IVANHOÉ CAMBRIDGE INC.

LOT-B RESIDENTIAL DEVELOPMENT, 100 BAYSHORE DR. OTTAWA, ON SITE SERVICING REPORT







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IVANHOÉ CAMBRIDGE INC.

FOR SITE PLAN APPROVAL

PROJECT NO.: 211-02810-00 DATE: APRIL 2021

WSP 2611 QUEENSVIEW DRIVE, SUITE 300 OTTAWA, ON, CANADA, K2B 8K2

WSP.COM

Ivanhoé Cambridge Inc. 95 Wellington St. W., #300 Toronto, ON M5J 2R2

Attention: Jean-François Lavallée

Dear Sir:

Subject: 100 Bayshore Drive, Ottawa, ON – Site Servicing and Stormwater Management Report

Please find attached our site servicing report issued for site plan approval application.

Yours sincerely,

Stephen McCaughey, P.Eng. Project Engineer

WSP ref.: 211-02810-00

2611 QUEENSVIEW DRIVE, SUITE 300 OTTAWA, ON, CANADA, K2B 8K2

QUALITY MANAGEMENT

ISSUE/REVISION	FIRST ISSUE	REVISION 1	REVISION 2	REVISION 3
Remarks	Issued for Site Plan Approval Application			
Date	2021-04-28			
Prepared by	Stephen McCaughey, P.Eng.			
Signature	Smy			
Checked by	James Johnston, P.Eng.			
Signature	Jaldm.E			
Authorised by				
Signature				
Project number	211-02810-00			
Report number				
File reference				

SIGNATURES

PREPARED BY

Stephen McCaughey, P.Eng. Project Engineer

REVIEWED BY

What-

James Johnston, P.Eng. Senior Project Engineer

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1 INTRODUCTION

1.1 EXECUTIVE SUMMARY

WSP was retained by Invanhoé Cambridge to provide servicing, grading and stormwater management design services in support of the site plan approval for the proposed residential development located at 100 Bayshore Dr. Lot B, in the City of Ottawa. The proposed work consists of two residential high-rise towers connected by an above-ground parking podium. The development will likely be constructed in two phases: West Tower first then East Tower. This report will provide sufficient detail to demonstrate that the proposed development can be supported by the existing municipal infrastructure services (watermain, sanitary and storm sewers) and that the servicing design conforms to the applicable standards and guidelines. The report will also include measures to be taken during the construction to minimize erosion and sedimentation. A separate report (100 Bayshore Dr. – Stormwater Management Report) is provided detailing the stormwater management approach and addressing the quantity control and quality measures in accordance with the applicable guidelines.

Currently, the site is an open grassed area with a small array of trees. The southeast corner of the lot has an existing pedestrian bridge between the Bayshore Shopping Centre and the Bayshore Transit Station. The total property area is 6,743 m² in size. The site is bounded by undeveloped land to the west, the transit station to the south, Woodridge Crescent to the north, and transit/shopping centre access road to the east.

The subject site is a single property with easements for Hydro along the west and north edges (refer to Appendix A for the Topographical Survey Plan). There is also an allowance for a multi-use pathway (MUP) that will run along the south and east edges of the site. The site generally slopes away from the centre outwards to the four sides. The site is not currently serviced for water or sanitary, though there are some minor storm sewers on site which will be demolished.

The City of Ottawa requires that the design of a drainage and stormwater management system in this development must be prepared in accordance with the following documents:

- Sewer Design Guidelines, City of Ottawa, October 2012;
- Stormwater Management Planning and Design Manual, Ministry of the Environment, March 2003; and
- Stormwater Management Facility Design Guidelines, City of Ottawa, April 2012

This report was prepared utilizing servicing design criteria obtained from the City of Ottawa and outlines the design for water, sanitary wastewater and stormwater facilities.

The format of this report matches that of the servicing study checklist found in Section 4 of the City of Ottawa's Servicing Study Guidelines for Development Applications, November 2009.

The following municipal services are available within Woodridge Cres. adjacent to the development as recorded from the following as-built drawings received from the City:

Woodridge Cres.

▶ 203 mm PVC watermain, 250 mm concrete sanitary sewer and 675 mm concrete stormwater sewer.

It is proposed that an on-site stormwater management system will be provided to collect and attenuate flow rates leaving the site. Refer to stormwater management report for details.

1.2 LOCATION MAP AND PLAN

The site at 100 Bayshore Dr. is shown in the centre of Figure 1-1 below as presented in the GeoOttawa website. The parcels are still shown separately, but it is our understanding that they have been merged as a single parcel.



Figure 1-1 Site Location

The proposed development will consist of two high-rise residential towers with a shared three storey parking podium (and one below grade parking). The building will have a gross floor area of approximately $50,000 \text{ m}^2$. See Appendix A for the architectural site plan. The project will be a phased development: the west tower will be constructed first then the east tower.

1.3 HIGHER LEVEL STUDIES

The review for servicing has been undertaken in conformance with, and utilizing information from, the following documents:

- Ottawa Sewer Design Guidelines, Second Edition, Document SDG002, October 2012, City of Ottawa including all amendments issued as part of Technical Bulletins.

- Ottawa Design Guidelines – Water Distribution, July 2010 (WDG001), including all amendments issued as part of Technical Bulletins.

- Stormwater Management Planning and Design Manual, Ontario Ministry of the Environment and Climate Change, March 2003 (SMPDM).

- Design Guidelines for Drinking-Water Systems, Ontario Ministry of the Environment and Climate Change, 2008 (GDWS).
- Fire Underwriters Survey, Water Supply for Public Fire Protection (FUS), 1999.

1.4 AVAILABLE EXISTING AND PROPOSED INFRASTRUCTURE

As described above, all municipal mains (sanitary, storm and watermain) are available and located along Woodridge Crescent. Valved water servicing will be provided as well as sanitary servicing with monitoring hole at or near the property line. Quantity and quality control is required to restrict the stormwater discharge leaving the site, thus the on-site storm runoff will be captured, detention storage provided, flow release restricted, treated for quality control requirements, and finally directed towards the existing storm sewer on Woodridge Crescent.

1.5 GEOTECHNICAL STUDY

Golder provided a draft geotechnical investigation report of the subject property dated September 2020. Based on the report, groundwater was measured between 2.7-5.6 m below grade. The recommendations of the report have been taken into account for this design development.

2 WATER DISTRIBUTION

2.1 SYSTEM CONSTRAINTS AND BOUNDARY CONDITIONS

Boundary conditions have been provided by the City of Ottawa at the existing connection along the Woodridge Cres. 203mm watermain (Zone 1W).

Scenario	Woodridge Cres.
Scenario	Connection
Average Day (MAX HGL)	115.2m
Peak Hour (MIN HGL)	106.3m
Max Day + Fire Flow	82.5m

 Table 2-1:
 Boundary Conditions (City of Ottawa)

2.2 CONFIRMATION OF ADEQUATE DOMESTIC SUPPLY AND PRESSURE

Water demands are based on Table 4.2 of the Ottawa Design Guidelines – Water Distribution for these residential demands based on the number of apartment units. For purpose of verification of supply, the full buildout (both towers) have been assumed. A water demand calculation sheet is included in Appendix B, and the total water demands are summarized as follows:

	West Tower	East Tower	Total
Average Day	1.35 L/s	1.52 L/s	2.86 L/s
Maximum Day	3.38 L/s	3.77 L/s	7.15 L/s
Peak Hour	7.44 L/s	8.28 L/s	15.72 L/s

Since the average day demand is greater than 50,000 L/d (0.58 L/s), twin 150mm services will be provided from Woodridge Cres. to the building, as shown in the site servicing drawing in Appendix D.

The pressure criteria identified in the guidelines are as follows:

Minimum Pressure	Minimum system pressure under peak hour demand conditions shall not be less than 276 kPa (40 psi)
Fire Flow	During the period of maximum day demand, the system pressure shall not be less than 140 kPa (20 psi) during a fire flow event.
Maximum Pressure	Maximum pressure at any point the distribution system shall not exceed 689 kPa (100 psi). In accordance with the Ontario Building/Plumbing Code, the maximum pressure should not exceed 552 kPa (80 psi). Pressure reduction controls may be required for buildings where it is not possible/feasible to maintain the system pressure below 552 kPa.

The site has been analyzed as summarized below and in Table 2-2 to ensure all the City of Ottawa minimum criteria for water pressures are met for the two conditions (maximum day + fire flow and peak hour). The analysis was carried out using

EPANET, hydraulic and water quality analysis based on the boundary conditions provided by the City of Ottawa. The detailed EPANET output results are also included in the Appendix B.

With respect to a max day + fire flow of 140.48 L/s, the model indicated that the pressure drop in the pipe was acceptable and within the City of Ottawa's minimum pressure requirements. Section 2.3 following details the fire flow estimation.

With respect to a peak hour demand of 15.72 L/s, the model indicated that the pressure drop in the pipe was also acceptable and within the City of Ottawa's minimum pressure requirements.

Refer to Appendix B for the detailed water distribution analysis output.

Scenario	Pressure at Building Connection	
Scenario		
	(psi)	(kPa)
Max Day + Fire	21	145
Flow		
Peak Hour (MIN	60	414
HGL)		
Average Day	73	502
(Max HGL)		

Table 2-2: Summary of Water Pressure from EPANET results

2.3 CONFIRMATION OF ADEQUATE FIRE FLOW PROTECTION

The fire flow rate has been calculated using the Fire Underwriters Survey (FUS) method. The method takes into account the type of building construction, the building occupancy, the use of sprinklers and the exposures to adjacent structures. For fire resistive construction with a full sprinkler system only the first four largest floors are taken into account, leading to the calculated fire flow demand of 8,000 L/min (133 L/s). A copy of the FUS calculations are included in Appendix B.

The maximum fire demand of 8,000 L/min can be delivered through the proposed twin 150mm services. Further, there is one Class AA fire hydrant within 75m of the building and two Class AA fire hydrants with 150m of the building along the same side of Woodridge Cres. capable of providing total 13,248 L/min per City of Ottawa Technical Bulletin ISTB-2018-02. The nearest hydrant will be replaced and slightly relocated to be within 45m of the building fire department connections.

The boundary condition for Maximum Day and Fire Flow results in a pressure of 145 kPa at the building. In the guidelines, a minimum residual pressure of 140 kPa must be maintained in the distribution system for a fire flow and maximum day event; therefore, the fire flow requirement is met.

3 WASTEWATER DISPOSAL

3.1 DESIGN CRITERIA

In accordance with the City of Ottawa's Sewer Design Guidelines, the following design criteria have been utilized in order to estimate wastewater flows generated by the subject site and verify existing capacity;

٠	Average sanitary flow for residential use	280 L/c/d
٠	Gross area Residential use	0.6
•	Infiltration & Foundation Allowance (Total)	0.33 L/ha/s

3.2 CALCULATIONS FOR SANITARY DEMAND

The criteria to determine anticipated peak flow based on site used as described in Ottawa Sewer Design Guidelines Appendix 4-A are as follows, refer to appendix C for detailed calculation. Since the building size and lot zoning is not changing, from a capacity verification standpoint there isn't a difference considered for current demand estimate to postrefit demand estimate. Detailed calculations are provided in Appendix C.

	West Tower	East Tower	Total
Average Day	1.35 L/s	1.51 L/s	2.86 L/s
Peak	4.61 L/s	5.11 L/s	2.86 L/s
Extraneous Day	0.10 L/s	0.10 L/s	0.20 L/s
Total	4.71 L/s	5.21 L/s	9.92 L/s

3.3 VERIFICATION OF AVAILABLE CAPACITY IN EXISTING SEWER

The sanitary demand will be serviced by a 150mm sewer with a minimum slope of 1% to the 250mm sewer on Woodridge Crescent, on a proposed maintenance hole installed on the existing sewer. A Sanitary Sewer Design Sheet is provided in Appendix C confirming capacity and minimum scouring velocity is achieved. Further, per communication with the City provided in Appendix F, the existing downstream sewer has sufficient capacity for the estimated peak flow.

4 SITE STORM SERVICING

4.1 EXISTING CONDITION

The subject site is located on the south side of Woodridge Crescent, west of the Bayshore Shopping Centre and north of the Bayshore Transit Station, currently undeveloped with grass, shrub and tree growth. The site contains some storm infrastructure (pipes, maintenance holes, catch basins) that will be removed/abandoned as part of the development. The storm sewer entering the site at the southwest is abandoned as part of the Phase 2 LRT Expansion. Most runoff from the subject site is ultimately directed to 675 mm diameter trunk storm sewer, which runs from east to west along Woodridge Cres.

4.2 DRAINAGE DRAWINGS

Site drawings are included in Appendix D including servicing, grading, drainage area, and erosion and sediment control.

4.3 WATER QUANTITY CONTROL OBJECTIVE

Refer to the Stormwater Management Report for the water quantity objective for the site.

4.4 WATER QUALITY CONTROL OBJECTIVE

Refer to the Stormwater Management Report for the water quality objective for the site.

4.5 PROPOSED MINOR SYSTEM

The development will be serviced by 375 mm storm service connection with a proposed maintenance hole on the existing 675 mm storm sewer on Woodridge Crescent. Runoff from the new development area of the site will be collected by a network of surface inlets and storm sewers. Prior to the site oil grit separator, a flow restrictor will be placed in a maintenance hole to restrict post-development flows to the allowable rate. An underground storage cistern will be installed in the building footprint where flows exceeding the allowable site discharge rate will backflow into the cistern, as well drainage from the building roofs will be directed directly into the cistern. The cistern will be complete with sump pumps to discharge at fixed rates back into the drainage system. The sewer design sheet for the site storm system is provided in Appendix E.

