Servicing and Stormwater Management Report – 176 Nepean Street and 293-307 Lisgar Street

Project 160401348

May 10, 2021

Prepared for:

Richcraft Homes Ltd.

Prepared by:

Stantec Consulting Ltd.

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LICENSED PROFESSIONAL ENGINEER
T.K. RATHNASOORIYA
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2021-05-10
PROVINCE OF ONTARIO

Prepared by ____
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Reviewed by ____
(signature)

Sheridan Gillis

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1.0 INTRODUCTION

Stantec Consulting Ltd. has been retained by Richcraft Homes Ltd. to prepare the following site servicing and stormwater management (SWM) report to satisfy the City of Ottawa Zoning and Site Plan Control Application process. The 0.27ha site proposed for re-development is located at the municipal addresses of 176 Nepean Street and 293-307 Lisgar Street in the City of Ottawa in-between Bank Street and O'Connor Street.

The proposed residential development consists of two 25 and 27 storey apartment buildings above a common ground floor. Six levels of underground parking are to be provided. A total of 475 condominium apartments are proposed with a total of 242 parking spaces. The site will be accessed from both Nepean Street and Lisgar Street.

The intent of this report is to provide a servicing scenario for the site that is free of conflicts, provides on-site servicing in accordance with City of Ottawa design guidelines, and utilizes the existing local infrastructure in accordance with the guidelines outlined per consultation with City of Ottawa staff.

The location of the site is provided in **Figure 1** below.

Figure 1: Site Location

1.1 OBJECTIVE

This Site Servicing and Stormwater Management Brief has been prepared to present a servicing scheme that is free of conflicts and which uses the existing infrastructure as obtained from available as-built drawings and in consultation with City of Ottawa staff. Infrastructure requirements for water supply, sanitary, and storm sewer services are presented in this report.

Criteria and constraints provided by the City of Ottawa have been used as a basis for the servicing design of the proposed development. Specific elements and potential development constraints to be addressed are as follows:

- Potable Water Servicing
    - Estimate water demands to characterize the proposed feed for the development which will be serviced from the existing 300 mm diameter watermains on Nepean Street and Lisgar Street.
    - Watermain servicing for the development is to be able to provide average day and maximum day (including peak hour) demands (i.e. non-emergency conditions) at pressures within the acceptable range of 50 to 80 psi (345 to 552 kPa).
    - Under fire flow (emergency) conditions with maximum day demands, the water distribution system is to maintain a minimum pressure greater than 20 psi (140 kPa).
- Prepare a grading plan in accordance with the proposed site plan and existing grades.
- Stormwater Management and Servicing
    - Define major and minor conveyance systems in conjunction with the proposed grading plan
    - Determine the stormwater management storage requirements to meet the allowable release rate for the site
    - Coordinate with the Mechanical Engineer to convey drainage from roof tops and amenity areas to the internal cistern and discharge to the proposed storm service lateral at the allowable release rate.
- Wastewater Servicing
    - Define and size the sanitary service lateral which will be connected to the existing 375 mm diameter sanitary sewer on Lisgar Street.

The accompanying drawings included in **Appendix E** illustrate the proposed internal servicing scheme for the site.

2.0 REFERENCES

The following background studies have been referenced during the preliminary servicing design for the proposed site:

- *Geotechnical Investigation Proposed Multi-Storey Buildings, 176 Nepean Street and 293-307 Lisgar , Ottawa, ON,* Paterson Group Inc., September 22, 2020
- *City of Ottawa Design Guidelines – Water Distribution*, City of Ottawa, July 2010
- *City of Ottawa Sewer Design Guidelines*, City of Ottawa, October 2012
- *Technical Bulletin ISDTB-2014-01*, City of Ottawa, February 2014
- *Technical Bulletin ISTB-2018-01*, City of Ottawa, March 21, 2018
- *Technical Bulletin ISTB-2018-02*, City of Ottawa, March 21, 2018
- *Technical Bulletin ISTB-2018-03*, City of Ottawa, March 21, 2018
- *Technical Bulletin PIEDTB -2016-01*, City of Ottawa, September 6, 2016

3.0 POTABLE WATER SERVICING

The proposed building is located in Pressure Zone 1W of the City of Ottawa's water distribution system. The proposed development will be serviced by the existing 300 mm diameter watermains on Nepean Street and Lisgar Street as shown on **Drawing SSGP-1** in **Appendix E**. Average ground elevations of the site are approximately 72.0m. Under normal operating conditions, hydraulic gradelines vary from approximately 107.0m to 116.1m as confirmed through boundary conditions as provided by the City of Ottawa at both connection locations on Nepean Street and Lisgar Street. Updated boundary conditions have been requested and will be included as part of the next submission to ensure present conditions are being represented.

3.1 WATER DEMANDS

Water demands were calculated using the City of Ottawa Water Distribution Guidelines (City of Ottawa, 2010) to determine the typical operating pressures to be expected at the building (see detailed calculations in **Appendix C.1**). A demand rate of 350 L/cap/day was applied for the population of the proposed site. Population densities have been assumed as 3.1 pers./three bedroom apartment unit, 2.1 pers./two bedroom apartment unit, and 1.4pers./one bedroom and studio apartment unit. See **Appendix C.1** for detailed domestic water demand estimates.

Maximum day (MXDY) demands were determined by multiplying the AVDY demands by a factor of 2.5 for residential areas. Peak hourly (PKHR) demands were determined by multiplying the MXDY demands by a factor of 2.2 for residential areas. The estimated demands are summarized in **Table 3-1** below.

Table 3-1: Estimated Water Demands

	Population/Area	AVDY (L/s)	MXDY (L/s)	PKHR (L/s)
Residential	783 persons	3.42	8.54	18.79
Total Site:		**3.17**	**7.93**	**17.45**

Non-combustible combustible construction was considered in the assessment for fire flow requirements according to the FUS Guidelines, with two hour fire separations separating each floor based on requirements for buildings over six storeys in the Ontario Building Code. As a result, the worst case scenario was estimated as the podium area connecting to two towers. The FUS Guidelines indicate that low hazard occupancies include apartments, dwellings, dormitories, hotels, and schools, and as such, a low hazard occupancy / limited combustible building contents credit was applied. A sprinkler system conforming to NFPA 13 was considered, and a credit applied per FUS Guidelines. Based on calculations per the FUS Guidelines (**Appendix C.2)**, the minimum required fire flows for this development are 167 L/s (10,000L/min).

Table 3-2 shows the hydraulic boundary conditions provided by the City of Ottawa on January 15, 2020 based on the estimated domestic and fire flow demands described above. The boundary conditions are also included in **Appendix C.3**.

Table 3-2: Boundary Conditions

	Connection 1 & 2 (Nepean Street and Lisgar Street)
Min. HGL (m)	107.0
Max. HGL (m)	116.1
Max. Day + Fire Flow (167 L/s) (m)	107.5

3.2 PROPOSED SERVICING

Per the boundary conditions provided by the City of Ottawa for both connections on Nepean and Lisgar Street and based on an approximate elevation on-site of 72.0m, adequate flows are available for the subject site with pressures ranging from 35.0m (49.8psi) to 44.1m (62.7psi). Domestic flows are available to service the proposed site through both proposed 150mm diameter watermain services laterals respectively. This pressure range is within the guidelines of 40-80 psi based on Ottawa's Design Guidelines for Water Distribution. Assuming a 5psi head loss per floor of development, pressures at the 27th level of the building will be below the required 40psi, and as such, booster pumps are to be designed by the mechanical engineering consultant will be required to service the upper levels of the development.

Using boundary conditions for the proposed development under maximum day demands and a fire flow requirement of 10,000L/min per the FUS methodology, it can be confirmed that the system will maintain a residual pressure of approximately 50.5 psi; which is in excess of the required 140 kPa (20 psi). The above demonstrates that the existing watermain within Nepean Street and Lisgar Street can individually provide adequate fire and domestic flows in excess of flow requirements for the subject site.

The proposed development has basic day demands exceeding 50 m^3/day, as such, two watermain service connections were provided on both the north and southern boundaries of the site to maintain looping. Existing hydrants are located both north and south of the subject site and is within 45m of the proposed buildings.

3.3 SUMMARY OF FINDINGS

In conclusion, based on the boundary conditions available, the 300 mm diameter watermain on Lisgar Street in combination with the 300mm diameter watermain on Nepean Street provide adequate fire flow capacity as per the requirements of the Fire Underwriters Survey. A 150 mm diameter service lateral connected to the 300 mm diameter watermain on Lisgar Street and a 150mm diameter service lateral connected to the 300mm watermain on Nepean Street will be capable of providing the anticipated water demands to the lower storeys. A booster pump, to be designed by the building's mechanical engineer, will be required to maintain minimum pressures of 350 kPa (50 psi) for the upper storeys.

4.0 WASTEWATER SERVICING

The overall site will be serviced through an existing 375mm diameter sanitary sewer situated withing the Lisgar Street ROW at the southern boundary of the site (as illustrated on **Drawing SSP-1)**. It is proposed to make one 200mm diameter service lateral connection directly to the existing sewer to service the proposed site.

4.1 DESIGN CRITERIA

As outlined in the City of Ottawa Sewer Design Guidelines and the MECP's Design Guidelines for Sewage Works, the following criteria were used to calculate estimated wastewater flow rates and to size the sanitary sewers:

- Minimum Velocity – 0.6 m/s (0.8 m/s for upstream sections)
- Maximum Velocity – 3.0 m/s
- Manning roughness coefficient for all smooth wall pipes – 0.013
- Minimum size – 200mm dia. for residential areas
- Average Wastewater Generation – 280L/cap/day
- Peak Factor – 4.0 (Harmon's)
- Extraneous Flow Allowance – 0.33 l/s/ha (conservative value)
- Manhole Spacing – 120 m
- Minimum Cover – 2.5m
- Population density for studio and single-bedroom apartments – 1.4 pers./apartment
- Population density for two-bedroom apartments (dorms) – 2.1 pers./bedroom
- Population density for two-bedroom apartments (dorms) – 3.1 pers./bedroom

4.2 PROPOSED SERVICING

The proposed site will be serviced by gravity sewers which will direct the wastewater flows (approx. 9.9 L/s with allowance for infiltration) to the existing 375mm diameter sanitary sewer. A Sanitary sewer design sheet for the proposed service lateral is included in **Appendix B**. Full port backwater valves are to be installed on all sanitary services within the site to prevent any surcharge from the downstream sewer main from impacting the proposed property.

5.0 STORMWATER MANAGEMENT AND SERVICING

5.1 OBJECTIVES

The objective of this stormwater servicing and stormwater management (SWM) plan is to determine the measures necessary to control the quantity and quality of stormwater released from the proposed development to meet the criteria established during the consultation process with the City of Ottawa, and to provide sufficient details required for approval and construction.

5.2 SWM CRITERIA AND CONSTRAINTS

Criteria were established by combining current design practices outlined by the City of Ottawa Design Guidelines (2012), and through consultation with City of Ottawa staff. The following summarizes the criteria, with the source of each criterion indicated in brackets:

General

- Use of the dual drainage principle (City of Ottawa).
- Wherever feasible and practical, site-level measures should be used to reduce and control the volume and rate of runoff. (City of Ottawa)
- Assess impact of 100-year storm event outlined in the City of Ottawa Sewer Design Guidelines on major & minor drainage system (City of Ottawa)

Storm Sewer & Inlet Controls

- All stormwater runoff from the site up to and including the 100-year storm event to be stored on site and released into the minor system at a maximum discharge equivalent to the 5 year storm predevelopment release rate at a maximum runoff coefficient of 0.5.
- Proposed site to discharge the existing 675mm diameter storm sewer running east along Lisgar Street ROW at the boundary of the subject site (City of Ottawa), which ultimately discharges into the Rideau Canal adjacent to Cooper Street.
- Minimum inlet time of concentration to be 10 minutes, or as determined through calculations.

5.3 STORMWATER MANAGEMENT

The intent of the stormwater management plan presented herein is to mitigate any negative impact that the proposed development will have on the existing storm sewer infrastructure, while providing adequate capacity to service the proposed buildings, parking and access areas. The proposed stormwater management plan is designed to detain runoff on the roof areas and direct the roof drain outflows to a storage cistern to ensure that peak flows after construction will not exceed the allowable site release rate detailed below.

A large portion of the site is covered by roof areas and pedestrian access walkways that constitutes as clean runoff, not requiring further quality control measures.

A summary of subareas and runoff coefficients is provided in **Appendix C**, and **Drawing SD-1** indicates the stormwater management subcatchments.

5.3.1 Allowable Release Rate

The Modified Rational Method was employed to assess the rate of runoff generated during pre-development conditions. Based on consultation with City of Ottawa staff, the peak post-development discharge from the subject site to be controlled to the 5-year predevelopment release rate, to a maximum runoff coefficient C of 0.5. The predevelopment release rate for the area has been determined using the rational method based on the criteria above. A time of concentration for the predevelopment area (10 minutes) was assigned based on the relatively small site and its proximity to the existing drainage outlet for the site. C coefficient values have been increased by 25% for the post-development 100-year storm event based on MTO Drainage Manual recommendations. Peak flow rates have been calculated using the rational method as follows:

Q = 2.78 CiA
Where: Q = peak flow rate, L/s
A = drainage area, ha
I = rainfall intensity, mm/hr (per Ottawa IDF curves)
C = site runoff coefficient

The target release rate for the site is summarized in **Table 3** below:

Table 3: Target Release Rate

Design Storm	Target Flow Rate (L/s)
5 and 100 year storm	39.1

5.3.2 Storage Requirements

The site requires quantity control measures to meet the restrictive stormwater release criteria. The use of controlled rooftop storage in addition to an underground cistern contained within the underground parking garage are proposed to reduce site peak outflow to target rates.

5.3.2.1 Rooftop Storage

It is proposed to retain stormwater on the 25th, and 27th storey rooftops by installing restricted flow roof drains. Stormwater flows from lower-level roofs will be uncontrolled and directed to the cistern. The following calculations assume that roofs will be equipped with a total of 12 Watts Model R1100 Accuflow Roof Drains open at 50%.

Watts Drainage "Accutrol" roof drain weir data has been used to calculate a practical roof release rate and detention storage volume for the rooftops. It should be noted that the "Accutrol" weir has been used as an example only, and that other products may be specified for use, provided that the total roof drain release rate is restricted to match the maximum rate of release indicated in **Table 5-4**, and that sufficient roof storage is provided to meet (or exceed) the resulting volume of detained stormwater. Storage volume and controlled release rate are summarized in **Table 5-4**:

Table 5-4: Summary of Rooftop Storage (100-Year Events)

Area ID	Number of Roof Drains	Ponding Depth (mm)	Discharge (L/s)	$V_{required}$ (m^3)	$V_{available}$ (m^3)
Nepean Tower (Roof 1)	6	113.9	6.2	23.3	60.9
Lisgar Tower (Roof 2)	6	113.7	6.2	23.0	60.3

*Drainage from roof enters the cisterns.

5.3.2.2 Subsurface Storage

It is proposed to detain stormwater within a 24 m^3 cistern below grade with a maximum controlled release rate of 28.0 L/s to the gravity storm service provided. The Modified Rational Method was used to determine the peak volume requirement for the cistern. Majority of the site was assumed to be captured and directed to the underground cistern where it is temporarily stored then pumped to the building storm service connection at a controlled release rate. The cistern is equipped to allow emergency overland flow to Lisgar Street through a gooseneck discharge pipe.

Table 5-5 summarizes the flow rates and volume of stormwater in the cistern during the 100-year storm event.

Table 5-5: Peak Controlled (Tributary) 100-Year Release Rates

Storm Return Period	Area ID	Area (ha)	$Q_{release}$ (L/s)	V_{stored} (m^3)	Vavailable (m^3)
100-year	ROOF 1, ROOF 2, CISTN-1	0.25	28.0	20.7	24

5.3.3 Uncontrolled Areas

Due to grading restrictions, two subcatchment areas have been designed without a storage component. The catchment area also discharges off-site uncontrolled to the adjacent Lisgar Street and Nepean Street

ROW. Peak discharges from uncontrolled areas have been considered in the overall SWM plan and have been balanced through overcontrolling proposed site discharge rates to meet target levels.

Table 5-6 summarizes the 5 and 100-year uncontrolled release rates from the proposed development.

Table 5-6: Peak Uncontrolled 5- and 100-Year Release Rates

Storm Return Period	Area ID	Area (ha)	Runoff 'C'	Tc (min)	$Q_{release}$ (L/s)
5-year	UNC-1	0.02	0.74	10	4.0
100-year	UNC-1	0.02	0.93	10	8.6
5-year	UNC-2	0.01	0.74	10	0.9
100-year	UNC-2	0.01	0.93	10	1.8

5.3.4 Results

Table 5-7 demonstrates that the proposed stormwater management plan provides adequate attenuation storage to meet the target peak outflow for the site.

