

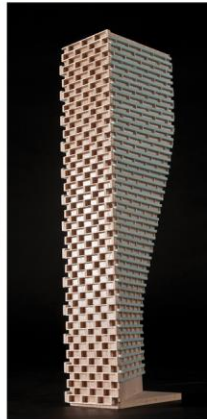
GRADIENTWIND

ENGINEERS & SCIENTISTS

PEDESTRIAN LEVEL WIND STUDY

770-774 Bronson Avenue
Ottawa, Ontario

Report: 20-264-PLW



February 2, 2021

PREPARED FOR

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PREPARED BY

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EXECUTIVE SUMMARY

This report describes a pedestrian level wind (PLW) study undertaken to satisfy the requirements for concurrent Zoning By-law Amendment (ZBLA) and Site Plan Control (SPC) applications for the proposed development located at 770-774 Bronson Avenue in Ottawa, Ontario (hereinafter referred to as “subject site”). Our mandate within this study is to investigate pedestrian wind comfort and safety within and surrounding the subject site, and to identify any areas where wind conditions may interfere with certain pedestrian activities so that mitigation measures may be considered, as required.

The study involves simulation of wind speeds for selected wind directions in a three-dimensional (3D) computer model using the computational fluid dynamics (CFD) technique, combined with meteorological data integration, to assess pedestrian wind comfort and safety within and surrounding the subject site according to City of Ottawa wind comfort and safety criteria. The results and recommendations derived from these considerations are detailed in the main body of the report (Section 5), illustrated in Figures 3A-5D, and summarized as follows:

- 1) All grade-level areas within and surrounding the subject site will be acceptable for the intended pedestrian uses throughout the year. Specifically, wind conditions over surrounding sidewalks, walkways, transit stops, patios, and building access points, are considered acceptable for the intended pedestrian uses throughout the year.
- 2) The amenity terraces at Levels 5 and 8 are predicted to be suitable for sitting during the summer season, which is considered acceptable.
- 3) The terrace atop the tall building at Level 27 will require mitigation to achieve the sitting comfort class during the summer season. Specifically, mitigation is recommended in the form of 1.8-m-tall solid wind screens along the full perimeter of the terrace, which is situated inboard of the roof perimeter. Additionally, since the amenity terrace is located atop the tower and exposed to most statistically prominent winds in Ottawa, we suggest outdoor furniture (e.g., tables and chairs) be fastened to the concrete deck.



- a. Peak wind uplift forces for outdoor furniture can only be accurately assessed using direct measurements of differential wind pressures on representative areas via wind tunnel testing of a physical scale model of the planned development at an appropriate scale.
- 4) Within the context of typical weather patterns, which exclude anomalous localized storm events such as tornadoes and downbursts, no pedestrian areas within and surrounding the subject site were found to experience conditions that could be considered uncomfortable or dangerous.
- 5) Regarding primary and secondary building access points, wind conditions predicted in this study are only applicable to pedestrian comfort and safety. As such, the results should not be construed to indicate wind loading on doors and associated hardware.



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1. INTRODUCTION

Gradient Wind Engineering Inc. (Gradient Wind) was retained by Katasa Groupe + Développement to undertake a pedestrian level wind (PLW) study to satisfy the requirements for concurrent Zoning By-law Amendment (ZBLA) and Site Plan Control (SPC) applications for the proposed development located at 770-774 Bronson Avenue in Ottawa, Ontario (hereinafter referred to as “subject site”). Our mandate within this study is to investigate pedestrian wind comfort and safety within and surrounding the subject site, and to identify any areas where wind conditions may interfere with certain pedestrian activities so that mitigation measures may be considered, as required.

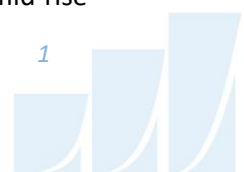
Our work is based on industry standard computer simulations using the computational fluid dynamics (CFD) technique and data analysis procedures, City of Ottawa wind comfort and safety criteria, architectural drawings prepared by Figurr Architects Collective, in January 2021, surrounding street layouts and existing and approved future building massing information obtained from the City of Ottawa, as well as recent satellite imagery.

2. TERMS OF REFERENCE

The subject site is located at 770-774 Bronson Avenue in Ottawa, Ontario on a nearly rectangular parcel of land bounded by Carling Avenue to the north, Bronson Avenue to the east, a private laneway to the south, and Cambridge Street South to the west. The development comprises a 26-storey residential apartment building (Phase 1) transitioning to a mid-rise 9-storey building (Phase 2). The development includes two levels of underground parking. The Phase 1 building continues to rise to the top level in a trapezoidal-shaped planform with upper floors comprising exclusively residential suites.

The ground floor comprises residential space and lobby, lounge, and common/amenity areas. Vehicular access to underground parking is provided from Bronson Avenue. The 9-storey building (Levels 2-9) comprise residential suites and protruding balconies on the north and south elevations. The floorplates set back at Levels 5 and 8 to provide for amenity terraces. An additional amenity terrace is provided at the top of the tall building (Level 27).

The near-field surroundings (defined as an area within 200 metres (m) of the subject site) include the open exposure of the Glebe Collegiate Institute track field to the northeast, a mix of low- and mid-rise



buildings to the south and to the northwest, and low-rise buildings in the remaining compass directions. The far-field surroundings (defined as an area beyond the near-field but within a 2-kilometre (km) radius of the subject site) are characterized by a mix of mostly low- and mid-rise buildings from the west-southwest clockwise to south-southeast, with isolated high-rise buildings to the west and to the north, and by a mix of low-rise buildings and the open exposure of Dow's Lake and the Central Experimental Farm for the remaining compass directions. The downtown Ottawa core lies approximately 2 km to the north, while Dow's Lake lies approximately 500 m to the south-southwest. The Rideau Canal flows southwest to northeast approximately 800 m to the south-southeast of the subject site.

Key areas under consideration include surrounding sidewalks, walkways, bus stops, and building access points. Figure 1 illustrates the subject site and surrounding context, while Figures 2A-2D illustrate the computational model used to conduct the study.

3. OBJECTIVES

The principal objectives of this study are to (i) determine pedestrian level wind comfort and safety conditions at key areas within and surrounding the development site; (ii) identify areas where wind conditions may interfere with the intended uses of outdoor spaces; and (iii) recommend suitable mitigation measures, where required.

4. METHODOLOGY

The approach followed to quantify pedestrian wind conditions over the site is based on CFD simulations of wind speeds across the study site within a virtual environment, meteorological analysis of the Ottawa area wind climate, and synthesis of computational data with City of Ottawa wind comfort and safety criteria¹. The following sections describe the analysis procedures, including a discussion of the noted pedestrian wind criteria.

¹ City of Ottawa Terms of References: Wind Analysis
https://documents.ottawa.ca/sites/default/files/torwindanalysis_en.pdf

4.1 Computer-Based Context Modelling

A computer based PLW study was performed to determine the influence of the wind environment on pedestrian comfort over the proposed development site. Pedestrian comfort predictions, based on the mechanical effects of wind, were determined by combining measured wind speed data from CFD simulations with statistical weather data obtained from Ottawa Macdonald-Cartier International Airport. The general concept and approach to CFD modelling is to represent building and topographic details in the immediate vicinity of the study site on the surrounding model, and to create suitable atmospheric wind profiles at the model boundary. The wind profiles are designed to have similar mean and turbulent wind properties consistent with actual site exposures.

An industry standard practice is to omit trees, vegetation, and other existing and planned landscape elements from the model due to the difficulty of providing accurate seasonal representation of vegetation. The omission of trees and other landscaping elements produces slightly more conservative (i.e., windier) wind speed values.

4.2 Wind Speed Measurements

The PLW analysis was performed by simulating wind flows and gathering velocity data over a CFD model of the site for 12 wind directions. The CFD simulation model was centered on the study building, complete with surrounding massing within a diameter of approximately 820 m.

