



# SITE SERVICING AND STORMWATER MANAGEMENT REPORT

## **FOR**

## METRO CANADA INC. 3831 CAMBRIAN ROAD – PHASE 1

**CITY OF OTTAWA** 

PROJECT NO.: 19-1135

CITY APPLICATION NO.: D07-12-20-0080

APRIL 2021 – REV 2 © DSEL

## SITE SERVICING AND STORMWATER MANAGEMENT REPORT FOR 3831 CAMBRIAN ROAD – PHASE 1

## **METRO CANADA**

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## SITE SERVICING AND STORMWATER MANAGEMENT REPORT FOR 3831 CAMBRIAN ROAD – PHASE 1 METRO CANADA APRIL 2021 – REV 2

CITY OF OTTAWA PROJECT NO.: 19-1135

#### 1.0 INTRODUCTION

David Schaeffer Engineering Limited (DSEL) has been retained by Metro Canada Inc. to prepare a Site Servicing and Stormwater Management report in support of the application for a Site Plan Control (SPC) at 3831 Cambrian Road.

The subject property is located within the City of Ottawa urban boundary, in Barrhaven ward. As illustrated in *Figure 1*, the subject property is located south of the intersection of Cambrian Road and Future Greenbank Road. Comprised of a single parcel the subject property measures approximately *2.2 ha* and is zoned General Mixed Use (GM).



Figure 1: Site Location

The proposed SPC would allow for the development of three commercial buildings fronting onto an internal drive aisle. The proposed development includes approximately  $6313 \ m^2$  of retail area,  $530 \ m^2$  of office area as well as surface parking, with access from Cambrian Drive and Future Greenbank Road. A copy of the Site Plan is included in Drawings/Figures.

The objective of this report is to provide sufficient detail to demonstrate that the proposed development is supported by existing municipal services.

## 1.1 Existing Conditions

The existing site a vacant lot used for staging of the adjacent subdivision construction consisting of aggregate piles and sandy the elevations range between 94.27 m and 93.00 m with a minimal grade change of approximate 0.45% from the Northeast to the Southwest corner of the property.

The existing soil conditions on the site consist of silty clay with gravel fill with practical refusal occurring between 5.25 m and 13 m in depth per the *Geotechnical Report*. Due to the existence of underlying silty clay, there are grade raise restrictions applicable to the proposed development. There is on-going surcharge under the proposed metro location and grade raise restrictions of 1.0 m to 1.5 m for the rest of the site. Refer to *Geotechnical Report* for grade raise restriction details.

Sewer and watermain mapping collected from the City of Ottawa indicate that the following services exist across the property frontages within the adjacent municipal right-of-ways:

#### **Cambrian Road**

- 406 mm diameter PVC watermain;
- 525 mm diameter concrete storm sewer tributary to the Todd Pond;
- > 375 mm diameter PVC storm sewer tributary to Todd Pond; and
- > 500 mm diameter concrete sanitary sewer tributary to the South Nepean Trunk.

#### **Future Greenbank Road**

- 2550 mm diameter concrete storm sewer tributary to Clarke Pond; and
- > 375 mm diameter PVC sanitary sewer tributary to the South Nepean Collector.

## 1.2 Required Permits / Approvals

The proposed development is subject to the site plan control approval process. The City of Ottawa must approve the engineering design drawings and reports prior to the issuance of site plan control.

The proposed development is a single parcel of land that is not industrial and would outlet to a storm sewer. As a result, the stormwater management system is exempt from sections 53(1) and (3) of the Ontario Water Resources Act under Ontario Regulation 525/98, and does not require Environmental Compliance Approval from the Ministry of Environment.

#### 1.3 Pre-consultation

Pre-consultation correspondence, along with the servicing guidelines checklist, is located in *Appendix A*.

#### 2.0 GUIDELINES, PREVIOUS STUDIES, AND REPORTS

## 2.1 Existing Studies, Guidelines, and Reports

The following studies were utilized in the preparation of this report:

- Ottawa Sewer Design Guidelines, City of Ottawa, SDG002, October 2012. (City Standards)
  - Technical Bulletin ISTB-2018-01
     City of Ottawa, March 21, 2018.
     (ISTB-2018-01)
  - Technical Bulletin ISTB-2018-03
     City of Ottawa, March 21, 2018.
     (ISTB-2018-03)
- Ottawa Design Guidelines Water Distribution City of Ottawa, July 2010. (Water Supply Guidelines)
  - Technical Bulletin ISD-2010-2
     City of Ottawa, December 15, 2010.
     (ISD-2010-2)
  - Technical Bulletin ISDTB-2014-02
     City of Ottawa, May 27, 2014.
     (ISDTB-2014-02)
  - Technical Bulletin ISDTB-2018-02
     City of Ottawa, March 21, 2018.
     (ISDTB-2018-02)
- Design Guidelines for Sewage Works,
   Ministry of the Environment, 2008.
   (MOE Design Guidelines)
- Stormwater Planning and Design Manual, Ministry of the Environment, March 2003. (SWMP Design Manual)
- Ontario Building Code Compendium Ministry of Municipal Affairs and Housing Building Development Branch, January 1, 2010 Update. (OBC)

## Barrhaven South Master Servicing Study Addendum Stantec, October 12, 2017. (BSMSS)

## Design Brief for the Clarke Stormwater Management Pond for the Half Moon Bay West Subdivision

J.F. Sabourin and Associates & DSEL Revised, October 19, 2017 (Clarke Pond Design Brief)

## Half Moon Bay West Subdivision Phase 2A/2B DSEL, November 6, 2019. (HMBW Phase 2 Design Brief)

## City of Ottawa Infrastructure Master Plan City of Ottawa, November 2013. (City of Ottawa IMP)

#### Stormwater Management Report for Phase 2 of the Half Moon Bay West Subdivision

J.F. Sabourin and Associates Updated, October 2019 (*Phase 2 SWM Report*)

## Geotechnical Investigation Report

PG2037-1 Revision 1, Paterson Group July 29, 2020 (Geotechnical Report)

#### 3.0 WATER SUPPLY SERVICING

#### 3.1 **Existing Water Supply Services**

The subject property lies within the City of Ottawa BARR pressure zone, as shown by the Pressure Zone map in Appendix B. A local 406 mm diameter watermain exists within the Cambrian Road right-of-way.

#### 3.2 **Water Supply Servicing Design**

It is proposed to service the development through a 200 mm internal looped watermain with two connections to the existing 406 mm diameter watermain within Cambrian Road.

Based on As-built drawings, there is one fire hydrant fronting the property along Cambrian Road.

**Table 1, below, summarizes the Water Supply Guidelines** employed in the preparation of the preliminary water demand estimate.

Table 1 **Water Supply Design Criteria** 

Design Parameter	Value
Commercial Retail	2.5 L/m <sup>2</sup> /d
Commercial Maximum Daily Demand	1.5 x avg. day
Commercial Maximum Hour Demand	1.8 x max. day
Minimum Watermain Size	150 mm diameter
Minimum Depth of Cover	2.4 m from top of watermain to finished grade
During normal operating conditions desired	350 kPa and 480 kPa
operating pressure is within	
During normal operating conditions pressure must	275 kPa
not drop below	
During normal operating conditions pressure must	552 kPa
not exceed	
During fire flow operating pressure must not drop	140 kPa
below	
*Daily average based on Appendix 4-A from Water Supply Guidelines	

**Table 2,** below, summarizes the estimated water supply demand and boundary conditions for the proposed development based on the Water Supply Guidelines.

<sup>\*\*</sup> Residential Max. Daily and Max. Hourly peaking factors per MOE Guidelines for Drinking-Water Systems Table 3-3 for 0 to 500 persons.
-Table updated to reflect ISD-2010-2

# Table 2 Water Demands and Boundary Conditions Proposed Conditions

Design Parameter	Estimated Demand <sup>1</sup> (L/min)	Boundary Condition <sup>2</sup> (m H <sub>2</sub> O / kPa) Connection 1	Boundary Condition <sup>2</sup> (m H <sub>2</sub> O / kPa) Connection 2
Average Daily Demand	13.9	62.5 / 613.1	62.0 / 608.2
Max Day + Fire Flow	20.9 + 6,000= 6,020.9	42.2 / 414.0	41.7 / 409.1
Peak Hour	37.6	45.6 / 447.3	45.1 / 442.4

1) Water demand calculation per Water Supply Guidelines. See Appendix B for detailed calculations.

Fire flow requirements are to be determined in accordance with City of Ottawa *Water Supply Guidelines* and the Ontario Building Code.

Fire flow requirements were estimated per City of Ottawa Technical Bulletin *ISTB-2018-02*. The following parameters were assumed for Phase 1:

- Type of construction Non-Combustible Construction;
- Occupancy type Limited Combustible; and
- Sprinkler Protection Fully-Supervised Sprinkled System.

The above assumptions result in an estimated fire flow of approximately *6,000 L/min*, noting that actual building materials selected will affect the estimated flow. A certified fire protection system specialist will need to be employed to design the building fire suppression system and confirm the actual fire flow demand.

Two private hydrants are proposed in order to accommodate the anticipated fire flow demand for the proposed development.

**Table 3**, below, summarizes the maximum available fire flow from the proposed hydrants as per *Table 18.5.4.3* of the *ISTB-2018-02*.

Table 3
Total Available Fire Flow from Proposed Hydrants

Number of Hydrants	Distance from Metro & Retail 1 (m)	Available Fire Flow per Table 18.5.4.3 of ISTB-2018-02 (L/min)
2	< 76	5,678 x 2
0	76 < and < 152	3,785 x 0
Total		11,356

Boundary conditions supplied by the City of Ottawa for the demands indicated; assumed ground elevation 93.4m at Connection 1 (Cambrian Road) and 93.9m at Connection 2 (Cambrian Road/Greenbank Road). See *Appendix B*.

The available fire flow from the hydrants is **11,356** L/min as per Table 18.5.4.3 of the **ISTB-2018-02**.

## 3.3 Watermain Modelling

EPANet was utilized to determine the availability of pressures throughout the system during average day, max day plus fire flow, and peak hour demands. This static model determines pressures based on the available head obtained from the anticipated maximum and minimum pressures at the connection points. The model will be updated with boundary conditions provided by the City of Ottawa once received.

The model utilizes the Hazen-Williams equation to determine pressure drop, while the pipe properties have been selected in accordance with *Water Supply Guidelines*. The model was prepared to assess the available pressure at each building, as well as, the pressures the watermain provides to fire hydrants during fire flow conditions.

The anticipated fire flow for the ultimate development was modeled through the proposed private hydrants. Please refer to *Appendix B* for a model sketch showing the node locations, fire demands assigned to each hydrant and the resulting pressures. *Table 4* indicates the resulting pressures at each node during the average day, peak hour and maximum day plus fire flow scenarios. *Appendix B* contains output reports and model schematics for each scenario.

Table 4
Model Simulation Output Summary

Model Simulation Output Summary				
Location	Average Day (kPa)	Max Day + Fire Flow (kPa)	Peak Hour (kPa)	
Metro	608.22	386.42	442.43	
2	609.69	387.89	443.90	
Bldg-A	609.20	382.20	443.41	
Hyd1	607.24	378.37	441.45	
Bldg-C	610.67	398.97	444.88	
Bldg-B	605.77	395.93	439.98	
Hyd2	608.71	392.60	442.92	

As demonstrated in *Table 4*, the anticipated pressures during the peak hour and max day + fire flow scenarios simulations are within the allowable pressure range described in *Table 1* from the *Water Supply Guidelines*. Pressures during average day demand are above the recommended pressures outlined in *Table 1*. A pressure check should be conducted at the time of construction to determine if pressure control is required.

## 3.4 Water Supply Conclusion

It is proposed to service the development through a looped internal watermain network via a 200 mm diameter watermains with two connections to the existing 406 mm watermain within Cambrian Road.

It is proposed that the development will be serviced by the two proposed internal hydrants. Based on *Table 18.5.4.3* of ISTB-2018-02, the fire flow demands of the proposed buildings can be supplied through both of the proposed hydrants.

An EPANET model was prepared for the average day, maximum day plus fire flow and peak hour scenarios. The EPANET water distribution model confirmed adequate pressure exists within fire hydrants during fire flow, and within the system for the Average Day, Max Day + Fire Flow and Peak Hour scenarios.

The proposed water supply design conforms to all relevant City Guidelines and Policies.

#### 4.0 WASTEWATER SERVICING

## 4.1 Existing Wastewater Services

The subject site lies within the South Nepean Trunk Sewer catchment area, as shown by the City sewer mapping included in *Appendix C*. An existing 500 mm diameter sanitary sewer within Cambrian Road is available to service the proposed development.

## 4.2 Wastewater Design

It is proposed that the development will be serviced via the existing 500 mm sanitary sewer within Cambrian Road via a 250 mm internal sanitary sewer.

A sanitary catch basin is proposed at the rear loading area of the Metro building to capture drainage from the waste bin pad. This area is proposed to be covered to reduce the storm runoff from entering the sanitary system.

**Table 5**, below, summarizes the **City Standards** employed in the design of the proposed wastewater sewer system.

Table 5
Wastewater Design Criteria

Design Parameter	Value
Peaking Factor	Harmon's Peaking Factor. Max 4.0, Min 2.0
	Harmon's Corrector Factor 0.8
Commercial Floor Space	5 L/m²/d
Infiltration and Inflow Allowance	0.05 L/s/ha (Dry Weather)
	0.28 L/s/ha (Wet Weather)
	0.33 L/s/ha (Total)
Sanitary sewers are to be sized employing the	1 2/ 1/
Manning's Equation	$Q = \frac{1}{1} A R^{\frac{2}{3}} S^{\frac{1}{2}}$
	n
Minimum Sewer Size (Non-Residential)	250 mm diameter
Minimum Manning's 'n'	0.013
Minimum Depth of Cover	2.5 m from crown of sewer to grade
Minimum Full Flowing Velocity	0.6 m/s
Maximum Full Flowing Velocity	3.0 m/s
Extracted from Sections 4 and 6 of the City of Ottawa Sew	ver Design Guidelines, October 2012.

*Table 6,* below, demonstrates the estimated peak flow from the proposed development. See *Appendix C* for associated calculations.

Table 6
Summary of Estimated Peak Wastewater Flow

Design Parameter	Total Flow (L/s)
Estimated Average Dry Weather Flow	0.94
Estimated Peak Dry Weather Flow	1.59
Estimated Peak Wet Weather Flow	2.21

The estimated sanitary flow based on the *Site Plan*, included in *Drawings/Figures*, results in a peak wet weather flow of *2.21 L/s*.

A sanitary sewer analysis was completed as part of the Barrhaven South Master Servicing Study (*BSMSS*) which included the existing sewers within Cambrian Road and those downstream. The subject property was contemplated as commercial lands in the study. Based on the *BSMSS* Sanitary Sewer Design Sheet, the controlling section of sewer is within Cambrian Road between MH13A and MH15A with an available capacity of *51.5 L/s*, which is sufficient to accommodate the sanitary flow from the proposed development. Extracted sanitary figures and design sheets from *BSMSS* and detailed calculations for the proposed site are included in *Appendix C*.

## 4.3 Wastewater Servicing Conclusions

The site is tributary to the South Nepean Trunk It is proposed to discharge wastewater to the existing 500 mm diameter sanitary sewer within Cambrian Road via a 250mm internal sanitary sewer.

Based on the above sanitary analysis, sufficient capacity is available to accommodate the anticipated *2.21 L/s* peak wet weather flow from the contemplated/proposed development.

The proposed wastewater design conforms to all relevant *City Standards*.

#### 5.0 STORMWATER MANAGEMENT

#### 5.1 Existing Stormwater Services

Stormwater runoff from the subject property is tributary to the City of Ottawa sewer system located within the Jock River sub-watershed. As such, approvals for proposed development within this area are under the approval authority of the City of Ottawa.

Flows that influence the watershed in which the subject property is located are further reviewed by the principal authority. The subject property is located within the Jock River watershed, and is therefore subject to review by the Rideau Valley Conservation Authority (RVCA). Consultation with the RVCA is located in *Appendix A*.

It was assumed that the existing development contained no stormwater management controls for flow attenuation. The estimated pre-development peak flows for the 2, 5, and 100-year events are summarized in *Table 7*, below:

Table 7
Summary of Existing Peak Storm Flow Rates

City of Ottawa Design Storm	Estimated Peak Flow Rate
	(L/s)
2-year	183.9
5-year	249.5
100-year	534.4

## 5.2 Post-development Stormwater Management Target

Stormwater management requirements for the proposed development were reviewed with the City of Ottawa and summarized in pre-consultation notes in *Appendix A*, where the proposed development is required to:

- Meet an allowable release rate based on a Rational Method Coefficient of 0.64, employing the City of Ottawa IDF parameters for a 5-year storm with a time of concentration equal to or less than 21.5 minutes and greater than or equal to 10 minutes:
- Attenuate all storms up to and including the City of Ottawa 100-year design event on site; and
- Quality controls are to be provided to achieve 80% Total Suspended Solids (TSS) removal as per the recommendation of the Rideau Valley Conservation Authority (RVCA).

Based on the above the allowable release rate for the proposed development is **263.4** L/s.

## 5.3 Proposed Stormwater Management System

The subject site was contemplated in the *HMBW Phase 2 Design Brief*, as well as, the *HMBW Phase 2 SWM Report*, to drain to the minor system within future Greenbank Road, eventually draining to the Clarke Pond and ultimately to the Jock River.

It is proposed that the stormwater outlet from the development will be to the existing 2550 mm diameter storm sewer within future Greenbank Road via a 750 mm connection to the existing sewer.

The *Clarke Pond Design Brief* contemplates the area in which the subject property falls within to be a 5-year capture area with onsite 100-year control.

Per the *HMBW Phase 2 Design Brief*, there is a Hydraulic Grade Line (HGL) elevation in the 100-year storm event of approximately *93.09 m* at the future *MH904* within future Greenbank Road storm sewer, located upstream of the proposed storm connection. Refer to *Plan & Profile of future Greenbank Road*, prepared by DSEL, revision 8, dated February 25, 2020 in *Appendix D*.

To meet the stormwater quantity control objectives the proposed development will employ rooftop and surface storage. To adhere to the allocated release rate, inlet control devices (ICDs) are proposed at catch basins and manholes to control flow. The 100-year HGL elevation was taken into account in the design of available storage. The downstream condition was set at **93.09** *m* to size the ICDs.

Stormwater drainage from parking areas (*A109*, *A110B*, *A110A*, *A114A*, *A113A*, *A108*, *A103B*, *A106*, *A107*) will be collected by catch basins and required stormwater storage will be provided via surface ponding. Flow from these areas as indicated on drawing *SWM-1* will be controlled via orifice controls located at the outlet of the catch basins.

Refer to detailed stormwater calculations located in *Appendix D* and drawing *SSP-1* and for ICD locations and sizing.

Building drainage from areas (**METRO**, **BLDG A**, **BLDG B**, **BLDG C**) indicated on drawing **SWM-1**, will be controlled via rooftop controls providing required stormwater storage on the rooftops.

**Table 8** illustrates anticipated release rates and required storage volumes for each drainage area.

**Table 8,** below, estimates post-development flow rates to the storm sewer within Greenbank Road.

Table 8
Stormwater Flow Rate Summary

Stormwater Flow Hate Summary					
Control Area	5-Year Release Rate	5-Year Required Storage	100-Year Release Rate	100-Year Required Storage	100-Year Available
					Storage
	(L/s)	(m³)	(L/s)	(m³)	(m³)
U1	4.7	0.0	10.1	0.0	0.0
U2	11.4	0.0	21.6	0.0	0.0
U3	13.5	0.0	28.9	0.0	0.0
U4	0.7	0.0	1.4	0.0	0.0
U5	2.5	0.0	5.3	0.0	0.0
METRO	24.2	55.5	31.9	126.8	317.5
BLDG A	7.5	10.7	10.0	25.3	73.6
BLDG B	7.3	9.0	9.8	21.4	65.7
BLDG C	5.1	5.7	6.9	13.7	43.5
A109	9.6	3.2	25.6	3.8	4.2
A110B	9.4	2.7	10.0	12.0	43.0
A110A	9.6	7.3	10.4	25.0	54.7
A114A	16.0	12.2	18.2	40.9	68.7
A113A	8.3	22.3	9.4	63.6	88.3
A108	8.2	23.4	8.9	57.3	114.5
A103B	7.9	8.7	8.4	24.3	76.9
A106 & A107	23.0	60.0	24.5	169.2	51.1
Total	168.9	220.8	241.4	583.4	1001.8

It is anticipated that approximately  $583.4 \, m^3$  of on-site storage will be required to attenuate flow to the established release rate of  $263.4 \, L/s$ . Storage calculations are contained within **Appendix D**. Sufficient surface storage is provided to satisfy the 100-year required storage.

"Enhanced" Quality control is provided by the Clarke Pond per the *Clarke Pond Design Brief*. Excerpts and figures extracted from the *Clarke Pond Design Brief* are included in *Appendix D*.

### 5.4 Stormwater Servicing Conclusions

The subject site was contemplated in the *HMBW Phase 2 Design Brief* and *HMBW Phase 2 SWM Report*. An allowalbe release rate of *263.4 L/s* is to be achieved with attenuation up to the 100-year storm event.

Controls are provided at each catch basin to restrict the total flow from the site to the allowable release rate. To attenuate flow to the allowable release rate,  $583.4 \, m^3$  of surface storage is required.

Quality control is provided by the Clarke Pond at an enhanced protection level per the *Clarke Pond Design Brief.* 

The proposed stormwater design conforms to all relevant *City Standards* and Policies for approval.

#### 6.0 UTILITIES

Gas and Hydro services currently exist within the Cambrian Road right-of-way. Utility servicing will be coordinated with the individual utility companies prior to site development.

The proposed development will be coordinated and approved by the utility company having jurisdiction.

#### 7.0 EROSION AND SEDIMENT CONTROL

Soil erosion occurs naturally and is a function of soil type, climate and topography. During construction the extent of erosion losses is exaggerated due to the removal of vegetation and the top layer of soil becoming agitated.

Prior to topsoil stripping, earthworks or underground construction, erosion and sediment controls will be implemented and will be maintained throughout construction.

Silt fence will be installed around the perimeter of the site and will be cleaned and maintained throughout construction. Silt fence will remain in place until the working areas have been stabilized and re-vegetated.

Catch basins will have SILTSACKs or an approved equivalent installed under the grate during construction to protect from silt entering the storm sewer system.

A mud mat will be installed at the construction access in order to prevent mud tracking onto adjacent roads.

Erosion and sediment controls must be in place during construction. The following recommendations to the contractor will be included in contract documents:

- Limit extent of exposed soils at any given time;
- Re-vegetate exposed areas as soon as possible;
- Minimize the area to be cleared and grubbed:
- Protect exposed slopes with plastic or synthetic mulches;
- Install silt fence to prevent sediment from entering existing ditches;
- No refueling or cleaning of equipment near existing watercourses;
- Provide sediment traps and basins during dewatering;
- Install filter cloth between catch basins and frames:
- Plan construction at proper time to avoid flooding; and
- Establish material stockpiles away from watercourses, so that barriers and filters may be installed.

The contractor will, at every rainfall, complete inspections and guarantee proper performance. The inspection is to include:

- Verification that water is not flowing under silt barriers; and
- Clean and change filter cloth at catch basins.

#### 8.0 CONCLUSION AND RECOMMENDATIONS

David Schaeffer Engineering Ltd. (DSEL) has been retained by Metro Canada Inc. to prepare a Site Servicing and Stormwater Management report in support of the application for a Site Plan Control (SPC) at 3831 Cambrian Road. The preceding report outlines the following:

- Based on boundary conditions provided by the City the existing municipal water infrastructure is capable of providing the proposed development with water within the City's required pressure range;
- The FUS method for estimating fire flow indicated **6,000 L/min** is required for proposed development;
- The contemplated development is anticipated to have a peak wet weather flow of **2.21** L/s; Based the **BSMSS** the existing municipal sewer infrastructure has sufficient capacity to support the development;
- Storm water quantity controls are proposed per the subdivision design, a maximum release rate of **263.4 L/s** is required and provided through the use of ICD's. Flow attenuation to be provided up to the 100-year storm event;
- It is proposed to attenuate flow through rooftop and surface storage. It is anticipated that *583.4 m*<sup>3</sup> of onsite surface storage will be required to attenuate flow to the established release rate above;
- Quality control is provided by the Clarke Pond at an enhanced protection level per the Clarke Pond Design Brief.

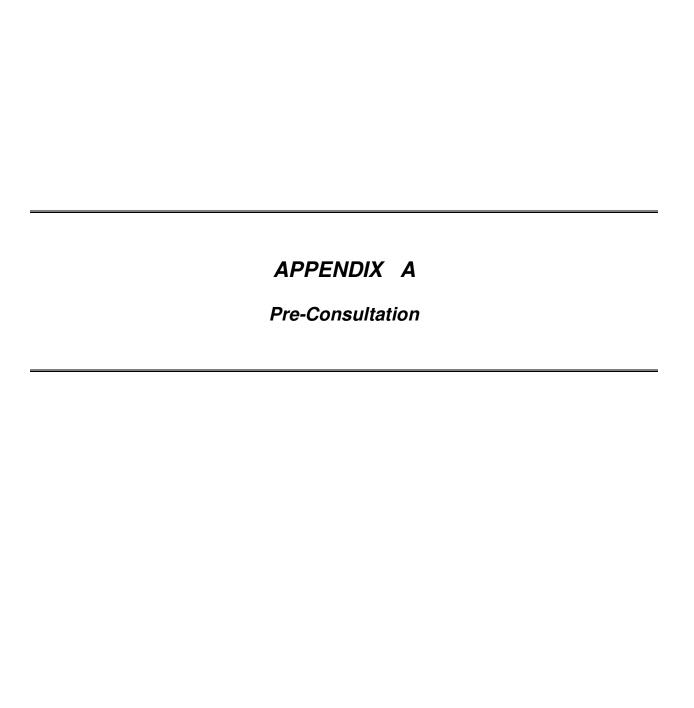
Prepared by, **David Schaeffer Engineering Ltd.** 



Per: Brandon N. Chow



Per: Adam D. Fobert, P.Eng



#### **Genavieve Greenberg**

From: Jaime Posen <posen@fotenn.com>
Sent: Friday, June 5, 2020 5:23 PM
To: Wayne Williams; Antony Cannell
Cc: Bria Aird; Fel Petti; Christopher Gordon
Subject: FW: Metro pre-consult - 3831 Cambrian Rd

Attachments: Pre-con Study and Plan Identification List.pdf; 3831 Cambrian Design Brief.pdf

Hello team,

Please see below and attached for the meeting minutes from the pre-application consultation meeting with the City of Ottawa for 3831 Cambrian Road.

After scanning the comments, I didn't see anything dramatically different than what was shared with us in the meeting, but please let me know if anything stands out as being problematic.

Mélanie also advised that Frank McKinney had shared a link with Chris Gordon to download some material related to the EAs for the surrounding roads.

Hope that's helpful, have a great weekend.

