

**ROADWAY TRAFFIC NOISE
ASSESSMENT**

3277 St. Joseph Boulevard
Ottawa, Ontario

REPORT: 21-401 – Traffic Noise



December 16, 2021

PREPARED FOR

Landric Homes

63 Montreal Road E

Gatineau, QC

J8M 1K3

PREPARED BY

Michael Lafortune, C.E.T., Environmental Scientist

Joshua Foster, P.Eng., Lead Engineer

EXECUTIVE SUMMARY

This report describes a roadway traffic noise assessment undertaken in support of site plan application for a proposed development located at 3277 St. Joseph Boulevard in Ottawa, Ontario. The proposed development comprises two nine-storey residential buildings with three levels of below-grade parking below each building. The building located to the east of the site (Building A) contains a floorplate change along the north elevation at level five, and an entrance to the southeast corner of the building. The second building to the west (Building B) is rectangular shaped and extends as far as the building to the east before the floorplate change. An outdoor amenity area is provided on roof of the five-storey component of Building A. The major sources of traffic noise are Highway 174, Tenth Line Road and St. Joseph Boulevard. Figure 1 illustrates a complete site plan with surrounding context.

The assessment is based on (i) theoretical noise prediction methods that conform to the Ministry of the Environment, Conservation and Parks (MECP) and City of Ottawa requirements; (ii) noise level criteria as specified by the City of Ottawa's Environmental Noise Control Guidelines (ENCG); (iii) future vehicular traffic volumes based on the City of Ottawa's Official Plan roadway classifications; and (iv) architectural drawings prepared by Rossmann Architecture.

The results of the current analysis indicate that noise levels will range between 67 and 73 dBA during the daytime period (07:00-23:00) and between 59 and 66 dBA during the nighttime period (23:00-07:00). The highest noise level (73 dBA) occurs at the east and south façades of Building A, which are nearest and most exposed to Tenth Line Road and St. Joseph Boulevard. Building components with a higher Sound Transmission Class (STC) rating will be required where exterior noise levels exceed 65 dBA, as indicated in Figure 3.

Results of the calculations also indicate that the development will require central air conditioning, which will allow occupants to keep windows closed and maintain a comfortable living environment. The following Type D Warning Clause will also be required be placed on all Lease, Purchase and Sale Agreements, as summarized in Section 6.

Noise levels at the Building A 6th Floor terrace (Receptor 7) are expected to approach 68 dBA during the daytime period. If this area is to be used as an outdoor living area, noise control measures are required to



reduce the L_{eq} to 60 dBA, and as close to 55 dBA as feasibly possible. Further analysis investigated the noise mitigating impact of surrounding the terrace with a 1.5 m noise barrier (base case) to 4.6 m above the walking surface. Results of the investigation proved that noise levels can only feasibly be reduced to 65 dBA. Reducing noise levels to 55 dBA would require excessive barrier heights that would not be feasible. Noise barriers must be constructed from materials having a minimum surface density of 20 kg/m² (STC rating of 30) and contain no gaps. Design of the guardrail will conform to the requirements outlined in Part 5 of the ENCG. The following information will be required by the City for review prior to installation of the barrier:

1. Shop drawings, signed and sealed by a qualified Professional Engineer licenced by the Professional Engineers of Ontario, showing the details of the acoustic barrier systems components, including material specifications.
2. Structural drawing(s), signed by a qualified Professional Engineer licenced by the Professional Engineers of Ontario, showing foundation details and specifying design criteria, climatic design loads, as well as applicable geotechnical data used in the design.
3. Layout plan, and wall elevations, showing proposed colours and patterns.

Regarding stationary noise, impacts from the surroundings on the study building are expected to be minimal. There are no significant sources of stationary noise in the area, and the study site is subject to elevated background noise levels from roadway traffic sources. Impacts from the development on the surroundings can be minimized by judicious placement mechanical equipment such as its placement on a roof or in a mechanical penthouse, or the incorporation of silencers and noise screens as necessary. It is recommended that any large pieces of HVAC equipment be placed in the middle of the roof, avoiding line of site with the surrounding residential dwellings.

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1. INTRODUCTION

Gradient Wind Engineering Inc. (Gradient Wind) was retained by Landric Homes to undertake a roadway traffic noise assessment in support of site plan application for a proposed development at 3277 St. Joseph Boulevard in Ottawa, Ontario. This report summarizes the methodology, results, and recommendations related to the assessment of exterior and interior noise levels generated by local roadway traffic.

Our work is based on theoretical noise calculation methods conforming to the City of Ottawa¹ and Ministry of the Environment, Conservation and Parks (MECP)² guidelines. Noise calculations were based on architectural drawings prepared by Rossmann Architecture, with future traffic volumes corresponding to the City of Ottawa's Official Plan (OP) roadway classifications.

2. TERMS OF REFERENCE

The proposed development comprises two nine-storey residential buildings with three levels of below-grade parking below each building. The building located to the east of the site (Building A) contains a floorplate change along the north elevation at level five, and an entrance to the southeast corner of the building. The second building to the west (Building B) is rectangular shaped and extends as far as the building to the east before the floorplate change. An outdoor amenity area is provided on roof of the five-storey component of Building A.

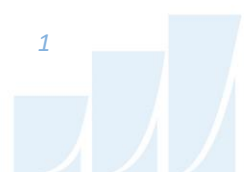
The site is surrounded by low-rise residential buildings in all directions. The major sources of traffic noise are Highway 174, Tenth Line Road and St. Joseph Boulevard. Figure 1 illustrates a complete site plan with surrounding context.

3. OBJECTIVES

The principal objectives of this study are to (i) calculate the future noise levels on the study buildings produced by local roadway traffic, and (ii) ensure that interior and exterior noise levels do not exceed the

¹ City of Ottawa Environmental Noise Control Guidelines, January 2016

² Ontario Ministry of the Environment and Climate Change – Environmental Noise Guidelines, Publication NPC-300, Queens Printer for Ontario, Toronto, 2013



allowable limits specified by the City of Ottawa's Environmental Noise Control Guidelines as outlined in Section 4.2 of this report.

4. METHODOLOGY

4.1 Background

Noise can be defined as any obtrusive sound. It is created at a source, transmitted through a medium, such as air, and intercepted by a receiver. Noise may be characterized in terms of the power of the source or the sound pressure at a specific distance. While the power of a source is characteristic of that particular source, the sound pressure depends on the location of the receiver and the path that the noise takes to reach the receiver. Measurement of noise is based on the decibel unit, dBA, which is a logarithmic ratio referenced to a standard noise level (2×10^{-5} Pascals). The 'A' suffix refers to a weighting scale, which better represents how the noise is perceived by the human ear. With this scale, a doubling of power results in a 3 dBA increase in measured noise levels and is just perceptible to most people. An increase of 10 dBA is often perceived to be twice as loud.

4.2 Roadway Traffic Noise

4.2.1 Criteria for Roadway Traffic Noise

For surface roadway traffic noise, the equivalent sound energy level, L_{eq} , provides a measure of the time varying noise levels, which is well correlated with the annoyance of sound. It is defined as the continuous sound level, which has the same energy as a time varying noise level over a period of time. For roadways, the L_{eq} is commonly calculated on the basis of a 16-hour (L_{eq16}) daytime (07:00-23:00) / 8-hour (L_{eq8}) nighttime (23:00-07:00) split to assess its impact on residential buildings. The City of Ottawa's Environmental Noise Control Guidelines (ENCG) specifies that the recommended indoor noise limit range (that is relevant to this study) is 45 and 40 dBA for living rooms and sleeping quarters respectively for roadway as listed in Table 1.



TABLE 1: INDOOR SOUND LEVEL CRITERIA (ROAD)³

Type of Space	Time Period	Leq (dBA)
General offices, reception areas, retail stores, etc.	07:00 – 23:00	50
Living/dining/den areas of residences , hospitals, schools, nursing/retirement homes, day-care centres, theatres, places of worship, libraries, individual or semi-private offices, conference rooms, etc.	07:00 – 23:00	45
Sleeping quarters of hotels/motels	23:00 – 07:00	45
Sleeping quarters of residences , hospitals, nursing/retirement homes, etc.	23:00 – 07:00	40

Predicted noise levels at the plane of window (POW) dictate the action required to achieve the recommended sound levels. An open window is considered to provide a 10 dBA reduction in noise, while a standard closed window is capable of providing a minimum 20 dBA noise reduction⁴. A closed window due to a ventilation requirement will bring noise levels down to achieve an acceptable indoor environment⁵. Therefore, where noise levels exceed 55 dBA daytime and 50 dBA nighttime, the ventilation for the building should consider the need for having windows and doors closed, which triggers the need for forced air heating with provision for central air conditioning. Where noise levels exceed 65 dBA daytime and 60 dBA nighttime, air conditioning will be required and building components will require higher levels of sound attenuation⁶.

The sound level criterion for outdoor living areas is 55 dBA, which applies during the daytime (07:00 to 23:00). When noise levels exceed 55 dBA, mitigation must be provided to reduce noise levels where technically and administratively feasible to acceptable levels at or below the criterion.

