

REPORT

SITE SERVICING REPORT & EROSION & CONTROL PLAN 78-90 BEECHWOOD/69-93 BARRETTE

Project: 125192-7.03.04



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1 INTRODUCTION

1.1 Scope

The purpose of this report is to outline the required municipal services, including water supply, stormwater management and wastewater disposal, needed to support the redevelopment of the subject property. The property is approximately 0.42 hectares in area and is located at the following current municipal addresses, 78-90 Beechwood Avenue and 69-93 Barrette Street. The site is bound by Beechwood Avenue to the north Barrette Street to the south. Please refer to **Figure 1 – Location** plan for more details.

This Site Servicing Study, which also includes the Stormwater Management Plan, Watermain Analysis and Erosion and Sedimentation Control Plans, is being completed in support of the current Re-zoning Application and the future Site Plan Application.

1.2 Subject Site

Minto Communities proposes to construct a mixed use building with 229 residential units along with 6,000 square feet (564 square metres) of ground floor retail space fronting along Beechwood Avenue. The proposed development also includes 2 levels of underground parking. Vehicular access to the site will be from both Beechwood Avenue and Barrette Street. Please refer to **Figure 2 – Site Plan** for more information.

The site currently consists of vacant lots along with some existing low rise residential and commercial structures. All existing structures within the subject property will be demolished to facilitate the proposed development.

1.3 Pre-consultation

It should be noted that a pre-consultation with the Ministry of the Environment is not required since this site is serviced by existing separated municipal sanitary and storm sewers and is a single owner residential site, thus an ECA is not required.

2 WATER DISTRIBUTION

2.1 Existing Conditions

As previously noted, the site is located south of Beechwood Ave, and north of Barrette Street. An existing 200 mm diameter watermain is located within the Beechwood Ave right of way and an existing 300 mm watermain is located within the Barrette Street right of way. The watermains fall within the City of Ottawa's pressure zone 1E which will provide the water supply to the site.

2.2 Design Criteria

2.2.1 Water Demands

The population for apartment buildings is assumed at 1.8 persons per unit as found in Table 4.1 of the Design Guidelines. A watermain demand calculation sheet is included in **Appendix A** and the total water demands are summarized as follows:

	<u>Subject Site</u>
Average Day	1.36 l/s
Maximum Day	3.38 l/s
Peak Hour	7.42 l/s

2.2.2 System Pressure

The Ottawa Design Guidelines – Water Distribution (WDG001), July 2010, City of Ottawa, Clause 4.2.2 states that the preferred practice for design of a new distribution system is to have normal operating pressures range between 345 kPa (50 psi) and 480 kPa (80 psi) under maximum daily flow conditions. Other pressure criteria identified in Clause 4.2.2 of the guidelines are as follows:

Minimum Pressure	Minimum system pressure un	der peak hour dema	nd conditions shall not
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be less than 276 kPa (40 psi)

Fire Flow During the period of maximum day demand, the system pressure shall

not be less than 140 kPa (20 psi) during a fire flow event.

Maximum Pressure In accordance with the Ontario Building/Plumbing Code, the maximum

pressure should not exceed 552 kPa (80 psi). Pressure reduction controls will be required for buildings where it is not possible/feasible to

maintain the system pressure below 552 kPa.

2.2.3 Fire Flow Rates

A calculation using the Fire Underwriting Survey (FUS) method was conducted to determine the fire flow requirement for the site. The building is considered non-combustible construction. Results of the analysis provides a maximum fire flow rate of 8,000 l/min or 133 l/s is required which is used in the hydraulic analysis. A copy of the FUS calculation is included in **Appendix A**.

2.2.4 Boundary Conditions

A boundary condition was provided by the City of Ottawa for the 305 mm diameter watermain on Barrette Street adjacent to the development. A copy of the boundary conditions is included in **Appendix A** and summarized as follows:

BOUNDAR	Y CONDITIONS
SCENARIO	HGL (m)
SCLIVARIO	Barrette (proposed connection)
Maximum HGL	118.3m
Minimum HGL (Peak Hour)	107.0m
Max Day + Fire Flow	89.0m

2.3 Proposed Water Plan

The minimum water pressure inside the building at the connection is determined by the difference between the water entry elevation of 55.95m and the minimum HGL condition, resulting in a pressure 500.8 kPa which exceeds the minimum requirement of 276 kPa per the guidelines. Because the pressure at the 9th floor under minimum HGL conditions is less than the minimum requirement of 276 kPa, a domestic water pump will be necessary for this building.

Maximum water pressure is determined by the difference between the water entry elevation of 55.95m and the maximum HGL condition resulting in a pressure of 66.6 kPa, which is greater than the 552 kPa threshold in the guideline in which pressure control is required. Based on this result, pressure control is required for this building.

The boundary condition for Maximum Day and Fire Flow results in a pressure of 324.2 kPa at the ground floor level. In the guidelines, a minimum residual pressure of 140 kPa must be maintained in the distribution system for a fire flow and maximum day event. As a pressure of 324.21 kPa is achieved, the fire flow requirement is exceeded.

