

# Site Servicing Report

2625 Sheffield Road, Ottawa, Ontario

Amazon Logistics

60634622

October 2022

Kelby Lodoen Unseth, MCIP, RPP  
Planner II/Development Review  
City of Ottawa  
100 Laurier Avenue West, 4<sup>th</sup> Floor  
Ottawa, Ontario K1P 1J1

October 6, 2022

**Project #**  
60634622

**Subject: Site Servicing Report – 2625 Sheffield Road, Ottawa, Ontario**

Dear Mr. Unseth:

Please find our Site Servicing Report, which is provided in support of the proposed Site Plan Application for the proposed works located at 2625 Sheffield Road, Ottawa, Ontario, Canada (to be referred to in this report as "Site").

This report presents the stormwater management plan and how the layout of the proposed site servicing (sanitary, water, stormwater) satisfy requirements set by the City of Ottawa and the Ministry of Environment, Conservation, and Parks (MECP). Please also be advised that no portion of the Site is located within a regulated area designated by the Rideau Valley Conservation Authority (RVCA) as per Ontario Regulation 174/06.

We request an approval of the subject application. If you have any questions or require additional information or clarification, please do not hesitate to contact the undersigned at 519-650-8669 or via e-mail: [kosta.paliouras@aecom.com](mailto:kosta.paliouras@aecom.com).

Sincerely,  
**AECOM Canada Ltd.**



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Encl.

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## Quality Information

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**Site Servicing Report**  
2625 Sheffield Road, Ottawa, Ontario

## Prepared for:

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# Executive Summary

This report addresses the proposed site servicing at 2625 Sheffield Road in Ottawa, Ontario, Canada.

The proposed works consists of demolishing the existing building structure and construction of a proposed building structure with a regrade and repave an existing parking lot area. Due to the construction of the proposed building, additional water quality and quantity controls are required to prevent detrimental impacts to the downstream outlets (municipal infrastructure on Sheffield Road and Humber Place). The objective for these stormwater management facilities is to provide water quality treatment, water quantity control, and groundwater recharge in accordance with the City's requirements for development.

The proposed stormwater management facilities will consist of multiple infiltration basins and two (2) underground chamber storage systems (StormTech MC-3500 systems or approved equivalent) with the capacity to accept surface runoff up to and including the 100-year storm event for the proposed building and parking lot area and provide water quality and quantity treatment prior to discharging downstream. The proposed infiltration basins will consist of clear stone bedding and capture runoff from the roof areas to encourage groundwater recharge. The chamber storage systems will consist of storage chambers with clear stone granular material bedding, surrounded by an impermeable liner to discourage infiltration of runoff from the parking lot area. The proposed underground chamber storage systems will then discharge to the municipal infrastructure on Humber Place and Sheffield Road and ultimately to Green's Creek.

The proposed stormwater management measures have met the design objectives of the City of Ottawa.

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# 1. Introduction

AECOM Canada Limited (AECOM) has prepared the following Site Servicing Report for the industrial facility located at 2625 Sheffield Road in Ottawa, Ontario, Canada (to be referred to in this report as “Site”).

The proposed works consists of demolishing the existing building structure and construction of a proposed building structure with a regrade and repave an existing parking lot area. Due to the construction of the proposed building, additional water quality and quantity controls are required to prevent detrimental impacts to the downstream outlets (municipal infrastructure on Sheffield Road and Humber Place). The key objective of this report is to provide a summary of existing Site conditions and illustrate how the proposed stormwater management measures would address adverse water quality/quantity, erosion control, and water balance objectives detailed by City of Ottawa staff and regulatory agencies.

## 2. Background Information

### 2.1 General Site Information

The Site is located at 2625 Sheffield Road in Ottawa, Ontario (Site location is provided in **Figure 1**). The Site is bordered by Humber Place to the south, industrial property to the north, Sheffield Road to the west, and a CN Rail railway to the east. The Site is approximately 7.05 hectares (ha) in total size, with an existing building structure footprint of approx. 3.346 ha.

The existing building structure was constructed in multiple stages. The Site was first developed in the 1960s, with building expansions in the 1970s and 1990s.

A Draft Geotechnical Study was completed by AECOM for the Site in January 2021 and borehole logs are provided in **Appendix A**. According to borehole investigations within the vicinity of the Site, the underlying soils consist of clayey silt material. No groundwater was observed during the investigation and in the monitoring wells.

The Site is located within the Ottawa Drain, a tributary of Green's Creek. AECOM has reviewed updated regulated area mapping available from the Rideau Valley Conservation Authority (RVCA) via the online regulated area mapping tool and mapping is provided in **Appendix B**. No portions of the Site is located within a regulated area as per Ontario Regulation 174/06 (Regulation of Development, Interference, with Wetlands and Alterations to Shorelines and Watercourses) and a permit from the RVCA would not be required.

There is also no Certificate of Approval or Environmental Compliance Approval permit associated with the Site, according to Ministry of Environment, Conservation, and Parks (MECP) records. Pre-consultation with the MECP (included in **Appendix C**) indicates that no ECA is required for the Site, as under Ontario Regulation 525/98 states that Subsection 53 (1) and (3) of the Act do not apply to lands designed as:

- one parcel, for which the Site and all proposed works will be contained;
- that discharge into a storm sewer that is not combined, for which is not the case at the Site, as sanitary and storm services currently are and will continue to be separate;
- does not service industrial or a structure located on industrial land; and
- is not located on industrial land.

Ontario Water Resources Act defines industrial land as “land used for the production, processing, repair, maintenance or storage of goods of materials, or the processing, storage, transfer or disposal of waste, but does not include land used primarily for the purpose of buying or selling, (a) goods or materials other than fuel, or (b) services other than vehicle repair services.”

Though the Site is located within a “Heavy Industrial Zone” according to the zoning by-law, the primary purpose of the proposed development will be for the distribution of goods and material, with only van and truck traffic through the proposed parking lot area. There will be no machinery or on-site processes that would require industrial water use to discharge to the municipal system and no outdoor storage of processed material or any contaminate material. Contaminates would include total suspended solids (TSS), vehicular oil and chlorides from the parking lot area. The proposed infiltration basins will only accept discharge from the proposed roof areas and an impermeable liner is proposed for the proposed underground chamber storage systems and therefore none of the runoff from the parking lot area will infiltrated into the underlying soil. The level of concern would be minimal.



Aerial photography provided by: City of Ottawa (2019)

- Legend**
- Property Limit
  - Base Layers**
  - Railway
  - Freeway
  - Watercourse



Base map provided by: MECP  Map Extents

|  |                |   |
|--|----------------|---|
| <p><b>Amazon LDC DYT3</b><br/> <b>2625 Sheffield Road</b><br/> <b>Site Servicing Report</b></p>  |                |   |
| <p><b>Site Location Plan</b></p>   |                |   |
|  |                |   |
| <p>Datum: North American 1983</p>  |                |   |
| <p>Feb, 2021</p>   | <p>1:5,000</p> | <p><b>Data Sources</b><br/>MECP, MMAH, City of Ottawa</p> |
| <p>P:60634622</p>  | <p>Rev:00</p>  |   |
| <p><b>AECOM</b></p>  |                | <p><b>Figure: 1</b></p>                                   |
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Project Location: E:\PRJ\AMZN\_LDC\_DYT3\_2625SHEFFIELD\AMZN\_LDC\_DYT3\_2625SHEFFIELD.swp  
Date Saved: 2/17/2021 10:36:46 AM User: orvis

## 2.2 Existing Water and Wastewater Services

The site is currently serviced from the existing 300 mm diameter watermain on Sheffield Road by two existing 200 mm diameter water service connections. The water service enters the west of the site through the office entrance driveway along Sheffield Road as well as the second most southern truck entrance. The service along the office entrance driveway supplies domestic water to the building in a 75 mm shoot-off, as well to an on-site hydrant system located around the building in a 200 mm diameter firemain. This firemain loop re-connects to the existing 300 mm diameter municipal main on Humber Place at the southeast corner of the site. The post-development design is not proposing any changes to the water servicing on the site.

The building currently discharges to two (2) sanitary services, one connection at the existing MH 1A on Sheffield and another connection to the existing MH 5A on Sheffield. The southerly sanitary service flow into a 200 mm sanitary flows in a 200 mm diameter service by gravity to the existing 375 mm diameter sanitary sewer on Sheffield Drive, in the southwest corner of the site.

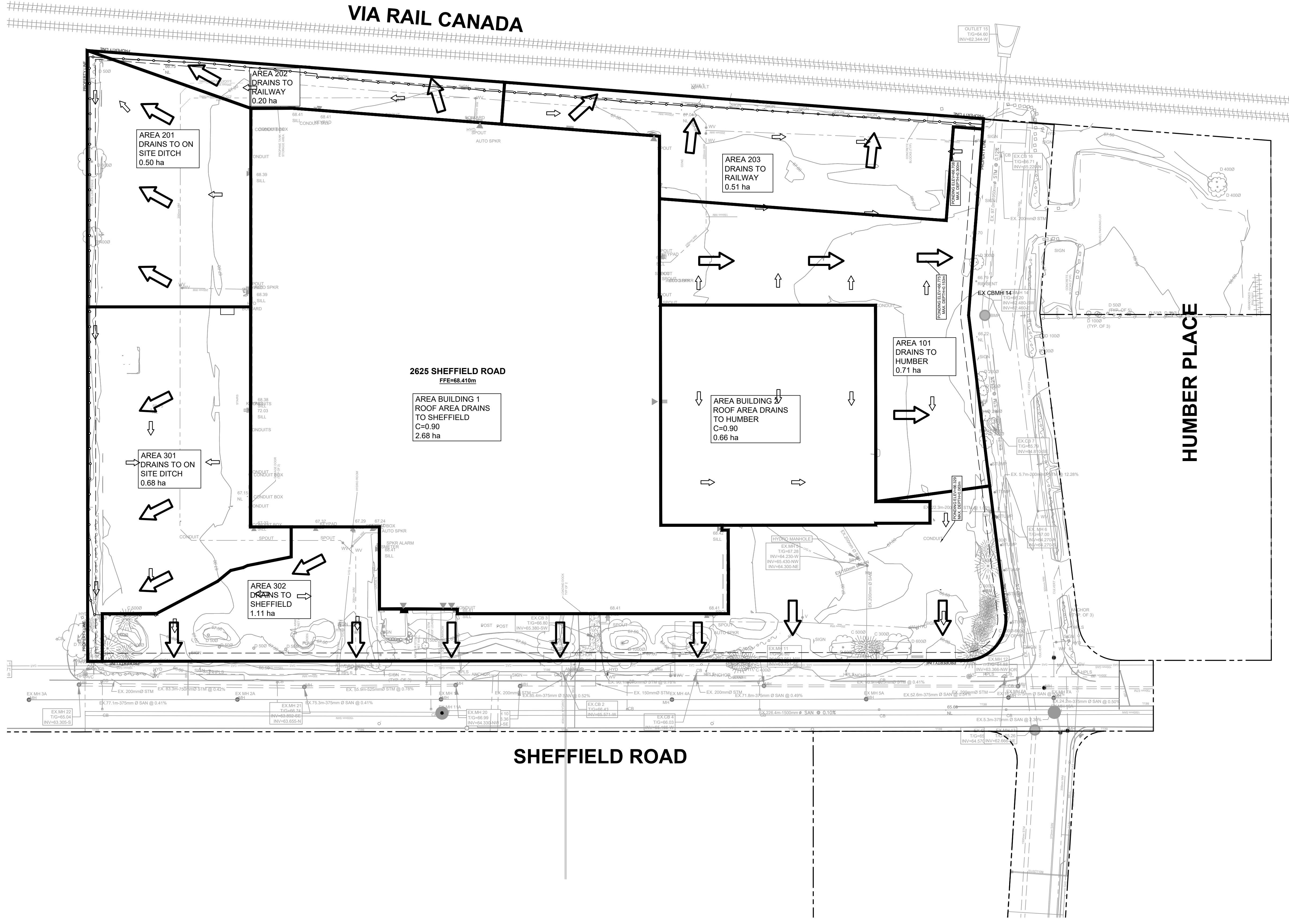
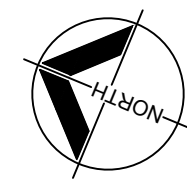
## 2.3 Existing Stormwater Management and Drainage Patterns

Existing drainage patterns at 2625 Sheffield Road (as indicated in **Figure 2** and **Figure 3**) consist of overland flow into an existing municipal storm sewer system and ultimately discharging into the City municipal system on Humber Place and Sheffield Road. Plan and profile servicing drawings for the Humber Place and Sheffield Road were obtained from the City and are provided in **Appendix D**.

The existing drainage patterns consist of the following flow paths:

- Runoff from the main parking lot area, located south of the existing building structure (Area 101) discharges overland directly into the existing City municipal storm sewer system on Humber Place. The existing storm sewer system ultimately discharges to the Ottawa Drain then to Green Creek.
- Runoff from the roof of the existing building structure is collected and discharges into the municipal storm sewer system on Sheffield Road and Humber place. A portion of the building roof structure (Building #1) discharges to the municipal storm sewer system on Sheffield Road, with another portion of the building roof structure (Building #2) discharges to the municipal storm sewer system on Humber Place.
- A portion of the existing parking lot area located north of the building structure, the access road east of the existing building structure, and portion of the main parking lot area (Area 200 series) discharges directly to a vegetated swale adjacent to the CN Rail railway and ultimately discharges to Green's Creek.
- A portion of the parking lot area located north of the existing building structure and the landscaped area adjacent to Sheffield Road (Areas 300 series) discharges directly to the City municipal storm sewer system on Sheffield Road. The existing storm sewer system ultimately discharges to Green's Creek.

According to site assessments, there are currently no on-Site surface water quality and quantity control infrastructure.



**SURVEY NOTES**

**METRIC NOTE**  
 ALL DISTANCES SHOWN HEREON ARE IN METERS AND CAN BE CONVERTED TO IMPERIAL FEET BY DIVIDING BY 0.3048.

**DISTANCE NOTE**  
 ALL DISTANCES ELECTRONICALLY MEASURED ON THIS PLAN ARE GRID DISTANCES.

**HORIZONTAL DATUM**  
 UNIVERSAL TRANSVERSE MERCATOR (UTM) PROJECTION, ZONE 18 NORTH, NAD-83 CSRS.

**VERTICAL DATUM**  
 NAD-83 VERTICAL DATUM - 1978 RE-ADJUSTMENT (GEODETIC)

**COMPLETION NOTE**  
 TOPOGRAPHIC DETAIL SHOWN HEREON WAS ACQUIRED IN JUNE, 2020 BY AECOM.

**PROPERTY BOUNDARIES**

PROPERTY BOUNDARY INFORMATION SHOWN HEREIN IS DERIVED FROM GIS AND FIELD OBSERVATIONS AND REGISTERED PLANS SR-12728 DATED MAY 25, 1989 AS WELL AS REF. NO. 8-783 GR DATED NOV 12, 1982. ALL DIMENSIONS ARE APPROXIMATE. THIS DOCUMENT IN ITSELF CAN NOT BE USED TO ESTABLISH PROPERTY LIMITS.

**SITE BENCHMARKS**

TBM #1 - TOP NUT OF HYDRANT LOCATED AT NORTH WEST CORNER OF 2625 SHEFFIELD ROAD ELEVATION = 67.198m

TBM #2 - STANDARD IRON BAR (SIB) LOCATED AT SOUTH WEST CORNER OF 2625 SHEFFIELD ROAD ELEVATION = 66.015m

**LEGEND**

- PROPERTY LINE
- SIB PROPERTY BAR
- 247.00 EX. CONTOUR
- X 247.50 EX. SPOT ELEVATION
- ~ EX. VEGETATION
- EX. CB, DCB, CBMH AND MH
- ~ EX. SWALE/ DITCH
- EX. CHAIN LINK FENCE
- EX. POST & WIRE FENCE
- EXISTING DRAINAGE AREA BOUNDARY
- ➔ MAJOR OVERLAND FLOW



**PROJECT**  
 DYT3  
 OTTAWA, ONTARIO  
 2625 SHEFFIELD ROAD

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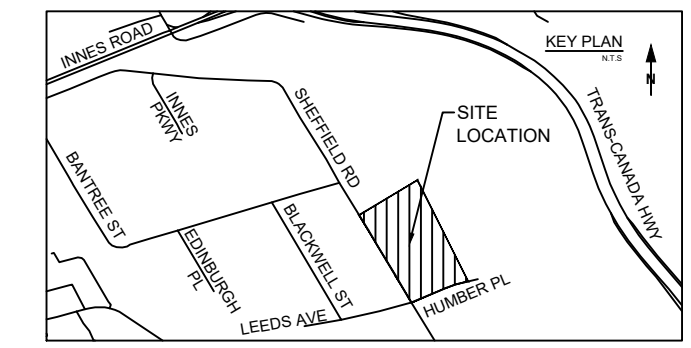
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**KEY PLAN**



**PROJECT NUMBER**

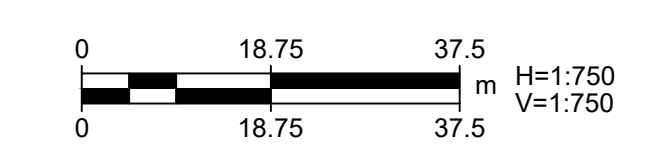
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**SHEET TITLE**

EXISTING STORM WATER DRAINAGE AREAS

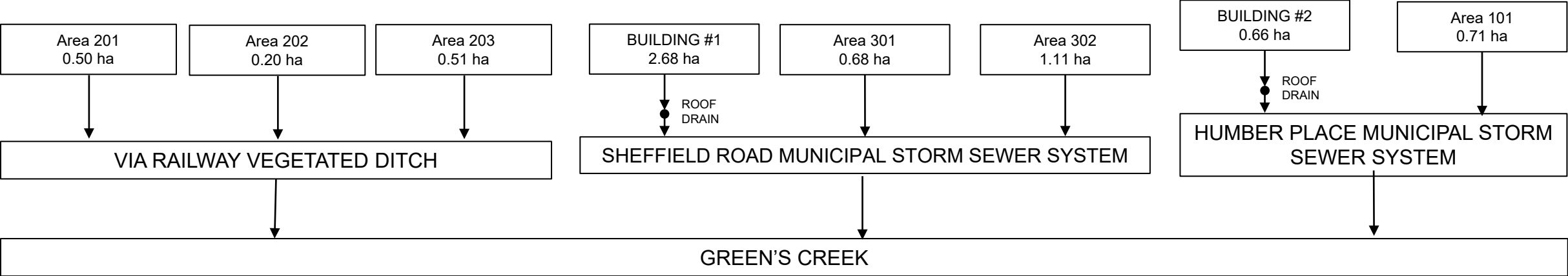
**SHEET NUMBER**

FIGURE 2



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**FIGURE 3: EXISTING CONDITIONS FLOW SCHEMATIC (DYT3)**



### 3. Design Criteria

Stormwater management within City of Ottawa conforms to the following regulatory documents:

- City of Ottawa Sewer Design Guidelines (October 2012) and subsequent Technical Bulletins.
- Ministry of Environment, Conservation, and Parks (MECP) Stormwater Management Planning and Design Manual (MECP, March 2003)
- TRCA/Credit Valley Conservation (CVC)/Lake Simcoe Region Conservation Authority (LSRC) Low Impact Development Stormwater Management Planning and Design Guide (2019)

Pre-consultation was completed in December 2020 with the City of Ottawa and RVCA, and comments are included in **Appendix C**. Based on the prevailing policy framework, general design criteria, objectives and practices have been identified to complete the assessment of the proposed drainage infrastructure within the study area limits using current policies and guidelines. Below are the design criteria, based on those regulations noted above:

- **Water Quantity**  
It is the policy of the City to require that 100-year post-development peak flows are controlled to pre-development 2-year peak flow to Humber Place. In their pre-consultation response, the City has requested that the allowable runoff coefficient for the pre-development drainage area is the lesser of the existing pre-development conditions to a maximum of 0.5.
- **Water Quality**  
According to the correspondence from the RVCA, the proposed water quality control measures are to be designed to provide Enhanced (Level 1) water quality control (80% total suspended solids [TSS] removal) and shall use the treatment train approach to stormwater management with source, conveyance and end-of-pipe measures.
- **Water Balance**  
The general hydrological cycle of the Site to be maintained, by replenishing the underlying aquifer through infiltration (where possible). The vast majority of the current Site conditions is impervious and the proposed works would have similar impervious levels. Where possible, roof drainage will be directed to proposed infiltration basins.

According to the 2012 TRCA/CVC Low Impact Development (LID) Guidelines though, it is not advised that runoff from high traffic areas to infiltrate into the underlying soils. Due to the purpose of the Site, there will be consistent van and truck traffic through the proposed parking lot area. The extent of untreated surface runoff discharging into any proposed infiltrative infrastructure during proposed conditions would originate from parking lot area and would include high levels of TSS and untreated contaminants such as oil and chlorides. Utilizing infiltrative infrastructure as part of the "treatment train" approach, before discharging through an oil/grit separator, would result in the infiltrative infrastructure becoming clogged with sediment quickly (becoming more ineffective when used in low permeable underlying soils) and allow for contaminants such as chlorides and oil to infiltrate into the groundwater when operational.

Additional measures that were consider include the following:

- Maintaining existing drainage patterns, where possible;
- Adjoining and/or downstream properties not to be adversely impacted by the proposed development;
- Water quality and quantity of runoff discharged from the Site to be controlled at the source;
- Discharge water may not also exceed over 45 degrees Celsius; and
- Erosion is limited to preserve the stability of small streams and rivers.

## 4. Proposed Conditions Site Servicing

Proposed Conditions Site Servicing Drawings are provided at the end of the report.

### 4.1 Proposed Water and Wastewater Services

#### 4.1.1 Water Supply Servicing Design

The development is proposed to be serviced via two 200 mm diameter service laterals, one located on the northwest side through the office entrance driveway along Sheffield Road and the other one located northeast side of the proposed building connected by the about mentioned loop.

The following table summarizes the preliminary water supply demand estimate for the proposed development based on Ottawa’s Water Distribution Design Guidelines and fire flow requirements using Fire Underwriters Survey (FUS) method. Refer to **Appendix E** for detailed calculations.

**Table 1: Water Demand Proposed Conditions**

| Parameter                                  | Demand (L/s) | Demand (gpm) |
|--|--------------|--------------|
| <b>Average Daily Demand</b>                | 2.86         | 45.33        |
| <b>Max. Day Demand</b>                     | 4.29         | 68.00        |
| <b>Peak Hour Demand</b>                    | 7.72         | 122.36       |
| <b>Fire Flow Demand</b>                    | 267.00       | 4232.05      |
| <b>Total Demand = Max. Day + Fire Flow</b> | 271.29       | 4300.05      |

Boundary conditions have been requested to the City of Ottawa, once the information is available the above calculations may be evaluated/ revised as to conform all relevant City Guidelines and Policies.

#### 4.1.2 Sanitary Servicing Design

It is anticipated that the proposed development will discharge to the two (2) existing sanitary connections mentioned above via 200 mm diameter service laterals.

The post-development sanitary flow was calculated according to Ontario Building Code section 7. Refer to **Appendix E** for detailed calculations.

**Table 2: Sanitary Proposed Conditions**

| Parameter                       | Flows (L/s) | Flows (gpm) |
|---------------------------------|-------------|-------------|
| <b>Sanitary Flow (Building)</b> | 4.35        | 69          |

Boundary conditions have been requested to the City of Ottawa, once the information is available the above calculations may be evaluated/ revised as to conform all relevant City Guidelines and Policies.

## 4.2 Proposed Stormwater Management and Drainage Patterns

Due to the demolition of the existing building structure and the expansion of the parking lot area, additional surface runoff will discharge off-Site and would require additional water quality and quantity control to not cause detrimental impacts to the downstream outlet.



Subcatchments under the proposed conditions were revised as shown in **Figure 4** and the respective flow schematic is shown in **Figure 5**. Proposed drainage patterns consist of the following flow paths:

- Runoff from a portion of the proposed roof of the building structure (Area 101) will be collected and discharges into a proposed infiltration basin to store up to 10 mm depth of runoff (Calculations are provided in **Appendix F**). The proposed infiltration basins will consist of 50 mm diameter clear stone, with an overflow outlet to the proposed storm sewer system and ultimately to the municipal storm sewer system on Sheffield Road. The municipal storm sewer system ultimately discharges to Green's Creek. Infiltration calculations are provided in .
- The parking lot area located north of the proposed building structure and existing vegetated area (Areas 1 to 10) will be regraded to allow conveyance of all storm events up to and including the 100-year storm event through a proposed storm sewer infrastructure (sizing calculations provided in **Appendix G**). Surface ponding will be limited to 0.30 m depth over the proposed catch basin and catch basin structures during storm events greater than the 100-year storm event.

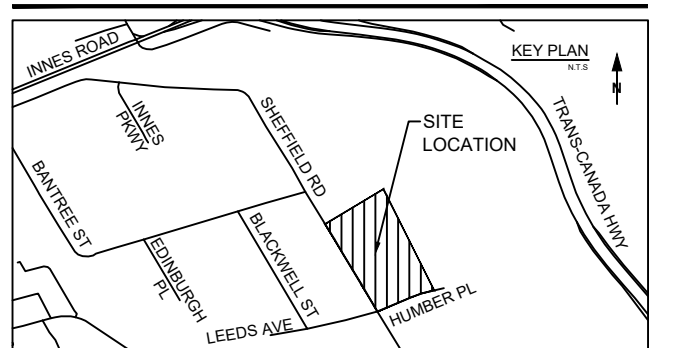
The proposed storm sewer system will discharge into a proposed underground storage system (StormTech MC-3500 or approved equivalent with total storage volume capacity of approximately 1,530 m<sup>3</sup>) to provide water quality and quantity control. Stage-storage table and product information for the proposed underground storage system is provided in **Appendix H**. The proposed system consists of an open bottom chamber, with surface runoff intercepted by the open-bottom chambers, which will then enter into the underground stone reservoirs and discharged controlled off-Site. The underground storage system will be wrapped with impermeable liner to discourage infiltration of surface runoff from the parking lot area. The system will also provide pre-treatment, which will consist of a row of chambers (known as an 'isolator row') wrapped in woven geotextile fabric (with two layers at the bottom). This acts as a filter strip that provides additional enhanced suspended solids and pollutant removal while providing surface area for runoff reduction.

The proposed underground storage system will then discharge into the proposed MH44 via two (2) outlet pipes w/ orifice plates to control flow during various storm events. A 75 mm orifice opening on a proposed 300 mm pipe will control flow for storms less than the 4-hour 25 mm storm event, allowing for discharge over a minimum 24-hr detention period. For storm event larger than the 4-hour 25 mm storm event, a proposed 150 mm pipe will provide additional flow control for discharging downstream.

The propose MH44 ultimately discharges to a proposed oil/grit separator (OGS, ADS FD-5HC or approved equivalent) to provide water quality control during first-flush conditions. The proposed OGS unit is Canadian ETV certified and is sized as part of a proposed treatment train approach to ultimately provide Enhanced-level treatment from the proposed parking lot areas. Sizing calculations and Canadian ETV certification for the proposed OGS unit is provided in **Appendix G**. Ultimately the proposed OGS discharges into the existing municipal storm sewer system on Sheffield Road and to Green's Creek.

- A portion of the landscaped area and entrance way along Sheffield Road (Area 2003) discharges to the existing municipal storm sewer system on Sheffield Road and ultimately to Green's Creek.
- Runoff from a portion of the proposed roof of the building structure (Area 102 and 103) will be collected and discharges into a proposed infiltration basin to store up to 10 mm depth of runoff. The proposed infiltration basins will consist of 50 mm diameter clear stone, with an overflow outlet to the proposed storm sewer system and ultimately to the municipal storm sewer system on Sheffield Road. The municipal storm sewer system ultimately discharges to Green's Creek. Infiltration calculations are provided in **Appendix F**.

| I/R | DATE | DESCRIPTION |
|-----|------|-------------|
|     |      |             |
|     |      |             |
|     |      |             |
|     |      |             |
|     |      |             |



**SURVEY NOTES**

**METRIC NOTE**  
ALL DISTANCES SHOWN HEREON ARE IN METERS AND CAN BE CONVERTED TO IMPERIAL FEET BY DIVIDING BY 0.3048.

**DISTANCE NOTE**  
ALL DISTANCES ELECTRONICALLY MEASURED ON THIS PLAN ARE GRID DISTANCES.

**HORIZONTAL DATUM**  
UNIVERSAL TRANSVERSE MERCATOR (UTM) PROJECTION, ZONE 18 NORTH, NAD-83 CSRS.

**VERTICAL DATUM**  
NAD-83 VERTICAL DATUM - 1978 RE-ADJUSTMENT (GEODETIC)

**COMPLETION NOTE**  
TOPOGRAPHIC DETAIL SHOWN HEREON WAS ACQUIRED IN JUNE, 2020 BY AECOM.

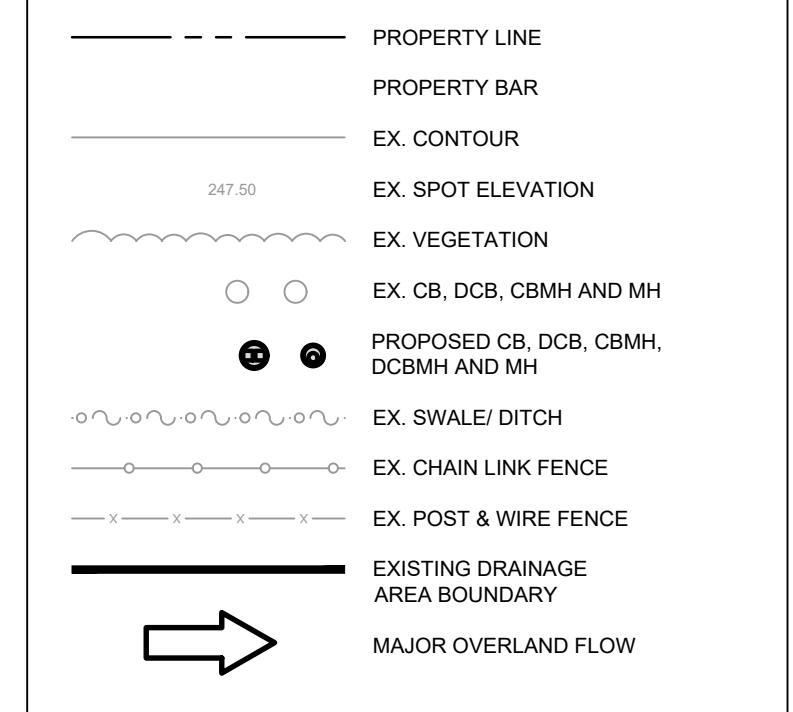
**PROPERTY BOUNDARIES**

PROPERTY BOUNDARY INFORMATION SHOWN HEREIN IS DERIVED FROM GIS AND FIELD OBSERVATIONS AND REGISTERED PLANS SR-17278 DATED MAY 25, 1989 AS WELL AS REF. NO. 8-783 GR DATED NOV 12, 1992. ALL DIMENSIONS ARE APPROXIMATE. THIS DOCUMENT IN ITSELF CANNOT BE USED TO ESTABLISH PROPERTY LIMITS.

**SITE BENCHMARKS**

TBM #1 - TOP NUT OF HYDRANT LOCATED AT NORTH WEST CORNER OF 2625 SHEFFIELD ROAD ELEVATION = 67.198m

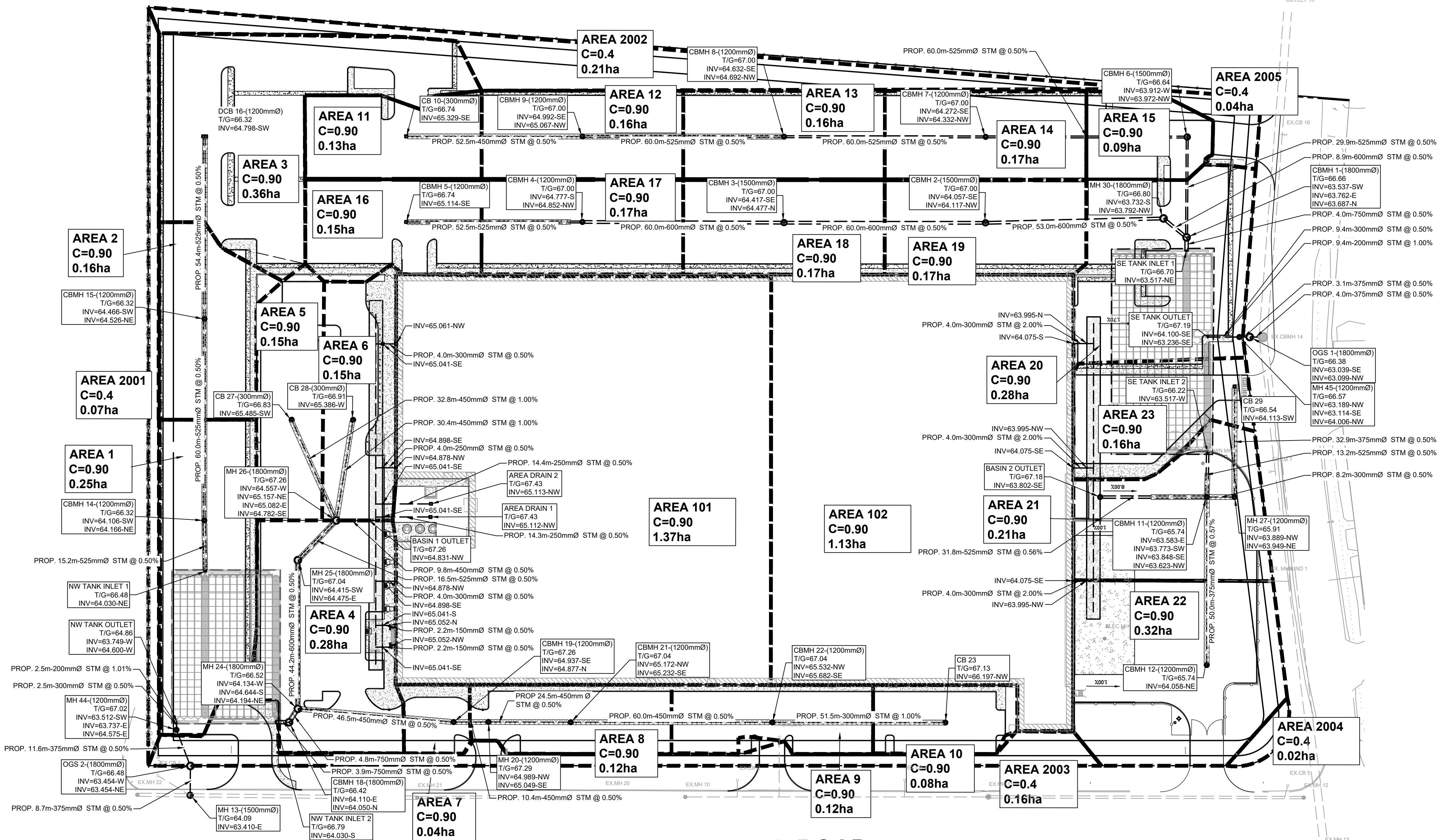
TBM #2 - STANDARD IRON BAR (SIB) LOCATED AT SOUTH WEST CORNER OF 2625 SHEFFIELD ROAD ELEVATION = 66.015m



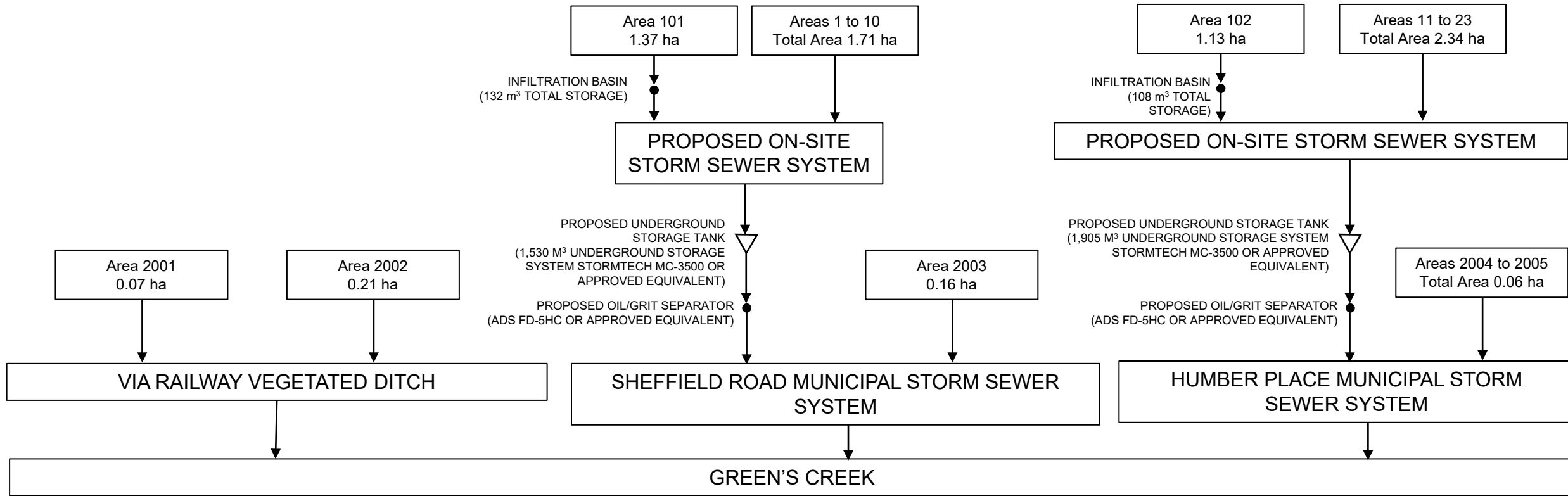
HUMBER PLACE

VIA RAIL CANADA

SHEFFIELD ROAD



**FIGURE 5: PROPOSED CONDITIONS FLOW SCHEMATIC (DYT3)**



- The parking lot area located south and west of the proposed building structure and existing vegetated area (Areas 11 to 24) will be regraded to allow conveyance of all storm events up to and including the 100-year storm event through a proposed storm sewer infrastructure (sizing calculations provided in **Appendix G**). Surface ponding will be limited to 0.30 m depth over the proposed catch basin and catch basin structures during storm events greater than the 100-year storm event.

The proposed storm sewer system will discharge into a proposed underground storage system (StormTech MC-3500 or approved equivalent with total storage volume capacity of approximately 1,905 m<sup>3</sup>) to provide water quality and quantity control. Stage-storage table and product information for the proposed underground storage system is provided in **Appendix H**. The proposed system consists of an open bottom chamber, with surface runoff intercepted by the open-bottom chambers, which will then enter into the underground stone reservoirs and discharged controlled off-Site. The underground storage system will be wrapped with impermeable liner to discourage infiltration of surface runoff from the parking lot area. The system will also provide pre-treatment via an isolator row.

The proposed underground storage system will then discharge into the proposed MH45 via two (2) outlet pipes w/ orifice plates to control flow during various storm events. A 75 mm orifice opening on a proposed 300 mm pipe will control flow for storms less than the 4-hour 25 mm storm event, allowing for discharge over a minimum 24-hr detention period. For storm event larger than the 4-hour 25 mm storm event, a proposed 300 mm pipe will provide additional flow control for discharging downstream.

The propose MH45 ultimately discharges to a proposed oil/grit separator (OGS, ADS FD-5HC or approved equivalent) to provide water quality control during first-flush conditions. The proposed OGS unit is Canadian ETV certified and is sized as part of a proposed treatment train approach to ultimately provide Enhanced-level treatment from the proposed parking lot areas. Sizing calculations and Canadian ETV certification for the proposed OGS unit is provided in **Appendix G**. The proposed OGS discharges into the existing municipal storm sewer system on Humber Place and ultimately to Green's Creek.

- A portion of the landscaped area along Humber Place (Areas 2004 and 2005) discharges to the existing municipal storm sewer system on Humber Place and ultimately to Green's Creek.
- A portion of the landscaped area along the CN Rail (Area 2002) discharges to the CN Railway land and ultimately to Green's Creek

## 4.3 Water Quantity

### 4.3.1 Hydrological Model Development

AECOM developed PCSWMM (Personal Computer Stormwater Management Model, 2021 version 7.4.3240) model for both existing and proposed conditions to confirm and compare the proposed peak flow and runoff volumes from the Site to those under existing conditions.

Site conditions were determined using aerial photography, discussions with design staff, and Site inspections. General modelling Site parameters are listed in **Table 3**. Existing and proposed conditions catchment parameters are provided in **Appendix I** and **Appendix J** respectively. Stage-storage and stage-discharge curves presented in **Appendix H** were provided by the manufacturer for the underground retention chamber system and were included in the hydrological model for analysis.

**Table 3: Main Hydrological Parameters Used**

| Hydrological Parameters                                   | Values |
|---|--------|
| <b>Manning Roughness Coefficient (Impervious Surface)</b> | 0.013  |
| <b>Manning Roughness Coefficient (pervious Surface)</b>   | 0.2    |
| <b>Depression Storage (Impervious Surface)</b>            | 1.57   |
| <b>Depression Storage (Pervious Surface)</b>              | 4.67   |
| <b>Drying Time</b>  | 7      |
| <b>Maximum Infiltration Rate</b>                          | 75     |
| <b>Minimum Infiltration Rate</b>                          | 0.5    |

The model was simulated for 4-hour 25 mm storm event, Chicago 3-hour and 6-hour 2-year, 5-year and 100-year design storm events which were derived from Section 5.4.2 and 5.4.3.2 respectively of the City of Ottawa Stormwater Management Design Guidelines (October 2012). Rainfall amounts are provided in **Table 4**. The proposed conditions peak discharge rates leaving the Site would be compared to that under existing condition to design the stormwater management requirements for water quantity and erosion control.

**Table 4: Rainfall Amounts**

| Storm Event         |        | Rainfall Amount (mm) |
|---------------------|--------|----------------------|
| <b>4-hour 25 mm</b> |        | 25.00                |
| <b>2-year</b>       | 3-hour | 31.88                |
|                     | 6-hour | 36.86                |
| <b>5-year</b>       | 3-hour | 42.54                |
|                     | 6-hour | 49.04                |
| <b>100-year</b>     | 3-hour | 71.68                |
|                     | 6-hour | 82.33                |

### 4.3.2 Hydrological Model Results

The PCSWMM hydrological modelling simulations were completed for existing and proposed Site conditions, with output files provided in **Appendix I** and **Appendix J** respectively. Peak flows to the City’s municipal storm sewer system on Humber Place and Sheffield Road for the 25 mm storm and Chicago 3-hr and 6-hr, 2-year, 5-year and 100-year storm events during existing and proposed conditions are provided in **Table 5** and **Table 6**, respectively. A stage-discharge table of the proposed north and south underground storage system is presented in **Table 7** and **Table 8**, respectively.

The hydrological model produced the following results:

- For proposed conditions, as per City guidelines and reiterated during pre-consultation, the 100-year proposed development discharge to Humber Place and Sheffield Road was compared to the 5-year existing development flow rate (with a runoff coefficient of 0.5). Utilizing the proposed stormwater management measures indicated in Section 4.2, proposed conditions discharge rates to Humber Place and Sheffield Road will be maintained to less than the allocated existing conditions discharge rate. For **Table 5** and **Table 6** below, flows were taken at the outfall node.
- Maximum runoff volumes and water depths within the proposed underground storage system were modelled during the 6-hour 100-year storm event.

**Table 5: Simulated Discharge Rate to Humber Place (m<sup>3</sup>/s)**

| Scenario | Drainage Area (ha) | 25 mm | 2-year Chicago |       | 5-year Chicago |       | 100-year Chicago |       |
|----------|--------------------|-------|----------------|-------|----------------|-------|------------------|-------|
|          |                    |       | 3-hr           | 6-hr  | 3-hr           | 6-hr  | 3-hr             | 6-hr  |
| Existing | 1.370              | 0.090 | 0.150          | 0.150 | 0.210          | 0.220 | 0.380            | 0.390 |
| Proposed | 3.53               | 0.01  | 0.012          | 0.018 | 0.055          | 0.061 | 0.127            | 0.135 |

**Table 6: Simulated Discharge Rate to Sheffield Road (m<sup>3</sup>/s)**

| Scenario | Drainage Area (ha) | 25 mm | 2-year Chicago |       | 5-year Chicago |       | 100-year Chicago |       |
|----------|--------------------|-------|----------------|-------|----------------|-------|------------------|-------|
|          |                    |       | 3-hr           | 6-hr  | 3-hr           | 6-hr  | 3-hr             | 6-hr  |
| Existing | 4.47               | 0.300 | 0.480          | 0.490 | 0.690          | 0.730 | 1.220            | 1.280 |
| Proposed | 3.24               | 0.030 | 0.039          | 0.042 | 0.067          | 0.079 | 0.219            | 0.236 |

**Table 7: Proposed Storage – Stage-Discharge (DYT3-N – 6-hour Storm Duration)**

| Storm Event | Water Depth m | Water Elevation m | Storage Volume m <sup>3</sup> | Peak Flow (m <sup>3</sup> /s) |        | Max. Outflow (m <sup>3</sup> /s) |
|-------------|---------------|-------------------|-------------------------------|-------------------------------|--------|----------------------------------|
|             |               |                   |                               | 75 mm Orifice                 | 200 mm |                                  |
| 25 mm*      | 0.74          | 64.49             | 587.0                         | 0.010                         | 0      | <b>0.010</b>                     |
| 2-year      | 0.93          | 64.68             | 783.0                         | 0.012                         | 0.015  | <b>0.027</b>                     |
| 5-year      | 1.06          | 64.81             | 924.6                         | 0.013                         | 0.061  | <b>0.074</b>                     |
| 100-yr      | 1.51          | 65.26             | 1371                          | 0.014                         | 0.208  | <b>0.223</b>                     |

Note: \* – 4-hour storm duration

**Table 8: Proposed Storage - Stage-Discharge (DTY3-S – 6-hour Storm Duration)**

| Storm Event | Water Depth m | Water Elevation m | Storage Volume m <sup>3</sup> | Peak Flow (m <sup>3</sup> /s) |        | Max. Outflow (m <sup>3</sup> /s) |
|-------------|---------------|-------------------|-------------------------------|-------------------------------|--------|----------------------------------|
|             |               |                   |                               | 75 mm Orifice                 | 200 mm |                                  |
| 25 mm*      | 0.70          | 63.93             | 679.7                         | 0.010                         | 0      | <b>0.010</b>                     |
| 2-year      | 0.91          | 64.15             | 956.8                         | 0.012                         | 0.007  | <b>0.018</b>                     |
| 5-year      | 1.04          | 64.27             | 1115.0                        | 0.012                         | 0.048  | <b>0.060</b>                     |
| 100-yr      | 1.54          | 64.78             | 1728                          | 0.015                         | 0.117  | <b>0.132</b>                     |

Note: \* – 4-hour storm duration

## 4.4 Water Quality

Annual TSS loading removal calculations were completed to determine if the proposed stormwater management measures would meet regulatory requirements for TSS. Treatment effectiveness information for the OGS and isolator row are provided in **Appendix H**.

Currently, there are no on-Site water quality controls. According to the calculations (summarized in **Appendix G**), the proposed stormwater management measures would provide over 80% annual pollutant loadings removal for TSS (and associated contaminants associated with particulates). The proposed OGS and isolator row, working as part of a ‘treatment train’ approach, will improve water quality discharging from the Site.

## 5. Erosion and Sediment Control

All activities should be controlled to prevent the entry of petroleum products, debris, rubble, concrete, or other deleterious substances into the natural features during construction. To prevent the discharge of these substances, several on-Site erosion and sediment controls (E&SC) measures are recommended. These would include the following E&SC measures (at a minimum):

- Light duty silt fencing; and
- Vegetate exposed graded soils with native, non-invasive grass seed species until final landscaping transpires.

These E&SC controls are illustrated in drawings provided in **Appendix E**. The E&SC Plan is in concordance with City and MECP guidelines and are recommended to be inspected daily, maintained, and continuously evaluated and upgraded when necessary or when directed by AECOM or City staff. The E&SC controls would be required to be installed prior to construction, especially prior to Site clearing. During construction, the selected contractor should monitor the local weather forecast to anticipate weather conditions and inspection of the E&SC controls should occur within 24 hrs of a 15 mm or greater rainfall event. Additional E&SC materials should be kept on-Site for emergencies and repairs. The selected contractor would seek final permission for the stockpile of material and storage of petroleum products and ensure that the proper E&SC controls are in place prior to placement or storage of material on-Site. At the end of construction, E&SC controls should be removed only when the Site conditions have been stabilized and vegetation has been established on disturbed areas, as approved by the on-Site inspector and City staff.

Groundwater levels is expected to fluctuate seasonally and dependent on precipitation events. The dewatering may not be required as no groundwater was observed during the current investigation. However, the dewatering assessment will be done during the construction, if necessary.

Please note that the E&SC Plan is a dynamic document that may be subject to change or modifications as a result of site developments or changes on-Site.

## 6. Operations and Maintenance

To meet regulatory requirements, the proposed stormwater management measures would need to be operated and maintained regularly effectively and efficiently. The following operation and maintenance measures would be required once the proposed stormwater management measures have been installed and in operation:

- The underground retention chamber system, isolator row, and OGS should be operated and maintained as per manufacturer's recommendations. The Operations and Maintenance (O&M) reports for the recommended products are provided in **Appendix G** and **H** respectively.
- The catch basins and storm sewer systems should be inspected and clean of sediment accumulation, with catch basin sumps to be clear of sediment accumulated as needed.



## 7. Conclusions

The proposed stormwater management facility meets the design objectives of the City.

# Drawings



# Appendix **A**

## Geotechnical Report





**LEGEND**

- Geotechnical Borehole - 1.5m Depth - Asphalt Pavement
- Geotechnical Borehole/Corehole - 1.5m Depth - Asphalt Pavement

**NOTES:**

This drawing has been prepared for the use of AECOM's client and may not be used, reproduced or relied upon by third parties, except as agreed by AECOM and its client, as required by law or for use by governmental reviewing agencies. AECOM accepts no responsibility, and denies any party that modifies this drawing without AECOM's express written consent.

**REFERENCE DRAWINGS**

| NO. | DATE | DESCRIPTION |
|-----|------|-------------|
|     |      |             |
|     |      |             |

**REVISIONS**

| REV. | DATE       | DESCRIPTION | BY | CHK |
|------|------------|-------------|----|-----|
| 0    | 2021.02.08 | BH Plan     | JH | TA  |

CLIENT NAME: **AMAZON LOGISTICS**

PROJECT LOCATION:  
**2625 Sheffield Rd, Ottawa ON**  
PROJECT NUMBER: 60634622

**AS-BUILT BOREHOLE LOCATION PLAN**

|              |                |                      |
|--------------|----------------|----------------------|
| DRAWN BY: JH | SCALE: 1:1500  | DRAWING No. <b>1</b> |
| CHECKED: TA  | DATE: FEB 2021 | REVISION 0           |

PROJECT: DYT3 - Ottawa  
 LOCATION: 2625 Sheffield Road  
 COORDINATES: N 5031369.8; E 451948.7  
 DATUM: Geodetic  
 AECOM PROJECT #: 60634622  
 CLIENT: Amazon Logistics

# RECORD OF BOREHOLE: BH-1

SHEET 1 OF 1

START DATE: Jan 12, 2021  
 END DATE: Jan 12, 2021  
 BORING METHOD: 203 mm O.D. Solid Stem Auger  
 CONTRACTOR: Aardvark Drilling Inc.

PENETRATION TEST HAMMER, 64kg; DROP, 760mm  
 SAMPLER HAMMER, 64kg; DROP, 760mm

| DEPTH SCALE<br>(METRES) | BORING METHOD  | SOIL PROFILE  |             | SAMPLES               |        |      | Standard Penetration Testing<br>(SPT) Number (blows/0.3m) |                       |  |  | SHEAR STRENGTH $C_u$ , kPa |                  |  |  | ADDITIONAL<br>LAB. TESTING<br>& GRAIN SIZE<br>DISTRIBUTION<br>(%) | WELL INSTALLATION<br>AND WATER LEVELS |           |            |
|-------------------------|--|---|-------------|-----------------------|--------|------|---|-----------------------|--|--|----------------------------|------------------|--|--|---|---------------------------------------|-----------|------------|
|                         |  | DESCRIPTION   | STRATA PLOT | ELEV.<br>DEPTH<br>(m) | NUMBER | TYPE | N VALUE   | rem V. - + Q - ●      |  |  |                            | nat V. - + U - Δ |  |  |   |                                       |           |            |
|                         |  |   |             |                       |        |      |   | WATER CONTENT PERCENT |  |  |                            | Wp   ○ W   WI    |  |  |   |                                       |           |            |
|                         |  | PAVEMENT  |             | 64.30                 |        |      |   |                       |  |  |                            |                  |  |  |   | GR SA SI CL                           |           |            |
| 0                       | Power Auger Drilling<br>203 mm O.D. Solid Stem Auger | ASPHALT: 60 mm thick<br>FILL: sand and gravel, 700 mm thick,<br>some clay with buried asphalt, grey,<br>moist, very dense   |             | 0.06                  | 1      | SS   | 53  |                       |  |  |                            |                  |  |  |   |                                       | 33 62 (5) |            |
| 1                       |  | SILTY CLAY: some sand, grey/brown,<br>moist, very stiff   |             | 0.76                  | 2      | SS   | 25  |                       |  |  |                            |                  |  |  |   |                                       |           |            |
| 2                       |  |   |             |                       | 62.17  | 3    | SS  | 17                    |  |  |                            |                  |  |  |   |                                       |           | 0 10 46 44 |
| 3                       |  | END OF BOREHOLE<br>Notes:<br>1. This log is to be read with the subject<br>report and project number as presented<br>above.<br>2. Interpretation assistance by AECOM is<br>required for projects excluding the above<br>mentioned project.<br>3. No abnormal odour or staining was<br>observed unless otherwise indicated.<br>4. No groundwater was observed in the<br>open hole upon the completion. |             | 2.13                  |        |      |   |                       |  |  |                            |                  |  |  |   |                                       |           |            |
| 4                       |  |   |             |                       |        |      |   |                       |  |  |                            |                  |  |  |   |                                       |           |            |
| 5                       |  |   |             |                       |        |      |   |                       |  |  |                            |                  |  |  |   |                                       |           |            |
| 6                       |  |   |             |                       |        |      |   |                       |  |  |                            |                  |  |  |   |                                       |           |            |
| 7                       |  |   |             |                       |        |      |   |                       |  |  |                            |                  |  |  |   |                                       |           |            |
| 8                       |  |   |             |                       |        |      |   |                       |  |  |                            |                  |  |  |   |                                       |           |            |
| 9                       |  |   |             |                       |        |      |   |                       |  |  |                            |                  |  |  |   |                                       |           |            |
| 10                      |  |   |             |                       |        |      |   |                       |  |  |                            |                  |  |  |   |                                       |           |            |

(LOG TO BE READ IN CONJUNCTION WITH REPORT)

DEPTH SCALE

1 : 50



LOGGED: WH

CHECKED: TA

AECOM\_BH\_001\_60634622\_DYT3.GPJ\_GAL-MISS.GDT\_21-2-16

PROJECT: DYT3 - Ottawa  
 LOCATION: 2625 Sheffield Road  
 COORDINATES: N 5031340.7; E 451960.8  
 DATUM: Geodetic  
 AECOM PROJECT #: 60634622  
 CLIENT: Amazon Logistics

## RECORD OF BOREHOLE: BH-2

SHEET 1 OF 1

START DATE: Jan 12, 2021  
 END DATE: Jan 12, 2021  
 BORING METHOD: 203 mm O.D. Solid Stem Auger  
 CONTRACTOR: Aardvark Drilling Inc.

PENETRATION TEST HAMMER, 64kg; DROP, 760mm  
 SAMPLER HAMMER, 64kg; DROP, 760mm

| DEPTH SCALE<br>(METRES) | BORING METHOD  | SOIL PROFILE  |                           |                       | SAMPLES |      |         | Standard Penetration Testing<br>(SPT) Number (blows/0.3m) |  |  |  | SHEAR STRENGTH Cu, kPa |  |  |  | ADDITIONAL<br>LAB. TESTING<br>& GRAIN SIZE<br>DISTRIBUTION<br>(%) | WELL INSTALLATION<br>AND WATER LEVELS |            |  |
|-------------------------|--|---|---------------------------|-----------------------|---------|------|---------|---|--|--|--|------------------------|--|--|--|---|---------------------------------------|------------|--|
|                         |  | DESCRIPTION   | STRATA PLOT               | ELEV.<br>DEPTH<br>(m) | NUMBER  | TYPE | N VALUE | 20 40 60 80   |  |  |  | 20 40 60 80            |  |  |  |   |                                       |            |  |
|                         |  |   |                           |                       |         |      |         | 100 200 300 400   |  |  |  | 10 20 30 40            |  |  |  |   |                                       |            |  |
| 0                       | Power Auger Drilling<br>203 mm O.D. Solid Stem Auger   | PAVEMENT  | 64.60<br><del>64.98</del> |                       |         |      |         |   |  |  |  |                        |  |  |  |   |                                       |            |  |
|                         |  | ASPHALT: 150 mm thick   | 64.98                     |                       |         |      |         |   |  |  |  |                        |  |  |  |   |                                       |            |  |
|                         |  | FILL: sand and gravel, 600 mm thick, some silt, grey, moist, very dense | 0.15                      | 1                     | SS      | 42   |         |   |  |  |  |                        |  |  |  |   |                                       | 23 67 (10) |  |
| 1                       |  | FILL: sand, some gravel, trace silt, brown, moist, dense                | 63.85<br>0.75             | 2                     | SS      | 46   |         |   |  |  |  |                        |  |  |  |   |                                       |            |  |
| 2                       | SILTY CLAY: trace gravel, some sand, brown, moist, stiff   | 63.08<br>1.52   | 3                         | SS                    | 12      |      |         |   |  |  |  |                        |  |  |  |   |                                       |            |  |
| 3                       | <b>END OF BOREHOLE</b><br>Notes:<br>1. This log is to be read with the subject report and project number as presented above.<br>2. Interpretation assistance by AECOM is required for projects excluding the above mentioned project.<br>3. No abnormal odour or staining was observed unless otherwise indicated.<br>4. No groundwater was observed in the open hole upon the completion. |   | 62.47<br>2.13             |                       |         |      |         |   |  |  |  |                        |  |  |  |   |                                       |            |  |

DRAFT

AECOM\_BH\_001\_60634622\_DYT3.GPJ\_GAL-MISS.GDT\_21-2-16

(LOG TO BE READ IN CONJUNCTION WITH REPORT)

DEPTH SCALE  
1 : 50



LOGGED: WH  
CHECKED: TA

PROJECT: DYT3 - Ottawa  
 LOCATION: 2625 Sheffield Road  
 COORDINATES: N 5031373.6; E 451984.0  
 DATUM: Geodetic  
 AECOM PROJECT #: 60634622  
 CLIENT: Amazon Logistics

## RECORD OF BOREHOLE: BH-3

SHEET 1 OF 1

START DATE: Jan 12, 2021  
 END DATE: Jan 12, 2021  
 BORING METHOD: 203 mm O.D. Solid Stem Auger  
 CONTRACTOR: Aardvark Drilling Inc.  
 PENETRATION TEST HAMMER, 64kg; DROP, 760mm  
 SAMPLER HAMMER, 64kg; DROP, 760mm

| DEPTH SCALE<br>(METRES) | BORING METHOD  | SOIL PROFILE   |             | SAMPLES               |        |      | Standard Penetration Testing<br>(SPT) Number (blows/0.3m) |                       |  |  | SHEAR STRENGTH $C_u$ , kPa<br>nat V. - + Q - ●<br>rem V. - ⊕ U - △ |  |  |  | ADDITIONAL<br>LAB. TESTING<br>& GRAIN SIZE<br>DISTRIBUTION<br>(%) | WELL INSTALLATION<br>AND WATER LEVELS |  |  |  |
|-------------------------|--|--|-------------|-----------------------|--------|------|---|-----------------------|--|--|--|--|--|--|---|---------------------------------------|--|--|--|
|                         |  | DESCRIPTION  | STRATA PLOT | ELEV.<br>DEPTH<br>(m) | NUMBER | TYPE | N VALUE   | WATER CONTENT PERCENT |  |  |  |  |  |  |   |                                       |  |  |  |
|                         |  |  |             |                       |        |      |   | Wp   ○ W   WI         |  |  |  |  |  |  |   |                                       |  |  |  |
|                         |  | PAVEMENT   |             | 64.00                 |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |  |
| 0                       | Power Auger Drilling<br>203 mm O.D. Solid Stem Auger | ASPHALT: 90 mm thick   |             | 0.00                  |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |  |
|                         |  | FILL: sand and gravel, some silt, 670 mm thick, grey, moist, very dense with crushed granulars   |             | 0.09                  | 1      | SS   | 57  |                       |  |  |  |  |  |  |   |                                       |  |  |  |
| 1                       |  | SILTY CLAY: trace gravel, some sand, brown, moist, stiff to very stiff   |             | 0.76                  | 2      | SS   | 12  |                       |  |  |  |  |  |  |   |                                       |  |  |  |
| 2                       |  |  |             | 63.24                 |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |  |
|                         |  |  |             | 0.76                  | 3      | SS   | 15  |                       |  |  |  |  |  |  |   |                                       |  |  |  |
| 2                       |  |  |             | 61.87                 |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |  |
|                         |  |  |             | 2.13                  |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |  |
| 3                       |  | <b>END OF BOREHOLE</b><br>Notes:<br>1. This log is to be read with the subject report and project number as presented above.<br>2. Interpretation assistance by AECOM is required for projects excluding the above mentioned project.<br>3. No abnormal odour or staining was observed unless otherwise indicated.<br>4. No groundwater was observed in the open hole. |             |                       |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |  |
| 4                       |  |  |             |                       |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |  |
| 5                       |  |  |             |                       |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |  |
| 6                       |  |  |             |                       |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |  |
| 7                       |  |  |             |                       |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |  |
| 8                       |  |  |             |                       |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |  |
| 9                       |  |  |             |                       |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |  |
| 10                      |  |  |             |                       |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |  |

(LOG TO BE READ IN CONJUNCTION WITH REPORT)

DEPTH SCALE

1 : 50



LOGGED: WH

CHECKED: TA

AECOM\_BH\_001\_60634622\_DYT3.GPJ\_GAL-MISS.GDT\_21-2-16

PROJECT: DYT3 - Ottawa  
 LOCATION: 2625 Sheffield Road  
 COORDINATES: N 50314365.9; E 452069.5  
 DATUM: Geodetic  
 AECOM PROJECT #: 60634622  
 CLIENT: Amazon Logistics

# RECORD OF BOREHOLE: BH-7

SHEET 1 OF 1

START DATE: Jan 12, 2021  
 END DATE: Jan 12, 2021  
 BORING METHOD: 203 mm O.D. Solid Stem Auger  
 CONTRACTOR: Aardvark Drilling Inc.

PENETRATION TEST HAMMER, 64kg; DROP, 760mm  
 SAMPLER HAMMER, 64kg; DROP, 760mm

| DEPTH SCALE (METRES) | BORING METHOD  | SOIL PROFILE   |             | SAMPLES         |        |      | Standard Penetration Testing (SPT) Number (blows/0.3m) |    |    |    | SHEAR STRENGTH $C_u$ , kPa |    |    |    | ADDITIONAL LAB. TESTING & GRAIN SIZE DISTRIBUTION (%) | WELL INSTALLATION AND WATER LEVELS |    |            |             |
|----------------------|--|--|-------------|-----------------|--------|------|--|----|----|----|----------------------------|----|----|----|---|------------------------------------|----|------------|-------------|
|                      |  | DESCRIPTION  | STRATA PLOT | ELEV. DEPTH (m) | NUMBER | TYPE | N VALUE  | 20 | 40 | 60 | 80                         | 20 | 40 | 60 |   |                                    | 80 |            |             |
| 0                    | Power Auger Drilling<br>203 mm O.D. Solid Stem Auger   | PAVEMENT   |             | 64.00           |        |      |  |    |    |    |                            |    |    |    |   |                                    |    |            |             |
|                      |  | ASPHALT: 80 mm thick   |             | 0.00            |        |      |  |    |    |    |                            |    |    |    |   |                                    |    |            |             |
|                      |  | FILL: sand and gravel, some silt and clay, 680 mm thick, grey, moist, dense with crushed granulars |             | 0.08            | 1      | SS   | 40   |    |    |    |                            |    |    |    |   |                                    |    |            | GR SA SI CL |
| 1                    |  | CLAYEY SILT: some to trace gravel, trace sand, grey, moist, stiff to very stiff                    |             | 63.24           | 2      | SS   | 8  |    |    |    |                            |    |    |    |   |                                    |    |            | 13 75 (12)  |
|                      |  |  |             | 0.76            |        |      |  |    |    |    |                            |    |    |    |   |                                    |    |            |             |
| 2                    |  |  |             | 3               | SS     | 16   |  |    |    |    |                            |    |    |    |   |                                    |    | 1 13 40 46 |             |
| 3                    |  | SILTY CLAY: grey, moist, firm  |             | 60.95           |        |      |  |    |    |    |                            |    |    |    |   |                                    |    |            |             |
|                      |  |  |             | 3.05            | 4      | SS   | 4  |    |    |    |                            |    |    |    |   |                                    |    |            |             |
| 5                    |  |  |             | 58.82           | 5      | SS   | 6  |    |    |    |                            |    |    |    |   |                                    |    | 0 1 92 7   |             |
|                      |  |  |             | 5.18            |        |      |  |    |    |    |                            |    |    |    |   |                                    |    |            |             |
| 6                    | <b>END OF BOREHOLE</b><br>Notes:<br>1. This log is to be read with the subject report and project number as presented above.<br>2. Interpretation assistance by AECOM is required for projects excluding the above mentioned project.<br>3. No abnormal odour or staining was observed unless otherwise indicated.<br>4. Water level encountered at approximately 4.0 mbgs during drilling operations. |  |             |                 |        |      |  |    |    |    |                            |    |    |    |   |                                    |    |            |             |
| 7                    |  |  |             |                 |        |      |  |    |    |    |                            |    |    |    |   |                                    |    |            |             |
| 8                    |  |  |             |                 |        |      |  |    |    |    |                            |    |    |    |   |                                    |    |            |             |
| 9                    |  |  |             |                 |        |      |  |    |    |    |                            |    |    |    |   |                                    |    |            |             |
| 10                   |  |  |             |                 |        |      |  |    |    |    |                            |    |    |    |   |                                    |    |            |             |

(LOG TO BE READ IN CONJUNCTION WITH REPORT)

DEPTH SCALE

1 : 50



LOGGED: WH

CHECKED: TA

AECOM\_BH\_001\_60634622\_DYT3.GPJ\_GAL-MISS.GDT\_21-2-16



PROJECT: DYT3 - Ottawa  
 LOCATION: 2625 Sheffield Road  
 COORDINATES: N 5031373.2; E 452134.3  
 DATUM: Geodetic  
 AECOM PROJECT #: 60634622  
 CLIENT: Amazon Logistics

# RECORD OF BOREHOLE: BH-10

SHEET 1 OF 1

START DATE: Jan 12, 2021  
 END DATE: Jan 12, 2021  
 BORING METHOD: 203 mm O.D. Solid Stem Auger  
 CONTRACTOR: Aardvark Drilling Inc.

PENETRATION TEST HAMMER, 64kg; DROP, 760mm  
 SAMPLER HAMMER, 64kg; DROP, 760mm

| DEPTH SCALE (METRES) | BORING METHOD  | SOIL PROFILE   |             | SAMPLES                        |        |      | Standard Penetration Testing (SPT) Number (blows/0.3m) |    |    |    | SHEAR STRENGTH $C_u$ , kPa |    |    |    | ADDITIONAL LAB. TESTING & GRAIN SIZE DISTRIBUTION (%) | WELL INSTALLATION AND WATER LEVELS |    |  |
|----------------------|--|--|-------------|--------------------------------|--------|------|--|----|----|----|----------------------------|----|----|----|---|------------------------------------|----|--|
|                      |  | DESCRIPTION  | STRATA PLOT | ELEV. DEPTH (m)                | NUMBER | TYPE | N VALUE  | 20 | 40 | 60 | 80                         | 20 | 40 | 60 |   |                                    | 80 |  |
| 0                    | Power Auger Drilling<br>203 mm O.D. Solid Stem Auger   | PAVEMENT   |             | 64.60                          |        |      |  |    |    |    |                            |    |    |    |   |                                    |    |  |
|                      |  | ASPHALT: 180 mm thick  |             | 0.00<br>64.42                  |        |      |  |    |    |    |                            |    |    |    |   |                                    |    |  |
|                      |  | FILL: sand and gravel, 660 mm thick, some silt, brown, moist, very dense |             | 0.18                           | 1      | SS   | 74   |    |    |    |                            |    |    |    |   |                                    |    |  |
| 1                    |  | FILL: gravelly sand, some silt, moist, compact with possible cobbles     |             | 63.84<br>0.76                  | 2      | SS   | 23   |    |    |    |                            |    |    |    |   |                                    |    |  |
|                      |  |  |             |                                | 3A     | SS   | 8  |    |    |    |                            |    |    |    |   |                                    |    |  |
| 2                    |  | CLAYEY SILT: some sand, grey, moist, stiff                               |             | 62.77<br>1.83<br>62.47<br>2.13 | 3B     |      |  |    |    |    |                            |    |    |    |   |                                    |    |  |
| 3                    | <b>END OF BOREHOLE</b><br>Notes:<br>1. This log is to be read with the subject report and project number as presented above.<br>2. Interpretation assistance by AECOM is required for projects excluding the above mentioned project.<br>3. No abnormal odour or staining was observed unless otherwise indicated.<br>4. No groundwater was observed in the open hole upon the completion. |  |             |                                |        |      |  |    |    |    |                            |    |    |    |   |                                    |    |  |
| 4                    |  |  |             |                                |        |      |  |    |    |    |                            |    |    |    |   |                                    |    |  |
| 5                    |  |  |             |                                |        |      |  |    |    |    |                            |    |    |    |   |                                    |    |  |
| 6                    |  |  |             |                                |        |      |  |    |    |    |                            |    |    |    |   |                                    |    |  |
| 7                    |  |  |             |                                |        |      |  |    |    |    |                            |    |    |    |   |                                    |    |  |
| 8                    |  |  |             |                                |        |      |  |    |    |    |                            |    |    |    |   |                                    |    |  |
| 9                    |  |  |             |                                |        |      |  |    |    |    |                            |    |    |    |   |                                    |    |  |
| 10                   |  |  |             |                                |        |      |  |    |    |    |                            |    |    |    |   |                                    |    |  |

(LOG TO BE READ IN CONJUNCTION WITH REPORT)

DEPTH SCALE

1 : 50



LOGGED: WH

CHECKED: TA

AECOM\_BH\_001\_60634622\_DYT3.GPJ\_GAL-MISS.GDT\_21-2-16

PROJECT: DYT3 - Ottawa  
 LOCATION: 2625 Sheffield Road  
 COORDINATES: N 5031311.5; E 452152.4  
 DATUM: Geodetic  
 AECOM PROJECT #: 60634622  
 CLIENT: Amazon Logistics

# RECORD OF BOREHOLE: BH-11

SHEET 1 OF 1

START DATE: Jan 12, 2021  
 END DATE: Jan 12, 2021  
 BORING METHOD: 203 mm O.D. Solid Stem Auger  
 CONTRACTOR: Aardvark Drilling Inc.

PENETRATION TEST HAMMER, 64kg; DROP, 760mm  
 SAMPLER HAMMER, 64kg; DROP, 760mm

| DEPTH SCALE (METRES) | BORING METHOD  | SOIL PROFILE   |             | SAMPLES         |        |      | Standard Penetration Testing (SPT) Number (blows/0.3m) |    |    |    | SHEAR STRENGTH $C_u$ , kPa |    |    |    | ADDITIONAL LAB. TESTING & GRAIN SIZE DISTRIBUTION (%) | WELL INSTALLATION AND WATER LEVELS |           |
|----------------------|--|--|-------------|-----------------|--------|------|--|----|----|----|----------------------------|----|----|----|---|------------------------------------|-----------|
|                      |  | DESCRIPTION  | STRATA PLOT | ELEV. DEPTH (m) | NUMBER | TYPE | N VALUE  | 20 | 40 | 60 | 80                         | 20 | 40 | 60 |   |                                    | 80        |
| 0                    | Power Auger Drilling<br>203 mm O.D. Solid Stem Auger | PAVEMENT   |             | 64.90           |        |      |  |    |    |    |                            |    |    |    |   | GR SA SI CL                        |           |
|                      |  | ASPHALT: 180 mm thick  |             | 64.90<br>64.72  |        |      |  |    |    |    |                            |    |    |    |   |                                    |           |
|                      |  | FILL: sand and gravel, 1040 mm thick, trace silt and clay, brown, moist, very dense to compact   |             | 0.18            | 1      | SS   | 56   |    |    |    |                            |    |    |    |   |                                    | 21 78 (1) |
| 1                    |  |  |             |                 | 63.68  | 2A   | SS   | 15 |    |    |                            |    |    |    |   |                                    |           |
|                      |  | CLAYEY SILT: trace gravel, trace sand, grey, moist, stiff  |             | 63.68<br>1.22   | 2B     | SS   |  |    |    |    |                            |    |    |    |   |                                    |           |
| 2                    |  |  |             | 62.77           | 3      | SS   | 11   |    |    |    |                            |    |    |    |   |                                    |           |
|                      |  | END OF BOREHOLE  |             | 62.77<br>2.13   |        |      |  |    |    |    |                            |    |    |    |   |                                    |           |
| 3                    |  | Notes:<br>1. This log is to be read with the subject report and project number as presented above.<br>2. Interpretation assistance by AECOM is required for projects excluding the above mentioned project.<br>3. No abnormal odour or staining was observed unless otherwise indicated.<br>4. No groundwater was observed in the open hole upon the completion. |             |                 |        |      |  |    |    |    |                            |    |    |    |   |                                    |           |
| 4                    |  |  |             |                 |        |      |  |    |    |    |                            |    |    |    |   |                                    |           |
| 5                    |  |  |             |                 |        |      |  |    |    |    |                            |    |    |    |   |                                    |           |
| 6                    |  |  |             |                 |        |      |  |    |    |    |                            |    |    |    |   |                                    |           |
| 7                    |  |  |             |                 |        |      |  |    |    |    |                            |    |    |    |   |                                    |           |
| 8                    |  |  |             |                 |        |      |  |    |    |    |                            |    |    |    |   |                                    |           |
| 9                    |  |  |             |                 |        |      |  |    |    |    |                            |    |    |    |   |                                    |           |
| 10                   |  |  |             |                 |        |      |  |    |    |    |                            |    |    |    |   |                                    |           |

(LOG TO BE READ IN CONJUNCTION WITH REPORT)

DEPTH SCALE

1 : 50



LOGGED: WH

CHECKED: TA

AECOM\_BH\_001\_60634622\_DYT3.GPJ\_GAL-MISS.GDT\_21-2-16

PROJECT: DYT3 - Ottawa  
 LOCATION: 2625 Sheffield Road  
 COORDINATES: N 5031275.1; E 452165342.0  
 DATUM: Geodetic  
 AECOM PROJECT #: 60634622  
 CLIENT: Amazon Logistics

## RECORD OF BOREHOLE: BH-12

SHEET 1 OF 1

START DATE: Jan 12, 2021  
 END DATE: Jan 12, 2021  
 BORING METHOD: 203 mm O.D. Solid Stem Auger  
 CONTRACTOR: Aardvark Drilling Inc.  
 PENETRATION TEST HAMMER, 64kg; DROP, 760mm  
 SAMPLER HAMMER, 64kg; DROP, 760mm

| DEPTH SCALE<br>(METRES) | BORING METHOD  | SOIL PROFILE   |             |                       | SAMPLES |      |         | Standard Penetration Testing<br>(SPT) Number (blows/0.3m) |  |  |  | SHEAR STRENGTH $C_u$ , kPa<br>nat V. - + Q - ●<br>rem V. - ⊕ U - △ |  |  |  | ADDITIONAL<br>LAB. TESTING<br>& GRAIN SIZE<br>DISTRIBUTION<br>(%) | WELL INSTALLATION<br>AND WATER LEVELS |  |
|-------------------------|--|--|-------------|-----------------------|---------|------|---------|---|--|--|--|--|--|--|--|---|---------------------------------------|--|
|                         |  | DESCRIPTION  | STRATA PLOT | ELEV.<br>DEPTH<br>(m) | NUMBER  | TYPE | N VALUE | 20 40 60 80   |  |  |  | 20 40 60 80  |  |  |  |   |                                       |  |
|                         |  |  |             |                       |         |      |         | 100 200 300 400   |  |  |  | 10 20 30 40  |  |  |  |   |                                       |  |
|                         |  | PAVEMENT   |             |                       |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |
| 0                       | Power Auger Drilling<br>203 mm O.D. Solid Stem Auger | ASPHALT: 90 mm thick   |             |                       | 64.60   |      |         |   |  |  |  |  |  |  |  |   |                                       |  |
|                         |  | FILL: sand and gravel, some silt, brown, moist, compact with crushed granulars   |             |                       | 0.00    |      |         |   |  |  |  |  |  |  |  |   |                                       |  |
|                         |  |  |             |                       | 0.09    | 1    | SS      | 22  |  |  |  |  |  |  |  |   |                                       |  |
| 1                       |  |  |             |                       | 63.38   | 2A   | SS      | 18  |  |  |  |  |  |  |  |   |                                       |  |
|                         |  | CLAYEY SILT: some gravel, trace sand, brown, moist, very stiff   |             |                       | 1.22    | 2B   | SS      |   |  |  |  |  |  |  |  |   |                                       |  |
| 2                       |  |  |             | 62.47                 | 3       | SS   | 16      |   |  |  |  |  |  |  |  |   | 0 21 51 28                            |  |
|                         |  | END OF BOREHOLE  |             |                       | 2.13    |      |         |   |  |  |  |  |  |  |  |   |                                       |  |
|                         |  | <p>Notes:</p> <ol style="list-style-type: none"> <li>This log is to be read with the subject report and project number as presented above.</li> <li>Interpretation assistance by AECOM is required for projects excluding the above mentioned project.</li> <li>No abnormal odour or staining was observed unless otherwise indicated.</li> <li>No groundwater was observed in the open hole upon the completion.</li> </ol> |             |                       |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |
| 3                       | DRAFT  |  |             |                       |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |
| 4                       |  |  |             |                       |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |
| 5                       |  |  |             |                       |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |
| 6                       |  |  |             |                       |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |
| 7                       |  |  |             |                       |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |
| 8                       |  |  |             |                       |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |
| 9                       |  |  |             |                       |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |
| 10                      |  |  |             |                       |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |

(LOG TO BE READ IN CONJUNCTION WITH REPORT)

DEPTH SCALE

1 : 50



LOGGED: WH

CHECKED: TA

AECOM\_BH\_001\_60634622\_DYT3.GPJ\_GAL-MISS.GDT\_21-2-16

PROJECT: DYT3 - Ottawa  
 LOCATION: 2625 Sheffield Road  
 COORDINATES: N 5031239.3; E 452118.1  
 DATUM: Geodetic  
 AECOM PROJECT #: 60634622  
 CLIENT: Amazon Logistics

# RECORD OF BOREHOLE: BH-14

SHEET 1 OF 1

START DATE: Jan 11, 2021  
 END DATE: Jan 11, 2021  
 BORING METHOD: 203 mm O.D. Solid Stem Auger  
 CONTRACTOR: Aardvark Drilling Inc.  
 PENETRATION TEST HAMMER, 64kg; DROP, 760mm  
 SAMPLER HAMMER, 64kg; DROP, 760mm

| DEPTH SCALE (METRES) | BORING METHOD  | SOIL PROFILE   |             | SAMPLES         |        |      | Standard Penetration Testing (SPT) Number (blows/0.3m) |    |    |    | SHEAR STRENGTH $C_u$ , kPa |    |    |    | ADDITIONAL LAB. TESTING & GRAIN SIZE DISTRIBUTION (%) | WELL INSTALLATION AND WATER LEVELS |
|----------------------|--|--|-------------|-----------------|--------|------|--|----|----|----|----------------------------|----|----|----|---|------------------------------------|
|                      |  | DESCRIPTION  | STRATA PLOT | ELEV. DEPTH (m) | NUMBER | TYPE | N VALUE  | 20 | 40 | 60 | 80                         | 20 | 40 | 60 |   |                                    |
|                      |  | PAVEMENT   |             | 64.60           |        |      |  |    |    |    |                            |    |    |    |   | GR SA SI CL                        |
| 0                    | Power Auger Drilling<br>203 mm O.D. Solid Stem Auger | ASPHALT: 40 mm thick   |             | 0.04            |        |      |  |    |    |    |                            |    |    |    |   |                                    |
|                      |  | FILL: sand and gravel, 1330 mm thick, trace silt and clay, brown/grey, moist, compact to dense with buried asphalt   |             | 1               | SS     | 23   |  |    |    |    |                            |    |    |    |   |                                    |
| 1                    |  |  |             |                 | 2      | SS   | 42   |    |    |    |                            |    |    |    |   |                                    |
|                      |  |  |             | 63.23           |        |      |  |    |    |    |                            |    |    |    |   |                                    |
|                      |  | END OF BOREHOLE  |             | 1.37            |        |      |  |    |    |    |                            |    |    |    |   |                                    |
| 2                    |  | Notes:<br>1. This log is to be read with the subject report and project number as presented above.<br>2. Interpretation assistance by AECOM is required for projects excluding the above mentioned project.<br>3. No abnormal odour or staining was observed unless otherwise indicated.<br>4. No groundwater was observed in the open hole upon the completion. |             |                 |        |      |  |    |    |    |                            |    |    |    |   |                                    |
| 3                    |  |  |             |                 |        |      |  |    |    |    |                            |    |    |    |   |                                    |
| 4                    |  |  |             |                 |        |      |  |    |    |    |                            |    |    |    |   |                                    |
| 5                    |  |  |             |                 |        |      |  |    |    |    |                            |    |    |    |   |                                    |
| 6                    |  |  |             |                 |        |      |  |    |    |    |                            |    |    |    |   |                                    |
| 7                    |  |  |             |                 |        |      |  |    |    |    |                            |    |    |    |   |                                    |
| 8                    |  |  |             |                 |        |      |  |    |    |    |                            |    |    |    |   |                                    |
| 9                    |  |  |             |                 |        |      |  |    |    |    |                            |    |    |    |   |                                    |
| 10                   |  |  |             |                 |        |      |  |    |    |    |                            |    |    |    |   |                                    |

(LOG TO BE READ IN CONJUNCTION WITH REPORT)

DEPTH SCALE

1 : 50



LOGGED: WH

CHECKED: TA

AECOM\_BH\_001\_60634622\_DYT3.GPJ\_GAL-MISS.GDT\_21-2-16

PROJECT: DYT3 - Ottawa  
 LOCATION: 2625 Sheffield Road  
 COORDINATES: N 5031205.4; E 452137.5  
 DATUM: Geodetic  
 AECOM PROJECT #: 60634622  
 CLIENT: Amazon Logistics

## RECORD OF BOREHOLE: BH-15

SHEET 1 OF 1

START DATE: Jan 11, 2021  
 END DATE: Jan 11, 2021  
 BORING METHOD: 203 mm O.D. Solid Stem Auger  
 CONTRACTOR: Aardvark Drilling Inc.  
 PENETRATION TEST HAMMER, 64kg; DROP, 760mm  
 SAMPLER HAMMER, 64kg; DROP, 760mm

| DEPTH SCALE (METRES) | BORING METHOD  | SOIL PROFILE   |             | SAMPLES         |        |      | Standard Penetration Testing (SPT) Number (blows/0.3m) |                       |   |  | SHEAR STRENGTH $C_u$ , kPa |                                      |  |  | ADDITIONAL LAB. TESTING & GRAIN SIZE DISTRIBUTION (%) | WELL INSTALLATION AND WATER LEVELS |  |  |  |  |
|----------------------|--|--|-------------|-----------------|--------|------|--|-----------------------|---|--|----------------------------|--------------------------------------|--|--|---|------------------------------------|--|--|--|--|
|                      |  | DESCRIPTION  | STRATA PLOT | ELEV. DEPTH (m) | NUMBER | TYPE | N VALUE  | WATER CONTENT PERCENT |   |  |                            | SHEAR STRENGTH                       |  |  |   |                                    |  |  |  |  |
|                      |  |  |             |                 |        |      |  | Wp  -----  Wl         |   |  |                            | nat V. - + Q - ●<br>rem V. - ⊕ U - △ |  |  |   |                                    |  |  |  |  |
|                      |  | PAVEMENT   |             | 64.30           |        |      |  |                       |   |  |                            |                                      |  |  |   |                                    |  |  |  |  |
| 0                    | Power Auger Drilling<br>203 mm O.D. Solid Stem Auger | <b>ASPHALT:</b> 90 mm thick<br><b>FILL:</b> sand and gravel, some silt, brown, moist, compact with buried asphalt and construction debris  |             | 0.00            |        |      |  |                       |   |  |                            |                                      |  |  |   |                                    |  |  |  |  |
|                      |  |  |             |                 | 0.09   |      |  |                       |   |  |                            |                                      |  |  |   |                                    |  |  |  |  |
| 1                    |  | <b>CLAYEY SILT:</b> some to trace sand, grey, moist, stiff   |             |                 | 63.39  |      | 2A   | SS                    | 6 |  |                            |                                      |  |  |   |                                    |  |  |  |  |
|                      |  |  |             |                 | 0.91   |      | 2B   | SS                    |   |  |                            |                                      |  |  |   |                                    |  |  |  |  |
| 2                    |  |  |             |                 |        | 3    | SS   | 12                    |   |  |                            |                                      |  |  |   |                                    |  |  |  |  |
| 3                    |  | <b>END OF BOREHOLE</b><br>Notes:<br>1. This log is to be read with the subject report and project number as presented above.<br>2. Interpretation assistance by AECOM is required for projects excluding the above mentioned project.<br>3. No abnormal odour or staining was observed unless otherwise indicated.<br>4. No groundwater was observed in the open hole upon the completion. |             | 62.17           |        |      |  |                       |   |  |                            |                                      |  |  |   |                                    |  |  |  |  |
|                      |  |  |             | 2.13            |        |      |  |                       |   |  |                            |                                      |  |  |   |                                    |  |  |  |  |

DRAFT

AECOM\_BH\_001\_60634622\_DYT3.GPJ\_GAL-MISS.GDT\_21-2-16

PROJECT: DYT3 - Ottawa  
 LOCATION: 2625 Sheffield Road  
 COORDINATES: N 5031180.9; E 452172.4  
 DATUM: Geodetic  
 AECOM PROJECT #: 60634622  
 CLIENT: Amazon Logistics

## RECORD OF BOREHOLE: BH-16

SHEET 1 OF 1

START DATE: Jan 11, 2021  
 END DATE: Jan 11, 2021  
 BORING METHOD: 203 mm O.D. Solid Stem Auger  
 CONTRACTOR: Aardvark Drilling Inc.  
 PENETRATION TEST HAMMER, 64kg; DROP, 760mm  
 SAMPLER HAMMER, 64kg; DROP, 760mm

| DEPTH SCALE<br>(METRES) | BORING METHOD  | SOIL PROFILE   |             | SAMPLES               |        |      | Standard Penetration Testing<br>(SPT) Number (blows/0.3m) |                       |  |  | SHEAR STRENGTH $C_u$ , kPa<br>nat V. - + Q - ●<br>rem V. - ⊕ U - △ |  |  |  | ADDITIONAL<br>LAB. TESTING<br>& GRAIN SIZE<br>DISTRIBUTION<br>(%) | WELL INSTALLATION<br>AND WATER LEVELS |  |  |
|-------------------------|--|--|-------------|-----------------------|--------|------|---|-----------------------|--|--|--|--|--|--|---|---------------------------------------|--|--|
|                         |  | DESCRIPTION  | STRATA PLOT | ELEV.<br>DEPTH<br>(m) | NUMBER | TYPE | N VALUE   | WATER CONTENT PERCENT |  |  |  |  |  |  |   |                                       |  |  |
|                         |  |  |             |                       |        |      |   | Wp   ○ W   WI         |  |  |  |  |  |  |   |                                       |  |  |
|                         |  | PAVEMENT   |             |                       |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |
| 0                       | Power Auger Drilling<br>203 mm O.D. Solid Stem Auger | ASPHALT: 90 mm thick   |             | 64.30                 |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |
|                         |  | FILL: sand and gravel, some silt, brown, moist, compact with buried asphalt and construction debris  |             | 0.00                  |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |
|                         |  |  |             | 0.09                  | 1      | SS   | 77  |                       |  |  |  |  |  |  |   |                                       |  |  |
| 1                       |  | CLAYEY SILT: some to trace sand, grey, moist, stiff  |             | 63.54                 |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |
|                         |  |  |             | 0.76                  |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |
|                         | 2  |  |             | 2                     | SS     | 19   |   |                       |  |  |  |  |  |  |   |                                       |  |  |
|                         |  |  |             | 62.17                 |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |
|                         | 3  |  |             | 3                     | SS     | 14   |   |                       |  |  |  |  |  |  |   |                                       |  |  |
|                         |  | END OF BOREHOLE  |             | 2.13                  |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |
|                         |  | <p>Notes:</p> <ol style="list-style-type: none"> <li>This log is to be read with the subject report and project number as presented above.</li> <li>Interpretation assistance by AECOM is required for projects excluding the above mentioned project.</li> <li>No abnormal odour or staining was observed unless otherwise indicated.</li> <li>No groundwater was observed in the open hole upon the completion.</li> </ol> |             |                       |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |

DRAFT

AECOM\_BH\_001\_60634622\_DYT3.GPJ\_GAL-MISS.GDT\_21-2-16

(LOG TO BE READ IN CONJUNCTION WITH REPORT)

DEPTH SCALE

1 : 50



LOGGED: WH  
 CHECKED: TA

PROJECT: DYT3 - Ottawa  
 LOCATION: 2625 Sheffield Road  
 COORDINATES: N 5031175.2; E 452190.1  
 DATUM: Geodetic  
 AECOM PROJECT #: 60634622  
 CLIENT: Amazon Logistics

## RECORD OF BOREHOLE: BH-17

SHEET 1 OF 1

START DATE: Jan 11, 2021  
 END DATE: Jan 11, 2021  
 BORING METHOD: 203 mm O.D. Solid Stem Auger  
 CONTRACTOR: Aardvark Drilling Inc.  
 PENETRATION TEST HAMMER, 64kg; DROP, 760mm  
 SAMPLER HAMMER, 64kg; DROP, 760mm

| DEPTH SCALE<br>(METRES) | BORING METHOD  | SOIL PROFILE  |             | SAMPLES               |        |      | Standard Penetration Testing<br>(SPT) Number (blows/0.3m) |                       |  |  | SHEAR STRENGTH $C_u$ , kPa<br>nat V. - + Q - ●<br>rem V. - ⊕ U - △ |  |  |  | ADDITIONAL<br>LAB. TESTING<br>& GRAIN SIZE<br>DISTRIBUTION<br>(%) | WELL INSTALLATION<br>AND WATER LEVELS |  |  |           |
|-------------------------|--|---|-------------|-----------------------|--------|------|---|-----------------------|--|--|--|--|--|--|---|---------------------------------------|--|--|-----------|
|                         |  | DESCRIPTION   | STRATA PLOT | ELEV.<br>DEPTH<br>(m) | NUMBER | TYPE | N VALUE   | WATER CONTENT PERCENT |  |  |  |  |  |  |   |                                       |  |  |           |
|                         |  |   |             |                       |        |      |   | Wp   ○ W   WI         |  |  |  |  |  |  |   |                                       |  |  |           |
|                         |  | PAVEMENT  |             | 64.00                 |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |           |
| 0                       | Power Auger Drilling<br>203 mm O.D. Solid Stem Auger   | ASPHALT: 110 mm thick   |             | 60.00                 |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |           |
|                         |  | FILL: sand and gravel, some silt, brown, moist, very dense with crushed granulars |             | 0.11                  | 1      | SS   | 79  |                       |  |  |  |  |  |  |   |                                       |  |  | 46 53 (1) |
| 1                       |  | CLAYEY SILT: some to trace sand, grey, moist, stiff                               |             | 63.24                 |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |           |
|                         |  |   |             | 0.76                  | 2      | SS   | 8   |                       |  |  |  |  |  |  |   |                                       |  |  |           |
| 2                       |  |   |             | 61.87                 |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |           |
|                         |  |   |             | 2.13                  | 3      | SS   | 13  |                       |  |  |  |  |  |  |   |                                       |  |  |           |
| 3                       | <b>END OF BOREHOLE</b><br>Notes:<br>1. This log is to be read with the subject report and project number as presented above.<br>2. Interpretation assistance by AECOM is required for projects excluding the above mentioned project.<br>3. No abnormal odour or staining was observed unless otherwise indicated.<br>4. No groundwater was observed in the open hole upon the completion. |   |             |                       |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |           |
| 4                       |  |   |             |                       |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |           |
| 5                       |  |   |             |                       |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |           |
| 6                       |  |   |             |                       |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |           |
| 7                       |  |   |             |                       |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |           |
| 8                       |  |   |             |                       |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |           |
| 9                       |  |   |             |                       |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |           |
| 10                      |  |   |             |                       |        |      |   |                       |  |  |  |  |  |  |   |                                       |  |  |           |

(LOG TO BE READ IN CONJUNCTION WITH REPORT)

DEPTH SCALE

1 : 50



LOGGED: WH

CHECKED: TA

AECOM\_BH\_001\_60634622\_DYT3.GPJ\_GAL-MASS.GDT\_21-2-16

PROJECT: DYT3 - Ottawa  
 LOCATION: 2625 Sheffield Road  
 COORDINATES: N 5031139.8; E 452131.3  
 DATUM: Geodetic  
 AECOM PROJECT #: 60634622  
 CLIENT: Amazon Logistics

## RECORD OF BOREHOLE: BH-18

SHEET 1 OF 1

START DATE: Jan 11, 2021  
 END DATE: Jan 11, 2021  
 BORING METHOD: 203 mm O.D. Solid Stem Auger  
 CONTRACTOR: Aardvark Drilling Inc.  
 PENETRATION TEST HAMMER, 64kg; DROP, 760mm  
 SAMPLER HAMMER, 64kg; DROP, 760mm

| DEPTH SCALE<br>(METRES) | BORING METHOD  | SOIL PROFILE  |             | SAMPLES               |        |      | Standard Penetration Testing<br>(SPT) Number (blows/0.3m) |                       |  |  | SHEAR STRENGTH $C_u$ , kPa<br>nat V. - + Q - ●<br>rem V. - ⊕ U - △ |  |   |   | ADDITIONAL<br>LAB. TESTING<br>& GRAIN SIZE<br>DISTRIBUTION<br>(%) | WELL INSTALLATION<br>AND WATER LEVELS |    |    |
|-------------------------|--|---|-------------|-----------------------|--------|------|---|-----------------------|--|--|--|--|---|---|---|---------------------------------------|----|----|
|                         |  | DESCRIPTION   | STRATA PLOT | ELEV.<br>DEPTH<br>(m) | NUMBER | TYPE | N VALUE   | WATER CONTENT PERCENT |  |  |  |  |   |   |   |                                       |    |    |
|                         |  |   |             |                       |        |      |   | Wp   ○ W   WI         |  |  |  |  |   |   |   |                                       |    |    |
|                         |  | PAVEMENT  |             | 63.40                 |        |      |   |                       |  |  |  |  |   |   |   |                                       |    |    |
| 0                       | Power Auger Drilling<br>203 mm O.D. Solid Stem Auger   | ASPHALT: 60 mm thick  |             | 0.06                  |        |      |   |                       |  |  |  |  |   |   |   |                                       |    |    |
|                         |  | FILL: sand and gravel, 700 mm thick,<br>trace silt and clay, brown/grey, moist,<br>very dense |             |                       |        | 1    | SS  | >50                   |  |  |  |  | ○ |   |   |                                       |    |    |
| 1                       |  | SILTY CLAY: some sand, grey, moist,<br>firm to stiff  |             | 62.64<br>0.76         |        |      |   |                       |  |  |  |  |   | ○ |   |                                       |    |    |
| 2                       |  |   |             | 61.27<br>2.13         |        |      |   |                       |  |  |  |  | ○ |   | 1   | 33                                    | 37 | 29 |
| 3                       | <b>END OF BOREHOLE</b><br>Notes:<br>1. This log is to be read with the subject report and project number as presented above.<br>2. Interpretation assistance by AECOM is required for projects excluding the above mentioned project.<br>3. No abnormal odour or staining was observed unless otherwise indicated.<br>4. No groundwater was observed in the open hole upon the completion. |   |             |                       |        |      |   |                       |  |  |  |  |   |   |   |                                       |    |    |
| 4                       |  |   |             |                       |        |      |   |                       |  |  |  |  |   |   |   |                                       |    |    |
| 5                       |  |   |             |                       |        |      |   |                       |  |  |  |  |   |   |   |                                       |    |    |
| 6                       |  |   |             |                       |        |      |   |                       |  |  |  |  |   |   |   |                                       |    |    |
| 7                       |  |   |             |                       |        |      |   |                       |  |  |  |  |   |   |   |                                       |    |    |
| 8                       |  |   |             |                       |        |      |   |                       |  |  |  |  |   |   |   |                                       |    |    |
| 9                       |  |   |             |                       |        |      |   |                       |  |  |  |  |   |   |   |                                       |    |    |
| 10                      |  |   |             |                       |        |      |   |                       |  |  |  |  |   |   |   |                                       |    |    |

(LOG TO BE READ IN CONJUNCTION WITH REPORT)

DEPTH SCALE

1 : 50



LOGGED: WH

CHECKED: TA

AECOM\_BH\_001\_60634622\_DYT3.GPJ\_GAL-MISS.GDT\_21-2-16



PROJECT: DYT3 - Ottawa  
 LOCATION: 2625 Sheffield Road  
 COORDINATES: N 5031134.8; E 452084.5  
 DATUM: Geodetic  
 AECOM PROJECT #: 60634622  
 CLIENT: Amazon Logistics

# RECORD OF BOREHOLE: BH-19

SHEET 1 OF 1

START DATE: Jan 11, 2021  
 END DATE: Jan 11, 2021  
 BORING METHOD: 203 mm O.D. Solid Stem Auger  
 CONTRACTOR: Aardvark Drilling Inc.