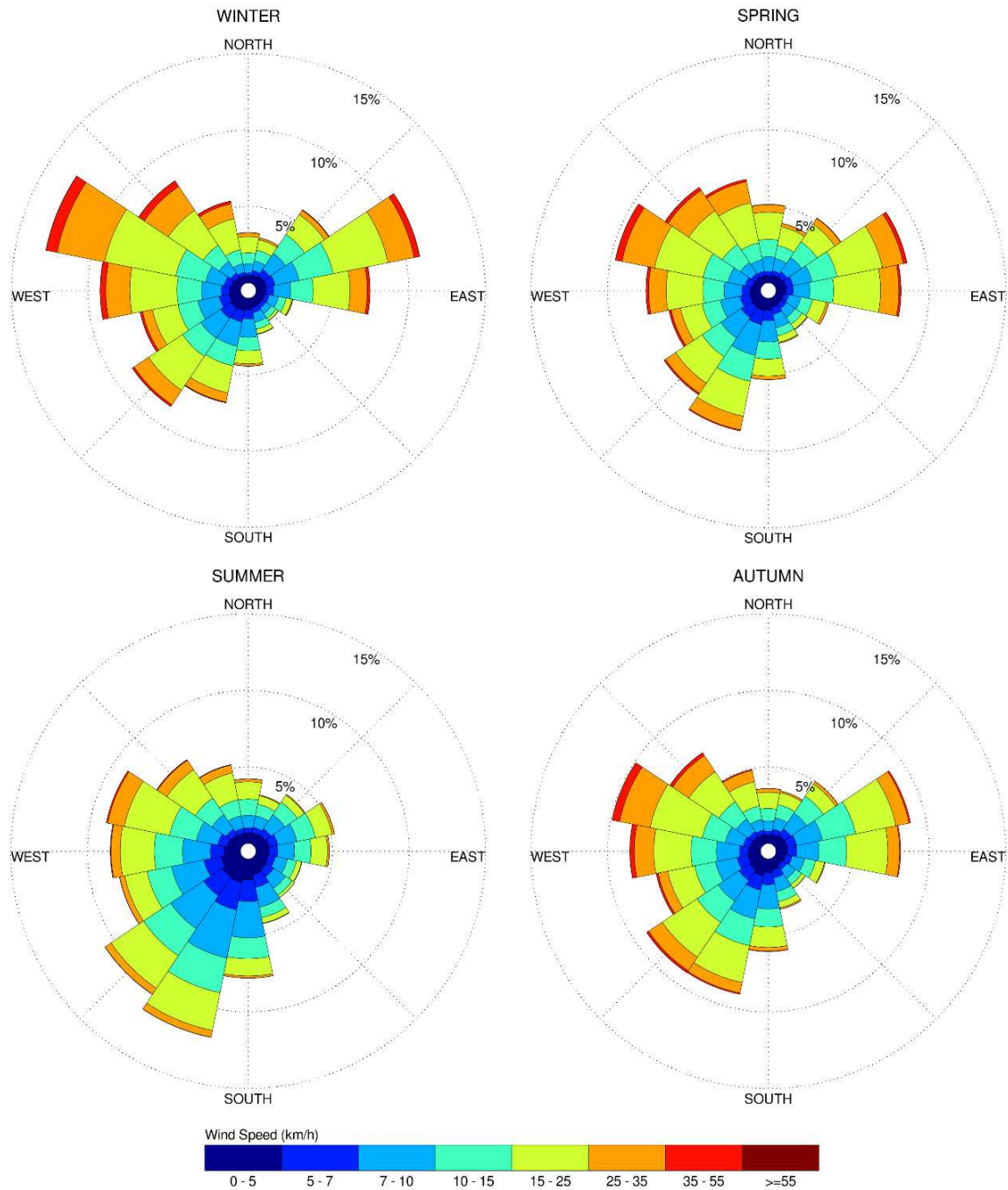
Mean and peak wind speed data obtained over the study site for each wind direction were interpolated to 36 wind directions at 10° intervals, representing the full compass azimuth. Measured wind speeds approximately 1.5 m above local grade and the common elevated amenity terraces were referenced to the wind speed at gradient height to generate mean and peak velocity ratios, which were used to calculate full-scale values. Gradient height represents the theoretical depth of the boundary layer of the earth's atmosphere, above which the mean wind speed remains constant. Further details of the wind flow simulation technique are presented in Appendix A.

4.3 Meteorological Data Analysis

A statistical model for winds in Ottawa was developed from approximately 40 years of hourly meteorological wind data recorded at Ottawa Macdonald-Cartier International Airport and obtained from Environment and Climate Change Canada. Wind speed and direction data were analyzed for each month of the year to determine the statistically prominent wind directions and corresponding speeds, and to characterize similarities between monthly weather patterns.

The statistical model of the Ottawa area wind climate, which indicates the directional character of local winds on a seasonal basis, is illustrated on the following page. The plots illustrate seasonal distribution of measured wind speeds and directions in kilometers per hour (km/h). Probabilities of occurrence of different wind speeds are represented as stacked polar bars in sixteen azimuth divisions. The radial direction represents the percentage of time for various wind speed ranges per wind direction during the measurement period. The preferred wind speeds and directions can be identified by the longer length of the bars. For Ottawa, the most common winds occur for westerly wind directions, followed by those from the east, while the most common wind speeds are below 36 km/h. The directional preference and relative magnitude of wind speed changes somewhat from season to season.

SEASONAL DISTRIBUTION OF WIND OTTAWA MACDONALD-CARTIER INTERNATIONAL AIRPORT



Notes:

1. Radial distances indicate percentage of time of wind events.
2. Wind speeds are mean hourly in km/h, measured at 10 m above the ground.

4.4 Pedestrian Comfort and Safety Criteria – City of Ottawa

Pedestrian comfort and safety criteria are based on the mechanical effects of wind without consideration of other meteorological conditions (i.e., temperature, relative humidity). The comfort criteria assume that pedestrians are appropriately dressed for a specified outdoor activity during any given season. Five pedestrian comfort classes are based on 80% non-exceedance mean wind speed ranges, which include (1) Sitting; (2) Standing; (3) Strolling; (4) Walking; and (5) Uncomfortable. More specifically, the comfort classes and associated mean wind speed ranges are summarized as follows:

- 1) **Sitting:** Mean wind speeds no greater than 10 km/h occurring at least 80% of the time. The equivalent gust wind speed is approximately 16 km/h.
- 2) **Standing:** Mean wind speeds no greater than 14 km/h occurring at least 80% of the time. The equivalent gust wind speed is approximately 22 km/h.
- 3) **Strolling:** Mean wind speeds no greater than 17 km/h occurring at least 80% of the time. The equivalent gust wind speed is approximately 27 km/h.
- 4) **Walking:** Mean wind speeds no greater than 20 km/h occurring at least 80% of the time. The equivalent gust wind speed is approximately 32 km/h.
- 5) **Uncomfortable:** Uncomfortable conditions are characterized by predicted values that fall below the 80% target for walking. Brisk walking and exercise, such as jogging, would be acceptable for moderate excesses of this criterion.

The pedestrian safety wind speed criterion is based on the approximate threshold that would cause a vulnerable member of the population to fall. A 0.1% exceedance gust wind speed of 90 km/h is classified as dangerous. The gust speeds, and equivalent mean speeds, are selected based on ‘The Beaufort Scale’, presented on the following page, which describes the effects of forces produced by varying wind speed levels on objects. Gust speeds are included because pedestrians tend to be more sensitive to wind gusts than to steady winds for lower wind speed ranges. For strong winds approaching dangerous levels, this effect is less important because the mean wind can also create problems for pedestrians. The mean gust speed ranges are selected based on ‘The Beaufort Scale’, which describes the effect of forces produced by varying wind speeds on levels on objects.