To service the property twin 200mm dia water services off Barrette are proposed, see site servicing plan 125192-C-001 in **Appendix D.** The proposed 200mm dia service will provide adequate supply to the building to meet demands while twining the service will provide service redundancy for this building.

3 WASTEWATER

3.1 Existing Conditions

The site is bound by 300mm concrete sanitary sewers located in both the Beechwood and Barrette ROWs. Given the proximity and elevation of the existing sewers, the sewer within the Barrette ROW has been chosen as the outlet for the subject development.

3.2 Design Criteria

The sanitary sewers for the subject site will be based on the City of Ottawa design criteria. It should be noted that the sanitary sewer design for this study incorporates the latest City of Ottawa design parameters identified in Technical Bulletin ISTB-2018-01. Some of the key criteria will include the following:

Commercial/Institutional flow 28,000 l/ha/d
 Residential flow 280 l/c/d

Peaking factor
 1.5 if ICI in contributing area >20%
 1.0 if ICI in contributing area <20%

Infiltration allowance 0.33 l/s/ha

Velocities
 0.60 m/s min. to 3.0 m/s max.

•

Given the above criteria, total wastewater flow from the proposed development will 4.72 l/s, the detailed sanitary sewer calculations are included in **Appendix B**.

3.3 Recommended Wastewater Plan

A 200mm dia sanitary service lateral is proposed to connect to the existing sanitary sewer in Barrette to service this site. Please refer to the site servicing plan 125192-C-001 in **Appendix D** for connection location details.

4 STORMWATER SYSTEM

4.1 Existing Conditions

Currently adjacent to the site is a 375mm dia storm sewer draining westward within the Barrette ROW and a 450mm dia storm sewer draining westward in the Beechwood ROW. The proposed storm sewer connection will be in keeping with the other services and connect to the Barrette Street sewer.

4.2 Design Criteria

Criteria for the stormwater management of existing infill sites discharging to separated sewers within the City of Ottawa are as follows;

- Existing adjacent storm sewers were designed to a 2 year level of service
- Site to be designed to limit the 100 year post development flow to a maximum of the 2 year pre development flow
- Pre development flow to use a maximum C of 0.5 and a minimum TC of 10 min.

The stormwater system was designed following the principles of dual drainage, making accommodations for both major and minor flow.

Some of the key criteria include the following:

•	Design Storm	1:2 year return (Ottawa)
•	Rational Method Sewer Sizing	
•	Initial Time of Concentration	10 minutes
•	Runoff Coefficients	
	- Landscaped Areas	C = 0.30
	- Asphalt/Concrete	C = 0.90
	- Roof	C = 0.90
•	Pipe Velocities	0.80 m/s to 6.0 m/s
•	Minimum Pipe Size	250 mm diameter (200 mm CB Leads)

4.3 Proposed Minor System

The detailed design for this site shows a storm sewer connection along with some uncontrolled surface drainage entering into the 375mm sewer within Barrette Street Road ROW. A limited amount of uncontrolled surface flow will also enter the 450mm storm sewer within the Beechwood Avenue ROW.

Using the above-noted criteria, the proposed on-site storm sewers were sized accordingly. A detailed storm sewer design sheet and the associated storm sewer drainage area plan are included in **Appendix C**. The current servicing drawing shows 5 surface catchbasin locations. As these are located above the underground parking structure all flows will be routed inside the building via the mechanical plumbing systems and directed to the building cistern.

4.4 Stormwater Management

The subject site will be limited to a release rate established using the criteria described in section 4.2. This will be achieved through an inlet control device (ICD) at the outlet of the cistern.

Flows generated that are in excess of the site's allowable release rate will be stored within the cistern located at the buildings SW corner. The cistern has been sized at 130 cubic metres.

At certain locations within the site, the opportunity to store runoff is limited due to grading constraints and building geometry. These locations are generally located at the perimeter of the site where it is necessary to tie into public boulevards and adjacent properties, and it is not always feasible to capture or store stormwater runoff. These "uncontrolled" areas, 0.05 hectares in total, have a weighted average C value of 0.9. Based on 1:100 year storm uncontrolled flows, the uncontrolled areas generate 22.3 l/s runoff (refer to Section 4.5 for calculation). The cistern has been sized to control water generated during the 1:100-year event, with no overflow leaving the site. Please refer to the SWM calculations in **Appendix C**.

4.5 Inlet Controls

The allowable release rate for the 0.42 Ha site can be calculated as follows:

```
Qallowable = 2.78 \times C \times i_{2yr} \times A where:

C = 0.5 (pre-development C*)

= Intensity of 2-year storm event (mm/hr)

= 732.951 \times (T_c + 6.199)^{0.81} = 76.81 mm/hr; where T_c = 10 minutes*

A = 44.84 \text{ L/s}
```

As noted in Section 4.4, a portion of the site will be left to discharge to the surrounding boulevards and roadways at an uncontrolled rate.