PENETRATION TEST HAMMER, 64kg; DROP, 760mm  
 SAMPLER HAMMER, 64kg; DROP, 760mm

| DEPTH SCALE (METRES) | BORING METHOD  | SOIL PROFILE   |             | SAMPLES         |        |      | Standard Penetration Testing (SPT) Number (blows/0.3m) |                 |  |  | SHEAR STRENGTH $C_u$ , kPa |             |  |  | ADDITIONAL LAB. TESTING & GRAIN SIZE DISTRIBUTION (%) | WELL INSTALLATION AND WATER LEVELS |    |     |
|----------------------|--|--|-------------|-----------------|--------|------|--|-----------------|--|--|----------------------------|-------------|--|--|---|------------------------------------|----|-----|
|                      |  | DESCRIPTION  | STRATA PLOT | ELEV. DEPTH (m) | NUMBER | TYPE | N VALUE  | 20 40 60 80     |  |  |                            | 20 40 60 80 |  |  |   |                                    |    |     |
|                      |  |  |             |                 |        |      |  | 100 200 300 400 |  |  |                            | 10 20 30 40 |  |  |   |                                    |    |     |
| 0                    | Power Auger Drilling<br>203 mm O.D. Solid Stem Auger | PAVEMENT   |             | 64.00           |        |      |  |                 |  |  |                            |             |  |  |   |                                    |    |     |
|                      |  | ASPHALT: 130 mm thick  |             | 60.00           |        |      |  |                 |  |  |                            |             |  |  |   |                                    |    |     |
|                      |  | FILL: crusher run limestone, grey, moist, very dense   |             | 0.13            | 1A     | SS   | 72   |                 |  |  |                            |             |  |  |   | 44                                 | 56 | (0) |
|                      |  | FILL: sand and gravel, some silt and clay, grey, moist, very dense   |             | 0.46            | 1B     | SS   |  |                 |  |  |                            |             |  |  |   |                                    |    |     |
| 1                    |  | CLAYEY SILT: some to trace sand, grey/brown, moist, very stiff to stiff  |             | 0.76            | 2      | SS   | 13   |                 |  |  |                            |             |  |  |   |                                    |    |     |
| 2                    |  |  |             | 3               | SS     | 8    |  |                 |  |  |                            |             |  |  | 0   | 10                                 | 49 | 41  |
| 2.13                 |  | END OF BOREHOLE  |             | 61.87           |        |      |  |                 |  |  |                            |             |  |  |   |                                    |    |     |
| 3                    |  | Notes:<br>1. This log is to be read with the subject report and project number as presented above.<br>2. Interpretation assistance by AECOM is required for projects excluding the above mentioned project.<br>3. No abnormal odour or staining was observed unless otherwise indicated.<br>4. No groundwater was observed in the open hole upon the completion. |             | 2.13            |        |      |  |                 |  |  |                            |             |  |  |   |                                    |    |     |
| 4                    |  |  |             |                 |        |      |  |                 |  |  |                            |             |  |  |   |                                    |    |     |
| 5                    |  |  |             |                 |        |      |  |                 |  |  |                            |             |  |  |   |                                    |    |     |
| 6                    |  |  |             |                 |        |      |  |                 |  |  |                            |             |  |  |   |                                    |    |     |
| 7                    |  |  |             |                 |        |      |  |                 |  |  |                            |             |  |  |   |                                    |    |     |
| 8                    |  |  |             |                 |        |      |  |                 |  |  |                            |             |  |  |   |                                    |    |     |
| 9                    |  |  |             |                 |        |      |  |                 |  |  |                            |             |  |  |   |                                    |    |     |
| 10                   |  |  |             |                 |        |      |  |                 |  |  |                            |             |  |  |   |                                    |    |     |

(LOG TO BE READ IN CONJUNCTION WITH REPORT)

DEPTH SCALE

1 : 50



LOGGED: WH

CHECKED: TA

AECOM\_BH\_001\_60634622\_DYT3.GPJ\_GAL-MISS.GDT\_21-2-16

PROJECT: DYT3 - Ottawa  
 LOCATION: 2625 Sheffield Road  
 COORDINATES: N 5031101.7; E 452049.5  
 DATUM: Geodetic  
 AECOM PROJECT #: 60634622  
 CLIENT: Amazon Logistics

## RECORD OF BOREHOLE: BH-20

SHEET 1 OF 1

START DATE: Jan 11, 2021  
 END DATE: Jan 11, 2021  
 BORING METHOD: 203 mm O.D. Solid Stem Auger  
 CONTRACTOR: Aardvark Drilling Inc.  
 PENETRATION TEST HAMMER, 64kg; DROP, 760mm  
 SAMPLER HAMMER, 64kg; DROP, 760mm

| DEPTH SCALE<br>(METRES) | BORING METHOD  | SOIL PROFILE   |             |                       | SAMPLES |      |         | Standard Penetration Testing<br>(SPT) Number (blows/0.3m) |  |  |  | SHEAR STRENGTH $C_u$ , kPa<br>nat V. - + Q - ●<br>rem V. - ⊕ U - △ |  |  |  | ADDITIONAL<br>LAB. TESTING<br>& GRAIN SIZE<br>DISTRIBUTION<br>(%) | WELL INSTALLATION<br>AND WATER LEVELS |  |  |
|-------------------------|--|--|-------------|-----------------------|---------|------|---------|---|--|--|--|--|--|--|--|---|---------------------------------------|--|--|
|                         |  | DESCRIPTION  | STRATA PLOT | ELEV.<br>DEPTH<br>(m) | NUMBER  | TYPE | N VALUE | WATER CONTENT PERCENT                                     |  |  |  |  |  |  |  |   |                                       |  |  |
|                         |  |  |             |                       |         |      |         | Wp   ○ W   WI   |  |  |  |  |  |  |  |   |                                       |  |  |
|                         |  | PAVEMENT   |             | 64.00                 |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |  |
| 0                       | Power Auger Drilling<br>203 mm O.D. Solid Stem Auger | <b>ASPHALT:</b> 100 mm thick<br><b>FILL:</b> sand and gravel, 660 mm thick,<br>trace silt, grey, moist, very dense   |             | 0.00<br>0.10          |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |  |
| 1                       |  | <b>CLAYEY SILT:</b> trace sand, grey/brown,<br>moist, very stiff   |             | 63.24<br>0.76         | 1       | SS   | >50     |   |  |  |  |  |  |  |  |   |                                       |  |  |
| 2                       |  |  |             | 61.87<br>2.13         | 2       | SS   | 21      |   |  |  |  |  |  |  |  |   |                                       |  |  |
| 3                       |  |  |             |                       | 3       | SS   | 18      |   |  |  |  |  |  |  |  |   |                                       |  |  |
| 4                       |  |  |             |                       |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |  |
| 5                       |  |  |             |                       |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |  |
| 6                       |  |  |             |                       |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |  |
| 7                       |  |  |             |                       |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |  |
| 8                       |  |  |             |                       |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |  |
| 9                       |  |  |             |                       |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |  |
| 10                      |  |  |             |                       |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |  |
|                         |  | <b>END OF BOREHOLE</b><br>Notes:<br>1. This log is to be read with the subject report and project number as presented above.<br>2. Interpretation assistance by AECOM is required for projects excluding the above mentioned project.<br>3. No abnormal odour or staining was observed unless otherwise indicated.<br>4. No groundwater was observed in the open hole upon the completion. |             |                       |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |  |

(LOG TO BE READ IN CONJUNCTION WITH REPORT)

DEPTH SCALE

1 : 50



LOGGED: WH

CHECKED: TA

AECOM\_BH\_001\_60634622\_DYT3.GPJ\_GAL-MISS.GDT\_21-2-16

PROJECT: DYT3 - Ottawa  
 LOCATION: 2625 Sheffield Road  
 COORDINATES: N 5031155.8; E 452042.6  
 DATUM: Geodetic  
 AECOM PROJECT #: 60634622  
 CLIENT: Amazon Logistics

## RECORD OF BOREHOLE: BH-21

SHEET 1 OF 1

START DATE: Jan 11, 2021  
 END DATE: Jan 11, 2021  
 BORING METHOD: 203 mm O.D. Solid Stem Auger  
 CONTRACTOR: Aardvark Drilling Inc.  
 PENETRATION TEST HAMMER, 64kg; DROP, 760mm  
 SAMPLER HAMMER, 64kg; DROP, 760mm

| DEPTH SCALE<br>(METRES) | BORING METHOD  | SOIL PROFILE   |             |                       | SAMPLES |      |         | Standard Penetration Testing<br>(SPT) Number (blows/0.3m) |  |  |  | SHEAR STRENGTH $C_u$ , kPa<br>nat V. - + Q - ●<br>rem V. - ⊕ U - △ |  |  |  | ADDITIONAL<br>LAB. TESTING<br>& GRAIN SIZE<br>DISTRIBUTION<br>(%) | WELL INSTALLATION<br>AND WATER LEVELS |  |             |
|-------------------------|--|--|-------------|-----------------------|---------|------|---------|---|--|--|--|--|--|--|--|---|---------------------------------------|--|-------------|
|                         |  | DESCRIPTION  | STRATA PLOT | ELEV.<br>DEPTH<br>(m) | NUMBER  | TYPE | N VALUE | WATER CONTENT PERCENT                                     |  |  |  |  |  |  |  |   |                                       |  |             |
|                         |  |  |             |                       |         |      |         | $W_p$   $W_L$   |  |  |  |  |  |  |  |   |                                       |  |             |
|                         |  | PAVEMENT   |             | 64.00                 |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |             |
| 0                       | Power Auger Drilling<br>203 mm O.D. Solid Stem Auger | ASPHALT: 100 mm thick  |             | 0.00                  |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |             |
|                         |  | FILL: sand and gravel, some to trace silt, brown/grey, moist, very dense to compact  |             | 0.10                  | 1       | SS   | 61      |   |  |  |  |  |  |  |  |   |                                       |  | GR SA SI CL |
| 1                       |  |  |             |                       | 62.48   |      |         |   |  |  |  |  |  |  |  |   |                                       |  | 47 49 (4)   |
|                         |  | CLAYEY SILT: trace gravel, grey, moist, stiff  |             | 1.52                  |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |             |
| 2                       |  |  |             | 61.87                 | 3       | SS   | 11      |   |  |  |  |  |  |  |  |   |                                       |  |             |
|                         |  | END OF BOREHOLE  |             | 2.13                  |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |             |
| 3                       |  | Notes:<br>1. This log is to be read with the subject report and project number as presented above.<br>2. Interpretation assistance by AECOM is required for projects excluding the above mentioned project.<br>3. No abnormal odour or staining was observed unless otherwise indicated.<br>4. No groundwater was observed in the open hole upon the completion. |             |                       |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |             |
| 4                       |  | DRAFT  |             |                       |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |             |
| 5                       |  |  |             |                       |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |             |
| 6                       |  |  |             |                       |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |             |
| 7                       |  |  |             |                       |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |             |
| 8                       |  |  |             |                       |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |             |
| 9                       |  |  |             |                       |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |             |
| 10                      |  |  |             |                       |         |      |         |   |  |  |  |  |  |  |  |   |                                       |  |             |

(LOG TO BE READ IN CONJUNCTION WITH REPORT)

DEPTH SCALE

1 : 50



LOGGED: WH

CHECKED: TA

AECOM\_BH\_001\_60634622\_DYT3.GPJ\_GAL-MISS.GDT\_21-2-16

PROJECT: DYT3 - Ottawa  
 LOCATION: 2625 Sheffield Road  
 COORDINATES: N 5031125.4; E 452039.9  
 DATUM: Geodetic  
 AECOM PROJECT #: 60634622  
 CLIENT: Amazon Logistics

## RECORD OF BOREHOLE: BH-22

SHEET 1 OF 1

START DATE: Jan 11, 2021  
 END DATE: Jan 11, 2021  
 BORING METHOD: 203 mm O.D. Solid Stem Auger  
 CONTRACTOR: Aardvark Drilling Inc.  
 PENETRATION TEST HAMMER, 64kg; DROP, 760mm  
 SAMPLER HAMMER, 64kg; DROP, 760mm

| DEPTH SCALE (METRES) | BORING METHOD  | SOIL PROFILE   |             | SAMPLES         |        |      | Standard Penetration Testing (SPT) Number (blows/0.3m) |                 |  |  | SHEAR STRENGTH Cu, kPa |             |   |  | ADDITIONAL LAB. TESTING & GRAIN SIZE DISTRIBUTION (%) | WELL INSTALLATION AND WATER LEVELS |  |                  |
|----------------------|--|--|-------------|-----------------|--------|------|--|-----------------|--|--|------------------------|-------------|---|--|---|------------------------------------|--|------------------|
|                      |  | DESCRIPTION  | STRATA PLOT | ELEV. DEPTH (m) | NUMBER | TYPE | N VALUE  | 20 40 60 80     |  |  |                        | 20 40 60 80 |   |  |   |                                    |  |                  |
|                      |  |  |             |                 |        |      |  | 100 200 300 400 |  |  |                        | 10 20 30 40 |   |  |   |                                    |  |                  |
| 0                    | Power Auger Drilling<br>203 mm O.D. Solid Stem Auger | PAVEMENT   |             | 64.30           |        |      |  |                 |  |  |                        |             |   |  |   |                                    |  |                  |
|                      |  | <b>TOPSOIL:</b> 50 mm thick<br><b>FILL:</b> silty clay, trace gravel, some sand, brown, moist, very stiff with buried organics<br><b>CLAYEY SILT:</b> trace gravel, grey/brown, moist, very stiff  |             | 0.05            | 1      | SS   | 19   |                 |  |  |                        | ○           |   |  |   |                                    |  |                  |
| 1                    |  |  |             |                 | 63.64  |      |  |                 |  |  |                        |             |   |  |   |                                    |  |                  |
|                      |  |  |             |                 | 0.66   | 2    | SS   | 28              |  |  |                        |             | ○ |  |   |                                    |  |                  |
| 2                    |  |  |             | 62.17           | 3      | SS   | 21   |                 |  |  |                        | ○           |   |  | 0 19 49 32  |                                    |  |                  |
| 3                    |  | <b>END OF BOREHOLE</b><br>Notes:<br>1. This log is to be read with the subject report and project number as presented above.<br>2. Interpretation assistance by AECOM is required for projects excluding the above mentioned project.<br>3. No abnormal odour or staining was observed unless otherwise indicated.<br>4. No groundwater was observed in the open hole upon the completion. |             | 2.13            |        |      |  |                 |  |  |                        |             |   |  |   |                                    |  | <br>Jan 14, 2021 |

DRAFT

AECOM\_BH\_001\_60634622\_DYT3.GPJ\_GAL-MASS.GDT\_21-2-16

(LOG TO BE READ IN CONJUNCTION WITH REPORT)  
 DEPTH SCALE  
 1 : 50



LOGGED: WH  
 CHECKED: TA

# Appendix **B**

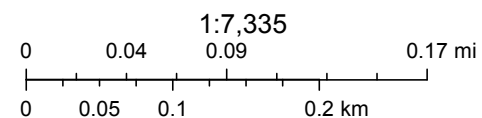
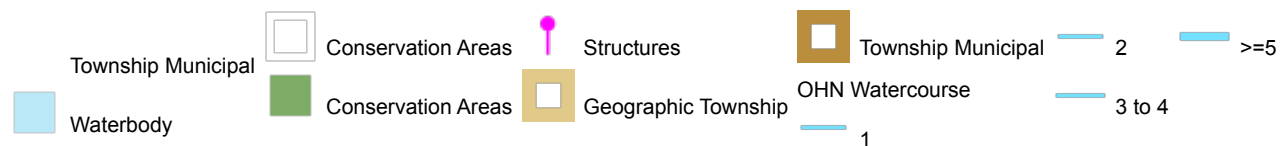
## Regulatory Information



# RVCA Regulations Mapping



2/16/2021, 8:49:30 AM



Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri

RVCA Regulations Mapping - Online Mapping  
Rideau Valley Conservation Authority (RVCA)

# Appendix **C**

## Pre-consultation Comments



## APPLICANT'S STUDY AND PLAN IDENTIFICATION LIST

Legend: **S** indicates that the study or plan is required with application submission.

**A** indicates that the study or plan may be required to satisfy a condition of approval/draft approval.

For information and guidance on preparing required studies and plans refer to:

<http://ottawa.ca/en/development-application-review-process-0/guide-preparing-studies-and-plans>

| S/A | Number of copies | ENGINEERING  |   | S/A | Number of copies |
|-----|------------------|--|---|-----|------------------|
| S   |                  | 1. Site Servicing Plan   | 2. Site Servicing Study                   | S   |                  |
| S   |                  | 3. Grade Control and Drainage Plan                                     | 4. Geotechnical Study                     | S   |                  |
| ■   |                  | 5. Composite Utility Plan  | 6. Groundwater Impact Study               | ■   |                  |
| ■   |                  | 7. Servicing Options Report  | 8. Wellhead Protection Study              | ■   |                  |
| S   |                  | 9. Community Transportation Study and / or Transportation Impact Study | 10. Erosion and Sediment Control Plan     | S   |                  |
| S   |                  | 11. Storm water Management Report                                      | 12. Hydro geological and Terrain Analysis | ■   |                  |
| ■   |                  | 13. Hydraulic Water main Analysis                                      | 14. Noise / Vibration Study               | ■   |                  |
| ■   |                  | 15. Roadway Modification Design Plan                                   | 16. Confederation Line Proximity Study    | ■   |                  |

| S/A | Number of copies | PLANNING / DESIGN / SURVEY                                  |  | S/A | Number of copies |
|-----|------------------|---|--|-----|------------------|
| ■   |                  | 17. Draft Plan of Subdivision                               | 18. Plan Showing Layout of Parking Garage  | ■   |                  |
| ■   |                  | 19. Draft Plan of Condominium                               | 20. Planning Rationale   | S   |                  |
| S   |                  | 21. Site Plan   | 22. Minimum Distance Separation (MDS)  | ■   |                  |
| ■   |                  | 23. Concept Plan Showing Proposed Land Uses and Landscaping | 24. Agrology and Soil Capability Study   | ■   |                  |
| ■   |                  | 25. Concept Plan Showing Ultimate Use of Land               | 26. Cultural Heritage Impact Statement   | ■   |                  |
| S   |                  | 27. Landscape Plan  | 28. Archaeological Resource Assessment<br>Requirements: <b>S</b> (site plan) <b>A</b> (subdivision, condo) | ■   |                  |
| S   |                  | 29. Survey Plan   | 30. Shadow Analysis  | ■   |                  |
| S   |                  | 31. Architectural Building Elevation Drawings (dimensioned) | 32. Design Brief   | S   |                  |
| ■   |                  | 33. Wind Analysis   |  | ■   |                  |

| S/A | Number of copies | ENVIRONMENTAL   |  | S/A | Number of copies |
|-----|------------------|---|--|-----|------------------|
| S   |                  | 34. Phase 1 Environmental Site Assessment                                     | 35. Impact Assessment of Adjacent Waste Disposal/Former Landfill Site        | ■   |                  |
| A   |                  | 36. Phase 2 Environmental Site Assessment (depends on the outcome of Phase 1) | 37. Assessment of Landform Features  | ■   |                  |
| ■   |                  | 38. Record of Site Condition  | 39. Mineral Resource Impact Assessment                                       | ■   |                  |
| S   |                  | 40. Tree Conservation Report  | 41. Environmental Impact Statement / Impact Assessment of Endangered Species | A   |                  |
| ■   |                  | 42. Mine Hazard Study / Abandoned Pit or Quarry Study                         | 43. Integrated Environmental Review (Draft, as part of Planning Rationale)   | ■   |                  |

|  |
|--|
| <b>Number of copies</b>                    |
| <b>Digital versions of all submissions</b> |

Meeting Date: August 18, 2022

Application Type: SPC – complex

File Lead (Assigned Planner): Kelby Lodoen Unseth

Infrastructure Approvals Project Manager: Sharif Sharif

Site Address (Municipal Address): 2625 Sheffield Rd

\*Preliminary Assessment: 1  2  3  4  5

\*One (1) indicates that considerable major revisions are required before a planning application is submitted, while five (5) suggests that proposal appears to meet the City's key land use policies and guidelines. **This assessment is purely advisory and does not consider technical aspects of the proposal or in any way guarantee application approval.**

*It is important to note that the need for additional studies and plans may result during application review. If following the submission of your application, it is determined that material that is not identified in this checklist is required to achieve complete application status, in accordance with the Planning Act and Official Plan requirements, the Planning, Infrastructure and Economic Development Department will notify you of outstanding material required within the required 30 day period. Mandatory pre-application consultation will not shorten the City's standard processing timelines, or guarantee that an application will be approved. It is intended to help educate and inform the applicant about submission requirements as well as municipal processes, policies, and key issues in advance of submitting a formal development application. This list is valid for one year following the meeting date. If the application is not submitted within this timeframe the applicant must again pre-consult with the Planning, Infrastructure and Economic Development Department.*



## Pre-consultation Notes

Meeting: Thursday August 18, 2022 @ 11am

### City Attendees:

Kelby Lodoen Unseth – Planner  
Sharif Sharif – Infrastructure Project  
Manager  
Matthew Hayley – Environmental  
Planner

Ann O'Connor – Urban Design  
Mark Richardson – Forestry

### Location:

2625 Sheffield Road

### Property Overview and Discussion:

The property is zone Heavy Industrial (IH). The purpose of the IH Zone is to:

- 1) permit a wide range of industrial uses, including those which, by their nature, generate noise, fumes, odours, and are hazardous or obnoxious, in accordance with the Employment Area designation of the Official Plan or, the General Urban Area designation where applicable;
- 2) allow in certain Employment Areas or General Urban Areas, a variety of complementary uses such as recreational, health and fitness uses and service commercial (e.g. convenience store, personal service business, restaurant, automobile service station and gas bar), occupying small sites as individual occupancies or in groupings as part of a small plaza, to serve the employees of the Employment or General Urban Area, the general public in the immediate vicinity, and passing traffic;
- 3) prohibit retail uses in areas designated as Employment Area but allow limited sample and showroom space that is secondary and subordinate to the primary use of buildings for the manufacturing or warehousing of the product; and
- 4) provide development standards that would ensure that the industrial uses would not impact on the adjacent non-industrial areas.

The current City of Ottawa Official Plan designates the property as Urban Employment, which identifies lands for a range of employment uses.

The new City of Ottawa Official Plan designates the property as Industrial and Logistics (Section 6.4) under Transect B3 (Outer Urban Transect). The Industrial and Logistics designation is characterized by traditional land uses such as warehousing, distribution, among other uses, requiring a range of parcel sizes.

## Pre-consultation Notes

Meeting: Thursday August 18, 2022 @ 11am

### Discussion:

The site appears to have strong pedestrian connections through the parking areas which is a positive. It is understood that the pedestrian walkway will be extended to the street near the north end of the property with a bus pad to be constructed. It may also be helpful to extend the walkway from the southern portion of the building to the street for pick-up and drop offs.

The City will be looking for a strong landscape plan as the site has substantial street frontage on both Sheffield Road and Humber Place. Although it is noted that above ground hydro lines run along Sheffield Road.

The vehicle and bicycle parking requirements will be confirmed through the Site Plan Control application, and the RVCA and VIA rail will be circulated on the development application.

The outdoor amenity area will be an asset, but consideration should be made to how much the location is shaded, due to the building height on three sides, and if a secondary space with more sun could be accommodated.

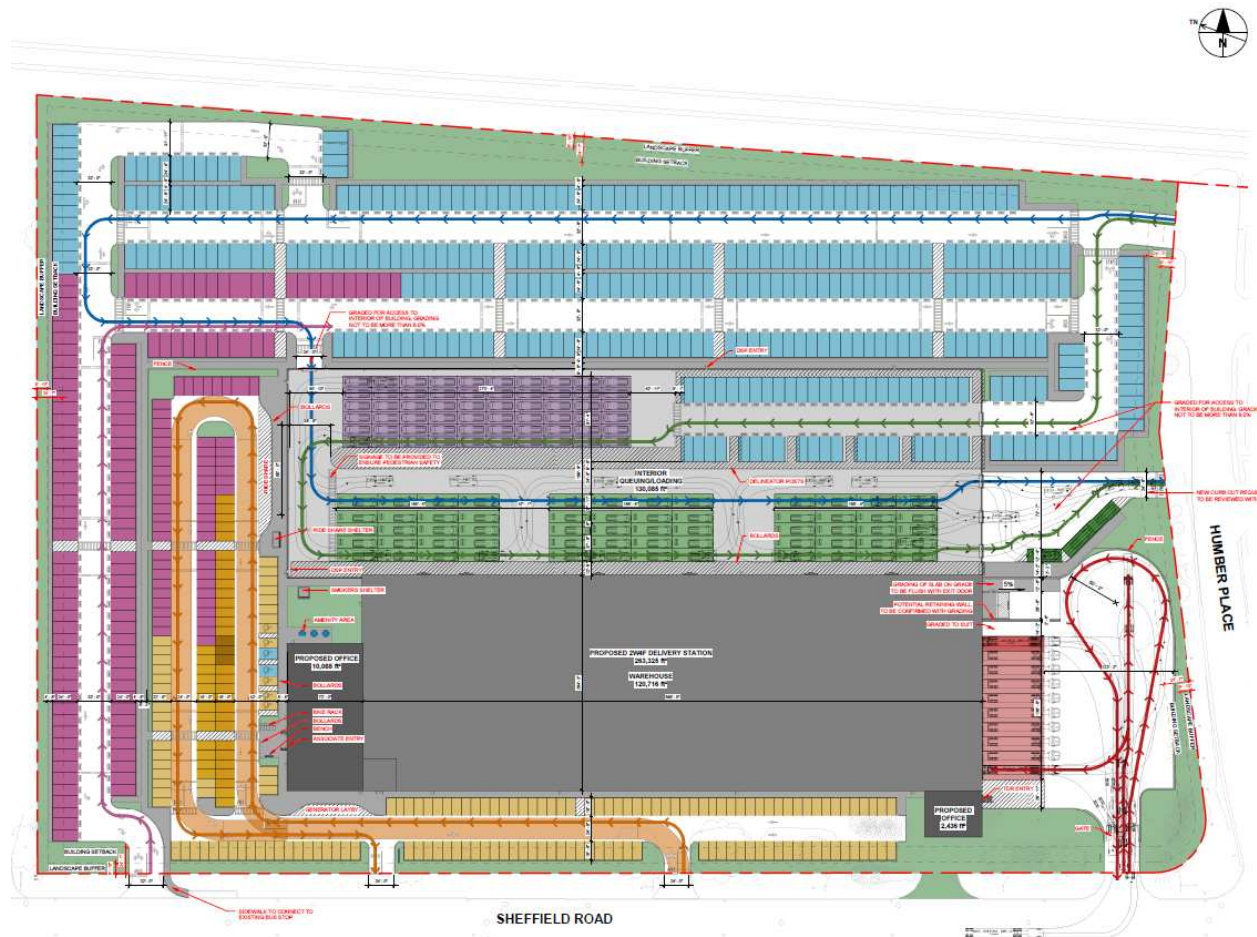
### Property:



# Pre-consultation Notes

Meeting: Thursday August 18, 2022 @ 11am

Site Plan Concept:



## Transportation:

1. A TIA is warranted proceed to scoping.
2. The application will not be deemed complete until the submission of the draft step 2-4, including the functional draft RMA package (if applicable) and/or monitoring report (if applicable).
3. Although a full review of the TIA Strategy report (Step 4) is not required prior to an application, it is strongly recommended.
4. Synchro files are required at Step 4.
5. ROW protection is N/A.
6. Corner sight triangle: 5m x 5m

## Pre-consultation Notes

### Meeting: Thursday August 18, 2022 @ 11am

7. The throat length requirements should follow the TAC guidelines for a collector road.
8. Noise study is not required.

#### **Environment:**

9. Natural Heritage - The property to the east is part of the National Capital Commission (NCC) Greenbelt and is identified New OP as Greenbelt Linkage in Schedule C12 and is indicated as a natural heritage feature on Schedule C11-C. As described above, adjacent lands to the development are to be identified as “greenbelt linkage”, this means that the site will need to ensure there is no negative impact on the linkage. However, an EIS is not triggered if the proposed development site is more than 30 m from the NCC lands. Given the adjacent natural area, lighting of the site will be a concern since it may attract wildlife from the greenbelt lands, some advice and guidance available in the EIS Guidelines and the Bird-safe guidelines.
10. Bird-safe Design - Given the size and type of the proposal the proposal will need to review and incorporate bird safe design elements. Some of the risk factors include glass and related design traps such as corner glass and fly-through conditions, ventilation grates and open pipes, landscaping, light pollution. More guidance and solutions are available in the guidelines which can be found here: [https://documents.ottawa.ca/sites/documents/files/birdsafedesign\\_guidelines\\_en.pdf](https://documents.ottawa.ca/sites/documents/files/birdsafedesign_guidelines_en.pdf)
11. Extreme heat - Please consider features that reduce the urban heat island effect (see OP 10.3.3) produced by the parking lot and a building footprint. For example, this impact can be reduced by adding large canopy trees, green roofs or vegetation walls, or constructing the parking lot or building differently.

#### **Forestry:**

##### **TCR requirements:**

12. a Tree Conservation Report (TCR) must be supplied for review along with the suite of other plans/reports required by the City
  - a) an approved TCR is a requirement of Site Plan approval.
  - b) The TCR may be combined with the LP provided all information is supplied
13. Any removal of privately-owned trees 10cm or larger in diameter, or city-owned trees of any diameter requires a tree permit issued under the Tree Protection Bylaw (Bylaw 2020 – 340); the permit will be based on an approved TCR and made available at or near plan approval.

## Pre-consultation Notes

### Meeting: Thursday August 18, 2022 @ 11am

14. The Planning Forester from Planning and Growth Management as well as foresters from Forestry Services will review the submitted TCR
  - a) If tree removal is required, both municipal and privately-owned trees will be addressed in a single permit issued through the Planning Forester
  - b) Compensation may be required for city owned trees – if so, it will need to be paid prior to the release of the tree permit
  
15. The TCR just contain 2 separate plans:
  - a) Plan/Map 1 - show existing conditions with tree cover information
  - b) Plan/Map 2 - show proposed development with tree cover information
  - c) Please ensure retained trees are shown on the landscape plan
  
16. the TCR must list all trees on site, as well as off-site trees if the CRZ extends into the developed area, by species, diameter and health condition
  
17. please identify trees by ownership – private onsite, private on adjoining site, city owned, co-owned (trees on a property line)
  
18. If trees are to be removed, the TCR must clearly show where they are, and document the reason they cannot be retained
  
19. All retained trees must be shown, and all retained trees within the area impacted by the development process must be protected as per City guidelines available at [Tree Protection Specification](#) or by searching [Ottawa.ca](#)
  - a) the location of tree protection fencing must be shown on the plan
  
20. the City encourages the retention of healthy trees; if possible, please seek opportunities for retention of trees that will contribute to the design/function of the site.
  
21. For more information on the process or help with tree retention options, contact Mark Richardson [mark.richardson@ottawa.ca](mailto:mark.richardson@ottawa.ca) or on [City of Ottawa](#)

### **LP tree planting requirements:**

For additional information on the following please contact [adam.palmer@Ottawa.ca](mailto:adam.palmer@Ottawa.ca)

#### 22. Minimum Setbacks

- a) Maintain 1.5m from sidewalk or MUP/cycle track or water service laterals.
- b) Maintain 2.5m from curb
- c) Coniferous species require a minimum 4.5m setback from curb, sidewalk or MUP/cycle track/pathway.
- d) Maintain 7.5m between large growing trees, and 4m between small growing trees. Park or open space planting should consider 10m spacing, except where otherwise approved in naturalization / afforestation areas. Adhere to

## Pre-consultation Notes

### Meeting: Thursday August 18, 2022 @ 11am

Ottawa Hydro's planting guidelines (species and setbacks) when planting around overhead primary conductors.

#### 23. Tree specifications

- a) Minimum stock size: 50mm tree caliper for deciduous, 200cm height for coniferous.
- b) Maximize the use of large deciduous species wherever possible to maximize future canopy coverage
- c) Tree planting on city property shall be in accordance with the City of Ottawa's Tree Planting Specification; and include watering and warranty as described in the specification (can be provided by Forestry Services).
- d) Plant native trees whenever possible
- e) No root barriers, dead-man anchor systems, or planters are permitted.
- f) No tree stakes unless necessary (and only 1 on the prevailing winds side of the tree)

#### 24. Hard surface planting

- a) Curb style planter is highly recommended
- b) No grates are to be used and if guards are required, City of Ottawa standard (which can be provided) shall be used.
- c) are to be planted at grade

#### 25. Soil Volume

- a) Please document on the LP that adequate soil volumes can be met:

| Tree Type/Size | Single Tree Soil Volume (m <sup>3</sup> ) | Multiple Tree Soil Volume (m <sup>3</sup> /tree) |
|----------------|---|--|
| Ornamental     | 15  | 9  |
| Columnar       | 15  | 9  |
| Small          | 20  | 12   |
| Medium         | 25  | 15   |
| Large          | 30  | 18   |
| Conifer        | 25  | 15   |

- b) Please note that these soil volumes are not applicable in cases with Sensitive Marine Clay.

#### 26. Sensitive Marine Clay

- a) Please follow the City's 2017 Tree Planting in Sensitive Marine Clay guidelines

#### 27. Tree Canopy Cover

- a) The landscape plan shall show how the proposed tree planting will replace and increase canopy cover on the site over time, to support the City's 40%

## Pre-consultation Notes

### Meeting: Thursday August 18, 2022 @ 11am

- b) At a site level, efforts shall be made to provide as much canopy cover as possible, through tree planting and tree retention, with an aim of 40% canopy cover at 40 years, as appropriate.
- c) Indicate on the plan the projected future canopy cover at 40 years for the site.

### **Urban Design:**

28. A Design Brief that follows the provided Terms of Reference is required upon submission of the application.
29. Consider ways to simplify wayfinding and vehicular circulation on site.
- a) Consider reducing the amount of egresses. It appears there are six egresses proposed: two onto Humber Place and four onto Sheffield Road. Are all of these necessary to meet the needs of the site?
  - b) Clarify on the Site Plan if there are fences/barriers proposed between the different programmed areas (areas of different colour-coding on the concept plan).
  - c) If different egresses are needed for different purposes, consider clearly labelling these egresses for the benefit of drivers, so they are able to clearly understand which entrance is appropriate for them. Please illustrate the signs on the Site Plan.
30. Consider providing a simplified Site Plan that removes the various flow directions and colour-coded parking breakdowns. This other Site Plan should focus on providing clarity on:
- a) setbacks (to building, parking lot, and internal roads);
  - b) providing all dimensions in metres (including for the proposed building, proposed amenity area, parking spaces, width of drive aisles and egresses, all setbacks etc.);
  - c) clearly identifying building entrances, all pedestrian pathways, surface materials, vehicular access/navigation on-site, etc.
  - d) clearly identifying the building footprint (including the loading area in the back that will be within the footprint).
31. Consider how the building facade facing Sheffield Rd can be designed to announce the building to the street. For example, consider:
- a) Incorporating glazing into the office portion
  - b) Making prominent entrances
  - c) Incorporating design elements to identify that this is the front of the building, and
  - d) Removing/reducing blank walls facing Sheffield
32. Consider pedestrian flow on site.
- a) Support for the design of the pathways connecting to the bus stop and the provision of a new bus stop.

## Pre-consultation Notes

### Meeting: Thursday August 18, 2022 @ 11am

- b) Consider providing a pedestrian pathway from Sheffield Rd to the entrance of the building, facing Sheffield Rd.
  - c) Continue to consider the desire-lines and safety of the drivers/staff walking around the site.
33. Consider how to facilitate a great amenity space.
- a) Consider moving the smoking area away from the picnic tables where non-smokers may choose to eat;
  - b) Consider adding a tree to provide shade;
  - c) Consider a location that will get sunlight;
  - d) Consider the most convenient location for staff;
  - e) Consider the views from people using the amenity area.
34. Consider ways to incorporate meaningful landscaping and tree plantings on-site.

### **Planning:**

35. Stie Plan Control: <https://ottawa.ca/en/planning-development-and-construction/development-information-residents/development-application-review-process/development-application-submission/development-applications/site-plan-control>
36. City of Ottawa Accessibility Design Standards: [https://documents.ottawa.ca/sites/documents/files/documents/accessibility\\_design\\_standards\\_en.pdf](https://documents.ottawa.ca/sites/documents/files/documents/accessibility_design_standards_en.pdf)
37. Please ensure that the Parking, Queuing and Loading Provisions are following and appropriate vehicle and bicycle parking is provided on-site (<https://ottawa.ca/en/part-4-parking-queuing-and-loading-provisions-sections-100-114#bicycle-parking-space-rates-and-provisions-sec-111>).
38. Please ensure that the Landscaping Provisions for Parking Lots is followed (<https://ottawa.ca/en/part-4-parking-queuing-and-loading-provisions-sections-100-114#section-110-landscaping-provisions-parking-lots>).
39. The Planning Rationale Terms of Reference may be found [here](#).
40. For information on Applications, including fees, please visit: <https://ottawa.ca/en/planning-development-and-construction/developing-property/development-application-review-process/development-application-submission/development-application-forms#site-plan-control>
41. The application processing timeline generally depends on the quality of the submission. For more information on standard processing timelines, please visit: <https://ottawa.ca/en/city-hall/planning-and-development/information->



## Pre-consultation Notes

### Meeting: Thursday August 18, 2022 @ 11am

[developers/development-application-review-process/development-application-submission/development-application-forms#site-plan-control](https://developers/development-application-review-process/development-application-submission/development-application-forms#site-plan-control)

42. Bird-safe design guidelines:

[https://documents.ottawa.ca/sites/documents/files/birdsafe\\_designguidelines\\_en.pdf](https://documents.ottawa.ca/sites/documents/files/birdsafe_designguidelines_en.pdf)

### **Engineering:**

*List of Reports and Plans (Site Plan Control):*

- Site Servicing Plan
- Grading Plan
- Drainage/ Ponding Plan
- Erosion and Sediment Control Plan
- Stormwater Management and Site Servicing Report
- Geotechnical Investigation Report

Please note the following information regarding the engineering design submissions for the above noted site:

46. The Servicing Study Guidelines for Development Applications are available at the following address:

<https://ottawa.ca/en/city-hall/planning-and-development/how-develop-property/development-application-review-process-2/guide-preparing-studies-and-plans>

47. Servicing and site works shall be in accordance with the following documents:

- Ottawa Sewer Design Guidelines, Second Edition, (October 2012), including Technical Bulletins, ISDTB-2014-01, PIEDTB-2016-01, ISTB 2018-01, ISTB-2018-04, and ISTB-2019-02
- Ottawa Design Guidelines – Water Distribution, First Edition, (July 2010), including Technical Bulletins ISD-2010-2, ISDTB-2014-02, ISTB-2018-02, and ISTB-2021-03
- Geotechnical Investigation and Reporting Guidelines for Development Applications in the City of Ottawa (Revised 2008)
- City of Ottawa Slope Stability Guidelines for Development Applications (Revised 2012)

## Pre-consultation Notes

### Meeting: Thursday August 18, 2022 @ 11am

- City of Ottawa Environmental Noise Control Guidelines (January, 2016)
- City of Ottawa Hydrogeological and Terrain Analysis Guidelines (March 2021)
- City of Ottawa Park and Pathway Development Manual (2012)
- City of Ottawa Accessibility Design Standards (2012)
- Ottawa Standard Tender Documents (latest version)
- Ontario Provincial Standards for Roads & Public Works (2013)

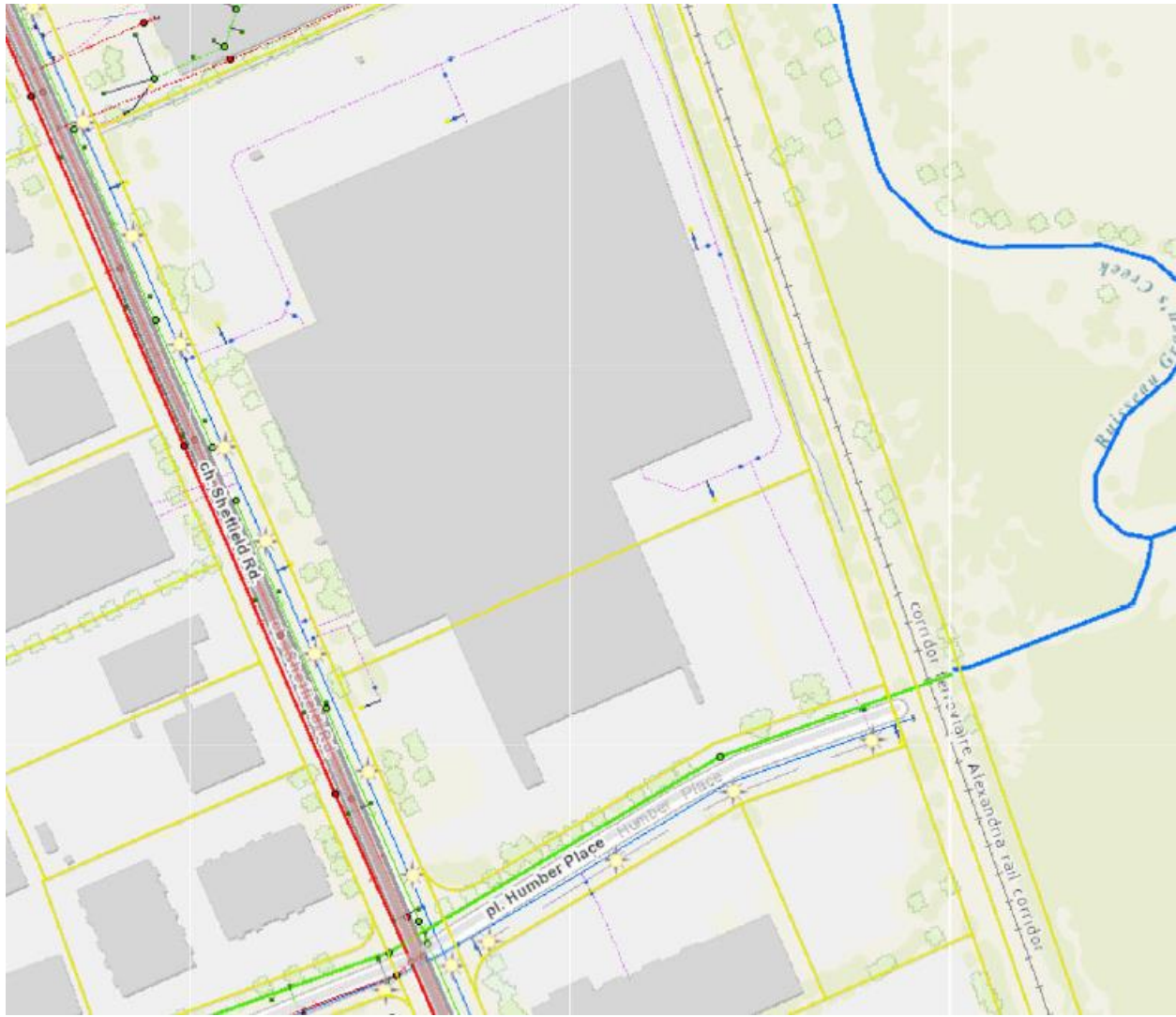
48. Record drawings and utility plans are also available for purchase from the City (Contact the City's Information Centre by email at [InformationCentre@ottawa.ca](mailto:InformationCentre@ottawa.ca) or by phone at (613) 580-2424 x 44455

49. The Stormwater Management Criteria for the subject site is to be based on the following:

- The pre-development runoff coefficient or a maximum equivalent 'C' of 0.5, whichever is less (§ 8.3.7.3).
- For separated sewer system built pre-1970 the design of the storm sewers are based on a 2 year storm.
- Flows to the storm sewer in excess of the 2-year pre-development storm release rate, up to and including the 100-year storm event, must be detained on site
- Ensure no overland flow for all storms up to and including the 100-year event.
- The 2-yr storm event using the IDF information derived from the Meteorological Services of Canada rainfall data, taken from the MacDonald Cartier Airport, collected 1966 to 1997.
- A calculated time of concentration (Cannot be less than 10 minutes).
- Quality control and sub watershed requirements to be provided by Rideau Valley Conservation Authority (RVCA)

# Pre-consultation Notes

Meeting: Thursday August 18, 2022 @ 11am



## 50. Deep Services:

### Hydrants



### Hydrant Laterals



### Trunk Sewers

- Sanitary Pipe (Red dashed line)
- Combined Pipe (Orange dashed line)
- Storm Pipe (Green dashed line)

### Water Pipes

- Public (Solid blue line)
- Private (Dashed blue line)

### Valves

- Valve (Blue square symbol)
- TVS, A, D (Black square symbol)

### Storm Manholes



### Storm Inlets



## Pre-consultation Notes

### Meeting: Thursday August 18, 2022 @ 11am

- i. *A plan view of the approximate services may be seen above. Services should ideally be grouped in a common trench to minimize the number of road cuts. The sizing of available future services is:*
  - a. Humber Pl:
    - i. Storm – 1950 mm (Trunk Sewer).
  - b. Sheffield Road:
    - i. Sanitary – 370 mm.
    - ii. Storm – 375/525 mm.
    - iii. Water – 300 mm.
- ii. *Provide existing servicing information and the recommended location for the proposed connections. Services should ideally be grouped in a common trench to minimize the number of road cuts.*
- iii. *Connections to trunk sewers and easement sewers are not permitted.*
- iv. *Provide information on the monitoring manhole requirements – should be located in an accessible location on private property near the property line (ie. Not in a parking area).*
- v. *Review provision of a high-level sewer.*
- vi. *Provide information on the type of connection permitted*

Sewer connections to be made above the springline of the sewermain as per:

- a. Std Dwg S11.1 for flexible main sewers – *connections made using approved tee or wye fittings.*
- b. Std Dwg S11 (For rigid main sewers) – *lateral must be less than 50% the diameter of the sewermain,*
- c. Std Dwg S11.2 (for rigid main sewers using bell end insert method) – *for larger diameter laterals where manufactured inserts are not available; lateral must be less than 50% the diameter of the sewermain,*
- d. *Connections to manholes permitted when the connection is to rigid main sewers where the lateral exceeds 50% the diameter of the sewermain. – Connect obvert to obvert with the outlet pipe unless pipes are a similar size.*
- e. *No submerged outlet connections.*
- vii. *Please provide estimated storm and sanitary flows before the first submission, to allow the City to confirm whether there are any downstream capacity constraints.*

51. Civil consultant must request boundary conditions from the City's assigned Project Manager prior to first submission. Water Boundary condition requests must include the location of the service and the expected loads required by the proposed development. Please provide the following information:

- i. Location of service(s)

## Pre-consultation Notes

### Meeting: Thursday August 18, 2022 @ 11am

- ii. Type of development and the amount of fire flow required (as per FUS, 1999).
- iii. Average daily demand: \_\_\_\_ l/s.
- iv. Maximum daily demand: \_\_\_\_ l/s.
- v. Maximum hourly daily demand: \_\_\_\_ l/s.
- vi. Hydrant location and spacing to meet City's Water Design guidelines.
- vii. Water supply redundancy will be required for more than 50 m<sup>3</sup>/day water demand.

52. Phase 1 ESAs and Phase 2 ESAs must conform to clause 4.8.4 of the Official Plan that requires that development applications conform to Ontario Regulation 153/04.

53. All development applications should be considered for an Environmental Compliance Approval (ECA) by the Ministry of the Environment, Conservation, and Parks (MECP);

- a. The consultants determine if an approval for sewage works under Section 53 of OWRA is required and determines what type of application. The City's project manager may help confirm and coordinate with the MECP as required.
- b. The project will be either transfer of review (standard), transfer of review (additional), direct submission, or exempt as per O. Reg. 525/98.
- c. Pre-consultation is not required if applying for standard or additional works (Schedule A of the Agreement) under Transfer Review.
- d. Pre-consultation with local District office of MECP is recommended for direct submission.
- e. Consultant completes an MECP request form for a pre-consultation. Send request to [moeccottawasewage@ontario.ca](mailto:moeccottawasewage@ontario.ca)
- f. ECA applications are required to be submitted online through the MECP portal. A business account required to submit ECA application. For more information visit <https://www.ontario.ca/page/environmental-compliance-approval>

NOTE: Site Plan Approval, or Draft Approval, is required before an application is sent to the MECP.

54. General Engineering Submission requirements:

- a. All industrial zone site must be verified eligibility/exemption for ECA process.
- b. Water supply redundancy will be required for more than 50 m<sup>3</sup>/day water demand.

## Pre-consultation Notes

### Meeting: Thursday August 18, 2022 @ 11am

- c. Discharge to Humber PI storm trunk require back water valve for storm sewer within the site as per previous discussion. Provide the correspondence with the report.
- d. As per section 53 of the Professional Engineers Act, O. Reg 941/40, R.S.O. 1990, all documents prepared by engineers must be signed and dated on the seal.
- e. All required plans are to be submitted on standard A1 size sheets (594mm x 841mm) sheets, utilizing a reasonable and appropriate metric scale as per City of Ottawa Servicing and Grading Plan Requirements: title blocks are to be placed on the right of the sheets and not along the bottom. Engineering plans may be combined, but the Site Plans must be provided separately. Plans shall include the survey monument used to confirm datum. Information shall be provided to enable a non-surveyor to locate the survey monument presented by the consultant.
- f. All required plans & reports are to be provided in \*.pdf format (at application submission and for any, and all, re-submissions).

### **Parks**

55. Comments outstanding.

### **Attachments:**

- Plan and study list
- Urban Design Terms of Reference

For any questions, please feel free to contact me at the information below. Please provide all submission documents electronically as paper copies of plans and reports are not being requested at this time.

Best regards,



**Kelby Lodoen Unseth** MCIP, RPP

Planner II | Urbaniste II

Development Review (South Services) | Examen des projets d'aménagement (services sud)

## Pre-consultation Notes

### Meeting: Thursday August 18, 2022 @ 11am

Planning, Infrastructure and Economic Development | Services de planification, d'infrastructure et de développement économique

City of Ottawa | Ville d'Ottawa

☎ 613.580.2424 ext./poste 12852

[ottawa.ca/planning](https://ottawa.ca/planning) / [ottawa.ca/urbanisme](https://ottawa.ca/urbanisme)

Enc.

### Description:

A Design Brief is the core submission document that illustrates how the development is designed to work with its existing and planned context, to improve its surroundings and also demonstrate how the proposal supports the overall goals of the Official Plan, relevant secondary plans, Council approved plans and design guidelines. The purpose of the Terms of Reference is to assist the applicant to organize and substantiate the design justification in support of the proposed development and to assist staff and the public in the review of the proposal.

### Authority to Request a Design Brief:

The *Planning Act* gives municipalities the authority to require that a Design Brief be prepared. Under Sections 22(4), (5) and Section 41(4) of the *Planning Act*, a Council has the authority to request such other information or material that the authority needs in order to evaluate and make a decision on an application. Section 5.2.6 of the Official Plan sets out the general requirement for a Design Brief.

### Preparation:

The Design Brief should be signed by an urban designer, licenced architect, landscape architect, or a full member of the Canadian Institute of Planners.

### When Required:

A Design Brief is required for a Site Plan Control planning application.

A Scoped Design Brief\* is required when the following planning applications are applied for and not accompanied by a Site Plan Control application:

- Official Plan Amendment
- Zoning By-law Amendment (exception: a change in use which does not result in an increase in height or massing)

The requirement and scope of a Design Brief will be determined at the formal pre-application consultation meeting. Should an application be required to go to the [Urban Design Review Panel \(UDRP\)](#), the Design Brief may be submitted as part of the submission materials to the panel.

### Contents for Design Brief Submissions:

A Design Brief will contain and/or address the points identified during the pre-consultation meeting. Failure to address the critical elements identified in the pre-consultation meeting may result in the application being considered incomplete.

\* A *Scoped Design Brief* is composed of:

- Section 1 should be combined into the *Planning Rationale* submission, and
- Section 2 items will be confirmed in the pre-application consultation meeting.



**SECTION 1** *Note: This section may be combined with the Planning Rationale report*

Application Submission:

Not Required

Required

State the: type of application, legal description, municipal address, purpose of the application and provide an overall vision statement and goals for the proposal.

Response to City Documents:

Not Required

Required

State the Official Plan land use designation for the subject property and demonstrate how the proposal conforms to the Official Plan as it relates to the design of the subject site. Reference specific policy numbers from the Official Plan to show consistency. Justify areas of non-compliance and explain why there is non-compliance.



State the applicable plans which apply to the subject proposal: community design plan, secondary plan, concept plan and design guideline. Reference the relevant design related policies within the applicable plans/guidelines and provide a comprehensive analysis as to how the proposed development incorporates the objectives or why it does not incorporate the objectives.

Context Plan:

Not Required

Required

Provide a contextual analysis that discusses/illustrates abutting properties, key destinations and linkages within a 100 meter radius (a larger radius may be requested for larger/more complex projects), such as transit stations, transportation networks for cars, cyclists, and pedestrians, focal points/nodes, gateways; parks/open spaces, topography, views towards the site, the urban pattern (streets, blocks), future and current proposals (if applicable), public art and heritage resources.



Photographs to illustrate existing site conditions and surrounding contexts. Include a map pinpointing (with numbers) where each photo is taken and correspond these numbers with the site photos. Arrows illustrating the direction the photo is taken is also useful.

### SECTION 2

#### Design Proposal:

The purpose of the Design Proposal is to show the building elevations, exterior details, transitions in form, treatment of the public realm and compatibility with adjacent buildings, using 3-D models, illustrations, diagrams, plans, and cross sections. Referencing Official Plan, Section 5.2.1, as determined at time of pre-application consultation meeting, submissions will need to address the following in the form of labelled graphics and written explanation:

#### **Massing and Scale**

Not Required

Required





#### *Images which show:*

#### Building massing – from:

- at least two sides set within its current context (showing the entire height and width of the building) **OR**
- all four sides set within its current context (showing the entire height and width of the building).





#### Views – of the entire block, from:

- at least two perspectives to show how the proposed building is set within its current context **OR**
- all four perspectives to show how the proposed building is set within its current context.



Building transition – to adjacent uses, with labelled explanation of the transition measures used.



Grading – if grades are an issue.



Alternative building massing – additional imagery and site layouts considered and provide justification for the ultimate proposal sought.

#### **Public Realm**

Not Required

Required



#### *Labelled graphics and a written explanation which show:*

Streetscape – cross sections which illustrate the street design and right of way (referencing the City's design manuals).



Relationship to the public realm – illustrating how the first few storeys of the proposed development responds to and relates to the existing context (e.g. through a podium plan and first floor plan). This is to include detailed explanation on:

- Architectural responses
- Landscaping details
- Public art features (in accordance with Official Plan, Section 4.11)
- For developments in Design Priority Areas, detail the building and site features, (in accordance with Official Plan, Section 4.11) which will enhance the public realm. Provide explanation for features which are not provided.

### **Building Design**

Not Required

Required

Labelled graphics (e.g. building elevations and floor plans) and a written explanation which document the proposed exterior architectural details and design (in accordance with Official Plan, Section 5.2.1).



For high-rise development applications, detail the building design and massing and scale elements and how they relate to the proposed high-rise development (in accordance with Official Plan, Section 5.2.1).

### **Sustainability**

Not Required

Required

Any sustainable design features to be incorporated, such as green roofs or walls, sun traps, reflective or permeable surfaces.

### **Heritage**

Not Required

Required

How the building relates to the historic details, materials, site and setting of any existing historic resources on or adjacent to the subject property (if applicable).

## **Additional Contents:**

Some proponents may be requested to provide submission material which complements the Design Brief. These additional requirements could be incorporated into the Design Brief submission for ease of review. These will be identified at the time of application consultation meeting:

- Site Plan
- Landscape Plan
- Elevations
- Plan showing existing and proposed servicing
- Shadow Analysis
- Wind Analysis

## **Submission Requirements**

- Digital copies only

## Paliouras, Kosta

---

**From:** Ahmed, Aziz (MECP) <Aziz.Ahmed@ontario.ca>  
**Sent:** Monday, August 29, 2022 9:22 AM  
**To:** Paliouras, Kosta  
**Cc:** Kuljanin, Milan; Warnock, Charles; Primeau, Charlie (MECP)  
**Subject:** [EXTERNAL] RE: 2625 Sheffield Road Ottawa ON

Kosta,

All is well, hope the same with you.

Based on the analysis you have provided that the works meets the criteria in s.3 of R525/98, I agree that the change in configuration of the development alone does not alter the exemption from the requirement to obtain an ECA.

Stay safe,

Aziz

**Aziz S. Ahmed, P.Eng.** | Manager

Municipal Water and Wastewater Permissions Section, Environmental Permissions Branch | Environmental Assessment and Permissions Division

**Ministry of the Environment, Conservation and Parks** | 40 St. Clair Ave. West, 2<sup>nd</sup> Floor, Toronto, ON M4V 1M2

Tel: 416.314.4625 | Cell: 416.712.7427 | Toll Free: 1-888-999-1305 | Fax: 416.314.1037 | ✉: [Aziz.Ahmed@ontario.ca](mailto:Aziz.Ahmed@ontario.ca)

**If you have any accommodation needs or require communication supports or alternate formats, please let me know.**

**Si vous avez des besoins en matière d'adaptation, ou si vous nécessitez des aides à la communication ou des médias substituts, veuillez me le faire savoir.**

---

**From:** Paliouras, Kosta <kosta.paliouras@aecom.com>

**Sent:** August-29-22 9:16 AM

**To:** Ahmed, Aziz (MECP) <Aziz.Ahmed@ontario.ca>

**Cc:** Kuljanin, Milan <Milan.Kuljanin@aecom.com>

**Subject:** FW: 2625 Sheffield Road Ottawa ON

**CAUTION -- EXTERNAL E-MAIL - Do not click links or open attachments unless you recognize the sender.**

Good morning Aziz

I hope all is fine and you've had a good summer.

In October 2021, you indicated to the City of Ottawa staff that the proposed works at 2625 Sheffield Road in Ottawa, ON would not require a Sewage Works ECA permit (email chain is below). Since October 2021, there was a change to the layout of the Site but the nature of the Site has not changed.

Attached is a letter requesting an exemption from requiring an Sewage Works ECA for the Site works.

Please review and let me know if you have any questions

Thank you,  
Kosta

**Kosta Paliouras**, P.Eng  
Senior Water Resources Engineer/Project Manager/Group Leader, Water  
D +1-519-650-8669  
M +1-226-749-0964  
[kosta.paliouras@aecom.com](mailto:kosta.paliouras@aecom.com)

*In light of the COVID-19 situation, I am currently working remotely away from the office. In any instance, please contact me at any of the numbers above*

---

**From:** Sharif, Golam <[sharif.sharif@ottawa.ca](mailto:sharif.sharif@ottawa.ca)>  
**Sent:** Tuesday, October 26, 2021 11:30 AM  
**To:** Kuljanin, Milan <[Milan.Kuljanin@aecom.com](mailto:Milan.Kuljanin@aecom.com)>  
**Subject:** [EXTERNAL] FW: 2625 Sheffield Road Ottawa ON

Good Morning Milan,

I have received a confirmation from the Toronto Office regarding the MECP ECA exemption. Please see the response below. I believe, according to the information you provided for the proposed development the land use do not fall under industrial use, thus Toronto Office confirmed no ECA will be required.

Please include this correspondence in your updated SWM and servicing report.

Thank you.

Sharif

---

**From:** Warnock, Charles <[Charles.Warnock@ottawa.ca](mailto:Charles.Warnock@ottawa.ca)>  
**Sent:** October 26, 2021 10:53 AM  
**To:** Sharif, Golam <[sharif.sharif@ottawa.ca](mailto:sharif.sharif@ottawa.ca)>  
**Subject:** 2625 Sheffield Road Ottawa ON

Hi Sharif, please see the response below from the MECP.  
They have concluded that the land use is not Industrial.  
If the proposal meets all conditions of O.Reg. 525/98 then I see no requirement to obtain an ECA.  
Thanks.  
Charles

---

**From:** Ahmed, Aziz (MECP) <[Aziz.Ahmed@ontario.ca](mailto:Aziz.Ahmed@ontario.ca)>  
**Sent:** October 26, 2021 9:54 AM  
**To:** Warnock, Charles <[Charles.Warnock@ottawa.ca](mailto:Charles.Warnock@ottawa.ca)>  
**Subject:** RE: 2625 Sheffield Road Ottawa ON

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Charles,

Hope you are well. Based on the landuse described, I agree that this does not fall under the classification of industrial use.

I would also like to draw your attention to the following:

We are happy to inform you that we have posted a notice on the Environmental Registry of Ontario (ERO) about our proposal to amend O. Reg. 525/98 under the *Ontario Water Resources Act*. The proposed changes would remove the requirement to obtain an Environmental Compliance Approval for low risk sewage works.

The proposal notice will be available for public comment for 45 days, closing on December 9, 2021. The [posting](#) can be accessed on the Environmental Registry of Ontario. The feedback that we receive during this 45-day consultation period will help finalize the amendments to the regulations.

Please provide comments on this if you are interested, including the definition of industrial land, and services on private property which you have raised previously.

Stay safe,

Aziz

**Aziz S. Ahmed, P.Eng.** | Manager

Municipal Water and Wastewater Permissions Section, Environmental Permissions Branch | Environmental Assessment and Permissions Division

**Ministry of the Environment, Conservation and Parks** | 40 St. Clair Ave. West, 2<sup>nd</sup> Floor, Toronto, ON M4V 1M2

Tel: 416.314.4625 | Cell: 416.712.7427 | Toll Free: 1-888-999-1305 | Fax: 416.314.1037 ✉: [Aziz.Ahmed@ontario.ca](mailto:Aziz.Ahmed@ontario.ca)

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**Si vous avez des besoins en matière d'adaptation, ou si vous nécessitez des aides à la communication ou des médias substitués, veuillez me le faire savoir.**

---

**From:** Warnock, Charles <[Charles.Warnock@ottawa.ca](mailto:Charles.Warnock@ottawa.ca)>

**Sent:** October-26-21 9:50 AM

**To:** Ahmed, Aziz (MECP) <[Aziz.Ahmed@ontario.ca](mailto:Aziz.Ahmed@ontario.ca)>

**Subject:** 2625 Sheffield Road Ottawa ON

**CAUTION -- EXTERNAL E-MAIL - Do not click links or open attachments unless you recognize the sender.**

Hi Ahmed, I hope you are well and having a good day.

I am just following up on this email.

Thanks and have a good day.

Charles

---

**From:** Warnock, Charles

**Sent:** October 21, 2021 11:38 AM

**To:** Aziz Ahmed ([aziz.ahmed@ontario.ca](mailto:aziz.ahmed@ontario.ca)) <[aziz.ahmed@ontario.ca](mailto:aziz.ahmed@ontario.ca)>

**Subject:** 2625 Sheffield Road Ottawa ON

Hi Ahmed, I hope you are well and having a good day.

I am just following up on this email.

Thanks and have a good day.

Charles

---

**From:** Warnock, Charles

**Sent:** October 13, 2021 1:40 PM

**To:** Aziz Ahmed ([aziz.ahmed@ontario.ca](mailto:aziz.ahmed@ontario.ca)) <[aziz.ahmed@ontario.ca](mailto:aziz.ahmed@ontario.ca)>

**Subject:** 2625 Sheffield Road Ottawa ON

Hi Aziz, I hope all is well with you and that you had a nice long weekend.

Would the MECP consider that an Industrial ECA is not required for this site?

Furthermore, if no Industrial ECA is required it meets the other requirements for an exemption and therefore no ECA would be required.

We have a site plan application at 2625 Sheffield Road Ottawa ON.

The owner is Choice Properties Reit.

AECOM the civil consultant for the owner has made a request to ask the MECP if an Industrial ECA is required

The proposed works consists of developing an existing vegetated area to expand a large parking area only. There is no expansion of the existing building and will not require an expansion of the existing sanitary and water servicing. Due to the expansion of the parking lot area into existing vegetated area, additional surface runoff will discharge off-Site and would require additional water quality and quantity controls to minimize detrimental impacts to the downstream outlet. The objective for these stormwater management facilities is to provide water quality treatment, water quantity control, and groundwater recharge in accordance with the City's requirements for development.

The proposed stormwater management facilities will consist of an underground chamber storage systems (StormTech MC-3500 systems or approved equivalent) with the capacity to accept surface runoff up to and including the 100-year storm event for the proposed parking lot area and provide water quality treatment prior to discharging downstream. The chamber storage systems will consist of storage chambers with clear stone granular material bedding, surrounded by a permeable liner to encourage infiltration of runoff from the parking lot area. The proposed underground chamber storage systems will then ultimately discharge to the municipal infrastructure on Leeds Road. Existing drainage patterns from the existing building structure and parking lot area located north and west of the building structure will be maintained. The existing discharge control and location will be maintained to regulate discharge as per City's requirements.

The Site is zoned 'IH' (Heavy Industrial Use). AECOM has indicated that *"there will be no machinery or on-site processes that would require industrial water use to discharge to the municipal system and no outdoor storage of processed material or any contaminate material. Due to the purpose of the Site, there will be consistent van and truck traffic through the proposed parking lot area. The extent of untreated surface runoff would originate from parking lot area and would include total suspended solids (TSS), vehicular oil and chlorides. The level of concern is minimal."*

Ontario Water Resources act defines industrial land as “land used for the production, processing, repair, maintenance or storage of goods or materials, or the processing, storage, transfer or disposal of waste, but does not include land used primarily for the purpose of buying or selling, (a) goods or materials other than fuel, or (b) services other than vehicle repair services.”

The proposed use meets the MECP’s definition of Industrial lands however the consultant has indicated that “*The level of concern is minimal.*”

The SWMF services only the subject parcel and the site outlets to an existing storm sewer.

Ontario Regulation 525/98 states that Subsection 53 (1) and (3) of the Act do not apply to lands designed as:

- one parcel,
- that discharge into a storm sewer that is not combined,
- does not service industrial and or located on industrial land.”

The development is a single parcel of land, out letting to a storm sewer that is not combined.

Please let of us know if an Industrial ECA is required.

Thank you in advance.  
Charles

,

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,



Aziz S. Ahmed, P.Eng.  
Manager, Municipal Water and Wastewater Permissions Section  
Environmental Branch - Environmental Assessment and Permissions  
Division  
Ministry of the Environment, Conservation, and Parks  
40 St. Clair Avenue West, 2<sup>nd</sup> Floor  
Toronto, Ontario M4V 1M2

August 29, 2022

**Project #**  
60684725

**DRAFT**

**Subject: Environmental Compliance Approval (ECA) Exemption  
DYT3 Distribution Facility  
2625 Sheffield Road, Ottawa, Ontario**

Dear Mr. Ahmed:

The following letter is to indicate that the proposed distribution facility at 2625 Sheffield Road in Ottawa, Ontario (Site) is exempted from requiring an Environmental Compliance Approval (ECA) permit from the Ministry of Environment, Conservation, and Parks (MECP), as per Ontario Regulation 525/98.

Existing Site conditions consist of a building structure, parking lot area, and vegetated area. The Site is approximately 7.06 hectares (ha) in total size, with an existing building structure footprint of approx. 3,796 square metres (m<sup>2</sup>). The proposed works consists of demolishing the existing building structure and parking lot area and redeveloping for a proposed 2,490 m<sup>2</sup> building structure and regraded parking lot area. Additional stormwater management infrastructure (such as infiltration basins, storm sewers, underground chamber storage, etc.) will be required to meet City of Ottawa discharge requirements.

#### Exemption Reasoning

Ontario Regulation 525/98 states that Subsection 53 (1) and (3) of the Act do not apply to lands designed as:

- one parcel, for which the Site and all proposed works will be contained;
- that discharge into a storm sewer that is not combined, for which is not the case at the Site, as sanitary and storm services currently are and will continue to be separate;
- does not service industrial or a structure located on industrial land; and
- is not located on industrial land.

Ontario Water Resources Act defines industrial land as “land used for the production, processing, repair, maintenance or storage of goods of materials, or the processing, storage, transfer or disposal of waste, but does not include land used primarily for the purpose of buying or selling, (a) goods or materials other than fuel, or (b) services other than vehicle repair services.”

Though the Site is located within a “Heavy Industrial Zone” according to the zoning by-law, the primary purpose of the proposed development will be for the distribution of goods and material, with only van and truck traffic through the proposed parking lot area. There will be no machinery or on-site processes that would require industrial water use to discharge to the municipal system and no outdoor storage of processed material or any contaminate material. Contaminates would include total suspended solids (TSS), vehicular oil and chlorides from the parking lot area. The proposed infiltration basins will only accept discharge from the proposed roof areas and an impermeable liner is proposed for the proposed underground chamber storage systems and

therefore none of the runoff from the parking lot area will infiltrated into the underlying soil. The level of concern would be minimal.

I hope this letter is to your satisfaction. If there are any questions, feel free to contact me at [kosta.paliouras@aecom.com](mailto:kosta.paliouras@aecom.com) or 519-650-8669.

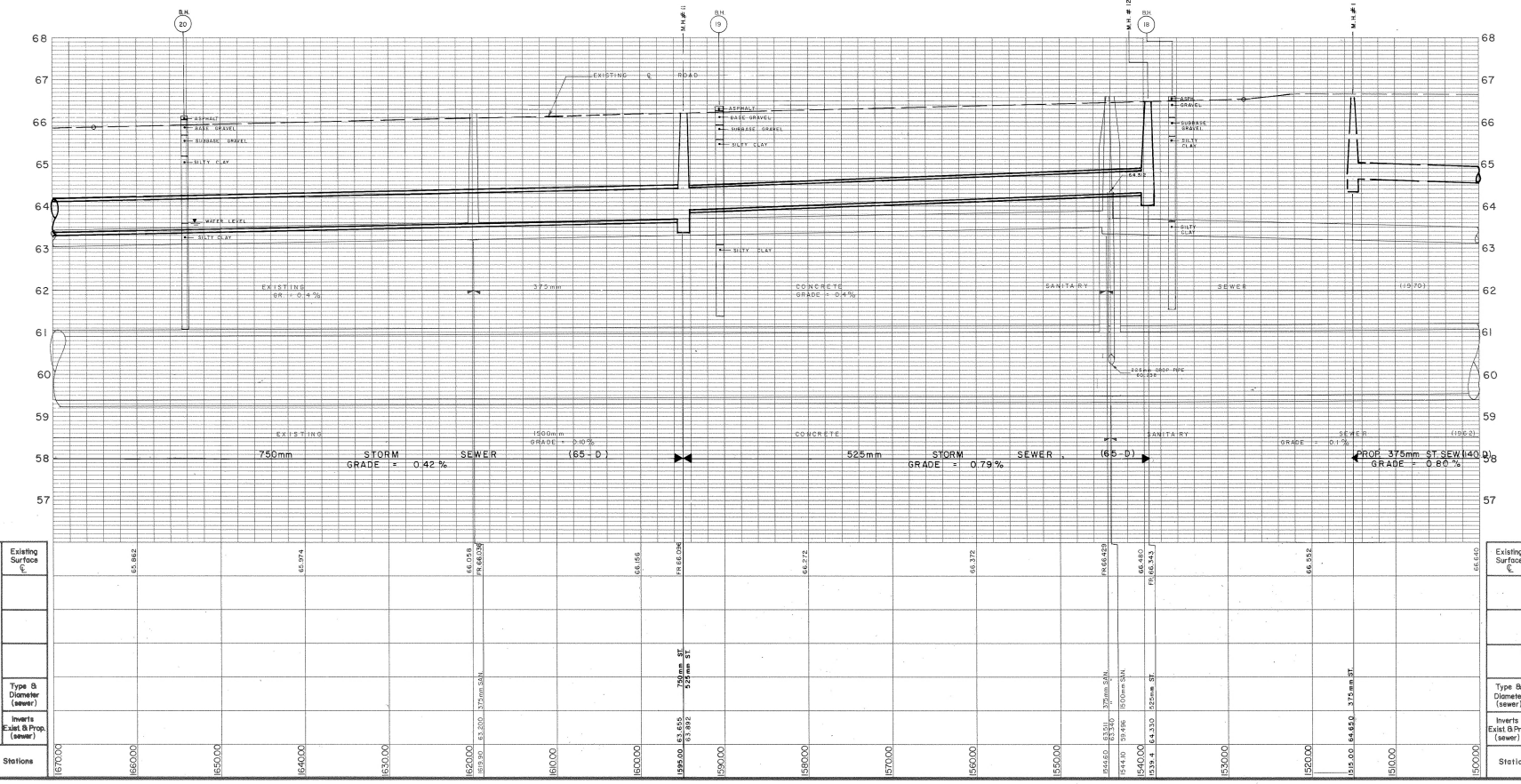
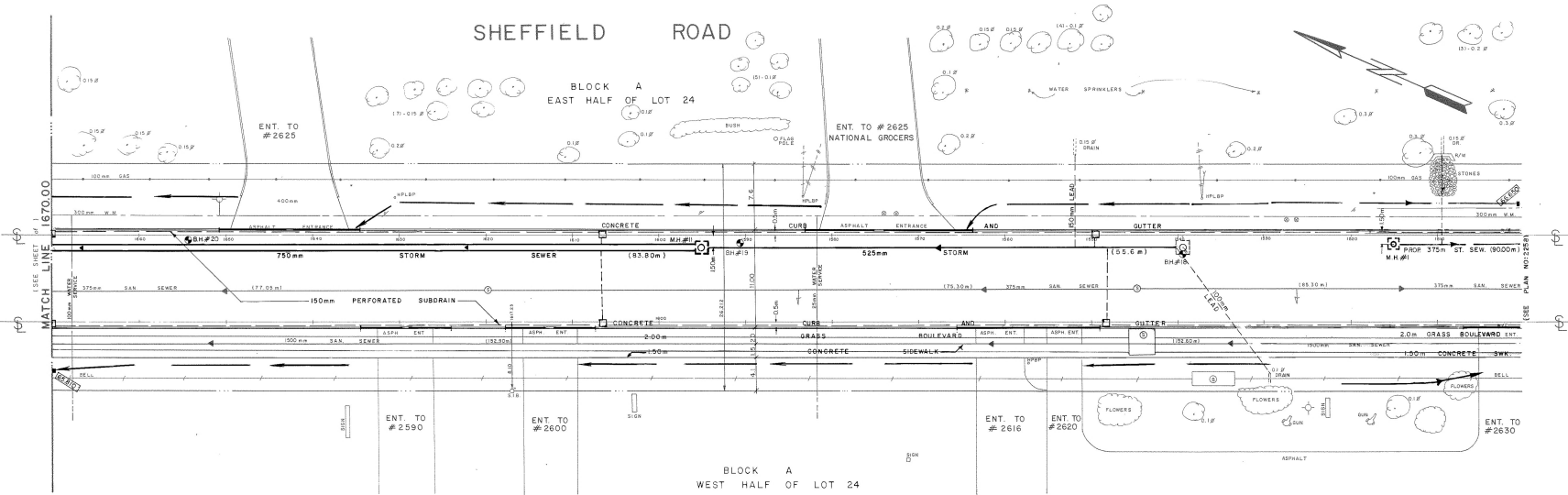
Sincerely,  
**AECOM Canada Ltd.**



Kosta Paliouras, P.Eng.  
Senior Water Resources Engineer/Project  
Manager/Group Leader, Water  
[kosta.paliouras@aecom.com](mailto:kosta.paliouras@aecom.com)

# Appendix **D**

**City of Ottawa Existing Drawings**



Revisions:

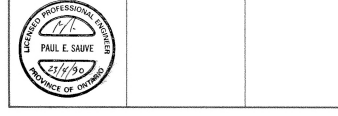
| No. | Date | Description | Drawn By | Appr'd By |
|-----|------|-------------|----------|-----------|
|     |      |             |          |           |

Final Measurements:

|                    |                |               |                  |
|--------------------|----------------|---------------|------------------|
| Construction Type  | SEWER AND ROAD | Inspector     | S. SAUVE         |
| Work Commenced     | JUNE 25, 1990  | Instrumentman | J. PINNEY        |
| Work Completed     | NOV. 16, 1990  | Field Book #  | 8226, 8228, 8227 |
| Contractor         | DISBLEE        | Date          | MARCH/1991       |
| Drafting Revisions | J. PINNEY      | Checked By    |                  |

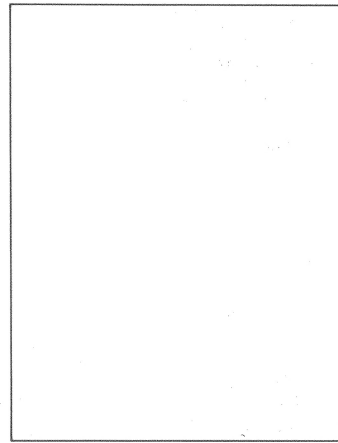
|                  |  |      |  |                     |  |
|------------------|--|------|--|---------------------|--|
| Designed By      |  | Date |  | Structural Check By |  |
| Survey Detail By |  |      |  | Checked By          |  |
| Drafting By      |  |      |  | Checked By          |  |

Chief: *Paul E. Sauve* Senior Const. Coord.



Notes:

- Utilities shown are taken from best available records. Contractor is requested to check with all utility companies before digging.
- Soil information shown is not guaranteed and contractors are advised to collect additional soils information as deemed necessary.
- Reference bench mark:
  - Proposed storm and sanitary sewers may be constructed in a common trench provided that a minimum horizontal distance of 450mm is maintained between outside barrels of pipe.
  - All pipes shall conform to the Canadian Standards Association (C.S.A.), A257.2 reinforced concrete sewer pipe with approved rubber gaskets.
  - A minimum of 460mm vertical clearance to be maintained between sewers and watermains where practical.
- Borehole soil descriptions are not based on sieve analysis but on visual inspection only, except where otherwise noted.
- Soil information taken from:
  - Date of television inspection:
    - This plan supersedes (in whole or in part) plan no.
      - Actual rock line recorded during construction of existing sewer.
      - Registered plan no.
- Caution, while illustrations and utilities shown are taken from best available information, they cannot be guaranteed.
- See additional notes on sheet #1

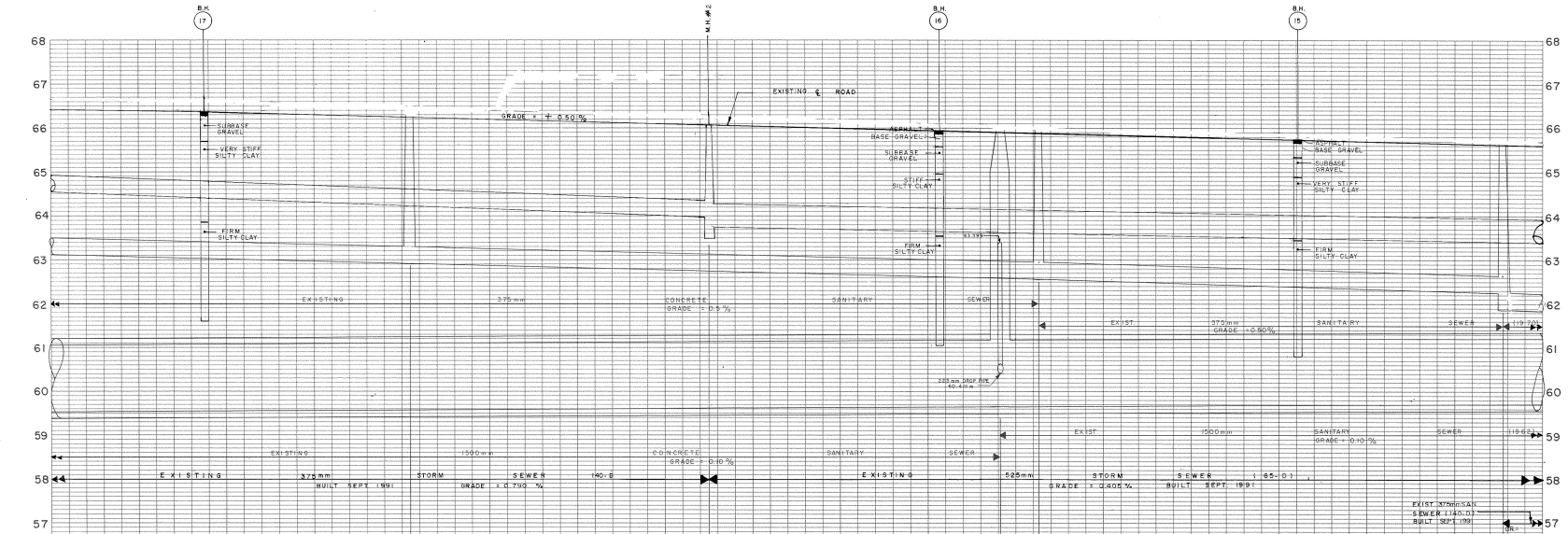
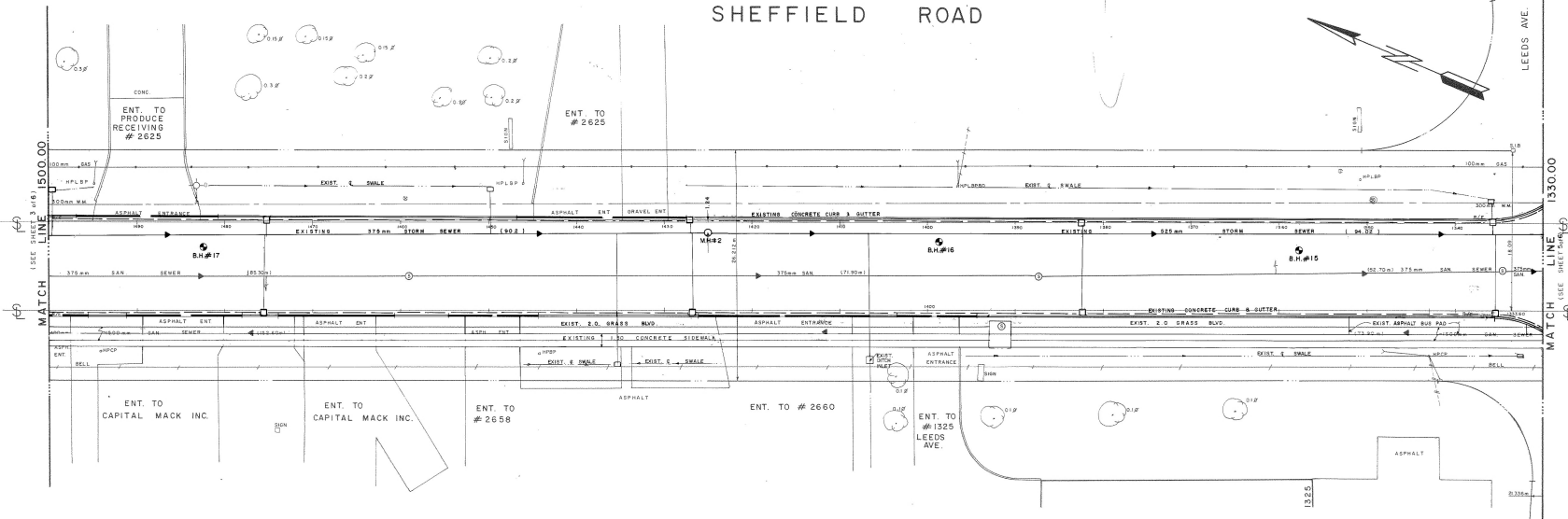


**City of Ottawa**

Department of Engineering And Works  
Engineering Branch  
Design And Construction Division  
800 SCOTT STREET - OTTAWA ONTARIO K1Y 4N7

|                                     |                  |                  |                              |
|-------------------------------------|------------------|------------------|------------------------------|
| Commissioner:                       | D. Curry P. Eng. | Branch Director: | W.R. Cole P. Eng.            |
| STORM SEWER AND ROAD RECONSTRUCTION |                  |                  |                              |
| <b>SHEFFIELD ROAD</b>               |                  |                  |                              |
| FROM CH: 1500.00 TO CH: 1670.00     |                  |                  |                              |
| Contract No.:                       | 90-25            | Survey Book:     | 4706, 4761, 4869, 4879, 4886 |
| Sheet:                              | 10 of 10         | Scale:           | HOR. 1:250<br>VERT. 1:50     |

SHEFFIELD ROAD



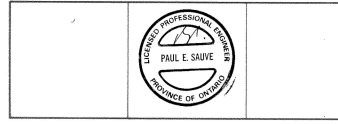
| Stations | Existing Surface Elevation | Type & Diameter (sewer) | Inverts (Exist & Prop. Sewer) | Existing Surface Elevation |
|----------|----------------------------|-------------------------|-------------------------------|----------------------------|
| 15000.00 | 66.415                     |                         |                               | 66.415                     |
| 14500.00 | 66.384                     |                         |                               | 66.384                     |
| 14800.00 | 66.352                     |                         |                               | 66.352                     |
| 14700.00 | 66.274                     |                         |                               | 66.274                     |
| 14500.00 | 66.335                     |                         |                               | 66.335                     |
| 14500.00 | 66.091                     |                         |                               | 66.091                     |
| 14400.00 | 66.044                     |                         |                               | 66.044                     |
| 14300.00 | 66.071                     |                         |                               | 66.071                     |
| 14220.00 | 66.097                     | 375mm ST                | 66.097                        | 66.097                     |
| 14200.00 | 66.044                     |                         |                               | 66.044                     |
| 14100.00 | 66.072                     |                         |                               | 66.072                     |
| 14000.00 | 66.930                     |                         |                               | 66.930                     |
| 13900.00 | 66.897                     |                         |                               | 66.897                     |
| 13820.00 | 66.944                     | 375mm ST                | 66.944                        | 66.944                     |
| 13800.00 | 66.932                     |                         |                               | 66.932                     |
| 13700.00 | 66.890                     |                         |                               | 66.890                     |
| 13600.00 | 66.748                     |                         |                               | 66.748                     |
| 13500.00 | 66.673                     |                         |                               | 66.673                     |
| 13400.00 | 66.631                     |                         |                               | 66.631                     |
| 13340.00 | 66.600                     |                         |                               | 66.600                     |
| 13300.00 | 66.575                     |                         |                               | 66.575                     |

Revisions:

| No. | Date | Description | Drawn By | Appr'd By |
|-----|------|-------------|----------|-----------|
|     |      |             |          |           |

Final Measurements:

| Construction Type | Storm & San Sewer                | Inspector               | Rick Lester  | Bill Corde |
|-------------------|----------------------------------|-------------------------|--------------|------------|
| Work Commenced    | May 1991                         | Instrumentation         | John France  |            |
| Work Completed    | Sept 1991                        | Field Book #            | 5327         | 5328       |
| Contractor        | Bracewell Construction Ltd. C.P. | Scale                   | Sept 30 1991 |            |
| Drafting Revision | Drawn By: Doug McEwen            | Checked By: [Signature] |              |            |



Notes:

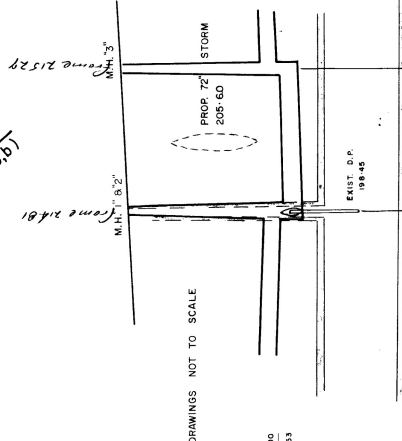
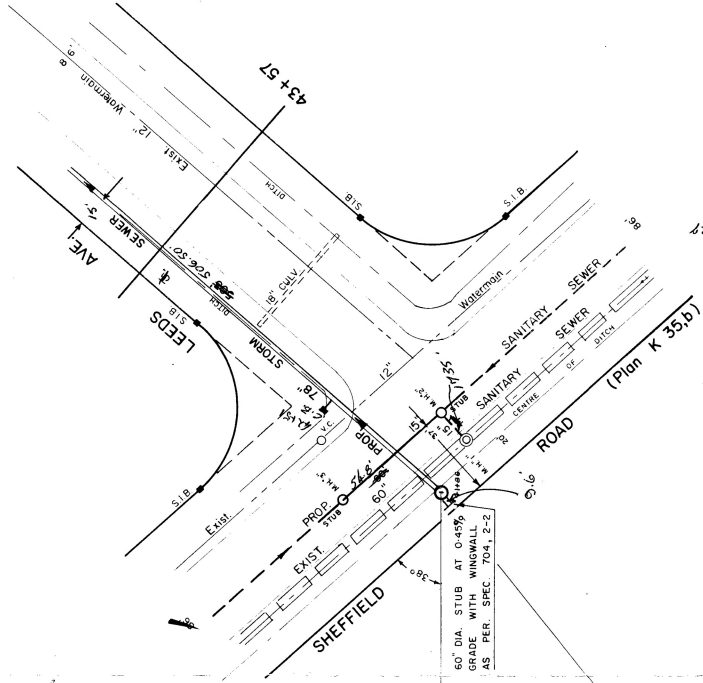
- Utilities shown are taken from best available records. Contractor is requested to check with all utility companies before digging.
- Soil information shown is not guaranteed and contractors are advised to collect additional soils information as deemed necessary.
- Reference bench mark: Proposed storm and sanitary sewers may be constructed in a common trench provided that a minimum horizontal distance of 400mm is maintained between outside barrels of pipe.
- All pipes shall conform to the Canadian Standards Association (C.S.A.), A2572 reinforced concrete sewer pipe with approved rubber gaskets.
- A minimum of 450mm vertical clearance to be maintained between sewers and watermain where practical.
- Borehole soil descriptions are not based on sieve analysis but on visual inspection only, except where otherwise noted.
- Soil information taken from:
  - Date of television inspection: [Blank]
  - This plan supercedes (in whole or in part) plan no: [Blank]
  - Actual rock line recorded during construction of existing sewer: [Blank]
  - Registered plan no: [Blank]
- Caution, while illustrations and utilities shown are taken from best available information, they cannot be guaranteed.
- See additional notes on sheet # 1.
- When reduced, the scale of this drawing is approximately 1:400 horizontally and 1:81 vertically. Do not scale this plan.

City of Ottawa  
 Department Of Engineering And Works  
 Engineering Branch  
 Design And Construction Division  
 1600 SCOTT STREET - OTTAWA, ONTARIO - K1V 4N7

Commissioner: D. Curry P. Eng.      Branch Director: W.R. Cole P. Eng.