³ Adapted from ENCG 2016 – Tables 2.2b and 2.2c

⁴ Burberry, P.B. (2014). Mitchell’s Environment and Services. Routledge, Page 125

⁵ MECP, Environmental Noise Guidelines, NPC 300 – Part C, Section 7.8

⁶ MECP, Environmental Noise Guidelines, NPC 300 – Part C, Section 7.1.3

4.2.2 Theoretical Roadway Noise Predictions

Noise predictions were performed with the aid of the MECP computerized noise assessment program, STAMSON 5.04, for road analysis. Appendix A includes the STAMSON 5.04 input and output data.

Roadway traffic noise calculations were performed by treating each roadway segment as separate line sources of noise. In addition to the traffic volumes summarized in Table 2, theoretical noise predictions were based on the following parameters:

- Truck traffic on all roadways was taken to comprise 5% heavy trucks and 7% medium trucks, as per ENCG requirements for noise level predictions.
- The day/night split for all streets was taken to be 92%/8%, respectively.
- Ground surfaces were taken to be reflective or absorptive based on intermediate ground characteristics.
- Topography was assumed to be a flat/gentle slope surrounding the study building. Highway 174 is approximately 4 m below local grade at the study site.
- Noise receptors were strategically placed at 7 locations around the study area (see Figure 2).
- Receptor distances and exposure angles are illustrated in Figures 4-6.

4.2.3 Roadway Traffic Volumes

The ENCG dictates that noise calculations should consider future sound levels based on a roadway's classification at the mature state of development. Therefore, traffic volumes are based on the roadway classifications outlined in the City of Ottawa's Official Plan (OP) and Transportation Master Plan⁷ which provide additional details on future roadway expansions. Average Annual Daily Traffic (AADT) volumes are then based on data in Table B1 of the ENCG for each roadway classification. Table 2 (below) summarizes the AADT values used for each roadway included in this assessment.

⁷ City of Ottawa Transportation Master Plan, November 2013

TABLE 2: ROADWAY TRAFFIC DATA

Segment	Roadway Traffic Data	Speed Limit (km/h)	Traffic Volumes
Highway 174	6-Lane Freeway	100	110,000
Tenth Line Road	4-Lane Urban Arterial Divided (4-UAD)	60	35,000
St. Joseph Boulevard	4-Lane Urban Arterial Divided (4-UAD)	60	35,000

4.3 Indoor Noise Calculations

The difference between outdoor and indoor noise levels is the noise attenuation provided by the building envelope. According to common industry practice, complete walls and individual wall elements are rated according to the Sound Transmission Class (STC). The STC ratings of common residential walls built in conformance with the Ontario Building Code (2012) typically exceed STC 35, depending on exterior cladding, thickness and interior finish details. For example, brick veneer walls can achieve STC 50 or more. Standard commercially sided exterior metal stud walls have around STC 45. Standard good quality double-glazed non-operable windows can have STC ratings ranging from 25 to 40, depending on the window manufacturer, pane thickness and inter-pane spacing. As previously mentioned, the windows are the known weak point in a partition.

As per Section 4.2, when daytime noise levels (from road and rail sources) at the plane of the window exceed 65 dBA, calculations must be performed to evaluate the sound transmission quality of the building components to ensure acceptable indoor noise levels. The calculation procedure⁸ considers:

- Window type and total area as a percentage of total room floor area
- Exterior wall type and total area as a percentage of the total room floor area
- Acoustic absorption characteristics of the room
- Outdoor noise source type and approach geometry
- Indoor sound level criteria, which varies according to the intended use of a space

⁸ Building Practice Note: Controlling Sound Transmission into Buildings by J.D. Quirt, National Research Council of Canada, September 1985



Based on published research⁹, exterior walls possess specific sound attenuation characteristics that are used as a basis for calculating the required STC ratings of windows in the same partition. Due to the limited information available at the time of the study, which was prepared for site plan approval, detailed floor layouts and building elevations have not been finalized; therefore, detailed STC calculations could not be performed at this time. As a guideline, the anticipated STC requirements for windows have been estimated based on the overall noise reduction required for each intended use of space (STC = outdoor noise level – targeted indoor noise levels).

5. RESULTS AND DISCUSSION

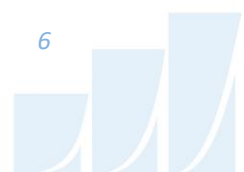
5.1 Roadway Traffic Noise Levels

The results of the roadway traffic noise calculations are summarized in Table 3 below. A complete set of input and output data from all STAMSON 5.04 calculations are available in Appendix A.

TABLE 3: EXTERIOR NOISE LEVELS DUE TO ROAD TRAFFIC

Receptor Number	Receptor Height Above Grade (m)	Receptor Location	STAMSON 5.04 Noise Level (dBA)	
			Day	Night
1	13.5	Building A – POW – 5 th Floor – North Façade	72	64
2	13.5	Building A – POW – 5 th Floor – East Façade	73	66
3	13.5	Building A – POW – 5 th Floor – South Façade	73	65
4	13.5	Building A – POW – 5 th Floor – West Façade	69	61
5	13.5	Building B – POW – 5 th Floor – North Façade	67	59
6	13.5	Building B – POW – 5 th Floor – South Façade	72	64
7	16.5	Building A – OLA – 6 th Floor Terrace	68	N/A

⁹ CMHC, Road & Rail Noise: Effects on Housing



The results of the current analysis indicate that noise levels will range between 67 and 73 dBA during the daytime period (07:00-23:00) and between 59 and 66 dBA during the nighttime period (23:00-07:00). The highest noise level (73 dBA) occurs at the east and south façades of Building A, which are nearest and most exposed to Tenth Line Road and St. Joseph Boulevard.

5.2 Noise Control Measures

The noise levels predicted due to roadway traffic exceed the criteria listed in Section 4.2 for building components. As discussed in Section 4.3, the anticipated STC requirements for windows have been estimated based on the overall noise reduction required for each intended use of space (STC = outdoor noise level – targeted indoor noise levels). As per city of Ottawa requirements, detailed STC calculations will be required to be completed prior to building permit application for each unit type. The STC requirements for the windows are summarized below for various units within the development (see Figure 3):

- **Bedroom Windows**
 - (i) Bedroom windows facing north, east and south on Building A, and south on Building B will require a minimum STC of 35
 - (ii) Bedroom windows facing west on Building A and east and west on Building B will require a minimum STC of 32
 - (iii) Bedroom windows facing north on Building B will require a minimum STC of 30

- **Living room Windows**
 - (i) Living room windows facing north, east and south on Building A, and south on Building B will require a minimum STC of 30
 - (ii) Living room windows facing west on Building A and east and west on Building B will require a minimum STC of 27
 - (iii) Living room windows facing north on Building B will require a minimum STC of 25

- **Exterior Walls**

- (i) Exterior wall components on these façades will require a minimum STC of 45, which will be achieved with brick cladding or an acoustical equivalent according to NRC test data¹⁰

The STC requirements apply to windows, doors, spandrel panels and curtainwall elements. Exterior wall components on these façades are recommended to have a minimum STC of 45, where a window/wall system is used. A review of window supplier literature indicates that the specified STC ratings can be achieved by a variety of window systems having a combination of glass thickness and inter-pane spacing. We have specified an example window configuration, however several manufacturers and various combinations of window components, such as those proposed, will offer the necessary sound attenuation rating. It is the responsibility of the manufacturer to ensure that the specified window achieves the required STC. This can only be assured by using window configurations that have been certified by laboratory testing. The requirements for STC ratings assume that the remaining components of the building are constructed and installed according to the minimum standards of the Ontario Building Code. The specified STC requirements also apply to swinging and/or sliding patio doors.

Results of the calculations also indicate that the development will require central air conditioning, which will allow occupants to keep windows closed and maintain a comfortable living environment. In addition to ventilation requirements, Warning Clauses will also be required in all Lease, Purchase and Sale Agreements, as summarized in Section 6.

5.3 Noise Barrier Calculation

Noise levels at the Building A 6th Floor terrace (Receptor 7) are expected to approach 68 dBA during the daytime period. If this area is to be used as an outdoor living area, noise control measures are required to reduce the L_{eq} to 60 dBA, and as close to 55 dBA as feasibly possible. Further analysis investigated the noise mitigating impact of surrounding the terrace with a 1.5 m noise barrier (base case) to 4.6 m above the walking surface. Results of the investigation proved that noise levels can only feasibly be reduced to 65 dBA. Reducing noise levels to 55 dBA would require excessive barrier heights that would not be feasible. Table 4 summarizes the results of the barrier investigation.

¹⁰ J.S. Bradley and J.A. Birta. Laboratory Measurements of the Sound Insulation of Building Façade Elements, National Research Council October 2000.



