



Stormwater Management Report and Site Servicing Brief

Proposed 3-Storey Apartment Building
1465 Morisset Avenue
Ottawa, Ontario

Prepared for:

Concorde Properties
408 Tweedsmuir Ave
Ottawa, ON
K1Z 5N5

Attention: Mr. Jordan Tannis

LRL File No.: 200572

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1 INTRODUCTION AND SITE DESCRIPTION

LRL Associates Ltd. was retained by Concorde Properties to complete a Stormwater Management Analysis and Site Servicing Study for a proposed three (3) storey residential development located at 1465 Morisset Avenue in Ottawa, Ontario. The property is legally described as Lot 230-238, Registered Plan 327, City of Ottawa, refer to Survey included in Appendix F. The location of the proposed development can be viewed in Figure 1 below.



Figure 1: Aerial View of Proposed Development

The proposed development has been previously submitted for Site Plan Control (Application file number: D07-12-21-0091 & Plan No:18532) and it is understood that a Site Plan Application was previously approved. However, a notable revision to the architectural Site Plan has occurred. As a result, the stormwater management report and site servicing design has been revised accordingly and now being submitted for a Site Plan Amendment application.

The proposed new apartment building will have a footprint of 563 m² and consist of 31 units (16x1-bedroom and 15x2-bedroom apartments). The site will also encompass a paved parking area in the eastern portion of the lot. The proposed development will have one vehicular entrance with a depressed sidewalk on Morisset Avenue and one pedestrian main entrance via a pathway to Morisset Ave.

This report has been prepared in consideration of the terms and conditions noted above and with the civil drawings prepared for the proposed new development. Should there be any changes in the design features, which may relate to the stormwater management and servicing design considerations, LRL Associates Ltd. should be advised to review the report recommendations.



2 EXISTING SITE AND DRAINAGE DESCRIPTION

The portion of land to be developed has a rectangular shape with a frontage of approximately 61 m along Morisset Avenue and a depth of approximately 30.7 m. With these dimensions, the property has a surface area of approximately 0.19 ha. The property is surrounded with residential buildings to the west and north, parking lot in the east, and Morisset Ave in the south. Currently, the proposed site is a parking lot which is being used by the apartment building in the east of the site. The existing parking lot will be demolished prior to development.

Along the west face of the existing site is an impervious asphalt pavement driveway with a retaining wall. Along the north side of the existing site is a small landscape area separated by a fence. Overland stormwater from the existing parking lot generally flow uncontrolled towards the low-lying area in the north and in the eastern portion of the parking lot which will eventually drains onto Morisset Ave.

3 SCOPE OF WORK

As per applicable guidelines, the scope of work includes the following:

Stormwater management

- Calculate the allowable stormwater release rate.
- Calculate the anticipated post-development stormwater release rates.
- Demonstrate how the target quantity objectives will be achieved.

Water services

- Calculate the expected water supply demand at average and peak conditions.
- Calculate the required fire flow as per the Ontario Building Code (OBC) method.
- Confirm the adequacy of water supply and pressure during peak flow and fire flow.
- Describe the proposed water distribution network and connection to the existing system.

Sanitary services

- Describe the existing sanitary sewers available to receive wastewater from the building.
- Calculate peak flow rates from the proposed development.
- Describe the proposed sanitary sewer system.
- Review impact of increased sanitary flow on downstream sanitary sewer.

4 REGULATORY APPROVALS

An MECP Environmental Compliance Approval is not expected to be required for installation of the proposed storm and sanitary sewers within the site. A Permit to Take Water is not anticipated to be required for pumping requirements for sewer installation. No other approval requirements from other regulatory agencies are anticipated.



5 STORMWATER MANAGEMENT

5.1 Existing Stormwater Infrastructure

The topography of the site in pre-development conditions was reviewed to determine the direction of flow from overland runoff. In pre-development conditions, majority of the stormwater appears to flow uncontrolled overland towards Morisset Ave. The balance, at the rear of the property, appears to flow uncontrolled overland into the neighbouring property along the north property border. Refer to Pre-development Watershed Plan (C701) in Appendix E.

As previously discussed, the south end of the subject property is bordered by Morisset Avenue. Hence, the proposed storm service connection will be located at Morisset Ave. At this location, a dedicated 375 mm diameter storm sewer, flowing east, is available on the north side of the street for a potential connection.

5.2 Design Criteria

The stormwater management criteria for this development were based on the initial pre-consultation with City of Ottawa officials, the City of Ottawa Sewer Design Guidelines, 2012 (City Standards), as well as the Ministry of the Environment's Stormwater Management Planning and Design Manual, 2003 (SWMPD Manual).

5.2.1 Water Quality

Based on correspondence with Rideau Valley Conservation Authority (RVCA), the distance to the downstream outlet is greater than 2 km, therefore, the stormwater runoff from the site does not require any additional on-site water quality controls. Refer to Appendix B for the RVCA's opinion on water quality controls.

5.2.2 Water Quantity

All storm events up to and including the 100-year event will be controlled to the 2-year pre-development level. The sites major overland flow route has been designed to ensure that storm events beyond the 100-year design storm can be safely conveyed overland towards the Morisset Ave-Right of Way (ROW). The minor systems (storm sewers) within the site are sized to convey the 2-year storm event flow from the site to the municipal storm sewer on Morisset Ave.

Based on the pre-development catchment area calculations, the pre-development weighted runoff was found to be $C=0.9$. Detailed calculations can be found in Appendix B.

Though post-development conditions are not introducing a large increase in impervious surfaces, quantity control will still have to be implemented. The allowable release rate is calculated using the maximum runoff coefficient of $C=0.5$, as per the City of Ottawa requirement. The 100-year and 2-year post development flows will be controlled to the 2-year allowable flow rate of the site. Events greater than the 100-year storm are permitted to flow overland to the ROW.



5.3 Method of Analysis

The modified Rational Method has been used to calculate the runoff rate from the site, and to quantify the detention storage required for quantity control of the development. Refer to Appendix B for allowable release rate as well as storage calculations.

5.4 Allowable Release Rate

The maximum allowable release rate was calculated using the Rational method for the 2-year pre-development runoff value. Runoff from post-development conditions must be controlled to the 2-year pre-development level using a maximum of $C=0.5$ for the runoff coefficient, for both minor and major storms (2-year up to 100-year storms), using a time of concentration not less than 10 minutes.

The Rational method runoff coefficients (C) for each catchment have been calculated based on appropriately assigned coefficients weighted by area of land cover within the drainage area. A summary of catchment areas with calculated C values is included in Appendix B.

Below is the allowable release rate calculation (2-year storm, $C=0.5$)

$$Q = 2.78CIA = 2.78 \times 0.5 \times 76.80 \times 0.185 = 19.70 \text{ L/s}$$

i.e. the allowable release rate for this site is 19.70 L/s.

5.5 Proposed Stormwater Quantity Controls

The proposed stormwater management quantity control for this development will be accomplished using a flow restrictor in the storm sewer, as well as roof drains restricting the flow leaving the rooftop. Ponding required as a result of quantity control will be accomplished through a combination of rooftop storage and parking lot surface storage.

The proposed site storm sewer and stormwater management system are shown on Site Servicing Plan C-401 (Appendix E) and detailed calculations including the design sheet can be found in Appendix B.

The existing site is delineated by catchment EWS-01 (see drawing C701 in Appendix E) which currently drains uncontrolled off the site towards Morisset Ave ROW and towards the rear of the property.

The site has been analyzed and post-development watersheds have been allocated, see drawing C701 in Appendix E. Watershed WS-01 consists of the landscape grassed area at the north of the building. Stormwater from this watershed will be drained to the Landscape catch-basin through overland grass swale. The catch-basin will eventually drain the stormwater to the storm sewer network within the site. Watersheds WS-02 and WS-03 consisting of asphalt parking areas will drain to their respective manholes upstream of the ICD and will be drained at a controlled release rate. Stormwater captured on the roof in the Watershed WS-04 will be controlled by the roof drains, and conveyed to the storm sewer network, downstream of the ICD. Watersheds WS-05 and WS-06, consisting of mostly grass area will flow uncontrolled towards Morisset Ave ROW. Stormwater from Watershed WS-07, consisting of the exterior landscape boundary (along south property line) and interlocking pavers (along west property line) will drain off to the proposed landscape catch-basin located at the south of the building through a grass swale. Stormwater captured within this landscape catch-basin will be drain to the storm sewer pipe, downstream of the ICD and as a result will flow uncontrolled to the city storm sewer.



Grading proposed will provide positive overland drainage to the proposed storm water management systems.

All overland stormwater captured using catch basin and catch basin manholes will ultimately be conveyed, via underground storm sewers, to the City storm sewer running along Morisset Ave. Table 1 summarizes the drainage areas, calculations can be found in Appendix B.

Table 1: Post-Development Drainage Areas

Drainage Area	Area (ha)	Weighted Runoff Coefficient	100-year Weighted Runoff Coefficient (25% increase)
WS-01 (controlled)	0.015	0.32	0.40
WS-02 (controlled)	0.049	0.82	1.00
WS-03 (controlled)	0.043	0.87	1.00
WS-04 (controlled)	0.055	0.90	1.00
WS-05 (uncontrolled)	0.003	0.22	0.28
WS-06 (uncontrolled)	0.005	0.38	0.48
WS-07 (uncontrolled)	0.014	0.51	0.64
Total	0.185	0.78	0.97

Tables 2 summarizes the release rates and storage volumes required to meet the allowable release rate for 100-year storm.

Table 2: Summary of Stormwater Release Rate & Storage Volume (100-Year)

Description	Area (ha)	Release Rate (L/s)	Storage Required (m ³)	Storage Provided (m ³)
WS-01 to WS-03 (ICD Controlled)	0.107	9.71	27.80	34.24
WS-04 (Roof Controlled)	0.055	3.78	18.77	27.03
WS-05 to WS-07 (Uncontrolled)	0.023	6.20	N/A	N/A
Total	0.185	19.70	46.57	61.27



The project runoff exceeding the allowable release rate will be stored on-site via surficial ponding and the building rooftop storage. The 100-year maximum ponding elevation and depths can be found on drawing “C601 – Stormwater Management Plan” of Appendix E.

5.5.1 Proposed Stormwater Quantity Controls

To throttle the 100-year storm flows, the stormwater will be controlled at CBMH03 using an Inlet Control Device (ICD), Hydrovex Vortex Flow Regulator 100VHV-1 (or approved equivalent). This ICD will control the stormwater runoff quantity during the storm events greater than 2-year. The site is graded to have a high-water level (HWL) of 97.82 m while providing storage as required with a maximum controlled release rate of 9.71 L/s (H=1.61 m) from the parking lot portion of the site. The storage created by this ICD can be seen on drawing C601 (Appendix E). Greater details on select ICD can be found in Appendix B.

While the storage required for 100- and 5-year storm events is proposed to be accommodated in the parking lot surface. The storage associated with 2-year storm event will be accommodated underground within the STM sewer (oversized pipes) and two (2) CBMHs which will provide a total storage of 9.03 m³, see calculations included in Appendix B.

5.5.2 Rooftop Storage & Release Rates

Rooftop detention of stormwater will be achieved through outlet control with the use of six (6) proposed roof drains (Watts roof drains or approved equivalent). These Watts drains are appropriately selected with an adjustable flow control set to “closed” position which will allow a maximum discharge of 0.63 L/s at a maximum flow depth of 0.15 m. Refer to Appendix B for additional detail on rooftop release rate and storage calculations and drawing C601 (Appendix E) for the extent of roof top storage. The flow through these drains is dependent on the height of water above the drains (head) and the type & setting of the drain. The rooftop has been assumed to be low sloping providing six separate ponding areas, each with a single roof drain restricting the discharge rate to 0.63 L/s per roof drain (at a maximum head of 150mm during the 100-year storm event). This results in a total release rate of 3.78 L/s from the roof.

6 WATER SUPPLY AND FIRE PROTECTION

6.1 Existing Water Supply Services and Fire Hydrant Coverage

The subject property is located to the north of an existing 150 mm dia. water main running in the east-west direction on the south side of Morisset Avenue.

There are three (3) existing fire hydrant (FH) along Morisset Ave in proximity to the proposed site: one (1) within 76 m and two (2) additional within 305 m. A schematic summarizing the locations of each FH can be seen in Appendix C.

6.2 Water Supply Demand and Fire Flow

According to the City of Ottawa Design Guidelines, the average daily water consumption rate for residential developments is 350 L/c/d.



The interior layout and architectural floor plans (Appendix F) have been reviewed, and it was determined that the building will house sixteen (16) 1-bedroom apartments and fifteen (15) 2-bedroom apartments. Based on the City of Ottawa Design guidelines for population projection, this translates to approximately 53.9 residents. Table 3 summarizes the population count of the proposed development as interpreted using Table 4.1 of the City of Ottawa Design Guidelines-Water Distribution, 2010.

Table 3: Residential Population Estimate

Proposed Unit type	Persons Per Unit	Number of Units	Population
1-Bedroom	1.4	16	22.4
2-Bedroom	2.1	15	31.5
	Total	31	53.9

The water supply requirements for the residential units in the proposed building are calculated using the following formula:

$$Q = (q \times P \times M)$$

Where,

q = Average water consumption (L/capita/day)

P = Design population (capita)

M = Peak factor

Calculated domestic water demands are summarized below, see Appendix C for calculation details.

- Average day demand = 0.22 L/s
- Maximum daily demand = 1.63 L/s
- Peak hour demand = 18.27 L/s

The fire flow requirements were estimated using the method prescribed by Ontario Building Code (OBC). This method is based on the volume of the building to be protected, the type of construction and the separation distances with adjoining building units.

Table 4 summarize the input parameters used for the fire flow calculations. A minimum fire flow demand of 75 L/s was calculated, refer to Appendix C for the fire flow calculation sheets.

Table 4: Input Parameters for Fire Flow Calculations

Type of Construction	Total Building Volume (m ³)	Exposure Distance (Spatial Coefficient)			
		North	East	South	West
Group C-Combustible Construction (K=18)	6788	> 10 m (0.00)	> 10 m (0.00)	> 10 m (0.00)	7.8 m (0.25)



Based on the boundary condition information provided by the City (refer to Appendix C), the available pressure at the proposed connection during maximum day + fire flow condition is 256.35 kPa (37.18 psi). This exceeds the required pressure of minimum 140kPa (20 psi) ensuring compliance with the City guidelines.

6.3 Water Supply Servicing Design

The proposed development falls under the provisions of Part 9 of the Ontario Building Code and is not required to be equipped with a sprinkler system. The proposed building will be serviced by a new 100 mm dia. water service lateral. The proposed service will be connected to the existing watermain on Morisset Ave to the south-east corner of the proposed building. Refer to servicing plan C401 for the layout of the proposed water services.

Table 5 below summarizes the design criteria which have been respected during the design of the water service connections at this development.

Table 5: Water Supply Design Criteria

Design Parameter	Value
Minimum cover	2.4 m
Desired pressure range under maximum daily flow condition	350 and 480 kPa
Minimum pressure under peak hourly flow condition	275 kPa
Minimum pressure under the maximum day plus fire flow condition	140 kPa

The boundary conditions provided by the City at the Morisset Avenue connection expressed as the level of hydraulic grade line (HGL) are summarized in Table 6.

Table 6: Boundary Conditions

Water Pressure at Morisset Ave			
HGL (m)		Pressure*	
		kPa	psi
Minimum	146.9	474.05	68.76
Maximum	158.3	585.85	84.97
Max Day + Fire Flow	124.7	256.35	37.18
*Assumed ground elevation at the connection point = 98.56 m			

Given the size and length of the proposed water service (15m-100 mm dia.), a negligible pressure loss is anticipated from the connection point to the service entry point at the proposed building. As such, the maximum pressure is anticipated to be more than 80 psi, therefore a pressure reducing valve is required as the residual pressure is not to exceed 80 psi. The required minimum pressure during peak hour and maximum day + fire flow scenarios corroborate with the design values mentioned in Table 5.



7 SANITARY SERVICE

7.1 Existing Sanitary Sewer Services

Existing infrastructure surrounding the proposed development were reviewed. It was determined that there is an existing 225 mm dia. sanitary sewer running east along Morisset Ave. Since the existing site is a parking lot, pre-development conditions did not generate sanitary flow. The post-development total peak flow was calculated to be 0.76 L/s as a result of residential population and a small portion of infiltration.

The City of Ottawa official was contacted regarding the remaining capacity of sanitary sewer along Morisset Ave. Based on the information received from the City (see Appendix D), it was confirmed that there is sufficient capacity in the sanitary sewer to accommodate the flow from this development.

7.2 Sanitary Sewer Servicing Design

The parameters used to calculate the anticipated sanitary flows are; residential average population per unit of 1.4 persons for 1-bedroom units and 2.1 persons for 2-bedroom units, a residential peaking factor of 4.0 and an infiltration rate of 0.33 L/s/ha. Based on these parameters and the total site area of 0.185 ha, the total anticipated sanitary flow was estimated to 0.76 L/s. Refer to Appendix D for the site sanitary sewer design sheet.

The proposed new building will be serviced with a new 150 mm dia. sanitary service which will connect to the existing 225 mm dia. sanitary sewer along Morisset Ave. The new service will be located at the south-east corner of the proposed building. The proposed 150mm dia. PVC sanitary service will be installed at a slope of 3% which will result calculated actual flow velocity greater than self-cleansing velocity during peak flow condition. Refer to Servicing Plan (C401) for the proposed sanitary servicing.

8 EROSION AND SEDIMENT CONTROL

During construction, erosion and sediment controls will be provided primarily via a sediment control fence to be erected along the perimeter of the site where runoff has the potential of leaving the site. Inlet sediment control devices are also to be provided in any catch basin and/or manholes in and around the site that may be impacted by the site construction. Construction and maintenance requirements for erosion and sediment controls are to comply with Ontario Provincial Standard Specification OPSS. MUNI 805. For additional details, refer to Erosion and Sediment Control Plan (C101).

9 CONCLUSION

This Stormwater Management Report and Servicing Brief for the proposed development at 1465 Morisset Avenue presents the rationale and details for the servicing requirements for the subject property.

In accordance with the report objectives, the servicing requirements for the development are summarized below:



Stormwater Management

- The storm water release rates from the proposed development will meet the pre-development allowable release rate of 19.70 L/s onto Morisset Ave.
- Stormwater quantity control will be achieved via an ICD proposed at CBMH03, which will limit the flow draining to the municipal sewer to the allowable release rate.
- Stormwater quantity control objectives will be met through on-site stormwater ponding on the roof and parking lot surface storage.

Water Service

- The anticipated maximum hour demand of the proposed development, based on estimated population & calculated peak factor, is 18.27 L/s.
- The maximum required fire flow was calculated at 75 L/s using the OBC method.
- For fire protection, there are three (3) existing fire hydrant along Morisset Ave in proximity to the proposed building.
- The proposed building will be serviced by a new 100 mm dia. water service to be connected to the existing 150 mm dia. watermain on Morisset Ave.

Sanitary Service

- The anticipated sanitary peak design flow from the proposed development is 0.76 L/s.
- The proposed building will be serviced by a new 150 mm dia. sanitary service to be connected to the existing 225 mm dia. sanitary sewer on Morisset Ave.

10 REPORT CONDITIONS AND LIMITATIONS

The report conclusions are applicable only to this specific project described in the preceding pages. Any changes, modifications or additions will require a subsequent review by LRL Associates Ltd. to ensure the compatibility with the recommendations contained in this document. If you have any questions or comments, please contact the undersigned.

Prepared by:
LRL Associates Ltd.



Sarthak Vora
Civil E.I.T

Mohan Basnet, P.Eng.
Civil Engineer



APPENDIX A
Pre-consultation/Correspondence

Site Plan Pre - Application Consultation Notes

Date: August 28, 2020

Site Location: 1435 Morisset

Type of Development: Residential (townhomes, stacked, singles, apartments), Office Space, Commercial, Retail, Institutional, Industrial, Other: N/A

Owner/Agent: Firm Capital Properties/FOTENN Consultants

Project Manager: Adam Baker

Assigned Planner: Kelby Lodoen Unseth

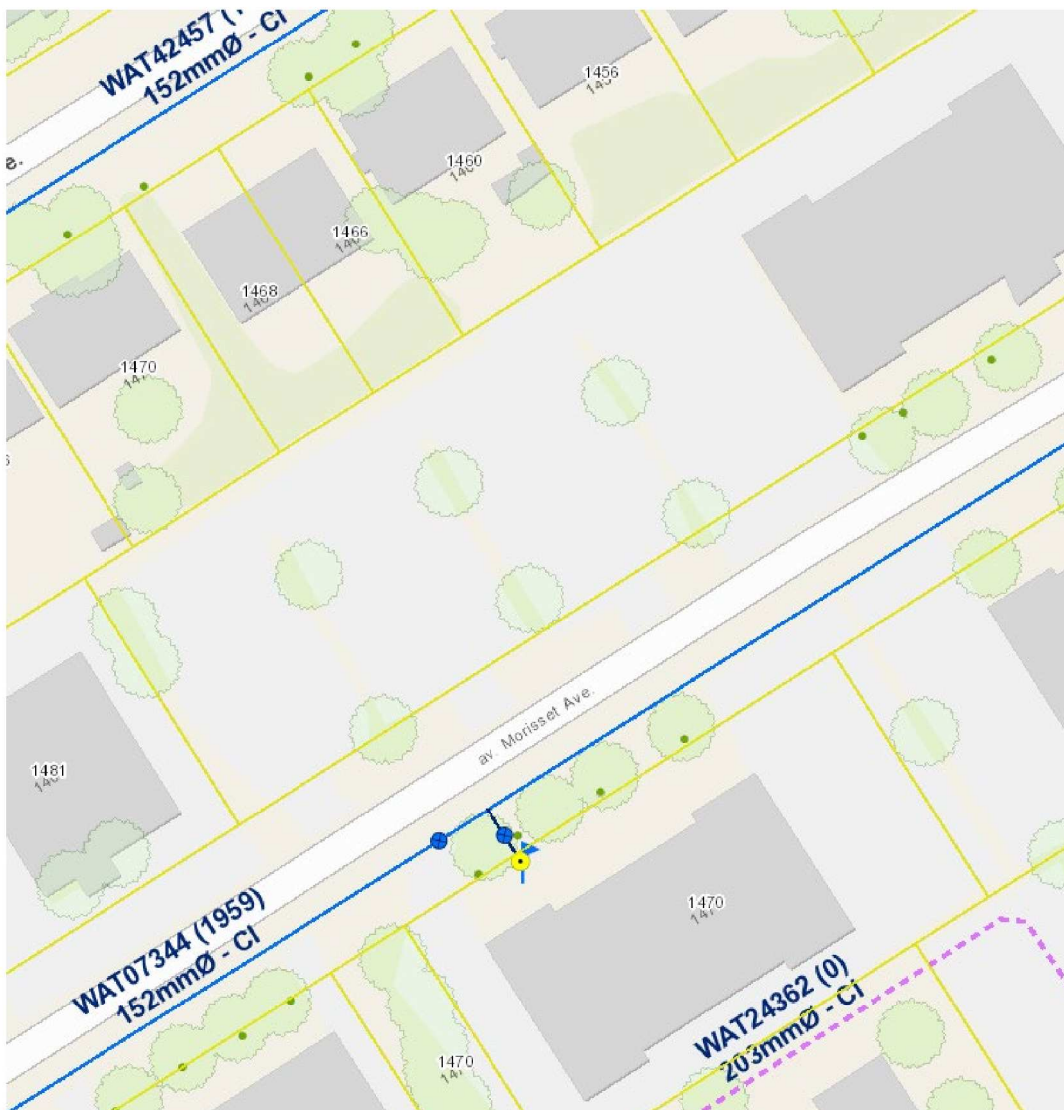
Infrastructure

Water

Please note that watermains in this area may experience lower than average pressures within the acceptable pressure range. Please submit your water boundary request to confirm these details.

Existing nearest public services:

- Morisset – 152mm Cast Iron



Watermain Frontage Fees to be paid (\$190.00 per metre) Yes No

- Service areas with a basic demand greater than 50 m³/day shall be connected with a minimum of two water services, separated by an isolation valve, to avoid creation of vulnerable service area.
- A District Metering Area Chamber (DMA) is required for services 150mm or greater in diameter.

Boundary conditions:

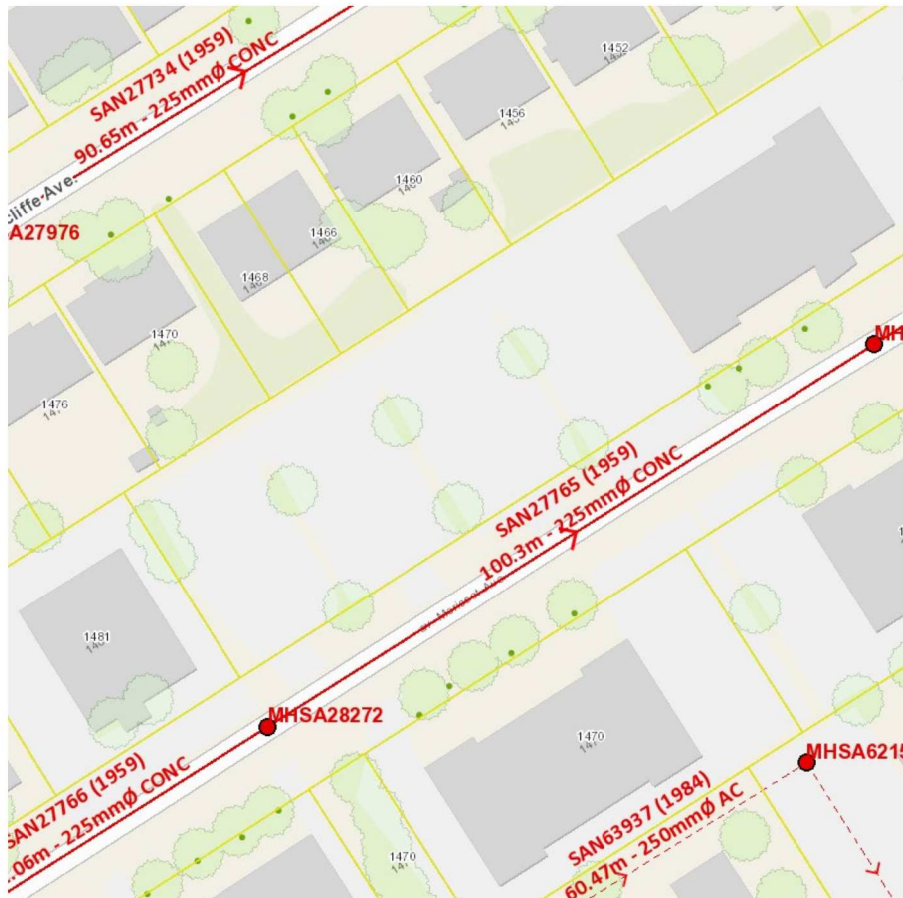
Civil consultant must request boundary conditions from the City's assigned Project Manager prior to first submission.

- Water boundary condition requests must include the location of the service(s) and the expected loads required by the proposed developments. Please provide all the following information:
 - Location of service(s)
 - Type of development and the amount of fire flow required (as per FUS, 1999).
 - Average daily demand: ___ l/s.
 - Maximum daily demand: ___ l/s.
 - Maximum hourly daily demand: ___ l/s.
- Fire protection (Fire demand, Hydrant Locations)
- A water meter sizing questionnaire [water card] will have to be completed prior to receiving a water permit (water card will be provided post approval)

Sanitary Sewer

Existing public services:

- Morisset – 225mm Conc.

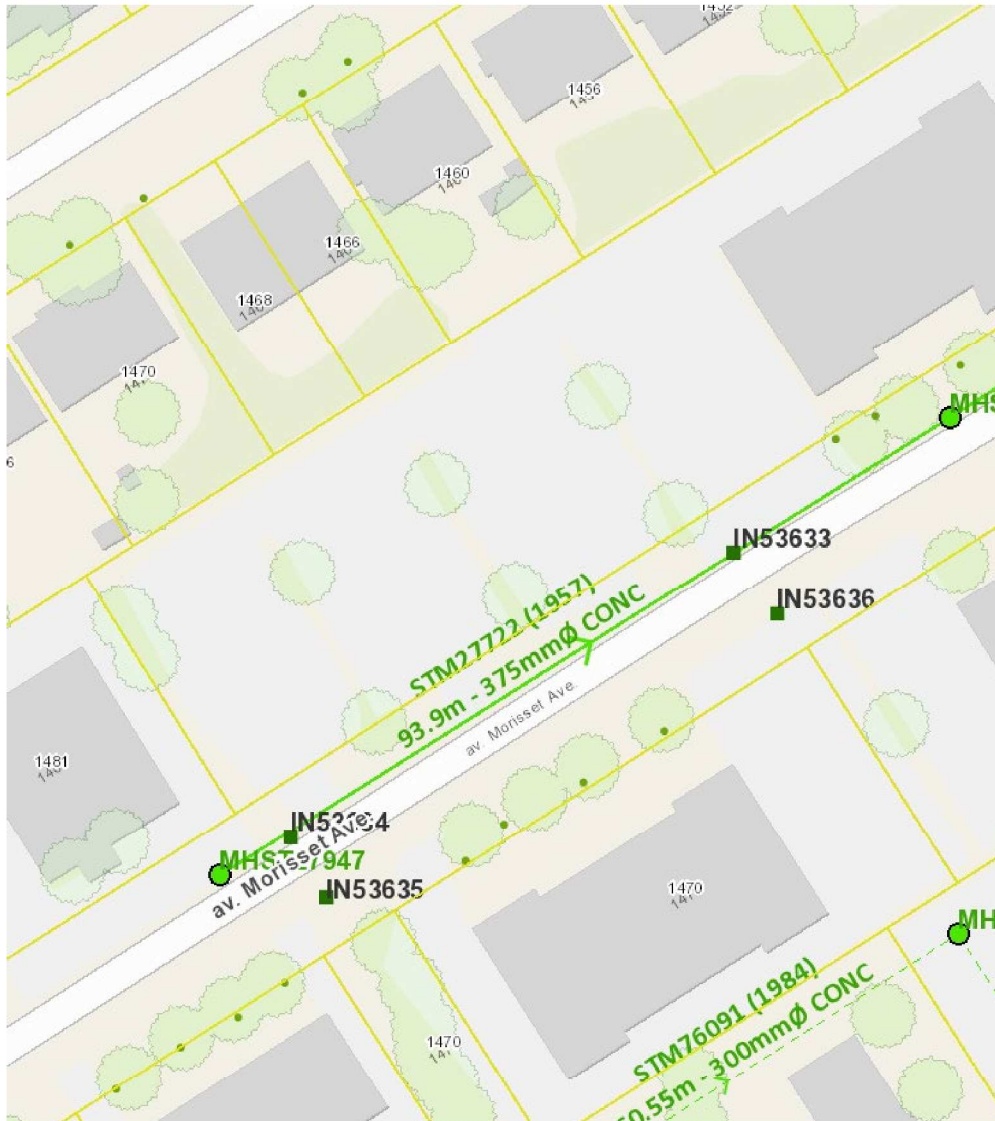


- The designer should be aware there may be limited capacity in the downstream sanitary sewer system. The sanitary demand needs to be coordinated with the City Planning Dept. to determine if the existing sanitary sewer system has sufficient capacity to support the proposed rezoning. Provide sanitary demands to the City project manager for coordination.
- Any premise in which there is commercial or institutional food preparation shall install a grease and oil inceptor on all fixtures.

Storm Sewer

Existing public services:

- Morisset – 375mm Conc.



Storm Sewer Notes:

- For concrete sewer pipe, maintenance holes shall be installed when the service is greater than 50% of the diameter of the mainline concrete pipe
- The Environmental Site Assessment (ESA) may provide recommendations where site contamination may be present. The recommendations from the ESA need to be coordinated with the servicing report to ensure compliance with the Sewer Use By-Law.

Stormwater Management

Quantity Control:

- Stormwater quantity controls will depend upon which outlet is chosen for the site. Once an outlet has been chosen, please confirm with the Project Manager the SWM criteria for the property. For the nearby public services, the criteria is as follows –
 - The pre-development runoff coefficient or a maximum equivalent 'C' of 0.5, whichever is less (§ 8.3.7.3).
 - A calculated time of concentration (Cannot be less than 10 minutes).
 - Flows to the storm sewer in excess of the 2-year storm release rate, up to and including the 100-year storm event, must be detained on site.

Ministry of Environment, Conservation and Parks (MECP)

All development applications should be considered for an Environmental Compliance Approval, under MECP regulations.

- a. The consultants determine if an approval for sewage works under Section 53 of OWRA is required and determines what type of application. The City's project manager may help confirm and coordinate with the MECP as required.
- b. The project will be either transfer of review (standard), transfer of review (additional), direct submission, or exempt as per O. Reg. 525/98.
- c. Pre-consultation is not required if applying for standard or additional works (Schedule A of the Agreement) under Transfer Review.
- d. Pre-consultation with local District office of MECP is recommended for direct submission.
- e. Consultant completes an MECP request form for a pre-consultation. Sends request to moeccottawasewage@ontario.ca
- f. ECA applications are required to be submitted online through the MECP portal. A business account required to submit ECA application. For more information visit <https://www.ontario.ca/page/environmental-compliance-approval>
- g. It is unclear if the proposed development will remain as one property. An ECA will be required where the stormwater management services more than one property parcel.

NOTE: Site Plan Approval, or Draft Approval, is required before any Ministry of the Environment and Climate Change (MOECC) application is sent

General Service Design Comments

- The City of Ottawa requests that all new services be located within the existing service trench to minimize necessary road cuts.
- Monitoring manholes should be located within the property near the property line in an accessible location to City forces and free from obstruction (i.e. not a parking).
- Where service length is greater than 30 m between the building and the first maintenance hole / connection, a cleanout is required.
- The City of Ottawa Standard Detail Drawings should be referenced where possible for all work within the Public Right-of-Way.
- The upstream and downstream manhole top of grate and invert elevations are required for all new sewer connections.
- Services crossing the existing watermain or sewers need to clearly provide the obvert/invert elevations to demonstration minimum separation distances. A watermain crossing table may be provided.

