

Stormwater Management and Servicing Report

Apartment Building 161 Hinchey Avenue Ottawa, Ontario

Prepared for:

Praveen Muppalla. 450 Creekview Way Ottawa, ON, K1Y 1L5

Attention: Mr. Praveen Muppalla

LRL File No.: 200295 Revision 1 – September 29st, 2020

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1 Introduction and Site Description

LRL Associates Ltd. was retained by Praveen Muppalla to complete a Stormwater Management Analysis and Servicing Brief for a proposed four (4) storey residential building located at 161 Hinchey Avenue in Ottawa, Ontario. The property is legally described as Lot 9, Registered Plan 35, Concession 1, City Ward 15 (Kitchissippi) and is zoned R4S. The location of the proposed development can be viewed in **Figure 1** below.



Figure 1: Arial View of Proposed Development

The site to be developed is rectangular shape with a frontage of approximately 15 m along Hinchey Avenue and a depth of approximately 30 m, and a surface area of approximately **0.046** ha.

The topographic survey of the property was completed by Annis, O'Sullivan, Vollebekk Ltd. (Ontario Land Surveyors). Two site benchmarks were established during the survey for future construction use. These benchmarks, cross-cut on sidewalk along Hinchey Avenue with elevation 63.51 (benchmark No. 1) and 63.75 (benchmark No.2), are shown on the *Legal Survey* included in *Drawings/Figures*.

The development proposes a new four (4) storey residential building consisting of 15 units. Vehicular parking is not proposed on site, however provision for bicycle parking (8 spaces bicycle

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storage room) is proposed. For additional information, refer to a copy of the **Site Plan (SP-01)** included in **Drawings/Figures**.

This report has been prepared in consideration of the terms and conditions noted above and with the civil drawings prepared for the new development. Should there be any changes in the design features, which may relate to the stormwater considerations, LRL Associates Ltd. should be advised to review the report recommendations.

2 EXISTING SITE AND DRAINAGE DESCRIPTION

The subject site measures **0.046** ha and currently consists of a single 2-storey residential building and a paved driveway. Elevations of existing site range between 63.99 m at northeast corner to 63.59 m at the west side of the site.

Sewer and watermain mapping, along with as-built information collected from the City of Ottawa indicate the following existing infrastructure located within the adjacent right-of-way:

Hinchey Avenue:

- 150 mm diameter PVC watermain
- 250 mm diameter PVC sanitary sewer
- 375 mm diameter PVC storm sewer

3 SCOPE OF WORK

As per applicable guidelines, the scope of work includes the following:

Stormwater management

- Calculate the allowable stormwater release rate.
- Calculate the anticipated post-development stormwater release rates.
- Demonstrate how the target quantity objectives will be achieved.

Water services

- Calculate the expected water supply demand at average and peak conditions.
- Calculate the required fire flow as per the Fire Underwriters Survey (FUS) method.
- Confirm the adequacy of water supply and pressure during peak flow and fire flow.
- Describe the proposed water distribution network and connection to the existing system.

Sanitary services

- Describe the existing sanitary sewers available to receive wastewater from the building.
- Calculate peak flow rates from the development.
- Describe the proposed sanitary sewer system.
- Review impact of increased sanitary flow on downstream sanitary sewer.

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4 REGULATORY APPROVALS

An MECP Environmental Compliance Approval is not expected to be required for installation of the proposed storm and sanitary sewers within the site. A Permit to Take Water is not anticipated to be required for pumping requirements for sewer installation. The Rideau Valley Conservation Authority will need to be consulted in order to obtain municipal approval for site development. No other approval requirements from other regulatory agencies are anticipated.

5 WATER SUPPLY AND FIRE PROTECTION

5.1 Existing Water Supply Services and Fire Hydrant Coverage

The subject property lies within the City of Ottawa 1W water distribution network pressure zone. The subject property is located to the east of an existing 150 mm dia. watermain along Hinchey Avenue. There are currently three (3) existing fire hydrants near the property; one within 75m and two within 150 m from proposed building entrance. Refer to *Appendix B* for the location of fire hydrants.

5.2 Water Supply Servicing Design

The subject property is proposed to be serviced via a 150 mm diameter service lateral connected to the 150 mm watermain located within Hinchey Avenue. Refer to Site Servicing Plan C.401 in *Appendix E* for servicing layout.

Table 1 summarizes the City of Ottawa Design Guidelines design parameters employed in the preparation of the water demand estimate.

Table 1: City of Ottawa Design Guidelines Design Parameters

| Design Parameter | Value |
|--|---|
| Residential Bachelor / 1 Bedroom Apartment | 1.4 P/unit |
| Residential 2 Bedroom Apartment | 2.1 P/unit |
| Average Daily Demand | 280 L/d/per |
| Minimum Depth of Cover | 2.4 m from top of watermain to finished grade |
| Desired operating pressure range during normal | 350 kPa and 480 kPa |
| operating conditions | |
| During normal operating conditions pressure must | 275 kPa |
| not drop below | |
| During normal operating conditions pressure shall | 552 kPa |
| not exceed | |
| During fire flow operating conditions pressure must | 140 kPa |
| not drop below | |
| *Table updated to reflect technical Bulletin ISDTB-2018-02 | |

The interior layout and architectural floor plans have been reviewed, and it was determined that the building will house nine (9) studio/1-bedroom apartments, and six (6) 2-bedroom units. Based on the City of Ottawa Design guidelines for population projection, this translates to approximately

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approximately 25.2 residents. Table 2 below summarizes the proposed development as interpreted using table 4.1 of the City of Ottawa Design Guidelines.

Table 2: Development Residential Population Estimate

| Proposed Unit type | Persons Per Unit | Number of Units | Population |
|---------------------|---------------------|---------------------------------|------------|
| Studio/1 Bedroom | 1.4 | 9 | 12.6 |
| 2 Bedroom Apartment | 2.1 | 6 | 12.6 |
| | | Total Residential Population | 25.2 |

The required water supply requirements for the residential units in proposed building have been calculated using the following formula:

Where:

$$Q = (q \times P \times M)$$

q = average water consumption (L/capita/day)

P = design population (capita)

M = Peak factor

Using a calculated Maximum Day Factor and Peak Hour factor of 10.3 and 15.5 respectively as per Table 3-3 in the MOE Design Guidelines, anticipated demands were calculated as follows:

- Average daily domestic water demand is 0.08 L/s,
- Maximum daily demand is 0.84 L/s, and
- Maximum hourly demand is 13.06 L/s.

Based on maximum hourly rate of 13.06 L/s a minimum of 100 mm dia. servicing is required. However, assuming the presence of sprinklers, it is recommended to upsize the water servicing to 150 mm. Refer to *Appendix B* for water demand calculations.

The City of Ottawa was contacted to obtain boundary conditions associated with the estimated water demand, as indicated in the boundary request correspondence included in *Appendix B*. Table 3 below summarizes boundary conditions for the proposed development.

Table 3: Summary of Anticipated Demands and Boundary Conditions

| Design Parameter | Anticipated Demand (L/min) | Boundary Conditions @ Hinchey Avenue* (m H2O / kPa) | | |
|-------------------------------|-------------------------------|---|--|--|
| Average Daily Demand | 4.9 | 115.2 / 505.2 | | |
| Max Day + Fire Flow (per FUS) | 50.5 + 9,000 | 93.0 / 287.6 | | |
| Peak Hour | 783.8 | 106.5 / 419.9 | | |

*Assumed Ground elevation at connection point = 63.65 m.

Water demand calculation per City of Ottawa Water Design guidelines. See Appendix B for details.

Calculated average day demand has increased by 0.02 L/s since boundary conditions were requested. As indicated in Table 3, pressures in all scenarios meet the required pressure range stated in Table 1 as per City of Ottawa Design Guidelines. Refer to *Appendix B* for Boundary Conditions.

The estimated fire flow for the proposed buildings was calculated in accordance with *ISTB-2018-02*. The following parameters were provided by the Architect.

- Type of construction Wood Frame Construction;
- Occupancy type Limited Combustibility; and
- Sprinkler Protection Standard Sprinkler System.

The estimated fire flow demand was estimated to be **9,000 L/min**, see **Appendix B** for details.

There are three (3) existing fire hydrants in close proximity to the proposed buildings that are available to provide the required fire flow demands of 9,000 L/min. Refer to *Appendix B* for fire hydrant locations. Table 4 below summarizes the aggregate fire flow of the contributing hydrants in close proximity to the proposed development based on Table 18.5.4.3 of *ISTB-2018-02*.

Table 4: Fire Protection Summary Table

| Building | Fire Flow | Fire | Fire | Available |
|-------------------------------|-----------|-------------|-------------|--|
| | Demand | Hydrants(s) | Hydrant(s) | Combined Fire |
| | (L/min) | within 75m | within 150m | Flow (L/min) |
| Proposed 4 Storey Building | 9,000 | 1 | 2 | (1 x 5678) + (2 x 3785) = 13,248 |

The total available fire flow from contributing hydrants is equal to **13,248 L/min** which is sufficient to provide adequate fire flow for the proposed development. A certified fire protection system specialist will need to be employed to design the building's fire suppression system and confirm the actual fire flow demand.

The proposed water supply design conforms to all relevant City Guidelines and Policies.

6 SANITARY SERVICE

6.1 Existing Sanitary Sewer Services

There is an existing 250 mm dia. sanitary sewer within Hinchey Avenue across the subject site. The wastewater flow is ultimately conveyed to the West Nepean Collector trunk sewer.

The pre-development conditions of the lot were reviewed to calculate a total wet wastewater flow of **0.09 L/s** based on assumed conditions of 2 semi-detached residential dwellings.

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The post development total flow was calculated to be is **0.30** L/s as a result of proposed residential population and a small portion of infiltration. Refer to *Appendix C* for further information on the calculated sanitary flows. The post development conditions increase existing wastewater flow by approximately **0.21** L/s as a result of additional residential population from pre-development conditions.

Based on existing as-built, refer to *Drawings/Figures* for as-built information, the existing 250mm dia. sanitary sewer within Hinchey Avenue is sloped at 0.70% and is calculated to have a maximum capacity of **49.75** L/s. The proposed increase in total wastewater flow of **0.21** L/s represents less than 1% of existing maximum capacity. Therefore, it is anticipated that the existing local sewer network has sufficient capacity to accommodate the proposed development.

6.2 Sanitary Sewer Servicing Design

The proposed development will be serviced via a 150 mm dia. sanitary service lateral which will connect to the existing 250mm dia. sanitary sewer located within Hinchey Avenue. Refer to LRL drawing C.401 for the proposed sanitary servicing.

The parameters used to calculate the anticipated sanitary flows are:; residential average population per unit of 1.4 person for single units and 2.1 persons for two-bedroom units, a residential daily demand of 280 L/p/day, a residential peaking factor of 4.0 and a total infiltration rate of 0.33 L/s/ha. Based on these parameters and the total site area of 0.046 ha, the total anticipated sanitary flow was estimated to **0.30 L/s**. Refer to **Appendix C** for the site sanitary sewer design sheet.

7 STORMWATER MANAGEMENT

7.1 Existing Stormwater Infrastructure

Stormwater runoff from the subject property is tributary to the City of Ottawa sewer system as such, approvals for the proposed development within this area are under the approval authority of the City of Ottawa.

In pre-development conditions, the stormwater runoff would flow uncontrolled overland to the west side of the site towards Hinchey Ave. right-of-way. There is an existing 375 mm diameter storm sewer within Hinchey Avenue right-of-way. Refer to *Appendix D* for pre- and post-development watershed information.

7.2 Design Criteria

The stormwater management criteria for this development are based on the pre-consultation with City of Ottawa officials, the City of Ottawa Sewer Design Guidelines including City of Ottawa Stormwater Management Design Guidelines, 2012 (City standards), as well as the Ministry of the Environment's Stormwater Planning and Design Manual, 2003 (SWMP Manual).

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7.2.1 Water Quality

The subject property lies within the Ottawa River West sub-watershed and is therefore subject to review by the Rideau Valley Conservation Authority (RVCA). It was determined that no further treatment is required for stormwater runoff from the proposed development. Correspondence with RVCA is included in *Appendix A*.

7.2.2 Water Quantity

Based on pre-consultation with the City, correspondence included in *Appendix A*, the following stormwater management requirements were identified for the subject site:

- ➤ Meet an allowable release rate based on the existing Rational Method Coefficient no greater than 0.50, employing the City of Ottawa IDF parameters for a 5-year storm with a calculated time of concentration equal to or greater than 10 minutes;
- Attenuate all storms up to and including the City of Ottawa 100-year storm event on site; and

The allowable release rate for the subject site was calculated to be **6.63 L/s**. Refer to *Appendix* **D** for calculations.

7.3 Method of Analysis

The Modified Rational Method has been used to calculate the runoff rate from the site to quantify the detention storage required for quantity control of the development. Refer to *Appendix D* for storage calculations.

7.4 Proposed Stormwater Quantity Controls

The proposed stormwater management quantity control for this development will be accomplished using a flow restrictor in the storm sewer, as well as roof drains restricting the flow leaving the rooftop. Storage required as a result of quantity control will be accomplished through a combination of rooftop storage and super-size pipe storage in the rear yard.

The subject site is proposed to be serviced via a 300 mm diameter perforated subdrain and 250 mm diameter storm sewers that outlet to the existing 375 mm diameter storm sewer within Hinchey Avenue. The proposed site storm sewer and stormwater management system are shown on drawing C.401 and detailed calculations, including the design sheet, can be found in *Appendix D*.

The existing site is delineated by catchments EWS-01 which currently drains uncontrolled towards the front of the property.

The site has been analyzed and post development watersheds have been allocated. Watershed WS-01 (0.005ha), consisting of grass and pavers, will flow uncontrolled. The runoff will be conveyed to the Hinchey Avenue right-of-way, as per the grading plan C301.

Overland flow within watershed WS-03 (0.018ha) will be captured by CBMH01. An IPEX Tempest LMF 45mm diameter ICD is proposed at CBMH01 to restricted collected runoff. Grading proposed

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will provide positive overland drainage to the proposed storm water collection and control systems.

Runoff from the roof, delineated by Watershed WS-02 (0.023ha), will be captured by the proposed roof drains. Stormwater captured on the rooftop will be controlled by the roof drains, and conveyed to the storm sewer network, downstream of the ICD.

Table 5 below summarizes post-development drainage areas. Calculations can be seen in *Appendix D*.

Table 5: Drainage Areas

| Drainage Area Name | Area | Weighted Runoff Coefficient | 100 Year Weighted Runoff Coefficient (25% increase) |
|----------------------|-------|--------------------------------|---|
| WS-01 (uncontrolled) | 0.005 | 0.73 | 0.91 |
| WS-02 (controlled) | 0.023 | 0.90 | 1.0 |
| WS-03 (controlled) | 0.018 | 0.57 | 0.71 |

Rooftop detention of stormwater is provided with outlet control through two (2) proposed roof drains. The building's rooftop was analysed and divided into two (2) ponding areas. A total of two (2) roof drains, each of which is restricting the discharge rate to **0.95** L/s, resulting in a total release rate from the roof of **1.90** L/s is proposed. The roof drain flow control device has been selected to provide a flow rate of **0.95** L/s at a maximum flow depth of **0.15** m. Proposed roof drains are to be Watts RD-100-A with a ¼ exposed weir opening. See *Appendix D* for more information about the selected roof drain and flow restrictor.

