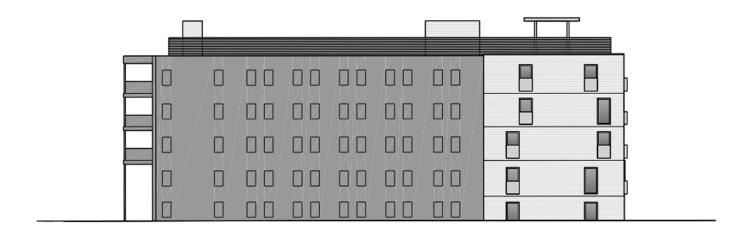
SERVICING & STORMWATER MANAGEMENT REPORT 330 MCLEOD STREET



Project No.: CCO-22-1647

City File No.: D07-12-21-0172

Prepared for:

Smart Living Properties 226 Argyle Avenue Ottawa, ON K2P 1B9

Prepared by:

McIntosh Perry Consulting Engineers Ltd. 115 Walgreen Road Carp, ON K0A 1L0

Revised December 12th, 2022

TABLE OF CONTENTS

1.0	PROJECT OVERVIEW	1
1.1	Purpose	1
1.2	Ste Description	1
1.3	Proposed Development and Statistics	2
1.4	Existing Conditions and Infrastructure	2
1.5	Approvals	2
2.0	BACKROUND STUDIES, STANDARDS AND REFERENCES	3
2.1	Background Reports / Reference Information	3
2.2	Applicable Guidelines and Standards	3
3.0	PRE-CONSULTATION SUMMARY	4
4.0	WATERMAIN	5
4.1	Existing Watermain	5
4.2	Proposed Watermain	5
5.0	SANITARY DESIGN	7
5.1	Existing Sanitary Sewer	7
5.2	Proposed Sanitary Sewer	7
6.0	STORM SEWER & STORMWATER MANAGEMENT DESIGN	8
6.1	Existing Storm Sewers	8
6.2	Proposed Storm Sewers	8
7.0	STORM WATER M ANAGEMENT	9
7.1	Design Criteria and Methodology	9
7.2	Quality Control	9
7.	.2.1 Punoff Calculations	9
7.3	Pre-Development Drainage	10
7.4	Post-Development Drainage	10
8.0	EROSION AND SEDIMENT CONTROL	12
8.1	Temporary Measures	12
8.2	Permanent Measures	12
9.0	SUMMARY	14
10.0	RECOMMENDATION	15
11.0	STATEMENT OF LIMITATIONS	16

LIST OF TABLES

Table 1: Water Supply Design Criteria	5
Table 2: Summary of Estimated Water Demand	
Table 3: Boundary Conditions Results	6
Table 4: Fire Protection Confirmation	6
Table 5: Sanitary Design Criteria	7
Table 6: Summary of Estimated Sanitary Flow	7
Table 7: Pre-Development Runoff Summary	.10
Table 8: Post-Development Runoff Summary	.10

APPENDICES

Appendix A: Site Location Plan

Appendix B: Background Documents

Appendix C: Watermain Calculations

Appendix D: Sanitary Calculations

Appendix E: Pre-Development Drainage Area Plan

Appendix F: Post-Development Drainage Area Plan

Appendix G: Stormwater Management Calculations

1.0 PROJECT OVERVIEW

1.1 Purpose

McIntosh Perry (MP) has been retained by Smart Living Properties to prepare this Servicing and Stormwater Management Report in support of the Zoning By-law Amendment (ZBLA) and Ste Plan Control (SPC) application process for the proposed development at 330 Mcleod Street, within the City of Ottawa.

The main purpose of this report is to present a servicing and stormwater management design for the development in accordance with the recommendations and guidelines provided by the City of Ottawa (City), the Rideau Valley Conservation Authority (RVCA), and the Ministry of the Environment, Conservation and Parks (MECP). This report will address the water, sanitary, and storm sewer servicing for the development, ensuring that existing infrastructure available will adequately service the proposed development.

This report should be read in conjunction with the following drawing:

- COO-22-1647, C101 Grading & Sediment and Erosion Control Plan
- COO-22-1647, C102 Servicing Plan
- CCO-22-1647, PRE Pre-Development Drainage Area Plan (Appendix E)
- COO-22-1647, POST Post-Development Drainage Area Plan (Appendix F)

1.2 Ste Description



Figure 1: Site Map

The subject property, herein referred to as the site, is located at 330 McLeod Street within the Somerset Ward in the City of Ottawa. The site covers approximately 0.11 ha and is located west of the McLeod Street and O'Connor Street intersection, as shown by Figure 1, above. The site is zoned for Residential Use (R4UD). Additional details are included on the Ste Location Plan included in Appendix A.

1.3 Proposed Development and Statistics

The proposed development incorporates a building addition to the existing residential building. 30 additional residential units to the existing 48 units are proposed, with street access from McLeod Street. The development is proposed within 0.056 ha of the site. Refer to Ste Plan prepared by Woodman Architect Associates LTD and included in Appendix B for further details.

1.4 Existing Conditions and Infrastructure

The property is located within the City of Ottawa's Central Sub-Watershed. A residential building exists within the site and is proposed to be retained. The existing building is currently serviced via the City's infrastructure within McLeod Street. The asphalt parking area is proposed to be removed as part of the development.

Sewer and watermain mapping collected from the City of Ottawa indicate that the following services exist across the property frontages within the adjacent municipal right-of-ways:

♦ McLeod Street

- 203 mm diameter PVC watermain; and
- 525 mm diameter concrete combined sewer, tributary to the Rideau Canal
 Interceptor and tributary to the Ottawa River, in the event of an overflow event.

1.5 Approvals

The proposed development is subject to the City of Ottawa site plan control approval and zoning by-law amendment processes. Site plan control requires the City to review, provided concurrence and approve the engineering design package. Permits to construct can be requested once the City has issued a site plan agreement.

Based on pre-consultation with the City of Ottawa, an Environmental Compliance Approval (ECA) through the Ministry of Environment, Conservation and Parks (MECP) may be required since the site is located within a combined sewer area and is tributary to the existing combined sewer within McLeod Street. An ECA is not anticipated since the alteration or use of an existing service is exempt under O. Reg 525/968 subsection 2(1)1 and since the stormwater management controls are proposed within the building.

2.0 BACKROUND STUDIES, STANDARDS AND REFERENCES

2.1 Background Reports / Reference Information

As-built drawings of existing services, provided by the City of Ottawa Information centre, within the vicinity of the site were reviewed in order to identify infrastructure available to service the proposed development.

A topographic survey (19839-19) of the site was completed by Annis, O'Sullivan, Vollebekk Ltd. dated October $23^{\rm rd}$, 2019.

The Site Plan (A001) was prepared by Woodman Architect Associates LTD dated July 20th, 2022 (Site Plan).

2.2 Applicable Guidelines and Standards

Oity of Ottawa:

- Ottawa Sewer Design Guidelines, Otty of Ottawa, SDG002, October 2012. (Ottawa Sewer Guidelines)
 - Technical Bulletin ISTB-2014-01 City of Ottawa, February 2014. (ISTB-2014-01)
 - Technical Bulletin PIEDTB-2016-01 City of Ottawa, September 2016. (PIEDTB-2016-01)
 - Technical Bulletin ISTB-2018-01 City of Ottawa, January 2018. (ISTB-2018-01)
 - Technical Bulletin ISTB-2019-01 City of Ottawa, January 2019. (ISTB-2019-01)
 - Technical Bulletin ISTB-2019-02 City of Ottawa, February 2019. (ISTB-2019-02)
- Ottawa Design Guidelines Water Distribution City of Ottawa, July 2010. (Ottawa Water Guidelines)
 - Technical Bulletin ISD-2010-2 City of Ottawa, December 15, 2010. (ISD-2010-2)
 - Technical Bulletin ISDTB-2014-02 City of Ottawa, May 2014. (ISDTB-2014-02)
 - Technical Bulletin ISTB-2018-02 City of Ottawa, March 2018. (ISTB-2018-02)

Ministry of Environment, Conservation and Parks:

◆ Stormwater Planning and Design Manual, Ministry of the Environment, March 2003. (MECP Stormwater Design Manual)

Design Guidelines for Sewage Works, Ministry of the Environment, 2008. (MECP Sewer Design Guidelines)

Other:

♦ Water Supply for Public Fire Protection, Fire Underwriters Survey, 2020. (FUS Guidelines)

3.0 PRE-CONSULTATION SUMMARY

A pre-consultation meeting was conducted on February 10th, 2021, regarding the proposed development at 330 McLeod Street. Specific design parameters to be incorporated within this design are noted by the City of Ottawa pre-consultation found in Appendix B and are noted below.

- ◆ Control 5 through 100-year post-development flows to the 2-year storm event with a combined C value to a maximum of 0.40.
- ◆ Quality controls are not required since the site is tributary to a combined sewer, ultimately tributary to Robert O. Pickard Environmental Centre (ROPEC).

4.0 WATERMAIN

4.1 Existing Watermain

The subject site is located within the 1W pressure zone, as shown by the Water Distribution figure located in Appendix C. There is an existing 203 mm diameter watermain, that runs the entire length of the property along McLeod Street. There are three public hydrants within 150 m of the site, as discussed in Section 4.2.

4.2 Proposed Watermain

It is proposed to service the proposed building addition through the existing building and 100 mm diameter water service. A mechanical consultant will need to review and confirm whether upgrades to the existing building service size are required to accommodate the addition.

Table 1, below, summarizes the water supply design criteria obtained from the Ottawa Water Guidelines and utilized for the water analysis.

Ste Area

Residential

Residential 280 L/day/person

Residential Apartment - Bachelor

Max Day Peaking Factor - Residential

Peak Hour Peaking Factor - Residential

1.4 person/unit
9.5 x avg. day

14.3 x avg. day

Table 1: Water Supply Design Criteria

The water analysis results have been summarized in Table 2, below. The fire flow demand accounted for both the existing above-ground floor area and the proposed area.

Table 2: Summary of Estimated Water Demand

Design Parameter	Total How (L/s) Existing	Total How (L/s) Proposed	Total How (L/s) Total
Average Daily Demand	0.22	0.14	0.36
Max Day Demand	2.09	1.29	3.39
Max Day + Fire How Demand (133.33 L/s)	-	-	136.72
Peak Hour Demand	3.15	1.95	5.10

The Fire Underwriters Survey 2020 (FUS) method was utilized to estimate the required fire flow for the site. Fire flow requirements were calculated per City of Ottawa Technical Bulletin ISTB-2018-02.

The following parameters were coordinated with the architect:

- ◆ Type of construction Non-Combustible Construction;
- ◆ Occupancy type Limited Combustibility;
- ♦ Sprinkler Protection Standard Sprinkler system.

The results of the calculations yielded a required fire flow of 133.33 L/s (8,000 L/min). The detailed calculations for the FUS can be found in Appendix C.

The City provided the estimated water pressures at both for the average day scenario, peak hour scenario and the max day plus fire flow scenario for the demands indicated by the correspondence in Appendix C. Site plan changes have resulted in a slightly reduced FUS fire demand, however this isn't anticipated to have an impact on the design. The resulting pressures for the boundary conditions results are shown in Table 3, below.

Table 3: Boundary Conditions Results

Scenario	Proposed Demands (Per Original Boundary Condition Request) (L/s)	Connection 1 HGL(m H₂O)*/kPa			
Average Day Demand	0.35	45.1 / 442.0			
Maximum Daily + Fire How Demand	153.33	35.4 / 346.9			
Peak Hourly Demand	5.01	36.6 / 358.7			
* Adjusted for an estimated ground elevation of 70.24m above the connection point for connection.					

The normal operating pressure range is anticipated to be 359 kPa to 442 kPa and will not be less than 275 kPa (40 psi) or exceed 689 kPa (100 psi). The proposed watermains will meet the minimum required 20 psi (140 kPa) from the Ottawa Water Guidelines at the ground level under maximum day demand and fire flow conditions.

To confirm the adequacy of fire flow to protect the proposed development, public fire hydrants within 150 m of the proposed building were accounted for per ISTB 2018-02 Appendix I.

Table 4: Fire Protection Confirmation

Fire How Demand	Fire Hydrant(s)	Fire Hydrant(s)	Combined Fire
(L∕ min.)	within 75m	within 150m	Flow (L∕ min)
8,000 L/min (133.33 L/s)	1 public	2 public	12,900 (215 L/s)

As demonstrated by Table 4, above, the existing hydrants located in the vicinity can provide adequate fire protection to the site based on city guidelines.

5.0 SANITARY DESIGN

5.1 Existing Sanitary Sewer

The subject site lies within the Rideau Canal Interceptor combined sewer area, tributary to ROPEC. There is an existing 525 mm diameter combined sewer within McLeod Street, tributary to the Rideau River Interceptor sewer approximately 140 m downstream.

5.2 Proposed Sanitary Sewer

It is proposed to service the proposed building addition through the existing building. A mechanical consultant will need to review and confirm whether upgrades to the existing building are required to accommodate the addition.

Table 5, below, summarizes the wastewater design criteria identified by the Ottawa Sewer Guidelines.

Design Parameter

Value

Residential Apartment – Bachelor

Average Daily Demand – Residential

Peaking Factor – Residential

Extraneous Flow Allowance

Value

1.4 persons/unit

280 L/day/person

3.59 (Total)

0.33 L/s/ha

Table 5: Sanitary Design Criteria

Based on coordination with Paterson Group, the ground water contamination rate directed to the sanitary sewer is estimated to be 10,000 L/day. Correspondence with Paterson Group is included in Appendix D for reference.

Table 6, below, summarizes the estimated wastewater flow from the proposed development. Refer to Appendix D for detailed calculations.

Table 6: Summary of Estimated Sanitary Flow

Design Parameter	Total How Existing (L/s)	Total How Proposed Addition (L/s)	Total How (L/s)
Total Estimated Average Dry Weather How	0.23	0.14	0.36
Total Estimated Peak Dry Weather Flow	0.80	0.50	1.28
Total Estimated Peak Wet Weather Flow	0.83	0.65	1.43

6.0 STORM SEWER & STORMWATER MANAGEMENT DESIGN

6.1 Existing Storm Sewers

Stormwater runoff from the site is currently tributary to the Rideau River Interceptor combined sewer area. There is an existing 525 mm diameter combined sewer within McLeod Street, tributary to the Rideau River Interceptor sewer approximately 140 m downstream.

6.2 Proposed Storm Sewers

A new 250 mm diameter storm service is proposed to be extended from 525 mm combined sewer within McLeod Street to the rear of the site. Refer to drawing C102 for a detailed servicing layout.

Runoff collected on the roof of the proposed building addition will be stored and controlled internally using one roof drain. The roof drain will be used to limit the flow from the roof to the specified allowable release rate. For calculation purposes a Watts Accutrol roof drain in the "fully exposed" position was used to estimate a reasonable roof flow. Other products may be specified at detailed building design so long as release rates and storage volumes are respected.

See COO-22-1647 - POST include in Appendix F of this report for more details. The Stormwater Management design for the subject property will be outlined in Section 7.0 of this report.

Foundation drainage is proposed to be connected to the existing building sanitary system. The internal servicing layout is to be reviewed by the mechanical engineer.

7.0 STORMWATER MANAGEMENT

7.1 Design Criteria and Methodology

The following design criteria will need to be employed to develop the stormwater management design for the site, as directed by the City:

Quality Control

 Quality controls are not required for this site as the development is tributary to a combined sewer outlet.

Quantity Control

 Post-development to be restricted to the 2-year storm event, based on a calculated time of concentration greater than 10 minutes and a rational method coefficient of 0.40. Refer to Section 7.2 for further details.

7.2 Quality Control

7.2.1 Runoff Calculations

Runoff calculations presented in this report are derived using the Rational Method, given as:

Q = 2.78 CIA (L/s)

Where: C = Runoff coefficient

= Rainfall intensity in mm/hr (City of Ottawa IDF curves)

A = Drainage area in hectares

It is recognized that the Pational Method tends to overestimate runoff rates. As a result, the conservative calculation of runoff ensures that any SWM facility sized using this method is expected to function as intended.

The following coefficients were used to develop an average Cfor each area:

Roofs/Concrete/Asphalt	0.90
Undeveloped and Grass	0.20

As per the Ottawa Sewer Guidelines, the 5-year balanced 'C' value must be increased by 25% for a 100-year storm event to a maximum of 1.0.

The time of concentration (Tc) used for pre- and post-development shall be calculated and no less than 10 minutes.

Based on the criteria listed in Section 7.2.1, the development will be required to restrict flow to the 2-year storm event. It is estimated that the target release rate during the 100-year event will be 4.80 L/s, based on the construction limit of 0.056 ha.

7.3 Pre-Development Drainage

A pre-development drainage area plan has been prepared for the site. As noted by drawing CCC-22-1647 - PRE, included in Appendix Eof this report, rear and side yard drainage currently spill overland towards McLeod Street.

It has been assumed that the existing development contained no stormwater management controls for flow attenuation. The estimated pre-development peak flows for the 5 and 100year events are summarized below in Table 7. See OOO-22-1647 - PRE in Appendix E and Appendix G for calculations.

Q(L/s)Drainage Area Area (ha) 2-Year 5-Year 100-Year Α1 0.056 10.70 14.51 27.64

Table 7: Pre-Development Runoff Summary

7.4 Post-Development Drainage

To meet the stormwater objectives the development will contain rooftop control.

Based on the criteria listed in Section 7.2.1, the development will be required to restrict flow to the 2-year storm event. It is estimated that the target release rate during the 100-year event will be 4.80 L/s based on the construction limit of 0.056 ha.

The proposed site drainage limits are demonstrated on the Post-Development Drainage Area Plan. See COO-22-1647 - POST in Appendix F of this report for more details. A summary of the Post-Development Runoff Calculations can be found below.

Table 8: Post-Development Runoff Summary

5-year 100-year 100-year 100-year Drainage Area Peak Flow Peak Flow Storage Required Storage Available Area (ha) (L/s)(L/s) (m^3) (m^3) 0.016 0.76 B1 0.38 6.42 7.34 B2 0.040 3.57 7.22 0.056 3.95 7.98 6.42 7.34 Total

McINTOSH PERRY 10

Runoff for area B1 will be stored on the roof of the proposed building addition and restricted using one Watts Accutrol roof drain (or equivalent product) to a maximum release rate of 0.76 L/s and will provide up to 7.34 m³ of storage.

Area B2 is 0.040 ha and will direct stormwater at a rate of 7.22 L/s during a 100-year storm event. The flow from Area B2 will enter proposed swales as it travels overland towards Mcleod Street. Runoff within the proposed swales will be collected by a series of landscaping catchbasins, where it will then be directed to the 525 mm diameter combined sewer within Mcleod Street. Controls within the rear yard of Area B2 were explored to further reduce drainage flow rates. Due to the small size of this primarily landscaped area, it was anticipated that flow from the walkway would need to be directed to this area to achieve any appreciable level of storage. Directing water to the rear yard from the walkway would raise the height of the emergency overland flow route and increase the risk of ponding against the foundation. As a result, rear yard storage was not deemed feasible.

As noted above, the target release rate for the site is 4.80 L/s. Based on the calculations shown in Table 8, the combined release rate during the 100-year storm is 7.98 L/s. While the development will slightly exceed its stormwater objective, there will be a reduction of 71% from the existing unrestricted flow rate of 27.64 L/s. Refer to Appendix G for detailed calculations.

Foundation drainage is proposed to be connected to the existing building drainage systems. Contaminated groundwater will need to discharge to the sanitary sewer system. The internal servicing layout will need to be reviewed by the mechanical engineer to adhere to the stormwater management design.

The remaining site area will be undisturbed.

8.0 EROSION AND SEDIMENT CONTROL

8.1 Temporary Measures

Before construction begins, temporary silt fence, straw bale or rock flow check dams will be installed at all-natural runoff outlets from the property. It is crucial that these controls be maintained throughout construction and inspection of sediment and erosion control will be facilitated by the Contractor or Contract Administration staff throughout the construction period.

Sit fences will be installed where shown on the final engineering plans, specifically along the downstream property limits. The Contractor, at their discretion or at the instruction of the City, Conservation Authority or the Contract Administrator shall increase the quantity of sediment and erosion controls on-site to ensure that the site is operating as intended and no additional sediment finds its way off site. The rock flow, straw bale & silt fence check dams and barriers shall be inspected weekly and after rainfall events. Care shall be taken to properly remove sediment from the fences and check dams as required. Fibre roll barriers are to be installed at all existing curb inlet catch basins and filter fabric is to be placed under the grates of all existing catch basins and manholes along the frontage of the site and any new structures immediately upon installation. The measures for the existing/proposed structures is to be removed only after all areas have been paved. Care shall be taken at the removal stage to ensure that any silt that has accumulated is properly handled and disposed of. Removal of silt fences without prior removal of the sediments shall not be permitted.

Although not anticipated, work through winter months shall be closely monitored for erosion along sloped areas. Should erosion be noted, the Contractor shall be alerted and shall take all necessary steps to rectify the situation. Should the Contractor's efforts fail at remediating the eroded areas, the Contractor shall contact the City and/or Conservation Authority to review the site conditions and determine the appropriate course of action. As the ground begins to thaw, the Contractor shall place silt fencing at all required locations as soon as ground conditions warrant. Please see the Ste Grading, Drainage and Sediment & Erosion Control Plan for additional details regarding the temporary measures to be installed and their appropriate OPSD references.