#### Jaime Posen, MCIP RPP

Senior Planner T 613.730.5709 ext. 236

From: Gervais, Melanie < Melanie. Gervais@ottawa.ca>

Sent: June 4, 2020 3:48 PM

To: Jaime Posen <posen@fotenn.com>

Subject: Metro pre-consult - 3831 Cambrian Rd

Hi Jaime,

Please find below a recap of our pre-consultation meeting. Please note that during the COVID-19 pandemic the department is accepting electronic applications. Please send pdfs of your submission material (including a scanned copy of the application form) to <a href="mailto:planningcirculations@ottawa.ca">planningcirculations@ottawa.ca</a> (and cc myself). They will create the file number and upload the files to the proper location. Following the receipt of the electronic submission I will send you an email with your new file number and the new process for submitting payment.

## Planning:

You will need to submit a New - Complex Site Plan application with a fee of \$35,487.53 + engineering review fees + \$1,015 (Conservation Authority fee).

The property is zoned GM[2340]-h which stands for General Mixed Use Zone Exception 2340 with a holding, the zoning provisions for Mixed Use Zone can be found <a href="here">here</a> and all the provisions for parking lots can be found <a href="here">here</a>. Please note that the holding zone can be lifted given that the Clarke Pond is operational.

The site is also with the Community Core in the Barrhaven South CDP. The CDP speaks to a Community Core Concept Plan and Design Framework which was completed by FoTenn and previously sent to you. Please ensure that the Planning Rationale indicated how the design elements identified in the plan have been met (Built Form, Architecture, and Land Use / Landscape and the Environment / Pedestrians and Cyclists / Vehicles and Parking...).

Proper landscaping will be required on site. This includes the addition of trees along the street edge, within landscape buffers and landscaped islands... Please note that all Landscape Plans need to be stamped by a Landscape Architect.

The Planning Rationale will have to explain the proposal, review the applicable Official Plan and CDP policies, review the applicable Zoning By-law provisions and review the Accessibility Design Standards.

The adjacent property to the south is the Dowitcher Park.

Please see the attached list identifying the submission requirements. Although the list identifies numbers of paper copies these are **not** required at this time.

#### Design:

More information is necessary to provide design comments and will be detailed in the Design Brief. Some of these will include:

- More details of the surrounding context and how it connects and supports it. (Using page 20 in the Community Design Plan as a guide for the extent of context requested);
- Additional details regarding the landscaping approach (Interim and future);
- How pedestrians will be directed across and through the site;
- How direct adjacency to the park will be considered and any negative impacts from the loading and access road will be mitigated;
- How the buildings will related to the streetscape with active entrances/facades etc. especially when the interim road is removed;

We recommend the site plan illustrate a future design that shows what will replace the interim road. The final design layout should illustrate the mediating solutions to achieve the ten-year plan (especially regarding building placement) when the interim access road that will separate the buildings from the future road is removed;

Please see the Design Brief Terms of Reference provided.

## Forestry:

Soil volume is fundamental to the success of newly planted trees. Please ensure newly planted trees have an adequate soil volume for their size at maturity. The following is a table of recommended minimum soil volumes:

Tree	Single Tree Soil	Multiple Tree
Type/Size	Volume (m3)	Soil Volume
	( - /	(m3/tree)

Ornamental	15	9
Columnar	15	9
Small	20	12
Medium	25	15
Large	30	18
Conifer	25	15

Plant for survival to maturity - choose the right species that for the site and one that will contribute to the design and function of the built site, ensure that salt tolerant species are selected for high salt areas

#### **Transportation**:

- Follow Traffic Impact Assessment Guidelines
  - Please begin the TIA report (Steps 1-3 must be submitted and approved prior to application or it will be deemed incomplete).
    - o <a href="https://ottawa.ca/en/transportation-impact-assessment-guidelines">https://ottawa.ca/en/transportation-impact-assessment-guidelines</a>
- Noise Impact Studies required for the following:
  - Stationary (any exposed mechanical equipment and loading zone) due to the proximity to neighboring noise sensitive land uses.
- Temporary access road on Greenbank will be permitted.
- Ensure that the Cambrian and Greenbank EAs are followed for right of way requirements and the intersection control at Cambrian and Greenbank temporary road.
- All maintenance of the temporary road will be at the applicant's expense.
- On site plan:
  - Show all details of the roads abutting the site up to and including the opposite curb;
     include such items as pavement markings, accesses and/or sidewalks.
  - Turning templates will be required for all accesses showing the largest vehicle to access
    the site; required for internal movements and at all access (entering and exiting and
    going in both directions).
  - Show all curb radii measurements; ensure that all curb radii are reduced as much as possible
  - Show lane/aisle widths.
  - Ensure pedestrian connections are provided on the site.
  - Grey out any area that will not be impacted by this application.
- AODA legislation (<u>link</u>) is in effect for all organizations, please ensure that the design conforms to these standards, see attached checklist for guidance.

For any transportation questions, please contact Mike Giampa (Mike.Giampa@ottawa.ca).

#### **Transportation Planning (Frank McKinney):**

- Although we are not opposed to a complete throw away of the temporary access road, it would be best if we could find a way to prevent this as much as possible.
- Metro will be required to restore the boulevard.
- The timing of realigned Greenbank from Jockvale to Cambrian Rd is 2031 while south of Cambrian Rd is still to be determined through the next TMP.

- Once realigned Greenbank is constructed up to Cambrian Rd, how will the temporary access tie up to the intersection?
- Please hide parking as much as possible

We are having problems locating the microstation files for the Cambrian Road Widening. Frank McKinney will send all information on to Chris Gordon as soon as it is available.

Please note that an email was sent to Patrick Sammon in ISD concerning the design for realigned Greenbank but he is unfortunately away from the office. We will provide you with more information on this as soon as possible and hopefully be able to provide you with more information on how the tie-in to the future intersection should be.

#### **Engineering**:

#### Water

Water District Plan No: 362-012

Existing public services:

Cambrian Road – 406 mm PVC



- Service areas with a basic demand greater than 50 m³/day shall be connected with a minimum of two water services, separated by an isolation valve, to avoid creation of vulnerable service area.
- District Metering Area Chambers are required for services 150mm or greater in diameter.
- A water meter sizing questionnaire [water card] will have to be completed prior to receiving a water permit (water card will be provided post approval)

#### **Boundary conditions:**

Civil consultant must request boundary conditions from the City's assigned Project Manager prior to first submission.

- Water boundary condition requests must include the location of the service(s) and the expected loads required by the proposed developments. Please provide all the following information:
  - Location of service(s)
  - Type of development and the amount of fire flow required (as per FUS, 1999).
  - Average daily demand: \_\_\_\_ l/s.
  - Maximum daily demand: \_\_\_l/s.
  - Maximum hourly daily demand: I/s.
- Fire protection (Fire demand, Hydrant Locations)
- A water meter sizing questionnaire [water card] will have to be completed prior to receiving a water permit (water card will be provided post approval)

## **Sanitary Sewer**

Existing public services:

Cambrian Road – 500 mm Conc.



- A monitoring manhole is required on private property.
- The sanitary sewer design has assumed a flow of 0.00058 m<sup>3</sup>/s/ha area. The sewer design should demonstrate that the proposed development is within that design criteria or that additional demand can be accommodated.

#### **Storm Sewer**

Existing public services:

- Future Greenbank Road 2550 mm Conc. Currently this storm sewer has been constructed to just south of Cambrian.
  - The outlet to the Clark Pond and the stormwater network north of Cambrian Road have been constructed by Mattamy as part of the Half Moon Bay West development. The stormwater

network ends just south of Cambrian Road and there are no immediate plans to extend the sewer south of Cambrian Road prior to the construction of the Future Greenbank Road.

- o The Zoning Hold can be lifted now that the Clarke Pond is operational.
- Cambrian Road 375 mm PVC (South) not designed for drainage from subject site
- Cambrian Road 525 mm Conc (North) not designed for drainage from subject site



#### **Stormwater Management**

#### Quality Control:

- Rideau Valley Conservation Authority to confirm quality control requirements. Quantity Control:
- Master Servicing Study:
  - Barrhaven South Creek Subwatershed Study (Jock River Reach 1)
  - Barrhaven South Master Servicing Study Oct 2017
  - o Half Moon Bay West Subdivision
- Allowable Run-off Coefficient: C = 0.64
- Time of concentration (Tc): Tc = pre-development; maximum Tc = 21.5 min
- Allowable flowrate: Control the 100-year storm events to the 5-year storm event

#### Ministry of Environment, Conservation and Parks (MECP)

All development applications should be considered for an Environmental Compliance Approval, under MECP regulations.

- a. Consultant determines if an approval for sewage works under Section 53 of OWRA is required. Consultant determines what type of application is required and the City's project manager confirms. (If the consultant is not clear if an ECA is required, they will work with the City to determine what is required. If unclear or there is a difference of opinion the City Project Manager will coordinate requirements with MECP).
- b. The project will be either transfer of review (standard), transfer of review (additional), direct submission, or exempt as per O. Reg. 525/98.
- c. Pre-consultation is not required if applying for standard or additional works (Schedule A of the Agreement) under Transfer Review.
- d. Pre-consultation with local District office of MECP is recommended for direct submission.
- e. Consultant completes an MECP request form for a pre-consultation. Sends request to moeccottawasewage@ontario.ca
- f. ECA applications are required to be submitted online through the MECP portal. A business account required to submit ECA application. For more information visit <a href="https://www.ontario.ca/page/environmental-compliance-approval">https://www.ontario.ca/page/environmental-compliance-approval</a>

#### NOTE: Site Plan Approval is required before any MECP application is signed

#### **General Service Design Comments**

- The City of Ottawa requests that all new services be located within the existing service trench to minimize necessary road cuts.
- Monitoring manholes should be located within the property near the property line in an accessible location to City forces and free from obstruction (i.e. not a parking).
- Where service length is greater than 30 m between the building and the first maintenance hole / connection, a cleanout is required.
- The City of Ottawa Standard Detail Drawings should be referenced where possible for all work within the Public Right-of-Way.
- The upstream and downstream manhole top of grate and invert elevations are required for all new sewer connections.
- Services crossing the existing watermain or sewers need to clearly provide the obvert/invert elevations to demonstration minimum separation distances. A watermain crossing table may be provided.

#### Other

Are there are Capital Works Projects scheduled that will impact the application? ☐ Yes ☒ No

#### References

• As per section 53 of the Professional Engineers Act, O. Reg 941/40, R.S.O. 1990, all documents prepared by engineers must be signed and dated on the seal.

## **CREO** (Corporate Real Estate Office)

Please provide a sketch showing area and dimensions of the portion of future Greenbank Road that want to lease for their access road. CREO will then undertake a circulation to all City departments and utility companies to determine if there are any objections to entering into a license with Metro.

CREO will need to seek Legal advice as to whether a license is appropriate in this case or whether it should be a lease given that it appears that you will be occupying City land for many years.

If you or the Metro consultant should provide some background and anticipated works to be completed on the property.

Once CREO receive the sketch and information, a request for an appraisal will be done.

#### **RVCA**

The RVCA would be looking for water quality protection of 80% TSS removal on-site as part of Site Plan.

\*\*\*

Please refer to the links to "<u>Guide to preparing studies and plans</u>" and <u>fees</u> for general information. Additional information is available related to <u>building permits</u>, <u>development charges</u>, and the <u>Accessibility Design Standards</u>. Be aware that other fees and permits may be required, outside of the

development review process. You may obtain background drawings by contacting <u>informationcentre@ottawa.ca</u> (613-580-2424 ext. 44455).

All required plans are to be submitted utilizing a reasonable and appropriate metric scale as per City of Ottawa Servicing and Grading Plan Requirements: title blocks are to be placed on the right of the sheets and not along the bottom. Engineering plans may be combined, but the Site Plans must be provided separately. Plans shall include the survey monument used to confirm datum. Information shall be provided to enable a non-surveyor to locate the survey monument presented by the consultant.

All required plans & reports are to be provided in \*.pdf format (at application submission and for any, and all, re-submissions).

These pre-consultation comments are valid for one year. If you submit a development application(s) after this time, you may be required to meet for another pre-consultation meeting and/or the submission requirements may change.

Please do not hesitate to contact me if you have any questions.

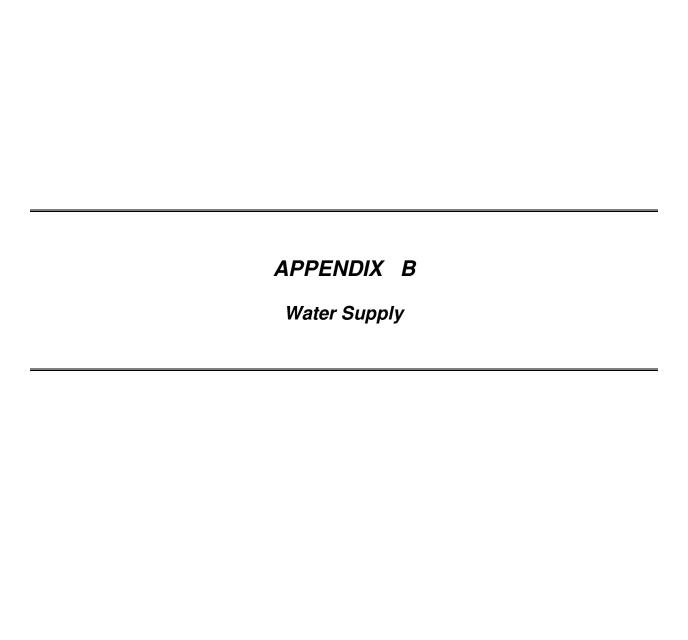
Regards,

Mélanie Gervais MCIP, RPP
Planner / Urbaniste
Development Review /
Examen des demandes d'aménagement
Planning, Infrastructure and Economic Development Department /
Services de la planification, de l'infrastructure et du développement économique
City of / Ville d'Ottawa
110, avenue Laurier Avenue West / Ouest,
4th Floor / 4ième étage
Ottawa, ON K1P 1J1
Tel.: 613-580-2424 ext. 24025
Fax / Télécopieur: 613-580-2576
E-mail / Courriel: Melanie.Gervais@ottawa.ca
Mail Code: 01-14

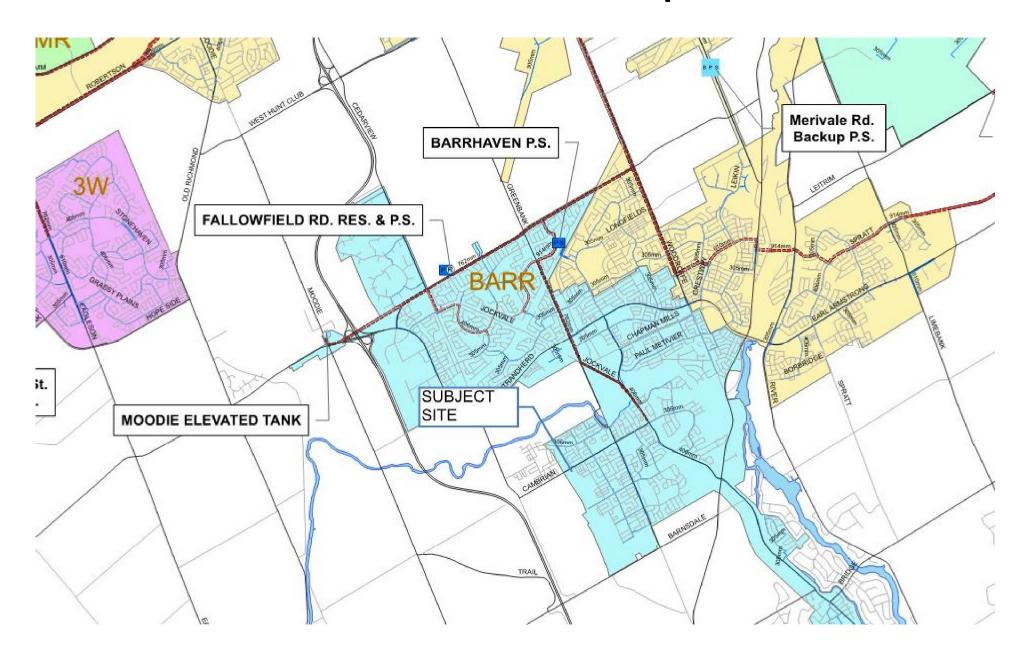
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## **Pressure Zone Map**



## Boundary Conditions 3831 Cambrian Road

## **Provided Information**

Scenario	Dema	Demand		
Scenario	L/min	L/s		
Average Daily Demand	12.00	0.2		
Maximum Daily Demand	18.00	0.3		
Peak Hour	31.80	0.53		
Fire Flow Demand 1	7,000.00	116.67		

## **Location**



## Results - Existing Conditions

#### Connection 1 - Cambrian Rd.

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	155.9	88.8
Peak Hour	139.0	64.8
Max Day plus Fire 1	135.6	60.0

<sup>&</sup>lt;sup>1</sup> Ground Elevation = 93.4 m

### Connection 2 - Cambrian Rd. / Greenbank Rd.

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	155.9	88.1
Peak Hour	139.0	64.1
Max Day plus Fire 1	135.6	59.3

<sup>&</sup>lt;sup>1</sup> Ground Elevation = 93.9 m

### Results - SUC Zone Reconfiguration

### Connection 1 - Cambrian Rd.

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	147.5	76.9
Peak Hour	143.4	71.0
Max Day plus Fire 1	143.5	71.2

<sup>&</sup>lt;sup>1</sup> Ground Elevation = 00.0 m

### Connection 2 - Cambrian Rd. / Greenbank Rd.

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	147.5	76.2
Peak Hour	143.4	70.3
Max Day plus Fire 1	143.5	70.5

<sup>&</sup>lt;sup>1</sup> Ground Elevation = 00.0 m

### **Notes**

- 1. As per the Ontario Building Code in areas that may be occupied, the static pressure at any fixture shall not exceed 552 kPa (80 psi.) Pressure control measures to be considered are as follows, in order of preference:
  - a. If possible, systems to be designed to residual pressures of 345 to 552 kPa (50 to 80 psi) in all occupied areas outside of the public right-of-way without special pressure control equipment.
  - b. Pressure reducing valves to be installed immediately downstream of the isolation valve in the home/ building, located downstream of the meter so it is owner maintained.

#### **Disclaimer**

The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation. Fire Flow analysis is a reflection of available flow in the watermain; there may be additional restrictions that occur between the watermain and the hydrant that the model cannot take into account.

Water Demand Design Flows per Unit Count City of Ottawa - Water Distribution Guidelines, July 2010



# Institutional / Commercial / Industrial Demand

				Avg. [	Daily	Max I	Day	Peak I	Hour
Property Type	Unit I	Rate	Units	m³/d	L/min	m³/d	L/min	m <sup>3</sup> /d	L/min
Metro	2.5	L/m <sup>2</sup> /d	4,024	10.06	7.0	15.1	10.5	27.2	18.9
Bldg A	2.5	L/m <sup>2</sup> /d	929	2.32	1.6	3.5	2.4	6.3	4.4
Bldg B	2.5	L/m <sup>2</sup> /d	830	2.08	1.4	3.1	2.2	5.6	3.9
Bldg C (Retail)	2.5	L/m <sup>2</sup> /d	530	1.33	0.9	2.0	1.4	3.6	2.5
Bldg C (Office)	75	L/9.3m <sup>2</sup> /d	530	4.27	3.0	6.4	4.5	11.5	8.0
		Total I/	CI Demand	20.1	13.9	30.1	20.9	54.2	37.6
		Tot	tal Demand _	20.1	13.9	30.1	20.9	54.2	37.6

# Metro Canada Inc. 3831 Cambrian Road Proposed Site Conditions Metro BLDG A

# Fire Flow Estimation per Fire Underwriters Survey

Water Supply For Public Fire Protection - 1999



# Fire Flow Required

1. Base Requirement

 $F=220C\sqrt{A}$  L/min Where **F** is the fire flow, **C** is the Type of construction and **A** is the Total floor area

Type of Construction: Non-Combustible Construction

C 0.8 Type of Construction Coefficient per FUS Part II, Section 1
 A 4,953 m<sup>2</sup> Total floor area based on FUS Part II section 1

Fire Flow 12386.4 L/min

12000.0 L/min rounded to the nearest 1,000 L/min

# **Adjustments**

2. Reduction for Occupancy Type

Limited Combustible -15%

Fire Flow 10200.0 L/min

3. Reduction for Sprinkler Protection

Sprinklered - Supervised -50%

Reduction -5100 L/min

4. Increase for Separation Distance

Cons. of Exposed Wall	S.D	Lw Ha	LH	EC	
N Non-Combustible	30.1m-45m	15	2	30	5%
S Non-Combustible	>45m	0	0	0	0%
E Non-Combustible	>45m	0	1	0	0%
W Non-Combustible	>45m	0	1	0	0%
	% Increase				5% value not to exceed 75%

Increase 510.0 L/min

Lw = Length of the Exposed Wall

Ha = number of storeys of the adjacent structure. Max 5 stories

LH = Length-height factor of exposed wall. Value rounded up.

EC = Exposure Charge

### **Total Fire Flow**

Fire Flow	5610.0 L/min	fire flow not to exceed 45,000 L/min nor be less than 2,000 L/min per FUS Section 4
	6000.0 L/min	rounded to the nearest 1.000 L/min

### Notes

-Type of construction, Occupancy Type and Sprinkler Protection information provided by \_\_\_\_\_

-Calculations based on Fire Underwriters Survey - Part II

### Metro Canada Inc. 3831 Cambrian Road Proposed Site Conditions BLDG B

# Fire Flow Estimation per Fire Underwriters Survey

Water Supply For Public Fire Protection - 1999



# Fire Flow Required

1. Base Requirement

 $F=220C\sqrt{A}$  L/min Where **F** is the fire flow, **C** is the Type of construction and **A** is the Total floor area

Type of Construction: Non-Combustible Construction

C 0.8 Type of Construction Coefficient per FUS Part II, Section 1

A 830 m<sup>2</sup> Total floor area based on FUS Part II section 1

Fire Flow 5070.5 L/min

**5000.0 L/min** rounded to the nearest 1,000 L/min

# **Adjustments**

2. Reduction for Occupancy Type

Limited Combustible -15%

Fire Flow 4250.0 L/min

3. Reduction for Sprinkler Protection

Non-Sprinklered 0%

Reduction 0 L/min

4. Increase for Separation Distance

Cons. of Exposed Wall	S.D	Lw Ha	LH	EC	
N Non-Combustible	>45m	0	0	0	0%
S Non-Combustible	>45m	0	0	0	0%
E Non-Combustible	>45m	0	0	0	0%
W Non-Combustible	30.1m-45m	30	1	30	5%
	% Increase				5% value not to exceed 75%

Increase 212.5 L/min

Lw = Length of the Exposed Wall

Ha = number of storeys of the adjacent structure. Max 5 stories

LH = Length-height factor of exposed wall. Value rounded up.

EC = Exposure Charge

### **Total Fire Flow**

Fire Flow	4462.5 L/min	fire flow not to exceed 45,000 L/min nor be less than 2,000 L/min per FUS Section 4
	4000.0 L/min	rounded to the nearest 1.000 L/min

### Notes

-Type of construction, Occupancy Type and Sprinkler Protection information provided by \_\_\_\_\_

-Calculations based on Fire Underwriters Survey - Part II

# Metro Canada Inc. 3831 Cambrian Road Proposed Site Conditions BLDG C

# Fire Flow Estimation per Fire Underwriters Survey

Water Supply For Public Fire Protection - 1999



# Fire Flow Required

1. Base Requirement

 $F=220C\sqrt{A}$  L/min Where **F** is the fire flow, **C** is the Type of construction and **A** is the Total floor area Type of Construction: Non-Combustible Construction

C 0.8 Type of Construction Coefficient per FUS Part II, Section 1
A 1,060 m<sup>2</sup> Total floor area based on FUS Part II section 1

Fire Flow 5730.1 L/min

6000.0 L/min rounded to the nearest 1,000 L/min

# **Adjustments**

2. Reduction for Occupancy Type

Limited Combustible -15%

Fire Flow 5100.0 L/min

3. Reduction for Sprinkler Protection

Non-Sprinklered 0%

Reduction 0 L/min

4. Increase for Separation Distance

Cons. of Exposed Wall	S.D	Lw Ha	LH	EC	
N Non-Combustible	>45m	0	0	0	0%
S Non-Combustible	>45m	0	0	0	0%
E Non-Combustible	>45m	0	0	0	0%
W Non-Combustible	30.1m-45m	40	1	40	5%
	% Increase				5% value not to exceed 75%

Increase 255.0 L/min

Lw = Length of the Exposed Wall

Ha = number of storeys of the adjacent structure. Max 5 stories

LH = Length-height factor of exposed wall. Value rounded up.

