UNIVERSITY OF OTTAWA

NOISE AND VIBRATION IMPACT ASSESSMENT LEES CAMPUS - FACULTY OF HEALTH SCIENCES BUILDING

OCTOBER 21, 2021



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UNIVERSITY OF OTTAWA

VERSION 2.0

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SIGNATURES

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Abbreviations

dB	decibel	
dBA	decibel, A-weighted	
Hz	Hertz	
ISO	International Organization for Standardization	
КРН	Kilometers per hour	
km	kilometre(s)	
Leq(16)	Daytime 16-hour (0700-2300) Energy Equivalent Sound Level (Leq)	
Leq(8)	Nighttime 8-hour (2300-0700) Energy Equivalent Sound Level (Leq)	
Leq	Energy Equivalent Sound Level over a period of time	
m	metre(s)	
m ²	square metre(s)	
MECP	Ontario Ministry of the Environment, Conservation and Parks	
ORNAMENT	Ontario Road Noise Analysis Method for Environment and Transportation	
POR	point of reception	
RMS	root mean square	
STEAM	Sound from Trains Environmental Analysis Method	

Glossary	
A-weighting	The weighting is applied to sound level data to account for changes in level sensitivity as a function of frequency. The A- weighting adjustment reflects average human ear.
decibel (dB)	A logarithmic quantity of generally used in the measurement of sound. The decibel (dB) provides the possibility of representing a large span of sound levels in a simplified manner. It is used for both sound pressure level as well as sound power level. When it is used to refer sound pressure level, a location or distance from a source is usually provided with the sound pressure level.
decibel, A-weighted (dBA)	A-weighted decibels (dBA). Most common units for expressing sound levels approximating the response of the human ear.
energy equivalent sound level	An energy-average sound level (Leq) over a specified period that would have the same sound energy as the actual (i.e., time varying) sound over the same period.
frequency	The number of times per second that the sine wave of sound repeats itself. It can be expressed in cycles per second, or Hertz (Hz).
frequency weighting (A, B, and C Weighting)	A method used to account for changes in sensitivity as a function of frequency. Three standard weighting networks, A, B, and C are used to account for different responses to sound pressure levels.
	Most commonly used weighting is A-weighting (see also A-weighting).
Hertz (Hz)	The unit of frequency also expressed as cycles per second.
noise	Unwanted sound.
octave band	The interval between two frequencies having a ratio of two to one. For acoustical measurements, the octaves start a 1,000 Hz centre frequency and go up or down from that point, at the 2:1 ratio. From 1,000 Hz, the next filter's centre frequency is 2,000 Hz, the next is 4,000 Hz, or 500 Hz, 250 Hz, etc.

point of reception (POR)	A noise-sensitive receptor such as a residence, campground, daycare, school, church, or hospital as defined in Ontario Ministry of the Environment and Climate Change Publication NPC-300.
root mean square (vibration)	The root mean square of a vibration velocity signal is the square root of the average of the squared velocity of the vibratory signal.
sound power level	The total sound energy radiated by a source per unit time. The unit of measurement is the Watt. The acoustical power radiated from a given sound source as related to a reference power level (i.e., typically 1E 12 watts, or 1 picowatt) and expressed as decibels. A sound power level of 1 watt = 120 decibels relative to a reference level of 1 picowatt.
sound pressure level	Logarithmic ratio of the root-mean-square sound pressure to the sound pressure at the threshold of human hearing (i.e., 20 micropascals).
vibration	Vibration is defined as an oscillatory motion of an element/particle. LRT related vibration is described in terms of the velocity. The velocity represents the instantaneous speed of the element/particle.

1 INTRODUCTION

WSP Canada Inc. (WSP) was retained by PCL Construction to prepare a Noise Impact Assessment for the proposed Faculty of Health Sciences Building at Lees Campus, University of Ottawa (Lees Campus or FHSB) to be located at 200 Lees Avenue, Ottawa, Ontario. This study addresses the noise impacts of stationary sources associated with the nearby buildings (Block A and Block B) as well as noise sources from development itself. In addition, it also considers the transportation sources associated with the nearby roads and LRT corridor on the proposed sensitive receptors. This report is prepared in support of a Site Plan Approval applications required at this stage of the development.

The noise impact assessment was conducted in accordance with the "Environmental Noise Control Guidelines", by City of Ottawa's, Planning Infrastructure and Economic Development (Ottawa Guidelines) as well as Ontario Ministry of the Environment, Conservation and Parks (MECP's) Noise Pollution Control (NPC) publication NPC-300 "Environmental Noise Guideline, Stationery and Transportation Sources – Approval and Planning".

In accordance with the Ottawa Guidelines as well as NPC-300 requirements, this report discusses environmental noise from stationary sources and transportation sources as well as vibration from LRT corridor on the development. The results are presented in Section 3. Summary of recommendations are presented in Section 4.

Road traffic data was obtained from Ottawa Guidelines and Ottawa LRT was obtained from operation schedule of Ottawa. This data was used to estimate future sound levels (LEQ) at the façades of the proposed FHSB. Using the traffic data, proposed site plan and design drawings a predictive analysis was completed to estimate the future sound level at the proposed building façade. Similarly, using the information in the mechanical design drawings stationary sources of sound from were estimated. Both sound level from transportation sources (i.e., noise from road and LRT transportation corridor) and stationary sources (e.g., noise from roof top units) were compared to the guideline limits provided in the Ottawa Guidelines and MECP publication NPC-300. Similarly, vibration from LRT operations were estimated and assessed against the appropriate limits to establish compliance. The details are discussed within this report.

2 SITE DESCRIPTION

The proposed development is located east of Ottawa LRT and Lees Road (200 Lees Road), south of Highway 417 and north of Rideau River.

The location of the proposed development and surrounding land uses are presented in Figure 1.

The proposed development will include 5-storey building. A mechanical penthouse is proposed on the top floor. The site plan of the proposed development is included in **Appendix A**.

The acoustical environment surrounding the site is considered urban in nature, where anthropogenic noise dominates day and nighttime acoustic environment. The surrounding area is zoned for commercial purpose and a zoning map from the City of Ottawa is provided in **Figure 2**.

3 IMPACT OF THE SURROUNDING ENVIRONMENT ON THE DEVELOPMENT

The environmental noise and vibration sources with potential to have effect on the development are discussed and assessed in this section. The following sources are identified:

- Transportation noise impacts from roads and LRT;
- Vibration impacts from LRT; and
- Stationary noise from Block A, Block B and development (Ref: Figure 3).

The proposed development is not within the noise influence area (i.e. Noise Exposure Forecast/Noise Exposure Projection (NEF/NEP) contours) of Ottawa International Airport; therefore, assessment of aircraft noise is not considered in this report.

On the east of the development, two existing buildings identified as Block A and Block B are located; these buildings are closer to the proposed development than any other buildings in the area. These buildings have existing stationary noise sources associated with them (i.e., HVAC units and exhaust fans). There are some residential and utility land uses such as 190 Lees Road apartment buildings to the west and Lees LRT station to the northwest of the Site. There are potential stationary noise sources associated with these types of facilities, however they are further away from the development and are not considered a significant stationary noise source. The buildings in the surrounding area and associated activities within those buildings are not considered significant sources of noise or vibration.

This section discusses the transportation noise sources, stationary sources as well as vibration from LRT operation.

3.1 TRANSPORTATION NOISE IMPACTS

3.1.1 NOISE SOURCES

The following transportation sources have the potential to contribute to the sound levels at the proposed development:

- Highway 417;
- Lees Avenue; and
- Ottawa LRT

The proposed FHSB is within 100 meters of Lees Road and LRT and within 250 meters of Highway 417; as per Ottawa Guideline, a noise study will be required.

3.1.2 NOISE GUIDELINES AND ASSESSMENT CRITERIA

Noise is recognized as a pollutant in the Environmental Protection Act, as uncontrolled noise can affect human activities. Ontario provincial noise control guidelines require that noise concerns are addressed in the planning of any new development.

In land use planning, although elimination or control of the source of pollution is usually a primary objective, there are general limits as to what is practical and technically possible. Therefore, Ottawa Guidelines and MECP Publication NPC-300, "Environmental Noise Guideline Stationery and Transportation Sources – Approval and Planning" provides sound level criteria for acceptable levels of transportation noise impacting on residential developments. These limits are discussed in **Table 3-1** below.