8.2 Permanent Measures

It is expected that the Contractor will promptly ensure that all disturbed areas receive topsoil and seed/sod and that grass be established as soon as possible. Any areas of excess fill shall be removed or levelled as soon as possible and must be located a sufficient distance from any watercourse to ensure that no sediment is washed out into the watercourse. As the vegetation growth within the site provides a key component to the control of sediment for the site, it must be properly maintained once established. Once the construction is complete, it will be up to

the landowner to maintain the vegetation and ensure that the vegetation is not overgrown or impeded by foreign objects.

9.0 SUMMARY

- The proposed development incorporates a building addition to the existing building within 330 McLeod Street. The Ste Plan proposes 30 units to the existing 48 residential units, with street access from McLeod Street. Development is proposed within 0.056 ha of the site.
- The FUS method estimated fire flow indicated that 8,000 L/min is required for the proposed development;
- The development is estimated to have a combined peak wet weather flow of 1.43 L/s;
- Based on City of Ottawa guidelines, the development will be required to attenuate post-development 5 and 100-year flows to the 2-year release rate of 4.80 L/s. This flow rate is based on the limit of work area of 0.056 ha;
- To meet the stormwater objectives the development will contain 7.34 m³ of rooftop storage for flow attenuation;
- The proposed release rate during the 100-year storm is 7.98 L/s, a reduction of 71% from existing conditions; and
- Quality controls are not required for this site as the development due to the combined sewer outlet.

10.0 RECOMMENDATION

Based on the information presented in this report, we recommend that City of Ottawa approve this Servicing and Stormwater Management report in support of the proposed development at 330 McLeod Street.

This report is respectfully being submitted for approval.

Regards,

McIntosh Perry Consulting Engineers Ltd.



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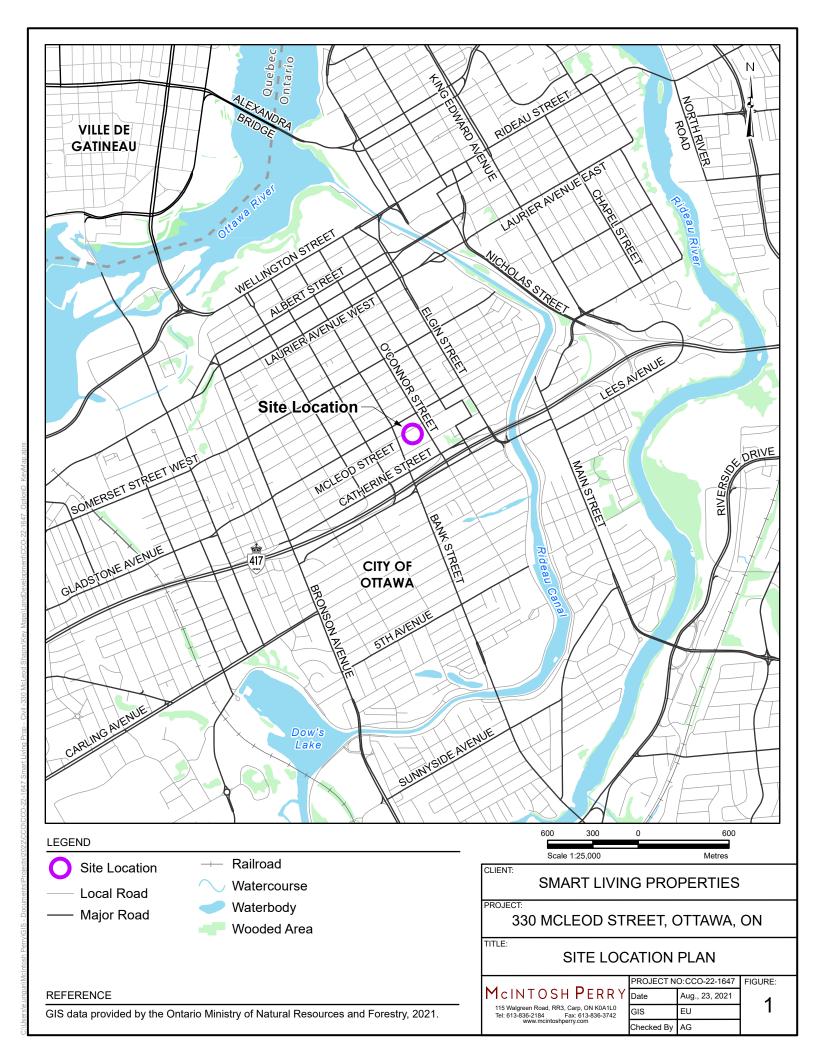
11.0 STATEMENT OF LIMITATIONS

This report was produced for the exclusive use of <u>Smart Living Properties</u>. The purpose of the report is to assess the existing stormwater management system and provide recommendations and designs for the post-construction scenario that are in compliance with the guidelines and standards from the Ministry of the Environment, Parks and Climate Change, City of Ottawa and local approval agencies. McIntosh Perry reviewed the site information and background documents listed in Section 2.0 of this report. While the previous data was reviewed by McIntosh Perry and site visits were performed, no field verification/measures of any information were conducted.

Any use of this review by a third party, or any reliance on decisions made based on it, without a reliance report is the responsibility of such third parties. McIntosh Perry accepts no responsibility for damages, if any, suffered by any third party as a result of decisions or actions made based on this review.

The findings, conclusions and/or recommendations of this report are only valid as of the date of this report. No assurance is made regarding any changes in conditions subsequent to this date. If additional information is discovered or becomes available at a future date, McIntosh Perry should be requested to re-evaluate the conclusions presented in this report, and provide amendments, if required.

APPENDIX A KEY PLAN



APPENDIX B BACKGROUND DOCUMENTS



Pre-consultation Site Plan Control & Zoning By-Law Amendment Applications 233 Argyle Ave and 330 Mcleod Street

Applicant: Jeremy Silburt

Owner: SMART LIVING ON 233 ARGYLE INC and SMART LIVING ON MCLEOD STREET INC.

Meeting Date: February 10, 2021

Attendees: Applicant Team

Jeremy Silburt, Smart Living Properties
Kris Benes, Architect, Open Plan Architects
Lisa Dalla Rosa, Planner, Fotenn Consultants
Rakan Abushaar, Smart Living Properties
Tamer Abaza, Smart Living Properties

City of Ottawa

Kimberley Baldwin, Development Review Planner Christopher Moise, Urban Designer John Wu, Civil Engineering Luis Juarez, Heritage Planner Mark Richardson, Forester Shukufa Sultonmamad, Planning Assistant

Centretown Citizens Community Association

Jack Hanna

Meeting Notes & Comments

Proposal: To extend the current buildings on 233 Argyle Ave and 330 McLeod St toward the rear of the lots.

- 233 Argyle Ave Proposal to construct a 3-storey rear yard addition to the existing 3-storey office building; addition will contain 13 bachelor residential units.
- 330 McLeod St Proposal to construct a rear yard addition to the existing 5-storey rooming house; addition will contain 30 additional rooming units.

Development Review Processes (File lead: Kimberley Baldwin)

- Zoning By-law Amendment application
 - We could look at these two developments under one Zoning Bylaw amendment application.
- Site Plan Control Applications
 - We advise filing two site plan control applications, one for each property
 - 330 McLeod St Site Plan Complex, Manager Approval, Public Consultation
 - 233 Argyle Ave Site Plan application type to be confirmed.
 - What will be the proposed size this building post-development?

<u>Heritage Process (Fie lead: Luis Juarez)</u>

- The two additions will not function as a single development, and therefore a heritage permit application for each new addition is requested.
- The 'Council-level authority Minor Application' type and fee of \$ \$2,243.00 is applicable for each addition and must be provided with the heritage permit application submission.

Application Requirements

- Application Form and Payment;
- Detailed description of the Proposed Work including total GFA stats and proposed restoration work;
- Site Plan and Landscape Plan;
- Coloured Elevations measured, with materials indicated, including the windows, and heights of adjacent buildings illustrated; and,
- A coloured streetscape rendering demonstrating the visual impact, if any, of the additions on the contributing property's streetscape (along Argyle Avenue).
- Based on the proposal, a Cultural Heritage Impact Statement will not be necessary for this
 application. A description and rationale should be provided to demonstrate how the
 addition meets the Centretown HCD Guidelines and the <u>Centretown Community Development</u>
 <u>Plan</u> Heritage policies (Section 6.5) from the Applicant's perspective.

Engineering Comments - John Wu

- This site is located at the combined sewer areas, it has to follow the combined sewer area storm
 water management requirement, and the ECA will be required. Typical storm water management
 will require control its storm water on site, using 2 year's storm and a C value of 0.4 to control up
 to 100 years' storm event.
- We also need a servicing study,
- Geotechnical study is required, phase one ESA will be required, possible Phase two ESA may be required depending on the result of phase one ESA study.
- A noise study may be required, it is within 100 meters to Bank Street, and within 500 meters from Highway 417.

Planning Comments – Kimberley Baldwin

- General comment is that we'll primarily be assessing each addition individually, as they appear as separate projects with no shared elements.
 - The applicant indicated that a shared bicycle storage facility is proposed in 330 Mcleod, to be used by both properties
 - Planning staff expressed a preference to see bicycle, waste storage provided for each individual property.
- Properties are designated General Urban Area in the Official Plan
 - Support for intensification in the General Urban Area where it complements the existing pattern and scale of development and planned function of the area.
 - Staff assess how new development enhances and builds upon desirable established patterns
 of built form and open spaces
 - There is an opportunity here to extend the existing soft landscape buffer that runs along the rear of adjacent properties.
 - It is also important to maintain adequate open space between properties, especially at the rear.
 - General Urban policies look how new development contributes to the balance of housing types and tenures to provide a full range of housing for a variety of demographic

profiles. In that regard, we encourage a mix of unit sizes, rather than all bachelor and rooming units.

- The applicant noted that buildings containing rooming units are not allowed to provide a mix of units within the same building.
- Properties are also located within the Centretown Secondary Plan
 - Central Character Area 'Residential Mixed Use Designation'
 - Low-rise apartment buildings are permitted uses in this designation
 - Commercial uses are limited to the first two floors of a building [check that the offices currently on the 3rd floor of the 233 Argyle were legally established]
 - 233 Argyle is identified as a Heritage Building in this plan.
- Zoning Residential Fourth Density Zone, Subzone UD, Urban Exception 479 with a Heritage Overlay and Mature Neighbourhoods Overlay. [R4UD(479)]
 - From a zoning perspective, the built form of both additions suggests an overdevelopment of these lots.
 - Both sites are deficient in providing adequate rear yard and side yard setbacks.
 - Space between the proposed additions should not be viewed as a shared space. As such
 please provide appropriate rear yard setbacks on each property.
 - Greater rear yard setbacks would the following benefits:
 - Allow for existing trees at the rear to be preserved and new soft landscaping to be established, creating a desirable amenity areas at grade for both future tenants as well as for the neighbouring properties in this block.
 - Allow for more of the units to be oriented towards the rear, rather than the side yards, improving the livability of each unit.
 - Respect privacy and provide adequate separation from existing amenity areas (balconies) on adjacent properties

Waste Management

233 Argyle:

 The adjacent apartment building to the east cantileavers over the driveway. There is also a short retaining wall at the side of the lot. These existing characteristics would present challenges for managing waste (with a large vehicle) on site.

330 Mcleod

- Narrow driveway, which could present challenges to on-site waste management
- How many existing rooms? Where is the existing waste storage for those units?
- In the planning rationale for each development, please look at the needs of existing and proposed uses and demonstrate that an adequate waste management plan is provided.
- Amenity area and bicycle parking Similarly, existing units should be taken into consideration in designing the amenity area and bicycle parking requirements for each building.
- If no vehicular parking is provided, demonstrate how alternative modes of transportation are being provided [eg. provide more bicycle parking storage, ideally at a 1:1 ratio (1 unit=1 bicycle parking space)]

Urban Design Comments- Christopher Moise

 This proposal exists within one of the City's Design Priority Areas and must attend the City's UDRP. Please consult the City's website for details regarding the UDRP schedule;

Comments/questions/concerns:

- Rear yard set-back/Block pattern reduction is a major concern. It would be helpful to illustrate the
 line of required set-back to show how much of that is being encroached upon by this proposal.
 Thirty percent of the lot is required. We recommend that the full rear yard set-back be provided to
 maintain the block pattern, access to day-light for the existing and future residents and for the
 residents of neighbouring buildings;
- The proposed units rely on side yards for light and views and when replicability of this proposal is considered (when neighbouring lots proposal similar reductions in set-backs), the resulting condition may further compromise exposure to day-light and negatively impact the proposed buildings;
- Roof top amenity: we question the quality of space proposed and should be further illustrated as over-look and privacy issues arise when adjacent to neighbouring mid and high-rise built form;
- Amenity provided at grade and in the rear yard is important to keep the middle of the block open for access to day-light and views and for new landscaping for this and adjacent buildings;
- Shared uses between buildings is concerning as each property is to provide required bike parking (to support relief from vehicular parking), garbage storage, amenity, etc. especially if ownership of the properties changes in the future;
- No concern about removing the at grade parking, but would recommend that the existing building
 green the parking lot and provide amenity and soft landscaping at grade instead of asphalt or built
 form:
- Once the footprint and massing of the proposal has been resolved then the issues of materiality and contextual relationships can be further addressed;
- A Design Brief is a required submittal for all Site Plan/Re-zoning applications. Please see the Design Brief Terms of Reference provided.

This is an exciting project in an area full of potential. We look forward to helping you achieve its goals with the highest level of design resolution. We are happy to assist and answer any questions regarding the above. Good luck.

Heritage Planning Comments – Luis Juarez

The subject properties are located within the Centretown Heritage Conservation District (HCD) and are designated under Part V of the *Ontario Heritage Act*.

- 233 Argyle Avenue is a category 2 property and is considered a 'contributing' property to the cultural heritage value of the Centretown HCD, whereas 330 McLeod Street is a category 4 property and is considered a 'non-contributing' property.
- As per the design brief submitted for the Pre-Consultation meeting, the proposed works include an extension of both buildings towards the rear of the lots for a total of 33 additional residential units (13 on Argyle, and 20 on McLeod).
- A new Centretown Heritage Conservation District Plan is being drafted. The application may be impacted by the new plan and the application will be subject to either the new or the old plan depending on the applications date of submission.
- Staff have provided preliminary comments based on the submitted materials. Should additional
 drawings or details be provided or should the design change, Staff may require further review and
 provide additional comments at that time.

Preliminary Comments on the Proposal

 Please review the Centretown HCD Plan guidelines, Section 3.7 of the Centretown Secondary Plan, and Section 6.5 of the Centretown CDP for direction on how additions to

- these properties can be compatible within the context of the HCD (Centretown HCD guidelines attached).
- Heritage Staff are conceptually supportive of infill development on these properties.
 Notwithstanding, Heritage Staff mirror Development Review and Urban Design comments related to the reduction in massing and proper provision of amenity space for each addition to ensure that the proposed infill development is compatible with the character of the HCD.

Massing

- The additions should be distinguishable, secondary and complimentary to the existing buildings.
- The proposed rooftop utilities and/or mechanical penthouse on the Argyle addition exceeds the height of the existing roofline. The applicant will need to demonstrate if additions have a visual impact on the contributing property's streetscape (along Argyle Avenue).

Conservation and Maintenance of Contributing Properties

- Staff encourage restoration of existing heritage attributes for 233 Argyle Avenue as part of this application. Please refer to Section VII.5.3 of the HCD guidelines (The Conservation and Restoration of Heritage Residential Properties) for guidance on proper restoration of building elements.
- Examples of heritage restoration projects for this site include but are not limited to the restoration
 of wood features including the second-floor balcony and third floor dormer; windows,
 soffit, and cornice.
- Restoration work may be eligible for a heritage restoration grant of up to \$10,000 (available on a
 matching basis). Refer to the <u>Built Heritage Funding page</u> for information on the City's grant
 program and to review the program guidelines. Heritage grants are available even if the Applicant
 does not proceed with the proposed development.

Cladding

The HCD guidelines suggest brick veneer as the primary cladding for infill development, however
given that the additions will not be visible from the street, the applicant could consider using a
type of horizontal cladding. Possible materials include wood clapboard or composite cladding (i.e.
fibre cement board with paint finish) that is distinct but complementary to the original brick of the
two existing buildings.

Forester Comments - Mark Richardson

TCR requirements:

- Tree Conservation Report (TCR) must be supplied for review along with the suite of other plans/reports required by the City
 - an approved TCR is a requirement of Site Plan approval.
- As of January 1 2021, any removal of privately or publicly (City) owned trees 10cm or larger in diameter requires a tree permit issued under the Tree Protection Bylaw (Bylaw 2020 340); the permit will be based on an approved TCR and made available at or near plan approval.
- The Planning Forester from Planning and Growth Management as well as foresters from Forestry Services will review the submitted TCR
 - If tree removal is required, both municipal and privately-owned trees will be addressed in a single permit issued through the Planning Forester
 - Compensation may be required for city owned trees if so, it will need to be paid prior to the release of the tree permit
- the TCR must list all trees on site by species, diameter and health condition
- the TCR must list all trees on adjacent sites if they have a critical root zone that extends onto the development site
- If trees are to be removed, the TCR must clearly show where they are, and document the reason they cannot be retained

- All retained trees must be shown and all retained trees within the area impacted by the
 development process must be protected as per City guidelines available at <u>Tree Protection</u>
 <u>Specification</u> or by searching Ottawa.ca
 - securities may be required for retained trees
 - the location of tree protection fencing must be shown on a plan
 - show the critical root zone of the retained trees
 - if excavation will occur within the critical root zone, please show the limits of excavation
- the City encourages the retention of healthy trees; if possible, please seek opportunities for retention of trees that will contribute to the design/function of the site.
- For more information on the process or help with tree retention options, contact Mark Richardson mark.richardson@ottawa.ca or on City of Ottawa

LP tree planting requirements:

For additional information on the following please contact Tracy.Smith@Ottawa.ca

Minimum Setbacks

- Maintain 1.5m from sidewalk or MUP/cycle track.
- Maintain 2.5m from curb
- Coniferous species require a minimum 4.5m setback from curb, sidewalk or MUP/cycle track/pathway.
- Maintain 7.5m between large growing trees, and 4m between small growing trees. Park or open space planting should consider 10m spacing.
- Adhere to Ottawa Hydro's planting guidelines (species and setbacks) when planting around overhead primary conductors.

Tree specifications

- Minimum stock size: 50mm tree caliper for deciduous, 200cm height for coniferous.
- Maximize the use of large deciduous species wherever possible to maximize future canopy coverage
- Tree planting on city property shall be in accordance with the City of Ottawa's Tree Planting Specification; and include watering and warranty as described in the specification (can be provided by Forestry Services).
- Plant native trees whenever possible
- No root barriers, dead-man anchor systems, or planters are permitted.
- No tree stakes unless necessary (and only 1 on the prevailing winds side of the tree)

Hard surface planting

- Curb style planter is highly recommended
- No grates are to be used and if guards are required, City of Ottawa standard (which can be provided) shall be used.
- Trees are to be planted at grade

Soil Volume

Please ensure adequate soil volumes are met:

Tree	Single Tree Soil	Multiple Tree Soil
Type/Size	Volume (m3)	Volume (m3/tree)
Ornamental	15	9
Columnar	15	9
Small	20	12
Medium	25	15
Large	30	18

Conifer	25	15

Please note that these soil volumes are not applicable in cases with Sensitive Marine Clay.

Sensitive Marine Clay

Please follow the City's 2017 Tree Planting in Sensitive Marine Clay guidelines

Community Association Comments (Jack Hanna, CCCA)

- In favour of density, as Centretown is in desperate need in affordable units
- Maintaining heritage is also good
- If vehicular parking is not provided, and future tenants won't be using cars, what will they be using? These proposal are deficient in providing bicycle parking
- Providing no vehicular parking will probably be a concern for surrounding community.
- Consider providing a car sharing space
- We want more units, but developers have a responsibility to give their tenants some nice amenity space on site. Rooftop amenity not a desirable approach.
- The community will look at Tree Conservation Report very closely
- The walkway to access the 330 McLeod units appears to be a bit of a canyon. Will the people using this walkway be walking past windows?
- Please hold a meeting with community to discuss building materials
- Consider providing space on site for e-scooters, which are becoming a popular alternate method of transportation downtown.

Application Submission Information

For information on Site Plan Control Thresholds under the Site Plan Control By-law, please visit: https://documents.ottawa.ca/sites/documents/files/siteplan_thresholds_en.pdf

For information on Applications, including fees, please visit: https://ottawa.ca/en/city-hall/planning-and-development-application-review-process/development-application-review-process/development-application-fees

The application processing timeline generally depends on the quality of the submission. For more information on standard processing timelines, please visit: https://ottawa.ca/en/city-hall/planning-and-development/information-development-application-review-process/development-application-submission/development-application-forms#site-plan-control

Prior to submitting a formal application, it is recommended that you pre-consult with the Ward Councillor.