Other

Are there are Capital Works Projects scheduled that will impact the application? Yes No

References and Resources

- As per section 53 of the Professional Engineers Act, O. Reg 941/40, R.S.O. 1990, all documents prepared by engineers must be signed and dated on the seal.
- All required plans are to be submitted on standard A1 size sheets (594mm x 841mm) sheets, utilizing a reasonable and appropriate metric scale as per City of Ottawa Servicing and Grading Plan Requirements: title blocks are to be placed on the right of the sheets and not along the bottom. Engineering plans may be combined, but the Site Plans must be provided separately. Plans shall include the survey monument used to confirm datum. Information shall be provided to enable a non-surveyor to locate the survey monument presented by the consultant.
- All required plans & reports are to be provided in *.pdf format (at application submission and for any, and all, re-submissions)
- Please find relevant City of Ottawa Links to Preparing Studies and Plans below:
<https://ottawa.ca/en/city-hall/planning-and-development/information-developers/development-application-review-process/development-application-submission/guide-preparing-studies-and-plans#standards-policies-and-guidelines>
- To request City of Ottawa plan(s) or report information please contact the City of Ottawa Information Centre:
InformationCentre@ottawa.ca<mailto:InformationCentre@ottawa.ca>
(613) 580-2424 ext. 44455
- geoOttawa <http://maps.ottawa.ca/geoOttawa/>

SITE PLAN APPLICATION – Municipal servicing

For information on preparing required studies and plans refer to:

<http://ottawa.ca/en/development-application-review-process-0/guide-preparing-studies-and-plans>

S/A	Number of copies	ENGINEERING		S/A	Number of copies
S		1. Site Servicing Plan	2. Site Servicing Study	S	
S		3. Grade Control and Drainage Plan	4. Geotechnical Study	S	
		5. Composite Utility Plan	6. Groundwater Impact Study		
		7. Servicing Options Report	8. Wellhead Protection Study		
		9. Community Transportation Study and/or Transportation Impact Study / Brief	10. Erosion and Sediment Control Plan / Brief	S	
S		11. Storm water Management Report	12. Hydro-geological and Terrain Analysis		
		13. Water main Analysis	14. Noise Study	S	
		15. Roadway Modification Design Plan	16. Confederation Line Proximity Study		

It is important to note that the need for additional studies and plans may result during application review. If following the submission of your application, it is determined that material that is not identified in this checklist is required to achieve complete application status, in accordance with the Planning Act and Official Plan requirements, City Planning will notify you of outstanding material required within the required 30 day period. Mandatory pre-application consultation will not shorten the City's standard processing timelines, or guarantee that an application will be approved. It is intended to help educate and inform the applicant about submission requirements as well as municipal processes, policies, and key issues in advance of submitting a formal development application. This list is valid for one year following the meeting date. If the application is not submitted within this timeframe the applicant must again pre-consult with the City.

Notes:

4. Geotechnical Study / Slope Stability Study – required as per Official Plan section 4.8.3. All site plan applications need to demonstrate the soils are suitable for development. A Slope Stability Study may be required with unique circumstances (Schedule K or topography may define slope stability concerns).

10. Erosion and Sediment Control Plan – required with all site plan applications as per Official Plan section 4.7.3.

11. Stormwater Management Report/Brief - required with all site plan applications as per Official Plan section 4.7.6.

14. Noise and Vibration Study – a Noise Study will be required if the noise sensitive development is proposed within 250 metres of an existing or proposed highway or a railway right-of-way, or 100 metres of an arterial or collector roadway or rapid-transit corridor. A Vibration Study will be required if the proposed development is within 75 metres of either an existing or proposed railway ROW. A Noise Study may also be required if the proposed development is adjacent to an existing or proposed stationary noise source..

APPENDIX B
Stormwater Management Calculations

Mohan Basnet

From: Baker, Adam <adam.baker@ottawa.ca>
Sent: May 27, 2021 8:22 AM
To: Mohan Basnet
Subject: RE: 200572-1435 Morisset Ave-Proposed Service Connection/SWM criteria

Follow Up Flag: Follow up
Flag Status: Flagged

Hi Mohan,

Please accept the following information with regards to the servicing criteria –

- SWM criteria for an outlet on Morisset Avenue:
 - The 2-yr storm or 5-yr storm event using the IDF information derived from the Meteorological Services of Canada rainfall data, taken from the MacDonald Cartier Airport, collected 1966 to 1997.
 - The pre-development runoff coefficient or a maximum equivalent 'C' of 0.5, whichever is less (§ 8.3.7.3).
 - A calculated time of concentration (Cannot be less than 10 minutes).
 - Flows to the storm sewer in excess of the 2-year storm release rate, up to and including the 100-year storm event, must be detained on site.
 - Please confirm any stormwater quality requirements with the relevant Conservation Authority.
- Sanitary Constraints:
 - Please confirm if the anticipated sanitary flow provided (0.76 L/s) is peak or average. From an average flow of 0.76 L/s, a resulting peak sanitary flow of 3.24 L/s is acceptable for this system. If the peak sanitary flows will exceed this, please let me know and I will re-confirm for you.

Thank you,
Adam

Adam Baker, EIT

Project Manager

Planning, Infrastructure and Economic Development Department - Services de la planification, de l'infrastructure et du développement économique

Development Review - South Branch

City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1

613.580.2424 ext./poste 26552, Adam.Baker@ottawa.ca

From: Mohan Basnet <mbasnet@lrl.ca>
Sent: May 12, 2021 2:09 PM
To: Baker, Adam <adam.baker@ottawa.ca>
Subject: 200572-1435 Morisset Ave-Proposed Service Connection/SWM criteria

CAUTION: This email originated from an External Sender. Please do not click links or open attachments unless you recognize the source.

ATTENTION : Ce courriel provient d'un expéditeur externe. Ne cliquez sur aucun lien et n'ouvrez pas de pièce jointe, excepté si vous connaissez l'expéditeur.

Good afternoon Adam,

At LRL, we are working for STM and servicing study for a proposed 3-storey residential apartment building at 1435 Morisset Ave.

As a follow-up from the pre-consultation notes (Aug 28, 2020):

- Can you please advise SWM criteria of the subject site with a proposed STM outlet at Morisset Ave?
- Can you also advise remaining capacity of SAN sewer along Morisset Ave? Anticipated SAN flow from the proposed building is 0.76 L/s

For your reference I have also attached schematic of proposed service connections.

Please let me know if you have any question.

Thank you,

Mohan Basnet, P.Eng.



Civil Engineering Services

LRL Associates Ltd.

5430 Canotek Road
Ottawa, Ontario K1J 9G2

T (613) 842-3434 or (877) 632-5664 ext 213

F (613) 842-4338

E mbasnet@lrl.ca

W www.lrl.ca

Given the current COVID-19 situation, please be aware that LRL has implemented alternative working conditions for our team. Many of us have now transitioned to working from home; however, communication and workability remains one of our top priorities.

We will continue to be reachable by cell phone or by calling LRL at 613-842-3434 which will prompt you to enter the extension of the person you are trying to reach.

In addition, we will continue to have access to all e-mail correspondence and do our best to return all inquiries in a timely manner.

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Mohan Basnet

From: Jamie Batchelor <jamie.batchelor@rvca.ca>
Sent: April 29, 2021 9:25 PM
To: Mohan Basnet
Cc: Eric Lalande
Subject: RE: 200572-1435/1455 Morisset Ave Proposed Residential Development - Stormwater Quality Control

Follow Up Flag: Follow up
Flag Status: Flagged

Good Evening Mohan,

Based on the distance of the downstream outlet being more than 2km from the site, the RVCA accepts that no additional on-site water quality treatment measures are required save and except best management practices. The RVCA strongly encourages that you explore the opportunity to incorporate LID measures in the stormwater management plan.

Jamie Batchelor, MCIP, RPP
Planner, ext. 1191
jamie.batchelor@rvca.ca



3889 Rideau Valley Drive
PO Box 599, Manotick ON K4M 1A5
T 613-692-3571 | 1-800-267-3504 F 613-692-0831 | www.rvca.ca

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From: Mohan Basnet <mbasnet@lrl.ca>
Sent: Wednesday, April 28, 2021 4:00 PM
To: Jamie Batchelor <jamie.batchelor@rvca.ca>
Subject: 200572-1435/1455 Morisset Ave Proposed Residential Development - Stormwater Quality Control

Hello Jamie,

We are working for a proposed 4-Storey Residential Development at 1435/1455 Morisset Ave, Ottawa. The existing site is a paved surface parking lot. The proposed development will also include paved parking lot providing 28 parking spots.

For stormwater management, we are planning to discharge controlled stormwater in a municipal storm sewer along Morisset Ave. Could you please advise stormwater quality control requirement for this site?

Thank you.

Mohan

Mohan Basnet, P.Eng.



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In addition, we will continue to have access to all e-mail correspondence and do our best to return all inquiries in a timely manner.

LRL Associates Ltd.

Storm Watershed Summary



LRL File No. 200572

Project: Proposed 3-Storey Apartment Building

Location: 1465 Morisset Ave, Ottawa

Date: December 18, 2024

Designed: Sarthak Vora

Checked: Mohan Basnet

Dwg Reference: C701, C702

Pre-Development Catchments

Watershed	C = 0.20	C = 0.80	C = 0.90	Total Area (ha)	Combined C
EWS-01 (uncontrolled)	0.000	0.000	0.185	0.185	0.90
Total	0.000	0.000	0.185	0.185	0.90

Post-Development Catchments

Watershed	C = 0.20	C = 0.8	C = 0.90	Total Area (ha)	Combined C
WS-01 (controlled)	0.012	0.003	0.000	0.015	0.32
WS-02 (controlled)	0.005	0.000	0.044	0.049	0.82
WS-03 (controlled)	0.002	0.000	0.041	0.043	0.87
WS-04 (controlled)	0.000	0.000	0.055	0.055	0.90
WS-05 (uncontrolled)	0.003	0.000	0.0001	0.003	0.22
WS-06 (uncontrolled)	0.004	0.000	0.001	0.005	0.38
WS-07 (uncontrolled)	0.008	0.000	0.006	0.014	0.51
Total	0.034	0.003	0.148	0.185	0.77



LRL File No. 200572
Project: Proposed 3-Storey Apartment Building
Location: 1465 Morisset Ave, Ottawa
Date: December 18, 2024
Designed: M. Basnet
Drawing Ref.: C601

Stormwater Management

STORM - 100 YEAR + "Stress Test"

Runoff Equation

Q = 2.78CIA (L/s)
 C = Runoff coefficient
 I = Rainfall intensity (mm/hr) = $A / (Td + C)^B$
 A = Area (ha)
 Td = Time of duration (min)

Pre-Development Catchments within Development Area

	Total Area =	0.185	ha	ΣR =	0.90
	EWS-01 (uncontrolled)	0.185	ha	R =	0.90
	Total Un-controlled =	0.185	ha	ΣR =	0.90

Pre-Development Release Rate

IDF Curve Equations

100-Year, $I_{100} = 1735.688 / (Td + 6.014)^{0.820}$ A = 1735.688 B = 0.820 C = 6.014

5-Year, $I_5 = 998.071 / (Td + 6.053)^{0.814}$ A = 998.071 B = 0.814 C = 6.053

2-Year, $I_2 = 732.951 / (Td + 6.199)^{0.810}$ A = 732.951 B = 0.810 C = 6.199

C = 0.50 (max 0.5 as per City Guidelines-Sewer)
 I_{100} = 178.6 mm/hr
 I_5 = 104.2 mm/hr
 I_2 = 76.8 mm/hr
 Td = 10 min

100-year Release Rate = 45.79 L/s
 5-year Release Rate = 26.72 L/s
 2-year Release Rate = 19.70 L/s

Allowable Release Rate = 19.70 L/s
 (2-year pre-development level)

Post-development Stormwater Management

					$\Sigma R_{2&5}$	ΣR_{100}
	Total Site Area =	0.185	ha	ΣR =	0.77	0.96
	WS-01 (controlled)	0.015	ha	R =	0.32	0.40
	WS-02 (controlled)	0.049	ha	R =	0.82	1.00
	WS-03 (controlled)	0.043	ha	R =	0.87	1.00
Roof	WS-04 (controlled)	0.055	ha	R =	0.90	1.00
	Total (Controlled)	0.162	ha	R =	0.82	1.00
	WS-05 (uncontrolled)	0.003	ha	R =	0.22	0.27
	WS-06 (uncontrolled)	0.005	ha	R =	0.38	0.48
	WS-07 (uncontrolled)	0.014	ha	R =	0.51	0.64
	Total (Uncontrolled)	0.023	ha	R =	0.44	0.55
	Total	0.185	ha	R =	0.77	0.96



LRL File No. 200572
Project: Proposed 3-Storey Apartment Building
Location: 1465 Morisset Ave, Ottawa
Date: December 18, 2024
Designed: M. Basnet
Drawing Ref.: C601

Stormwater Management

100-Year Post-development Stormwater Management (WS-04 Roof)

Time (min)	*Intensity (mm/hr)	Controlled Runoff (L/s)	Storage Volume (m ³)	Controlled Release Rate (L/s)	Uncontrolled Runoff (L/s)	Total Release Rate (L/s)
10	214.27	33.00	17.53	3.78	0.00	3.78
15	171.47	26.41	20.37	3.78	0.00	3.78
20	143.94	22.17	22.07	3.78	0.00	3.78
25	124.62	19.19	23.12	3.78	0.00	3.78
30	110.24	16.98	23.76	3.78	0.00	3.78
35	99.09	15.26	24.11	3.78	0.00	3.78
40	90.17	13.89	24.26	3.78	0.00	3.78
45	82.86	12.76	24.25	3.78	0.00	3.78
50	76.74	11.82	24.12	3.78	0.00	3.78
55	71.55	11.02	23.89	3.78	0.00	3.78
60	67.07	10.33	23.58	3.78	0.00	3.78
65	63.18	9.73	23.20	3.78	0.00	3.78
70	59.75	9.20	22.77	3.78	0.00	3.78
75	56.71	8.73	22.29	3.78	0.00	3.78
80	53.99	8.31	21.77	3.78	0.00	3.78
85	51.54	7.94	21.21	3.78	0.00	3.78
90	49.33	7.60	20.62	3.78	0.00	3.78
95	47.32	7.29	20.00	3.78	0.00	3.78
100	45.48	7.01	19.35	3.78	0.00	3.78
105	43.80	6.75	18.68	3.78	0.00	3.78
110	42.24	6.51	17.99	3.78	0.00	3.78
115	40.81	6.28	17.28	3.78	0.00	3.78
120	39.47	6.08	16.56	3.78	0.00	3.78

Note: *20% increase in rainfall values

On-site stormwater detention

Storage required = 24.26 m³
Storage provided
 Available roof surface for storage = 540.60 m²
 Maximum ponding depth = 150 mm Overflow scuppers to be installed at this height
Available roof storage = 27.03 m³
 Proposed roof drains: WATTS adjustable roof drain w/ weir opening-closed
 Maximum flow per roof drain = 0.63 L/s
 Number of roof drain = 6
 Total flow from roof drains = 3.79 L/s

100-Year Post-development Stormwater Management (except WS-04 Roof)

Time (min)	*Intensity (mm/hr)	Controlled Runoff (L/s)	Storage Volume (m ³)	Controlled Release Rate (L/s)	Uncontrolled Runoff (L/s)	Total Release Rate (L/s)
10	214.27	58.28	29.14	9.71	7.44	17.16
15	171.47	46.64	33.23	9.71	5.96	15.67
20	143.94	39.15	35.32	9.71	5.00	14.71
25	124.62	33.89	36.27	9.71	4.33	14.04
30	110.24	29.98	36.49	9.71	3.83	13.54
35	99.09	26.95	36.20	9.71	3.44	13.16
40	90.17	24.53	35.55	9.71	3.13	12.85
45	82.86	22.54	34.62	9.71	2.88	12.59
50	76.74	20.87	33.48	9.71	2.67	12.38
55	71.55	19.46	32.16	9.71	2.49	12.20
60	67.07	18.24	30.71	9.71	2.33	12.04
65	63.18	17.18	29.13	9.71	2.20	11.91
70	59.75	16.25	27.46	9.71	2.08	11.79
75	56.71	15.42	25.69	9.71	1.97	11.68
80	53.99	14.68	23.86	9.71	1.88	11.59
85	51.54	14.02	21.96	9.71	1.79	11.50
90	49.33	13.42	20.00	9.71	1.71	11.43
95	47.32	12.87	18.00	9.71	1.64	11.36
100	45.48	12.37	15.95	9.71	1.58	11.29
105	43.80	11.91	13.85	9.71	1.52	11.23
110	42.24	11.49	11.72	9.71	1.47	11.18
115	40.81	11.10	9.56	9.71	1.42	11.13
120	39.47	10.74	7.37	9.71	1.37	11.08

Note: *20% increase in rainfall values

On-site stormwater detention

Storage required = 36.49 m³
Storage provided = 36.37 m³ (Parking lot surface storage)



LRL File No. 200572
Project: Proposed 3-Storey Apartment Building
Location: 1465 Morisset Ave, Ottawa
Date: December 18, 2024
Designed: M. Basnet
Drawing Ref.: C601

Stormwater Management

STORM - 100 YEAR

Runoff Equation

$Q = 2.78CIA$ (L/s)
 C = Runoff coefficient
 I = Rainfall intensity (mm/hr) = $A / (Td + C)^B$
 A = Area (ha)
 Td = Time of duration (min)

Pre-Development Catchments within Development Area

	Total Area =	0.185	ha	ΣR =	0.90
	EWS-01 (uncontrolled)	0.185	ha	R =	0.90
	Total Uncontrolled =	0.185	ha	ΣR =	0.90

Pre-Development Release Rate

IDF Curve Equations

100-Year, $I_{100} = 1735.688 / (Td + 6.014)^{0.820}$ A = 1735.688 B = 0.820 C = 6.014
 5-Year, $I_5 = 998.071 / (Td + 6.053)^{0.814}$ A = 998.071 B = 0.814 C = 6.053
 2-Year, $I_2 = 732.951 / (Td + 6.199)^{0.810}$ A = 732.951 B = 0.810 C = 6.199

C = 0.50 (max 0.5 as per City Guidelines-Sewer)
 I_{100} = 178.6 mm/hr
 I_5 = 104.2 mm/hr
 I_2 = 76.8 mm/hr
 Td = 10 min

100-year Release Rate = 45.79 L/s
 5-year Release Rate = 26.72 L/s
 2-year Release Rate = 19.70 L/s

Allowable Release Rate = 19.70 L/s
 (2-year pre-development level)

Post-development Stormwater Management

				$\Sigma R_{2&5}$	ΣR_{100}
	Total Site Area =	0.185	ha	ΣR =	0.77
	WS-01 (controlled)	0.015	ha	R =	0.40
	WS-02 (controlled)	0.049	ha	R =	0.82
	WS-03 (controlled)	0.043	ha	R =	0.87
Roof	WS-04 (controlled)	0.055	ha	R =	0.90
	Total (Controlled)	0.162	ha	R =	0.82
	WS-05 (uncontrolled)	0.003	ha	R =	0.22
	WS-06 (uncontrolled)	0.005	ha	R =	0.38
	WS-07 (uncontrolled)	0.014	ha	R =	0.51
	Total (Uncontrolled)	0.023	ha	R =	0.44
	Total	0.185	ha	R =	0.77



LRL File No. 200572
Project: Proposed 3-Storey Apartment Building
Location: 1465 Morisset Ave, Ottawa
Date: December 18, 2024
Designed: M. Basnet
Drawing Ref.: C601

Stormwater Management

100-Year Post-development Stormwater Management (WS-04 Roof)

Time (min)	Intensity (mm/hr)	Controlled Runoff (L/s)	Storage Volume (m ³)	Controlled Release Rate (L/s)	Uncontrolled Runoff (L/s)	Total Release Rate (L/s)
10	178.56	27.50	14.23	3.78	0.00	3.78
15	142.89	22.01	16.40	3.78	0.00	3.78
20	119.95	18.47	17.63	3.78	0.00	3.78
25	103.85	15.99	18.32	3.78	0.00	3.78
30	91.87	14.15	18.66	3.78	0.00	3.78
35	82.58	12.72	18.77	3.78	0.00	3.78
40	75.15	11.57	18.70	3.78	0.00	3.78
45	69.05	10.63	18.51	3.78	0.00	3.78
50	63.95	9.85	18.21	3.78	0.00	3.78
55	59.62	9.18	17.83	3.78	0.00	3.78
60	55.89	8.61	17.38	3.78	0.00	3.78
65	52.65	8.11	16.88	3.78	0.00	3.78
70	49.79	7.67	16.33	3.78	0.00	3.78
75	47.26	7.28	15.74	3.78	0.00	3.78
80	44.99	6.93	15.12	3.78	0.00	3.78
85	42.95	6.62	14.46	3.78	0.00	3.78
90	41.11	6.33	13.78	3.78	0.00	3.78
95	39.43	6.07	13.07	3.78	0.00	3.78
100	37.90	5.84	12.35	3.78	0.00	3.78
105	36.50	5.62	11.60	3.78	0.00	3.78
110	35.20	5.42	10.83	3.78	0.00	3.78
115	34.01	5.24	10.05	3.78	0.00	3.78
120	32.89	5.07	9.26	3.78	0.00	3.78

On-site stormwater detention

Storage required = 18.77 m³
Storage provided
 Available roof surface for storage = 540.60 m²
 Maximum ponding depth = 150 mm
Available roof storage = 27.03 m³
 Proposed roof drains: WATTS adjustable roof drain w/ weir opening-closed
 Maximum flow per roof drain = 0.63 L/s
 Number of roof drain = 6
 Total flow from roof drains = 3.78 L/s

100-Year Post-development Stormwater Management (except WS-04 Roof)

Time (min)	Intensity (mm/hr)	Controlled Runoff (L/s)	Storage Volume (m ³)	Controlled Release Rate (L/s)	Uncontrolled Runoff (L/s)	Total Release Rate (L/s)
10	178.56	48.56	23.31	9.71	6.20	15.92
15	142.89	38.86	26.24	9.71	4.96	14.68
20	119.95	32.62	27.49	9.71	4.17	13.88
25	103.85	28.24	27.80	9.71	3.61	13.32
30	91.87	24.99	27.49	9.71	3.19	12.90
35	82.58	22.46	26.77	9.71	2.87	12.58
40	75.15	20.44	25.74	9.71	2.61	12.32
45	69.05	18.78	24.48	9.71	2.40	12.11
50	63.95	17.39	23.04	9.71	2.22	11.93
55	59.62	16.22	21.46	9.71	2.07	11.78
60	55.89	15.20	19.76	9.71	1.94	11.65
65	52.65	14.32	17.96	9.71	1.83	11.54
70	49.79	13.54	16.08	9.71	1.73	11.44
75	47.26	12.85	14.13	9.71	1.64	11.35
80	44.99	12.24	12.11	9.71	1.56	11.28
85	42.95	11.68	10.04	9.71	1.49	11.21
90	41.11	11.18	7.93	9.71	1.43	11.14
95	39.43	10.73	5.77	9.71	1.37	11.08
100	37.90	10.31	3.57	9.71	1.32	11.03
105	36.50	9.93	1.35	9.71	1.27	10.98
110	35.20	9.57	0.00	9.71	1.22	10.94
115	34.01	9.25	0.00	9.71	1.18	10.89
120	32.89	8.95	0.00	9.71	1.14	10.86

On-site stormwater detention

Storage required = 27.80 m³
Storage provided = 34.24 m³ (Parking lot surface storage)



LRL File No. 200572
Project: Proposed 3-Storey Apartment Building
Location: 1465 Morisset Ave, Ottawa
Date: December 18, 2024
Designed: M. Basnet
Drawing Ref.: C601

Stormwater Management

STORM - 5 YEAR

Runoff Equation

Q = 2.78CIA (L/s)
 C = Runoff coefficient
 I = Rainfall intensity (mm/hr) = $A / (Td + C)^B$
 A = Area (ha)
 Td = Time of duration (min)

Pre-Development Catchments within Development Area

	Total Area =	0.185	ha	∑R =	0.90
	EWS-01 (uncontrolled)	0.185	ha	R =	0.90
	Total Un-controlled =	0.185	ha	∑R =	0.90

Pre-Development Release Rate

IDF Curve Equations

100-Year, $I_{100} = 1735.688 / (Td + 6.014)^{0.820}$	A = 1735.688	B = 0.820	C = 6.014
5-Year, $I_5 = 998.071 / (Td + 6.053)^{0.814}$	A = 998.071	B = 0.814	C = 6.053
2-Year, $I_2 = 732.951 / (Td + 6.199)^{0.810}$	A = 732.951	B = 0.810	C = 6.199

C =	0.50	(max 0.5 as per City Guidelines-Sewer)
I_{100} =	178.6	mm/hr
I_5 =	104.2	mm/hr
I_2 =	76.8	mm/hr
Td =	10	min

100-year Release Rate =	45.79	L/s
5-year Release Rate =	26.72	L/s
2-year Release Rate =	19.70	L/s

Allowable Release Rate = 19.70 L/s
 (2-year pre-development level)

Post-development Stormwater Management

					$\sum R_{2&5}$	$\sum R_{100}$
	Total Site Area =	0.185	ha	∑R =	0.77	0.96
	WS-01 (controlled)	0.015	ha	R =	0.32	0.40
	WS-02 (controlled)	0.049	ha	R =	0.82	1.00
	WS-03 (controlled)	0.043	ha	R =	0.87	1.00
Roof	WS-04 (controlled)	0.055	ha	R =	0.90	1.00
	Total (Controlled)	0.162	ha	R =	0.82	1.00
	WS-05 (uncontrolled)	0.003	ha	R =	0.22	0.27
	WS-06 (uncontrolled)	0.005	ha	R =	0.38	0.48
	WS-07 (uncontrolled)	0.014	ha	R =	0.51	0.64
	Total (Uncontrolled)	0.023	ha	R =	0.44	0.55
	Total (Controlled+Uncontrolled)	0.185	ha	R =	0.77	0.96



LRL File No. 200572
 Project: Proposed 3-Storey Apartment Building
 Location: 1465 Morisset Ave, Ottawa
 Date: December 18, 2024
 Designed: M. Basnet
 Drawing Ref.: C601

Stormwater Management

5-Year Post-development Stormwater Management (WS-04 Roof)

Time (min)	Intensity (mm/hr)	Controlled Runoff (L/s)	Storage Volume (m ³)	Controlled Release Rate (L/s)	Uncontrolled Runoff (L/s)	Total Release Rate (L/s)
10	104.19	14.44	6.40	3.78	0.00	3.78
15	83.56	11.58	7.02	3.78	0.00	3.78
20	70.25	9.74	7.15	3.78	0.00	3.78
25	60.90	8.44	6.99	3.78	0.00	3.78
30	53.93	7.47	6.65	3.78	0.00	3.78
35	48.52	6.73	6.18	3.78	0.00	3.78
40	44.18	6.12	5.63	3.78	0.00	3.78
45	40.63	5.63	5.00	3.78	0.00	3.78
50	37.65	5.22	4.32	3.78	0.00	3.78
55	35.12	4.87	3.59	3.78	0.00	3.78
60	32.94	4.57	2.83	3.78	0.00	3.78
65	31.04	4.30	2.04	3.78	0.00	3.78
70	29.37	4.07	1.22	3.78	0.00	3.78
75	27.89	3.87	0.39	3.78	0.00	3.78
80	26.56	3.68	0.00	3.78	0.00	3.78
85	25.37	3.52	0.00	3.78	0.00	3.78
90	24.29	3.37	0.00	3.78	0.00	3.78
95	23.31	3.23	0.00	3.78	0.00	3.78
100	22.41	3.11	0.00	3.78	0.00	3.78
105	21.58	2.99	0.00	3.78	0.00	3.78
110	20.82	2.89	0.00	3.78	0.00	3.78
115	20.12	2.79	0.00	3.78	0.00	3.78
120	19.47	2.70	0.00	3.78	0.00	3.78

On-site stormwater detention

Storage required = 7.15 m³
 Storage provided = 27.03 m³
 Available roof surface for storage = 540.60 m²
 Maximum ponding depth = 150 mm
 Available roof storage = 27.03 m³
 Proposed roof drains = Six (6) WATTS adjustable roof drain w/ weir opening-closed

5-Year Post-development Stormwater Management (except WS-04 Roof)

Time (min)	Intensity (mm/hr)	Controlled Runoff (L/s)	Storage Volume (m ³)	Controlled Release Rate (L/s)	Uncontrolled Runoff (L/s)	Total Release Rate (L/s)
10	104.19	23.93	8.53	9.71	2.90	12.61
15	83.56	19.19	8.53	9.71	2.32	12.04
20	70.25	16.13	7.70	9.71	1.95	11.67
25	60.90	13.98	6.41	9.71	1.69	11.41
30	53.93	12.38	4.81	9.71	1.50	11.21
35	48.52	11.14	3.00	9.71	1.35	11.06
40	44.18	10.15	1.04	9.71	1.23	10.94
45	40.63	9.33	0.00	9.71	1.13	10.84
50	37.65	8.65	0.00	9.71	1.05	10.76
55	35.12	8.07	0.00	9.71	0.98	10.69
60	32.94	7.57	0.00	9.71	0.92	10.63
65	31.04	7.13	0.00	9.71	0.86	10.58
70	29.37	6.75	0.00	9.71	0.82	10.53
75	27.89	6.40	0.00	9.71	0.78	10.49
80	26.56	6.10	0.00	9.71	0.74	10.45
85	25.37	5.83	0.00	9.71	0.71	10.42
90	24.29	5.58	0.00	9.71	0.68	10.39
95	23.31	5.35	0.00	9.71	0.65	10.36
100	22.41	5.15	0.00	9.71	0.62	10.34
105	21.58	4.96	0.00	9.71	0.60	10.31
110	20.82	4.78	0.00	9.71	0.58	10.29
115	20.12	4.62	0.00	9.71	0.56	10.27
120	19.47	4.47	0.00	9.71	0.54	10.25

On-site stormwater detention

Storage required = 8.53 m³
 Storage provided = 34.24 m³ (Parking lot surface storage)



LRL File No. 200572
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Stormwater Management

STORM - 2 YEAR

Runoff Equation

$Q = 2.78CIA$ (L/s)
 C = Runoff coefficient
 I = Rainfall intensity (mm/hr) = $A / (Td + C)^B$
 A = Area (ha)
 Td = Time of duration (min)

Pre-Development Catchments within Development Area

	Total Area =	0.185	ha	ΣR =	0.90
	EWS-01 (uncontrolled)	0.185	ha	R =	0.90
	Total Un-controlled =	0.185	ha	ΣR =	0.90

Pre-Development Release Rate

IDF Curve Equations

100-Year, $I_{100} = 1735.688 / (Td + 6.014)^{0.820}$ A = 1735.688 B = 0.820 C = 6.014

5-Year, $I_5 = 998.071 / (Td + 6.053)^{0.814}$ A = 998.071 B = 0.814 C = 6.053

2-Year, $I_2 = 732.951 / (Td + 6.199)^{0.810}$ A = 732.951 B = 0.810 C = 6.199

C = 0.50 (max 0.5 as per City Guidelines-Sewer)
 I_{100} = 178.6 mm/hr
 I_5 = 104.2 mm/hr
 I_2 = 76.8 mm/hr
 Td = 10 min

100-year Release Rate = 45.79 L/s
 5-year Release Rate = 26.72 L/s
 2-year Release Rate = 19.70 L/s

Allowable Release Rate = 19.70 L/s
 (2-year pre-development level)

Post-development Stormwater Management

				$\Sigma R_{2\&5}$	ΣR_{100}
	Total Site Area =	0.185	ha	ΣR =	0.77
	WS-01 (controlled)	0.015	ha	R =	0.40
	WS-02 (controlled)	0.049	ha	R =	1.00
	WS-03 (controlled)	0.043	ha	R =	1.00
Roof	WS-04 (controlled)	0.055	ha	R =	1.00
	Total (Controlled)	0.162	ha	R =	0.82
	WS-05 (uncontrolled)	0.003	ha	R =	0.27
	WS-06 (uncontrolled)	0.005	ha	R =	0.48
	WS-07 (uncontrolled)	0.014	ha	R =	0.64
	Total (Uncontrolled)	0.023	ha	R =	0.55
	Total	0.185	ha	R =	0.96



LRL File No. 200572
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Stormwater Management

2-Year Post-development Stormwater Management (WS-04 Roof)

Time (min)	Intensity (mm/hr)	Controlled Runoff (L/s)	Storage Volume (m ³)	Controlled Release Rate (L/s)	Uncontrolled Runoff (L/s)	Total Release Rate (L/s)
10	76.81	10.65	4.12	3.78	0.00	3.78
15	61.77	8.56	4.30	3.78	0.00	3.78
20	52.03	7.21	4.12	3.78	0.00	3.78
25	45.17	6.26	3.72	3.78	0.00	3.78
30	40.04	5.55	3.19	3.78	0.00	3.78
35	36.06	5.00	2.56	3.78	0.00	3.78
40	32.86	4.56	1.86	3.78	0.00	3.78
45	30.24	4.19	1.11	3.78	0.00	3.78
50	28.04	3.89	0.32	3.78	0.00	3.78
55	26.17	3.63	0.00	3.78	0.00	3.78
60	24.56	3.40	0.00	3.78	0.00	3.78
65	23.15	3.21	0.00	3.78	0.00	3.78
70	21.91	3.04	0.00	3.78	0.00	3.78
75	20.81	2.88	0.00	3.78	0.00	3.78
80	19.83	2.75	0.00	3.78	0.00	3.78
85	18.94	2.63	0.00	3.78	0.00	3.78
90	18.14	2.51	0.00	3.78	0.00	3.78
95	17.41	2.41	0.00	3.78	0.00	3.78
100	16.75	2.32	0.00	3.78	0.00	3.78
105	16.13	2.24	0.00	3.78	0.00	3.78
110	15.57	2.16	0.00	3.78	0.00	3.78
115	15.05	2.09	0.00	3.78	0.00	3.78
120	14.56	2.02	0.00	3.78	0.00	3.78