NPC-300 and Ottawa Guideline provides sound level limits in terms of energy equivalent (average) sound levels $[L_{EQ}]$ in units of A-weighted decibels [dBA] at a specific noise-sensitive location.

Table 3-1 NPC-300 Sound Level Criteria for Road and LRT Noise

AREA	TIME PERIOD	L _{EQ} (dBA) -ROAD	L _{EQ} (dBA) -LRT
Outdoor Living Area (OLA)	Daytime (0700 – 2300h)	Ę	55
hospitals,	Daytime (0700 – 2300h)	45	40
nursing homes, schools	Nighttime (2300 – 0700h)	45	40

3.1.3 OUTDOOR REQUIREMENTS

If the future daytime (0700 - 2300h) sound level in an OLA is 55 dBA or less, no control is required; an excess of daytime sound level up to 5 dBA over the 55 dBA limit is often acceptable without noise control, however such excess should be notified to the future occupants (in case of residential receptors) with a warning clause. If sound level exceeds 60 dBA, feasibility of controlling the noise in terms of economic, technical and administrative feasibility should be investigated and where possible noise control is to be included in the design. **Table 3-2** summarizes the requirements for OLAs and also provide warning clause requirements typically considered in residential developments.

Table 3-2 Requirements for Outdoor Living Areas

AREA	TIME PERIOD	SOUND EXPOSURE LEVEL LEQ 16- HR (dBA)	WARNING CLAUSE REQUIREMENTS
U		<u><</u> 55	None
		> 55 and <u><</u> 60	 Noise mitigation to reduce noise to 55 dBA or below; Warning Clause (Type A) – generally considered for residential development and not typically considered for institutional development
Outdoor Living Area (OLA)	Daytime (0700 – 2300h)	> 60	 Preferred: Noise mitigation to reduce noise to 55 dBA or Noise mitigation to reduce noise to 60 dBA and Warning Clause (Type B) – generally considered for residential development and not typically considered for institutional development Mitigation can be: Distance Setback with Soft Ground Insertion of insensitive land use between source and receptor

 Orientation of buildings to provide sheltered zones in rear yards Shared outdoor amenity areas
Berm or barrier

3.1.4 VENTILATION, BUILDING REQUIREMENTS

In order to decide appropriate control to achieve the above noted sound level limits, NPC-300 and Ottawa Guideline has provided further guidance.

To achieve indoor sound levels listed in **Table 3-1**, the MECP and Ottawa guideline provides guidelines based on predicted sound level at the façade/plane of window. If the predicted sound level at the plane of window exceeds, additional considerations such as the type of ventilation; type of windows, exterior walls, and doors that will be required must be selected. It also provides guidance for warning clauses that are usually considered for residential development. The key control requirements are summarized below in **Table 3-3**.

AREA	TIME PERIOD	SOUND LEVEL EXPOSURE LEQ (DBA) ROAD AND LRT ^[2]	VENTILATION REQUIREMENTS
	Daytime (0700 – 2300h)	< 55	None
		>55 and <65	Forced Air Heating with provision for central air condition
		> 65	Central air conditioning is required
Plane of	Nighttime (2300 – 0700h)	< 50	None
		>51 and <60	Forced Air Heating with the provision to add central air conditioning
		> 60	Central air conditioning is required

Table 3-3 Ventilation Requirements

Notes: [1] Plane of Window.

[2] Daytime: L_{EQ 16HR}; Nighttime: L_{EQ 8-HR}.

Table 3-4 provides sound level thresholds which if exceeded, will require building façade construction to be designed and selected to meet indoor sound criteria in **Table 3-1** is met. Building component requirements are assessed separately for road and railway noise. The resultant sound isolation parameter is required to be combined to determine the overall acoustic parameter.

Table 3-4 Building Requirements

AREA	TIME PERIOD	SOUND EXPOSURE LEVEL (dBA) ROAD ^[2]	SOUND EXPOSURE LEVEL (dBA) LRT ^[2]	BUILDING COMPONENT REQUIREMENTS
Plane of Window ^[1]	Daytime (0700 – 2300h)	<u><</u> 65	<u><</u> 60	Building components compliant with Ontario Building Code (OBC)
		> 65	> 60	Building components designed/selected to meet Indoor Requirements

	Nighttime (2300 – 0700h)	<u><</u> 60	<u><</u> 55	Building components compliant with Ontario Building Code (OBC)
		> 60	> 55	Building components designed/selected to meet Indoor Requirements

Notes: [1] Plane of Window.

[2] Daytime: L_{EQ 16HR}; Nighttime: L_{EQ 8-HR}.

Note about Warning Clauses:

The warning clauses are generally applied for residential developments, where purchases, lease or rentals are expected to inform future occupants. In this case the Faculty of Health Sciences Building will be designed to meet the requirements and there are no specific purchase, lease or rental anticipated in an institutional facility and therefore warning clauses are not considered applicable or discuss further.

3.1.5 TRAFFIC DATA

Road traffic volumes were obtained from the Ottawa Guideline (dated January 2016). Traffic data is provided in **Appendix B** for Highway 417 and Lees Road and is summarized in **Table 3-5**. The data taken from the Ottawa Guideline provides ultimate future traffic volume data for various roadways based on roadway class and number of lanes. The traffic data used represents future traffic volumes and corresponding to a "mature state of development", in the City's Official Plan.

ROAD	TRAFFIC VOLUMES (AADT)	NO. OF LANES	DAY/NIGHT SPLIT (%)	MEDIUM TRUCKS (%)	HEAVY TRUCKS (%)	POSTED SPEED LIMIT (KPH)
Highway 417	183,33 ^[1]	10	92/8	7%	5%	100
Lees Road	15,000	2	92/8	7%	5%	50

Table 3-5 Summary of Road Traffic Data Used in the Transportation Analysis

Notes: [1] AADT per lane.

Road traffic data and calculations used for the study are included in Appendix B.

The subway data was obtained from posted schedule. This information is provided in **Appendix B** and is summarized in **Table 3-6**.

Table 3-6 Summary of LRT Traffic Data Used in the Transportation Analysis

TYPE	DAYTIME	NIGHTTIME	LOCOMOTIVE	SPEED LIMIT (KPH)
LRT	234	44	LRT	50

3.1.6 NOISE IMPACT ASSESSMENT METHODS

Per MECP Guidelines, the impact at receptors was estimated for the road and LRT traffic. The sound level predictions were made using STAMSON version 5.04, a computer algorithm developed by the MECP. Figures 4 to 9 shows the angles of exposure and distance from the roads for each receptor. The receptor height is included in **Table 3.7**. A copy of the sample STAMSON output file is also included in **Appendix C**. Since there are no at-grade level crossings in the vicinity, whistle noise was not included in the calculations.

The following factors were taken into account in the analysis:

- Vehicle/Train speeds;
- Road and LRT traffic and volumes;
- Percentage of trucks;
- Horizontal and vertical road/LRT-receiver geometry;
- Ground absorption; and
- Screening provided by terrain, houses or existing barriers.

Most impacted receptor locations (in terms of façade and height) were chosen as representative receptor locations for each facade. The modelled receptor locations are shown in the site plan included in **Figure 3**. The parameters used in STAMSON to assess the noise impacts at the receiver locations can be found in Table C1 in **Appendix C**. **Figures 4** to **9** shows the corresponding angles and distances used in the model.

3.1.7 RESULTS

3.1.7.1 PLANE OF WINDOW

Sound levels were predicted at the most impacted façades during the daytime and nighttime hours. The predicted sound levels were used to investigate ventilation and building construction requirements. The results of these predictions are summarized in **Table 3-7**.

LOC ID	DESCRIPTION	RECEIVER HEIGHT (M)	SPL – DAYTIME (dBA)	SPL – NIGHTTIME (dBA)
POR01	Southeast - South Façade (5th Level)	22.2	51	47
POR02	Southwest - South Façade (5th Level)	22.2	55	51
POR03	Southwest - West Façade (5th Level)	22.2	69	61
POR04	Southwest - West Façade (2nd Level)	9.6	70	63
POR05	Northwest- West Façade (5th Level)	22.2	71	64
POR06	Northwest- North Façade (5th Level)	22.2	74	66
POR07	Northeast - East Façade (5th Level)	22.2	75	67
POR08	East Façade (5th Level)	22.2	74	66
POR09	North Façade of east wing (5th Level)	22.2	73	65
POR10	Northeast - North Façade of east wing (5th Level)	22.2	74	67
POR11	East Façade on east wing (5th level)	22.2	72	65

Table 3-7 Summary of Predicted Facade Sound Levels – Transportation (Road & LRT)

The façade level indicates that due to the magnitude of exterior sound level, there is potential to exceed indoor sound level; therefore, as per NPC-300 noise control façade construction and ventilation requirements are required.