Application Submission Requirements

For information on the preparation of Studies and Plans and the City's Planning and Engineering requirements, please visit: https://ottawa.ca/en/city-hall/planning-and-development/information-

<u>developers/development-application-review-process/development-application-submission/guide-preparing-studies-and-plans</u>

Please provide electronic copy (PDF) of all plans and studies required.

All plans and drawings must be produced on A1-sized paper and folded to 21.6 cm x 27.9 cm $(8\frac{1}{2}$ "x 11").

Note that many of the plans and studies collected with this application must be signed, sealed and dated by a qualified engineer, architect, surveyor, planner or designated specialist.



APPLICANT'S STUDY AND PLAN IDENTIFICATION LIST

Legend: **S** indicates that the study or plan is required with application submission.

A indicates that the study or plan may be required to satisfy a condition of approval/draft approval.

For information and guidance on preparing required studies and plans refer here:

S/A	Number of copies	ENGINEERING			Number of copies
S	<mark>15</mark>	1. Site Servicing Plan	Site Servicing Study / Assessment of Adequacy of Public Services		3
S	<mark>15</mark>	3. Grade Control and Drainage Plan	4. Geotechnical Study / Slope Stability Study	S	<mark>3</mark>
	2	5. Composite Utility Plan	6. Groundwater Impact Study		3
	3	7. Servicing Options Report	8. Wellhead Protection Study		3
	9	9. Transportation Impact Assessment (TIA)	10.Erosion and Sediment Control Plan / Brief	S	3
S	<mark>3</mark>	11.Storm water Management Report / Brief	12.Hydro geological and Terrain Analysis		3
	3	13.Hydraulic Water main Analysis	14.Noise / Vibration Study	S	3
	PDF only	15.Roadway Modification Functional Design	16.Confederation Line Proximity Study		3

S/A	Number of copies	PLANNING / DESIGN / SURVEY			Number of copies
	15	17.Draft Plan of Subdivision	18.Plan Showing Layout of Parking Garage		2
	5	19.Draft Plan of Condominium	20.Planning Rationale	S	3
S	<mark>15</mark>	21.Site Plan	22.Minimum Distance Separation (MDS)		3
	15	23.Concept Plan Showing Proposed Land Uses and Landscaping	24.Agrology and Soil Capability Study		3
	3	25.Concept Plan Showing Ultimate Use of Land	26.Cultural Heritage Impact Statement		3
S	<mark>15</mark>	27.Landscape Plan (can combine with site plan)	28.Archaeological Resource Assessment Requirements: S (site plan) A (subdivision, condo)		3
S	<mark>2</mark>	29.Survey Plan	30.Shadow Analysis		3
S	3	31.Architectural Building Elevation Drawings (dimensioned)	32.Design Brief (includes the Design Review Panel Submission Requirements)	S	Available online
	3	33.Wind Analysis			

S/A	Number of copies	ENVIRONMENTAL			Number of copies
S	3	34.Phase 1 Environmental Site Assessment	35.Impact Assessment of Adjacent Waste Disposal/Former Landfill Site		3
S	3	36.Phase 2 Environmental Site Assessment (depends on the outcome of Phase 1)	37.Assessment of Landform Features		3
	3	38.Record of Site Condition	39.Mineral Resource Impact Assessment		3
S	3	40.Tree Conservation Report	41.Environmental Impact Statement / Impact Assessment of Endangered Species		3
	3	42.Mine Hazard Study / Abandoned Pit or Quarry Study	43.Integrated Environmental Review (Draft, as part of Planning Rationale)		3

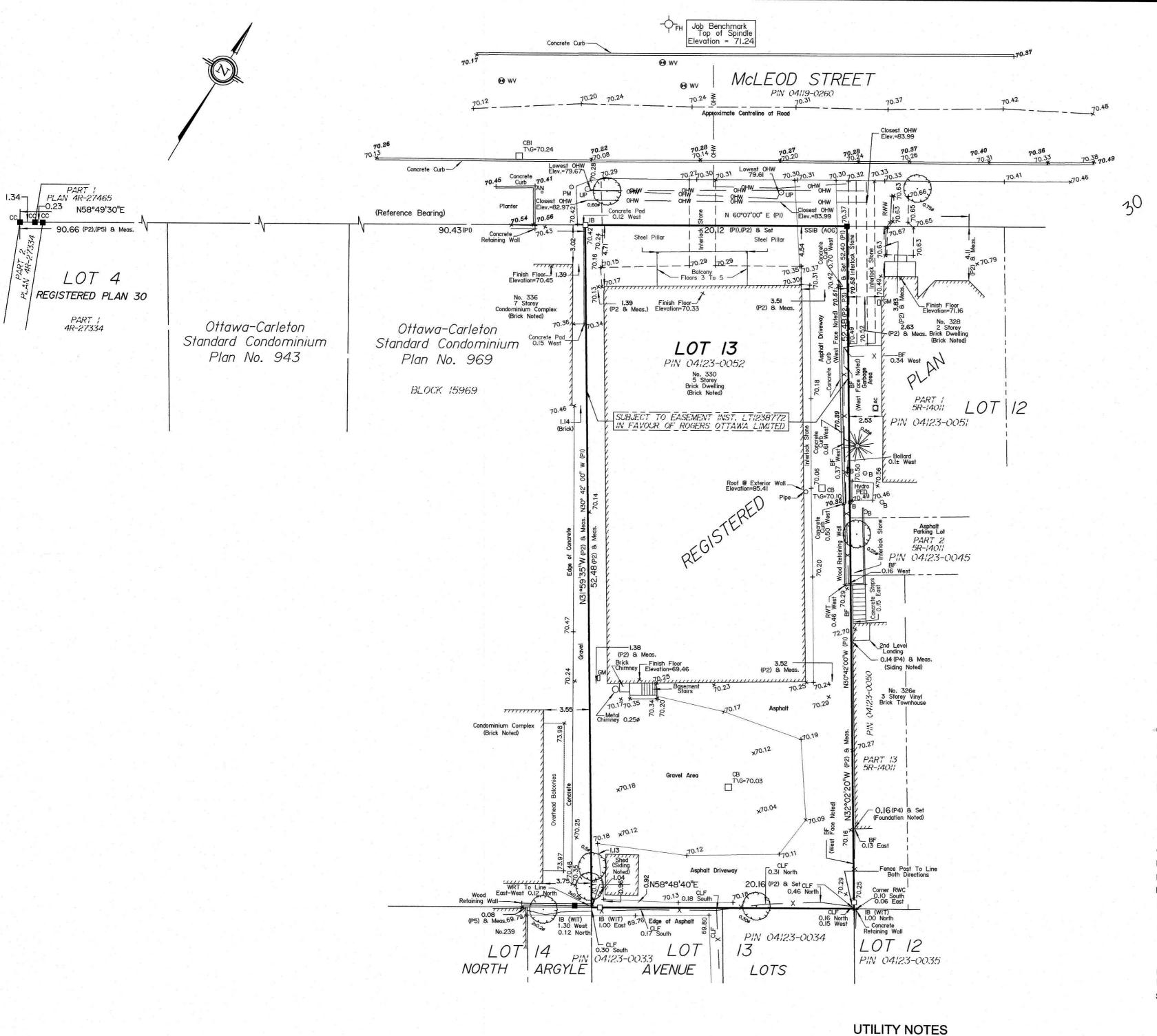
S/A	Number of copies	ADDITIONAL REQUIREMENTS			Number of copies
S	1	44. Applicant's Public Consultation Strategy (may be provided as part of the Planning Rationale)	45.Site Lighting Plan and Certification Letter	S	3

Meeting Date: February 10, 2021	Application Type: Site Plan Control /Zoning By-Law Amendme	nt
File Lead (Assigned Planner): Kimberley Baldwin	Infrastructure Approvals Project Manager: John Wu	
Site Address (Municipal Address): 233 Argyle Ave and 35	30 Mcleod Street *Preliminary Assessment: 1 2	3

*One (1) indicates that considerable major revisions are required before a planning application is submitted, while five (5) suggests that proposal appears to meet the City's key land use policies and guidelines. This assessment is purely advisory and does not consider technical aspects of the proposal or in any way guarantee application approval.

It is important to note that the need for additional studies and plans may result during application review. If following the submission of your application, it is determined that material that is not identified in this checklist is required to achieve complete application status, in accordance with the Planning Act and Official Plan requirements, the Planning, Infrastructure and Economic Development Department will notify you of outstanding material required within the required 30 day period. Mandatory pre-application consultation will not shorten the City's standard processing timelines, or guarantee that an application will be approved. It is intended to help educate and inform the applicant about submission requirements as well as municipal processes, policies, and key issues in advance of submitting a formal development application. This list is valid for one year following the meeting date. If the application is not submitted within this timeframe the applicant must again preconsult with the Planning, Infrastructure and Economic Development Department.

Visit us: Ottawa.ca/planning Visitez-nous: Ottawa.ca/urbanisme



ELEVATION NOTES

agrees with the information shown on this drawing.

1. Elevations shown are geodetic and are referred to the CGVD28 geodetic datum.

2. It is the responsibility of the user of this information to verify that the job benchmark

has not been altered or disturbed and that it's relative elevation and description

TOPOGRAPHICAL PLAN OF SURVEY OF

PART OF LOT 13 (SOUTH McLEOD STREET) **REGISTERED PLAN 30 CITY OF OTTAWA**

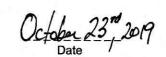
Prepared by Annis, O'Sullivan, Vollebekk Ltd.

Scale 1:200

DISTANCES SHOWN ON THIS PLAN ARE IN METRES AND CAN BE CONVERTED TO FEET BY DIVIDING BY 0.3048

Surveyor's Certificate

- 1. This survey and plan are correct and in accordance with the Surveys Act, the Surveyors Act and the Land Titles Act and the regulations made under them.
- 2. The survey was completed on the 22nd day of October, 2019.



Richard R. Gauthier Ontario Land Surveyor

Notes & Legend

		,	
De	enotes		
-0-	•	Survey Monument Planted	
		Survey Monument Found	
SIB		Standard Iron Bar	
SSIB	•	Short Standard Iron Bar	
IB		Iron Bar	
CC		Cut Cross	
CP		Concrete Pin	
(WIT)		Witness	
Meas.	"	Measured	
(AOG)	•	Annis, O'Sullivan, Vollebekk Ltd.	
(PI)	π	Registered Plan 30	
(P2)		(AOG) Plan March 25, 2004	
(P3)	и	Plan 5R-8481	
(P4)		(AOG) Plan December 7, 1989	
(P5)		Ottawa-Carleton Standard	
		Condominium Plan No.969	
PED		Hydro Pedestal	
OHW		Overhead Wires	
O UP	•	Utility Pole	
· AN		Anchor	
□ СВ		Catch Basin	
O _{FH}		Fire Hydrant	
⊗ w	D.	Water Valve	
□ GM		Gas Meter	
Ø PM	T	Parking Meter	
\bigcirc		Deciduous Tree	
		Coniferous Tree	
0 B	n	Bollard	
CLF		Chain Link Fence	
BF		Board Fence	
RWW	·	Retaining Wall Wood	
RWC	.ii	Retaining Wall Concrete	
Ø	og s	Diameter	AS
+65.00		Location of Elevations	D.
+ 65.00		Top of Concrete Curb Elevation	PL
		, and a minimum of the control of th	

Bearings are astronomic, derived from the Southerly Limit of McLeod Street, shown on to be N58°49'30"E on plan (P2). Site Area = 1056.9 square metres

SSOCIATION OF ONTARIO LAND SURVEYORS PLAN SUBMISSION FORM 2104034



THIS PLAN IS NOT VALID UNLESS IT IS AN EMBOSSED ORIGINAL COPY ISSUED BY THE SURVEYO IN ACCORDANCE WITH Regulation 1026, Section 29 (3)

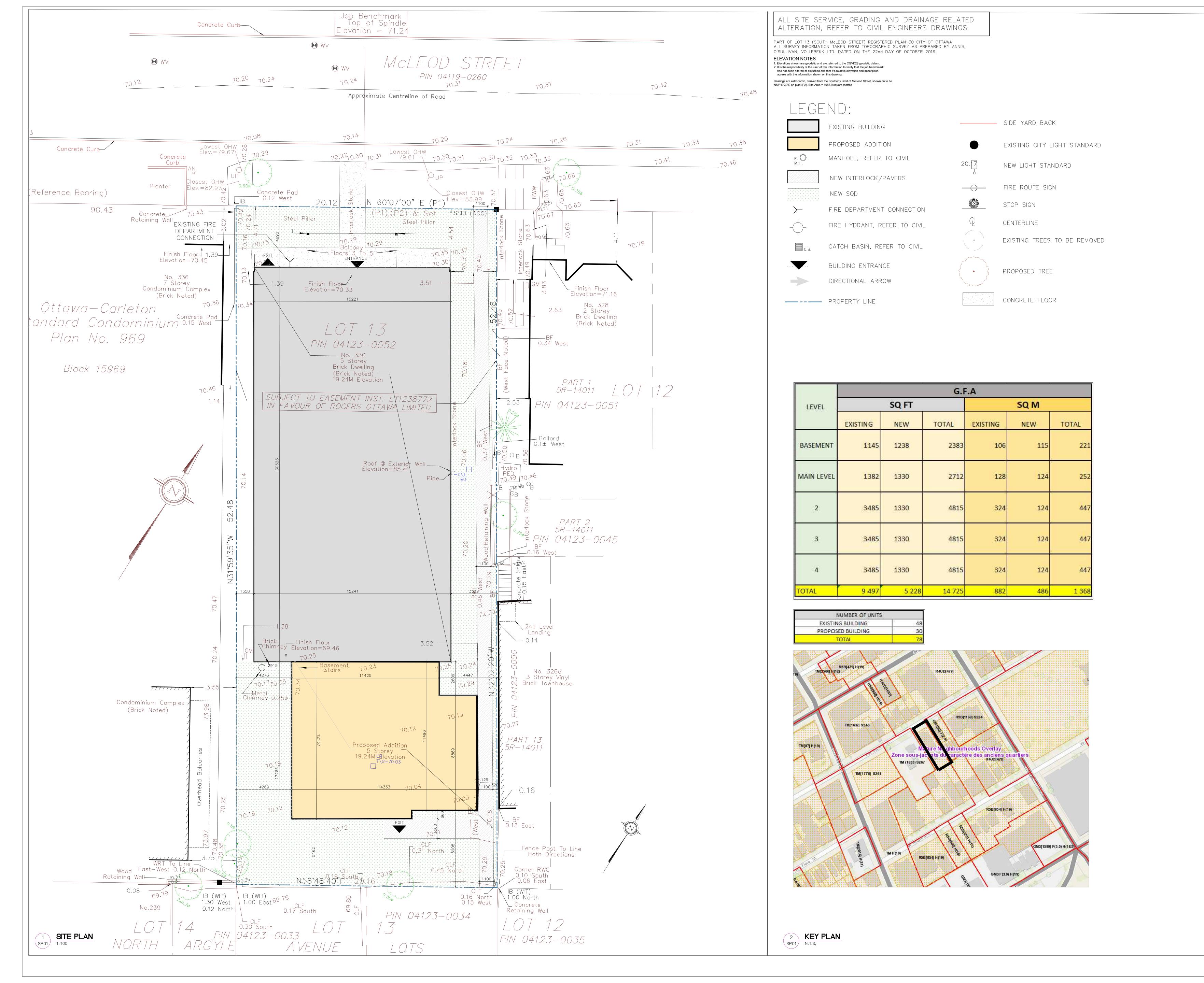
- 1. This drawing cannot be accepted as acknowledging all of the utilities and it will be the responsibility of the user to contact the respective utility authorities for confirmation.
- 2. Only visible surface utilities were located.
- 3. A field location of underground plant by the pertinent utility authority is mandatory before any work involving breaking ground, probing, excavating etc.

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ANNIS, O'SULLIVAN, VOLLEBEKK LTD. 14 Concourse Gate, Suite 500 Nepean, Ont. K2E 7S6

Phone: (613) 727-0850 / Fax: (613) 727-1079 Email: Nepean@aovltd.com

Land Surveyors Job No. 19839-19 SmartLiving Lt13 RP30 T F



EY PLAN PROJECT —

ALL CONTRACTORS TO VERIFY ALL DIMENSIONS ON SITE AND TO REPORT ALL ERRORS AND/OR

OMISSIONS TO THE ARCHITECT. ALL CONTRACTORS MUST COMPLY WITH ALL CODES AND BYLAWS AND OTHER AUTHORITIES HAVING JURISDICTION OVER THE WORK. DO NOT SCALE DRAWINGS. THIS DRAWING MAY NOT BE USED FOR CONSTRUCTION UNTIL SIGNED BY THE

ARCHITECT.

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DD/MM/YR 17/06/22 10/18/22 10/28/22 11/02/22 ISSUED FOR REVIEW

ISSUED FOR APPROVAL

ISSUED FOR COORDINATION ISSUED FOR COORDINATION





WOODMAN ARCHITECT

4 BEECHWOOD, SUITE 201 OTTAWA, ONTARIO, CANADA K1L 8L9 TEL: 613 228 9850 • FAX 613 228 9848 • mailbox@woodmanarchitect.com

TRUCTURAL -

.ECTRICAL

ANDSCAPING PROJECT

330 MCLEOD

SITE PLAN

DATE	13/05/2022	JOB NO. 2217
SC ALE	1:100	DRAWING NO.
DRAWN BY	JG/AS	∥ SP01
REVIEWED BY	RW	

Sewerteks Inc.



McINTOSH PERRY

SANITARY AND STORM SEWER CCTV CONDITION ASSESSMENT AND LOCATES JOB LOCATION: 330 MCLEOD STREET OTTAWA, ONTARIO

JOB DATE:

Tuesday, October 18, 2022

Sewerteks Inc.



Sewerteks Inc.



TABLE OF CONTENT

Cover Page	pages 1-1
Table of content	pages 2-2
Project summary	pages 3-5
Storm & Sanitary Detail Inspections	pages 6-26
Fracing Pictures	pages 27-31
Мар	pages 32-32
WRC Code Descriptions	pages 33-35

Sewerteks Inc.



Sewerteks Inc.



PROJECT SUMMARY

The following is the result from the camera inspections of the sanitary and storm sewers located at 330 McLeod Street in Ottawa. Ontario.

CLEANING

The lines were not cleaned prior to the CCTV condition assessment.

PLR

Each inspected pipe segment has a unique identification ID. This unique ID is the Pipe Line Reference ID or PLR. All the IDs are labeled in the map.

REPORT NAVIGATION

The PLR is used to navigate this report online. It's a link to the video inspection and video file. You can jump from the Summary to the actual inspection details by clicking the PLR link. The report also has a table of contents that are also link to each section of the report. In addition, the report has a link to re-direct you to the table of contents in every page.

DVD/USB DRIVE

The DVD or USB drive contains the digital report and videos.

STRUCTURAL AND OPERATIONAL DEFECTS

The following table#1 below describes the structural and operational defects of each individual pipe segment inspected identified by its unique ID or PipeLine Reference ID. The comments depict any additional information about each segment inspected.

Sewerteks Inc.





Table#1 below describes the structural and operational defects of each individual sanitary pipe segment inspected identified by its unique ID or Pipel ine Reference ID

PIPELINE REF. ID (PLR)	STRUCTURAL DEFECTS	OPERATIONAL DEFETCS	COMMENTS
<u>STM1R</u>	JDM	DE	The pipe segment is composed of No corrode pipe (paper) PVC and a clay fitting at the deviation. 10 to 30 percent water levels with 10% debris gravel sand and silt were also observed. In addition, the no corrode pipe segments are deformed about 10%, the caly fitting is offset at the turn. CB1 has a flow restrictor. The inspection ended at CB1 at 25.4 meters from CB2.
STM2	JDL, JDM, OJL, SSL	None	The wall around the No corrode pipe is broken at the start. The no corrode pipe is deformed throughout its length. In addition, the pipe has a clay fitting at the left deviation. At the deviations, there are offset joints. As a result, the inspection was abandoned at 19.6 meters from CB2.
<u>STM3R</u>	None	DE	10% debris sand, silt and gravel were observed. The inspection was abandoned at the Tee connection in the building at 0.8 meters from CB2. Note that this is the buildings foundation drain weeping tile outlet that exits at CB2.
STM4	JDM	DE	Vegetation was observed in the line. The line drops at 0.2 meters from CB3 and deviates down to possibly the line from CB (STM2) However, the inspection was abandoned at 0.8 meters at the TEE connection at 0.8 meters. The pipe material appears to be No Corrode (paper with tar).
SANTF1	JDM, SWL	None	Surface wear large in the cast iron segment. Water level changes from 0 to 25 percent. A medium offset joint And multiple pipe material changes from ABS to PVC were observed in the line. The

Sewerteks Inc.



To the table of content Page 4 of 35





Table#1 below describes the structural and operational defects of each individual sanitary pipe segment inspected identified by its unique ID or PipeLine Reference ID.

