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## **Stormwater Management Report and Servicing Brief**

Proposed Halo Car Wash  
3555 Borrisokane Rd  
Barrhaven, Ontario

Prepared for:

Halo Car Wash Inc.  
18 Adelaide Street  
Maxville, ON  
K0C 1T0

Attention: Mr. Jordan Lupovici

Revised July 07, 2023  
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LRL File No.: 210691



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## 1 INTRODUCTION AND SITE DESCRIPTION

LRL Associates Ltd. was retained by Halo Car Wash Inc. to complete a Stormwater Management Analysis and Servicing Brief for the construction of a car-wash development located at 3555 Borriskane Rd, Barrhaven, Ontario. The property is legally described as Part of Lot 11, Concession 3 (Rideau Front), geographic Township of Nepean and Zoning IL – Light Industrial. The location of the proposed development can be viewed in Figure 1.



**Figure 1: Aerial View of Proposed Development**

The development proposes construction of a Halo Tunnel Car Wash ( $\pm 513$  sqm). The site will be accessible from a 7.5 m wide entrance located off Flagstaff Drive. This entrance will be a shared ROW once the future development to the south is developed. For additional details of the proposed development, refer to Site Plan C201 included in Appendix E.

This report has been prepared in consideration of the terms and conditions noted above and with the civil drawings prepared for the proposed new development. Should there be any changes in the design features, which may relate to the stormwater management and servicing considerations, LRL Associates Ltd. should be advised to review the report recommendations.

## 2 EXISTING SITE AND DRAINAGE DESCRIPTION

The subject site measures approximately 0.534 ha and is currently undeveloped, consisting of grassed area and treed area. Elevations of existing site range between 93.01 near the northeast corner to 92.23 at the southwest corner of the site.

Sewer and watermain locations were adopted from the current subdivision design produced by DSEL Engineering. It indicates the following infrastructures located within the adjacent right-of-way:

### Flagstaff Drive

- 200 mm diameter PVC watermain stub
- 200 mm diameter PVC sanitary sewer

### Borrisokane Rd

- Roadside ditch

The design intentions are to continue the water and sanitary services that were provided through this subject property and stub them past the proposed curb for future development to the south. This development will be connected to those services, and the storm outlet will be directed to the roadside ditch along Borrisokane Rd.

## 3 SCOPE OF WORK

As per applicable guidelines, the scope of work includes the following:

### Stormwater management

- Calculate the allowable stormwater release rate.
- Calculate the anticipated post-development stormwater release rates.
- Demonstrate how the target quantity control objectives will be achieved.
- Demonstrate how the target quality control objectives will be achieved.

### Water services

- Calculate the expected water supply demand at average and peak conditions.
- Calculate the required fire flow as per the Fire Underwriters Survey (FUS) method.
- Confirm the adequacy of water supply and pressure during peak flow and fire flow.
- Describe the proposed water distribution network and connection to the existing system.



## **Sanitary services**

- Describe the existing sanitary sewers available to receive wastewater from the proposed development.
- Calculate peak flow rates from the proposed development.
- Describe the proposed sanitary sewer system.

## **4 REGULATORY APPROVALS**

An MECP Environmental Compliance Approval (ECA) is expected to be required for installation of the proposed storm and sanitary sewers within the site. A Permit to Take Water is not anticipated to be required for pumping requirements for sewer installation. The Rideau Valley Conservation Authority (RVCA) will need to be consulted in order to obtain municipal approval for site development. No other approval requirements from other regulatory agencies are anticipated.

## **5 WATER SUPPLY AND FIRE PROTECTION**

### **5.1 Existing Water Supply Services**

The subject property is located to the south of a proposed 300 mm dia. watermain along Flagstaff Drive. A 200 mm dia. water service stub is available near the northeast corner of the property for service connection.

### **5.2 Water Supply Servicing Design**

The subject property is proposed to be serviced via a 100 mm dia. water servicing to be connected to the 200 mm dia. watermain which will be extended from the existing stub located within Flagstaff Drive at the northeast corner of the site. Since the average water demand exceeds 50 m<sup>3</sup>/day, a looped system separated by an isolation valve is proposed. For servicing layout, refer to Site Servicing Plan C401 (Appendix E).

Table 1 summarizes the City of Ottawa Design Guidelines design parameters employed in the preparation of the water demand estimate.



**Table 1: City of Ottawa Water Servicing Design Parameters**

<b>Design Parameters</b>	<b>Value</b>
Average Day Demand - Commercial	28,000 L/gross ha/day
Average Day Demand - Light Industrial	35,000 L/gross ha/day
Maximum Day Demand-Commercial/Industrial	1.5 × Average Day Demand
Maximum Hour Demand-Commercial/Industrial	1.8 × Maximum Day Demand
Minimum Depth of Cover	2.4 m from top of watermain to finished grade
Desired operating pressure during Maximum Day Flow	345 kPa (50 psi) to 552 kPa (80 psi)
Minimum allowable pressure during Peak Hour Flow	275 kPa (40 psi)
Minimum allowable pressure during Fire Flow Conditions	140 kPa (20 psi)

Below is a summary of anticipated water demands calculated by using the parameters mentioned in Table 1 together with anticipated car wash demand & demands from south parcels (Part 3 & Part 5) as per the Servicing Brief prepared by Pearson Engineering, dated Nov 17, 2022. Refer to Appendix B for calculation details.

- Average Day Demand = 1.85 L/s
- Maximum Day Demand = 3.14 L/s
- Peak Hour Demand = 7.74 L/s

The City of Ottawa provided boundary conditions associated with the estimated water demand (correspondence included in Appendix B). Table 2 below summarizes the boundary conditions for the proposed development.



**Table 2: Summary of Boundary Conditions**

Design Parameter	Anticipated Demand (L/s)	Boundary Conditions @ Flagstaff Dr.	
		*Existing Conditions (m H2O / psi)	*Future Conditions (SUC Pressure Zone) (m H2O / psi)
Average Daily Demand	1.85	156.4/89.4	146.7/75.6
Peak Hour	7.74	142.4/69.5	142.7/68.9
Max Day + Fire Flow	3.14 + 65	137.4/62.4	142.3/69.3
<i>*Ground elevation assumed at 93.5 m for Connection 1 @ Flagstaff Dr.</i>			

Hydraulic analysis of the proposed watermain & servicing network was performed using EPANET (Version 2.2). Below is the summary of calculated residual pressures above finished grade at the service entry node (J-7) at Halo Car Wash Building.

Existing Conditions (Pressure Zone 3SW)

- Scenario 1: Average Day = 89.24 psi
- Scenario 2: Peak Hour = 69.05 psi
- Scenario 3: Max Day + Fire Flow = 62.21 psi

Future Conditions (Pressure Zone SUC)

- Scenario 4: Average Day = 75.45 psi
- Scenario 5: Peak Hour = 69.48 psi
- Scenario 6: Max Day + Fire Flow = 69.17 psi

The available pressure mentioned above corroborates with the City design criteria mentioned in Table 1, except for the average day demand (Scenario 1) when the maximum pressure exceeds 80 psi. Therefore, a pressure reducing valve (PRV) is needed as the residual pressure is not to exceed 80 psi. For modeling results, see Appendix B.

The estimated fire flow for the proposed buildings was determined in accordance with Fire Underwriters Survey (FUS) using the formula:

$$F = 220C\sqrt{A}$$

where,

F = The required fire flow (L/min)

C = Coefficient related to the type of construction





A = The total floor area (m<sup>2</sup>)

The estimated fire flow demand is calculated 3900 L/min, see Appendix B for calculation details. Two (2) fire hydrants in proximity to the site along Flagstaff Dr is expected to provide required fire flow for the subject site. Refer to Servicing Plan C401 for the location of available fire hydrants.

## 6 SANITARY SERVICE

### 6.1 Existing Sanitary Sewer Services

There is an existing 200 mm dia. sanitary sewer service stub extending to the property line from Flagstaff Dr. at the northeast corner of the subject site.

### 6.2 Sanitary Sewer Servicing Design

As previously stated, the sanitary sewer will be extended along the south extent of the property and stubbed at the proposed curb. The proposed development will be serviced via 150 mm dia. sanitary sewers which will be connected to the proposed 200mm dia. sanitary sewer extending to the subject site. Refer to LRL drawing C401 for the proposed sanitary servicing layout. Table 3 summarizes the City of Ottawa Design Guidelines design parameters used in the estimation of wastewater flow.

**Table 3: City of Ottawa Wastewater Design Parameters**

Design Parameters	Value
Commercial Average Flow	28,000 L/gross ha/day
Average Light Industrial Flow	35,000 L/gross ha/day
Commercial Peak Factor	1.5
Industrial Peak Factor	Appendix 4-B (City Guidelines-Sewer)
Infiltration Allowance (Dry Weather)	0.05 L/s/gross ha
Infiltration Allowance (Wet Weather)	0.28 L/s/gross ha
Total Infiltration Allowance	0.33 L/s/gross ha



Based on these parameters, City of Ottawa's Appendix 4-A (Daily Sewage Flow for Various Types of Establishments), and the car wash information as per Halo Car Wash, the anticipated post-development peak design wastewater flow for the subject site is calculated 6.32 L/s. Anticipated flow from future development is also included sanitary sewer design sheet, refer to Appendix C for calculation details.

## **7 STORMWATER MANAGEMENT**

### **7.1 Existing Stormwater Infrastructure**

There is an existing roadside ditch along Borrisokane Rd. at the west extent of the site.

In pre-development conditions, the stormwater runoff would flow uncontrolled overland to the existing ditch. Refer to Appendix D for pre- and post-development watershed information.

### **7.2 Design Criteria**

The stormwater management criteria for this development is based on pre-consultation meeting with the City of Ottawa officials, the City of Ottawa Sewer Design Guidelines, 2012 (City standards), as well as the Ministry of the Environment's Stormwater Management, Planning and Design Manual, 2003.

#### **7.2.1 Water Quality**

Based on site plan pre-consultation meeting note and correspondence with Rideau Valley Conservation Authority (RVCA), it was advised to achieve enhanced water quality protection (80% TSS removal) either through on-site or downstream infrastructure prior to discharging stormwater to a natural watercourse.

To address water quality objective, a treatment train approach is proposed. First, the stormwater TSS removal of 80.9% is achieved using StormTech Isolator Row Plus located downstream of STM MH08 and STM MH10. Second, TSS removal of 53.0% is achieved using Hydro International OGS unit (model FD-4HC) installed downstream of STM MH11. Together, the treatment train approach will provide a combined TSS removal of 90.9%. Greater detail of the treatment train sizing can be found in Appendix D.

#### **7.2.2 Water Quantity**

The allowable release rate for the subject site has been calculated to 5-yr pre-development level and was determined 30.95 L/s. Post-development storm events up to and including 100-yr storm



will be controlled to 5-yr pre-development level. For calculations, refer to STM design calculation sheets in Appendix D.

### 7.3 Method of Analysis

The modified Rational Method has been used to calculate the peak flow rate from the proposed site and to quantify the storage required for quantity control for the proposed development.

$$Q = 2.78CIA$$

Where,

Q = Flow (L/s)

C = Runoff Coefficient

I = Rainfall Intensity (mm/hr), determined from the City of Ottawa IDF curves

A = Area (ha)

Refer to Appendix D for runoff and storage calculations.

### 7.4 Proposed Stormwater Quantity Controls

The proposed stormwater management quantity control for this development will be accomplished using an Inlet Control Device (ICD). Storage required as a result of quantity control will be accomplished through surface storage in the parking lot and underground storage.

A network of storm sewers is proposed to service the site which will outlet to the existing ditch along Borrisokane Rd and eventually to the existing 800mm dia. culvert crossing Borrisokane Rd. Refer to Site Servicing Plan C401 and Appendix D for calculation details.

The existing site is delineated by catchments EWS-01 which currently drains uncontrolled towards the west and outlet to the existing ditch. Refer to Pre-development Watershed Plan C701 (Appendix E). The site has been analyzed and post-development watersheds have been allocated. A few watersheds WS-09 and WS-10 consisting of grass area will flow un-controlled off the site. For additional details, refer to Post-development Watershed Plan C702 (Appendix E). Overland flow in Halo Car Wash area within watersheds WS-01A, WS-01B, WS-02, WS-03, WS-04, WS-05, WS-06, WS-07 & WS-08 will be captured by a several CB/CBMHs. An ICD, Hydrovex Vortex Flow Regulator 125VHV-2 (or approved equivalent), is proposed at STM MH11 to restrict



the collected runoff and control the release rate at 24.86 L/s (H=2.06 m). For additional details on select ICD, refer to Appendix D. Table 4 summarizes post-development drainage areas. Additional details and calculations can be found in Appendix D.

**Table 4: Drainage Areas and Runoff Coefficients**

Watersheds	Area (ha)	Weighted Runoff Coefficient (C)
WS-01A (controlled)	0.045	0.29
WS-01B (controlled)	0.017	0.79
WS-02 (controlled)	0.049	0.90
WS-03 (controlled)	0.030	0.87
WS-04 (controlled)	0.101	0.58
WS-05 (controlled)	0.053	0.90
WS-06 (controlled)	0.123	0.87
WS-07 (controlled)	0.039	0.76
WS-08 (controlled)	0.027	0.20
WS-09 (uncontrolled)	0.029	0.20
WS-10 (uncontrolled)	0.020	0.20
<b>Total</b>	<b>0.534</b>	<b>0.67</b>

Table 5 summarizes the release rates, storage volume required and available storage in the proposed site. Refer to Appendix D for runoff and storage calculation details.

**Table 5: Summary of Stormwater Release Rates & Storage**

Watersheds	Area (ha)	Release Rate (L/s)			Storage Required (m <sup>3</sup> )			Total Storage Provided (m <sup>3</sup> )
		100-yr	5-yr	2-yr	100-yr	5-yr	2-yr	
Controlled (WS-01 to WS-08)	0.485	24.86	24.86	24.86	199.45	71.96	46.81	206.62
Uncontrolled (WS-09 to WS-10)	0.049	6.09	2.84	2.10	N/A	N/A	N/A	N/A
<b>Total</b>	<b>0.534</b>	<b>30.95</b>	<b>27.70</b>	<b>26.96</b>	<b>199.45</b>	<b>71.96</b>	<b>46.81</b>	<b>206.62</b>

The runoff exceeding the allowable release rate will be stored on-site via surficial ponding and underground storage in StormTech Chambers. For 100-yr storm event, it is calculated that a total of 199.45 m<sup>3</sup> of storage will be required to attenuate flows to the allowable release rate of 24.86 L/s (controlled release). The required storage will be accommodated through surface ponding in the parking lot which will provide 115.86 m<sup>3</sup> of storage and underground storage in StormTech chambers providing 90.76 m<sup>3</sup> of additional storage. It is important to note that the required storage for 2- and 5-yr storm will be accommodated underground within the StormTech chambers. The storm events greater than 100-yr will flow overland towards Borrisokane roadside ditch from the



spillover point (depressed curve) provided at 100-yr HWL elevation of 93.20, refer to Grading Plan (C301). The maximum ponding elevation and depths can be found on Stormwater Management Plan C601 (Appendix E).

## **8 EROSION AND SEDIMENT CONTROL**

During construction, erosion and sediment controls will be provided primarily via a sediment control fence to be erected along the perimeter of the site where runoff has the potential of leaving the site. Inlet sediment control devices are also to be provided in any catch basin and/or manholes in and around the site that may be impacted by the site construction. Construction and maintenance requirements for erosion and sediment controls are to comply with Ontario Provincial Standard Specification OPSS 577. Refer to Erosion and Sediment Control Plan C101 for additional details.

## **9 CONCLUSION**

This Stormwater Management and Servicing Report for the proposed development at 3555 Borrisokane Rd presents the rationale and details for the servicing requirements for the subject property. In accordance with the report objectives, the servicing requirements for the development are summarized below.

### **Water Service**

- The anticipated maximum hour demand of the proposed development is 6.72 L/s.
- The maximum required fire flow is 65.00 L/, calculated using the FUS method.
- The fire hydrants along Flagstaff Dr will service the proposed development.
- The proposed development will be serviced with a new 100 mm dia. water servicing which will connect to the proposed dual 200 mm dia. watermain to be extended from Flagstaff Dr.
- Boundary conditions received from the City of Ottawa show that adequate pressure is available to service the proposed development.

### **Sanitary Service**

- The anticipated sanitary flow from the proposed development is 6.32 L/s.



- The proposed development will be serviced by a network of 150 mm dia. sanitary sewers which will connect to the proposed 200 mm dia. SAN sewer to be extended from the existing stub.

### Stormwater Management

- Stormwater quality control requirements of 80% TSS removal will be met with a treatment train approach by using StormTech Isolator Row Plus & Hydro International OGS (FD-4HC) or approved equivalent.
- The storm water release rates from the proposed development will meet contemplated allowable release rate of 30.95 L/s (24.86 L/s controlled and 6.09 L/s uncontrolled).
- Stormwater quantity control objectives will be met using an Inlet Control Device (ICD) to restrict flow and on-site stormwater surface storage and underground storage.

## 10 REPORT CONDITIONS AND LIMITATIONS

The report conclusions are applicable only to this specific project described in the preceding pages. Any changes, modifications or additions will require a subsequent review by LRL Associates Ltd. to ensure the compatibility with the recommendations contained in this document.

If you have any questions or comments, please contact the undersigned.

Prepared by:

**LRL Associates Ltd.**

*Maxime Longtin*

Maxime Longtin  
Civil Engineering Technologist



Mohan Basnet, P.Eng.  
Civil Engineer



## **APPENDIX A**

**Pre-consultation / Correspondance**

**3555 Borrisokane Road**  
Meeting Summary Notes  
Sept 23, 2021. Online Teams Meeting

**Attendees:**

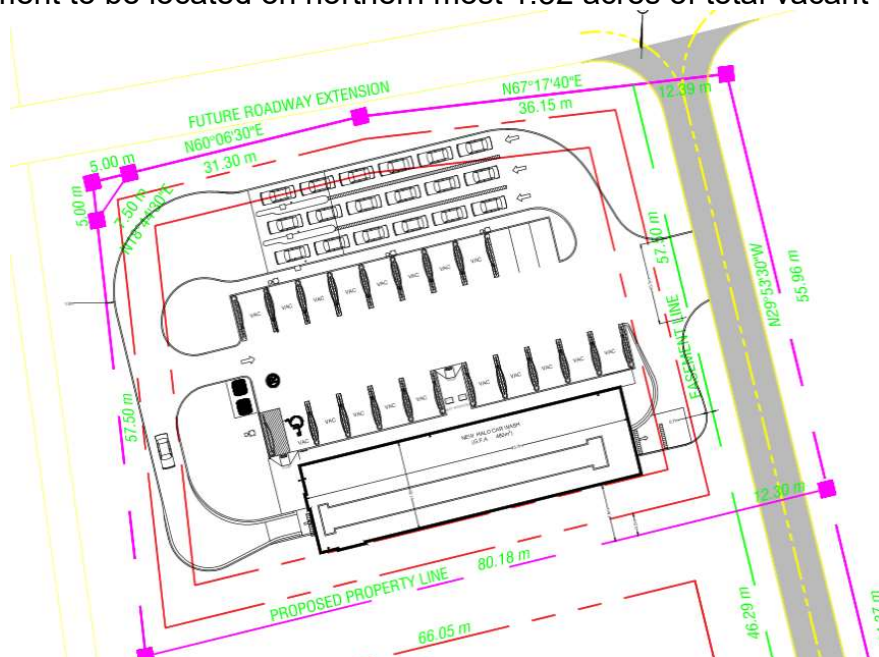
- Jonah Bonn (Applicant, First Bay Properties Inc.)
- Bill Holzman (Applicant, Holzman Consultants)
- Philippe Paquette (LRL Associates)
- Peter MacEwen (MacEwen)
- Brad Moore (MacEwen)
- Greg Pedersen (Halowash)
- Jordan Lupovici (Halowash)
- Katie Morphet (File Lead, Panner, City of Ottawa)
- Jeff Shillington (Project Manager, City of Ottawa)
- Neeti Paudel (Transportation Project Manager, City of Ottawa)
- Sami Rehman (Environmental, City of Ottawa)
- Jeannette Krabicka (Parks, City of Ottawa)

**Not in Attendance:**

- Mark Richardson (Forestry, City of Ottawa)
- RVCA

**Issue of Discussion:**

- Site Plan Control for a new 1-storey 480 sq. m drive-through carwash with 3 queuing lanes for 18 cars and 21 parking spaces (18 of which are vacuum accessible).
- Development to be located on northern most 1.32 acres of total vacant property.





### 1. Official Plan - designated "General Urban Area".

Car wash a permitted use

Barrhaven South CDP – property identified as institutional

### 2. Zoning Information

Zoned IL [304]

Urban Exception 304 permits place of worship as an additional use.

IL Zone permits Drive-Through Facility and Car wash uses

Zoning interpretation has confirmed that Section 203 (2)(c) limits the Car wash use to 300 sq. m.

Floodplain overlay on a portion of the site – RVCA has confirmed that this floodplain area has been removed from their mapping. It will still need to be removed from the City's mapping.

Within the 400 m MTO Permit Control Area

### 3. Infrastructure/Servicing – Jeff Shillington

- Servicing for the subdivision is currently being designed by DSEL for Mattamy. To coordinate service locations please contact Jen Ailey at DSEL (email: [jailey@dssel.ca](mailto:jailey@dssel.ca), cell no. 613-222-6476)
- The current design has not yet been approved, however a 2<sup>nd</sup> submission of the detailed design is currently under review. There were no significant concerns with any of the servicing proposed for this area.
- The current design shows the following:
  - 300 mm dia. sanitary sewer along Flagstaff with a 200 mm service and control MH proposed just inside the property in the northeast corner.
  - 300 mm watermain along Flagstaff with a 200 mm service and valve on the property line in the northeast corner of the property.
  - No storm sewer is proposed along Flagstaff. Stormwater could be outlet into the ditch on Borrisokane Road. A C=0.80 for the 5 year event should be used for the design. As per RVCA requirements the stormwater must maintain enhanced water quality protection either through on-site or down stream infrastructure prior to outletting to the Jock River.

- A MECP ECA is likely required for the stormwater outlet to the Borrisokane ditch.
- As discussed at the meeting a shared servicing corridor along the private road would be possible to service the neighboring site to the south. A joint use maintenance agreement and MECP ECA for the shared sanitary sewer would be required.

#### **4. Initial Planning Comments – Katie Morphet**

- Please add table to submitted site plan to identify all required zone and applicable general provisions and that they are being met.
- I have been able to confirm that Section 203 (2)(c) does limit the proposed car wash use to 300 sq.m. If you wish to move forward with a footprint of this size a minor variance would need to be approved prior to the Site Plan being finalized and approved. I understand that the minor variance process is severely backed up due to covid so I would inquire with the Committee timing for the next available meeting.
- The floodplain overlay will need to be removed from the property prior to approval of a Site Plan.

The flood plain can be dealt with multiple ways.

1. You can undertake a site-specific ZBA;
  2. If the timing works for both the applicant and the zoning group the City can add it to the omnibus report. The next omnibus report is expected in Q1 of 2022. This means it could go forward at the end of April 2022; or
  3. It will be removed when the City undertakes flood plain mapping updates. The floodplain mapping for this area is expected to be updated by the end of the year but it is not guaranteed.
- A Survey Plan will be required to clarify property boundaries and lot ownership.
  - The Site Plan design drawings and agreement and will apply to entire lot if it is yet to be severed at the time of application.
  - The site is within 400m of the High 416 – MTO Permit control Area – please confirm with MTO whether you require a permit from them.

## 5. Parks – Jeanette Krabicka

Please see the attached comments.

## 6. Trees - Mark Richardson

- 1) if there are trees >10cm in diameter on site a tree removal permit will required and a TCR will need to be submitted with their application
- 2) they will need to contact [mark.richardson@ottawa.ca](mailto:mark.richardson@ottawa.ca) for information on the permitting and TCR process.

## 7. Environment – Sami Rehman

The subject property is located adjacent to an Urban Natural Feature (UNF) called Cambrian Woods North and the proposal requires an Environmental Impact Statement (EIS) as outlined in OP section 3.2.3 and 4.7.8. As such, the EIS will need to address:

- potential impacts from the development on the UNF
- potential impacts from the development on the adjacent watercourse
- significant habitat for threatened or endangered species
- review and draw recommendations from the Jock River Reach 1 Subwatershed Plan
- review and draw recommendations from the Protocol for Wildlife Protection during Construction

Further details on the EIS requirements can be found in OP Section 4.7.8 or the EIS guidelines:

[https://documents.ottawa.ca/sites/documents/files/documents/eis\\_guidelines2015\\_en.pdf](https://documents.ottawa.ca/sites/documents/files/documents/eis_guidelines2015_en.pdf)

City staff will be looking to ensure that the proposal's design includes buffering along the adjacent watercourse.

Staff are also recommending landscaping and design elements that will reduce energy and water consumption, as outlined in OP Section 4.9.

Given the subject property's proximity to the UNF, the adjacent watercourse and the Jock River, staff will be anticipating using only locally appropriate native species in their landscape plan.

I recommend contacting the Trail Road Waste Facility to identify their comments or advice for this proposed development because the subject property is within 500m of the facility.

I would also recommend consulting with the Rideau Valley Conservation Authority to determine if any permits or approvals are required under their regulations.

While not explicitly discussed in this meeting, a severance will trigger the requirement for an EIS and the advice provided above would be applicable to that EIS and severance application.

## 8. Conservation Authority – Eric Lalande (RVCA)

For the floodplain, mapping below shows that the floodplain does not extend onto the property. This was confirmed and updated on our end earlier this year, and mapping at the City should be updated through an omnibus zoning amendment.

As for SWM and TSS removal, you are required to maintain enhanced water quality protection either through on-site or down stream infrastructure prior to any outlet to a natural watercourse. Note that setbacks and stormwater should take into consideration the realigned channel adjacent to your site (along the easterly property boundary).

Given the use, I would also suggest you contact the City's HydroG related to any groundwater constraints given the use.

## 9. Transportation – Neeti Paudel

Follow Traffic Impact Assessment Guidelines

- Complete the screening form as soon as possible and submit it to the Neeti Paudel at [neeti.paudel@ottawa.ca](mailto:neeti.paudel@ottawa.ca) for review. Please include the **site generated trips** for the trip generation trigger. Once reviewed, and if, the triggers are met, proceed to Step 2.
- **Applicant advised that their application will not be deemed complete until the submission of the draft step 1-4, including the functional draft RMA package (if applicable) and/or monitoring report (if applicable). Collaboration and communication between development proponents and City staff are required at the end of every step in the TIA process**
- Request base mapping asap if RMA is required. Contact Engineering Services (<https://ottawa.ca/en/city-hall/planning-and-development/engineering-services>)
- Noise Impact Studies required for the following:
  - Stationary (if, within 100m of noise sensitive land use).
- Ensure clear throat length requirements as per TAC are met at the accesses.

- On site plan:
  - Show all details of the roads abutting the site up to and including the opposite curb; include such items as pavement markings, accesses and/or sidewalks.
  - Turning templates will be required for all accesses showing the largest vehicle to access the site; required for internal movements and at all access (entering and exiting and going in both directions).
  - Show all curb radii measurements; ensure that all curb radii are reduced as much as possible
  
- As the proposed site is for general public use, AODA legislation applies. Consider using the City's Accessibility Design Standards.
  
- Number of accessible parking spaces should meet the requirements from Table 3 of the City's accessible Design Standards.
  
- Site triangles at the following locations on the final plan will be required:
  - Local Road to Local Road: 3 metre x 3 metres
  - Local Road to Collector Road: 5 metre x 5 metres
  - Collector Road to Collector Road: 5 metre x 5 metres
  - Collector Road to Arterial Road: 5 metre x 5 metres

## **10. General Information**

- a. Ensure that all plans and studies are prepared as per City guidelines – as available online...  
<https://ottawa.ca/en/city-hall/planning-and-development/information-developers/development-application-review-process/development-application-submission/guide-preparing-studies-and-plans>

## Mohan Basnet

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**From:** Eric Lalande <eric.lalande@rvca.ca>  
**Sent:** September 24, 2021 10:42 AM  
**To:** Philippe Paquette; Jamie Batchelor  
**Cc:** katie.morphet@ottawa.ca; Brad Moore; Jordan Lupovici; Jonah Bonn  
**Subject:** RE: Future Halo carwash Borrisokane Rd. Barrhaven ON. (LRL#210691)

Hi Philippe,

As for the floodplain, mapping below shows that the floodplain does not extend onto the property. This was confirmed and updated on our end earlier this year, and mapping at the City should be updated through an omnibus zoning amendment.

As for SWM and TSS removal, you are required to maintain enhanced water quality protection either through on-site or down stream infrastructure prior to any outlet to a natural watercourse. Note that setbacks and stormwater should take into consideration the realigned channel adjacent to your site (along the easterly property boundary).

Given the use, I would also suggest you contact the City's HydroG related to any groundwater constraints given the use.

Cheers,



**Eric Lalande, MCIP, RPP**  
Planner, RVCA  
613-692-3571 x1137

---

**From:** Philippe Paquette <ppaquette@lrl.ca>  
**Sent:** Thursday, September 23, 2021 4:25 PM

**To:** Jamie Batchelor <jamie.batchelor@rvca.ca>; Eric Lalande <eric.lalande@rvca.ca>

**Cc:** katie.morphet@ottawa.ca; Brad Moore <b.moore@macewen.ca>; Jordan Lupovici <jlupovici@halowash.com>;  
Jonah Bonn <jbonn@firstbay.ca>

**Subject:** Future Halo carwash Borrisokane Rd. Barrhaven ON. (LRL#210691)

Hi Jamie and Eric,

After pre-consulting with the City of Ottawa this morning regrading the above mentioned project, the City of Ottawa planner assigned to the file (Katie Morphet) gave me your contacts in order to discuss about the flood plain crossing this property, SWM and TSS removal criterion. To put you in context, our client wishes to purchase a piece of land located at the north end of the employment block of the Mattamy Homes Half Moon bay West Subdivision. Refer to the attached document for more info. Also attached is a preliminary plan of what they want to develop.

Let us know of your availability so we can book a meeting very soon.

Thanks for your time.

**Philippe Paquette, C.E.T.**

Certified Engineering Technologist



**LRL Engineering**

5430 Canotek Road  
Ottawa, Ontario K1J 9G2

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**C** (613) 880-9793

**F** (613) 842-4338

**E** [ppaquette@lrl.ca](mailto:ppaquette@lrl.ca)

**W** [www.lrl.ca](http://www.lrl.ca)

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*In addition, we will continue to have access to all e-mail correspondence and do our best to return all inquiries in a timely manner.*



**APPENDIX B**  
**Water Supply Calculations**





## Water Service Calculations

LRL File No. : 210691

Project : Proposed Development - Halo Car Wash

Location : 3555 Borrisokane Rc

Date : February 7, 2023

Designed by : M. Basnet

### Water Demand

Site area =  ha (Part 1)

Average day demand = 35000 L / ha · day (based on Table 4.2 of Ottawa Design Guidelines-Water Distribution)  
 = 18690 L / day  
 = 0.22 L / s

Maximum daily peak factor = 1.5  
**Maximum daily demand = 0.32 L / s**

Maximum hour peak factor = 1.8  
**Maximum hour demand = 0.58 L / s**

### Adjustment - Car Wash (as per Halo Car Wash Inc.)

Estimated vol. of water/car wash =  L

Average day demand = 93151 L / day (assuming 200000 car wash/year)  
**1.08 L / s**

Maximum daily demand = **1.97 L / s** (assuming 1000 car wash/day)

Maximum hour demand = **6.14 L / s** (assuming 130 car wash/hour)

### Total Anticipated Water Demand (L/s)

	<u>Part 1</u>	<u>Part 3*</u>	<u>Part 5*</u>	<u>Total (L/s)</u>
Average day demand =	1.29	0.15	0.41	1.85
Maximum daily demand =	2.29	0.23	0.62	3.14
Maximum hour demand =	6.72	0.28	0.74	7.74

Note:\*Water demands for south parcels (Part 3 and 5) were taken from Functional Servicing Brief, prepared by Pearson Engineering, dated Nov 17, 2022

### Water Service Pipe Sizing (Part 1)

Q = VA Where: V = velocity  
 A = area of water service pipe  
 Q = water supply flow rate

By deriving the above formula with an assumed max. V=1.5 m/s

Minimum pipe diameter:  $d = (4Q/\pi V)^{1/2}$   
 $d = 0.076$  m  
 $d = 76$  mm (minimum required size)

Proposed pipe diameter:  mm



**Fire Flow Calculations**

**LRL File No.** 210691

**Project:** Proposed Development-Halo Car Wash

**Location:** 3535 Borrisokane Rd, Barrhaven, ON

**Date:** April 14, 2022

**Method:** Fire Underwriters Survey (FUS)

**Prepared by:** M. Basnet

Step	Task	Term	Options	Multiplier	Choose:	Value	Unit	Fire Flow	
<b>Structural Framing Material</b>									
1	Choose frame used for building	Coefficient C related to the type of construction	Wood Frame	1.5	Non-combustible Construction	0.8			
			Ordinary Construction	1.0					
			Non-combustible construction	0.8					
			Fire resistive construction <2 hrs	0.7					
			Fire resistive construction >2 hrs	0.6					
<b>Floor Space Area (A)</b>									
2			Total area			485	m <sup>2</sup>		
3	Obtain fire flow before reductions	Required fire flow	$Fire\ Flow = 220 \times C \times A^{0.5}$				L/min	3,876	
<b>Reductions or surcharge due to factors affecting burning</b>									
4	Choose combustibility of contents	Occupancy hazard reduction or surcharge	Non-combustible	-25%	Combustible	0%	L/min	3,876	
			Limited combustible	-15%					
			Combustible	0%					
			Free burning	15%					
			Rapid burning	25%					
5	Choose reduction for sprinklers	Sprinkler reduction	Full automatic sprinklers	-30%	False	0%	L/min	3,876	
			Water supply is standard for both the system and fire department hose lines		-10%	False			0%
			Fully supervised system	-10%	False	0%			
6	Choose separation	Exposure distance between units	North side	>45m	0%	0%	L/min	3,876	
			East side	>45m	0%				
			South side	>45m	0%				
			West side	>45m	0%				
<b>Net required fire flow</b>									
7	Obtain fire flow, duration, and volume					Minimum required fire flow rate (rounded to nearest 100)	L/min	3,900	
						Minimum required fire flow rate	L/s	65.0	
						Required duration of fire flow	hr	1.5	

## Mohan Basnet

---

**From:** Bramah, Bruce <bruce.bramah@ottawa.ca>  
**Sent:** February 14, 2023 3:45 PM  
**To:** Mohan Basnet  
**Cc:** Kelly, Siobhan; Jordan Lupovici; Maxime Longtin  
**Subject:** RE: Halo Car Wash\_3535 Borrisokane Rd\_ Revised Boundary Condition (LRL210691)

Hi Mohan,

Yes, the HGL would be the same for both connections.

Thanks,

--

**Bruce Bramah, EIT**

Project Manager

Planning, Real Estate and Economic Development Department / Direction générale de la planification, des biens immobiliers et du développement économique

Development Review - South Branch

City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1

613.580.2424 ext./poste 29686, [Bruce.Bramah@ottawa.ca](mailto:Bruce.Bramah@ottawa.ca)

---

**From:** Mohan Basnet <mbasnet@lrl.ca>  
**Sent:** February 14, 2023 2:30 PM  
**To:** Bramah, Bruce <bruce.bramah@ottawa.ca>  
**Cc:** Kelly, Siobhan <siobhan.kelly@ottawa.ca>; Jordan Lupovici <jlupovici@halowash.com>; Maxime Longtin <mlongtin@lrl.ca>  
**Subject:** RE: Halo Car Wash\_3535 Borrisokane Rd\_ Revised Boundary Condition (LRL210691)

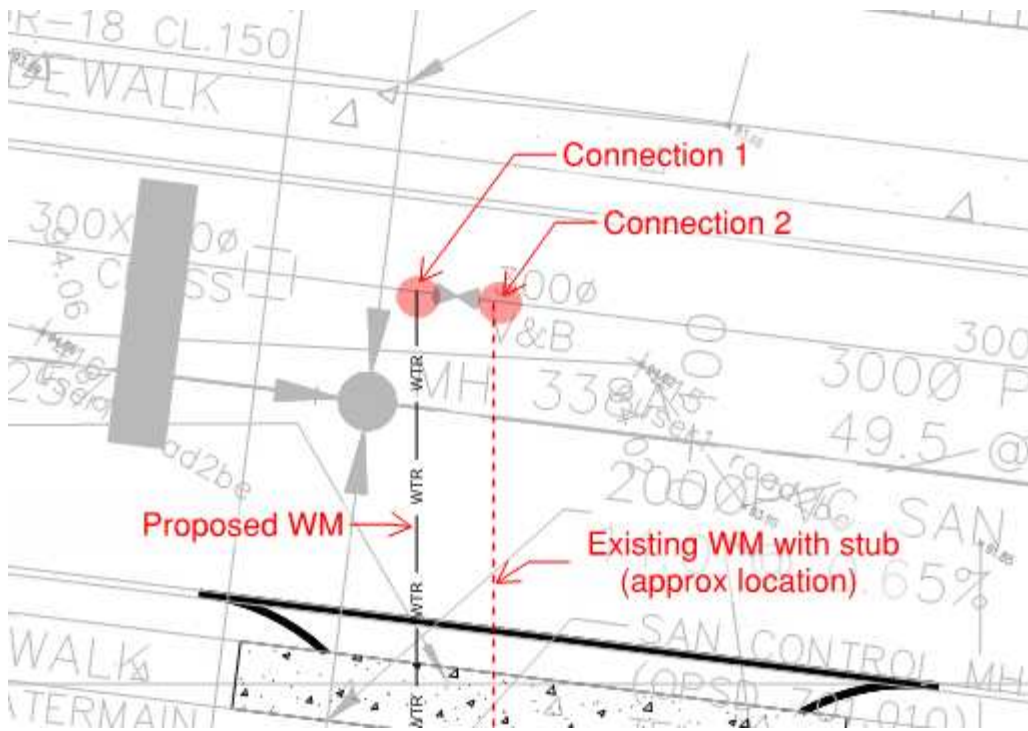
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Thank you Bruce!

The BC received shows only 1 connection. However, actually there are 2 connections.

Is the BC received is applicable for both connections?



Thank you,

**Mohan Basnet, P.Eng.**

Civil Engineer

**LRL Engineering**

5430 Canotek Road  
Ottawa, Ontario K1J 9G2

T (613) 842-3434

C (613) 229-6819

F (613) 842-4338

E [mbasnet@lrl.ca](mailto:mbasnet@lrl.ca)

W [www.lrl.ca](http://www.lrl.ca)

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*In addition, we will continue to have access to all e-mail correspondence and do our best to return all inquiries in a timely manner.*



**From:** Bramah, Bruce <[bruce.bramah@ottawa.ca](mailto:bruce.bramah@ottawa.ca)>

**Sent:** February 13, 2023 2:44 PM

**To:** Mohan Basnet <[mbasnet@lrl.ca](mailto:mbasnet@lrl.ca)>

**Cc:** Kelly, Siobhan <[siobhan.kelly@ottawa.ca](mailto:siobhan.kelly@ottawa.ca)>; Jordan Lupovici <[jlupovici@halowash.com](mailto:jlupovici@halowash.com)>;

Maxime Longtin <[mlongtin@lrl.ca](mailto:mlongtin@lrl.ca)>

**Subject:** RE: Halo Car Wash\_3535 Borrisokane Rd\_ Revised Boundary Condition (LRL210691)

Good afternoon,

Please see the attached Boundary Conditions.

Thank you,

--

**Bruce Bramah, EIT**

Project Manager

Planning, Real Estate and Economic Development Department / Direction générale de la planification, des biens immobiliers et du développement économique

Development Review - South Branch

City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1

613.580.2424 ext./poste 29686, [Bruce.Bramah@ottawa.ca](mailto:Bruce.Bramah@ottawa.ca)

---

**From:** Mohan Basnet <[mbasnet@lrl.ca](mailto:mbasnet@lrl.ca)>

**Sent:** February 08, 2023 10:36 AM

**To:** Bramah, Bruce <[bruce.bramah@ottawa.ca](mailto:bruce.bramah@ottawa.ca)>

**Cc:** Kelly, Siobhan <[siobhan.kelly@ottawa.ca](mailto:siobhan.kelly@ottawa.ca)>; Jordan Lupovici <[jlupovici@halowash.com](mailto:jlupovici@halowash.com)>; Maxime Longtin <[mlongtin@lrl.ca](mailto:mlongtin@lrl.ca)>

**Subject:** RE: Halo Car Wash\_3535 Borrisokane Rd\_ Revised Boundary Condition (LRL210691)

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Hi Bruce:

We are working to address SPA-2<sup>nd</sup> review comments for the proposed Halo Car Wash Development at 3535 Borrisokane Rd and require a boundary conditions at this site to proceed. Please use the following data to provide the revised boundary conditions.

- Service location/type: Dual connections at flagstaff drive (existing 200mm dia. stub + proposed 200mm dia. WM), please see attached draft servicing plan C401.
- Type of development: Proposed Car Wash building
- Average daily demand: 1.85 L/s (Part 1+Part 3+Part 5)
- Maximum daily demand: 3.14 L/s (Part 1+Part 3+Part 5)
- Peak hourly demand: 7.74 L/s (Part 1+Part 3+Part 5)
- FUS fire flow demand: 65.00 L/s (Part 1-Halo Car Wash)

Please note that water demands for the south parcels (Part 3 and Part 5) were taken from the Servicing Brief prepared by Pearson Engineering (Nov 17, 2022).

For your reference, I have also included copies of revised water demand calculations and FUS fire flow calculations along with this email.

Please let me know if you have any questions.

Thank you

**Mohan Basnet, P.Eng.**

Civil Engineer

**LRL Engineering**

5430 Canotek Road  
Ottawa, Ontario K1J 9G2

**T** (613) 842-3434

**C** (613) 229-6819

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**W** [www.lrl.ca](http://www.lrl.ca)

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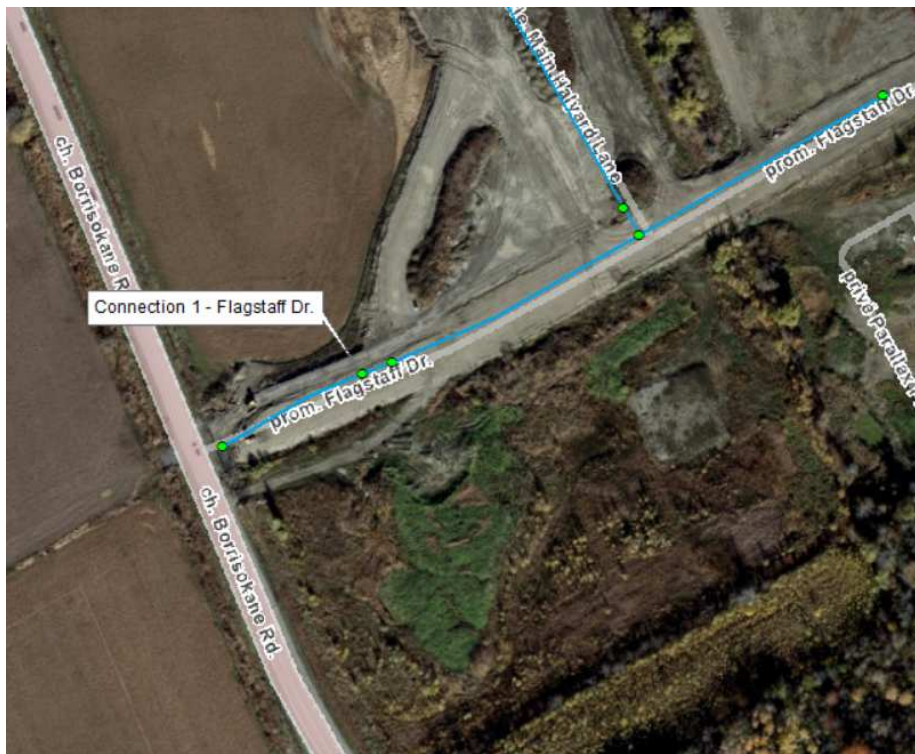
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## Boundary Conditions 3535 Borrisokane Rd (Halo Car Wash)

### Provided Information

Scenario	Demand	
	L/min	L/s
Average Daily Demand	111	1.85
Maximum Daily Demand	188	3.14
Peak Hour	464	7.74
Fire Flow Demand #1	3,900	65.00

### Location



### Results

#### Existing Conditions (Pressure Zone 3SW)

##### Connection 1 – Flagstaff Dr.

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	156.4	89.4
Peak Hour	142.4	69.5
Max Day plus Fire Flow	137.4	62.4

<sup>1</sup> Ground Elevation = 93.5 m

## Future Conditions (Pressure Zone SUC)

### Connection 1 – Flagstaff Dr.

Demand Scenario	Head (m)	Pressure <sup>1</sup> (psi)
Maximum HGL	146.7	75.6
Peak Hour	142.7	69.9
Max Day plus Fire Flow	142.3	69.3

<sup>1</sup> Ground Elevation = 93.5 m

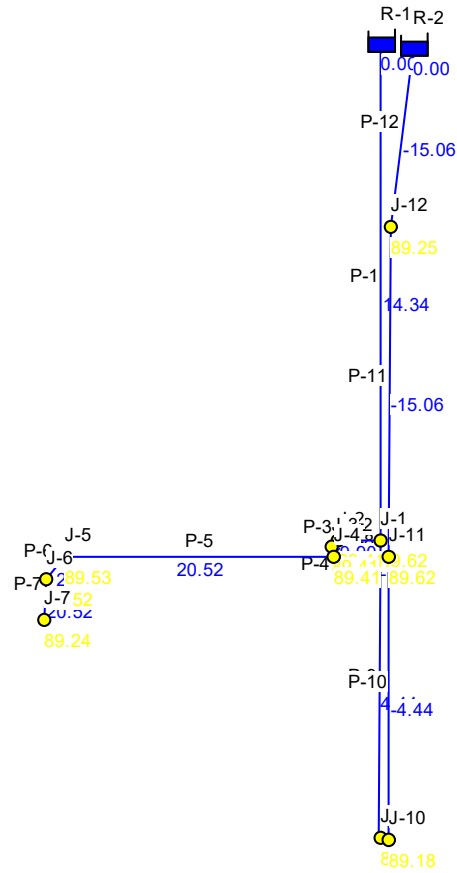
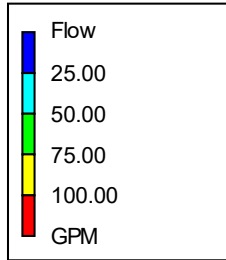
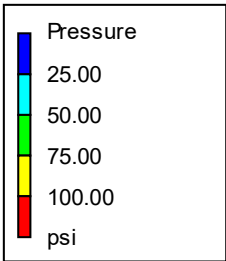
### Notes

1. As per the Ontario Building Code in areas that may be occupied, the static pressure at any fixture shall not exceed 552 kPa (80 psi.) Pressure control measures to be considered are as follows, in order of preference:
  - a. If possible, systems to be designed to residual pressures of 345 to 552 kPa (50 to 80 psi) in all occupied areas outside of the public right-of-way without special pressure control equipment.
  - b. Pressure reducing valves to be installed immediately downstream of the isolation valve in the home/ building, located downstream of the meter so it is owner maintained.