Table 5-7: Estimated Post-Development Discharge (5-Year, and 100-Year)

	5-Year Peak Discharge (L/s)	100-Year Peak Discharge (L/s)
Uncontrolled	4.9	10.4
Controlled – Cistern	28.0	28.0
Total	**32.9**	**38.4**
Target	**39.1**	**39.1**

6.0 GRADING AND DRAINAGE

The proposed site measures approximately 0.27 ha in area and is currently used as an at grade parking lot. The existing parking lot is generally flat with approximately 0.5m of grade change between Lisgar Street to Nepean Street. The site slopes gradually from west to east in keeping with the surrounding streets. A detailed grading plan (see **Drawing SSGP-1**) has been provided to satisfy the stormwater management requirements of the proposed site plan. The grading will adhere to any geotechnical restrictions for the site and to provide sufficient cover over the underground parking garage. Site grading has been established to provide emergency overland flow routes required for stormwater management in accordance with City of Ottawa requirements.

The subject site maintains emergency overland flow routes to Nepean Street and Lisgar Street ROW to the north and south as depicted on **Drawings SSGP-1** and **SD-1**.

7.0 UTILITIES

Hydro, Bell, Gas and Cable servicing for the proposed development should be readily available within subsurface utility infrastructure within the Nepean Street and Lisgar Street ROW. Exact size, location and routing of utilities, along with determination of any off-site works required for redevelopment, will be finalized after design circulation.

8.0 APPROVALS

An Ontario Ministry of the Environment, Conservation and Parks (MECP) Environmental Compliance Approval (ECAs, formerly Certificates of Approval C of A) under the Ontario Water Resources Act is not anticipated for the proposed site.

Requirement for a MECP Permit to Take Water (PTTW) for pumping during construction of the underground parking levels will be confirmed by the geotechnical consultant.

9.0 EROSION CONTROL DURING CONSTRUCTION

In order to protect downstream water quality and prevent sediment build up in catch basins and storm sewers, erosion and sediment control measures must be implemented during construction. The following recommendations will be included in the contract documents.

1. Implement best management practices to provide appropriate protection of the existing and proposed drainage system and the receiving water course(s).

2. Limit the extent of the exposed soils at any given time.

3. Re-vegetate exposed areas as soon as possible.

4. Minimize the area to be cleared and grubbed.

5. Protect exposed slopes with geotextiles, geogrid, or synthetic mulches.

6. Provide sediment traps and basins during dewatering works.

7. Install sediment traps (such as SiltSack® by Terrafix) between catch basins and frames.

8. Schedule the construction works at times which avoid flooding due to seasonal rains.

The Contractor will also be required to complete inspections and guarantee the proper performance. The inspections are to include:

• Verification that water is not flowing under silt barriers.

• Cleaning and changing the sediment traps placed on catch basins.

Refer to **Drawing EC/DS-1** for the proposed location of silt fences, straw bales, and other erosion control measures.

10.0 GEOTECHNICAL INVESTIGATION

10.1 GEOTECHNICAL INVESTIGATION

A geotechnical investigation was conducted by Paterson Group in September 2020. Subsurface soil conditions within the site were determined by 6 boreholes distributed across the proposed site. As stated in the geotechnical investigation, the subsurface profile across the site consists of a asphalt concrete layer underlying by loose to compact silty sand to silty clay with gravel and cobbles. Followed by a stiff to firm, brown to grey silty clay layer overlying native glacial till deposits consisting of silty clay with sand, gravel, cobbles, and boulders.

Groundwater levels were measured in boreholes BH1 to BH6. Groundwater levels recorded on August 31st, 2017 ranged from 10.20 to 11.31 m below the existing ground surface and are subject to seasonal fluctuations.

Pavement structures for car only parking areas and access lane routes are provided in **Table 8** and **Table 9** below.

Table 8: Pavement Structure – Car Only Parking Areas

Thickness (mm)	Material Description
50	Wear Course – HL-3 or Superpave 12.5 Asphaltic Concrete
150	Base – OPSS Granular A Crushed Stone
300	Subbase - OPSS Granular B Type II
-	Subgrade – Either fill, in situ soil or OPSS Granular B Type I or II material placed over in situ soil or fill.

Table 9: Pavement Structure – Access Lanes

Thickness (mm)	Material Description
40	Wear Course – HL-3 or Superpave 12.5 Asphaltic Concrete
50	Binder Course – HL-8 or Superpave 19.0 Asphaltic Concrete
150	Base – OPSS Granular A Crushed Stone
400	Subbase - OPSS Granular B Type II
-	Subgrade – Either fill, in situ soil or OPSS Granular B Type I or II material placed over in situ soil or fill.

11.0 CONCLUSIONS

11.1 POTABLE WATER SERVICING

Based on the supplied boundary conditions for existing watermains and estimated domestic and fire flow demands for the subject site, it is anticipated that the proposed servicing in this development will provide sufficient capacity to sustain both the required domestic demands and emergency fire flow demands of the proposed site.

11.2 WASTEWATER SERVICING

The proposed sanitary sewer network is sufficiently sized to provide gravity drainage of the site. The proposed site will be serviced by a gravity sewer service lateral which will direct wastewater flows (approx. 9.9 L/s) to the existing 375mm dia. sanitary sewer service within Lisgar Street ROW at the southern boundary of the property.

11.3 STORMWATER MANAGEMENT AND SERVICING

The proposed stormwater management plan is in compliance with goals specified through consultation with the City of Ottawa. Rooftop storage including controlled and uncontrolled roof drains directed to a cistern located within the underground parking area, which will be pumped meet the allowable release rate to the exiting 675mm storm sewer on Lisgar Street ROW. The post development release rates for all storm events are controlled to 5-year predevelopment levels as determined by the City of Ottawa staff.

11.4 GRADING

Grading for the site has been designed to provide an emergency overland flow route as per City requirements and reflects the recommendations in the Geotechnical Investigation Report prepared by Paterson Group. Erosion and sediment control measures will be implemented during construction to reduce the impact on existing facilities.

11.5 UTILITIES

Utility infrastructure exists within the Lisgar Street and Nepean Street ROW at the southern and northern boundary of the proposed site. It is anticipated that existing infrastructure will be sufficient to provide a means of distribution for the proposed site. Exact size, location and routing of utilities will be finalized after design circulation.

11.6 APPROVALS/PERMITS

An Ontario Ministry of the Environment, Conservation and Parks (MECP) Environmental Compliance Approval (ECAs, formerly Certificates of Approval C of A) under the Ontario Water Resources Act is not anticipate to be required. Requirement for a MECP Permit to Take Water (PTTW) for sewer and building construction will be confirmed by the geotechnical consultant.

APPENDICES

Appendix A POTABLE WATER SERVICING

C.1 WATER DEMAND CALCULATIONS

176 Nepean and 293-307 Lisgar - Domestic Water Demand Estimates
- Based on Graziani + Corazza Architchs (Mar 4, 2021)

Unit type	Number of Units	Person Per Unit
Studio	43	1.4
1 Bedroom	276	1.4
2 Bedroom	147	2.1
3 Bedroom	9	3.1

Building ID	Area (m^2)	Population	Daily Rate of Demand [1] (L/cap/day)	Avg Day Demand [1]		Max Day Demand [2]		Peak Hour Demand [2]	
				(L/min)	(L/s)	(L/min)	(L/s)	(L/min)	(L/s)
Residential	-	783.20	350	190.4	3.17	475.9	7.93	1047.0	17.45
Total Site :				**190.4**	**3.17**	**475.9**	**7.93**	**1047.0**	**17.45**

1 For the purpose of this study it is predicted that residential demands are based on 350 L/cap/day.
2 Water demand criteria used to estimate peak demand rates for residential areas are as follows:
maximum day demand rate = 2.5 x average day demand rate
maximum hour demand rate = 2.2 x maximum day demand rate

C.2 FIRE FLOW REQUIREMENTS PER FUS GUIDELINES

Stantec

FUS Fire Flow Calculation Sheet

Stantec Project #: 160401348
Project Name: 176 Nepean St. and 293-307 Lisgar St.
Date: 10/19/2020
Fire Flow Calculation #: 1
Description: Apartment Building

Notes:

Step	Task	Notes						Value Used	Req'd Fire Flow (L/min)
1	Determine Type of Construction	Non-Combustible Construction						0.8	-
2	Determine Ground Floor Area of One Unit	-						2700	-
	Determine Number of Adjoining Units	-						1	-
3	Determine Height in Storeys	Does not include floors >50% below grade or open attic space						1	-
4	Determine Required Fire Flow	(F = 220 x C x $A^{1/2}$). Round to nearest 1000 L/min						-	9000
5	Determine Occupancy Charge	Limited Combustible						-15%	7650
6	Determine Sprinkler Reduction	Conforms to NFPA 13						-30%	-3060
		Standard Water Supply						-10%	
		Not Fully Supervised or N/A						0%	
		% Coverage of Sprinkler System						100%	
7	Determine Increase for Exposures (Max. 75%)	Direction	Exposure Distance (m)	Exposed Length (m)	Exposed Height (Stories)	Length-Height Factor (m x stories)	Construction of Adjacent Wall	-	-
		North	20.1 to 30	42	1	31-60	Wood Frame or Non-Combustible	8%	5049
		East	0 to 3	58	16	> 120	Wood Frame or Non-Combustible	25%	
		South	20.1 to 30	47	1	31-60	Wood Frame or Non-Combustible	8%	
		West	0 to 3	58	3	> 120	Wood Frame or Non-Combustible	25%	
8	Determine Final Required Fire Flow	Total Required Fire Flow in L/min, Rounded to Nearest 1000L/min							10000
		Total Required Fire Flow in L/s							166.7
		Required Duration of Fire Flow (hrs)							2.00
		Required Volume of Fire Flow (m^3)							1200

C.3 BOUNDARY CONDITIONS

From:	Wu, John
To:	Rathnasooriya, Thakshika
Cc:	Gillis, Sheridan
Subject:	RE: Hydraulic Boundary Conditions - 176 Nepean St and 293-307 Lisgar St
Date:	Monday, January 15, 2018 9:21:44 AM
Attachments:	176 Nepean Jan 2018.pdf

Here is the result:

The following are boundary conditions, HGL, for hydraulic analysis at 176 Nepean/293 Lisgar (zone 1W) assumed to be connected to the 305mm on Nepean and 305mm on Lisgar (see attached PDF for location).

Minimum HGL = 107.0m, same at both locations

Maximum HGL = 116.1m, same at both locations

Max Day + Fire Flow (167L/s) = 107.5m, same at both locations

These are for current conditions and are based on computer model simulation.

Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation.

Thanks.

John

From: Rathnasooriya, Thakshika [mailto:Thakshika.Rathnasooriya@stantec.com]
Sent: Wednesday, January 10, 2018 9:22 AM
To: Wu, John <John.Wu@ottawa.ca>
Cc: Gillis, Sheridan <Sheridan.Gillis@stantec.com>
Subject: Hydraulic Boundary Conditions - 176 Nepean St and 293-307 Lisgar St

Good morning John,

I am looking for watermain hydraulic boundary conditions for the proposed site at 176 Nepean Street and 293-307 Lisgar Street. The high-rise will consist of 463 units in the form of two (2) apartment towers linked by a common elevator lobby. We anticipate connecting to the existing 300mm watermain on Nepean Street for the north tower and the existing 300mm watermain on

Lisgar Street for the south tower.

The intended land use is a combination of both commercial and residential.

Estimated domestic demands and fire flow requirements for the site are as follows:
Average Day Demand – 3.4L/s
Max Day Demand - 8.4L/s
Peak Hour Demand - 18.4L/s
Fire Flow Requirement per FUS - 167 (2 hour fire separation between each floor)

Thanks,

Shika Rathnasooriya
Engineering Intern

Direct: (613) 724-4081

Stantec Consulting Ltd.
400 - 1331 Clyde Avenue
Ottawa ON K2C 3G4 CA

Appendix B SANITARY SERVICING

Stantec

SUBDIVISION:

176 Nepean Street and 293 - 307 Lisgar Street

DATE: 3/10/2021
REVISION: 2
DESIGN BY: TR
CHECKED BY:

SANITARY SEWER DESIGN SHEET
(City of Ottawa)

FILE NUMBER: 160401348

DESIGN PARAMETERS

MAX PEAK FACTOR (RES.)=	4.0	AVG. DAILY FLOW / PERSON	280	l/p/day	MINIMUM VELOCITY	0.60	m/s
MIN PEAK FACTOR (RES.)=	2.0	COMMERCIAL	28,000	l/ha/day	MAXIMUM VELOCITY	3.00	m/s
PEAKING FACTOR (INDUSTRIAL):	2.4	INDUSTRIAL (HEAVY)	55,000	l/ha/day	MANNINGS n	0.013	
PEAKING FACTOR (COMM., INST.):	1.5	INDUSTRIAL (LIGHT)	35,000	l/ha/day	BEDDING CLASS	B	
PERSONS / 1 BED APT / STUDIO	1.4	INSTITUTIONAL	28,000	l/ha/day	MINIMUM COVER	2.50	m
PERSONS / 2 BED APT	2.1	INFILTRATION	0.33	l/s/Ha			
PERSONS / 3 BED APT	3.1				HARMON CORRECTION FACTOR	0.8	

LOCATION			RESIDENTIAL AREA AND POPULATION									COMMERCIAL		INDUSTRIAL (L)		INDUSTRIAL (H)		INSTITUTIONAL		GREEN / UNUSED		C+I+I	INFILTRATION			TOTAL	PIPE								
AREA ID NUMBER	FROM M.H.	TO M.H.	AREA (ha)	UNITS 1 BED / STUDIO	2 BED	3 BED	POP.	CUMULATIVE AREA (ha)	POP.	PEAK FACT.	PEAK FLOW (l/s)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	AREA (ha)	ACCU. AREA (ha)	PEAK FLOW (l/s)	TOTAL AREA (ha)	ACCU. AREA (ha)	INFILT. FLOW (l/s)	FLOW (l/s)	LENGTH (m)	DIA (mm)	MATERIAL	CLASS	SLOPE (%)	CAP. (FULL) (l/s)	CAP. V PEAK FLOW (%)	VEL. (FULL) (m/s)	VEL. (ACT.) (m/s)
BLDG	BLDG	TEE	0.27	319	147	9	783	0.27	783	3.87	9.81	0.000	0.000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.269	0.27	0.09	9.90	7.4	200 375	PVC	SDR 35	1.00	33.4	**29.61%**	1.05	0.77

Appendix C STORMWATER SERVICING AND MANAGEMENT

C.1 STORM SEWER DESIGN SHEET

Stantec

176 Nepean Street and 293 - 307 Lisgar Street		**STORM SEWER DESIGN SHEET (City of Ottawa)**	
DATE:	2021-03-10		
REVISION:	2		
DESIGNED BY:	TR	**FILE NUMBER:**	**160401348**
CHECKED BY:			

DESIGN PARAMETERS

$I = a / (t+b)^c$ (As per City of Ottawa Guidelines, 2012)

	1:2 yr	1:5 yr	1:10 yr	1:100 yr				
a =	732.951	998.071	1174.184	1735.688	MANNING'S n =	0.013	BEDDING CLASS =	B
b =	6.199	6.053	6.014	6.014	MINIMUM COVER:	2.00	m	
c =	0.810	0.814	0.816	0.820	TIME OF ENTRY	10	min	

LOCATION / DRAINAGE AREA

AREA ID NUMBER	FROM M.H.	TO M.H.	AREA (2-YEAR) (ha)	AREA (5-YEAR) (ha)	AREA (10-YEAR) (ha)	AREA (100-YEAR) (ha)	AREA (ROOF) (ha)	C (2-YEAR) (-)	C (5-YEAR) (-)	C (10-YEAR) (-)	C (100-YEAR) (-)	A x C (2-YEAR) (ha)	ACCUM AxC (2YR) (ha)	A x C (5-YEAR) (ha)	ACCUM. AxC (5YR) (ha)
BLDG	BLDG	MAIN	0.00	0.27	0.00	0.00	0.00	0.00	0.90	0.00	0.00	0.000	0.000	0.242	0.242

DRAINAGE AREA (continued)

AREA ID NUMBER	A x C (10-YEAR) (ha)	ACCUM. AxC (10YR) (ha)	A x C (100-YEAR) (ha)	ACCUM. AxC (100YR) (ha)	T of C (min)	I_{2-YEAR} (mm/h)	I_{5-YEAR} (mm/h)	$I_{10-YEAR}$ (mm/h)	$I_{100-YEAR}$ (mm/h)	$Q_{CONTROL}$ (L/s)	ACCUM. $Q_{CONTROL}$ (L/s)	Q_{ACT} (CIA/360) (L/s)
BLDG	0.000	0.000	0.000	0.000	10.00	76.81	104.19	122.14	178.56	0.0	0.0	70.1
					10.08							

PIPE SELECTION

AREA ID NUMBER	LENGTH (m)	PIPE WIDTH OR DIAMETE (mm)	PIPE HEIGHT (mm)	PIPE SHAPE (-)	MATERIAL (-)	CLASS (-)	SLOPE %	Q_{CAP} (FULL) (L/s)	% FULL (-)	VEL. (FULL) (m/s)	VEL. (ACT) (m/s)	TIME OF FLOW (min)
BLDG	6.2	300	300	CIRCULAR	PVC	-	1.00	96.2	**72.93%**	1.37	1.31	0.08
		675	675									

C.2 MODIFIED RATIONAL METHOD CALCULATIONS

Stormwater Management Calculations

File No: **160401348**
Project: **176 Neapean Street and 293-307 Lisgar Street**
Date: **10-May-21**

