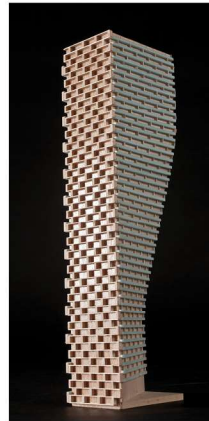


**ROADWAY TRAFFIC NOISE
ASSESSMENT**

1509 Merivale Road
Ottawa, Ontario

REPORT: GW21-198 – Traffic Noise



December 17, 2021

PREPARED FOR

Katasa Groupe + Développement

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EXECUTIVE SUMMARY

This report describes a traffic noise assessment undertaken in support of a Site Plan Control Application (SPA) for a proposed residential building located at 1509 Merivale Road in Ottawa, Ontario. For the purposes of this study, the elevation facing Merivale Road will be referred to as the west elevation. The focus of this study is Phase 1 of the proposed residential development which features a C-shaped nine-storey residential building. The major sources of traffic noise are Merivale Road, Clyde Avenue, and Lotta Avenue. Figure 1 illustrates a complete site plan with the surrounding context.

The assessment is based on (i) theoretical noise prediction methods that conform to the Ministry of the Environment, Conservation and Parks (MECP) and City of Ottawa requirements; (ii) noise level criteria as specified by the City of Ottawa's Environmental Noise Control Guidelines (ENCG); (iii) future vehicular traffic volumes based on the City of Ottawa's Official Plan roadway classifications; and (iv) architectural drawings prepared by RLA Architecture dated May 20, 2021.

The results of the current analysis indicate that noise levels will range between 64 and 73 dBA during the daytime period (07:00-23:00) and between 56 and 65 dBA during the nighttime period (23:00-07:00). The highest noise level (73 dBA) occurs at the west façade, which is nearest and most exposed to Merivale Road. Building components with a higher Sound Transmission Class (STC) rating will be required where exterior noise levels exceed 65 dBA, as indicated in Figure 3.

Results of the calculations also indicate that the development will require central air conditioning, which will allow occupants to keep windows closed and maintain a comfortable living environment. A Warning Clause will also be required in all Lease, Purchase and Sale Agreements, as summarized in section 6.

With regards to stationary noise impacts from the building on the surroundings and itself, noise can be controlled by judicious selection of the mechanical equipment and its placement on a high roof or in a mechanical penthouse. Where necessary noise screens, silencers, or acoustic louvers can be incorporated into the design to ensure compliance with the ENCG sound level limits. A stationary noise study will be performed once mechanical plans for the proposed building become available. This study will include recommendations for any noise control measures that may be necessary to ensure noise levels meet ENCG criteria.



Addendum: The architectural drawings of the subject site were updated following the completion of the traffic noise assessment¹, which was completed based on architectural drawings provided to Gradient Wind in June 2021. The only difference between the two drawing sets that could be considered important for the purpose of the traffic noise assessment is the reduction in height of the building along the east side of the property (currently 6 storeys above grade, previously 7 storeys above grade). The noted update is not expected to change the conclusions of the traffic noise assessment; the noise predictions summarized in Section 5 of the report are expected to be representative of the current architectural design.

¹ RLA Architecture, '1509 Merivale Road – Issued for Site Plan Control' [Dec 20, 2021]



TABLE OF CONTENTS

1. INTRODUCTION 1

2. TERMS OF REFERENCE 1

3. OBJECTIVES 2

4. METHODOLOGY..... 2

4.1 Background.....2

4.2 Roadway Traffic Noise.....2

4.2.1 Criteria for Roadway Traffic Noise2

4.2.2 Theoretical Roadway Noise Predictions4

4.2.1 Roadway Traffic Volumes.....4

4.3 Indoor Noise Calculations5

5. RESULTS AND DISCUSSION 6

5.1 Roadway Traffic Noise Levels.....6

5.2 Noise Control Measures7

6. CONCLUSIONS AND RECOMMENDATIONS 8

FIGURES

APPENDICES

Appendix A – STAMSON 5.04 Input and Output Data and Supporting Information



1. INTRODUCTION

Gradient Wind Engineering Inc. (Gradient Wind) was retained by Katasa Groupe + Développement to undertake a traffic noise assessment in support of a Site Plan Control application (SPA) for a proposed residential development located at 1509 Merivale Road in Ottawa, Ontario. This report summarizes the methodology, results, and recommendations related to the assessment of exterior and interior noise levels generated by local roadway traffic.

Our work is based on theoretical noise calculation methods conforming to the City of Ottawa² and Ministry of the Environment, Conservation and Parks (MECP)³ guidelines. Noise calculations were based on architectural drawings prepared by RLA Architecture dated May 20, 2021, with future traffic volumes corresponding to the City of Ottawa's Official Plan (OP) roadway classifications.

2. TERMS OF REFERENCE

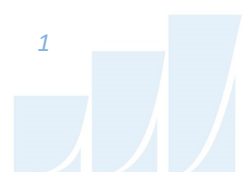
The focus of this traffic noise assessment is the Phase 1 of the proposed residential development, which features a C-shaped nine-storey residential building, located at 1509 Merivale Road in Ottawa, Ontario. For the purposes of this study, the elevation facing Merivale Road will be referred to as the west elevation. The study site is located on an irregular shaped parcel of land bordered by Merivale Road to the west, near the intersection of Merivale Road and Lotta Avenue.

The proposed development comprises a nine-storey building of C-shaped planform. The building's ground floor comprises amenities, a residential lobby, building support functions, and residential units. Residential units occupy floors 2-9, while the floorplate is set back from the east elevation beginning at Level 7. The site is surrounded by low-rise residential neighbourhoods to the east and west, and a variety of low- and mid-rise commercial buildings along Merivale Road.

The major sources of traffic noise are Merivale Road, Clyde Avenue, and Lotta Avenue. Arterial or collector roadways beyond 100 meters from the study site are not included as sources influencing the study site as per ENCG Section 2.1. Figure 1 illustrates a complete site plan with the surrounding context.

² City of Ottawa Environmental Noise Control Guidelines, January 2016

³ Ontario Ministry of the Environment and Climate Change – Environmental Noise Guidelines, Publication NPC-300, Queens Printer for Ontario, Toronto, 2013



3. OBJECTIVES

The principal objectives of this study are to (i) calculate the future noise levels on the study buildings produced by local roadway traffic, and (ii) ensure that interior and exterior noise levels do not exceed the allowable limits specified by the City of Ottawa's Environmental Noise Control Guidelines as outlined in Section 4.2 of this report.

4. METHODOLOGY

4.1 Background

Noise can be defined as any obtrusive sound. It is created at a source, transmitted through a medium, such as air, and intercepted by a receiver. Noise may be characterized in terms of the power of the source or the sound pressure at a specific distance. While the power of a source is characteristic of that particular source, the sound pressure depends on the location of the receiver and the path that the noise takes to reach the receiver. Measurement of noise is based on the decibel unit, dBA, which is a logarithmic ratio referenced to a standard noise level (2×10^{-5} Pascals). The 'A' suffix refers to a weighting scale, which better represents how the noise is perceived by the human ear. With this scale, a doubling of power results in a 3 dBA increase in measured noise levels and is just perceptible to most people. An increase of 10 dBA is often perceived to be twice as loud.

4.2 Roadway Traffic Noise

4.2.1 Criteria for Roadway Traffic Noise

For surface roadway traffic noise, the equivalent sound energy level, L_{eq} , provides a measure of the time varying noise levels, which is well correlated with the annoyance of sound. It is defined as the continuous sound level, which has the same energy as a time varying noise level over a period of time. For roadways, the L_{eq} is commonly calculated on the basis of a 16-hour (L_{eq16}) daytime (07:00-23:00) / 8-hour (L_{eq8}) nighttime (23:00-07:00) split to assess its impact on residential buildings. The City of Ottawa's Environmental Noise Control Guidelines (ENCG) specifies that the recommended indoor noise limit range (that is relevant to this study) is 45 and 40 dBA for living rooms and sleeping quarters respectively for roadway as listed in Table 1. However, to account for deficiencies in building construction and to control peak noise, these levels should be targeted toward 42 and 37 dBA.



TABLE 1: INDOOR SOUND LEVEL CRITERIA (ROAD)⁴

Type of Space	Time Period	Leq (dBA)
General offices, reception areas, retail stores, etc.	07:00 – 23:00	50
Living/dining/den areas of residences , hospitals, schools, nursing/retirement homes, day-care centres, theatres, places of worship, libraries, individual or semi-private offices, conference rooms, etc.	07:00 – 23:00	45
Sleeping quarters of hotels/motels	23:00 – 07:00	45
Sleeping quarters of residences , hospitals, nursing/retirement homes, etc.	23:00 – 07:00	40

Predicted noise levels at the plane of window (POW) dictate the action required to achieve the recommended sound levels. An open window is considered to provide a 10 dBA reduction in noise, while a standard closed window is capable of providing a minimum 20 dBA noise reduction⁵. A closed window due to a ventilation requirement will bring noise levels down to achieve an acceptable indoor environment⁶. Therefore, where noise levels exceed 55 dBA daytime and 50 dBA nighttime, the ventilation for the building should consider the need for having windows and doors closed, which triggers the need for forced air heating with provision for central air conditioning. Where noise levels exceed 65 dBA daytime and 60 dBA nighttime, air conditioning will be required and building components will require higher levels of sound attenuation⁷.