### **Disclaimer**

*The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation. Fire Flow analysis is a reflection of available flow in the watermain; there may be additional restrictions that occur between the watermain and the hydrant that the model cannot take into account.*





# Scenario 1: Average Day

```

*****
*                               E P A N E T                               *
*                               Hydraulic and Water Quality                 *
*                               Analysis for Pipe Networks                   *
*                               Version 2.2                                 *
*****
    
```

Input File: 210691\_Avg Day.net

Link - Node Table:

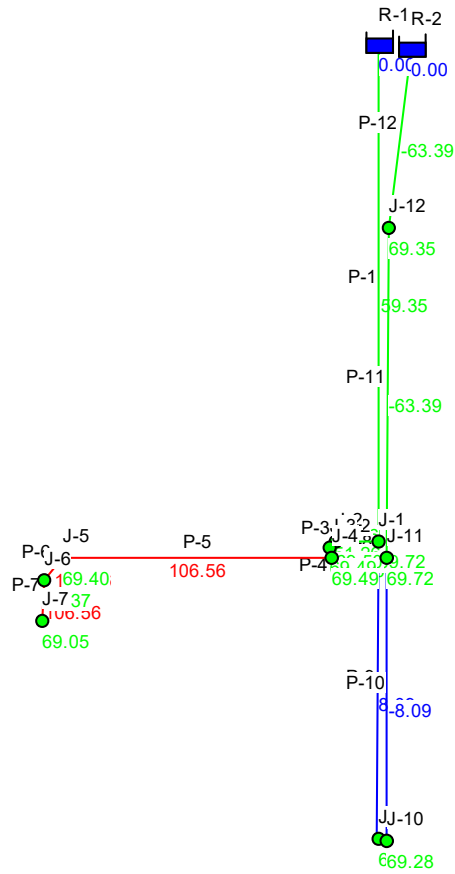
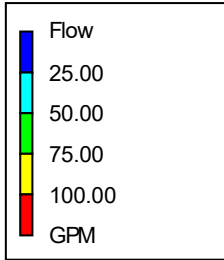
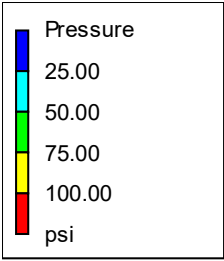
Link ID	Start Node	End Node	Length ft	Diameter in
P-1	R-1	J-1	150.88	8
P-3	J-2	J-3	2.95	4
P-4	J-3	J-4	2.95	4
P-5	J-4	J-5	80.03	4
P-6	J-5	J-6	9.84	4
P-7	J-6	J-7	13.12	4
P-8	J-4	J-11	15	4
P-9	J-1	J-9	88.56	8
P-10	J-10	J-11	85.28	8
P-11	J-11	J-12	101.68	8
P-12	J-12	R-2	54.45	8
P-2	J-1	J-2	12.5	4

Node Results:

Node ID	Demand GPM	Head ft	Pressure psi	Quality
J-1	0.00	512.99	89.62	0.00
J-2	0.00	512.99	89.41	0.00
J-3	0.00	512.99	89.41	0.00
J-4	0.00	512.99	89.41	0.00
J-5	0.00	512.96	89.53	0.00
J-6	0.00	512.96	89.52	0.00
J-7	20.52	512.96	89.24	0.00
J-9	4.44	512.99	89.18	0.00
J-10	4.44	512.99	89.18	0.00
J-11	0.00	512.99	89.62	0.00
J-12	0.00	512.99	89.25	0.00
R-1	-14.34	512.99	0.00	0.00 Reservoir
R-2	-15.06	512.99	0.00	0.00 Reservoir

Link Results:

Link ID	Flow GPM	Velocity fps	Unit Headloss ft/Kft	Status
P-1	14.34	0.09	0.01	Open
P-3	9.90	0.25	0.06	Open
P-4	9.90	0.25	0.08	Open
P-5	20.52	0.52	0.31	Open
P-6	20.52	0.52	0.30	Open
P-7	20.52	0.52	0.31	Open
P-8	-10.62	0.27	0.09	Open
P-9	4.44	0.03	0.00	Open
P-10	-4.44	0.03	0.00	Open
P-11	-15.06	0.10	0.01	Open
P-12	-15.06	0.10	0.01	Open
P-2	9.90	0.25	0.08	Open



## Scenario 2: Peak Hour

```

*****
*                               E P A N E T                               *
*                               Hydraulic and Water Quality                 *
*                               Analysis for Pipe Networks                   *
*                               Version 2.2                                 *
*****
    
```

Input File: 210691\_Peak Hour.net

Link - Node Table:

Link ID	Start Node	End Node	Length ft	Diameter in
P-1	R-1	J-1	150.88	8
P-3	J-2	J-3	2.95	4
P-4	J-3	J-4	2.95	4
P-5	J-4	J-5	80.03	4
P-6	J-5	J-6	9.84	4
P-7	J-6	J-7	13.12	4
P-8	J-4	J-11	15	4
P-9	J-1	J-9	88.56	8
P-10	J-10	J-11	85.28	8
P-11	J-11	J-12	101.68	8
P-12	J-12	R-2	54.45	8
P-2	J-1	J-2	12.5	4

Node Results:

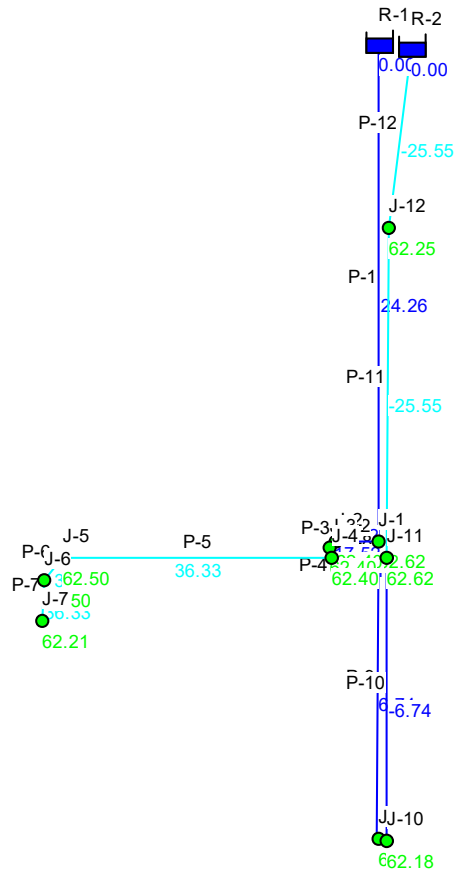
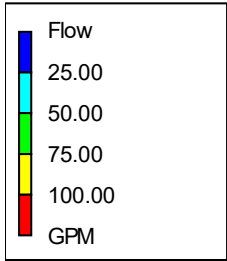
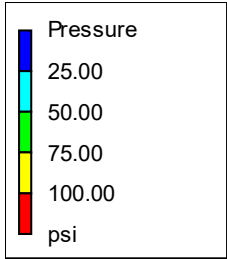
Node ID	Demand GPM	Head ft	Pressure psi	Quality
J-1	0.00	467.06	69.72	0.00
J-2	0.00	467.04	69.50	0.00
J-3	0.00	467.03	69.49	0.00
J-4	0.00	467.03	69.49	0.00
J-5	0.00	466.51	69.40	0.00
J-6	0.00	466.45	69.37	0.00
J-7	106.56	466.36	69.05	0.00
J-9	8.09	467.06	69.28	0.00
J-10	8.09	467.06	69.28	0.00
J-11	0.00	467.06	69.72	0.00
J-12	0.00	467.07	69.35	0.00
R-1	-59.35	467.07	0.00	0.00 Reservoir
R-2	-63.39	467.07	0.00	0.00 Reservoir

## Link Results:

---

Link ID	Flow GPM	Velocity fps	Unit Headloss ft/Kft	Status
P-1	59.35	0.38	0.08	Open
P-3	51.26	1.31	1.68	Open
P-4	51.26	1.31	1.68	Open
P-5	106.56	2.72	6.49	Open
P-6	106.56	2.72	6.49	Open
P-7	106.56	2.72	6.48	Open
P-8	-55.30	1.41	1.92	Open
P-9	8.09	0.05	0.00	Open
P-10	-8.09	0.05	0.00	Open
P-11	-63.39	0.40	0.08	Open
P-12	-63.39	0.40	0.08	Open
P-2	51.26	1.31	1.67	Open

---



### Scenario 3: Max Day + Fire Flow

```

*****
*                               E P A N E T                               *
*                               Hydraulic and Water Quality                *
*                               Analysis for Pipe Networks                  *
*                               Version 2.2                                *
*****
    
```

Input File: 210691\_Max Day+FF.net

Link - Node Table:

Link ID	Start Node	End Node	Length ft	Diameter in
P-1	R-1	J-1	150.88	8
P-3	J-2	J-3	2.95	4
P-4	J-3	J-4	2.95	4
P-5	J-4	J-5	80.03	4
P-6	J-5	J-6	9.84	4
P-7	J-6	J-7	13.12	4
P-8	J-4	J-11	15	4
P-9	J-1	J-9	88.56	8
P-10	J-10	J-11	85.28	8
P-11	J-11	J-12	101.68	8
P-12	J-12	R-2	54.45	8
P-2	J-1	J-2	12.5	4

Node Results:

Node ID	Demand GPM	Head ft	Pressure psi	Quality
J-1	0.00	450.67	62.62	0.00
J-2	0.00	450.66	62.40	0.00
J-3	0.00	450.66	62.40	0.00
J-4	0.00	450.66	62.40	0.00
J-5	0.00	450.59	62.50	0.00
J-6	0.00	450.58	62.50	0.00
J-7	36.33	450.57	62.21	0.00
J-9	6.74	450.67	62.18	0.00
J-10	6.74	450.67	62.18	0.00
J-11	0.00	450.67	62.62	0.00
J-12	0.00	450.67	62.25	0.00
R-1	-24.26	450.67	0.00	0.00 Reservoir
R-2	-25.55	450.67	0.00	0.00 Reservoir

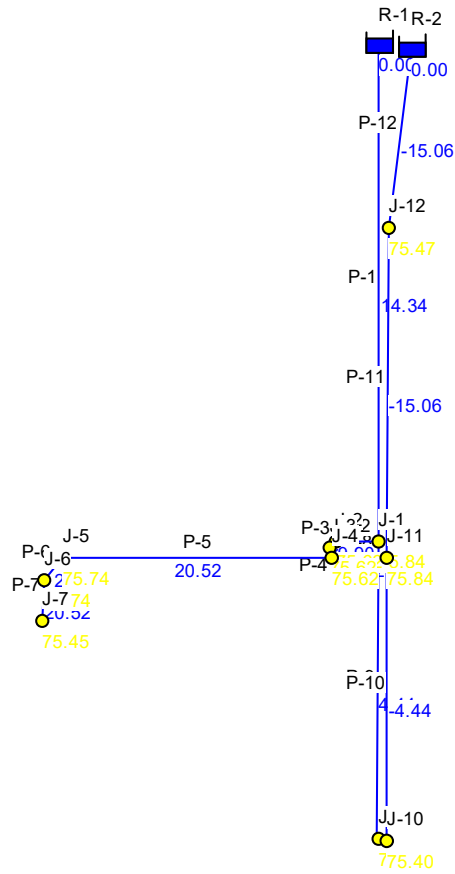
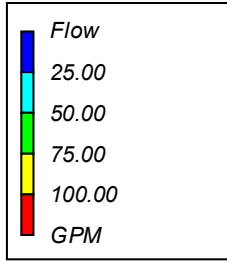
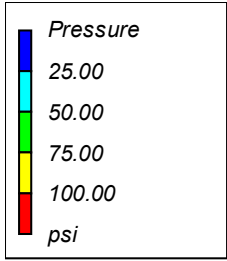


## Link Results:

---

Link ID	Flow GPM	Velocity fps	Unit Headloss ft/Kft	Status
P-1	24.26	0.15	0.01	Open
P-3	17.52	0.45	0.23	Open
P-4	17.52	0.45	0.23	Open
P-5	36.33	0.93	0.88	Open
P-6	36.33	0.93	0.88	Open
P-7	36.33	0.93	0.88	Open
P-8	-18.81	0.48	0.26	Open
P-9	6.74	0.04	0.00	Open
P-10	-6.74	0.04	0.00	Open
P-11	-25.55	0.16	0.02	Open
P-12	-25.55	0.16	0.02	Open
P-2	17.52	0.45	0.23	Open

---



### Scenario 4: Average Day (Pressure Zone SUC)

```

*****
*                               E P A N E T                               *
*                               Hydraulic and Water Quality                 *
*                               Analysis for Pipe Networks                   *
*                               Version 2.2                                 *
*****
    
```

Input File: 210691\_Avg Day - SUC.net

Link - Node Table:

Link ID	Start Node	End Node	Length ft	Diameter in
P-1	R-1	J-1	150.88	8
P-3	J-2	J-3	2.95	4
P-4	J-3	J-4	2.95	4
P-5	J-4	J-5	80.03	4
P-6	J-5	J-6	9.84	4
P-7	J-6	J-7	13.12	4
P-8	J-4	J-11	15	4
P-9	J-1	J-9	88.56	8
P-10	J-10	J-11	85.28	8
P-11	J-11	J-12	101.68	8
P-12	J-12	R-2	54.45	8
P-2	J-1	J-2	12.5	4

Node Results:

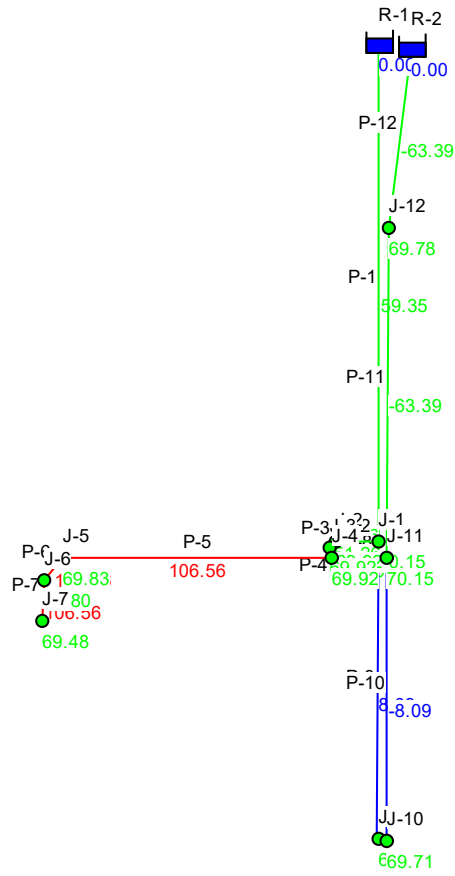
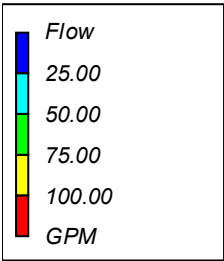
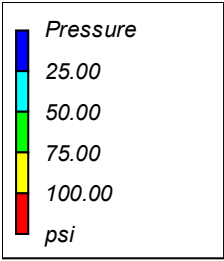
Node ID	Demand GPM	Head ft	Pressure psi	Quality
J-1	0.00	481.18	75.84	0.00
J-2	0.00	481.18	75.62	0.00
J-3	0.00	481.18	75.62	0.00
J-4	0.00	481.18	75.62	0.00
J-5	0.00	481.15	75.74	0.00
J-6	0.00	481.15	75.74	0.00
J-7	20.52	481.15	75.45	0.00
J-9	4.44	481.18	75.40	0.00
J-10	4.44	481.18	75.40	0.00
J-11	0.00	481.18	75.84	0.00
J-12	0.00	481.18	75.47	0.00
R-1	-14.34	481.18	0.00	0.00 Reservoir
R-2	-15.06	481.18	0.00	0.00 Reservoir

## Link Results:

---

Link ID	Flow GPM	Velocity fps	Unit Headloss ft/Kft	Status
P-1	14.34	0.09	0.01	Open
P-3	9.90	0.25	0.08	Open
P-4	9.90	0.25	0.08	Open
P-5	20.52	0.52	0.31	Open
P-6	20.52	0.52	0.31	Open
P-7	20.52	0.52	0.31	Open
P-8	-10.62	0.27	0.09	Open
P-9	4.44	0.03	0.00	Open
P-10	-4.44	0.03	0.00	Open
P-11	-15.06	0.10	0.01	Open
P-12	-15.06	0.10	0.01	Open
P-2	9.90	0.25	0.08	Open

---



## Scenario 5: Peak Hour (Pressure Zone SUC)

```

*****
*                               E P A N E T                               *
*                               Hydraulic and Water Quality                *
*                               Analysis for Pipe Networks                  *
*                               Version 2.2                                *
*****
    
```

Input File: 210691\_Peak Hour - SUC.net

Link - Node Table:

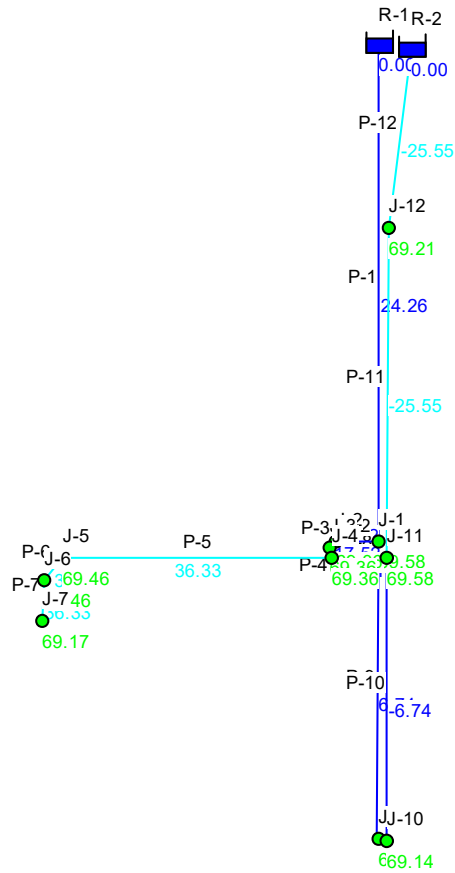
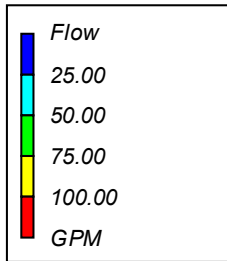
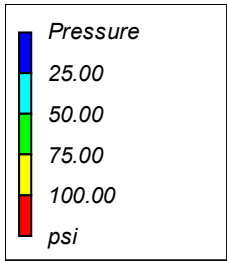
Link ID	Start Node	End Node	Length ft	Diameter in
P-1	R-1	J-1	150.88	8
P-3	J-2	J-3	2.95	4
P-4	J-3	J-4	2.95	4
P-5	J-4	J-5	80.03	4
P-6	J-5	J-6	9.84	4
P-7	J-6	J-7	13.12	4
P-8	J-4	J-11	15	4
P-9	J-1	J-9	88.56	8
P-10	J-10	J-11	85.28	8
P-11	J-11	J-12	101.68	8
P-12	J-12	R-2	54.45	8
P-2	J-1	J-2	12.5	4

Node Results:

Node ID	Demand GPM	Head ft	Pressure psi	Quality
J-1	0.00	468.05	70.15	0.00
J-2	0.00	468.03	69.92	0.00
J-3	0.00	468.02	69.92	0.00
J-4	0.00	468.02	69.92	0.00
J-5	0.00	467.50	69.83	0.00
J-6	0.00	467.44	69.80	0.00
J-7	106.56	467.35	69.48	0.00
J-9	8.09	468.05	69.71	0.00
J-10	8.09	468.05	69.71	0.00
J-11	0.00	468.05	70.15	0.00
J-12	0.00	468.06	69.78	0.00
R-1	-59.35	468.06	0.00	0.00 Reservoir
R-2	-63.39	468.06	0.00	0.00 Reservoir

## Link Results:

Link ID	Flow GPM	Velocity fps	Unit Headloss ft/Kft	Status
P-1	59.35	0.38	0.08	Open
P-3	51.26	1.31	1.67	Open
P-4	51.26	1.31	1.68	Open
P-5	106.56	2.72	6.49	Open
P-6	106.56	2.72	6.48	Open
P-7	106.56	2.72	6.49	Open
P-8	-55.30	1.41	1.92	Open
P-9	8.09	0.05	0.00	Open
P-10	-8.09	0.05	0.00	Open
P-11	-63.39	0.40	0.08	Open
P-12	-63.39	0.40	0.08	Open
P-2	51.26	1.31	1.67	Open



## Scenario 6: Max Day + Fire Flow (Pressure Zone SUC)



```

*****
*                               E P A N E T                               *
*                               Hydraulic and Water Quality                 *
*                               Analysis for Pipe Networks                 *
*                               Version 2.2                               *
*****
    
```

Input File: 210691\_Max Day+FF - SUC.net

Link - Node Table:

Link ID	Start Node	End Node	Length ft	Diameter in
P-1	R-1	J-1	150.88	8
P-3	J-2	J-3	2.95	4
P-4	J-3	J-4	2.95	4
P-5	J-4	J-5	80.03	4
P-6	J-5	J-6	9.84	4
P-7	J-6	J-7	13.12	4
P-8	J-4	J-11	15	4
P-9	J-1	J-9	88.56	8
P-10	J-10	J-11	85.28	8
P-11	J-11	J-12	101.68	8
P-12	J-12	R-2	54.45	8
P-2	J-1	J-2	12.5	4

Node Results:

Node ID	Demand GPM	Head ft	Pressure psi	Quality
J-1	0.00	466.74	69.58	0.00
J-2	0.00	466.73	69.36	0.00
J-3	0.00	466.73	69.36	0.00
J-4	0.00	466.73	69.36	0.00
J-5	0.00	466.66	69.46	0.00
J-6	0.00	466.65	69.46	0.00
J-7	36.33	466.64	69.17	0.00
J-9	6.74	466.74	69.14	0.00
J-10	6.74	466.74	69.14	0.00
J-11	0.00	466.74	69.58	0.00
J-12	0.00	466.74	69.21	0.00
R-1	-24.26	466.74	0.00	0.00 Reservoir
R-2	-25.55	466.74	0.00	0.00 Reservoir

## Link Results:

---

Link ID	Flow GPM	Velocity fps	Unit Headloss ft/Kft	Status
P-1	24.26	0.15	0.01	Open
P-3	17.52	0.45	0.23	Open
P-4	17.52	0.45	0.24	Open
P-5	36.33	0.93	0.88	Open
P-6	36.33	0.93	0.88	Open
P-7	36.33	0.93	0.88	Open
P-8	-18.81	0.48	0.26	Open
P-9	6.74	0.04	0.00	Open
P-10	-6.74	0.04	0.00	Open
P-11	-25.55	0.16	0.02	Open
P-12	-25.55	0.16	0.02	Open
P-2	17.52	0.45	0.23	Open

---

**APPENDIX C**  
**Wastewater Calculations**



**LRL File No.** 210691  
**Project:** Proposed Development-Halo Car Wash  
**Location:** 3535 Borrisokane Rd, Barrhaven, ON  
**Date:** February 17, 2023

**Sanitary Design Parameters**  
 Average Daily Flow = 280 L/p/day  
 Commercial & Institutional Flow = 28000 L/ha/day  
 Light Industrial Flow = 35000 L/ha/day  
 Heavy Industrial Flow = 55000 L/ha/day  
 Maximum Residential Peak Factor = 4.0  
 Commercial & Institutional Peak Factor = 1.5

**Pipe Design Parameters**  
 Industrial Peak Factor = as per Appendix 4-B  
 Extraneous Flow = 0.33 L/s/gross ha  
 (as Per Tech Bulletin ISTB-2018-01)

Minimum Velocity = 0.60 m/s  
 Manning's n = 0.013

LOCATION			RESIDENTIAL AREA AND POPULATION						COMMERCIAL		INDUSTRIAL			INSTITUTIONAL		C+I+I	INFILTRATION			TOTAL FLOW	PIPE				
STREET/SITE	FROM MH	TO MH	AREA (Ha)	POP.	CUMMULATIVE		PEAK FLOW (l/s)	AREA (Ha)	ACCU. AREA (Ha)	AREA (Ha)	ACCU. AREA (Ha)	PEAK FACT.	AREA (Ha)	ACCU. AREA (Ha)	*PEAK FLOW (l/s)	TOTAL AREA (Ha)	ACCU. AREA (Ha)	INFILT. FLOW (l/s)	TOTAL FLOW (l/s)	LENGTH (m)	DIA. (mm)	SLOPE (%)	MATERIAL	CAP. (FULL) (l/s)	VEL. (FULL) (m/s)
					AREA (Ha)	POP.																			
	Bldg.	SAN MH03																	0.003	1.4	150	2.00%	PVC	21.54	1.22
	SAN MH03	SAN MH06																	0.003	14.7	150	2.00%	PVC	21.54	1.22
	**SAN MH01	SAN MH06							0.534					6.139	0.534	0.534	0.176	6.318	19.4	150	1.26%	PVC	17.09	0.97	
	SAN MH06	SAN MH02																6.320	17.4	150	1.26%	PVC	17.09	0.97	
	*Future Dev.	SAN MH02																2.360	34.4	200	0.65%	PVC	26.44	0.84	
	SAN MH02	SAN MH04																8.680	22.6	200	0.65%	PVC	26.44	0.84	
															Designed: M. B./M.L.	PROJECT: Proposed Halo Car Wash									
															Checked: M.B.	LOCATION: 3535 Borrisokane Rd, Barrhaven, ON									
															Dwg. Reference: C401	File Ref.: 210691	Date: 2023-02-17	Sheet No. 1 of 1							


Note:  
 \* Peak Design Flow from Future Development (Part 3 + Part 5) was taken from Servicing Brief Prepared by Pearson Engineering, dated November 17, 2022  
 \*\*Peak flow including anticipated waste water from Halo Car Wash (6.141 L/s), see below

Site Description	Qty	L/Qty	Total	
			L/day	L/s
<b>Halo Car Wash</b>				
Anticipated Employees	2	75	150	0.002
Total x Peak Factor (1.5)				<b>0.003</b>
Estimated Car Wash/Hour (based on info by Halo Car Wash)	130	170		<b>6.139</b>
<b>Total Anticipated Peak Design Flow</b> (dry weather flow)				<b>6.141</b>

**APPENDIX D**  
**Stormwater Management Calculations**

# LRL Associates Ltd.

## Storm Watershed Summary



**LRL**  
ENGINEERING | INGÉNIERIE

**LRL File No.** 210691

**Project:** Proposed Development-Halo Car Wash

**Location:** 3555 Borrisokane Rd (Barrhaven, ON)

**Date:** July 7, 2023

**Designed:** M. Longtin

**Checked:** M. Basnet

**Dwg Reference:** C701, C702

### Pre-Development Catchments

Watershed	C = 0.20	C = 0.80	C = 0.90	Total Area (ha)	Combined C
EWS-01 (uncontrolled)	0.534	0.000	0.000	0.534	0.20
<b>Total</b>	<b>0.534</b>	<b>0.000</b>	<b>0.000</b>	<b>0.534</b>	<b>0.20</b>

### Post-Development Catchments

Watershed	C = 0.20	C = 0.8	C = 0.90	Total Area (ha)	Combined C
WS-01A (controlled)	0.040	0.000	0.006	0.045	0.29
WS-01B (controlled)	0.003	0.000	0.015	0.017	0.79
WS-02 (controlled)	0.000	0.000	0.049	0.049	0.90
WS-03 (controlled)	0.001	0.000	0.028	0.030	0.87
WS-04 (controlled)	0.046	0.000	0.055	0.101	0.58
WS-05 (controlled)	0.000	0.000	0.053	0.053	0.90
WS-06 (controlled)	0.005	0.000	0.118	0.123	0.87
WS-07 (controlled)	0.008	0.000	0.031	0.039	0.76
WS-08 (controlled)	0.027	0.000	0.000	0.027	0.20
WS-09 (uncontrolled)	0.029	0.000	0.000	0.029	0.20
WS-10 (uncontrolled)	0.020	0.000	0.000	0.020	0.20
<b>Total</b>	<b>0.179</b>	<b>0.000</b>	<b>0.355</b>	<b>0.534</b>	<b>0.67</b>



LRL File No. 210691  
 Project: Proposed Development-Halo Car Wash  
 Location: 3555 Borrisokane Rd (Barrhaven, ON)  
 Date: July 7, 2023  
 Designed: M. Longtin  
 Checked: M. Basnet  
 Drawing Ref.: C701, C702

Stormwater Management  
 Design Sheet

**STORM - 100 YEAR**

**Runoff Equation**

Q = 2.78CIA (L/s)  
 C = Runoff coefficient  
 I = Rainfall intensity (mm/hr) = A / (Td + C)<sup>B</sup>  
 A = Area (ha)  
 T<sub>c</sub> = Time of concentration (min)

**Pre-Development Catchments within Development Area**

	Total Area =	0.534	ha	ΣR=	0.20
Un-Controlled	EWS-01	0.534	ha	R=	0.20
	Total Uncontrolled =	0.534	ha	ΣR=	0.20

**Pre-development Stormwater Management (5-Yr)**

$I_5 = 998.071 / (Td + 6.053)^{0.814}$       A = 998.071      B = 0.814      C = 6.053

C = 0.20      max of 0.5 as per City of Ottawa  
 I = 104.2      mm/hr  
 T<sub>c</sub> = 10      min  
 Total Area = 0.534      ha  
 Release Rate = 30.95      L/s

**Pre-development Stormwater Management (100-Yr)**

$I_{100} = 1735.688 / (Td + 6.014)^{0.820}$       A = 1735.688      B = 0.820      C = 6.014

C = 0.20  
 I = 178.6      mm/hr  
 T<sub>c</sub> = 10      min  
 Total Area = 0.534      ha  
 Release Rate = 52.99      L/s

Allowable Release Rate = 30.95 L/s  
 (5-yr pre-development level corresponding to EWS-01, see drawing C701)

**Post-development Stormwater Management**

					ΣR <sub>2&amp;5</sub>	ΣR <sub>100</sub>	
		Total Site Area =	0.534	ha	ΣR=	0.67	0.83
Controlled	WS-01A	0.045	ha	R=	0.29	0.36	
	WS-01B	0.017	ha	R=	0.79	0.99	
	WS-02	0.049	ha	R=	0.90	1.00	
	WS-03	0.030	ha	R=	0.87	1.00	
	WS-04	0.101	ha	R=	0.58	0.73	
	WS-05	0.053	ha	R=	0.90	1.00	
	WS-06	0.123	ha	R=	0.87	1.00	
	WS-07	0.039	ha	R=	0.76	0.95	
	WS-08	0.027	ha	R=	0.20	0.25	
Total Controlled =		0.485	ha	ΣR=	0.71	0.89	
Uncontrolled	WS-09	0.029	ha	R=	0.20	0.25	
	WS-10	0.020	ha	R=	0.20	0.25	
	Total Uncontrolled =		0.049	ha	ΣR=	0.20	0.25

**Post-development Stormwater Management (100-Yr)**

Time (min)	Intensity (mm/hr)	Controlled Runoff (L/s)	Storage Volume (m <sup>3</sup> )	*Controlled Release Rate (L/s)	Uncontrolled Runoff (L/s)	Total Release Rate (L/s)
10	178.56	214.24	121.09	12.43	6.09	18.52
15	142.89	171.45	143.12	12.43	4.88	17.31
20	119.95	143.92	157.79	12.43	4.09	16.52
25	103.85	124.60	168.26	12.43	3.54	15.97
30	91.87	110.23	176.04	12.43	3.13	15.56
35	82.58	99.08	181.97	12.43	2.82	15.25
40	75.15	90.16	186.56	12.43	2.56	14.99
45	69.05	82.85	190.13	12.43	2.36	14.79
50	63.95	76.74	192.92	12.43	2.18	14.61
55	59.62	71.54	195.06	12.43	2.03	14.46
60	55.89	67.07	196.69	12.43	1.91	14.34
65	52.65	63.17	197.88	12.43	1.80	14.23
70	49.79	59.74	198.70	12.43	1.70	14.13
75	47.26	56.70	199.21	12.43	1.61	14.04
80	44.99	53.98	199.45	12.43	1.54	13.97
85	42.95	51.54	199.45	12.43	1.47	13.90
90	41.11	49.33	199.24	12.43	1.40	13.83
95	39.43	47.32	198.85	12.43	1.35	13.78
100	37.90	45.48	198.29	12.43	1.29	13.72
105	36.50	43.79	197.58	12.43	1.25	13.68
110	35.20	42.24	196.73	12.43	1.20	13.63
115	34.01	40.80	195.76	12.43	1.16	13.59
120	32.89	39.47	194.68	12.43	1.12	13.55

\*Average release rate taken as 50% of max. allowable controlled release rate for storage calculation

**On-site stormwater detention**

Storage required = 199.45 m<sup>3</sup>  
 Surface storage provided = 115.86 m<sup>3</sup> (See Dwg C601)  
 Underground storage provided = 90.76 m<sup>3</sup> (StormTech Chambers)  
 Total storage provided = 206.62 m<sup>3</sup>



LRL File No. 210691  
 Project: Proposed Development-Halo Car Wash  
 Location: 3555 Borrisokane Rd (Barrhaven, ON)  
 Date: July 7, 2023  
 Designed: M. Longtin  
 Checked: M. Basnet  
 Drawing Ref.: C701, C702

Stormwater Management  
 Design Sheet

**STORM - 5 YEAR**

**Runoff Equation**

Q = 2.78CIA (L/s)  
 C = Runoff coefficient  
 I = Rainfall intensity (mm/hr) =  $A / (Td + C)^B$   
 A = Area (ha)  
 T<sub>c</sub> = Time of concentration (min)

**Pre-Development Catchments within Development Area**

	Total Area =	0.534	ha	ΣR=	0.20
Un-Controlled	EWS-01	0.534	ha	R=	0.20
	Total Uncontrolled =	0.534	ha	ΣR=	0.20

**Pre-development Stormwater Management (5-Yr)**

$I_5 = 998.071 / (Td + 6.053)^{0.814}$       A = 998.071      B = 0.814      C = 6.053

C = 0.20      max of 0.5 as per City of Ottawa  
 I = 104.2      mm/hr  
 T<sub>c</sub> = 10      min  
 Total Area = 0.534      ha  
 Release Rate = 30.95      L/s

**Pre-development Stormwater Management (100-Yr)**

$I_{100} = 1735.688 / (Td + 6.014)^{0.820}$       A = 1735.688      B = 0.820      C = 6.014

C = 0.20  
 I = 178.6      mm/hr  
 T<sub>c</sub> = 10      min  
 Total Area = 0.534      ha  
 Release Rate = 52.99      L/s

Allowable Release Rate = 30.95 L/s

(5-yr pre-development level corresponding to EWS-01, see drawing C701)

**Post-development Stormwater Management**

				ΣR <sub>2&amp;5</sub>	ΣR <sub>100</sub>		
Controlled	Total Site Area =	0.534	ha	ΣR=	0.67		
	WS-01A	0.045	ha	R=	0.29		
	WS-01B	0.017	ha	R=	0.79		
	WS-02	0.049	ha	R=	0.90		
	WS-03	0.030	ha	R=	0.87		
	WS-04	0.101	ha	R=	0.58		
	WS-05	0.053	ha	R=	0.90		
	WS-06	0.123	ha	R=	0.87		
	WS-07	0.039	ha	R=	0.76		
	WS-08	0.027	ha	R=	0.20		
Total Controlled =				0.485	ha	ΣR=	0.71
Uncontrolled	WS-09	0.029	ha	R=	0.20		
	WS-10	0.020	ha	R=	0.20		
	Total Uncontrolled =				0.049	ha	ΣR=

**Post-development Stormwater Management (5-Yr)**

Time (min)	Intensity (mm/hr)	Controlled Runoff (L/s)	Storage Volume (m <sup>3</sup> )	*Controlled Release Rate (L/s)	Uncontrolled Runoff (L/s)	Total Release Rate (L/s)
10	104.19	100.01	52.55	12.43	2.84	15.27
15	83.56	80.20	61.00	12.43	2.28	14.71
20	70.25	67.43	66.00	12.43	1.92	14.35
25	60.90	58.45	69.03	12.43	1.66	14.09
30	53.93	51.76	70.80	12.43	1.47	13.90
35	48.52	46.57	71.70	12.43	1.32	13.75
40	44.18	42.41	71.96	12.43	1.21	13.64
45	40.63	39.00	71.74	12.43	1.11	13.54
50	37.65	36.14	71.14	12.43	1.03	13.46
55	35.12	33.71	70.24	12.43	0.96	13.39
60	32.94	31.62	69.09	12.43	0.90	13.33
65	31.04	29.80	67.74	12.43	0.85	13.28
70	29.37	28.19	66.21	12.43	0.80	13.23
75	27.89	26.77	64.53	12.43	0.76	13.19
80	26.56	25.50	62.72	12.43	0.73	13.15
85	25.37	24.35	60.80	12.43	0.69	13.12
90	24.29	23.31	58.77	12.43	0.66	13.09
95	23.31	22.37	56.66	12.43	0.64	13.07
100	22.41	21.51	54.47	12.43	0.61	13.04
105	21.58	20.72	52.21	12.43	0.59	13.02
110	20.82	19.99	49.88	12.43	0.57	13.00
115	20.12	19.31	47.49	12.43	0.55	12.98
120	19.47	18.69	45.05	12.43	0.53	12.96

\*Average release rate taken as 50% of max. allowable controlled release rate for storage calculations

**On-site stormwater detention**

Storage required = 71.96 m<sup>3</sup>  
 Underground Storage provided = 90.76 m<sup>3</sup> (StormTech Chambers)





**LRL File No.** 210691  
**Project:** Proposed Development-Halo Car Wash  
**Location:** 3555 Borrisokane Rd (Barrhaven, ON)  
**Date:** July 7, 2023  
**Designed:** M. Longtin  
**Checked:** M. Basnet  
**Drawing Ref.:** C701, C702

**Stormwater Management  
Design Sheet**

**STORM - 2 YEAR**

Runoff Equation

**Q = 2.78CIA (L/s)**  
 C = Runoff coefficient  
 I = Rainfall intensity (mm/hr) =  $A / (Td + C)^B$   
 A = Area (ha)  
 T<sub>c</sub> = Time of concentration (min)

**Pre-Development Catchments within Development Area**

	Total Area =	<b>0.534</b>	ha	ΣR=	<b>0.20</b>
<b>Un-Controlled</b>	EWS-01	0.534	ha	R=	0.20
	Total Uncontrolled =	<b>0.534</b>	ha	ΣR=	<b>0.20</b>

**Pre-development Stormwater Management (2-Yr)**

$I_2 = 732.951 / (Td + 6.199)^{0.810}$ 
A = **732.951**
B = **0.810**
C = **6.199**

C = 0.20 max of 0.5 as per City of Ottawa  
 I = 76.8 mm/hr  
 T<sub>c</sub> = 10 min  
 Total Area = 0.534 ha  
 Release Rate = 22.82 L/s

**Pre-development Stormwater Management (5-Yr)**

$I_5 = 998.071 / (Td + 6.053)^{0.814}$ 
A = **998.071**
B = **0.814**
C = **6.053**

C = 0.20 max of 0.5 as per City of Ottawa  
 I = 104.2 mm/hr  
 T<sub>c</sub> = 10 min  
 Total Area = 0.534 ha  
 Release Rate = 30.95 L/s

**Pre-development Stormwater Management (100-Yr)**

$I_{100} = 1735.688 / (Td + 6.014)^{0.820}$ 
A = **1735.688**
B = **0.820**
C = **6.014**

C = 0.20 max of 0.5 as per City of Ottawa  
 I = 178.6 mm/hr  
 T<sub>c</sub> = 10 min  
 Total Area = 0.534 ha  
 Release Rate = 52.99 L/s

**Allowable Release Rate = 30.95 L/s**  
 (5-yr pre-development level corresponding to EWS-01, see drawing C701)

**Post-development Stormwater Management**

					ΣR <sub>2&amp;5</sub>	ΣR <sub>100</sub>
	Total Site Area =	<b>0.534</b>	ha	ΣR=	<b>0.67</b>	<b>0.83</b>
<b>Controlled</b>	WS-01A	0.045	ha	R=	0.29	0.36
	WS-01B	0.017	ha	R=	0.79	0.99
	WS-02	0.049	ha	R=	0.90	1.00
	WS-03	0.030	ha	R=	0.87	1.00
	WS-04	0.101	ha	R=	0.58	0.73
	WS-05	0.053	ha	R=	0.90	1.00
	WS-06	0.123	ha	R=	0.87	1.00
	WS-07	0.039	ha	R=	0.76	0.95
	WS-08	0.027	ha	R=	0.20	0.25
	Total Controlled =	<b>0.485</b>	ha	ΣR=	<b>0.71</b>	<b>0.89</b>
<b>Uncontrolled</b>	WS-09	0.029	ha	R=	0.20	0.25
	WS-10	0.020	ha	R=	0.20	0.25
	Total Uncontrolled =	<b>0.049</b>	ha	ΣR=	<b>0.20</b>	<b>0.25</b>



**LRL File No.** 210691  
**Project:** Proposed Development-Halo Car Wash  
**Location:** 3555 Borrisokane Rd (Barrhaven, ON)  
**Date:** July 7, 2023  
**Designed:** M. Longtin  
**Checked:** M. Basnet  
**Drawing Ref.:** C701, C702

**Stormwater Management  
Design Sheet**

**Post-development Stormwater Management (2-Yr)**

Time (min)	Intensity (mm/hr)	Controlled Runoff (L/s)	Storage Volume (m <sup>3</sup> )	*Controlled Release Rate (L/s)	Uncontrolled Runoff (L/s)	Total Release Rate (L/s)
10	76.81	73.72	36.78	12.43	2.10	14.53
15	61.77	59.29	42.17	12.43	1.69	14.12
20	52.03	49.94	45.02	12.43	1.42	13.85
25	45.17	43.35	46.39	12.43	1.23	13.66
30	40.04	38.44	46.81	12.43	1.09	13.52
35	36.06	34.61	46.58	12.43	0.98	13.41
40	32.86	31.55	45.88	12.43	0.90	13.33
45	30.24	29.03	44.81	12.43	0.83	13.26
50	28.04	26.92	43.46	12.43	0.77	13.20
55	26.17	25.12	41.88	12.43	0.71	13.14
60	24.56	23.57	40.11	12.43	0.67	13.10
65	23.15	22.22	38.19	12.43	0.63	13.06
70	21.91	21.03	36.14	12.43	0.60	13.03
75	20.81	19.98	33.97	12.43	0.57	13.00
80	19.83	19.03	31.70	12.43	0.54	12.97
85	18.94	18.18	29.35	12.43	0.52	12.95
90	18.14	17.41	26.92	12.43	0.50	12.93
95	17.41	16.71	24.42	12.43	0.48	12.91
100	16.75	16.07	21.87	12.43	0.46	12.89
105	16.13	15.49	19.26	12.43	0.44	12.87
110	15.57	14.94	16.60	12.43	0.43	12.85
115	15.05	14.44	13.89	12.43	0.41	12.84
120	14.56	13.98	11.15	12.43	0.40	12.83

\*Average release rate taken as 50% of max. allowable controlled release rate for storage calculation

**On-site stormwater detention**

**Storage required = 46.81 m<sup>3</sup>**  
 Underground Storage provided = 90.76 m<sup>3</sup> (StormTech Chambers)

LRL Associates Ltd.  
Storm Design Sheet



**LRL File No.** 210691  
**Project:** Proposed Development-Halo Car Wash  
**Location:** 3555 Borrisokane Rd (Barrhaven, ON)  
**Date:** July 7, 2023  
**Designed:** M. Longtin  
**Checked:** M. Basnet  
**Drawing Reference:** C702, C401

**Storm Design Parameters**

Rational Method

Q = 2.78CIA  
 Q = Peak flow (L/s)  
 A = Drainage area (ha)  
 C = Runoff coefficient  
 I = Rainfall intensity (mm/hr)

Runoff Coefficient (C)

Grass 0.20  
 Gravel 0.80  
 Asphalt / rooftop 0.90

City of Ottawa IDF curve equation

(5 year event, intensity in mm/hr)  
 $I_5 = 998.071 / (Td + 6.053)^{0.814}$   
 Min. velocity = 0.80 m/s  
 Manning's "n" = 0.013

LOCATION			AREA (ha)			FLOW						STORM SEWER							
WATERSHED / STREET	From MH	To MH	C = 0.20	C = 0.80	C = 0.90	Indiv. 2.78AC	Accum. 2.78AC	Time of Conc. (min.)	Rainfall Intensity (mm/hr)	Peak Flow Q (L/s)	Controlled Flow Q (L/s)	Pipe Diameter (mm)	Type	Slope (%)	Length (m)	Capacity Full (L/s)	Velocity Full (m/s)	Time of Flow (min.)	Ratio (Q/Q <sub>FULL</sub> )
WS-01A	CB01	CBMH02	0.040	0.000	0.006	0.04	0.04	10.00	104.19	3.73		250	PVC	0.45%	8.60	39.9	0.81	0.18	0.09
WS-01B	CBMH02	CBMH03	0.003	0.000	0.015	0.04	0.07	10.18	103.27	7.63		250	PVC	0.45%	22.9	39.9	0.81	0.47	0.19
WS-02	CB11	CBMH12	0.000	0.000	0.049	0.12	0.12	10.00	104.19	12.83		250	PVC	0.50%	8.4	42.0	0.86	0.16	0.31
	CBMH12	CBMH03					0.12	10.16	103.34	12.72		250	PVC	0.45%	10.4	39.9	0.81	0.21	0.32
WS-03	CBMH03	CBMH05	0.001	0.000	0.028	0.07	0.27	10.38	102.24	27.43		300	PVC	0.35%	16.7	57.2	0.81	0.34	0.48
WS-04	CB04	CBMH05	0.046	0.000	0.055	0.16	0.16	10.00	104.19	17.02		250	PVC	0.45%	14.9	39.9	0.81	0.31	0.43
WS-05	CBMH05	CBMH06	0.000	0.000	0.053	0.13	0.56	10.47	101.78	57.50		375	PVC	0.25%	21.7	87.7	0.79	0.46	0.66
WS-06	CBMH06	MH08	0.005	0.000	0.118	0.30	0.86	10.92	99.55	85.90		450	PVC	0.21%	21.8	130.7	0.82	0.44	0.66
WS-07	CBMH07	MH08	0.008	0.000	0.031	0.08	0.08	10.00	104.19	8.52		250	PVC	0.45%	10.0	39.9	0.81	0.21	0.21
	MH08	StormTech Chambers					0.94	11.13	98.58	93.13									
WS-08	CBMH09	MH10	0.027	0.000	0.000	0.02	0.02	10.00	104.19	1.58		250	PVC	0.50%	7.3	42.0	0.86	0.14	0.04
	MH10	StormTech Chambers					0.02												
	MH11 w/ ICD	OGS					0.96	11.13	98.58	94.63	24.86	250	PVC	1.00%	3.5	59.5	1.21	0.05	0.42
	OGS	Ex. STM					0.96	11.18	98.36	94.41	24.86	250	PVC	1.00%	9.5	59.5	1.21	0.13	0.42

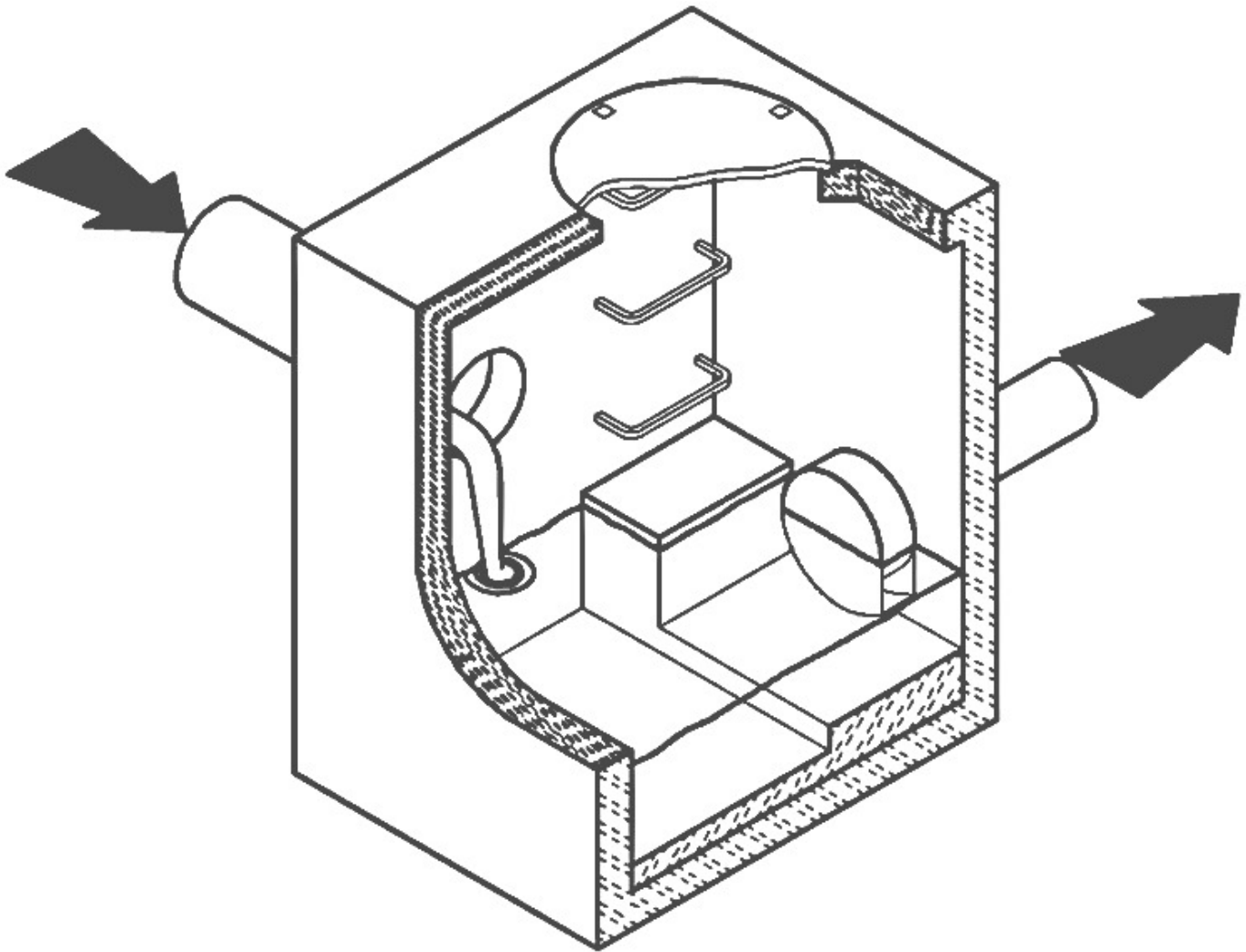
**Note**

The Peak flow will be controlled by an ICD at the outlet of STM MH11

# CSO/STORMWATER MANAGEMENT



**HYDROVEX<sup>®</sup> VHV / SVHV**  
Vertical Vortex Flow Regulator



**JOHN MEUNIER**

# HYDROVEX® VHV / SVHV VERTICAL VORTEX FLOW REGULATOR

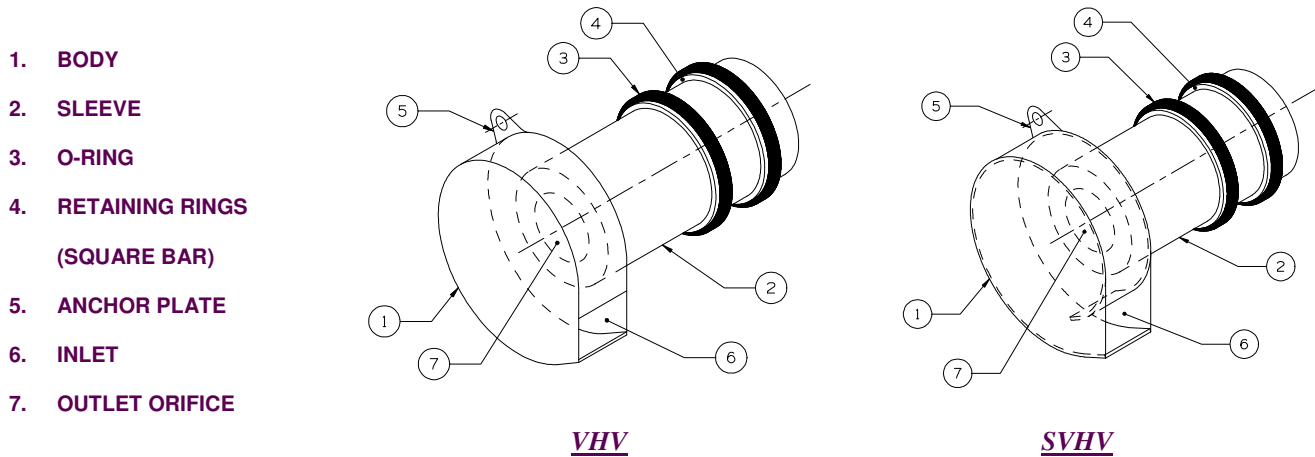
## APPLICATIONS

One of the major problems of urban wet weather flow management is the runoff generated after a heavy rainfall. During a storm, uncontrolled flows may overload the drainage system and cause flooding. Due to increased velocities, sewer pipe wear is increased dramatically and results in network deterioration. In a combined sewer system, the wastewater treatment plant may also experience significant increases in flows during storms, thereby losing its treatment efficiency.

