

Stormwater Management Report and Servicing Brief

Apartment Building 161 Hinchey Avenue Ottawa, Ontario

Prepared for:

Praveen Muppalla. 450 Creekview Way Ottawa, ON, K1Y 1L5

Attention: Mr. Praveen Muppalla

LRL File No.: 200295

Revision 1 – September 29st, 2020 Revision 2 – April 23rd, 2021 Revision 3 – July 9th, 2021

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1 INTRODUCTION AND SITE DESCRIPTION

LRL Associates Ltd. was retained by Praveen Muppalla to complete a Stormwater Management Analysis and Servicing Brief for a proposed four (4) storey residential building located at 161 Hinchey Avenue in Ottawa, Ontario. The property is legally described as Lot 9, Registered Plan 35, Concession 1, City Ward 15 (Kitchissippi) and is zoned R4S. The location of the proposed development can be viewed in **Figure 1** below.



Figure 1: Arial View of Proposed Development

The site to be developed is rectangular shape with a frontage of approximately 15 m along Hinchey Avenue and a depth of approximately 30 m, and a surface area of approximately **0.046 ha**.

The topographic survey of the property was completed by Annis, O'Sullivan, Vollebekk Ltd. (Ontario Land Surveyors). Two site benchmarks were established during the survey for future construction use. These benchmarks, cross-cut on sidewalk along Hinchey Avenue with elevation 63.51 (benchmark No. 1) and 63.75 (benchmark No.2), are shown on the *Legal Survey* included in *Drawings/Figures*.

The development proposes a new four (4) storey residential building consisting of 15 units. Vehicular parking is not proposed on site, however provision for bicycle parking (8 spaces bicycle

storage room) is proposed. For additional information, refer to a copy of the *Site Plan (SP-01)* included in *Drawings/Figures*.

This report has been prepared in consideration of the terms and conditions noted above and with the civil drawings prepared for the new development. Should there be any changes in the design features, which may relate to the stormwater considerations, LRL Associates Ltd. should be advised to review the report recommendations.

2 EXISTING SITE AND DRAINAGE DESCRIPTION

The subject site measures **0.046 ha** and currently consists of a single 2-storey residential building and a paved driveway. Elevations of existing site range between 63.99 m at northeast corner to 63.59 m at the west side of the site.

Sewer and watermain mapping, along with as-built information collected from the City of Ottawa indicate the following existing infrastructure located within the adjacent right-of-way:

Hinchey Avenue:

- 150 mm diameter PVC watermain
- 250 mm diameter PVC sanitary sewer
- 375 mm diameter PVC storm sewer

3 SCOPE OF WORK

As per applicable guidelines, the scope of work includes the following:

Stormwater management

- Calculate the allowable stormwater release rate.
- Calculate the anticipated post-development stormwater release rates.
- Demonstrate how the target quantity objectives will be achieved.

Water services

- Calculate the expected water supply demand at average and peak conditions.
- Calculate the required fire flow as per the Fire Underwriters Survey (FUS) method.
- Confirm the adequacy of water supply and pressure during peak flow and fire flow.
- Describe the proposed water distribution network and connection to the existing system.

Sanitary services

- Describe the existing sanitary sewers available to receive wastewater from the building.
- Calculate peak flow rates from the development.
- Describe the proposed sanitary sewer system.
- Review impact of increased sanitary flow on downstream sanitary sewer.

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4 **REGULATORY APPROVALS**

An MECP Environmental Compliance Approval is not expected to be required for installation of the proposed storm and sanitary sewers within the site. A Permit to Take Water is not anticipated to be required for pumping requirements for sewer installation. The Rideau Valley Conservation Authority will need to be consulted in order to obtain municipal approval for site development. No other approval requirements from other regulatory agencies are anticipated.

5 WATER SUPPLY AND FIRE PROTECTION

5.1 Existing Water Supply Services and Fire Hydrant Coverage

The subject property lies within the City of Ottawa 1W water distribution network pressure zone. The subject property is located to the east of an existing 150 mm dia. watermain along Hinchey Avenue. There are currently three (3) existing fire hydrants near the property; one within 75m and two within 150 m from proposed building entrance. Refer to *Appendix B* for the location of fire hydrants.

5.2 Water Supply Servicing Design

The subject property is proposed to be serviced via a 150 mm dia. service lateral connected to the 150 mm dia. watermain located within Hinchey Avenue. Refer to Site Servicing Plan C.401 in *Appendix E* for servicing layout.

Table 1 summarizes the City of Ottawa Design Guidelines design parameters employed in the preparation of the water demand estimate.

Design Parameter	Value
Residential Bachelor / 1 Bedroom Apartment	1.4 P/unit
Residential 2 Bedroom Apartment	2.1 P/unit
Average Daily Demand	280 L/d/per
Minimum Depth of Cover	2.4 m from top of watermain to finished grade
Desired operating pressure range during normal	350 kPa and 480 kPa
operating conditions	
During normal operating conditions pressure must	275 kPa
not drop below	
During normal operating conditions pressure shall	552 kPa
not exceed	
During fire flow operating conditions pressure must	140 kPa
not drop below	
*Table updated to reflect technical Bulletin ISDTB-2018-02	

 Table 1: City of Ottawa Design Guidelines Design Parameters

The interior layout and architectural floor plans have been reviewed, and it was determined that the building will house nine (9) studio/1-bedroom apartments, and six (6) 2-bedroom units. Based on the City of Ottawa Design guidelines for population projection, this translates to approximately

25.2 residents. Table 2 below summarizes the proposed development as interpreted using table 4.1 of the City of Ottawa Design Guidelines.

Proposed Unit type	Persons Per Unit	Number of Units	Population
Studio/1 Bedroom	1.4	9	12.6
2 Bedroom Apartment	2.1	6	12.6
		Total Residential Population	25.2

Table 2: Development Residential Population Es	timate
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The required water supply requirements for the residential units in proposed building have been calculated using the following formula:

Where:

$$Q = (q \times P \times M)$$

q = average water consumption (L/capita/day)

P = design population (capita)

M = Peak factor

Using a calculated Maximum Day Factor and Peak Hour factor of *10.3* and *15.5* respectively as per Table 3-3 in the *MOE Design Guidelines*, anticipated demands were calculated as follows:

- > Average daily domestic water demand is **0.08** L/s,
- > Maximum daily demand is **0.84** L/s, and
- > Maximum hourly demand is **13.06** L/s.

Based on maximum hourly rate of 13.06 L/s a minimum of 100 mm dia. servicing is required. However, assuming the presence of sprinklers, it is recommended to upsize the water servicing to 150 mm. Refer to *Appendix B* for water demand calculations.

The City of Ottawa was contacted to obtain boundary conditions associated with the estimated water demand, as indicated in the boundary request correspondence included in *Appendix B*. Table 3 below summarizes boundary conditions for the proposed development.

Table 3: Summary of Anticipated	Demands and Boundary Conditions
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Design Parameter	Anticipated Demand (L/min)	Boundary Conditions @ Hinchey Avenue* (m H2O / kPa)
Average Daily Demand	4.9	115.2 / 505.2
Max Day + Fire Flow (per FUS)	50.5 + 9,000	93.0 / 287.6
Peak Hour	783.8	106.5 / 419.9
*Assumed Ground elevation at connection p	oint = 63.65 m.	
Water demand calculation per City of Ottawa	a Water Design guidelines. See Appendi x	c B for details.

Calculated average day demand has increased by 0.02 L/s since boundary conditions were requested. As indicated in Table 3, pressures in all scenarios meet the required pressure range stated in Table 1 as per City of Ottawa Design Guidelines. Refer to *Appendix B* for Boundary Conditions.

The estimated fire flow for the proposed buildings was calculated in accordance with *ISTB-2018-02*. The following parameters were provided by the Architect.

- Type of construction Wood Frame Construction;
- Occupancy type Limited Combustibility; and
- Sprinkler Protection Standard Sprinkler System.

The estimated fire flow demand was estimated to be 9,000 L/min, see Appendix B for details.

There are three (3) existing fire hydrants in close proximity to the proposed buildings that are available to provide the required fire flow demands of 9,000 L/min. Refer to *Appendix B* for fire hydrant locations. Table 4 below summarizes the aggregate fire flow of the contributing hydrants in close proximity to the proposed development based on Table 18.5.4.3 of *ISTB-2018-02*.

Table 4: Fire Protection Summary Table

Building	Fire Flow Demand (L/min)	Fire Hydrants(s) within 75m	Fire Hydrant(s) within 150m	Available Combined Fire Flow (L/min)
Proposed 4 Storey Building	9,000	1	2	(1 x 5678) + (2 x 3785) = 13,248

The total available fire flow from contributing hydrants is equal to **13,248 L/min** which is sufficient to provide adequate fire flow for the proposed development. A certified fire protection system specialist will need to be employed to design the building's fire suppression system and confirm the actual fire flow demand.

The proposed water supply design conforms to all relevant City Guidelines and Policies.

6 SANITARY SERVICE

6.1 Existing Sanitary Sewer Services

There is an existing 250 mm dia. sanitary sewer within Hinchey Avenue across the subject site. The wastewater flow is ultimately conveyed to the West Nepean Collector trunk sewer.

The pre-development conditions of the lot were reviewed to calculate a total wet wastewater flow of **0.09 L/s** based on assumed conditions of 2 semi-detached residential dwellings.

The post development total flow was calculated to be is **0.34 L/s** as a result of proposed residential population and a small portion of infiltration. Refer to *Appendix C* for further information on the calculated sanitary flows. The post development conditions increase existing wastewater flow by approximately **0.25 L/s** as a result of additional residential population from pre-development conditions.

Based on existing as-built, refer to *Drawings/Figures* for as-built information, the existing 250mm dia. sanitary sewer within Hinchey Avenue is sloped at 0.70% and is calculated to have a maximum capacity of **49.75 L/s**. The proposed increase in total wastewater flow of **0.25 L/s** represents less than 1% of existing maximum capacity. Therefore, it is anticipated that the existing local sewer network has sufficient capacity to accommodate the proposed development.

6.2 Sanitary Sewer Servicing Design

The proposed development will be serviced via a 150 mm dia. sanitary service lateral which will connect to the existing 250mm dia. sanitary sewer located within Hinchey Avenue. Refer to LRL drawing C.401 for the proposed sanitary servicing.

The parameters used to calculate the anticipated sanitary flows are:; residential average population per unit of 1.4 person for single units and 2.1 persons for two-bedroom units, a residential average daily flow of 280 L/p/day, a residential peaking factor of 4.0 and a total infiltration rate of 0.33 L/s/ha. Based on these parameters and the total site area of 0.046 ha, the total wet anticipated sanitary flow was estimated to **0.34 L/s**. Refer to *Appendix C* for the site sanitary sewer design sheet.

7 STORMWATER MANAGEMENT

7.1 Existing Stormwater Infrastructure

Stormwater runoff from the subject property is tributary to the City of Ottawa sewer system. As such, approvals for the proposed development within this area are under the approval authority of the City of Ottawa.

In pre-development conditions, the stormwater runoff would flow uncontrolled overland to the west side of the site towards Hinchey Ave. right-of-way. There is an existing 375 mm diameter storm sewer within Hinchey Avenue right-of-way. Refer to *Appendix D* for pre- and post-development watershed information.

7.2 Design Criteria

The stormwater management criteria for this development are based on the pre-consultation with City of Ottawa officials, the City of Ottawa Sewer Design Guidelines including City of Ottawa Stormwater Management Design Guidelines, 2012 (City standards), as well as the Ministry of the Environment's Stormwater Management Planning and Design Manual, 2003 (SWMPD Manual).

Stormwater Management Report and Servicing Brief Apartment Buildings 161 Hinchey Avenue, Ottawa, Ontario

7.2.1 Water Quality

The subject property lies within the Ottawa River West sub-watershed and is therefore subject to review by the Rideau Valley Conservation Authority (RVCA). It was determined that no further treatment is required for stormwater runoff from the proposed development. Correspondence with RVCA is included in *Appendix A*.

7.2.2 Water Quantity

Based on pre-consultation with the City, correspondence included in *Appendix A*, the following stormwater management requirements were identified for the subject site:

- Meet an allowable release rate based on the existing Rational Method Coefficient no greater than 0.50, employing the City of Ottawa IDF parameters for a 5-year storm with a calculated time of concentration equal to or greater than 10 minutes;
- Attenuate all storms up to and including the City of Ottawa 100-year storm event on site; and

The allowable release rate for the subject site was calculated to be **6.63 L/s**. Refer to *Appendix D* for calculations.

7.3 Method of Analysis

The Modified Rational Method has been used to calculate the runoff rate from the site to quantify the detention storage required for quantity control of the development. Refer to *Appendix D* for storage calculations.

7.4 Proposed Stormwater Quantity Controls

The proposed stormwater management quantity control for this development will be accomplished using roof drains restricting the flow leaving the rooftop. Storage required as a result of quantity control will be accomplished through rooftop storage.

The subject site is proposed to be serviced via a 250 mm diameter perforated subdrain and 250 mm diameter storm sewers that outlet to the existing 375 mm diameter storm sewer within Hinchey Avenue. The proposed site storm sewer and stormwater management system are shown on drawing C.401 and detailed calculations, including the design sheet, can be found in *Appendix D*.

The existing site is delineated by catchments EWS-01 which currently drains uncontrolled towards the front of the property.

The site has been analyzed and post-development watersheds have been allocated. Watershed WS-01 (0.023 ha), consisting of grass and pavers, will flow uncontrolled. The runoff will be conveyed to the Hinchey Avenue right-of-way, as per the grading plan C301.

Runoff from the roof, delineated by Watershed WS-02 (0.023 ha), will be captured by the proposed roof drains. Stormwater captured on the rooftop will be controlled by the roof drains and conveyed to the storm sewer network.

Table 5 below summarizes post-development drainage areas. Calculations can be seen in *Appendix D.*

Table 5: Drainage Areas

Drainage Area Name	Area	Weighted Runoff Coefficient	100 Year Weighted Runoff Coefficient (25% increase)
WS-01 (uncontrolled)	0.023	0.63	0.79
WS-02 (controlled)	0.023	0.90	1.0

Rooftop detention of stormwater is provided with outlet control through two (2) proposed roof drains. The building's rooftop was analysed and divided into two (2) ponding areas. A total of two (2) roof drains, each of which is restricting the discharge rate to **0.63 L/s**, resulting in a total release rate from the roof of **1.26 L/s** is proposed. The roof drain flow control device has been selected to provide a flow rate of **0.63 L/s** at a maximum flow depth of **0.15 m**. Proposed roof drains are to be Watts RD-100-A with a <u>closed</u> exposed weir opening. See *Appendix D* for more information about the selected roof drain.

The total available roof storage (m^3) has been calculated using the following formula:

$$V = \left(\frac{D_{Sl} * A_{Eff}}{3}\right)$$

Where:

V = available (provided) rooftop storage (m^3) D_{Sl} = slope ponding depth (m) A_{Eff} = effective roof area (m^2)

Based on the equation above, it was calculated that 9.00 m^3 of rooftop storage is available in the 100-year event. For additional details on the calculations for available area of rooftop storage, refer to *Appendix D*.

Table 6 below summarize the release rates and storage volumes required to meet the allowable release rate of **6.63 L/s** for 100-year flow rates.

Catchment Area	Drainage Area (ha)	100-year Release Rate (L/s)	100-Year Required Storage (m ³)	Total Available Storage (m ³)
WS-01 (Un-controlled)	0.023	9.13	0	0
WS-02 (Roof Controlled)	0.023	1.26	8.26	9.00
TOTAL	0.046	10.39	8.26	9.00

All overland stormwater captured will ultimately be conveyed, via underground storm sewers, to the City storm sewer running along 161 Hinchey Avenue at a maximum release rate of **10.39 L/s** (calculated controlled and uncontrolled flow). As per coordination with City of Ottawa staff, the subject site was permitted to exceed the specified allowable release rate by **3.76 L/s** in order to avoid the use of small inlet control devices that may cause maintenance issues.

Therefore, it is calculated that a total of **8.26** m^3 of rooftop storage will be required to attenuate flows to the release rate of **10.39** L/s. The project runoff exceeding the allowable release rate will be stored on-site via rooftop ponding at the building rooftop. The 100-year maximum ponding extents can be found on drawing "C601 – Stormwater Management Plan" of *Appendix E*.

8 EROSION AND SEDIMENT CONTROL

During construction, erosion and sediment controls will be provided primarily via a sediment control fence to be erected along the perimeter of the site where runoff has the potential of leaving the site. Inlet sediment control devices are also to be provided in any catch basin and/or manholes in and around the site that may be impacted by the site construction. Construction and maintenance requirements for erosion and sediment controls are to comply with Ontario Provincial Standard Specification OPSS 577. Refer to LRL Associates drawing C.101 for erosion and sediment control details.

9 CONCLUSION

This Stormwater Management and Servicing Report for the development proposed at 161 Hinchey Avenue presents the rationale and details for the servicing requirements for the subject property. In accordance with the report objectives, the servicing requirements for the development are summarized below:

Water Service

- The maximum required fire flow was calculated at **9,000 L/min** using the FUS method.
- There are three (3) existing fire hydrants available to service the proposed development which will provide a combined fire flow of **13,248 L/min** to the site.
- The new development/expansion will be serviced with a new 150 mm dia. water service to be connected to the existing 150 mm dia. watermain within Hinchey Avenue.
- Boundary conditions received from the City of Ottawa indicate that sufficient pressure is available to service the proposed site.

Sanitary Service

- The anticipated sanitary flow from the proposed development is **0.34 L/s**.
- The proposed development will be serviced by a 150 mm dia. sanitary service that connects to the existing 250 mm dia. sanitary sewer within Hinchey Avenue.

Stormwater Management

- Stormwater quality control is not required as per consultation with RVCA.
- As per coordination with City of Ottawa staff, the stormwater release rates from the proposed development will exceed the calculated allowable release rate of 6.63 L/s, by an additional 3.76 L/s, to discharge at a maximum release rate of 10.39 L/s during 100-yr storm event.
- Stormwater quantity control objectives will be met through on-site storm water ponding on the roof.

10 REPORT CONDITIONS AND LIMITATIONS

The report conclusions are applicable only to this specific project described in the preceding pages. Any changes, modifications or additions will require a subsequent review by LRL Associates Ltd. to ensure the compatibility with the recommendations contained in this document. If you have any questions or comments, please contact the undersigned.

Prepared by: LRL Associates Ltd.