EC = Exposure Charge

### **Total Fire Flow**

Fire Flow	5355.0 L/min	fire flow not to exceed 45,000 L/min nor be less than 2,000 L/min per FUS Section 4
	5000.0 L/min	rounded to the nearest 1.000 L/min

### Notes:

- -Type of construction, Occupancy Type and Sprinkler Protection information provided by \_\_\_\_\_
- -Calculations based on Fire Underwriters Survey Part II

# [TITLE]

[JUNCTIONS];ID Metro 2 Bldg-A hyd1 Bldg-C Bldg-B hyd2 [RESERVOIRS]	Elev 93.90 93.75 93.80 94.00 93.65 94.15 93.85	Demand 7.0 0 1.6 0 3.9 1.4	Pattern	;		
;ID 7 1	Head 155.9 155.9	Pattern	;			
[TANKS] ;ID VolCurve	Elevation	InitLevel	MinLevel	MaxLevel	Diameter	MinVol
[PIPES]; ID MinorLoss  1 1.4 2 3.4 3 0.6 4 0.6 5 1.6 9 2 10 2.0 6 0.8	Node1 Status Bldg-B Open; 2 Open; 2 Open; Bldg-A Open; hyd1 Open; Bldg-C Open; Bldg-B Open; hyd2 Open;	Node2 2 Metro Bldg-A hyd1 hyd2 1 7 Bldg-C		Length 64 109 28.5 7 73 53 52 18	Diameter 200 200 200 200 200 200 200 200	Roughness 110 110 110 110 110 110 110 110 110
[PUMPS];ID	Node1	Node2		Parameters		
[VALVES] ;ID MinorLoss	Node1	Node2		Diameter	Type Settin	g
[TAGS] [DEMANDS] ;Junction	Demand	Pattern	Catego	ry		
[STATUS];ID	Status/Setting					
[PATTERNS];ID	Multipliers					
[CURVES];ID	X-Value	Y-Value				
[CONTROLS]						
[RULES]						
[ENERGY] Global Efficiency	75					

```
Demand Charge
[EMITTERS]
                        Coefficient
;Junction
[QUALITY]
                        InitQual
;Node
[SOURCES]
;Node
                        Type
                                        Quality
                                                         Pattern
[REACTIONS]
                Pipe/Tank
                                        Coefficient
;Type
[REACTIONS]
Order Bulk
Order Tank
                        1
Order Wall
                        1
Global Bulk
                        0
Global Wall
                        0
Limiting Potential
                        0
Roughness Correlation
[MIXING]
                        Model
;Tank
[TIMES]
Duration
                        0
Hydraulic Timestep
                        1:00
                        0:05
Quality Timestep
Pattern Timestep
                        1:00
Pattern Start
                        0:00
 Report Timestep
                        1:00
 Report Start
                        0:00
 Start ClockTime
                        12 am
Statistic
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Status
Summary
                        No
Page
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Headloss
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Specific Gravity
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Viscosity
                        1
                        40
Trials
 Accuracy
                        0.001
 CHECKFREQ
                        2
MAXCHECK
                        10
DAMPLIMIT
Unbalanced
                        Continue 10
Pattern
Demand Multiplier
 Emitter Exponent
                        0.5
Quality
                        None mg/L
Diffusivity
Tolerance
                        0.01
[COORDINATES]
Node
                        X-Coord
                                                 Y-Coord
Metro
                        2805.56
                                                 8311.11
                        1616.67
                                                 5644.44
Bldg-A
                        2661.11
                                                 5655.56
hyd1
                        3061.11
                                                 5644.44
```

4138.89

3000.00

Global Price

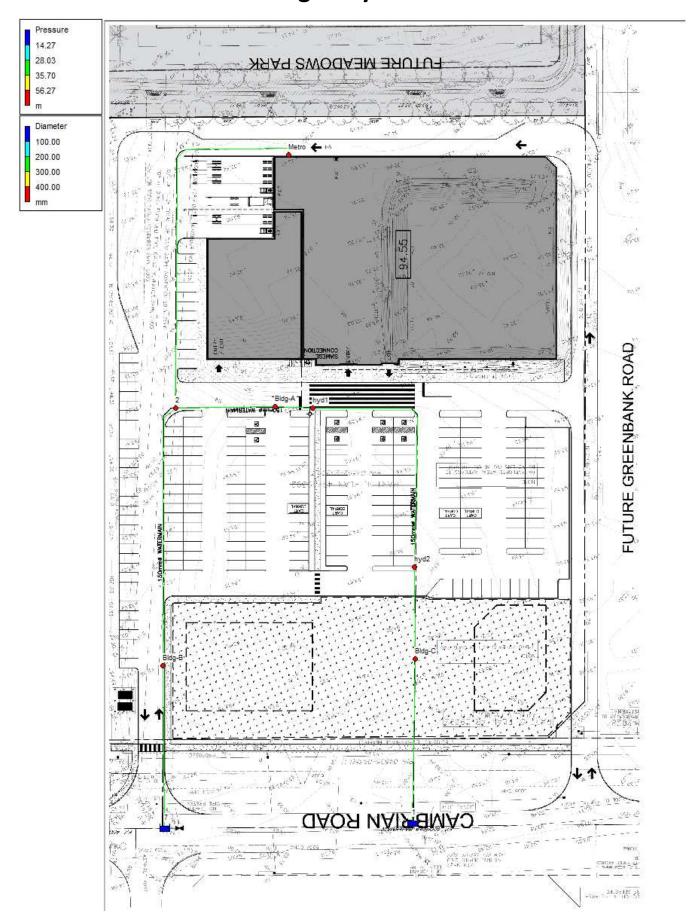
Bldg-C

0

Bldg-B	1480.16	2928.57		
hyd2	4127.78	3966.67		
7	1494.44	1211.11		
1	4105.56	1266.67		
[VERTICES]				
;Link	X-Coord	Y-Coord		
1	1483.33	5533.33		
2	1627.78	8277.78		
2	1716.67	8366.67		
2	2816.67	8377.78		
5	4105.56	5644.44		
5	4161.11	5544.44		
[LABELS]				
;X-Coord	Y-Coord	Label & Anchor Node		
[BACKDROP]				
DIMENSIONS	0.00	0.00	10000.00	10000.00
UNITS	None			
FILE	Z:\Project	ts\19-1135 Metro - Greenbank		
Rd\B_Design\B1_An	alysis\B1-5_Water	\EPANet\Background\2020-07-28	Greenbank-Metro_spa_base	-fig-11x17.bmp
OFFSET	0.00	0.00		- '

[END]

# **Average Day Demand**



# AVERAGE DAY

\* E P A N E T \*

\* Hydraulic and Water Quality \*

\* Analysis for Pipe Networks \*

Input File: 1135\_Avg-Day.net

Link - Node Table:

Link ID	Start Node	End Node	Length m	Diameter mm
1	Bldg-B	2	64	200
2	2	Metro	109	200
3	2	Bldg-A	28.5	200
4	Bldg-A	hyd1	7	200
5	hyd1	hyd2	73	200
9	Bldg-C	1	53	200
10	Bldg-B	7	52	200
6	hyd2	Bldg-C	18	200

### Node Results:

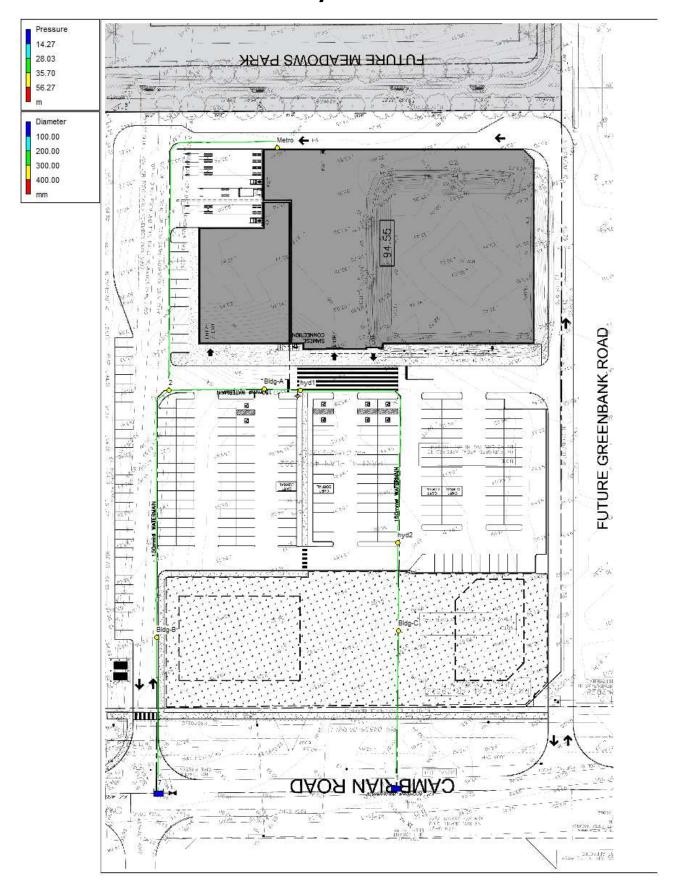
Node ID	Demand LPM	Head m	Pressure m	Quality	
Metro	7.00	155.90	62.00	0.00	
2	0.00	155.90	62.15	0.00	
Bldg-A	1.60	155.90	62.10	0.00	
hyd1	0.00	155.90	61.90	0.00	
Bldg-C	3.90	155.90	62.25	0.00	
Bldg-B	1.40	155.90	61.75	0.00	
hyd2	0.00	155.90	62.05	0.00	
7	-6.65	155.90	0.00	0.00	Reservoir
1	-7.25	155.90	0.00	0.00	Reservoir

### Link Results:

Link ID	Flow LPM	VelocityUni m/s	t Headloss m/km	Status	
1	5.25	0.00	0.00	Open	
2	7.00	0.00	0.00	0pen	
3	-1.75	0.00	0.00	0pen	
4	-3.35	0.00	0.00	0pen	
5	-3.35	0.00	0.00	0pen	
9	-7.25	0.00	0.00	0pen	
10	-6.65	0.00	0.00	0pen	
6	-3.35	0.00	0.00	0pen	

↑ Page 2

# Max Day + Fire Flow



# MAX DAY + FIRE FLOW

\* EPANET \*

\* Hydraulic and Water Quality \*

\* Analysis for Pipe Networks \*

\* Version 2.0

Input File: 1135\_Max-Day+FF.net

### Link - Node Table:

Link ID	Start Node	End Node	Length m	Diameter mm
1	Bldg-B	2	64	200
2	2	Metro	109	200
3	2	Bldg-A	28.5	200
4	Bldg-A	hyd1	7	200
5	hyd1	hyd2	73	200
9	Bldg-C	1	53	200
10	Bldg-B	7	52	200
6	hyd2	Bldg-C	18	200

### Node Results:

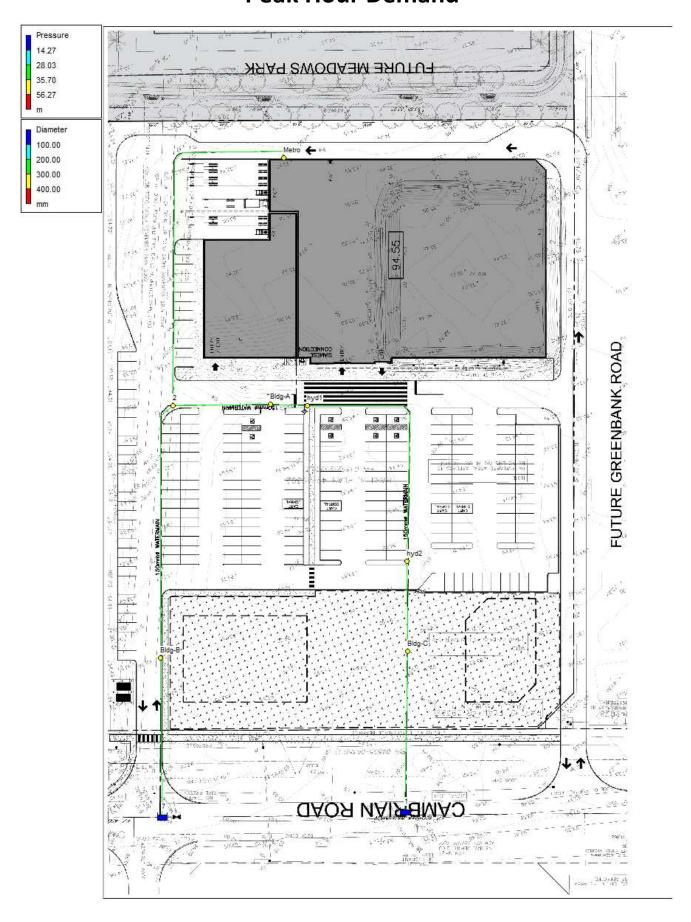
Node ID	Demand LPM	Head m	Pressure m	Quality	
Metro	10.50	133.29	39.39	0.00	
2	0.00	133.29	39.54	0.00	
Bldg-A	2.40	132.76	38.96	0.00	
hyd1	5678.00	132.57	38.57	0.00	
Bldg-C	5.90	134.32	40.67	0.00	
Bldg-B	2.20	134.51	40.36	0.00	
hyd2	322.00	133.87	40.02	0.00	
7	-2896.89	135.60	0.00	0.00	Reservoir
1	-3124.11	135.60	0.00	0.00	Reservoir

# Link Results:

Link ID	Flow LPM	VelocityUnit m/s	Headloss m/km	Status
1	2894.69	1.54	18.99	0pen
2	10.50	0.01	0.00	0pen
3	2884.19	1.53	18.76	0pen
4	2881.79	1.53	26.43	0pen
5	-2796.21	1.48	17.80	0pen
9	-3124.11	1.66	24.12	0pen
10	-2896.89	1.54	21.01	0pen
6	-3118.21	1.65	24.97	0pen

↑ Page 2

# **Peak Hour Demand**



#### PEAK HOUR 2021-04-06 1:42:20 PM

EPANET Hydraulic and Water Quality Analysis for Pipe Networks Version 2.0

Input File: 1135\_Peak-Hour.net

Link - Node Table:

Link	Start	End	Length	Diameter
ID	Node	Node	m	mm
1	Bldg-B	2	64	200
2	2	Metro	109	200
3	2	Bldg-A	28.5	200
4	Bldg-A	hyd1	7	200
5	hyd1	hyd2	73	200
9	Bldg-C	1	53	200
10	Bldg-B	7	52	200
6	hyd2	Bldg-C	18	200

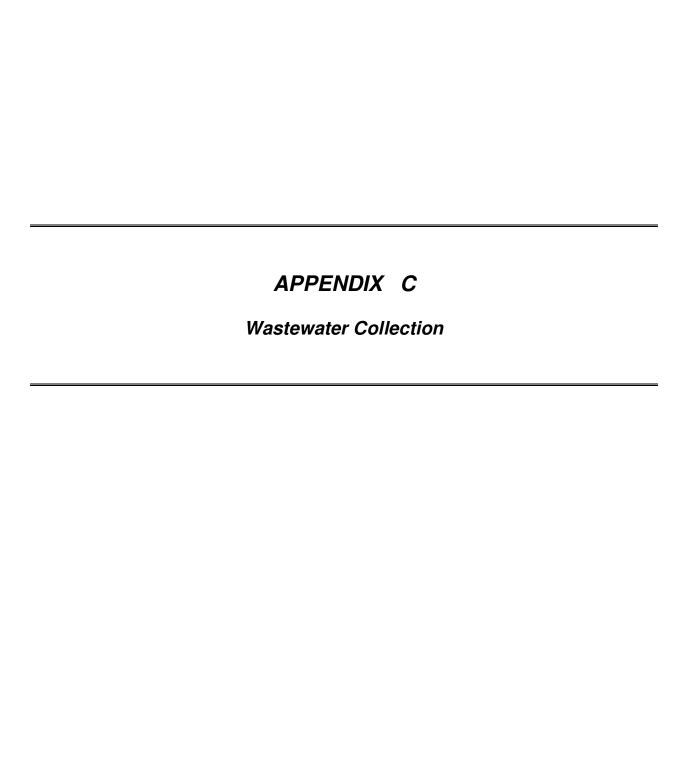
### Node Results:

Demand	Head	Pressure	Quality	
LPM	m	m		
18.90	139.00	45.10	0.00	
0.00	139.00	45.25	0.00	
4.40	139.00	45.20	0.00	
0.00	139.00	45.00	0.00	
10.50	139.00	45.35	0.00	
3.90	139.00	44.85	0.00	
0.00	139.00	45.15	0.00	
-18.07	139.00	0.00	0.00	Reservoir
-19.63	139.00	0.00	0.00	Reservoir
	18.90 0.00 4.40 0.00 10.50 3.90 0.00 -18.07	LPM m  18.90 139.00 0.00 139.00 4.40 139.00 0.00 139.00 10.50 139.00 3.90 139.00 0.00 139.00 -18.07 139.00	LPM m m  18.90 139.00 45.10  0.00 139.00 45.25  4.40 139.00 45.20  0.00 139.00 45.00  10.50 139.00 45.35  3.90 139.00 44.85  0.00 139.00 45.15  -18.07 139.00 0.00	LPM m m  18.90 139.00 45.10 0.00 0.00 139.00 45.25 0.00 4.40 139.00 45.20 0.00 0.00 139.00 45.00 0.00 10.50 139.00 45.35 0.00 3.90 139.00 44.85 0.00 0.00 139.00 45.15 0.00 -18.07 139.00 0.00 0.00

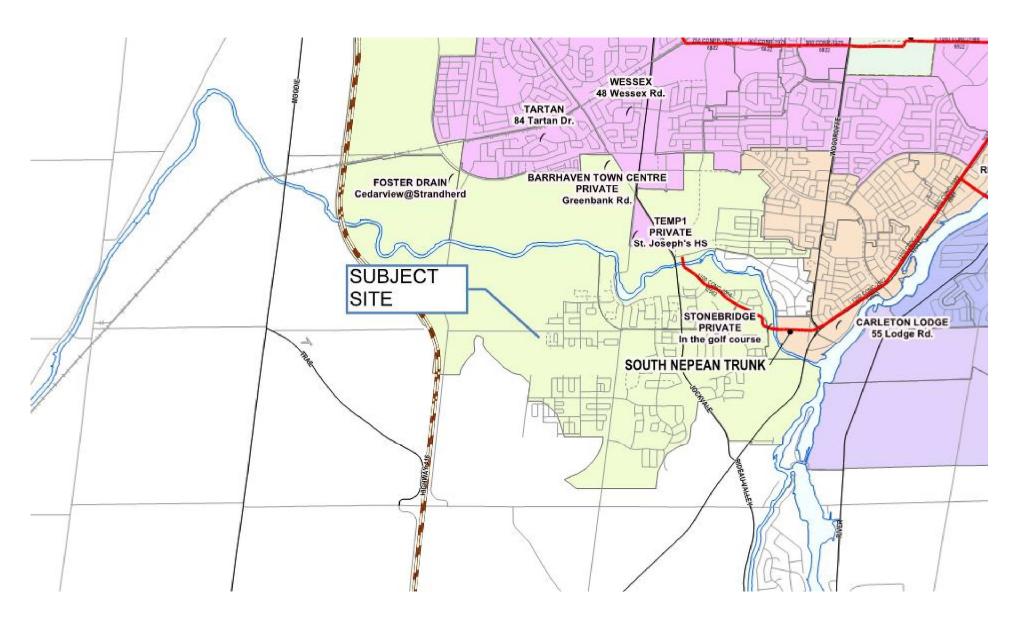
# Link Results:

Link ID	Flow LPM	VelocityUni m/s	it Headloss m/km	Status	
1	14.17	0.01	0.00	Open	
2	18.90	0.01	0.00	0pen	
3	-4.73	0.00	0.00	0pen	
4	-9.13	0.00	0.00	0pen	
5	-9.13	0.00	0.00	0pen	
9	-19.63	0.01	0.00	0pen	
10	-18.07	0.01	0.00	0pen	
6	-9.13	0.00	0.00	0pen	

↑ Page 2



# **Sanitary Trunk Sewer and Collection Area Map**



# Metro Canada Inc. 3831 Cambrian Road Proposed Site Conditions

Wastewater Design Flows per Unit Count City of Ottawa Sewer Design Guidelines, 2004



Site Area 2.200 ha

**Extraneous Flow Allowances** 

Infiltration / Inflow (Dry) 0.11 L/s
Infiltration / Inflow (Wet) 0.62 L/s
Infiltration / Inflow (Total) 0.73 L/s

Institutional / Commercial / Industrial Contributions

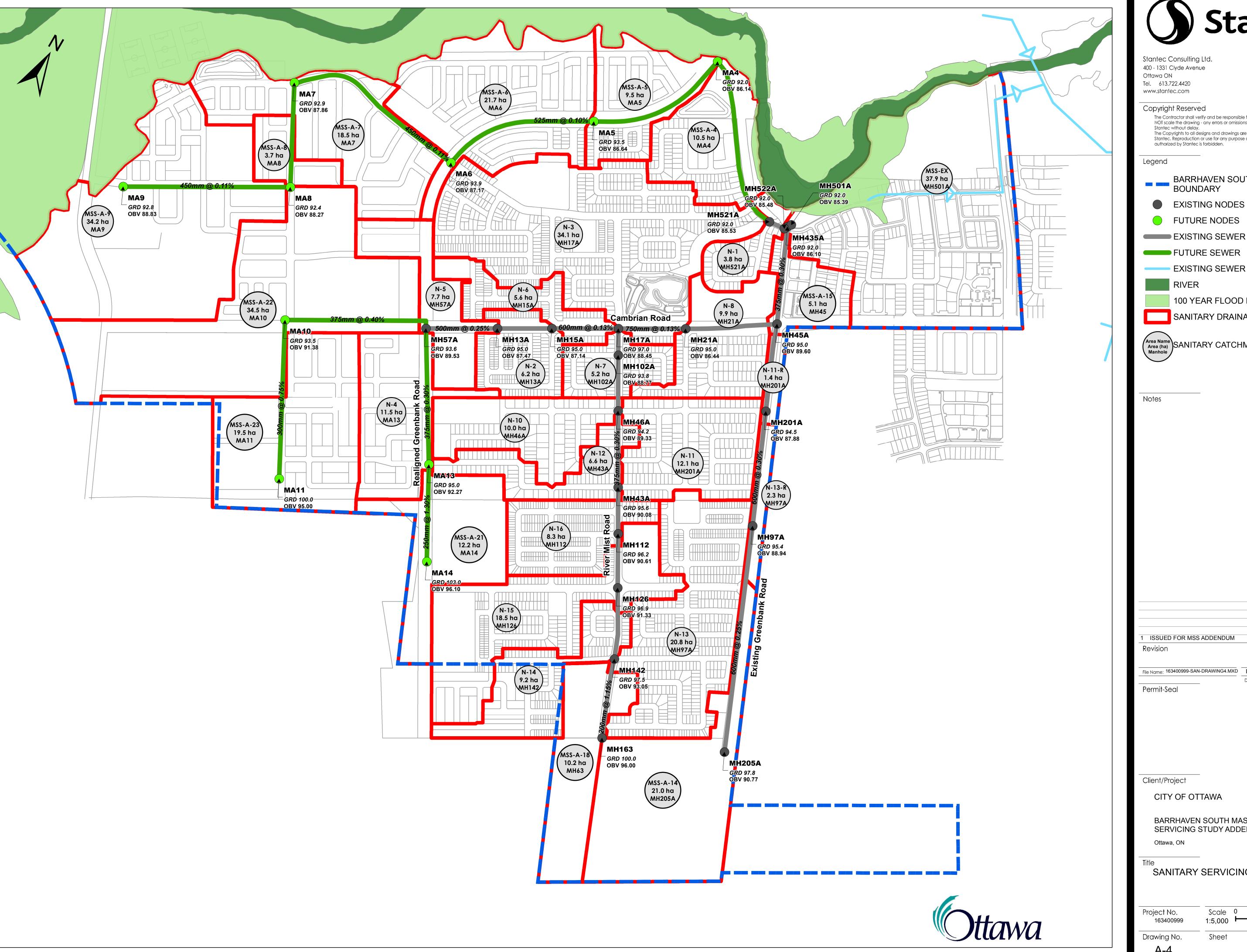
Property Type	Unit Rat	е	No. of Units	Avg Wastewater (L/s)
Metro	5 L/r	n²/d	4,024	0.47
Bldg A	5 L/r	n²/d	929	0.11
Bldg B	5 L/r	n²/d	830	0.10
Bldg C (Retail)	5 L/r	n²/d	530	0.06
Bldg C (Office)	75 L/9	9.3m <sup>2</sup> /d	530	0.10
		Av	erage I/C/I Flow	0.83

Average 1/O/11 low	0.03
Peak Institutional / Commercial Flow	1.24
Peak I/C/I Flow	1.48

<sup>\*</sup> assuming a 12 hour commercial operation

<sup>\*\*</sup> peak industrial flow per City of Ottawa Sewer Design Guidelines Appendix 4B

Total Estimated Average Dry Weather Flow Rate	0.94 L/s
Total Estimated Peak Dry Weather Flow Rate	1.59 L/s
Total Estimated Peak Wet Weather Flow Rate	2.21 L/s





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BARRHAVEN SOUTH COMMUNITY

EXISTING NODES **Node Name Ground Elevation** Top Obvert Elevation

EXISTING SEWER (FROM 2007 MSS)

RIVER

100 YEAR FLOOD PLAIN

SANITARY DRAINAGE CATCHMENTS

(Area Name ) SANITARY CATCHMENT INFORMATION

ISSUED FOR MSS ADDENDUM File Name: 163400999-SAN-DRAWING4.MXD LP AP LP 14.11.28 Dwn. Chkd. Dsgn. YY.MM.DD

CITY OF OTTAWA

BARRHAVEN SOUTH MASTER SERVICING STUDY ADDENDUM

SANITARY SERVICING PLAN

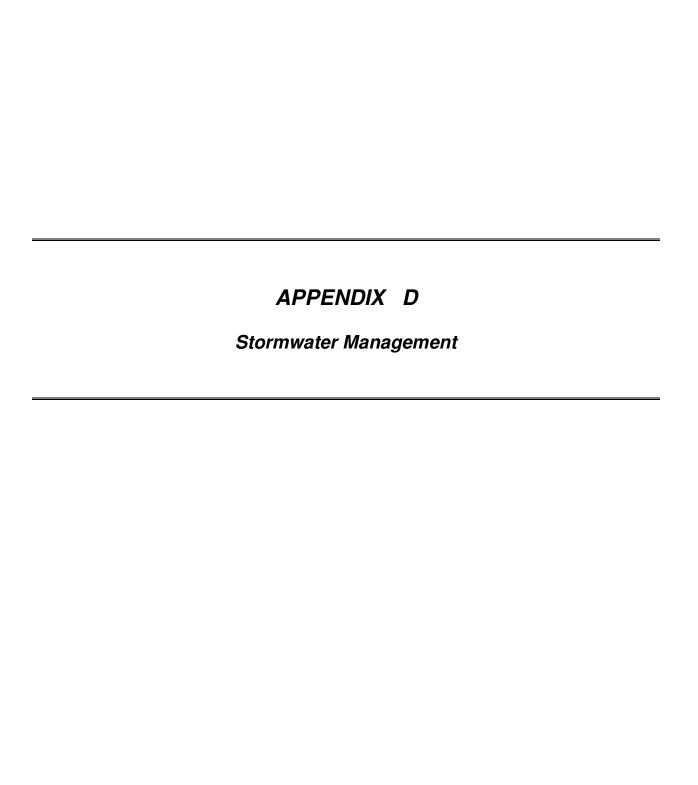
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163400999	1:5,000	,	,	Meters	, ,	
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A-4		4 of 9	)		1	

