Geotechnical Engineering

Environmental Engineering

Hydrogeology

Geological Engineering

**Materials Testing** 

**Building Science** 

**Noise and Vibration Studies** 

### **Groundwater Impact Assessment**

Proposed Residential Building 1185 Beaverwood Road Ottawa, Ontario

### **Prepared For**

Ark Construction Ltd.

December 13, 2022

Report PH4499-REP.01R

#### Paterson Group Inc.

Consulting Engineers 9 Auriga Drive Ottawa, Ontario Canada K2E 7T9

Tel: (613) 226-7381 www.patersongroup.ca



### TABLE OF CONTENTS

### PAGE

1.0	INTRODUCTION         1           1.1         Proposed Project         1
2.0	BACKGROUND INFORMATION
3.0	SITE CONDITIONS33.1Geology33.2Hydrogeology4
4.0	POTENTIAL IMPACTS74.1Adverse Effects on Adjacent Structures.74.2Adverse Effects on Neighbouring Water Wells74.3Soil, Surface Water, and Groundwater94.4Adjacent Permits to Take Water104.5Existing Servicing.10
5.0	RECOMMENDATIONS 11
6.0	STATEMENT OF LIMITATIONS

### APPENDICES

- Appendix 1 Drawing PH4499 1 Site Plan Drawing PH4499 - 2 - MECP Water Well Location Plan
- Appendix 2 Borehole Logs PG6160 - 1 - Test Hole Location Plan
- Appendix 3 Project1 Studio Architects Plan/Profile Drawings Correspondence



### 1.0 INTRODUCTION

Paterson Group (Paterson) was commissioned by Ark Construction Ltd. to complete a groundwater impact assessment for the proposed residential building to be located at 1185 Beaverwood Road in the City of Ottawa, Ontario (Refer to Drawing PH4499-1 - Site Plan attached to the current report).

The following report has been prepared specifically and solely for the aforementioned project described herein. It contains a hydrogeological review and assessments pertaining to the proposed development as it is understood by Paterson at the time of writing this report.

### **1.1 Proposed Development**

Based on available design plans, it is understood that the proposed development will consist of a multi-storey residential building with a partial below-grade level which will daylight to the east. At finished grades, the proposed building will be surrounded by landscaped areas, asphalt-paved access lanes and parking areas. It is anticipated the proposed development will be municipally serviced.



### 2.0 Background Information

The field program for the geotechnical investigation was carried out on March 1, 2022. At that time, a total of four (4) boreholes were advanced across the site to a maximum depth of 4.5 m below ground surface (bgs) using a track mounted drill rig. The test hole locations were distributed in a manner to provide general coverage of the subject site. The approximate locations of the test holes are presented on drawing PG6160 - 1 - Test Hole Location Plan included in Appendix 2.

### 3.0 SITE CONDITIONS

At the time of the geotechnical field investigation, the subject site consisted of an approximately 0.6 acre property bounded by a residential property to the north, Scharfield Road to the east, Beaverwood Road to the south, and a vacant property to the west. The ground surface across the site slopes downward toward the east side of the property from approximate geodetic elevations of 94.5 to 90.5 m.

The western half of the subject site is occupied by an existing residential dwelling and detached garage structure which are surrounded on all sides by mature trees. The eastern half of the site is vacant and grass covered.

### 3.1 Geology

Generally, the soil profile at the borehole locations consists of topsoil or asphaltic concrete overlying fill material which is underlain by brown, stiff to very stiff silty clay. The silty clay was further underlain by a glacial till deposit consisting of a silty sand to sandy silt matrix with gravel, cobbles and boulders. Practical refusal to augering was encountered at each test hole location at depths ranging from approximately 0.2 to 4.5 m bgs. Specific details of the soil profile at each test hole location are presented on the borehole logs included in Appendix 2.

Based on surficial mapping prepared by the Ontario Geological Survey, the subject site is located in an area where surficial geology predominately consists of marine deposited clay and silt as well as drumlinized glacial till. This information is consistent with the results of Paterson's field investigation.

### Fill

Fill material consisting of a silty sand to silty clay with trace amounts of gravel was observed underlying the topsoil or asphaltic concrete and extended to a maximum depth of 1.2 m bgs.

### Silty Clay

A hard to very stiff brown silty clay was encountered underlying the fill material at all borehole locations with the exception of BH 2-22 and extended to a maximum depth of 3.4 m bgs.

### Glacial Till

A compact glacial till deposit comprised of a brown silty sand to sandy silt matrix with various amounts of gravel, cobbles, and boulders was encountered underlying the silty clay layer at all test hole locations with the exception of borehole BH 2-22. This layer extended a maximum depth of 4.5 m bgs.

### Bedrock

Based on available geological mapping provided by the Ontario Geological Survey (OGS), bedrock consists of dolomite from the Oxford formation with an overburden drift thickness of approximately 5 to 10 m depth.

### **Karst Features**

The term "karst" refers to a geologic formation characterized by the dissolution of carbonate bedrock, such as limestone or dolostone. In order for karstification to occur, precipitation must be allowed to infiltrate the top of the bedrock to dissolutionally enlarge previously existing joints and bedding planes. Based on available mapping by the Ontario Geological Survey, there is no inferred, potential or known karstification in the subject area.

### 3.2 Hydrogeology

### Existing Aquifer Systems

Aquifer systems may be defined as a geological media, either overburden soils or fractured bedrock, which permit the movement of groundwater under hydraulic gradients. Although groundwater has been observed within the overburden material at the subject site, the overburden aquifer does not allow for the development of significant water supply wells. Water supply wells in the vicinity are instead likely found in the bedrock aquifer.

Bedrock aquifer mapping, provided by Natural Resources Canada Urban Geology of the National Capital Region mapping, was reviewed as part of this assessment. Using this tool, it was found that the subject site is situated entirely on the Oxford formation aquifer system.

Wells completed in the Oxford formation within a 500 m radius of the subject site encountered water-bearing fractures at depths typically ranging from 12 m to 49 m bgs.



### Groundwater Levels

Groundwater was observed in the piezometers and monitoring well installed in the overburden at the borehole locations. Based on a review of water well records, groundwater is also present in the bedrock at depth.

Water levels at the subject site were observed to vary from 1.3 to 3.1 m bgs at the time of the geotechnical field investigation. It should be noted that water can become trapped in backfilled boreholes completed in low permeability materials resulting in an artificially elevated water table, and that groundwater levels can fluctuate both seasonally and in conjunction with precipitation events. As such, water levels may vary at the time of construction.

#### Hydraulic Gradients

Vertical hydraulic gradients were not measured at the subject site as the previous studies completed did not warrant the installation of monitoring well nests.

Based on groundwater measurements taken from the piezometers and monitoring wells at the time of the time of the field investigation, an approximate horizontal hydraulic gradient and direction was calculated in the overburden material. The horizontal hydraulic gradient between any 2 points is the slope of the hydraulic head between those points:

i=(h2-h1)/L

Where: i=horizontal hydraulic gradient h=water level (m asl) L=horizontal distance between test hole locations

Using the above noted formula, the horizontal hydraulic gradient has been calculated to range from approximately 0.04 to 0.05 in an eastern direction. Shallow groundwater flow in the vicinity of the subject site is expected to reflect local topography. Regional groundwater flow is considered to be in a eastern direction towards the nearby Rideau River.