Based on a 1:100 year event, the flow from the 0.05 Ha uncontrolled area can be determined as:

```
\begin{array}{ll} \textbf{Q}_{uncontrolled} &= \textbf{2.78} \times \textbf{C} \times \textbf{i}_{100yr} \times \textbf{A} \quad \text{where:} \\ \textbf{C} &= \text{Average runoff coefficient of uncontrolled area} = 0.9 \\ \textbf{i}_{100yr} &= \text{Intensity of 100-year storm event (mm/hr)} \\ &= 1735.688 \times (T_c + 6.014)^{0.820} = 178.56 \text{ mm/hr; where } T_c = 10 \text{ minutes} \\ \textbf{A} &= \text{Uncontrolled Area} = 0.05 \text{ Ha} \end{array}
```

Therefore, the uncontrolled release rate can be determined as:

```
Quncontrolled = 2.78 \times C \times i_{100yr} \times A
= 2.78 \times 0.9 \times 178.56 \times 0.05
= 22.34L/s
```

^{*}based on pre development calculations, see Appendix C

The maximum allowable release rate from the remainder of the site can then be determined as:

Qmax allowable = Qrestricted - Quncontrolled = 44.84 L/s - 22.34 L/s= 22.50 L/s

4.6 On-Site Detention

As noted in section 4.4 any excess storm water up to the 100-year event is to be stored on-site within the building cistern in order to not surcharge the downstream municipal storm sewer system. As the cistern is located inside the building, coordination with the architect, structural and mechanical engineers will be needed to design the structure and associated inlet control device.

4.6.1 Site Inlet Control

The following Table summarizes the on-site storage requirements during both the 1:5-year and 1:100-year events.

ICD	TRIBUTARY	AVAILABLE	100-YEAF	RSTORM	5-YEAR S	STORM
AREA	AREA	STORAGE (M³)	RESTRICTE D FLOW (L/S)	REQUIRED STORAGE (M³)	RESTRICTED FLOW (L/S)	REQUIRED STORAGE (M³)
Cistern	0.37	130.00	22.50	129.67	22.50	51.13
Unrestricted	0.05					
TOTAL	0.42	130.00	22.50	129.67	22.50	51.13

In all instances the required storage is met with the building cistern.

4.6.2 Overall Release Rate

As demonstrated above, the site uses an inlet control device to restrict the 100 year storm event to the criteria approved by the City of Ottawa. Restricted stormwater will be contained onsite by the building cistern. In the 100 year event, there will be no overflow off-site from restricted areas.

The sum of restrictions on the site is 22.50 l/s, which is equal to the allowable release of 22.50 l/s noted in section 4.5.

5 SEDIMENT AND EROSION CONTROL PLAN

During construction, existing stream and storm water conveyance systems can be exposed to significant sediment loadings. A number of construction techniques designed to reduce unnecessary construction sediment loadings may be used such as;

- Filter socks will remain on open surface structures such as manholes and catchbasins until these structures are commissioned and put into use;
- Installation of silt fence, where applicable, around the perimeter of the proposed work area.

During construction of the services, any trench dewatering using pumps will be fitted with a "filter sock." Thus, any pumped groundwater will be filtered prior to release to the existing surface runoff. The contractor will inspect and maintain the filter sock as needed including sediment removal and disposal.

All catchbasins, and to a lesser degree manholes, convey surface water to sewers. Consequently, until the surrounding surface has been completed these structures will be protected with a sediment capture filter sock to prevent sediment from entering the minor storm sewer system. These will stay in place and be maintained during construction and build-out until it is appropriate to remove them.

The Sediment and Erosion Control Plan 125192-C-010 is included in Appendix D.

6 CONCLUSIONS

Municipal water, wastewater and stormwater systems required to accommodate the proposed development are available to service the proposed development. Prior to construction, existing sewers are to be CCTV inspected to assess sewer condition.

This report has demonstrated sanitary and storm flows from and water supply to the subject site can be accommodated by the existing infrastructure. Also, the proposed servicing has been designed in accordance with MECP and City of Ottawa current level of service requirements.

The use of lot level controls, conveyance controls and end of pipe controls outlined in the report will result in effective treatment of surface stormwater runoff from the site. Adherence to the sediment and erosion control plan during construction will minimize harmful impacts on surface water.

Based on the information provided herein, the development can be serviced to meet City of Ottawa requirements.

Report prepared by:

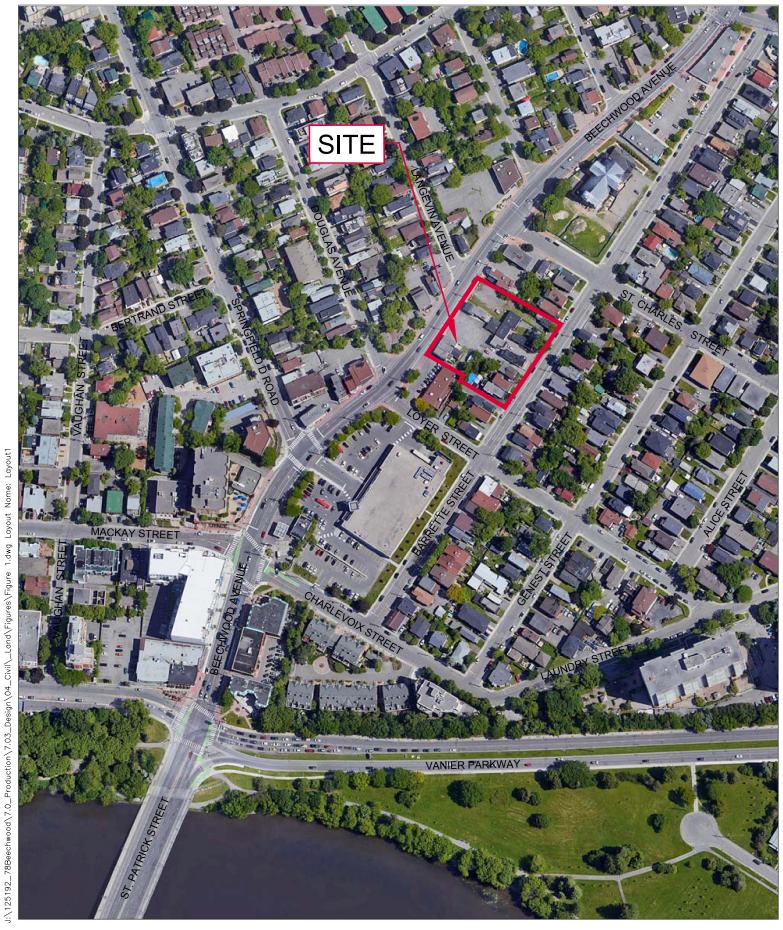
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D. G. Yannoulopoulos Property of the Control of the Control

Demetrius Yannculopoulos, P. Eng. Director, Ottawa Office Lead

James Battison C.E.T

[&]quot;J:\125192_78Beechwood\7.0_Production\7.03_Design\04_Civil_Report\3rd Submission\CTR-site-srvcng-erosion-2021-05-07.docx"



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Project Title Drawing Title Sheet No.

IBI

Scale

N.T.S.

Project Title

Drawing Title

Sheet No.

APPENDIX A

WATERMAIN DEMAND CALCULATION SHEET

IBI GROUP

333 PRESTON STREET

OTTAWA, ON

K1S 5N4

PROJECT: 78 Beechwood Ave.

LOCATION: City of Ottawa

DEVELOPER: Minto Communities - Canada

FILE: 125192-6.4.4
DATE PRINTED: 2020-12-18

DESIGN: 2020-05-13

PAGE: 1 OF 1

		RESIDE	ENTIAL		NON	N-RESIDEN	TIAL	A۱	/ERAGE D	AILY	MA	XIMUM DA	\ILY	MAX	IMUM HOL	FIRE	
NODE					INDTRL	COMM.	RETAIL		DEMAND	(I/s)	D	EMAND (I	/s)	DI	EMAND (I	/s)	DEMAND
11052	Single	Town	Apt	POP'N	(ha.)	(ha.)	(m²)	Res.	Non-res.	Total	Res.	Non-res.	Total	Res.	Non-res.	Total	(l/min)
BUILDING			229	412			564	1.34	0.02	1.36	3.34	0.04	3.38	7.35	0.07	7.42	8,000

ASSUMPTIONS

RESIDENTIAL DENSITIES

Apartment (ave) 1.8 p/p/u

** Residential Daily Demand reduced to coincide with current waste water guidelines

AVG. DAILY DEMAND

Residential:** 280 I / cap / day
Industrial: I / ha / day
Commercial: I / ha / day

Retail: 2,500 I / 1000m² / day

MAX. DAILY DEMAND

Residential: 700 I / cap / day Industrial: I / ha / day

Commercial: I / ha / day

Retail: 6,250 I / 1000m² / day

MAX. HOURLY DEMAND

Residential: 1,540 I / cap / day
Industrial: I / ha / day
Commercial: I / ha / day

Retail: 11,250 I / 1000m² / day

FIRE FLOW

From FUS Calculation 28,000 I / min

Fire Flow Requirement from Fire Underwriters Survey - 78 Beechwood Avenue

78 Beechwood

509	Floor Area (3 & 4) % Floor Area (5 to 10) Total Floor Area	5,013 m ² 4,480 9,493 m ²	
F = 220C√A			
C A	0.6 9,493 m ²	C =	1.5 wood frame 1.0 ordinary 0.8 non-combustible
F use	12,861 l/min 13,000 l/min		0.6 fire-resistive

Occupancy Adjustment

Use -15%

Adjustment -1950 l/min Fire flow 11,050 l/min

Sprinkler Adjustment

Use -30%

Adjustment -3315 l/min -25% non-combustible

-15% limited combustible 0% combustible

+15% free burning +25% rapid burning

-30% system conforming to NFPA 13 -50% complete automatic system

Exposure Adjustment

Building	Separation	Adja	cent Expos	ed Wall	Exposure
Face	(m)	Length	Stories	L*H Factor	Charge *
north	21.0	32.3	2	65	8%
east	3.1	46.6	2	93	19%
south	20.8	24.9	2	50	7%
west	7.9	28.8	2	58	16%

Total

Adjustment I/min

Total adjustments (3,315) I/min Fire flow 7,735 l/min Use 8,000 l/min 133 l/s

Floor	Area (m²)	Two Largerst Floor	Floors Above at 50%
1	2218		
2	2447		
3	2519	2519	
4	2494	2494	
5	2494		1247
6	2214		1107
7	1428		714
8	1171		585.5
9	1271		635.5
10	382		191
Total	18638	-	9493

 $(\underline{\textbf{Note}}:$ For fire-resistive buildings, consider two largest adjoining floors plus 50% of each of any floors immediately above them up to eight.)