Amr Salem Civil Designer



Mohan Basnet, P.Eng. Civil Engineer

APPENDIX A

Pre-consultation / Correspondence

Project #: 200295	
Date: 2020-07-30	
4.1 General Content Executive Summary (for larger reports only).	N/A
Date and revision number of the report.	Report Cover Hsee
Location map and plan showing municipal address, boundary, and layout of proposed development.	Drawings/Figures
Plan showing the site and location of all existing services.	Figure 1
Development statistics, land use, density, adherence to zoning and official plan, and reference to applicable subwatershed and watershed plans that provide context to which individual developments must adhere.	Section 1.0
Summary of Pre-consultation Meetings with City and other approval agencies.	Section 4.0 & Appen A
Reference and confirm conformance to higher level studies and reports (Master Servicing Studies, Environmental Assessments, Community Design Plans), or in the case where it is not in conformance, the proponent must provide justification and develop a defendable design criteria.	Section 5.1, 6.1, 7.
Statement of objectives and servicing criteria.	Section 1.0
Identification of existing and proposed infrastructure available in the immediate area.	Section 5.1, 6.1, 7.
Identification of Environmentally Significant Areas, watercourses and Municipal Drains potentially impacted by the proposed development (Reference can be made to the Natural Heritage Studies, if available).	Section 7.0
Concept level master grading plan to confirm existing and proposed grades in the development. This is required to confirm the feasibility of proposed stormwater management and drainage, soil removal and fill constraints, and potential impacts to neighbouring properties. This is also required to confirm that the proposed grading will not impede existing major system flow paths.	C301

Identification of potential impacts of proposed piped services on private services (such as wells and septic fields on adjacent lands) and mitigation required to address potential impacts.	N/A		
Proposed phasing of the development, if applicable.	N/A		
Reference to geotechnical studies and recommendations concerning servicing.	C401		
All preliminary and formal site plan submissions should have the following information:			
∘Metric scale			
∘North arrow (including construction North)			
∘⊠ey plan			
∘Name and contact information of applicant and property owner	C401		
 Property limits including bearings and dimensions 			
∘Existing and proposed structures and parking areas			
∘Easements, road widening and rights-of-way			
∘Adjacent street names			
4.2 Development Servicing Report: Water			
Confirm consistency with Master Servicing Study, if available	N/A		
Availability of public infrastructure to service proposed development	Section 5.1		
Identification of system constraints	Section 5.1		
Identify boundary conditions	Section 5.2		
Confirmation of adequate domestic supply and pressure	Section 5.2		

Confirmation of adequate fire flow protection and confirmation that fire flow is calculated as per the Fire Underwriter's Survey. Output should Section 5.2 show available fire flow at locations throughout the development.

Provide a check of high pressures. If pressure is found to be high, an assessment is required to confirm the application of pressure reducing valves.	Section 5.2
Definition of phasing constraints. Hydraulic modeling is required to confirm servicing for all defined phases of the project including the ultimate design	N/A
Address reliability requirements such as appropriate location of shut-off valves	N/A
Check on the necessity of a pressure zone boundary modification.	N/A
Reference to water supply analysis to show that major infrastructure is capable of delivering sufficient water for the proposed land use. This includes data that shows that the expected demands under average day, peak hour and fire flow conditions provide water within the required pressure range	Section 5.2
Description of the proposed water distribution network, including locations of proposed connections to the existing system, provisions for necessary looping, and appurtenances (valves, pressure reducing valves, valve chambers, and fire hydrants) including special metering provisions.	Section 5.2
Description of off -site required feedermains, booster pumping stations, and other water infrastructure that will be ultimately required to service proposed development, including financing, interim facilities, and timing of implementation.	N/A
Confirmation that water demands are calculated based on the City of Ottawa Design Guidelines.	Section 5.2
Provision of a model schematic showing the boundary conditions locations, streets, parcels, and building locations for reference.	N/A
4.3 Development Servicing Report: Wastewater	
Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitored flow data from relatively new infrastructure cannot be used to justify capacity requirements for proposed infrastructure).	Section 6.2
Confirm consistency with Master Servicing Study and/or justifications for deviations.	N/A

Consideration of local conditions that may contribute to extraneous flows that are higher than the recommended flows in the guidelines. This includes groundwater and soil conditions, and age and condition of sewers.	N.A
Description of existing sanitary sewer available for discharge of wastewater from proposed development.	Section 6.1
Verify available capacity in downstream sanitary sewer and/or identification of upgrades necessary to service the proposed development. (Reference can be made to previously completed Master Servicing Study if applicable)	Section 6.2
Calculations related to dry-weather and wet-weather flow rates from the development in standard MOE sanitary sewer design table (Appendix 'C') format.	Section 6.2 Appendix C
Description of proposed sewer network including sewers, pumping stations, and forcemains.	Section 6.2
Discussion of previously identified environmental constraints and impact on servicing (environmental constraints are related to limitations imposed on the development in order to preserve the physical condition of watercourses, vegetation, soil cover, as well as protecting against water quantity and quality).	N/A
Pumping stations: impacts of proposed development on existing pumping stations or requirements for new pumping station to service development.	Section 6.1
Forcemain capacity in terms of operational redundancy, surge pressure and maximum flow velocity.	N/A
Identification and implementation of the emergency overflow from sanitary pumping stations in relation to the hydraulic grade line to protect against basement flooding.	N/A
Special considerations such as contamination, corrosive environment etc.	N/A
4.4 Development Servicing Report: Stormwater Checklist	
Description of drainage outlets and downstream constraints including legality of outlets (i.e. municipal drain, right-of-way, watercourse, or private property)	Section 7.1

Analysis of available capacity in existing public infrastructure.	N/A
A drawing showing the subject lands, its surroundings, the receiving watercourse, existing drainage patterns, and proposed drainage pattern.	N/A
Water quantity control objective (e.g. controlling post-development peak flows to pre-development level for storm events ranging from the 2 or 5 year event (dependent on the receiving sewer design) to 100 year return period); if other objectives are being applied, a rationale must be included with reference to hydrologic analyses of the potentially affected subwatersheds, taking into account long-term cumulative effects.	Section 7.2.2
Water Quality control objective (basic, normal or enhanced level of protection based on the sensitivities of the receiving watercourse) and storage requirements.	Section 7.2.1
Description of the stormwater management concept with facility locations and descriptions with references and supporting information.	Section 7.4
Set-back from private sewage disposal systems.	N/A
Watercourse and hazard lands setbacks.	N/A
Record of pre-consultation with the Ontario Ministry of Environment and the Conservation Authority that has jurisdiction on the affected watershed.	N/A
Confirm consistency with sub-watershed and Master Servicing Study, if applicable study exists.	N/A
Storage requirements (complete with calculations) and conveyance capacity for minor events (1:5 year return period) and major events (1:100 year return period).	Section 7.4
Identification of watercourses within the proposed development and how watercourses will be protected, or, if necessary, altered by the proposed development with applicable approvals.	N/A
Calculate pre and post development peak flow rates including a description of existing site conditions and proposed impervious areas and drainage catchments in comparison to existing conditions.	Section 7.4 Appendix D

Any proposed diversion of drainage catchment areas from one outlet to another.	N/A
Proposed minor and major systems including locations and sizes of stormwater trunk sewers, and stormwater management facilities.	Appendix D
If quantity control is not proposed, demonstration that downstream system has adequate capacity for the post-development flows up to and including the 100 year return period storm event.	N/A
Identification of potential impacts to receiving watercourses Identification of municipal drains and related approval requirements.	N/A
Descriptions of how the conveyance and storage capacity will be achieved for the development.	Section 7.4
100 year flood levels and major flow routing to protect proposed development from flooding for establishing minimum building elevations (MBE) and overall grading.	NA
Inclusion of hydraulic analysis including hydraulic grade line elevations.	N/A
Description of approach to erosion and sediment control during construction for the protection of receiving watercourse or drainage corridors.	Section 8.0
Identification of floodplains – proponent to obtain relevant floodplain information from the appropriate Conservation Authority. The proponent may be required to delineate floodplain elevations to the satisfaction of the Conservation Authority if such information is not available or if information does not match current conditions.	N/A
Identification of fill constraints related to floodplain and geotechnical investigation	N/A
4.5 Approval and Permit Requirements: Checklist	

Conservation Authority as the designated approval agency for modification of floodplain, potential impact on fish habitat, proposed works in or adjacent to a watercourse, cut/fill permits and Approval under Lakes and Rivers Improvement Act. The Conservation Authority is not the approval authority for the Lakes and Rivers Improvement Act. Where there are Conservation Authority regulations in place, approval under the Lakes and Rivers Improvement Act is not required, except in cases of dams as defined in the Act.

Application for Certificate of Approval (CofA) under the Ontario Water Resources Act.	N/A
Changes to Municipal Drains.	N/A

Other permits (National Capital Commission, Parks Canada, Public Works and Government Services Canada, Ministry of Transportation etc.)

4.6 Conclusion Checklist

Clearly stated conclusions and recommendations		
Comments received from review agencies including the City of Ottawa and information on how the comments were addressed. Final sign-off from the responsible reviewing agency.	Noted	
All draft and final reports shall be signed and stamped by a professional Engineer registered in Ontario	Noted	

161 Hinchey Avenue – Infrastructure Notes

Available Infrastructure:

Sanitary: 250mm PVC (Install 2000) Storm: 375mm Conc (Install 2000) Water: 150mm PVC (Install 2000)

Water Boundary Conditions:

Will be provided at request of consultant. Requests must include the location of the service and the expected loads required by the proposed development. Please provide the following and <u>submit Fire Flow Calculation Sheet</u> per FUS method with the request:

- Location of service
- Type of development and amount of required fire flow (per FUS method <u>include FUS</u> <u>calculation sheet with request</u>)
- Average Daily Demand (I/s)
- Maximum Hourly Demand (I/s)
- Maximum Daily Demand (I/s)
- Water Supply Redundancy Fire Flow: Applicant to ensure that a second service with an inline valve chamber be provided where the average daily demand exceeds 50 m³ / day (0.5787 l/s per day)

Water services larger than 19 mm require a Water Data Card. Please complete card and submit.

Stormwater Management:

- Coefficient (C) of runoff determined **as per existing conditions** but in no case more than 0.5
- TC = To be calculated, minimum 10 minutes
- Any storm events greater than 5 year, up to 100 year, and including 100-year storm event must be detained on site.
- Foundation drains are to be independently connected to sewer main unless being pumped with appropriate back up power, sufficient sized pump and back flow prevention.
- Roof drains are to be connected downstream of any incorporated ICD within the SWM system.

Stormwater management criteria (Quality Control)

Include a section in the SWM report concerning quality control requirements. It is the consultant's responsibility to check with the relevant Conservation Authority for quality control issues and include this information in the SWM report.

Phase I and Phase II ESA:

- Phase I ESA is required; Phase II ESA may be required depending on the results of the Phase I ESA. Phase I ESA must include an EcoLog ERIS Report.
- Phase I ESA and Phase II ESAs must conform to clause 4.8.4 of the Official Plan that requires that development applications conform to Ontario Regulation 153/04.

Required Studies

- Stormwater Management Report
- Site Servicing Study
- Geotechnical Study
- Phase I ESA
- Phase II ESA (depends on outcome of Phase I)

Required Plans

- Site Servicing Plan
- Grade Control and Drainage Plan
- Erosion and Sediment Control Plan (Can be combined with grading plan)

Relevant information

- 1. The Servicing Study Guidelines for Development Applications are available at the following address: <u>https://ottawa.ca/en/city-hall/planning-and-development/information-development-application-review-process/development-application-submission/guide-preparing-studies-and-plans#servicing-study-guidelines-development-applications</u>
- 2. Servicing and site works shall be in accordance with the following documents:
 - ⇒ Ottawa Sewer Design Guidelines (October 2012)
 - ⇒ Ottawa Design Guidelines Water Distribution (2010)
 - ➡ Geotechnical Investigation and Reporting Guidelines for Development Applications in the City of Ottawa (2007)
 - ⇒ City of Ottawa Slope Stability Guidelines for Development Applications (revised 2012)
 - ⇒ City of Ottawa Environmental Noise Control Guidelines (January, 2016)
 - ⇒ City of Ottawa Park and Pathway Development Manual (2012)
 - ⇒ City of Ottawa Accessibility Design Standards (2012)
 - ⇒ Ottawa Standard Tender Documents (latest version)
 - ⇒ Ontario Provincial Standards for Roads & Public Works (2013)
- Record drawings and utility plans are also available for purchase from the City (Contact the City's Information Centre by email at <u>InformationCentre@ottawa.ca</u> or by phone at (613) 580-2424 x.44455).
- 4. Any proposed work in utility easements requires written consent of easement owner.

Amr Salem

From:	Jamie Batchelor <jamie.batchelor@rvca.ca></jamie.batchelor@rvca.ca>
Sent:	July 9, 2020 11:40 AM
To:	Amr Salem
Cc:	Mohan Basnet; Maxime Longtin
Subject:	RE: 161 Hinchey Avenue - Stormwater Quality Controls
Follow Up Flag:	Follow up
Flag Status:	Flagged

Good Morning Amr,

Given that the site will have no surface parking areas proposed, no additional water quality control will be required save and except best management practices.

Jamie Batchelor, MCIP, RPP Planner, ext. 1191 Jamie.batchelor@rvca.ca



3889 Rideau Valley Drive PO Box 599, Manotick ON K4M 1A5 T 613-692-3571 | 1-800-267-3504 F 613-692-0831 | www.rvca.ca

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From: Amr Salem <asalem@lrl.ca>
Sent: Monday, July 6, 2020 2:52 PM
To: Jamie Batchelor <jamie.batchelor@rvca.ca>
Cc: Mohan Basnet <mbasnet@lrl.ca>; Maxime Longtin <mlongtin@lrl.ca>
Subject: 161 Hinchey Avenue - Stormwater Quality Controls

Good morning Jamie,

I wanted to consult with you regarding a residential development we are working on located at 161 Hinchey Avenue.

Existing runoff from the site drains into municipal sewer along Hinchey Ave and travels approx. 610m before discharging into the Ottawa River.

The development proposes a residential 4-storey building, with <u>no surface parking</u>. The site will be landscape with stormwater coming primarily from rooftop and landscaped rear yard. *Refer to draft site plan attached for reference*.

Existing site area consists of an existing residential building and paved area.

Please provide your input about quality controls that may be required for this site.



Thank you,



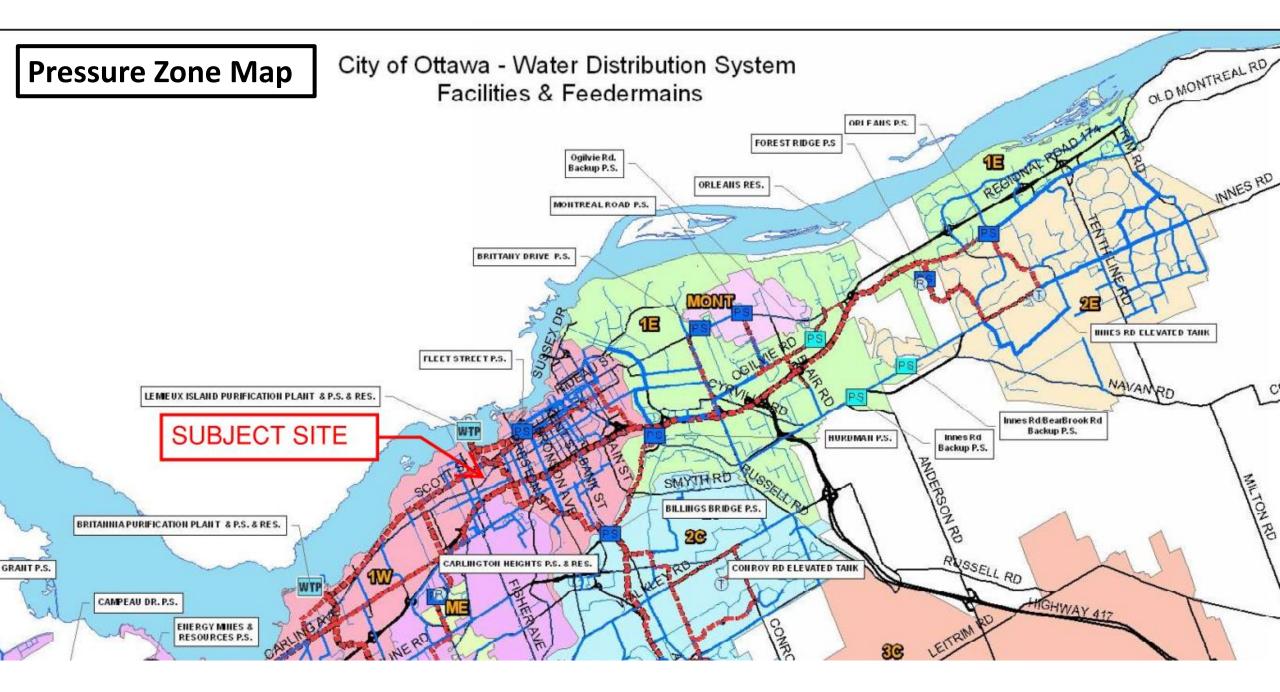
Amr Salem Civil Designer LRL Associates Ltd. 5430 Canotek Road Ottawa, Ontario K1J 9G2 T (613) 842-3434 or (877) 632-5664 ext 248 F (613) 842-4338 E asalem@lrl.ca W www.lrl.ca

We care deeply, so let us know how we did by completing our <u>Customer Satisfaction Survey</u>. Nous nous soucions profondément de votre opinion, nous vous invitons donc à nous faire savoir si nous avons satisfait vos attentes en remplissant notre <u>sondage sur la satisfaction de la clientèle</u>



APPENDIX B

Water Supply Calculations



Water Supply Calculations



LRL File No. 200295 Date September 21, 2020 Prepared by Amr Salem

Residential Demand based on the City of Ottawa Design Guidelines-Water Distribution, 2010

Unit Type	Persons Per Unit	Number of Units	Population
1 Bedroom Apartment	1.4	9	12.6
2 Bedroom Apartment	2.1	6	12.6
	Total	15	25.2

Average Water Consumption Rate	280	L/c/d	
Average Day Demand	7,056	L/d	0.08 L/s
Maximum Day Factor	10.3		(MOE Table 3-3)
Maximum Daily Demand	72,654	L/d	0.84 L/s
Peak Hour Factor	15.5		(MOE Table 3-3)
Maximum Hour Demand	1,128,733	L/d	13.06 L/s

Water Service Pipe Sizing

Q = VA

Where: V = velocity A = area of pipe Q = flow rate

Assuming a maximum velocity of 1.8m/s, the diameter of pipe is calculated as:

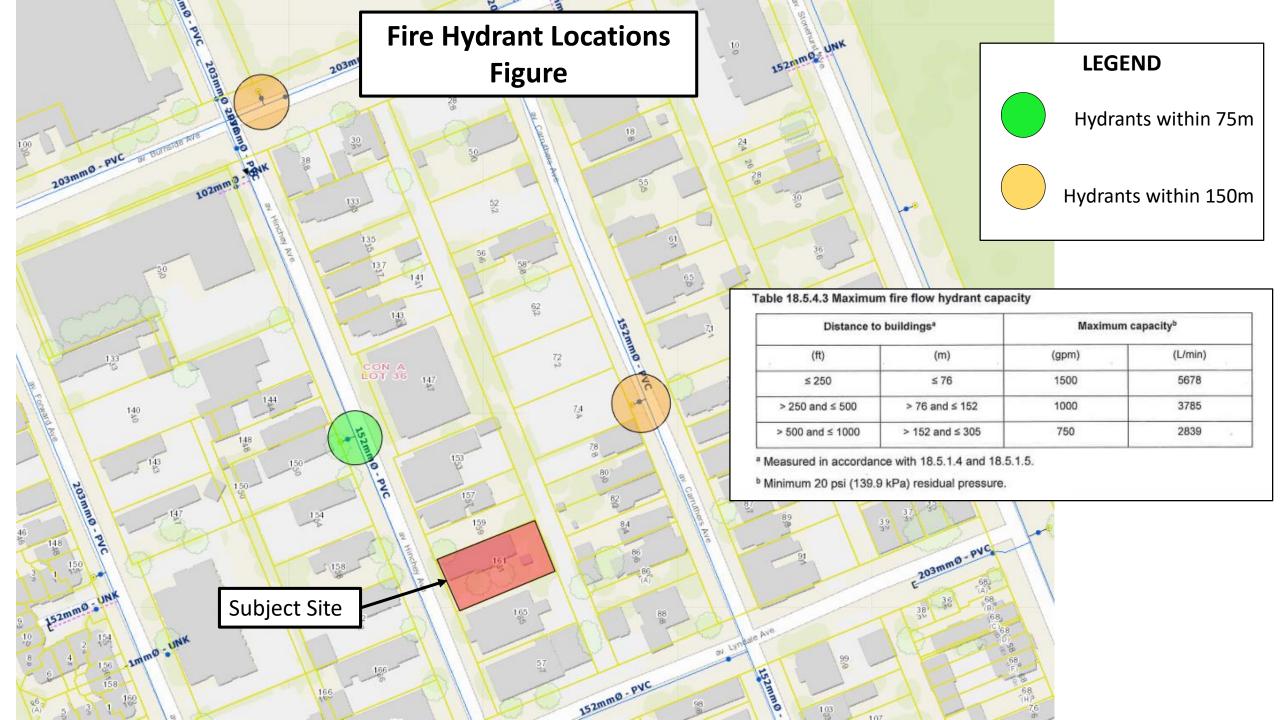
Minimum pipe diameter (d) =	(4Q/πV) ^{1/2}	
=	0.096	m
=	96	mm
Proposed pipe diameter (d) =	150	mm
=	6	Inches