A simple means of controlling excessive water runoff is by controlling excessive flows at their origin (manholes). **John Meunier Inc.** manufactures the **HYDROVEX® VHV / SVHV** line of vortex flow regulators to control stormwater flows in sewer networks, as well as manholes.

The vortex flow regulator design is based on the fluid mechanics principle of the forced vortex. This grants flow regulation without any moving parts, thus reducing maintenance. The operation of the regulator, depending on the upstream head and discharge, switches between orifice flow (gravity flow) and vortex flow. Although the concept is quite simple, over 12 years of research have been carried out in order to get a high performance.

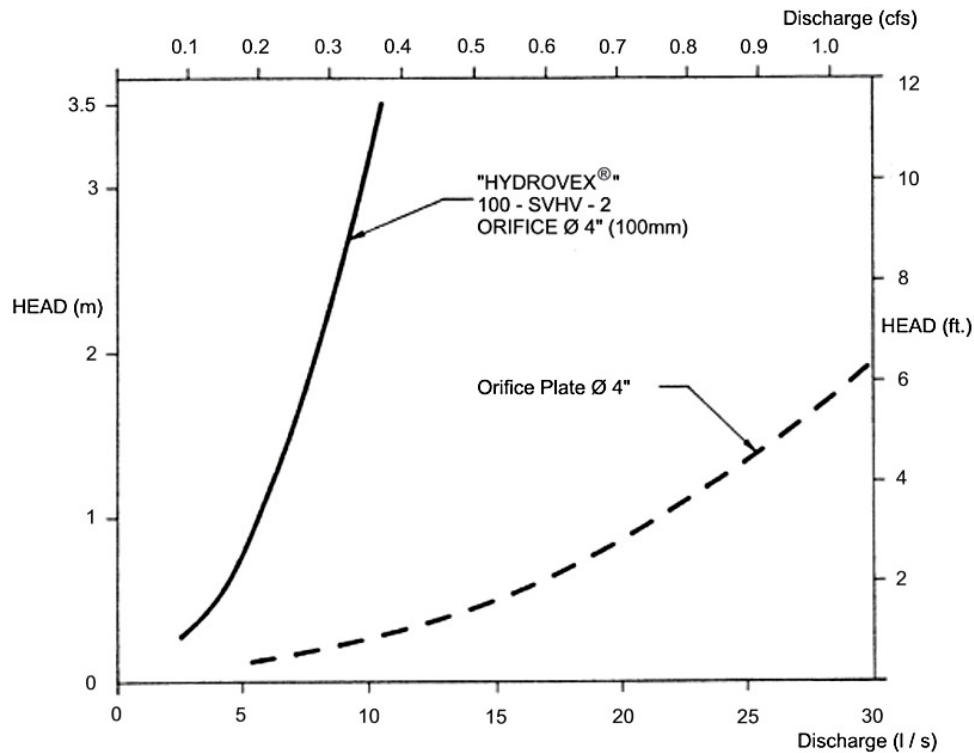
The **HYDROVEX® VHV / SVHV** Vertical Vortex Flow Regulators (refer to **Figure 1**) are manufactured entirely of stainless steel, and consist of a hollow body (1) (in which flow control takes place) and an outlet orifice (7). Two rubber "O" rings (3) seal and retain the unit inside the outlet pipe. Two stainless steel retaining rings (4) are welded on the outlet sleeve to ensure that there is no shifting of the "O" rings during installation and use.



**FIGURE 1: HYDROVEX® VHV-SVHV VERTICAL VORTEX FLOW REGULATORS**

## ADVANTAGES

- The **HYDROVEX® VHV / SVHV** line of flow regulators are manufactured entirely of stainless steel, making them durable and corrosion resistant.
- Having no moving parts, they require minimal maintenance.
- The geometry of the **HYDROVEX® VHV / SVHV** flow regulators allows a control equal to an orifice plate, having a cross section area 4 to 6 times smaller. This decreases the chance of blockage of the regulator, due to sediments and debris found in stormwater flows. **Figure 2** illustrates the comparison between a regulator model 100 SVHV-2 and an equivalent orifice plate. One can see that for the same height of water, the regulator controls a flow approximately four times smaller than an equivalent orifice plate.
- Installation of the **HYDROVEX® VHV / SVHV** flow regulators is quick and straightforward and is performed after all civil works are completed.
- Installation requires no special tools or equipment and may be carried out by any contractor.
- Installation may be carried out in existing structures.



**FIGURE 2: DISCHARGE CURVE SHOWING A HYDROVEX® FLOW REGULATOR VS AN ORIFICE PLATE**

## SELECTION

Selection of a **VHV** or **SVHV** regulator can be easily made using the selection charts found at the back of this brochure (see **Figure 3**). These charts are a graphical representation of the maximum upstream water pressure (head) and the maximum discharge at the manhole outlet. The maximum design head is the difference between the maximum upstream water level and the invert of the outlet pipe. All selections should be verified by John Meunier Inc. personnel prior to fabrication.

### Example:

- ✓ Maximum design head      2m (6.56 ft.)
- ✓ Maximum discharge        6 L/s (0.2 cfs)
- ✓ Using **Figure 3** - VHV      model required is a **75 VHV-1**

## INSTALLATION REQUIREMENTS

All **HYDROVEX®** **VHV** / **SVHV** flow regulators can be installed in circular or square manholes. **Figure 4** gives the various minimum dimensions required for a given regulator. *It is imperative to respect the minimum clearances shown to ensure easy installation and proper functioning of the regulator.*

## SPECIFICATIONS

In order to specify a **HYDROVEX**<sup>®</sup> regulator, the following parameters must be defined:

- The model number (ex: 75-VHV-1)
- The diameter and type of outlet pipe (ex: 6" diam. SDR 35)
- The desired discharge (ex: 6 l/s or 0.21 CFS)
- The upstream head (ex: 2 m or 6.56 ft.) \*
- The manhole diameter (ex: 36" diam.)
- The minimum clearance "H" (ex: 10 inches)
- The material type (ex: 304 s/s, 11 Ga. standard)

\* *Upstream head is defined as the difference in elevation between the maximum upstream water level and the invert of the outlet pipe where the **HYDROVEX**<sup>®</sup> flow regulator is to be installed.*

***PLEASE NOTE THAT WHEN REQUESTING A PROPOSAL, WE SIMPLY REQUIRE THAT YOU PROVIDE US WITH THE FOLLOWING:***

- *project design flow rate*
- *pressure head*
- *chamber's outlet pipe diameter and type*



*Typical VHV model in factory*

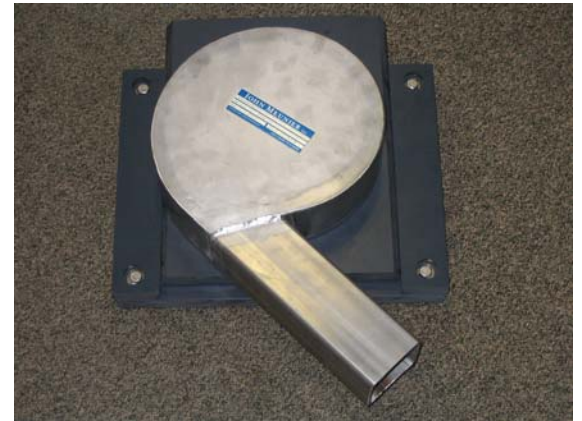
# OPTIONS



*FV – SVHV (mounted on sliding plate)*



*VHV-1-O (standard model with odour control inlet)*



*FV – VHV-O (mounted on sliding plate with odour control inlet)*



*VHV with Gooseneck assembly in existing chamber without minimum release at the bottom*



*VHV with air vent for minimal slopes*





# VHV Vertical Vortex Flow Regulator

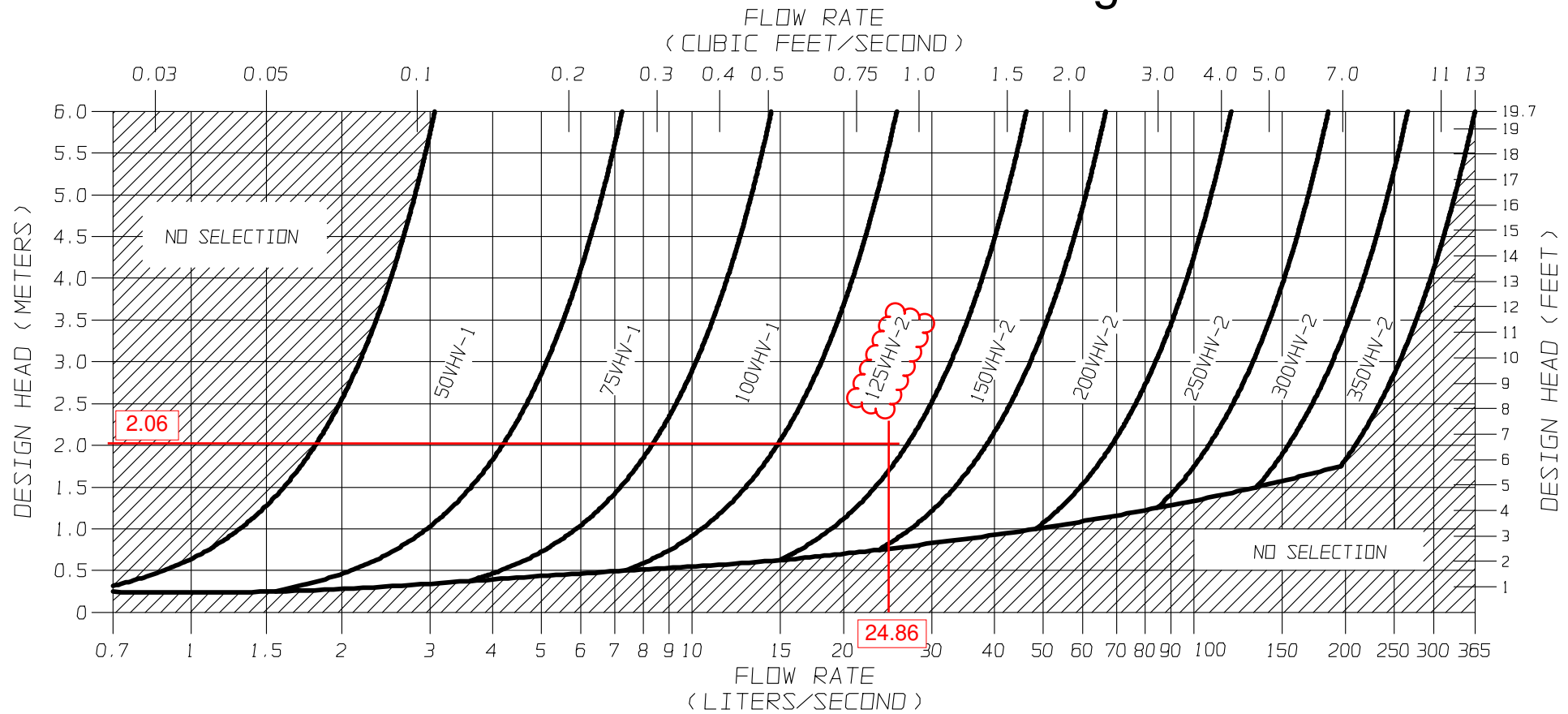
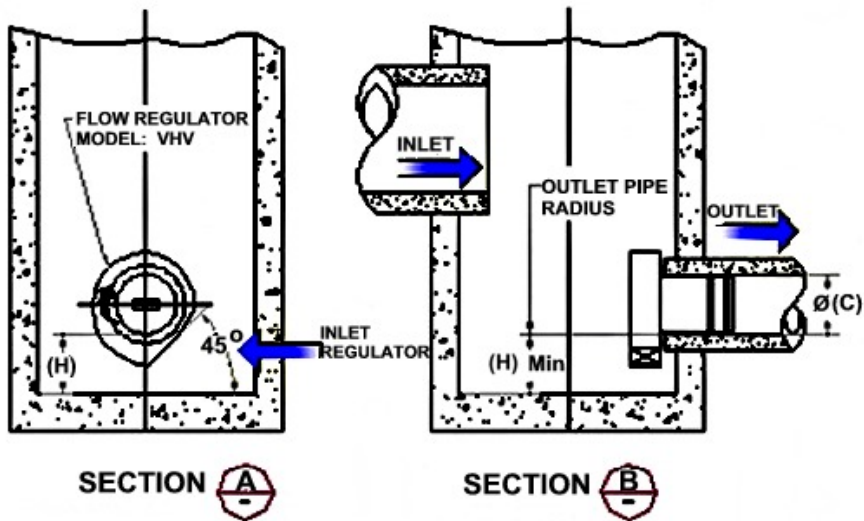
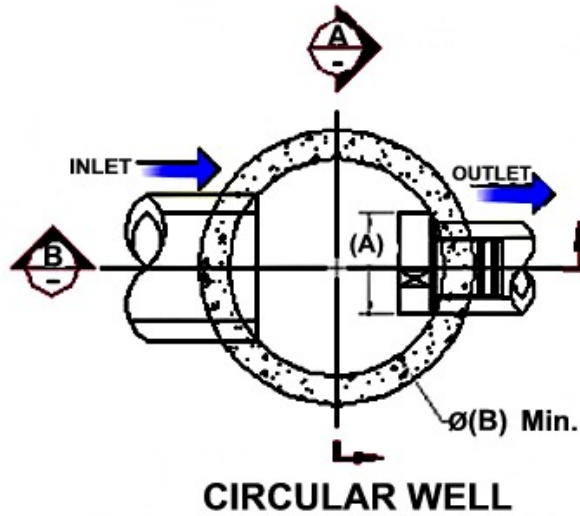


FIGURE 3 - VHV

**JOHN MEUNIER**

**FLOW REGULATOR TYPICAL INSTALLATION IN CIRCULAR MANHOLE  
FIGURE 4 (MODEL VHV)**

Model Number	Regulator Diameter		Minimum Manhole Diameter		Minimum Outlet Pipe Diameter		Minimum Clearance	
	A (mm)	A (in.)	B (mm)	B (in.)	C (mm)	C (in.)	H (mm)	H (in.)
50VHV-1	150	6	600	24	150	6	150	6
75VHV-1	250	10	600	24	150	6	150	6
100VHV-1	325	13	900	36	150	6	200	8
125VHV-2	275	11	900	36	150	6	200	8
150VHV-2	350	14	900	36	150	6	225	9
200VHV-2	450	18	1200	48	200	8	300	12
250VHV-2	575	23	1200	48	250	10	350	14
300VHV-2	675	27	1600	64	250	10	400	16
350VHV-2	800	32	1800	72	300	12	500	20



## INSTALLATION

The installation of a **HYDROVEX**<sup>®</sup> regulator may be undertaken once the manhole and piping is in place. Installation consists of simply fitting the regulator into the outlet pipe of the manhole. **John Meunier Inc.** recommends the use of a lubricant on the outlet pipe, in order to facilitate the insertion and orientation of the flow controller.

## MAINTENANCE

**HYDROVEX**<sup>®</sup> regulators are manufactured in such a way as to be maintenance free; however, a periodic inspection (every 3-6 months) is suggested in order to ensure that neither the inlet nor the outlet has become blocked with debris. The manhole should undergo periodically, particularly after major storms, inspection and cleaning as established by the municipality

## GUARANTY

The **HYDROVEX**<sup>®</sup> line of **VHV / SVHV** regulators are guaranteed against both design and manufacturing defects for a period of 5 years. Should a unit be defective, **John Meunier Inc.** is solely responsible for either modification or replacement of the unit.

### **John Meunier Inc.**

ISO 9001 : 2008

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# ADS Treatment Train Sizing

<b>Project Name:</b>	Halo Car Wash - 3555 Borrisokane Road	
<b>Consulting Engineer:</b>	LRL Engineering	
<b>Location:</b>	Barrhaven, ON	
<b>Sizing Completed By:</b>	Haider Nasrullah	<b>Email:</b> <a href="mailto:haider.nasrullah@adspipe.com">haider.nasrullah@adspipe.com</a>

Summary of Results	
Isolator Row PLUS TSS Removal:	80.9%
FD-4HC TSS Removal:	53.0%
<b>Combined TSS Removal:</b>	<b>90.9%</b>
<b>Total Volume Treated:</b>	<b>90.0%</b>

Individual OGS Results		
Model	TSS Removal	Volume Treated
FD-4HC	53.0%	>90%
FD-5HC	56.0%	>90%
FD-6HC	59.0%	>90%
FD-8HC	63.0%	>90%
FD-10HC	66.0%	>90%

Overall System Capacities	
Total Sediment Storage Capacity:	2.18 m <sup>3</sup>
Oil Storage Capacity:	723 L
Max. OGS Pipe Diameter:	600 mm
Peak OGS Flow Capacity:	510 L/s
Peak Stormtech Inlet Flow Capacity:	311 L/s
Peak IR PLUS Water Quality Flow:	51.8 L/s

OGS Specifications	
Inlet Pipe Diameter (A):	450 mm
Unit Diameter (B):	1,200 mm
Outlet Pipe Diameter (C):	450 mm
Rim Elevation (D):	93.70 m
Bottom of Sump Elevation (E):	89.15 m
Inlet Pipe Elevation (F):	91.14 m
Outlet Pipe Elevation (G):	90.65 m

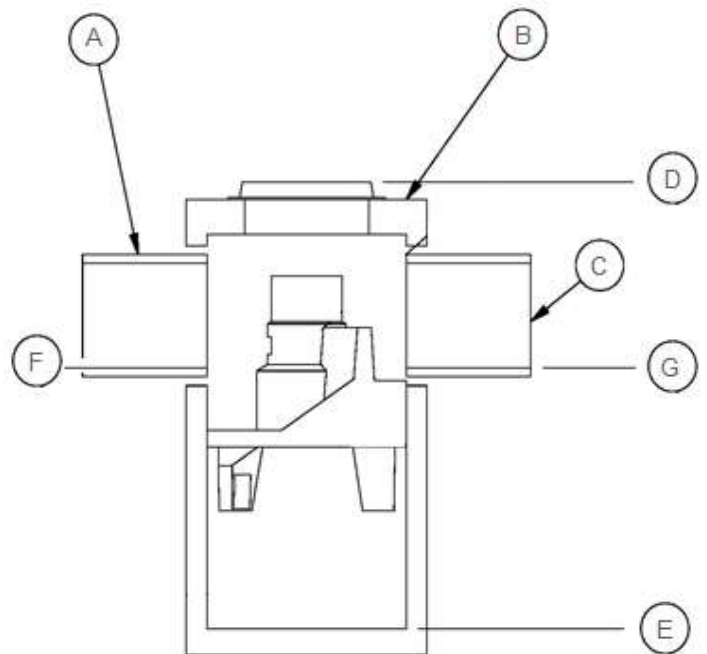
Site Details	
Site Area (ha):	0.485
Rational C:	0.71
Particle Size Distribution:	ETV
Rainfall Station:	Ottawa, ONT

Notes: OGS results based on ETV PSD and results from ETV testing protocols.

Stormtech Details	
Chamber Model:	MC-7200
No. Chambers in Isolator Row PLUS:	4
Volume Treated by Isolator Row PLUS:	99.6%

Notes: Refer to Stormtech drawings for full IR+ configuration.

Isolator Row PLUS must include Flared End Ramp (FLAMP) for proper performance.



## Notes:

Isolator Row PLUS removal efficiency based on verified ETV test report. For dimensions and configuration of Isolator Row PLUS, please see Stormtech drawing package.



Project Name: Halo Car Wash - 3555 Borrisokane Road  
 Consulting Engineer: LRL Engineering  
 Location: Barrhaven, ON

### Net Annual Removal Efficiency Summary

Rainfall Intensity	Fraction of Rainfall	Removal Efficiency		Combined Removal Efficiency	Combined Weighted Removal Efficiency
		FD-4HC	IR PLUS <sup>(2)</sup>		
mm/hr	%	%	%	%	%
0.50	0.1%	68.1%	81.2%	94.0%	0.1%
1.00	14.1%	63.2%	81.2%	93.1%	13.1%
1.50	14.2%	60.2%	81.2%	92.5%	13.1%
2.00	14.1%	58.2%	81.2%	92.1%	13.0%
2.50	4.2%	56.6%	81.2%	91.8%	3.8%
3.00	1.5%	55.2%	81.2%	91.6%	1.4%
3.50	8.5%	54.1%	81.2%	91.4%	7.8%
4.00	5.4%	53.2%	81.2%	91.2%	5.0%
4.50	1.2%	52.3%	81.2%	91.0%	1.1%
5.00	5.5%	51.6%	81.2%	90.9%	5.0%
6.00	4.3%	50.3%	81.2%	90.6%	3.9%
7.00	4.5%	49.1%	81.2%	90.4%	4.1%
8.00	3.1%	48.2%	81.2%	90.3%	2.8%
9.00	2.3%	47.3%	81.2%	90.1%	2.1%
10.00	2.6%	46.6%	81.2%	90.0%	2.3%
20.00	9.2%	41.6%	81.2%	89.0%	8.2%
30.00	2.6%	38.7%	81.2%	88.5%	2.3%
40.00	1.2%	36.6%	81.2%	88.1%	1.0%
50.00	0.5%	0.0%	81.2%	81.2%	0.4%
100.00	0.7%	0.0%	44.0%	44.0%	0.3%
150.00	0.1%	0.0%	29.3%	29.3%	0.0%
200.00	0.0%	0.0%	22.0%	22.0%	0.0%
<b>Total Net Annual Removal Efficiency</b>					<b>90.9%</b>
<b>Total Runoff Volume Treated</b>					<b>90.0%</b>

**Notes:**

- (1) Rainfall Data: 1960:2007, HLY03, Ottawa, ONT, 6105976 & 6105978.
- (2) IR PLUS removal based on ETV PSD and ETV protocols.
- (3) Rainfall adjusted to 5 min peak intensity based on hourly average.
- (4) Combined removal efficiencies calculated based on NCDENR Stormwater BMP Manual, Section 3.9.4, where Total Removal Efficiency = 1st BMP Efficiency + 2nd BMP Efficiency - (1st BMP Efficiency x 2nd BMP Efficiency)

PROJECT INFORMATION	
ENGINEERED PRODUCT MANAGER:	HAIDER NASRULLAH 647-850-9417 HAIDER.NASRULLAH@ADSPIPE.COM
ADS SALES REP:	RYAN MARTIN 705-207-2059 RYAN.MARTIN@ADSPIPE.COM
PROJECT NO:	S359205
ONTARIO SITE COORDINATOR:	RYAN RUBENSTEIN 519-710-3687 RYAN.RUBENSTEIN@ADS-PIPE.COM



# HALO CAR WASH

## BARRHAVEN, ON

### MC-3500 STORMTECH CHAMBER SPECIFICATIONS

- CHAMBERS SHALL BE STORMTECH MC-3500.
- CHAMBERS SHALL BE ARCH-SHAPED AND SHALL BE MANUFACTURED FROM VIRGIN, IMPACT-MODIFIED POLYPROPYLENE COPOLYMERS.
- CHAMBERS SHALL MEET THE REQUIREMENTS OF ASTM F2418, "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS" CHAMBER CLASSIFICATION 45x76 DESIGNATION SS.
- CHAMBER ROWS SHALL PROVIDE CONTINUOUS, UNOBSTRUCTED INTERNAL SPACE WITH NO INTERNAL SUPPORTS THAT WOULD IMPEDE FLOW OR LIMIT ACCESS FOR INSPECTION.
- THE STRUCTURAL DESIGN OF THE CHAMBERS, THE STRUCTURAL BACKFILL, AND THE INSTALLATION REQUIREMENTS SHALL ENSURE THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET FOR: 1) LONG-DURATION DEAD LOADS AND 2) SHORT-DURATION LIVE LOADS, BASED ON THE AASHTO DESIGN TRUCK WITH CONSIDERATION FOR IMPACT AND MULTIPLE VEHICLE PRESENCES.
- CHAMBERS SHALL BE DESIGNED, TESTED AND ALLOWABLE LOAD CONFIGURATIONS DETERMINED IN ACCORDANCE WITH ASTM F2787, "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS". LOAD CONFIGURATIONS SHALL INCLUDE: 1) INSTANTANEOUS (<1 MIN) AASHTO DESIGN TRUCK LIVE LOAD ON MINIMUM COVER 2) MAXIMUM PERMANENT (75-YR) COVER LOAD AND 3) ALLOWABLE COVER WITH PARKED (1-WEEK) AASHTO DESIGN TRUCK.
- REQUIREMENTS FOR HANDLING AND INSTALLATION:
  - TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING, CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS.
  - TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL, THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 3".
  - TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION, a) THE ARCH STIFFNESS CONSTANT SHALL BE GREATER THAN OR EQUAL TO 450 LBS/FT/%. THE ASC IS DEFINED IN SECTION 6.2.8 OF ASTM F2418. AND b) TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES (ABOVE 73° F / 23° C), CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS.
- ONLY CHAMBERS THAT ARE APPROVED BY THE SITE DESIGN ENGINEER WILL BE ALLOWED. UPON REQUEST BY THE SITE DESIGN ENGINEER OR OWNER, THE CHAMBER MANUFACTURER SHALL SUBMIT A STRUCTURAL EVALUATION FOR APPROVAL BEFORE DELIVERING CHAMBERS TO THE PROJECT SITE AS FOLLOWS:
  - THE STRUCTURAL EVALUATION SHALL BE SEALED BY A REGISTERED PROFESSIONAL ENGINEER.
  - THE STRUCTURAL EVALUATION SHALL DEMONSTRATE THAT THE SAFETY FACTORS ARE GREATER THAN OR EQUAL TO 1.95 FOR DEAD LOAD AND 1.75 FOR LIVE LOAD, THE MINIMUM REQUIRED BY ASTM F2787 AND BY SECTIONS 3 AND 12.12 OF THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS FOR THERMOPLASTIC PIPE.
  - THE TEST DERIVED CREEP MODULUS AS SPECIFIED IN ASTM F2418 SHALL BE USED FOR PERMANENT DEAD LOAD DESIGN EXCEPT THAT IT SHALL BE THE 75-YEAR MODULUS USED FOR DESIGN.
- CHAMBERS AND END CAPS SHALL BE PRODUCED AT AN ISO 9001 CERTIFIED MANUFACTURING FACILITY.

### IMPORTANT - NOTES FOR THE BIDDING AND INSTALLATION OF MC-3500 CHAMBER SYSTEM

- STORMTECH MC-3500 CHAMBERS SHALL NOT BE INSTALLED UNTIL THE MANUFACTURER'S REPRESENTATIVE HAS COMPLETED A PRE-CONSTRUCTION MEETING WITH THE INSTALLERS.
- STORMTECH MC-3500 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH MC-3500/MC-4500 CONSTRUCTION GUIDE".
- CHAMBERS ARE NOT TO BE BACKFILLED WITH A DOZER OR AN EXCAVATOR SITUATED OVER THE CHAMBERS. STORMTECH RECOMMENDS 3 BACKFILL METHODS:
  - STONESHOOTER LOCATED OFF THE CHAMBER BED.
  - BACKFILL AS ROWS ARE BUILT USING AN EXCAVATOR ON THE FOUNDATION STONE OR SUBGRADE.
  - BACKFILL FROM OUTSIDE THE EXCAVATION USING A LONG BOOM HOE OR EXCAVATOR.
- THE FOUNDATION STONE SHALL BE LEVELED AND COMPACTED PRIOR TO PLACING CHAMBERS.
- JOINTS BETWEEN CHAMBERS SHALL BE PROPERLY SEATED PRIOR TO PLACING STONE.
- MAINTAIN MINIMUM - 6" (150 mm) SPACING BETWEEN THE CHAMBER ROWS.
- INLET AND OUTLET MANIFOLDS MUST BE INSERTED A MINIMUM OF 12" (300 mm) INTO CHAMBER END CAPS.
- EMBEDMENT STONE SURROUNDING CHAMBERS MUST BE A CLEAN, CRUSHED, ANGULAR STONE MEETING THE AASHTO M43 DESIGNATION OF #3 OR #4.
- STONE MUST BE PLACED ON THE TOP CENTER OF THE CHAMBER TO ANCHOR THE CHAMBERS IN PLACE AND PRESERVE ROW SPACING.
- THE CONTRACTOR MUST REPORT ANY DISCREPANCIES WITH CHAMBER FOUNDATION MATERIALS BEARING CAPACITIES TO THE SITE DESIGN ENGINEER.
- ADS RECOMMENDS THE USE OF "FLEXSTORM CATCH IT" INSERTS DURING CONSTRUCTION FOR ALL INLETS TO PROTECT THE SUBSURFACE STORMWATER MANAGEMENT SYSTEM FROM CONSTRUCTION SITE RUNOFF.

### NOTES FOR CONSTRUCTION EQUIPMENT

- STORMTECH MC-3500 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH MC-3500/MC-4500 CONSTRUCTION GUIDE".
- THE USE OF EQUIPMENT OVER MC-3500 CHAMBERS IS LIMITED:
  - NO EQUIPMENT IS ALLOWED ON BARE CHAMBERS.
  - NO RUBBER Tired LOADER, DUMP TRUCK, OR EXCAVATORS ARE ALLOWED UNTIL PROPER FILL DEPTHS ARE REACHED IN ACCORDANCE WITH THE "STORMTECH MC-3500/MC-4500 CONSTRUCTION GUIDE".
  - WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT CAN BE FOUND IN THE "STORMTECH MC-3500/MC-4500 CONSTRUCTION GUIDE".
- FULL 36" (900 mm) OF STABILIZED COVER MATERIALS OVER THE CHAMBERS IS REQUIRED FOR DUMP TRUCK TRAVEL OR DUMPING.

**USE OF A DOZER TO PUSH EMBEDMENT STONE BETWEEN THE ROWS OF CHAMBERS MAY CAUSE DAMAGE TO CHAMBERS AND IS NOT AN ACCEPTABLE BACKFILL METHOD. ANY CHAMBERS DAMAGED BY USING THE "DUMP AND PUSH" METHOD ARE NOT COVERED UNDER THE STORMTECH STANDARD WARRANTY.**

CONTACT STORMTECH AT 1-888-892-2694 WITH ANY QUESTIONS ON INSTALLATION REQUIREMENTS OR WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT.

**PROPOSED LAYOUT**

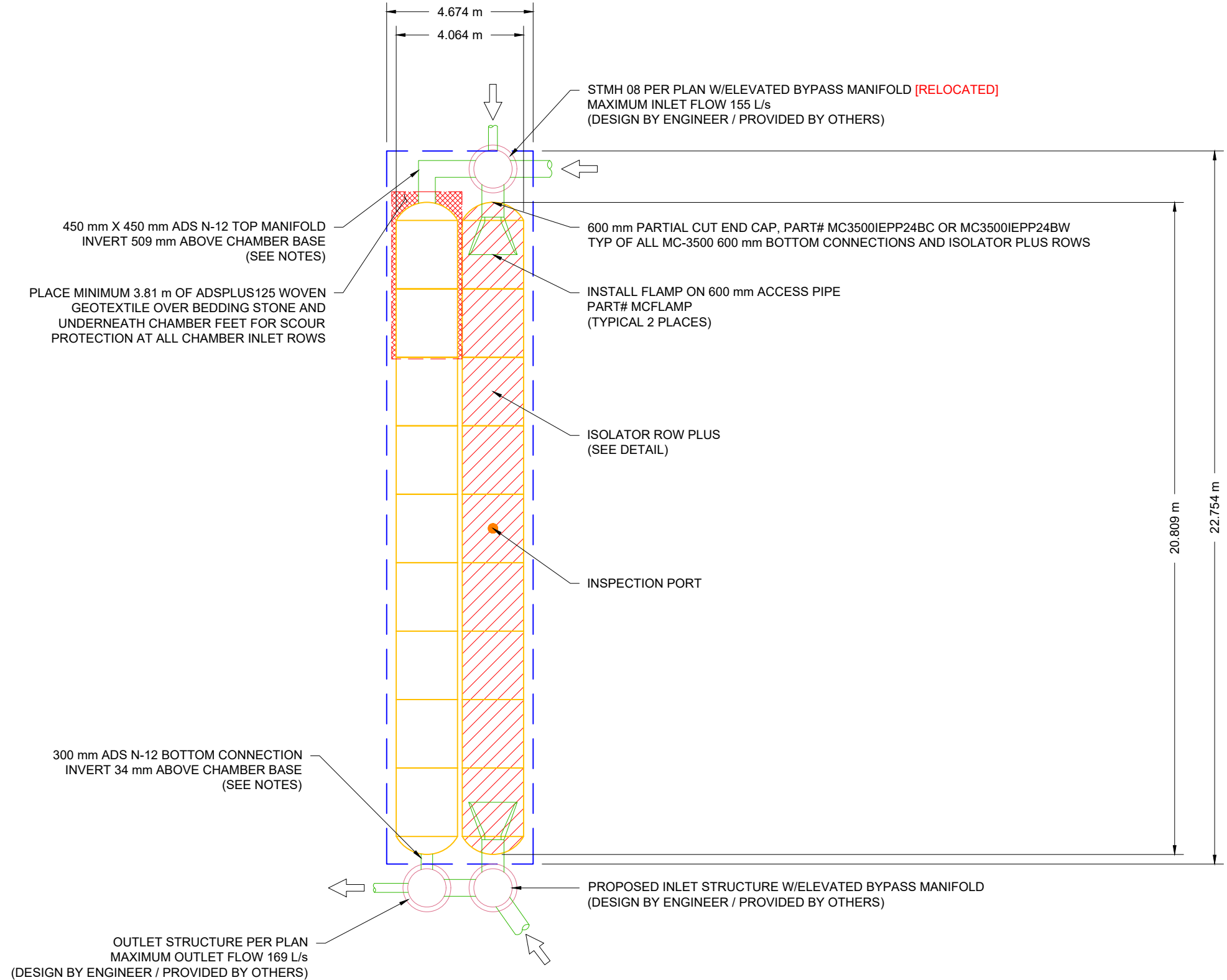
18	STORMTECH MC-3500 CHAMBERS
4	STORMTECH MC-3500 END CAPS
305	STONE ABOVE (mm)
229	STONE BELOW (mm)
40	% STONE VOID
<b>93.1</b>	<b>INSTALLED SYSTEM VOLUME (m³) ABOVE ELEVATION 91.202 (PERIMETER STONE INCLUDED)</b>
106.3	SYSTEM AREA (m²)
54.8	SYSTEM PERIMETER (m)

**PROPOSED ELEVATIONS**

94.749	MAXIMUM ALLOWABLE GRADE (TOP OF PAVEMENT/UNPAVED):
92.921	MINIMUM ALLOWABLE GRADE (UNPAVED WITH TRAFFIC):
92.768	MINIMUM ALLOWABLE GRADE (UNPAVED NO TRAFFIC):
92.768	MINIMUM ALLOWABLE GRADE (BASE OF FLEXIBLE PAVEMENT):
92.768	MINIMUM ALLOWABLE GRADE (TOP OF RIGID PAVEMENT):
92.616	TOP OF STONE:
92.311	TOP OF MC-3500 CHAMBER:
91.677	450 mm TOP MANIFOLD INVERT:
91.220	600 mm ISOLATOR ROW PLUS INVERT:
91.202	300 mm BOTTOM CONNECTION INVERT:
91.168	BOTTOM OF MC-3500 CHAMBER:
90.939	BOTTOM OF STONE:

**NOTES**

- MANIFOLD SIZE TO BE DETERMINED BY SITE DESIGN ENGINEER. SEE TECHNICAL NOTE 6.32 FOR MANIFOLD SIZING GUIDANCE.
- DUE TO THE ADAPTATION OF THIS CHAMBER SYSTEM TO SPECIFIC SITE AND DESIGN CONSTRAINTS, IT MAY BE NECESSARY TO CUT AND COUPLE ADDITIONAL PIPE TO STANDARD MANIFOLD COMPONENTS IN THE FIELD.
- THE SITE DESIGN ENGINEER MUST REVIEW ELEVATIONS AND IF NECESSARY ADJUST GRADING TO ENSURE THE CHAMBER COVER REQUIREMENTS ARE MET.
- THIS CHAMBER SYSTEM WAS DESIGNED WITHOUT SITE-SPECIFIC INFORMATION ON SOIL CONDITIONS OR BEARING CAPACITY. THE SITE DESIGN ENGINEER IS RESPONSIBLE FOR DETERMINING THE SUITABILITY OF THE SOIL AND PROVIDING THE BEARING CAPACITY OF THE INSITU SOILS. THE BASE STONE DEPTH MAY BE INCREASED OR DECREASED ONCE THIS INFORMATION IS PROVIDED.



HALO CAR WASH

BARRHAVEN, ON

DATE: 06/09/2023 DRAWN: JF

PROJECT #: S359205 CHECKED: XXX

DATE	DESCRIPTION
6/29/23	REVISED PER NEW PLAN
	DRWN CHKD
	DATE

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Chamber System

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4640 TRUEMAN BLVD  
HILLIARD, OH 43026

SCALE = 1 : 150

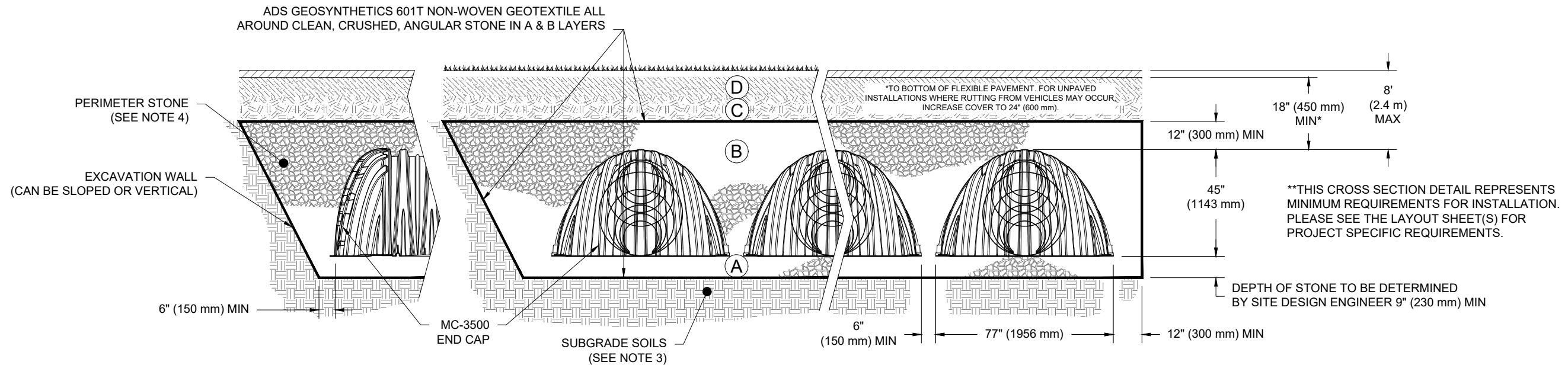
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## ACCEPTABLE FILL MATERIALS: STORMTECH MC-3500 CHAMBER SYSTEMS

MATERIAL LOCATION	DESCRIPTION	AASHTO MATERIAL CLASSIFICATIONS	COMPACTION / DENSITY REQUIREMENT
D	<b>FINAL FILL:</b> FILL MATERIAL FOR LAYER 'D' STARTS FROM THE TOP OF THE 'C' LAYER TO THE BOTTOM OF FLEXIBLE PAVEMENT OR UNPAVED FINISHED GRADE ABOVE. NOTE THAT PAVEMENT SUBBASE MAY BE PART OF THE 'D' LAYER	N/A	PREPARE PER SITE DESIGN ENGINEER'S PLANS. PAVED INSTALLATIONS MAY HAVE STRINGENT MATERIAL AND PREPARATION REQUIREMENTS.
C	<b>INITIAL FILL:</b> FILL MATERIAL FOR LAYER 'C' STARTS FROM THE TOP OF THE EMBEDMENT STONE ('B' LAYER) TO 24" (600 mm) ABOVE THE TOP OF THE CHAMBER. NOTE THAT PAVEMENT SUBBASE MAY BE A PART OF THE 'C' LAYER.	AASHTO M145 <sup>1</sup> A-1, A-2-4, A-3  OR AASHTO M43 <sup>1</sup> 3, 357, 4, 467, 5, 56, 57, 6, 67, 68, 7, 78, 8, 89, 9, 10	BEGIN COMPACTIONS AFTER 24" (600 mm) OF MATERIAL OVER THE CHAMBERS IS REACHED. COMPACT ADDITIONAL LAYERS IN 12" (300 mm) MAX LIFTS TO A MIN. 95% PROCTOR DENSITY FOR WELL GRADED MATERIAL AND 95% RELATIVE DENSITY FOR PROCESSED AGGREGATE MATERIALS.
B	<b>EMBEDMENT STONE:</b> FILL SURROUNDING THE CHAMBERS FROM THE FOUNDATION STONE ('A' LAYER) TO THE 'C' LAYER ABOVE.	CLEAN, CRUSHED, ANGULAR STONE  AASHTO M43 <sup>1</sup> 3, 4	NO COMPACTION REQUIRED.
A	<b>FOUNDATION STONE:</b> FILL BELOW CHAMBERS FROM THE SUBGRADE UP TO THE FOOT (BOTTOM) OF THE CHAMBER.	CLEAN, CRUSHED, ANGULAR STONE  AASHTO M43 <sup>1</sup> 3, 4	PLATE COMPACT OR ROLL TO ACHIEVE A FLAT SURFACE. <sup>2,3</sup>

**PLEASE NOTE:**

- THE LISTED AASHTO DESIGNATIONS ARE FOR GRADATIONS ONLY. THE STONE MUST ALSO BE CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR NO. 4 (AASHTO M43) STONE".
- STORMTECH COMPACTION REQUIREMENTS ARE MET FOR 'A' LOCATION MATERIALS WHEN PLACED AND COMPACTED IN 9" (230 mm) (MAX) LIFTS USING TWO FULL COVERAGES WITH A VIBRATORY COMPACTOR.
- WHERE INFILTRATION SURFACES MAY BE COMPROMISED BY COMPACTION, FOR STANDARD DESIGN LOAD CONDITIONS, A FLAT SURFACE MAY BE ACHIEVED BY RAKING OR DRAGGING WITHOUT COMPACTION EQUIPMENT. FOR SPECIAL LOAD DESIGNS, CONTACT STORMTECH FOR COMPACTION REQUIREMENTS.
- ONCE LAYER 'C' IS PLACED, ANY SOIL/MATERIAL CAN BE PLACED IN LAYER 'D' UP TO THE FINISHED GRADE. MOST PAVEMENT SUBBASE SOILS CAN BE USED TO REPLACE THE MATERIAL REQUIREMENTS OF LAYER 'C' OR 'D' AT THE SITE DESIGN ENGINEER'S DISCRETION.



