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Restoration



Brookstreet Apartments

525 Legget Drive

359 Terry Fox Drive

Servicing and Stormwater Management Brief

**BROOKSTREET APARTMENTS
525 LEGGET DRIVE
359 TERRY FOX DRIVE**

SITE SERVICING AND SWM BRIEF

Prepared for:

KRP Properties

Prepared by:

NOVATECH

Suite 200, 240 Michael Cowpland Drive
Kanata, Ontario
K2M 1P6

Issued: October 1 , 2021

Ref: R-2021-131
Novatech File No. 120202

October 1, 2021

City of Ottawa
110 Laurier Ave. West, 4th Floor
Ottawa, Ontario
K1P 1J1

Attention: Mr. Damien Whittaker

**Re: Brookstreet Apartments
525 Legget Drive and 359 Terry Fox Drive
Site Servicing and Stormwater Management Brief**

Please find enclosed the Site Servicing and Stormwater Management Brief for the proposed development at 525 Legget Drive and 359 Terry Fox Drive. This report is submitted in support of a zoning amendment and site plan control application on behalf of KRP Properties.

If you have any questions, please contact the undersigned.

Sincerely,

NOVATECH



Greg MacDonald, P.Eng.
Director | Land Development & Public Sector Infrastructure

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1.0 INTRODUCTION

This Site Servicing and Stormwater Management Brief has been prepared in support of a zoning amendment and site plan control application for the construction of a 28 – story apartment building attached to the existing hotel expansion constructed in 2016. The building will contain 224 apartment units, ground floor amenities, an extension of the existing ball room and a roof top restaurant. Two levels of underground parking will provide 110 parking spaces. The existing parking structure will provide another 288 spaces on the two lower levels. Refer to **Figure 1 – Brookstreet Apartments** for an overview.



Figure 1 Brookstreet Apartments

The stormwater management for the site will continue in the current pattern with little impact from the additional building. The storm flows will be conveyed in the existing storm sewer to the existing stormwater management pond. The existing stormwater pond has surplus capacity for this development.

The sanitary service for the expansion will be provided by connecting to an existing 250mm sanitary service in the vicinity of the hotel building. The existing sanitary service only services the underground parking facility and the recently constructed expansion and has excess capacity to service the proposed apartment building.

The apartment building will connect to the existing municipal water service on Terry Fox Drive. Dual water services will be provided.

Servicing and Grading Plans for the development are included in **Appendix A**.

2.0 GEOTECHNICAL INVESTIGATION

A subsurface investigation was carried out at the site by Paterson Group. The results of that investigation are provided in the report entitled “Geotechnical Investigation, Proposed Brookstreet Development, Report No. PG5673-1, June 10, 2021”. The principal findings of the geotechnical investigations are as follows:

- A surficial layer of pavement structure and/or topsoil and surficial fill of thickness from 0.3m to 0.6m.
- A silty sand and silty clay layer of thickness up to 2 metres was encountered below the pavement structure/topsoil in all boreholes.
- A glacial till layer at depths of 1.5m to 2.5m below existing ground surface
- The boreholes were terminated in bedrock at depths of about 1.5m to 2.5m below ground surface.

3.0 STORMWATER MANAGEMENT

The stormwater management strategy for the Kanata Research Park is described in the Kanata Research Park Stormwater Management Report (April, 2000) for the 188 ha site. In brief, there are four SWM ponds (Pond 1, Pond 2, Pond 3, and the Duck Pond) which were used to control post-development peak flows to pre-development levels up to the 100-year storm as well as to provide water quality control. The Brookstreet Apartment lands are part of Area 1 in that SWM plan and drain to Pond 1. Area 1 is 19.85 ha in size with an imperviousness of 80%. Pond 1 has a 100-year required storage volume of 5210 m³ and a maximum allowable 100-year release rate of 1.514m³/s.

The proposed building footprint is approximately 1300 m² most of which is situated over existing impervious areas. The additional impervious areas because of hard landscaping are approximately 1500 m². In the 100-year rainfall event, this additional impervious area is projected to create 144 m³ of additional runoff resulting in an increase in pond depth of 9.6 mm. Refer to **Appendix B** for calculations.

The increase in volume represents a 2.7 % increase in the required volume of the pond and less than a 10mm increase in the total water level in the pond. These increases are negligible and will not affect the function of Pond 1 and are within the modelling error tolerance for the SWM facility. Moreover, while Pond 1 only requires 5210 m³ of storage, according to the MOE Certificate of Approval the total available storage capacity of the constructed pond is 28,920 m³. The pond has been oversized and has substantial additional storage capacity to accommodate development in the area.

The expansion is proposed to drain via roof drains and an internal drainage system to the storm sewer which runs along the west side of the existing parking structure. This storm sewer is a 900mm pipe set at a slope of 0.32% and drains directly to the Pond 1 forebay. Due to the extent of the proposed parking structure this storm sewer will be relocated around the parking structure to the SWMF as shown on drawing 120202-GP2. A storm sewer design sheet and storm drainage area plans are included in **Appendix B**.

4.0 SANITARY SEWER SYSTEM

The proposed Apartment Building will be serviced by connecting to an existing 250mm sanitary service that currently services the existing parking garage and the recent expansion to the hotel. The existing 250mm sanitary sewer outlets to the main 250mm sanitary sewer to the west of the hotel which in turn outlets to the 750mm dia. March Trunk Sewer on the Marshes Golf Course lands. The March Trunk Sewer was designed to accommodate flow from the tributary drainage areas shown on the Sanitary Drainage Area Plan (98066-SAN) in **Appendix C**.

As part of previous investigations, the capacity of the existing sanitary sewer system on Kanata Research Park Lands has been documented within the report Sanitary and Storm Trunk Sewer Design Brief Kanata Research Park Lands by Novatech dated November 12, 2014. Contained in the report are the tributary sanitary flows from the Brookstreet Hotel as well as the underground parking structure. A Sanitary Sewer Design Sheet and Drainage Area Plan from this report are contained in **Appendix C**, as well as flows from the recent expansion .

The City of Ottawa design criteria were used to calculate the theoretical sanitary flows for the proposed Apartment Building.

Apartment Building

- Per capita flow 280 L/cap/day
- Peak Factor = $1 + 14/(4 + P^{1/2}) \times 0.80 = 3.10$; Commercial Peak Factor 1.5
- 0.33 L/sec/ha extraneous flows
- Restaurant 30L/seat/day; Typical Floor Space/Seat: 1.25m²/seat
- Design Population: 361 m² / 1.25m²/seat = 288 seats

Table 3.1 identifies the theoretical sanitary flows from the Apartment Building.

Table 3.1 Theoretical Sanitary Flows based on the Design Population

Component	Floor Area (m ²)	Floor Area per Seat	Design Population	Flow per Seat (L/seat/day)	Average Flow (L/s)	Peaking Factor	Peak Flow (L/s)
Commercial	361	1.25m ² /seat	288 seats	30	0.10	1.5	0.15
Component	Units	Pop/Unit	Population	Per Capita Flow	Average Flow	Peak Factor	Peak Flow
1 Bdr	162	1.4	227	280 L/day	0.74		
2 Bdr	93	2.1	195	280 L/day	0.56		
3 Bdr	1	3.1	3	280 L/day	0.11		
	224		425		1.41	3.40	4.79
Extraneous Flow = 0.53 ha x 0.33 L/sec/ha = 0.17 L/sec							0.17
Total Flow = 5.11 L/sec							

In the Sanitary and Storm Trunk Sewer Design Brief Kanata Research Park Lands by Novatech dated November 12, 2014, the existing underground parking area tributary to the sanitary sewer system had no peak population flow and a peak design flow of 0.36 L/s that included extraneous flows. The recent expansion added a population flow of 0.45 L/s. The new apartment building will add a peak design flow of 5.11L/sec. From the 2014 report, the total peak design flow in the sanitary sewer downstream of the proposed hotel expansion connection was 13.91 L/s, and amended to include the recent expansion to 14.36 L/sec. With the increase in population flow from the proposed apartment building, the peak design flow is now 19.47 L/s (14.36 + 5.11). The capacity in the 250 mm diameter sewer to convey these flows to the City’s trunk sewer is 44.74 L/sec. See Sanitary Sewer Design Sheet in **Appendix C**.

5.0 WATER SUPPLY

The proposed Apartment Building will be connected to the existing municipal water service within Terry Fox Drive. The existing 150 mm diameter watermain that services the Monmouth Building will be extended to the parking garage of the proposed apartment building. A second 150 mm diameter water service will be constructed from Terry Fox Drive to the parking structure. A valve will be placed on the Terry Fox main between the two watermain services.

The theoretical water demands for the proposed apartment building were calculated using City of Ottawa Design Criteria as follows:

Residential

- Average Day Demand = Design Population x 350 L/cap/day
- Maximum Day Demand = 2.5 x Average Day Demand
- Peak Hour Demand = 2.2 x Maximum Day Demand

Commercial (Restaurant)

- Average Day Demand = 5 L/m²/day
- Maximum Day Demand = 1.5 x Average Day Demand
- Peak Hour Demand = 1.8 x Maximum Day Demand

Table 4.1 Theoretical Average Water Demand Brookstreet Apartments

Site Component	Floor Area (m ²)		Population (m2)		Average Flow (L/s)
Commercial	361		5 L/m2/day		0.02
Site Component	Units	Pop/Unit	Population	Per Capita Flow	Average Flow (L/s)
Residential	224	1.9	425	350 L/day	1.73

Based on the above, water demands are summarized as follows:

Average Day = 1.75 L/sec
Maximum Day = (0.02 x 1.5) + (1.73 x 2.5) = 4.35 L/sec
Peak Hour = (0.02 x 1.5 x 1.8) + (1.73 x 2.5 x 2.2) = 9.57 L/sec

Fire Underwriters Survey (FUS) was used to provide water demands to the City to obtain the boundary conditions in the existing water mains on Terry Fox Drive. A fire demand of 6,000 L/min was calculated which is included in **Appendix D**.

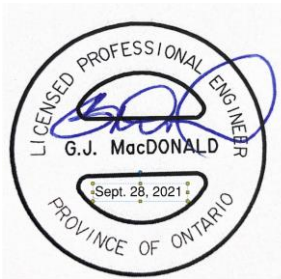
6.0 EROSION AND SEDIMENT CONTROL

Temporary erosion and sediment control measures will be implemented during construction in accordance with the “Guidelines on Erosion and Sediment Control for Urban Construction Sites” (Government of Ontario, May 1987). These measures include:

- Placement of filter socks or bags under all catch basins and maintenance holes;
- Silt fences around the area under construction placed as per OPSS 577 and OPSD 219.110;
- Light duty straw bale check dam per OPSD 219.180;
- Application of topsoil and sod to disturbed areas