The sound level criterion for outdoor living areas is 55 dBA, which applies during the daytime (07:00 to 23:00). When noise levels exceed 55 dBA, mitigation must be provided to reduce noise levels where technically and administratively feasible to acceptable levels at or below the criterion.

⁴ Adapted from ENCG 2016 – Tables 2.2b and 2.2c

⁵ Burberry, P.B. (2014). Mitchell’s Environment and Services. Routledge, Page 125

⁶ MECP, Environmental Noise Guidelines, NPC 300 – Part C, Section 7.8

⁷ MECP, Environmental Noise Guidelines, NPC 300 – Part C, Section 7.1.3

4.2.2 Theoretical Roadway Noise Predictions

Noise predictions were performed with the aid of the MECP computerized noise assessment program, STAMSON 5.04, for road analysis. Appendix A includes the STAMSON 5.04 input and output data.

Roadway traffic noise calculations were performed by treating each roadway segment as separate line sources of noise. In addition to the traffic volumes summarized in Table 2, theoretical noise predictions were based on the following parameters:

- Truck traffic on all roadways was taken to comprise 5% heavy trucks and 7% medium trucks, as per ENCG requirements for noise level predictions.
- The day/night split for all streets was taken to be 92%/8%, respectively.
- Ground surfaces were taken to be reflective due to the presence of hard (paved) ground.
- Topography was assumed to be a flat/gentle slope surrounding the study building.
- Noise receptors were strategically placed at 6 locations around the study area (see Figure 2).
- Receptor height was taken to be 27.5 metres at Level 9 for the centre of the window (height to the 9th floor slab + 1.5 metres) for POW Receptors 1-4; and 18.5 metres for Receptors 5 and 6.
- Receptor distances and exposure angles are illustrated in Appendix Figures A1 - A6.

4.2.1 Roadway Traffic Volumes

The ENCG dictates that noise calculations should consider future sound levels based on a roadway's classification at the mature state of development. Therefore, traffic volumes are based on the roadway classifications outlined in the City of Ottawa's Official Plan (OP) and Transportation Master Plan⁸ which provide additional details on future roadway expansions. Average Annual Daily Traffic (AADT) volumes are then based on data in Table B1 of the ENCG for each roadway classification. Table 2 (below) summarizes the AADT values used for each roadway included in this assessment.

⁸ City of Ottawa Transportation Master Plan, November 2013

TABLE 2: ROADWAY TRAFFIC DATA

Segment	Roadway Traffic Data	Speed Limit (km/h)	Traffic Volumes
Route 17 (Merivale Road/Clyde Avenue)	6 Lane Urban Arterial Divided	60	50,000
Route 63 (Merivale Road)	4 Lane Urban Arterial Divided	60	35,000
Lotta Avenue	2 Lane Urban Collector	40	8,000

4.3 Indoor Noise Calculations

The difference between outdoor and indoor noise levels is the noise attenuation provided by the building envelope. According to common industry practice, complete walls and individual wall elements are rated according to the Sound Transmission Class (STC). The STC ratings of common residential walls built in conformance with the Ontario Building Code (2012) typically exceed STC 35, depending on exterior cladding, thickness and interior finish details. For example, brick veneer walls can achieve STC 50 or more. Standard commercially-sided exterior metal stud walls have around STC 45. Standard good quality double-glazed non-operable windows can have STC ratings ranging from 25 to 40, depending on the window manufacturer, pane thickness and inter-pane spacing. As previously mentioned, the windows are the known weak point in a partition.

As per Section 4.2, when daytime noise levels (from road and rail sources) at the plane of the window exceed 65 dBA, calculations must be performed to evaluate the sound transmission quality of the building components to ensure acceptable indoor noise levels. The calculation procedure⁹ considers:

- Window type and total area as a percentage of total room floor area
- Exterior wall type and total area as a percentage of the total room floor area
- Acoustic absorption characteristics of the room
- Outdoor noise source type and approach geometry
- Indoor sound level criteria, which varies according to the intended use of a space

⁹ Building Practice Note: Controlling Sound Transmission into Buildings by J.D. Quirt, National Research Council of Canada, September 1985

Based on published research¹⁰, exterior walls possess specific sound attenuation characteristics that are used as a basis for calculating the required STC ratings of windows in the same partition. Due to the limited information available at the time of the study, which was prepared for site plan approval, detailed floor layouts and building elevations have not been finalized; therefore, detailed STC calculations could not be performed at this time. As a guideline, the anticipated STC requirements for windows have been estimated based on the overall noise reduction required for each intended use of space (STC = outdoor noise level – targeted indoor noise levels).

5. RESULTS AND DISCUSSION

5.1 Roadway Traffic Noise Levels

The results of the roadway traffic noise calculations are summarized in Table 3 below. A complete set of input and output data from all STAMSON 5.04 calculations are available in Appendix A.

TABLE 3: EXTERIOR NOISE LEVELS DUE TO ROAD TRAFFIC

Receptor Number	Receptor Height Above Grade (m)	Receptor Location	STAMSON 5.04 Noise Level (dBA)	
			Day	Night
1	27.5	POW – 9th Floor – North Façade	70	62
2	27.5	POW – 9th Floor – West Façade	73	65
3	27.5	POW – 9th Floor – South Façade (West Side)	69	62
4	27.5	POW – 9th Floor – South Façade (Inset)	64	56
5	18.5	POW – 6th Floor – South Façade (East Side)	65	57
6	18.5	POW – 6th Floor – West Façade (East Side)	65	57

The results of the current analysis indicate that noise levels will range between 64 and 73 dBA during the daytime period (07:00-23:00) and between 56 and 65 dBA during the nighttime period (23:00-07:00). The highest noise level (73 dBA) occurs at the west façade, which is nearest and most exposed to Merivale Road.

¹⁰ CMHC, Road & Rail Noise: Effects on Housing

5.2 Noise Control Measures

The noise levels predicted due to roadway traffic exceed the criteria listed in Section 4.2 for building components. As discussed in Section 4.3, the anticipated STC requirements for windows have been estimated based on the overall noise reduction required for each intended use of space (STC = outdoor noise level – targeted indoor noise levels). As per city of Ottawa requirements, detailed STC calculations will be required to be completed prior to building permit application for each unit type. The STC requirements for the windows are summarized below for various units within the development (see Figure 3):

- **Bedroom Windows**
 - (i) Bedroom windows facing north will require a minimum STC of 33
 - (ii) Bedroom windows facing east will require a minimum STC of 36
 - (iii) Bedroom windows facing south on the west side of the building will require a minimum STC of 32
 - (iv) All other bedroom windows are to satisfy Ontario Building Code (OBC 2012) requirements

- **Living Room Windows**
 - (i) Living room windows facing north will require a minimum STC of 28
 - (ii) Living room windows facing east will require a minimum STC of 31
 - (iii) Living room windows facing south on the west side of the building require a minimum STC of 27
 - (iv) All other living room windows are to satisfy Ontario Building Code (OBC 2012) requirements

- **Exterior Walls**
 - (i) Exterior wall components on the south, east and west façades will require a minimum STC of 45, which will be achieved with brick cladding or an acoustical equivalent according to NRC test data¹¹

The STC requirements apply to windows, doors, spandrel panels and curtainwall elements. Exterior wall components on these façades are recommended to have a minimum STC of 45, where a window/wall system is used. A review of window supplier literature indicates that the specified STC ratings can be achieved by a variety of window systems having a combination of glass thickness and inter-pane spacing.

¹¹ J.S. Bradley and J.A. Birta. Laboratory Measurements of the Sound Insulation of Building Façade Elements, National Research Council October 2000.

We have specified an example window configuration, however, several manufacturers and various combinations of window components, such as those proposed, will offer the necessary sound attenuation rating. It is the responsibility of the manufacturer to ensure that the specified window achieves the required STC. This can only be assured by using window configurations that have been certified by laboratory testing. The requirements for STC ratings assume that the remaining components of the building are constructed and installed according to the minimum standards of the Ontario Building Code. The specified STC requirements also apply to swinging and/or sliding patio doors.

Results of the calculations also indicate that the development will require central air conditioning, which will allow occupants to keep windows closed and maintain a comfortable living environment. In addition to ventilation requirements, Warning Clauses will also be required in all Lease, Purchase and Sale Agreements, as summarized in Section 6.

6. CONCLUSIONS AND RECOMMENDATIONS

The results of the current analysis indicate that noise levels will range between 64 and 73 dBA during the daytime period (07:00-23:00) and between 56 and 65 dBA during the nighttime period (23:00-07:00). The highest noise level (73 dBA) occurs at the west façade, which is nearest and most exposed to Merivale Road. Building components with a higher Sound Transmission Class (STC) rating will be required where exterior noise levels exceed 65 dBA, as indicated in Figure 3.