On-site stormwater detention

Storage required = 4.30 m³
Storage provided
 Available roof surface for storage = 540.60 m²
 Maximum ponding depth = 150 mm
Available roof storage = 27.03 m³
 Proposed roof drains = Six (6) WATTS adjustable roof drain w/ weir opening-closed

2-Year Post-development Stormwater Management (except WS-04 Roof)-surface storage consideration

Time (min)	Intensity (mm/hr)	Controlled Runoff (L/s)	Storage Volume (m ³)	Controlled Release Rate (L/s)	Uncontrolled Runoff (L/s)	Total Release Rate (L/s)
10	76.81	17.64	4.76	9.71	2.13	11.85
15	61.77	14.18	4.02	9.71	1.72	11.43
20	52.03	11.95	2.68	9.71	1.45	11.16
25	45.17	10.37	0.99	9.71	1.26	10.97
30	40.04	9.20	0.00	9.71	1.11	10.83
35	36.06	8.28	0.00	9.71	1.00	10.72
40	32.86	7.55	0.00	9.71	0.91	10.63
45	30.24	6.94	0.00	9.71	0.84	10.55
50	28.04	6.44	0.00	9.71	0.78	10.49
55	26.17	6.01	0.00	9.71	0.73	10.44
60	24.56	5.64	0.00	9.71	0.68	10.40
65	23.15	5.32	0.00	9.71	0.64	10.36
70	21.91	5.03	0.00	9.71	0.61	10.32
75	20.81	4.78	0.00	9.71	0.58	10.29
80	19.83	4.55	0.00	9.71	0.55	10.26
85	18.94	4.35	0.00	9.71	0.53	10.24
90	18.14	4.17	0.00	9.71	0.50	10.22
95	17.41	4.00	0.00	9.71	0.48	10.20
100	16.75	3.85	0.00	9.71	0.47	10.18
105	16.13	3.71	0.00	9.71	0.45	10.16
110	15.57	3.58	0.00	9.71	0.43	10.15
115	15.05	3.46	0.00	9.71	0.42	10.13
120	14.56	3.34	0.00	9.71	0.40	10.12

On-site stormwater detention Storage required = 4.76 m³



LRL File No. 200572
Project: Proposed 3-Storey Apartment Building
Location: 1465 Morisset Ave, Ottawa
Date: December 18, 2024
Designed: M. Basnet
Drawing Ref.: C601

Stormwater Management

2-Year Post-development Stormwater Management (except WS-04 Roof)-underground storage consideration

Time (min)	Intensity (mm/hr)	Controlled Runoff (L/s)	Storage Volume (m ³)	*Controlled Release Rate (L/s)	Uncontrolled Runoff (L/s)	Total Release Rate (L/s)
10	76.81	17.64	7.67	4.86	2.13	6.99
15	61.77	14.18	8.40	4.86	1.72	6.57
20	52.03	11.95	8.51	4.86	1.45	6.30
25	45.17	10.37	8.27	4.86	1.26	6.11
30	40.04	9.20	7.81	4.86	1.11	5.97
35	36.06	8.28	7.19	4.86	1.00	5.86
40	32.86	7.55	6.46	4.86	0.91	5.77
45	30.24	6.94	5.64	4.86	0.84	5.70
50	28.04	6.44	4.75	4.86	0.78	5.64
55	26.17	6.01	3.81	4.86	0.73	5.58
60	24.56	5.64	2.82	4.86	0.68	5.54
65	23.15	5.32	1.79	4.86	0.64	5.50
70	21.91	5.03	0.74	4.86	0.61	5.47
75	20.81	4.78	0.00	4.86	0.58	5.43
80	19.83	4.55	0.00	4.86	0.55	5.41
85	18.94	4.35	0.00	4.86	0.53	5.38
90	18.14	4.17	0.00	4.86	0.50	5.36
95	17.41	4.00	0.00	4.86	0.48	5.34
100	16.75	3.85	0.00	4.86	0.47	5.32
105	16.13	3.71	0.00	4.86	0.45	5.30
110	15.57	3.58	0.00	4.86	0.43	5.29
115	15.05	3.46	0.00	4.86	0.42	5.27
120	14.56	3.34	0.00	4.86	0.40	5.26

Note: *50% of controlled release rate for underground storage consideration

On-site stormwater detention

Storage required = 8.51 m³

Available Storage

Pipe Storage

STM Pipe Length = 38.4 m

STM Pipe dia. = 0.45 m

Storage Volume = 6.11 m³

CBMH Storage

	dia. (m)	Depth (T/G -Inv) (m)	Storage Volume (m ³)
CBMH02	1.2	1.27	1.44
CBMH03	1.2	1.31	1.48
Total			2.92

Total Available Underground Storage = 9.03 m³



LRL File No. 200572

Project: Proposed 3-Storey Apartment Building

Location: 1465 Morisset Ave, Ottawa

Date: December 18, 2024

Designed: M. Basnet

Dwg. Reference: C401,C702

Rational Method

Q = 2.78CIA

Q = Peak flow (L/s)

A = Drainage area (ha)

C = Runoff coefficient

I = Rainfall intensity (mm/hr)

Runoff coefficient (C)

Grass = 0.2

Gravel = 0.8

Asphalt / rooftop = 0.9

IDF curve

Ottawa Macdonald-Cartier International Airport

Storm event: 2 Years

Intensity equation:

$$I_2 = 732.951 / (Td + 6.199)^{0.810} \text{ (mm/hr)}$$

Pipe Design Parameters

Minimum velocity = 0.80 m/s

Manning's "n" = 0.013

LOCATION			AREA (ha)			FLOW						STORM SEWER							
WATERSHED / STREET	From MH	To MH	C = 0.20	C = 0.80	C = 0.90	Indiv. 2.78AC	Accum. 2.78AC	Time of Conc.	Rainfall Intensity	Peak Flow (Q)	Controlled Flow (Q)	Pipe Dia.	Type	Slope	Length	Capacity Full (Q _{FULL})	Velocity Full	Time of Flow	Ratio Q / Q _{FULL}
									(mm/hr)	(L/s)	(L/s)								
WS-01	CB01	CBMH02	0.012	0.003	0.000	0.01	0.01	10.00	76.81	1.01		450	CONC	0.34%	24.2	166.24	1.05	0.39	0.01
WS-02	CBMH02	CBMH03	0.005	0.000	0.044	0.11	0.13	10.39	75.35	9.51		450	CONC	0.30%	14.2	156.16	0.98	0.24	0.06
WS-07	CB 04	STM Connection*	0.008	0.000	0.006	0.02	0.02	10.00	76.81	1.55		200	PVC	3.00%	22.7	56.81	1.81	0.21	0.03
WS-03	CBMH03**	MH05	0.002	0.000	0.041	0.10	0.23	10.63	74.48	17.10	9.71	300	PVC	1.00%	14.2	96.70	1.37	0.17	0.18

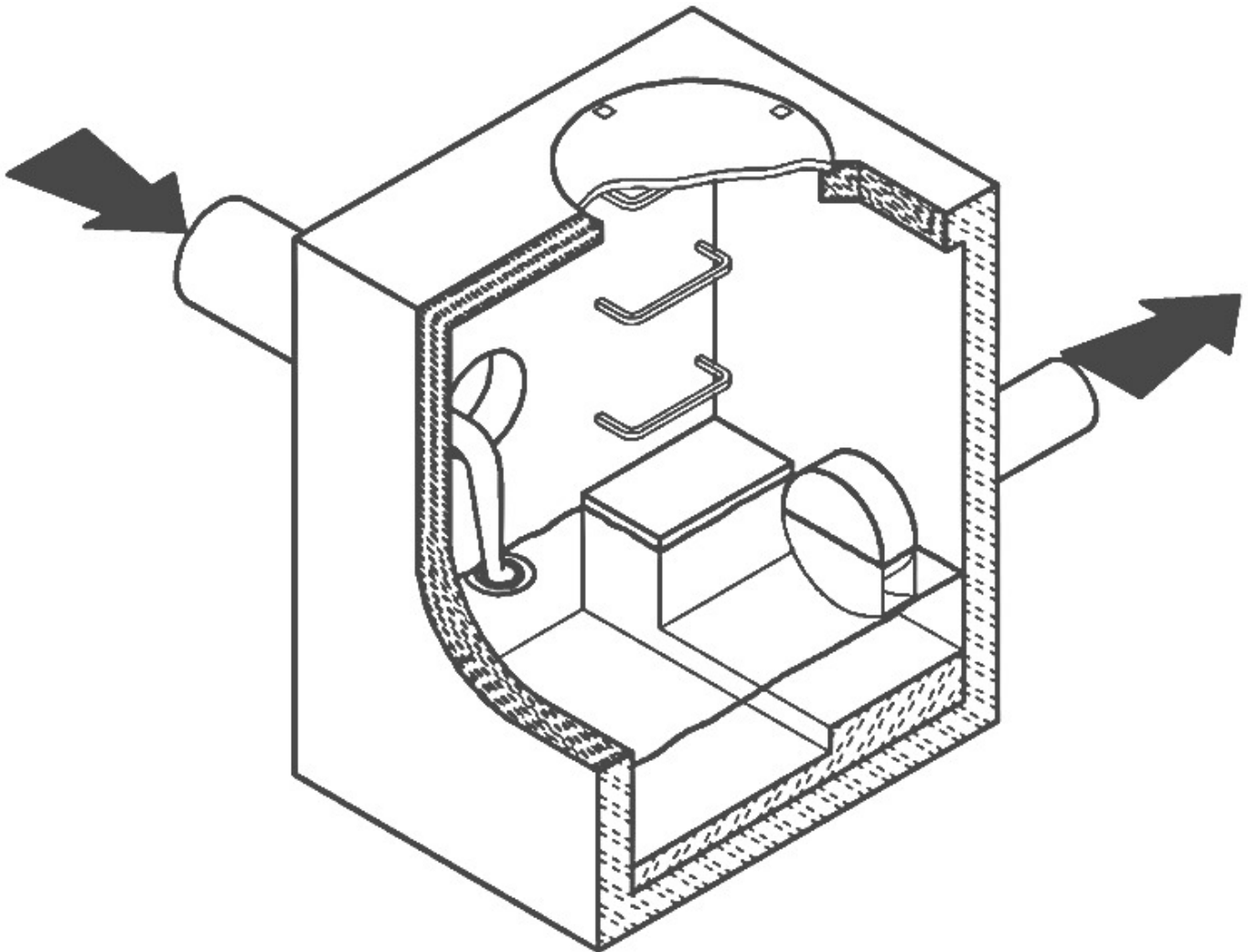
Note:

* STM connection downstream of CBMH03

**An ICD to be installed at CBMH03 will control flow at 9.71 L/s



HYDROVEX[®] VHV / SVHV
Vertical Vortex Flow Regulator



JOHN MEUNIER

HYDROVEX® VHV / SVHV VERTICAL VORTEX FLOW REGULATOR

APPLICATIONS

One of the major problems of urban wet weather flow management is the runoff generated after a heavy rainfall. During a storm, uncontrolled flows may overload the drainage system and cause flooding. Due to increased velocities, sewer pipe wear is increased dramatically and results in network deterioration. In a combined sewer system, the wastewater treatment plant may also experience significant increases in flows during storms, thereby losing its treatment efficiency.

A simple means of controlling excessive water runoff is by controlling excessive flows at their origin (manholes). **John Meunier Inc.** manufactures the **HYDROVEX® VHV / SVHV** line of vortex flow regulators to control stormwater flows in sewer networks, as well as manholes.

The vortex flow regulator design is based on the fluid mechanics principle of the forced vortex. This grants flow regulation without any moving parts, thus reducing maintenance. The operation of the regulator, depending on the upstream head and discharge, switches between orifice flow (gravity flow) and vortex flow. Although the concept is quite simple, over 12 years of research have been carried out in order to get a high performance.

The **HYDROVEX® VHV / SVHV** Vertical Vortex Flow Regulators (refer to **Figure 1**) are manufactured entirely of stainless steel, and consist of a hollow body (1) (in which flow control takes place) and an outlet orifice (7). Two rubber "O" rings (3) seal and retain the unit inside the outlet pipe. Two stainless steel retaining rings (4) are welded on the outlet sleeve to ensure that there is no shifting of the "O" rings during installation and use.

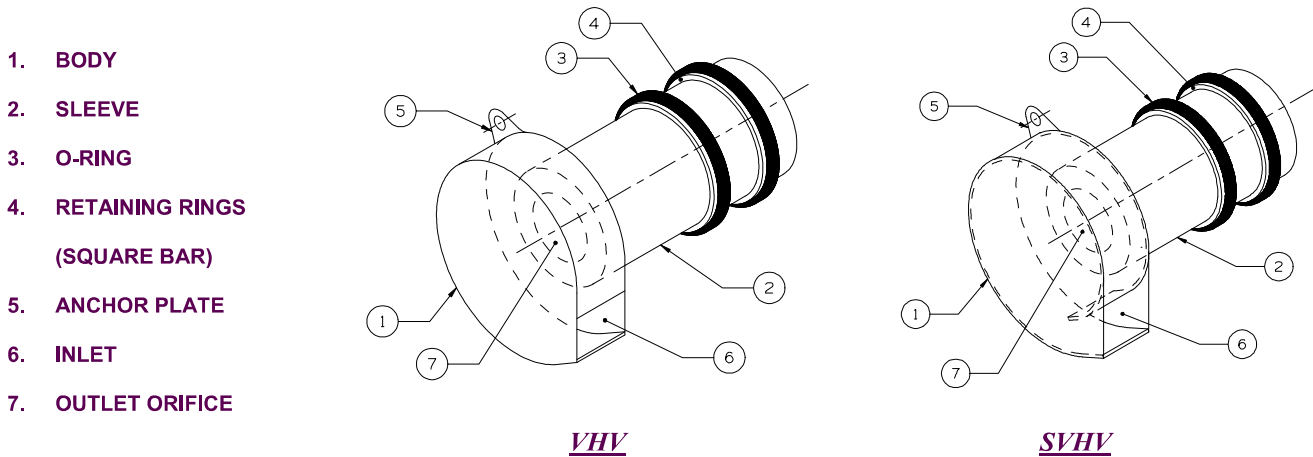


FIGURE 1: HYDROVEX® VHV-SVHV VERTICAL VORTEX FLOW REGULATORS

ADVANTAGES

- The **HYDROVEX® VHV / SVHV** line of flow regulators are manufactured entirely of stainless steel, making them durable and corrosion resistant.
- Having no moving parts, they require minimal maintenance.
- The geometry of the **HYDROVEX® VHV / SVHV** flow regulators allows a control equal to an orifice plate, having a cross section area 4 to 6 times smaller. This decreases the chance of blockage of the regulator, due to sediments and debris found in stormwater flows. **Figure 2** illustrates the comparison between a regulator model 100 SVHV-2 and an equivalent orifice plate. One can see that for the same height of water, the regulator controls a flow approximately four times smaller than an equivalent orifice plate.
- Installation of the **HYDROVEX® VHV / SVHV** flow regulators is quick and straightforward and is performed after all civil works are completed.
- Installation requires no special tools or equipment and may be carried out by any contractor.
- Installation may be carried out in existing structures.

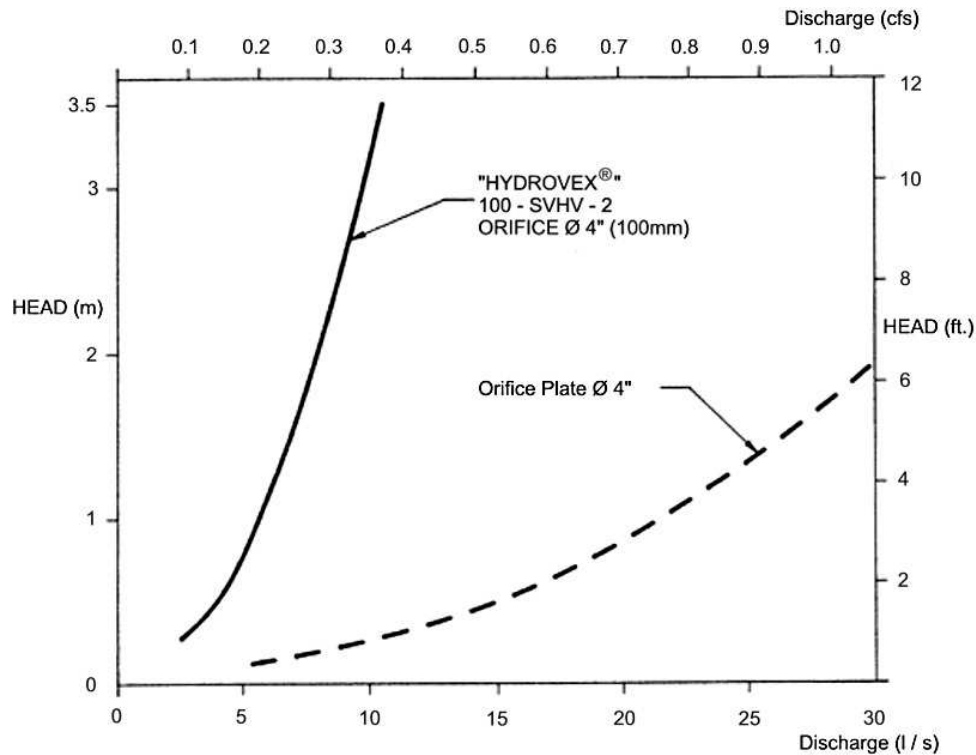


FIGURE 2: DISCHARGE CURVE SHOWING A HYDROVEX® FLOW REGULATOR VS AN ORIFICE PLATE

SELECTION

Selection of a **VHV** or **SVHV** regulator can be easily made using the selection charts found at the back of this brochure (see **Figure 3**). These charts are a graphical representation of the maximum upstream water pressure (head) and the maximum discharge at the manhole outlet. The maximum design head is the difference between the maximum upstream water level and the invert of the outlet pipe. All selections should be verified by John Meunier Inc. personnel prior to fabrication.

Example:

- ✓ Maximum design head 2m (6.56 ft.)
- ✓ Maximum discharge 6 L/s (0.2 cfs)
- ✓ Using **Figure 3** - VHV model required is a **75 VHV-1**

INSTALLATION REQUIREMENTS

All **HYDROVEX®** **VHV** / **SVHV** flow regulators can be installed in circular or square manholes. **Figure 4** gives the various minimum dimensions required for a given regulator. *It is imperative to respect the minimum clearances shown to ensure easy installation and proper functioning of the regulator.*

SPECIFICATIONS

In order to specify a **HYDROVEX**[®] regulator, the following parameters must be defined:

- The model number (ex: 75-VHV-1)
- The diameter and type of outlet pipe (ex: 6" diam. SDR 35)
- The desired discharge (ex: 6 l/s or 0.21 CFS)
- The upstream head (ex: 2 m or 6.56 ft.) *
- The manhole diameter (ex: 36" diam.)
- The minimum clearance "H" (ex: 10 inches)
- The material type (ex: 304 s/s, 11 Ga. standard)

* *Upstream head is defined as the difference in elevation between the maximum upstream water level and the invert of the outlet pipe where the **HYDROVEX**[®] flow regulator is to be installed.*

PLEASE NOTE THAT WHEN REQUESTING A PROPOSAL, WE SIMPLY REQUIRE THAT YOU PROVIDE US WITH THE FOLLOWING:

- *project design flow rate*
- *pressure head*
- *chamber's outlet pipe diameter and type*



Typical VHV model in factory

OPTIONS



FV – SVHV (mounted on sliding plate)



VHV-1-O (standard model with odour control inlet)



FV – VHV-O (mounted on sliding plate with odour control inlet)



VHV with Gooseneck assembly in existing chamber without minimum release at the bottom



VHV with air vent for minimal slopes



VHV Vertical Vortex Flow Regulator

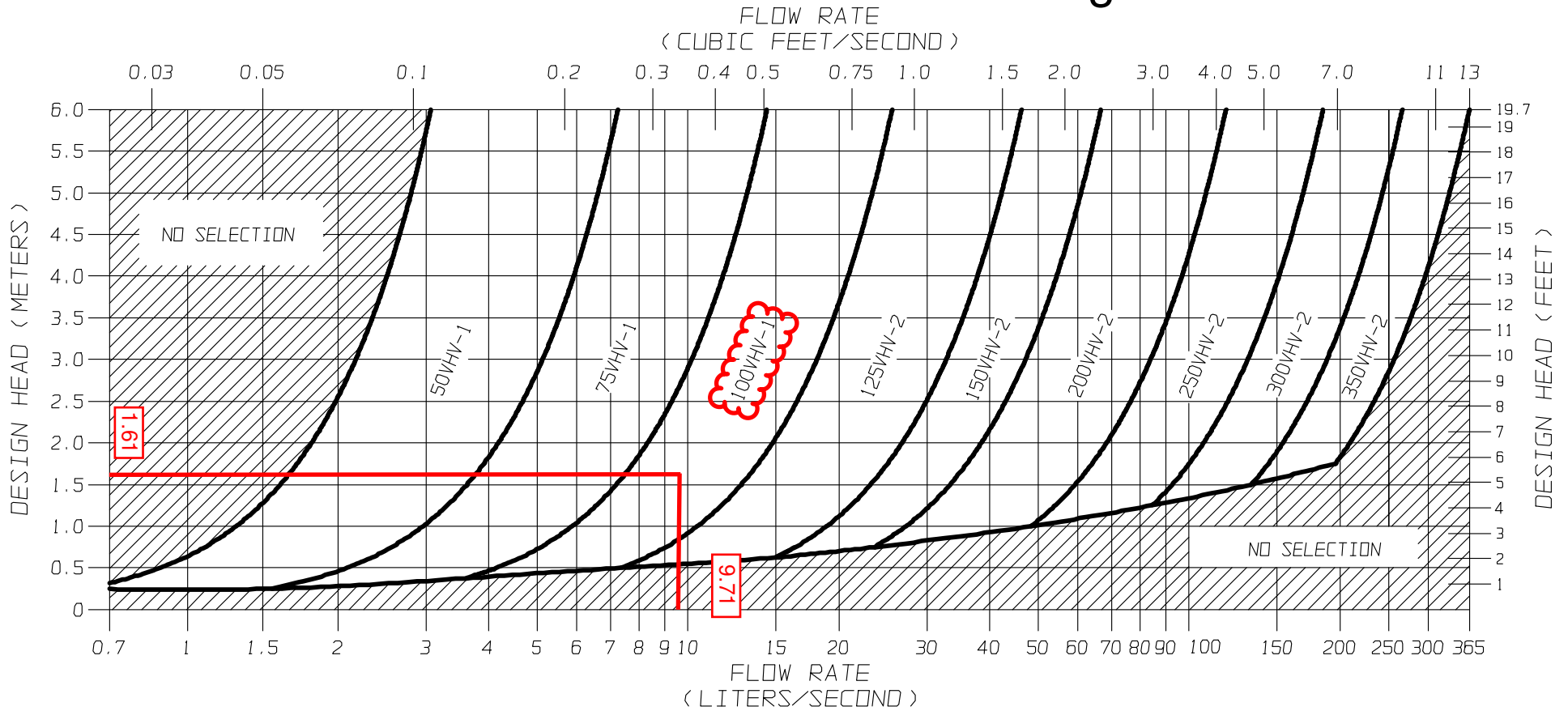
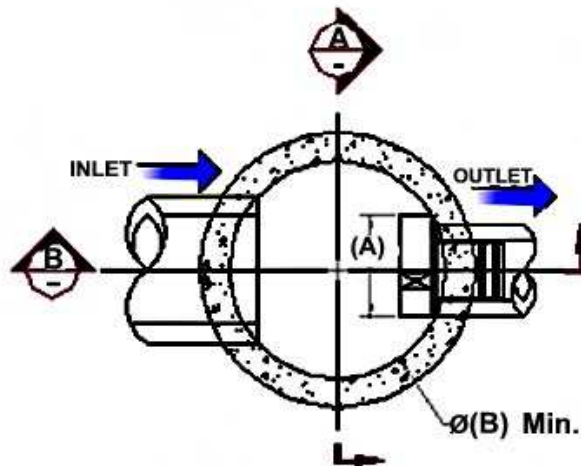


FIGURE 3 - VHV

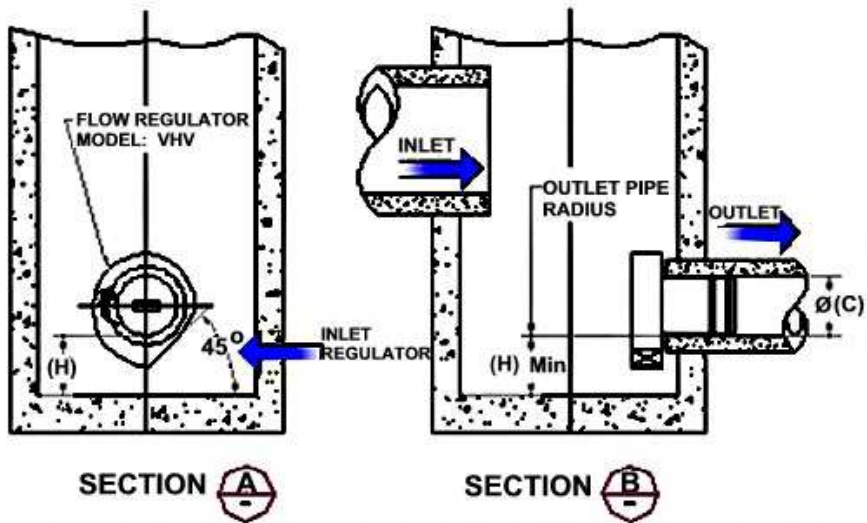
JOHN MEUNIER

**FLOW REGULATOR TYPICAL INSTALLATION IN CIRCULAR MANHOLE
FIGURE 4 (MODEL VHV)**

Model Number	Regulator Diameter		Minimum Manhole Diameter		Minimum Outlet Pipe Diameter		Minimum Clearance	
	A (mm)	A (in.)	B (mm)	B (in.)	C (mm)	C (in.)	H (mm)	H (in.)
50VHV-1	150	6	600	24	150	6	150	6
75VHV-1	250	10	600	24	150	6	150	6
100VHV-1	325	13	900	36	150	6	200	8
125VHV-2	275	11	900	36	150	6	200	8
150VHV-2	350	14	900	36	150	6	225	9
200VHV-2	450	18	1200	48	200	8	300	12
250VHV-2	575	23	1200	48	250	10	350	14
300VHV-2	675	27	1600	64	250	10	400	16
350VHV-2	800	32	1800	72	300	12	500	20



CIRCULAR WELL



SECTION A

SECTION B

INSTALLATION

The installation of a **HYDROVEX**[®] regulator may be undertaken once the manhole and piping is in place. Installation consists of simply fitting the regulator into the outlet pipe of the manhole. **John Meunier Inc.** recommends the use of a lubricant on the outlet pipe, in order to facilitate the insertion and orientation of the flow controller.

MAINTENANCE

HYDROVEX[®] regulators are manufactured in such a way as to be maintenance free; however, a periodic inspection (every 3-6 months) is suggested in order to ensure that neither the inlet nor the outlet has become blocked with debris. The manhole should undergo periodically, particularly after major storms, inspection and cleaning as established by the municipality

GUARANTY

The **HYDROVEX**[®] line of **VHV / SVHV** regulators are guaranteed against both design and manufacturing defects for a period of 5 years. Should a unit be defective, **John Meunier Inc.** is solely responsible for either modification or replacement of the unit.

John Meunier Inc.

ISO 9001 : 2008

Head Office

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Saint-Laurent (Quebec) Canada H4S 2B3

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Glenside, PA USA 19038

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Fax: 215-885-4741 astele@johnmeunier.com



ADJUSTABLE ACCUTROL (for Large Sump Roof Drains only)

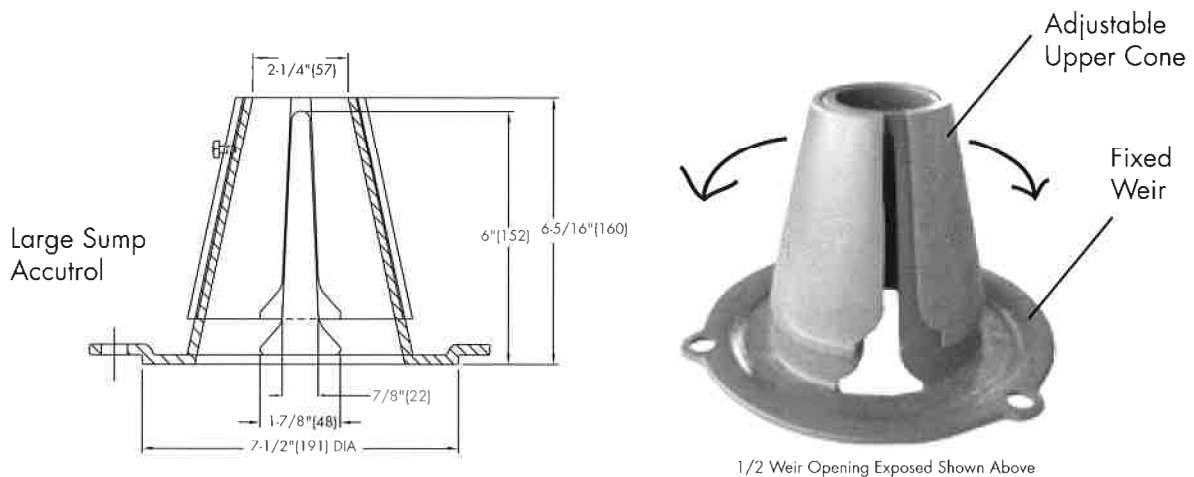
For more flexibility in controlling flow with heads deeper than 2", Watts Drainage offers the Adjustable Accutrol. The Adjustable Accutrol Weir is designed with a single parabolic opening that can be covered to restrict flow above 2" of head to less than 5 gpm per inch, up to 6" of head. To adjust the flow rate for depths over 2" of head, set the slot in the adjustable upper cone according to the flow rate required. Refer to Table 1 below.

Note: Flow rates are directly proportional to the amount of weir opening that is exposed.

EXAMPLE:

For example, if the adjustable upper cone is set to cover 1/2 of the weir opening, flow rates above 2" of head will be restricted to 2-1/2 gpm per inch of head.

Therefore, at 3" of head, the flow rate through the Accutrol Weir that has 1/2 the slot exposed will be:
 [5 gpm(per inch of head) x 2 inches of head] + 2-1/2 gpm(for the third inch of head) = 12-1/2 gpm.


TABLE 1. Adjustable Accutrol Flow Rate Settings

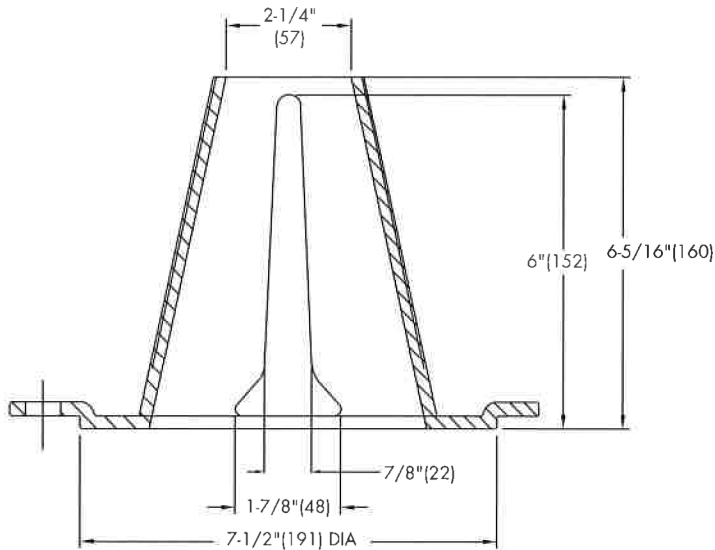
Weir Opening Exposed	Head of Water					
	1"	2"	3"	4"	5"	6"
	Flow Rate (gallons per minute)					
Fully Exposed	5	10	15	20	25	30
3/4	5	10	13.75	17.5	21.25	25
1/2	5	10	12.5	15	17.5	20
1/4	5	10	11.25	12.5	13.75	15
Closed	5	10	10	10	10	10

Job Name _____ Model No. _____
 Job Location _____ Contractor _____
 Engineer _____ Representative _____

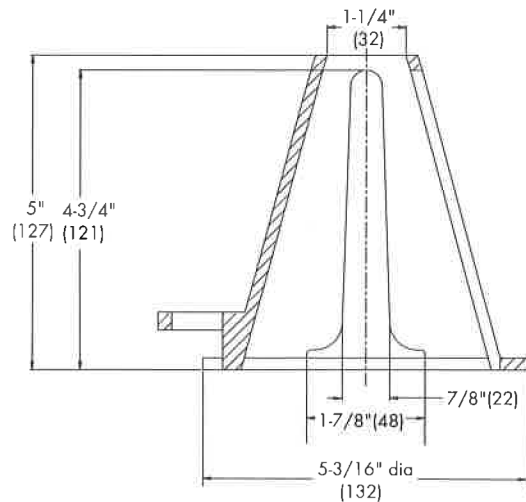
ACCUTROL WEIR FLOW CONTROL

SPECIFICATION: Watts Drainage Products epoxy coated cast iron Accutrol Weir is designed with parabolic openings which limit the flow of rain water off a roof. Each weir slot controls flow to 5 gpm per inch of head to a maximum of 30 gpm at 6" head (for large sump), 25 gpm at 5" head (for small sump). The Accutrol Weir is secured to the flashing clamp of the roof drain. The Accutrol Weir is available with 1 to 4 slots for the large sump drain and up to 3 slots for the small sump drain.