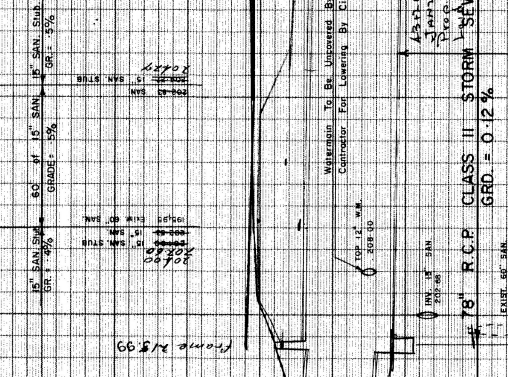
**SHEFFIELD ROAD**

Contract No.: 91-38      Survey Book: 4706, 4761, 4869, 4879, 4886      Scale: HOR. 1:250 VERT. 1:50      Plan No.: 2459      Sheet 4 of 6



NOTE  
 ALL SANITARY SEWERS TO BE  
 EXTRA STR. CONC. PIPE ASTM  
 C-14-61 WITH APPR. RUBBER GASKETS

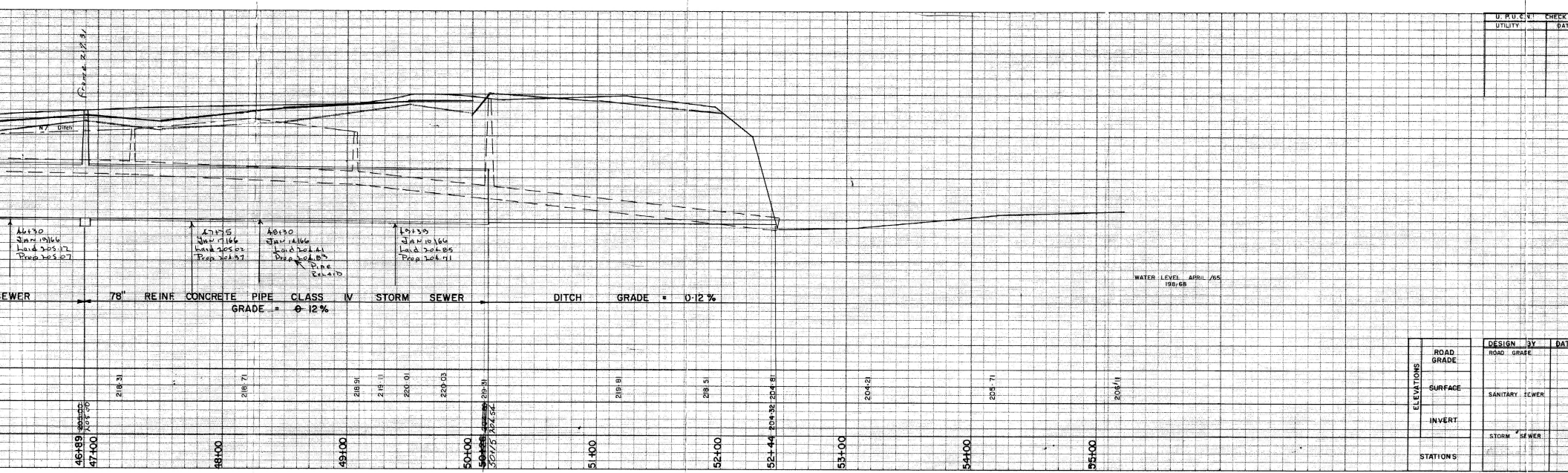
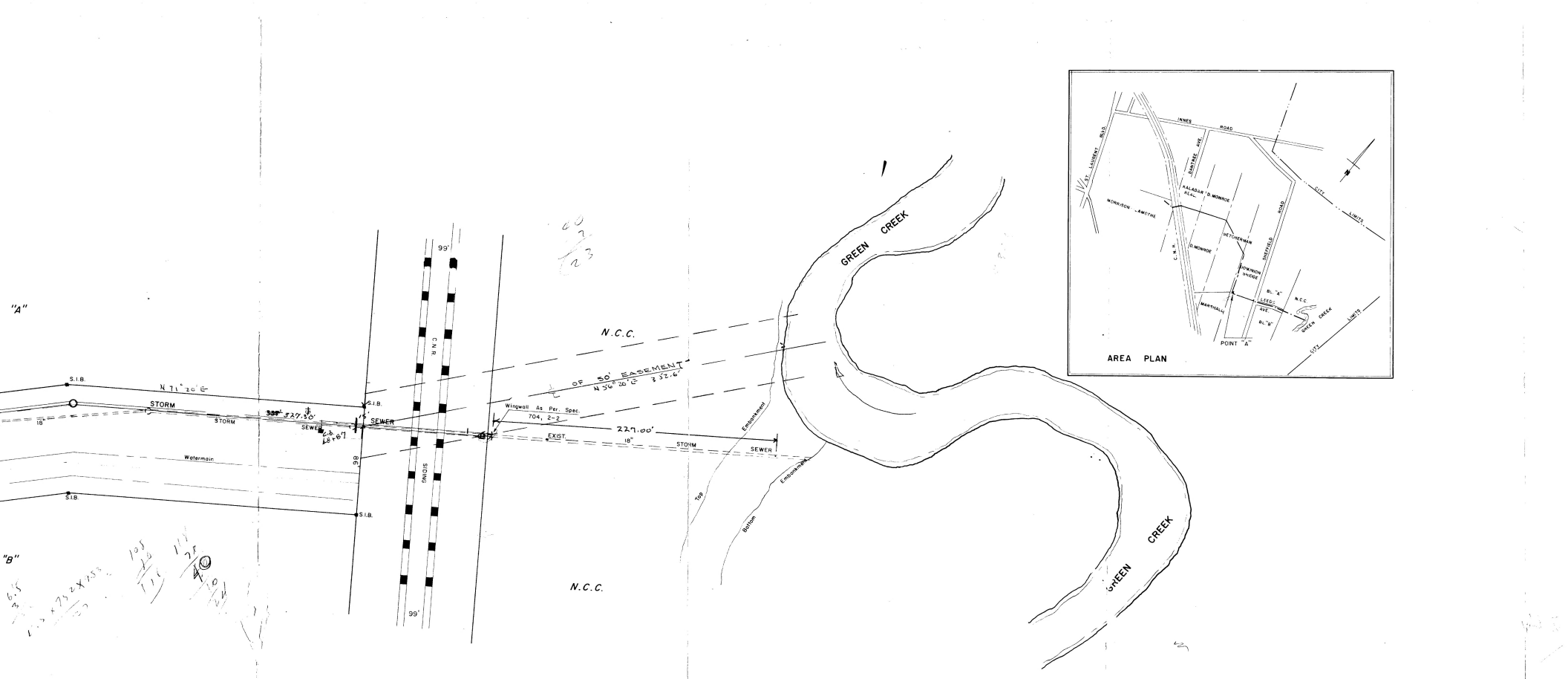
|     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|
| 235 | 230 | 225 | 220 | 215 | 210 | 205 | 200 |
|-----|-----|-----|-----|-----|-----|-----|-----|



|       |        |        |        |        |        |
|-------|--------|--------|--------|--------|--------|
| 43+57 | 43+00  | 42+00  | 41+00  | 40+00  | 39+00  |
| 215.5 | 215.41 | 215.34 | 215.25 | 215.16 | 215.07 |

0.20%  
 SOLID GRADE

54  
 12  
 72



| U. P. U. C. V | CHECK |
|---------------|-------|
| UTILITY       | DATE  |

WATER LEVEL APRIL /65  
190.68

| ELEVATIONS | ROAD GRADE     | DESIGN BY  | DATE |
|------------|----------------|------------|------|
|            | SURFACE        | ROAD GRADE |      |
| INVERT     | SANITARY SEWER |            |      |
|            | STORM SEWER    |            |      |
| STATIONS   |                |            |      |

THIS DESIGN IS THE PROPERTY OF  
ENGINEERING FIRM  
1111 N. W. 11th St.  
MIAMI, FLORIDA 33136

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MIAMI, FLORIDA 33136

50+15  
227  
52+42

200

# Appendix **E**

## Design Drawings





## Domestic Water and Sanitary Load Calculation Chart

|                        |                    |
|------------------------|--------------------|
| <b>Project Name:</b>   | <b>DYT3</b>        |
| <b>Project Number:</b> | <b>60634622</b>    |
| <b>Date:</b>           | <b>14-Sep-2022</b> |

**References**

FUs: OBC 2012 Tables 7.4.9.3., 7.6.3.2.A, B, C and D  
 FUs to gpm for drains: OBC 2012 Tables 7.4.10.5 and A.7.4.10.5  
 Horizontal sanitary sizing: OBC 2012 7.4.10.8

|                          |                        |
|--------------------------|------------------------|
| <b>Number of floors</b>  | <b>1</b>               |
| <b>Basement (Yes/No)</b> | <b>No</b>              |
| <b>Building type</b>     | <b>Office Building</b> |

| DOMESTIC WATER & SANITARY LOAD CALCULATION CHART      |                              |                              |                             |           |            |                    |                      |                   |                      |             |             |            |
|---|------------------------------|------------------------------|-----------------------------|-----------|------------|--------------------|----------------------|-------------------|----------------------|-------------|-------------|------------|
| FIXTURE   | SUPPLY / OUTLET              | No of<br>FIXTURES<br>PRIVATE | No of<br>FIXTURES<br>PUBLIC | TOTAL     | SANITARY   |                    | PUBLIC USE           |                   |                      |             |             |            |
|   |                              |                              |                             |           | F.U.       | TOTAL              | COLD                 |                   | HOT                  |             | TOTAL       |            |
|   |                              |                              |                             |           |            |                    | F.U.                 | TOTAL             | F.U.                 | TOTAL       | F.U.        | TOTAL      |
| Bathroom group with 6 LPF flush tank (max 3 fixtures) | N/A                          |                              |                             | 0         | 6          | 0                  | -                    | -                 | -                    | -           | -           | -          |
| Bathtub, regular                                      | 1/2" H&CW / 1.5"             |                              |                             | 0         | 1.5        | 0                  | 3                    | 0                 | 3                    | 0           | 4           | 0          |
| Bathtub with 3/4" spout                               | 3/4" H&CW / 1.5"             |                              |                             | 0         | 1.5        | 0                  | 7.5                  | 0                 | 7.5                  | 0           | 10          | 0          |
| Clothes washer, 3.5 kg                                | 1/2" H&CW / 2"               |                              |                             | 0         | 1.5        | 0                  | 2.25                 | 0                 | 2.25                 | 0           | 3           | 0          |
| Clothes washer, 6.8 kg                                | 1/2" H&CW / 2"               |                              |                             | 0         | 2          | 0                  | 3                    | 0                 | 3                    | 0           | 4           | 0          |
| Clothes washer, commercial                            | manufact.                    |                              |                             | 0         | 3          | 0                  | 0                    | 0                 | 0                    | 0           | 0           | 0          |
| Dishwasher, commercial                                | manufact. / 2"               |                              |                             | 0         | 3          | 0                  | 0                    | 0                 | 0                    | 0           | 0           | 0          |
| Dishwasher, domestic                                  | 1/2" HW / 1.5"               |                              |                             | 0         | 1          | 0                  | -                    | -                 | -                    | -           | -           | -          |
| <b>Drinking fountain</b>                              | <b>1/2" CW / 1.25"</b>       |                              | <b>14</b>                   | <b>14</b> | <b>2</b>   | <b>28</b>          | <b>0.25</b>          | <b>3.5</b>        | -                    | -           | <b>0.25</b> | <b>3.5</b> |
| <b>Floor drain</b>                                    | <b>- / 3"</b>                |                              | <b>16</b>                   | <b>16</b> | <b>3</b>   | <b>48</b>          | -                    | -                 | -                    | -           | -           | -          |
| <b>Hose bib</b>                                       | <b>1/2" CW / -</b>           |                              | <b>4</b>                    | <b>4</b>  | -          | -                  | <b>2.5</b>           | <b>10</b>         | -                    | -           | <b>2.5</b>  | <b>10</b>  |
| Hose bib  | 3/4" CW / -                  |                              |                             | 0         | -          | -                  | 6                    | 0                 | -                    | -           | 6           | 0          |
| Hose bib, combination                                 | 1/2" H&CW / -                |                              |                             | 0         | -          | -                  | 1.9                  | 0                 | 1.9                  | 0           | 2.5         | 0          |
| <b>Lavatory, 8.3 L/min or less</b>                    | <b>1/2" H&amp;CW / 1.25"</b> |                              | <b>13</b>                   | <b>13</b> | <b>1</b>   | <b>13</b>          | <b>1.5</b>           | <b>19.5</b>       | <b>1.5</b>           | <b>19.5</b> | <b>2</b>    | <b>26</b>  |
| Shower head, 9.5 L/min or less                        | 1/2" H&CW / 1.5"             |                              |                             | 0         | 1.5        | 0                  | 3                    | 0                 | 3                    | 0           | 4           | 0          |
| Shower, multi-head, FU per head                       | manufact. / 2"               |                              |                             | 0         | 3          | 0                  | 3                    | 0                 | 3                    | 0           | 4           | 0          |
| Sink, bar   | 1/2" H&CW / 1.5"             |                              |                             | 0         | 1.5        | 0                  | 1.5                  | 0                 | 1.5                  | 0           | 2           | 0          |
| <b>Sink, kitchen, commercial, per faucet</b>          | <b>1/2" H&amp;CW / 2"</b>    |                              | <b>1</b>                    | <b>1</b>  | <b>2</b>   | <b>2</b>           | <b>3</b>             | <b>3</b>          | <b>3</b>             | <b>3</b>    | <b>4</b>    | <b>4</b>   |
| <b>Sink, kitchen, domestic, 8.3 L/min or less</b>     | <b>1/2" H&amp;CW / 1.5"</b>  |                              | <b>2</b>                    | <b>2</b>  | <b>1.5</b> | <b>3</b>           | <b>1</b>             | <b>2</b>          | <b>1</b>             | <b>2</b>    | <b>1.4</b>  | <b>2.8</b> |
| Sink, laundry   | 1/2" H&CW / 1.5"             |                              |                             | 0         | 1.5        | 0                  | 1                    | 0                 | 1                    | 0           | 1.4         | 0          |
| <b>Sink, mop (janitor's)</b>                          | <b>1/2" H&amp;CW / 3"</b>    |                              | <b>2</b>                    | <b>2</b>  | <b>3</b>   | <b>6</b>           | <b>2.25</b>          | <b>4.5</b>        | <b>2.25</b>          | <b>4.5</b>  | <b>3</b>    | <b>6</b>   |
| <b>Urinal, flush valve</b>                            | <b>3/4" CW / 2"</b>          |                              | <b>3</b>                    | <b>3</b>  | <b>4</b>   | <b>12</b>          | <b>N/A</b>           | <b>45</b>         | -                    | -           | <b>N/A</b>  | <b>45</b>  |
| Urinal, flush tank                                    | 1/2" CW / 1.5"               |                              |                             | 0         | 1.5        | 0                  | 3                    | 0                 | -                    | -           | 3           | 0          |
| WC, 6 LPF or less, tank                               | 1/2" CW / 3"                 |                              |                             | 0         | 4          | 0                  | 2.2                  | 0                 | -                    | -           | 2.2         | 0          |
| <b>WC, flush valve</b>                                | <b>1" CW / 3"</b>            |                              | <b>12</b>                   | <b>12</b> | <b>6</b>   | <b>72</b>          | <b>N/A</b>           | <b>185</b>        | -                    | -           | <b>N/A</b>  | <b>185</b> |
| Penal Fixture   | 1" CW / 3"                   |                              |                             | 0         | 6          | 0                  | N/A                  | 0                 | -                    | -           | N/A         | 0          |
| Reserve for MHE-Sanitary only                         |                              |                              | 1                           | 1         | 5          | 5                  |                      | 0                 |                      | 0           |             | 0          |
| Reserve for Landscape and MHE-Plumbing only           |                              |                              | 1                           | 1         |            | 0                  | 75                   | 75                | 10                   | 10          | 85          | 85         |
|   |                              |                              |                             | <b>69</b> | <b>69</b>  | <b>Total = 189</b> | <b>Total = 347.5</b> | <b>Total = 39</b> | <b>Total = 367.3</b> |             |             |            |

| SANITARY  |   |                |                 |                     |   |    |         |
|---|---|----------------|-----------------|---------------------|---|----|---------|
| Plumbing System Sanitary Load                             | = | 189 FUs        | = 69 gpm        | Main Drain Size     | = | 6" | per OBC |
| Other Sanitary Load (pool drain, cooling tower, sump pit) | = |                | = [ ] gpm       | Building Sewer Size | = | 6" | per OBC |
| <b>Building Sanitary Load</b>                             | = | <b>189 FUs</b> | = <b>69 gpm</b> |                     |   |    |         |

| DOMESTIC COLD AND HOT WATER  |   |                |                     |                      |   |    |         |
|------------------------------|---|----------------|---------------------|----------------------|---|----|---------|
| Total Cold Water             | = | 348 FUs        | = 119.08 gpm        | Dom. Cold Water Pipe | = | 3" | per OBC |
| Total Hot Water              | = | 39 FUs         | = 40.8 gpm          | Dom. Hot Water Pipe  | = | 2" | per OBC |
| <b>System Domestic Water</b> | = | <b>367 FUs</b> | = <b>121.94 gpm</b> | Main Cold Water Pipe | = | 3" | per OBC |

## City of Ottawa Water Demands



Project: 2625 Sheffield Road-DYT3-Ottawa  
 Project No.: 60648725  
 Designed By: German Verbel  
 Checked By: \_\_\_\_\_  
 Date: 9/27/2022  
 Ste Area (ha): 7.06

### Average Daily Demand

| Demand Type                  | Amount      | Units           |
|------------------------------|-------------|-----------------|
| Residential                  | 350         | L/c/d           |
| Industrial - Light           | 35,000      | L/gross ha/d    |
| Industrial - Heavy           | 55,000      | L/gross ha/d    |
| Commercial and Institutional |             |                 |
| Shopping Centres             | 2500        | L/(1000m2/d)    |
| Hospitals                    | 900         | L/(bed/day)     |
| Schools                      | 70          | L/(Student/d)   |
| Trailer Parks no Hook-Ups    | 340         | L/(space/d)     |
| Trailer Parks with Hook-Ups  | 800         | L/(space/d)     |
| Campgrounds                  | 225         | L/(campsite/d)  |
| Mobile Home Parks            | 1000        | L/(Space/d)     |
| Motels                       | 150         | L/(bed-space/d) |
| Hotels                       | 225         | L/(bed-space/d) |
| Tourist Commercial           | 28,000      | L/gross ha/d    |
| Other Commercial             | 28,000      | L/gross ha/d    |
| <b>Average Daily Demand</b>  | <b>2.86</b> | <b>L/s</b>      |

### Maximum Daily Demand

|                             |                |              |
|-----------------------------|----------------|--------------|
| Residential                 | 2.5 x avg. day | L/c/d        |
| Industrial                  | 1.5 x avg. day | L/gross ha/d |
| Commercial                  | 1.5 x avg. day | L/gross ha/d |
| Institutional               | 1.5 x avg. day | L/gross ha/d |
| <b>Maximum Daily Demand</b> | <b>4.29</b>    | <b>L/s</b>   |

### Maximum Hour Demand

|                             |                |              |
|-----------------------------|----------------|--------------|
| Residential                 | 2.2 x max. day | L/c/d        |
| Industrial                  | 1.8 x max. day | L/gross ha/d |
| Commercial                  | 1.8 x max. day | L/gross ha/d |
| Institutional               | 1.8 x max. day | L/gross ha/d |
| <b>Maximum Daily Demand</b> | <b>7.72</b>    | <b>L/s</b>   |

Ottawa Design Guidelines - Water Distribution First Edition, July 2010 - WDG001  
 Technical Bulletin ISD-2010-2

**Fire Flow Calculations**  
1999 Fire Underwriters Survey (FUS) Method



Project: DYT3 2625 Sheffield Road Ottawa, Ontario  
Project #: 60648725

Calculated by: GV  
Date: 23-Sep-22

Checked by: KS  
Date: 23-Sep-22

**Building A**

**Fire Flow Formula**  $F = 220 \cdot C \cdot \sqrt{A}$

**A) C = Structure Coefficient**

- 1.5 Wood Frame Construction - Essentially all combustible (Max Value of C)
- 1.0 Ordinary Construction - Brick/Masonry Walls, Combustible Floor & Interior
- 0.8 Non-Combustible - Unprotected metal structural, masonry, or metal walls
- 0.6 Fire Resistive Construction - Fully protected frame, floors, roof (Min Value of C)

C =

**B) A = Floor Area**

**C) # Floors (excl. basement)**

Includes all storeys, but exclude basements >50% below grade.

For fire-resistive buildings with unprotected vertical openings: add two largest adjoining floors plus 50% of any floors immediately above/below them up to to 8  
For fire-resistive buildings with protected vertical openings (1hr rating): add largest floors plus 25% of each adjoining floor area

A =  m<sup>2</sup>

**D)**

F =  (L/min)  
Rounded =  (L/min)

**Occupancy Reduction/Surcharge**

**E) Type of occupancy/contents**

- Non-Combustible
- Free Burning
- Limited Combustible
- Rapid Burning
- Combustible

Fire hazard adjustment =   
Adjustment =  (L/min)  
F<sub>adj</sub> =  (L/min)

Generally Low-Hazard Occupancy is Non-/Limited Combustible (National Building Group A, B, C, D)  
Generally High-Hazard Occupancy is Free/Rapid Burning (National Building Group F, Division 1 & 2)

**F) Sprinkler System Reduction**

Revised F may be reduced up to:

- 50% for a complete automatic sprinkler system (incl. water flow/control valve alarm system)
- 30% for a sprinkler system conforming to NFPA Code 13
- Add'l credit up to 10% can be applied if water supply is standard for both the sprinkler system and fire dept hose lines

Reduction =   
Reduction =  (L/min)

**G) Exposure Surcharge**

Sum of all exposures must be less than 75%

If building face is unpierced party wall (min. 2hr rating), choose "Fire Wall"

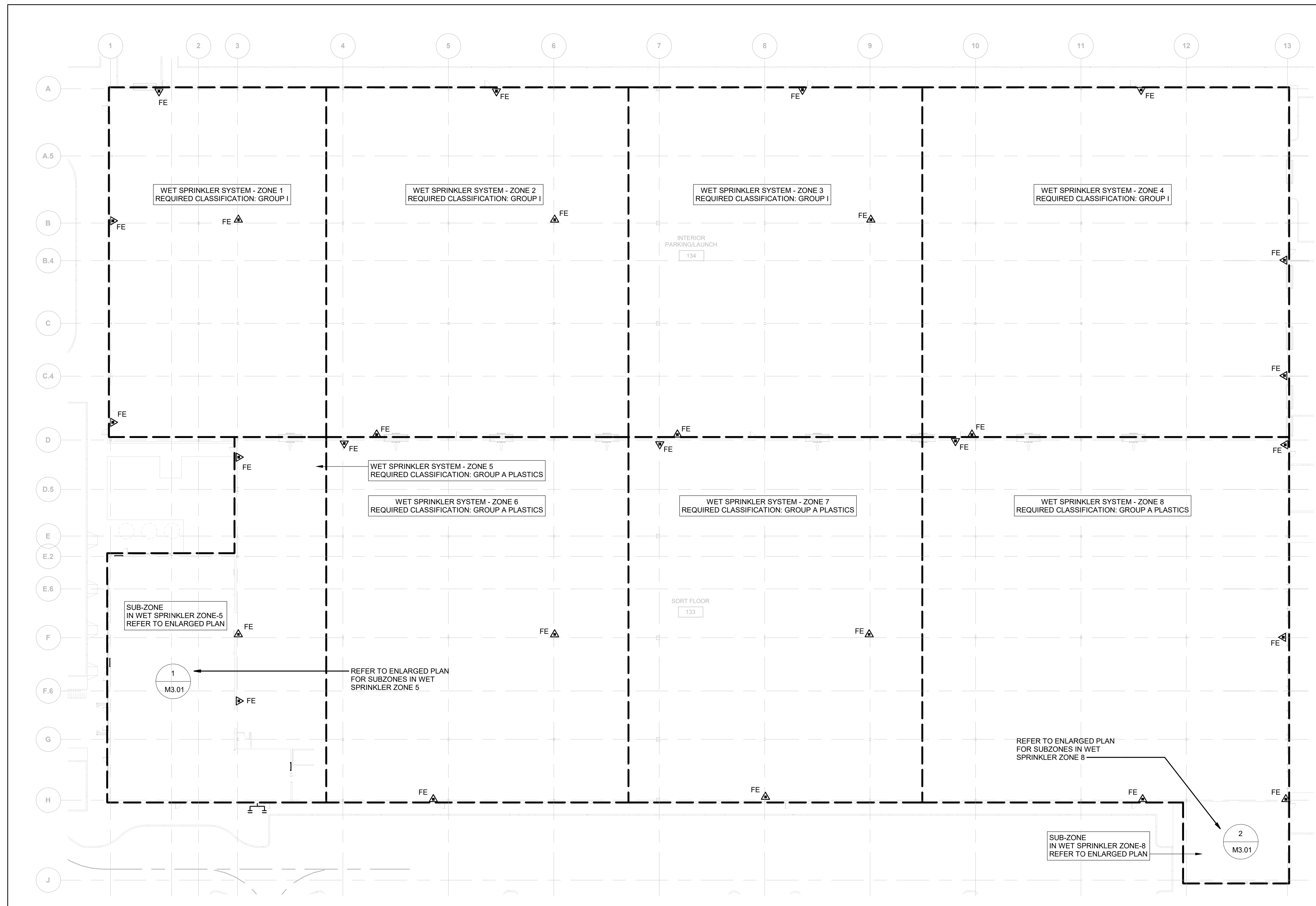
Distance to nearest building (m) % addition

|                        |      |                  |
|------------------------|------|------------------|
| North                  | >45m | 0%               |
| East                   | >45m | 0%               |
| South                  | >45m | 0%               |
| West                   | >45m | 0%               |
| <b>Surcharge %</b>     |      | <b>0%</b>        |
| <b>Surcharge Add'n</b> |      | <b>0</b> (L/min) |

**H) Total Fire Flow**

Minimum 2000L/min; Max 40 000L/min (rounded to nearest 1000L/min)

=  L/min  
=  L/sec



1 GROUND FLOOR - FIRE PROTECTION  
 M3.00 1 : 350

| SPRINKLER HAZARD CLASSIFICATIONS |                     |                     |                                  |
|----------------------------------|---------------------|---------------------|----------------------------------|
| OCCUPANCY                        | MAX PROTECTION AREA | DESIGN DENSITY      | MINIMUM PRESSURE REQUIREMENT     |
| LIGHT HAZARD                     | 20 m <sup>2</sup>   | 4.1 mm/min          | 15 PSI                           |
| ORDINARY HAZARD GROUP 1          | 12 m <sup>2</sup>   | 6.1 mm/min          | 20 PSI                           |
| ORDINARY HAZARD GROUP 2          | 12 m <sup>2</sup>   | 8.1 mm/min          | 20 PSI                           |
| OCCUPANCY                        | K FACTOR            | MAX PROTECTION AREA | NO. OF SPRINKLERS IN DESIGN AREA |
| GROUP A PLASTICS                 | 25.2                | 9 m <sup>2</sup>    | 12                               |

| WEIGHT OF FULL SPRINKLER MAINS |              |
|--------------------------------|--------------|
| SIZE OF SPRINKLER MAIN         | WEIGHT       |
|                                | kg/m lbs/ft. |
| 150 mm (6 in.)                 | 35 23        |
| 200 mm (8 in.)                 | 60 40        |
| 250 mm (10 in.)                | 83 56        |

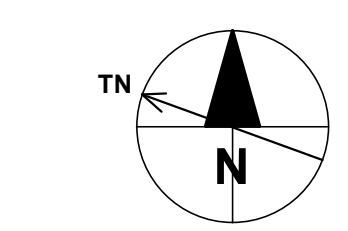
GENERAL FIRE PROTECTION SYSTEM NOTES:

- FIRE PROTECTION CONTRACTOR SHALL PROVIDE DRAWINGS AND HYDRAULIC CALCULATIONS SIGNED AND SEALED BY A PROFESSIONAL ENGINEER.
- THE SPRINKLER LAYOUTS SHALL INCLUDE ALL PIPING AND SPRINKLERS NECESSARY TO SUIT THE ARCHITECTURAL CEILING PLANS. PROPOSED LAYOUTS SHALL BE PROVIDED AS SHOP DRAWINGS FOR REVIEW PRIOR TO INSTALLATION.
- INSTALL AUTOMATIC SPRINKLERS BELOW OBSTRUCTIONS 600 mm WIDE AND LARGER SUCH AS DUCTS, DECKS, OPEN GRATE FLOORING, CUTTING TABLES, AND OVERHEAD DOORS IN ACCORDANCE WITH NFPA 13. REFER TO STANDARD DETAILS FOR MORE OBSTRUCTION REQUIREMENTS AND CLEARANCES OF ESFR SPRINKLERS. COORDINATE WITH ALL OTHER TRADES PRIOR TO SYSTEM INSTALLATION.
- OFFSET SPRINKLER PIPING AWAY FROM VERTICAL OBSTRUCTIONS SUCH AS VERTICAL DUCTWORK AND COLUMNS IN ACCORDANCE WITH NFPA 13. SPRINKLERS SHOULD BE KEPT 30mm AWAY FROM VERTICAL OBSTRUCTIONS UP TO 300 mm WIDE, 600 mm AWAY FROM VERTICAL OBSTRUCTIONS 300 mm TO 600 mm WIDE, AND ON EITHER SIDE OF THE OBSTRUCTION OR VERTICAL OBSTRUCTIONS LARGER THAN 600 mm WIDE.
- INSTALL AUTOMATIC SPRINKLERS TO ACCOMMODATE HVLS FANS IN ACCORDANCE WITH NFPA 13.
- FIRE PROTECTION CONTRACTOR TO PROVIDE VENTS AND DRAINAGE CONNECTION FOR COMMISSIONING AND SERVICING OF THE SYSTEM.
- PROVIDE HIGH TEMPERATURE HEADS WITH GUARDS IN ALL ELECTRICAL, COMMUNICATIONS AND SPRINKLER ROOMS.
- FLOW INDICATION AND PRESSURE SWITCHES ARE SHOWN ON SCHEMATICS FOR CLARITY AND ARE CONSIDERED PART OF A COMPLETE LISTED ALARM CHECK VALVE ASSEMBLY.
- ELEVATED PLATFORMS AND CONVEYERS WIDER THAN 1.2 m (48 in.) SHALL BE PROVIDED WITH SPRINKLER PROTECTION UNDERNEATH. SPRINKLER SHALL BE UPRIGHT OR PENDENT K11.2 QUICK-RESPONSE SPRINKLERS LISTED FOR STORAGE APPLICATIONS. SYSTEMS SHALL BE DESIGNED TO PROTECT EXTRA HAZARD GROUP 2 AND ALL CRITERIA SHALL BE VALIDATED BY THE AUTHORITY HAVING JURISDICTION.
- SPRINKLERS SHALL NOT BE REQUIRED BELOW CONVEYORS THAT ARE 1.2 m (4 ft.) WIDE OR LESS, ARE OVER PERSONNEL WALKWAYS, WOULD NOT ALLOW FOR COMBUSTIBLE STORAGE UNDERNEATH, AND/OR ARE FLOOR MOUNTED UP TO A HEIGHT OF 900 mm (3 ft.), UNLESS REQUESTED BY THE AUTHORITY HAVING JURISDICTION.
- WHERE SPRINKLERS ARE REQUIRED UNDERNEATH CONVEYORS AND/OR CONVEYOR EQUIPMENT PLATFORMS, PROVIDE HEAD GUARDS FOR THOSE SPRINKLERS.
- AT THE COMPLETION OF THE PROJECT, FIRE PROTECTION CONTRACTOR SHALL ISSUE A LETTER SIGNED AND SEALED BY A PROFESSIONAL ENGINEER CONFIRMING THE INSTALLATION COMPLIES WITH NFPA 13.
- REFER TO ARCHITECTURAL DRAWINGS FOR REFLECTED CEILING PLANS.

**AECOM**  
 PROJECT  
**DYT3 GEN 3.1 BTS,**  
**OTTAWA, ONTARIO**  
**2625 SHEFFIELD ROAD**

CLIENT  
 AECOM Canada Architects Ltd.  
 50 Sportsworld Crossing Road, Suite 290  
 Kitchener, Ontario, N2P 0A4  
 519 650 5313 tel 519 650 3424 fax  
 www.aecom.com

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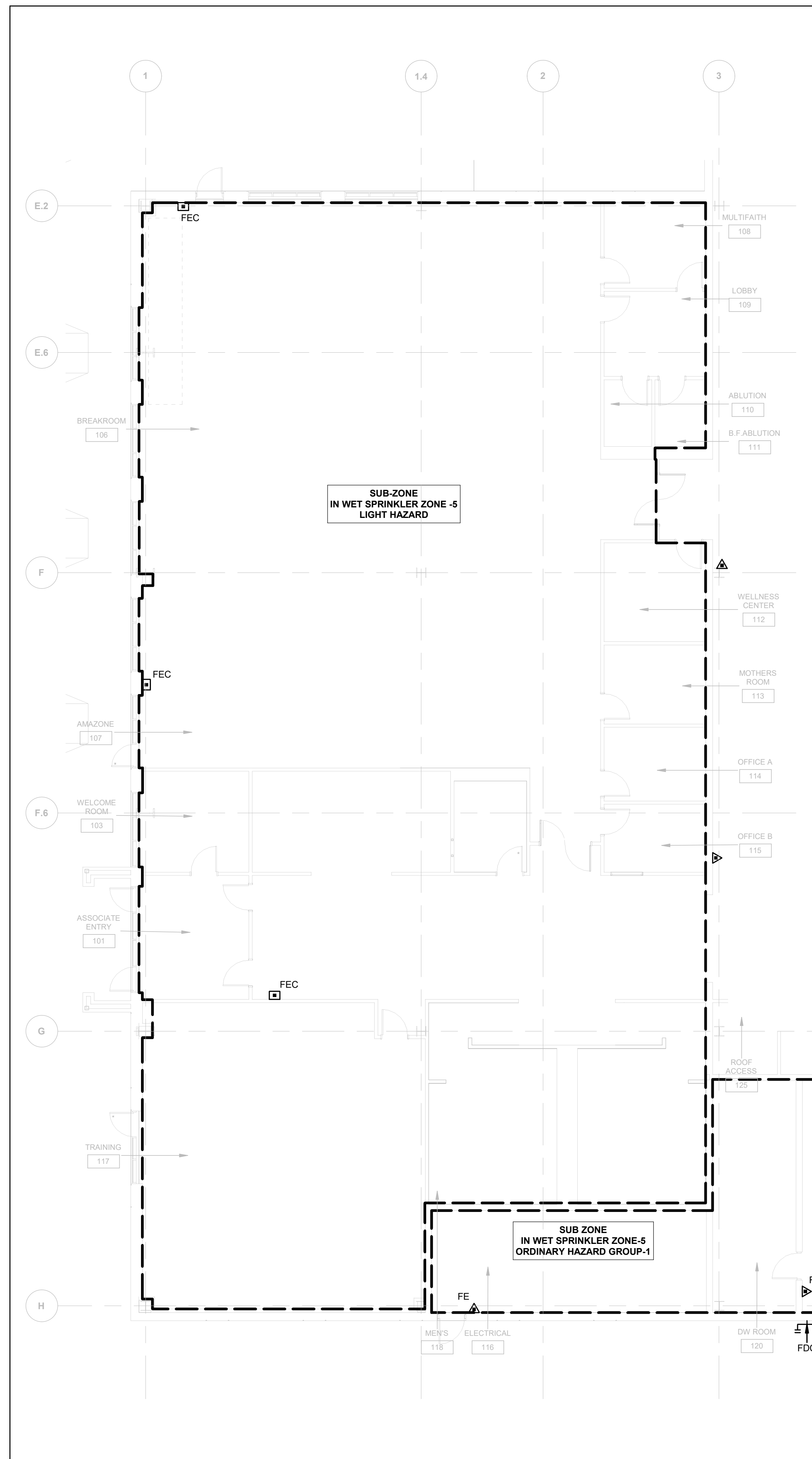


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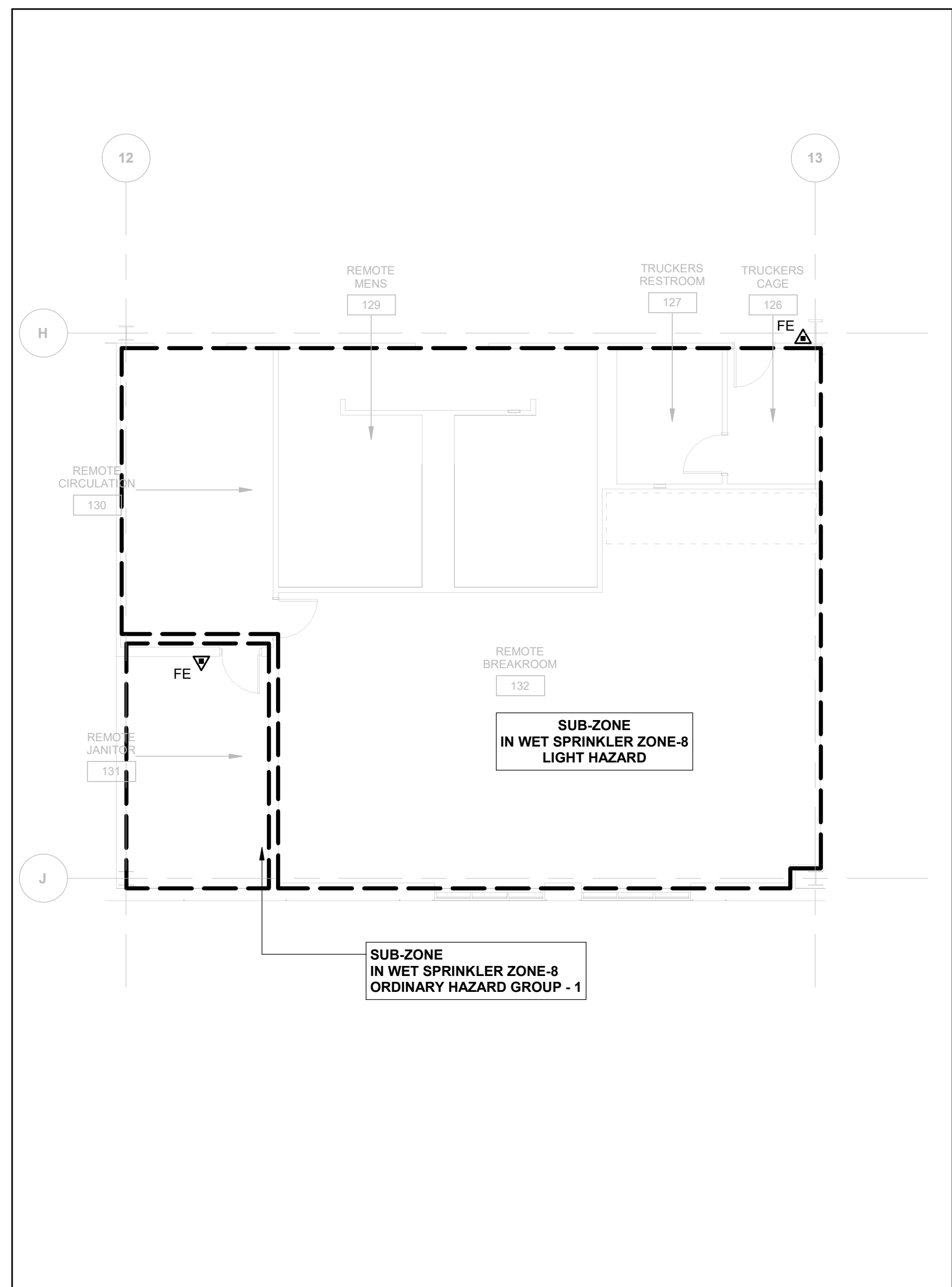
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PROJECT NUMBER  
 00000000  
 SHEET TITLE  
 OVERALL FLOOR PLAN - FIRE PROTECTION  
 SHEET NUMBER  
 M3.00

NOT FOR CONSTRUCTION



1 ENLARGED PLAN - OFFICE BLOCK - FIRE PROTECTION  
 M3.01 1:100



2 ENLARGED PLAN -REMOTE AREA -FIRE PROTECTION  
 M3.01 1:100

GENERAL FIRE PROTECTION SYSTEM NOTES:

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- REFER TO ARCHITECTURAL DRAWINGS FOR REFLECTED CEILING PLANS.

| SPRINKLER HAZARD CLASSIFICATIONS |                     |                     |                                  |
|----------------------------------|---------------------|---------------------|----------------------------------|
| OCCUPANCY                        | MAX PROTECTION AREA | DESIGN DENSITY      | MINIMUM PRESSURE REQUIREMENT     |
| LIGHT HAZARD                     | 20 m <sup>2</sup>   | 4.1 mm/min          | 15 PSI                           |
| ORDINARY HAZARD GROUP 1          | 12 m <sup>2</sup>   | 6.1 mm/min          | 20 PSI                           |
| ORDINARY HAZARD GROUP 2          | 12 m <sup>2</sup>   | 8.1 mm/min          | 20 PSI                           |
| OCCUPANCY                        | K FACTOR            | MAX PROTECTION AREA | NO. OF SPRINKLERS IN DESIGN AREA |
| GROUP A PLASTICS                 | 25.2                | 9 m <sup>2</sup>    | 12                               |

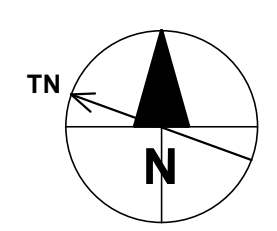
| WEIGHT OF FULL SPRINKLER MAINS |        |         |
|--------------------------------|--------|---------|
| SIZE OF SPRINKLER MAIN         | WEIGHT |         |
|                                | kg/m   | lbs/ft. |
| 150 mm (6 in.)                 | 35     | 23      |
| 200 mm (8 in.)                 | 60     | 40      |
| 250 mm (10 in.)                | 83     | 56      |

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NOT FOR CONSTRUCTION

# Appendix **F**

## **Supporting Engineering Documentation and Calculations – Infiltration Basin Calculations**

**Infiltration Basin Sizing - DYT3**

| Site Conditions  |                             |  |                             |
|--|-----------------------------|--|-----------------------------|
| Rainfall Amount  | 10 mm                       |  |                             |
|  | 0.01 m                      |  |                             |
| <b>Site Areas</b>  |                             |  |                             |
| Total Building Area  | 2 ha                        |  |                             |
|  | 24800 m <sup>2</sup>        |  |                             |
| Area 101 Footprint Area  | 1.36 ha                     |  |                             |
|  | 13600 m <sup>2</sup>        |  |                             |
| Area 102 Footprint Area  | 1.12 ha                     |  |                             |
|  | 11200 m <sup>2</sup>        |  |                             |
| <b>Runoff Coefficient</b>  |                             |  |                             |
| Impervious Area  | 0.9                         |  |                             |
| Area 101   |                             | Area 102   |                             |
| Required Clear Stone Bedding Infiltration Basin Sizing Calculation |                             | Required Clear Stone Bedding Infiltration Basin Sizing Calculation |                             |
| <b>Volume (Total - Building Area)</b>                              | <b>122.40 m<sup>3</sup></b> | <b>Volume (Total - Building Area)</b>                              | <b>100.80 m<sup>3</sup></b> |
| Stone Void Ratio   | 0.4                         | Stone Void Ratio   | 0.4                         |
| Depth  | 0.75 m                      | Depth  | 0.75 m                      |
| Length   | 66.72 m                     | Length   | 165.00 m                    |
| Width  | 6.12 m                      | Width  | 2.04 m                      |
| Proposed Clear Stone Bedding Infiltration Basin Sizing Calculation |                             | Proposed Clear Stone Bedding Infiltration Basin Sizing Calculation |                             |
| <b>Volume (Total - Building Area)</b>                              | <b>132.00 m<sup>3</sup></b> | <b>Volume (Total - Building Area)</b>                              | <b>108.00 m<sup>3</sup></b> |
| Stone Void Ratio   | 0.4                         | Stone Void Ratio   | 0.4                         |
| Depth  | 0.75 m                      | Depth  | 0.75 m                      |
| Length   | 110.00 m                    | Length   | 90.00 m                     |
| Width  | 4.00 m                      | Width  | 4.00 m                      |
| Infiltration Basin Bottom Area (Equation 4.3, MECP 2003)           |                             | Infiltration Basin Bottom Area (Equation 4.3, MECP 2003)           |                             |
| Runoff Volume  | 132.00 m <sup>3</sup>       | Runoff Volume  | 108.00 m <sup>3</sup>       |
| Percolation Rate   | 42 mm/hr                    | Percolation Rate   | 42 mm/hr                    |
| Factor of Safety   | 2.5                         | Factor of Safety   | 2.5                         |
| Porosity   | 0.4                         | Porosity   | 0.4                         |
| Retention Time   | 48 hr                       | Retention Time   | 48 hr                       |
| <b>Bottom Area</b>   | <b>409.23 m<sup>2</sup></b> | <b>Bottom Area</b>   | <b>334.82 m<sup>2</sup></b> |
| <b>Proposed Bottom Area</b>  | <b>440.00 m<sup>2</sup></b> | <b>Proposed Bottom Area</b>  | <b>360.00 m<sup>2</sup></b> |
| Maximum Allowable Basin Depth (Equation 4.2, MECP, 2003)           |                             | Maximum Allowable Basin Depth (Equation 4.2, MECP, 2003)           |                             |
| Percolation Rate   | 42 mm/hr                    | Percolation Rate   | 42 mm/hr                    |
| Factor of Safety   | 2.5                         | Factor of Safety   | 2.5                         |
| Retention Time   | 48 hr                       | Retention Time   | 48 hr                       |
| <b>Maximum Allowable Depth</b>                                     | <b>0.81 m</b>               | <b>Maximum Allowable Depth</b>                                     | <b>0.81 m</b>               |
| <b>Proposed Depth</b>  | <b>0.75 m</b>               | <b>Proposed Depth</b>  | <b>0.75 m</b>               |

# Appendix **G**

**Supporting Engineering Documentation  
and Calculations – Oil/Grit Separator  
and Storm Sewer**





# ADS Treatment Train Sizing

|                             |              |  |
|-----------------------------|--------------|--|
| <b>Project Name:</b>        | DYT3 - North |  |
| <b>Consulting Engineer:</b> | AECOM        |  |
| <b>Location:</b>            | Ottawa, ON   |  |
| <b>Sizing Completed By:</b> | C. Neath     | <b>Email:</b> <a href="mailto:cody.neath@adspipe.com">cody.neath@adspipe.com</a> |

| Summary of Results             |              |
|--------------------------------|--------------|
| Isolator Row PLUS TSS Removal: | 80.6%        |
| FD-4HC TSS Removal:            | 34.0%        |
| <b>Combined TSS Removal:</b>   | <b>87.0%</b> |
| <b>Total Volume Treated:</b>   | <b>99.4%</b> |

| Individual OGS Results |             |                |
|------------------------|-------------|----------------|
| Model                  | TSS Removal | Volume Treated |
| FD-4HC                 | 34.0%       | >90%           |
| FD-5HC                 | 37.0%       | >90%           |
| FD-6HC                 | 39.0%       | >90%           |
| FD-8HC                 | 42.0%       | >90%           |
| FD-10HC                | 44.0%       | >90%           |

| Overall System Capacities           |                     |
|-------------------------------------|---------------------|
| Total Sediment Storage Capacity:    | 6.88 m <sup>3</sup> |
| Oil Storage Capacity:               | 723 L               |
| Max. OGS Pipe Diameter:             | 600 mm              |
| Peak OGS Flow Capacity:             | 510 L/s             |
| Peak Stormtech Inlet Flow Capacity: | 311 L/s             |
| Peak IR PLUS Water Quality Flow:    | 211.1 L/s           |

| OGS Specifications            |          |
|-------------------------------|----------|
| Inlet Pipe Diameter (A):      | 375 mm   |
| Unit Diameter (B):            | 1,200 mm |
| Outlet Pipe Diameter (C):     | 375 mm   |
| Rim Elevation (D):            | 66.74 m  |
| Bottom of Sump Elevation (E): | 61.97 m  |
| Inlet Pipe Elevation (F):     | 63.53 m  |
| Outlet Pipe Elevation (G):    | 63.47 m  |

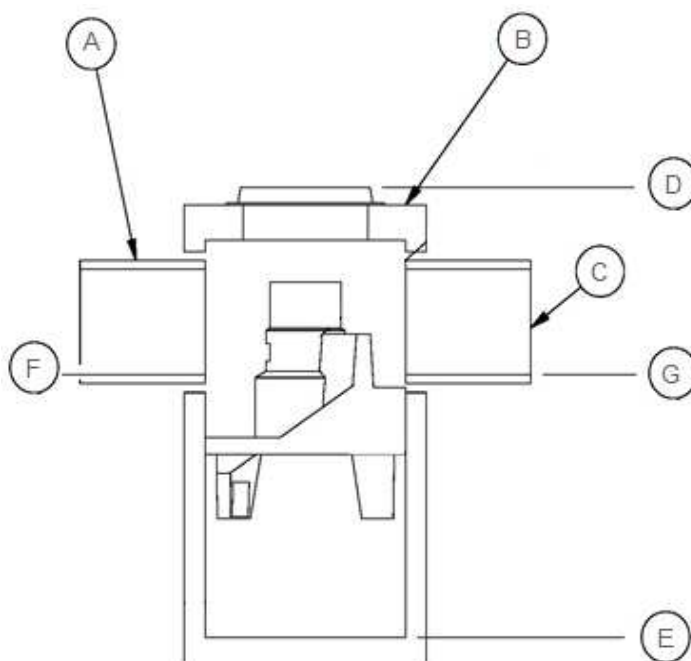
| Site Details                |             |
|-----------------------------|-------------|
| Site Area (ha):             | 2.33        |
| Rational C:                 | 0.9         |
| Particle Size Distribution: | ETV         |
| Rainfall Station:           | Ottawa, ONT |

Notes: OGS results based on ETV PSD and results from ETV testing protocols.

| Stormtech Details                    |         |
|--------------------------------------|---------|
| Chamber Model:                       | MC-3500 |
| No. Chambers in Isolator Row PLUS:   | 19      |
| Volume Treated by Isolator Row PLUS: | 99.2%   |

Notes: Refer to Stormtech drawings for full IR+ configuration.

Isolator Row PLUS must include Flared End Ramp (FLAMP) for proper performance.



## Notes:

Isolator Row PLUS removal efficiency based on verified ETV test report. For dimensions and configuration of Isolator Row PLUS, please see Stormtech drawing package.



Project Name: DYT3 - North  
 Consulting Engineer: AECOM  
 Location: Ottawa, ON

### Net Annual Removal Efficiency Summary

| Rainfall Intensity | Fraction of Rainfall | Removal Efficiency                         |                        | Combined Removal Efficiency | Combined Weighted Removal Efficiency |
|--------------------|----------------------|--|------------------------|-----------------------------|--------------------------------------|
|                    |                      | FD-4HC                                     | IR PLUS <sup>(2)</sup> |                             |                                      |
| mm/hr              | %                    | %  | %                      | %                           | %                                    |
| 0.50               | 0.1%                 | 55.1%                                      | 81.2%                  | 91.6%                       | 0.1%                                 |
| 1.00               | 14.1%                | 50.1%                                      | 81.2%                  | 90.6%                       | 12.8%                                |
| 1.50               | 14.2%                | 47.2%                                      | 81.2%                  | 90.1%                       | 12.8%                                |
| 2.00               | 14.1%                | 45.2%                                      | 81.2%                  | 89.7%                       | 12.7%                                |
| 2.50               | 4.2%                 | 43.5%                                      | 81.2%                  | 89.4%                       | 3.7%                                 |
| 3.00               | 1.5%                 | 42.2%                                      | 81.2%                  | 89.1%                       | 1.3%                                 |
| 3.50               | 8.5%                 | 41.1%                                      | 81.2%                  | 88.9%                       | 7.6%                                 |
| 4.00               | 5.4%                 | 40.2%                                      | 81.2%                  | 88.8%                       | 4.8%                                 |
| 4.50               | 1.2%                 | 39.3%                                      | 81.2%                  | 88.6%                       | 1.0%                                 |
| 5.00               | 5.5%                 | 38.6%                                      | 81.2%                  | 88.4%                       | 4.9%                                 |
| 6.00               | 4.3%                 | 37.2%                                      | 81.2%                  | 88.2%                       | 3.8%                                 |
| 7.00               | 4.5%                 | 36.1%                                      | 81.2%                  | 88.0%                       | 4.0%                                 |
| 8.00               | 3.1%                 | 0.0%                                       | 81.2%                  | 81.2%                       | 2.5%                                 |
| 9.00               | 2.3%                 | 0.0%                                       | 81.2%                  | 81.2%                       | 1.9%                                 |
| 10.00              | 2.6%                 | 0.0%                                       | 81.2%                  | 81.2%                       | 2.1%                                 |
| 20.00              | 9.2%                 | 0.0%                                       | 81.2%                  | 81.2%                       | 7.5%                                 |
| 30.00              | 2.6%                 | 0.0%                                       | 81.2%                  | 81.2%                       | 2.1%                                 |
| 40.00              | 1.2%                 | 0.0%                                       | 73.6%                  | 73.6%                       | 0.9%                                 |
| 50.00              | 0.5%                 | 0.0%                                       | 58.9%                  | 58.9%                       | 0.3%                                 |
| 100.00             | 0.7%                 | 0.0%                                       | 29.4%                  | 29.4%                       | 0.2%                                 |
| 150.00             | 0.1%                 | 0.0%                                       | 19.6%                  | 19.6%                       | 0.0%                                 |
| 200.00             | 0.0%                 | 0.0%                                       | 14.7%                  | 14.7%                       | 0.0%                                 |
|                    |                      |  |                        |                             |                                      |
|                    |                      | <b>Total Net Annual Removal Efficiency</b> |                        |                             | <b>87.0%</b>                         |
|                    |                      | <b>Total Runoff Volume Treated</b>         |                        |                             | <b>99.4%</b>                         |

#### Notes:

- (1) Rainfall Data: 1960:2007, HLY03, Ottawa, ONT, 6105976 & 6105978.
- (2) IR PLUS removal based on ETV PSD and ETV protocols.
- (3) Rainfall adjusted to 5 min peak intensity based on hourly average.
- (4) Combined removal efficiencies calculated based on NCDENR Stormwater BMP Manual, Section 3.9.4, where  
 Total Removal Efficiency = 1st BMP Efficiency + 2nd BMP Efficiency - (1st BMP Efficiency x 2nd BMP Efficiency)



# ADS Treatment Train Sizing

|                             |              |  |
|-----------------------------|--------------|--|
| <b>Project Name:</b>        | DYT3 - South |  |
| <b>Consulting Engineer:</b> | AECOM        |  |
| <b>Location:</b>            | Ottawa, ON   |  |
| <b>Sizing Completed By:</b> | C. Neath     | <b>Email:</b> <a href="mailto:cody.neath@adspipe.com">cody.neath@adspipe.com</a> |

| Summary of Results             |              |
|--------------------------------|--------------|
| Isolator Row PLUS TSS Removal: | 76.7%        |
| FD-4HC TSS Removal:            | 26.0%        |
| <b>Combined TSS Removal:</b>   | <b>81.5%</b> |
| <b>Total Volume Treated:</b>   | <b>95.6%</b> |

| Individual OGS Results |             |                |
|------------------------|-------------|----------------|
| Model                  | TSS Removal | Volume Treated |
| FD-4HC                 | 26.0%       | >90%           |
| FD-5HC                 | 28.0%       | >90%           |
| FD-6HC                 | 29.0%       | >90%           |
| FD-8HC                 | 32.0%       | >90%           |
| FD-10HC                | 34.0%       | >90%           |

| Overall System Capacities           |                     |
|-------------------------------------|---------------------|
| Total Sediment Storage Capacity:    | 5.28 m <sup>3</sup> |
| Oil Storage Capacity:               | 723 L               |
| Max. OGS Pipe Diameter:             | 600 mm              |
| Peak OGS Flow Capacity:             | 510 L/s             |
| Peak Stormtech Inlet Flow Capacity: | 311 L/s             |
| Peak IR PLUS Water Quality Flow:    | 155.5 L/s           |

| OGS Specifications            |          |
|-------------------------------|----------|
| Inlet Pipe Diameter (A):      | 375 mm   |
| Unit Diameter (B):            | 1,200 mm |
| Outlet Pipe Diameter (C):     | 375 mm   |
| Rim Elevation (D):            | 66.64 m  |
| Bottom of Sump Elevation (E): | 61.56 m  |
| Inlet Pipe Elevation (F):     | 63.12 m  |
| Outlet Pipe Elevation (G):    | 63.06 m  |

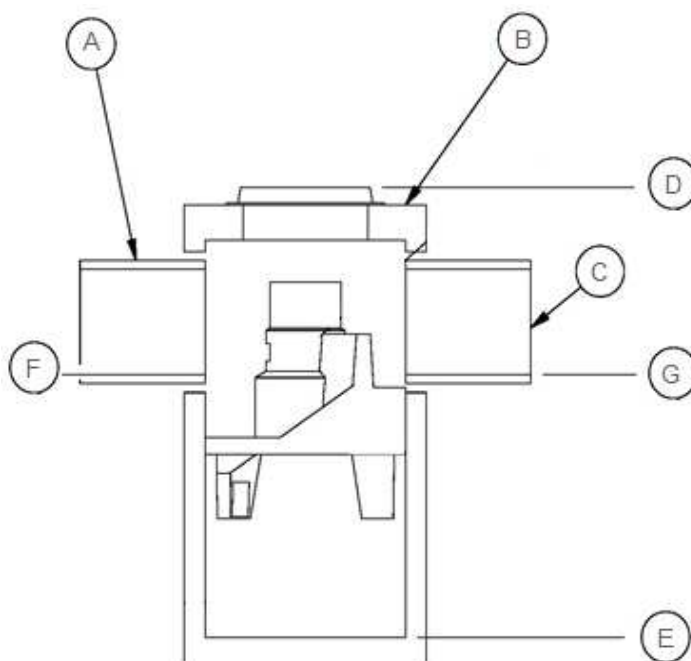
| Site Details                |             |
|-----------------------------|-------------|
| Site Area (ha):             | 4.21        |
| Rational C:                 | 0.9         |
| Particle Size Distribution: | ETV         |
| Rainfall Station:           | Ottawa, ONT |

Notes: OGS results based on ETV PSD and results from ETV testing protocols.

| Stormtech Details                    |         |
|--------------------------------------|---------|
| Chamber Model:                       | MC-3500 |
| No. Chambers in Isolator Row PLUS:   | 14      |
| Volume Treated by Isolator Row PLUS: | 94.5%   |

Notes: Refer to Stormtech drawings for full IR+ configuration.

Isolator Row PLUS must include Flared End Ramp (FLAMP) for proper performance.



## Notes:

Isolator Row PLUS removal efficiency based on verified ETV test report. For dimensions and configuration of Isolator Row PLUS, please see Stormtech drawing package.



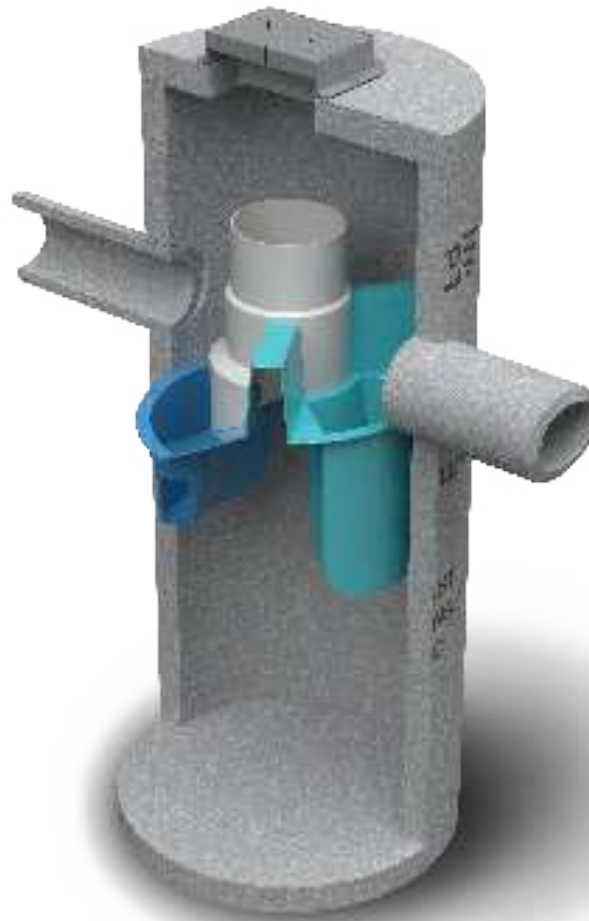
Project Name: DYT3 - South  
 Consulting Engineer: AECOM  
 Location: Ottawa, ON

### Net Annual Removal Efficiency Summary

| Rainfall Intensity                         | Fraction of Rainfall | Removal Efficiency |                        | Combined Removal Efficiency | Combined Weighted Removal Efficiency |
|--|----------------------|--------------------|------------------------|-----------------------------|--------------------------------------|
|  |                      | FD-4HC             | IR PLUS <sup>(2)</sup> |                             |                                      |
| mm/hr                                      | %                    | %                  | %                      | %                           | %                                    |
| 0.50                                       | 0.1%                 | 50.9%              | 81.2%                  | 90.8%                       | 0.1%                                 |
| 1.00                                       | 14.1%                | 45.9%              | 81.2%                  | 89.8%                       | 12.7%                                |
| 1.50                                       | 14.2%                | 43.0%              | 81.2%                  | 89.3%                       | 12.7%                                |
| 2.00                                       | 14.1%                | 40.9%              | 81.2%                  | 88.9%                       | 12.6%                                |
| 2.50                                       | 4.2%                 | 39.3%              | 81.2%                  | 88.6%                       | 3.7%                                 |
| 3.00                                       | 1.5%                 | 38.0%              | 81.2%                  | 88.3%                       | 1.3%                                 |
| 3.50                                       | 8.5%                 | 36.9%              | 81.2%                  | 88.1%                       | 7.5%                                 |
| 4.00                                       | 5.4%                 | 35.9%              | 81.2%                  | 88.0%                       | 4.8%                                 |
| 4.50                                       | 1.2%                 | 0.0%               | 81.2%                  | 81.2%                       | 0.9%                                 |
| 5.00                                       | 5.5%                 | 0.0%               | 81.2%                  | 81.2%                       | 4.5%                                 |
| 6.00                                       | 4.3%                 | 0.0%               | 81.2%                  | 81.2%                       | 3.5%                                 |
| 7.00                                       | 4.5%                 | 0.0%               | 81.2%                  | 81.2%                       | 3.7%                                 |
| 8.00                                       | 3.1%                 | 0.0%               | 81.2%                  | 81.2%                       | 2.5%                                 |
| 9.00                                       | 2.3%                 | 0.0%               | 81.2%                  | 81.2%                       | 1.9%                                 |
| 10.00                                      | 2.6%                 | 0.0%               | 81.2%                  | 81.2%                       | 2.1%                                 |
| 20.00                                      | 9.2%                 | 0.0%               | 60.0%                  | 60.0%                       | 5.5%                                 |
| 30.00                                      | 2.6%                 | 0.0%               | 40.0%                  | 40.0%                       | 1.0%                                 |
| 40.00                                      | 1.2%                 | 0.0%               | 30.0%                  | 30.0%                       | 0.3%                                 |
| 50.00                                      | 0.5%                 | 0.0%               | 24.0%                  | 24.0%                       | 0.1%                                 |
| 100.00                                     | 0.7%                 | 0.0%               | 12.0%                  | 12.0%                       | 0.1%                                 |
| 150.00                                     | 0.1%                 | 0.0%               | 8.0%                   | 8.0%                        | 0.0%                                 |
| 200.00                                     | 0.0%                 | 0.0%               | 6.0%                   | 6.0%                        | 0.0%                                 |
|  |                      |                    |                        |                             |                                      |
| <b>Total Net Annual Removal Efficiency</b> |                      |                    |                        | <b>81.5%</b>                |                                      |
| <b>Total Runoff Volume Treated</b>         |                      |                    |                        | <b>95.6%</b>                |                                      |

**Notes:**

- (1) Rainfall Data: 1960:2007, HLY03, Ottawa, ONT, 6105976 & 6105978.
- (2) IR PLUS removal based on ETV PSD and ETV protocols.
- (3) Rainfall adjusted to 5 min peak intensity based on hourly average.
- (4) Combined removal efficiencies calculated based on NCDENR Stormwater BMP Manual, Section 3.9.4, where  
 Total Removal Efficiency = 1st BMP Efficiency + 2nd BMP Efficiency - (1st BMP Efficiency x 2nd BMP Efficiency)



## Operation and Maintenance Manual

**First Defense<sup>®</sup> High Capacity and First Defense<sup>®</sup> Optimum**

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Vortex Separator for Stormwater Treatment

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**DISCLAIMER:** Information and data contained in this manual is exclusively for the purpose of assisting in the operation and maintenance of Hydro International plc's First Defense®. No warranty is given nor can liability be accepted for use of this information for any other purpose. Hydro International plc has a policy of continuous product development and reserves the right to amend specifications without notice.

# I. First Defense® by Hydro International

## Introduction

The First Defense® is an enhanced vortex separator that combines an effective and economical stormwater treatment chamber with an integral peak flow bypass. It efficiently removes total suspended solids (TSS), trash and hydrocarbons from stormwater runoff without washing out previously captured pollutants. The First Defense® is available in several model configurations to accommodate a wide range of pipe sizes, peak flows and depth constraints.

The two product models described in this guide are the First Defense® High Capacity and the First Defense® Optimum; they are inspected and maintained identically.

## Operation

The First Defense® operates on simple fluid hydraulics. It is self-activating, has no moving parts, no external power requirement and is fabricated with durable non-corrosive components. No manual procedures are required to operate the unit and maintenance is limited to monitoring accumulations of stored pollutants and periodic clean-outs. The First Defense® has been designed to allow for easy and safe access for inspection, monitoring and clean-out procedures. Neither entry into the unit nor removal of the internal components is necessary for maintenance, thus safety concerns related to confined-space-entry are avoided.

## Pollutant Capture and Retention

The internal components of the First Defense® have been designed to optimize pollutant capture. Sediment is captured and retained in the base of the unit, while oil and floatables are stored on the water surface in the inner volume (Fig.1).

The pollutant storage volumes are isolated from the built-in bypass chamber to prevent washout during high-flow storm events. The sump of the First Defense® retains a standing water level between storm events. This ensures a quiescent flow regime at the onset of a storm, preventing resuspension and washout of pollutants captured during previous events.

Accessories such as oil absorbent pads are available for enhanced oil removal and storage. Due to the separation of the oil and floatable storage volume from the outlet, the potential for washout of stored pollutants between clean-outs is minimized.

## Applications

- Stormwater treatment at the point of entry into the drainage line
- Sites constrained by space, topography or drainage profiles with limited slope and depth of cover
- Retrofit installations where stormwater treatment is placed on or tied into an existing storm drain line
- Pretreatment for filters, infiltration and storage

## Advantages

- Inlet options include surface grate or multiple inlet pipes
- Integral high capacity bypass conveys large peak flows without the need for “offline” arrangements using separate junction manholes
- Long flow path through the device ensures a long residence time within the treatment chamber, enhancing pollutant settling
- Delivered to site pre-assembled and ready for installation

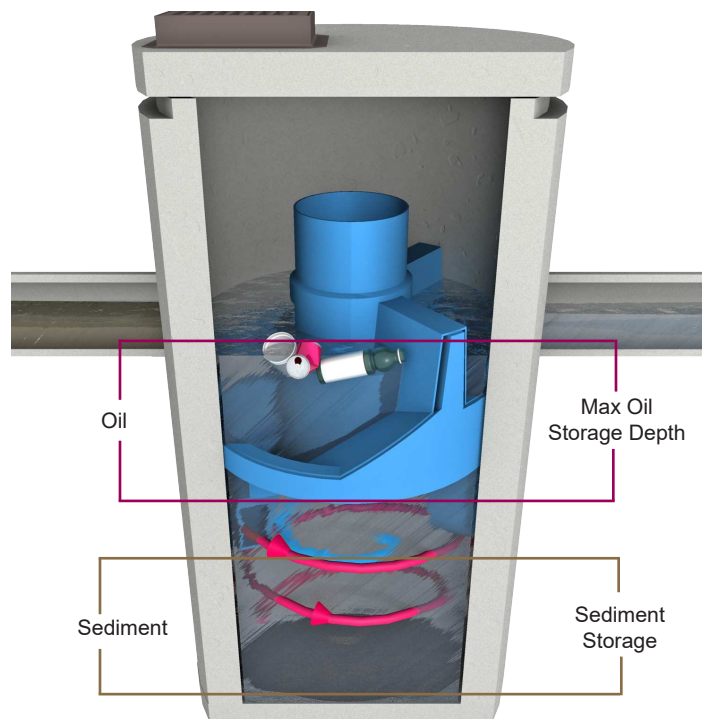


Fig.1 Pollutant storage volumes in the First Defense®.

## II. Model Sizes & Configurations

The First Defense® inlet and internal bypass arrangements are available in several model sizes and configurations. The components have modified geometries allowing greater design flexibility to accommodate various site constraints.

All First Defense® models include the internal components that are designed to remove and retain total suspended solids (TSS), gross solids, floatable trash and hydrocarbons (Fig.2). First Defense® model sizes (diameter) are shown in Table 1.

## III. Maintenance

### First Defense® Components

- |                    |                             |                         |
|--------------------|-----------------------------|-------------------------|
| 1. Built-In Bypass | 4. Floatables Draw-off Port | 7. Sediment Storage     |
| 2. Inlet Pipe      | 5. Outlet Pipe              | 8. Inlet Grate or Cover |
| 3. Inlet Chute     | 6. Floatables Storage       |                         |

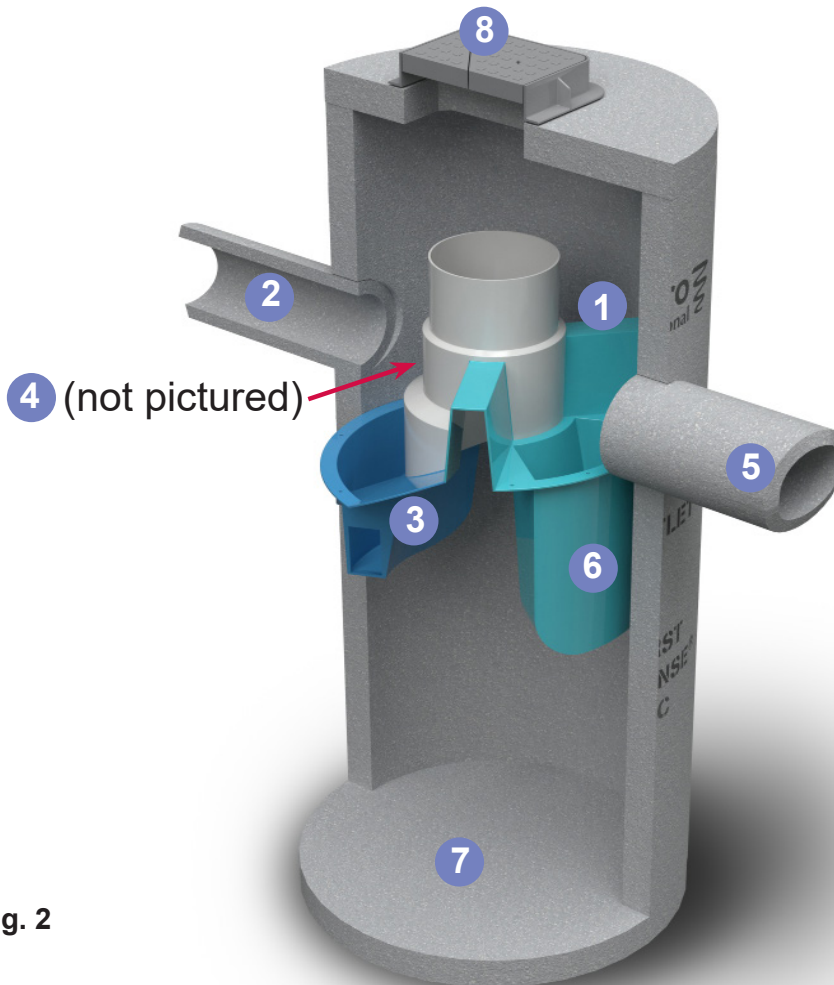


Fig. 2

Table 1

| First Defense®<br>Model Sizes |
|-------------------------------|
| (ft / m) diameter             |
| 3 / 0.9                       |
| 4 / 1.2                       |
| 5 / 1.5                       |
| 6 / 1.8                       |
| 8 / 2.4                       |
| 10 / 3.0                      |



## Overview

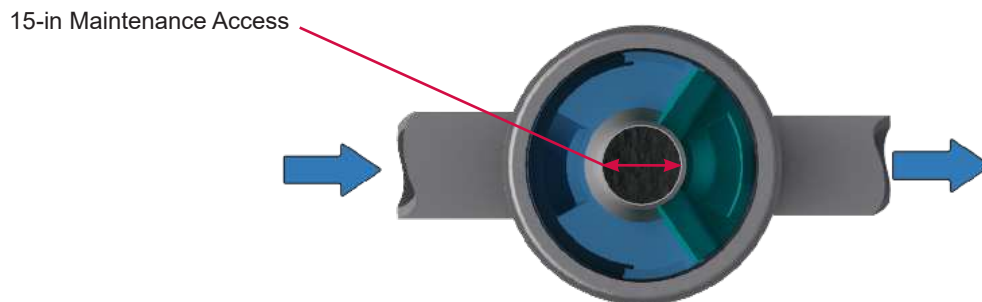
The First Defense® protects the environment by removing a wide range of pollutants from stormwater runoff. Periodic removal of these captured pollutants is essential to the continuous, long-term functioning of the First Defense®. The First Defense® will capture and retain sediment and oil until the sediment and oil storage volumes are full to capacity. When sediment and oil storage capacities are reached, the First Defense® will no longer be able to store removed sediment and oil.

The First Defense® allows for easy and safe inspection, monitoring and clean-out procedures. A commercially or municipally owned sump-vac is used to remove captured sediment and floatables. Access ports are located in the top of the manhole.

Maintenance events may include Inspection, Oil & Floatables Removal, and Sediment Removal. Maintenance events do not require entry into the First Defense®, nor do they require the internal components of the First Defense® to be removed. In the case of inspection and floatables removal, a vactor truck is not required. However, a vactor truck is required if the maintenance event is to include oil removal and/or sediment removal.

## Maintenance Equipment Considerations

The internal components of the First Defense® have a centrally located circular shaft through which the sediment storage sump can be accessed with a sump vac hose. The open diameter of this access shaft is 15 inches in diameter (Fig.3). Therefore, the nozzle fitting of any vactor hose used for maintenance should be less than 15 inches in diameter.



*Fig.3 The central opening to the sump of the First Defense® is 15 inches in diameter.*

## Determining Your Maintenance Schedule

The frequency of clean out is determined in the field after installation. During the first year of operation, the unit should be inspected every six months to determine the rate of sediment and floatables accumulation. A simple probe such as a Sludge-Judge® can be used to determine the level of accumulated solids stored in the sump. This information can be recorded in the maintenance log (see page 9) to establish a routine maintenance schedule.

The vactor procedure, including both sediment and oil / floatables removal, for First Defense® typically takes less than 30 minutes and removes a combined water/oil volume of about 765 gallons.

### Inspection Procedures

1. Set up any necessary safety equipment around the access port or grate of the First Defense® as stipulated by local ordinances. Safety equipment should notify passing pedestrian and road traffic that work is being done.
2. Remove the grate or lid to the manhole.
3. Without entering the vessel, look down into the chamber to inspect the inside. Make note of any irregularities. Fig.4 shows the standing water level that should be observed.
4. Without entering the vessel, use the pole with the skimmer net to remove floatables and loose debris from the components and water surface.
5. Using a sediment probe such as a Sludge Judge®, measure the depth of sediment that has collected in the sump of the vessel.
6. On the Maintenance Log (see page 9), record the date, unit location, estimated volume of floatables and gross debris removed, and the depth of sediment measured. Also note any apparent irregularities such as damaged components or blockages.
7. Securely replace the grate or lid.
8. Take down safety equipment.
9. Notify Hydro International of any irregularities noted during inspection.

### Floatables and Sediment Clean Out

Floatables clean out is typically done in conjunction with sediment removal. A commercially or municipally owned sump-vac is used to remove captured sediment and floatables (Fig.4).

Floatables and loose debris can also be netted with a skimmer and pole. The access port located at the top of the manhole provides unobstructed access for a vactor hose to be lowered to the base of the sump.

### Scheduling

- Floatables and sump clean out are typically conducted once a year during any season.
- Floatables and sump clean out should occur as soon as possible following a spill in the contributing drainage area.



Fig.4 Floatables are removed with a vactor hose

### Recommended Equipment

- Safety Equipment (traffic cones, etc)
- Crow bar or other tool to remove grate or lid
- Pole with skimmer or net (if only floatables are being removed)
- Sediment probe (such as a Sludge Judge®)
- Vactor truck (flexible hose recommended)
- First Defense® Maintenance Log

### *Floatables and Sediment Clean Out Procedures*

1. Set up any necessary safety equipment around the access port or grate of the First Defense® as stipulated by local ordinances. Safety equipment should notify passing pedestrian and road traffic that work is being done.
2. Remove the grate or lid to the manhole.
3. Without entering the vessel, look down into the chamber to inspect the inside. Make note of any irregularities.
4. Remove oil and floatables stored on the surface of the water with the vacator hose or with the skimmer or net
5. Using a sediment probe such as a Sludge Judge®, measure the depth of sediment that has collected in the sump of the vessel and record it in the Maintenance Log (page 9).
6. Once all floatables have been removed, drop the vacator hose to the base of the sump. Vacator out the sediment and gross debris off the sump floor
7. Retract the vacator hose from the vessel.
8. On the Maintenance Log provided by Hydro International, record the date, unit location, estimated volume of floatables and gross debris removed, and the depth of sediment measured. Also note any apparent irregularities such as damaged components, blockages, or irregularly high or low water levels.
9. Securely replace the grate or lid.

## Maintenance at a Glance

|                            |  |
|----------------------------|--|
| Inspection                 | <ul style="list-style-type: none"> <li>- Regularly during first year of installation</li> <li>- Every 6 months after the first year of installation</li> </ul> |
| Oil and Floatables Removal | <ul style="list-style-type: none"> <li>- Once per year, with sediment removal</li> <li>- Following a spill in the drainage area</li> </ul>                     |
| Sediment Removal           | <ul style="list-style-type: none"> <li>- Once per year or as needed</li> <li>- Following a spill in the drainage area</li> </ul>                               |

NOTE: For most clean outs the entire volume of liquid does not need to be removed from the manhole. Only remove the first few inches of oils and floatables from the water surface to reduce the total volume of liquid removed during a clean out.



## First Defense® Installation Log

|                                       |               |
|---------------------------------------|---------------|
| HYDRO INTERNATIONAL REFERENCE NUMBER: |               |
| SITE NAME:                            |               |
| SITE LOCATION:                        |               |
| OWNER:                                | CONTRACTOR:   |
| CONTACT NAME:                         | CONTACT NAME: |
| COMPANY NAME:                         | COMPANY NAME: |
| ADDRESS:                              | ADDRESS:      |
| TELEPHONE:                            | TELEPHONE:    |
| FAX:                                  | FAX:          |

INSTALLATION DATE:    /    /

MODEL SIZE (CIRCLE ONE):    [3-FT]    [4-FT]    [5-FT]    [6-FT]    [8-FT]    [10-FT]

INLET (CIRCLE ALL THAT APPLY):    GRATED INLET (CATCH BASIN)    INLET PIPE (FLOW THROUGH)



**First Defense® Inspection and Maintenance Log**

| Date | Initials | Depth of Floatables and Oils | Sediment Depth Measured | Volume of Sediment Removed | Site Activity and Comments |
|------|----------|------------------------------|-------------------------|----------------------------|----------------------------|
|      |          |                              |                         |                            |                            |
|      |          |                              |                         |                            |                            |
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|      |          |                              |                         |                            |                            |







## Stormwater Solutions

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[www.hydro-int.com](http://www.hydro-int.com)

Turning Water Around...®

FD\_O+M\_J\_2009(2)





# Verification Statement



## Hydro International First Defense® HC Oil Grit Separator Registration number: (V-2018-10-01) Date of issue: 2018-October-15 (rev 2019-02-01)

|                        |  |
|------------------------|--|
| <b>Technology type</b> | Oil Grit Separator   |
| <b>Application</b>     | Technology to remove oil, sediment, trash and debris from stormwater and snowmelt runoff as well as other pollutants that attach to sediment particles, such as nutrients and metals |
| <b>Company</b>         | Hydro International  |
| <b>Address</b>         | 94 Hutchins Drive, Portland, Maine <b>Phone</b> +1-207-756 6200<br>USA 04102   |
| <b>Website</b>         | <a href="https://www.hydro-int.com">https://www.hydro-int.com</a>  |
| <b>E-mail</b>          | dscott@hydro-int.com   |

### Verified Performance Claims

The Hydro International First Defense® High Capacity (HC) Oil Grit Separator (OGS) was tested by Good Harbour Laboratories Inc. (GHL), Mississauga, Ontario, Canada in 2018. The performance test results were verified by Toronto and Region Conservation Authority (TRCA), Vaughan, Ontario, Canada following the requirements of ISO 14034:2016 and the VerifiGlobal Performance Verification Protocol. The following performance claims were verified:

#### **Capture test<sup>1</sup>:**

With a false floor set to 50% of the manufacturer’s recommended maximum sediment storage depth and an influent test sediment concentration of 200 mg/L, the First Defense® HC OGS device removes 67, 60, 55, 50, 45, 45, and 41 percent of influent sediment by mass at surface loading rates of 40, 80, 200, 400, 600, 1000, and 1400 L/min/m<sup>2</sup>, respectively.

#### **Scour test<sup>1</sup>:**

With 10.2 cm (4 inches) of test sediment pre-loaded onto a false floor reaching 50% of the manufacturer’s recommended maximum sediment storage depth, the First Defense® HC OGS device generates adjusted effluent<sup>2</sup> concentrations of 0, 0, 11, 2, and 0 mg/L at 5-minute duration surface loading rates of 200, 800, 1400, 2000, and 2600 L/min/m<sup>2</sup>, respectively.

<sup>1</sup> The claims can be applied to other units smaller or larger than the tested unit as long as the untested units meet the scaling rule specified in the Procedure for Laboratory of Testing of Oil Grit Separators (Version 3.0, June 2014)

<sup>2</sup> The effluent suspended sediment concentration is adjusted based on the background concentration and the smallest 5% of particles captured during the 40 L/min/m<sup>2</sup> sediment capture test (see Table 2)

## Technology Application

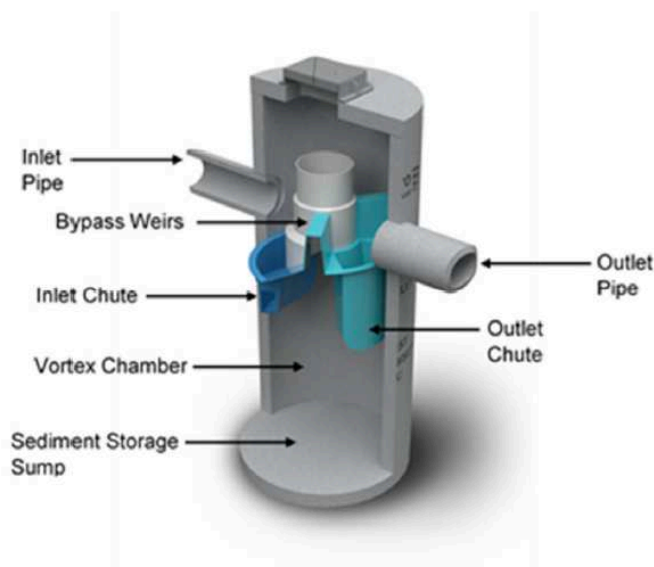
The First Defense® HC (FDHC) Oil Grit Separator can be used as a stand-alone stormwater treatment technology, depending on water quality objectives, or as a pretreatment component in a treatment train when higher TSS removals are required and polishing or volume reduction best management practices (BMPs), such as infiltration or bio-infiltration, are installed downstream. FDHC applications include: stormwater treatment at the point of entry into the drainage line; sites constrained by space, topography or drainage profiles with limited slope and depth of cover; retrofit installations where stormwater treatment is placed on or tied into an existing storm drain line; pre-treatment for filters, infiltration, other sedimentation BMPs and storage.

## Technology Description

The Hydro International First Defense® HC (FDHC) is an Oil Grit Separator designed to remove oil, sediment, trash and debris from stormwater and snowmelt runoff as well as other pollutants that attach to sediment particles, such as nutrients and metals. The patented flow modifying internal components are designed to be inserted into standard precast concrete manholes where they collect and treat runoff as part of the drainage system (Figure 1).

Flow entering the manhole via an inlet pipe or inlet grate is diverted into a vortex chamber beneath a separation module that includes both inlet/outlet chutes and bypass weirs. The internal bypass weirs divert flows greater than the maximum design treatment flow rate over the separation module and away from the vortex chamber where oil, sediment, debris and attached pollutants are accumulating. This function prevents high velocities from re-suspending previously captured pollutants during large storm events. The FDHC can be designed and sized to function effectively in either online or offline configurations.

Figure 1: Hydro International First Defense® HC Oil Grit Separator



---

The test unit was 1.2 m (4 foot) in diameter with a 1.51 m (59 5/8 inches) sump depth measured from the outlet invert to the floor of the unit. The effective treatment area (also known as the effective sedimentation area) is 1.2 m<sup>2</sup> (12.6 ft<sup>2</sup>). The maximum sediment storage depth is 0.457 m (18 inches).

### Description of Test Procedure

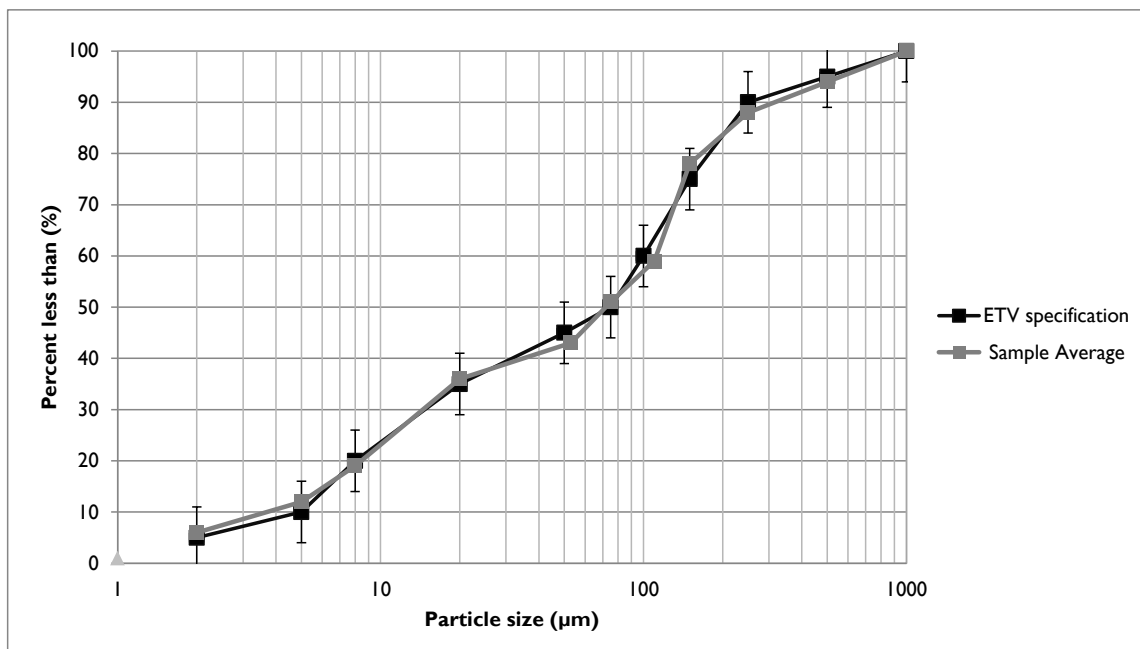
The test data and results for this verification were obtained from independent testing conducted on a 1.2 m (48 inch) diameter Hydro International First Defense® HC OGS device, in accordance with the *Procedure for Laboratory Testing of Oil-Grit Separators (Version 3.0, June 2014)*. The laboratory test procedure was originally prepared by the Toronto and Region Conservation Authority (TRCA) in association with a 31 member advisory committee from various stakeholder groups.

### Verification Results

Toronto and Region Conservation Authority verified the performance test data and other information pertaining to the First Defense® HC Oil Grit Separator. A Verification Plan was prepared to guide the verification process based on the requirements of ISO 14034:2016 and the VerifiGlobal Performance Verification Protocol.

The test sediment consisted of ground silica (1 – 1000 micron) with a specific gravity of 2.65, uniformly mixed to meet the particle size distribution specified in the testing procedure. The *Procedure for Laboratory Testing of Oil Grit Separators* requires that the three sample average of the test sediment particle size distribution (PSD) meet the specified PSD percent less than values within a boundary threshold of 6%, and a median particle size no greater than 75 µm. Comparison of the individual sample and average test sediment PSD to the specified PSD shown in Figure 2 indicates that the test sediment used for the capture and scour tests met this condition. The median particle size was 73 µm. Samples from test sediment batches used for each run met the specified PSD within the required tolerance thresholds.

**Figure 2 - The three sample average particle size distribution (PSD) of the test sediment used for the capture and scour test compared to the specified PSD**



The capacity of the device to retain sediment was determined at seven surface loading rates using the modified mass balance method. This method involved measuring the mass and particle size distribution of the injected and retained sediment for each test run. Performance was evaluated with a false floor simulating the technology filled to 50% of the manufacturer’s recommended maximum sediment storage depth. The test was carried out with clean water that maintained a sediment concentration below 20 mg/L. Based on these conditions, removal efficiencies for individual particle size classes and for the test sediment as a whole were determined for each of the tested surface loading rates (Table 1).

In some instances, the removal efficiencies were above 100% for certain particle size fractions. These discrepancies are not unique to any one test laboratory and are attributed to errors relating to the blending of sediment, collection of representative samples for laboratory submission, and laboratory analysis of PSD. Due to these errors, caution should be exercised in applying the removal efficiencies by particle size fraction for the purposes of sizing the tested device (see Bulletin # CETV 2016-11-0001). The results for “all particle sizes by mass balance” (see Table 1) are based on measurements of the total injected and retained sediment mass, and are therefore not subject to blending, sampling or PSD analysis errors.

**Table 1 - Removal efficiencies (%) of the First Defence HC at specified surface loading rates**

| Particle size fraction (µm)                   | Surface loading rate (L/min/m <sup>2</sup> ) |             |             |             |             |             |             |
|---|--|-------------|-------------|-------------|-------------|-------------|-------------|
|   | 40   | 80          | 200         | 400         | 600         | 1000        | 1400        |
| >500  | 100*   | 100*        | 100*        | 81          | 72          | 86          | 80          |
| 250 - 500                                     | 100*   | 97          | 99          | 100*        | 100*        | 59          | 88          |
| 150 - 250                                     | 100*   | 91          | 95          | 93          | 47          | 100*        | 84          |
| 105 - 150                                     | 96   | 89          | 94          | 89          | 90          | 70          | 75          |
| 75 - 105                                      | 100*   | 90          | 95          | 77          | -20**       | 100         | 51          |
| 53 - 75                                       | 74   | 100*        | 97          | 62          | 100*        | 46          | 37          |
| 20 - 53                                       | 60   | 33          | 10          | 5           | 4           | 0           | 0           |
| 8 - 20  | 29   | 16          | 8           | 3           | 3           | 1           | 1           |
| 5 - 8   | 8  | 5           | 8           | 4           | 4           | 4           | 3           |
| <5  | 5  | 3           | 0           | 0           | 0           | 3           | 3           |
| <b>All particle sizes<br/>By mass balance</b> | <b>66.5</b>                                  | <b>59.9</b> | <b>55.4</b> | <b>50.2</b> | <b>44.9</b> | <b>45.2</b> | <b>40.5</b> |

\* Removal efficiencies were calculated to be above 100%. Calculated values ranged between 101 and 184% (average 115%). See text and Bulletin # CETV 2016-11-0001 for more information.

\*\* An outlier in the retained sediment sample sieve data resulted in negative removal for this size fraction. The outlier at the 75 µm particle size is shown in Figure 3.

**Figure 3 - Particle size distribution of sediment retained in the First Defence HC in relation to the injected test sediment average**

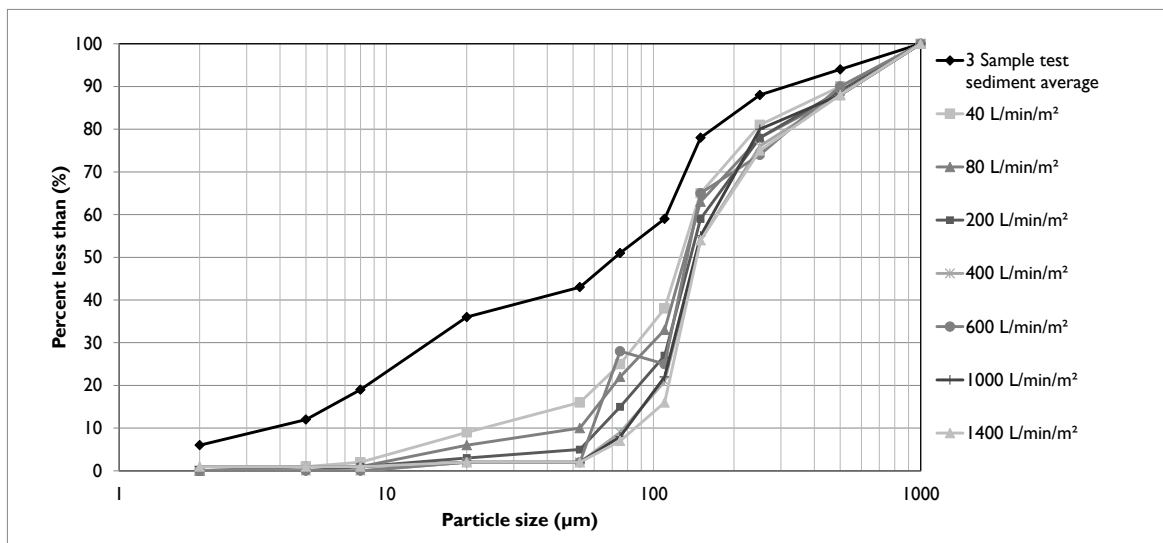


Figure 3 compares the particle size distribution (PSD) of the three sample average of the test sediment to the PSD of the sediment retained by the FDHC device at each of the tested surface loading rates. As expected, the capture efficiency for fine particles was generally found to decrease as surface loading rates increased, particularly in the 40 to 400 L/min/m<sup>2</sup> range.



Table 2 shows the results of the sediment scour and re-suspension test for the First Defense® HC unit. The scour test involved preloading 10.2 cm (4 inches) of fresh test sediment into the sedimentation sump of the device. The sediment was placed on a false floor to mimic a device filled to 50% of the maximum recommended sediment storage depth. Clean water was run through the device at five surface loading rates over a 30 minute period. Each flow rate was maintained for 5 minutes with a one minute transition time between flow rates. Effluent samples were collected at one minute sampling intervals and analyzed for Suspended Sediment Concentration (SSC) and PSD by recognized methods. The effluent samples were subsequently adjusted based on the background concentration of the influent water. The smallest 5% of particles captured during the 40 L/min/m<sup>2</sup> sediment capture test (13.5 μm in this case) was used to further adjust the effluent sediment concentrations, as per the method described in Bulletin # CETV 2016-09-0001. Results showed average adjusted effluent sediment concentrations below 11 mg/L at all surface loading rates. Effluent concentrations would be expected to decrease at higher flow rates since bypass over the insert bypass weirs was observed to begin at 1,032 L/min/m<sup>2</sup>.

**Table 2 - Scour test adjusted effluent sediment concentration at each surface loading rate**

| Run | Surface loading rate (L/min/m <sup>2</sup> ) | Run time (min) | Background sample concentration (mg/L) | Average adjusted effluent suspended sediment concentration (mg/L)* |
|-----|--|----------------|--|--|
| 1   | 200  | 1:00 – 6:00    | 0.8                                    | 0  |
| 2   | 800  | 7:00 – 12:00   | 1.0                                    | 0  |
| 3   | 1400   | 13:00 – 18:00  | 1.1                                    | 10.6   |
| 4   | 2000   | 19:00 – 24:00  | 2.8                                    | 2.4  |
| 5   | 2600   | 25:00 – 30:00  | 6.6                                    | 0  |

\*The effluent suspended sediment concentration is adjusted based on the background concentration and the smallest 5% of particles captured during the 40 L/min/m<sup>2</sup> sediment capture test, as per the method described in Bulletin # CETV 2016-09-0001.

### Variations from the Procedure

Minor variations from the *Procedure for Laboratory Testing of Oil-Grit Separators* used as the basis of testing for this verification were as follows:

1. The *Procedure* states that the tested device “must be a full scale commercially available device with the same configuration and components as would be typical for an actual installation.” The unit tested for this verification had the same internal components as would be typical for a commercial installation, but the internal components were placed inside a structure constructed of composite materials, rather than a manhole made of concrete, the latter of which is typical for most installations. The dimensions of the structure were the same as would have been the case had the manhole been concrete. The use of alternate materials for the structure was not believed to significantly affect system performance.

2. As part of the capture test, evaluation of the 40 and 80 L/min/m<sup>2</sup> surface loading rate was split into 3 and 2 parts, respectively. The test was conducted in parts because of the long duration (i.e. over 10 hours) needed to feed the required minimum 11.3 kg of test sediment into the unit. At the end of the first and second parts of the test, the flow rates were gradually decreased to prevent capture of particles that would have been washed out under normal circumstances. The requirement to split the test into parts was not anticipated in the *Procedure for Laboratory Testing of Oil-Grit Separators*, but has been a common feature of testing at the 40 L/min/m<sup>2</sup> surface loading rate. Conducting the test in two parts for the 80 L/min/m<sup>2</sup> surface loading rate is less common. The testing did not assess the significance of the breaks, however, the test laboratory and verifier do not believe that the breaks significantly affected the test results.



3. During the sediment scour test, the flow rate coefficient of variation (COV) at the 200 L/min/m<sup>2</sup> surface loading rate of 0.045 slightly exceeded the target COV of 0.04. The average flow rate during the test remained within ±10% of the target flow rate.

**Quality assurance**

Performance testing and verification of the First Defense® HC Oil Grit Separator were performed in accordance with the requirements of ISO 14034:2016 and the VerifiGlobal Performance Verification Protocol. The verifier, Toronto and Region Conservation Authority, has confirmed that quality assurance requirements were addressed throughout the performance testing process and in the generation of performance test results. This includes reviewing all data sheets and data downloads, as well as overall management of the test system, quality control and data integrity.

**Verification Summary**

In summary, the First Defense® HC Oil Grit Separator is designed to remove oil, sediment, trash and debris from stormwater and snowmelt runoff as well as other pollutants that attach to sediment particles, such as nutrients and metals. Verification of performance claims for the Hydro International First Defense® HC Oil Grit Separator was conducted by Toronto and Region Conservation Authority based on independent third-party performance test results provided by Good Harbour Laboratories, as well as additional information provided by Hydro International. Table 3 summarizes the verification results in relation to the technology performance parameters that were identified to determine the efficacy of the First Defense® HC Oil Grit Separator.

**Table 3 - Summary of Verification Results Against Performance Parameters**

| <b>Performance Parameter</b> | <b>Verified Performance</b>  |
|------------------------------|--|
| Sediment Removal Rate        | The sediment removal rate of the FDHC is dependent upon flow rate, particle density and particle size. Removal efficiency decreased with increasing surface loading rate from 67% at 40 L/min/m <sup>2</sup> to 41% at 1400 L/min/m <sup>2</sup> . The weighted average removal efficiency achieved by the unit will vary depending on the rainfall distribution of the jurisdiction in which it is installed, and site characteristics.   |
| Sediment Scour               | When pre-loaded with sediment with a particle size distribution matching that of the feed sediment used in the sediment capture test, the FDHC generated effluent suspended solids concentrations of less than 11 mg/L at surface loading rates ranging from 200 to 2600 L/min/m <sup>2</sup> .  |
| Bypass flow rate             | The flow rate at which bypass occurs will vary based on model size. For the 1.2 m (4 foot) diameter test unit, the flow rate at which bypass occurred over the insert bypass weirs was 1238 L/min (327 gpm).   |
| Head loss                    | The loss of hydraulic head across the FDHC was determined by measuring the water elevation difference between the inlet and outlet sides of the insert. Head loss may vary based on model size. For the tested unit the head loss ranged from 2 mm (0.08 inches) at 93.5 L/min (12.3 gpm) to 100 mm (3.94 inches) at 1238 L/min (327 gpm) when bypass was observed to occur. At 327 gpm, when bypass occurred, the depth of the water was 177 mm upstream and 77 mm downstream for a difference of 100 mm (3.94 inches). The highest water elevation difference was 111mm (4.37 inches) at a flow rate of 1635 L/min (431.8 gpm), after which head loss declined up to the maximum measured flow rate of 3036 L/min (801.9 gpm). |



**What is ISO 14034?**

The purpose of environmental technology verification is to provide a credible and impartial account of the performance of environmental technologies. Environmental technology verification is based on a number of principles to ensure that verifications are performed and reported accurately, clearly, unambiguously and objectively. The International Organization for Standardization (ISO) standard for environmental technology verification (ETV) is ISO 14034, which was published in November 2016.