The total available roof storage (m^3) has been calculated using the following formula:

$$V = \left(\frac{D_{Sl} * A_{Eff}}{3}\right)$$

Where:

V = available (provided) rooftop storage (m^3)

 D_{Sl} = slope ponding depth (m)

 A_{Eff} = effective roof area (m^2)

Based on the equation above, it was calculated that 9.00 m^3 of rooftop storage is available in the 100-year event. For additional details on the calculations for available area of rooftop storage, refer to *Appendix D*.

All overland stormwater captured will ultimately be conveyed, via underground storm sewers, to

the City storm sewer running along 161 Hinchey Avenue at a maximum release rate of **6.63 L/s** (calculated controlled and uncontrolled flow).

Table 6 below summarize the release rates and storage volumes required to meet the allowable release rate of **6.63 L/s** for 100-year flow rates.

Table 6: Stormwater Release Rate & Storage Volume Summary (100 Year)

| Catchment Area | Drainage Area (ha) | 100-year Release Rate (L/s) | 100-Year Required Storage (m³) | Total Available Storage (m³) |
|-------------------------|--------------------------|-----------------------------------|--------------------------------------|------------------------------------|
| WS-01 (Un-controlled) | 0.005 | 2.40 | 0 | 0 |
| WS-02 (Roof Controlled) | 0.023 | 1.90 | 6.92 | 9.00 |
| WS-03 (Controlled) | 0.018 | 2.34 | 2.45 | 3.20 |
| TOTAL | 0.046 | 6.63 | 9.37 | 12.20 |

It is calculated that a total of **9.37 m³** of storage will be required to attenuate flows to the allowable release rate of **6.63 L/s**. The project runoff exceeding the allowable release rate will be stored on-site via rooftop ponding at the building rooftop and underground pipe storage. The 100-year maximum ponding depths can be found on drawing "C601 – Stormwater Management Plan" of *Appendix E*.

8 EROSION AND SEDIMENT CONTROL

During construction, erosion and sediment controls will be provided primarily via a sediment control fence to be erected along the perimeter of the site where runoff has the potential of leaving the site. Inlet sediment control devices are also to be provided in any catch basin and/or manholes in and around the site that may be impacted by the site construction. Construction and maintenance requirements for erosion and sediment controls are to comply with Ontario Provincial Standard Specification OPSS 577. Refer to LRL Associates drawing C.101 for erosion and sediment control details.

9 Conclusion

This Stormwater Management and Servicing Report for the development proposed at 161 Hinchey Avenue presents the rationale and details for the servicing requirements for the subject property.

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In accordance with the report objectives, the servicing requirements for the development are summarized below:

Water Service

- The maximum required fire flow was calculated at **9,000.0 L/min** using the FUS method.
- There are three (3) existing fire hydrants available to service the proposed development. They will provide a combined fire flow of **13,248 L/min** to the site.
- The new development/expansion will be serviced with a new 150 mmΦ water service to be connected to the existing 150mmΦ watermain within Hinchey Avenue.
- Boundary conditions received from the City of Ottawa indicate that sufficient pressure is available to service the proposed site.

Sanitary Service

- The anticipated sanitary flow from the proposed development is 0.30 L/s.
- The proposed development will be serviced by a 150 mm diameter sanitary service that connects to the existing 250mm dia. sanitary sewer within Hinchey Avenue.

Stormwater Management

- Stormwater quality control is not required as per consultation with RVCA.
- The storm water release rates from the proposed development will meet calculated allowable release rate of **6.63 L/s**.
- Stormwater quantity control objectives will be met through on-site storm water ponding on the roof and sub-surface storage.

10 REPORT CONDITIONS AND LIMITATIONS

The report conclusions are applicable only to this specific project described in the preceding pages. Any changes, modifications or additions will require a subsequent review by LRL Associates Ltd. to ensure the compatibility with the recommendations contained in this document. If you have any questions or comments, please contact the undersigned.

Prepared by:

LRL Associates Ltd.



Mohan Basnet, P. Eng. Civil Engineer

Jem Salema

Amr Salem Civil Designer

APPENDIX A

Pre-consultation / Correspondence

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161 Hinchey Avenue - Infrastructure Notes

Available Infrastructure:

Sanitary: 250mm PVC (Install 2000) Storm: 375mm Conc (Install 2000) Water: 150mm PVC (Install 2000)

Water Boundary Conditions:

Will be provided at request of consultant. Requests must include the location of the service and the expected loads required by the proposed development. Please provide the following and <u>submit Fire Flow Calculation Sheet</u> per FUS method with the request:

- Location of service
- Type of development and amount of required fire flow (per FUS method <u>include FUS calculation sheet with request</u>)
- Average Daily Demand (I/s)
- Maximum Hourly Demand (I/s)
- Maximum Daily Demand (I/s)
- Water Supply Redundancy Fire Flow:
 Applicant to ensure that a second service with an inline valve chamber be provided where the average daily demand exceeds 50 m³ / day (0.5787 l/s per day)

Water services larger than 19 mm require a Water Data Card. Please complete card and submit.

Stormwater Management:

- Coefficient (C) of runoff determined as per existing conditions but in no case more than 0.5
- TC = To be calculated, minimum 10 minutes
- Any storm events greater than 5 year, up to 100 year, and including 100-year storm event must be detained on site.
- Foundation drains are to be independently connected to sewer main unless being pumped with appropriate back up power, sufficient sized pump and back flow prevention.
- Roof drains are to be connected downstream of any incorporated ICD within the SWM system.

Stormwater management criteria (Quality Control)

Include a section in the SWM report concerning quality control requirements. It is the consultant's responsibility to check with the relevant Conservation Authority for quality control issues and include this information in the SWM report.

Phase I and Phase II ESA:

- Phase I ESA is required; Phase II ESA may be required depending on the results of the Phase I ESA. Phase I ESA must include an EcoLog ERIS Report.
- Phase I ESA and Phase II ESAs must conform to clause 4.8.4 of the Official Plan that requires that development applications conform to Ontario Regulation 153/04.

Required Studies

- Stormwater Management Report
- Site Servicing Study
- Geotechnical Study
- Phase I ESA
- Phase II ESA (depends on outcome of Phase I)

Required Plans

- Site Servicing Plan
- Grade Control and Drainage Plan
- Erosion and Sediment Control Plan (Can be combined with grading plan)

Relevant information

- 1. The Servicing Study Guidelines for Development Applications are available at the following address: https://ottawa.ca/en/city-hall/planning-and-development/information-development-application-submission/guide-preparing-studies-and-plans#servicing-study-guidelines-development-applications
- 2. Servicing and site works shall be in accordance with the following documents:
 - ⇒ Ottawa Sewer Design Guidelines (October 2012)
 - Ottawa Design Guidelines Water Distribution (2010)
 - ⇒ Geotechnical Investigation and Reporting Guidelines for Development Applications in the City of Ottawa (2007)
 - ⇒ City of Ottawa Slope Stability Guidelines for Development Applications (revised 2012)
 - ⇒ City of Ottawa Environmental Noise Control Guidelines (January, 2016)
 - ⇒ City of Ottawa Park and Pathway Development Manual (2012)
 - ⇒ City of Ottawa Accessibility Design Standards (2012)

 - ⇒ Ontario Provincial Standards for Roads & Public Works (2013)
- 3. Record drawings and utility plans are also available for purchase from the City (Contact the City's Information Centre by email at lnformationCentre@ottawa.ca or by phone at (613) 580-2424 x.44455).
- 4. Any proposed work in utility easements requires written consent of easement owner.

Amr Salem

From: Jamie Batchelor < jamie.batchelor@rvca.ca>

Sent: July 9, 2020 11:40 AM

To: Amr Salem

Cc: Mohan Basnet; Maxime Longtin

Subject: RE: 161 Hinchey Avenue - Stormwater Quality Controls

Follow Up Flag: Follow up Flag Status: Flagged

Good Morning Amr,

Given that the site will have no surface parking areas proposed, no additional water quality control will be required save and except best management practices.

Jamie Batchelor, MCIP, RPP Planner, ext. 1191
Jamie.batchelor@rvca.ca



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From: Amr Salem <asalem@lrl.ca>
Sent: Monday, July 6, 2020 2:52 PM

To: Jamie Batchelor < jamie.batchelor@rvca.ca>

Cc: Mohan Basnet <mbasnet@lrl.ca>; Maxime Longtin <mlongtin@lrl.ca>

Subject: 161 Hinchey Avenue - Stormwater Quality Controls

Good morning Jamie,

I wanted to consult with you regarding a residential development we are working on located at 161 Hinchey Avenue.

Existing runoff from the site drains into municipal sewer along Hinchey Ave and travels approx. 610m before discharging into the Ottawa River.

The development proposes a residential 4-storey building, with <u>no surface parking</u>. The site will be landscape with stormwater coming primarily from rooftop and landscaped rear yard. *Refer to draft site plan attached for reference*.

Existing site area consists of an existing residential building and paved area.

Please provide your input about quality controls that may be required for this site.



Thank you,



Amr Salem

Civil Designer

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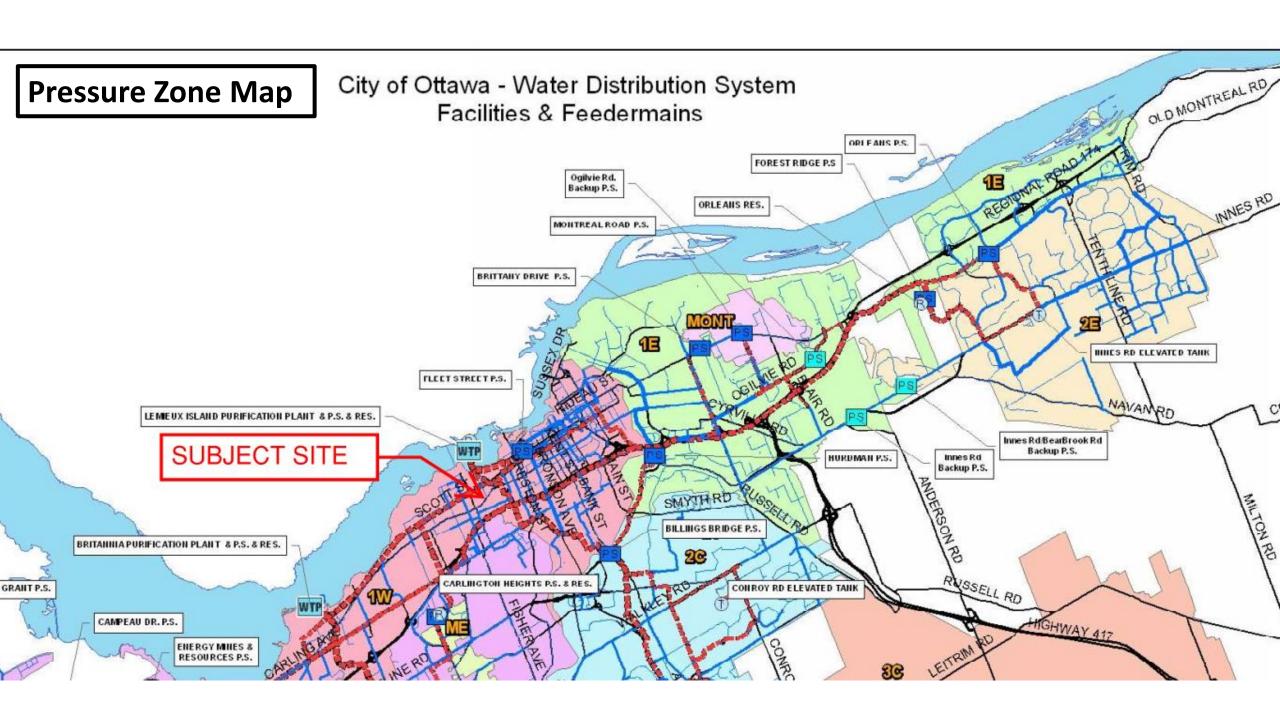
We care deeply, so let us know how we did by completing our <u>Customer Satisfaction Survey</u>.

Nous nous soucions profondément de votre opinion, nous vous invitons donc à nous faire savoir si nous avons satisfait vos attentes en remplissant notre <u>sondage sur la satisfaction de la clientèle</u>



APPENDIX B Water Supply Calculations







Water Supply Calculations

LRL File No. 200295

Date September 21, 2020

Prepared by Amr Salem

Residential Demand based on the City of Ottawa Design Guidelines-Water Distribution, 2010

| Unit Type | Persons Per Unit | Number of Units | Population |
|---------------------|------------------|-----------------|------------|
| 1 Bedroom Apartment | 1.4 | 9 | 12.6 |
| 2 Bedroom Apartment | 2.1 | 6 | 12.6 |
| | Total | 15 | 25.2 |

Average Water Consumption Rate 280 L/c/d

Average Day Demand 7,056 L/d 0.08 L/s Maximum Day Factor 10.3 (MOE Table 3-3) **Maximum Daily Demand** 72,654 L/d 0.84 L/s (MOE Table 3-3) Peak Hour Factor 15.5 **Maximum Hour Demand** 1,128,733 L/d 13.06 L/s

Water Service Pipe Sizing

Q = VA Where: V = velocity

A = area of pipe

Q = flow rate

Assuming a maximum velocity of 1.8m/s, the diameter of pipe is calculated as:

Minimum pipe diameter (d) = $(4Q/\pi V)^{1/2}$

= 0.096 m = 96 mm

Proposed pipe diameter (d) = 150 mm

= 6 Inches



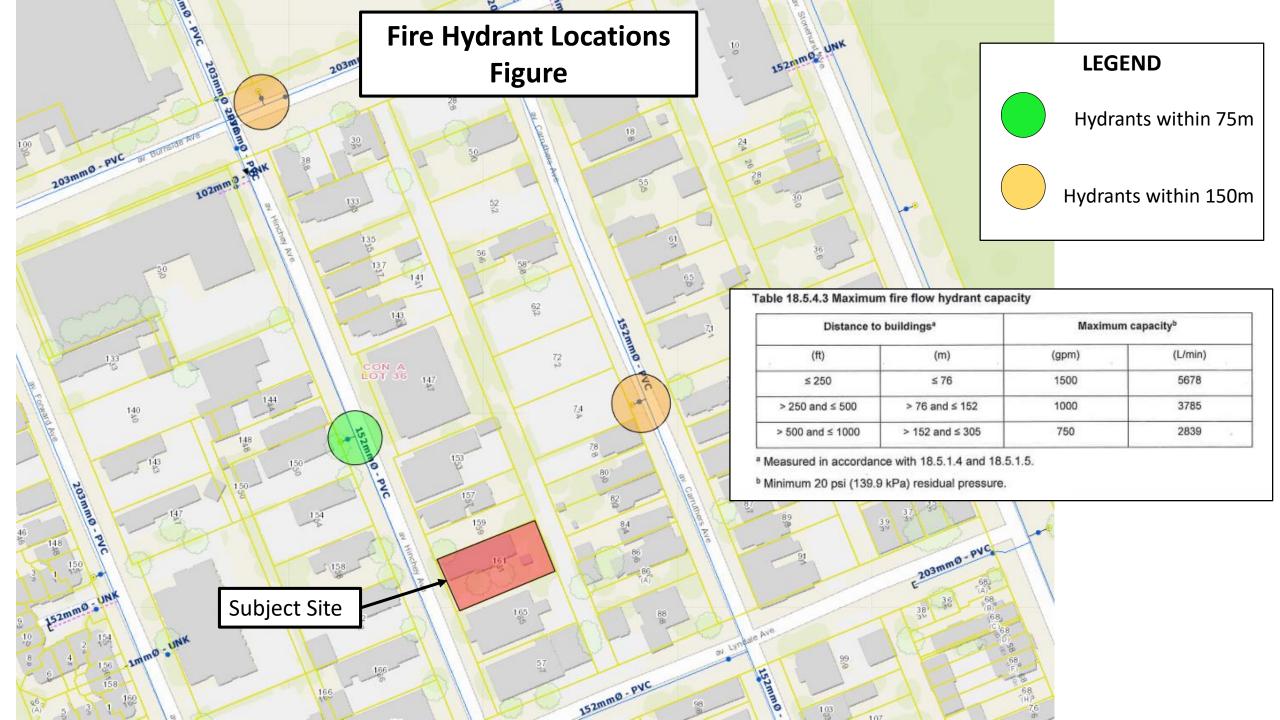
Fire Flow Calculations

LRL File No. 200295
Date July 14, 2020

Method Fire Underwriters Survey (FUS)

Prepared by Amr Salem

| Step | Task | Term | Options | Multiplier | Choose: | Value | Unit | Fire Flow |
|------------------------|--|---------------------------------|---|-----------------|---|-------------|----------------|-----------|
| | | | Structural Framing M | aterial | | | | |
| | Choose frame used for | | Wood Frame | 1.5 | | | | |
| | | Coefficient C | Ordinary Construction | 1.0 | | | | |
| 1 | building | related to the type of | Non-combustible construction | 0.8 | Ordinary Construction | 1 | | |
| | building | construction | Fire resistive construction <2 hrs | 0.7 | | | | |
| | | | Fire resistive construction >2 hrs | 0.6 | | | | |
| | | | Floor Space Area | (A) | | | | |
| 2 | | | Total area | | | 1,104 | m ² | |
| 3 | Obtain fire flow before reductions | Required fire flow | Fire I | Flow = 220 x C | x A ^{0.5} | | L/min | 7,310 |
| | | | Reductions or surcharge due to fact | ors affecting b | urning | | | |
| | Choose combustibility of contents | | Non-combustible | -25% | | | | |
| | | Occupancy hazard | Limited combustible | -15% | | | | |
| 4 | | , , , | Combustible | 0% | Limited combustible -1 | -15% | L/min | 6,213 |
| | | | Free burning | 15% | | | | |
| | | | Rapid burning | 25% | | | | |
| | | | Full automatic sprinklers | -30% | False | 0% | | |
| 5 | Choose reduction for sprinklers Sprinkler reduction | Sprinkler reduction | Water supply is standard for both the system and fire department hose lines | -10% | True | -10% | L/min | 5,592 |
| | | | Fully supervised system | -10% | False | 0% | | |
| | | | North side | 3.1 to 10m | 20% | | | |
| 6 | Chanca congration | Exposure distance | East side | 20.1 to 30m | 10% | | L/min | 9.227 |
| " | Choose separation | between units | South side | 3.1 to 10m | 20% | | | 9,221 |
| | | | West side | 10.1 to 20m | 15% | 65% | | |
| Net required fire flow | | | | | | | | |
| | Obtain fire flow, | | | Minimum | required fire flow rate (rounded to neare | est 1000) | L/min | 9,000 |
| 7 | duration, and volume | Minimum required tire flow rate | | | | | L/s | 150.0 |
| | , | | | | Required duration of | f fire flow | hr | 2 |



Amr Salem

From: Fawzi, Mohammed <mohammed.fawzi@ottawa.ca>

Sent: July 17, 2020 1:52 PM

To: Amr Salem
Cc: Mohan Basnet

Subject: RE: 200295 - 161 Hinchey Avenue Boundary Conditions Request

Attachments: 161 Hinchey July 2020.pdf

Follow Up Flag: Follow up Flag Status: Follow up

Good Afternoon Amr,

The following are boundary conditions, HGL, for hydraulic analysis at 161 Hinchey (zone 1W) assumed to be connected to the 152mm on Hinchey (see attached PDF for location).

Minimum HGL = 106.5m

Maximum HGL = 115.2m

MaxDay + FireFlow (150 L/s) = 93.0m

These are for current conditions and are based on computer model simulation.

Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation.

Thank you.

Best Regards,

Mohammed Fawzi, E.I.T.

Engineering Intern

Planning, Infrastructure and Economic Development Department - Services de la planification, de l'infrastructure et du développement économique

Development Review - Central Branch

City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1

613.580.2424 ext./poste 20120, Mohammed.Fawzi@ottawa.ca

From: Fawzi, Mohammed Sent: July 17, 2020 11:23 AM To: Amr Salem <asalem@lrl.ca>
Cc: Mohan Basnet <mbasnet@lrl.ca>

Subject: RE: 200295 - 161 Hinchey Avenue Boundary Conditions Request

Hi Amr,

Thank you. The request has been sent.

Best Regards,

Mohammed Fawzi, E.I.T.

Engineering Intern

Planning, Infrastructure and Economic Development Department - Services de la planification, de l'infrastructure et du développement économique

Development Review - Central Branch

City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1 613.580.2424 ext./poste 20120, Mohammed.Fawzi@ottawa.ca

From: Amr Salem <asalem@lrl.ca> Sent: July 15, 2020 1:36 PM

To: Fawzi, Mohammed < mohammed.fawzi@ottawa.ca>

Cc: Mohan Basnet <mbasnet@lrl.ca>

Subject: 200295 - 161 Hinchey Avenue Boundary Conditions Request

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ATTENTION : Ce courriel provient d'un expéditeur externe. Ne cliquez sur aucun lien et n'ouvrez pas de pièce jointe, excepté si vous connaissez l'expéditeur.

Good afternoon Mohammed,

We would like to kindly request boundary conditions for the proposed development at 161 Hinchey Avenue using the following proposed development demands:

- Location of Service / Street Number: 161 Hinchey Ave
- Type of development: one 4-storey residential building consisting of a total of 12 units.
- Proposed Connection Point: a single connection the 150mm watermain along Hinchey Avenue.



 Please provide pressures for the following water demand scenarios required for the proposed development:

| | L/min | L/s |
|---------------|--------------|------------|
| Avg. Daily | 3.6 | 0.06 |
| Max Day + FUS | 42.0 + 9,000 | 0.70 + 150 |
| Peak Hour | 747.0 | 12.45 |

Please contact me if you have any questions.



Thanks,

Amr Salem
Civil Designer
LRL Associates Ltd.
5430 Canotek Road
Ottawa, Ontario K1J 9G2

- T (613) 842-3434 or (877) 632-5664 ext 248
- **F** (613) 842-4338



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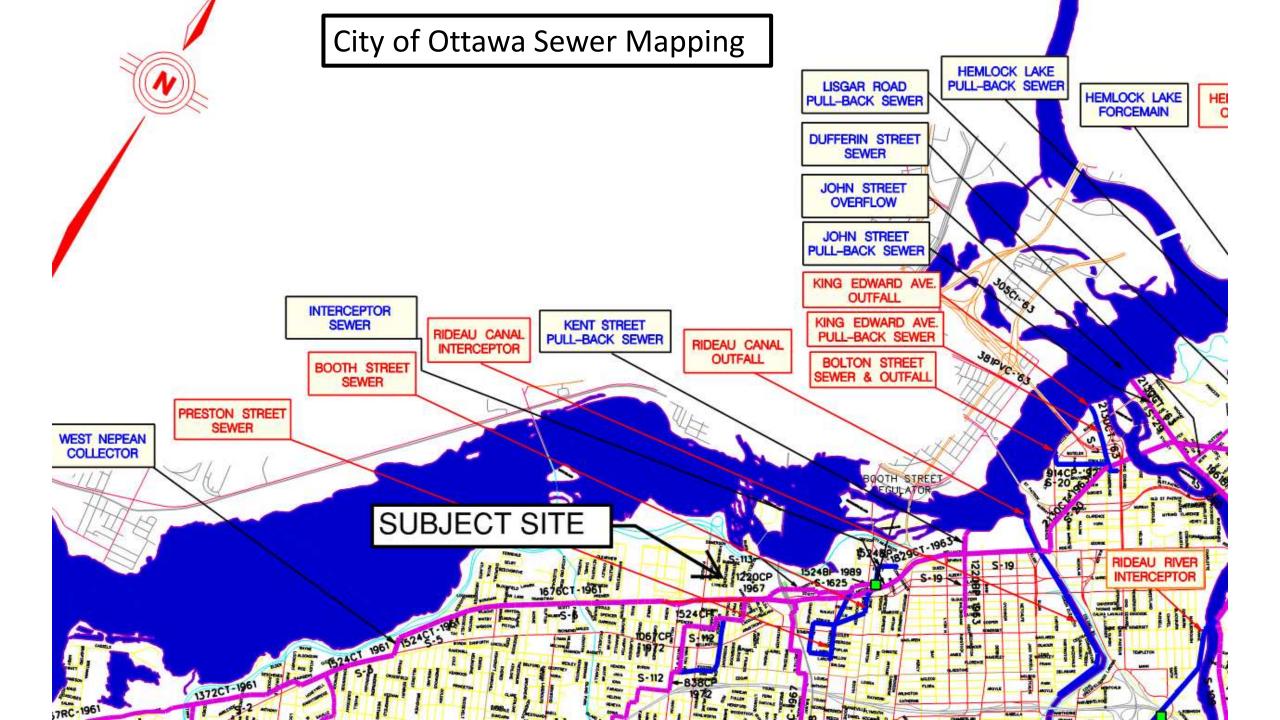
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4



APPENDIX C Wastewater Collection Calculations







LRL File No. 200295

Project: Apartment Building
Location: 161 Hinchey Avenue
Date: July 31, 2020

Sanitary Design Parameters

Industrial Peak Factor = as per Appendix 4-B = 7
Extraneous Flow = 0.33L/s/gross ha

Pipe Design Parameters

Minimum Velocity = 0.60 m/s Manning's n = 0.013

| | LOCATION | RESIDENTIAL AREA AND POPULATION COMMERCIAL INDUSTRIAL | | | | | TRIAL INSTITUTIONAL C+I+I | | | INFILTRATION | | | TOTAL | PIPE | | | | | | | | | | | | |
|--------|--|---|--------------|------|--------------|------|---------------------------|-----------------------|--------------|-----------------------|--------------|-----------------------|---------------|--------------|-----------------------|-----------------------|---------------------------|-----------------------|--------------------------|------|---------------|--------------|---------------------|----------|-------------------------|-------------------------|
| STREET | FROM MH | ТО МН | AREA (Ha) | POP. | AREA (Ha) | POP. | PEAK FACT. | PEAK FLOW (I/s) | AREA (Ha) | ACCU. AREA (Ha) | AREA (Ha) | ACCU. AREA (Ha) | PEAK FACT. | AREA (Ha) | ACCU. AREA (Ha) | PEAK FLOW (l/s) | TOTAL AREA (Ha) | ACCU. AREA (Ha) | INFILT. FLOW (I/s) | | LENGTH (m) | DIA. (mm) | SLOPE (%) | MATERIAL | CAP. (FULL) (l/s) | VEL. (FULL) (m/s) |
| SITE | PROP. BLDG | EX. SAN | 0.046 | 21.7 | 0.05 | 21.7 | 4.0 | 0.28 | 0.000 | 0.000 | 0.00 | 0.00 | 7.0 | 0.0 | 0.0 | 0.00 | 0.05 | 0.05 | 0.02 | 0.30 | 7.4 | 250 | 0.70% | PVC | 49.75 | 1.01 |
| NOTES | NOTES Existing inverts and slopes are estimated. They are to be confirmed on-site. | | | | | | | | | Designed | : A.S. | | | | | | | Apartme | OJECT: ent Building |) | | | | | | |
| | | | | | | | | | | | | | | Checked: | M.B. | | | | | | | | ATION: hey Avenu | e | | |
| | | | | | | | | | | | | | | Dwg. Ref | | | File Ref.: | | | | Date: | | | | | Shee |
| | | | | | | | | | | | | | | | C.401 | | 200295 July 24, 2020 1 of | | | | | | | | | |

Average Daily Flow = 280 L/p/day

Heavy Industrial Flow = 55000 L/ha/day

Maximum Residential Peak Factor = 4.0

Commercial & Institutional Peak Factor = 1.5

Commercial & Institutional Flow = 50000 L/ha/day Light Industrial Flow = 35000 L/ha/day

APPENDIX D

Stormwater Management Calculations LMF ICD Curves Watts Roof Drain Specification

5430 Canotek Road | Ottawa, ON, K1J 9G2 | info@Irl.ca | www.Irl.ca | (613) 842-3434

LRL Associates Ltd. Storm Watershed Summary



LRL File No. 200295

Project: Apartment Building
Location: 161 Hinchey Ave
Date: September 17, 2020

Designed: Amr Salem **Drawing Reference:** C701/C702

Pre-Development Catchments

| WATERSHED | C = 0.2 | C = 0.80 | C = 0.90 | Total Area (m²) | Total Area (ha) | Combined C |
|-----------|---------|----------|----------|-----------------|-----------------|------------|
| EWS-01 | 226.0 | 0.0 | 232.0 | 458.0 | 0.046 | 0.55 |
| TOTAL | 226.0 | 0.0 | 232.0 | 458.0 | 0.046 | 0.55 |