			Area:	ARRHAV	EN SOU	TU					NITAR													DESI	GN PARAMET	ERS_										
				BY:	VICING S		FILE NUM	BER:		16340099	, -	Colour code: Hard code Caculated	d values	HMB values Most US M Estimated	iH .		MIN PEAK FA PEAKING FA PEAKING FA	ACTOR (RES.): ACTOR (RES.): CTOR (INDUS CTOR (COMM SINGLE UNIT	= TRIAL):	4.0 2.0 2.4 1.5 3.4		AVG. DAILY F COMMERCIAI INDUSTRIAL ( INDUSTRIAL ( INSTITUTION	HEAVY) LIGHT)	N	350 50,000 55,000 35,000 50,000	L/ha/day L/ha/day		MINIMUM VE MAXIMUM VE MANNINGS n BEDDING CL MINIMUM CO	ELOCITY ASS	0.60 3.00 0.013 B 2.50	m/s m/s	AS PER CDP (U LOW DENSIT SEMI-DETACH TOWN HOUSE APARTMENTS COMMUNITY	Y RESIDENTIA HED ES	L		26 52 82 120 60
										updated v	alue	Value from design	subdivision	MH receivi sewers	ng flow from	2 or more	PERSONS / PERSONS / /			2.7 1.8		INFILTRATION	I		0.28	L/s/ha						AVERAGE PE	RSONS/ha			107
AREA ID	OCATION	FROM	ТО	DEV	DEV	ADD'N	RESI ADD'N	TOTAL	EA AND POPU TOTAL		ULATIVE	PEAK	PEAK	COMN AREA	ACCU.	INDUS AREA	ACCU.	INDUST AREA	ACCU.	INSTITU AREA	ACCU.	GREEN / AREA	ACCU.	C+I+I PEAK	TOTAL	ACCU.	INFILT.	TOTAL FLOW	LENGTH	DIA	MATERIAL	PIPE SLOPE	CAP.	CAP. V	VEL.	VEL.
NUMBER	Source	M.H.	M.H.	AREA (ha)	POP	RES AREA (ha)	POP	AREA (ha)	POP	AREA (ha)	POP.	FACT.	FLOW (L/s)	(ha)	AREA (ha)	(ha)	AREA (ha)	(ha)	AREA (ha)	(ha)	AREA (ha)	(ha)	AREA (ha)	FLOW (L/s)	AREA (ha)	AREA (ha)	FLOW (L/s)	(L/s)	(m)	(mm)		(%)	(FULL) (L/s)	PEAK FLOW (%)	(FULL) (m/s)	(ACT.) (m/s)
MSS-A-23 MSS-A-22		MA11 MA10	MA10 MH57A	0.00	0	14.2 12.8	1,523 1,371	14.2 12.8	1,523 1,371	14.20 27.00	1,523 2,894	3.67 3.46	22.6 40.6	0.0 0.0	0.0 0.0	0.0	0.0 0.0	0.0	0.0	2.8 7.2	2.8 10.0	2.5 14.5	2.5 17.0	2 8.7	19.5 34.5	19.5 54.0	5.5 15.1	30.1 64.4	482.1 449.7	300 375	PVC PVC	0.75 0.40	87.6 115.1	34% 56%	1.20 1.01	1.08 1.04
Realigned Greenbank Road MSS-A-21 N-4	I	MA14 MA13	MA13 MH57A	0.0	0	4.8 11.0	513 1,176	4.8 11.0	513 1,176	4.8 15.8	513 1,689	3.97 3.64	8.3 24.9	0.0 0.0	0.0 0.0	0.0	0.0 0.0	0.0	0.0	7.5 0.0	7.5 7.5	0.0 0.5	0.0 0.5	6.5 6.5	12.3 11.5	12.3 23.8	3.4 6.7	18.2 38.1	295.0 413.1	250 375	PVC PVC	1.30 0.30	71.4 100.3	25% 38%	1.40 0.88	1.12 0.81
Cambrian Road N-5 N-2 N-6		MH57A MH13A MH15A	MH13A MH15A MH17A	0.0 6.2 5.6	0 631 868	4.3 0.0 0.0	458 3 2	4.3 6.2 5.6	458 634 870	47.1 53.3 58.9	5,041 5,675 6,545	3.24 3.19 3.13	66.2 73.3 83.0	3.4 0.0 0.0	3.4 3.4 3.4	0.0 0.0 0.0	0.0 0.0 0.0	0.0 0.0 0.0	0.0 0.0 0.0	0.0 0.0 0.0	17.5 17.5 17.5	0.0 0.0 0.0	17.5 17.5 17.5	18.1 18.1 18.1	7.7 6.2 5.6	85.5 91.7 97.3	23.9 25.7 27.2	108.2 117.1 128.3	216.5 165.2 202.0	500 500 600	CPP CPP CPP	0.25 0.20 0.13	188.2 168.6 230.7	57% 69% 56%	0.96 0.86 0.79	0.99 0.93 0.81
River Mist Road MSS-A-18 N-14 N-15 N-16	Stantec Stantec Stantec Stantec Stantec Stantec Stantec Stantec Stantec Stantec Stantec	MH163 162 161 EX151 MH142 EX139 EX136 MH126 EX123 MH112	162 161 EX151 MH142 EX139 EX136 MH126 EX123 MH112 EX102	6.5 0.0 0.0 0.0 8.2 0.0 0.0 16.5 0.0 8.3	543 0 0 0 825 0 0 954 0	0.0 0.0 0.0 0.0 1.0 0.0 0.0 0.0 0.0	0 0 0 0 102 0 0 0	6.5 0.0 0.0 0.0 9.2 0.0 0.0 16.5 0.0 8.3	543 0 0 0 927 0 0 954 0 689	6.5 6.5 6.5 6.5 15.7 15.7 15.7 22.2 32.2 40.5	543 543 543 543 1,470 1,470 2,424 2,424 3,113	3.96 3.96 3.96 3.96 3.69 3.69 3.52 3.52 3.43	8.7 8.7 8.7 22.0 22.0 22.0 34.6 34.6 43.3	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	2.8 0.0 0.0 0.0 0.0 0.0 0.0 0.0 2.1 0.0	2.8 2.8 2.8 2.8 2.8 2.8 4.9 4.9	0.9 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.9 0.9 0.9 0.9 0.9 0.9 0.9	2.4 2.4 2.4 2.4 2.4 2.4 2.4 4.3 4.3	10.2 0.0 0.0 0.0 9.2 0.0 0.0 18.6 0.0 8.3	10.2 10.2 10.2 10.2 19.4 19.4 19.4 38.0 38.0 46.3	2.9 2.9 2.9 2.9 5.4 5.4 10.6 10.6 13.0	14.0 14.0 14.0 14.0 29.8 29.8 29.8 49.5 49.5 60.6	36.3 87.2 75.6 44.4 74.8 64.7 78.9 71.3 90.3 68.0	200 250 250 300 300 300 300 375 375	PVC	1.15 1.15 1.15 1.40 0.40 0.40 0.41 0.45 0.42	35.8 67.3 67.3 119.0 63.5 63.5 64.2 122.0 118.6 101.5	39% 21% 21% 12% 47% 47% 46% 41% 42% 60%	1.12 1.32 1.32 1.63 0.87 0.87 0.88 1.07 1.04 0.89	1.04 1.00 1.00 1.08 0.85 0.85 0.86 1.01 0.99
N-12 N-10 N-7		EX102 EX101 MH43A MH44A MH45A MH46A MH47A MH101A MH102A	EX101 MH43A MH44A MH45A MH46A MH47A MH101A MH102A MH17A	0.0 0.0 6.6 0.0 0.0 8.4 0.0 0.0 4.0	0 0 352 0 0 562 0 0 291	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.2	0 0 0 0 0 0 0 0 0	0.0 0.0 6.6 0.0 0.0 8.4 0.0 0.0 5.2	0 0 352 0 0 562 0 0 420	40.5 40.5 47.1 47.1 47.1 55.5 55.5 55.5 60.7	3,113 3,113 3,465 3,465 3,465 4,027 4,027 4,027 4,047	3.43 3.43 3.39 3.39 3.39 3.33 3.33 3.33	43.3 43.3 47.6 47.6 47.6 54.3 54.3 59.3	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	4.9 4.9 4.9 4.9 4.9 4.9 4.9	0.0 0.0 0.0 0.0 0.0 1.6 0.0 0.0	0.9 0.9 0.9 0.9 0.9 2.5 2.5 2.5	4.3 4.3 4.3 4.3 4.3 4.3 4.3 4.3 4.3	0.0 0.0 6.6 0.0 0.0 10.0 0.0 5.2	46.3 46.3 52.9 52.9 52.9 62.9 62.9 62.9 68.1	13.0 13.0 14.8 14.8 14.8 17.6 17.6 17.6	60.6 60.6 66.7 66.7 76.2 76.2 76.2 82.7	34.0 38.0 81.0 64.0 85.0 41.0 64.0 64.0 81.0	375 375 375 375 375 375 375 375 375 375	PVC	0.29 0.30 0.30 0.30 0.30 0.30 0.30 0.30 0.3	98.0 100.3 100.3 100.3 100.3 100.3 100.3 100.3 100.3	62% 60% 67% 67% 67% 76% 76% 76% 82%	0.86 0.88 0.88 0.88 0.88 0.88 0.88 0.88	0.91 0.92 0.95 0.95 0.95 0.98 0.98 0.98
Cambrian Road N-3 N-8		MH17A MH21A	MH21A MH45	26.0 7.0	1,956 408	0.0	0	26.0 7.0	1,956 408	145.6 152.6	12,948 13,356	2.84 2.83	149.0 153.1	0.0	3.4 3.4	0.0	0.0	0.0	0.0	3.0 0.0	25.4 25.4	5.1 2.9	25.1 28.0	25.0 25.0	34.1 9.9	199.5 209.4	55.9 58.6	229.9 236.7	204.3 277.8	750 750	CPP CPP	0.13 0.13	419.5 419.5	55% 56%	0.92 0.92	0.94 0.95
Greenbank Road MSS-A-14 N-13, N-13-R N-11, N-11-R MSS-A-15	IBI	MH201A MH201B MH200A MH200C	MH200C	0.0	0 0 0 0 0 0 0 1,625 0 0 787 0	21.0 0.0 0.0 0.0 0.0 0.0 0.1 0.0 0.0 0.0	2,246 0 0 0 0 0 0 0 6 0 0 0 0 0 0 0 0 0 0 0	21.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 12.1 0.0 0.0 0.0	2,246 0 0 0 0 0 1,631 0 0 787 0 0	21.0 21.0 21.0 21.0 21.0 21.0 41.0 41.0 41.0 53.1 53.1 53.1	2,246 2,246 2,246 2,246 2,246 3,877 3,877 4,664 4,664 4,664	3.55 3.55 3.55 3.55 3.55 3.55 3.35 3.35	32.3 32.3 32.3 32.3 32.3 52.6 52.6 52.6 61.8 61.8 61.8	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.8 0.8 0.8 0.8	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	21.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 12.1 0.0 0.0 0.0	21.0 21.0 21.0 21.0 21.0 21.0 21.0 41.8 41.8 53.9 53.9 53.9 53.9	5.9 5.9 5.9 5.9 5.9 5.9 11.7 11.7 15.1 15.1 15.1 75.2	38.2 38.2 38.2 38.2 38.2 38.2 64.3 64.3 76.9 76.9 76.9	126.0 125.0 108.0 105.0 103.0 125.0 98.0 129.0 123.0 124.0 48.0 26.0	600 600 600 600 600 600 600 600 600 600	CPP	0.25 0.25 0.25 0.25 0.25 0.30 0.30 0.30 0.30 0.30 0.30 0.30	321.2 321.2 321.2 321.2 321.2 321.2 350.4 350.4 350.4 350.4 452.6 221.9	12% 12% 12% 12% 12% 12% 18% 18% 22% 22% 51%	1.10 1.10 1.10 1.10 1.10 1.10 1.20 1.20	0.73 0.73 0.73 0.73 0.73 0.73 0.89 0.89 0.89 0.94 0.94 1.12 0.68
MSS-A-9 MSS-A-8 MSS-A-7 MSS-A-6 MSS-A-5 MSS-A-4		MH5200A MH520A MH521A	MA8 MA7 MA6 MA5 M27A MH5200A MH520A MH521A MH522A MH435A	0.0	0 0 0 0 0 0 0 0 0 0 177 0	22.2 2.9 18.5 21.7 9.5 8.1 0.0 0.0 0.5 0.0	2,378 308 1,979 2,320 1,020 863 0 0 54 0	22.2 2.9 18.5 21.7 9.5 8.1 0.0 0.0 3.8 0.0	2,378 308 1,979 2,320 1,020 863 0 0 231 0	22.2 25.1 43.6 65.3 74.8 82.9 82.9 82.9 86.7 86.7	2,378 2,686 4,665 6,985 8,005 8,868 8,868 9,099 9,099	3.53 3.48 3.27 3.11 3.05 3.01 3.01 3.01 3.00 3.00	34.0 37.9 61.8 88.0 98.9 108.1 108.1 110.6 110.6	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	2.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5	9.5 0.8 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	9.5 10.3 10.3 10.3 10.3 10.3 10.3 10.3 10.3	2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2	34.2 3.7 18.5 21.7 9.5 8.1 0.0 0.0 3.8 0.0	34.2 37.9 56.4 78.1 87.6 95.7 95.7 95.7 99.5 99.5	9.6 10.6 15.8 21.9 24.5 26.8 26.8 27.9 27.9	45.8 50.7 79.8 112.1 125.6 137.1 137.1 137.1 140.7 411.5	507.5 317.1 573.1 473.9 220.0 501.5 46.0 44.4 50.1 10.8		CPP	0.11 0.11 0.11 0.10 0.10 0.15 0.08 0.10 0.09 0.21	98.4 98.4 98.4 201.5 201.5 248.2 181.0 201.5 192.7 292.0	47% 52% 81% 56% 62% 55% 76% 68% 73% 48%	0.60 0.60 0.69 0.69 0.85 0.62 0.69 0.66 1.00	0.59 0.61 0.67 0.71 0.73 0.87 0.69 0.75 0.73 0.99 1.02

SANITARY SEWER DESIGN SHEET BARRHAVEN SOUTH MASTER SERVICING MAS

			MAS	STU	DY											
			DATE:	2017/09/29						PIPE D	DESIGN					
			REVISION:								Colour code:					
			DESIGNED	LP		FILE NUMI	BER:		163400999	)	Hard coded	values	Most US MI	Н		
			CHECKED	/							Caculated va	alue	Estimated v	alue		
											Value from s	subdivision	MH receiving	g flow from	2 or more	
											design		sewers			
	LOCATION				CAL	CULATED VAI				UPST	REAM				STREAM	
AREA ID		FROM	TO	ACTUAL	AREA	HYDR.	SURCHARGE		GROUND	OBVERT	INVERT	U/S	GROUND	OBVERT	INVERT	D/S
NUMBER	Source	M.H.	M.H.	PIPE SIZE		RADIUS	VELOCITY	OF FLOW	ELEVATION	ELEVATION	ELEVATION	COVER	ELEVATION	ELEVATION	ELEVATION	COVER
				(mm)	(m <sup>2</sup> )		(m/s)	(m)	(m)	(m)	(m)	(m)	(m)	(m)	(m)	(m)
1400 1 00			14440	005	0.070	0.070			400.00	05.000	04.005	<b>5</b> 00	00.50	04.004	04.070	0.40
MSS-A-23		MA11	MA10	305	0.073	0.076			100.00	95.000	94.695	5.00	93.50	91.384	91.079	2.12
MSS-A-22		MA10	MH57A	381	0.114	0.095			93.50	91.324	90.943	2.18	93.60	89.525	89.144 st be above 8	4.07
Realigned Greenbank Ro	ad													·· IIIu	st be above o	00.01
MSS-A-21	uu	MA14	MA13	254	0.051	0.064			103.00	96.100	95.846	6.90	95.00	92.265	92.011	2.74
N-4		MA13	MH57A	381	0.114	0.095			95.00	89.800	89.419	5.20	93.60	88.561	88.180	5.04
															above plug	
Cambrian Road																
N-5		MH57A	MH13A	500	0.196	0.125			93.60	88.010	87.510	5.59	95.00	87.469	86.969	7.53
N-2		MH13A	MH15A	500	0.196	0.125			95.00	87.469	86.969	7.53	95.00	87.139	86.639	7.86
N-6		MH15A	MH17A	610	0.292	0.152			95.00	87.139	86.529	7.86	97.00	86.876	86.266	10.12
River Mist Road	01		400	000	0.655	0.075	0.000	0.675	400.00	00.000	05.50	4.00	00	05.500	0.5.000	0.67
MSS-A-18	Stantec	MH163	162	203	0.032	0.050	0.333	0.058	100.00	96.000	95.797	4.00	99.55	95.580	95.380	3.97
	Stantec	162	161	254	0.051	0.064	0.284	0.053	99.55	95.580	95.330	3.97	98.55	94.580	94.327	3.97
	Stantec	161 EY151	EX151	254 305	0.051	0.064	0.285	0.053	98.55	94.540	94.292	4.00	97.88	93.670	93.423	4.21
N-14	Stantec Stantec	EX151 MH142	MH142 EX139	305 305	0.073 0.073	0.076 0.076	0.201 0.351	0.036 0.120	97.88 97.48	93.670 93.030	93.373 92.732	4.21 4.44	97.48 96.84	93.050 92.730	92.752 92.433	4.42 4.11
14-14	Stantec	EX139	EX136	305	0.073	0.076	0.366	0.126	96.84	92.710	92.411	4.13	96.66	92.450	92.152	4.21
	Stantec	EX136	MH126	305	0.073	0.076	0.383	0.129	96.66	91.650	91.350	5.01	96.85	91.320	91.024	5.53
N-15	Stantec	MH126	EX123	381	0.114	0.095	0.415	0.147	96.85	91.330	90.959	5.52	96.41	91.010	90.639	5.39
	Stantec	EX123	MH112	381	0.114	0.095	0.441	0.161	96.41	90.990	90.616	5.42	96.22	90.610	90.236	5.61
N-16	Stantec	MH112	EX102	381	0.114	0.095	0.497	0.213	96.22	90.590	90.213	5.63	95.71	90.380	90.003	5.33
	Stantec	EX102	EX101	381	0.114	0.095	0.562	0.246	95.71	90.360	89.984	5.35	95.69	90.260	89.884	5.43
	IBI	EX101	MH43A	381	0.114	0.095			95.69	90.265	89.884	5.43	95.60	90.090	89.709	5.51
N-12	IBI	MH43A	MH44A	381	0.114	0.095			95.60	90.070	89.689	5.53	95.50	89.826	89.445	5.67
	IBI	MH44A	MH45A	381	0.114	0.095			95.50	89.806	89.425	5.69	95.00	89.604	89.223	5.40
	IBI	MH45A	MH46A	381	0.114	0.095			95.00	89.594	89.213	5.41	94.20	89.339	88.958	4.86
N-10	IBI	MH46A	MH47A	381	0.114	0.095			94.20	89.319	88.938	4.88	94.20	89.181	88.800	5.02
	DSEL	MH47A MH101A	MH101A	381	0.114	0.095			94.20	89.181	88.800	5.02	94.20	88.989	88.608	5.21
N-7	DSEL DSEL	MH101A	MH102A MH17A	381 381	0.114 0.114	0.095 0.095			94.20 93.80	88.969 88.693	88.588 88.312	5.23 5.11	93.80 93.40	88.777 88.451	88.396 88.070	5.02 4.95
14-7	DOEL	WITHIUZA	WILLIA	361	0.114	0.095			93.00	00.093	00.312	5.11	93.40	00.401	00.070	4.95
Cambrian Road																
N-3		MH17A	MH21A	762	0.456	0.190			97.00	86.876	86.114	10.12	95.00	86.773	86.011	8.23
N-8		MH21A	MH45	762	0.456	0.190			95.00	86.773	86.011	8.23	94.50	86.412	85.650	8.09
Greenbank Road																
MSS-A-14	IBI	MH205A	MH98A	610	0.292	0.152			97.80	90.780	90.170	7.02	97.40	90.465	89.855	6.94
	IBI	MH98A	MH99A	610	0.292	0.152			97.40	90.443	89.833	6.96	96.90	90.130	89.520	6.77
	IBI	MH99A	MH100A	610	0.292	0.152			96.90	90.105	89.495	6.80	96.60	89.835	89.225	6.77
	IBI	MH100A	MH204A	610	0.292	0.152			96.60	89.803	89.193	6.80	96.20	89.540	88.930	6.66
	IBI IBI	MH204A MH206A	MH206A MH97A	610 610	0.292 0.292	0.152 0.152			96.20 95.80	89.517 89.260	88.907 88.650	6.68 6.54	95.80 95.40	89.260 88.948	88.650 88.338	6.54 6.45
N-13, N-13-R	IBI	MH97A	MH96A	610	0.292	0.152			95.80 95.40	88.938	88.328	6.46	95.40	88.643	88.033	6.56
14 10, 14-10-10	IBI	MH96A	MH95A	610	0.292	0.152			95.20	88.643	88.033	6.56	95.00	88.256	87.646	6.74
	IBI	MH95A	MH201A	610	0.292	0.152			95.00	88.256	87.646	6.74	94.50	87.887	87.277	6.61
N-11, N-11-R	IBI	MH201A	MH201B	610	0.292	0.152			94.50	87.887	87.277	6.61	94.70	87.514	86.904	7.19
	IBI	MH201B	MH200A	610	0.292	0.152			94.70	87.510	86.900	7.19	94.40	87.307	86.697	7.09
	IBI	MH200A	MH200C	610	0.292	0.152			94.40	87.241	86.631	7.16	94.80	87.001	86.391	7.80
	IBI	MH200C	MH45	610	0.292	0.152			94.80	87.001	86.391	7.80	94.50	86.405	85.795	8.10
MSS-A-15		MH45	MH435A	914	0.656	0.228			94.50	86.405	85.491	8.10	92.60	86.108	85.194	6.49
North																
North MSS-A-9		MA9	MA8	457	0.164	0.114			92.75	89.550	89.093	3.20	92.35	88.992	88.535	3.36
MSS-A-9 MSS-A-8		MA8	MA7	457	0.164	0.114			92.75	88.932	88.475	3.42	92.35	88.583	88.126	4.32
MSS-A-7		MA7	MA6	457	0.164	0.114			92.90	88.523	88.066	4.38	93.90	87.893	87.436	6.01
MSS-A-6		MA6	MA5	610	0.292	0.114			93.90	87.833	87.223	6.07	93.50	87.359	86.749	6.14
MSS-A-5		MA5	M27A	610	0.292	0.152			93.50	87.299	86.689	6.20	93.00	87.079	86.469	5.92
MSS-A-4		M27A	MH5200A	610	0.292	0.152			93.00	87.019	86.409	5.98	93.00	86.267	85.657	6.73
		MH5200A		610	0.292	0.152			93.00	86.231	85.621	6.77	93.80	86.194	85.584	7.61
		MH520A	MH521A	610	0.292	0.152			93.70	86.155	85.545	7.55	93.80	86.111	85.501	7.69
N-1		MH521A		610	0.292	0.152			93.80	86.078	85.468	7.72	92.60	86.033	85.423	6.57
		MH522A	MH435A	610	0.292	0.152			92.60	86.005	85.395	6.60	92.60	85.982	85.372	6.62
		MH435A	MH501A	914	0.656	0.228			92.60	85.982	85.068	6.62	92.60	85.967	85.053	6.63





Estimated Peak Stormwater Flow Rate City of Ottawa Sewer Design Guidelines, 2012



# **Existing Drainage Charateristics From Internal Site**

Area	2.21 ha
С	0.39 Rational Method runoff coefficient
L	152 m
Up Elev	94.71 m
Dn Elev	93.62 m
Slope	0.7 %
Tc	31.9 min

1) Time of Concentration per Federal Aviation Administration

$$t_c = \frac{1.8(1.1 - C)L^{0.5}}{S^{0.333}}$$

tc, in minutes

C, rational method coefficient, (-)

L, length in ft

S, average watershed slope in %

# **Estimated Peak Flow**

	2-year	5-year	100-year
i	76.8	104.2	178.6 mm/hr
Q	183.9	249.5	534.4 L/s

# Note:

C value for the 100-year storm is increased by 25%, to a maximum of 1.0 per Ottawa Sewer Design Guidelines (5.4.5.2.1)

**Stormwater - Proposed Development** City of Ottawa Sewer Design Guidelines, 2012



# **Target Flow Rate**

Area 2.21 ha

С 0.64 Rational Method runoff coefficient

21.5 min

5-year 67.1 mm/hr Q 263.4 L/s

# **Estimated Post Development Peak Flow from Unattenuated Areas**

С

Area ID **Total Area**  U1

0.071 ha

0.30 Rational Method runoff coefficient

		5-year					100-year				
	t <sub>c</sub> (min)	i (mm/hr)	Q <sub>actual</sub> (L/s)	Q <sub>release</sub> (L/s)	Q <sub>stored</sub> (L/s)	V <sub>stored</sub> (m <sup>3</sup> )	i (mm/hr)	Q <sub>actual</sub> * (L/s)	Q <sub>release</sub> (L/s)	Q <sub>stored</sub> (L/s)	V <sub>stored</sub> (m <sup>3</sup> )
ĺ	16.2	79.9	4.7	4.7	0.0	0.0	136.6	10.1	10.1	0.0	0.0

C value for the 100-year storm is increased by 25%, to a maximum of 1.0 per Ottawa Sewer Design Guidelines (5.4.5.2.1)

Area ID U2

Total Area

0.057 ha

0.90 Rational Method runoff coefficient

	5-Year					100-year				
t <sub>c</sub> (min)	i (mm/hr)	Q <sub>actual</sub> (L/s)	Q <sub>release</sub> (L/s)	Q <sub>stored</sub> (L/s)	V <sub>stored</sub> (m <sup>3</sup> )	i (mm/hr)	Q <sub>actual</sub> (L/s)	Q <sub>release</sub> (L/s)	Q <sub>stored</sub> (L/s)	V <sub>stored</sub> (m <sup>3</sup> )
16.2	79.9	11.4	11.4	0.0	0.0	136.6	21.6	21.6	0.0	0.0

5-Year Qattenuated 11.39 L/s 100-year Qattenuated 21.63 L/s 0.0 m<sup>3</sup> 0.0 m<sup>3</sup> 5-Year Max. Storage Required 100-year Max. Storage Required

U3 Area ID

Total Area

0.122 ha

0.50 Rational Method runoff coefficient Note: Rational Method Coefficient "C" increased by 25% for 100-year calculations

	5-Year					100-year				
t <sub>c</sub>	i	Q <sub>actual</sub>	Q <sub>release</sub>	Q <sub>stored</sub>	$V_{\text{stored}}$	i	Q <sub>actual</sub>	$\mathbf{Q}_{release}$	<b>Q</b> <sub>stored</sub>	$V_{\text{stored}}$
(min)	(mm/hr)	(L/s)	(L/s)	(L/s)	(m <sup>3</sup> )	(mm/hr)	(L/s)	(L/s)	(L/s)	(m <sup>3</sup> )
16.2	79.9	13.5	13.5	0.0	0.0	136.6	28.9	28.9	0.0	0.0

100-year Qattenuated 13.54 L/s 5-Year Qattenuated 28.93 L/s 5-Year Max. Storage Required  $0.0 \text{ m}^3$ 100-year Max. Storage Required  $0.0 \text{ m}^3$ 

Area ID U4

**Total Area** 

0.015 ha

0.20 Rational Method runoff coefficient Note: Rational Method Coefficient "C" increased by 25% for 100-year calculations

			5-Year					100-year				
ſ	t <sub>c</sub> (min)		i (mm/hr)	Q <sub>actual</sub> (L/s)	Q <sub>release</sub> (L/s)	Q <sub>stored</sub> (L/s)	V <sub>stored</sub> (m <sup>3</sup> )	i (mm/hr)	Q <sub>actual</sub> (L/s)	Q <sub>release</sub> (L/s)	Q <sub>stored</sub> (L/s)	V <sub>stored</sub> (m <sup>3</sup> )
t	` 1	6.2	79.9	0.7	0.7	0.0	0.0	, ,	1.4	1.4	0.0	0.0

0.67 L/s 1.42 L/s 5-Year Qattenuated 100-year Qattenuated  $0.0 \text{ m}^3$ 100-year Max. Storage Required  $0.0 \, \text{m}^3$ 5-Year Max. Storage Required

Area ID U5

**Total Area** 

0.028 ha

0.40 Rational Method runoff coefficient Note: Rational Method Coefficient "C" increased by 25% for 100-year calculations

	5-Year					100-year					
t <sub>c</sub>	i	<b>Q</b> actual	Q <sub>release</sub>	Q <sub>stored</sub>	V <sub>stored</sub>	i	Q <sub>actual</sub>	<b>Q</b> <sub>release</sub>	Q <sub>stored</sub>	V <sub>stored</sub>	
(min)	(mm/hr)	(L/s)	(L/s)	(L/s)	(m³)	(mm/hr)	(L/s)	(L/s)	(L/s)	(m <sup>3</sup> )	
16.2	79.9	2.5	2.5	0.0	0.0	136.6	5.3	5.3	0.0	0.0	