TABLE 4: RESULTS OF NOISE BARRIER INVESTIGATION

Location	Reference Receptor	Barrier Height (m)	Daytime Leq Noise Levels (dBA)
Building A 6 th Floor Terrace	7	No Barrier	68
		1.5	65
		4.6	60

6. CONCLUSIONS AND RECOMMENDATIONS

The results of the current analysis indicate that noise levels will range between 67 and 73 dBA during the daytime period (07:00-23:00) and between 59 and 66 dBA during the nighttime period (23:00-07:00). The highest noise level (73 dBA) occurs at the east and south façades of Building A, which are nearest and most exposed to Tenth Line Road and St. Joseph Boulevard. Building components with a higher Sound Transmission Class (STC) rating will be required where exterior noise levels exceed 65 dBA, as indicated in Figure 3.

Results of the calculations also indicate that the development will require central air conditioning, which will allow occupants to keep windows closed and maintain a comfortable living environment. The following Type D Warning Clause¹¹ will also be required be placed on all Lease, Purchase and Sale Agreements, as summarized below:

"This dwelling unit has been supplied with a central air conditioning system which will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the sound level limits of the Municipality and the Ministry of the Environment, Conservation and Parks."

Noise levels at the Building A 6th Floor terrace (Receptor 7) are expected to approach 68 dBA during the daytime period. If this area is to be used as an outdoor living area, noise control measures are required to reduce the L_{eq} to 60 dBA, and as close to 55 dBA as feasibly possible. Further analysis investigated the noise mitigating impact of surrounding the terrace with a 1.5 m noise barrier (base case) to 4.6 m above the walking surface. Results of the investigation proved that noise levels can only feasibly be reduced to

¹¹ City of Ottawa Environmental Noise Control Guidelines, January 2016



65 dBA. Reducing noise levels to 55 dBA would require excessive barrier heights that would not be feasible.

Regarding stationary noise, impacts from the surroundings on the study building are expected to be minimal. There are no significant sources of stationary noise in the area, and the study site is subject to elevated background noise levels from roadway traffic sources. Impacts from the development on the surroundings can be minimized by judicious placement mechanical equipment such as its placement on a roof or in a mechanical penthouse, or the incorporation of silencers and noise screens as necessary. It is recommended that any large pieces of HVAC equipment be placed in the middle of the roof, avoiding line of site with the surrounding residential dwellings.

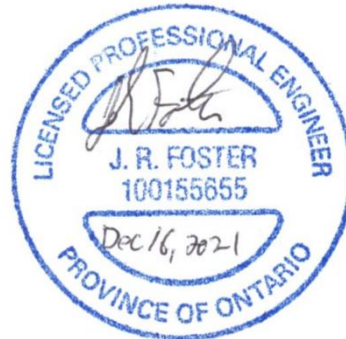
This concludes our traffic noise assessment and report. If you have any questions or wish to discuss our findings, please advise us. In the interim, we thank you for the opportunity to be of service.

Sincerely,

Gradient Wind Engineering Inc.



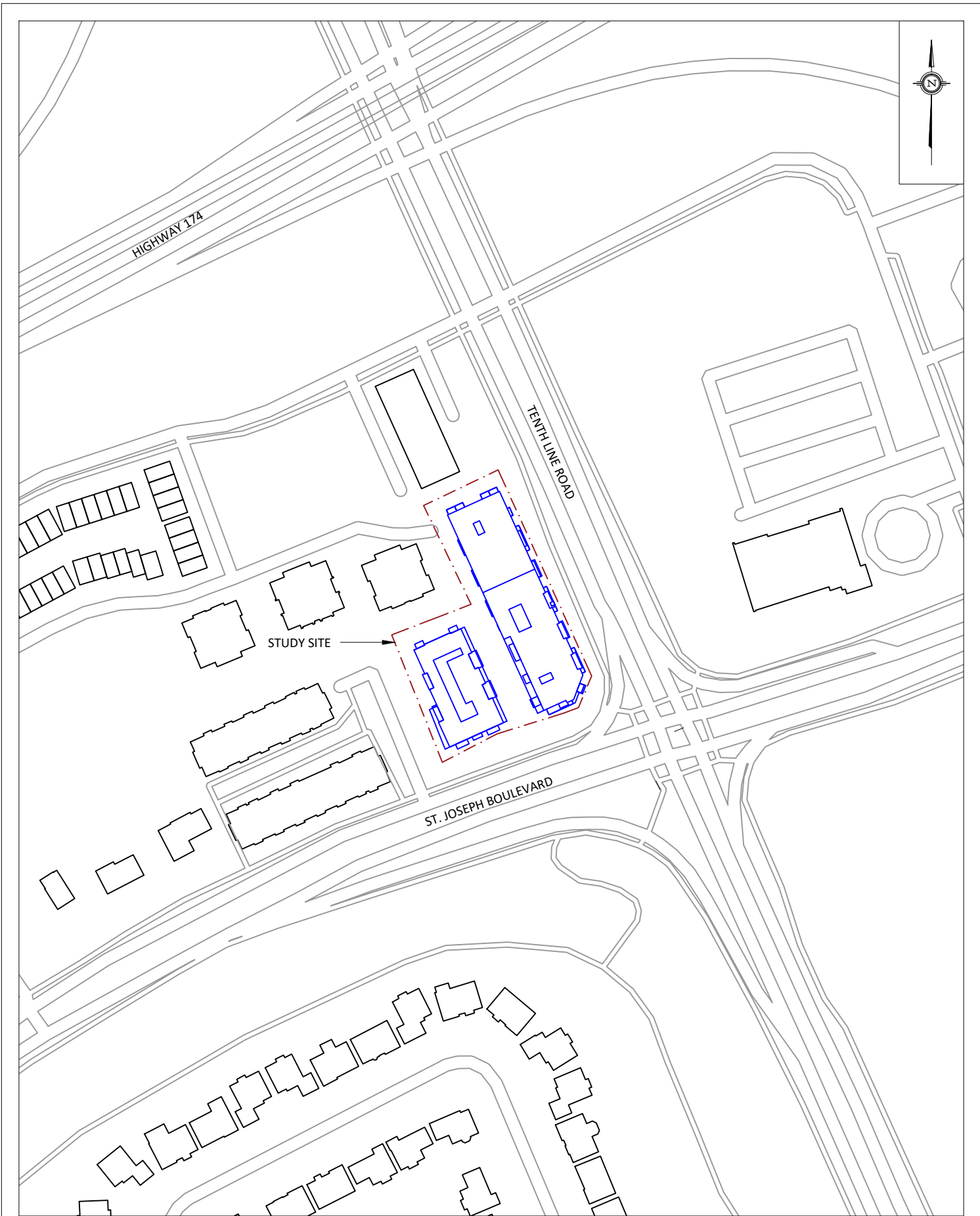
Michael Lafortune, C.E.T.
Environmental Scientist



Joshua Foster, P.Eng.
Lead Engineer

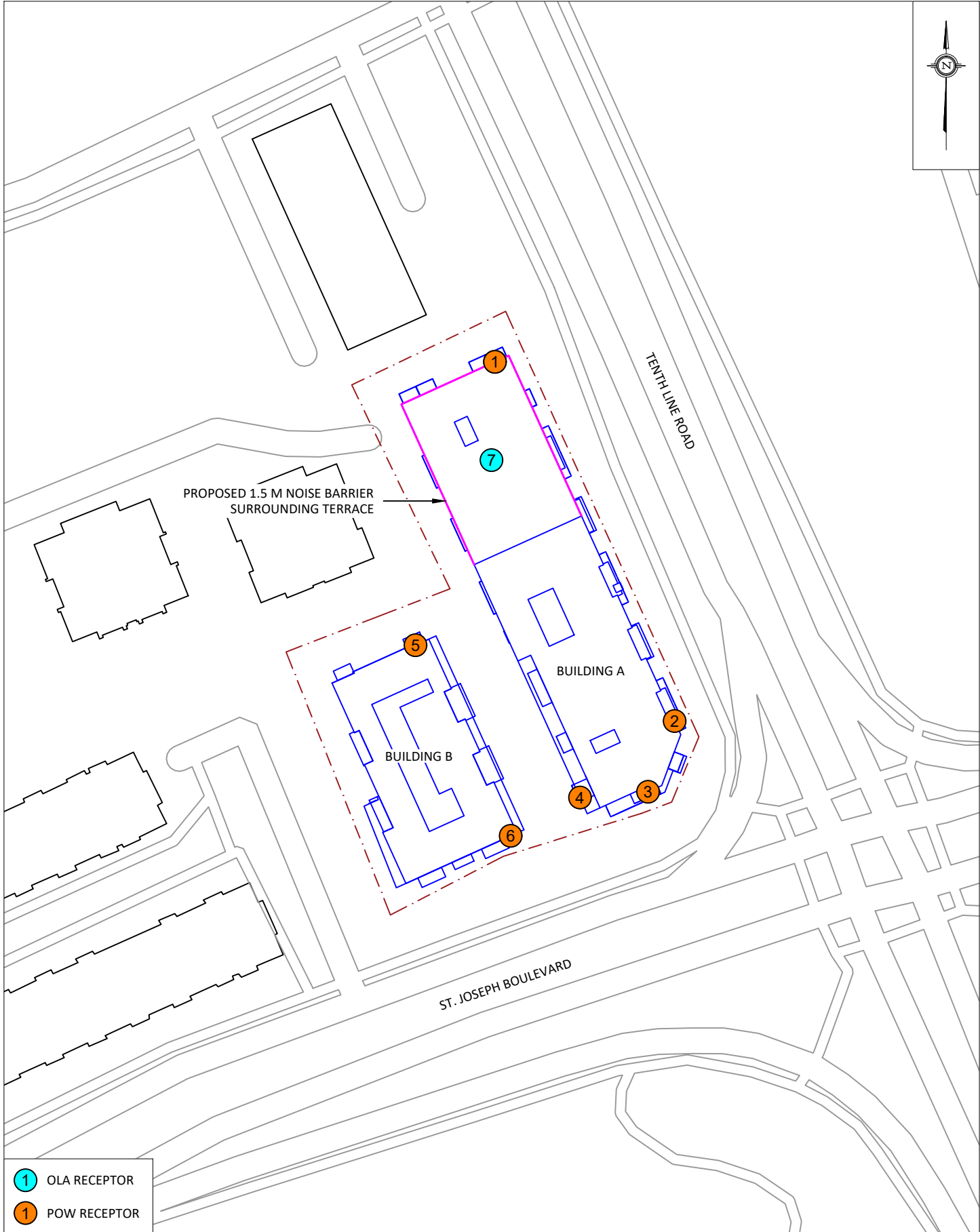
Gradient Wind File #21-401-Traffic Noise