Post-Development Catchments

| WATERSHED | C = 0.20 | C = 0.80 | C = 0.90 | Total Area (m²) | Total Area (ha) | Combined C |
|---------------------|----------|----------|----------|-----------------|-----------------|------------|
| WS-01(UNCONTROLLED) | 13.0 | 0.0 | 40.0 | 53.0 | 0.005 | 0.73 |
| WS-02 (CONTROLLED) | 0.0 | 0.0 | 225.0 | 225.0 | 0.023 | 0.90 |
| WS-03 (CONTROLLED) | 86.0 | 0.0 | 94.0 | 180.0 | 0.018 | 0.57 |
| TOTAL | 99.0 | 0.0 | 359.0 | 458.0 | 0.0458 | 0.75 |



a = 998.071 b = 0.814 C = 6.053

a = 1735.688 b = 0.820 C = 6.014

 $\begin{aligned} &Q = 2.78CIA \left(L/a\right) \\ &C = Runoff coefficient \\ &I = Rainfal intensity (numbr) \\ &A = Rana \left(l/a\right) \\ &T_c = Time of concentration (min) \end{aligned}$

| Post-development Stormwai | Dat-Geveropment Scomward Management | | | | | | | | | | | | | |
|---------------------------|-------------------------------------|--------|----|------|------------|------------|--|--|--|--|--|--|--|--|
| | Total Site Area = | 0.0458 | ha | 5R= | ∑R 0.75 | ∑R 0.94 | | | | | | | | |
| | WS-02 (Roof) | 0.023 | ha | Be . | 0.90 | 1.00 | | | | | | | | |
| Controlled | WS-03 | 0.018 | ha | Re . | 0.57 | 0.71 | | | | | | | | |
| | Total Controlled = | 0.041 | ha | 5B= | 0.75 | 0.94 | | | | | | | | |
| Un-controlled | WS-01 | 0.005 | ha | Re . | 0.73 | 0.91 | | | | | | | | |
| On-controlled | Total Un-Controlled = | 0.005 | ha | 5R= | 0.73 | 0.91 | | | | | | | | |

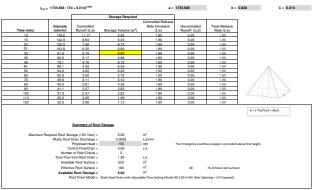
L_{vv} = 1735.588 / (Td + 6.014)⁶⁰⁰ a = 1735.588 b = 0.020 C = 6.014

| 1735.680 | To - 6.045| | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100

Total Storage Required = 2.45 m³ refer to LRL Plan C.601

Available Subsurface Storage = 3.20 m³ "Storage accounted for in superpipe and CMM**

Post-development Stormwater Management (WS-02 On Roof)



| Total Storage Required = | 6.92 m² | Available Roof Storage = | 9.00 m² | refer to LRL Plan C.601

| Catchment Area | Drainage Area (ha) | Rate (L/s) | 100-Year Required Storage (m3) | Storage (m3) |
|-----------------------|-----------------------|---------------|-----------------------------------|-----------------|
| WS-01 | 0.005 | 2.40 | 0 | 0 |
| WS-02 (Roof Controls) | 0.023 | 1.90 | 6.92 | 9.00 |
| WS-03 | 0.018 | 2.34 | 2.45 | 3.20 |
| TOTAL | 0.046 | 6.63 | 9.37 | 12.20 |

LRL Associates Ltd. Storm Design Sheet

LRJ

LRL File No. 200295

Project: Apartment Building
Location: 161 Hinchey Ave
Date: July 30, 2020
Designed: Amr Salem
Drawing Reference: C.401

Storm Design Parameters

Rational Method Q = 2.78CIA

Q = Peak flow in litres per second (L/s)
A = Drainage area in hectares (ha)
C = Runoff coefficient

I = Rainfall intensity (mm/hr)

Runoff Coefficient (C)

 Grass
 0.20

 Gravel
 0.80

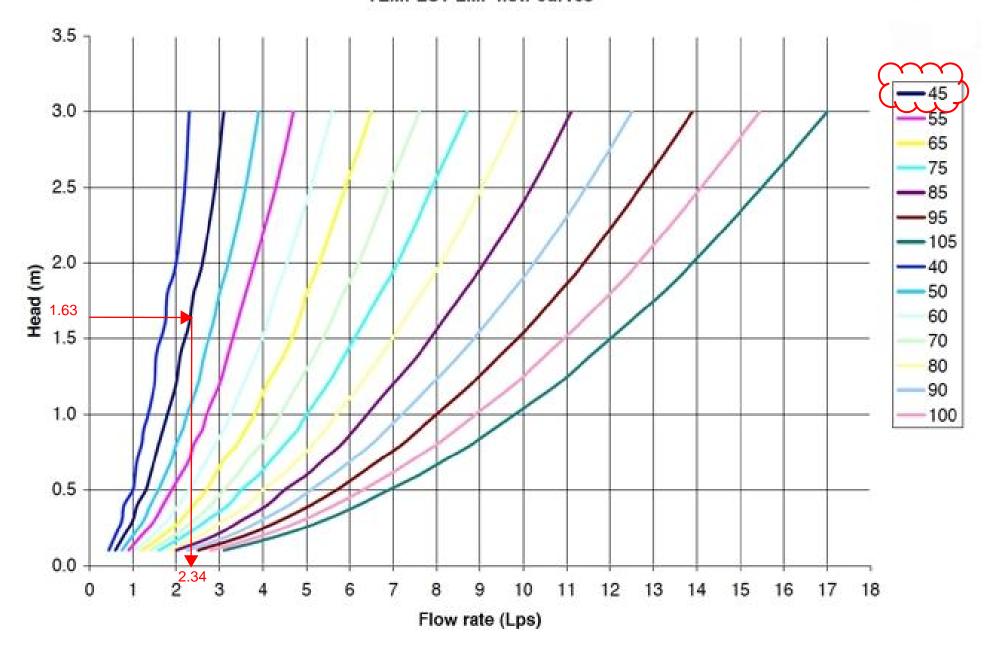
 Asphalt / rooftop
 0.90

Ottawa Macdonald-Cartier International Airport IDF curve equation (5 year event, intensity in mm/hr)

 $I = 998.071 / (T_c + 6.053)^{0.814}$ Min. velocity = 0.80 m/s Manning's "n" = 0.013

| LOCATION AREA (ha) | | | | | | | | | FLOW | | | STORM SEWER | | | | | | | |
|-----------------------|---------|---------|----------|----------|----------|------------------|------------------|----------------------------|----------------------------------|----------------------|-------------------------------|--------------------------|------|-----------|------------|------------------------|---------------------------|---------------------------|------------------------------|
| WATERSHED / STREET | From MH | То МН | C = 0.20 | C = 0.80 | C = 0.90 | Indiv. 2.78AC | Accum. 2.78AC | Time of Conc. (min.) | Rainfall Intensity (mm/hr) | Peak Flow Q (L/s) | Controlled Flow Q (L/s) | Pipe Diameter (mm) | Туре | Slope (%) | Length (m) | Capacity Full (L/s) | Velocity Full (m/s) | Time of Flow (min.) | Ratio (Q/Q _{FULL}) |
| WS-03 | CB | CBMH01 | 0.009 | 0.000 | 0.009 | 0.028 | 0.03 | 10.00 | 104.2 | 2.95 | 2.34 | 450 | HDPE | 0.50% | 8.6 | 201.6 | 1.27 | 0.11 | 0.01 |
| WS-02 - Roof Controls | CBMH01 | CBMH02 | 0.000 | 0.000 | 0.023 | 0.056 | 0.08 | 10.11 | 103.6 | 8.76 | 1.90 | 250 | PVC | 1.00% | 28.5 | 59.5 | 1.21 | 0.39 | 0.15 |
| | CBMH02 | EX. STM | 0.00 | 0.00 | 0.00 | 0.000 | 0.08 | 10.51 | 101.6 | 8.59 | 4.24 | 250 | PVC | 1.00% | 5.0 | 59.5 | 1.21 | 0.07 | 0.14 |
| | | | | · | | | | • | · | | • | • | • | | • | • | | | |

TEMPEST LMF flow curves





RD-100-A

Tag: _

Large Capacity Roof Drain

Components:



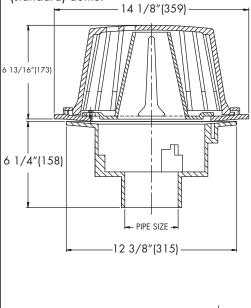


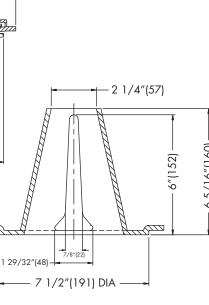




Order Code: RD-10 -A - - -

SPECIFICATION: Watts Drainage Products RD-100 epoxy coated cast iron roof drain with deep sump, wide serrated flashing flange, flashing clamp device with integral gravel stop, accutrol weir and self-locking polyethylene (standard) dome.





Free Area Sq. In.

Deck opening 10" (254) with sump receiver 13-1/4" (337)

** Side Outlet (-SO) option only available in 2"(51), 3"(76), 4"(102) pipe sizes. Underdeck Clamp (-BED and -D options) are not available when -SO is selected.

| Optional Body Material (NH Onl Suffix Description | | | | |
|--|-----|--------------------------|---|--|
| | -60 | PVC Body w/Socket Outlet | [| |
| | -61 | ARS Body w/Socket Outlet | | |

Ex. RD-102P-K
Pipe Sizing (Select On

| Pipe Sizing (Select One) | | | | | |
|--------------------------|-------------------|--|--|--|--|
| Suffix | Description | | | | |
| 2 | 2"(51) Pipe Size | | | | |
| 3 | 3"(76) Pipe Size | | | | |
| 4 | 4"(102) Pipe Size | | | | |
| 5 | 5"(127) Pipe Size | | | | |
| 6 | 6"(152) Pipe Size | | | | |
| 8 | 8"(203) Pipe Size | | | | |

| Oulier Type (Select Oile) | | | | |
|---------------------------|-----------------|--|--|--|
| Suffix | Description | | | |
| NH | NH No Hub (M) | | | |
| Р | Push On | | | |
| T | Threaded Outlet | | | |
| Χ | Inside Caulk | | | |

Outlet Type (Select One)

| Options (Select One or More) Suffix Description | | | | |
|---|--|--|--|--|
| -B | Sump Receiver Flange | | | |
| -BED | Sump Receiver, Adj Ext., Deck Clamp | | | |
| -C | Secondary Membrane Clamp | | | |
| -D | Underdeck Clamp | | | |
| -E | Adjustable Extension | | | |
| -GSS -H | Stainless Steel Ballast Guard Adj. to 6" IRMA Ballast Guard | | | |

| -K8U | Aluminum Dome |
|------|----------------------------------|
| -L | Vandal Proof Dome |
| -R | 2" High External Water Dam |
| -SO | Side Outlet** |
| -V | Fixed Extension (1-1/2",2",3",4" |
| -W | Adi. Water Level Regulator |

Ductile Iron Dome

| | rial rraisi zoroi mogoraroi | |
|------|-------------------------------|--|
| -W-1 | Waterproofing Flange | |
| -Z | Extended Integral Wide Flange | |
| -5 | Sediment Bucket | |
| -6 | Vandal Proof Top | |
| -12 | Galvanized Dome | |
| | | |

| -12 | Galvanized Dome |
|-----|-------------------|
| -13 | All Galvanized |
| -83 | Mesh Covered Dome |

-113M Special Epoxy from 3M Range

Job Name _____ Contractor _____

Job Location ____ Contractor's P.O. No. _____

Engineer ____ Representative _____

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WAI 15

A Watts Water Technologies Company

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Adjustable Accutrol Weir

Adjustable Flow Control for Roof Drains

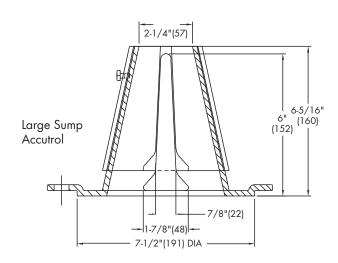
ADJUSTABLE ACCUTROL (for Large Sump Roof Drains only)

For more flexibility in controlling flow with heads deeper than 2", Watts Drainage offers the Adjustable Accutrol. The Adjustable Accutrol Weir is designed with a single parabolic opening that can be covered to restrict flow above 2" of head to less than 5 gpm per inch, up to 6" of head. To adjust the flow rate for depths over 2" of head, set the slot in the adjustable upper cone according to the flow rate required. Refer to Table 1 below. Note: Flow rates are directly proportional to the amount of weir opening that is exposed.

EXAMPLE:

For example, if the adjustable upper cone is set to cover 1/2 of the weir opening, flow rates above 2"of head will be restricted to 2-1/2 gpm per inch of head.

Therefore, at 3" of head, the flow rate through the Accutrol Weir that has 1/2 the slot exposed will be: [5 gpm (per inch of head) \times 2 inches of head] + 2-1/2 gpm (for the third inch of head) = 12-1/2 gpm.



Adjustable Upper Cone

Fixed Weir

1/2 Weir Opening Exposed Shown Above

TABLE 1. Adjustable Accutrol Flow Rate Settings

| Wain Ononing | 1" | 2" | 3" | 4" | 5" | 6" |
|-------------------------|--------------------------------|----|-------|------|-------|----|
| Weir Opening Exposed | Flow Rate (gallons per minute) | | | | | |
| Fully Exposed | 5 | 10 | 15 | 20 | 25 | 30 |
| 3/4 | 5 | 10 | 13.75 | 17.5 | 21.25 | 25 |
| 1/2 | 5 | 10 | 12.5 | 15 | 17.5 | 20 |
| 1/4 | 5 | 10 | 11.25 | 12.5 | 13.75 | 15 |
| Closed | 5 | 5 | 5 | 5 | 5 | 5 |

| Job Name | Contractor |
|---------------|-----------------------|
| lab l apation | Contractorio D.O. No |
| Job Location | Contractor's P.O. No. |
| Engineer | Representative |
| <u>e</u> | · |

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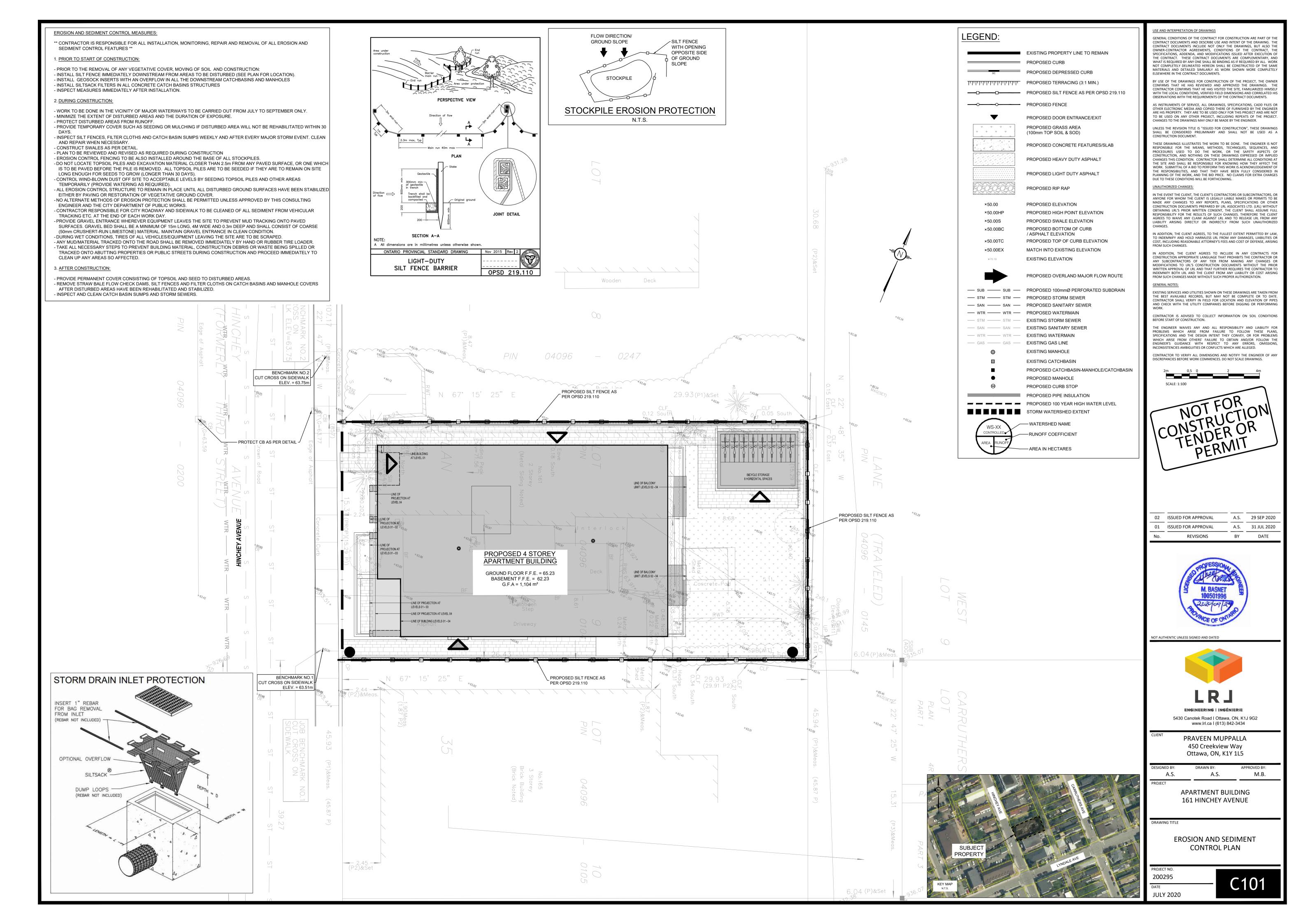