THE BEAUFORT SCALE

| Number | Description | Wind Speed (km/h) | | Description |
|--------|-----------------|-------------------|--------|---|
| | | Mean | Gust | |
| 2 | Light Breeze | 6-11 | 9-17 | Wind felt on faces |
| 3 | Gentle Breeze | 12-19 | 18-29 | Leaves and small twigs in constant motion; wind extends light flags |
| 4 | Moderate Breeze | 20-28 | 30-42 | Wind raises dust and loose paper; small branches are moved |
| 5 | Fresh Breeze | 29-38 | 43-57 | Small trees in leaf begin to sway |
| 6 | Strong Breeze | 39-49 | 58-74 | Large branches in motion; Whistling heard in electrical wires; umbrellas used with difficulty |
| 7 | Moderate Gale | 50-61 | 75-92 | Whole trees in motion; inconvenient walking against wind |
| 8 | Gale | 62-74 | 93-111 | Breaks twigs off trees; generally impedes progress |

Experience and research on people’s perception of mechanical wind effects has shown that if the wind speed levels are exceeded for more than 20% of the time, the activity level would be judged to be uncomfortable by most people. For instance, if a mean wind speed of 10 km/h were exceeded for more than 20% of the time most pedestrians would judge that location to be too windy for sitting. Similarly, if mean wind speed of 20 km/h at a location were exceeded for more than 20% of the time, walking or less vigorous activities would be considered uncomfortable. As these criteria are based on subjective reactions of a population to wind forces, their application is partly based on experience and judgment.

Once the pedestrian wind speed predictions have been established throughout the site, the assessment of pedestrian comfort involves determining the suitability of the predicted wind conditions for discrete regions within and surrounding the subject site. This step involves comparing the predicted comfort classes to the desired comfort classes, which are dictated by the location type for each region (i.e., a sidewalk, building entrance, amenity space, or other). An overview of common pedestrian location types and their desired comfort classes are summarized on the following page.

DESIRED PEDESTRIAN COMFORT CLASSES FOR VARIOUS LOCATION TYPES

| Location Types | Desired Comfort Classes |
|--|--------------------------------|
| Primary Building Entrance | Standing |
| Secondary Building Access Point | Standing / Strolling / Walking |
| Primary Public Sidewalk | Strolling / Walking |
| Secondary Public Sidewalk / Bicycle Path | Walking |
| Outdoor Amenity Space | Sitting / Standing / Strolling |
| Café / Patio / Bench / Garden | Sitting |
| Transit Stop | Sitting / Standing |
| Public Park / Plaza | Standing / Strolling |
| Garage / Service Entrance | Walking |
| Parking Lot | Strolling / Walking |
| Vehicular Drop-Off Zone | Standing / Strolling / Walking |

5. RESULTS AND DISCUSSION

The following discussion of predicted pedestrian wind conditions is accompanied by Figures 3A-3D and Figures 4A-4D (following the main text), illustrating seasonal wind comfort conditions at grade level and within the common amenity terraces, respectively. Wind conditions are presented as continuous contours of wind comfort within and surrounding the subject site.

The colour contours indicate various wind comfort classes predicted for certain regions, which correspond to the City of Ottawa wind comfort criteria in Section 4.4. Wind conditions comfortable for sitting or more sedentary activities are represented by the colour green, standing are represented by yellow, strolling by orange, and walking by blue. Uncomfortable conditions are represented by magenta. In addition, Figures 5A-5D illustrate the percentage of time the terraces are predicted to be suitable for sitting. Pedestrian conditions are summarized below for each area of interest.

5.1 Wind Comfort Conditions – Grade Level

Sidewalk and Building Entrances along Bronson Avenue: The sidewalk along Bronson Avenue is predicted to be mostly suitable for sitting during the summer, with a small area near the northwest corner of the building predicted to be suitable for standing. During the spring, winter, and autumn, the sidewalks are predicted to be suitable for a mix of sitting and standing, with a small area near the northwest corner of the building being suitable for strolling during the spring and winter. Owing to the protection of the building façade, conditions at building entrances are generally calmer than the adjacent sidewalk. Conditions in the vicinity of building entrances along Bronson Avenue are predicted to be suitable for sitting throughout the year. The noted conditions are considered acceptable.

Sidewalk and Building Entrances along Carling Avenue: The sidewalk along Carling Avenue is predicted to be suitable for a mix of sitting and standing during the summer, becoming suitable for a mix of strolling and standing throughout the remainder of the year. Owing to the protection of the building façade, conditions in the vicinity of building entrances along Carling Avenue are predicted to be suitable for sitting during the summer, becoming suitable for a mix of sitting and standing throughout the remainder of the year. The noted conditions are considered acceptable.

Sidewalk and Building Entrances along Cambridge Street South: The sidewalk along Cambridge Street South is predicted to be suitable for sitting during the summer, becoming suitable for a mix of sitting and standing throughout the remainder of the year. Owing to the protection of the building façade, conditions in the vicinity of building entrances along Cambridge Street South are predicted to be suitable for sitting throughout the year. The noted conditions are considered acceptable.

Grade Level Patio: The patio at the northwest corner of the subject site will be suitable for sitting during the typical use period of late spring through early autumn, becoming suitable for standing during the colder months. These conditions are considered acceptable.

Bus Stop: The bus stop to the southeast of the subject site is predicted to be suitable for sitting during the summer, becoming suitable for standing throughout the remainder of the year. The noted conditions are considered acceptable.

Walkway and Building Entrances along South Elevation: The walkway and building entrances along the south elevation are predicted to be mostly suitable for sitting throughout the year, with some standing conditions near the southeast corner of the walkway during the winter. The noted conditions are considered acceptable.

Walkway and Building Entrances along North Elevation of Phase 2: The walkway along the north elevation of the Phase 2 portion of the building is predicted to be suitable for sitting during the summer, becoming suitable for a mix of sitting and standing throughout the remainder of the year. Owing to the protection of the building façade, conditions in the vicinity of building entrances are predicted to be suitable for sitting throughout the year. The noted conditions are considered acceptable.

5.2 Wind Comfort Conditions – Common Amenity Terraces

Amenity Terrace, Levels 5 and 8: Conditions over the Level 5 amenity terrace, on the west side of the development, are predicted to be suitable for sitting during the summer season, as illustrated in Figure 4B, becoming suitable for a mix of sitting and standing throughout the remainder of the year. Additionally, during the shoulder seasons of spring and autumn, the terrace is also predicted to be suitable for sitting at least 75% of the time in most areas, as illustrated in Figures 5A and 5C, respectively. These conditions are considered acceptable according to the comfort criteria in Section 4.4.

Conditions over the Level 8 amenity terrace, on the east side of the development, are predicted to be mostly suitable for sitting during the summer season, as illustrated in Figure 4B, becoming mostly suitable for standing throughout the remainder of the year. Additionally, wind conditions during the summer season are also predicted to be suitable for sitting for at least 75% of the time (Figure 5B), while conditions during the shoulder seasons of autumn and spring are predicted to be suitable for sitting at least 70% and 65% of the time, respectively illustrated in Figures 5C and 5A. These conditions are considered acceptable according to the comfort criteria in Section 4.4.

Amenity Terrace, Level 27: Regarding the amenity terrace atop the tall building (Level 27), wind conditions are predicted to be suitable for standing during the summer season (Figure 4B), suitable for strolling during the autumn season (Figure 4C), and suitable for walking during the spring season (Figure 4A). During the summer season, while the sitting comfort class is not achieved, the terrace is predicted to be suitable for sitting for at least 60% of the time (Figure 5B), while conditions during the shoulder



seasons of autumn and spring are predicted to be suitable for sitting at least 55% and 50% of the time, respectively illustrated in Figures 5C and 5A.

The terrace will require mitigation to achieve the sitting comfort class during the summer season. Specifically, mitigation is recommended in the form of 1.8-m-tall solid wind screens along the full perimeter of the terrace, which is situated inboard of the roof perimeter.

Additionally, since the Level 27 amenity terrace is located atop the tower and exposed to most statistically prominent winds in Ottawa, roof uplift considerations are expected to be of importance. While we anticipate strong wind suctions on the roof and pavers (if applicable), a roof uplift study based on wind tunnel testing of a physical scale model of the planned development in its surroundings has not been completed. As such, based on the information from the PLW study and experience with roof uplift studies for numerous similar developments in Ottawa and throughout Canada, we suggest terrace furniture (e.g., tables and chairs) be fastened to the concrete deck.