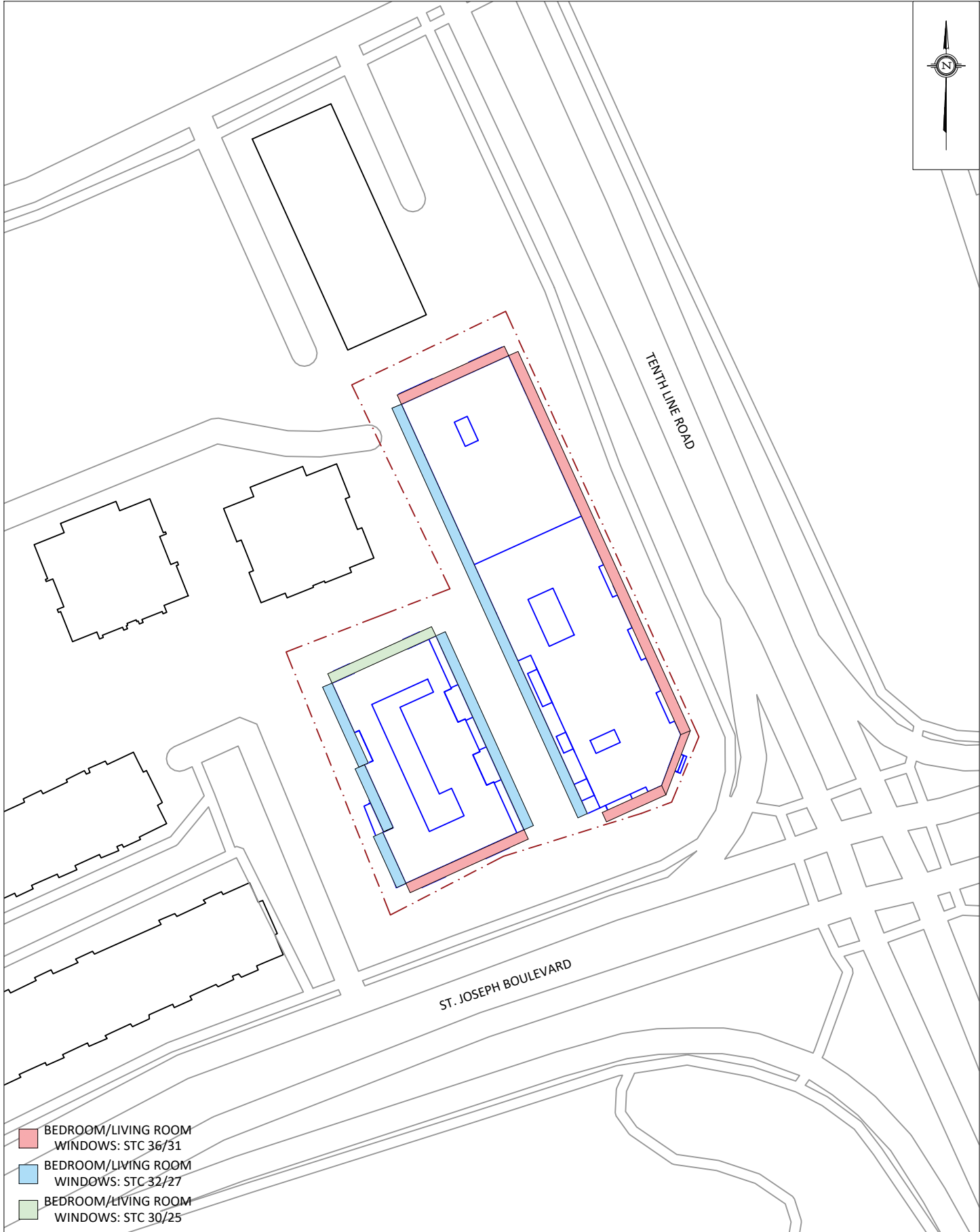
PROJECT	3277 ST. JOSEPH BOULEVARD, OTTAWA ROADWAY TRAFFIC NOISE ASSESSMENT	
SCALE	1:2000 (APPROX.)	DRAWING NO. GW21-401-1
DATE	DECEMBER 10, 2021	DRAWN BY M.L.

DESCRIPTION	FIGURE 1: SITE PLAN AND SURROUNDING CONTEXT
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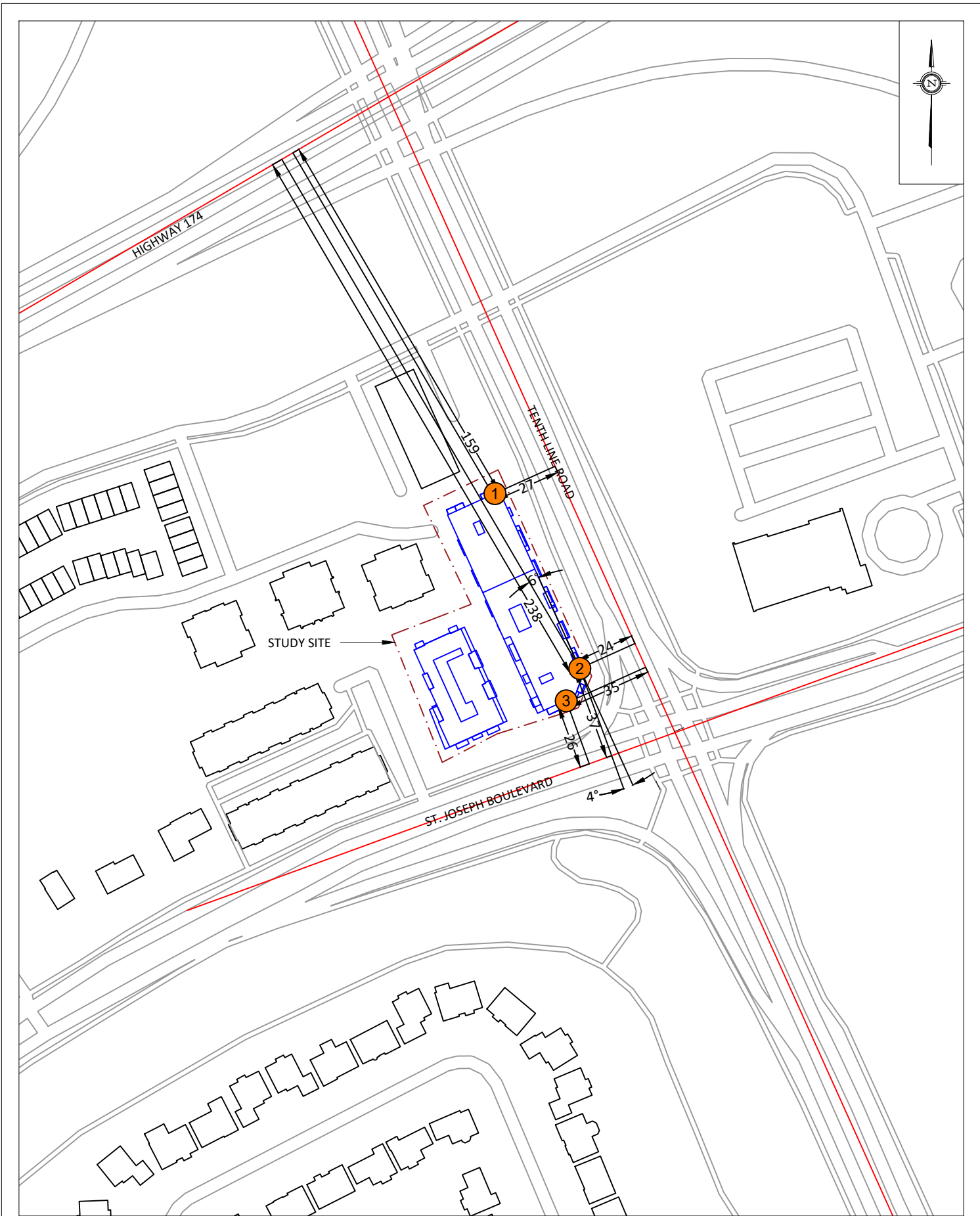
- ① OLA RECEPTOR
- ① POW RECEPTOR

PROJECT	3277 ST. JOSEPH BOULEVARD, OTTAWA ROADWAY TRAFFIC NOISE ASSESSMENT	
SCALE	1:1000 (APPROX.)	DRAWING NO. GW21-401-2
DATE	DECEMBER 10, 2021	DRAWN BY M.L.