**NOTES:**

- CHAMBERS SHALL MEET THE REQUIREMENTS OF ASTM F2418, "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS" CHAMBER CLASSIFICATION 45x76 DESIGNATION SS.
- MC-3500 CHAMBERS SHALL BE DESIGNED IN ACCORDANCE WITH ASTM F2787 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- THE SITE DESIGN ENGINEER IS RESPONSIBLE FOR ASSESSING THE BEARING RESISTANCE (ALLOWABLE BEARING CAPACITY) OF THE SUBGRADE SOILS AND THE DEPTH OF FOUNDATION STONE WITH CONSIDERATION FOR THE RANGE OF EXPECTED SOIL MOISTURE CONDITIONS.
- PERIMETER STONE MUST BE EXTENDED HORIZONTALLY TO THE EXCAVATION WALL FOR BOTH VERTICAL AND SLOPED EXCAVATION WALLS.
- REQUIREMENTS FOR HANDLING AND INSTALLATION:
  - TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING, CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS.
  - TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL, THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 3".
  - TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION, a) THE ARCH STIFFNESS CONSTANT AS DEFINED IN SECTION 6.2.8 OF ASTM F2418 SHALL BE GREATER THAN OR EQUAL TO 500 LBS/FT/%. AND b) TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES (ABOVE 73° F / 23° C), CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS.

HALO CAR WASH

BARRHAVEN, ON

DATE: 06/09/2023 DRAWN: JF

PROJECT #: S359205 CHECKED: XXX

6/29/23 DATE

RCT REVISED PER NEW PLAN DESCRIPTION

RCT DRWN CHKD

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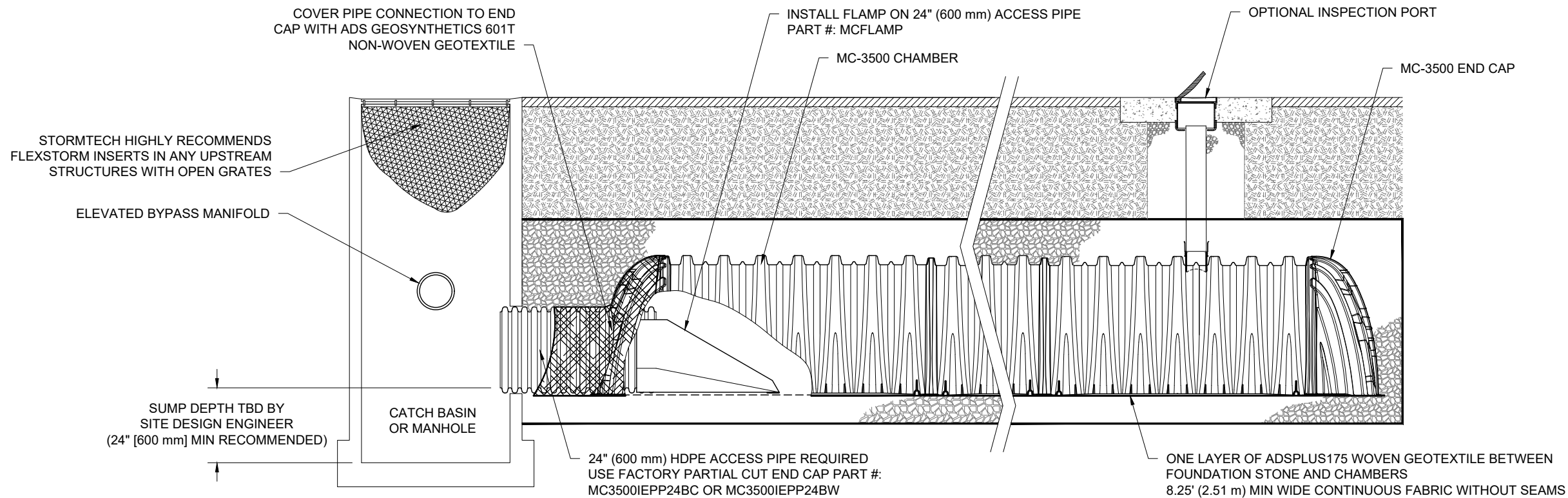
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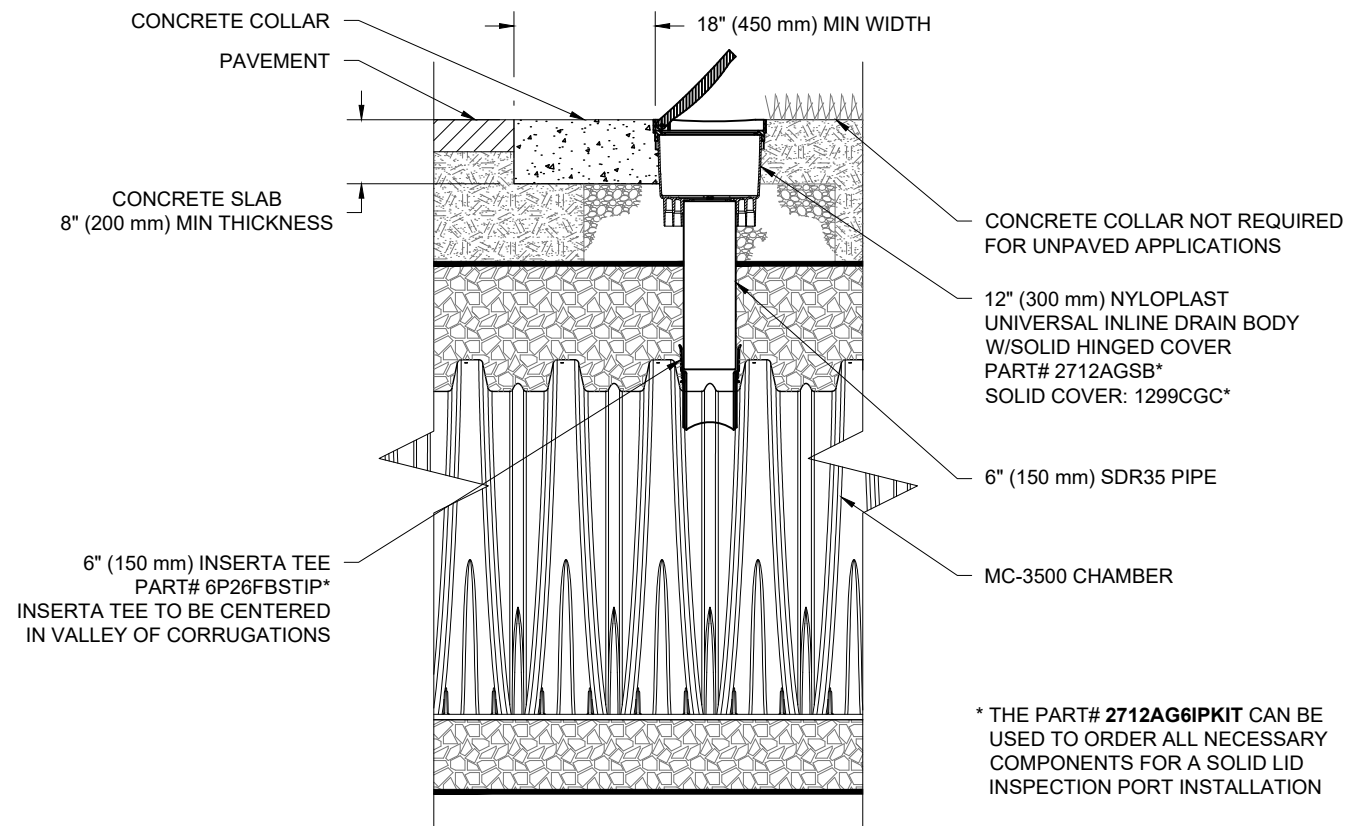
**MC-3500 ISOLATOR ROW PLUS DETAIL**  
NTS

**INSPECTION & MAINTENANCE**

- STEP 1) INSPECT ISOLATOR ROW PLUS FOR SEDIMENT
- A. INSPECTION PORTS (IF PRESENT)
    - A.1. REMOVE/OPEN LID ON NYLOPLAST INLINE DRAIN
    - A.2. REMOVE AND CLEAN FLEXSTORM FILTER IF INSTALLED
    - A.3. USING A FLASHLIGHT AND STADIA ROD, MEASURE DEPTH OF SEDIMENT AND RECORD ON MAINTENANCE LOG
    - A.4. LOWER A CAMERA INTO ISOLATOR ROW PLUS FOR VISUAL INSPECTION OF SEDIMENT LEVELS (OPTIONAL)
    - A.5. IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3.
  - B. ALL ISOLATOR PLUS ROWS
    - B.1. REMOVE COVER FROM STRUCTURE AT UPSTREAM END OF ISOLATOR ROW PLUS
    - B.2. USING A FLASHLIGHT, INSPECT DOWN THE ISOLATOR ROW PLUS THROUGH OUTLET PIPE
      - i) MIRRORS ON POLES OR CAMERAS MAY BE USED TO AVOID A CONFINED SPACE ENTRY
      - ii) FOLLOW OSHA REGULATIONS FOR CONFINED SPACE ENTRY IF ENTERING MANHOLE
    - B.3. IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3.
- STEP 2) CLEAN OUT ISOLATOR ROW PLUS USING THE JETVAC PROCESS
- A. A FIXED CULVERT CLEANING NOZZLE WITH REAR FACING SPREAD OF 45" (1.1 m) OR MORE IS PREFERRED
  - B. APPLY MULTIPLE PASSES OF JETVAC UNTIL BACKFLUSH WATER IS CLEAN
  - C. VACUUM STRUCTURE SUMP AS REQUIRED
- STEP 3) REPLACE ALL COVERS, GRATES, FILTERS, AND LIDS; RECORD OBSERVATIONS AND ACTIONS.
- STEP 4) INSPECT AND CLEAN BASINS AND MANHOLES UPSTREAM OF THE STORMTECH SYSTEM.

**NOTES**

1. INSPECT EVERY 6 MONTHS DURING THE FIRST YEAR OF OPERATION. ADJUST THE INSPECTION INTERVAL BASED ON PREVIOUS OBSERVATIONS OF SEDIMENT ACCUMULATION AND HIGH WATER ELEVATIONS.
2. CONDUCT JETTING AND VACTORING ANNUALLY OR WHEN INSPECTION SHOWS THAT MAINTENANCE IS NECESSARY.



**MC-3500 6" (150 mm) INSPECTION PORT DETAIL**  
NTS

HALO CAR WASH  
BARRHAVEN, ON  
DATE: 06/09/2023 DRAWN: JF  
PROJECT #: S359205 CHECKED: XXX

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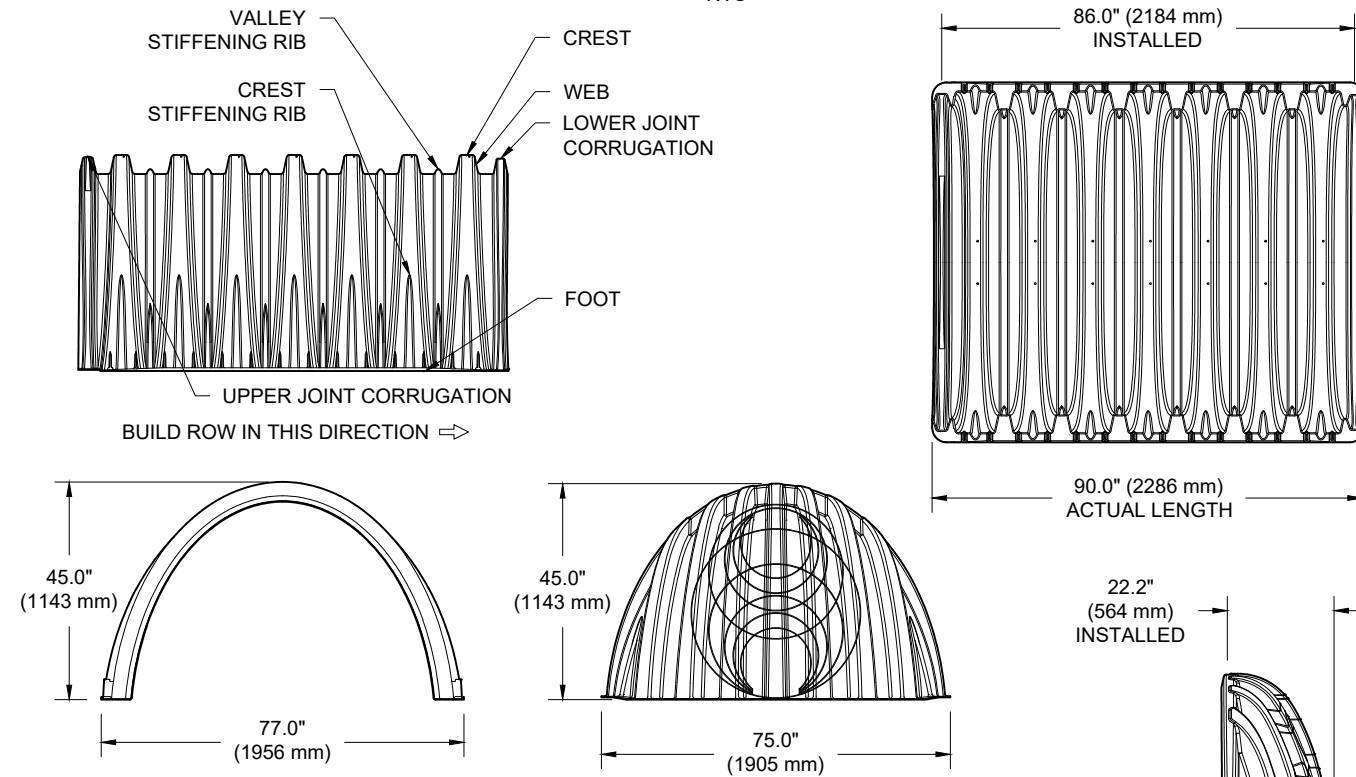
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### MC-3500 TECHNICAL SPECIFICATION

NTS



NOMINAL CHAMBER SPECIFICATIONS		
SIZE (W X H X INSTALLED LENGTH)	77.0" X 45.0" X 86.0"	(1956 mm X 1143 mm X 2184 mm)
CHAMBER STORAGE	109.9 CUBIC FEET	(3.11 m <sup>3</sup> )
MINIMUM INSTALLED STORAGE*	175.0 CUBIC FEET	(4.96 m <sup>3</sup> )
WEIGHT	134 lbs.	(60.8 kg)

NOMINAL END CAP SPECIFICATIONS		
SIZE (W X H X INSTALLED LENGTH)	75.0" X 45.0" X 22.2"	(1905 mm X 1143 mm X 564 mm)
END CAP STORAGE	14.9 CUBIC FEET	(0.42 m <sup>3</sup> )
MINIMUM INSTALLED STORAGE*	45.1 CUBIC FEET	(1.28 m <sup>3</sup> )
WEIGHT	49 lbs.	(22.2 kg)

\*ASSUMES 12" (305 mm) STONE ABOVE, 9" (229 mm) STONE FOUNDATION, 6" (152 mm) STONE BETWEEN CHAMBERS, 6" (152 mm) STONE PERIMETER IN FRONT OF END CAPS AND 40% STONE POROSITY.

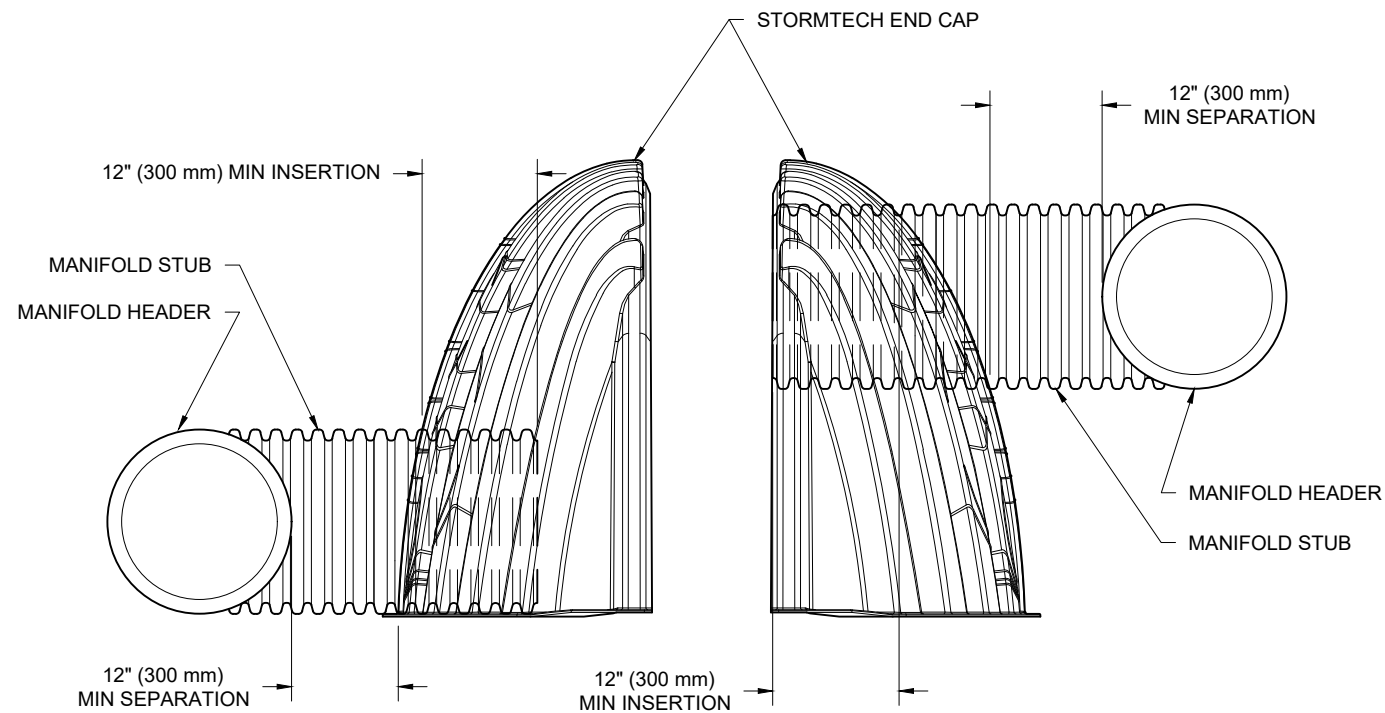
PARTIAL CUT HOLES AT BOTTOM OF END CAP FOR PART NUMBERS ENDING WITH "B"  
 PARTIAL CUT HOLES AT TOP OF END CAP FOR PART NUMBERS ENDING WITH "T"  
 END CAPS WITH A PREFABRICATED WELDED STUB END WITH "W"  
 END CAPS WITH A WELDED CROWN PLATE END WITH "C"

PART #	STUB	B	C
MC3500IEPP06T	6" (150 mm)	33.21" (844 mm)	---
MC3500IEPP06B		---	0.66" (17 mm)
MC3500IEPP08T	8" (200 mm)	31.16" (791 mm)	---
MC3500IEPP08B		---	0.81" (21 mm)
MC3500IEPP10T	10" (250 mm)	29.04" (738 mm)	---
MC3500IEPP10B		---	0.93" (24 mm)
MC3500IEPP12T	12" (300 mm)	26.36" (670 mm)	---
MC3500IEPP12B		---	1.35" (34 mm)
MC3500IEPP15T	15" (375 mm)	23.39" (594 mm)	---
MC3500IEPP15B		---	1.50" (38 mm)
MC3500IEPP18TC	18" (450 mm)	20.03" (509 mm)	---
MC3500IEPP18TW			---
MC3500IEPP18BC		---	1.77" (45 mm)
MC3500IEPP18BW		---	---
MC3500IEPP24TC	24" (600 mm)	14.48" (368 mm)	---
MC3500IEPP24TW			---
MC3500IEPP24BC		---	2.06" (52 mm)
MC3500IEPP24BW		---	---
MC3500IEPP30BC	30" (750 mm)	---	2.75" (70 mm)

CUSTOM PARTIAL CUT INVERTS ARE AVAILABLE UPON REQUEST. INVENTORIED MANIFOLDS INCLUDE 12-24" (300-600 mm) SIZE ON SIZE AND 15-48" (375-1200 mm) ECCENTRIC MANIFOLDS. CUSTOM INVERT LOCATIONS ON THE MC-3500 END CAP CUT IN THE FIELD ARE NOT RECOMMENDED FOR PIPE SIZES GREATER THAN 10" (250 mm). THE INVERT LOCATION IN COLUMN 'B' ARE THE HIGHEST POSSIBLE FOR THE PIPE SIZE.

### MC-SERIES END CAP INSERTION DETAIL

NTS



NOTE: MANIFOLD STUB MUST BE LAID HORIZONTAL FOR A PROPER FIT IN END CAP OPENING.

NOTE: ALL DIMENSIONS ARE NOMINAL

HALO CAR WASH

BARRHAVEN, ON

DATE: 06/09/2023 DRAWN: JF

PROJECT #: S359205 CHECKED: XXX

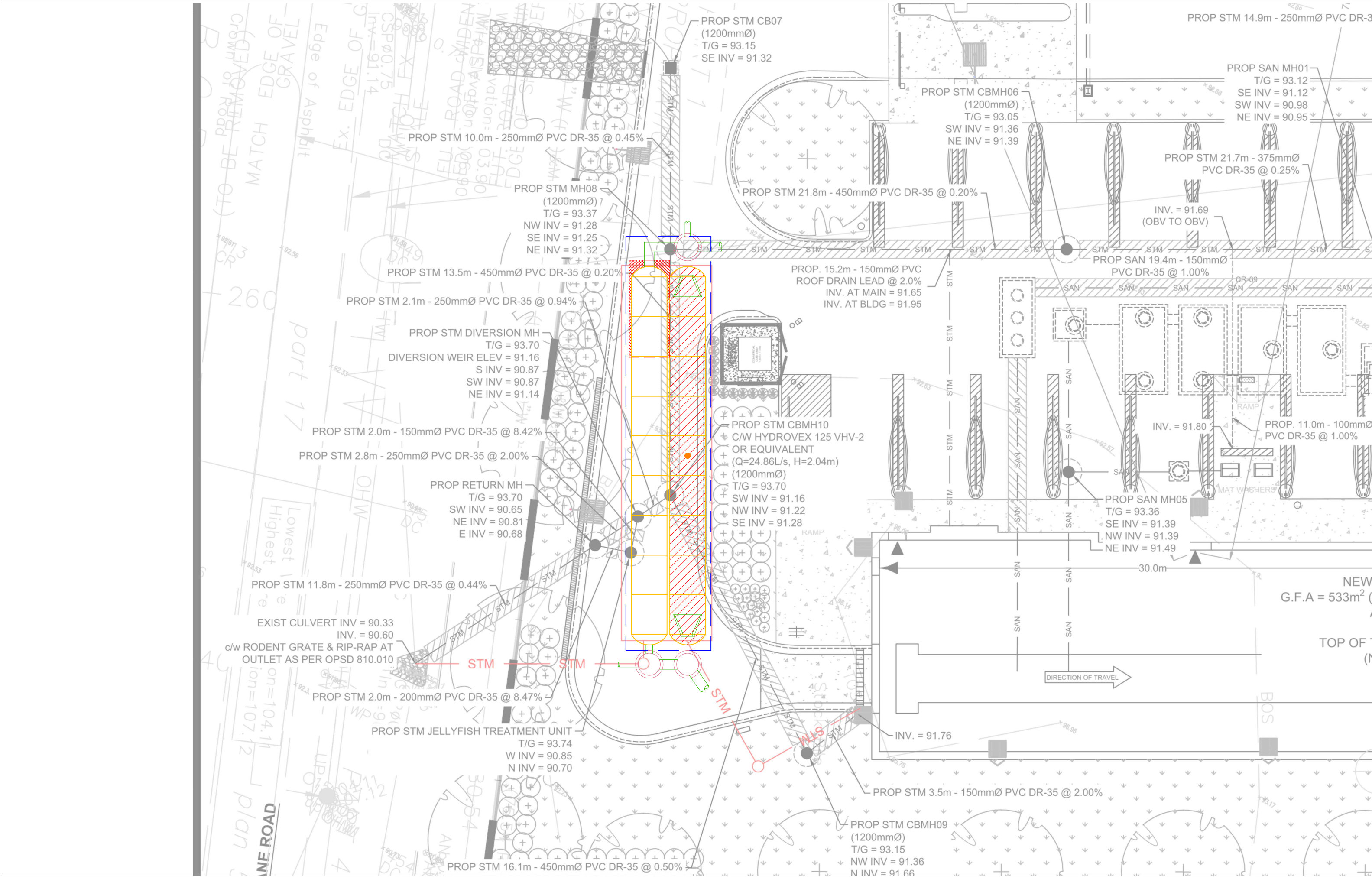
REVISED PER NEW PLAN	DESCRIPTION
6/29/23	DATE
RC1	DRWN
RC1	CHKD

**StormTech**<sup>®</sup>  
Chamber System  
888-892-2694 | WWW.STORMTECH.COM

4640 TRUEMAN BLVD  
HILLIARD, OH 43026



THIS DRAWING HAS BEEN PREPARED BASED ON INFORMATION PROVIDED TO ADS UNDER THE DIRECTION OF THE SITE DESIGN ENGINEER OR OTHER PROJECT REPRESENTATIVE. THE SITE DESIGN ENGINEER SHALL REVIEW THIS DRAWING PRIOR TO CONSTRUCTION. IT IS THE ULTIMATE RESPONSIBILITY OF THE SITE DESIGN ENGINEER TO ENSURE THAT THE PRODUCT(S) DEPICTED AND ALL ASSOCIATED DETAILS MEET ALL APPLICABLE LAWS, REGULATIONS, AND PROJECT REQUIREMENTS.



PROP STM CB07  
(1200mmØ)  
T/G = 93.15  
SE INV = 91.32

PROP STM 14.9m - 250mmØ PVC DR-35

PROP SAN MH01  
T/G = 93.12  
SE INV = 91.12  
SW INV = 90.98  
NE INV = 90.95

PROP STM 10.0m - 250mmØ PVC DR-35 @ 0.45%

PROP STM CBMH06  
(1200mmØ)  
T/G = 93.05  
SW INV = 91.36  
NE INV = 91.39

PROP STM 21.7m - 375mmØ  
PVC DR-35 @ 0.25%

PROP STM MH08  
(1200mmØ)  
T/G = 93.37  
NW INV = 91.28  
SE INV = 91.25  
NE INV = 91.32

PROP STM 21.8m - 450mmØ PVC DR-35 @ 0.20%

INV. = 91.69  
(OBV TO OBV)

PROP STM 13.5m - 450mmØ PVC DR-35 @ 0.20%

PROP. 15.2m - 150mmØ PVC  
ROOF DRAIN LEAD @ 2.0%  
INV. AT MAIN = 91.65  
INV. AT BLDG = 91.95

PROP SAN 19.4m - 150mmØ  
PVC DR-35 @ 1.00%

PROP STM 2.1m - 250mmØ PVC DR-35 @ 0.94%

PROP STM DIVERSION MH  
T/G = 93.70  
DIVERSION WEIR ELEV = 91.16  
S INV = 90.87  
SW INV = 90.87  
NE INV = 91.14

PROP STM 2.0m - 150mmØ PVC DR-35 @ 8.42%

PROP STM CBMH10  
C/W HYDROVEX 125 VHV-2  
OR EQUIVALENT  
(Q=24.86L/s, H=2.04m)  
(1200mmØ)  
T/G = 93.70  
SW INV = 91.16  
NW INV = 91.22  
SE INV = 91.28

PROP STM 2.8m - 250mmØ PVC DR-35 @ 2.00%

PROP RETURN MH  
T/G = 93.70  
SW INV = 90.65  
NE INV = 90.81  
E INV = 90.68

PROP SAN MH05  
T/G = 93.36  
SE INV = 91.39  
NW INV = 91.39  
NE INV = 91.49

PROP STM 11.8m - 250mmØ PVC DR-35 @ 0.44%

EXIST CULVERT INV = 90.33  
INV. = 90.60  
c/w RODENT GRATE & RIP-RAP AT  
OUTLET AS PER OPSD 810.010

PROP STM 2.0m - 200mmØ PVC DR-35 @ 8.47%

PROP STM JELLYFISH TREATMENT UNIT  
T/G = 93.74  
W INV = 90.85  
N INV = 90.70

INV. = 91.76

PROP STM 3.5m - 150mmØ PVC DR-35 @ 2.00%

PROP STM CBMH09  
(1200mmØ)  
T/G = 93.15  
NW INV = 91.36  
N INV = 91.66

PROP STM 16.1m - 450mmØ PVC DR-35 @ 0.50%

NEW  
G.F.A = 533m<sup>2</sup>

TOP OF

DIRECTION OF TRAVEL

LINE ROAD

Project: **Halo Car Wash**



Include Perimeter Stone in Calculations

Click for Stage Area Data

Click to Invert Stage Area Data

[Click Here for Imperial](#)

Chamber Model -	MC-7200
Units -	Metric
Number of Chambers -	8
Number of End Caps -	4
Voids in the stone (porosity) -	40 %
Base of Stone Elevation -	90.93 m
Amount of Stone Above Chambers -	305 mm
Amount of Stone Below Chambers -	229 mm

78 sq.meters Min. Area - 57.13 sq.meters

**StormTech MC-7200 Cumulative Storage Volumes**

Height of System (mm)	Incremental Single Chamber (cubic meters)	Incremental Single End Cap (cubic meters)	Incremental Chambers (cubic meters)	Incremental End Cap (cubic meters)	Incremental Stone (cubic meters)	Incremental Ch. and Stone (cubic meters)	Cumulative System (cubic meters)	Elevation (meters)
2057	0.00	0.00	0.00	0.00	0.792	0.79	90.76	92.99
2032	0.00	0.00	0.00	0.00	0.792	0.79	89.96	92.97
2007	0.00	0.00	0.00	0.00	0.792	0.79	89.17	92.94
1981	0.00	0.00	0.00	0.00	0.792	0.79	88.38	92.91
1956	0.00	0.00	0.00	0.00	0.792	0.79	87.59	92.89
1930	0.00	0.00	0.00	0.00	0.792	0.79	86.79	92.86
1905	0.00	0.00	0.00	0.00	0.792	0.79	86.00	92.84
1880	0.00	0.00	0.00	0.00	0.792	0.79	85.21	92.81
1854	0.00	0.00	0.00	0.00	0.792	0.79	84.42	92.79
1829	0.00	0.00	0.00	0.00	0.792	0.79	83.63	92.76
1803	0.00	0.00	0.00	0.00	0.792	0.79	82.83	92.74
1778	0.00	0.00	0.00	0.00	0.792	0.79	82.04	92.71
1753	0.00	0.00	0.01	0.00	0.786	0.80	81.25	92.69
1727	0.01	0.00	0.04	0.00	0.773	0.82	80.45	92.66
1702	0.01	0.00	0.06	0.01	0.765	0.83	79.63	92.63
1676	0.01	0.00	0.08	0.01	0.757	0.85	78.80	92.61
1651	0.01	0.00	0.10	0.01	0.747	0.86	77.95	92.58
1626	0.02	0.00	0.17	0.01	0.720	0.90	77.09	92.56
1600	0.03	0.00	0.25	0.01	0.687	0.95	76.19	92.53
1575	0.04	0.00	0.30	0.02	0.665	0.98	75.24	92.51
1549	0.04	0.01	0.34	0.02	0.648	1.01	74.26	92.48
1524	0.05	0.01	0.37	0.02	0.632	1.03	73.25	92.46
1499	0.05	0.01	0.41	0.03	0.618	1.05	72.22	92.43
1473	0.05	0.01	0.43	0.03	0.606	1.07	71.17	92.41
1448	0.06	0.01	0.46	0.03	0.594	1.09	70.09	92.38
1422	0.06	0.01	0.49	0.04	0.583	1.11	69.00	92.36
1397	0.06	0.01	0.51	0.04	0.572	1.12	67.90	92.33
1372	0.07	0.01	0.53	0.04	0.562	1.14	66.78	92.30
1346	0.07	0.01	0.55	0.05	0.553	1.15	65.64	92.28
1321	0.07	0.01	0.57	0.05	0.544	1.16	64.49	92.25
1295	0.07	0.01	0.59	0.05	0.535	1.18	63.32	92.23
1270	0.08	0.01	0.61	0.06	0.527	1.19	62.15	92.20
1245	0.08	0.01	0.62	0.06	0.519	1.20	60.96	92.18
1219	0.08	0.02	0.64	0.06	0.512	1.21	59.76	92.15
1194	0.08	0.02	0.66	0.06	0.504	1.22	58.54	92.13
1168	0.08	0.02	0.67	0.07	0.498	1.23	57.32	92.10
1143	0.09	0.02	0.68	0.07	0.491	1.24	56.09	92.08
1118	0.09	0.02	0.70	0.07	0.484	1.25	54.84	92.05
1092	0.09	0.02	0.71	0.07	0.479	1.26	53.59	92.03
1067	0.09	0.02	0.72	0.08	0.472	1.27	52.33	92.00
1041	0.09	0.02	0.74	0.08	0.466	1.28	51.05	91.97
1016	0.09	0.02	0.75	0.08	0.461	1.29	49.77	91.95
991	0.09	0.02	0.76	0.08	0.455	1.30	48.48	91.92
965	0.10	0.02	0.77	0.09	0.450	1.31	47.19	91.90
940	0.10	0.02	0.78	0.09	0.445	1.31	45.88	91.87
914	0.10	0.02	0.79	0.09	0.440	1.32	44.57	91.85
889	0.10	0.02	0.80	0.09	0.435	1.33	43.25	91.82
864	0.10	0.02	0.81	0.09	0.431	1.33	41.92	91.80
838	0.10	0.02	0.82	0.10	0.427	1.34	40.59	91.77
813	0.10	0.02	0.83	0.10	0.423	1.35	39.25	91.75
787	0.10	0.03	0.83	0.10	0.418	1.36	37.90	91.72
762	0.11	0.03	0.84	0.10	0.414	1.36	36.55	91.70
737	0.11	0.03	0.85	0.10	0.411	1.36	35.19	91.67
711	0.11	0.03	0.86	0.10	0.408	1.37	33.83	91.64
686	0.11	0.03	0.86	0.11	0.404	1.37	32.46	91.62
660	0.11	0.03	0.87	0.11	0.401	1.38	31.08	91.59
635	0.11	0.03	0.88	0.11	0.398	1.38	29.70	91.57
610	0.11	0.03	0.88	0.11	0.394	1.39	28.32	91.54
584	0.11	0.03	0.89	0.11	0.393	1.39	26.93	91.52
559	0.11	0.03	0.89	0.11	0.389	1.40	25.54	91.49
533	0.11	0.03	0.90	0.11	0.386	1.40	24.14	91.47
508	0.11	0.03	0.90	0.12	0.384	1.40	22.74	91.44
483	0.11	0.03	0.91	0.12	0.381	1.41	21.34	91.42
457	0.11	0.03	0.91	0.12	0.379	1.41	19.93	91.39
432	0.11	0.03	0.92	0.12	0.377	1.41	18.52	91.36
406	0.12	0.03	0.92	0.12	0.375	1.42	17.11	91.34
381	0.12	0.03	0.93	0.12	0.374	1.42	15.69	91.31
356	0.12	0.03	0.93	0.12	0.372	1.42	14.27	91.29
330	0.12	0.03	0.93	0.12	0.370	1.43	12.85	91.26
305	0.12	0.03	0.94	0.12	0.368	1.43	11.42	91.24
279	0.12	0.03	0.94	0.12	0.367	1.43	9.99	91.21
254	0.12	0.03	0.94	0.13	0.364	1.43	8.56	91.19
229	0.00	0.00	0.00	0.00	0.792	0.79	7.13	91.16
203	0.00	0.00	0.00	0.00	0.792	0.79	6.34	91.14
178	0.00	0.00	0.00	0.00	0.792	0.79	5.54	91.11
152	0.00	0.00	0.00	0.00	0.792	0.79	4.75	91.09
127	0.00	0.00	0.00	0.00	0.792	0.79	3.96	91.06
102	0.00	0.00	0.00	0.00	0.792	0.79	3.17	91.03
76	0.00	0.00	0.00	0.00	0.792	0.79	2.38	91.01
51	0.00	0.00	0.00	0.00	0.792	0.79	1.58	90.98
25	0.00	0.00	0.00	0.00	0.792	0.79	0.79	90.96

# StormTech® Isolator® Row Plus

The StormTech Isolator Row Plus is an enhancement to our proven water quality treatment system. This updated system is both a NJCAT and ETV verified water quality treatment device that can be incorporated into any system layout.

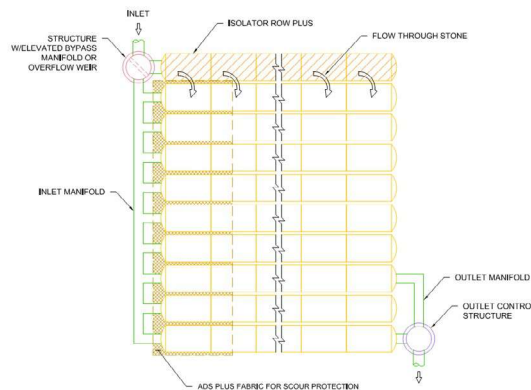
## Features

- Isolator Row Plus is now ETV verified. As a Manufactured Treatment Device it achieves over 81% TSS removal per the ISO 14034:2016 ETV standard and the Canadian Environmental Technology Verification Process.
- A patented Flamp™ (Flared End Ramp) provides a smooth transition from pipe invert to fabric bottom. The FLAMP is attached to the inlet pipe inside the chamber end cap and improves chamber function over time by distributing sediment and debris that would otherwise collect at the inlet. It also serves to improve the fluid and solid flow back into the inlet pipe during maintenance and cleaning.
- Proprietary ADS Plus fabric maintains durability and sediment removal while allowing for higher water quality flow rates. A single layer of ADS Plus fabric is placed between the angular base stone and the Isolator Row Plus chambers.

## Technology Descriptions

The Isolator Row Plus is designed to capture the “first flush” runoff and offers the versatility to be sized on a volume or a flow basis. Considered an LID (low impact development) technology, the Isolator Row Plus can be part of the treatment train design for water quality. An upstream manhole not only provides access to the Isolator Row Plus but includes a high/low concept such that stormwater flow rates or volumes that exceed the capacity of the Isolator Row Plus bypass through a manifold to the other chambers. This creates a differential between the Isolator Row Plus row of chambers and the manifold to the rest of the system, thus allowing for settlement time in the Isolator Row Plus. Stormwater is then either infiltrated into the soils below or passed at a controlled rate through an outlet manifold and outlet control structure.

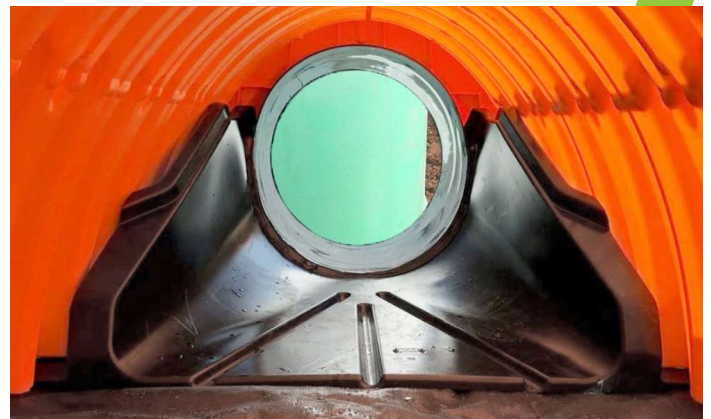
## Schematic of the StormTech Isolator Row PLUS System



## Summary of Verified Claims<sup>1</sup>

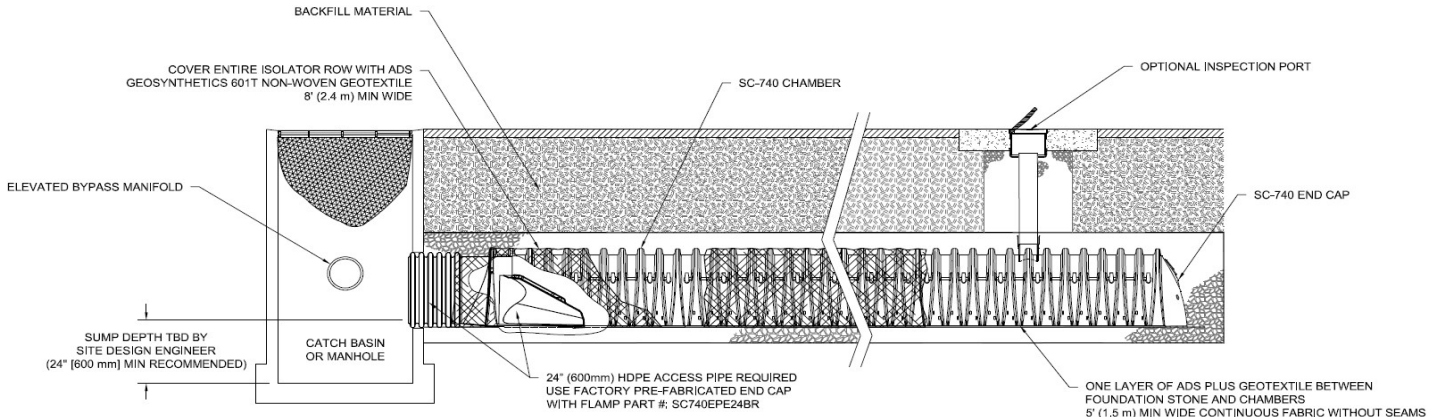
Maximum Treatment Flow Rate (MTFR) (L/s/m <sup>2</sup> )	2.8
Effective Filtration Treatment Area (m <sup>2</sup> )	5.06
Test Sediment Size (microns)	1-1000
Mean Particle Concentration (mg/L)	200
TSS Removal Efficiency	81%

<sup>1</sup> Verification of StormTech SC-740 Isolator Row PLUS test results in accordance with the ISO 14034:2016 ETV standard. The full Verification Statement for the StormTech SC-740 Isolator Row PLUS can be downloaded from the VerifiGlobal website



## StormTech Isolator Row Plus (not to scale)

Note: Non-woven fabric is only required over the chambers for the SC-310 and SC-740 chamber models.



## Maintenance

The Isolator Row Plus was designed to reduce the cost of periodic maintenance. By “isolating” sediment to just one row of the StormTech system, costs are dramatically reduced by eliminating the need to clean out each row of the entire storage bed. If inspection indicates the potential need for maintenance, access is provided via a manhole(s) located on the end(s) of the row for cleanout. Maintenance is accomplished with the JetVac process. The JetVac® process utilizes a high-pressure water nozzle to propel itself down the Isolator Row Plus while scouring and suspending sediment. As the nozzle is retrieved, the captured pollutants are flushed back into the manhole for vacuuming. Most sewer and pipe maintenance companies have vacuum/JetVac combination vehicles. Selection of an appropriate JetVac nozzle will improve maintenance efficiency.

	Chamber Storage	Chamber Footprint	Treatment Rate
SC-160LP	0.42 m <sup>3</sup> (15.0 cf)	1.06 m <sup>2</sup> (11.45 sf)	3.11 L/s (0.11 cfs)
SC-310	0.88 m <sup>3</sup> (31.0 cf)	1.64 m <sup>2</sup> (17.7 sf)	4.53 L/s (0.16 cfs)
SC-740	2.12 m <sup>3</sup> (74.9 cf)	2.58 m <sup>2</sup> (27.8 sf)	7.36 L/s (0.26 cfs)
DC-780	2.22 m <sup>3</sup> (78.4 cf)	2.58 m <sup>2</sup> (27.8 sf)	7.36 L/s (0.26 cfs)
MC-3500	4.96 m <sup>3</sup> (175.0 cf)	3.99 m <sup>2</sup> (42.9 sf)	11.32 L/s (0.40 cfs)
MC-4500	4.60 m <sup>3</sup> (162.6 cf)	2.80 m <sup>2</sup> (30.1 sf)	7.93 L/s (0.28 cfs)

## Installation

Installation of the stormwater treatment unit(s) shall be performed per manufacture’s installation instructions. Such instructions can be obtained by calling Advanced Drainage systems at 888-367-7473 or by logging on to [www.ads-pipe.com](http://www.ads-pipe.com) or [www.stormtech.com](http://www.stormtech.com).