For Large Sump Roof Drains Specify the "-A" option and number of slots required. (ie. "RD-100-A2" for two slot weir)
For Small Sump Roof Drains Specify the "-A" option and number of slots required. (ie. "RD-200-A1" for one slot weir)



LARGE SUMP ACCUTROL WEIR



SMALL SUMP ACCUTROL WEIR

Job Name _____ Model No. _____
 Job Location _____ Contractor _____
 Engineer _____ Representative _____

APPENDIX C
Water Supply Calculations

Sarthak Vora

From: Cassidy, Tyler <tyler.cassidy@ottawa.ca>
Sent: Friday, December 13, 2024 11:08 AM
To: Sarthak Vora
Cc: Mohan Basnet; Lodoen Unseth, Kelby
Subject: Boundary Conditions: 1435 Morisset Avenue
Attachments: 1435 Morisset Ave November 2024.pdf

Good Morning,

Please find below the boundary conditions for 1435 Morisset Avenue.

******The following information may be passed on to the consultant, but do NOT forward this e-mail directly.******

The following are boundary conditions, HGL, for hydraulic analysis at 1435 Morisset Avenue (zone ME) assumed to be connected to the 152mm watermain on Morisset Avenue. (see attached PDF for location).

Minimum HGL = 146.9 m

Maximum HGL = 158.3 m

Max Day + Fire Flow (75 L/s) = 124.7 m

These are for current conditions and are based on computer model simulation.

Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation. Fire Flow analysis is a reflection of available flow in the watermain; there may be additional restrictions that occur between the watermain and the hydrant that the model cannot take into account.

Thank you,

I will be away on leave from December 16th, 2024, returning January 27th, 2025. Please contact Roshni Thakur at roshni.thakur@ottawa.ca for all inquiries and submissions.

Tyler Cassidy, P.Eng

Infrastructure Project Manager,

Planning, Development and Building Services department (PDBS)/ Direction générale des services de la planification, de l'aménagement et du bâtiment (DGSPAB) - South Branch

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613.580.2424 ext./poste 12977, Tyler.Cassidy@ottawa.ca

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Water Supply Calculations

LRL File No. 200572

Project: Proposed 3-Storey Apartment Building

Location: 1465 Morisset Ave, Ottawa, ON

Date: December 5, 2024

Prepared by: M. Basnet

Residential Demand based on the City of Ottawa Design Guidelines-Water Distribution, 2010

Unit Type	Persons Per Unit	Number of Units	Population
1-Bedroom Apartment	1.4	16	22.4
2-Bedroom Apartment	2.1	15	31.5
Total		31	53.9

Average Water Consumption Rate	350 L/c/d	
Average Day Demand	18,865 L/d	0.22 L/s
Maximum Day Factor	7.5	(MOE Table 3-3)
Maximum Daily Demand	140,721 L/d	1.63 L/s
Peak Hour Factor	11.2	(MOE Table 3-3)
Maximum Hour Demand	1,578,953 L/d	18.27 L/s

Water Service Pipe Sizing

$$Q = VA$$

Where:

V = velocity

A = area of pipe

Q = flow rate

Assuming a maximum velocity of 1.8m/s, the diameter of pipe is calculated as:

$$\begin{aligned} \text{Minimum pipe diameter (d)} &= (4Q/\pi V)^{1/2} \\ &= 0.114 \quad \text{m} \\ &= 114 \quad \text{mm} \end{aligned}$$

$$\text{Proposed pipe diameter (d)} = 100 \quad \text{mm}$$



Fire Flow Calculations as per Ontario Building Code (OBC)

LRL File No. : 200572

Project : Proposed 3-Storey Low-Rise Apartment

Location : 1465 Morisset Ave, Ottawa, ON

Date : December 5, 2024

Prepared by : S. Vora

Fire Protection Water Supply Calculations

$$Q = KVS_{Tot}$$

where

Q = minimum supply of water (L)

K = water supply coefficient from Table 1 of the OFM guidelines

V = total building volume (m³)

S_{Tot} = total of spatial coefficient values from property line exposures on all sides

$$S_{Tot} = 1.0 + (S_{side1} + S_{side2} + S_{side3} + S_{side4})$$

	Exposure Distance (m)
S _{Side1} = 0.00	>10 (North)
S _{Side2} = 0.00	>10 (East)
S _{Side3} = 0.00	>10 (South)
S _{Side4} = 0.25	7.8 (West)
S_{Tot} = 1.25	

K = 18 (Group C-combustible construction with fire separations and fire resistance ratings)

Building Information based on Architectural Drawing

Floor Area = 561 m²

Prop Bldg Height = 12.10 m

V = 6788 m³

Q = 152732 L

Required Minimum Water Supply Flow Rate = 4500 L / min (as per OFM Table 2)
75 L/s

Fire Hydrant Distance to Bldg.

-  ≤ 76 m
-  $\geq 152 \leq 305$ m

SUBJECT SITE



APPENDIX D
Sanitary Calculations

From: Cassidy, Tyler <tyler.cassidy@ottawa.ca>
Sent: Wednesday, November 27, 2024 3:29 PM
To: Sarthak Vora
Cc: Mohan Basnet; Lodoen Unseth, Kelby
Subject: RE: 1435 &1455 Morisset_Boundary Condition & Sanitary Sewer capacity req

Hi Sarthak,

There is sufficient capacity in the sanitary sewer to accommodate this proposal.

I have submitted the boundary conditions to our Water Resources group, please allow for up to 10 business days for the results to be provided.

Thank you,

I will be away on leave from December 16th, 2024, returning January 23rd, 2025.

Tyler Cassidy, P.Eng

Infrastructure Project Manager,

Planning, Development and Building Services department (PDBS)/ Direction générale des services de la planification, de l'aménagement et du bâtiment (DGSPAB) - South Branch

City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1

613.580.2424 ext./poste 12977, Tyler.Cassidy@ottawa.ca

From: Sarthak Vora <svora@lrl.ca>
Sent: November 26, 2024 3:54 PM
To: Cassidy, Tyler <tyler.cassidy@ottawa.ca>
Cc: Mohan Basnet <mbasnet@lrl.ca>; Lodoen Unseth, Kelby <Kelby.LodoenUnseth@ottawa.ca>
Subject: RE: 1435 &1455 Morisset_Boundary Condition & Sanitary Sewer capacity req

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Hi Tyler,

Please find attached the correspondence email from Adam Baker dated June 14, 2021, regarding the OBC fire flow calculation, in pdf format.

Regarding the sanitary demand, the total flow from the site is calculated as 0.76L/s, which includes:

- Peak flow - 0.70L/s
- Infiltration flow - 0.06L/s

This brings the total flow to 0.76L/s.

Please let me know if any additional clarification/ details are required.

Regards,

Sarthak Vora, Civil E.I.T



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From: Cassidy, Tyler <tyler.cassidy@ottawa.ca>

Sent: Tuesday, November 26, 2024 3:31 PM

To: Sarthak Vora <svora@lrl.ca>

Cc: Mohan Basnet <mbasnet@lrl.ca>; Lodoen Unseth, Kelby <Kelby.LodoenUnseth@ottawa.ca>

Subject: RE: 1435 &1455 Morisset_Boundary Condition & Sanitary Sewer capacity req

Hi Sarthak,

Are you able to provide the correspondence that indicated you should be using the OBC method to calculate fire flow? We don't typically allow that and always request the FUS 2020 calculations per our technical bulletins/guidelines. If not, could you please provide the FUS calculations for required fire flow? I will then be able to proceed with the request to our water resources and fire protection services groups.

For the sanitary demand, is the 0.76 L/s peak flow or average flow? Please confirm.

Thank you,

I will be away on leave from December 16th, 2024, returning January 23rd, 2025.

Tyler Cassidy, P.Eng

Infrastructure Project Manager,

Planning, Development and Building Services department (PDBS)/ Direction générale des services de la planification, de l'aménagement et du bâtiment (DGSPAB) - South Branch

City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1

613.580.2424 ext./poste 12977, Tyler.Cassidy@ottawa.ca

From: Sarthak Vora <svora@lrl.ca>

Sent: November 26, 2024 2:25 PM

To: Cassidy, Tyler <tyler.cassidy@ottawa.ca>

Cc: Mohan Basnet <mbasnet@lrl.ca>; Lodoen Unseth, Kelby <Kelby.LodoenUnseth@ottawa.ca>

Subject: RE: 1435 &1455 Morisset_Boundary Condition & Sanitary Sewer capacity req

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Good Afternoon Tyler,

Thankyou for assisting us with the confirmation.

I would like to confirm the boundary conditions and sanitary sewer capacity for the proposed development at 1435 Morisset Avenue. The project involves the construction of a 3-storey building with a total of 31 units. We are proposing a 150mm diameter service connection to the 150mm diameter municipal watermain on Morisset Avenue.

We previously requested boundary conditions on May 11, 2021 (see attached email PDF) and received the following results:

Minimum HGL = 143.7 m

Maximum HGL = 158.2 m

Available Flow at 20 psi = 85 L/s, assuming ground elevation of 97.6 m

The water demand for the proposed development has not changed since the last request and remains consistent. Could you kindly provide the current boundary conditions? For your reference, I have included the proposed development demands below, along with the domestic demand and OBC fire flow calculations. Please note that we were advised to use OBC fire flow calcs due to lower than average pressure in the watermain and the required fire flow rate is less than 9000L/min.

	Demand (L/s)
Avg. Daily	0.22
Max. Day + OBC	1.63 + 75
Peak Hour	18.27

Sanitary Connection

We also determined that the sanitary sewer discharge from the site would stay constant to be **0.76L/s**. We are proposing to tie into the 225mm Conc Sanitary Sewer located within Morisset Avenue. The previous Sanitary Sewer confirmation is attached. Please re-confirm if the existing sanitary sewer will have sufficient capacity to accommodate our site.



I am currently working towards a pressing submission deadline and would greatly appreciate your prompt response. Please let me know if any additional information is required.

Regards,

Sarthak Vora, Civil E.I.T



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www.lrl.ca

From: Cassidy, Tyler <tyler.cassidy@ottawa.ca>

Sent: Tuesday, November 26, 2024 11:10 AM

To: Sarthak Vora <svora@lrl.ca>

Cc: Mohan Basnet <mbasnet@lrl.ca>; Lodoen Unseth, Kelby <Kelby.LodoenUnseth@ottawa.ca>
Subject: RE: 1435 &1455 Morisset_Boundary Condition & Sanitary Sewer capacity req

Hi Sarthak,

I can help you with your request. If you could please provide your proposed sanitary peak flows, as well as the following information for boundary conditions, then I will confirm capacity/pressure for you:

- Location of service
- Type of development and the amount of fire flow required (as per FUS)
- FUS calculations
- Average daily demand: ___ l/s.
- Maximum daily demand: ___ l/s.
- Maximum hourly daily demand: ___ l/s

Thank you,

I will be away on leave from December 16th, 2024, returning January 23rd, 2025.

Tyler Cassidy, P.Eng

Infrastructure Project Manager,

Planning, Development and Building Services department (PDBS)/ Direction générale des services de la planification, de l'aménagement et du bâtiment (DGSPAB) - South Branch

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110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1

613.580.2424 ext./poste 12977, Tyler.Cassidy@ottawa.ca

From: Sarthak Vora <svora@lrl.ca>

Sent: November 25, 2024 3:40 PM

To: Shillington, Jeffrey <jeff.shillington@ottawa.ca>; Sharif, Golam <sharif.sharif@ottawa.ca>

Cc: Mohan Basnet <mbasnet@lrl.ca>

Subject: Re: 1435 &1455 Morisset_Boundary Condition & Sanitary Sewer capacity req

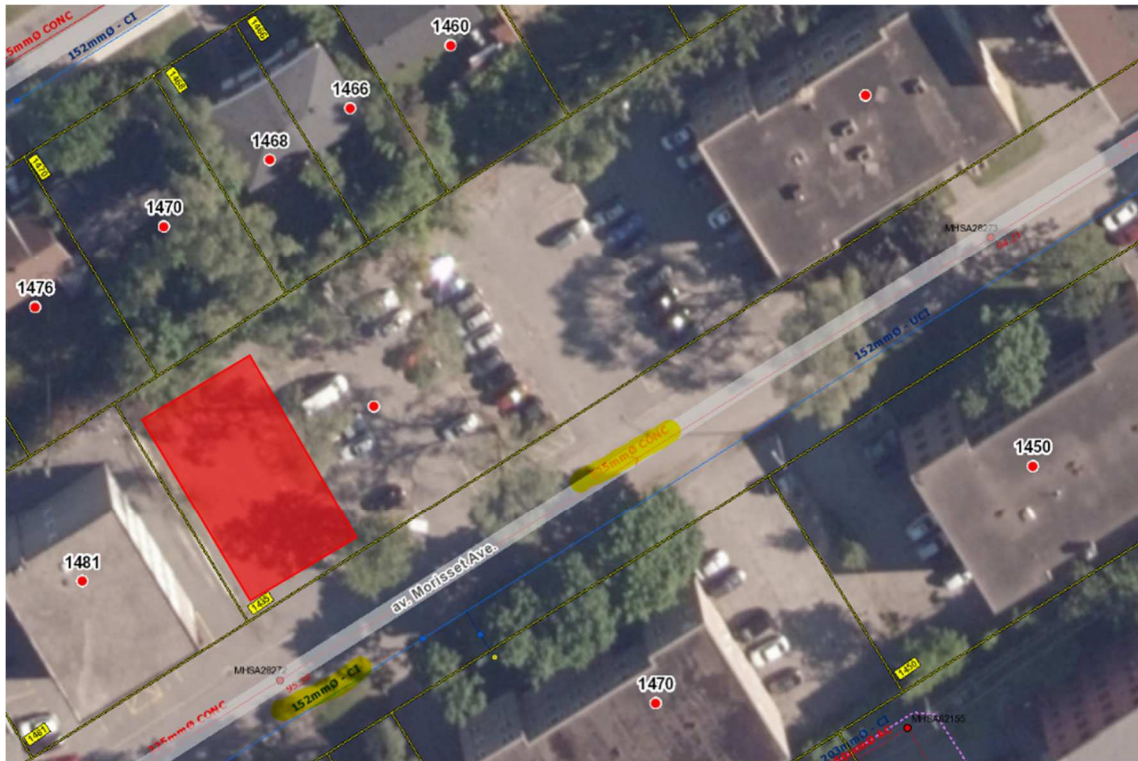
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Good Afternoon, Jeff/ Sharif,

We are working on a proposed development at 1435 &1455 Morisset Avenue and would like to confirm the **boundary conditions and sanitary sewer capacity** for the project. The development includes the construction of a 3-storey building with a total of 31 units. A full SPC package was previously completed, and we had requested and received boundary conditions from Adam Baker (adam.baker@ottawa.ca) on May 11, 2021. However, due to a revision in the site plan, the civil drawings and calculations now need to be updated for the SPC amendment. I re-requested the boundary conditions from Adam

last week but have not yet received a response.



Would you be able to assist me with this request, or should I reach out to someone else for further support?

Thank you for your time and assistance.

Sarthak Vora, Civil E.I.T



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'



LRL File No.: 200572
Project: Proposed Low Rise Apartment
Location: 1465 Morisset Ave, Ottawa, ON
Date: 2024/12/05
Designed: M. Basnet

Average Daily Flow = 280 L/p/day
 Commercial & Institutional Flow = 28000 L/ha/day
 Light Industrial Flow = 35000 L/ha/day
 Heavy Industrial Flow = 55000 L/ha/day
 Maximum Residential Peak Factor = 4.0
 Commercial & Institutional Peak Factor = 1.5

Sanitary Design Parameters

Industrial Peak Factor = as per Appendix 4-B
 Extraneous Flow = 0.33 L/s/gross ha
 (as Per Tech Bulletin ISTB-2018-01)

Pipe Design Parameters

Minimum Velocity = 0.60 m/s
 Manning's n = 0.013

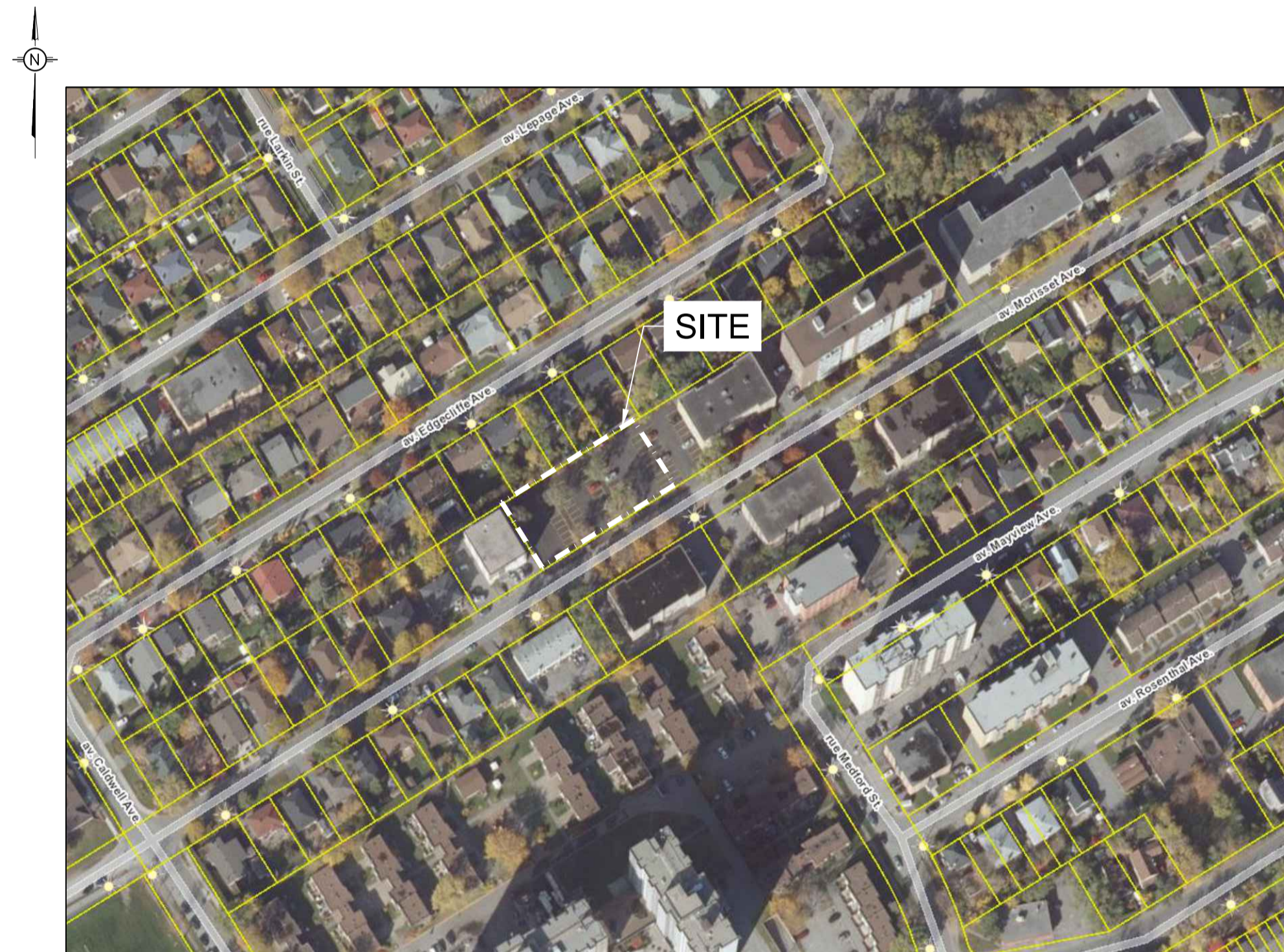
LOCATION			RESIDENTIAL AREA AND POPULATION						COMMERCIAL		INDUSTRIAL			INSTITUTIONAL		C+I+I	INFILTRATION			TOTAL FLOW	PIPE						
STREET/SITE	FROM MH	TO MH	AREA (Ha)	POP.	CUMMULATIVE		PEAK FACT.	PEAK FLOW (l/s)	AREA (Ha)	ACCU. AREA (Ha)	AREA (Ha)	ACCU. AREA (Ha)	PEAK FACT.	AREA (Ha)	ACCU. AREA (Ha)	PEAK FLOW (l/s)	TOTAL AREA (Ha)	ACCU. AREA (Ha)	INFILT. FLOW (l/s)	TOTAL FLOW (l/s)	LENGTH (m)	DIA. (mm)	SLOPE (%)	MATERIAL	CAP. (FULL) (l/s)	VEL. (FULL) (m/s)	*VEL. (ACTUAL) (m/s)
					AREA (Ha)	POP.																					
	Bldg.	SAN MH01	0.185	53.9	0.19	53.9	4.0	0.70									0.19	0.19	0.06	0.76	13.7	150	3.00%	PVC	26.38	1.49	0.66

Note:
 * Actual velocity > self-cleansing velocity

APPENDIX E
Civil Engineering Drawings

PROPOSED 3-STOREY APARTMENT BUILDING 1465 MORISSET AVE, OTTAWA, ON

REVISION 02



KEY PLAN (N.T.S.)

DRAWING INDEX	
TITLE PAGE	
GENERAL NOTES	C001
SEDIMENT AND EROSION CONTROL PLAN	C101
DEMOLITION PLAN	C102
GRADING AND DRAINAGE PLAN	C301
SERVICING PLAN	C401
STORMWATER MANAGEMENT PLAN	C601
PRE-DEVELOPMENT WATERSHED PLAN	C701
POST-DEVELOPMENT WATERSHED PLAN	C702
CONSTRUCTION DETAIL PLAN	C901



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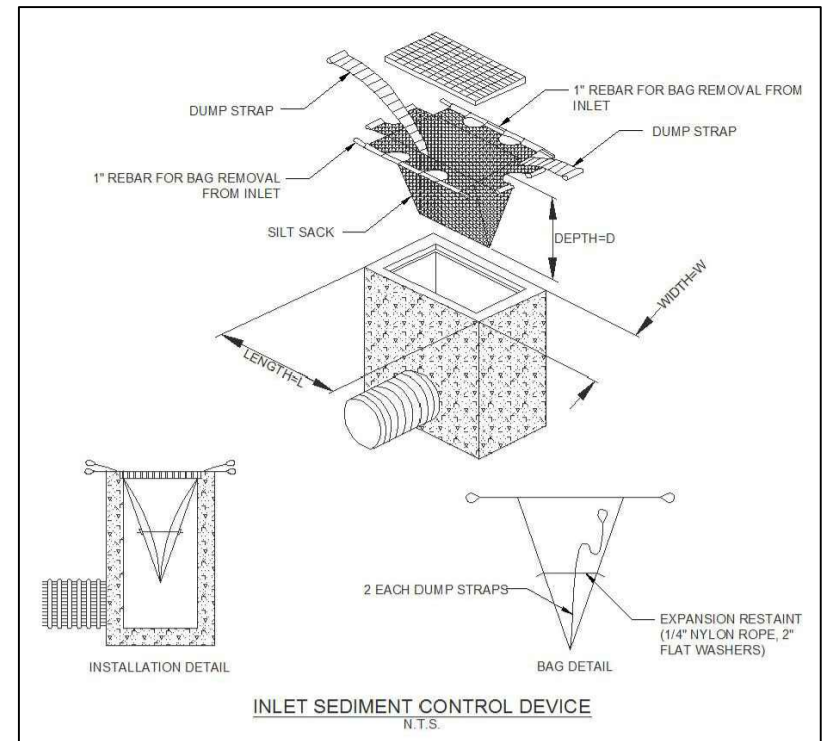
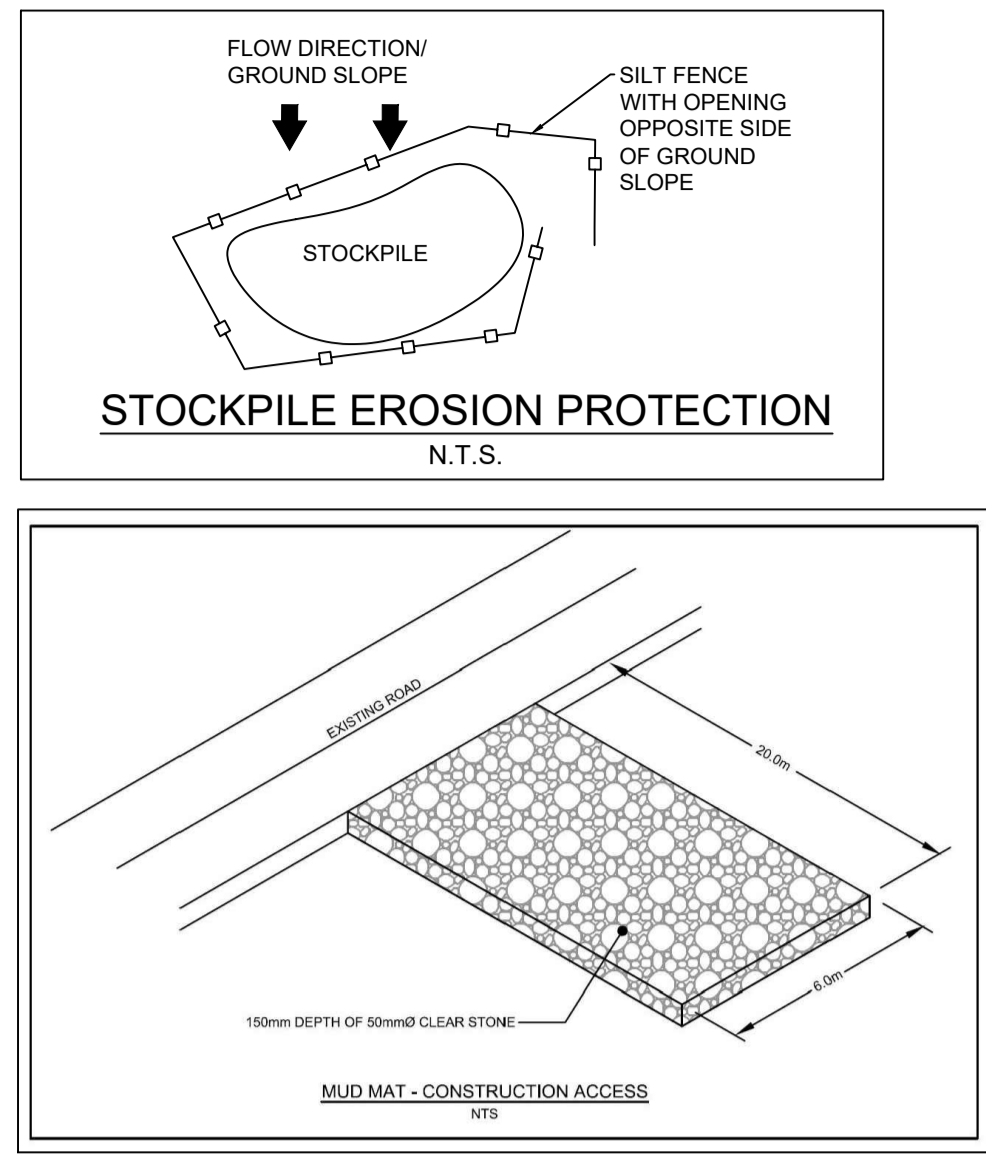
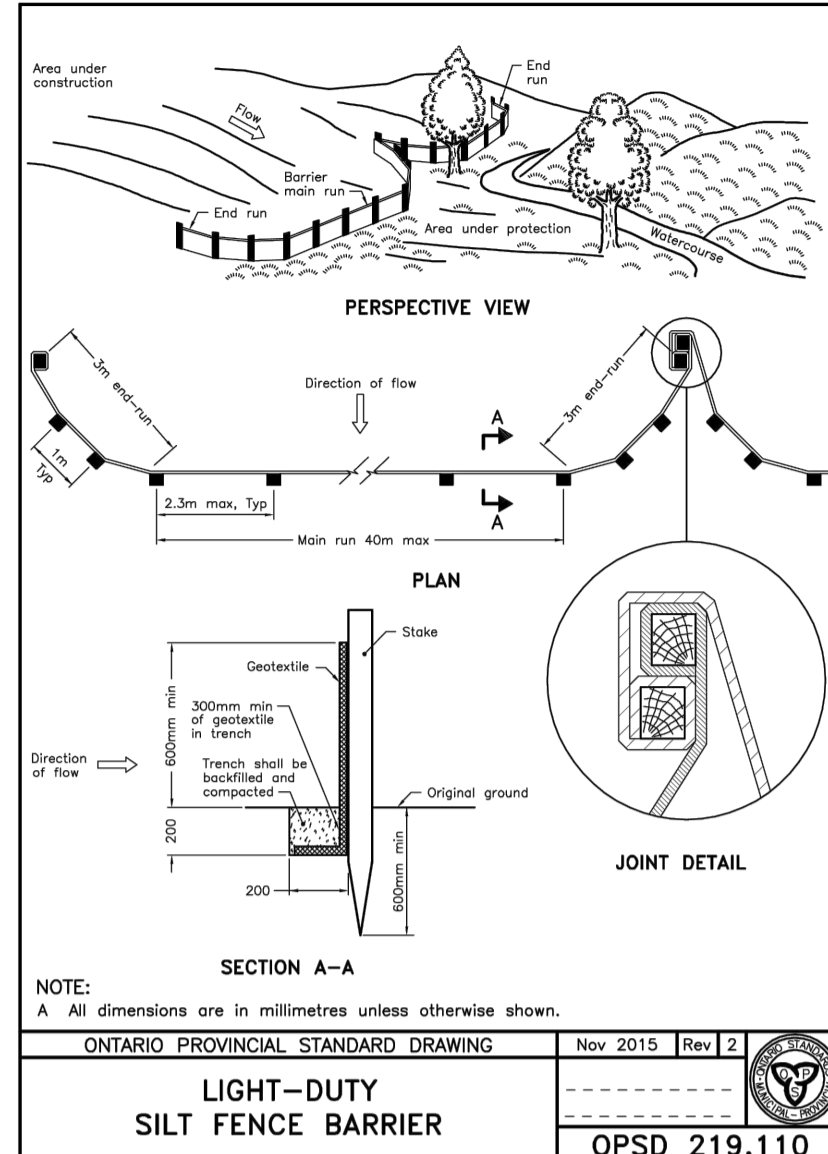
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www.lrl.ca | (613) 842-3434

PROPOSED 3-STOREY APARTMENT BUILDING
1465 MORISSET AVE, OTTAWA, ON
REV.02 - ISSUED FOR SPC AMENDMENT - JANUARY 27, 2025
LRL PROJECT no: 200572



NOT AUTHENTIC UNLESS SIGNED AND DATED



LEGEND:

	EXISTING PROPERTY LINE TO REMAIN
	PROPOSED CURB
	PROPOSED DEPRESSED CURB
	PROPOSED TERRACING (3:1 MIN.)
	PROPOSED SILT FENCE AS PER OPSD 219.110
	PROPOSED FENCE
	PROPOSED DOOR ENTRANCE/EXIST
	PROPOSED GRASS AREA (100mm TOP SOIL & SOD)
	PROPOSED CONCRETE FEATURES/SLAB
	PROPOSED HEAVY DUTY ASPHALT
	PROPOSED LIGHT DUTY ASPHALT
	PROPOSED RIP RAP
	PROPOSED ELEVATION
	PROPOSED HIGH POINT ELEVATION
	PROPOSED SWALE ELEVATION
	PROPOSED BOTTOM OF CURB / ASPHALT ELEVATION
	PROPOSED TOP OF CURB ELEVATION
	PROPOSED EXPOSED BOTTOM OF RETAINING WALL
	PROPOSED TOP OF RETAINING WALL
	MATCH INTO EXISTING ELEVATION
	EXISTING ELEVATION
	PROPOSED OVERLAND MAJOR FLOW ROUTE
	PROPOSED 100mm PERFORATED SUBDRAIN
	PROPOSED STORM SEWER
	PROPOSED SANITARY SEWER
	PROPOSED WATERMAIN
	EXISTING STORM SEWER
	EXISTING SANITARY SEWER
	EXISTING WATERMAIN
	EXISTING GAS LINE
	EXISTING MANHOLE
	EXISTING CATCHBASIN
	PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN
	PROPOSED MANHOLE/CATCHBASIN-MANHOLE
	PROPOSED CURB STOP
	PROPOSED PIPE INSULATION
	PROPOSED 100 YEAR HIGH WATER LEVEL
	STORM WATERSHED EXTENT
	WATERSHED NAME
	RUNOFF COEFFICIENT
	AREA IN HECTARES

USE AND INTERPRETATION OF DRAWINGS

GENERAL CONDITIONS OF THE CONTRACT FOR CONSTRUCTION ARE PART OF THE CONTRACT DOCUMENTS AND DESCRIBE USE AND INTENT OF THE DRAWINGS. THE CONTRACTOR SHALL REVIEW AND INTERPRET THE DRAWINGS AND THE CONTRACT DOCUMENTS BEFORE COMMENCING WORK. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL NECESSARY PERMITS AND APPROVALS FROM THE APPROPRIATE AGENCIES. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL NECESSARY INFORMATION FROM THE OWNER AND THE ENGINEER. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL NECESSARY INFORMATION FROM THE OWNER AND THE ENGINEER. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL NECESSARY INFORMATION FROM THE OWNER AND THE ENGINEER.

BY USE OF THE DRAWINGS FOR CONSTRUCTION OF THE PROJECT, THE OWNER AGREES TO WAIVE ANY CLAIM AGAINST LRL AND TO RELEASE LRL FROM ANY LIABILITY ARISING DIRECTLY OR INDIRECTLY FROM SUCH UNAUTHORIZED CHANGES.