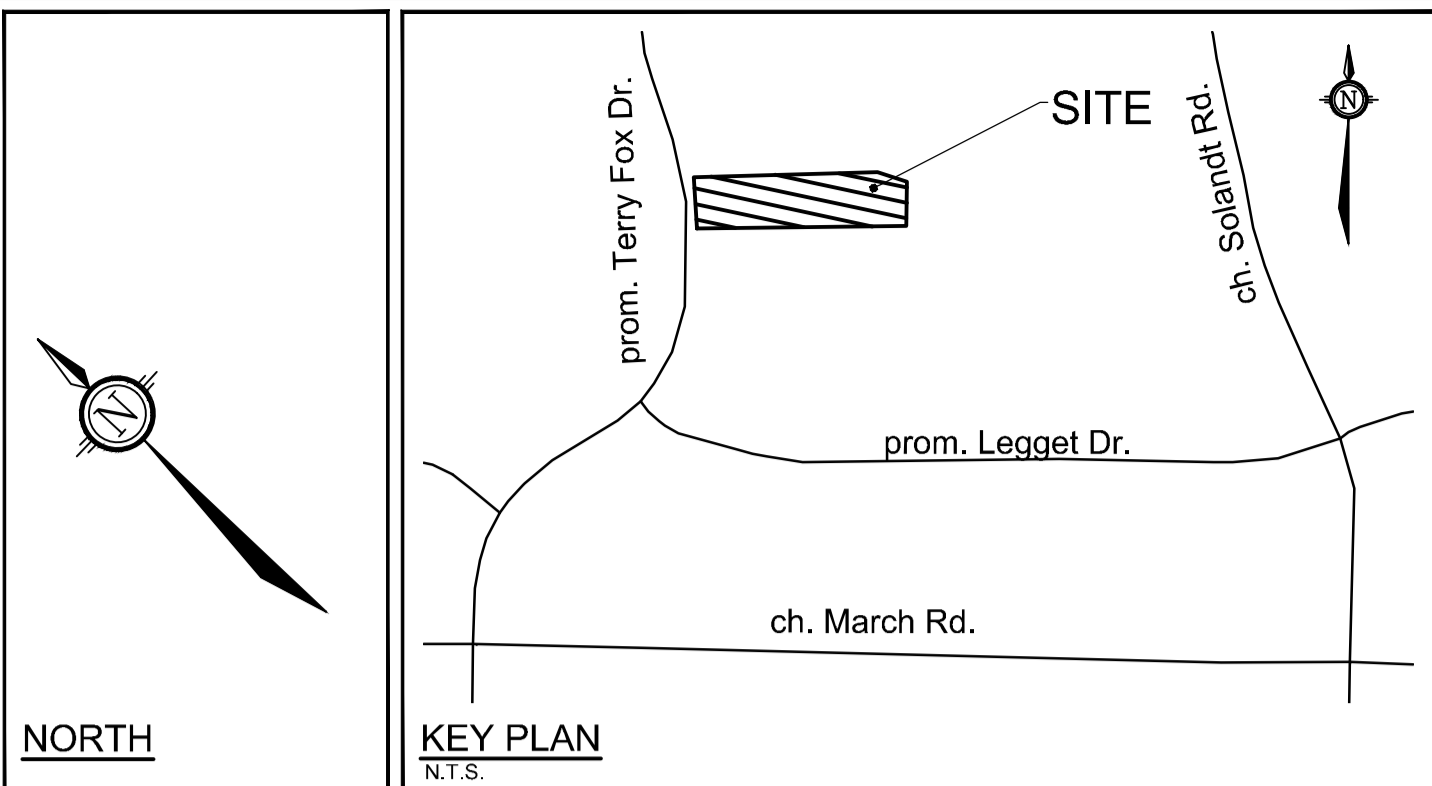
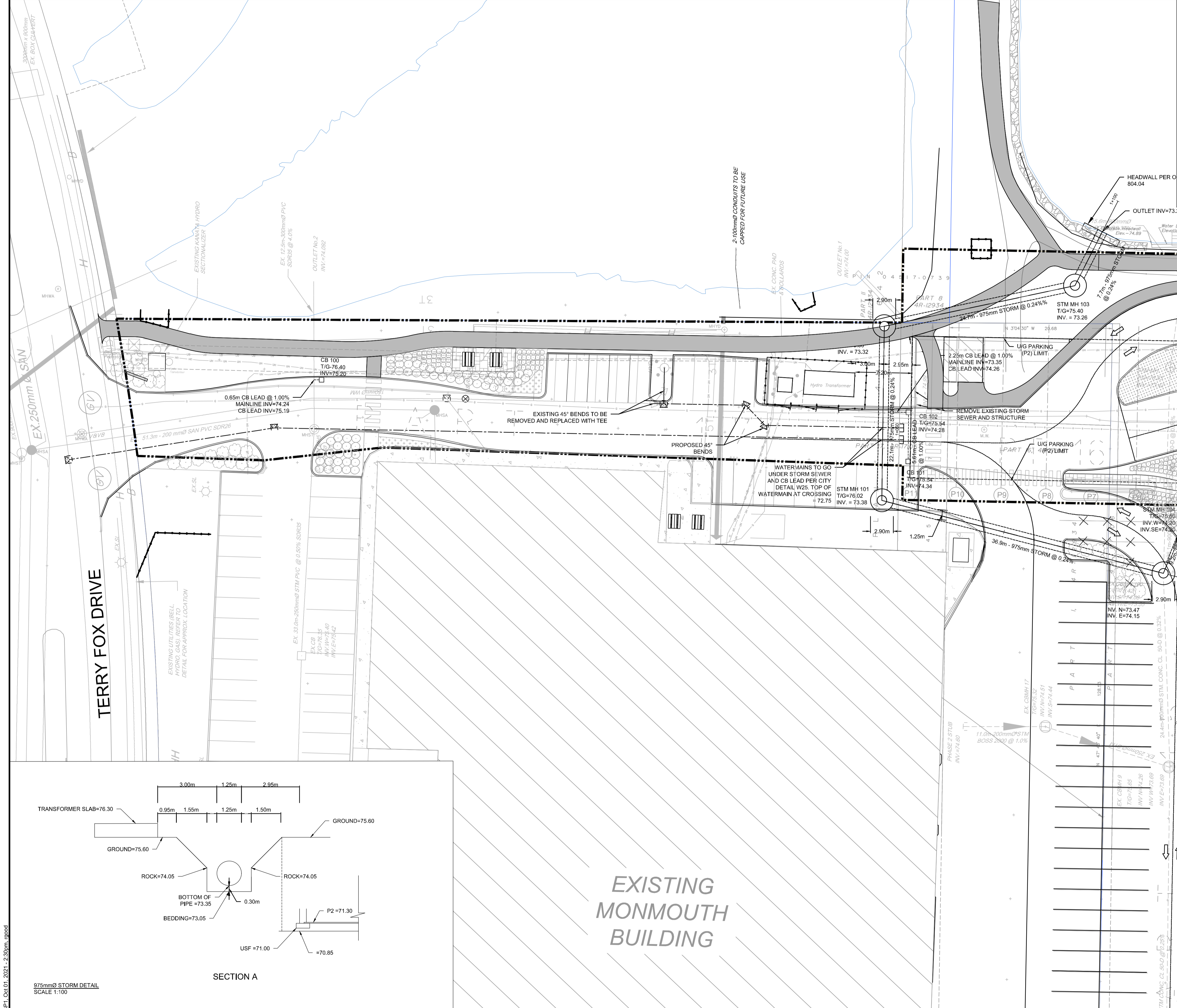
The proposed erosion and sediment control measures will be implemented prior to construction and will remain in place during construction until vegetation is established. There will be regular inspection and maintenance of the sediment control measures.

NOVATECH



Greg MacDonald, P.Eng.
Director
Land Development and Public Sector Infrastructure

APPENDIX A
Servicing and Grading Drawings



- LEGEND**
- PROPOSED PROPERTY LINE
 - PROPOSED STORM MANHOLE AND SEWER
 - PROPOSED STORM MANHOLE AND SEWER
 - PROPOSED WATERMAIN WITH BEND
 - EXISTING STORM MANHOLE AND SEWER
 - EXISTING STORM MANHOLE AND SEWER
 - EXISTING WATERMAIN WITH BEND

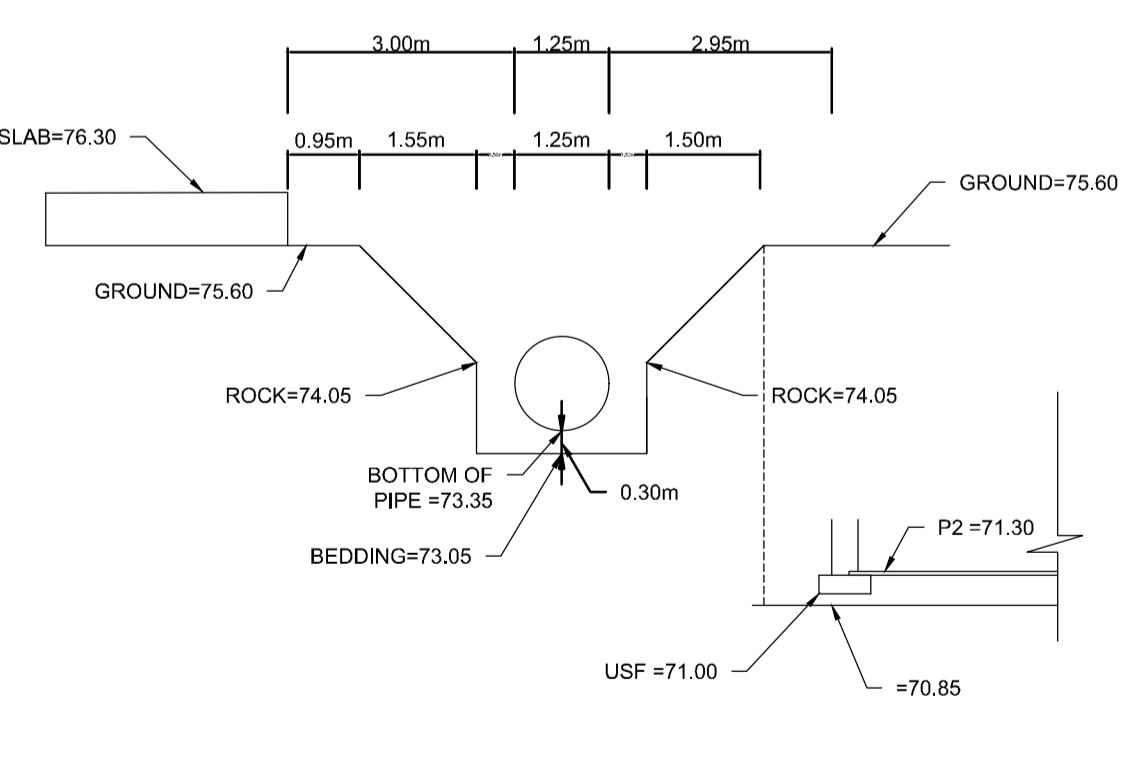
- NOTES**
- GENERAL NOTES:**
- COORDINATE AND SCHEDULE ALL WORK WITH OTHER TRADES AND CONTRACTORS.
 - DETERMINE THE EXACT LOCATION, SIZE, MATERIAL AND ELEVATION OF ALL EXISTING UTILITIES PRIOR TO COMMENCING CONSTRUCTION. PROTECT AND ASSUME RESPONSIBILITY FOR ALL EXISTING UTILITIES WHETHER OR NOT SHOWN ON THIS DRAWING.
 - OBTAIN ALL NECESSARY PERMITS AND APPROVALS FROM THE CITY OF OTTAWA BEFORE COMMENCING CONSTRUCTION.
 - BEFORE COMMENCING CONSTRUCTION OBTAIN AND PROVIDE PROOF OF COMPREHENSIVE, ALL RISK AND OPERATIONAL LIABILITY INSURANCE FOR \$5,000,000.00. INSURANCE POLICY TO NAME OWNERS, ENGINEERS AND ARCHITECTS AS CO-INSURED. (Amount of liability insurance to be verified on a project by project basis)
 - RESTORE ALL DISTURBED AREAS ON-SITE AND OFF-SITE, INCLUDING TRENCHES AND SURFACES ON PUBLIC ROAD ALLOWANCES TO EXISTING CONDITIONS OR BETTER TO THE SATISFACTION OF THE CITY OF OTTAWA AND ENGINEER.
 - REMOVE FROM SITE ALL EXCESS EXCAVATED MATERIAL, ORGANIC MATERIAL AND DEBRIS UNLESS OTHERWISE INSTRUCTED BY ENGINEER. EXCAVATE AND REMOVE FROM SITE ANY CONTAMINATED MATERIAL. ALL CONTAMINATED MATERIAL SHALL BE DISPOSED OF AT A LICENSED LANDFILL FACILITY.
 - ALL ELEVATIONS ARE GEODETIC.
 - REFER TO GEOTECHNICAL REPORT (No. PG5673-1 DATED JUNE 10, 2021 BY PATTERSON GROUP) FOR SUBSURFACE CONDITIONS, CONSTRUCTION RECOMMENDATIONS, AND GEOTECHNICAL INSPECTION REQUIREMENTS. THE GEOTECHNICAL CONSULTANT IS TO REVIEW ON-SITE CONDITIONS AFTER EXCAVATION PRIOR TO PLACEMENT OF THE GRANULAR MATERIAL.
 - REFER TO ARCHITECT'S AND LANDSCAPE ARCHITECT'S DRAWINGS FOR BUILDING AND HARDSURFACE AREAS AND DIMENSIONS.
 - REFER TO SITE SERVICING AND STORMWATER MANAGEMENT BRIEF (REPORT NO. R-2021-131, DATED OCTOBER 01, 2021) PREPARED BY NOVATECH ENGINEERING CONSULTANTS LTD.
 - SAW CUT AND KEY GRIND ASPHALT AT ALL ROAD CUTS AND ASPHALT TIE IN POINTS AS PER CITY OF OTTAWA STANDARDS (R10).
 - PROVIDE LINE/PARKING PAINTING.
 - CONTRACTOR TO PROVIDE THE CONSULTANT WITH A GENERAL PLAN OF SERVICES INDICATING ALL SERVICING AS-BUILT INFORMATION SHOWN ON THIS PLAN. AS-BUILT INFORMATION MUST INCLUDE: PIPE MATERIAL, SIZES, LENGTHS, SLOPES, INVERT AND T/G ELEVATIONS, STRUCTURE LOCATIONS, VALVE AND HYDRANT LOCATIONS, TWM ELEVATIONS AND ANY ALIGNMENT CHANGES, ETC.

- SEWER NOTES:**
- SPECIFICATIONS:

ITEM	SPEC. No.	REFERENCE
CATCH BASIN (600x600mm)	705.010	OPSD
STORM / SANITARY MANHOLE (12000)	701.010	OPSD
CB, FRAME & COVER	400.020	OPSD
STORM / SANITARY MH FRAME & COVER	401.010	OPSD
SEWER TRENCH - BEDDING (GRANULAR A)		
COVER (GRANULAR A OR GRANULAR B TYPE I, WITH MAXIMUM PARTICLE SIZE=25mm)		
STORM SEWER	PVC DR 35	
SANITARY SEWER	PVC DR 35	
CATCH BASIN LEAD	PVC DR 35	
 - INSULATE ALL PIPES (SAN/STM) THAT HAVE LESS THAN 1.5m COVER WITH 50mmX1200mm HI-40 INSULATION. PROVIDE 150mm CLEARANCE BETWEEN PIPE AND INSULATION.
 - SERVICES ARE TO BE CONSTRUCTED TO 1.0m FROM FACE OF BUILDING AT A MINIMUM SLOPE OF 1.0%.
 - PIPE BEDDING, COVER AND BACKFILL ARE TO BE COMPACTED TO AT LEAST 95% OF THE STANDARD PROCTOR MAXIMUM DRY DENSITY. THE USE OF CLEAR CRUSHED STONE AS A BEDDING LAYER SHALL NOT BE PERMITTED.
 - FLEXIBLE CONNECTIONS ARE REQUIRED FOR CONNECTING PIPES TO MANHOLES (FOR EXAMPLE KOR-N-SEAL, PSX POSITIVE SEAL AND DURASEAL). THE CONCRETE CRADLE FOR THE PIPE CAN BE ELIMINATED.
 - THE OWNER SHALL REQUIRE THAT THE SITE SERVICING CONTRACTOR PERFORM FIELD TESTS FOR QUALITY CONTROL OF ALL SANITARY SEWERS. LEAKAGE TESTING SHALL BE COMPLETED IN ACCORDANCE WITH OPSS 410.07.16, 410.07.16.04 AND 407.07.24. DYE TESTING IS TO BE COMPLETED ON ALL SANITARY SERVICES TO CONFIRM PROPER CONNECTION TO THE SANITARY SEWER MAIN. THE FIELD TESTS SHALL BE PERFORMED IN THE PRESENCE OF A CERTIFIED PROFESSIONAL ENGINEER WHO SHALL SUBMIT A CERTIFIED COPY OF THE TEST RESULTS.
 - STORM MANHOLES AND CBMHs ARE TO HAVE 300mm SUMPS UNLESS OTHERWISE INDICATED.
 - CONTRACTOR TO TELEVIEW (CCTV) ALL PROPOSED SEWERS, 200mmØ OR GREATER PRIOR TO BASE COURSE ASPHALT. UPON COMPLETION OF CONTRACT, THE CONTRACTOR IS RESPONSIBLE TO FLUSH AND CLEAN ALL SEWERS & APPURTENANCES.