SWM Approach:
Post-development to Pre-development flows

Post-Development Site Conditions:

Overall Runoff Coefficient for Site and Sub-Catchment Areas

Runoff Coefficient Table								
Sub-catchment Area Catchment Type	**ID / Description**		**Area (ha) "A"**		**Runoff Coefficient "C"**		**"A x C"**	**Overall Runoff Coefficient**
Uncontrolled - Tributary	CISTN-1	Hard	0.099		0.9	0.089		
		Soft	0.000		0.2	0.000		
	Subtotal			0.0987			0.08883	0.900
Roof	ROOF 2	Hard	0.074		0.9	0.067		
		Soft	0.000		0.2	0.000		
	Subtotal			0.0743			0.06687	0.900
Uncontrolled - Tributary	UNC-2	Hard	0.003		0.9	0.003		
		Soft	0.001		0.2	0.000		
	Subtotal			0.004			0.00296	0.740
Uncontrolled - Tributary	UNC-1	Hard	0.014		0.9	0.013		
		Soft	0.004		0.2	0.001		
	Subtotal			0.0187			0.013838	0.740
Roof	ROOF 1	Hard	0.075		0.9	0.068		
		Soft	0.000		0.2	0.000		
	Subtotal			0.075			0.0675	0.900
Total				**0.271**			**0.240**	
Overall Runoff Coefficient= C:								**0.89**

Total Roof Areas	**0.149 ha**
Total Tributary Surface Areas (Controlled and Uncontrolled)	**0.121 ha**
Total Tributary Area to Outlet	**0.271 ha**
Total Uncontrolled Areas (Non-Tributary)	**0.000 ha**
Total Site	**0.271 ha**

Stormwater Management Calculations

Project #160401348, 176 Neapean Street and 293-307 Lisgar Street
Modified Rational Method Calculatons for Storage

5 yr Intensity | I = a/(t + b)^c
City of Ottawa

a =	998.071
b =	6.053
c =	0.814

t (min)	I (mm/hr)
5	141.18
10	104.19
15	83.56
20	70.25
25	60.90
30	53.93
35	48.52
40	44.18
45	40.63
50	37.65
55	35.12
60	32.94

5 YEAR Predevelopment Target Release from Portion of Site

Subdrainage Area: Predevelopment Tributary Area to Outlet
Area (ha): 0.27
C: 0.50

Typical Time of Concentration

tc (min)	I (5 yr) (mm/hr)	Qtarget (L/s)
10	104.19	**39.10**

5 YEAR Modified Rational Method for Entire Site

Subdrainage Area: CISTN-1 — Uncontrolled - Tributary
Area (ha): 0.10
C: 0.90

tc (min)	I (5 yr) (mm/hr)	Qactual (L/s)	Qrelease (L/s)	Qstored (L/s)	Vstored (m^3)
10	104.19	25.73	25.73		
20	70.25	17.35	17.35		
30	53.93	13.32	13.32		
40	44.18	10.91	10.91		
50	37.65	9.30	9.30		
60	32.94	8.14	8.14		
70	29.37	7.25	7.25		
80	26.56	6.56	6.56		
90	24.29	6.00	6.00		
100	22.41	5.53	5.53		
110	20.82	5.14	5.14		
120	19.47	4.81	4.81		

Subdrainage Area: Overall Cistern

tc (min)	I (5 yr) (mm/hr)	Qactual (L/s)	Qrelease (L/s)	Qstored (L/s)	Vstored (m^3)
10	104.19	35.99	28.00	7.99	**4.79**
20	70.25	27.80	28.00	0.00	0.00
30	53.93	23.63	28.00	0.00	0.00
40	44.18	20.98	28.00	0.00	0.00
50	37.65	19.09	28.00	0.00	0.00
60	32.94	17.63	28.00	0.00	0.00
70	29.37	16.29	28.00	0.00	0.00
80	26.56	15.15	28.00	0.00	0.00
90	24.29	14.18	28.00	0.00	0.00
100	22.41	13.34	28.00	0.00	0.00
110	20.82	12.56	28.00	0.00	0.00
120	19.47	11.79	28.00	0.00	0.00

1) All roof flows and subcatchment CISTN-1 will be directed to the cistern.
2) Outflow from cistern to be set by pump (maximum outflow rate of 28 L/s).

	Stage	Head (m)	Discharge (L/s)	Vreq (cu. m)	Vavail (cu. m)	Volume Check
5-year Water Level	N/A	N/A	28.00	4.79	24.00	OK

Subdrainage Area: ROOF 2 — Roof
Area (ha): 0.07 — Maximum Storage Depth: 150 mm
C: 0.90

tc (min)	I (5 yr) (mm/hr)	Qactual (L/s)	Qrelease (L/s)	Qstored (L/s)	Vstored (m^3)	Depth (mm)	
10	104.19	19.37	5.13	14.24	8.54	85.5	0.00
20	70.25	13.06	5.22	7.84	**9.40**	88.0	0.00
30	53.93	10.03	5.15	4.87	8.77	86.1	0.00
40	44.18	8.21	5.03	3.18	7.64	82.9	0.00
50	37.65	7.00	4.89	2.11	6.33	79.2	0.00
60	32.94	6.12	4.74	1.38	4.97	75.3	0.00
70	29.37	5.46	4.51	0.95	4.01	69.0	0.00
80	26.56	4.94	4.28	0.65	3.14	63.2	0.00
90	24.29	4.52	4.08	0.44	2.35	57.8	0.00
100	22.41	4.17	3.89	0.27	1.63	52.9	0.00
110	20.82	3.87	3.69	0.18	1.16	48.8	0.00
120	19.47	3.62	3.47	0.14	1.04	45.9	0.00

Storage: Roof Storage

	Depth (mm)	Head (m)	Discharge (L/s)	Vreq (cu. m)	Vavail (cu. m)	Discharge Check
5-year Water Level	87.96	0.09	5.22	9.40	60.30	0.00

Subdrainage Area: UNC-2 — Uncontrolled - Tributary
Area (ha): 0.004
C: 0.74

tc (min)	I (5 yr) (mm/hr)	Qactual (L/s)	Qrelease (L/s)	Qstored (L/s)	Vstored (m^3)
10	104.19	0.86	0.86		

Project #160401348, 176 Neapean Street and 293-307 Lisgar Street
Modified Rational Method Calculatons for Storage

100 yr Intensity | I = a/(t + b)^c
City of Ottawa

a =	1735.688
b =	6.014
c =	0.820

t (min)	I (mm/hr)
5	242.70
10	178.56
15	142.89
20	119.95
25	103.85
30	91.87
35	82.58
40	75.15
45	69.05
50	63.95
55	59.62
60	55.89

100 YEAR Predevelopment Target Release from Portion of Site

100 YEAR Modified Rational Method for Entire Site

Subdrainage Area: CISTN-1 — Uncontrolled - Tributary
Area (ha): 0.10
C: 1.00

tc (min)	I (100 yr) (mm/hr)	Qactual (L/s)	Qrelease (L/s)	Qstored (L/s)	Vstored (m^3)
10	178.56	48.99	48.99		
20	119.95	32.91	32.91		
30	91.87	25.21	25.21		
40	75.15	20.62	20.62		
50	63.95	17.55	17.55		
60	55.89	15.34	15.34		
70	49.79	13.66	13.66		
80	44.99	12.34	12.34		
90	41.11	11.28	11.28		
100	37.90	10.40	10.40		
110	35.20	9.66	9.66		
120	32.89	9.03	9.03		

Subdrainage Area: Overall Cistern

tc (min)	I (100 yr) (mm/hr)	Qactual (L/s)	Qrelease (L/s)	Qstored (L/s)	Vstored (m^3)
10	178.56	60.90	28.00	32.90	19.74
20	119.95	45.24	28.00	17.24	**20.69**
30	91.87	37.61	28.00	9.61	17.29
40	75.15	32.96	28.00	4.96	11.90
50	63.95	29.77	28.00	1.77	5.30
60	55.89	27.40	28.00	0.00	0.00
70	49.79	25.54	28.00	0.00	0.00
80	44.99	24.04	28.00	0.00	0.00
90	41.11	22.78	28.00	0.00	0.00
100	37.90	21.68	28.00	0.00	0.00
110	35.20	20.65	28.00	0.00	0.00
120	32.89	19.73	28.00	0.00	0.00

1) All roof flows and subcatchment CISTN-1 will be directed to the cistern.
2) Outflow from cistern to be set by pump (maximum outflow rate of 28 L/s).

	Stage	Head (m)	Discharge (L/s)	Vreq (cu. m)	Vavail (cu. m)	Volume Check
100-year Water Level	N/A	N/A	28.00	20.69	24.00	OK
					3.31	

Subdrainage Area: ROOF 2 — Roof
Area (ha): 0.07 — Maximum Storage Depth: 150 mm
C: 1.00

tc (min)	I (100 yr) (mm/hr)	Qactual (L/s)	Qrelease (L/s)	Qstored (L/s)	Vstored (m^3)	Depth (mm)	
10	178.56	36.88	5.95	30.93	18.56	107.2	0.00
20	119.95	24.78	6.16	18.62	22.34	112.8	0.00
30	91.87	18.98	6.20	12.78	**23.00**	113.7	0.00
40	75.15	15.52	6.17	9.35	22.45	112.9	0.00
50	63.95	13.21	6.10	7.11	21.32	111.3	0.00
60	55.89	11.55	6.02	5.52	19.87	109.2	0.00
70	49.79	10.28	5.94	4.35	18.26	106.8	0.00
80	44.99	9.29	5.84	3.45	16.57	104.3	0.00
90	41.11	8.49	5.75	2.75	14.83	101.8	0.00
100	37.90	7.83	5.63	2.20	13.18	98.8	0.00
110	35.20	7.27	5.48	1.79	11.81	94.8	0.00
120	32.89	6.79	5.34	1.46	10.48	91.0	0.00

Storage: Roof Storage

	Depth (mm)	Head (m)	Discharge (L/s)	Vreq (cu. m)	Vavail (cu. m)	Discharge Check
100-year Water Level	113.73	0.11	6.20	23.00	60.30	0.00

Subdrainage Area: UNC-2 — Uncontrolled - Tributary
Area (ha): 0.004
C: 0.93

tc (min)	I (100 yr) (mm/hr)	Qactual (L/s)	Qrelease (L/s)	Qstored (L/s)	Vstored (m^3)
10	178.56	1.84	1.84		

Stormwater Management Calculations

Project #160401348, 176 Neapean Street and 293-307 Lisgar Street
Modified Rational Method Calculatons for Storage

20	70.25	0.58	0.58
30	53.93	0.44	0.44
40	44.18	0.36	0.36
50	37.65	0.31	0.31
60	32.94	0.27	0.27
70	29.37	0.24	0.24
80	26.56	0.22	0.22
90	24.29	0.20	0.20
100	22.41	0.18	0.18
110	20.82	0.17	0.17
120	19.47	0.16	0.16

Subdrainage Area: UNC-1 Uncontrolled - Tributary
Area (ha): 0.02
C: 0.74

tc (min)	I (5 yr) (mm/hr)	Qactual (L/s)	Qrelease (L/s)	Qstored (L/s)	Vstored (m^3)
10	104.19	4.01	4.01		
20	70.25	2.70	2.70		
30	53.93	2.07	2.07		
40	44.18	1.70	1.70		
50	37.65	1.45	1.45		
60	32.94	1.27	1.27		
70	29.37	1.13	1.13		
80	26.56	1.02	1.02		
90	24.29	0.93	0.93		
100	22.41	0.86	0.86		
110	20.82	0.80	0.80		
120	19.47	0.75	0.75		

Subdrainage Area: ROOF 1 Roof
Area (ha): 0.08 Maximum Storage Depth: 150 mm
C: 0.90

tc (min)	I (5 yr) (mm/hr)	Qactual (L/s)	Qrelease (L/s)	Qstored (L/s)	Vstored (m^3)	Depth (mm)	
10	104.19	19.55	5.13	14.42	8.65	85.6	0.00
20	70.25	13.18	5.23	7.95	**9.55**	88.1	0.00
30	53.93	10.12	5.16	4.96	8.92	86.3	0.00
40	44.18	8.29	5.04	3.25	7.80	83.2	0.00
50	37.65	7.07	4.90	2.17	6.50	79.5	0.00
60	32.94	6.18	4.75	1.43	5.14	75.6	0.00
70	29.37	5.51	4.53	0.98	4.13	69.6	0.00
80	26.56	4.98	4.31	0.68	3.26	63.7	0.00
90	24.29	4.56	4.10	0.46	2.46	58.4	0.00
100	22.41	4.20	3.92	0.29	1.73	53.4	0.00
110	20.82	3.91	3.73	0.18	1.19	49.2	0.00
120	19.47	3.65	3.51	0.15	1.06	46.3	0.00

Storage: Roof Storage

	Depth (mm)	Head (m)	Discharge (L/s)	Vreq (cu. m)	Vavail (cu. m)	Discharge Check
5-year Water Level	88.11	0.09	5.23	9.55	60.88	0.00

SUMMARY TO OUTLET

Tributary Area	0.248	ha
Total 5yr Flow to Sewer	28	L/s
Tributary Uncontrolled Area	0.023	ha
Total 5yr Flow Uncontrolled	5	L/s
Total Area	0.271	ha
Total 5yr Flow	32.9	L/s
Target	39.1	L/s

Project #160401348, 176 Neapean Street and 293-307 Lisgar Street
Modified Rational Method Calculatons for Storage

20	119.95	1.23	1.23
30	91.87	0.94	0.94
40	75.15	0.77	0.77
50	63.95	0.66	0.66
60	55.89	0.57	0.57
70	49.79	0.51	0.51
80	44.99	0.46	0.46
90	41.11	0.42	0.42
100	37.90	0.39	0.39
110	35.20	0.36	0.36
120	32.89	0.34	0.34

Subdrainage Area: UNC-1 Uncontrolled - Tributary
Area (ha): 0.02
C: 0.93

tc (min)	I (100 yr) (mm/hr)	Qactual (L/s)	Qrelease (L/s)	Qstored (L/s)	Vstored (m^3)
10	178.56	8.59	8.59		
20	119.95	5.77	5.77		
30	91.87	4.42	4.42		
40	75.15	3.61	3.61		
50	63.95	3.08	3.08		
60	55.89	2.69	2.69		
70	49.79	2.39	2.39		
80	44.99	2.16	2.16		
90	41.11	1.98	1.98		
100	37.90	1.82	1.82		
110	35.20	1.69	1.69		
120	32.89	1.58	1.58		

Subdrainage Area: ROOF 1 Roof
Area (ha): 0.08 Maximum Storage Depth: 150 mm
C: 1.00

tc (min)	I (100 yr) (mm/hr)	Qactual (L/s)	Qrelease (L/s)	Qstored (L/s)	Vstored (m^3)	Depth (mm)	
10	178.56	37.23	5.95	31.28	18.77	107.3	0.00
20	119.95	25.01	6.16	18.84	22.61	112.9	0.00
30	91.87	19.15	6.20	12.95	**23.31**	113.9	0.00
40	75.15	15.67	6.17	9.49	22.78	113.1	0.00
50	63.95	13.33	6.11	7.22	21.67	111.5	0.00
60	55.89	11.65	6.03	5.62	20.23	109.4	0.00
70	49.79	10.38	5.95	4.44	18.63	107.1	0.00
80	44.99	9.38	5.85	3.53	16.93	104.6	0.00
90	41.11	8.57	5.76	2.81	15.19	102.1	0.00
100	37.90	7.90	5.65	2.25	13.50	99.3	0.00
110	35.20	7.34	5.50	1.84	12.12	95.4	0.00
120	32.89	6.86	5.36	1.50	10.78	91.6	0.00

Storage: Roof Storage

	Depth (mm)	Head (m)	Discharge (L/s)	Vreq (cu. m)	Vavail (cu. m)	Discharge Check
100-year Water Level	113.87	0.11	6.20	23.31	60.88	0.00

SUMMARY TO OUTLET

Tributary Area	0.248	ha
Total 100yr Flow to Sewer	28	L/s
Tributary Uncontrolled Area	0.023	ha
Total 100yr Flow Uncontrolled	10	L/s
Total Area	0.271	ha
Total 100yr Flow	38.4	L/s
Target	39.1	L/s

Project #160401348, 176 Neapean Street and 293-307 Lisgar Street
Roof Drain Design Sheet, Area ROOFS 1-4
Standard Watts Model R1100 Accuflow Roof Drain

Rating Curve				Volume Estimation				
Elevation (m)	Discharge Rate (cu.m/s)	Outlet Discharge (cu.m/s)	Storage (cu. m)	Elevation (m)	Area (sq. m)	Volume (cu. m) Increment	Volume (cu. m) Accumulated	Water Depth (m)
0.000	0.0000	0.0000	0	0.000	0	0	0	0.000
0.025	0.0003	0.0019	0	0.025	17	0	0	0.025
0.050	0.0006	0.0038	1	0.050	67	1	1	0.050
0.075	0.0008	0.0047	5	0.075	150	4	5	0.075
0.100	0.0009	0.0057	14	0.100	267	9	14	0.100
0.125	0.0011	0.0066	31	0.125	417	17	31	0.125
0.150	0.0013	0.0076	61	0.150	600	30	61	0.150

Drawdown Estimate			
Total Volume (cu.m)	Total Time (sec)	Vol (cu.m)	Detention Time (hr)
0.0	0.0	0.0	0
1.1	286.9	1.1	0.0797
4.8	781.9	3.7	0.29691
13.6	1552.3	8.8	0.72809
30.9	2605.7	17.3	1.45188
60.7	3946.1	29.9	2.54802

Rooftop Storage Summary

Total Building Area (sq.m)		750
Assume Available Roof Area (sq.	80%	600
Roof Imperviousness		0.99
Roof Drain Requirement (sq.m/Notch)		232
Number of Roof Notches*		6
Max. Allowable Depth of Roof Ponding (m)		0.15
Max. Allowable Storage (cu.m)		61
Estimated 100 Year Drawdown Time (h)		1.1

* As per Ontario Building Code section OBC 7.4.10.4.(2)(c).