**Benefits of ETV**

ETV contributes to protection and conservation of the environment by promoting and facilitating market uptake of innovative environmental technologies, especially those that perform better than relevant alternatives. ETV is particularly applicable to those environmental technologies whose innovative features or performance cannot be fully assessed using existing standards. Through the provision of objective evidence, ETV provides an independent and impartial confirmation of the performance of an environmental technology based on reliable test data. ETV aims to strengthen the credibility of new, innovative technologies by supporting informed decision-making among interested parties.

|   |  |
|---|--|
| For more information on the First Defense® HC Oil Grit Separator, contact:  | For more information on VerifiGlobal, contact:   |
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| Signed for Hydro International:<br><br><i>Original signed by:</i><br><b>David Scott</b><br><br>David Scott<br>Technical Product Manager,<br>Americas Stormwater | Signed for VerifiGlobal:<br><br><i>Original signed by:</i><br><b>Thomas Bruun</b><br>Thomas Bruun, Managing Director<br><br><i>Original signed by:</i><br><b>John Neate</b><br>John Neate, Managing Director |

**NOTICE:** Verifications are based on an evaluation of technology performance under specific, predetermined operational conditions and parameters and the appropriate quality assurance procedures. VerifiGlobal and the Verification Expert, Toronto and Region Conservation Authority, make no expressed or implied warranties as to the performance of the technology and do not certify that a technology will always operate as verified. The end user is solely responsible for complying with any and all applicable regulatory requirements. Mention of commercial product names does not imply endorsement.

VerifiGlobal and the Verification Expert, Toronto and Region Conservation Authority, provide the verification services solely on the basis of the information supplied by the applicant or vendor and assume no liability thereafter. The responsibility for the information supplied remains solely with the applicant or vendor and the liability for the purchase, installation, and operation (whether consequential or otherwise) is not transferred to any other party as a result of the verification.

# Appendix **H**

## **Supporting Engineering Documentation and Calculations – Underground Storage System**



Project: **DYT3 - North - Rev 2**



Include Perimeter Stone in Calculations

Click for Stage Area Data

Click to Invert Stage Area Data

[Click Here for Imperial](#)

|                                  |         |
|----------------------------------|---------|
| Chamber Model -                  | MC-3500 |
| Units -                          | Metric  |
| Number of Chambers -             | 285     |
| Number of End Caps -             | 30      |
| Void in the stone (porosity) -   | 40 %    |
| Base of Stone Elevation -        | 63.55 m |
| Amount of Stone Above Chambers - | 305 mm  |
| Amount of Stone Below Chambers - | 229 mm  |

1477.325 sq.meters    Min. Area -    1357.38 sq.meters

**StormTech MC-3500 Cumulative Storage Volumes**

| Height of System (mm) | Incremental Single Chamber (cubic meters) | Incremental Single End Cap (cubic meters) | Incremental Chambers (cubic meters) | Incremental End Cap (cubic meters) | Incremental Stone (cubic meters) | Incremental Ch, EC and Stone (cubic meters) | Cumulative System (cubic meters) | Elevation (meters) |
|-----------------------|---|---|-------------------------------------|------------------------------------|----------------------------------|---|----------------------------------|--------------------|
| 1676                  | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 15.002                           | 15.00                                       | 1530.15                          | 65.22              |
| 1651                  | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 15.002                           | 15.00                                       | 1515.15                          | 65.20              |
| 1626                  | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 15.002                           | 15.00                                       | 1500.14                          | 65.17              |
| 1600                  | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 15.002                           | 15.00                                       | 1485.14                          | 65.15              |
| 1575                  | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 15.002                           | 15.00                                       | 1470.14                          | 65.12              |
| 1549                  | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 15.002                           | 15.00                                       | 1455.14                          | 65.10              |
| 1524                  | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 15.002                           | 15.00                                       | 1440.14                          | 65.07              |
| 1499                  | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 15.002                           | 15.00                                       | 1425.13                          | 65.05              |
| 1473                  | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 15.002                           | 15.00                                       | 1410.13                          | 65.02              |
| 1448                  | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 15.002                           | 15.00                                       | 1395.13                          | 64.99              |
| 1422                  | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 15.002                           | 15.00                                       | 1380.13                          | 64.97              |
| 1397                  | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 15.002                           | 15.00                                       | 1365.13                          | 64.94              |
| 1372                  | 0.00                                      | 0.00                                      | 0.47                                | 0.00                               | 14.815                           | 15.28                                       | 1350.12                          | 64.92              |
| 1346                  | 0.01                                      | 0.00                                      | 1.57                                | 0.02                               | 14.367                           | 15.95                                       | 1334.84                          | 64.89              |
| 1321                  | 0.01                                      | 0.00                                      | 2.37                                | 0.03                               | 14.040                           | 16.44                                       | 1318.89                          | 64.87              |
| 1295                  | 0.01                                      | 0.00                                      | 3.26                                | 0.04                               | 13.682                           | 16.98                                       | 1302.44                          | 64.84              |
| 1270                  | 0.02                                      | 0.00                                      | 5.55                                | 0.06                               | 12.761                           | 18.36                                       | 1285.46                          | 64.82              |
| 1245                  | 0.03                                      | 0.00                                      | 8.30                                | 0.07                               | 11.653                           | 20.03                                       | 1267.10                          | 64.79              |
| 1219                  | 0.04                                      | 0.00                                      | 10.08                               | 0.09                               | 10.932                           | 21.11                                       | 1247.07                          | 64.77              |
| 1194                  | 0.04                                      | 0.00                                      | 11.48                               | 0.11                               | 10.368                           | 21.95                                       | 1225.96                          | 64.74              |
| 1168                  | 0.04                                      | 0.00                                      | 12.70                               | 0.12                               | 9.875                            | 22.69                                       | 1204.01                          | 64.72              |
| 1143                  | 0.05                                      | 0.00                                      | 13.78                               | 0.14                               | 9.436                            | 23.35                                       | 1181.32                          | 64.69              |
| 1118                  | 0.05                                      | 0.01                                      | 14.76                               | 0.15                               | 9.038                            | 23.95                                       | 1157.96                          | 64.66              |
| 1092                  | 0.05                                      | 0.01                                      | 15.64                               | 0.17                               | 8.679                            | 24.49                                       | 1134.02                          | 64.64              |
| 1067                  | 0.06                                      | 0.01                                      | 16.47                               | 0.19                               | 8.340                            | 25.00                                       | 1109.53                          | 64.61              |
| 1041                  | 0.06                                      | 0.01                                      | 17.23                               | 0.20                               | 8.031                            | 25.46                                       | 1084.53                          | 64.59              |
| 1016                  | 0.06                                      | 0.01                                      | 17.95                               | 0.21                               | 7.737                            | 25.90                                       | 1059.07                          | 64.56              |
| 991                   | 0.07                                      | 0.01                                      | 18.62                               | 0.23                               | 7.465                            | 26.31                                       | 1033.17                          | 64.54              |
| 965                   | 0.07                                      | 0.01                                      | 19.25                               | 0.24                               | 7.209                            | 26.69                                       | 1006.87                          | 64.51              |
| 940                   | 0.07                                      | 0.01                                      | 19.85                               | 0.25                               | 6.964                            | 27.06                                       | 980.17                           | 64.49              |
| 914                   | 0.07                                      | 0.01                                      | 20.40                               | 0.26                               | 6.736                            | 27.40                                       | 953.11                           | 64.46              |
| 889                   | 0.07                                      | 0.01                                      | 20.93                               | 0.27                               | 6.520                            | 27.73                                       | 925.71                           | 64.44              |
| 864                   | 0.08                                      | 0.01                                      | 21.44                               | 0.28                               | 6.314                            | 28.03                                       | 897.99                           | 64.41              |
| 838                   | 0.08                                      | 0.01                                      | 21.91                               | 0.29                               | 6.119                            | 28.33                                       | 869.95                           | 64.39              |
| 813                   | 0.08                                      | 0.01                                      | 22.37                               | 0.31                               | 5.934                            | 28.60                                       | 841.63                           | 64.36              |
| 787                   | 0.08                                      | 0.01                                      | 22.80                               | 0.32                               | 5.757                            | 28.87                                       | 813.02                           | 64.33              |
| 762                   | 0.08                                      | 0.01                                      | 23.21                               | 0.33                               | 5.589                            | 29.12                                       | 784.15                           | 64.31              |
| 737                   | 0.08                                      | 0.01                                      | 23.60                               | 0.34                               | 5.428                            | 29.36                                       | 755.03                           | 64.28              |
| 711                   | 0.08                                      | 0.01                                      | 23.97                               | 0.35                               | 5.276                            | 29.59                                       | 725.67                           | 64.26              |
| 686                   | 0.09                                      | 0.01                                      | 24.31                               | 0.36                               | 5.135                            | 29.80                                       | 696.08                           | 64.23              |
| 660                   | 0.09                                      | 0.01                                      | 24.64                               | 0.36                               | 5.000                            | 30.01                                       | 666.28                           | 64.21              |
| 635                   | 0.09                                      | 0.01                                      | 24.97                               | 0.37                               | 4.864                            | 30.21                                       | 636.27                           | 64.18              |
| 610                   | 0.09                                      | 0.01                                      | 25.26                               | 0.38                               | 4.743                            | 30.39                                       | 606.06                           | 64.16              |
| 584                   | 0.09                                      | 0.01                                      | 25.55                               | 0.39                               | 4.626                            | 30.57                                       | 575.67                           | 64.13              |
| 559                   | 0.09                                      | 0.01                                      | 25.82                               | 0.40                               | 4.514                            | 30.73                                       | 545.10                           | 64.11              |
| 533                   | 0.09                                      | 0.01                                      | 26.08                               | 0.41                               | 4.408                            | 30.89                                       | 514.37                           | 64.08              |
| 508                   | 0.09                                      | 0.01                                      | 26.32                               | 0.42                               | 4.308                            | 31.04                                       | 483.48                           | 64.06              |
| 483                   | 0.09                                      | 0.01                                      | 26.55                               | 0.42                               | 4.211                            | 31.19                                       | 452.43                           | 64.03              |
| 457                   | 0.09                                      | 0.01                                      | 26.78                               | 0.43                               | 4.119                            | 31.33                                       | 421.25                           | 64.00              |
| 432                   | 0.09                                      | 0.01                                      | 26.99                               | 0.44                               | 4.032                            | 31.46                                       | 389.92                           | 63.98              |
| 406                   | 0.10                                      | 0.01                                      | 27.19                               | 0.44                               | 3.950                            | 31.58                                       | 358.46                           | 63.95              |
| 381                   | 0.10                                      | 0.01                                      | 27.38                               | 0.45                               | 3.871                            | 31.70                                       | 326.88                           | 63.93              |
| 356                   | 0.10                                      | 0.02                                      | 27.56                               | 0.46                               | 3.797                            | 31.81                                       | 295.18                           | 63.90              |
| 330                   | 0.10                                      | 0.02                                      | 27.74                               | 0.46                               | 3.722                            | 31.92                                       | 263.37                           | 63.88              |
| 305                   | 0.10                                      | 0.02                                      | 27.91                               | 0.47                               | 3.653                            | 32.03                                       | 231.45                           | 63.85              |
| 279                   | 0.10                                      | 0.02                                      | 28.07                               | 0.47                               | 3.584                            | 32.13                                       | 199.43                           | 63.83              |
| 254                   | 0.10                                      | 0.02                                      | 28.29                               | 0.51                               | 3.485                            | 32.28                                       | 167.30                           | 63.80              |
| 229                   | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 15.002                           | 15.00                                       | 135.02                           | 63.78              |
| 203                   | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 15.002                           | 15.00                                       | 120.02                           | 63.75              |
| 178                   | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 15.002                           | 15.00                                       | 105.01                           | 63.72              |
| 152                   | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 15.002                           | 15.00                                       | 90.01                            | 63.70              |
| 127                   | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 15.002                           | 15.00                                       | 75.01                            | 63.67              |
| 102                   | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 15.002                           | 15.00                                       | 60.01                            | 63.65              |
| 76                    | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 15.002                           | 15.00                                       | 45.01                            | 63.62              |
| 51                    | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 15.002                           | 15.00                                       | 30.00                            | 63.60              |
| 25                    | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 15.002                           | 15.00                                       | 15.00                            | 63.57              |



Chamber Model -  
 Units -  
 Number of Chambers -  
 Number of End Caps -  
 Voids in the stone (porosity) -  
 Base of Stone Elevation -  
 Amount of Stone Above Chambers -  
 Amount of Stone Below Chambers -  
 Area of system -

|               |   |   |                    |
|---------------|---|---|--------------------|
| MC-3500       |   |   |                    |
| <b>Metric</b> | <a href="#">Click Here for Imperial</a> |   |                    |
| 354           |   |   |                    |
| 38            |   |   |                    |
| 40            |   |   |                    |
| 40            | %                                       |   |                    |
| 63.15         | m                                       |   |                    |
| 305           | mm                                      | <input checked="" type="checkbox"/> Include Perimeter Stone in Calculations |                    |
| 229           | mm                                      |   |                    |
| 1841.8        | sq.meters                               | Min. Area -   | 1748.581 sq.meters |

**StormTech MC-3500 Cumulative Storage Volumes**

| Height of System (mm) | Incremental Single Chamber (cubic meters) | Incremental Single End Cap (cubic meters) | Incremental Chambers (cubic meters) | Incremental End Cap (cubic meters) | Incremental Stone (cubic meters) | Incremental Chamber, End Cap and Stone (cubic meters) | Cumulative System (cubic meters) | Elevation (meters) |
|-----------------------|---|---|-------------------------------------|------------------------------------|----------------------------------|---|----------------------------------|--------------------|
| 1676                  | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 18.703                           | 18.70   | 1905.36                          | 64.83              |
| 1651                  | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 18.703                           | 18.70   | 1886.65                          | 64.80              |
| 1626                  | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 18.703                           | 18.70   | 1867.95                          | 64.78              |
| 1600                  | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 18.703                           | 18.70   | 1849.25                          | 64.75              |
| 1575                  | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 18.703                           | 18.70   | 1830.54                          | 64.73              |
| 1549                  | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 18.703                           | 18.70   | 1811.84                          | 64.70              |
| 1524                  | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 18.703                           | 18.70   | 1793.14                          | 64.68              |
| 1499                  | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 18.703                           | 18.70   | 1774.43                          | 64.65              |
| 1473                  | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 18.703                           | 18.70   | 1755.73                          | 64.63              |
| 1448                  | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 18.703                           | 18.70   | 1737.03                          | 64.60              |
| 1422                  | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 18.703                           | 18.70   | 1718.32                          | 64.57              |
| 1397                  | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 18.703                           | 18.70   | 1699.62                          | 64.55              |
| 1372                  | 0.00                                      | 0.00                                      | 0.58                                | 0.00                               | 18.470                           | 19.05   | 1680.92                          | 64.52              |
| 1346                  | 0.01                                      | 0.00                                      | 1.95                                | 0.03                               | 17.915                           | 19.89   | 1661.86                          | 64.50              |
| 1321                  | 0.01                                      | 0.00                                      | 2.95                                | 0.04                               | 17.508                           | 20.50   | 1641.98                          | 64.47              |
| 1295                  | 0.01                                      | 0.00                                      | 4.05                                | 0.06                               | 17.063                           | 21.16   | 1621.48                          | 64.45              |
| 1270                  | 0.02                                      | 0.00                                      | 6.89                                | 0.07                               | 15.919                           | 22.88   | 1600.32                          | 64.42              |
| 1245                  | 0.03                                      | 0.00                                      | 10.31                               | 0.09                               | 14.542                           | 24.94   | 1577.44                          | 64.40              |
| 1219                  | 0.04                                      | 0.00                                      | 12.53                               | 0.12                               | 13.647                           | 26.29   | 1552.49                          | 64.37              |
| 1194                  | 0.04                                      | 0.00                                      | 14.26                               | 0.14                               | 12.946                           | 27.34   | 1526.20                          | 64.35              |
| 1168                  | 0.04                                      | 0.00                                      | 15.77                               | 0.16                               | 12.333                           | 28.26   | 1498.87                          | 64.32              |
| 1143                  | 0.05                                      | 0.00                                      | 17.11                               | 0.18                               | 11.788                           | 29.08   | 1470.61                          | 64.30              |
| 1118                  | 0.05                                      | 0.01                                      | 18.33                               | 0.20                               | 11.293                           | 29.82   | 1441.53                          | 64.27              |
| 1092                  | 0.05                                      | 0.01                                      | 19.42                               | 0.22                               | 10.847                           | 30.49   | 1411.71                          | 64.24              |
| 1067                  | 0.06                                      | 0.01                                      | 20.46                               | 0.23                               | 10.426                           | 31.12   | 1381.23                          | 64.22              |
| 1041                  | 0.06                                      | 0.01                                      | 21.40                               | 0.25                               | 10.043                           | 31.69   | 1350.11                          | 64.19              |
| 1016                  | 0.06                                      | 0.01                                      | 22.30                               | 0.27                               | 9.677                            | 32.24   | 1318.41                          | 64.17              |
| 991                   | 0.07                                      | 0.01                                      | 23.12                               | 0.29                               | 9.339                            | 32.75   | 1286.17                          | 64.14              |
| 965                   | 0.07                                      | 0.01                                      | 23.91                               | 0.30                               | 9.021                            | 33.23   | 1253.42                          | 64.12              |
| 940                   | 0.07                                      | 0.01                                      | 24.65                               | 0.32                               | 8.717                            | 33.68   | 1220.19                          | 64.09              |
| 914                   | 0.07                                      | 0.01                                      | 25.34                               | 0.33                               | 8.434                            | 34.11   | 1186.51                          | 64.07              |
| 889                   | 0.07                                      | 0.01                                      | 26.00                               | 0.35                               | 8.165                            | 34.51   | 1152.40                          | 64.04              |
| 864                   | 0.08                                      | 0.01                                      | 26.62                               | 0.36                               | 7.909                            | 34.89   | 1117.89                          | 64.02              |
| 838                   | 0.08                                      | 0.01                                      | 27.22                               | 0.37                               | 7.667                            | 35.26   | 1083.00                          | 63.99              |
| 813                   | 0.08                                      | 0.01                                      | 27.78                               | 0.39                               | 7.436                            | 35.60   | 1047.74                          | 63.96              |
| 787                   | 0.08                                      | 0.01                                      | 28.32                               | 0.40                               | 7.217                            | 35.93   | 1012.14                          | 63.94              |
| 762                   | 0.08                                      | 0.01                                      | 28.82                               | 0.41                               | 7.008                            | 36.25   | 976.20                           | 63.91              |
| 737                   | 0.08                                      | 0.01                                      | 29.31                               | 0.43                               | 6.808                            | 36.55   | 939.96                           | 63.89              |
| 711                   | 0.08                                      | 0.01                                      | 29.77                               | 0.44                               | 6.619                            | 36.83   | 903.41                           | 63.86              |
| 686                   | 0.09                                      | 0.01                                      | 30.20                               | 0.45                               | 6.444                            | 37.09   | 866.58                           | 63.84              |
| 660                   | 0.09                                      | 0.01                                      | 30.61                               | 0.46                               | 6.276                            | 37.34   | 829.49                           | 63.81              |
| 635                   | 0.09                                      | 0.01                                      | 31.02                               | 0.47                               | 6.107                            | 37.60   | 792.15                           | 63.79              |
| 610                   | 0.09                                      | 0.01                                      | 31.38                               | 0.49                               | 5.957                            | 37.82   | 754.55                           | 63.76              |
| 584                   | 0.09                                      | 0.01                                      | 31.73                               | 0.50                               | 5.812                            | 38.04   | 716.72                           | 63.74              |
| 559                   | 0.09                                      | 0.01                                      | 32.07                               | 0.51                               | 5.672                            | 38.25   | 678.68                           | 63.71              |
| 533                   | 0.09                                      | 0.01                                      | 32.39                               | 0.52                               | 5.541                            | 38.45   | 640.43                           | 63.69              |
| 508                   | 0.09                                      | 0.01                                      | 32.69                               | 0.53                               | 5.415                            | 38.64   | 601.99                           | 63.66              |
| 483                   | 0.09                                      | 0.01                                      | 32.98                               | 0.54                               | 5.296                            | 38.81   | 563.35                           | 63.63              |
| 457                   | 0.09                                      | 0.01                                      | 33.26                               | 0.54                               | 5.181                            | 38.99   | 524.54                           | 63.61              |
| 432                   | 0.09                                      | 0.01                                      | 33.52                               | 0.55                               | 5.073                            | 39.15   | 485.55                           | 63.58              |
| 406                   | 0.10                                      | 0.01                                      | 33.77                               | 0.56                               | 4.971                            | 39.30   | 446.40                           | 63.56              |
| 381                   | 0.10                                      | 0.01                                      | 34.01                               | 0.57                               | 4.872                            | 39.45   | 407.10                           | 63.53              |
| 356                   | 0.10                                      | 0.02                                      | 34.23                               | 0.58                               | 4.781                            | 39.59   | 367.65                           | 63.51              |
| 330                   | 0.10                                      | 0.02                                      | 34.45                               | 0.58                               | 4.688                            | 39.73   | 328.06                           | 63.48              |
| 305                   | 0.10                                      | 0.02                                      | 34.66                               | 0.59                               | 4.602                            | 39.85   | 288.34                           | 63.46              |
| 279                   | 0.10                                      | 0.02                                      | 34.87                               | 0.60                               | 4.516                            | 39.98   | 248.48                           | 63.43              |
| 254                   | 0.10                                      | 0.02                                      | 35.14                               | 0.64                               | 4.393                            | 40.17   | 208.50                           | 63.41              |
| 229                   | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 18.703                           | 18.70   | 168.33                           | 63.38              |
| 203                   | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 18.703                           | 18.70   | 149.63                           | 63.36              |
| 178                   | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 18.703                           | 18.70   | 130.92                           | 63.33              |
| 152                   | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 18.703                           | 18.70   | 112.22                           | 63.30              |
| 127                   | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 18.703                           | 18.70   | 93.52                            | 63.28              |
| 102                   | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 18.703                           | 18.70   | 74.81                            | 63.25              |
| 76                    | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 18.703                           | 18.70   | 56.11                            | 63.23              |
| 51                    | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 18.703                           | 18.70   | 37.41                            | 63.20              |
| 25                    | 0.00                                      | 0.00                                      | 0.00                                | 0.00                               | 18.703                           | 18.70   | 18.70                            | 63.18              |

# STORMTECH MC-3500 CHAMBER

Designed to meet the most stringent industry performance standards for superior structural integrity while providing designers with a cost-effective method to save valuable land and protect water resources. The StormTech system is designed primarily to be used under parking lots, thus maximizing land usage for private (commercial) and public applications. StormTech chambers can also be used in conjunction with Green Infrastructure, thus enhancing the performance and extending the service life of these practices.

## STORMTECH MC-3500 CHAMBER (not to scale)

### Nominal Chamber Specifications

**Size (L x W x H)**  
90" x 77" x 45"  
2,286 mm x 1,956 mm x 1,143 mm

**Chamber Storage**  
109.9 ft<sup>3</sup> (3.11 m<sup>3</sup>)

**Min. Installed Storage\***  
175.0 ft<sup>3</sup> (4.96 m<sup>3</sup>)

**Weight**  
134 lbs (60.8 kg)

**Shipping**  
15 chambers/pallet  
7 end caps/pallet  
7 pallets/truck

\*Assumes a minimum of 12" (300 mm) of stone above, 9" (230 mm) of stone below chambers, 6" (150 mm) of stone between chambers/end caps and 40% stone porosity.

## STORMTECH MC-3500 END CAP (not to scale)

### Nominal End Cap Specifications

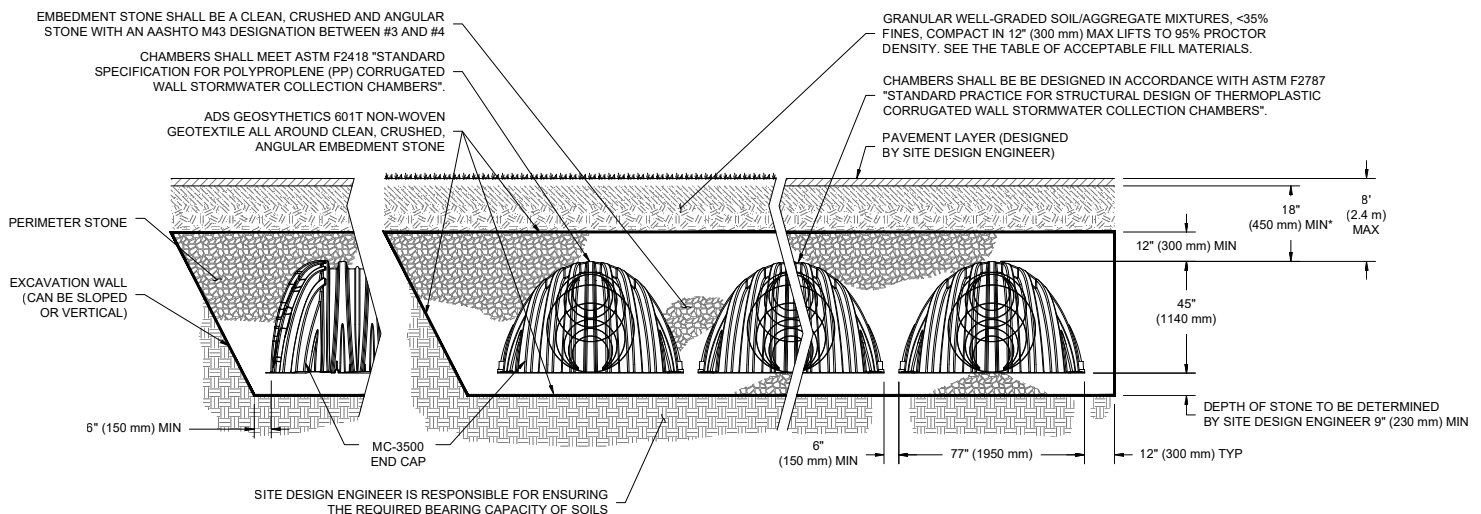
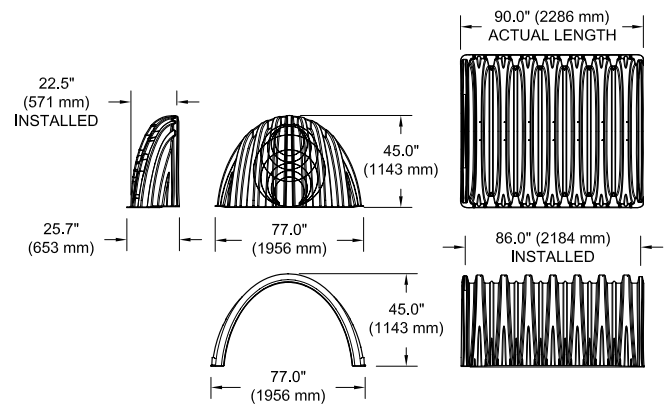
**Size (L x W x H)**  
26.5" x 71" x 45.1"  
673 mm x 1,803 mm x 1,145 mm

**End Cap Storage**  
14.9 ft<sup>3</sup> (0.42 m<sup>3</sup>)

**Min. Installed Storage\***  
45.1 ft<sup>3</sup> (1.28 m<sup>3</sup>)

**Weight**  
49 lbs (22.2 kg)

\*Assumes a minimum of 12" (300 mm) of stone above, 9" (230 mm) of stone below, 6" (150 mm) of stone between chambers, 6" (150 mm) of stone between chambers/end caps and 40% stone porosity.



\*MINIMUM COVER TO BOTTOM OF FLEXIBLE PAVEMENT. FOR UNPAVED INSTALLATIONS WHERE RUTTING FROM VEHICLES MAY OCCUR, INCREASE COVER TO 24" (600 mm).

## MC-3500 CHAMBER SPECIFICATION

### STORAGE VOLUME PER CHAMBER FT<sup>3</sup> (M<sup>3</sup>)

|                 | Bare Chamber Storage ft <sup>3</sup> (m <sup>3</sup> ) | Chamber and Stone Foundation Depth in. (mm) |              |              |              |
|-----------------|--|---|--------------|--------------|--------------|
|                 |  | 9" (230 mm)                                 | 12" (300 mm) | 15" (375 mm) | 18" (450 mm) |
| MC-3500 Chamber | 109.9 (3.11)   | 175.0 (4.96)                                | 179.9 (5.09) | 184.9 (5.24) | 189.9 (5.38) |
| MC-3500 End Cap | 14.9 (.42)   | 45.1 (1.28)                                 | 46.6 (1.32)  | 48.3 (1.37)  | 49.9 (1.41)  |

**Note:** Assumes 6" (150 mm) row spacing, 40% stone porosity, 12" (300 mm) stone above and includes the bare chamber/end cap volume.

### AMOUNT OF STONE PER CHAMBER

| ENGLISH TONS (yds <sup>3</sup> )   | Stone Foundation Depth |            |            |            |
|------------------------------------|------------------------|------------|------------|------------|
|                                    | 9"                     | 12"        | 15"        | 18"        |
| MC-3500 Chamber                    | 8.5 (6.0)              | 9.1 (6.5)  | 9.7 (6.9)  | 10.4 (7.4) |
| MC-3500 End Cap                    | 3.9 (2.8)              | 4.1 (2.9)  | 4.3 (3.1)  | 4.5 (3.2)  |
| METRIC KILOGRAMS (m <sup>3</sup> ) | 230 mm                 | 300 mm     | 375 mm     | 450 mm     |
| MC-3500 Chamber                    | 7711 (4.6)             | 8255 (5.0) | 8800 (5.3) | 9435 (5.7) |
| MC-3500 End Cap                    | 3538 (2.1)             | 3719 (2.2) | 3901 (2.4) | 4082 (2.5) |

**Note:** Assumes 12" (300 mm) of stone above and 6" (150 mm) row spacing and 6" (150 mm) of perimeter stone in front of end caps.

### VOLUME EXCAVATION PER CHAMBER YD<sup>3</sup> (M<sup>3</sup>)

|                 | Stone Foundation Depth |              |             |              |
|-----------------|------------------------|--------------|-------------|--------------|
|                 | 9" (230 mm)            | 12" (300 mm) | 15" (375mm) | 18" (450 mm) |
| MC-3500 Chamber | 11.9 (9.1)             | 12.4 (9.5)   | 12.8(9.8)   | 13.3 (10.2)  |
| MC-3500 End Cap | 4.0 (3.1)              | 4.1 (3.2)    | 4.3 (3.3)   | 4.4 (3.4)    |

**Note:** Assumes 6" (150 mm) of separation between chamber rows and 24" (600 mm) of cover. The volume of excavation will vary as depth of cover increases.



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 and utilize the StormTech Design Tool

For more information on the StormTech MC-3500 Chamber and other ADS products, please contact our Customer Service Representatives at 1-800-821-6710

# Verification Statement



## StormTech Isolator® Row PLUS Registration number: (V-2020-10-01) Date of issue: (2020-October-27)

|                        |  |                              |
|------------------------|--|------------------------------|
| <b>Technology type</b> | Stormwater Filtration Device   |                              |
| <b>Application</b>     | Stormwater filtration technology to remove sediments, nutrients, heavy metals, and organic contaminants from stormwater runoff |                              |
| <b>Company</b>         | StormTech, LLC.  |                              |
| <b>Address</b>         | 520 Cromwell Avenue, Rocky Hill,<br>CT 06067 USA   | <b>Phone</b> +1-888-892-2694 |
| <b>Website</b>         | www.stormtech.com  |                              |
| <b>E-mail</b>          | info@stormtech.com   |                              |

### Verified Performance Claims

The StormTech Isolator® Row PLUS technology was tested at the Mid-Atlantic Storm Water Research Center (MASWRC), under the supervision of Boggs Environmental Consultants, Inc. The performance test results for two overlapping StormTech Isolator® Row PLUS chambers (commercial unit model SC-740) were verified by Good Harbour Laboratories Inc. (GHL), following the requirements of ISO 14034:2016 and the VerifiGlobal Performance Verification Protocol. Based on the laboratory testing conducted, the verified performance claims are as follows:

**Total Suspended Solids (TSS) Removal Efficiency** - The StormTech Isolator® Row PLUS achieved  $82\% \pm 1\%$  removal efficiency of suspended sediment concentration (SCC) at a 95% confidence level.

**Average Loading Rate** - Based on the reported flow rate data and the effective sedimentation and filtration treatment area of the test unit, the average loading rate of the test unit was  $4.15 \pm 0.03$  GPM/ft<sup>2</sup> at a 95% confidence level.

**Maximum Treatment Flow Rate (MTFR)** - Although the MTFR varies among the StormTech Isolator® Row PLUS model sizes and the number of chambers, the design surface loading rate remains the same (4.13 gpm/ ft<sup>2</sup> of treatment surface area). The test unit consisted of two overlapping StormTech SC-740 chambers with a nominal MTFR of 225 GPM (0.501 CFS) and an effective filtration treatment area (EFTA) of approximately 54.5 ft<sup>2</sup>.

**Detention Time and Volume** - The StormTech Isolator Row PLUS detention time and wet volume varies with model size. The unit tested had a wet volume of approximately 65.1 ft<sup>3</sup> and a detention time of 2.2 minutes.

**Maximum Sediment Storage Depth and Volume** - The sediment storage volume and depth vary according to the StormTech Isolator® Row PLUS model sizes and system configuration. For the two overlapping StormTech SC-740 chambers tested, the maximum sediment storage volume is 2.3 ft<sup>3</sup> at a sediment depth of 0.5 inches.

**Effective Sedimentation/Filtration Treatment Areas** - The Effective Sedimentation Area (ESA) and the Effective Filtration Treatment Area (EFTA) increase as the size of the system increases. For the two overlapping StormTech SC-740 chambers tested, the ESA and the ratio of ESA/EFTA were 54.5 ft<sup>2</sup> and 1.0, respectively.

**Sediment Mass Load Capacity** - The sediment mass load capacity varies according to the StormTech Isolator® Row PLUS model sizes and system configuration. For the two overlapping StormTech SC-740 chambers tested, the mass loading capture was 158.4 lbs ± 0.8 lbs (2.91 ± 0.01 lbs/ ft<sup>2</sup>) following a total sediment loading of 195.2 lbs.

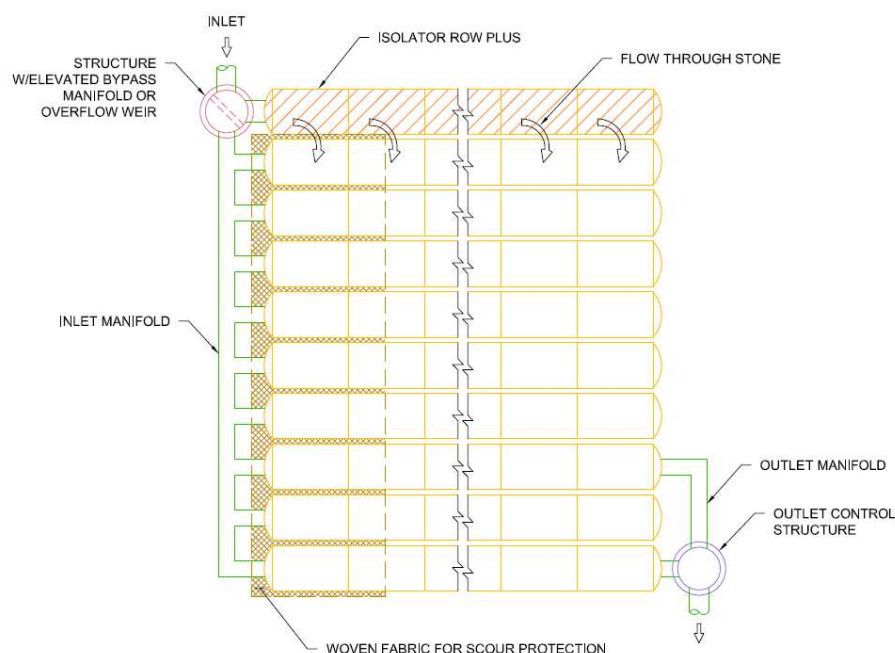
### Technology Application

The StormTech “Isolator® Row PLUS” is a stormwater treatment technology designed for use under parking lots, roadways and heavy earth loads while providing a superior and durable structural system. The technology comprises a row of chambers covered in a non-woven geotextile fabric with a single layer of proprietary woven fabric at the bottom that serves as a filter strip, providing surface area for infiltration and runoff reduction with enhanced suspended solids and pollutant removal. The following features make the Isolator® Row PLUS effective as a water quality solution:

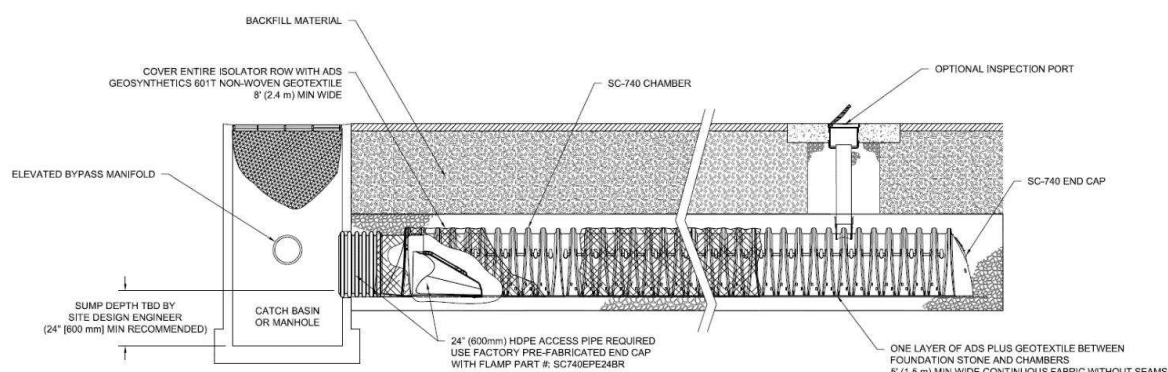
- Enhanced infiltration Surface Area
- Runoff Volume Reduction
- Peak Flow Reduction
- Sediment/Pollutant Removal
- Internal Water Storage (IWS)
- Water Temperature Cooling (Thermal Buffer).

### Technology Description

The Isolator® Row PLUS (shown in Figures 1 and 2) is the first row of StormTech chambers that is surrounded with filter fabric and connected to a closely located manhole for easy access. The Isolator® Row PLUS provides for settling and filtration of sediment as stormwater rises in the chamber and ultimately passes through the filter fabric. The open-bottom chambers allow stormwater to flow out of the chambers, while sediment is captured in the Isolator® Row PLUS.



**Figure 1: Schematic of the StormTech Isolator® Row PLUS System**



**Figure 2: Isolator® Row PLUS Detail**

A single layer of proprietary Advanced Drainage Systems (ADS) PLUS fabric is placed between the angular base stone and the Isolator Row PLUS chamber. The geotextile provides the means for stormwater filtration and provides a durable surface for maintenance operations. A 6 oz. non-woven fabric is placed over the chambers.

The Isolator® Row PLUS is designed to capture the “first flush” and offers the versatility to be sized on a volume basis or a flow-rate basis. An upstream manhole not only provides access to the Isolator® Row PLUS but includes a high low/concept such that stormwater flow rates or volumes that exceed the capacity of the Isolator® Row PLUS bypass through a manifold to the other chambers. This is achieved with either a high-flow weir or an elevated manifold. This creates a differential between the Isolator® Row PLUS and the manifold, thus allowing for settlement time in the Isolator® Row PLUS. After Stormwater flows through the Isolator® Row PLUS and into the rest of the StormTech chamber system it is either infiltrated into the soils below or passed at a controlled rate through an outlet manifold and outlet control structure.

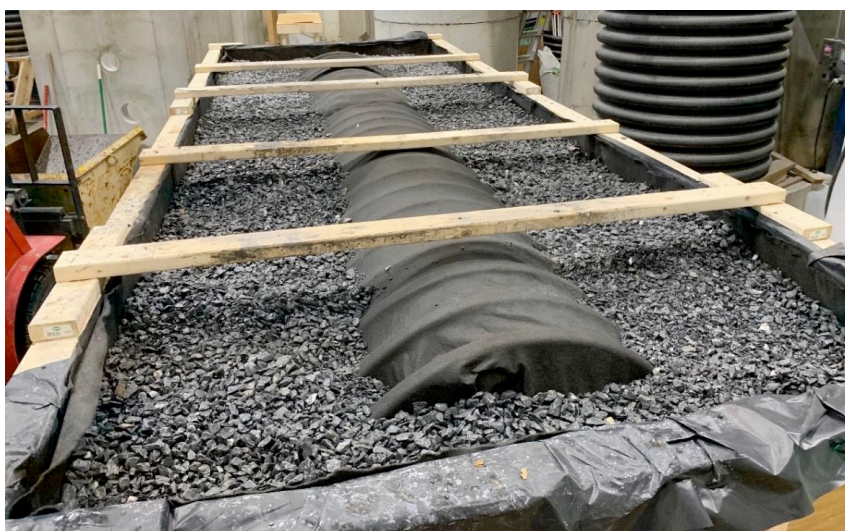
StormTech developed and owns the Isolator® Row PLUS technology and has filed a number of patent applications relating to the Isolator® Row PLUS system.<sup>1</sup>

**Description of Test Procedure for the StormTech Isolator® Row PLUS**

In January 2020, two overlapping StormTech SC-740 Isolator® Row PLUS commercial size chambers were installed at the Mid-Atlantic Storm Water Research Center (MASWRC, a subsidiary of BaySaver), in Mount Airy, Maryland, to evaluate the performance of the Isolator® Row PLUS system for Total Suspended Solid (TSS) removal (Figure 3) All testing and data collection procedures were supervised by Boggs Environmental Consultants, Inc. (BEC), who was hired by ADS for third party oversight, and were in accordance with the *New Jersey Department of Environmental Protection Laboratory Protocol to Assess Total Suspended Solids Removal by a Filtration Manufactured Treatment Device (January 2013)*.

Prior to the start of testing, a Quality Assurance Project Plan (QAPP), revision dated January 09, 2020, was submitted and approved by the New Jersey Corporation for Advanced Technology (NJCAT), c/o Center for Environmental Systems, Stevens Institute of Technology, Castle Point on Hudson, Hoboken, NJ 07030.

<sup>1</sup> (U.S. Provisional Application No. 62/753,050, filed October 30, 2018; U.S. Non-Provisional Application No. 16/670,628, filed October 31, 2019; International Application No. PCT/US2019/059283, filed October 31, 2019; U.S. Application No. 16/938,482, filed July 24, 2020; U.S. Application No. 16/938,657, filed July 24, 2020; PCT International Application No. PCT/US2020/043543, filed July 24, 2020; PCT International Application No. PCT/US2020/043557, filed July 24, 2020.



**Figure 3: StormTech “Isolator® Row PLUS” Test Set-up at MASWRC**

**Verification Results**

The verification process for the StormTech Isolator® Row PLUS technology was conducted by GHIL in accordance with the VerifiGlobal Verification Plan for the StormTech “Isolator® Row PLUS” Technology – 2020-09-09. The technology performance claims verified by GHIL are summarized at the front of this Verification Statement and in Table 6 on Page 8 under the heading “Verification Summary”.

Particle size distribution analysis was performed by ECS Mid-Atlantic, LLC of Frederick, MD in accordance with ASTM D422-63(2007). ECS is accredited by the American Association of State Highways and Transportation Officials (AASHTO).

ASTM D422-63(2007) is a sieve and hydrometer method where the larger particles, > 75 microns, are measured using a standard sieve stack while the smaller particles are measured based on their settling time using a hydrometer.

The PSD meets the requirements of NJDEP, which is generally accepted as representative of the type of particle sizes an OGS would be designed to treat. Actual PSD is site and rainfall event specific, so it was necessary to choose a standard PSD to make testing and comparison manageable.

Table 1 shows the NJDEP PSD specification. Table 2 and Figure 4 show the incoming material PSD as determined by ECS Mid-Atlantic and confirmed by the verifier.

**Table 1: NJDEP PSD Specification**

| Particle Size (µm) | NJDEP Minimum Specification |
|--------------------|-----------------------------|
| 1000               | 98                          |
| 500                | 93                          |
| 250                | 88                          |
| 150                | 73                          |
| 100                | 58                          |
| 75                 | 48                          |
| 50                 | 43                          |
| 20                 | 33                          |
| 8                  | 18                          |
| 5                  | 8                           |
| 2                  | 3                           |
| d <sub>50</sub>    | < 75 µm                     |

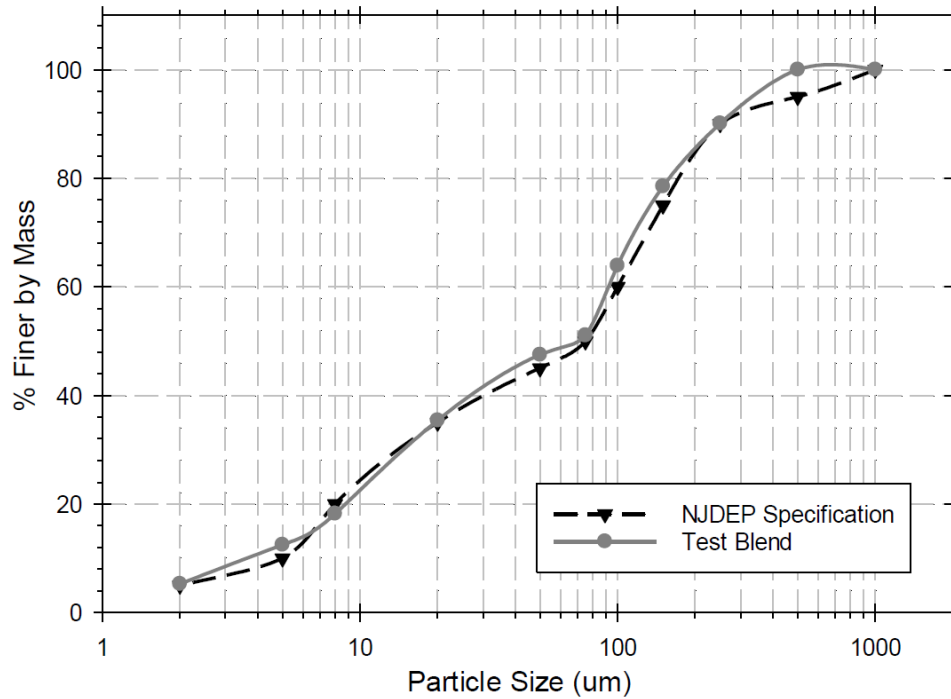


**Table 2 – Particle Size Distribution (PSD) of Test Sediment**

| Mesh (mm) | US Sieve Size     | Sample ID     |       |       |
|-----------|-------------------|---------------|-------|-------|
|           |                   | PSD A         | PSD B | PSD C |
|           |                   | Percent Finer |       |       |
| 9.525     | 0.375             | 100.0         | 100.0 | 100.0 |
| 4.750     | #4                | 100.0         | 100.0 | 100.0 |
| 4.000     | #5                | 100.0         | 100.0 | 100.0 |
| 2.360     | #8                | 100.0         | 100.0 | 100.0 |
| 2.000     | #10               | 100.0         | 100.0 | 100.0 |
| 1.180     | #16               | 100.0         | 100.0 | 100.0 |
| 1.000     | #18               | 100.0         | 100.0 | 100.0 |
| 0.500     | #35               | 100.0         | 100.0 | 100.0 |
| 0.425     | #40               | 93.3          | 93.0  | 93.6  |
| 0.250     | #60               | 90.3          | 89.8  | 90.2  |
| 0.150     | #100              | 79.3          | 78.1  | 78.1  |
| 0.125     | #120              | 73.6          | 71.7  | 71.7  |
| 0.106     | #140              | 68.4          | 65.2  | 64.8  |
| 0.090     | #170              | 60.2          | 58.3  | 57.5  |
| 0.075     | #200              | 52.0          | 50.9  | 50.3  |
| 0.053     | #270              | 48.0          | 48.3  | 47.8  |
| 0.045     | <b>Hydrometer</b> | 46.6          | 46.7  | 46.7  |
| 0.032     |                   | 42.8          | 42.9  | 41.0  |
| 0.021     |                   | 37.1          | 37.2  | 35.3  |
| 0.0125    |                   | 25.7          | 25.7  | 25.8  |
| 0.0090    |                   | 20.1          | 20.1  | 19.2  |
| 0.0064    |                   | 16.3          | 16.4  | 14.5  |
| 0.0032    |                   | 8.8           | 8.7   | 7.8   |
| 0.0014    |                   | 3.8           | 3.7   | 3.8   |

The suspended sediment concentration analysis was completed by Fredericktowne Labs Inc., Meyersville, MD. Fredericktowne Labs is accredited by the Maryland Department of Environment as Maryland Certified Water Quality Laboratory. The analysis procedure was ASTM D3977-97, Suspended Sediment Concentration. The sampling procedure and submission of samples to the test lab were overseen by the independent observer, Boggs Environmental Consultants, Inc.

All test data and calculations were detailed in the report “NJCAT TECHNOLOGY VERIFICATION Isolator® Row PLUS StormTech, LLC”, July 2020, which was submitted to and verified by the New Jersey Corporation for Advanced Technology (NJCAT).



**Figure 4– Particle Size Distribution (PSD)**

The data in Table 3 (Flow Rate and Temperature) and Table 4 (Removal Efficiency) form the basis for the verified technology performance claim, specifically, flow rate, sediment captured and removal efficiency.

**Table 3: Flow Rate and Temperature Summary**

| Run | Max Flow (gpm) | Min Flow (gpm) | Average Flow (gpm) | Flow COV | Flow Compliance (COV < 0.1) | Maximum Temperature (Fahrenheit) | NJDEP Temperature Compliance (< 80 F) |
|-----|----------------|----------------|--------------------|----------|-----------------------------|----------------------------------|---------------------------------------|
| 1   | 232.8          | 223.9          | 226.3              | 0.0078   | Y                           | 48.2                             | Y                                     |
| 2   | 228.9          | 218.6          | 220.8              | 0.0104   | Y                           | 51.5                             | Y                                     |
| 3   | 229.4          | 220.0          | 227.2              | 0.0094   | Y                           | 44.7                             | Y                                     |
| 4   | 230.2          | 218.7          | 223.2              | 0.0138   | Y                           | 40.5                             | Y                                     |
| 5   | 228.7          | 216.9          | 222.2              | 0.0103   | Y                           | 44.7                             | Y                                     |
| 6   | 227.6          | 217.0          | 224.2              | 0.0115   | Y                           | 46.7                             | Y                                     |
| 7   | 229.7          | 221.9          | 226.4              | 0.0092   | Y                           | 44.6                             | Y                                     |
| 8   | 230.3          | 222.2          | 226.8              | 0.0089   | Y                           | 43.5                             | Y                                     |
| 9   | 233.2          | 218.4          | 225.6              | 0.0136   | Y                           | 45.5                             | Y                                     |
| 10  | 232.2          | 219.7          | 228.4              | 0.0126   | Y                           | 44.7                             | Y                                     |
| 11  | 226.9          | 219.2          | 224.1              | 0.0088   | Y                           | 52.4                             | Y                                     |
| 12  | 232.2          | 222.1          | 226.9              | 0.0107   | Y                           | 48.5                             | Y                                     |
| 13  | 234.7          | 221.2          | 226.1              | 0.0109   | Y                           | 48.5                             | Y                                     |
| 14  | 231.9          | 223.4          | 228.7              | 0.0103   | Y                           | 45.6                             | Y                                     |
| 15  | 236.8          | 224.1          | 231.4              | 0.0131   | Y                           | 52.2                             | Y                                     |
| 16  | 232.5          | 221.3          | 229.0              | 0.0137   | Y                           | 47.8                             | Y                                     |

Table 4: Removal Efficiency Results

| Run                                      | Average Influent TSS (mg/L) | Influent Water Volume (gal) | Adjusted Average Effluent TSS (mg/L) | Effluent Water Volume (gal) | Adjusted Average Drain Down TSS (mg/L) | Drain Down Water Volume (gal) | Single Run Removal Efficiency (%) | Mass of Captured Sediment (g) | Cumulative Removal Efficiency (%) |
|--|-----------------------------|-----------------------------|--------------------------------------|-----------------------------|--|-------------------------------|-----------------------------------|-------------------------------|-----------------------------------|
| 1  | 203                         | 7166                        | 46                                   | 6881                        | 34                                     | 285                           | 77.8                              | 4282                          | 77.8                              |
| 2  | 199                         | 6993                        | 32                                   | 6639                        | 27                                     | 354                           | 84.0                              | 4415                          | 80.8                              |
| 3  | 207                         | 7197                        | 37                                   | 6793                        | 27                                     | 403                           | 82.6                              | 4654                          | 81.4                              |
| 4  | 217                         | 7068                        | 33                                   | 6635                        | 29                                     | 433                           | 84.9                              | 4923                          | 82.3                              |
| 5  | 215                         | 7037                        | 39                                   | 6593                        | 29                                     | 444                           | 82.2                              | 4705                          | 82.3                              |
| 6  | 207                         | 7097                        | 40                                   | 6643                        | 31                                     | 454                           | 81.2                              | 4504                          | 82.1                              |
| 7  | 198                         | 7169                        | 37                                   | 6693                        | 30                                     | 476                           | 81.6                              | 4386                          | 82.0                              |
| 8  | 201                         | 7184                        | 37                                   | 6716                        | 32                                     | 468                           | 81.6                              | 4473                          | 82.0                              |
| 9  | 205                         | 7147                        | 38                                   | 6675                        | 30                                     | 472                           | 81.8                              | 4539                          | 82.0                              |
| 10                                       | 203                         | 7235                        | 38                                   | 6759                        | 31                                     | 476                           | 81.4                              | 4523                          | 81.9                              |
| 11                                       | 208                         | 7096                        | 38                                   | 6624                        | 30                                     | 472                           | 81.8                              | 4567                          | 81.9                              |
| 12                                       | 209                         | 7185                        | 41                                   | 6709                        | 30                                     | 476                           | 80.7                              | 4584                          | 81.8                              |
| 13                                       | 198                         | 7162                        | 41                                   | 6680                        | 32                                     | 482                           | 79.7                              | 4277                          | 81.6                              |
| 14                                       | 200                         | 7242                        | 43                                   | 6757                        | 34                                     | 485                           | 78.8                              | 4318                          | 81.4                              |
| 15                                       | 196                         | 7329                        | 41                                   | 6842                        | 32                                     | 487                           | 79.5                              | 4320                          | 81.3                              |
| 16                                       | 202                         | 7254                        | 44                                   | 6769                        | 31                                     | 485                           | 78.9                              | 4384                          | 81.2                              |
| <b>Avg.</b>                              | <b>204.2</b>                | <b>7160</b>                 | <b>39</b>                            | <b>6713</b>                 | <b>31</b>                              | <b>447</b>                    | <b>81.2</b>                       | <b>4491</b>                   | <b>N/A</b>                        |
| <b>Cumulative Mass Removed (g)</b>       |                             |                             |                                      |                             |  |                               | <b>71854</b>                      |                               |                                   |
| <b>Cumulative Mass Removed (lb)</b>      |                             |                             |                                      |                             |  |                               | <b>158.4</b>                      |                               |                                   |
| <b>Total Mass Loaded (lb)</b>            |                             |                             |                                      |                             |  |                               | <b>195.2</b>                      |                               |                                   |
| <b>Cumulative Removal Efficiency (%)</b> |                             |                             |                                      |                             |  |                               | <b>81.2</b>                       |                               |                                   |

**Quality Assurance**

Performance verification of the StormTech Isolator® Row PLUS technology was performed in accordance with the requirements of ISO 14034:2016 and the VerifiGlobal Performance Verification Protocol. This included reviewing all data sheets and calculated values, as well as overall management of the test system, quality control and data integrity.

Additional information on quality control measures taken can be found in section 5 of the QAPP for StormTech Isolator Row New Jersey Department of Environmental Protection Testing, Rev. 1/9/2020.

Specific QA/QC measures reviewed by the verifier are summarized in Table 5 below.

Table 5. Validation of QA/QC Procedures

| QC Parameter   | Acceptance Criteria  |
|--|--|
| Independence of observer                               | Confirmed in letter from Boggs Environmental Consultants, Inc. to NJCAT  |
| Consistency of procedure                               | Daily logs confirm proper procedure  |
| Existence of QAPP                                      | Confirmed. "QAPP For StormTech Isolator Row New Jersey Department of Environmental Protection Testing", Rev. 1/9/2020)                                     |
| Use of appropriate sample analysis method – ASTM D3799 | Confirmed by method reference on lab reports from Fredericktowne Labs Inc.   |
| Test method appropriate for the technology             | Used industry stakeholder approved protocol: <i>New Jersey Department of Environmental Protection Laboratory Protocol to Assess Total Suspended Solids</i> |

|   |  |
|---|--|
|   | <i>Removal by a Filtration Manufactured Treatment Device (January 2013)</i>                      |
| Test parameters stayed within required limits | Confirmed in report “NJCAT TECHNOLOGY VERIFICATION Isolator® Row PLUS StormTech, LLC”, July 2020 |
| Third party verified data                     | All testing was observed and reviewed by Boggs Environmental Consultants, Inc.                   |

**Variance**

Performance claims regarding structural load limitations were not verified as they are outside the scope of the performance testing that was conducted in accordance with the ‘Quality Assurance Project Plan (QAPP) for StormTech Isolator Row, New Jersey Department of Environmental Protection Testing’, revision dated January 09, 2020.

**Verification Summary**

The StormTech “Isolator® Row PLUS” is a stormwater treatment technology designed for use under parking lots, roadways and heavy earth loads while providing a superior and durable structural system. The technology comprises a row of chambers wrapped in woven geotextile fabric with two layers at the bottom that serve as a filter strip, providing surface area for infiltration and runoff reduction with enhanced suspended solids and pollutant removal.

The StormTech Isolator® Row PLUS technology was tested at the Mid-Atlantic Storm Water Research Center (MASWRC), under the supervision of Boggs Environmental Consultants, Inc. The performance test results for two overlapping StormTech Isolator® Row PLUS chambers (commercial unit model SC-740) were verified by Good Harbour Laboratories Inc. (GHL), following the requirements of ISO 14034:2016 and the VerifiGlobal Performance Verification Protocol. Table 6 summarizes the verification results in relation to the technology performance parameters that were identified in the Verification Plan to determine the efficacy of the StormTech Isolator® Row PLUS technology.

**Table 6 - Summary of Verification Results Against Performance Parameters**

| Parameters                                      | Verified Claims  | Accuracy                            |
|---|--|-------------------------------------|
| Total Suspended Solids (TSS) Removal Efficiency | Based on the laboratory testing conducted, the StormTech Isolator® Row PLUS achieved an average 82% removal efficiency of SSC  | ± 1% (95% confidence level)         |
| Average Loading Rate                            | Based on the laboratory testing parameters, the StormTech Isolator® Row PLUS maintained a loading rate of 4.15 GPM/sf  | ±0.03 GPM/sf (95% confidence level) |
| Maximum Treatment Flow Rate (MTFR)              | Although the MTFR varies among the StormTech Isolator® Row PLUS model sizes and the number of chambers, the design surface loading rate remains the same (4.13 GPM/ft <sup>2</sup> of treatment surface area). The test unit consisted of two overlapping StormTech SC-740 chambers with a nominal MTFR of 225 GPM (0.501 CFS) and an effective filtration treatment area (EFTA) of approximately 54.5 ft <sup>2</sup> . | ± 1.4 GPM (95% confidence level)    |
| Detention Time and Volume                       | Detention time and wet volume varies with model size. The unit tested had a wet volume of approximately 65.1 ft <sup>3</sup> (based on   | N/A                                 |

|  |  |   |
|--|--|---|
|  | physical measurement) and a detention time of 2.2 minutes.   |   |
| Maximum Sediment Storage Depth and Volume          | The sediment storage volume and depth vary according to the StormTech Isolator® Row PLUS model sizes and system configuration. For the two overlapping StormTech SC-740 chambers tested, the maximum sediment storage volume is 2.3 ft <sup>3</sup> at a sediment depth of 0.5 inches.                   | N/A   |
| Effective Sedimentation/ Filtration Treatment Area | The effective sedimentation and filtration treatment area increases as the size of the chamber increases. Under the tested conditions using 2 overlapping chambers, the treatment area was 54.5 ft <sup>2</sup>  | The sedimentation /filtration area was determined from the actual physical dimensions of the test unit* |
| Sediment Mass Load Capacity                        | The sediment mass load capacity varies according to the StormTech Isolator® Row PLUS model sizes and system configuration. For the two overlapping StormTech SC-740 chambers tested, the mass loading capture was 158.4 lbs (2.91 lbs/ ft <sup>2</sup> ) following a total sediment loading of 195.2 lbs | ± 0.8 lbs (±0.01 lbs/ft <sup>2</sup> ) (95% confidence level)   |

\*Note: These numbers are determined based on physical measurement or a dimensional drawing, which is standard practice. Highly accurate measurements are not practical.

In conclusion, the StormTech Isolator® Row PLUS is a viable technology that can be used to remove contaminants from stormwater runoff via filtration. This technology has proven effective at removing suspended sediment from stormwater through in-lab testing using an industry recognized laboratory protocol.

By extension of sediment removal, this technology should also remove particle bound nutrients, heavy metals, and a wide variety of organic contaminants. Performance is a function of pollutant properties, hydraulic retention time, filter media, pre-treatment, and flow rate, such that proper design of the system is critical to achieving the desired results.

**What is ISO 14034?**

The purpose of environmental technology verification is to provide a credible and impartial account of the performance of environmental technologies. Environmental technology verification is based on a number of principles to ensure that verifications are performed and reported accurately, clearly, unambiguously and objectively. The International Organization for Standardization (ISO) standard for environmental technology verification (ETV) is ISO 14034, which was published in November 2016.

**Benefits of ETV**

ETV contributes to protection and conservation of the environment by promoting and facilitating market uptake of innovative environmental technologies, especially those that perform better than relevant alternatives. ETV is particularly applicable to those environmental technologies whose innovative features or performance cannot be fully assessed using existing standards. Through the provision of objective evidence, ETV provides an independent and impartial confirmation of the performance of an environmental technology based on reliable test data. ETV aims to strengthen the credibility of new, innovative technologies by supporting informed decision-making among interested parties.

|  |  |
|--|--|
| For more information on the StormTech “Isolator® Row PLUS” technology, contact:  | For more information on VerifiGlobal, contact:   |
| StormTech, LLC.<br>520 Cromwell Avenue, Rocky Hill, CT<br>06067 USA<br>t: +1-888-892-2694<br>e: info@stormtech.com<br>w: www.stormtech.com | VerifiGlobal c/o ETA-Danmark A/S<br>Göteborg Plads 1, DK-2150 Nordhaven<br>t +45 7224 5900<br>e: info@verifiglobal.com<br>w: www.verifiglobal.com  |
| Signed for StormTech:<br><br><i>Original signed by:</i><br><i>Greg Spires</i><br>Greg Spires, P.E.<br>General Manager                      | Signed for VerifiGlobal:<br><br><i>Original signed by:</i><br><i>Thomas Bruun</i><br>Thomas Bruun, Managing Director<br><br><i>Original signed by:</i><br><i>John Neate</i><br>John Neate, Managing Director |

**NOTICE:** Verifications are based on an evaluation of technology performance under specific, predetermined operational conditions and parameters and the appropriate quality assurance procedures. VerifiGlobal and the Verification Expert, Good Harbour Laboratories, make no expressed or implied warranties as to the performance of the technology and do not certify that a technology will always operate as verified. The end user is solely responsible for complying with any and all applicable regulatory requirements. Mention of commercial product names does not imply endorsement.

VerifiGlobal and the Verification Expert, Good Harbour Laboratories, provide the verification services solely on the basis of the information supplied by the applicant or vendor and assume no liability thereafter. The responsibility for the information supplied remains solely with the applicant or vendor and the liability for the purchase, installation, and operation (whether consequential or otherwise) is not transferred to any other party as a result of the verification.

# Isolator<sup>®</sup> Row O&M Manual



## THE ISOLATOR<sup>®</sup> ROW

### INTRODUCTION

An important component of any Stormwater Pollution Prevention Plan is inspection and maintenance. The StormTech Isolator Row is a technique to inexpensively enhance Total Suspended Solids (TSS) removal and provide easy access for inspection and maintenance.

### THE ISOLATOR ROW

The Isolator Row is a row of StormTech chambers, either SC-160LP, SC-310, SC-310-3, SC-740, DC-780, MC-3500 or MC-4500 models, that is surrounded with filter fabric and connected to a closely located manhole for easy access. The fabric-wrapped chambers provide for settling and filtration of sediment as storm water rises in the Isolator Row and ultimately passes through the filter fabric. The open bottom chambers and perforated sidewalls (SC-310, SC-310-3 and SC-740 models) allow storm water to flow both vertically and horizontally out of the chambers. Sediments are captured in the Isolator Row protecting the storage areas of the adjacent stone and chambers from sediment accumulation.

Two different fabrics are used for the Isolator Row. A woven geotextile fabric is placed between the stone and the Isolator Row chambers. The tough geotextile provides a media for storm water filtration and provides a durable surface for maintenance operations. It is also designed to prevent scour of the underlying stone and remain intact during high pressure jetting. A non-woven fabric is placed over the chambers to provide a filter media for flows passing through the perforations in the sidewall of the chamber. The non-woven fabric is not required over the SC-160LP, DC-780, MC-3500 or MC-4500 models as these chambers do not have perforated side walls.

The Isolator Row is typically designed to capture the “first flush” and offers the versatility to be sized on a volume basis or flow rate basis. An upstream manhole not only provides access to the Isolator Row but typically includes a high flow weir such that storm water flowrates or volumes that exceed the capacity of the Isolator Row overtop the overflow weir and discharge through a manifold to the other chambers.

The Isolator Row may also be part of a treatment train. By treating storm water prior to entry into the chamber system, the service life can be extended and pollutants such as hydrocarbons can be captured. Pre-treatment best management practices can be as simple as deep sump catch basins, oil-water separators or can be innovative storm water treatment devices. The design of the treatment train and selection of pretreatment devices by the design engineer is often driven by regulatory requirements. Whether pretreatment is used or not, the Isolator Row is recommended by StormTech as an effective means to minimize maintenance requirements and maintenance costs.

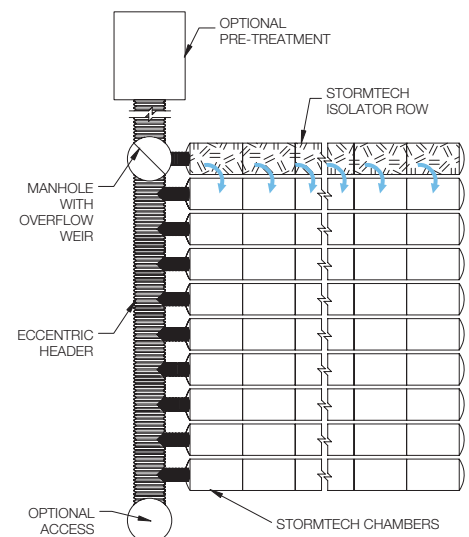
*Note: See the StormTech Design Manual for detailed information on designing inlets for a StormTech system, including the Isolator Row.*



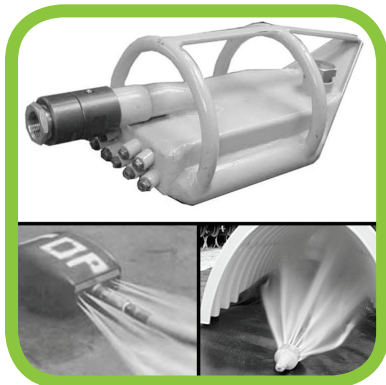
Looking down the Isolator Row from the manhole opening, woven geotextile is shown between the chamber and stone base.



StormTech Isolator Row with Overflow Spillway (not to scale)







## ISOLATOR ROW INSPECTION/MAINTENANCE

### INSPECTION

The frequency of inspection and maintenance varies by location. A routine inspection schedule needs to be established for each individual location based upon site specific variables. The type of land use (i.e. industrial, commercial, residential), anticipated pollutant load, percent imperviousness, climate, etc. all play a critical role in determining the actual frequency of inspection and maintenance practices.

At a minimum, StormTech recommends annual inspections. Initially, the Isolator Row should be inspected every 6 months for the first year of operation. For subsequent years, the inspection should be adjusted based upon previous observation of sediment deposition.

The Isolator Row incorporates a combination of standard manhole(s) and strategically located inspection ports (as needed). The inspection ports allow for easy access to the system from the surface, eliminating the need to perform a confined space entry for inspection purposes.

If upon visual inspection it is found that sediment has accumulated, a stadia rod should be inserted to determine the depth of sediment. When the average depth of sediment exceeds 3 inches throughout the length of the Isolator Row, clean-out should be performed.

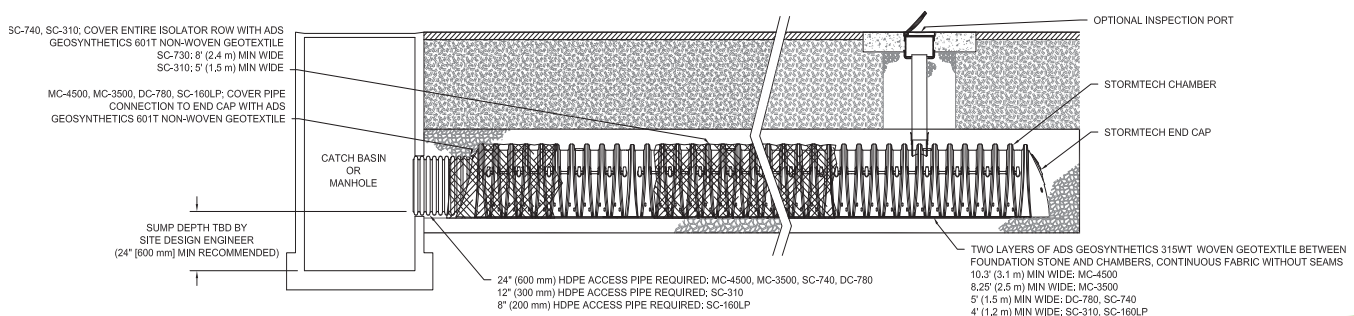
### MAINTENANCE

The Isolator Row was designed to reduce the cost of periodic maintenance. By “isolating” sediments to just one row, costs are dramatically reduced by eliminating the need to clean out each row of the entire storage bed. If inspection indicates the potential need for maintenance, access is provided via a manhole(s) located on the end(s) of the row for cleanout. If entry into the manhole is required, please follow local and OSHA rules for a confined space entries.

Maintenance is accomplished with the JetVac process. The JetVac process utilizes a high pressure water nozzle to propel itself down the Isolator Row while scouring and suspending sediments. As the nozzle is retrieved, the captured pollutants are flushed back into the manhole for vacuuming. Most sewer and pipe maintenance companies have vacuum/JetVac combination vehicles. Selection of an appropriate JetVac nozzle will improve maintenance efficiency. Fixed nozzles designed for culverts or large diameter pipe cleaning are preferable. Rear facing jets with an effective spread of at least 45” are best. Most JetVac reels have 400 feet of hose allowing maintenance of an Isolator Row up to 50 chambers long. **The JetVac process shall only be performed on StormTech Isolator Rows that have AASHTO class 1 woven geotextile (as specified by StormTech) over their angular base stone.**

### StormTech Isolator Row (not to scale)

*Note: Non-woven fabric is only required over the inlet pipe connection into the end cap for SC-160LP, DC-780, MC-3500 and MC-4500 chamber models and is not required over the entire Isolator Row.*



# ISOLATOR ROW STEP BY STEP MAINTENANCE PROCEDURES

## STEP 1

Inspect Isolator Row for sediment.

- A) Inspection ports (if present)
  - i. Remove lid from floor box frame
  - ii. Remove cap from inspection riser
  - iii. Using a flashlight and stadia rod, measure depth of sediment and record results on maintenance log.
  - iv. If sediment is at or above 3 inch depth, proceed to Step 2. If not, proceed to Step 3.
- B) All Isolator Rows
  - i. Remove cover from manhole at upstream end of Isolator Row
  - ii. Using a flashlight, inspect down Isolator Row through outlet pipe
    - 1. Mirrors on poles or cameras may be used to avoid a confined space entry
    - 2. Follow OSHA regulations for confined space entry if entering manhole
  - iii. If sediment is at or above the lower row of sidewall holes (approximately 3 inches), proceed to Step 2. If not, proceed to Step 3.

## STEP 2

Clean out Isolator Row using the JetVac process.

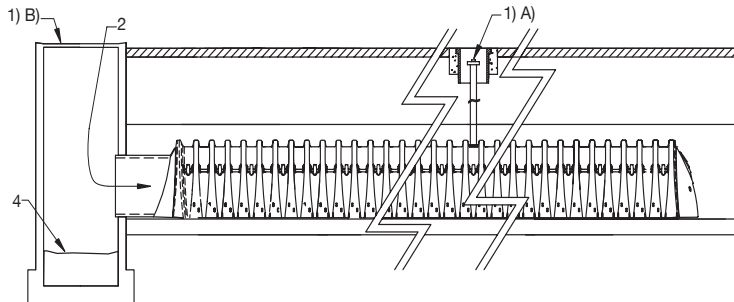
- A) A fixed floor cleaning nozzle with rear facing nozzle spread of 45 inches or more is preferable
- B) Apply multiple passes of JetVac until backflush water is clean
- C) Vacuum manhole sump as required

## STEP 3

Replace all caps, lids and covers, record observations and actions.

## STEP 4

Inspect & clean catch basins and manholes upstream of the StormTech system.



## SAMPLE MAINTENANCE LOG

| Date    | Stadia Rod Readings                  |                                       | Sediment Depth<br>(1)-(2) | Observations/Actions   | Inspector |
|---------|--------------------------------------|---------------------------------------|---------------------------|--|-----------|
|         | Fixed point to chamber<br>bottom (1) | Fixed point to top of<br>sediment (2) |                           |  |           |
| 3/15/11 | 6.3 ft                               | none                                  |                           | New installation. Fixed point is CI frame at grade                         | DJM       |
| 9/24/11 |                                      | 6.2                                   | 0.1 ft                    | Some grit felt   | SM        |
| 6/20/13 |                                      | 5.8                                   | 0.5 ft                    | Mucky feel, debris visible in manhole and in Isolator Row, maintenance due | NV        |
| 7/7/13  | 6.3 ft                               |                                       | 0                         | System jetted and vacuumed   | DJM       |

# Appendix **I**

## **PCSWMM Input/Output Documentation – Existing Conditions**

Input

[TITLE]

;;Project Title/Notes

[OPTIONS]

;;Option Value  
FLOW\_UNITS CMS  
INFILTRATION HORTON  
FLOW\_ROUTING DYNWAVE  
LINK\_OFFSETS ELEVATION  
MIN\_SLOPE 0  
ALLOW\_PONDING NO  
SKIP\_STEADY\_STATE NO

START\_DATE 12/11/2020  
START\_TIME 00:00:00  
REPORT\_START\_DATE 12/11/2020  
REPORT\_START\_TIME 00:00:00  
END\_DATE 12/21/2020  
END\_TIME 00:00:00  
SWEEP\_START 01/01  
SWEEP\_END 12/31  
DRY\_DAYS 0  
REPORT\_STEP 00:01:00  
WET\_STEP 00:05:00  
DRY\_STEP 00:05:00  
ROUTING\_STEP 5  
RULE\_STEP 00:00:00

INERTIAL\_DAMPING PARTIAL  
NORMAL\_FLOW\_LIMITED BOTH  
FORCE\_MAIN\_EQUATION H-W  
VARIABLE\_STEP 0.75  
LENGTHENING\_STEP 0  
MIN\_SURFAREA 0  
MAX\_TRIALS 8  
HEAD\_TOLERANCE 0.0015  
SYS\_FLOW\_TOL 5  
LAT\_FLOW\_TOL 5  
MINIMUM\_STEP 0.5  
THREADS 6

[EVAPORATION]

;;Data Source Parameters  
;;-----  
CONSTANT 0.0  
DRY\_ONLY NO

[RAINGAGES]

| ;;Name    | Format    | Interval | SCF | Source               |
|-----------|-----------|----------|-----|----------------------|
| 25mm      | INTENSITY | 0:05     | 1.0 | TIMESERIES 25mm      |
| 3hr-100yr | INTENSITY | 0:10     | 1.0 | TIMESERIES 3hr-100yr |
| 3hr-2yr   | INTENSITY | 0:05     | 1.0 | TIMESERIES 3hr-2yr   |
| 3hr-5yr   | INTENSITY | 0:05     | 1.0 | TIMESERIES 3hr-5yr   |
| 6hr-100yr | INTENSITY | 0:10     | 1.0 | TIMESERIES 6hr-100yr |
| 6hr-2yr   | INTENSITY | 0:05     | 1.0 | TIMESERIES 6hr-2yr   |
| 6hr-5yr   | INTENSITY | 0:05     | 1.0 | TIMESERIES 6hr-5yr   |

[SUBCATCHMENTS]

| ;;Name | Rain Gage | Outlet       | Area | %Imperv | Width | %Slope | CurbLen | SnowPack |
|--------|-----------|--------------|------|---------|-------|--------|---------|----------|
| EX_N   | 6hr-100yr | SHEFFIELD_RD | 4.47 | 40      | 447   | 1      | 0       |          |
| EX_S   | 6hr-100yr | HUMBER_PL    | 1.37 | 40      | 137   | 1      | 0       |          |

[SUBAREAS]

| ;;Subcatchment | N-Imperv | N-Perv | S-Imperv | S-Perv | PctZero | RouteTo | PctRouted |
|----------------|----------|--------|----------|--------|---------|---------|-----------|
| EX_N           | 0.013    | 0.2    | 1.57     | 4.67   | 0       | OUTLET  |           |
| EX_S           | 0.013    | 0.2    | 1.57     | 4.67   | 0       | OUTLET  |           |

[INFILTRATION]

| ;;Subcatchment | Param1 | Param2 | Param3 | Param4 | Param5 |
|----------------|--------|--------|--------|--------|--------|
| EX_N           | 75     | 0.5    | 4      | 7      | 0      |
| EX_S           | 75     | 0.5    | 4      | 7      | 0      |

[OUTFALLS]

| ;;Name       | Elevation | Type | Stage Data | Gated | Route To |
|--------------|-----------|------|------------|-------|----------|
| HUMBER_PL    | 62.477    | FREE |            | NO    |          |
| SHEFFIELD_RD | 64        | FREE |            | NO    |          |

[CURVES]

| ;;Name | Type    | X-Value | Y-Value |
|--------|---------|---------|---------|
| ADS    | Storage | 0.025   | 530     |
| ADS    |         | 0.051   | 530     |
| ADS    |         | 0.076   | 530     |
| ADS    |         | 0.102   | 530     |
| ADS    |         | 0.127   | 530     |
| ADS    |         | 0.152   | 530     |
| ADS    |         | 0.178   | 530     |
| ADS    |         | 0.203   | 530     |

|     |       |     |
|-----|-------|-----|
| ADS | 0.229 | 530 |
| ADS | 0.254 | 590 |
| ADS | 0.279 | 638 |
| ADS | 0.305 | 678 |
| ADS | 0.33  | 711 |
| ADS | 0.356 | 739 |
| ADS | 0.381 | 764 |
| ADS | 0.406 | 785 |
| ADS | 0.432 | 803 |
| ADS | 0.457 | 819 |
| ADS | 0.483 | 833 |
| ADS | 0.508 | 846 |
| ADS | 0.533 | 857 |
| ADS | 0.559 | 866 |
| ADS | 0.584 | 875 |
| ADS | 0.61  | 883 |
| ADS | 0.635 | 889 |
| ADS | 0.66  | 895 |
| ADS | 0.686 | 901 |
| ADS | 0.711 | 905 |
| ADS | 0.737 | 910 |
| ADS | 0.762 | 913 |
| ADS | 0.787 | 916 |
| ADS | 0.813 | 919 |
| ADS | 0.838 | 921 |
| ADS | 0.864 | 922 |
| ADS | 0.889 | 924 |
| ADS | 0.914 | 925 |
| ADS | 0.94  | 925 |
| ADS | 0.965 | 925 |
| ADS | 0.991 | 925 |
| ADS | 1.016 | 925 |
| ADS | 1.041 | 924 |
| ADS | 1.067 | 923 |
| ADS | 1.092 | 921 |
| ADS | 1.118 | 919 |
| ADS | 1.143 | 917 |
| ADS | 1.168 | 914 |
| ADS | 1.194 | 911 |
| ADS | 1.219 | 908 |
| ADS | 1.245 | 903 |
| ADS | 1.27  | 898 |
| ADS | 1.295 | 892 |
| ADS | 1.321 | 886 |
| ADS | 1.346 | 880 |
| ADS | 1.372 | 874 |
| ADS | 1.397 | 868 |
| ADS | 1.422 | 862 |
| ADS | 1.448 | 856 |
| ADS | 1.473 | 850 |
| ADS | 1.499 | 845 |
| ADS | 1.524 | 840 |
| ADS | 1.549 | 834 |
| ADS | 1.575 | 830 |
| ADS | 1.6   | 825 |
| ADS | 1.626 | 820 |
| ADS | 1.651 | 816 |
| ADS | 1.676 | 811 |

|           |         |   |      |
|-----------|---------|---|------|
| STORAGE_N | Storage | 0 | 1500 |
| STORAGE_N |         | 1 | 1500 |

|           |         |   |      |
|-----------|---------|---|------|
| STORAGE_S | Storage | 0 | 1800 |
| STORAGE_S |         | 1 | 1800 |

**[TIMESERIES]**

| ;;Name  | Date  | Time  | Value  |
|---------|-------|-------|--------|
| ;;----- | ----- | ----- | -----  |
| 25mm    |       | 0:00  | 1.423  |
| 25mm    |       | 0:05  | 1.423  |
| 25mm    |       | 0:10  | 1.574  |
| 25mm    |       | 0:15  | 1.574  |
| 25mm    |       | 0:20  | 1.769  |
| 25mm    |       | 0:25  | 1.769  |
| 25mm    |       | 0:30  | 2.028  |
| 25mm    |       | 0:35  | 2.028  |
| 25mm    |       | 0:40  | 2.389  |
| 25mm    |       | 0:45  | 2.389  |
| 25mm    |       | 0:50  | 2.933  |
| 25mm    |       | 0:55  | 2.933  |
| 25mm    |       | 1:00  | 3.859  |
| 25mm    |       | 1:05  | 3.859  |
| 25mm    |       | 1:10  | 5.821  |
| 25mm    |       | 1:15  | 5.821  |
| 25mm    |       | 1:20  | 13.337 |
| 25mm    |       | 1:25  | 13.337 |
| 25mm    |       | 1:30  | 61.503 |
| 25mm    |       | 1:35  | 61.503 |
| 25mm    |       | 1:40  | 15.65  |
| 25mm    |       | 1:45  | 15.65  |
| 25mm    |       | 1:50  | 7.793  |
| 25mm    |       | 1:55  | 7.793  |
| 25mm    |       | 2:00  | 5.294  |
| 25mm    |       | 2:05  | 5.294  |
| 25mm    |       | 2:10  | 4.057  |

|      |      |       |
|------|------|-------|
| 25mm | 2:15 | 4.057 |
| 25mm | 2:20 | 3.314 |
| 25mm | 2:25 | 3.314 |
| 25mm | 2:30 | 2.817 |
| 25mm | 2:35 | 2.817 |
| 25mm | 2:40 | 2.459 |
| 25mm | 2:45 | 2.459 |
| 25mm | 2:50 | 2.189 |
| 25mm | 2:55 | 2.189 |
| 25mm | 3:00 | 1.977 |
| 25mm | 3:05 | 1.977 |
| 25mm | 3:10 | 1.805 |
| 25mm | 3:15 | 1.805 |
| 25mm | 3:20 | 1.664 |
| 25mm | 3:25 | 1.664 |
| 25mm | 3:30 | 1.545 |
| 25mm | 3:35 | 1.545 |
| 25mm | 3:40 | 1.444 |
| 25mm | 3:45 | 1.444 |
| 25mm | 3:50 | 1.356 |
| 25mm | 3:55 | 1.356 |
| 25mm | 4:00 | 0     |

|           |      |        |
|-----------|------|--------|
| 3hr-100yr | 0:00 | 0      |
| 3hr-100yr | 0:10 | 6.05   |
| 3hr-100yr | 0:20 | 7.54   |
| 3hr-100yr | 0:30 | 10.17  |
| 3hr-100yr | 0:40 | 15.98  |
| 3hr-100yr | 0:50 | 40.76  |
| 3hr-100yr | 1:00 | 178.56 |
| 3hr-100yr | 1:10 | 54.04  |
| 3hr-100yr | 1:20 | 27.31  |
| 3hr-100yr | 1:30 | 18.23  |
| 3hr-100yr | 1:40 | 13.73  |
| 3hr-100yr | 1:50 | 11.05  |
| 3hr-100yr | 2:00 | 9.28   |
| 3hr-100yr | 2:10 | 8.02   |
| 3hr-100yr | 2:20 | 7.08   |
| 3hr-100yr | 2:30 | 6.34   |
| 3hr-100yr | 2:40 | 5.76   |
| 3hr-100yr | 2:50 | 5.28   |
| 3hr-100yr | 3:00 | 4.88   |

;Chicago design storm, a = 732.951, b = 6.199, c = 0.81, Duration = 180 minutes, r = 0.35, rain units = mm/hr.

|         |      |         |
|---------|------|---------|
| 3hr-2yr | 0:00 | 2.393   |
| 3hr-2yr | 0:05 | 2.588   |
| 3hr-2yr | 0:10 | 2.823   |
| 3hr-2yr | 0:15 | 3.109   |
| 3hr-2yr | 0:20 | 3.466   |
| 3hr-2yr | 0:25 | 3.927   |
| 3hr-2yr | 0:30 | 4.543   |
| 3hr-2yr | 0:35 | 5.41    |
| 3hr-2yr | 0:40 | 6.721   |
| 3hr-2yr | 0:45 | 8.935   |
| 3hr-2yr | 0:50 | 13.427  |
| 3hr-2yr | 0:55 | 26.893  |
| 3hr-2yr | 1:00 | 103.571 |
| 3hr-2yr | 1:05 | 49.651  |
| 3hr-2yr | 1:10 | 27.587  |
| 3hr-2yr | 1:15 | 17.967  |
| 3hr-2yr | 1:20 | 13.238  |
| 3hr-2yr | 1:25 | 10.466  |
| 3hr-2yr | 1:30 | 8.658   |
| 3hr-2yr | 1:35 | 7.391   |
| 3hr-2yr | 1:40 | 6.455   |
| 3hr-2yr | 1:45 | 5.737   |
| 3hr-2yr | 1:50 | 5.169   |
| 3hr-2yr | 1:55 | 4.707   |
| 3hr-2yr | 2:00 | 4.326   |
| 3hr-2yr | 2:05 | 4.005   |
| 3hr-2yr | 2:10 | 3.731   |
| 3hr-2yr | 2:15 | 3.494   |
| 3hr-2yr | 2:20 | 3.288   |
| 3hr-2yr | 2:25 | 3.107   |
| 3hr-2yr | 2:30 | 2.945   |
| 3hr-2yr | 2:35 | 2.801   |
| 3hr-2yr | 2:40 | 2.672   |
| 3hr-2yr | 2:45 | 2.555   |
| 3hr-2yr | 2:50 | 2.449   |
| 3hr-2yr | 2:55 | 2.351   |
| 3hr-2yr | 3:00 | 0       |

;Chicago design storm, a = 998.071, b = 6.053, c = 0.814, Duration = 180 minutes, r = 0.35, rain units = mm/hr.

|         |      |        |
|---------|------|--------|
| 3hr-5yr | 0:00 | 3.128  |
| 3hr-5yr | 0:05 | 3.385  |
| 3hr-5yr | 0:10 | 3.693  |
| 3hr-5yr | 0:15 | 4.069  |
| 3hr-5yr | 0:20 | 4.54   |
| 3hr-5yr | 0:25 | 5.147  |
| 3hr-5yr | 0:30 | 5.959  |
| 3hr-5yr | 0:35 | 7.105  |
| 3hr-5yr | 0:40 | 8.84   |
| 3hr-5yr | 0:45 | 11.775 |
| 3hr-5yr | 0:50 | 17.755 |
| 3hr-5yr | 0:55 | 35.83  |

|         |      |         |
|---------|------|---------|
| 3hr-5yr | 1:00 | 141.179 |
| 3hr-5yr | 1:05 | 66.682  |
| 3hr-5yr | 1:10 | 36.749  |
| 3hr-5yr | 1:15 | 23.822  |
| 3hr-5yr | 1:20 | 17.501  |
| 3hr-5yr | 1:25 | 13.81   |
| 3hr-5yr | 1:30 | 11.408  |
| 3hr-5yr | 1:35 | 9.727   |
| 3hr-5yr | 1:40 | 8.488   |
| 3hr-5yr | 1:45 | 7.538   |
| 3hr-5yr | 1:50 | 6.786   |
| 3hr-5yr | 1:55 | 6.177   |
| 3hr-5yr | 2:00 | 5.673   |
| 3hr-5yr | 2:05 | 5.25    |
| 3hr-5yr | 2:10 | 4.889   |
| 3hr-5yr | 2:15 | 4.577   |
| 3hr-5yr | 2:20 | 4.306   |
| 3hr-5yr | 2:25 | 4.066   |
| 3hr-5yr | 2:30 | 3.854   |
| 3hr-5yr | 2:35 | 3.665   |
| 3hr-5yr | 2:40 | 3.495   |
| 3hr-5yr | 2:45 | 3.341   |
| 3hr-5yr | 2:50 | 3.201   |
| 3hr-5yr | 2:55 | 3.073   |
| 3hr-5yr | 3:00 | 0       |

|           |      |        |
|-----------|------|--------|
| 6hr-100yr | 0:00 | 0      |
| 6hr-100yr | 0:10 | 2.91   |
| 6hr-100yr | 0:20 | 3.17   |
| 6hr-100yr | 0:30 | 3.48   |
| 6hr-100yr | 0:40 | 3.88   |
| 6hr-100yr | 0:50 | 4.39   |
| 6hr-100yr | 1:00 | 5.08   |
| 6hr-100yr | 1:10 | 6.05   |
| 6hr-100yr | 1:20 | 7.55   |
| 6hr-100yr | 1:30 | 10.17  |
| 6hr-100yr | 1:40 | 15.98  |
| 6hr-100yr | 1:50 | 40.67  |
| 6hr-100yr | 2:00 | 178.56 |
| 6hr-100yr | 2:10 | 54.04  |
| 6hr-100yr | 2:20 | 27.31  |
| 6hr-100yr | 2:30 | 18.23  |
| 6hr-100yr | 2:40 | 13.73  |
| 6hr-100yr | 2:50 | 11.05  |
| 6hr-100yr | 3:00 | 9.28   |
| 6hr-100yr | 3:10 | 8.02   |
| 6hr-100yr | 3:20 | 7.08   |
| 6hr-100yr | 3:30 | 6.34   |
| 6hr-100yr | 3:40 | 5.76   |
| 6hr-100yr | 3:50 | 5.28   |
| 6hr-100yr | 4:00 | 4.88   |
| 6hr-100yr | 4:10 | 4.54   |
| 6hr-100yr | 4:20 | 4.25   |
| 6hr-100yr | 4:30 | 3.99   |
| 6hr-100yr | 4:40 | 3.77   |
| 6hr-100yr | 4:50 | 3.57   |
| 6hr-100yr | 5:00 | 3.4    |
| 6hr-100yr | 5:10 | 3.24   |
| 6hr-100yr | 5:20 | 3.1    |
| 6hr-100yr | 5:30 | 2.97   |
| 6hr-100yr | 5:40 | 2.85   |
| 6hr-100yr | 5:50 | 2.74   |
| 6hr-100yr | 6:00 | 2.64   |

;Chicago design storm, a = 732.951, b = 6.199, c = 0.81, Duration = 360 minutes, r = 0.35, rain units = mm/hr.

|         |      |         |
|---------|------|---------|
| 6hr-2yr | 0:00 | 1.274   |
| 6hr-2yr | 0:05 | 1.32    |
| 6hr-2yr | 0:10 | 1.37    |
| 6hr-2yr | 0:15 | 1.425   |
| 6hr-2yr | 0:20 | 1.485   |
| 6hr-2yr | 0:25 | 1.55    |
| 6hr-2yr | 0:30 | 1.623   |
| 6hr-2yr | 0:35 | 1.703   |
| 6hr-2yr | 0:40 | 1.793   |
| 6hr-2yr | 0:45 | 1.894   |
| 6hr-2yr | 0:50 | 2.008   |
| 6hr-2yr | 0:55 | 2.139   |
| 6hr-2yr | 1:00 | 2.29    |
| 6hr-2yr | 1:05 | 2.467   |
| 6hr-2yr | 1:10 | 2.677   |
| 6hr-2yr | 1:15 | 2.93    |
| 6hr-2yr | 1:20 | 3.242   |
| 6hr-2yr | 1:25 | 3.636   |
| 6hr-2yr | 1:30 | 4.15    |
| 6hr-2yr | 1:35 | 4.851   |
| 6hr-2yr | 1:40 | 5.864   |
| 6hr-2yr | 1:45 | 7.456   |
| 6hr-2yr | 1:50 | 10.31   |
| 6hr-2yr | 1:55 | 16.817  |
| 6hr-2yr | 2:00 | 41.518  |
| 6hr-2yr | 2:05 | 103.571 |
| 6hr-2yr | 2:10 | 39.807  |
| 6hr-2yr | 2:15 | 22.769  |
| 6hr-2yr | 2:20 | 15.728  |
| 6hr-2yr | 2:25 | 11.97   |

|         |      |       |
|---------|------|-------|
| 6hr-2yr | 2:30 | 9.658 |
| 6hr-2yr | 2:35 | 8.101 |
| 6hr-2yr | 2:40 | 6.985 |
| 6hr-2yr | 2:45 | 6.147 |
| 6hr-2yr | 2:50 | 5.495 |
| 6hr-2yr | 2:55 | 4.973 |
| 6hr-2yr | 3:00 | 4.546 |
| 6hr-2yr | 3:05 | 4.191 |
| 6hr-2yr | 3:10 | 3.89  |
| 6hr-2yr | 3:15 | 3.632 |
| 6hr-2yr | 3:20 | 3.409 |
| 6hr-2yr | 3:25 | 3.213 |
| 6hr-2yr | 3:30 | 3.04  |
| 6hr-2yr | 3:35 | 2.886 |
| 6hr-2yr | 3:40 | 2.748 |
| 6hr-2yr | 3:45 | 2.624 |
| 6hr-2yr | 3:50 | 2.511 |
| 6hr-2yr | 3:55 | 2.409 |
| 6hr-2yr | 4:00 | 2.315 |
| 6hr-2yr | 4:05 | 2.229 |
| 6hr-2yr | 4:10 | 2.149 |
| 6hr-2yr | 4:15 | 2.076 |
| 6hr-2yr | 4:20 | 2.008 |
| 6hr-2yr | 4:25 | 1.944 |
| 6hr-2yr | 4:30 | 1.885 |
| 6hr-2yr | 4:35 | 1.83  |
| 6hr-2yr | 4:40 | 1.778 |
| 6hr-2yr | 4:45 | 1.729 |
| 6hr-2yr | 4:50 | 1.684 |
| 6hr-2yr | 4:55 | 1.64  |
| 6hr-2yr | 5:00 | 1.599 |
| 6hr-2yr | 5:05 | 1.561 |
| 6hr-2yr | 5:10 | 1.524 |
| 6hr-2yr | 5:15 | 1.489 |
| 6hr-2yr | 5:20 | 1.456 |
| 6hr-2yr | 5:25 | 1.425 |
| 6hr-2yr | 5:30 | 1.395 |
| 6hr-2yr | 5:35 | 1.366 |
| 6hr-2yr | 5:40 | 1.339 |
| 6hr-2yr | 5:45 | 1.312 |
| 6hr-2yr | 5:50 | 1.287 |
| 6hr-2yr | 5:55 | 1.263 |
| 6hr-2yr | 6:00 | 0     |

;Chicago design storm, a = 998.071, b = 6.053, c = 0.814, Duration = 360 minutes, r = 0.35, rain units = mm/hr.