Fire Flow Calculations

LRL File No.	200295		
Date	July 14, 2020		
Method	Fire Underwriters Survey (FUS)		
Prepared by	Amr Salem		

Step	Task	Term	Options	Multiplier	Choose:	Value	Unit	Fire Flow	
Structural Framing Material									
1	Choose frame used for building	Coefficient C related to the type of construction	Wood Frame	1.5	Ordinary Construction	1			
			Ordinary Construction	1.0					
			Non-combustible construction	0.8					
			Fire resistive construction <2 hrs	0.7					
			Fire resistive construction >2 hrs	0.6					
	Floor Space Area (A)								
2			Total area			1,104	m ²		
3	Obtain fire flow before reductions	Required fire flow	Fire Flow = 220 x C x A ^{0.5}				L/min	7,310	
	Reductions or surcharge due to factors affecting burning								
		Occupancy hazard reduction or surcharge	Non-combustible	-25%	Limited combustible -1			6,213	
4			Limited combustible	-15%		-15%	L/min		
			Combustible	0%					
			Free burning	15%					
			Rapid burning	25%					
	Choose reduction for sprinklers	Sprinkler reduction	Full automatic sprinklers	-30%	False	0%	L/min	5,592	
5			Water supply is standard for both the system and fire department hose lines	-10%	True	-10%			
			Fully supervised system	-10%	False	0%			
6	Choose separation	Exposure distance between units	North side	3.1 to 10m	20%		L/min	9,227	
			East side	20.1 to 30m	10%				
°			South side	3.1 to 10m	20%				
			West side	10.1 to 20m	15%	65%			
Net required fire flow									
	Obtain fire flow, duration, and volume	Minimum required fire flow rate (rounded to nearest 1000)						9,000	
7		Minimum required fire flow rate						150.0	
		Required duration of fire flow					hr	2	



Amr Salem

From:	Fawzi, Mohammed <mohammed.fawzi@ottawa.ca></mohammed.fawzi@ottawa.ca>
Sent:	July 17, 2020 1:52 PM
To:	Amr Salem
Cc:	Mohan Basnet
Subject:	RE: 200295 - 161 Hinchey Avenue Boundary Conditions Request
Attachments:	161 Hinchey July 2020.pdf
Follow Up Flag:	Follow up
Flag Status:	Completed

Good Afternoon Amr,

The following are boundary conditions, HGL, for hydraulic analysis at 161 Hinchey (zone 1W) assumed to be connected to the 152mm on Hinchey (see attached PDF for location).

Minimum HGL = 106.5m Maximum HGL = 115.2m MaxDay + FireFlow (150 L/s) = 93.0m

These are for current conditions and are based on computer model simulation.

Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation.

Thank you.

Best Regards,

Mohammed Fawzi, E.I.T. Engineering Intern Planning, Infrastructure and Economic Development Department - Services de la planification, de l'infrastructure et du développement économique Development Review - Central Branch City of Ottawa | Ville d'Ottawa 110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1 613.580.2424 ext./poste 20120, <u>Mohammed.Fawzi@ottawa.ca</u>

From: Fawzi, Mohammed Sent: July 17, 2020 11:23 AM To: Amr Salem <asalem@lrl.ca>
Cc: Mohan Basnet <mbasnet@lrl.ca>
Subject: RE: 200295 - 161 Hinchey Avenue Boundary Conditions Request

Hi Amr,

Thank you. The request has been sent.

Best Regards,

Mohammed Fawzi, E.I.T.

Engineering Intern Planning, Infrastructure and Economic Development Department - Services de la planification, de l'infrastructure et du développement économique Development Review - Central Branch City of Ottawa | Ville d'Ottawa 110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1 613.580.2424 ext./poste 20120, <u>Mohammed.Fawzi@ottawa.ca</u>

From: Amr Salem <<u>asalem@lrl.ca</u>> Sent: July 15, 2020 1:36 PM To: Fawzi, Mohammed <<u>mohammed.fawzi@ottawa.ca</u>> Cc: Mohan Basnet <<u>mbasnet@lrl.ca</u>> Subject: 200295 - 161 Hinchey Avenue Boundary Conditions Request

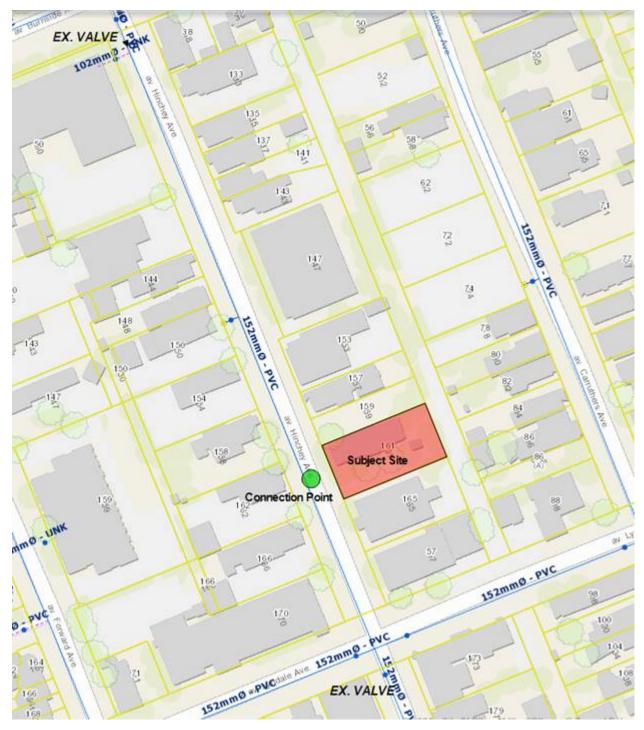
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ATTENTION : Ce courriel provient d'un expéditeur externe. Ne cliquez sur aucun lien et n'ouvrez pas de pièce jointe, excepté si vous connaissez l'expéditeur.

Good afternoon Mohammed,

We would like to kindly request boundary conditions for the proposed development at *161 Hinchey Avenue* using the following proposed development demands:

- Location of Service / Street Number: 161 Hinchey Ave
- Type of development: one 4-storey residential building consisting of a total of 12 units.
- Proposed Connection Point: a single connection the 150mm watermain along Hinchey Avenue .



• Please provide pressures for the following water demand scenarios required for the proposed development:

	L/min	L/s
Avg. Daily	3.6	0.06
Max Day + FUS	42.0 + 9,000	0.70 + 150
Peak Hour	747.0	12.45

Please contact me if you have any questions.



Thanks,

Amr Salem Civil Designer LRL Associates Ltd. 5430 Canotek Road Ottawa, Ontario K1J 9G2 T (613) 842-3434 or (877) 632-5664 ext 2

E <u>asalem@lrl.ca</u> W www.lrl.ca

T (613) 842-3434 or (877) 632-5664 ext 248 F (613) 842-4338

We care deeply, so let us know how we did by completing our <u>Customer Satisfaction Survey</u>. Nous nous soucions profondément de votre opinion, nous vous invitons donc à nous faire savoir si nous avons satisfait vos attentes en remplissant notre <u>sondage sur la satisfaction de la clientèle</u>



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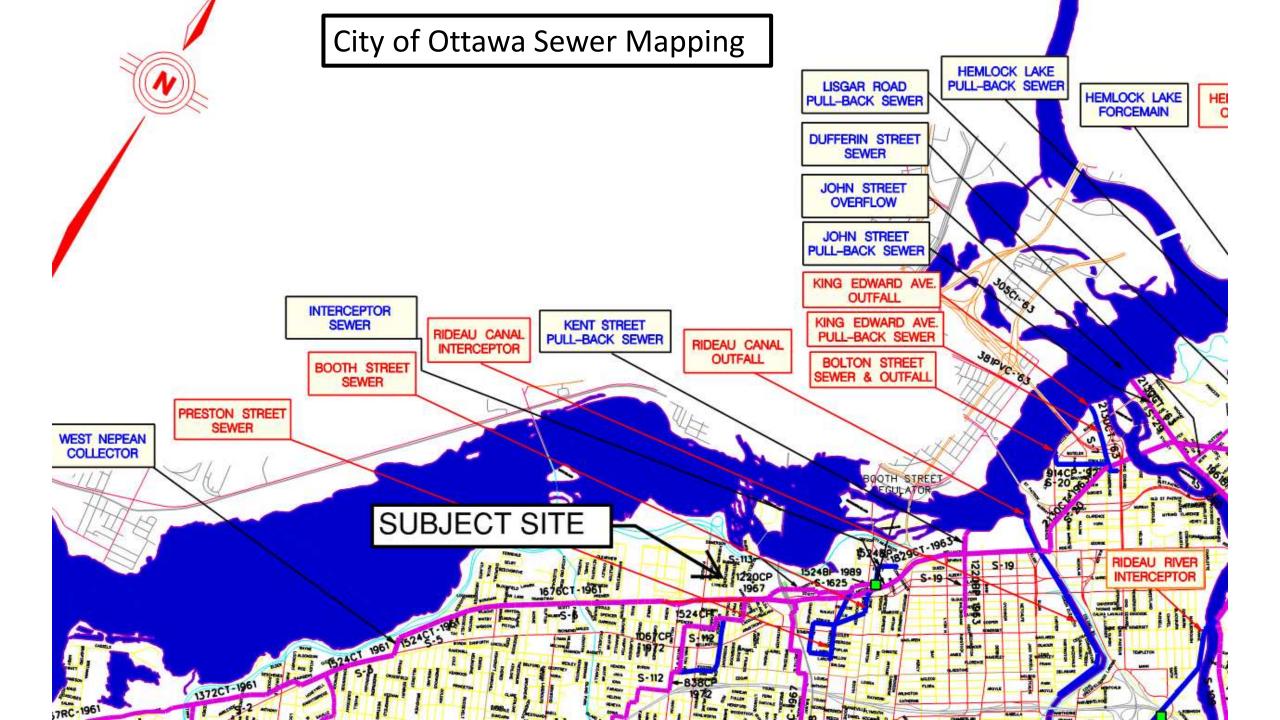
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APPENDIX C

Wastewater Collection Calculations



		LRL File No Project: Location: Date:).	200295 Apartment I 161 Hinche April 19, 20	y Avenue					Commerce Light Indus Heavy Ind Maximum	al & Institu strial Flow ustrial Flov Residentia	= 280 L/p/d Itional Flow = 35000 L/l w = 55000 l al Peak Fac Itional Peak	= 50000 L ha/day _/ha/day tor = 4.0	·				rameters Peak Facto us Flow = 0	•		4-B = 7			Pipe Design Minimum Ve Manning's n	locity = 0.6		
	LOCATION			RESIDEN	ITIAL ARE	A AND POP	ULATION		COMM	ERCIAL	I	NDUSTRIA	L	INSTITU	TIONAL	C+I+I	IN	IFILTRATIO	ON				F	PIPE			
STREET	FROM MH	TO MH	AREA (Ha)	POP.	CUMM AREA (Ha)	POP.	PEAK FACT.	PEAK FLOW (l/s)	AREA (Ha)	ACCU. AREA (Ha)	AREA (Ha)	ACCU. AREA (Ha)	PEAK FACT.	AREA (Ha)	ACCU. AREA (Ha)	PEAK FLOW (l/s)	TOTAL AREA (Ha)	ACCU. AREA (Ha)	INFILT. FLOW (I/s)	TOTAL FLOW (l/s)	LENGTH (m)	DIA. (mm)	SLOPE (%)	MATERIAL	CAP. (FULL) (I/s)	VEL. (FULL) (m/s)	
SITE	PROP. BLDG	EX. SAN	0.046	25.2	0.05	25.2	4.0	0.33	0.000	0.000	0.00	0.00	7.0	0.0	0.0	0.00	0.05	0.05	0.02	0.34	7.4	150	2.00%	PVC	21.54	1.22	
NOTES	Existing inverts	and slopes a	re estimate	ed. They are t	to be confin	med on-site.]		Designed: Checked:	A.S. M.B.							Apartme LOC	OJECT: ent Building CATION: chey Avenu				
														Dwg. Refe	erence: C.401		File Ref.:	200	295		Date:	202	1-04-19			Sheet N 1 of 1	

APPENDIX D

Stormwater Management Calculations Watts Roof Drain Specification

LRL Associates Ltd. Storm Watershed Summary

	LRL File No.	200295
	Project:	Apartment Building
	Location:	161 Hinchey Ave
	Date:	July 6, 2021
	Designed:	Amr Salem
INGINEERING I INGÉNIERIE	Drawing Reference:	C701/C702

Pre-Development Catchments

WATERSHED	C = 0.2	C = 0.70	C = 0.90	Total Area (m ²)	Total Area (ha)	Combined C
EWS-01	226.0	0.0	232.0	458.0	0.0458	0.55
TOTAL	226.0	0.0	232.0	458.0	0.0458	0.55

Post-Development Catchments

WATERSHED	C = 0.20	C = 0.70	C = 0.90	Total Area (m ²)	Total Area (ha)	Combined C
WS-01(UNCONTROLLED)	88.0	5.0	140.0	233.0	0.023	0.63
WS-02 (CONTROLLED)	0.0	0.0	225.0	225.0	0.023	0.90
TOTAL	88.0	5.0	365.0	458.0	0.0458	0.76