3.1.7.2 OUTDOOR LIVING AREA (OLA)

A review of site plans indicates that there are outdoor areas such as social areas, outdoor academic quad, river terrace; these areas are considered outdoor amenity areas for completeness. The terrace is located at the southwest corner of the building and others are located on the east of proposed building. The predicted sound levels for the three (3) outdoor amenity areas shown in Figure 3, Figures 7 to 9 are summarized in **Table 3-8**.

PREDICTION LOCATION	DESCRIPTION	DAYTIME SOUND LEVEL (DBA)
OLA1	At grade outdoor amenity area - southwest corner of the property (River Terrace)	56
OLA2	At grade outdoor amenity area – east of the proposed building (Academic Quad)	60
OLA3	At grade outdoor amenity area – east of the proposed building (Indigenous Pavilion & Firepit gathering circle)	60

Table 3-8 Summary of Predicted OLA Sound Levels – Transportation (Road)

3.1.8 RECOMMENDATIONS

The following discussion outlines the preliminary recommendations for outdoor and building facade constructions, and ventilation requirements to achieve the noise criteria stated in **Table 3-1**.

3.1.8.1 OUTDOOR LIVING AREA

The sound levels the OLAs are predicted to be below 60 dBA and the design includes 3 m screens as shown in Figures 8 and 9. Up to 60 dBA sound level is considered acceptable to the MECP and PIED and is within the discretionary range without requiring any noise mitigation measures.

3.1.8.2 VENTILATION REQUIREMENTS

The predicted sound level at the plane of window is in the range of 51 - 75 dBA during the daytime and 47 to 67 dBA during the nighttime. Therefore, as per the MECP's requirements, alternative means of ventilation to open windows is required; A central air conditioning system is provided to the building and mechanical design drawing is included in **Appendix A**.

3.1.8.3 BUILDING REQUIREMENTS

Based on the predicted sound level at the plane of window the sound exceeds 60 dBA during the daytime and 55 dBA during the nighttime. Therefore, the upgraded window glazing and façade constructions exceeding the minimum requirements of Ontario Building Code (OBC) are required to meet indoor sound level requirements as outlined in **Table 3-4**.

Exterior wall: Exterior wall can be constructed with a variety or material providing an STC-45 or more. The exterior façade can be brick veneer, masonry, spandrel glass or metal panels; the selected exterior façade for occupied spaces are provided below:

E01 - EXTERIOR STEEL STUD ALUMINIUM PARTITION

- Pre-Painted Alum. Panel On
- Thermally Broken Furring
- Min 25mm Air Space
- 100mm (Min) Mineral Wool Insulation
- Air Barrier
- 15mm Exterior Sheathing

- Steel Stud Wall W/
- 50mm Spray Foam Insulation (Vap. Bar.)
- 16mm Gyp. Bd.
- Paint Finish

E01a - EXTERIOR STEEL STUD ALUMINIUM PARTITION

- Pre-Painted Alum. Panel On
- Thermally Broken Furring
- Min 25mm Air Space
- 100mm (Min) Mineral Wool Insulation
- Air Barrier
- Concrete Shear Wall

E02 - EXTERIOR MASONRY PARTITION

- Masonry Veneer
- Min 25mm Air Space
- 100mm (Min) Mineral Wool Insulation
- Masonry Block Wall

E02a - EXTERIOR MASONRY PARTITION

- Masonry Veneer
- Min 25mm Air Space
- 100mm (Min) Mineral Wool Insulation
- Masonry Block Wall

E03 - EXTERIOR ALUMINIUM CURTAIN WALL

- Thermally Broken Aluminum Curtain Wall
- 25mm Igu Tinted Glass, Solarban60, Argon Filled Thermally Broken Spacer
- Spandrel Glass W/100mm Mineral Wool Insulation W/ Stl. Stud & Gyp. Bd Back-Up Wall

<u>Window assembly</u> - It was confirmed that the building will include double glazed window assembly. The selected window includes 6mm Solarban 60 with 12.7mm air space and 6mm clear window glazing assembly providing a STC 38 or better. Typical window assemblies may include small operable portion within the window assembly. A good weather seal should be included for this operable portion to minimize the noise flanking.

With the wall assemblies providing STC-45 or better and window assemblies providing STC-38 (Sealed) or better, the indoor sound level of 40 dB or less is achieved.

3.2 VIBRATION IMPACTS

3.2.1 VIBRATION GUIDELINES

There are no guideline limits for vibration from the MECP for Railway vibration in land use planning. The Federation of Canadian Municipalities and The Railway Association of Canada (FCM/RAC) developed a document entitled "Guidelines for New Development in Proximity to Railway Operations" ("FCM/RAC Proximity Guidelines"), dated May 2013. This document provides guidance with respect to issues arising from Railway vibration for new sensitive developments near Rail corridors. This document also includes procedures for vibration measurements, such as selection of measurement locations, number of train pass-by events, equipment capabilities, and a general vibration zone of influence (ZOI) from Railway operations. The FCM/RAC Proximity Guidelines discuss a 75 m ZOI from the Rail right of way.

The FCM/RAC guideline require measurements of ground-borne vibration when residential developments or similar developments are to be located within 75 metres of a principal mainline such as the CN LRT line to the north of the site. There are no requirements noted for institutional buildings.

FCM/RAC guidelines requires that residential developments or similar developments to be assessed as follows:

- Ground-borne vibration transmission to be evaluated through site testing.
- Proposed developments within 75 metres of the rights-of-way shall be evaluated with a limit of 0.14 mm (vibration velocity in RMS) between 4 Hz and 200 Hz.
- If in excess of the limit were measured, isolation measures shall be investigated to ensure living areas do not exceed 0.14 mm/sec RMS.

The limits for commercial/institutional buildings are provided in International Organization for Standardization's (ISO's) publication ISO-2361-2 "Guideline for whole body vibration is buildings" is 0.4 mm/s (RMS). Since the University of Ottawa's FHSB is considered a sensitive building and the building is less than 50 meters away from the nearest right of way the assessment considered the same criteria considered for residential development.

3.2.2 VIBRATION ASSESSMENT SUMMARY

Vibration measurements completed and reported by RWDI Inc., in the University of Ottawa, Volume 3, Guidelines, Lists, Reference, Reports document were reviewed. The vibration measurements were completed on June 4th, 2020 by RWDI. The measurements were taken along the foundation at the proposed development site, at a location closest to the LRT line. RWDI reported completing the ground-borne vibration measurements using a LMS SCADAS Data acquisition system equipped with triaxial sensors. The measured vibration levels are provided in **Table 3-9**.

Table 3-9 Measured Vibration Levels (RMS)

DESCRIPTION	RMS VIBRATION (OMM/S)
LRT - Northbound	0.076
LRT - Southbound	0.082

The measured vibration is less than the limit considered (i.e. 0.14 mm/s) and therefore vibration is not considered further. However, it should be noted that the proposed build is a concreate structure with spread concrete column footings. As noted in the Federal Transit Administration (FTA) guidelines, large masonry buildings with spread footings have a low response to ground vibration. Therefore, the concrete structure will minimize any residual vibration associated with the presence of the transit system.

3.3 STATIONARY NOISE IMPACTS

Stationary source is defined in MECP publication NPC-300 as source of sound or combination of sources of sound that are included and normally operated within the property lines of a facility. Accordingly, noise from the nearby Block A and B as well as noise from electro-mechanical unites within the proposed development are is considered as stationary sources and therefore MECP's guidelines (Section B of the NPC-300) applies to those noise sources

The roof top units on Block A and Block B is generally HVAC and exhaust fans. A site visit was not conducted but noise source data for Block A and B associated sources were taken from available information.

The noise sources associated with the proposed development are expected to be rooftop HVAC units and other similar mechanical units (refer **Appendix A**). These units have potential to cause noise impact, this section qualitatively assess noise impact from these units on:

- 1. the surrounding environment; and
- 2. itself

These aspects are discussed in this section.