PIPELINE REF. ID (PLR) STRUCTURAL DEFECTS

OPERATIONAL DEFETCS

COMMENTS

inspection ended at the city main line in Mcleod Street at 31.4 meters from the top of the basement wahsroom toilet flange.







Date	10/18/2022	Sew	ver Type	STORM			Pipe	Size (mm)	100MM		
Client	McINTOSH PERRY				Wor	c order	•	501			
Contact	ALISON GOSLING				Pipe	Materi	ial	NO CORRODE/PVC/CLAY			
Start	CATCH BASIN 1 (CB1)				Cam	era Dir	ection	on Against Flow			
End	CB2				DVD	#/USB	B# 1				
Further Location	THE ACCESS CATCH BA SHOWN IN THE MAP OF	-) AS	Vide	Video name (PLR) STM1R.mpg			трд		
Details	SHOWN IN THE MAP OF	INIS KI	PORT.		Repo	Report No 1					
Job Address	330 MCLEOD STREET O	TTAWA,	ONTARIO		Ope	ator		Saul Ce	erna		
Comments	percent water levels with	10% de	ebris grave	el sand and	d silt were	per) PVC and a clay fitting at the deviation. 10 to 30 silt were also observed. In addition, the no corrode pipoffset at the turn. CB1 has a flow restrictor. The inspec					
	segments are deformed	about 1	,					·			
DISTANCE (m)	CODE DESCRIPTION	%		LENGTH (m)	CLOCK		ОСК	REMARKS			
	<u> </u>		SIZE	_			<u> </u>		s point CATCH BASIN 2 (CB2)		
(m)	CODE DESCRIPTION		SIZE	_			<u> </u>		s point CATCH BASIN 2 (CB2)		
(m) 0.0	CODE DESCRIPTION Start of inspection	%	SIZE	_			<u> </u>		s point CATCH BASIN 2 (CB2)		
0.0 0.0	CODE DESCRIPTION Start of inspection Water Level	% 5	SIZE	_					s point CATCH BASIN 2 (CB2)		
(m) 0.0 0.0 0.4	CODE DESCRIPTION Start of inspection Water Level Deformed Sewer	% 5	SIZE	_				Start at access	s point CATCH BASIN 2 (CB2)		
(m) 0.0 0.0 0.4 1.2	CODE DESCRIPTION Start of inspection Water Level Deformed Sewer Material Change	% 5	SIZE (mm)	_	FROM) 	Start at access	s point CATCH BASIN 2 (CB2)		
(m) 0.0 0.0 0.4 1.2 1.4	CODE DESCRIPTION Start of inspection Water Level Deformed Sewer Material Change Connection	% 5	SIZE (mm)	_	FROM		F	Start at access	s point CATCH BASIN 2 (CB2)		
(m) 0.0 0.0 0.4 1.2 1.4 1.8	CODE DESCRIPTION Start of inspection Water Level Deformed Sewer Material Change Connection Material Change	% 5 10	SIZE (mm)	_	FROM			Start at access PVC No corrode	s point CATCH BASIN 2 (CB2)		
0.0 0.0 0.4 1.2 1.4 1.8	Start of inspection Water Level Deformed Sewer Material Change Connection Material Change Debris	% 5 10	SIZE (mm)	_	FROM		F	Start at access PVC No corrode Sans/silt	s point CATCH BASIN 2 (CB2)		
(m) 0.0 0.0 0.4 1.2 1.4 1.8 1.8 3.0	Start of inspection Water Level Deformed Sewer Material Change Connection Material Change Debris Deformed Sewer	% 5 10 10	SIZE (mm)	(m)	FROM		F	Start at access PVC No corrode Sans/silt Dval	s point CATCH BASIN 2 (CB2)		
(m) 0.0 0.0 0.4 1.2 1.4 1.8 1.8 3.0 5.0	CODE DESCRIPTION Start of inspection Water Level Deformed Sewer Material Change Connection Material Change Debris Deformed Sewer Debris	% 5 10 10 10 10	SIZE (mm)	(m)	FROM		F	Start at access PVC No corrode Sans/silt Dval	s point CATCH BASIN 2 (CB2)		
(m) 0.0 0.0 0.4 1.2 1.4 1.8 1.8 3.0 5.0 6.0	Start of inspection Water Level Deformed Sewer Material Change Connection Material Change Debris Deformed Sewer Debris Water Level	% 5 10 10 10 10	SIZE (mm)	(m)	FROM		F 1 2 2 2 2 2 2 2 2 2	Start at access PVC No corrode Sans/silt Dval Gravel			
(m) 0.0 0.0 0.4 1.2 1.4 1.8 3.0 5.0 6.0 7.0	Start of inspection Water Level Deformed Sewer Material Change Connection Material Change Debris Deformed Sewer Debris Deformed Sewer Debris	% 5 10 10 10 10	SIZE (mm)	(m)	FROM			Start at access PVC No corrode Sans/silt Dval Gravel	water		
(m) 0.0 0.0 0.4 1.2 1.4 1.8 1.8 3.0 5.0 6.0 7.0 11.4	Start of inspection Water Level Deformed Sewer Material Change Connection Material Change Debris Deformed Sewer Debris Water Level Debris Water Level Debris	% 5 10 10 10 10 10	SIZE (mm)	(m)	FROM			Start at access PVC No corrode Sans/silt Dval Gravel gravel Camera under	water		

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Date	10/18/2022	Sewe	er Type	STORM		Pi	pe Size (mm)	100MM	
Client	McINTOSH PERRY	•			Work	order	501		
Contact	ALISON GOSLING				Pipe N	Material	NO COR	RODE/PVC/CLAY	
Start	CATCH BASIN 1 (CB1)				Came	ra Directio	n Against	Against Flow	
End	CB2				DVD#	/USB#	1		
Further Location	THE ACCESS CATCH BA	_		AS	Video	name (PL	R) STM1R.ı	npg	
Details	SHOWN IN THE MAP OF	· IUI2 KEI	PURT.		Repoi	rt No	1		
Job Address	330 MCLEOD STREET O	TTAWA, C	ONTARIO		Opera	itor	Saul Ce	erna	
Comments	The pipe segment is con percent water levels with segments are deformed	h 10% del	bris grave	el sand and	silt were	also obse	rved. In addition		
Comments DISTANCE (m)	percent water levels with	h 10% del	bris grave %, the cal	el sand and ly fitting is	silt were offset at t	also obse the turn. (rved. In addition	on, the no corrode pipe	
DISTANCE	percent water levels with segments are deformed	h 10% del about 10°	bris grave %, the ca	el sand and ly fitting is	I silt were offset at t	also obse the turn. (rved. In addition	on, the no corrode pipe	
DISTANCE (m)	percent water levels with segments are deformed	h 10% del about 10°	bris grave %, the cal	el sand and ly fitting is	silt were offset at t	also obse the turn. (rved. In addition the control of the	on, the no corrode pipe	
DISTANCE (m) 15.4	percent water levels with segments are deformed CODE DESCRIPTION Material Change	h 10% del about 10°	bris grave %, the cal	el sand and ly fitting is	silt were offset at t	also obse the turn. (rved. In addition the control of the	on, the no corrode pipe	
DISTANCE (m) 15.4	percent water levels with segments are deformed CODE DESCRIPTION Material Change Water Level	h 10% del about 10°	bris grave %, the cal	el sand and ly fitting is	silt were offset at t	also obse the turn. (rved. In addition	on, the no corrode pipe	
DISTANCE (m) 15.4 15.4 15.6	percent water levels with segments are deformed CODE DESCRIPTION Material Change Water Level Material Change	h 10% del about 10°	bris grave %, the cal	el sand and ly fitting is	silt were offset at t	also obse the turn. (rved. In addition	on, the no corrode pipe	
15.4 15.6 15.6	percent water levels with segments are deformed CODE DESCRIPTION Material Change Water Level Material Change Line Deviates Right	h 10% del about 10° %	bris grave %, the cal	el sand and ly fitting is LENGTH (m)	silt were offset at t	also obse the turn. (REMARKS Clay fitting No corrode	on, the no corrode pipe	
15.4 15.4 15.6 15.6 15.8	percent water levels with segments are deformed CODE DESCRIPTION Material Change Water Level Material Change Line Deviates Right Debris	h 10% del about 10° % 5	bris grave %, the cal	el sand and ly fitting is LENGTH (m)	silt were offset at t	also obse the turn. (REMARKS Clay fitting No corrode	on, the no corrode pipe	
15.4 15.4 15.6 15.6 15.8 20.8	percent water levels with segments are deformed CODE DESCRIPTION Material Change Water Level Material Change Line Deviates Right Debris Water Level	h 10% del about 10° % 5	bris grave %, the cal	el sand and ly fitting is LENGTH (m)	silt were offset at t	also obse the turn. (REMARKS Clay fitting No corrode Gravel	on, the no corrode pipe	
15.4 15.4 15.6 15.6 15.8 20.8	percent water levels with segments are deformed CODE DESCRIPTION Material Change Water Level Material Change Line Deviates Right Debris Water Level Material Change	h 10% del about 10° % 5	bris grave %, the cal	el sand and ly fitting is LENGTH (m)	silt were offset at t	also obse the turn. (REMARKS Clay fitting No corrode Gravel	on, the no corrode pipe	
15.4 15.4 15.6 15.6 15.8 20.8 22.2 22.2	percent water levels with segments are deformed CODE DESCRIPTION Material Change Water Level Material Change Line Deviates Right Debris Water Level Material Change Line Deviates Right Debris	h 10% del about 10° % 5 10 20	bris grave %, the cal	el sand and ly fitting is LENGTH (m)	silt were offset at t	also obse the turn. (REMARKS Clay fitting No corrode Gravel	on, the no corrode pipe	
DISTANCE (m) 15.4 15.4 15.6 15.6 15.8 20.8 22.2 22.2 22.2	percent water levels with segments are deformed CODE DESCRIPTION Material Change Water Level Material Change Line Deviates Right Debris Water Level Material Change Line Deviates Right Water Level Material Change Line Deviates Right Water Level	h 10% del about 10° % 5 10 20	bris grave %, the cal	el sand and ly fitting is LENGTH (m)	silt were offset at t	also obse the turn. (REMARKS Clay fitting No corrode Gravel	on, the no corrode pipe	

Sewerteks Inc.



To the table of content Page 7 of 35



PROJECT NAME VIDEO NAME

SANITARY AND STORM SEWER CCTV CONDITION ASSESSMENT AND LOCATES

STM1R

Figure#1: Start of inspection at access point CATCH BASIN 2 (CB2)



0.0



pipe's surface area lost due to the deformed pipe at 0.4 meters from the



m

Figure#5: A view to the 100mm 3 o'clock connection at 1.2 meters from the top CATCH BASIN 1 (CB1).



Figure#2: A view to the 5% water level at 0 meters from the top of CATCH BASIN 1 (CB1).

0.0

1.2



Figure#4: A view to the material change to PVC at 1.2 meters from the top of CATCH BASIN 1 (CB1).



Figure#6: A view to the material change to No corrode and sand/silt at 1.8 meters from the top of CATCH BASIN 1

1.8



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To the table of content Page 8 of 35



PROJECT NAME VIDEO NAME

SANITARY AND STORM SEWER CCTV CONDITION ASSESSMENT AND LOCATES

Figure#7: A view to the 10 % Debris sand and silt at 1.8 meters from the top of CATCH BASIN 1 (CB1).



m

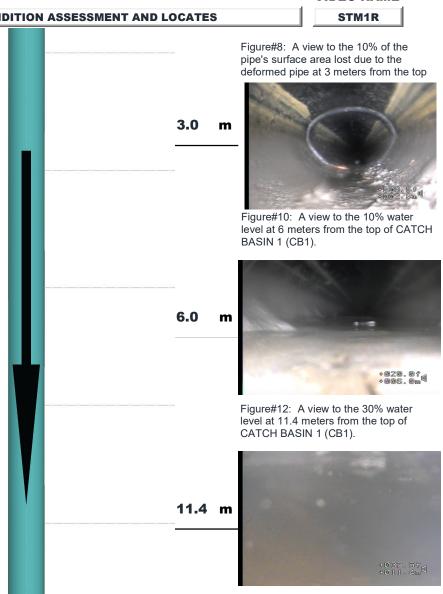
Figure#9: A view to the 10 % Debris gravel at 5.0 meters from the top of CATCH BASIN 1 (CB1).



5.0 m

Figure#11: A view to the 5 % Debris gravel at 7 meters from the top of CATCH BASIN 1 (CB1).





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To the table of content Page 9 of 35



PROJECT NAME VIDEO NAME

SANITARY AND STORM SEWER CCTV CONDITION ASSESSMENT AND LOCATES

STM1R

Figure#13: A view to the 20% water level at 13.6 meters from the top of CATCH BASIN 1 (CB1).



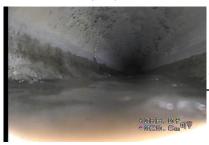
13.6 m

Figure#15: A view to the material change to No corrode at 15.4 meters from the top of CATCH BASIN 1 (CB1).



15.4 m

Figure#17: A view to the 20% water level at 20.8 meters from the top of CATCH BASIN 1 (CB1).



20.8 m

Figure#14: A view to the right line deviation, offset joint and material change to clay at 15.2 meters from the





Figure#16: A view to the 20 % Debris at 15.8 meters from the top of CATCH BASIN 1 (CB1).

15.8 m



Figure#18: A view to the material change to PVC and right deviation at 22.2 meters from the top of CATCH

22.2 m



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PROJECT NAME VIDEO NAME

SANITARY AND STORM SEWER CCTV CONDITION ASSESSMENT AND LOCATES

STM1R

Figure#19: A view to the 0% water level and material change to PVC at 22.8 meters from the top of (CB1).



22.8 m

25.4 m

Figure#20: A view to the end point CB1 and flow restrictor at 25.4 meters from the top of CATCH BASIN 1 (CB1).







Date	10/18/2022	Sewer Type	STORM		Р	ipe Size (mm)	100MM
Client	McINTOSH PERRY			Work	order	501	
Contact	ALISON GOSLING			Pipe N	/laterial	NO COF	RODE
Start	CATCH BASIN 2 (CB2)			Came	ra Directio	on With Flo	DW .
End	19.6 meters			DVD#/	USB#	1	
Further Location	THE ACCESS CATCH BASI		D AS	Video	Video name (PLR)		npg
Details	SHOWN IN THE MAI OF T	TIIS KEI OKT.		Repor	t No	1	
Job Address	330 MCLEOD STREET OTT	AWA, ONTARIO		Opera	tor	Saul C	erna
Comments	The wall around the No co length. In addition, the pip result, the inspection was	ing at the l	eft deviatio				
DISTANCE (m)	CODE DESCRIPTION	% SIZE (mm)	LENGTH (m)	CLOCK FROM	CLOCK	REMARKS	

DISTANCE (m)	CODE DESCRIPTION	%	SIZE (mm)	LENGTH (m)	CLOCK FROM	CLOCK TO	REMARKS
0.0	Start of inspection						Start at access point CATCH BASIN 2 (CB2)
0.0	Water Level	0					
0.0	General observation						Broken CB wall around outlet
2.0	Deformed Sewer	10					
4.0	General observation						Oval joint due to deformation
4.6	Deformed Sewer	10		1.0	3	9	
6.8	Surface Spalling Medium				11		Shear wall
9.0	General observation						Deformed pipe
9.6	Deformed Sewer	5			5	7	
11.6	Deformed Sewer	20					
12.0	Water Level	5					
13.4	Water Level	0					
14.0	Deformed Sewer	10					
14.2	Open Joint Large						
16.8	Line Deviates Left						

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To the table of content



Date	10/18/2022	Sewe	r Type	STORM			Pi	pe Size (mm)	100MM
Client	McINTOSH PERRY				w	ork or	der	501	
Contact	ALISON GOSLING				Pi	ре Ма	iterial	NO COR	RODE
Start	CATCH BASIN 2 (CB2)				Camera Direction			n With Flo	w
End	19.6 meters				ים	/D#/U	SB#	1	
Further Location	THE ACCESS CATCH BAS) AS	Vi	deo n	ame (PL	R) STM2.m	pg
Details	SHOWN IN THE MAP OF	INIS KEP	OKI.		R	eport l	No	1	
Job Address	330 MCLEOD STREET OT	TAWA, O	NTARIO		0	perato	or	Saul Ce	rna
Comments	The wall around the No collength. In addition, the piresult, the inspection was	pe has a	clay fitti	ng at the l	eft dev	iation			
DISTANCE (m)	CODE DESCRIPTION	%	SIZE (mm)	LENGTH (m)	CLO		CLOCK	REMARKS	
16.8	Joint Displace Large			•				Void visible	
19.4	Line Deviates Left								
19.2	Joint Displace Medium							pipe wall expos	sed
19.2	Material Change							Clay	
19.4	Material Change							No Corrode	
19.6	Survey Abandoned							Due to an angu	ılar offset joint

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To the table of content



PROJECT NAME VIDEO NAME

SANITARY AND STORM SEWER CCTV CONDITION ASSESSMENT AND LOCATES

STM2

Figure#1: Start of inspection at access point CATCH BASIN 2 (CB2)



0.0 m

Figure#3: A view to the at 0 meters from the top of CATCH BASIN 2 (CB2).



0.0 m

Figure#5: A view to the Oval joint due to deformation at 4.0 meters from the top of CATCH BASIN 2 (CB2).



4.0 m

Figure#2: A view to the 0% water level at 0.0 meters from the top of CATCH BASIN 2 (CB2).

0.0

1.8



Figure#4: A view to the 10% deformed pipe at 1.8 meters from the top of CATCH BASIN 2 (CB2).



Figure#6: A view to the 10% deformed pipe at 4.6 meters from the top of CATCH BASIN 2 (CB2).

4.6 m







PROJECT NAME VIDEO NAME

SANITARY AND STORM SEWER CCTV CONDITION ASSESSMENT AND LOCATES

m

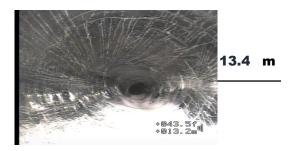
Figure#7: A view to the sheared pipe wall at 11 o'clock at 6.6 meters from the access CB2.

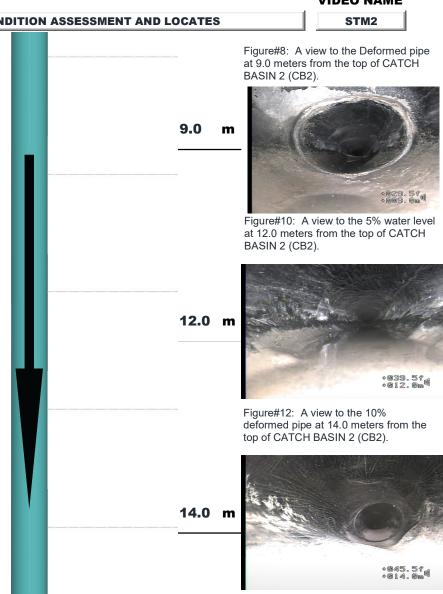


Figure#9: A view to the 20% deformed pipe at 11.4 meters from the top of CATCH BASIN 2 (CB2).



Figure#11: A view to the 0% water level and deformed pipe at 13.4 meters from the top of CATCH BASIN 2 (CB2).









PROJECT NAME VIDEO NAME

SANITARY AND STORM SEWER CCTV CONDITION ASSESSMENT AND LOCATES

STM2

Figure#13: A view to the large open joint at 14.2 meters from CB2.



14.2 m

Figure#15: A view to the joint displaced large at 16.8 meters from the top of CATCH BASIN 2 (CB2).



16.8 m

Figure#17: A view to the material change to No Corrode and offset joint at 19.2 meters from the top of CATCH



19.2 m

Figure#14: A view to the left line deviation and large angular offset joint at 16.8 meters from the top of CATCH

16.8 m

Figure#16: A view to the left line deviation, material change to clay and offsert joint at 19.2 meters from the top

m





Date	10/18/2022	Sewe	r Type	STORM			Pi	pe Size (mm)	100MM
Client	McINTOSH PERRY				Wor	k orde	r	501	
Contact	ALISON GOSLING				Pipe	Mater	rial	NO COR	RODE
Start	CATCH BASIN 2 (CB2)				Can	nera Di	rectio	n With Flo	w
End	TEE connection (0.8 METI	ERS)			DVE	#/USB	3 #	1	
Further Location	THE ACCESS CATCH BAS			D AS	Vid	eo nam	ne (PLI	R) STM3R.r	mpg
Details	SHOWN IN THE MAP OF	INIS KEP	OKI.		Rep	ort No		1	
Job Address	330 MCLEOD STREET OT	TAWA, O	NTARIO		Оре	rator		Saul Ce	rna
Comments	10% debris sand, silt and building at 0.8 meters fro CB2.								
DISTANCE (m)	CODE DESCRIPTION	%	SIZE (mm)	LENGTH (m)	CLOC	-	OCK O	REMARKS	
0.0	Start of inspection							Start at access	s point CATCH BASIN 2 (CB2)
0.0	Water Level	0							
0.0	Debris	10		0.5				Silt and sand	
0.8	Connection		100					TEE	
0.8	Survey Abandoned							Right angle tur	n.