		LRL File No. Project: Location: Date: Designed: Drawing Ref.:	200295 Apartment Building 161 Hinchey Ave July 6, 2021 Amr Salem C.601			Storm	water Managerr Design Sheet	ient]
off Equation									
	Q = 2.78CIA (L/s	0							
	C = Runoff coeffi	cient							
	I = Rainfall inten	sity (mm/tr)	= A / (Td + C) [®]						
	A = Area (ha) T _c = Time of cono								
	1 ₄ = 1 ime of cono	entration (min)							
development Stor	mwater Managemer I _{s =} 998.071 / (Te	11 d + 6.053) ^{0.814}		a =	998.071	b=	0.814	c	6.053
	C = 0.50	max of 0.5 as pe	r City of Ottawa						
	1= 104.2	mmhr	or only of onland						
	Tc = 10	min							
Total A	Area = 0.046	ha							
Allow	vable Release Rate:	6.63	L/s						
t-development Sto	rmwater Manageme	_					۶R _{ms}	ΣR _{sea}	1
		Total Site WS-02		0.046	ha	SR=	0.76	0.95	-
Controlled		WS-02 Total Cor		0.023	ha	SB=	0.90	1.00	1
Un-controlled		WS- Total Un-Cr	01	0.023	ha	Be	0.63	0.79	
Children		Total Un-Ci	ontrolled =	0.023	ha	5B=	0.63	0.79	
Year Storm Event:					1735.688		0.820	. c.	6.014
	1 - 1795 699 / /7								
	l _{ent} = 1735.688 / (1				1735.966		0.020		
Time (min)	Intensity	Uncontrolled	Controlled Release Rate	Total Release Rate	1735,866		0.020		
Time (min) 10 t-development Sto		Uncontrolled Runoff (L/s) 9.13	Constant (L/s) 0.00		1/35.866				
10	Intensity (mm/hr) 178.6 rmwater Manageme	Uncontrolled Runoff (L/s) 9.13 ant (WS-02 On Ro	Constant (L/s) 0.00	a Total Release Rate (L/s) 9.13]				
10 t-development Sto	Intensity (mm/hr) 178.6	Uncontrolled Runoff (L/s) 9.13 ant (WS-02 On Ro	Constant (L's) 0.00	a Total Release Rate (L/s) 9.13]		0.820		= 6.014
10 t-development Sto	Intensity (mm/hr) 178.6 rmwater Manageme	Uncontrolled Runoff (L/s) 9.13 ant (WS-02 On Ro	Constant (L/s) 0.00	Total Release Rate (Us) 9.13]				
10 t-development Sto	Intensity (mm/hr) 178.6 rmwater Manageme	Uncontrolled Runoff (L/s) 9.13 ant (WS-02 On Ro	Constant (L's) 0.00	Total Release Rate (Us) 0.13 a = Controlled Release]				
10 E-development Sto Year Storm Evert: Time (min)	Intensity (mm/hr) 178.6 wmwater Manageme km = 1735.688 / (1 Intensity (mm/hr)	Uncontrolled Runoff (Lis) 9.13 ant (WS-02 On Ro Fd + 6.014) ^{0.800} Controlled Runoff (Lis)	Constant (L's) 0.00 of) Storage Required Storage Volume (m ²)	a Total Release Rate (L/s) 9.13 9.13 a = Controlled Release Rate Constant (L/s)	1735.688 Uncontrolled Runoff (L/s)	b = Total Release Rate (Us)			
10 t-development Sto Year Storm Evert: Time (min) 10	Intensity (mm/br) 178.6 mmwater Manageme Las = 1735.688 / (1 Intensity (mm/br) 178.6	Uncontrolled Runoff (L/s) 9.13 ant (WS-02 On Ro rd + 6.014) ^{6.00}	Constant (L'a) 0.00 eff Storage Required Storage Volume (m ²) 5.95	a Total Release Rate (Lia) 9.13 a = Controlled Release Rate Constant (Lia) 1.26	1735.688 Uncontrolled Ranoff (L/s) 0.0.0	b = Total Release Rate (L/s) 1.26			
10 I-development Sto Year Storm Event: Time (min) 15	Intensity (mm/hr) 178.5 mmwater Manageme km = 1735.688 / (1 Intensity (mm/hr) 178.6 142.9	Uncontrolled Runoff (Lis) 9.13 ant (WS-02 On Ro Fd + 6.014) ^{0.800} Controlled Runoff (Lis)	Constant (L's) 0.00 of) Storage Required Storage Volume (m ²) 5.95 6.91	Total Release Rate (U3) 0.13 0.13 Controlled Release Rate Constant (U3) 1.26	1735.688 Uncontrolled Runoff (L/s)	b = Total Release Rate (Us)			
10 I-development Sto Year Storm Event: Time (min) 10 15 20 25	Intensity (mm/br) 178.6 mmwater Manageme Isaa = 1735.688 / (1 Intensity (mm/br) 178.6 142.9 120.0 103.8	Uncontrolled Runoff (Lis) 9.13 ant (WS-02 On Ro (WS-02 On Ro)(WS-02 On Ro (WS-02 On Ro)(WS-02 ON	Storage Required Storage Required Storage Volume (m ²) 9.91 7.85	Total Release Rate (U3) (U3) 0.13 0.13 Controlled Release Rate Constant (U3) 1.26 1.26 1.26	1735.688 Uncontrolled Runoff (Us) 0.00 0.00 0.00	b = Total Release Rate (Us) 1.26 1.26 1.26			
10 i-development Sto Year Storm Evert: <u>Time (min)</u> 10 15 20 25 30	Intensity (mms br) 178.6 mmwater Manageme Las = 1735.688 / (1 Intensity (mms br) 1728.6 142.9 122.0 103.8 91.9	Uncontrolled Runotff (Lis) 9.13 ant (WS-02 On Ro Td + 6.014) ^{0.800} Controlled Runoff (Lis) 11.17 8.94 7.50 6.50 5.75	Constant (L/3) 0.00 efg Storage Required Storage Volume (m ²) 6.95 1.749 7.49 7.49 8.06	Total Release Rate (U3) 9.13 9.13 2.13 Controlled Release Rate Constance (U3) (U3) (1.26 1.26 1.26 1.26 1.26	1735.688 Uncontrolled Runoff (Lis) 0.00 0.00 0.00 0.00	b = Total Rolexia Rate (Lia) 1.26 1.26 1.26 1.26			
10 - development Sto - Vear Storm Event: 	Intensity (mm/br) 178.6 mmwater Manageme has = 1735.688 / (1 Intensity (mm/br) 178.6 142.9 120.0 103.8 91.9 82.6	Uncontrolled Runoff (Lis) 9.13 ant (WS-02 On Ro Controlled Runoff (Lis) 11.17 8.94 7.50 5.75 5.17	Constant (L's) 0.00 off Storage Required Storage Volume (m ²) 6.55 6.91 7.46 8.08 8.08 8.08 8.08 8.08 8.08 8.08 8.0	a Total Release Rate (Us) 0.13 a = Controlled Release Rate Constant (Us) 1.26 1.26 1.26 1.26 1.26	1735.688 Uncontrolled Runoff (Us) 0.00 0.00 0.00 0.00 0.00	b = Total Release Rate (Us) 126 126 126 126 126 126			
10 I-development Sto Year Storm Evert: Time (min) 15 20 25 30 35 40	Intensity (mms/br) 178.6 mmwater Manageme Las = 1735.688 / (1 Intensity (mms/br) 1726.5 142.9 122.0 103.8 91.9 82.6 75.1	Uncontrolled Runoff (L5) 9.13 ant (WS-02 On Ro Controlled Runoff (L5) 11.17 8.94 7.50 6.50 5.75 5.17 4.70	Constant (Us) 0.00 0.00 eth Storage Required Storage Required Storage Required 9.00 Storage Required 9.00 Storage Required 9.00 0.00 0.00 0.00 0.00	a Total Release Rate (Lis) 0.13 0.13 a = Controlled Release Rate Constant (Lis) 1.26 1.26 1.26 1.26 1.26 1.26	1735.688 Uncontrolled Runoff (Us) 0.00 0.00 0.00 0.00 0.00 0.00 0.00	b = Total Rolesse Rate (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 1.26			
10 I-development Sto Year Storm Event: Time (min) 10 15 20 25 30 35 40 45 50	Intensity (mm.fbr) 178.6 immwater Manageme Intensity (mm.fbr) 178.6 1735.688 / (1 178.6 178.6 172.6 162.9 178.6 162.9 178.6 172.5 1735.688 / (1 178.6 1735.688 / (1 178.6 177.6 17	Uncontrolled Runoff (L/s) 9.13 et (WS-02 On Ro rd + 6.014) ^{6.800} Controlled Runoff (L/s) 11.17 5.75 6.50 5.75 5.17 4.70 4.32	Storage Required Storage R	■ Total Release Rate (Us) 0.13 ■ = Controlled Release Rate Constant (Us) 1.26 1.26 1.26 1.26 1.26 1.26	1735.688 Uncontrolled Runoff (L/s) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	b = Total Release Rate (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26			
10 	Intensity (mm.htv) 178.6 mmutar Manageme Intensity (mm.htv) 178.688 / (f) 178.6 142.9 120.0 102.5 120.0 102.5 120.0 120.	Uncontrolled Runoff (L.b.) 9.13 ant (WS-62 On Re Controlled Runoff (L.b.) 11.17 8.94 1.57 6.55 6.55 6.55 6.55 6.55 6.55 6.55 6	Constant (Ls) 0.00 0.00 eff Storage Required Storage Required 6.00 5.00 0.00 1 0.00 5.00 0.00 1 0.00 1 0.00 1 0.00 1 0.00 1 0.00 1 0.00 1 0.00 1 0.00 1 0.00 0 0.00 0 0.00 0 0.00	Total Release Rate (Lis) 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26	1735.688 Uncontrolled Rundff (Ls) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	b = Total Rebase Rate (Ls) 128 128 128 128 128 128 128 128 128 128			
10 E-development Sto Year Storm Evert: Time (min) 10 10 15 20 25 30 35 40 45 50 70	Intensity (men.hr) 178.6 Immuster Manageme hun = 1735.588 / (I Intensity (men.hr) 178.6 120.0 120.1 120.2 120.2 120.3 69.1 65.5 40.3	Uncontrolled Figure 17 (L's) 9.13 ent (WS-02 On Re ent (WS-02 On Re Controlled Runoff (L's) 6.50 5.75 5.17 5.17 5.17 4.70 4.32 4.00 3.50 3.51	Storage Required Storage Required Storage Volume (m ²) 5.8 5.9 7.85 8.08 8.08 8.20 8.22 8.22 8.05 7.79	Total Release Rate (L/S) 2.13 2.13 Controlled Release Rate Constant (L/S) 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26	1735.588 Uncontrolled Brandf (Ly) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	b = Total Rebase Rate (L/s) 128 128 128 128 128 128 128 128 128 128			
10 :-development Sto Year Storm Evert: Time (min) 10 15 20 25 30 40 40 50 50 80	Intensity (men.hg) 178.4 178.588/0 Intensity (men.hg) 178.588/0 Intensity (men.hg) 125.588/0 <td>Uncontrolled Runoff (L.b.) 9.13 Int (WS-62 On Ro Controlled Runoff (L.b.) 6.60 1.11, 7.50 6.50 6.50 6.50 6.50 6.50 6.50 6.50 6</td> <td>Constant (Ls) 0.00 0.00 eff 0.00 Storage Required 0.00 Storage Required 0.00 0.00 0.00 <</td> <td>Controlled Release Alexandree Controlled Release Rate Constant (L3) (L3)</td> <td>1735.688 Uncontrolled Runoff (Lu) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.</td> <td>b = Total Release Rate (Ls) 125 126 126 126 126 126 126 126 126 126 126</td> <td></td> <td></td> <td></td>	Uncontrolled Runoff (L.b.) 9.13 Int (WS-62 On Ro Controlled Runoff (L.b.) 6.60 1.11, 7.50 6.50 6.50 6.50 6.50 6.50 6.50 6.50 6	Constant (Ls) 0.00 0.00 eff 0.00 Storage Required 0.00 Storage Required 0.00 0.00 0.00 <	Controlled Release Alexandree Controlled Release Rate Constant (L3)	1735.688 Uncontrolled Runoff (Lu) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	b = Total Release Rate (Ls) 125 126 126 126 126 126 126 126 126 126 126			
10 E-development Sto Year Storm Evert: Time (min) 10 10 15 20 25 30 35 40 45 50 70	Intensity (men.hr) 178.6 Immuster Manageme hun = 1735.588 / (I Intensity (men.hr) 178.6 120.0 120.1 120.2 120.2 120.3 69.1 65.5 40.3	Uncontrolled Figure 17 (L's) 9.13 ent (WS-02 On Re ent (WS-02 On Re Controlled Runoff (L's) 6.50 5.75 5.17 5.17 5.17 4.70 4.32 4.00 3.50 3.51	Storage Required Storage Required Storage Volume (m ²) 5.8 5.9 7.85 8.08 8.08 8.20 8.22 8.22 8.05 7.79	Total Release Rate (L/S) 2.13 2.13 Controlled Release Rate Constant (L/S) 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26	1735.588 Uncontrolled Brandf (Ly) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	b = Total Rebase Rate (L/s) 128 128 128 128 128 128 128 128 128 128			
10 10 10 every storm Ever: 10 10 10 10 10 20 20 20 20 20 20 20 20 20 2	Intensity (new.h/s) 178.6 mmwater Managana mmwater Managana (mm.h/s) 178.6 km z 1735.688 / (0 1735.688 / 0 1735.688 / 0 1735.788 / 0 1735.7888 / 0 1735.788 / 0 1735.788 / 0 1735.788 / 0 1735.788 / 0 1	Uncontrolled Runoff (Lb) 8.18 at (WS-82 On Re Controlled Runoff (Lb) 6.50 6.50 6.50 6.57 6.57 6.57 6.57 6.57 6.57 6.57 6.57	Storage Required 5.00 8 Storage Required 9 Storage Volume (m) 5.5 6.31 6.36 7.85 6.30 8.00 7.85 8.00 7.75 7.72 7.76 7.26 7.26 6.32 6.32	Total Release Rate 103 211 21	1735.588 Uncertification Resolution Resoluti	b = Total Release Rate (15) 127 128 128 128 128 128 128 128 128			
10 14 development Stor Year Storn Evert: Time (min) 10 15 20 25 30 35 40 40 40 50 30 70 80 90 100 100 100 115 15 15 15 15 15 15 15 15 1	Intensity (ms.hr) 172.6 immadzer Managama km z 1735.588 / (f immadzer Managama intensity (ms.hr) 172.6 intensity (ms.hr) 172.6 (ms.hr) 172.6 (ms.hr) (ms.hr) 172.6 (ms.hr) (ms.hr) 172.6 (ms.hr)	Uncontrolled Runoff (Lb) 9.13 nt (WS-02 On Ro rd + 6.014) ^{4.83} Controlled Runoff (Lb) 11.17 8.34 2.50 5.75 5.17 4.70 4.32 4.32 4.30 3.50 1.2 2.57 2.37	Storage Required Storage Required Storage Volume (m ²) 5.0 5.0 Storage Volume (m ²) 5.0 5	Total Relices Rate (33) 0.13 0.13 0.13 0.13 0.13 0.1280 0.12800000000000000000000000000000000000	1735.688 Uscontrolled 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	b = Total Release Rate (Ls) 1 28 1 28 1 28 1 28 1 28 1 28 1 28 1 28	0.820		
10 12 development Bion 24 development Bion 10 10 10 10 10 10 10 10 10 10	Intensity Intensity 178.4 Intensity umwels* Manageme Las = 1735.688 / 0 Intensity Intensity Intensity	Lincentre official Participant (LS) 1 13 art (WS 62 On Re- rd + 6.014) ^{4,833} Controlled Randf (LS) 1 34 7 50 6 50 7 50 8 50 7 50 8 50 7 50 8 50 7 50 8	Constant (.4) 100 100 100 100 100 100 100 10	a Total Pateaus Atlas (1-9) a 11 a 12 a 12 a 12 a 12 a 12 a 12 a 12	1735.588 Uncertification Resolution Resoluti	b = Total Rabase Rate (La) 1.22 1.23 1.24 1.25 1	0.820 V-(P	C :	
10 - development Stor -	Intensity Intensity 178.4 Intensity memory 178.4 memory 178.5 intensity Intensity	Uncontrolled Renet (4:) 101 (4:)	Constant (.4) 1.00 1.0	1 Fold Palasase Rule 0.53 0.53 0.51 0.53 0.52 0.53 0.52 0.53 0.52 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.54 0.53 0.54 0.54 0.54 0.54 0.54 0.54	1725.688 Uncontrolled 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	b = Total Rabase Rate (La) 1.22 1.23 1.24 1.25 1	0.820 V-(P	C :	
10 12 development Bion 24 development Bion 10 10 10 10 10 10 10 10 10 10	International (month) (178.4) (178.4) (178.6)	Lacontrolled Penod (Ls) 9.13 eff (Ls) 9.15 eff (Ls) 9.15 eff (Ls) 10.15 eff (Ls) eff (Ls) 10.15	Constant (.s) 100	Controlled Relaxes field (1-3) (1	1725.688 Uncontrolled 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	b = Total Rabase Rate (La) 1.22 1.23 1.24 1.25 1	0.520	C :	
10 12 development Bion 24 development Bion 10 10 10 10 10 10 10 10 10 10	Intensity Intensity 128.4 128.4 immuter Manageme 14.2 immuter Manageme 44.2 immuter Manageme 14.2 immuter Manageme 44.2 immuter Manageme 14.2 immu	Uncontrolled Pennet (Ls) 9.13 mt (W5.92 On Re Td + 6.014) ^{5.85} Td + 6.014) ^{5.85} Td + 6.014) ^{5.85} Td + 6.014) ^{5.85} Controlled Runnet (Ls) 9.55	Constant (Ls) Constant (Ls) 10 Storage Neguler Storage Neguler Storage Neguler 10 10 10 10 10 10 10 10 10 10	Controller Relates Controller Relates Rel Controller Relates Rel 128 128 128 128 128 128 128 128 128 128 128 128 128 128 129	1725.588 Uncontrolled Numin (Lui) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	b = Total Release Ridt Us) 128 129 128 129	0.520	C :	
10 12 development Bion 24 development Bion 10 10 10 10 10 10 10 10 10 10	Intensity Intensity 128.4 128.4 immuter Manageme 14.2 immuter Manageme 44.2 immuter Manageme 14.2 immuter Manageme 44.2 immuter Manageme 14.2 immu	Uncontrolled Pennet (Ls) 9.13 mt (W5.92 On Re Td + 6.014) ^{5.85} Td + 6.014) ^{5.85} Td + 6.014) ^{5.85} Td + 6.014) ^{5.85} Controlled Runnet (Ls) 9.55	Constant (.s) 100	Controller Relates Controller Relates Rel Controller Relates Rel 128 128 128 128 128 128 128 128 128 128 128 128 128 128 129	1725.588 Uncontrolled Numin (Lui) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	b = Total Release Ridt Us) 128 129 128 129	0.520	C :	
10 - development Stor -	Intensity Intensity 128.4 128.4 immuter Manageme 14.2 immuter Manageme 44.2 immuter Manageme 14.2 immuter Manageme 44.2 immuter Manageme 14.2 immu	Uncontrolled Pennet (Ls) 9.13 mt (W5.92 On Re Td + 6.014) ^{5.85} Td + 6.014) ^{5.85} Td + 6.014) ^{5.85} Td + 6.014) ^{5.85} Controlled Runnet (Ls) 9.55	Constant (Ls) 10 Storage Neguler Storage Neguler Storage Neguler Storage Neguler 10 10 10 10 10 10 10 10 10 10	Controller Relates Controller Relates Rel Controller Relates Rel 128 128 128 128 128 128 128 128 128 128 128 128 128 128 129	1725.588 Uncontrolled Numin (Lui) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	b = Total Release Ridt Us) 128 129 128 129	0.520	C :	
10 12 development Bion 24 development Bion 10 10 10 10 10 10 10 10 10 10	Intensity (month) 178.4 manutor Monagene manutor Monagene 178.5 178.6 178.6 178.6 178.6 178.6 178.6 180.0 100.1 100.1 100.2	Uncontrolled Pennet (Ls) 9.13 mt (W5.92 On Re Td + 6.014) ^{5.85} Td + 6.014) ^{5.85} Td + 6.014) ^{5.85} Td + 6.014) ^{5.85} Controlled Runnet (Ls) 9.55	Constant (.s.) 1.00 1.	Controller Relates Controller Relates Rel Controller Relates Rel 128 128 128 128 128 128 128 128 128 128 128 128 128 128 129	1725.588 Uncontrolled Numin (Lui) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	b = Total Release Ridt Us) 128 129 128 129	0.520	C :	

Summary of release Rates and St	orage Volumes				
Catchment Area	Drainage Area (ha)	100-year Release Rate (L/s)	100-Year Required Storage (m3)	Total Available Storage (m3)	
WS-01	0.023	9.13	0	0	*Uncontrolled flow exceeding allowable release rate has been approved by City of Ottawa
WS-02 (Roof Controls)	0.023	1.26	8.26	9.00	
TOTAL	0.046	10.39	8.26	9.00	

	LRL File No. Project: Location: Date: Designed: Drawing Ref.:	200295 Apartment Building 161 Hinchey Ave July 6, 2021 Ann Salem C.601			Stormw	ater Managem esign Sheet	ent	
unoff Equation								
Q = 2.78	CIA (L/s)							
C = Runo	ff coefficient							
	all intensity (mm/hr)	= A / (Td + C) ^{ik}						
A = Area								
I _a = Time	of concentration (min)							
re-development Stormwater Man	agement							
l _s = 998.0	071 / (Td + 6.053) ^{0.816}		a =	998.071	b =	0.814	C =	6.053
_								
	0.50 max of 0.5 as pe 04.2 mm/hr	r City of Ottawa						
	10 min							
	1.046 ha							
Allowable Releas	e Ratez 6.63							
Allowable Heleas	e Kate: 6.63	Lis						
ost-development Stormwater Ma	nagement							
						∑R _{ma}	ΣRann	
	Total Site	e Area =	0.046	ha	5R=	0.76	0.95	
Controlled	WS-02 Total Cor	(Roof)	0.023	ha	Be	0.90	1.00	
	WS		0.023	ha	SR= Br	0.90	0.79	
Un-controlled	WS- Total Un-Cr	ontrolled =	0.023	ha	Re SR-	0.63	0.79	
			0.025	ne	>n=	0,65	9.72	

5 Ye	ar Storn Event: I, =	998.071 / (Td	+ 6.053) ^{8.816}			998.071	b = 0.814	C =	6.053	
	Time (min) 10	(mm/hr) 104.2	Uncontrolled Runoff (L/s) 4.26	Controlled Release Rate Constant (L/s) 0.00	Total Release Rate (L/s) 4.25]				

								6.053
			Storage Required		1			
Time (min)	Intensity (mm/br)	Controlled Bunoff (L/s)	Storage Volume (m ²)	Controlled Release Rate Constant (L/s)	Uncontrolled Bunoff (L/s)	Total Release Rate (L/s)		
10	104.2	5.87	2.76	1.26	0.00	1.26		
15	83.6	4.70	3.10	1.26	0.00	1.26		
20	70.3	3.95	3.23	1.26	0.00	1.26		
25	60.9	3.43	3.25	1.26	0.00	1.26		
30	53.9	3.04	3.20	1.26	0.00	1.26		
35	48.5	2.73	3.09	1.26	0.00	1.26		
40	44.2	2.49	2.95	1.26	0.00	1.26		
45	40.6	2.29	2.77	1.26	0.00	1.26		
50	37.7	2.12	2.58	1.26	0.00	1.26		
60	32.9	1.85	2.14	1.26	0.00	1.26		
70	29.4	1.65	1.65	1.26	0.00	1.26		
80	26.6	1.50	1.13	1.26	0.00	1.26		
90	24.3	1.37	0.58	1.26	0.00	1.26		
100	22.4	1.26	0.00	1.26	0.00	1.26		
110	20.8	1.17	0.00	1.26	0.00	1.26		
120	19.5	1.10	0.00	1.26	0.00	1.26		

of release Rates and Storage Volumes

Catchment Area	Drainage Area (ha)	5-year Release Rate (L/s)	5-Year Required Storage (m3)	Total Available Storage (m3)
WS-01	0.023	4.26	0	0
WS-02 (Roof Controls)	0.023	1.26	3.25	9.00
TOTAL	0.046	5.52	3.25	9.00

LRL Associates Ltd. Storm Design Sheet



LRL File No.200295Project:Apartment BuildingLocation:161 Hinchey AveDate:July 9, 2021Designed:Amr SalemDrawing Reference:C.401

	Storm Design Parameters	
Rational Method Q = 2.78CIA		Ottawa Macdonald-Cartier International Airport IDF curve
		equation (5 year event, intensity in mm/hr)
Q = Peak flow in litres per second (L/s)	Runoff Coefficient (C)	$I = 998.071 / (T_c + 6.053)^{0.814}$
A = Drainage area in hectares (ha)	Grass 0.20	Min. velocity = 0.80 m/s
C = Runoff coefficient	Gravel 0.80	Manning's "n" = 0.013
I = Rainfall intensity (mm/hr)	Asphalt / rooftop 0.90	

LOCATION			AREA (ha)		FLOW				STORM SEWER										
WATERSHED / STREET	From MH	To MH	C = 0.20	C = 0.70	C = 0.90	Indiv. 2.78AC	Accum. 2.78AC	Time of Conc. (min.)	Rainfall Intensity (mm/hr)	Peak Flow Q (L/s)	Controlled Flow Q (L/s)	Pipe Diameter (mm)	Туре	Slope (%)	Length (m)	Capacity Full (L/s)	Velocity Full (m/s)	Time of Flow (min.)	Ratio (Q/Q _{FULL})
WS-01 - Uncontrolled	CB	CBMH01	0.009	0.001	0.014	0.041	0.04	10.00	104.2	4.26	4.26	250	HDPE	0.50%	8.6	42.0	0.86	0.17	0.10
WS-02 - Roof Controls	CBMH01	CBMH02	0.000	0.000	0.023	0.056	0.10	10.17	103.3	10.04	1.26	250	PVC	1.00%	28.5	59.5	1.21	0.39	0.17
	CBMH02	EX. STM	0.00	0.00	0.00	0.000	0.10	10.56	101.3	9.85	5.52	250	PVC	1.00%	5.0	59.5	1.21	0.07	0.17



Adjustable Flow Control for Roof Drains

ADJUSTABLE ACCUTROL (for Large Sump Roof Drains only)

WATTS®

For more flexibility in controlling flow with heads deeper than 2", Watts Drainage offers the Adjustable Accutrol. The Adjustable Accutrol Weir is designed with a single parabolic opening that can be covered to restrict flow above 2" of head to less than 5 gpm per inch, up to 6" of head. To adjust the flow rate for depths over 2" of head, set the slot in the adjustable upper cone according to the flow rate required. Refer to Table 1 below. Note: Flow rates are directly proportional to the amount of weir opening that is exposed.