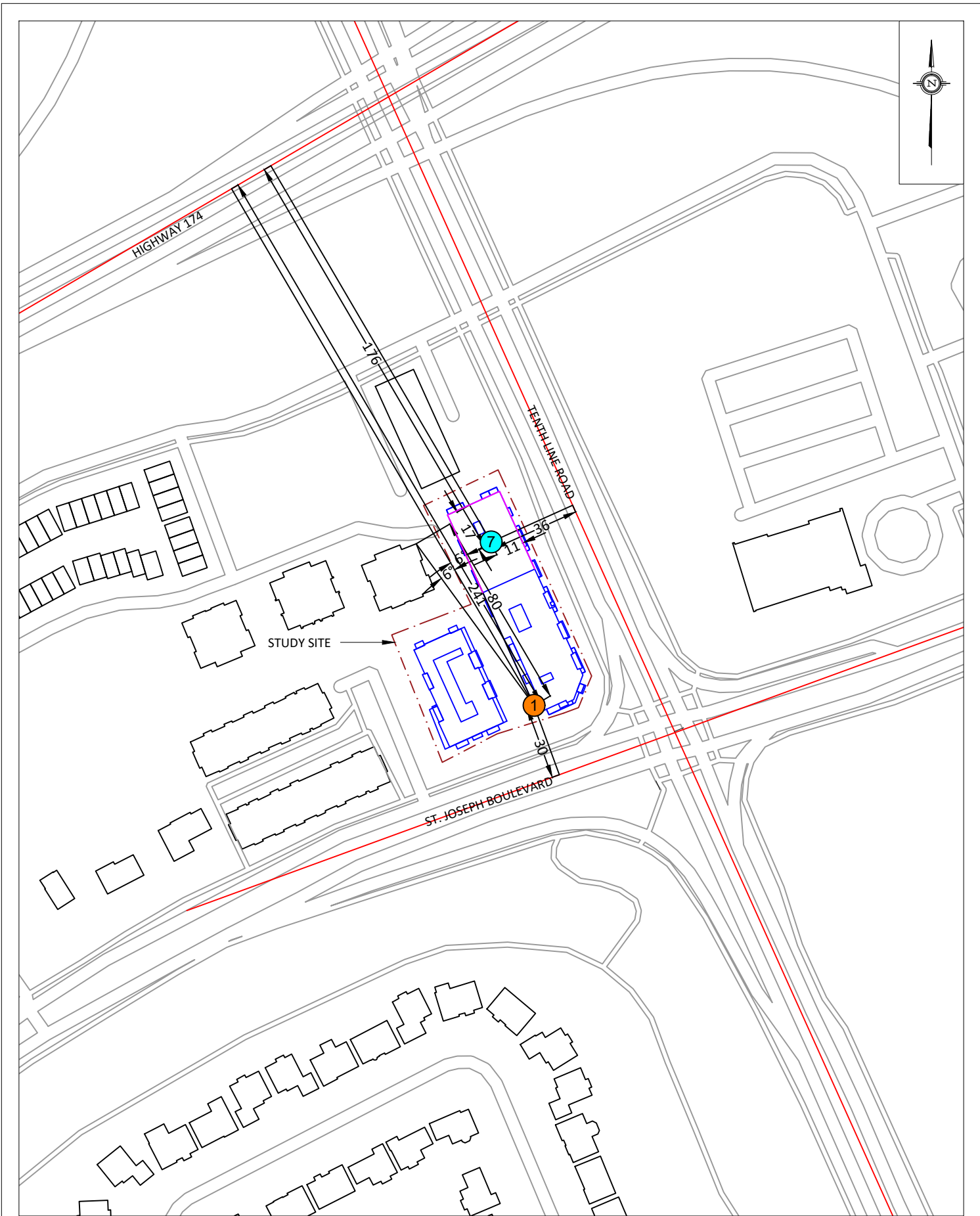


- BEDROOM/LIVING ROOM
WINDOWS: STC 36/31
- BEDROOM/LIVING ROOM
WINDOWS: STC 32/27
- BEDROOM/LIVING ROOM
WINDOWS: STC 30/25

PROJECT	3277 ST. JOSEPH BOULEVARD, OTTAWA ROADWAY TRAFFIC NOISE ASSESSMENT	
SCALE	1:1000 (APPROX.)	DRAWING NO. GW21-401-3
DATE	DECEMBER 10, 2021	DRAWN BY M.L.

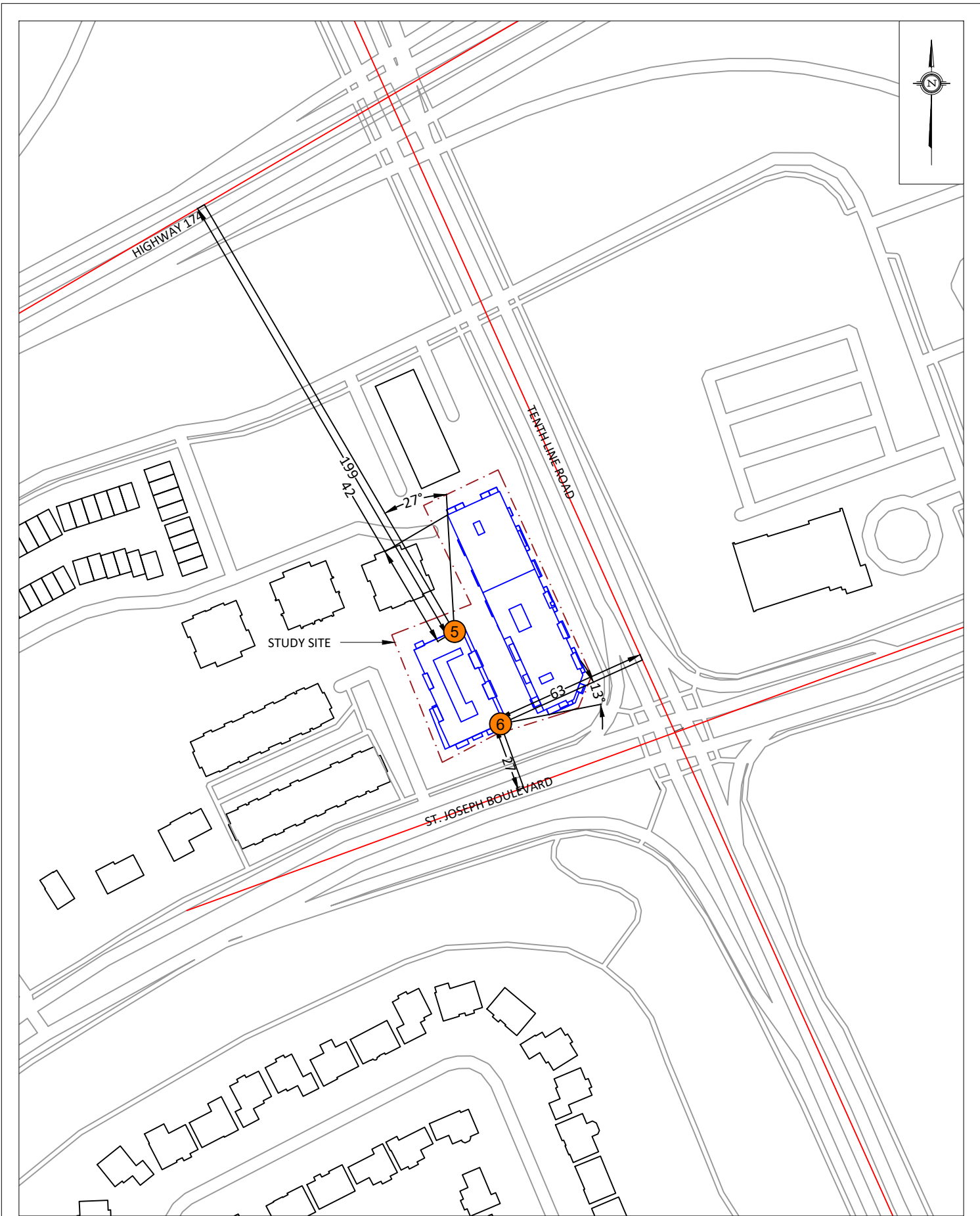


PROJECT	3277 ST. JOSEPH BOULEVARD, OTTAWA ROADWAY TRAFFIC NOISE ASSESSMENT	
SCALE	1:2000 (APPROX.)	DRAWING NO. GW21-401-4
DATE	DECEMBER 10, 2021	DRAWN BY M.L.