Results of the calculations also indicate that the development will require central air conditioning, which will allow occupants to keep windows closed and maintain a comfortable living environment. The following 'Type D' Warning Clause¹² will also be required to be placed on all Lease, Purchase and Sale Agreements, as summarized below:

"This dwelling unit has been supplied with a central air conditioning system which will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the sound level limits of the Municipality and the Ministry of the Environment."

¹² MECP, Environmental Noise Guidelines, NPC 300

With regards to stationary noise impacts from the building on the surroundings and itself, noise can be controlled by judicious selection of the mechanical equipment and its placement on a high roof or in a mechanical penthouse. Where necessary noise screens, silencers, or acoustic louvers can be incorporated into the design to ensure compliance with the ENCG sound level limits. A stationary noise study will be performed once mechanical plans for the proposed building become available. This study will include recommendations for any noise control measures that may be necessary to ensure noise levels meet ENCG criteria.

This concludes our traffic noise assessment and report. If you have any questions or wish to discuss our findings please advise us. In the interim, we thank you for the opportunity to be of service.

Sincerely,

Gradient Wind Engineering Inc.

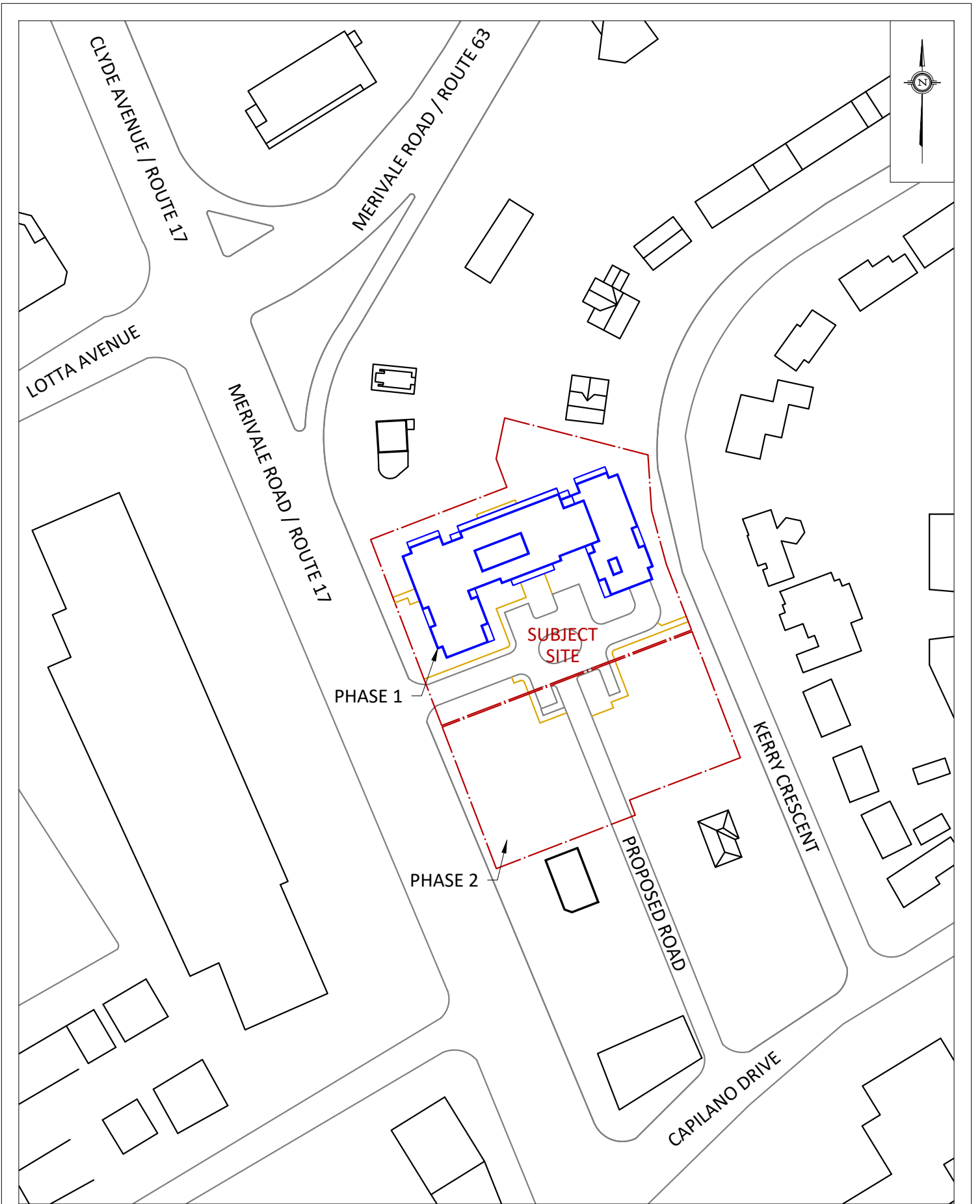


Tanyon Matheson-Fitchett, B.Eng.
Junior Environmental Scientist

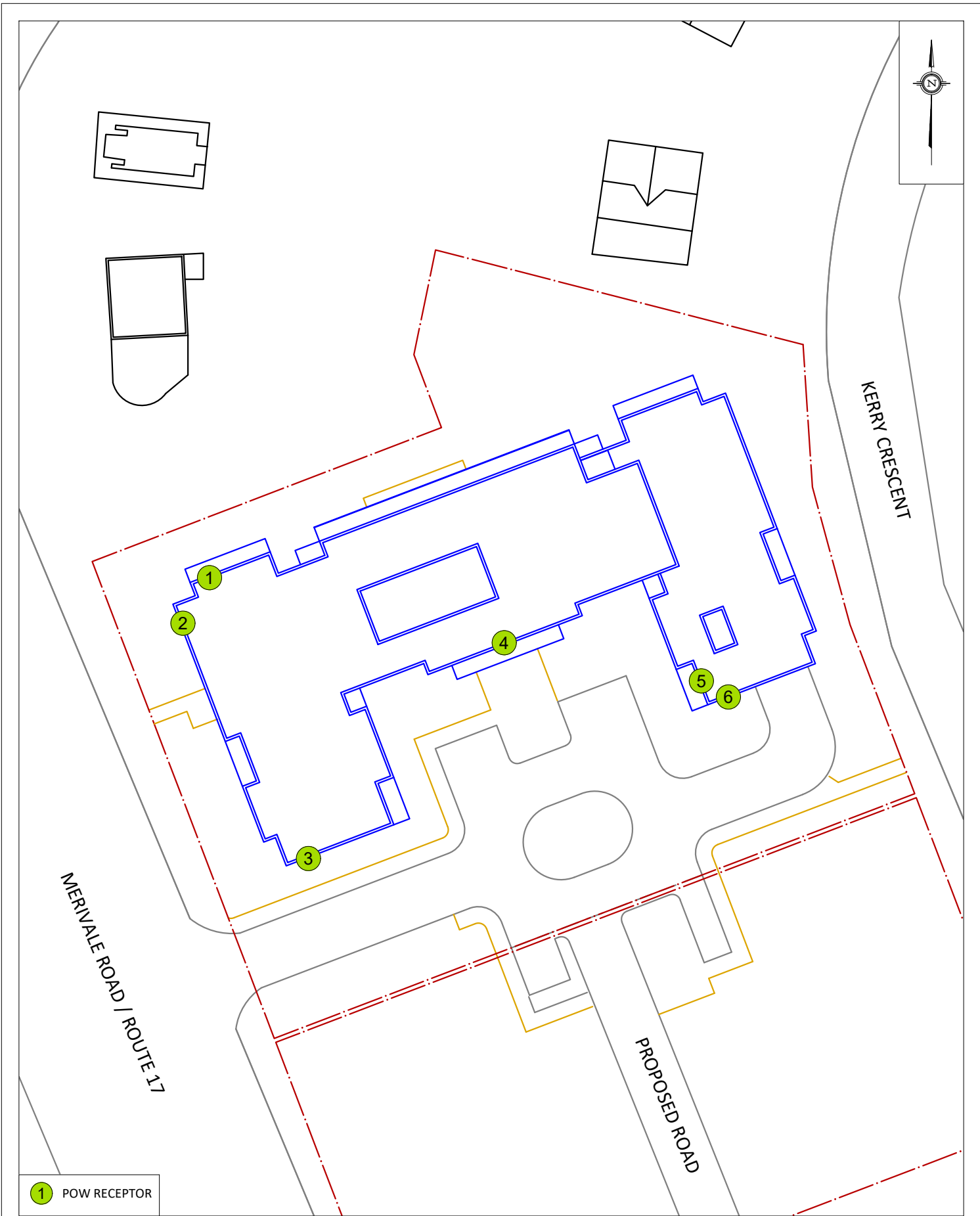
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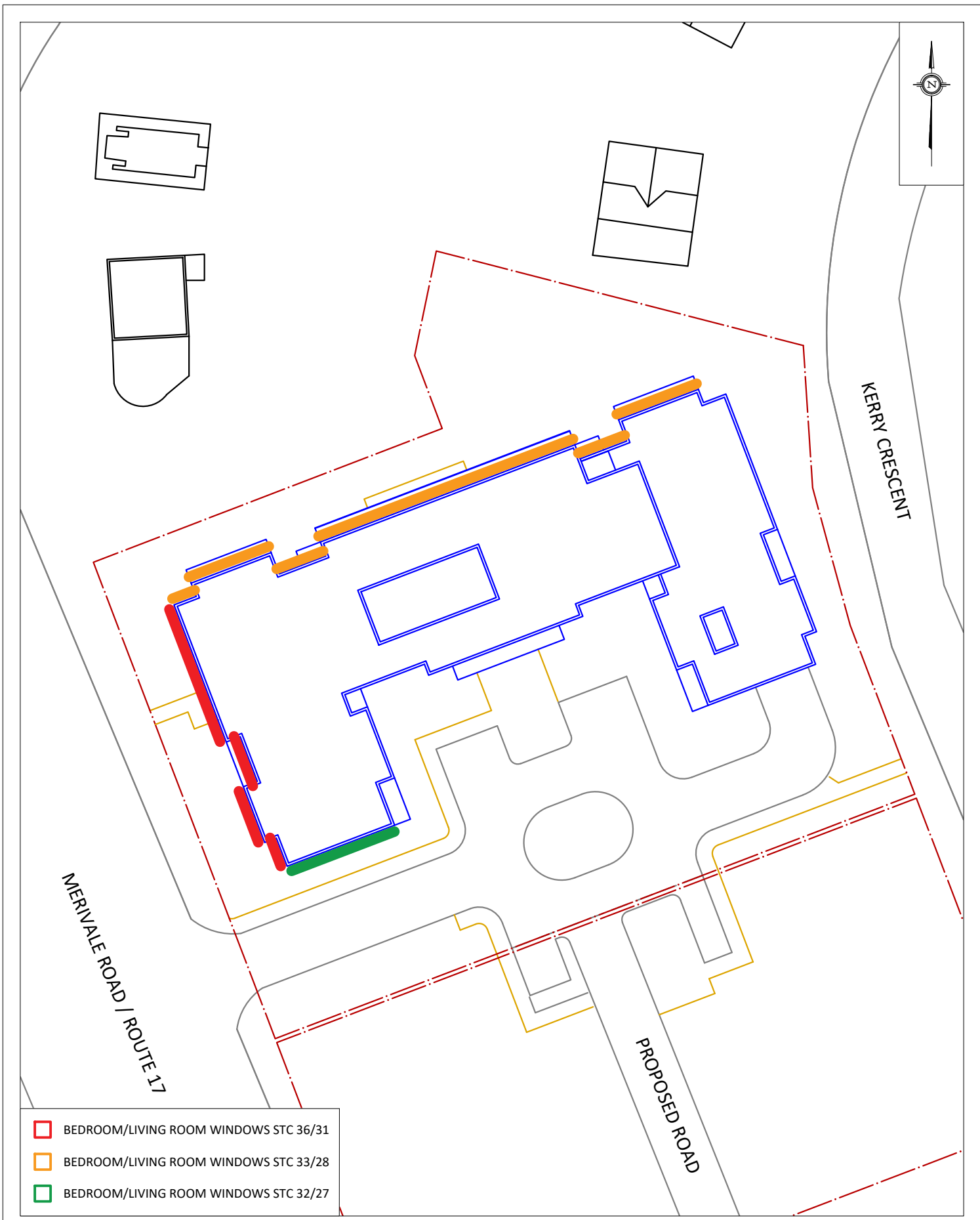
Joshua Foster, P.Eng.
Lead Engineer