100-year Qattenuated 5-Year Qattenuated 2.49 L/s 5.31 L/s 0.0 m<sup>3</sup> 0.0 m<sup>3</sup> 5-Year Max. Storage Required 100-year Max. Storage Required

# **Estimated Post Development Peak Flow from Attenuated Areas**

Building IDMETRORoof Area0.401 haAvail Storage Area0.381

C 0.90 Rational Method runoff coefficient Note: Rational Method Coefficient "C" increased by 25% for 100-year calculations

10 min, tc at outlet without restriction

Estimated Number of Roof Drains
Building Length 69
Building Width 55.6
Number of Drains 21

m<sup>2</sup> / Drain 181.4 max 232.25m<sup>2</sup>/notch as recommended by Zurn for Ottawa

Roof Top Rating Curve per Zurn Model Z-105-5												
d	Α	V <sub>acc</sub>	V <sub>avail</sub>	Q <sub>notch</sub>	$Q_{roof}$	V <sub>drawdown</sub>						
(m)	(m²)	(m <sup>3</sup> )	(m <sup>3</sup> )	(L/s)	(L/s)	(hr)						
0.000	0	0.0	0.0	0.00	0.00	0.00						
0.025	238.1	2.0	2.0	0.38	7.98	0.07						
0.050	952.4	13.9	15.9	0.77	16.17	0.31						
0.075	2142.8	37.7	53.6	1.14	23.94	0.75						
0.100	3809.5	73.4	127.0	1.52	31.92	1.38						
0.125	3809.5	95.2	222.2	1.90	39.90	2.05						
0.150	3809.5	95.2	317.5	2.28	47.88	2.60						

<sup>\*</sup> Assumes one notch opening per drain, assumes maximum slope of 10cm

	5-year					100-year				
t <sub>c</sub>	i	Q <sub>actual</sub>	Q <sub>release</sub>	Q <sub>stored</sub>	V <sub>stored</sub>	i	Q <sub>actual</sub>	Q <sub>release</sub>	Q <sub>stored</sub>	V <sub>stored</sub>
(min)	(mm/hr)	(L/s)	(L/s)	(L/s)	(m³)	(mm/hr)	(L/s)	(L/s)	(L/s)	(m <sup>3</sup> )
10	104.2	104.5	24.2	80.3	48.2	178.6	198.9	31.9	167.0	100.2
15	83.6	83.8	24.2	59.6	53.7	142.9	159.2	31.9	127.3	114.5
20	70.3	70.4	24.2	46.3	55.5	120.0	133.6	31.9	101.7	122.1
25	60.9	61.0	24.2	36.9	55.3	103.8	115.7	31.9	83.8	125.7
30	53.9	54.1	24.2	29.9	53.8	91.9	102.3	31.9	70.4	126.8
35	48.5	48.6	24.2	24.5	51.4	82.6	92.0	31.9	60.1	126.2
40	44.2	44.3	24.2	20.1	48.3	75.1	83.7	31.9	51.8	124.3
45	40.6	40.7	24.2	16.6	44.8	69.1	76.9	31.9	45.0	121.5
50	37.7	37.7	24.2	13.6	40.8	64.0	71.2	31.9	39.3	118.0
55	35.1	35.2	24.2	11.1	36.5	59.6	66.4	31.9	34.5	113.9
60	32.9	33.0	24.2	8.9	31.9	55.9	62.3	31.9	30.4	109.3
65	31.0	31.1	24.2	7.0	27.2	52.6	58.6	31.9	26.7	104.3
70	29.4	29.4	24.2	5.3	22.2	49.8	55.5	31.9	23.6	99.0
75	27.9	28.0	24.2	3.8	17.1	47.3	52.6	31.9	20.7	93.3
80	26.6	26.6	24.2	2.5	11.9	45.0	50.1	31.9	18.2	87.4
85	25.4	25.4	24.2	1.3	6.5	43.0	47.8	31.9	15.9	81.3
90	24.3	24.3	24.2	0.2	1.1	41.1	45.8	31.9	13.9	75.0
95	23.3	23.4	23.4	0.0	0.0	39.4	43.9	31.9	12.0	68.6
100	22.4	22.5	22.5	0.0	0.0	37.9	42.2	31.9	10.3	61.9
105	21.6	21.6	21.6	0.0	0.0	36.5	40.7	31.9	8.8	55.2
110	20.8	20.9	20.9	0.0	0.0	35.2	39.2	31.9	7.3	48.3

 $\begin{array}{ccc} & & & 5\text{-year Q}_{\text{roof}} & 24.15 \text{ L/s} \\ & 5\text{-year Max. Storage Required} & 55.5 \text{ m}^3 \\ & & 5\text{-year Storage Depth} & 0.076 \text{ m} \\ & 5\text{-year Estimated Drawdown Time} & 0.76 \text{ hr} \end{array}$ 

100-year Q<sub>roof</sub> 31.90 L/s 100-year Max. Storage Required 126.8 m<sup>3</sup> 100-year Storage Depth 0.100 m 00-year Estimated Drawdown Time 1.38 hr Building ID BLDG A
Roof Area 0.093 ha
Avail Storage Area 0.088

C 0.90 Rational Method runoff coefficient Note: Rational Method Coefficient "C" increased by 25% for 100-year calculations

10 min, tc at outlet without restriction

Estimated Number of Roof Drains
Building Length 33
Building Width 26
Number of Drains 7

m<sup>2</sup> / Drain 126.2 max 232.25m<sup>2</sup>/notch as recommended by Zurn for Ottawa

Deaf Tan Dation Owner and Town Madel 7 405 5												
	Roof Top Rating Curve per Zurn Model Z-105-5											
d	Α	$V_{acc}$	$V_{avail}$	$\mathbf{Q}_{notch}$	$\mathbf{Q}_{roof}$	$V_{drawdown}$						
(m)	(m²)	(m <sup>3</sup> )	(m <sup>3</sup> )	(L/s)	(L/s)	(hr)						
0.000	0	0.0	0.0	0.00	0.00	0.00						
0.025	55.2	0.5	0.5	0.38	2.66	0.05						
0.050	220.9	3.2	3.7	0.77	5.39	0.21						
0.075	497.0	8.7	12.4	1.14	7.98	0.52						
0.100	883.5	17.0	29.5	1.52	10.64	0.96						
0.125	883.5	22.1	51.5	1.90	13.30	1.42						
0.150	883.5	22.1	73.6	2.28	15.96	1.81						

<sup>\*</sup> Assumes one notch opening per drain, assumes maximum slope of 10cm

	5-year					100-year				
t <sub>c</sub> (min)	i (mm/hr)	Q <sub>actual</sub> (L/s)	Q <sub>release</sub> (L/s)	Q <sub>stored</sub> (L/s)	V <sub>stored</sub> (m <sup>3</sup> )	i (mm/hr)	Q <sub>actual</sub> (L/s)	Q <sub>release</sub> (L/s)	Q <sub>stored</sub> (L/s)	V <sub>stored</sub> (m <sup>3</sup> )
10	104.2	24.2	7.5	16.7	10.0	178.6	46.1	10.0	36.1	21.7
15	83.6	19.4	7.5	11.9	10.7	142.9	36.9	10.0	26.9	24.2
20	70.3	16.3	7.5	8.8	10.6	120.0	31.0	10.0	21.0	25.2
25	60.9	14.2	7.5	6.7	10.0	103.8	26.8	10.0	16.8	25.3
30	53.9	12.5	7.5	5.1	9.1	91.9	23.7	10.0	13.7	24.7
35	48.5	11.3	7.5	3.8	8.0	82.6	21.3	10.0	11.3	23.8
40	44.2	10.3	7.5	2.8	6.7	75.1	19.4	10.0	9.4	22.6
45	40.6	9.4	7.5	2.0	5.3	69.1	17.8	10.0	7.9	21.2
50	37.7	8.8	7.5	1.3	3.8	64.0	16.5	10.0	6.5	19.6
55	35.1	8.2	7.5	0.7	2.3	59.6	15.4	10.0	5.4	17.9
60	32.9	7.7	7.5	0.2	0.6	55.9	14.4	10.0	4.5	16.0
65	31.0	7.2	7.2	0.0	0.0	52.6	13.6	10.0	3.6	14.1
70	29.4	6.8	6.8	0.0	0.0	49.8	12.9	10.0	2.9	12.1
75	27.9	6.5	6.5	0.0	0.0	47.3	12.2	10.0	2.2	10.0
80	26.6	6.2	6.2	0.0	0.0	45.0	11.6	10.0	1.6	7.9
85	25.4	5.9	5.9	0.0	0.0	43.0	11.1	10.0	1.1	5.7
90	24.3	5.6	5.6	0.0	0.0	41.1	10.6	10.0	0.6	3.4
95	23.3	5.4	5.4	0.0	0.0	39.4	10.2	10.0	0.2	1.1
100	22.4	5.2	5.2	0.0	0.0	37.9	9.8	9.8	0.0	0.0
105	21.6	5.0	5.0	0.0	0.0	36.5	9.4	9.4	0.0	0.0
110	20.8	4.8	4.8	0.0	0.0	35.2	9.1	9.1	0.0	0.0

5-year Q<sub>roof</sub>
7.48 L/s
5-year Max. Storage Required
5-year Storage Depth
5-year Estimated Drawdown Time
7.48 L/s
0.070 m

100-year Q<sub>roof</sub> 9.99 L/s 100-year Max. Storage Required 25.3 m<sup>3</sup> 100-year Storage Depth 0.094 m 00-year Estimated Drawdown Time 0.85 hr Building ID BLDG B
Roof Area 0.083 ha
Avail Storage Area 0.079

C 0.90 Rational Method runoff coefficient Note: Rational Method Coefficient "C" increased by 25% for 100-year calculations

10 min, tc at outlet without restriction

Estimated Number of Roof Drains
Building Length 34
Building Width 23
Number of Drains 7

m<sup>2</sup> / Drain 112.6 max 232.25m<sup>2</sup>/notch as recommended by Zurn for Ottawa

Roof Top Rating Curve per Zurn Model Z-105-5												
d	Α	V <sub>acc</sub>	V <sub>avail</sub>	Q <sub>notch</sub>	$Q_{roof}$	$V_{drawdown}$						
(m)	(m²)	(m <sup>3</sup> )	(m <sup>3</sup> )	(L/s)	(L/s)	(hr)						
0.000	0	0.0	0.0	0.00	0.00	0.00						
0.025	49.3	0.4	0.4	0.38	2.66	0.04						
0.050	197.1	2.9	3.3	0.77	5.39	0.19						
0.075	443.5	7.8	11.1	1.14	7.98	0.46						
0.100	788.5	15.2	26.3	1.52	10.64	0.86						
0.125	788.5	19.7	46.0	1.90	13.30	1.27						
0.150	788.5	19.7	65.7	2.28	15.96	1.61						

\* Assumes one notch opening per drain, assumes maximum slope of 10cm

	5-year					100-year				
t <sub>c</sub> (min)	i (mm/hr)	Q <sub>actual</sub> (L/s)	Q <sub>release</sub> (L/s)	Q <sub>stored</sub> (L/s)	V <sub>stored</sub> (m <sup>3</sup> )	i (mm/hr)	Q <sub>actual</sub> (L/s)	Q <sub>release</sub> (L/s)	Q <sub>stored</sub> (L/s)	V <sub>stored</sub> (m <sup>3</sup> )
10	104.2	21.6	7.3	14.3	8.6	178.6	41.2	9.8	31.4	18.8
15	83.6	17.3	7.3	10.0	9.0	142.9	32.9	9.8	23.2	20.8
20	70.3	14.6	7.3	7.3	8.7	120.0	27.7	9.8	17.9	21.4
25	60.9	12.6	7.3	5.3	8.0	103.8	23.9	9.8	14.2	21.2
30	53.9	11.2	7.3	3.9	7.0	91.9	21.2	9.8	11.4	20.5
35	48.5	10.1	7.3	2.8	5.8	82.6	19.0	9.8	9.2	19.4
40	44.2	9.2	7.3	1.9	4.5	75.1	17.3	9.8	7.5	18.1
45	40.6	8.4	7.3	1.1	3.1	69.1	15.9	9.8	6.1	16.5
50	37.7	7.8	7.3	0.5	1.5	64.0	14.7	9.8	5.0	14.9
55	35.1	7.3	7.3	0.0	0.0	59.6	13.7	9.8	4.0	13.1
60	32.9	6.8	6.8	0.0	0.0	55.9	12.9	9.8	3.1	11.1
65	31.0	6.4	6.4	0.0	0.0	52.6	12.1	9.8	2.3	9.2
70	29.4	6.1	6.1	0.0	0.0	49.8	11.5	9.8	1.7	7.1
75		5.8	5.8	0.0	0.0	47.3	10.9	9.8	1.1	5.0
80	26.6	5.5	5.5	0.0	0.0	45.0	10.4	9.8	0.6	2.8
85	25.4	5.3	5.3	0.0	0.0	43.0	9.9	9.8	0.1	0.6
90	24.3	5.0	5.0	0.0	0.0	41.1	9.5	9.5	0.0	0.0
95	23.3	4.8	4.8	0.0	0.0	39.4	9.1	9.1	0.0	0.0
100	22.4	4.6	4.6	0.0	0.0	37.9	8.7	8.7	0.0	0.0
105	21.6	4.5	4.5	0.0	0.0	36.5	8.4	8.4	0.0	0.0
110	20.8	4.3	4.3	0.0	0.0	35.2	8.1	8.1	0.0	0.0

5-year Q<sub>roof</sub>
7.30 L/s
5-year Max. Storage Required
5-year Storage Depth
5-year Estimated Drawdown Time
7.30 L/s
9.0 m<sup>3</sup>
0.068 m
0.39 hr

100-year Q<sub>roof</sub> 9.79 L/s 100-year Max. Storage Required 21.4 m<sup>3</sup> 100-year Storage Depth 0.092 m 00-year Estimated Drawdown Time 0.73 hr 2021-04-06

Building ID BLDG C
Roof Area 0.055 ha
Avail Storage Area 0.052

C 0.90 Rational Method runoff coefficient Note: Rational Method Coefficient "C" increased by 25% for 100-year calculations

10 min, tc at outlet without restriction

Estimated Number of Roof Drains
Building Length 29
Building Width 19
Number of Drains 5

m<sup>2</sup> / Drain 104.5 max 232.25m<sup>2</sup>/notch as recommended by Zurn for Ottawa

Roof Top Rating Curve per Zurn Model Z-105-5											
d	A	V <sub>acc</sub>	V <sub>avail</sub>	Q <sub>notch</sub>	Q <sub>roof</sub>	V <sub>drawdown</sub>					
(m)	(m²)	(m <sup>3</sup> )	(m <sup>3</sup> )	(L/s)	(L/s)	(hr)					
0.000	0	0.0	0.0	0.00	0.00	0.00					
0.025	32.7	0.3	0.3	0.38	1.90	0.04					
0.050	130.6	1.9	2.2	0.77	3.85	0.18					
0.075	293.9	5.2	7.3	1.14	5.70	0.43					
0.100	522.5	10.1	17.4	1.52	7.60	0.80					
0.125	522.5	13.1	30.5	1.90	9.50	1.18					
0.150	522.5	13.1	43.5	2.28	11.40	1.50					

<sup>\*</sup> Assumes one notch opening per drain, assumes maximum slope of 10cm

	5-year					100-year				
t <sub>c</sub> (min)	i (mm/hr)	Q <sub>actual</sub> (L/s)	Q <sub>release</sub> (L/s)	Q <sub>stored</sub> (L/s)	V <sub>stored</sub> (m <sup>3</sup> )	i (mm/hr)	Q <sub>actual</sub> (L/s)	Q <sub>release</sub> (L/s)	Q <sub>stored</sub> (L/s)	V <sub>stored</sub> (m <sup>3</sup> )
10	104.2	14.3	5.1	9.2	5.5	178.6	27.3	6.9	20.4	12.2
15	83.6	11.5	5.1	6.4	5.7	142.9	21.8	6.9	14.9	13.4
20	70.3	9.7	5.1	4.5	5.4	120.0	18.3	6.9	11.4	13.7
25	60.9	8.4	5.1	3.3	4.9	103.8	15.9	6.9	9.0	13.4
30	53.9	7.4	5.1	2.3	4.1	91.9	14.0	6.9	7.1	12.8
35	48.5	6.7	5.1	1.5	3.3	82.6	12.6	6.9	5.7	12.0
40	44.2	6.1	5.1	1.0	2.3	75.1	11.5	6.9	4.6	11.0
45	40.6	5.6	5.1	0.5	1.3	69.1	10.5	6.9	3.6	9.9
50	37.7	5.2	5.1	0.1	0.2	64.0	9.8	6.9	2.9	8.6
55	35.1	4.8	4.8	0.0	0.0	59.6	9.1	6.9	2.2	7.3
60	32.9	4.5	4.5	0.0	0.0	55.9	8.5	6.9	1.6	5.9
65	31.0	4.3	4.3	0.0	0.0	52.6	8.0	6.9	1.1	4.5
70	29.4	4.0	4.0	0.0	0.0	49.8	7.6	6.9	0.7	3.0
75	27.9	3.8	3.8	0.0	0.0	47.3	7.2	6.9	0.3	1.4
80	26.6	3.7	3.7	0.0	0.0	45.0	6.9	6.9	0.0	0.0
85	25.4	3.5	3.5	0.0	0.0	43.0	6.6	6.6	0.0	0.0
90	24.3	3.3	3.3	0.0	0.0	41.1	6.3	6.3	0.0	0.0
95	23.3	3.2	3.2	0.0	0.0	39.4	6.0	6.0	0.0	0.0
100	22.4	3.1	3.1	0.0	0.0	37.9	5.8	5.8	0.0	0.0
105	21.6	3.0	3.0	0.0	0.0	36.5	5.6	5.6	0.0	0.0
110	20.8	2.9	2.9	0.0	0.0	35.2	5.4	5.4	0.0	0.0

5-year Q<sub>roof</sub>
5-12 L/s
5-year Max. Storage Required
5-year Storage Depth
5-year Estimated Drawdown Time
5.12 L/s
0.067 m
0.35 hr

100-year Q<sub>roof</sub> 6.90 L/s 100-year Max. Storage Required 13.7 m<sup>3</sup> 100-year Storage Depth 0.091 m 00-year Estimated Drawdown Time 0.66 hr **Proposed Conditions** 

Area ID A109 Available Sub-surface Storage

Total Subsurface Storage (m<sup>3</sup>) 0.0

**Stage Attenuated Areas Storage Summary** 

-			Surface	Storage		Surface and Subsurface Storage				
	Stage	Ponding	100-Year HGL	Head (Stage to 100-year HGL)	delta d	V*	V <sub>acc</sub> **	Q <sub>release</sub> †	V <sub>drawdown</sub>	
	(m)	$(m^2)$	(m)	(m)	(m)	(m <sup>3</sup> )	(m³)	(L/s)	(hr)	
Orifice INV	91.29	·					0.0	0.0	0.00	
TG	93.55	0.4	93.09	0.46	0.46	0.2	0.2	22.6	0.00	
0.10m ponding	93.65	43.8	93.09	0.56	0.10	1.6	1.8	24.9	0.02	
Max Ponding	93.69	78.0	93.09	0.60	0.04	2.4	4.2	25.8	0.05	

<sup>\*</sup> V=Incremental storage volume

125

Orifice Location Total Area STM109

Dia

0.103 ha

0.50 Rational Method runoff coefficient

Note: Rational Method Coefficient "C" increased by 25% for 100-year calculations

	5-Year					100-year				
t <sub>c</sub>	i	Q <sub>actual</sub>	Q <sub>release</sub>	$\mathbf{Q}_{stored}$	V <sub>stored</sub>	i	Q <sub>actual</sub>	Q <sub>release</sub>	Q <sub>stored</sub>	V <sub>stored</sub>
(min)	(mm/hr)	(L/s)	(L/s)	(L/s)	(m <sup>3</sup> )	(mm/hr)	(L/s)	(L/s)	(L/s)	(m³)
10	104.2	14.9	9.6	5.3	3.2	178.6	31.9	25.6	6.3	3.8
20	70.3	10.0	9.6	0.4	0.5		21.4	21.4	0.0	0.0
30	53.9	7.7	7.7	0.0	0.0	91.9	16.4	21.4	0.0	0.0
40	44.2	6.3	6.3	0.0		75.1	13.4	21.4	0.0	0.0
50	37.7	5.4	5.4	0.0	0.0	64.0	11.4	21.4	0.0	0.0
60	32.9	4.7	4.7	0.0	0.0	55.9	10.0	21.4	0.0	0.0
70	29.4	4.2	4.2	0.0	0.0	49.8	8.9	21.4	0.0	0.0
80	26.6	3.8	3.8	0.0	0.0	45.0	8.0	21.4	0.0	0.0
90	24.3	3.5	3.5	0.0	0.0	41.1	7.4	21.4	0.0	0.0
100	22.4	3.2	3.2	0.0	0.0	37.9	6.8	21.4	0.0	0.0
110		3.0	3.0	0.0		35.2	6.3	21.4	0.0	0.0
120	19.5	2.8	2.8	0.0	0.0	32.9	5.9	21.4	0.0	0.0
130		2.6	2.6	0.0	0.0	30.9	5.5	21.4	0.0	0.0
140	17.3	2.5	2.5	0.0	0.0	29.2	5.2	21.4	0.0	0.0
150		2.3	2.3	0.0		27.6	4.9	21.4	0.0	0.0
160	15.6	2.2	2.2	0.0	0.0	26.2	4.7	21.4	0.0	0.0
170		2.1	2.1	0.0	0.0	25.0	4.5	21.4	0.0	0.0
180	14.2	2.0	2.0	0.0	0.0	23.9	4.3	21.4	0.0	0.0
190		1.9	1.9	0.0		22.9	4.1	21.4	0.0	0.0
200	13.0	1.9	1.9	0.0	0.0	22.0	3.9	21.4	0.0	0.0
210	12.6	1.8	1.8	0.0	0.0	21.1	3.8	21.4	0.0	0.0
220	12.1	1.7	1.7	0.0	0.0	20.4	3.6	21.4	0.0	0.0
230		1.7	1.7	0.0	0.0	19.7	3.5	21.4	0.0	0.0
240		1.6	1.6	0.0	0.0	19.0	3.4	21.4	0.0	0.0
250		1.6	1.6	0.0	0.0	18.4	3.3	21.4	0.0	0.0
260	10.6	1.5	1.5	0.0	0.0	17.8	3.2	21.4	0.0	0.0

5-Year Qattenuated 5-Year Max. Storage Required Est. 5-Year Storage Elevation 9.60 L/s 3.2 m<sup>3</sup> 93.67 m 100-year Q<sub>attenuated</sub> 100-year Max. Storage Required Est. 100-year Storage Elevation 25.63 L/s 3.8 m<sup>3</sup> 93.68 m

<sup>\*\*</sup> $V_{acc}$ =Total surface and sub-surface

 $<sup>\</sup>dagger$  Q<sub>release</sub> = Release rate calculated from orifice equation

**Proposed Conditions** 

Area ID A110B Available Sub-surface Storage

Total Subsurface Storage (m<sup>3</sup>) 0.0

Stage Attenuated Areas Storage Summary

itteriaatea Areas Storage Sar	u. y								
			Surface	Storage		Surfa	ce and Sub	surface Sto	rage
	Stage	Ponding	100-Year HGL	Head (Stage to 100-year HGL)	delta d	V*	V <sub>acc</sub> **	Q <sub>release</sub> †	V <sub>drawdown</sub>
	(m)	(m²)	(m)	(m)	(m)	(m <sup>3</sup> )	(m <sup>3</sup> )	(L/s)	(hr)
Orifice INV	92.05						0.0	0.0	0.00
TG	93.55	0.36	93.09	0.46	0.46	0.2	0.2	9.3	0.01
Max Ponding	93.85	416	93.09	0.76	0.30	42.9	43.0	11.9	1.01

<sup>\*</sup> V=Incremental storage volume

80

Orifice Location Total Area **CB110B** 0.060 ha

**Dia** 

0.80 Rational Method runoff coefficient

Note: Rational Method Coefficient "C" increased by 25% for 100-year calculations

	5-Year					100-year				
t <sub>c</sub>	i	Q <sub>actual</sub>	Q <sub>release</sub>	Q <sub>stored</sub>	V <sub>stored</sub>	i	Q <sub>actual</sub>	Q <sub>release</sub>	Q <sub>stored</sub>	V <sub>stored</sub>
(min)	(mm/hr)	(L/s)	(L/s)	(L/s)	(m <sup>3</sup> )	(mm/hr)	(L/s)	(L/s)	(L/s)	V <sub>stored</sub> (m³)
10	104.2	13.9	9.4	4.5	2.7	178.6	29.8	10.0	19.8	11.9
20	70.3	9.4	9.4	0.0	0.0	120.0	20.0	10.0	10.0	12.0
30	53.9	7.2	7.2	0.0	0.0	91.9	15.3	10.0	5.3	9.6
40	44.2	5.9	5.9	0.0	0.0	75.1	12.5	10.0	2.5	6.1
50	37.7	5.0	5.0	0.0	0.0	64.0	10.7	10.0	0.7	2.0
60	32.9	4.4	4.4	0.0	0.0	55.9	9.3	10.0	0.0	0.0
70	29.4	3.9	3.9	0.0	0.0	49.8	8.3	10.0	0.0	0.0
80	26.6	3.5	3.5	0.0	0.0	45.0	7.5	10.0	0.0	0.0
90	24.3	3.2	3.2	0.0	0.0	41.1	6.9	10.0	0.0	0.0
100		3.0	3.0	0.0		37.9	6.3	10.0	0.0	0.0
110	20.8	2.8	2.8	0.0		35.2	5.9	10.0	0.0	0.0
120		2.6	2.6	0.0	0.0	32.9	5.5	10.0	0.0	0.0
130	18.3	2.4	2.4	0.0	0.0	30.9	5.1	10.0	0.0	0.0
140	17.3	2.3	2.3	0.0	0.0	29.2	4.9	10.0	0.0	0.0
150	16.4	2.2	2.2	0.0	0.0	27.6	4.6	10.0	0.0	0.0
160		2.1	2.1	0.0	0.0	26.2	4.4	10.0	0.0	0.0
170		2.0	2.0	0.0	0.0	25.0	4.2	10.0	0.0	0.0
180		1.9	1.9	0.0	0.0	23.9	4.0	10.0	0.0	0.0
190	13.6	1.8	1.8	0.0	0.0	22.9	3.8	10.0	0.0	0.0
200	13.0	1.7	1.7	0.0	0.0	22.0	3.7	10.0	0.0	0.0
210	12.6	1.7	1.7	0.0	0.0	21.1	3.5	10.0	0.0	0.0
220	12.1	1.6	1.6	0.0	0.0	20.4	3.4	10.0	0.0	0.0
230		1.6	1.6	0.0	0.0	19.7	3.3	10.0	0.0	0.0
240	11.3	1.5	1.5	0.0	0.0	19.0	3.2	10.0	0.0	0.0
250	10.9	1.5	1.5	0.0	0.0	18.4	3.1	10.0	0.0	0.0
260	10.6	1.4	1.4	0.0	0.0	17.8	3.0	10.0	0.0	0.0