- WATERMAIN NOTES:**
- SPECIFICATIONS:

ITEM	SPEC. No.	REFERENCE
WATERMAIN TRENCHING	W17	CITY OF OTTAWA
THERMAL INSULATION IN SHALLOW TRENCHES	W22	CITY OF OTTAWA
WATERMAIN CROSSING BELOW SEWER	W25	CITY OF OTTAWA
WATERMAIN	PVC DR 18	
 - SUPPLY AND CONSTRUCT ALL WATERMANS AND APPURTENANCES IN ACCORDANCE WITH THE CITY OF OTTAWA STANDARDS AND SPECIFICATIONS. EXCAVATION, INSTALLATION, BACKFILL AND RESTORATION OF ALL WATERMANS BY THE CONTRACTOR. CONNECTIONS AND SHUT-OFFS AT THE MAIN AND CHLORINATION OF THE WATER SYSTEM SHALL BE PERFORMED BY CITY OFFICIALS.
 - WATERMAIN SHALL BE MINIMUM 2.4m DEPTH BELOW GRADE UNLESS OTHERWISE INDICATED.
 - PROVIDE MINIMUM 0.25m CLEARANCE BETWEEN OUTSIDE OF PIPES AT ALL CROSSINGS.
 - WATER SERVICE IS TO BE CONSTRUCTED TO WITHIN 1.0m OF FOUNDATION WALL AND CAPPED, UNLESS OTHERWISE INDICATED.
 - WATER DEMAND = TBD



975mmØ STORM DETAIL
SCALE 1:100

EXISTING
MONMOUTH
BUILDING

NOTE:
THE POSITION OF ALL POLE LINES, CONDUITS, WATERMANS, SEWERS AND OTHER UNDERGROUND AND OVERGROUND UTILITIES AND STRUCTURES IS NOT NECESSARILY SHOWN ON THE CONTRACT DRAWINGS, AND WHERE SHOWN, THE ACCURACY OF THE POSITION OF SUCH UTILITIES AND STRUCTURES IS NOT GUARANTEED. BEFORE STARTING WORK, DETERMINE THE EXACT LOCATION OF ALL SUCH UTILITIES AND STRUCTURES AND ASSUME ALL LIABILITY FOR DAMAGE TO THEM.

Owner:
Wesley Clover International
c/o Richard Goldstein
KRP Properties
300-555 Legget Drive, Tower B,
Kanata, ON K2K 2X3

No.	REVISION	DATE	BY
1.	ISSUED WITH ZONING AND SITE PLAN APPLICATION	OCT 01/21	GJM

DESIGN	DESIGNER
GJM	GJM
CHECKED	GJM
DRAWN	RJG
CHECKED	GJM
APPROVED	GJM

FOR REVIEW ONLY

SCALE: 1:250

0 2 4 6 8 10

PROFESSIONAL ENGINEER
G. J. MacDONALD
OCT 1, 2021

NOVATECH
Engineers, Planners & Landscape Architects
Suite 200, 240 Michael Cowpland Drive
Ottawa, Ontario, Canada K2M 1P6
Telephone: (613) 254-9643
Facsimile: (613) 254-5867
Website: www.novatech-eng.com

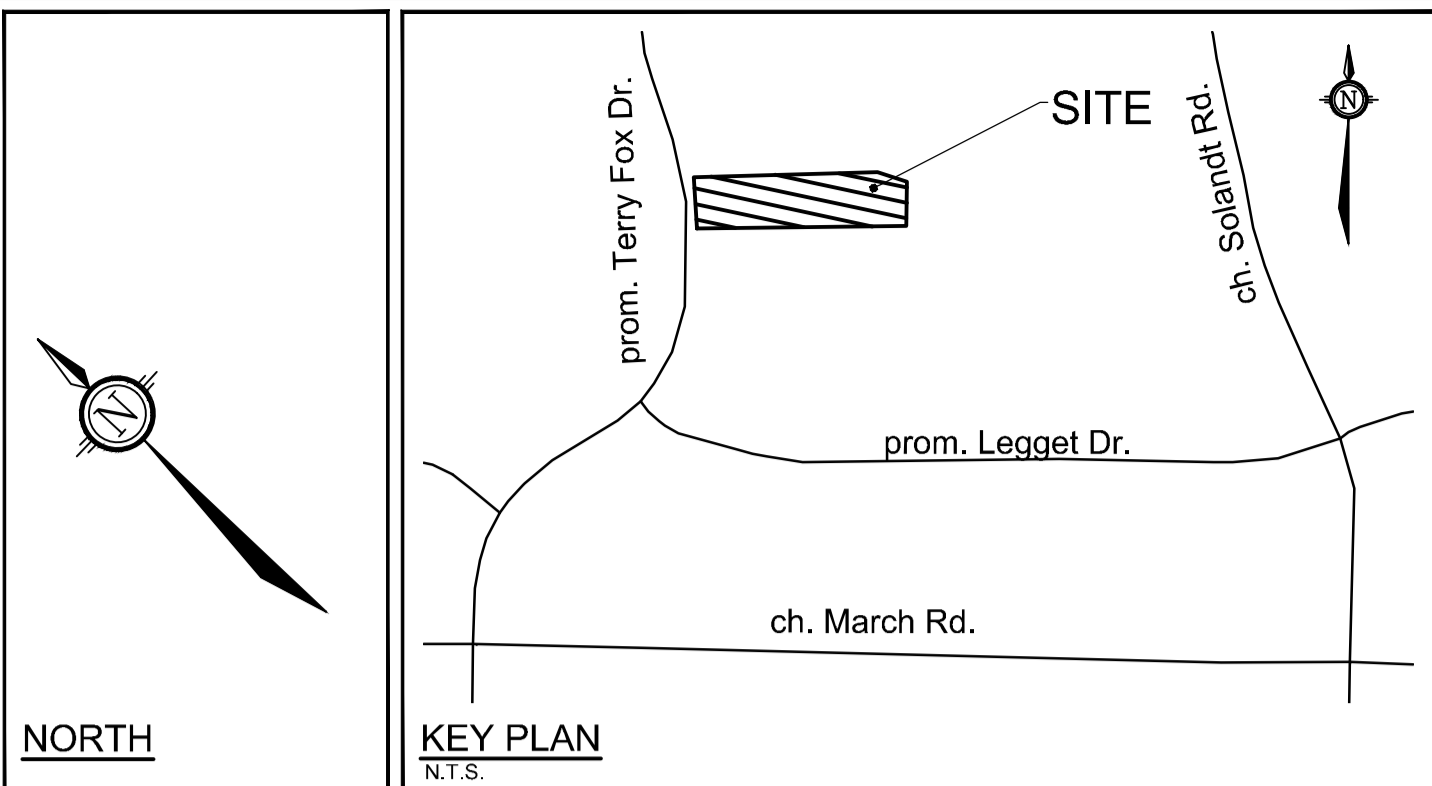
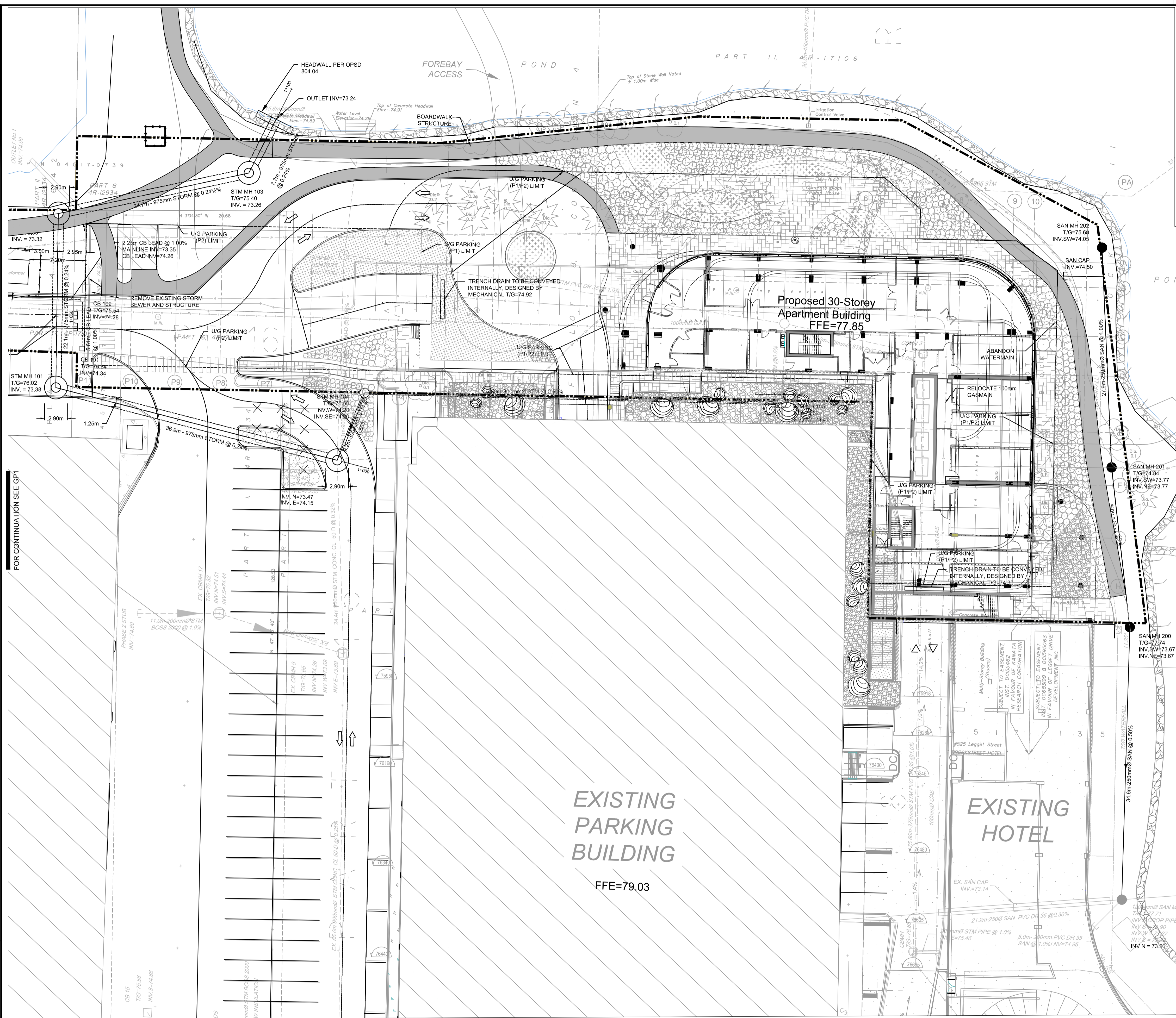
LOCATION
CITY OF OTTAWA
BROOKSTREET APARTMENTS

DRAWING NAME
GENERAL PLAN OF SERVICES

PROJECT No.
120202-00

REV
REV 1

DRAWING No.
120202-GP1



LEGEND

	PROPOSED PROPERTY LINE		EXISTING STORM MANHOLE AND SEWER
	PROPOSED STORM MANHOLE AND SEWER		EXISTING STORM MANHOLE AND SEWER
	PROPOSED STORM MANHOLE AND SEWER		EXISTING WATERMAIN WITH BEND
	PROPOSED WATERMAIN WITH BEND		EXISTING WATERMAIN WITH BEND
	PROPOSED RETAINING WALL		

- GENERAL NOTES:**
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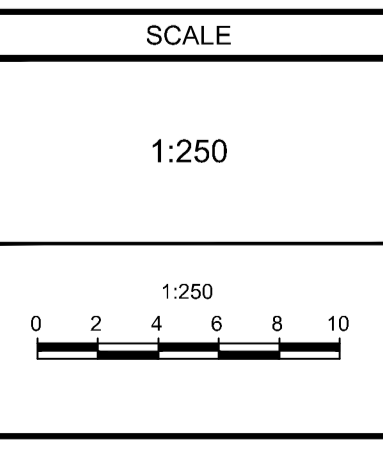
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- WATER SERVICE IS TO BE CONSTRUCTED TO WITHIN 1.0m OF FOUNDATION WALL AND CAPPED, UNLESS OTHERWISE INDICATED.
- WATER DEMAND = TBD

NOTE: THE POSITION OF ALL POLE LINES, CONDUITS, WATERMANS, SEWERS AND OTHER UNDERGROUND AND OVERGROUND UTILITIES AND STRUCTURES IS NOT NECESSARILY SHOWN ON THE CONTRACT DRAWINGS, AND WHERE SHOWN, THE ACCURACY OF THE POSITION OF SUCH UTILITIES AND STRUCTURES IS NOT GUARANTEED. BEFORE STARTING WORK, DETERMINE THE EXACT LOCATION OF ALL SUCH UTILITIES AND STRUCTURES AND ASSUME ALL LIABILITY FOR DAMAGE TO THEM.

Owner:
Wesley Clover International
c/o Richard Goldstein
KRP Properties
300-555 Leggett Drive, Tower B,
Kanata, ON K2K 2X3

No.	REVISION	DATE	BY
1.	ISSUED WITH ZONING AND SITE PLAN APPLICATION	OCT 01/21	GJM



FOR REVIEW ONLY

DESIGN	GJM
CHECKED	GJM
DRAWN	RJG
CHECKED	GJM
APPROVED	GJM

NOVATECH
Engineers, Planners & Landscape Architects
Suite 200, 240 Michael Cowland Drive
Ottawa, Ontario, Canada K2M 1R6
Telephone: (613) 254-9643
Facsimile: (613) 254-5867
Website: www.novatech-eng.com