* Note: Number of drains can be reduced if multiple-notch drain used.

From Watts Drain Catalogue

Head (m)	L/min Open	L/s 75%	Notch Rating **50%**	25%	Closed
0.025	0.3155	0.3155	**0.3155**	0.3155	0.3155
0.050	0.6309	0.6309	**0.6309**	0.6309	0.3155
0.075	0.9464	0.8675	**0.7886**	0.7098	0.3155
0.100	1.2618	1.1041	**0.9464**	0.7886	0.3155
0.125	1.5773	1.3407	**1.1041**	0.8675	0.3155
0.150	1.8927	1.5773	**1.2618**	0.9464	0.3155

Calculation Results

	5yr	100yr	Available
Qresult (cu.m/s)	0.005	0.006	-
Depth (m)	0.088	0.114	0.150
Volume (cu.m)	9.5	23.3	60.9
Draintime (hrs)	0.5	1.1	

Project #160401348, 176 Neapean Street and 293-307 Lisgar Street
Roof Drain Design Sheet, Area RoofS 5-8
Standard Watts Model R1100 Accuflow Roof Drain

Rating Curve				Volume Estimation				
Elevation (m)	Discharge Rate (cu.m/s)	Outlet Discharge (cu.m/s)	Storage (cu. m)	Elevation (m)	Area (sq. m)	Volume (cu. m) Increment	Volume (cu. m) Accumulated	Water Depth (m)
0.000	0.0000	0.0000	0	0.000	0	0	0	0.000
0.025	0.0003	0.0019	0	0.025	17	0	0	0.025
0.050	0.0006	0.0038	1	0.050	66	1	1	0.050
0.075	0.0008	0.0047	5	0.075	149	4	5	0.075
0.100	0.0009	0.0057	14	0.100	264	9	14	0.100
0.125	0.0011	0.0066	31	0.125	413	17	31	0.125
0.150	0.0013	0.0076	60	0.150	594	30	60	0.150

Drawdown Estimate			
Total Volume (cu.m)	Total Time (sec)	Vol (cu.m)	Detention Time (hr)
0.0	0.0	0.0	0
1.1	284.2	1.1	0.07894
4.7	774.6	3.7	0.29409
13.5	1537.6	8.7	0.72122
30.6	2581.2	17.1	1.43822
60.2	3909.1	29.6	2.52407

Rooftop Storage Summary

Total Building Area (sq.m)		743
Assume Available Roof Area (sq.	80%	594.4
Roof Imperviousness		0.99
Roof Drain Requirement (sq.m/Notch)		232
Number of Roof Notches*		6
Max. Allowable Depth of Roof Ponding (m)		0.15
Max. Allowable Storage (cu.m)		60
Estimated 100 Year Drawdown Time (h)		1.1

* As per Ontario Building Code section OBC 7.4.10.4.(2)(c).

* Note: Number of drains can be reduced if multiple-notch drain used.

From Watts Drain Catalogue

Head (m) L/min L/s Notch Rating

Head (m)	Open	75%	**50%**	25%	Closed
0.025	0.3155	0.3155	**0.3155**	0.3155	0.3155
0.050	0.6309	0.6309	**0.6309**	0.6309	0.3155
0.075	0.9464	0.8675	**0.7886**	0.7098	0.3155
0.100	1.2618	1.1041	**0.9464**	0.7886	0.3155
0.125	1.5773	1.3407	**1.1041**	0.8675	0.3155
0.150	1.8927	1.5773	**1.2618**	0.9464	0.3155

Calculation Results

	5yr	100yr	Available
Qresult (cu.m/s)	0.005	0.006	-
Depth (m)	0.088	0.114	0.150
Volume (cu.m)	9.4	23.0	60.3
Draintime (hrs)	0.5	1.1	

Appendix D GEOTECHNICAL INVESTIGATION

patersongroup

Geotechnical Investigation

Proposed Multi-Storey Buildings
176 Nepean Street & 293-307 Lisgar Street
Ottawa, Ontario

Prepared For

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September 22, 2020

Report: PG4238-1
Revision 1

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Appendices

1.0 Introduction

Paterson Group (Paterson) was commissioned by the Richcraft (Lisgar) Limited (Richcraft) to conduct a geotechnical investigation for the proposed multi-storey buildings to be located at 176 Nepean Street and 293-307 Lisgar Street in the City of Ottawa (refer to Figure 1 - Key Plan presented in Appendix 2).

The objectives of the geotechnical investigation were to:

❏ Determine the subsoil and groundwater conditions at this site by means of boreholes.

❏ Provide geotechnical recommendations for the design of the proposed development including construction considerations which may affect its design.

The following report has been prepared specifically and solely for the aforementioned project which is described herein. It contains our findings and includes geotechnical recommendations pertaining to the design and construction of the subject development as they are understood at the time of writing this report.

Investigating the presence or potential presence of contamination on the subject property was not part of the scope of work of this present investigation. A report addressing environmental issues for the subject site was prepared under separate cover.

2.0 Proposed Project

It is our understanding that the proposed development consists of 2 high rise towers along with several low rise buildings constructed over 6 levels of underground parking encompassing the majority of the subject site.

3.0 Method of Investigation

3.1 Field Investigation

The field program for the geotechnical investigation was carried out on August 21 to 24, 2017. At that time, a total of six (6) boreholes were advanced to a maximum depth of 19.4 m. The borehole locations were determined in the field by Paterson personnel taking into consideration site features and underground services. The locations of the boreholes are shown on Drawing PG4238-1 - Test Hole Location Plan included in Appendix 2.

The boreholes were advanced using a truck-mounted auger drill rig operated by a two person crew. All fieldwork was conducted under the full-time supervision of personnel from Paterson's geotechnical division under the direction of a senior engineer. The testing procedure consisted of augering and rock coring to the required depths at the selected locations and sampling the overburden.

Sampling and In Situ Testing

Soil samples were collected from the boreholes either directly from the auger flights or using a 50 mm diameter split-spoon sampler. Rock cores were obtained using 47.6 mm inside diameter coring equipment. All samples were visually inspected and initially classified on site. The auger and split-spoon samples were placed in sealed plastic bags, and rock cores were placed securely in cardboard boxes. All samples were transported to our laboratory for further examination and classification. The depths at which the auger, split spoon and rock core samples were recovered from the boreholes are shown as AU, SS and RC, respectively, on the Soil Profile and Test Data sheets presented in Appendix 1.

The Standard Penetration Test (SPT) was conducted in conjunction with the recovery of the split-spoon samples. The SPT results are recorded as "N" values on the Soil Profile and Test Data sheets. The "N" value is the number of blows required to drive the split-spoon sampler 300 mm into the soil after a 150 mm initial penetration using a 63.5 kg hammer falling from a height of 760 mm.

The recovery value and a Rock Quality Designation (RQD) value were calculated for each drilled section of bedrock and are presented on the borehole logs. The recovery value is the length of the bedrock sample recovered over the length of the drilled section. The RQD value is the total length of intact rock pieces longer than 100 mm over the length of the core run. The values indicate the bedrock quality.

The subsurface conditions observed in the boreholes were recorded in detail in the field. The soil profiles are presented on the Soil Profile and Test Data sheets in Appendix 1 of this report.

Groundwater

Monitoring wells and flexible standpipes were installed in the boreholes to permit monitoring of the groundwater levels subsequent to the completion of the sampling program.

Sample Storage

All samples will be stored in the laboratory for a period of one month after issuance of this report. They will then be discarded unless we are otherwise directed.

3.2 Field Survey

The borehole locations were determined by Paterson personnel taking into consideration the presence of underground and aboveground services. The location and ground surface elevation at each borehole location was surveyed by Paterson personnel. The ground surface elevation at the borehole locations were surveyed with respect to a temporary benchmark (TBM), consisting of the top of a catch basin located within the northeast corner of the existing site. A geodetic elevation of 72.57 m was provided for the TBM. The borehole locations and ground surface elevation at each borehole location are presented on Drawing PG4238-1 - Test Hole Location Plan in Appendix 2.

3.3 Laboratory Testing

The soil samples and rock cores recovered from the subject site were examined in our laboratory to review the results of the field logging.

3.4 Analytical Testing

One soil sample was submitted to assess the corrosion potential for exposed ferrous metals and the potential of sulphate attacks against subsurface concrete structures. The sample was analyzed to determine the concentration of sulphate and chloride, the resistivity and the pH of the sample. The results are discussed in Subsection 6.7 and shown in Appendix 1.

4.0 Observations

4.1 Surface Conditions

The subject site is currently occupied by an at-grade parking lot. The site is bordered to the north by Nepean Street, to the south by Lisgar Street, and to the east and west by multi-storey buildings. The ground surface across the site is relatively flat and at grade with the neighbouring properties.

4.2 Subsurface Profile

Overburden

Generally, the subsurface profile encountered at the borehole locations consists of a pavement structure at the ground surface, which is composed of asphalt concrete overlying crushed stone with silt and sand. The pavement structure overlies a fill layer, consisting of loose to compact silty sand to silty clay with gravel and cobbles which extends to a depth of approximately 1.0 to 1.5 m.

A layer of very stiff to firm, brown to grey silty clay was encountered underlying the above-noted fill layer to depths of approximately 3.7 to 5.3 m.

A native glacial till deposit was encountered underlying the silty clay layer, which generally consisted of silty clay with sand, gravel, cobbles, and boulders.

Reference should be made to the Soil Profile and Test Data sheets in Appendix 1 for specific details of the soil profiles encountered at each test hole location.

Bedrock

Shale bedrock was encountered underlying the glacial till deposit at approximate depths of 6.3 to 7.6 m. Generally, the bedrock is weathered and of poor quality within the upper 3 to 5 m, becoming fair to excellent quality at depth based on the RQD values.

Based on available geological mapping, the subject site is located in an area where the bedrock mainly consists of shale of the Billings formation.

4.3 Groundwater

Groundwater levels were recorded in the monitoring wells and piezometers installed at the borehole locations on August 31, 2017. The groundwater level readings noted at that time are presented in Table 1. Based on these observations, the long-term groundwater table can be anticipated at an approximate 10 to 11 m depth. However, it should be noted that groundwater levels are subject to seasonal fluctuations and could vary at the time of construction.

Table 1 - Summary of Groundwater Level Readings

Test Hole Number	Ground Elevation (m)	Groundwater Levels (m)		Recording Date
		Depth	Elevation	
BH 1	71.84	10.20	61.64	August 31, 2017
BH 2	71.76	11.16	60.60	August 31, 2017
BH 3	71.51	10.70	60.81	August 31, 2017
BH 4	72.02	Dry	-	August 31, 2017
BH 5	72.00	11.31	60.69	August 31, 2017
BH 6	71.75	Dry	-	August 31, 2017

5.0 Discussion

5.1 Geotechnical Assessment

From a geotechnical perspective, the subject site is suitable for the proposed multi-storey buildings. The proposed buildings are recommended to be founded on conventional spread footings placed on clean, surface sounded bedrock.

Bedrock removal will be required to complete the six (6) levels of underground parking. Line drilling and controlled blasting is recommended where large quantities of bedrock need to be removed. The blasting operations should be planned and completed under the guidance of a professional engineer with experience in blasting operations.

The above and other considerations are further discussed in the following sections.

5.2 Site Grading and Preparation

Stripping Depth

Due to the anticipated founding level for the proposed building, all existing overburden material will be excavated from within the proposed building footprint. Bedrock removal will be required for the construction of the underground parking garage levels.

Bedrock Removal

Based on the bedrock encountered in the area, it is expected that line-drilling in conjunction with hoe-ramming or controlled blasting will be required to remove the bedrock. In areas of weathered bedrock and where only a small quantity of bedrock is to be removed, bedrock removal may be possible by hoe-ramming.

Prior to considering blasting operations, the effects on the existing services, buildings and other structures should be addressed. A pre-blast or construction survey located in proximity of the blasting operations should be conducted prior to commencing construction. The extent of the survey should be determined by the blasting consultant and sufficient to respond to any inquiries/claims related to the blasting operations.

As a general guideline, peak particle velocity (measured at the structures) should not exceed 25 mm/s during the blasting program to reduce the risks of damage to the existing structures.

The blasting operations should be planned and conducted under the supervision of a licensed professional engineer who is an experienced blasting consultant.

Excavation side slopes in sound bedrock could be completed with almost vertical side walls. Where bedrock is of lower quality, the excavation face should be free of any loose rock. An area specific review should be completed by the geotechnical consultant at the time of construction to determine if rock bolting or other remedial measures are required to provide a safe excavation face for areas where low quality bedrock is encountered.

Vibration Considerations

Construction operations could cause vibrations, and possibly, sources of nuisance to the community. Therefore, means to reduce the vibration levels as much as possible should be incorporated in the construction operations to maintain a cooperative environment with the residents.

The following construction equipments could cause vibrations: piling equipment, hoe ram, compactor, dozer, crane, truck traffic, etc. The construction of a temporary shoring system with soldier piles or sheet piling would require these pieces of equipment. Vibrations, caused by blasting or construction operations, could cause detrimental vibrations on the adjoining buildings and structures. Therefore, it is recommended that all vibrations be limited.

Two parameters determine the recommended vibration limit: the maximum peak particle velocity and the frequency. For low frequency vibrations, the maximum allowable peak particle velocity is less than that for high frequency vibrations. As a guideline, the peak particle velocity should be less than 15 mm/s between frequencies of 4 to 12 Hz, and 50 mm/s above a frequency of 40 Hz (interpolate between 12 and 40 Hz). These guidelines are for current construction standards. These guidelines are above perceptible human level and, in some cases, could be very disturbing to some people, a pre-construction survey is recommended to minimize the risks of claims during or following the construction of the proposed building.

Fill Placement

Fill used for grading beneath the building areas should consist, unless otherwise specified, of clean imported granular fill, such as Ontario Provincial Standard Specifications (OPSS) Granular A or Granular B Type II. This material should be tested and approved prior to delivery to the site.

The fill should be placed in lifts no greater than 300 mm thick and compacted using suitable compaction equipment for the lift thickness. Fill placed beneath the proposed building areas should be compacted to at least 98% of its standard Proctor maximum dry density (SPMDD).

Non-specified existing fill along with site-excavated soil can be used as general landscaping fill and beneath parking areas where settlement of the ground surface is of minor concern. In landscaped areas, these materials should be spread in thin lifts and at least compacted by the tracks of the spreading equipment to minimize voids. If these materials are to be used to build up the subgrade level for areas to be paved, they should be compacted in thin lifts to a minimum density of 95% of their respective SPMDD. Non-specified existing fill and site-excavated soils are not suitable for use as backfill against foundation walls unless a composite drainage blanket connected to a perimeter drainage system is provided.

5.3 Foundation Design

Bearing Resistance Values

Footings placed on a clean, surface sounded shale bedrock surface can be designed using a factored bearing resistance value at ultimate limit states (ULS) of **2,500 kPa**, incorporating a geotechnical resistance factor of 0.5.

A clean, surface-sounded bedrock bearing surface should be free of loose materials, and have no near surface seams, voids, fissures or open joints which can be detected from surface sounding with a rock hammer.

Lateral Support

The bearing medium under footing-supported structures is required to be provided with adequate lateral support with respect to excavations and different foundation levels. Adequate lateral support is provided to a sound bedrock bearing medium when a plane extending down and out from the bottom edge of the footing at a minimum of 1H:6V (or flatter) passes only through sound bedrock or a material of the same or higher capacity as the bedrock, such as concrete. A weathered bedrock bearing medium will require a lateral support zone of 1H:1V (or flatter).

Settlement

Footings bearing on an acceptable bedrock bearing surface and designed for the bearing resistance values provided herein will be subjected to negligible potential post-construction total and differential settlements.

5.4 Design for Earthquakes

Shear wave velocity testing was completed for the subject site to accurately determine the applicable seismic site classification for the proposed buildings in accordance with Table 4.1.8.4.A of the Ontario Building Code (OBC) 2012. The shear wave velocity testing was completed by Paterson personnel. The results of the shear wave velocity test are attached to the present report.