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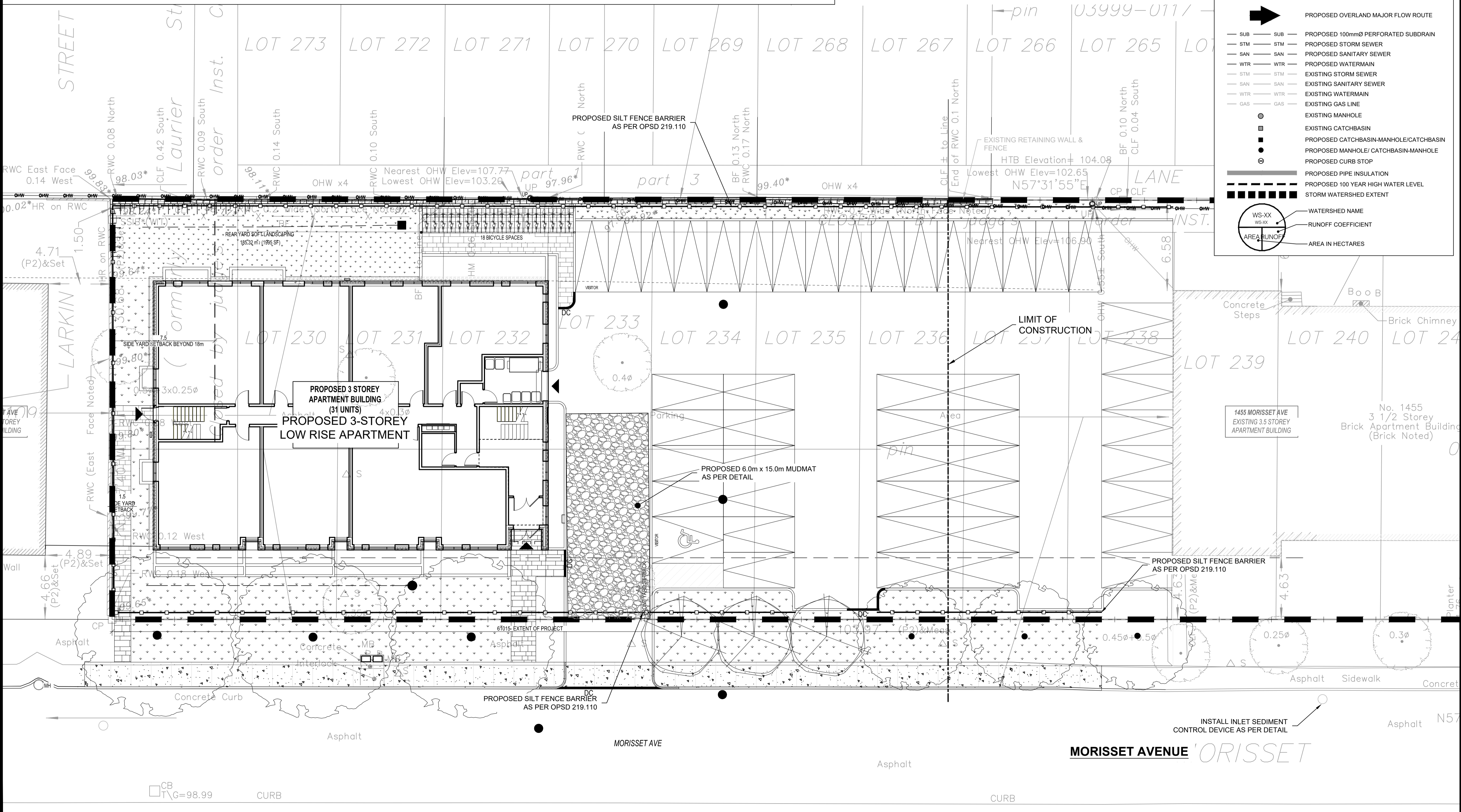
GENERAL NOTES:

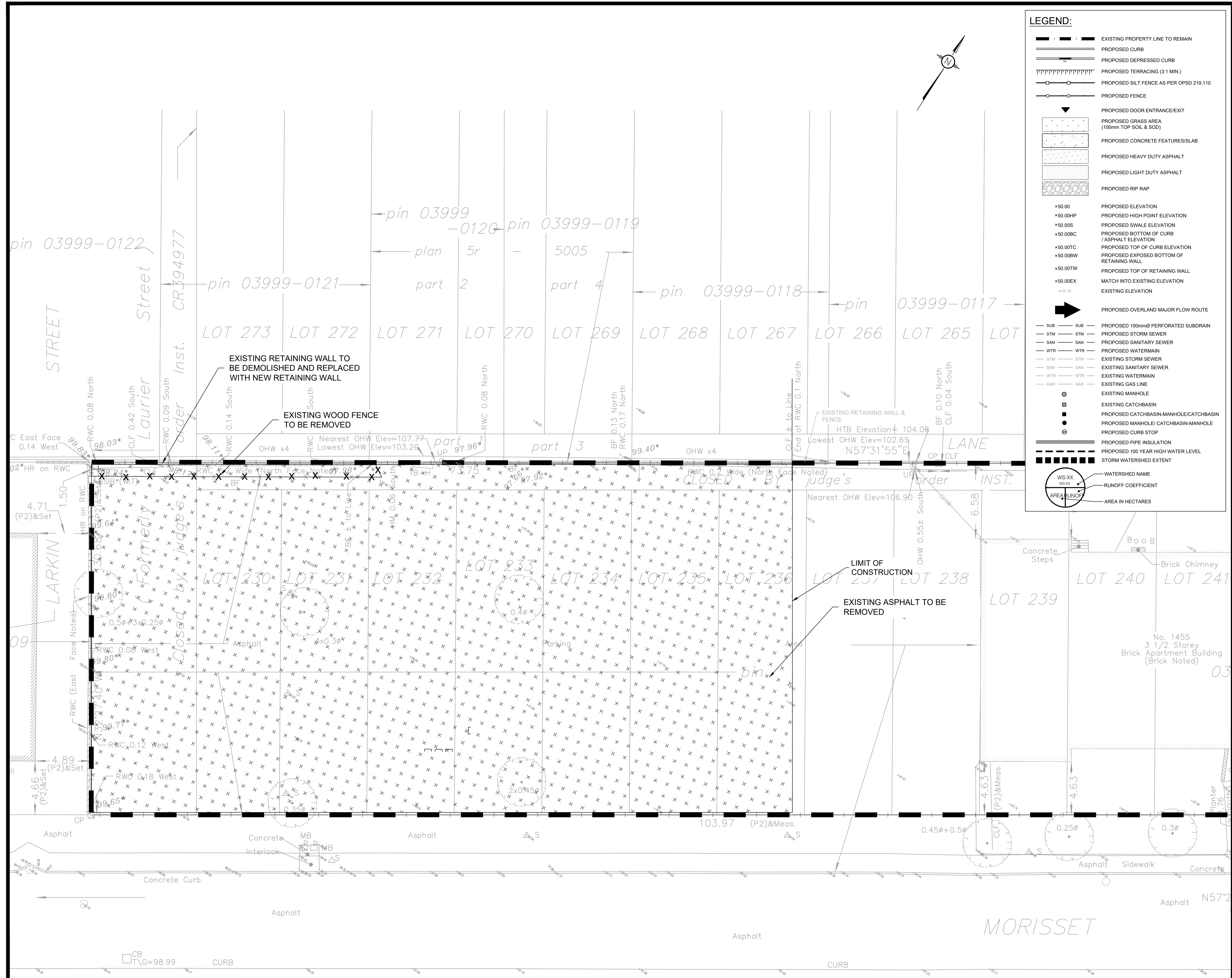
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- PROPOSED SILT FENCE AS PER OPSD 219.110
- PROPOSED FENCE
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No.	REVISIONS	BY	DATE
02	ISSUED FOR SPC AMENDMENT	M.S.	27 JAN 2025
01	ISSUED FOR SPC AMENDMENT	S.V.	18 DEC 2024

NOT AUTHENTIC UNLESS SIGNED AND DATED

LRL
ENGINEERING | INGENIERIE
5430 Canotek Road | Ottawa, ON, K1J 9G2
www.lrl.ca | (613) 842-3434

CLIENT: **CONCORDE PROPERTIES**

DESIGNED BY: M.B. DRAWN BY: S.V. APPROVED BY: M.B.

PROJECT: **PROPOSED 3-STOREY APARTMENT BUILDING 1465 MORISSET AVE, OTTAWA (ON)**

DRAWING TITLE: **DEMOLITION PLAN**

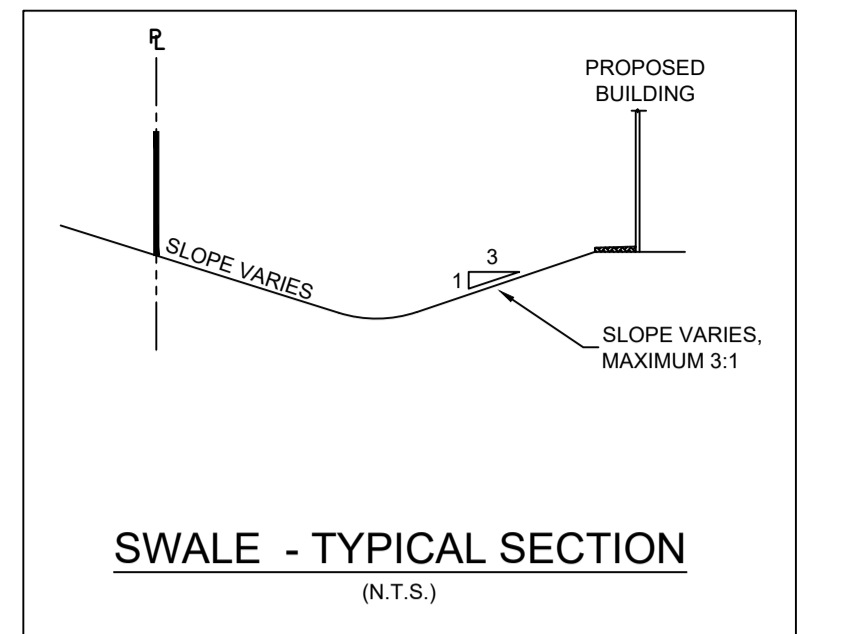
PROJECT NO: 200572 DATE: DECEMBER 2024

C102

PAVEMENT STRUCTURE

COURSE	MATERIAL	THICKNESS (mm)	
		AUTOMOBILE PARKING	TRUCK ROUTE (HEAVY TRAFFIC)
SURFACE	HL.3 A/C	50	40
BINDER	HL.8 A/C	-	50
BASECOURSE	OPSS GRANULAR "A"	150	150
SUBBASE	OPSS GRANULAR "B"	300	400

NOTE: IN PREPARATION FOR PAVEMENT CONSTRUCTION AT THIS SITE, ANY SURFICIAL OR NEAR SURFACE/SUBGRADE LEVEL TOPSOIL AND ANY SOFT, WET OR DELETERIOUS MATERIALS SHOULD BE REMOVED FROM THE PROPOSED PAVED AREAS. THE EXPOSED SUBGRADE SHOULD BE INSPECTED AND APPROVED BY GEOTECHNICAL PERSONNEL AND ANY SOFT AREAS EVIDENT SHOULD BE SUBEXCAVATED AND REPLACED WITH SUITABLE EARTH BORROW APPROVED BY THE GEOTECHNICAL ENGINEER. THE SUBGRADE SHOULD BE SHAPED AND CROWNED TO PROMOTE DRAINAGE OF THE SITE DRAINAGE STRUCTURES. FOLLOWING APPROVAL OF THE PREPARATION OF THE SUBGRADE, THE PAVEMENT GRANULARS WILL BE PLACED. RECOMMENDED PAVEMENT STRUCTURE AS PER GEOTECHNICAL REPORT PREPARED BY LRL ASSOCIATES INC., APRIL 8, 2021



Bearings are grid, derived from Can-Net 2016 Real Time Network GPS observations and are referred to the Central Meridian of WTM Zone 9 (78°30' West Longitude) NAD-83 (original). For comparison purposes, a rotation of 0°30'50" counter-clockwise was applied to bearings on P2.

ELEVATION NOTES
 1. Elevations shown are geodetic and are referred to the CGVD28 geodetic datum, derived from City of Ottawa Benchmark No. N-26, having an elevation of 77.347.
 2. It is the responsibility of the user of this information to verify that the job benchmark has not been altered or disturbed and that its relative elevation and description agrees with the information shown on this drawing.

UTILITY NOTES
 1. This drawing cannot be accepted as acknowledging all of the utilities and it will be the responsibility of the user to contact the respective utility authorities for confirmation.
 2. Only visible surface utilities were located.
 3. A field location of underground plant by the pertinent utility authority is mandatory before any work involving breaking ground, probing, excavating etc.
 4. Underground utility locations derived by City of Ottawa Utility Coordinate Committee Sheets numbers H-05-12 and H-05-17, and utility inverts provided by City of Ottawa Engineering Department plans dated July 2, 1999, April 4, 1993 (Storm Sewer), and April 4, 1993 (Sewer).

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SCALE: 1:150

3.0m 1.5 0 3.0 6.0m

No.	REVISIONS	BY	DATE
02	ISSUED FOR SPC AMENDMENT	M.S.	27 JAN 2025
01	ISSUED FOR SPC AMENDMENT	S.V.	18 DEC 2024

LICENSED PROFESSIONAL ENGINEER
 M. BASNET
 100501996
 2025/01/27
 PROVINCE OF ONTARIO

LRL
 ENGINEERING | INGENIERIE
 5430 Canotek Road | Ottawa, ON, K1J 9G2
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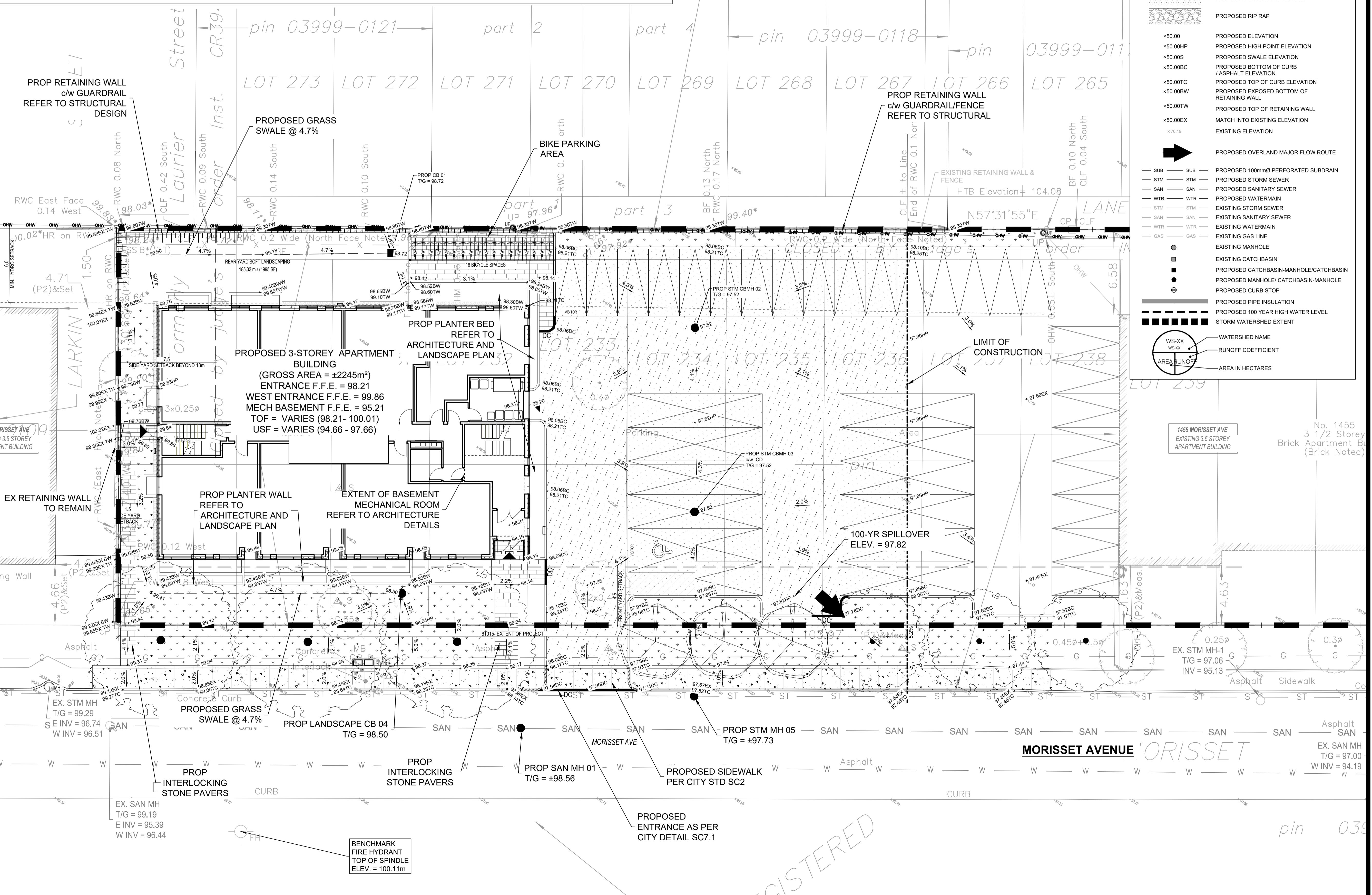
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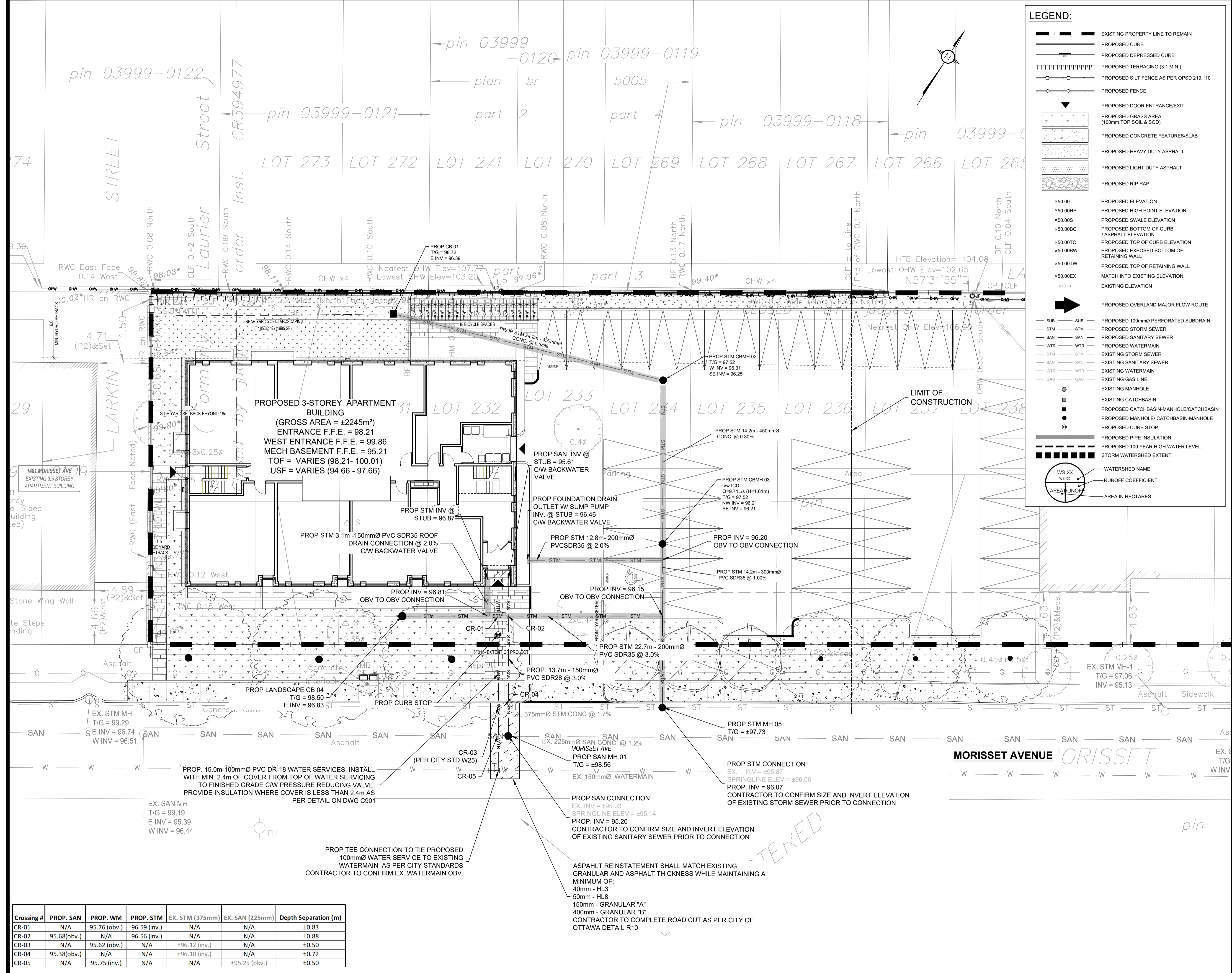
DESIGNED BY: M.B. DRAWN BY: S.V. APPROVED BY: M.B.

PROJECT
 PROPOSED 3-STORY APARTMENT BUILDING
 1455 MORISSET AVE, OTTAWA (ON)

DRAWING TITLE
 GRADING AND DRAINAGE PLAN

PROJECT NO. 200572
DATE DECEMBER 2024
C301





LEGEND:

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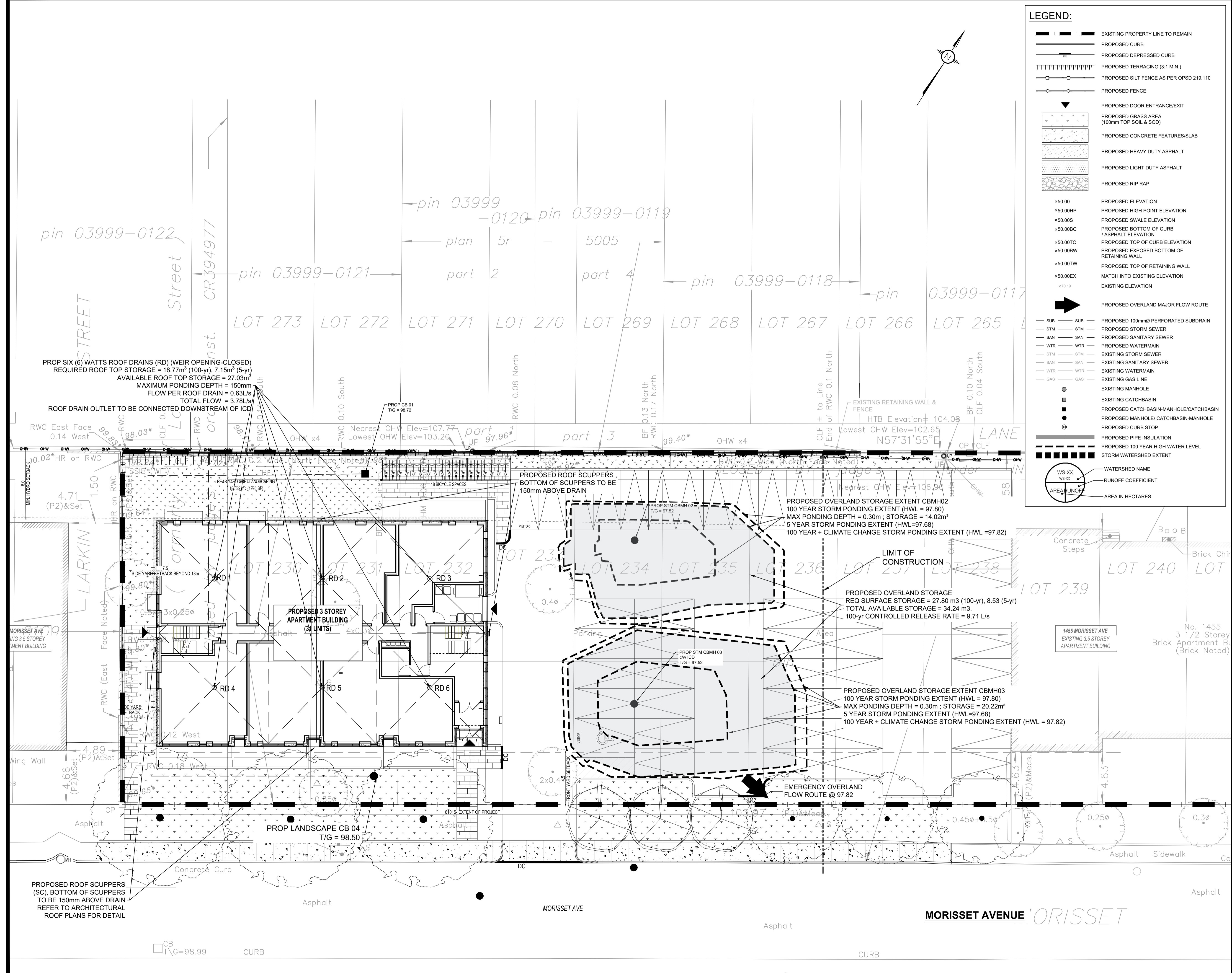
DESIGNED BY: M.B. DRAWN BY: S.V. APPROVED BY: M.B.

PROJECT: **PROPOSED 3-STORY APARTMENT BUILDING 1465 MORISSET AVE, OTTAWA (ON)**

DRAWING TITLE: **SERVICING PLAN**

PROJECT NO: 200572
 DATE: DECEMBER 2024
C401

Crossing #	PROP. SAN	PROP. WM	PROP. STM	EX. STM (375mm)	EX. SAN (225mm)	Depth Separation (m)
CR-01	N/A	95.76 (obv.)	96.59 (inv.)	N/A	N/A	±0.83
CR-02	95.68 (obv.)	N/A	96.56 (inv.)	N/A	N/A	±0.88
CR-03	N/A	95.62 (obv.)	N/A	±96.12 (inv.)	N/A	±0.50
CR-04	95.38 (obv.)	N/A	N/A	±96.10 (inv.)	N/A	±0.72
CR-05	N/A	95.75 (inv.)	N/A	N/A	±95.25 (obv.)	±0.50



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	PROPOSED 100mm PERFORATED SUBDRAIN
	PROPOSED STORM SEWER
	PROPOSED SANITARY SEWER
	PROPOSED WATERMAIN
	EXISTING STORM SEWER
	EXISTING SANITARY SEWER
	EXISTING WATERMAIN
	EXISTING GAS LINE
	EXISTING MANHOLE
	EXISTING CATCHBASIN
	PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN
	PROPOSED MANHOLE/CATCHBASIN-MANHOLE
	PROPOSED CURB STOP
	PROPOSED PIPE INSULATION
	PROPOSED 100 YEAR HIGH WATER LEVEL
	STORM WATERSHED EXTENT
	WATERSHED NAME
	RUNOFF COEFFICIENT
	AREA IN HECTARES

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CONTRACTOR IS ADVISED TO COLLECT INFORMATION ON SOIL CONDITIONS BEFORE START OF CONSTRUCTION.

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3.0m 1.5m 0 3.0m 6.0m
SCALE: 1:150

02	ISSUED FOR SPC AMENDMENT	M.S.	27 JAN 2025
01	ISSUED FOR SPC AMENDMENT	S.V.	18 DEC 2024
No.	REVISIONS	BY	DATE

PROFESSIONAL ENGINEER
M. BASNET
100501996
2025/01/27
PROVINCE OF ONTARIO

NOT AUTHENTIC UNLESS SIGNED AND DATED

LRL
ENGINEERING | INGENIERIE
5430 Canotek Road | Ottawa, ON, K1J 9G2
www.lrl.ca | (613) 842-3434

CLIENT: **CONCORDE PROPERTIES**

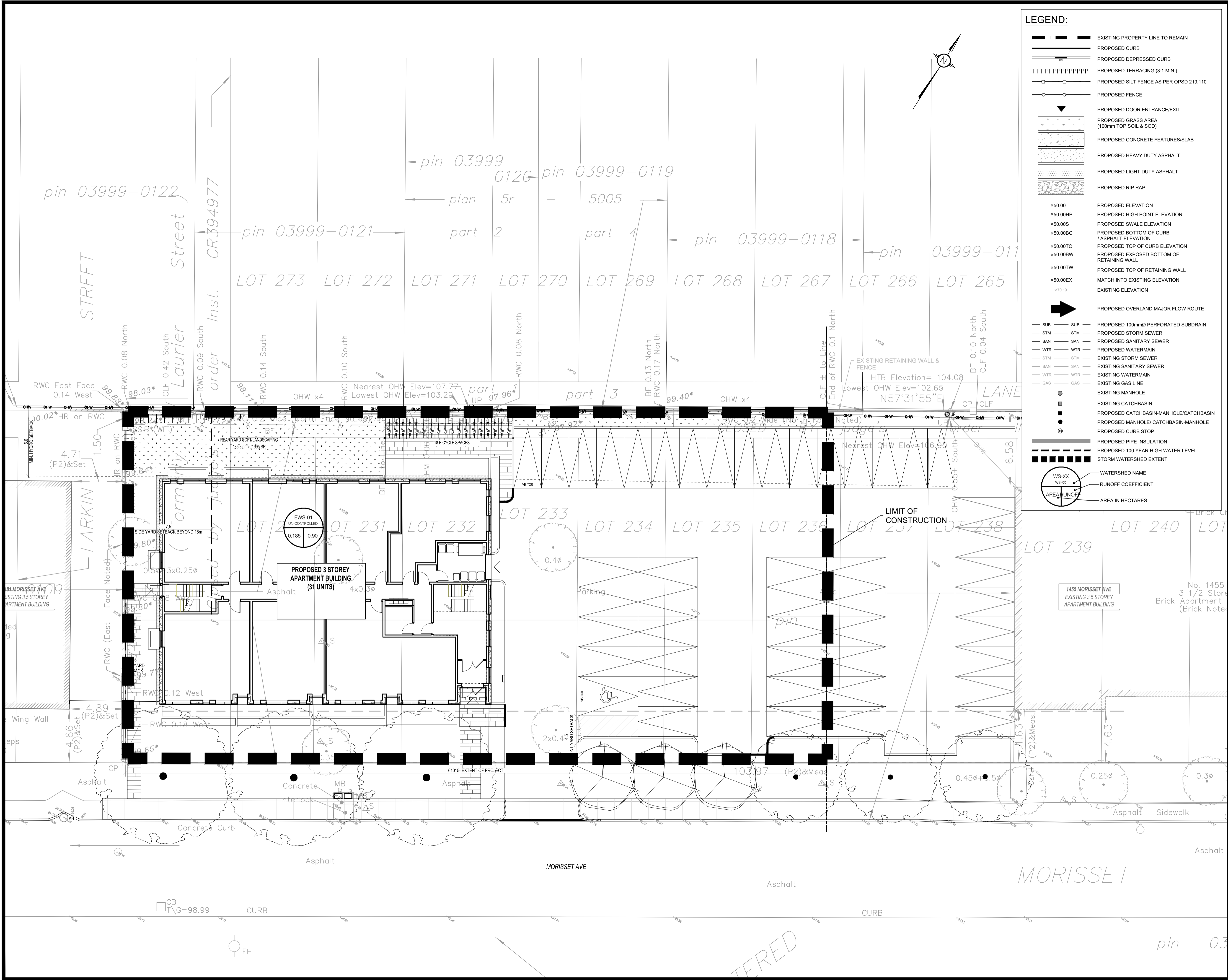
DESIGNED BY: M.B. DRAWN BY: S.V. APPROVED BY: M.B.

PROJECT: **PROPOSED 3-STOREY APARTMENT BUILDING
1455 MORISSET AVE, OTTAWA (ON)**

DRAWING TITLE: **STORMWATER MANAGEMENT PLAN**

PROJECT NO: 200572 DATE: DECEMBER 2024

C601



LEGEND:

- EXISTING PROPERTY LINE TO REMAIN
- PROPOSED CURB
- PROPOSED DEPRESSED CURB
- PROPOSED TERRACING (3:1 MIN.)
- PROPOSED SILT FENCE AS PER OPSD 219.110
- PROPOSED FENCE
- PROPOSED DOOR ENTRANCE/EXIT
- PROPOSED GRASS AREA (100mm TOP SOIL & SOD)
- PROPOSED CONCRETE FEATURES/SLAB
- PROPOSED HEAVY DUTY ASPHALT
- PROPOSED LIGHT DUTY ASPHALT
- PROPOSED RIP RAP
- PROPOSED ELEVATION
- PROPOSED HIGH POINT ELEVATION
- PROPOSED SWALE ELEVATION
- PROPOSED BOTTOM OF CURB / ASPHALT ELEVATION
- PROPOSED TOP OF CURB ELEVATION
- PROPOSED EXPOSED BOTTOM OF RETAINING WALL
- PROPOSED TOP OF RETAINING WALL
- MATCH INTO EXISTING ELEVATION
- EXISTING ELEVATION
- PROPOSED OVERLAND MAJOR FLOW ROUTE
- PROPOSED 100mm PERFORATED SUBDRAIN
- PROPOSED STORM SEWER
- PROPOSED SANITARY SEWER
- PROPOSED WATERMAIN
- EXISTING STORM SEWER
- EXISTING SANITARY SEWER
- EXISTING WATERMAIN
- EXISTING GAS LINE
- EXISTING MANHOLE
- EXISTING CATCHBASIN
- PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN
- PROPOSED MANHOLE/CATCHBASIN-MANHOLE
- PROPOSED CURB STOP
- PROPOSED PIPE INSULATION
- PROPOSED 100 YEAR HIGH WATER LEVEL
- STORM WATERSHED EXTENT
- WATERSHED NAME
- RUNOFF COEFFICIENT
- AREA IN HECTARES

USE AND INTERPRETATION OF DRAWINGS

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No.	REVISIONS	BY	DATE
02	ISSUED FOR SPC AMENDMENT	M.S.	27 JAN 2025
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CLIENT: CONCORDE PROPERTIES

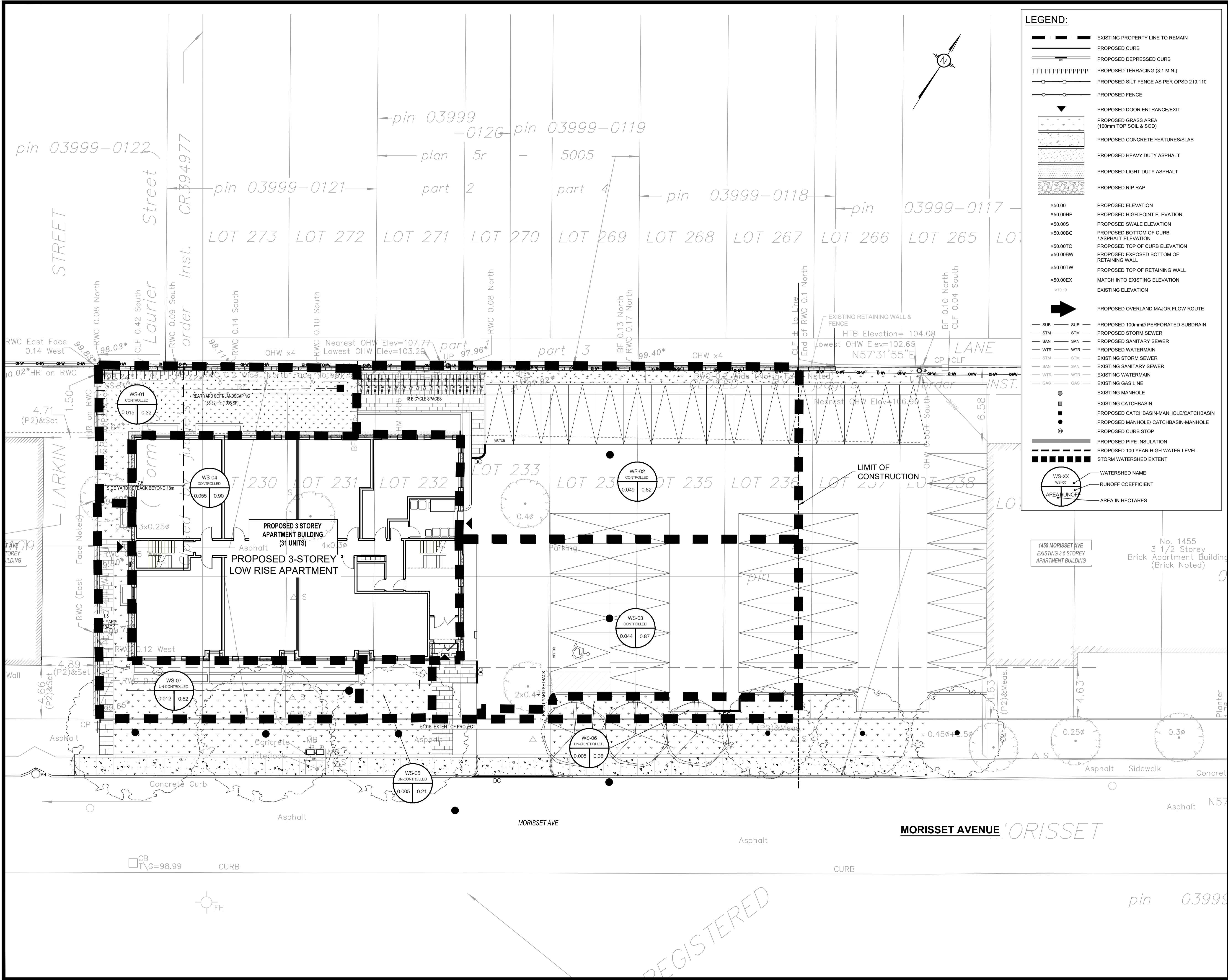
DESIGNED BY: M.B. DRAWN BY: S.V. APPROVED BY: M.B.