PROJECT	3277 ST. JOSEPH BOULEVARD, OTTAWA ROADWAY TRAFFIC NOISE ASSESSMENT	
SCALE	1:2000 (APPROX.)	DRAWING NO. GW21-401-5
DATE	DECEMBER 10, 2021	DRAWN BY M.L.

DESCRIPTION	FIGURE 5: STAMSON INPUT PARAMETERS - RECEPTOR 4,7
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PROJECT	3277 ST. JOSEPH BOULEVARD, OTTAWA ROADWAY TRAFFIC NOISE ASSESSMENT	
SCALE	1:2000 (APPROX.)	DRAWING NO. GW21-401-6
DATE	DECEMBER 10, 2021	DRAWN BY M.L.

DESCRIPTION	FIGURE 6: STAMSON INPUT PARAMETERS - RECEPTOR 5,6
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GRADIENTWIND

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APPENDIX A

STAMSON 5.04 – INPUT AND OUTPUT DATA

GRADIENTWIND

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STAMSON 5.0 NORMAL REPORT Date: 10-12-2021 13:27:32
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r1.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: 174 (day/night)

Car traffic volume : 89056/7744 veh/TimePeriod *
Medium truck volume : 7084/616 veh/TimePeriod *
Heavy truck volume : 5060/440 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 110000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: 174 (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 159.00 / 159.00 m
Receiver height : 13.50 / 13.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00



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Road data, segment # 2: Tenth (day/night)

Car traffic volume : 28336/2464 veh/TimePeriod *
Medium truck volume : 2254/196 veh/TimePeriod *
Heavy truck volume : 1610/140 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 35000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: Tenth (day/night)

Angle1 Angle2 : -90.00 deg 0.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 27.00 / 27.00 m
Receiver height : 13.50 / 13.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00



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Results segment # 1: 174 (day)

Source height = 1.50 m

ROAD (0.00 + 69.06 + 0.00) = 69.06 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

SubLeq

--									
-90	90	0.30	83.16	0.00	-13.33	-0.77	0.00	0.00	0.00
69.06									

Segment Leq : 69.06 dBA

Results segment # 2: Tenth (day)

Source height = 1.50 m

ROAD (0.00 + 68.11 + 0.00) = 68.11 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

SubLeq

--									
-90	0	0.00	73.68	0.00	-2.55	-3.01	0.00	0.00	0.00
68.11									

Segment Leq : 68.11 dBA

Total Leq All Segments: 71.62 dBA



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Results segment # 1: 174 (night)

Source height = 1.50 m

ROAD (0.00 + 61.46 + 0.00) = 61.46 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

SubLeq

--									
-90	90	0.30	75.56	0.00	-13.33	-0.77	0.00	0.00	0.00
61.46									

Segment Leq : 61.46 dBA

Results segment # 2: Tenth (night)

Source height = 1.50 m

ROAD (0.00 + 60.52 + 0.00) = 60.52 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

SubLeq

--									
-90	0	0.00	66.08	0.00	-2.55	-3.01	0.00	0.00	0.00
60.52									

Segment Leq : 60.52 dBA

Total Leq All Segments: 64.03 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 71.62
(NIGHT): 64.03



GRADIENTWIND

ENGINEERS & SCIENTISTS

STAMSON 5.0 NORMAL REPORT Date: 10-12-2021 13:27:36
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r2.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: 174 (day/night)

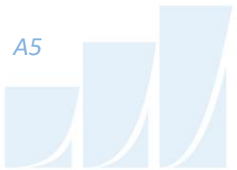
Car traffic volume : 89056/7744 veh/TimePeriod *
Medium truck volume : 7084/616 veh/TimePeriod *
Heavy truck volume : 5060/440 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 110000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: 174 (day/night)

Angle1 Angle2 : 6.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 238.00 / 238.00 m
Receiver height : 13.50 / 13.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00



Road data, segment # 2: Tenth (day/night)

Car traffic volume : 28336/2464 veh/TimePeriod *
Medium truck volume : 2254/196 veh/TimePeriod *
Heavy truck volume : 1610/140 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 35000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: Tenth (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 24.00 / 24.00 m
Receiver height : 13.50 / 13.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00



GRADIENTWIND

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Road data, segment # 3: SJB (day/night)

Car traffic volume : 28336/2464 veh/TimePeriod *
Medium truck volume : 2254/196 veh/TimePeriod *
Heavy truck volume : 1610/140 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 35000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: SJB (day/night)

Angle1 Angle2 : -90.00 deg -4.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 37.00 / 37.00 m
Receiver height : 13.50 / 13.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00



GRADIENTWIND

ENGINEERS & SCIENTISTS

Results segment # 1: 174 (day)

Source height = 1.50 m

ROAD (0.00 + 63.41 + 0.00) = 63.41 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

SubLeq

6	90	0.30	83.16	0.00	-15.61	-4.14	0.00	0.00	0.00
---	----	------	-------	------	--------	-------	------	------	------

Segment Leq : 63.41 dBA

Results segment # 2: Tenth (day)

Source height = 1.50 m

ROAD (0.00 + 71.63 + 0.00) = 71.63 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

SubLeq

-90	90	0.00	73.68	0.00	-2.04	0.00	0.00	0.00	0.00
-----	----	------	-------	------	-------	------	------	------	------

Segment Leq : 71.63 dBA



Results segment # 3: SJB (day)

Source height = 1.50 m

ROAD (0.00 + 66.55 + 0.00) = 66.55 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--									
-90	-4	0.00	73.68	0.00	-3.92	-3.21	0.00	0.00	0.00
66.55									

Segment Leq : 66.55 dBA

Total Leq All Segments: 73.28 dBA

Results segment # 1: 174 (night)

Source height = 1.50 m

ROAD (0.00 + 55.81 + 0.00) = 55.81 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--									
6	90	0.30	75.56	0.00	-15.61	-4.14	0.00	0.00	0.00
55.81									

Segment Leq : 55.81 dBA



GRADIENTWIND

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Results segment # 2: Tenth (night)

Source height = 1.50 m

ROAD (0.00 + 64.04 + 0.00) = 64.04 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--									
-90	90	0.00	66.08	0.00	-2.04	0.00	0.00	0.00	0.00
64.04									

Segment Leq : 64.04 dBA

Results segment # 3: SJB (night)

Source height = 1.50 m

ROAD (0.00 + 58.95 + 0.00) = 58.95 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--									
-90	-4	0.00	66.08	0.00	-3.92	-3.21	0.00	0.00	0.00
58.95									

Segment Leq : 58.95 dBA

Total Leq All Segments: 65.68 dBA

TOTAL Leq FROM ALL SOURCES (DAY) : 73.28
(NIGHT) : 65.68



GRADIENTWIND

ENGINEERS & SCIENTISTS

STAMSON 5.0 NORMAL REPORT Date: 10-12-2021 13:27:40
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r3.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: Tenth (day/night)

Car traffic volume : 28336/2464 veh/TimePeriod *
Medium truck volume : 2254/196 veh/TimePeriod *
Heavy truck volume : 1610/140 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 35000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: Tenth (day/night)

Angle1 Angle2 : 0.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 35.00 / 35.00 m
Receiver height : 13.50 / 13.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00



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Road data, segment # 2: SJB (day/night)

Car traffic volume : 28336/2464 veh/TimePeriod *
Medium truck volume : 2254/196 veh/TimePeriod *
Heavy truck volume : 1610/140 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 35000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: SJB (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 26.00 / 26.00 m
Receiver height : 13.50 / 13.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00



Results segment # 1: Tenth (day)

Source height = 1.50 m

ROAD (0.00 + 66.99 + 0.00) = 66.99 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--									
	0	90	0.00	73.68	0.00	-3.68	-3.01	0.00	0.00
	66.99								

Segment Leq : 66.99 dBA

Results segment # 2: SJB (day)

Source height = 1.50 m

ROAD (0.00 + 71.29 + 0.00) = 71.29 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--									
	-90	90	0.00	73.68	0.00	-2.39	0.00	0.00	0.00
	71.29								

Segment Leq : 71.29 dBA

Total Leq All Segments: 72.66 dBA



GRADIENTWIND

ENGINEERS & SCIENTISTS

Results segment # 1: Tenth (night)

Source height = 1.50 m

ROAD (0.00 + 59.39 + 0.00) = 59.39 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