|         |      |         |
|---------|------|---------|
| 6hr-5yr | 0:00 | 1.659   |
| 6hr-5yr | 0:05 | 1.72    |
| 6hr-5yr | 0:10 | 1.786   |
| 6hr-5yr | 0:15 | 1.857   |
| 6hr-5yr | 0:20 | 1.936   |
| 6hr-5yr | 0:25 | 2.022   |
| 6hr-5yr | 0:30 | 2.117   |
| 6hr-5yr | 0:35 | 2.222   |
| 6hr-5yr | 0:40 | 2.34    |
| 6hr-5yr | 0:45 | 2.472   |
| 6hr-5yr | 0:50 | 2.623   |
| 6hr-5yr | 0:55 | 2.794   |
| 6hr-5yr | 1:00 | 2.993   |
| 6hr-5yr | 1:05 | 3.225   |
| 6hr-5yr | 1:10 | 3.501   |
| 6hr-5yr | 1:15 | 3.834   |
| 6hr-5yr | 1:20 | 4.244   |
| 6hr-5yr | 1:25 | 4.763   |
| 6hr-5yr | 1:30 | 5.442   |
| 6hr-5yr | 1:35 | 6.367   |
| 6hr-5yr | 1:40 | 7.706   |
| 6hr-5yr | 1:45 | 9.813   |
| 6hr-5yr | 1:50 | 13.603  |
| 6hr-5yr | 1:55 | 22.285  |
| 6hr-5yr | 2:00 | 55.656  |
| 6hr-5yr | 2:05 | 141.179 |
| 6hr-5yr | 2:10 | 53.291  |
| 6hr-5yr | 2:15 | 30.263  |
| 6hr-5yr | 2:20 | 20.826  |
| 6hr-5yr | 2:25 | 15.811  |
| 6hr-5yr | 2:30 | 12.736  |
| 6hr-5yr | 2:35 | 10.669  |
| 6hr-5yr | 2:40 | 9.189   |
| 6hr-5yr | 2:45 | 8.079   |
| 6hr-5yr | 2:50 | 7.217   |
| 6hr-5yr | 2:55 | 6.528   |
| 6hr-5yr | 3:00 | 5.965   |
| 6hr-5yr | 3:05 | 5.496   |
| 6hr-5yr | 3:10 | 5.099   |
| 6hr-5yr | 3:15 | 4.759   |
| 6hr-5yr | 3:20 | 4.464   |
| 6hr-5yr | 3:25 | 4.206   |
| 6hr-5yr | 3:30 | 3.979   |
| 6hr-5yr | 3:35 | 3.776   |
| 6hr-5yr | 3:40 | 3.595   |
| 6hr-5yr | 3:45 | 3.431   |
| 6hr-5yr | 3:50 | 3.283   |
| 6hr-5yr | 3:55 | 3.148   |
| 6hr-5yr | 4:00 | 3.025   |
| 6hr-5yr | 4:05 | 2.912   |



|         |      |       |
|---------|------|-------|
| 6hr-5yr | 4:10 | 2.808 |
| 6hr-5yr | 4:15 | 2.711 |
| 6hr-5yr | 4:20 | 2.622 |
| 6hr-5yr | 4:25 | 2.539 |
| 6hr-5yr | 4:30 | 2.461 |
| 6hr-5yr | 4:35 | 2.389 |
| 6hr-5yr | 4:40 | 2.32  |
| 6hr-5yr | 4:45 | 2.257 |
| 6hr-5yr | 4:50 | 2.196 |
| 6hr-5yr | 4:55 | 2.14  |
| 6hr-5yr | 5:00 | 2.086 |
| 6hr-5yr | 5:05 | 2.035 |
| 6hr-5yr | 5:10 | 1.987 |
| 6hr-5yr | 5:15 | 1.942 |
| 6hr-5yr | 5:20 | 1.898 |
| 6hr-5yr | 5:25 | 1.857 |
| 6hr-5yr | 5:30 | 1.818 |
| 6hr-5yr | 5:35 | 1.78  |
| 6hr-5yr | 5:40 | 1.744 |
| 6hr-5yr | 5:45 | 1.71  |
| 6hr-5yr | 5:50 | 1.677 |
| 6hr-5yr | 5:55 | 1.646 |
| 6hr-5yr | 6:00 | 0     |

**[REPORT]**

```
;;Reporting Options
INPUT      YES
CONTROLS   NO
SUBCATCHMENTS ALL
NODES ALL
LINKS ALL
```

**[TAGS]**

**[MAP]**

```
DIMENSIONS      922195.2104      5041730.342      922454.7796      5042003.582
UNITS            Meters
```

**[COORDINATES]**

```
;;Node          X-Coord          Y-Coord
;;-----
HUMBER_PL       922268.498          5041894.2
SHEFFIELD_RD   922422.12           5041745.436
```

**[VERTICES]**

```
;;Link          X-Coord          Y-Coord
;;-----
```

**[POLYGONS]**

```
;;Subcatchment X-Coord          Y-Coord
;;-----
EX_N            922405.17           5041835.648
EX_N            922442.981           5041761.954
EX_N            922393.45           5041742.762
EX_N            922362.523           5041813.337
EX_N            922405.17           5041835.648
EX_S            922249.656           5041991.162
EX_S            922287.467           5041917.468
EX_S            922237.936           5041898.276
EX_S            922207.009           5041968.851
EX_S            922249.656           5041991.162
```

**[SYMBOLS]**

```
;;Gage          X-Coord          Y-Coord
;;-----
```

25 mm

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.015)

\*\*\*\*\*  
Element Count  
\*\*\*\*\*  
Number of rain gages ..... 7  
Number of subcatchments ... 2  
Number of nodes ..... 2  
Number of links ..... 0  
Number of pollutants ..... 0  
Number of land uses ..... 0

\*\*\*\*\*  
Raingage Summary  
\*\*\*\*\*

| Name      | Data Source | Data Type | Recording Interval |
|-----------|-------------|-----------|--------------------|
| 25mm      | 25mm        | INTENSITY | 5 min.             |
| 3hr-100yr | 3hr-100yr   | INTENSITY | 10 min.            |
| 3hr-2yr   | 3hr-2yr     | INTENSITY | 5 min.             |
| 3hr-5yr   | 3hr-5yr     | INTENSITY | 5 min.             |
| 6hr-100yr | 6hr-100yr   | INTENSITY | 10 min.            |
| 6hr-2yr   | 6hr-2yr     | INTENSITY | 5 min.             |
| 6hr-5yr   | 6hr-5yr     | INTENSITY | 5 min.             |

\*\*\*\*\*  
Subcatchment Summary  
\*\*\*\*\*

| Name | Area | Width  | %Imperv | %Slope | Rain Gage | Outlet       |
|------|------|--------|---------|--------|-----------|--------------|
| EX_N | 4.47 | 447.00 | 40.00   | 1.0000 | 25mm      | SHEFFIELD_RD |
| EX_S | 1.37 | 137.00 | 40.00   | 1.0000 | 25mm      | HUMBER_PL    |

\*\*\*\*\*  
Node Summary  
\*\*\*\*\*

| Name         | Type    | Invert Elev. | Max. Depth | Ponded Area | External Inflow |
|--------------|---------|--------------|------------|-------------|-----------------|
| HUMBER_PL    | OUTFALL | 62.48        | 0.00       | 0.0         |                 |
| SHEFFIELD_RD | OUTFALL | 64.00        | 0.00       | 0.0         |                 |

\*\*\*\*\*  
NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
\*\*\*\*\*

\*\*\*\*\*  
Analysis Options  
\*\*\*\*\*

Flow Units ..... CMS  
Process Models:  
  Rainfall/Runoff ..... YES  
  RDII ..... NO  
  Snowmelt ..... NO  
  Groundwater ..... NO  
  Flow Routing ..... NO  
  Water Quality ..... NO  
Infiltration Method ..... HORTON  
Surcharge Method ..... EXTRAN  
Starting Date ..... 12/11/2020 00:00:00  
Ending Date ..... 12/21/2020 00:00:00  
Antecedent Dry Days ..... 0.0  
Report Time Step ..... 00:01:00  
Wet Time Step ..... 00:05:00  
Dry Time Step ..... 00:05:00

|                            | Volume hectare-m | Depth mm |
|----------------------------|------------------|----------|
| Runoff Quantity Continuity |                  |          |
| Total Precipitation        | 0.146            | 25.000   |
| Evaporation Loss           | 0.000            | 0.000    |
| Infiltration Loss          | 0.087            | 14.982   |
| Surface Runoff             | 0.055            | 9.483    |
| Final Storage              | 0.004            | 0.628    |
| Continuity Error (%)       | -0.374           |          |

|                         | Volume hectare-m | Volume 10^6 ltr |
|-------------------------|------------------|-----------------|
| Flow Routing Continuity |                  |                 |
| Dry Weather Inflow      | 0.000            | 0.000           |

|                            |       |       |
|----------------------------|-------|-------|
| Wet Weather Inflow .....   | 0.055 | 0.554 |
| Groundwater Inflow .....   | 0.000 | 0.000 |
| RDII Inflow .....          | 0.000 | 0.000 |
| External Inflow .....      | 0.000 | 0.000 |
| External Outflow .....     | 0.055 | 0.554 |
| Flooding Loss .....        | 0.000 | 0.000 |
| Evaporation Loss .....     | 0.000 | 0.000 |
| Exfiltration Loss .....    | 0.000 | 0.000 |
| Initial Stored Volume .... | 0.000 | 0.000 |
| Final Stored Volume .....  | 0.000 | 0.000 |
| Continuity Error (%) ..... | 0.000 |       |

\*\*\*\*\*  
Subcatchment Runoff Summary  
\*\*\*\*\*

| Subcatchment | Total Precip<br>mm | Total Runon<br>mm | Total Evap<br>mm | Total Infil<br>mm | Imperv<br>Runoff<br>mm | Perv<br>Runoff<br>mm | Total<br>Runoff<br>mm | Total<br>Runoff<br>10 <sup>6</sup> ltr | Peak<br>Runoff<br>CMS | Runoff<br>Coeff |
|--------------|--------------------|-------------------|------------------|-------------------|------------------------|----------------------|-----------------------|--|-----------------------|-----------------|
| EX_N         | 25.00              | 0.00              | 0.00             | 14.98             | 9.47                   | 0.02                 | 9.48                  | 0.42                                   | 0.30                  | 0.379           |
| EX_S         | 25.00              | 0.00              | 0.00             | 14.98             | 9.47                   | 0.02                 | 9.48                  | 0.13                                   | 0.09                  | 0.379           |

Analysis begun on: Wed Oct 5 21:27:16 2022  
Analysis ended on: Wed Oct 5 21:27:16 2022

Total elapsed time: < 1 sec

2-yr, 3-hour

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.015)

```

*****
Element Count
*****
Number of rain gages ..... 7
Number of subcatchments ... 2
Number of nodes ..... 2
Number of links ..... 0
Number of pollutants ..... 0
Number of land uses ..... 0
    
```

\*\*\*\*\*  
 Raingage Summary  
 \*\*\*\*\*

| Name      | Data Source | Data Type | Recording Interval |
|-----------|-------------|-----------|--------------------|
| 25mm      | 25mm        | INTENSITY | 5 min.             |
| 3hr-100yr | 3hr-100yr   | INTENSITY | 10 min.            |
| 3hr-2yr   | 3hr-2yr     | INTENSITY | 5 min.             |
| 3hr-5yr   | 3hr-5yr     | INTENSITY | 5 min.             |
| 6hr-100yr | 6hr-100yr   | INTENSITY | 10 min.            |
| 6hr-2yr   | 6hr-2yr     | INTENSITY | 5 min.             |
| 6hr-5yr   | 6hr-5yr     | INTENSITY | 5 min.             |

\*\*\*\*\*  
 Subcatchment Summary  
 \*\*\*\*\*

| Name | Area | Width  | %Imperv | %Slope | Rain Gage | Outlet       |
|------|------|--------|---------|--------|-----------|--------------|
| EX_N | 4.47 | 447.00 | 40.00   | 1.0000 | 3hr-2yr   | SHEFFIELD_RD |
| EX_S | 1.37 | 137.00 | 40.00   | 1.0000 | 3hr-2yr   | HUMBER_PL    |

\*\*\*\*\*  
 Node Summary  
 \*\*\*\*\*

| Name         | Type    | Invert Elev. | Max. Depth | Ponded Area | External Inflow |
|--------------|---------|--------------|------------|-------------|-----------------|
| HUMBER_PL    | OUTFALL | 62.48        | 0.00       | 0.0         |                 |
| SHEFFIELD_RD | OUTFALL | 64.00        | 0.00       | 0.0         |                 |

\*\*\*\*\*  
 NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
 \*\*\*\*\*

\*\*\*\*\*  
 Analysis Options  
 \*\*\*\*\*

```

Flow Units ..... CMS
Process Models:
  Rainfall/Runoff ..... YES
  RDII ..... NO
  Snowmelt ..... NO
  Groundwater ..... NO
  Flow Routing ..... NO
  Water Quality ..... NO
Infiltration Method ..... HORTON
Surcharge Method ..... EXTRAN
Starting Date ..... 12/11/2020 00:00:00
Ending Date ..... 12/21/2020 00:00:00
Antecedent Dry Days ..... 0.0
Report Time Step ..... 00:01:00
Wet Time Step ..... 00:05:00
Dry Time Step ..... 00:05:00
    
```

|                            | Volume hectare-m | Depth mm |
|----------------------------|------------------|----------|
| Runoff Quantity Continuity |                  |          |
| Total Precipitation        | 0.186            | 31.880   |
| Evaporation Loss           | 0.000            | 0.000    |
| Infiltration Loss          | 0.091            | 15.601   |
| Surface Runoff             | 0.092            | 15.782   |
| Final Storage              | 0.004            | 0.628    |
| Continuity Error (%)       | -0.410           |          |

|                         | Volume hectare-m | Volume 10^6 ltr |
|-------------------------|------------------|-----------------|
| Flow Routing Continuity |                  |                 |
| Dry Weather Inflow      | 0.000            | 0.000           |

|                            |       |       |
|----------------------------|-------|-------|
| Wet Weather Inflow .....   | 0.092 | 0.922 |
| Groundwater Inflow .....   | 0.000 | 0.000 |
| RDII Inflow .....          | 0.000 | 0.000 |
| External Inflow .....      | 0.000 | 0.000 |
| External Outflow .....     | 0.092 | 0.922 |
| Flooding Loss .....        | 0.000 | 0.000 |
| Evaporation Loss .....     | 0.000 | 0.000 |
| Exfiltration Loss .....    | 0.000 | 0.000 |
| Initial Stored Volume .... | 0.000 | 0.000 |
| Final Stored Volume .....  | 0.000 | 0.000 |
| Continuity Error (%) ..... | 0.000 |       |

\*\*\*\*\*  
Subcatchment Runoff Summary  
\*\*\*\*\*

| Subcatchment | Total<br>Precip<br>mm | Total<br>Runon<br>mm | Total<br>Evap<br>mm | Total<br>Infil<br>mm | Imperv<br>Runoff<br>mm | Perv<br>Runoff<br>mm | Total<br>Runoff<br>mm | Total<br>Runoff<br>10 <sup>6</sup> ltr | Peak<br>Runoff<br>CMS | Runoff<br>Coeff |
|--------------|-----------------------|----------------------|---------------------|----------------------|------------------------|----------------------|-----------------------|--|-----------------------|-----------------|
| EX_N         | 31.88                 | 0.00                 | 0.00                | 15.60                | 12.25                  | 3.53                 | 15.78                 | 0.71                                   | 0.48                  | 0.495           |
| EX_S         | 31.88                 | 0.00                 | 0.00                | 15.60                | 12.25                  | 3.53                 | 15.78                 | 0.22                                   | 0.15                  | 0.495           |

Analysis begun on: Wed Oct 5 21:27:34 2022  
Analysis ended on: Wed Oct 5 21:27:34 2022

Total elapsed time: < 1 sec

2-yr, 6-hour

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.015)

\*\*\*\*\*  
Element Count  
\*\*\*\*\*  
Number of rain gages ..... 7  
Number of subcatchments ... 2  
Number of nodes ..... 2  
Number of links ..... 0  
Number of pollutants ..... 0  
Number of land uses ..... 0

\*\*\*\*\*  
Raingage Summary  
\*\*\*\*\*

| Name      | Data Source | Data Type | Recording Interval |
|-----------|-------------|-----------|--------------------|
| 25mm      | 25mm        | INTENSITY | 5 min.             |
| 3hr-100yr | 3hr-100yr   | INTENSITY | 10 min.            |
| 3hr-2yr   | 3hr-2yr     | INTENSITY | 5 min.             |
| 3hr-5yr   | 3hr-5yr     | INTENSITY | 5 min.             |
| 6hr-100yr | 6hr-100yr   | INTENSITY | 10 min.            |
| 6hr-2yr   | 6hr-2yr     | INTENSITY | 5 min.             |
| 6hr-5yr   | 6hr-5yr     | INTENSITY | 5 min.             |

\*\*\*\*\*  
Subcatchment Summary  
\*\*\*\*\*

| Name | Area | Width  | %Imperv | %Slope | Rain Gage | Outlet       |
|------|------|--------|---------|--------|-----------|--------------|
| EX_N | 4.47 | 447.00 | 40.00   | 1.0000 | 6hr-2yr   | SHEFFIELD_RD |
| EX_S | 1.37 | 137.00 | 40.00   | 1.0000 | 6hr-2yr   | HUMBER_PL    |

\*\*\*\*\*  
Node Summary  
\*\*\*\*\*

| Name         | Type    | Invert Elev. | Max. Depth | Ponded Area | External Inflow |
|--------------|---------|--------------|------------|-------------|-----------------|
| HUMBER_PL    | OUTFALL | 62.48        | 0.00       | 0.0         |                 |
| SHEFFIELD_RD | OUTFALL | 64.00        | 0.00       | 0.0         |                 |

\*\*\*\*\*  
NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
\*\*\*\*\*

\*\*\*\*\*  
Analysis Options  
\*\*\*\*\*

Flow Units ..... CMS  
Process Models:  
Rainfall/Runoff ..... YES  
RDII ..... NO  
Snowmelt ..... NO  
Groundwater ..... NO  
Flow Routing ..... NO  
Water Quality ..... NO  
Infiltration Method ..... HORTON  
Surcharge Method ..... EXTRAN  
Starting Date ..... 12/11/2020 00:00:00  
Ending Date ..... 12/21/2020 00:00:00  
Antecedent Dry Days ..... 0.0  
Report Time Step ..... 00:01:00  
Wet Time Step ..... 00:05:00  
Dry Time Step ..... 00:05:00

|                            | Volume    | Depth  |
|----------------------------|-----------|--------|
| Runoff Quantity Continuity | hectare-m | mm     |
| -----                      | -----     | -----  |
| Total Precipitation .....  | 0.215     | 36.865 |
| Evaporation Loss .....     | 0.000     | 0.000  |
| Infiltration Loss .....    | 0.094     | 16.058 |
| Surface Runoff .....       | 0.119     | 20.301 |
| Final Storage .....        | 0.004     | 0.628  |
| Continuity Error (%) ..... | -0.330    |        |

|                         | Volume    | Volume   |
|-------------------------|-----------|----------|
| Flow Routing Continuity | hectare-m | 10^6 ltr |

```

*****
Dry Weather Inflow ..... 0.000 0.000
Wet Weather Inflow ..... 0.119 1.186
Groundwater Inflow ..... 0.000 0.000
RDII Inflow ..... 0.000 0.000
External Inflow ..... 0.000 0.000
External Outflow ..... 0.119 1.186
Flooding Loss ..... 0.000 0.000
Evaporation Loss ..... 0.000 0.000
Exfiltration Loss ..... 0.000 0.000
Initial Stored Volume .... 0.000 0.000
Final Stored Volume ..... 0.000 0.000
Continuity Error (%) ..... 0.000

```

```

*****
Subcatchment Runoff Summary
*****

```

| Subcatchment | Total<br>Precip<br>mm | Total<br>Runon<br>mm | Total<br>Evap<br>mm | Total<br>Infil<br>mm | Imperv<br>Runoff<br>mm | Perv<br>Runoff<br>mm | Total<br>Runoff<br>mm | Total<br>Runoff<br>10 <sup>6</sup> ltr | Peak<br>Runoff<br>CMS | Runoff<br>Coeff |
|--------------|-----------------------|----------------------|---------------------|----------------------|------------------------|----------------------|-----------------------|--|-----------------------|-----------------|
| EX_N         | 36.86                 | 0.00                 | 0.00                | 16.06                | 14.22                  | 6.08                 | 20.30                 | 0.91                                   | 0.49                  | 0.551           |
| EX_S         | 36.86                 | 0.00                 | 0.00                | 16.06                | 14.22                  | 6.08                 | 20.30                 | 0.28                                   | 0.15                  | 0.551           |

```

Analysis begun on: Wed Oct 5 21:27:45 2022
Analysis ended on: Wed Oct 5 21:27:45 2022
Total elapsed time: < 1 sec

```

5-yr, 3-hour

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.015)

\*\*\*\*\*  
Element Count  
\*\*\*\*\*  
Number of rain gages ..... 7  
Number of subcatchments ... 2  
Number of nodes ..... 2  
Number of links ..... 0  
Number of pollutants ..... 0  
Number of land uses ..... 0

\*\*\*\*\*  
Raingage Summary  
\*\*\*\*\*

| Name      | Data Source | Data Type | Recording Interval |
|-----------|-------------|-----------|--------------------|
| 25mm      | 25mm        | INTENSITY | 5 min.             |
| 3hr-100yr | 3hr-100yr   | INTENSITY | 10 min.            |
| 3hr-2yr   | 3hr-2yr     | INTENSITY | 5 min.             |
| 3hr-5yr   | 3hr-5yr     | INTENSITY | 5 min.             |
| 6hr-100yr | 6hr-100yr   | INTENSITY | 10 min.            |
| 6hr-2yr   | 6hr-2yr     | INTENSITY | 5 min.             |
| 6hr-5yr   | 6hr-5yr     | INTENSITY | 5 min.             |

\*\*\*\*\*  
Subcatchment Summary  
\*\*\*\*\*

| Name | Area | Width  | %Imperv | %Slope | Rain Gage | Outlet       |
|------|------|--------|---------|--------|-----------|--------------|
| EX_N | 4.47 | 447.00 | 40.00   | 1.0000 | 3hr-5yr   | SHEFFIELD_RD |
| EX_S | 1.37 | 137.00 | 40.00   | 1.0000 | 3hr-5yr   | HUMBER_PL    |

\*\*\*\*\*  
Node Summary  
\*\*\*\*\*

| Name         | Type    | Invert Elev. | Max. Depth | Ponded Area | External Inflow |
|--------------|---------|--------------|------------|-------------|-----------------|
| HUMBER_PL    | OUTFALL | 62.48        | 0.00       | 0.0         |                 |
| SHEFFIELD_RD | OUTFALL | 64.00        | 0.00       | 0.0         |                 |

\*\*\*\*\*  
NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
\*\*\*\*\*

\*\*\*\*\*  
Analysis Options  
\*\*\*\*\*

Flow Units ..... CMS  
Process Models:  
  Rainfall/Runoff ..... YES  
  RDII ..... NO  
  Snowmelt ..... NO  
  Groundwater ..... NO  
  Flow Routing ..... NO  
  Water Quality ..... NO  
Infiltration Method ..... HORTON  
Surcharge Method ..... EXTRAN  
Starting Date ..... 12/11/2020 00:00:00  
Ending Date ..... 12/21/2020 00:00:00  
Antecedent Dry Days ..... 0.0  
Report Time Step ..... 00:01:00  
Wet Time Step ..... 00:05:00  
Dry Time Step ..... 00:05:00

|                            | Volume hectare-m | Depth mm |
|----------------------------|------------------|----------|
| Runoff Quantity Continuity |                  |          |
| Total Precipitation        | 0.248            | 42.540   |
| Evaporation Loss           | 0.000            | 0.000    |
| Infiltration Loss          | 0.092            | 15.728   |
| Surface Runoff             | 0.154            | 26.404   |
| Final Storage              | 0.004            | 0.628    |
| Continuity Error (%)       | -0.516           |          |

|                         | Volume hectare-m | Volume 10^6 ltr |
|-------------------------|------------------|-----------------|
| Flow Routing Continuity |                  |                 |
| Dry Weather Inflow      | 0.000            | 0.000           |



|                            |       |       |
|----------------------------|-------|-------|
| Wet Weather Inflow .....   | 0.154 | 1.542 |
| Groundwater Inflow .....   | 0.000 | 0.000 |
| RDII Inflow .....          | 0.000 | 0.000 |
| External Inflow .....      | 0.000 | 0.000 |
| External Outflow .....     | 0.154 | 1.542 |
| Flooding Loss .....        | 0.000 | 0.000 |
| Evaporation Loss .....     | 0.000 | 0.000 |
| Exfiltration Loss .....    | 0.000 | 0.000 |
| Initial Stored Volume .... | 0.000 | 0.000 |
| Final Stored Volume .....  | 0.000 | 0.000 |
| Continuity Error (%) ..... | 0.000 |       |

\*\*\*\*\*  
Subcatchment Runoff Summary  
\*\*\*\*\*

| Subcatchment | Total<br>Precip<br>mm | Total<br>Runon<br>mm | Total<br>Evap<br>mm | Total<br>Infil<br>mm | Imperv<br>Runoff<br>mm | Perv<br>Runoff<br>mm | Total<br>Runoff<br>mm | Total<br>Runoff<br>10 <sup>6</sup> ltr | Peak<br>Runoff<br>CMS | Runoff<br>Coeff |
|--------------|-----------------------|----------------------|---------------------|----------------------|------------------------|----------------------|-----------------------|--|-----------------------|-----------------|
| EX_N         | 42.54                 | 0.00                 | 0.00                | 15.73                | 16.54                  | 9.86                 | 26.40                 | 1.18                                   | 0.69                  | 0.621           |
| EX_S         | 42.54                 | 0.00                 | 0.00                | 15.73                | 16.54                  | 9.86                 | 26.40                 | 0.36                                   | 0.21                  | 0.621           |

Analysis begun on: Wed Oct 5 21:28:01 2022  
Analysis ended on: Wed Oct 5 21:28:01 2022

Total elapsed time: < 1 sec

5-yr, 6-hour

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.015)

\*\*\*\*\*  
Element Count  
\*\*\*\*\*  
Number of rain gages ..... 7  
Number of subcatchments ... 2  
Number of nodes ..... 2  
Number of links ..... 0  
Number of pollutants ..... 0  
Number of land uses ..... 0

\*\*\*\*\*  
Raingage Summary  
\*\*\*\*\*

| Name      | Data Source | Data Type | Recording Interval |
|-----------|-------------|-----------|--------------------|
| 25mm      | 25mm        | INTENSITY | 5 min.             |
| 3hr-100yr | 3hr-100yr   | INTENSITY | 10 min.            |
| 3hr-2yr   | 3hr-2yr     | INTENSITY | 5 min.             |
| 3hr-5yr   | 3hr-5yr     | INTENSITY | 5 min.             |
| 6hr-100yr | 6hr-100yr   | INTENSITY | 10 min.            |
| 6hr-2yr   | 6hr-2yr     | INTENSITY | 5 min.             |
| 6hr-5yr   | 6hr-5yr     | INTENSITY | 5 min.             |

\*\*\*\*\*  
Subcatchment Summary  
\*\*\*\*\*

| Name | Area | Width  | %Imperv | %Slope | Rain Gage | Outlet       |
|------|------|--------|---------|--------|-----------|--------------|
| EX_N | 4.47 | 447.00 | 40.00   | 1.0000 | 6hr-5yr   | SHEFFIELD_RD |
| EX_S | 1.37 | 137.00 | 40.00   | 1.0000 | 6hr-5yr   | HUMBER_PL    |

\*\*\*\*\*  
Node Summary  
\*\*\*\*\*

| Name         | Type    | Invert Elev. | Max. Depth | Ponded Area | External Inflow |
|--------------|---------|--------------|------------|-------------|-----------------|
| HUMBER_PL    | OUTFALL | 62.48        | 0.00       | 0.0         |                 |
| SHEFFIELD_RD | OUTFALL | 64.00        | 0.00       | 0.0         |                 |

\*\*\*\*\*  
NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
\*\*\*\*\*

\*\*\*\*\*  
Analysis Options  
\*\*\*\*\*

Flow Units ..... CMS  
Process Models:  
  Rainfall/Runoff ..... YES  
  RDII ..... NO  
  Snowmelt ..... NO  
  Groundwater ..... NO  
  Flow Routing ..... NO  
  Water Quality ..... NO  
Infiltration Method ..... HORTON  
Surcharge Method ..... EXTRAN  
Starting Date ..... 12/11/2020 00:00:00  
Ending Date ..... 12/21/2020 00:00:00  
Antecedent Dry Days ..... 0.0  
Report Time Step ..... 00:01:00  
Wet Time Step ..... 00:05:00  
Dry Time Step ..... 00:05:00

|                            | Volume hectare-m | Depth mm |
|----------------------------|------------------|----------|
| Runoff Quantity Continuity |                  |          |
| Total Precipitation        | 0.286            | 49.044   |
| Evaporation Loss           | 0.000            | 0.000    |
| Infiltration Loss          | 0.094            | 16.153   |
| Surface Runoff             | 0.190            | 32.489   |
| Final Storage              | 0.004            | 0.628    |
| Continuity Error (%)       | -0.461           |          |

|                         | Volume hectare-m | Volume 10^6 ltr |
|-------------------------|------------------|-----------------|
| Flow Routing Continuity |                  |                 |
| Dry Weather Inflow      | 0.000            | 0.000           |

|                            |       |       |
|----------------------------|-------|-------|
| Wet Weather Inflow .....   | 0.190 | 1.897 |
| Groundwater Inflow .....   | 0.000 | 0.000 |
| RDII Inflow .....          | 0.000 | 0.000 |
| External Inflow .....      | 0.000 | 0.000 |
| External Outflow .....     | 0.190 | 1.897 |
| Flooding Loss .....        | 0.000 | 0.000 |
| Evaporation Loss .....     | 0.000 | 0.000 |
| Exfiltration Loss .....    | 0.000 | 0.000 |
| Initial Stored Volume .... | 0.000 | 0.000 |
| Final Stored Volume .....  | 0.000 | 0.000 |
| Continuity Error (%) ..... | 0.000 |       |

\*\*\*\*\*  
Subcatchment Runoff Summary  
\*\*\*\*\*

| Subcatchment | Total Precip<br>mm | Total Runon<br>mm | Total Evap<br>mm | Total Infil<br>mm | Imperv<br>Runoff<br>mm | Perv<br>Runoff<br>mm | Total<br>Runoff<br>mm | Total<br>Runoff<br>10^6 ltr | Peak<br>Runoff<br>CMS | Runoff<br>Coeff |
|--------------|--------------------|-------------------|------------------|-------------------|------------------------|----------------------|-----------------------|-----------------------------|-----------------------|-----------------|
| EX_N         | 49.04              | 0.00              | 0.00             | 16.15             | 19.12                  | 13.37                | 32.49                 | 1.45                        | 0.73                  | 0.662           |
| EX_S         | 49.04              | 0.00              | 0.00             | 16.15             | 19.12                  | 13.37                | 32.49                 | 0.45                        | 0.22                  | 0.662           |

Analysis begun on: Wed Oct 5 21:28:15 2022  
Analysis ended on: Wed Oct 5 21:28:16 2022

Total elapsed time: 00:00:01

100-yr, 3-hour

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.015)

\*\*\*\*\*  
Element Count  
\*\*\*\*\*  
Number of rain gages ..... 7  
Number of subcatchments ... 2  
Number of nodes ..... 2  
Number of links ..... 0  
Number of pollutants ..... 0  
Number of land uses ..... 0

\*\*\*\*\*  
Raingage Summary  
\*\*\*\*\*

| Name      | Data Source | Data Type | Recording Interval |
|-----------|-------------|-----------|--------------------|
| 25mm      | 25mm        | INTENSITY | 5 min.             |
| 3hr-100yr | 3hr-100yr   | INTENSITY | 10 min.            |
| 3hr-2yr   | 3hr-2yr     | INTENSITY | 5 min.             |
| 3hr-5yr   | 3hr-5yr     | INTENSITY | 5 min.             |
| 6hr-100yr | 6hr-100yr   | INTENSITY | 10 min.            |
| 6hr-2yr   | 6hr-2yr     | INTENSITY | 5 min.             |
| 6hr-5yr   | 6hr-5yr     | INTENSITY | 5 min.             |

\*\*\*\*\*  
Subcatchment Summary  
\*\*\*\*\*

| Name | Area | Width  | %Imperv | %Slope | Rain Gage | Outlet       |
|------|------|--------|---------|--------|-----------|--------------|
| EX_N | 4.47 | 447.00 | 40.00   | 1.0000 | 3hr-100yr | SHEFFIELD_RD |
| EX_S | 1.37 | 137.00 | 40.00   | 1.0000 | 3hr-100yr | HUMBER_PL    |

\*\*\*\*\*  
Node Summary  
\*\*\*\*\*

| Name         | Type    | Invert Elev. | Max. Depth | Ponded Area | External Inflow |
|--------------|---------|--------------|------------|-------------|-----------------|
| HUMBER_PL    | OUTFALL | 62.48        | 0.00       | 0.0         |                 |
| SHEFFIELD_RD | OUTFALL | 64.00        | 0.00       | 0.0         |                 |

\*\*\*\*\*  
NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
\*\*\*\*\*

\*\*\*\*\*  
Analysis Options  
\*\*\*\*\*

Flow Units ..... CMS  
Process Models:  
  Rainfall/Runoff ..... YES  
  RDII ..... NO  
  Snowmelt ..... NO  
  Groundwater ..... NO  
  Flow Routing ..... NO  
  Water Quality ..... NO  
Infiltration Method ..... HORTON  
Surcharge Method ..... EXTRAN  
Starting Date ..... 12/11/2020 00:00:00  
Ending Date ..... 12/21/2020 00:00:00  
Antecedent Dry Days ..... 0.0  
Report Time Step ..... 00:01:00  
Wet Time Step ..... 00:05:00  
Dry Time Step ..... 00:05:00

|                            | Volume hectare-m | Depth mm |
|----------------------------|------------------|----------|
| Runoff Quantity Continuity |                  |          |
| Total Precipitation        | 0.419            | 71.677   |
| Evaporation Loss           | 0.000            | 0.000    |
| Infiltration Loss          | 0.093            | 15.893   |
| Surface Runoff             | 0.325            | 55.588   |
| Final Storage              | 0.004            | 0.628    |
| Continuity Error (%)       | -0.603           |          |

|                         | Volume hectare-m | Volume 10^6 ltr |
|-------------------------|------------------|-----------------|
| Flow Routing Continuity |                  |                 |
| Dry Weather Inflow      | 0.000            | 0.000           |

|                            |       |       |
|----------------------------|-------|-------|
| Wet Weather Inflow .....   | 0.325 | 3.246 |
| Groundwater Inflow .....   | 0.000 | 0.000 |
| RDII Inflow .....          | 0.000 | 0.000 |
| External Inflow .....      | 0.000 | 0.000 |
| External Outflow .....     | 0.325 | 3.246 |
| Flooding Loss .....        | 0.000 | 0.000 |
| Evaporation Loss .....     | 0.000 | 0.000 |
| Exfiltration Loss .....    | 0.000 | 0.000 |
| Initial Stored Volume .... | 0.000 | 0.000 |
| Final Stored Volume .....  | 0.000 | 0.000 |
| Continuity Error (%) ..... | 0.000 |       |

\*\*\*\*\*  
Subcatchment Runoff Summary  
\*\*\*\*\*

| Subcatchment | Total<br>Precip<br>mm | Total<br>Runon<br>mm | Total<br>Evap<br>mm | Total<br>Infil<br>mm | Imperv<br>Runoff<br>mm | Perv<br>Runoff<br>mm | Total<br>Runoff<br>mm | Total<br>Runoff<br>10 <sup>6</sup> ltr | Peak<br>Runoff<br>CMS | Runoff<br>Coeff |
|--------------|-----------------------|----------------------|---------------------|----------------------|------------------------|----------------------|-----------------------|--|-----------------------|-----------------|
| EX_N         | 71.68                 | 0.00                 | 0.00                | 15.89                | 28.25                  | 27.33                | 55.59                 | 2.48                                   | 1.22                  | 0.776           |
| EX_S         | 71.68                 | 0.00                 | 0.00                | 15.89                | 28.25                  | 27.33                | 55.59                 | 0.76                                   | 0.38                  | 0.776           |

Analysis begun on: Wed Oct 5 21:28:29 2022  
Analysis ended on: Wed Oct 5 21:28:29 2022

Total elapsed time: < 1 sec

100-yr, 6-hour

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.015)

\*\*\*\*\*  
Element Count  
\*\*\*\*\*  
Number of rain gages ..... 7  
Number of subcatchments ... 2  
Number of nodes ..... 2  
Number of links ..... 0  
Number of pollutants ..... 0  
Number of land uses ..... 0

\*\*\*\*\*  
Raingage Summary  
\*\*\*\*\*

| Name      | Data Source | Data Type | Recording Interval |
|-----------|-------------|-----------|--------------------|
| 25mm      | 25mm        | INTENSITY | 5 min.             |
| 3hr-100yr | 3hr-100yr   | INTENSITY | 10 min.            |
| 3hr-2yr   | 3hr-2yr     | INTENSITY | 5 min.             |
| 3hr-5yr   | 3hr-5yr     | INTENSITY | 5 min.             |
| 6hr-100yr | 6hr-100yr   | INTENSITY | 10 min.            |
| 6hr-2yr   | 6hr-2yr     | INTENSITY | 5 min.             |
| 6hr-5yr   | 6hr-5yr     | INTENSITY | 5 min.             |

\*\*\*\*\*  
Subcatchment Summary  
\*\*\*\*\*

| Name | Area | Width  | %Imperv | %Slope | Rain Gage | Outlet       |
|------|------|--------|---------|--------|-----------|--------------|
| EX_N | 4.47 | 447.00 | 40.00   | 1.0000 | 6hr-100yr | SHEFFIELD_RD |
| EX_S | 1.37 | 137.00 | 40.00   | 1.0000 | 6hr-100yr | HUMBER_PL    |

\*\*\*\*\*  
Node Summary  
\*\*\*\*\*

| Name         | Type    | Invert Elev. | Max. Depth | Ponded Area | External Inflow |
|--------------|---------|--------------|------------|-------------|-----------------|
| HUMBER_PL    | OUTFALL | 62.48        | 0.00       | 0.0         |                 |
| SHEFFIELD_RD | OUTFALL | 64.00        | 0.00       | 0.0         |                 |

\*\*\*\*\*  
NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
\*\*\*\*\*

\*\*\*\*\*  
Analysis Options  
\*\*\*\*\*

Flow Units ..... CMS  
Process Models:  
  Rainfall/Runoff ..... YES  
  RDII ..... NO  
  Snowmelt ..... NO  
  Groundwater ..... NO  
  Flow Routing ..... NO  
  Water Quality ..... NO  
Infiltration Method ..... HORTON  
Surcharge Method ..... EXTRAN  
Starting Date ..... 12/11/2020 00:00:00  
Ending Date ..... 12/21/2020 00:00:00  
Antecedent Dry Days ..... 0.0  
Report Time Step ..... 00:01:00  
Wet Time Step ..... 00:05:00  
Dry Time Step ..... 00:05:00

|                            | Volume    | Depth  |
|----------------------------|-----------|--------|
| Runoff Quantity Continuity | hectare-m | mm     |
| -----                      | -----     | -----  |
| Total Precipitation .....  | 0.481     | 82.325 |
| Evaporation Loss .....     | 0.000     | 0.000  |
| Infiltration Loss .....    | 0.096     | 16.366 |
| Surface Runoff .....       | 0.384     | 65.763 |
| Final Storage .....        | 0.004     | 0.628  |
| Continuity Error (%) ..... | -0.524    |        |

\*\*\*\*\*  
Flow Routing Continuity      Volume      Volume  
                                 hectare-m      10^6 ltr

```

*****
Dry Weather Inflow ..... 0.000 0.000
Wet Weather Inflow ..... 0.384 3.841
Groundwater Inflow ..... 0.000 0.000
RDII Inflow ..... 0.000 0.000
External Inflow ..... 0.000 0.000
External Outflow ..... 0.384 3.841
Flooding Loss ..... 0.000 0.000
Evaporation Loss ..... 0.000 0.000
Exfiltration Loss ..... 0.000 0.000
Initial Stored Volume .... 0.000 0.000
Final Stored Volume ..... 0.000 0.000
Continuity Error (%) ..... 0.000

```

```

*****
Subcatchment Runoff Summary
*****

```

| Subcatchment | Total<br>Precip<br>mm | Total<br>Runon<br>mm | Total<br>Evap<br>mm | Total<br>Infil<br>mm | Imperv<br>Runoff<br>mm | Perv<br>Runoff<br>mm | Total<br>Runoff<br>mm | Total<br>Runoff<br>10 <sup>6</sup> ltr | Peak<br>Runoff<br>CMS | Runoff<br>Coeff |
|--------------|-----------------------|----------------------|---------------------|----------------------|------------------------|----------------------|-----------------------|--|-----------------------|-----------------|
| EX_N         | 82.33                 | 0.00                 | 0.00                | 16.37                | 32.50                  | 33.26                | 65.76                 | 2.94                                   | 1.28                  | 0.799           |
| EX_S         | 82.32                 | 0.00                 | 0.00                | 16.37                | 32.50                  | 33.26                | 65.76                 | 0.90                                   | 0.39                  | 0.799           |

```

Analysis begun on: Wed Oct 5 21:28:42 2022
Analysis ended on: Wed Oct 5 21:28:42 2022
Total elapsed time: < 1 sec

```

# Appendix **J**

## **PCSWMM Input/Output Documentation – Proposed Conditions**



Input

[TITLE]

;;Project Title/Notes

[OPTIONS]

;;Option Value  
FLOW\_UNITS CMS  
INFILTRATION HORTON  
FLOW\_ROUTING DYNWAVE  
LINK\_OFFSETS ELEVATION  
MIN\_SLOPE 0  
ALLOW\_PONDING NO  
SKIP\_STEADY\_STATE NO

START\_DATE 12/11/2020  
START\_TIME 00:00:00  
REPORT\_START\_DATE 12/11/2020  
REPORT\_START\_TIME 00:00:00  
END\_DATE 12/21/2020  
END\_TIME 00:00:00  
SWEEP\_START 01/01  
SWEEP\_END 12/31  
DRY\_DAYS 0  
REPORT\_STEP 00:01:00  
WET\_STEP 00:01:00  
DRY\_STEP 00:01:00  
ROUTING\_STEP 1  
RULE\_STEP 00:00:00

INERTIAL\_DAMPING PARTIAL  
NORMAL\_FLOW\_LIMITED BOTH  
FORCE\_MAIN\_EQUATION H-W  
VARIABLE\_STEP 0.75  
LENGHTENING\_STEP 0  
MIN\_SURFAREA 0  
MAX\_TRIALS 8  
HEAD\_TOLERANCE 0.0015  
SYS\_FLOW\_TOL 5  
LAT\_FLOW\_TOL 5  
MINIMUM\_STEP 0.5  
THREADS 6

[EVAPORATION]

;;Data Source Parameters  
;;-----  
CONSTANT 0.0  
DRY\_ONLY NO

[RAINGAGES]

| ;;Name    | Format    | Interval | SCF | Source               |
|-----------|-----------|----------|-----|----------------------|
| 25mm      | INTENSITY | 0:05     | 1.0 | TIMESERIES 25mm      |
| 3hr-100yr | INTENSITY | 0:10     | 1.0 | TIMESERIES 3hr-100yr |
| 3hr-2yr   | INTENSITY | 0:05     | 1.0 | TIMESERIES 3hr-2yr   |
| 3hr-5yr   | INTENSITY | 0:05     | 1.0 | TIMESERIES 3hr-5yr   |
| 6hr-100yr | INTENSITY | 0:10     | 1.0 | TIMESERIES 6hr-100yr |
| 6hr-2yr   | INTENSITY | 0:05     | 1.0 | TIMESERIES 6hr-2yr   |
| 6hr-5yr   | INTENSITY | 0:05     | 1.0 | TIMESERIES 6hr-5yr   |

[SUBCATCHMENTS]

| ;;Name    | Rain Gage | Outlet    | Area | %Imperv | Width   | %Slope | CurbLen | SnowPack |
|-----------|-----------|-----------|------|---------|---------|--------|---------|----------|
| Area_1    | 25mm      | CBMH_14   | 0.25 | 90      | 83.333  | 1      | 0       |          |
| Area_10   | 25mm      | CB_23     | 0.08 | 90      | 26.667  | 1      | 0       |          |
| Area_101  | 25mm      | MH_26     | 1.37 | 95      | 137     | 0.5    | 0       |          |
| Area_102  | 25mm      | CBMH_11   | 1.13 | 95      | 113     | 0.5    | 0       |          |
| Area_11   | 25mm      | CB_10     | 0.13 | 90      | 43.333  | 1      | 0       |          |
| Area_12   | 25mm      | CBMH_9    | 0.16 | 90      | 53.333  | 1      | 0       |          |
| Area_13   | 25mm      | CBMH_8    | 0.16 | 90      | 53.333  | 1      | 0       |          |
| Area_14   | 25mm      | CBMH_7    | 0.17 | 90      | 56.667  | 1      | 0       |          |
| Area_15   | 25mm      | CBMH_6    | 0.09 | 90      | 30      | 1      | 0       |          |
| Area_16   | 25mm      | CB_5      | 0.15 | 90      | 50      | 1      | 0       |          |
| Area_17   | 25mm      | CBMH_4    | 0.17 | 90      | 56.667  | 1      | 0       |          |
| Area_18   | 25mm      | CBMH_3    | 0.17 | 90      | 56.667  | 1      | 0       |          |
| Area_19   | 25mm      | CBMH_2    | 0.17 | 90      | 56.667  | 1      | 0       |          |
| Area_2    | 25mm      | CBMH_15   | 0.16 | 90      | 53.333  | 1      | 0       |          |
| Area_20   | 25mm      | J13       | 0.28 | 90      | 93.333  | 1      | 0       |          |
| Area_2001 | 25mm      | OF2       | 0.07 | 25      | 7       | 0.5    | 0       |          |
| Area_2002 | 25mm      | OF2       | 0.21 | 90      | 21      | 0.5    | 0       |          |
| Area_2003 | 25mm      | OF1       | 0.16 | 90      | 16      | 1      | 0       |          |
| Area_2004 | 25mm      | Humber_Pl | 0.02 | 5       | 13.333  | 0.5    | 0       |          |
| Area_2005 | 25mm      | Humber_Pl | 0.04 | 5       | 26.667  | 0.5    | 0       |          |
| Area_21   | 25mm      | CBMH_11   | 0.21 | 90      | 70      | 1      | 0       |          |
| Area_22   | 25mm      | CBMH_12   | 0.32 | 90      | 106.667 | 1      | 0       |          |
| Area_23   | 25mm      | CB_29     | 0.16 | 90      | 53.333  | 1      | 0       |          |
| Area_3    | 25mm      | DCB_16    | 0.36 | 90      | 120     | 1      | 0       |          |
| Area_4    | 25mm      | CBMH_18   | 0.28 | 90      | 93.333  | 1      | 0       |          |
| Area_5    | 25mm      | CB_27     | 0.15 | 90      | 50      | 1      | 0       |          |
| Area_6    | 25mm      | CB_28     | 0.15 | 90      | 50      | 1      | 0       |          |
| Area_7    | 25mm      | CBMH_19   | 0.04 | 90      | 13.333  | 1      | 0       |          |
| Area_8    | 25mm      | CBMH_21   | 0.12 | 90      | 40      | 1      | 0       |          |
| Area_9    | 25mm      | CBMH_22   | 0.12 | 90      | 40      | 1      | 0       |          |

[SUBAREAS]

| ;;Subcatchment | N-Imperv | N-Perv | S-Imperv | S-Perv | PctZero | RouteTo | PctRouted |
|----------------|----------|--------|----------|--------|---------|---------|-----------|
| Area_1         | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_10        | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_101       | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_102       | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_11        | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_12        | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_13        | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_14        | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_15        | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_16        | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_17        | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_18        | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_19        | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_2         | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_20        | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_2001      | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_2002      | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_2003      | 0.013    | 0.2    | 2        | 5      | 100     | OUTLET  |           |
| Area_2004      | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_2005      | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_21        | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_22        | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_23        | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_3         | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_4         | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_5         | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_6         | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_7         | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_8         | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |
| Area_9         | 0.013    | 0.2    | 1.57     | 4.67   | 100     | OUTLET  |           |

**[INFILTRATION]**

| ;;Subcatchment | Param1 | Param2 | Param3 | Param4 | Param5 |
|----------------|--------|--------|--------|--------|--------|
| Area_1         | 75     | 0.5    | 4      | 7      | 0      |
| Area_10        | 75     | 0.5    | 4      | 7      | 0      |
| Area_101       | 75     | 0.5    | 4      | 7      | 0      |
| Area_102       | 75     | 0.5    | 4      | 7      | 0      |
| Area_11        | 75     | 0.5    | 4      | 7      | 0      |
| Area_12        | 75     | 0.5    | 4      | 7      | 0      |
| Area_13        | 75     | 0.5    | 4      | 7      | 0      |
| Area_14        | 75     | 0.5    | 4      | 7      | 0      |
| Area_15        | 75     | 0.5    | 4      | 7      | 0      |
| Area_16        | 75     | 0.5    | 4      | 7      | 0      |
| Area_17        | 75     | 0.5    | 4      | 7      | 0      |
| Area_18        | 75     | 0.5    | 4      | 7      | 0      |
| Area_19        | 75     | 0.5    | 4      | 7      | 0      |
| Area_2         | 75     | 0.5    | 4      | 7      | 0      |
| Area_20        | 75     | 0.5    | 4      | 7      | 0      |
| Area_2001      | 75     | 0.5    | 4      | 7      | 0      |
| Area_2002      | 75     | 0.5    | 4      | 7      | 0      |
| Area_2003      | 75     | 0.5    | 4      | 7      | 0      |
| Area_2004      | 75     | 0.5    | 4      | 7      | 0      |
| Area_2005      | 75     | 0.5    | 4      | 7      | 0      |
| Area_21        | 75     | 0.5    | 4      | 7      | 0      |
| Area_22        | 75     | 0.5    | 4      | 7      | 0      |
| Area_23        | 75     | 0.5    | 4      | 7      | 0      |
| Area_3         | 75     | 0.5    | 4      | 7      | 0      |
| Area_4         | 75     | 0.5    | 4      | 7      | 0      |
| Area_5         | 75     | 0.5    | 4      | 7      | 0      |
| Area_6         | 75     | 0.5    | 4      | 7      | 0      |
| Area_7         | 75     | 0.5    | 4      | 7      | 0      |
| Area_8         | 75     | 0.5    | 4      | 7      | 0      |
| Area_9         | 75     | 0.5    | 4      | 7      | 0      |

**[JUNCTIONS]**

| ;;Name  | Elevation | MaxDepth | InitDepth | SurDepth | Aponded |
|---------|-----------|----------|-----------|----------|---------|
| CB_10   | 65.329    | 1.411    | 0         | 0        | 10      |
| CB_23   | 66.197    | 0.933    | 0         | 0        | 10      |
| CB_27   | 65.485    | 1.345    | 0         | 0        | 10      |
| CB_28   | 65.386    | 1.524    | 0         | 0        | 10      |
| CB_29   | 64.113    | 2.427    | 0         | 0        | 0       |
| CB_5    | 65.114    | 1.626    | 0         | 0        | 10      |
| CBMH_11 | 63.583    | 2.157    | 0         | 0        | 10      |
| CBMH_12 | 64.058    | 1.682    | 0         | 0        | 10      |
| CBMH_14 | 64.106    | 2.214    | 0         | 0        | 10      |
| CBMH_15 | 64.466    | 1.854    | 0         | 0        | 10      |
| CBMH_18 | 64.05     | 2.54     | 0         | 0        | 0       |
| CBMH_19 | 64.877    | 2.383    | 0         | 0        | 10      |
| CBMH_2  | 64.057    | 2.943    | 0         | 0        | 10      |
| CBMH_21 | 65.172    | 1.868    | 0         | 0        | 10      |
| CBMH_22 | 65.532    | 1.508    | 0         | 0        | 10      |
| CBMH_3  | 64.417    | 2.583    | 0         | 0        | 10      |
| CBMH_4  | 64.777    | 2.223    | 0         | 0        | 10      |
| CBMH_6  | 63.912    | 2.728    | 0         | 0        | 10      |
| CBMH_7  | 64.272    | 2.728    | 0         | 0        | 10      |
| CBMH_8  | 64.632    | 2.368    | 0         | 0        | 10      |
| CBMH_9  | 64.992    | 2.008    | 0         | 0        | 10      |
| DCB_16  | 64.798    | 1.522    | 0         | 0        | 10      |
| J1      | 63.749    | 3.271    | 0         | 0        | 0       |
| J13     | 63.537    | 3.103    | 0         | 0        | 10      |
| J2      | 63.236    | 3.334    | 0         | 0        | 0       |

|       |        |       |   |   |    |
|-------|--------|-------|---|---|----|
| MH_20 | 64.989 | 2.301 | 0 | 0 | 0  |
| MH_24 | 64.134 | 2.496 | 0 | 0 | 10 |
| MH_25 | 64.415 | 2.625 | 0 | 0 | 0  |
| MH_26 | 64.557 | 2.703 | 0 | 0 | 0  |
| MH_27 | 63.889 | 2.021 | 0 | 0 | 0  |
| MH_30 | 63.732 | 3.078 | 0 | 0 | 0  |
| MH_44 | 63.512 | 3.508 | 0 | 0 | 0  |
| MH_45 | 63.114 | 3.456 | 0 | 0 | 0  |
| OGS_1 | 63.039 | 3.341 | 0 | 0 | 0  |
| OGS_2 | 63.469 | 3.011 | 0 | 0 | 0  |

**[OUTFALLS]**

| ;;Name    | Elevation | Type | Stage Data | Gated | Route To |
|-----------|-----------|------|------------|-------|----------|
| Humber_P1 | 62.477    | FREE |            | NO    |          |
| OF1       | 63.41     | FREE |            | NO    |          |
| OF2       | 0         | FREE |            | NO    |          |

**[STORAGE]**

| ;;Name | Elev.  | MaxDepth | InitDepth | Shape   | Curve Name/Params | N/A | Fevap | Psi | Ksat | IMD |
|--------|--------|----------|-----------|---------|-------------------|-----|-------|-----|------|-----|
| SU_N   | 63.749 | 3.041    | 0         | TABULAR | STORAGE_N         | 0   | 0     |     |      |     |
| SU_S   | 63.236 | 3.334    | 0         | TABULAR | STORAGE_S         | 0   | 0     |     |      |     |

**[CONDUITS]**

| ;;Name | From Node | To Node   | Length | Roughness | InOffset | OutOffset | InitFlow | MaxFlow |
|--------|-----------|-----------|--------|-----------|----------|-----------|----------|---------|
| C1     | SU_N      | MH_44     | 2.5    | 0.009     | 64.6     | 64.575    | 0        | 0       |
| C10    | CB_28     | MH_26     | 30.4   | 0.011     | 65.386   | 65.082    | 0        | 0       |
| C11    | CB_27     | MH_26     | 32.8   | 0.011     | 65.485   | 65.157    | 0        | 0       |
| C12    | MH_26     | MH_25     | 16.5   | 0.011     | 64.557   | 64.475    | 0        | 0       |
| C13    | MH_24     | CBMH_18   | 4.8    | 0.011     | 64.134   | 64.11     | 0        | 0       |
| C14    | CB_23     | CBMH_22   | 51.5   | 0.011     | 66.197   | 65.682    | 0        | 0       |
| C15    | CBMH_22   | CBMH_21   | 60     | 0.011     | 65.532   | 65.232    | 0        | 0       |
| C16    | CBMH_21   | MH_20     | 24.5   | 0.011     | 65.172   | 65.049    | 0        | 0       |
| C17    | MH_20     | CBMH_19   | 10.4   | 0.011     | 64.989   | 64.937    | 0        | 0       |
| C18    | CBMH_19   | MH_24     | 46.5   | 0.011     | 64.877   | 64.644    | 0        | 0       |
| C19    | CB_10     | CBMH_9    | 52.5   | 0.011     | 65.329   | 65.067    | 0        | 0       |
| C2     | MH_44     | OGS_2     | 11.6   | 0.011     | 63.512   | 63.454    | 0        | 0       |
| C20    | CBMH_9    | CBMH_8    | 60     | 0.011     | 64.992   | 64.692    | 0        | 0       |
| C21    | CBMH_8    | CBMH_7    | 60     | 0.011     | 64.632   | 64.332    | 0        | 0       |
| C22    | CBMH_7    | CBMH_6    | 60     | 0.011     | 64.272   | 63.972    | 0        | 0       |
| C23    | CBMH_6    | J13       | 29.9   | 0.011     | 63.912   | 63.762    | 0        | 0       |
| C24    | J13       | SU_S      | 4      | 0.011     | 63.537   | 63.517    | 0        | 0       |
| C25    | CB_5      | CBMH_4    | 52.5   | 0.011     | 65.114   | 64.852    | 0        | 0       |
| C26    | CBMH_4    | CBMH_3    | 60     | 0.011     | 64.777   | 64.477    | 0        | 0       |
| C27    | CBMH_3    | CBMH_2    | 60     | 0.011     | 64.417   | 64.117    | 0        | 0       |
| C28    | CBMH_2    | MH_30     | 53.4   | 0.011     | 64.057   | 63.792    | 0        | 0       |
| C29    | CBMH_12   | CBMH_11   | 50     | 0.011     | 64.058   | 63.773    | 0        | 0       |
| C3     | J1        | MH_44     | 2.5    | 0.011     | 63.749   | 63.737    | 0        | 0       |
| C30    | MH_30     | J13       | 9.3    | 0.011     | 63.732   | 63.687    | 0        | 0       |
| C31    | MH_27     | CBMH_11   | 8.2    | 0.011     | 63.889   | 63.848    | 0        | 0       |
| C32    | CBMH_11   | SU_S      | 13.2   | 0.011     | 63.568   | 63.517    | 0        | 0       |
| C33    | OGS_1     | Humber_P1 | 4      | 0.011     | 63.039   | 62.48     | 0        | 0       |
| C34    | OGS_2     | OF1       | 8.7    | 0.011     | 63.454   | 63.41     | 0        | 0       |
| C35    | MH_25     | MH_24     | 44.2   | 0.011     | 64.415   | 64.194    | 0        | 0       |
| C36    | CBMH_18   | SU_N      | 3.9    | 0.011     | 64.05    | 64.03     | 0        | 0       |
| C37    | CB_29     | MH_27     | 32.9   | 0.011     | 64.113   | 63.949    | 0        | 0       |
| C4     | SU_S      | MH_45     | 9.4    | 0.009     | 64.1     | 64.006    | 0        | 0       |
| C5     | J2        | MH_45     | 9.4    | 0.011     | 63.236   | 63.189    | 0        | 0       |
| C6     | MH_45     | OGS_1     | 3.1    | 0.011     | 63.114   | 63.099    | 0        | 0       |
| C7     | DCB_16    | CBMH_15   | 54.4   | 0.011     | 64.798   | 64.526    | 0        | 0       |
| C8     | CBMH_15   | CBMH_14   | 60     | 0.011     | 64.466   | 64.166    | 0        | 0       |
| C9     | CBMH_14   | SU_N      | 15.2   | 0.011     | 64.106   | 64.03     | 0        | 0       |

**[ORIFICES]**

| ;;Name | From Node | To Node | Type | Offset | Qcoeff | Gated | CloseTime |
|--------|-----------|---------|------|--------|--------|-------|-----------|
| OR1    | SU_S      | J2      | SIDE | 63.236 | 0.65   | NO    | 0         |
| OR2    | SU_N      | J1      | SIDE | 63.749 | 0.65   | NO    | 0         |

**[XSECTIONS]**

| ;;Link | Shape    | Geom1 | Geom2 | Geom3 | Geom4 | Barrels | Culvert |
|--------|----------|-------|-------|-------|-------|---------|---------|
| C1     | CIRCULAR | 0.2   | 0     | 0     | 0     | 1       |         |
| C10    | CIRCULAR | 0.45  | 0     | 0     | 0     | 1       |         |
| C11    | CIRCULAR | 0.45  | 0     | 0     | 0     | 1       |         |
| C12    | CIRCULAR | 0.525 | 0     | 0     | 0     | 1       |         |
| C13    | CIRCULAR | 0.6   | 0     | 0     | 0     | 1       |         |
| C14    | CIRCULAR | 0.375 | 0     | 0     | 0     | 1       |         |
| C15    | CIRCULAR | 0.45  | 0     | 0     | 0     | 1       |         |
| C16    | CIRCULAR | 0.45  | 0     | 0     | 0     | 1       |         |
| C17    | CIRCULAR | 0.45  | 0     | 0     | 0     | 1       |         |
| C18    | CIRCULAR | 0.45  | 0     | 0     | 0     | 1       |         |
| C19    | CIRCULAR | 0.45  | 0     | 0     | 0     | 1       |         |
| C2     | CIRCULAR | 0.375 | 0     | 0     | 0     | 1       |         |
| C20    | CIRCULAR | 0.525 | 0     | 0     | 0     | 1       |         |
| C21    | CIRCULAR | 0.525 | 0     | 0     | 0     | 1       |         |
| C22    | CIRCULAR | 0.525 | 0     | 0     | 0     | 1       |         |
| C23    | CIRCULAR | 0.525 | 0     | 0     | 0     | 1       |         |
| C24    | CIRCULAR | 0.75  | 0     | 0     | 0     | 1       |         |
| C25    | CIRCULAR | 0.525 | 0     | 0     | 0     | 1       |         |
| C26    | CIRCULAR | 0.6   | 0     | 0     | 0     | 1       |         |
| C27    | CIRCULAR | 0.6   | 0     | 0     | 0     | 1       |         |

|     |          |       |   |   |   |   |
|-----|----------|-------|---|---|---|---|
| C28 | CIRCULAR | 0.6   | 0 | 0 | 0 | 1 |
| C29 | CIRCULAR | 0.375 | 0 | 0 | 0 | 1 |
| C3  | CIRCULAR | 0.3   | 0 | 0 | 0 | 1 |
| C30 | CIRCULAR | 0.6   | 0 | 0 | 0 | 1 |
| C31 | CIRCULAR | 0.375 | 0 | 0 | 0 | 1 |
| C32 | CIRCULAR | 0.525 | 0 | 0 | 0 | 1 |
| C33 | CIRCULAR | 0.375 | 0 | 0 | 0 | 1 |
| C34 | CIRCULAR | 0.375 | 0 | 0 | 0 | 1 |
| C35 | CIRCULAR | 0.6   | 0 | 0 | 0 | 1 |
| C36 | CIRCULAR | 0.75  | 0 | 0 | 0 | 1 |
| C37 | CIRCULAR | 0.375 | 0 | 0 | 0 | 1 |
| C4  | CIRCULAR | 0.2   | 0 | 0 | 0 | 1 |
| C5  | CIRCULAR | 0.3   | 0 | 0 | 0 | 1 |
| C6  | CIRCULAR | 0.375 | 0 | 0 | 0 | 1 |
| C7  | CIRCULAR | 0.525 | 0 | 0 | 0 | 1 |
| C8  | CIRCULAR | 0.525 | 0 | 0 | 0 | 1 |
| C9  | CIRCULAR | 0.6   | 0 | 0 | 0 | 1 |
| OR1 | CIRCULAR | 0.075 | 0 | 0 | 0 |   |
| OR2 | CIRCULAR | 0.075 | 0 | 0 | 0 |   |

[LOSSES]

```
;;Link      Kentry  Kexit   Kavg    Flap Gate  Seepage
;;-----
```

[CURVES]

```
;;Name      Type      X-Value  Y-Value
;;-----
```

|     |         |       |     |
|-----|---------|-------|-----|
| ADS | Storage | 0.025 | 530 |
| ADS |         | 0.051 | 530 |
| ADS |         | 0.076 | 530 |
| ADS |         | 0.102 | 530 |
| ADS |         | 0.127 | 530 |
| ADS |         | 0.152 | 530 |
| ADS |         | 0.178 | 530 |
| ADS |         | 0.203 | 530 |
| ADS |         | 0.229 | 530 |
| ADS |         | 0.254 | 590 |
| ADS |         | 0.279 | 638 |
| ADS |         | 0.305 | 678 |
| ADS |         | 0.33  | 711 |
| ADS |         | 0.356 | 739 |
| ADS |         | 0.381 | 764 |
| ADS |         | 0.406 | 785 |
| ADS |         | 0.432 | 803 |
| ADS |         | 0.457 | 819 |
| ADS |         | 0.483 | 833 |
| ADS |         | 0.508 | 846 |
| ADS |         | 0.533 | 857 |
| ADS |         | 0.559 | 866 |
| ADS |         | 0.584 | 875 |
| ADS |         | 0.61  | 883 |
| ADS |         | 0.635 | 889 |
| ADS |         | 0.66  | 895 |
| ADS |         | 0.686 | 901 |
| ADS |         | 0.711 | 905 |
| ADS |         | 0.737 | 910 |
| ADS |         | 0.762 | 913 |
| ADS |         | 0.787 | 916 |
| ADS |         | 0.813 | 919 |
| ADS |         | 0.838 | 921 |
| ADS |         | 0.864 | 922 |
| ADS |         | 0.889 | 924 |
| ADS |         | 0.914 | 925 |
| ADS |         | 0.94  | 925 |
| ADS |         | 0.965 | 925 |
| ADS |         | 0.991 | 925 |
| ADS |         | 1.016 | 925 |
| ADS |         | 1.041 | 924 |
| ADS |         | 1.067 | 923 |
| ADS |         | 1.092 | 921 |
| ADS |         | 1.118 | 919 |
| ADS |         | 1.143 | 917 |
| ADS |         | 1.168 | 914 |
| ADS |         | 1.194 | 911 |
| ADS |         | 1.219 | 908 |
| ADS |         | 1.245 | 903 |
| ADS |         | 1.27  | 898 |
| ADS |         | 1.295 | 892 |
| ADS |         | 1.321 | 886 |
| ADS |         | 1.346 | 880 |
| ADS |         | 1.372 | 874 |
| ADS |         | 1.397 | 868 |
| ADS |         | 1.422 | 862 |
| ADS |         | 1.448 | 856 |
| ADS |         | 1.473 | 850 |
| ADS |         | 1.499 | 845 |
| ADS |         | 1.524 | 840 |
| ADS |         | 1.549 | 834 |
| ADS |         | 1.575 | 830 |
| ADS |         | 1.6   | 825 |
| ADS |         | 1.626 | 820 |
| ADS |         | 1.651 | 816 |
| ADS |         | 1.676 | 811 |

```
STORAGE_N  Storage  0      0
```

|           |       |             |
|-----------|-------|-------------|
| STORAGE_N | 0.025 | 600         |
| STORAGE_N | 0.051 | 588.2352941 |
| STORAGE_N | 0.076 | 592.2368421 |
| STORAGE_N | 0.102 | 588.3333333 |
| STORAGE_N | 0.127 | 590.6299213 |
| STORAGE_N | 0.152 | 592.1710526 |
| STORAGE_N | 0.178 | 589.9438202 |
| STORAGE_N | 0.203 | 591.2315271 |
| STORAGE_N | 0.229 | 589.6069869 |
| STORAGE_N | 0.254 | 658.6614173 |
| STORAGE_N | 0.279 | 714.8028674 |
| STORAGE_N | 0.305 | 758.852459  |
| STORAGE_N | 0.33  | 798.0909091 |
| STORAGE_N | 0.356 | 829.1573034 |
| STORAGE_N | 0.381 | 857.9527559 |
| STORAGE_N | 0.406 | 882.9064039 |
| STORAGE_N | 0.432 | 902.5925926 |
| STORAGE_N | 0.457 | 921.7724289 |
| STORAGE_N | 0.483 | 936.7080745 |
| STORAGE_N | 0.508 | 951.7322835 |
| STORAGE_N | 0.533 | 965.0469043 |
| STORAGE_N | 0.559 | 975.1341682 |
| STORAGE_N | 0.584 | 985.7363014 |
| STORAGE_N | 0.61  | 993.5409836 |
| STORAGE_N | 0.635 | 1002        |
| STORAGE_N | 0.66  | 1009.515152 |
| STORAGE_N | 0.686 | 1014.693878 |
| STORAGE_N | 0.711 | 1020.632911 |
| STORAGE_N | 0.737 | 1024.464043 |
| STORAGE_N | 0.762 | 1029.068241 |
| STORAGE_N | 0.787 | 1033.062262 |
| STORAGE_N | 0.813 | 1035.215252 |
| STORAGE_N | 0.838 | 1038.126492 |
| STORAGE_N | 0.864 | 1039.340278 |
| STORAGE_N | 0.889 | 1041.293588 |
| STORAGE_N | 0.914 | 1042.789934 |
| STORAGE_N | 0.94  | 1042.734043 |
| STORAGE_N | 0.965 | 1043.388601 |
| STORAGE_N | 0.991 | 1042.552977 |
| STORAGE_N | 1.016 | 1042.391732 |
| STORAGE_N | 1.041 | 1041.815562 |
| STORAGE_N | 1.067 | 1039.859419 |
| STORAGE_N | 1.092 | 1038.479853 |
| STORAGE_N | 1.118 | 1035.742397 |
| STORAGE_N | 1.143 | 1033.525809 |
| STORAGE_N | 1.168 | 1030.830479 |
| STORAGE_N | 1.194 | 1026.767169 |
| STORAGE_N | 1.219 | 1023.027071 |
| STORAGE_N | 1.245 | 1017.751004 |
| STORAGE_N | 1.27  | 1012.173228 |
| STORAGE_N | 1.295 | 1005.745174 |
| STORAGE_N | 1.321 | 998.4027252 |
| STORAGE_N | 1.346 | 991.7087667 |
| STORAGE_N | 1.372 | 984.0524781 |
| STORAGE_N | 1.397 | 977.1868289 |
| STORAGE_N | 1.422 | 970.5555556 |
| STORAGE_N | 1.448 | 963.4875691 |
| STORAGE_N | 1.473 | 957.3183978 |
| STORAGE_N | 1.499 | 950.7204803 |
| STORAGE_N | 1.524 | 944.9737533 |
| STORAGE_N | 1.549 | 939.4060684 |
| STORAGE_N | 1.575 | 933.4222222 |
| STORAGE_N | 1.6   | 928.2125    |
| STORAGE_N | 1.626 | 922.595326  |
| STORAGE_N | 1.651 | 917.7165354 |
| STORAGE_N | 1.676 | 912.977327  |

|           |         |       |      |
|-----------|---------|-------|------|
| STORAGE_S | Storage | 0     | 0    |
| STORAGE_S |         | 0.025 | 736  |
| STORAGE_S |         | 0.051 | 736  |
| STORAGE_S |         | 0.076 | 736  |
| STORAGE_S |         | 0.102 | 736  |
| STORAGE_S |         | 0.127 | 736  |
| STORAGE_S |         | 0.152 | 736  |
| STORAGE_S |         | 0.178 | 736  |
| STORAGE_S |         | 0.203 | 736  |
| STORAGE_S |         | 0.229 | 736  |
| STORAGE_S |         | 0.254 | 821  |
| STORAGE_S |         | 0.279 | 889  |
| STORAGE_S |         | 0.305 | 946  |
| STORAGE_S |         | 0.33  | 994  |
| STORAGE_S |         | 0.356 | 1034 |
| STORAGE_S |         | 0.381 | 1069 |
| STORAGE_S |         | 0.406 | 1098 |
| STORAGE_S |         | 0.432 | 1124 |
| STORAGE_S |         | 0.457 | 1147 |
| STORAGE_S |         | 0.483 | 1167 |
| STORAGE_S |         | 0.508 | 1185 |
| STORAGE_S |         | 0.533 | 1201 |
| STORAGE_S |         | 0.559 | 1215 |
| STORAGE_S |         | 0.584 | 1227 |
| STORAGE_S |         | 0.61  | 1238 |
| STORAGE_S |         | 0.635 | 1247 |
| STORAGE_S |         | 0.66  | 1256 |
| STORAGE_S |         | 0.686 | 1264 |

|           |         |       |         |
|-----------|---------|-------|---------|
| STORAGE_S | 0.711   | 1270  |         |
| STORAGE_S | 0.737   | 1276  |         |
| STORAGE_S | 0.762   | 1281  |         |
| STORAGE_S | 0.787   | 1285  |         |
| STORAGE_S | 0.813   | 1289  |         |
| STORAGE_S | 0.838   | 1292  |         |
| STORAGE_S | 0.864   | 1294  |         |
| STORAGE_S | 0.889   | 1296  |         |
| STORAGE_S | 0.914   | 1298  |         |
| STORAGE_S | 0.94    | 1298  |         |
| STORAGE_S | 0.965   | 1299  |         |
| STORAGE_S | 0.991   | 1298  |         |
| STORAGE_S | 1.016   | 1298  |         |
| STORAGE_S | 1.041   | 1296  |         |
| STORAGE_S | 1.067   | 1295  |         |
| STORAGE_S | 1.092   | 1293  |         |
| STORAGE_S | 1.118   | 1290  |         |
| STORAGE_S | 1.143   | 1287  |         |
| STORAGE_S | 1.168   | 1283  |         |
| STORAGE_S | 1.194   | 1278  |         |
| STORAGE_S | 1.219   | 1273  |         |
| STORAGE_S | 1.245   | 1267  |         |
| STORAGE_S | 1.27    | 1260  |         |
| STORAGE_S | 1.295   | 1252  |         |
| STORAGE_S | 1.321   | 1243  |         |
| STORAGE_S | 1.346   | 1234  |         |
| STORAGE_S | 1.372   | 1226  |         |
| STORAGE_S | 1.397   | 1217  |         |
| STORAGE_S | 1.422   | 1208  |         |
| STORAGE_S | 1.448   | 1200  |         |
| STORAGE_S | 1.473   | 1192  |         |
| STORAGE_S | 1.499   | 1184  |         |
| STORAGE_S | 1.524   | 1177  |         |
| STORAGE_S | 1.549   | 1169  |         |
| STORAGE_S | 1.575   | 1162  |         |
| STORAGE_S | 1.6     | 1156  |         |
| STORAGE_S | 1.626   | 1149  |         |
| STORAGE_S | 1.651   | 1143  |         |
| STORAGE_S | 1.676   | 1137  |         |
| TEST      | Storage | 0     | 1193.31 |
| TEST      |         | 1.676 | 1193.31 |

[TIMESERIES]

| ;;Name | Date | Time | Value  |
|--------|------|------|--------|
| 25mm   |      | 0:00 | 1.423  |
| 25mm   |      | 0:05 | 1.423  |
| 25mm   |      | 0:10 | 1.574  |
| 25mm   |      | 0:15 | 1.574  |
| 25mm   |      | 0:20 | 1.769  |
| 25mm   |      | 0:25 | 1.769  |
| 25mm   |      | 0:30 | 2.028  |
| 25mm   |      | 0:35 | 2.028  |
| 25mm   |      | 0:40 | 2.389  |
| 25mm   |      | 0:45 | 2.389  |
| 25mm   |      | 0:50 | 2.933  |
| 25mm   |      | 0:55 | 2.933  |
| 25mm   |      | 1:00 | 3.859  |
| 25mm   |      | 1:05 | 3.859  |
| 25mm   |      | 1:10 | 5.821  |
| 25mm   |      | 1:15 | 5.821  |
| 25mm   |      | 1:20 | 13.337 |
| 25mm   |      | 1:25 | 13.337 |
| 25mm   |      | 1:30 | 61.503 |
| 25mm   |      | 1:35 | 61.503 |
| 25mm   |      | 1:40 | 15.65  |
| 25mm   |      | 1:45 | 15.65  |
| 25mm   |      | 1:50 | 7.793  |
| 25mm   |      | 1:55 | 7.793  |
| 25mm   |      | 2:00 | 5.294  |
| 25mm   |      | 2:05 | 5.294  |
| 25mm   |      | 2:10 | 4.057  |
| 25mm   |      | 2:15 | 4.057  |
| 25mm   |      | 2:20 | 3.314  |
| 25mm   |      | 2:25 | 3.314  |
| 25mm   |      | 2:30 | 2.817  |
| 25mm   |      | 2:35 | 2.817  |
| 25mm   |      | 2:40 | 2.459  |
| 25mm   |      | 2:45 | 2.459  |
| 25mm   |      | 2:50 | 2.189  |
| 25mm   |      | 2:55 | 2.189  |
| 25mm   |      | 3:00 | 1.977  |
| 25mm   |      | 3:05 | 1.977  |
| 25mm   |      | 3:10 | 1.805  |
| 25mm   |      | 3:15 | 1.805  |
| 25mm   |      | 3:20 | 1.664  |
| 25mm   |      | 3:25 | 1.664  |
| 25mm   |      | 3:30 | 1.545  |
| 25mm   |      | 3:35 | 1.545  |
| 25mm   |      | 3:40 | 1.444  |
| 25mm   |      | 3:45 | 1.444  |
| 25mm   |      | 3:50 | 1.356  |
| 25mm   |      | 3:55 | 1.356  |
| 25mm   |      | 4:00 | 0      |

|           |      |        |
|-----------|------|--------|
| 3hr-100yr | 0:00 | 0      |
| 3hr-100yr | 0:10 | 6.05   |
| 3hr-100yr | 0:20 | 7.54   |
| 3hr-100yr | 0:30 | 10.17  |
| 3hr-100yr | 0:40 | 15.98  |
| 3hr-100yr | 0:50 | 40.76  |
| 3hr-100yr | 1:00 | 178.56 |
| 3hr-100yr | 1:10 | 54.04  |
| 3hr-100yr | 1:20 | 27.31  |
| 3hr-100yr | 1:30 | 18.23  |
| 3hr-100yr | 1:40 | 13.73  |
| 3hr-100yr | 1:50 | 11.05  |
| 3hr-100yr | 2:00 | 9.28   |
| 3hr-100yr | 2:10 | 8.02   |
| 3hr-100yr | 2:20 | 7.08   |
| 3hr-100yr | 2:30 | 6.34   |
| 3hr-100yr | 2:40 | 5.76   |
| 3hr-100yr | 2:50 | 5.28   |
| 3hr-100yr | 3:00 | 4.88   |

;Chicago design storm, a = 732.951, b = 6.199, c = 0.81, Duration = 180 minutes, r = 0.35, rain units = mm/hr.

|         |      |         |
|---------|------|---------|
| 3hr-2yr | 0:00 | 2.393   |
| 3hr-2yr | 0:05 | 2.588   |
| 3hr-2yr | 0:10 | 2.823   |
| 3hr-2yr | 0:15 | 3.109   |
| 3hr-2yr | 0:20 | 3.466   |
| 3hr-2yr | 0:25 | 3.927   |
| 3hr-2yr | 0:30 | 4.543   |
| 3hr-2yr | 0:35 | 5.41    |
| 3hr-2yr | 0:40 | 6.721   |
| 3hr-2yr | 0:45 | 8.935   |
| 3hr-2yr | 0:50 | 13.427  |
| 3hr-2yr | 0:55 | 26.893  |
| 3hr-2yr | 1:00 | 103.571 |
| 3hr-2yr | 1:05 | 49.651  |
| 3hr-2yr | 1:10 | 27.587  |
| 3hr-2yr | 1:15 | 17.967  |
| 3hr-2yr | 1:20 | 13.238  |
| 3hr-2yr | 1:25 | 10.466  |
| 3hr-2yr | 1:30 | 8.658   |
| 3hr-2yr | 1:35 | 7.391   |
| 3hr-2yr | 1:40 | 6.455   |
| 3hr-2yr | 1:45 | 5.737   |
| 3hr-2yr | 1:50 | 5.169   |
| 3hr-2yr | 1:55 | 4.707   |
| 3hr-2yr | 2:00 | 4.326   |
| 3hr-2yr | 2:05 | 4.005   |
| 3hr-2yr | 2:10 | 3.731   |
| 3hr-2yr | 2:15 | 3.494   |
| 3hr-2yr | 2:20 | 3.288   |
| 3hr-2yr | 2:25 | 3.107   |
| 3hr-2yr | 2:30 | 2.945   |
| 3hr-2yr | 2:35 | 2.801   |
| 3hr-2yr | 2:40 | 2.672   |
| 3hr-2yr | 2:45 | 2.555   |
| 3hr-2yr | 2:50 | 2.449   |
| 3hr-2yr | 2:55 | 2.351   |
| 3hr-2yr | 3:00 | 0       |

;Chicago design storm, a = 998.071, b = 6.053, c = 0.814, Duration = 180 minutes, r = 0.35, rain units = mm/hr.

|         |      |         |
|---------|------|---------|
| 3hr-5yr | 0:00 | 3.128   |
| 3hr-5yr | 0:05 | 3.385   |
| 3hr-5yr | 0:10 | 3.693   |
| 3hr-5yr | 0:15 | 4.069   |
| 3hr-5yr | 0:20 | 4.54    |
| 3hr-5yr | 0:25 | 5.147   |
| 3hr-5yr | 0:30 | 5.959   |
| 3hr-5yr | 0:35 | 7.105   |
| 3hr-5yr | 0:40 | 8.84    |
| 3hr-5yr | 0:45 | 11.775  |
| 3hr-5yr | 0:50 | 17.755  |
| 3hr-5yr | 0:55 | 35.83   |
| 3hr-5yr | 1:00 | 141.179 |
| 3hr-5yr | 1:05 | 66.682  |
| 3hr-5yr | 1:10 | 36.749  |
| 3hr-5yr | 1:15 | 23.822  |
| 3hr-5yr | 1:20 | 17.501  |
| 3hr-5yr | 1:25 | 13.81   |
| 3hr-5yr | 1:30 | 11.408  |
| 3hr-5yr | 1:35 | 9.727   |
| 3hr-5yr | 1:40 | 8.488   |
| 3hr-5yr | 1:45 | 7.538   |
| 3hr-5yr | 1:50 | 6.786   |
| 3hr-5yr | 1:55 | 6.177   |
| 3hr-5yr | 2:00 | 5.673   |
| 3hr-5yr | 2:05 | 5.25    |
| 3hr-5yr | 2:10 | 4.889   |
| 3hr-5yr | 2:15 | 4.577   |
| 3hr-5yr | 2:20 | 4.306   |
| 3hr-5yr | 2:25 | 4.066   |
| 3hr-5yr | 2:30 | 3.854   |
| 3hr-5yr | 2:35 | 3.665   |
| 3hr-5yr | 2:40 | 3.495   |
| 3hr-5yr | 2:45 | 3.341   |

|           |      |        |
|-----------|------|--------|
| 3hr-5yr   | 2:50 | 3.201  |
| 3hr-5yr   | 2:55 | 3.073  |
| 3hr-5yr   | 3:00 | 0      |
| 6hr-100yr | 0:00 | 0      |
| 6hr-100yr | 0:10 | 2.91   |
| 6hr-100yr | 0:20 | 3.17   |
| 6hr-100yr | 0:30 | 3.48   |
| 6hr-100yr | 0:40 | 3.88   |
| 6hr-100yr | 0:50 | 4.39   |
| 6hr-100yr | 1:00 | 5.08   |
| 6hr-100yr | 1:10 | 6.05   |
| 6hr-100yr | 1:20 | 7.55   |
| 6hr-100yr | 1:30 | 10.17  |
| 6hr-100yr | 1:40 | 15.98  |
| 6hr-100yr | 1:50 | 40.67  |
| 6hr-100yr | 2:00 | 178.56 |
| 6hr-100yr | 2:10 | 54.04  |
| 6hr-100yr | 2:20 | 27.31  |
| 6hr-100yr | 2:30 | 18.23  |
| 6hr-100yr | 2:40 | 13.73  |
| 6hr-100yr | 2:50 | 11.05  |
| 6hr-100yr | 3:00 | 9.28   |
| 6hr-100yr | 3:10 | 8.02   |
| 6hr-100yr | 3:20 | 7.08   |
| 6hr-100yr | 3:30 | 6.34   |
| 6hr-100yr | 3:40 | 5.76   |
| 6hr-100yr | 3:50 | 5.28   |
| 6hr-100yr | 4:00 | 4.88   |
| 6hr-100yr | 4:10 | 4.54   |
| 6hr-100yr | 4:20 | 4.25   |
| 6hr-100yr | 4:30 | 3.99   |
| 6hr-100yr | 4:40 | 3.77   |
| 6hr-100yr | 4:50 | 3.57   |
| 6hr-100yr | 5:00 | 3.4    |
| 6hr-100yr | 5:10 | 3.24   |
| 6hr-100yr | 5:20 | 3.1    |
| 6hr-100yr | 5:30 | 2.97   |
| 6hr-100yr | 5:40 | 2.85   |
| 6hr-100yr | 5:50 | 2.74   |
| 6hr-100yr | 6:00 | 2.64   |

;Chicago design storm, a = 732.951, b = 6.199, c = 0.81, Duration = 360 minutes, r = 0.35, rain units = mm/hr.

|         |      |         |
|---------|------|---------|
| 6hr-2yr | 0:00 | 1.274   |
| 6hr-2yr | 0:05 | 1.32    |
| 6hr-2yr | 0:10 | 1.37    |
| 6hr-2yr | 0:15 | 1.425   |
| 6hr-2yr | 0:20 | 1.485   |
| 6hr-2yr | 0:25 | 1.55    |
| 6hr-2yr | 0:30 | 1.623   |
| 6hr-2yr | 0:35 | 1.703   |
| 6hr-2yr | 0:40 | 1.793   |
| 6hr-2yr | 0:45 | 1.894   |
| 6hr-2yr | 0:50 | 2.008   |
| 6hr-2yr | 0:55 | 2.139   |
| 6hr-2yr | 1:00 | 2.29    |
| 6hr-2yr | 1:05 | 2.467   |
| 6hr-2yr | 1:10 | 2.677   |
| 6hr-2yr | 1:15 | 2.93    |
| 6hr-2yr | 1:20 | 3.242   |
| 6hr-2yr | 1:25 | 3.636   |
| 6hr-2yr | 1:30 | 4.15    |
| 6hr-2yr | 1:35 | 4.851   |
| 6hr-2yr | 1:40 | 5.864   |
| 6hr-2yr | 1:45 | 7.456   |
| 6hr-2yr | 1:50 | 10.31   |
| 6hr-2yr | 1:55 | 16.817  |
| 6hr-2yr | 2:00 | 41.518  |
| 6hr-2yr | 2:05 | 103.571 |
| 6hr-2yr | 2:10 | 39.807  |
| 6hr-2yr | 2:15 | 22.769  |
| 6hr-2yr | 2:20 | 15.728  |
| 6hr-2yr | 2:25 | 11.97   |
| 6hr-2yr | 2:30 | 9.658   |
| 6hr-2yr | 2:35 | 8.101   |
| 6hr-2yr | 2:40 | 6.985   |
| 6hr-2yr | 2:45 | 6.147   |
| 6hr-2yr | 2:50 | 5.495   |
| 6hr-2yr | 2:55 | 4.973   |
| 6hr-2yr | 3:00 | 4.546   |
| 6hr-2yr | 3:05 | 4.191   |
| 6hr-2yr | 3:10 | 3.89    |
| 6hr-2yr | 3:15 | 3.632   |
| 6hr-2yr | 3:20 | 3.409   |
| 6hr-2yr | 3:25 | 3.213   |
| 6hr-2yr | 3:30 | 3.04    |
| 6hr-2yr | 3:35 | 2.886   |
| 6hr-2yr | 3:40 | 2.748   |
| 6hr-2yr | 3:45 | 2.624   |
| 6hr-2yr | 3:50 | 2.511   |
| 6hr-2yr | 3:55 | 2.409   |
| 6hr-2yr | 4:00 | 2.315   |
| 6hr-2yr | 4:05 | 2.229   |
| 6hr-2yr | 4:10 | 2.149   |
| 6hr-2yr | 4:15 | 2.076   |



|         |      |       |
|---------|------|-------|
| 6hr-2yr | 4:20 | 2.008 |
| 6hr-2yr | 4:25 | 1.944 |
| 6hr-2yr | 4:30 | 1.885 |
| 6hr-2yr | 4:35 | 1.83  |
| 6hr-2yr | 4:40 | 1.778 |
| 6hr-2yr | 4:45 | 1.729 |
| 6hr-2yr | 4:50 | 1.684 |
| 6hr-2yr | 4:55 | 1.64  |
| 6hr-2yr | 5:00 | 1.599 |
| 6hr-2yr | 5:05 | 1.561 |
| 6hr-2yr | 5:10 | 1.524 |
| 6hr-2yr | 5:15 | 1.489 |
| 6hr-2yr | 5:20 | 1.456 |
| 6hr-2yr | 5:25 | 1.425 |
| 6hr-2yr | 5:30 | 1.395 |
| 6hr-2yr | 5:35 | 1.366 |
| 6hr-2yr | 5:40 | 1.339 |
| 6hr-2yr | 5:45 | 1.312 |
| 6hr-2yr | 5:50 | 1.287 |
| 6hr-2yr | 5:55 | 1.263 |
| 6hr-2yr | 6:00 | 0     |

;Chicago design storm, a = 998.071, b = 6.053, c = 0.814, Duration = 360 minutes, r = 0.35, rain units = mm/hr.

|         |      |         |
|---------|------|---------|
| 6hr-5yr | 0:00 | 1.659   |
| 6hr-5yr | 0:05 | 1.72    |
| 6hr-5yr | 0:10 | 1.786   |
| 6hr-5yr | 0:15 | 1.857   |
| 6hr-5yr | 0:20 | 1.936   |
| 6hr-5yr | 0:25 | 2.022   |
| 6hr-5yr | 0:30 | 2.117   |
| 6hr-5yr | 0:35 | 2.222   |
| 6hr-5yr | 0:40 | 2.34    |
| 6hr-5yr | 0:45 | 2.472   |
| 6hr-5yr | 0:50 | 2.623   |
| 6hr-5yr | 0:55 | 2.794   |
| 6hr-5yr | 1:00 | 2.993   |
| 6hr-5yr | 1:05 | 3.225   |
| 6hr-5yr | 1:10 | 3.501   |
| 6hr-5yr | 1:15 | 3.834   |
| 6hr-5yr | 1:20 | 4.244   |
| 6hr-5yr | 1:25 | 4.763   |
| 6hr-5yr | 1:30 | 5.442   |
| 6hr-5yr | 1:35 | 6.367   |
| 6hr-5yr | 1:40 | 7.706   |
| 6hr-5yr | 1:45 | 9.813   |
| 6hr-5yr | 1:50 | 13.603  |
| 6hr-5yr | 1:55 | 22.285  |
| 6hr-5yr | 2:00 | 55.656  |
| 6hr-5yr | 2:05 | 141.179 |
| 6hr-5yr | 2:10 | 53.291  |
| 6hr-5yr | 2:15 | 30.263  |
| 6hr-5yr | 2:20 | 20.826  |
| 6hr-5yr | 2:25 | 15.811  |
| 6hr-5yr | 2:30 | 12.736  |
| 6hr-5yr | 2:35 | 10.669  |
| 6hr-5yr | 2:40 | 9.189   |
| 6hr-5yr | 2:45 | 8.079   |
| 6hr-5yr | 2:50 | 7.217   |
| 6hr-5yr | 2:55 | 6.528   |
| 6hr-5yr | 3:00 | 5.965   |
| 6hr-5yr | 3:05 | 5.496   |
| 6hr-5yr | 3:10 | 5.099   |
| 6hr-5yr | 3:15 | 4.759   |
| 6hr-5yr | 3:20 | 4.464   |
| 6hr-5yr | 3:25 | 4.206   |
| 6hr-5yr | 3:30 | 3.979   |
| 6hr-5yr | 3:35 | 3.776   |
| 6hr-5yr | 3:40 | 3.595   |
| 6hr-5yr | 3:45 | 3.431   |
| 6hr-5yr | 3:50 | 3.283   |
| 6hr-5yr | 3:55 | 3.148   |
| 6hr-5yr | 4:00 | 3.025   |
| 6hr-5yr | 4:05 | 2.912   |
| 6hr-5yr | 4:10 | 2.808   |
| 6hr-5yr | 4:15 | 2.711   |
| 6hr-5yr | 4:20 | 2.622   |
| 6hr-5yr | 4:25 | 2.539   |
| 6hr-5yr | 4:30 | 2.461   |
| 6hr-5yr | 4:35 | 2.389   |
| 6hr-5yr | 4:40 | 2.32    |
| 6hr-5yr | 4:45 | 2.257   |
| 6hr-5yr | 4:50 | 2.196   |
| 6hr-5yr | 4:55 | 2.14    |
| 6hr-5yr | 5:00 | 2.086   |
| 6hr-5yr | 5:05 | 2.035   |
| 6hr-5yr | 5:10 | 1.987   |
| 6hr-5yr | 5:15 | 1.942   |
| 6hr-5yr | 5:20 | 1.898   |
| 6hr-5yr | 5:25 | 1.857   |
| 6hr-5yr | 5:30 | 1.818   |
| 6hr-5yr | 5:35 | 1.78    |
| 6hr-5yr | 5:40 | 1.744   |
| 6hr-5yr | 5:45 | 1.71    |
| 6hr-5yr | 5:50 | 1.677   |
| 6hr-5yr | 5:55 | 1.646   |

6hr-5yr 6:00 0

[REPORT]

;;Reporting Options  
INPUT YES  
CONTROLS NO  
SUBCATCHMENTS ALL  
NODES ALL  
LINKS ALL

[TAGS]

[MAP]

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UNITS Meters

[COORDINATES]

;;Node X-Coord Y-Coord  
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CB\_27 922174.44 5042163.651  
CB\_28 922183.823 5042138.927  
CB\_29 922311.039 5041911.888  
CB\_5 922241.227 5042156.669  
CBMH\_11 922268.343 5041907.04  
CBMH\_12 922226.064 5041886.711  
CBMH\_14 922119.051 5042161.391  
CBMH\_15 922187.216 5042194.27  
CBMH\_18 922101.491 5042122.208  
CBMH\_19 922112.299 5042084.028  
CBMH\_2 922320.148 5042000.64  
CBMH\_21 922131.832 5042046.581  
CBMH\_22 922160.736 5041992.512  
CBMH\_3 922294.476 5042054.025  
CBMH\_4 922264.811 5042107.553  
CBMH\_6 922368.578 5041956.48  
CBMH\_7 922344.579 5042017.069  
CBMH\_8 922319.775 5042064.766  
CBMH\_9 922291.331 5042119.713  
DCB\_16 922244.166 5042219.719  
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J13 922346.799 5041946.002  
J2 922329.977 5041930.789  
MH\_20 922120.386 5042071.917  
MH\_24 922098.64 5042113.25  
MH\_25 922131.745 5042141.429  
MH\_26 922150.032 5042150.054  
MH\_27 922274.874 5041890.955  
MH\_30 922343.248 5041959.86  
MH\_44 922084.598 5042122.314  
MH\_45 922334.286 5041926.103  
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OGS\_2 922081.054 5042120.627  
Humber\_pl 922336.187 5041918.196  
OF1 922072.924 5042114.432  
OF2 922274.791 5042250.679  
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SU\_S 922332.618 5041935.618

[VERTICES]

;;Link X-Coord Y-Coord  
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C4 922337.658 5041932.991

[POLYGONS]

