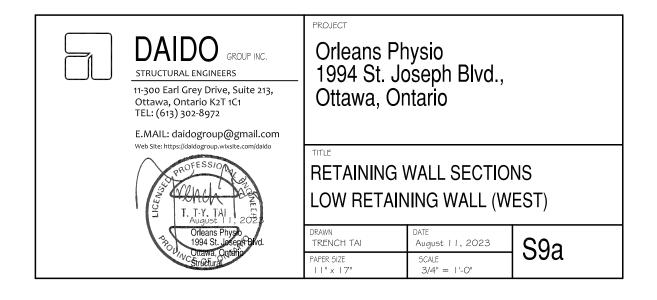


SECTION THRU. LOW RETAINING WALL AREA

(WEST)

Notes:

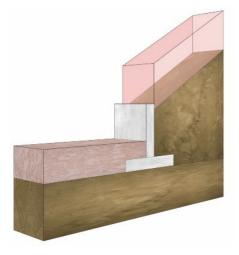
- $\overline{\hspace{1cm}}$ Bearing capacity assumed to be 100 kPa (SLS) for clay material, to be confirmed by soil engineer
- \sim Concrete to be 25 mPa at 28 days, with 5% air (+/-1%)
- ~ Rebar 400 mPa
- ~ Provide Rigid insulation to protect the frost penetration since one side of the retaining wall is above the frost cover, details to be specified by soil engineer
- ~ Lap 42 x bar diameter, which is 25" for 15m bar
- ~ concrete cover 3" typical



Retaining Wall Calculations - Detailed Report

REFERENCES CALCULATIONS RESULTS

INPUTS:



Stem:

Layer	Height	Base width	Top width	Front offset	Back offset
1	1.156	0.254	0.254	0.000	0.000

Stem total height: $H_{stem}\,=\,1.155701~\mathrm{m}$

Footing:

Base thickness: $H_{base} = 0.25399 \; \mathrm{m}$ Toe width: $W_{toe}\,=0.6096\;\mathrm{m}$ Heel width: $W_{heel} = 0.6604~\mathrm{m}$

Soil:

Substructure:

	Layer	Height	Unit weight	Friction angle	Cohesion	Allowable pressure	Soil-concrete friction	Name
		m	${ m kN/m^3}$	o	kPa	kPa		
ŀ	1	1.000	19.000	20.000	40.000	100.000	0.550	Loam

Total sub soil height: $H_{soil,\ sub}\,=1\ \mathrm{m}$

Active:

I	Layer	Height	Unit weight	Friction angle	Cohesion	Inclination	Name
		m	$\mathrm{kN/m^3}$	o	kPa	٥	
	1	1.791	18.000	30.000	-	30.000	Medium Clay

Total active soil height: $H_{soil,\;active}\,=1.790979\;\mathrm{m}$

Passive:

Layer	Height	Unit weight	Friction angle	Cohesion	Name
	m	$\rm kN/m^3$	o	kPa	
1	0.610	18.000	25.000	-	Sand

Total passive soil height: $H_{soil,\;passive}\,=\,0.6096\;\mathrm{m}$

Loads:

Active:

Load Id	Туре	Magnitude	Length	Start pos.	
		kN	m	m	
1	Uniform	1.680	0.763	0.000	



Notes:

1. All the calculated forces, pressures, distributed loads and design results are for a unitary (1 m) strip of the wall.

SOIL PROPERTIES:

Active soil:

Principles of Foundation Engineering, Braja Das, 7th Ed. - Eqn. 7.19

Rankine active earth pressure coefficient Simplified for the case of Inclined Granular Backfill with Vertical Back Face $K_{a,1}$

$$K_{a,1} = \cos(lpha_{soil\ active}) \cdot rac{\cos(lpha_{soil\ active}) - \sqrt{\cos^2(lpha_{soil\ active}) - \cos^2(\phi_{soil\ active},1)}}{\cos(lpha_{soil\ active}) + \sqrt{\cos^2(lpha_{soil\ active}) - \cos^2(\phi_{soil\ active},1)}}$$

$$K_{a,1} = \cos(30\ ^\circ) \cdot rac{\cos(30\ ^\circ) - \sqrt{\cos^2(30\ ^\circ) - \cos^2(30\ ^\circ)}}{\cos(30\ ^\circ) + \sqrt{\cos^2(30\ ^\circ) - \cos^2(30\ ^\circ)})} = 0.86603$$