SubLeq

--									
0	90	0.00	66.08	0.00	-3.68	-3.01	0.00	0.00	0.00
59.39									

Segment Leq : 59.39 dBA

Results segment # 2: SJB (night)

Source height = 1.50 m

ROAD (0.00 + 63.69 + 0.00) = 63.69 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

SubLeq

--									
-90	90	0.00	66.08	0.00	-2.39	0.00	0.00	0.00	0.00
63.69									

Segment Leq : 63.69 dBA

Total Leq All Segments: 65.06 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 72.66
(NIGHT): 65.06



GRADIENTWIND

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STAMSON 5.0 NORMAL REPORT Date: 10-12-2021 13:27:45
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r4.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: 174 (day/night)

Car traffic volume : 89056/7744 veh/TimePeriod *
Medium truck volume : 7084/616 veh/TimePeriod *
Heavy truck volume : 5060/440 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 110000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: 174 (day/night)

Angle1 Angle2 : -90.00 deg 6.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 241.00 / 241.00 m
Receiver height : 13.50 / 13.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -90.00 deg Angle2 : -6.00 deg
Barrier height : 10.00 m
Barrier receiver distance : 80.00 / 80.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00



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Road data, segment # 2: SJB (day/night)

Car traffic volume : 28336/2464 veh/TimePeriod *
Medium truck volume : 2254/196 veh/TimePeriod *
Heavy truck volume : 1610/140 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 35000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: SJB (day/night)

Angle1 Angle2 : 0.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 30.00 / 30.00 m
Receiver height : 13.50 / 13.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00



GRADIENTWIND

ENGINEERS & SCIENTISTS

Results segment # 1: 174 (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	13.50	9.52	9.52

ROAD (0.00 + 62.72 + 55.72) = 63.51 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

-90	-6	0.00	83.16	0.00	-12.06	-3.31	0.00	0.00	-5.07
62.72									

-6	6	0.30	83.16	0.00	-15.68	-11.76	0.00	0.00	0.00
55.72									

Segment Leq : 63.51 dBA



Results segment # 2: SJB (day)

Source height = 1.50 m

ROAD (0.00 + 67.66 + 0.00) = 67.66 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

0	90	0.00	73.68	0.00	-3.01	-3.01	0.00	0.00	0.00
67.66									

Segment Leq : 67.66 dBA

Total Leq All Segments: 69.07 dBA

Results segment # 1: 174 (night)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	13.50	9.52	9.52

ROAD (0.00 + 55.12 + 48.12) = 55.91 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

-90	-6	0.00	75.56	0.00	-12.06	-3.31	0.00	0.00	-5.07
55.12									

-6	6	0.30	75.56	0.00	-15.68	-11.76	0.00	0.00	0.00
48.12									

Segment Leq : 55.91 dBA



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Results segment # 2: SJB (night)

Source height = 1.50 m

ROAD (0.00 + 60.06 + 0.00) = 60.06 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

SubLeq

--
0 90 0.00 66.08 0.00 -3.01 -3.01 0.00 0.00 0.00
60.06

--

Segment Leq : 60.06 dBA

Total Leq All Segments: 61.47 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 69.07
(NIGHT): 61.47



GRADIENTWIND

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STAMSON 5.0 NORMAL REPORT Date: 10-12-2021 13:27:52
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r5.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: 174L (day/night)

Car traffic volume : 89056/7744 veh/TimePeriod *
Medium truck volume : 7084/616 veh/TimePeriod *
Heavy truck volume : 5060/440 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 110000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: 174L (day/night)

Angle1 Angle2 : -90.00 deg 27.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 199.00 / 199.00 m
Receiver height : 13.50 / 13.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -90.00 deg Angle2 : 27.00 deg
Barrier height : 10.00 m
Barrier receiver distance : 42.00 / 42.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00



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Road data, segment # 2: 174R (day/night)

Car traffic volume : 89056/7744 veh/TimePeriod *
Medium truck volume : 7084/616 veh/TimePeriod *
Heavy truck volume : 5060/440 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 110000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: 174R (day/night)

Angle1 Angle2 : 27.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 199.00 / 199.00 m
Receiver height : 13.50 / 13.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : 27.00 deg Angle2 : 90.00 deg
Barrier height : 15.00 m
Barrier receiver distance : 42.00 / 42.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00



GRADIENTWIND

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Results segment # 1: 174L (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	13.50	10.97	10.97

ROAD (0.00 + 66.10 + 0.00) = 66.10 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

-90	27	0.00	83.16	0.00	-11.23	-1.87	0.00	0.00	-4.44
65.62*									
-90	27	0.30	83.16	0.00	-14.60	-2.46	0.00	0.00	0.00
66.10									

* Bright Zone !

Segment Leq : 66.10 dBA



GRADIENTWIND

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Results segment # 2: 174R (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	13.50	10.97	10.97

ROAD (0.00 + 58.67 + 0.00) = 58.67 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
27	90	0.00	83.16	0.00	-11.23	-4.56	0.00	0.00	-8.70

SubLeq

58.67

Segment Leq : 58.67 dBA

Total Leq All Segments: 66.82 dBA



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Results segment # 1: 174L (night)

 Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	! Receiver ! Height (m)	! Barrier ! Height (m)	! Elevation of ! Barrier Top (m)
1.50	!	13.50	!
		10.97	!
			10.97

ROAD (0.00 + 58.50 + 0.00) = 58.50 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--	-90	27	0.00	75.56	0.00	-11.23	-1.87	0.00	0.00	-4.44
58.03*	-90	27	0.30	75.56	0.00	-14.60	-2.46	0.00	0.00	0.00
58.50										

 --
 * Bright Zone !

Segment Leq : 58.50 dBA



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Results segment # 2: 174R (night)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	13.50	10.97	10.97

ROAD (0.00 + 51.08 + 0.00) = 51.08 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
27	90	0.00	75.56	0.00	-11.23	-4.56	0.00	0.00	-8.70

SubLeq
51.08

Segment Leq : 51.08 dBA

Total Leq All Segments: 59.22 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 66.82
(NIGHT): 59.22



GRADIENTWIND

ENGINEERS & SCIENTISTS

STAMSON 5.0 NORMAL REPORT Date: 10-12-2021 13:27:57
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r6.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: Tenth (day/night)

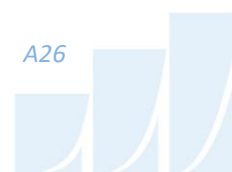
Car traffic volume : 28336/2464 veh/TimePeriod *
Medium truck volume : 2254/196 veh/TimePeriod *
Heavy truck volume : 1610/140 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 35000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: Tenth (day/night)

Angle1 Angle2 : 13.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 63.00 / 63.00 m
Receiver height : 13.50 / 13.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00



GRADIENTWIND

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Road data, segment # 2: SJB (day/night)

Car traffic volume : 28336/2464 veh/TimePeriod *
Medium truck volume : 2254/196 veh/TimePeriod *
Heavy truck volume : 1610/140 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 35000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: SJB (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 27.00 / 27.00 m
Receiver height : 13.50 / 13.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00



GRADIENTWIND

ENGINEERS & SCIENTISTS

Results segment # 1: Tenth (day)

Source height = 1.50 m

ROAD (0.00 + 63.76 + 0.00) = 63.76 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

SubLeq

13	90	0.00	73.68	0.00	-6.23	-3.69	0.00	0.00	0.00
----	----	------	-------	------	-------	-------	------	------	------

Segment Leq : 63.76 dBA

Results segment # 2: SJB (day)

Source height = 1.50 m

ROAD (0.00 + 71.12 + 0.00) = 71.12 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

SubLeq

-90	90	0.00	73.68	0.00	-2.55	0.00	0.00	0.00	0.00
-----	----	------	-------	------	-------	------	------	------	------

Segment Leq : 71.12 dBA

Total Leq All Segments: 71.85 dBA



GRADIENTWIND

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Results segment # 1: Tenth (night)

Source height = 1.50 m

ROAD (0.00 + 56.16 + 0.00) = 56.16 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

SubLeq

13	90	0.00	66.08	0.00	-6.23	-3.69	0.00	0.00	0.00
----	----	------	-------	------	-------	-------	------	------	------

Segment Leq : 56.16 dBA

Results segment # 2: SJB (night)

Source height = 1.50 m

ROAD (0.00 + 63.53 + 0.00) = 63.53 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

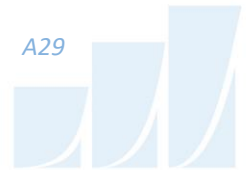
SubLeq

-90	90	0.00	66.08	0.00	-2.55	0.00	0.00	0.00	0.00
-----	----	------	-------	------	-------	------	------	------	------

Segment Leq : 63.53 dBA

Total Leq All Segments: 64.26 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 71.85
(NIGHT): 64.26



GRADIENTWIND

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STAMSON 5.0 NORMAL REPORT Date: 10-12-2021 13:28:02
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r7.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: 174 (day/night)

