Un-controlled	Total Un-Controlled =	0.905	ha	$\Sigma R_{100} =$	0.44	0.55

##### Post-development Stormwater Management

$$I_5 = 998.071 / (Td + 6.053)^{0.814}$$

a = 998.071

b = 0.814

C = 6.053

Time (min)	Intensity (mm/hr)	Controlled Runoff** (L/s)	Storage Volume* (m <sup>3</sup> )	Controlled Release Rate* (L/s)	Halved Controlled Release Rate (L/s)	Uncontrolled Runoff (L/s)	Total Release Rate (L/s)
5	141.2	270.34	76.90	28.00	14.00	157.58	171.58
10	104.2	199.52	111.31	28.00	14.00	116.30	130.30
15	83.6	160.00	131.40	28.00	14.00	93.26	107.26
20	70.3	134.52	144.63	28.00	14.00	78.41	92.41
30	53.9	103.26	160.68	28.00	14.00	60.19	74.19
35	48.5	92.90	165.70	28.00	14.00	54.15	68.15
40	44.2	84.61	169.46	28.00	14.00	49.32	63.32
45	40.6	77.80	172.26	28.00	14.00	45.35	59.35
50	37.7	72.10	174.30	28.00	14.00	42.03	56.03
60	32.9	63.08	176.70	28.00	14.00	36.77	50.77
70	29.4	56.24	177.42	28.00	14.00	32.78	46.78
80	26.6	50.86	176.94	28.00	14.00	29.65	43.65
90	24.3	46.51	175.55	28.00	14.00	27.11	41.11

\* for volume calculation, controlled release rate taken as half of the discharge rate of 28.00L/s



**LRL File No.** 170132-10  
**Project:** Hindu Heritage Centre  
**Location:** 4835 Bank Street, Ottawa  
**Date:** April 8, 2025  
**Designed:** K. Herold  
**Checked:** M. Basnet  
**Drawing Ref.:** C.401

Stormwater Management  
Design Sheet

**STORM - 5 YEAR**

**Onsite Stormwater Retention**

<b>Total Storage Required =</b>	<b>177.42 m<sup>3</sup></b>
Pipe Storage =	0.00 m <sup>3</sup>
CB/MH Storage =	0.00 m <sup>3</sup>
Underground Storage =	0.00 m <sup>3</sup>
Surface/Detention Area Storage =	210.92 m <sup>3</sup>
<b>Total Available Storage =</b>	<b>210.92 m<sup>3</sup></b>

refer to LRL Plans C301 & C601

**LRL Associates Ltd.**  
Storm Design Sheet

 <p><b>LRL File No.</b> 170132-10  <b>Project:</b> Hindu Heritage Centre  <b>Location:</b> 4835 Bank Street, Ottawa  <b>Date:</b> April 8, 2025  <b>Designed:</b> K. Herold  <b>Checked:</b> M. Basnet  <b>Drawing Reference:</b> C.401</p>	<p>Rational Method      <math>Q = 2.78CIA</math></p> <p><math>Q</math> = Peak flow in litres per second (L/s)  <math>A</math> = Drainage area in hectares (ha)  <math>C</math> = Runoff coefficient  <math>I</math> = Rainfall intensity (mm/hr)</p>	<p><b>Storm Design Parameters</b></p> <table> <tr> <td>Runoff Coefficient (C)</td> <td></td> </tr> <tr> <td>Grass</td> <td>0.20</td> </tr> <tr> <td>Gravel</td> <td>0.80</td> </tr> <tr> <td>Asphalt / rooftop</td> <td>0.90</td> </tr> </table>	Runoff Coefficient (C)		Grass	0.20	Gravel	0.80	Asphalt / rooftop	0.90	<p>Ottawa Macdonald-Cartier International Airport IDF curve equation (5 year event, intensity in mm/hr)  <math>I = 998.071 / (T_c + 6.053)^{0.814}</math>  Min. velocity = 0.80 m/s  Manning's "n" = 0.013</p>
Runoff Coefficient (C)											
Grass	0.20										
Gravel	0.80										
Asphalt / rooftop	0.90										

LOCATION			AREA (ha)			FLOW						STORM SEWER								MANHOLE							
WATERSHED / STREET	From MH	To MH	C = 0.20	C = 0.80	C = 0.90	Indiv. 2.78AC	Accum. 2.78AC	Time of Conc. (min.)	Rainfall Intensity (mm/hr)	Peak Flow Q (l/s)	Pipe Diameter (mm)	Type	Slope (%)	Length (m)	Capacity Full (L/s)	Velocity Full (m/s)	Time of Flow (min.)	Ratio (Q/Q <sub>FULL</sub> )	Up Invert (m)	Down Invert (m)	T/G Up Stream	T/G Down Stream	Up Depth obv (m)	Down Depth obv (m)	Up Depth inv (m)		
<b>STORMWATER DETENTION AREA OUTLET</b>																											
WS-01	/	CB02	0.571	0.023	0.722	2.18	2.18	15.00	83.56	181.74	450	PVC	0.60%	2.6	220.84	1.39	0.03	<b>0.82</b>									
<b>UPSTREAM CULVERT, SW ENT. TO PARKING LOT</b>																											
WS-01 (PARTIAL)*	DET. AREA	0.301	0.003	0.226	0.74	0.74	15.00	83.56	61.79	500	CSP	0.50%	20.0	267.00	1.36	0.25	<b>0.23</b>										
<b>DOWNSTREAM CULVERT, SE ENT. TO PARKING LOT</b>																											
WS-01 (PARTIAL)**	DET. AREA	0.370	0.011	0.577	1.67	1.67	15.00	83.56	139.86	500	CSP	0.50%	14.0	267.00	1.36	0.17	<b>0.52</b>										

Note: The Peak flow controlled by the orifice plates are shown in this design sheet.

\*REFER TO CIVIL PLAN C301 & C401

\*design takes into consideration existing building, existing asphalt entrance and grass area south of existing building

\*\*design takes into consideration existing building, existing asphalt entrance, grass area south of existing building, south half of existing parking lot, proposed entrances and existing ditch

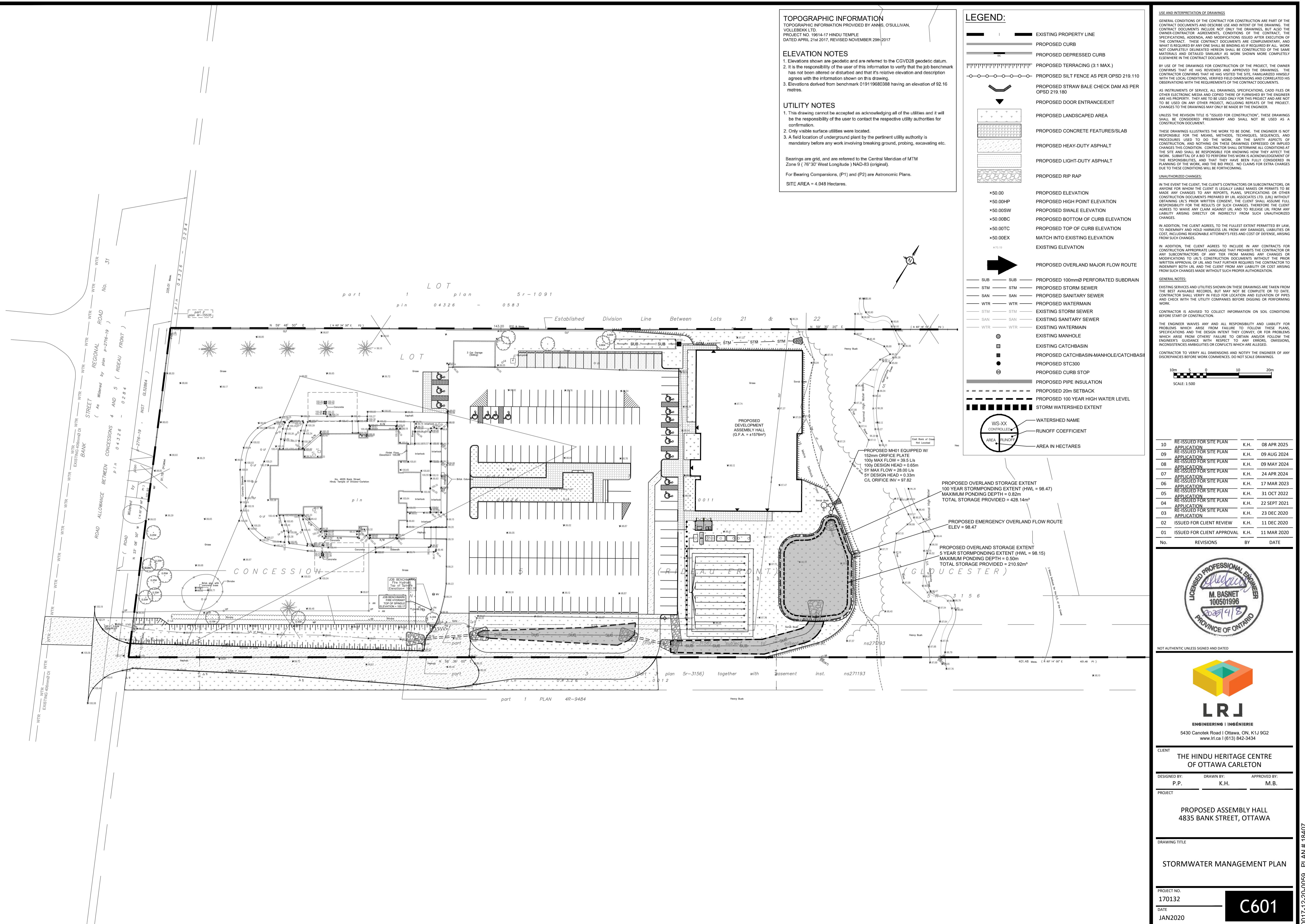
**APPENDIX O**  
**Civil Engineering Plans**