Equivalent Rankine active earth pressure coefficient Equivalent Rankine earth pressure coefficient for all the layers K_{a*}

$$K_{a*} = rac{\sum K_{a,i} \cdot h_i}{H_{soil,\;active}}$$

$$K_{a*} = \frac{1.551 \text{ m}}{1.791 \text{ m}} = 0.86603$$

Passive soil:

Principles of Foundation Engineering, Braja Das, 7th Ed. - Eqn. 7.61

Rankine passive earth pressure coefficient $K_{p,1}$

$$K_{p,1} = an^2igg(45\,\,{}^{\circ} + rac{\phi_{
m soil\,\,passive,\,\,1}}{2}igg)$$

$$K_{p,1} = an^2igg(45\ ^\circ + rac{25\ ^\circ}{2}igg) = 2.4639$$

ACTING FORCES:

Vertical forces:

Self-weight of the structure:

Stem wall weight:
$$P = \gamma_{concrete, \; stem} \; \cdot V_{stem} \; = 23.58 \; \mathrm{kN/m^3 \cdot 0.29354 \; m^3} = 6.9217 \; \mathrm{kN}$$

Base weight:
$$P=\gamma_{concrete,\ footing} \ \cdot V_{base}=23.58\ \mathrm{kN/m^3} \cdot 0.38708\ \mathrm{m^3}=9.1274\ \mathrm{kN}$$

Self-weight of the soil:

$$P_{active,~1} = \gamma_{soil~active,~1} \cdot V_{soil~active,~1} = 18~\rm kN/m^3 \cdot 0.84717~m^3 = 15.249~\rm kN$$
 Total active soil weight: $P_{active} = 15.249011~\rm kN$

$$P_{passive,~1}=\gamma_{soil~passive,~1}\cdot V_{soil~passive,~1}=18~{\rm kN/m^3\cdot 0.21678~m^3}=3.902~{\rm kN}$$
 Total passive soil weight: $P_{passive}=3.902039~{\rm kN}$

Vertical component of the pressure from retained soil:

$$\begin{split} P_1 &= P_{0,\ 1\ (vert)} \cdot H_{soil\ active,\ 1} + \frac{1}{2} \cdot \gamma_{soil\ active,\ 1} \cdot H_{soil\ active,\ 1}^2 \cdot 1\ \text{m} \cdot K_{a,1} \cdot \sin(\alpha_{soil\ active}) \\ P_1 &= 0\ \text{kN/m}^1 \cdot 1.791\ \text{m} + \frac{1}{2} \cdot 18\ \text{kN/m}^3 \cdot 1.791\ \text{m}^2 \cdot 1\ \text{m} \cdot 0.86603 \cdot \sin(30\ ^\circ) = 12.5\ \text{kN} \end{split}$$

Total vertical active pressure:
$$P_{a.\ retained\ (vertical)}=12.500404\ \mathrm{kN}$$

Superimposed loads resultants:

Surcharge resultant (uniform): $P_1=q_{active,~1}\cdot L_{active,~1}=1.68~\mathrm{kN/m^1}\cdot 0.76258~\mathrm{m}=1.2811~\mathrm{kN}$

Vertical soil pressure due to superimposed loads:

Surcharge pressure (vertical):
$$P_{uniform, \ vertical, 1} = q_{active, \ 1} \cdot H_{soil, \ active} \cdot K_{a*} \cdot \sin(\alpha_{soil \ active})$$
 $P_{uniform, \ vertical, 1} = 1.68 \ kN/m^1 \cdot 1.791 \ m \cdot 0.86603 \cdot \sin(30\ ^\circ) = 1.3029 \ kN$

Total vertical force downwards:
$$\sum P_{vertical} = 50.284533 \; ext{kN}$$

Horizontal forces:

Rankine active force

Rankine Active horizontal resultant force per unit length, due to retained earth

$$P_{a, \ retained, \ horizontal, 1} = P_{0, \ 1} \cdot H_{soil \ active, \ 1} + \frac{1}{2} \cdot \gamma_{soil \ active, \ 1} \cdot H_{soil \ active, \ 1}^2 \cdot 1 \ \text{m} \cdot K_{a, 1} \cdot \cos(\alpha_{soil \ active})$$

$$P_{a, \ retained, \ horizontal, 1} = 0 \ \text{kN/m}^1 \cdot 1.791 \ \text{m} + \frac{1}{2} \cdot 18 \ \text{kN/m}^3 \cdot 1.791 \ \text{m}^2 \cdot 1 \ \text{m} \cdot 0.86603 \cdot \cos(30 \ ^\circ) = 21.651 \ \text{kN}$$

Total horizontal force (active soil): $P_{a, \ retained, \ horizontal} = 21.651335 \ \mathrm{kN}$

The Reinforced

Concrete Design Handbook, ACI SP-17(14), Vol. 2

Rankine active force

Rankine Active horizontal resultant force per unit length, due to superimposed loads

$$\begin{array}{ll} P_{a,\;uniform,\;horizontal,1} &= q_{active,\;1} \cdot H_{soil,\;active} \cdot K_{a*} \cdot \cos(\alpha_{soil\;active}\;) \\ P_{a,\;uniform,\;horizontal,1} &= 1.68\;\mathrm{kN/m^1} \cdot 1.791\;\mathrm{m} \cdot 0.86603 \cdot \cos(30\;°) = 2.2566\;\mathrm{kN} \end{array}$$

Total horizontal force leftwards: $\sum P_{horizontal\ leftwards}~=23.907968\ \mathrm{kN}$

Rankine passive force

Horizontal Rankine passive resultant force per unit length

$$\begin{split} P_{p,1} &= P_{0,\ 1} \cdot H_{soil\ passive,\ 1} + \frac{1}{2} \cdot \gamma_{soil\ passive,\ 1} \cdot H_{soil\ passive,\ 1}^2 \cdot 1\ \text{m} \cdot K_{p,1} \\ P_{p,1} &= 0\ \text{kN/m}^1 \cdot 0.6096\ \text{m} + \frac{1}{2} \cdot 18\ \text{kN/m}^3 \cdot 0.6096\ \text{m}^2 \cdot 1\ \text{m} \cdot 2.4639 = 8.2406\ \text{kN} \end{split}$$

Total horizontal force (passive soil): $P_p = 8.24058 \; \mathrm{kN}$

Total horizontal force rightwards: $\sum P_{horizontal\ rightwards}\ = 8.24058\ \mathrm{kN}$

STABILITY CHECKS:

Overturning:

Restoring moment

The self-weight of the retaining wall and the soil, the distributed load above the heel, the passive soil weight and its associated horizontal pressure, if considered, tend to counteract the overturning moment. Moments taken about the front edge of base (toe):

$$M = P \cdot d_{lever}$$

Moment	Force, ${\cal P}$	Lever, d	$\mathbf{Moment,}\ M$
	$/\mathrm{kN,}1^{\mathit{NaN}}$	m	$kN\cdot m$
Stem wall	6.922	0.737	5.099
Base	9.127	0.762	6.955
Active soil weight (layer 1)	15.249	1.216	18.537
Passive soil weight (layer 1)	3.902	0.305	1.189
Surcharge (load 1)	1.281	1.194	1.529
Vertical active soil pressure (all layers)	12.500	1.524	19.051
Vertical surcharge soil pressure (load 1)	1.303	1.524	1.986
Passive pressure (layer 1)	8.241	0.203	1.674