GRADIENTWIND ENGINEERS & SCIENTISTS 127 WALGREEN ROAD, OTTAWA, ON 613 836 0934 • GRADIENTWIND.COM	PROJECT 1509 MERIVALE ROAD, OTTAWA ROADWAY TRAFFIC NOISE ASSESSMENT		DESCRIPTION FIGURE 1: SITE PLAN AND SURROUNDING CONTEXT
	SCALE 1:1500	DRAWING NO. GW21-198-1	
	DATE JULY 8, 2021	DRAWN BY T.M.F.	

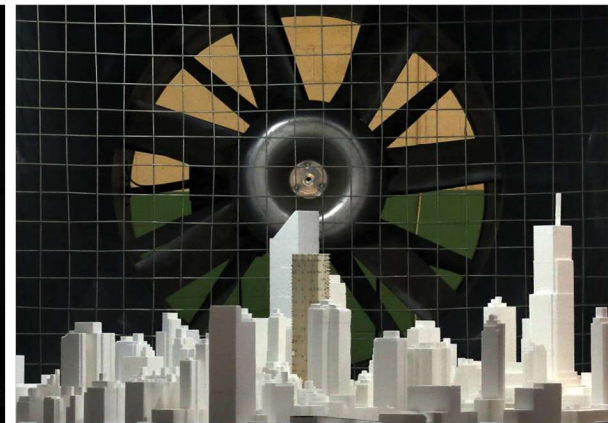
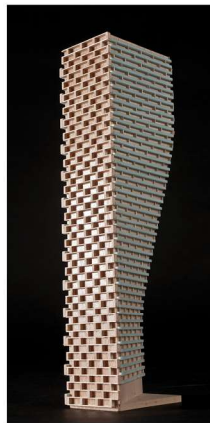


PROJECT	1509 MERIVALE ROAD, OTTAWA ROADWAY TRAFFIC NOISE ASSESSMENT	
SCALE	1:600	DRAWING NO. GW21-198-2
DATE	JULY 8, 2021	DRAWN BY T.M.F.



- BEDROOM/LIVING ROOM WINDOWS STC 36/31
- BEDROOM/LIVING ROOM WINDOWS STC 33/28
- BEDROOM/LIVING ROOM WINDOWS STC 32/27

PROJECT	1509 MERIVALE ROAD, OTTAWA ROADWAY TRAFFIC NOISE ASSESSMENT	
SCALE	1:600	DRAWING NO. GW21-198-3
DATE	JULY 12, 2021	DRAWN BY T.M.F.



APPENDIX A

STAMSON 5.04 – INPUT AND OUTPUT DATA

GRADIENTWIND

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STAMSON 5.0 NORMAL REPORT Date: 08-07-2021 13:47:03
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r1.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: LOTTA (day/night)

Car traffic volume : 6477/563 veh/TimePeriod *
Medium truck volume : 515/45 veh/TimePeriod *
Heavy truck volume : 368/32 veh/TimePeriod *
Posted speed limit : 40 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 8000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: LOTTA (day/night)

Angle1 Angle2 : -90.00 deg -12.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 96.00 / 96.00 m
Receiver height : 27.50 / 27.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00



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Road data, segment # 2: Route 63_1 (day/night)

Car traffic volume : 28336/2464 veh/TimePeriod *
Medium truck volume : 2254/196 veh/TimePeriod *
Heavy truck volume : 1610/140 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 35000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: Route 63_1 (day/night)

Angle1 Angle2 : -12.00 deg 29.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 96.00 / 96.00 m
Receiver height : 27.50 / 27.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00



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Road data, segment # 3: Route 63_1 (day/night)

Car traffic volume : 28336/2464 veh/TimePeriod *
Medium truck volume : 2254/196 veh/TimePeriod *
Heavy truck volume : 1610/140 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 35000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: Route 63_1 (day/night)

Angle1 Angle2 : 52.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 57.00 / 57.00 m
Receiver height : 27.50 / 27.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00



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Road data, segment # 4: Route 17 (day/night)

Car traffic volume : 40480/3520 veh/TimePeriod *
Medium truck volume : 3220/280 veh/TimePeriod *
Heavy truck volume : 2300/200 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 50000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 4: Route 17 (day/night)

Angle1 Angle2 : 2.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 32.00 / 32.00 m
Receiver height : 27.50 / 27.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00



Results segment # 1: LOTTA (day)

Source height = 1.50 m

ROAD (0.00 + 52.26 + 0.00) = 52.26 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	-12	0.00	63.96	0.00	-8.06	-3.63	0.00	0.00	0.00	52.26

Segment Leq : 52.26 dBA

Results segment # 2: Route 63_1 (day)

Source height = 1.50 m

ROAD (0.00 + 59.19 + 0.00) = 59.19 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-12	29	0.00	73.68	0.00	-8.06	-6.42	0.00	0.00	0.00	59.19

Segment Leq : 59.19 dBA



Results segment # 3: Route 63_1 (day)

Source height = 1.50 m

ROAD (0.00 + 61.12 + 0.00) = 61.12 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
52	90	0.00	73.68	0.00	-5.80	-6.75	0.00	0.00	0.00	61.12

Segment Leq : 61.12 dBA

Results segment # 4: Route 17 (day)

Source height = 1.50 m

ROAD (0.00 + 68.83 + 0.00) = 68.83 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
2	90	0.00	75.22	0.00	-3.29	-3.11	0.00	0.00	0.00	68.83

Segment Leq : 68.83 dBA

Total Leq All Segments: 69.97 dBA



Results segment # 1: LOTTA (night)

Source height = 1.50 m

ROAD (0.00 + 44.67 + 0.00) = 44.67 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	-12	0.00	56.36	0.00	-8.06	-3.63	0.00	0.00	0.00	44.67

Segment Leq : 44.67 dBA

Results segment # 2: Route 63_1 (night)

Source height = 1.50 m

ROAD (0.00 + 51.59 + 0.00) = 51.59 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-12	29	0.00	66.08	0.00	-8.06	-6.42	0.00	0.00	0.00	51.59