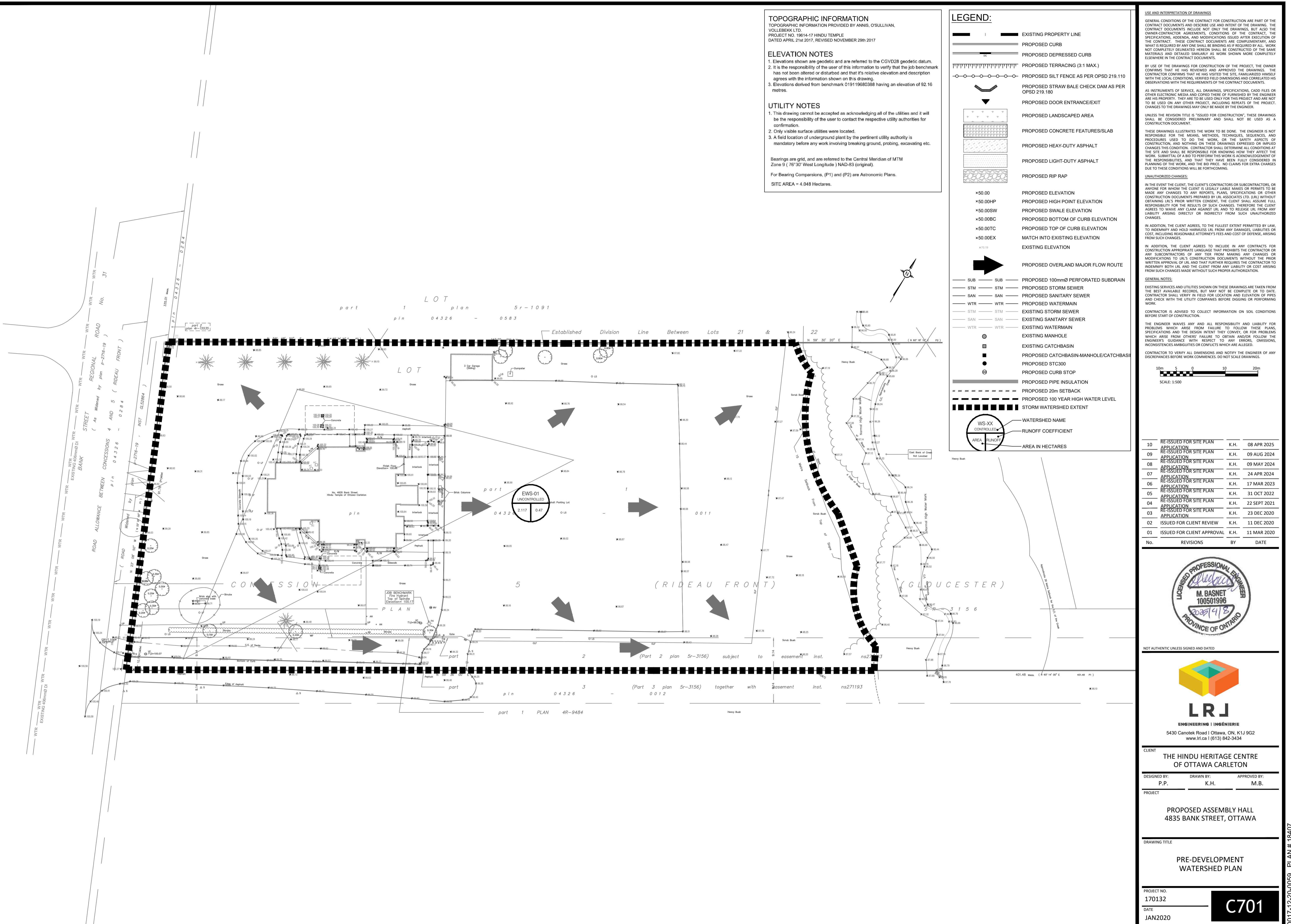


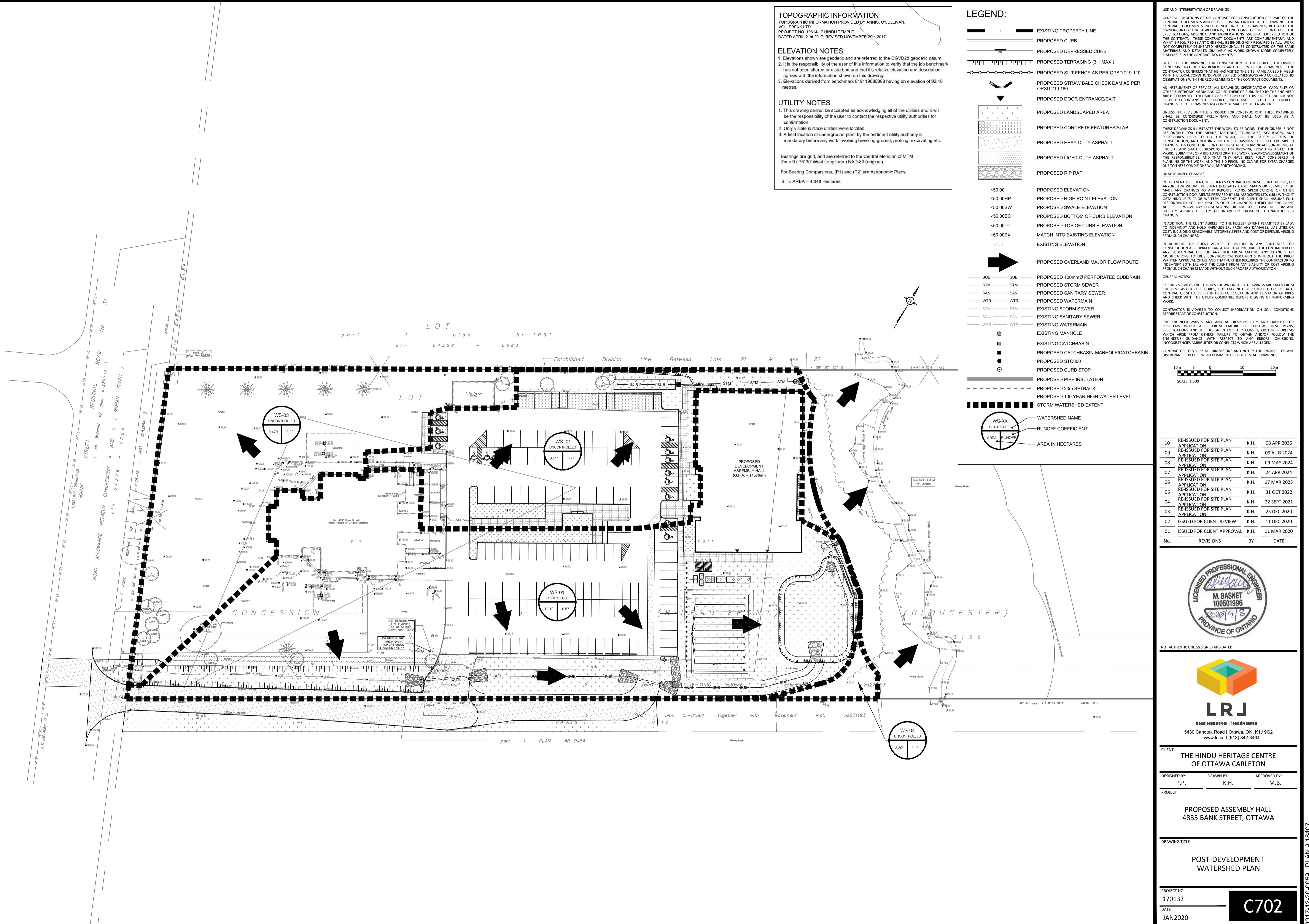




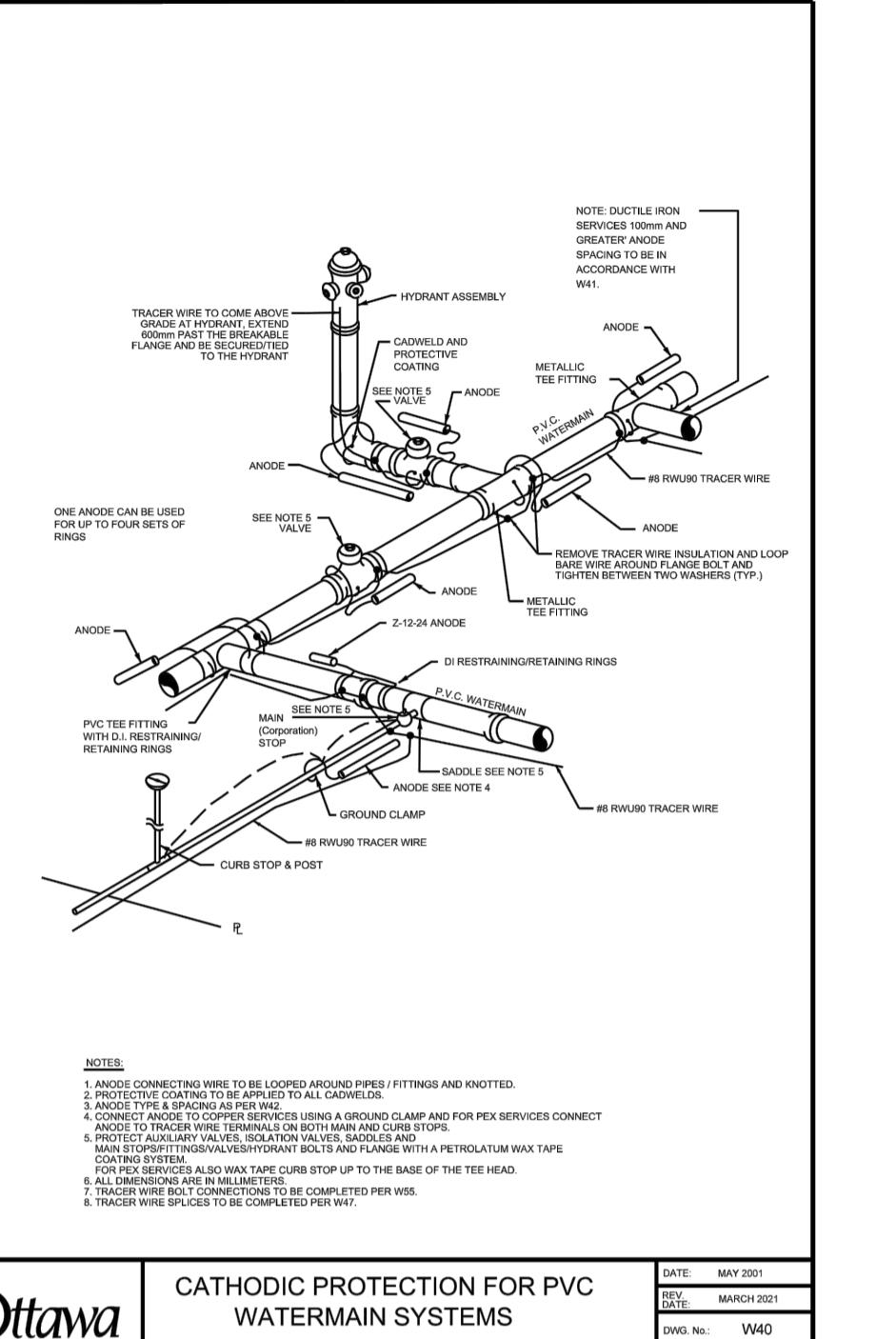
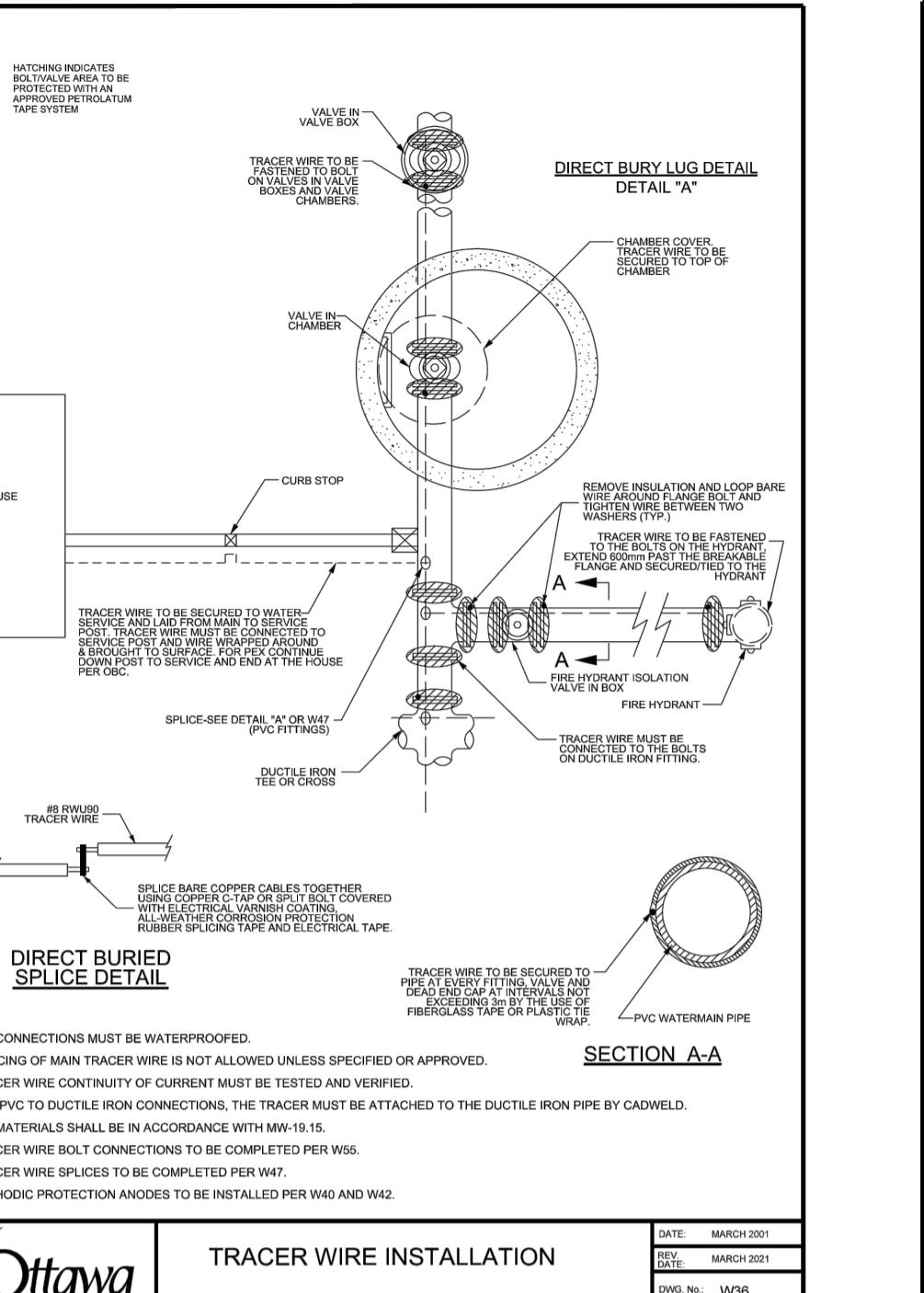
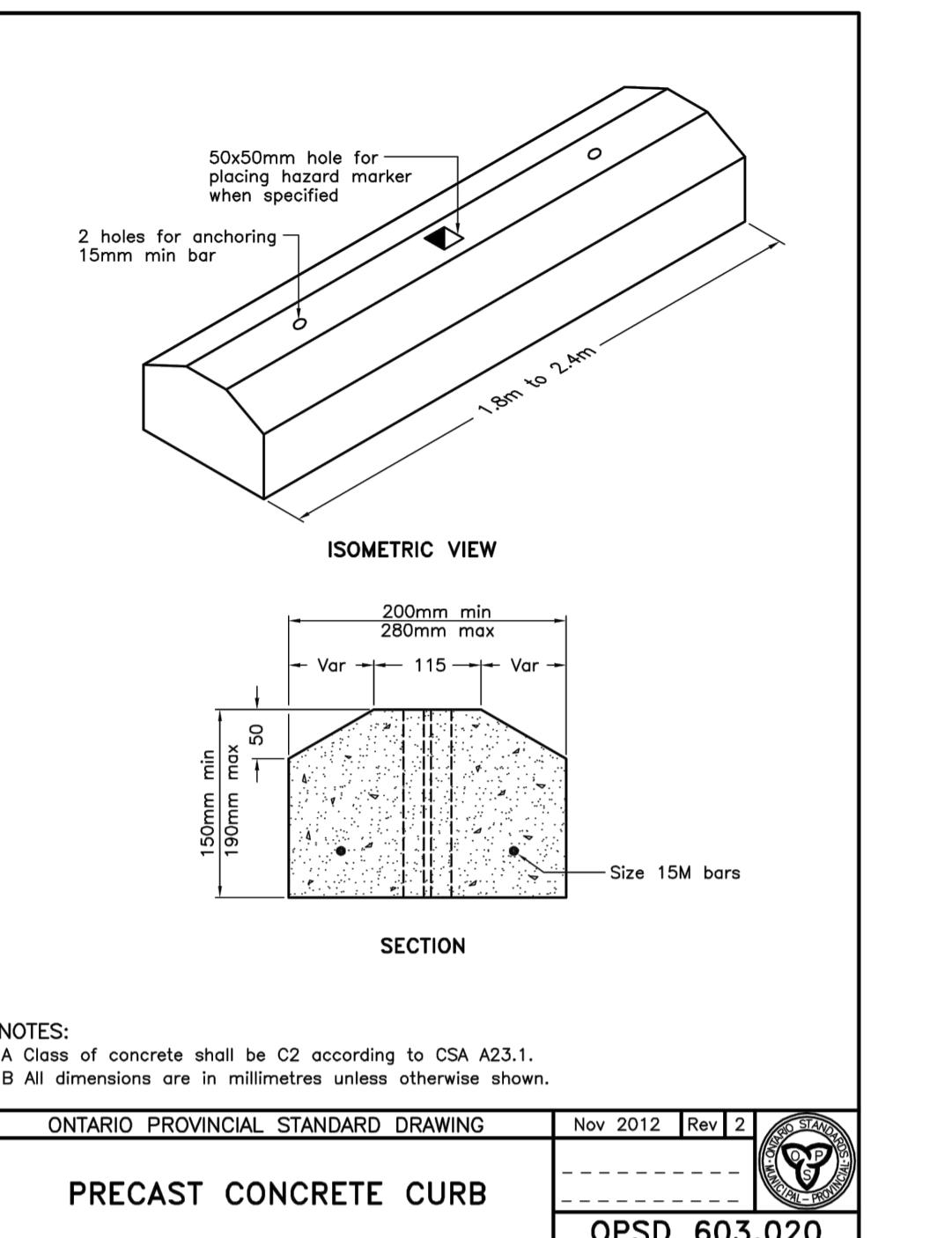
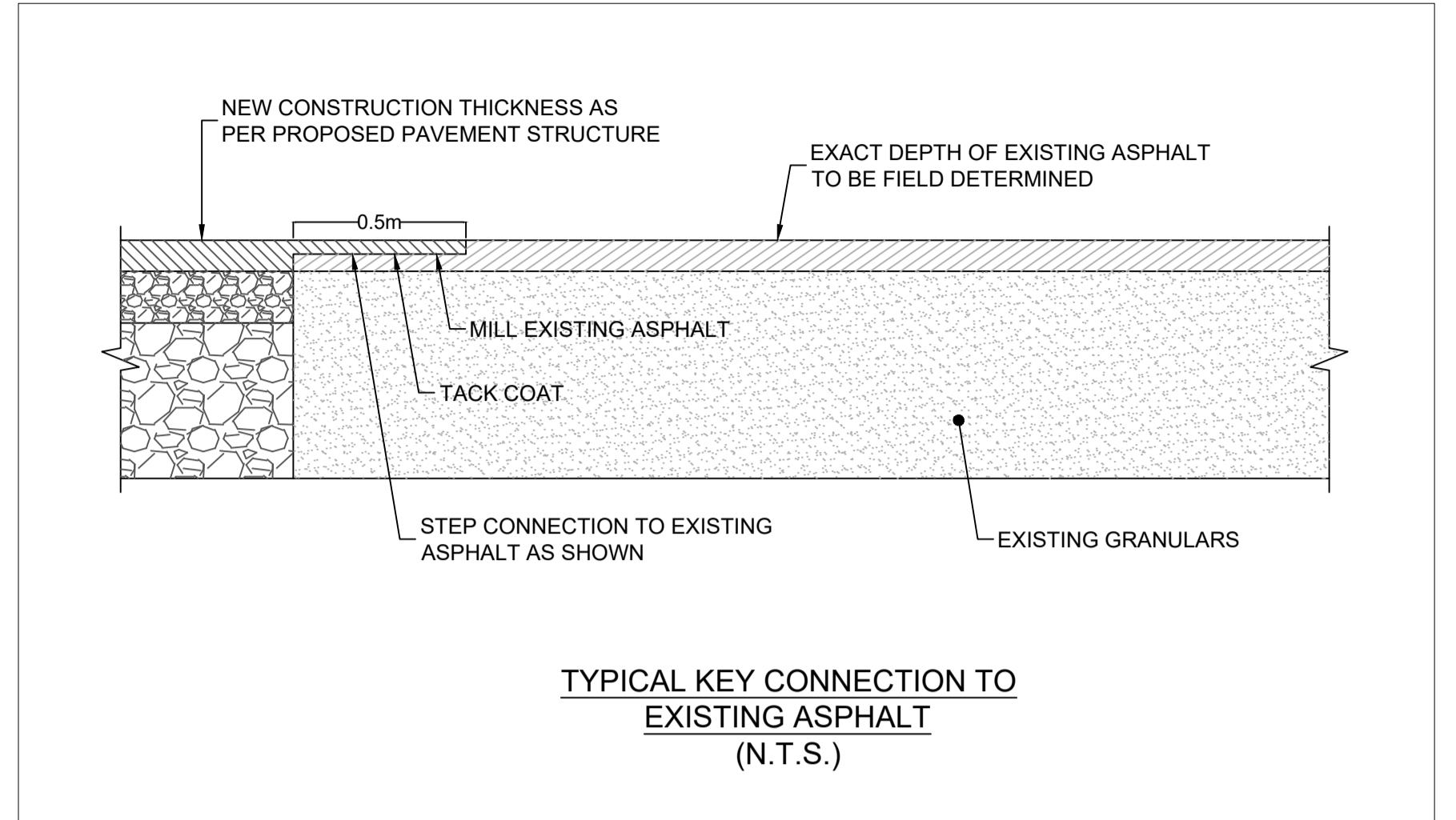












USE AND INTERPRETATION OF DRAWINGS  
GENERAL CONDITIONS OF THE CONTRACT FOR CONSTRUCTION ARE PART OF THE CONTRACT DOCUMENTS AND DESCRIBE USE AND INTENT OF THE DRAWING. THE CONTRACT DOCUMENTS INCLUDE NOT ONLY THE DRAWINGS, BUT ALSO THE DRAWING SPECIFICATIONS, CONTRACT CONDITIONS, CONTRACT DOCUMENTS, SPECIFICATIONS, ADDENDA, AND MODIFICATIONS ISSUED AFTER EXECUTION OF THE CONTRACT. THESE CONTRACT DOCUMENTS ARE COMPLEMENTARY, AND UNLESS OTHERWISE PROVIDED, THE CONTRACT DOCUMENTS SHALL GOVERN. IF ANY PART OF THE CONTRACT DOCUMENTS IS INCONCISE OR NOT COMPLETELY DELINERATED HERON SHALL BE CONSTRUCTED AS SHOWN MORE COMPLETELY ELSEWHERE.

BY USE OF THE DRAWINGS FOR CONSTRUCTION OF THE PROJECT, THE OWNER CONFRMS THAT HE HAS REVIEWED AND APPROVED THE DRAWINGS. THE CONTRACTOR CONFRMS THAT HE HAS VISITED THE SITE, FAMILIARIZED HIMSELF WITH THE DRAWINGS, AND THAT HE IS TO USE THE DRAWINGS FOR THIS PROJECT AND MODIFICATIONS ISSUED AFTER EXECUTION OF THE CONTRACT. THESE DRAWINGS ARE TO BE USED FOR THE WORK TO BE DONE. THE ENGINEER IS NOT RESPONSIBLE FOR THE MEANS, METHODS, TECHNIQUES, SECURITIES, AND EQUIPMENT USED TO DO THE WORK. THE SAFETY ASPECTS OF CONSTRUCTION, AND NOT ONLY THE DRAWINGS, EXPRESSED OR IMPLIED, ARE THE RESPONSIBILITY OF THE CONTRACTOR. THE CONTRACTOR SHALL DETERMINE ALL CONDITIONS AND THE SITE AND SHALL BE RESPONSIBLE FOR KNOWING HOW THEY AFFECT THE WORK. THE CONTRACTOR IS A SOLELY RESPONSIBLE FOR THE WORK, AND THAT HE HAS BEEN FULLY CONSIDERED IN PLANNING OF THE WORK, AND THE BID PRICE. NO CLAIMS FOR EXTRA CHARGES DUE TO THESE CONDITIONS WILL BE MADE BY THE ENGINEER.

AS INSTRUMENTS OF SERVICE, ALL DRAWINGS, SPECIFICATIONS, CAD FILES OR OTHER ELECTRONIC MEDIA AND COPIED THEREOF FURNISHED BY THE ENGINEER ARE THE PROPERTY OF THE ENGINEER AND ARE TO BE USED FOR THIS PROJECT AND MODIFICATIONS ISSUED AFTER EXECUTION OF THE CONTRACT. THESE DRAWINGS SHALL BE CONSIDERED PRELIMINARY AND SHALL NOT BE USED AS A CONSTRUCTION DOCUMENT.

THESE DRAWINGS ILLUSTRATE THE WORK TO BE DONE. THE ENGINEER IS NOT RESPONSIBLE FOR THE MEANS, METHODS, TECHNIQUES, SECURITIES, AND EQUIPMENT USED TO DO THE WORK. THE SAFETY ASPECTS OF CONSTRUCTION, AND NOT ONLY THE DRAWINGS, EXPRESSED OR IMPLIED, ARE THE RESPONSIBILITY OF THE CONTRACTOR. THE CONTRACTOR SHALL DETERMINE ALL CONDITIONS AND THE SITE AND SHALL BE RESPONSIBLE FOR KNOWING HOW THEY AFFECT THE WORK. THE CONTRACTOR IS A SOLELY RESPONSIBLE FOR THE WORK, AND THAT HE HAS BEEN FULLY CONSIDERED IN PLANNING OF THE WORK, AND THE BID PRICE. NO CLAIMS FOR EXTRA CHARGES DUE TO THESE CONDITIONS WILL BE MADE BY THE ENGINEER.

UNAUTHORIZED CHANGES:  
IN THE EVENT THE CLIENT, THE CLIENT'S CONTRACTORS OR SUBCONTRACTORS, OR OTHER PERSONS ARE TO MAKE ANY CHANGES TO THE DRAWINGS, THE CONTRACTOR IS NOT RESPONSIBLE FOR THE MEANS, METHODS, TECHNIQUES, SECURITIES, AND EQUIPMENT USED TO DO THE WORK. THE SAFETY ASPECTS OF CONSTRUCTION, AND NOT ONLY THE DRAWINGS, EXPRESSED OR IMPLIED, ARE THE RESPONSIBILITY OF THE CONTRACTOR. THE CONTRACTOR SHALL DETERMINE ALL CONDITIONS AND THE SITE AND SHALL BE RESPONSIBLE FOR KNOWING HOW THEY AFFECT THE WORK. THE CONTRACTOR IS A SOLELY RESPONSIBLE FOR THE WORK, AND THAT HE HAS BEEN FULLY CONSIDERED IN PLANNING OF THE WORK, AND THE BID PRICE. NO CLAIMS FOR EXTRA CHARGES DUE TO THESE CONDITIONS WILL BE MADE BY THE ENGINEER.

IN ADDITION, THE CLIENT AGREES, TO THE FULLEST EXTENT PERMITTED BY LAW, TO INDEMNIFY AND HOLD HARMLESS LRL FROM ANY DAMAGES, LIABILITY OR COST, INCLUDING REASONABLE ATTORNEY'S FEES AND COST OF DEFENSE, ARISING FROM UNAUTHORIZED CHANGES.

IN ADDITION, THE CLIENT AGREES, TO INCLUDE IN ANY CONTRACTS FOR CONSTRUCTION APPROPRIATE LANGUAGE THAT PROHIBITS THE CONTRACTOR OR ANY SUBCONTRACTORS, OF ANY TIER FROM MAKING ANY CHANGES OR MODIFICATIONS TO THE DRAWINGS, UNLESS APPROVED IN WRITING BY THE CONTRACTOR. THE CONTRACTOR SHALL NOT MAKE ANY CHANGES OR MODIFICATIONS TO THE DRAWINGS, UNLESS APPROVED IN WRITING BY LRL AND THAT FURTHER REQUIRES THE CONTRACTOR TO INDEMNIFY BOTH LRL AND THE CLIENT FROM ANY LIABILITY OR COST ARISING FROM SUCH CHANGES MADE WITHOUT SUCH PROPER AUTHORIZATION.