### Hydraulic Conductivity

The hydraulic conductivity values were conservatively estimated based upon previous experience at similar sites in the area and typical published values for similar stratigraphy. The hydraulic conductivity values are interpreted to range from approximately  $1 \times 10^{-7}$  to  $1 \times 10^{-9}$  m/sec for stiff silty clay and are dependent on the moisture level and consistency of the deposit. The hydraulic conductivity values are interpreted to range from approximately  $1 \times 10^{-9}$  m/sec for  $1 \times 10^{-9}$  m/sec for glacial till and is dependent on the ratios of the various materials in the deposit.

Based on the available drawings for the subject site, the maximum depth of footing excavation is expected to be approximately 5.5 m, while the maximum depth of foundation excavation is expected to be approximately 3.5 m bgs. Given the observed groundwater infiltration levels in the test holes and approximate excavation depths, it is conservatively estimated that a maximum saturated depth of excavation of 4 m could be expected during the foundation excavation at the time of construction.

### **Groundwater Recharge and Discharge**

In general, groundwater will follow the path of least resistance from areas of higher hydraulic head to areas of lower hydraulic head. While upward and downward hydraulic gradients may be indicative of discharge and recharge respectively, other factors must be considered.

Based on the hydraulic conductivity estimates obtained from published literature, the glacial till with a silty sand matrix is considered to have a higher hydraulic conductivity than the silty clay overburden soil, which is generally considered to act as a confining layer. It is expected that the majority of surface water will either flow down-gradient as perched water within the fill material or as sheet drainage where silty clay is present. Isolated areas were identified with only a thin layer of silty clay where recharge may be occurring through the till deposit. However given the intermittent nature of the surficial higher permeability soils, the volume of recharge within the site boundaries is expected to be minimal.

With regards to discharge zones, neither the topographical or geological conditions are suitable for discharge to be occurring on a large scale at the subject site, with only limited discharge potential in the drainage ditches located in the surrounding area.

patersongroup North Bay

Ottawa

#### **Potential Impacts** 4.0

#### 4.1 Adverse Effects on Adjacent Structures

The overburden in the area generally consists of topsoil or asphaltic concrete overlying fill material which is further underlain by silty clay an glacial till. Practical refusal to augering was encountered at each test hole location at depths ranging from 0.2 m to 4.5 m bgs. The potential dewatering volumes due to groundwater infiltration into the excavation footprint is anticipated to be low to moderate depending on variations in the majority composition of the overburden material. It is anticipated that pumping from open sumps will be sufficient to control the groundwater influx through the sides of the excavations. Additionally, given the nature of the development (residential multi-storey building with one basement level), the duration of the excavation on site is expected to be short term in duration. Furthermore, the radius of influence expected to develop as a result of dewatering during construction will be minimal. As such, any effects related to ground surface settlement due to the water taking activities during construction are expected to be negligible.

#### 4.2 Adverse Effects on Neighbouring Water Wells

A search of the Ontario Water Well Records database indicates there are several wells within 500 m of the site as depicted on drawing PH4499-2 - MECP Water Well Location Plan. The wells that are currently in use were noted to be screened in the bedrock aguifer system with sufficient vertical and horizontal separation between the maximum potential depth of excavation and the depth of the wells. Furthermore, water takings at the subject site are expected to be short term in duration, given the nature of the proposed development. Due to the vertical/horizontal separation between the maximum potential depth of excavation, the short term nature of the water takings and the limited radius of influence expected to develop as a result of dewatering activities, it is not expected that any of the water takings will negatively affect the water quantity and/or quality of nearby well users. It is worth noting that specific construction methodologies were unknown at the time of report preparation. However, it is understood that no bedrock excavation is anticipated to be required as part of the foundation excavation.

Ditawa North Bay

A series of calculations were carried out on theoretical radii of influence for a maximum building excavation of 6 m deep and withdrawing water from the upper 3.0 m to 4.0 m of the saturated zone. These calculations were completed based on Sichardt (1992) using the equation:

 $R = r_e + 3000^* \Delta h(k^{0.5})$ 

- R = radius of influence (m)
- $r_e = equivalent radius of excavation (m)$
- Δh = thickness of drawdown within the aquifer (m)
- k = hydraulic conductivity (m/sec)

For the purposes of completing the calculations, the following assumptions were made:

- □ r<sub>e</sub> = 20.1 m
- $\Box \qquad k = 1 \times 10^{-6} \text{ m/s for glacial till}$
- $\Box$   $\Delta h = 3.0$  m to 5.0 m, to review potential minimum/maximum variable conditions.

Using the above equation and assumptions, a radius of influence of approximately 9 to 15 m will develop as a steady state condition, extending from the edge of the excavation, in the area of the subject site.

Given the hydrogeological characteristics of the subject site, the theoretical radii of influence for the potential excavation related to the development and the depth of water supply wells within 500 m, a long-term groundwater monitoring program is not required to be implemented based on our review.

However, a baseline water quality sampling program was previously recommended to be completed prior to commencing construction on site, with the program now having been completed at the time of the current report preparation. The premise of the program was to obtain groundwater quality information from the water supply wells in the vicinity of the proposed development prior to the project commencing. This ensured that all parties involved (developer, homeowners, and City of Ottawa) were protected should a concern arise during or after construction.



### Baseline Water Sampling Program

As noted above, the theoretical radius of influence for the proposed development is expected to range from 9 to 15 m dependant on the depth of excavation and elevation of the water table at the time of construction. Additionally, the domestic wells in the area are assumed to be screened within a bedrock aquifer. Furthermore, no bedrock excavation is anticipated as part of the proposed development. Therefore, a conservative radius for the baseline water sampling program of 100 m was agreed upon as a result of pre-consultation undertaken with City of Ottawa staff. Based on the water service mapping provided by the City of Ottawa, a total of eight (8) potential unserviced lots were identified within 100 m of the subject site. Reference should be made to the correspondence included in Appendix 3 of this report.

Municipal addresses on Beaverwood Road that were contacted are: 1191. Municipal addresses on Maple Avenue that were contacted are: 1186, 1190, 1194, 1195, and 1198. Municipal addresses on Colony Heights Road that were contacted are: 5533 and 5534.

The homeowners of the aforementioned properties were presented with a registered letter delivered by Canada Post. Interested homeowners were interviewed for the purpose of obtaining baseline water quality and quantity information followed by raw water sample.

The parameters that were analyzed as part of the sampling program consisted of the "Subdivision Water Quality Package" offered by Eurofins Environmental Testing Canada Inc. This package includes; alkalinity, bacteria, colour, conductivity, pH, hardness, IC anions, NH3, TKN, DOC, phenols, sulphide, metals, Tannin & Lignin, TDS and turbidity.

A draft copy of the registered letter was submitted to the City of Ottawa for review and approval prior to distribution and commencing the baseline water quality sampling program outlined above.

### 4.3 Soil, Surface Water, and Groundwater

A search of the MECP Brownfields Environmental Site Registry was conducted as part of the assessment of the site, neighbouring properties, and the general vicinity of the property. No recorded Brownfield sites were identified within 500 m of the subject site.