4.6 PROPOSED MAJOR SYSTEM

The major overland flow routes lead out to Woodridge Crescent, with the overflow elevations at the driveway entrances to the ROW at minimum 300mm below the building entrances (66.50m). Additionally, the spillover point is less than 300mm from the catch basin elevation so there will be no ponding greater than 300mm even in cases of catch basin blockage. The storm sewers are sized such that no ponding will occur during the 2-year and even 100-year storm, with capacity exceedances backflowing into the cistern. The storm sewer design sheets are provided in Appendix E.

5 SEDIMENT AND EROSION CONTROL

5.1 GENERAL

Prior to topsoil stripping, earthworks or underground construction, erosion and sediment controls will be implemented and will be maintained throughout construction. Silt fences will be installed around the perimeter of the site and will be cleaned and maintained throughout construction. Silt fences will remain in place until the working areas have been stabilized or re-vegetated. Catch basins and manholes will have filter fabric installed under the grate during construction to protect from silt entering the storm sewer system. A mud mat will be installed at the construction access to reduce risk of mud tracking onto adjacent roads.

Erosion and sediment controls must be in place during construction. Recommendations to the contractor will be included in the erosion and sediment control plan C05 in Appendix D and are summarized below:

During all construction activities, erosion and sedimentation shall be controlled by the following techniques:

Prior to start of construction:

- ▶ Install silt fence along the perimeter of the property line.
- Install filter fabric or silt sack filters in all the catchbasins and manholes that capture runoff from the construction area.

During construction:

- Minimize the extent of disturbed areas and the duration of exposure and impacts to existing grading.
- Perimeter vegetation to remain in place until permanent storm water management is in place otherwise, immediately install silt fence when the existing site is disturbed at the perimeter.
- Protect disturbed areas from overland flow by providing temporary swales to the satisfaction of the field engineer. Tie-in temporary swale to existing catchbasins as required.
- > Provide temporary cover such as seeding or mulching if disturbed area will not be rehabilitated within 30 days.
- ▶ Inspect silt fences, filter fabric filters and catch basin sumps weekly and within 24 hours after a storm event. Clean and repair when necessary.
- Drawing to be reviewed and revised as required during construction.
- Erosion control fencing to be also installed around the base of all stockpiles.
- Do not locate topsoil piles and excavation material closer than 2.5m from any paved surface, or one which is to be paved before the pile is removed. All topsoil piles are to be seeded if they are to remain on site long enough for seeds to grow (longer than 30 days).
- Control dust blown off-site by seeding topsoil piles and other areas temporarily (provide watering as required and to the satisfaction of the engineer).
- ▶ No alternate methods of erosion protection shall be permitted unless approved by the field engineer.
- City roadway and sidewalk to be cleaned of all sediment from vehicular tracking as required.
- > Provide gravel entrance (mud mat) wherever equipment leaves the site to provide mud tracking onto paved surfaces.

During wet conditions, tires of all vehicles/equipment leaving the site are to be scrapped.

Any mud/material tracked onto the road shall be removed immediately by hand or rubber tire loader.

Take all necessary steps to prevent building material, construction debris or waste being spilled or tracked onto abutting properties or public streets during construction and proceed immediately to clean up any areas so affected.

All erosion control structure to remain in place until all disturbed ground surfaces have been stabilized either by paving or restoration of vegetative ground cover.

• During the course of construction, if the engineer believes that additional prevention methods are required to control erosion and sedimentation, the contractor will install additional silt fences or other methods as required to the satisfaction of the engineer.

► The contractor shall implement best management practices, to provide for protection of the area drainage system and the receiving watercourse, during construction activities. The contractor acknowledges that failure to implement appropriate erosion and sediment control measures may be subject to penalties imposed by any applicable regulatory agency.

6.1 **GENERAL**

The proposed development is subject to City of Ottawa site plan approval and criteria from the Rideau Valley Conservation Authority.

No other permits or approvals are anticipated to be required from the Ontario Ministry of the Environment, Conservation and Parks (MECP), Ontario Ministry of Transportation, National Capital Commission, Parks Canada, Public Works and Government Services Canada, or any other provincial or federal regulatory agency except those noted above.

7 CONCLUSION CHECKLIST

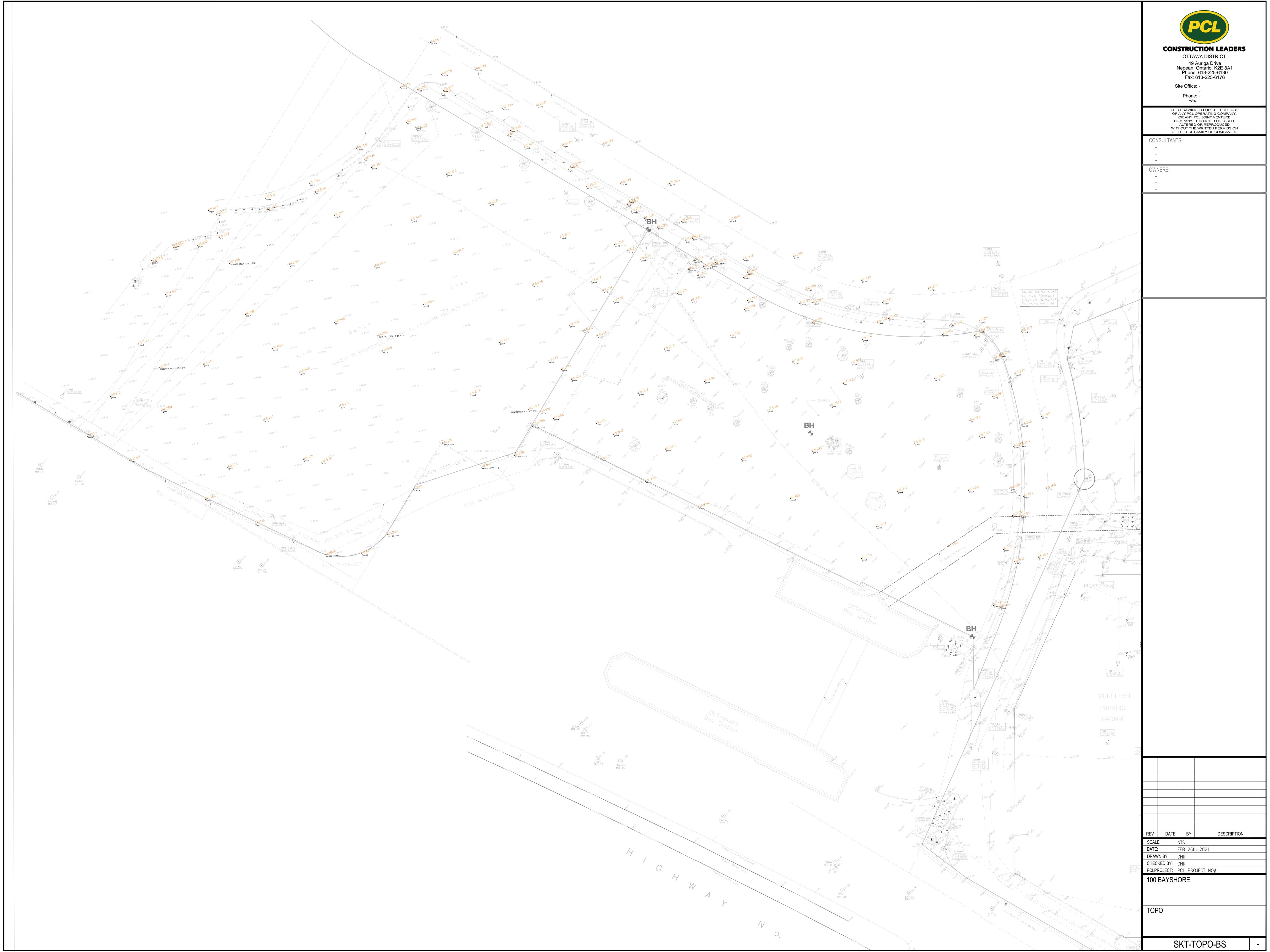
7.1 CONCLUSIONS AND RECOMMENDATIONS

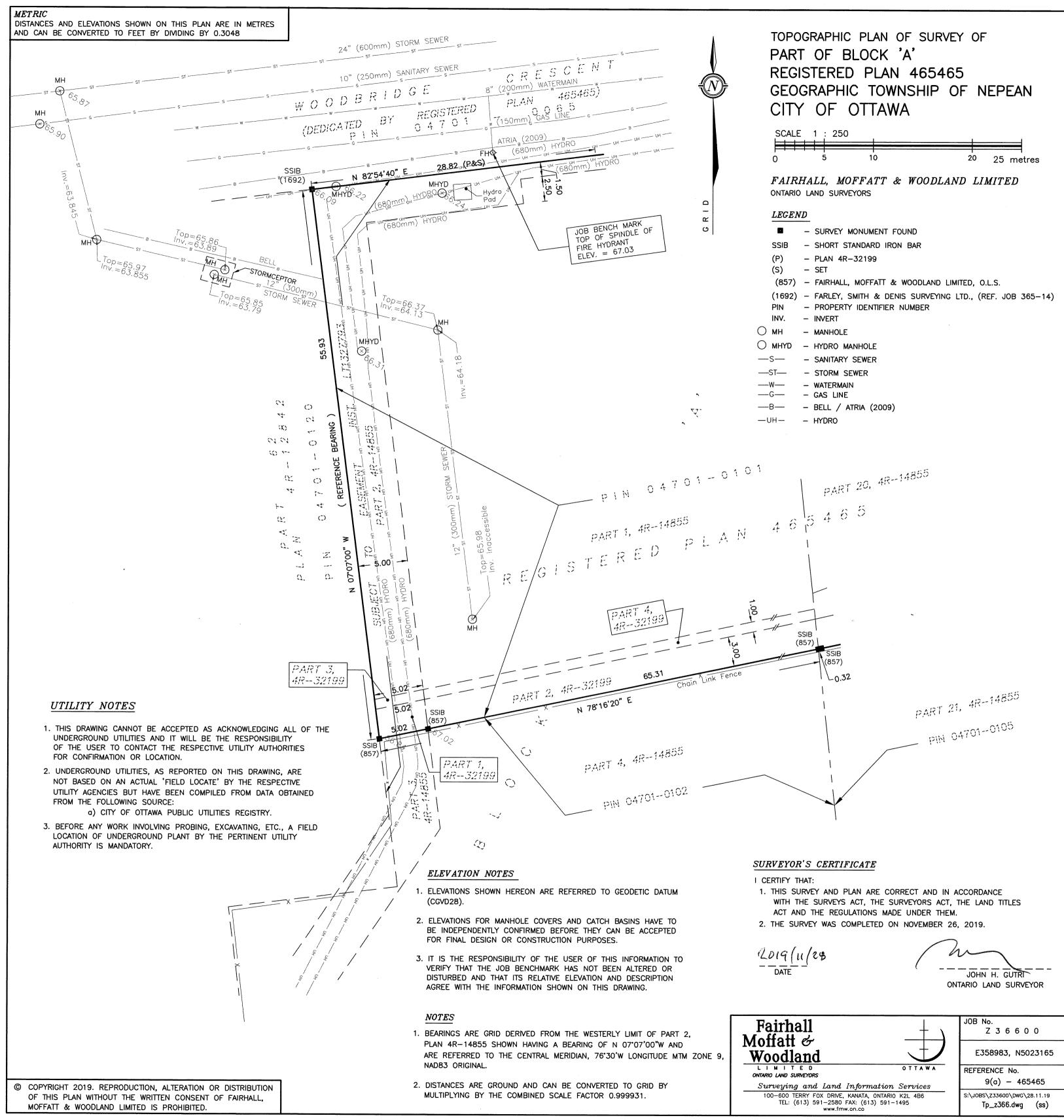
It is concluded that the proposed development can meet all provided servicing constraints and associated requirements. It is recommended that this report be submitted to the City of Ottawa in support of the application for site plan approval.