Field Program

The seismic array testing location was placed across the site in an approximate northwest-southeast direction as presented in Drawing PG4238-1 - Test Hole Location Plan in Appendix 2. Paterson field personnel placed 18 horizontal 4.5 Hz geophones mounted to the surface by means of two 75 mm ground spikes attached to the geophone land case. The geophones were spaced at 2 m intervals and connected by a geophone spread cable to a Geode 24 Channel seismograph.

The seismograph was also connected to a computer laptop and a hammer trigger switch attached to a 12 pound dead blow hammer. The hammer trigger switch sends a start signal to the seismograph. The hammer is used to strike an I-Beam seated into the ground surface, which creates a polarized shear wave. The hammer shots are repeated between four (4) to eight (8) times at each shot location to improve signal to noise ratio. The shot locations are also completed in forward and reverse directions (i.e.- striking both sides of the I-Beam seated parallel to the geophone array). The shot locations are located at 24, 4.5 and 3 m away from the first geophone, 16, 4.5, and 3 m away from the last geophone, and at the centre of the seismic array.

Data Processing and Interpretation

Interpretation for the shear wave velocity results were completed by Paterson personnel. Shear wave velocity measurement was made using reflection/refraction methods. The interpretation is performed by recovering arrival times from direct and refracted waves. The interpretation is repeated at each shot location to provide an average shear wave velocity, Vs_{30}, of the upper 30 m profile, immediately below the building's foundation. The layer intercept times, velocities from different layers and critical distances are interpreted from the shear wave records to compute the bedrock depth at each location. The bedrock velocity was interpreted using the main refractor wave velocity, which is considered a conservative estimate of the bedrock velocity due to the increasing quality of the bedrock with depth. It should be noted that as bedrock quality increases, the bedrock shear wave velocity also increases.

Given the depth of the bedrock encountered in the boreholes at the site, it is anticipated that the proposed building will be founded directly on the bedrock. Based on our testing results, the bedrock shear wave velocity is **2,408 m/s**.

The Vs_{30} was calculated using the standard equation for average shear wave velocity provided in the Ontario Building Code (OBC) 2012, and as presented below.

$$V_{s30} = \frac{Depth_{OfInterest}(m)}{\left(\frac{(Depth_{Layer1}(m)}{Vs_{Layer1}(m/s)} + \frac{Depth_{Layer2}(m)}{Vs_{Layer2}(m/s)}\right)}$$

$$V_{s30} = \frac{30m}{\left(\frac{30m}{2{,}408m/s}\right)}$$

$$V_{s30} = 2{,}408m/s$$

Based on the results of the seismic testing, the average shear wave velocity, Vs_{30}, for foundations placed on bedrock is 2,408 m/s. Therefore, a **Site Class A** is applicable for design of the proposed building founded on bedrock, as per Table 4.1.8.4. A of the OBC 2012. The soils underlying the subject site are not susceptible to liquefaction.

5.5 Basement Slab

All overburden soil will be removed for the proposed building and the basement floor slab will be founded on a bedrock medium. OPSS Granular A or Granular B Type II, with a maximum particle size of 50 mm, are recommended for backfilling below the floor slab. It is recommended that the upper 200 mm of sub-slab fill consists of a 19 mm clear crushed stone.

In consideration of the groundwater conditions encountered during the investigation, a sub-floor drainage system, consisting of lines of perforated drainage pipe subdrains connected to a positive outlet, should be provided in the clear crushed stone backfill under the lower basement floor. This is discussed further in Section 6.1.

5.6 Basement Wall

There are several combinations of backfill materials and retained soils that could be applicable for the basement walls of the subject structure. However, the conditions can be well-represented by assuming the retained soil consists of a material with an angle of internal friction of 30 degrees and a bulk (drained) unit weight of 20 kN/m^3.

Where undrained conditions are anticipated (i.e. below the groundwater level), the applicable effective (undrained) unit weight of the retained soil can be taken as 13 kN/m^3, where applicable. A hydrostatic pressure should be added to the total static earth pressure when using the effective unit weight.

It is also expected that a portion of the basement walls are to be poured against a composite drainage blanket, which will be placed against the exposed bedrock face. A nominal coefficient of at-rest earth pressure of 0.05 is recommended in conjunction with a dry unit weight of 23.5 kN/m^3 (effective unit weight of 15.5 kN/m^3) where this condition occurs. A seismic earth pressure component will not be applicable for the foundation wall, which is to be poured against the bedrock face. It is expected that the seismic earth pressure will be transferred to the underground floor slabs, which should be designed to accommodate these pressures. A hydrostatic groundwater pressure should be added for the portion below the groundwater level.

Two distinct conditions, static and seismic, should be reviewed for design calculations. The parameters for design calculations for the two conditions are presented below.

Static Conditions

The static horizontal earth pressure (P_o) could be calculated with a triangular earth pressure distribution equal to $K_o \cdot \gamma \cdot H$ where:

K_o = at-rest earth pressure coefficient of the applicable retained material, 0.5
γ = unit weight of fill of the applicable retained material (kN/m^3)
H = height of the wall (m)

An additional pressure with a magnitude equal to $K_o \cdot q$ and acting on the entire height of the wall should be added to the above diagram for any surcharge loading, q (kPa), that may be placed at ground surface adjacent to the wall. The surcharge pressure will only be applicable for static analyses and should not be used in conjunction with the seismic loading case.

Actual earth pressures could be higher than the “at-rest” case if care is not exercised during the compaction of the backfill materials to maintain a minimum separation of 0.3 m from the walls with the compaction equipment.

Seismic Conditions

The total seismic force (P_{AE}) includes both the earth force component (P_o) and the seismic component (ΔP_{AE}).

The seismic earth force (ΔP_{AE}) could be calculated using $0.375 \cdot a_c \cdot \gamma \cdot H^2/g$ where:

a_c = $(1.45 - a_{max}/g)a_{max}$
γ = unit weight of fill of the applicable retained material (kN/m^3)
H = height of the wall (m)
g = gravity, 9.81 m/s^2

The peak ground acceleration, (a_{max}), for the Ottawa area is 0.32g according to OBC 2012. The vertical seismic coefficient is assumed to be zero.

The earth force component (P_o) under seismic conditions could be calculated using $P_o = 0.5\ K_o\ \gamma\ H^2$, where $K_o = 0.5$ for the soil conditions presented above.

The total earth force (P_{AE}) is considered to act at a height, h (m), from the base of the wall, where:

$h = \{P_o \cdot (H/3) + \Delta P_{AE} \cdot (0.6 \cdot H)\}/P_{AE}$

The earth forces calculated are unfactored. For the ULS case, the earth loads should be factored as live loads, as per OBC 2012.

5.7 Pavement Structure

For design purposes, the pavement structure presented in the following tables could be used for the design of car parking areas and access lanes.

Table 2 - Recommended Pavement Structure - Car Only Parking Areas

Thickness (mm)	Material Description
50	**Wear Course** - HL 3 or Superpave 12.5 Asphaltic Concrete
150	**BASE** - OPSS Granular A Crushed Stone
300	**SUBBASE** - OPSS Granular B Type II
SUBGRADE - Either fill, in situ soil or OPSS Granular B Type I or II material placed over in situ soil or fill	

Table 3 - Recommended Pavement Structure - Access Lanes	
Thickness (mm)	**Material Description**
40	**Wear Course -** HL3 or Superpave 12.5 Asphaltic Concrete
50	**Binder Course -** HL8 or Superpave 19.0 Asphaltic Concrete
150	**BASE** - OPSS Granular A Crushed Stone
400	**SUBBASE** - OPSS Granular B Type II
SUBGRADE - Either fill, in situ soil or OPSS Granular B Type I or II material placed over in situ soil or fill	

Minimum Performance Graded (PG) 58-34 asphalt cement should be used for this project.

If soft spots develop in the subgrade during compaction or due to construction traffic, the affected areas should be excavated to a competent layer and replaced with OPSS Granular B Type II material. Weak subgrade conditions may be experienced over service trench fill materials. This may require the use of a geotextile, such as Terratrack 200 or equivalent, thicker subbase or other measures that can be recommended at the time of construction as part of the field observation program.

The pavement granular base and subbase should be placed in maximum 300 mm thick lifts and compacted to a minimum of 100% of the material's SPMDD using suitable vibratory equipment, noting that excessive compaction can result in subgrade softening.

6.0 Design and Construction Precautions

6.1 Foundation Drainage and Backfill

It is expected that the upper portion of the foundation walls will be blind poured against a drainage system which is fastened to the temporary shoring system or the vertical bedrock face.

For the portion of the proposed building foundation walls located below the long-term groundwater table, it is recommended to install a groundwater infiltration control system. In this case, a perimeter foundation drainage system will also be required as a secondary system to account for any groundwater which comes in contact with the proposed building's foundation walls.

For the groundwater infiltration control system for the lower portion of the foundation walls, the following is recommended:

- ❏ Line drill the excavation perimeter.
- ❏ Hoe ram any irregularities and prepare bedrock surface. Shotcrete areas to fill in cavities and smooth out angular features at the bedrock surface, as required based on site inspection by Paterson.
- ❏ Place a suitable membrane against the prepared bedrock surface, such as a bentomat liner system or equivalent. The membrane liner should extend from 10 m below existing grade down to footing level. The membrane liner should also extend horizontally a minimum 600 mm below the footing at underside of footing level.
- ❏ Place a composite drainage layer, such as Delta Drain 6000 or equivalent, over the membrane (as a secondary system). The composite drainage layer should extend from finished grade to underside of footing level.
- ❏ Pour foundation wall against the composite drainage system.

It is also recommended that 100 mm diameter sleeves at 3 m centres be cast in the footing or at the foundation wall/footing interface to allow the infiltration of any water that breaches the waterproofing system to flow to an interior perimeter drainage pipe. The perimeter drainage pipe should direct water to sump pit(s) within the lower basement area.

Underfloor Drainage

It is anticipated that underfloor drainage will be required to control water infiltration. For preliminary design purposes, we recommend that 150 mm in perforated pipes be placed at 6 m centres. The spacing of the underfloor drainage system should be confirmed at the time of completing the excavation when water infiltration can be better assessed.

Foundation Backfill

Where sufficient space is available for conventional backfilling of foundation walls, backfill against the exterior sides of the foundation walls should consist of free-draining, non-frost susceptible granular materials. Imported granular materials, such as clean sand or OPSS Granular B Type I granular material, should be used for this purpose.

6.2 Protection Against Frost Action

Perimeter footings of heated structures are required to be insulated against the deleterious effects of frost action. A minimum of 1.5 m of soil cover alone, or a minimum of 0.6 m of soil cover in conjunction with adequate foundation insulation, should be provided.

Exterior unheated footings, such as those for isolated exterior piers, are more prone to deleterious movement associated with frost action than the exterior walls of the heated structure and require additional protection, such as soil cover of 2.1 m or an equivalent combination of soil cover and foundation insulation.

However, the footings are generally not expected to require protection against frost action due to the founding depth. Unheated structures such as the access ramp may require insulation for protection against the deleterious effects of frost action.

6.3 Excavation Side Slopes

The side slopes of excavations in the soil and fill overburden materials should be either cut back at acceptable slopes or should be retained by shoring systems from the start of the excavation until the structure is backfilled. Given that the proposed building is anticipated to extend to the property lines, it is expected that a temporary shoring will be required to support the excavation.

Unsupported Excavations

For excavations undertaken by open-cut methods (i.e. unsupported excavations), the excavation side slopes above the groundwater level extending to a maximum depth of 3 m should be cut back at 1H:1V or flatter. The flatter slope is required for excavation below groundwater level. The subsoil at this site is considered to be mainly Type 2 and 3 soil according to the Occupational Health and Safety Act and Regulations for Construction Projects.

Excavated soil should not be stockpiled directly at the top of excavations and heavy equipment should be kept away from the excavation sides.

Slopes in excess of 3 m in height should be periodically inspected by the geotechnical consultant in order to detect if the slopes are exhibiting signs of distress.

It is recommended that a trench box be used at all times to protect personnel working in trenches with steep or vertical sides. It is expected that services will be installed by "cut and cover" methods and excavations will not be left open for extended periods of time.

Temporary Shoring

As noted above, a temporary shoring is anticipated to be required to support the overburden soils. The design and approval of the shoring system will be the responsibility of the shoring contractor and the shoring designer hired by the shoring contractor. It is the responsibility of the shoring contractor to ensure that the temporary shoring is in compliance with safety requirements, designed to avoid any damage to adjacent structures and include dewatering control measures. In the event that subsurface conditions differ from the approved design during the actual installation, it is the responsibility of the shoring contractor to commission the required experts to re-assess the design and implement the required changes. The shoring designer should also take into account the impact of a significant precipitation event and designate design measures to ensure that a precipitation will not negatively impact the shoring system or soils supported by the system. Any changes to the approved shoring design system should be reported immediately to the owner's structural design prior to implementation.

The temporary system could consist of soldier pile and lagging system or interlocking steel sheet piling. Any additional loading due to street traffic, construction equipment, adjacent structures and facilities, etc., should be included to the earth pressures described below. These systems could be cantilevered, anchored or braced. Generally, the shoring systems should be provided with tie-back rock anchors to ensure stability. The shoring system is recommended to be adequately supported to resist toe failure, if required, by means of rock bolts or extending the piles into the bedrock through pre-augered holes if a soldier pile and lagging system is the preferred method.

The earth pressures acting on the shoring system may be calculated with the following parameters.

Table 4 - Soil Parameters

Parameters	Values
Active Earth Pressure Coefficient (K_a)	0.33
Passive Earth Pressure Coefficient (K_p)	3
At-Rest Earth Pressure Coefficient (K_o)	0.5
Dry Unit Weight (γ), kN/m^3	20
Effective Unit Weight (γ), kN/m^3	13

The active earth pressure should be calculated where wall movements are permissible while the at-rest pressure should be calculated if no movement is permissible. The dry unit weight should be calculated above the groundwater level while the effective unit weight should be calculated below the groundwater level.

The hydrostatic groundwater pressure should be included to the earth pressure distribution wherever the effective unit weight are calculated for earth pressures. If the groundwater level is lowered, the dry unit weight for the soil/bedrock should be calculated full weight, with no hydrostatic groundwater pressure component.

For design purposes, the minimum factor of safety of 1.5 should be calculated.

6.4 Pipe Bedding and Backfill

A minimum of 300 mm of OPSS Granular A should be placed for bedding for sewer or water pipes when placed on bedrock subgrade. The bedding should extend to the spring line of the pipe. Cover material, from the spring line to a minimum of 300 mm above the pipe obvert should consist of OPSS Granular A (concrete or PSM PVC pipes) or sand (concrete pipe). The bedding and cover materials should be placed in maximum 225 mm thick lifts compacted to a minimum of 95% of the SPMDD.

Where hard surface areas are considered above the trench backfill, the trench backfill material within the frost zone (about 1.8 m below finished grade) should match the soils exposed at the trench walls to reduce the potential differential frost heaving. The trench backfill should be placed in maximum 300 mm thick loose lifts and compacted to a minimum of 95% of the SPMDD.

6.5 Groundwater Control

Groundwater Control for Building Construction

The contractor should be prepared to direct water away from all bearing surfaces and subgrades, regardless of the source, to prevent disturbance to the founding medium.

Infiltration levels are anticipated to be low through the excavation face, and the groundwater infiltration is anticipated to be controllable with open sumps and pumps.

A temporary Ministry of the Environment, Conservation and Parks (MECP) permit to take water (PTTW) may be required for this project if more than 400,000 L/day of ground and/or surface water is to be pumped during the construction phase. A minimum of 4 to 5 months should be allocated for completion of the PTTW application package and issuance of the permit by the MOECC.

For typical ground or surface water volumes being pumped during the construction phase, typically between 50,000 to 400,000 L/day, it is required to register on the Environmental Activity and Sector Registry (EASR). A minimum of two to four weeks should be allotted for completion of the EASR registration and the Water Taking and Discharge Plan to be prepared by a Qualified Person as stipulated under O.Reg. 63/16. If a project qualifies for a PTTW based upon anticipated conditions, an EASR will not be allowed as a temporary dewatering measure while awaiting the MECP review of the PTTW application.

Long-term Groundwater Control

Our recommendations for the proposed building's long-term groundwater control are presented in Subsection 6.1. Any groundwater which breaches the building's perimeter groundwater infiltration control system will be directed to the proposed building's sump pit. Provided the proposed groundwater infiltration control system is properly implemented and approved by the geotechnical consultant at the time of construction, it is expected that groundwater flow will be very low to negligible (less than 2,000 L/day), with peak periods noted after rain events. A more accurate estimate can be provided at the time of construction, once groundwater infiltration levels are observed. It is anticipated that the groundwater flow will be controllable using conventional open sumps.

Impacts on Neighbouring Structures

Based on our observations, a local groundwater lowering is not anticipated under short-term conditions due to construction of the proposed building. It should be noted that the extent of any significant groundwater lowering will take place within a limited range of the subject site due to the minimal temporary groundwater lowering.

The neighbouring structures are expected to be founded within native glacial till and/or directly over a bedrock bearing surface. Therefore, issues are not expected with respect to groundwater lowering that would cause long term damage to adjacent structures surrounding the proposed building.

6.6 Winter Construction

Precautions must be taken if winter construction is considered for this project.