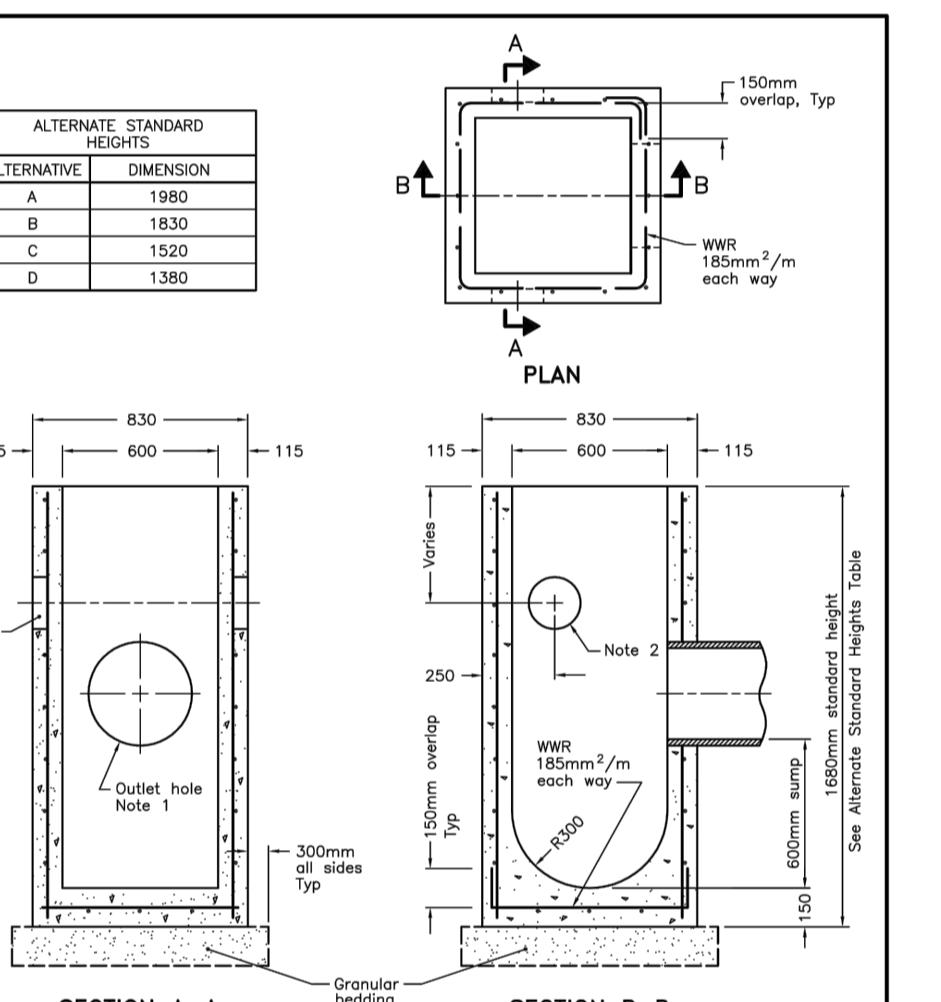
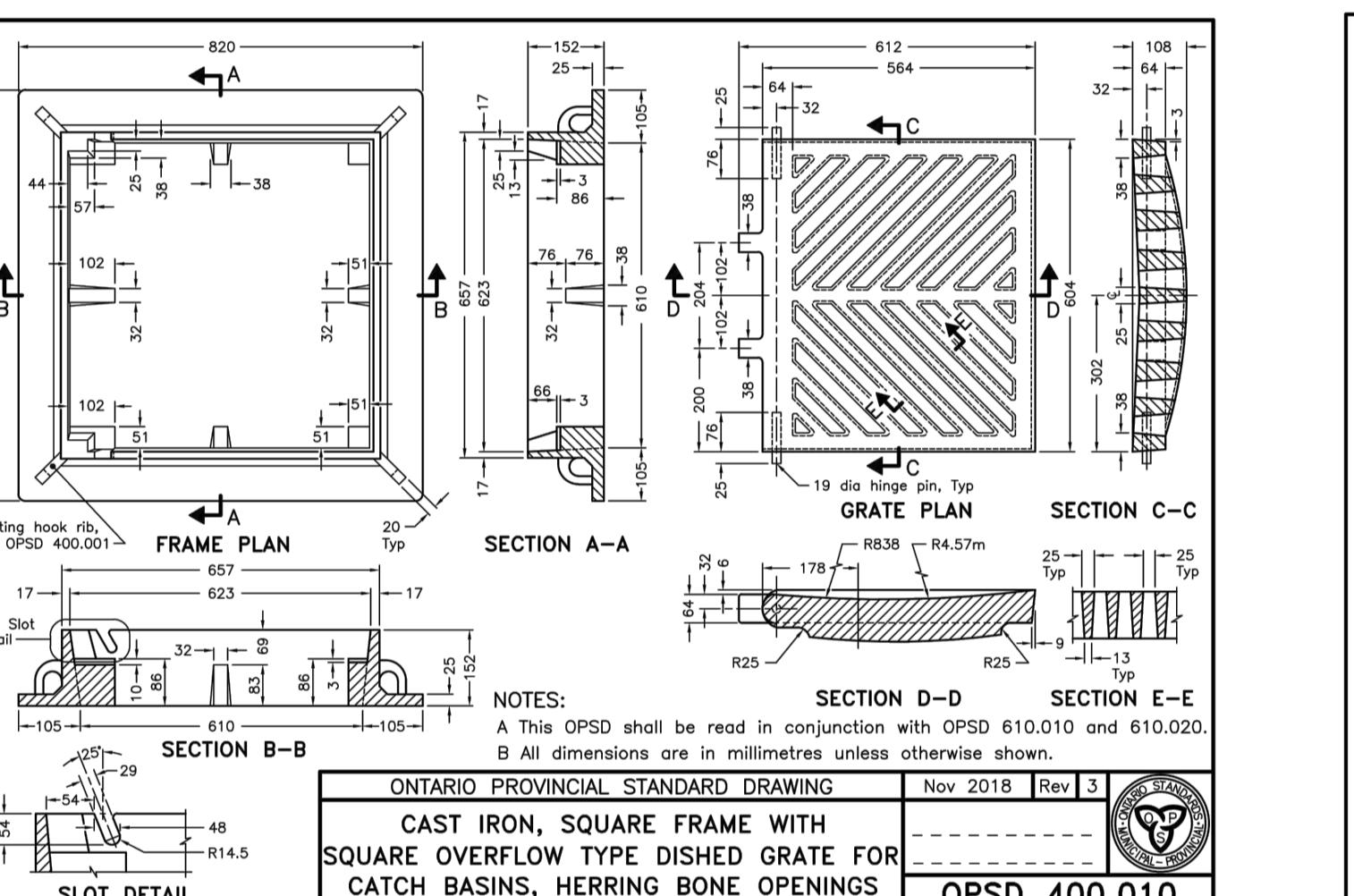
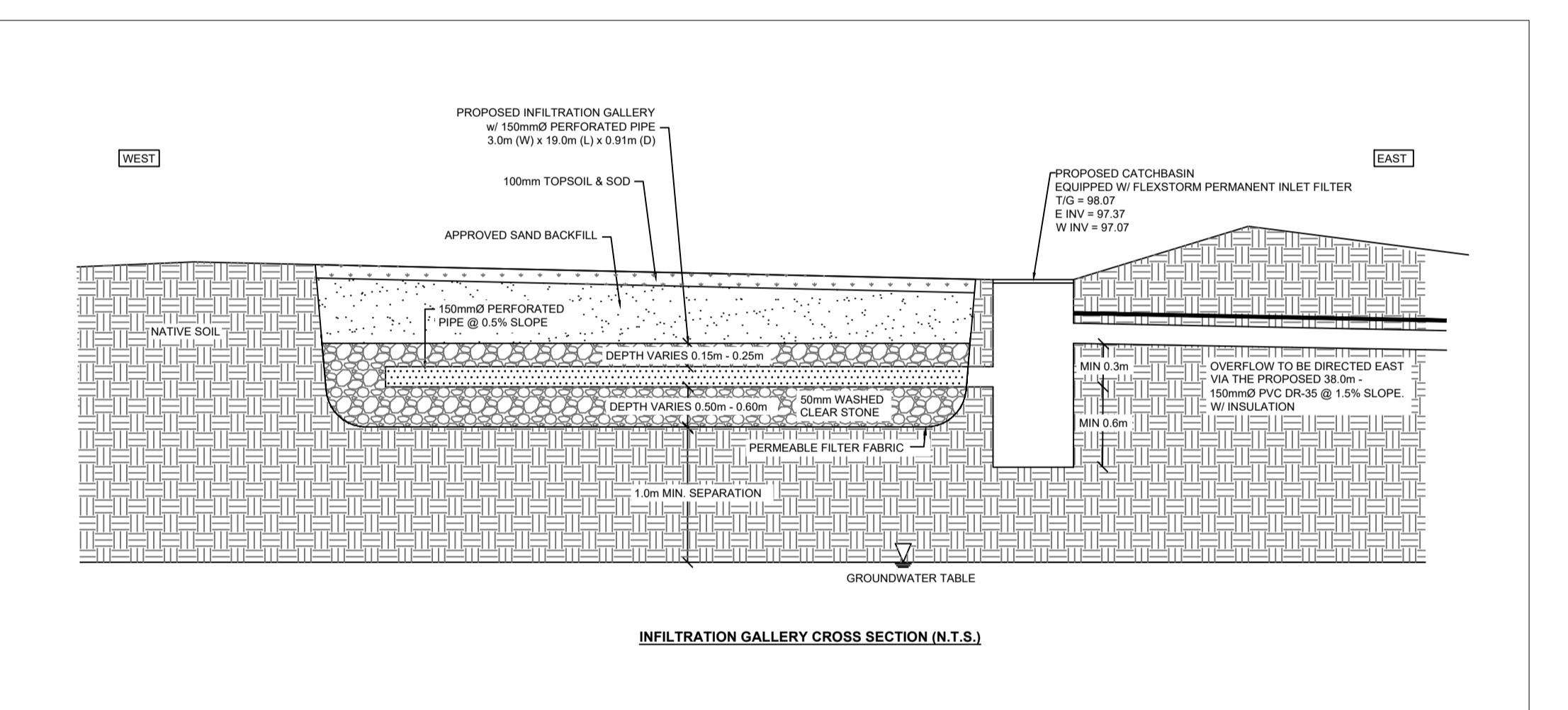
GENERAL NOTES:

EXISTING SERVICES AND UTILITIES SHOWN ON THESE DRAWINGS ARE TAKEN FROM THE ENGINEER'S INFORMATION. THE CONTRACTOR SHALL NOT USE THESE DRAWINGS FOR CONSTRUCTION. THE CONTRACTOR SHALL VERIFY IN FIELD FOR LOCATION AND ELEVATION OF PIPES AND CHECK WITH THE UTILITY COMPANIES BEFORE DIGGING OR PERFORMING WORK.

CONTRACTOR IS ADVISED TO COLLECT INFORMATION ON SOIL CONDITIONS BEFORE START OF CONSTRUCTION.

THE ENGINEER WAIVES ANY AND ALL RESPONSIBILITY AND LIABILITY FOR PROBLEMS WHICH ARISE FROM FAILURE TO FOLLOW THESE PLANS, SPECIFICATIONS AND THE DESIGN INTENT. THEY CONFER NO PROTECTION AGAINST OTHER PROBLEMS WHICH MAY ARISE. THE CONTRACTOR AND ENGINEER'S GUIDANCE, WITH RESPECT TO ANY ERRORS, OMISSIONS, INCONSISTENCIES AMBIGUITIES OR CONFLICTS WHICH ARE ALLEGED.

CONTRACTOR TO VERIFY ALL DIMENSIONS AND NOTIFY THE ENGINEER OF ANY DISCREPANCIES BEFORE WORK COMMENCES. DO NOT SCALE DRAWINGS.



10	RE-ISSUED FOR SITE PLAN	K.H.	08 APR 2025
09	APPLICATION FOR SITE PLAN	K.H.	09 AUG 2024
08	RE-ISSUED FOR SITE PLAN	K.H.	09 MAY 2024
07	APPLICATION FOR SITE PLAN	K.H.	24 APR 2024
06	RE-ISSUED FOR SITE PLAN	K.H.	17 MAR 2023
05	APPLICATION FOR SITE PLAN	K.H.	31 OCT 2022
04	RE-ISSUED FOR SITE PLAN	K.H.	22 SEPT 2021
03	APPLICATION FOR SITE PLAN	K.H.	23 DEC 2020
02	ISSUED FOR CLIENT REVIEW	K.H.	11 DEC 2020
01	ISSUED FOR CLIENT APPROVAL	K.H.	11 MAR 2020
	REVISIONS	BY	DATE



NOT AUTHENTIC UNLESS SIGNED AND DATED

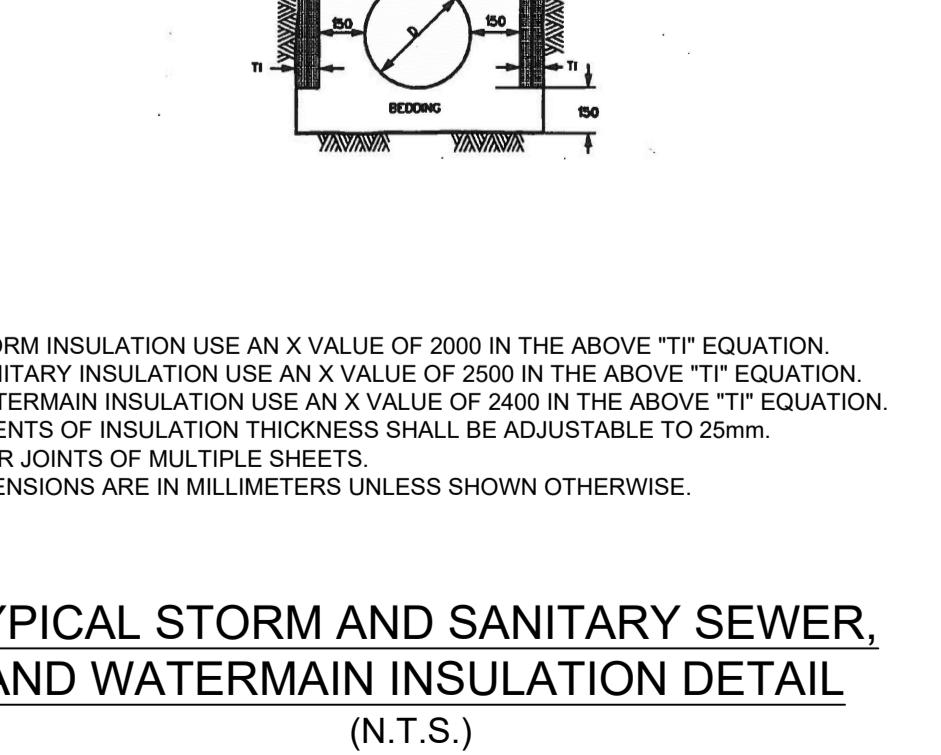


ENGINEERING | INGÉNIERIE  
5430 Canotek Road | Ottawa, ON, K1J 9G2  
www.lrl.ca | (613) 842-3434

CLIENT: THE HINDU HERITAGE CENTRE OF OTTAWA CARLETON

DESIGNED BY: P.P. DRAWN BY: K.H. APPROVED BY: M.B.

PROJECT: PROPOSED ASSEMBLY HALL 4835 BANK STREET, OTTAWA





## **APPENDIX P**

### **Septic Design**



# Green Valley Environmental Inc.

## LETTER OF AUTHORIZATION

**Owner:** Hindu Temple of Ottawa Carleton (attention: Harish Gupta)

**Address:** 4835 Bank Street  
Ottawa, Ontario

**Phone No.:** 613-737-5939 **Cell No.:** 613-866-2984

**Work No.:** **Fax No.:**

### LOCATION OF PROPERTY:

**Lot No.:** 22

**Concession No.:** 5RF

**Sub lot/Part No.:**

**R. Plan No.:** 5R3156

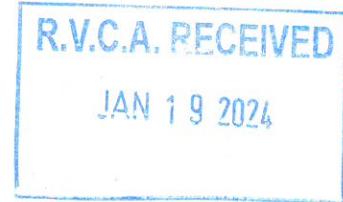
**Civic Address:** 4835 Bank Street

**Municipality:** Gloucester

**Roll No.:**

**Commercial:** (provide description of building and intended use)

Place of Worship with **Assembly Hall**



**SEPTIC FILE #**

**24-016**

**OTTAWA**

I, the above – mentioned authorize Green Valley Environmental Services to act as my agent to apply for and obtain a sewage system permit from the responsible Approval Agency.

Signature: Jessica Arthurs

Date: January 11, 2024

# Application for a Permit to Construct or Demolish

This form is authorized under subsection 8(1.1) of the *Building Code Act, 1992*

<p>Application number: <b>R.V.C.A. RECEIVED</b></p> <p>Date received: <b>JAN 19 2024</b></p>		<p><b>For use by Principal Authority</b></p> <p>Permit number (if different): <b>SEPTIC FILE #</b></p> <p>Roll number: <b>24-016</b></p>																																																									
<p><b>OTTAWA</b> OTTAWA SEPTIC SYSTEM OFFICE (Name of municipality, upper-tier municipality, board of health or conservation authority)</p>																																																											
<p><b>A. Project information</b></p>																																																											
<p>Building number, street name <b>4835 Bank St.</b></p>		<p>Unit number</p>	<p>Lot/con. <b>22/5RF</b></p>																																																								
<p>Municipality <b>Gloucester</b></p>	<p>Postal code <b>K1X 1G6</b></p>	<p>Plan number/other description <b>SR3156</b></p>																																																									
<p>Project value est. \$</p>		<p>Area of work (m<sup>2</sup>)</p>																																																									
<p><b>B. Purpose of application</b></p>																																																											
<p>New construction</p>	<p>Addition to an existing building</p>	<p>Alteration/repair</p>	<p>Demolition</p>	<p>Conditional Permit</p>																																																							
<p>Proposed use of building <b>Commercial Assembly bldg.</b></p>		<p>Current use of building</p>																																																									
<p>Description of proposed work <b>Install a new septic system for proposed assembly building.</b></p>																																																											
<p><b>C. Applicant</b></p>																																																											
<table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 25%; vertical-align: top;"> <p>Applicant is:</p> </td> <td style="width: 25%; vertical-align: top;"> <p>Owner or</p> </td> <td colspan="3" style="width: 50%; vertical-align: top;"> <p>Authorized agent of owner</p> </td> </tr> <tr> <td style="vertical-align: top;"> <p>Last name <b>Patel</b></p> </td> <td style="vertical-align: top;"> <p>First name <b>David</b></p> </td> <td colspan="3" style="vertical-align: top;"> <p>Corporation or partnership <b>Green Valley Environmental Inc.</b></p> </td> </tr> <tr> <td colspan="2" style="vertical-align: top;"> <p>Street address <b>6107 First Line. Rd.</b></p> </td> <td style="width: 15%; text-align: center; vertical-align: top;"> <p>Unit number</p> </td> <td colspan="2" style="width: 30%; text-align: center; vertical-align: top;"> <p>Lot/con.</p> </td> </tr> <tr> <td style="vertical-align: top;"> <p>Municipality <b>North Glouc.</b></p> </td> <td style="vertical-align: top;"> <p>Postal code <b>K1M 1A7</b></p> </td> <td style="width: 15%; text-align: center; vertical-align: top;"> <p>Province <b>ON</b></p> </td> <td colspan="2" style="width: 30%; text-align: center; vertical-align: top;"> <p>E-mail <b>engineering@gregroup.ca</b></p> </td> </tr> <tr> <td colspan="2" style="vertical-align: top;"> <p>Telephone number <b>(613) 692-2616</b></p> </td> <td style="width: 15%; text-align: center; vertical-align: top;"> <p>Fax <b>(613) 692-1802</b></p> </td> <td colspan="2" style="width: 30%; text-align: center; vertical-align: top;"> <p>Cell number <b>( )</b></p> </td> </tr> <tr> <td colspan="5" style="background-color: #f2f2f2; padding: 5px;"> <p><b>D. 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Application for a Permit to Construct or Demolish – Effective January 1, 2014

<b>E. Builder (optional)</b>			
Last name	First name	Corporation or partnership (if applicable)	
Street address			Unit number _____ Lot/Con. _____ <b>SEPTIC FILE #</b>
Municipality	Postal code	Province	E-mail <b>24-016</b>
Telephone number ( )	Fax ( )	Cell number ( ) <b>OTTAWA</b>	
<b>F. Tarion Warranty Corporation (Ontario New Home Warranty Program)</b>			
i. Is proposed construction for a new home as defined in the <i>Ontario New Home Warranties Plan Act</i> ? If no, go to section G.		Yes	No <input checked="" type="checkbox"/>
ii. Is registration required under the <i>Ontario New Home Warranties Plan Act</i> ?		Yes	No <input checked="" type="checkbox"/>
iii. If yes to (ii) provide registration number(s): _____			
<b>G. Required Schedules</b>			
i) Attach Schedule 1 for each individual who reviews and takes responsibility for design activities.			
ii) Attach Schedule 2 where application is to construct on-site, install or repair a sewage system.			
<b>H. Completeness and compliance with applicable law</b>			
i) This application meets all the requirements of clauses 1.3.1.3 (5) (a) to (d) of Division C of the Building Code (the application is made in the correct form and by the owner or authorized agent, all applicable fields have been completed on the application and required schedules, and all required schedules are submitted).		Yes <input checked="" type="checkbox"/>	No
Payment has been made of all fees that are required, under the applicable by-law, resolution or regulation made under clause 7(1)(c) of the <i>Building Code Act, 1992</i> , to be paid when the application is made.		Yes <input checked="" type="checkbox"/>	No
ii) This application is accompanied by the plans and specifications prescribed by the applicable by-law, resolution or regulation made under clause 7(1)(b) of the <i>Building Code Act, 1992</i> .		Yes <input checked="" type="checkbox"/>	No
iii) This application is accompanied by the information and documents prescribed by the applicable by-law, resolution or regulation made under clause 7(1)(b) of the <i>Building Code Act, 1992</i> which enable the chief building official to determine whether the proposed building, construction or demolition will contravene any applicable law.		Yes <input checked="" type="checkbox"/>	No
iv) The proposed building, construction or demolition will not contravene any applicable law.		Yes <input checked="" type="checkbox"/>	No
<b>I. Declaration of applicant</b>			
I <u>Davis Patel</u> (print name)		declare that:	
<ol style="list-style-type: none"> <li>The information contained in this application, attached schedules, attached plans and specifications, and other attached documentation is true to the best of my knowledge.</li> <li>If the owner is a corporation or partnership, I have the authority to bind the corporation or partnership.</li> </ol>			
Date	<u>Dec 21, 2023</u>	Signature of applicant	<u>Davis</u>

Personal information contained in this form and schedules is collected under the authority of subsection 8(1.1) of the *Building Code Act, 1992*, and will be used in the administration and enforcement of the *Building Code Act, 1992*. Questions about the collection of personal information may be addressed to: a) duties of a chief building official in relation to sewage systems or plumbing for an upper-tier municipality, board of health or conservation authority to whom this application is made, or, c) Director, Building and Development Branch, Ministry of Municipal Affairs and Housing 777 Bay St., 2nd Floor, Toronto, M5G 2E5 (416) 585-6666.

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JAN 19 2024

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Schedule 1: Designer Information

OTTAWA

Use one form for each individual who reviews and takes responsibility for design activities with respect to the project.

**A. Project Information**

Building number, street name	4835 Bank St.		
Municipality	Postal code	Unit no.	
Gloucester	K1X 1B6	Lot/cont.	
5R3156			

**B. Individual who reviews and takes responsibility for design activities**

Name	Davis Patel	Firm	Green Valley Environmental Inc.
Street address	6107 First Line Rd.	Unit no.	Lot/cont.
Municipality	North Gower	Postal code	ON
Telephone number	(613) 692-2616	Fax number	(613) 692-1802
E-mail: engineering@greggroup.ca Cell Number: ( )			

**C. Design activities undertaken by individual identified in Section B. [Building Code Table 3.5.2.1. of Division C]**

House	HVAC – House	Building Structural
Small Buildings	Building Services	Plumbing – House
Large Buildings	Detection, Lighting and Power	Plumbing – All Buildings
Complex Buildings	Fire Protection	On-site Sewage Systems

Description of designer's work

Design a septic system for proposed assembly building!