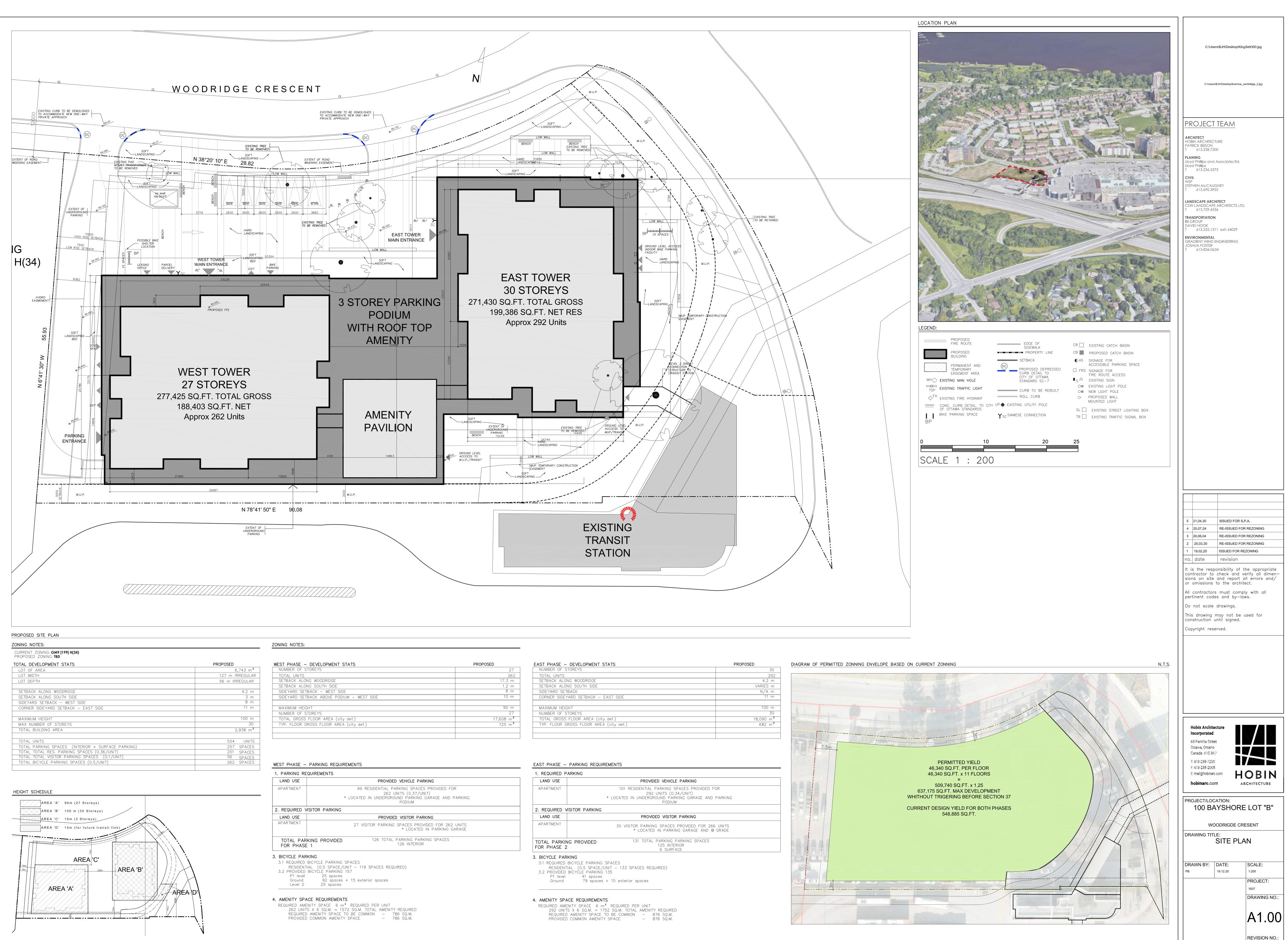
7.2 COMMENTS RECEIVED FROM REVIEW AGENCIES

Minutes from a pre-consultation meeting held with the City of Ottawa are provided in Appendix F.

A TOPOGRAPHICAL SURVEY & ARCHITECTURAL PLAN







5	PROPOSED
	27
	262
	17.3 m
	1.2 m
	8 m
- WEST SIDE	10 m
	90 m
	27
)	17,608 m²
y def.)	725 m ²

AST PHASE – DEVELOPMENT STATS	PROPOSEI
NUMBER OF STOREYS	
TOTAL UNITS	
SETBACK ALONG WOODRIDGE	
SETBACK ALONG SOUTH SIDE	
SIDEYARD SETBACK	
CORNER SIDEYARD SETBACK – EAST SIDE	
MAXIMUM HEIGHT	
NUMBER OF STOREYS	
TOTAL GROSS FLOOR AREA (city def.)	
TYP. FLOOR GROSS FLOOR AREA (city def.)	

ITS	
PROVIDED VEHICLE PARKING	
99 RESIDENTIAL PARKING SPACES PROVIDED FOR	

LAND USE		PROVIDED VEHICLE PARKING			
APARTMENT		101 RESIDENTIAL PARKING SPACES PROVIDED FOR			
		292 UNITS (0.34/UNIT)			
		* LOCATED IN UNDERGROUND PARKING GÁRAGE AND PARKING PODIUM			
2. REQUIRED V	ISITOR PARKING				
LAND USE		PROVIDED VISITOR PARKING			
APARTMENT		30 VISITOR PARKING SPACES PROVIDED FOR 266 UNITS * LOCATED IN PARKING GARAGE AND @ GRADE			
TOTAL PARKIN		131 TOTAL PARKING PARKING SPACES			
FOR PHASE 2		125 INTERIOR 6 SURFACE			
. BICYCLE PAR	KING				
3.1 REQUIRED	BICYCLE PARKING	SPACES			
•		UNIT – 133 SPACES REQUIRED)			



Lot-B Residential Development, 100 Bayshore Dr. Ottawa, ON Project No. 211-02810-00 Ivanhoé Cambridge Inc.

211-02810-00

WATER DISTRIBUTION - PROPOSED DOMESTIC DEMANDS

Demand Type		Amount	Units	
Average Day Demand				
Residential	=	280	L/c/d	
Light Industrial	=	35000	L/gross ha/d	
Heavy Industrial	=	55000	L/gross ha/d	
Shopping Centres	=	2500	L/(1000m2/d)	
Hospitals	=	900	L/(bed/d)	
Schools	=	70	L/(Students/d)	
Trailer Parks no Hook-Ups	=	340	L/(space/d)	
Trailer Parks with Hook-Ups	=	800	L/(space/d)	
Campgrounds	=	225	L/(campsite/d)	
Mobile Home Parks	=	1000	L/(Space/d)	
Motels	=	150	L/(bed-space/d)	
Hotels	=	225	L/(bed-space/d)	
Tourist Commercial	=	28000	L/gross ha/d	
Other Commercial	=	28000	L/gross ha/d	
Maximum Daily Demand:				
Residential	=		average day	L/c/d
Industrial	=		average day	L/gross ha/d
Commercial	=	1.5 x	average day	L/gross ha/d
Institutional	=	1.5 x	average day	L/gross ha/d
Maximum Hour Demand:				
Residential	=	2.2 x	maximum day	L/c/d
Industrial	_		maximum day	L/gross ha/d
Commercial	=		maximum day	L/gross ha/d
Institutional	=		maximum day	L/gross ha/d

Unit Type	Person / Unit
Single Family	3.4
Semi-detached	2.7
Duplex	2.3
Townhouse (row)	2.7
Apartments:	· ·
Bachelor	1.4
1 Bedroom	1.4
2 Bedroom	2.1
3 Bedroom	3.1
Average Apt.	1.8

Population Calculator	East Tower	West Tower
Single Family		
Semi-detached		
Duplex		
Townhouse (row)		
Bachelor		
1 Bedroom	212	190
2 Bedroom	80	72
3 Bedroom		
Avergage Apt.		
Total Population	465	417

	E	ast Tower	W	lest Tower	Combined Demand
Demand Type =	Residential		Residential		
Average Day Demand =	280	L/c/d	280	L/c/d	
Population =	465		417		
=	280 x	465	280	x 417	
=	130,144	L/day	116,816	L/day	
Average Daily Flow =	1.51	L/s	1.35	L/s	2.86
Daily Demand Type =	Residential		Residential		
Max. Daily Factor =	2.5	L/c/d	2.5	L/c/d	
=	2.5 x	Average Daily Flow	2.5	 Average Daily Flow 	
=	2.5 x	130,144	2.5	x 116,816	
=	325,360	L/day	292,040	L/day	
Maximum Daily Demand =	3.77	L/s	3.38	L/s	7.15
Hour Demand Type =	Residential		Residential		
Max. Hour Factor =	2.2	L/c/d	2.2	L/c/d	
=	2.2 x	Maximum Daily Demand	2.2	x Maximum Daily Demand	
=	2.2 x	,	2.2	x 292,040	
=	715,792	L/day	642,488	L/day	
Maximum Hour Demand =	8.28	L/s	7.44	L/s	15.72

WATER DISTRIBUTION - PROPOSED FIRE FLOW DEMANDS

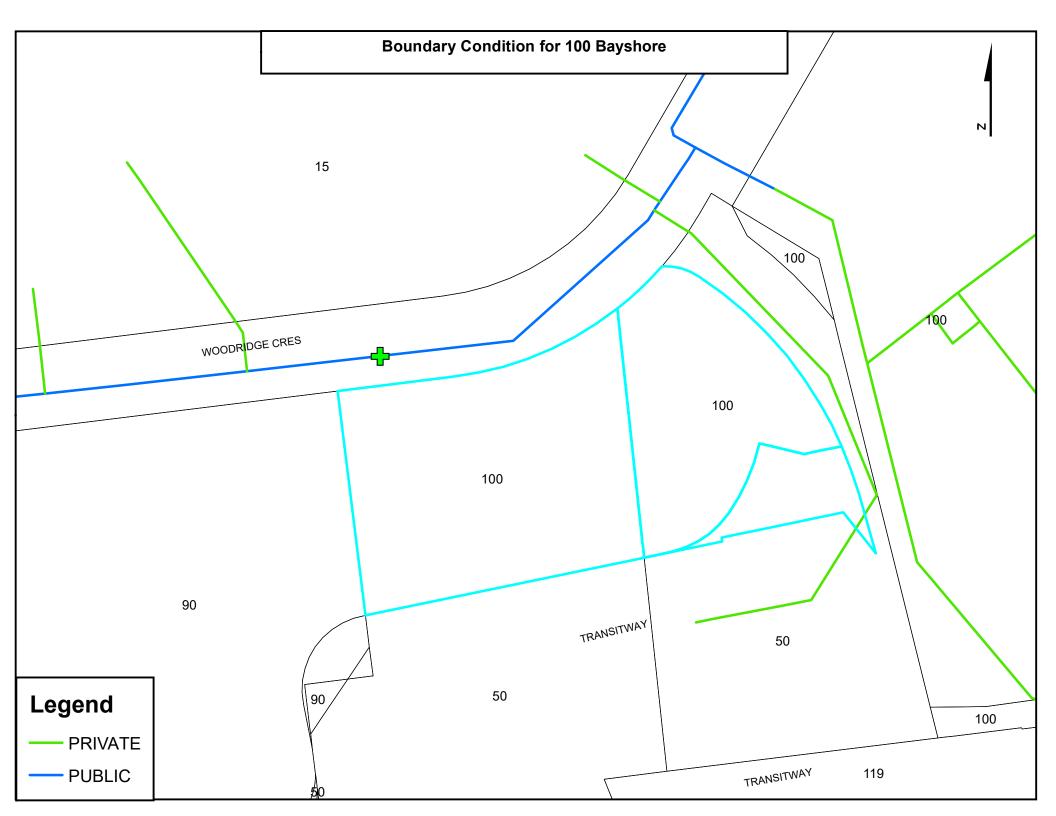
F = 220 C √ A

Type of Construction Coefficient:		Comments
Wood Frame	1.5	(all structurally combustible)
Ordinary	1.0	(brick, masonry wall, combustible floor and interior)
Non-Combustible	0.8	(unprotected metal structural component, masonry or metal walls)
Fire Resistive	0.6	(fully protected frame, floors and roof)
Combustibility:		
Non-Combustible	-25%	
Limited Combustible	-15%	
Combustible	0%	
Free Burning	15%	
Rapid Burning	25%	
Sprinkler Protection:	1	
Complete Sprinkler System	-50%	(max.)
NFPA 13 Conformed	-30%	(max.)
If Water Supply Standard for Both System and Fire Lines	-10%	additional (max.)
Fully Supervised System	-10%	additional (max.)
None	0%	

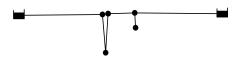
	East Tower			West Tower		
Type of Construction Coefficient	Fire Resistive			Fire Resistive		
		0.6	•		0.6	
Gross Floor Area (m ²)		10,926	m2		10,915 m	12
Fire Flow, F		13,798	L/min		13,791 L/	/min
F(round)		14,000	L/min		14,000 L/	'min
Modification 1: Occupancy Combustibility	Limited Combustible			Limited Combustible		
		-15%			-15%	
Occupancy Credit		-2,100			-2,100 L/	
F(mod1) = F(round) + Occupancy Credit		11,900	L/min		11,900 L/	min
Modification 2: Sprinkler Protection	Complete Sprinkler System			Complete Sprinkler System		
		-50%			-50%	
Additional Credit	If Water Supply Standard for Both System and Fire Lines			If Water Supply Standard for Both System and Fin	re Lines	
	0			0		
Sprinkler Credit		-5,950			-5,950 L/	
F(mod2) = F(mod1) + Sprinkler Credit		5,950	L/min		5,950 L/	min
Modification 3: Exposure Distances North		>45	m 0%		>45 m	n 0'
South		>45			>45 m	
East		>45			20 m	
West		20			>45 m	
west		Total %			Total %	= 159
			x 0.15		11,900	x 0.15
Exposure Credit		1,785			1,785 L/	
F(mod3) = F(mod2) + Exposure Credit		7,735			7,735 L/	
F(final) = F(mod3) rounded to nearest 1,000L/min		8,000			8,000 L/	
F(final)		133			133 L/	s

	East Tower	West Tower		
Average Daily Demand	1.51	1.35	2.86	-
Maximum Daily Demand	3.77	3.38	7.15	L/s
Peak Hour Demand	8.28	7.44	15.72	L/s
Fire Flow	133	133		L/s

Max Day + Fire Flow 140.48 L/s



Day 1,



Page 1 *******	****	3/16/2021 3:54:37 PM
*	ΕΡΑΝΕΤ	*
*	Hydraulic and Water Quality	*
*	Analysis for Pipe Networks	*
*	Version 2.0	*
*****	*****	*****