EXAMPLE:

For example, if the adjustable upper cone is set to cover 1/2 of the weir opening, flow rates above 2" of head will be restricted to 2-1/2 gpm per inch of head.

Therefore, at 3" of head, the flow rate through the Accutrol Weir that has 1/2 the slot exposed will be: [5 gpm(per inch of head) x 2 inches of head] + $2 \cdot 1/2$ gpm(for the third inch of head) = $12 \cdot 1/2$ gpm.

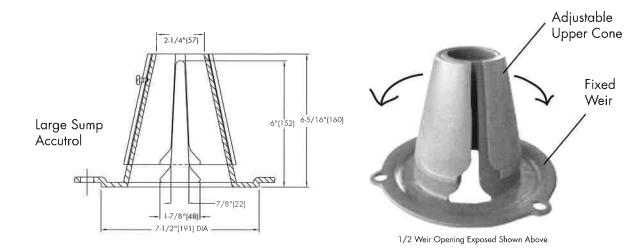


TABLE 1. Adjustable Accutrol Flow Rate Settings

3		Head of Water							
Weir Opening Exposed	1"	2"	3"	4"	5"	6"			
LAPOSed	Flow Rate (gallons per minute)								
Fully Exposed	5	10	15	20	25	30			
3/4	5	10	13.75	17.5	21.25	25			
1/2	5	10	12.5	15	17.5	20			
1/4	5	10	11.25	12.5	13.75	15			
Closed	5	10	10	10	10	10			
ob Name ob Location ngineer			Contractor						
WATTS Drainage reserves the right to modify or change product design or construction without prior notice and without incurring any obligation to make similar changes and modifications to products previously or subsequently sold. See your WATTS Drainage representative for any clarification. Dimensions are subject to manufacturing tolerances.						ing M			
pecification Drainage Pro	ducts C	ANADA: 5435 North Service R	oad, Burlington, ON, L7L 5H7 1	EL: 905-332-6718 TOLL-FR	EE: 1-888-208-8927 Website: w	ww.wattscanada.ca			

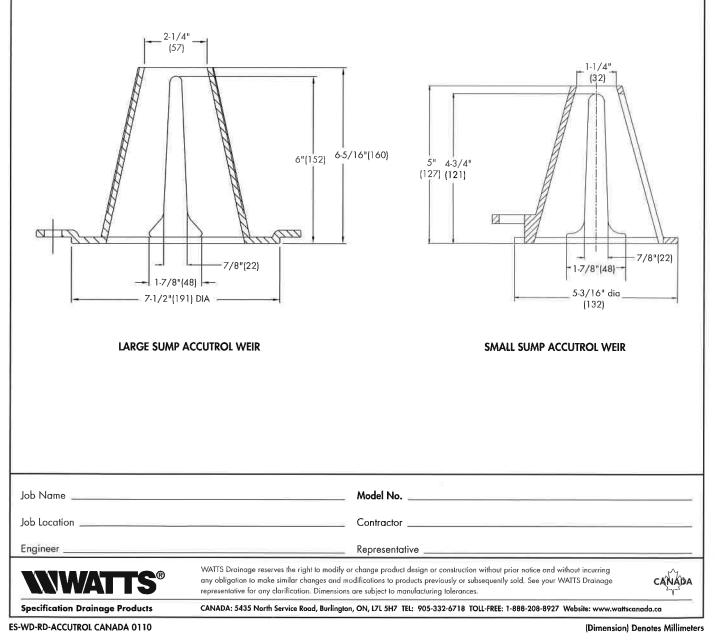
ES-WD-RD-ACCUTROLADJ CANADA 0110



ACCUTROL WEIR FLOW CONTROL

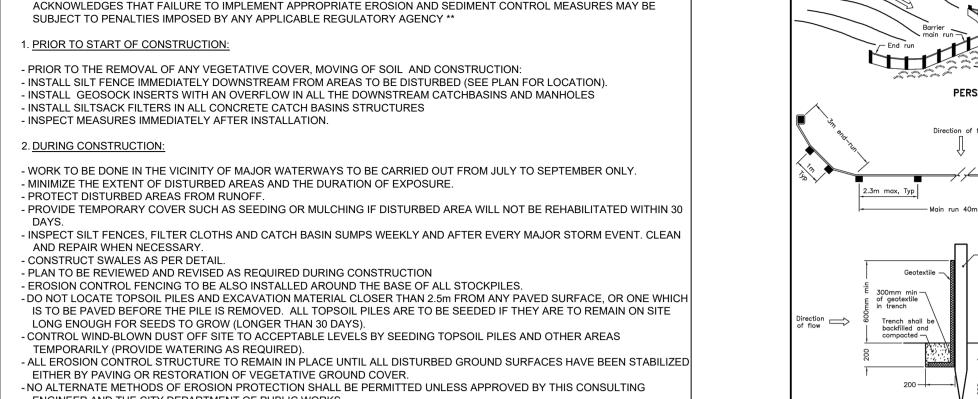
SPECIFICATION: Watts Drainage Products epoxy coated cast iron Accutrol Weir is designed with parabolic openings which limit the flow of rain water off a roof. Each weir slot controls flow to 5 gpm per inch of head to a maximum of 30 gpm at 6" head(for large sump), 25 gpm at 5" head(for small sump) . The Accutrol Weir is secured to the flashing clamp of the roof drain. The Accutrol Weir is available with 1 to 4 slots for the large sump drain and up to 3 slots for the small sump drain.

For Large Sump Roof Drains Specify the "-A" option and number of slots required. (ie. "RD-100-A2" for two slot weir) For Small Sump Roof Drains Specify the "-A" option and number of slots required. (ie. "RD-200-A1" for one slot weir)



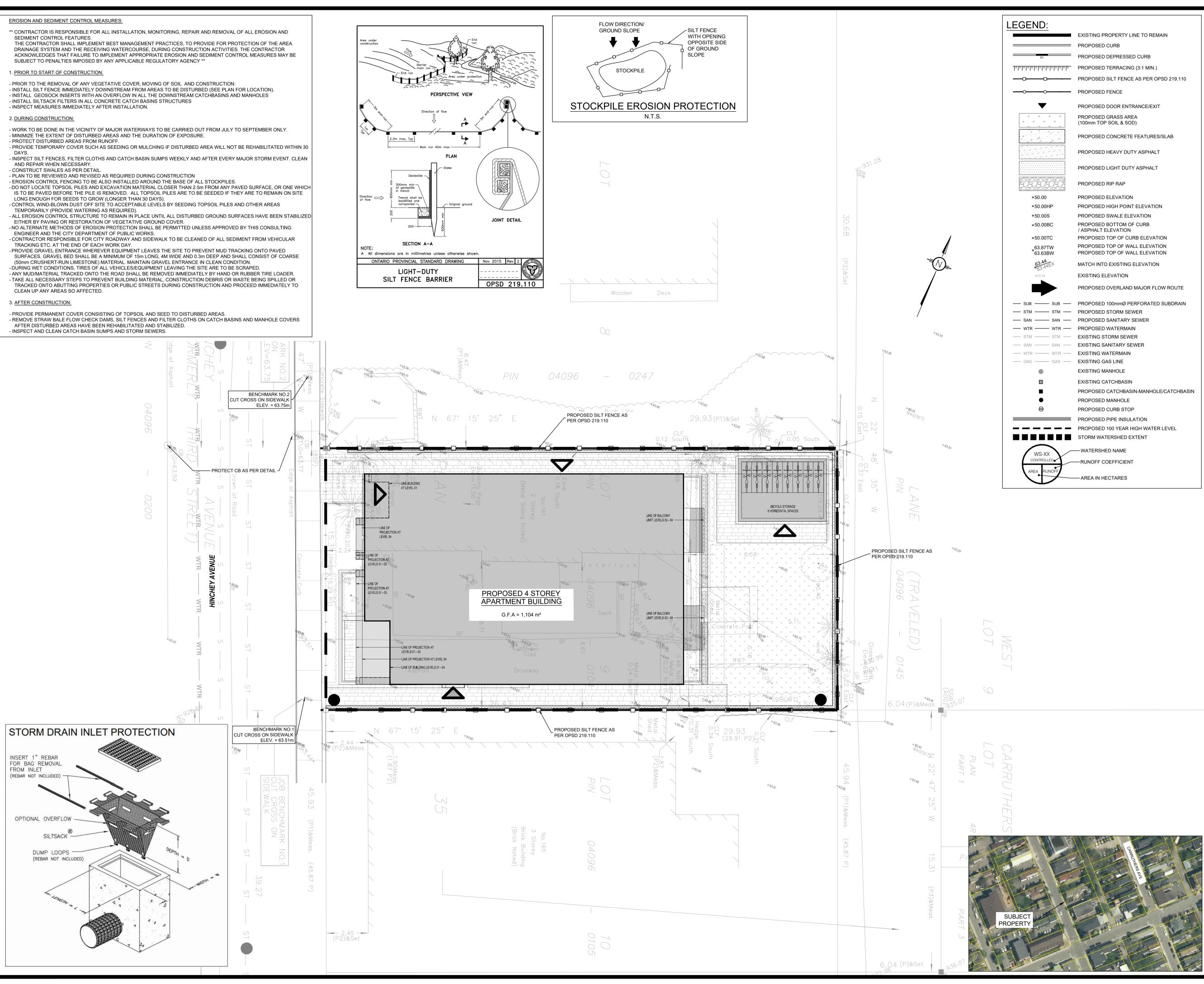
APPENDIX E

Civil Engineering Drawings



- TRACKING ETC. AT THE END OF EACH WORK DAY. PROVIDE GRAVEL ENTRANCE WHEREVER EQUIPMENT LEAVES THE SITE TO PREVENT MUD TRACKING ONTO PAVED
- (50mm CRUSHERT-RUN LIMESTONE) MATERIAL. MAINTAIN GRAVEL ENTRANCE IN CLEAN CONDITION. - DURING WET CONDITIONS. TIRES OF ALL VEHICLES/EQUIPMENT LEAVING THE SITE ARE TO BE SCRAPED.
- TAKE ALL NECESSARY STEPS TO PREVENT BUILDING MATERIAL, CONSTRUCTION DEBRIS OR WASTE BEING SPILLED OR TRACKED ONTO ABUTTING PROPERTIES OR PUBLIC STREETS DURING CONSTRUCTION AND PROCEED IMMEDIATELY TO CLEAN UP ANY AREAS SO AFFECTED.

- REMOVE STRAW BALE FLOW CHECK DAMS, SILT FENCES AND FILTER CLOTHS ON CATCH BASINS AND MANHOLE COVERS AFTER DISTURBED AREAS HAVE BEEN REHABILITATED AND STABILIZED.



USE AND INTERPRETATION OF DRAWINGS

GENERAL CONDITIONS OF THE CONTRACT FOR CONSTRUCTION ARE PART OF THE CONTRACT DOCUMENTS AND DESCRIBE USE AND INTENT OF THE DRAWING. T ONTRACT DOCUMENTS INCLUDE NOT ONLY THE DRAWINGS, BUT ALSO TH WNER-CONTRACTOR AGREEMENTS, CONDITIONS OF THE CONTRACT, T SPECIFICATIONS, ADDENDA, AND MODIFICATIONS ISSUED AFTER EXECUTION OF THE CONTRACT. THESE CONTRACT DOCUMENTS ARE COMPLEMENTARY, AND WHAT IS REQUIRED BY ANY ONE SHALL BE BINDING AS IF REQUIRED BY ALL. WORK NOT COMPLETELY DELINEATED HEREON SHALL BE CONSTRUCTED OF THE SAME MATERIALS AND DETAILED SIMILARLY AS WORK SHOWN MORE COMPLETELY ELSEWHERE IN THE CONTRACT DOCUMENTS.

BY USE OF THE DRAWINGS FOR CONSTRUCTION OF THE PROJECT, THE OWNER CONFIRMS THAT HE HAS REVIEWED AND APPROVED THE DRAWINGS. THI CONTRACTOR CONFIRMS THAT HE HAS VISITED THE SITE, FAMILIARIZED HIMSEL WITH THE LOCAL CONDITIONS. VERIFIED FIELD DIMENSIONS AND CORRELATED HIS BSERVATIONS WITH THE REQUIREMENTS OF THE CONTRACT DOCUMENTS.

AS INSTRUMENTS OF SERVICE, ALL DRAWINGS, SPECIFICATIONS, CADD FILES OR AS INSTRUMENTS OF SERVICE, ALL DRAWINGS, SPECIFICATIONS, CADD FILES ON OTHER ELECTRONIC MEDIA AND COPIED THERE OF FURNISHED BY THE ENGINEER ARE HIS PROPERTY. THEY ARE TO BE USED ONLY FOR THIS PROJECT AND ARE NOT TO BE USED ON ANY OTHER PROJECT, INCLUDING REPEATS OF THE PROJECT. HANGES TO THE DRAWINGS MAY ONLY BE MADE BY THE ENGINEER

UNLESS THE REVISION TITLE IS "ISSUED FOR CONSTRUCTION", THESE DRAWINGS SHALL BE CONSIDERED PRELIMINARY AND SHALL NOT BE USED AS A CONSTRUCTION DOCUMENT. THESE DRAWINGS ILLUSTRATES THE WORK TO BE DONE. THE ENGINEER IS NOT

RESPONSIBLE FOR THE MEANS, METHODS, TECHNIQUES, SEQUENCES, AND PROCEDURES USED TO DO THE WORK, OR THE SAFETY ASPECTS OF CONSTRUCTION, AND NOTHING ON THESE DRAWINGS EXPRESSED OR IMPLIED CHANGES THIS CONDITION. CONTRACTOR SHALL DETERMINE ALL CONDITIONS AT THE SITE AND SHALL BE RESPONSIBLE FOR KNOWING HOW THEY AFFECT THE WORK. SUBMITTAL OF A BID TO PERFORM THIS WORK IS ACKNOWLEDGEMENT OF THE RESPONSIBILITIES, AND THAT THEY HAVE BEEN FULLY CONSIDERED IN PLANNING OF THE WORK, AND THE BID PRICE. NO CLAIMS FOR EXTRA CHARGES DUE TO THESE CONDITIONS WILL BE FORTHCOMING. UNAUTHORIZED CHANGES:

IN THE EVENT THE CLIENT, THE CLIENT'S CONTRACTORS OR SUBCONTRACTORS, OR

ANYONE FOR WHOM THE CLIENT IS LEGALLY LIABLE MAKES OR PERMITS TO BE MADE ANY CHANGES TO ANY REPORTS, PLANS, SPECIFICATIONS OR OTHER CONSTRUCTION DOCUMENTS PREPARED BY LRL ASSOCIATES LTD. (LRL) WITHOUT OBTAINING LRL'S PRIOR WRITTEN CONSENT, THE CLIENT SHALL ASSUME FULL RESPONSIBILITY FOR THE RESULTS OF SUCH CHANGES. THEREFORE THE CLIENT AGREES TO WAIVE ANY CLAIM AGAINST LRI AND TO BELEASE LRI FROM ANY LIABILITY ARISING DIRECTLY OR INDIRECTLY FROM SUCH UNAUTHORIZED CHANGES.

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BEFORE START OF CONSTRUCTION. THE ENGINEER WAIVES ANY AND ALL RESPONSIBILITY AND LIABILITY FOR PROBLEMS WHICH ARISE FROM FAILURE TO FOLLOW THESE PLANS, SPECIFICATIONS AND THE DESIGN INTENT THEY CONVEY, OR FOR PROBLEMS WHICH ARISE FROM OTHERS' FAILURE TO OBTAIN AND/OR FOLLOW THE NGINEER'S GUIDANCE WITH RESPECT TO ANY ERRORS, OMISSIONS INCONSISTENCIES AMBIGUITIES OR CONFLICTS WHICH ARE ALLEGED.

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SCALE: 1:100



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> PRAVEEN MUPPALLA 450 Creekview Way Ottawa, ON, K1Y 1L5 TEL: 613-805-8278

ESIGNED B **APPROVED BY** A.S. A.S. M.B.