It is anticipated that the material on site will be disposed of or re-used as per the MECP policy (Management of Excess Soil - A Guide for Best Management Practices dated January, 2014.)



With respect to surface water features, there are none located within the theoretical radius of influence for the subject site. The nearest surface water feature is the Rideau River, located approximately 500 m east of the site.

It is expected that a multi-barrier approach (such as hay bales, geosocks, silt fencing, etc.) to a non-frozen, well vegetated area will be utilized in order to promote reinfiltration of discharge water prior to reaching the adjacent surface water features noted above. In addition, the turbidity of the water shall not exceed 8 NTU above background levels when discharging within 30 m of a watercourse. Therefore, adverse effects to surface water features resulting from dewatering activities at the subject site are expected to be negligible.

The groundwater that is pumped from the excavations must be managed in an appropriate manner. The contractor may be required to implement a water management and treatment program to dispose of the pumped water. It is expected the groundwater will be discharged to overland. Further treatment may be required should the discharge not meet the required guidelines

### 4.4 Adjacent Permits to Take Water

A search of the MECP Permit to Take Water (PTTW) database provided no active PTTW within 500 m of the subject site. A search of the MECP Environmental Activity and Sector Registry (EASR) database provided no water taking permits within 500 m of the subject site.

### 4.5 Existing Servicing

There are no wells known to exist at the residential dwelling. If any wells are encountered, they will be required to be properly decommissioned by a licensed well contractor as per O.Reg. 903 prior to construction.

### 5.0 Recommendations

Further testing and site preparation is recommended for the detailed Groundwater Impact Assessment. The following aspects of the program should be performed prior to commencing construction for the proposed residential development:

- □ All existing wells within the proposed residential development should be properly decommissioned as per *O.Reg. 903* and prior to construction.
- □ In the interest of public perception, a baseline water sampling program is recommended prior to commencing construction on site.
- Prior to and during site development, it is recommended that construction best management practices with respect to fuels and chemical handling, spill prevention, and erosion and sediment control be followed.
- □ For any water taking of volumes greater than 50,000 L/day, either an Environmental Activity and Sector Registration (EASR) or a Permit To Take Water (PTTW) is required from the MECP, dependent on dewatering requirements.



### 6.0 STATEMENT OF LIMITATIONS

The recommendations provided in this report are in accordance with our present understanding of the project.

A hydrogeological review of this nature is a limited sampling of a site. The recommendations are based on information gathered at the specific test locations and can only be extrapolated to an undefined limited area around the test locations. Should any conditions at the site be encountered which differ from those at the test locations, we request notification immediately in order to permit reassessment of our recommendations.

The present report applies only to the project described in this document. Use of this report for purposes other than those described herein or by person(s) other than Ark Construction Ltd. or their agent(s) is not authorized without review by Paterson Group for the applicability of our recommendations to the altered use of the report.

### Paterson Group Inc.

-Kevin A. Pickard, EIT

Michael Laflamme, P.Geo.