PROJECT: PROPOSED 3-STORY APARTMENT BUILDING
1455 MORISSET AVE, OTTAWA (ON)

DRAWING TITLE: PRE-DEVELOPMENT WATERSHED PLAN

PROJECT NO: 200572 DATE: DECEMBER 2024

C701



LEGEND:

- — — — — EXISTING PROPERTY LINE TO REMAIN
- — — — — PROPOSED CURB
- — — — — PROPOSED TERRACED CURB
- ||||| PROPOSED TERRACING (3:1 MIN.)
- — — — — PROPOSED SILT FENCE AS PER OPSD 219.110
- — — — — PROPOSED FENCE
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- PROPOSED LIGHT DUTY ASPHALT
- PROPOSED RIP RAP
- ×50.00 PROPOSED ELEVATION
- ×50.00HP PROPOSED HIGH POINT ELEVATION
- ×50.00S PROPOSED SWALE ELEVATION
- ×50.00BC PROPOSED BOTTOM OF CURB / ASPHALT ELEVATION
- ×50.00TC PROPOSED TOP OF CURB ELEVATION
- ×50.00BW PROPOSED EXPOSED BOTTOM OF RETAINING WALL
- ×50.00TW PROPOSED TOP OF RETAINING WALL
- ×50.00EX MATCH INTO EXISTING ELEVATION
- ×70.10
- ➔ PROPOSED OVERLAND MAJOR FLOW ROUTE
- SUB — SUB — PROPOSED 100mmØ PERFORATED SUBDRAIN
- STM — STM — PROPOSED STORM SEWER
- SAN — SAN — PROPOSED SANITARY SEWER
- WTR — WTR — PROPOSED WATERMAIN
- STM — STM — EXISTING STORM SEWER
- SAN — SAN — EXISTING SANITARY SEWER
- WTR — WTR — EXISTING WATERMAIN
- GAS — GAS — EXISTING GAS LINE
- EXISTING MANHOLE
- EXISTING CATCHBASIN
- PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN
- PROPOSED MANHOLE/CATCHBASIN-MANHOLE
- PROPOSED CURB STOP
- — — — — PROPOSED PIPE INSULATION
- — — — — PROPOSED 100 YEAR HIGH WATER LEVEL
- — — — — STORM WATERSHED EXTENT
- WS-XX CONTROLLED
- WS-XX UNCONTROLLED
- AREA RUNOFF
- AREA IN HECTARES

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3.0m 1.5 0 3.0 6.0m
SCALE: 1:150

02	ISSUED FOR SPC AMENDMENT	M.S.	27 JAN 2025
01	ISSUED FOR SPC AMENDMENT	S.V.	18 DEC 2024
No.	REVISIONS	BY	DATE

PROFESSIONAL ENGINEER
M. BASNET
100501996
2025/01/27
PROVINCE OF ONTARIO

NOT AUTHENTIC UNLESS SIGNED AND DATED

LRL
ENGINEERING | INGENIERIE
5430 Canotek Road | Ottawa, ON, K1J 9G2
www.lrl.ca | (613) 842-3434

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DESIGNED BY: M.B. DRAWN BY: S.V. APPROVED BY: M.B.

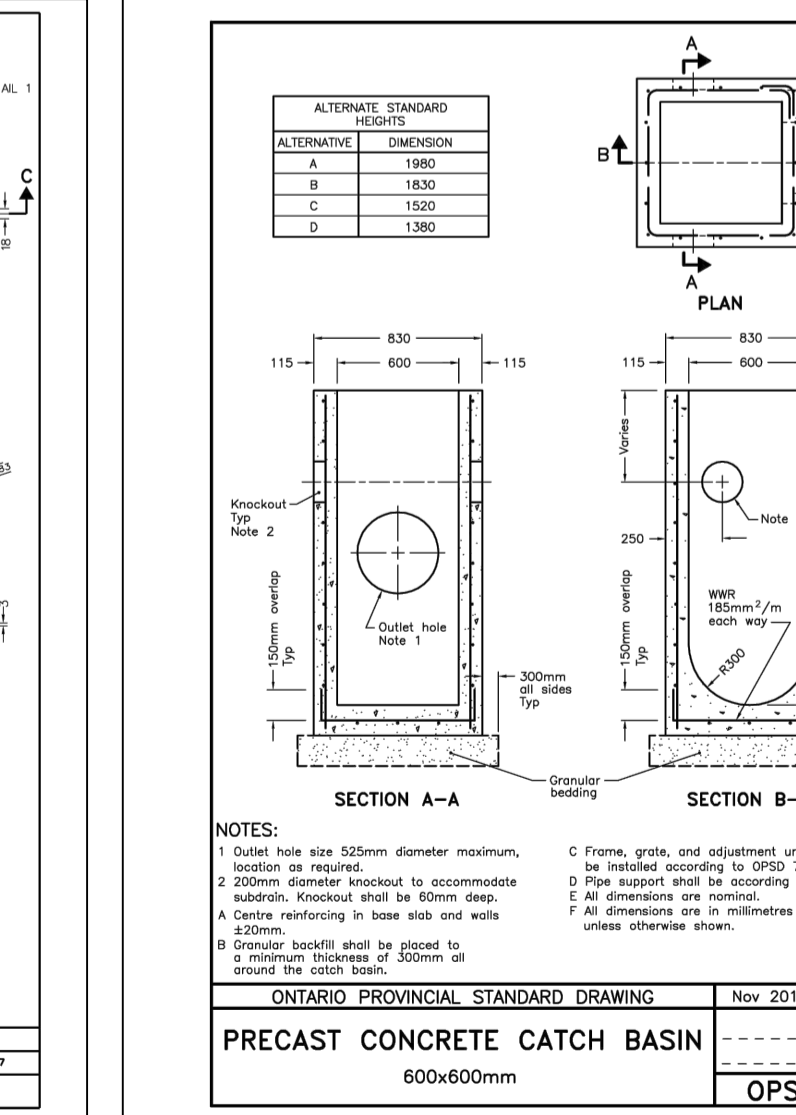
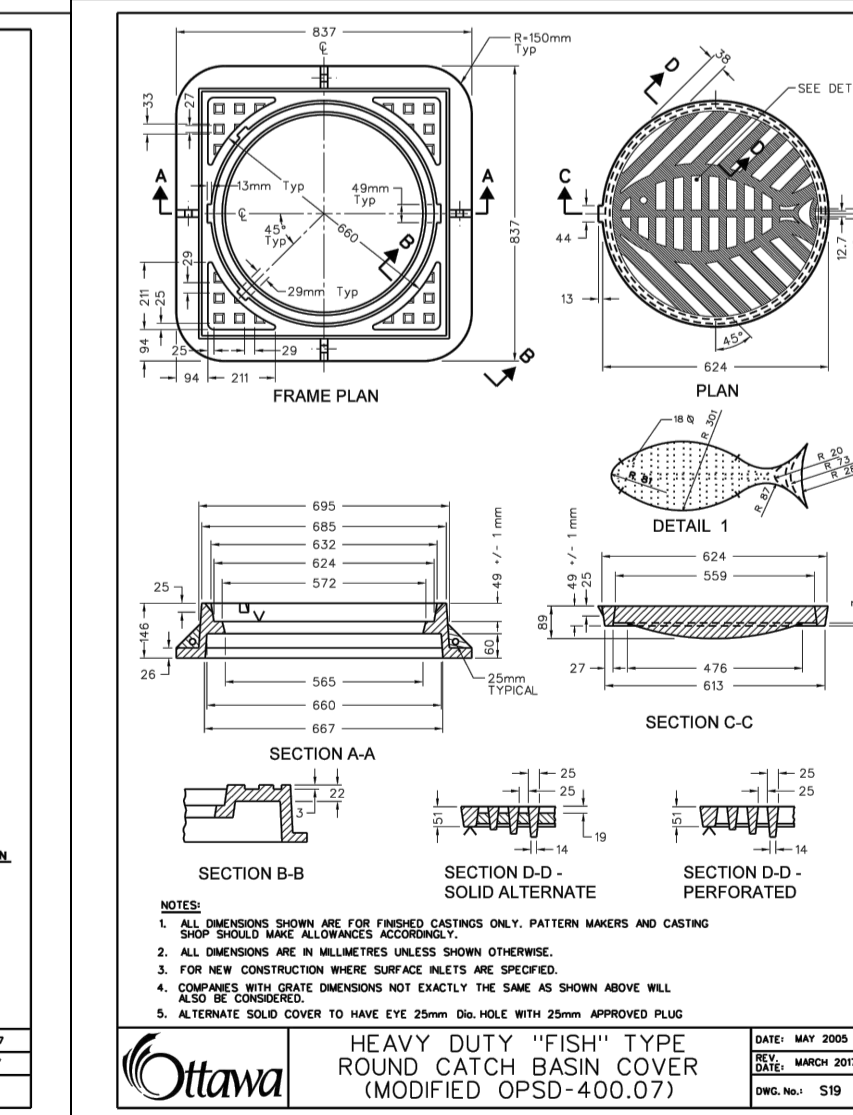
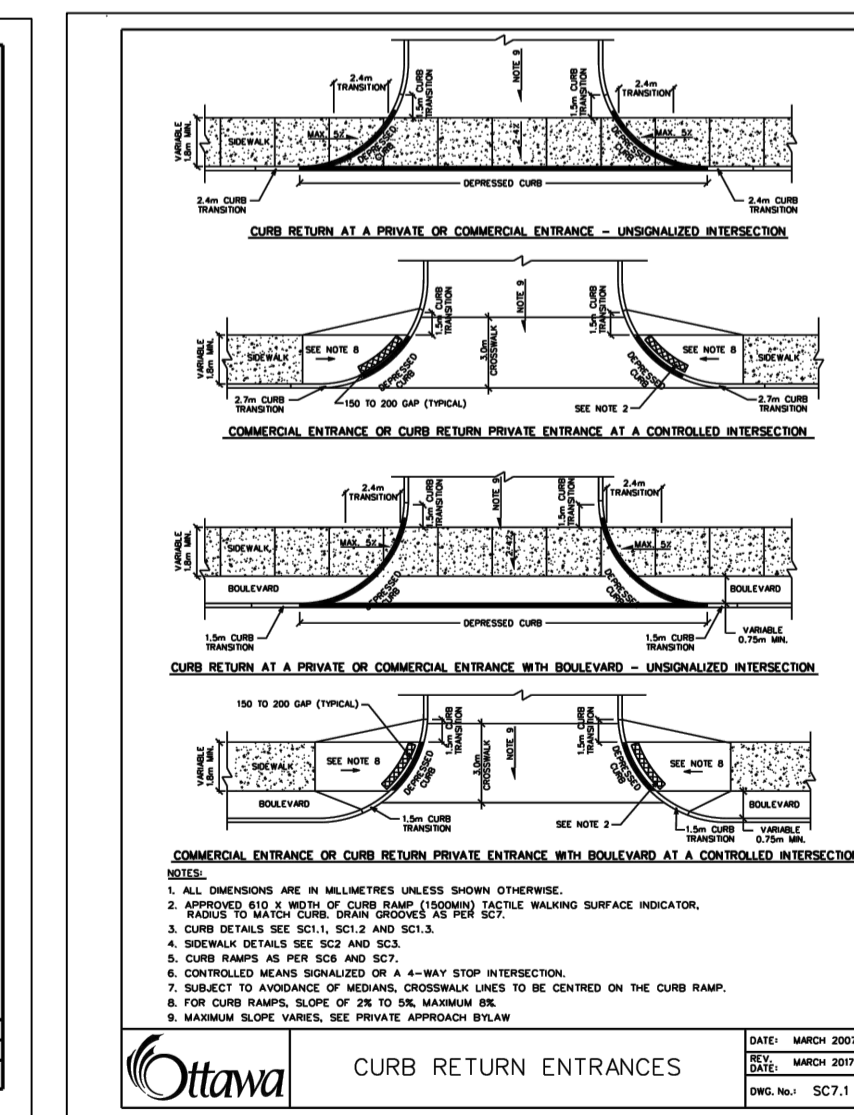
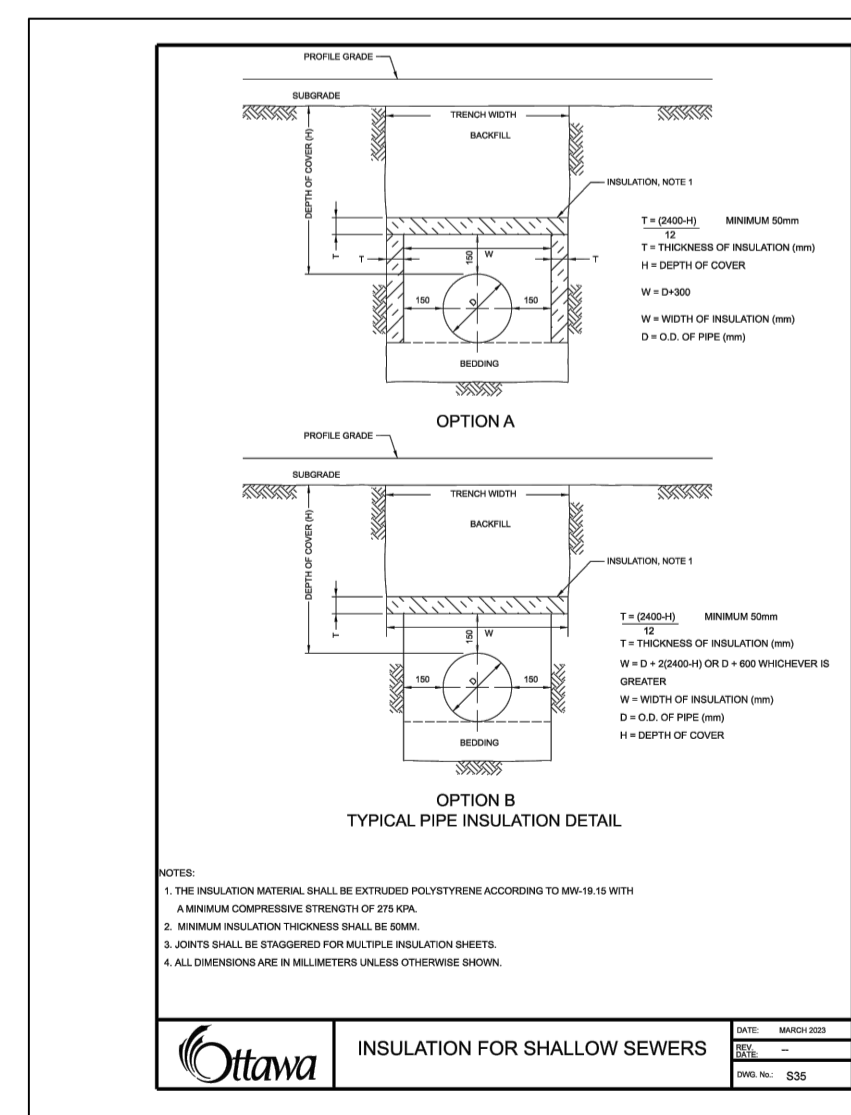
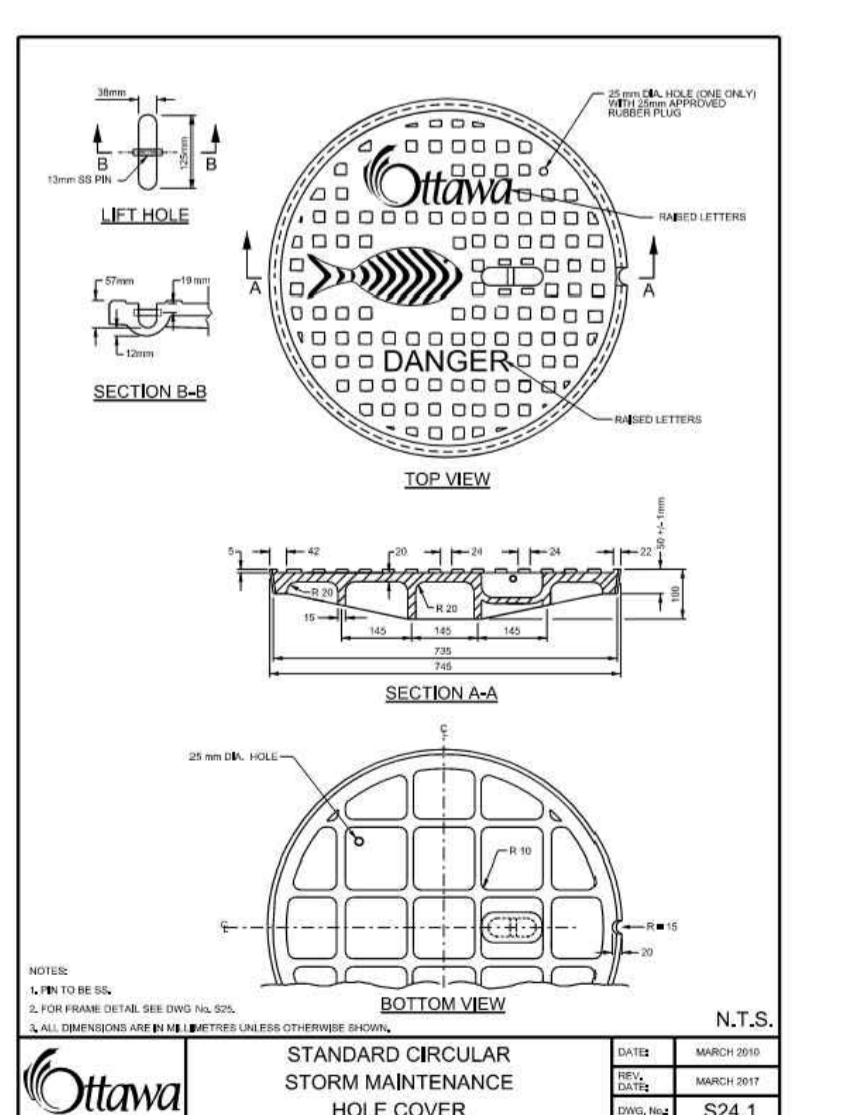
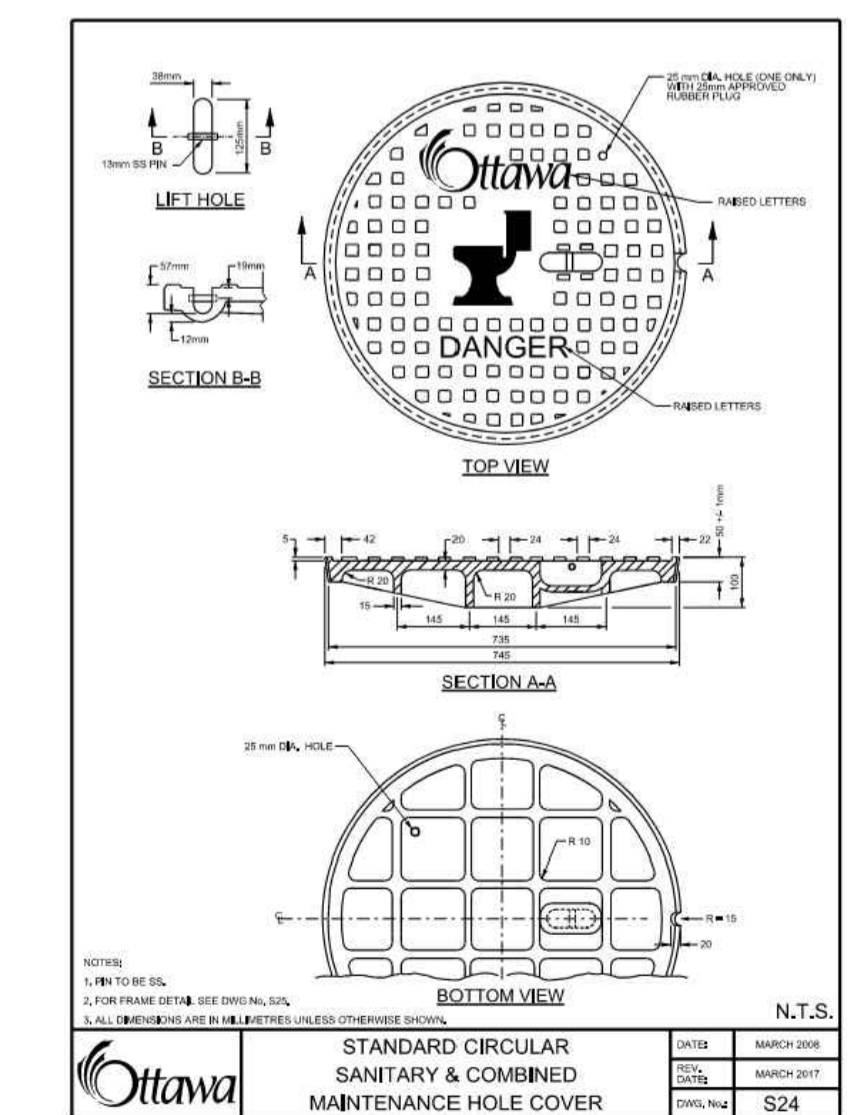
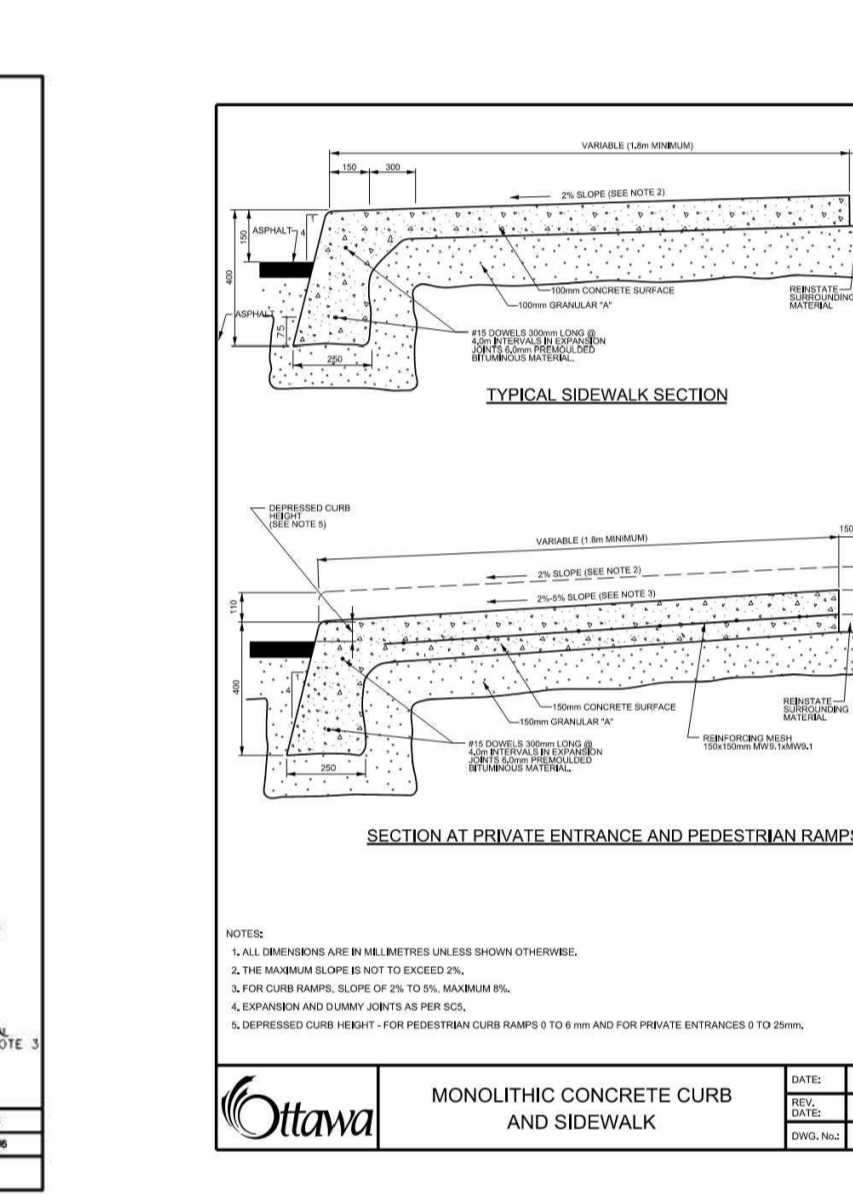
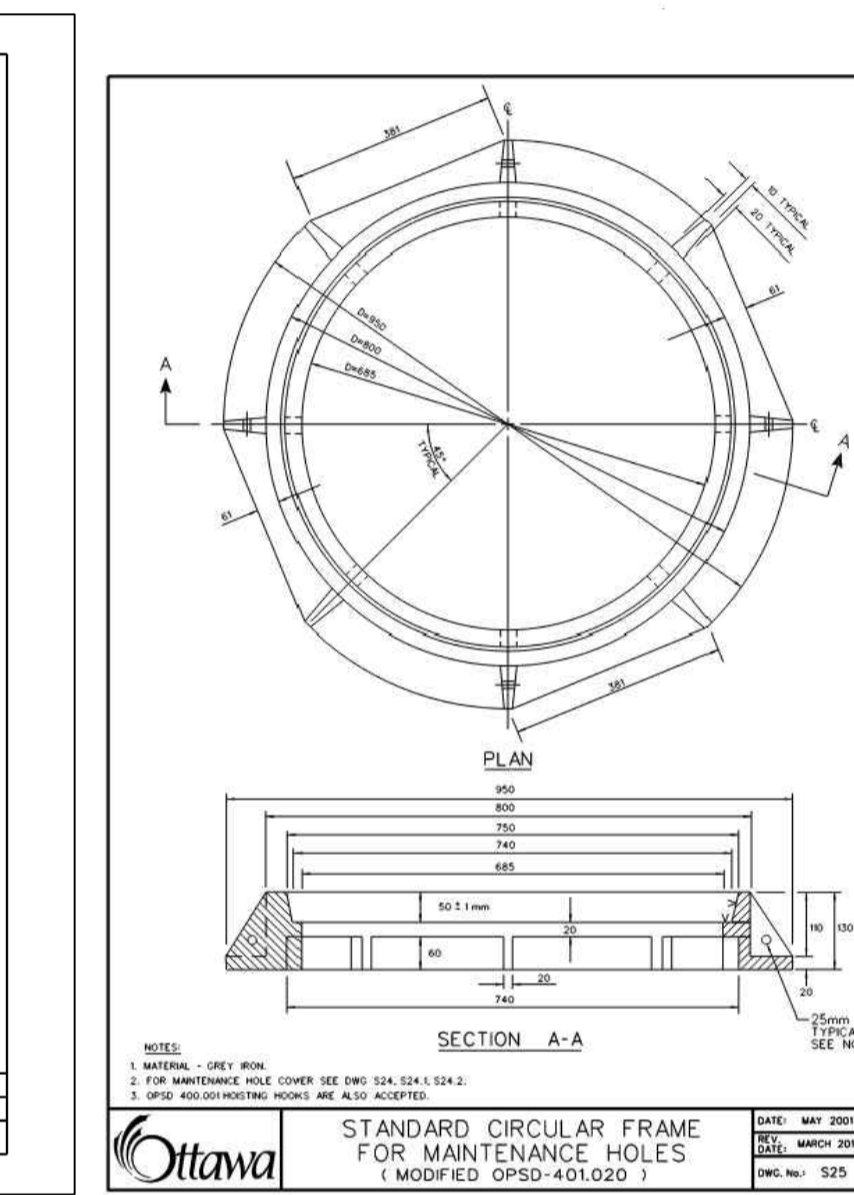
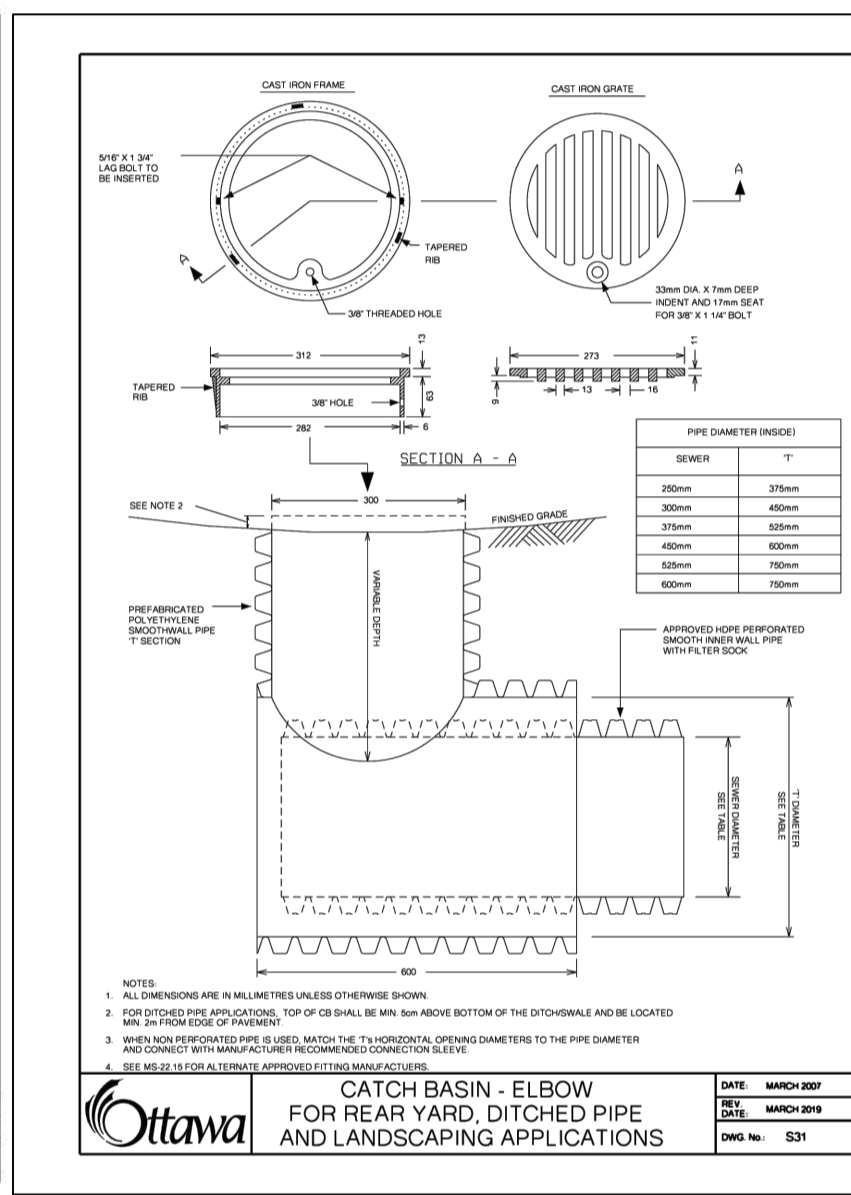
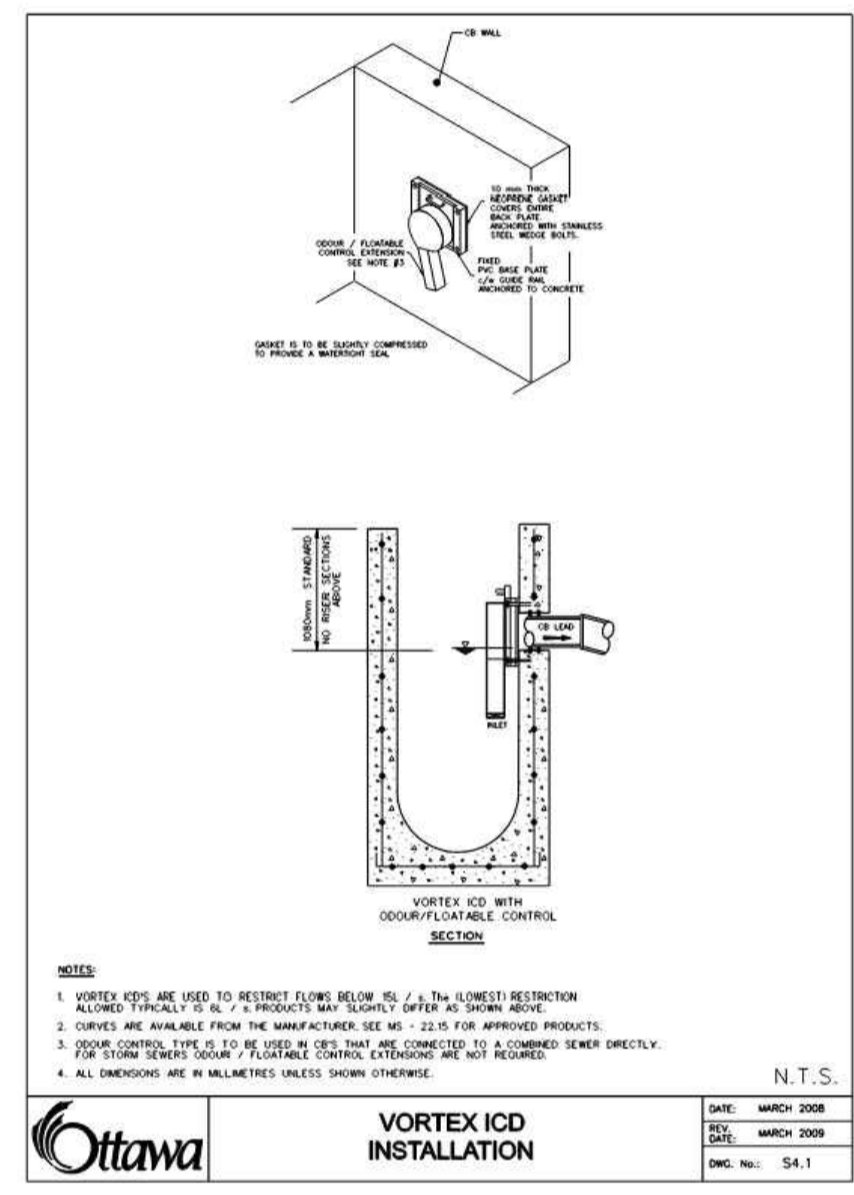
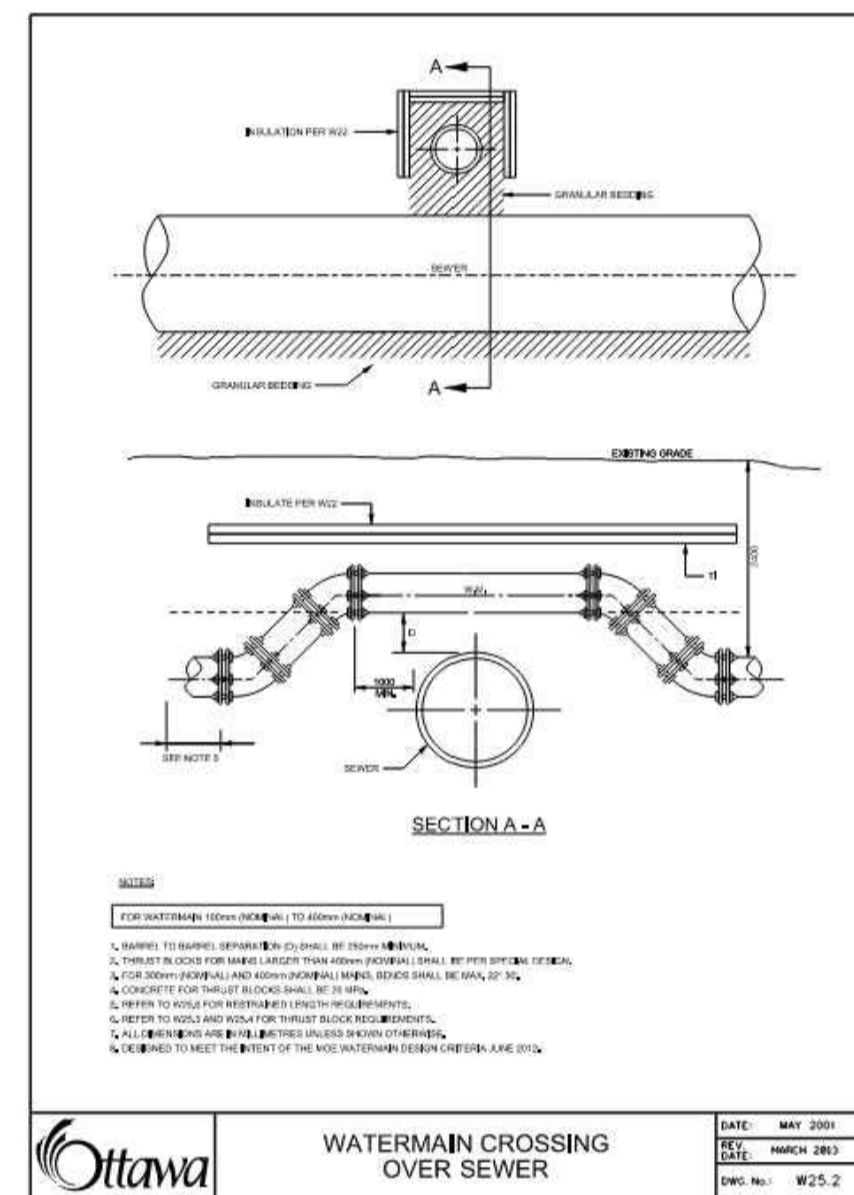
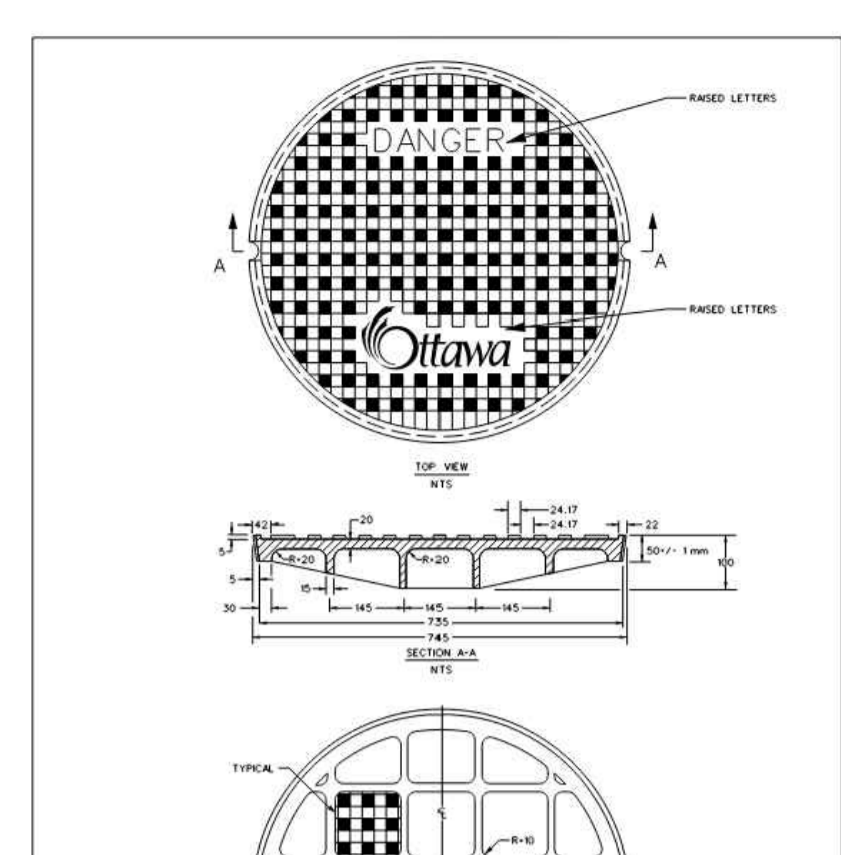
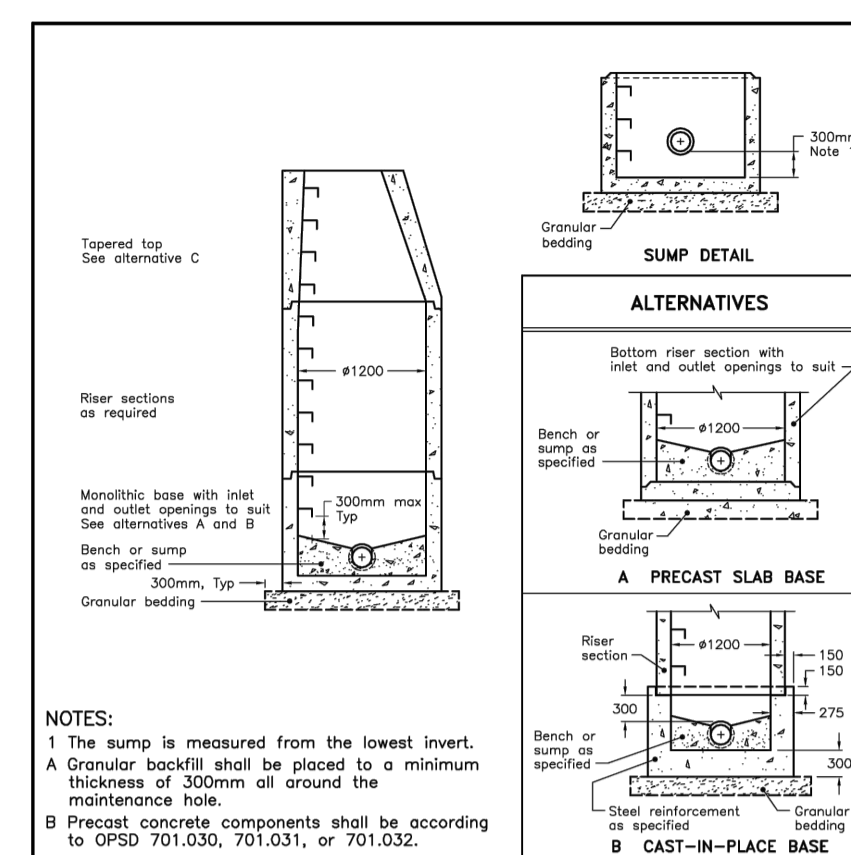
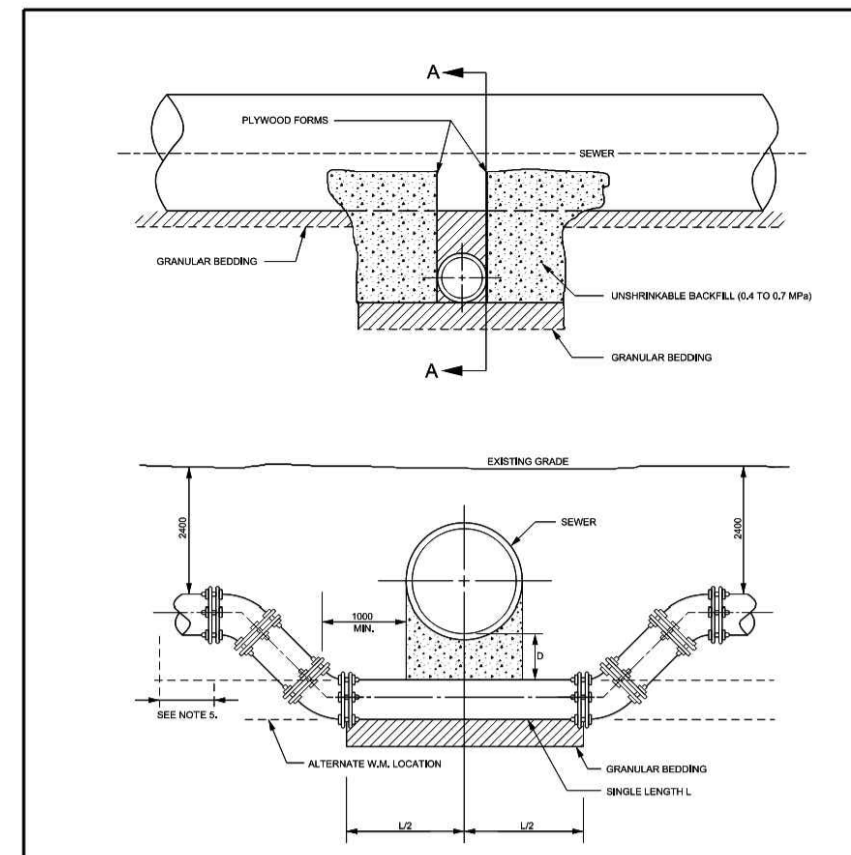
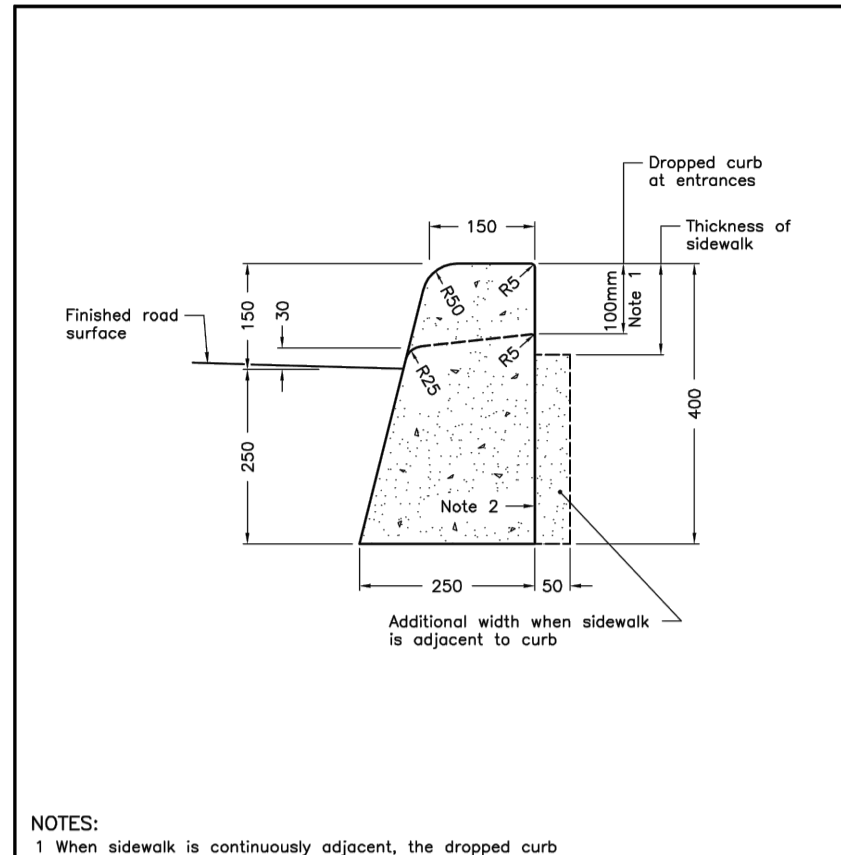
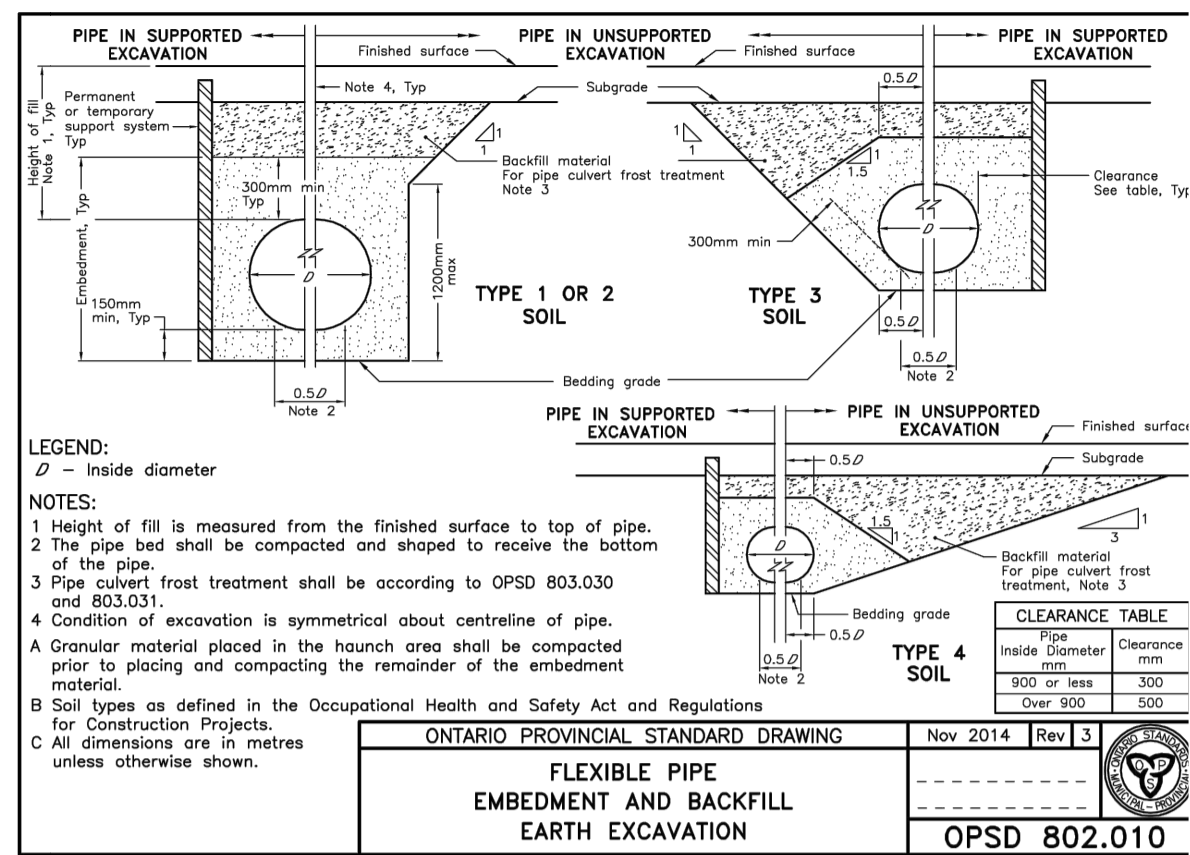
PROJECT: **PROPOSED 3-STORY APARTMENT BUILDING
1465 MORISSET AVE, OTTAWA (ON)**