Total restoring moment: $\sum M_R = 56.019805 \; \mathrm{kN*m}$

Overturning moment

The horizontal components of the active soil lateral pressure tend to overturn the retaining wall about the front edge of the base (toe):

$$M = P \cdot d_{lever}$$

Moment	Force, ${\cal P}$	Lever, \boldsymbol{d}	$\qquad \qquad {\rm Moment,} \ M$	
	$/\mathrm{kN,}1^{\mathit{NaN}}$	m	$kN\cdot m$	
Active pressure (layer 1)	21.651	0.597	12.926	
Surcharge earth pressure	2.257	0.895	2.021	

Total overturning moment: $M_{OTM}\,=\,14.946486~\mathrm{kN*m}$

Stability requirement against overturning

Factor of safety FS

$$FS = rac{\sum M_R}{M_{OTM}}$$

$$FS = rac{56.02 \; ext{kNm}}{14.946 \; ext{kNm}} = 3.748 \geq 2$$

Bearing:

Soil Pressure Resultant Distance

To calculate soil pressure, the location of the vertical resultant force must be determined.

Soil pressure resultant distance \boldsymbol{a}

$$a = rac{\sum M_R - M_{OTM}}{\sum P_{vertical}}$$

$$a = \frac{56.02 \text{ kNm} - 14.946 \text{ kNm}}{50.285 \text{ kN}} = 0.81682 \text{ m}$$

OVERTURNING: PASS FS: 3.75



Soil pressure resultant eccentricity \boldsymbol{e}

$$e = \left| rac{W_{base}}{2} - a
ight|$$

$$e = \left| \frac{1.524 \text{ m}}{2} - 0.81682 \text{ m} \right| = 0.054818 \text{ m}$$

Uplift check

Check if the resultant falls within the middle third of the base.

$$rac{W_{base}}{6} = rac{1.5240 \; m}{6} = 0.254 \; m \; > e = 0.055 \; m$$

Minimum soil pressure q_{min}

Applied soil pressure distribution

$$q_{min} = rac{\sum P_{vertical}}{W_{base} \cdot 1 \; m} \cdot \left(1 - rac{6 \cdot e}{W_{base}}
ight)$$

$$q_{min} = \frac{50.285 \text{ kN}}{1.524 \text{ m} \cdot 1 \text{ m}} \cdot \left(1 - \frac{6 \cdot 0.054818 \text{ m}}{1.524 \text{ m}}\right) = 25.874 \text{ kPa} > 0 \text{ kPa}$$

Maximum soil pressure q_{max}

$$q_{max} = rac{\sum P_{vertical}}{W_{base} \cdot 1 \; m} \cdot \left(1 + rac{6 \cdot e}{W_{base}}
ight)$$

$$q_{max} = \frac{50.285 \text{ kN}}{1.524 \text{ m} \cdot 1 \text{ m}} \cdot \left(1 + \frac{6 \cdot 0.054818 \text{ m}}{1.524 \text{ m}}\right) = 40.116 \text{ kPa}$$

Stability requirement against bearing capacity failure

Factor of safety ${\cal F}{\cal S}$

$$FS = rac{q_{soil \; sub, \; 1}}{q_{max}}$$

$$FS = \frac{100 \text{ kPa}}{40.116 \text{ kPa}} = 2.4928 \ge 2$$

Sliding:

Horizontal frictional resisting force

Horizontal frictional resisting force considering passive contribution $\mu \sum P + P_p$

$$\mu \sum P + P_p = \mu_{soil-concrete\ sub,\ 1} \cdot \sum P_{vertical} + P_p$$

$$\mu \sum P + P_p = 0.55 \cdot 50.285 \ \mathrm{kN} + 8.2406 \ \mathrm{kN} = 35.897 \ \mathrm{kN}$$

Total horizontal acting force

$$\sum P_{horizontal\ leftwards} = 23.907968\ kN$$

Stability requirement against sliding

Factor of safety FS

$$FS = rac{\mu \sum P + P_p}{\sum P_{horizontal\ leftwards}}$$

$$FS = \frac{35.897 \text{ kN}}{23.908 \text{ kN}} = 1.5015 \ge 1.5$$

UPLIFT CHECK 1: PASS Ratio: 0.216

UPLIFT CHECK 2: PASS Value: 25.87 > 0

BEARING: PASS FS: 2.49

SLIDING: PASS FS: 1.50