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PROJECT NAME VIDEO NAME

SANITARY AND STORM SEWER CCTV CONDITION ASSESSMENT AND LOCATES

STM3R

0.0

Figure#3: A view to the 10 % Debris Silt and sand at 0.4 meters from the top of

Figure#1: Start of inspection at access

point CATCH BASIN 2 (CB2)



m

m

Figure#2: A view to the 0% water level and 10% debris sand/gravel and silt at 0.0 meters from the top of TEE.



Figure#4: A view to the 100 mm TEEconnection at 0.8 meters from CB2.



0.0

8.0





Date	10/18/2022	Sev	wer Type	STORM			Pipe S	ize (mm)	100MM
Client	McINTOSH PERRY				Work	order		501	
Contact	ALISON GOSLING				Pipe N	Pipe Material Corrugate			ted Plastic
Start	CATCH BASIN 3 (CB3)				Came	ra Direc	ction	With Flo	w
End	0.8 METERS				DVD#	/USB#		1	
Further Location	THE ACCESS CATCH BAS			AS	Video	name ((PLR)	STM4.m	pg
Details	SHOWN IN THE MAP OF	THIS K	EPORT.		Repoi	rt No		1	
1				Operator				Saul Cerna	
Job Address	330 MCLEOD STREET OT	ΓΤΑWA,	ONTARIO		Opera	ator		Saul Ce	rna
	Vegetation was observed	in the	line. The line	n was aba	t 0.2 mete	rs from		nd deviate	
Address	Vegetation was observed line from CB (STM2) How	in the	line. The line he inspectio No Corrode	n was aba	t 0.2 mete	rs from	eters a	nd deviate	s down to possibly the
Address Comments DISTANCE	Vegetation was observed line from CB (STM2) How The pipe material appear	in the vever, thes	line. The line he inspection No Corrode	n was aba (paper w	t 0.2 mete andoned at rith tar).	rs from t 0.8 m	eters a	nd deviate t the TEE o	s down to possibly the
Address Comments DISTANCE (m)	Vegetation was observed line from CB (STM2) How The pipe material appear	in the vever, thes	line. The line he inspection No Corrode	n was aba (paper w	t 0.2 mete andoned at rith tar).	rs from t 0.8 m	eters a	nd deviate t the TEE o	s down to possibly the connection at 0.8 meters.
Address Comments DISTANCE (m) 0.0	Vegetation was observed line from CB (STM2) How The pipe material appear CODE DESCRIPTION Start of inspection	in the vever, the second to be	line. The line he inspection No Corrode	n was aba (paper w	t 0.2 mete andoned at rith tar).	rs from t 0.8 m	CK R	nd deviate t the TEE o	s down to possibly the connection at 0.8 meters.
Address Comments DISTANCE (m) 0.0 0.0	Vegetation was observed line from CB (STM2) How The pipe material appear CODE DESCRIPTION Start of inspection Water Level	in the vever, the second to be	line. The line he inspection No Corrode	n was aba (paper w	t 0.2 mete andoned at rith tar).	rs from t 0.8 m	CK R	nd deviate t the TEE o EMARKS art at access	s down to possibly the connection at 0.8 meters.
Address Comments DISTANCE (m) 0.0 0.0 0.1	Vegetation was observed line from CB (STM2) How The pipe material appear CODE DESCRIPTION Start of inspection Water Level Debris	in the vever, the second to be	line. The line he inspection No Corrode	n was aba (paper w	t 0.2 mete andoned at rith tar).	rs from t 0.8 m	St Ve	nd deviate t the TEE of EMARKS art at access getation	s down to possibly the connection at 0.8 meters.
Address Comments DISTANCE (m) 0.0 0.0 0.1 0.2	Vegetation was observed line from CB (STM2) How The pipe material appear CODE DESCRIPTION Start of inspection Water Level Debris Line deviates down	in the vever, the second to be	line. The line he inspection No Corrode	n was aba (paper w	t 0.2 mete andoned at rith tar).	rs from t 0.8 m	St Ve	nd deviate t the TEE of EMARKS art at access getation be wall thicknown	s down to possibly the connection at 0.8 meters.

Sewerteks Inc.



To the table of content Page 19 of 35



PROJECT NAME VIDEO NAME

SANITARY AND STORM SEWER CCTV CONDITION ASSESSMENT AND LOCATES

STM4

Figure#1: Start of inspection at access point CATCH BASIN 3 (CB3)

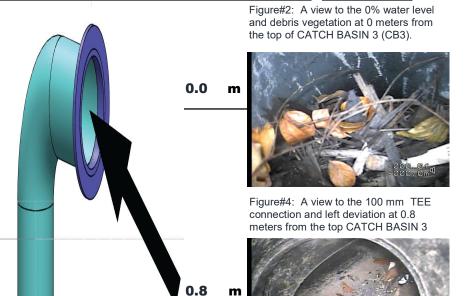


Figure#3: A view to the line deviation downwards and medium offset joint at 0.2 meters from the top of (CB3).



0.2 m

m



ľ





Date	10/18/2022	Sewer ⁻	уре	SANITA	RY	Pi	pe Size (mm)	100MM
Client	McINTOSH PERRY				Work	order	501	
Contact	ALISON GOSLING		P		Pipe I	Material	ABS/PV	
Start	TOILET FLANGE (TF1)					ra Directio	n With Flo	w
End	CITY MAIN LINE					/USB#	1	
Further Location	THE ACCESS TOILET FLA				Video	name (PL	R) SANTF1	.mpg
Details	THE MAP OF THIS REPOR		1 A3 311	OWN IN	Repo	rt No	1	
Job	330 MCLEOD STREET OT	TAWA ON	TARIO		Opera	ntor	Saul Ce	urna
Address		.,,	,		Орего		Saul Ce	cilia
Comments	Surface wear large in the And multiple pipe materia main line in Mcleod Stree	cast iron s al changes t at 31.4 m	egment. From ABS eters fro	S to PVC on the to	vel change were obse p of the b	es from 0 rved in th asement v	to 25 percent. e line. The insp vahsroom toile	A medium offset joint pection ended at the city
Comments	Surface wear large in the And multiple pipe materia	cast iron s al changes t at 31.4 m	egment. From ABS eters fro	S to PVC	vel change were obse	es from 0 rved in th asement v	to 25 percent. e line. The insp	A medium offset joint pection ended at the city
Comments	Surface wear large in the And multiple pipe materia main line in Mcleod Stree	cast iron s al changes t at 31.4 m	egment. From ABS eters fro	S to PVC on the to	vel change were obse p of the b	es from 0 rved in th asement v	to 25 percent. e line. The insp vahsroom toile	A medium offset joint pection ended at the city
Comments DISTANCE (m)	Surface wear large in the And multiple pipe materia main line in Mcleod Stree	cast iron s al changes t at 31.4 m	egment. From ABS eters fro	S to PVC on the to	vel change were obse p of the b	es from 0 rved in th asement v	to 25 percent. e line. The insp vahsroom toile	A medium offset joint pection ended at the city t flange.
Comments DISTANCE (m) 0.0	Surface wear large in the And multiple pipe materia main line in Mcleod Stree CODE DESCRIPTION Start of inspection	cast iron s al changes t at 31.4 m	egment. From ABS eters fro	S to PVC of the top th	vel change were obse p of the b	es from 0 rved in th asement v	to 25 percent. e line. The inspondent to the ins	A medium offset joint pection ended at the city t flange.
Comments DISTANCE (m) 0.0 0.0	Surface wear large in the And multiple pipe materia main line in Mcleod Stree CODE DESCRIPTION Start of inspection Line deviates down	cast iron s al changes t at 31.4 m % S	egment. From ABS eters fro	S to PVC of the top th	vel change were obse p of the b	es from 0 rved in th asement v	to 25 percent. e line. The inspondent to the ins	A medium offset joint pection ended at the city t flange.
Comments DISTANCE (m) 0.0 0.0 0.4	Surface wear large in the And multiple pipe materia main line in Mcleod Stree CODE DESCRIPTION Start of inspection Line deviates down Water Level	cast iron s al changes t at 31.4 m % S	egment. from ABS eters fro IZE L nm)	S to PVC of the top th	vel change were obse p of the be CLOCK FROM	es from 0 rved in th asement v	to 25 percent. e line. The inspondent to the ins	A medium offset joint pection ended at the city t flange.
Onments DISTANCE (m) 0.0 0.0 0.4 1.0	Surface wear large in the And multiple pipe materia main line in Mcleod Stree CODE DESCRIPTION Start of inspection Line deviates down Water Level Connection	cast iron s al changes t at 31.4 m % S	egment. from ABS eters fro IZE L nm)	S to PVC of the top th	vel change were obse p of the be CLOCK FROM	es from 0 rved in th asement v	to 25 percent. e line. The inspondent to the ins	A medium offset joint pection ended at the city t flange.
Comments DISTANCE (m) 0.0 0.0 0.4 1.0 3.4	Surface wear large in the And multiple pipe materia main line in Mcleod Stree CODE DESCRIPTION Start of inspection Line deviates down Water Level Connection Line Deviates Left	cast iron s al changes t at 31.4 m % S	egment. From ABS eters from IZE L	S to PVC of the top th	vel change were obse p of the be CLOCK FROM	es from 0 rved in th asement v	to 25 percent. e line. The inspondent to the ins	A medium offset joint pection ended at the city t flange.
Omments DISTANCE (m) 0.0 0.0 0.4 1.0 3.4 3.4	Surface wear large in the And multiple pipe materia main line in Mcleod Stree CODE DESCRIPTION Start of inspection Line deviates down Water Level Connection Line Deviates Left Connection	cast iron s al changes t at 31.4 m % S	egment. From ABS eters from IZE L	S to PVC of the top th	vel change were obse p of the be CLOCK FROM	es from 0 rved in th asement v	to 25 percent. e line. The inspends room toile REMARKS Start at acces Drop into the l	A medium offset joint pection ended at the city t flange.
0.0 0.0 0.4 1.0 3.4 3.4 3.6	Surface wear large in the And multiple pipe materia main line in Mcleod Stree CODE DESCRIPTION Start of inspection Line deviates down Water Level Connection Line Deviates Left Connection Wye into A Line	cast iron s al changes t at 31.4 m % S	egment. From ABS eters from IZE L	S to PVC of the top th	vel change were obse p of the be CLOCK FROM	es from 0 rved in th asement v	to 25 percent. e line. The inspends room toile REMARKS Start at acces Drop into the l	A medium offset joint pection ended at the city t flange.
Comments DISTANCE (m) 0.0 0.0 0.4 1.0 3.4 3.4 3.6 6.0	Surface wear large in the And multiple pipe materia main line in Mcleod Stree CODE DESCRIPTION Start of inspection Line deviates down Water Level Connection Line Deviates Left Connection Wye into A Line Line Deviates Right	cast iron s al changes t at 31.4 m % S	egment. From ABS eters from IZE L	S to PVC of the top th	vel change were obse p of the be CLOCK FROM	es from 0 rved in th asement v	to 25 percent. e line. The inspends room toile REMARKS Start at acces Drop into the l	A medium offset joint pection ended at the city t flange.

Sewerteks Inc.

150

100

Dimesion of Sewer Changes

Connection

Wye into A Line

Material Change

7.4

8.0

8.6

9.0



Deviates left

cast iron

To the table of content Page 21 of 35



Date	10/18/2022	Sew	er Type	SANITA	RY	Р	ipe Size (mm	100MM	
Client	McINTOSH PERRY				Work	order	501		
Contact	ALISON GOSLING				Pipe I	Material	ABS/	PVC	
Start	TOILET FLANGE (TF1)				Came	Camera Direction		With Flow	
End	CITY MAIN LINE				DVD#	DVD#/USB#		1	
Further Location	THE ACCESS TOILET FLA				Video	name (PL	R) SANT	F1.mpg	
Details	THE MAP OF THIS REPOR		JOM AS S	IIOWN IN	Repo	t No	1		
Job Address	330 MCLEOD STREET OT	TAWA,	ONTARIO		Opera	itor	Saul	Cerna	
Comments		al chang	es from Al	BS to PVC v	vere obse	rved in th	ne line. The	ent. A medium offset joint inspection ended at the city pilet flange.	
DISTANCE (m)	CODE DESCRIPTION	%	SIZE (mm)	LENGTH (m)	CLOCK	CLOCK	REMARI	KS	
9.0	Surface Wear Large			9.2	8	4			
11.6	Water Level	20							
12.0	Connection		150		12		1		
12.4					12				
40.4	Line Deviates Right				12				
12.4	Line Deviates Right Water Level	10			12				
14.0	· ·	10 25			12		Camera un	der water	
	Water Level				12		Camera un		
14.0	Water Level Water Level	25			12		1		
14.0 15.6	Water Level Water Level Water Level	25	100		3		Camera ab	ove water	
14.0 15.6 18.2	Water Level Water Level Water Level Material Change	25	100				Camera ab	ove water	
14.0 15.6 18.2 21.2	Water Level Water Level Water Level Material Change Connection Defective Intrudi	25	100				Camera ab Transite Possibly lin	ove water	
14.0 15.6 18.2 21.2 22.4	Water Level Water Level Water Level Material Change Connection Defective Intrudi Material Change	25	100				Camera ab Transite Possibly lin	ove water e STM2.	
14.0 15.6 18.2 21.2 22.4 22.4	Water Level Water Level Water Level Material Change Connection Defective Intrudi Material Change Joint Displace Medium	25	100				Camera ab Transite Possibly lin PVC Pipe wall th	ove water e STM2.	
14.0 15.6 18.2 21.2 22.4 22.4 30.0	Water Level Water Level Water Level Material Change Connection Defective Intrudi Material Change Joint Displace Medium Line Deviates Left Down	25	100				Camera ab Transite Possibly lin PVC Pipe wall th Gradually	ove water e STM2.	

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Finish Survey

31.4



End at CITY MAIN LINE.



PROJECT NAME VIDEO NAME

SANITARY AND STORM SEWER CCTV CONDITION ASSESSMENT AND LOCATES

SAN1

Figure#1: Start of inspection at access point TOILET FLANGE (TF1)



0.0 m

Figure#3: A view to the left line deviation at 3.0 meters from the top of TOILET FLANGE (TF1).



3.0 m

Figure#5: A view to the right line deviation at 5.8 meters from the top of TOILET FLANGE (TF1).



5.8 m

Figure#2: A view to the 5% water level at 0.6 meters from the top of TOILET FLANGE (TF1).



Figure#4: A view to the wye connection to the line CITY MAIN LINE at 3.4 meters from the top of TOILET FLANGE



Figure#6: A view to the right deviation downwards at 7 meters from the top of TOILET FLANGE (TF1).

7.0 m

0.6

3.4







PROJECT NAME VIDEO NAME

SANITARY AND STORM SEWER CCTV CONDITION ASSESSMENT AND LOCATES

SAN1

Figure#7: A view to the diameter change to 150 mm at 11 o'clock connection and left deviation at 7.8



7.4 m

Figure#9: A view to the material change to cast iron at 9 meters from the top of TOILET FLANGE (TF1).



9.0 m

Figure#11: A view to the 20% water level and 12 o'clock connection at 11.6 meters from the top of TOILET FLANGE (TF1)



Figure#8: A view to the wye connection to a line at 8.0 meters from the top of TOILET FLANGE (TF1).



Figure#10: A view to the Surface Wear Large due to corrosion at 9.6 meters from the top of TOILET FLANGE (TF1).



Figure#12: A view to the 150mm 12 o'clock connection at 11.8 meters from the top TOILET FLANGE (TF1).

11.8 m

8.0

9.6



Sewerteks Inc.





PROJECT NAME VIDEO NAME

SANITARY AND STORM SEWER CCTV CONDITION ASSESSMENT AND LOCATES

Figure#13: A view to the right line deviation at 12.0 meters from the top of TOILET FLANGE (TF1).



12.0 m

Figure#15: A view to the 10% water level at 15.6 meters from the top of TOILET FLANGE (TF1).

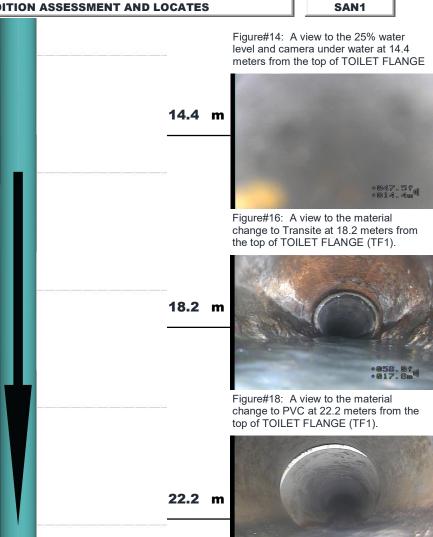


15.6 m

Figure#17: A view to the 3 o'clock connection intruding about 0.25 mm at 21.2 meters from the top of (TF1).



LINE STM2 TIES HERE



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To the table of content Page 25 of 35



PROJECT NAME VIDEO NAME

SANITARY AND STORM SEWER CCTV CONDITION ASSESSMENT AND LOCATES

SAN1

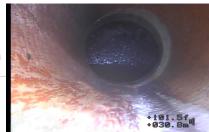
Figure#19: A view to the line deviation downwards gradually at 30.2 meters from the top of TOILET FLANGE (TF1).



30.2 m

30.8 m

Figure#20: A view to the end point CITY MAIN LINE at 30.8 meters from the top of TOILET FLANGE (TF1).





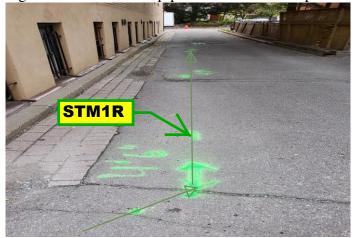


TRACING PICTURES OF 330 MCLEOD STREET

Figure#1 A view to CB1 and pipe orientation in the back of the building.



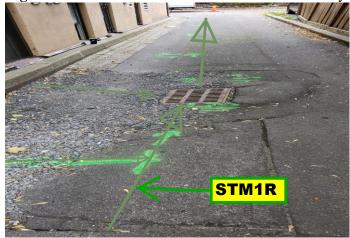
Figure#3 A view to the pipe orientation and depth



Figure#2 A view to CB1 cover with vegetation and flow restrictor



Figure#4 A view to catch basin CB2 in the driveway



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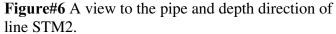




To the table of content Page 27 of 35

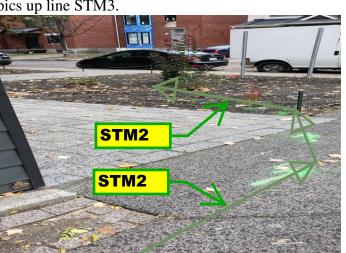


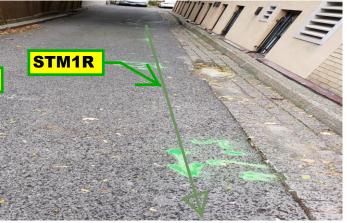
Figure#5 A view to CB2 inlets and outlet. The outlet has a flow restrictor, They are 100 mm in diameter.



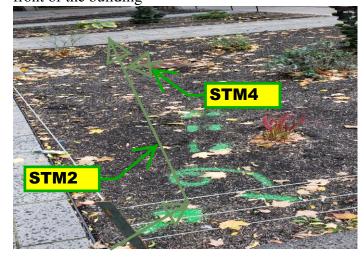


Figure#7 A view to the pipe STM2 orientation. It pics up line STM3.





Figure#8 A view to the pipe orientation and CB3 in front of the building



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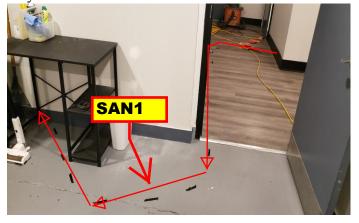
To the table of content Page 28 of 35



Figure#9: Access toilet flange and pipe direction of line SAN1. Washroom is in the basement.



Figure#11 A view to the pipe orientation in the bicycle rack room.



Figure#10: A view to the pipe SAN1 orientation in the basement



Figure#12 A view to the pipe orientation in the first floor lobby.



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< 1 > <<

To the table of content Page 29 of 35



Figure#13: Line SAN1 outside of building.



Figure#15 A view to the sanitary line in the street with its depth



Figure#14: A view to the pipe SAN1 orientation heading to the city main line.



Figure#16 The Water main feed is 38.1 mm diameter.



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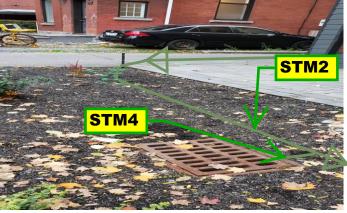




To the table of content Page 30 of 35



Figure#17: A view to CB3 located in front of the building.



Figure#19 Removed the debris and only one outlet was found.



Figure#18: A view to the pipe outlet STM4 orientation heading towards the building and not the street.



Figure#20 The Water main feed is 38.1 mm diameter.