The drawings indicate that there will be a mechanical penthouse provided to this development. The majority of other mechanical units such as the chiller, boiler, elevator machine, water softener and pumps are located inside mechanical rooms. Cooling load is higher during the daytime than during the nighttime and therefore full load conditions during the daytime and lower cooling load during the largely unoccupied nighttime were considered consistent with assessment approaches

3.3.1 NOISE GUIDELINES AND ASSESSMENT CRITERIA

For stationary sources, the MECP Publication NPC-300 provides criteria based on one-hour equivalent sound level. In order to comply with the noise impact from stationary sources, the predicted sound level must comply with the noise guidelines stipulated in the MECP publication, NPC-300.

NPC-300 provides sound level limits for development (or receptors) based on the acoustical environment in which the development is located. NPC-300 categorizes the acoustical environment into four classes: Class 1 (urban), Class 2 (suburban), Class 3 (rural), or Class 4 (special cases). This classification depends on the local land use and the existing ambient sound environment. **Table 3-10** summarizes the MECP exclusionary limits for Class 1, 2, 3 and 4 areas.

	CLA	SS 1	CLA	SS 2	CLA	SS 3	CLA	SS 4
PERIOD	PLANE OF WINDOW ²	OUTDOOR POR ¹						
Daytime (07:00 – 19:00)	50	50	50	50	45	45	60	55
Evening (19:00 – 23:00)	50	50	50	45	40	40	60	55
Night-time (23:00 – 07:00)	45	N/A ³	45	N/A ³	40	N/A ³	55	N/A ³

Table 3-10 MECP's Exclusion Limits in dBA

Notes:

1 PoR means point of reception; representing a point in a receptor location as defined by MECP.

2 Plane of window means a point in space corresponding with the location of the centre of a window of a noise sensitive space. The noise effects assessment excludes the effect of sound reflection from the plane of the window on which it is located. In general, the plane of a window is a point used for prediction (including extrapolation), rather than measurement, of sound levels (MOE 2013).

Since the area is considered a Class 1 acoustical environment, the sound level limit corresponding to Class 1 is considered in the assessment (i.e. 50 dBA during the daytime and 45 dBA during the nighttime).

3.3.2 SOURCE DATA

Based on the available information the following sources were identified in **Table 3-11** and the source locations are shown in **Figure 10**.

Table 3-11 Stationary Source Sound Data

SOURCE ID ¹	DESCRIPTION	POWER LEVEL [DBA REF 10-12 W]	DAY	NIGHT	REMARKS
EF1 to EF 18	Exhaust Fans	80	Yes	Yes	
AHU01 to AHU 08	Air Handling Units	87	Yes	Yes	Inside mechanical rooms
GEN	New Generator	93	Yes	Yes	With silencer
LEF-1	LEF-1	76	Yes	Yes	
LEF-2	LEF-2	81	Yes	Yes	
KEF-1	KEF-1	81	Yes	Yes	
LEF-2	LEF-2	81	Yes	Yes	
FLF1	Food lab Fume Hood	81	Yes	Yes	
FLF2	Wet Lab Fume Hood	81	Yes	Yes	
GEN1	Existing Generator	105	Yes	Yes	With silencer
Vent	Vent	81	Yes	Yes	Vent mechanical room
Int	Intake	71	Yes	Yes	Air intake opening

3.3.3 RESULTS AND DISCUSSION

The following table compares the predicted sound level to the criteria. The sample calculations are included in **Appendix C.**

Table 3-12 Predicted sound level

			SOUND LEVEL DAY/NIGHT		
PREDICTION		RECEIVER	[DBA REF 10-6	LIMIT DAY/NIGHT	MEETING THE
LOCATION1	DESCRIPTION	HEIGHT (M)	PA]	[DBA REF 10-6 PA]	LIMIT?
POR01	South Façade	22.2	30 / 27	50 / 45	Yes
POR02	South Façade	22.2	28 / 27	50 / 45	Yes
POR03	West Façade	22.2	44 / 44	50 / 45	Yes
POR04	West Façade	9.6	46 / 45	50 / 45	Yes
POR05	West Façade	22.2	47 / 45	50 / 45	Yes
POR06	North Façade	22.2	37 / 36	50 / 45	Yes
POR07	East Facade	22.2	47 / 45	50 / 45	Yes
POR08	East Facade	22.2	47 / 45	50 / 45	Yes
POR09	East Facade	22.2	46 / 44	50 / 45	Yes
POR10	East Facade	7.5	46 / 45	50 / 45	Yes
POR11	East Facade	7.5	45 / 44	50 / 45	Yes

Notes:

1 Refer to Figure 3 for receptor locations. It should be noted that outdoor locations (e.g. terraces, academic quad) associated with a noise sensitive institutional purpose is not considered to be a point of reception as per NPC-300 and Ottawa Noise Guideline.

The receptor locations at the proposed development meets the required the limits with the estimated day and nighttime Leq (1 hour).

3.3.4 RECOMMENDATIONS

The sound levels associated with stationary noise sources from the nearby buildings as well as from the development itself meet the day and nighttime limits. The following are shown in the design drawings and considered part of the noise mitigations.

- 1. Generator will be inside the mechanical room and includes muffler for engine exhaust and intake and discharge silencers.
- 2. Air compressor, vacuum pump, Humidifiers 1 to 4 (DOAS-1, DOAS-2 etc.), Chillers 1 to 4, Chilled water pumps will be located indoors.
- 3. Cooling tower to include a screen of similar or greater height than the cooling tower

4 CONCLUSIONS AND CLOSURE

The predicted sound levels from surface transportation and stationary sources were assessed separately per MECP publication NPC-300 requirements. Each noise source type was assessed at the points of reception and their compliance with the NPC-300 requirements is evaluated. Noise from transportation sources are discussed in Section 3.1, vibration assessment is discussed in Section 3.2, and Stationary sources are discussed in Section 3.3. The development does not have dominant effect on its surrounding.

4.1 SUMMARY OF RECOMMENDATIONS

The following recommendations are offered:

- 1. The development will require central air conditioning system as an alternate means of open window and the development includes central air condition system
- 2. The preliminary acoustical performance requirements for exterior façade elements (i.e. exterior walls, and windows) for the development are discussed in Section 3.1
 - a. Exterior wall: Exterior wall providing an STC-45 or more will be required;
 - b. Exterior window: Exterior windows glazing into sensitives spaces providing a STC 38 or better
- 3. Noise control for stationary sources are discussed in Section 3.3
 - a. Generator will be inside the mechanical room and includes muffler for engine exhaust and intake and discharge silencers.
 - b. Air compressor, vacuum pump, Humidifiers 1 to 4 (DOAS-1, DOAS-2 etc.), Chillers 1 to 4, Chilled water pumps will be located indoors.
 - c. All vents to mechanical rooms include louvers

4.2 CONCLUSIONS AND CLOSURE

Based on the content of this impact study it is concluded that developing the proposed development is in compliance with the City's and MECP's noise criteria.

This report has been prepared to support the site plan approval application being prepared. Once the design is finalized and details becomes available it will be reviewed further by the design team.

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25 EXISTING BUS STOP 26 EXISTING NORTH BOUI		ORM	
27 EXISTING STAIR TO LR 28 TERRACED SEATING 29 RAMP WITH TACTILE M		ACE	
INDICATORS 30 NEW TEMPORARY LAN 31 EXISTING TOPE COOL			CLIENT:
<u>SITE AND</u>	BUILDIN	<u>IG</u>	u Ottawa
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AREA OF LOT		69,319m ²	CLIENT REF. #: BT20-18477 PROJECT:
OT COVERAGE		13,551m²	University of Ottawa - Faculty of Health
			Sciences Building
			200 LEES AVENUE OTTAWA, ON
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PARKING REMOVED	PACES	125 SPACES	
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A-2 MECHANICAL DRAWINGS







A-3 ARCHITECTURAL DRAWINGS



APPENDIX

B TRAFFIC DATA





Appendix B: Table of Traffic and Road Parameters To Be Used For Sound Level Predictions

Table B1 Traffic And Road Parameters To Be Used For Sound Level Predictions												
Row Width (m)	Implied Roadway Class	AADT Vehicles/Day	Posted Speed Km/Hr	Day/Night Split %	Medium Trucks %	Heavy Trucks % ¹						
NA ²	Freeway, Queensway, Highway	18,333 per lane	100	92/8	7	5						
37.5-44.5	6-Lane Urban Arterial-Divided (6 UAD)	50,000	50-80	92/8	7	5						
34-37.5	4-Lane Urban Arterial-Divided (4-UAD)	35,000	50-80	92/8	7	5						
23-34	4-Lane Urban Arterial-Undivided (4-UAU)	30,000	50-80	92/8	7	5						
23-34	4-Lane Major Collector (4-UMCU)	24,000	40-60	92/8	7	5						
30-35.5	2-Lane Rural Arterial (2-RAU)	15,000	50-80	92/8	7	5						
20-30	2-Lane Urban Arterial (2-UAU)	15,000	50-80	92/8	7	5						
20-30	2-Lane Major Collector (2-UMCU)	12,000	40-60	92/8	7	5						
30-35.5	2-Lane Outer Rural Arterial (near the extremities of the City) (2-RAU)	10,000	50-80	92/8	7	5						
20-30	2-Lane Urban Collector (2-UCU)	8,000	40-50	92/8	7	5						

¹ The MOE Vehicle Classification definitions should be used to estimate automobiles, medium trucks and heavy trucks.