LOCATION
CITY OF OTTAWA
BROOKSTREET APARTMENTS

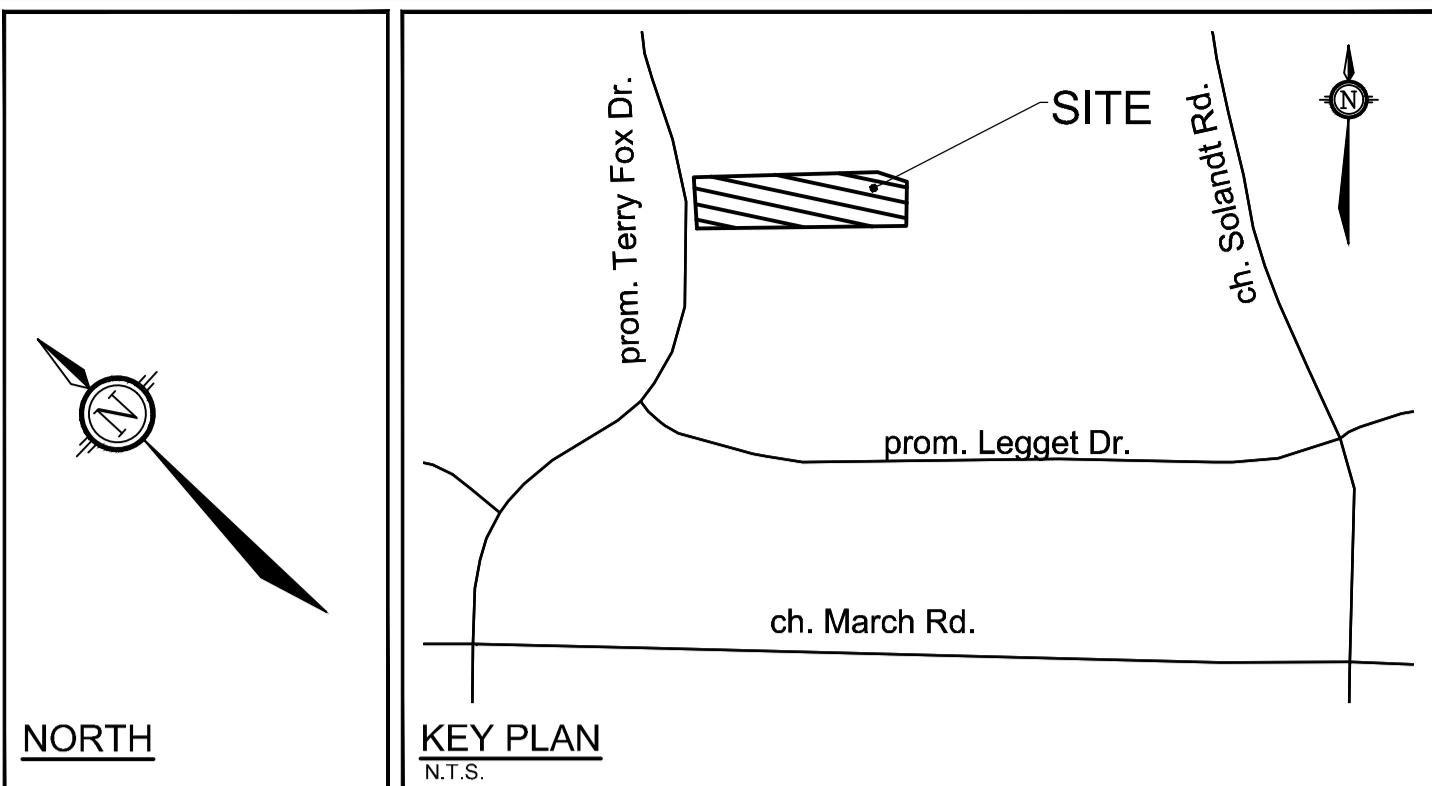
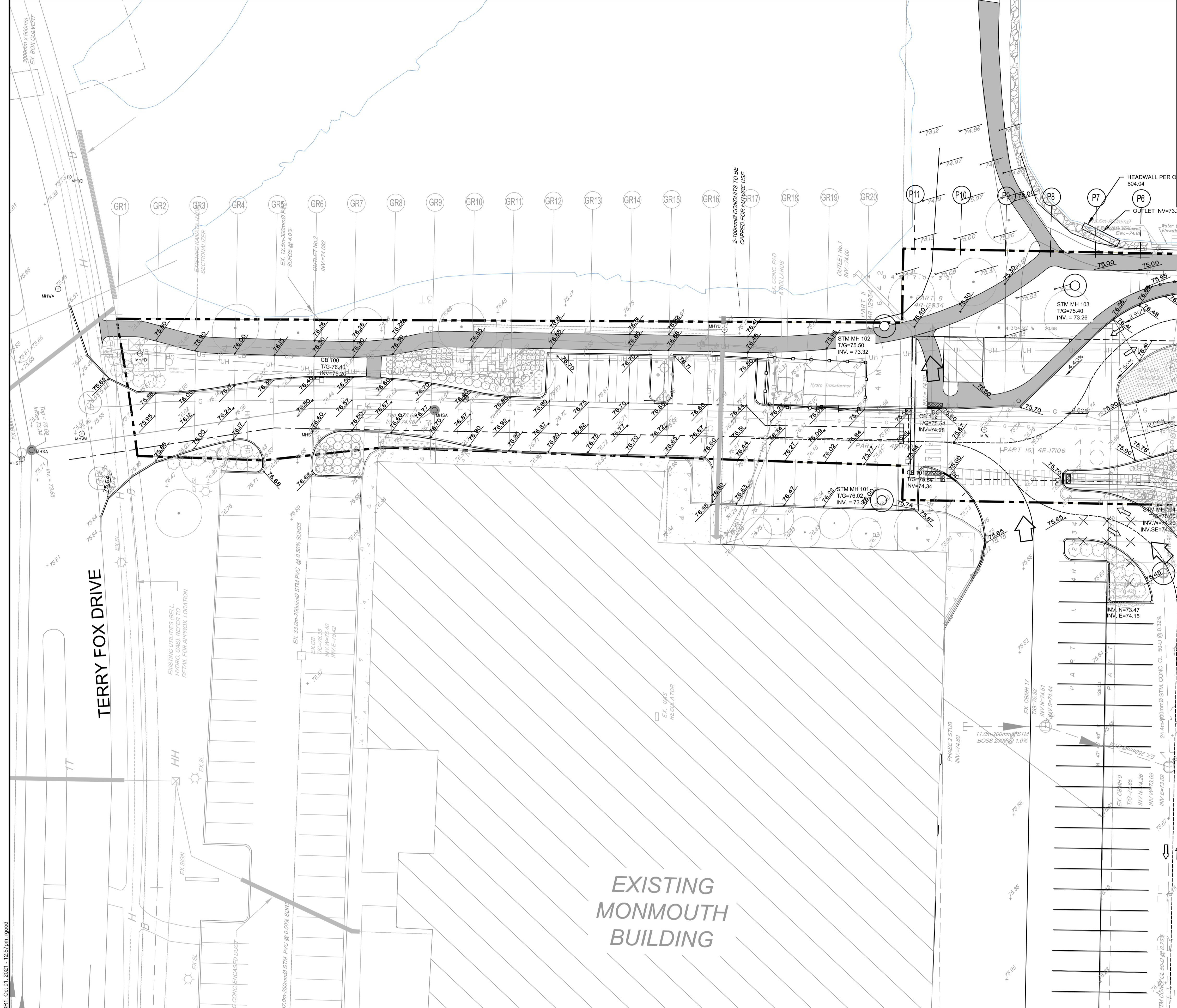
DRAWING NAME
GENERAL PLAN OF SEVICES

PROJECT No.
120202-00

REV
REV 1

DRAWING No.
120202-GP2

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LEGEND

- PROPOSED PROPERTY LINE
- PROPOSED RETAINING WALL
- PROPOSED ELEVATION
- EXISTING TERRACE
- PROPOSED TERRACE GRADING 3:1 MAX
- PROPOSED TACTILE WALKING SURFACE INDICATOR (TWSI)

PAVEMENT STRUCTURE:

- PARKING STALLS
50mm HL3 OR SUPERPAVE 12.5
150mm GRAN "A"
300mm GRAN "B"
- DRIVING AISLES
40mm HL3 OR SUPERPAVE 12.5
50mm HL8 OR SUPERPAVE 19.0
150mm GRAN "A"
450mm GRAN "B"

- NOTES**
- GENERAL NOTES:**
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SCALE

1:250

DESIGN	GJM
CHECKED	GJM
DRAWN	RJG
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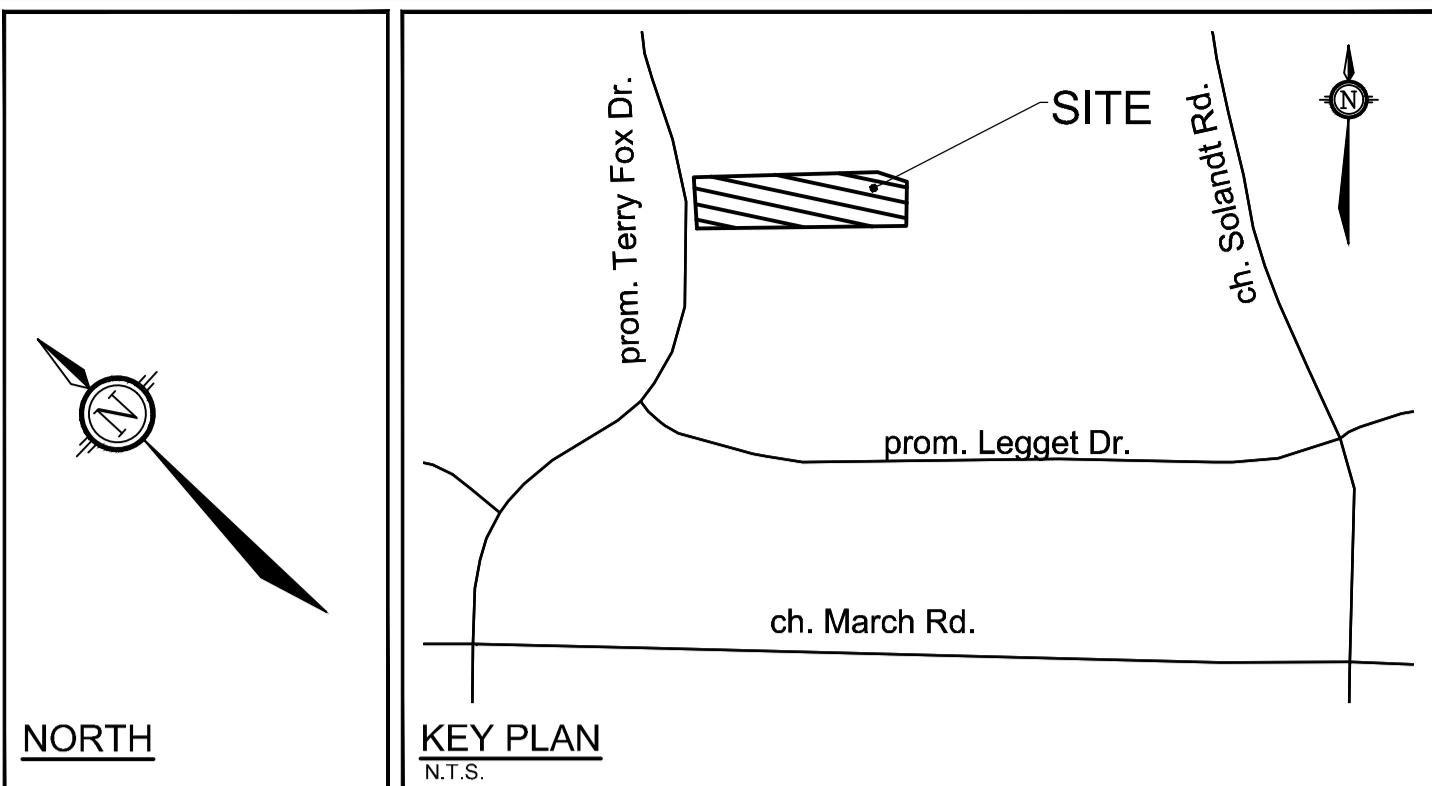
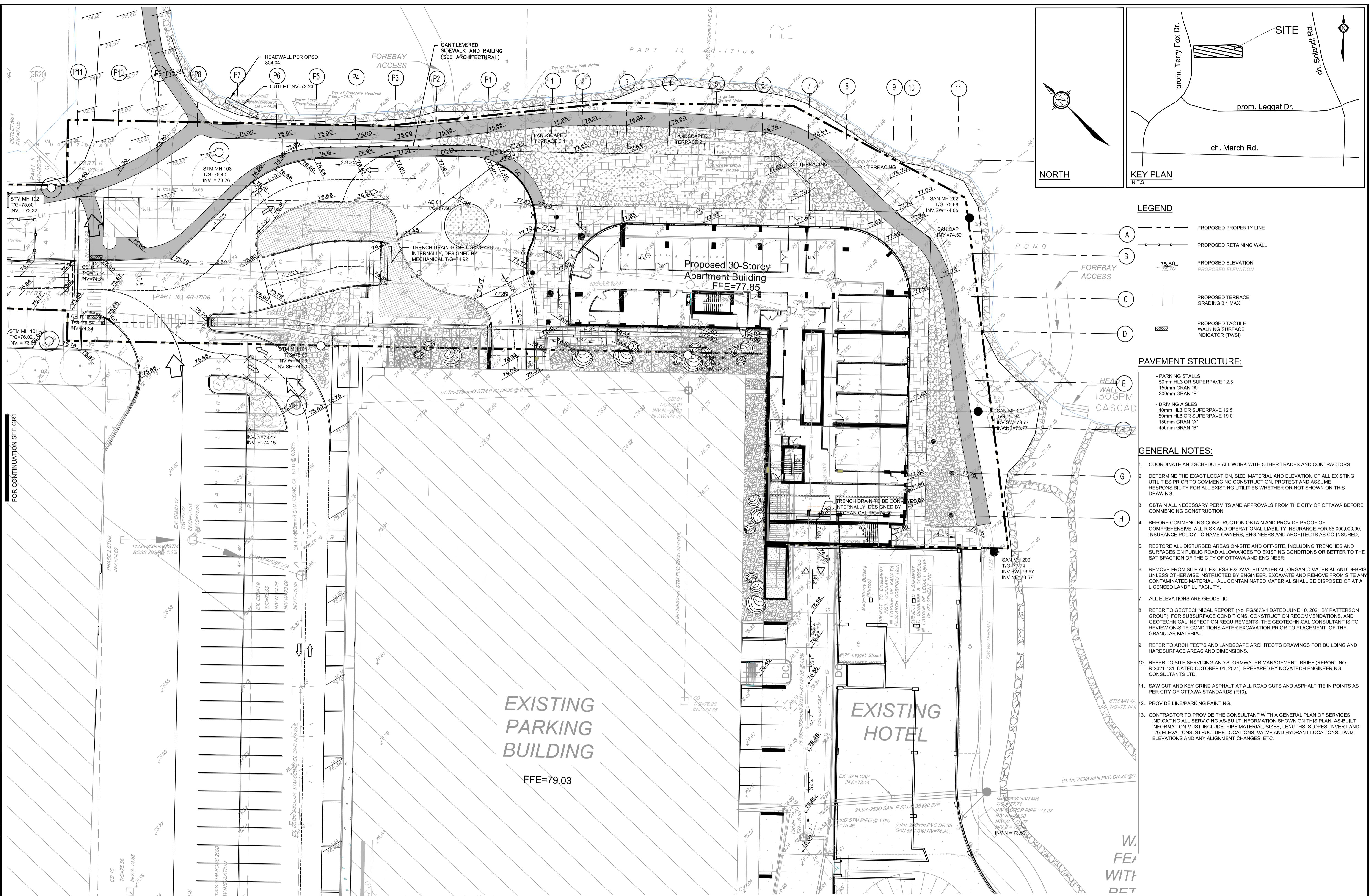
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LOCATION CITY OF OTTAWA BROOKSTREET APARTMENTS	PROJECT No. 120202-00
DRAWING NAME GRADING PLAN	REV REV 1
	DRAWING No. 120202-GR1