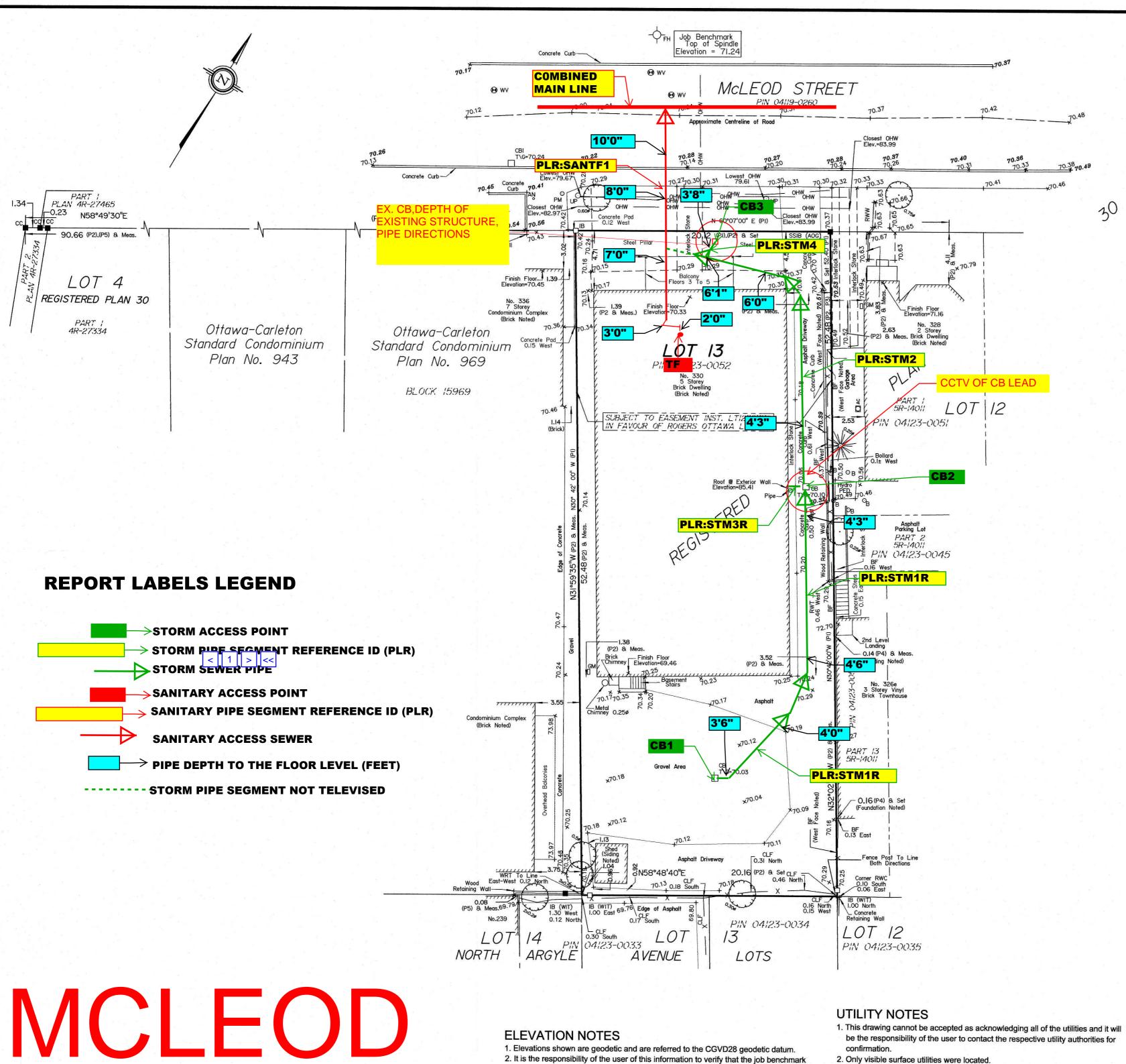


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To the table of content Page 31 of 35



TOPOGRAPHICAL PLAN OF SURVEY OF

PART OF LOT 13 (SOUTH McLEOD STREET) **REGISTERED PLAN 30 CITY OF OTTAWA**

Prepared by Annis, O'Sullivan, Vollebekk Ltd.

Scale 1:200

DISTANCES SHOWN ON THIS PLAN ARE IN METRES AND CAN BE CONVERTED TO FEET BY DIVIDING BY 0.3048

Surveyor's Certificate

- 1. This survey and plan are correct and in accordance with the Surveys Act, the Surveyors Act and the Land Titles Act and the regulations
- 2. The survey was completed on the 22nd day of October, 2019.

Richard R. Gauthier Ontario Land Surveyor

Notes & Legend

Survey Monument Planted Survey Monument Found Standard Iron Bar Short Standard Iron Bar Iron Bar CC **Cut Cross** Concrete Pin (WIT) Measured (AOG) Annis, O'Sullivan, Vollebekk Ltd. (PI) Registered Plan 30 (P2) (AOG) Plan March 25, 2004 (P3) Plan 5R-8481 (P4) (AOG) Plan December 7, 1989 (P5) Ottawa-Carleton Standard Condominium Plan No.969 Hydro Pedestal Overhead Wires **Utility Pole** Anchor ☐ CB Catch Basin Fire Hydrant Water Valve Parking Meter Coniferous Tree Bollard CLF Chain Link Fence BF **Board Fence** RWW Retaining Wall Wood **RWC** Retaining Wall Concrete Diameter Location of Elevations Top of Concrete Curb Elevation

Bearings are astronomic, derived from the Southerly Limit of McLeod Street, shown on to be N58°49'30"E on plan (P2). Site Area = 1056.9 square metres

ASSOCIATION OF ONTARIO LAND SURVEYORS PLAN SUBMISSION FORM 2104034



HIS PLAN IS NOT VALID UNLESS IT IS AN EMBOSSED ORIGINAL COPY ISSUED BY THE SURVEYO IN ACCORDANCE WITH Regulation 1026, Section 29 (3)

Land Surveyors Job No. 19839-19 SmartLiving Lt13 RP30 T F

© Annis, O'Sullivan, Vollebekk Ltd, 2019. "THIS PLAN IS PROTECTED BY COPYRIGHT" ANNIS, O'SULLIVAN, VOLLEBEKK LTD. 14 Concourse Gate, Suite 500 Nepean, Ont. K2E 7S6 Phone: (613) 727-0850 / Fax: (613) 727-1079

Email: Nepean@aovltd.com

ELEVATION NOTES

- 1. Elevations shown are geodetic and are referred to the CGVD28 geodetic datum.
- 2. It is the responsibility of the user of this information to verify that the job benchmark has not been altered or disturbed and that it's relative elevation and description agrees with the information shown on this drawing.

UTILITY NOTES

- 1. This drawing cannot be accepted as acknowledging all of the utilities and it will be the responsibility of the user to contact the respective utility authorities for
- 2. Only visible surface utilities were located.
- 3. A field location of underground plant by the pertinent utility authority is mandatory before any work involving breaking ground, probing, excavating etc.

Observations

<u>Problem</u>

Structural Condition - Brickwork

DB – Displaced Bricks DI – Dropped Invert MB – Missing Bricks

Structural Condition - Mortar Missing

MM - Mortar missing medium MS – Mortar missing slight MT – Mortar missing total

<u>Structural Condition - Surface damage</u>

SSL - Spalling large SSM - Spalling medium SSS - Spalling slight SWL - Wear large SWM - Wear medium SWS - Wear slight

<u>Structural Condition – Joint Displaced</u>

JDL – Joint Displaced Large JDM – Joint Displaced Medium

Structural Condition - Open Joint

OJL – Open Joint Large OJM – Open Joint Medium

Structural Condition – Cracked

CC – Crack Circumferential CL – Crack Longitudinal CM – Crack multiple

Structural Condition - Fractured

FC – Fracture Circumferential FL – Fracture Longitudinal FM – Fracture Multiple

Structural Condition – Broken (pipe sewers)

B- Broken H – Hole

Structural Condition – Deformed

D – Deformed Sewer

<u>Structural Condition - Collapsed</u>

X – Collapsed

Construction Features - Connection

CN – Connection

CNI – Connection intruding CX – Connection defective

CXI - Connection defective intruding

WYE - End point connection / End of a line

Construction Features – Junction

JN – Junction

JX – Junction Defective

Construction Features – Lining defect

LN – Lining defect

Construction Features – Major branch

BR – Branch major

Construction Features – Manhole/node

MH – Manhole/Node

Miscellaneous Features

CU – Camera underwater

DC – Dimension of sewers changes

GO - General Observation

GP – General Photograph

LC – Lining Change

MC – Material change

PC – Pipe length change

SC – Shape change

V – Vermin (rats and/or mice)

WL – Water Level

Service Defects - Roots

RF – Roots fine

RFJ – Roots fine at joint

RM – Roots mass

RMJ – roots mass at joint

RT – Roots tap

RJ – Roots tap at joint

Service Defects – Infiltration

ID – Infiltration dripper

IDJ – Infiltration dripper at joint

IG – Infiltration gusher

IGJ – Infiltration gusher at joint

IR – Infiltration runner

IRJ – Infiltration runner at joint

IS – Infiltration seeper

ISJ – Infiltration seeper at joint

Service Defects – Encrustation

EH – Encrustation heavy

EHJ – Encrustation heavy at joint

EL – Encrustation light

ELJ – Encrustation light at joint

EM – Encrustation medium

EMJ – Encrustation medium at joint

Service Defects – Debris

DE – Debris

DEG – Debris grease

DES - Debris silt

<u>Service Defects – Line</u>

LD – Line deviates down

LL – Line deviates left

LR – Line deviates right

LU – Line deviates up

Service Defects – Obstruction

OB – Debris grease

Other Codes

Inspections

CID – Continue inspection downstream

CIU – Continue inspection upstream

FH - Finish Survey

SA – Survey abandoned

ST – Start of Survey

Weather

- 1- Dry
- 2- Heavy Rain
- 3- Light Rain
- 4- Showers
- 5- Snow

Reasons & Purpose

- A- Structural or service condition defects
- **B-** Infiltration
- C- Assessment of complete remedial or renovation works
- D- Pre-adoption
- E- Pre-acceptance
- F- Sample survey to determine asset condition
- G- Associated with future capital scheme including drainage area planning
- H- Resurvey for any reason
- X- Other
- Z- Not known

Surface Type & Location

- A- Main road (urban)
- B- Main road (suburban/rural)
- C- Light road
- D- Footpath or verge (within the highway boundary)
- E- Fields (farmland and public open space)
- F- Gardens (within private property)
- G- Woodland
- X- Difficult access (motorway, railway, watercourse, inside building)

Pipe Type

AC – Alkathene

AK – Alkathene

BR – Brick

CC – Concrete box culvert

CI – Cast Iron

CO - Concrete

CSB – Concrete segments (bolted)

CSU – Concrete segments (unbolted)

DI – Ductile Iron

GRC – Glass reinforced cement

GRP – Glass reinforced plastic

MAC – Masonry (in regular courses)

MAR – Masonry (randomly coursed)

PE – Polyethylene

PF - Pitch fibre

PP – Polypropylene

PSC – Plastic/steel composite

PVC – Polyvinyl chloride

RPM – Reinforced plastic matrix

SI – Spun (grey) iron

ST – Steel

TRA - Transite

VC – Vitrified clay

XXX – Other

ZZZ – Not known

Pipe Shape

- A- Arched (with flat bottom)
- B- Barrel
- C- Circular
- E- Egg shaped
- H- Horseshoe
- O- Oval
- R- Rectangular
- S- Square
- T- Trapezoidal
- U- U-shaped with flat top
- X- Other

Use of Sewer

A- Combined

F- Foul

S- Surface water

T- Trade effluent

W- Watercourse (culverted)

X- Other

Z- Not known

Lining Method

BL – Bitumen

CL – Cement

CPP – Cured in place

IS – Soft inversion type liner

PL – Plastic

RL – Resin

XXX - Other

ZZ – Not known

Pre-Cleaning

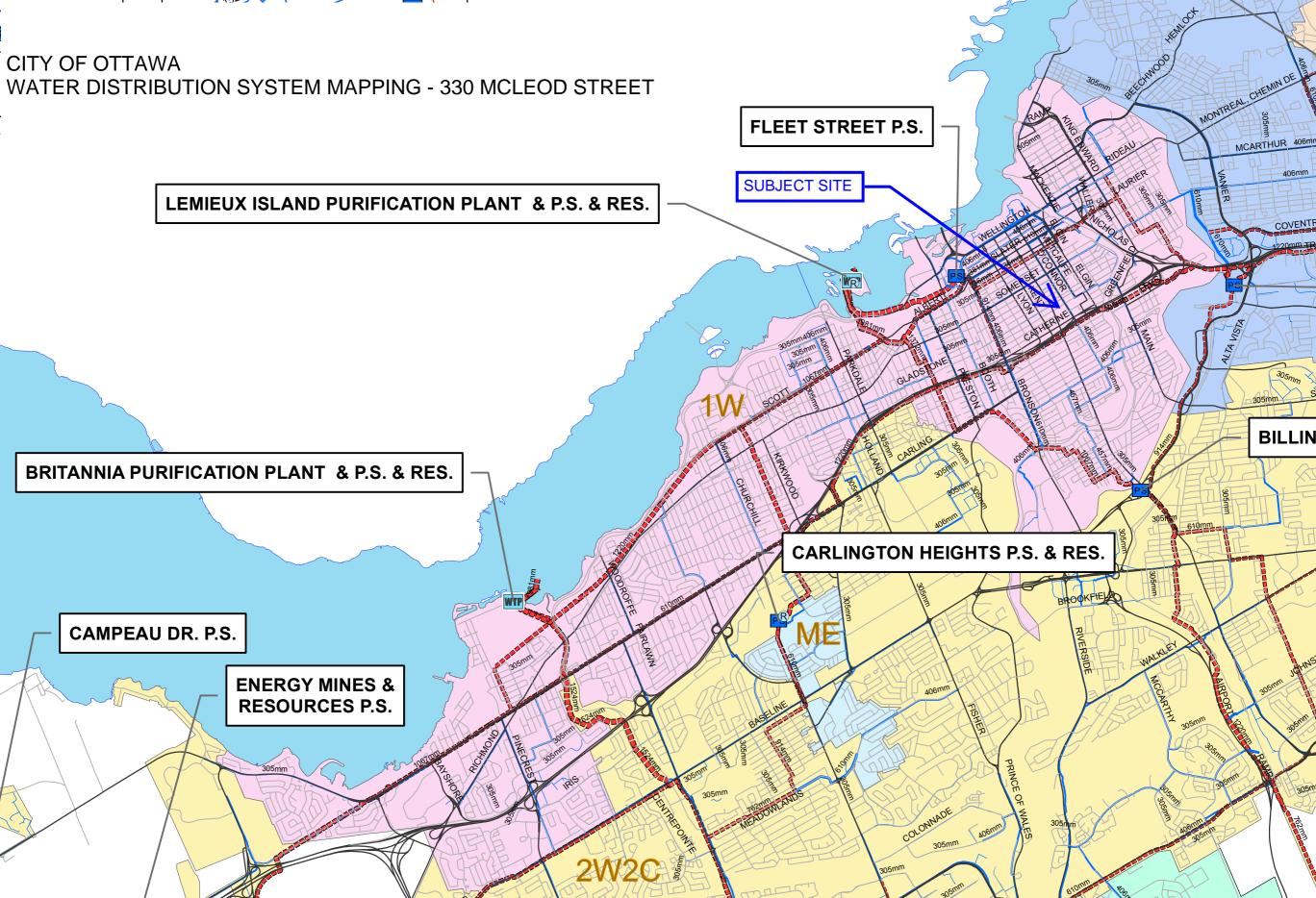
N- No pre-cleaning

Y- Pre-cleaning was carried out

Z- Not known

APPENDIX C WATERMAIN CALCULATIONS

McINTOSH PERRY



McINTOSH PERRY

000-22-1647 - 330 Mcleod Street - Proposed Water Demands

Project: 330 Mcleod Street

Project No.: 000-22-1647

Designed By: FV
Checked By: AG

Date: July 19, 2022

Site Area: 0.106 gross ha

Residential (Existing) NUMBER OF UNITS UNIT RATE

Bachelor Apartment 48 units 1.4 persons/unit

Total Population 68 persons

AVERAGE DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS	
Residential	280	L/c/d	1
Industrial - Light	35,000	L/gross ha/d	
Industrial - Heavy	55,000	L/gross ha/d	
Shopping Centres	2,500	L/ (1000m² /d	
Hospital	900	L/ (bed/ day)	1
Schools	70	L/(Student/d)	1
Trailer Park with no Hook-Ups	340	L/(space/d)	
Trailer Park with Hook-Ups	800	L/(space/d)	1
Campgrounds	225	L/(campsite/d)	1
Mobile Home Parks	1,000	L/(Space/d)	1
Motels	150	L/(bed-space/d)	1
Hotels	225	L/(bed-space/d)	1
Tourist Commercial	28,000	L/gross ha/d	1
Other Commercial	28,000	L/gross ha/d	
	Residential	0.22	L/s
AVERAGE DAILY DEMAND	Commerical/Industrial		
	/Institutional	0.00	L/s

MAXIMUM DAILY DEMAND

DEMAND TYPE	A	MOUNT	UNITS
Residential	9.5	x avg. day	L/c/d
Industrial	1.5	x avg. day	L/gross ha/d
Commercial	1.5	x avg. day	L/gross ha/d
Institutional	1.5	x avg. day	L/gross ha/d
	Residential	2.09	L/s
MAXIMUM DAILY DEMAND	Commerical/Industrial		
	/ Institutional	0.00	L/s

MAXIMUM HOUR DEMAND

DEMAND TYPE	AMOUNT		UNITS
Residential	14.3	x avg. day	L/c/d
Industrial	1.8	x max. day	L/gross ha/d
Commercial	1.8	x max. day	L/gross ha/d
Institutional	1.8	x max. day	L/gross ha/d
	Residential	3.15	L/s
MAXIMUM HOUR DEMAND	Commerical/Industrial		
	/Institutional	0.00	L/s

WATER DEMAND DESIGN FLOWS PER UNIT COUNT

CITY OF OTTAWA - WATER DISTRIBUTION GUIDELINES, JULY 2010

AVERAGE DAILY DEMAND	0.22	L/s
MAXIMUM DAILY DEMAND	2.09	L/s
MAXIMUM HOUR DEMAND	3.15	L/s

McINTOSH PERRY

000-22-1647 - 330 Mcleod Street - Proposed Water Demands

Project: 330 Mcleod Street

Project No.: COO-22-1647

Designed By: FV

Checked By: AG

Date: July 19, 2022

Ste Area: 0.106 gross ha

Residential (Proposed) NUMBER OF UNITS UNIT RATE

Bachelor Apartment 30 units 1.4 persons/unit

Total Population 42 persons

AVERAGE DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS]
Residential	280	L/c/d	1
Industrial - Light	35,000	L/ gross ha/d	
Industrial - Heavy	55,000	L/ gross ha/d	
Shopping Centres	2,500	L/ (1000m² /d	
Hospital	900	L/ (bed/day)	
Schools	70	L/(Student/d)	
Trailer Park with no Hook-Ups	340	L/(space/d)	
Trailer Park with Hook-Ups	800	L/(space/d)	
Campgrounds	225	L/(campsite/d)	
Mobile Home Parks	1,000	L/(Space/d)	
Motels	150	L/ (bed-space/d)	
Hotels	225	L/ (bed-space/d)	
Tourist Commercial	28,000	L/ gross ha/ d	
Other Commercial	28,000	L/ gross ha/ d	
	Residential	0.14	L∕s
AVERAGE DAILY DEM AND	Commerical/Industrial/		
	Institutional	0.00	L/s

MAXIMUM DAILY DEMAND

DEMAND TYPE	A	MOUNT	UNITS
Residential	9.5	x avg. day	L/c/d
Industrial	1.5	x avg. day	L/ gross ha/ d
Commercial	1.5	x avg. day	L/ gross ha/ d
Institutional	1.5	x avg. day	L/ gross ha/ d
	Residential	1.29	L/s
MAXIMUM DAILY DEMAND	Commerical/Industrial/		
	Institutional	0.00	L/s

MAXIMUM HOUR DEMAND

DBM AND TYPE	AMOUNT		UNITS
Residential	14.3	x avg. day	L/c/d
Industrial	1.8	x max. day	L/ gross ha/ d
Commercial	1.8	x max. day	L/ gross ha/ d
Institutional	1.8	x max. day	L/ gross ha/ d
	Residential	1.95	L/s
MAXIMUM HOUR DEMAND	Commerical/Industrial/		
	Institutional	0.00	L/s