 $^{2}\,$ The number of lanes is determined by the future mature state of the roadway.

Environmental Noise Control Guidelines Part 4: Technical Requirements For Environmental Noise Control Studies And Implementation

Schedules & Maps

The next service change is on Sunday, June 20.

Schedule times are based on typical driving conditions and may vary. Please arrive at your stop a few minutes early to allow for any fluctuations in schedule.

1 Tunney's Pasture

Thu, Jun 17

	CYRVILLE O- TRAIN WEST / OUEST	ST-LAURENT O- TRAIN WEST / OUEST	TREMBLAY O- TRAIN WEST / OUEST	HURDMAN O- TRAIN WEST / OUEST	LEES O-TRAIN WEST / OUEST	UOTTAWA O- TRAIN WEST / OUEST	RIDEAU O-TRAIN WEST / OUEST	PARLIAMENT / PARLEMENT O- TRAIN WEST / OUEST	LYON O-TRAIN WEST / OUEST	PIMISI O-TRAIN WEST / OUEST	BAYVIEW O- TRAIN WEST / OUEST	TUNNEY'S PASTURE C TRAIN
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BLAIR O-TRAIN WEST / OUEST	CYRVILLE O- TRAIN WEST / OUEST	ST-LAURENT O- TRAIN WEST / OUEST	TREMBLAY O- TRAIN WEST / OUEST	HURDMAN O- TRAIN WEST / OUEST	LEES O-TRAIN WEST / OUEST	UOTTAWA O- TRAIN WEST / OUEST	RIDEAU O-TRAIN WEST / OUEST	PARLIAMENT / PARLEMENT O- TRAIN WEST / OUEST	LYON O-TRAIN WEST / OUEST	PIMISI O-TRAIN WEST / OUEST	BAYVIEW O- TRAIN WEST / OUEST	TUNNEY'S PASTURE O- TRAIN
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C SAMPLE CALCULATIONS



C-1 SAMPLE - STAMSON

Table C-1: Stamson Parameters and Results

ID	Description	Stamson File Name	Road/Rail Segment	Road/Rail An A1	l Viewable gle A2	Source - Receiver Distance (m)	Ground Type (Hard/Soft)	Topograp hy Type	Wood Depth	No. Rows of Houses	Density of House (%)	Receiever I Day	Height (m) Night	Total Road/Rail Leq (dBA) D	Combined Leq (dBA) ay	Total Road/Rail Leq (dBA) Nig	Combined Leq (dBA) ght	Ventilation Requirements	Building Component Requirements
POR01	Southeast corner on South Facade (5th Level)	UOA.TE	LRT	-90	25	132	Hard	1	0	0	20%	22.2	22.2	51	51	47	47	None	OBC
POR02	Southwest corner on South Façade (5th Level)	UOB.TE	LRT	-90	0	38	Hard	1	0	0	20%	22.2	22.2	55	55	51	51	Forced Air	OBC
			417EB1	-80	-33	202	Hard	1	0	0	20%	22.2	22.2						
			417EB2	-80	-33	206	Hard	1	0	0	20%	22.2	22.2						
	Southwast corner on Wast Escado (Eth Loval)		417WB1	-80	-33	211	Hard	1	0	0	20%	22.2	22.2	68	60	61	61	Central Air	Designed /
F OLUJ	Southwest corner on west Façade (Stil Level)	UUCC.TE	417WB2	-80	-33	215	Hard	1	0	0	20%	22.2	22.2		09		01	Conditioning	Selected
			LEE	-35	20	130	Hard	1	0	0	20%	22.2	22.2						
			LRT	-90	65	36	Hard	1	0	0	20%	22.2	22.2	58		54			
			417EB1	-82	-27	197	Hard	1	0	0	20%	9.6	9.6						
			417EB2	-82	-27	201	Hard	1	0	0	20%	9.6	9.6						
POR04	Southwest corner on West Facade (2nd Level)	UOCD.TE	417WB1	-82	-27	206	Hard	1	0	0	20%	9.6	9.6	69	70	62	63	Central Air	Designed /
			417WB2	-82	-27	210	Hard	1	0	0	20%	9.6	9.6					Conditioning	Selected
			LEE	-35	20	120	Hard	1	0	0	20%	9.6	9.6						
			LRT	-90	65	31	Hard	1	0	0	20%	9.6	9.6	59		54			
			417EB1	-80	-20	135	Hard	1	0	0	20%	22.2	22.2						
			417EB2	-80	-20	139	Hard	1	0	0	20%	22.2	22.2	74		6.4		Control Air	Decision ed (
POR05	Northwest corner on West Façade (5th Level)	UOCE.TE	41/WB1	-80	-20	144	Hard	1	0	0	20%	22.2	22.2	/1	71	64	64	Central Air	Designed /
			41/WB2	-80	-20	148	Hard	1	0	0	20%	22.2	22.2					Conditioning	Selected
				-90	25	60	Hard	1	0	0	20%	22.2	22.2	F 7		E 2			
				-90	24	121	Hard	1	0	0	20%	22.2	22.2	57		55			
			41/ED1 417ED2	-80	24	131	Hard	1	0	0	20%	22.2	22.2						
			417EBZ	-80	24	135	Hard	1	0	0	20%	22.2	22.2	74		66		Central Air	Designed /
POR06	Northwest corner on North Façade (5th Level)	UOCF.TE	417WB1	-80	24	140	Hard	1	0	0	20%	22.2	22.2	74	74	00	66	Conditioning	Selected
			1 FF	-90	50	58	Hard	1	0	0	20%	22.2	22.2					conditioning	Scietted
			IRT	0	55	48	Hard	1	0	0	20%	22.2	22.2	52		48			
			417EB1	-40	90	126	Hard	1	0	0	20%	22.2	22.2	52		10			
			417EB2	-40	90	130	Hard	1	0	0	20%	22.2	22.2						
POR07	Northeast corner on East Façade (5th Level)	UOCL.TE	417WB1	-40	90	135	Hard	1	0	0	20%	22.2	22.2	75	75	67	67	Central Air	Designed /
			417WB2	-40	90	139	Hard	1	0	0	20%	22.2	22.2					Conditioning	Selected
			LEE	20	42	77	Hard	1	0	0	20%	22.2	22.2						
			417EB1	-40	90	150	Hard	1	0	0	20%	22.2	22.2						
			417EB2	-40	90	154	Hard	1	0	0	20%	22.2	22.2					Control Air	Designed /
POR08	East Façade (5th Level)	UOCM.TE	417WB1	-40	90	159	Hard	1	0	0	20%	22.2	22.2	74	74	66	66	Conditioning	Selected
			417WB2	-40	90	163	Hard	1	0	0	20%	22.2	22.2					conditioning	Selected
			LEE	20	40	100	Hard	1	0	0	20%	22.2	22.2						
			417EB1	-55	70	172	Hard	1	0	0	20%	22.2	22.2						
			417EB2	-55	70	176	Hard	1	0	0	20%	22.2	22.2					Central Air	Designed /
POR09	North Façade of east wing (5th Level)	UOCN.TE	417WB1	-55	70	181	Hard	1	0	0	20%	22.2	22.2	73	73	65	65	Conditioning	Selected
			417WB2	-55	70	185	Hard	1	0	0	20%	22.2	22.2					0	
			LEE	10	35	150	Hard	1	0	0	20%	22.2	22.2						
			417EB1	-75	75	154	Hard	1	0	0	20%	22.2	22.2						
00040	Northeast corner on North Façade of east wing (5th		417EB2	-75	75	158	Hard	1	0	0	20%	22.2	22.2	74	74	67	67	Central Air	Designed /
PORTU	Level)	UOCO.TE	41/WB1	-75	75	163	Hard	1	0	0	20%	22.2	22.2	74	74	67	67	Conditioning	Selected
			41/WB2	-/5	/5	16/	Hard	1	0	0	20%	22.2	22.2						
				-15	25	190	Hard	1	0		20%	22.2	22.2						
			41/EB1 417ED2	-15	90	160	Hard	1	0		20%	22.2	22.2					Central Air	Designed /
POR11	East Façade on east wing (5th level)	UOCP.TE	417\A/D1	-15	90	17/	Hard	1	0	0	20%	22.2	22.2	72	72	65	65	Conditioning	Selected
			417\N/R2	-15	90	179	Hard	1	0	0	20%	22.2	22.2					conditioning	Jeletteu
			71/002	10	50	1,0	naru	1	0	, U	2070	22.2	22.2						