DRAWING TITLE: **POST-DEVELOPMENT WATERSHED PLAN**

PROJECT NO: 200572 DATE: DECEMBER 2024

C702

07-12-21-0091 118532



USE AND INTERPRETATION OF DRAWINGS

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IN ADDITION, THE CLIENT AGREES, TO THE FULLEST EXTENT PERMITTED BY LAW, TO INDEMNIFY AND HOLD HARMLESS LRL FROM ANY DAMAGES, LIABILITIES OR COSTS, INCLUDING REASONABLE ATTORNEY'S FEES AND COST OF DEFENSE, ARISING FROM SUCH CHANGES.

IN ADDITION, THE CLIENT AGREES TO INCLUDE IN ANY CONTRACTS FOR CONSTRUCTION APPROPRIATE LANGUAGE THAT PROHIBITS THE CONTRACTOR OR ANY SUBCONTRACTORS OF ANY TIER FROM MAKING ANY CHANGES OR MODIFICATIONS TO LRL'S CONSTRUCTION DOCUMENTS WITHOUT THE PRIOR WRITTEN APPROVAL OF LRL AND THAT FURTHER REQUIRES THE CONTRACTOR TO INDEMNIFY BOTH LRL AND THE CLIENT FROM ANY LIABILITY OR COST ARISING FROM SUCH CHANGES MADE WITHOUT SUCH PROPER AUTHORIZATION.

EXISTING SERVICES AND UTILITIES SHOWN ON THESE DRAWINGS ARE TAKEN FROM THE BEST AVAILABLE RECORDS, BUT MAY NOT BE COMPLETE OR TO DATE. CONTRACTOR SHALL VERIFY IN FIELD FOR LOCATION AND ELEVATION OF PIPES AND CHECK WITH THE UTILITY COMPANIES BEFORE DIGGING OR PERFORMING WORK.

CONTRACTOR IS ADVISED TO COLLECT INFORMATION ON SOIL CONDITIONS BEFORE START OF CONSTRUCTION.

THE ENGINEER WAIVES ANY AND ALL RESPONSIBILITY AND LIABILITY FOR PROBLEMS WHICH ARISE FROM FAILURE TO FOLLOW THESE PLANS, SPECIFICATIONS AND THE DESIGN INTENT THEY CONVEY, OR FOR PROBLEMS WHICH ARISE FROM OTHERS' FAILURE TO OBTAIN AND/OR FOLLOW THE ENGINEER'S GUIDANCE WITH RESPECT TO ANY ERRORS, OMISSIONS, INCONSISTENCIES, AMBIGUITIES OR CONFLICTS WHICH ARE ALLEGED.

CONTRACTOR TO VERIFY ALL DIMENSIONS AND NOTIFY THE ENGINEER OF ANY DISCREPANCIES BEFORE WORK COMMENCES. DO NOT SCALE DRAWINGS.

No.	REVISIONS	BY	DATE
02	ISSUED FOR SPC AMENDMENT	M.S.	27 JAN 2025
01	ISSUED FOR SPC AMENDMENT	S.V.	18 DEC 2024



NOT AUTHENTIC UNLESS SIGNED AND DATED



CLIENT
CONCORDE PROPERTIES

DESIGNED BY: M.B. DRAWN BY: S.V. APPROVED BY: M.B.

PROJECT
**PROPOSED 3-STORY APARTMENT BUILDING
 1465 MORISSET AVE, OTTAWA (ON)**

DRAWING TITLE
CONSTRUCTION DETAIL PLAN

PROJECT NO.
 200572

DATE
 DECEMBER 2024

C901

APPENDIX F
Survey
As-Built
Architectural Drawings

**PLAN OF SURVEY OF
LOTS 230 TO 251 (BOTH INCLUSIVE)
AND PART OF CAVAN STREET
AND PART OF LARKIN STREET
(Closed by Judge's Order Inst. CR394977)
AND PART OF THE LANE
(Closed by Judge's Order Inst. CR404252)
REGISTERED PLAN 327
CITY OF OTTAWA**

Surveyed by Annis, O'Sullivan, Vollebek Ltd.
Scale 1 : 300



Metric
DISTANCES SHOWN ON THIS PLAN ARE IN METRES AND
CAN BE CONVERTED TO FEET BY DIVIDING BY 0.3048

Surveyor's Certificate
I CERTIFY THAT:
1. This survey and plan are correct and in accordance with the Surveys Act, the Surveyors Act and the Land Titles Act and the regulations made under them.
2. The survey was completed on the 12th day of February, 2021.

Feb. 26, 2021
Date
E. H. Herweyer
Ontario Land Surveyor

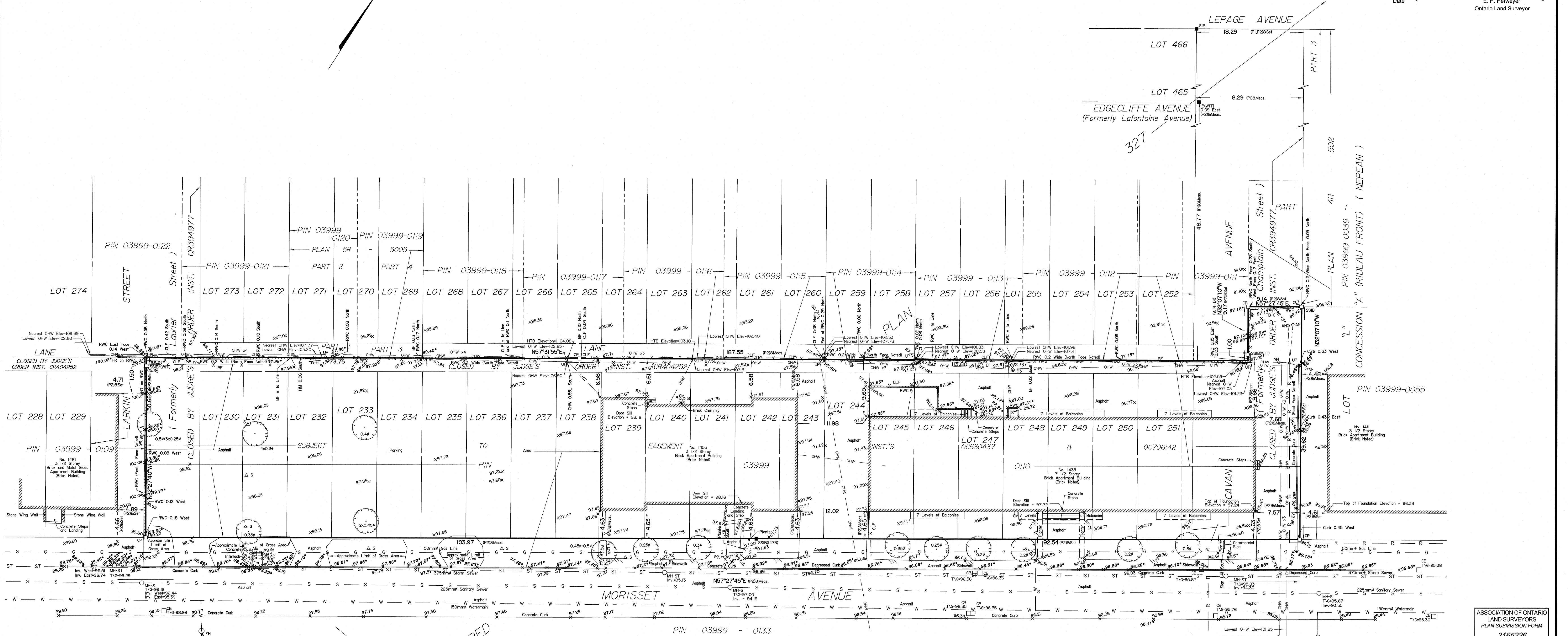
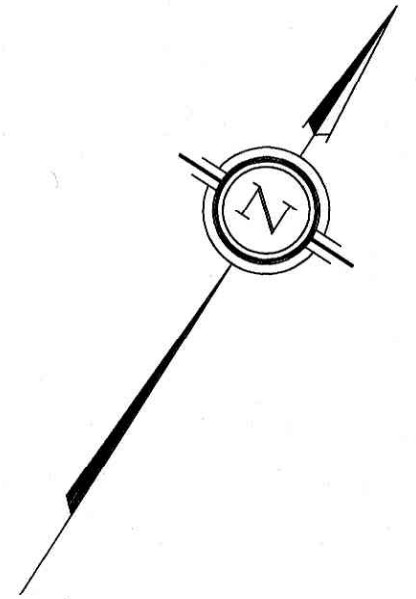
Notes & Legend

□ CB	Catch Basin	□ CB	Gas Meter
TVG	Top of Grate	□ CM	Hydro Meter
Inv.	Invert	□ HW	Cable Terminal Box
□ CM	Gas Meter	□ TB-C	Hydro Terminal Box
□ HW	Hydro Meter	□ TB-H	Bollard
□ TB-C	Cable Terminal Box	○ B	Sign
□ TB-H	Hydro Terminal Box	△ S	Chain Link Fence
○ B	Bollard	BF	Board Fence
△ S	Sign	HR	Handrail
△ S	Chain Link Fence	RWC	Concrete Retaining Wall
BF	Board Fence	○ UP	Utility Pole
HR	Handrail	○ AN	Anchor
RWC	Concrete Retaining Wall	HTB	Hydro Transformer Bolt
○ UP	Utility Pole	○ LS	Light Standard
○ AN	Anchor	□ MB	Mail Box
HTB	Hydro Transformer Bolt	□ G	Diameter
○ LS	Light Standard	□ G	Location of Elevations
□ MB	Mail Box	□ G	Top of Concrete Curb and Retaining Wall Elevation
□ G	Diameter	Elev	Elevation
□ G	Location of Elevations	C/L	Centreline
□ G	Top of Concrete Curb and Retaining Wall Elevation		
Elev	Elevation		
C/L	Centreline		

Bearings are grid, derived from Can-Net 2016 Real Time Network GPS observations and are referred to the Central Meridian of MTM Zone 9 (76°30' West Longitude) NAD-83 (original).
For comparison purposes, a rotation of 0°30'50" counter-clockwise was applied to bearings on P2.

ELEVATION NOTES
1. Elevations shown are geodetic and are referred to the CGVD28 geodetic datum, derived from City of Ottawa Benchmark No. N-29, having an elevation of 77.347.
2. It is the responsibility of the user of this information to verify that the job benchmark has not been altered or disturbed and that its relative elevation and description agrees with the information shown on this drawing.

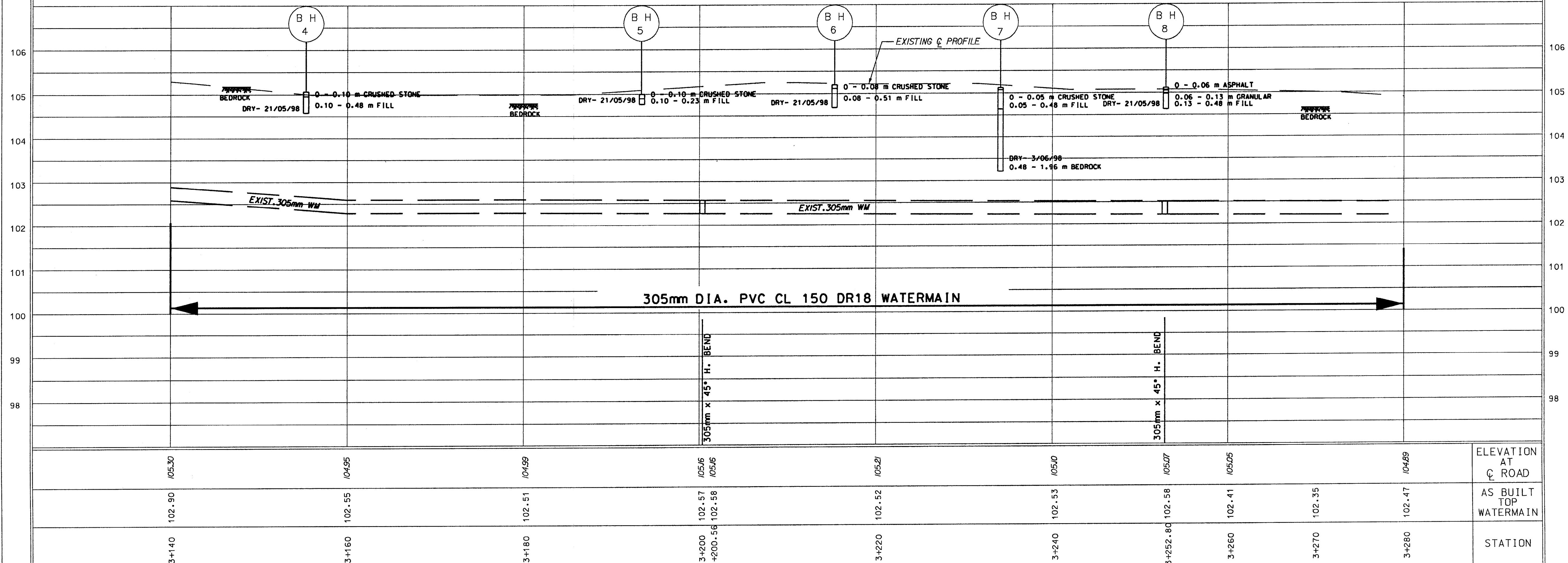
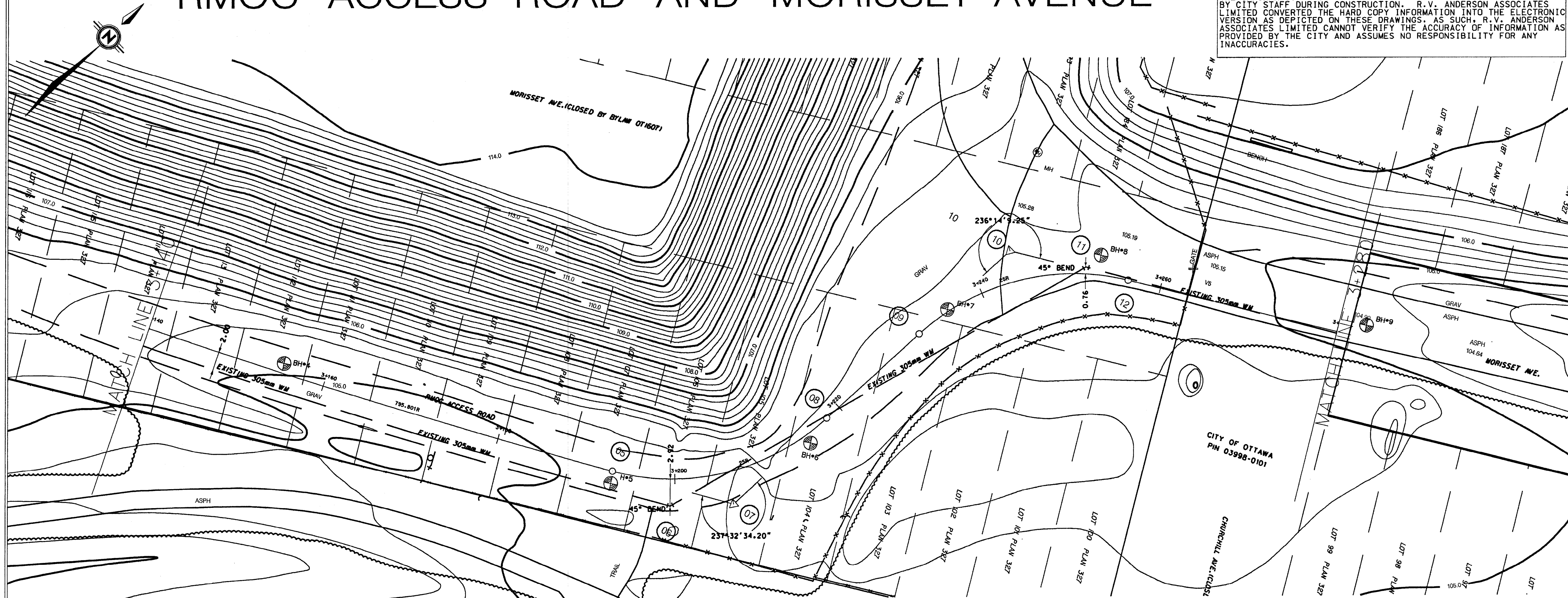
UTILITY NOTES
1. This drawing cannot be accepted as acknowledging all of the utilities and it will be the responsibility of the user to contact the respective utility authorities for confirmation.
2. Only visible surface utilities were located.
3. A field location of underground plant by the pertinent utility authority is mandatory before any work involving breaking ground, probing, excavating etc.
4. Underground utility locations derived by City of Ottawa Utility Coordinate Committee Sheets numbers H-05-12 and H-05-17, and utility inverts provided by City of Ottawa Engineering Department plans dated July 2, 1999, April 4, 1963 (Storm Sewer), and April 4, 1963 (Sewer).