;;Subcatchment X-Coord Y-Coord  
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Area\_1 922115.018 5042141.948  
Area\_1 922097.108 5042135.258  
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Area\_1 922078.404 5042141.433  
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Area\_101 922164.013 5042006.979  
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Area\_101 922161.602 5042120.253  
Area\_101 922173.064 5042124.967  
Area\_101 922228.053 5042151.46  
Area\_101 922238.998 5042129.891  
Area\_101 922274.182 5042060.554  
Area\_102 922274.182 5042060.554

|           |            |             |
|-----------|------------|-------------|
| Area_102  | 922293.417 | 5042022.648 |
| Area_102  | 922318.903 | 5041972.423 |
| Area_102  | 922292.345 | 5041958.947 |
| Area_102  | 922264.29  | 5041944.711 |
| Area_102  | 922197.507 | 5041910.823 |
| Area_102  | 922189.979 | 5041925.657 |
| Area_102  | 922202.152 | 5041931.834 |
| Area_102  | 922164.013 | 5042006.979 |
| Area_102  | 922274.182 | 5042060.554 |
| Area_11   | 922264.237 | 5042142.698 |
| Area_11   | 922240.449 | 5042189.576 |
| Area_11   | 922262.695 | 5042201.089 |
| Area_11   | 922272.999 | 5042180.783 |
| Area_11   | 922274.904 | 5042166.229 |
| Area_11   | 922280.04  | 5042166.668 |
| Area_11   | 922287.842 | 5042154.676 |
| Area_11   | 922264.237 | 5042142.698 |
| Area_12   | 922291.446 | 5042089.077 |
| Area_12   | 922264.237 | 5042142.698 |
| Area_12   | 922287.841 | 5042154.676 |
| Area_12   | 922315.053 | 5042101.05  |
| Area_12   | 922291.446 | 5042089.077 |
| Area_13   | 922318.655 | 5042035.455 |
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| Area_13   | 922342.258 | 5042047.437 |
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| Area_14   | 922345.865 | 5041981.834 |
| Area_14   | 922318.655 | 5042035.455 |
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| Area_15   | 922365.904 | 5041952.636 |
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| Area_16   | 922238.998 | 5042129.891 |
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| Area_16   | 922221.355 | 5042159.491 |
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| Area_17   | 922291.446 | 5042089.077 |
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|           |            |             |
|-----------|------------|-------------|
| Area_2001 | 922063.194 | 5042152.009 |
| Area_2001 | 922264.858 | 5042254.388 |
| Area_2001 | 922259.515 | 5042248.266 |
| Area_2002 | 922379.025 | 5041976.492 |
| Area_2002 | 922287.841 | 5042154.678 |
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| Area_2002 | 922297.19  | 5042169.092 |
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| Area_2002 | 922289.978 | 5042186.538 |
| Area_2002 | 922259.517 | 5042248.262 |
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| Area_2003 | 922063.163 | 5042152.017 |
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| Area_2003 | 922078.89  | 5042141.459 |
| Area_2003 | 922091.7   | 5042141.95  |
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| Area_2003 | 922095.417 | 5042131.52  |
| Area_2003 | 922097.809 | 5042127.104 |
| Area_2003 | 922097.503 | 5042125.683 |
| Area_2003 | 922084.342 | 5042119.006 |
| Area_2003 | 922109.135 | 5042069.705 |
| Area_2003 | 922113.823 | 5042069.046 |
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| Area_2003 | 922150.409 | 5041998.871 |
| Area_2003 | 922151.992 | 5041996.657 |
| Area_2003 | 922155.734 | 5041986.203 |
| Area_2003 | 922153.387 | 5041982.171 |
| Area_2003 | 922181.001 | 5041928.076 |
| Area_2003 | 922187.058 | 5041928.291 |
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| Area_2003 | 922192.103 | 5041898.561 |
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| Area_2004 | 922209.02  | 5041865.313 |
| Area_2004 | 922235.292 | 5041858.36  |
| Area_2004 | 922233.17  | 5041856.72  |
| Area_2004 | 922230.811 | 5041855.444 |
| Area_2004 | 922228.277 | 5041854.564 |
| Area_2004 | 922225.635 | 5041854.104 |
| Area_2004 | 922222.953 | 5041854.076 |
| Area_2004 | 922220.302 | 5041854.481 |
| Area_2004 | 922217.757 | 5041855.423 |
| Area_2004 | 922215.4   | 5041856.768 |
| Area_2004 | 922213.295 | 5041858.48  |
| Area_2004 | 922211.498 | 5041860.514 |
| Area_2004 | 922210.057 | 5041862.813 |
| Area_2004 | 922209.011 | 5041865.318 |
| Area_2004 | 922209.02  | 5041865.313 |
| Area_2005 | 922371.594 | 5041938.235 |
| Area_2005 | 922368.998 | 5041945.932 |
| Area_2005 | 922365.962 | 5041952.377 |
| Area_2005 | 922369.637 | 5041951.745 |
| Area_2005 | 922378.755 | 5041956.1   |
| Area_2005 | 922378.739 | 5041976.704 |
| Area_2005 | 922391.466 | 5041946.493 |
| Area_2005 | 922371.707 | 5041938.282 |
| Area_2005 | 922371.594 | 5041938.235 |
| Area_21   | 922237.628 | 5041931.182 |
| Area_21   | 922264.427 | 5041944.78  |
| Area_21   | 922274.121 | 5041925.898 |
| Area_21   | 922277.379 | 5041923.323 |
| Area_21   | 922284.651 | 5041920.109 |
| Area_21   | 922298.899 | 5041916.291 |
| Area_21   | 922301.752 | 5041903.119 |
| Area_21   | 922264.403 | 5041877.966 |
| Area_21   | 922237.628 | 5041931.182 |
| Area_22   | 922192.103 | 5041898.562 |
| Area_22   | 922197.507 | 5041910.823 |
| Area_22   | 922237.628 | 5041931.182 |
| Area_22   | 922262.14  | 5041882.443 |
| Area_22   | 922264.403 | 5041877.966 |
| Area_22   | 922235.292 | 5041858.36  |
| Area_22   | 922209.013 | 5041865.315 |
| Area_22   | 922192.103 | 5041898.562 |
| Area_23   | 922292.345 | 5041958.947 |
| Area_23   | 922295.881 | 5041959.172 |
| Area_23   | 922320.146 | 5041915.507 |
| Area_23   | 922301.752 | 5041903.119 |
| Area_23   | 922298.899 | 5041916.291 |
| Area_23   | 922284.651 | 5041920.109 |
| Area_23   | 922277.379 | 5041923.323 |
| Area_23   | 922274.121 | 5041925.898 |
| Area_23   | 922264.411 | 5041944.772 |
| Area_23   | 922292.345 | 5041958.947 |
| Area_3    | 922280.091 | 5042166.581 |
| Area_3    | 922274.904 | 5042166.229 |
| Area_3    | 922273.008 | 5042180.81  |
| Area_3    | 922262.695 | 5042201.089 |
| Area_3    | 922217.934 | 5042178.15  |
| Area_3    | 922210.247 | 5042181.824 |
| Area_3    | 922211.001 | 5042202.867 |
| Area_3    | 922215.404 | 5042210.581 |

|        |            |             |
|--------|------------|-------------|
| Area_3 | 922209.221 | 5042222.74  |
| Area_3 | 922232.117 | 5042234.358 |
| Area_3 | 922259.517 | 5042248.262 |
| Area_3 | 922291.901 | 5042181.949 |
| Area_3 | 922297.215 | 5042169.271 |
| Area_3 | 922297.618 | 5042167.941 |
| Area_3 | 922287.842 | 5042154.676 |
| Area_3 | 922280.091 | 5042166.581 |
| Area_4 | 922143.181 | 5042156.27  |
| Area_4 | 922161.483 | 5042120.204 |
| Area_4 | 922156.344 | 5042116.484 |
| Area_4 | 922118.26  | 5042097.159 |
| Area_4 | 922114.257 | 5042092.55  |
| Area_4 | 922109.378 | 5042089.904 |
| Area_4 | 922101.037 | 5042085.662 |
| Area_4 | 922084.076 | 5042119.088 |
| Area_4 | 922089.477 | 5042121.836 |
| Area_4 | 922097.449 | 5042125.976 |
| Area_4 | 922097.726 | 5042126.825 |
| Area_4 | 922095.579 | 5042131.056 |
| Area_4 | 922095.563 | 5042134.473 |
| Area_4 | 922115.018 | 5042141.948 |
| Area_4 | 922143.181 | 5042156.27  |
| Area_5 | 922152.032 | 5042138.87  |
| Area_5 | 922143.185 | 5042156.239 |
| Area_5 | 922200.513 | 5042185.631 |
| Area_5 | 922210.247 | 5042181.824 |
| Area_5 | 922217.934 | 5042178.15  |
| Area_5 | 922215.802 | 5042170.903 |
| Area_5 | 922152.032 | 5042138.87  |
| Area_6 | 922215.755 | 5042170.747 |
| Area_6 | 922221.427 | 5042159.476 |
| Area_6 | 922229.627 | 5042155.107 |
| Area_6 | 922228.053 | 5042151.46  |
| Area_6 | 922227.484 | 5042152.582 |
| Area_6 | 922173.058 | 5042124.965 |
| Area_6 | 922161.483 | 5042120.204 |
| Area_6 | 922151.987 | 5042138.959 |
| Area_6 | 922215.755 | 5042170.747 |
| Area_7 | 922128.26  | 5042077.453 |
| Area_7 | 922122.858 | 5042074.827 |
| Area_7 | 922118.32  | 5042072.395 |
| Area_7 | 922113.587 | 5042069.511 |
| Area_7 | 922108.959 | 5042069.833 |
| Area_7 | 922101.037 | 5042085.662 |
| Area_7 | 922114.159 | 5042092.581 |
| Area_7 | 922118.26  | 5042097.159 |
| Area_7 | 922128.26  | 5042077.453 |
| Area_8 | 922118.345 | 5042072.41  |
| Area_8 | 922128.26  | 5042077.453 |
| Area_8 | 922155.476 | 5042023.817 |
| Area_8 | 922137.141 | 5042014.511 |
| Area_8 | 922114.851 | 5042058.188 |
| Area_8 | 922115.066 | 5042058.458 |
| Area_8 | 922117.071 | 5042062.608 |
| Area_8 | 922113.617 | 5042069.414 |
| Area_8 | 922118.345 | 5042072.41  |
| Area_9 | 922137.14  | 5042014.511 |
| Area_9 | 922155.476 | 5042023.817 |
| Area_9 | 922182.686 | 5041970.194 |
| Area_9 | 922164.343 | 5041960.893 |
| Area_9 | 922153.575 | 5041982.125 |
| Area_9 | 922155.734 | 5041986.203 |
| Area_9 | 922151.992 | 5041996.657 |
| Area_9 | 922150.409 | 5041998.871 |
| Area_9 | 922146.183 | 5041996.693 |
| Area_9 | 922137.32  | 5042014.602 |
| Area_9 | 922137.14  | 5042014.511 |

[SYMBOLS]

;;Gage X-Coord Y-Coord  
;;-----

25mm

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.015)

WARNING 03: negative offset ignored for Link C2  
WARNING 03: negative offset ignored for Link C32  
WARNING 03: negative offset ignored for Link C34

\*\*\*\*\*

Element Count

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Number of rain gages ..... 7  
Number of subcatchments ... 30  
Number of nodes ..... 40  
Number of links ..... 39  
Number of pollutants ..... 0  
Number of land uses ..... 0

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Raingage Summary

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| Name      | Data Source | Data Type | Recording Interval |
|-----------|-------------|-----------|--------------------|
| 25mm      | 25mm        | INTENSITY | 5 min.             |
| 3hr-100yr | 3hr-100yr   | INTENSITY | 10 min.            |
| 3hr-2yr   | 3hr-2yr     | INTENSITY | 5 min.             |
| 3hr-5yr   | 3hr-5yr     | INTENSITY | 5 min.             |
| 6hr-100yr | 6hr-100yr   | INTENSITY | 10 min.            |
| 6hr-2yr   | 6hr-2yr     | INTENSITY | 5 min.             |
| 6hr-5yr   | 6hr-5yr     | INTENSITY | 5 min.             |

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Subcatchment Summary

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| Name      | Area | Width  | %Imperv | %Slope | Rain Gage | Outlet    |
|-----------|------|--------|---------|--------|-----------|-----------|
| Area_1    | 0.25 | 83.33  | 90.00   | 1.0000 | 25mm      | CBMH_14   |
| Area_10   | 0.08 | 26.67  | 90.00   | 1.0000 | 25mm      | CB_23     |
| Area_101  | 1.37 | 137.00 | 95.00   | 0.5000 | 25mm      | MH_26     |
| Area_102  | 1.13 | 113.00 | 95.00   | 0.5000 | 25mm      | CBMH_11   |
| Area_11   | 0.13 | 43.33  | 90.00   | 1.0000 | 25mm      | CB_10     |
| Area_12   | 0.16 | 53.33  | 90.00   | 1.0000 | 25mm      | CBMH_9    |
| Area_13   | 0.16 | 53.33  | 90.00   | 1.0000 | 25mm      | CBMH_8    |
| Area_14   | 0.17 | 56.67  | 90.00   | 1.0000 | 25mm      | CBMH_7    |
| Area_15   | 0.09 | 30.00  | 90.00   | 1.0000 | 25mm      | CBMH_6    |
| Area_16   | 0.15 | 50.00  | 90.00   | 1.0000 | 25mm      | CB_5      |
| Area_17   | 0.17 | 56.67  | 90.00   | 1.0000 | 25mm      | CBMH_4    |
| Area_18   | 0.17 | 56.67  | 90.00   | 1.0000 | 25mm      | CBMH_3    |
| Area_19   | 0.17 | 56.67  | 90.00   | 1.0000 | 25mm      | CBMH_2    |
| Area_2    | 0.16 | 53.33  | 90.00   | 1.0000 | 25mm      | CBMH_15   |
| Area_20   | 0.28 | 93.33  | 90.00   | 1.0000 | 25mm      | J13       |
| Area_2001 | 0.07 | 7.00   | 25.00   | 0.5000 | 25mm      | OF2       |
| Area_2002 | 0.21 | 21.00  | 90.00   | 0.5000 | 25mm      | OF2       |
| Area_2003 | 0.16 | 16.00  | 90.00   | 1.0000 | 25mm      | OF1       |
| Area_2004 | 0.02 | 13.33  | 5.00    | 0.5000 | 25mm      | Humber_Pl |
| Area_2005 | 0.04 | 26.67  | 5.00    | 0.5000 | 25mm      | Humber_Pl |
| Area_21   | 0.21 | 70.00  | 90.00   | 1.0000 | 25mm      | CBMH_11   |
| Area_22   | 0.32 | 106.67 | 90.00   | 1.0000 | 25mm      | CBMH_12   |
| Area_23   | 0.16 | 53.33  | 90.00   | 1.0000 | 25mm      | CB_29     |
| Area_3    | 0.36 | 120.00 | 90.00   | 1.0000 | 25mm      | DCB_16    |
| Area_4    | 0.28 | 93.33  | 90.00   | 1.0000 | 25mm      | CBMH_18   |
| Area_5    | 0.15 | 50.00  | 90.00   | 1.0000 | 25mm      | CB_27     |
| Area_6    | 0.15 | 50.00  | 90.00   | 1.0000 | 25mm      | CB_28     |
| Area_7    | 0.04 | 13.33  | 90.00   | 1.0000 | 25mm      | CBMH_19   |
| Area_8    | 0.12 | 40.00  | 90.00   | 1.0000 | 25mm      | CBMH_21   |
| Area_9    | 0.12 | 40.00  | 90.00   | 1.0000 | 25mm      | CBMH_22   |

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Node Summary

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| Name    | Type     | Invert Elev. | Max. Depth | Ponded Area | External Inflow |
|---------|----------|--------------|------------|-------------|-----------------|
| CB_10   | JUNCTION | 65.33        | 1.41       | 10.0        |                 |
| CB_23   | JUNCTION | 66.20        | 0.93       | 10.0        |                 |
| CB_27   | JUNCTION | 65.48        | 1.34       | 10.0        |                 |
| CB_28   | JUNCTION | 65.39        | 1.52       | 10.0        |                 |
| CB_29   | JUNCTION | 64.11        | 2.43       | 0.0         |                 |
| CB_5    | JUNCTION | 65.11        | 1.63       | 10.0        |                 |
| CBMH_11 | JUNCTION | 63.58        | 2.16       | 10.0        |                 |
| CBMH_12 | JUNCTION | 64.06        | 1.68       | 10.0        |                 |
| CBMH_14 | JUNCTION | 64.11        | 2.21       | 10.0        |                 |
| CBMH_15 | JUNCTION | 64.47        | 1.85       | 10.0        |                 |
| CBMH_18 | JUNCTION | 64.05        | 2.54       | 0.0         |                 |
| CBMH_19 | JUNCTION | 64.88        | 2.38       | 10.0        |                 |
| CBMH_2  | JUNCTION | 64.06        | 2.94       | 10.0        |                 |
| CBMH_21 | JUNCTION | 65.17        | 1.87       | 10.0        |                 |
| CBMH_22 | JUNCTION | 65.53        | 1.51       | 10.0        |                 |

|           |          |       |      |      |
|-----------|----------|-------|------|------|
| CBMH_3    | JUNCTION | 64.42 | 2.58 | 10.0 |
| CBMH_4    | JUNCTION | 64.78 | 2.22 | 10.0 |
| CBMH_6    | JUNCTION | 63.91 | 2.73 | 10.0 |
| CBMH_7    | JUNCTION | 64.27 | 2.73 | 10.0 |
| CBMH_8    | JUNCTION | 64.63 | 2.37 | 10.0 |
| CBMH_9    | JUNCTION | 64.99 | 2.01 | 10.0 |
| DCB_16    | JUNCTION | 64.80 | 1.52 | 10.0 |
| J1        | JUNCTION | 63.75 | 3.27 | 0.0  |
| J13       | JUNCTION | 63.54 | 3.10 | 10.0 |
| J2        | JUNCTION | 63.24 | 3.33 | 0.0  |
| MH_20     | JUNCTION | 64.99 | 2.30 | 0.0  |
| MH_24     | JUNCTION | 64.13 | 2.50 | 10.0 |
| MH_25     | JUNCTION | 64.42 | 2.63 | 0.0  |
| MH_26     | JUNCTION | 64.56 | 2.70 | 0.0  |
| MH_27     | JUNCTION | 63.89 | 2.02 | 0.0  |
| MH_30     | JUNCTION | 63.73 | 3.08 | 0.0  |
| MH_44     | JUNCTION | 63.51 | 3.51 | 0.0  |
| MH_45     | JUNCTION | 63.11 | 3.46 | 0.0  |
| OGS_1     | JUNCTION | 63.04 | 3.34 | 0.0  |
| OGS_2     | JUNCTION | 63.47 | 3.01 | 0.0  |
| Humber_P1 | OUTFALL  | 62.48 | 0.38 | 0.0  |
| OF1       | OUTFALL  | 63.41 | 0.38 | 0.0  |
| OF2       | OUTFALL  | 0.00  | 0.00 | 0.0  |
| SU_N      | STORAGE  | 63.75 | 3.04 | 0.0  |
| SU_S      | STORAGE  | 63.24 | 3.33 | 0.0  |

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Link Summary  
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| Name | From Node | To Node   | Type    | Length | %Slope  | Roughness |
|------|-----------|-----------|---------|--------|---------|-----------|
| C1   | SU_N      | MH_44     | CONDUIT | 2.5    | 1.0001  | 0.0090    |
| C10  | CB_28     | MH_26     | CONDUIT | 30.4   | 1.0001  | 0.0110    |
| C11  | CB_27     | MH_26     | CONDUIT | 32.8   | 1.0001  | 0.0110    |
| C12  | MH_26     | MH_25     | CONDUIT | 16.5   | 0.4970  | 0.0110    |
| C13  | MH_24     | CBMH_18   | CONDUIT | 4.8    | 0.5000  | 0.0110    |
| C14  | CB_23     | CBMH_22   | CONDUIT | 51.5   | 1.0001  | 0.0110    |
| C15  | CBMH_22   | CBMH_21   | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C16  | CBMH_21   | MH_20     | CONDUIT | 24.5   | 0.5020  | 0.0110    |
| C17  | MH_20     | CBMH_19   | CONDUIT | 10.4   | 0.5000  | 0.0110    |
| C18  | CBMH_19   | MH_24     | CONDUIT | 46.5   | 0.5011  | 0.0110    |
| C19  | CB_10     | CBMH_9    | CONDUIT | 52.5   | 0.4991  | 0.0110    |
| C2   | MH_44     | OGS_2     | CONDUIT | 11.6   | 0.3707  | 0.0110    |
| C20  | CBMH_9    | CBMH_8    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C21  | CBMH_8    | CBMH_7    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C22  | CBMH_7    | CBMH_6    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C23  | CBMH_6    | J13       | CONDUIT | 29.9   | 0.5017  | 0.0110    |
| C24  | J13       | SU_S      | CONDUIT | 4.0    | 0.5000  | 0.0110    |
| C25  | CB_5      | CBMH_4    | CONDUIT | 52.5   | 0.4991  | 0.0110    |
| C26  | CBMH_4    | CBMH_3    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C27  | CBMH_3    | CBMH_2    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C28  | CBMH_2    | MH_30     | CONDUIT | 53.4   | 0.4963  | 0.0110    |
| C29  | CBMH_12   | CBMH_11   | CONDUIT | 50.0   | 0.5700  | 0.0110    |
| C3   | J1        | MH_44     | CONDUIT | 2.5    | 0.4800  | 0.0110    |
| C30  | MH_30     | J13       | CONDUIT | 9.3    | 0.4839  | 0.0110    |
| C31  | MH_27     | CBMH_11   | CONDUIT | 8.2    | 0.5000  | 0.0110    |
| C32  | CBMH_11   | SU_S      | CONDUIT | 13.2   | 0.5000  | 0.0110    |
| C33  | OGS_1     | Humber_P1 | CONDUIT | 4.0    | 14.1135 | 0.0110    |
| C34  | OGS_2     | OF1       | CONDUIT | 8.7    | 0.6782  | 0.0110    |
| C35  | MH_25     | MH_24     | CONDUIT | 44.2   | 0.5000  | 0.0110    |
| C36  | CBMH_18   | SU_N      | CONDUIT | 3.9    | 0.5128  | 0.0110    |
| C37  | CB_29     | MH_27     | CONDUIT | 32.9   | 0.4985  | 0.0110    |
| C4   | SU_S      | MH_45     | CONDUIT | 9.4    | 1.0001  | 0.0090    |
| C5   | J2        | MH_45     | CONDUIT | 9.4    | 0.5000  | 0.0110    |
| C6   | MH_45     | OGS_1     | CONDUIT | 3.1    | 0.4839  | 0.0110    |
| C7   | DCB_16    | CBMH_15   | CONDUIT | 54.4   | 0.5000  | 0.0110    |
| C8   | CBMH_15   | CBMH_14   | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C9   | CBMH_14   | SU_N      | CONDUIT | 15.2   | 0.5000  | 0.0110    |
| OR1  | SU_S      | J2        | ORIFICE |        |         |           |
| OR2  | SU_N      | J1        | ORIFICE |        |         |           |

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Cross Section Summary  
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| Conduit | Shape    | Full Depth | Full Area | Hyd. Rad. | Max. Width | No. of Barrels | Full Flow |
|---------|----------|------------|-----------|-----------|------------|----------------|-----------|
| C1      | CIRCULAR | 0.20       | 0.03      | 0.05      | 0.20       | 1              | 0.05      |
| C10     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.34      |
| C11     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.34      |
| C12     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C13     | CIRCULAR | 0.60       | 0.28      | 0.15      | 0.60       | 1              | 0.51      |
| C14     | CIRCULAR | 0.38       | 0.11      | 0.09      | 0.38       | 1              | 0.21      |
| C15     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C16     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C17     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C18     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C19     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C2      | CIRCULAR | 0.38       | 0.11      | 0.09      | 0.38       | 1              | 0.13      |
| C20     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C21     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C22     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C23     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |

|     |          |      |      |      |      |   |      |
|-----|----------|------|------|------|------|---|------|
| C24 | CIRCULAR | 0.75 | 0.44 | 0.19 | 0.75 | 1 | 0.93 |
| C25 | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C26 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C27 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C28 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C29 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.16 |
| C3  | CIRCULAR | 0.30 | 0.07 | 0.07 | 0.30 | 1 | 0.08 |
| C30 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.50 |
| C31 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.15 |
| C32 | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C33 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.78 |
| C34 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.17 |
| C35 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C36 | CIRCULAR | 0.75 | 0.44 | 0.19 | 0.75 | 1 | 0.94 |
| C37 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.15 |
| C4  | CIRCULAR | 0.20 | 0.03 | 0.05 | 0.20 | 1 | 0.05 |
| C5  | CIRCULAR | 0.30 | 0.07 | 0.07 | 0.30 | 1 | 0.08 |
| C6  | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.14 |
| C7  | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C8  | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C9  | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |

\*\*\*\*\*  
NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
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\*\*\*\*\*  
Analysis Options  
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Flow Units ..... CMS  
Process Models:  
  Rainfall/Runoff ..... YES  
  RDII ..... NO  
  Snowmelt ..... NO  
  Groundwater ..... NO  
  Flow Routing ..... YES  
  Ponding Allowed ..... NO  
  Water Quality ..... NO  
Infiltration Method ..... HORTON  
Flow Routing Method ..... DYNWAVE  
Surcharge Method ..... EXTRAN  
Starting Date ..... 12/11/2020 00:00:00  
Ending Date ..... 12/21/2020 00:00:00  
Antecedent Dry Days ..... 0.0  
Report Time Step ..... 00:01:00  
Wet Time Step ..... 00:01:00  
Dry Time Step ..... 00:01:00  
Routing Time Step ..... 1.00 sec  
Variable Time Step ..... YES  
Maximum Trials ..... 8  
Number of Threads ..... 6  
Head Tolerance ..... 0.001500 m

| *****                      |           |        |
|----------------------------|-----------|--------|
|                            | Volume    | Depth  |
| Runoff Quantity Continuity | hectare-m | mm     |
| *****                      |           |        |
| -----                      |           |        |
| Total Precipitation .....  | 0.176     | 25.000 |
| Evaporation Loss .....     | 0.000     | 0.000  |
| Infiltration Loss .....    | 0.017     | 2.383  |
| Surface Runoff .....       | 0.160     | 22.630 |
| Final Storage .....        | 0.000     | 0.000  |
| Continuity Error (%) ..... | -0.049    |        |

| *****                       |           |          |
|-----------------------------|-----------|----------|
|                             | Volume    | Volume   |
| Flow Routing Continuity     | hectare-m | 10^6 ltr |
| *****                       |           |          |
| -----                       |           |          |
| Dry Weather Inflow .....    | 0.000     | 0.000    |
| Wet Weather Inflow .....    | 0.160     | 1.595    |
| Groundwater Inflow .....    | 0.000     | 0.000    |
| RDII Inflow .....           | 0.000     | 0.000    |
| External Inflow .....       | 0.000     | 0.000    |
| External Outflow .....      | 0.160     | 1.596    |
| Flooding Loss .....         | 0.000     | 0.000    |
| Evaporation Loss .....      | 0.000     | 0.000    |
| Exfiltration Loss .....     | 0.000     | 0.000    |
| Initial Stored Volume ..... | 0.000     | 0.000    |
| Final Stored Volume .....   | 0.000     | 0.000    |
| Continuity Error (%) .....  | -0.034    |          |

\*\*\*\*\*  
Time-Step Critical Elements  
\*\*\*\*\*  
None

\*\*\*\*\*  
Highest Flow Instability Indexes  
\*\*\*\*\*



Link C2 (2)  
 Link OR1 (1)  
 Link OR2 (1)

\*\*\*\*\*  
 Routing Time Step Summary  
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Minimum Time Step : 0.74 sec  
 Average Time Step : 1.00 sec  
 Maximum Time Step : 1.00 sec  
 Percent in Steady State : 0.00  
 Average Iterations per Step : 2.00  
 Percent Not Converging : 0.00  
 Time Step Frequencies :  
 1.000 - 0.871 sec : 99.97 %  
 0.871 - 0.758 sec : 0.03 %  
 0.758 - 0.660 sec : 0.00 %  
 0.660 - 0.574 sec : 0.00 %  
 0.574 - 0.500 sec : 0.00 %

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 Subcatchment Runoff Summary  
 \*\*\*\*\*

| Subcatchment | Total Precip<br>mm | Total Runon<br>mm | Total Evap<br>mm | Total Infil<br>mm | Imperv Runoff<br>mm | Perv Runoff<br>mm | Total Runoff<br>mm | Total Runoff<br>10 <sup>6</sup> ltr | Peak Runoff<br>CMS | Runoff Coeff |
|--------------|--------------------|-------------------|------------------|-------------------|---------------------|-------------------|--------------------|-------------------------------------|--------------------|--------------|
| Area_1       | 25.00              | 0.00              | 0.00             | 2.48              | 22.52               | 0.02              | 22.54              | 0.06                                | 0.04               | 0.902        |
| Area_10      | 25.00              | 0.00              | 0.00             | 2.48              | 22.52               | 0.02              | 22.54              | 0.02                                | 0.01               | 0.902        |
| Area_101     | 25.00              | 0.00              | 0.00             | 1.24              | 23.76               | 0.01              | 23.76              | 0.33                                | 0.19               | 0.951        |
| Area_102     | 25.00              | 0.00              | 0.00             | 1.24              | 23.76               | 0.01              | 23.76              | 0.27                                | 0.16               | 0.951        |
| Area_11      | 25.00              | 0.00              | 0.00             | 2.48              | 22.52               | 0.02              | 22.54              | 0.03                                | 0.02               | 0.902        |
| Area_12      | 25.00              | 0.00              | 0.00             | 2.48              | 22.52               | 0.02              | 22.54              | 0.04                                | 0.02               | 0.902        |
| Area_13      | 25.00              | 0.00              | 0.00             | 2.48              | 22.52               | 0.02              | 22.54              | 0.04                                | 0.02               | 0.902        |
| Area_14      | 25.00              | 0.00              | 0.00             | 2.48              | 22.52               | 0.02              | 22.54              | 0.04                                | 0.03               | 0.902        |
| Area_15      | 25.00              | 0.00              | 0.00             | 2.48              | 22.52               | 0.02              | 22.54              | 0.02                                | 0.01               | 0.902        |
| Area_16      | 25.00              | 0.00              | 0.00             | 2.48              | 22.52               | 0.02              | 22.54              | 0.03                                | 0.02               | 0.902        |
| Area_17      | 25.00              | 0.00              | 0.00             | 2.48              | 22.52               | 0.02              | 22.54              | 0.04                                | 0.03               | 0.902        |
| Area_18      | 25.00              | 0.00              | 0.00             | 2.48              | 22.52               | 0.02              | 22.54              | 0.04                                | 0.03               | 0.902        |
| Area_19      | 25.00              | 0.00              | 0.00             | 2.48              | 22.52               | 0.02              | 22.54              | 0.04                                | 0.03               | 0.902        |
| Area_2       | 25.00              | 0.00              | 0.00             | 2.48              | 22.52               | 0.02              | 22.54              | 0.04                                | 0.02               | 0.902        |
| Area_20      | 25.00              | 0.00              | 0.00             | 2.48              | 22.52               | 0.02              | 22.54              | 0.06                                | 0.04               | 0.902        |
| Area_2001    | 25.00              | 0.00              | 0.00             | 18.74             | 6.25                | 0.01              | 6.27               | 0.00                                | 0.00               | 0.251        |
| Area_2002    | 25.00              | 0.00              | 0.00             | 2.49              | 22.51               | 0.01              | 22.52              | 0.05                                | 0.03               | 0.901        |
| Area_2003    | 25.00              | 0.00              | 0.00             | 2.50              | 22.51               | 0.00              | 22.51              | 0.04                                | 0.02               | 0.900        |
| Area_2004    | 25.00              | 0.00              | 0.00             | 23.68             | 1.25                | 0.07              | 1.32               | 0.00                                | 0.00               | 0.053        |
| Area_2005    | 25.00              | 0.00              | 0.00             | 23.68             | 1.25                | 0.07              | 1.32               | 0.00                                | 0.00               | 0.053        |
| Area_21      | 25.00              | 0.00              | 0.00             | 2.48              | 22.52               | 0.02              | 22.54              | 0.05                                | 0.03               | 0.902        |
| Area_22      | 25.00              | 0.00              | 0.00             | 2.48              | 22.52               | 0.02              | 22.54              | 0.07                                | 0.05               | 0.902        |
| Area_23      | 25.00              | 0.00              | 0.00             | 2.48              | 22.52               | 0.02              | 22.54              | 0.04                                | 0.02               | 0.902        |
| Area_3       | 25.00              | 0.00              | 0.00             | 2.48              | 22.52               | 0.02              | 22.54              | 0.08                                | 0.06               | 0.902        |
| Area_4       | 25.00              | 0.00              | 0.00             | 2.48              | 22.52               | 0.02              | 22.54              | 0.06                                | 0.04               | 0.902        |
| Area_5       | 25.00              | 0.00              | 0.00             | 2.48              | 22.52               | 0.02              | 22.54              | 0.03                                | 0.02               | 0.902        |
| Area_6       | 25.00              | 0.00              | 0.00             | 2.48              | 22.52               | 0.02              | 22.54              | 0.03                                | 0.02               | 0.902        |
| Area_7       | 25.00              | 0.00              | 0.00             | 2.48              | 22.52               | 0.02              | 22.54              | 0.01                                | 0.01               | 0.902        |
| Area_8       | 25.00              | 0.00              | 0.00             | 2.48              | 22.52               | 0.02              | 22.54              | 0.03                                | 0.02               | 0.902        |
| Area_9       | 25.00              | 0.00              | 0.00             | 2.48              | 22.52               | 0.02              | 22.54              | 0.03                                | 0.02               | 0.902        |

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 Node Depth Summary  
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| Node    | Type     | Average Depth<br>Meters | Maximum Depth<br>Meters | Maximum HGL<br>Meters | Time of Max Occurrence<br>days hr:min | Reported Max Depth<br>Meters |
|---------|----------|-------------------------|-------------------------|-----------------------|---------------------------------------|------------------------------|
| CB_10   | JUNCTION | 0.00                    | 0.09                    | 65.42                 | 0 01:40                               | 0.09                         |
| CB_23   | JUNCTION | 0.00                    | 0.06                    | 66.26                 | 0 01:40                               | 0.06                         |
| CB_27   | JUNCTION | 0.00                    | 0.08                    | 65.56                 | 0 01:40                               | 0.08                         |
| CB_28   | JUNCTION | 0.00                    | 0.08                    | 65.47                 | 0 01:40                               | 0.08                         |
| CB_29   | JUNCTION | 0.00                    | 0.10                    | 64.22                 | 0 01:40                               | 0.10                         |
| CB_5    | JUNCTION | 0.00                    | 0.09                    | 65.20                 | 0 01:40                               | 0.09                         |
| CBMH_11 | JUNCTION | 0.01                    | 0.35                    | 63.93                 | 0 04:04                               | 0.35                         |
| CBMH_12 | JUNCTION | 0.00                    | 0.14                    | 64.20                 | 0 01:40                               | 0.14                         |
| CBMH_14 | JUNCTION | 0.01                    | 0.38                    | 64.49                 | 0 04:02                               | 0.38                         |
| CBMH_15 | JUNCTION | 0.00                    | 0.17                    | 64.63                 | 0 01:40                               | 0.17                         |
| CBMH_18 | JUNCTION | 0.02                    | 0.44                    | 64.49                 | 0 04:03                               | 0.44                         |
| CBMH_19 | JUNCTION | 0.00                    | 0.15                    | 65.02                 | 0 01:40                               | 0.15                         |
| CBMH_2  | JUNCTION | 0.00                    | 0.18                    | 64.24                 | 0 01:40                               | 0.18                         |
| CBMH_21 | JUNCTION | 0.00                    | 0.14                    | 65.31                 | 0 01:40                               | 0.14                         |
| CBMH_22 | JUNCTION | 0.00                    | 0.11                    | 65.64                 | 0 01:40                               | 0.11                         |
| CBMH_3  | JUNCTION | 0.00                    | 0.15                    | 64.57                 | 0 01:40                               | 0.15                         |
| CBMH_4  | JUNCTION | 0.00                    | 0.13                    | 64.90                 | 0 01:40                               | 0.13                         |
| CBMH_6  | JUNCTION | 0.00                    | 0.20                    | 64.11                 | 0 01:40                               | 0.20                         |
| CBMH_7  | JUNCTION | 0.00                    | 0.18                    | 64.46                 | 0 01:40                               | 0.18                         |
| CBMH_8  | JUNCTION | 0.00                    | 0.16                    | 64.79                 | 0 01:40                               | 0.16                         |
| CBMH_9  | JUNCTION | 0.00                    | 0.12                    | 65.12                 | 0 01:40                               | 0.12                         |
| DCB_16  | JUNCTION | 0.00                    | 0.14                    | 64.94                 | 0 01:40                               | 0.14                         |
| J1      | JUNCTION | 0.01                    | 0.07                    | 63.82                 | 0 04:01                               | 0.07                         |

|           |          |      |      |       |   |       |      |
|-----------|----------|------|------|-------|---|-------|------|
| J13       | JUNCTION | 0.02 | 0.40 | 63.94 | 0 | 04:04 | 0.40 |
| J2        | JUNCTION | 0.01 | 0.07 | 63.31 | 0 | 04:05 | 0.07 |
| MH_20     | JUNCTION | 0.00 | 0.14 | 65.13 | 0 | 01:40 | 0.14 |
| MH_24     | JUNCTION | 0.01 | 0.35 | 64.49 | 0 | 04:03 | 0.35 |
| MH_25     | JUNCTION | 0.00 | 0.29 | 64.70 | 0 | 01:40 | 0.28 |
| MH_26     | JUNCTION | 0.00 | 0.31 | 64.87 | 0 | 01:40 | 0.31 |
| MH_27     | JUNCTION | 0.00 | 0.10 | 63.99 | 0 | 01:40 | 0.10 |
| MH_30     | JUNCTION | 0.01 | 0.20 | 63.94 | 0 | 04:03 | 0.20 |
| MH_44     | JUNCTION | 0.01 | 0.07 | 63.58 | 0 | 04:02 | 0.07 |
| MH_45     | JUNCTION | 0.01 | 0.07 | 63.18 | 0 | 04:05 | 0.07 |
| OGS_1     | JUNCTION | 0.00 | 0.03 | 63.07 | 0 | 04:05 | 0.03 |
| OGS_2     | JUNCTION | 0.01 | 0.06 | 63.53 | 0 | 04:02 | 0.06 |
| Humber_P1 | OUTFALL  | 0.00 | 0.00 | 62.48 | 0 | 00:00 | 0.00 |
| OF1       | OUTFALL  | 0.01 | 0.06 | 63.47 | 0 | 04:02 | 0.06 |
| OF2       | OUTFALL  | 0.00 | 0.00 | 0.00  | 0 | 00:00 | 0.00 |
| SU_N      | STORAGE  | 0.05 | 0.74 | 64.49 | 0 | 04:01 | 0.74 |
| SU_S      | STORAGE  | 0.05 | 0.70 | 63.93 | 0 | 04:05 | 0.70 |

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Node Inflow Summary  
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| Node      | Type     | Maximum Lateral Inflow CMS | Maximum Total Inflow CMS | Time of Max Occurrence days hr:min | Lateral Inflow Volume 10^6 ltr | Total Inflow Volume 10^6 ltr | Flow Balance Error Percent |
|-----------|----------|----------------------------|--------------------------|------------------------------------|--------------------------------|------------------------------|----------------------------|
| CB_10     | JUNCTION | 0.020                      | 0.020                    | 0 01:40                            | 0.0293                         | 0.0293                       | -0.009                     |
| CB_23     | JUNCTION | 0.012                      | 0.012                    | 0 01:40                            | 0.018                          | 0.018                        | -0.006                     |
| CB_27     | JUNCTION | 0.023                      | 0.023                    | 0 01:40                            | 0.0338                         | 0.0338                       | -0.003                     |
| CB_28     | JUNCTION | 0.023                      | 0.023                    | 0 01:40                            | 0.0338                         | 0.0338                       | -0.003                     |
| CB_29     | JUNCTION | 0.025                      | 0.025                    | 0 01:40                            | 0.0361                         | 0.0361                       | -0.005                     |
| CB_5      | JUNCTION | 0.023                      | 0.023                    | 0 01:40                            | 0.0338                         | 0.0338                       | -0.010                     |
| CBMH_11   | JUNCTION | 0.189                      | 0.262                    | 0 01:40                            | 0.316                          | 0.424                        | 0.077                      |
| CBMH_12   | JUNCTION | 0.049                      | 0.049                    | 0 01:40                            | 0.0721                         | 0.0721                       | 0.212                      |
| CBMH_14   | JUNCTION | 0.038                      | 0.118                    | 0 01:40                            | 0.0563                         | 0.179                        | -0.120                     |
| CBMH_15   | JUNCTION | 0.025                      | 0.080                    | 0 01:40                            | 0.0361                         | 0.117                        | 0.514                      |
| CBMH_18   | JUNCTION | 0.043                      | 0.330                    | 0 01:40                            | 0.0631                         | 0.543                        | 0.004                      |
| CBMH_19   | JUNCTION | 0.006                      | 0.055                    | 0 01:40                            | 0.00902                        | 0.0811                       | -0.006                     |
| CBMH_2    | JUNCTION | 0.026                      | 0.101                    | 0 01:40                            | 0.0383                         | 0.149                        | 0.169                      |
| CBMH_21   | JUNCTION | 0.018                      | 0.049                    | 0 01:40                            | 0.027                          | 0.0721                       | -0.003                     |
| CBMH_22   | JUNCTION | 0.018                      | 0.031                    | 0 01:40                            | 0.027                          | 0.0451                       | -0.007                     |
| CBMH_3    | JUNCTION | 0.026                      | 0.075                    | 0 01:40                            | 0.0383                         | 0.11                         | -0.011                     |
| CBMH_4    | JUNCTION | 0.026                      | 0.049                    | 0 01:40                            | 0.0383                         | 0.0721                       | -0.008                     |
| CBMH_6    | JUNCTION | 0.014                      | 0.108                    | 0 01:40                            | 0.0203                         | 0.16                         | 0.120                      |
| CBMH_7    | JUNCTION | 0.026                      | 0.095                    | 0 01:40                            | 0.0383                         | 0.14                         | -0.007                     |
| CBMH_8    | JUNCTION | 0.025                      | 0.069                    | 0 01:40                            | 0.0361                         | 0.101                        | -0.010                     |
| CBMH_9    | JUNCTION | 0.025                      | 0.044                    | 0 01:40                            | 0.0361                         | 0.0654                       | -0.007                     |
| DCB_16    | JUNCTION | 0.055                      | 0.055                    | 0 01:40                            | 0.0811                         | 0.0811                       | -0.010                     |
| J1        | JUNCTION | 0.000                      | 0.010                    | 0 04:01                            | 0                              | 0.711                        | -0.006                     |
| J13       | JUNCTION | 0.043                      | 0.251                    | 0 01:40                            | 0.0631                         | 0.378                        | -0.053                     |
| J2        | JUNCTION | 0.000                      | 0.010                    | 0 04:05                            | 0                              | 0.796                        | -0.006                     |
| MH_20     | JUNCTION | 0.000                      | 0.049                    | 0 01:40                            | 0                              | 0.0721                       | -0.001                     |
| MH_24     | JUNCTION | 0.000                      | 0.290                    | 0 01:40                            | 0                              | 0.476                        | -0.198                     |
| MH_25     | JUNCTION | 0.000                      | 0.235                    | 0 01:40                            | 0                              | 0.393                        | 0.257                      |
| MH_26     | JUNCTION | 0.190                      | 0.236                    | 0 01:40                            | 0.326                          | 0.393                        | -0.000                     |
| MH_27     | JUNCTION | 0.000                      | 0.024                    | 0 01:40                            | 0                              | 0.0361                       | 0.014                      |
| MH_30     | JUNCTION | 0.000                      | 0.101                    | 0 01:40                            | 0                              | 0.151                        | -0.116                     |
| MH_44     | JUNCTION | 0.000                      | 0.010                    | 0 04:01                            | 0                              | 0.711                        | 0.007                      |
| MH_45     | JUNCTION | 0.000                      | 0.010                    | 0 04:05                            | 0                              | 0.796                        | 0.001                      |
| OGS_1     | JUNCTION | 0.000                      | 0.010                    | 0 04:05                            | 0                              | 0.796                        | -0.001                     |
| OGS_2     | JUNCTION | 0.000                      | 0.010                    | 0 04:02                            | 0                              | 0.711                        | -0.007                     |
| Humber_P1 | OUTFALL  | 0.001                      | 0.010                    | 0 04:00                            | 0.000793                       | 0.797                        | 0.000                      |
| OF1       | OUTFALL  | 0.023                      | 0.030                    | 0 01:40                            | 0.036                          | 0.747                        | 0.000                      |
| OF2       | OUTFALL  | 0.031                      | 0.031                    | 0 01:40                            | 0.0517                         | 0.0517                       | 0.000                      |
| SU_N      | STORAGE  | 0.000                      | 0.448                    | 0 01:40                            | 0                              | 0.719                        | -0.099                     |
| SU_S      | STORAGE  | 0.000                      | 0.513                    | 0 01:40                            | 0                              | 0.799                        | -0.085                     |

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Node Surcharge Summary  
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No nodes were surcharged.

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Node Flooding Summary  
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No nodes were flooded.

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Storage Volume Summary  
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| Storage Unit | Average Volume 1000 m3 | Avg Full | Evap Loss | Exfil Loss | Maximum Volume 1000 m3 | Max Full | Time of Max Occurrence days hr:min | Maximum Outflow CMS |
|--------------|------------------------|----------|-----------|------------|------------------------|----------|------------------------------------|---------------------|
| SU_N         | 0.032                  | 1        | 0         | 0          | 0.587                  | 23       | 0 04:01                            | 0.012               |

SU\_s 0.043 1 0 0 0.680 20 0 04:05 0.013

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 Outfall Loading Summary  
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| Outfall Node | Flow Freq Pent | Avg Flow CMS | Max Flow CMS | Total Volume 10^6 ltr |
|--------------|----------------|--------------|--------------|-----------------------|
| Humber_Pl    | 24.35          | 0.004        | 0.010        | 0.797                 |
| OF1          | 20.58          | 0.004        | 0.030        | 0.747                 |
| OF2          | 2.58           | 0.002        | 0.031        | 0.052                 |
| System       | 15.84          | 0.010        | 0.069        | 1.596                 |

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 Link Flow Summary  
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| Link | Type    | Maximum  Flow  CMS | Time of Max Occurrence days hr:min | Maximum  Veloc  m/sec | Max/ Full Flow | Max/ Full Depth |
|------|---------|--------------------|------------------------------------|-----------------------|----------------|-----------------|
| C1   | CONDUIT | 0.000              | 0 00:00                            | 0.00                  | 0.00           | 0.00            |
| C10  | CONDUIT | 0.023              | 0 01:40                            | 1.21                  | 0.07           | 0.18            |
| C11  | CONDUIT | 0.023              | 0 01:40                            | 1.21                  | 0.07           | 0.18            |
| C12  | CONDUIT | 0.235              | 0 01:40                            | 1.77                  | 0.66           | 0.59            |
| C13  | CONDUIT | 0.290              | 0 01:40                            | 1.87                  | 0.56           | 0.61            |
| C14  | CONDUIT | 0.012              | 0 01:40                            | 1.03                  | 0.06           | 0.16            |
| C15  | CONDUIT | 0.031              | 0 01:40                            | 1.03                  | 0.13           | 0.24            |
| C16  | CONDUIT | 0.049              | 0 01:40                            | 1.18                  | 0.20           | 0.31            |
| C17  | CONDUIT | 0.049              | 0 01:40                            | 1.18                  | 0.21           | 0.31            |
| C18  | CONDUIT | 0.055              | 0 01:40                            | 1.22                  | 0.23           | 0.33            |
| C19  | CONDUIT | 0.020              | 0 01:40                            | 0.91                  | 0.08           | 0.20            |
| C2   | CONDUIT | 0.010              | 0 04:02                            | 0.78                  | 0.08           | 0.18            |
| C20  | CONDUIT | 0.044              | 0 01:40                            | 1.13                  | 0.12           | 0.24            |
| C21  | CONDUIT | 0.069              | 0 01:40                            | 1.28                  | 0.19           | 0.30            |
| C22  | CONDUIT | 0.094              | 0 01:40                            | 1.40                  | 0.26           | 0.35            |
| C23  | CONDUIT | 0.108              | 0 01:40                            | 1.46                  | 0.30           | 0.38            |
| C24  | CONDUIT | 0.251              | 0 01:40                            | 1.79                  | 0.27           | 0.54            |
| C25  | CONDUIT | 0.023              | 0 01:40                            | 0.93                  | 0.06           | 0.17            |
| C26  | CONDUIT | 0.049              | 0 01:40                            | 1.15                  | 0.10           | 0.21            |
| C27  | CONDUIT | 0.075              | 0 01:40                            | 1.30                  | 0.15           | 0.26            |
| C28  | CONDUIT | 0.101              | 0 01:40                            | 1.41                  | 0.20           | 0.30            |
| C29  | CONDUIT | 0.049              | 0 01:40                            | 1.26                  | 0.31           | 0.38            |
| C3   | CONDUIT | 0.010              | 0 04:01                            | 0.78                  | 0.13           | 0.24            |
| C30  | CONDUIT | 0.101              | 0 01:40                            | 1.39                  | 0.20           | 0.38            |
| C31  | CONDUIT | 0.024              | 0 01:40                            | 0.99                  | 0.17           | 0.28            |
| C32  | CONDUIT | 0.262              | 0 01:40                            | 1.82                  | 0.73           | 0.73            |
| C33  | CONDUIT | 0.010              | 0 04:05                            | 2.44                  | 0.01           | 0.08            |
| C34  | CONDUIT | 0.010              | 0 04:02                            | 0.85                  | 0.06           | 0.17            |
| C35  | CONDUIT | 0.235              | 0 01:40                            | 1.78                  | 0.46           | 0.48            |
| C36  | CONDUIT | 0.330              | 0 01:40                            | 1.94                  | 0.35           | 0.60            |
| C37  | CONDUIT | 0.024              | 0 01:40                            | 0.99                  | 0.17           | 0.28            |
| C4   | CONDUIT | 0.000              | 0 00:00                            | 0.00                  | 0.00           | 0.00            |
| C5   | CONDUIT | 0.010              | 0 04:05                            | 0.78                  | 0.12           | 0.24            |
| C6   | CONDUIT | 0.010              | 0 04:05                            | 0.75                  | 0.07           | 0.18            |
| C7   | CONDUIT | 0.055              | 0 01:40                            | 1.21                  | 0.15           | 0.26            |
| C8   | CONDUIT | 0.079              | 0 01:40                            | 1.34                  | 0.22           | 0.33            |
| C9   | CONDUIT | 0.118              | 0 01:40                            | 1.48                  | 0.23           | 0.70            |
| OR1  | ORIFICE | 0.010              | 0 04:05                            |                       |                | 1.00            |
| OR2  | ORIFICE | 0.010              | 0 04:01                            |                       |                | 1.00            |

\*\*\*\*\*  
 Flow Classification Summary  
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| Conduit | Adjusted /Actual Length | Fraction of Time in Flow Class |          |         |          |         |           |           |           |      |
|---------|-------------------------|--------------------------------|----------|---------|----------|---------|-----------|-----------|-----------|------|
|         |                         | Up Dry                         | Down Dry | Sub Dry | Sup Crit | Up Crit | Down Crit | Norm Crit | Inlet Ltd | Ctrl |
| C1      | 1.00                    | 1.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 0.00      | 0.00      | 0.00 |
| C10     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C11     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C12     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C13     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.06     | 0.00    | 0.00      | 0.94      | 0.00      | 0.00 |
| C14     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C15     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C16     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C17     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C18     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C19     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C2      | 1.00                    | 0.00                           | 0.10     | 0.00    | 0.79     | 0.12    | 0.00      | 0.00      | 0.79      | 0.00 |
| C20     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C21     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C22     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C23     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.04     | 0.00    | 0.00      | 0.96      | 0.03      | 0.00 |
| C24     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.08     | 0.00    | 0.00      | 0.92      | 0.00      | 0.00 |

|     |      |      |      |      |      |      |      |      |      |      |
|-----|------|------|------|------|------|------|------|------|------|------|
| C25 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C26 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C27 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C28 | 1.00 | 0.00 | 0.00 | 0.00 | 0.03 | 0.00 | 0.00 | 0.97 | 0.03 | 0.00 |
| C29 | 1.00 | 0.00 | 0.00 | 0.00 | 0.04 | 0.00 | 0.00 | 0.96 | 0.04 | 0.00 |
| C3  | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C30 | 1.00 | 0.00 | 0.00 | 0.00 | 0.05 | 0.00 | 0.00 | 0.95 | 0.01 | 0.00 |
| C31 | 1.00 | 0.00 | 0.00 | 0.00 | 0.02 | 0.00 | 0.00 | 0.98 | 0.01 | 0.00 |
| C32 | 1.00 | 0.00 | 0.00 | 0.00 | 0.08 | 0.00 | 0.00 | 0.92 | 0.01 | 0.00 |
| C33 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C34 | 1.00 | 0.00 | 0.00 | 0.00 | 0.77 | 0.23 | 0.00 | 0.00 | 0.04 | 0.00 |
| C35 | 1.00 | 0.00 | 0.00 | 0.00 | 0.05 | 0.00 | 0.00 | 0.95 | 0.04 | 0.00 |
| C36 | 1.00 | 0.00 | 0.00 | 0.00 | 0.07 | 0.00 | 0.00 | 0.93 | 0.00 | 0.00 |
| C37 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C4  | 1.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| C5  | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C6  | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C7  | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C8  | 1.00 | 0.00 | 0.00 | 0.00 | 0.05 | 0.00 | 0.00 | 0.95 | 0.05 | 0.00 |
| C9  | 1.00 | 0.00 | 0.00 | 0.00 | 0.07 | 0.00 | 0.00 | 0.93 | 0.01 | 0.00 |

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 Conduit Surcharge Summary  
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No conduits were surcharged.

Analysis begun on: Wed Oct 5 20:17:15 2022  
 Analysis ended on: Wed Oct 5 20:17:45 2022

Total elapsed time: 00:00:30

2-yr, 3-hour

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.015)

WARNING 03: negative offset ignored for Link C2  
 WARNING 03: negative offset ignored for Link C32  
 WARNING 03: negative offset ignored for Link C34

\*\*\*\*\*  
 Element Count  
 \*\*\*\*\*  
 Number of rain gages ..... 7  
 Number of subcatchments ... 30  
 Number of nodes ..... 40  
 Number of links ..... 39  
 Number of pollutants ..... 0  
 Number of land uses ..... 0

\*\*\*\*\*  
 Raingage Summary  
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| Name      | Data Source | Data Type | Recording Interval |
|-----------|-------------|-----------|--------------------|
| 25mm      | 25mm        | INTENSITY | 5 min.             |
| 3hr-100yr | 3hr-100yr   | INTENSITY | 10 min.            |
| 3hr-2yr   | 3hr-2yr     | INTENSITY | 5 min.             |
| 3hr-5yr   | 3hr-5yr     | INTENSITY | 5 min.             |
| 6hr-100yr | 6hr-100yr   | INTENSITY | 10 min.            |
| 6hr-2yr   | 6hr-2yr     | INTENSITY | 5 min.             |
| 6hr-5yr   | 6hr-5yr     | INTENSITY | 5 min.             |

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 Subcatchment Summary  
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| Name      | Area | Width  | %Imperv | %Slope | Rain Gage | Outlet    |
|-----------|------|--------|---------|--------|-----------|-----------|
| Area_1    | 0.25 | 83.33  | 90.00   | 1.0000 | 3hr-2yr   | CBMH_14   |
| Area_10   | 0.08 | 26.67  | 90.00   | 1.0000 | 3hr-2yr   | CB_23     |
| Area_101  | 1.37 | 137.00 | 95.00   | 0.5000 | 3hr-2yr   | MH_26     |
| Area_102  | 1.13 | 113.00 | 95.00   | 0.5000 | 3hr-2yr   | CBMH_11   |
| Area_11   | 0.13 | 43.33  | 90.00   | 1.0000 | 3hr-2yr   | CB_10     |
| Area_12   | 0.16 | 53.33  | 90.00   | 1.0000 | 3hr-2yr   | CBMH_9    |
| Area_13   | 0.16 | 53.33  | 90.00   | 1.0000 | 3hr-2yr   | CBMH_8    |
| Area_14   | 0.17 | 56.67  | 90.00   | 1.0000 | 3hr-2yr   | CBMH_7    |
| Area_15   | 0.09 | 30.00  | 90.00   | 1.0000 | 3hr-2yr   | CBMH_6    |
| Area_16   | 0.15 | 50.00  | 90.00   | 1.0000 | 3hr-2yr   | CB_5      |
| Area_17   | 0.17 | 56.67  | 90.00   | 1.0000 | 3hr-2yr   | CBMH_4    |
| Area_18   | 0.17 | 56.67  | 90.00   | 1.0000 | 3hr-2yr   | CBMH_3    |
| Area_19   | 0.17 | 56.67  | 90.00   | 1.0000 | 3hr-2yr   | CBMH_2    |
| Area_2    | 0.16 | 53.33  | 90.00   | 1.0000 | 3hr-2yr   | CBMH_15   |
| Area_20   | 0.28 | 93.33  | 90.00   | 1.0000 | 3hr-2yr   | J13       |
| Area_2001 | 0.07 | 7.00   | 25.00   | 0.5000 | 3hr-2yr   | OF2       |
| Area_2002 | 0.21 | 21.00  | 90.00   | 0.5000 | 3hr-2yr   | OF2       |
| Area_2003 | 0.16 | 16.00  | 90.00   | 1.0000 | 3hr-2yr   | OF1       |
| Area_2004 | 0.02 | 13.33  | 5.00    | 0.5000 | 3hr-2yr   | Humber_P1 |
| Area_2005 | 0.04 | 26.67  | 5.00    | 0.5000 | 3hr-2yr   | Humber_P1 |
| Area_21   | 0.21 | 70.00  | 90.00   | 1.0000 | 3hr-2yr   | CBMH_11   |
| Area_22   | 0.32 | 106.67 | 90.00   | 1.0000 | 3hr-2yr   | CBMH_12   |
| Area_23   | 0.16 | 53.33  | 90.00   | 1.0000 | 3hr-2yr   | CB_29     |
| Area_3    | 0.36 | 120.00 | 90.00   | 1.0000 | 3hr-2yr   | DCB_16    |
| Area_4    | 0.28 | 93.33  | 90.00   | 1.0000 | 3hr-2yr   | CBMH_18   |
| Area_5    | 0.15 | 50.00  | 90.00   | 1.0000 | 3hr-2yr   | CB_27     |
| Area_6    | 0.15 | 50.00  | 90.00   | 1.0000 | 3hr-2yr   | CB_28     |
| Area_7    | 0.04 | 13.33  | 90.00   | 1.0000 | 3hr-2yr   | CBMH_19   |
| Area_8    | 0.12 | 40.00  | 90.00   | 1.0000 | 3hr-2yr   | CBMH_21   |
| Area_9    | 0.12 | 40.00  | 90.00   | 1.0000 | 3hr-2yr   | CBMH_22   |

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 Node Summary  
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| Name    | Type     | Invert Elev. | Max. Depth | Ponded Area | External Inflow |
|---------|----------|--------------|------------|-------------|-----------------|
| CB_10   | JUNCTION | 65.33        | 1.41       | 10.0        |                 |
| CB_23   | JUNCTION | 66.20        | 0.93       | 10.0        |                 |
| CB_27   | JUNCTION | 65.48        | 1.34       | 10.0        |                 |
| CB_28   | JUNCTION | 65.39        | 1.52       | 10.0        |                 |
| CB_29   | JUNCTION | 64.11        | 2.43       | 0.0         |                 |
| CB_5    | JUNCTION | 65.11        | 1.63       | 10.0        |                 |
| CBMH_11 | JUNCTION | 63.58        | 2.16       | 10.0        |                 |
| CBMH_12 | JUNCTION | 64.06        | 1.68       | 10.0        |                 |
| CBMH_14 | JUNCTION | 64.11        | 2.21       | 10.0        |                 |
| CBMH_15 | JUNCTION | 64.47        | 1.85       | 10.0        |                 |
| CBMH_18 | JUNCTION | 64.05        | 2.54       | 0.0         |                 |
| CBMH_19 | JUNCTION | 64.88        | 2.38       | 10.0        |                 |
| CBMH_2  | JUNCTION | 64.06        | 2.94       | 10.0        |                 |
| CBMH_21 | JUNCTION | 65.17        | 1.87       | 10.0        |                 |
| CBMH_22 | JUNCTION | 65.53        | 1.51       | 10.0        |                 |

|           |          |       |      |      |
|-----------|----------|-------|------|------|
| CBMH_3    | JUNCTION | 64.42 | 2.58 | 10.0 |
| CBMH_4    | JUNCTION | 64.78 | 2.22 | 10.0 |
| CBMH_6    | JUNCTION | 63.91 | 2.73 | 10.0 |
| CBMH_7    | JUNCTION | 64.27 | 2.73 | 10.0 |
| CBMH_8    | JUNCTION | 64.63 | 2.37 | 10.0 |
| CBMH_9    | JUNCTION | 64.99 | 2.01 | 10.0 |
| DCB_16    | JUNCTION | 64.80 | 1.52 | 10.0 |
| J1        | JUNCTION | 63.75 | 3.27 | 0.0  |
| J13       | JUNCTION | 63.54 | 3.10 | 10.0 |
| J2        | JUNCTION | 63.24 | 3.33 | 0.0  |
| MH_20     | JUNCTION | 64.99 | 2.30 | 0.0  |
| MH_24     | JUNCTION | 64.13 | 2.50 | 10.0 |
| MH_25     | JUNCTION | 64.42 | 2.63 | 0.0  |
| MH_26     | JUNCTION | 64.56 | 2.70 | 0.0  |
| MH_27     | JUNCTION | 63.89 | 2.02 | 0.0  |
| MH_30     | JUNCTION | 63.73 | 3.08 | 0.0  |
| MH_44     | JUNCTION | 63.51 | 3.51 | 0.0  |
| MH_45     | JUNCTION | 63.11 | 3.46 | 0.0  |
| OGS_1     | JUNCTION | 63.04 | 3.34 | 0.0  |
| OGS_2     | JUNCTION | 63.47 | 3.01 | 0.0  |
| Humber_P1 | OUTFALL  | 62.48 | 0.38 | 0.0  |
| OF1       | OUTFALL  | 63.41 | 0.38 | 0.0  |
| OF2       | OUTFALL  | 0.00  | 0.00 | 0.0  |
| SU_N      | STORAGE  | 63.75 | 3.04 | 0.0  |
| SU_S      | STORAGE  | 63.24 | 3.33 | 0.0  |

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Link Summary  
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| Name | From Node | To Node   | Type    | Length | %Slope  | Roughness |
|------|-----------|-----------|---------|--------|---------|-----------|
| C1   | SU_N      | MH_44     | CONDUIT | 2.5    | 1.0001  | 0.0090    |
| C10  | CB_28     | MH_26     | CONDUIT | 30.4   | 1.0001  | 0.0110    |
| C11  | CB_27     | MH_26     | CONDUIT | 32.8   | 1.0001  | 0.0110    |
| C12  | MH_26     | MH_25     | CONDUIT | 16.5   | 0.4970  | 0.0110    |
| C13  | MH_24     | CBMH_18   | CONDUIT | 4.8    | 0.5000  | 0.0110    |
| C14  | CB_23     | CBMH_22   | CONDUIT | 51.5   | 1.0001  | 0.0110    |
| C15  | CBMH_22   | CBMH_21   | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C16  | CBMH_21   | MH_20     | CONDUIT | 24.5   | 0.5020  | 0.0110    |
| C17  | MH_20     | CBMH_19   | CONDUIT | 10.4   | 0.5000  | 0.0110    |
| C18  | CBMH_19   | MH_24     | CONDUIT | 46.5   | 0.5011  | 0.0110    |
| C19  | CB_10     | CBMH_9    | CONDUIT | 52.5   | 0.4991  | 0.0110    |
| C2   | MH_44     | OGS_2     | CONDUIT | 11.6   | 0.3707  | 0.0110    |
| C20  | CBMH_9    | CBMH_8    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C21  | CBMH_8    | CBMH_7    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C22  | CBMH_7    | CBMH_6    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C23  | CBMH_6    | J13       | CONDUIT | 29.9   | 0.5017  | 0.0110    |
| C24  | J13       | SU_S      | CONDUIT | 4.0    | 0.5000  | 0.0110    |
| C25  | CB_5      | CBMH_4    | CONDUIT | 52.5   | 0.4991  | 0.0110    |
| C26  | CBMH_4    | CBMH_3    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C27  | CBMH_3    | CBMH_2    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C28  | CBMH_2    | MH_30     | CONDUIT | 53.4   | 0.4963  | 0.0110    |
| C29  | CBMH_12   | CBMH_11   | CONDUIT | 50.0   | 0.5700  | 0.0110    |
| C3   | J1        | MH_44     | CONDUIT | 2.5    | 0.4800  | 0.0110    |
| C30  | MH_30     | J13       | CONDUIT | 9.3    | 0.4839  | 0.0110    |
| C31  | MH_27     | CBMH_11   | CONDUIT | 8.2    | 0.5000  | 0.0110    |
| C32  | CBMH_11   | SU_S      | CONDUIT | 13.2   | 0.5000  | 0.0110    |
| C33  | OGS_1     | Humber_P1 | CONDUIT | 4.0    | 14.1135 | 0.0110    |
| C34  | OGS_2     | OF1       | CONDUIT | 8.7    | 0.6782  | 0.0110    |
| C35  | MH_25     | MH_24     | CONDUIT | 44.2   | 0.5000  | 0.0110    |
| C36  | CBMH_18   | SU_N      | CONDUIT | 3.9    | 0.5128  | 0.0110    |
| C37  | CB_29     | MH_27     | CONDUIT | 32.9   | 0.4985  | 0.0110    |
| C4   | SU_S      | MH_45     | CONDUIT | 9.4    | 1.0001  | 0.0090    |
| C5   | J2        | MH_45     | CONDUIT | 9.4    | 0.5000  | 0.0110    |
| C6   | MH_45     | OGS_1     | CONDUIT | 3.1    | 0.4839  | 0.0110    |
| C7   | DCB_16    | CBMH_15   | CONDUIT | 54.4   | 0.5000  | 0.0110    |
| C8   | CBMH_15   | CBMH_14   | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C9   | CBMH_14   | SU_N      | CONDUIT | 15.2   | 0.5000  | 0.0110    |
| OR1  | SU_S      | J2        | ORIFICE |        |         |           |
| OR2  | SU_N      | J1        | ORIFICE |        |         |           |

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Cross Section Summary  
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| Conduit | Shape    | Full Depth | Full Area | Hyd. Rad. | Max. Width | No. of Barrels | Full Flow |
|---------|----------|------------|-----------|-----------|------------|----------------|-----------|
| C1      | CIRCULAR | 0.20       | 0.03      | 0.05      | 0.20       | 1              | 0.05      |
| C10     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.34      |
| C11     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.34      |
| C12     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C13     | CIRCULAR | 0.60       | 0.28      | 0.15      | 0.60       | 1              | 0.51      |
| C14     | CIRCULAR | 0.38       | 0.11      | 0.09      | 0.38       | 1              | 0.21      |
| C15     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C16     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C17     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C18     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C19     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C2      | CIRCULAR | 0.38       | 0.11      | 0.09      | 0.38       | 1              | 0.13      |
| C20     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C21     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C22     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C23     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |

|     |          |      |      |      |      |   |      |
|-----|----------|------|------|------|------|---|------|
| C24 | CIRCULAR | 0.75 | 0.44 | 0.19 | 0.75 | 1 | 0.93 |
| C25 | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C26 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C27 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C28 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C29 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.16 |
| C3  | CIRCULAR | 0.30 | 0.07 | 0.07 | 0.30 | 1 | 0.08 |
| C30 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.50 |
| C31 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.15 |
| C32 | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C33 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.78 |
| C34 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.17 |
| C35 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C36 | CIRCULAR | 0.75 | 0.44 | 0.19 | 0.75 | 1 | 0.94 |
| C37 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.15 |
| C4  | CIRCULAR | 0.20 | 0.03 | 0.05 | 0.20 | 1 | 0.05 |
| C5  | CIRCULAR | 0.30 | 0.07 | 0.07 | 0.30 | 1 | 0.08 |
| C6  | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.14 |
| C7  | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C8  | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C9  | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |

\*\*\*\*\*  
NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
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\*\*\*\*\*  
Analysis Options  
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Flow Units ..... CMS  
Process Models:  
  Rainfall/Runoff ..... YES  
  RDII ..... NO  
  Snowmelt ..... NO  
  Groundwater ..... NO  
  Flow Routing ..... YES  
  Ponding Allowed ..... NO  
  Water Quality ..... NO  
Infiltration Method ..... HORTON  
Flow Routing Method ..... DYNWAVE  
Surcharge Method ..... EXTRAN  
Starting Date ..... 12/11/2020 00:00:00  
Ending Date ..... 12/21/2020 00:00:00  
Antecedent Dry Days ..... 0.0  
Report Time Step ..... 00:01:00  
Wet Time Step ..... 00:01:00  
Dry Time Step ..... 00:01:00  
Routing Time Step ..... 1.00 sec  
Variable Time Step ..... YES  
Maximum Trials ..... 8  
Number of Threads ..... 6  
Head Tolerance ..... 0.001500 m

| *****                      |           |        |
|----------------------------|-----------|--------|
|                            | Volume    | Depth  |
| Runoff Quantity Continuity | hectare-m | mm     |
| *****                      |           |        |
| Total Precipitation .....  | 0.225     | 31.880 |
| Evaporation Loss .....     | 0.000     | 0.000  |
| Infiltration Loss .....    | 0.017     | 2.387  |
| Surface Runoff .....       | 0.208     | 29.513 |
| Final Storage .....        | 0.000     | 0.000  |
| Continuity Error (%) ..... | -0.066    |        |

| *****                       |           |          |
|-----------------------------|-----------|----------|
|                             | Volume    | Volume   |
| Flow Routing Continuity     | hectare-m | 10^6 ltr |
| *****                       |           |          |
| Dry Weather Inflow .....    | 0.000     | 0.000    |
| Wet Weather Inflow .....    | 0.208     | 2.081    |
| Groundwater Inflow .....    | 0.000     | 0.000    |
| RDII Inflow .....           | 0.000     | 0.000    |
| External Inflow .....       | 0.000     | 0.000    |
| External Outflow .....      | 0.208     | 2.081    |
| Flooding Loss .....         | 0.000     | 0.000    |
| Evaporation Loss .....      | 0.000     | 0.000    |
| Exfiltration Loss .....     | 0.000     | 0.000    |
| Initial Stored Volume ..... | 0.000     | 0.000    |
| Final Stored Volume .....   | 0.000     | 0.000    |
| Continuity Error (%) .....  | -0.037    |          |

\*\*\*\*\*  
Time-Step Critical Elements  
\*\*\*\*\*  
None

\*\*\*\*\*  
Highest Flow Instability Indexes  
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Link C2 (3)  
 Link OR1 (1)  
 Link OR2 (1)

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 Routing Time Step Summary  
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Minimum Time Step : 0.30 sec  
 Average Time Step : 1.00 sec  
 Maximum Time Step : 1.00 sec  
 Percent in Steady State : 0.00  
 Average Iterations per Step : 2.00  
 Percent Not Converging : 0.00  
 Time Step Frequencies :  
 1.000 - 0.871 sec : 99.92 %  
 0.871 - 0.758 sec : 0.08 %  
 0.758 - 0.660 sec : 0.00 %  
 0.660 - 0.574 sec : 0.00 %  
 0.574 - 0.500 sec : 0.00 %

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 Subcatchment Runoff Summary  
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| Subcatchment | Total Precip<br>mm | Total Runon<br>mm | Total Evap<br>mm | Total Infil<br>mm | Imperv Runoff<br>mm | Perv Runoff<br>mm | Total Runoff<br>mm | Total Runoff<br>10 <sup>6</sup> ltr | Peak Runoff<br>CMS | Runoff Coeff |
|--------------|--------------------|-------------------|------------------|-------------------|---------------------|-------------------|--------------------|-------------------------------------|--------------------|--------------|
| Area_1       | 31.88              | 0.00              | 0.00             | 2.46              | 28.72               | 0.73              | 29.45              | 0.07                                | 0.06               | 0.924        |
| Area_10      | 31.88              | 0.00              | 0.00             | 2.46              | 28.72               | 0.73              | 29.45              | 0.02                                | 0.02               | 0.924        |
| Area_101     | 31.88              | 0.00              | 0.00             | 1.24              | 30.30               | 0.35              | 30.65              | 0.42                                | 0.26               | 0.961        |
| Area_102     | 31.88              | 0.00              | 0.00             | 1.24              | 30.30               | 0.35              | 30.65              | 0.35                                | 0.21               | 0.961        |
| Area_11      | 31.88              | 0.00              | 0.00             | 2.46              | 28.72               | 0.73              | 29.45              | 0.04                                | 0.03               | 0.924        |
| Area_12      | 31.88              | 0.00              | 0.00             | 2.46              | 28.72               | 0.73              | 29.45              | 0.05                                | 0.04               | 0.924        |
| Area_13      | 31.88              | 0.00              | 0.00             | 2.46              | 28.72               | 0.73              | 29.45              | 0.05                                | 0.04               | 0.924        |
| Area_14      | 31.88              | 0.00              | 0.00             | 2.46              | 28.72               | 0.73              | 29.45              | 0.05                                | 0.04               | 0.924        |
| Area_15      | 31.88              | 0.00              | 0.00             | 2.46              | 28.72               | 0.73              | 29.45              | 0.03                                | 0.02               | 0.924        |
| Area_16      | 31.88              | 0.00              | 0.00             | 2.46              | 28.72               | 0.73              | 29.45              | 0.04                                | 0.04               | 0.924        |
| Area_17      | 31.88              | 0.00              | 0.00             | 2.46              | 28.72               | 0.73              | 29.45              | 0.05                                | 0.04               | 0.924        |
| Area_18      | 31.88              | 0.00              | 0.00             | 2.46              | 28.72               | 0.73              | 29.45              | 0.05                                | 0.04               | 0.924        |
| Area_19      | 31.88              | 0.00              | 0.00             | 2.46              | 28.72               | 0.73              | 29.45              | 0.05                                | 0.04               | 0.924        |
| Area_2       | 31.88              | 0.00              | 0.00             | 2.46              | 28.72               | 0.73              | 29.45              | 0.05                                | 0.04               | 0.924        |
| Area_20      | 31.88              | 0.00              | 0.00             | 2.46              | 28.72               | 0.73              | 29.45              | 0.08                                | 0.07               | 0.924        |
| Area_2001    | 31.88              | 0.00              | 0.00             | 19.96             | 7.98                | 3.95              | 11.93              | 0.01                                | 0.00               | 0.374        |
| Area_2002    | 31.88              | 0.00              | 0.00             | 2.50              | 28.70               | 0.68              | 29.39              | 0.06                                | 0.04               | 0.922        |
| Area_2003    | 31.88              | 0.00              | 0.00             | 2.52              | 28.71               | 0.66              | 29.37              | 0.05                                | 0.03               | 0.921        |
| Area_2004    | 31.88              | 0.00              | 0.00             | 23.95             | 1.60                | 6.34              | 7.94               | 0.00                                | 0.00               | 0.249        |
| Area_2005    | 31.88              | 0.00              | 0.00             | 23.95             | 1.60                | 6.34              | 7.94               | 0.00                                | 0.00               | 0.249        |
| Area_21      | 31.88              | 0.00              | 0.00             | 2.46              | 28.72               | 0.73              | 29.45              | 0.06                                | 0.05               | 0.924        |
| Area_22      | 31.88              | 0.00              | 0.00             | 2.46              | 28.72               | 0.73              | 29.45              | 0.09                                | 0.08               | 0.924        |
| Area_23      | 31.88              | 0.00              | 0.00             | 2.46              | 28.72               | 0.73              | 29.45              | 0.05                                | 0.04               | 0.924        |
| Area_3       | 31.88              | 0.00              | 0.00             | 2.46              | 28.72               | 0.73              | 29.45              | 0.11                                | 0.09               | 0.924        |
| Area_4       | 31.88              | 0.00              | 0.00             | 2.46              | 28.72               | 0.73              | 29.45              | 0.08                                | 0.07               | 0.924        |
| Area_5       | 31.88              | 0.00              | 0.00             | 2.46              | 28.72               | 0.73              | 29.45              | 0.04                                | 0.04               | 0.924        |
| Area_6       | 31.88              | 0.00              | 0.00             | 2.46              | 28.72               | 0.73              | 29.45              | 0.04                                | 0.04               | 0.924        |
| Area_7       | 31.88              | 0.00              | 0.00             | 2.46              | 28.72               | 0.73              | 29.45              | 0.01                                | 0.01               | 0.924        |
| Area_8       | 31.88              | 0.00              | 0.00             | 2.46              | 28.72               | 0.73              | 29.45              | 0.04                                | 0.03               | 0.924        |
| Area_9       | 31.88              | 0.00              | 0.00             | 2.46              | 28.72               | 0.73              | 29.45              | 0.04                                | 0.03               | 0.924        |

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 Node Depth Summary  
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| Node    | Type     | Average Depth<br>Meters | Maximum Depth<br>Meters | Maximum HGL<br>Meters | Time of Max Occurrence<br>days hr:min | Reported Max Depth<br>Meters |
|---------|----------|-------------------------|-------------------------|-----------------------|---------------------------------------|------------------------------|
| CB_10   | JUNCTION | 0.00                    | 0.11                    | 65.44                 | 0 01:05                               | 0.11                         |
| CB_23   | JUNCTION | 0.00                    | 0.08                    | 66.28                 | 0 01:05                               | 0.08                         |
| CB_27   | JUNCTION | 0.00                    | 0.10                    | 65.59                 | 0 01:05                               | 0.10                         |
| CB_28   | JUNCTION | 0.00                    | 0.10                    | 65.49                 | 0 01:05                               | 0.10                         |
| CB_29   | JUNCTION | 0.00                    | 0.13                    | 64.25                 | 0 01:05                               | 0.13                         |
| CB_5    | JUNCTION | 0.00                    | 0.11                    | 65.23                 | 0 01:05                               | 0.11                         |
| CBMH_11 | JUNCTION | 0.03                    | 0.53                    | 64.12                 | 0 03:08                               | 0.53                         |
| CBMH_12 | JUNCTION | 0.00                    | 0.19                    | 64.25                 | 0 01:05                               | 0.19                         |
| CBMH_14 | JUNCTION | 0.02                    | 0.56                    | 64.67                 | 0 02:58                               | 0.56                         |
| CBMH_15 | JUNCTION | 0.00                    | 0.22                    | 64.68                 | 0 01:05                               | 0.22                         |
| CBMH_18 | JUNCTION | 0.03                    | 0.61                    | 64.66                 | 0 02:59                               | 0.61                         |
| CBMH_19 | JUNCTION | 0.00                    | 0.19                    | 65.07                 | 0 01:05                               | 0.19                         |
| CBMH_2  | JUNCTION | 0.00                    | 0.23                    | 64.29                 | 0 01:05                               | 0.23                         |
| CBMH_21 | JUNCTION | 0.00                    | 0.18                    | 65.35                 | 0 01:05                               | 0.18                         |
| CBMH_22 | JUNCTION | 0.00                    | 0.14                    | 65.67                 | 0 01:05                               | 0.14                         |
| CBMH_3  | JUNCTION | 0.00                    | 0.20                    | 64.61                 | 0 01:05                               | 0.20                         |
| CBMH_4  | JUNCTION | 0.00                    | 0.16                    | 64.94                 | 0 01:05                               | 0.16                         |
| CBMH_6  | JUNCTION | 0.01                    | 0.25                    | 64.17                 | 0 01:05                               | 0.25                         |
| CBMH_7  | JUNCTION | 0.00                    | 0.24                    | 64.51                 | 0 01:05                               | 0.24                         |
| CBMH_8  | JUNCTION | 0.00                    | 0.20                    | 64.83                 | 0 01:05                               | 0.20                         |
| CBMH_9  | JUNCTION | 0.00                    | 0.16                    | 65.15                 | 0 01:05                               | 0.16                         |
| DCB_16  | JUNCTION | 0.00                    | 0.18                    | 64.98                 | 0 01:05                               | 0.18                         |
| J1      | JUNCTION | 0.01                    | 0.08                    | 63.83                 | 0 02:59                               | 0.08                         |



|           |          |      |      |       |   |       |      |
|-----------|----------|------|------|-------|---|-------|------|
| J13       | JUNCTION | 0.03 | 0.60 | 64.13 | 0 | 03:02 | 0.59 |
| J2        | JUNCTION | 0.01 | 0.08 | 63.31 | 0 | 03:07 | 0.08 |
| MH_20     | JUNCTION | 0.00 | 0.18 | 65.17 | 0 | 01:05 | 0.18 |
| MH_24     | JUNCTION | 0.02 | 0.53 | 64.66 | 0 | 02:59 | 0.53 |
| MH_25     | JUNCTION | 0.01 | 0.35 | 64.77 | 0 | 01:05 | 0.35 |
| MH_26     | JUNCTION | 0.00 | 0.40 | 64.95 | 0 | 01:05 | 0.39 |
| MH_27     | JUNCTION | 0.01 | 0.23 | 64.12 | 0 | 03:08 | 0.23 |
| MH_30     | JUNCTION | 0.01 | 0.39 | 64.12 | 0 | 03:06 | 0.39 |
| MH_44     | JUNCTION | 0.01 | 0.10 | 63.62 | 0 | 03:00 | 0.10 |
| MH_45     | JUNCTION | 0.01 | 0.07 | 63.19 | 0 | 03:07 | 0.07 |
| OGS_1     | JUNCTION | 0.00 | 0.03 | 63.07 | 0 | 03:08 | 0.03 |
| OGS_2     | JUNCTION | 0.01 | 0.09 | 63.56 | 0 | 02:59 | 0.09 |
| Humber_P1 | OUTFALL  | 0.00 | 0.00 | 62.48 | 0 | 00:00 | 0.00 |
| OF1       | OUTFALL  | 0.01 | 0.09 | 63.50 | 0 | 03:00 | 0.09 |
| OF2       | OUTFALL  | 0.00 | 0.00 | 0.00  | 0 | 00:00 | 0.00 |
| SU_N      | STORAGE  | 0.06 | 0.91 | 64.66 | 0 | 02:59 | 0.91 |
| SU_S      | STORAGE  | 0.07 | 0.88 | 64.12 | 0 | 03:07 | 0.88 |

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Node Inflow Summary  
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| Node      | Type     | Maximum Lateral Inflow<br>CMS | Maximum Total Inflow<br>CMS | Time of Max Occurrence<br>days hr:min | Lateral Inflow Volume<br>10^6 ltr | Total Inflow Volume<br>10^6 ltr | Flow Balance Error<br>Percent |
|-----------|----------|-------------------------------|-----------------------------|---------------------------------------|-----------------------------------|---------------------------------|-------------------------------|
| CB_10     | JUNCTION | 0.033                         | 0.033                       | 0 01:05                               | 0.0383                            | 0.0383                          | -0.012                        |
| CB_23     | JUNCTION | 0.020                         | 0.020                       | 0 01:05                               | 0.0236                            | 0.0236                          | -0.007                        |
| CB_27     | JUNCTION | 0.038                         | 0.038                       | 0 01:05                               | 0.0442                            | 0.0442                          | -0.004                        |
| CB_28     | JUNCTION | 0.038                         | 0.038                       | 0 01:05                               | 0.0442                            | 0.0442                          | -0.004                        |
| CB_29     | JUNCTION | 0.040                         | 0.040                       | 0 01:05                               | 0.0471                            | 0.0471                          | 0.120                         |
| CB_5      | JUNCTION | 0.038                         | 0.038                       | 0 01:05                               | 0.0442                            | 0.0442                          | -0.012                        |
| CBMH_11   | JUNCTION | 0.265                         | 0.384                       | 0 01:05                               | 0.408                             | 0.549                           | -0.020                        |
| CBMH_12   | JUNCTION | 0.080                         | 0.080                       | 0 01:05                               | 0.0942                            | 0.0942                          | 0.854                         |
| CBMH_14   | JUNCTION | 0.063                         | 0.190                       | 0 01:05                               | 0.0736                            | 0.255                           | -0.264                        |
| CBMH_15   | JUNCTION | 0.040                         | 0.129                       | 0 01:05                               | 0.0471                            | 0.155                           | 0.586                         |
| CBMH_18   | JUNCTION | 0.070                         | 0.480                       | 0 01:05                               | 0.0824                            | 0.697                           | -0.003                        |
| CBMH_19   | JUNCTION | 0.010                         | 0.088                       | 0 01:05                               | 0.0118                            | 0.106                           | -0.007                        |
| CBMH_2    | JUNCTION | 0.043                         | 0.160                       | 0 01:05                               | 0.0501                            | 0.194                           | 0.319                         |
| CBMH_21   | JUNCTION | 0.030                         | 0.079                       | 0 01:05                               | 0.0353                            | 0.0942                          | -0.003                        |
| CBMH_22   | JUNCTION | 0.030                         | 0.050                       | 0 01:05                               | 0.0353                            | 0.0589                          | -0.010                        |
| CBMH_3    | JUNCTION | 0.043                         | 0.120                       | 0 01:05                               | 0.0501                            | 0.144                           | -0.012                        |
| CBMH_4    | JUNCTION | 0.043                         | 0.080                       | 0 01:05                               | 0.0501                            | 0.0942                          | -0.011                        |
| CBMH_6    | JUNCTION | 0.023                         | 0.170                       | 0 01:05                               | 0.0265                            | 0.21                            | 0.058                         |
| CBMH_7    | JUNCTION | 0.043                         | 0.150                       | 0 01:05                               | 0.0501                            | 0.183                           | 0.147                         |
| CBMH_8    | JUNCTION | 0.040                         | 0.111                       | 0 01:05                               | 0.0471                            | 0.133                           | -0.011                        |
| CBMH_9    | JUNCTION | 0.040                         | 0.072                       | 0 01:05                               | 0.0471                            | 0.0854                          | -0.010                        |
| DCB_16    | JUNCTION | 0.090                         | 0.090                       | 0 01:05                               | 0.106                             | 0.106                           | 0.166                         |
| J1        | JUNCTION | 0.000                         | 0.012                       | 0 02:59                               | 0                                 | 0.878                           | -0.005                        |
| J13       | JUNCTION | 0.070                         | 0.394                       | 0 01:05                               | 0.0824                            | 0.578                           | -0.037                        |
| J2        | JUNCTION | 0.000                         | 0.011                       | 0 03:07                               | 0                                 | 1.03                            | -0.004                        |
| MH_20     | JUNCTION | 0.000                         | 0.078                       | 0 01:05                               | 0                                 | 0.0942                          | -0.001                        |
| MH_24     | JUNCTION | 0.000                         | 0.420                       | 0 01:05                               | 0                                 | 0.612                           | -0.310                        |
| MH_25     | JUNCTION | 0.000                         | 0.332                       | 0 01:05                               | 0                                 | 0.508                           | 0.360                         |
| MH_26     | JUNCTION | 0.257                         | 0.331                       | 0 01:05                               | 0.42                              | 0.508                           | 0.047                         |
| MH_27     | JUNCTION | 0.000                         | 0.040                       | 0 01:05                               | 0                                 | 0.0471                          | -0.032                        |
| MH_30     | JUNCTION | 0.000                         | 0.160                       | 0 01:05                               | 0                                 | 0.21                            | -0.281                        |
| MH_44     | JUNCTION | 0.000                         | 0.021                       | 0 02:59                               | 0                                 | 0.924                           | 0.006                         |
| MH_45     | JUNCTION | 0.000                         | 0.012                       | 0 03:08                               | 0                                 | 1.04                            | 0.001                         |
| OGS_1     | JUNCTION | 0.000                         | 0.012                       | 0 03:08                               | 0                                 | 1.04                            | -0.000                        |
| OGS_2     | JUNCTION | 0.000                         | 0.021                       | 0 02:59                               | 0                                 | 0.924                           | -0.006                        |
| Humber_P1 | OUTFALL  | 0.001                         | 0.012                       | 0 03:05                               | 0.00476                           | 1.04                            | 0.000                         |
| OF1       | OUTFALL  | 0.033                         | 0.039                       | 0 01:05                               | 0.047                             | 0.971                           | 0.000                         |
| OF2       | OUTFALL  | 0.043                         | 0.043                       | 0 01:05                               | 0.0701                            | 0.0701                          | 0.000                         |
| SU_N      | STORAGE  | 0.000                         | 0.667                       | 0 01:05                               | 0                                 | 0.951                           | -0.092                        |
| SU_S      | STORAGE  | 0.000                         | 0.776                       | 0 01:05                               | 0                                 | 1.11                            | -0.107                        |

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Node Surcharge Summary  
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No nodes were surcharged.

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Node Flooding Summary  
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No nodes were flooded.