**D. Declaration of Designer**

I Davis Patel declare that (choose one as appropriate):  
(print name)

I review and take responsibility for the design work on behalf of a firm registered under subsection 3.2.4. of Division C, of the Building Code. I am qualified, and the firm is registered, in the appropriate classes/categories.

Individual BCIN: 119685

Firm BCIN: 16035

I review and take responsibility for the design and am qualified in the appropriate category as an "other designer" under subsection 3.2.5. of Division C, of the Building Code.

Individual BCIN: \_\_\_\_\_

Basis for exemption from registration: \_\_\_\_\_

The design work is exempt from the registration and qualification requirements of the Building Code.

Basis for exemption from registration and qualification: \_\_\_\_\_

I certify that:

1. The information contained in this schedule is true to the best of my knowledge.
2. I have submitted this application with the knowledge and consent of the firm.

Date

Dec 21, 2023

Signature of Designer

Davis

NOTE:

1. For the purposes of this form, "individual" means the "person" referred to in Clause 3.2.4.7(1) (c) of Division C, Article 3.2.5.1. of Division C, and all other persons who are exempt from qualification under Subsections 3.2.4. and 3.2.5. of Division C.
2. Schedule 1 is not required to be completed by a holder of a license, temporary license, or a certificate of practice, issued by the Ontario Association of Architects. Schedule 1 is also not required to be completed by a holder of a license to practise, a limited license to practise, or a certificate of authorization, issued by the Association of Professional Engineers of Ontario.

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## Schedule 2: Sewage System Installer Information

<b>A. Project Information</b>			
Building number/street name	4835 Bank St.		Unit number
Municipality	Gloucester	Postal code	Plan number/ other description K1X 1G6 5R3156
<b>B. Sewage system installer</b>			
Is the installer of the sewage system engaged in the business of constructing on-site, installing, repairing, servicing, cleaning or emptying sewage systems, in accordance with Building Code Article 3.3.1.1, Division C?			
<input checked="" type="checkbox"/> Yes (Continue to Section C)		No (Continue to Section E)	
		Installer unknown at time of application (Continue to Section E)	
<b>C. Registered installer information (where answer to B is "Yes")</b>			
Name	Green Valley Environmental Inc.		BCIN 11234
Street address	6107 7th Line Rd.		Unit number
Municipality	North Glouster	Postal code K1M 1A8	Province ON
Telephone number (613) 692-2616	Fax (613) 692-1802	E-mail Cell number (613) 229-3900	
<b>D. Qualified supervisor information (where answer to section B is "Yes")</b>			
Name of qualified supervisor(s) Bill Seabrook	Building Code Identification Number (BCIN) 11234		
<b>E. Declaration of Applicant:</b>			
<u>Davis Patel</u> (print name)			declare that:
I am the applicant for the permit to construct the sewage system. If the installer is unknown at time of application, I shall submit a new Schedule 2 prior to construction when the installer is known;			
OR I am the holder of the permit to construct the sewage system, and am submitting a new Schedule 2, now that the installer is known.			
I certify that:			
<ol style="list-style-type: none"><li>1. The information contained in this schedule is true to the best of my knowledge.</li><li>2. If the owner is a corporation or partnership, I have the authority to bind the corporation or partnership.</li></ol>			
Date	Dec 21, 2023	Signature of applicant	<u>Davis</u>



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Schedule 4

Proposed Services

Complete Sections 1 thru 7

1. Engineered

Yes  
 No

3. Type of work proposed

New Installation  
 Replacement  
 Alteration

5. Residential Sewage Design Flow Info.

Bedrooms

House (floor area) \_\_\_\_\_ m<sup>2</sup>

People

Total Fixture Units \_\_\_\_\_ (Schedule 8)

Residential Flow \_\_\_\_\_ L/day

2. Water supply

Proposed  
 Existing

4. Type of Well

Dug/bored/Sandpoint well  
 Drilled well  
 Municipal  
 Other

6. Sewage Design Flow Other Occupancies

Design Flow 4000 L/day

Detailed sewage flow calculations:

No flood preparation in assembly building  
500x8 = 4000 L/day (50 people)

Class 4 – BMEC Area Bed (Schedule 11)

Fully raised

Partially raised

In-ground

Class 4 – “Type A” Dispersal (Schedule 13)

Fully raised

Partially raised

In-ground

Class 4 – “Type B” Dispersal (Schedule 14)

Fully raised

Partially raised

In-ground

Class 5 – Holding Tank (9000L min)

Tank/TreatmentUnit/PumpChamber ONLY

Effluent Filter/Risers ONLY

7. Type of System

Treatment Unit Norweco HK 4730-3M

Class 2 – Leaching Pit

Class 3 – Cesspool

Class 4 – Shallow Buried Trench

12 runs, 13.08m each.

Class 4 – Trench (Schedule 9)

Fully raised

Partially raised

In-ground

Class 4 – Filter Media (Schedule 10)

Fully raised

Partially raised

In-ground



Ottawa Septic  
System Office



Bureau des systèmes  
septiques d'Ottawa

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Permit No \_\_\_\_\_  
Revision No \_\_\_\_\_  
Date \_\_\_\_\_

Schedule 5  
Sewage System Details

Type of System Class 4 Shallow Buried French Bed Schedule 4)

Septic/Holding Tank Size: 9000 Litres

Make: MAC GREGOR

Septic Tank Effluent Filter Make: POLYLOK

Model: PL250

Tertiary Treatment System

Treatment Unit - Make & Model Norineco MK 4730-3M

Number of Units: 1

Other: 800 GAL PUMP CHAMBER

Refer to Typical Drawing # PC-5-1174

Pump(s) required Liberty 280/0.5hp

Mantle Information:

Pump Rate \_\_\_\_\_ L/15min

Native or imported = 15m in \_\_\_\_\_ direction(s)

Note: Alarm required for all

pumping systems

Slope subgrade \_\_\_\_\_ % slope  
\_\_\_\_\_ direction(s)

Site to be Scarified (If clay) YES / NO

Clay Seal Required (If bedrock) YES / NO

Trench

Distribution Pipe Length \_\_\_\_\_ m

Shallow Buried Trench

Pipe Length 156.96 \_\_\_\_\_ m

Loading Area \_\_\_\_\_ m<sup>2</sup>

12 runs of 13.08m each.

Type of Chamber \_\_\_\_\_

Filter Media Bed

Length of Chamber \_\_\_\_\_ m

Stone \_\_\_\_\_ m<sup>2</sup>

Dispersal Bed

Extended Base \_\_\_\_\_ m<sup>2</sup>

BMEC  Type A  Type B

Pipe \_\_\_\_\_ m

Stone \_\_\_\_\_ m<sup>2</sup>

Weight of Filter Media \_\_\_\_\_ Kg

Sand \_\_\_\_\_ m<sup>2</sup>

Loading Area \_\_\_\_\_ m

Pipe \_\_\_\_\_ m<sup>2</sup>

Linear Loading \_\_\_\_\_ L/m<sup>2</sup>

Tank/Treatment Unit/Pump Chamber Replacement ONLY

Effluent Filter & Riser ONLY

Construction Notes: Any contaminated material present in the excavation area to be removed and replaced with sand fill. Trees within 5m of the septic system to be removed.



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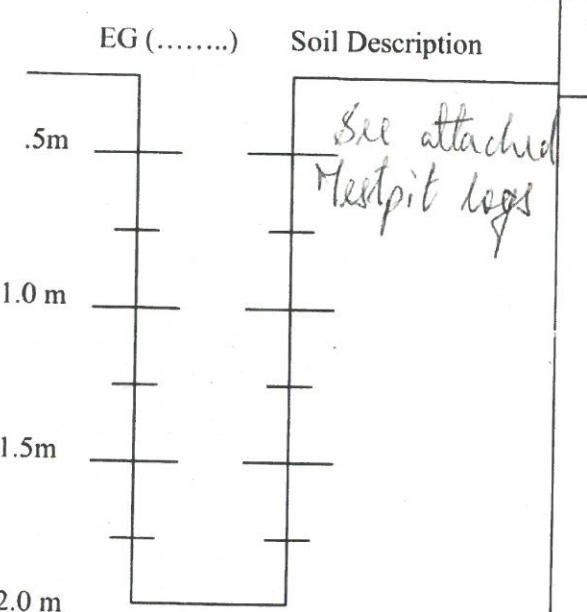
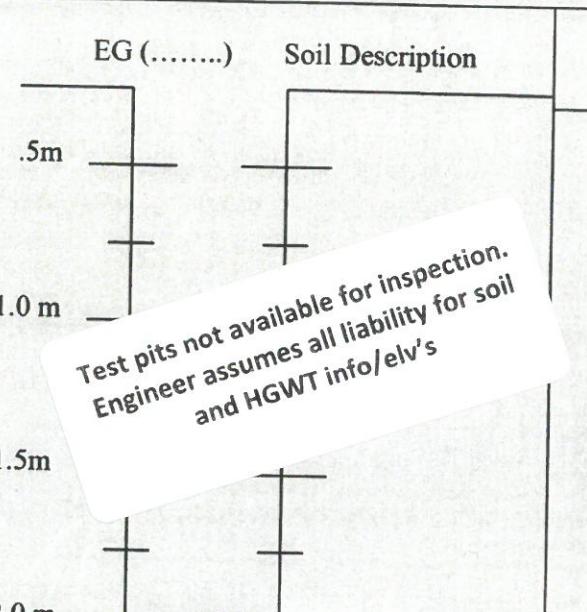
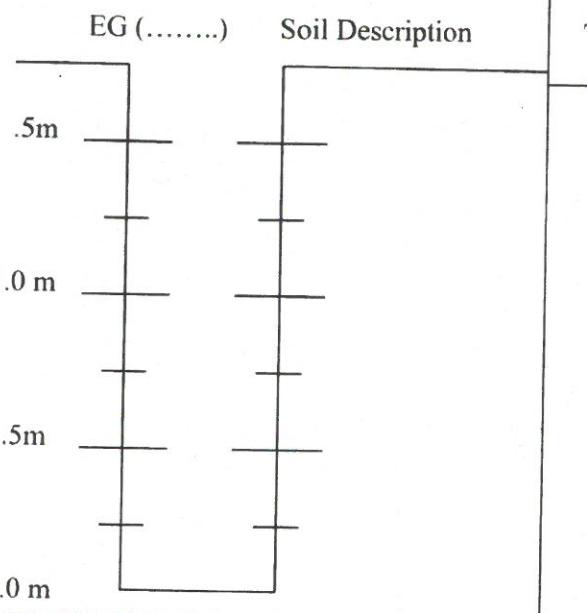
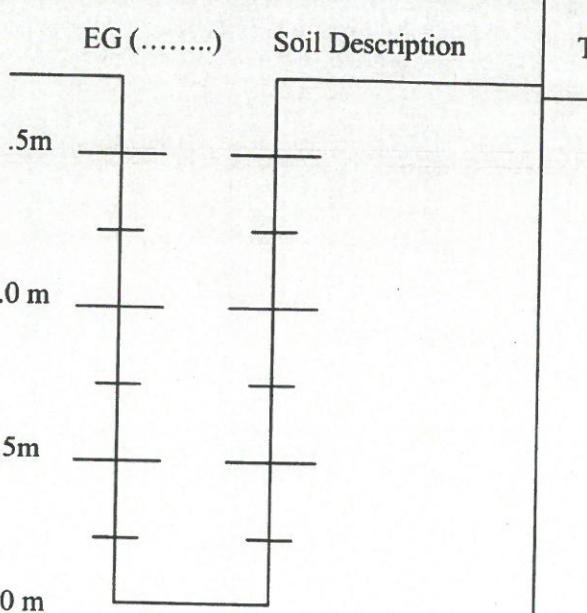
Permit # - 016

Revision #

Date OTTAWA

Schedule 6

Soil and Water Table Information  
(Minimum depth of test pit: 2 metres)

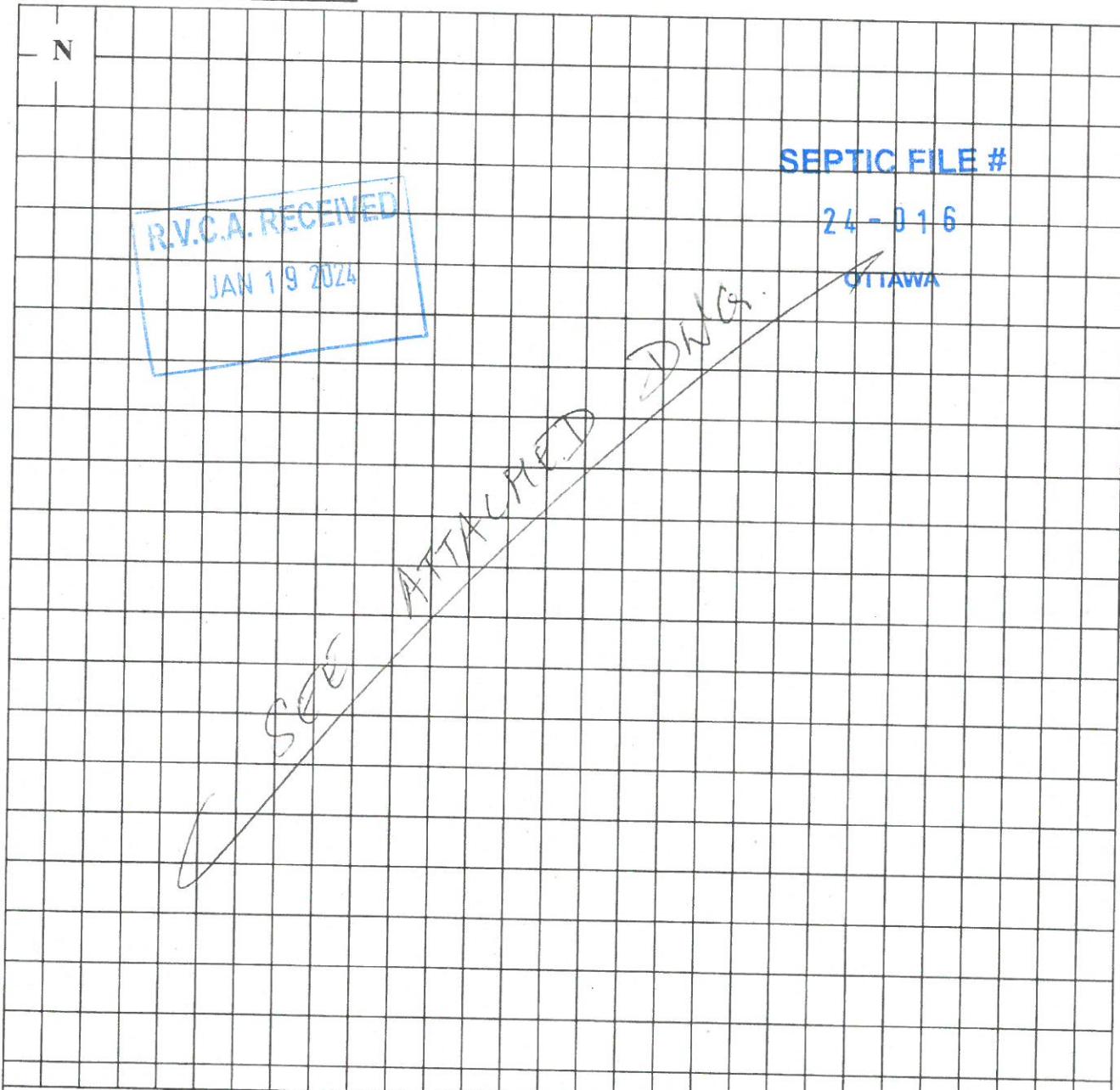
Name of Applicant/Agent: <u>LRL</u> Date: <u>May 8, 2017</u> Time: <u>10 AM</u> Applicant/Agent Signature: <u>lrl</u>			Inspector: _____ Date: _____ Time: _____ Inspector Signature: _____		
EG (.....)      Soil Description      T 			EG (.....)      Soil Description      T 		
EG (.....)      Soil Description      T 			EG (.....)      Soil Description      T 		
<b>LEGEND</b> BR = Bedrock GWT = Ground water table HGWT = High ground water table M = metres EG = Existing grade T = percolation rate					



Scale: 1 Block = NTS

**Schedule 7  
Layout Section**

Do Not Complete  
Permit # \_\_\_\_\_  
Revision # \_\_\_\_\_  
Date \_\_\_\_\_



○ Dug Well • Drilled Well ▲ Neighbouring Homes ◊ Benchmark --- Tile Drainage — Property Line

Elevations (metric only)

B.M. 100.17 m

B.M. Description East arm of hydrant located west of Isolthus  
Exact Location entrance to site

Min. of 5 elevations in proposed system area (in X pattern)

~~X<sub>1</sub> \_\_\_\_\_  
X<sub>3</sub> \_\_\_\_\_  
X<sub>5</sub> \_\_\_\_\_  
X<sub>7</sub> \_\_\_\_\_ X<sub>2</sub> \_\_\_\_\_  
X<sub>4</sub> \_\_\_\_\_  
X<sub>6</sub> (toe) \_\_\_\_\_  
X<sub>8</sub> \_\_\_\_\_~~



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**Schedule 8**  
**Fixture unit count**

Fixtures	# Existing	+ # Proposed	X	unit count	=	Fixture Count
<b>Bathroom</b>						
Bathroom group (toilet, sink and tub or shower) installed in the <u>same</u> room		+		X	6	=
<u>Urinal wall mounted washout type</u>		+	10	X	1.5	= 15
Shower stall		+	2	X	1.5	= 3
Wash basin (SINK) (1½inch trap)		+	19	X	1.5	= 28.5
Watercloset (TOILET) tank operated		+	22	X	4	= 88
Bidet		+		X	1	=
<b>Kitchen</b>						
Dishwasher		+		X	1	=
Sink with/without garbage grinder(s), domestic and other small type single, double or 2 single with a common trap		+		X	1.5	=
<b>Other</b>						
Domestic washing machine		+		X	1.5	=
Combination sink and laundry tray single or double (Installed on 1½ trap)		+		X	1.5	=

**\*Total: 134.5**

**\*Insert the TOTAL in section 5 of Schedule 4 (0.Reg 151/13 Table 7.4.9.3)**

1. **Sump pumps and floor drains are not to be connected to the sewage system.** Connection of such fixtures to a sewage system may lead to a hydraulic failure of the said system. The above mentioned fixtures should be discharged separately to an approved Class 2 (leaching pit) sewage system.
2. Where laundry waste is not more than 20% of the total daily design sanitary sewage flow, it may discharge to a sewage system (Part 8, OBC, 8.1.3.1(2) ).