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- LEGEND**
- (A) --- PROPOSED PROPERTY LINE
 - (B) --- PROPOSED RETAINING WALL
 - (C) --- PROPOSED ELEVATION
 - (D) --- PROPOSED TERRACE GRADING 3:1 MAX
 - (E) --- PROPOSED TACTILE WALKING SURFACE INDICATOR (TWSI)

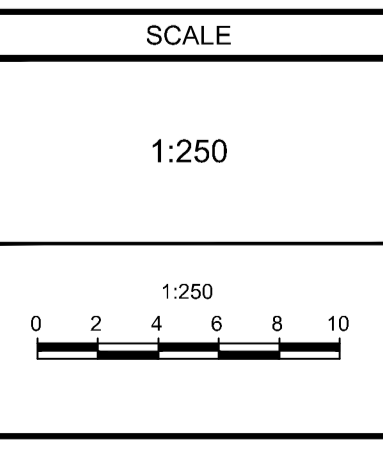
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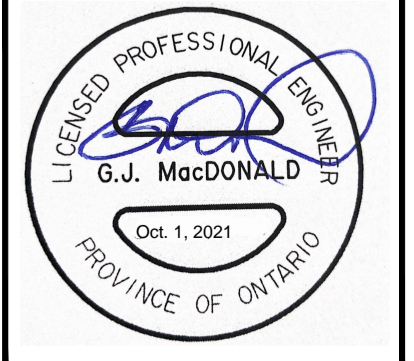
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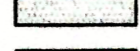


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LOCATION CITY OF OTTAWA BROOKSTREET APARTMENTS	
DRAWING NAME GRADING PLAN	PROJECT No. 120202-00
	REV REV.1
	DRAWING No. 120202-GR2

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APPENDIX B
Storm Sewer Design Sheet and Drawing

LEGEND

-  KANATA RESEARCH PARK STORM DRAINAGE AREAS
-  SUBWATERSHED BOUNDARY; REFER TO "SHIRLEY'S BROOK & WATTS CREEK SUBWATERSHED STUDY" (DILLON 1998)
-  CATCHMENT AREA; REFER TO "SHIRLEY'S BROOK & WATTS CREEK SUBWATERSHED STUDY" (DILLON 1998)
-  WETLAND
-  EXISTING WETLAND
-  CONCEPTUAL STORM OUTLET
-  STORM OUTLET
-  FUTURE DEVELOPMENT BUFFER
-  FUTURE DEVELOPMENT AREA
-  GOLF COURSE FEATURES (TEES, FAIRWAYS, GREENS)
-  PROPOSED STORMWATER MANAGEMENT POND
-  PROPOSED WETLAND
-  EXISTING WETLAND
-  PROPOSED LAKE

S-7
163

S-6
124

5
12.5

W-5
388

K-3
353

K-2
300

S-6
124

S-4
324

3
40.6

10
6.5

3
25.5

9
8.1

8
2.9

6
9.5

1
19.9

STORMWATER MANAGEMENT TECHNIQUE		
AREA	QUANTITY	QUALITY
1	POND 1	POND 1
2	POND 2	POND 2 & TURF MANAGEMENT
3	POND 3	POND 3
4	DUCK POND	DUCK POND
5	NOT REQ'D	TURF MANAGEMENT
6	NOT REQ'D	TURF MANAGEMENT
7	NOT REQ'D	TURF MANAGEMENT
8	POND 2	POND 2 & OIL & GRIT SEPARATOR
9	ON-SITE	ON-SITE
10	POND 3	POND 3 & OIL & GRIT SEPARATOR
11	NOT REQ'D	TURF MANAGEMENT

KANATA RESEARCH PARK

Kanata Research Park Corporation
555 Legget Drive, Suite 200, Kanata, Ontario, Canada, K2K 2K3
(613) 591-8594

**STORMWATER MANAGEMENT
CONCEPT PLAN
93063-SWM2**

KANATA RESEARCH PARK CORPORATION
CITY OF KANATA
REGIONAL MUNICIPALITY OF OTTAWA-CARLETON
APRIL 2000

SCALE 1 : 4000



ENGINEERING CONSULTANTS LTD.
OTTAWA, ONTARIO

Calculation Summary

Project: 120202

Brookstreet Apartment Building

Additional Volume:

1600m² additional impervious area

$$V = CA d$$

$$V = (0.9) \times (1330m^2) \times (100mm \text{ rainfall})$$

$$V = 144 m^3$$

Pond Impacts:

$$\begin{aligned} \text{Volume Increase} &= \frac{\text{Added Volume}}{\text{Existing Volume}} \\ &= \frac{144m^3}{5210m^3} \\ &= 0.027 \end{aligned}$$

$$\text{Depth Increase, } d = \frac{\text{Added Volume}}{\text{Surface Area}}$$

$$d = \frac{144m^3}{15,000m^2}$$

$$d = 9.6 \text{ mm}$$



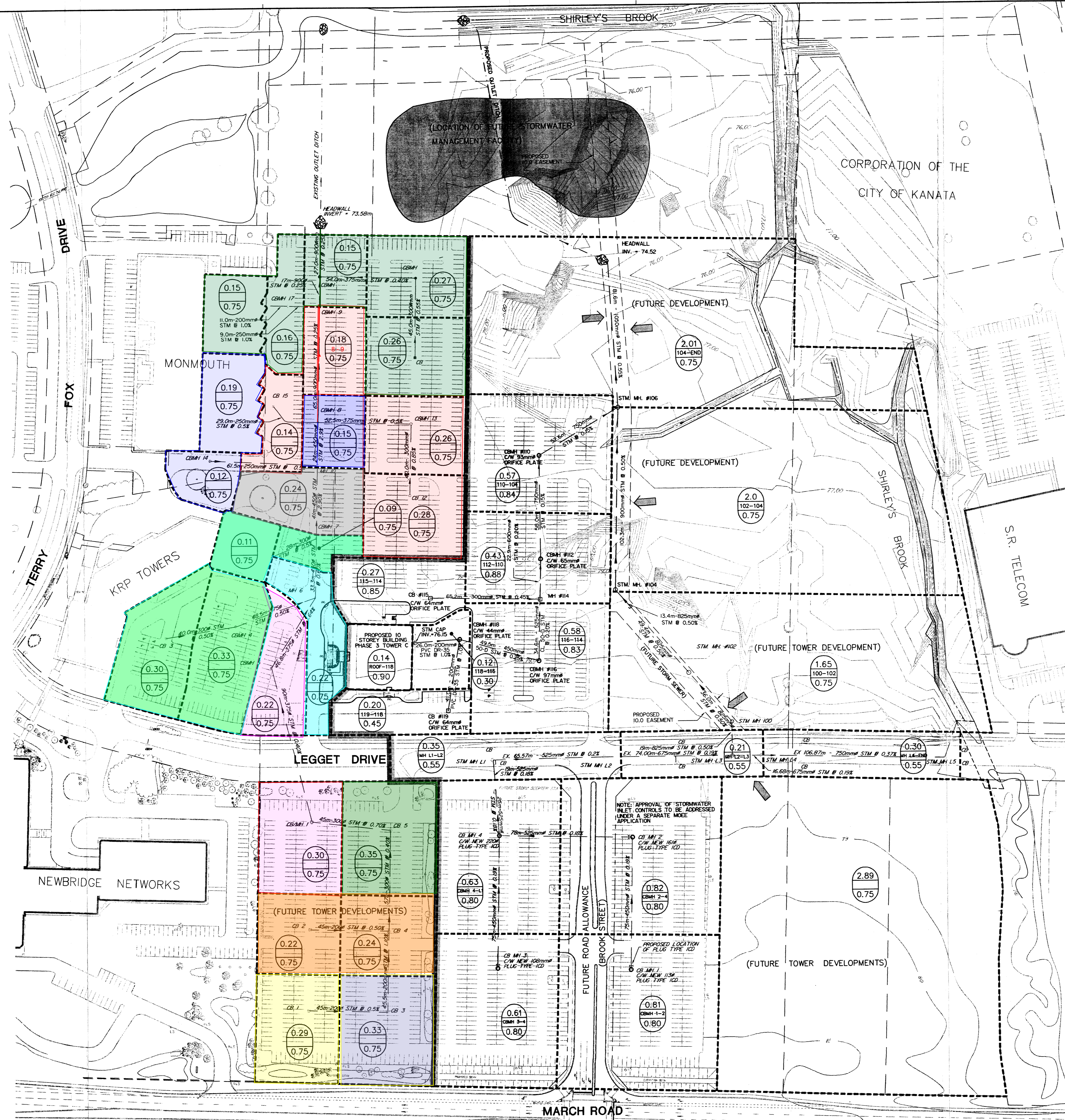
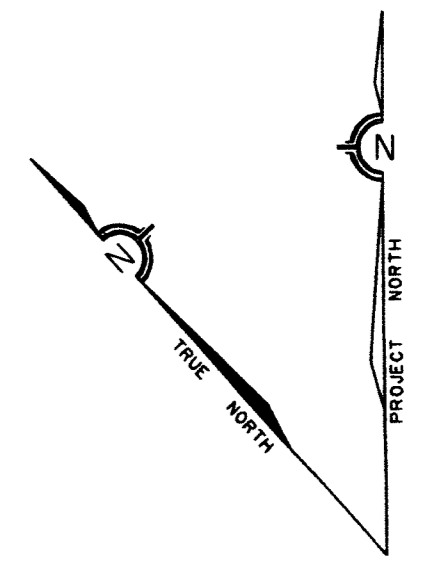
Storm Sewer Design Sheet

LOCATION			FLOW								PROPOSED SEWER											
STREET	FROM	TO	AREA ID	R= 0.25	R= 0.55	R= 0.75	R= 0.90	INDIV 2.78 AR	ACCUM 2.78 AR	TIME OF CONC.	RAINFALL INTENSITY I	PEAK FLOW Q (l/s)	NOMINAL SIZE (mm)	PIPE SIZE (mm)	PIPE SLOPE (%)	LENGTH (m)	CAPACITY (l/s)	FULL FLOW VELOCITY (m/s)	TIME OF FLOW (min.)	EXCESS CAPACITY (l/s)	Q/Qfull	
	CB1	CB2	Refer to 98066-STM			0.290		0.60	0.60	10.00	104.19	63.00	200	203	0.50	45.0	24.22	0.75	1.01	-38.78	2.60	
	CB3	CB4				0.330		0.69	0.69	11.01	99.17	68.23	200	203	1.10	45.5	35.92	1.11	0.69	-32.31	1.90	
	CB4	CB5				0.460		0.96	1.65	11.69	96.04	158.19	300	305	0.40	57.0	63.87	0.87	1.09	-94.32	2.48	
	CB5	CBMH1				0.350		0.73	2.38	12.78	91.50	217.49	300	305	0.70	45.0	84.49	1.16	0.65	-133.00	2.57	
	CBMH1	CBMH5				0.520		1.08	3.46	13.43	89.02	308.09	375	381	0.40	90.0	115.80	1.01	1.48	-192.29	2.66	
	CBMH5	MH6				0.220		0.46	3.92	14.90	83.87	328.75	375	381	0.64	46.8	146.48	1.28	0.61	-182.28	2.24	
	MH6	CBMH7				0.630		1.73	5.65	15.51	81.94	462.99	450	457	0.60	33.3	230.62	1.40	0.40	-232.37	2.01	
	CBMH7	MH10				0.240		0.50	6.15	15.91	80.74	496.60	450	457	2.90	41.0	507.02	3.09	0.22	10.43	0.98	
	MH10	CBMH8				0.460		0.96	7.11	16.13	80.08	569.36	450	457	2.90	24.0	507.02	3.09	0.13	-62.34	1.12	
	CBMH8	CBMH9				0.860		1.79	8.90	16.26	79.70	709.58	900	914	0.25	65.0	945.25	1.44	0.75	235.67	0.75	
	CBMH9	CBMH100	Refer to 120202-STM			0.990		2.06	10.97	17.01	77.58	850.78	900	914	0.32	24.4	1069.42	1.63	0.25	218.64	0.80	
	CBMH100	STM MH 101				0.150		0.31	11.28	17.26	76.90	867.40	975	991	0.24	36.9	1146.51	1.49	0.41	279.11	0.76	
	STM MH 101	STM MH102				0.000	0.110	0.28	11.56	17.68	75.80	875.93	975	991	0.24	22.1	1146.51	1.49	0.25	270.58	0.76	
	STM MH 102	STM MH103				0.000		0.00	11.56	17.92	75.17	868.55	975	991	0.24	24.7	1146.51	1.49	0.28	277.96	0.76	
	STM MH103	OUTLET				0.000		0.00	11.56	18.20	74.47	860.47	975	991	0.24	7.7	1146.51	1.49	0.09	286.04	0.75	

Definitions
 Q = 2.78 AIR
 Q = Peak Flow, in Litres per second (L/s)
 A = Area in hectares (ha)
 I = Rainfall Intensity (mm/h)

Notes:
 1) Ottawa Rainfall-Intensity Curve
 2) Min Velocity = 0.80 m/sec.

Reference Plans
 Drawing No. 98066-STM Rev. 2
 Drawing No. 120202-STM Rev. 1



- LEGEND**
- 2.02 DRAINAGE AREA (hectares)
 - 100-102 MANHOLE TO MANHOLE
 - 0.6 RUN-OFF COEFFICIENT
 - STORM DRAINAGE AREA
 - STORM DRAINAGE AREA BOUNDARY
 - MH #100 EXISTING STORM SEWER AND MANHOLE
 - CBM# #116 EXISTING CATCHBASIN MANHOLE
 - CB #119 EXISTING CATCHBASIN
 - DIRECTION OF FLOW
 - ← MINOR STORM SYSTEM FLOW ROUTING (UNDEVELOPED AREAS)

- NOTE:**
1. RUNOFF COEFFICIENTS FOR TOWER 'C' PHASE 3 DEVELOPMENT ARE AS OUTLINED IN 'KANATA RESEARCH PARK - TOWER 'C' STORMWATER MANAGEMENT REPORT' (NECL, Dec 1998)
 2. APPROVAL OF STORMWATER INLET CONTROLS FOR THE EXISTING NEWBRIDGE PARKING LOT (PLUG TYPE ICD'S) TO BE ADDRESSED UNDER A SEPARATE MOEE APPLICATION.