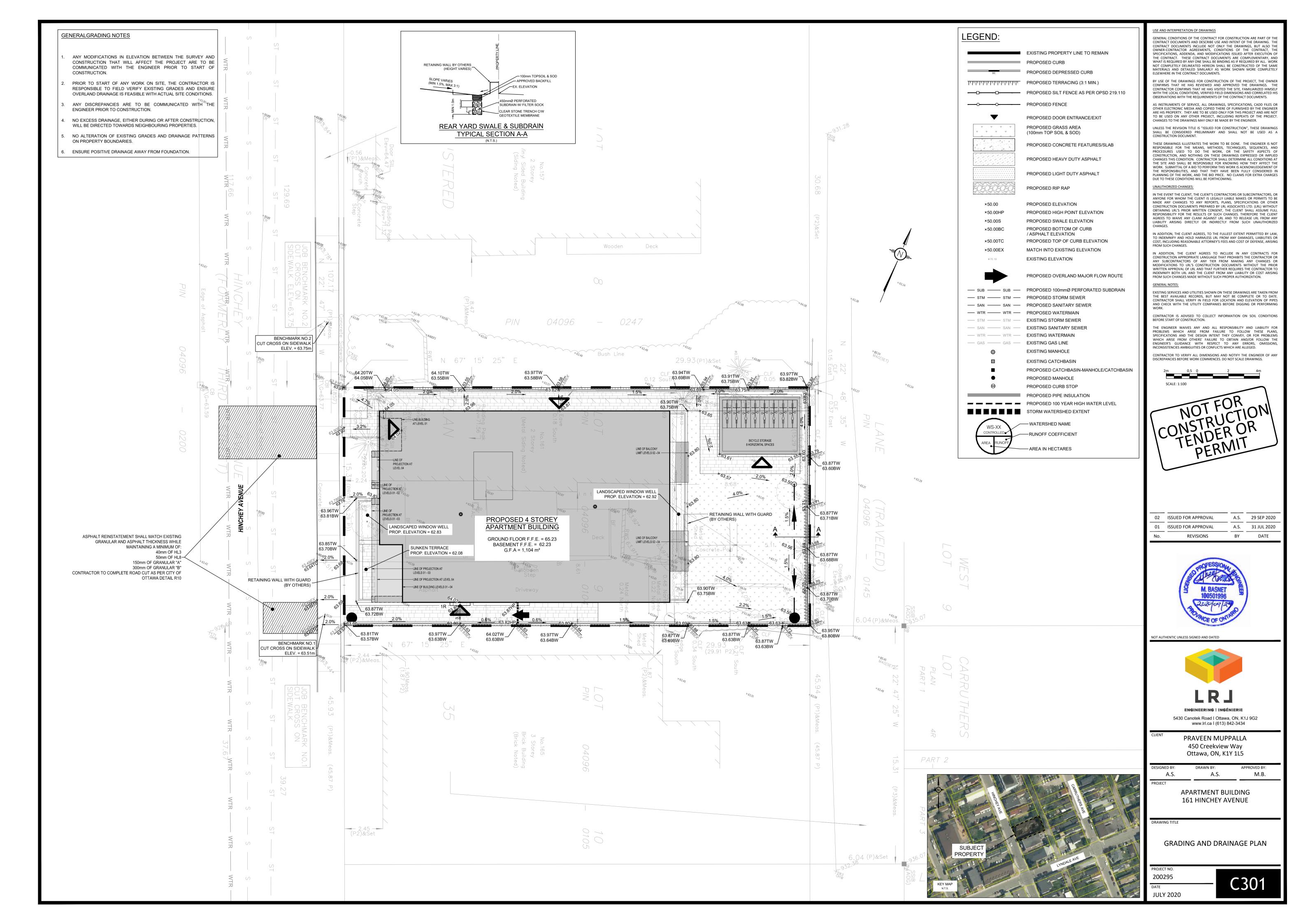
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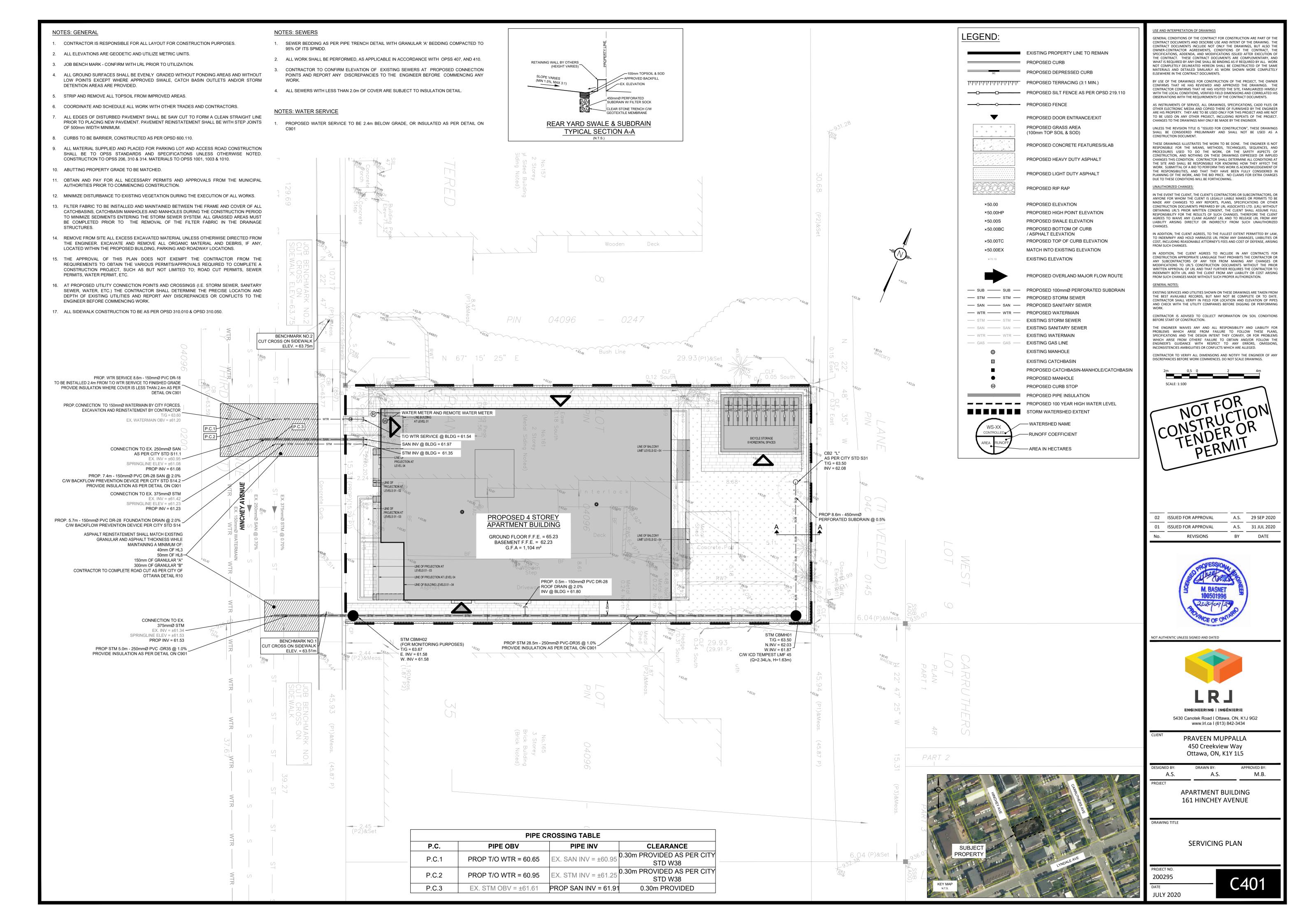
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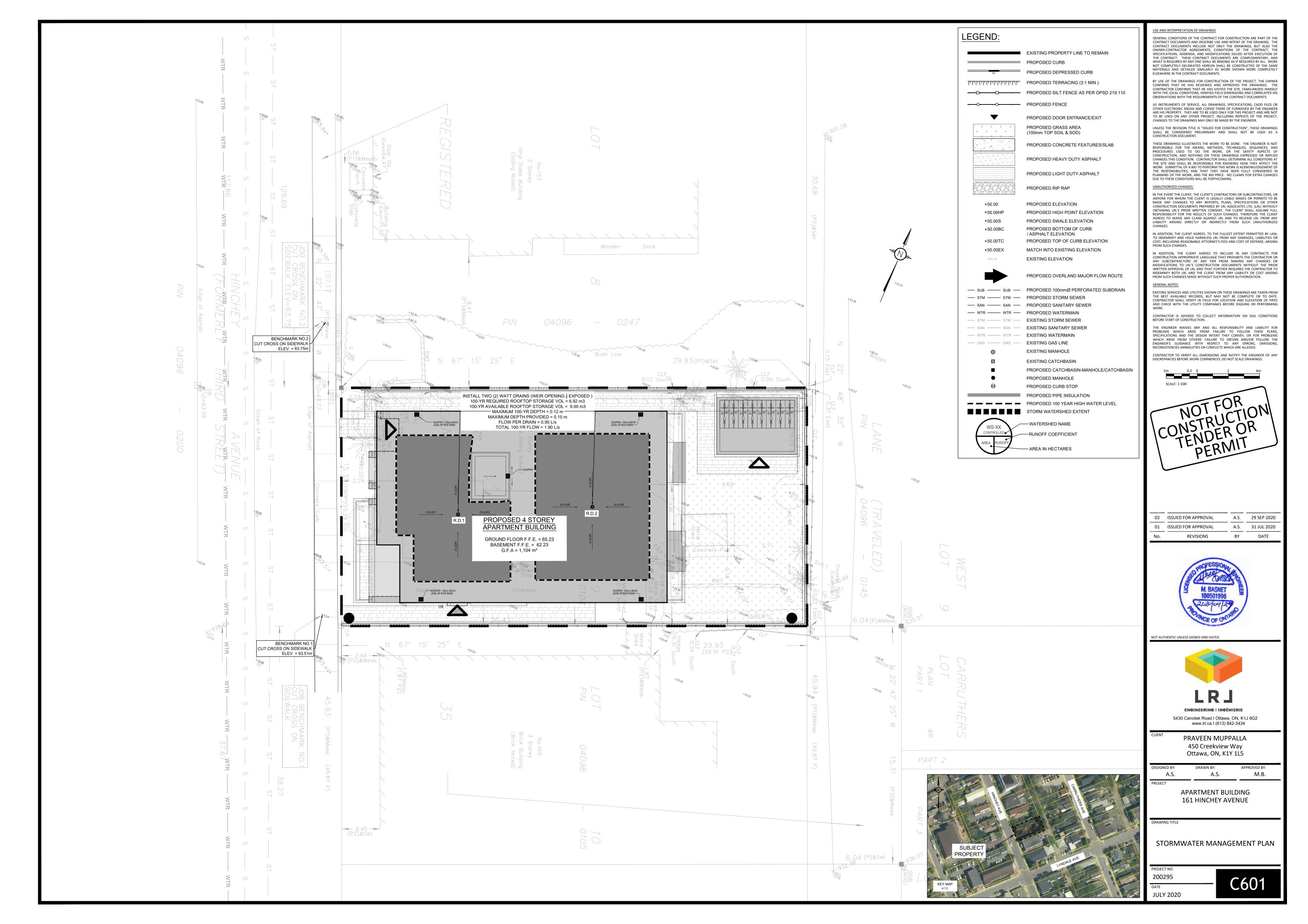
APPENDIX ECivil Engineering Drawings