Input File: 100 Bayshore Dr - Model.net

Link - Node Table: _____ Link Start End Length Diameter ID Node Node m mm _____ SiteConnection1SiteConnection23203SiteConnection1Building13150SiteConnection2Building13150SiteConnection2SiteHydrantConnection8SiteHydrantConnection50 10 11 12 13 203 SiteHydrantConnectionEastSupply 50 203 14 15 WestSupply SiteConnection1 50 203 6 150 16 SiteHydrantConnectionSiteHydrant Node Results:

 Node
 Demand LPS
 Head m
 Pressure m
 Quality

 ID
 LPS
 m
 m
 m
 m

 SiteConnection2
 0.00
 115.20
 51.50
 0.00

 Building
 2.86
 115.20
 51.20
 0.00

 SiteConnection1
 0.00
 115.20
 51.50
 0.00

 SiteHydrantConnection
 0.00
 115.20
 51.50
 0.00

 SiteHydrant
 0.00
 115.20
 0.00
 0.00

 SiteHydrant
 0.00
 115.20
 0.00
 0.00

 SiteHydrant
 0.00
 115.20
 0.00
 0.00

 WestSupply
 -1.49
 115.20
 0.00
 0.00
 Reservoir

 EastSupply
 -1.37
 115.20
 0.00
 0.00
 Reservoir

Link Results:

Link	Flow	VelocityUnit	Headloss	Status
ID	LPS	m/s	m/km	
10 11 12 13 14 15 16	$\begin{array}{c} 0.06 \\ 1.43 \\ 1.43 \\ -1.37 \\ -1.37 \\ 1.49 \\ 0.00 \end{array}$	0.00 0.08 0.08 0.04 0.04 0.04 0.05 0.00	0.00 0.12 0.12 0.02 0.02 0.02 0.02 0.02	Open Open Open Open Open Open Open

Page 1 ******	*****	3/16/2021 3:56:40 PM
*	ΕΡΑΝΕΤ	*
*	Hydraulic and Water Quality	*
*	Analysis for Pipe Networks	*
*	Version 2.0	*
*****	******	*****

Input File: 100 Bayshore Dr - Model.net

Link - Node Table: _____ Link Start End Length Diameter ID Node Node m mm _____ SiteConnection1siteConnection23203SiteConnection1Building13150SiteConnection2Building13150SiteConnection2siteHydrantConnection8SiteHydrantConnectionEastSupply50WestSupplySiteConnection150SiteHydrantConnection56 10 11 12 13 203 14 203 15 SiteHydrantConnectionSiteHydrant 6 150 16 Node Results:

Node ID	Demand LPS	Head m	Pressure m	Quality	
SiteConnection2 Building SiteConnection1 SiteHydrantConnectio SiteHydrant WestSupply EastSupply	0.00 15.72 0.00 0n -8.17 -7.55	$\begin{array}{c} 106.27\\ 106.24\\ 106.27\\ 0.00 \\ 106.28\\ 106.30\\ 106.30\\ 106.30 \end{array}$	42.57 42.24 42.57 06.28 39.28 0.00 0.00		0.00 Reservoir Reservoir

Link Results:

Link	Flow	VelocityUnit	Headloss	Status
ID	LPS	m/s	m/km	
10 11 12 13 14 15 16	0.31 7.86 7.86 -7.55 -7.55 8.17 0.00	0.01 0.44 0.44 0.23 0.23 0.25 0.00	0.00 2.75 2.75 0.49 0.49 0.57 0.00	Open Open Open Open Open Open Open Open

Page 1 ********************	****	3/16/2021 3:51:56 PM
*	EPANET	*
*	Hydraulic and Water Quality	*
*	Analysis for Pipe Networks	*
*	Version 2.0	*
*****	******	*****

Input File: 100 Bayshore Dr - Model.net

Link - Node Table: -----Link Start End Length Diameter ID Node Node m mm SiteConnection1SiteConnection23203SiteConnection1Building13150SiteConnection2Building13150SiteConnection2SiteHydrantConnection8SiteHydrantConnectionEastSupply50WestSupplySiteConnection150SiteHydrantConnectionSiteHydrant6 10 11 12 13 203 203 14 15 6 SiteHydrantConnectionSiteHydrant 150 16 Node Results: -----Node Demand Head Pressure Quality ID LPS m m SiteConnection20.0080.8617.160.00Building140.4878.7914.790.00SiteConnection10.0080.8617.160.00SiteHydrantConnection0.0081.0917.390.00SiteHydrant0.0081.0914.090.00WestSupply-73.0582.500.000.00 ReservoirEastSupply-67.4382.500.000.00 Reservoir Link Results: _____ Flow VelocityUnit Headloss Status ∟ink

ID	LPS	m/s	m/km	
10	2.81	0.09	0.08	Open
11	70.24	3.97	158.92	Open
12	70.24	3.97	158.91	Open
13	-67.43	2.08	28.29	Open
14	-67.43	2.08	28.29	Open
15	73.05	2.26	32.81	Open
16	0.00	0.00	0.00	Open



SANITARY SEWAGE - PROPOSED SANITARY FLOWS

Average Wastewater Flows:		
Residential	280	L/c/d
Commercial	28,000	L/gross ha/d
Institutional	28,000	L/gross ha/d
Light Industrial	35,000	L/gross ha/d
Heavy Industrial	55,000	L/gross ha/d

Harmon Equation
1.5
1.0
1.5
1.0
Per Figure in Appendix 4-B

Peak Extraneous Flows:	
Infiltration Allowance	0.33
Less than 10 ha:	
Foundation Drain Allowance	5.0
10 ha - 100 ha:	
Foundation Drain Allowance	3.0
Greater than 100 ha:	
Foundation Drain Allowance	2.0

DE _ 1 + /	· 14)	νV
P.F. = 1 + ($4 + \left(\frac{P}{1000}\right)^{\circ}0.5$	*К
	· /	

where P = population K = correction factor = 0.8

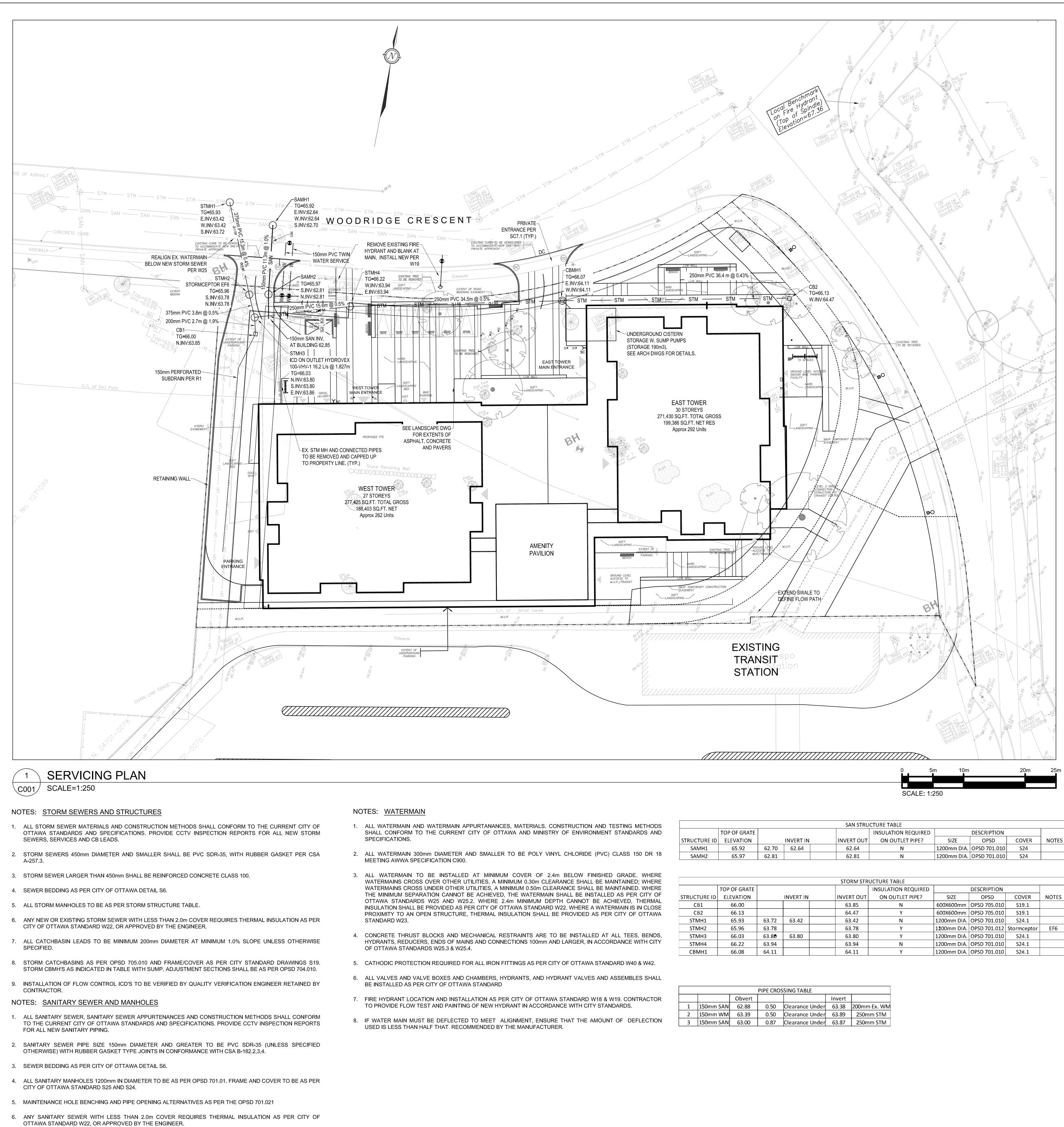
Unit Type	Person Per Unit	East Tower	West Tower	
Single Family	3.4			
Semi-detached	2.7			
Duplex	2.3			
Townhouse (row)	2.7			
Apartments:				
Bachelor	1.4			
1 Bedroom	1.4	212	190	
2 Bedroom	2.1	80	72	
3 Bedroom	3.1			
Average Apt.	1.8			
	Total Population:	465	417	8
	Total Area (ha):	0.3	0.3	C

	Phase	1 (East T	'ower)	Phase 2 (West To	ower)
Demand Type=	Residential			Residential		
Average Day Demand=	280		L/c/d	280		L/c/d
Population	465			417		
Site Area (ha)	0.300			0.300		
	280	х	465	280	х	417
	130,144		L/day	116,816		L/day
Average Daily Flow=	1.51		L/s	1.35		L/s
Peaking Factor Type	Residential			Residential		
Peaking Factor	3.39		*Max=4	3.41		*Max=4
	3.39	х	average day	3.41	x	average day
	3.39	х	130,144	3.41	x	116,816
	441,482		L/day	398,427		L/day
Peak Daily Flow=	5.11		L/s	4.61		L/s
Infiltration Allowance	0.33			0.33		
	0.33	х	lot area	0.33	х	lot area
	0.33	х	0.3	0.33	х	0.3
Peak Extraneous Flow=	0.10		L/s	0.10		L/s
	peak daily flow	+	extraneous flow	peak daily flow	+	extraneous flow
	5.11	+	0.10	4.61	+	0.10
Total Peak Design Flow=	5.21		L/s	4.71		L/s

Phase 1 (East Tower) - Peak	
Design Flow =	5.21 L/s
Phase 2 (West Tower) - Peak	
Design Flow =	4.71 L/s
Total Peak Design Flow =	9.92 L/s

LOCATION				RESIDEN	ITIAL ARE	A AND P	OPULATIO	ON	INSTITU	JTIONAL	C+I+I	IN	FILTRATI	ON	TOTAL				PIPE		
CONNECTIONS	FROM MH	ТО МН	AREA (Ha)	POP.	AREA	POP.	PEAK FACT.	PEAK FLOW (I/s)	AREA (Ha)	ACCU. AREA	PEAK FLOW	TOTAL AREA	AREA	INFILT. FLOW	FLOW (I/s)	LENGTH (m)	DIA. (mm)	SLOPE (%)	CAP. (FULL)	PIPE CAPACITY	VEL. (FULL)
	+		. ,		(Ha)			. ,	. ,	(Ha)	(l/s)	(Ha)	(Ha)	(l/s)		. ,	. ,		(l/s)	USED (%)	(m/s)
Building	Building	SANMH2	0.6	882	0.60	882	3.4	9.72	0.000	0.000	0.00	0.6	0.6	0.20	9.92	3.8	150.00	1.1%	15.63	63.5%	0.88
	SANMH2	SANMH1	0.0	0	0.60	882	0.0	9.72	0.000	0.000	0.00	0.0	0.6	0.20	9.92	11.3	150.00	1.0%	15.03	66.0%	0.85
	DES	IGN PARAMETER	S						Designed	:		PROJEC	T:								
									Stephen McCaughey, P.Eng. 100 Bayshore Lot "B"												
Residential: 280 L/cap/d									Checked: LOCATION:												
Peak Factor = 3.4			Ishaque Jafferjee, P.Eng. 100 Bayshore Dr., I						Dr. Lot P	Dr., Lot B, Woodridge Cres., Ottawa, ON											
Extraneous Flow = 0.33 l/s/ha									isnaqu	Jallerjee	-			100	Dayshore	DI., LOUB,	woounug	e cies., O	llawa, ON		
Minimum Velocity = 0.60 m/s									Dwg. Ref	erence:		File Ref.:				Date:					Sheet
Manning's n = 0.013	Vanning's n = 0.013																April	2021			1 of 1