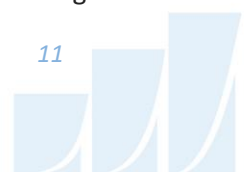
Note: Peak wind uplift forces for outdoor furniture can only be accurately assessed using direct measurements of differential wind pressures on representative areas via wind tunnel testing of a physical scale model of the planned development at an appropriate scale.

5.3 Wind Safety

Within the context of typical weather patterns, which exclude anomalous localized storm events such as tornadoes and downbursts, no pedestrian areas surrounding the subject site at grade level or on the common elevated amenity terraces were found to experience conditions that could be considered dangerous, as defined in Section 4.4.

5.4 Applicability of Results

Wind conditions over surrounding sidewalks beyond the subject site, as well as at nearby primary building entrances, will be acceptable for their intended pedestrian uses during each seasonal period upon the introduction of the subject site. Pedestrian wind comfort and safety have been quantified for the specific configuration of existing and foreseeable construction around the study site. Future changes (i.e., construction or demolition) of these surroundings may cause changes to the wind effects in two ways, namely: (i) changes beyond the immediate vicinity of the site would alter the wind profile approaching



the site; and (ii) development in proximity to the site would cause changes to local flow patterns. In general, development in urban centers generally creates reduction in the mean wind speeds and localized increases in the gustiness of the wind.

Regarding primary and secondary building access points, wind conditions predicted in this study are only applicable to pedestrian comfort and safety. As such, the results should not be construed to indicate wind loading on doors and associated hardware.

6. CONCLUSIONS AND RECOMMENDATIONS

A complete summary of the predicted wind conditions is provided in Section 5 and illustrated in Figures 3A-5D. Based on computer simulations using the CFD technique, meteorological data analysis of the Ottawa wind climate, City of Ottawa wind comfort and safety criteria, and experience with similar developments in Ottawa, we conclude the following:

- 1) All grade-level areas within and surrounding the subject site will be acceptable for the intended pedestrian uses throughout the year. Specifically, wind conditions over surrounding sidewalks, walkways, transit stops, patios, and building access points, are considered acceptable for the intended pedestrian uses throughout the year.
- 2) The amenity terraces at Levels 5 and 8 are predicted to be suitable for sitting during the summer season, which is considered acceptable.
- 3) The terrace atop the tall building at Level 27 will require mitigation to achieve the sitting comfort class during the summer season. Specifically, mitigation is recommended in the form of 1.8-m-tall solid wind screens along the full perimeter of the terrace, which is situated inboard of the roof perimeter. Additionally, since the amenity terrace is located atop the tower and exposed to most statistically prominent winds in Ottawa, we suggest outdoor furniture (e.g., tables and chairs) be fastened to the concrete deck.
 - a. Peak wind uplift forces for outdoor furniture can only be accurately assessed using direct measurements of differential wind pressures on representative areas via wind tunnel testing of a physical scale model of the planned development at an appropriate scale.



- 4) Within the context of typical weather patterns, which exclude anomalous localized storm events such as tornadoes and downbursts, no pedestrian areas within and surrounding the subject site were found to experience conditions that could be considered uncomfortable or dangerous.
- 5) Regarding primary and secondary building access points, wind conditions predicted in this study are only applicable to pedestrian comfort and safety. As such, the results should not be construed to indicate wind loading on doors and associated hardware.

This concludes our PLW study and report. Please advise the undersigned of any questions or comments.

Sincerely,

Gradient Wind Engineering Inc.

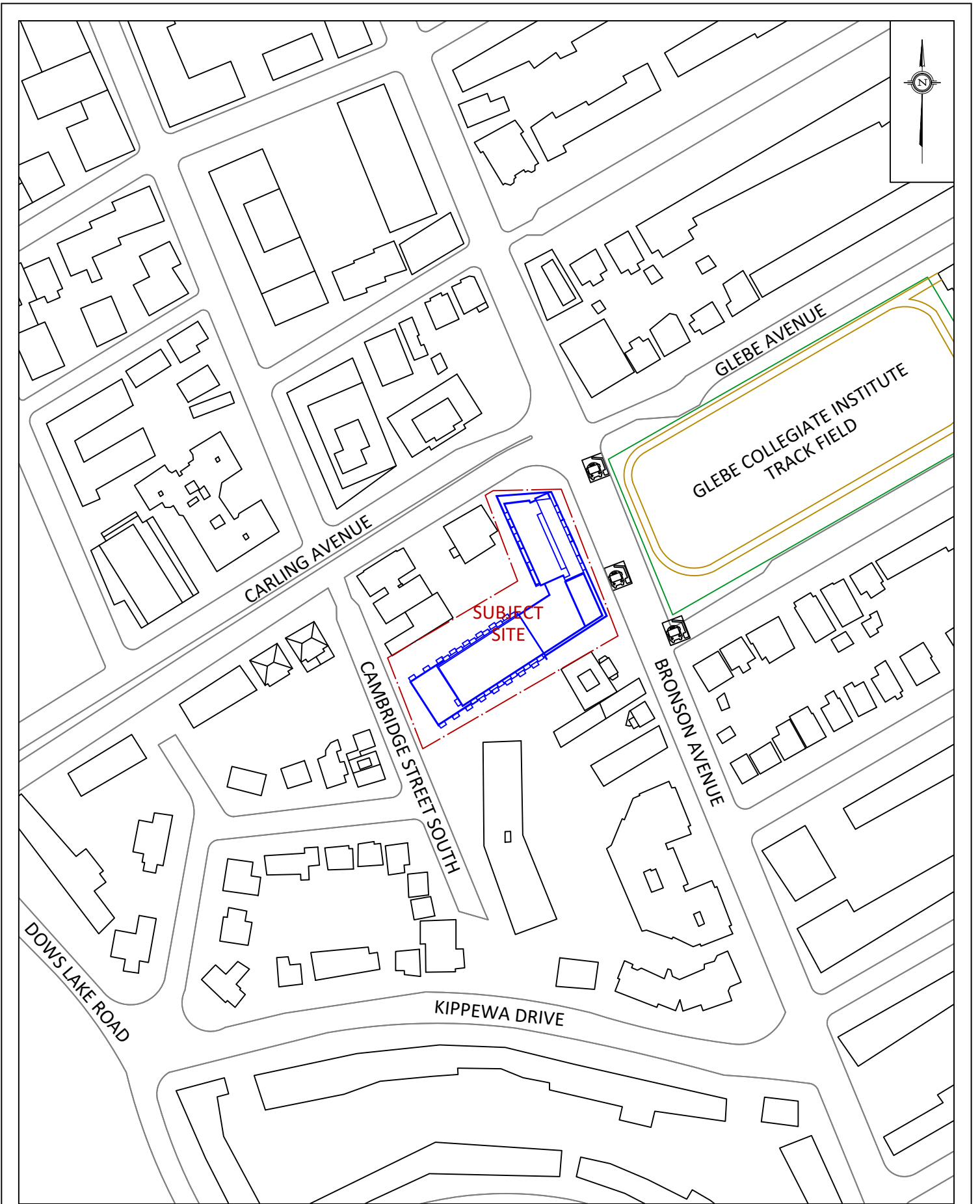


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| | | |
|---------|---|-----------------------------|
| PROJECT | 770-774 BRONSON AVENUE, OTTAWA PEDESTRIAN LEVEL WIND STUDY | |
| SCALE | 1:2000 | DRAWING NO. 20-264-PLW-1 |
| DATE | JANUARY 22, 2021 | DRAWN BY O.R. |