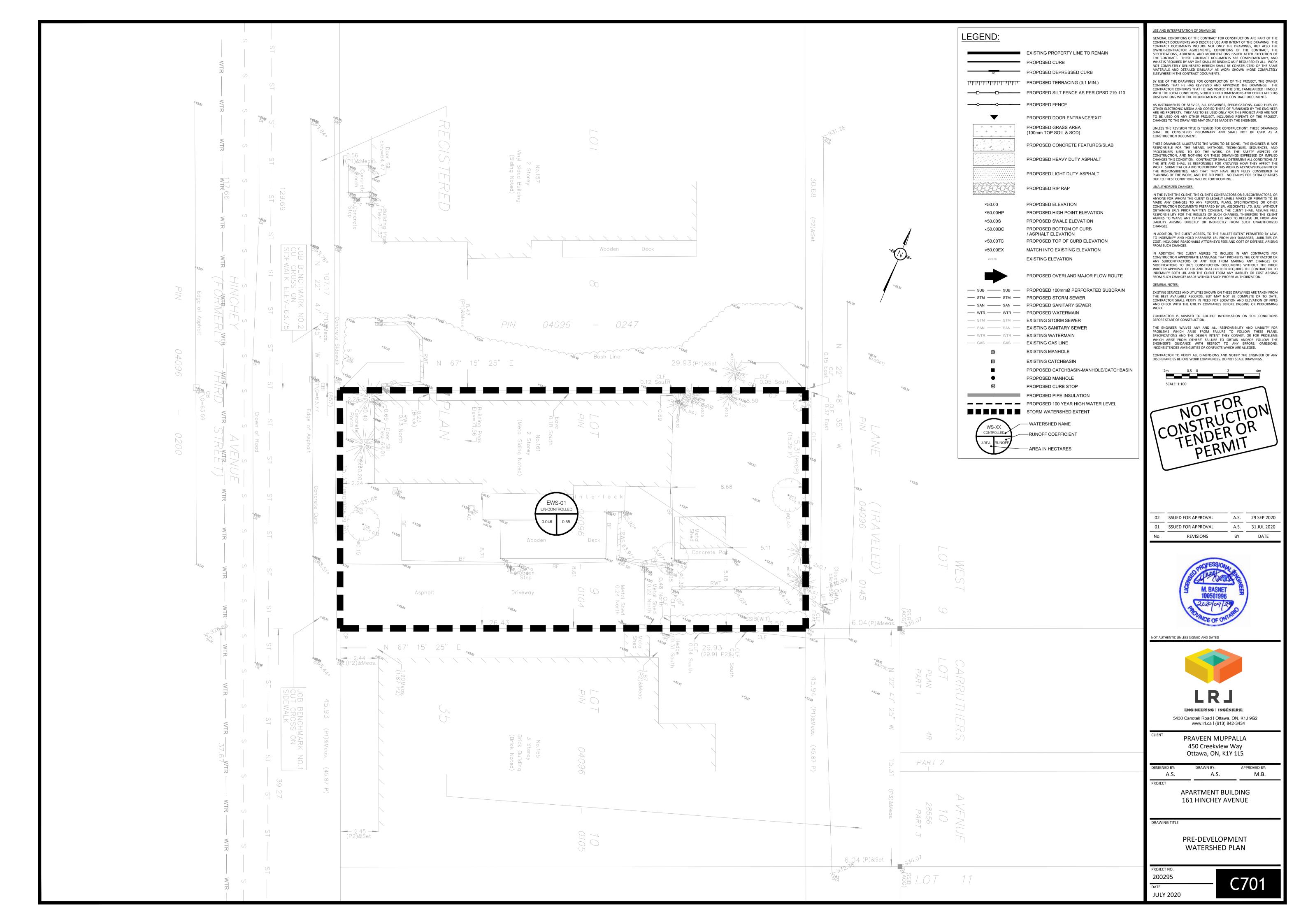


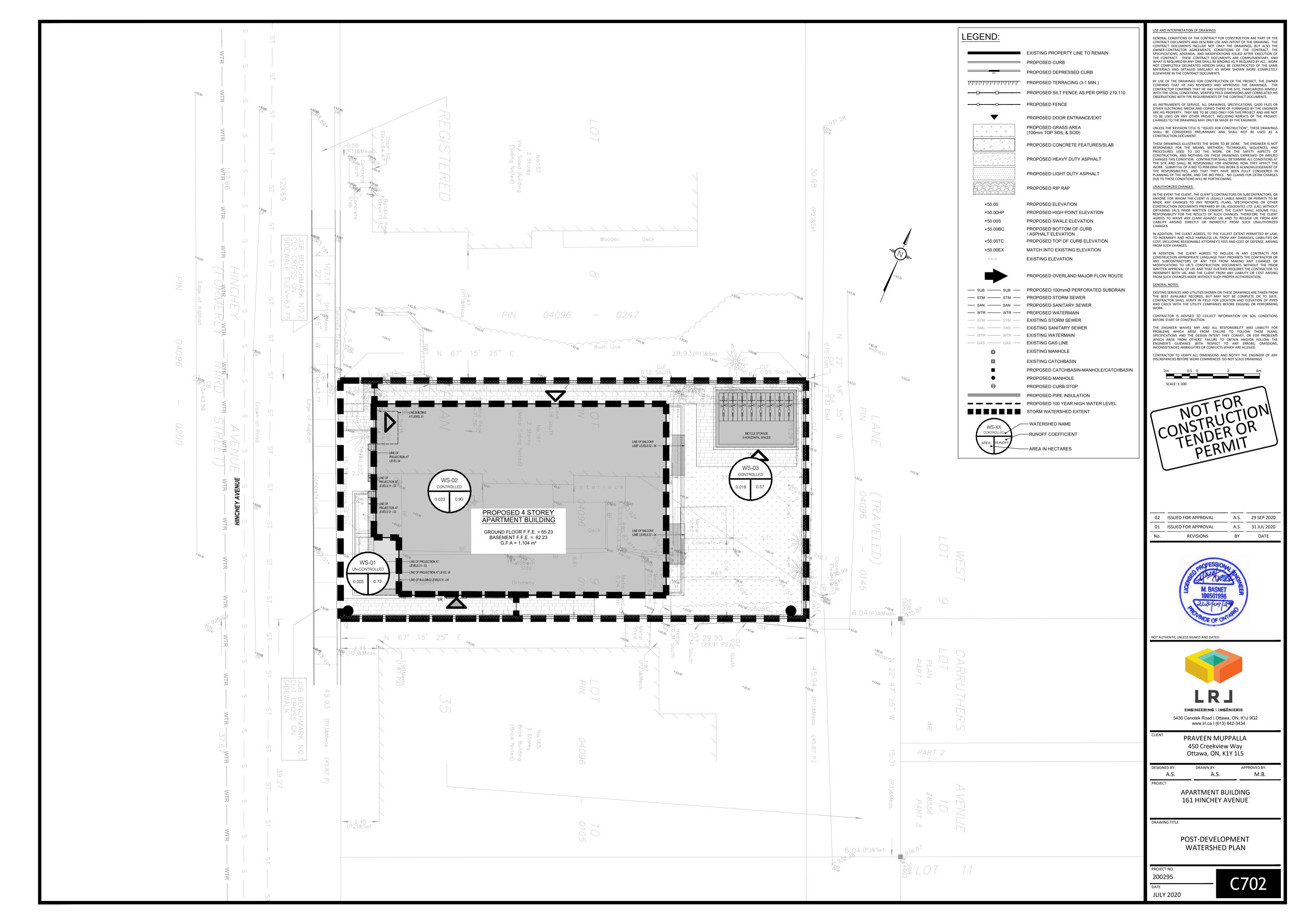


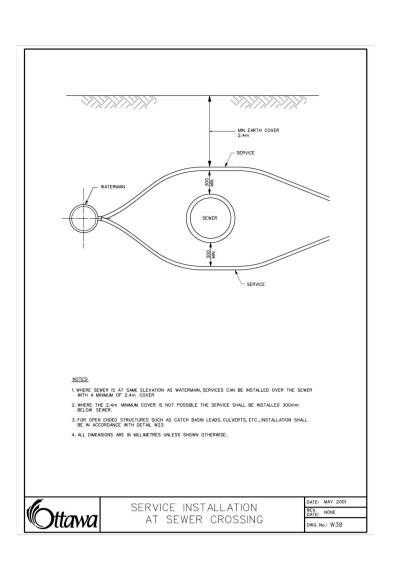


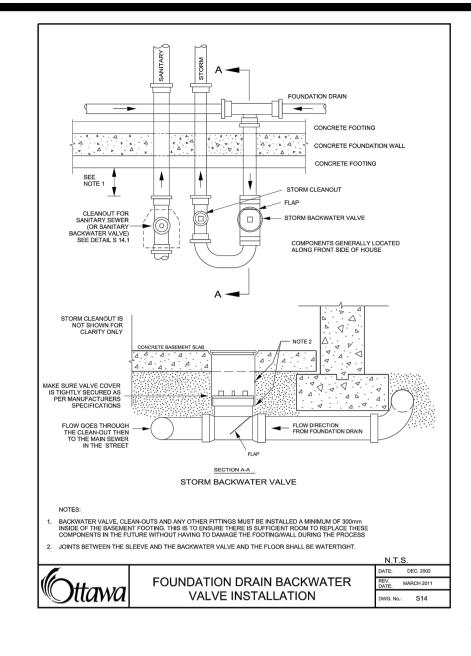


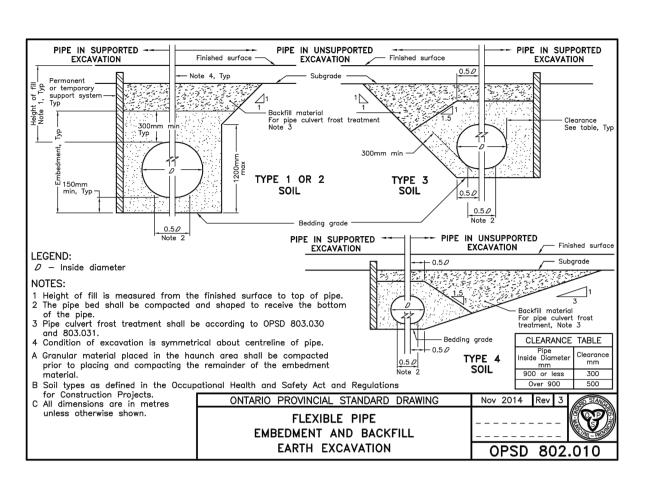


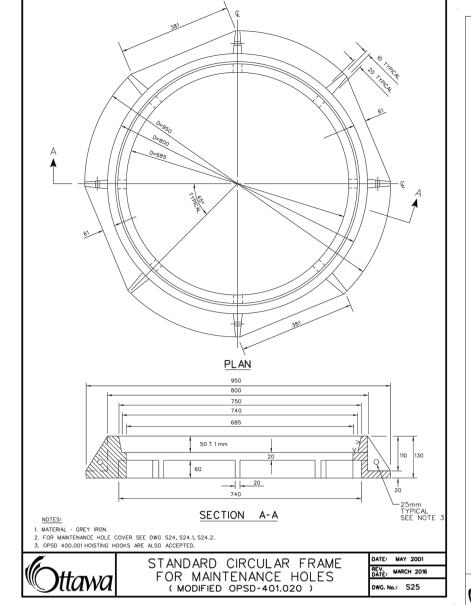


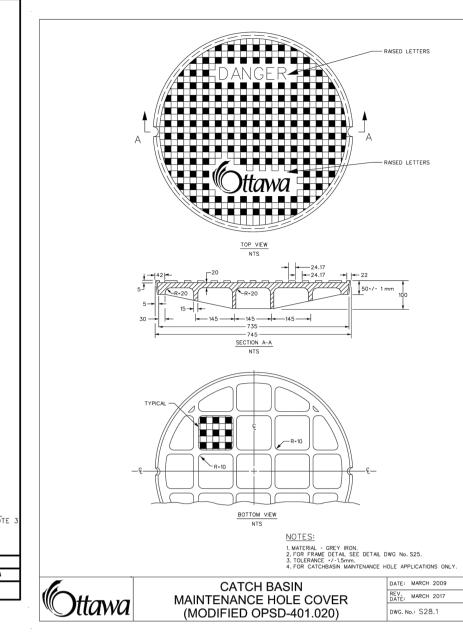


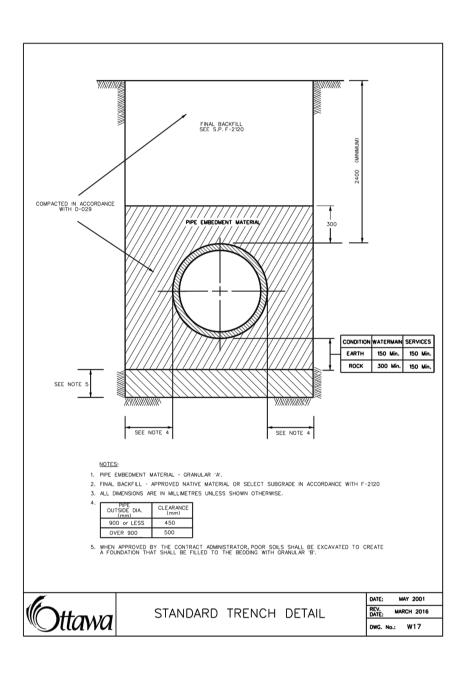


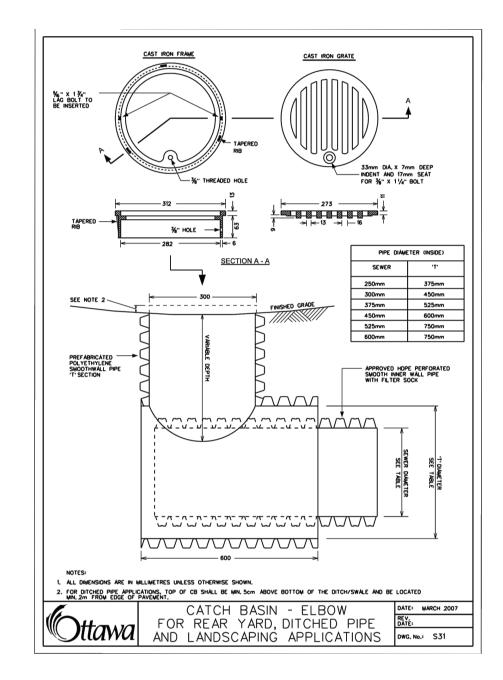


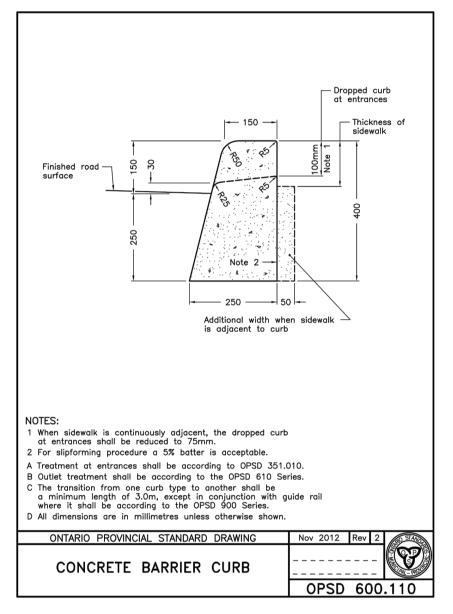


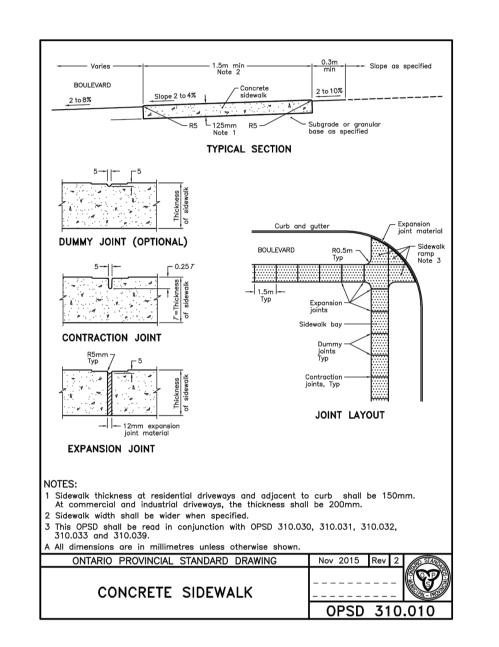


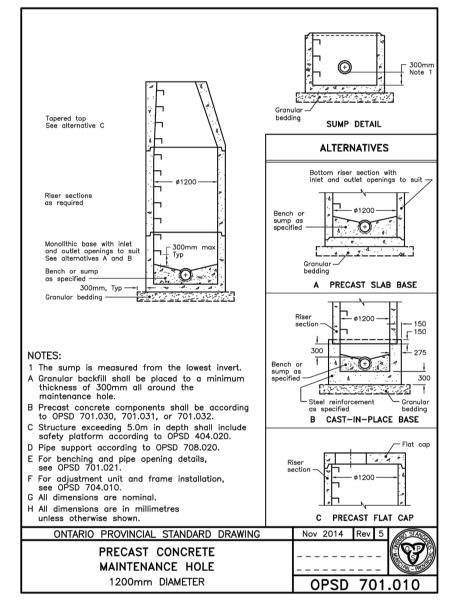


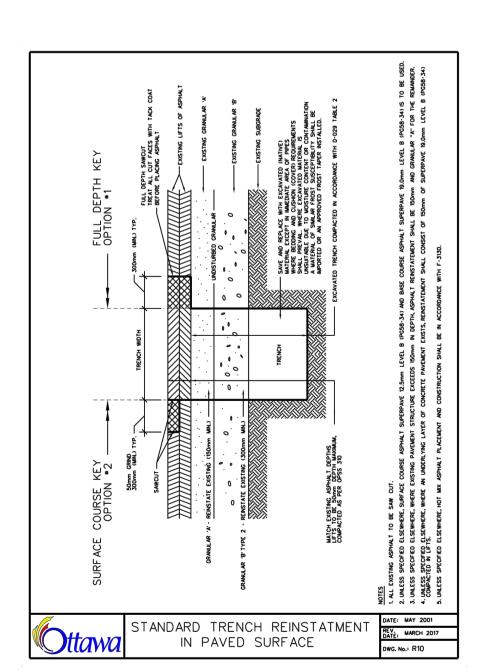


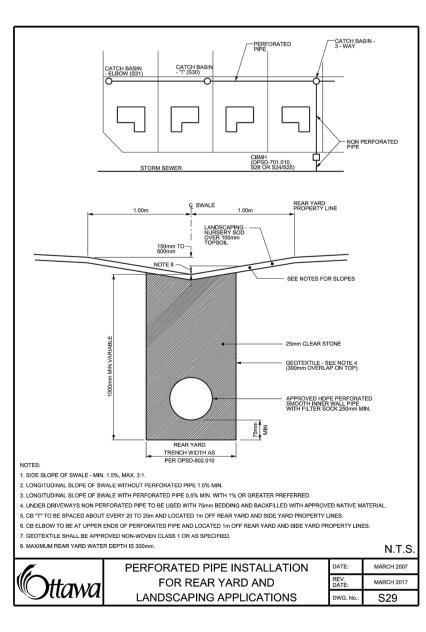


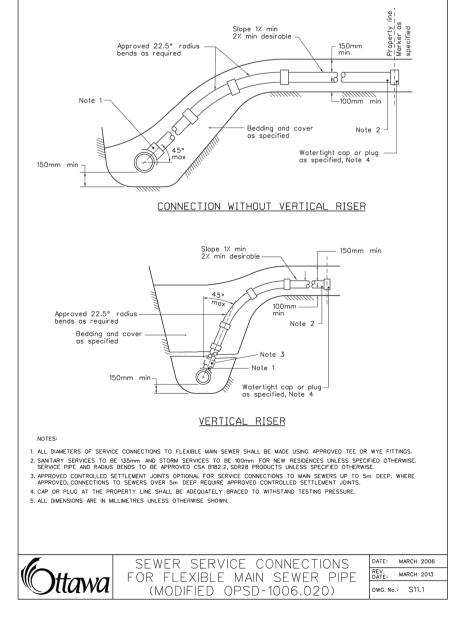


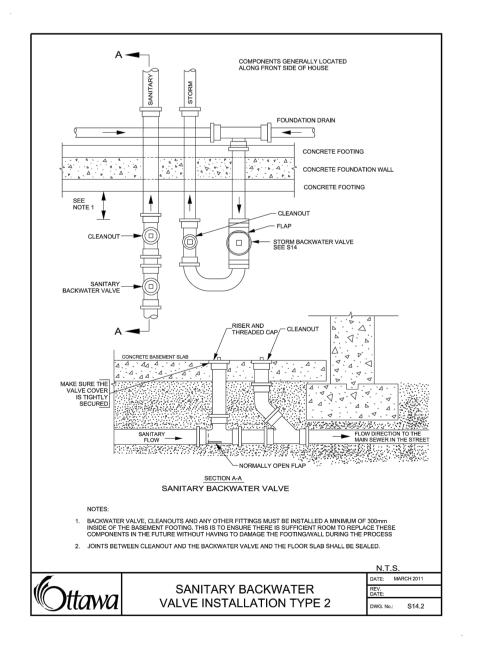


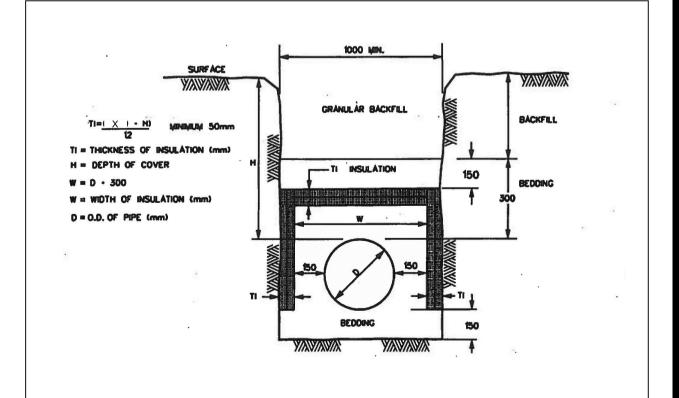












NOTES:
-FOR STORM INSULATION USE AN X VALUE OF 2000 IN THE ABOVE "TI" EQUATION.
-FOR SANITARY INSULATION USE AN X VALUE OF 2500 IN THE ABOVE "TI" EQUATION.
-FOR WATERMAIN INSULATION USE AN X VALUE OF 2400 IN THE ABOVE "TI" EQUATION.
-INCREMENTS OF INSULATION THICKNESS SHALL BE ADJUSTABLE TO 25mm.
-STAGGER JOINTS OF MULTIPLE SHEETS.
-ALL DIMENSIONS ARE IN MILLIMETERS UNLESS SHOWN OTHERWISE.

TYPICAL STORM AND SANITARYSEWER AND
WATERMAIN INSULATION DETAIL
(N.T.S.)

USE AND INTERPRETATION OF DRAWINGS

GENERAL CONDITIONS OF THE CONTRACT FOR CONSTRUCTION ARE PART OF THE CONTRACT DOCUMENTS AND DESCRIBE USE AND INTENT OF THE DRAWING. THE CONTRACT DOCUMENTS INCLUDE NOT ONLY THE DRAWINGS, BUT ALSO THE OWNER-CONTRACTOR AGREEMENTS, CONDITIONS OF THE CONTRACT, THE SPECIFICATIONS, ADDENDA, AND MODIFICATIONS ISSUED AFTER EXECUTION OF THE CONTRACT. THESE CONTRACT DOCUMENTS ARE COMPLEMENTARY, AND WHAT IS REQUIRED BY ANY ONE SHALL BE BINDING AS IF REQUIRED BY ALL. WORK NOT COMPLETELY DELINEATED HEREON SHALL BE CONSTRUCTED OF THE SAME MATERIALS AND DETAILED SIMILARLY AS WORK SHOWN MORE COMPLETELY ELSEWHERE IN THE CONTRACT DOCUMENTS.

MATERIALS AND DETAILED SIMILARLY AS WORK SHOWN MORE COMPLETELY ELSEWHERE IN THE CONTRACT DOCUMENTS.

BY USE OF THE DRAWINGS FOR CONSTRUCTION OF THE PROJECT, THE OWNER CONFIRMS THAT HE HAS REVIEWED AND APPROVED THE DRAWINGS. THE CONTRACTOR CONFIRMS THAT HE HAS VISITED THE SITE, FAMILIARIZED HIMSELF

OBSERVATIONS WITH THE REQUIREMENTS OF THE CONTRACT DOCUMENTS.

AS INSTRUMENTS OF SERVICE, ALL DRAWINGS, SPECIFICATIONS, CADD FILES OR OTHER ELECTRONIC MEDIA AND COPIED THERE OF FURNISHED BY THE ENGINEER ARE HIS PROPERTY. THEY ARE TO BE USED ONLY FOR THIS PROJECT AND ARE NOT TO BE USED ON ANY OTHER PROJECT, INCLUDING REPEATS OF THE PROJECT.

WITH THE LOCAL CONDITIONS, VERIFIED FIELD DIMENSIONS AND CORRELATED HIS

UNLESS THE REVISION TITLE IS "ISSUED FOR CONSTRUCTION", THESE DRAWINGS SHALL BE CONSIDERED PRELIMINARY AND SHALL NOT BE USED AS A CONSTRUCTION DOCUMENT.