WATER DEMAND DESIGN FLOWS PER UNIT COUNT CITY OF OTTAWA - WATER DISTRIBUTION GUIDELINES, JULY 2010

AVERAGE DAILY DEMAND	0.14	L/s
MAXIMUM DAILY DEMAND	1.29	L/s
MAXIMUM HOUR DEMAND	1.95	L/s

000-22-1647 - 330 Mcleod Street - Total Water Demands

 Project:
 330 Mcleod Street

 Project No.:
 COO-22-1647

 Designed By:
 FV

 Checked By:
 AG

 Date:
 July 19, 2022

 Ste Area:
 0.106 gross ha

Residential (Existing) NUMBER OF UNITS UNIT RATE

Bachelor Apartment 48 units 1.4 persons/unit

Residential (Proposed) NUMBER OF UNITS UNIT RATE

Bachelor Apartment 30 units 1.4 persons/unit

Total Population 110 persons

AVERAGE DAILY DEM AND

DEM AND TYPE	AMOUNT	UNITS	
Residential	280	L/c/d	
Industrial - Light	35,000	L/ gross ha/ d	
Industrial - Heavy	55,000	L/ gross ha/ d	
Shopping Centres	2,500	L/ (1000m² /d	
Hospital	900	L/ (bed/day)	
Schools	70	L/(Student/d)	
Trailer Park with no Hook-Ups	340	L/(space/d)	
Trailer Park with Hook-Ups	800	L/(space/d)	
Campgrounds	225	L/(campsite/d)	
Mobile Home Parks	1,000	L/(Space/d)	
Motels	150	L/ (bed-space/d)	
Hotels	225	L/ (bed-space/d)	
Tourist Commercial	28,000	L/ gross ha/ d	
Other Commercial	28,000	L/gross ha/d	
	Residential	0.36	L/s
AVERAGE DAILY DEM AND	Commerical/Industrial/		
	Institutional	0.00	L∕s

MAXIMUM DAILY DEMAND

DEMAND TYPE	AMOUNT		UNITS	
Residential	9.5	x avg. day	L/c/d	
Industrial	1.5	x avg. day	L/ gross ha/ d	
Commercial	1.5	x avg. day	L/gross ha/d	
Institutional	1.5	x avg. day	L/ gross ha/ d	
	Residential	3.39	L/s	
MAXIMUM DAILY DEMAND	Commerical/Industrial/			
	Institutional	0.00	L/s	

MAXIMUM HOUR DEMAND

DEMAND TYPE	A	MOUNT	UNITS	
Residential	14.3	x avg. day	L/c/d	
Industrial	1.8	x max. day	L/gross ha/d	
Commercial	1.8	x max. day	L/gross ha/d	
Institutional	1.8	x max. day	L/gross ha/d	
	Residential	5.10	L/s	
MAXIMUM HOUR DEMAND	Commerical/Industrial/			
	Institutional	0.00	L/s	

WATER DEMAND DESIGN FLOWS PER UNIT COUNT

CITY OF OTTAWA - WATER DISTRIBUTION GUIDELINES, JULY 2010

AVERAGE DAILY DEMAND	0.36	L/s
MAXIMUM DAILY DEMAND	3.39	L/s
MAXIMUM HOUR DEMAND	5.10	L/s

000-22-1647 - 330 Mcleod Street - OBC Fire Calculations

 Project:
 330 Mcleod Street

 Project No.:
 COO-22-1647

 Designed By:
 FV

 Checked By:
 AG

 Date:
 July 19, 2022

Ontario 2006 Building Code Compendium (Div. B - Part 3)

Water Supply for Fire-Fighting - Apartment Building

Building is classified as Group: C- Residential Occupancies

(from table 3.2.2.55)

Building is of combustible construction with fire separations and fire resistance ratings provided in accordance with Subsection 3.2.2., including loadbearing walls, columns and arches. Noncombustible construction may be used in lieu of fire-resistance

From Div. B A-3.2.5.7. of the Ontario Building Code - 3. Building On-Ste Water Supply:

(a) $Q = K \times V \times Stot$

where:

Q = minimum supply of water in litres

K = water supply coefficient from Table 1

V = total building volume in cubic metres

Stot = total of spatial coefficient values from the property line exposures on all sides as obtained from the formula:

Stot = 1.0 + [Sside1 + Sside2 + Sside3 + ...etc.]

К	18	(from Table 1 pg A-31)
V	11,717	(Total building volume in m³.)
Stot	2.0	(From figure 1 pg A-32)
Q=	421,817.76	L

From Figure
1 (A-32)

Shorth
4.54 m 0.5
Seast 0.3 m 0.5
Seouth
4.45 m 0.5
Swest 1.35 m 0.5

* approximate distances

From Table 2: Required Minimum Water Supply Flow Rate (L/ s)

9000 L/min if Q > 270,000 L 2378 gpm

000-22-1647 - 330 Moleod Street - Fire Underwriters Survey

 Project:
 330 Mcleod Greet

 Project No.:
 CCC-22-1647

 Designed By:
 FV

 Checked By:
 AG

 Date:
 July 19, 2022

From the Fire Underwriters Survey (2020)

From Part II – Guide for Determination of Required Fire Flow Copyright I.S.O.: City of Ottawa Technical Bulletin ISTB-2018-02 Applied Where Applicable

A. BASE REQUIREMENT (Rounded to the nearest 1000 L/min)

 $F = 220 \times C \times VA$ Where: F = Required fire flow in liters per minute

C = Coefficient related to the type of construction.

A = The total floor area in square meters (including all storey's, but excluding basements at least 50 percent below grade)

in the building being considered.

Construction Type Non-Combustible Construction

C 0.8 A 2,435.0 m²

Total Floor Area (per the 2020 FUS Page 20 - Total Effective Area) 1,827.0 m²

 Calculated Fire Flow
 7,522.8 L/ min

 8,000.0 L/ min
 8,000.0 L/ min

B. REDUCTION FOR OCCUPANCY TYPE (No Rounding)

From Page 24 of the Fire Underwriters Survey:

Limited Combustible -15%

Fire Flow 6.800.0 L/min

C. REDUCTION FOR SPRINKLER TYPE (No Rounding)

10.1 to 20

E Total Fire Flow (Rounded to the Nearest 1000 L/min)

Exposure 3

Exposure 4

Standard Water Supply Sprinklered -40%

Feduction				-2,720.0	⊔ min		
D. INCRE	ASE FOR EXPOSURE (No Rounding)						
	Separation Distance (m)	Cons.of Exposed Wall	Length Exposed Adjacent Wall (m)	Height (Stories)	Length-Height Factor		
Exposure 1	20.1 to 30	Wood frame	10.1	2	20.2	0%	
Exposure 2	0 to 3	Wood frame	17	3	51.0	22%	

7.79

3

23.4

11%

 0 to 3
 Wood frame
 47.2
 7
 330.4
 25%

 % Increase*
 58%

Increase* 3,944.0 L/min

Wood frame

Hre How 8.024.0 U

^{*} In accordance with Part II, Section 4, the Increase for separation distance is not to exceed 75%

^{**} In accordance with Section 4 the Fire flow is not to exceed 45,000 L/min or be less than 2,000 L/min

000-22-1647 - 330 Mcleod Street - Boundary Condition Unit Conversion

 Project:
 330 Mcleod Street

 Project No.:
 COO-22-1647

 Designed By:
 FV

 Checked By:
 AG

 Date:
 July 19, 2022

Boundary Conditions Unit Conversion

Mcleod Street

Scenario	Height (m)	Elevation (m)	m H₂O	PSI	kPa
Avg. DD	115.3	70.2	45.1	64.1	442.0
Fire Flow (150 L/s or 9,000 L/min)	105.6	70.2	35.4	50.3	346.9
Peak Hour	106.8	70.2	36.6	52.0	358.7

Alison Gosling

From: Wu, John <John.Wu@ottawa.ca> **Sent:** September 7, 2021 1:25 PM

To: Alison Gosling

Subject: RE: 22-1647 330 McLeod Street - Boundary Condition Request

Attachments: 330 McLeod Street September 2021.pdf

Follow Up Flag: Follow up Flag Status: Flagged

Here is the result:

****The following information may be passed on to the consultant, but do NOT forward this e-mail directly.****

The following are boundary conditions, HGL, for hydraulic analysis at 330 McLeod Street (zone 1W) assumed connected to the 203 mm watermain on McLeod Street (see attached PDF for location).

Minimum HGL: 106.8 m Maximum HGL: 115.3 m

Max Day + FF (150 L/s): 105.6 m

These are for current conditions and are based on computer model simulation.

Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation.

John

From: Alison Gosling <a.gosling@mcintoshperry.com>

Sent: August 30, 2021 4:22 PM
To: Wu, John < John. Wu@ottawa.ca>

Subject: 22-1647 330 McLeod Street - Boundary Condition Request

CAUTION: This email originated from an External Sender. Please do not click links or open attachments unless you recognize the source.

ATTENTION : Ce courriel provient d'un expéditeur externe. Ne cliquez sur aucun lien et n'ouvrez pas de pièce jointe, excepté si vous connaissez l'expéditeur.

Good afternoon John,

We would like to request Boundary Conditions for the proposed site located at 330 McLeod Street. The proposed development consists of a 4-storey building addition containing 30 units to the existing building containing 47 units. The proposed connection will be to the existing 203mm dia. watermain within McLeod Street.

- The estimated fire flow is 9,000 L/min based on the FUS
- The estimated fire flow is 2,700 L/min based on the OBC
- Average daily demand: 0.14 L/s OR 0.35 L/s with the existing building
- Maximum daily demand: 1.29 L/s OR 3.33 L/s with the existing building
- Maximum hourly daily demand: 1.95 L/s OR 5.01 L/s with the existing building

Attached is a map showing the proposed connection location along with the calculations prepared for the demands listed above.

Please let me know if you have any questions.

Thank you,

Alison Gosling, P.Eng.

Project Engineer, Land Development
115 Walgreen Road, Carp, ON, K0A 1L0
T. 613.714.4629
a.gosling@mcintoshperry.com | www.mcintoshperry.com

McINTOSH PERRY

Turning Possibilities Into Reality





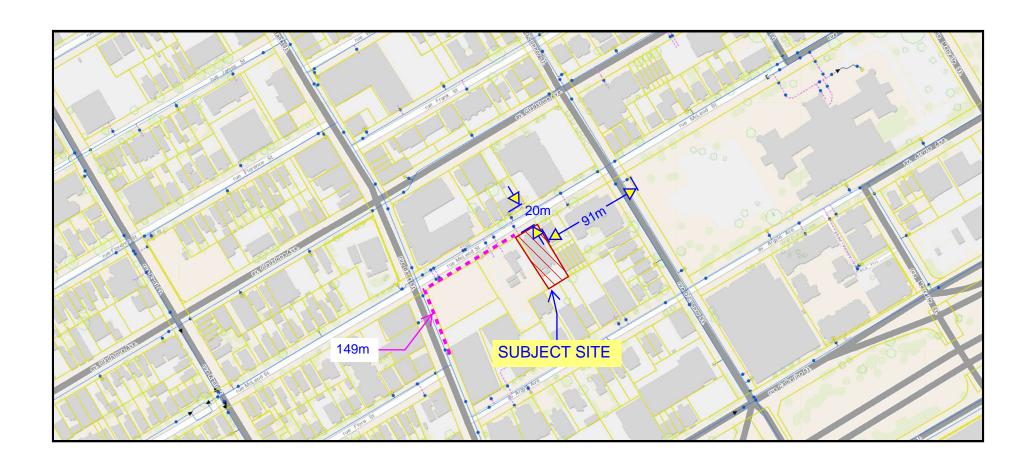
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330 McLeod Street Hydrant Coverage Figure



https://maps.ottawa.ca/geoOttawa/

APPENDIX D SANITARY CALCULATIONS

00-22-1647 - 330 McLeod Street - Sanitary Demands - Existing

Project: 330 McLeod Street Project No.: O-22-1647 AJG Designed By: Checked By: AJG Date: July 18, 2022 Ste Area 0.106 Gross ha Bachelor 48 1.40 Persons per unit Total Population 68 Persons

DESIGN PARAMETERS

Residential Peaking Factor 3.63 * Using Harmon Formula = $1+(14/(4+P^0.5))*0.8$

where P = population in thousands, Harmon's Correction Factor = 0.8

Mannings coefficient (n)0.013Demand (per capita)280L/dayInfiltration allowance0.33L/s/Ha

EXTRANEOUS FLOW ALLOWANCES

Infiltration / Inflow	How (L/s)
Dry	0.005
Wet	0.030
Total	0.035

AVERAGE DAILY DEM AND

DEM AND TYPE	AMOUNT	UNITS	POPULATION / AREA	Flow (L/s)
Residential	280	L/ c/ d	68	0.220
Industrial - Light**	35,000	L/ gross ha/ d		0
Industrial - Heavy* *	55,000	L/ gross ha/ d		0
Commercial / Amenity	2,800	L/(1000m ² /d)		0
Hospital	900	L/(bed/day)		0
Schools	70	L/(Student/d)		0
Trailer Parks no Hook-Ups	340	L/(space/d)		0
Trailer Park with Hook-Ups	800	L/(space/d)		0
Campgrounds	225	L/ (campsite/d)		0
Mobile Home Parks	1,000	L/(Space/d)		0
Motels	150	L/ (bed-space/d)		0
Hotels	225	L/ (bed-space/d)		0
Office	75	L/7.0m ² /d		0
Tourist Commercial	28,000	L/ gross ha/ d		0
Other Commercial	28,000	L/ gross ha/ d		0

AVERAGE RESIDENTIAL FLOW	0.220	L/s	
PEAK RESIDENTIAL FLOW	0.800	L/s	
AVERAGE ICI FLOW	0.00	L/s	
PEAK INSTITUTIONAL/ COMMERCIAL FLOW	0.00	L/s	
PEAK INDUSTRIAL FLOW	0.00	L/s	
TOTAL PEAK ICI FLOW	0.00	L/s	

TOTAL SANITARY DEMAND

TOTAL ESTIMATED AVERAGE DRY WEATHER FLOW	0.23	L/s
TOTAL ESTIMATED PEAK DRY WEATHER FLOW	0.80	L/s
TOTAL ESTIMATED PEAK WET WEATHER FLOW	0.83	L/s

OO-22-1647 - 330 McLeod Street - Sanitary Demands - Proposed Building Addition

Project: 330 McLeod Street Project No.: O-22-1647 AJG Designed By: Checked By: AJG Date: July 18, 2022 Ste Area 0.106 Gross ha Bachelor 30 1.40 Persons per unit **Total Population** 42 Persons

DESIGN PARAMETERS

Pesidential Peaking Factor 3.66 * Using Harmon Formula = $1+(14/(4+P^{N}0.5))*0.8$

where P = population in thousands, Harmon's Correction Factor = 0.8

Mannings coefficient (n) 0.013

Demand (per capita) 280 L/day Infiltration allowance 0.33 L/s/Ha Groundwater Contamination 10000 L/day

* Per Paterson Group Memo

EXTRANEOUS FLOW ALLOWANCES

	Infiltration / Inflow	How (L/s)
ſ	Dry	0.005
ſ	Wet	0.145
Ī	Total	0.151

AVERAGE DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS	POPULATION / AREA	Flow (L/s)
Residential	280	L/ c/ d	42	0.136
Industrial - Light**	35,000	L/ gross ha/ d		0
Industrial - Heavy**	55,000	L/ gross ha/ d		0
Commercial / Amenity	2,800	L/(1000m²/d)		0
Hospital	900	L/ (bed/day)		0
Schools	70	L/(Student/d)		0
Trailer Parks no Hook-Ups	340	L/ (space/d)		0
Trailer Park with Hook-Ups	800	L/(space/d)		0
Campgrounds	225	L/ (campsite/d)		0
Mobile Home Parks	1,000	L/ (Space/d)		0
Motels	150	L/ (bed-space/d)		0
Hotels	225	L/ (bed-space/d)		0
Office	75	L/7.0m ² /d		0
Tourist Commercial	28,000	L/ gross ha/ d		0
Other Commercial	28,000	L/ gross ha/ d		0

AVERAGE RESIDENTIAL FLOW	0.14	L/s
PEAK RESIDENTIAL FLOW	0.50	L/s
AVERAGE ICI FLOW	0.00	L/s
PEAK INSTITUTIONAL/ COMMERCIAL FLOW	0.00	L/s
PEAK INDUSTRIAL FLOW	0.00	L/s
TOTAL PEAK ICI FLOW	0.00	L/s

TOTAL SANITARY DEMAND

TOTAL ESTIMATED AVERAGE DRY WEATHER FLOW	0.14	L/s
TOTAL ESTIMATED PEAK DRY WEATHER FLOW	0.50	L/s
TOTAL ESTIMATED PEAK WET WEATHER FLOW	0.65	L/s

00-22-1647 - 330 McLeod Street - Sanitary Demands - Total

Project: 330 McLeod Street Project No.: O-22-1647 AJG Designed By: AJG Checked By: Date: July 18, 2022

Ste Area 0.106 Gross ha Bachelor 78 1.40 Persons per unit

Total Population 110 Persons

DESIGN PARAMETERS

Institutional/Commercial Peaking Factor 1.5

Residential Peaking Factor 3.59 * Using Harmon Formula = $1+(14/(4+P^{0.5}))*0.8$

where P = population in thousands, Harmon's Correction Factor = 0.8

Mannings coefficient (n) 0.013

Demand (per capita) 280 L/day Infiltration allowance 0.33 L/s/Ha Groundwater Contamination 10000 L/day

* Per Paterson Group Memo

EXTRANEOUS FLOW ALLOWANCES

Infiltration / Inflow	Flow (L/s)
Dry	0.005
Wet	0.145
Total	0.151

AVERAGE DAILY DEM AND

DEMAND TYPE	AMOUNT	UNITS	POPULATION / AREA	Flow (L/s)
Residential	280	L/ c/ d	110	0.356
Industrial - Light**	35,000	L/gross ha/d		0
Industrial - Heavy**	55,000	L/gross ha/d		0
Commercial / Amenity	2,800	L/(1000m ² /d)		0
Hospital	900	L/(bed/day)		0
Schools	70	L/(Student/d)		0
Trailer Parks no Hook-Ups	340	L/(space/d)		0
Trailer Park with Hook-Ups	800	L/(space/d)		0
Campgrounds	225	L/ (campsite/d)		0
Mobile Home Parks	1,000	L/(Space/d)		0
Motels	150	L/(bed-space/d)		0
Hotels	225	L/(bed-space/d)		0
Office	75	L/7.0m ² /d		0
Tourist Commercial	28,000	L/ gross ha/ d		0
Other Commercial	28,000	L/gross ha/d		0

AVERAGE RESIDENTIAL FLOW	0.36	L/s
PEAK RESIDENTIAL FLOW	1.28	L/s
AVERAGEICI FLOW	0.000	L/s
PEAK INSTITUTIONAL/ COMMERCIAL FLOW	0.000	L/s
PEAK INDUSTRIAL FLOW	0.000	L/s
TOTAL PEAK ICI FLOW	0.000	L/s

TOTAL SANITARY DEMAND

TOTAL ESTIMATED AVERAGE DRY WEATHER FLOW	0.36	L/s
TOTAL ESTIMATED PEAK DRY WEATHER FLOW	1.28	L/s
TOTAL ESTIMATED PEAK WET WEATHER FLOW	1.43	L/s

Francis Valenti

Subject: FW: 233 Argyle / 330 McLeod Technical Comments

From: Mark D'Arcy < mdarcy@patersongroup.ca>

Sent: July 13, 2022 5:36 PM

To: Alison Gosling <a.gosling@mcintoshperry.com>
Co: dallarosa@fotenn.com; warren@fotenn.com

Subject: FW: 233 Argyle / 330 McLeod Technical Comments

Hi Alison,

I had Kevin here look at your request for flow rates and below is what he has estimated.

Should you require anything else in this regard, please let us know.