| | |
|-------------|--|
| DESCRIPTION | FIGURE 1: SITE PLAN AND SURROUNDING CONTEXT |
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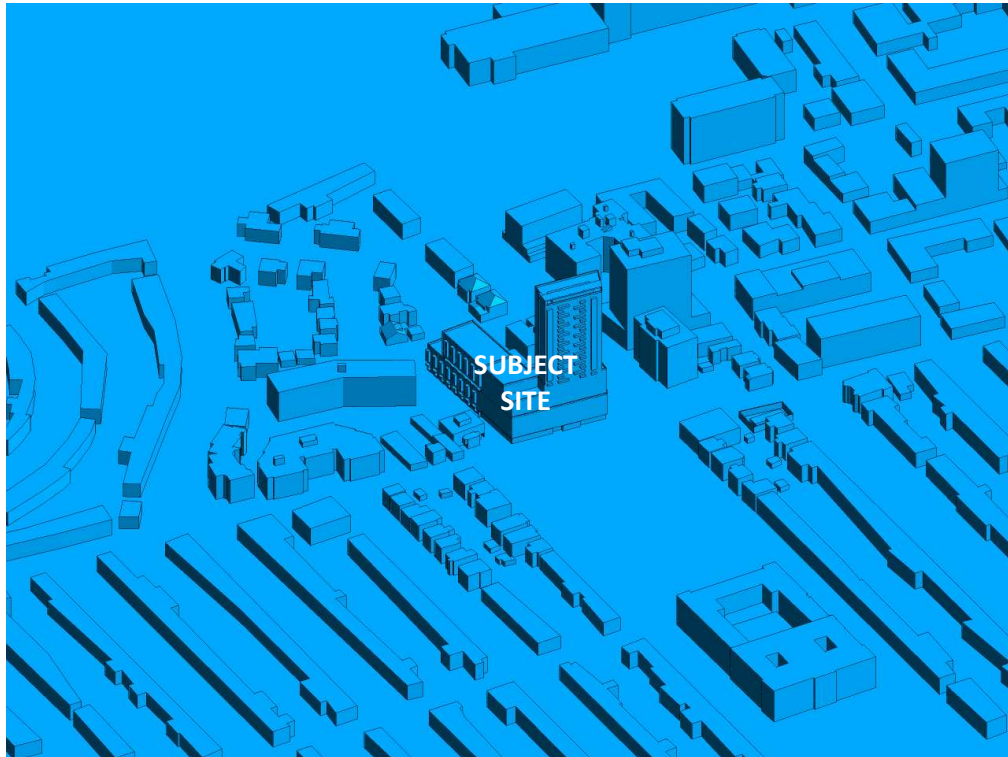