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 Kanata Research Park
 Corporation
 555 Legget Drive, Suite 300, Kanata, Ontario, Canada, K1R 3T3
 416-811-1114

No.	REVISION	DATE	BY
2	REVISED STORM SEWER PER R.M.O.C. COMMENTS	APR. 15/99	OSH
1	ISSUED FOR COMMENTS	DEC. 11/98	OSH

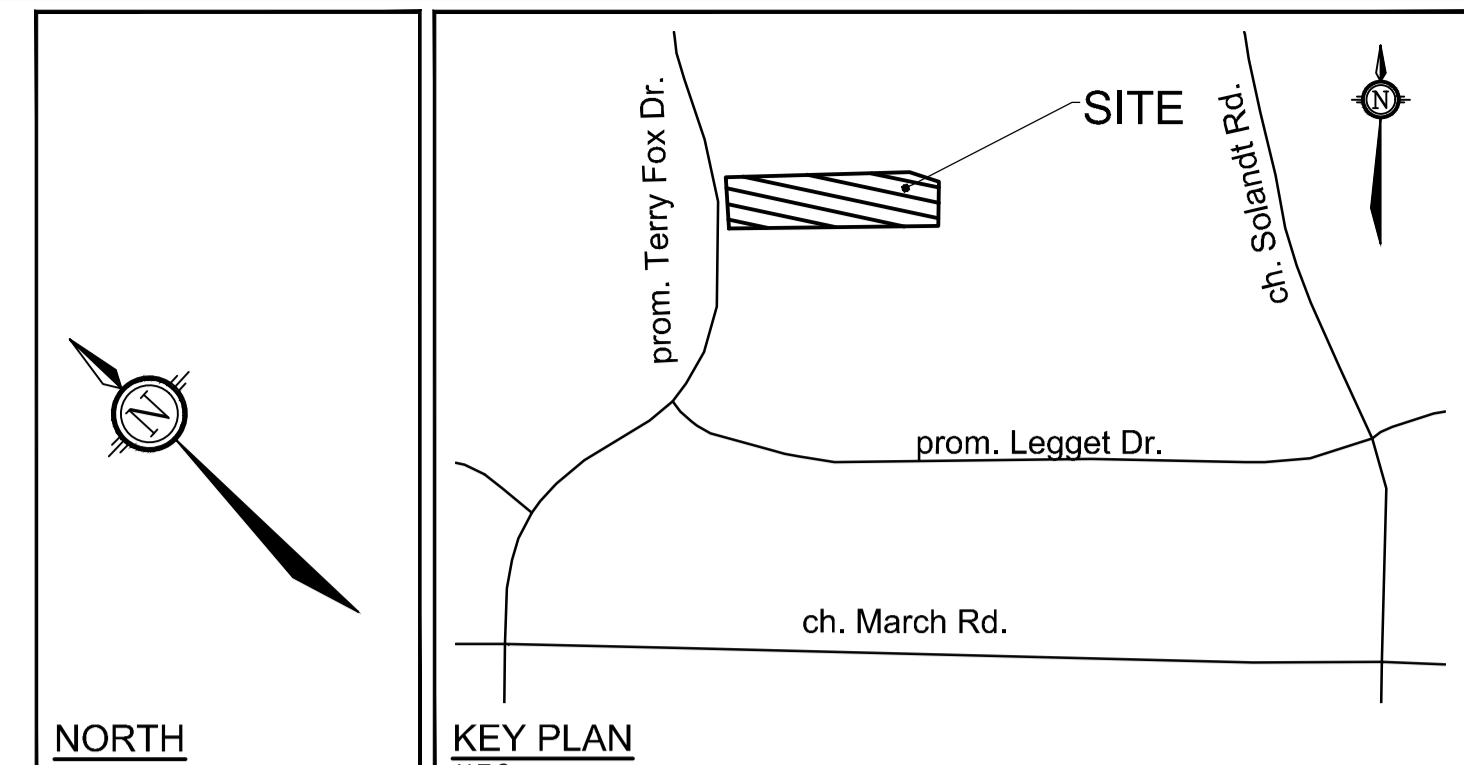
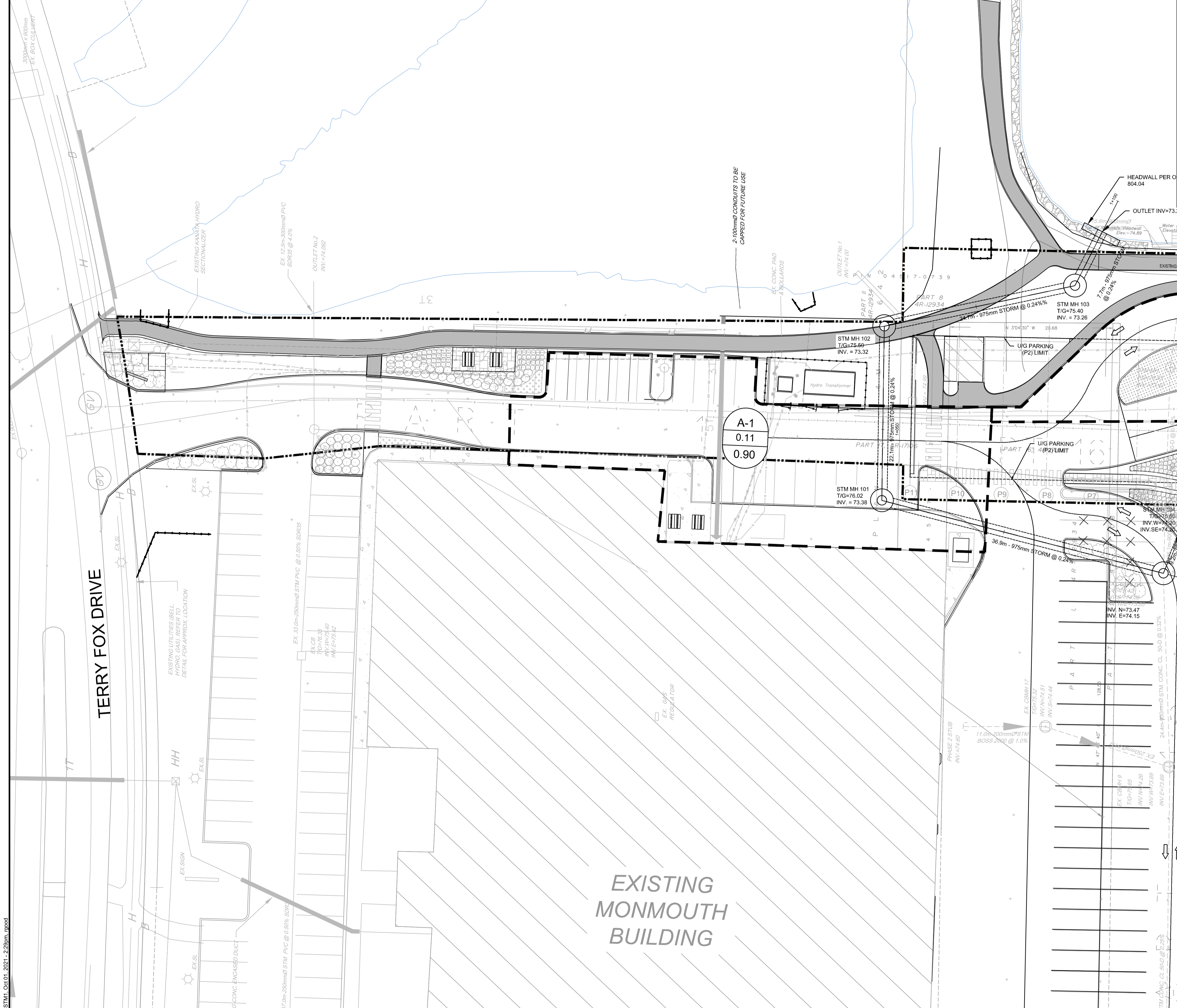


Novatech
 CONSULTING ENGINEERS & PLANNERS
 Suite 17, 77 Auriga Drive
 Nepean, Ontario
 K2E 7Z7
 Telephone: (613) 727-1658
 Facsimile: (613) 727-6972

DESIGN	SCALE
OSH	1:1000
UB	
DU	
GSH	
UB	

CITY OF KANATA
**KANATA RESEARCH PARK
 TOWER 'C' PROJECT**
STORM DRAINAGE AREA PLAN

PROJECT No.	DATE	DRAWING No.
98066	SEPTEMBER 1998	98066-STM



LEGEND

	PROPOSED PROPERTY LINE		EXISTING STORM MANHOLE AND SEWER
	PROPOSED STORM MANHOLE AND SEWER		EXISTING CATCHBASIN MANHOLE AND SEWER
	PROPOSED STORM DRAINAGE AREA		DIRECTION OF MAJOR OVERLAND FLOW ROUTE
	DRAINAGE AREA ID		
	DRAINAGE AREA (HECTARES)		
	RUNOFF COEFFICIENT		

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 - CONTRACTOR TO PROVIDE THE CONSULTANT WITH A GENERAL PLAN OF SERVICES INDICATING ALL SERVICING AS-BUILT INFORMATION SHOWN ON THIS PLAN. AS-BUILT INFORMATION MUST INCLUDE: PIPE MATERIAL, SIZES, LENGTHS, SLOPES, INVERT AND TIG ELEVATIONS, STRUCTURE LOCATIONS, VALVE AND HYDRANT LOCATIONS, TWM ELEVATIONS AND ANY ALIGNMENT CHANGES, ETC.

SEWER NOTES:

- SPECIFICATIONS:

ITEM	SPEC. No.	REFERENCE
CATCHBASIN (600x600mm)	705.010	OPSD
STORM / SANITARY MANHOLE (1200Ø)	701.010	OPSD
CB, FRAME & COVER	400.020	OPSD
STORM / SANITARY MH FRAME & COVER	401.010	OPSD
SEWER TRENCH - BEDDING (GRANULAR A)		
COVER (GRANULAR A OR GRANULAR B TYPE I, WITH MAXIMUM PARTICLE SIZE=25mm)		
STORM SEWER	PVC DR 35	
SANITARY SEWER	PVC DR 35	
CATCHBASIN LEAD	PVC DR 35	
- INSULATE ALL PIPES (SAN/STM) THAT HAVE LESS THAN 1.5m COVER WITH 50mmX1200mm HI-40 INSULATION. PROVIDE 150mm CLEARANCE BETWEEN PIPE AND INSULATION.
- SERVICES ARE TO BE CONSTRUCTED TO 1.0m FROM FACE OF BUILDING AT A MINIMUM SLOPE OF 1.0%.
- PIPE BEDDING, COVER AND BACKFILL ARE TO BE COMPACTED TO AT LEAST 95% OF THE STANDARD PROCTOR MAXIMUM DRY DENSITY. THE USE OF CLEAR CRUSHED STONE AS A BEDDING LAYER SHALL NOT BE PERMITTED.
- FLEXIBLE CONNECTIONS ARE REQUIRED FOR CONNECTING PIPES TO MANHOLES (FOR EXAMPLE KOR-N-SEAL, PSX POSITIVE SEAL AND DURASEAL). THE CONCRETE CRADLE FOR THE PIPE CAN BE ELIMINATED.
- THE OWNER SHALL REQUIRE THAT THE SITE SERVICING CONTRACTOR PERFORM FIELD TESTS FOR QUALITY CONTROL OF ALL SANITARY SEWERS. LEAKAGE TESTING SHALL BE COMPLETED IN ACCORDANCE WITH OPSS 410.07.16, 410.07.16.04 AND 407.07.24. DYE TESTING IS TO BE COMPLETED ON ALL SANITARY SERVICES TO CONFIRM PROPER CONNECTION TO THE SANITARY SEWER MAIN. THE FIELD TESTS SHALL BE PERFORMED IN THE PRESENCE OF A CERTIFIED PROFESSIONAL ENGINEER WHO SHALL SUBMIT A CERTIFIED COPY OF THE TEST RESULTS.
- STORM MANHOLES AND CBMHS ARE TO HAVE 300mm SLUMPS UNLESS OTHERWISE INDICATED.
- CONTRACTOR TO TELEPHONE (CCTV) ALL PROPOSED SEWERS, 200mmØ OR GREATER PRIOR TO BASE COURSE ASPHALT. UPON COMPLETION OF CONTRACT, THE CONTRACTOR IS RESPONSIBLE TO FLUSH AND CLEAN ALL SEWERS & APPURTENANCES.

NOTE: THE POSITION OF ALL POLE LINES, CONDUITS, WATERMANS, SEWERS AND OTHER UNDERGROUND AND OVERGROUND UTILITIES AND STRUCTURES IS NOT NECESSARILY SHOWN ON THE CONTRACT DRAWINGS, AND WHERE SHOWN, THE ACCURACY OF THE POSITION OF SUCH UTILITIES AND STRUCTURES IS NOT GUARANTEED. BEFORE STARTING WORK, DETERMINE THE EXACT LOCATION OF ALL SUCH UTILITIES AND STRUCTURES AND ASSUME ALL LIABILITY FOR DAMAGE TO THEM.