D SITE DRAWINGS

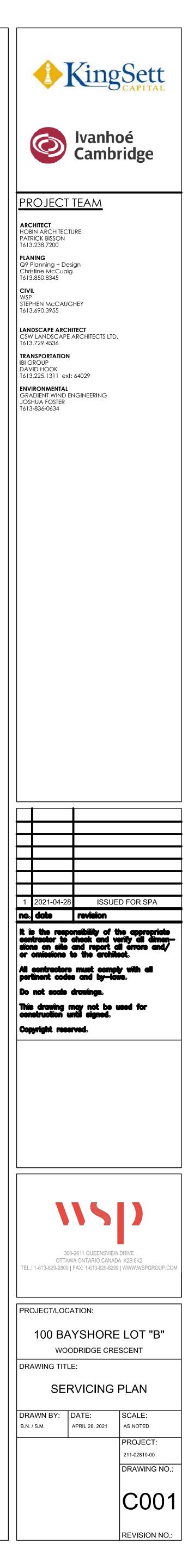


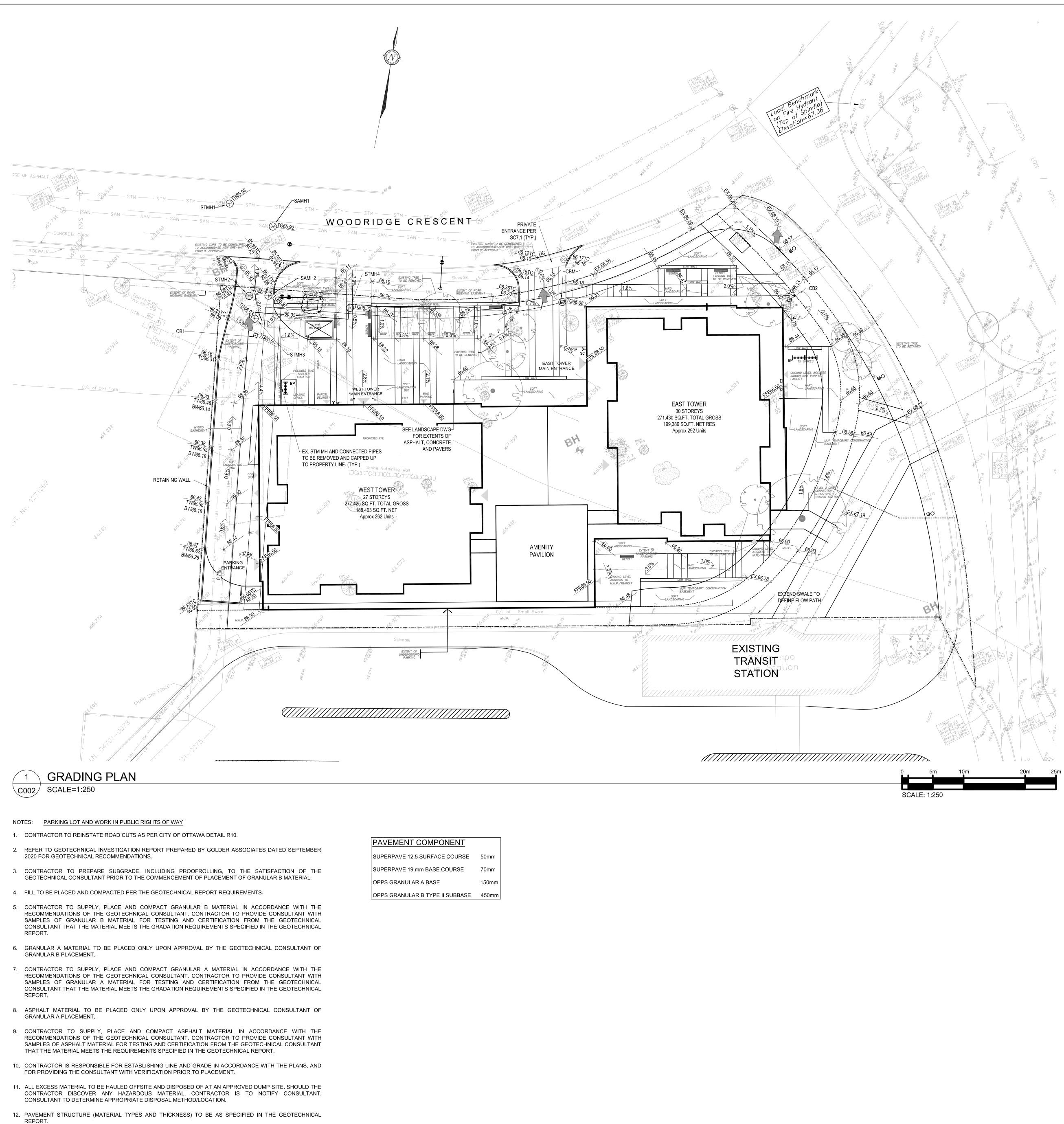
				SAN STRU	CTURE TABLE
	TOP OF GRATE				INSULATION REQUI
STRUCTURE ID	ELEVATION		INVERT IN	INVERT OUT	ON OUTLET PIPE?
SAMH1	65.92	62.70	62.64	62.64	Ν
SAMH2	65.97	62.81		62.81	Ν

				STORM STR	UCTURE TABLE
	TOP OF GRATE				INSULATION REQUIRE
STRUCTURE ID	ELEVATION		INVERT IN	INVERT OUT	ON OUTLET PIPE?
CB1	66.00			63.85	Ν
CB2	66.13			64.47	Y
STMH1	65.93	63.72	63.42	63.42	Ν
STMH2	65.96	63.78		63.78	Y
STMH3	66.03	63.80	63.80	63.80	Y
STMH4	66.22	63.94		63.94	Ν
CBMH1	66.08	64.11		64.11	Y

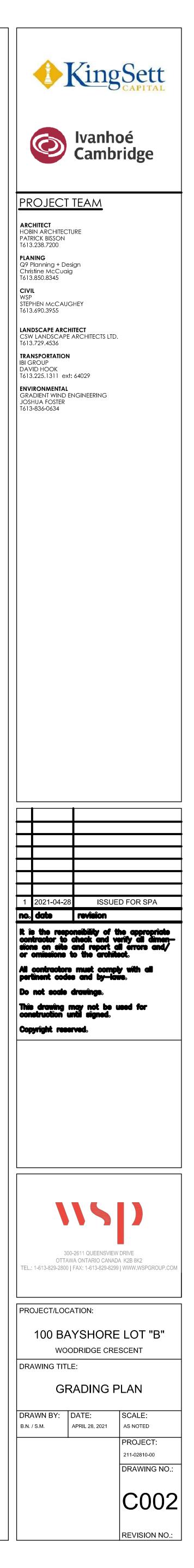
			PIPE CROS	SING TABLE		
		Obvert			Invert	
1	150mm SAN	62.88	0.50	Clearance Under	63.38	200mm Ex. WM
2	150mm WM	63.39	0.50	Clearance Under	63.89	250mm STM
3	150mm SAN	63.00	0.87	Clearance Under	63.87	250mm STM

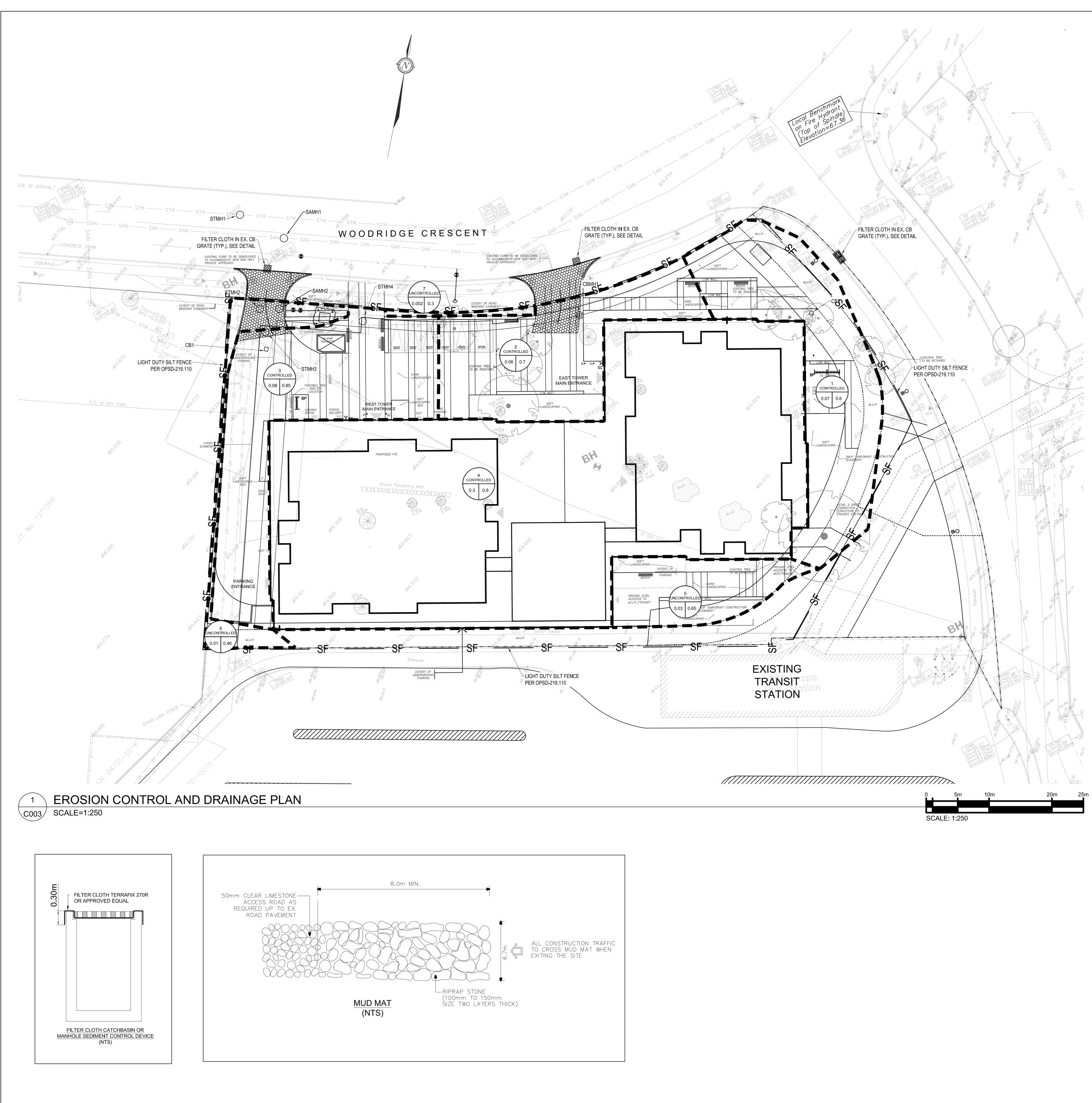
LEGEND	
★ 66.50	PROPOSED GRADE ELEVATION
$ imes rac{66.50 \mathrm{TC}}{66.35}$	PROPOSED TOP AND BOTTOM OF CURB
◯ STMH	PROPOSED STORM SEWER MANHOLE
SAMH	PROPOSED SANITARY SEWER MANHOLE
🗇 СВМН	PROPOSED CATCHBASIN MANHOLE
🗆 СВ	PROPOSED CATCHBASIN
- STM	PROPOSED STORM SEWER
- SAN	PROPOSED SANITARY SEWER
- w —	PROPOSED WATER SERVICE LINE
٢	PROPOSED VALVE BOX
∇	PROPOSED REDUCER
ራ FH	PROPOSED FIRE HYDRANT
DC	PROPOSED DEPRESSED CURB
×65.96	EXISTING GRADE ELEVATION
\otimes MH	EXISTING MANHOLE
🖗 СВ	EXISTING CATCHBASIN
ØVB	EXISTING VALVE & BOX
🗑 FH	EXISTING FIRE HYDRANT
- stm —	EXISTING STORM SEWER
- SAN	EXISTING SANITARY SEWER
- W	EXISTING WATERMAIN
- G —	EXISTING GASMAIIN





LEGEND	
★ 66.50	PROPOSED GRADE ELEVATION
$ imes rac{66.50 \mathrm{TC}}{66.35}$	PROPOSED TOP AND BOTTOM OF CURB
◯ STMH	PROPOSED STORM SEWER MANHOLE
SAMH	PROPOSED SANITARY SEWER MANHOLE
🗇 СВМН	PROPOSED CATCHBASIN MANHOLE
🗆 СВ	PROPOSED CATCHBASIN
• STM	PROPOSED STORM SEWER
· SAN ——	PROPOSED SANITARY SEWER
• W —	PROPOSED WATER SERVICE LINE
٢	PROPOSED VALVE BOX
∇	PROPOSED REDUCER
ራ FH	PROPOSED FIRE HYDRANT
DC	PROPOSED DEPRESSED CURB
×65.96	EXISTING GRADE ELEVATION
⊗ MH	EXISTING MANHOLE
🖗 СВ	EXISTING CATCHBASIN
Ø VB	EXISTING VALVE & BOX
€ FH	EXISTING FIRE HYDRANT
- STM ——	EXISTING STORM SEWER
SAN —	EXISTING SANITARY SEWER
- W	EXISTING WATERMAIN
G —	EXISTING GASMAIIN