Where excavations are completed in proximity of existing structures which may be adversely affected due to the freezing conditions. In particular, where a shoring system is constructed, the soil behind the shoring system will be subjected to freezing conditions and could result in heaving of the structure(s) placed within or above frozen soil. Provisions should be made in the contract document to protect the walls of the excavations from freezing, if applicable.

In the event of construction during below zero temperatures, the founding stratum should be protected from freezing temperatures by the installation of straw, propane heaters and tarpaulins or other suitable means. The base of the excavations should be insulated from sub-zero temperatures immediately upon exposure and until such time as heat is adequately supplied to the building and the footings are protected with sufficient soil cover to prevent freezing at founding level.

Trench excavations and pavement construction are difficult activities to complete during freezing conditions without introducing frost in the subgrade or in the excavation walls and bottoms. Precautions should be considered if such activities are to be completed during freezing conditions. Additional information could be provided, if required.

6.7 Corrosion Potential and Sulphate

The results of analytical testing show that the sulphate content is less than 0.1%. This result is indicative that Type 10 Portland cement (normal cement) would be appropriate for this site. The chloride content and the pH of the sample indicate that they are not significant factors in creating a corrosive environment for exposed ferrous metals at this site, whereas the resistivity is indicative of an aggressive to very aggressive corrosive environment.

7.0 Recommendations

It is recommended that the following be carried out once the master plan and site development are determined:

- ❑ Review the Contractor's design of the temporary shoring system.
- ❑ Observation of all bearing surfaces prior to the placement of concrete.
- ❑ Sampling and testing of the concrete and fill materials used.
- ❑ Periodic observation of the condition of unsupported excavation side slopes in excess of 3 m in height, if applicable.
- ❑ Observation of all subgrades prior to backfilling.
- ❑ Field density tests to determine the level of compaction achieved.
- ❑ Sampling and testing of the bituminous concrete including mix design reviews.

A report confirming that these works have been conducted in general accordance with our recommendations could be issued upon request, following the completion of a satisfactory material testing and observation program by the geotechnical consultant.

8.0 Statement of Limitations

The recommendations made in this report are in accordance with our present understanding of the project. Our recommendations should be reviewed when the drawings and specifications are complete.

A geotechnical investigation is a limited sampling of a site. Should any conditions at the site be encountered which differ from those at the test hole locations, we request immediate notification in order to reassess our recommendations.

The recommendations provided should only be used by the design professionals associated with this project. The recommendations are not intended for contractors bidding on or constructing the project. The later should evaluate the factual information provided in the report. The contractor should also determine the suitability and completeness for the intended construction schedule and methods. Additional testing may be required for the contractors' purpose.

The present report applies only to the project described in this document. Use of this report for purposes other than those described herein or by person(s) other than Richcraft (Lisgar) Ltd. or their agent(s) is not authorized without review by this firm for the applicability of our recommendations to the altered use of the report.

Paterson Group Inc.

Scott S. Dennis, P.Eng.

David J. Gilbert, P.Eng.

LICENSED PROFESSIONAL ENGINEER
Sept. 22, 2020
D. J. GILBERT
100116130
PROVINCE OF ONTARIO

Report Distribution:

- ❏ Richcraft (Lisgar) Ltd. (3 copies)
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APPENDIX 1

SOIL PROFILE AND TEST DATA SHEETS

SYMBOLS AND TERMS

ANALYTICAL TESTING RESULTS

patersongroup Consulting Engineers

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

SOIL PROFILE AND TEST DATA

Geotechnical Investigation
176 Nepean Street and 293-307 Lisgar Street
Ottawa, Ontario

DATUM TBM - Top spindle of fire hydrant located on the south side of Lisgar Street, opposite subject site. Geodetic elevation = 72.57m.

REMARKS

BORINGS BY CME 55 Power Auger

DATE August 21, 2017

FILE NO. PG4238

HOLE NO. BH 1

SOIL DESCRIPTION	SAMPLE TYPE	NUMBER	% RECOVERY	N VALUE or RQD	DEPTH (m)	ELEV. (m)
GROUND SURFACE					0	71.84
FILL: Crushed stone with silty sand (0.13)	AU	1				
FILL: Brown silty sand, trace gravel, cobbles and construction debris (1.45)	SS	2	54	17	1	70.84
Very stiff to stiff, brown **SILTY CLAY,** trace sand (3.71)	SS	3	83	16	2	69.84
	SS	4	50	11	3	68.84
	SS	5	100	5		
GLACIAL TILL: Brown to grey silty clay, some sand, trace gravel (7.32)	SS	6	33	7	4	67.84
	SS	7	42	12	5	66.84
	SS	8	29	15	6	65.84
	SS	9	46	19		
	SS	10	67	12	7	64.84
BEDROCK: Black shale (19.18)	SS	11	83	33	8	63.84
	SS	12	60	50+	9	62.84
	RC	1	35	0	10	61.84
	RC	2	100	58	11	60.84
	RC	3	98	85	12	59.84
	RC	4	100	94	13	58.84
	RC	5	99	73	14	57.84
	RC	6	100	61	15	56.84
	RC	7	98	71	16	55.84
					17	54.84
					18	53.84
					19	52.84

End of Borehole

(GWL @ 10.21m-August 31, 2017)

Pen. Resist. Blows/0.3m
● 50 mm Dia. Cone

○ Water Content %

20 40 60 80

Monitoring Well Construction

20 40 60 80 100

Shear Strength (kPa)

▲ Undisturbed △ Remoulded

patersongroup Consulting Engineers

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

SOIL PROFILE AND TEST DATA

Geotechnical Investigation
176 Nepean Street and 293-307 Lisgar Street
Ottawa, Ontario

DATUM TBM - Top spindle of fire hydrant located on the south side of Lisgar Street, opposite subject site. Geodetic elevation = 72.57m.

REMARKS

BORINGS BY CME 55 Power Auger

DATE August 23, 2017

FILE NO. PG4238

HOLE NO. BH 1A

SOIL DESCRIPTION	STRATA PLOT	SAMPLE TYPE	SAMPLE NUMBER	SAMPLE % RECOVERY	SAMPLE N VALUE or RQD	DEPTH (m)	ELEV. (m)	Pen. Resist. Blows/0.3m ● 50 mm Dia. Cone / ○ Water Content % (20 40 60 80)	Monitoring Well Construction
GROUND SURFACE						0	71.82		
						1	70.82		
						2	69.82		
						3	68.82		
OVERBURDEN						4	67.82		
						5	66.82		
						6	65.82		
7.62						7	64.82		
		RC	1	28	0	8	63.82		
		RC	2	18	0	9	62.82		
BEDROCK: Black shale						10	61.82		
		RC	3	93	42	11	60.82		
12.19		RC	4	100	66	12	59.82		
End of Borehole									
(GWL @ 10.29m-August 31, 2017)									

Shear Strength (kPa): 20 40 60 80 100

▲ Undisturbed △ Remoulded

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154 Colonnade Road South, Ottawa, Ontario K2E 7J5

SOIL PROFILE AND TEST DATA

Geotechnical Investigation
176 Nepean Street and 293-307 Lisgar Street
Ottawa, Ontario

DATUM TBM - Top spindle of fire hydrant located on the south side of Lisgar Street, opposite subject site. Geodetic elevation = 72.57m.

REMARKS

BORINGS BY CME 55 Power Auger

DATE August 24, 2017

FILE NO. PG4238

HOLE NO. BH 2

SOIL DESCRIPTION	Strata depth (m)	TYPE	NUMBER	% RECOVERY	N VALUE or RQD	DEPTH (m)	ELEV. (m)
GROUND SURFACE						0	71.76
25mm Asphaltic concrete over crushed stone with silty sand	0.23	AU	1				
FILL: Brown silty sand, trace gravel, cobbles, boulders, clay and construction debris	1.04	SS	2	67	4	1	70.76
		SS	3	75	5	2	69.76
Very stiff to stiff, brown **SILTY CLAY,** trace sand		SS	4	100	4	3	68.76
		SS	5	100	P		
	4.40	SS	6	42	P	4	67.76
GLACIAL TILL: Grey silty clay, some sand, trace gravel, cobbles and boulders		SS	7	42	7	5	66.76
		SS	8	58	15	6	65.76
		SS	9	71	7		
	7.01	SS	10	50	30	7	64.76
BEDROCK: Black shale		RC	1	89	0	8	63.76
		RC	2	94	30	9	62.76
		RC	3	91	24	10	61.76
		RC	4	100	66	11	60.76
		RC	5	100	79	12	59.76
		RC	6	97	75	13	58.76
		RC	7	100	83	14	57.76
		RC	8	100	82	15	56.76
						16	55.76
						17	54.76
						18	53.76
	19.25					19	52.76
End of Borehole							

(GWL @ 11.16m-August 31, 2017)

Pen. Resist. Blows/0.3m
● 50 mm Dia. Cone

○ Water Content %

20 40 60 80

Monitoring Well Construction

20 40 60 80 100
Shear Strength (kPa)
▲ Undisturbed △ Remoulded

patersongroup Consulting Engineers

154 Colonnade Road South, Ottawa, Ontario K2E 7J5

SOIL PROFILE AND TEST DATA

Geotechnical Investigation
176 Nepean Street and 293-307 Lisgar Street
Ottawa, Ontario

DATUM TBM - Top spindle of fire hydrant located on the south side of Lisgar Street, opposite subject site. Geodetic elevation = 72.57m.

REMARKS

BORINGS BY CME 55 Power Auger

DATE August 22, 2017

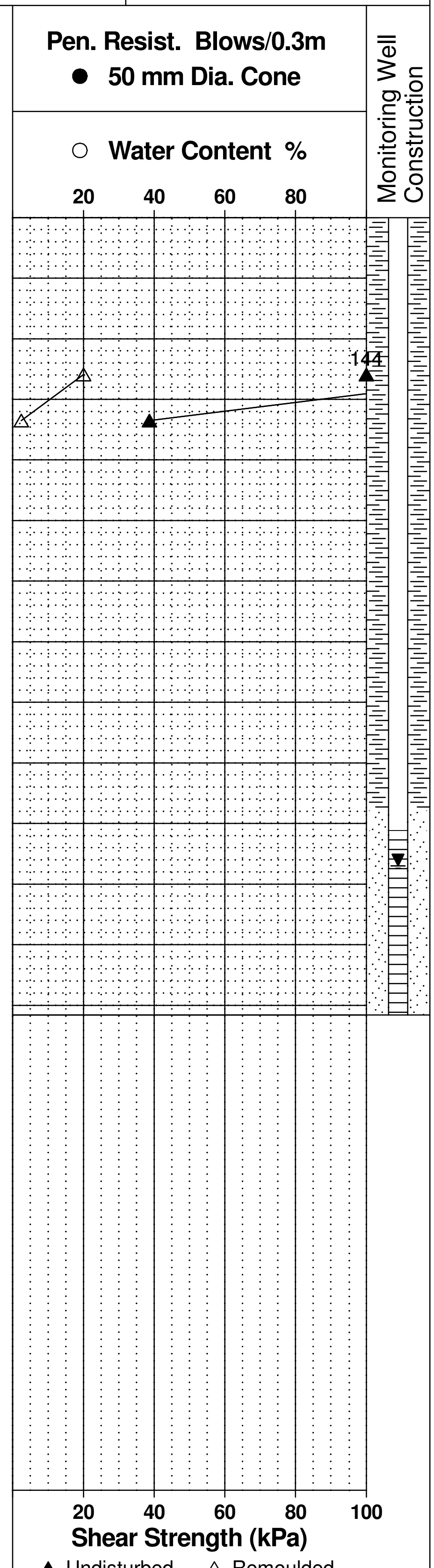
FILE NO. PG4238

HOLE NO. BH 3

SOIL DESCRIPTION	TYPE	NUMBER	% RECOVERY	N VALUE or RQD	DEPTH (m)	ELEV. (m)
GROUND SURFACE					0	71.51
FILL: 38mm Asphaltic concrete over crushed stone with silty sand 0.20	AU	1				
FILL: Brown silty sand, some brick, trace gravel, cobbles, boulders, clay 1.30	SS	2	50	12	1	70.51
Very stiff to firm, brown to grey **SILTY CLAY,** trace sand 3.73	SS	3	83	7	2	69.51
	SS	4			3	68.51
	SS		100			
GLACIAL TILL: Grey silty clay, some sand, gravel and cobbles 6.25	SS	6	71	2	4	67.51
	SS	7	42	37	5	66.51
	SS	8	50	4	6	65.51
BEDROCK: Black shale 13.16	SS	9	79	24		
	SS	10	50	50+	7	64.51
	RC	1	45	0	8	63.51
	RC	2	92	12	9	62.51
	RC	3	45	0	10	61.51
					11	60.51
	RC	4	95	62	12	59.51
					13	58.51

End of Borehole

(GWL @ 13.16m-August 31, 2017)



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154 Colonnade Road South, Ottawa, Ontario K2E 7J5

SOIL PROFILE AND TEST DATA

Geotechnical Investigation
176 Nepean Street and 293-307 Lisgar Street
Ottawa, Ontario

DATUM TBM - Top spindle of fire hydrant located on the south side of Lisgar Street, opposite subject site. Geodetic elevation = 72.57m.

REMARKS

BORINGS BY CME 55 Power Auger

DATE August 21, 2017

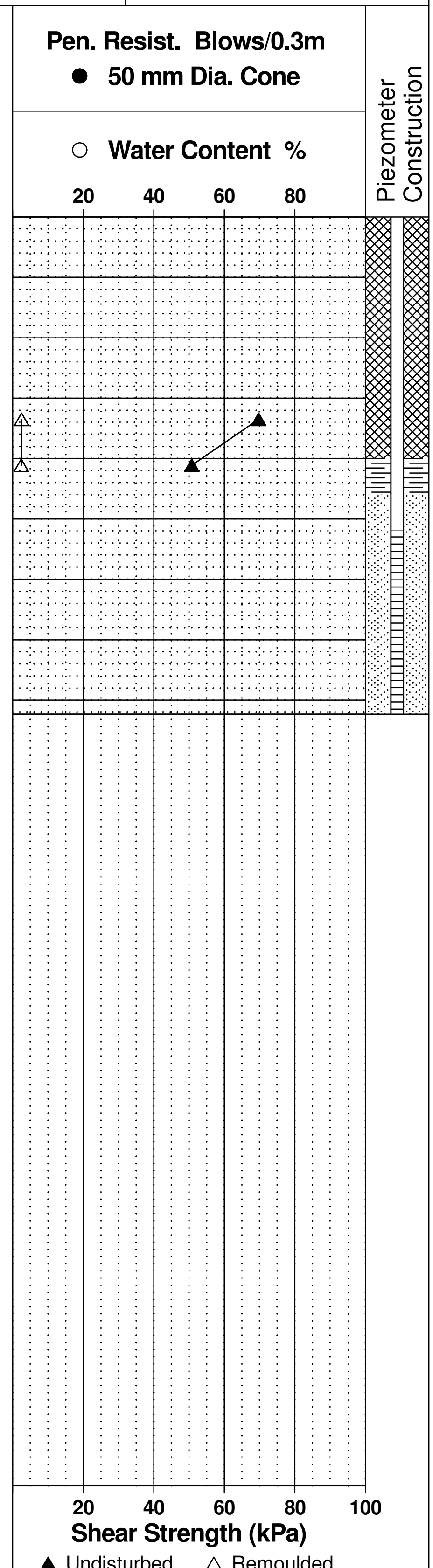
FILE NO. PG4238

HOLE NO. BH 4

SOIL DESCRIPTION	Strata depth (m)	SAMPLE TYPE	NUMBER	% RECOVERY	N VALUE or RQD	DEPTH (m)	ELEV. (m)
GROUND SURFACE						0	72.02
FILL: 50mm Asphaltic concrete over crushed stone with silty sand	0.36	AU	1				
FILL: Brown silty sand, trace gravel and cobbles	1.45	SS	2	17	3	1	71.02
Very stiff to stiff, brown to grey **SILTY CLAY,** trace sand		SS	3	83	10	2	70.02
		SS	4	100	7	3	69.02
		SS	5	100	P		
	4.50	SS	6	100	P	4	68.02
GLACIAL TILL: Grey silty clay, some sand, trace gravel and cobbles		SS	7	50	1	5	67.02
		SS	8	46	1	6	66.02
	7.01	SS	9	58	15		
BEDROCK: Black shale		SS	10	56	24	7	65.02
	8.23	SS	11	71	50+	8	64.02

End of Borehole

(BH dry - August 31, 2017)



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154 Colonnade Road South, Ottawa, Ontario K2E 7J5

SOIL PROFILE AND TEST DATA

Geotechnical Investigation
176 Nepean Street and 293-307 Lisgar Street
Ottawa, Ontario

DATUM TBM - Top spindle of fire hydrant located on the south side of Lisgar Street, opposite subject site. Geodetic elevation = 72.57m.