Owner:
Wesley Clover International
c/o Richard Goldstein
KRP Properties
300-555 Legget Drive, Tower B,
Kanata, ON K2K 2X3

No.	REVISION	DATE	BY
1.	ISSUED WITH ZONING AND SITE PLAN APPLICATION	OCT 01/21	GJM

FOR REVIEW ONLY

SCALE: 1:250

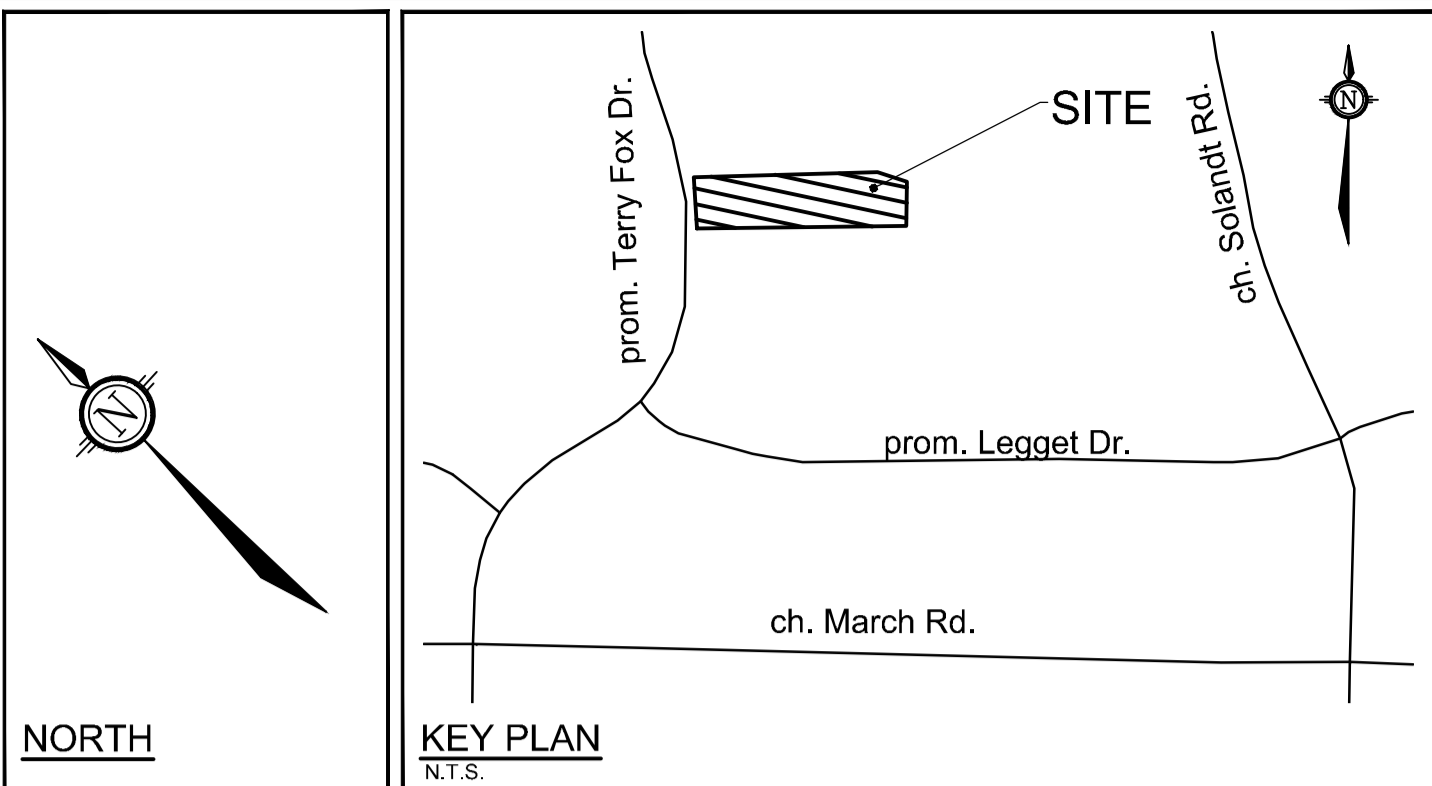
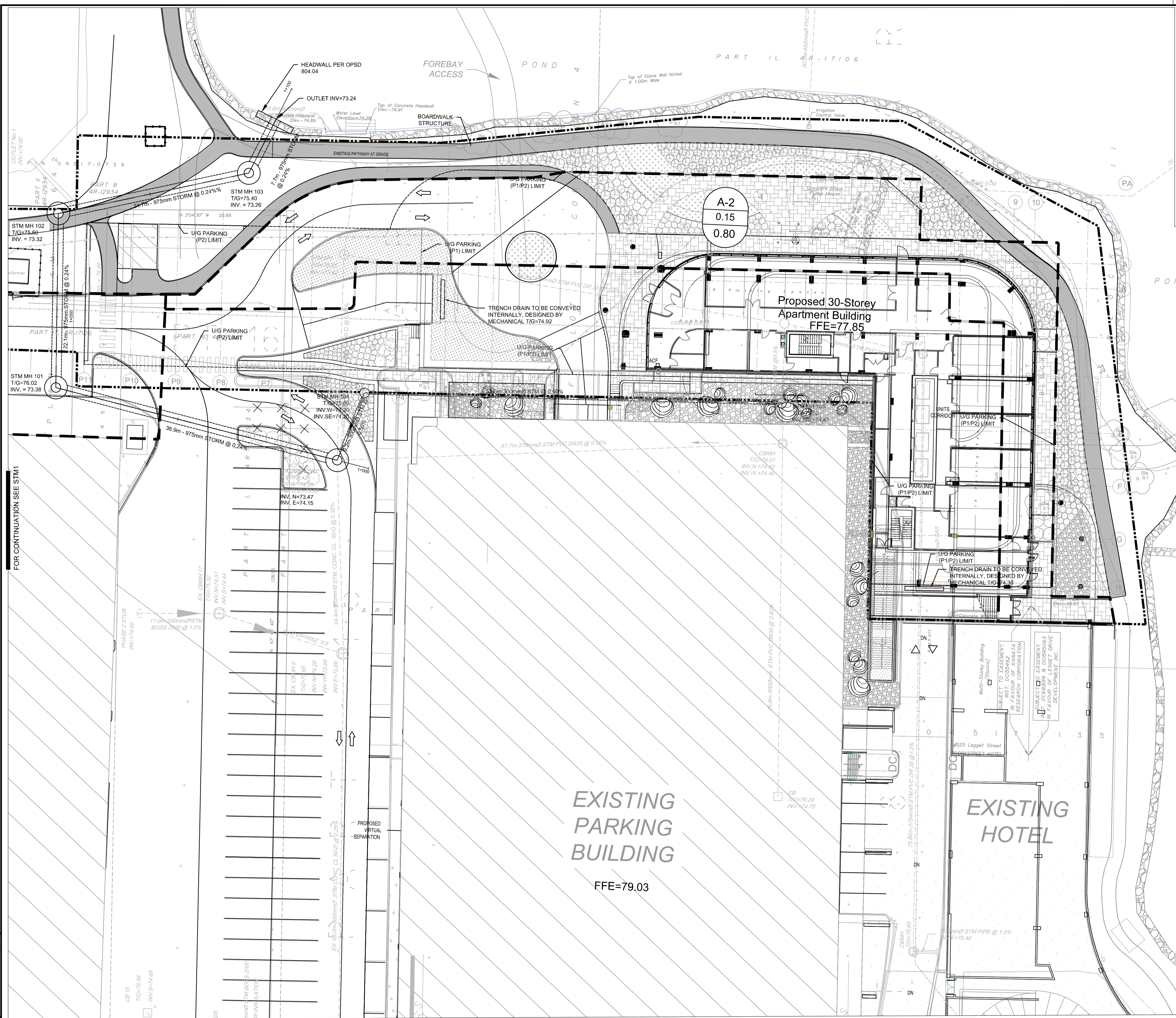
DESIGN: GJM
CHECKED: GJM
DRAWN: RJG
CHECKED: GJM
APPROVED: GJM

Professional Engineer Seal: G.J. MacDONALD, Oct 1, 2021

NOVATECH
Engineers, Planners & Landscape Architects
Suite 200, 240 Michael Cowpland Drive
Ottawa, Ontario, Canada K2M 1P6
Telephone: (613) 254-9643
Facsimile: (613) 254-5867
Website: www.novatech-eng.com

LOCATION CITY OF OTTAWA BROOKSTREET APARTMENTS	PROJECT No. 120202-00
DRAWING NAME STORM DRAINAGE AREA PLAN	REV REV 1
	DRAWING No. 120202-STM1

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LEGEND

	PROPOSED PROPERTY LINE		EXISTING STORM MANHOLE AND SEWER
	PROPOSED STORM MANHOLE AND SEWER		EXISTING STORM MANHOLE AND SEWER
	PROPOSED STORM DRAINAGE AREA		EXISTING CATCHBASIN MANHOLE AND SEWER
	DRAINAGE AREA ID		DIRECTION OF MAJOR OVERLAND FLOW ROUTE
	DRAINAGE AREA (HECTARES)		
	RUNOFF COEFFICIENT		

- NOTES**
- GENERAL NOTES:**
- COORDINATE AND SCHEDULE ALL WORK WITH OTHER TRADES AND CONTRACTORS.
 - DETERMINE THE EXACT LOCATION, SIZE, MATERIAL AND ELEVATION OF ALL EXISTING UTILITIES PRIOR TO COMMENCING CONSTRUCTION. PROTECT AND ASSUME RESPONSIBILITY FOR ALL EXISTING UTILITIES WHETHER OR NOT SHOWN ON THIS DRAWING.
 - OBTAIN ALL NECESSARY PERMITS AND APPROVALS FROM THE CITY OF OTTAWA BEFORE COMMENCING CONSTRUCTION.
 - BEFORE COMMENCING CONSTRUCTION OBTAIN AND PROVIDE PROOF OF COMPREHENSIVE, ALL RISK AND OPERATIONAL LIABILITY INSURANCE FOR \$5,000,000.00, INSURANCE POLICY TO NAME OWNERS, ENGINEERS AND ARCHITECTS AS CO-INSURED. (amount of liability insurance to be verified on a project by project basis)
 - RESTORE ALL DISTURBED AREAS ON-SITE AND OFF-SITE, INCLUDING TRENCHES AND SURFACES ON PUBLIC ROAD ALLOWANCES TO EXISTING CONDITIONS OR BETTER TO THE SATISFACTION OF THE CITY OF OTTAWA AND ENGINEER.
 - REMOVE FROM SITE ALL EXCESS EXCAVATED MATERIAL, ORGANIC MATERIAL AND DEBRIS UNLESS OTHERWISE INSTRUCTED BY ENGINEER. EXCAVATE AND REMOVE FROM SITE ANY CONTAMINATED MATERIAL. ALL CONTAMINATED MATERIAL SHALL BE DISPOSED OF AT A LICENSED LANDFILL FACILITY.
 - ALL ELEVATIONS ARE GEODETIC.
 - REFER TO GEOTECHNICAL REPORT (No. PG5673-1 DATED JUNE 10, 2021 BY PATTERSON GROUP) FOR SUBSURFACE CONDITIONS, CONSTRUCTION RECOMMENDATIONS, AND GEOTECHNICAL INSPECTION REQUIREMENTS. THE GEOTECHNICAL CONSULTANT IS TO REVIEW ON-SITE CONDITIONS AFTER EXCAVATION PRIOR TO PLACEMENT OF THE GRANULAR MATERIAL.
 - REFER TO ARCHITECT'S AND LANDSCAPE ARCHITECT'S DRAWINGS FOR BUILDING AND HARDSURFACE AREAS AND DIMENSIONS.
 - REFER TO SITE SERVICING AND STORMWATER MANAGEMENT BRIEF (REPORT NO. R-2021-131, DATED OCTOBER 01, 2021) PREPARED BY NOVATECH ENGINEERING CONSULTANTS LTD.
 - SAW CUT AND KEY GRIND ASPHALT AT ALL ROAD CUTS AND ASPHALT TIE IN POINTS AS PER CITY OF OTTAWA STANDARDS (R10).
 - PROVIDE LINE/PARKING PAINTING.
 - CONTRACTOR TO PROVIDE THE CONSULTANT WITH A GENERAL PLAN OF SERVICES INDICATING ALL SERVICING AS-BUILT INFORMATION SHOWN ON THIS PLAN. AS-BUILT INFORMATION MUST INCLUDE: PIPE MATERIAL, SIZES, LENGTHS, SLOPES, INVERT AND TIG ELEVATIONS, STRUCTURE LOCATIONS, VALVE AND HYDRANT LOCATIONS, TWM ELEVATIONS AND ANY ALIGNMENT CHANGES, ETC.

SEWER NOTES:

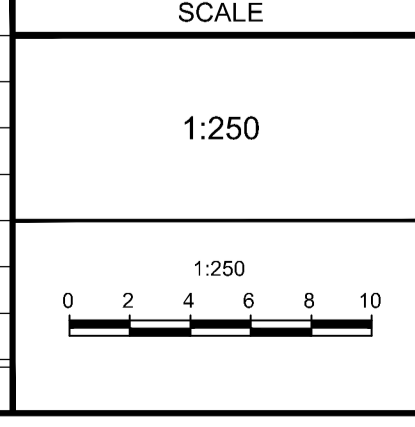
- SPECIFICATIONS:

ITEM	SPEC. No.	REFERENCE
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COVER (GRANULAR A OR GRANULAR B TYPE I, WITH MAXIMUM PARTICLE SIZE=25mm)		
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- CONTRACTOR TO TELEVIEW (CCTV) ALL PROPOSED SEWERS, 200mmØ OR GREATER PRIOR TO BASE COURSE ASPHALT. UPON COMPLETION OF CONTRACT, THE CONTRACTOR IS RESPONSIBLE TO FLUSH AND CLEAN ALL SEWERS & APURTENANCES.