5-Year Qattenuated 5-Year Max. Storage Required Est. 5-Year Storage Elevation 9.41 L/s 2.7 m<sup>3</sup> 93.57 m 100-year Q<sub>attenuated</sub> 100-year Max. Storage Required Est. 100-year Storage Elevation 9.98 L/s

12.0 m<sup>3</sup>

93.63 m

<sup>\*\*</sup>V<sub>acc</sub>=Total surface and sub-surface

 $<sup>\</sup>dagger$  Q<sub>release</sub> = Release rate calculated from orifice equation

**Proposed Conditions** 

Area ID A110A Available Sub-surface Storage

> Total Subsurface Storage (m<sup>3</sup>) 0.0

**Stage Attenuated Areas Storage Summary** 

-	ĺ		Surface	Storage		Surfa	ace and Sub	surface Stor	rage
	Stage	Ponding	100-Year HGL	Head (Stage to 100-year HGL)	delta d	V*	V <sub>acc</sub> **	Q <sub>release</sub> †	V <sub>drawdown</sub>
	(m)	(m²)	(m)	(m)	(m)	(m <sup>3</sup> )	(m³)	(L/s)	(hr)
Orifice INV	92.05						0.0	0.0	0.00
TG	93.55	0.36	93.09	0.46	0.46	0.2	0.2	9.3	0.01
Max Ponding	93.85	531	93.09	0.76	0.30	54.5	54.7	11.9	1.28

<sup>\*</sup> V=Incremental storage volume

80

Orifice Location **Total Area** 

CB110A

Dia

0.094 ha

0.80 Rational Method runoff coefficient

Note: Rational Method Coefficient "C" increased by 25% for 100-year calculations

	5-Year					100-year				
t <sub>c</sub>	i	Q <sub>actual</sub>	Q <sub>release</sub>	Q <sub>stored</sub>	V <sub>stored</sub>	i	Q <sub>actual</sub>	Q <sub>release</sub>	Q <sub>stored</sub>	V <sub>stored</sub>
(min)	(mm/hr)	(L/s)	(L/s)	(L/s)	(m <sup>3</sup> )	(mm/hr)	(L/s)	(L/s)	(L/s)	V <sub>stored</sub> (m³)
10	104.2	21.8	9.6	12.2	7.3	178.6	46.6	10.4	36.2	21.7
20	70.3	14.7	9.6	5.1	6.1	120.0	31.3	10.4	20.9	25.0
30	53.9	11.3	9.6	1.7	3.0	91.9	24.0	10.4	13.5	24.4
40	44.2	9.2	9.2	0.0	0.0	75.1	19.6	10.4	9.2	22.0
50	37.7	7.9	7.9	0.0	0.0	64.0	16.7	10.4	6.3	18.8
60	32.9	6.9	6.9	0.0	0.0	55.9	14.6	10.4	4.1	14.9
70	29.4	6.1	6.1	0.0	0.0	49.8	13.0	10.4	2.6	10.7
80	26.6	5.5	5.5	0.0	0.0	45.0	11.7	10.4	1.3	6.2
90	24.3	5.1	5.1	0.0	0.0	41.1	10.7	10.4	0.3	1.6
100		4.7	4.7	0.0		37.9	9.9	10.4	0.0	0.0
110	20.8	4.3	4.3	0.0		35.2	9.2	10.4	0.0	0.0
120		4.1	4.1	0.0	0.0	32.9	8.6	10.4	0.0	0.0
130	18.3	3.8	3.8	0.0	0.0	30.9	8.1	10.4	0.0	0.0
140	17.3	3.6	3.6	0.0	0.0	29.2	7.6	10.4	0.0	0.0
150	16.4	3.4	3.4	0.0	0.0	27.6	7.2	10.4	0.0	0.0
160		3.2	3.2	0.0	0.0	26.2	6.9	10.4	0.0	0.0
170		3.1	3.1	0.0	0.0	25.0	6.5	10.4	0.0	0.0
180		3.0	3.0	0.0	0.0	23.9	6.2	10.4	0.0	0.0
190	13.6	2.8	2.8	0.0	0.0	22.9	6.0	10.4	0.0	0.0
200	13.0	2.7	2.7	0.0	0.0	22.0	5.7	10.4	0.0	0.0
210	12.6	2.6	2.6	0.0	0.0	21.1	5.5	10.4	0.0	0.0
220	12.1	2.5	2.5	0.0	0.0	20.4	5.3	10.4	0.0	0.0
230	11.7	2.4	2.4	0.0	0.0	19.7	5.1	10.4	0.0	0.0
240	11.3	2.4	2.4	0.0	0.0	19.0	5.0	10.4	0.0	0.0
250	10.9	2.3	2.3	0.0	0.0	18.4	4.8	10.4	0.0	0.0
260	10.6	2.2	2.2	0.0	0.0	17.8	4.7	10.4	0.0	0.0

5-Year Qattenuated 5-Year Max. Storage Required Est. 5-Year Storage Elevation

9.59 L/s 7.3 m<sup>3</sup> 93.59 m

100-year Q<sub>attenuated</sub> 100-year Max. Storage Required Est. 100-year Storage Elevation

10.45 L/s 25.0 m<sup>3</sup> 93.69 m

<sup>\*\*</sup> $V_{acc}$ =Total surface and sub-surface

 $<sup>\</sup>dagger$  Q<sub>release</sub> = Release rate calculated from orifice equation

Area ID A106 & A107 Available Sub-surface Storage

Total Subsurface Storage (m<sup>3</sup>) 0.0

Stage Attenuated Areas Storage Summary

			Surface	Storage		Surfa	ce and Sub	surface Sto	rage
	Stage	Ponding	100-Year HGL	Head (Stage to 100-year HGL)	delta d	V*	V <sub>acc</sub> **	Q <sub>release</sub> †	V <sub>drawdown</sub>
	(m)	(m²)	(m)	(m)	(m)	(m <sup>3</sup> )	(m <sup>3</sup> )	(L/s)	(hr)
Orifice INV	91.37						0.0	0.0	0.00
TG	93.50	1.4	93.09	0.41	0.41	0.6	0.6	19.6	0.01
0.15m Ponding	93.65	972.0	93.09	0.56	0.15	50.5	51.1	22.9	0.62
Max Ponding	93.80	2,037.0	93.09	0.71	0.15	220.8	271.9	25.8	2.93

<sup>\*</sup> V=Incremental storage volume

120

Orifice Location Total Area

CBMH106

Dia

0.455 ha

0.82 Rational Method runoff coefficient

Note: Rational Method Coefficient "C" increased by 25% for 100-year calculations

	5-Year					100-year				
t <sub>c</sub>	i	Q <sub>actual</sub>	Q <sub>release</sub>	$\mathbf{Q}_{stored}$	V <sub>stored</sub>	-	Q <sub>actual</sub>	Q <sub>release</sub>	Q <sub>stored</sub>	V <sub>stored</sub>
(min)	(mm/hr)	(L/s)	(L/s)	(L/s)	(m <sup>3</sup> )	(mm/hr)	(L/s)	(L/s)	(L/s)	(m³)
10	104.2	108.3	23.0	85.3	51.2	178.6	225.7	24.5	201.2	120.7
20	70.3	73.0		50.0	60.0	120.0	151.6	24.5	127.1	152.6
30	53.9	56.1	23.0	33.0	59.4	91.9	116.1	24.5	91.6	165.0
40	44.2	45.9	23.0	22.9			95.0	24.5	70.5	169.2
50	37.7	39.1	23.0	16.1	48.3	64.0	80.8	24.5	56.4	169.1
60	32.9	34.2	23.0	11.2		55.9	70.6	24.5	46.2	166.2
70	29.4	30.5	23.0	7.5	31.5		62.9	24.5	38.5	161.5
80	26.6	27.6	23.0	4.6		45.0	56.9	24.5	32.4	155.5
90	24.3	25.2	23.0	2.2	11.9	41.1	52.0	24.5	27.5	148.5
100	22.4	23.3	23.0	0.2	1.5		47.9	24.5	23.4	140.6
110	20.8	21.6	21.6	0.0	0.0	35.2	44.5	24.5	20.0	132.2
120	19.5	20.2	20.2	0.0	0.0	32.9	41.6	24.5	17.1	123.2
130	18.3	19.0	19.0	0.0	0.0	30.9	39.1	24.5	14.6	113.8
140	17.3	18.0	18.0	0.0	0.0	29.2	36.8	24.5	12.4	104.0
150	16.4	17.0	17.0	0.0		27.6	34.9	24.5	10.4	93.9
160	15.6	16.2	16.2	0.0	0.0	26.2	33.2	24.5	8.7	83.5
170	14.8	15.4	15.4	0.0	0.0	25.0	31.6	24.5	7.1	72.9
180	14.2	14.7	14.7	0.0	0.0	23.9	30.2	24.5	5.7	62.0
190	13.6	14.1	14.1	0.0		22.9	28.9	24.5	4.5	51.0
200	13.0	13.6	13.6	0.0	0.0	22.0	27.8	24.5	3.3	39.8
210	12.6	13.1	13.1	0.0	0.0	21.1	26.7	24.5	2.3	28.4
220	12.1	12.6	12.6	0.0	0.0	20.4	25.8	24.5	1.3	16.9
230	11.7	12.1	12.1	0.0	0.0	19.7	24.9	24.5	0.4	5.3
240	11.3	11.7	11.7	0.0	0.0	19.0	24.0	24.5	0.0	0.0
250	10.9	11.4	11.4	0.0	0.0	18.4	23.2	24.5	0.0	0.0
260	10.6	11.0	11.0	0.0	0.0	17.8	22.5	24.5	0.0	0.0

5-Year Qattenuated 5-Year Max. Storage Required Est. 5-Year Storage Elevation 23.04 L/s 60.0 m<sup>3</sup> 93.66 m

100-year Q<sub>attenuated</sub> 100-year Max. Storage Required Est. 100-year Storage Elevation 24.47 L/s 169.2 m<sup>3</sup> 93.73 m

<sup>\*\*</sup>V<sub>acc</sub>=Total surface and sub-surface

 $<sup>\</sup>dagger$  Q<sub>release</sub> = Release rate calculated from orifice equation

Area ID A114A Available Sub-surface Storage

Total Subsurface Storage (m<sup>3</sup>) 0.0

**Stage Attenuated Areas Storage Summary** 

-	-		Surface	Storage		Surface and Subsurface Storage				
	Stage	Ponding	100-Year HGL	Head (Stage to 100-year HGL)	delta d	V*	V <sub>acc</sub> **	Q <sub>release</sub> †	V <sub>drawdown</sub>	
	(m)	(m²)	(m)	(m)	(m)	(m³)	(m³)	(L/s)	(hr)	
Orifice INV	92.00						0.0	0.0	0.00	
TG	93.50	0.4	93.09	0.41	0.41	0.1	0.1	15.0	0.00	
Max Ponding	93.85	573.0	93.09	0.76	0.35	68.6	68.7	20.4	0.93	

<sup>\*</sup> V=Incremental storage volume

105

Orifice Location Total Area CB114A

Dia

0.157 ha
0.80 Rational Method runoff coefficient

Note: Rational Method Coefficient "C" increased by 25% for 100-year calculations

	5-Year					100-year				
t <sub>c</sub>	i	Q <sub>actual</sub>	Q <sub>release</sub>	Q <sub>stored</sub>	V <sub>stored</sub>	i	Q <sub>actual</sub>	Q <sub>release</sub>	Q <sub>stored</sub>	V <sub>stored</sub>
(min)	(mm/hr)	(L/s)	(L/s)	(L/s)	(m³)	(mm/hr)	(L/s)	(L/s)	(L/s)	(m³)
10	104.2	36.4	16.0	20.4	12.2	178.6	77.9	18.2	59.6	35.8
20	70.3	24.5	16.0	8.5	10.2	120.0	52.3	18.2	34.1	40.9
30	53.9	18.8	16.0	2.8	5.1	91.9	40.1	18.2	21.8	39.3
40	44.2	15.4	15.4	0.0	0.0	75.1	32.8	18.2	14.5	34.9
50	37.7	13.1	13.1	0.0	0.0	64.0	27.9	18.2	9.6	28.9
60	32.9	11.5	11.5	0.0	0.0	55.9	24.4	18.2	6.1	22.1
70	29.4	10.2	10.2	0.0	0.0	49.8	21.7	18.2	3.5	14.6
80	26.6	9.3	9.3	0.0	0.0	45.0	19.6	18.2	1.4	6.6
90	24.3	8.5	8.5	0.0	0.0	41.1	17.9	18.2	0.0	0.0
100	22.4	7.8	7.8	0.0	0.0	37.9	16.5	18.2	0.0	0.0
110	20.8	7.3	7.3	0.0	0.0	35.2	15.4	18.2	0.0	0.0
120	19.5	6.8	6.8	0.0	0.0	32.9	14.3	18.2	0.0	0.0
130	18.3	6.4	6.4	0.0	0.0	30.9	13.5	18.2	0.0	0.0
140	17.3	6.0	6.0	0.0	0.0	29.2	12.7	18.2	0.0	0.0
150	16.4	5.7	5.7	0.0	0.0	27.6	12.0	18.2	0.0	0.0
160	15.6	5.4	5.4	0.0	0.0	26.2	11.4	18.2	0.0	0.0
170	14.8	5.2	5.2	0.0	0.0	25.0	10.9	18.2	0.0	0.0
180	14.2	4.9	4.9	0.0	0.0	23.9	10.4	18.2	0.0	0.0
190	13.6	4.7	4.7	0.0	0.0	22.9	10.0	18.2	0.0	0.0
200	13.0	4.6	4.6	0.0	0.0	22.0	9.6	18.2	0.0	0.0
210	12.6	4.4	4.4	0.0	0.0	21.1	9.2	18.2	0.0	0.0
220	12.1	4.2	4.2	0.0	0.0	20.4	8.9	18.2	0.0	0.0
230	11.7	4.1	4.1	0.0	0.0	19.7	8.6	18.2	0.0	0.0
240	11.3	3.9	3.9	0.0	0.0	19.0	8.3	18.2	0.0	0.0
250	10.9	3.8	3.8	0.0	0.0	18.4	8.0	18.2	0.0	0.0
260	10.6	3.7	3.7	0.0	0.0	17.8	7.8	18.2	0.0	0.0

5-Year Qattenuated 5-Year Max. Storage Required Est. 5-Year Storage Elevation 15.99 L/s 12.2 m<sup>3</sup> 93.56 m

100-year Q<sub>attenuated</sub> 100-year Max. Storage Required Est. 100-year Storage Elevation 18.24 L/s 40.9 m<sup>3</sup> 93.71 m

<sup>\*\*</sup>V<sub>acc</sub>=Total surface and sub-surface

 $<sup>\</sup>dagger Q_{release}$  = Release rate calculated from orifice equation

Area ID A113A Available Sub-surface Storage

> Total Subsurface Storage (m<sup>3</sup>) 0.0

**Stage Attenuated Areas Storage Summary** 

			Surface	Storage		Surfa	ace and Sub	surface Sto	rage
	Stage	Ponding	100-Year HGL	Head (Stage to 100-year HGL)	delta d	V*	V <sub>acc</sub> **	Q <sub>release</sub> +	V <sub>drawdown</sub>
	(m)	(m²)	(m)	(m)	(m)	(m <sup>3</sup> )	(m <sup>3</sup> )	(L/s)	(hr)
Orifice INV	92.00	·		·		·	0.0	0.0	0.00
TG	93.50	0.36	93.09	0.41	0.41	0.1	0.1	7.7	0.01
Max Ponding	93.80	864	93.09	0.71	0.30	88.2	88.3	10.1	2.43

\* V=Incremental storage volume

**Orifice Location Total Area** 

**CB113A** 

Dia

75

0.172 ha 0.80 Rational Method runoff coefficient

Note: Rational Method Coefficient "C" increased by 25% for 100-year calculations

	5-Year					100-year				
t <sub>c</sub>	i	Q <sub>actual</sub>	Q <sub>release</sub>	Q <sub>stored</sub>	V <sub>stored</sub>	i	Q <sub>actual</sub>	Q <sub>release</sub>	Q <sub>stored</sub>	V <sub>stored</sub>
(min)	(mm/hr)	(L/s)	(L/s)	(L/s)	(m <sup>3</sup> )	(mm/hr)	(L/s)	(L/s)	(L/s)	(m <sup>3</sup> )
10	104.2	39.8	8.3	31.5	18.9	178.6	85.3	9.4	75.9	45.5
20	70.3	26.9	8.3	18.6	22.3	120.0	57.3	9.4	47.9	57.5
30	53.9	20.6	8.3	12.3	22.2	91.9	43.9	9.4	34.5	62.1
40	44.2	16.9	8.3	8.6	20.7	75.1	35.9	9.4	26.5	63.6
50	37.7	14.4	8.3	6.1	18.3	64.0	30.6	9.4	21.2	63.5
60	32.9	12.6	8.3	4.3	15.5	55.9	26.7	9.4	17.3	62.3
70	29.4	11.2	8.3	3.0	12.4	49.8	23.8	9.4	14.4	60.4
80	26.6	10.2	8.3	1.9	9.0	45.0	21.5	9.4	12.1	58.0
90	24.3	9.3	8.3	1.0	5.4	41.1	19.6	9.4	10.2	55.3
100	22.4	8.6	8.3	0.3	1.7	37.9	18.1	9.4	8.7	52.2
110	20.8	8.0	8.0	0.0	0.0	35.2	16.8	9.4	7.4	48.9
120	19.5	7.4	7.4	0.0	0.0	32.9	15.7	9.4	6.3	45.5
130	18.3	7.0	7.0	0.0	0.0	30.9	14.8	9.4	5.4	41.8
140	17.3	6.6	6.6	0.0	0.0	29.2	13.9	9.4	4.5	38.0
150	16.4	6.3	6.3	0.0	0.0	27.6	13.2	9.4	3.8	34.1
160	15.6	5.9	5.9	0.0	0.0	26.2	12.5	9.4	3.1	30.1
170	14.8	5.7	5.7	0.0	0.0	25.0	11.9	9.4	2.5	26.0
180	14.2	5.4	5.4	0.0	0.0	23.9	11.4	9.4	2.0	21.8
190	13.6	5.2	5.2	0.0	0.0	22.9	10.9	9.4	1.5	17.5
200	13.0	5.0	5.0	0.0	0.0	22.0	10.5	9.4	1.1	13.2
210	12.6	4.8	4.8	0.0	0.0	21.1	10.1	9.4	0.7	8.8
220	12.1	4.6	4.6	0.0	0.0	20.4	9.7	9.4	0.3	4.4
230	11.7	4.5	4.5	0.0	0.0	19.7	9.4	9.4	0.0	0.0
240	11.3	4.3	4.3	0.0	0.0	19.0	9.1	9.4	0.0	0.0
250	10.9	4.2	4.2	0.0	0.0	18.4	8.8	9.4	0.0	0.0
260	10.6	4.1	4.1	0.0	0.0	17.8	8.5	9.4	0.0	0.0

5-Year Qattenuated 5-Year Max. Storage Required Est. 5-Year Storage Elevation

8.28 L/s 22.3 m<sup>3</sup> 93.58 m

100-year Qattenuated 100-year Max. Storage Required Est. 100-year Storage Elevation

9.40 L/s 63.6 m<sup>3</sup> 93.72 m

 $<sup>^{**}</sup>V_{acc}$ =Total surface and sub-surface  $\uparrow$  Q<sub>release</sub> = Release rate calculated from orifice equation

Area ID A108 Available Sub-surface Storage

Total Subsurface Storage (m<sup>3</sup>) 0.0

**Stage Attenuated Areas Storage Summary** 

outsurface Storage (m ) 0.0

	-		Surface	Storage		Surfa	ace and Sub	surface Sto	rage
	Stage	Ponding	100-Year HGL	Head (Stage to 100-year HGL)	delta d	V*	V <sub>acc</sub> **	$\mathbf{Q}_{release}$ †	V <sub>drawdown</sub>
	(m)	(m²)	(m)	(m)	(m)	(m <sup>3</sup> )	(m <sup>3</sup> )	(L/s)	(hr)
Orifice INV	92.00						0.0	0.0	0.00
TG	93.50	0.36	93.09	0.41	0.41	0.1	0.1	7.7	0.01
Max Ponding	93.80	1,123	93.09	0.71	0.30	114.3	114.5	10.1	3.16

<sup>\*</sup> V=Incremental storage volume

75

Orifice Location Total Area

**CB108A** 0.157 ha

**A Dia** 7 ha

0.90 Rational Method runoff coefficient

Note: Rational Method Coefficient "C" increased by 25% for 100-year calculations

	5-Year					100-year				
t <sub>c</sub>	i	Q <sub>actual</sub>	Q <sub>release</sub>	Q <sub>stored</sub>	V <sub>stored</sub>	i	Q <sub>actual</sub>	Q <sub>release</sub>	Q <sub>stored</sub>	V <sub>stored</sub>
(min)	(mm/hr)	(L/s)	(L/s)	(L/s)	(m <sup>3</sup> )	(mm/hr)	(L/s)	(L/s)	(L/s)	(m <sup>3</sup> )
10	104.2	40.9	8.2	32.7	19.6	178.6	77.9	8.9	69.0	41.4
20	70.3	27.6	8.2	19.4	23.3	120.0	52.3	8.9	43.4	52.1
30	53.9	21.2	8.2	13.0	23.4	91.9	40.1	8.9	31.2	56.1
40	44.2	17.3	8.2	9.2	22.0	75.1	32.8	8.9	23.9	57.3
50	37.7	14.8	8.2	6.6	19.9	64.0	27.9	8.9	19.0	57.0
60	32.9	12.9	8.2	4.8	17.2	55.9	24.4	8.9	15.5	55.8
70	29.4	11.5	8.2	3.4	14.1	49.8	21.7	8.9	12.8	53.9
80	26.6	10.4	8.2	2.3	10.9	45.0	19.6	8.9	10.7	51.6
90	24.3	9.5	8.2	1.4	7.4	41.1	17.9	8.9	9.1	48.9
100	22.4	8.8	8.2	0.6	3.8	37.9	16.5	8.9	7.7	45.9
110	20.8	8.2	8.2	0.0	0.1	35.2	15.4	8.9	6.5	42.7
120	19.5	7.6	7.6	0.0	0.0	32.9	14.3	8.9	5.5	39.4
130	18.3	7.2	7.2	0.0	0.0	30.9	13.5	8.9	4.6	35.9
140	17.3	6.8	6.8	0.0	0.0	29.2	12.7	8.9	3.8	32.2
150	16.4	6.4	6.4	0.0	0.0	27.6	12.0	8.9	3.2	28.5
160	15.6	6.1	6.1	0.0	0.0	26.2	11.4	8.9	2.6	24.6
170	14.8	5.8	5.8	0.0	0.0	25.0	10.9	8.9	2.0	20.7
180	14.2	5.6	5.6	0.0	0.0	23.9	10.4	8.9	1.5	16.7
190	13.6	5.3	5.3	0.0	0.0	22.9	10.0	8.9	1.1	12.6
200	13.0	5.1	5.1	0.0	0.0	22.0	9.6	8.9	0.7	8.5
210	12.6	4.9	4.9	0.0	0.0	21.1	9.2	8.9	0.3	4.3
220	12.1	4.7	4.7	0.0	0.0	20.4	8.9	8.9	0.0	0.1
230	11.7	4.6	4.6	0.0	0.0	19.7	8.6	8.9	0.0	0.0
240	11.3	4.4	4.4	0.0	0.0	19.0	8.3	8.9	0.0	0.0
250	10.9	4.3	4.3	0.0	0.0	18.4	8.0	8.9	0.0	0.0
260	10.6	4.2	4.2	0.0	0.0	17.8	7.8	8.9	0.0	0.0

5-Year Qattenuated 5-Year Max. Storage Required Est. 5-Year Storage Elevation 8.16 L/s 23.4 m<sup>3</sup> 93.56 m 100-year Q<sub>attenuated</sub> 100-year Max. Storage Required Est. 100-year Storage Elevation 8.88 L/s

57.3 m<sup>3</sup>

93.65 m

<sup>\*\*</sup>V<sub>acc</sub>=Total surface and sub-surface

 $<sup>\</sup>dagger$  Q<sub>release</sub> = Release rate calculated from orifice equation

Area ID A103B Available Sub-surface Storage

> Total Subsurface Storage (m<sup>3</sup>) 0.0

Stage Attenuated Areas Storage Summary

			Surface	Storage		Surface and Subsurface Storage				
	Stage	Ponding	100-Year HGL	Head (Stage to 100-year HGL)	delta d	V*	V <sub>acc</sub> **	Q <sub>release</sub> †	V <sub>drawdown</sub>	
	(m)	(m²)	(m)	(m)	(m)	(m <sup>3</sup> )	(m <sup>3</sup> )	(L/s)	(hr)	
Orifice INV	92.00						0.0	0.0	0.00	
TG	93.50	0.36	93.09	0.41	0.41	0.1	0.1	7.7	0.01	
Max Ponding	93.80	751	93.09	0.71	0.30	76.7	76.9	10.1	2.12	

<sup>\*</sup> V=Incremental storage volume

75

Orifice Location CB103B Dia **Total Area** 0.086 ha

0.90 Rational Method runoff coefficient Note: Rational Method Coefficient "C" increased by 25% for 100-year calculations

	5-Year					100-year				
t <sub>c</sub>	i	Q <sub>actual</sub>	Q <sub>release</sub>	Q <sub>stored</sub>	V <sub>stored</sub>	i	Q <sub>actual</sub>	Q <sub>release</sub>	Q <sub>stored</sub>	V <sub>stored</sub>
(min)	(mm/hr)	(L/s)	(L/s)	(L/s)	(m <sup>3</sup> )	(mm/hr)	(L/s)	(L/s)	(L/s)	(m <sup>3</sup> )
10	104.2	22.4	7.9	14.5	8.7	178.6	42.7	8.4	34.2	20.5
20	70.3	15.1	7.9	7.2	8.6	120.0	28.7	8.4	20.2	24.3
30	53.9	11.6	7.9	3.7	6.6	91.9	21.9	8.4	13.5	24.3
40	44.2	9.5	7.9	1.6	3.7	75.1	18.0	8.4	9.5	22.9
50	37.7	8.1	7.9	0.2	0.5	64.0	15.3	8.4	6.8	20.5
60	32.9	7.1	7.1	0.0	0.0	55.9	13.4	8.4	4.9	17.7
70	29.4	6.3	6.3	0.0	0.0	49.8	11.9	8.4	3.5	14.5
80	26.6	5.7	5.7	0.0	0.0	45.0	10.7	8.4	2.3	11.1
90	24.3	5.2	5.2	0.0	0.0	41.1	9.8	8.4	1.4	7.5
100	22.4	4.8	4.8	0.0	0.0	37.9	9.1	8.4	0.6	3.7
110	20.8	4.5	4.5	0.0	0.0	35.2	8.4	8.4	0.0	0.0
120	19.5	4.2	4.2	0.0	0.0	32.9	7.9	8.4	0.0	0.0
130	18.3	3.9	3.9	0.0	0.0	30.9	7.4	8.4	0.0	0.0
140	17.3	3.7	3.7	0.0	0.0	29.2	7.0	8.4	0.0	0.0
150	16.4	3.5	3.5	0.0	0.0	27.6	6.6	8.4	0.0	0.0
160	15.6	3.3	3.3	0.0	0.0	26.2	6.3	8.4	0.0	0.0
170		3.2	3.2	0.0	0.0	25.0	6.0	8.4	0.0	0.0
180	14.2	3.0	3.0	0.0	0.0	23.9	5.7	8.4	0.0	0.0
190	13.6	2.9	2.9	0.0	0.0	22.9	5.5	8.4	0.0	0.0
200	13.0	2.8	2.8	0.0	0.0	22.0	5.3	8.4	0.0	0.0
210	12.6	2.7	2.7	0.0	0.0	21.1	5.1	8.4	0.0	0.0
220	12.1	2.6	2.6	0.0	0.0	20.4	4.9	8.4	0.0	0.0
230	11.7	2.5	2.5	0.0	0.0	19.7	4.7	8.4	0.0	0.0
240	11.3	2.4	2.4	0.0	0.0	19.0	4.5	8.4	0.0	0.0
250	10.9	2.4	2.4	0.0	0.0	18.4	4.4	8.4	0.0	0.0
260	10.6	2.3	2.3	0.0	0.0	17.8	4.3	8.4	0.0	0.0