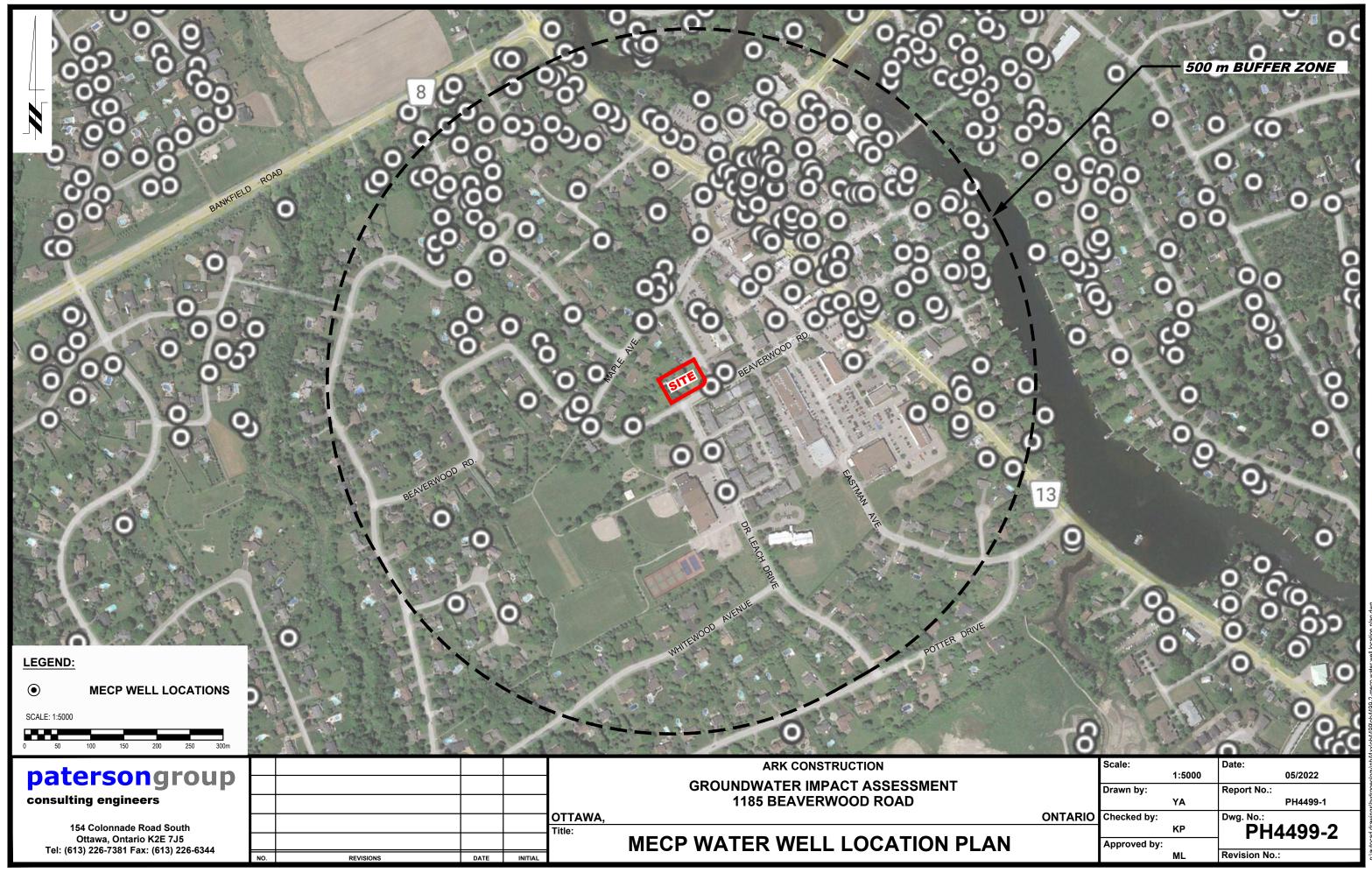


# **APPENDIX 1**

Drawing PH4499 - 1 - Site Plan

Drawing PH4499 - 2 - MECP Water Well Location Plan





# **APPENDIX 2**

Borehole Logs

Drawing PG6160 - 1 - Test Hole Location Plan

# patersongroup Consulting Engineers

### SOIL PROFILE AND TEST DATA

20

40

Shear Strength (kPa)  $\blacktriangle$  Undisturbed  $\triangle$  Remoulded

60

80

100

154 Colonnade Road South, Ottawa, Ont	tario I	-		1116613	Pr	eotechnic oposed I 85 Beave	Developm		wa, C	Ontario	)	
DATUM Geodetic					1				FILE	NO.	PG616	n
REMARKS									HOLE		PG010	5
BORINGS BY CME-55 Low Clearance I	Drill			D	ATE 2	2022 Mar	ch 1				BH 1-22	2
SOIL DESCRIPTION	PLOT		SAN	<b>IPLE</b>		DEPTH (m)	ELEV. (m)	Pen. R • 5		Blow Dia. C		eter ction
	STRATA	ТҮРЕ	NUMBER	% RECOVERY	N VALUE or RQD		()	• <b>v</b>	/ater (	Conte	nt %	Piezometer Construction
GROUND SURFACE			z	RE	zö	0-	-94.24	20	40	60	80	
Asphalt 0.05 FILL: Brown silty sand trace gravel and topsoil 0.69		AU	1				07.24		)			աներությունները հերերերիներին հերերերին։ Դերերերերին երերերերին երերերերին հերերերին
Very stiff brown <b>SILTY CLAY</b> trace sand and gravel		SS	2	50	6	1-	-93.24	O				
GLACIAL TILL: Compact brown silty sand to sandy silt with gravel, cobbles trace clay and boulders 1.98		ss	3	56	50				0			
End of Borehole												
Practical refusal to augering at 1.98m depth (GWL at 1.34 m depth - Mar 9, 2022)												

### SOIL PROFILE AND TEST DATA

Undisturbed

△ Remoulded

### **Geotechnical Investigation** Proposed Development

TUM Geodetic IARKS Moved east approx 1 m from BH 1-	-22 loca						FILE	DCG160	
<b>IARKS</b> Moved east approx 1 m from BH 1-	-22 1003							PG6160	
	22 1000						HOL	E NO. BH 1A-22	n
RINGS BY CME-55 Low Clearance Drill		DA	ATE 2	022 Mar	ch 1				<b>∠</b> T
SOIL DESCRIPTION 법	SAI	MPLE		DEPTH	ELEV.			. Blows/0.3m n Dia. Cone	ter
STRATA 1 TYPE	NUMBER	% RECOVERY	VALUE SE ROD	(m)	(m)			Content %	Piezometer
OUND SURFACE		RECO	N OF			20	40	60 80	Ē
bhalt0.05				0-	-94.24				+
ERBURDEN									
				1-	-93.24				
d of Borehole ctical refusal to augering at 2.13m th				2-	-92.24				

### SOIL PROFILE AND TEST DATA

Geotechnical Investigation Proposed Development 1185 Beaverwood Road - Otta

154 Colonnade Road South, Ottawa, Ont	ario K	(2E 7J	5		Pi	85 Beave	erwood R	nent Road - Otta	wa, Ontario		
DATUM Geodetic									FILE NO.	G6160	
REMARKS											
BORINGS BY CME-55 Low Clearance	Drill			D	ATE	2022 Mar	ch 1	1	BH	2-22	
SOIL DESCRIPTION	ргот		SAN	IPLE		DEPTH	ELEV.		esist. Blows/0 0 mm Dia. Con		ter stion
	STRATA	ТҮРЕ	NUMBER	% RECOVERY	N VALUE or RQD	(m)	(m)	• <b>v</b>	Vater Content 9	%	Piezometer Construction
GROUND SURFACE	-		Z	RE	z <sup>o</sup>	0-	-94.46	20	40 60	80	
Asphalt 0.05 FILL: Brown silty sand with gravel and crushed stone 0.23 End of Borehole		AU	1				54.40		D		
Practical refusal to augering at 0.23m depth											
						1-	-93.46				
						2-	-92.46				
							52.40				
								20		80 10	00
								Shea	ar Strength (kP urbed △ Remo		

### SOIL PROFILE AND TEST DATA

Shear Strength (kPa)

△ Remoulded

▲ Undisturbed

**Geotechnical Investigation** Proposed Development

	ntario ł	<2E 7.	J5			85 Beave		Road - Otta	wa, C	Ontario	<b>o</b>	
ATUM Geodetic									FILE	NO.	PG61	60
EMARKS Moved north approx 1 m	from E	8H 2-2	22 loca	ation					HOL			
ORINGS BY CME-55 Low Clearance	Drill			C	DATE 2	2022 Mar	ch 1				BH 2A	-22
	Ę		SAN	<b>IPLE</b>				Pen. R	esist.	Blow	/s/0.3m	
SOIL DESCRIPTION	PLOT					DEPTH (m)	ELEV. (m)			n Dia. C		eter .
		E	BER	% RECOVERY	N VALUE or RQD	(,	(,					Piezometer
	STRATA	ТУРЕ	NUMBER		I VA					Conte		Pie.
ROUND SURFACE				8	2	0-	-94.46	20	40	60	80	
sphalt0.0 VERBURDEN	5	/-					-					
<u>0.2</u>	3											
nd of Borehole	<u></u>											
ractical refusal to augering at 0.23m												
epth												******
						1-	-93.46					
						2-	-92.46					
								20	40	60	80	100

# pate

patersongr		ır	Con	sulting		SOIL	_ PRO	FILE A	ND 1	<b>ES</b>	T D/	4TA	L .
154 Colonnade Road South, Ottawa, Ont		-		ineers	P	eotechnic roposed [ 185 Beave	Developn		awa. (	Ontari	io		
DATUM Geodetic									FILE			6160	
REMARKS									ноц	E NO.			
BORINGS BY CME-55 Low Clearance	Drill	1		DA	TE	2022 Mar	ch 1	1			BH:	3-22	
SOIL DESCRIPTION	PLOT		SAN	<b>IPLE</b>		DEPTH (m)	ELEV. (m)	Pen. R	esist. 0 mm	-			ster ction
	STRATA	ТҮРЕ	NUMBER	* RECOVERY	N VALUE or ROD		(11)	0 V	Vater	Conte	ent %	,	Piezometer Construction
GROUND SURFACE	ß		N	RE	z °	0-	-91.65	20	40	60	8	0	
<b>TOPSOIL</b> 0.10							31.00						
FILL: Brown silty clay trace sand and gravel								0					
			1					<b></b>					ระจากการกำนักการการการการการการการการการการการการการ
1.22		SS	2	33	11	1-	-90.65						
Very stiff brown SILTY CLAY									0				
<u><b>GLACIAL TILL:</b></u> Compact brown silty sand to sandy silt with gravel, trace clay, cobbles and boulders		ss	3	90	12	2-	-89.65						
End of Borehole 2.18		¶_] ↓											
Practical refusal to augering at 2.18m depth													
(Monitoring well dry - Mar 9, 2022)													

20

▲ Undisturbed

40

Shear Strength (kPa)