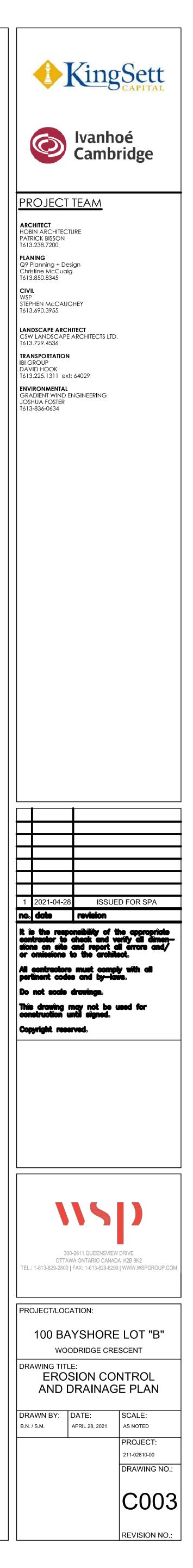
LEGEND	
★ 66.50	PROPOSED GRADE ELEVATION
$ imes rac{66.50 \mathrm{TC}}{66.35}$	PROPOSED TOP AND BOTTOM OF CURB
STMH	PROPOSED STORM SEWER MANHOLE
SAMH	PROPOSED SANITARY SEWER MANHOLE
🗇 СВМН	PROPOSED CATCHBASIN MANHOLE
🗆 СВ	PROPOSED CATCHBASIN
STM	PROPOSED STORM SEWER
SAN	PROPOSED SANITARY SEWER
— w —	PROPOSED WATER SERVICE LINE
۲	PROPOSED VALVE BOX
\bigtriangledown	PROPOSED REDUCER
ራ FH	PROPOSED FIRE HYDRANT
	PROPOSED DEPRESSED CURB
×65.96	EXISTING GRADE ELEVATION
\otimes MH	EXISTING MANHOLE
🐼 СВ	EXISTING CATCHBASIN
Ø ∨B	EXISTING VALVE & BOX
€ FH	EXISTING FIRE HYDRANT
STM	EXISTING STORM SEWER
—— SAN ——	EXISTING SANITARY SEWER
W	EXISTING WATERMAIN
G	EXISTING GASMAIIN

NOTES: <u>EROSION AND SEDIMENT CONTROL</u>

- ** CONTRACTOR IS RESPONSIBLE FOR ALL INSTALLATION, MONITORING, REPAIR AND REMOVAL OF ALL EROSION AND SEDIMENT CONTROL FEATURES. **
- PRIOR TO START OF CONSTRUCTION:
- 1.1. INSTALL SILT FENCE IN LOCATION SHOWN ON DWG C12.
- INSTALL FILTER FABRIC OR SILT SACK FILTERS IN ALL THE CATCHBASINS AND MANHOLES TO REMAIN 1.2. DURING CONSTRUCTION WITHIN THE SITE (SEE TYPICAL DETAIL). 1.3. INSPECT MEASURES IMMEDIATELY AFTER INSTALLATION.

DURING CONSTRUCTION:

- MINIMIZE THE EXTENT OF DISTURBED AREAS AND THE DURATION OF EXPOSURE AND IMPACTS TO 2.1. EXISTING GRADING.
- PERIMETER VEGETATION TO REMAIN IN PLACE UNTIL PERMANENT STORM WATER MANAGEMENT IS IN 2.2. PLACE. OTHERWISE, IMMEDIATELY INSTALL SILT FENCE WHEN THE EXISTING SITE IS DISTURBED AT THE PERIMETER.
- 2.3. PROTECT DISTURBED AREAS FROM OVERLAND FLOW BY PROVIDING TEMPORARY SWALES TO THE SATISFACTION OF THE FIELD ENGINEER. TIE-IN TEMPORARY SWALE TO EXISTING CB'S AS REQUIRED. PROVIDE TEMPORARY COVER SUCH AS SEEDING OR MULCHING IF DISTURBED AREA WILL NOT BE REHABILITATED WITHIN 30 DAYS. 2.5. INSPECT SILT FENCES, FILTER FABRIC FILTERS AND CATCH BASIN SUMPS WEEKLY AND WITHIN 24 HOURS
- AFTER A STORM EVENT. CLEAN AND REPAIR WHEN NECESSARY. 2.6. DRAWING TO BE REVIEWED AND REVISED AS REQUIRED DURING CONSTRUCTION.
- 2.7. EROSION CONTROL FENCING TO BE ALSO INSTALLED AROUND THE BASE OF ALL STOCKPILES.
- 2.8. DO NOT LOCATE TOPSOIL PILES AND EXCAVATION MATERIAL CLOSER THAN 2.5m FROM ANY PAVED SURFACE, OR ONE WHICH IS TO BE PAVED BEFORE THE PILE IS REMOVED. ALL TOPSOIL PILES ARE TO BE SEEDED IF THEY ARE TO REMAIN ON SITE LONG ENOUGH FOR SEEDS TO GROW (LONGER THAN 30 DAYS). 2.9. CONTROL WIND-BLOWN DUST OFF SITE BY SEEDING TOPSOIL PILES AND OTHER AREAS TEMPORARILY (PROVIDE WATERING AS REQUIRED AND TO THE SATISFACTION OF THE ENGINEER).
- 2.10. NO ALTERNATE METHODS OF EROSION PROTECTION SHALL BE PERMITTED UNLESS APPROVED BY THE FIELD ENGINEER. 2.11. CITY ROADWAY AND SIDEWALK TO BE CLEANED OF ALL SEDIMENT FROM VEHICULAR TRACKING AS
- REQUIRED. 2.12. DURING WET CONDITIONS, TIRES OF ALL VEHICLES/EQUIPMENT LEAVING THE SITE ARE TO BE SCRAPED. 2.13. ANY MUD/MATERIAL TRACKED ONTO THE ROAD SHALL BE REMOVED IMMEDIATELY BY HAND OR RUBBER TIRE LOADER.
- 2.14. TAKE ALL NECESSARY STEPS TO PREVENT BUILDING MATERIAL, CONSTRUCTION DEBRIS OR WASTE BEING SPILLED OR TRACKED ONTO ABUTTING PROPERTIES OR PUBLIC STREETS DURING CONSTRUCTION AND PROCEED IMMEDIATELY TO CLEAN UP ANY AREAS SO AFFECTED.
- 2.15. ALL EROSION CONTROL STRUCTURE TO REMAIN IN PLACE UNTIL ALL DISTURBED GROUND SURFACES HAVE BEEN STABILIZED EITHER BY PAVING OR RESTORATION OF VEGETATIVE GROUND COVER. 2.16. THE CONTRACTOR SHALL IMPLEMENT BEST MANAGEMENT PRACTICES, TO PROVIDE FOR PROTECTION OF
- THE AREA DRAINAGE SYSTEM AND THE RECEIVING WATERCOURSE, DURING CONSTRUCTION ACTIVITIES. THE CONTRACTOR ACKNOWLEDGES THAT FAILURE TO IMPLEMENT APPROPRIATE EROSION AND SEDIMENT CONTROL MEASURES MAY BE SUBJECT TO PENALTIES IMPOSED BY ANY APPLICABLE REGULATORY AGENCY.



E STORM SEWER DESIGN SHEET

Lot-B Residential Development, 100 Bayshore Dr. Ottawa, ON Project No. 211-02810-00 Ivanhoé Cambridge Inc.

WSP Canada Storm Sewer Design Sheet

	LOCATION							FLOW							PIPE				MAN	HOLE
Catchment Area	FROM MH	TO MH	Coefficient	Area (m2)	Indiv. 2.78*AC	Cum. 2.78*AC	Time of Conc. (min.)	Rainfall Intensity (mm.hr)	Indiv. Area Flow (L/s)	Cum. Flow (L/s)	Controlled Cum. Flow (L/s)	Length (m)	Dia. (mm)	Slope (%)	Cap. (Full) (L/s)	Velocity (Full) (m/s)	Time of flow (min.)	Ratio (Q/Qfull)	UP INVERT (m)	DOWN INVERT (m)
1	CB2	CBMH1	0.6	687	0.115	0.115	10.00	76.81	8.80	8.80	8.80	36.40	250	0.99%	59.14	1.2	0.50	15%	64.47	64.11
4	BLDG*	CBMH1	0.9	3000	0.751	0.751	10.00	76.81	57.65	57.65	57.65	1.50	300	2.67%	157.91	2.2	0.01	37%	64.15	64.11
2	CBMH1	STMH4	0.7	575	0.112	0.977	10.07	76.55	8.57	74.79	74.79	34.50	250	0.49%	41.74	0.9	0.68	179%	64.11	63.94
	STMH4	STMH3	0.0	0	0.000	0.977	10.74	74.06	0.00	72.37	72.37	15.60	250	0.51%	42.59	0.9	0.30	170%	63.94	63.86
3	CB1	STMH3	0.9	791	0.187	0.187	10.00	76.81	14.36	14.36	14.36	2.70	200	2.22%	48.89	1.6	0.03	29%	63.86	63.80
	STMH3**	STMH2	0.0	0	0.000	1.164	10.88	73.58	0.00	85.65	16.20	3.80	375	0.53%	127.20	1.2	0.05	13%	63.80	63.78
	STMH2***	STMH1	0.0	0	0.000	1.164	10.94	73.39	0.00	85.43	16.20	15.30	375	0.39%	109.80	1.0	0.26	15%	63.78	63.72
		[DESIGN PAR	AMETERS				Designed:							PROJEC	:T:				
Q = 2.78CIA where	э,		Ottawa IDF	Curve										400						
Q = Peak flow in L	/s		IDF Curve E	quation (2y	r storm)				Stephen McCa	augney, P.Eng.				100	Bayshore	Lot "B"				
A = Drainage area	in ha		l = 732.951/	(T+6.199)^0).81			Checked:							LOCATIC	N:				
I = Rainfall intensity	y (mm/hr)		Min. velocity	= 0.8 m/s																
C = Runoff coeffici	ient		Manning 'n'	= 0.013					James John	ston, P.Eng.				100 Bay	shore Lot	"B", Ottaw	/a			
			5					Dwg. Reference:				File Ref.:				Date:		Sheet No.		
																April 202	!1	1 of 1		

Note: * Underground storage in building footprint ** ICD on STMH3 outlet controlled to 16.2 L/s *** Oil Grit Separator

201-02810-00

201-02810-00	
201-02810-00	

	LOCATION							FLOW							PIPE				MAN	HOLE
Catchment Area	FROM MH	ТО МН	Coefficient	Area (m2)	Indiv. 2.78*AC	Cum. 2.78*AC	Time of Conc. (min.)	Rainfall Intensity (mm.hr)	Indiv. Area Flow (L/s)	Cum. Flow (L/s)	Controlled Cum. Flow (L/s)	Length (m)	Dia. (mm)	Slope (%)	Cap. (Full) (L/s)	Velocity (Full) (m/s)	Time of flow (min.)	Ratio (Q/Qfull)	UP INVERT (m)	DOWN INVERT (m)
	0.50	001414		007	0.440	0.440	40.00	170.50	05.50	05.50	05.50	00.40	050	0.000/	50.44	1.0	0.50	100/	04.47	
1	CB2 BLDG*	CBMH1 CBMH1	0.8	687 3000	0.143	0.143	10.00	178.56 178.56	25.58 148.92	25.58 148.92	25.58 148.92	36.40 1.50	250 300	0.99%	59.14 157.91	1.2	0.50	43% 94%	64.47 64.15	64.11 64.11
4	CBMH1	STMH4	1.0 0.9	575	0.834	1.117	10.00	178.56	24.88	148.92	148.92	34.50	250	2.67% 0.49%	41.74	0.9	0.01	94% 476%	64.15	63.94
2	STMH4	STMH4 STMH3	0.9	0	0.140	1.117													-	
				-			10.75	171.99	0.00	192.13	192.13	15.60	250	0.51%	42.59	0.9	0.30	451%	63.94	63.86
3	CB1	STMH3	1.0	791	0.220	0.220	10.00	178.56	39.26	39.26	39.26	2.70	200	2.22%	48.89	1.6	0.03	80%	63.86	63.80
	STMH3**	STMH2	0.0	0	0.000	1.337	10.88	170.89	0.00	228.48	16.20	3.80	375	0.53%	127.20	1.2	0.05	13%	63.80	63.78
	STMH2***	STMH1	0.0	0	0.000	1.337	10.94	170.43	0.00	227.87	16.20	15.30	375	0.39%	109.80	1.0	0.26	15%	63.78	63.72
		[DESIGN PAR	AMETERS				Designed:							PROJEC	T:				
Q = 2.78CIA when	e,		Ottawa IDF	Curve																
Q = Peak flow in L	/s		IDF Curve E	quation (10))vr storm)				Stephen McCa	iughey, P.Eng.				100	Bayshore	Lot "B"				
A = Drainage area			I = 1735.688					Checked:							LOCATIO	N:				
I = Rainfall intensit	ty (mm/hr)		Min. velocity	= 0.8 m/s					James John	ston P Eng				100 Bay	shore I of '	"B", Ottaw	9			
C = Runoff coefficient Manning 'n' = 0.013										100 Day	SHOLE FOR	D, Ollaw	u							
								Dwg. Reference:				File Ref.:				Date:		Sheet No.		
																April 202	1	1 of 1		

Note: * Underground storage in building footprint ** ICD on STMH3 outlet controlled to 16.2 L/s *** Oil Grit Separator