5-Year Qattenuated 7.94 L/s 8.7 m<sup>3</sup> 5-Year Max. Storage Required Est. 5-Year Storage Elevation 93.53 m

100-year Q<sub>attenuated</sub> 100-year Max. Storage Required Est. 100-year Storage Elevation 93.59 m

8.43 L/s

24.3 m<sup>3</sup>

Summary of Release Rates and Storage Volumes

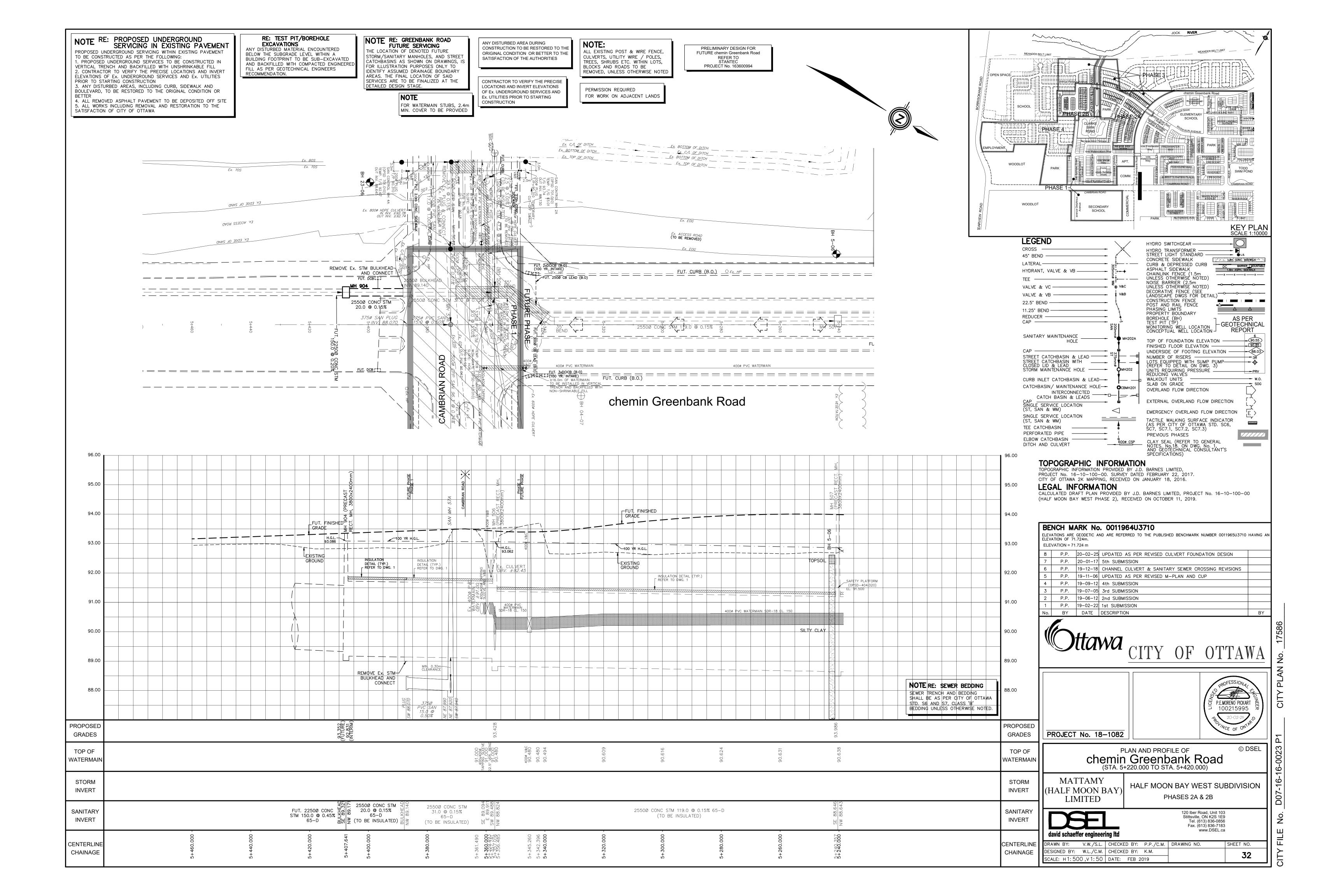
Control Area	5-Year Release	5-Year	100-Year	100-Year	100-Year
	Rate	Required	Release	Required	Available
		Storage	Rate	Storage	Storage
	(L/s)	(m <sup>3</sup> )	(L/s)	(m <sup>3</sup> )	(m <sup>3</sup> )
U1	4.7	0.0	10.1	0.0	0.0
U2	11.4	0.0	21.6	0.0	0.0
U3	13.5	0.0	28.9	0.0	0.0
U4	0.7	0.0	1.4	0.0	0.0
U5	2.5	0.0	5.3	0.0	0.0
METRO	24.2	55.5	31.9	126.8	317.5
BLDG A	7.5	10.7	10.0	25.3	73.6
BLDG B	7.3	9.0	9.8	21.4	65.7
BLDG C	5.1	5.7	6.9	13.7	43.5
A109	9.6	3.2	25.6	3.8	4.2
A110B	9.4	2.7	10.0	12.0	43.0
A110A	9.6	7.3	10.4	25.0	54.7
A114A	16.0	12.2	18.2	40.9	68.7
A113A	8.3	22.3	9.4	63.6	88.3
A108	8.2	23.4	8.9	57.3	114.5
A103B	7.9	8.7	8.4	24.3	76.9
A106 & A107	23.0	60.0	24.5	169.2	51.1
Total	168.9	220.8	241.4	583.4	1001.8

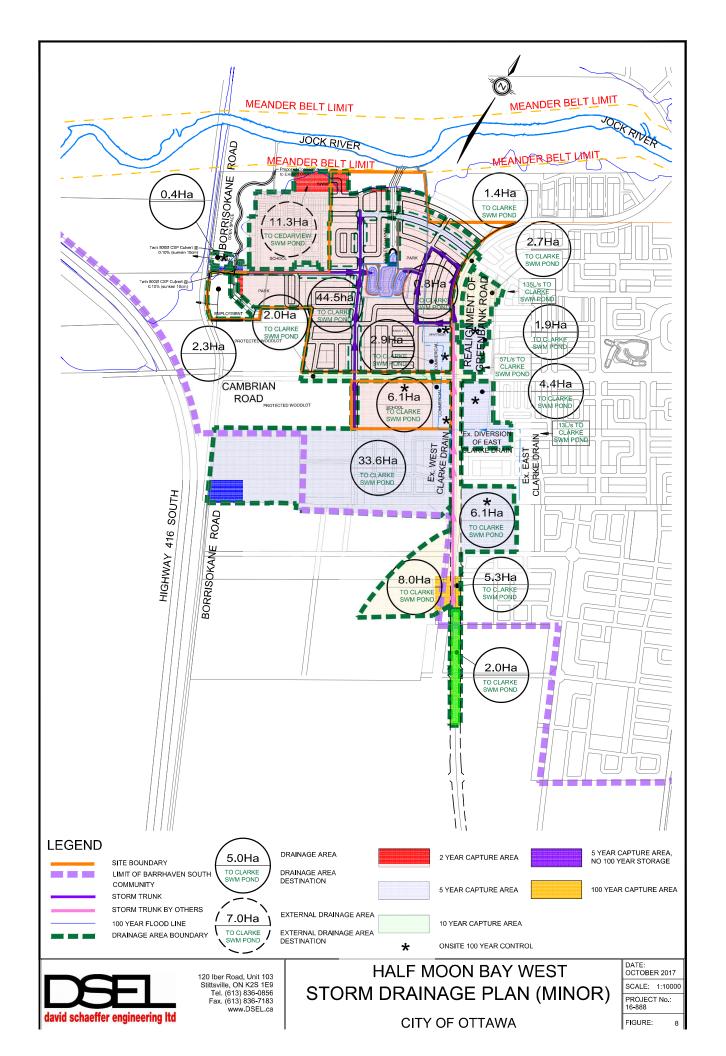
<sup>\*\*</sup>V<sub>acc</sub>=Total surface and sub-surface

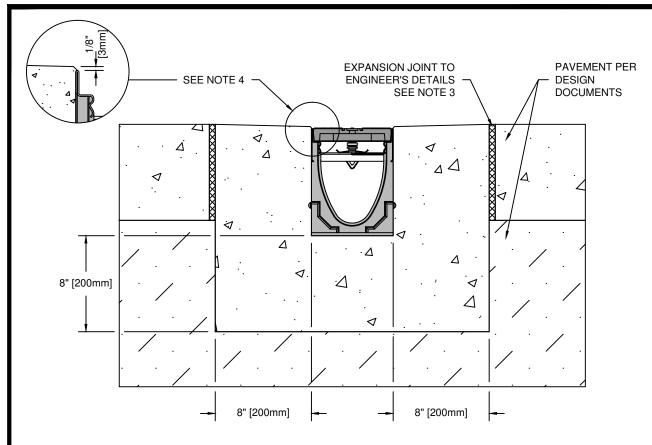
 $<sup>\</sup>dagger$  Q<sub>release</sub> = Release rate calculated from orifice equation

										Sewer Data								
Area ID	Up	Down	Area	С	Indiv AxC	Acc AxC	T <sub>C</sub>	ı	Q	DIA	Slope	Length	A <sub>hydraulic</sub>	R	Velocity	Qcap	Time Flow	Q / Q full
			(ha)	(-)			(min)	(mm/hr)	(L/s)	(mm)	(%)	(m)	(m <sup>2</sup> )	(m)	(m/s)	(L/s)	(min)	(-)
110	CTM110	CTM111	0.100	0.50	0.06	0.06	10.0	104.0	17.7	200	0.40	75	0.071	0.075	0.07	61.0	1.4	0.00
U3 U2	STM112 STM111	STM111 STM110	0.122	0.50			10.0 11.4		62.0	300 375	0.40		0.071 0.110	0.075 0.094	0.87 1.00	61.2 110.9		0.29 0.56
BLDG A	STM110	STM110	0.093	0.80			12.6		68.9	375	0.40		0.110	0.094	0.87	96.0		0.36
DEDG A	STIVITIO	STWITOO	0.093	0.90	0.00	0.31	14.04		00.3	373	0.50	70.5	0.110	0.034	0.07	30.0	1.5	0.72
						0.01												
A107	CBMH107	CBMH106	0.205	0.85	0.17	0.17	10.0	104.2	50.4	300	0.50	20.8	0.071	0.075	0.97	68.4	0.4	0.74
A106	CBMH106	STM104	0.250	0.80	0.20	0.37	10.4	102.3	106.4	375	0.50	12.2	0.110	0.094	1.12	124.0	0.2	0.86
					-	0.37	10.5											
BLDG B			0.083	0.90	0.07	0.07	10.0	104.2	9.8									
DEDG B			0.003	0.30	0.07	0.07	10.0		3.0									
						0.07	10.0											
U4	STM105	STM104	0.015	0.20	0.00	0.08	10.0	104.2	10.7	300	0.50	30.8	0.071	0.075	0.97	68.4	0.5	0.16
						0.08	10.5											
	STM104	STM113			0.00		10.5		127.3	450	0.50	22.5	0.159	0.113	1.27	201.6	0.3	0.63
						0.45	10.8											
A114A, U5	STM114	STM113	0.185	0.74	0.14	0.14	10.0	104.2	39.6	300	0.50	35.2	0.071	0.075	0.97	68.4	0.6	0.58
7111471, 00	OTIVITIT	OTIVITIO	0.100	0.74	0.14	0.14	10.6		00.0	000	0.00	00.2	0.071	0.070	0.57	00.4	0.0	0.00
A113A	STM113	STM103	0.172	0.80	0.14	0.73	10.8	100.0	201.7	525	0.50	16.6	0.216	0.131	1.40	304.1	0.2	0.66
						0.73	11.0											
METRO			0.404	0.00	0.00	0.00	100	1010	0.1.0									
METRO			0.401	0.90	0.36		10.0		31.9									
						0.36	10.0											
A109	STM109	STM108	0.083	0.40	0.03	0.39	10.0	104.2	41.5	375	0.50	39.8	0.110	0.094	1.12	124.0	0.6	0.33
71100	01111100	C1111100	0.000	0	0.00	0.39	10.6			0.0	0.00	30.0	00	0.00			3.0	0.00
A108	STM108	STM103	0.157	0.85	0.13		14.0		202.7	525	0.28	51.5	0.216	0.131	1.05	227.6	0.8	0.89
						0.84	14.9											
BLDG C			0.055	0.00	0.05	0.05	10.0	104.0	6.0									
BLDG C			0.055	0.90	0.05	0.05 0.05	10.0		6.9									
						0.03	10.0											
A103B	STM103	STM102	0.086	0.90	0.08	1.69	14.9	84.0	390.8	750	0.30	39.8	0.442	0.188	1.38	609.8	0.5	0.64
A102	STM102	STM101			0.00		15.3		388.2	750	0.20		0.442	0.188	1.13	497.9		0.78
A101	STM101	Fut. MH 904			0.00	1.69	15.7	81.4	383.2	750	0.20		0.442	0.188	1.13	497.9		0.77
				_		1.69	16.19				_							_
**Controlled 100	D-year Building	Flow																
Controlled 100	J-year Bullulling	1 1000																

2020-08-05









#### NOTES:

- 1. IT IS NECESSARY TO ENSURE MINIMUM DIMENSIONS SHOWN ARE SUITABLE FOR EXISTING GROUND CONDITIONS. ENGINEERING ADVICE MAY BE REQUIRED.
- 2. MINIMUM CONCRETE STRENGTH OF 4,000 PSI IS RECOMMENDED. CONCRETE SHOULD BE VIBRATED TO ELIMINATE AIR POCKETS.
- 3. EXPANSION AND CONTRACTION CONTROL JOINTS AND REINFORCEMENT ARE RECOMMENDED TO PROTECT CHANNEL AND CONCRETE SURROUND. ENGINEERING ADVICE MAY BE REQUIRED.
- 4. THE FINISHED LEVEL OF THE CONCRETE SURROUND MUST BE APPROX. 1/8" [3mm] ABOVE THE TOP OF THE CHANNEL EDGE.
- 5. CONCRETE BASE THICKNESS SHOULD MATCH SLAB THICKNESS. ENGINEERING ADVICE MAY BE REQUIRED TO DETERMINE PROPER LOAD CLASS.
- 6. REFER TO ACO'S LATEST INSTALLATION INSTRUCTIONS FOR FURTHER DETAILS.

#### SPECIFICATION CLAUSE

#### K100 KLASSIKDRAIN - LOAD CLASS E

#### **GENERAL**

THE SURFACE DRAINAGE SYSTEM SHALL BE POLYMER CONCRETE K100 CHANNEL SYSTEM WITH GALVANIZED STEEL EDGE RAILS AS MANUFACTURED BY ACO POLYMER PRODUCTS, INC.

#### **MATERIALS**

CHANNELS SHALL BE MANUFACTURED FROM POLYESTER RESIN POLYMER CONCRETE WITH AN INTEGRALLY CAST-IN GALVANIZED STEEL EDGE RAIL. MINIMUM PROPERTIES OF POLYMER CONCRETE WILL BE AS FOLLOWS:

COMPRESSIVE STRENGTH: 14,000 PSI
FLEXURAL STRENGTH: 4,000 PSI
TENSILE STRENGTH: 1,500 PSI
WATER ABSORPTION: 0.07%
FROST PROOF YES
DILUTE ACID AND ALKALI RESISTANT
B117 SALT SPRAY TEST COMPLIANT YES

THE SYSTEM SHALL BE 4" (100mm) NOMINAL INTERNAL WIDTH WITH A 5.1" (130mm) OVERALL WIDTH AND A BUILT-IN SLOPE OF 0.5%. CHANNEL INVERT SHALL HAVE DEVELOPED "V" SHAPE. ALL CHANNELS SHALL BE INTERLOCKING WITH A MALE/FEMALE JOINT.

THE COMPLETE DRAINAGE SYSTEM SHALL BE BY ACO POLYMER PRODUCTS, INC. ANY DEVIATION OR PARTIAL SYSTEM DESIGN AND/OR IMPROPER INSTALLATION WILL VOID ANY AND ALL WARRANTIES PROVIDED BY ACO POLYMER PRODUCTS, INC.

CHANNEL SHALL WITHSTAND LOADING TO PROPER LOAD CLASS AS OUTLINED BY EN 1433. GRATE TYPE SHALL BE APPROPRIATE TO MEET THE SYSTEM LOAD CLASS SPECIFIED AND INTENDED APPLICATION. GRATES SHALL BE SECURED USING 'QUICKLOK' BOLTLESS LOCKING SYSTEM. CHANNEL AND GRATE SHALL BE CERTIFIED TO MEET THE SPECIFIED EN 1433 LOAD CLASS. THE SYSTEM SHALL BE INSTALLED IN ACCORDANCE WITH THE MANUFACTURER'S INSTRUCTIONS AND RECOMMENDATIONS.

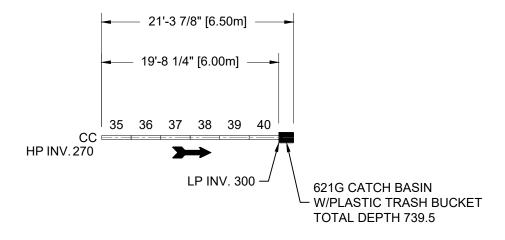
# K1-E-ECP ACO DATE: 08/24/15

# K100 - KLASSIKDRAIN - LOAD CLASS: E Exposed Concrete Pavement

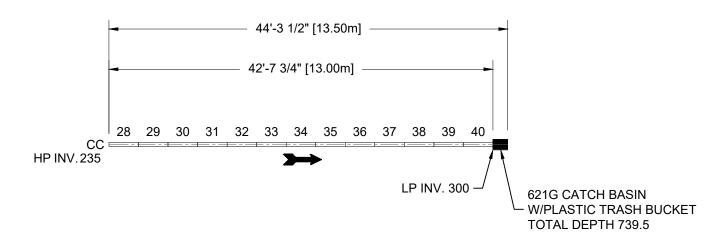
**INSTALLATION DRAWING - ACO DRAIN** 

ACO Polymer Products, Inc.

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TD - 2



#### **GENERAL NOTES**

- 1. IT IS CUSTOMERS RESPONSIBILITY TO ENSURE THAT EACH PRODUCT IS FIT FOR IT'S INTENDED PURPOSE AND THAT THE ACTUAL CONDITIONS ARE SUITABLE.
- 2. IT IS THE CUSTOMERS RESPONSIBILITY TO FOLLOW ACO POLYMER PRODUCTS, INC. INSTALLATION INSTRUCTIONS FOR EACH PRODUCT. SEEK ENGINEERING ADVISE FOR INSTALLATIONS NOT ILLUSTRATED IN THE INSTALLATION GUIDELINES.
- 3. FOR FURTHER PRODUCT INFORMATION, CUT SHEETS, SPECIFICATIONS AND INSTALLATION INSTRUCTIONS, PLEASE VISIT US AT OUR WEBSITE: WWW.ACOUSA.COM.
- ACO IS NOT RESPONSIBLE TO ENSURE PROPER FLOW TO SYSTEMS OUTLETS OR CATCH BASINS, REFER TO GRADING PLANS. ALL TRENCH DRAIN LAYOUTS ARE DESIGNED AT 0.0% LONGITUDINAL PAVEMENT SLOPE UNLESS OTHERWISE NOTED.

#### **TRENCH NOTES**

- 1. ALL FABRICATIONS TO BE COMPLETED BY INSTALLING CONTRACTOR.
- 2. DIMENSIONS ARE FROM OUTSIDE TO OUTSIDE

ALL DRAWINGS ARE AS ACCURATE AS THE INFORMATION SUPPLIED. ALL REASONABLE CARE HAS BEEN TAKEN IN COMPILING THE INFORMATION WITHIN. PLEASE REVIEW THIS INFORMATION FOR ACCURACY.

☐ APPROVED ☐ APPROVED AS NOTED	REVISE AND RESUBMIT REJECTED
SIGNED:	
DATE:	

LEGEND CHANNEL CC = CLOSING CAP OC = OUTLET CAP CENTER LINE INV = INVERT INSTALLATION DIRECTION HP = HIGH POINT OF CHANNEL LP = LOW POINT VOA = VERTICAL OUTLET ADAPTER BO = BOTTOM OUTLET BAU = BRICKSLOT ACCESS UNIT

METR	O GREENBANK		TRENCH DRAIN LAYOUT							
ON		SYS	ГЕМ(S) <b>К100</b>	GRATE(S) <b>461Q S</b>	LOTTED	D.I.				
DRAWN BY:	EMAIL:			REVISIONS						
KZ	kyle.zheng@aco.com	NO.	DESCRIPTION		DATE	BY				
DATE <b>08-13-2020</b>	CHECKED BY:	A	-		-					
** ** ***	DESIGN SERV NO REV.	B								
SHEET NO.	DESIGN SERV. NO. REV.	$\vdash \overline{}$								
SHEET 1 OF 1	920-558									



COMMENTS:

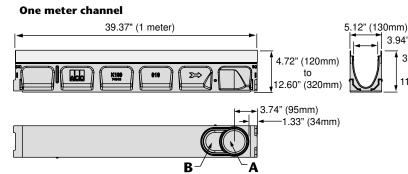


## KlassikDrain - K100 Galvanized steel edge rail channel system

3.94" (100mm)

11.81" (300mm)

3.94" (100mm) Half meter channel



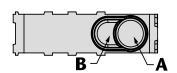
19.69" (0.5 meter)

6.69" (170mm) K1-0103

8.66" (220mm) K1-0203

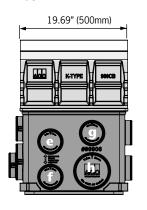
10.63" (270mm) K1-0303

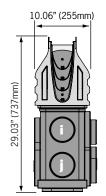
12.60" (320mm) K1-0403

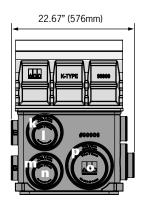


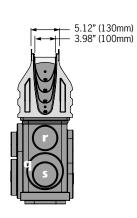
## Type K901G In-line catch basin

Knock-outs included on every 5th channel







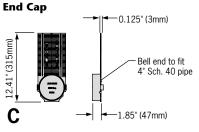


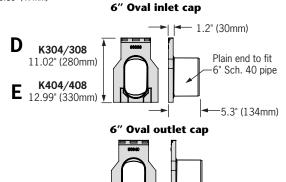
Total capacity = 10.49 gallons

#### Outlet flow rates

Outlet	Product	Outlet size (Sch. 40)	Invert Depth	GPM	CFS
Α	Bottom outlet - K00	4" round	3.94"	108	0.24
Α	Bottom outlet - K40	4" round	11.81"	187	0.42
В	Bottom outlet - K00	6" oval	3.94"	177	0.39
В	Bottom outlet - K40	6" oval	11.81"	306	0.68
C	End outlet - K20	4" round	7.87"	132	0.29
C	End outlet - K40	4" round	11.81"	171	0.38
D	K1-308-6 6" outlet cap	6" oval	9.84"	233	0.52
E	K1-408-6 6" outlet cap	6" oval	11.81"	264	0.59
F	Type K1-901G	4" round	19.30"	226	0.50
G	Type K1-901G	4" round	25.67"	265	0.59
Н	Type K1-901G	4" round	25.30"	263	0.59
I	Type K1-901G	4" round	18.56"	222	0.49
J	Type K1-901G	6" round	25.85"	586	1.30
K	Type K1-901G	4" round	26.43"	269	0.60
L	Type K1-901G	4" round	19.36"	227	0.51
M	Type K1-901G	6" round	27.30"	604	1.35
N	Type K1-901G	6" round	19.99"	505	1.12
0	Type K1-901G	8" round	27.30"	1051	2.34
P	Type K1-901G	6" round	26.43"	593	1.32
Q	Type K1-901G	4" round	27.17"	273	0.61
R	Type K1-901G	4" round	20.68"	235	0.52
S	Type K1-901G	4" round	18.99"	224	0.50
Т	Type K1-901G	6" round	27.17"	6.02	1.34

**Note:** These are the pipe flow rates at the specified outlet, **NOT** channel flow rates. Catch basin flow rates are without trash bucket - using trash bucket reduces flow.