Segment Leq : 51.59 dBA



Results segment # 3: Route 63_1 (night)

Source height = 1.50 m

ROAD (0.00 + 53.53 + 0.00) = 53.53 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
52	90	0.00	66.08	0.00	-5.80	-6.75	0.00	0.00	0.00	53.53

Segment Leq : 53.53 dBA

Results segment # 4: Route 17 (night)

Source height = 1.50 m

ROAD (0.00 + 61.23 + 0.00) = 61.23 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
2	90	0.00	67.63	0.00	-3.29	-3.11	0.00	0.00	0.00	61.23

Segment Leq : 61.23 dBA

Total Leq All Segments: 62.37 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 69.97
(NIGHT): 62.37



GRADIENTWIND

ENGINEERS & SCIENTISTS

STAMSON 5.0 NORMAL REPORT Date: 08-07-2021 13:40:46
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r2.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: LOTTA (day/night)

Car traffic volume : 6477/563 veh/TimePeriod *
Medium truck volume : 515/45 veh/TimePeriod *
Heavy truck volume : 368/32 veh/TimePeriod *
Posted speed limit : 40 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 8000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: LOTTA (day/night)

Angle1 Angle2 : -90.00 deg -8.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 99.00 / 99.00 m
Receiver height : 27.50 / 27.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00



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Road data, segment # 2: Route 63 (day/night)

Car traffic volume : 28336/2464 veh/TimePeriod *
Medium truck volume : 2254/196 veh/TimePeriod *
Heavy truck volume : 1610/140 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 35000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: Route 63 (day/night)

Angle1 Angle2 : -8.00 deg 9.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 99.00 / 99.00 m
Receiver height : 27.50 / 27.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00



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Road data, segment # 3: Route 17 (day/night)

Car traffic volume : 40480/3520 veh/TimePeriod *
Medium truck volume : 3220/280 veh/TimePeriod *
Heavy truck volume : 2300/200 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 50000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: Route 17 (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 27.00 / 26.00 m
Receiver height : 27.50 / 27.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00



Results segment # 1: LOTTA (day)

Source height = 1.50 m

ROAD (0.00 + 52.35 + 0.00) = 52.35 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	-8	0.00	63.96	0.00	-8.20	-3.41	0.00	0.00	0.00	52.35

Segment Leq : 52.35 dBA

Results segment # 2: Route 63 (day)

Source height = 1.50 m

ROAD (0.00 + 55.23 + 0.00) = 55.23 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-8	9	0.00	73.68	0.00	-8.20	-10.25	0.00	0.00	0.00	55.23

Segment Leq : 55.23 dBA



Results segment # 3: Route 17 (day)

Source height = 1.50 m

ROAD (0.00 + 72.67 + 0.00) = 72.67 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	90	0.00	75.22	0.00	-2.55	0.00	0.00	0.00	0.00	72.67

Segment Leq : 72.67 dBA

Total Leq All Segments: 72.79 dBA

Results segment # 1: LOTTA (night)

Source height = 1.50 m

ROAD (0.00 + 44.75 + 0.00) = 44.75 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	-8	0.00	56.36	0.00	-8.20	-3.41	0.00	0.00	0.00	44.75

Segment Leq : 44.75 dBA



Results segment # 2: Route 63 (night)

Source height = 1.50 m

ROAD (0.00 + 47.64 + 0.00) = 47.64 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-8	9	0.00	66.08	0.00	-8.20	-10.25	0.00	0.00	0.00	47.64

Segment Leq : 47.64 dBA

Results segment # 3: Route 17 (night)

Source height = 1.50 m

ROAD (0.00 + 65.24 + 0.00) = 65.24 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	90	0.00	67.63	0.00	-2.39	0.00	0.00	0.00	0.00	65.24

Segment Leq : 65.24 dBA

Total Leq All Segments: 65.35 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 72.79
(NIGHT): 65.35



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STAMSON 5.0 NORMAL REPORT Date: 08-07-2021 13:51:02
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r3.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: Route 17 (day/night)

Car traffic volume : 40480/3520 veh/TimePeriod *
Medium truck volume : 3220/280 veh/TimePeriod *
Heavy truck volume : 2300/200 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 50000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: Route 17 (day/night)

Angle1 Angle2 : -90.00 deg 2.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 30.00 / 30.00 m
Receiver height : 27.50 / 27.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00



Results segment # 1: Route 17 (day)

Source height = 1.50 m

ROAD (0.00 + 69.30 + 0.00) = 69.30 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	2	0.00	75.22	0.00	-3.01	-2.91	0.00	0.00	0.00	69.30

Segment Leq : 69.30 dBA

Total Leq All Segments: 69.30 dBA

Results segment # 1: Route 17 (night)

Source height = 1.50 m

ROAD (0.00 + 61.70 + 0.00) = 61.70 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	2	0.00	67.63	0.00	-3.01	-2.91	0.00	0.00	0.00	61.70

Segment Leq : 61.70 dBA

Total Leq All Segments: 61.70 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 69.30
(NIGHT): 61.70



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STAMSON 5.0 NORMAL REPORT Date: 08-07-2021 13:52:59
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r4.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: Route 17 (day/night)

Car traffic volume : 40480/3520 veh/TimePeriod *
Medium truck volume : 3220/280 veh/TimePeriod *
Heavy truck volume : 2300/200 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 50000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: Route 17 (day/night)

Angle1 Angle2 : -90.00 deg 2.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 61.00 / 61.00 m
Receiver height : 27.50 / 27.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -36.00 deg Angle2 : 2.00 deg
Barrier height : 29.00 m
Barrier receiver distance : 18.00 / 18.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00



Results segment # 1: Route 17 (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	27.50	19.83	19.83

ROAD (63.90 + 42.38 + 0.00) = 63.93 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	-36	0.00	75.22	0.00	-6.09	-5.23	0.00	0.00	0.00	63.90
-36	2	0.00	75.22	0.00	-6.09	-6.75	0.00	0.00	-20.00	42.38

Segment Leq : 63.93 dBA

Total Leq All Segments: 63.93 dBA



Results segment # 1: Route 17 (night)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	27.50	19.83	19.83

ROAD (56.31 + 34.78 + 0.00) = 56.34 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	-36	0.00	67.63	0.00	-6.09	-5.23	0.00	0.00	0.00	56.31
-36	2	0.00	67.63	0.00	-6.09	-6.75	0.00	0.00	-20.00	34.78

Segment Leq : 56.34 dBA

Total Leq All Segments: 56.34 dBA

TOTAL Leq FROM ALL SOURCES (DAY) : 63.93
(NIGHT) : 56.34



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STAMSON 5.0 NORMAL REPORT Date: 08-07-2021 14:03:48
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r5.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: Route 17 (day/night)

Car traffic volume : 40480/3520 veh/TimePeriod *
Medium truck volume : 3220/280 veh/TimePeriod *
Heavy truck volume : 2300/200 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 50000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: Route 17 (day/night)

Angle1 Angle2 : -90.00 deg 21.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 81.00 / 81.00 m
Receiver height : 18.50 / 18.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -2.00 deg Angle2 : 21.00 deg
Barrier height : 29.00 m
Barrier receiver distance : 40.00 / 40.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00



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Road data, segment # 2: Route 17 (day/night)

Car traffic volume : 40480/3520 veh/TimePeriod *
Medium truck volume : 3220/280 veh/TimePeriod *
Heavy truck volume : 2300/200 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 50000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: Route 17 (day/night)

Angle1 Angle2 : 21.00 deg 47.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 81.00 / 81.00 m
Receiver height : 18.50 / 18.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : 21.00 deg Angle2 : 47.00 deg
Barrier height : 29.00 m
Barrier receiver distance : 20.00 / 20.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00



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Results segment # 1: Route 17 (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	18.50	10.10	10.10

ROAD (64.79 + 38.97 + 0.00) = 64.80 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	-2	0.00	75.22	0.00	-7.32	-3.11	0.00	0.00	0.00	64.79
-2	21	0.00	75.22	0.00	-7.32	-8.94	0.00	0.00	-20.00	38.97

Segment Leq : 64.80 dBA

Results segment # 2: Route 17 (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	18.50	14.30	14.30

ROAD (0.00 + 39.50 + 0.00) = 39.50 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
21	47	0.00	75.22	0.00	-7.32	-8.40	0.00	0.00	-20.00	39.50

Segment Leq : 39.50 dBA

Total Leq All Segments: 64.81 dBA



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Results segment # 1: Route 17 (night)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	18.50	10.10	10.10

ROAD (57.20 + 31.37 + 0.00) = 57.21 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	-2	0.00	67.63	0.00	-7.32	-3.11	0.00	0.00	0.00	57.20
-2	21	0.00	67.63	0.00	-7.32	-8.94	0.00	0.00	-20.00	31.37

Segment Leq : 57.21 dBA

Results segment # 2: Route 17 (night)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	18.50	14.30	14.30

ROAD (0.00 + 31.90 + 0.00) = 31.90 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
21	47	0.00	67.63	0.00	-7.32	-8.40	0.00	0.00	-20.00	31.90