[ads-pipcanada.ca](http://ads-pipcanada.ca)

519-699-0222

# Verification Statement



## StormTech Isolator® Row PLUS Registration number: (V-2020-10-01) Date of issue: (2020-October-27)

<b>Technology type</b>	Stormwater Filtration Device	
<b>Application</b>	Stormwater filtration technology to remove sediments, nutrients, heavy metals, and organic contaminants from stormwater runoff	
<b>Company</b>	StormTech, LLC.	
<b>Address</b>	520 Cromwell Avenue, Rocky Hill, CT 06067 USA	<b>Phone</b> +1-888-892-2694
<b>Website</b>	www.stormtech.com	
<b>E-mail</b>	info@stormtech.com	

### Verified Performance Claims

The StormTech Isolator® Row PLUS technology was tested at the Mid-Atlantic Storm Water Research Center (MASWRC), under the supervision of Boggs Environmental Consultants, Inc. The performance test results for two overlapping StormTech Isolator® Row PLUS chambers (commercial unit model SC-740) were verified by Good Harbour Laboratories Inc. (GHL), following the requirements of ISO 14034:2016 and the VerifiGlobal Performance Verification Protocol. Based on the laboratory testing conducted, the verified performance claims are as follows:

**Total Suspended Solids (TSS) Removal Efficiency** - The StormTech Isolator® Row PLUS achieved  $82\% \pm 1\%$  removal efficiency of suspended sediment concentration (SCC) at a 95% confidence level.

**Average Loading Rate** - Based on the reported flow rate data and the effective sedimentation and filtration treatment area of the test unit, the average loading rate of the test unit was  $4.15 \pm 0.03$  GPM/ft<sup>2</sup> at a 95% confidence level.

**Maximum Treatment Flow Rate (MTFR)** - Although the MTFR varies among the StormTech Isolator® Row PLUS model sizes and the number of chambers, the design surface loading rate remains the same (4.13 gpm/ ft<sup>2</sup> of treatment surface area). The test unit consisted of two overlapping StormTech SC-740 chambers with a nominal MTFR of 225 GPM (0.501 CFS) and an effective filtration treatment area (EFTA) of approximately 54.5 ft<sup>2</sup>.

**Detention Time and Volume** - The StormTech Isolator Row PLUS detention time and wet volume varies with model size. The unit tested had a wet volume of approximately 65.1 ft<sup>3</sup> and a detention time of 2.2 minutes.

**Maximum Sediment Storage Depth and Volume** - The sediment storage volume and depth vary according to the StormTech Isolator® Row PLUS model sizes and system configuration. For the two overlapping StormTech SC-740 chambers tested, the maximum sediment storage volume is 2.3 ft<sup>3</sup> at a sediment depth of 0.5 inches.

**Effective Sedimentation/Filtration Treatment Areas** - The Effective Sedimentation Area (ESA) and the Effective Filtration Treatment Area (EFTA) increase as the size of the system increases. For the two overlapping StormTech SC-740 chambers tested, the ESA and the ratio of ESA/EFTA were 54.5 ft<sup>2</sup> and 1.0, respectively.

**Sediment Mass Load Capacity** - The sediment mass load capacity varies according to the StormTech Isolator® Row PLUS model sizes and system configuration. For the two overlapping StormTech SC-740 chambers tested, the mass loading capture was 158.4 lbs ± 0.8 lbs (2.91 ± 0.01 lbs/ ft<sup>2</sup>) following a total sediment loading of 195.2 lbs.

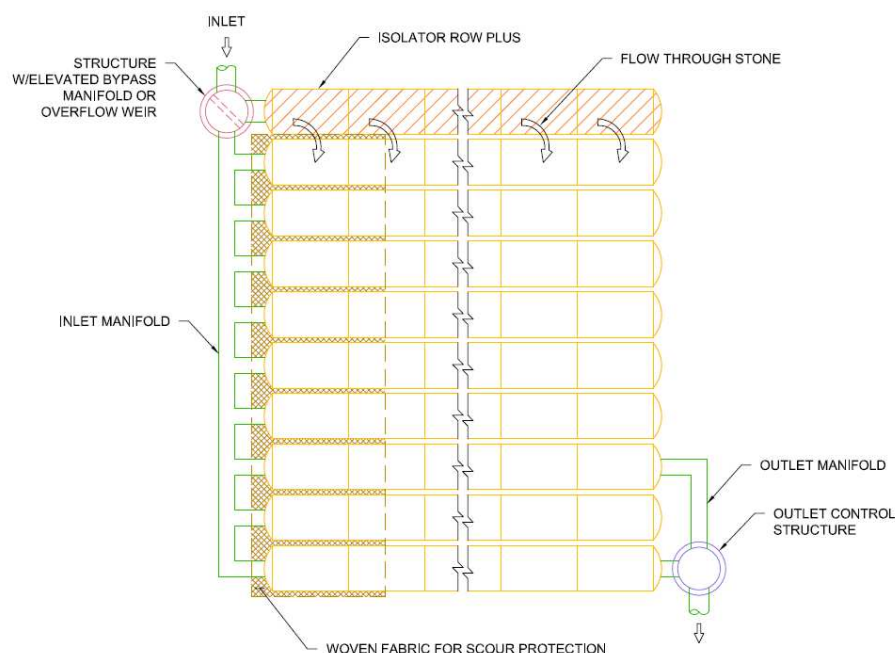
### Technology Application

The StormTech “Isolator® Row PLUS” is a stormwater treatment technology designed for use under parking lots, roadways and heavy earth loads while providing a superior and durable structural system. The technology comprises a row of chambers covered in a non-woven geotextile fabric with a single layer of proprietary woven fabric at the bottom that serves as a filter strip, providing surface area for infiltration and runoff reduction with enhanced suspended solids and pollutant removal. The following features make the Isolator® Row PLUS effective as a water quality solution:

- Enhanced infiltration Surface Area
- Runoff Volume Reduction
- Peak Flow Reduction
- Sediment/Pollutant Removal
- Internal Water Storage (IWS)
- Water Temperature Cooling (Thermal Buffer).

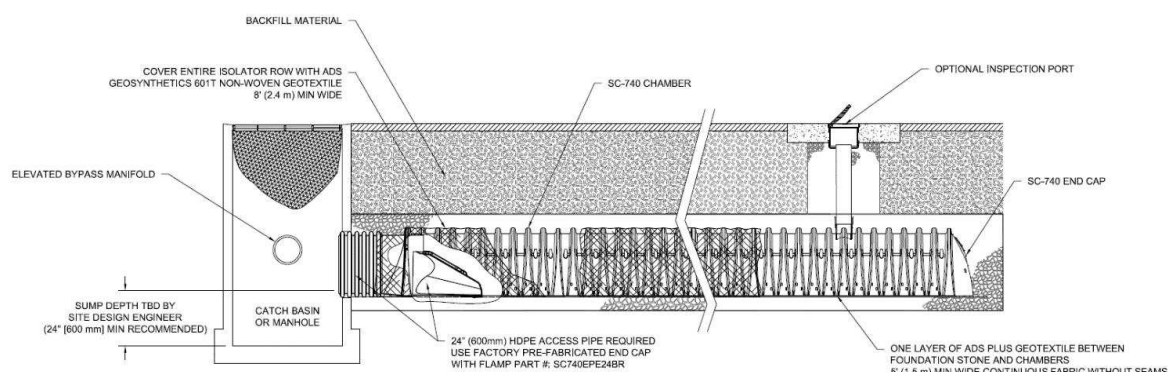
### Technology Description

The Isolator® Row PLUS (shown in Figures 1 and 2) is the first row of StormTech chambers that is surrounded with filter fabric and connected to a closely located manhole for easy access. The Isolator® Row PLUS provides for settling and filtration of sediment as stormwater rises in the chamber and ultimately passes through the filter fabric. The open-bottom chambers allow stormwater to flow out of the chambers, while sediment is captured in the Isolator® Row PLUS.



**Figure 1: Schematic of the StormTech Isolator® Row PLUS System**





**Figure 2: Isolator® Row PLUS Detail**

A single layer of proprietary Advanced Drainage Systems (ADS) PLUS fabric is placed between the angular base stone and the Isolator Row PLUS chamber. The geotextile provides the means for stormwater filtration and provides a durable surface for maintenance operations. A 6 oz. non-woven fabric is placed over the chambers.

The Isolator® Row PLUS is designed to capture the “first flush” and offers the versatility to be sized on a volume basis or a flow-rate basis. An upstream manhole not only provides access to the Isolator® Row PLUS but includes a high low/concept such that stormwater flow rates or volumes that exceed the capacity of the Isolator® Row PLUS bypass through a manifold to the other chambers. This is achieved with either a high-flow weir or an elevated manifold. This creates a differential between the Isolator® Row PLUS and the manifold, thus allowing for settlement time in the Isolator® Row PLUS. After Stormwater flows through the Isolator® Row PLUS and into the rest of the StormTech chamber system it is either infiltrated into the soils below or passed at a controlled rate through an outlet manifold and outlet control structure.

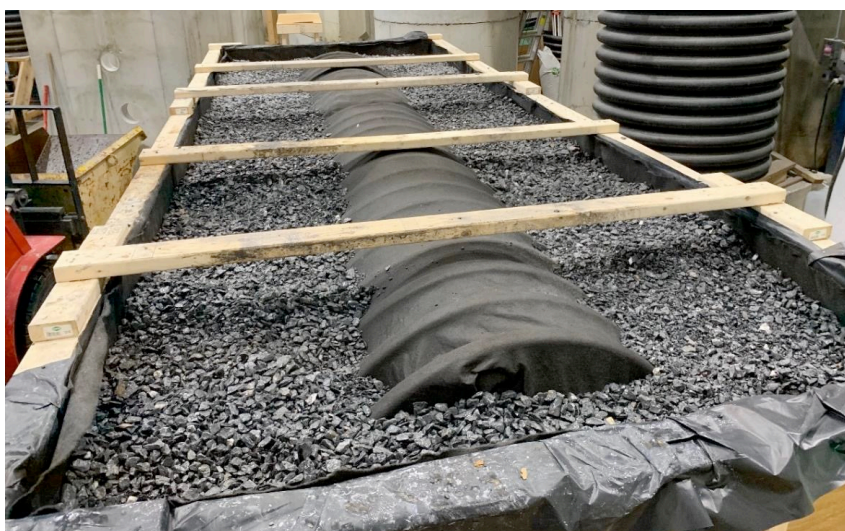
StormTech developed and owns the Isolator® Row PLUS technology and has filed a number of patent applications relating to the Isolator® Row PLUS system.<sup>1</sup>

**Description of Test Procedure for the StormTech Isolator® Row PLUS**

In January 2020, two overlapping StormTech SC-740 Isolator® Row PLUS commercial size chambers were installed at the Mid-Atlantic Storm Water Research Center (MASWRC, a subsidiary of BaySaver), in Mount Airy, Maryland, to evaluate the performance of the Isolator® Row PLUS system for Total Suspended Solid (TSS) removal (Figure 3) All testing and data collection procedures were supervised by Boggs Environmental Consultants, Inc. (BEC), who was hired by ADS for third party oversight, and were in accordance with the *New Jersey Department of Environmental Protection Laboratory Protocol to Assess Total Suspended Solids Removal by a Filtration Manufactured Treatment Device (January 2013)*.

Prior to the start of testing, a Quality Assurance Project Plan (QAPP), revision dated January 09, 2020, was submitted and approved by the New Jersey Corporation for Advanced Technology (NJCAT), c/o Center for Environmental Systems, Stevens Institute of Technology, Castle Point on Hudson, Hoboken, NJ 07030.

<sup>1</sup> (U.S. Provisional Application No. 62/753,050, filed October 30, 2018; U.S. Non-Provisional Application No. 16/670,628, filed October 31, 2019; International Application No. PCT/US2019/059283, filed October 31, 2019; U.S. Application No. 16/938,482, filed July 24, 2020; U.S. Application No. 16/938,657, filed July 24, 2020; PCT International Application No. PCT/US2020/043543, filed July 24, 2020; PCT International Application No. PCT/US2020/043557, filed July 24, 2020.



**Figure 3: StormTech “Isolator® Row PLUS” Test Set-up at MASWRC**

**Verification Results**

The verification process for the StormTech Isolator® Row PLUS technology was conducted by GHIL in accordance with the VerifiGlobal Verification Plan for the StormTech “Isolator® Row PLUS” Technology – 2020-09-09. The technology performance claims verified by GHIL are summarized at the front of this Verification Statement and in Table 6 on Page 8 under the heading “Verification Summary”.

Particle size distribution analysis was performed by ECS Mid-Atlantic, LLC of Frederick, MD in accordance with ASTM D422-63(2007). ECS is accredited by the American Association of State Highways and Transportation Officials (AASHTO).

ASTM D422-63(2007) is a sieve and hydrometer method where the larger particles, > 75 microns, are measured using a standard sieve stack while the smaller particles are measured based on their settling time using a hydrometer.

The PSD meets the requirements of NJDEP, which is generally accepted as representative of the type of particle sizes an OGS would be designed to treat. Actual PSD is site and rainfall event specific, so it was necessary to choose a standard PSD to make testing and comparison manageable.

Table 1 shows the NJDEP PSD specification. Table 2 and Figure 4 show the incoming material PSD as determined by ECS Mid-Atlantic and confirmed by the verifier.

**Table 1: NJDEP PSD Specification**

Particle Size (µm)	NJDEP Minimum Specification
1000	98
500	93
250	88
150	73
100	58
75	48
50	43
20	33
8	18
5	8
2	3
d <sub>50</sub>	< 75 µm

Table 2 – Particle Size Distribution (PSD) of Test Sediment

Mesh (mm)	US Sieve Size	Sample ID		
		PSD A	PSD B	PSD C
		Percent Finer		
9.525	0.375	100.0	100.0	100.0
4.750	#4	100.0	100.0	100.0
4.000	#5	100.0	100.0	100.0
2.360	#8	100.0	100.0	100.0
2.000	#10	100.0	100.0	100.0
1.180	#16	100.0	100.0	100.0
1.000	#18	100.0	100.0	100.0
0.500	#35	100.0	100.0	100.0
0.425	#40	93.3	93.0	93.6
0.250	#60	90.3	89.8	90.2
0.150	#100	79.3	78.1	78.1
0.125	#120	73.6	71.7	71.7
0.106	#140	68.4	65.2	64.8
0.090	#170	60.2	58.3	57.5
0.075	#200	52.0	50.9	50.3
0.053	#270	48.0	48.3	47.8
0.045	Hydrometer	46.6	46.7	46.7
0.032		42.8	42.9	41.0
0.021		37.1	37.2	35.3
0.0125		25.7	25.7	25.8
0.0090		20.1	20.1	19.2
0.0064		16.3	16.4	14.5
0.0032		8.8	8.7	7.8
0.0014		3.8	3.7	3.8

The suspended sediment concentration analysis was completed by Fredericktowne Labs Inc., Meyersville, MD. Fredericktowne Labs is accredited by the Maryland Department of Environment as Maryland Certified Water Quality Laboratory. The analysis procedure was ASTM D3977-97, Suspended Sediment Concentration. The sampling procedure and submission of samples to the test lab were overseen by the independent observer, Boggs Environmental Consultants, Inc.

All test data and calculations were detailed in the report “NJCAT TECHNOLOGY VERIFICATION Isolator® Row PLUS StormTech, LLC”, July 2020, which was submitted to and verified by the New Jersey Corporation for Advanced Technology (NJCAT).

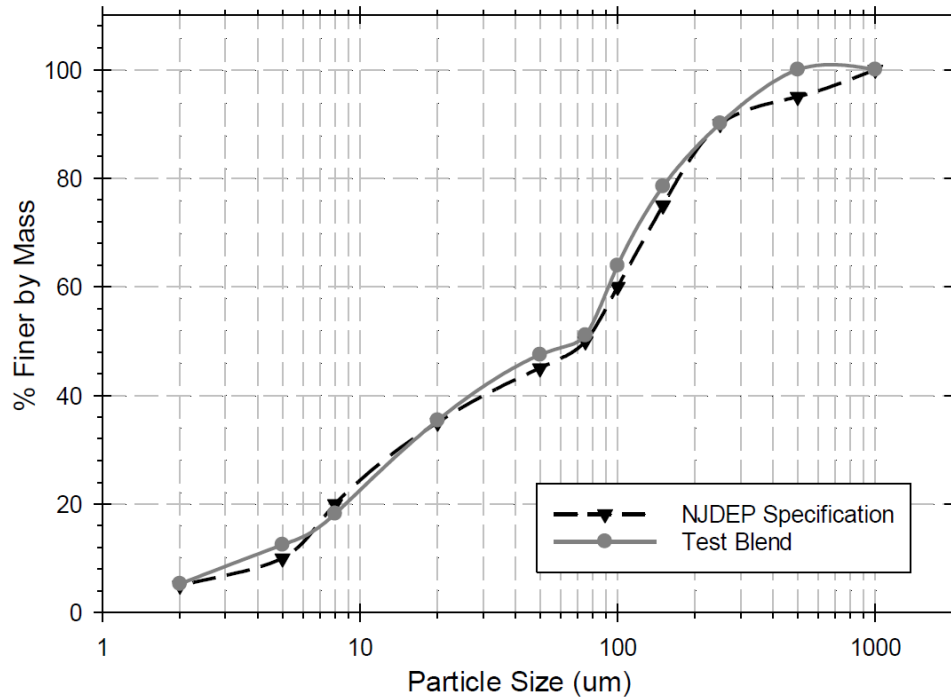


Figure 4– Particle Size Distribution (PSD)

The data in Table 3 (Flow Rate and Temperature) and Table 4 (Removal Efficiency) form the basis for the verified technology performance claim, specifically, flow rate, sediment captured and removal efficiency.

Table 3: Flow Rate and Temperature Summary

Run	Max Flow (gpm)	Min Flow (gpm)	Average Flow (gpm)	Flow COV	Flow Compliance (COV < 0.1)	Maximum Temperature (Fahrenheit)	NJDEP Temperature Compliance (< 80 F)
1	232.8	223.9	226.3	0.0078	Y	48.2	Y
2	228.9	218.6	220.8	0.0104	Y	51.5	Y
3	229.4	220.0	227.2	0.0094	Y	44.7	Y
4	230.2	218.7	223.2	0.0138	Y	40.5	Y
5	228.7	216.9	222.2	0.0103	Y	44.7	Y
6	227.6	217.0	224.2	0.0115	Y	46.7	Y
7	229.7	221.9	226.4	0.0092	Y	44.6	Y
8	230.3	222.2	226.8	0.0089	Y	43.5	Y
9	233.2	218.4	225.6	0.0136	Y	45.5	Y
10	232.2	219.7	228.4	0.0126	Y	44.7	Y
11	226.9	219.2	224.1	0.0088	Y	52.4	Y
12	232.2	222.1	226.9	0.0107	Y	48.5	Y
13	234.7	221.2	226.1	0.0109	Y	48.5	Y
14	231.9	223.4	228.7	0.0103	Y	45.6	Y
15	236.8	224.1	231.4	0.0131	Y	52.2	Y
16	232.5	221.3	229.0	0.0137	Y	47.8	Y

Table 4: Removal Efficiency Results

Run	Average Influent TSS (mg/L)	Influent Water Volume (gal)	Adjusted Average Effluent TSS (mg/L)	Effluent Water Volume (gal)	Adjusted Average Drain Down TSS (mg/L)	Drain Down Water Volume (gal)	Single Run Removal Efficiency (%)	Mass of Captured Sediment (g)	Cumulative Removal Efficiency (%)
1	203	7166	46	6881	34	285	77.8	4282	77.8
2	199	6993	32	6639	27	354	84.0	4415	80.8
3	207	7197	37	6793	27	403	82.6	4654	81.4
4	217	7068	33	6635	29	433	84.9	4923	82.3
5	215	7037	39	6593	29	444	82.2	4705	82.3
6	207	7097	40	6643	31	454	81.2	4504	82.1
7	198	7169	37	6693	30	476	81.6	4386	82.0
8	201	7184	37	6716	32	468	81.6	4473	82.0
9	205	7147	38	6675	30	472	81.8	4539	82.0
10	203	7235	38	6759	31	476	81.4	4523	81.9
11	208	7096	38	6624	30	472	81.8	4567	81.9
12	209	7185	41	6709	30	476	80.7	4584	81.8
13	198	7162	41	6680	32	482	79.7	4277	81.6
14	200	7242	43	6757	34	485	78.8	4318	81.4
15	196	7329	41	6842	32	487	79.5	4320	81.3
16	202	7254	44	6769	31	485	78.9	4384	81.2
<b>Avg.</b>	<b>204.2</b>	<b>7160</b>	<b>39</b>	<b>6713</b>	<b>31</b>	<b>447</b>	<b>81.2</b>	<b>4491</b>	<b>N/A</b>
<b>Cumulative Mass Removed (g)</b>							<b>71854</b>		
<b>Cumulative Mass Removed (lb)</b>							<b>158.4</b>		
<b>Total Mass Loaded (lb)</b>							<b>195.2</b>		
<b>Cumulative Removal Efficiency (%)</b>							<b>81.2</b>		

**Quality Assurance**

Performance verification of the StormTech Isolator® Row PLUS technology was performed in accordance with the requirements of ISO 14034:2016 and the VerifiGlobal Performance Verification Protocol. This included reviewing all data sheets and calculated values, as well as overall management of the test system, quality control and data integrity.

Additional information on quality control measures taken can be found in section 5 of the QAPP for StormTech Isolator Row New Jersey Department of Environmental Protection Testing, Rev. 1/9/2020.

Specific QA/QC measures reviewed by the verifier are summarized in Table 5 below.

Table 5. Validation of QA/QC Procedures

QC Parameter	Acceptance Criteria
Independence of observer	Confirmed in letter from Boggs Environmental Consultants, Inc. to NJCAT
Consistency of procedure	Daily logs confirm proper procedure
Existence of QAPP	Confirmed. "QAPP For StormTech Isolator Row New Jersey Department of Environmental Protection Testing", Rev. 1/9/2020)
Use of appropriate sample analysis method – ASTM D3799	Confirmed by method reference on lab reports from Fredericktowne Labs Inc.
Test method appropriate for the technology	Used industry stakeholder approved protocol: <i>New Jersey Department of Environmental Protection Laboratory Protocol to Assess Total Suspended Solids</i>

	<i>Removal by a Filtration Manufactured Treatment Device (January 2013)</i>
Test parameters stayed within required limits	Confirmed in report “NJCAT TECHNOLOGY VERIFICATION Isolator® Row PLUS StormTech, LLC”, July 2020
Third party verified data	All testing was observed and reviewed by Boggs Environmental Consultants, Inc.

**Variance**

Performance claims regarding structural load limitations were not verified as they are outside the scope of the performance testing that was conducted in accordance with the ‘Quality Assurance Project Plan (QAPP) for StormTech Isolator Row, New Jersey Department of Environmental Protection Testing’, revision dated January 09, 2020.

**Verification Summary**

The StormTech “Isolator® Row PLUS” is a stormwater treatment technology designed for use under parking lots, roadways and heavy earth loads while providing a superior and durable structural system. The technology comprises a row of chambers wrapped in woven geotextile fabric with two layers at the bottom that serve as a filter strip, providing surface area for infiltration and runoff reduction with enhanced suspended solids and pollutant removal.

The StormTech Isolator® Row PLUS technology was tested at the Mid-Atlantic Storm Water Research Center (MASWRC), under the supervision of Boggs Environmental Consultants, Inc. The performance test results for two overlapping StormTech Isolator® Row PLUS chambers (commercial unit model SC-740) were verified by Good Harbour Laboratories Inc. (GHL), following the requirements of ISO 14034:2016 and the VerifiGlobal Performance Verification Protocol. Table 6 summarizes the verification results in relation to the technology performance parameters that were identified in the Verification Plan to determine the efficacy of the StormTech Isolator® Row PLUS technology.

**Table 6 - Summary of Verification Results Against Performance Parameters**

Parameters	Verified Claims	Accuracy
Total Suspended Solids (TSS) Removal Efficiency	Based on the laboratory testing conducted, the StormTech Isolator® Row PLUS achieved an average 82% removal efficiency of SSC	± 1% (95% confidence level)
Average Loading Rate	Based on the laboratory testing parameters, the StormTech Isolator® Row PLUS maintained a loading rate of 4.15 GPM/sf	±0.03 GPM/sf (95% confidence level)
Maximum Treatment Flow Rate (MTFR)	Although the MTFR varies among the StormTech Isolator® Row PLUS model sizes and the number of chambers, the design surface loading rate remains the same (4.13 GPM/ft <sup>2</sup> of treatment surface area). The test unit consisted of two overlapping StormTech SC-740 chambers with a nominal MTFR of 225 GPM (0.501 CFS) and an effective filtration treatment area (EFTA) of approximately 54.5 ft <sup>2</sup> .	± 1.4 GPM (95% confidence level)
Detention Time and Volume	Detention time and wet volume varies with model size. The unit tested had a wet volume of approximately 65.1 ft <sup>3</sup> (based on	N/A

	physical measurement) and a detention time of 2.2 minutes.	
Maximum Sediment Storage Depth and Volume	The sediment storage volume and depth vary according to the StormTech Isolator® Row PLUS model sizes and system configuration. For the two overlapping StormTech SC-740 chambers tested, the maximum sediment storage volume is 2.3 ft <sup>3</sup> at a sediment depth of 0.5 inches.	N/A
Effective Sedimentation/ Filtration Treatment Area	The effective sedimentation and filtration treatment area increases as the size of the chamber increases. Under the tested conditions using 2 overlapping chambers, the treatment area was 54.5 ft <sup>2</sup>	The sedimentation /filtration area was determined from the actual physical dimensions of the test unit*
Sediment Mass Load Capacity	The sediment mass load capacity varies according to the StormTech Isolator® Row PLUS model sizes and system configuration. For the two overlapping StormTech SC-740 chambers tested, the mass loading capture was 158.4 lbs (2.91 lbs/ ft <sup>2</sup> ) following a total sediment loading of 195.2 lbs	± 0.8 lbs (±0.01 lbs/ft <sup>2</sup> ) (95% confidence level)

\*Note: These numbers are determined based on physical measurement or a dimensional drawing, which is standard practice. Highly accurate measurements are not practical.

In conclusion, the StormTech Isolator® Row PLUS is a viable technology that can be used to remove contaminants from stormwater runoff via filtration. This technology has proven effective at removing suspended sediment from stormwater through in-lab testing using an industry recognized laboratory protocol.

By extension of sediment removal, this technology should also remove particle bound nutrients, heavy metals, and a wide variety of organic contaminants. Performance is a function of pollutant properties, hydraulic retention time, filter media, pre-treatment, and flow rate, such that proper design of the system is critical to achieving the desired results.

**What is ISO 14034?**

The purpose of environmental technology verification is to provide a credible and impartial account of the performance of environmental technologies. Environmental technology verification is based on a number of principles to ensure that verifications are performed and reported accurately, clearly, unambiguously and objectively. The International Organization for Standardization (ISO) standard for environmental technology verification (ETV) is ISO 14034, which was published in November 2016.



**Benefits of ETV**

ETV contributes to protection and conservation of the environment by promoting and facilitating market uptake of innovative environmental technologies, especially those that perform better than relevant alternatives. ETV is particularly applicable to those environmental technologies whose innovative features or performance cannot be fully assessed using existing standards. Through the provision of objective evidence, ETV provides an independent and impartial confirmation of the performance of an environmental technology based on reliable test data. ETV aims to strengthen the credibility of new, innovative technologies by supporting informed decision-making among interested parties.

For more information on the StormTech “Isolator® Row PLUS” technology, contact:	For more information on VerifiGlobal, contact:
StormTech, LLC. 520 Cromwell Avenue, Rocky Hill, CT 06067 USA t: +1-888-892-2694 e: info@stormtech.com w: www.stormtech.com	VerifiGlobal c/o ETA-Danmark A/S Göteborg Plads 1, DK-2150 Nordhaven t +45 7224 5900 e: info@verifiglobal.com w: www.verifiglobal.com
Signed for StormTech:  <i>Original signed by:</i> <i>Greg Spires</i> Greg Spires, P.E. General Manager	Signed for VerifiGlobal:  <i>Original signed by:</i> <i>Thomas Bruun</i> Thomas Bruun, Managing Director  <i>Original signed by:</i> <i>John Neate</i> John Neate, Managing Director

**NOTICE:** Verifications are based on an evaluation of technology performance under specific, predetermined operational conditions and parameters and the appropriate quality assurance procedures. VerifiGlobal and the Verification Expert, Good Harbour Laboratories, make no expressed or implied warranties as to the performance of the technology and do not certify that a technology will always operate as verified. The end user is solely responsible for complying with any and all applicable regulatory requirements. Mention of commercial product names does not imply endorsement.

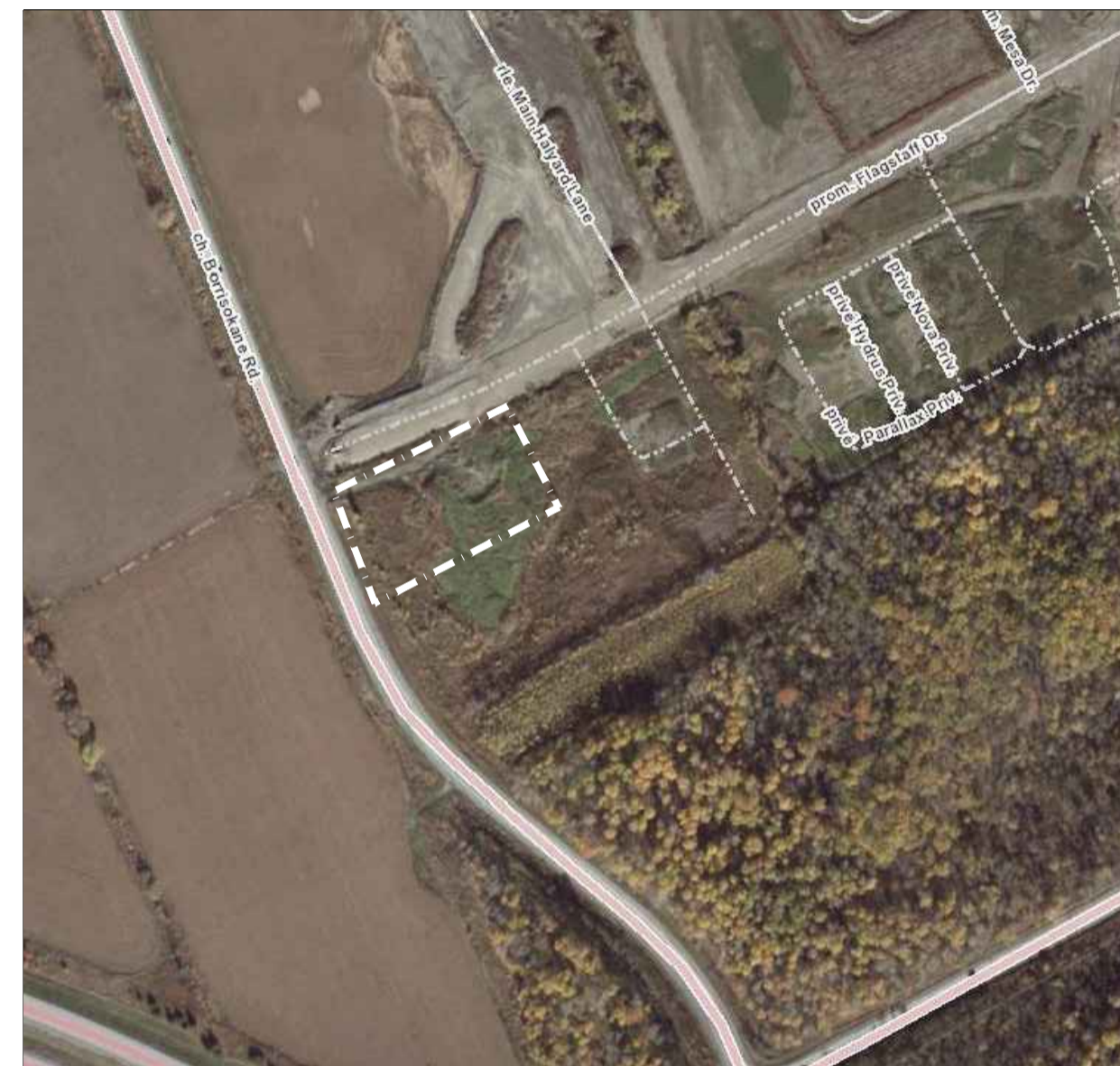
VerifiGlobal and the Verification Expert, Good Harbour Laboratories, provide the verification services solely on the basis of the information supplied by the applicant or vendor and assume no liability thereafter. The responsibility for the information supplied remains solely with the applicant or vendor and the liability for the purchase, installation, and operation (whether consequential or otherwise) is not transferred to any other party as a result of the verification.



**APPENDIX E**  
**Civil Engineering Drawings**

# HALO CAR WASH 3555 BORRISOKANE RD BARRHAVEN, ON

## REVISION 11



KEY PLAN (N.T.S.)

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CONSTRUCTION DETAIL PLAN	C904



# LRL

ENGINEERING | INGÉNIERIE

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HALO CAR WASH  
3555 BORRISOKANE RD, BARRHAVEN, ON  
REV.11 - RE-ISSUED FOR APPROVAL - JULY 07, 2023  
LRL PROJECT no: 210691



NOT AUTHENTIC UNLESS SIGNED AND DATED

D07-12-22-0085

#18788

GENERAL NOTES

- 1. ALL WORKS MATERIALS SHALL CONFIRM TO THE LAST REVISION OF THE STANDARDS AND SPECIFICATIONS FOR THE CITY OF OTTAWA, ONTARIO PROVINCIAL STANDARD DRAWINGS (OPSD) AND SPECIFICATIONS (OPSS), WHERE APPLICABLE. LOCAL UTILITY STANDARDS AND MINISTRY OF TRANSPORTATION STANDARDS WILL APPLY WHERE REQUIRED.

EROSION AND SEDIMENT CONTROL NOTES

GENERAL

THE CONTRACTOR SHALL IMPLEMENT BEST MANAGEMENT PRACTICES, TO PROVIDE FOR PROTECTION OF THE AREA DRAINAGE SYSTEM AND THE RECEIVING WATERCOURSE, DURING CONSTRUCTION ACTIVITIES. THE CONTRACTOR ACKNOWLEDGES THAT FAILURE TO IMPLEMENT APPROPRIATE EROSION AND SEDIMENT CONTROL MEASURES MAY BE SUBJECT TO PENALTIES IMPOSED BY ANY APPLICABLE REGULATORY AGENCY.

THE CONTRACTOR ACKNOWLEDGES THAT SURFACE EROSION AND SEDIMENT RUNOFF RESULTING FROM THEIR CONSTRUCTION OPERATIONS HAS POTENTIAL TO CAUSE A DETRIMENTAL IMPACT TO ANY DOWNSTREAM WATERCOURSE OR SEWER, AND THAT ALL CONSTRUCTION OPERATIONS THAT MAY IMPACT UPON WATER QUALITY SHALL BE CARRIED OUT IN MANNER THAT STRICTLY MEETS THE REQUIREMENT OF ALL APPLICABLE LEGISLATION AND REGULATIONS.

AS SUCH, THE CONTRACTOR SHALL BE RESPONSIBLE FOR CARRYING OUT THEIR OPERATIONS, AND SUPPLYING AND INSTALLING ANY APPROPRIATE CONTROL MEASURES, SO AS TO PREVENT SEDIMENT LADEN RUNOFF ENTERING ANY SEWER OR WATERCOURSE WITHIN OR DOWNSTREAM OF THE WORKING AREA.

THE CONTRACTOR ACKNOWLEDGES THAT NO ONE MEASURE IS LIKELY TO BE 100% EFFECTIVELY FOR EROSION PROTECTION AND CONTROLLING SEDIMENT RUNOFF AND DISCHARGES FROM THE SITE. THEREFORE, WHERE NECESSARY THE CONTRACTOR SHALL IMPLEMENT ADDITIONAL MEASURES ARRANGED IN SUCH MANNER AS TO MITIGATE SEDIMENT RELEASE FROM THE CONSTRUCTION OPERATIONS AND ACHIEVE SPECIFIC MAXIMUM PERMITTED CRITERIA WHERE APPLICABLE. SUGGESTED ON-SITE MEASURES MAY INCLUDE, BUT SHALL NOT BE LIMITED TO, THE FOLLOWING METHODS: SEDIMENT PONDS, FILTER BAGS, PUMP FILTERS, SETTLING TANKS, SILT FENCE, STRAW BALES, FILTER CLOTHS, CATCH BASIN FILTERS, CHECK DAMS AND/OR OTHER RECOGNIZED TECHNOLOGIES AND METHOD AVAILABLE AT THE TIME OF CONSTRUCTION. SPECIFIC MEASURES SHALL BE INSTALLED IN ACCORDANCE WITH REQUIREMENTS OF OPSS 577 WHERE APPROPRIATE, OR IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATIONS.

WHERE, IN THE OPINION OF THE CONTRACT ADMINISTRATOR OR REGULATORY AGENCY, THE INSTALLED CONTROL MEASURES FAIL TO PERFORM ADEQUATELY, THE CONTRACTOR SHALL SUPPLY AND INSTALL ADDITIONAL OR ALTERNATIVE MEASURES AS DIRECTED BY THE CONTRACT ADMINISTRATOR OR REGULATORY AGENCY. AS SUCH, THE CONTRACTOR SHALL HAVE ADDITIONAL CONTROL MATERIALS ON SITE AT ALL TIME WHICH ARE EASILY ACCESSIBLE AND MAY BE IMPLEMENTED BY HIM AT THE MOMENT'S NOTICE.

PRIOR TO COMMENCING WORK, THE CONTRACTOR SHALL SUBMIT TO THE CONTRACT ADMINISTRATOR SIX COPIES OF A DETAILED EROSION AND SEDIMENT CONTROL PLAN (ESCP). THE ESCP WILL CONSIST OF WRITTEN DESCRIPTION AND DETAILED DRAWINGS INDICATING THE ON-SITE ACTIVITIES AND MEASURES TO BE USED TO CONTROL EROSION AND SEDIMENT MOVEMENT FOR EACH STEP OF THE WORK.

CONTRACTOR'S RESPONSIBILITIES

THE CONTRACTOR SHALL ENSURE THAT ALL WORKERS, INCLUDING SUB-CONTRACTOR, IN THE WORKING AREA ARE AWARE OF THE IMPORTANCE OF THE EROSION AND SEDIMENT CONTROL MEASURES AND INFORMED OF THE CONSEQUENCES OF THE FAILURE TO COMPLY WITH THE REQUIREMENTS OF ALL REGULATORY AGENCIES.

THE CONTRACTOR SHALL PERIODICALLY, AND WHEN REQUESTED BY THE CONTRACT ADMINISTRATOR, CLEAN OUT ACCUMULATED SEDIMENT DEPOSITS AS REQUIRED AT THE SEDIMENT CONTROL DEVICES, INCLUDING THOSE DEPOSITS THAT MAY ORIGINATE FROM OUTSIDE THE CONSTRUCTION AREA. ACCUMULATED SEDIMENT SHALL BE REMOVED IN SUCH A MANNER THAT PREVENTS THE DEPOSITION OF THIS MATERIAL INTO THE SEWER WATERCOURSE AND AVOIDS DAMAGE TO CONTROL MEASURES. THE SEDIMENT SHALL BE REMOVED FROM THE SITE AT THE CONTRACTOR'S EXPENSE AND MANAGED IN COMPLIANCE WITH REQUIREMENTS FRO EXCESS EARTH MATERIAL, AS SPECIFIED ELSEWHERE IN THE CONTRACT.

THE CONTRACTOR SHALL IMMEDIATELY REPORT TO THE CONTRACT ADMINISTRATOR ANY ACCIDENTAL DISCHARGES OF SEDIMENT MATERIAL INTO EITHER THE WATERCOURSE OR THE STORM SEWER SYSTEM. FAILURE TO REPORT WILL BE CONSTITUTE A BREACH OF THIS SPECIFICATION AND THE CONTRACTOR MAY ALSO BE SUBJECT TO THE PENALTIES IMPOSED BY THE APPLICABLE REGULATORY AGENCY. APPROPRIATE RESPONSE MEASURES, INCLUDING ANY REPAIRS TO EXISTING CONTROL MEASURES OR THE IMPLEMENTATION OF ADDITIONAL CONTROL MEASURES, SHALL BE CARRIED OUT BY THE CONTRACTOR WITHOUT DELAY.

THE SEDIMENT CONTROL MEASURES SHALL ONLY BE REMOVED WHEN, IN THE OPINION OF THE CONTRACT ADMINISTRATOR, THE MEASURE OR MEASURES, IS NO LONGER REQUIRED. NO CONTROL MEASURE MAY BE PERMANENTLY REMOVED WITHOUT PRIOR AUTHORIZATION FROM THE CONTRACT ADMINISTRATOR. ALL SEDIMENT AND EROSION CONTROL MEASURES SHALL BE REMOVED IN A MANNER THAT AVOIDS THE ENTRY OF ANY EQUIPMENT, OTHER THAN HAND-HOLD EQUIPMENT, INTO ANY WATERCOURSE, AND PREVENTS THE RELEASE OF ANY SEDIMENT OR DEBRIS INTO ANY SEWER OR WATERCOURSE WITHIN OR DOWNSTREAM OF THE WORKING AREA. ALL ACCUMULATED SEDIMENT SHALL BE REMOVED FROM THE WORKING AREA AT THE CONTRACTOR'S EXPENSE AND MANAGED IN COMPLIANCE WITH THE REQUIREMENTS FOR EXCESS EARTH MATERIAL.

WHERE, IN THE OPINION OF EITHER THE CONTRACT ADMINISTRATOR OR A REGULATORY AGENCY, ANY OF THE TERMS SPECIFIED HEREIN HAVE NOT BEEN COMPLIED WITH OR PERFORMED IN A SUITABLE MANNER, OR THAT ALL THE CONTRACTOR ADMINISTRATOR OR A REGULATORY AGENCY HAS THE RIGHT TO IMMEDIATELY WITHDRAW ITS PERMISSION TO CONTINUE THE WORK BUT MAY REVEW ITS PERMISSION UPON BEING SATISFIED THAT THE DEFAULTS OR DEFICIENCIES IN THE PERFORMANCE OF THIS SPECIFICATION BY THE CONTRACTOR HAVE BEEN REMEDIED.

SPILL CONTROL NOTES

- 1. ALL CONSTRUCTION EQUIPMENT SHALL BE RE-FUELED, MAINTAINED, AND STORED NO LESS THAN 30 METRES FROM WATERCOURSE, STREAMS, CREEKS, WOODLOTS, AND ANY ENVIRONMENTALLY SENSITIVE AREAS, OR AS OTHERWISE SPECIFIED.

MUD MAT NOTES

- 1. THE GRANULAR MATERIAL WILL REQUIRE PERIODIC REPLACEMENT AS IT BECOMES CONTAMINATED BY VEHICLE TRAFFIC.

SITE GRADING NOTES

- 1. PRIOR TO THE COMMENCEMENT OF THE SITE GRADING WORKS, ALL SILTATION CONTROL DEVICES SHALL BE INSTALLED AND OPERATIONAL PER EROSION CONTROL PLAN.

ROADWORK SPECIFICATIONS

- 1. ROADWORK TO BE COMPLETED IN ACCORDANCE WITH GEOTECHNICAL REPORT, PREPARED BY LRL ASSOCIATES, DATED NOVEMBER 2020.

SANITARY, FOUNDATION DRAIN, STORM SEWER AND WATERMAIN NOTES

GENERAL

- 1. LASER ALIGNMENT CONTROL TO BE UTILIZED ON ALL SEWER INSTALLATIONS.

SANITARY

- 1. ALL SANITARY SEWER INSTALLATION SHALL CONFORM TO THE LATEST REVISIONS OF THE CITY OF OTTAWA AND THE ONTARIO PROVINCIAL STANDARD DRAWINGS (OPSD) AND SPECIFICATIONS (OPSS).

STORM

- 17. ALL REINFORCED CONCRETE STORM SEWER PIPE SHALL BE IN ACCORDANCE WITH CSA A257.2, OR LATEST AMENDMENT. ALL NON-REINFORCED CONCRETE STORM SEWER PIPE SHALL BE IN ACCORDANCE WITH CSA A257.1, OR LATEST AMENDMENT. PIPE SHALL BE JOINED WITH STD. RUBBER GASKETS AS PER CSA A257.2, OR LATEST AMENDMENT.

WATERMAIN

- 30. ALL WATERMAIN INSTALLATION SHALL CONFORM TO THE LATEST REVISIONS OF THE CITY OF OTTAWA AND THE ONTARIO PROVINCIAL STANDARD DRAWINGS (OPSD) AND SPECIFICATIONS (OPSS).

USE AND INTERPRETATION OF DRAWINGS

GENERAL CONDITIONS OF THE CONTRACT FOR CONSTRUCTION ARE PART OF THE CONTRACT DOCUMENTS AND DESCRIBE USE AND INTENT OF THE DRAWING. THE CONTRACT DOCUMENTS INCLUDE NOT ONLY THE DRAWINGS, BUT ALSO THE OWNER-CONTRACTOR AGREEMENTS, CONDITIONS OF THE CONTRACT, THE SPECIFICATIONS, ADDENDA, AND MODIFICATIONS ISSUED AFTER EXECUTION OF THE CONTRACT. THESE CONTRACT DOCUMENTS ARE COMPLEMENTARY, AND WHAT IS REQUIRED BY ANY ONE SHALL BE BINDING AS IF REQUIRED BY ALL. WORK NOT COMPLETELY DELINEATED HEREON SHALL BE CONSTRUCTED OF THE SAME MATERIALS AND DETAILED SIMILARLY AS WORK SHOWN MORE COMPLETELY ELSEWHERE IN THE CONTRACT DOCUMENTS.

BY USE OF THE DRAWINGS FOR CONSTRUCTION OF THE PROJECT, THE OWNER CONFIRMS THAT HE HAS REVIEWED AND APPROVED THE DRAWINGS. THE CONTRACTOR CONFIRMS THAT HE HAS VISITED THE SITE, FAMILIARIZED HIMSELF WITH THE LOCAL CONDITIONS, VERIFIED FIELD DIMENSIONS AND CORRELATED HIS OBSERVATIONS WITH THE REQUIREMENTS OF THE CONTRACT DOCUMENTS.

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IN ADDITION, THE CLIENT AGREES, TO THE FULLEST EXTENT PERMITTED BY LAW, TO INDEMNIFY AND HOLD HARMLESS LRL FROM ANY DAMAGES, LIABILITIES OR COST, INCLUDING REASONABLE ATTORNEY'S FEES AND COST OF DEFENSE, ARISING FROM SUCH CHANGES.