## KlassikDrain - K100 Galvanized steel edge rail channel system



		Inve		
Description	Part			Weight
	No.	Inches®	mm <sup>2</sup>	Lbs.
K1-00 Neutral channel - 39.37" (1m) <sup>©</sup>	74041	3.94	100	28.1
K1-1 Sloped channel - 39.37" (1m)	74001	4.13	105	28.1
K1-2 Sloped channel - 39.37" (1m)	74002	4.33	110	28.9
K1-3 Sloped channel - 39.37" (1m)	74003	4.53	115	29.7
K1-4 Sloped channel - 39.37" (1m)	74004	4.72	120	30.5
K1-5 Sloped channel - 39.37" (1m) $^{\oplus}$	74005	4.92	125	31.3
K1-6 Sloped channel - 39.37" (1m)	74006	5.12	130	32.1
K1-7 Sloped channel - 39.37" (1m)	74007	5.31	135	32.9
K1-8 Sloped channel - 39.37" (1m)	74008	5.51	140	33.7
K1-9 Sloped channel - 39.37" (1m)	74009	5.71	145	34.5
K1-10 Sloped channel - 39.37" (1m) $^{\mathbb{D}}$	74010	5.91	150	35.3
K1-010 Neutral channel - 39.37" (1m) <sup>©</sup>	74043	5.91	150	35.3
K1-0103 Neutral channel - 19.69" $(0.5m)^{\mathbb{D}}$	74044	5.91	150	17.0
K1-11 Sloped channel - 39.37" (1m)	74011	6.10	155	36.1
K1-12 Sloped channel - 39.37" (1m)	74012	6.30	160	36.9
K1-13 Sloped channel - 39.37" (1m)	74013	6.50	165	37.7
K1-14 Sloped channel - 39.37" (1m)	74014	6.69	170	38.5
K1-15 Sloped channel - 39.37" (1m) <sup>©</sup>	74015	6.89	175	39.3
K1-16 Sloped channel - 39.37" (1m)	74016	7.09	180	40.1
K1-17 Sloped channel - 39.37" (1m)	74017	7.28	185	40.9
K1-18 Sloped channel - 39.37" (1m)	74018	7.48	190	41.7
K1-19 Sloped channel - 39.37" (1m)	74019	7.68	195	42.5
K1-20 Sloped channel - 39.37" (1m) $^{\circ}$	74020	7.87	200	43.4
K1-020 Neutral channel - 39.37" (1m) <sup>©</sup>	74045	7.87	200	43.4
K1-0203 Neutral channel - 19.69" (0.5m) $^{\circ}$	74046	7.87	200	20.5
K1-21 Sloped channel - 39.37" (1m)	74021	8.07	205	44.2
K1-22 Sloped channel - 39.37" (1m)	74022	8.27	210	45.0
K1-23 Sloped channel - 39.37" (1m)	74023	8.46	215	45.8
K1-24 Sloped channel - 39.37" (1m)	74024	8.66	220	46.6
K1-25 Sloped channel - 39.37" (1m) <sup>©</sup>	74025	8.86	225	47.4
K1-26 Sloped channel - 39.37" (1m)	74026	9.06	230	48.2
K1-27 Sloped channel - 39.37" (1m)	74027	9.25	235	49.0

Description	Part	Inve	ert	Weight
Description	No.	Inches®	mm <sup>2</sup>	Lbs.
K1-28 Sloped channel - 39.37" (1m)	74028	9.45	240	49.8
K1-29 Sloped channel - 39.37" (1m)	74029	9.65	245	50.6
K1-30 Sloped channel - 39.37" (1m) <sup>①</sup>	74030	9.84	250	51.4
K1-030 Neutral channel - 39.37" (1m) <sup>D</sup>	74047	9.84	250	51.4
K1-0303 Neutral channel - 19.69" (0.5m) <sup>©</sup>	74048	9.84	250	24.0
K1-31 Sloped channel - 39.37" (1m)	74031	10.04	255	52.2
K1-32 Sloped channel - 39.37" (1m)	74032	10.24	260	53.0
K1-33 Sloped channel - 39.37" (1m)	74033	10.43	265	53.8
K1-34 Sloped channel - 39.37" (1m)	74034	10.63	270	54.6
K1-35 Sloped channel - 39.37" (1m) <sup>D</sup>	74035	10.83	275	55.4
K1-36 Sloped channel - 39.37" (1m)	74036	11.02	280	56.2
K1-37 Sloped channel - 39.37" (1m)	74037	11.22	285	57.0
K1-38 Sloped channel - 39.37" (1m)	74038	11.42	290	57.9
K1-39 Sloped channel - 39.37" (1m)	74039	11.61	295	58.7
K1-40 Sloped channel - 39.37" (1m) <sup>D</sup>	74040	11.81	300	59.5
K1-040 Neutral channel - 39.37" (1m) <sup>D</sup>	74049	11.81	300	59.5
K1-0403 Neutral channel - 19.69" (0.5m) <sup>©</sup>	74050	11.81	300	27.5
K1-901G In-line catch basin - 19.69" (0.5m) <sup>®</sup>	94608	28.81	701.9	52.6
K1-621G catch basin - 19.69" (0.5m) <sup>®</sup>	94617	28.84	732.5	55.8
K1-631G catch basin - 19.69" (0.5m)®	94631	40.84	1037.4	65.8
K1-Series 600 Optional plastic riser	99902	-	-	10.0
Foul air trap - fits both 900 & 600 series basins	90854	-	-	1.2
K1-304-6 6" Inlet Cap	96839	9.84	250	5.2
K1-308-6 6" Outlet Cap	96840	9.84	250	5.0
K1-404-6 6" Inlet Cap	96834	11.81	300	6.0
K1-408-6 6" Outlet Cap	96836	11.81	300	5.8
Universal end cap	96822	11.81	300	0.4
Debris strainer for 4" bottom knockout	93488	-	-	0.2
4" Oval to 6" round outlet adapter	95140	-	-	1.1
K1-Installation device	97477	-	-	2.8
Grate removal tool	01318	-	-	0.3
K1-QuickLok locking bar	02899	-	_	0.1

#### Notes:

- 1. This channel offers a bottom knockout feature; 4" round/6" oval.
- 2. Inverts shown are for the male end; for female invert depth subtract 5mm (≈0.2") from the male invert (except for neutral channels, where it will be same as male invert). To calculate the overall channel depth add 20mm (≈0.8") to invert depth.
- 3. This catch basin kit includes a polymer concrete top, removable Quicklok locking bar, trash bucket and plastic base. Select an appropriate grate.
- 4. This catch basin kit includes a polymer concrete top, removable Quicklok locking bar, deep trash bucket, plastic riser and plastic base. Select an appropriate grate.

#### **Specifications**

#### General

The surface drainage system shall be ACO Drain K100 complete with gratings secured with 'QuickLok' locking as manufactured by ACO, Inc. or approved equal.

#### **Materials**

The trench system bodies shall be manufactured from polyester polymer concrete with the minimum properties as follows:

Compressive strength: 14,000 psi Flexural strength: 4,000 psi Water absorption 0.07%
Frost proof YES
Salt proof YES
Dilute acid and alkali resistant YES

The nominal clear opening shall be 4" (100mm) with overall width of 5.12" (130mm). Pre-cast units shall be manufactured with either an invert slope of 0.5% or with neutral invert and have a wall thickness of at least 0.50" (13mm). Each unit will feature a partial radius in the trench bottom and a male to female interconnecting end profile. Units shall have horizontal cast in anchoring keys on the outside wall to ensure maximum mechanical bond to the surrounding bedding material and pavement surface. The galvanized steel edge rail will be integrally

cast in by the manufacturer to ensure maximum homogeneity between polymer concrete body and edge rail. Each edge rail shall be at least 3/32" (2.5mm) thick.

#### Grates

Grates shall be specified. See separate ACO Spec Info grate sheets for details. After removal of grates and 'QuickLok' bar there shall be uninterrupted access to the trench to aid maintenance.

#### Installation

The trench drain system shall be installed in accordance with the manufacturer's installation instructions and recommendations.

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## **Electronic Contact:** info@ACODrain.us www.ACODrain.us



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## Type 461Q Ductile iron slotted grate







#### **Product Features**

- Certified to EN 1433 Load Class E 135,000 lbs 2,788 psi
- · Uses 'QuickLok' boltless locking system
- Suitable for use with K100, KS100, C100, H100-8, H100-10, H100K-8 H100KS-8, and NW100 channels



### **Specifications**

#### General

The surface drainage system shall be ACO Drain K100, KS100, C100, H100-8, H100-10, H100K-8, H100KS-8, and NW100 channels\* complete with ACO Type 461Q Ductile iron slotted grate with 'QuickLok' locking as manufactured by ACO Polymer Products, Inc. or similar approved.

#### Materials

The covers shall be manufactured from ductile iron and have  ${\it minimum}$  properties as follows:

- Independently certified to meet Load Class E to EN 1433 - 135,000 lbs - 2,788 psi
- Ductile iron to ASTM A 536-84 Grade 65-45-12
- Intake area of 46.94 sq. in. (302.84 cm²) per half meter of grate

The overall width of 4.84" (123mm) and overall length of 19.69" (500mm). Slots measure at a maximum of 3.95" (100.2mm).

#### Installation

The trench drain system and grates shall be installed in accordance with the manufacturer's installation instructions and recommendations.

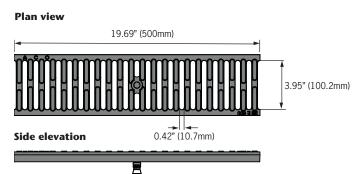
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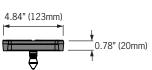












Description	Part No.	Length inches <i>(mm)</i>	Width inches (mm)	Weight lbs.
QuickLok grate Type 461Q Ductile iron slotted grate	96752	19.69 ( <i>500</i> )	4.84 (123)	10.2
QuickLok locking bar	02899	-	- '	0.1
QuickLok grate removal tool	01318	-	-	0.3

#### 'QuickLok' locking mechanism ACO 'QuickLok' is a patented boltless locking system, grates are removed and replaced with the Channel minimum time and effort for ease of maintenance. The unique design provides a positive 'snap down' fit into the locking bar. A stud is fixed to the grate which 'locks' into the -Grate spring clip in the locking bar. 'QuickLok' locking The 'QuickLok' stud is made from stud (fixed to grate) stainless steel and high density 'QuickLok' locking spring (fixed to nylon, the locking bar and clip are locking bar) stainless steel, for use in both 10 'QuickLok' locking general purpose and corrosive bar (side and plan environments.

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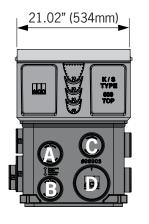
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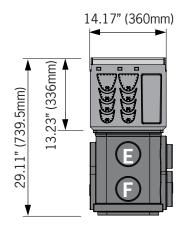


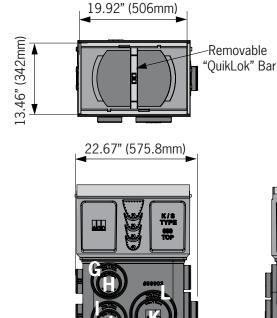
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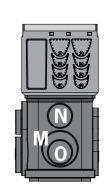
## K1-621G Catch Basin

#### K1-621G Catch Basin









#### **Outlet flow rates**

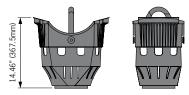
Outlet	Product	Outlet size (Sch. 40)	Invert Depth	GPM	CFS
Α	Type K1-621G	4" round	21.29"	239	0.53
В	Type K1-621G	4" round	27.79"	276	0.62
C	Type K1-621G	4" round	19.72"	229	0.51
D	Type K1-621G	6" round	27.79"	610	1.36
E	Type K1-621G	4" round	19.84"	230	0.51
F	Type K1-621G	4" round	26.34"	269	0.60
G	Type K1-621G	6" round	20.62"	514	1.15
Н	Type K1-621G	4" round	20.07"	231	0.52
I	Type K1-621G	6" round	27.76"	609	1.36
J	Type K1-621G	4" round	27.19"	273	0.61
K	Type K1-621G	6" round	27.19"	602	1.34
L	Type K1-621G	8" round	27.76"	1061	2.36
M	Type K1-621G	6" round	26.28"	591	1.32
N	Type K1-621G	4" round	19.15"	225	0.50
0	Type K1-621G	4" round	25.86"	266	0.59

#### Notes:

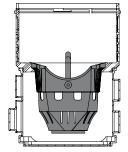
- 1. These are the pipe flow rates at the specified outlet, **NOT** channel flow rates.
- ${}^\star \text{Flow}$  rates without trash bucket using trash bucket or filter bag reduces flow rates.
- 2. 4" diameter foul air trap, part# 90854, can be fitted to catch basin base at outlet positions A/B and E/F  $\,$

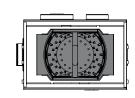
#### **Trash Bucket**





Note: Openings in trash bucket are 35.7"2 (23,033mm²)





Note: Trash bucket position within K1-621G catch basin body and base



ACO Specificat

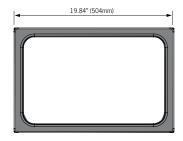
**April 2018** 

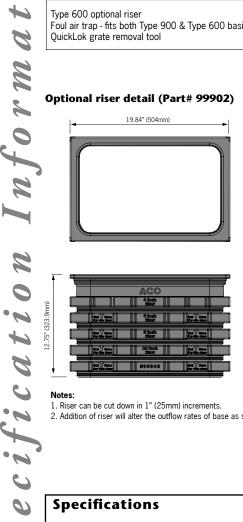
## K1-621G Catch Basin

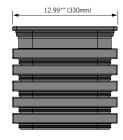
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Description	Part No.	Invert inches	Depth mm	Weight lbs.
Type K1-621G Catch basin assembly - top, removable "QuikLok" bar, trash bucket & base	94617	28.86	733.2	55.8
Catch Basin Components				
Type 600 optional riser Foul air trap - fits both Type 900 & Type 600 basins QuickLok grate removal tool	99902 90854 01318	40.86 - -	1038 - -	10.0 1.2 0.3

#### Optional riser detail (Part# 99902)







#### Notes:

- 1. Riser can be cut down in 1" (25mm) increments.
- 2. Addition of riser will alter the outflow rates of base as shown on table overleaf.

## Specifications

#### General

The catch basin shall be ACO Drain K1-621G Catch Basin - comprising of top section, trash bucket and base as manufactured by ACO, Inc. or similar approved.

#### Materials

The top unit body shall be manufactured from polyester polymer concrete with minimum properties as follows:

14,000 psi Compressive strength: 4,000 psi Flexural strength: Water absorption 0.07% Frost proof YES

Salt proof YES Dilute acid and alkali resistant

The nominal clear opening shall be 13.46" (342mm) wide by 19.92" (506mm) long. Overall width of 22.70" (575.8mm) by 15.38" (390.6mm) long. Type K1-621G catch basin assembly has overall depth of 29.11" (739.5mm). Polymer concrete top units shall incorporate a cast in galvanized steel frame manufactured with drillouts for channel connection and have a wall thickness of at least 0.59" (15mm). Top units shall have horizontal cast in anchoring key features on the outside to ensure maximum mechanical bond to the surrounding bedding material and pavement surface. The base unit shall be a LLDPE plastic molding and incorporate molded plastic pipe stubbs to facilitate pipe connection.

#### Optional Riser

Optional riser can be useful between polymer concrete top unit and LLDPE base unit. Use of riser is determined by acess and local building codes.

#### Grates

Grates shall be specified. See separate ACO Spec Info grate sheets for details. After removal of grates and 'QuickLok' bar there shall be uninterrupted access to the catch basin to aid maintenance. Accepts all half-meter ACO K300 Drainlok grates or K300 Quicklok grates with optional QL bar.

The trench drain/catch basin system shall be installed in accordance with the manufacturer's installation instructions and recommendations.

#### ACO, Inc. **Northeast Sales Office**

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**Electronic Contact:** 

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## Type 861Q Ductile iron slotted grate







#### **Product Features**

- Certified to EN 1433 Load Class E 135,000 lbs 2,788 psi
- · Uses 'QuickLok' boltless locking system
- Suitable for use with K300, KS300, H300K-13, and H300KS-13 channels and 621G, 621S, 631G, 631S catch basins
- Manufactured from ductile iron to ASTM A 536-84 Grade 65-45-12



#### **Specifications**

#### General

The surface drainage system shall be ACO Drain K300, KS300, H300K-13, and H300KS-13, channels\* and 621G, 621S, 631G, and 631S catch basins complete with ACO Type 861Q Ductile iron slotted grate with 'QuickLok' locking as manufactured by ACO Polymer Products, Inc. or similar approved.

#### Materials

The covers shall be manufactured from ductile iron and have  ${\it minimum}$  properties as follows:

- Independently certified to meet Load Class E to EN 1433 - 135,000 lbs - 2,788 psi
- Ductile iron to ASTM A 536-84 Grade 65-45-12
- Intake area of 128.71 sq. in. (803.39 cm²) per half meter of grate

The overall width of 13.31" (338mm) and overall length of 19.69" (500mm). Slots measure at a maximum of 5.71" (145mm).

#### Installation

The trench drain system and grates shall be installed in accordance with the manufacturer's installation instructions and recommendations.

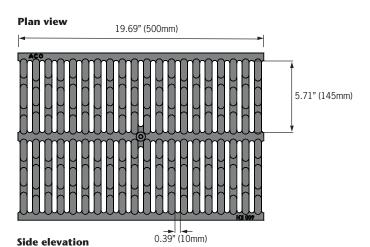
\* delete as appropriate



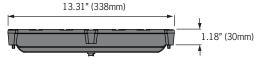




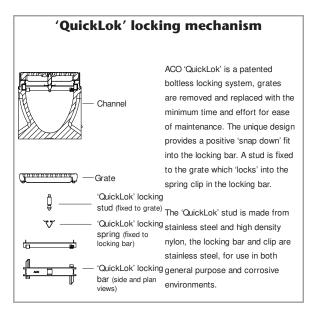








Description	Part No.	Length inches <i>(mm)</i>	Width inches (mm)	Weight lbs.
QuickLok grate Type 861Q Ductile iron slotted grate	10431	19.69 ( <i>500</i> )	13.35 (339)	48.0
QuickLok locking bar	10458	-	-	0.5
QuickLok grate removal tool	01318	-	-	0.3



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**Project Details** Date: 2020-08-13 : METRO GREENBANK Page: 1 of 5

Project Name Project Number : 920 558

Street Address, City

State zip code

Input Data

Location

Innut Data				
Eman	•			
Email				
Phone	•			
State zip code	:			
	•			
Street Address, City	:			
Contact Name	•			
Company	:			
Customer				

Number	Catchment Description	Area [m²]	С	D [min]	F [a]	l [mm/hr]	Catchment Surface Type	Installation
1	TD1	168.0	0.90	0	0	150	Asphalt	E600
2	TD2	336.0	0.90	0	0	150	Asphalt	E600

Channel type	Catchment (s)	Catchment Area [m²]	Cm	Total run length [m]	Application
TD1	1	168.00	0.90	6.50	
TD2	2	336.00	0.90	13.50	
_					

**Notes** 

Prepared By: KYLE ZHENG ACO SYSTEMS LTD. Phone

: 905-829-0665 1-2880 BRIGHTON RD : KYLE.ZHENG@ACO.COM Email L6H5S3 OAKVILLE, ONTARIO Website : WWW.ACOCAN.CA

## **ACO Technical Services**



**Project Details** Date: 2020-08-13 Page: 2 of 5

Project Name : METRO GREENBANK

Project Number : 920 558 Street Address, City State zip code

Input

Channel type : TD1 Trench drain system : K100

Sloping, Neutral or Combination layout

Roughness Coefficient (Strickler) inverse Mannings: 95 Invert Type

: Channel Slope Type of Outlet : sump unit-DN/OD200

Run Length : 6.50 [m] Catchment Area [m<sup>2</sup>] : 168 **Runoff Coefficient** [Cm] : 0.90

Hydraulic run length [m] : 6.50

All run segments combine to give the total run lenth.

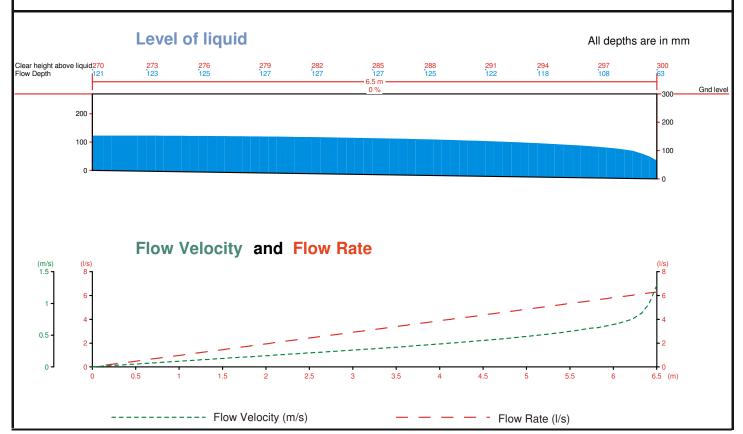
Section		1	2	3	4	5	6	7	8	9	10
Internal Width	[mm]	98									
Upstream Invert	[mm]	270									
Downstream Invert	[mm]	300									
Run Length	[m]	7									
Groundslope	[%]	0.000									

#### Results

Discharge [l/s] : 6.30 Flow Velocity [m/s]: 1.28

: 149.08, X = 0.00 mMinimum Freeboard [mm] (Freeboard Depth)

**Drain Capacity Utilised** : 32.21 [%]





**ACO Technical Services** 

**Project Details** Date: 2020-08-13 Project Name : METRO GREENBANK Page: 3 of 5

Project Number : 920 558

Street Address, City

State zip code

Channel type : TD1 Trench drain system : K100

Sloping, Neutral or Combination layout

Type of Outlet : sump unit-DN/OD200

Run Length [m] : 6.50 Hydraulic run length : 6.50 [m]

Notes	3
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#### Installation

**Legend**LC = Load Class according to EN1433 (A15; B125; C250; D400; E600; F900)

SU = Catch Basin

AU = Access Unit

VO = Vertical Outlet

FO = Free Outflow EO = End Outlet LO = Lateral Outlet

A = Adapter

## **ACO Technical Services**



**Project Details** Date: 2020-08-13 Page: 4 of 5

Project Name : METRO GREENBANK

Project Number : 920 558 Street Address, City State zip code

Input

Channel type : TD2 : K100 Trench drain system

Sloping, Neutral or Combination layout

Roughness Coefficient (Strickler) inverse Mannings: 95

Invert Type : Channel Slope Type of Outlet : sump unit-DN/OD200

Run Length : 13.50 [m] Catchment Area [m<sup>2</sup>] : 336 **Runoff Coefficient** [Cm] : 0.90

Hydraulic run length [m] : 13.50

All run segments combine to give the total run lenth.

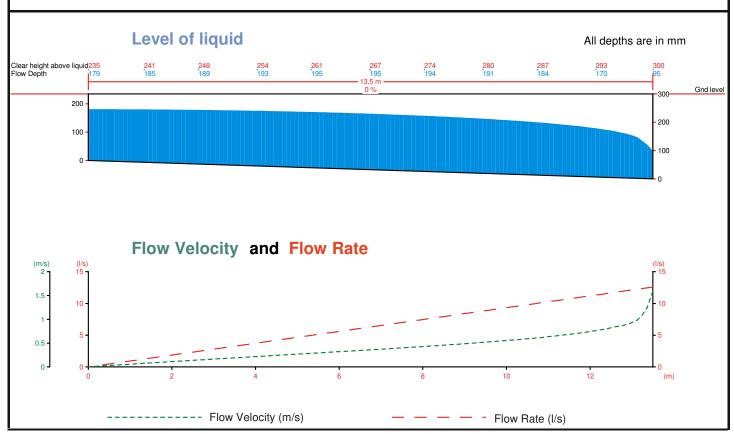
Section		1	2	3	4	5	6	7	8	9	10
Internal Width	[mm]	98									
Upstream Invert	[mm]	235									
Downstream Invert	[mm]	300									
Run Length	[m]	14									
Groundslope	[%]	0.000									

#### Results

Discharge [l/s] : 12.60 Flow Velocity [m/s]

Minimum Freeboard [mm] : 56.29, X = 0.00 m (Freeboard Depth)

**Drain Capacity Utilised** [%] : 71.30



## Trench Hydraulic Calculation for ACO Drainage Systems **ACO Technical Services**



Page: 5 of 5

**Project Details** Date: 2020-08-13

Project Name : METRO GREENBANK : 920 558

Project Number Street Address, City

State zip code

Channel type : TD2 Trench drain system : K100 Sloping, Neutral or Combination layout

Type of Outlet : sump unit-DN/OD200

Run Length [m] : 13.50 Hydraulic run length : 13.50 [m]

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#### Installation

**Legend**LC = Load Class according to EN1433 (A15; B125; C250; D400; E600; F900)

SU = Catch Basin

AU = Access Unit

VO = Vertical Outlet

FO = Free Outflow EO = End Outlet LO = Lateral Outlet

A = Adapter

#### ACO KlassikDrain - K100 w/ 461Q - Specifications:

#### General

The surface drainage system shall be ACO KlassikDrain K100 complete with Type 461Q class "E" slotted ductile Iron gratings secured with 'QuickLok' boltless locking mechanism as manufactured by ACO Systems Ltd. For technical assistance or supply information, please contact ACO Canada (905)-829-0665 or info@acocan.ca.

#### Materials

The trench system bodies shall be manufactured from polymer concrete with minimum properties as follows:

Compressive strength: 14,000 psi Flexural strength: 4,000 psi Water absorption 0.07% Frost proof Salt proof Dilute acid and alkali resistant

The nominal clear opening shall be 4.00" (100mm) with overall width of 5.12" (130mm). Pre-cast units shall be manufactured with either an invert slope of 0.5% or with neutral invert and have a wall thickness of at least 0.50" (13mm). Each unit will feature a partial radius in the trench bottom and a male to female interconnecting end profile. Units shall have horizontal cast in anchoring features on the outside wall to ensure maximum mechanical bond to the surrounding bedding material and pavement surface. The galvanized steel edge rail will be integrally cast in by the manufacturer to ensure maximum homogeneity between polymer concrete body and edge rail. Each edge rail shall be at least 3/32" (2.5mm) thick.

#### **Grates**

The grates shall be Type 461 slotted ductile iron with 'QuickLok' boltless locking mechanism as manufactured by ACO Systems Ltd. After removal of the grates and 'QuickLok' bar there shall be uninterrupted access to the trench to aid in maintenance.

#### Materials

The grates shall be manufactured from ductile iron and have **minimum** properties as follows;

- Independently certified to meet Load Class E to DIN 19580 135,000 lbs 2,788 psi.
- Ductile iron to ASTM A 536-84 Grade 65-45-12.
- Intake area of 20.79 sq. in. (134.13cm²) per half meter of grate.

The overall width of 4.84" (123mm) and overall length of 19.69" (500mm). Slots measure 3.94" (100mm) by 0.39" (10mm) per half meter of grate.

#### Installation

The trench drain system shall be installed in accordance with the manufacturer's installation instructions and recommendations.

#### 2.2 Findings of the Functional Servicing and Stormwater Management Report

The *Functional Servicing and Stormwater Management Report* (DSEL, December 2016) established the stormwater control criteria, the pond location and the general stormwater management scheme.

The proposed stormwater management facility is to be designed with the following characteristics:

- ➤ **Water Quality Control:** The permanent pool should be sized for an enhanced level of protection. A 40 m³/ha active volume portion for water quality control should be provided in accordance with the **SWMP Design Manual**.
- A sediment forebay shall be provided.
- Emergency overflow conveyance will be provided to safely pass emergency flows.

A summary of the required SWM pond characteristics is provided in Table 1.

#### 3.0 DRAINAGE ANALYSIS

The pond design characteristics and requirements, based on a 123.414 ha total drainage area to the pond (121.656 ha contributing minor system flows requiring quality control treatment), as shown in *Figure 2*, are summarized in *Table 1* as follows:

Table 1
SWM Pond Design Characteristics

Item	Target	Comments
Drainage Area	123.414 ha total; 121.656 ha minor flows	121.121 ha future development, 0.535 ha existing Half Moon Bay park block, 1.758 ha major flows only from existing Half Moon Bay subdivision
Imperviousness	67%	
Required Permanent Pool Volume	21,655 m <sup>3</sup>	Based on 178.00 m <sup>3</sup> /ha <sup>(1)</sup>
Required Quality Control Volume	4,866 m <sup>3</sup>	40 m <sup>3</sup> /ha
Allowable Release Rate for Quality Control	141 L/s	Minimum extended detention time between 24 to 48 hours (2)

<sup>(1)</sup> Note: Interpolated for 67% imperviousness, enhanced protection level for wet pond, as per Table 3.2 of the SWM Planning and Design Manual. Refer to Tables B-1 and B-2 of *Appendix B*.

Furthermore, the detailed design of the facility has been completed in general conformance with the **SWMP Design Manual**.

<sup>(2)</sup> Refer to Tables B-3 and B-4 of *Appendix B*.