Regards

Mark D'Arcy, P.Eng. QPESA Director – Environmental Division

patersongroup

solution oriented engineering over 60 years serving our clients

New regulations for excess soil are in effect January 1, 2021; ask us how we can help

9 Auriga Drive

Ottawa, Ontario, K2E 7T9 Tel: (613) 226-7381 Ext. (207)

From: Kevin Pickard < KPickard@patersongroup.ca>

Sent: July 13, 2022 3:08 PM

To: Mark D'Arcy <mdarcy@patersongroup.ca>

Cc: Mike Laflamme < MLaflamme@patersongroup.ca > Subject: RE: 233 Argyle / 330 McLeod Technical Comments

Hi Mark,

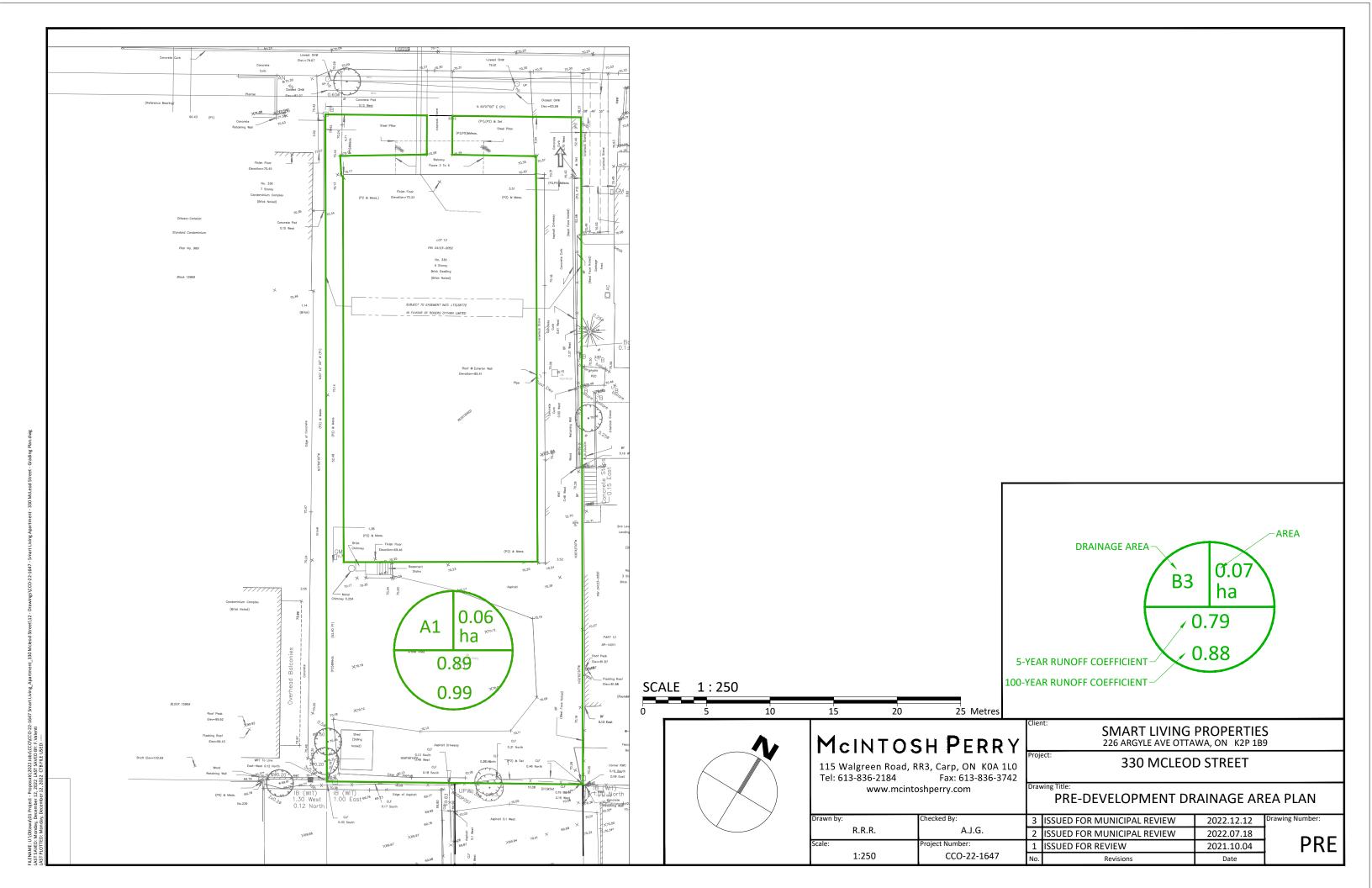
Based on the hydraulic conductivity of the grey silty clay expected at the underside of footing elevation and the anticipated size of the building addition, we should expect that less the 10 m3/day or 10,000L/day of water will be directed to the city sanitary sewer from the building addition.

Pleases let me know if you need anything else.

Thanks,

Kevin Pickard, EIT Project Manager – Geotechnical Department

APPENDIX E PRE-DEVELOPMENT DRAINAGE PLAN



APPENDIX F POST-DEVELOPMENT DRAINAGE PLAN

APPENDIX G STORMWATER MANAGEMENT CALCULATIONS

CCO-22-1647 - 330 McLeod Street - Runoff Calculations

1 of 4

Pre-Development Runoff Coefficient

Drainage Area	Area (ha)	Impervious Area (m²)	С	Gravel Area (m²)	С	Pervious Area (m²)	С	C _{AVG} 2/5-Year	C _{AVG} 100-Year
A1	0.056	555.09	0.90	0.00	0.60	7.13	0.20	0.89	0.99

Pre-Development Runoff Calculations

Drainage	Area		C Tc						Q		
Area	(ha)				(mm/hr)				(L/s)		
Alea	(IIa)	J- Teal	100-Teal	(111111)	2-Year	5-Year	100-Year	2-Year	5-Year	100-Year	
A1	0.056	0.89	0.99	10	76.8	104.2	178.6	10.7	14.51	27.64	
Total	0.056							10.70	14.51	27.64	

Post-Development Runoff Coefficient

Drainage Area	Area (ha)	Impervious Area (m²)	С	Gravel Area (m²)	С	Pervious Area (m²)	С	C _{AVG} 2/5-Year	C _{AVG} 100-Year
B1	0.016	163.10	0.90	0.00	0.60	0.00	0.20	0.90	1.00
B2	0.040	68.82	0.90	0.00	0.60	306.26	0.20	0.31	0.36

Post-Development Runoff Calculations

Drainage Area	Area (ha)	C 2/5-Year	C 100-Year	Tc (min)		l n/hr)		Q /s)
Area (na) 2/5-fear	2/ 5- Teal	100-Teal	(111111)	5-Year	100-Year	5-Year	100-Year	
B1	0.016	0.90	1.00	10	104.2	178.6	4.25	8.10
B2	0.040	0.31	0.36	10	104.2	178.6	3.57	7.22
Total	0.056						7.82	15.31

Required Restricted Flow

Drainage Area	Area (ha)	C 5-Year	Tc (min)	l (mm/ hr) 2-Year	Q (L/ s) 2-Year
A1	0.056	0.40	10	76.8	4.80

Post-Development Restricted Runoff Calculations

Drainage Area		cted Flow /s)		ed Row s)	_	Required n ³)		Provided า ³)	
Alea	5-Year	100-Year	5-Year	100-Year	5-Year	100-Year	5-Year	100-Year	
B1	4.25	8.10	0.38	0.76	3.47	6.42	3.67	7.34	Restricted
B2	3.57	7.22	3.57	7.22					Unrestricted
Total	7.82	15.31	3.95	7.98	3.47	6.42	3.67	7.34	

CCO-22-1647 - 330 McLeod Street - Runoff Calculations

2 of 4

Storage Requirements for Area B1

5-Year Storm Event

Tc (min)	l (mm/hr)	B1 Runoff (L/s)	Allowable Outflow (L/s)	Runoff to be Stored (L/s)	Storage Required (m³)
10	104.2	4.25	0.38	3.87	2.32
20	70.3	2.87	0.38	2.49	2.98
30	53.9	2.20	0.38	1.82	3.28
40	44.2	1.80	0.38	1.42	3.42
50	37.7	1.54	0.38	1.16	3.47
60	32.9	1.34	0.38	0.96	3.47
70	29.4	1.20	0.38	0.82	3.44
80	26.6	1.08	0.38	0.70	3.38
90	24.3	0.99	0.38	0.61	3.30
100	22.4	0.91	0.38	0.53	3.21

Maximum Storage Required 5-Year (m³) =

3.47

100-Year Storm Event

Tc (min)	l (mm/hr)	B1 Runoff (L/s)	Allowable Outflow (L/s)	Runoff to be Stored (L/s)	Storage Required (m³)
10	178.6	8.10	0.76	7.34	4.40
20	120.0	5.44	0.76	4.68	5.61
30	91.9	4.17	0.76	3.41	6.13
40	75.1	3.41	0.76	2.65	6.35
50	64.0	2.90	0.76	2.14	6.42
60	55.9	2.53	0.76	1.77	6.39
70	49.8	2.26	0.76	1.50	6.29
80	45.0	2.04	0.76	1.28	6.14

Maximum Storage Required 100-Year (m³) =

6.42

Storage Occupied In Area B1

5-Year Storm Event

o roar aonn	o roar aonn Evon					
Roof Storage						
Location	Area*	Depth	Volume (m³)			
Roof	122.33	0.030	3.67			
		Total	3.67			

100-Year Storm Event

100 Todi domi Evoni						
Roof Storage						
Location	Area*	Depth	Volume (m³)			
Roof	122.33	0.060	7.34			
		Total	7.34			

3.67

3.47

Storage Available (m³) =

Storage Required (m³) =

^{*}Storage area is 75% of the total roof area

CCO-22-1647 - 330 McLeod Street - Runoff Calculations

Roof Drain Flow (B1)

) (I					
Roof Drains Summary					
Type of Control Device Watts Drainage - Accutrol Weir					
Number of Roof Drains	1				
	5-Year	100-Year			
Pooftop Storage (m ³)	3.67	7.34			
Storage Depth (m)	0.030	0.060			
How (Per Roof Drain) (L/s)	0.38	0.76			
Total How (L/s)	0.38	0.76			

Flow Pate Vs. Build-Up (One Weir)				
Depth (mm)	How (L/s)			
15	0.19			
20	0.25			
25	0.32			
30	0.38			
35	0.44			
40	0.50			
45	0.57			
50	0.63			
55	0.69			

^{*} Roof Drain model to be Accutrol Weirs, See attached sheets

CALCULATING ROOF FLOW EXAMPLES

2 roof drains during a 5 year storm elevation of water = 30mm How leaving 2 roof drains = $(2 \times 0.36 \text{ L/s}) = 0.72 \text{ L/s}$

2 roof drains during a 100 year storm elevation of water = 45mm How leaving 2 roof drains = $(2 \times 0.54 \text{ L/s}) = 1.08 \text{ L/s}$

	Roof Drain How					
	How (I/s)	Storage Depth (mm)	Drains How (I/s)			
	0.19	15	0.19			
	0.25	20	0.25			
	0.32	25	0.32			
5-Year	0.38	30	0.38			
	0.44	35	0.44			
	0.50	40	0.50			
	0.57	45	0.57			
	0.63	50	0.63			
	0.69	55	0.69			
100-Year	0.76	60	0.76			
	0.82	65	0.82			
	0.88	70	0.88			
	0.95	75	0.95			
	1.01	80	1.01			
	1.07	85	1.07			
	1.13	90	1.13			
	1.20	95	1.20			
	1.26	100	1.26			
	1.32	105	1.32			
	1.39	110	1.39			
	1.45	115	1.45			
	1.51	120	1.51			
	1.58	125	1.58			
	1.64	130	1.64			
	1.70	135	1.70			
	1.76	140	1.76			
	1.83	145	1.83			
	1.89	150	1.89			

3 of 4

 $\underline{\text{Note:}}$ The flow leaving through a restricted roof drain is based on flow vs. head information

^{*} Roof Drain Row information taken from Watts Drainage website

CCO-22-1647 - 330 McLeod Street - Runoff Calculations

4 of 4

Time of Concentration Pre-Development

Drainage Area	Sheet Flow	Slope of	Tc (min)	Tc (min)
ID	Distance (m)	Land (%)	(5-Year)	(100-Year)
A1	65	1.20	5	5

* Therefore, a Tc of 10 can be used

 $Tc = (3.26(1.1-c)L^0.5/S^0.33)$

c= Balanced Runoff Coefficient
L= Length of Drainage Area
S= Average Sope of Watershed

APPENDIX H CITY OF OTTAWA DESIGN CHECKLIST

City of Ottawa

4. Development Servicing Study Checklist

The following section describes the checklist of the required content of servicing studies. It is expected that the proponent will address each one of the following items for the study to be deemed complete and ready for review by City of Ottawa Infrastructure Approvals staff.

The level of required detail in the Servicing Study will increase depending on the type of application. For example, for Official Plan amendments and re-zoning applications, the main issues will be to determine the capacity requirements for the proposed change in land use and confirm this against the existing capacity constraint, and to define the solutions, phasing of works and the financing of works to address the capacity constraint. For subdivisions and site plans, the above will be required with additional detailed information supporting the servicing within the development boundary.

4.1 General Content

Criteria	Location (if applicable)
☐ Executive Summary (for larger reports only).	N/A
☐ Date and revision number of the report.	On Cover
 Location map and plan showing municipal address, boundary, and layout of proposed development. 	Appendix A
☐ Plan showing the site and location of all existing services.	Site Servicing Plan (C102)
 Development statistics, land use, density, adherence to zoning and official plan, and reference to applicable subwatershed and watershed plans that provide context to which individual 	1.1 Purpose 1.2 Site Description
developments must adhere.	6.0 Stormwater Management
☐ Summary of pre-consultation meetings with City and other approval agencies.	Appendix B
☐ Reference and confirm conformance to higher level studies and reports (Master Servicing Studies, Environmental Assessments,	1.1 Purpose
Community Design Plans), or in the case where it is not in conformance, the proponent must provide justification and	1.2 Site Description
develop a defendable design criteria.	6.0 Stormwater Management
☐ Statement of objectives and servicing criteria.	3.0 Pre-Consultation Summary



☐ Identification of existing and proposed infrastructure available in the immediate area.	N/A
☐ Identification of Environmentally Significant Areas, watercourses and Municipal Drains potentially impacted by the proposed development (Reference can be made to the Natural Heritage Studies, if available).	Site Grading Plan (C101)
Concept level master grading plan to confirm existing and proposed grades in the development. This is required to confirm the feasibility of proposed stormwater management and drainage, soil removal and fill constraints, and potential impacts to neighbouring properties. This is also required to confirm that the proposed grading will not impede existing major system flow paths.	Site Grading Plan (C101)
☐ Identification of potential impacts of proposed piped services on private services (such as wells and septic fields on adjacent lands) and mitigation required to address potential impacts.	N/A
☐ Proposed phasing of the development, if applicable.	N/A
☐ Reference to geotechnical studies and recommendations concerning servicing.	Section 2.0 Background Studies, Standards and References
 All preliminary and formal site plan submissions should have the following information: Metric scale North arrow (including construction North) Key plan Name and contact information of applicant and property owner Property limits including bearings and dimensions Existing and proposed structures and parking areas Easements, road widening and rights-of-way Adjacent street names 	Site Grading Plan (C101)

4.2 Development Servicing Report: Water

Criteria	Location (if applicable)
☐ Confirm consistency with Master Servicing Study, if available	N/A
Availability of public infrastructure to service proposed development	N/A
☐ Identification of system constraints	N/A
☐ Identify boundary conditions	Appendix C
☐ Confirmation of adequate domestic supply and pressure	N/A
 Confirmation of adequate fire flow protection and confirmation that fire flow is calculated as per the Fire Underwriter's Survey. Output should show available fire flow at locations throughout the development. 	Appendix C
 Provide a check of high pressures. If pressure is found to be high, an assessment is required to confirm the application of pressure reducing valves. 	N/A
 Definition of phasing constraints. Hydraulic modeling is required to confirm servicing for all defined phases of the project including the ultimate design 	N/A
☐ Address reliability requirements such as appropriate location of shut-off valves	N/A
☐ Check on the necessity of a pressure zone boundary modification.	N/A
Reference to water supply analysis to show that major infrastructure is capable of delivering sufficient water for the proposed land use. This includes data that shows that the expected demands under average day, peak hour and fire flow conditions provide water within the required pressure range	Appendix C, Section 4.2

Description of the proposed water distribution network, including locations of proposed connections to the existing system, provisions for necessary looping, and appurtenances (valves, pressure reducing valves, valve chambers, and fire hydrants) including special metering provisions.	Site Servicing Plan (C101)
 Description of off-site required feedermains, booster pumping stations, and other water infrastructure that will be ultimately required to service proposed development, including financing, interim facilities, and timing of implementation. 	N/A
☐ Confirmation that water demands are calculated based on the City of Ottawa Design Guidelines.	Appendix C
 Provision of a model schematic showing the boundary conditions locations, streets, parcels, and building locations for reference. 	N/A

4.3 Development Servicing Report: Wastewater

Criteria	Location (if applicable)
☐ Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitored flow data from relatively new infrastructure cannot be used to justify capacity requirements for proposed infrastructure).	N/A
☐ Confirm consistency with Master Servicing Study and/or justifications for deviations.	N/A
Consideration of local conditions that may contribute to extraneous flows that are higher than the recommended flows in the guidelines. This includes groundwater and soil conditions, and age and condition of sewers.	N/A
Description of existing sanitary sewer available for discharge of wastewater from proposed development.	Section 5.2 Proposed Sanitary Sewer

☐ Verify available capacity in downstream sanitary sewer and/or identification of upgrades necessary to service the proposed development. (Reference can be made to previously completed Master Servicing Study if applicable)	Section 5.3 Proposed Sanitary Design
☐ Calculations related to dry-weather and wet-weather flow rates from the development in standard MOE sanitary sewer design table (Appendix 'C') format.	N/A
 Description of proposed sewer network including sewers, pumping stations, and forcemains. 	Section 5.2 Proposed Sanitary Sewer
Discussion of previously identified environmental constraints and impact on servicing (environmental constraints are related to limitations imposed on the development in order to preserve the physical condition of watercourses, vegetation, soil cover, as well as protecting against water quantity and quality).	N/A
 Pumping stations: impacts of proposed development on existing pumping stations or requirements for new pumping station to service development. 	N/A
☐ Forcemain capacity in terms of operational redundancy, surge pressure and maximum flow velocity.	N/A
☐ Identification and implementation of the emergency overflow from sanitary pumping stations in relation to the hydraulic grade line to protect against basement flooding.	N/A
☐ Special considerations such as contamination, corrosive environment etc.	N/A

4.4 Development Servicing Report: Stormwater Checklist

Criteria	Location (if applicable)
 Description of drainage outlets and downstream constraints including legality of outlets (i.e. municipal drain, right-of-way, watercourse, or private property) 	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
☐ Analysis of available capacity in existing public infrastructure.	N/A
☐ A drawing showing the subject lands, its surroundings, the receiving watercourse, existing drainage patterns, and proposed drainage pattern.	Pre & Post-Development Plans
☐ Water quantity control objective (e.g. controlling post-development peak flows to pre-development level for storm events ranging from the 2 or 5-year event (dependent on the receiving sewer design) to 100-year return period); if other objectives are being applied, a rationale must be included with reference to hydrologic analyses of the potentially affected subwatersheds, taking into account long-term cumulative effects.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
☐ Water Quality control objective (basic, normal or enhanced level of protection based on the sensitivities of the receiving watercourse) and storage requirements.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
 Description of the stormwater management concept with facility locations and descriptions with references and supporting information. 	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
☐ Set-back from private sewage disposal systems.	N/A
☐ Watercourse and hazard lands setbacks.	N/A
Record of pre-consultation with the Ontario Ministry of Environment and the Conservation Authority that has jurisdiction on the affected watershed.	N/A
☐ Confirm consistency with sub-watershed and Master Servicing Study, if applicable study exists.	N/A
☐ Storage requirements (complete with calculations) and conveyance capacity for minor events (1:5-year return period) and major events (1:100-year return period).	Appendix G

☐ Identification of watercourses within the proposed development and how watercourses will be protected, or, if necessary, altered by the proposed development with applicable approvals.	Site Grading Plan
☐ Calculate pre-and post development peak flow rates including a description of existing site conditions and proposed impervious areas and drainage catchments in comparison to existing conditions.	Section 7.0 Proposed Stormwater Management Appendix G
☐ Any proposed diversion of drainage catchment areas from one outlet to another.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
 Proposed minor and major systems including locations and sizes of stormwater trunk sewers, and stormwater management facilities. 	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
☐ If quantity control is not proposed, demonstration that downstream system has adequate capacity for the post-development flows up to and including the 100-year return period storm event.	N/A
☐ Identification of potential impacts to receiving watercourses	N/A
 Identification of municipal drains and related approval requirements. 	N/A
 Descriptions of how the conveyance and storage capacity will be achieved for the development. 	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
100-year flood levels and major flow routing to protect proposed development from flooding for establishing minimum building elevations (MBE) and overall grading.	Site Grading Plan (C101)
☐ Inclusion of hydraulic analysis including hydraulic grade line elevations.	N/A

 Description of approach to erosion and sediment control during construction for the protection of receiving watercourse or drainage corridors. 	Section 8.0 Sediment & Erosion Control
☐ Identification of floodplains — proponent to obtain relevant floodplain information from the appropriate Conservation Authority. The proponent may be required to delineate floodplain elevations to the satisfaction of the Conservation Authority if such information is not available or if information does not match current conditions.	N/A
☐ Identification of fill constraints related to floodplain and geotechnical investigation.	N/A

4.5 Approval and Permit Requirements: Checklist

The Servicing Study shall provide a list of applicable permits and regulatory approvals necessary for the proposed development as well as the relevant issues affecting each approval. The approval and permitting shall include but not be limited to the following:

Criteria	Location (if applicable)
☐ Conservation Authority as the designated approval agency for modification of floodplain, potential impact on fish habitat, proposed works in or adjacent to a watercourse, cut/fill permits and Approval under Lakes and Rivers Improvement Act. The Conservation Authority is not the approval authority for the Lakes and Rivers Improvement Act. Where there are Conservation Authority regulations in place, approval under the Lakes and Rivers Improvement Act is not required, except in cases of dams as defined in the Act.	N/A
☐ Application for Certificate of Approval (CofA) under the Ontario Water Resources Act.	N/A
☐ Changes to Municipal Drains.	N/A
 Other permits (National Capital Commission, Parks Canada, Public Works and Government Services Canada, Ministry of Transportation etc.) 	N/A

4.6 Conclusion Checklist

Criteria	Location (if applicable)
Clearly stated conclusions and recommendations	Section 9.0 Summary
	Section 10.0 Recommendations
☐ Comments received from review agencies including the City of Ottawa and information on how the comments were addressed. Final sign-off from the responsible reviewing agency.	All are stamped
☐ All draft and final reports shall be signed and stamped by a professional Engineer registered in Ontario	All are stamped