RMOC ACCESS ROAD AND MORISSET AVENUE

CAUTION

THE INFORMATION SHOWN ON THE AS-BUILT DRAWINGS WAS COLLECTED BY CITY STAFF DURING CONSTRUCTION. R.V. ANDERSON ASSOCIATES LIMITED CONVERTED THE HARD COPY INFORMATION INTO THE ELECTRONIC VERSION AS DEPICTED ON THESE DRAWINGS. AS SUCH, R.V. ANDERSON ASSOCIATES LIMITED CANNOT VERIFY THE ACCURACY OF INFORMATION AS PROVIDED BY THE CITY AND ASSUMES NO RESPONSIBILITY FOR ANY INACCURACIES.



Ottawa-Carleton

ENVIRONMENT
and
TRANSPORTATION
DEPARTMENT

M.J.E. SHEFLIN P.Eng.
ENVIRONMENT and TRANSPORTATION
COMMISSIONER

Approved by: _____

Environmental Projects Branch

Date: _____

Project Manager: _____ Date: _____

Drawn by: **Ziad A. Ghadban** Sakkia * Date: _____

Survey details by: **W. Curry** Book * Date: _____

"As Built" Inspection by: _____ Date: _____

NOTES ARE TYPICAL FROM SHEET B1

R.V. Anderson Associates Limited
consulting engineers, architects, technology managers
RVA 4925
1780 Courtwood Crescent, Suite 220, Ottawa, Ontario, Canada, K2C 3B5
Tel: (613) 226-1144 Fax: (613) 226-8220 E-mail: rva@rvaa.com

KPT AS BUILT RECORD	MARCH 10 2003
GAB ISSUED FOR TENDER	MARCH 02 1999

By	Description	Date

Scales: HORIZ. 1:250
VERT. 1:50

Project Title:
**PART A
RMOC ACCESS ROAD
AND
MORISSET AVENUE
AS BUILT
305mm WATERMAIN**

STA. 3+140.000
+
STA. 3+280.000

Drawing No.: **98-3292** Sheet No.: **02**

MORISSET AVENUE

CAUTION

THE INFORMATION SHOWN ON THE AS-BUILT DRAWINGS WAS COLLECTED BY CITY STAFF DURING CONSTRUCTION. R.V. ANDERSON ASSOCIATES LIMITED CONVERTED THE HARD COPY INFORMATION INTO THE ELECTRONIC VERSION AS DEPICTED ON THESE DRAWINGS. AS SUCH, R.V. ANDERSON ASSOCIATES LIMITED CANNOT VERIFY THE ACCURACY OF INFORMATION AS PROVIDED BY THE CITY AND ASSUMES NO RESPONSIBILITY FOR ANY INACCURACIES.



ENVIRONMENT
and
TRANSPORTATION
DEPARTMENT

M.J.E. SHEFLIN P.Eng.
ENVIRONMENT and TRANSPORTATION
COMMISSIONER

Approved by: _____

Environmental Projects Branch

Date: _____

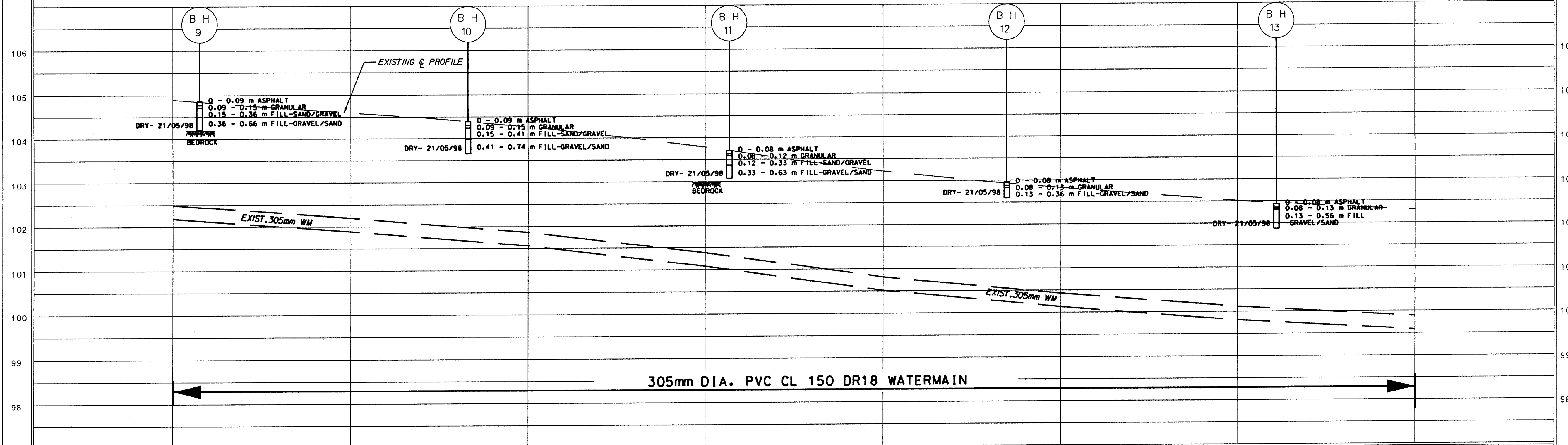
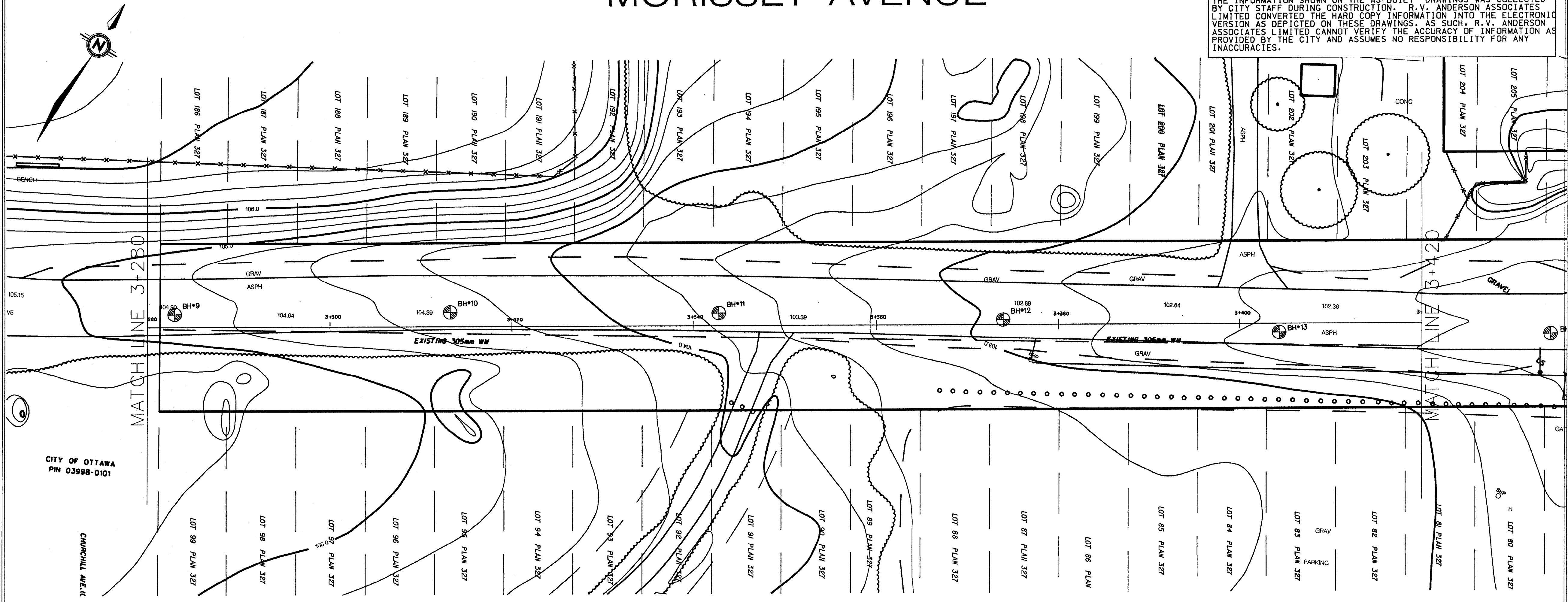
Project Manager: Ziad A. Ghodban Date: _____

Drawn by: W. Curry Book: Sakkia Date: _____

Survey details by: _____ Date: _____

"As Built" inspection by: _____ Date: _____

NOTES ARE TYPICAL FROM SHEET #1



STATION	ELEVATION AT C/Road	AS BUILT TOP WATERMAIN
3+280	102.49	102.49
3+290	102.34	102.34
3+300	102.20	102.20
3+310	102.02	102.02
3+320	101.79	101.79
3+340	101.37	101.37
3+360	100.81	100.81
3+380	100.43	100.43
3+385	100.45	100.45
3+400	100.14	100.14
3+420	99.95	99.95

R.V. Anderson Associates Limited
consulting engineers, architects, technology managers
1750 Courtwood Crescent, Suite 220, Ottawa, Ontario, Canada, K2C 2R5
Telephone: (613) 226-1844 Fax: (613) 226-8320 E-mail: ottawa@rvanderson.com

KPT	AS BUILT RECORD	MARCH 10 2003
GAB	ISSUED FOR TENDER	MARCH 02 1999

By: _____ Description: _____ Date: _____

Scales: HORIZ. 1:250
VERT. 1:50

Project Title:
PART A
MORISSET AVENUE

AS BUILT
305mm WATERMAIN

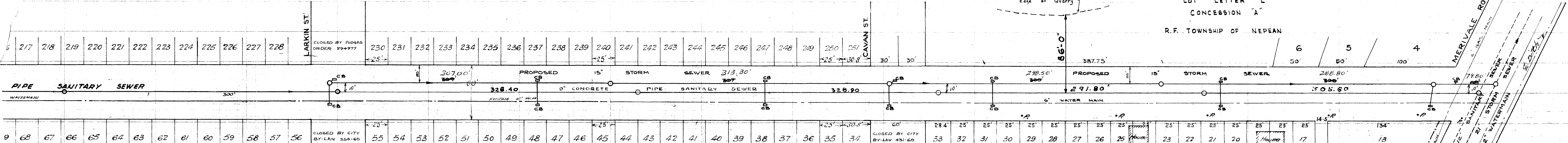
STA. 3+280.000
to
STA. 3+420.000

Drawing No.: **98-3293** Sheet No.: **03**

T A V E.

Rock Elevations

2435	30220	Solid Rock	(Begins)
3100	30210	Solid Rock	(Ends)
3140	30570	Solid Rock	(Begins)
4130	31040	Solid Rock	(Ends)
5100	31500		
6100	31900		
7100	32300		
8100	32700		
9100	33100		
10130	33500		
11150	33900		
12120	34300		
13170	34700		
13709	35100		



NOTE: SANITARY SEWER LARKIN TO LOTS 201 & 76
 Work commenced: Oct. 1/59
 Work completed: Oct. 10/59
 Contractor: Purcell
 Inspector: Z. Gusewsky
 Final Measurements: Book 470
 Page: 21
 Date: Oct. 28/59

WORK COMMENCED: AUG. 1957
 WORK COMPLETED: SEPT. 1957
 CONTRACTOR: H.P. HEAFLEY
 INSPECTOR: K.HAY
 FINAL MEASUREMENTS: BOOK 331 Page 10
 DATE: SEPT. 6 1957

MORISSET AVENUE
 MERIVALE RD TO LARKIN AVE.
 STORM SEWER

DESIGNED BY: G.L.P.
 DRAWN BY: G.L.P.
 CHECKED BY: G.L.P.
 DATE: APR. 1955

INSPECTOR: Z. GUSEWSKY

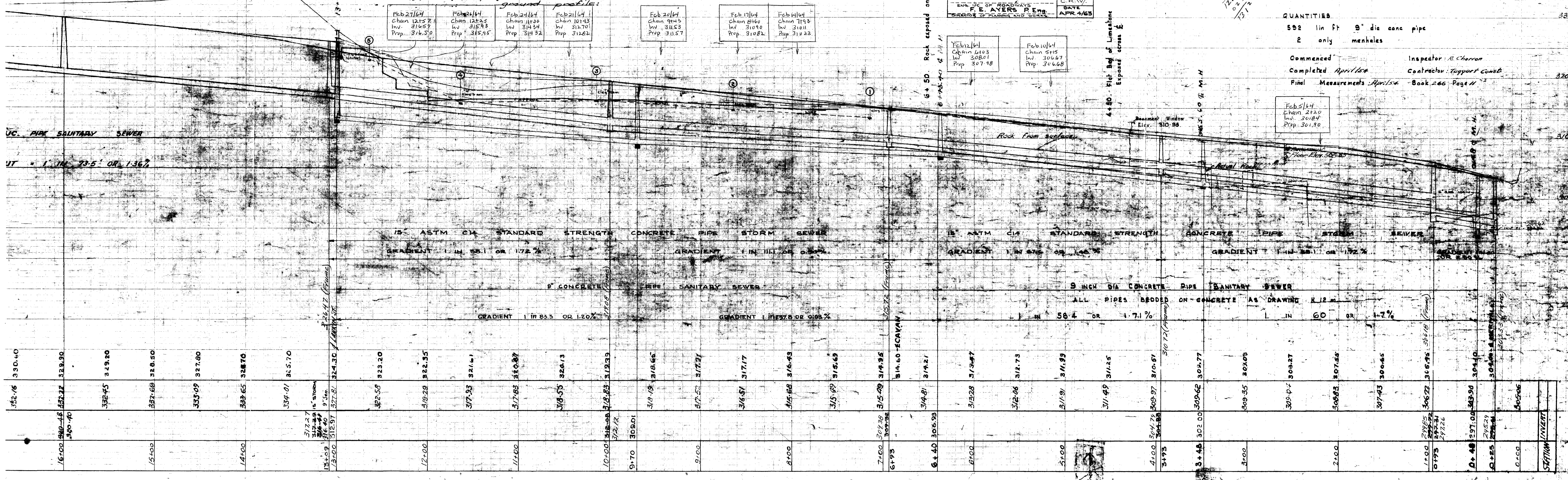
Survey: Book 503 page 9-10
 Levels: Book 501 - 68-69-70-71-72

Note: Rock elevation is same as ground profile

Work commenced: Oct. 1/59
 Work completed: Oct. 10/59
 Contractor: Purcell
 Inspector: Z. Gusewsky
 Final Measurements: Book 470
 Page: 21
 Date: Oct. 28/59

Note: Rock Elevation same as ground profile:

Feb 23/54	Chain 2127	Inv. 31657	Prop. 31650
Feb 24/54	Chain 1825	Inv. 31573	Prop. 31545
Feb 24/54	Chain 1825	Inv. 31573	Prop. 31545
Feb 24/54	Chain 1825	Inv. 31573	Prop. 31545
Feb 24/54	Chain 1825	Inv. 31573	Prop. 31545
Feb 24/54	Chain 1825	Inv. 31573	Prop. 31545
Feb 24/54	Chain 1825	Inv. 31573	Prop. 31545



WORK COMMENCED: Oct. 1/59
 WORK COMPLETED: Oct. 10/59
 CONTRACTOR: Purcell
 INSPECTOR: Z. Gusewsky
 Final Measurements: Book 470
 Page: 21
 Date: Oct. 28/59

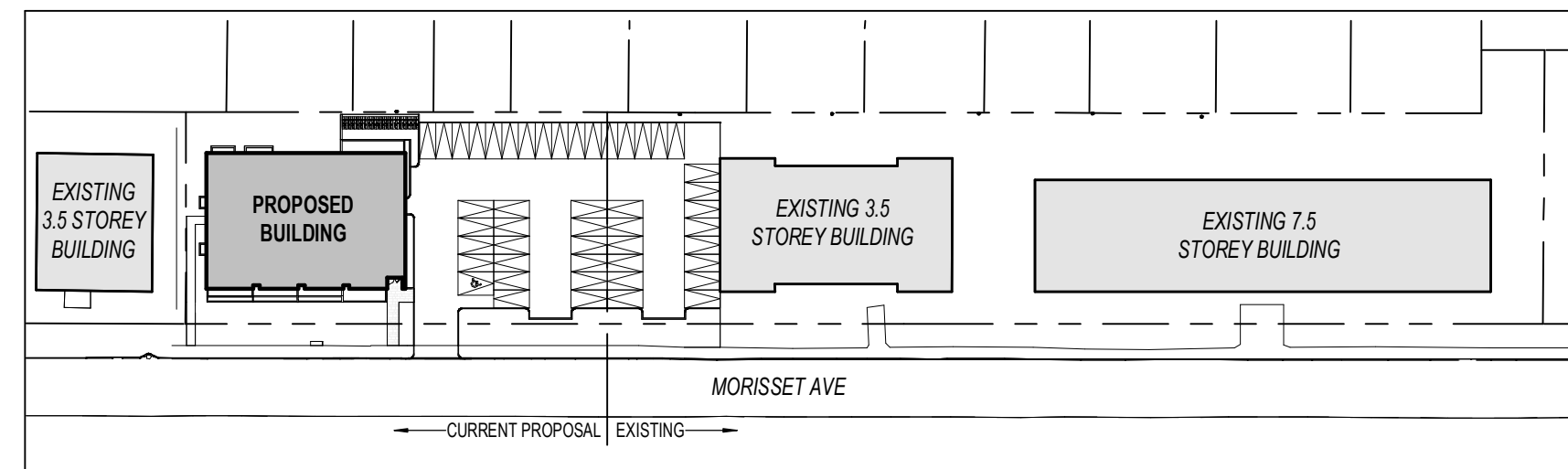
CITY OF OTTAWA
 ENGINEER-IN-CHIEF

MORISSET MERIVALE

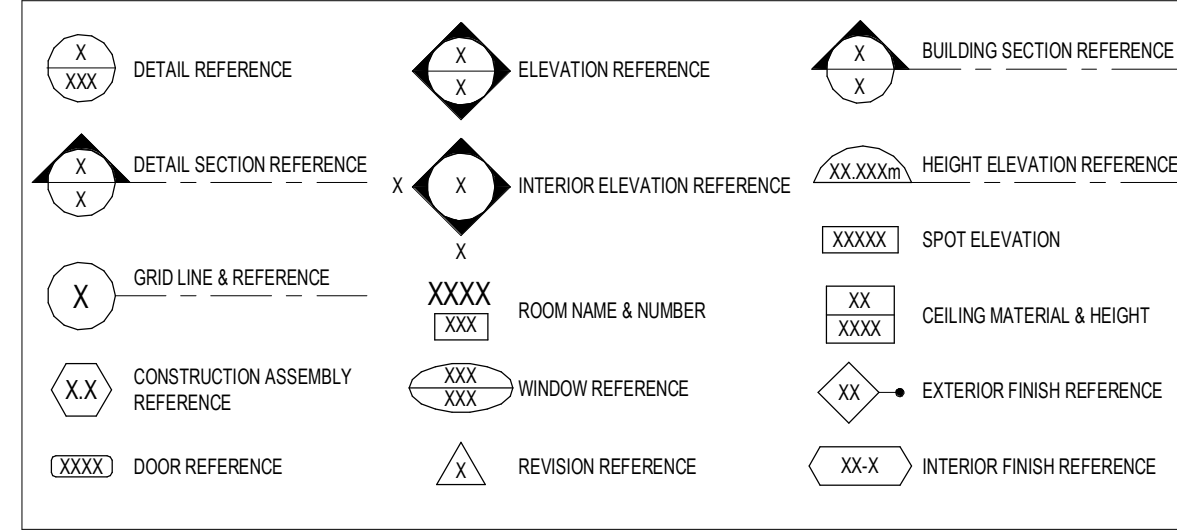
Commissioner of Works
 Asst. Commissioner of Works
 Surveyor
 Designing Engineer



3 LOCATION PLAN
SP-01 SCALE: N.T.S.



2 KEY PLAN
SP-01 SCALE: 1:1000



4 NOTATION LEGEND
SP-01 SCALE: N.T.S.

UNIT COUNT						
BEDS	LVL 00	LVL 01	LVL 02	LVL 03	TOTAL	%
1-BED	1	2	2	2	8	23%
1-BED + DEN	0	2	2	2	6	20%
1-BED BF	2	0	0	0	2	7%
2-BED	1	4	4	4	13	43%
2-BED BF	2	0	0	0	2	7%
TOTAL	6	8	8	8	31	100%

RESIDENTIAL UNIT SCHEDULE			
NUMBER	UNIT TYPE	BEDS	AREA
LEVEL 00			
001	TYPE E-BF	2-BED BF	86.62 m ²
002	TYPE F-BF	1-BED BF	59.08 m ²
003	TYPE D	2-BED	67.48 m ²
004	TYPE A-BF	2-BED BF	73.94 m ²
005	TYPE B-BF	1-BED BF	60.12 m ²
006	TYPE C	1-BED	58.67 m ²
007	TYPE D	1-BED	58.32 m ²
LEVEL 01			
101	TYPE K	2-BED	67.15 m ²
102	TYPE L	1-BED	59.10 m ²
103	TYPE L	1-BED	59.08 m ²
104	TYPE K1	2-BED	67.48 m ²
105	TYPE H	2-BED	73.94 m ²
106	TYPE I	1-BED + DEN	60.12 m ²
107	TYPE I (MIR)	1-BED + DEN	60.12 m ²
108	TYPE J	2-BED	73.95 m ²
LEVEL 02			
201	TYPE K	2-BED	66.47 m ²
202	TYPE L	1-BED	58.22 m ²
203	TYPE L	1-BED	58.01 m ²
204	TYPE K2	2-BED	66.38 m ²
205	TYPE H	2-BED	73.94 m ²
206	TYPE I	1-BED + DEN	60.12 m ²
207	TYPE I (MIR)	1-BED + DEN	60.12 m ²
208	TYPE J	2-BED	73.95 m ²
LEVEL 03			
301	TYPE K	2-BED	66.56 m ²
302	TYPE L	1-BED	58.22 m ²
303	TYPE L	1-BED	58.01 m ²
304	TYPE K2	2-BED	66.38 m ²
305	TYPE H	2-BED	73.94 m ²
306	TYPE I	1-BED + DEN	60.12 m ²
307	TYPE I (MIR)	1-BED + DEN	60.12 m ²
308	TYPE J	2-BED	73.95 m ²

GROSS AREA		
LEVEL	AREA	AREA (SF)
LEVEL 00	561.13 m ²	6040 SF
LEVEL 01	563.15 m ²	6062 SF
LEVEL 02	559.99 m ²	6028 SF
LEVEL 03	556.47 m ²	5990 SF
TOTAL	2,240.74 m²	24,118 SF

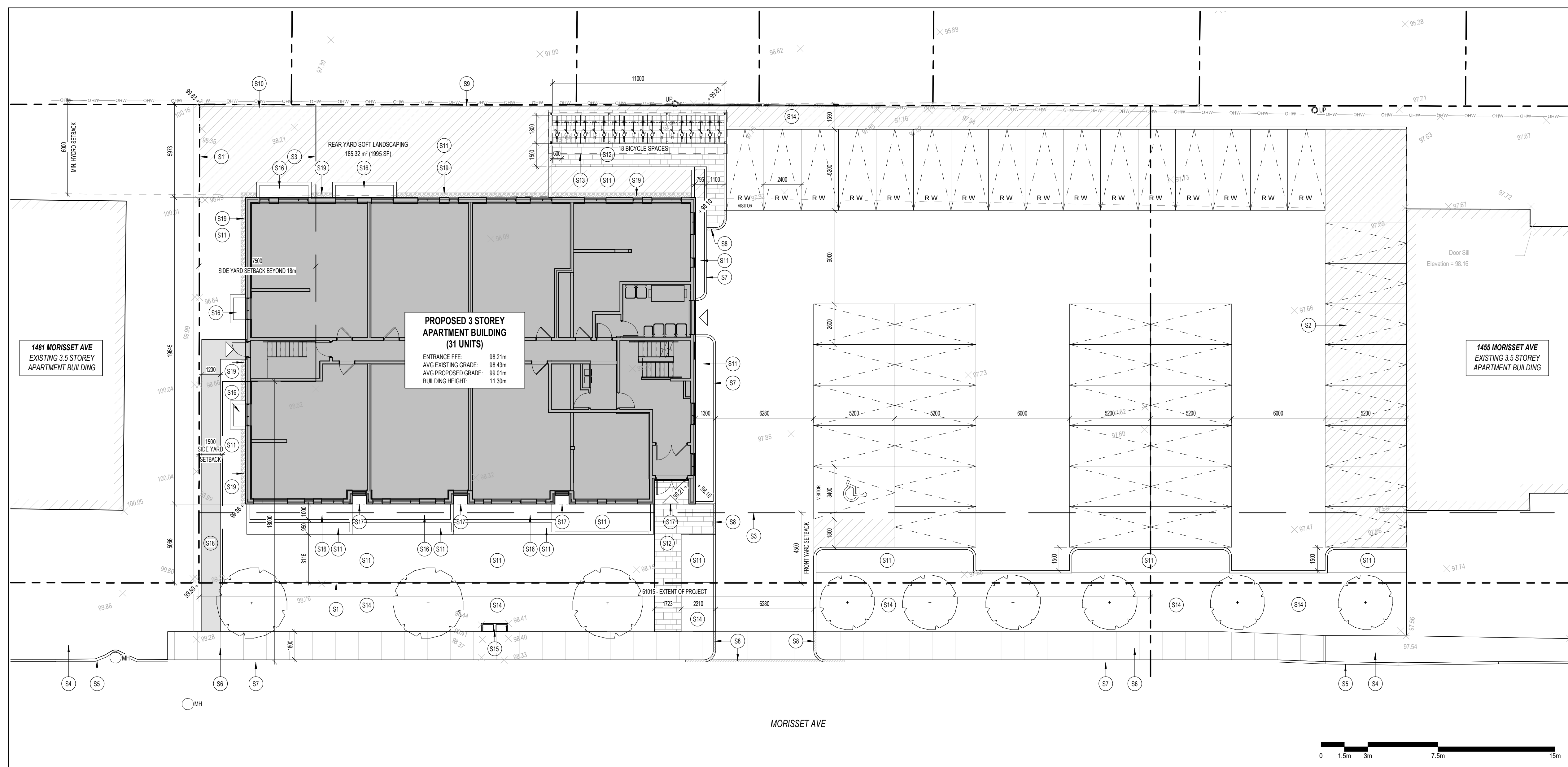
RENTABLE AREA (RESIDENTIAL)		
LEVEL	AREA	AREA (SF)
LEVEL 00	461.23 m ²	4,965 SF
LEVEL 01	520.94 m ²	5,607 SF
LEVEL 02	517.20 m ²	5,557 SF
LEVEL 03	517.30 m ²	5,558 SF
TOTAL	2,016.67 m²	21,707 SF

SITE STATISTICS		
Current Zoning Designation:	R4 - UC	
Lot Width:	61.0 m	
Total Lot Area:	6,092 m ²	
Average Existing Grade:	96.44 m	
Gross Floor Area:	2,240.74 m ²	
Building Area:	561.54 m ²	
Floor Space Index:	0.37	

PROPOSED DEVELOPMENT - 3 STOREY LOW-RISE APARTMENT BUILDING		
Existing 7.5 Storey Mid-Rise Apartment Building - 1435 Morisset Ave & Existing 3.5 Storey Low-Rise Apartment Building - 1455 Morisset Ave (135 Units Combined)		
Proposed 3 Storey Low-Rise Apartment Building - (31 Units)		
Zoning Mechanism		
Minimum Lot Width 162A	Required	Provided
162A	N/A	EXISTING - 196.5 m PROPOSED SCOPE - 61 m
Minimum Lot Area 162A	1,400 m ²	6,092 m ²
Min. Front Yard Setback 162A	4.5 m	5.06m
Min. Interior Side Yard Setback 162B(1/3)	1.5 m (first 18m from street) 7.5 m (beyond 18m)	3 m
Min. Rear Yard Setback 162B(4)	7.5 m	5.97 m
Maximum Building Height 162A	11 m	11.3 m
Hydro Setback	6 m	6 m
Parking Space Rates 101 (Sch. 1A - Area Y)	10 Spaces 0 spaces for the first 12 units - Section 101(3) 0.5 spaces / unit for 19 units - Table 101(R15)	45 Spaces within area of work + 19 existing spaces = 64 spaces total
Minimum Visitor Parking Rates 101 (Sch. 1A - Area Y)	2 Spaces 0 spaces for first 12 units - Section 102(2) 0.1 spaces / unit for 19 units - Table 102	2 Spaces within area of work + 13 existing spaces = 15 spaces total
Bicycle Parking Rates Table 111A (Sch. 1 - Area X)	16 Spaces 0.5 spaces / unit for 31 units [111A(b)]	18 Spaces
Landscaped Areas	560.78 m ² (30% of Lot Area) 180.58 m ² (30% of Rear Yard) 109.82 m ² (40% of Front Yard)	436.83 m ² (23% of Lot Area) 155.44 m ² (25% of Rear Yard) 167.99 m ² (61% of Front Yard)

GENERAL ARCHITECTURAL NOTES:

- This drawing is the property of the Architect and may not be reproduced or used without the expressed consent of the Architect.
- Drawings are not to be scaled. The Contractor is responsible for checking and verifying all levels and dimensions and shall report all discrepancies to the Architect and obtain clarification prior to commencing work.
- Upon notice in writing, the Architect will provide written clarification or supplementary information regarding the intent of the Contract Documents.
- The Architectural drawings are to be read in conjunction with all other Contract Documents including Project Manuals and the Structural, Mechanical and Electrical Drawings.
- Positions of exposed or finished Mechanical or Electrical devices, fittings and fixtures are indicated on the Architectural Drawings. Locations shown on the Architectural Drawings shall govern over Mechanical and Electrical Drawings. Mechanical and Electrical items not clearly located will be located as directed by the Architect.
- These documents are not to be used for construction unless specifically noted for such purpose.



PLAN OF SURVEY OF LOTS 230 TO 251 (BOTH INCLUSIVE) AND PART OF CAVAN STREET AND PART OF LARKIN STREET AND PART OF THE LANE REGISTERED PLAN 327 CITY OF OTTAWA
ANNIS, OSULLIVAN, VOLLEBEKK LTD. 2021

SURVEY INFO
SCALE: N.T.S.

SITE PLAN NOTES

- S1 PROPERTY LINE
- S2 HATCH DENOTES EXTENT OF EXISTING ASPHALT TO REMAIN
- S3 LINE DENOTES LOCATION OF SETBACK
- S4 EXISTING ASPHALT SIDEWALK
- S5 EXISTING CONCRETE CURB
- S6 PROPOSED CONCRETE SIDEWALK
- S7 CONCRETE CURB
- S8 DEPRESSED CURB
- S9 EXISTING RETAINING WALL AND FENCE TO BE REMOVED AND REPLACED
- S10 NEW RETAINING WALL AND FENCE REFER TO CIVIL
- S11 PLANTING BED
- S12 INTERLOCKING STONE PAVERS
- S13 LINE DENOTES EXTENT OF COVERED BIKE STORAGE
- S14 SOFT LANDSCAPING
- S15 EXISTING MAILBOXES TO REMAIN
- S16 WINDOW WELL
- S17 LINE OF BUILDING ABOVE
- S18 ASPHALT WALKWAY
- S19 MAINTENANCE STRIP, REFER TO LANDSCAPE

SITE PLAN SYMBOLS LEGEND

- BUILDING ENTRANCE
- BUILDING EXIT
- BICYCLE PARKING
- INTERLOCKING STONE PAVERS
- PROPERTY LINE
- SETBACK LINE
- OVERHEAD WIRE
- FDC FIRE DEPARTMENT CONNECTION
- FH FIRE HYDRANT
- UP EXISTING UTILITY POLE TO REMAIN
- MH EXISTING MANHOLE

ISSUE RECORD

9	ISSUED FOR BUILDING PERMIT	24-12-06
8	ISSUED FOR COORDINATION	24-12-05
5	ISSUED FOR COORDINATION	24-11-22
4	ISSUED FOR COORDINATION	24-11-19
3	ISSUED FOR COORDINATION	24-10-24
2	ISSUED FOR COORDINATION	24-10-18
1	ISSUED FOR COORDINATION	24-10-08



project1 studio
Project1 Studio Incorporated
[613.884.3939 | mail@project1studio.ca]

1465 MORISSET
1465 Morisset Avenue
Ottawa, ON K1Z 8H4

PROJ	SCALE	DRAWN	REVIEWED
2412	NOTED	JDH/BH	RMK

SITE PLAN

SP-01

1 SITE PLAN
SP-01 SCALE: 1:150