FIGURE 2A: COMPUTATIONAL MODEL, EAST PERSPECTIVE

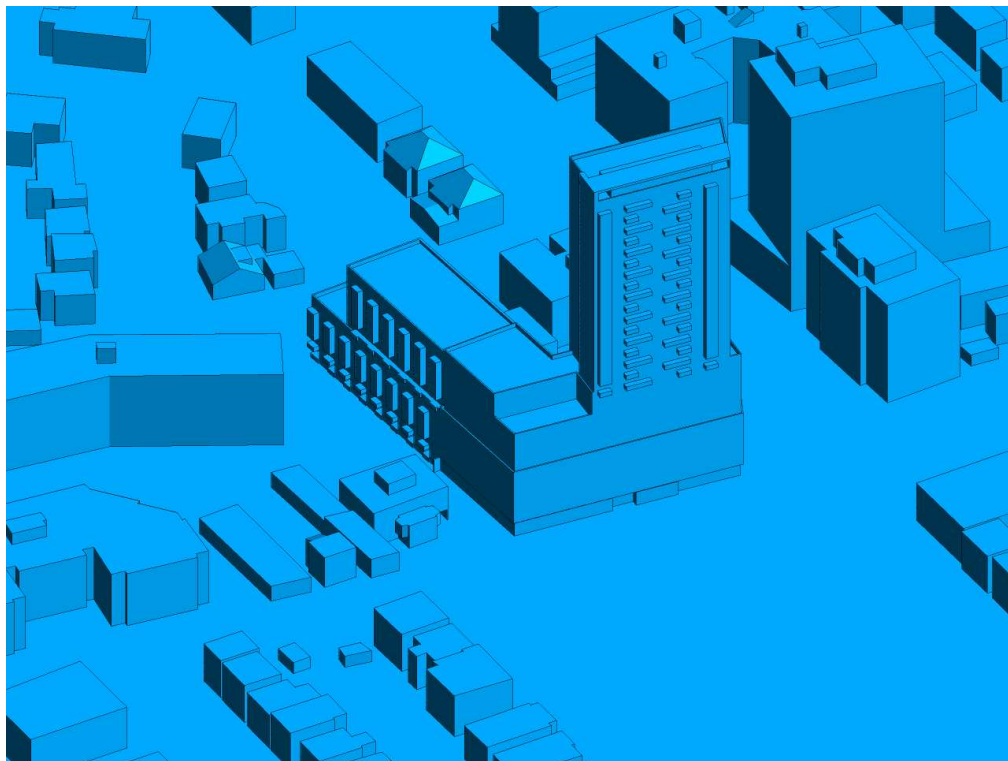


FIGURE 2B: CLOSE UP OF FIGURE 2A



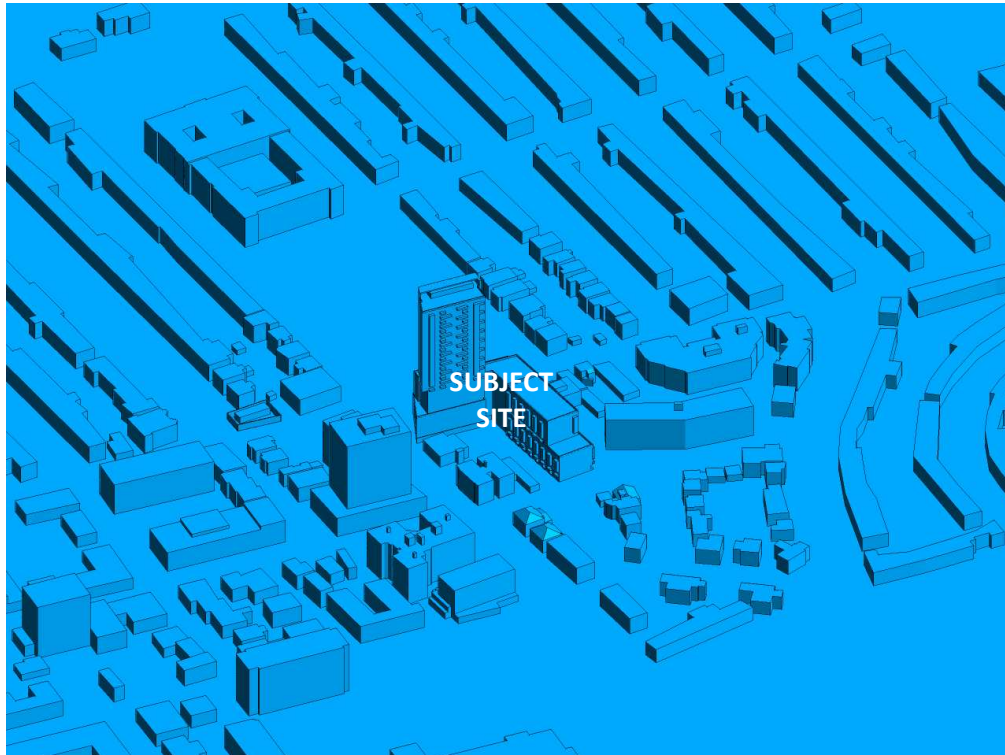


FIGURE 2C: COMPUTATIONAL MODEL, WEST PERSPECTIVE

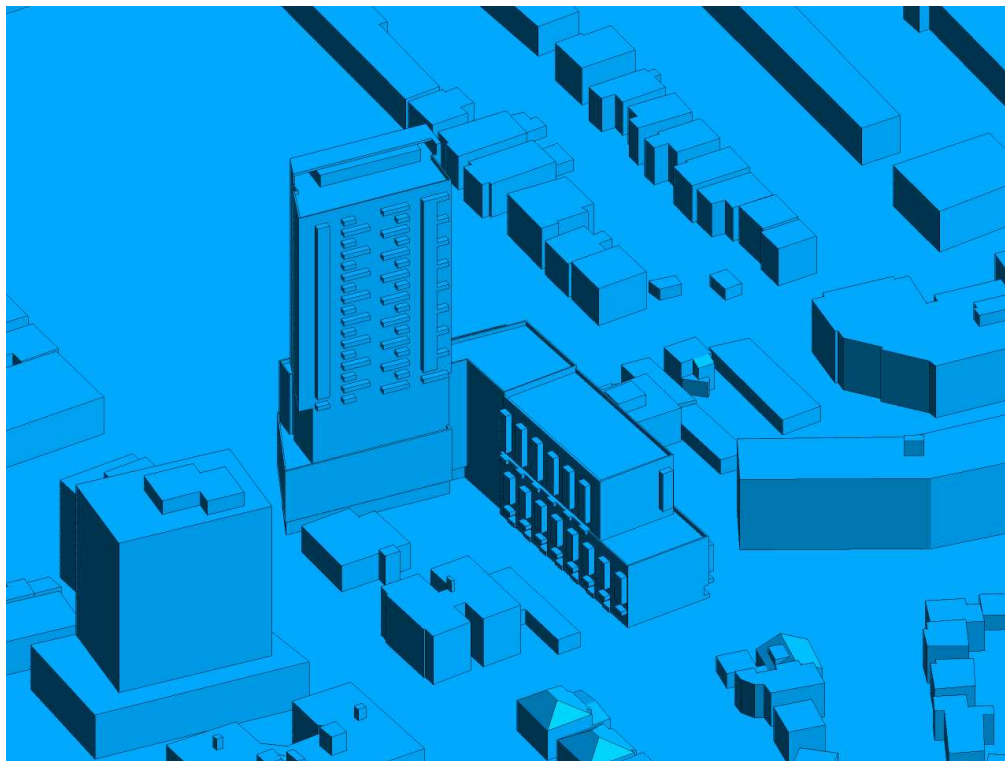


FIGURE 2D: CLOSE UP OF FIGURE 2C





FIGURE 3A: SPRING – WIND COMFORT CLASSES, GRADE LEVEL



FIGURE 3B: SUMMER – WIND COMFORT CLASSES, GRADE LEVEL





FIGURE 3C: AUTUMN – WIND COMFORT CLASSES, GRADE LEVEL



FIGURE 3D: WINTER – WIND COMFORT CLASSES, GRADE LEVEL



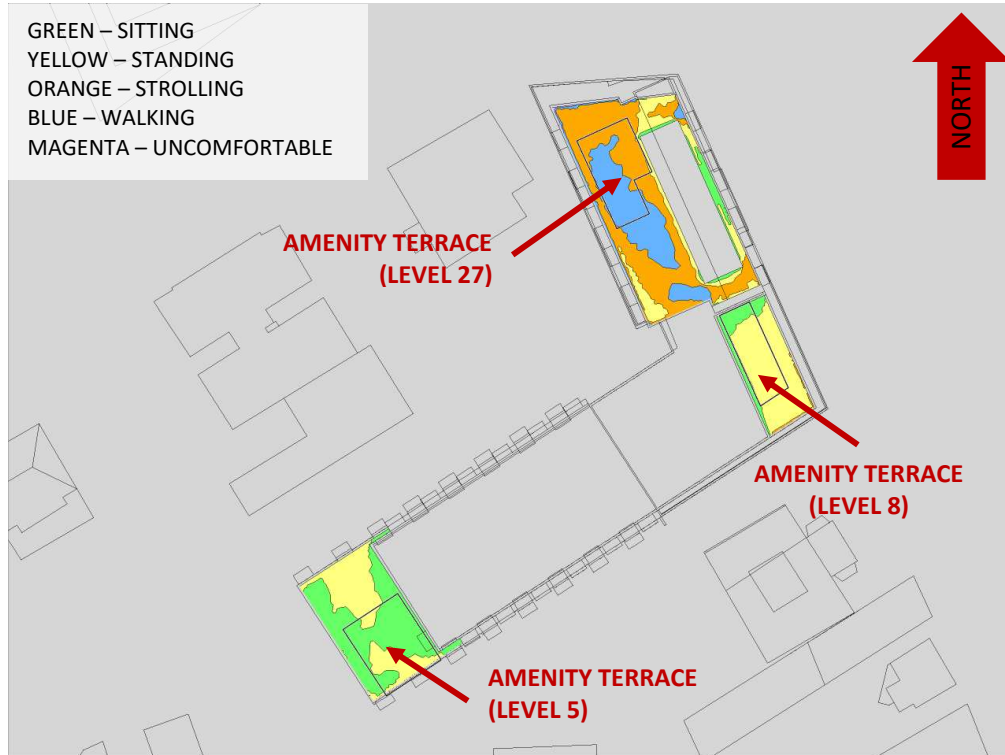


FIGURE 4A: SPRING – WIND COMFORT CLASSES, AMENITY TERRACES

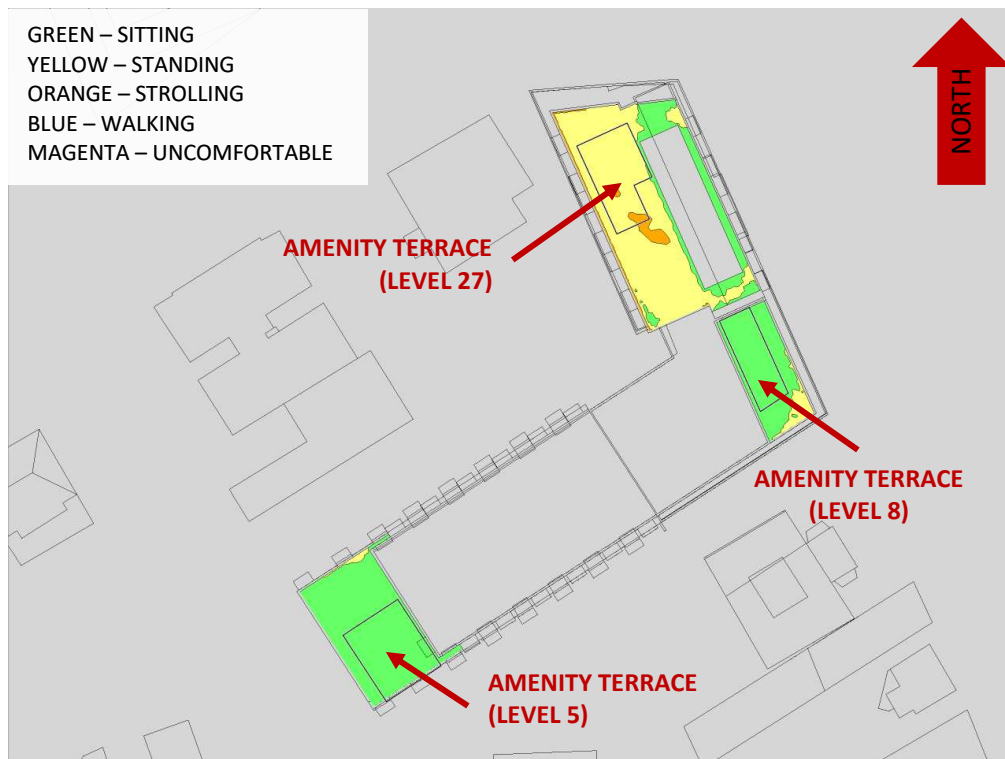


FIGURE 4B: SUMMER – WIND COMFORT CLASSES, AMENITY TERRACES

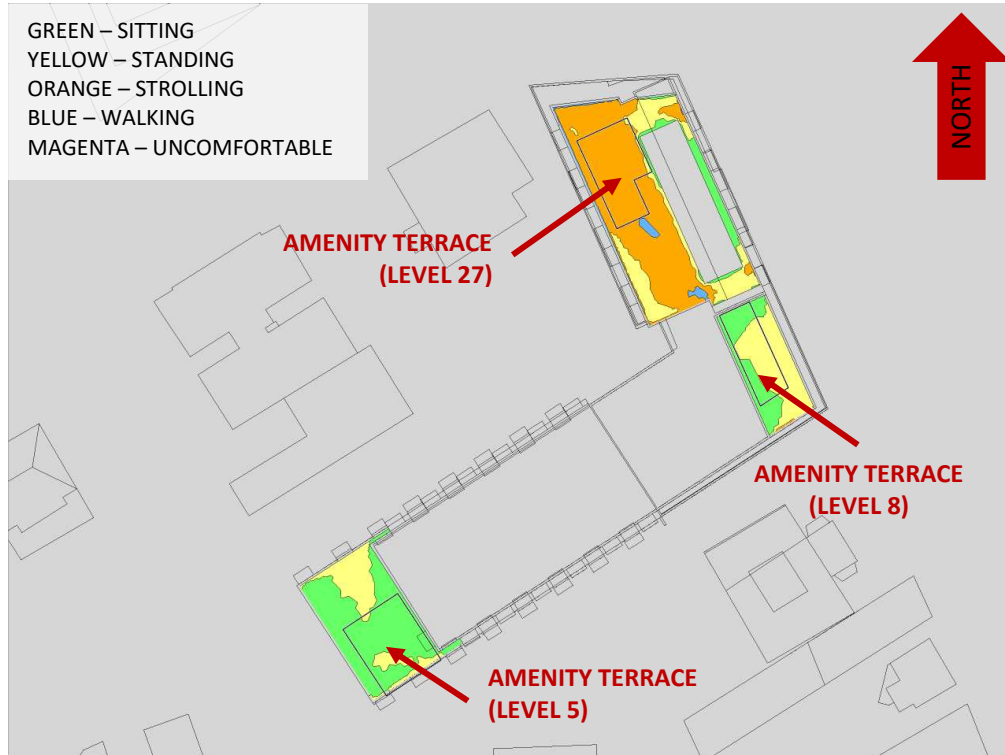


FIGURE 4C: AUTUMN – WIND COMFORT CLASSES, AMENITY TERRACES

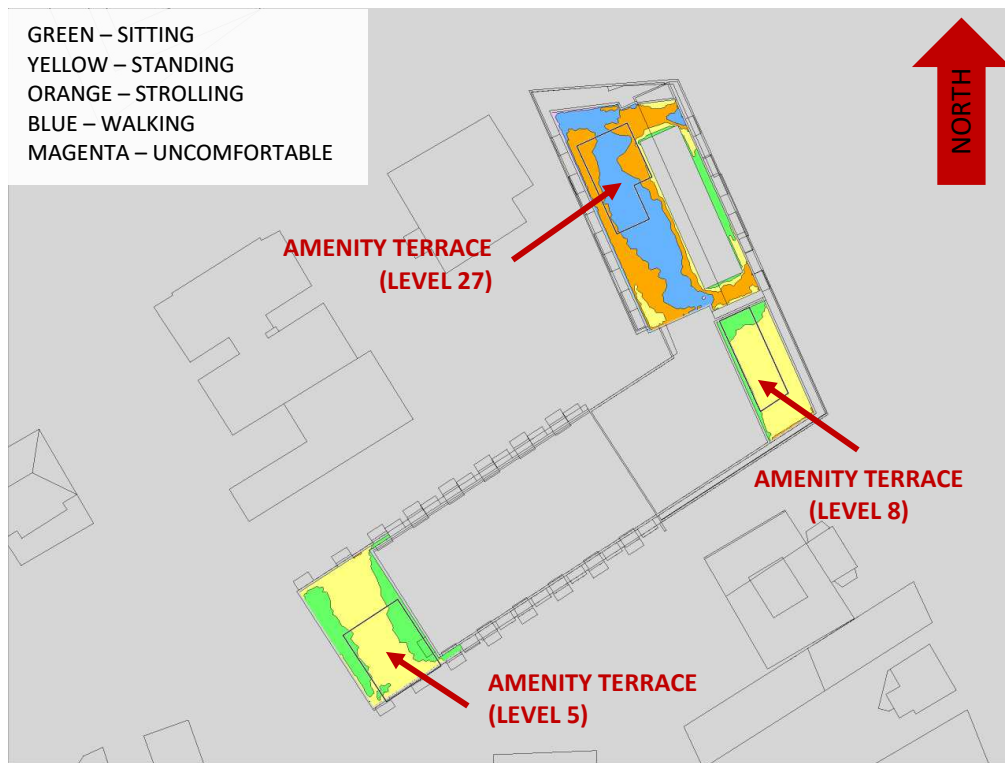


FIGURE 4D: WINTER – WIND COMFORT CLASSES, AMENITY TERRACES

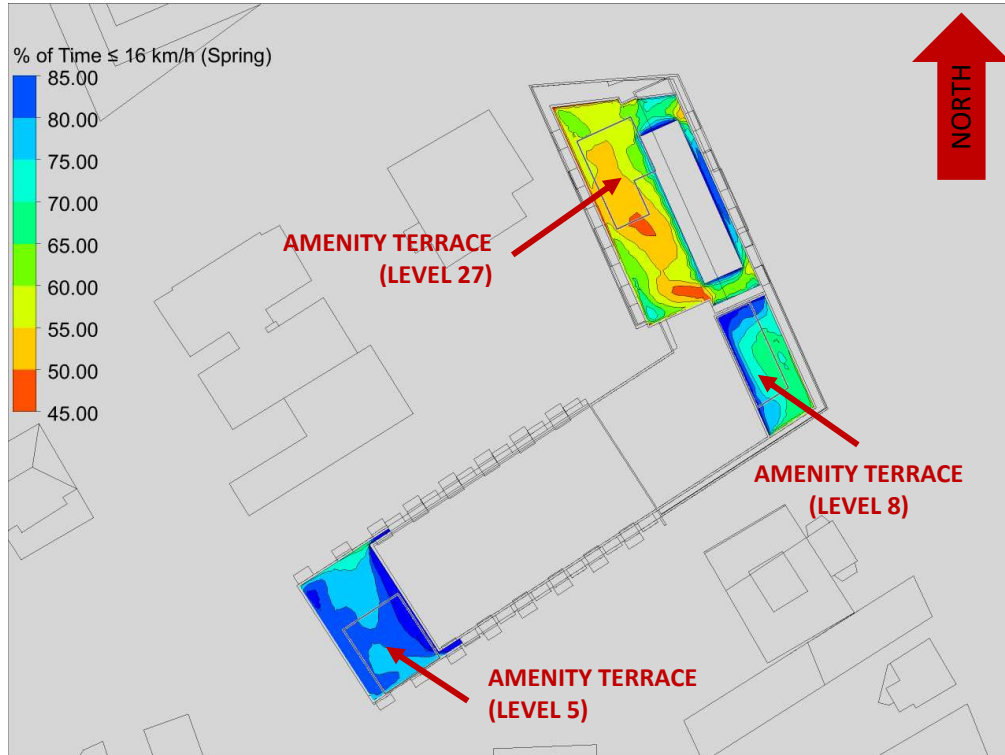


FIGURE 5A: SPRING – PERCENTAGE OF TIME SUITABLE FOR SITTING, AMENITY TERRACES

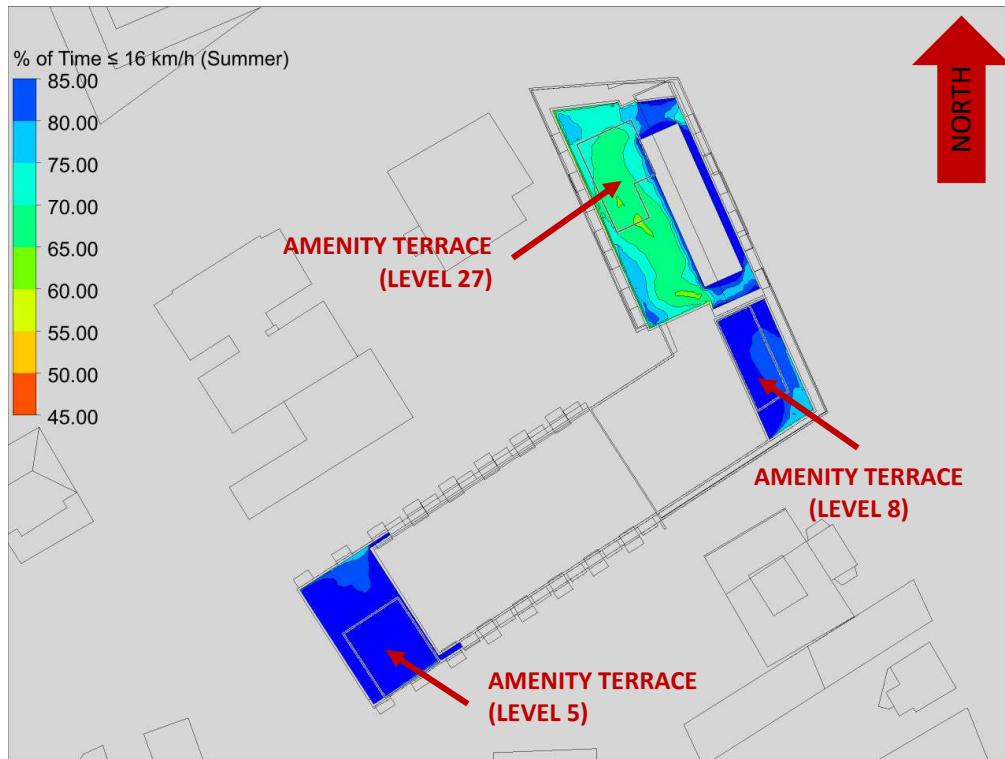


FIGURE 5B: SUMMER – PERCENTAGE OF TIME SUITABLE FOR SITTING, AMENITY TERRACES

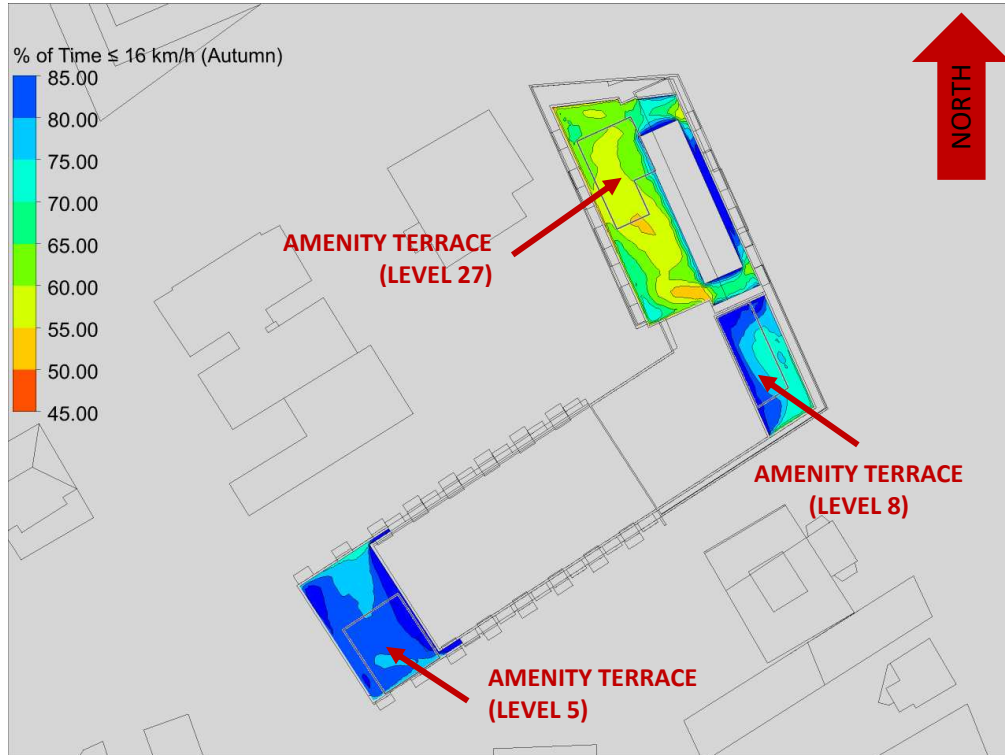


FIGURE 5C: AUTUMN – PERCENTAGE OF TIME SUITABLE FOR SITTING, AMENITY TERRACES



FIGURE 5D: WINTER – PERCENTAGE OF TIME SUITABLE FOR SITTING, AMENITY TERRACES



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APPENDIX A

SIMULATION OF THE ATMOSPHERIC BOUNDARY LAYER

SIMULATION OF THE ATMOSPHERIC BOUNDARY LAYER