APARTMENT BUILDING **161 HINCHEY AVENUE**

200295

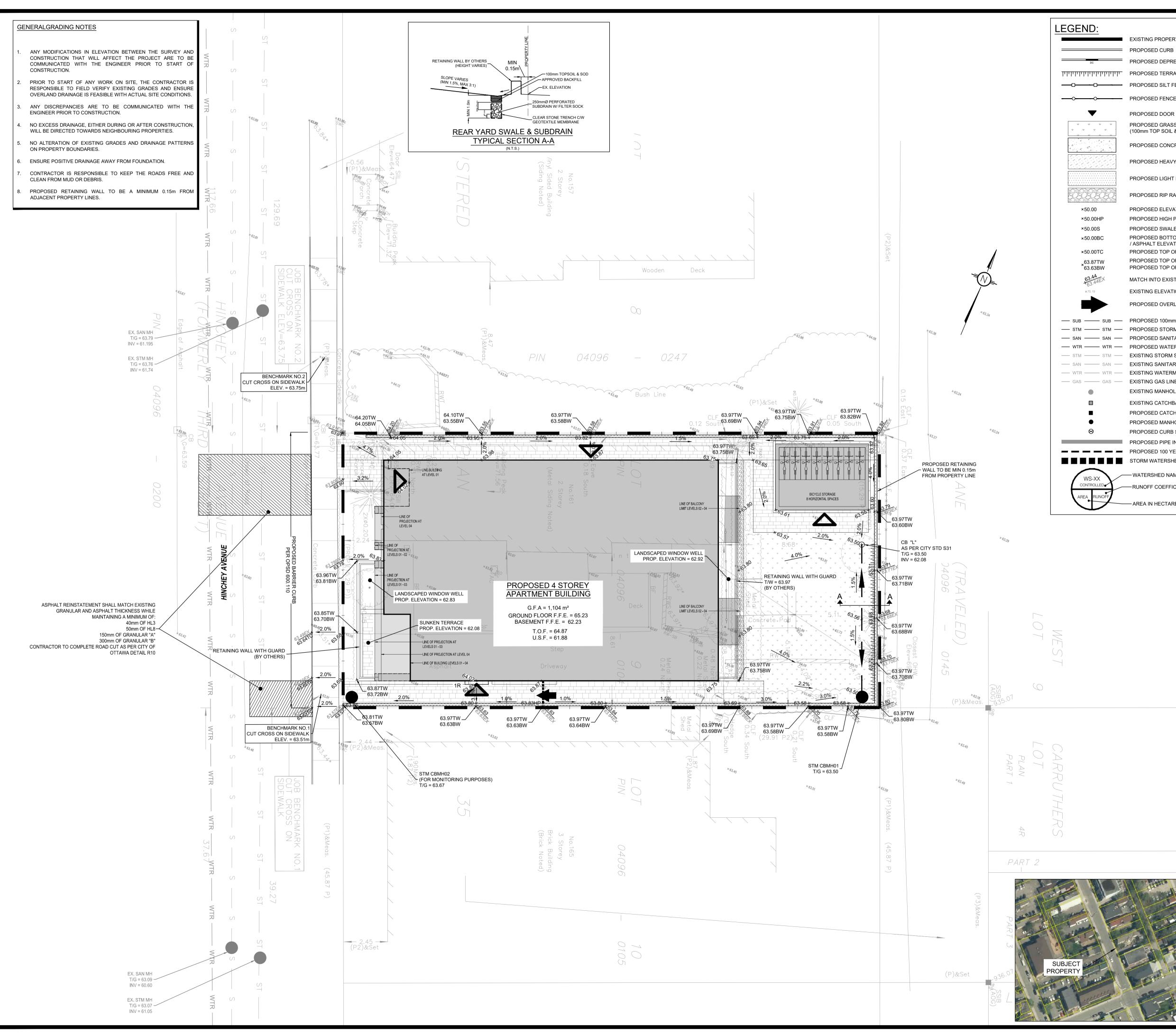
EROSION AND SEDIMENT CONTROL PLAN

[101

JULY 2020

#18320

42 0



PROPOSED DEPRESSED CURB

 $\psi = \psi$

×50.00 ×50.00HP ×50.00S

×50.00BC ×50.00TC ..63.87TW ^{*}63.63BW

63.44 (63.44E) ×70.19

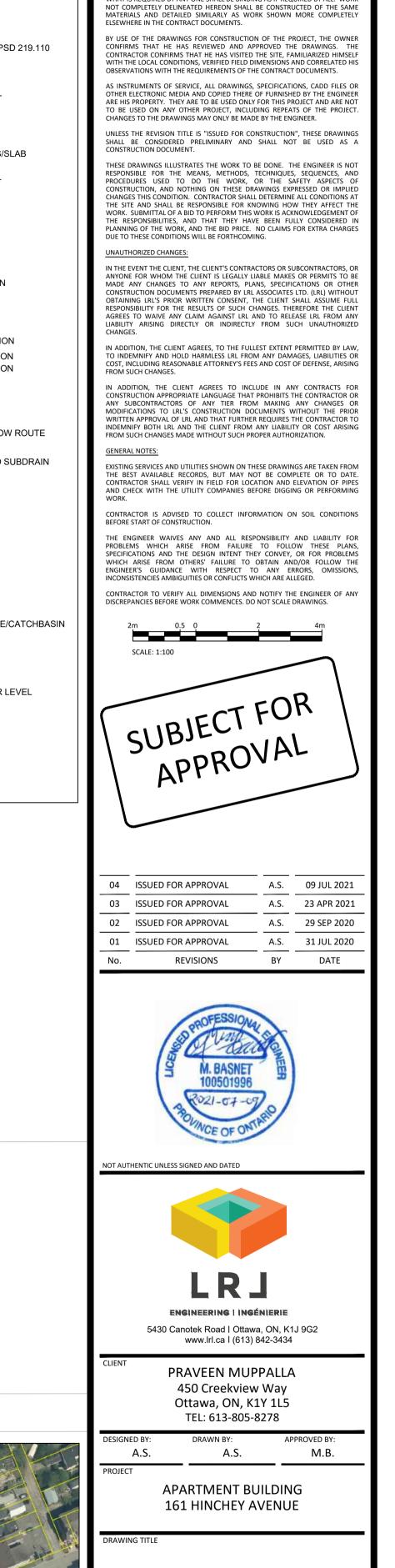
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WS-XX CONTROLLED

PROPOSED SILT FENCE AS PER OPSD 219.110 ----O------ PROPOSED FENCE PROPOSED DOOR ENTRANCE/EXIT PROPOSED GRASS AREA (100mm TOP SOIL & SOD) PROPOSED CONCRETE FEATURES/SLAB PROPOSED HEAVY DUTY ASPHALT PROPOSED LIGHT DUTY ASPHALT PROPOSED RIP RAP PROPOSED ELEVATION PROPOSED HIGH POINT ELEVATION PROPOSED SWALE ELEVATION PROPOSED BOTTOM OF CURB / ASPHALT ELEVATION PROPOSED TOP OF CURB ELEVATION PROPOSED TOP OF WALL ELEVATION PROPOSED TOP OF WALL ELEVATION MATCH INTO EXISTING ELEVATION EXISTING ELEVATION PROPOSED OVERLAND MAJOR FLOW ROUTE - SUB - SUB - PROPOSED 100mmØ PERFORATED SUBDRAIN - SAN - SAN PROPOSED SANITARY SEWER - WTR - WTR PROPOSED WATERMAIN ----- STM ----- EXISTING STORM SEWER ----- SAN ----- SAN ---- EXISTING SANITARY SEWER EXISTING GAS LINE EXISTING MANHOLE EXISTING CATCHBASIN PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN PROPOSED MANHOLE PROPOSED CURB STOP PROPOSED 100 YEAR HIGH WATER LEVEL

EXISTING PROPERTY LINE TO REMAIN

PROPOSED PIPE INSULATION STORM WATERSHED EXTENT - WATERSHED NAME -RUNOFF COEFFICIENT -AREA IN HECTARES



USE AND INTERPRETATION OF DRAWINGS

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GRADING AND DRAINAGE PLAN

ROJECT NO 200295

JULY 2020

C301

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#18320

NOTES: GENERAL

- JOB BENCH MARK CONFIRM WITH LRL PRIOR TO UTILIZATION
- DETENTION AREAS ARE PROVIDED
- ALL MATERIAL SUPPLIED AND PLACED FOR PARKING LOT AND ACCESS ROAD CONSTRUCTION SHALL BE TO OPSS STANDARDS AND SPECIFICATIONS UNLESS OTHERWISE NOTED.
- ABUTTING PROPERTY GRADE TO BE MATCHED.
- MINIMIZE DISTURBANCE TO EXISTING VEGETATION DURING THE EXECUTION OF ALL WORKS. CATCHBASINS, CATCHBASIN MANHOLES AND MANHOLES DURING THE CONSTRUCTION PERIOD
- THE ENGINEER. EXCAVATE AND REMOVE ALL ORGANIC MATERIAL AND DEBRIS, IF ANY, LOCATED WITHIN THE PROPOSED BUILDING, PARKING AND ROADWAY LOCATIONS.
- CONSTRUCTION PROJECT, SUCH AS BUT NOT LIMITED TO; ROAD CUT PERMITS, SEWER PERMITS, WATER PERMIT, ETC.
- ENGINEER BEFORE COMMENCING WORK

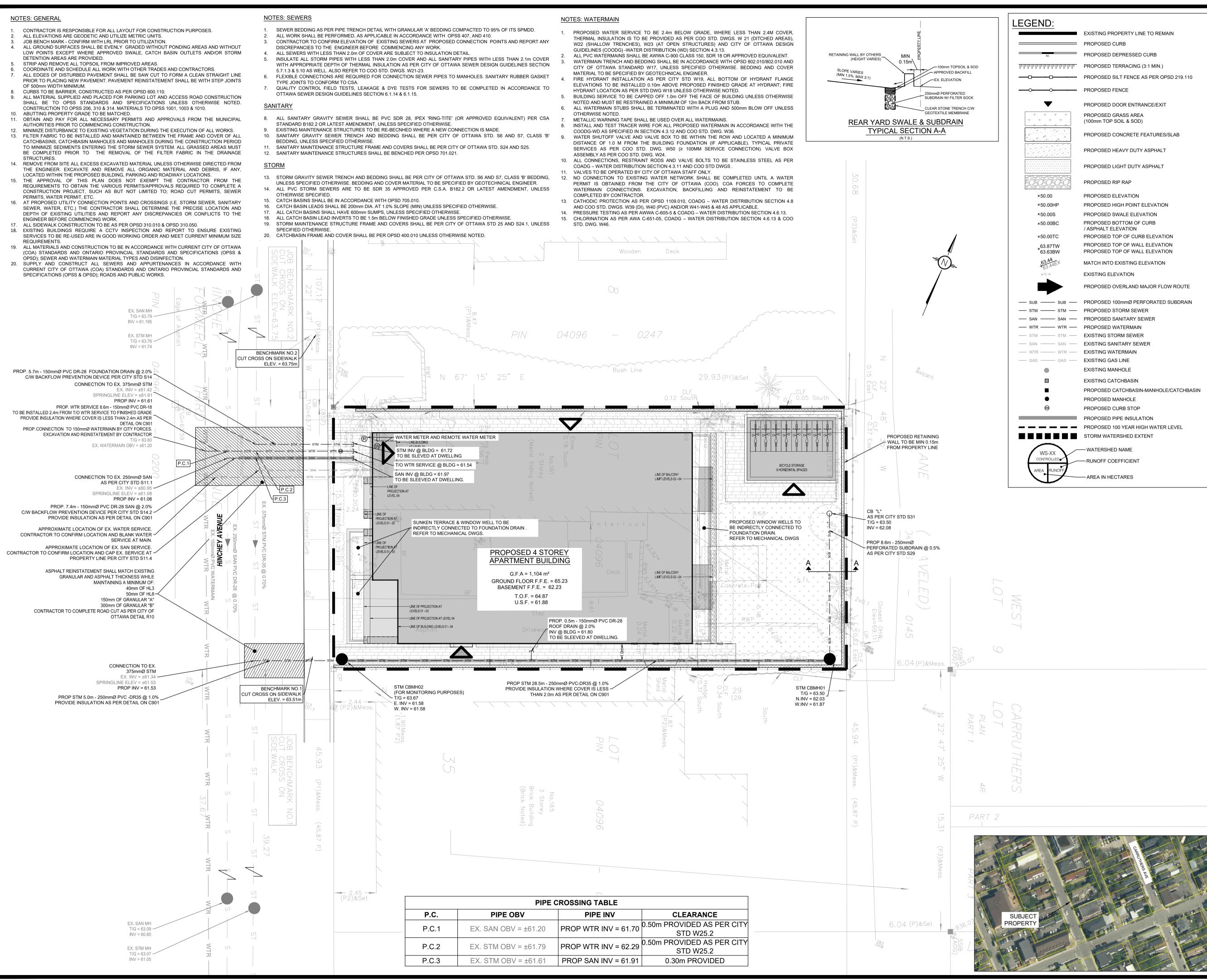


- ALL WORK SHALL BE PERFORMED, AS APPLICABLE IN ACCORDANCE WITH OPSS 407, AND 410.
- DISCREPANCIES TO THE ENGINEER BEFORE COMMENCING ANY WORK.

- OTTAWA SEWER DESIGN GUIDELINES SECTION 6.1.14 & 6.1.15.

- 10 BEDDING UNLESS SPECIFIED OTHERWISE

- CATCH BASINS SHALL BE IN ACCORDANCE WITH OPSD 705.010.
- ALL CATCH BASINS SHALL HAVE 600mm SUMPS. UNLESS SPECIFIED OTHERWISE.
- SPECIFIED OTHERWISE 20. CATCHBASIN FRAME AND COVER SHALL BE PER OPSD 400.010 UNLESS OTHERWISE NOTED.



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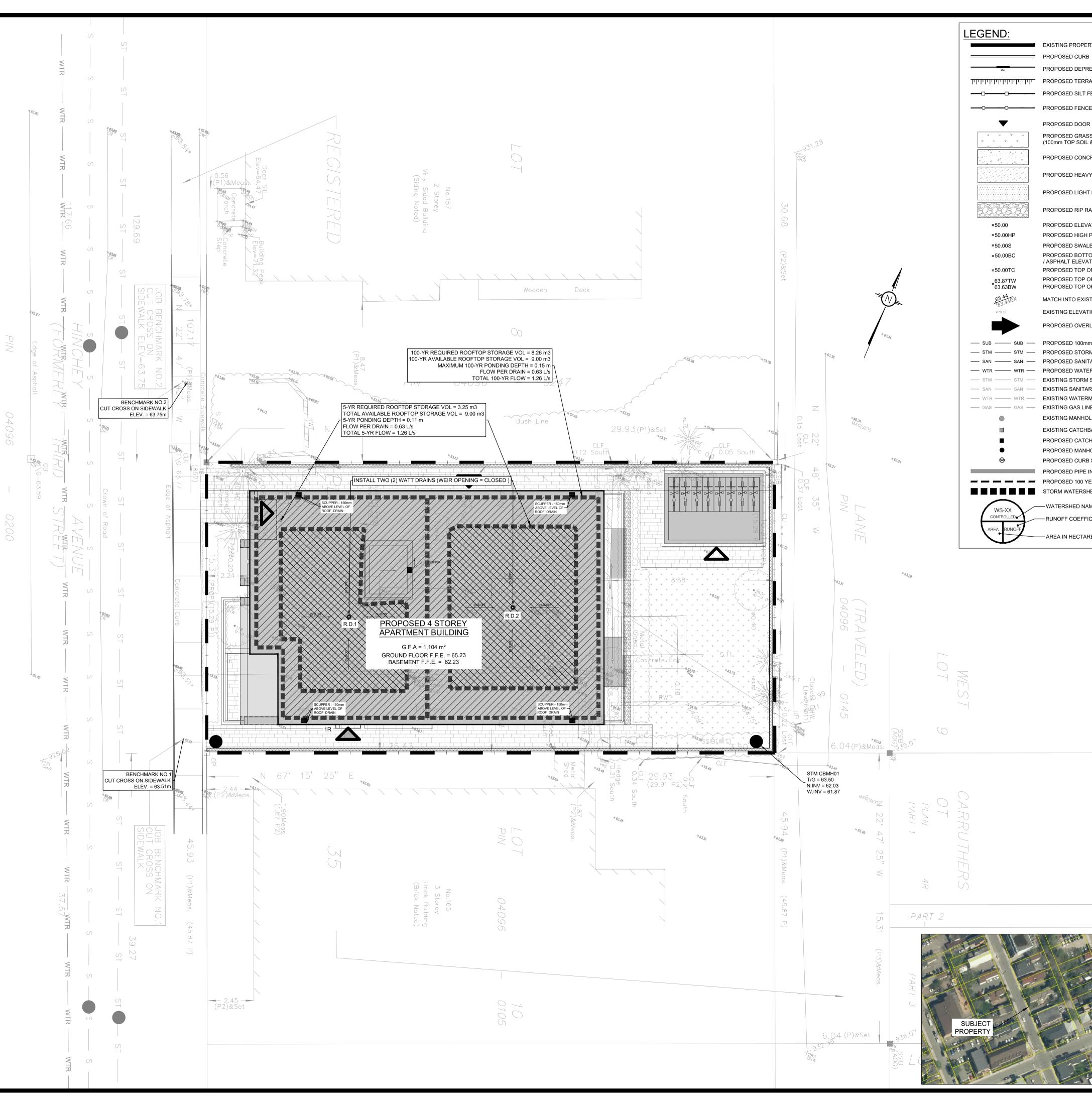
200295

JULY 2020

FSIGNED B

SERVICING PLAN





PROPOSED DEPRESSED CURB

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×50.00 ×50.00HP ×50.00S

×50.00TC ..63.87TW ^{*}63.63BW 63.44 63.44EX

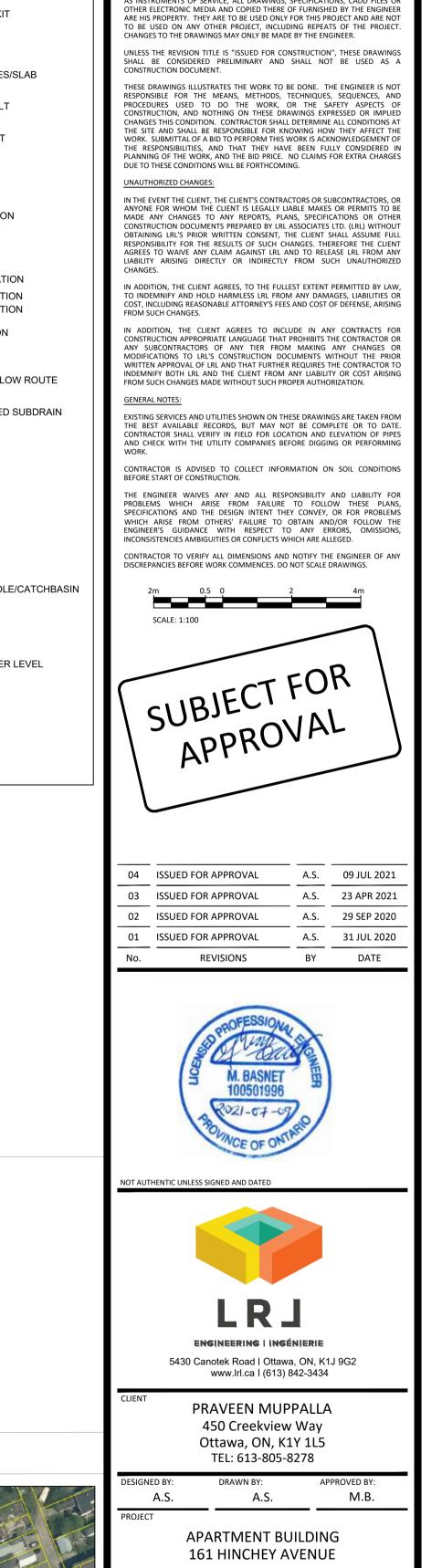
×70.19

WS-XX CONTROLLED

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EXISTING PROPERTY LINE TO REMAIN

-RUNOFF COEFFICIENT -AREA IN HECTARES



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DRAWING TITLE

PROJECT NO 200295

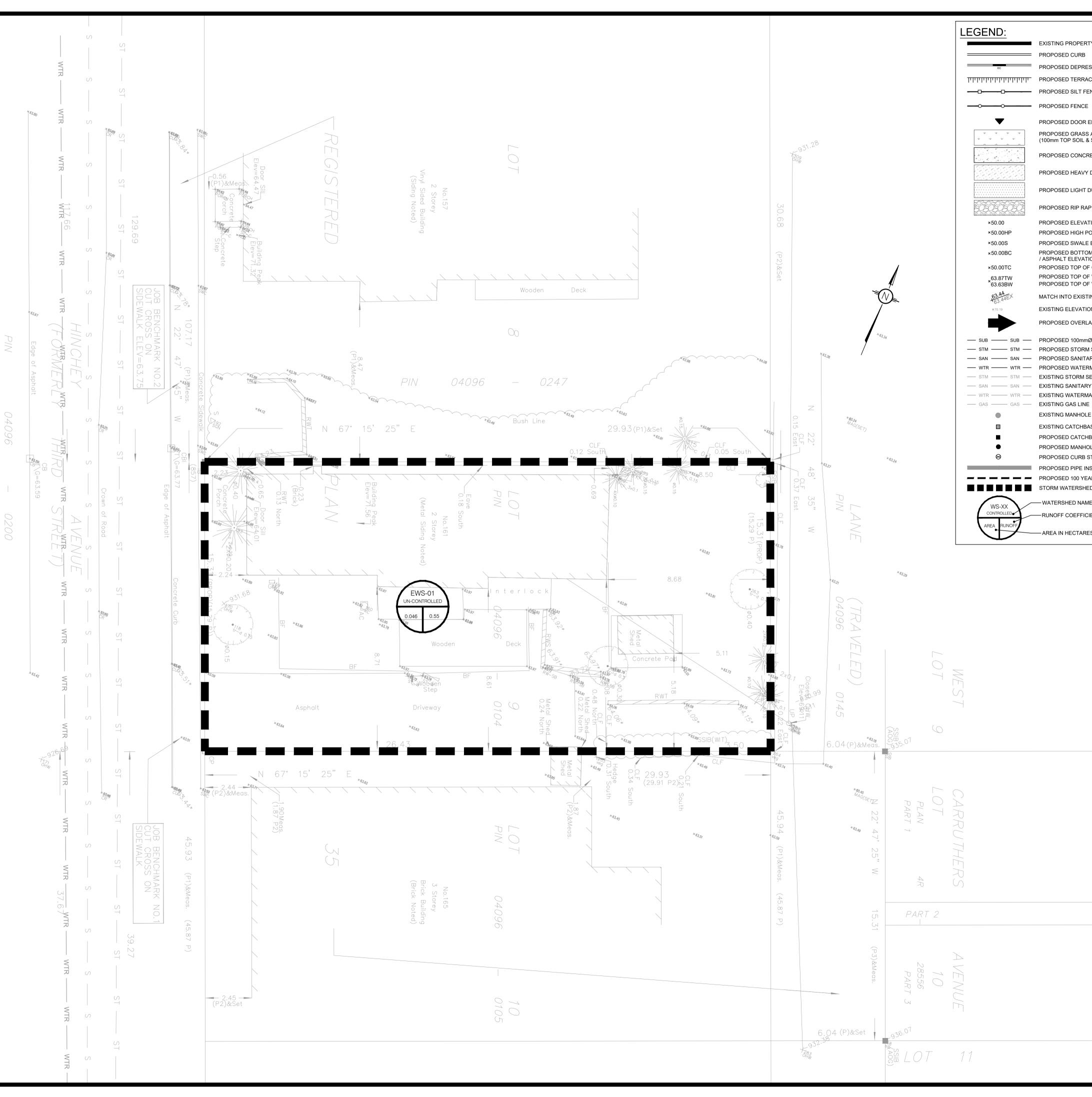
STORMWATER MANAGEMENT PLAN

C601

JULY 2020

#18320

42



DC	
pppp	

EXISTING PROPERTY LINE TO REMAIN

PROPOSED DEPRESSED CURB

PROPOSED TERRACING (3:1 MIN.)