Segment Leq : 31.90 dBA

Total Leq All Segments: 57.22 dBA

TOTAL Leq FROM ALL SOURCES (DAY) : 64.81
(NIGHT) : 57.22



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STAMSON 5.0 NORMAL REPORT Date: 08-07-2021 15:31:34
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r6.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: Route 17 (day/night)

Car traffic volume : 40480/3520 veh/TimePeriod *
Medium truck volume : 3220/280 veh/TimePeriod *
Heavy truck volume : 2300/200 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 50000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: Route 17 (day/night)

Angle1 Angle2 : -90.00 deg 2.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 83.00 / 83.00 m
Receiver height : 18.50 / 18.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00



Results segment # 1: Route 17 (day)

Source height = 1.50 m

ROAD (0.00 + 64.88 + 0.00) = 64.88 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	2	0.00	75.22	0.00	-7.43	-2.91	0.00	0.00	0.00	64.88

Segment Leq : 64.88 dBA

Total Leq All Segments: 64.88 dBA

Results segment # 1: Route 17 (night)

Source height = 1.50 m

ROAD (0.00 + 57.28 + 0.00) = 57.28 dBA

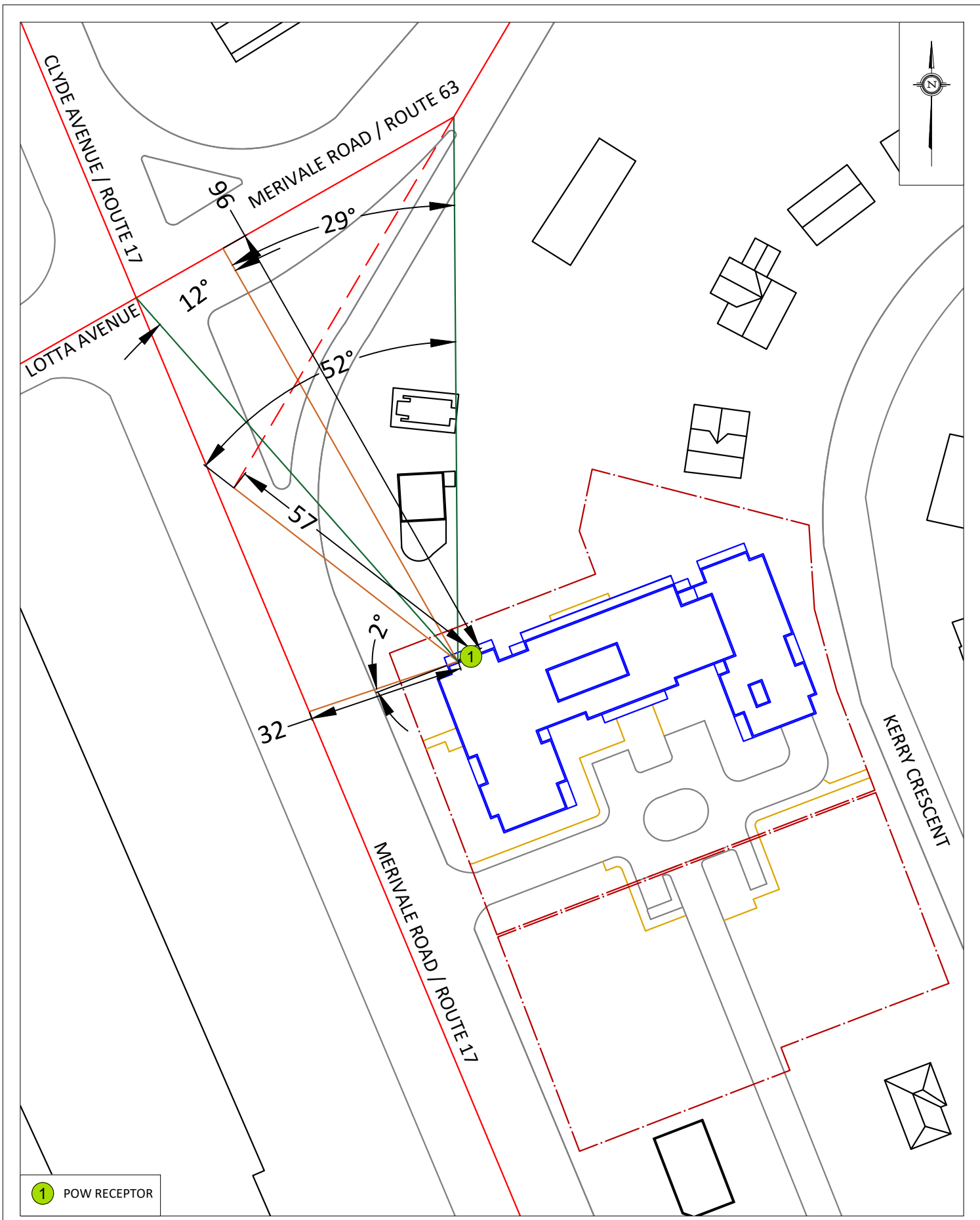
Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-90	2	0.00	67.63	0.00	-7.43	-2.91	0.00	0.00	0.00	57.28

Segment Leq : 57.28 dBA

Total Leq All Segments: 57.28 dBA

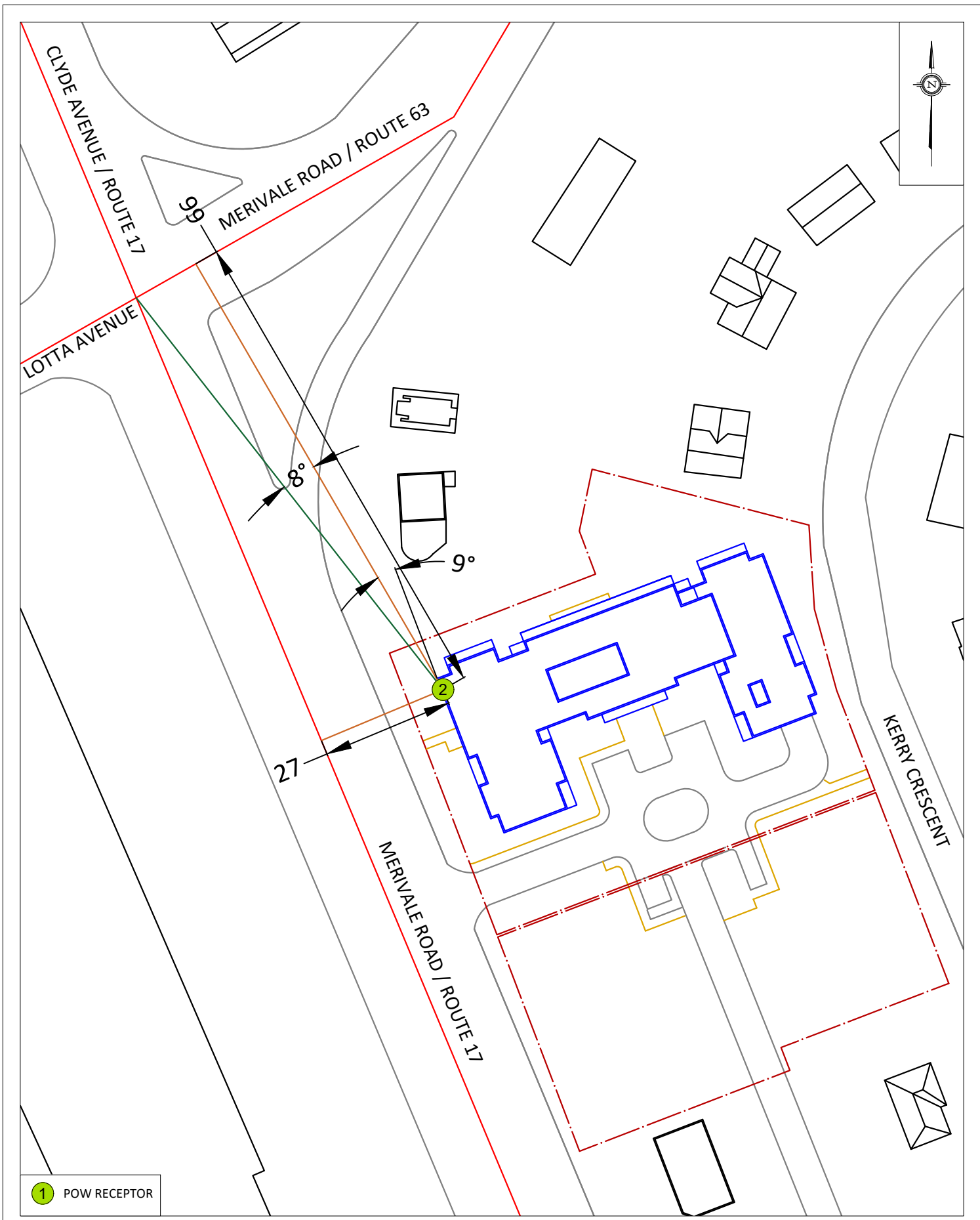
TOTAL Leq FROM ALL SOURCES (DAY): 64.88
(NIGHT): 57.28