 $0\% \,\, (\underline{\text{Note}} : \text{According to Page G-104 in Tech bulletin ISTB-2018-02} \,\, \text{Revisions to}$ Ottawa Design Guidelines - Water Distribution, "If the exposing wall of the building being considered is taller than the exposed wall of the adjacent structure, no exposure charge applies".)

Water Boundary Condition Request - 78 Beechwood Ave.

Wessel, Shawn <shawn.wessel@ottawa.ca>

Tue 5/19/2020 9:45 AM

To: Amy Zhuang <Amy.Zhuang@ibigroup.com>

Cc: O'Connor, Ann < Ann.O'Connor@ottawa.ca>; James Battison < James.Battison@ibigroup.com>; Demetrius Yannoulopoulos <dyannoulopoulos@IBIGroup.com>



1 attachments (80 KB)

78 Beechwood May 2020.pdf;

Good morning everyone.

Please find requested conditions.

Please refer to Guidelines and Technical bulletin ISDTB-2014-02 concerning basic day demands greater than 0.5 L/s.

The following are boundary conditions, HGL, for hydraulic analysis at 78 Beechwood (zone 1E) assumed to be connected to the 305mm on Barrette (see attached PDF for location).

Minimum HGL = 107.0m

Maximum HGL = 118.3m. The maximum pressure is estimated to be more than 80 psi. A pressure check at completion of construction is recommended to determine if pressure control is required.

MaxDay + FireFlow (467 L/s) = 89.0m

These are for current conditions and are based on computer model simulation.

Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation.

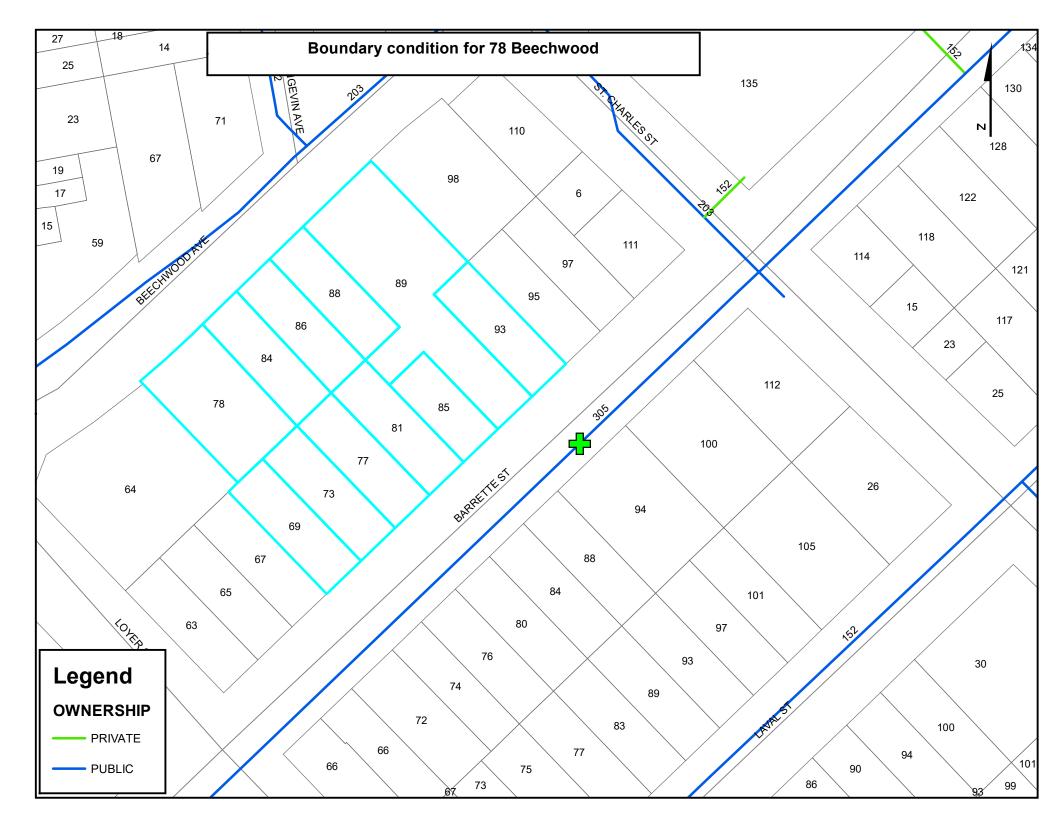
If you require additional information or clarification, please do not hesitate to contact me anytime.