STAMSON 5.0 NORMAL REPORT Date: 18-06-2021 22:37:40 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT Filename: UOA.te Time Period: Day/Night 16/8 hours Description: Location A RT/Custom data, segment # 1: LRT (day/night) _____ 1 - CLRV: Traffic volume : 234/44 veh/TimePeriod Speed : 50 km/h Data for Segment # 1: LRT (day/night) ------: -90.00 deg 25.00 deg Angle1 Angle2 : 0 (No woods.) Wood depth : 0 / 0 2 No of house rows Surface (Reflective ground surface) : Receiver source distance : 132.00 / 132.00 m Receiver height : 22.20 / 22.20 m : 1 (Flat/gentle slope; no barrier) Topography : 0.00 Reference angle Results segment # 1: LRT (day) _____ Source height = 0.50 mRT/Custom (0.00 + 50.93 + 0.00) = 50.93 dBAAngle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq -90 25 0.00 62.32 -9.44 -1.95 0.00 0.00 0.00 50.93 _____ Segment Leq : 50.93 dBA Total Leg All Segments: 50.93 dBA Results segment # 1: LRT (night) -----Source height = 0.50 mRT/Custom (0.00 + 46.68 + 0.00) = 46.68 dBAAngle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq _____ 25 0.00 58.07 -9.44 -1.95 0.00 0.00 0.00 46.68 -90 _____ Segment Leq : 46.68 dBA Total Leg All Segments: 46.68 dBA TOTAL Leg FROM ALL SOURCES (DAY): 50.93 (NIGHT): 46.68

Table C-1: Stamson Parameters and Results

ID	Description	Stamson File Name	Road/Rail Segment	Road/Rail An	l Viewable Igle	Source - Receiver Distance	Ground Type	Topograp hy Type	Wood Depth	No. Rows of Houses	Density of House	Receiever	Height (m)	Total Road/Rail Leq (dBA)	Combined Leq (dBA)	Total Road/Rail Leq (dBA)	Combined Leq (dBA)	Ventilation Requirements	Building Component Requirements
				A1	A2	(m)	(Hard/Soft)				(%)	Day	Night	D	ay	Ni	ght		
OLA1	Outdoor Amenity Area - River Terrace (southwest corner)	OLA1.TE	LRT	-90	30	40	Hard	1	0	0	20%	1.5		56	56			-	
			417EB1	0	6	166	Hard	1	0	0	20%	1.5							
	Outdoor Amenity Area - Academic Quad (East Side		417EB2	0	6	170	Hard	1	0	0	20%	1.5		60	60				
OLAZ	Courtyard Area)	ULAZ.TL	417WB1	0	6	175	Hard	1	0	0	20%	1.5		00					
			417WB2	0	6	179	Hard	1	0	0	20%	1.5							
			417EB1	-85	-80	115	Hard	1	0	0	20%	1.5							
	Outdoor Amenity Area - Indigenouse Pavilion & Firepit		417EB2	-85	-80	119	Hard	1	0	0	20%	1.5							
OLA3	Gathering Circle (East side of proposed building, near	OLA3.TE	417WB1	-85	-80	124	Hard	1	0	0	20%	1.5		60	60				
	existing Block A Building)		417WB2	-85	-80	128	Hard	1	0	0	20%	1.5							
			LEE	-2	3	103	Hard	1	0	0	20%	1.5							





C-2 SAMPLE – CADNA/A

Configuration	
Configuration	
Parameter	Value
General	
Country	(user defined)
Max. Error (dB)	0
Max. Search Radius (#(Unit,LEN))	2000
Min. Dist Src to Rcvr	0
Partition	
Raster Factor	0.5
Max. Length of Section (#(Unit,LEN))	1000
Min. Length of Section (#(Unit,LEN))	1
Min. Length of Section (%)	0
Proj. Line Sources	On
Proj. Area Sources	On
Ref. Time	
Reference Time Day (min)	960
Reference Time Night (min)	480
Daytime Penalty (dB)	0
Recr. Time Penalty (dB)	6
Night-time Penalty (dB)	10
DTM	
Standard Height (m)	0
Model of Terrain	Triangulation
Reflection	
max. Order of Reflection	1
Search Radius Src	100
Search Radius Rcvr	100
Max. Distance Source - Rcvr	1000.00 1000.00
Min. Distance Rvcr - Reflector	1.00 1.00
Min. Distance Source - Reflector	0.1
Industrial (ISO 9613)	
Lateral Diffraction	some Obj
Obst. within Area Src do not shield	On
Screening	Excl. Ground Att. over Barrier
	Dz with limit (20/25)
Barrier Coefficients C1,2,3	3.0 20.0 0.0
Temperature (#(Unit,TEMP))	10
rel. Humidity (%)	70
Ground Absorption G	0.7
Wind Speed for Dir. (#(Unit,SPEED))	3
Roads (TNM)	
Railways (Schall 03 (1990))	
Strictly acc. to Schall 03 / Schall-Transrapid	
Aircraft (???)	
Strictly acc. to AzB	

Receiver Name: POR02 ID: POR02

X: 447680.85 m

Y: 5029295.73 m

Z: 22.20 m

				Ve	ert. Ar	ea Soi	urce, IS	O 961	13, Name	e: "Ve	nt", I	D: "Ve	ent"		-					
Nr.	Х	Y	Z	Refl.	DEN	Freq.	Lw	l/a	Optime	K0	Di	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
15	447670.97	5029320.00	21.50	0	DEN	Α	70.8	0.5	0.0	0.0	0.0	39.4	0.4	-0.9	0.0	0.0	19.0	0.0	0.0	13.4
17	447671.86	5029317.19	21.50	0	DEN	Α	70.8	6.8	0.0	0.0	0.0	38.3	0.4	-0.9	0.0	0.0	19.0	0.0	0.0	20.8

			Po	oint So	ource,	ISO 9	613, N	ame:	'Wet Lat	o Fum	ne Ho	od", Il	D: "Flf	-2"						
Nr.	Х	Y	Z	Refl.	DEN	Freq.	Lw	l/a	Optime	K0	Di	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
21	447679.04	5029329.30	28.20	0	DEN	A	80.6	0.0	0.0	0.0	0.0	41.7	0.2	-0.9	0.0	0.0	18.4	0.0	0.0	21.3

				F	Point S	Source	, ISO 9	613, N	lame: "C	GEN1	", ID:	"GEN	1"							
Nr.	Nr. X Y Z Refl. DEN Freq. Lw I/a Optime K0 Di Adiv Aatm Agr Afol Ahous Abar Cmet RL Lr																			
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
30	447865.45	5029418.59	2.00	0	D	A	105.3	0.0	-3.0	0.0	0.0	58.0	1.3	-0.3	0.0	0.0	24.6	0.0	0.0	18.8

			Po	oint So	ource,	ISO 9	613, Na	ame: '	'Food lat	o Fum	ne Ho	od", I[D: "FLF	-1"						
Nr.	Х	Y	Z	Refl.	DEN	Freq.	Lw	l/a	Optime	K0	Di	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
50	447668.89	5029354.67	28.20	0	DEN	Α	80.6	0.0	0.0	0.0	0.0	46.6	0.3	-0.9	0.0	0.0	18.0	0.0	0.0	16.5