60

80

 $\triangle$  Remoulded

100

### SOIL PROFILE AND TEST DATA

▲ Undisturbed △ Remoulded

**Geotechnical Investigation** Proposed Development

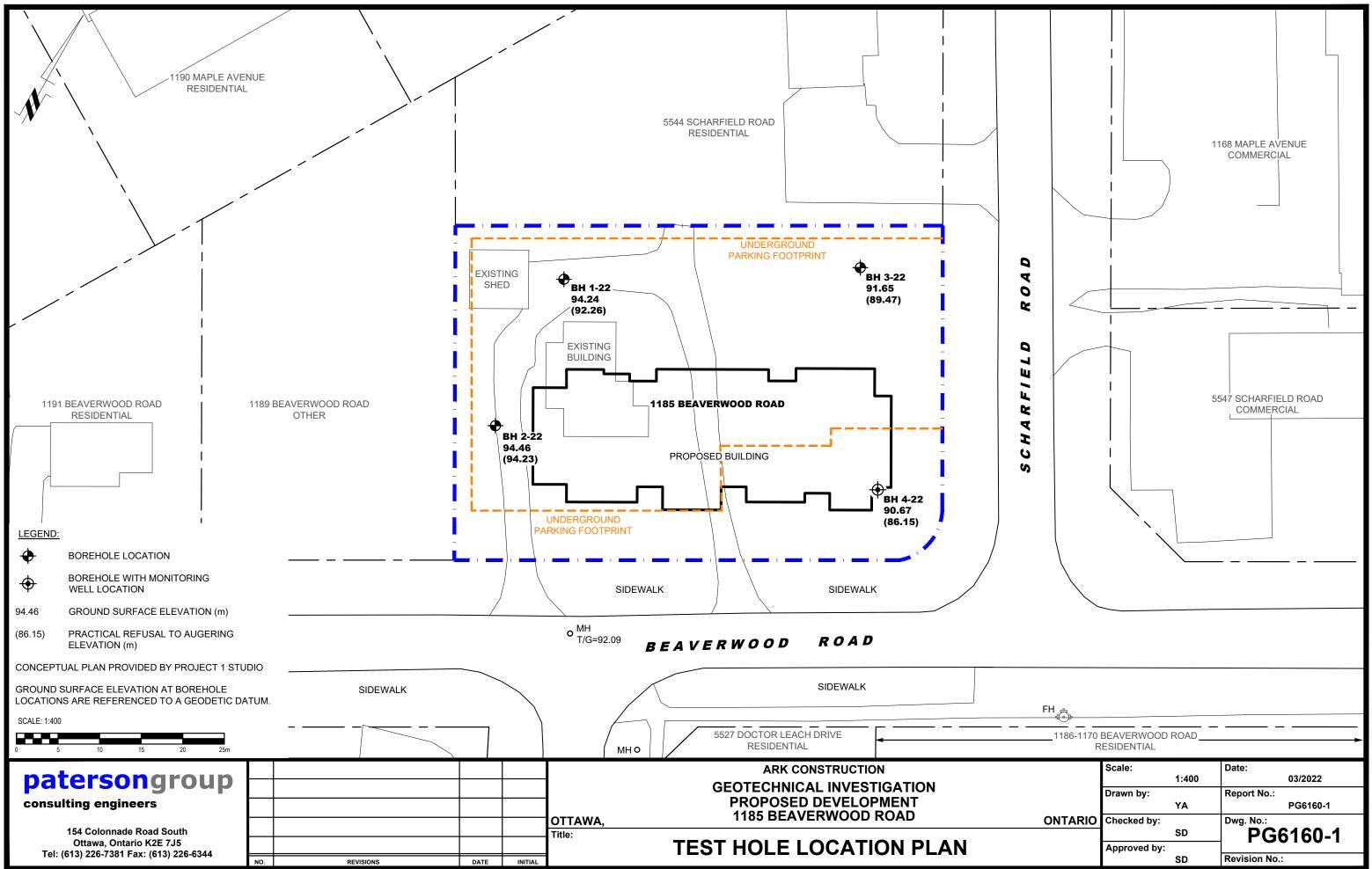
154 Colonnade Road South, Ottawa, On	ario r	(2E /J	15		11	85 Beave	rwood R	load - Otta	wa, Ont	ario	
DATUM Geodetic									FILE NO	PG6160	
<b>REMARKS</b> Moved north approx 1 m fr	om B	H 3-2	2 loca	ation					HOLE N	0	
BORINGS BY CME-55 Low Clearance	Drill	i		D	ATE 2	2022 Mar	ch 1			<sup>••</sup> BH 3A-2	2
SOIL DESCRIPTION	PLOT		SAN	<b>IPLE</b>	1	DEPTH	ELEV.			lows/0.3m a. Cone	ter stion
	STRATA	ТҮРЕ	NUMBER	% RECOVERY	N VALUE or RQD	(m)	(m)	• <b>N</b>	/ater Co	ntent %	Piezometer Construction
GROUND SURFACE	07		4	RE	zv	0-	-91.65	20	40	60    80	
TOPSOIL <u>0.10</u> OVERBURDEN											
						1-	-90.65				
						2-	-89.65				
End of Borehole Practical refusal to augering at 2.18m depth								20	40	60 80 1 jth (kPa)	

# patersongroup Consulting SOIL PROFILE A Geotechnical Investigation

### SOIL PROFILE AND TEST DATA

▲ Undisturbed △ Remoulded

154 Colonnade Road South, Ottawa, On	tario k	∎ (2E 7J	5		Pr 11	oposed Deve 85 Beaverwo	elopme	ent	wa. Onta	rio	
DATUM Geodetic					1				FILE NO.	PG6160	
REMARKS									HOLE NO.		
BORINGS BY CME-55 Low Clearance	Drill			DA	TE	2022 March 1				BH 4-22	
SOIL DESCRIPTION	РГОТ		SAN	IPLE		-	.EV.		esist. Blo 0 mm Dia		Nell on
	STRATA	ТҮРЕ	NUMBER	% RECOVERY	VALUE SE ROD	(m) (i	m)	0 <b>V</b>	Vater Con	tent %	Monitoring Well Construction
GROUND SURFACE	5		NC	REC	N OF OF			20	40 60	0 80	Cor
TOPSOIL0.10		\$2\$\$\$\$1 -				- 0+90.	.67 –		0		
Hard to very stiff brown <b>SILTY</b>		SS AU	1 2	75	10	1-89.	.67		O		
		ss	3	42	7	2-88.			φ		
		ss	4	42	4	3-87.			Ò		
3.35 GLACIAL TILL: Compact brown silty sand to sandy silt with gravel, trace clay, cobbles and boulders		ss	5	50	2				D		
4 50		ss	6	50	30	4-86.		Ō			
End of Borehole 4.52	<u></u>										
Practical refusal to augering at 4.52m depth											
(GWL at 3.14 m depth - Mar 9, 2022)								20	40 60	0 80 1	00
	1								ar Strengt		-