*Barry*

*Dec 21, 2023*

Agent/Owner signature

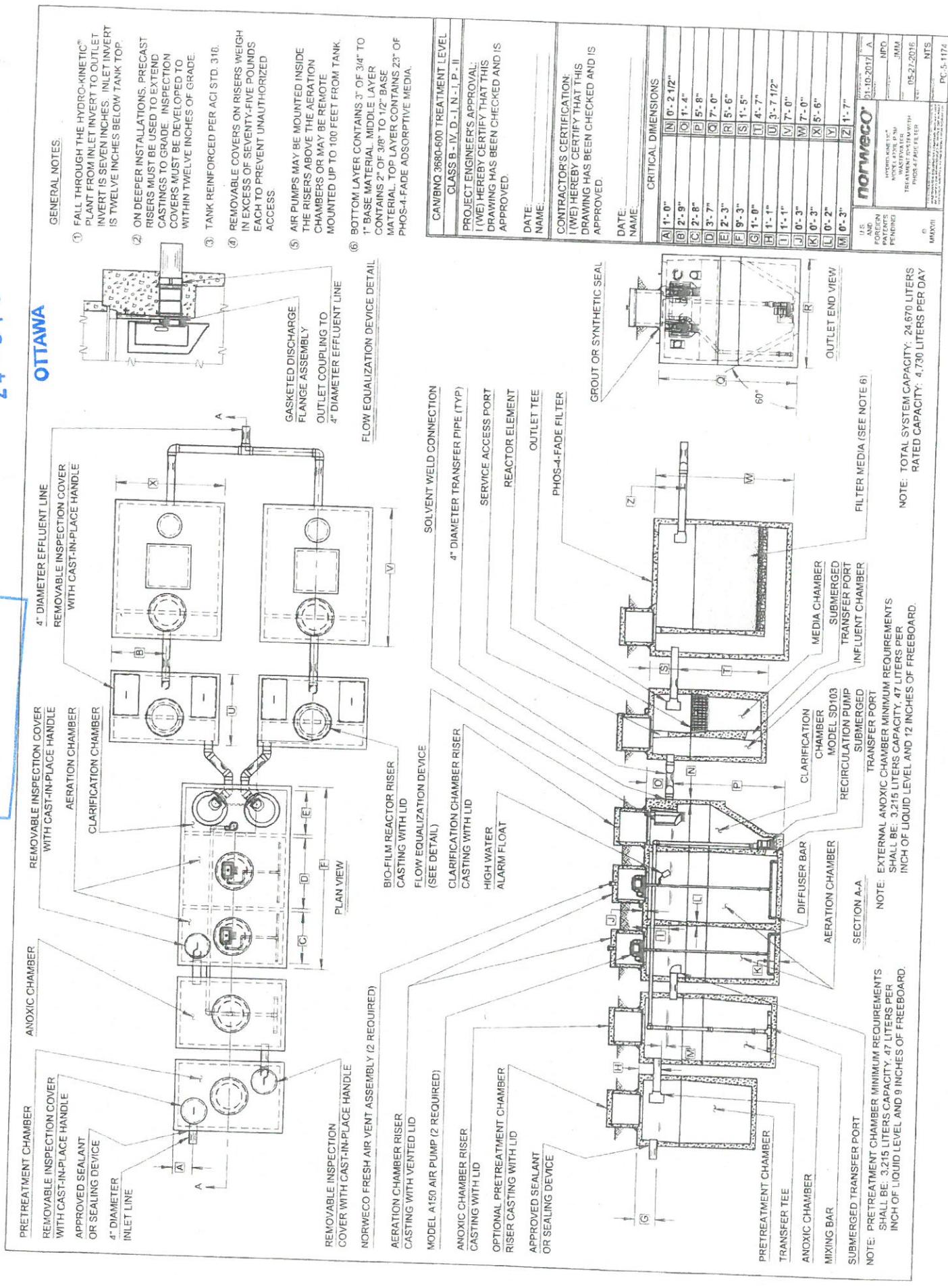
Date

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SEPTIC FILE #

24-016

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```

graph TD
    A[Number of orifices(m)] --> B[Input spacing of orifices(m)]
    B --> C[Length of a lateral (m)]
    