The atmospheric boundary layer (ABL) is defined by the velocity and turbulence profiles according to industry standard practices. The mean wind profile can be represented, to a good approximation, by a power law relation, Equation (1), giving height above ground versus wind speed [1], [2].

$$U = U_g \left(\frac{Z}{Z_g} \right)^\alpha \quad \text{Equation (1)}$$

where, U = mean wind speed, U_g = gradient wind speed, Z = height above ground, Z_g = depth of the boundary layer (gradient height), and α is the power law exponent.

For the model, U_g is set to 6.5 metres per second (m/s), which approximately corresponds to the 60% mean wind speed for Ottawa based on historical climate data and statistical analyses. When the results are normalized by this velocity, they are relatively insensitive to the selection of gradient wind speed.

Z_g is set to 540 m. The selection of gradient height is relatively unimportant, so long as it exceeds the building heights surrounding the subject site. The value has been selected to correspond to our physical wind tunnel reference value.

α is determined based on the upstream exposure of the far-field surroundings (i.e., the area that it not captured within the simulation model).

Table 1 presents the values of α used in this study, while Table 2 presents several reference values of α . When the upstream exposure of the far-field surroundings is a mixture of multiple types of terrain, the α values are a weighted average with terrain that is closer to the subject site given greater weight.

TABLE 1: UPSTREAM EXPOSURE (ALPHA VALUE) VS TRUE WIND DIRECTION

| Wind Direction (° True) | Alpha (α) Value |
|-------------------------|--------------------------|
| 0 | 0.27 |
| 49 | 0.25 |
| 74 | 0.24 |
| 103 | 0.24 |
| 167 | 0.22 |
| 197 | 0.21 |