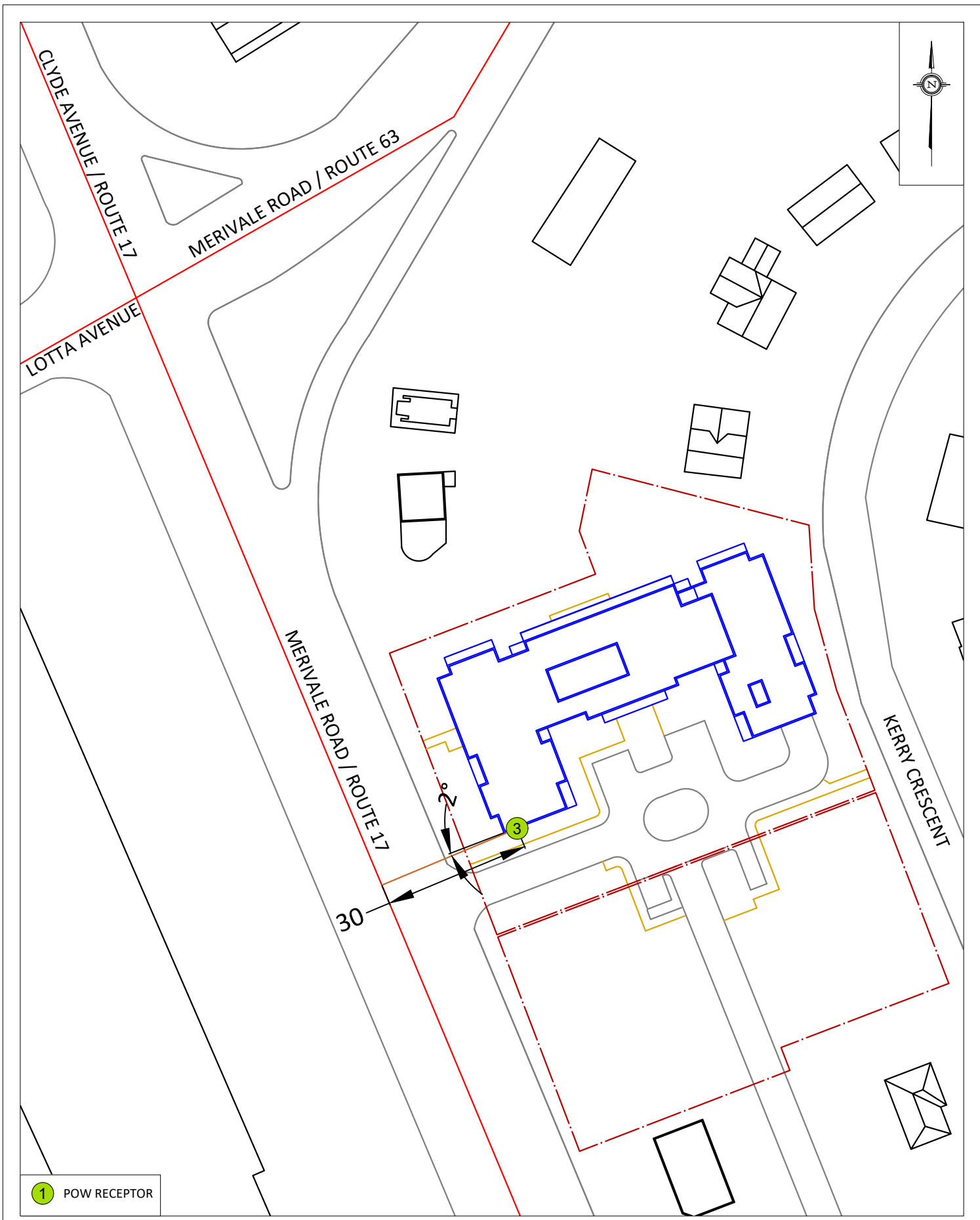
1 POW RECEPTOR

GRADIENTWIND ENGINEERS & SCIENTISTS 127 WALGREEN ROAD, OTTAWA, ON 613 836 0934 • GRADIENTWIND.COM	PROJECT	1509 MERIVALE ROAD, OTTAWA ROADWAY TRAFFIC NOISE ASSESSMENT		DESCRIPTION	FIGURE A1: RECEPTOR 1 STAMSON INPUT PARAMETERS
	SCALE	1:1000	DRAWING NO.	GW21-198-A1	
	DATE	JULY 8, 2021	DRAWN BY	T.M.F.	



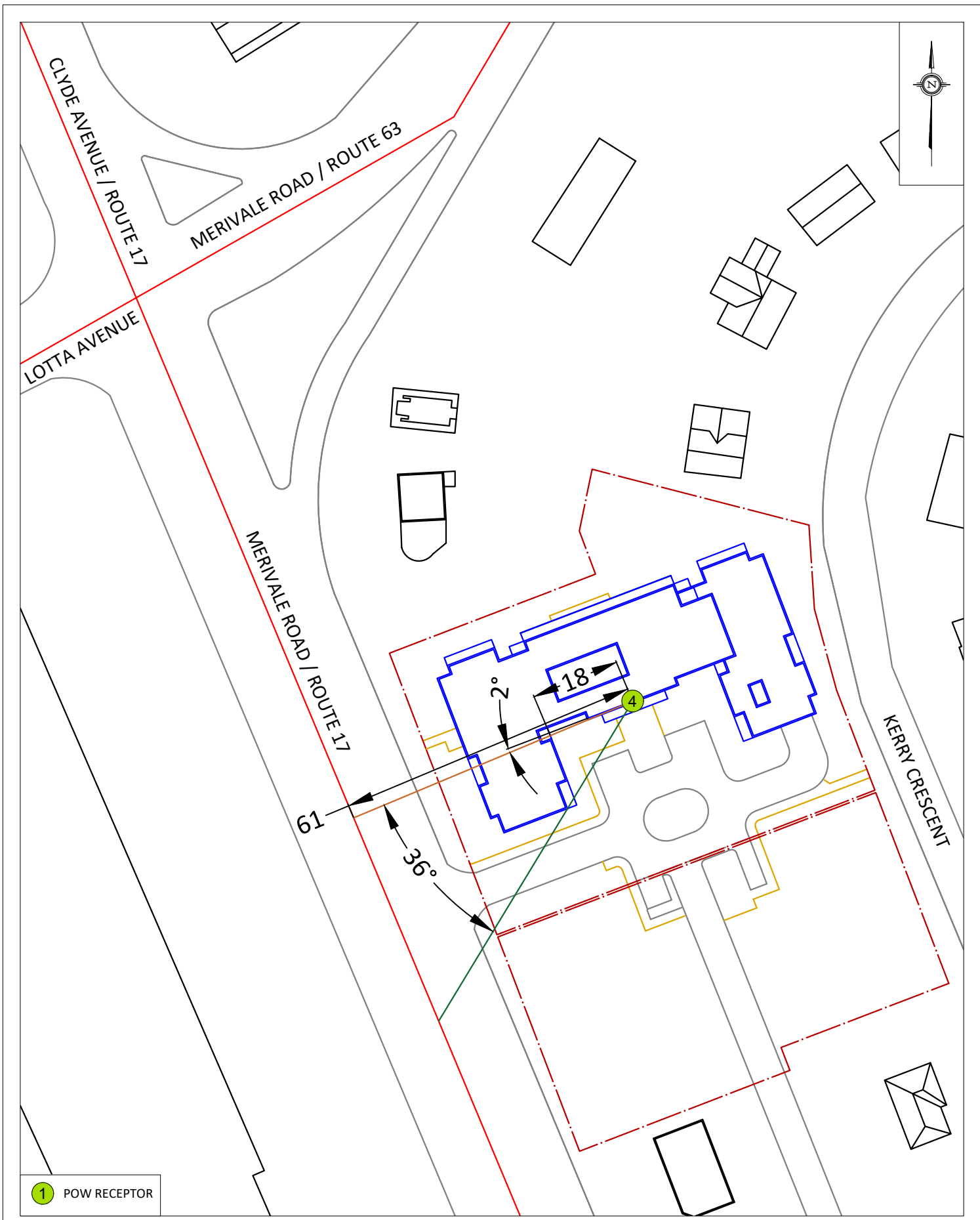
1 POW RECEPTOR

GRADIENTWIND ENGINEERS & SCIENTISTS 127 WALGREEN ROAD, OTTAWA, ON 613 836 0934 • GRADIENTWIND.COM	PROJECT 1509 MERIVALE ROAD, OTTAWA ROADWAY TRAFFIC NOISE ASSESSMENT		DESCRIPTION FIGURE A2: RECEPTOR 2 STAMSON INPUT PARAMETERS
	SCALE 1:1000	DRAWING NO. GW21-198-A2	
	DATE JULY 9, 2021	DRAWN BY T.M.F.	