```

Diameter of orifice (inch):	
Squirt height (feet):	
Discharge of orifice (US gal/orifice x minutes)	
Flow in a lateral (US gal/min x lateral)	
Total discharge (US gal/min)	
Total discharge (L/min)	
Total discharge (Imp. gal/min)	

0.12	0.12	0.12	0.12	0.12	0.12	0.12
2.00	5.00	6.00	7.00	8.00	9.00	20.00
0.24	0.39	0.42	0.46	0.49	0.52	0.77
4.88	7.71	8.45	9.13	9.76	10.35	15.43
9.76	15.43	16.90	18.25	19.51	20.70	30.85
36.93	58.39	63.97	69.09	73.86	78.35	116.79
8.12	12.85	14.07	15.20	16.25	17.23	25.69

		(Imperial)			
		65.62	65.62	65.62	65.62
20.00	65.62	65.62	65.62	65.62	65.62
3.81	1.50	1.50	1.50	1.50	1.50
2.00	6.55	6.55	6.55	6.55	6.55
3.81	1.50	1.50	1.50	1.50	1.50
13.08	42.91	42.91	42.91	42.91	42.91
3.81	1.50	1.50	1.50	1.50	1.50
0.19	0.61	1.42	1.68	1.94	2.20
0.01	0.02	0.05	0.06	0.06	0.07
0.01	0.04	0.09	0.10	0.12	0.13
3.05	10.00	10.00	10.00	10.00	10.00
0.61	2.00	5.00	6.00	7.00	8.00
4.00	13.12	13.12	13.12	13.12	13.12

7.86	25.79	29.68	30.97	32.25	33.53	34.80	48.73
	9.76	15.43	16.90	18.25	19.51	20.70	30.85

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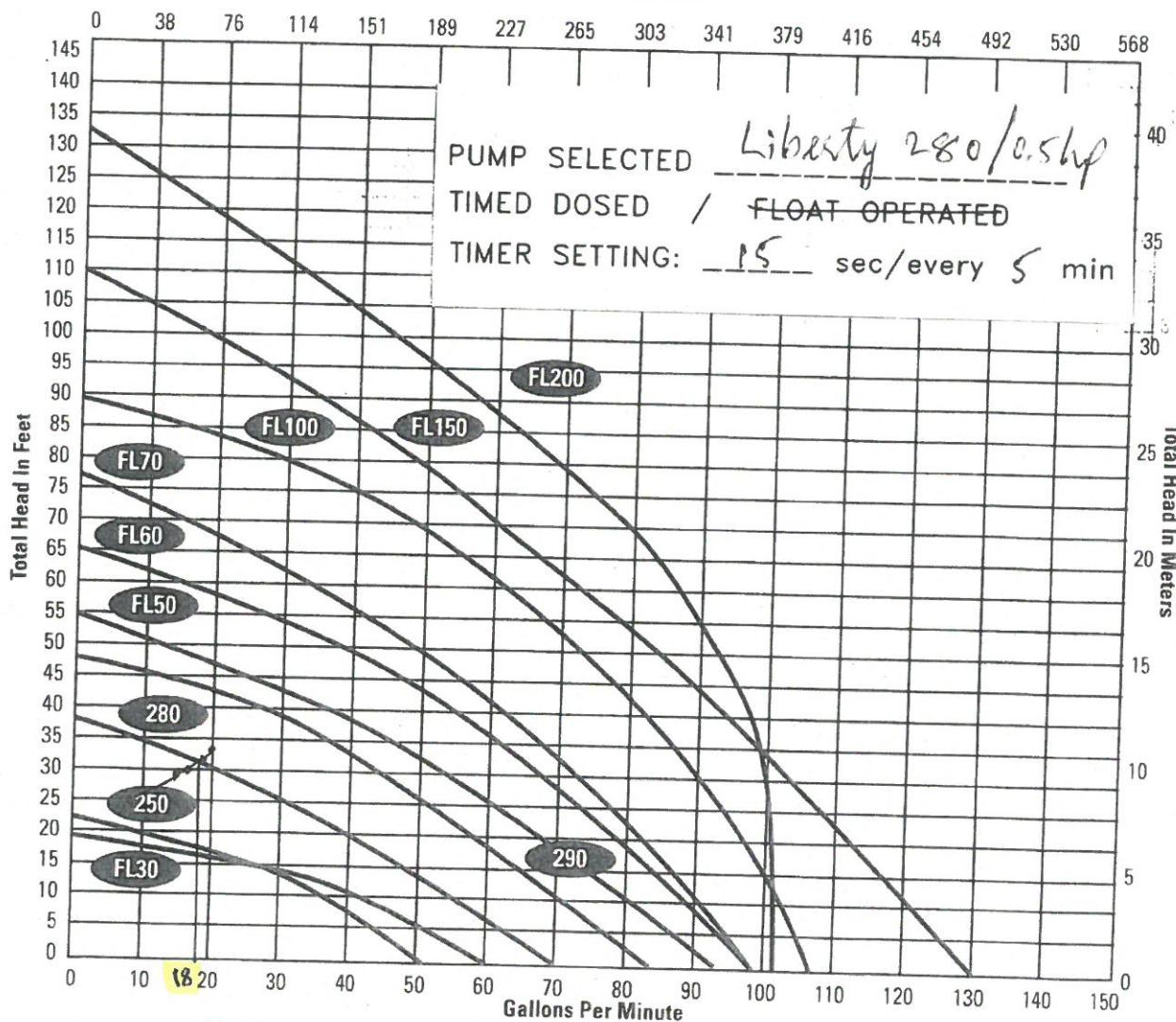
OTTAWA

# Liberty Pumps®

## Effluent Pumps

### Performance Curve Data 60 hz.

Liters Per Minute



innovate. evolve.

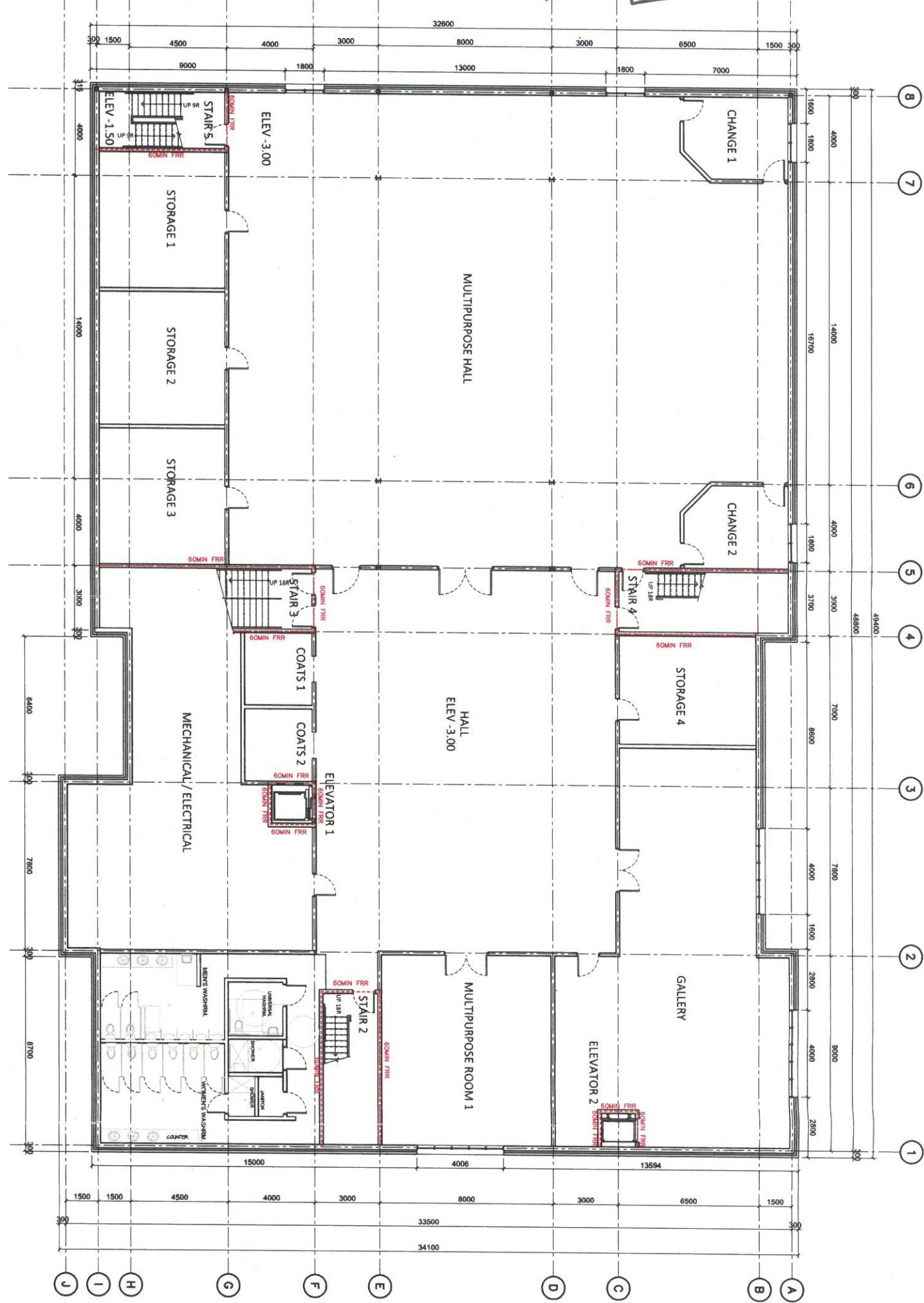
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JAN 26 2024

REFER TO:

SEPTIC FILE #  
24-016

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PROJECT MANAGER HARISH GUPTA B. ARCH	jd planning 1065 PI ANTE DRIVE OTTAWA, ON K1Y 9E6 T: 613-855-2984 C: 613-855-2984
ARCHITECT ANNIS OSULLIVAN, VOLBERK LTD. 14 Concourse Gdns, St. Jacobs, ON N0B 2Z0 Phone: (613) 227-0550 Fax: (613) 227-0739	Associate D. J. Halpern & Lombardy ON K0G 1L0 613-812-1728 jessica@jdpln.com

STRUCTURAL CONSULTANT D. J. Halpern & Lombardy ON K0G 1L0	GENERAL NOTES
MECHANICAL & ELECTRICAL CONSULTANT JAMES B. LENNOX & ASSOCIATES INC. 3332 Cartier Ave. OTTAWA, ON K1Y 7P1 Phone: (613) 739 9500 Fax: (613) 722-0550	<ol style="list-style-type: none"> <li>1. CONTRACTORS MUST VERIFY ALL CO. DIMENSIONS, DRAWINGS, &amp; REPORT ANY DISCREPANCIES TO THE OWNER.</li> <li>2. ALL DRAWINGS &amp; SPECIFICATIONS ARE INSTRUMENTS WHICH MUST BE OBSERVED &amp; THE PROPERTY OF THE OWNER. COPIES OF THE DRAWINGS &amp; SPECIFICATIONS MAY NOT BE REPRODUCED WITHOUT THEIR WRITTEN PERMISSION.</li> </ol>



FLOOR PLAN -  
LEVEL 0

PROJECT AND LOCATION  
HERITAGE CENTRE -  
HINDU TEMPLE - PHASE 2,  
4835 BANK ST., OTTAWA, ON  
PIN 04326-0011

ARCHITECT  
VECTOR DESIGN ARCHITECTS  
14 STRATHBURY STREET  
OTTAWA, ONTARIO K2G 5N8  
TELEPHONE: (613) 421-9806  
EMAIL: [vector@gmail.com](mailto:vector@gmail.com)

CIV. CONSULTANT  
L.R.J.  
DESIGN & SYSTEMS  
SUITE 251, 2370 RUE L'ALLEE  
OTTAWA, ON K2B 7S5  
Phone: (613) 739 9500  
Fax: (613) 722-0550

Mechanical & Electrical Consultant  
CHIARRELLI KORBER  
ENGINEERING LTD.  
1040 CLOTHIER ROAD  
KINGSTON, ON K7M 1L7

STRUCTURAL CONSULTANT  
JAMES B. LENNOX &  
ASSOCIATES INC.  
3332 Cartier Ave.  
OTTAWA, ON K1Y 7P1  
Phone: (613) 739 9500  
Fax: (613) 722-0550

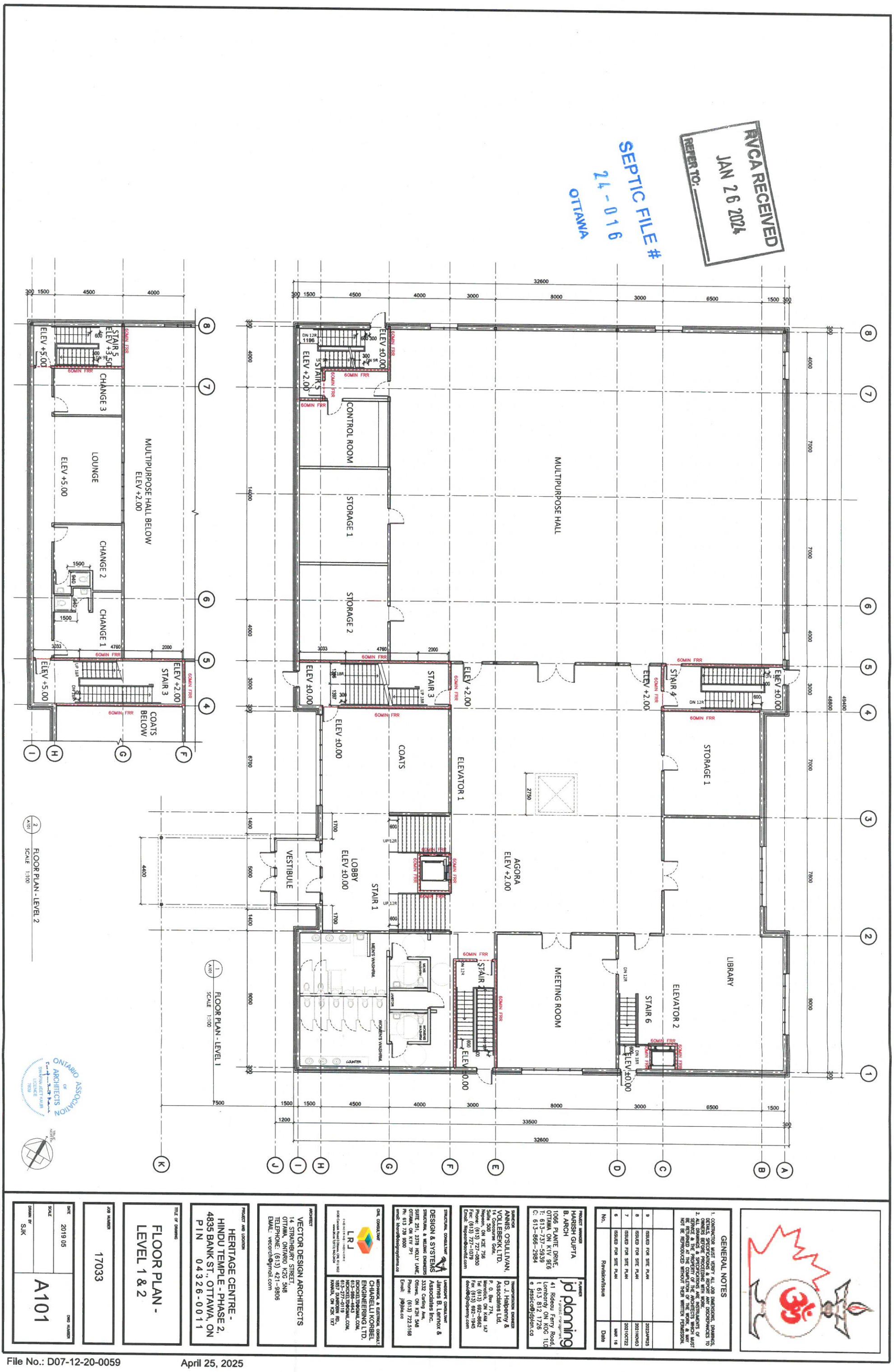
MECHANICAL & ELECTRICAL CONSULTANT  
DODDOKUTUMBAHANNA LTD.  
613-588-4463  
1040 CLOTHIER ROAD  
KINGSTON, ON K7M 1L7

GENERAL NOTES

1. CONTRACTORS MUST VERIFY ALL CO. DIMENSIONS, DRAWINGS, & REPORT ANY DISCREPANCIES TO THE OWNER.
2. ALL DRAWINGS & SPECIFICATIONS ARE INSTRUMENTS WHICH MUST BE OBSERVED & THE PROPERTY OF THE OWNER. COPIES OF THE DRAWINGS & SPECIFICATIONS MAY NOT BE REPRODUCED WITHOUT THEIR WRITTEN PERMISSION.



DATE 2019-05	JOB NUMBER 17033
SCALE	
OWNER BY SJK	A100







# PROPOSED ASSEMBLY BUILDING

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OTTAWA

9000L BALANCING TANK WITH  
LE40-SERIES SEWAGE PUMP TO  
BE INSTALLED WITH TIMER  
SETTING TO PREVENT PEAK  
LOADING IN THE NORWECO  
TREATMENT UNIT.

4" ABS PIPE @ MIN.  
2% SLOPE

CLAY SEPARATION LAYER TO BE  
INSTALLED ON SIDES FACING  
THE SEPTIC BED. SEE DETAIL ON  
URL DRAWING C301.

PROPOSED OVERLAND STORAGE  
EXTENT  
5 YEAR STORMPONDING EXTENT  
(HML = 98.15)  
MAXIMUM PONDING DEPTH = 0.50m  
TOTAL STORAGE PROVIDED =  
210.92m<sup>3</sup>

INSTALL NORWECO HK 4730L-3M  
TREATMENT UNIT. SYSTEM  
COMPONENTS TO MEET MINIMUM  
REQUIREMENTS AS PER ATTACHED  
SCHEMATIC.

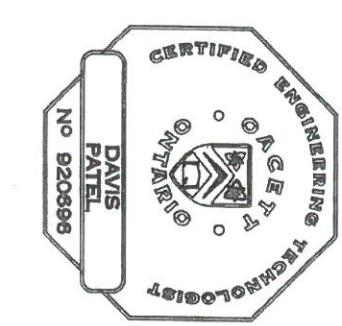
EXISTING PARKING AREA

INSTALL 600 GAL PUMP CHAMBER  
WITH 0.5 hp LIBERTY 280  
EFFLUENT PUMP, TIMER DOSED @  
15 SEC5./5 MINS.

FORCEMAN, POLYETHYLENE  
PIPE, 1.5" Ø, BURIED 1.5m  
DEEP, OR SELF DRAINING, OR  
INSULATED.

K-RAIN MULTIZONE VALVE MODEL  
660G CAMMED FOR 6 ZONE  
OPERATION TO BE PROTECTED  
WITH RISER AND LID.

NOTE: ANY CONTAMINATED  
MATERIAL PRESENT IN THE  
EXCAVATION AREA TO BE  
REMOVED AND REPLACED  
WITH SANDFILL.



DAVIS  
PATEL  
No 920696

PROPOSED STORM WATER  
DRAINAGE SYSTEM

NOTES:  
1. ALL TREATMENT UNITS AND LEACHING BED ARE TO BE INSTALLED IN  
ACCORDANCE WITH MINIMUM OBC CLEARANCE DISTANCES. ANY  
OMISSIONS OR INACCURACIES SHALL BE BROUGHT TO THE ATTENTION  
OF GVE AND OSO.

2. CARE IS TO BE EXERCISED DURING CONSTRUCTION ACTIVITIES NEAR  
OVERHEAD HYDRO WIRES.

3. EXISTING ELEVATIONS ARE APPROXIMATE. CONTRACTOR MUST  
VERIFY ALL ELEVATIONS AND DIMENSIONS PRIOR TO CONSTRUCTION.

4. SOIL CONDITIONS ARE ACCURATE FOR THE LOCATIONS SHOWN.  
CONTRACTOR MUST CONTACT THE DESIGN ENGINEER OR REGULATORY  
AUTHORITY SHOULD SOIL CONDITIONS DIFFER.

5. ALL DIMENSIONS AND CONDITIONS TO BE VERIFIED ON SITE.  
FIGURED DIMENSIONS TAKE PREDENCE OVER SCALE.

6. UTILITY LOCATES SHALL BE COMPLETED PRIOR TO ANY EXCAVATION.

7. THIS IS NOT A PLAN OF SURVEY AND SHALL NOT BE USED EXCEPT  
FOR THE PURPOSE INDICATED IN THE TITLE BLOCK.

8. THIS DOCUMENT IS COPYRIGHT PROTECTED AND IS THE SOLE  
PROPERTY OF GVE GROUP. THIS DRAWING SHALL NOT BE ALTERED IN  
ANY MANNER.

9. EXISTING LOT SERVICED WITH MUNICIPAL WATER.

METRIC:  
DISTANCES AND ELEVATIONS SHOWN ON THIS PLAN ARE IN METERS  
AND MAY BE CONVERTED TO FEET BY DIVIDING BY 0.3048.

LEGEND:  
X PROPOSED ELEVATION  
— EXISTING ELEVATION  
PROPOSED SEWAGE WORKS  
FENCE LINE  
PROPERTY LINE  
TEST PIT LOCATION  
TEMPORARY BENCH MARK  
(DESCRIPTION: TOP OF EAST ARM OF HYDRANT)

SEPARATION DISTANCES:  
1. MINIMUM CLEARANCE FROM SEPTIC PIPE TO:  
LOT LINE = 5.0m  
HOUSE = 7.0m  
DRILLED WELL = 17.0m  
2. MINIMUM CLEARANCE FROM TREATMENT UNITS TO:  
LOT LINE = 3.0m  
HOUSE = 1.5m  
DRILLED WELL = 15.0m

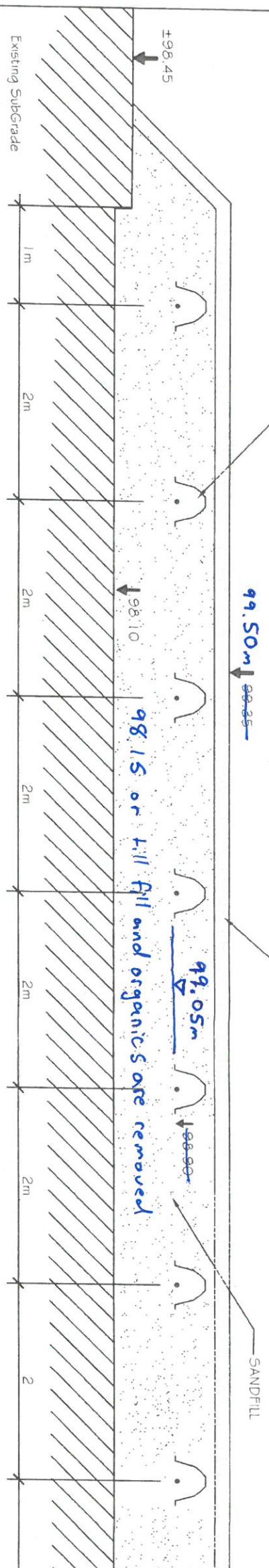
Drawn by DP	Drawn by DP	Checked by WS	
Rev.	Description	Date	Approved
Township	Plan#	Lot	Sublot
			SP6951-22-PRB
City	Green Valley	Date	12/01/24
	GREEN VALLEY ST.	Scale	1:200

THE HINDU TEMPLE OF OTTAWA CARLETON

BIODIFFUSOR  
CHAMBERS WITH 1-1/2"  
PVC DISTRIBUTION PIPE

Feb 1/24

1. THIS CROSS SECTION IS NOT TO SCALE, ALL FIGURED DIMENSIONS TAKE PRECEDENCE OVER SCALE.
2. THIS DOCUMENT IS COPYRIGHT PROTECTED AND IS THE SOLE PROPERTY OF GREEN VALLEY ENVIRONMENTAL INC. THIS DRAWING SHALL NOT BE ALTERED IN ANY MANNER.



#### PRETREATMENT TANK

- INSTALL MIN. 3215L PRETREATMENT TANK.
- A MAXIMUM OF 300mm OF SOIL SHALL COVER THE PRETREATMENT TANK.
- RISERS AND LIDS SHALL BE INSTALLED FOR EASE OF ACCESS

#### SHALLOW BURIED TRENCH BED

- THE TREATMENT UNIT SHALL CONSIST OF A NORWEKO HYDRO-KINETIC 4730L-3M TREATMENT UNIT.
- THE TREATMENT UNIT SHALL BE INSTALLED IN SERIES AND DOWN STREAM FROM THE PRETREATMENT TANK.
- THE TREATMENT UNIT SHALL PRODUCE A TERTIARY TREATMENT EFFLUENT QUALITY IN ACCORDANCE WITH COLUMN 2 AND 3 OPPOSITE A LEVEL IV TREATMENT UNIT OF TABLE 8.6.2-2. OF THE ONTARIO BUILDING CODE.
- THE TREATMENT UNIT SHALL BE INSTALLED ACCORDING TO THE MANUFACTURER'S SPECIFICATIONS BY A CERTIFIED INSTALLER.
- THE OWNER OF THE TREATMENT UNIT MUST ENTER INTO A MAINTENANCE AGREEMENT WITH THE MANUFACTURER'S REPRESENTATIVE.
- THE TREATMENT UNIT SHALL BE BACKFILLED AND COMPACTED IN LIFTS, WITH SELECT GRANULAR FILL, SUCH AS SAND OR CLEAR STONE.
- THE TOP OF THE TREATMENT UNIT SHALL BE ACCESSIBLE TO THE SURFACE. INSTALL RISERS AND LIDS TO SUIT.

#### MINIMUM CLEARANCE DISTANCE FROM LEACHING BED

- 3.0m FROM ANY PROPERTY LINE
- 1.5m FROM ANY STRUCTURE
- 15.0m FROM ANY DRILLED WELL

#### MINIMUM CLEARANCE DISTANCE FROM TANKS

- THE BACKWASH WATERS FROM ANY HOUSEHOLD TREATMENT SUCH AS WATER SOFTENER SHALL NOT DISCHARGE INTO THE SEWAGE SYSTEM CONTRACTOR SHALL BE QUALIFIED AND REGISTERED UNDER PART B OF THE ONTARIO BUILDING CODE.
- CONTRACTOR SHALL VISIT THE SITE AND REVIEW ALL DOCUMENTATION TO DETERMINE SUITABLE METHODS OF CONSTRUCTION.
- INSPECTION BY THE REGULATING AUTHORITIES IS A REQUIREMENT BY SOME REGULATING AUTHORITIES AND IS STRONGLY RECOMMENDED BY GREEN VALLEY ENVIRONMENTAL INC.
- IT IS RECOMMENDED THAT ALL TREES WITHIN 5m OF THE BED AREA BE REMOVED TO PREVENT ROOTS FROM INFILTRATING THE SYSTEM.
- ALL TANKS TO BE FILLED WITH WATER AFTER INSTALLATION.
- THE CONTRACTOR SHALL BE RESPONSIBLE TO LOCATE AND PROTECT ALL EXISTING UNDERGROUND SERVICES.
- SHOULD THE CONTRACTOR AT ANY TIME DURING CONSTRUCTION ENCOUNTER CONDITIONS THAT DIFFER FROM THE DESIGN CRITERIA IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO NOTIFY THE DESIGNER AND THE REGULATING AUTHORITY.
- GREEN VALLEY ENVIRONMENTAL INC. HAS PROVIDED DESIGNS BASED ON OUR INTERPRETATION OF THE ONTARIO BUILDING CODE AND THE TEST HOLES DUG ON THE PROPERTY.

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#### PUMP & PUMP CHAMBER

- INSTALL 800 GAL PUMP CHAMBER WITH 0.5hp LIBERTY 280 EFFLUENT PUMP, TIMER DOSED @ 15 sec./5 mins

Drawn By	Drawn By	Checked By	
Rev.	Description	Date	Approved
Township	Plan#	Lot	Sublot
County	Section	Block	Con

4835 BANK ST.  
GREEN VALLEY ENVIRONMENTAL  
On Site Septic Treatment Plan for the Residence of  
THE HINDU TEMPLE OF OTTAWA CARLETON



# Permit

## Part 8 – Sewage System Ontario Building Code

Do Not Complete	24-016
Permit No	
Revision No	
Date	
Related Application	

**A copy of this permit must be posted on the property at all time during construction. OBC, Division C — Part 1, Section 1.3.2.1**

This permit verifies that the on-site sewage system was reviewed and approved for construction under the *Ontario Building Code* and *O.Reg. 323/12* as amended by *O.Reg. 151/13*.

Inspected & Recommended by: Ryan Hiemstra Owner: Hindu Temple of Ottawa Carleton  
Inspection Date & Time: \_\_\_\_\_ Weather: \_\_\_\_\_  
Civic Address: 4835 Bank Street Legal: Lot 22, Con 5RF, R.Plan 5R3156  
In the former Township/City of Gloucester

Design Flow for Commercial / Institutional / Industrial (as per Table 8.2.1.3.B)

Q: 500 x 8 L/day (assembly hall) = 4000 L/day

pretreatment tank	<input checked="" type="checkbox"/>	_____ L	weigh bills for	<input type="checkbox"/> yes	<input checked="" type="checkbox"/> no
effluent filter	YES		grain size analysis required	<input type="checkbox"/> yes	<input checked="" type="checkbox"/> no
pump rate	Timer dosed		site to be scarified	<input checked="" type="checkbox"/> yes	<input type="checkbox"/> no
treatment unit	Norweco HK 4730-3M		clay seal inspection	<input type="checkbox"/> yes	<input checked="" type="checkbox"/> no
number of units	1		mantle required	<input type="checkbox"/> yes	<input checked="" type="checkbox"/> no
			sub-grade inspection	<input checked="" type="checkbox"/> yes	<input type="checkbox"/> no

**ELEVATION**  In Ground  Partially Raised  Fully Raised

**TYPE OF SYSTEM**

Trench  
 Pipe and Stone or  Chambers

type of chamber \_\_\_\_\_

loading area \_\_\_\_\_ m<sup>2</sup>

total trench length \_\_\_\_\_ m

trench configuration \_\_\_\_\_

Dispersal Bed

BMEC  Type A  Type B

stone \_\_\_\_\_ m<sup>2</sup>

sand \_\_\_\_\_ m<sup>2</sup>

pipe \_\_\_\_\_

weight of sand \_\_\_\_\_ kg

Shallow Buried Trench

pipe length 156.96 (12@13.08) m

orifice spacing 0.6 m

Filter Media Bed

stone \_\_\_\_\_ m<sup>2</sup>

extended base \_\_\_\_\_ m<sup>2</sup>

pipe \_\_\_\_\_

weight of filter media \_\_\_\_\_ kg

loading area \_\_\_\_\_ m<sup>2</sup>

Class 5 Holding Tank

Septic Tank Only

Manager, Septic System Approvals: Tony Davidson

Permit Date: JUNE 17, 2024

Comments: 1. There shall be no preparation of food or service of food within the assembly building

2. RVCA to inspect subgrade before the placement of sandfill

maintenance/pumping required

ESA permit # required

engineer to verify

subgrade

squirt height

Class 5 Holding Tank approval only valid for three years from date of issue

Manager, Septic System Approvals: \_\_\_\_\_

Revision Date: \_\_\_\_\_

Comments: \_\_\_\_\_



# Green Valley Environmental Inc.

## LETTER OF AUTHORIZATION

**Owner:** Hindu Temple of Ottawa Carleton (attention: Harish Gupta)  
**Address:** 4835 Bank Street  
Ottawa, Ontario

**Phone No.:** 613-737-5939      **Cell No.:** 613-866-2984  
**Work No.:**      **Fax No.:**

### LOCATION OF PROPERTY:

**Lot No.:** 22  
**Concession No.:** 5RF  
**Sub lot/Part No.:**  
**R. Plan No.:** 5R3156  
**Civic Address:** 4835 Bank Street  
**Municipality:** Gloucester  
**Roll No.:**



**Commercial:** (provide description of building and intended use)  
Place of Worship (Existing Building)  
7 Apartments (2 person per apartment)

I, the above – mentioned authorize Green Valley Environmental Services to act as my agent to apply for and obtain a sewage system permit from the responsible Approval Agency.

Signature: Jessica Arthurs