				Poir	t Source	e, ISO 9	613, N	Name: "L	.EF-2	", ID:	"LEF-	·2"							
Nr.	Ir. X Y Z Refl. DEN Freq. Lw I/a Optime K0 Di Adiv Aatm Agr Afol Ahous Abar Cmet RL Lr																		
	(m)	(m)	(m)		(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
53	447662.35	5029366.63	28.20	0 DE	N A	80.6	0.0	0.0	0.0	0.0	48.3	0.4	-0.9	0.0	0.0	17.7	0.0	0.0	15.1

				Р	oint S	Source	, ISO 9	613, N	lame: "K	EF-1	", ID:	"KEF	-1"							
Nr.	Х	Y	Z	Refl.	DEN	Freq.	Lw	l/a	Optime	K0	Di	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
65	447659.28	5029372.37	28.20	0	DEN	A	80.6	0.0	0.0	0.0	0.0	49.0	0.4	-0.9	0.0	0.0	17.6	0.0	0.0	14.5

				Po	oint So	ource,	ISO 96	13, N	ame: "Al	HU08	", ID:	"AHU	08"							
Nr.	Jr. X Y Z Refl. DEN Freq. Lw I/a Optime K0 Di Adiv Aatm Agr Afol Ahous Abar Cmet RL Lr																			
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
67	447809.13	5029372.88	10.50	0	D	A	87.2	0.0	0.0	0.0	0.0	54.5	1.4	-0.9	0.0	0.0	24.5	0.0	0.0	7.7

				Po	oint So	ource,	ISO 96	13, N	ame: "Al	HU07	", ID:	"AHU	07''							
Nr.	Ir. X Y Z Refl. DEN Freq. Lw I/a Optime K0 Di Adiv Aatm Agr Afol Ahous Abar Cmet RL Lr																			
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
70	447815.28	5029375.63	10.50	0	D	A	87.2	0.0	0.0	0.0	0.0	54.9	1.5	-0.9	0.0	0.0	24.5	0.0	0.0	7.3

				Po	oint So	ource,	ISO 96	13, N	ame: "Al	HU01	", ID:	"AHU	01"							
Nr.	Nr. X Y Z Refl. DEN Freq. Lw 1/a Optime K0 Di Adiv Aatm Agr Afol Ahous Abar Cmet RL Lr																			
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
73	447826.51	5029361.65	10.50	0	D	A	87.2	0.0	0.0	0.0	0.0	55.1	1.5	-0.9	0.0	0.0	24.3	0.0	0.0	7.3

				P	oint So	ource,	ISO 96	13, N	ame: "Al	HU02	", ID:	"AHU	02''							
Nr.	Nr. X Y Z Refl. DEN Freq. Lw I/a Optime K0 Di Adiv Aatm Agr Afol Ahous Abar Cmet RL Lr																			
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
75	447826.51	5029372.03	10.50	0	D	A	87.2	0.0	0.0	0.0	0.0	55.3	1.5	-0.9	0.0	0.0	24.4	0.0	0.0	6.9

				Po	oint S	ource	, ISO 9	613, 1	Name: "L	EF-2	", ID:	"LEF-	2"							
Nr.	Nr. X Y Z Refl. DEN Freq. Lw I/a Optime K0 Di Adiv Aatm Agr Afol Ahous Abar Cmet RL Lr																			
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
86	447653.67	5029357.55	7.40	0	D	Α	79.6	0.0	0.0	0.0	0.0	47.8	0.4	-0.9	0.0	0.0	16.3	0.0	0.0	16.1

				Po	oint So	ource,	ISO 96	13, N	ame: "Al	HU03	", ID:	"AHU	03"							
Nr.	Х	Y	Z	Refl.	DEN	Freq.	Lw	l/a	Optime	K0	Di	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
125	447829.69	5029380.93	10.50	0	D	A	87.2	0.0	0.0	0.0	0.0	55.7	1.6	-0.9	0.0	0.0	24.4	0.0	0.0	6.5

				P	oint So	ource,	ISO 96	13, N	ame: "Al	HU06	", ID:	"AHU	06''							
Nr.	Nr. X Y Z Refl. DEN Freq. Lw I/a Optime K0 Di Adiv Aatm Agr Afol Ahous Abar Cmet RL Lr																			
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
128	447829.26	5029396.40	10.50	0	D	A	87.2	0.0	0.0	0.0	0.0	56.1	1.6	-0.9	0.0	0.0	24.7	0.0	0.0	5.7

				Po	oint So	ource,	ISO 96	13, N	ame: "Al	HU05	", ID:	"AHU	05"							
Nr.	Ir. X Y Z Refl. DEN Freq. Lw I/a Optime K0 Di Adiv Aatm Agr Afol Ahous Abar Cmet RL Lr																			
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
131	447835.41	5029406.36	10.50	0	D	A	87.2	0.0	0.0	0.0	0.0	56.6	1.7	-0.9	0.0	0.0	24.7	0.0	0.0	5.1

				Po	oint Se	ource,	ISO 96	13, N	ame: "Al	HU04	", ID:	"AHU	04"							
Nr.	r. X Y Z Refl. DEN Freq. Lw I/a Optime K0 Di Adiv Aatm Agr Afol Ahous Abar Cmet RL Lr																			
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
144	447842.61	5029398.52	10.50	0	D	A	87.2	0.0	0.0	0.0	0.0	56.7	1.7	-0.9	0.0	0.0	24.7	0.0	0.0	5.0

			v	ert. A	rea So	ource,	ISO 96	13, N	ame: "Ge	en Di	sch",	ID: "G	en_Di	s"						
Nr.	Х	Y	Z	Refl.	DEN	Freq.	Lw	l/a	Optime	K0	Di	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
148	447693.96	5029368.67	4.50	0	D	A	75.5	5.9	0.0	0.0	0.0	48.6	0.4	-0.6	0.0	0.0	24.8	0.0	0.0	8.1
163	447693.63	5029369.41	4.50	1	D	A	75.5	2.3	0.0	0.0	0.0	49.5	0.4	-0.6	0.0	0.0	24.8	0.0	2.0	1.5

					Point	Sourc	e, ISO	9613,	Name: "	Ex14	", ID:	"Ex14	t"							
Nr.	Х	Y	Z	Refl.	DEN	Freq.	Lw	l/a	Optime	K0	Di	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
167	447765.70	5029409.75	11.00	0	DEN	A	79.6	0.0	0.0	0.0	0.0	54.1	0.7	-0.9	0.0	0.0	23.9	0.0	0.0	1.9

					Point	Sourc	e, ISO	9613,	Name: "	Ex10	", ID:	"Ex10)''							
Nr.	X	Y	Z	Refl.	DEN	Freq.	Lw	l/a	Optime	K0	Di	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
170	447808.50	5029361.23	10.50	0	DEN	A	79.6	0.0	0.0	0.0	0.0	54.2	0.7	-0.9	0.0	0.0	23.7	0.0	0.0	2.0

					Point	Source	e, ISO	9613,	Name: "	Ex12	", ID:	"Ex12								
Nr.	Х	Y	Z	Refl.	DEN	Freq.	Lw	l/a	Optime	K0	Di	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
172	447804.90	5029379.66	11.00	0	DEN	Α	79.6	0.0	0.0	0.0	0.0	54.5	0.7	-0.9	0.0	0.0	24.1	0.0	0.0	1.2

					Point	Sourc	e, ISO	9613,	Name: "	Ex09	", ID:	"Ex09)''							
Nr.	r. X Y Z Refl. DEN Freq. Lw I/a Optime K0 Di Adiv Aatm Agr Afol Ahous Abar Cmet RL Lr																			
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
204	447821.63	5029350.21	11.00	0	DEN	A	79.6	0.0	0.0	0.0	0.0	54.6	0.7	-0.9	0.0	0.0	23.4	0.0	0.0	1.8

					Point	Sourc	e, ISO	9613,	Name: "	Ex18	", ID:	"Ex18	3''							
Nr.	Х	Y	Z	Refl.	DEN	Freq.	Lw	l/a	Optime	K0	Di	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
236	447777.99	5029416.53	11.00	0	DEN	A	79.6	0.0	0.0	0.0	0.0	54.8	0.8	-0.9	0.0	0.0	23.9	0.0	0.0	1.1