IN ADDITION, THE CLIENT AGREES TO INCLUDE IN ANY CONTRACTS FOR CONSTRUCTION APPROPRIATE LANGUAGE THAT PROHIBITS THE CONTRACTOR OR ANY SUBCONTRACTORS OF ANY TIER FROM MAKING ANY CHANGES OR MODIFICATIONS TO LRL'S CONSTRUCTION DOCUMENTS WITHOUT THE PRIOR WRITTEN APPROVAL OF LRL AND THAT FURTHER REQUIRES THE CONTRACTOR TO INDEMNIFY BOTH LRL AND THE CLIENT FROM ANY LIABILITY OR COST ARISING FROM SUCH CHANGES MADE WITHOUT SUCH PROPER AUTHORIZATION.

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SUBJECT FOR APPROVAL

Table with 4 columns: No., REVISIONS, BY, DATE. It lists various revision items from 01 to 11, including 'RE-ISSUED FOR APPROVAL', 'ISSUED FOR COMMITTEE OF ADJUSTMENT', 'REVISED FLOOR AREA FOR MV APPLICATION', and 'REVISIONS'.



NOT AUTHENTIC UNLESS SIGNED AND DATED



LRL

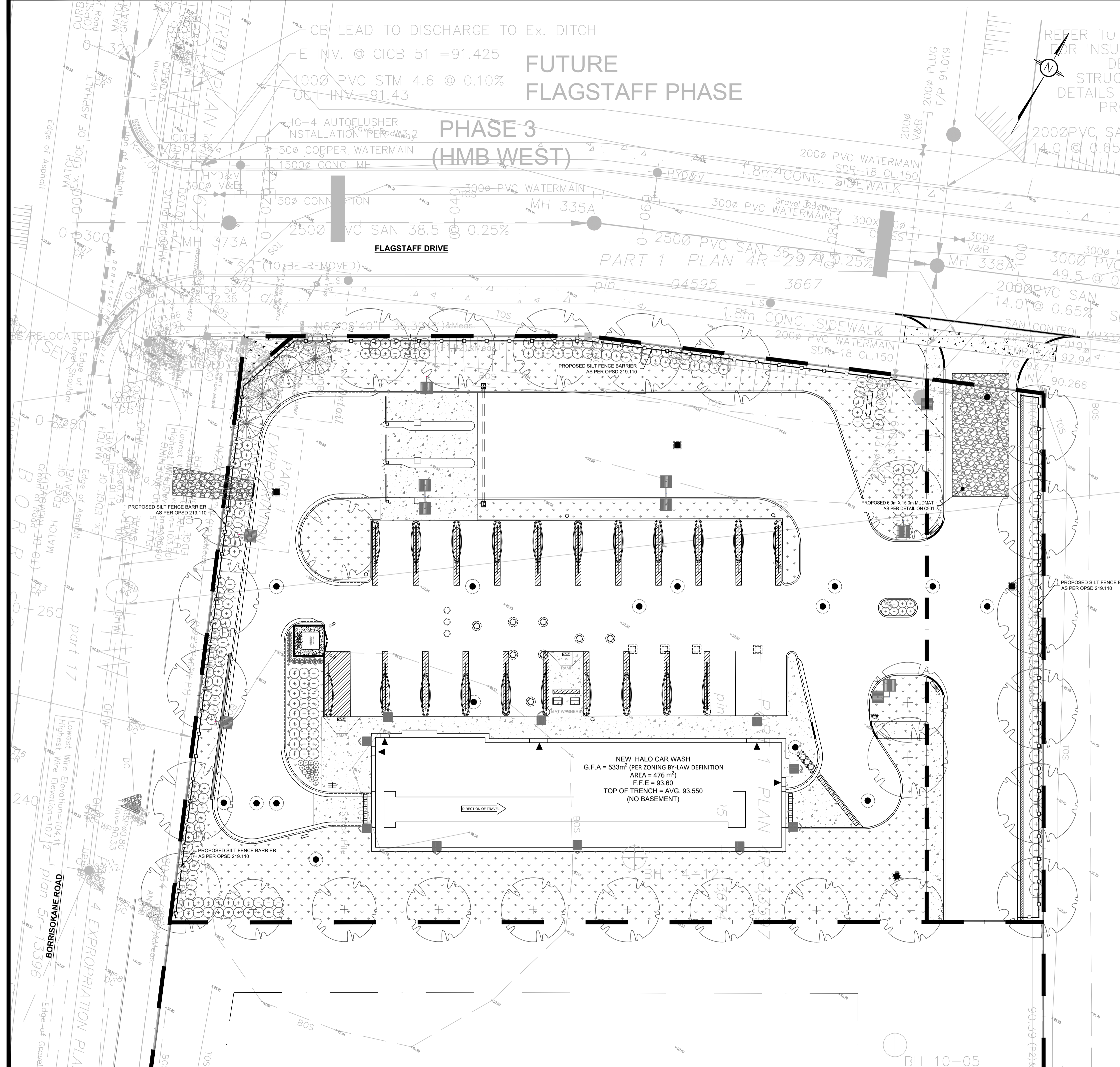
ENGINEERING | INGÉNIÉRIE

5430 Canotek Road | Ottawa, ON, K1J 9G2 www.lrl.ca | (613) 842-3434

Client information form for HALO CAR WASH INC. including fields for DESIGNED BY, DRAWN BY, APPROVED BY, PROJECT, DRAWING TITLE, and GENERAL NOTES.

PROJECT NO. 210691 DATE JANUARY 2022





**LEGEND:**

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SCALE: 1:200

**SUBJECT FOR APPROVAL**

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CLIENT: HALO CAR WASH INC.

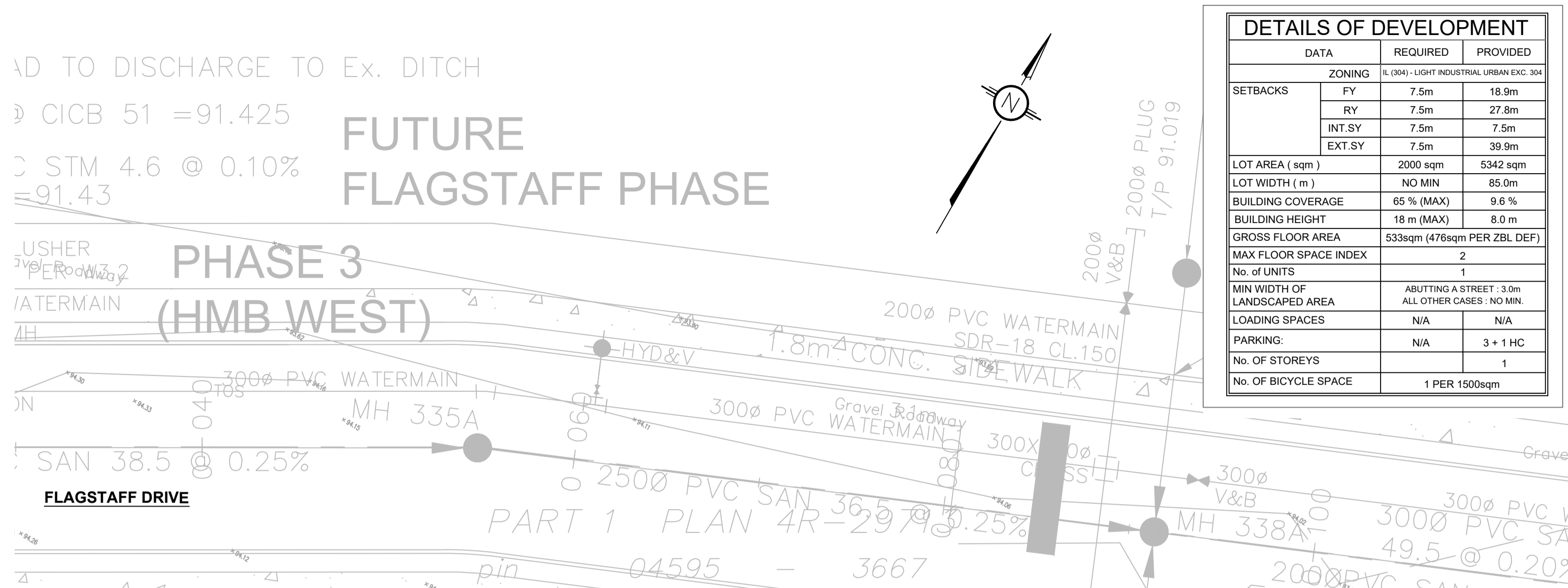
DESIGNED BY: M.L. / P.P.    DRAWN BY: M.L.    APPROVED BY: M.B.

PROJECT: HALO CAR WASH  
3555 BORRISOKANE RD  
BARRHAVEN, ON

DRAWING TITLE: EROSION AND SEDIMENT CONTROL PLAN

PROJECT NO: 210691    DATE: JANUARY 2022    **C101**

D07-12-22-0085



DETAILS OF DEVELOPMENT		
DATA	REQUIRED	PROVIDED
ZONING % (0.00) - LIGHT INDUSTRIAL URBAN EXC. 304		
SETBACKS	FY 7.5m	18.9m
	RY 7.5m	27.8m
	INT.SY 7.5m	7.5m
	EXT.SY 7.5m	39.9m
LOT AREA (sqm)	2000 sqm	5342 sqm
LOT WIDTH (m)	NO MIN	85.0m
BUILDING COVERAGE	65% (MAX)	9.6%
BUILDING HEIGHT	18 m (MAX)	8.0 m
GROSS FLOOR AREA	533sqm (476sqm PER ZBL DEF)	
MAX FLOOR SPACE INDEX	2	
No. of UNITS	1	
MIN WIDTH OF LANDSCAPED AREA	ABUTTING A STREET: 3.0m	ALL OTHER CASES: NO MIN.
LOADING SPACES	N/A	N/A
PARKING	N/A	3 + 1 HC
No. of STOREYS	1	
No. of BICYCLE SPACE	1 PER 1500sqm	

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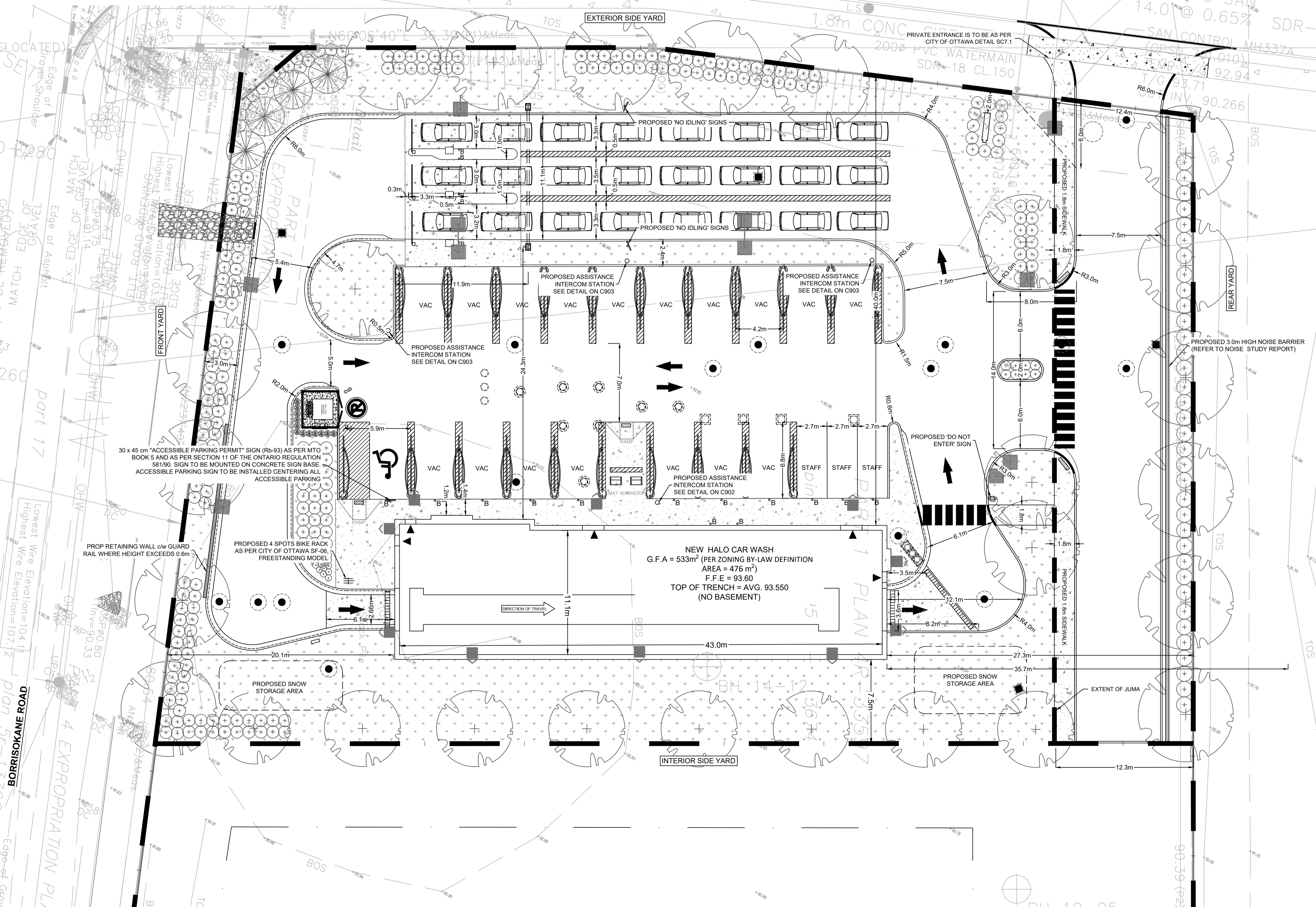
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SCALE: 1:200



### TOPOGRAPHIC INFORMATION

TOPOGRAPHIC INFORMATION PROVIDED BY ANNIS, O'SULLIVAN, VOLLEBEKK LTD. PART OF LOT 11, CONCESSION 3 (RIDEAU FRONT), GEOGRAPHIC TOWNSHIP OF NEPEAN, CITY OF OTTAWA DATED JANUARY 21st 2022

### ELEVATION NOTES

- Elevations shown are geodetic and are referred to the CGVD28 geodetic datum.
- It is the responsibility of the user of this information to verify that the job benchmark has not been altered or disturbed and that its relative elevation and description agrees with the information shown on this drawing.

### UTILITY NOTES

- This drawing cannot be accepted as acknowledging all of the utilities and it will be the responsibility of the user to contact the respective utility authorities for confirmation.
- Only visible surface utilities were located.
- A field location of underground plant by the pertinent utility authority is mandatory before any work involving breaking ground, probing, excavating etc.

Bearings are grid, derived from Can-Net 2016 Real Time Network GPS observations referenced to Specified Control Points 01919761338 and 01919871649, MTM Zone 9 (76°30' West Longitude) NAD-83 (original).

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CLIENT: **HALO CAR WASH INC.**

DESIGNED BY: M.L. / P.P.      DRAWN BY: M.L.      APPROVED BY: M.B.

PROJECT: **HALO CAR WASH  
3555 BORRISOKANE RD  
BARRHAVEN, ON**

DRAWING TITLE: **SITE DEVELOPMENT PLAN**

PROJECT NO: 210691      DATE: JANUARY 2022

**C201**

**PAVEMENT STRUCTURE**

COURSE	MATERIAL	THICKNESS (mm)	
		AUTOMOBILE PARKING	TRUCK ROUTE (HEAVY TRAFFIC)
SURFACE	HL 3 A/C (PG 58-28)	50	40
BINDER	HL 8 A/C (PG 58-28)	-	50
BASECOURSE	OPSS GRANULAR "A"	150	150
SUBBASE	OPSS GRANULAR "B" TYPE II	350	450

NOTE: IN PREPARATION FOR PAVEMENT CONSTRUCTION AT THIS SITE, ANY SURFICIAL OR NEAR SURFACE/SUBGRADE LEVEL TOPSOIL AND ANY SOFT, WET OR DELETERIOUS MATERIALS SHOULD BE REMOVED FROM THE PROPOSED PAVED AREAS. THE EXPOSED SUBGRADE SHOULD BE INSPECTED AND APPROVED BY GEOTECHNICAL PERSONNEL, AND ANY SOFT AREAS EVIDENT SHOULD BE SUBCAVATED AND REPLACED WITH SUITABLE EARTH BORROW APPROVED BY THE GEOTECHNICAL ENGINEER. THE SUBGRADE SHOULD BE SHAPED AND CROWNED TO PROMOTE DRAINAGE OF THE SITE DRAINAGE STRUCTURES. FOLLOWING APPROVAL OF THE PREPARATION OF THE SUBGRADE, THE PAVEMENT GRANULARS MAY BE PLACED. REFER TO LATEST GEOTECHNICAL REPORT PREPARED BY LRL ENGINEERING LTD.

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SCALE: 1:200

**SUBJECT FOR APPROVAL**

No.	REVISIONS	BY	DATE
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ENGINEERING | INGENIERIE  
5430 Canotek Road | Ottawa, ON, K1J 9G2  
www.lrl.ca | (613) 842-3434

CLIENT: HALO CAR WASH INC.

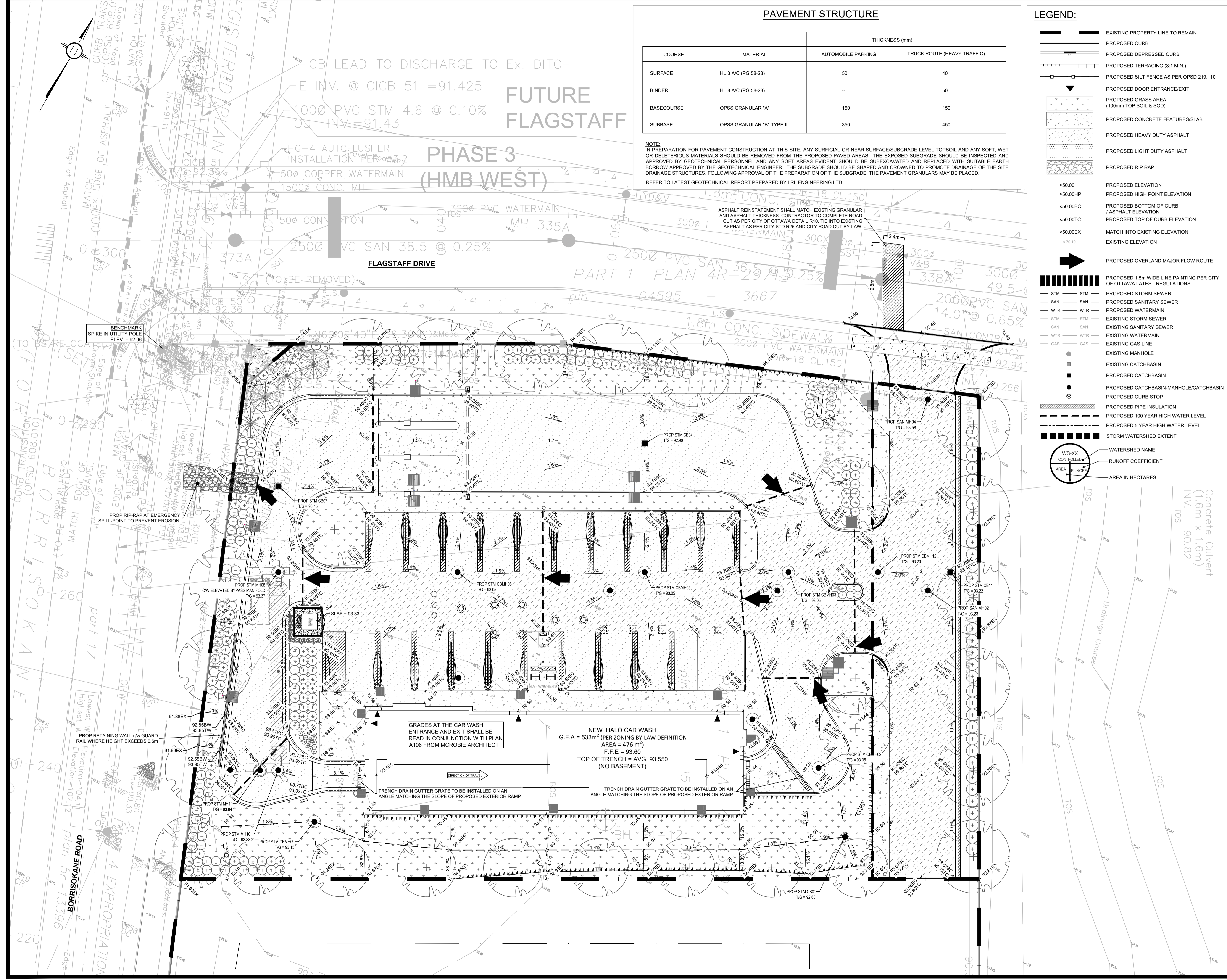
DESIGNED BY: M.L. / P.P. DRAWN BY: M.L. APPROVED BY: M.B.

PROJECT: HALO CAR WASH  
3555 BORRISOKANE RD  
BARRHAVEN, ON

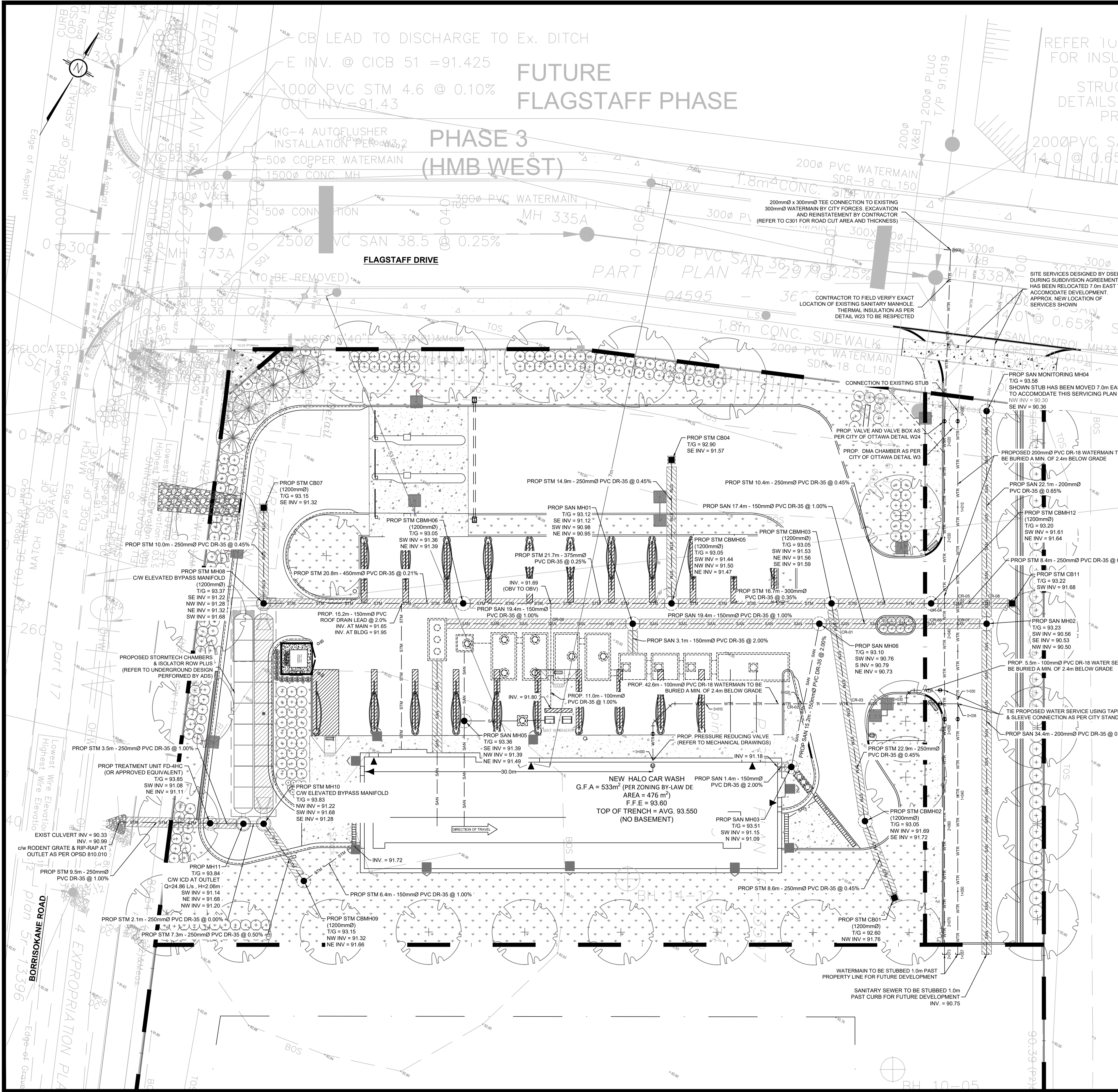
DRAWING TITLE: GRADING AND DRAINAGE PLAN

PROJECT NO. 210691  
DATE: JANUARY 2022

**C301**



D07-12-22-0085



### LEGEND:

- EXISTING PROPERTY LINE TO REMAIN
- PROPOSED CURB
- PROPOSED DEPRESSED CURB
- PROPOSED TERRACING (3:1 MIN)
- PROPOSED SILT FENCE AS PER OPSD 219.110
- PROPOSED DOOR ENTRANCE/EXIST
- PROPOSED GRASS AREA (100mm TOP SOIL & SOD)
- PROPOSED CONCRETE FEATURES/SLAB
- PROPOSED HEAVY DUTY ASPHALT
- PROPOSED LIGHT DUTY ASPHALT
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- PROPOSED ELEVATION
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- PROPOSED OVERLAND MAJOR FLOW ROUTE
- PROPOSED 1.5m WIDE LINE PAINTING PER CITY OF OTTAWA LATEST REGULATIONS
- PROPOSED STORM SEWER
- PROPOSED SANITARY SEWER
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- PROPOSED CURB STOP
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- PROPOSED 5 YEAR HIGH WATER LEVEL
- STORM WATERSHED EXTENT
- WATERSHED NAME
- RUNOFF COEFFICIENT
- AREA IN HECTARES

**NOTE:**  
CLAY DYKES ARE TO BE INSTALLED DOWNSTREAM FROM EACH OF THE MANHOLES/CATCH BASINS. THESE DYKES SHOULD EXTEND FROM THE BASE OF THE SERVICE TRENCH TO THE SUBGRADE LEVEL, HAVING MIN. WIDTH OF 1.0m. REFER TO GEOTECHNICAL REPORT FOR FURTHER DETAILS.

**Crossing Table**

Crossing #	WM	STM	SAN	Depth Separation (m)
CR-01	N/A	91.74 (inv.)	90.87 (obv.)	0.87
CR-02	91.63 (inv.)	N/A	91.11 (obv.)	0.52
CR-03	90.92 (obv.)	91.77 (inv.)	N/A	0.85
CR-04	91.04 (obv.)	91.79 (inv.)	N/A	0.75
CR-05	91.03 (obv.)	91.79 (inv.)	N/A	0.76
CR-06	91.27 (inv.)	N/A	90.75 (obv.)	0.52
CR-07	91.28 (inv.)	N/A	90.74 (obv.)	0.54
CR-08	N/A	91.81 (inv.)	90.64 (obv.)	1.17
CR-09	N/A	91.87 (inv.)	91.22 (obv.)	0.65

WM crossing above sewer per City STD W2.2  
WM crossing below sewer per City STD W25

**Watermain Table**

Description	Chainage	Finish Grade	Obvert of Watermain	Cover (m)
100mm Water Service	0+000	93.41	91.01	2.40
45° Bend	0+004	93.34	90.94	2.40
45° Bend	0+007	93.27	90.87	2.40
100mm Water Service	0+010	93.32	90.92	2.40
100mm Water Service	0+020	93.25	91.63	1.62
100mm Water Service	0+030	93.37	90.97	2.40
Tee	0+036	93.05	90.65	2.40
200mm Watermain	1+000	93.56	91.16	2.40
200mm Watermain	1+010	93.35	90.95	2.40
200mm Watermain	1+020	93.17	90.77	2.40
200mm Watermain	1+030	93.05	90.65	2.40
Tee	1+031	93.04	90.64	2.40
200mm Watermain	1+040	93.02	90.62	2.40
200mm Watermain	1+050	93.15	90.75	2.40
200mm Watermain	1+057	92.75	90.35	2.40
200mm Watermain	2+000	94.02	91.62	2.40
200mm Watermain	2+010	93.60	91.20	2.40
200mm Watermain	2+020	93.50	91.10	2.40
200mm Watermain	2+030	93.30	90.90	2.40
200mm Watermain	2+040	93.15	90.75	1.68
200mm Watermain	2+046	93.10	90.70	2.40
200mm Watermain	2+050	93.05	90.65	2.40
200mm Watermain	2+060	93.10	90.70	2.40
200mm Watermain	2+070	93.25	90.85	2.40
200mm Watermain	2+073	92.75	90.35	2.40

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www.lrl.ca | (613) 842-3434

CLIENT: **HALO CAR WASH INC.**

DESIGNED BY: M.L. / P.P. DRAWN BY: M.L. APPROVED BY: M.B.

PROJECT: **HALO CAR WASH  
3555 BORRISOKANE RD  
BARRHAVEN, ON**

DRAWING TITLE: **SERVICING PLAN**

PROJECT NO: **210691**

DATE: **JANUARY 2022**

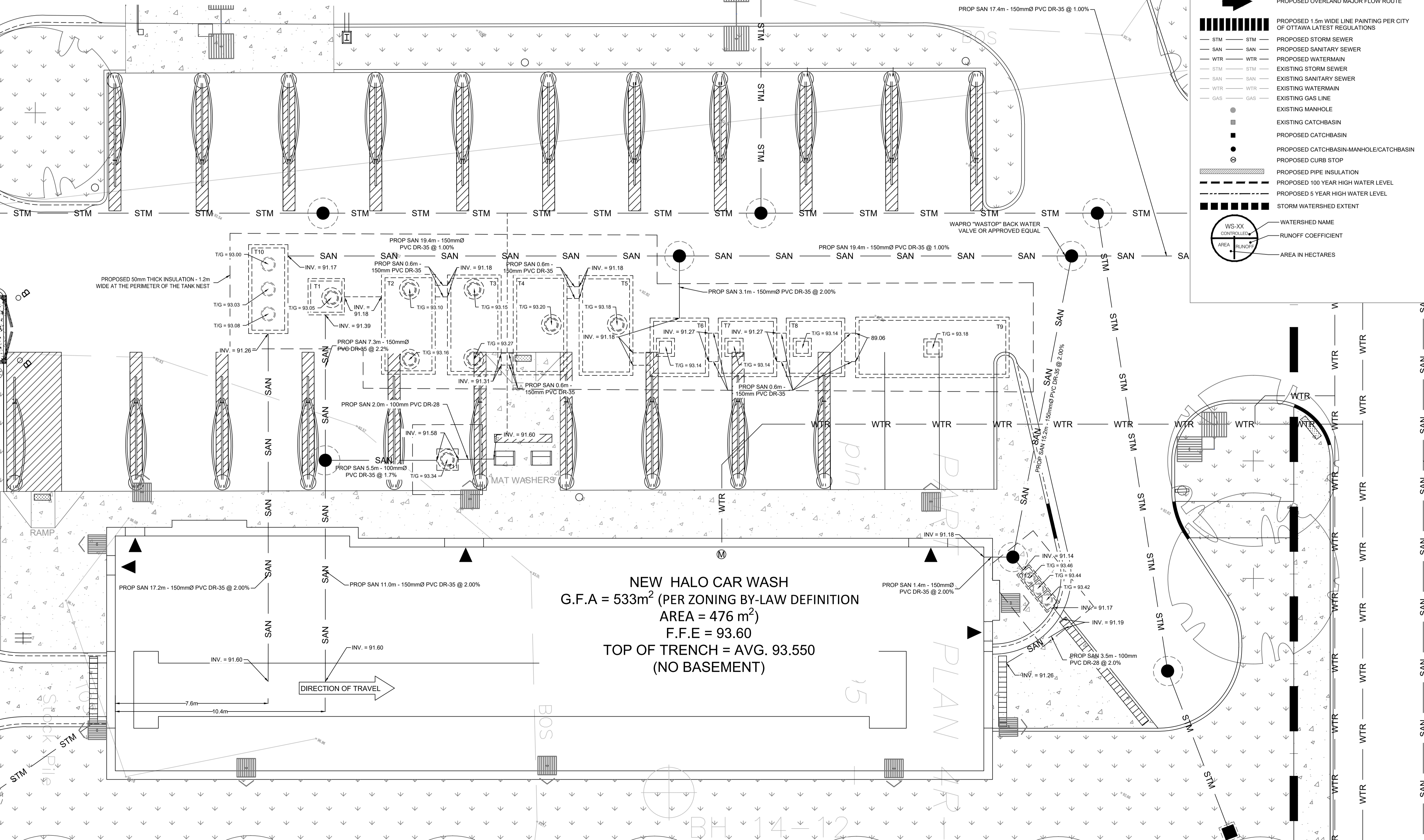
**C401**

#18788

# List of Underground Tanks

Water Reclamation Tanks			
For Validation	Tank ID	Tank Name	Model
	T1	Wilkinson Sand Tank	Wilkinson Model H4H
	T2	Wilkinson Settling Tank	Wilkinson Model H22.2H
	T3	Wilkinson Settling Tank	Wilkinson Model H22.2H
	T4	Wilkinson Settling Tank	Wilkinson Model H22.2H
	T5	Wilkinson Settling Tank	Wilkinson Model H22.2H
	T6	Wilkinson Aeration Tank	Wilkinson Model 2.5M
	T7	Wilkinson Clean Water Tank	Wilkinson Model 2.5M
	T8	Wilkinson Clarifier Tank	Wilkinson Model 2.5M
	T9	Wilkinson Biological Tank	Wilkinson Model H50.1S
Sediment Trap and other tanks on site			
	T10	Wilkinson Oil Grit Separator	Wilkinson Model 1075
	T11	Wilkinson Mat Washer Grit Tank	Wilkinson Model H1.355
	T12	Wilkinson Oil Interceptor	Wilkinson Model 230

NOTE: FOR ADDITIONAL INFORMATION, REFER TO WATER RECLAMATION SYSTEM DESIGN BY AQUA BIO. ALL THE PROPOSED UNDERGROUND WILKINSON TANKS TO BE TRAFFIC RATED AND TO BE PROPERLY INSTALLED AS PER WILKINSON INSTALLATIONS GUIDELINES.



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DESIGNED BY: M.L. / P.P. DRAWN BY: M.L. APPROVED BY: M.B.

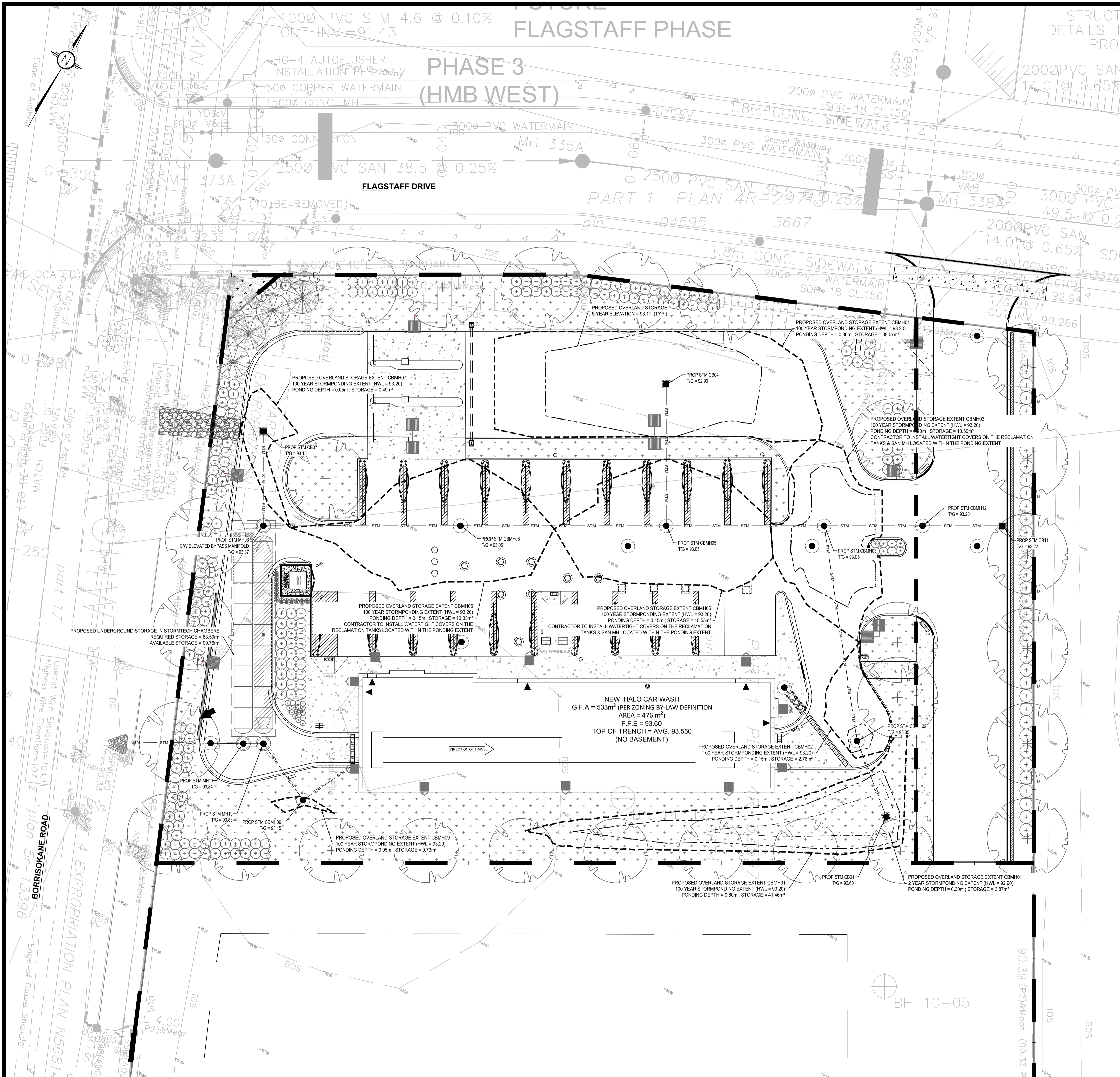
PROJECT: HALO CAR WASH  
3555 BORRISOKANE RD  
BARRHAVEN, ON

DRAWING TITLE: CAR WASH WASTEWATER TREATMENT & RECLAMATION SYSTEM

PROJECT NO: 210691 DATE: JANUARY 2022

**C402**





**LEGEND:**

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- AREA IN HECTARES

**USE AND INTERPRETATION OF DRAWINGS**

GENERAL CONDITIONS OF THE CONTRACT FOR CONSTRUCTION ARE PART OF THE CONTRACT DOCUMENTS AND DESCRIBE THE SCOPE AND INTENT OF THE DRAWINGS. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL NECESSARY PERMITS AND APPROVALS FROM THE LOCAL AUTHORITY. THE CONTRACTOR SHALL BE RESPONSIBLE FOR VERIFYING THE ACCURACY OF ALL INFORMATION PROVIDED BY THE CLIENT AND FOR OBTAINING ALL NECESSARY PERMITS AND APPROVALS FROM THE LOCAL AUTHORITY. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL NECESSARY PERMITS AND APPROVALS FROM THE LOCAL AUTHORITY. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL NECESSARY PERMITS AND APPROVALS FROM THE LOCAL AUTHORITY.

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THESE DRAWINGS ILLUSTRATE THE WORK TO BE DONE. THE ENGINEER IS NOT RESPONSIBLE FOR THE MANS, METHODS, TECHNIQUES, SEQUENCES, AND PROCEDURES USED TO DO THE WORK, OR THE SAFETY ASPECTS OF CONSTRUCTION, AND NOTHING ON THESE DRAWINGS EXPRESSED OR IMPLIED CHANGES THIS CONDITION. CONTRACTOR SHALL DETERMINE ALL CONDITIONS AT THE SITE AND SHALL BE RESPONSIBLE FOR KNOWING HOW THEY AFFECT THE WORK. SUBMITTAL OF A BID TO PERFORM THIS WORK IS ACKNOWLEDGEMENT OF THE RESPONSIBILITIES, AND THAT THEY HAVE BEEN FULLY CONSIDERED IN PLANNING OF THE WORK AND THE BIDDING. NO CLAIMS FOR EXTRA CHARGES DUE TO THESE CONDITIONS WILL BE FORTHCOMING.

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CONTRACTOR TO VERIFY ALL DIMENSIONS AND NOTIFY THE ENGINEER OF ANY DISCREPANCIES BEFORE WORK COMMENCES. DO NOT SCALE DRAWINGS.

**SUBJECT FOR APPROVAL**

No.	REVISIONS	BY	DATE
11	RE-ISSUED FOR APPROVAL	M.L.	07 JULY 2023
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**LRL**  
ENGINEERING | INGENIERIE  
5430 Canotek Road | Ottawa, ON, K1J 9G2  
www.lrl.ca | (613) 842-3434

CLIENT: HALO CAR WASH INC.

DESIGNED BY: M.L. / P.P.      DRAWN BY: M.L.      APPROVED BY: M.B.

PROJECT: HALO CAR WASH  
3555 BORRISOKANE RD  
BARRHAVEN, ON

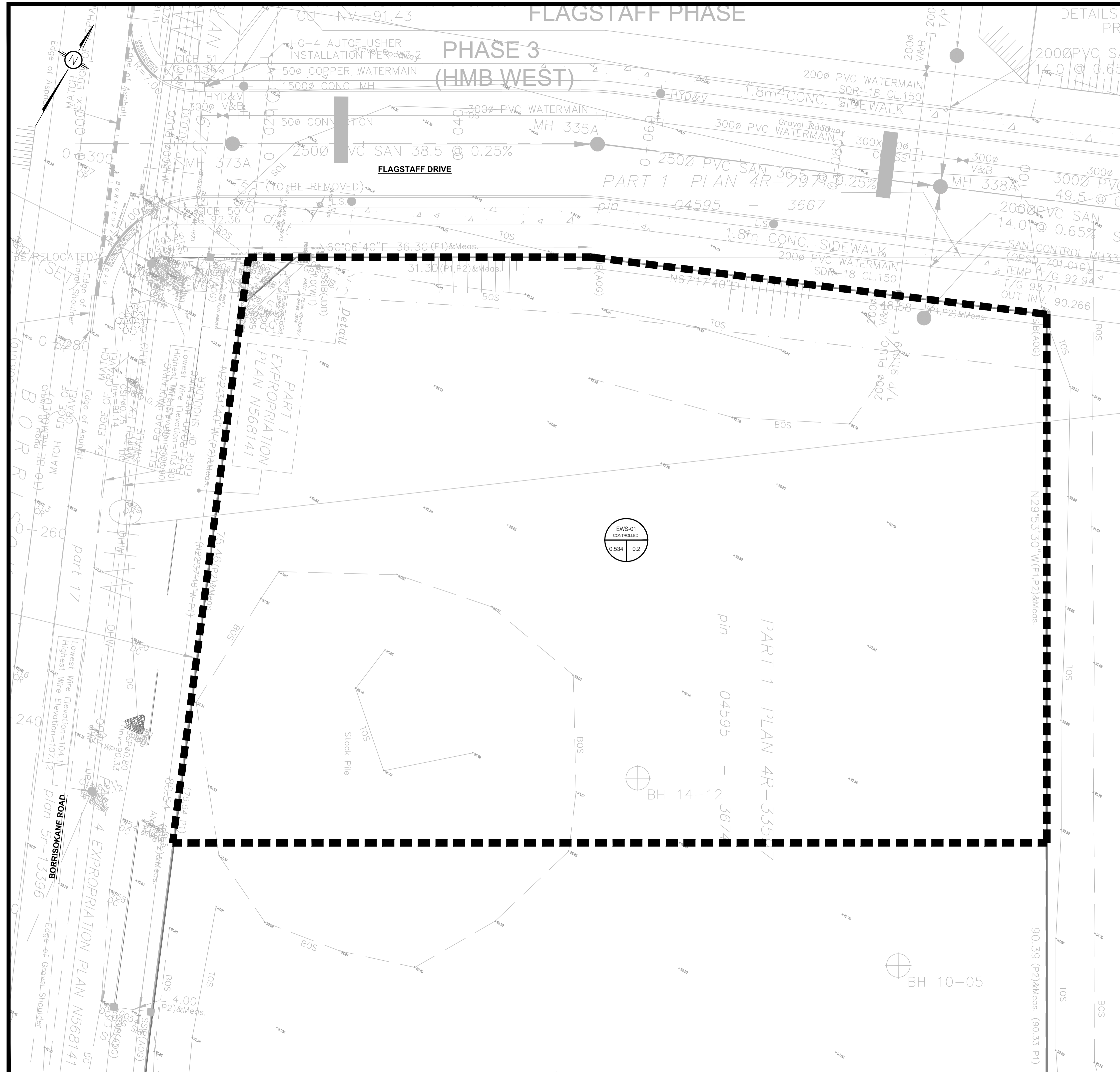
DRAWING TITLE: STORMWATER MANAGEMENT PLAN

PROJECT NO: 210691

DATE: JANUARY 2022

**C601**

D07-12-22-0085



**LEGEND:**

- EXISTING PROPERTY LINE TO REMAIN
- PROPOSED CURB
- PROPOSED DEPRESSED CURB
- PROPOSED TERRACING (3:1 MIN.)
- PROPOSED SILT FENCE AS PER OPSD 219.110
- PROPOSED DOOR ENTRANCE/EXIST
- PROPOSED GRASS AREA (100mm TOP SOIL & SOD)
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- PROPOSED RIP RAP
- PROPOSED ELEVATION
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- EXISTING WATERMAIN
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- EXISTING MANHOLE
- EXISTING CATCHBASIN
- PROPOSED CATCHBASIN
- PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN
- PROPOSED CURB STOP
- PROPOSED PIPE INSULATION
- PROPOSED 100 YEAR HIGH WATER LEVEL
- PROPOSED 5 YEAR HIGH WATER LEVEL
- STORM WATERSHED EXTENT

**Watershed Name:** WS-XX CONTROLLED

**Runoff Coefficient:** AREA RUNOFF

**Area in Hectares:** AREA IN HECTARES

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SCALE: 1:200

**SUBJECT FOR APPROVAL**

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www.lrl.ca | (613) 842-3434

CLIENT: **HALO CAR WASH INC.**

DESIGNED BY: M.L. / P.P.    DRAWN BY: M.L.    APPROVED BY: M.B.