Date: January 11, 2024

# Application for a Permit to Construct or Demolish

This form is authorized under subsection 8(1.1) of the Building Code Act, 1992

For use by Principal Authority	
Application number:	Permit number (if different):
Date received:	Roll number:

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## OTTAWA SEPTIC SYSTEM OFFICE

Application submitted to: \_\_\_\_\_  
(Name of municipality, upper-tier municipality, board of health or conservation authority)

### A. Project information

Building number, street name <i>4835 Bank St.</i>		Unit number	Lot/con. <i>22/5RF</i>
Municipality <i>Gloucester</i>	Postal code <i>K1X 1G6</i>	Plan number/other description <i>5R3156</i>	
Project value est. \$		Area of work (m <sup>2</sup> )	

### B. Purpose of application

New construction	Addition to an existing building	Alteration/repair	Demolition	Conditional Permit
Proposed use of building <i>Commercial worship building</i>		Current use of building <i>Commercial worship building</i>		

### Description of proposed work

*Install a new septic system for existing temple/worship building. Revision to permit 21-343*

C. Applicant	Applicant is:	Owner or	<input checked="" type="checkbox"/> Authorized agent of owner		
Last name <i>Patel</i>	First name <i>Navis</i>	Corporation or partnership <i>Green Valley Environmental Inc.</i>			
Street address <i>6107 First Line Rd.</i>			Unit number	Lot/con.	
Municipality <i>North Gloucest</i>	Postal code <i>K4M 1A7</i>	Province <i>ON</i>	E-mail <i>engineering@greenvalley.ca</i>		
Telephone number <i>(613) 692-2616</i>	Fax <i>(613) 692-1802</i>	Cell number <i>( )</i>			

### D. Owner (if different from applicant)

Last name <i>Gupta</i>	First name <i>Harish</i>	Corporation or partnership <i>The Hindu Temple</i>			
Street address <i>4835 Bank St.</i>			Unit number	Lot/con. <i>22/5RF</i>	
Municipality <i>Gloucester</i>	Postal code <i>K1X 1G6</i>	Province <i>ON</i>	E-mail		
Telephone number <i>(613) 737-5939</i>	Fax <i>( )</i>	Cell number <i>(613) 866-2984</i>			

Application for a Permit to Construct or Demolish – Effective January 1, 2014

**E. Builder (optional)**

Last name	First name	Corporation or partnership (if applicable)	
Street address		Unit number	4 lot/con. <i>JUN - 4 2024</i>
Municipality	Postal code	Province	E-mail
Telephone number ( )	Fax ( )	Cell number ( )	

**F. Tarion Warranty Corporation (Ontario New Home Warranty Program)**

i. Is proposed construction for a new home as defined in the <i>Ontario New Home Warranties Plan Act</i> ? If no, go to section G.	Yes	No <input checked="" type="checkbox"/>
ii. Is registration required under the <i>Ontario New Home Warranties Plan Act</i> ?	Yes	No <input checked="" type="checkbox"/>

iii. If yes to (ii) provide registration number(s): \_\_\_\_\_

**G. Required Schedules**

i) Attach Schedule 1 for each individual who reviews and takes responsibility for design activities.

ii) Attach Schedule 2 where application is to construct on-site, install or repair a sewage system.

**H. Completeness and compliance with applicable law**

i) This application meets all the requirements of clauses 1.3.1.3 (5) (a) to (d) of Division C of the Building Code (the application is made in the correct form and by the owner or authorized agent, all applicable fields have been completed on the application and required schedules, and all required schedules are submitted).	Yes <input checked="" type="checkbox"/>	No
Payment has been made of all fees that are required, under the applicable by-law, resolution or regulation made under clause 7(1)(c) of the <i>Building Code Act</i> , 1992, to be paid when the application is made.	Yes <input checked="" type="checkbox"/>	No
ii) This application is accompanied by the plans and specifications prescribed by the applicable by-law, resolution or regulation made under clause 7(1)(b) of the <i>Building Code Act</i> , 1992.	Yes <input checked="" type="checkbox"/>	No
iii) This application is accompanied by the information and documents prescribed by the applicable by-law, resolution or regulation made under clause 7(1)(b) of the <i>Building Code Act</i> , 1992 which enable the chief building official to determine whether the proposed building, construction or demolition will contravene any applicable law.	Yes <input checked="" type="checkbox"/>	No
iv) The proposed building, construction or demolition will not contravene any applicable law.	Yes <input checked="" type="checkbox"/>	No

**I. Declaration of applicant**

I Davis Patel declare that:  
 (print name)

1. The information contained in this application, attached schedules, attached plans and specifications, and other attached documentation is true to the best of my knowledge.
2. If the owner is a corporation or partnership, I have the authority to bind the corporation or partnership.

Date

May 27, 2024

Signature of applicant

Davis

Personal information contained in this form and schedules is collected under the authority of subsection 8(1.1) of the *Building Code Act*, 1992, and will be used in the administration and enforcement of the *Building Code Act*, 1992. Questions about the collection of personal information may be addressed to: a) the Chief Building Official of the municipality or upper-tier municipality to which this application is being made, or, b) the inspector having the powers and duties of a chief building official in relation to sewage systems or plumbing for an upper-tier municipality, board of health or conservation authority to whom this application is made, or, c) Director, Building and Development Branch, Ministry of Municipal Affairs and Housing 777 Bay St., 2nd Floor, Toronto, M5G 2E5 (416) 585-6666

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## Schedule 1: Designer Information

Use one form for each individual who reviews and takes responsibility for design activities with respect to the project.

## A. Project Information

Building number, street name	4835 Bank St.		
Unit no.			
Municipality	Postal code	Plan number/ other description	
Guelph	KIX 1G6	5R3156	

## B. Individual who reviews and takes responsibility for design activities

Name	Firm	Green Valley Environmental	
Street address	6107 First Line Rd.	Unit no.	Lot/con.
Municipality	Postal code	Province	E-mail
North Guelph	K4M 1A7	ON	engineering@greenvy.ca
Telephone number	Fax number	Cell number	( )
(613) 692-2616	(613) 692-1802		

## C. Design activities undertaken by individual identified in Section B. [Building Code Table 3.5.2.1. of Division C]

House	HVAC – House	Building Structural
Small Buildings	Building Services	Plumbing – House
Large Buildings	Detection, Lighting and Power	Plumbing – All Buildings
Complex Buildings	Fire Protection	On-site Sewage Systems

Description of designer's work

Design a new septic system to suit existing commercial building. Revision to permit 21-343

## D. Declaration of Designer

I Davis Patel declare that (choose one as appropriate):  
(print name)

I review and take responsibility for the design work on behalf of a firm registered under subsection 3.2.4 of Division C of the Building Code. I am qualified, and the firm is registered, in the appropriate classes/categories.

Individual BCIN: 119685Firm BCIN: 16035

I review and take responsibility for the design and am qualified in the appropriate category as an "other designer" under subsection 3.2.5 of Division C, of the Building Code.

Individual BCIN: \_\_\_\_\_

Basis for exemption from registration: \_\_\_\_\_

The design work is exempt from the registration and qualification requirements of the Building Code.

Basis for exemption from registration and qualification: \_\_\_\_\_

I certify that:

1. The information contained in this schedule is true to the best of my knowledge.
2. I have submitted this application with the knowledge and consent of the firm.

Date May 27, 2024Signature of Designer Davis

## NOTE:

1. For the purposes of this form, "individual" means the "person" referred to in Clause 3.2.4.7(1) (c) of Division C, Article 3.2.5.1. of Division C, and all other persons who are exempt from qualification under Subsections 3.2.4. and 3.2.5. of Division C.
2. Schedule 1 is not required to be completed by a holder of a license, temporary license, or a certificate of practice, issued by the Ontario Association of Architects. Schedule 1 is also not required to be completed by a holder of a license to practise, a limited license to practise, or a certificate of authorization, issued by the Association of Professional Engineers of Ontario.

## Schedule 2: Sewage System Installer Information

<b>A. Project Information</b>			
Building number, street name 4835 Bank St.		Unit number	Lot/con. 2215RF
Municipality Gloucester	Postal code K1X 1G6	Plan number/ other description 5R3156	
<b>B. Sewage system installer</b>			
Is the installer of the sewage system engaged in the business of constructing on-site, installing, repairing, servicing, cleaning or emptying sewage systems, in accordance with Building Code Article 3.3.1.1, Division C?			
<input checked="" type="checkbox"/> Yes (Continue to Section C)		<input type="checkbox"/> No (Continue to Section E)	
		Installer unknown at time of application (Continue to Section E) <i>RECEIVED MAY - 2024</i>	
<b>C. Registered installer information (where answer to B is "Yes")</b>			
Name Green Valley Environmental	BCIN 11234		
Street address 6107 First Line Rd.	Unit number	Lot/con.	
Municipality North Glouster	Postal code K4M 1A7	Province ON	E-mail
Telephone number (613) 692-2616	Fax (613) 692-1802	Cell number (613) 229-3900	
<b>D. Qualified supervisor information (where answer to section B is "Yes")</b>			
Name of qualified supervisor(s) Bill Seabrook	Building Code Identification Number (BCIN) 11234		
<b>E. Declaration of Applicant:</b>			
<i>Davis Patel</i> (print name)			declare that:
I am the applicant for the permit to construct the sewage system. If the installer is unknown at time of application, I shall submit a new Schedule 2 prior to construction when the installer is known;			
<b>OR</b> I am the holder of the permit to construct the sewage system, and am submitting a new Schedule 2, now that the installer is known.			
I certify that:			
<ol style="list-style-type: none"> <li>1. The information contained in this schedule is true to the best of my knowledge.</li> <li>2. If the owner is a corporation or partnership, I have the authority to bind the corporation or partnership.</li> </ol>			
Date May 27, 2024	Signature of applicant <i>Bank</i>		



**Schedule 4**  
**Proposed Services**  
Complete Sections 1 thru 7

**1. Engineered**

Yes  
 No

**3. Type of work proposed**

New Installation  
 Replacement  
 Alteration

**5. Residential** Sewage Design Flow Info.

Bedrooms \_\_\_\_\_

House (floor area) \_\_\_\_\_ m<sup>2</sup>

People \_\_\_\_\_

Total Fixture Units \_\_\_\_\_ (Schedule 8)

Residential Flow \_\_\_\_\_ L/day

**7. Type of System**

Treatment Unit Norweco 5670 HK-3M  
 Class 2 – Leaching Pit  
 Class 3 – Cesspool  
 Class 4 – Shallow Buried Trench  
5 Runs, 28.3m each.

Class 4 – Trench (Schedule 9)

Fully raised  
 Partially raised  
 In-ground

Class 4 – Filter Media (Schedule 10)

Fully raised  
 Partially raised  
 In-ground

**2. Water supply**

Proposed  
 Existing

**4. Type of Well**

Dug/bored/Sandpoint well  
 Drilled well  
 Municipal  
 Other

**6. Sewage Design Flow Other Occupancies**

Design Flow 4200 L/day

Detailed sewage flow calculations:

Worship building → 250 people × 8 = 2000 L/day  
4 Single Residential Apartments → 8 people × 275 = 2200 L/day  
Total Flow → 4200 L/day

Class 4 – BMEC Area Bed (Schedule 11)

Fully raised  
 Partially raised  
 In-ground

Class 4 – “Type A” Dispersal (Schedule 13)

Fully raised  
 Partially raised  
 In-ground

Class 4 – “Type B” Dispersal (Schedule 14)

Fully raised  
 Partially raised  
 In-ground

Class 5 – Holding Tank (9000L min)

Tank/TreatmentUnit/PumpChamber ONLY

Effluent Filter/Risers ONLY



# Green Valley Environmental

23-May-24

The Hindu Temple

4835 Bank St., Ottawa (Existing Building)

North Side Septic Tank (North half of bldg: Ground Floor Toilets & Basement fixtures)			
250 People(no Kitchen)	8L/d	Per seat	2000 L/day
Sub-total			2000 L/day

South Side Septic Tank (South half of bldg: 4 Apartments & Basement fixtures)			
4 Apartments (8 people)	275L/d	Per Person	2200 L/day
Sub-total			2200 L/day

Total			4200 L/day
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**Schedule 5  
Sewage System Details**

Do Not Complete	<b>R.I.C.A. RECEIVED</b>
Permit No.	
Revision No.	
Date	JUN - 4 2024

Type of System	<u>Class 4 Shallow Buried Trench Bed (Schedule 4)</u>		
Septic/Holding Tank Size:	<u>9000</u>	Litres x 2	Make: <u>Existing septic tank</u>
Septic Tank Effluent Filter Make:	<u>POLYLOK</u>		
Model:	<u>PL250</u>		

Treatment Unit - Make & Model Norwesco HK 5670 (Tertiary Treatment System)  
 Number of Units: 1  
 Refer to Typical Drawing # PC-5-1176  
 Mantle Information:  
 Native or imported = 15m in N/A direction(s)  
 Slope subgrade 1:4 % slope  
direction(s)

Other: \_\_\_\_\_  
 Pump(s) required Liberty 280, 0.5 hp → T  
 Pump Rate Liberty 280, 0.5 hp → F  
 Note: Alarm required for all pumping systems  
 T: Timer closed  
 F: Float operated

Site to be Scarified (If clay)	YES <u>NO</u>