Thank you

Regards,

Shawn Wessel, A.Sc.T.,rcji **Project Manager - Infrastructure Approvals** Gestionnaire de projet – Approbation des demandes d'infrastructures

Development Review Central Branch | Direction de l'examen des projets d'aménagement, Centrale







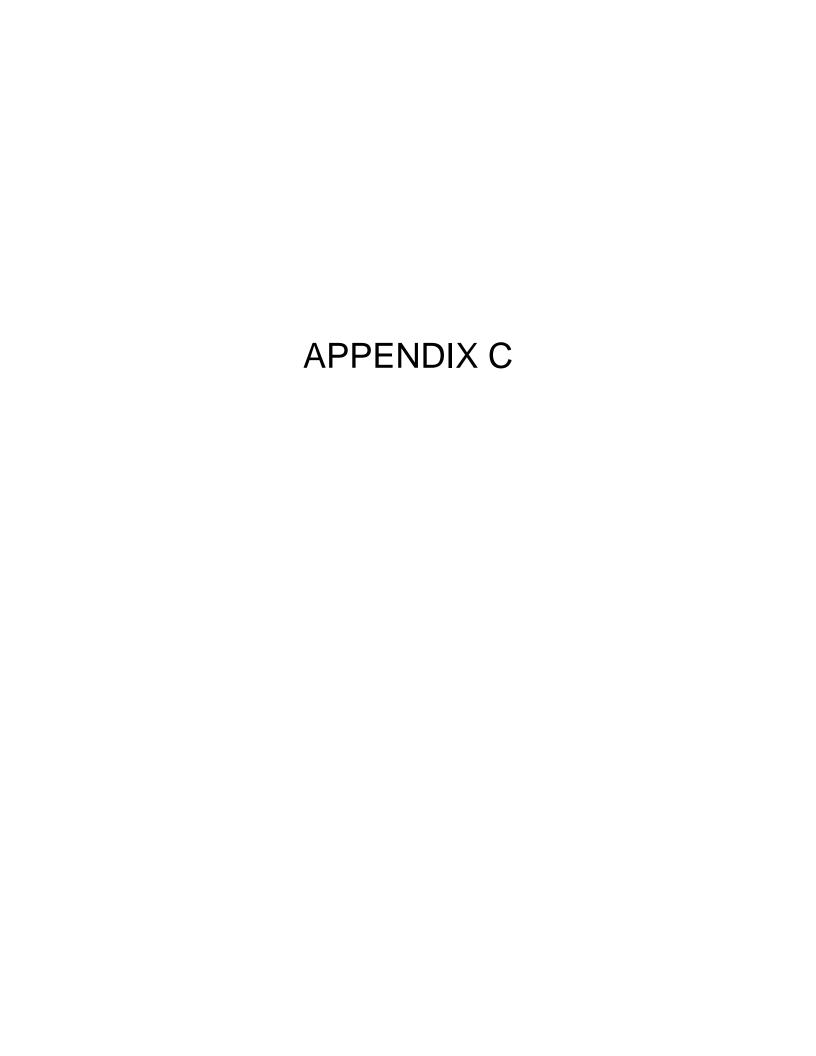


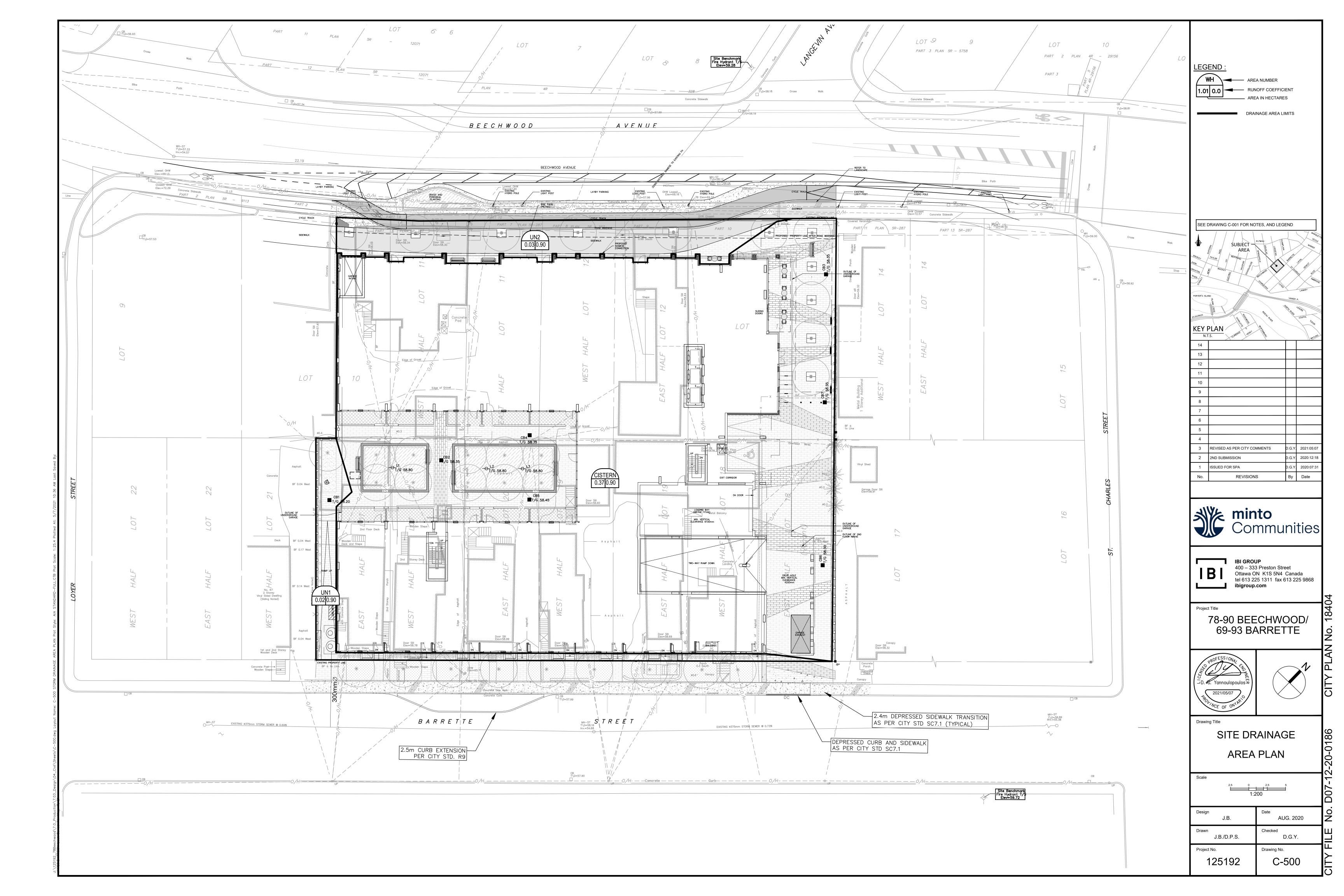
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tel 613 225 1311 fax 613 225 9868