| 217 | 0.21 |
| 237 | 0.23 |
| 262 | 0.27 |
| 282 | 0.27 |
| 302 | 0.26 |
| 324 | 0.26 |

TABLE 2: DEFINITION OF UPSTREAM EXPOSURE (ALPHA VALUE)

| Upstream Exposure Type | α |
|------------------------|-----------|
| Open Water | 0.14-0.15 |
| Open Field | 0.16-0.19 |
| Light Suburban | 0.21-0.24 |
| Heavy Suburban | 0.24-0.27 |
| Light Urban | 0.28-0.30 |
| Heavy Urban | 0.31-0.33 |

The turbulence model in the computational fluid dynamics (CFD) simulations is a two-equation shear-stress transport (SST) model, and thus the ABL turbulence profile requires that two parameters be defined at the inlet of the domain. The turbulence profile is defined following the recommendations of the Architectural Institute of Japan for flat terrain [3].

$$I(Z) = \begin{cases} 0.1 \left(\frac{Z}{Z_g} \right)^{-\alpha-0.05}, & Z > 10 \text{ m} \\ 0.1 \left(\frac{10}{Z_g} \right)^{-\alpha-0.05}, & Z \leq 10 \text{ m} \end{cases} \quad \text{Equation (2)}$$

$$L_t(Z) = \begin{cases} 100 \text{ m} \sqrt{\frac{Z}{30}}, & Z > 30 \text{ m} \\ 100 \text{ m}, & Z \leq 30 \text{ m} \end{cases} \quad \text{Equation (3)}$$

where, I = turbulence intensity, L_t = turbulence length scale, Z = height above ground, and α is the power law exponent used for the velocity profile in Equation (1).

Boundary conditions on all other domain boundaries are defined as follows: the ground is a no-slip surface; the side walls of the domain have a symmetry boundary condition; the top of the domain has a specified shear, which maintains a constant wind speed at gradient height; and the outlet has a static pressure boundary condition.

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