Clay Seal Required (If bedrock)	YES <u>NO</u>

**Trench**

Distribution Pipe Length \_\_\_\_\_ m

Loading Area \_\_\_\_\_ m<sup>2</sup>

Type of Chamber \_\_\_\_\_

Length of Chamber \_\_\_\_\_ m

**Dispersal Bed**

**BMEC**  **Type A**  **Type B**

Stone \_\_\_\_\_ m<sup>2</sup>

Sand \_\_\_\_\_ m<sup>2</sup>

Pipe \_\_\_\_\_ m<sup>2</sup>

Linear Loading \_\_\_\_\_ L/m<sup>2</sup>

**Shallow Buried Trench**

Pipe Length 141.7 m  
(5 x 28.34m)

**Filter Media Bed**

Stone \_\_\_\_\_ m<sup>2</sup>

Extended Base \_\_\_\_\_ m<sup>2</sup>

Pipe \_\_\_\_\_ m

Weight of Filter Media \_\_\_\_\_ Kg

Loading Area \_\_\_\_\_ m

**Tank/Treatment Unit/Pump Chamber Replacement ONLY**

**Effluent Filter & Riser ONLY**

Construction Notes:

Moles within 5m of the septic system to be removed. Any contaminated material present during the excavation to be removed.



Do Not Complete

Permit #

Revision #

Date

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JUN - 4 2024

Schedule 6

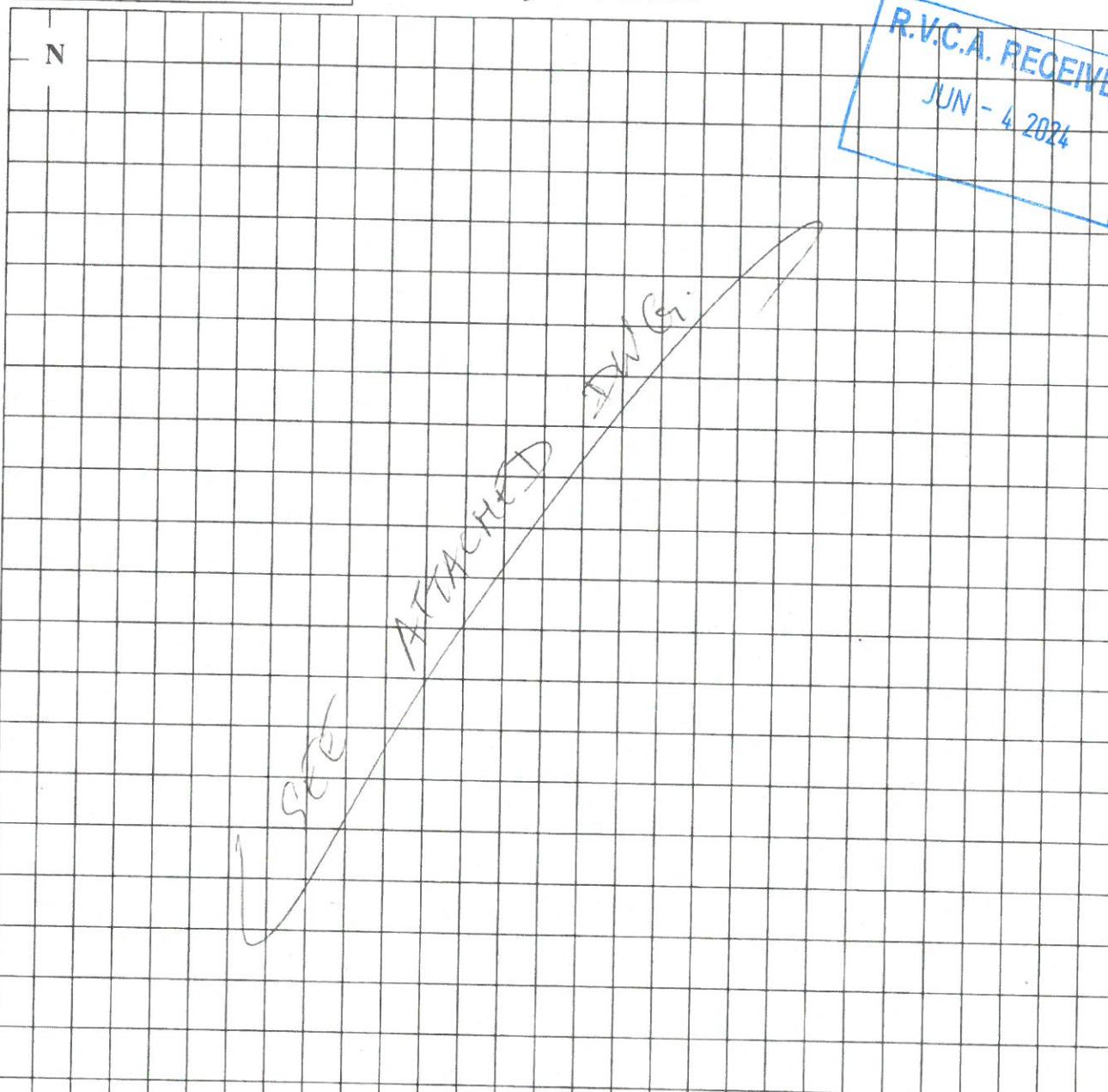
Soil and Water Table Information  
(Minimum depth of test pit: 2 metres)

Name of Applicant/Agent: <u>Davis Patel</u>																																									
Date: <u>30 May, 2024</u> Time: <u>10:05 AM</u>																																									
Applicant/Agent Signature: <u>Kash</u>																																									
Inspector: <u>Ryan Hiemstra</u>																																									
Date: <u>June 4/24</u> Time: <u>11:45 am</u>																																									
Inspector Signature: <u>Ryan Hiestra</u>																																									
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<b>LEGEND</b> BR = Bedrock GWT = Ground water table																																									
HGWT = High ground water table M = metres																																									
EG = Existing grade T = percolation rate																																									



Scale: 1 Block = NTS

**Schedule 7**  
**Layout Section**



- Dug Well
- Drilled Well
- ▲ Neighbouring Homes
- ◊ Benchmark
- Tile Drainage
- Property Line

Elevations (metric only)

B.M. 100.17 m

B.M. Description East arm of hydrant  
located west of south west entrance

Exact Location to site

Min. of 5 elevations in proposed system area (in X pattern)

X<sub>1</sub> \_\_\_\_\_ X<sub>2</sub> \_\_\_\_\_  
X<sub>3</sub> \_\_\_\_\_ X<sub>4</sub> \_\_\_\_\_  
X<sub>5</sub> \_\_\_\_\_ X<sub>6</sub> (toe) \_\_\_\_\_  
X<sub>7</sub> \_\_\_\_\_ X<sub>8</sub> \_\_\_\_\_



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Revision #  
Date JUN - 4 2024

**Schedule 8**  
**Fixture unit count**

Fixtures	# South	+	# North	X	unit count	=	Fixture Count
<b>Bathroom</b>							
Bathroom group (toilet, sink and tub or shower) installed in the <u>same</u> room	4	+		X	6	=	
Bathtub with/without overhead shower		+		X	1.5	=	
Shower stall		+		X	1.5	=	
Wash basin (SINK) (1½inch trap) <u>13</u>	3	+	13	X	1.5	=	
Watercloset (TOILET) tank operated	1	+	4	X	4	=	
Bidet		+		X	1	=	
<b>Kitchen</b>							
Dishwasher	0	+	0	X	1	=	
Sink with/without garbage grinder(s), domestic and other small type single, double or 2 single with a common trap	4	+		X	1.5	=	
<b>Other</b>							
Domestic washing machine	1	+		X	1.5	=	
Combination sink and laundry tray single or double (Installed on 1½ trap)		+		X	1.5	=	

40      35.5      \*Total: 75.5

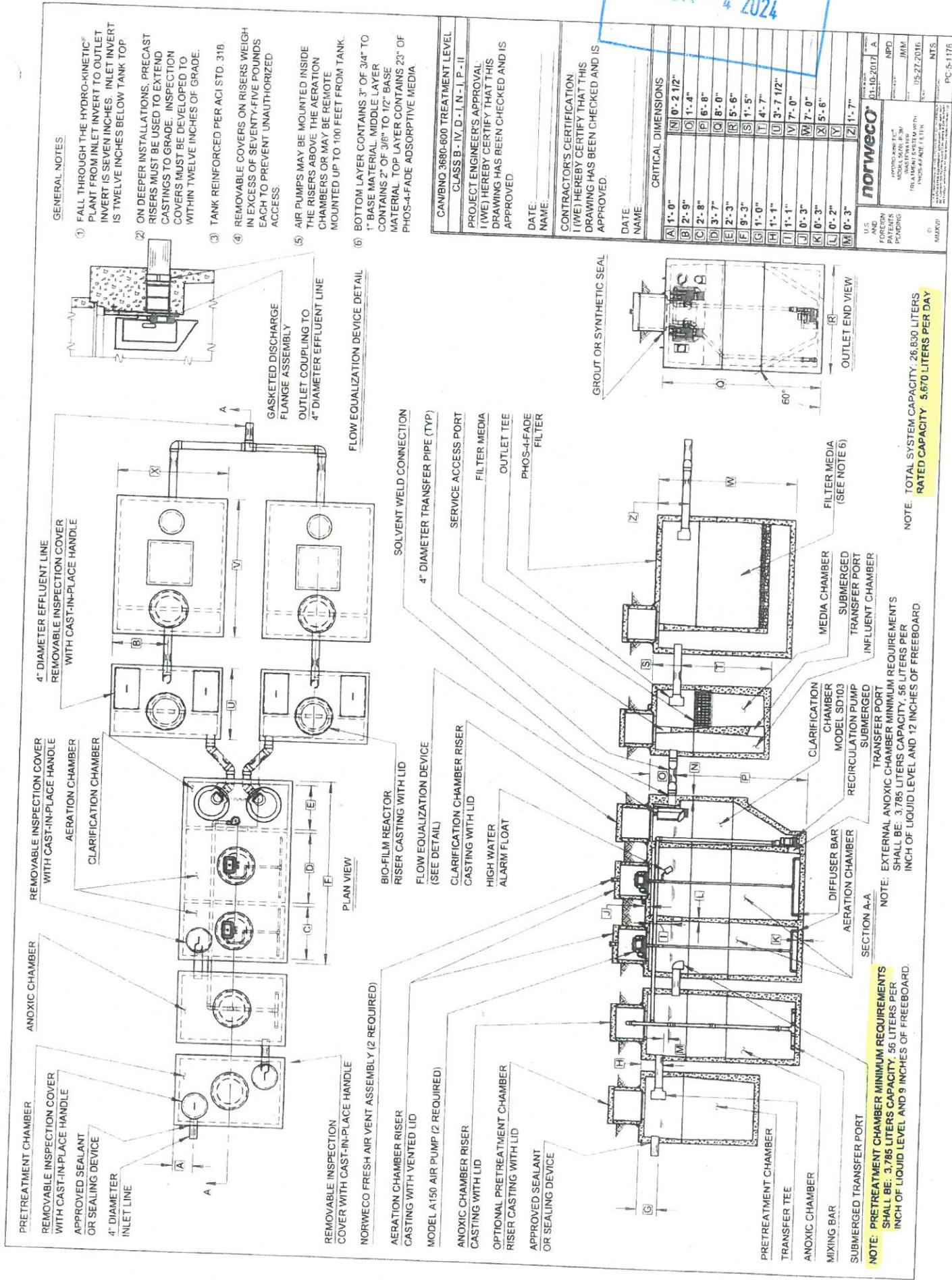
\*Insert the TOTAL in section 5 of Schedule 4 (0.Reg 151/13 Table 7.4.9.3)

1. **Sump pumps and floor drains are not to be connected to the sewage system.** Connection of such fixtures to a sewage system may lead to a hydraulic failure of the said system. The above mentioned fixtures should be discharged separately to an approved Class 2 (leaching pit) sewage system.
2. Where laundry waste is not more than 20% of the total daily design sanitary sewage flow, it may discharge to a sewage system (Part 8, OBC, 8.1.3.1(2)).

*[Signature]*  
Agent/Owner signature

Date

*May 13, 2024*



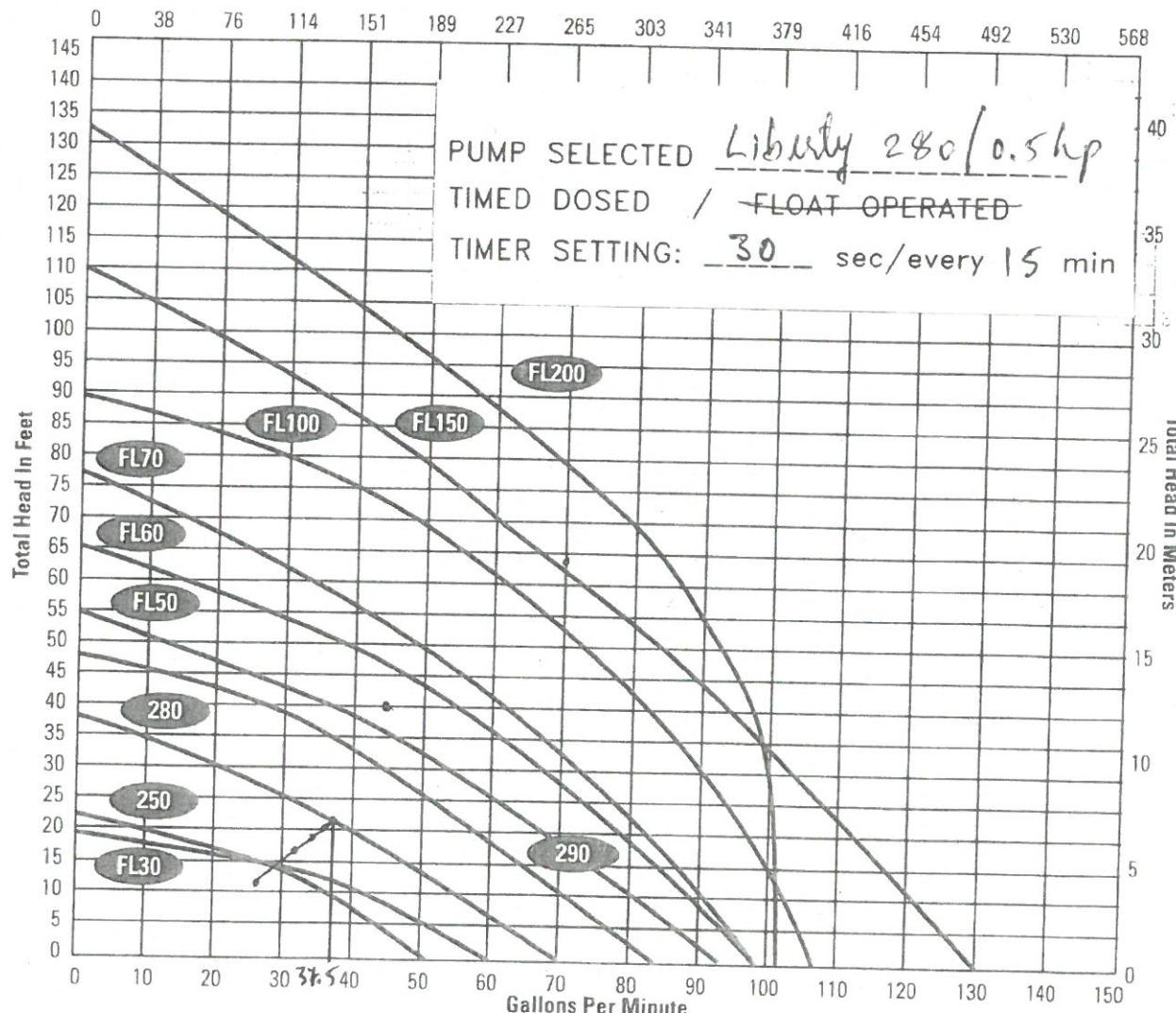


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JUN - 4 2024

## Effluent Pumps

### Performance Curve Data 60 hz.

Liters Per Minute



innovate. evolve.

## Existing Worship Building

diameter of orifice(inch):

Squirt height (feet):

Discharge of orifice (US gal/orifice x min)

Flow in a lateral (US gal/min x lateral)

Total discharge (US gal/min)

### Total discharge (L/min)

Total discharge (Imp. gal/min)

### Total Dynamic Head (ft)

		(inches/in)				
input	Length of force main(m)	27.00	88.58	88.58	88.58	88.58
input	Diameter of force main (in/cm)	3.81	1.50	1.50	1.50	1.50
input	Length of manifold (m)	8.00	26.20	26.20	26.20	26.20
input	Diameter of manifold (in/cm)	3.81	1.50	1.50	1.50	1.50
input	Length of lateral (m)	28.34	92.98	92.98	92.98	92.98
input	Diameter of lateral (in)	3.81	1.50	1.50	1.50	1.50
output	Friction loss in forcemain (m/ft)	0.32	1.07	2.49	3.40	3.84
output	Friction loss in manifold (m/ft)	0.03	0.11	0.25	0.29	0.33
output	Friction loss in lateral (m/ft)	0.11	0.37	0.87	1.03	1.19
estimated	Fittings' loss (estimated) (m/ft)	3.05	10.00	10.00	10.00	10.00
input	Residual head on orifice (ft)	0.61	2.00	5.00	6.00	7.00
input	Elevation difference(assumed,	4.00	13.12	13.12	13.12	13.12

output	TDH (estimated) (m/ft)	Q (gpm)						
8.13	26.67 11.22	31.73 17.74	33.39 19.43	35.04 20.99	36.69 22.44	38.33 22.44	56.11 23.80	35.48

6107 First Line Road, Manotick, Ontario, K4M 1A7  
Box 882, Tel. (613) 692-2616. Fax: (613) 693-1802

# HARISH GUPTA

1066 PLANTE DRIVE, OTTAWA, ONTARIO K1V-9E6 TEL: 613.737.5939  
e-mail: [harishgee40@yahoo.com](mailto:harishgee40@yahoo.com)

May 13, 2024

Rideau Valley Conservation Authority  
3889 Rideau Valley Drive  
Ottawa ON  
K4M 1A5



**Attn: Mr. Terry Davidson**

**Re: Hindu Temple, 4835 Bank Street Ottawa ONT**

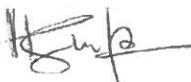
This relates to septic permits (expired and to be renewed) for the existing and proposed development.

This will confirm as follows:

- Total occupants in existing building- 250 individuals.
- There will not be any cooking, existing warm up kitchen and related items will be removed.

Attached is an updated plan to reflect noted revisions.

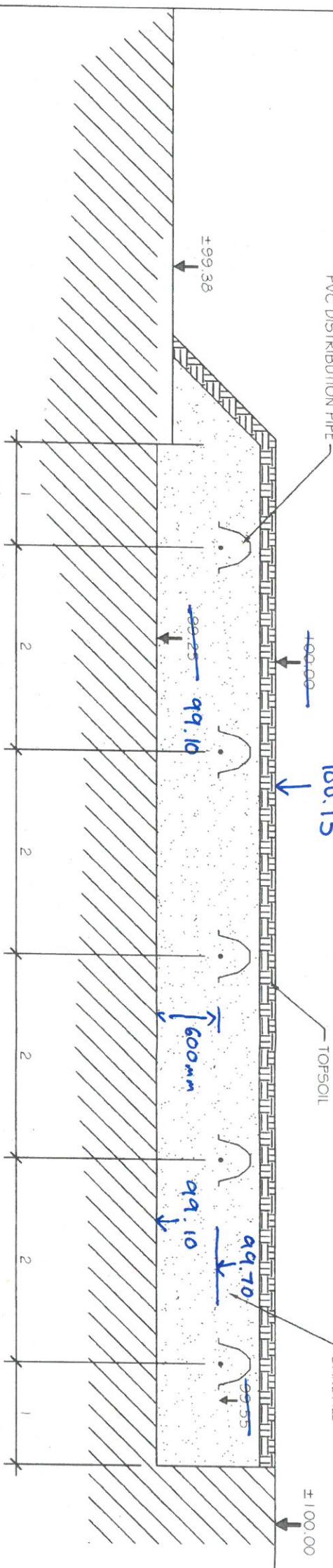
Trusting this is the information you required in order to re-new the expired permits.

A handwritten signature in black ink, appearing to read "H. Gupta".

Harish Gupta B. Arch

Project Manager





#### PRETREATMENT TANK

- INSTALL MIN. 4500L PRETREATMENT TANK.
- A MAXIMUM OF 300mm OF SOIL SHALL COVER THE PRETREATMENT TANK.
- RISERS AND LIDS SHALL BE INSTALLED FOR EASE OF ACCESS.

#### NORWECCO TREATMENT UNIT

- THE TREATMENT UNIT SHALL CONSIST OF A NORWECCO HYDRO-KINETIC 5670-3M TREATMENT UNIT.
- THE TREATMENT UNIT SHALL BE INSTALLED IN SERIES AND DOWN STREAM FROM THE PRETREATMENT TANK.
- THE TREATMENT UNIT SHALL PRODUCE A TERTIARY TREATMENT EFFLUENT QUALITY IN ACCORDANCE WITH COLUMN 2 AND 3 OPPOSITE A LEVEL IV TREATMENT UNIT OF TABLE B.6.2.2. OF THE ONTARIO BUILDING CODE.
- THE TREATMENT UNIT SHALL BE INSTALLED ACCORDING TO THE MANUFACTURER'S SPECIFICATIONS BY A CERTIFIED INSTALLER.
- THE OWNER OF THE TREATMENT UNIT MUST ENTER INTO A MAINTENANCE AGREEMENT WITH THE MANUFACTURER'S REPRESENTATIVE.
- THE TREATMENT UNIT SHALL BE BACKFILLED AND COMPACTED, IN LIFTS, WITH SELECT GRANULAR FILL, SUCH AS SAND OR CLEAR STONE.
- THE TOP OF THE TREATMENT UNIT SHALL BE ACCESSIBLE TO THE SURFACE. INSTALL RISERS AND LIDS TO SUIT.

#### NORWECCO FILTER VAULT(S)

- FILTER VAULT(S) SHALL BE INSTALLED IN ACCORDANCE WITH MANUFACTURER'S SPECIFICATIONS
- FILTER VAULT(S) SHALL BE INSTALLED IN SERIES AND DOWN STREAM FROM THE TREATMENT UNIT
- FILTER VAULT(S) SHALL BE ACCESSIBLE TO THE SURFACE.
- INSTALL RISERS AND LIDS TO SUIT.

#### PUMP & PUMP CHAMBER

- INSTALL 600GAL PUMP CHAMBER WITH 0.5hp LIBERTY 280 EFFLUENT PUMP, FLOAT OPERATED ON THE NORTH SIDE OF THE BUILDING
- INSTALL 600GAL PUMP CHAMBER WITH 0.5hp LIBERTY 280 EFFLUENT PUMP, TIME DOSED AT 30SEC./15MIN. ON THE SOUTH SIDE OF THE BUILDING.

#### SHALLOW BURIED TRENCH BED

- THE DISPERSAL BED SHALL CONSIST OF A TOTAL LENGTH EQUAL TO Q30 = 4200/30 = 140 TOTAL LENGTH USED = 141.7m SAND FILL SHALL EXTEND 1.0m ON ALL SIDES. REMOVE LAYER OF TOP SOIL TO APPROXIMATE FOOT PRINT OF SEPTIC BED AND SIDE SLOPES. THE PRESSURIZED DISTRIBUTION SYSTEM SHALL HAVE A PRESSURE HEAD OF NOT LESS THAN 600mm WHEN MEASURED AT THE MOST DISTANT POINT FROM THE PUMP.
- DISPERAL BED SHALL BE BACKFILLED SO AS TO ENSURE THAT THE SURFACE WILL NOT FORM ANY DEPRESSIONS.
- ALL SIDE SLOPES SHALL BE AT 1:4
- AT NO POINT DURING OR AFTER CONSTRUCTION SHALL A WHEELED VEHICLE DRIVE OVER THE SEPTIC BED AREA.
- EACH RUN SHALL CONSIST OF ONLY FULL CHAMBERS.
- SEPTIC DESIGN BASED ON ADS BIO3 CHAMBERS. EACH RUN SHALL CONSIST OF 13 FULL ADS BIO3 CHAMBERS WITH A TOTAL OF 65 FULL BIO3 CHAMBERS FOR THE ENTIRE SEPTIC BED.

#### MINIMUM CLEARANCE DISTANCE FROM LEACHING BED

- 4.2m FROM ANY PROPERTY LINE
- 6.2m FROM ANY STRUCTURE
- 16.2m FROM ANY DRILLED WELL

#### MINIMUM CLEARANCE DISTANCE FROM TANKS

- 3.0m FROM ANY PROPERTY LINE
- 1.5m FROM ANY STRUCTURE
- 15.0m FROM ANY DRILLED WELL

#### GENERAL

- THE BACKWASH WATERS FROM ANY HOUSEHOLD TREATMENT SUCH AS WATER SOFTENER SHALL NOT DISCHARGE INTO THE SEWAGE SYSTEM
- CONTRACTOR SHALL BE QUALIFIED AND REGISTERED UNDER PART 8 OF THE ONTARIO BUILDING CODE.
- CONTRACTOR SHALL VISIT THE SITE AND REVIEW ALL DOCUMENTATION TO DETERMINE SUITABLE METHODS OF CONSTRUCTION.
- INSPECTION BY THE REGULATING AUTHORITIES IS A REQUIREMENT BY SOME REGULATING AUTHORITIES AND IS STRONGLY RECOMMENDED BY GREEN VALLEY ENVIRONMENTAL INC.
- IT IS RECOMMENDED THAT ALL TREES WITHIN 5m OF THE BED AREA BE REMOVED TO PREVENT ROOTS FROM INFILTRATING THE SYSTEM.
- THE CONTRACTOR SHALL BE RESPONSIBLE TO LOCATE AND PROTECT ALL EXISTING UNDERGROUND SERVICES.
- SHOULD THE CONTRACTOR AT ANY TIME DURING CONSTRUCTION ENCOUNTER CONDITIONS THAT DIFFER FROM THE DESIGN CRITERIA IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO NOTIFY THE DESIGNER AND THE REGULATING AUTHORITY.
- GREEN VALLEY ENVIRONMENTAL INC. HAS PROVIDED DESIGNS BASED ON OUR INTERPRETATION OF THE ONTARIO BUILDING CODE AND THE TEST HOLES DUG ON THE PROPERTY.

**R.V.C.A. RECEIVED**

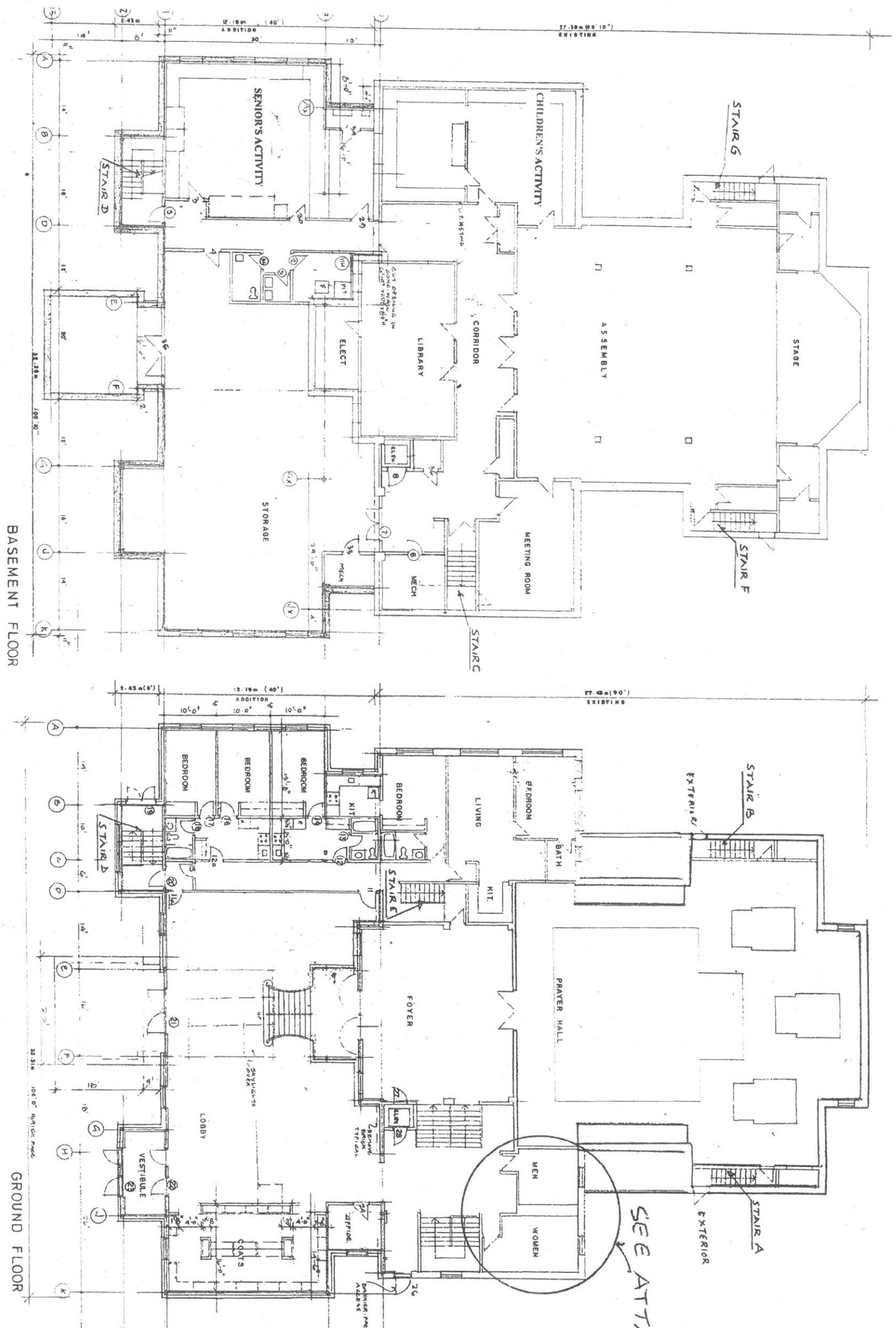
JUN - 4 2024

*John H. June 11/24*

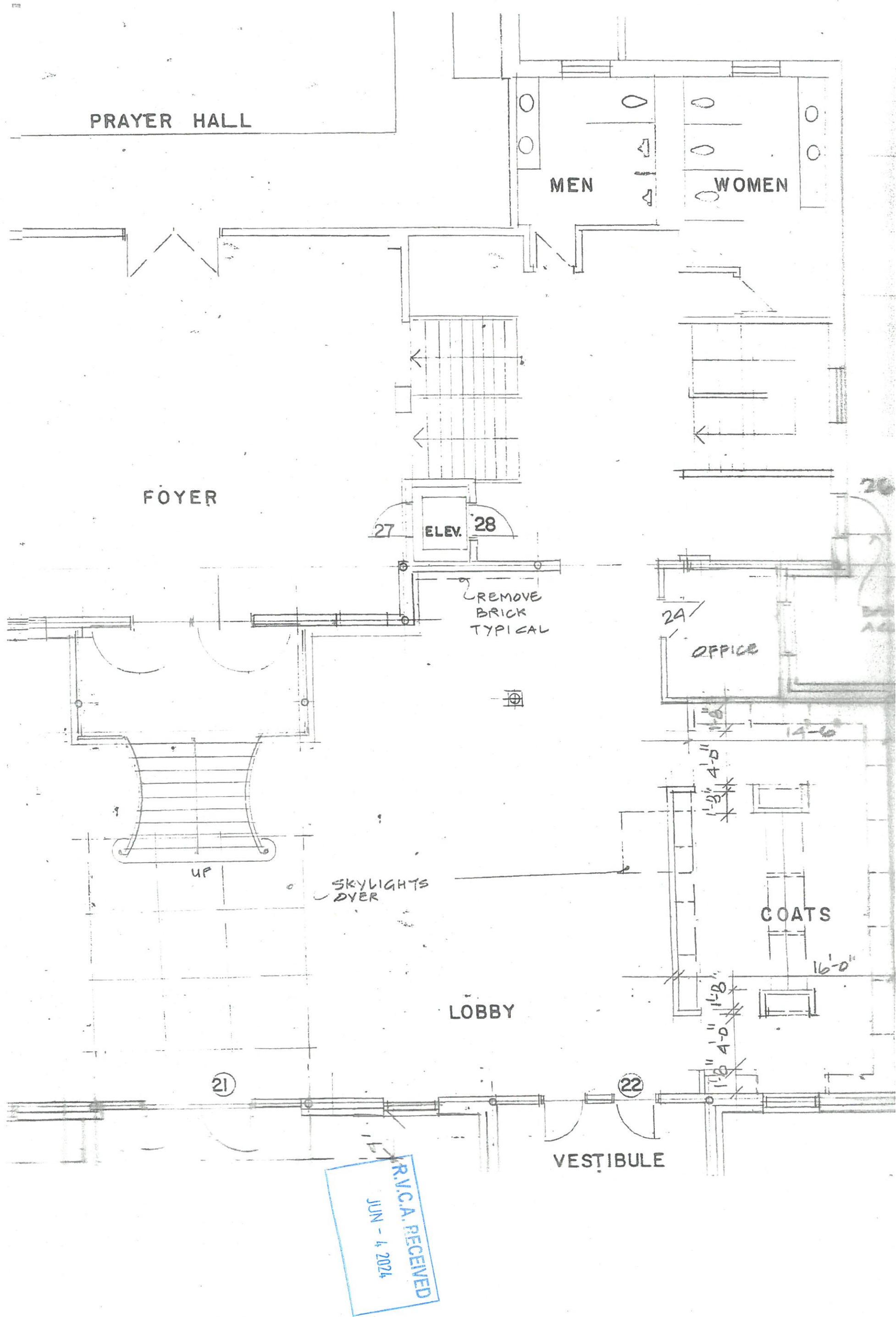
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Rev.	DP	DP	DP	Comments	WS
Rev.	Description			Date	Approved
1	Township	Plan#	Lot	Sublot	Con
2	2024	4835 BANK ST.		04/06/24	NTS

## HINDU TEMPLE



R.V.C.A. RECEIVED  
JUN - 4 2024





# Permit

## Part 8 – Sewage System Ontario Building Code

Do Not Complete  
Permit No 24-017  
Revision No \_\_\_\_\_  
Date \_\_\_\_\_  
Related Application  
B-24-023

**A copy of this permit must be posted on the property at all time during construction. OBC, Division C — Part 1, Section 1.3.2.1**

This permit verifies that the on-site sewage system was reviewed and approved for construction under the *Ontario Building Code* and *O.Reg. 323/12* as amended by *O.Reg. 151/13*.

Inspected & Recommended by: Ryan Hiemstra Owner: Hindu Temple of Ottawa Carleton  
Inspection Date & Time: June 3, 2024 @ 11:45am Weather: Clear  
Civic Address: 4835 Bank Street Legal: Lot 22, Con 5RF  
In the former Township/City of Gloucester

Design Flow for Commercial / Institutional / Industrial (as per Table 8.2.1.3.B)

Q: 4200 L/day

pretreatment tank	<u>2x (4500L min)</u>	L	weigh bills for	<input type="checkbox"/> yes	<input checked="" type="checkbox"/> no
effluent filter	<u>YES</u>		grain size analysis required	<input type="checkbox"/> yes	<input checked="" type="checkbox"/> no
pump rate	<u>time dosed</u>	<u>L/15 MIN</u>	site to be scarified	<input checked="" type="checkbox"/> yes	<input type="checkbox"/> no
treatment unit	<u>Norweco HK6570</u>		clay seal inspection	<input type="checkbox"/> yes	<input checked="" type="checkbox"/> no
number of units	<u>1</u>		mantle required	<input type="checkbox"/> yes	<input checked="" type="checkbox"/> no
			sub-grade inspection	<input checked="" type="checkbox"/> yes	<input type="checkbox"/> no

**ELEVATION**  In Ground  Partially Raised  Fully Raised

**TYPE OF SYSTEM**

Trench  
 Pipe and Stone or  Chambers

type of chamber \_\_\_\_\_

loading area \_\_\_\_\_ m<sup>2</sup>

total trench length \_\_\_\_\_ m

trench configuration \_\_\_\_\_

Dispersal Bed

BMEC  Type A  Type B

stone \_\_\_\_\_ m<sup>2</sup>

sand \_\_\_\_\_ m<sup>2</sup>

pipe \_\_\_\_\_

weight of sand \_\_\_\_\_ kg

Shallow Buried Trench

pipe length 5@28.34 m

orifice spacing 0.67 m

Filter Media Bed

stone \_\_\_\_\_ m<sup>2</sup>

extended base \_\_\_\_\_ m<sup>2</sup>

pipe \_\_\_\_\_

weight of filter media \_\_\_\_\_ kg

loading area \_\_\_\_\_ m<sup>2</sup>

Class 5 Holding Tank

Septic Tank Only

Manager, Septic System Approvals: Tony Davidson

Permit Date: June 12, 2029

Comments: 1. RVCA to inspect subgrade prior to backfilling sand

2. No food is to be served or prepared outside of the temple apartments

maintenance/pumping required

ESA permit # required

engineer to verify

subgrade

squirt height

Class 5 Holding Tank approval only valid for three years from date of issue

Manager, Septic System Approvals: \_\_\_\_\_

Revision Date: \_\_\_\_\_

Comments: \_\_\_\_\_