ibigroup.com

78 Beechwood Ave CITY OF OTTAWA Minto Communities Inc.

	LOCATI	ON						RESIDEN	ITIAL								ICI A	REAS			INFILTR	ATION ALL	OWANCE	FIVED	FLOW (L/s)	TOTAL			PROPO	SED SEWER	R DESIGN		
	LOCATI	ION		AREA		UNIT	TYPES		AREA	POPUL	ATION	RES	PEAK			AREA			ICI	PEAK	ARE/	A (Ha)	FLOW	T FIXED	FLOW (L/S)	FLOW	CAPACITY	LENGTH	DIA	SLOPE	VELOCITY	AVAI	LABLE
STREET	AREA II	D FROM MH	TO MH	w/ Units (Ha)	SF	SD	ТН	APT	w/o Units (Ha)	IND	CUM	PEAK FACTOR	FLOW (L/s)	INSTITU IND	TIONAL	COMME	RCIAL CUM	INDUST IND	PEAK FACTOR	FLOW (L/s)	IND	CUM	(L/s)	IND	CUM	(L/s)	(L/s)	(m)	(mm)	(%)	(full) (m/s)	CAP L/s	ACITY (%)
8 Beechwood Ave.		Building	MH1A	0.42				229		412.2	412.2	3.41	4.56			0.06	0.06				0.48	0.48	0.16	1		4.72	48.39	1.07	200	2.00	1.492	43.67	90.25%
'8 Beechwood Ave.		MH1A	Main	0.42				225		0.0	412.2	3.41	4.56			0.00	0.06				0.00	0.48	0.16			4.72	48.39	10.59	200	2.00	1.492	43.67	90.25%
														1										1									
Design Parameters:				Notes:								Designed:		JEB			No.					I	Revision								Date		
				1. Manning	s coefficient	(n) =	0.0	013									1.					Issued for R	e-Zoning Appl	lication							2020-07-31		
Residential		ICI Areas		2. Demand	I (per capita):	:	280 L/d	day	200	L/day							2.					2nd C	ty Submissior	n							2020-12-18		
SF 3.4 p/p/u				Infiltration	n allowance:		0.33 L/s	s/Ha				Checked:		DY																			
TH/SD 2.7 p/p/u	INST 2	28,000 L/Ha/day		4. Residen	tial Peaking I	Factor:																											
APT 1.8 p/p/u	COM	28,000 L/Ha/day			Harmon F	formula = 1+(14/(4+(P/1000)/	^0.5))0.8																									
Other 60 p/p/Ha	IND :	35,000 L/Ha/day	MOE Cha	rt	where K =	0.8 Correction	on Factor					Dwg. Refere	ence:	125192-C-0	01																		
		17000 L/Ha/day		5. Commer	cial and Instit	tutional Peak	Factors based	on total ar	ea,								F	ile Reference						Date:							Sheet No:		
		•			reater than 2				-							- 1		125192.7.03						2020-07-3							1 of 1		







IBI

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Ottawa, Ontario K1S 5N4 Canada
tel 613 225 1311 fax 613 225 9868
ibigroup.com