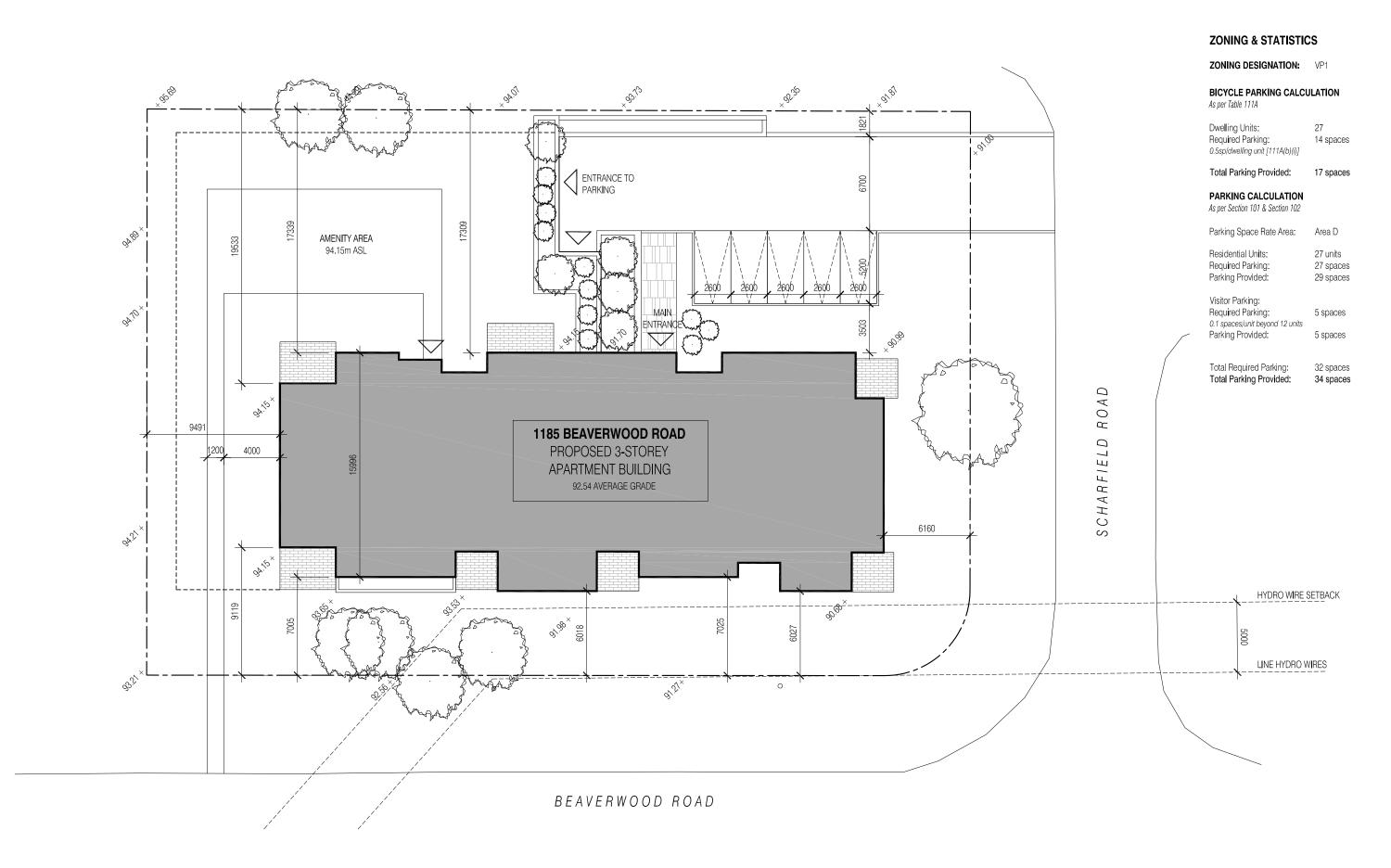


autocad drawings\geotechnical\pg61xx\pg6160\pg6160-1-test hole location p

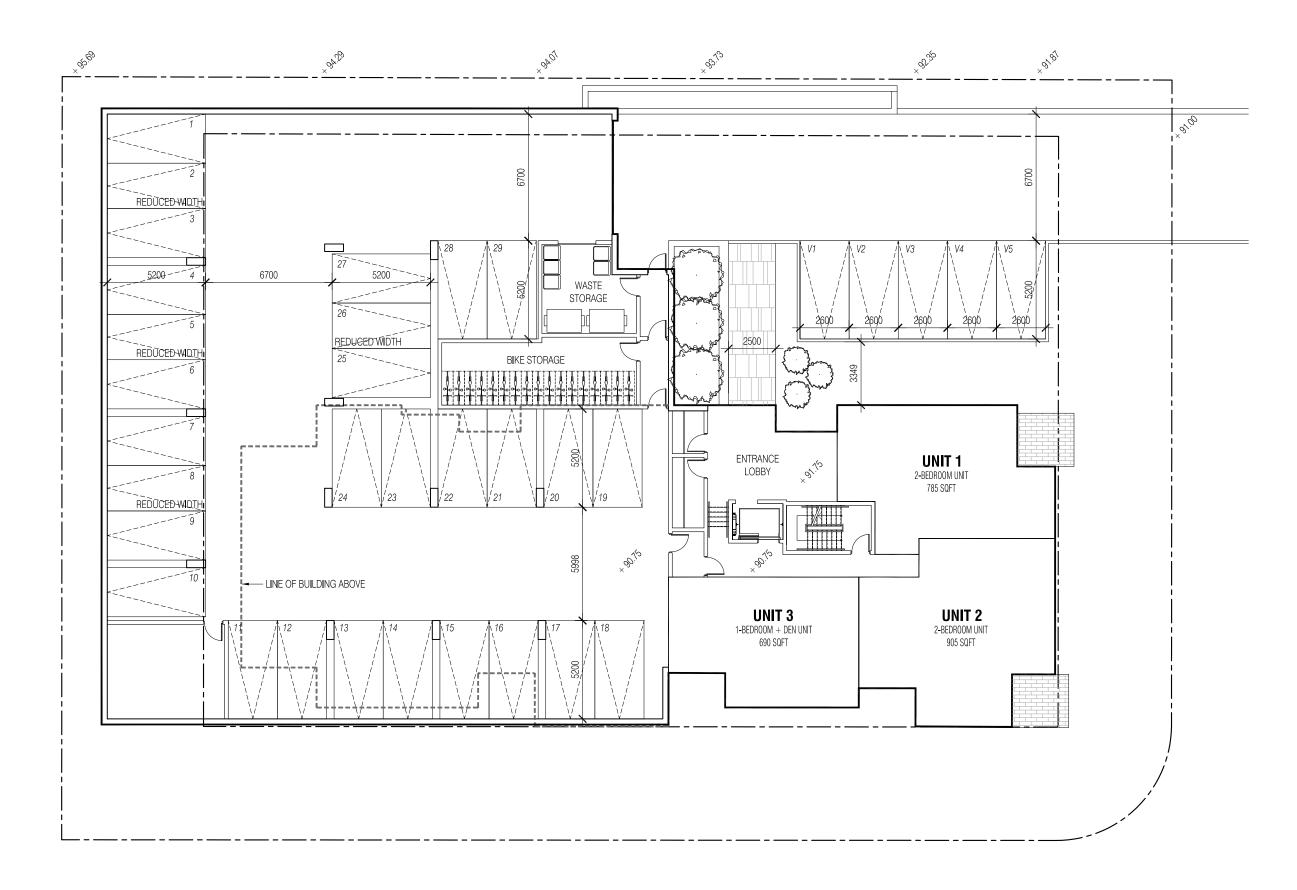
# **APPENDIX 3**

Project1 Studio Architects - Plan/Profile Drawings

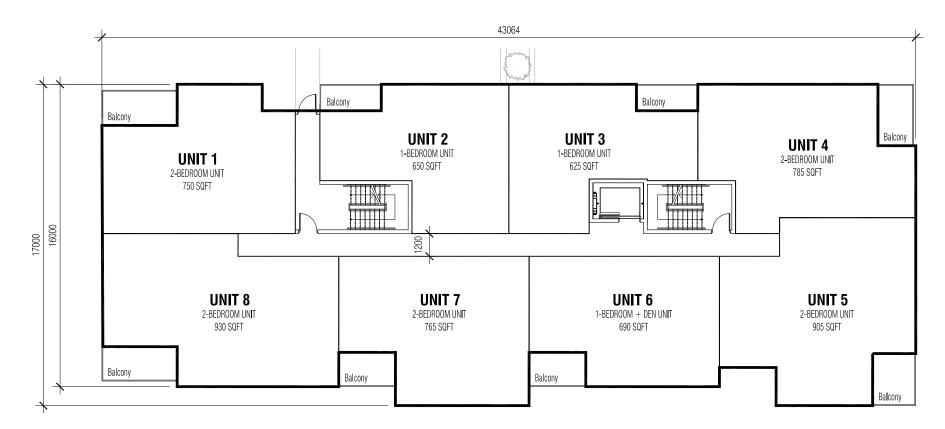
Correspondence



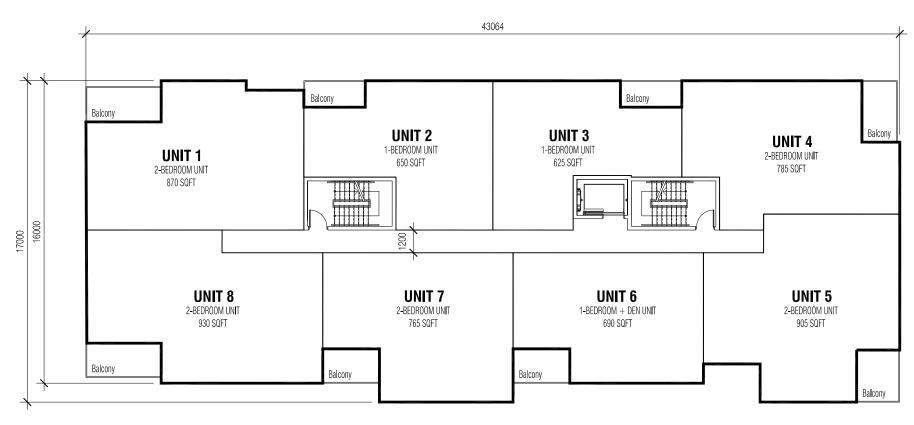
# project1 studio



## project1 studio

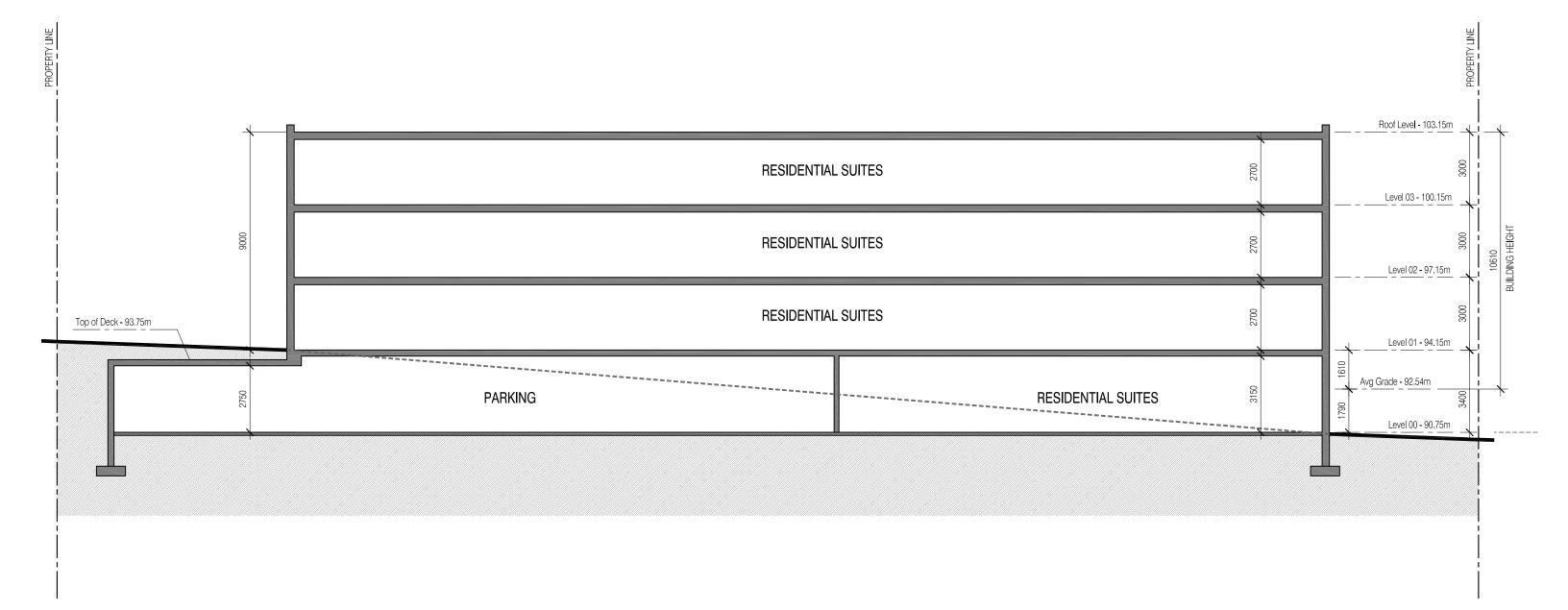


LEVEL 01 FLOOR PLAN



LEVEL 02 - 03 FLOOR PLANS







### 1185 BEAVERWOOD ROAD | 3-STOREYS

	BUILDING AREA CALCULATIONS								
Level	Gross Building Area	Gross Leasble Area	Efficiency						
Level 00	3,323.0	2,383.0	72%						
Level 01	6,952.0	6,109.0	88%						
Level 02	6,982.0	6,232.0	89%						
Level 03	6,982.0	6,232.0	89%						
TOTAL	24,239.0	20,956.0	86%						

		UNIT N	MATRIX		
Level	studio	1 bed	1bed+den	2 bed	TOTAL
Level 00	_	-	1	2	3
Level 01	-	2	1	5	8
Level 02	-	2	1	5	8
Level 03	-	2	1	5	8
TOTAL	0	6	4	17	27
	0%	22%	15%	63%	



#### **Mike Laflamme**

From:	Kearney, Michel <michel.kearney@ottawa.ca></michel.kearney@ottawa.ca>
Sent:	May 10, 2022 4:27 PM
То:	Erik Ardley
Cc:	Michael Killam; Mike Laflamme; Whittaker, Damien
Subject:	RE: Baseline Sampling Program - 1185 Beaverwood Road

Hi Erik,

The letter looks good from my perspective.

Best Regards, Michel

From: Erik Ardley <EArdley@patersongroup.ca>
Sent: May 10, 2022 4:12 PM
To: Kearney, Michel <Michel.Kearney@ottawa.ca>
Cc: Michael Killam <mkillam@patersongroup.ca>; mlaflamme@patersongroup.ca; Whittaker, Damien <Damien.Whittaker@ottawa.ca>
Subject: RE: Baseline Sampling Program - 1185 Beaverwood Road

CAUTION: This email originated from an External Sender. Please do not click links or open attachments unless you recognize the source.