REMARKS

BORINGS BY CME 55 Power Auger

DATE August 23, 2017

FILE NO. PG4238

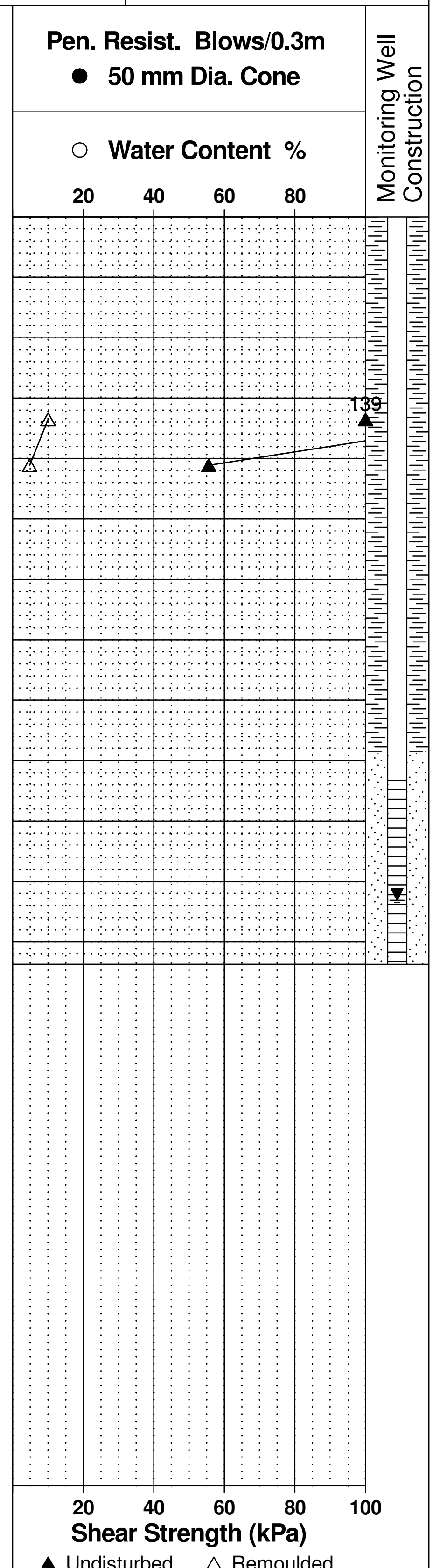
HOLE NO. BH 5

SOIL DESCRIPTION	Depth to base (m)	SAMPLE TYPE	NUMBER	% RECOVERY	N VALUE or RQD
GROUND SURFACE					
FILL: Asphaltic concrete over crushed stone with silty sand	0.25	AU	1		
FILL: Brown silty sand, trace gravel	1.30	SS	2	58	9
Very stiff to stiff, brown to grey **SILTY CLAY,** trace sand	4.50	SS	3	83	10
		SS	4	83	6
		SS	5	100	P
		SS	6	100	P
GLACIAL TILL: Grey silty clay, some sand, trace gravel and cobbles	7.54	SS	7	100	3
		SS	8	100	3
		SS	9	83	5
		SS	10	58	9
BEDROCK: Black shale	12.37	SS	11	83	26
		SS	12	81	50+
		RC	1	55	10
		RC	2	100	28
		RC	3	100	20

End of Borehole

(GWL @ 11.31m-August 31, 2017)

DEPTH (m)	ELEV. (m)
0	72.00
1	71.00
2	70.00
3	69.00
4	68.00
5	67.00
6	66.00
7	65.00
8	64.00
9	63.00
10	62.00
11	61.00
12	60.00



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SOIL PROFILE AND TEST DATA

Geotechnical Investigation
176 Nepean Street and 293-307 Lisgar Street
Ottawa, Ontario

DATUM TBM - Top spindle of fire hydrant located on the south side of Lisgar Street, opposite subject site. Geodetic elevation = 72.57m.

REMARKS

BORINGS BY CME 55 Power Auger

DATE August 24, 2017

FILE NO. PG4238

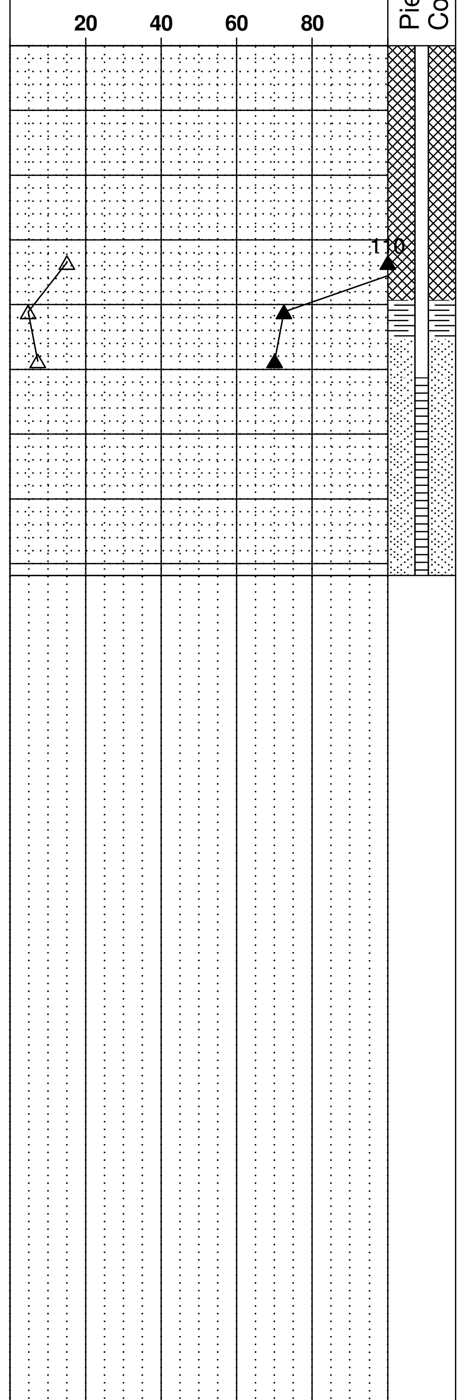
HOLE NO. BH 6

SOIL DESCRIPTION	Depth to base (m)	SAMPLE TYPE	NUMBER	% RECOVERY	N VALUE or RQD	DEPTH (m)	ELEV. (m)
GROUND SURFACE						0	71.75
FILL: Crushed stone with silt and sand	0.18	AU	1				
FILL: Brown silty clay, some sand, trace gravel and cobbles	1.27	SS	2	50	7	1	70.75
Very stiff to stiff, brown to grey **SILTY CLAY,** trace sand	5.26	SS	3	83	8	2	69.75
		SS	4	83	7		
		SS	5	100	P	3	68.75
		SS	6	100	P	4	67.75
		SS	7	100	P	5	66.75
GLACIAL TILL: Grey silty clay, some sand, trace gravel, cobbles and boulders	7.16	SS	8	50	24		
		SS	9	58	2	6	65.75
		SS	10	67	16	7	64.75
BEDROCK: Black shale	8.18	SS	11	32	51	8	63.75

End of Borehole

(BH dry - August 31, 2017)

Pen. Resist. Blows/0.3m
● 50 mm Dia. Cone
○ Water Content %



Shear Strength (kPa)
▲ Undisturbed △ Remoulded

Piezometer Construction

SYMBOLS AND TERMS

SOIL DESCRIPTION

Behavioural properties, such as structure and strength, take precedence over particle gradation in describing soils. Terminology describing soil structure are as follows:

Desiccated	-	having visible signs of weathering by oxidation of clay minerals, shrinkage cracks, etc.
Fissured	-	having cracks, and hence a blocky structure.
Varved	-	composed of regular alternating layers of silt and clay.
Stratified	-	composed of alternating layers of different soil types, e.g. silt and sand or silt and clay.
Well-Graded	-	Having wide range in grain sizes and substantial amounts of all intermediate particle sizes (see Grain Size Distribution).
Uniformly-Graded	-	Predominantly of one grain size (see Grain Size Distribution).

The standard terminology to describe the strength of cohesionless soils is the relative density, usually inferred from the results of the Standard Penetration Test (SPT) 'N' value. The SPT N value is the number of blows of a 63.5 kg hammer, falling 760 mm, required to drive a 51 mm O.D. split spoon sampler 300 mm into the soil after an initial penetration of 150 mm.

Relative Density	'N' Value	Relative Density %
Very Loose	<4	<15
Loose	4-10	15-35
Compact	10-30	35-65
Dense	30-50	65-85
Very Dense	>50	>85

The standard terminology to describe the strength of cohesive soils is the consistency, which is based on the undisturbed undrained shear strength as measured by the in situ or laboratory vane tests, penetrometer tests, unconfined compression tests, or occasionally by Standard Penetration Tests.

Consistency	Undrained Shear Strength (kPa)	'N' Value
Very Soft	<12	<2
Soft	12-25	2-4
Firm	25-50	4-8
Stiff	50-100	8-15
Very Stiff	100-200	15-30
Hard	>200	>30

SYMBOLS AND TERMS (continued)

SOIL DESCRIPTION (continued)

Cohesive soils can also be classified according to their “sensitivity”. The sensitivity is the ratio between the undisturbed undrained shear strength and the remoulded undrained shear strength of the soil.

Terminology used for describing soil strata based upon texture, or the proportion of individual particle sizes present is provided on the Textural Soil Classification Chart at the end of this information package.

ROCK DESCRIPTION

The structural description of the bedrock mass is based on the Rock Quality Designation (RQD).

The RQD classification is based on a modified core recovery percentage in which all pieces of sound core over 100 mm long are counted as recovery. The smaller pieces are considered to be a result of closely-spaced discontinuities (resulting from shearing, jointing, faulting, or weathering) in the rock mass and are not counted. RQD is ideally determined from NXL size core. However, it can be used on smaller core sizes, such as BX, if the bulk of the fractures caused by drilling stresses (called “mechanical breaks”) are easily distinguishable from the normal in situ fractures.

RQD %	ROCK QUALITY
90-100	Excellent, intact, very sound
75-90	Good, massive, moderately jointed or sound
50-75	Fair, blocky and seamy, fractured
25-50	Poor, shattered and very seamy or blocky, severely fractured
0-25	Very poor, crushed, very severely fractured

SAMPLE TYPES

SS	-	Split spoon sample (obtained in conjunction with the performing of the Standard Penetration Test (SPT))
TW	-	Thin wall tube or Shelby tube
PS	-	Piston sample
AU	-	Auger sample or bulk sample
WS	-	Wash sample
RC	-	Rock core sample (Core bit size AXT, BXL, etc.). Rock core samples are obtained with the use of standard diamond drilling bits.

SYMBOLS AND TERMS (continued)

GRAIN SIZE DISTRIBUTION

MC%	-	Natural moisture content or water content of sample, %
LL	-	Liquid Limit, % (water content above which soil behaves as a liquid)
PL	-	Plastic limit, % (water content above which soil behaves plastically)
PI	-	Plasticity index, % (difference between LL and PL)
Dxx	-	Grain size which xx% of the soil, by weight, is of finer grain sizes These grain size descriptions are not used below 0.075 mm grain size
D10	-	Grain size at which 10% of the soil is finer (effective grain size)
D60	-	Grain size at which 60% of the soil is finer
Cc	-	Concavity coefficient = $(D30)^2 / (D10 \times D60)$
Cu	-	Uniformity coefficient = D60 / D10

Cc and Cu are used to assess the grading of sands and gravels:
Well-graded gravels have: 1 < Cc < 3 and Cu > 4
Well-graded sands have: 1 < Cc < 3 and Cu > 6
Sands and gravels not meeting the above requirements are poorly-graded or uniformly-graded.
Cc and Cu are not applicable for the description of soils with more than 10% silt and clay (more than 10% finer than 0.075 mm or the #200 sieve)

CONSOLIDATION TEST

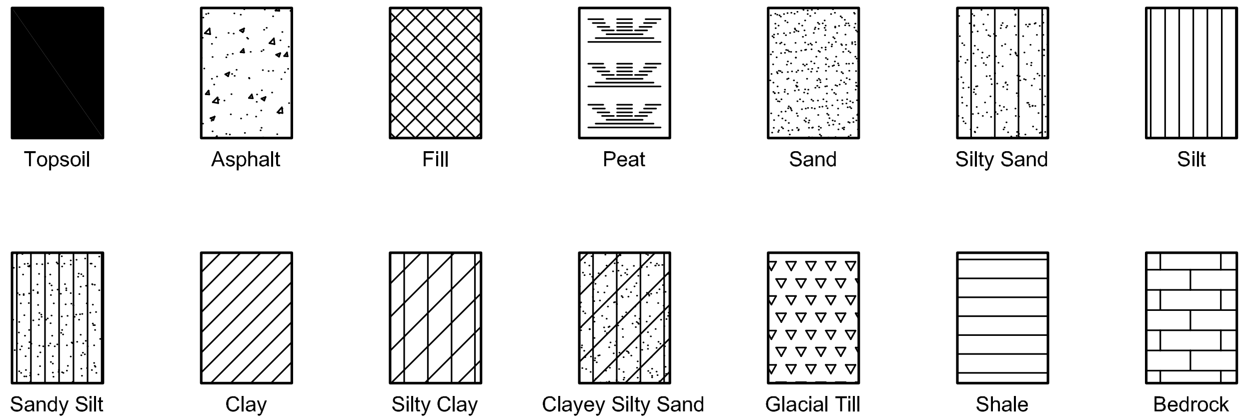
p'_o	-	Present effective overburden pressure at sample depth
p'_c	-	Preconsolidation pressure of (maximum past pressure on) sample
Ccr	-	Recompression index (in effect at pressures below p'_c)
Cc	-	Compression index (in effect at pressures above p'_c)
OC Ratio		Overconsolidaton ratio = p'_c / p'_o
Void Ratio		Initial sample void ratio = volume of voids / volume of solids
Wo	-	Initial water content (at start of consolidation test)

PERMEABILITY TEST

k	-	Coefficient of permeability or hydraulic conductivity is a measure of the ability of water to flow through the sample. The value of k is measured at a specified unit weight for (remoulded) cohesionless soil samples, because its value will vary with the unit weight or density of the sample during the test.

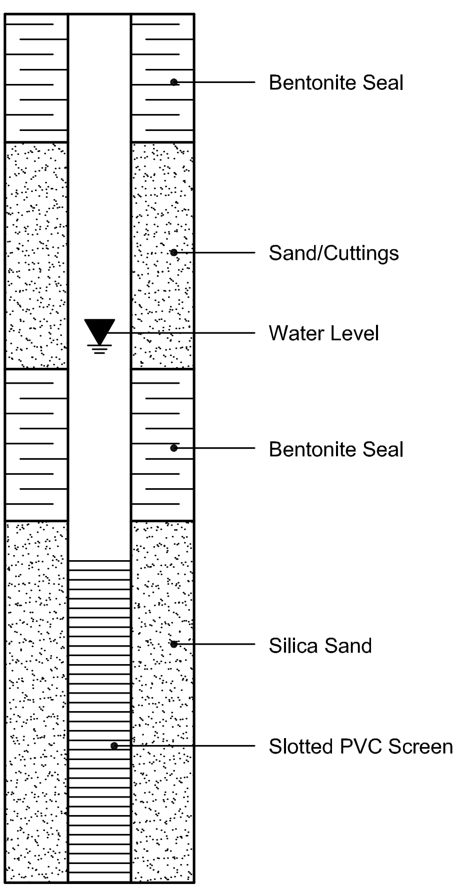
SYMBOLS AND TERMS (continued)

STRATA PLOT

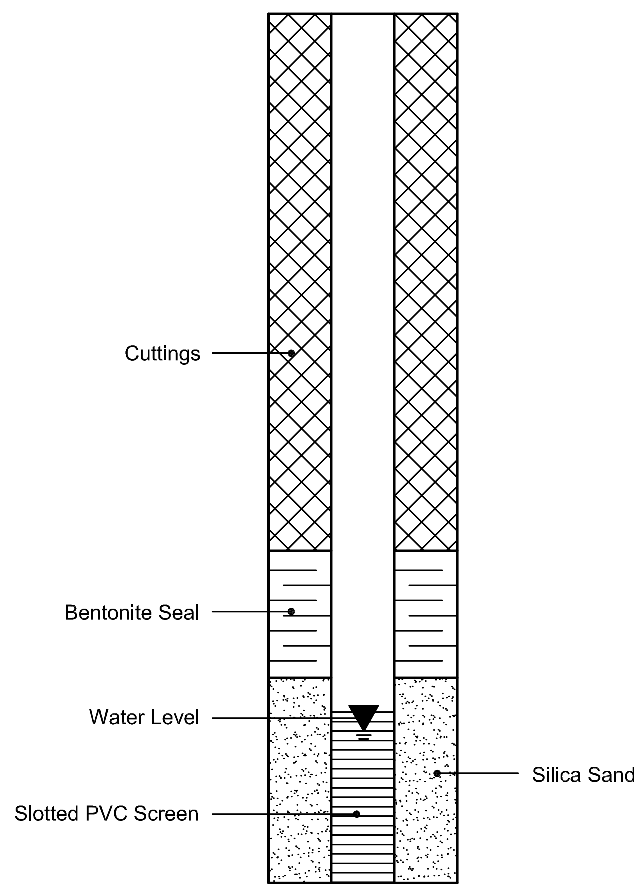


MONITORING WELL AND PIEZOMETER CONSTRUCTION

MONITORING WELL CONSTRUCTION



PIEZOMETER CONSTRUCTION



Certificate of Analysis

Client: Paterson Group Consulting Engineers

Client PO: 22178

Report Date: 31-Aug-2017

Order Date: 25-Aug-2017

Project Description: PG4238

	Client ID:	BH2-SS5	-	-	-
	Sample Date:	24-Aug-17	-	-	-
	Sample ID:	1735031-01	-	-	-
	MDL/Units	Soil	-	-	-
Physical Characteristics					
% Solids	0.1 % by Wt.	63.4	-	-	-
General Inorganics					
pH	0.05 pH Units	7.60	-	-	-
Resistivity	0.10 Ohm.m	6.51	-	-	-
Anions					
Chloride	5 ug/g dry	805	-	-	-
Sulphate	5 ug/g dry	100	-	-	-