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Storage Volume Summary  
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| Storage Unit | Average Volume<br>1000 m3 | Avg Full | Evap Loss | Exfil Loss | Maximum Volume<br>1000 m3 | Max Full | Time of Max Occurrence<br>days hr:min | Maximum Outflow<br>CMS |
|--------------|---------------------------|----------|-----------|------------|---------------------------|----------|---------------------------------------|------------------------|
| SU_N         | 0.045                     | 2        | 0         | 0          | 0.767                     | 30       | 0 02:59                               | 0.028                  |

SU\_s 0.065 2 0 0 0.914 26 0 03:07 0.061

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 Outfall Loading Summary  
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| Outfall Node | Flow Freq Pent | Avg Flow CMS | Max Flow CMS | Total Volume 10^6 ltr |
|--------------|----------------|--------------|--------------|-----------------------|
| Humber_Pl    | 26.62          | 0.005        | 0.012        | 1.040                 |
| OF1          | 22.05          | 0.005        | 0.039        | 0.971                 |
| OF2          | 2.60           | 0.003        | 0.043        | 0.070                 |
| System       | 17.09          | 0.013        | 0.090        | 2.081                 |

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 Link Flow Summary  
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| Link | Type    | Maximum  Flow  CMS | Time of Max Occurrence days hr:min | Maximum  Veloc  m/sec | Max/ Full Flow | Max/ Full Depth |
|------|---------|--------------------|------------------------------------|-----------------------|----------------|-----------------|
| C1   | CONDUIT | 0.010              | 0 02:59                            | 1.18                  | 0.20           | 0.31            |
| C10  | CONDUIT | 0.037              | 0 01:05                            | 1.40                  | 0.11           | 0.23            |
| C11  | CONDUIT | 0.037              | 0 01:05                            | 1.40                  | 0.11           | 0.23            |
| C12  | CONDUIT | 0.332              | 0 01:05                            | 1.92                  | 0.93           | 0.75            |
| C13  | CONDUIT | 0.419              | 0 01:05                            | 2.02                  | 0.82           | 0.90            |
| C14  | CONDUIT | 0.020              | 0 01:05                            | 1.19                  | 0.10           | 0.21            |
| C15  | CONDUIT | 0.049              | 0 01:05                            | 1.18                  | 0.21           | 0.31            |
| C16  | CONDUIT | 0.078              | 0 01:05                            | 1.35                  | 0.33           | 0.39            |
| C17  | CONDUIT | 0.079              | 0 01:05                            | 1.35                  | 0.33           | 0.40            |
| C18  | CONDUIT | 0.088              | 0 01:05                            | 1.39                  | 0.37           | 0.42            |
| C19  | CONDUIT | 0.032              | 0 01:05                            | 1.05                  | 0.13           | 0.25            |
| C2   | CONDUIT | 0.021              | 0 02:59                            | 0.94                  | 0.17           | 0.26            |
| C20  | CONDUIT | 0.071              | 0 01:05                            | 1.30                  | 0.20           | 0.30            |
| C21  | CONDUIT | 0.109              | 0 01:05                            | 1.46                  | 0.30           | 0.38            |
| C22  | CONDUIT | 0.150              | 0 01:05                            | 1.59                  | 0.42           | 0.45            |
| C23  | CONDUIT | 0.171              | 0 01:05                            | 1.64                  | 0.47           | 0.55            |
| C24  | CONDUIT | 0.394              | 0 01:05                            | 2.02                  | 0.42           | 0.80            |
| C25  | CONDUIT | 0.037              | 0 01:05                            | 1.07                  | 0.10           | 0.22            |
| C26  | CONDUIT | 0.078              | 0 01:05                            | 1.32                  | 0.15           | 0.26            |
| C27  | CONDUIT | 0.119              | 0 01:05                            | 1.48                  | 0.23           | 0.33            |
| C28  | CONDUIT | 0.160              | 0 01:05                            | 1.60                  | 0.31           | 0.38            |
| C29  | CONDUIT | 0.080              | 0 01:05                            | 1.33                  | 0.51           | 0.57            |
| C3   | CONDUIT | 0.012              | 0 02:59                            | 0.80                  | 0.15           | 0.26            |
| C30  | CONDUIT | 0.160              | 0 01:05                            | 1.58                  | 0.32           | 0.69            |
| C31  | CONDUIT | 0.040              | 0 01:05                            | 1.09                  | 0.27           | 0.66            |
| C32  | CONDUIT | 0.382              | 0 01:05                            | 2.05                  | 1.06           | 1.00            |
| C33  | CONDUIT | 0.012              | 0 03:08                            | 2.58                  | 0.02           | 0.09            |
| C34  | CONDUIT | 0.021              | 0 03:00                            | 1.05                  | 0.12           | 0.24            |
| C35  | CONDUIT | 0.332              | 0 01:05                            | 1.93                  | 0.65           | 0.59            |
| C36  | CONDUIT | 0.480              | 0 01:05                            | 2.14                  | 0.51           | 0.83            |
| C37  | CONDUIT | 0.040              | 0 01:05                            | 1.13                  | 0.27           | 0.36            |
| C4   | CONDUIT | 0.001              | 0 03:08                            | 0.54                  | 0.01           | 0.08            |
| C5   | CONDUIT | 0.011              | 0 03:07                            | 0.81                  | 0.14           | 0.25            |
| C6   | CONDUIT | 0.012              | 0 03:08                            | 0.79                  | 0.08           | 0.20            |
| C7   | CONDUIT | 0.089              | 0 01:05                            | 1.38                  | 0.25           | 0.34            |
| C8   | CONDUIT | 0.128              | 0 01:05                            | 1.53                  | 0.36           | 0.66            |
| C9   | CONDUIT | 0.189              | 0 01:05                            | 1.68                  | 0.37           | 0.97            |
| OR1  | ORIFICE | 0.011              | 0 03:07                            |                       |                | 1.00            |
| OR2  | ORIFICE | 0.012              | 0 02:59                            |                       |                | 1.00            |

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 Flow Classification Summary  
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| Conduit | Adjusted /Actual Length | Fraction of Time in Flow Class |          |         |          |         |           |           |           |      |
|---------|-------------------------|--------------------------------|----------|---------|----------|---------|-----------|-----------|-----------|------|
|         |                         | Up Dry                         | Down Dry | Sub Dry | Sup Crit | Up Crit | Down Crit | Norm Crit | Inlet Ltd | Ctrl |
| C1      | 1.00                    | 0.99                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 0.01      | 0.00      | 0.00 |
| C10     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C11     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C12     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.03     | 0.00    | 0.00      | 0.97      | 0.01      | 0.00 |
| C13     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.08     | 0.00    | 0.00      | 0.92      | 0.00      | 0.00 |
| C14     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C15     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C16     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C17     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C18     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C19     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C2      | 1.00                    | 0.00                           | 0.11     | 0.00    | 0.76     | 0.13    | 0.00      | 0.00      | 0.79      | 0.00 |
| C20     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C21     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C22     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.03     | 0.00    | 0.00      | 0.97      | 0.03      | 0.00 |
| C23     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.06     | 0.00    | 0.00      | 0.94      | 0.03      | 0.00 |
| C24     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.10     | 0.00    | 0.00      | 0.90      | 0.01      | 0.00 |

|     |      |      |      |      |      |      |      |      |      |      |
|-----|------|------|------|------|------|------|------|------|------|------|
| C25 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C26 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C27 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C28 | 1.00 | 0.00 | 0.00 | 0.00 | 0.06 | 0.00 | 0.00 | 0.94 | 0.05 | 0.00 |
| C29 | 1.00 | 0.00 | 0.00 | 0.00 | 0.06 | 0.00 | 0.00 | 0.94 | 0.06 | 0.00 |
| C3  | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C30 | 1.00 | 0.00 | 0.00 | 0.00 | 0.07 | 0.00 | 0.00 | 0.92 | 0.01 | 0.00 |
| C31 | 1.00 | 0.00 | 0.00 | 0.00 | 0.05 | 0.00 | 0.00 | 0.95 | 0.01 | 0.00 |
| C32 | 1.00 | 0.00 | 0.00 | 0.00 | 0.10 | 0.00 | 0.00 | 0.90 | 0.01 | 0.00 |
| C33 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C34 | 1.00 | 0.00 | 0.00 | 0.00 | 0.76 | 0.24 | 0.00 | 0.00 | 0.04 | 0.00 |
| C35 | 1.00 | 0.00 | 0.00 | 0.00 | 0.07 | 0.00 | 0.00 | 0.93 | 0.03 | 0.00 |
| C36 | 1.00 | 0.00 | 0.00 | 0.00 | 0.09 | 0.00 | 0.00 | 0.91 | 0.00 | 0.00 |
| C37 | 1.00 | 0.00 | 0.00 | 0.00 | 0.03 | 0.00 | 0.00 | 0.97 | 0.03 | 0.00 |
| C4  | 1.00 | 0.99 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 |
| C5  | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C6  | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C7  | 1.00 | 0.00 | 0.00 | 0.00 | 0.02 | 0.00 | 0.00 | 0.98 | 0.02 | 0.00 |
| C8  | 1.00 | 0.00 | 0.00 | 0.00 | 0.07 | 0.00 | 0.00 | 0.93 | 0.04 | 0.00 |
| C9  | 1.00 | 0.00 | 0.00 | 0.00 | 0.09 | 0.00 | 0.00 | 0.91 | 0.01 | 0.00 |

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 Conduit Surcharge Summary  
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| Conduit | Hours Full |          |          | Hours                  |                        |
|---------|------------|----------|----------|------------------------|------------------------|
|         | Both Ends  | Upstream | Dnstream | Above Full Normal Flow | Hours Capacity Limited |
| C32     | 0.83       | 0.83     | 4.15     | 0.02                   | 0.01                   |
| C9      | 0.01       | 0.01     | 1.77     | 0.01                   | 0.01                   |

Analysis begun on: Wed Oct 5 20:35:01 2022  
 Analysis ended on: Wed Oct 5 20:35:31 2022  
 Total elapsed time: 00:00:30

2-yr, 6-hour

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.015)

WARNING 03: negative offset ignored for Link C2  
WARNING 03: negative offset ignored for Link C32  
WARNING 03: negative offset ignored for Link C34

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Element Count

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Number of rain gages ..... 7  
Number of subcatchments ... 30  
Number of nodes ..... 40  
Number of links ..... 39  
Number of pollutants ..... 0  
Number of land uses ..... 0

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Raingage Summary

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| Name      | Data Source | Data Type | Recording Interval |
|-----------|-------------|-----------|--------------------|
| 25mm      | 25mm        | INTENSITY | 5 min.             |
| 3hr-100yr | 3hr-100yr   | INTENSITY | 10 min.            |
| 3hr-2yr   | 3hr-2yr     | INTENSITY | 5 min.             |
| 3hr-5yr   | 3hr-5yr     | INTENSITY | 5 min.             |
| 6hr-100yr | 6hr-100yr   | INTENSITY | 10 min.            |
| 6hr-2yr   | 6hr-2yr     | INTENSITY | 5 min.             |
| 6hr-5yr   | 6hr-5yr     | INTENSITY | 5 min.             |

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Subcatchment Summary

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| Name      | Area | Width  | %Imperv | %Slope | Rain Gage | Outlet    |
|-----------|------|--------|---------|--------|-----------|-----------|
| Area_1    | 0.25 | 83.33  | 90.00   | 1.0000 | 6hr-2yr   | CBMH_14   |
| Area_10   | 0.08 | 26.67  | 90.00   | 1.0000 | 6hr-2yr   | CB_23     |
| Area_101  | 1.37 | 137.00 | 95.00   | 0.5000 | 6hr-2yr   | MH_26     |
| Area_102  | 1.13 | 113.00 | 95.00   | 0.5000 | 6hr-2yr   | CBMH_11   |
| Area_11   | 0.13 | 43.33  | 90.00   | 1.0000 | 6hr-2yr   | CB_10     |
| Area_12   | 0.16 | 53.33  | 90.00   | 1.0000 | 6hr-2yr   | CBMH_9    |
| Area_13   | 0.16 | 53.33  | 90.00   | 1.0000 | 6hr-2yr   | CBMH_8    |
| Area_14   | 0.17 | 56.67  | 90.00   | 1.0000 | 6hr-2yr   | CBMH_7    |
| Area_15   | 0.09 | 30.00  | 90.00   | 1.0000 | 6hr-2yr   | CBMH_6    |
| Area_16   | 0.15 | 50.00  | 90.00   | 1.0000 | 6hr-2yr   | CB_5      |
| Area_17   | 0.17 | 56.67  | 90.00   | 1.0000 | 6hr-2yr   | CBMH_4    |
| Area_18   | 0.17 | 56.67  | 90.00   | 1.0000 | 6hr-2yr   | CBMH_3    |
| Area_19   | 0.17 | 56.67  | 90.00   | 1.0000 | 6hr-2yr   | CBMH_2    |
| Area_2    | 0.16 | 53.33  | 90.00   | 1.0000 | 6hr-2yr   | CBMH_15   |
| Area_20   | 0.28 | 93.33  | 90.00   | 1.0000 | 6hr-2yr   | J13       |
| Area_2001 | 0.07 | 7.00   | 25.00   | 0.5000 | 6hr-2yr   | OF2       |
| Area_2002 | 0.21 | 21.00  | 90.00   | 0.5000 | 6hr-2yr   | OF2       |
| Area_2003 | 0.16 | 16.00  | 90.00   | 1.0000 | 6hr-2yr   | OF1       |
| Area_2004 | 0.02 | 13.33  | 5.00    | 0.5000 | 6hr-2yr   | Humber_P1 |
| Area_2005 | 0.04 | 26.67  | 5.00    | 0.5000 | 6hr-2yr   | Humber_P1 |
| Area_21   | 0.21 | 70.00  | 90.00   | 1.0000 | 6hr-2yr   | CBMH_11   |
| Area_22   | 0.32 | 106.67 | 90.00   | 1.0000 | 6hr-2yr   | CBMH_12   |
| Area_23   | 0.16 | 53.33  | 90.00   | 1.0000 | 6hr-2yr   | CB_29     |
| Area_3    | 0.36 | 120.00 | 90.00   | 1.0000 | 6hr-2yr   | DCB_16    |
| Area_4    | 0.28 | 93.33  | 90.00   | 1.0000 | 6hr-2yr   | CBMH_18   |
| Area_5    | 0.15 | 50.00  | 90.00   | 1.0000 | 6hr-2yr   | CB_27     |
| Area_6    | 0.15 | 50.00  | 90.00   | 1.0000 | 6hr-2yr   | CB_28     |
| Area_7    | 0.04 | 13.33  | 90.00   | 1.0000 | 6hr-2yr   | CBMH_19   |
| Area_8    | 0.12 | 40.00  | 90.00   | 1.0000 | 6hr-2yr   | CBMH_21   |
| Area_9    | 0.12 | 40.00  | 90.00   | 1.0000 | 6hr-2yr   | CBMH_22   |

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Node Summary

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| Name    | Type     | Invert Elev. | Max. Depth | Ponded Area | External Inflow |
|---------|----------|--------------|------------|-------------|-----------------|
| CB_10   | JUNCTION | 65.33        | 1.41       | 10.0        |                 |
| CB_23   | JUNCTION | 66.20        | 0.93       | 10.0        |                 |
| CB_27   | JUNCTION | 65.48        | 1.34       | 10.0        |                 |
| CB_28   | JUNCTION | 65.39        | 1.52       | 10.0        |                 |
| CB_29   | JUNCTION | 64.11        | 2.43       | 0.0         |                 |
| CB_5    | JUNCTION | 65.11        | 1.63       | 10.0        |                 |
| CBMH_11 | JUNCTION | 63.58        | 2.16       | 10.0        |                 |
| CBMH_12 | JUNCTION | 64.06        | 1.68       | 10.0        |                 |
| CBMH_14 | JUNCTION | 64.11        | 2.21       | 10.0        |                 |
| CBMH_15 | JUNCTION | 64.47        | 1.85       | 10.0        |                 |
| CBMH_18 | JUNCTION | 64.05        | 2.54       | 0.0         |                 |
| CBMH_19 | JUNCTION | 64.88        | 2.38       | 10.0        |                 |
| CBMH_2  | JUNCTION | 64.06        | 2.94       | 10.0        |                 |
| CBMH_21 | JUNCTION | 65.17        | 1.87       | 10.0        |                 |
| CBMH_22 | JUNCTION | 65.53        | 1.51       | 10.0        |                 |

|           |          |       |      |      |
|-----------|----------|-------|------|------|
| CBMH_3    | JUNCTION | 64.42 | 2.58 | 10.0 |
| CBMH_4    | JUNCTION | 64.78 | 2.22 | 10.0 |
| CBMH_6    | JUNCTION | 63.91 | 2.73 | 10.0 |
| CBMH_7    | JUNCTION | 64.27 | 2.73 | 10.0 |
| CBMH_8    | JUNCTION | 64.63 | 2.37 | 10.0 |
| CBMH_9    | JUNCTION | 64.99 | 2.01 | 10.0 |
| DCB_16    | JUNCTION | 64.80 | 1.52 | 10.0 |
| J1        | JUNCTION | 63.75 | 3.27 | 0.0  |
| J13       | JUNCTION | 63.54 | 3.10 | 10.0 |
| J2        | JUNCTION | 63.24 | 3.33 | 0.0  |
| MH_20     | JUNCTION | 64.99 | 2.30 | 0.0  |
| MH_24     | JUNCTION | 64.13 | 2.50 | 10.0 |
| MH_25     | JUNCTION | 64.42 | 2.63 | 0.0  |
| MH_26     | JUNCTION | 64.56 | 2.70 | 0.0  |
| MH_27     | JUNCTION | 63.89 | 2.02 | 0.0  |
| MH_30     | JUNCTION | 63.73 | 3.08 | 0.0  |
| MH_44     | JUNCTION | 63.51 | 3.51 | 0.0  |
| MH_45     | JUNCTION | 63.11 | 3.46 | 0.0  |
| OGS_1     | JUNCTION | 63.04 | 3.34 | 0.0  |
| OGS_2     | JUNCTION | 63.47 | 3.01 | 0.0  |
| Humber_P1 | OUTFALL  | 62.48 | 0.38 | 0.0  |
| OF1       | OUTFALL  | 63.41 | 0.38 | 0.0  |
| OF2       | OUTFALL  | 0.00  | 0.00 | 0.0  |
| SU_N      | STORAGE  | 63.75 | 3.04 | 0.0  |
| SU_S      | STORAGE  | 63.24 | 3.33 | 0.0  |

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Link Summary  
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| Name | From Node | To Node   | Type    | Length | %Slope  | Roughness |
|------|-----------|-----------|---------|--------|---------|-----------|
| C1   | SU_N      | MH_44     | CONDUIT | 2.5    | 1.0001  | 0.0090    |
| C10  | CB_28     | MH_26     | CONDUIT | 30.4   | 1.0001  | 0.0110    |
| C11  | CB_27     | MH_26     | CONDUIT | 32.8   | 1.0001  | 0.0110    |
| C12  | MH_26     | MH_25     | CONDUIT | 16.5   | 0.4970  | 0.0110    |
| C13  | MH_24     | CBMH_18   | CONDUIT | 4.8    | 0.5000  | 0.0110    |
| C14  | CB_23     | CBMH_22   | CONDUIT | 51.5   | 1.0001  | 0.0110    |
| C15  | CBMH_22   | CBMH_21   | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C16  | CBMH_21   | MH_20     | CONDUIT | 24.5   | 0.5020  | 0.0110    |
| C17  | MH_20     | CBMH_19   | CONDUIT | 10.4   | 0.5000  | 0.0110    |
| C18  | CBMH_19   | MH_24     | CONDUIT | 46.5   | 0.5011  | 0.0110    |
| C19  | CB_10     | CBMH_9    | CONDUIT | 52.5   | 0.4991  | 0.0110    |
| C2   | MH_44     | OGS_2     | CONDUIT | 11.6   | 0.3707  | 0.0110    |
| C20  | CBMH_9    | CBMH_8    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C21  | CBMH_8    | CBMH_7    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C22  | CBMH_7    | CBMH_6    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C23  | CBMH_6    | J13       | CONDUIT | 29.9   | 0.5017  | 0.0110    |
| C24  | J13       | SU_S      | CONDUIT | 4.0    | 0.5000  | 0.0110    |
| C25  | CB_5      | CBMH_4    | CONDUIT | 52.5   | 0.4991  | 0.0110    |
| C26  | CBMH_4    | CBMH_3    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C27  | CBMH_3    | CBMH_2    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C28  | CBMH_2    | MH_30     | CONDUIT | 53.4   | 0.4963  | 0.0110    |
| C29  | CBMH_12   | CBMH_11   | CONDUIT | 50.0   | 0.5700  | 0.0110    |
| C3   | J1        | MH_44     | CONDUIT | 2.5    | 0.4800  | 0.0110    |
| C30  | MH_30     | J13       | CONDUIT | 9.3    | 0.4839  | 0.0110    |
| C31  | MH_27     | CBMH_11   | CONDUIT | 8.2    | 0.5000  | 0.0110    |
| C32  | CBMH_11   | SU_S      | CONDUIT | 13.2   | 0.5000  | 0.0110    |
| C33  | OGS_1     | Humber_P1 | CONDUIT | 4.0    | 14.1135 | 0.0110    |
| C34  | OGS_2     | OF1       | CONDUIT | 8.7    | 0.6782  | 0.0110    |
| C35  | MH_25     | MH_24     | CONDUIT | 44.2   | 0.5000  | 0.0110    |
| C36  | CBMH_18   | SU_N      | CONDUIT | 3.9    | 0.5128  | 0.0110    |
| C37  | CB_29     | MH_27     | CONDUIT | 32.9   | 0.4985  | 0.0110    |
| C4   | SU_S      | MH_45     | CONDUIT | 9.4    | 1.0001  | 0.0090    |
| C5   | J2        | MH_45     | CONDUIT | 9.4    | 0.5000  | 0.0110    |
| C6   | MH_45     | OGS_1     | CONDUIT | 3.1    | 0.4839  | 0.0110    |
| C7   | DCB_16    | CBMH_15   | CONDUIT | 54.4   | 0.5000  | 0.0110    |
| C8   | CBMH_15   | CBMH_14   | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C9   | CBMH_14   | SU_N      | CONDUIT | 15.2   | 0.5000  | 0.0110    |
| OR1  | SU_S      | J2        | ORIFICE |        |         |           |
| OR2  | SU_N      | J1        | ORIFICE |        |         |           |

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Cross Section Summary  
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| Conduit | Shape    | Full Depth | Full Area | Hyd. Rad. | Max. Width | No. of Barrels | Full Flow |
|---------|----------|------------|-----------|-----------|------------|----------------|-----------|
| C1      | CIRCULAR | 0.20       | 0.03      | 0.05      | 0.20       | 1              | 0.05      |
| C10     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.34      |
| C11     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.34      |
| C12     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C13     | CIRCULAR | 0.60       | 0.28      | 0.15      | 0.60       | 1              | 0.51      |
| C14     | CIRCULAR | 0.38       | 0.11      | 0.09      | 0.38       | 1              | 0.21      |
| C15     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C16     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C17     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C18     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C19     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C2      | CIRCULAR | 0.38       | 0.11      | 0.09      | 0.38       | 1              | 0.13      |
| C20     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C21     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C22     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C23     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |

|     |          |      |      |      |      |   |      |
|-----|----------|------|------|------|------|---|------|
| C24 | CIRCULAR | 0.75 | 0.44 | 0.19 | 0.75 | 1 | 0.93 |
| C25 | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C26 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C27 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C28 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C29 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.16 |
| C3  | CIRCULAR | 0.30 | 0.07 | 0.07 | 0.30 | 1 | 0.08 |
| C30 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.50 |
| C31 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.15 |
| C32 | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C33 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.78 |
| C34 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.17 |
| C35 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C36 | CIRCULAR | 0.75 | 0.44 | 0.19 | 0.75 | 1 | 0.94 |
| C37 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.15 |
| C4  | CIRCULAR | 0.20 | 0.03 | 0.05 | 0.20 | 1 | 0.05 |
| C5  | CIRCULAR | 0.30 | 0.07 | 0.07 | 0.30 | 1 | 0.08 |
| C6  | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.14 |
| C7  | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C8  | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C9  | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |

\*\*\*\*\*  
NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
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\*\*\*\*\*  
Analysis Options  
\*\*\*\*\*

Flow Units ..... CMS  
Process Models:  
  Rainfall/Runoff ..... YES  
  RDII ..... NO  
  Snowmelt ..... NO  
  Groundwater ..... NO  
  Flow Routing ..... YES  
  Ponding Allowed ..... NO  
  Water Quality ..... NO  
Infiltration Method ..... HORTON  
Flow Routing Method ..... DYNWAVE  
Surcharge Method ..... EXTRAN  
Starting Date ..... 12/11/2020 00:00:00  
Ending Date ..... 12/21/2020 00:00:00  
Antecedent Dry Days ..... 0.0  
Report Time Step ..... 00:01:00  
Wet Time Step ..... 00:01:00  
Dry Time Step ..... 00:01:00  
Routing Time Step ..... 1.00 sec  
Variable Time Step ..... YES  
Maximum Trials ..... 8  
Number of Threads ..... 6  
Head Tolerance ..... 0.001500 m

| *****                      |           |        |
|----------------------------|-----------|--------|
|                            | Volume    | Depth  |
| Runoff Quantity Continuity | hectare-m | mm     |
| *****                      |           |        |
| Total Precipitation        | 0.260     | 36.865 |
| Evaporation Loss           | 0.000     | 0.000  |
| Infiltration Loss          | 0.017     | 2.475  |
| Surface Runoff             | 0.243     | 34.409 |
| Final Storage              | 0.000     | 0.000  |
| Continuity Error (%)       | -0.052    |        |

| *****                   |           |          |
|-------------------------|-----------|----------|
|                         | Volume    | Volume   |
| Flow Routing Continuity | hectare-m | 10^6 ltr |
| *****                   |           |          |
| Dry Weather Inflow      | 0.000     | 0.000    |
| Wet Weather Inflow      | 0.243     | 2.426    |
| Groundwater Inflow      | 0.000     | 0.000    |
| RDII Inflow             | 0.000     | 0.000    |
| External Inflow         | 0.000     | 0.000    |
| External Outflow        | 0.243     | 2.427    |
| Flooding Loss           | 0.000     | 0.000    |
| Evaporation Loss        | 0.000     | 0.000    |
| Exfiltration Loss       | 0.000     | 0.000    |
| Initial Stored Volume   | 0.000     | 0.000    |
| Final Stored Volume     | 0.000     | 0.000    |
| Continuity Error (%)    | -0.032    |          |

\*\*\*\*\*  
Time-Step Critical Elements  
\*\*\*\*\*  
Link C33 (1.54%)

\*\*\*\*\*  
Highest Flow Instability Indexes  
\*\*\*\*\*

Link C2 (4)  
 Link OR1 (1)  
 Link OR2 (1)

\*\*\*\*\*  
 Routing Time Step Summary  
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Minimum Time Step : 0.15 sec  
 Average Time Step : 1.00 sec  
 Maximum Time Step : 1.00 sec  
 Percent in Steady State : 0.00  
 Average Iterations per Step : 2.00  
 Percent Not Converging : 0.00  
 Time Step Frequencies :  
 1.000 - 0.871 sec : 99.94 %  
 0.871 - 0.758 sec : 0.05 %  
 0.758 - 0.660 sec : 0.01 %  
 0.660 - 0.574 sec : 0.00 %  
 0.574 - 0.500 sec : 0.00 %

\*\*\*\*\*  
 Subcatchment Runoff Summary  
 \*\*\*\*\*

| Subcatchment | Total Precip<br>mm | Total Runon<br>mm | Total Evap<br>mm | Total Infil<br>mm | Imperv Runoff<br>mm | Perv Runoff<br>mm | Total Runoff<br>mm | Total Runoff<br>10 <sup>6</sup> ltr | Peak Runoff<br>CMS | Runoff Coeff |
|--------------|--------------------|-------------------|------------------|-------------------|---------------------|-------------------|--------------------|-------------------------------------|--------------------|--------------|
| Area_1       | 36.86              | 0.00              | 0.00             | 2.56              | 33.20               | 1.13              | 34.33              | 0.09                                | 0.06               | 0.931        |
| Area_10      | 36.86              | 0.00              | 0.00             | 2.56              | 33.20               | 1.13              | 34.33              | 0.03                                | 0.02               | 0.931        |
| Area_101     | 36.86              | 0.00              | 0.00             | 1.29              | 35.03               | 0.56              | 35.59              | 0.49                                | 0.28               | 0.965        |
| Area_102     | 36.86              | 0.00              | 0.00             | 1.29              | 35.03               | 0.56              | 35.59              | 0.40                                | 0.23               | 0.965        |
| Area_11      | 36.86              | 0.00              | 0.00             | 2.56              | 33.20               | 1.13              | 34.33              | 0.04                                | 0.03               | 0.931        |
| Area_12      | 36.86              | 0.00              | 0.00             | 2.56              | 33.20               | 1.13              | 34.33              | 0.05                                | 0.04               | 0.931        |
| Area_13      | 36.86              | 0.00              | 0.00             | 2.56              | 33.20               | 1.13              | 34.33              | 0.05                                | 0.04               | 0.931        |
| Area_14      | 36.86              | 0.00              | 0.00             | 2.56              | 33.20               | 1.13              | 34.33              | 0.06                                | 0.04               | 0.931        |
| Area_15      | 36.86              | 0.00              | 0.00             | 2.56              | 33.20               | 1.13              | 34.33              | 0.03                                | 0.02               | 0.931        |
| Area_16      | 36.86              | 0.00              | 0.00             | 2.56              | 33.20               | 1.13              | 34.33              | 0.05                                | 0.04               | 0.931        |
| Area_17      | 36.86              | 0.00              | 0.00             | 2.56              | 33.20               | 1.13              | 34.33              | 0.06                                | 0.04               | 0.931        |
| Area_18      | 36.86              | 0.00              | 0.00             | 2.56              | 33.20               | 1.13              | 34.33              | 0.06                                | 0.04               | 0.931        |
| Area_19      | 36.86              | 0.00              | 0.00             | 2.56              | 33.20               | 1.13              | 34.33              | 0.06                                | 0.04               | 0.931        |
| Area_2       | 36.86              | 0.00              | 0.00             | 2.56              | 33.20               | 1.13              | 34.33              | 0.05                                | 0.04               | 0.931        |
| Area_20      | 36.86              | 0.00              | 0.00             | 2.56              | 33.20               | 1.13              | 34.33              | 0.10                                | 0.07               | 0.931        |
| Area_2001    | 36.86              | 0.00              | 0.00             | 20.55             | 9.22                | 7.10              | 16.32              | 0.01                                | 0.00               | 0.443        |
| Area_2002    | 36.86              | 0.00              | 0.00             | 2.59              | 33.19               | 1.10              | 34.29              | 0.07                                | 0.04               | 0.930        |
| Area_2003    | 36.86              | 0.00              | 0.00             | 2.61              | 33.19               | 1.08              | 34.27              | 0.05                                | 0.03               | 0.930        |
| Area_2004    | 36.86              | 0.00              | 0.00             | 24.74             | 1.84                | 10.29             | 12.13              | 0.00                                | 0.00               | 0.329        |
| Area_2005    | 36.86              | 0.00              | 0.00             | 24.74             | 1.84                | 10.29             | 12.13              | 0.00                                | 0.00               | 0.329        |
| Area_21      | 36.86              | 0.00              | 0.00             | 2.56              | 33.20               | 1.13              | 34.33              | 0.07                                | 0.05               | 0.931        |
| Area_22      | 36.86              | 0.00              | 0.00             | 2.56              | 33.20               | 1.13              | 34.33              | 0.11                                | 0.08               | 0.931        |
| Area_23      | 36.86              | 0.00              | 0.00             | 2.56              | 33.20               | 1.13              | 34.33              | 0.05                                | 0.04               | 0.931        |
| Area_3       | 36.86              | 0.00              | 0.00             | 2.56              | 33.20               | 1.13              | 34.33              | 0.12                                | 0.09               | 0.931        |
| Area_4       | 36.86              | 0.00              | 0.00             | 2.56              | 33.20               | 1.13              | 34.33              | 0.10                                | 0.07               | 0.931        |
| Area_5       | 36.86              | 0.00              | 0.00             | 2.56              | 33.20               | 1.13              | 34.33              | 0.05                                | 0.04               | 0.931        |
| Area_6       | 36.86              | 0.00              | 0.00             | 2.56              | 33.20               | 1.13              | 34.33              | 0.05                                | 0.04               | 0.931        |
| Area_7       | 36.86              | 0.00              | 0.00             | 2.56              | 33.20               | 1.13              | 34.33              | 0.01                                | 0.01               | 0.931        |
| Area_8       | 36.86              | 0.00              | 0.00             | 2.56              | 33.20               | 1.13              | 34.33              | 0.04                                | 0.03               | 0.931        |
| Area_9       | 36.86              | 0.00              | 0.00             | 2.56              | 33.20               | 1.13              | 34.33              | 0.04                                | 0.03               | 0.931        |

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 Node Depth Summary  
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| Node    | Type     | Average Depth<br>Meters | Maximum Depth<br>Meters | Maximum HGL<br>Meters | Time of Max Occurrence<br>days hr:min | Reported Max Depth<br>Meters |
|---------|----------|-------------------------|-------------------------|-----------------------|---------------------------------------|------------------------------|
| CB_10   | JUNCTION | 0.00                    | 0.11                    | 65.44                 | 0 02:10                               | 0.11                         |
| CB_23   | JUNCTION | 0.00                    | 0.08                    | 66.28                 | 0 02:10                               | 0.08                         |
| CB_27   | JUNCTION | 0.00                    | 0.10                    | 65.59                 | 0 02:10                               | 0.10                         |
| CB_28   | JUNCTION | 0.00                    | 0.10                    | 65.49                 | 0 02:10                               | 0.10                         |
| CB_29   | JUNCTION | 0.00                    | 0.14                    | 64.25                 | 0 02:10                               | 0.14                         |
| CB_5    | JUNCTION | 0.00                    | 0.12                    | 65.23                 | 0 02:10                               | 0.12                         |
| CBMH_11 | JUNCTION | 0.03                    | 0.57                    | 64.15                 | 0 04:41                               | 0.57                         |
| CBMH_12 | JUNCTION | 0.00                    | 0.19                    | 64.25                 | 0 02:10                               | 0.19                         |
| CBMH_14 | JUNCTION | 0.03                    | 0.58                    | 64.68                 | 0 03:37                               | 0.57                         |
| CBMH_15 | JUNCTION | 0.01                    | 0.22                    | 64.69                 | 0 02:10                               | 0.22                         |
| CBMH_18 | JUNCTION | 0.03                    | 0.63                    | 64.68                 | 0 03:42                               | 0.63                         |
| CBMH_19 | JUNCTION | 0.00                    | 0.19                    | 65.07                 | 0 02:10                               | 0.19                         |
| CBMH_2  | JUNCTION | 0.00                    | 0.23                    | 64.29                 | 0 02:10                               | 0.23                         |
| CBMH_21 | JUNCTION | 0.00                    | 0.18                    | 65.35                 | 0 02:10                               | 0.18                         |
| CBMH_22 | JUNCTION | 0.00                    | 0.14                    | 65.67                 | 0 02:10                               | 0.14                         |
| CBMH_3  | JUNCTION | 0.00                    | 0.20                    | 64.62                 | 0 02:10                               | 0.20                         |
| CBMH_4  | JUNCTION | 0.00                    | 0.16                    | 64.94                 | 0 02:10                               | 0.16                         |
| CBMH_6  | JUNCTION | 0.01                    | 0.26                    | 64.17                 | 0 02:10                               | 0.26                         |
| CBMH_7  | JUNCTION | 0.00                    | 0.24                    | 64.51                 | 0 02:10                               | 0.24                         |
| CBMH_8  | JUNCTION | 0.00                    | 0.20                    | 64.83                 | 0 02:10                               | 0.20                         |
| CBMH_9  | JUNCTION | 0.00                    | 0.16                    | 65.15                 | 0 02:10                               | 0.16                         |
| DCB_16  | JUNCTION | 0.00                    | 0.18                    | 64.98                 | 0 02:10                               | 0.18                         |
| J1      | JUNCTION | 0.01                    | 0.08                    | 63.83                 | 0 03:39                               | 0.08                         |

|           |          |      |      |       |   |       |      |
|-----------|----------|------|------|-------|---|-------|------|
| J13       | JUNCTION | 0.04 | 0.62 | 64.16 | 0 | 04:18 | 0.62 |
| J2        | JUNCTION | 0.01 | 0.08 | 63.31 | 0 | 04:41 | 0.08 |
| MH_20     | JUNCTION | 0.00 | 0.18 | 65.17 | 0 | 02:10 | 0.18 |
| MH_24     | JUNCTION | 0.03 | 0.55 | 64.68 | 0 | 03:42 | 0.54 |
| MH_25     | JUNCTION | 0.01 | 0.37 | 64.79 | 0 | 02:10 | 0.37 |
| MH_26     | JUNCTION | 0.00 | 0.41 | 64.97 | 0 | 02:10 | 0.41 |
| MH_27     | JUNCTION | 0.01 | 0.26 | 64.15 | 0 | 04:41 | 0.26 |
| MH_30     | JUNCTION | 0.02 | 0.42 | 64.15 | 0 | 04:39 | 0.42 |
| MH_44     | JUNCTION | 0.01 | 0.12 | 63.63 | 0 | 03:39 | 0.12 |
| MH_45     | JUNCTION | 0.01 | 0.09 | 63.20 | 0 | 04:41 | 0.09 |
| OGS_1     | JUNCTION | 0.01 | 0.04 | 63.08 | 0 | 04:41 | 0.04 |
| OGS_2     | JUNCTION | 0.01 | 0.10 | 63.57 | 0 | 03:39 | 0.10 |
| Humber_P1 | OUTFALL  | 0.00 | 0.00 | 62.48 | 0 | 00:00 | 0.00 |
| OF1       | OUTFALL  | 0.01 | 0.10 | 63.51 | 0 | 03:39 | 0.10 |
| OF2       | OUTFALL  | 0.00 | 0.00 | 0.00  | 0 | 00:00 | 0.00 |
| SU_N      | STORAGE  | 0.07 | 0.93 | 64.68 | 0 | 03:39 | 0.93 |
| SU_S      | STORAGE  | 0.08 | 0.91 | 64.15 | 0 | 04:41 | 0.91 |

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Node Inflow Summary  
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| Node      | Type     | Maximum Lateral Inflow CMS | Maximum Total Inflow CMS | Time of Max Occurrence days hr:min | Lateral Inflow Volume 10^6 ltr | Total Inflow Volume 10^6 ltr | Flow Balance Error Percent |
|-----------|----------|----------------------------|--------------------------|------------------------------------|--------------------------------|------------------------------|----------------------------|
| CB_10     | JUNCTION | 0.033                      | 0.033                    | 0 02:10                            | 0.0446                         | 0.0446                       | -0.008                     |
| CB_23     | JUNCTION | 0.021                      | 0.021                    | 0 02:10                            | 0.0275                         | 0.0275                       | -0.005                     |
| CB_27     | JUNCTION | 0.038                      | 0.038                    | 0 02:10                            | 0.0515                         | 0.0515                       | -0.003                     |
| CB_28     | JUNCTION | 0.038                      | 0.038                    | 0 02:10                            | 0.0515                         | 0.0515                       | -0.003                     |
| CB_29     | JUNCTION | 0.041                      | 0.041                    | 0 02:10                            | 0.0549                         | 0.0549                       | 0.137                      |
| CB_5      | JUNCTION | 0.038                      | 0.038                    | 0 02:10                            | 0.0515                         | 0.0515                       | -0.009                     |
| CBMH_11   | JUNCTION | 0.283                      | 0.405                    | 0 02:10                            | 0.474                          | 0.638                        | -0.024                     |
| CBMH_12   | JUNCTION | 0.082                      | 0.082                    | 0 02:10                            | 0.11                           | 0.11                         | 0.895                      |
| CBMH_14   | JUNCTION | 0.064                      | 0.194                    | 0 02:10                            | 0.0858                         | 0.28                         | -0.250                     |
| CBMH_15   | JUNCTION | 0.041                      | 0.132                    | 0 02:10                            | 0.0549                         | 0.179                        | 0.547                      |
| CBMH_18   | JUNCTION | 0.072                      | 0.505                    | 0 02:10                            | 0.0961                         | 0.915                        | -0.006                     |
| CBMH_19   | JUNCTION | 0.010                      | 0.090                    | 0 02:10                            | 0.0137                         | 0.124                        | 0.005                      |
| CBMH_2    | JUNCTION | 0.044                      | 0.164                    | 0 02:10                            | 0.0584                         | 0.226                        | 0.273                      |
| CBMH_21   | JUNCTION | 0.031                      | 0.080                    | 0 02:10                            | 0.0412                         | 0.11                         | -0.002                     |
| CBMH_22   | JUNCTION | 0.031                      | 0.051                    | 0 02:10                            | 0.0412                         | 0.0687                       | -0.007                     |
| CBMH_3    | JUNCTION | 0.044                      | 0.123                    | 0 02:10                            | 0.0584                         | 0.168                        | 0.068                      |
| CBMH_4    | JUNCTION | 0.044                      | 0.081                    | 0 02:10                            | 0.0584                         | 0.11                         | -0.007                     |
| CBMH_6    | JUNCTION | 0.023                      | 0.174                    | 0 02:10                            | 0.0309                         | 0.243                        | 0.055                      |
| CBMH_7    | JUNCTION | 0.044                      | 0.154                    | 0 02:10                            | 0.0584                         | 0.213                        | 0.159                      |
| CBMH_8    | JUNCTION | 0.041                      | 0.113                    | 0 02:10                            | 0.0549                         | 0.155                        | -0.008                     |
| CBMH_9    | JUNCTION | 0.041                      | 0.074                    | 0 02:10                            | 0.0549                         | 0.0996                       | -0.007                     |
| DCB_16    | JUNCTION | 0.092                      | 0.092                    | 0 02:10                            | 0.124                          | 0.124                        | 0.183                      |
| J1        | JUNCTION | 0.000                      | 0.012                    | 0 03:39                            | 0                              | 0.953                        | -0.005                     |
| J13       | JUNCTION | 0.072                      | 0.404                    | 0 02:10                            | 0.0961                         | 0.664                        | -0.052                     |
| J2        | JUNCTION | 0.000                      | 0.012                    | 0 04:41                            | 0                              | 1.15                         | -0.004                     |
| MH_20     | JUNCTION | 0.000                      | 0.080                    | 0 02:10                            | 0                              | 0.11                         | -0.001                     |
| MH_24     | JUNCTION | 0.000                      | 0.445                    | 0 02:10                            | 0                              | 0.764                        | -0.276                     |
| MH_25     | JUNCTION | 0.000                      | 0.354                    | 0 02:10                            | 0                              | 0.591                        | 0.349                      |
| MH_26     | JUNCTION | 0.278                      | 0.354                    | 0 02:10                            | 0.488                          | 0.591                        | 0.049                      |
| MH_27     | JUNCTION | 0.000                      | 0.041                    | 0 02:10                            | 0                              | 0.0549                       | -0.048                     |
| MH_30     | JUNCTION | 0.000                      | 0.163                    | 0 02:10                            | 0                              | 0.242                        | -0.287                     |
| MH_44     | JUNCTION | 0.000                      | 0.027                    | 0 03:39                            | 0                              | 1.08                         | 0.005                      |
| MH_45     | JUNCTION | 0.000                      | 0.018                    | 0 04:41                            | 0                              | 1.21                         | 0.001                      |
| OGS_1     | JUNCTION | 0.000                      | 0.018                    | 0 04:41                            | 0                              | 1.21                         | -0.000                     |
| OGS_2     | JUNCTION | 0.000                      | 0.027                    | 0 03:39                            | 0                              | 1.08                         | -0.005                     |
| Humber_P1 | OUTFALL  | 0.001                      | 0.018                    | 0 04:38                            | 0.00728                        | 1.21                         | 0.000                      |
| OF1       | OUTFALL  | 0.034                      | 0.042                    | 0 02:10                            | 0.0548                         | 1.13                         | 0.000                      |
| OF2       | OUTFALL  | 0.046                      | 0.046                    | 0 02:10                            | 0.0834                         | 0.0834                       | 0.000                      |
| SU_N      | STORAGE  | 0.000                      | 0.697                    | 0 02:10                            | 0                              | 1.14                         | -0.093                     |
| SU_S      | STORAGE  | 0.000                      | 0.807                    | 0 02:10                            | 0                              | 1.29                         | -0.100                     |

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Node Surcharge Summary  
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No nodes were surcharged.

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Node Flooding Summary  
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No nodes were flooded.

\*\*\*\*\*  
Storage Volume Summary  
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| Storage Unit | Average Volume 1000 m3 | Avg Full | Evap Loss | Exfil Loss | Maximum Volume 1000 m3 | Max Full | Time of Max Occurrence days hr:min | Maximum Outflow CMS |
|--------------|------------------------|----------|-----------|------------|------------------------|----------|------------------------------------|---------------------|
| SU_N         | 0.052                  | 2        | 0         | 0          | 0.783                  | 30       | 0 03:39                            | 0.034               |



SU\_s 0.076 2 0 0 0.957 28 0 04:41 0.058

\*\*\*\*\*  
 Outfall Loading Summary  
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| Outfall Node | Flow Freq Pent | Avg Flow CMS | Max Flow CMS | Total Volume 10^6 ltr |
|--------------|----------------|--------------|--------------|-----------------------|
| Humber_Pl    | 28.18          | 0.005        | 0.018        | 1.213                 |
| OF1          | 23.24          | 0.006        | 0.042        | 1.130                 |
| OF2          | 3.86           | 0.003        | 0.046        | 0.083                 |
| System       | 18.42          | 0.014        | 0.097        | 2.427                 |

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 Link Flow Summary  
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| Link | Type    | Maximum  Flow  CMS | Time of Max Occurrence days hr:min | Maximum  Veloc  m/sec | Max/ Full Flow | Max/ Full Depth |
|------|---------|--------------------|------------------------------------|-----------------------|----------------|-----------------|
| C1   | CONDUIT | 0.015              | 0 03:39                            | 1.34                  | 0.31           | 0.39            |
| C10  | CONDUIT | 0.038              | 0 02:10                            | 1.41                  | 0.11           | 0.23            |
| C11  | CONDUIT | 0.038              | 0 02:10                            | 1.41                  | 0.11           | 0.23            |
| C12  | CONDUIT | 0.354              | 0 02:10                            | 1.97                  | 0.99           | 0.78            |
| C13  | CONDUIT | 0.443              | 0 02:10                            | 2.04                  | 0.86           | 0.93            |
| C14  | CONDUIT | 0.020              | 0 02:10                            | 1.19                  | 0.10           | 0.21            |
| C15  | CONDUIT | 0.050              | 0 02:10                            | 1.19                  | 0.21           | 0.31            |
| C16  | CONDUIT | 0.080              | 0 02:10                            | 1.36                  | 0.34           | 0.40            |
| C17  | CONDUIT | 0.080              | 0 02:10                            | 1.35                  | 0.34           | 0.40            |
| C18  | CONDUIT | 0.090              | 0 02:10                            | 1.40                  | 0.38           | 0.42            |
| C19  | CONDUIT | 0.033              | 0 02:10                            | 1.05                  | 0.14           | 0.25            |
| C2   | CONDUIT | 0.027              | 0 03:39                            | 1.00                  | 0.21           | 0.29            |
| C20  | CONDUIT | 0.073              | 0 02:10                            | 1.30                  | 0.20           | 0.31            |
| C21  | CONDUIT | 0.112              | 0 02:10                            | 1.47                  | 0.31           | 0.38            |
| C22  | CONDUIT | 0.153              | 0 02:10                            | 1.60                  | 0.43           | 0.46            |
| C23  | CONDUIT | 0.175              | 0 02:10                            | 1.65                  | 0.48           | 0.61            |
| C24  | CONDUIT | 0.405              | 0 02:10                            | 2.03                  | 0.43           | 0.84            |
| C25  | CONDUIT | 0.038              | 0 02:10                            | 1.08                  | 0.11           | 0.22            |
| C26  | CONDUIT | 0.080              | 0 02:10                            | 1.32                  | 0.16           | 0.27            |
| C27  | CONDUIT | 0.122              | 0 02:10                            | 1.49                  | 0.24           | 0.33            |
| C28  | CONDUIT | 0.163              | 0 02:10                            | 1.61                  | 0.32           | 0.39            |
| C29  | CONDUIT | 0.082              | 0 02:10                            | 1.32                  | 0.52           | 0.62            |
| C3   | CONDUIT | 0.012              | 0 03:39                            | 0.80                  | 0.15           | 0.26            |
| C30  | CONDUIT | 0.164              | 0 02:10                            | 1.59                  | 0.32           | 0.74            |
| C31  | CONDUIT | 0.041              | 0 02:10                            | 1.08                  | 0.28           | 0.75            |
| C32  | CONDUIT | 0.403              | 0 02:10                            | 2.10                  | 1.12           | 1.00            |
| C33  | CONDUIT | 0.018              | 0 04:41                            | 2.92                  | 0.02           | 0.11            |
| C34  | CONDUIT | 0.027              | 0 03:39                            | 1.12                  | 0.16           | 0.27            |
| C35  | CONDUIT | 0.356              | 0 02:10                            | 1.95                  | 0.69           | 0.62            |
| C36  | CONDUIT | 0.505              | 0 02:10                            | 2.17                  | 0.54           | 0.85            |
| C37  | CONDUIT | 0.041              | 0 02:10                            | 1.14                  | 0.28           | 0.36            |
| C4   | CONDUIT | 0.007              | 0 04:41                            | 1.06                  | 0.14           | 0.25            |
| C5   | CONDUIT | 0.012              | 0 04:41                            | 0.81                  | 0.14           | 0.26            |
| C6   | CONDUIT | 0.018              | 0 04:41                            | 0.89                  | 0.13           | 0.24            |
| C7   | CONDUIT | 0.091              | 0 02:10                            | 1.39                  | 0.25           | 0.34            |
| C8   | CONDUIT | 0.131              | 0 02:10                            | 1.53                  | 0.36           | 0.69            |
| C9   | CONDUIT | 0.193              | 0 02:10                            | 1.69                  | 0.38           | 0.98            |
| OR1  | ORIFICE | 0.012              | 0 04:41                            |                       |                | 1.00            |
| OR2  | ORIFICE | 0.012              | 0 03:39                            |                       |                | 1.00            |

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 Flow Classification Summary  
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| Conduit | Adjusted /Actual Length | Fraction of Time in Flow Class |          |         |          |         |           |           |           |      |
|---------|-------------------------|--------------------------------|----------|---------|----------|---------|-----------|-----------|-----------|------|
|         |                         | Up Dry                         | Down Dry | Sub Dry | Sup Crit | Up Crit | Down Crit | Norm Crit | Inlet Ltd | Ctrl |
| C1      | 1.00                    | 0.98                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 0.02      | 0.00      | 0.00 |
| C10     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C11     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C12     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.04     | 0.00    | 0.00      | 0.96      | 0.01      | 0.00 |
| C13     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.09     | 0.00    | 0.00      | 0.91      | 0.00      | 0.00 |
| C14     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C15     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C16     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C17     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C18     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C19     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C2      | 1.00                    | 0.00                           | 0.10     | 0.00    | 0.76     | 0.14    | 0.00      | 0.00      | 0.78      | 0.00 |
| C20     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C21     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.00     | 0.00    | 0.00      | 1.00      | 0.00      | 0.00 |
| C22     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.04     | 0.00    | 0.00      | 0.96      | 0.04      | 0.00 |
| C23     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.07     | 0.00    | 0.00      | 0.93      | 0.03      | 0.00 |
| C24     | 1.00                    | 0.00                           | 0.00     | 0.00    | 0.12     | 0.00    | 0.00      | 0.88      | 0.01      | 0.00 |

|     |      |      |      |      |      |      |      |      |      |      |
|-----|------|------|------|------|------|------|------|------|------|------|
| C25 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C26 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C27 | 1.00 | 0.00 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0.99 | 0.01 | 0.00 |
| C28 | 1.00 | 0.00 | 0.00 | 0.00 | 0.07 | 0.00 | 0.00 | 0.93 | 0.05 | 0.00 |
| C29 | 1.00 | 0.00 | 0.00 | 0.00 | 0.07 | 0.00 | 0.00 | 0.93 | 0.05 | 0.00 |
| C3  | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C30 | 1.00 | 0.00 | 0.00 | 0.00 | 0.09 | 0.00 | 0.00 | 0.91 | 0.01 | 0.00 |
| C31 | 1.00 | 0.00 | 0.00 | 0.00 | 0.06 | 0.00 | 0.00 | 0.94 | 0.01 | 0.00 |
| C32 | 1.00 | 0.00 | 0.00 | 0.00 | 0.12 | 0.00 | 0.00 | 0.88 | 0.01 | 0.00 |
| C33 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C34 | 1.00 | 0.00 | 0.00 | 0.00 | 0.74 | 0.26 | 0.00 | 0.00 | 0.04 | 0.00 |
| C35 | 1.00 | 0.00 | 0.00 | 0.00 | 0.07 | 0.00 | 0.00 | 0.93 | 0.03 | 0.00 |
| C36 | 1.00 | 0.00 | 0.00 | 0.00 | 0.10 | 0.00 | 0.00 | 0.90 | 0.00 | 0.00 |
| C37 | 1.00 | 0.00 | 0.00 | 0.00 | 0.04 | 0.00 | 0.00 | 0.96 | 0.03 | 0.00 |
| C4  | 1.00 | 0.98 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.02 | 0.00 | 0.00 |
| C5  | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C6  | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C7  | 1.00 | 0.00 | 0.00 | 0.00 | 0.03 | 0.00 | 0.00 | 0.97 | 0.03 | 0.00 |
| C8  | 1.00 | 0.00 | 0.00 | 0.00 | 0.08 | 0.00 | 0.00 | 0.92 | 0.04 | 0.00 |
| C9  | 1.00 | 0.00 | 0.00 | 0.00 | 0.09 | 0.00 | 0.00 | 0.90 | 0.01 | 0.00 |

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 Conduit Surcharge Summary  
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| Conduit | Hours Full |          |          | Hours                  |                        |
|---------|------------|----------|----------|------------------------|------------------------|
|         | Both Ends  | Upstream | Dnstream | Above Full Normal Flow | Hours Capacity Limited |
| C29     | 0.01       | 0.01     | 1.00     | 0.01                   | 0.01                   |
| C32     | 4.03       | 4.03     | 6.86     | 0.04                   | 0.01                   |
| C9      | 0.01       | 0.01     | 3.57     | 0.01                   | 0.01                   |

Analysis begun on: Wed Oct 5 21:11:37 2022  
 Analysis ended on: Wed Oct 5 21:12:08 2022  
 Total elapsed time: 00:00:31

5-yr, 3-hour

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.015)

WARNING 03: negative offset ignored for Link C2  
WARNING 03: negative offset ignored for Link C32  
WARNING 03: negative offset ignored for Link C34

\*\*\*\*\*  
Element Count

\*\*\*\*\*  
Number of rain gages ..... 7  
Number of subcatchments ... 30  
Number of nodes ..... 40  
Number of links ..... 39  
Number of pollutants ..... 0  
Number of land uses ..... 0

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Raingage Summary

\*\*\*\*\*  
Name Data Source Data Type Recording Interval

| Name      | Data Source | Data Type | Recording Interval |
|-----------|-------------|-----------|--------------------|
| 25mm      | 25mm        | INTENSITY | 5 min.             |
| 3hr-100yr | 3hr-100yr   | INTENSITY | 10 min.            |
| 3hr-2yr   | 3hr-2yr     | INTENSITY | 5 min.             |
| 3hr-5yr   | 3hr-5yr     | INTENSITY | 5 min.             |
| 6hr-100yr | 6hr-100yr   | INTENSITY | 10 min.            |
| 6hr-2yr   | 6hr-2yr     | INTENSITY | 5 min.             |
| 6hr-5yr   | 6hr-5yr     | INTENSITY | 5 min.             |

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Subcatchment Summary

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Name Area Width %Imperv %Slope Rain Gage Outlet

| Name      | Area | Width  | %Imperv | %Slope | Rain Gage | Outlet    |
|-----------|------|--------|---------|--------|-----------|-----------|
| Area_1    | 0.25 | 83.33  | 90.00   | 1.0000 | 3hr-5yr   | CBMH_14   |
| Area_10   | 0.08 | 26.67  | 90.00   | 1.0000 | 3hr-5yr   | CB_23     |
| Area_101  | 1.37 | 137.00 | 95.00   | 0.5000 | 3hr-5yr   | MH_26     |
| Area_102  | 1.13 | 113.00 | 95.00   | 0.5000 | 3hr-5yr   | CBMH_11   |
| Area_11   | 0.13 | 43.33  | 90.00   | 1.0000 | 3hr-5yr   | CB_10     |
| Area_12   | 0.16 | 53.33  | 90.00   | 1.0000 | 3hr-5yr   | CBMH_9    |
| Area_13   | 0.16 | 53.33  | 90.00   | 1.0000 | 3hr-5yr   | CBMH_8    |
| Area_14   | 0.17 | 56.67  | 90.00   | 1.0000 | 3hr-5yr   | CBMH_7    |
| Area_15   | 0.09 | 30.00  | 90.00   | 1.0000 | 3hr-5yr   | CBMH_6    |
| Area_16   | 0.15 | 50.00  | 90.00   | 1.0000 | 3hr-5yr   | CB_5      |
| Area_17   | 0.17 | 56.67  | 90.00   | 1.0000 | 3hr-5yr   | CBMH_4    |
| Area_18   | 0.17 | 56.67  | 90.00   | 1.0000 | 3hr-5yr   | CBMH_3    |
| Area_19   | 0.17 | 56.67  | 90.00   | 1.0000 | 3hr-5yr   | CBMH_2    |
| Area_2    | 0.16 | 53.33  | 90.00   | 1.0000 | 3hr-5yr   | CBMH_15   |
| Area_20   | 0.28 | 93.33  | 90.00   | 1.0000 | 3hr-5yr   | J13       |
| Area_2001 | 0.07 | 7.00   | 25.00   | 0.5000 | 3hr-5yr   | OF2       |
| Area_2002 | 0.21 | 21.00  | 90.00   | 0.5000 | 3hr-5yr   | OF2       |
| Area_2003 | 0.16 | 16.00  | 90.00   | 1.0000 | 3hr-5yr   | OF1       |
| Area_2004 | 0.02 | 13.33  | 5.00    | 0.5000 | 3hr-5yr   | Humber_P1 |
| Area_2005 | 0.04 | 26.67  | 5.00    | 0.5000 | 3hr-5yr   | Humber_P1 |
| Area_21   | 0.21 | 70.00  | 90.00   | 1.0000 | 3hr-5yr   | CBMH_11   |
| Area_22   | 0.32 | 106.67 | 90.00   | 1.0000 | 3hr-5yr   | CBMH_12   |
| Area_23   | 0.16 | 53.33  | 90.00   | 1.0000 | 3hr-5yr   | CB_29     |
| Area_3    | 0.36 | 120.00 | 90.00   | 1.0000 | 3hr-5yr   | DCB_16    |
| Area_4    | 0.28 | 93.33  | 90.00   | 1.0000 | 3hr-5yr   | CBMH_18   |
| Area_5    | 0.15 | 50.00  | 90.00   | 1.0000 | 3hr-5yr   | CB_27     |
| Area_6    | 0.15 | 50.00  | 90.00   | 1.0000 | 3hr-5yr   | CB_28     |
| Area_7    | 0.04 | 13.33  | 90.00   | 1.0000 | 3hr-5yr   | CBMH_19   |
| Area_8    | 0.12 | 40.00  | 90.00   | 1.0000 | 3hr-5yr   | CBMH_21   |
| Area_9    | 0.12 | 40.00  | 90.00   | 1.0000 | 3hr-5yr   | CBMH_22   |

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Node Summary

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Name Type Invert Elev. Max. Depth Poned Area External Inflow

| Name    | Type     | Invert Elev. | Max. Depth | Poned Area | External Inflow |
|---------|----------|--------------|------------|------------|-----------------|
| CB_10   | JUNCTION | 65.33        | 1.41       | 10.0       |                 |
| CB_23   | JUNCTION | 66.20        | 0.93       | 10.0       |                 |
| CB_27   | JUNCTION | 65.48        | 1.34       | 10.0       |                 |
| CB_28   | JUNCTION | 65.39        | 1.52       | 10.0       |                 |
| CB_29   | JUNCTION | 64.11        | 2.43       | 0.0        |                 |
| CB_5    | JUNCTION | 65.11        | 1.63       | 10.0       |                 |
| CBMH_11 | JUNCTION | 63.58        | 2.16       | 10.0       |                 |
| CBMH_12 | JUNCTION | 64.06        | 1.68       | 10.0       |                 |
| CBMH_14 | JUNCTION | 64.11        | 2.21       | 10.0       |                 |
| CBMH_15 | JUNCTION | 64.47        | 1.85       | 10.0       |                 |
| CBMH_18 | JUNCTION | 64.05        | 2.54       | 0.0        |                 |
| CBMH_19 | JUNCTION | 64.88        | 2.38       | 10.0       |                 |
| CBMH_2  | JUNCTION | 64.06        | 2.94       | 10.0       |                 |
| CBMH_21 | JUNCTION | 65.17        | 1.87       | 10.0       |                 |
| CBMH_22 | JUNCTION | 65.53        | 1.51       | 10.0       |                 |

|           |          |       |      |      |
|-----------|----------|-------|------|------|
| CBMH_3    | JUNCTION | 64.42 | 2.58 | 10.0 |
| CBMH_4    | JUNCTION | 64.78 | 2.22 | 10.0 |
| CBMH_6    | JUNCTION | 63.91 | 2.73 | 10.0 |
| CBMH_7    | JUNCTION | 64.27 | 2.73 | 10.0 |
| CBMH_8    | JUNCTION | 64.63 | 2.37 | 10.0 |
| CBMH_9    | JUNCTION | 64.99 | 2.01 | 10.0 |
| DCB_16    | JUNCTION | 64.80 | 1.52 | 10.0 |
| J1        | JUNCTION | 63.75 | 3.27 | 0.0  |
| J13       | JUNCTION | 63.54 | 3.10 | 10.0 |
| J2        | JUNCTION | 63.24 | 3.33 | 0.0  |
| MH_20     | JUNCTION | 64.99 | 2.30 | 0.0  |
| MH_24     | JUNCTION | 64.13 | 2.50 | 10.0 |
| MH_25     | JUNCTION | 64.42 | 2.63 | 0.0  |
| MH_26     | JUNCTION | 64.56 | 2.70 | 0.0  |
| MH_27     | JUNCTION | 63.89 | 2.02 | 0.0  |
| MH_30     | JUNCTION | 63.73 | 3.08 | 0.0  |
| MH_44     | JUNCTION | 63.51 | 3.51 | 0.0  |
| MH_45     | JUNCTION | 63.11 | 3.46 | 0.0  |
| OGS_1     | JUNCTION | 63.04 | 3.34 | 0.0  |
| OGS_2     | JUNCTION | 63.47 | 3.01 | 0.0  |
| Humber_P1 | OUTFALL  | 62.48 | 0.38 | 0.0  |
| OF1       | OUTFALL  | 63.41 | 0.38 | 0.0  |
| OF2       | OUTFALL  | 0.00  | 0.00 | 0.0  |
| SU_N      | STORAGE  | 63.75 | 3.04 | 0.0  |
| SU_S      | STORAGE  | 63.24 | 3.33 | 0.0  |

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Link Summary  
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| Name | From Node | To Node   | Type    | Length | %Slope  | Roughness |
|------|-----------|-----------|---------|--------|---------|-----------|
| C1   | SU_N      | MH_44     | CONDUIT | 2.5    | 1.0001  | 0.0090    |
| C10  | CB_28     | MH_26     | CONDUIT | 30.4   | 1.0001  | 0.0110    |
| C11  | CB_27     | MH_26     | CONDUIT | 32.8   | 1.0001  | 0.0110    |
| C12  | MH_26     | MH_25     | CONDUIT | 16.5   | 0.4970  | 0.0110    |
| C13  | MH_24     | CBMH_18   | CONDUIT | 4.8    | 0.5000  | 0.0110    |
| C14  | CB_23     | CBMH_22   | CONDUIT | 51.5   | 1.0001  | 0.0110    |
| C15  | CBMH_22   | CBMH_21   | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C16  | CBMH_21   | MH_20     | CONDUIT | 24.5   | 0.5020  | 0.0110    |
| C17  | MH_20     | CBMH_19   | CONDUIT | 10.4   | 0.5000  | 0.0110    |
| C18  | CBMH_19   | MH_24     | CONDUIT | 46.5   | 0.5011  | 0.0110    |
| C19  | CB_10     | CBMH_9    | CONDUIT | 52.5   | 0.4991  | 0.0110    |
| C2   | MH_44     | OGS_2     | CONDUIT | 11.6   | 0.3707  | 0.0110    |
| C20  | CBMH_9    | CBMH_8    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C21  | CBMH_8    | CBMH_7    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C22  | CBMH_7    | CBMH_6    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C23  | CBMH_6    | J13       | CONDUIT | 29.9   | 0.5017  | 0.0110    |
| C24  | J13       | SU_S      | CONDUIT | 4.0    | 0.5000  | 0.0110    |
| C25  | CB_5      | CBMH_4    | CONDUIT | 52.5   | 0.4991  | 0.0110    |
| C26  | CBMH_4    | CBMH_3    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C27  | CBMH_3    | CBMH_2    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C28  | CBMH_2    | MH_30     | CONDUIT | 53.4   | 0.4963  | 0.0110    |
| C29  | CBMH_12   | CBMH_11   | CONDUIT | 50.0   | 0.5700  | 0.0110    |
| C3   | J1        | MH_44     | CONDUIT | 2.5    | 0.4800  | 0.0110    |
| C30  | MH_30     | J13       | CONDUIT | 9.3    | 0.4839  | 0.0110    |
| C31  | MH_27     | CBMH_11   | CONDUIT | 8.2    | 0.5000  | 0.0110    |
| C32  | CBMH_11   | SU_S      | CONDUIT | 13.2   | 0.5000  | 0.0110    |
| C33  | OGS_1     | Humber_P1 | CONDUIT | 4.0    | 14.1135 | 0.0110    |
| C34  | OGS_2     | OF1       | CONDUIT | 8.7    | 0.6782  | 0.0110    |
| C35  | MH_25     | MH_24     | CONDUIT | 44.2   | 0.5000  | 0.0110    |
| C36  | CBMH_18   | SU_N      | CONDUIT | 3.9    | 0.5128  | 0.0110    |
| C37  | CB_29     | MH_27     | CONDUIT | 32.9   | 0.4985  | 0.0110    |
| C4   | SU_S      | MH_45     | CONDUIT | 9.4    | 1.0001  | 0.0090    |
| C5   | J2        | MH_45     | CONDUIT | 9.4    | 0.5000  | 0.0110    |
| C6   | MH_45     | OGS_1     | CONDUIT | 3.1    | 0.4839  | 0.0110    |
| C7   | DCB_16    | CBMH_15   | CONDUIT | 54.4   | 0.5000  | 0.0110    |
| C8   | CBMH_15   | CBMH_14   | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C9   | CBMH_14   | SU_N      | CONDUIT | 15.2   | 0.5000  | 0.0110    |
| OR1  | SU_S      | J2        | ORIFICE |        |         |           |
| OR2  | SU_N      | J1        | ORIFICE |        |         |           |

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Cross Section Summary  
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| Conduit | Shape    | Full Depth | Full Area | Hyd. Rad. | Max. Width | No. of Barrels | Full Flow |
|---------|----------|------------|-----------|-----------|------------|----------------|-----------|
| C1      | CIRCULAR | 0.20       | 0.03      | 0.05      | 0.20       | 1              | 0.05      |
| C10     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.34      |
| C11     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.34      |
| C12     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C13     | CIRCULAR | 0.60       | 0.28      | 0.15      | 0.60       | 1              | 0.51      |
| C14     | CIRCULAR | 0.38       | 0.11      | 0.09      | 0.38       | 1              | 0.21      |
| C15     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C16     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C17     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C18     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C19     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C2      | CIRCULAR | 0.38       | 0.11      | 0.09      | 0.38       | 1              | 0.13      |
| C20     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C21     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C22     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C23     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |

|     |          |      |      |      |      |   |      |
|-----|----------|------|------|------|------|---|------|
| C24 | CIRCULAR | 0.75 | 0.44 | 0.19 | 0.75 | 1 | 0.93 |
| C25 | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C26 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C27 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C28 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C29 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.16 |
| C3  | CIRCULAR | 0.30 | 0.07 | 0.07 | 0.30 | 1 | 0.08 |
| C30 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.50 |
| C31 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.15 |
| C32 | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C33 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.78 |
| C34 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.17 |
| C35 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C36 | CIRCULAR | 0.75 | 0.44 | 0.19 | 0.75 | 1 | 0.94 |
| C37 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.15 |
| C4  | CIRCULAR | 0.20 | 0.03 | 0.05 | 0.20 | 1 | 0.05 |
| C5  | CIRCULAR | 0.30 | 0.07 | 0.07 | 0.30 | 1 | 0.08 |
| C6  | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.14 |
| C7  | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C8  | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C9  | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |

\*\*\*\*\*  
NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
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\*\*\*\*\*  
Analysis Options  
\*\*\*\*\*

Flow Units ..... CMS  
Process Models:  
  Rainfall/Runoff ..... YES  
  RDII ..... NO  
  Snowmelt ..... NO  
  Groundwater ..... NO  
  Flow Routing ..... YES  
  Ponding Allowed ..... NO  
  Water Quality ..... NO  
Infiltration Method ..... HORTON  
Flow Routing Method ..... DYNWAVE  
Surcharge Method ..... EXTRAN  
Starting Date ..... 12/11/2020 00:00:00  
Ending Date ..... 12/21/2020 00:00:00  
Antecedent Dry Days ..... 0.0  
Report Time Step ..... 00:01:00  
Wet Time Step ..... 00:01:00  
Dry Time Step ..... 00:01:00  
Routing Time Step ..... 1.00 sec  
Variable Time Step ..... YES  
Maximum Trials ..... 8  
Number of Threads ..... 6  
Head Tolerance ..... 0.001500 m

| *****                      |           |        |
|----------------------------|-----------|--------|
|                            | Volume    | Depth  |
| Runoff Quantity Continuity | hectare-m | mm     |
| *****                      |           |        |
|                            | -----     | -----  |
| Total Precipitation .....  | 0.300     | 42.540 |
| Evaporation Loss .....     | 0.000     | 0.000  |
| Infiltration Loss .....    | 0.017     | 2.395  |
| Surface Runoff .....       | 0.283     | 40.179 |
| Final Storage .....        | 0.000     | 0.000  |
| Continuity Error (%) ..... | -0.080    |        |

| *****                       |           |          |
|-----------------------------|-----------|----------|
|                             | Volume    | Volume   |
| Flow Routing Continuity     | hectare-m | 10^6 ltr |
| *****                       |           |          |
|                             | -----     | -----    |
| Dry Weather Inflow .....    | 0.000     | 0.000    |
| Wet Weather Inflow .....    | 0.283     | 2.832    |
| Groundwater Inflow .....    | 0.000     | 0.000    |
| RDII Inflow .....           | 0.000     | 0.000    |
| External Inflow .....       | 0.000     | 0.000    |
| External Outflow .....      | 0.283     | 2.834    |
| Flooding Loss .....         | 0.000     | 0.000    |
| Evaporation Loss .....      | 0.000     | 0.000    |
| Exfiltration Loss .....     | 0.000     | 0.000    |
| Initial Stored Volume ..... | 0.000     | 0.000    |
| Final Stored Volume .....   | 0.000     | 0.000    |
| Continuity Error (%) .....  | -0.061    |          |

\*\*\*\*\*  
Time-Step Critical Elements  
\*\*\*\*\*  
Link C33 (1.37%)

\*\*\*\*\*  
Highest Flow Instability Indexes  
\*\*\*\*\*

Link C2 (4)  
 Link OR1 (1)  
 Link OR2 (1)

\*\*\*\*\*  
 Routing Time Step Summary  
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Minimum Time Step : 0.44 sec  
 Average Time Step : 0.99 sec  
 Maximum Time Step : 1.00 sec  
 Percent in Steady State : -0.00  
 Average Iterations per Step : 2.00  
 Percent Not Converging : 0.00  
 Time Step Frequencies :  
 1.000 - 0.871 sec : 98.11 %  
 0.871 - 0.758 sec : 0.37 %  
 0.758 - 0.660 sec : 0.50 %  
 0.660 - 0.574 sec : 0.57 %  
 0.574 - 0.500 sec : 0.46 %

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 Subcatchment Runoff Summary  
 \*\*\*\*\*

| Subcatchment | Total Precip<br>mm | Total Runon<br>mm | Total Evap<br>mm | Total Infil<br>mm | Imperv Runoff<br>mm | Perv Runoff<br>mm | Total Runoff<br>mm | Total Runoff<br>10 <sup>6</sup> ltr | Peak Runoff<br>CMS | Runoff<br>Coeff |
|--------------|--------------------|-------------------|------------------|-------------------|---------------------|-------------------|--------------------|-------------------------------------|--------------------|-----------------|
| Area_1       | 42.54              | 0.00              | 0.00             | 2.47              | 38.33               | 1.79              | 40.12              | 0.10                                | 0.09               | 0.943           |
| Area_10      | 42.54              | 0.00              | 0.00             | 2.47              | 38.33               | 1.79              | 40.12              | 0.03                                | 0.03               | 0.943           |
| Area_101     | 42.54              | 0.00              | 0.00             | 1.24              | 40.43               | 0.89              | 41.32              | 0.57                                | 0.38               | 0.971           |
| Area_102     | 42.54              | 0.00              | 0.00             | 1.24              | 40.43               | 0.89              | 41.32              | 0.47                                | 0.31               | 0.971           |
| Area_11      | 42.54              | 0.00              | 0.00             | 2.47              | 38.33               | 1.79              | 40.12              | 0.05                                | 0.05               | 0.943           |
| Area_12      | 42.54              | 0.00              | 0.00             | 2.47              | 38.33               | 1.79              | 40.12              | 0.06                                | 0.06               | 0.943           |
| Area_13      | 42.54              | 0.00              | 0.00             | 2.47              | 38.33               | 1.79              | 40.12              | 0.06                                | 0.06               | 0.943           |
| Area_14      | 42.54              | 0.00              | 0.00             | 2.47              | 38.33               | 1.79              | 40.12              | 0.07                                | 0.06               | 0.943           |
| Area_15      | 42.54              | 0.00              | 0.00             | 2.47              | 38.33               | 1.79              | 40.12              | 0.04                                | 0.03               | 0.943           |
| Area_16      | 42.54              | 0.00              | 0.00             | 2.47              | 38.33               | 1.79              | 40.12              | 0.06                                | 0.05               | 0.943           |
| Area_17      | 42.54              | 0.00              | 0.00             | 2.47              | 38.33               | 1.79              | 40.12              | 0.07                                | 0.06               | 0.943           |
| Area_18      | 42.54              | 0.00              | 0.00             | 2.47              | 38.33               | 1.79              | 40.12              | 0.07                                | 0.06               | 0.943           |
| Area_19      | 42.54              | 0.00              | 0.00             | 2.47              | 38.33               | 1.79              | 40.12              | 0.07                                | 0.06               | 0.943           |
| Area_2       | 42.54              | 0.00              | 0.00             | 2.47              | 38.33               | 1.79              | 40.12              | 0.06                                | 0.06               | 0.943           |
| Area_20      | 42.54              | 0.00              | 0.00             | 2.47              | 38.33               | 1.79              | 40.12              | 0.11                                | 0.10               | 0.943           |
| Area_2001    | 42.54              | 0.00              | 0.00             | 20.24             | 10.64               | 11.67             | 22.31              | 0.02                                | 0.01               | 0.524           |
| Area_2002    | 42.54              | 0.00              | 0.00             | 2.51              | 38.30               | 1.74              | 40.05              | 0.08                                | 0.06               | 0.941           |
| Area_2003    | 42.54              | 0.00              | 0.00             | 2.53              | 38.31               | 1.73              | 40.03              | 0.06                                | 0.05               | 0.941           |
| Area_2004    | 42.54              | 0.00              | 0.00             | 24.03             | 2.13                | 16.39             | 18.52              | 0.00                                | 0.00               | 0.435           |
| Area_2005    | 42.54              | 0.00              | 0.00             | 24.03             | 2.13                | 16.39             | 18.52              | 0.01                                | 0.00               | 0.435           |
| Area_21      | 42.54              | 0.00              | 0.00             | 2.47              | 38.33               | 1.79              | 40.12              | 0.08                                | 0.08               | 0.943           |
| Area_22      | 42.54              | 0.00              | 0.00             | 2.47              | 38.33               | 1.79              | 40.12              | 0.13                                | 0.12               | 0.943           |
| Area_23      | 42.54              | 0.00              | 0.00             | 2.47              | 38.33               | 1.79              | 40.12              | 0.06                                | 0.06               | 0.943           |
| Area_3       | 42.54              | 0.00              | 0.00             | 2.47              | 38.33               | 1.79              | 40.12              | 0.14                                | 0.13               | 0.943           |
| Area_4       | 42.54              | 0.00              | 0.00             | 2.47              | 38.33               | 1.79              | 40.12              | 0.11                                | 0.10               | 0.943           |
| Area_5       | 42.54              | 0.00              | 0.00             | 2.47              | 38.33               | 1.79              | 40.12              | 0.06                                | 0.05               | 0.943           |
| Area_6       | 42.54              | 0.00              | 0.00             | 2.47              | 38.33               | 1.79              | 40.12              | 0.06                                | 0.05               | 0.943           |
| Area_7       | 42.54              | 0.00              | 0.00             | 2.47              | 38.33               | 1.79              | 40.12              | 0.02                                | 0.01               | 0.943           |
| Area_8       | 42.54              | 0.00              | 0.00             | 2.47              | 38.33               | 1.79              | 40.12              | 0.05                                | 0.04               | 0.943           |
| Area_9       | 42.54              | 0.00              | 0.00             | 2.47              | 38.33               | 1.79              | 40.12              | 0.05                                | 0.04               | 0.943           |

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 Node Depth Summary  
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| Node    | Type     | Average<br>Depth<br>Meters | Maximum<br>Depth<br>Meters | Maximum<br>HGL<br>Meters | Time of Max<br>Occurrence<br>days hr:min | Reported<br>Max Depth<br>Meters |
|---------|----------|----------------------------|----------------------------|--------------------------|--|---------------------------------|
| CB_10   | JUNCTION | 0.00                       | 0.13                       | 65.46                    | 0 01:05                                  | 0.13                            |
| CB_23   | JUNCTION | 0.00                       | 0.09                       | 66.29                    | 0 01:05                                  | 0.09                            |
| CB_27   | JUNCTION | 0.00                       | 0.12                       | 65.61                    | 0 01:05                                  | 0.12                            |
| CB_28   | JUNCTION | 0.00                       | 0.12                       | 65.51                    | 0 01:05                                  | 0.12                            |
| CB_29   | JUNCTION | 0.00                       | 0.16                       | 64.28                    | 0 01:04                                  | 0.16                            |
| CB_5    | JUNCTION | 0.00                       | 0.14                       | 65.25                    | 0 01:05                                  | 0.14                            |
| CBMH_11 | JUNCTION | 0.04                       | 0.66                       | 64.25                    | 0 02:10                                  | 0.66                            |
| CBMH_12 | JUNCTION | 0.00                       | 0.24                       | 64.30                    | 0 01:05                                  | 0.24                            |
| CBMH_14 | JUNCTION | 0.03                       | 0.68                       | 64.79                    | 0 01:56                                  | 0.68                            |
| CBMH_15 | JUNCTION | 0.01                       | 0.32                       | 64.79                    | 0 01:53                                  | 0.32                            |
| CBMH_18 | JUNCTION | 0.04                       | 0.74                       | 64.79                    | 0 01:55                                  | 0.74                            |
| CBMH_19 | JUNCTION | 0.00                       | 0.23                       | 65.11                    | 0 01:05                                  | 0.23                            |
| CBMH_2  | JUNCTION | 0.00                       | 0.28                       | 64.34                    | 0 01:05                                  | 0.28                            |
| CBMH_21 | JUNCTION | 0.00                       | 0.22                       | 65.39                    | 0 01:05                                  | 0.22                            |
| CBMH_22 | JUNCTION | 0.00                       | 0.17                       | 65.70                    | 0 01:05                                  | 0.17                            |
| CBMH_3  | JUNCTION | 0.00                       | 0.24                       | 64.66                    | 0 01:05                                  | 0.24                            |
| CBMH_4  | JUNCTION | 0.00                       | 0.19                       | 64.97                    | 0 01:05                                  | 0.19                            |
| CBMH_6  | JUNCTION | 0.01                       | 0.34                       | 64.25                    | 0 02:09                                  | 0.33                            |
| CBMH_7  | JUNCTION | 0.00                       | 0.29                       | 64.57                    | 0 01:05                                  | 0.29                            |
| CBMH_8  | JUNCTION | 0.00                       | 0.24                       | 64.88                    | 0 01:05                                  | 0.24                            |
| CBMH_9  | JUNCTION | 0.00                       | 0.19                       | 65.18                    | 0 01:05                                  | 0.19                            |
| DCB_16  | JUNCTION | 0.00                       | 0.22                       | 65.02                    | 0 01:05                                  | 0.22                            |
| J1      | JUNCTION | 0.01                       | 0.08                       | 63.83                    | 0 01:55                                  | 0.08                            |

|           |          |      |      |       |   |       |      |
|-----------|----------|------|------|-------|---|-------|------|
| J13       | JUNCTION | 0.04 | 0.77 | 64.31 | 0 | 02:14 | 0.75 |
| J2        | JUNCTION | 0.01 | 0.08 | 63.32 | 0 | 02:10 | 0.08 |
| MH_20     | JUNCTION | 0.00 | 0.22 | 65.21 | 0 | 01:05 | 0.22 |
| MH_24     | JUNCTION | 0.03 | 0.65 | 64.79 | 0 | 01:55 | 0.65 |
| MH_25     | JUNCTION | 0.01 | 0.47 | 64.88 | 0 | 01:05 | 0.46 |
| MH_26     | JUNCTION | 0.01 | 0.55 | 65.10 | 0 | 01:05 | 0.55 |
| MH_27     | JUNCTION | 0.01 | 0.36 | 64.25 | 0 | 02:10 | 0.36 |
| MH_30     | JUNCTION | 0.02 | 0.52 | 64.25 | 0 | 02:11 | 0.52 |
| MH_44     | JUNCTION | 0.01 | 0.19 | 63.70 | 0 | 01:55 | 0.19 |
| MH_45     | JUNCTION | 0.01 | 0.16 | 63.27 | 0 | 02:10 | 0.16 |
| OGS_1     | JUNCTION | 0.01 | 0.07 | 63.11 | 0 | 02:10 | 0.07 |
| OGS_2     | JUNCTION | 0.01 | 0.16 | 63.63 | 0 | 01:55 | 0.16 |
| Humber_P1 | OUTFALL  | 0.00 | 0.00 | 62.48 | 0 | 00:00 | 0.00 |
| OF1       | OUTFALL  | 0.01 | 0.16 | 63.57 | 0 | 01:55 | 0.16 |
| OF2       | OUTFALL  | 0.00 | 0.00 | 0.00  | 0 | 00:00 | 0.00 |
| SU_N      | STORAGE  | 0.07 | 1.04 | 64.79 | 0 | 01:55 | 1.04 |
| SU_S      | STORAGE  | 0.09 | 1.01 | 64.25 | 0 | 02:10 | 1.01 |

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Node Inflow Summary  
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| Node      | Type     | Maximum Lateral Inflow<br>CMS | Maximum Total Inflow<br>CMS | Time of Max Occurrence<br>days hr:min | Lateral Inflow Volume<br>10^6 ltr | Total Inflow Volume<br>10^6 ltr | Flow Balance Error<br>Percent |
|-----------|----------|-------------------------------|-----------------------------|---------------------------------------|-----------------------------------|---------------------------------|-------------------------------|
| CB_10     | JUNCTION | 0.047                         | 0.047                       | 0 01:05                               | 0.0521                            | 0.0521                          | -0.013                        |
| CB_23     | JUNCTION | 0.029                         | 0.029                       | 0 01:05                               | 0.0321                            | 0.0321                          | -0.008                        |
| CB_27     | JUNCTION | 0.054                         | 0.054                       | 0 01:05                               | 0.0602                            | 0.0602                          | -0.005                        |
| CB_28     | JUNCTION | 0.054                         | 0.054                       | 0 01:05                               | 0.0602                            | 0.0602                          | -0.005                        |
| CB_29     | JUNCTION | 0.058                         | 0.058                       | 0 01:05                               | 0.0642                            | 0.0642                          | 0.550                         |
| CB_5      | JUNCTION | 0.054                         | 0.054                       | 0 01:05                               | 0.0602                            | 0.0602                          | -0.014                        |
| CBMH_11   | JUNCTION | 0.389                         | 0.556                       | 0 01:05                               | 0.551                             | 0.743                           | -0.003                        |
| CBMH_12   | JUNCTION | 0.115                         | 0.115                       | 0 01:05                               | 0.128                             | 0.128                           | 0.786                         |
| CBMH_14   | JUNCTION | 0.090                         | 0.271                       | 0 01:05                               | 0.1                               | 0.307                           | -0.410                        |
| CBMH_15   | JUNCTION | 0.058                         | 0.185                       | 0 01:05                               | 0.0642                            | 0.208                           | 0.631                         |
| CBMH_18   | JUNCTION | 0.101                         | 0.700                       | 0 01:05                               | 0.112                             | 0.943                           | -0.006                        |
| CBMH_19   | JUNCTION | 0.014                         | 0.126                       | 0 01:05                               | 0.016                             | 0.144                           | 0.268                         |
| CBMH_2    | JUNCTION | 0.061                         | 0.230                       | 0 01:05                               | 0.0682                            | 0.266                           | 0.330                         |
| CBMH_21   | JUNCTION | 0.043                         | 0.113                       | 0 01:05                               | 0.0481                            | 0.128                           | -0.003                        |
| CBMH_22   | JUNCTION | 0.043                         | 0.071                       | 0 01:05                               | 0.0481                            | 0.0802                          | -0.011                        |
| CBMH_3    | JUNCTION | 0.061                         | 0.172                       | 0 01:05                               | 0.0682                            | 0.197                           | 0.230                         |
| CBMH_4    | JUNCTION | 0.061                         | 0.114                       | 0 01:05                               | 0.0682                            | 0.128                           | -0.012                        |
| CBMH_6    | JUNCTION | 0.032                         | 0.244                       | 0 01:05                               | 0.0361                            | 0.284                           | -0.010                        |
| CBMH_7    | JUNCTION | 0.061                         | 0.216                       | 0 01:05                               | 0.0682                            | 0.249                           | 0.346                         |
| CBMH_8    | JUNCTION | 0.058                         | 0.158                       | 0 01:05                               | 0.0642                            | 0.181                           | -0.010                        |
| CBMH_9    | JUNCTION | 0.058                         | 0.103                       | 0 01:05                               | 0.0642                            | 0.116                           | -0.011                        |
| DCB_16    | JUNCTION | 0.129                         | 0.129                       | 0 01:05                               | 0.144                             | 0.144                           | 0.380                         |
| J1        | JUNCTION | 0.000                         | 0.012                       | 0 01:55                               | 0                                 | 0.911                           | -0.005                        |
| J13       | JUNCTION | 0.101                         | 0.565                       | 0 01:05                               | 0.112                             | 0.791                           | -0.108                        |
| J2        | JUNCTION | 0.000                         | 0.012                       | 0 02:10                               | 0                                 | 1.11                            | -0.004                        |
| MH_20     | JUNCTION | 0.000                         | 0.112                       | 0 01:05                               | 0                                 | 0.128                           | -0.001                        |
| MH_24     | JUNCTION | 0.000                         | 0.610                       | 0 01:05                               | 0                                 | 0.828                           | -0.376                        |
| MH_25     | JUNCTION | 0.000                         | 0.490                       | 0 01:05                               | 0                                 | 0.686                           | 0.292                         |
| MH_26     | JUNCTION | 0.380                         | 0.487                       | 0 01:05                               | 0.566                             | 0.686                           | 0.091                         |
| MH_27     | JUNCTION | 0.000                         | 0.058                       | 0 01:05                               | 0                                 | 0.0639                          | -0.391                        |
| MH_30     | JUNCTION | 0.000                         | 0.229                       | 0 01:05                               | 0                                 | 0.29                            | -0.451                        |
| MH_44     | JUNCTION | 0.000                         | 0.064                       | 0 01:55                               | 0                                 | 1.25                            | 0.010                         |
| MH_45     | JUNCTION | 0.000                         | 0.054                       | 0 02:10                               | 0                                 | 1.41                            | 0.000                         |
| OGS_1     | JUNCTION | 0.000                         | 0.054                       | 0 02:10                               | 0                                 | 1.41                            | -0.000                        |
| OGS_2     | JUNCTION | 0.000                         | 0.065                       | 0 01:55                               | 0                                 | 1.25                            | -0.007                        |
| Humber_P1 | OUTFALL  | 0.004                         | 0.055                       | 0 02:10                               | 0.0111                            | 1.42                            | 0.000                         |
| OF1       | OUTFALL  | 0.047                         | 0.067                       | 0 01:54                               | 0.064                             | 1.32                            | 0.000                         |
| OF2       | OUTFALL  | 0.063                         | 0.063                       | 0 01:05                               | 0.0997                            | 0.0997                          | 0.000                         |
| SU_N      | STORAGE  | 0.000                         | 0.968                       | 0 01:05                               | 0                                 | 1.25                            | -0.110                        |
| SU_S      | STORAGE  | 0.000                         | 1.119                       | 0 01:05                               | 0                                 | 1.51                            | -0.111                        |

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Node Surcharge Summary  
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Surcharging occurs when water rises above the top of the highest conduit.

| Node    | Type     | Hours Surcharged | Max. Height Above Crown<br>Meters | Min. Depth Below Rim<br>Meters |
|---------|----------|------------------|-----------------------------------|--------------------------------|
| CBMH_11 | JUNCTION | 1.32             | 0.024                             | 1.493                          |
| CBMH_14 | JUNCTION | 1.85             | 0.080                             | 1.534                          |
| J13     | JUNCTION | 0.01             | 0.023                             | 2.330                          |

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Node Flooding Summary  
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No nodes were flooded.

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Storage Volume Summary

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| Storage Unit | Average Volume<br>1000 m3 | Avg Pcnt Full | Evap Pcnt Loss | Exfil Pcnt Loss | Maximum Volume<br>1000 m3 | Max Pcnt Full | Time of Max Occurrence<br>days hr:min | Maximum Outflow<br>CMS |
|--------------|---------------------------|---------------|----------------|-----------------|---------------------------|---------------|---------------------------------------|------------------------|
| SU_N         | 0.054                     | 2             | 0              | 0               | 0.896                     | 35            | 0 01:55                               | 0.064                  |
| SU_S         | 0.080                     | 2             | 0              | 0               | 1.082                     | 31            | 0 02:10                               | 0.136                  |

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 Outfall Loading Summary  
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| Outfall Node | Flow Freq<br>Pcnt | Avg Flow<br>CMS | Max Flow<br>CMS | Total Volume<br>10^6 ltr |
|--------------|-------------------|-----------------|-----------------|--------------------------|
| Humber_Pl    | 27.80             | 0.007           | 0.055           | 1.417                    |
| OF1          | 22.80             | 0.008           | 0.067           | 1.317                    |
| OF2          | 3.48              | 0.005           | 0.063           | 0.100                    |
| System       | 18.03             | 0.020           | 0.129           | 2.834                    |

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 Link Flow Summary  
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| Link | Type    | Maximum  Flow <br>CMS | Time of Max Occurrence<br>days hr:min | Maximum  Veloc <br>m/sec | Max/ Full<br>Flow | Max/ Full<br>Depth |
|------|---------|-----------------------|---------------------------------------|--------------------------|-------------------|--------------------|
| C1   | CONDUIT | 0.052                 | 0 01:55                               | 1.72                     | 1.09              | 0.93               |
| C10  | CONDUIT | 0.054                 | 0 01:05                               | 1.55                     | 0.16              | 0.27               |
| C11  | CONDUIT | 0.054                 | 0 01:05                               | 1.55                     | 0.16              | 0.27               |
| C12  | CONDUIT | 0.490                 | 0 01:05                               | 2.32                     | 1.37              | 0.94               |
| C13  | CONDUIT | 0.611                 | 0 01:05                               | 2.38                     | 1.19              | 1.00               |
| C14  | CONDUIT | 0.028                 | 0 01:05                               | 1.32                     | 0.14              | 0.25               |
| C15  | CONDUIT | 0.070                 | 0 01:05                               | 1.31                     | 0.29              | 0.37               |
| C16  | CONDUIT | 0.112                 | 0 01:05                               | 1.48                     | 0.47              | 0.48               |
| C17  | CONDUIT | 0.112                 | 0 01:05                               | 1.48                     | 0.47              | 0.48               |
| C18  | CONDUIT | 0.125                 | 0 01:05                               | 1.52                     | 0.53              | 0.52               |
| C19  | CONDUIT | 0.046                 | 0 01:05                               | 1.16                     | 0.19              | 0.30               |
| C2   | CONDUIT | 0.065                 | 0 01:55                               | 1.31                     | 0.52              | 0.46               |
| C20  | CONDUIT | 0.102                 | 0 01:05                               | 1.43                     | 0.28              | 0.36               |
| C21  | CONDUIT | 0.157                 | 0 01:05                               | 1.61                     | 0.44              | 0.46               |
| C22  | CONDUIT | 0.214                 | 0 01:05                               | 1.74                     | 0.60              | 0.56               |
| C23  | CONDUIT | 0.244                 | 0 01:05                               | 1.79                     | 0.68              | 0.82               |
| C24  | CONDUIT | 0.565                 | 0 01:05                               | 2.21                     | 0.61              | 0.99               |
| C25  | CONDUIT | 0.053                 | 0 01:05                               | 1.19                     | 0.15              | 0.26               |
| C26  | CONDUIT | 0.112                 | 0 01:05                               | 1.46                     | 0.22              | 0.32               |
| C27  | CONDUIT | 0.171                 | 0 01:05                               | 1.64                     | 0.33              | 0.40               |
| C28  | CONDUIT | 0.229                 | 0 01:05                               | 1.76                     | 0.45              | 0.54               |
| C29  | CONDUIT | 0.114                 | 0 01:05                               | 1.30                     | 0.73              | 0.82               |
| C3   | CONDUIT | 0.012                 | 0 01:55                               | 0.82                     | 0.16              | 0.27               |
| C30  | CONDUIT | 0.229                 | 0 01:05                               | 1.74                     | 0.45              | 0.93               |
| C31  | CONDUIT | 0.064                 | 0 01:05                               | 1.08                     | 0.43              | 0.98               |
| C32  | CONDUIT | 0.555                 | 0 01:05                               | 2.60                     | 1.54              | 1.00               |
| C33  | CONDUIT | 0.054                 | 0 02:10                               | 4.04                     | 0.07              | 0.18               |
| C34  | CONDUIT | 0.064                 | 0 01:55                               | 1.43                     | 0.38              | 0.42               |
| C35  | CONDUIT | 0.485                 | 0 01:05                               | 2.10                     | 0.95              | 0.80               |
| C36  | CONDUIT | 0.700                 | 0 01:05                               | 2.34                     | 0.74              | 0.99               |
| C37  | CONDUIT | 0.058                 | 0 01:05                               | 1.21                     | 0.39              | 0.58               |
| C4   | CONDUIT | 0.042                 | 0 02:10                               | 1.70                     | 0.88              | 0.73               |
| C5   | CONDUIT | 0.012                 | 0 02:10                               | 0.82                     | 0.15              | 0.27               |
| C6   | CONDUIT | 0.054                 | 0 02:10                               | 1.21                     | 0.38              | 0.42               |
| C7   | CONDUIT | 0.128                 | 0 01:05                               | 1.53                     | 0.36              | 0.41               |
| C8   | CONDUIT | 0.183                 | 0 01:05                               | 1.68                     | 0.51              | 0.81               |
| C9   | CONDUIT | 0.271                 | 0 01:05                               | 1.84                     | 0.53              | 1.00               |
| OR1  | ORIFICE | 0.012                 | 0 02:10                               |                          |                   | 1.00               |
| OR2  | ORIFICE | 0.012                 | 0 01:55                               |                          |                   | 1.00               |

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 Flow Classification Summary  
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| Conduit | Adjusted /Actual Length | Fraction of Time in Flow Class |        |          |          |          |         |           |          |            |
|---------|-------------------------|--------------------------------|--------|----------|----------|----------|---------|-----------|----------|------------|
|         |                         | Dry                            | Up Dry | Down Dry | Sub Crit | Sup Crit | Up Crit | Down Crit | Norm Ltd | Inlet Ctrl |
| C1      | 1.00                    | 0.98                           | 0.00   | 0.00     | 0.00     | 0.00     | 0.00    | 0.02      | 0.00     | 0.00       |
| C10     | 1.00                    | 0.00                           | 0.00   | 0.00     | 0.00     | 0.00     | 0.00    | 1.00      | 0.00     | 0.00       |
| C11     | 1.00                    | 0.00                           | 0.00   | 0.00     | 0.00     | 0.00     | 0.00    | 1.00      | 0.00     | 0.00       |
| C12     | 1.00                    | 0.00                           | 0.00   | 0.00     | 0.04     | 0.00     | 0.00    | 0.96      | 0.01     | 0.00       |
| C13     | 1.00                    | 0.00                           | 0.00   | 0.00     | 0.09     | 0.00     | 0.00    | 0.91      | 0.00     | 0.00       |
| C14     | 1.00                    | 0.00                           | 0.00   | 0.00     | 0.00     | 0.00     | 0.00    | 1.00      | 0.00     | 0.00       |
| C15     | 1.00                    | 0.00                           | 0.00   | 0.00     | 0.00     | 0.00     | 0.00    | 1.00      | 0.00     | 0.00       |
| C16     | 1.00                    | 0.00                           | 0.00   | 0.00     | 0.00     | 0.00     | 0.00    | 1.00      | 0.00     | 0.00       |
| C17     | 1.00                    | 0.00                           | 0.00   | 0.00     | 0.00     | 0.00     | 0.00    | 1.00      | 0.00     | 0.00       |



|     |      |      |      |      |      |      |      |      |      |      |
|-----|------|------|------|------|------|------|------|------|------|------|
| C18 | 1.00 | 0.00 | 0.00 | 0.00 | 0.02 | 0.00 | 0.00 | 0.98 | 0.01 | 0.00 |
| C19 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C2  | 1.00 | 0.00 | 0.10 | 0.00 | 0.76 | 0.14 | 0.00 | 0.00 | 0.78 | 0.00 |
| C20 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C21 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C22 | 1.00 | 0.00 | 0.00 | 0.00 | 0.04 | 0.00 | 0.00 | 0.96 | 0.04 | 0.00 |
| C23 | 1.00 | 0.00 | 0.00 | 0.00 | 0.08 | 0.00 | 0.00 | 0.92 | 0.03 | 0.00 |
| C24 | 1.00 | 0.00 | 0.00 | 0.00 | 0.12 | 0.00 | 0.00 | 0.88 | 0.01 | 0.00 |
| C25 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C26 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C27 | 1.00 | 0.00 | 0.00 | 0.00 | 0.02 | 0.00 | 0.00 | 0.98 | 0.01 | 0.00 |
| C28 | 1.00 | 0.00 | 0.00 | 0.00 | 0.07 | 0.00 | 0.00 | 0.93 | 0.04 | 0.00 |
| C29 | 1.00 | 0.00 | 0.00 | 0.00 | 0.08 | 0.00 | 0.00 | 0.92 | 0.05 | 0.00 |
| C3  | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C30 | 1.00 | 0.00 | 0.00 | 0.00 | 0.09 | 0.00 | 0.00 | 0.91 | 0.01 | 0.00 |
| C31 | 1.00 | 0.00 | 0.00 | 0.00 | 0.06 | 0.00 | 0.00 | 0.94 | 0.02 | 0.00 |
| C32 | 1.00 | 0.00 | 0.00 | 0.00 | 0.12 | 0.00 | 0.00 | 0.88 | 0.01 | 0.00 |
| C33 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C34 | 1.00 | 0.00 | 0.00 | 0.00 | 0.75 | 0.25 | 0.00 | 0.00 | 0.04 | 0.00 |
| C35 | 1.00 | 0.00 | 0.00 | 0.00 | 0.07 | 0.00 | 0.00 | 0.93 | 0.03 | 0.00 |
| C36 | 1.00 | 0.00 | 0.00 | 0.00 | 0.10 | 0.00 | 0.00 | 0.90 | 0.00 | 0.00 |
| C37 | 1.00 | 0.00 | 0.00 | 0.00 | 0.05 | 0.00 | 0.00 | 0.95 | 0.03 | 0.00 |
| C4  | 1.00 | 0.98 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.02 | 0.00 | 0.00 |
| C5  | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.01 | 0.00 | 0.99 | 0.00 | 0.00 |
| C6  | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C7  | 1.00 | 0.00 | 0.00 | 0.00 | 0.03 | 0.00 | 0.00 | 0.97 | 0.03 | 0.00 |
| C8  | 1.00 | 0.00 | 0.00 | 0.00 | 0.08 | 0.00 | 0.00 | 0.92 | 0.04 | 0.00 |
| C9  | 1.00 | 0.00 | 0.00 | 0.00 | 0.09 | 0.00 | 0.00 | 0.90 | 0.01 | 0.00 |

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 Conduit Surcharge Summary  
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| Conduit | Hours Full |          |          | Hours                  |                        |
|---------|------------|----------|----------|------------------------|------------------------|
|         | Both Ends  | Upstream | Dnstream | Above Full Normal Flow | Hours Capacity Limited |
| C1      | 0.01       | 0.01     | 0.01     | 0.73                   | 0.01                   |
| C12     | 0.01       | 0.01     | 0.01     | 0.10                   | 0.01                   |
| C13     | 1.44       | 1.44     | 1.80     | 0.05                   | 0.01                   |
| C23     | 0.01       | 0.01     | 0.01     | 0.01                   | 0.01                   |
| C24     | 0.01       | 0.01     | 0.01     | 0.01                   | 0.01                   |
| C29     | 0.01       | 0.01     | 2.84     | 0.01                   | 0.01                   |
| C30     | 0.01       | 0.01     | 0.01     | 0.01                   | 0.01                   |
| C31     | 0.01       | 0.01     | 1.32     | 0.01                   | 0.01                   |
| C32     | 4.08       | 4.11     | 6.43     | 0.14                   | 0.01                   |
| C36     | 0.01       | 0.01     | 0.44     | 0.01                   | 0.01                   |
| C8      | 0.01       | 0.01     | 2.04     | 0.01                   | 0.01                   |
| C9      | 1.85       | 1.85     | 3.14     | 0.01                   | 0.01                   |

Analysis begun on: Wed Oct 5 21:15:03 2022  
 Analysis ended on: Wed Oct 5 21:15:33 2022  
 Total elapsed time: 00:00:30

5-yr, 6-hour

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.015)

WARNING 03: negative offset ignored for Link C2  
WARNING 03: negative offset ignored for Link C32  
WARNING 03: negative offset ignored for Link C34

\*\*\*\*\*  
Element Count

\*\*\*\*\*  
Number of rain gages ..... 7  
Number of subcatchments ... 30  
Number of nodes ..... 40  
Number of links ..... 39  
Number of pollutants ..... 0  
Number of land uses ..... 0

\*\*\*\*\*  
Raingage Summary

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| Name      | Data Source | Data Type | Recording Interval |
|-----------|-------------|-----------|--------------------|
| 25mm      | 25mm        | INTENSITY | 5 min.             |
| 3hr-100yr | 3hr-100yr   | INTENSITY | 10 min.            |
| 3hr-2yr   | 3hr-2yr     | INTENSITY | 5 min.             |
| 3hr-5yr   | 3hr-5yr     | INTENSITY | 5 min.             |
| 6hr-100yr | 6hr-100yr   | INTENSITY | 10 min.            |
| 6hr-2yr   | 6hr-2yr     | INTENSITY | 5 min.             |
| 6hr-5yr   | 6hr-5yr     | INTENSITY | 5 min.             |

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Subcatchment Summary

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| Name      | Area | Width  | %Imperv | %Slope | Rain Gage | Outlet    |
|-----------|------|--------|---------|--------|-----------|-----------|
| Area_1    | 0.25 | 83.33  | 90.00   | 1.0000 | 6hr-5yr   | CBMH_14   |
| Area_10   | 0.08 | 26.67  | 90.00   | 1.0000 | 6hr-5yr   | CB_23     |
| Area_101  | 1.37 | 137.00 | 95.00   | 0.5000 | 6hr-5yr   | MH_26     |
| Area_102  | 1.13 | 113.00 | 95.00   | 0.5000 | 6hr-5yr   | CBMH_11   |
| Area_11   | 0.13 | 43.33  | 90.00   | 1.0000 | 6hr-5yr   | CB_10     |
| Area_12   | 0.16 | 53.33  | 90.00   | 1.0000 | 6hr-5yr   | CBMH_9    |
| Area_13   | 0.16 | 53.33  | 90.00   | 1.0000 | 6hr-5yr   | CBMH_8    |
| Area_14   | 0.17 | 56.67  | 90.00   | 1.0000 | 6hr-5yr   | CBMH_7    |
| Area_15   | 0.09 | 30.00  | 90.00   | 1.0000 | 6hr-5yr   | CBMH_6    |
| Area_16   | 0.15 | 50.00  | 90.00   | 1.0000 | 6hr-5yr   | CB_5      |
| Area_17   | 0.17 | 56.67  | 90.00   | 1.0000 | 6hr-5yr   | CBMH_4    |
| Area_18   | 0.17 | 56.67  | 90.00   | 1.0000 | 6hr-5yr   | CBMH_3    |
| Area_19   | 0.17 | 56.67  | 90.00   | 1.0000 | 6hr-5yr   | CBMH_2    |
| Area_2    | 0.16 | 53.33  | 90.00   | 1.0000 | 6hr-5yr   | CBMH_15   |
| Area_20   | 0.28 | 93.33  | 90.00   | 1.0000 | 6hr-5yr   | J13       |
| Area_2001 | 0.07 | 7.00   | 25.00   | 0.5000 | 6hr-5yr   | OF2       |
| Area_2002 | 0.21 | 21.00  | 90.00   | 0.5000 | 6hr-5yr   | OF2       |
| Area_2003 | 0.16 | 16.00  | 90.00   | 1.0000 | 6hr-5yr   | OF1       |
| Area_2004 | 0.02 | 13.33  | 5.00    | 0.5000 | 6hr-5yr   | Humber_P1 |
| Area_2005 | 0.04 | 26.67  | 5.00    | 0.5000 | 6hr-5yr   | Humber_P1 |
| Area_21   | 0.21 | 70.00  | 90.00   | 1.0000 | 6hr-5yr   | CBMH_11   |
| Area_22   | 0.32 | 106.67 | 90.00   | 1.0000 | 6hr-5yr   | CBMH_12   |
| Area_23   | 0.16 | 53.33  | 90.00   | 1.0000 | 6hr-5yr   | CB_29     |
| Area_3    | 0.36 | 120.00 | 90.00   | 1.0000 | 6hr-5yr   | DCB_16    |
| Area_4    | 0.28 | 93.33  | 90.00   | 1.0000 | 6hr-5yr   | CBMH_18   |
| Area_5    | 0.15 | 50.00  | 90.00   | 1.0000 | 6hr-5yr   | CB_27     |
| Area_6    | 0.15 | 50.00  | 90.00   | 1.0000 | 6hr-5yr   | CB_28     |
| Area_7    | 0.04 | 13.33  | 90.00   | 1.0000 | 6hr-5yr   | CBMH_19   |
| Area_8    | 0.12 | 40.00  | 90.00   | 1.0000 | 6hr-5yr   | CBMH_21   |
| Area_9    | 0.12 | 40.00  | 90.00   | 1.0000 | 6hr-5yr   | CBMH_22   |