Car traffic volume : 89056/7744 veh/TimePeriod *
Medium truck volume : 7084/616 veh/TimePeriod *
Heavy truck volume : 5060/440 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 110000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: 174 (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 176.00 / 176.00 m
Receiver height : 16.50 / 16.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -90.00 deg Angle2 : 90.00 deg
Barrier height : 15.00 m
Barrier receiver distance : 17.00 / 17.00 m
Source elevation : -4.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00



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Road data, segment # 2: Tenth (day/night)

Car traffic volume : 28336/2464 veh/TimePeriod *
Medium truck volume : 2254/196 veh/TimePeriod *
Heavy truck volume : 1610/140 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 35000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: Tenth (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 36.00 / 36.00 m
Receiver height : 16.50 / 16.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -90.00 deg Angle2 : 90.00 deg
Barrier height : 15.00 m
Barrier receiver distance : 11.00 / 11.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00



GRADIENTWIND

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Results segment # 1: 174 (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	16.50	14.66	14.66

ROAD (0.00 + 67.34 + 0.00) = 67.34 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	90	0.00	83.16	0.00	-10.69	0.00	0.00	0.00	-5.12

SubLeq
67.34

Segment Leq : 67.34 dBA

Results segment # 2: Tenth (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	16.50	11.92	11.92

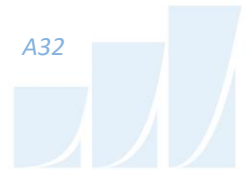
ROAD (0.00 + 58.40 + 0.00) = 58.40 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	90	0.00	73.68	0.00	-3.80	0.00	0.00	0.00	-11.47

SubLeq
58.40

Segment Leq : 58.40 dBA

Total Leq All Segments: 67.86 dBA



GRADIENTWIND

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Results segment # 1: 174 (night)

 Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	! Receiver ! Height (m)	! Barrier ! Height (m)	! Elevation of ! Barrier Top (m)
1.50	!	16.50	!
		14.66	!
			14.66

ROAD (0.00 + 59.75 + 0.00) = 59.75 dBA

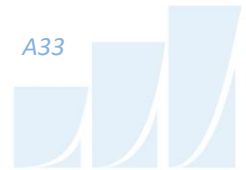
Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	90	0.00	75.56	0.00	-10.69	0.00	0.00	0.00	-5.12

SubLeq

 --
 59.75

 --

Segment Leq : 59.75 dBA



GRADIENTWIND

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Results segment # 2: Tenth (night)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	16.50	11.92	11.92

ROAD (0.00 + 50.81 + 0.00) = 50.81 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	90	0.00	66.08	0.00	-3.80	0.00	0.00	0.00	-11.47

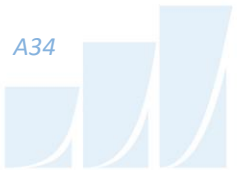
SubLeq

50.81

Segment Leq : 50.81 dBA

Total Leq All Segments: 60.27 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 67.86
(NIGHT): 60.27



GRADIENTWIND

ENGINEERS & SCIENTISTS

STAMSON 5.0 NORMAL REPORT Date: 10-12-2021 13:28:07
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r7b1.te Time Period: Day/Night 16/8 hours
Description: 1.5 m Barrier

Road data, segment # 1: 174 (day/night)

Car traffic volume : 89056/7744 veh/TimePeriod *
Medium truck volume : 7084/616 veh/TimePeriod *
Heavy truck volume : 5060/440 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 110000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: 174 (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 176.00 / 176.00 m
Receiver height : 16.50 / 16.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -90.00 deg Angle2 : 90.00 deg
Barrier height : 16.50 m
Barrier receiver distance : 17.00 / 17.00 m
Source elevation : -4.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00



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Road data, segment # 2: Tenth (day/night)

Car traffic volume : 28336/2464 veh/TimePeriod *
Medium truck volume : 2254/196 veh/TimePeriod *
Heavy truck volume : 1610/140 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 35000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: Tenth (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 36.00 / 36.00 m
Receiver height : 16.50 / 16.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -90.00 deg Angle2 : 90.00 deg
Barrier height : 16.50 m
Barrier receiver distance : 11.00 / 11.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00



GRADIENTWIND

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Results segment # 1: 174 (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	16.50	14.66	14.66

ROAD (0.00 + 64.89 + 0.00) = 64.89 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	90	0.00	83.16	0.00	-10.69	0.00	0.00	0.00	-7.58

SubLeq

64.89

Segment Leq : 64.89 dBA



GRADIENTWIND

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Results segment # 2: Tenth (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	16.50	11.92	11.92

ROAD (0.00 + 55.80 + 0.00) = 55.80 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	90	0.00	73.68	0.00	-3.80	0.00	0.00	0.00	-14.08

SubLeq

55.80

Segment Leq : 55.80 dBA

Total Leq All Segments: 65.39 dBA



GRADIENTWIND

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Results segment # 1: 174 (night)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	16.50	14.66	14.66

ROAD (0.00 + 57.29 + 0.00) = 57.29 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	90	0.00	75.56	0.00	-10.69	0.00	0.00	0.00	-7.58

SubLeq

57.29

Segment Leq : 57.29 dBA



GRADIENTWIND

ENGINEERS & SCIENTISTS

Results segment # 2: Tenth (night)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	16.50	11.92	11.92

ROAD (0.00 + 48.20 + 0.00) = 48.20 dBA

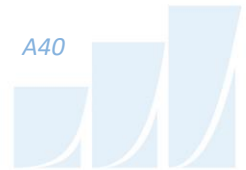
Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	90	0.00	66.08	0.00	-3.80	0.00	0.00	0.00	-14.08

SubLeq

Segment Leq : 48.20 dBA

Total Leq All Segments: 57.79 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 65.39
(NIGHT): 57.79



GRADIENTWIND

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STAMSON 5.0 NORMAL REPORT Date: 10-12-2021 13:28:12
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r7b2.te Time Period: Day/Night 16/8 hours
Description: 4.6 m Barrier

Road data, segment # 1: 174 (day/night)

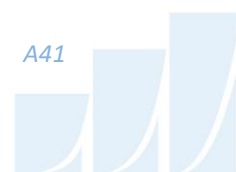
Car traffic volume : 89056/7744 veh/TimePeriod *
Medium truck volume : 7084/616 veh/TimePeriod *
Heavy truck volume : 5060/440 veh/TimePeriod *
Posted speed limit : 100 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 110000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: 174 (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 176.00 / 176.00 m
Receiver height : 16.50 / 16.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -90.00 deg Angle2 : 90.00 deg
Barrier height : 19.60 m
Barrier receiver distance : 17.00 / 17.00 m
Source elevation : -4.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00



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Road data, segment # 2: Tenth (day/night)

Car traffic volume : 28336/2464 veh/TimePeriod *
Medium truck volume : 2254/196 veh/TimePeriod *
Heavy truck volume : 1610/140 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 35000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: Tenth (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 36.00 / 36.00 m
Receiver height : 16.50 / 16.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -90.00 deg Angle2 : 90.00 deg
Barrier height : 19.60 m
Barrier receiver distance : 11.00 / 11.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00



GRADIENTWIND

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Results segment # 1: 174 (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	16.50	14.66	14.66

ROAD (0.00 + 59.67 + 0.00) = 59.67 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	90	0.00	83.16	0.00	-10.69	0.00	0.00	0.00	-12.80

SubLeq

59.67

Segment Leq : 59.67 dBA



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Results segment # 2: Tenth (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	16.50	11.92	11.92

ROAD (0.00 + 52.81 + 0.00) = 52.81 dBA

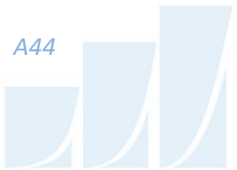
Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	90	0.00	73.68	0.00	-3.80	0.00	0.00	0.00	-17.07

SubLeq

52.81

Segment Leq : 52.81 dBA

Total Leq All Segments: 60.48 dBA



GRADIENTWIND

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Results segment # 1: 174 (night)

 Source height = 1.50 m

Barrier height for grazing incidence

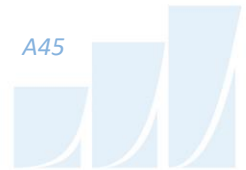
Source Height (m)	! Receiver ! Height (m)	! Barrier ! Height (m)	! Elevation of ! Barrier Top (m)
1.50	!	16.50	!
		14.66	!
			14.66

ROAD (0.00 + 52.07 + 0.00) = 52.07 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

-90	90	0.00	75.56	0.00	-10.69	0.00	0.00	0.00	-12.80
52.07									

 Segment Leq : 52.07 dBA



GRADIENTWIND

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Results segment # 2: Tenth (night)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	16.50	11.92	11.92

ROAD (0.00 + 45.21 + 0.00) = 45.21 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-90	90	0.00	66.08	0.00	-3.80	0.00	0.00	0.00	-17.07

SubLeq

--

45.21

--

Segment Leq : 45.21 dBA

Total Leq All Segments: 52.88 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 60.48
(NIGHT): 52.88