201-02810-00	
201-02810-00	

	LOCATION							FLOW							PIPE				MAN	HOLE
Catchment Area	FROM MH	ТО МН	Coefficient	Area (m2)	Indiv. 2.78*AC	Cum. 2.78*AC	Time of Conc. (min.)	Rainfall Intensity + 20% (mm.hr)	Indiv. Area Flow (L/s)	Cum. Flow (L/s)	Controlled Cum. Flow (L/s)	Length (m)	Dia. (mm)	Slope (%)	Cap. (Full) (L/s)	Velocity (Full) (m/s)	Time of flow (min.)	Ratio (Q/Qfull)	UP INVERT (m)	DOW INVEF (m)
1	CB2	CBMH1	0.8	687	0.143	0.143	10.00	214.27	30.69	30.69	30.69	36.40	250	0.99%	59.14	1.2	0.50	52%	64.47	64.11
4	BLDG*	CBMH1	1.0	3000	0.834	0.834	10.00	214.27	178.70	178.70	178.70	1.50	300	2.67%	157.91	2.2	0.00	113%	64.15	64.1
2	CBMH1	STMH4	0.9	575	0.140	1.117	10.07	213.47	29.86	238.47	238.47	34.50	250	0.49%	41.74	0.9	0.68	571%	64.11	63.94
	STMH4	STMH3	0.0	0	0.000	1.117	10.75	206.39	0.00	230.56	230.56	15.60	250	0.51%	42.59	0.9	0.30	541%	63.94	63.86
3	CB1	STMH3	1.0	791	0.220	0.220	10.00	214.27	47.12	47.12	47.12	2.70	200	2.22%	48.89	1.6	0.03	96%	63.86	63.80
	STMH3**	STMH2	0.0	0	0.000	1.337	10.88	205.06	0.00	274.17	16.20	3.80	375	0.53%	127.20	1.2	0.05	13%	63.80	63.78
	STMH2***	STMH1	0.0	0	0.000	1.337	10.94	204.52	0.00	273.44	16.20	15.30	375	0.39%	109.80	1.0	0.26	15%	63.78	63.72
			DESIGN PAR	AMETERS				Designed:							PROJEC	T:				
Q = 2.78CIA where Q = Peak flow in L	,		Ottawa IDF)yr storm)				Stephen McCa	aughey, P.Eng.				100	Bayshore	Lot "B"				
A = Drainage area	in ha		l = 1735.688	/(T+6.014)^	0.82			Checked:							LOCATIC	DN:				
I = Rainfall intensity (mm/hr) Min. velocity = 0.8 m/s C = Runoff coefficient Manning 'n' = 0.013			James Johnston, P.Eng.				100 Bayshore L			shore Lot	ot "B", Ottawa									
			°,					Dwg. Reference:				File Ref.:				Date:		Sheet No.		
																April 202	1	1 of 1		

Note: * Underground storage in building footprint ** ICD on STMH3 outlet controlled to 16.2 L/s *** Oil Grit Separator

WSP Canada

CORRESPONDENCES

Lot-B Residential Development, 100 Bayshore Dr. Ottawa, ON Project No. 211-02810-00 Ivanhoé Cambridge Inc.

McCaughey, Stephen

Subject:
Attachments:

FW: Pre-Consultation Follow-Up: 100 Bayshore Drive Plans & Study List.pdf; design_brief_TOR_100 Bayshore.pdf

From: "McCreight, Laurel" <Laurel.McCreight@ottawa.ca>
Date: March 3, 2021 at 9:55:19 AM EST
To: Christine McCuaig <christine@q9planning.com>
Subject: Pre-Consultation Follow-Up: 100 Bayshore Drive

Hi Christine,

Please refer to the below regarding the Pre-Application for 100 Bayshore Drive for a Site Plan Control Application for a residential development containing two high-rise towers. I have also attached the required Plans & Study List for application submission.

Below are staff's preliminary comments based on the information available at the time of the preconsultation meeting:

Planning / Urban Design

- A Design Brief is required for the site plan control application. The Terms of Reference is attached for convenience.
 - Please note a secondary wind study is required for the application. Please refer to the <u>Terms of Reference of the wind study</u> for details.
 - The preliminary wind study prepared for the OPA and rezoning identifies a number of areas that will experience rather windy conditions.
 - The detailed design should respond and mitigate such conditions to the extent possible.
 - The secondary wind study should confirm the adequacy of the design measures.
- The site is not within a Design Priority Area. However, as identified in the zoning exception, the applicant is required to visit the Urban Design Review Panel (UDRP) for formal approval.
- Please contact <u>udrp@ottawa.ca</u> for any questions regarding UDRP.
- Regarding the detailed design:
 - Please investigate possible architectural and landscaping measures to mitigate wind impacts/improve conditions in the public realm as well as at the roof top patio.
 - Some refined sculpting at the building corners and Tower A may be helpful.
 - The front yard of the site should be designed as a welcoming pedestrian forecourt through landscaping details where vehicular functions are accommodated but not dominating.
 - Considerations should be given to paving the entire area with interlocks, using depressed curbs, and locating parking only on one side of the central pedestrian walkway.
 - The entrances of both towers should be treated equally within the pedestrian forecourt through landscape design.
 - Please provide details of the parking lot screens.
 - Considerations may be given to refining the building facades to display some commercial characteristics.
 - Considerations should be given to exterior lighting.
- Cash-in-lieu of Parkland will be required.
- Please consult the new <u>Draft Official Plan</u> for emerging directions.

- Please refer to the recently approved <u>Bird-Friendly Design Guidelines</u>.
- LRT Proximity Study Confirm details with File Lead prior to application submission. In process of reviewing Stage 2 requirements.
- You are encouraged to contact the Ward Councillor, Councillor <u>Theresa Kavanagh</u>, about the proposal.
 - It is recommended to reach out to the Councillor to discuss the working group as required per the direction of Council.
 - I would be happy to attend this meeting as well.

Engineering

• All exterior light fixtures must be included and approved as part of the site plan approval. Therefore, the lights must be clearly identified by make, model and part number. All external light fixtures must meet the criteria for full cut-off classification as recognized by the Illuminating Engineering Society of North America (IESNA or IES), and must result in minimal light spillage onto adjacent properties (as a guideline, 0.5 fc is normally the maximum allowable spillage). In order to satisfy these criteria, the applicant must provide certification from an acceptable professional engineer. The location of all exterior fixtures, a table showing the fixture types (including make, model, part number), and the mounting heights must be included on a plan

Servicing and site works shall be in accordance with the following documents:

Ottawa Sewer Design Guidelines (October 2012)

Ottawa Design Guidelines - Water Distribution (2010)

Geotechnical Investigation and Reporting Guidelines for Development Applications in the City of Ottawa (2007)

City of Ottawa Slope Stability Guidelines for Development Applications (revised 2012) City of Ottawa Environmental Noise Control Guidelines (January, 2016)

City of Ottawa Park and Pathway Development Manual (2012)

City of Ottawa Accessibility Design Standards (2012)

Ottawa Standard Tender Documents (latest version)

Ontario Provincial Standards for Roads & Public Works (2013)

Record drawings and utility plans are also available for purchase from the City (Contact the City's Information Centre by email at <u>InformationCentre@ottawa.ca</u> or by phone at (613) 580- 2424 x.44455).

The Stormwater Management Criteria, for the subject site, is to be based on the following: The IDF information derived from the Meteorological Services of Canada rainfall data,

taken from the MacDonald Cartier Airport, collected 1966 to 1997.

The existing storm system in the RoW was built pre-1970, as such the post-development peak flow rate for storm events up to and including the 100 year event will need to be controlled to the 2 year pre-development storm event. Runoff will need to be detained onsite to control all storm events, up to and including the 100 year event, with an allowable release rate calculated based on the peak flow for the predevelopment 2 year event.

The pre-development runoff coefficient or a maximum equivalent 'C' of 0.5, whichever is less (§ 8.3.7.3).

A calculated time of concentration (cannot be less than 10 minutes).

Redevelopment will be expected to provide water quality protection at an enhanced level (minimum 80% TSS removal), as per the RVCA.

The proposed sanitary flows need to be provided to the City to confirm capacity / identify the impact on the downstream West Nepean Collector.

Deep Services (Storm, Sanitary & Water Supply)

- Provide existing servicing information and the recommended location for the proposed connections. Services should ideally be grouped in a common trench to minimize the number of road cuts.
- Connections to trunk sewers and easement sewers are typically not permitted.
- Provide information on the monitoring manhole requirements should be located in an accessible location on private property near the property line (ie. Not in a parking area).
- Review provision of a high-level sewer.
- Provide information on the type of connection permitted
 - Sewer connections to be made above the springline of the sewermain as per:
 - Std Dwg S11.1 for flexible main sewers connections made using approved tee or wye fittings.
 - Std Dwg S11 (For rigid main sewers) lateral must be less that 50% the diameter of the sewermain,
 - Std Dwg S11.2 (for rigid main sewers using bell end insert method) for larger diameter laterals where manufactured inserts are not available; lateral must be less that 50% the diameter of the sewermain,
 - Connections to manholes permitted when the connection is to rigid main sewers where the lateral exceeds 50% the diameter of the sewermain. – Connect obvert to obvert with the outlet pipe unless pipes are a similar size.

No submerged outlet connections.

Please refer to ISDTB – 2014-2: individual residential facilities with a basic day demand greater than 50 m3/day shall be connected with a minimum of two water services, separated by an isolation valve, to avoid the creation of a vulnerable service area.

Water Boundary condition requests must include the location of the service and the expected loads required by the proposed development. Please provide the following information:

- Location of service
- Type of development and the amount of fire flow required (as per FUS, 1999).
- Average daily demand: _____l/s.
- Maximum daily demand: ____l/s.
- Maximum hourly daily demand:_____l/s.
- Note that if Accora Village is proposed to re-develop in its entirety, the proponent may be required to (or may consider) modelling the loop along Woodridge Crescent to provide sub-division level details above.

Phase 1 ESAs and Phase 2 ESAs must conform to clause 4.8.4 of the Official Plan that requires that development applications conform to Ontario Regulation 153/04.

Please refer to Ontario Regulation 153/04:

"the date the last work on all of the records review, interviews and site reconnaissance required for the phase one environmental site assessment that is the subject of the report was done is no later than 18 months before the submission of the record of site condition or the commencement of the phase two environmental site assessment" and "the date the last work on all of the planning the site investigation, conducting the site investigation and reviewing and evaluating the information gathered through the site investigation required for the phase two environmental site assessment that is the subject of the report was done is no later than 18 months before the submission of the record of site condition or the commencement of the risk assessment".

MOECC ECA Requirements

- Please note that an ECA is not required for zoning amendment however the following applies to the Site Plan Control process:
- An MOECC Environmental Compliance Approval (Municipal/Private Sewage Works) will be required for the proposed development where the storm sewer network is designed to service more than one lot or parcel of land. The proposed development boundary appears to include two parcels of land.
- Although not required for the rezoning amendment, please note that for Site Plan Control, there is an existing public STM sewer running through the site. Please identify the easement associated with this sewer and provide details of how this will be taken into consideration in the proposed design.
- Although not required for the rezoning amendment, please note that for Site Plan Control, please ensure that all easements within the property and adjacent to the subject property are identified on the drawing set and please provide details for all easements identified.

Please contact Infrastructure Project Manager <u>Ahmed Elsayed</u> for follow-up questions.

Transportation

- Please submit an addendum/memo to the Transportation Impact Assessment previously provided.
- A noise study is required.

Please contact Transportation Project Manager, <u>Mike Giampa</u> for follow-up questions.

Other

Please refer to the links to "<u>Guide to preparing studies and plans</u>" and <u>fees</u> for general information. Additional information is available related to <u>building permits</u>, <u>development charges</u>, <u>and the</u> <u>Accessibility Design Standards</u>. Be aware that other fees and permits may be required, outside of the development review process. You may obtain background drawings by contacting <u>informationcentre@ottawa.ca</u>.

These pre-consultation comments are valid for one year. If you submit a development application(s) after this time, you may be required to meet for another pre-consultation meeting and/or the submission requirements may change. You are as well encouraged to contact us for a follow-up meeting if the plan/concept will be further refined.

Please do not hesitate to contact me if you have any questions.

Regards, Laurel

Laurel McCreight MCIP, RPP

Planner Development Review West Urbaniste Examen des demandes d'aménagement ouest City of Ottawa | Ville d'Ottawa

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613.580.2424 ext./poste 16587 ottawa.ca/planning / ottawa.ca/urbanisme

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Description:

A Design Brief is the core submission document that illustrates how the development is designed to work with its existing and planned context, to improve its surroundings and also demonstrate how the proposal supports the overall goals of the Official Plan, relevant secondary plans, Council approved plans and design guidelines. The purpose of the Terms of Reference is to assist the applicant to organize and substantiate the design justification in support of the proposed development and to assist staff and the public in the review of the proposal.

Authority to Request a Design Brief:

The *Planning Act* gives municipalities the authority to require that a Design Brief be prepared. Under Sections 22(4), (5) and Section 41(4) of the *Planning Act*, a Council has the authority to request such other information or material that the authority needs in order to evaluate and make a decision on an application. Section 5.2.6 of the Official Plan sets out the general requirement for a Design Brief.

Preparation:

The Design Brief should be signed by an urban designer, licenced architect, landscape architect, or a full member of the Canadian Institute of Planners.

When Required:

A Design Brief is required for a Site Plan Control planning application.

A Scoped Design Brief* is required when the following planning applications are applied for and not accompanied by a Site Plan Control application:

- Official Plan Amendment
- Zoning By-law Amendment (exception: a change in use which does not result in an increase in height or massing)

The requirement and scope of a Design Brief will be determined at the formal pre-application consultation meeting. Should an application be required to go to the <u>Urban Design Review Panel (UDRP)</u>, the Design Brief may be submitted as part of the submission materials to the panel.