78 Beechwood Ave City of Ottawa Minto Communitis Inc.

	LOCATION							AREA	(Ha)										F	RATIONAL D	ESIGN FLO	OW										SEWER DA	ΓΑ			'
OTDEET	ADEAID	ED OM	то.	C=	C=	C=	C=	C=	C=	C=	C= C=	C=	IND	CUM	INLET	TIME	TOTAL	i (2)	i (5)	i (10)	i (100)	2yr PEAK	5yr PEAK	10yr PEAK	K 100yr PEA	FIXED	DESIGN	CAPACITY	LENGTH		PIPE SIZE (n	nm)	SLOPE	VELOCITY	AVAIL (CAP (2yr
STREET	AREA ID	FROM	ТО	0.20	0.25	0.30	0.50	0.57		0.69	0.70 0.7	6 0.90	2.78AC	2.78AC	(min)	IN PIPE	(min)	(mm/hr)	(mm/hr)	(mm/hr)	(mm/hr)	FLOW (L/s	FLOW (L/s)	FLOW (L/s	s) FLÓW (L/s	FLOW (L/s	FLOW (L/s)	(L/s)	(m)	DIA	W	Н	(%)	(m/s)	(L/s)	(%)
												+	1																							+
Beechwood		Cistern	Main									0.37	0.93	0.93	10.00	0.09	10.09	76.81	104.19	122.14	178.56	71.10	96.46	113.07	165.30		71.10	142.67	10.75	300			2.00	1.955	71.57	50.16
												-	1																							+
efinitions:	•	•	•	Notes:	•	•	•	•	•	•	•	•	-	•	Designe	d:	JEB	•	•	•	No.						Revision			•	•		•	Date		
) = 2.78CiA, where:) = Peak Flow in Litre:	s per Second (L/s)			1. Manr	nings coe	efficient	t (n) =	0.013													1.				lssı	ued for Re-Z	oning Applicati	on						2020-07-31		
= Area in Hectares (Checked	l:	DY																			
= Rainfall intensity in [i = 732.951 / (TC+6		r (mm/hr) 2 YEAR																																		
[i = 998.071 / (TC+6	5.053)^0.814]	5 YEAR													Dwg. Re	ference:	125192-50	00																		
[i = 1174.184 / (TC+	-6.014)^0.816]	10 YEAR																				File R	eference:					Date:						Sheet No:		
[i = 1735.688 / (TC+	-6.014)^0.820]	100 YEAR																				125°	192.7.03					2020-07-31						1 of 1		

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PROJECT: 78 Beechwood Ave. **DATE:** 2020-07-31 **FILE:** 125192.7.03 **REV** #: 1

DESIGNED BY: JB CHECKED BY: DY

STORMWATER MANAGEMENT

Formulas and Descriptions

 i_{2yr} = 1:2 year Intensity = 732.951 / $(T_c+6.199)^{0.810}$ $i_{5yr} = 1.5$ year Intensity = 998.071 / $(T_c + 6.053)^{0.814}$ $i_{100yr} = 1:100 \text{ year Intensity} = 1735.688 / (T_c+6.014)^{0.820}$ T_c = Time of Concentration (min) C = Average Runoff Coefficient A = Area (Ha) Q = Flow = 2.78CiA (L/s)

Maximum Allowable Release Rate

Flow Allocation

C =0.5 (Pre-Development) $T_c =$ 10 min 76.81 mm/hr $i_{2yr} =$ 0.42 Ha $A_{TOTAL} =$ $Q_{TOTAL} =$ 44.84 L/s

Uncontrolled Release (Q_{uncontrolled} = 2.78*C*i_{100yr}*A_{uncontrolled})

C = 0.9 $T_c =$ 10 min 178.56 mm/hr $i_{100yr} =$ 0.050 Ha A uncontrolled = 22.34 L/s Q uncontrolled =

Maximum Allowable Release Rate ($Q_{max allowable} = Q_{restricted} - Q_{uncontrolled}$)

Q _{max allowable} = 22.50 L/s

MODIFIED RATIONAL METHOD (100-Year & 5-YearPonding)

Drainage Area	Cister	rn				
Area (Ha)	0.37	70			_	
C =	0.0	99 Restricted Flow Q _r (L	Restricted Flow Q_r (L/s)=			
		100-Year Pondir	ng			
T _c Variable	i _{100yr}	Peak Flow Q _p =2.78xCi _{100yr} A	Q_r	Q_p - Q_r	Volume 100yr	
(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m³)	
36	80.96	82.45	22.50	59.95	129.48	
38	77.93	79.36	22.50	56.86	129.64	
39	76.51	77.91	22.50	55.41	129.67	
40	75.15	76.52	22.50	54.02	129.65	
42	72 57	73 90	22 50	51 40	129 52	

Drainage Area	Cistern							
Area (Ha)	0.370				_			
C =	0.90	Restricted Flow Q _r (L/s						
5-Year Ponding								
T _c Variable	i _{5yr}	Peak Flow Q _p =2.78xCi _{5yr} A	Q _r	Q_p - Q_r	Volume 5yr			
(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m³)			
19	72.53	67.14	22.50	44.64	50.89			
21	68.13	63.07	22.50	40.57	51.12			
22	66.15	61.23	22.50	38.73	51.13			
23	64.29	59.51	22.50	37.01	51.08			
25	60.90	56.37	22.50	33.87	50.81			

Storage (m ³)				Sto	orage (m³)				
Overflow	Required	Surface	Cistern	Balance	Overflow	Required	Surface	Cistern	Balance
0.00	129.67	0.00	130.00	0.00	0.00	51.13	0.00	130.00	0.00