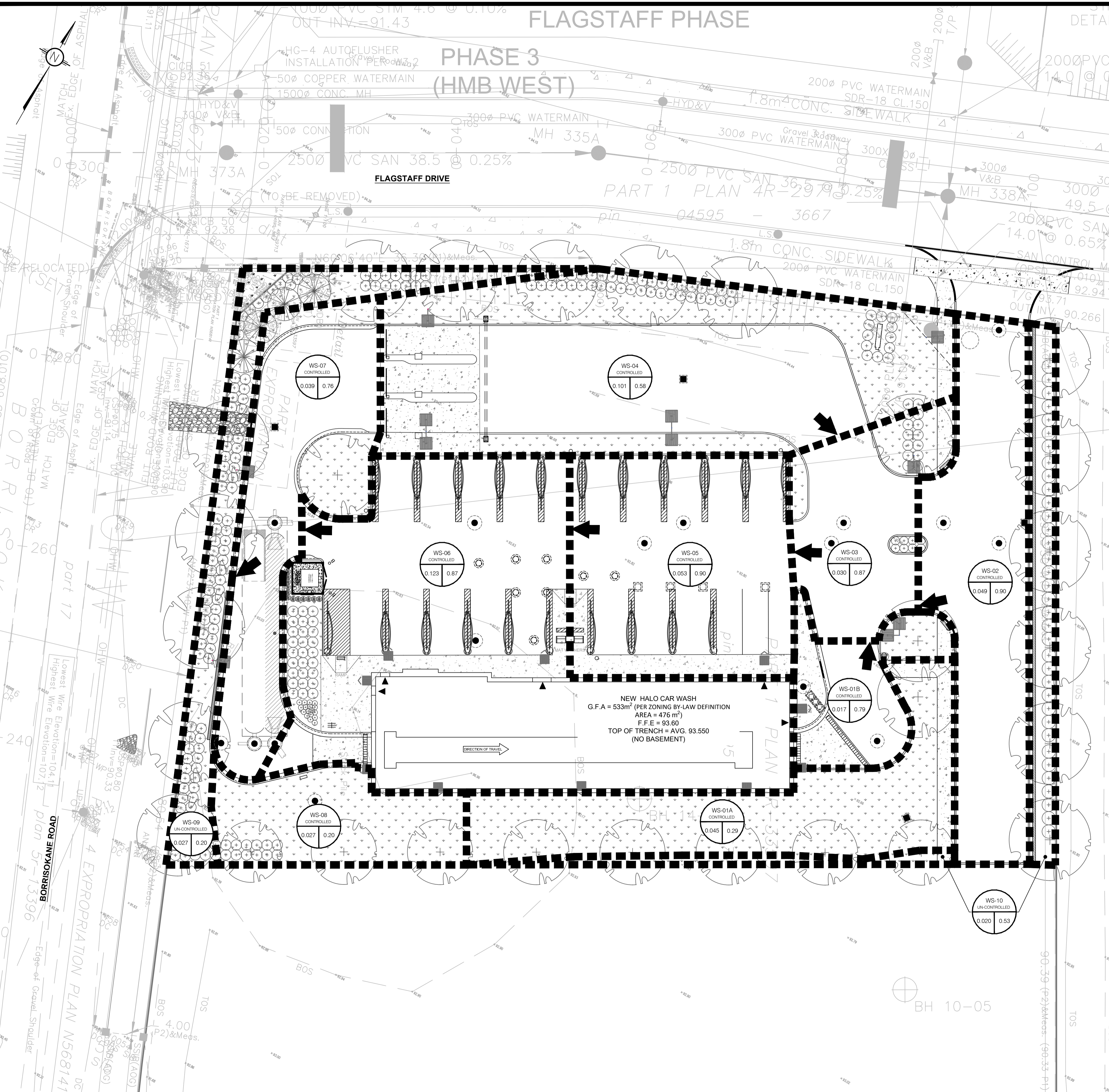
PROJECT: **HALO CAR WASH  
3555 BORRISOKANE RD  
BARRHAVEN, ON**

DRAWING TITLE: **PRE-DEVELOPMENT  
WATERSHED PLAN**

PROJECT NO: 210691    DATE: JANUARY 2022

**C701**

#18788



**LEGEND:**

- EXISTING PROPERTY LINE TO REMAIN
- PROPOSED CURB
- PROPOSED DEPRESSED CURB
- PROPOSED TERRACING (3:1 MIN.)
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- PROPOSED CATCHBASIN
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**SUBJECT FOR APPROVAL**

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CLIENT  
**HALO CAR WASH INC.**

DESIGNED BY: M.L. / P.P. DRAWN BY: M.L. APPROVED BY: M.B.

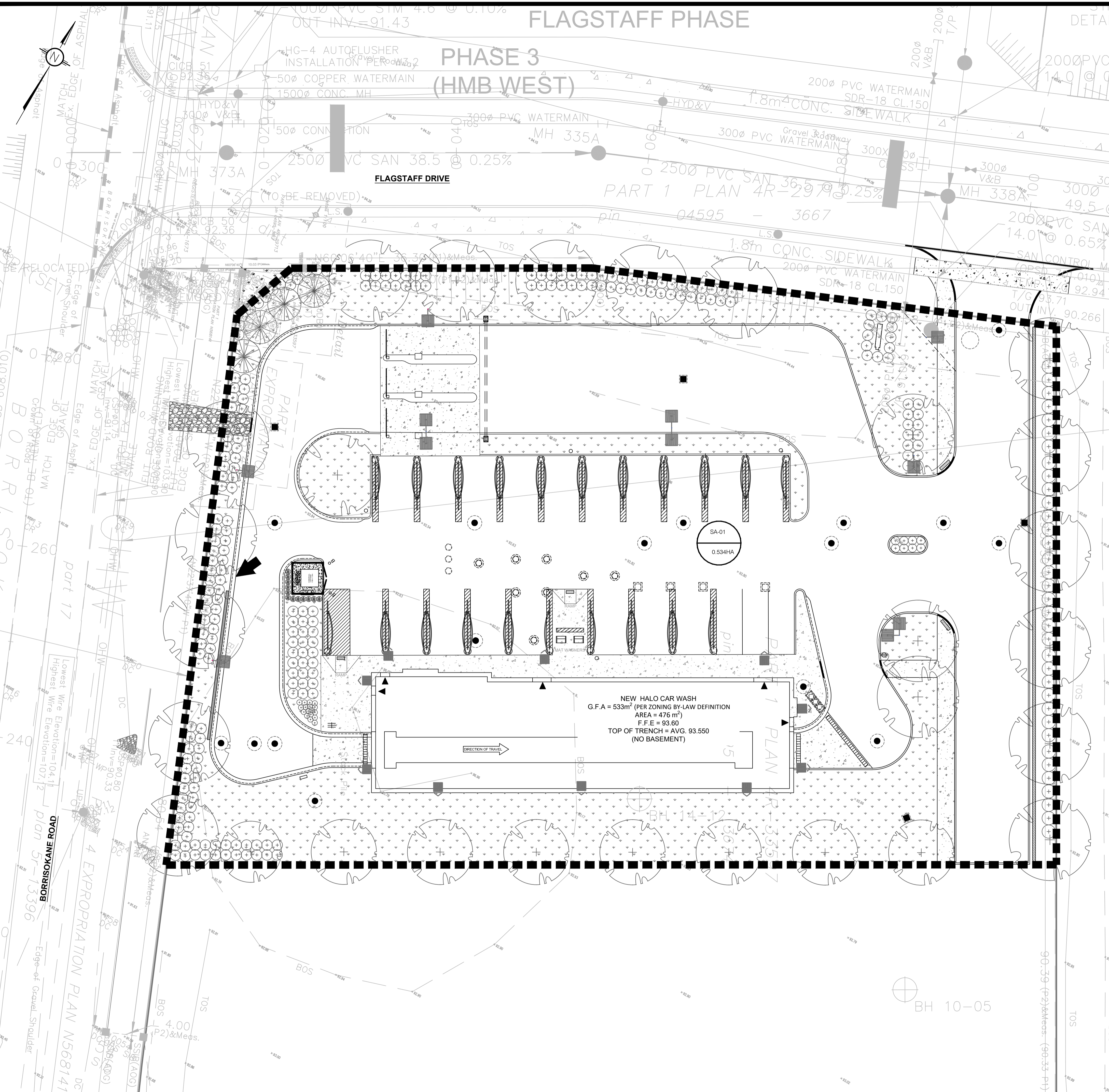
PROJECT  
**HALO CAR WASH  
3555 BORRISOKANE RD  
BARRHAVEN, ON**

DRAWING TITLE  
**POST-DEVELOPMENT  
WATERSHED PLAN**

PROJECT NO.  
**210691**

DATE  
**JANUARY 2022**

**C702**



**LEGEND:**

- EXISTING PROPERTY LINE TO REMAIN
- PROPOSED CURB
- PROPOSED DEPRESSED CURB
- PROPOSED TERRACING (3:1 MIN.)
- PROPOSED SILT FENCE AS PER OPSD 219.110
- PROPOSED DOOR ENTRANCE/EXIST
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03	REVISED FLOOR AREA FOR MV. APPLICATION	P.P.	13 JULY 2022
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01	ISSUED FOR APPROVAL	M.L.	22 APR 2022

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**LRL**  
ENGINEERING | INGENIERIE  
5430 Canotek Road | Ottawa, ON, K1J 9G2  
www.lrl.ca | (613) 842-3434

CLIENT  
**HALO CAR WASH INC.**

DESIGNED BY: M.L. / P.P.    DRAWN BY: M.L.    APPROVED BY: M.B.

PROJECT  
**HALO CAR WASH  
3555 BORRISOKANE RD  
BARRHAVEN, ON**

DRAWING TITLE  
**SANITARY DRAINAGE AREA**

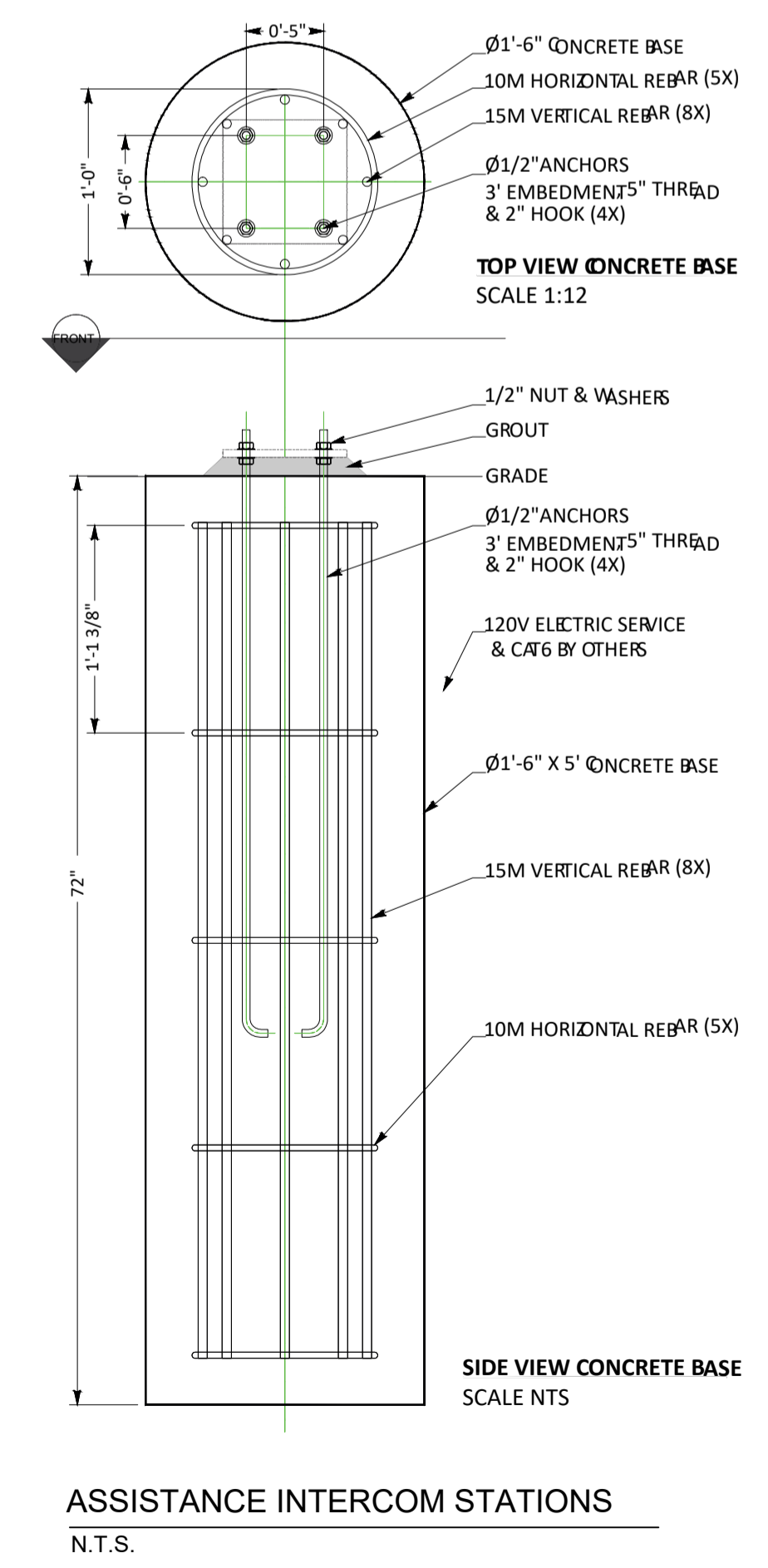
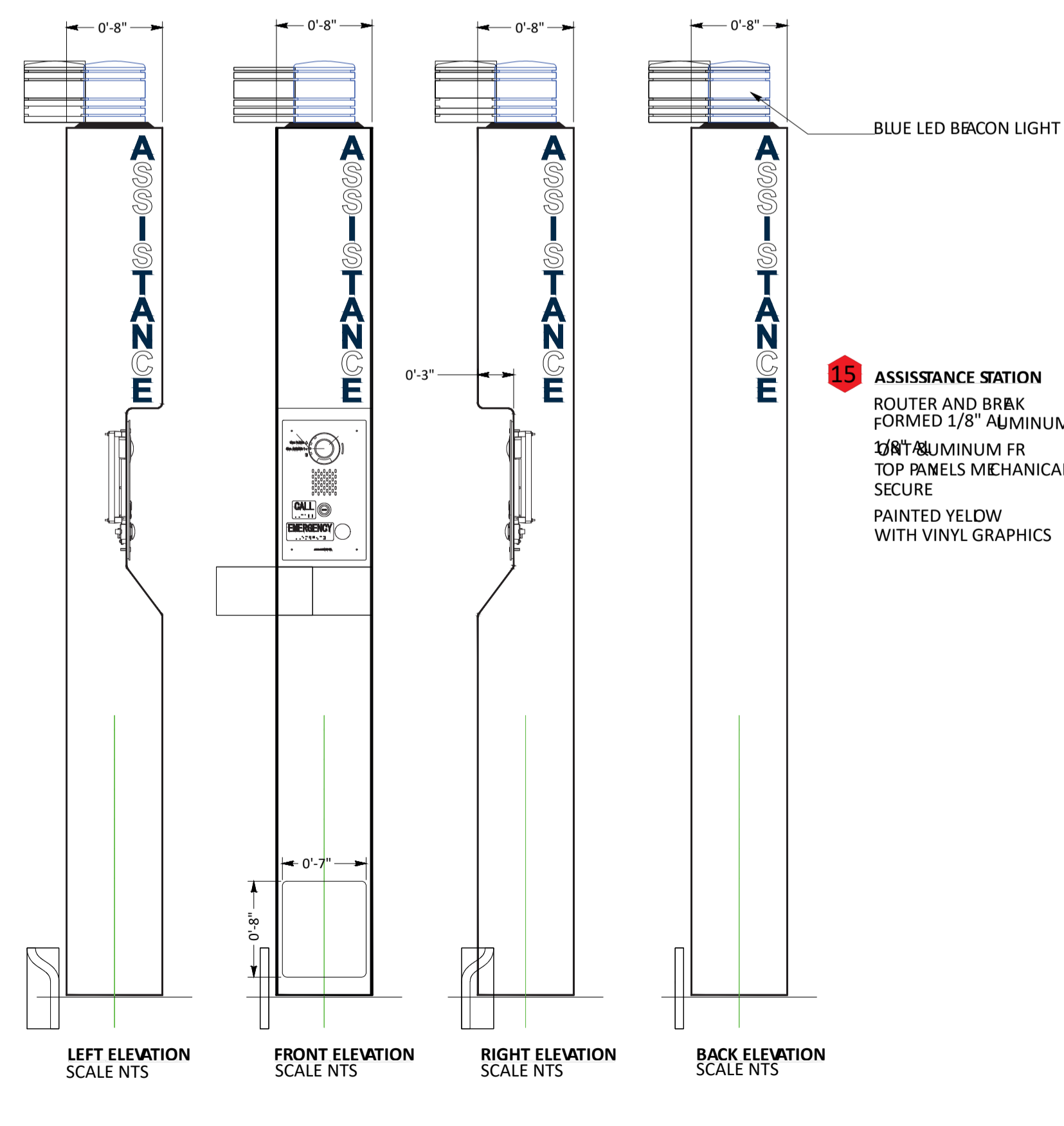
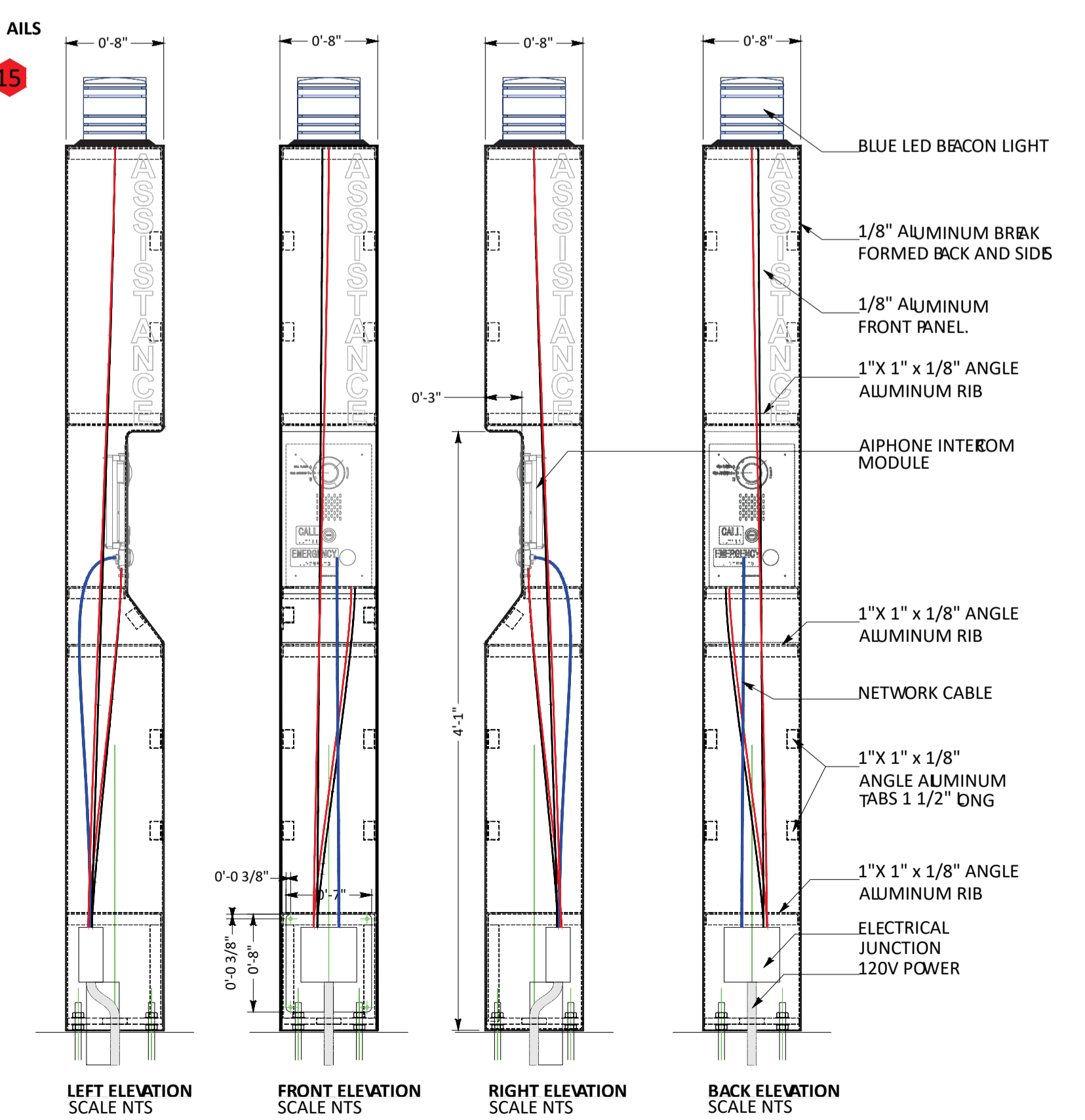
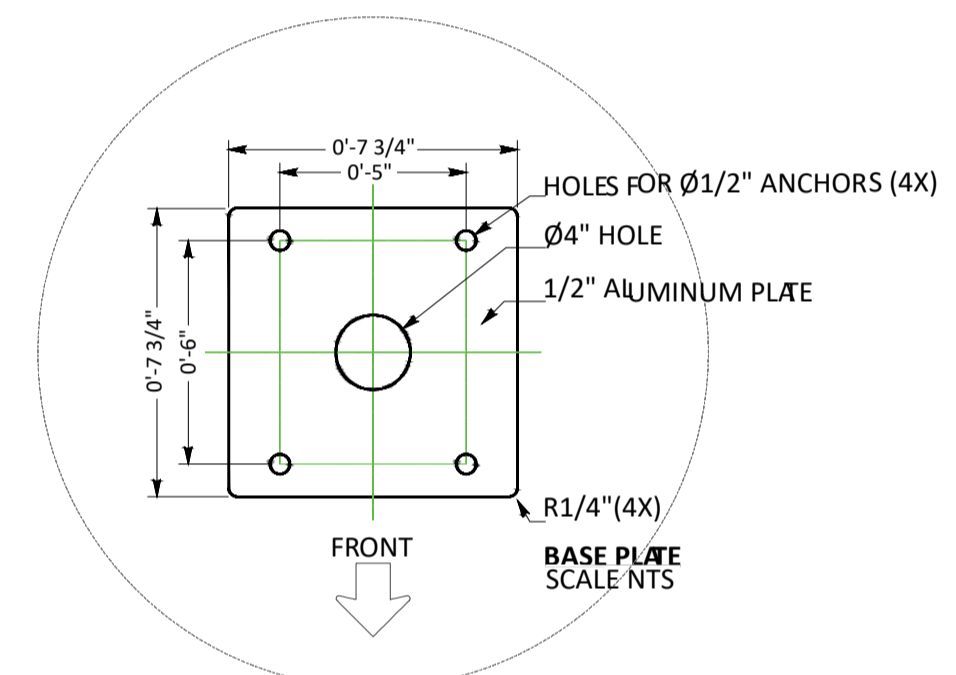
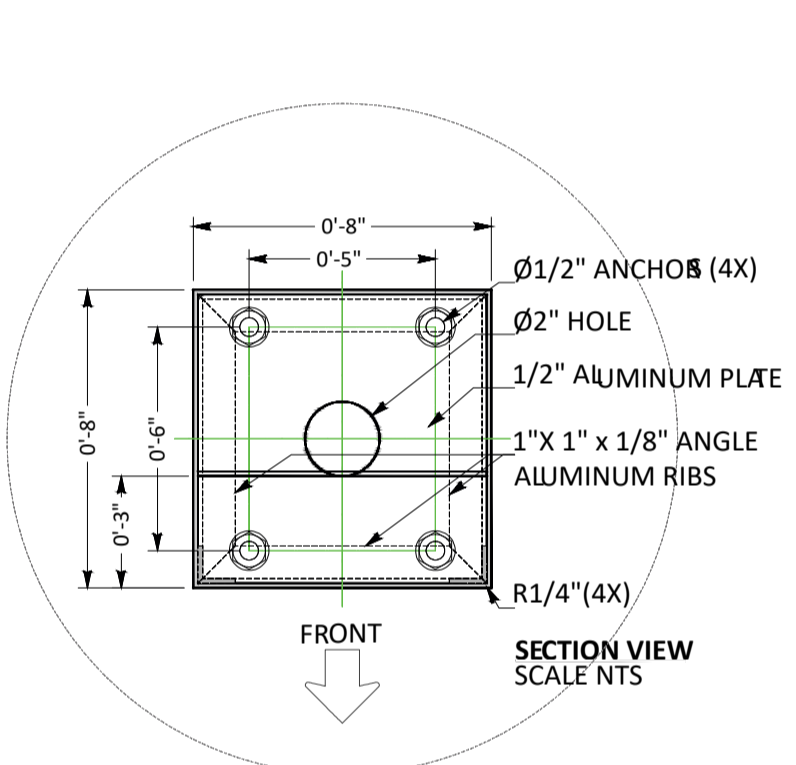
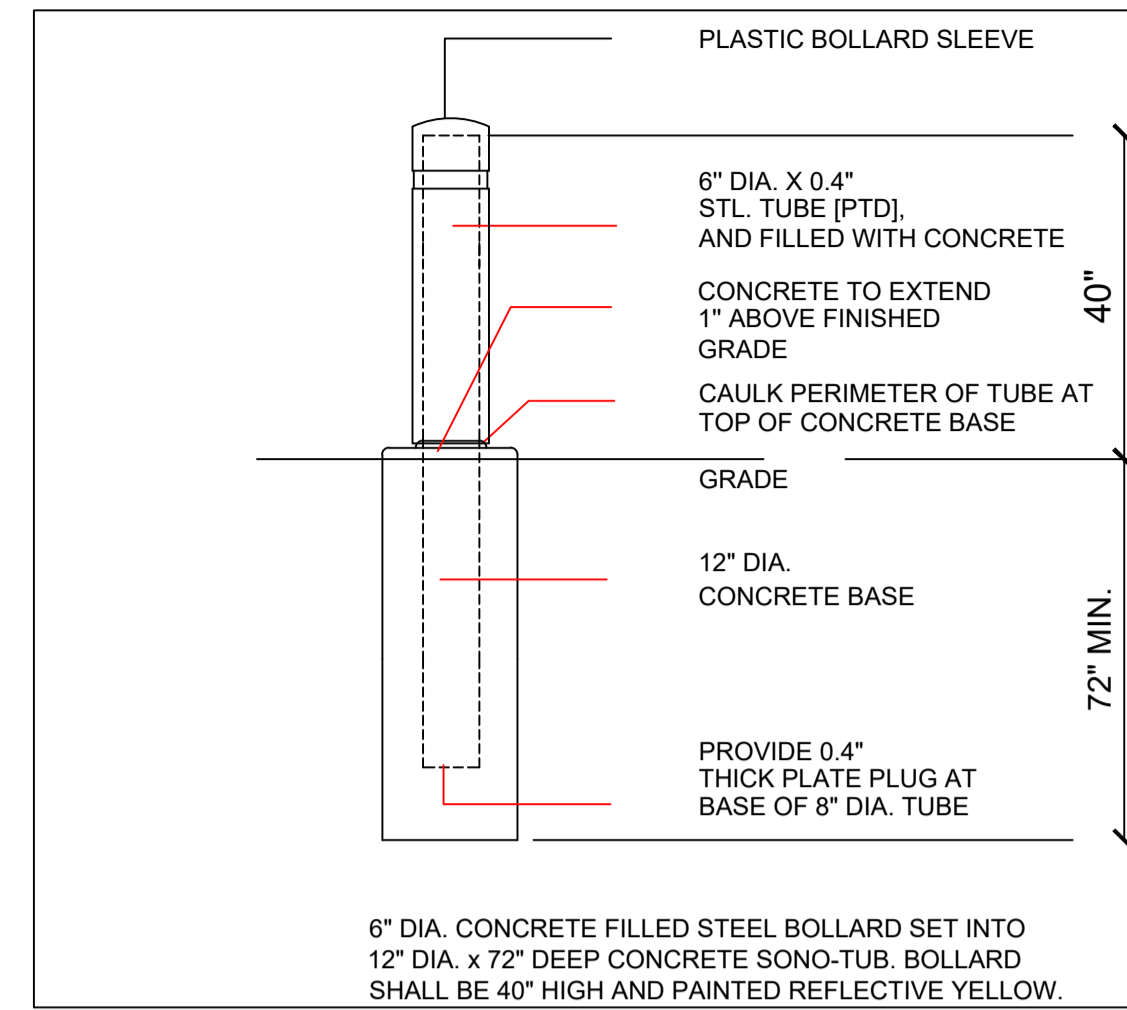
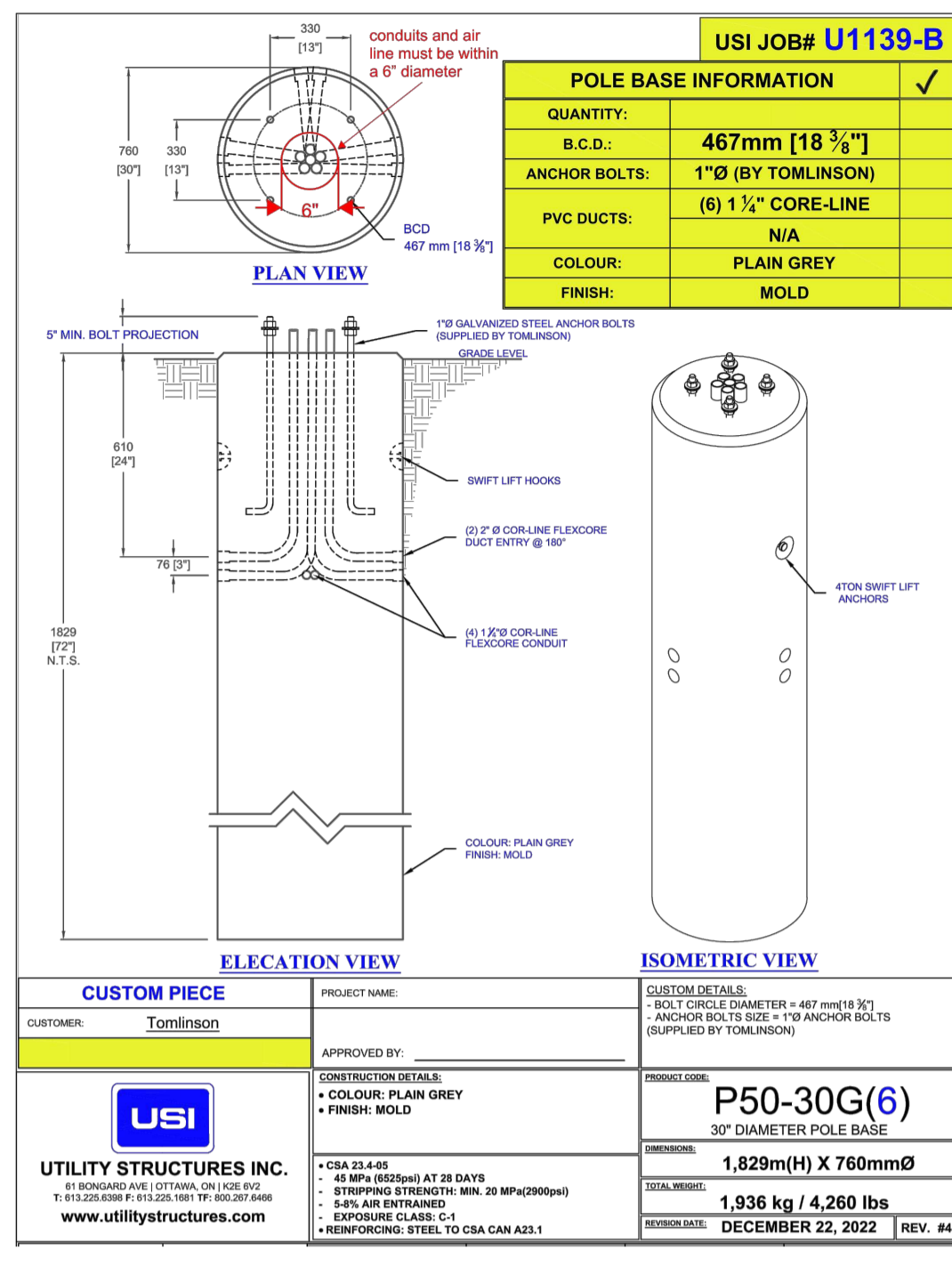
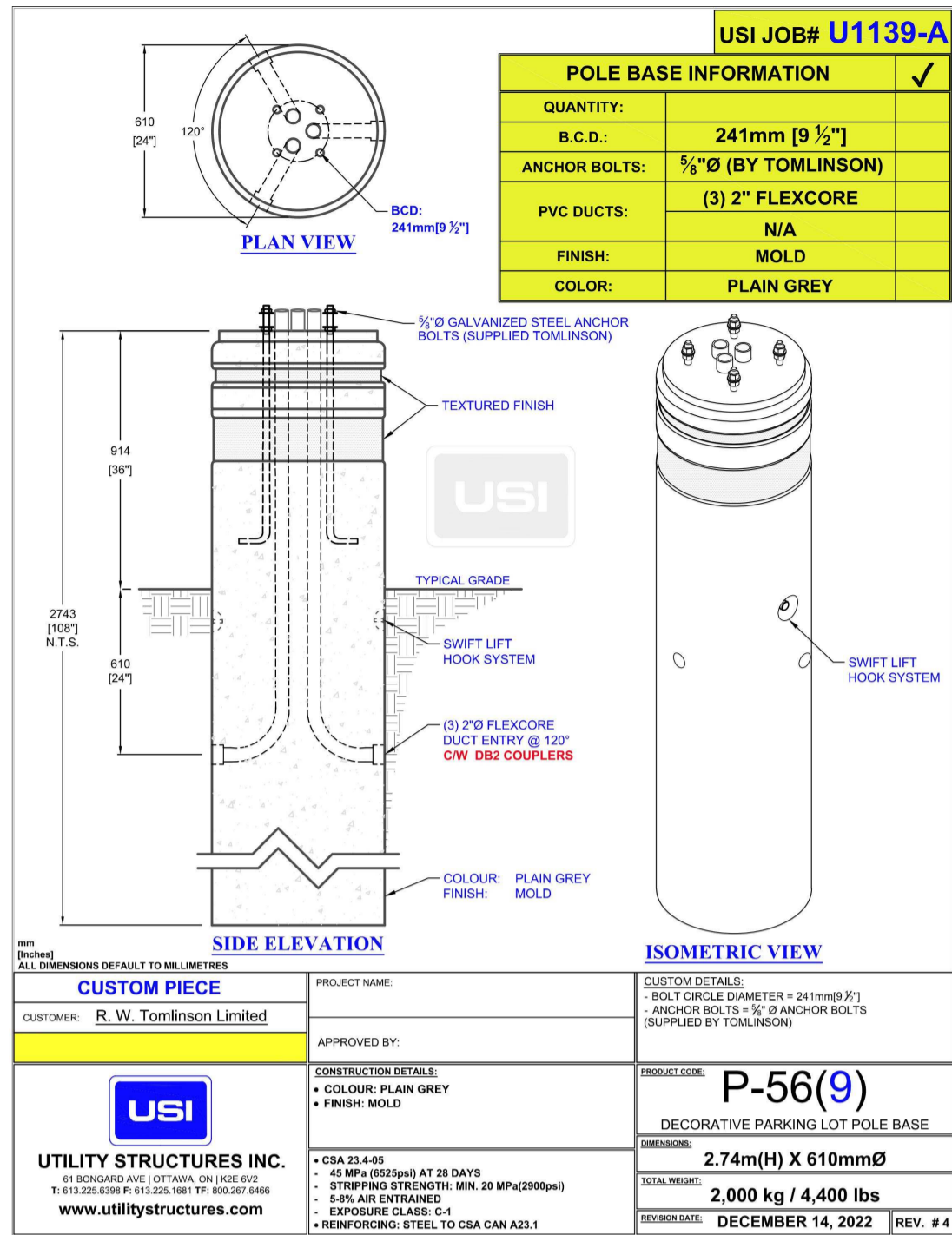
PROJECT NO.  
**210691**

DATE  
**JANUARY 2022**

**C703**

D07-12-22-0085 #18788





**ASSISTANCE INTERCOM STATIONS**

N.T.S.

**ASSISTANCE INTERCOM STATIONS**

N.T.S.

NOTE: DETAIL TO BE VERIFIED AND STAMPED BY A STRUCTURAL ENGINEER PRIOR TO CONSTRUCTION

**USE AND INTERPRETATION OF DRAWINGS**

GENERAL CONDITIONS OF THE CONTRACT FOR CONSTRUCTION ARE PART OF THE CONTRACT DOCUMENTS AND DESCRIBE THE USE AND INTENT OF THE DRAWING. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING AND REVIEWING THE CONTRACT DOCUMENTS AND DESCRIBING THE USE AND INTENT OF THE DRAWING. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING AND REVIEWING THE CONTRACT DOCUMENTS AND DESCRIBING THE USE AND INTENT OF THE DRAWING. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING AND REVIEWING THE CONTRACT DOCUMENTS AND DESCRIBING THE USE AND INTENT OF THE DRAWING.

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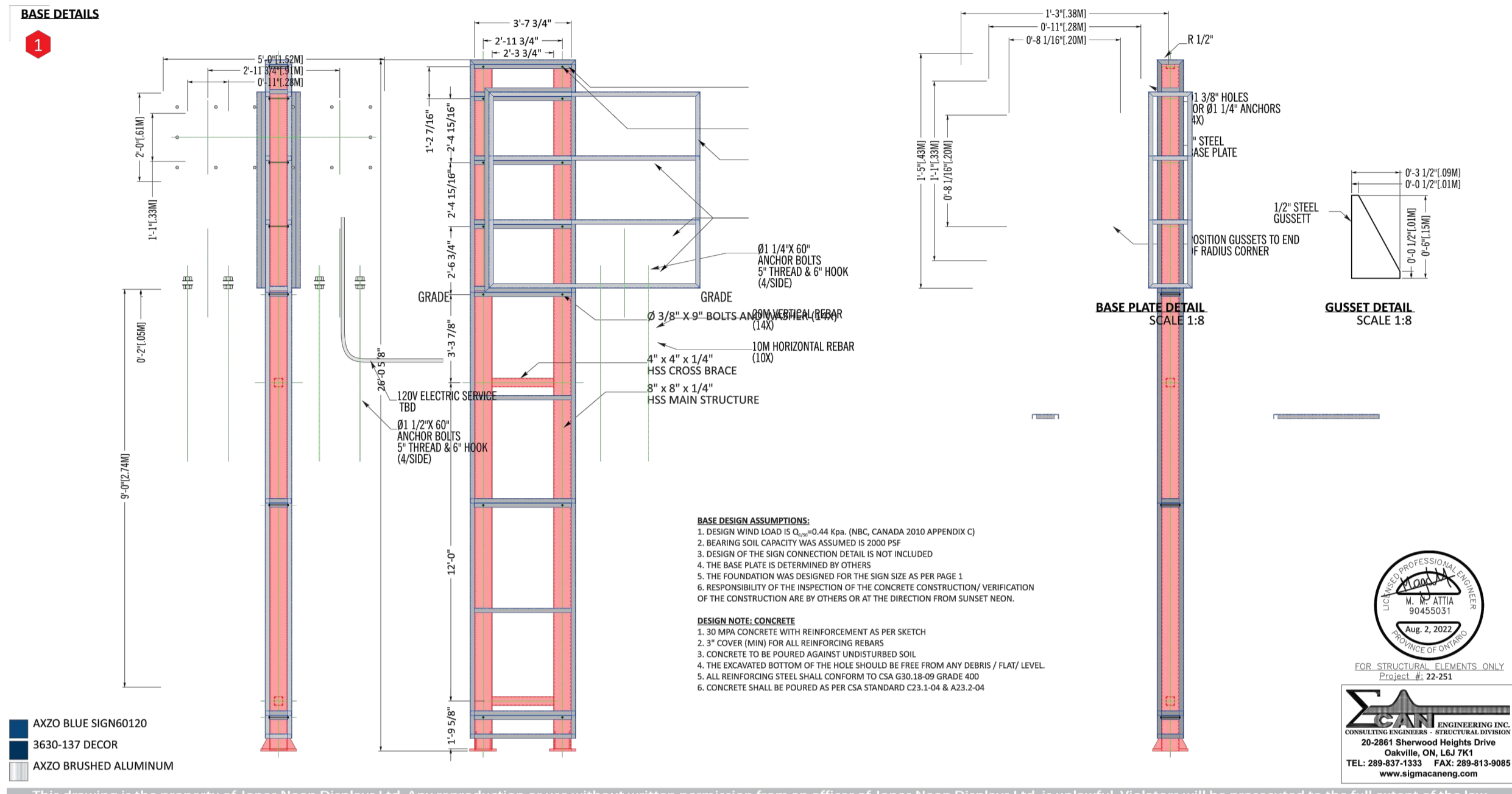
PROJECT: HALO CAR WASH 3555 BORRISOKANE RD BARRHAVEN, ON

DRAWING TITLE: CONSTRUCTION DETAIL PLAN

PROJECT NO: 210691

DATE: JANUARY 2022

**C902**



**BASE DESIGN ASSUMPTIONS:**

- DESIGN WIND LOAD IS 1.0 kPa (IBC CANADA 2010 APPENDIX C)
- BEARING SOIL CAPACITY WAS ASSUMED IS 2000 PSF
- DESIGN OF THE SIGN CONNECTIONS TO BE NOT INCLUDED
- THE BASE PLATE IS DETERMINED BY OTHERS
- THE FOUNDATION WAS DESIGNED FOR THE SIGN SIZE AS PER PAGE 1
- RESPONSIBILITY OF THE INSPECTION OF THE CONCRETE CONSTRUCTION/ VERIFICATION OF THE CONSTRUCTION ARE BY OTHERS OR AT THE DISCRETION FROM SUNSET NEON.