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Owner:
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KRP Properties
300-555 Leggett Drive, Tower B,
Kanata, ON K2K 2X3

No.	REVISION	DATE	BY
1.	ISSUED WITH ZONING AND SITE PLAN APPLICATION	OCT 01/21	GJM



FOR REVIEW ONLY

DESIGN	GJM
CHECKED	GJM
DRAWN	RJG
CHECKED	GJM
APPROVED	GJM

NOVATECH
Engineers, Planners & Landscape Architects
Suite 200, 240 Michael Cowpland Drive
Ottawa, Ontario, Canada K2M 1R6

Telephone (613) 254-9643
Facsimile (613) 254-5867
Website www.novatech-eng.com

LOCATION
CITY OF OTTAWA
BROOKSTREET APARTMENTS

DRAWING NAME
STORM AREA DRAINAGE PLAN

PROJECT No.
120202-00

REV
REV 1

DRAWING No.
120202-STM2

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APPENDIX C
Sanitary Sewer Design Sheet

SANITARY TRUNK SEWER
Sanitary Sewer Design Sheet
Brookstreet Apartments



PROJECT : 120202
 DESIGNED BY: GMAC
 DATE: Sept. 23, 2021

LOCATION			INDIVIDUAL		CUMULATIVE		PEAK FLOWS			PROPOSED SEWER							
AREA	FROM MH	TO MH	FLOW RATE (L/s)	Infiltration Area (ha)	FLOW RATE (L/s)	Infiltration Area (ha)	PEAK FACTOR M	PEAK FLOW Q (p) (L/s)	PEAK EXTRAN.FLOW Q(i) (L/s)	PEAK DESIGN FLOW Q (d) (L/s)	LENGTH (m)	PIPE SIZE (mm)	TYPE OF PIPE	GRADE %	CAPACITY (L/s)	FULL FLOW VELOCITY (m/s)	
528 March Road Site	SAN MH 4	EX. SAN MH A	0.35	2.20	0.35	2.20	5.7	2.00	0.62	2.61	25.4	250	PVC	0.50	43.87	0.87	
Legget Drive	EX. SAN MH A	EX. SAN MH B	0.00	0.00	0.35	2.20	5.7	2.00	0.62	2.61	55.1	250	PVC	0.33	35.64	0.70	
Legget Drive (Newbridge)	EX. SAN MH	EX. SAN MH C	1.69	4.05	1.69	4.05	1.5	2.54	1.13	3.67	60.3	250	PVC	0.31	34.54	0.68	
Legget Drive	EX. SAN MH C	EX. SAN MH B	0.00	0.00	1.69	4.05	1.5	2.54	1.13	3.67	68.0	250	PVC	0.29	33.41	0.66	
**	Legget Drive	EX. SAN MH B	SAN MH 3	0.00	0.00	2.04	6.25	1.5	3.06	1.75	4.81	26.7	250	PVC	0.25	31.02	0.61
*	KRP Site	SAN MH 3	SAN MH 2	0.00	0.00	2.04	6.25	1.5	3.06	1.75	4.81	50.4	250	PVC	0.50	43.87	0.87
*	KRP Site	SAN MH 2	SAN MH 1	0.00	0.00	2.04	6.25	1.5	3.06	1.75	4.81	44.0	250	PVC	0.50	43.87	0.87
*	KRP Site	SAN MH 1	EX. SAN MH D	0.00	0.00	2.04	6.25	1.5	3.06	1.75	4.81	9.1	250	PVC	1.00	62.04	1.22
	KRP Site (Tower C)	TOWER C	EX. SAN MH D	0.96	1.23	0.96	1.23	1.5	1.44	0.34	1.79	114.3	250	PVC	0.40	39.24	0.77
*	KRP Site	EX. SAN MH D	EX. SAN MH E	0.00	0.00	3.00	7.48	1.5	4.50	2.09	6.60	9.5	250	PVC	1.00	62.04	1.22
*	KRP Site	EX. SAN MH E	EX. SAN MH F	0.00	0.00	3.00	7.48	1.5	4.50	2.09	6.60	48.1	250	PVC	0.67	50.78	1.00
	KRP Site (Tower D)	TOWER D	EX. SAN MH F	0.96	3.37	0.96	3.37	1.5	1.44	0.94	2.39	34.0	200	PVC	1.30	39.01	1.20
*	KRP Site	EX. SAN MH F	EX. SAN MH G	0.00	0.00	3.96	10.85	1.5	5.95	3.04	8.98	61.9	250	PVC	0.35	36.70	0.72
†	KRP Site (Brookstreet Hotel)	HOTEL	EX. SAN MH G	2.21	4.49	2.21	4.49	1.5 - 4.0	7.07	1.26	8.33	22.0	200	PVC	0.90	32.46	1.00
*	KRP Site	EX. SAN MH G	EX. SAN MH H	0.00	0.00	6.17	15.34	1.5	9.26	4.30	13.56	21.0	250	PVC	0.38	38.24	0.75
	KRP Site (Parking Structure)	PRKG STRUCT	EX. SAN MH H	0.30	1.28	0.30	1.28	1.5	0.45	0.36	0.81	91.1	250	PVC	0.40	39.24	0.77
*	KRP Site	EX. SAN MH H	EX. SAN MH I	0.00	0.00	6.47	16.62	1.5	9.71	4.65	14.36	88.9	250	PVC	0.38	38.24	0.75
*	KRP Site	EX. SAN MH I	EX. 750 TRUNK	0.00	0.00	6.47	16.62	1.5	9.71	4.65	14.36	100.1	250	PVC	0.52	44.74	0.88
	Brookstreet Apartments	EX SAN MH I	EX 750 TRUNK						4.94	0.17	19.47	100.1	250	PVC	0.52	44.74	0.88

Notes:

- Q(d) = Q(p) + Q(i) , where
 Q(d) = Design Flow (L/sec)
 Q(p) = Population Flow (L/sec)
 Q(i) = Extraneous Flow (L/sec)
 - Q(i) = 0.28 L/sec/ha
 - Daily Sewage Flow from Office Towers = 75 L/person/day (Appendix 4-A, Ottawa Sewer Design Guidelines)
 - Commercial Peaking Factor = 1.5 (Figure 4.3 Ottawa Sewer Design Guidelines)
 - Refer to Sanitary Drainage Area Plan (114060-SAN, C200) for details of drainage areas
 - Refer to the 'Sanitary and Storm Sewer Design Brief' for a breakdown of Daily Sewage Flow components and applicable peaking factors from the Brookstreet Hotel
- * Denotes sewers applicable to this MOE ECA application. All other sewers shown on this design sheet are private sewers tributary to the sanitary trunk sewer under application for MOE approval and/or have MOE approval under an existing C of A.
- ** An existing C of A covers the sanitary stub from SAN MH B north approx. 16.1m to the existing cap. The 10.7m of proposed sewer from the cap to SAN MH 3 is applicable to the new MOE ECA application.
- † Total peak sanitary flow from hotel site = 8.33 L/s, including Extraneous Flows (Also refer to Note 6 above for further details)

SANITARY TRUNK SEWER Sanitary Sewer Design Sheet



PROJECT : 114060
 DESIGNED BY: SM/FST
 CHECKED BY: FST
 DATE: 25-Sep-14

LOCATION			INDIVIDUAL		CUMULATIVE		PEAK FLOWS				PROPOSED SEWER					
AREA	FROM MH	TO MH	FLOW RATE (L/s)	Infiltration Area (ha)	FLOW RATE (L/s)	Infiltration Area (ha)	PEAK FACTOR M	PEAK FLOW Q (p) (L/s)	PEAK EXTRAN.FLOW Q(i) (L/s)	PEAK DESIGN FLOW Q (d) (L/s)	LENGTH (m)	PIPE SIZE (mm)	TYPE OF PIPE	GRADE %	CAPACITY (L/s)	FULL FLOW VELOCITY (m/s)
528 March Road Site	SAN MH 4	EX. SAN MH A	0.35	2.20	0.35	2.20	5.7	2.00	0.62	2.61	25.4	250	PVC	0.50	43.87	0.87
Legget Drive	EX. SAN MH A	EX. SAN MH B	0.00	0.00	0.35	2.20	5.7	2.00	0.62	2.61	55.1	250	PVC	0.33	35.64	0.70
Legget Drive (Newbridge)	EX. SAN MH	EX. SAN MH C	1.69	4.05	1.69	4.05	1.5	2.54	1.13	3.67	60.3	250	PVC	0.31	34.54	0.68
Legget Drive	EX. SAN MH C	EX. SAN MH B	0.00	0.00	1.69	4.05	1.5	2.54	1.13	3.67	68.0	250	PVC	0.29	33.41	0.66
** Legget Drive	EX. SAN MH B	SAN MH 3	0.00	0.00	2.04	6.25	1.5	3.06	1.75	4.81	26.7	250	PVC	0.25	31.02	0.61
* KRP Site	SAN MH 3	SAN MH 2	0.00	0.00	2.04	6.25	1.5	3.06	1.75	4.81	50.4	250	PVC	0.50	43.87	0.87
* KRP Site	SAN MH 2	SAN MH 1	0.00	0.00	2.04	6.25	1.5	3.06	1.75	4.81	44.0	250	PVC	0.50	43.87	0.87
* KRP Site	SAN MH 1	EX. SAN MH D	0.00	0.00	2.04	6.25	1.5	3.06	1.75	4.81	9.1	250	PVC	1.00	62.04	1.22
KRP Site (Tower C)	TOWER C	EX. SAN MH D	0.96	1.23	0.96	1.23	1.5	1.44	0.34	1.79	114.3	250	PVC	0.40	39.24	0.77
* KRP Site	EX. SAN MH D	EX. SAN MH E	0.00	0.00	3.00	7.48	1.5	4.50	2.09	6.60	9.5	250	PVC	1.00	62.04	1.22
* KRP Site	EX. SAN MH E	EX. SAN MH F	0.00	0.00	3.00	7.48	1.5	4.50	2.09	6.60	48.1	250	PVC	0.67	50.78	1.00
KRP Site (Tower D)	TOWER D	EX. SAN MH F	0.96	3.37	0.96	3.37	1.5	1.44	0.94	2.39	34.0	200	PVC	1.30	39.01	1.20
* KRP Site	EX. SAN MH F	EX. SAN MH G	0.00	0.00	3.96	10.85	1.5	5.95	3.04	8.98	61.9	250	PVC	0.35	36.70	0.72
† KRP Site (Brookstreet Hotel)	HOTEL	EX. SAN MH G	2.21	4.49	2.21	4.49	1.5 - 4.0	7.07	1.26	8.33	22.0	200	PVC	0.90	32.46	1.00
* KRP Site	EX. SAN MH G	EX. SAN MH H	0.00	0.00	6.17	15.34	1.5	9.26	4.30	13.56	21.0	250	PVC	0.38	38.24	0.75
KRP Site (Parking Structure)	PRKG STRUCT	EX. SAN MH H	0.00	1.28	0.00	1.28	1.5	0.00	0.36	0.36	91.1	250	PVC	0.40	39.24	0.77
* KRP Site	EX. SAN MH H	EX. SAN MH I	0.00	0.00	6.17	16.62	1.5	9.26	4.65	13.91	88.9	250	PVC	0.38	38.24	0.75
* KRP Site	EX. SAN MH I	EX. 750 TRUNK	0.00	0.00	6.17	16.62	1.5	9.26	4.65	13.91	100.1	250	PVC	0.52	44.74	0.88

Notes:

- Q(d) = Q(p) + Q(i) , where
 Q(d) = Design Flow (L/sec)
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APPENDIX D
Fire Demand per FUS

FUS - Fire Flow Calculations

As per 1999 Fire Underwriter's Survey Guidelines



Engineers, Planners & Landscape Architects

Novatech Project #: 120202

Project Name: Brookstreet Apartments

Date: 9/15/2021

Input By: Jazmine Gauthier

Reviewed By: Greg MacDonald

Legend

Input by User

No Information or Input Required

Building Description: 31 story building (incl. 4 story podium)

Fire Resistive Construction

Step		Choose		Value Used	Total Fire Flow (L/min)	
Base Fire Flow						
1	Construction Material			Multiplier		
	Coefficient related to type of construction C	Wood frame		1.5	0.6	
		Ordinary construction		1		
		Non-combustible construction		0.8		
		Modified Fire resistive construction (2 hrs)	Yes	0.6		
Fire resistive construction (> 3 hrs)			0.6			
2	Floor Area					
	A	Podium Level Footprint (m ²)	1536			
		Total Floors/Storeys (Podium)	4			
		Tower Footprint (m ²)	887			
		Total Floors/Storeys (Tower)	27			
		Protected Openings (1 hr)	Yes			
	Area of structure considered (m ²)			2,304		
F	Base fire flow without reductions				6,000	
$F = 220 C (A)^{0.5}$						
Reductions or Surcharges						
3	Occupancy hazard reduction or surcharge			Reduction/Surcharge		
	(1)	Non-combustible		-25%	-15%	
		Limited combustible	Yes	-15%		
		Combustible		0%		
		Free burning		15%		
Rapid burning			25%			
4	Sprinkler Reduction			Reduction		
	(2)	Adequately Designed System (NFPA 13)	Yes	-30%	-30%	
		Standard Water Supply	Yes	-10%	-10%	
		Fully Supervised System	Yes	-10%	-10%	
Cumulative Total			-50%			
5	Exposure Surcharge (cumulative %)			Surcharge		
	(3)	North Side	0 - 3 m		25%	
		East Side	> 45.1m		0%	
		South Side	20.1 - 30 m		10%	
		West Side	0 - 3 m		25%	
Cumulative Total			60%			
Results						
6	(1) + (2) + (3)	Total Required Fire Flow, rounded to nearest 1000L/min			L/min	6,000
		(2,000 L/min < Fire Flow < 45,000 L/min)			or	100
					or	1,585
7	Storage Volume	Required Duration of Fire Flow (hours)			Hours	2
		Required Volume of Fire Flow (m ³)			m ³	720

FUS - Fire Flow Calculations - User Guide - Fire Resistive

<p>Novatech Project #: 120202 Project Name: Brookstreet Apartments Date: 9/15/2021 Input By: Jazmine Gauthier Reviewed By: Greg MacDonald</p>	<ul style="list-style-type: none"> Please use the notes below as a guide when completing the FUS Fire Flow Calculations When in doubt, confirm construction material, firewalls, etc. with architect/owner When in doubt, err on conservative side
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Note: This form only applies for Fire Resistive

Enter a description of the building or unit being considered, i.e. use/most stringent condition/address

Summary	
Construction Type	Fire Resistive Construction
Floor Area Considered	2,304 m ²
Occupancy Reduction	-15%
Sprinkler Reduction	-50%
Exposure Surcharge	60%
Total Fire Flow	6,000 L/min

Base Fire Flow

1	<p>Construction Material Does not apply for this form Does not apply for this form Does not apply for this form Only Use if can be confirmed with client/architect (ISO CI 5) Only Use if can be confirmed with client/architect (ISO CI 6)</p>	<p>Project Manager Review Date: _____ Name: _____ Signature: _____</p>
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Floor Area

If considered gross floor area, then enter 1 floor/storey. If Fire wall, then reduce footprint accordingly.

Un-Protected = number of floors above first 2, up to max of 10 floors total

Protected = number of additional immediately adjoining floors to be considered, up to 2

Do vertical openings have minimum 1 hour rating between floors? Confirm this with the architect.

For unprotected openings scenario only, can be mix of podium and tower

Reductions or Surcharges

Occupancy hazard reduction or surcharge

- | | |
|----------|---|
| 3 | Residential - with no garage
Residential - with garage
General Commercial - Generally, no reduction
Check usage with FUS
Check usage with FUS |
|----------|---|

Sprinkler Reduction

- | | |
|----------|--|
| 4 | Only Use if can be confirmed with client/architect
Only Use if can be confirmed with client/architect
Only Use if can be confirmed with client/architect |
|----------|--|

Exposure Surcharge (cumulative %)

For Fire walls: FUS considers a Fire wall to have a minimum 2 hour rating per NBC.

5

Results

6 NOTE: Refer to City Technical Bulletin ISDTB-2014-02 for additional considerations to cap this value at 10,000L/min

If IGPM is needed, divide USGPM by 1.20095

7 For Rural areas, or where required