PROPOSED DOOR ENTRANCE/EXIT

PROPOSED HEAVY DUTY ASPHALT

PROPOSED LIGHT DUTY ASPHALT

PROPOSED HIGH POINT ELEVATION

PROPOSED TOP OF CURB ELEVATION

PROPOSED TOP OF WALL ELEVATION

PROPOSED TOP OF WALL ELEVATION

MATCH INTO EXISTING ELEVATION

PROPOSED SWALE ELEVATION PROPOSED BOTTOM OF CURB

PROPOSED RIP RAP

PROPOSED ELEVATION

/ ASPHALT ELEVATION

PROPOSED CONCRETE FEATURES/SLAB

PROPOSED GRASS AREA

(100mm TOP SOIL & SOD)

PROPOSED CURB

PROPOSED SILT FENCE AS PER OPSD 219.110

 $\psi \quad \psi$

×50.00 ×50.00HP ×50.00S ×50.00BC

×50.00TC ..63.87TW ^{*}63.63BW 63.44 63.44EX

×70.19

WS-XX

EXISTING ELEVATION PROPOSED OVERLAND MAJOR FLOW ROUTE - STM - STM - PROPOSED STORM SEWER ----- STM ----- EXISTING STORM SEWER — SAN — SAN — EXISTING SANITARY SEWER — GAS — GAS — EXISTING GAS LINE EXISTING MANHOLE EXISTING CATCHBASIN PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN PROPOSED MANHOLE PROPOSED CURB STOP PROPOSED PIPE INSULATION PROPOSED 100 YEAR HIGH WATER LEVEL STORM WATERSHED EXTENT

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APPROVED BY DRAWN B A.S. M.B.

APARTMENT BUILDING **161 HINCHEY AVENUE**

DRAWING TITLE

DATE

DESIGNED BY

PROJECT

A.S.

PRE-DEVELOPMENT WATERSHED PLAN

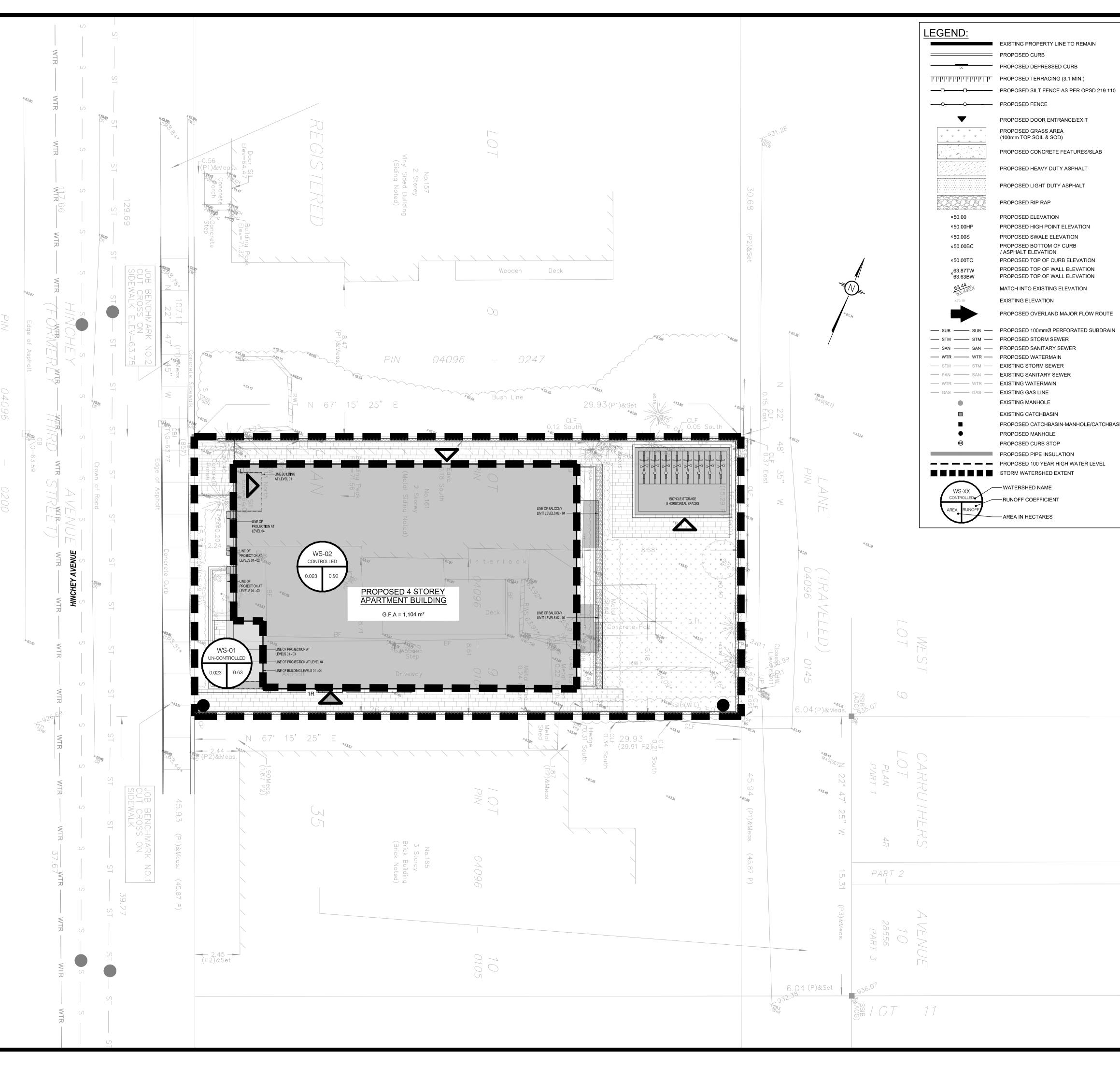
PROJECT NO. 200295

JULY 2020

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PROPOSED DEPRESSED CURB דיןידיןידיןידיןידיןידייידי PROPOSED TERRACING (3:1 MIN.)

EXISTING PROPERTY LINE TO REMAIN

PROPOSED DOOR ENTRANCE/EXIT

PROPOSED HEAVY DUTY ASPHALT

PROPOSED CONCRETE FEATURES/SLAB

PROPOSED GRASS AREA

(100mm TOP SOIL & SOD)

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×50.00HP ×50.00S ×50.00BC

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PROPOSED LIGHT DUTY ASPHALT PROPOSED RIP RAP PROPOSED ELEVATION PROPOSED HIGH POINT ELEVATION PROPOSED SWALE ELEVATION PROPOSED BOTTOM OF CURB / ASPHALT ELEVATION ×50.00TC PROPOSED TOP OF CURB ELEVATION PROPOSED TOP OF WALL ELEVATION PROPOSED TOP OF WALL ELEVATION MATCH INTO EXISTING ELEVATION EXISTING ELEVATION PROPOSED OVERLAND MAJOR FLOW ROUTE ----- STM ----- EXISTING STORM SEWER ----- SAN ----- EXISTING SANITARY SEWER EXISTING GAS LINE EXISTING MANHOLE EXISTING CATCHBASIN

PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN PROPOSED MANHOLE PROPOSED CURB STOP PROPOSED PIPE INSULATION PROPOSED 100 YEAR HIGH WATER LEVEL STORM WATERSHED EXTENT

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RESPONSIBLE FOR THE MEANS, METHODS, TECHNIQUES, SEQUENCES, AND PROCEDURES USED TO DO THE WORK, OR THE SAFETY ASPECTS OF CONSTRUCTION, AND NOTHING ON THESE DRAWINGS EXPRESSED OR IMPLIED CHANGES THIS CONDITION. CONTRACTOR SHALL DETERMINE ALL CONDITIONS AT THE SITE AND SHALL BE RESPONSIBLE FOR KNOWING HOW THEY AFFECT THE WORK. SUBMITTAL OF A BID TO PERFORM THIS WORK IS ACKNOWLEDGEMENT OF THE RESPONSIBILITIES, AND THAT THEY HAVE BEEN FULLY CONSIDERED IN PLANNING OF THE WORK, AND THE BID PRICE. NO CLAIMS FOR EXTRA CHARGES DUE TO THESE CONDITIONS WILL BE FORTHCOMING. UNAUTHORIZED CHANGES:

IN THE EVENT THE CLIENT, THE CLIENT'S CONTRACTORS OR SUBCONTRACTORS, OR

ANYONE FOR WHOM THE CLIENT IS LEGALLY LIABLE MAKES OR PERMITS TO BE MADE ANY CHANGES TO ANY REPORTS, PLANS, SPECIFICATIONS OR OTHER CONSTRUCTION DOCUMENTS PREPARED BY LRL ASSOCIATES LTD. (LRL) WITHOUT OBTAINING LRL'S PRIOR WRITTEN CONSENT, THE CLIENT SHALL ASSUME FULL RESPONSIBILITY FOR THE RESULTS OF SUCH CHANGES. THEREFORE THE CLIENT AGREES TO WAIVE ANY CLAIM AGAINST LIL AND TO RELEASE LRL FROM ANY LIABILITY ARISING DIRECTLY OR INDIRECTLY FROM SUCH UNAUTHORIZED CHANGES.

IN ADDITION, THE CLIENT AGREES, TO THE FULLEST EXTENT PERMITTED BY LAW, TO INDEMNIFY AND HOLD HARMLESS LRL FROM ANY DAMAGES, LIABILITIES OR COST, INCLUDING REASONABLE ATTORNEY'S FEES AND COST OF DEFENSE, ARISING FROM SUCH CHANGES.

IN ADDITION, THE CLIENT AGREES TO INCLUDE IN ANY CONTRACTS FOR CONSTRUCTION APPROPRIATE LANGUAGE THAT PROHIBITS THE CONTRACTOR OR ANY SUBCONTRACTORS OF ANY TIER FROM MAKING ANY CHANGES OR MODIFICATIONS TO LRL'S CONSTRUCTION DOCUMENTS WITHOUT THE PRIOR WRITTEN APPROVAL OF LRL AND THAT FURTHER REQUIRES THE CONTRACTOR TO INDEMNIFY BOTH LRL AND THAT FORMER REQUIRES THE CONTRACTOR TO FROM SUCH CHANGES MADE WITHOUT SUCH PROPER AUTHORIZATION. GENERAL NOTES:

EXISTING SERVICES AND UTILITIES SHOWN ON THESE DRAWINGS ARE TAKEN FROM THE BEST AVAILABLE RECORDS, BUT MAY NOT BE COMPLETE OR TO DATE. CONTRACTOR SHALL VERIFY IN FIELD FOR LOCATION AND ELEVATION OF PIPES AND CHECK WITH THE UTILITY COMPANIES BEFORE DIGGING OR PERFORMING WORK.

CONTRACTOR IS ADVISED TO COLLECT INFORMATION ON SOIL CONDITIONS BEFORE START OF CONSTRUCTION. THE ENGINEER WAIVES ANY AND ALL RESPONSIBILITY AND LIABILITY FOR

PROBLEMS WHICH ARISE FROM FAILURE TO FOLLOW THESE PLANS, SPECIFICATIONS AND THE DESIGN INTENT THEY CONVEY, OR FOR PROBLEMS WHICH ARISE FROM OTHERS' FAILURE TO OBTAIN AND/OR FOLLOW THE ENGINEER'S GUIDANCE WITH RESPECT TO ANY ERRORS, OMISSIONS, INCONSISTENCIES AMBIGUITIES OR CONFLICTS WHICH ARE ALLEGED. CONTRACTOR TO VERIFY ALL DIMENSIONS AND NOTIFY THE ENGINEER OF ANY DISCREPANCIES BEFORE WORK COMMENCES. DO NOT SCALE DRAWINGS.

SCALE: 1:100 SUBJECT FOR

04	ISSUED FOR APPROVAL	A.S.	09 JUL 2021
03	ISSUED FOR APPROVAL	A.S.	23 APR 2021
02	ISSUED FOR APPROVAL	A.S.	29 SEP 2020
01	ISSUED FOR APPROVAL	A.S.	31 JUL 2020
No.	REVISIONS	BY	DATE



NOT AUTHENTIC UNLESS SIGNED AND DATED



ENGINEERING | INGÉNIERIE 5430 Canotek Road | Ottawa, ON, K1J 9G2 www.lrl.ca | (613) 842-3434

> PRAVEEN MUPPALLA 450 Creekview Way Ottawa, ON, K1Y 1L5 TEL: 613-805-8278

APPROVED BY: DRAWN BY A.S. M.B.

APARTMENT BUILDING **161 HINCHEY AVENUE**

DRAWING TITLE

DESIGNED BY

PROJECT

A.S.