THESE DRAWINGS ILLUSTRATES THE WORK TO BE DONE. THE ENGINEER IS NOT RESPONSIBLE FOR THE MEANS, METHODS, TECHNIQUES, SEQUENCES, AND PROCEDURES USED TO DO THE WORK, OR THE SAFETY ASPECTS OF CONSTRUCTION, AND NOTHING ON THESE DRAWINGS EXPRESSED OR IMPLIED CHANGES THIS CONDITION. CONTRACTOR SHALL DETERMINE ALL CONDITIONS AT THE SITE AND SHALL BE RESPONSIBLE FOR KNOWING HOW THEY AFFECT THE WORK. SUBMITTAL OF A BID TO PERFORM THIS WORK IS ACKNOWLEDGEMENT OF THE RESPONSIBILITIES, AND THAT THEY HAVE BEEN FULLY CONSIDERED IN PLANNING OF THE WORK, AND THE BID PRICE. NO CLAIMS FOR EXTRA CHARGES DUE TO THESE CONDITIONS WILL BE FORTHCOMING.

UNAUTHORIZED CHANGES:

IN THE EVENT THE CLIENT, THE CLIENT'S CONTRACTORS OR SUBCONTRACTORS, OR ANYONE FOR WHOM THE CLIENT IS LEGALLY LIABLE MAKES OR PERMITS TO BE MADE ANY CHANGES TO ANY REPORTS, PLANS, SPECIFICATIONS OR OTHER CONSTRUCTION DOCUMENTS PREPARED BY LRL ASSOCIATES LTD. (LRL) WITHOUT OBTAINING LRL'S PRIOR WRITTEN CONSENT, THE CLIENT SHALL ASSUME FULL RESPONSIBILITY FOR THE RESULTS OF SUCH CHANGES. THEREFORE THE CLIENT AGREES TO WAIVE ANY CLAIM AGAINST LRL AND TO RELEASE LRL FROM ANY LIABLITY ARISING DIRECTLY OR INDIRECTLY FROM SUCH UNAUTHORIZED

IN ADDITION, THE CLIENT AGREES, TO THE FULLEST EXTENT PERMITTED BY LAW, TO INDEMNIFY AND HOLD HARMLESS LRL FROM ANY DAMAGES, LIABILITIES OR COST, INCLUDING REASONABLE ATTORNEY'S FEES AND COST OF DEFENSE, ARISING FROM SUCH CHANGES.

IN ADDITION, THE CLIENT AGREES TO INCLUDE IN ANY CONTRACTS FOR CONSTRUCTION APPROPRIATE LANGUAGE THAT PROHIBITS THE CONTRACTOR OR ANY SUBCONTRACTORS OF ANY TIER FROM MAKING ANY CHANGES OR MODIFICATIONS TO LRL'S CONSTRUCTION DOCUMENTS WITHOUT THE PRIOR WRITTEN APPROVAL OF LRL AND THAT FURTHER REQUIRES THE CONTRACTOR TO INDEMNIFY BOTH LRL AND THE CLIENT FROM ANY LIABILITY OR COST ARISING FROM SUCH CHANGES MADE WITHOUT SUCH PROPER AUTHORIZATION.

GENERAL NOTES:

EXISTING SERVICES AND

EXISTING SERVICES AND UTILITIES SHOWN ON THESE DRAWINGS ARE TAKEN FROM THE BEST AVAILABLE RECORDS, BUT MAY NOT BE COMPLETE OR TO DATE CONTRACTOR SHALL VERIFY IN FIELD FOR LOCATION AND ELEVATION OF PIPES AND CHECK WITH THE UTILITY COMPANIES BEFORE DIGGING OR PERFORMING

CONTRACTOR IS ADVISED TO COLLECT INFORMATION ON SOIL CONDITIONS BEFORE START OF CONSTRUCTION.

THE ENGINEER WAIVES ANY AND ALL RESPONSIBILITY AND LIABILITY FOR PROBLEMS WHICH ARISE FROM FAILURE TO FOLLOW THESE PLANS, SPECIFICATIONS AND THE DESIGN INTENT THEY CONVEY, OR FOR PROBLEMS WHICH ARISE FROM OTHERS' FAILURE TO OBTAIN AND/OR FOLLOW THE ENGINEER'S GUIDANCE WITH RESPECT TO ANY ERRORS, OMISSIONS, INCONSISTENCIES AMBIGUITIES OR CONFLICTS WHICH ARE ALLEGED.

CONTRACTOR TO VERIFY ALL DIMENSIONS AND NOTIFY THE ENGINEER OF ANY DISCREPANCIES BEFORE WORK COMMENCES. DO NOT SCALE DRAWINGS.



 02
 ISSUED FOR APPROVAL
 A.S.
 29 SEP 2020

 01
 ISSUED FOR APPROVAL
 A.S.
 31 JUL 2020

 No.
 REVISIONS
 BY
 DATE



NOT AUTHENTIC UNLESS SIGNED AND DATED



ENGINEERING I INGÉNIERIE 5430 Canotek Road I Ottawa, ON, K1J 9G2 www.lrl.ca I (613) 842-3434

PRAVEEN MUPPALLA 450 Creekview Way

Ottawa, ON, K1Y 1L5

A.S.

APARTMENT BUILDING
161 HINCHEY AVENUE

RAWING TITLE

A.S.