					Point	Sourc	e, ISO	9613,	Name: "	Ex08	", ID:	"Ex08	3"							
Nr.	Yr. X Y Z Refl. DEN Freq. Lw I/a Optime K0 Di Adiv Aatm Agr Afol Ahous Abar Cmet RL Lr																			
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
239	447836.68	5029334.95	11.00	0	DEN	A	79.6	0.0	0.0	0.0	0.0	55.1	0.8	-0.9	0.0	0.0	21.9	0.0	0.0	2.7

				l	Point	Sourc	e, ISO	9613,	Name: "	Ex07	", ID:	"Ex07	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,							
Nr.	Х	Y	Z	Refl.	DEN	Freq.	Lw	l/a	Optime	K0	Di	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
242	447843.03	5029338.34	11.00	0	DEN	A	79.6	0.0	0.0	0.0	0.0	55.5	0.8	-0.9	0.0	0.0	22.0	0.0	0.0	2.3

				F	Point	Sourc	e, ISO	9613,	Name: "	Ex17	", ID:	"Ex17	711							
Nr.	Ir. X Y Z Refl. DEN Freq. Lw I/a Optime K0 Di Adiv Aatm Agr Afol Ahous Abar Cmet RL Lr																			
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
245	447798.11	5029417.37	11.00	0	DEN	A	79.6	0.0	0.0	0.0	0.0	55.6	0.8	-0.9	0.0	0.0	23.9	0.0	0.0	0.3

Point Source, ISO 9613, Name: "Ex16", ID: "Ex16"																				
Nr.	Х	Y	Z	Refl.	DEN	Frea.	Lw	l/a	Optime	K0	Di	Adiv	Aatm	Aar	Afol	Ahous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
201	117705 57	5020421 40	11.00	0			70.6		0.0			55.6					23.0			0.2
231	447735.57	5029421.40	11.00	0	DLIN		73.0	0.0	0.0	0.0	0.0	55.0	0.0	-0.3	0.0	0.0	25.5	0.0	0.0	0.2
					Point	Sourc		9613	Name [.] "	Ev15	יחו "	"Ev15								
Nr	V	V	7	Dof		Eroa		1/0	Ontimo		, ישו וח	Adiv	Actm	Aar	Afol	About	Abor	Cmot	Ы	ار
INI.	<u>^</u>	(m)	<u>(m)</u>	Rell.	DEN	rieq.		1/a	JD					Agi (JD)						
007	(11)	(11)	(11)		DEN				UD 0.0											
307	447793.67	5029425.64	11.00	0	DEN	A	79.6	0.0	0.0	0.0	0.0	55.7	0.8	-0.9	0.0	0.0	23.8	0.0	0.0	0.1
					D - !+	<u></u>	. 100	0040	NI	E										
	X	X		D (1	Point	Sourc	e, 150	9613,	Name:	EXTI	, ID:	EXII		•				0		
Nr.	X	Y	Z	Refl.	DEN	Freq.	LW	I/a	Optime	K0	DI	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
309	447821.63	5029395.76	11.00	0	DEN	A	79.6	0.0	0.0	0.0	0.0	55.8	0.8	-0.9	0.0	0.0	24.0	0.0	0.0	-0.0
					<u> </u>		10.0	0040		- 05										
			_		Point	Sourc	e, ISO	9613,	Name:	EXU5	", ID:	EXU5)" • · ·					a (
Nr.	X	Y		Refl.	DEN	Freq.	LW	l/a	Optime	K0	Di	Adiv	Aatm	Agr	Atol	Ahous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
333	447837.52	5029370.34	11.00	0	DEN	A	79.6	0.0	0.0	0.0	0.0	55.8	0.8	-0.9	0.0	0.0	23.3	0.0	0.0	0.6
Point Source ISO 9613 Name: "EVO6" ID: "EVO6"																				
				D C	Point	Sourc	e, ISO	9613,	Name: "	EX06	", ID:	Ex06)" • • •	•			•	A	D .	
Nr.	X	Y	<u> </u>	Refl.	DEN	⊢req.	LW	1/a	Optime	K0	Di	Adiv	Aatm	Agr	Atol	Anous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
336	447839.64	5029366.31	11.00	0	DEN	A	79.6	0.0	0.0	0.0	0.0	55.8	0.8	-0.9	0.0	0.0	23.3	0.0	0.0	0.6
Daint Source, ISO 0642, Name: "Capiling Toward", ID: "OT"																				
				Poi	nt Sou	urce, IS	SO 961	3, Nar	ne: "Coo	oling	ower	", ID:	"CT"					-	_	
Nr.	X	Y	Z	Refl.	DEN	Freq.	Lw	l/a	Optime	K0	Di	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
339	447650.19	5029364.32	6.40	0	D	A	79.8	0.0	-3.0	0.0	0.0	48.7	0.5	-0.8	0.0	0.0	14.8	0.0	0.0	13.6
				_																
					oint S	Source	, ISO 9	613, N	Name: "L	.EF-1	", ID:	"LEF-	1"					-		
Nr.	Х	Y	Z	Refl.	DEN	Freq.	Lw	l/a	Optime	K0	Di	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
343	447652.07	5029361.69	7.40	0	D	A	75.9	0.0	0.0	0.0	0.0	48.3	0.3	-0.9	0.0	0.0	15.1	0.0	0.0	13.1
				ve	rt. Are	ea Sou	irce, IS	O 961	3, Name	: "Inta	akes"	, ID: "	Nt"							
Nr.	Х	Y	Z	Refl.	DEN	Freq.	Lw	l/a	Optime	K0	Di	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
354	447681.35	5029365.58	21.50	0	DEN	A	63.0	6.0	0.0	0.0	0.0	47.9	0.1	-1.1	0.0	0.0	22.7	0.0	0.0	-0.5
365	447682.51	5029362.96	21.50	0	DEN	A	63.0	2.5	0.0	0.0	0.0	47.6	0.1	-1.1	0.0	0.0	22.7	0.0	0.0	-3.7
					Point	Sourc	e, ISO	9613,	Name: "	Ex13	", ID:	"Ex13	"							
Nr.	Х	Y	Z	Refl.	DEN	Freq.	Lw	l/a	Optime	K0	Di	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
367	447828.41	5029411.23	11.00	0	DEN	A	79.6	0.0	0.0	0.0	0.0	56.5	0.9	-0.9	0.0	0.0	23.9	0.0	0.0	-0.7
-					Point	Sourc	e, ISO	9613,	Name: "	Ex01	", ID:	"Ex01	"						_	
Nr.	Х	Y	Z	Refl.	DEN	Freq.	Lw	l/a	Optime	K0	Di	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
386	447863.37	5029393.86	11.00	0	DEN	A	79.6	0.0	0.0	0.0	0.0	57.3	1.0	-0.9	0.0	0.0	23.3	0.0	0.0	-1.0
					- ·			00 · -												
				_	Point	Sourc	e, ISO	9613,	Name: "	Ex02	", ID:	''Ex02						-	-	
Nr.	Х	Y	Z	Refl.	DEN	Freq.	Lw	l/a	Optime	K0	Di	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
408	447859.56	5029401.70	11.00	0	DEN	A	79.6	0.0	0.0	0.0	0.0	57.4	1.0	-0.9	0.0	0.0	23.3	0.0	0.0	-1.1
					<u> </u>			<u> </u>												
					Point	Sourc	e, ISO	9613,	Name: "	Ex03	", ID:	Ex03	5" • · · · ·				• · · ·	<u> </u>	-	
Nr.	X	Y	Z	Refl.	DEN	Freq.	Lw	l/a	Optime	K0	Di	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
435	447855.11	5029410.59	11.00	0	DEN	A	79.6	0.0	0.0	0.0	0.0	57.4	1.0	-0.9	0.0	0.0	23.9	0.0	0.0	-1.8
						_														
				_	Point	Sourc	e, ISO	9613,	Name: "	Ex04	", ID:	"Ex04	."					-		
Nr.	Х	Y	Z	Refl.	DEN	Freq.	Lw	l/a	Optime	K0	Di	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	dB(A)
439	447848.54	5029421.19	11.00	0	DEN	A	79.6	0.0	0.0	0.0	0.0	57.4	1.0	-0.9	0.0	0.0	23.9	0.0	0.0	-1.7

vert. Area Source, ISO 9613, Name: "Gen Intake", ID: "Gen_Int"																				
Nr.	Х	Y	Z	Refl.	DEN	Freq.	Lw	l/a	Optime	K0	Di	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL	Lr
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	dB(A)						
460	447690.77	5029361.74	4.50	0	D	A	65.2	4.8	0.0	0.0	0.0	47.8	0.4	-0.8	0.0	0.0	24.9	0.0	0.0	-2.1