POST-DEVELOPMENT WATERSHED PLAN

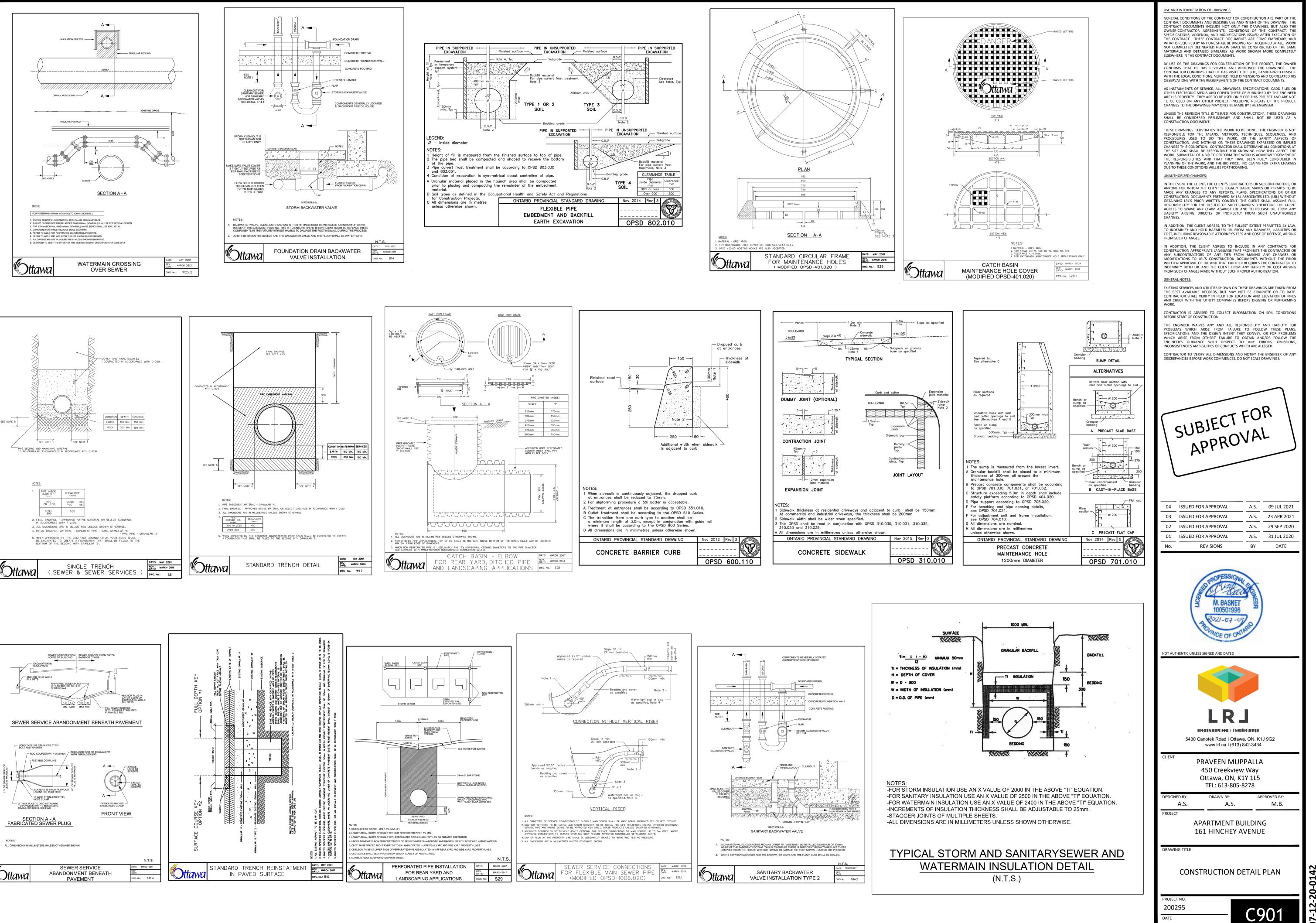
PROJECT NO. 200295

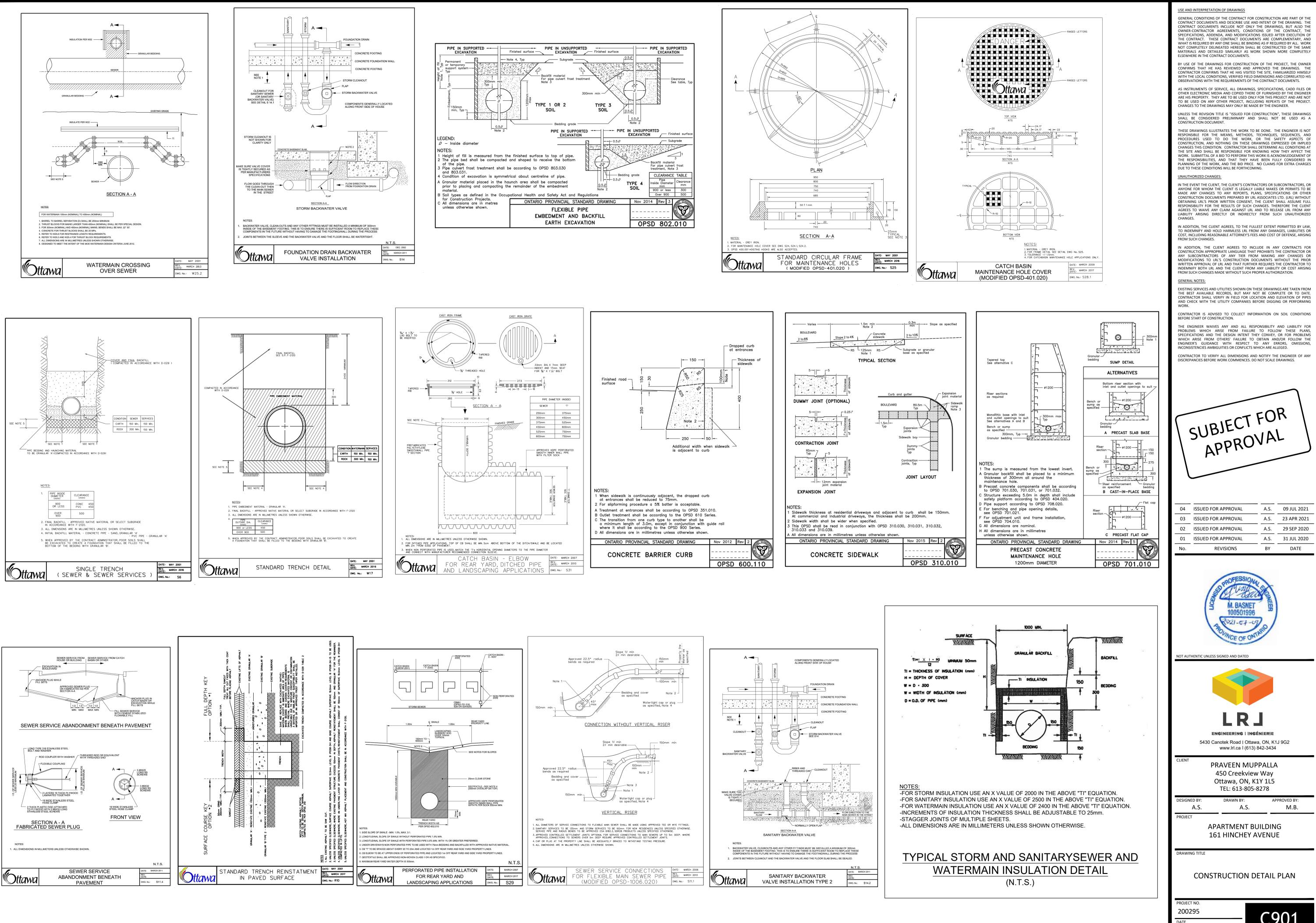
DATE JULY 2020

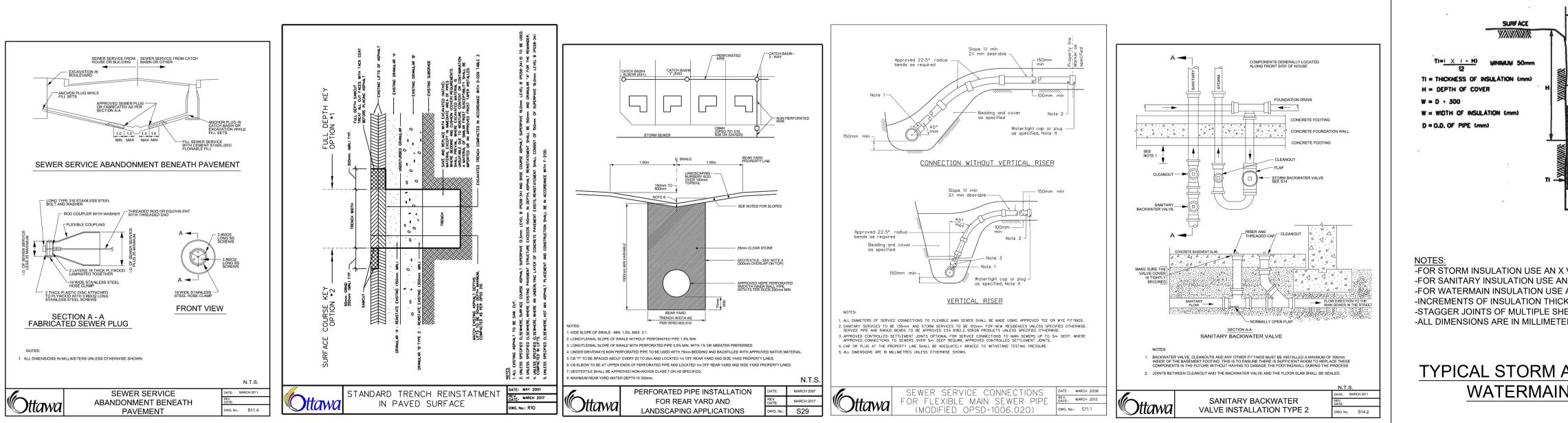


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JULY 2020

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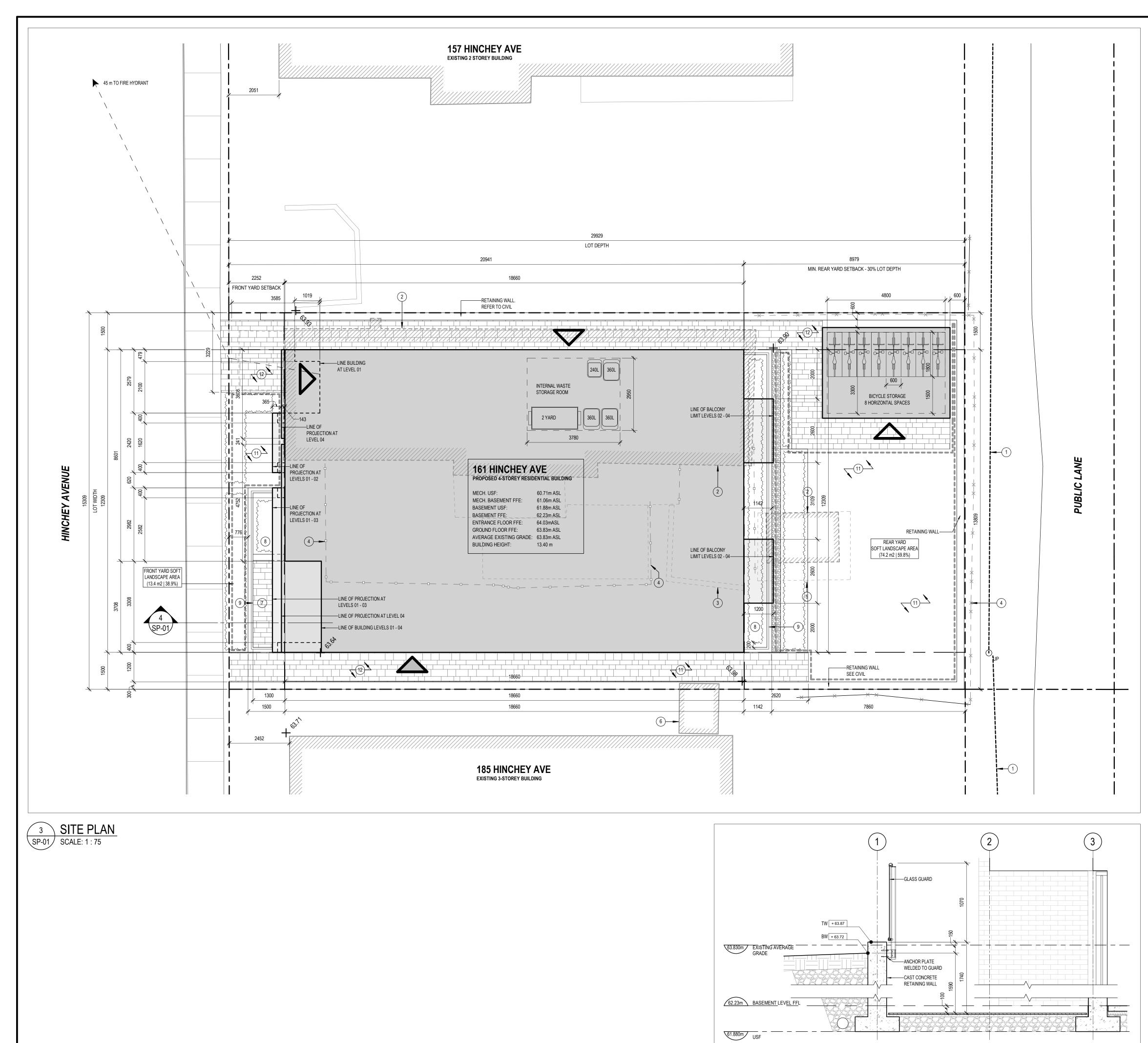
42

-01

20

DRAWINGS/FIGURES

Proposed Site Plan Legal Survey As-builts



4 SECTION AT TERRACE SP-01 SCALE: 1:25

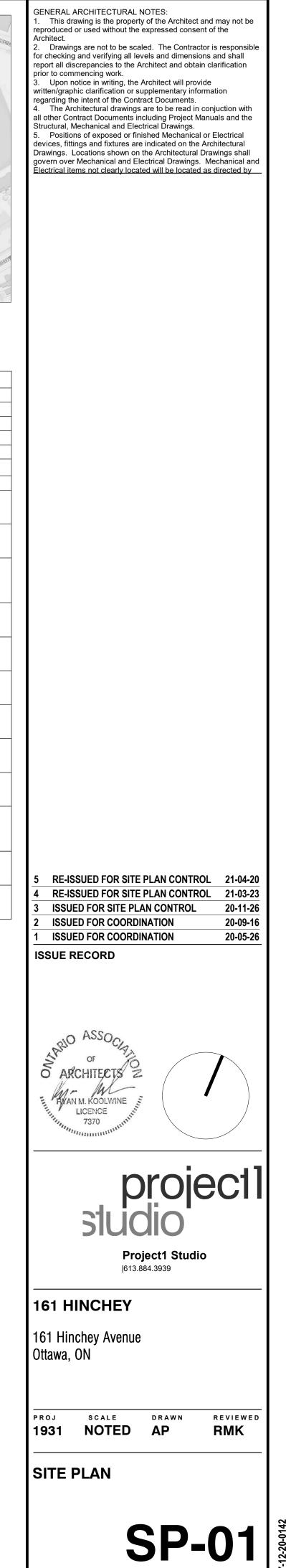


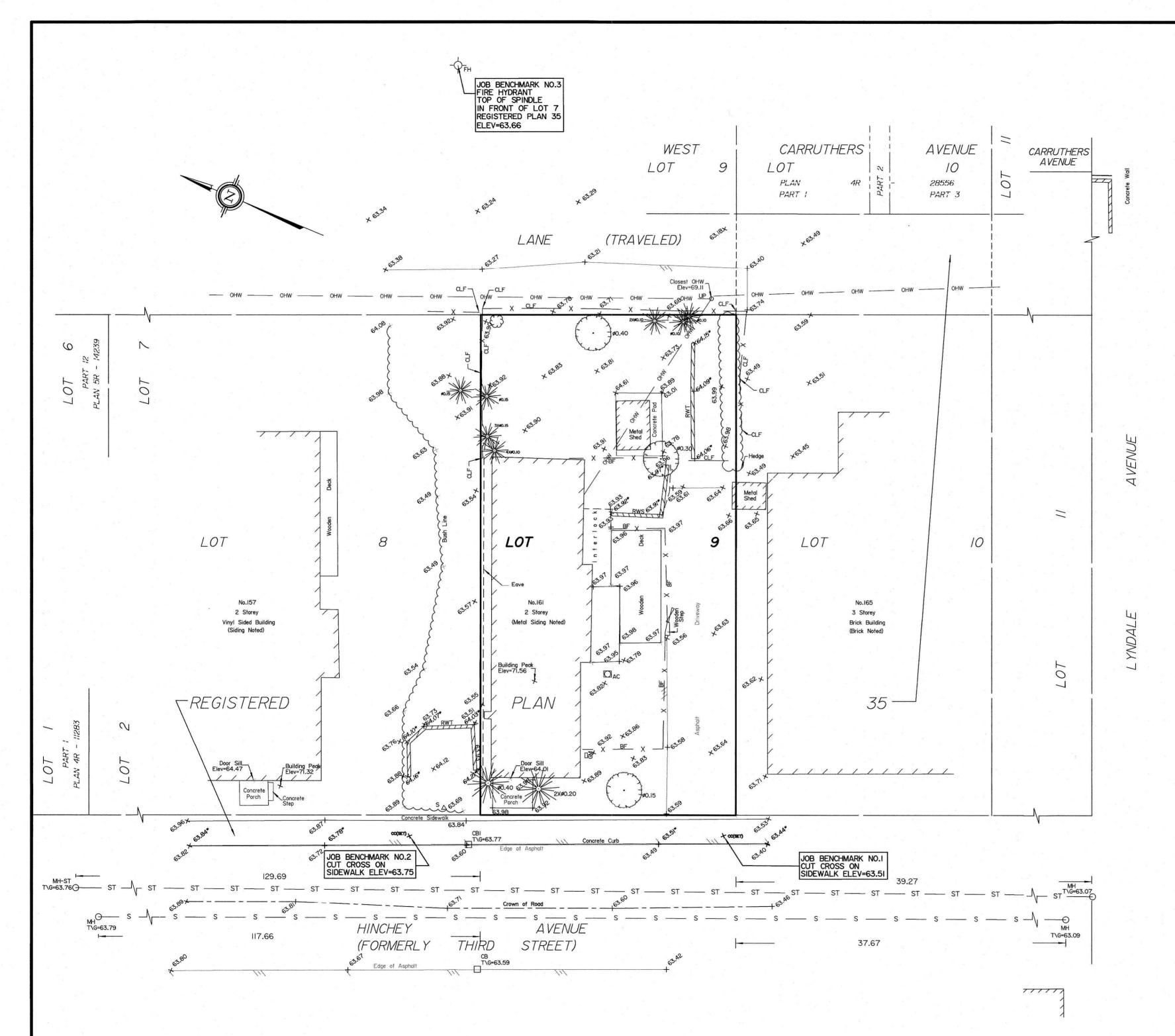
2 LOCATION PLAN SP-01 SCALE: NTS

Site Statistics						
Zoning Designation:	R4-UD					
Lot Width:	15.31m					
Lot Depth:	29.93m					
Total Lot Area:	458.2m2					
	· ·					
Proposed Development - 15 U	Init Low-Rise Apartment					
Zoning Mechanism	Required	Provided				
Minimum Lot Width 162(a)	15m	15.31m				
Minimum Lot Area 162(a)	450m2	458.2m2				
Min. Front Yard Setback 139(3)(b)	2.25m (Average of the setbacks of the existing buildings on the abutting lots)	2.25m				
Min. Interior Side Yard Setback 162(a)	1.5m	1.5m				
Min Rear Yard Setback 161(a)(iii)	8.979m (30% of Lot Depth)	8.979m				
Maximum Building height 162(a)	14.5m	13.4m				
Parking Space Rates 101(2)	0 Spaces (Area Z)	0 Spaces				
Minimum Visitor Parking Rates 102(2)(i)	0 Spaces (0.1 spaces/unit beyond 12 units)	0 Spaces				
Bicycle Parking Rates Table 111A(b)(i)	8 Spaces (12 units x 0.5)	8 Spaces				
Soft Landscaping <i>161 (13)(b)(iii)</i>	68.7m2 (Lots 450m2 or greater, at least 50% of the rear yard)	74.2 m2 (59.8%)				
Front Yard Soft Landscaping Table 161	6.9m2 (20% of Front Yard)	13.4 m2 (38.9%)				
Minimum 2-Bedroom Unit Rates 161(14)(ii)	4 Units (At least 25% of units)	6 Units (50% of Units)				

1 ZONING INFORMATION

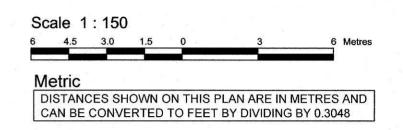
SP-01 SCALE: N.T.S. (1) OVERHEAD WIRE TOPOGRAPHIC PLAN OF SURVEY OF LOT 9 **REGISTERED PLAN 35** (2) EXISTING BUILDING TO BE DEMOLISHED (EAST HINCHEY AVENUE LOTS) CITY OF OTTAWA (3) EXISTING RETAINING WALL TO BE REMOVED ANNIS, O'SULLIVAN, VOLLEBEKK LTD. 2020 (4) EXISTING FENCE TO BE REMOVED (5) EXISTING CONCRETE PAD TO BE REMOVED SURVEY INFO (6) EXISTING SHED SCALE: NTS (7) SUNKEN TERRACE (8) LANDSCPAED WINDOW WELL SITE PLAN SYMBOLS LEGEND (9) CLEAR GLASS GUARD BUILDING ENTRANCE (11) SOFT LANDSCAPING (12) INTERLOCKING CONCRETE PAVERS BUILDING EXIT $\left|\right\rangle$ 0,00 - EXISTING ELEVATION ----- BOARD FENCE KEYNOTE LEGEND SYMBOLS LEGEND SCALE: NTS SCALE: N.T.S.





SKETCH OF BENCHMARK LOCATIONS 161 HINCHEY AVENUE OTTAWA

Surveyed by Annis, O'Sullivan, Vollebekk Ltd.



Notes & Legend

	Denotes	
-0		Survey Monument Planted
		Survey Monument Found
SSIB	10	Short Standard Iron Bar
IB	ч	Iron Bar
CP		Concrete Pin
Meas.		Measured
(AOG)		Annis, O'Sullivan, Vollebekk Ltd.
(P)	.	Registered Plan 35
(PI)		(857) Plan August 9, 2010
(P2)		(687) Plan November 25,1985
(P3)		Plan 4R-28556
RWT		Retaining Wall Timber
RWS		Retaining Wall Stone
—— они –		Overhead Wires
O UP		Utility Pole
СВ	3 0 5	Catch Basin
СВ-1	а ,	Catch Basin Inlet
OFH		Fire Hydrant
GM		Gas Meter
ΔS		Sign
CLF		Chain Link Fence
BF		Board Fence
X		Gate
O AC	્ય	Air Conditioner
0		Shrub
$\left\{\cdot\right\}$		Deciduous Tree
Xur		
X		Coniferous Tree
M		Connerous Tree
O MH-ST	an an	Maintenance Hole (Storm Sewer)
O MH-S		Maintenance Hole (Sanitary)
ST	11	Underground Storm Sewer
— s —	u	Underground Sanitary Sewer
Ø		Diameter
+ 65.00		Location of Elevation
+ 65.00*		Top of Concrete Curb Elevation
+ 6 ^{5.00*}	"	Top of Retaining Wall Elevation
C/L		Centreline
-		Property Line

UTILITY NOTES

1. This drawing cannot be accepted as acknowledging all of the utilities and it will be the responsibility of the user to contact the respective utility authorities for confirmation.

- 2. Only visible surface utilities were located.
- 3. Underground utility data derived from City of Ottawa utility sheet reference

 A field location of underground plant by the pertinent utility authority is mandatory before any work involving breaking ground, probing, excavating etc.

ELEVATION NOTES

 Elevations shown are geodetic and are referred to the CGVD28 geodetic datum.
 It is the responsibility of the user of this information to verify that the job benchmark has not been altered or disturbed and that it's relative elevation and description agrees with the information shown on this drawing.