Contents for Design Brief Submissions:

A Design Brief will contain and/or address the points identified during the pre-consultation meeting. Failure to address the critical elements identified in the pre-consultation meeting may result in the application being considered incomplete.

* A Scoped Design Brief is composed of:

- Section 1 should be combined into the Planning Rationale submission, and
- Section 2 items will be confirmed in the pre-application consultation meeting.



SECTION 1 Note: This section will be combined with the Planning Rationale report.

Applicati Not Requ	on Submission: ired Required	State the: type of application, legal description, municipal address, purpose of the application and provide an overall vision statement and goals for the proposal.
<u>Respons</u> Not Requ	se to City Documen uired Required X	ts: State the Official Plan land use designation for the subject property and demonstrate how the proposal conforms to the Official Plan as it relates to the design of the subject site. Reference specific policy numbers from the Official Plan to show consistency. Justify areas of non-compliance and explain why there is non-compliance.
	X	State the applicable plans which apply to the subject proposal: community design plan, secondary plan, concept plan and design guideline. Reference the relevant design related polices within the applicable plans/guidelines and provide a comprehensive analysis as to how the proposed development incorporates the objectives or why it does not incorporate the objectives.
Context Not Requ Note: Although zoning has a approved, it is still use broader area context i submission, including connections, parks an and different uses.	already been oful include a n the pedestrian	Provide a contextual analysis that discusses/illustrates abutting properties, key destinations and linkages within a 100 meter radius (a larger radius may be requested for larger/more complex projects), such as transit stations, transportation networks for cars, cyclists, and pedestrians, focal points/nodes, gateways; parks/open spaces, topography, views towards the site, the urban pattern (streets, blocks), future and current proposals (if applicable), public art and heritage resources. Photographs to illustrate existing site conditions and surrounding contexts. Include a map pinpointing (with numbers) where each photo is taken and correspond these numbers with the site photos. Arrows illustrating the direction the photo is taken is also useful.



SECTION 2

Design Proposal:

The purpose of the Design Proposal is to show the building elevations, exterior details, transitions in form, treatment of the public realm and compatibility with adjacent buildings, using 3-D models, illustrations, diagrams, plans, and cross sections. Referencing Official Plan, Section 5.2.1, as determined at time of pre-application consultation meeting, submissions will need to address the following in the form of labelled graphics and written explanation:

Massing and Sca Not Required	a le Required	
	 	 Images which show: Building massing – from: at least two sides set within it current context (showing the entire height and width of the building) OR all four sides set within it current context (showing the entire height and width of the building).
	×	 <u>Views</u> – of the entire block, from: at least two perspectives to show how the proposed building is set within its current context OR all four perspectives to show how the proposed building is set within its current context.
	X	<u>Building transition</u> – to adjacent uses, with labelled explanation of the transition measures used.
	×	<u>Grading</u> – if grades are an issue.
	X	<u>Alternative building massing</u> – additional imagery and site layouts considered and provide justification for the ultimate proposal sought.
Public Realm Not Required	Required	Labelled graphics and a written explanation which show:
	X	<u>Streetscape</u> – cross sections which illustrate the street design and right of way (referencing the City's design manuals).
	X	 <u>Relationship to the public realm</u> – illustrating how the first few storeys of the proposed development responds to and relates to the existing context (e.g. through a podium plan and first floor plan). This is to include detailed explanation on: Architectural responses Landscaping details Public art features (in accordance with Official Plan, Section 4.11) For developments in Design Priority Areas, detail the building and site features, (in accordance with Official Plan, Section 4.11) which will enhance the public realm. Provide explanation for features which are not provided.



Building Design Not Required	Required X	Labelled graphics (e.g. building elevations and floor plans) and a written explanation which document the proposed exterior architectural details and design (in accordance with Official Plan, Section 5.2.1).
	X	For high-rise development applications, detail the building design and massing and scale elements and how they relate to the proposed high-rise development (in accordance with Official Plan, Section 5.2.1).
Sustainability Not Required	Required X	Any sustainable design features to be incorporated, such as green roofs or walls, sun traps, reflective or permeable surfaces.
Heritage Not Required	Required	How the building relates to the historic details, materials, site and setting of any existing historic resources on or adjacent to the subject property (if applicable).

Additional Contents:

Some proponents may be requested to provide submission material which complements the Design Brief. These additional requirements could be incorporated into the Design Brief submission for ease of review. These will be identified at the time of application consultation meeting:

- X Site Plan
- X Landscape Plan
- X Plan showing existing and proposed servicing
- X Shadow Analysis
- **x** Wind Analysis

Submission Requirements

• Six hard copies and one digital copy



APPLICANT'S STUDY AND PLAN IDENTIFICATION LIST

S indicates that the study or plan is required with application submission. Legend: A indicates that the study or plan may be required to satisfy a condition of approval/draft approval.

For information and guidance on preparing required studies and plans refer here:

S/A	Number of copies	ENG	SINEERING	S/A	Number of copies
S	<mark>3</mark>	1. Site Servicing Plan	2. Site Servicing Study	S	<mark>3</mark>
S	<mark>3</mark>	3. Grade Control and Drainage Plan	4. Geotechnical Study	S	<mark>3</mark>
	2	5. Composite Utility Plan	6. Groundwater Impact Study		3
	3	7. Servicing Options Report	8. Wellhead Protection Study		3
S	<mark>4</mark>	9. Transportation Impact Assessment (TIA)	10. Erosion and Sediment Control Plan	S	<mark>3</mark>
S	<mark>3</mark>	11.Storm water Management Report	12.Hydro geological and Terrain Analysis		3
S	3	13.Water Main Protection and Contingency Plan	14.Noise and vibration Study	S	<mark>3</mark>
	PDF only	15.Roadway Modification Functional Design	16.LRT Proximity Study	S	<mark>3</mark>

S/A	Number of copies	PLANNING	/ DESIGN / SURVEY	S/A	Number of copies
	15	17.Draft Plan of Subdivision	18.Plan Showing Layout of Parking Garage	S	<mark>2</mark>
	5	19.Draft Plan of Condominium	20.Planning Rationale	<mark>0</mark>	<mark>3</mark>
S	<mark>10</mark>	21.Site Plan	22.Minimum Distance Separation (MDS)		3
	15	23.Concept Plan Showing Proposed Land Uses and Landscaping	24.Agrology and Soil Capability Study		3
	3	25.Concept Plan Showing Ultimate Use of Land	26.Cultural Heritage Impact Statement		3
S	3	27.Landscape Plan	28.Archaeological Resource Assessment Requirements: S (site plan) A (subdivision, condo)		3
S	<mark>1</mark>	29.Survey Plan	30.Shadow Analysis	S	<mark>3</mark>
S	3	31.Architectural Building Elevation Drawings (dimensioned)	32.Design Brief (includes the Design Review Panel Submission Requirements)	S	<mark>Available</mark> online
<mark>s</mark>	3	33.Wind Analysis			

S/A	Number of copies	ENV	IRONMENTAL	S/A	Number of copies
S	<mark>3</mark>	34.Phase 1 Environmental Site Assessment	35.Impact Assessment of Adjacent Waste Disposal/Former Landfill Site		3
S	<mark>3</mark>	36.Phase 2 Environmental Site Assessment (depends on the outcome of Phase 1)	37.Assessment of Landform Features		3
S	3	38.Record of Site Condition (condition of Site Plan)	39.Mineral Resource Impact Assessment		3
	3	40.Tree Conservation Report	41.Environmental Impact Statement / Impact Assessment of Endangered Species		3
	3	42.Mine Hazard Study / Abandoned Pit or Quarry Study	43.Integrated Environmental Review (Draft, as part of Planning Rationale)		3

S/A	Number of copies	ADDITION	S/A	Number of copies	
<mark>s</mark>	1	44. Applicant's Public Consultation Strategy (may be provided as part of the Planning Rationale)	45. Site Lighting Plan & Certificate	<mark>s</mark>	1

Meeting Date: February 17, 2021

Application Type: Site Plan Control

File Lead (Assigned Planner): Laurel McCreight

Infrastructure Approvals PM: Ahmed Elsayed

Site Address (Municipal Address): 100 Bayshore Drive *Preliminary Assessment: 1 2 3 4 5

*One (1) indicates that considerable major revisions are required before a planning application is submitted, while five (5) suggests that proposal appears to meet the City's key land use policies and guidelines. This assessment is purely advisory and does not consider technical aspects of the proposal or in any way guarantee application approval.

It is important to note that the need for additional studies and plans may result during application review. If following the submission of your application, it is determined that material that is not identified in this checklist is required to achieve complete application status, in accordance with the Planning Act and Official Plan requirements, the Planning, Infrastructure and Economic Development Department will notify you of outstanding material required within the required 30 day period. Mandatory pre-application consultation will not shorten the City's standard processing timelines, or guarantee that an application will be approved. It is intended to help educate and inform the applicant about submission requirements as well as municipal processes, policies, and key issues in advance of submitting a formal development application. This list is valid for one year following the meeting date. If the application is not submitted within this timeframe the applicant must again preconsult with the Planning, Infrastructure and Economic Development Department.

> 110 Laurier Avenue West, Ottawa ON K1P 1J1 110, av. Laurier Ouest, Ottawa (Ontario) K1P 1J1 Courrier interne : 01-14

Mail code: 01-14

Visit us: Ottawa.ca/planning Visitez-nous : Ottawa.ca/urbanisme

McCaughey, Stephen

From:	Elsayed, Ahmed <ahmed.elsayed@ottawa.ca></ahmed.elsayed@ottawa.ca>
Sent:	Monday, March 15, 2021 10:20 AM
То:	McCaughey, Stephen
Cc:	McCreight, Laurel
Subject:	RE: 100 Bayshore Drive - Inquiries for Site Plan Application

Hi Stephen,

Thanks for your follow up, about the Sanitary, there is no issue with the flows shown below, as for water, it takes 10 business days for IPU to get to us.

I will keep you posted.

Ahmed

From: McCaughey, Stephen <Stephen.Mccaughey@wsp.com>
Sent: Monday, March 15, 2021 9:38 AM
To: Elsayed, Ahmed <ahmed.elsayed@ottawa.ca>
Cc: McCreight, Laurel <Laurel.McCreight@ottawa.ca>
Subject: FW: 100 Bayshore Drive - Inquiries for Site Plan Application

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ATTENTION : Ce courriel provient d'un expéditeur externe. Ne cliquez sur aucun lien et n'ouvrez pas de pièce jointe, excepté si vous connaissez l'expéditeur.

Hi Ahmed,

Just touching base from my inquiry last Monday, are there any questions or further information you need for water boundary conditions and sanitary capacity?

Thank you,

Stephen McCaughey, P.Eng. T +1 613-690-3955 (Direct) T +1 613-829-2800 (Office)

wsp

From: McCaughey, Stephen
Sent: Monday, March 08, 2021 2:38 PM
To: <u>ahmed.elsayed@ottawa.ca</u>
Subject: 100 Bayshore Drive - Inquiries for Site Plan Application

Hi Ahmed,

Wanted to inquire regarding civil servicing capacity for this 100 Bayshore Dr. site we had a pre-consultation meeting with Laurel McCreight on.

Water Boundary condition requests must include the location of the service and the expected loads required by the proposed development. Please provide the following information:

Location of service see attached (note conceptual servicing using older architectural site plan for reference, proposed location of services however is still valid)

Type of development and the amount of fire flow required (as per FUS, 1999). 8,000 L/min (133 L/s) based on letter from the Architect confirming fire resistive construction. This justification was previously presented for the site with the rezoning application.

Average daily demand: <u>2.86</u>/s. Maximum daily demand: <u>7.15</u>/s. Maximum hourly daily demand: <u>15.72</u>/s.

The proposed sanitary flows need to be provided to the City to confirm capacity / identify the impact on the downstream West Nepean Collector. Peak sanitary 9.92 L/s

Thank you and let me know if there are any questions,

Stephen McCaughey, P.Eng. Project Engineer Municipal Infrastructure

wsp

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McCaughey, Stephen

From:	Elsayed, Ahmed <ahmed.elsayed@ottawa.ca></ahmed.elsayed@ottawa.ca>
Sent:	Tuesday, March 16, 2021 12:25 PM
То:	McCaughey, Stephen
Cc:	McCreight, Laurel
Subject:	RE: 100 Bayshore Drive - Inquiries for Site Plan Application
Attachments:	100 Bayshore March 2021.pdf

Hi Stephen,

Hereunder are the BC as received from IPU.

The following are boundary conditions, HGL, for hydraulic analysis at 100 Bayshore (zone 1W) assumed to be connected to the 203 mm on Bayshore Ave (see attached PDF for location). Minimum HGL = 106.3 m Maximum HGL = 115.2 m Max Day + Fire Flow (133 L/s) = 82.5 m These are for current conditions and are based on computer model simulation. *Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation.*

Please let me know if you have any questions.

Ahmed

From: McCaughey, Stephen <Stephen.Mccaughey@wsp.com>
Sent: Monday, March 15, 2021 9:38 AM
To: Elsayed, Ahmed <ahmed.elsayed@ottawa.ca>
Cc: McCreight, Laurel <Laurel.McCreight@ottawa.ca>
Subject: FW: 100 Bayshore Drive - Inquiries for Site Plan Application

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Hi Ahmed,

Just touching base from my inquiry last Monday, are there any questions or further information you need for water boundary conditions and sanitary capacity?

Thank you,