ATTENTION : Ce courriel provient d'un expéditeur externe. Ne cliquez sur aucun lien et n'ouvrez pas de pièce jointe, excepté si vous connaissez l'expéditeur.

Good afternoon Michel,

I have attached a Homeowner Notification Letter for the Baseline Water Well Testing Program for the development to be located at 1185 Beaverwood Road for your approval. Ideally we will be sending our registered letters tomorrow. Please do not hesitate to reach out if you would like anything to be updated.

Thanks, Erik

Erik Ardley Hydrogeologist BSc. Geology, GIT APGO

## patersongroup

#### solution oriented engineering over 60 years serving our clients

154 Colonnade Road South Ottawa, Ontario, K2E 7J5 Tel: (613) 226-7381 Ext. 246 Cell: **613-808-9776**  Email: eardley@patersongroup.ca

From: Kearney, Michel <<u>Michel.Kearney@ottawa.ca</u>>
Sent: Wednesday, May 4, 2022 3:26 PM
To: Mike Laflamme <<u>MLaflamme@patersongroup.ca</u>>
Cc: Michael Killam <<u>MKillam@patersongroup.ca</u>>; Whittaker, Damien <<u>Damien.Whittaker@ottawa.ca</u>>
Subject: RE: Baseline Sampling Program - 1185 Beaverwood Road

Thanks Mike. I defer to your recent experiences.

### Michel

From: Mike Laflamme <<u>MLaflamme@patersongroup.ca</u>
Sent: May 04, 2022 3:21 PM
To: Kearney, Michel <<u>Michel.Kearney@ottawa.ca</u>>
Cc: Michael Killam <<u>mkillam@patersongroup.ca</u>>; Whittaker, Damien <<u>Damien.Whittaker@ottawa.ca</u>>
Subject: RE: Baseline Sampling Program - 1185 Beaverwood Road

Hey Michel,

It's no problem; thanks for the response.

We weren't planning to knock on doors as well. We've had much better success with the registered letters since we started using them a few months ago than we've ever had with knocking on doors (especially since COVID started).

Thanks,

Mike Laflamme, P.Geo.

# patersongroup

solution oriented engineering over 60 years serving our clients

154 Colonnade Road South Ottawa, Ontario, K2E 7J5 Tel: (613) 226-7381 Ext. 244 Email: <u>mlaflamme@patersongroup.ca</u>

From: Kearney, Michel <<u>Michel.Kearney@ottawa.ca</u>>
Sent: May 4, 2022 2:47 PM
To: Mike Laflamme <<u>MLaflamme@patersongroup.ca</u>>
Cc: Michael Killam <<u>MKillam@patersongroup.ca</u>>; Whittaker, Damien <<u>Damien.Whittaker@ottawa.ca</u>>
Subject: FW: Baseline Sampling Program - 1185 Beaverwood Road

Hi Mike,

Sorry for the delay in my response. The attached baseline sampling program locations are in accordance with our conversation. In addition to the registered letters, will you be knocking on doors?

### Best Regards,

#### Michel Kearney, P.Geo.

Senior Hydrogeologist Asset Management Infrastructure and Water Services Department

Hydrogéologue principal Gestion des actifs Direction générale des services d'infrastructure et d'eau

City of Ottawa | Ville d'Ottawa Cell: 613-606-5862 ottawa.ca/planning / ottawa.ca/urbanisme

From: Mike Laflamme <<u>MLaflamme@patersongroup.ca</u>>
Sent: May 03, 2022 1:55 PM
To: Kearney, Michel <<u>Michel.Kearney@ottawa.ca</u>>
Cc: Michael Killam <<u>mkillam@patersongroup.ca</u>>
Subject: FW: Baseline Sampling Program - 1185 Beaverwood Road

Afternoon Michel,

Hope you had a nice weekend (the weather was perfect)!

I wanted to follow up regarding the attached baseline sampling program for the site at 1185 Beaverwood Road. If you have a minute sometime this week, could you please take a quick look at the program and confirm you're ok for us to proceed.

If you have any questions, just let me know.

Thanks,

Mike Laflamme, P.Geo.

### patersongroup

solution oriented engineering over 60 years serving our clients

154 Colonnade Road South Ottawa, Ontario, K2E 7J5 Tel: (613) 226-7381 Ext. 244 Email: <u>mlaflamme@patersongroup.ca</u> From: Mike Laflamme Sent: April 21, 2022 12:33 PM To: Kearney, Michel <<u>Michel.Kearney@ottawa.ca</u>> Subject: FW: Baseline Sampling Program - 1185 Beaverwood Road

Afternoon Michel,

I just wanted to follow up regarding the baseline sampling program for the site on Beaverwood Road.

My client is looking to get started on this sooner rather than later so if you could review the details and get back to me as soon as you can, it would be greatly appreciated.

If you have any questions, just let me know.

Thanks,

Mike Laflamme, P.Geo.

## patersongroup

solution oriented engineering over 60 years serving our clients

154 Colonnade Road South Ottawa, Ontario, K2E 7J5 Tel: (613) 226-7381 Ext. 244 Email: <u>mlaflamme@patersongroup.ca</u>

From: Mike Laflamme
Sent: April 8, 2022 5:29 PM
To: Kearney, Michel <<u>Michel.Kearney@ottawa.ca</u>>
Subject: Baseline Sampling Program - 1185 Beaverwood Road

Afternoon Michel,

I've prepared a memo regarding the proposed baseline sampling program for my clients development at 1185 Beaverwood Road (see attached).

If you could take a few moments to review it sometime next week and get back to me, it would be greatly appreciated.

Have a nice weekend!

Thanks,

Mike Laflamme, P.Geo.

### patersongroup

solution oriented engineering over 60 years serving our clients

154 Colonnade Road South

ı

. .

' '

ı

This e-mail originates from the City of Ottawa e-mail system. Any distribution, use or copying of this e-mail or the information it contains by other than the intended recipient(s) is unauthorized. Thank you.

Le présent courriel a été expédié par le système de courriels de la Ville d'Ottawa. Toute distribution, utilisation ou reproduction du courriel ou des renseignements qui s'y trouvent par une personne autre que son destinataire prévu est interdite. Je vous remercie de votre collaboration.

This e-mail originates from the City of Ottawa e-mail system. Any distribution, use or copying of this e-mail or the information it contains by other than the intended recipient(s) is unauthorized. Thank you.

Le présent courriel a été expédié par le système de courriels de la Ville d'Ottawa. Toute distribution, utilisation ou reproduction du courriel ou des renseignements qui s'y trouvent par une personne autre que son destinataire prévu est interdite. Je vous remercie de votre collaboration.

This e-mail originates from the City of Ottawa e-mail system. Any distribution, use or copying of this e-mail or the information it contains by other than the intended recipient(s) is unauthorized. Thank you.

Le présent courriel a été expédié par le système de courriels de la Ville d'Ottawa. Toute distribution, utilisation ou reproduction du courriel ou des renseignements qui s'y trouvent par une personne autre que son destinataire prévu est interdite. Je vous remercie de votre collaboration.