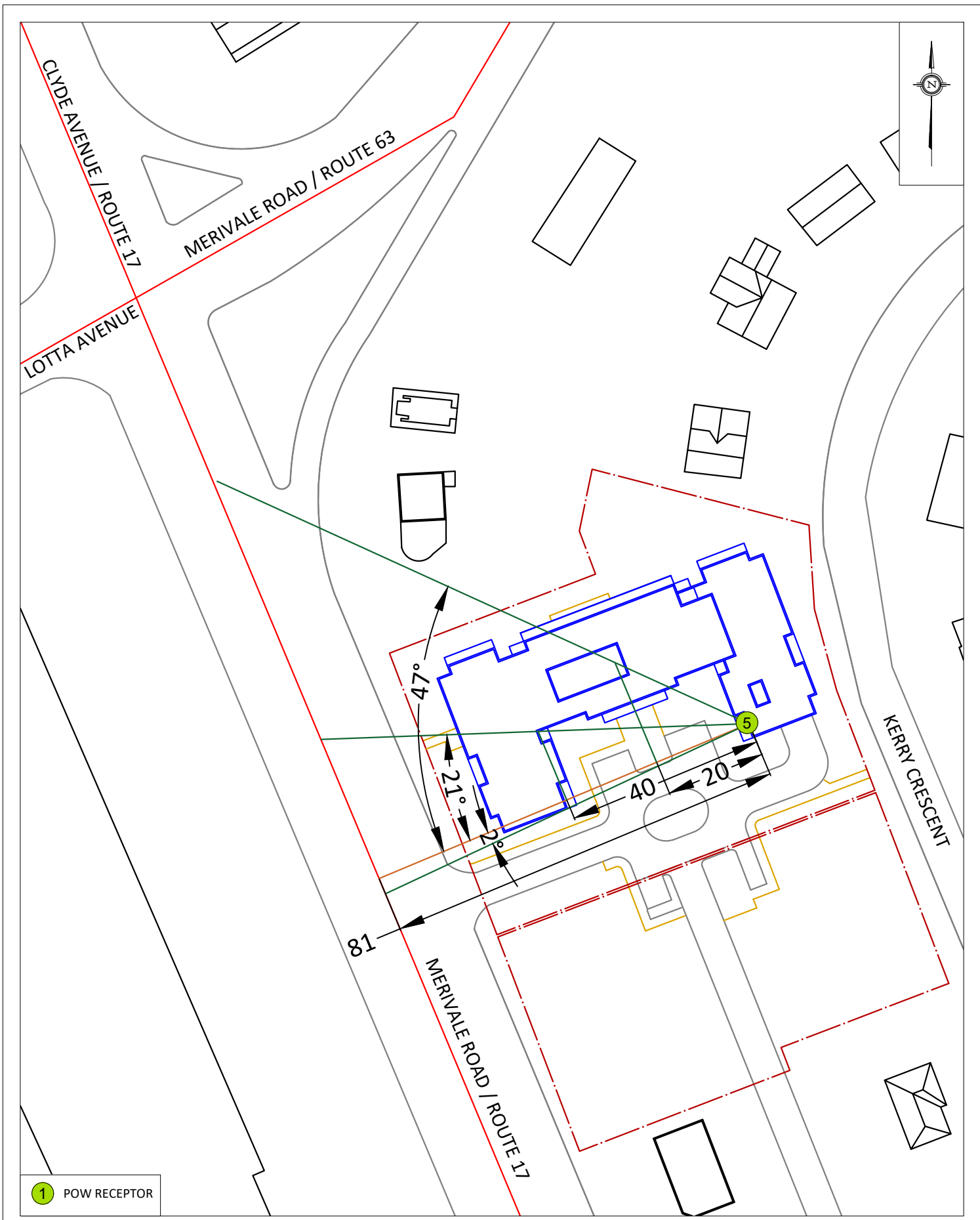
1 POW RECEPTOR

GRADIENTWIND ENGINEERS & SCIENTISTS 127 WALGREEN ROAD, OTTAWA, ON 613 836 0934 • GRADIENTWIND.COM	PROJECT	1509 MERIVALE ROAD, OTTAWA ROADWAY TRAFFIC NOISE ASSESSMENT		DESCRIPTION	FIGURE A3: RECEPTOR 3 STAMSON INPUT PARAMETERS
	SCALE	1:1000	DRAWING NO.	GW21-198-A3	
	DATE	JULY 9, 2021	DRAWN BY	T.M.F.	



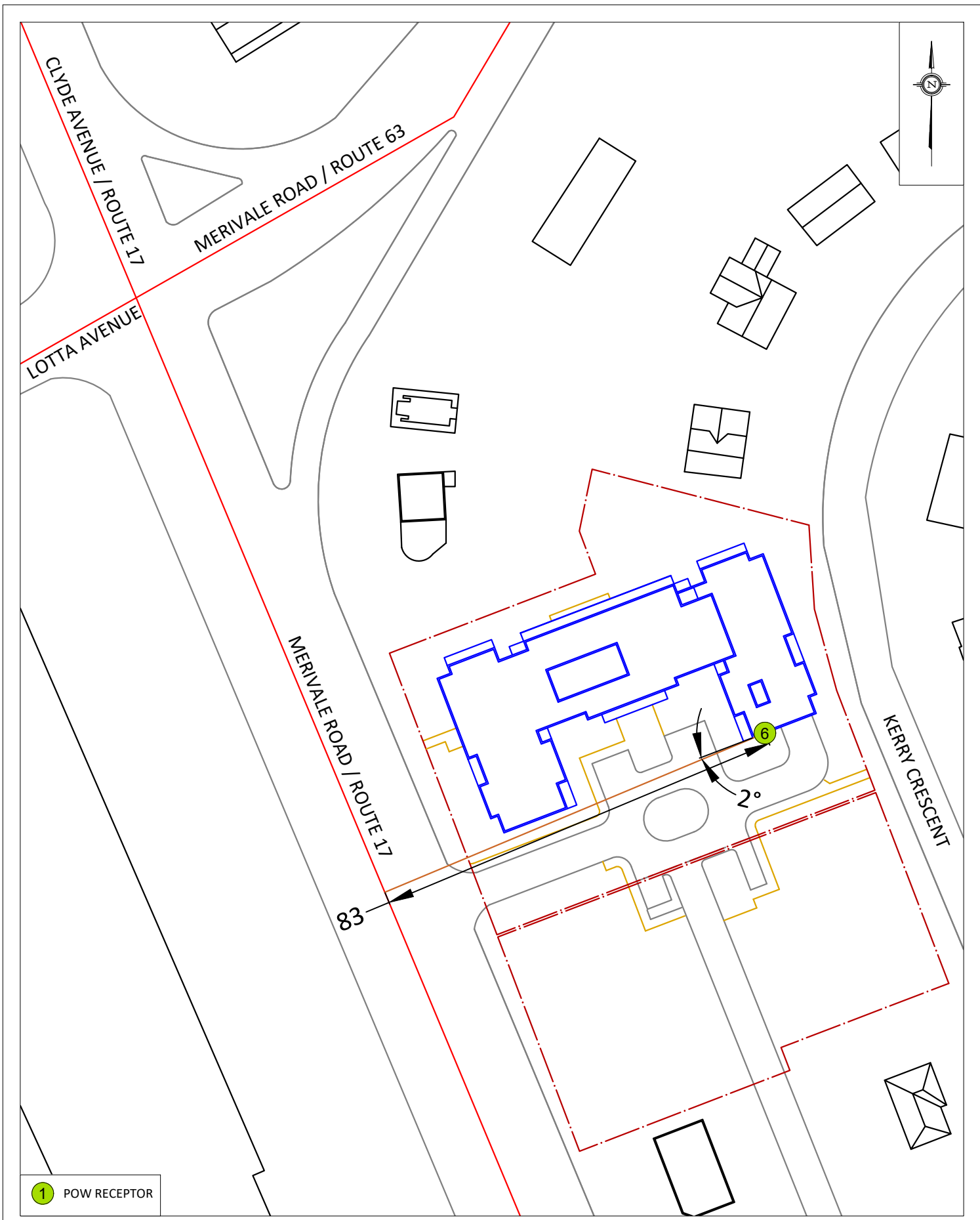
1 POW RECEPTOR

GRADIENTWIND ENGINEERS & SCIENTISTS 127 WALGREEN ROAD, OTTAWA, ON 613 836 0934 • GRADIENTWIND.COM	PROJECT	1509 MERIVALE ROAD, OTTAWA ROADWAY TRAFFIC NOISE ASSESSMENT		DESCRIPTION	FIGURE A4: RECEPTOR 4 STAMSON INPUT PARAMETERS
	SCALE	1:1000	DRAWING NO.	GW21-198-A4	
	DATE	JULY 9, 2021	DRAWN BY	T.M.F.	



1 POW RECEPTOR

GRADIENTWIND ENGINEERS & SCIENTISTS 127 WALGREEN ROAD, OTTAWA, ON 613 836 0934 • GRADIENTWIND.COM	PROJECT	1509 MERIVALE ROAD, OTTAWA ROADWAY TRAFFIC NOISE ASSESSMENT		DESCRIPTION	FIGURE A5: RECEPTOR 5 STAMSON INPUT PARAMETERS
	SCALE	1:1000	DRAWING NO.	GW21-198-A5	
	DATE	JULY 9, 2021	DRAWN BY	T.M.F.	



PROJECT	1509 MERIVALE ROAD, OTTAWA ROADWAY TRAFFIC NOISE ASSESSMENT	
SCALE	1:1000	DRAWING NO. GW21-198-A6
DATE	JULY 9, 2021	DRAWN BY T.M.F.