CONSTRUCTION DETAIL PLAN

PROJECT NO. **200295**

JULY 2020

- C9

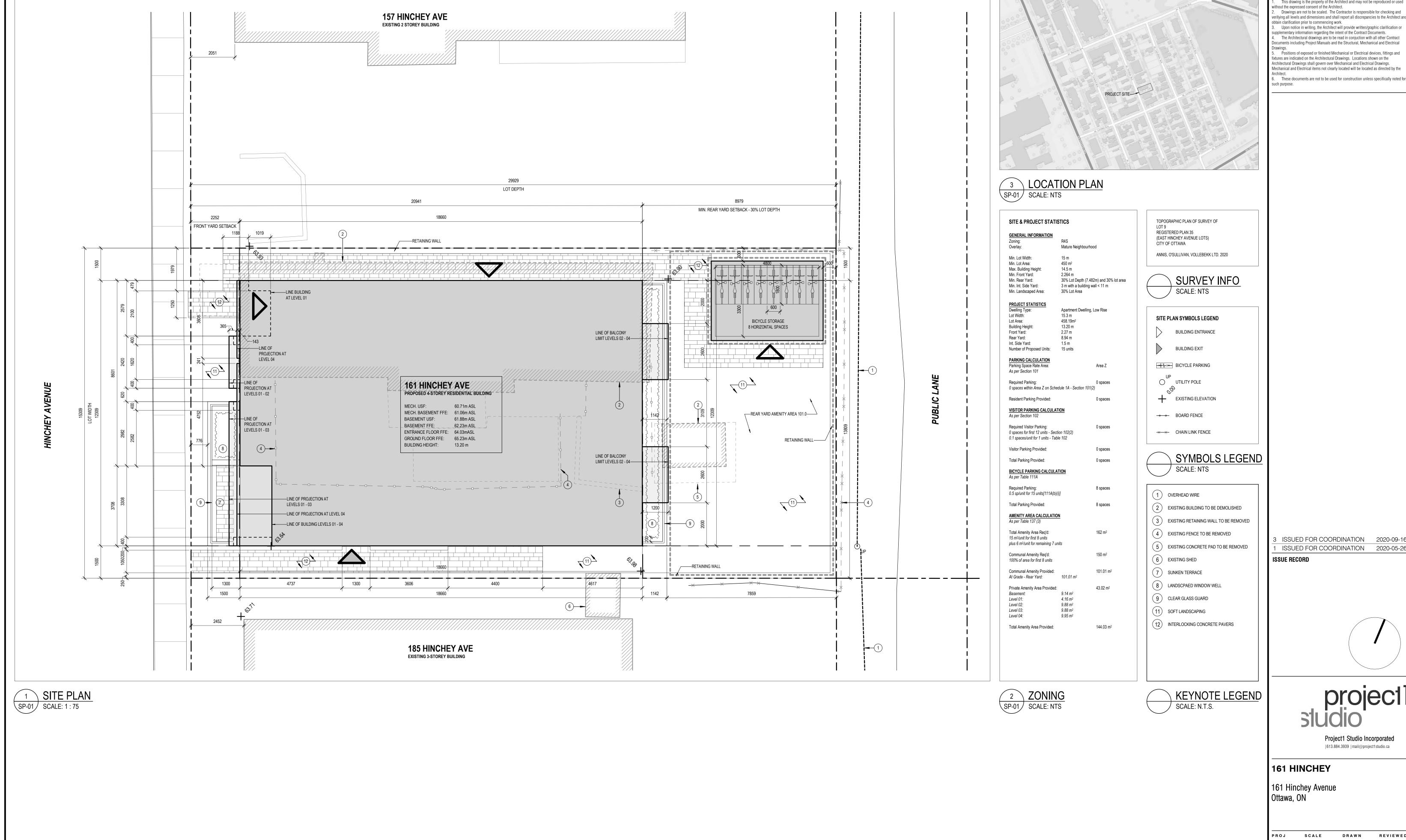


M.B.

DRAWINGS/FIGURES

Proposed Site Plan Legal Survey As-builts

5430 Canotek Road | Ottawa, ON, K1J 9G2 | info@lrl.ca | www.lrl.ca | (613) 842-3434



NERAL ARCHITECTURAL NOTES:

This drawing is the property of the Architect and may not be reproduced or used out the expressed consent of the Architect. Drawings are not to be scaled. The Contractor is responsible for checking and ifying all levels and dimensions and shall report all discrepancies to the Architect and tain clarification prior to commencing work. Upon notice in writing, the Architect will provide written/graphic clarification or olementary information regarding the intent of the Contract Documents.

The Architectural drawings are to be read in conjuction with all other Contract uments including Project Manuals and the Structural, Mechanical and Electrical Positions of exposed or finished Mechanical or Electrical devices, fittings and xtures are indicated on the Architectural Drawings. Locations shown on the chitectural Drawings shall govern over Mechanical and Electrical Drawings. lechanical and Electrical items not clearly located will be located as directed by the

ISSUED FOR COORDINATION 2020-09-16 1 ISSUED FOR COORDINATION 2020-05-26

ISSUE RECORD

Project1 Studio Incorporated |613.884.3939 | mail@project1studio.ca

161 HINCHEY

161 Hinchey Avenue Ottawa, ON

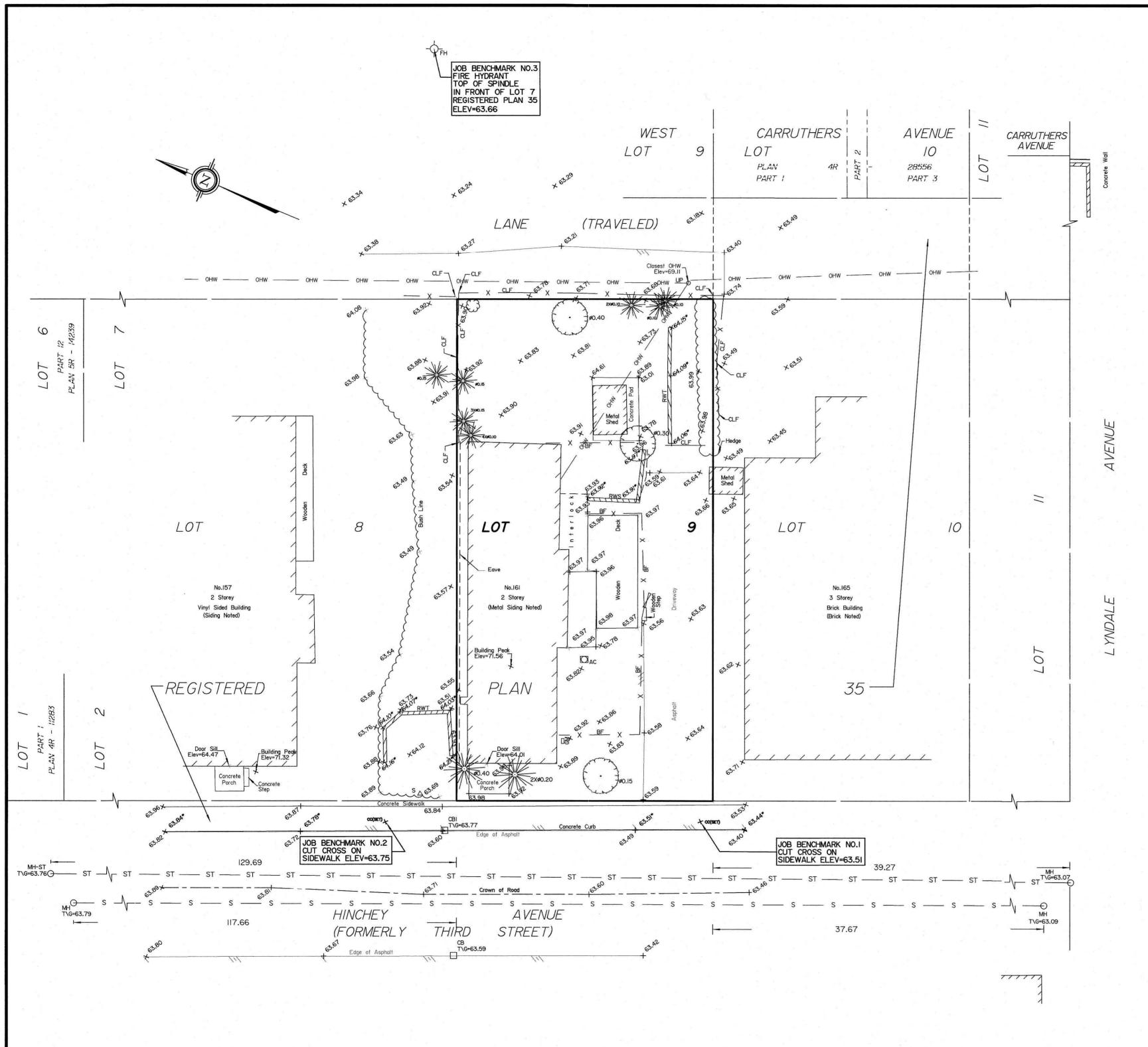
1931 NOTED AP

SITE PLAN

DRAWN

REVIEWED

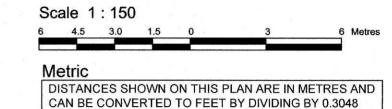
RMK



SKETCH OF BENCHMARK LOCATIONS

161 HINCHEY AVENUE OTTAWA

Surveyed by Annis, O'Sullivan, Vollebekk Ltd.



Notes & Legend

| | 9 | A STANDARD CONTRACTOR OF THE STANDARD CO. |
|-----------------|------------|---|
| | enotes | Survey Manument Planted |
| | | Survey Monument Planted |
| SSIB | | Survey Monument Found |
| | | Short Standard Iron Bar |
| IB CD | " | Iron Bar |
| CP | | Concrete Pin |
| Meas. | 10 | Measured |
| (AOG) | an . | Annis, O'Sullivan, Vollebekk Ltd. |
| (P) | 3 0 | Registered Plan 35 |
| (PI) | OH . | (857) Plan August 9, 2010 |
| (P2) | Off I | (687) Plan November 25,1985 |
| (P3) | | Plan 4R-28556 |
| RWT | ч | Retaining Wall Timber |
| RWS | п | Retaining Wall Stone |
| —— онw —— | - 0 | Overhead Wires |
| O UP | 30 | Utility Pole |
| СВ | 30 | Catch Basin |
| CB-I | n | Catch Basin Inlet |
| O _{FH} | in . | Fire Hydrant |
| □ GM | u | Gas Meter |
| ΔS | | Sign |
| CLF | 11 | Chain Link Fence |
| BF | | Board Fence |
| \sim | | Gate |
| ◯ AC | 10 | Air Conditioner |
| \odot | iu . | Shrub |
| £. 3 | | Deciduous Tree |
| مرسيا | | |
| We . | | |
| 1 | | Coniferous Tree |
| O MH-ST | an . | Maintenance Hole (Storm Sewer) |
| O MH−S | 11 | Maintenance Hole (Sanitary) |
| ST | × 30 | Underground Storm Sewer |
| s | a . | Underground Sanitary Sewer |
| Ø | n | Diameter |
| +65.00 | | Location of Elevation |
| +65.00* | | Top of Concrete Curb Elevation |
| + 65.00* | TI TI | Top of Retaining Wall Elevation |
| C/L | 0 | Centreline |
| | | |

UTILITY NOTES

 This drawing cannot be accepted as acknowledging all of the utilities and it will be the responsibility of the user to contact the respective utility authorities for confirmation.

Property Line

- 2. Only visible surface utilities were located.
- 3. Underground utility data derived from City of Ottawa utility sheet reference
- A field location of underground plant by the pertinent utility authority is mandatory before any work involving breaking ground, probing, excavating etc.

ELEVATION NOTES

1. Elevations shown are geodetic and are referred to the CGVD28 geodetic datum.

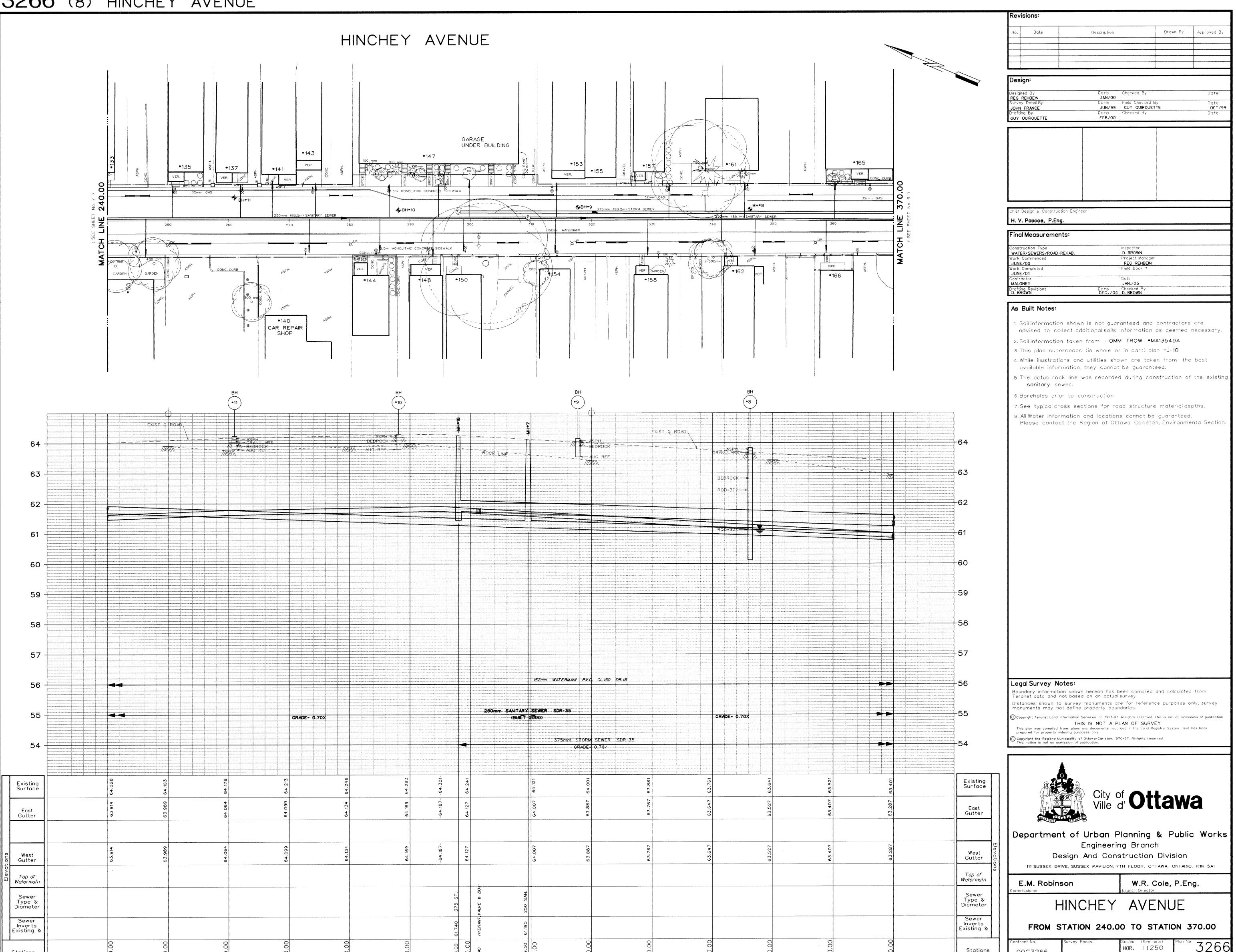
Land Surveyors Job No. 20365-19 Canada Inc-bm Sketch

It is the responsibility of the user of this information to verify that the job benchmark has not been altered or disturbed and that it's relative elevation and description agrees with the information shown on this drawing.

ANNIS, O'SULLIVAN, VOLLEBEKK LTD.

14 Concourse Gate, Suite 500
Nepean, Ont. K2E 7S6
Phone: (613) 727-0850 / Fax: (613) 727-1079
Email: Nepean@aovitd.com

Stations



VERT. 1:50

Stations

00C3266