**DESIGNER NOTES/ COMMENT:**

- 30 MPA CONCRETE WITH REINFORCEMENT AS PER SKETCH
- 3" COVER (MIN) FOR ALL REINFORCING REBARS
- CONCRETE TO BE POURED AGAINST UNDISTURBED SOIL
- THE EXCAVATED BOTTOM OF THE HOLE SHOULD BE FREE FROM ANY DEBRIS / FLAT LEVEL
- ALL REINFORCING STEEL SHALL CONFORM TO CSA G30.18 OR GRADE 600
- CONCRETE SHALL BE POURED AS PER CSA STANDARD C23.1-04 & A33.2-04

**BASE NOTE:**

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Customer: Halo Car Wash

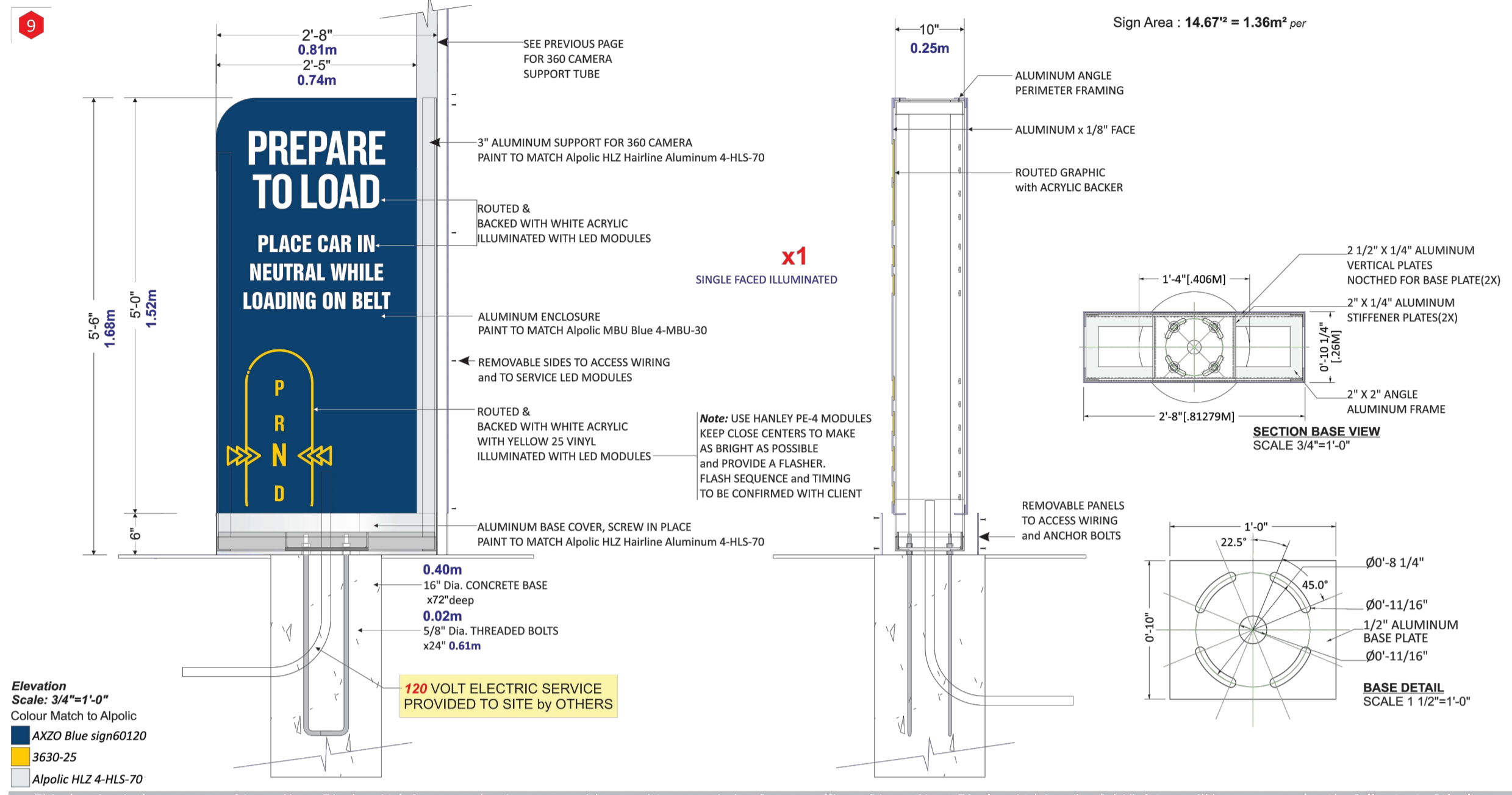
Date: 22/07/11  
Scale: as shown

Revision: R2  
22/07/20/VN, ADDRESS NUMBER CHANGE  
22/07/27/VN, REVISE DRAWING

Permit Required  
Conceptual artwork  
Production artwork  
Site check completed  
Indoor  
Outdoor

Production Approval:  
Signature: [Signature]  
Date:

JONES neon displays  
1140 Blair Road, Burlington, ON L7M 1K9  
e: info@jonesneon.com  
t: 905.335.6664 | f: 905.335.2712



**Elevation**  
Scale: 3/4"=1'-0"  
Colour Match to Alpicol

Customer: Halo Car Wash

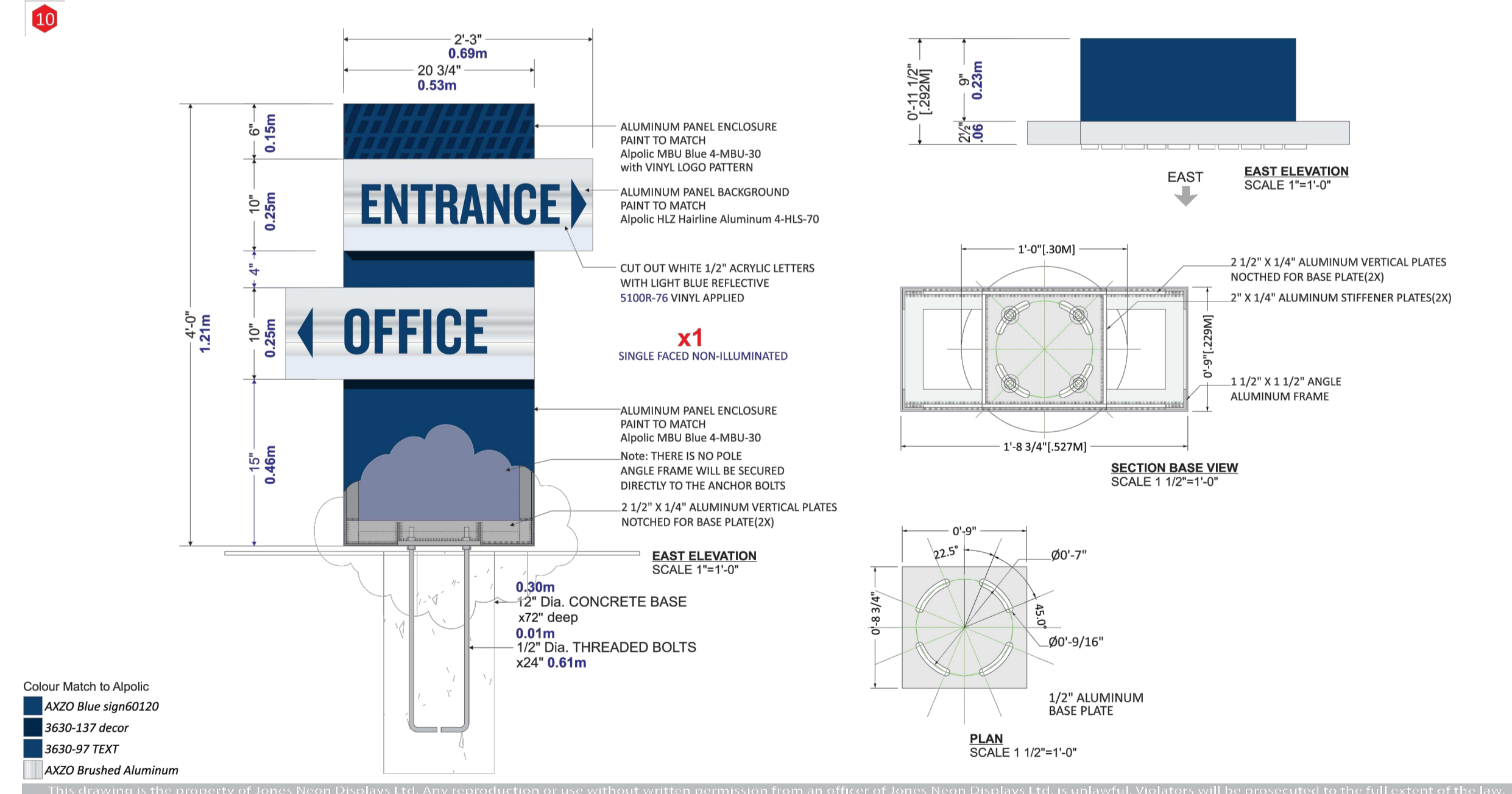
Date: Feb 8/2022  
Scale: as shown

Revision: R7  
22/02/17/VN, SIGNS ADDED  
22/05/12/VN, VACUUM BOOTH QNTY CHANGE

Permit Required  
Conceptual artwork  
Production artwork  
Site check completed  
Indoor  
Outdoor

Production Approval:  
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Date:

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**Elevation**  
Scale: 1 1/2"=1'-0"

Customer: Halo Car Wash

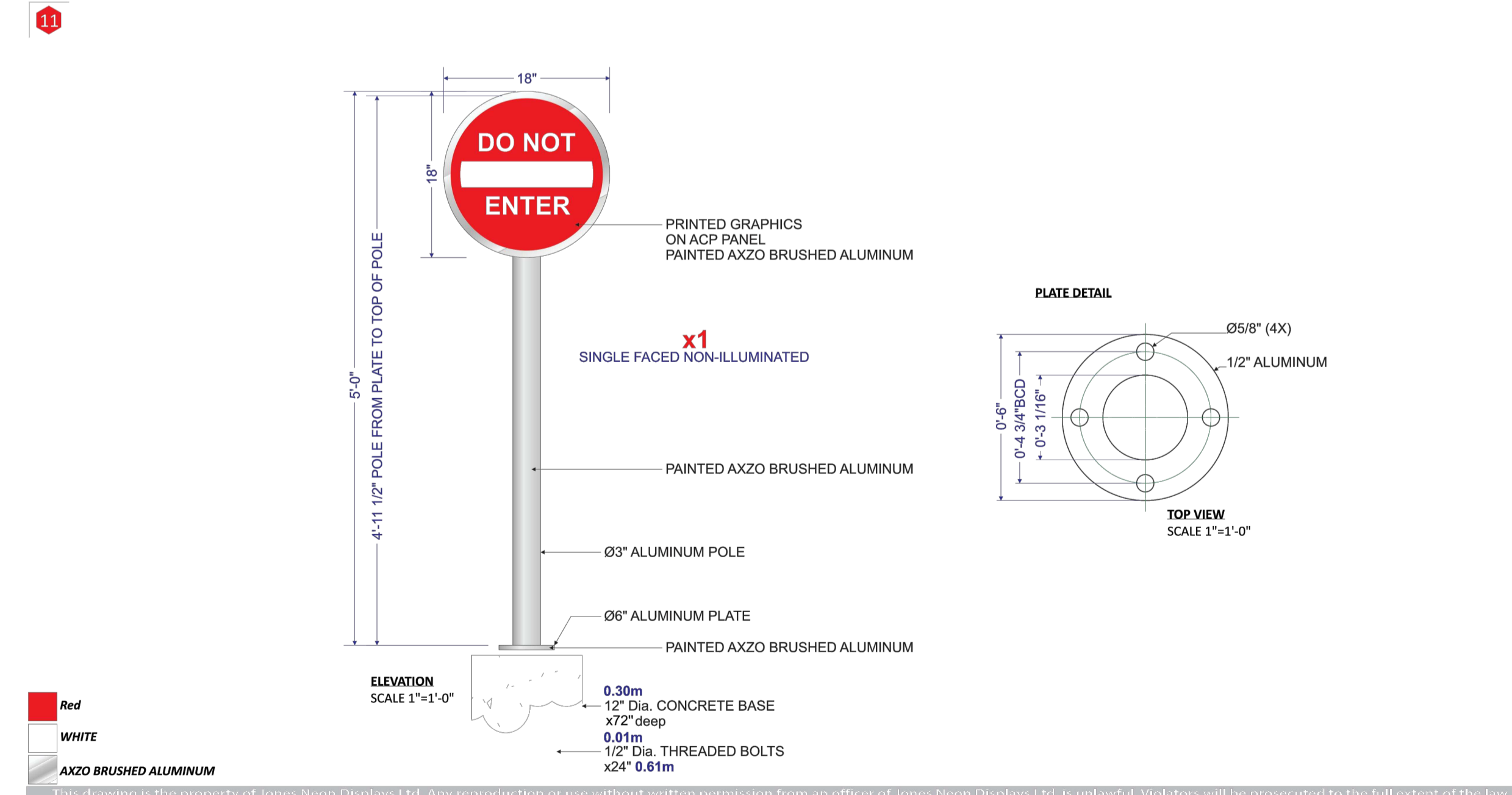
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22/02/17/VN, SIGNS ADDED  
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Scale: 1"=1'-0"

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DRAWING TITLE: CONSTRUCTION DETAIL PLAN

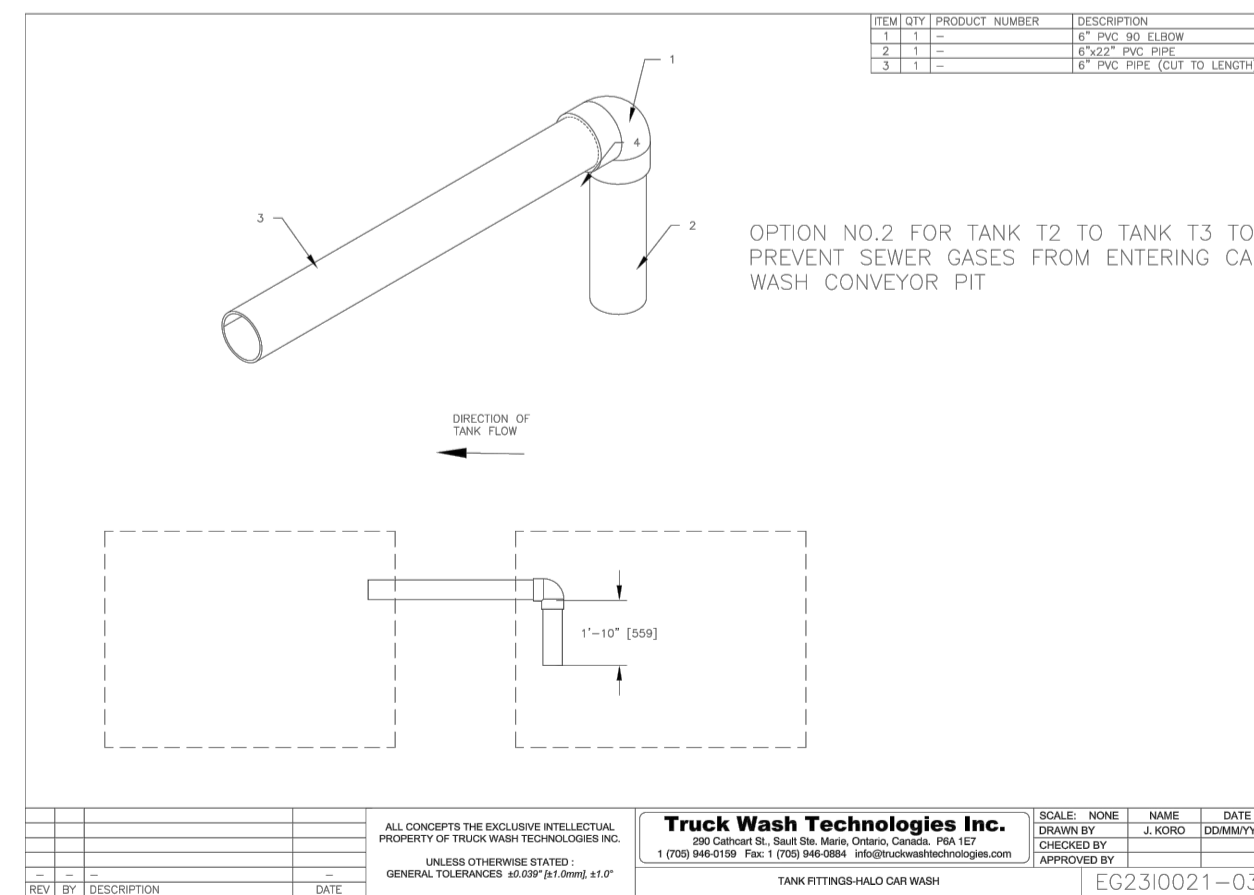
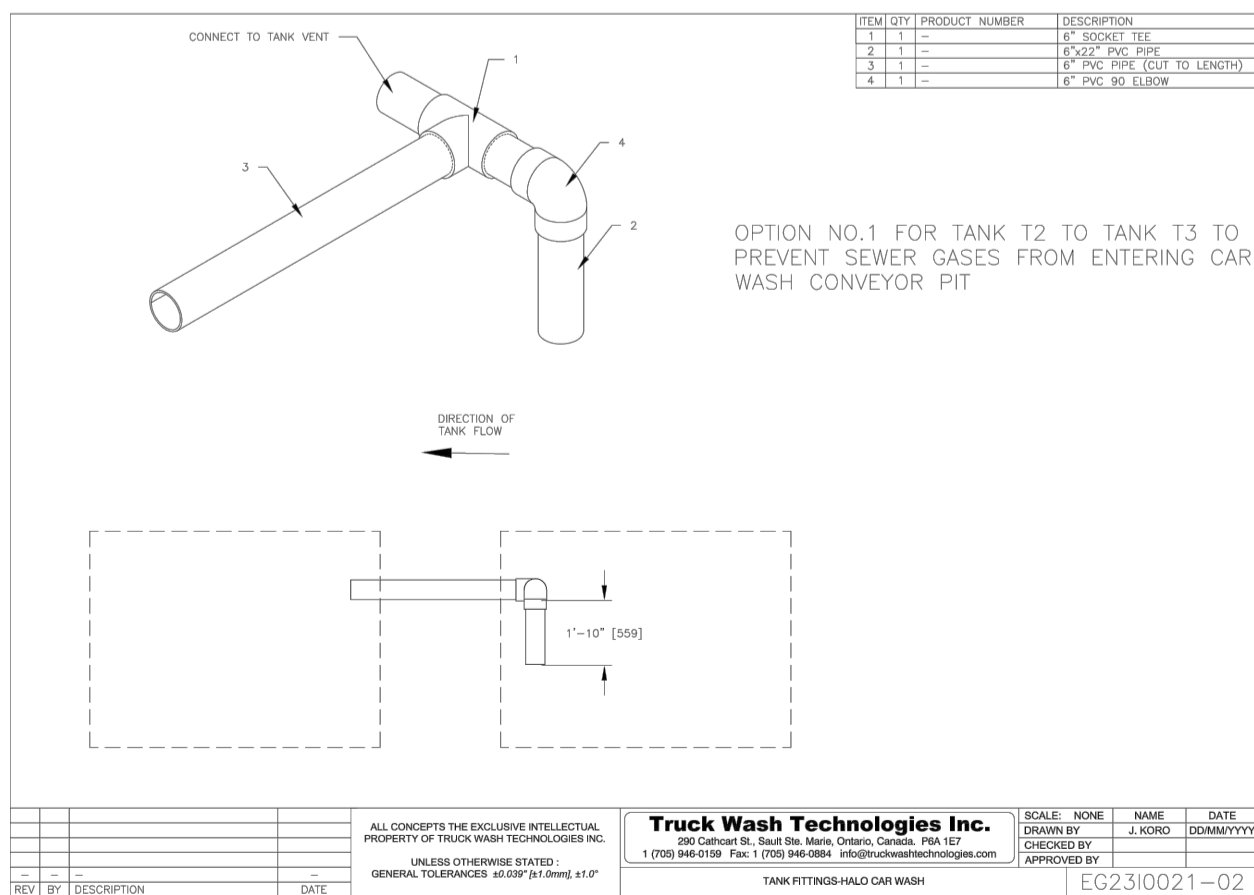
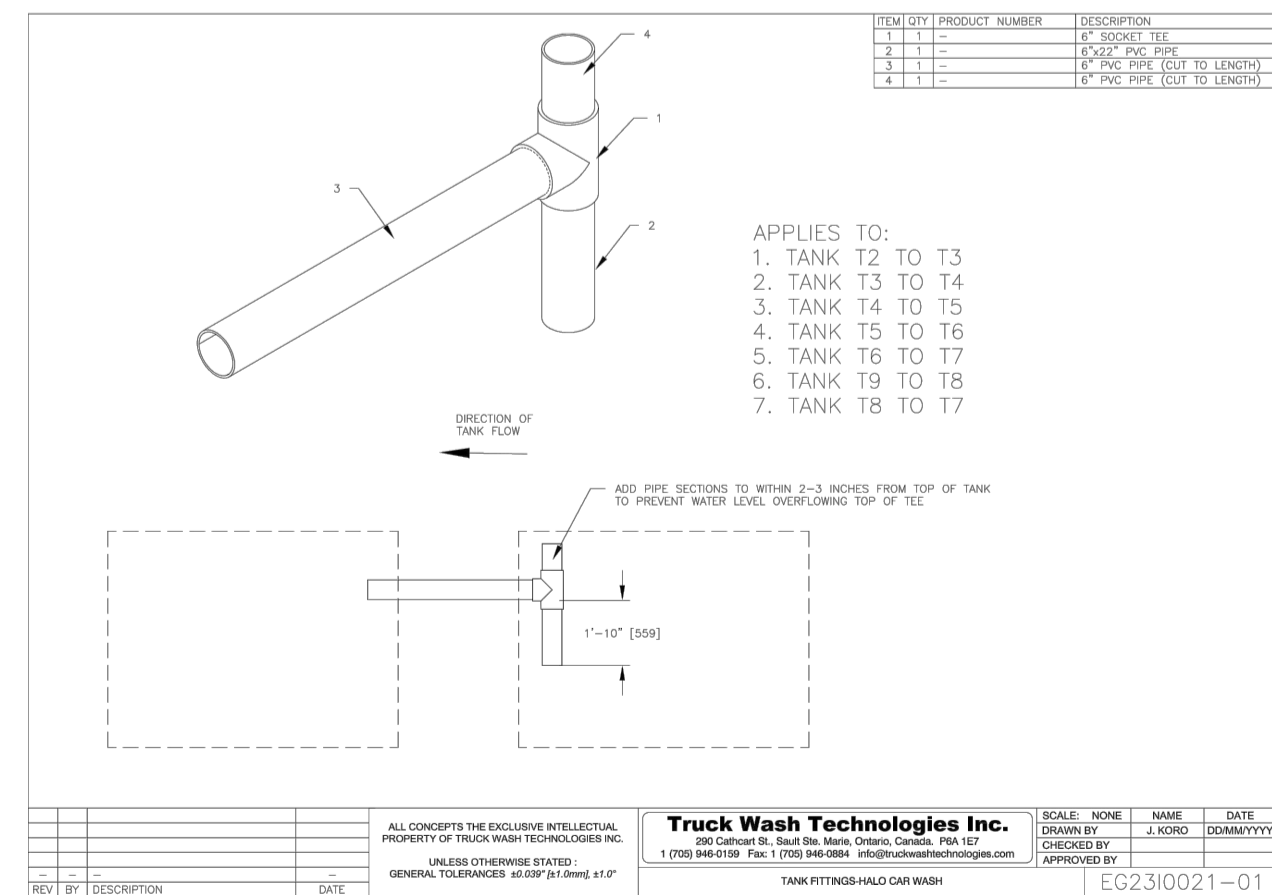
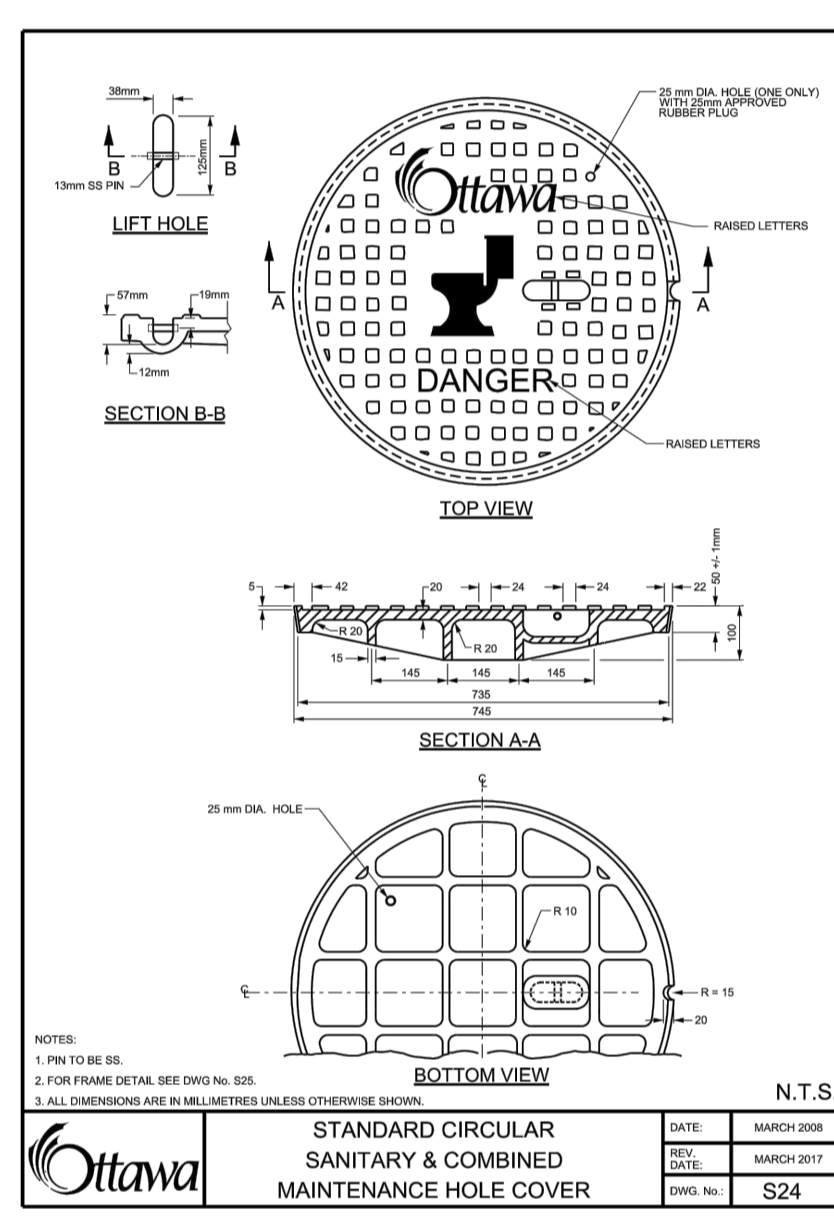
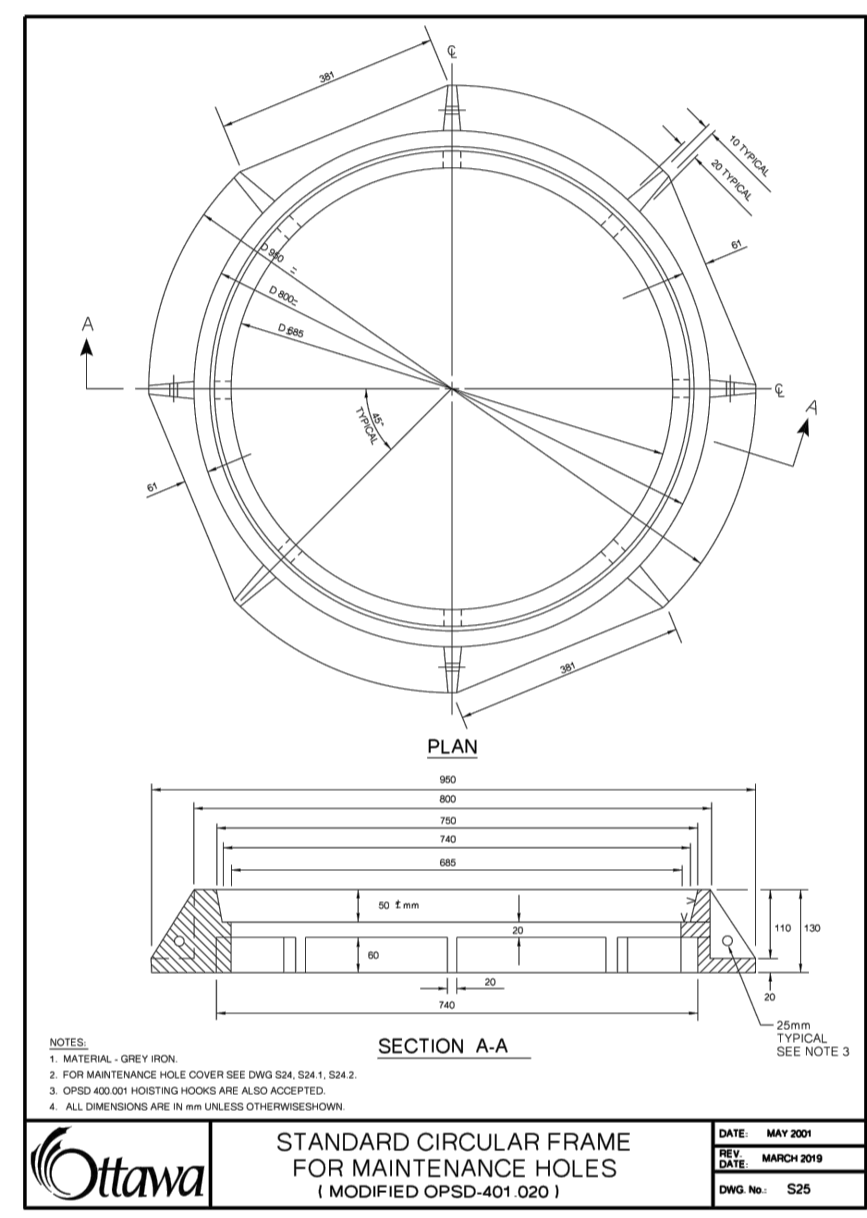
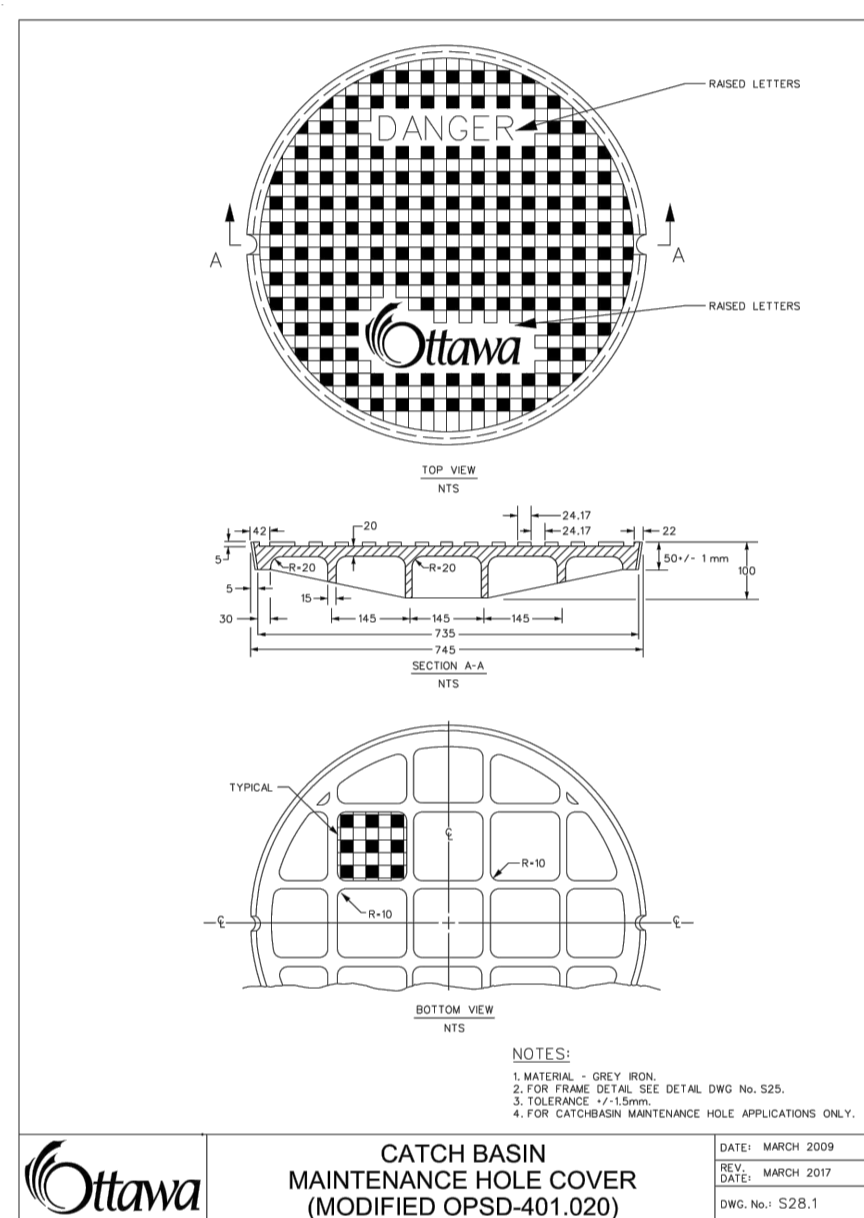
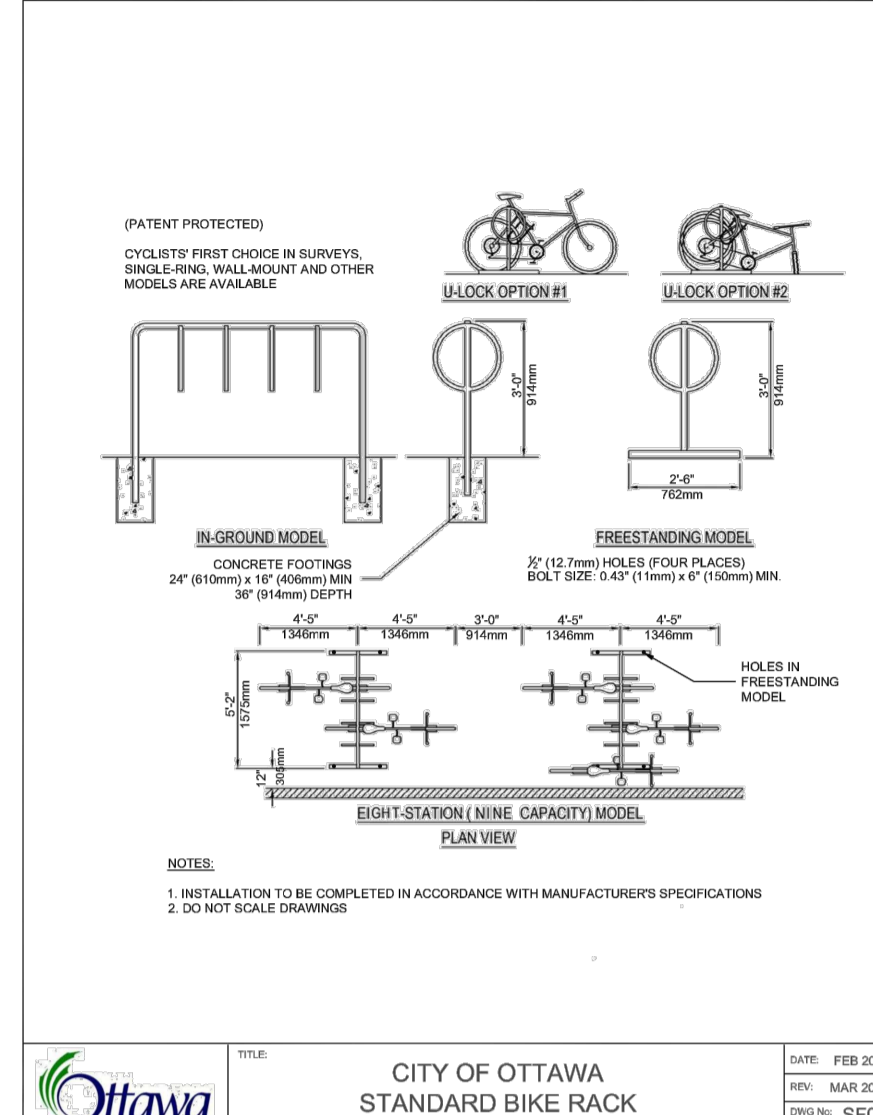
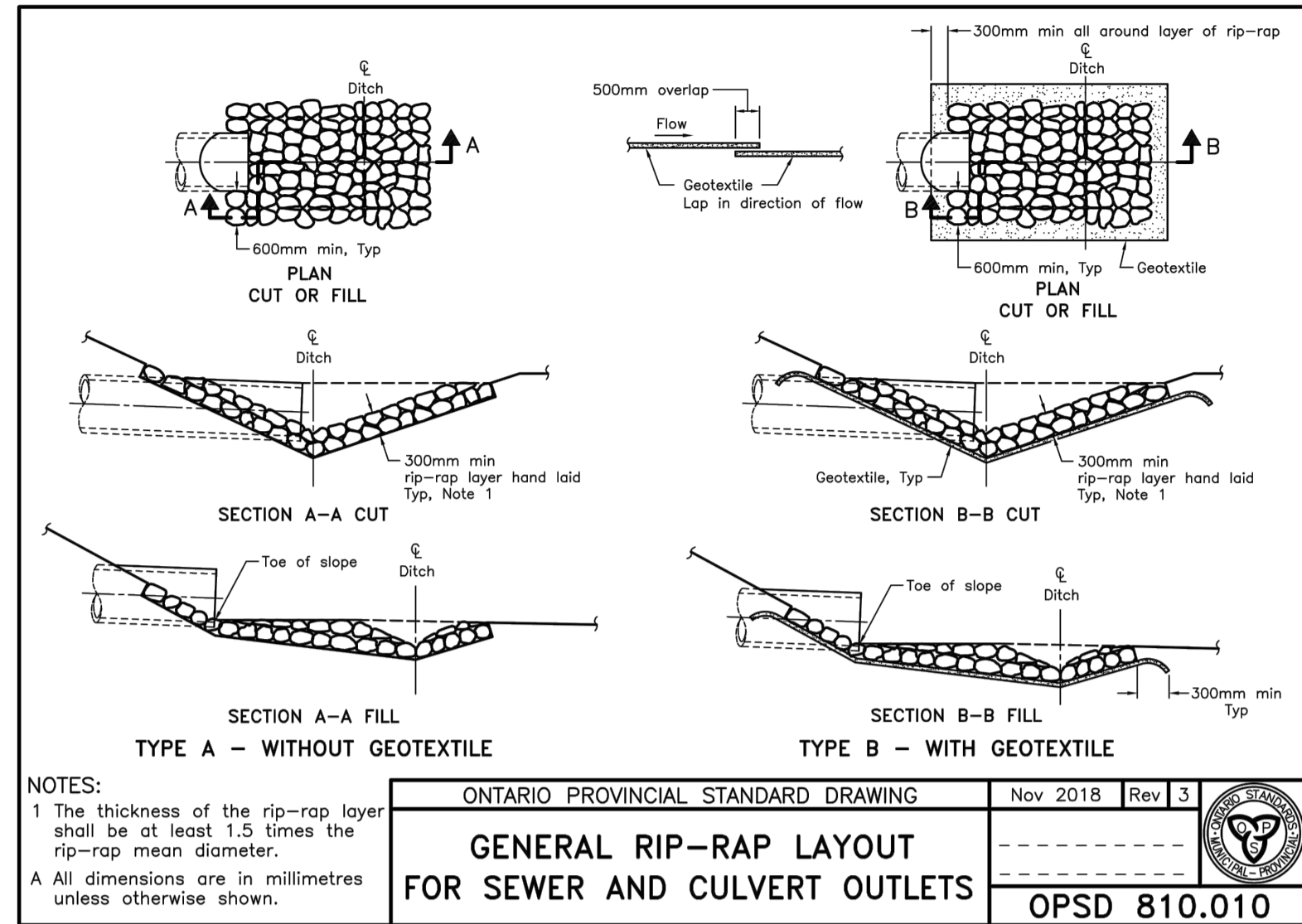
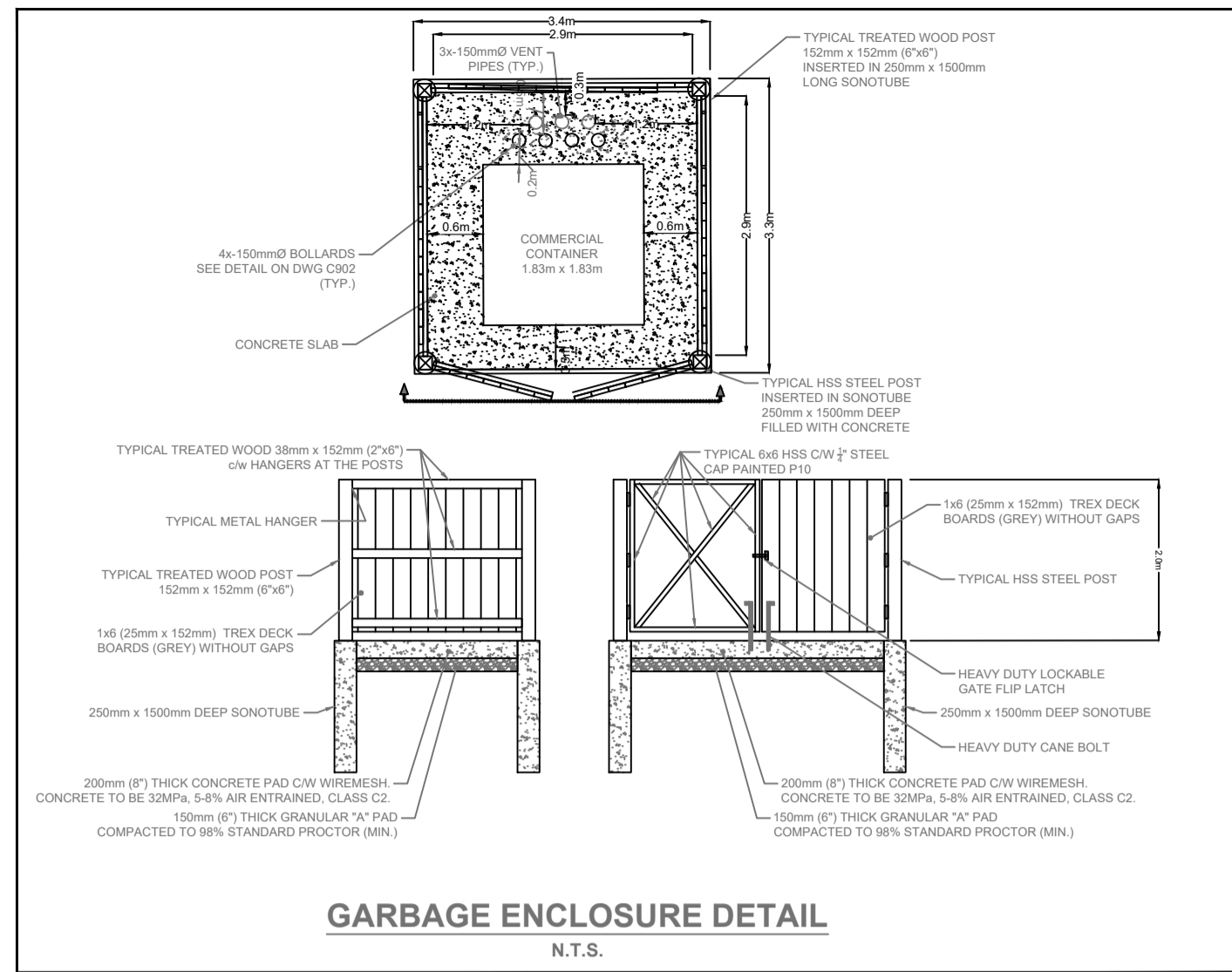
PROJECT NO: 210691

DATE: JANUARY 2022

C903

D07-12-22-0085

#1878



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03	REVISED FLOOR AREA FOR MV APPLICATION	P.P.	13 JULY 2022
02	REVISED FLOOR AREA FOR MV APPLICATION	P.P.	23 JUNE 2022
01	ISSUED FOR APPROVAL	M.L.	22 APR 2022



NOT AUTHENTIC UNLESS SIGNED AND DATED

**LRL**  
ENGINEERING | INGENIERIE  
5430 Canotek Road | Ottawa, ON, K1J 9G2  
www.lrl.ca | (613) 842-3434

CLIENT: HALO CAR WASH INC.

DESIGNED BY: M.L. / P.P. DRAWN BY: M.L. APPROVED BY: M.B.

PROJECT: HALO CAR WASH  
3555 BORRISOKANE RD  
BARRHAVEN, ON

DRAWING TITLE: CONSTRUCTION DETAIL PLAN

PROJECT NO: 210691  
DATE: JANUARY 2022  
C904

D07-12-22-0085



**APPENDIX F**  
**Survey, As-Builts**

TOPOGRAPHICAL PLAN OF SURVEY OF  
**PART OF LOT 11**  
**CONCESSION 3 (RIDEAU FRONT)**  
**Geographic Township of Nepean**  
**CITY OF OTTAWA**  
 Surveyed by Annis, O'Sullivan, Vollebek Ltd.

Scale 1 : 400

**Metric**  
 DISTANCES SHOWN ON THIS PLAN ARE IN METRES AND  
 CAN BE CONVERTED TO FEET BY DIVIDING BY 0.3048

**Surveyor's Certificate**  
 I CERTIFY THAT :  
 1. This survey and plan are correct and in accordance with the Surveys  
 Act and the Surveyors Act and the regulations made under them.  
 2. The survey was completed on the 19th day of January, 2022.

Date: Jan 21/22  
 T. Hartwick  
 Ontario Land Surveyor

**Notes & Legend**

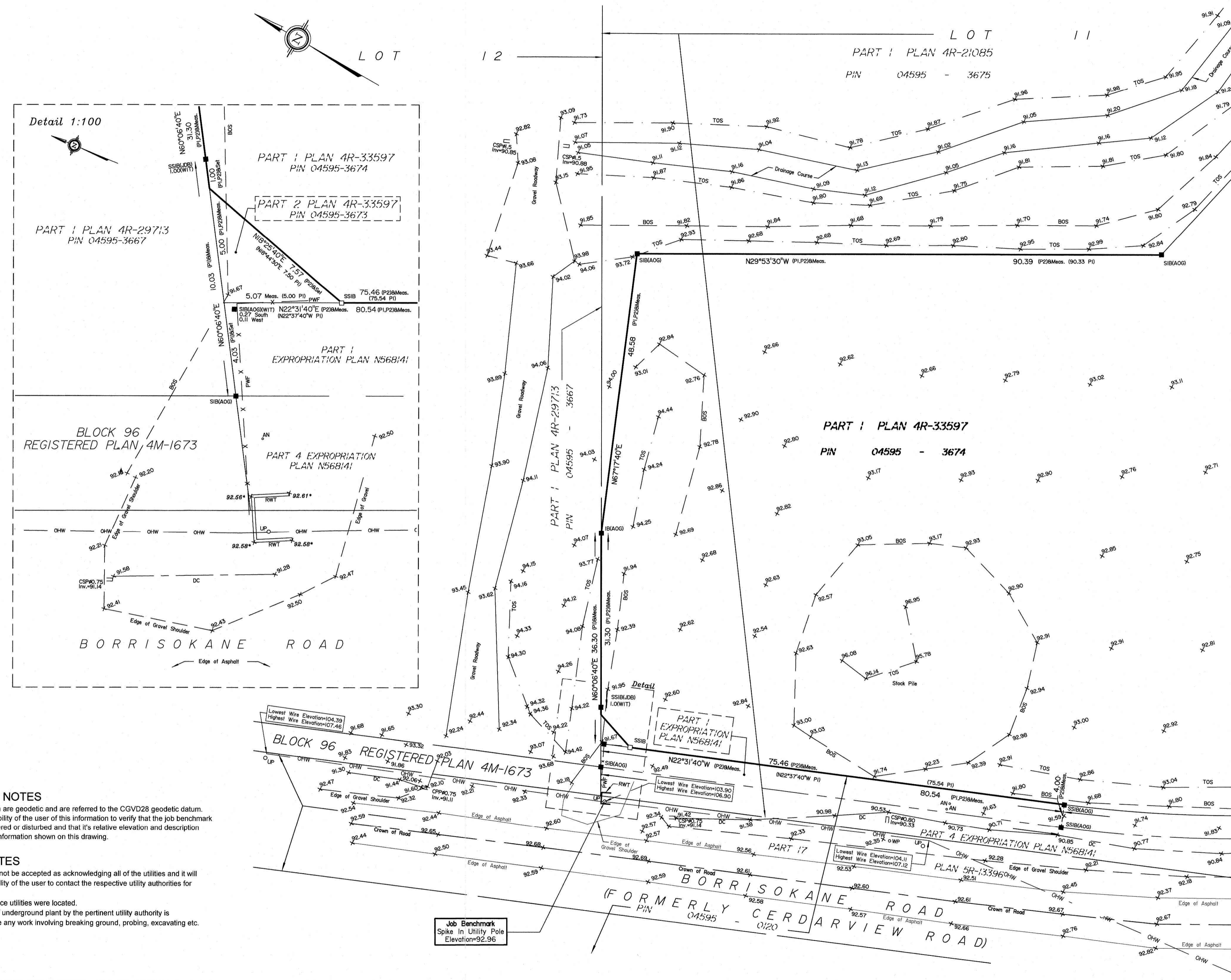
Symbol	Denotes	Description
□	"	Survey Monument Planted
■	"	Survey Monument Found
SIB	"	Standard Iron Bar
SSIB	"	Short Standard Iron Bar
IB	"	Iron Bar
CC	"	Cut Cross
(WIT)	"	Witness
Meas.	"	Measured
(AOG)	"	Annis, O'Sullivan, Vollebek Ltd.
(PI)	"	Plan 4R-33597
(P2)	"	(AOG) Plan dated October 29, 2021.
— OHW —	"	Overhead Wires
CSP	"	Corrugated Steel Pipe
CPP	"	Corrugated Plastic Pipe
CCP	"	Concrete Pipe
CLF	"	Chain Link Fence
PWF	"	Post and Wire Fence
BOS	"	Bottom of Slope
TOS	"	Top of Slope
DC	"	Ditch Centerline
Inv.	"	Invert
RWT	"	Timber Retaining Wall
o WP	"	Wood Pole
o UP	"	Utility Pole
o AN	"	Anchor
o	"	Diameter
+ 65.00	"	Location of Elevations
+ 65.00*	"	Top of Retaining Wall Elevation

Distances shown on this plan are ground distances and can be converted to grid distances by multiplying by the combined scale factor of 0.999933.

Bearings are grid, derived from Can-Net 2016 Real Time Network GPS observations referenced to Specified Control Points 01919791338 and 01919871649, MTM Zone 9 (76°30' West Longitude) NAD-83 (original).

ASSOCIATION OF ONTARIO  
 LAND SURVEYORS  
 PLAN SUBMISSION FORM  
**V-22497**  
  
 THIS PLAN IS NOT VALID UNLESS  
 IT IS AN EMBOSSED ORIGINAL  
 COPY ISSUED BY THE SURVEYOR  
 In accordance with  
 Regulation 1026, Section 29 (3).

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**ANNIS, O'SULLIVAN, VOLLEBEK LTD.**  
 14 Concourse Gate, Suite 500  
 Nepean, Ont. K2E 7S6  
 Phone: (613) 727-0850 / Fax: (613) 727-1079  
 Email: Nepean@aosvlltd.com  
 Job No. 22410-21 Borrisokane January 21, 2022(2)



Job Benchmark  
 Spike In Utility Pole  
 Elevation=92.96

- ELEVATION NOTES**
1. Elevations shown are geodetic and are referred to the CGVD28 geodetic datum.
  2. It is the responsibility of the user of this information to verify that the job benchmark has not been altered or disturbed and that its relative elevation and description agrees with the information shown on this drawing.
- UTILITY NOTES**
1. This drawing cannot be accepted as acknowledging all of the utilities and it will be the responsibility of the user to contact the respective utility authorities for confirmation.
  2. Only visible surface utilities were located.
  3. A field location of underground plant by the pertinent utility authority is mandatory before any work involving breaking ground, probing, excavating etc.

N:\2021\22410-21\_Borrisokane\_Rd\_Topog\Aerials\Topo\Aerials\Topo\Borrisokane January 21, 2022(2).dwg, 2022-01-21 1:46:18 PM