APPENDIX 2

FIGURE 1 - KEY PLAN
FIGURE 2 - SHEAR WAVE VELOCITY PROFILE AT SHOT LOCATION - 24 M
FIGURE 3 - SHEAR WAVE VELOCITY PROFILE AT SHOT LOCATION - 4.5 M
DRAWING PG4238-1 - TEST HOLE LOCATION PLAN

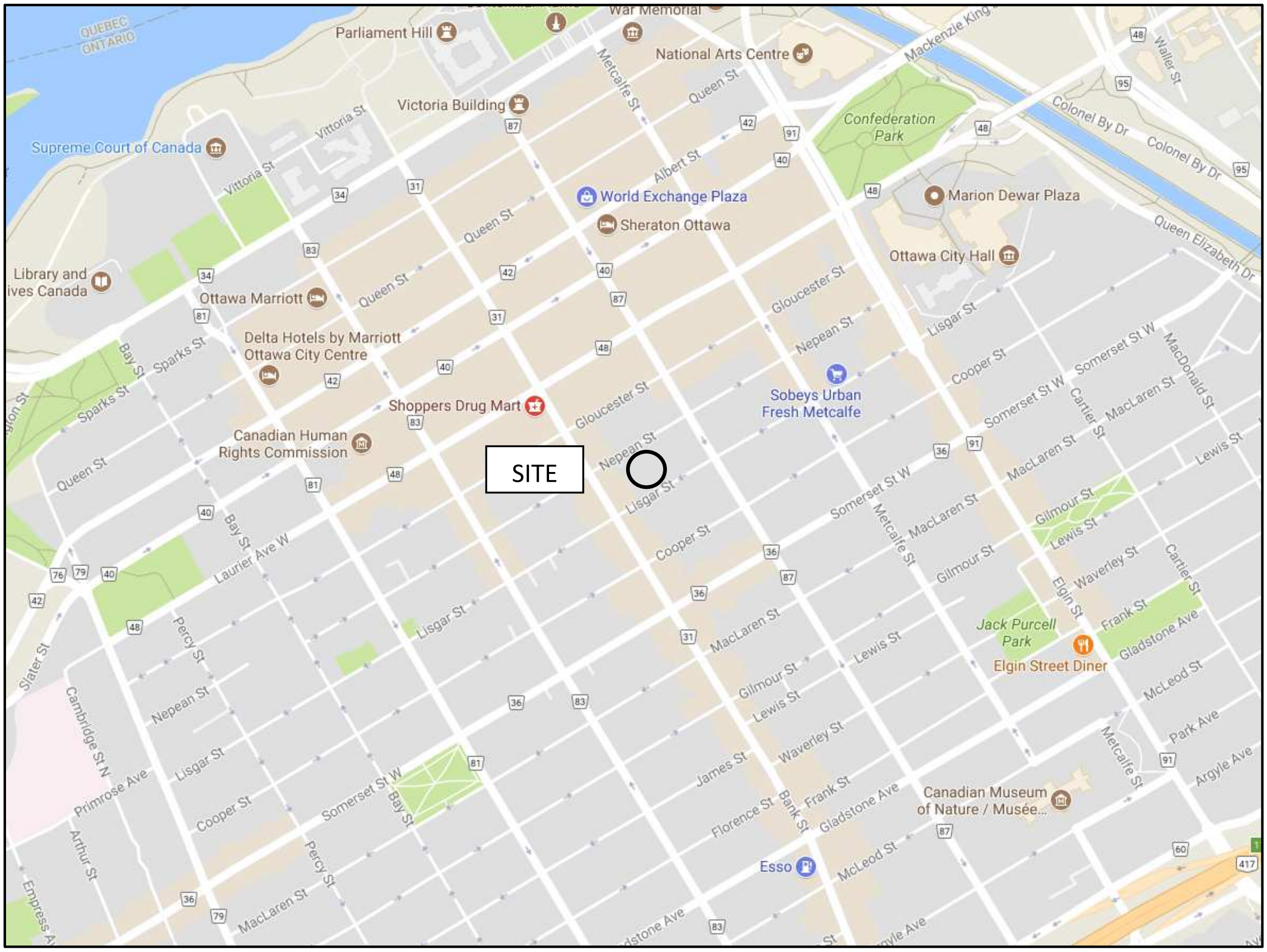


FIGURE 1

KEY PLAN

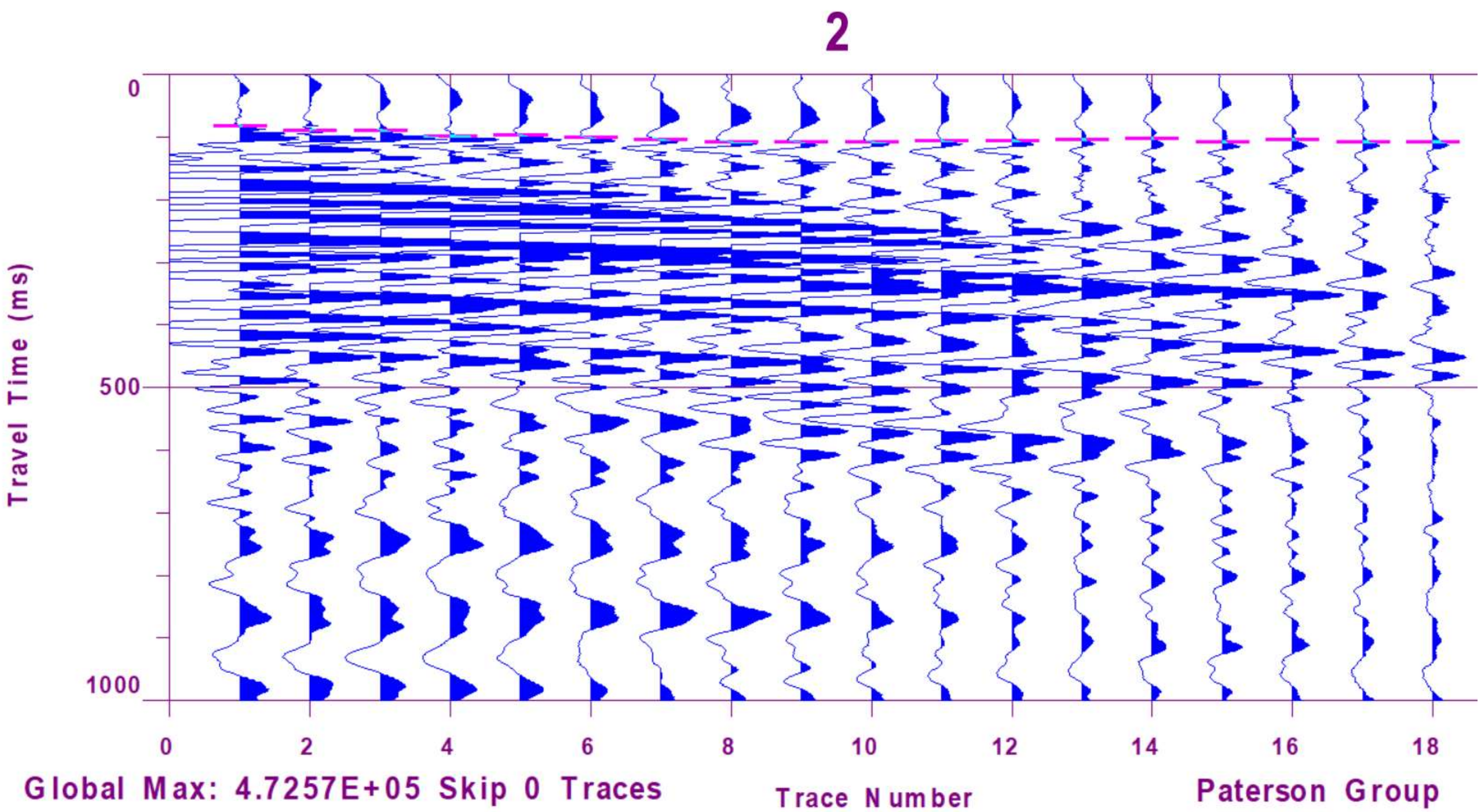


FIGURE 2

SHEAR WAVE VELOCITY PROFILE AT SHOT LOCATION -24 M

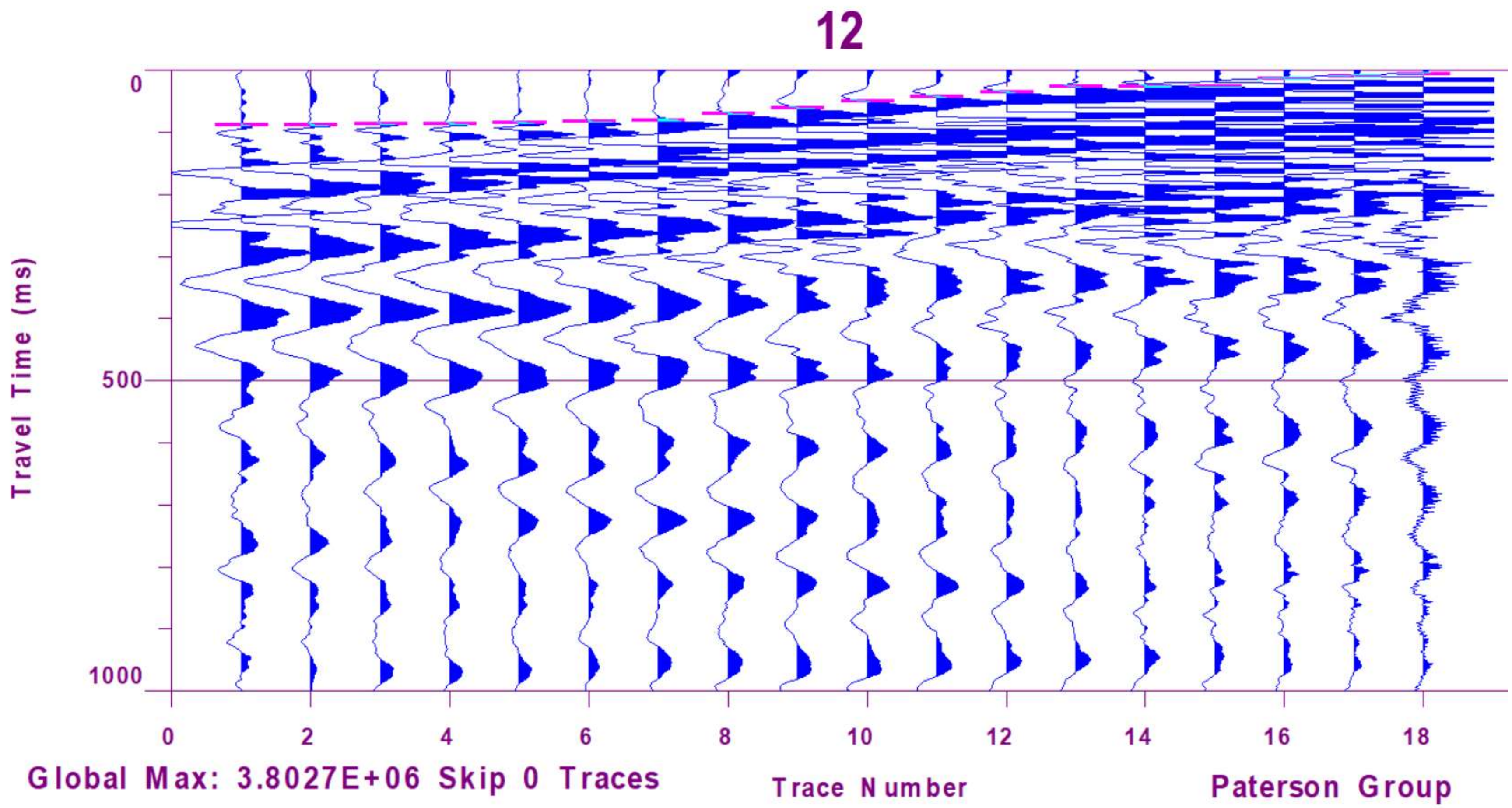
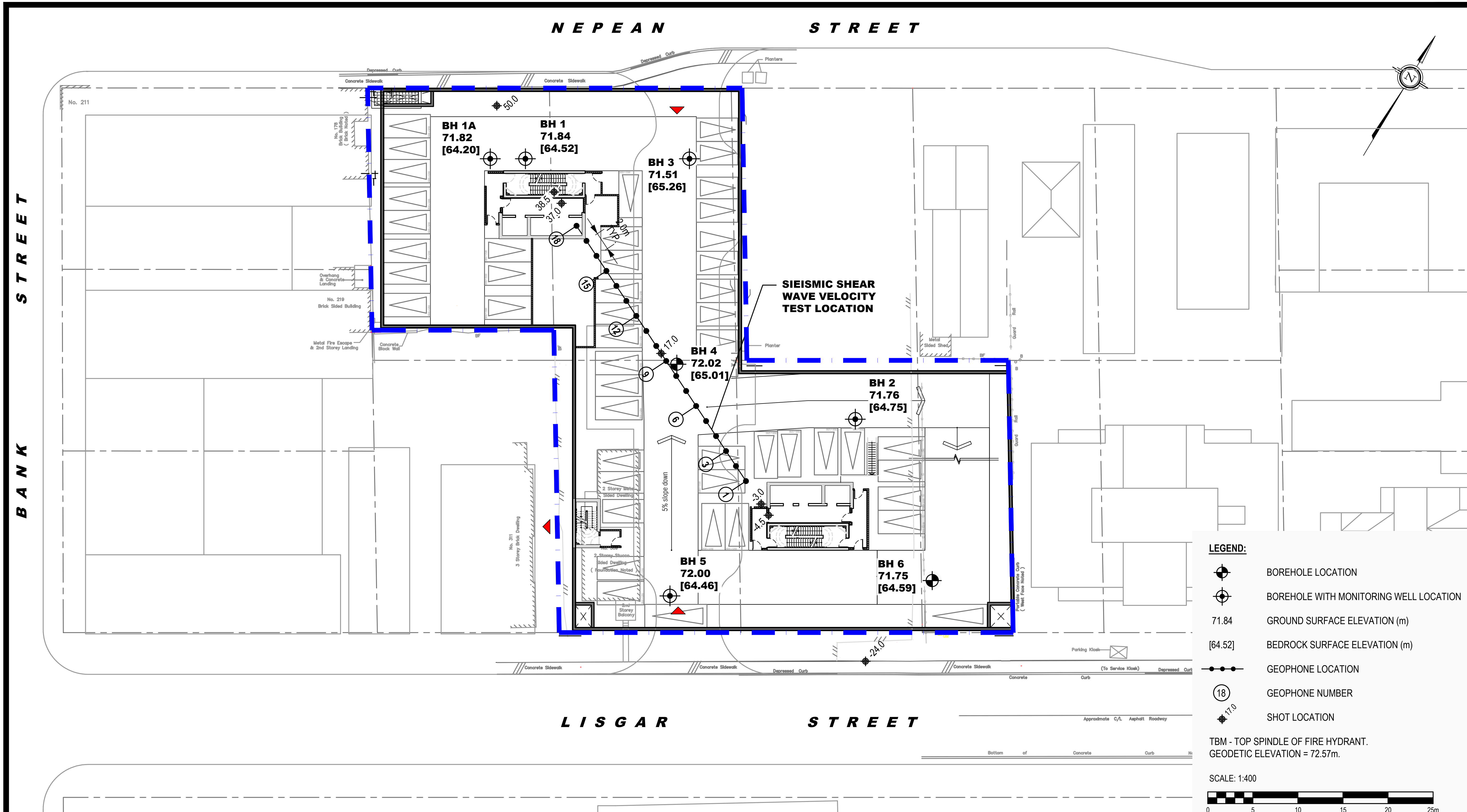


FIGURE 3

SHEAR WAVE VELOCITY PROFILE AT SHOT LOCATION 4.5 M



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NO.	REVISIONS	DATE	INITIAL
3	UPDATED TO LATEST BASE PLAN	14/09/2020	MS
2	SEISMIC SURVEY INFORMATION ADDED	14/05/2018	SD
1	UPDATED TO LATEST BASE PLAN	02/02/2018	DJG

RICHCRAFT (LISGAR) LIMITED
GEOTECHNICAL INVESTIGATION
PROP. MULTI-STOREY BUILDING - 176 NEPEAN ST. & 293-307 LISGAR ST.
OTTAWA, ONTARIO

Title:

TEST HOLE LOCATION PLAN

Scale: 1:400	Date: 09/2017
Drawn by: RCG	Report No.: PG4238-1
Checked by: NC	Dwg. No.: PG4238-1
Approved by: DJG	Revision No.: 3

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Appendix E DRAWINGS