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Node Summary

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| Name    | Type     | Invert Elev. | Max. Depth | Ponded Area | External Inflow |
|---------|----------|--------------|------------|-------------|-----------------|
| CB_10   | JUNCTION | 65.33        | 1.41       | 10.0        |                 |
| CB_23   | JUNCTION | 66.20        | 0.93       | 10.0        |                 |
| CB_27   | JUNCTION | 65.48        | 1.34       | 10.0        |                 |
| CB_28   | JUNCTION | 65.39        | 1.52       | 10.0        |                 |
| CB_29   | JUNCTION | 64.11        | 2.43       | 0.0         |                 |
| CB_5    | JUNCTION | 65.11        | 1.63       | 10.0        |                 |
| CBMH_11 | JUNCTION | 63.58        | 2.16       | 10.0        |                 |
| CBMH_12 | JUNCTION | 64.06        | 1.68       | 10.0        |                 |
| CBMH_14 | JUNCTION | 64.11        | 2.21       | 10.0        |                 |
| CBMH_15 | JUNCTION | 64.47        | 1.85       | 10.0        |                 |
| CBMH_18 | JUNCTION | 64.05        | 2.54       | 0.0         |                 |
| CBMH_19 | JUNCTION | 64.88        | 2.38       | 10.0        |                 |
| CBMH_2  | JUNCTION | 64.06        | 2.94       | 10.0        |                 |
| CBMH_21 | JUNCTION | 65.17        | 1.87       | 10.0        |                 |
| CBMH_22 | JUNCTION | 65.53        | 1.51       | 10.0        |                 |

|           |          |       |      |      |
|-----------|----------|-------|------|------|
| CBMH_3    | JUNCTION | 64.42 | 2.58 | 10.0 |
| CBMH_4    | JUNCTION | 64.78 | 2.22 | 10.0 |
| CBMH_6    | JUNCTION | 63.91 | 2.73 | 10.0 |
| CBMH_7    | JUNCTION | 64.27 | 2.73 | 10.0 |
| CBMH_8    | JUNCTION | 64.63 | 2.37 | 10.0 |
| CBMH_9    | JUNCTION | 64.99 | 2.01 | 10.0 |
| DCB_16    | JUNCTION | 64.80 | 1.52 | 10.0 |
| J1        | JUNCTION | 63.75 | 3.27 | 0.0  |
| J13       | JUNCTION | 63.54 | 3.10 | 10.0 |
| J2        | JUNCTION | 63.24 | 3.33 | 0.0  |
| MH_20     | JUNCTION | 64.99 | 2.30 | 0.0  |
| MH_24     | JUNCTION | 64.13 | 2.50 | 10.0 |
| MH_25     | JUNCTION | 64.42 | 2.63 | 0.0  |
| MH_26     | JUNCTION | 64.56 | 2.70 | 0.0  |
| MH_27     | JUNCTION | 63.89 | 2.02 | 0.0  |
| MH_30     | JUNCTION | 63.73 | 3.08 | 0.0  |
| MH_44     | JUNCTION | 63.51 | 3.51 | 0.0  |
| MH_45     | JUNCTION | 63.11 | 3.46 | 0.0  |
| OGS_1     | JUNCTION | 63.04 | 3.34 | 0.0  |
| OGS_2     | JUNCTION | 63.47 | 3.01 | 0.0  |
| Humber_P1 | OUTFALL  | 62.48 | 0.38 | 0.0  |
| OF1       | OUTFALL  | 63.41 | 0.38 | 0.0  |
| OF2       | OUTFALL  | 0.00  | 0.00 | 0.0  |
| SU_N      | STORAGE  | 63.75 | 3.04 | 0.0  |
| SU_S      | STORAGE  | 63.24 | 3.33 | 0.0  |

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Link Summary  
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| Name | From Node | To Node   | Type    | Length | %Slope  | Roughness |
|------|-----------|-----------|---------|--------|---------|-----------|
| C1   | SU_N      | MH_44     | CONDUIT | 2.5    | 1.0001  | 0.0090    |
| C10  | CB_28     | MH_26     | CONDUIT | 30.4   | 1.0001  | 0.0110    |
| C11  | CB_27     | MH_26     | CONDUIT | 32.8   | 1.0001  | 0.0110    |
| C12  | MH_26     | MH_25     | CONDUIT | 16.5   | 0.4970  | 0.0110    |
| C13  | MH_24     | CBMH_18   | CONDUIT | 4.8    | 0.5000  | 0.0110    |
| C14  | CB_23     | CBMH_22   | CONDUIT | 51.5   | 1.0001  | 0.0110    |
| C15  | CBMH_22   | CBMH_21   | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C16  | CBMH_21   | MH_20     | CONDUIT | 24.5   | 0.5020  | 0.0110    |
| C17  | MH_20     | CBMH_19   | CONDUIT | 10.4   | 0.5000  | 0.0110    |
| C18  | CBMH_19   | MH_24     | CONDUIT | 46.5   | 0.5011  | 0.0110    |
| C19  | CB_10     | CBMH_9    | CONDUIT | 52.5   | 0.4991  | 0.0110    |
| C2   | MH_44     | OGS_2     | CONDUIT | 11.6   | 0.3707  | 0.0110    |
| C20  | CBMH_9    | CBMH_8    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C21  | CBMH_8    | CBMH_7    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C22  | CBMH_7    | CBMH_6    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C23  | CBMH_6    | J13       | CONDUIT | 29.9   | 0.5017  | 0.0110    |
| C24  | J13       | SU_S      | CONDUIT | 4.0    | 0.5000  | 0.0110    |
| C25  | CB_5      | CBMH_4    | CONDUIT | 52.5   | 0.4991  | 0.0110    |
| C26  | CBMH_4    | CBMH_3    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C27  | CBMH_3    | CBMH_2    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C28  | CBMH_2    | MH_30     | CONDUIT | 53.4   | 0.4963  | 0.0110    |
| C29  | CBMH_12   | CBMH_11   | CONDUIT | 50.0   | 0.5700  | 0.0110    |
| C3   | J1        | MH_44     | CONDUIT | 2.5    | 0.4800  | 0.0110    |
| C30  | MH_30     | J13       | CONDUIT | 9.3    | 0.4839  | 0.0110    |
| C31  | MH_27     | CBMH_11   | CONDUIT | 8.2    | 0.5000  | 0.0110    |
| C32  | CBMH_11   | SU_S      | CONDUIT | 13.2   | 0.5000  | 0.0110    |
| C33  | OGS_1     | Humber_P1 | CONDUIT | 4.0    | 14.1135 | 0.0110    |
| C34  | OGS_2     | OF1       | CONDUIT | 8.7    | 0.6782  | 0.0110    |
| C35  | MH_25     | MH_24     | CONDUIT | 44.2   | 0.5000  | 0.0110    |
| C36  | CBMH_18   | SU_N      | CONDUIT | 3.9    | 0.5128  | 0.0110    |
| C37  | CB_29     | MH_27     | CONDUIT | 32.9   | 0.4985  | 0.0110    |
| C4   | SU_S      | MH_45     | CONDUIT | 9.4    | 1.0001  | 0.0090    |
| C5   | J2        | MH_45     | CONDUIT | 9.4    | 0.5000  | 0.0110    |
| C6   | MH_45     | OGS_1     | CONDUIT | 3.1    | 0.4839  | 0.0110    |
| C7   | DCB_16    | CBMH_15   | CONDUIT | 54.4   | 0.5000  | 0.0110    |
| C8   | CBMH_15   | CBMH_14   | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C9   | CBMH_14   | SU_N      | CONDUIT | 15.2   | 0.5000  | 0.0110    |
| OR1  | SU_S      | J2        | ORIFICE |        |         |           |
| OR2  | SU_N      | J1        | ORIFICE |        |         |           |

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Cross Section Summary  
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| Conduit | Shape    | Full Depth | Full Area | Hyd. Rad. | Max. Width | No. of Barrels | Full Flow |
|---------|----------|------------|-----------|-----------|------------|----------------|-----------|
| C1      | CIRCULAR | 0.20       | 0.03      | 0.05      | 0.20       | 1              | 0.05      |
| C10     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.34      |
| C11     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.34      |
| C12     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C13     | CIRCULAR | 0.60       | 0.28      | 0.15      | 0.60       | 1              | 0.51      |
| C14     | CIRCULAR | 0.38       | 0.11      | 0.09      | 0.38       | 1              | 0.21      |
| C15     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C16     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C17     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C18     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C19     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C2      | CIRCULAR | 0.38       | 0.11      | 0.09      | 0.38       | 1              | 0.13      |
| C20     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C21     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C22     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C23     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |

|     |          |      |      |      |      |   |      |
|-----|----------|------|------|------|------|---|------|
| C24 | CIRCULAR | 0.75 | 0.44 | 0.19 | 0.75 | 1 | 0.93 |
| C25 | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C26 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C27 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C28 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C29 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.16 |
| C3  | CIRCULAR | 0.30 | 0.07 | 0.07 | 0.30 | 1 | 0.08 |
| C30 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.50 |
| C31 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.15 |
| C32 | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C33 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.78 |
| C34 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.17 |
| C35 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C36 | CIRCULAR | 0.75 | 0.44 | 0.19 | 0.75 | 1 | 0.94 |
| C37 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.15 |
| C4  | CIRCULAR | 0.20 | 0.03 | 0.05 | 0.20 | 1 | 0.05 |
| C5  | CIRCULAR | 0.30 | 0.07 | 0.07 | 0.30 | 1 | 0.08 |
| C6  | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.14 |
| C7  | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C8  | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C9  | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |

\*\*\*\*\*  
NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
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\*\*\*\*\*  
Analysis Options  
\*\*\*\*\*

Flow Units ..... CMS  
Process Models:  
  Rainfall/Runoff ..... YES  
  RDII ..... NO  
  Snowmelt ..... NO  
  Groundwater ..... NO  
  Flow Routing ..... YES  
  Ponding Allowed ..... NO  
  Water Quality ..... NO  
Infiltration Method ..... HORTON  
Flow Routing Method ..... DYNWAVE  
Surcharge Method ..... EXTRAN  
Starting Date ..... 12/11/2020 00:00:00  
Ending Date ..... 12/21/2020 00:00:00  
Antecedent Dry Days ..... 0.0  
Report Time Step ..... 00:01:00  
Wet Time Step ..... 00:01:00  
Dry Time Step ..... 00:01:00  
Routing Time Step ..... 1.00 sec  
Variable Time Step ..... YES  
Maximum Trials ..... 8  
Number of Threads ..... 6  
Head Tolerance ..... 0.001500 m

| *****                      |           |        |
|----------------------------|-----------|--------|
|                            | Volume    | Depth  |
| Runoff Quantity Continuity | hectare-m | mm     |
| *****                      |           |        |
| Total Precipitation        | 0.346     | 49.044 |
| Evaporation Loss           | 0.000     | 0.000  |
| Infiltration Loss          | 0.018     | 2.482  |
| Surface Runoff             | 0.328     | 46.593 |
| Final Storage              | 0.000     | 0.000  |
| Continuity Error (%)       | -0.065    |        |

| *****                   |           |          |
|-------------------------|-----------|----------|
|                         | Volume    | Volume   |
| Flow Routing Continuity | hectare-m | 10^6 ltr |
| *****                   |           |          |
| Dry Weather Inflow      | 0.000     | 0.000    |
| Wet Weather Inflow      | 0.328     | 3.285    |
| Groundwater Inflow      | 0.000     | 0.000    |
| RDII Inflow             | 0.000     | 0.000    |
| External Inflow         | 0.000     | 0.000    |
| External Outflow        | 0.329     | 3.286    |
| Flooding Loss           | 0.000     | 0.000    |
| Evaporation Loss        | 0.000     | 0.000    |
| Exfiltration Loss       | 0.000     | 0.000    |
| Initial Stored Volume   | 0.000     | 0.000    |
| Final Stored Volume     | 0.000     | 0.000    |
| Continuity Error (%)    | -0.045    |          |

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Time-Step Critical Elements  
\*\*\*\*\*  
Link C33 (2.13%)

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Highest Flow Instability Indexes  
\*\*\*\*\*

Link C2 (5)  
 Link OR1 (1)

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 Routing Time Step Summary  
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Minimum Time Step : 0.43 sec  
 Average Time Step : 0.99 sec  
 Maximum Time Step : 1.00 sec  
 Percent in Steady State : 0.00  
 Average Iterations per Step : 2.00  
 Percent Not Converging : 0.00  
 Time Step Frequencies :  
 1.000 - 0.871 sec : 97.27 %  
 0.871 - 0.758 sec : 0.63 %  
 0.758 - 0.660 sec : 0.72 %  
 0.660 - 0.574 sec : 0.63 %  
 0.574 - 0.500 sec : 0.75 %

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 Subcatchment Runoff Summary  
 \*\*\*\*\*

| Subcatchment | Total Precip<br>mm | Total Runon<br>mm | Total Evap<br>mm | Total Infil<br>mm | Imperv Runoff<br>mm | Perv Runoff<br>mm | Total Runoff<br>mm | Total Runoff<br>10 <sup>6</sup> ltr | Peak Runoff<br>CMS | Runoff Coeff |
|--------------|--------------------|-------------------|------------------|-------------------|---------------------|-------------------|--------------------|-------------------------------------|--------------------|--------------|
| Area_1       | 49.04              | 0.00              | 0.00             | 2.56              | 44.17               | 2.35              | 46.52              | 0.12                                | 0.09               | 0.949        |
| Area_10      | 49.04              | 0.00              | 0.00             | 2.56              | 44.17               | 2.35              | 46.52              | 0.04                                | 0.03               | 0.949        |
| Area_101     | 49.04              | 0.00              | 0.00             | 1.29              | 46.61               | 1.17              | 47.77              | 0.65                                | 0.41               | 0.974        |
| Area_102     | 49.04              | 0.00              | 0.00             | 1.29              | 46.61               | 1.17              | 47.77              | 0.54                                | 0.34               | 0.974        |
| Area_11      | 49.04              | 0.00              | 0.00             | 2.56              | 44.17               | 2.35              | 46.52              | 0.06                                | 0.05               | 0.949        |
| Area_12      | 49.04              | 0.00              | 0.00             | 2.56              | 44.17               | 2.35              | 46.52              | 0.07                                | 0.06               | 0.949        |
| Area_13      | 49.04              | 0.00              | 0.00             | 2.56              | 44.17               | 2.35              | 46.52              | 0.07                                | 0.06               | 0.949        |
| Area_14      | 49.04              | 0.00              | 0.00             | 2.56              | 44.17               | 2.35              | 46.52              | 0.08                                | 0.06               | 0.949        |
| Area_15      | 49.04              | 0.00              | 0.00             | 2.56              | 44.17               | 2.35              | 46.52              | 0.04                                | 0.03               | 0.949        |
| Area_16      | 49.04              | 0.00              | 0.00             | 2.56              | 44.17               | 2.35              | 46.52              | 0.07                                | 0.06               | 0.949        |
| Area_17      | 49.04              | 0.00              | 0.00             | 2.56              | 44.17               | 2.35              | 46.52              | 0.08                                | 0.06               | 0.949        |
| Area_18      | 49.04              | 0.00              | 0.00             | 2.56              | 44.17               | 2.35              | 46.52              | 0.08                                | 0.06               | 0.949        |
| Area_19      | 49.04              | 0.00              | 0.00             | 2.56              | 44.17               | 2.35              | 46.52              | 0.08                                | 0.06               | 0.949        |
| Area_2       | 49.04              | 0.00              | 0.00             | 2.56              | 44.17               | 2.35              | 46.52              | 0.07                                | 0.06               | 0.949        |
| Area_20      | 49.04              | 0.00              | 0.00             | 2.56              | 44.17               | 2.35              | 46.52              | 0.13                                | 0.10               | 0.949        |
| Area_2001    | 49.04              | 0.00              | 0.00             | 20.73             | 12.27               | 16.06             | 28.33              | 0.02                                | 0.01               | 0.578        |
| Area_2002    | 49.04              | 0.00              | 0.00             | 2.60              | 44.16               | 2.31              | 46.46              | 0.10                                | 0.06               | 0.947        |
| Area_2003    | 49.04              | 0.00              | 0.00             | 2.62              | 44.16               | 2.29              | 46.45              | 0.07                                | 0.05               | 0.947        |
| Area_2004    | 49.04              | 0.00              | 0.00             | 24.83             | 2.45                | 21.78             | 24.23              | 0.00                                | 0.00               | 0.494        |
| Area_2005    | 49.04              | 0.00              | 0.00             | 24.83             | 2.45                | 21.78             | 24.23              | 0.01                                | 0.00               | 0.494        |
| Area_21      | 49.04              | 0.00              | 0.00             | 2.56              | 44.17               | 2.35              | 46.52              | 0.10                                | 0.08               | 0.949        |
| Area_22      | 49.04              | 0.00              | 0.00             | 2.56              | 44.17               | 2.35              | 46.52              | 0.15                                | 0.12               | 0.949        |
| Area_23      | 49.04              | 0.00              | 0.00             | 2.56              | 44.17               | 2.35              | 46.52              | 0.07                                | 0.06               | 0.949        |
| Area_3       | 49.04              | 0.00              | 0.00             | 2.56              | 44.17               | 2.35              | 46.52              | 0.17                                | 0.13               | 0.949        |
| Area_4       | 49.04              | 0.00              | 0.00             | 2.56              | 44.17               | 2.35              | 46.52              | 0.13                                | 0.10               | 0.949        |
| Area_5       | 49.04              | 0.00              | 0.00             | 2.56              | 44.17               | 2.35              | 46.52              | 0.07                                | 0.06               | 0.949        |
| Area_6       | 49.04              | 0.00              | 0.00             | 2.56              | 44.17               | 2.35              | 46.52              | 0.07                                | 0.06               | 0.949        |
| Area_7       | 49.04              | 0.00              | 0.00             | 2.56              | 44.17               | 2.35              | 46.52              | 0.02                                | 0.01               | 0.949        |
| Area_8       | 49.04              | 0.00              | 0.00             | 2.56              | 44.17               | 2.35              | 46.52              | 0.06                                | 0.04               | 0.949        |
| Area_9       | 49.04              | 0.00              | 0.00             | 2.56              | 44.17               | 2.35              | 46.52              | 0.06                                | 0.04               | 0.949        |

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 Node Depth Summary  
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| Node    | Type     | Average Depth<br>Meters | Maximum Depth<br>Meters | Maximum HGL<br>Meters | Time of Max Occurrence<br>days hr:min | Reported Max Depth<br>Meters |
|---------|----------|-------------------------|-------------------------|-----------------------|---------------------------------------|------------------------------|
| CB_10   | JUNCTION | 0.00                    | 0.14                    | 65.47                 | 0 02:10                               | 0.14                         |
| CB_23   | JUNCTION | 0.00                    | 0.10                    | 66.29                 | 0 02:10                               | 0.10                         |
| CB_27   | JUNCTION | 0.00                    | 0.12                    | 65.61                 | 0 02:10                               | 0.12                         |
| CB_28   | JUNCTION | 0.00                    | 0.12                    | 65.51                 | 0 02:10                               | 0.12                         |
| CB_29   | JUNCTION | 0.00                    | 0.17                    | 64.28                 | 0 02:10                               | 0.17                         |
| CB_5    | JUNCTION | 0.00                    | 0.14                    | 65.25                 | 0 02:10                               | 0.14                         |
| CBMH_11 | JUNCTION | 0.04                    | 0.70                    | 64.28                 | 0 02:57                               | 0.69                         |
| CBMH_12 | JUNCTION | 0.01                    | 0.25                    | 64.31                 | 0 02:10                               | 0.25                         |
| CBMH_14 | JUNCTION | 0.04                    | 0.71                    | 64.81                 | 0 02:53                               | 0.71                         |
| CBMH_15 | JUNCTION | 0.01                    | 0.35                    | 64.81                 | 0 02:50                               | 0.35                         |
| CBMH_18 | JUNCTION | 0.04                    | 0.76                    | 64.81                 | 0 02:52                               | 0.76                         |
| CBMH_19 | JUNCTION | 0.00                    | 0.24                    | 65.11                 | 0 02:10                               | 0.24                         |
| CBMH_2  | JUNCTION | 0.01                    | 0.29                    | 64.35                 | 0 02:10                               | 0.29                         |
| CBMH_21 | JUNCTION | 0.00                    | 0.22                    | 65.39                 | 0 02:10                               | 0.22                         |
| CBMH_22 | JUNCTION | 0.00                    | 0.17                    | 65.70                 | 0 02:10                               | 0.17                         |
| CBMH_3  | JUNCTION | 0.00                    | 0.24                    | 64.66                 | 0 02:10                               | 0.24                         |
| CBMH_4  | JUNCTION | 0.00                    | 0.19                    | 64.97                 | 0 02:10                               | 0.19                         |
| CBMH_6  | JUNCTION | 0.01                    | 0.36                    | 64.27                 | 0 03:08                               | 0.36                         |
| CBMH_7  | JUNCTION | 0.00                    | 0.30                    | 64.57                 | 0 02:10                               | 0.30                         |
| CBMH_8  | JUNCTION | 0.00                    | 0.25                    | 64.88                 | 0 02:10                               | 0.25                         |
| CBMH_9  | JUNCTION | 0.00                    | 0.20                    | 65.19                 | 0 02:10                               | 0.20                         |
| DCB_16  | JUNCTION | 0.00                    | 0.22                    | 65.02                 | 0 02:10                               | 0.22                         |
| J1      | JUNCTION | 0.01                    | 0.08                    | 63.83                 | 0 02:52                               | 0.08                         |
| J13     | JUNCTION | 0.05                    | 0.78                    | 64.31                 | 0 02:57                               | 0.75                         |

|           |          |      |      |       |   |       |      |
|-----------|----------|------|------|-------|---|-------|------|
| J2        | JUNCTION | 0.01 | 0.08 | 63.32 | 0 | 03:08 | 0.08 |
| MH_20     | JUNCTION | 0.00 | 0.22 | 65.21 | 0 | 02:10 | 0.22 |
| MH_24     | JUNCTION | 0.03 | 0.68 | 64.81 | 0 | 02:52 | 0.68 |
| MH_25     | JUNCTION | 0.01 | 0.49 | 64.90 | 0 | 02:10 | 0.48 |
| MH_26     | JUNCTION | 0.01 | 0.57 | 65.13 | 0 | 02:10 | 0.57 |
| MH_27     | JUNCTION | 0.01 | 0.38 | 64.27 | 0 | 03:04 | 0.38 |
| MH_30     | JUNCTION | 0.03 | 0.54 | 64.28 | 0 | 03:06 | 0.54 |
| MH_44     | JUNCTION | 0.01 | 0.20 | 63.71 | 0 | 02:54 | 0.20 |
| MH_45     | JUNCTION | 0.01 | 0.17 | 63.28 | 0 | 03:02 | 0.17 |
| OGS_1     | JUNCTION | 0.01 | 0.07 | 63.11 | 0 | 03:08 | 0.07 |
| OGS_2     | JUNCTION | 0.01 | 0.17 | 63.64 | 0 | 02:55 | 0.17 |
| Humber_P1 | OUTFALL  | 0.00 | 0.00 | 62.48 | 0 | 00:00 | 0.00 |
| OF1       | OUTFALL  | 0.01 | 0.17 | 63.58 | 0 | 02:53 | 0.17 |
| OF2       | OUTFALL  | 0.00 | 0.00 | 0.00  | 0 | 00:00 | 0.00 |
| SU_N      | STORAGE  | 0.08 | 1.06 | 64.81 | 0 | 02:52 | 1.06 |
| SU_S      | STORAGE  | 0.10 | 1.04 | 64.27 | 0 | 03:08 | 1.04 |

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Node Inflow Summary  
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| Node      | Type     | Maximum Lateral Inflow<br>CMS | Maximum Total Inflow<br>CMS | Time of Max Occurrence<br>days hr:min | Lateral Inflow Volume<br>10^6 ltr | Total Inflow Volume<br>10^6 ltr | Flow Balance Error<br>Percent |
|-----------|----------|-------------------------------|-----------------------------|---------------------------------------|-----------------------------------|---------------------------------|-------------------------------|
| CB_10     | JUNCTION | 0.048                         | 0.048                       | 0 02:10                               | 0.0605                            | 0.0605                          | -0.010                        |
| CB_23     | JUNCTION | 0.030                         | 0.030                       | 0 02:10                               | 0.0372                            | 0.0372                          | -0.006                        |
| CB_27     | JUNCTION | 0.056                         | 0.056                       | 0 02:10                               | 0.0698                            | 0.0698                          | -0.004                        |
| CB_28     | JUNCTION | 0.056                         | 0.056                       | 0 02:10                               | 0.0698                            | 0.0698                          | -0.004                        |
| CB_29     | JUNCTION | 0.059                         | 0.059                       | 0 02:10                               | 0.0744                            | 0.0744                          | 0.570                         |
| CB_5      | JUNCTION | 0.056                         | 0.056                       | 0 02:10                               | 0.0698                            | 0.0698                          | -0.010                        |
| CBMH_11   | JUNCTION | 0.415                         | 0.587                       | 0 02:10                               | 0.637                             | 0.86                            | 0.024                         |
| CBMH_12   | JUNCTION | 0.119                         | 0.119                       | 0 02:10                               | 0.149                             | 0.149                           | 0.588                         |
| CBMH_14   | JUNCTION | 0.093                         | 0.281                       | 0 02:10                               | 0.116                             | 0.355                           | -0.502                        |
| CBMH_15   | JUNCTION | 0.059                         | 0.191                       | 0 02:10                               | 0.0744                            | 0.241                           | 0.899                         |
| CBMH_18   | JUNCTION | 0.104                         | 0.741                       | 0 02:10                               | 0.13                              | 1.09                            | -0.003                        |
| CBMH_19   | JUNCTION | 0.015                         | 0.130                       | 0 02:10                               | 0.0186                            | 0.167                           | 0.246                         |
| CBMH_2    | JUNCTION | 0.063                         | 0.238                       | 0 02:10                               | 0.0791                            | 0.307                           | 0.310                         |
| CBMH_21   | JUNCTION | 0.044                         | 0.117                       | 0 02:10                               | 0.0558                            | 0.149                           | -0.002                        |
| CBMH_22   | JUNCTION | 0.044                         | 0.074                       | 0 02:10                               | 0.0558                            | 0.093                           | -0.008                        |
| CBMH_3    | JUNCTION | 0.063                         | 0.179                       | 0 02:10                               | 0.0791                            | 0.228                           | 0.268                         |
| CBMH_4    | JUNCTION | 0.063                         | 0.118                       | 0 02:10                               | 0.0791                            | 0.149                           | -0.009                        |
| CBMH_6    | JUNCTION | 0.033                         | 0.253                       | 0 02:10                               | 0.0419                            | 0.329                           | -0.031                        |
| CBMH_7    | JUNCTION | 0.063                         | 0.224                       | 0 02:10                               | 0.0791                            | 0.288                           | 0.369                         |
| CBMH_8    | JUNCTION | 0.059                         | 0.164                       | 0 02:10                               | 0.0744                            | 0.209                           | -0.007                        |
| CBMH_9    | JUNCTION | 0.059                         | 0.107                       | 0 02:10                               | 0.0744                            | 0.135                           | -0.008                        |
| DCB_16    | JUNCTION | 0.133                         | 0.133                       | 0 02:10                               | 0.167                             | 0.167                           | 0.399                         |
| J1        | JUNCTION | 0.000                         | 0.013                       | 0 02:52                               | 0                                 | 0.978                           | -0.004                        |
| J13       | JUNCTION | 0.104                         | 0.588                       | 0 02:10                               | 0.13                              | 0.854                           | -0.156                        |
| J2        | JUNCTION | 0.000                         | 0.012                       | 0 03:08                               | 0                                 | 1.18                            | -0.004                        |
| MH_20     | JUNCTION | 0.000                         | 0.116                       | 0 02:10                               | 0                                 | 0.149                           | -0.001                        |
| MH_24     | JUNCTION | 0.000                         | 0.648                       | 0 02:10                               | 0                                 | 0.958                           | -0.364                        |
| MH_25     | JUNCTION | 0.000                         | 0.520                       | 0 02:10                               | 0                                 | 0.793                           | 0.309                         |
| MH_26     | JUNCTION | 0.409                         | 0.520                       | 0 02:10                               | 0.654                             | 0.794                           | 0.091                         |
| MH_27     | JUNCTION | 0.000                         | 0.059                       | 0 02:10                               | 0                                 | 0.074                           | -0.452                        |
| MH_30     | JUNCTION | 0.000                         | 0.237                       | 0 02:10                               | 0                                 | 0.321                           | -0.447                        |
| MH_44     | JUNCTION | 0.000                         | 0.074                       | 0 02:51                               | 0                                 | 1.45                            | 0.009                         |
| MH_45     | JUNCTION | 0.000                         | 0.060                       | 0 03:01                               | 0                                 | 1.63                            | 0.001                         |
| OGS_1     | JUNCTION | 0.000                         | 0.060                       | 0 03:08                               | 0                                 | 1.63                            | -0.000                        |
| OGS_2     | JUNCTION | 0.000                         | 0.076                       | 0 02:50                               | 0                                 | 1.45                            | -0.010                        |
| Humber_P1 | OUTFALL  | 0.005                         | 0.061                       | 0 02:51                               | 0.0145                            | 1.64                            | 0.000                         |
| OF1       | OUTFALL  | 0.050                         | 0.079                       | 0 02:44                               | 0.0743                            | 1.52                            | 0.000                         |
| OF2       | OUTFALL  | 0.068                         | 0.068                       | 0 02:10                               | 0.117                             | 0.117                           | 0.000                         |
| SU_N      | STORAGE  | 0.000                         | 1.017                       | 0 02:10                               | 0                                 | 1.45                            | -0.108                        |
| SU_S      | STORAGE  | 0.000                         | 1.173                       | 0 02:10                               | 0                                 | 1.7                             | -0.102                        |

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Node Surcharge Summary  
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Surcharging occurs when water rises above the top of the highest conduit.

| Node    | Type     | Hours Surcharged | Max. Height Above Crown<br>Meters | Min. Depth Below Rim<br>Meters |
|---------|----------|------------------|-----------------------------------|--------------------------------|
| CBMH_11 | JUNCTION | 1.78             | 0.061                             | 1.456                          |
| CBMH_14 | JUNCTION | 2.17             | 0.107                             | 1.507                          |
| CBMH_18 | JUNCTION | 0.56             | 0.013                             | 1.777                          |
| J13     | JUNCTION | 0.04             | 0.026                             | 2.327                          |

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Node Flooding Summary  
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No nodes were flooded.

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Storage Volume Summary

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| Storage Unit | Average Volume<br>1000 m3 | Avg Pcnt Full | Evap Pcnt Loss | Exfil Pcnt Loss | Maximum Volume<br>1000 m3 | Max Pcnt Full | Time of Max Occurrence<br>days hr:min | Maximum Outflow<br>CMS |
|--------------|---------------------------|---------------|----------------|-----------------|---------------------------|---------------|---------------------------------------|------------------------|
| SU_N         | 0.061                     | 2             | 0              | 0               | 0.925                     | 36            | 0 02:52                               | 0.074                  |
| SU_S         | 0.089                     | 3             | 0              | 0               | 1.115                     | 32            | 0 03:08                               | 0.094                  |

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Outfall Loading Summary  
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| Outfall Node | Flow Freq<br>Pcnt | Avg Flow<br>CMS | Max Flow<br>CMS | Total Volume<br>10^6 ltr |
|--------------|-------------------|-----------------|-----------------|--------------------------|
| Humber_Pl    | 28.97             | 0.008           | 0.061           | 1.644                    |
| OF1          | 23.99             | 0.009           | 0.079           | 1.525                    |
| OF2          | 4.75              | 0.004           | 0.068           | 0.117                    |
| System       | 19.24             | 0.022           | 0.147           | 3.286                    |

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Link Flow Summary  
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| Link | Type    | Maximum  Flow <br>CMS | Time of Max Occurrence<br>days hr:min | Maximum  Veloc <br>m/sec | Max/ Full<br>Flow | Max/ Full<br>Depth |
|------|---------|-----------------------|---------------------------------------|--------------------------|-------------------|--------------------|
| C1   | CONDUIT | 0.061                 | 0 02:44                               | 1.95                     | 1.29              | 1.00               |
| C10  | CONDUIT | 0.055                 | 0 02:10                               | 1.57                     | 0.16              | 0.27               |
| C11  | CONDUIT | 0.055                 | 0 02:10                               | 1.57                     | 0.16              | 0.27               |
| C12  | CONDUIT | 0.520                 | 0 02:10                               | 2.45                     | 1.45              | 0.95               |
| C13  | CONDUIT | 0.648                 | 0 02:10                               | 2.48                     | 1.26              | 1.00               |
| C14  | CONDUIT | 0.029                 | 0 02:10                               | 1.33                     | 0.14              | 0.25               |
| C15  | CONDUIT | 0.073                 | 0 02:10                               | 1.32                     | 0.30              | 0.38               |
| C16  | CONDUIT | 0.116                 | 0 02:10                               | 1.50                     | 0.49              | 0.49               |
| C17  | CONDUIT | 0.116                 | 0 02:10                               | 1.49                     | 0.49              | 0.49               |
| C18  | CONDUIT | 0.130                 | 0 02:10                               | 1.54                     | 0.54              | 0.53               |
| C19  | CONDUIT | 0.047                 | 0 02:10                               | 1.17                     | 0.20              | 0.30               |
| C2   | CONDUIT | 0.076                 | 0 02:50                               | 1.38                     | 0.60              | 0.50               |
| C20  | CONDUIT | 0.105                 | 0 02:10                               | 1.45                     | 0.29              | 0.37               |
| C21  | CONDUIT | 0.162                 | 0 02:10                               | 1.63                     | 0.45              | 0.47               |
| C22  | CONDUIT | 0.222                 | 0 02:10                               | 1.76                     | 0.62              | 0.57               |
| C23  | CONDUIT | 0.254                 | 0 02:10                               | 1.81                     | 0.70              | 0.84               |
| C24  | CONDUIT | 0.588                 | 0 02:10                               | 2.23                     | 0.63              | 1.00               |
| C25  | CONDUIT | 0.055                 | 0 02:10                               | 1.20                     | 0.15              | 0.26               |
| C26  | CONDUIT | 0.116                 | 0 02:10                               | 1.47                     | 0.23              | 0.32               |
| C27  | CONDUIT | 0.177                 | 0 02:10                               | 1.65                     | 0.35              | 0.41               |
| C28  | CONDUIT | 0.237                 | 0 02:10                               | 1.78                     | 0.46              | 0.58               |
| C29  | CONDUIT | 0.116                 | 0 02:10                               | 1.27                     | 0.74              | 0.83               |
| C3   | CONDUIT | 0.013                 | 0 02:52                               | 0.82                     | 0.16              | 0.27               |
| C30  | CONDUIT | 0.238                 | 0 02:10                               | 1.76                     | 0.47              | 0.95               |
| C31  | CONDUIT | 0.067                 | 0 02:10                               | 1.03                     | 0.45              | 1.00               |
| C32  | CONDUIT | 0.586                 | 0 02:10                               | 2.74                     | 1.63              | 1.00               |
| C33  | CONDUIT | 0.060                 | 0 03:08                               | 4.17                     | 0.08              | 0.19               |
| C34  | CONDUIT | 0.074                 | 0 02:53                               | 1.49                     | 0.43              | 0.46               |
| C35  | CONDUIT | 0.518                 | 0 02:10                               | 2.16                     | 1.01              | 0.83               |
| C36  | CONDUIT | 0.741                 | 0 02:10                               | 2.36                     | 0.79              | 1.00               |
| C37  | CONDUIT | 0.059                 | 0 02:10                               | 1.21                     | 0.40              | 0.64               |
| C4   | CONDUIT | 0.048                 | 0 02:58                               | 1.72                     | 1.00              | 0.88               |
| C5   | CONDUIT | 0.012                 | 0 03:07                               | 0.82                     | 0.15              | 0.29               |
| C6   | CONDUIT | 0.060                 | 0 03:08                               | 1.24                     | 0.42              | 0.45               |
| C7   | CONDUIT | 0.132                 | 0 02:10                               | 1.54                     | 0.37              | 0.42               |
| C8   | CONDUIT | 0.189                 | 0 02:10                               | 1.69                     | 0.53              | 0.83               |
| C9   | CONDUIT | 0.278                 | 0 02:10                               | 1.84                     | 0.54              | 1.00               |
| OR1  | ORIFICE | 0.012                 | 0 03:08                               |                          |                   | 1.00               |
| OR2  | ORIFICE | 0.013                 | 0 02:52                               |                          |                   | 1.00               |

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Flow Classification Summary  
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| Conduit | Adjusted /Actual Length | Fraction of Time in Flow Class |        |          |          |          |         |           |          |            |
|---------|-------------------------|--------------------------------|--------|----------|----------|----------|---------|-----------|----------|------------|
|         |                         | Dry                            | Up Dry | Down Dry | Sub Crit | Sup Crit | Up Crit | Down Crit | Norm Ltd | Inlet Ctrl |
| C1      | 1.00                    | 0.97                           | 0.00   | 0.00     | 0.00     | 0.00     | 0.00    | 0.03      | 0.00     | 0.00       |
| C10     | 1.00                    | 0.00                           | 0.00   | 0.00     | 0.00     | 0.00     | 0.00    | 1.00      | 0.00     | 0.00       |
| C11     | 1.00                    | 0.00                           | 0.00   | 0.00     | 0.00     | 0.00     | 0.00    | 1.00      | 0.00     | 0.00       |
| C12     | 1.00                    | 0.00                           | 0.00   | 0.00     | 0.05     | 0.00     | 0.00    | 0.95      | 0.01     | 0.00       |
| C13     | 1.00                    | 0.00                           | 0.00   | 0.00     | 0.09     | 0.00     | 0.00    | 0.91      | 0.00     | 0.00       |
| C14     | 1.00                    | 0.00                           | 0.00   | 0.00     | 0.00     | 0.00     | 0.00    | 1.00      | 0.00     | 0.00       |
| C15     | 1.00                    | 0.00                           | 0.00   | 0.00     | 0.00     | 0.00     | 0.00    | 1.00      | 0.00     | 0.00       |
| C16     | 1.00                    | 0.00                           | 0.00   | 0.00     | 0.00     | 0.00     | 0.00    | 1.00      | 0.00     | 0.00       |
| C17     | 1.00                    | 0.00                           | 0.00   | 0.00     | 0.00     | 0.00     | 0.00    | 1.00      | 0.00     | 0.00       |

|     |      |      |      |      |      |      |      |      |      |      |
|-----|------|------|------|------|------|------|------|------|------|------|
| C18 | 1.00 | 0.00 | 0.00 | 0.00 | 0.02 | 0.00 | 0.00 | 0.98 | 0.01 | 0.00 |
| C19 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C2  | 1.00 | 0.00 | 0.10 | 0.00 | 0.75 | 0.15 | 0.00 | 0.00 | 0.78 | 0.00 |
| C20 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C21 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C22 | 1.00 | 0.00 | 0.00 | 0.00 | 0.05 | 0.00 | 0.00 | 0.95 | 0.04 | 0.00 |
| C23 | 1.00 | 0.00 | 0.00 | 0.00 | 0.08 | 0.00 | 0.00 | 0.92 | 0.03 | 0.00 |
| C24 | 1.00 | 0.00 | 0.00 | 0.00 | 0.12 | 0.00 | 0.00 | 0.87 | 0.01 | 0.00 |
| C25 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C26 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C27 | 1.00 | 0.00 | 0.00 | 0.00 | 0.03 | 0.00 | 0.00 | 0.97 | 0.02 | 0.00 |
| C28 | 1.00 | 0.00 | 0.00 | 0.00 | 0.08 | 0.00 | 0.00 | 0.92 | 0.04 | 0.00 |
| C29 | 1.00 | 0.00 | 0.00 | 0.00 | 0.08 | 0.00 | 0.00 | 0.92 | 0.05 | 0.00 |
| C3  | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C30 | 1.00 | 0.00 | 0.00 | 0.00 | 0.10 | 0.00 | 0.00 | 0.90 | 0.01 | 0.00 |
| C31 | 1.00 | 0.00 | 0.00 | 0.00 | 0.07 | 0.00 | 0.00 | 0.93 | 0.02 | 0.00 |
| C32 | 1.00 | 0.00 | 0.00 | 0.00 | 0.13 | 0.00 | 0.00 | 0.87 | 0.01 | 0.00 |
| C33 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C34 | 1.00 | 0.00 | 0.00 | 0.00 | 0.74 | 0.26 | 0.00 | 0.00 | 0.05 | 0.00 |
| C35 | 1.00 | 0.00 | 0.00 | 0.00 | 0.08 | 0.00 | 0.00 | 0.92 | 0.03 | 0.00 |
| C36 | 1.00 | 0.00 | 0.00 | 0.00 | 0.11 | 0.00 | 0.00 | 0.89 | 0.00 | 0.00 |
| C37 | 1.00 | 0.00 | 0.00 | 0.00 | 0.06 | 0.00 | 0.00 | 0.94 | 0.03 | 0.00 |
| C4  | 1.00 | 0.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.03 | 0.00 | 0.00 |
| C5  | 1.00 | 0.00 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0.99 | 0.00 | 0.00 |
| C6  | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C7  | 1.00 | 0.00 | 0.00 | 0.00 | 0.04 | 0.00 | 0.00 | 0.96 | 0.03 | 0.00 |
| C8  | 1.00 | 0.00 | 0.00 | 0.00 | 0.09 | 0.00 | 0.00 | 0.91 | 0.04 | 0.00 |
| C9  | 1.00 | 0.00 | 0.00 | 0.00 | 0.10 | 0.00 | 0.00 | 0.89 | 0.01 | 0.00 |

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 Conduit Surcharge Summary  
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| Conduit | Hours Full |          |          | Hours                  |                        |
|---------|------------|----------|----------|------------------------|------------------------|
|         | Both Ends  | Upstream | Dnstream | Above Full Normal Flow | Hours Capacity Limited |
| C1      | 0.13       | 0.56     | 0.13     | 1.12                   | 0.13                   |
| C12     | 0.01       | 0.03     | 0.01     | 0.09                   | 0.01                   |
| C13     | 1.67       | 1.67     | 2.09     | 0.06                   | 0.01                   |
| C23     | 0.01       | 0.01     | 0.04     | 0.01                   | 0.01                   |
| C24     | 0.04       | 0.04     | 0.49     | 0.01                   | 0.01                   |
| C29     | 0.01       | 0.01     | 4.24     | 0.01                   | 0.01                   |
| C30     | 0.01       | 0.01     | 0.04     | 0.01                   | 0.01                   |
| C31     | 0.65       | 0.65     | 1.78     | 0.01                   | 0.01                   |
| C32     | 5.48       | 5.53     | 7.81     | 0.11                   | 0.01                   |
| C35     | 0.01       | 0.01     | 0.69     | 0.01                   | 0.01                   |
| C36     | 0.56       | 0.56     | 0.95     | 0.01                   | 0.01                   |
| C4      | 0.01       | 0.01     | 0.01     | 0.45                   | 0.01                   |
| C8      | 0.01       | 0.01     | 2.53     | 0.01                   | 0.01                   |
| C9      | 2.17       | 2.17     | 4.46     | 0.01                   | 0.01                   |

Analysis begun on: Wed Oct 5 21:16:09 2022  
 Analysis ended on: Wed Oct 5 21:16:39 2022  
 Total elapsed time: 00:00:30



100-yr, 3-hour

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.015)

WARNING 03: negative offset ignored for Link C2  
WARNING 03: negative offset ignored for Link C32  
WARNING 03: negative offset ignored for Link C34

\*\*\*\*\*  
Element Count

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Number of rain gages ..... 7  
Number of subcatchments ... 30  
Number of nodes ..... 40  
Number of links ..... 39  
Number of pollutants ..... 0  
Number of land uses ..... 0

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Raingage Summary

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| Name      | Data Source | Data Type | Recording Interval |
|-----------|-------------|-----------|--------------------|
| 25mm      | 25mm        | INTENSITY | 5 min.             |
| 3hr-100yr | 3hr-100yr   | INTENSITY | 10 min.            |
| 3hr-2yr   | 3hr-2yr     | INTENSITY | 5 min.             |
| 3hr-5yr   | 3hr-5yr     | INTENSITY | 5 min.             |
| 6hr-100yr | 6hr-100yr   | INTENSITY | 10 min.            |
| 6hr-2yr   | 6hr-2yr     | INTENSITY | 5 min.             |
| 6hr-5yr   | 6hr-5yr     | INTENSITY | 5 min.             |

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Subcatchment Summary

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| Name      | Area | Width  | %Imperv | %Slope | Rain Gage | Outlet    |
|-----------|------|--------|---------|--------|-----------|-----------|
| Area_1    | 0.25 | 83.33  | 90.00   | 1.0000 | 3hr-100yr | CBMH_14   |
| Area_10   | 0.08 | 26.67  | 90.00   | 1.0000 | 3hr-100yr | CB_23     |
| Area_101  | 1.37 | 137.00 | 95.00   | 0.5000 | 3hr-100yr | MH_26     |
| Area_102  | 1.13 | 113.00 | 95.00   | 0.5000 | 3hr-100yr | CBMH_11   |
| Area_11   | 0.13 | 43.33  | 90.00   | 1.0000 | 3hr-100yr | CB_10     |
| Area_12   | 0.16 | 53.33  | 90.00   | 1.0000 | 3hr-100yr | CBMH_9    |
| Area_13   | 0.16 | 53.33  | 90.00   | 1.0000 | 3hr-100yr | CBMH_8    |
| Area_14   | 0.17 | 56.67  | 90.00   | 1.0000 | 3hr-100yr | CBMH_7    |
| Area_15   | 0.09 | 30.00  | 90.00   | 1.0000 | 3hr-100yr | CBMH_6    |
| Area_16   | 0.15 | 50.00  | 90.00   | 1.0000 | 3hr-100yr | CB_5      |
| Area_17   | 0.17 | 56.67  | 90.00   | 1.0000 | 3hr-100yr | CBMH_4    |
| Area_18   | 0.17 | 56.67  | 90.00   | 1.0000 | 3hr-100yr | CBMH_3    |
| Area_19   | 0.17 | 56.67  | 90.00   | 1.0000 | 3hr-100yr | CBMH_2    |
| Area_2    | 0.16 | 53.33  | 90.00   | 1.0000 | 3hr-100yr | CBMH_15   |
| Area_20   | 0.28 | 93.33  | 90.00   | 1.0000 | 3hr-100yr | J13       |
| Area_2001 | 0.07 | 7.00   | 25.00   | 0.5000 | 3hr-100yr | OF2       |
| Area_2002 | 0.21 | 21.00  | 90.00   | 0.5000 | 3hr-100yr | OF2       |
| Area_2003 | 0.16 | 16.00  | 90.00   | 1.0000 | 3hr-100yr | OF1       |
| Area_2004 | 0.02 | 13.33  | 5.00    | 0.5000 | 3hr-100yr | Humber_P1 |
| Area_2005 | 0.04 | 26.67  | 5.00    | 0.5000 | 3hr-100yr | Humber_P1 |
| Area_21   | 0.21 | 70.00  | 90.00   | 1.0000 | 3hr-100yr | CBMH_11   |
| Area_22   | 0.32 | 106.67 | 90.00   | 1.0000 | 3hr-100yr | CBMH_12   |
| Area_23   | 0.16 | 53.33  | 90.00   | 1.0000 | 3hr-100yr | CB_29     |
| Area_3    | 0.36 | 120.00 | 90.00   | 1.0000 | 3hr-100yr | DCB_16    |
| Area_4    | 0.28 | 93.33  | 90.00   | 1.0000 | 3hr-100yr | CBMH_18   |
| Area_5    | 0.15 | 50.00  | 90.00   | 1.0000 | 3hr-100yr | CB_27     |
| Area_6    | 0.15 | 50.00  | 90.00   | 1.0000 | 3hr-100yr | CB_28     |
| Area_7    | 0.04 | 13.33  | 90.00   | 1.0000 | 3hr-100yr | CBMH_19   |
| Area_8    | 0.12 | 40.00  | 90.00   | 1.0000 | 3hr-100yr | CBMH_21   |
| Area_9    | 0.12 | 40.00  | 90.00   | 1.0000 | 3hr-100yr | CBMH_22   |

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Node Summary

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| Name    | Type     | Invert Elev. | Max. Depth | Ponded Area | External Inflow |
|---------|----------|--------------|------------|-------------|-----------------|
| CB_10   | JUNCTION | 65.33        | 1.41       | 10.0        |                 |
| CB_23   | JUNCTION | 66.20        | 0.93       | 10.0        |                 |
| CB_27   | JUNCTION | 65.48        | 1.34       | 10.0        |                 |
| CB_28   | JUNCTION | 65.39        | 1.52       | 10.0        |                 |
| CB_29   | JUNCTION | 64.11        | 2.43       | 0.0         |                 |
| CB_5    | JUNCTION | 65.11        | 1.63       | 10.0        |                 |
| CBMH_11 | JUNCTION | 63.58        | 2.16       | 10.0        |                 |
| CBMH_12 | JUNCTION | 64.06        | 1.68       | 10.0        |                 |
| CBMH_14 | JUNCTION | 64.11        | 2.21       | 10.0        |                 |
| CBMH_15 | JUNCTION | 64.47        | 1.85       | 10.0        |                 |
| CBMH_18 | JUNCTION | 64.05        | 2.54       | 0.0         |                 |
| CBMH_19 | JUNCTION | 64.88        | 2.38       | 10.0        |                 |
| CBMH_2  | JUNCTION | 64.06        | 2.94       | 10.0        |                 |
| CBMH_21 | JUNCTION | 65.17        | 1.87       | 10.0        |                 |
| CBMH_22 | JUNCTION | 65.53        | 1.51       | 10.0        |                 |

|           |          |       |      |      |
|-----------|----------|-------|------|------|
| CBMH_3    | JUNCTION | 64.42 | 2.58 | 10.0 |
| CBMH_4    | JUNCTION | 64.78 | 2.22 | 10.0 |
| CBMH_6    | JUNCTION | 63.91 | 2.73 | 10.0 |
| CBMH_7    | JUNCTION | 64.27 | 2.73 | 10.0 |
| CBMH_8    | JUNCTION | 64.63 | 2.37 | 10.0 |
| CBMH_9    | JUNCTION | 64.99 | 2.01 | 10.0 |
| DCB_16    | JUNCTION | 64.80 | 1.52 | 10.0 |
| J1        | JUNCTION | 63.75 | 3.27 | 0.0  |
| J13       | JUNCTION | 63.54 | 3.10 | 10.0 |
| J2        | JUNCTION | 63.24 | 3.33 | 0.0  |
| MH_20     | JUNCTION | 64.99 | 2.30 | 0.0  |
| MH_24     | JUNCTION | 64.13 | 2.50 | 10.0 |
| MH_25     | JUNCTION | 64.42 | 2.63 | 0.0  |
| MH_26     | JUNCTION | 64.56 | 2.70 | 0.0  |
| MH_27     | JUNCTION | 63.89 | 2.02 | 0.0  |
| MH_30     | JUNCTION | 63.73 | 3.08 | 0.0  |
| MH_44     | JUNCTION | 63.51 | 3.51 | 0.0  |
| MH_45     | JUNCTION | 63.11 | 3.46 | 0.0  |
| OGS_1     | JUNCTION | 63.04 | 3.34 | 0.0  |
| OGS_2     | JUNCTION | 63.47 | 3.01 | 0.0  |
| Humber_P1 | OUTFALL  | 62.48 | 0.38 | 0.0  |
| OF1       | OUTFALL  | 63.41 | 0.38 | 0.0  |
| OF2       | OUTFALL  | 0.00  | 0.00 | 0.0  |
| SU_N      | STORAGE  | 63.75 | 3.04 | 0.0  |
| SU_S      | STORAGE  | 63.24 | 3.33 | 0.0  |

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Link Summary  
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| Name | From Node | To Node   | Type    | Length | %Slope  | Roughness |
|------|-----------|-----------|---------|--------|---------|-----------|
| C1   | SU_N      | MH_44     | CONDUIT | 2.5    | 1.0001  | 0.0090    |
| C10  | CB_28     | MH_26     | CONDUIT | 30.4   | 1.0001  | 0.0110    |
| C11  | CB_27     | MH_26     | CONDUIT | 32.8   | 1.0001  | 0.0110    |
| C12  | MH_26     | MH_25     | CONDUIT | 16.5   | 0.4970  | 0.0110    |
| C13  | MH_24     | CBMH_18   | CONDUIT | 4.8    | 0.5000  | 0.0110    |
| C14  | CB_23     | CBMH_22   | CONDUIT | 51.5   | 1.0001  | 0.0110    |
| C15  | CBMH_22   | CBMH_21   | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C16  | CBMH_21   | MH_20     | CONDUIT | 24.5   | 0.5020  | 0.0110    |
| C17  | MH_20     | CBMH_19   | CONDUIT | 10.4   | 0.5000  | 0.0110    |
| C18  | CBMH_19   | MH_24     | CONDUIT | 46.5   | 0.5011  | 0.0110    |
| C19  | CB_10     | CBMH_9    | CONDUIT | 52.5   | 0.4991  | 0.0110    |
| C2   | MH_44     | OGS_2     | CONDUIT | 11.6   | 0.3707  | 0.0110    |
| C20  | CBMH_9    | CBMH_8    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C21  | CBMH_8    | CBMH_7    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C22  | CBMH_7    | CBMH_6    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C23  | CBMH_6    | J13       | CONDUIT | 29.9   | 0.5017  | 0.0110    |
| C24  | J13       | SU_S      | CONDUIT | 4.0    | 0.5000  | 0.0110    |
| C25  | CB_5      | CBMH_4    | CONDUIT | 52.5   | 0.4991  | 0.0110    |
| C26  | CBMH_4    | CBMH_3    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C27  | CBMH_3    | CBMH_2    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C28  | CBMH_2    | MH_30     | CONDUIT | 53.4   | 0.4963  | 0.0110    |
| C29  | CBMH_12   | CBMH_11   | CONDUIT | 50.0   | 0.5700  | 0.0110    |
| C3   | J1        | MH_44     | CONDUIT | 2.5    | 0.4800  | 0.0110    |
| C30  | MH_30     | J13       | CONDUIT | 9.3    | 0.4839  | 0.0110    |
| C31  | MH_27     | CBMH_11   | CONDUIT | 8.2    | 0.5000  | 0.0110    |
| C32  | CBMH_11   | SU_S      | CONDUIT | 13.2   | 0.5000  | 0.0110    |
| C33  | OGS_1     | Humber_P1 | CONDUIT | 4.0    | 14.1135 | 0.0110    |
| C34  | OGS_2     | OF1       | CONDUIT | 8.7    | 0.6782  | 0.0110    |
| C35  | MH_25     | MH_24     | CONDUIT | 44.2   | 0.5000  | 0.0110    |
| C36  | CBMH_18   | SU_N      | CONDUIT | 3.9    | 0.5128  | 0.0110    |
| C37  | CB_29     | MH_27     | CONDUIT | 32.9   | 0.4985  | 0.0110    |
| C4   | SU_S      | MH_45     | CONDUIT | 9.4    | 1.0001  | 0.0090    |
| C5   | J2        | MH_45     | CONDUIT | 9.4    | 0.5000  | 0.0110    |
| C6   | MH_45     | OGS_1     | CONDUIT | 3.1    | 0.4839  | 0.0110    |
| C7   | DCB_16    | CBMH_15   | CONDUIT | 54.4   | 0.5000  | 0.0110    |
| C8   | CBMH_15   | CBMH_14   | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C9   | CBMH_14   | SU_N      | CONDUIT | 15.2   | 0.5000  | 0.0110    |
| OR1  | SU_S      | J2        | ORIFICE |        |         |           |
| OR2  | SU_N      | J1        | ORIFICE |        |         |           |

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Cross Section Summary  
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| Conduit | Shape    | Full Depth | Full Area | Hyd. Rad. | Max. Width | No. of Barrels | Full Flow |
|---------|----------|------------|-----------|-----------|------------|----------------|-----------|
| C1      | CIRCULAR | 0.20       | 0.03      | 0.05      | 0.20       | 1              | 0.05      |
| C10     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.34      |
| C11     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.34      |
| C12     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C13     | CIRCULAR | 0.60       | 0.28      | 0.15      | 0.60       | 1              | 0.51      |
| C14     | CIRCULAR | 0.38       | 0.11      | 0.09      | 0.38       | 1              | 0.21      |
| C15     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C16     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C17     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C18     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C19     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C2      | CIRCULAR | 0.38       | 0.11      | 0.09      | 0.38       | 1              | 0.13      |
| C20     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C21     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C22     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C23     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |

|     |          |      |      |      |      |   |      |
|-----|----------|------|------|------|------|---|------|
| C24 | CIRCULAR | 0.75 | 0.44 | 0.19 | 0.75 | 1 | 0.93 |
| C25 | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C26 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C27 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C28 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C29 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.16 |
| C3  | CIRCULAR | 0.30 | 0.07 | 0.07 | 0.30 | 1 | 0.08 |
| C30 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.50 |
| C31 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.15 |
| C32 | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C33 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.78 |
| C34 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.17 |
| C35 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C36 | CIRCULAR | 0.75 | 0.44 | 0.19 | 0.75 | 1 | 0.94 |
| C37 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.15 |
| C4  | CIRCULAR | 0.20 | 0.03 | 0.05 | 0.20 | 1 | 0.05 |
| C5  | CIRCULAR | 0.30 | 0.07 | 0.07 | 0.30 | 1 | 0.08 |
| C6  | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.14 |
| C7  | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C8  | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C9  | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |

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NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
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Analysis Options  
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Flow Units ..... CMS  
Process Models:  
  Rainfall/Runoff ..... YES  
  RDII ..... NO  
  Snowmelt ..... NO  
  Groundwater ..... NO  
  Flow Routing ..... YES  
  Ponding Allowed ..... NO  
  Water Quality ..... NO  
Infiltration Method ..... HORTON  
Flow Routing Method ..... DYNWAVE  
Surcharge Method ..... EXTRAN  
Starting Date ..... 12/11/2020 00:00:00  
Ending Date ..... 12/21/2020 00:00:00  
Antecedent Dry Days ..... 0.0  
Report Time Step ..... 00:01:00  
Wet Time Step ..... 00:01:00  
Dry Time Step ..... 00:01:00  
Routing Time Step ..... 1.00 sec  
Variable Time Step ..... YES  
Maximum Trials ..... 8  
Number of Threads ..... 6  
Head Tolerance ..... 0.001500 m

| *****                      |           |        |
|----------------------------|-----------|--------|
|                            | Volume    | Depth  |
| Runoff Quantity Continuity | hectare-m | mm     |
| *****                      |           |        |
| Total Precipitation        | 0.505     | 71.677 |
| Evaporation Loss           | 0.000     | 0.000  |
| Infiltration Loss          | 0.017     | 2.413  |
| Surface Runoff             | 0.489     | 69.322 |
| Final Storage              | 0.000     | 0.000  |
| Continuity Error (%)       | -0.082    |        |

| *****                   |           |          |
|-------------------------|-----------|----------|
|                         | Volume    | Volume   |
| Flow Routing Continuity | hectare-m | 10^6 ltr |
| *****                   |           |          |
| Dry Weather Inflow      | 0.000     | 0.000    |
| Wet Weather Inflow      | 0.489     | 4.886    |
| Groundwater Inflow      | 0.000     | 0.000    |
| RDII Inflow             | 0.000     | 0.000    |
| External Inflow         | 0.000     | 0.000    |
| External Outflow        | 0.489     | 4.888    |
| Flooding Loss           | 0.000     | 0.000    |
| Evaporation Loss        | 0.000     | 0.000    |
| Exfiltration Loss       | 0.000     | 0.000    |
| Initial Stored Volume   | 0.000     | 0.000    |
| Final Stored Volume     | 0.000     | 0.000    |
| Continuity Error (%)    | -0.037    |          |

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Time-Step Critical Elements  
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Link C33 (3.80%)

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Highest Flow Instability Indexes  
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Link C2 (4)  
 Link OR1 (1)  
 Link OR2 (1)

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 Routing Time Step Summary  
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Minimum Time Step : 0.50 sec  
 Average Time Step : 0.98 sec  
 Maximum Time Step : 1.00 sec  
 Percent in Steady State : 0.00  
 Average Iterations per Step : 2.00  
 Percent Not Converging : 0.01  
 Time Step Frequencies :  
 1.000 - 0.871 sec : 96.49 %  
 0.871 - 0.758 sec : 0.30 %  
 0.758 - 0.660 sec : 0.28 %  
 0.660 - 0.574 sec : 0.66 %  
 0.574 - 0.500 sec : 2.28 %

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 Subcatchment Runoff Summary  
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| Subcatchment | Total Precip<br>mm | Total Runon<br>mm | Total Evap<br>mm | Total Infil<br>mm | Imperv Runoff<br>mm | Perv Runoff<br>mm | Total Runoff<br>mm | Total Runoff<br>10 <sup>6</sup> ltr | Peak Runoff<br>CMS | Runoff<br>Coeff |
|--------------|--------------------|-------------------|------------------|-------------------|---------------------|-------------------|--------------------|-------------------------------------|--------------------|-----------------|
| Area_1       | 71.68              | 0.00              | 0.00             | 2.48              | 64.57               | 4.70              | 69.27              | 0.17                                | 0.12               | 0.966           |
| Area_10      | 71.68              | 0.00              | 0.00             | 2.48              | 64.57               | 4.70              | 69.27              | 0.06                                | 0.04               | 0.966           |
| Area_101     | 71.68              | 0.00              | 0.00             | 1.25              | 68.12               | 2.34              | 70.46              | 0.97                                | 0.65               | 0.983           |
| Area_102     | 71.68              | 0.00              | 0.00             | 1.25              | 68.12               | 2.34              | 70.46              | 0.80                                | 0.53               | 0.983           |
| Area_11      | 71.68              | 0.00              | 0.00             | 2.48              | 64.57               | 4.70              | 69.27              | 0.09                                | 0.06               | 0.966           |
| Area_12      | 71.68              | 0.00              | 0.00             | 2.48              | 64.57               | 4.70              | 69.27              | 0.11                                | 0.08               | 0.966           |
| Area_13      | 71.68              | 0.00              | 0.00             | 2.48              | 64.57               | 4.70              | 69.27              | 0.11                                | 0.08               | 0.966           |
| Area_14      | 71.68              | 0.00              | 0.00             | 2.48              | 64.57               | 4.70              | 69.27              | 0.12                                | 0.08               | 0.966           |
| Area_15      | 71.68              | 0.00              | 0.00             | 2.48              | 64.57               | 4.70              | 69.27              | 0.06                                | 0.04               | 0.966           |
| Area_16      | 71.68              | 0.00              | 0.00             | 2.48              | 64.57               | 4.70              | 69.27              | 0.10                                | 0.07               | 0.966           |
| Area_17      | 71.68              | 0.00              | 0.00             | 2.48              | 64.57               | 4.70              | 69.27              | 0.12                                | 0.08               | 0.966           |
| Area_18      | 71.68              | 0.00              | 0.00             | 2.48              | 64.57               | 4.70              | 69.27              | 0.12                                | 0.08               | 0.966           |
| Area_19      | 71.68              | 0.00              | 0.00             | 2.48              | 64.57               | 4.70              | 69.27              | 0.12                                | 0.08               | 0.966           |
| Area_2       | 71.68              | 0.00              | 0.00             | 2.48              | 64.57               | 4.70              | 69.27              | 0.11                                | 0.08               | 0.966           |
| Area_20      | 71.68              | 0.00              | 0.00             | 2.48              | 64.57               | 4.70              | 69.27              | 0.19                                | 0.14               | 0.966           |
| Area_2001    | 71.68              | 0.00              | 0.00             | 20.52             | 17.93               | 33.25             | 51.18              | 0.04                                | 0.01               | 0.714           |
| Area_2002    | 71.68              | 0.00              | 0.00             | 2.53              | 64.54               | 4.64              | 69.18              | 0.15                                | 0.10               | 0.965           |
| Area_2003    | 71.68              | 0.00              | 0.00             | 2.55              | 64.54               | 4.62              | 69.17              | 0.11                                | 0.08               | 0.965           |
| Area_2004    | 71.68              | 0.00              | 0.00             | 24.23             | 3.59                | 43.89             | 47.48              | 0.01                                | 0.01               | 0.662           |
| Area_2005    | 71.68              | 0.00              | 0.00             | 24.23             | 3.59                | 43.89             | 47.48              | 0.02                                | 0.01               | 0.662           |
| Area_21      | 71.68              | 0.00              | 0.00             | 2.48              | 64.57               | 4.70              | 69.27              | 0.15                                | 0.10               | 0.966           |
| Area_22      | 71.68              | 0.00              | 0.00             | 2.48              | 64.57               | 4.70              | 69.27              | 0.22                                | 0.16               | 0.966           |
| Area_23      | 71.68              | 0.00              | 0.00             | 2.48              | 64.57               | 4.70              | 69.27              | 0.11                                | 0.08               | 0.966           |
| Area_3       | 71.68              | 0.00              | 0.00             | 2.48              | 64.57               | 4.70              | 69.27              | 0.25                                | 0.18               | 0.966           |
| Area_4       | 71.68              | 0.00              | 0.00             | 2.48              | 64.57               | 4.70              | 69.27              | 0.19                                | 0.14               | 0.966           |
| Area_5       | 71.68              | 0.00              | 0.00             | 2.48              | 64.57               | 4.70              | 69.27              | 0.10                                | 0.07               | 0.966           |
| Area_6       | 71.68              | 0.00              | 0.00             | 2.48              | 64.57               | 4.70              | 69.27              | 0.10                                | 0.07               | 0.966           |
| Area_7       | 71.68              | 0.00              | 0.00             | 2.48              | 64.57               | 4.70              | 69.27              | 0.03                                | 0.02               | 0.966           |
| Area_8       | 71.68              | 0.00              | 0.00             | 2.48              | 64.57               | 4.70              | 69.27              | 0.08                                | 0.06               | 0.966           |
| Area_9       | 71.68              | 0.00              | 0.00             | 2.48              | 64.57               | 4.70              | 69.27              | 0.08                                | 0.06               | 0.966           |

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 Node Depth Summary  
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| Node    | Type     | Average<br>Depth<br>Meters | Maximum<br>Depth<br>Meters | Maximum<br>HGL<br>Meters | Time of Max<br>Occurrence<br>days hr:min | Reported<br>Max Depth<br>Meters |
|---------|----------|----------------------------|----------------------------|--------------------------|--|---------------------------------|
| CB_10   | JUNCTION | 0.00                       | 0.16                       | 65.49                    | 0 01:10                                  | 0.16                            |
| CB_23   | JUNCTION | 0.00                       | 0.11                       | 66.31                    | 0 01:10                                  | 0.11                            |
| CB_27   | JUNCTION | 0.00                       | 0.31                       | 65.80                    | 0 01:10                                  | 0.30                            |
| CB_28   | JUNCTION | 0.00                       | 0.39                       | 65.78                    | 0 01:10                                  | 0.37                            |
| CB_29   | JUNCTION | 0.01                       | 0.86                       | 64.98                    | 0 01:08                                  | 0.60                            |
| CB_5    | JUNCTION | 0.00                       | 0.16                       | 65.28                    | 0 01:10                                  | 0.16                            |
| CBMH_11 | JUNCTION | 0.06                       | 1.13                       | 64.71                    | 0 01:52                                  | 1.13                            |
| CBMH_12 | JUNCTION | 0.02                       | 1.51                       | 65.57                    | 0 01:03                                  | 0.84                            |
| CBMH_14 | JUNCTION | 0.04                       | 1.08                       | 65.19                    | 0 01:32                                  | 1.08                            |
| CBMH_15 | JUNCTION | 0.01                       | 1.34                       | 65.81                    | 0 01:16                                  | 0.72                            |
| CBMH_18 | JUNCTION | 0.05                       | 1.14                       | 65.19                    | 0 01:32                                  | 1.14                            |
| CBMH_19 | JUNCTION | 0.00                       | 0.32                       | 65.19                    | 0 01:33                                  | 0.32                            |
| CBMH_2  | JUNCTION | 0.02                       | 0.66                       | 64.72                    | 0 01:53                                  | 0.66                            |
| CBMH_21 | JUNCTION | 0.00                       | 0.27                       | 65.44                    | 0 01:10                                  | 0.27                            |
| CBMH_22 | JUNCTION | 0.00                       | 0.20                       | 65.73                    | 0 01:10                                  | 0.20                            |
| CBMH_3  | JUNCTION | 0.00                       | 0.30                       | 64.71                    | 0 01:53                                  | 0.30                            |
| CBMH_4  | JUNCTION | 0.00                       | 0.23                       | 65.00                    | 0 01:10                                  | 0.23                            |
| CBMH_6  | JUNCTION | 0.02                       | 0.80                       | 64.71                    | 0 01:52                                  | 0.80                            |
| CBMH_7  | JUNCTION | 0.01                       | 0.44                       | 64.71                    | 0 01:50                                  | 0.44                            |
| CBMH_8  | JUNCTION | 0.00                       | 0.30                       | 64.93                    | 0 01:10                                  | 0.30                            |
| CBMH_9  | JUNCTION | 0.00                       | 0.23                       | 65.22                    | 0 01:10                                  | 0.23                            |
| DCB_16  | JUNCTION | 0.00                       | 0.39                       | 65.19                    | 0 01:32                                  | 0.39                            |
| J1      | JUNCTION | 0.01                       | 0.18                       | 63.93                    | 0 01:32                                  | 0.18                            |

|           |          |      |      |       |   |       |      |
|-----------|----------|------|------|-------|---|-------|------|
| J13       | JUNCTION | 0.06 | 1.17 | 64.71 | 0 | 01:52 | 1.17 |
| J2        | JUNCTION | 0.01 | 0.14 | 63.37 | 0 | 01:53 | 0.14 |
| MH_20     | JUNCTION | 0.00 | 0.27 | 65.26 | 0 | 01:10 | 0.27 |
| MH_24     | JUNCTION | 0.04 | 1.06 | 65.19 | 0 | 01:31 | 1.06 |
| MH_25     | JUNCTION | 0.02 | 0.99 | 65.40 | 0 | 01:10 | 0.98 |
| MH_26     | JUNCTION | 0.01 | 1.23 | 65.78 | 0 | 01:10 | 1.22 |
| MH_27     | JUNCTION | 0.03 | 0.82 | 64.71 | 0 | 01:52 | 0.82 |
| MH_30     | JUNCTION | 0.04 | 0.98 | 64.71 | 0 | 01:52 | 0.98 |
| MH_44     | JUNCTION | 0.02 | 0.42 | 63.93 | 0 | 01:32 | 0.42 |
| MH_45     | JUNCTION | 0.02 | 0.26 | 63.37 | 0 | 01:53 | 0.26 |
| OGS_1     | JUNCTION | 0.01 | 0.10 | 63.14 | 0 | 01:53 | 0.10 |
| OGS_2     | JUNCTION | 0.01 | 0.35 | 63.82 | 0 | 01:32 | 0.35 |
| Humber_P1 | OUTFALL  | 0.00 | 0.00 | 62.48 | 0 | 00:00 | 0.00 |
| OF1       | OUTFALL  | 0.01 | 0.33 | 63.74 | 0 | 01:32 | 0.33 |
| OF2       | OUTFALL  | 0.00 | 0.00 | 0.00  | 0 | 00:00 | 0.00 |
| SU_N      | STORAGE  | 0.09 | 1.44 | 65.19 | 0 | 01:32 | 1.44 |
| SU_S      | STORAGE  | 0.11 | 1.47 | 64.71 | 0 | 01:53 | 1.47 |

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Node Inflow Summary  
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| Node      | Type     | Maximum Lateral Inflow<br>CMS | Maximum Total Inflow<br>CMS | Time of Max Occurrence<br>days hr:min | Lateral Inflow Volume<br>10^6 ltr | Total Inflow Volume<br>10^6 ltr | Flow Balance Error<br>Percent |
|-----------|----------|-------------------------------|-----------------------------|---------------------------------------|-----------------------------------|---------------------------------|-------------------------------|
| CB_10     | JUNCTION | 0.064                         | 0.064                       | 0 01:10                               | 0.09                              | 0.09                            | -0.012                        |
| CB_23     | JUNCTION | 0.039                         | 0.039                       | 0 01:10                               | 0.0554                            | 0.0554                          | -0.007                        |
| CB_27     | JUNCTION | 0.074                         | 0.074                       | 0 01:10                               | 0.104                             | 0.104                           | 0.357                         |
| CB_28     | JUNCTION | 0.074                         | 0.074                       | 0 01:10                               | 0.104                             | 0.104                           | 0.478                         |
| CB_29     | JUNCTION | 0.079                         | 0.079                       | 0 01:10                               | 0.111                             | 0.111                           | 0.583                         |
| CB_5      | JUNCTION | 0.074                         | 0.074                       | 0 01:10                               | 0.104                             | 0.104                           | -0.013                        |
| CBMH_11   | JUNCTION | 0.636                         | 0.872                       | 0 01:10                               | 0.942                             | 1.27                            | 0.040                         |
| CBMH_12   | JUNCTION | 0.157                         | 0.157                       | 0 01:10                               | 0.222                             | 0.222                           | 0.322                         |
| CBMH_14   | JUNCTION | 0.123                         | 0.378                       | 0 01:07                               | 0.173                             | 0.53                            | -0.516                        |
| CBMH_15   | JUNCTION | 0.079                         | 0.258                       | 0 01:09                               | 0.111                             | 0.358                           | 0.361                         |
| CBMH_18   | JUNCTION | 0.138                         | 1.071                       | 0 01:10                               | 0.194                             | 1.62                            | 0.006                         |
| CBMH_19   | JUNCTION | 0.020                         | 0.177                       | 0 01:10                               | 0.0277                            | 0.249                           | 0.857                         |
| CBMH_2    | JUNCTION | 0.084                         | 0.323                       | 0 01:10                               | 0.118                             | 0.458                           | 0.370                         |
| CBMH_21   | JUNCTION | 0.059                         | 0.157                       | 0 01:10                               | 0.0831                            | 0.222                           | 0.067                         |
| CBMH_22   | JUNCTION | 0.059                         | 0.098                       | 0 01:10                               | 0.0831                            | 0.139                           | 0.041                         |
| CBMH_3    | JUNCTION | 0.084                         | 0.241                       | 0 01:10                               | 0.118                             | 0.338                           | 0.207                         |
| CBMH_4    | JUNCTION | 0.084                         | 0.157                       | 0 01:10                               | 0.118                             | 0.222                           | 0.640                         |
| CBMH_6    | JUNCTION | 0.044                         | 0.348                       | 0 01:10                               | 0.0623                            | 0.487                           | -0.394                        |
| CBMH_7    | JUNCTION | 0.084                         | 0.304                       | 0 01:10                               | 0.118                             | 0.427                           | 0.625                         |
| CBMH_8    | JUNCTION | 0.079                         | 0.221                       | 0 01:10                               | 0.111                             | 0.311                           | 0.562                         |
| CBMH_9    | JUNCTION | 0.079                         | 0.142                       | 0 01:10                               | 0.111                             | 0.201                           | 0.228                         |
| DCB_16    | JUNCTION | 0.177                         | 0.177                       | 0 01:10                               | 0.249                             | 0.249                           | 0.955                         |
| J1        | JUNCTION | 0.000                         | 0.014                       | 0 01:32                               | 0                                 | 0.951                           | -0.005                        |
| J13       | JUNCTION | 0.138                         | 0.802                       | 0 01:08                               | 0.194                             | 1.14                            | -0.232                        |
| J2        | JUNCTION | 0.000                         | 0.015                       | 0 01:53                               | 0                                 | 1.21                            | -0.004                        |
| MH_20     | JUNCTION | 0.000                         | 0.157                       | 0 01:10                               | 0                                 | 0.221                           | -0.019                        |
| MH_24     | JUNCTION | 0.000                         | 0.940                       | 0 01:10                               | 0                                 | 1.42                            | -0.507                        |
| MH_25     | JUNCTION | 0.000                         | 0.764                       | 0 01:10                               | 0                                 | 1.17                            | 0.262                         |
| MH_26     | JUNCTION | 0.646                         | 0.771                       | 0 01:08                               | 0.965                             | 1.17                            | 0.074                         |
| MH_27     | JUNCTION | 0.000                         | 0.080                       | 0 01:08                               | 0                                 | 0.11                            | -0.540                        |
| MH_30     | JUNCTION | 0.000                         | 0.323                       | 0 01:10                               | 0                                 | 0.459                           | -0.800                        |
| MH_44     | JUNCTION | 0.000                         | 0.207                       | 0 01:32                               | 0                                 | 2.15                            | 0.012                         |
| MH_45     | JUNCTION | 0.000                         | 0.124                       | 0 01:53                               | 0                                 | 2.42                            | 0.000                         |
| OGS_1     | JUNCTION | 0.000                         | 0.124                       | 0 01:53                               | 0                                 | 2.42                            | -0.000                        |
| OGS_2     | JUNCTION | 0.000                         | 0.207                       | 0 01:32                               | 0                                 | 2.15                            | -0.011                        |
| Humber_P1 | OUTFALL  | 0.017                         | 0.127                       | 0 01:50                               | 0.0285                            | 2.45                            | 0.000                         |
| OF1       | OUTFALL  | 0.076                         | 0.219                       | 0 01:30                               | 0.111                             | 2.26                            | 0.000                         |
| OF2       | OUTFALL  | 0.110                         | 0.110                       | 0 01:10                               | 0.181                             | 0.181                           | 0.000                         |
| SU_N      | STORAGE  | 0.000                         | 1.442                       | 0 01:08                               | 0                                 | 2.15                            | -0.100                        |
| SU_S      | STORAGE  | 0.000                         | 1.654                       | 0 01:08                               | 0                                 | 2.42                            | -0.085                        |

\*\*\*\*\*  
Node Surcharge Summary  
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Surcharging occurs when water rises above the top of the highest conduit.

| Node    | Type     | Hours Surcharged | Max. Height Above Crown<br>Meters | Min. Depth Below Rim<br>Meters |
|---------|----------|------------------|-----------------------------------|--------------------------------|
| CB_29   | JUNCTION | 2.31             | 0.490                             | 1.562                          |
| CBMH_11 | JUNCTION | 3.90             | 0.488                             | 1.029                          |
| CBMH_12 | JUNCTION | 2.66             | 1.140                             | 0.167                          |
| CBMH_14 | JUNCTION | 2.80             | 0.483                             | 1.131                          |
| CBMH_15 | JUNCTION | 0.87             | 0.755                             | 0.514                          |
| CBMH_18 | JUNCTION | 2.17             | 0.389                             | 1.401                          |
| CBMH_2  | JUNCTION | 0.01             | 0.002                             | 2.281                          |
| CBMH_6  | JUNCTION | 2.15             | 0.213                             | 1.930                          |
| J13     | JUNCTION | 3.32             | 0.422                             | 1.931                          |
| MH_24   | JUNCTION | 0.70             | 0.097                             | 1.439                          |
| MH_25   | JUNCTION | 1.20             | 0.389                             | 1.636                          |
| MH_26   | JUNCTION | 0.04             | 0.176                             | 1.477                          |
| MH_27   | JUNCTION | 3.20             | 0.387                             | 1.199                          |
| MH_30   | JUNCTION | 2.69             | 0.319                             | 2.099                          |

\*\*\*\*\*  
Node Flooding Summary  
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No nodes were flooded.

\*\*\*\*\*  
Storage Volume Summary  
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| Storage Unit | Average Volume<br>1000 m3 | Avg Pcnt Full | Evap Pcnt Loss | Exfil Pcnt Loss | Maximum Volume<br>1000 m3 | Max Pcnt Full | Time of Max Occurrence<br>days hr:min | Maximum Outflow<br>CMS |
|--------------|---------------------------|---------------|----------------|-----------------|---------------------------|---------------|---------------------------------------|------------------------|
| SU_N         | 0.067                     | 3             | 0              | 0               | 1.304                     | 50            | 0 01:32                               | 0.207                  |
| SU_S         | 0.107                     | 3             | 0              | 0               | 1.664                     | 48            | 0 01:53                               | 0.124                  |

\*\*\*\*\*  
Outfall Loading Summary  
\*\*\*\*\*

| Outfall Node | Flow Freq<br>Pcnt | Avg Flow<br>CMS | Max Flow<br>CMS | Total Volume<br>10^6 ltr |
|--------------|-------------------|-----------------|-----------------|--------------------------|
| Humber_Pl    | 29.10             | 0.014           | 0.127           | 2.446                    |
| OF1          | 23.64             | 0.018           | 0.219           | 2.261                    |
| OF2          | 4.45              | 0.008           | 0.110           | 0.181                    |
| System       | 19.06             | 0.040           | 0.370           | 4.888                    |

\*\*\*\*\*  
Link Flow Summary  
\*\*\*\*\*

| Link | Type    | Maximum  Flow <br>CMS | Time of Max Occurrence<br>days hr:min | Maximum  Veloc <br>m/sec | Max/ Full<br>Flow | Max/ Full<br>Depth |
|------|---------|-----------------------|---------------------------------------|--------------------------|-------------------|--------------------|
| C1   | CONDUIT | 0.193                 | 0 01:32                               | 6.13                     | 4.07              | 1.00               |
| C10  | CONDUIT | 0.079                 | 0 01:11                               | 1.65                     | 0.24              | 0.94               |
| C11  | CONDUIT | 0.087                 | 0 01:10                               | 1.66                     | 0.26              | 0.85               |
| C12  | CONDUIT | 0.764                 | 0 01:10                               | 3.53                     | 2.13              | 1.00               |
| C13  | CONDUIT | 0.935                 | 0 01:10                               | 3.31                     | 1.82              | 1.00               |
| C14  | CONDUIT | 0.039                 | 0 01:10                               | 1.45                     | 0.19              | 0.29               |
| C15  | CONDUIT | 0.098                 | 0 01:10                               | 1.40                     | 0.41              | 0.45               |
| C16  | CONDUIT | 0.157                 | 0 01:10                               | 1.61                     | 0.66              | 0.59               |
| C17  | CONDUIT | 0.157                 | 0 01:10                               | 1.60                     | 0.66              | 0.59               |
| C18  | CONDUIT | 0.177                 | 0 01:10                               | 1.65                     | 0.74              | 0.85               |
| C19  | CONDUIT | 0.064                 | 0 01:10                               | 1.28                     | 0.27              | 0.35               |
| C2   | CONDUIT | 0.207                 | 0 01:32                               | 1.90                     | 1.64              | 0.96               |
| C20  | CONDUIT | 0.142                 | 0 01:10                               | 1.52                     | 0.40              | 0.45               |
| C21  | CONDUIT | 0.221                 | 0 01:10                               | 1.70                     | 0.61              | 0.58               |
| C22  | CONDUIT | 0.304                 | 0 01:10                               | 1.86                     | 0.85              | 0.92               |
| C23  | CONDUIT | 0.347                 | 0 01:09                               | 1.95                     | 0.96              | 1.00               |
| C24  | CONDUIT | 0.800                 | 0 01:07                               | 2.37                     | 0.86              | 1.00               |
| C25  | CONDUIT | 0.074                 | 0 01:10                               | 1.31                     | 0.21              | 0.31               |
| C26  | CONDUIT | 0.157                 | 0 01:10                               | 1.59                     | 0.31              | 0.38               |
| C27  | CONDUIT | 0.240                 | 0 01:10                               | 1.78                     | 0.47              | 0.74               |
| C28  | CONDUIT | 0.323                 | 0 01:10                               | 1.91                     | 0.63              | 1.00               |
| C29  | CONDUIT | 0.157                 | 0 01:10                               | 1.42                     | 1.00              | 1.00               |
| C3   | CONDUIT | 0.014                 | 0 01:33                               | 0.84                     | 0.18              | 0.63               |
| C30  | CONDUIT | 0.320                 | 0 01:08                               | 1.73                     | 0.63              | 1.00               |
| C31  | CONDUIT | 0.080                 | 0 01:08                               | 0.97                     | 0.55              | 1.00               |
| C32  | CONDUIT | 0.872                 | 0 01:10                               | 4.03                     | 2.42              | 1.00               |
| C33  | CONDUIT | 0.124                 | 0 01:53                               | 5.15                     | 0.16              | 0.27               |
| C34  | CONDUIT | 0.207                 | 0 01:32                               | 1.97                     | 1.21              | 0.90               |
| C35  | CONDUIT | 0.764                 | 0 01:10                               | 2.70                     | 1.49              | 1.00               |
| C36  | CONDUIT | 1.071                 | 0 01:10                               | 2.67                     | 1.14              | 1.00               |
| C37  | CONDUIT | 0.080                 | 0 01:08                               | 1.20                     | 0.55              | 1.00               |
| C4   | CONDUIT | 0.110                 | 0 01:53                               | 3.49                     | 2.31              | 1.00               |
| C5   | CONDUIT | 0.015                 | 0 01:53                               | 0.82                     | 0.18              | 0.54               |
| C6   | CONDUIT | 0.124                 | 0 01:53                               | 1.52                     | 0.86              | 0.69               |
| C7   | CONDUIT | 0.179                 | 0 01:09                               | 1.62                     | 0.50              | 0.88               |
| C8   | CONDUIT | 0.256                 | 0 01:07                               | 1.77                     | 0.71              | 1.00               |
| C9   | CONDUIT | 0.376                 | 0 01:08                               | 1.95                     | 0.73              | 1.00               |
| OR1  | ORIFICE | 0.015                 | 0 01:53                               |                          |                   | 1.00               |
| OR2  | ORIFICE | 0.014                 | 0 01:32                               |                          |                   | 1.00               |

\*\*\*\*\*  
Flow Classification Summary  
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| Adjusted /Actual | Fraction of Time in Flow Class |      |     |     |    |      |      |       |
|------------------|--------------------------------|------|-----|-----|----|------|------|-------|
|                  | Up                             | Down | Sub | Sup | Up | Down | Norm | Inlet |

| Conduit | Length | Dry  | Dry  | Dry  | Crit | Crit | Crit | Crit | Ltd  | Ctrl |
|---------|--------|------|------|------|------|------|------|------|------|------|
| C1      | 1.00   | 0.97 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.03 | 0.00 | 0.00 |
| C10     | 1.00   | 0.00 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0.99 | 0.00 | 0.00 |
| C11     | 1.00   | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C12     | 1.00   | 0.00 | 0.00 | 0.00 | 0.05 | 0.00 | 0.00 | 0.95 | 0.01 | 0.00 |
| C13     | 1.00   | 0.00 | 0.00 | 0.00 | 0.10 | 0.00 | 0.00 | 0.90 | 0.00 | 0.00 |
| C14     | 1.00   | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C15     | 1.00   | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C16     | 1.00   | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.99 | 0.00 | 0.00 |
| C17     | 1.00   | 0.00 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0.99 | 0.00 | 0.00 |
| C18     | 1.00   | 0.00 | 0.00 | 0.00 | 0.03 | 0.00 | 0.00 | 0.97 | 0.01 | 0.00 |
| C19     | 1.00   | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C2      | 1.00   | 0.00 | 0.09 | 0.00 | 0.77 | 0.14 | 0.00 | 0.00 | 0.78 | 0.00 |
| C20     | 1.00   | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C21     | 1.00   | 0.00 | 0.00 | 0.00 | 0.02 | 0.00 | 0.00 | 0.98 | 0.01 | 0.00 |
| C22     | 1.00   | 0.00 | 0.00 | 0.00 | 0.06 | 0.00 | 0.00 | 0.94 | 0.03 | 0.00 |
| C23     | 1.00   | 0.00 | 0.00 | 0.00 | 0.09 | 0.00 | 0.00 | 0.91 | 0.03 | 0.00 |
| C24     | 1.00   | 0.00 | 0.00 | 0.00 | 0.13 | 0.00 | 0.00 | 0.87 | 0.01 | 0.00 |
| C25     | 1.00   | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C26     | 1.00   | 0.00 | 0.00 | 0.00 | 0.02 | 0.00 | 0.00 | 0.98 | 0.01 | 0.00 |
| C27     | 1.00   | 0.00 | 0.00 | 0.00 | 0.04 | 0.00 | 0.00 | 0.96 | 0.01 | 0.00 |
| C28     | 1.00   | 0.00 | 0.00 | 0.00 | 0.09 | 0.00 | 0.00 | 0.91 | 0.04 | 0.00 |
| C29     | 1.00   | 0.00 | 0.00 | 0.00 | 0.09 | 0.00 | 0.00 | 0.91 | 0.05 | 0.00 |
| C3      | 1.00   | 0.00 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0.99 | 0.00 | 0.00 |
| C30     | 1.00   | 0.00 | 0.00 | 0.00 | 0.10 | 0.00 | 0.00 | 0.90 | 0.01 | 0.00 |
| C31     | 1.00   | 0.00 | 0.00 | 0.00 | 0.08 | 0.00 | 0.00 | 0.92 | 0.02 | 0.00 |
| C32     | 1.00   | 0.00 | 0.00 | 0.00 | 0.13 | 0.00 | 0.00 | 0.87 | 0.01 | 0.00 |
| C33     | 1.00   | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C34     | 1.00   | 0.00 | 0.00 | 0.00 | 0.75 | 0.25 | 0.00 | 0.00 | 0.04 | 0.00 |
| C35     | 1.00   | 0.00 | 0.00 | 0.00 | 0.09 | 0.00 | 0.00 | 0.91 | 0.03 | 0.00 |
| C36     | 1.00   | 0.00 | 0.00 | 0.00 | 0.11 | 0.00 | 0.00 | 0.89 | 0.00 | 0.00 |
| C37     | 1.00   | 0.00 | 0.00 | 0.00 | 0.06 | 0.00 | 0.00 | 0.94 | 0.03 | 0.00 |
| C4      | 1.00   | 0.96 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.04 | 0.00 | 0.00 |
| C5      | 1.00   | 0.00 | 0.00 | 0.00 | 0.03 | 0.00 | 0.00 | 0.97 | 0.00 | 0.00 |
| C6      | 1.00   | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| C7      | 1.00   | 0.00 | 0.00 | 0.00 | 0.04 | 0.00 | 0.00 | 0.96 | 0.02 | 0.00 |
| C8      | 1.00   | 0.00 | 0.00 | 0.00 | 0.09 | 0.00 | 0.00 | 0.91 | 0.04 | 0.00 |
| C9      | 1.00   | 0.00 | 0.00 | 0.00 | 0.10 | 0.00 | 0.00 | 0.89 | 0.01 | 0.00 |

\*\*\*\*\*  
Conduit Surcharge Summary  
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| Conduit | Hours Full |          | Hours             |      | Hours Capacity Limited |
|---------|------------|----------|-------------------|------|------------------------|
|         | Both Ends  | Upstream | Above Normal Flow | Full |                        |
| C1      | 2.08       | 2.16     | 2.08              | 2.35 | 2.08                   |
| C10     | 0.01       | 0.01     | 0.07              | 0.01 | 0.01                   |
| C11     | 0.01       | 0.01     | 0.04              | 0.01 | 0.01                   |
| C12     | 0.98       | 1.01     | 1.25              | 0.22 | 0.18                   |
| C13     | 2.58       | 2.64     | 2.76              | 0.18 | 0.07                   |
| C18     | 0.01       | 0.01     | 0.70              | 0.01 | 0.01                   |
| C2      | 0.01       | 0.69     | 0.01              | 1.46 | 0.01                   |
| C22     | 0.01       | 0.01     | 2.15              | 0.01 | 0.01                   |
| C23     | 2.46       | 2.46     | 3.32              | 0.01 | 0.01                   |
| C24     | 3.32       | 3.32     | 3.45              | 0.01 | 0.01                   |
| C27     | 0.01       | 0.01     | 0.01              | 0.01 | 0.01                   |
| C28     | 0.99       | 0.99     | 2.69              | 0.01 | 0.01                   |
| C29     | 2.66       | 2.66     | 4.96              | 0.03 | 0.03                   |
| C30     | 3.04       | 3.04     | 3.32              | 0.01 | 0.01                   |
| C31     | 3.58       | 3.58     | 3.90              | 0.01 | 0.01                   |
| C32     | 6.08       | 6.11     | 8.35              | 0.23 | 0.18                   |
| C34     | 0.01       | 0.01     | 0.01              | 0.88 | 0.01                   |
| C35     | 1.13       | 1.20     | 2.22              | 0.15 | 0.06                   |
| C36     | 2.17       | 2.17     | 2.28              | 0.09 | 0.01                   |
| C37     | 2.31       | 2.31     | 3.20              | 0.01 | 0.01                   |
| C4      | 2.89       | 3.23     | 2.89              | 3.45 | 2.89                   |
| C7      | 0.01       | 0.01     | 0.87              | 0.01 | 0.01                   |
| C8      | 1.13       | 1.13     | 2.95              | 0.01 | 0.01                   |
| C9      | 2.80       | 2.80     | 3.93              | 0.01 | 0.01                   |

Analysis begun on: Wed Oct 5 21:19:30 2022  
Analysis ended on: Wed Oct 5 21:20:01 2022  
Total elapsed time: 00:00:31

100-yr, 6-hour

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.015)

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WARNING 03: negative offset ignored for Link C2  
WARNING 03: negative offset ignored for Link C32  
WARNING 03: negative offset ignored for Link C34

\*\*\*\*\*  
Element Count  
\*\*\*\*\*  
Number of rain gages ..... 7  
Number of subcatchments ... 30  
Number of nodes ..... 40  
Number of links ..... 39  
Number of pollutants ..... 0  
Number of land uses ..... 0

\*\*\*\*\*  
Raingage Summary  
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| Name      | Data Source | Data Type | Recording Interval |
|-----------|-------------|-----------|--------------------|
| 25mm      | 25mm        | INTENSITY | 5 min.             |
| 3hr-100yr | 3hr-100yr   | INTENSITY | 10 min.            |
| 3hr-2yr   | 3hr-2yr     | INTENSITY | 5 min.             |
| 3hr-5yr   | 3hr-5yr     | INTENSITY | 5 min.             |
| 6hr-100yr | 6hr-100yr   | INTENSITY | 10 min.            |
| 6hr-2yr   | 6hr-2yr     | INTENSITY | 5 min.             |
| 6hr-5yr   | 6hr-5yr     | INTENSITY | 5 min.             |

\*\*\*\*\*  
Subcatchment Summary  
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| Name      | Area | Width  | %Imperv | %Slope | Rain Gage | Outlet    |
|-----------|------|--------|---------|--------|-----------|-----------|
| Area_1    | 0.25 | 83.33  | 90.00   | 1.0000 | 6hr-100yr | CBMH_14   |
| Area_10   | 0.08 | 26.67  | 90.00   | 1.0000 | 6hr-100yr | CB_23     |
| Area_101  | 1.37 | 137.00 | 95.00   | 0.5000 | 6hr-100yr | MH_26     |
| Area_102  | 1.13 | 113.00 | 95.00   | 0.5000 | 6hr-100yr | CBMH_11   |
| Area_11   | 0.13 | 43.33  | 90.00   | 1.0000 | 6hr-100yr | CB_10     |
| Area_12   | 0.16 | 53.33  | 90.00   | 1.0000 | 6hr-100yr | CBMH_9    |
| Area_13   | 0.16 | 53.33  | 90.00   | 1.0000 | 6hr-100yr | CBMH_8    |
| Area_14   | 0.17 | 56.67  | 90.00   | 1.0000 | 6hr-100yr | CBMH_7    |
| Area_15   | 0.09 | 30.00  | 90.00   | 1.0000 | 6hr-100yr | CBMH_6    |
| Area_16   | 0.15 | 50.00  | 90.00   | 1.0000 | 6hr-100yr | CB_5      |
| Area_17   | 0.17 | 56.67  | 90.00   | 1.0000 | 6hr-100yr | CBMH_4    |
| Area_18   | 0.17 | 56.67  | 90.00   | 1.0000 | 6hr-100yr | CBMH_3    |
| Area_19   | 0.17 | 56.67  | 90.00   | 1.0000 | 6hr-100yr | CBMH_2    |
| Area_2    | 0.16 | 53.33  | 90.00   | 1.0000 | 6hr-100yr | CBMH_15   |
| Area_20   | 0.28 | 93.33  | 90.00   | 1.0000 | 6hr-100yr | J13       |
| Area_2001 | 0.07 | 7.00   | 25.00   | 0.5000 | 6hr-100yr | OF2       |
| Area_2002 | 0.21 | 21.00  | 90.00   | 0.5000 | 6hr-100yr | OF2       |
| Area_2003 | 0.16 | 16.00  | 90.00   | 1.0000 | 6hr-100yr | OF1       |
| Area_2004 | 0.02 | 13.33  | 5.00    | 0.5000 | 6hr-100yr | Humber_P1 |
| Area_2005 | 0.04 | 26.67  | 5.00    | 0.5000 | 6hr-100yr | Humber_P1 |
| Area_21   | 0.21 | 70.00  | 90.00   | 1.0000 | 6hr-100yr | CBMH_11   |
| Area_22   | 0.32 | 106.67 | 90.00   | 1.0000 | 6hr-100yr | CBMH_12   |
| Area_23   | 0.16 | 53.33  | 90.00   | 1.0000 | 6hr-100yr | CB_29     |
| Area_3    | 0.36 | 120.00 | 90.00   | 1.0000 | 6hr-100yr | DCB_16    |
| Area_4    | 0.28 | 93.33  | 90.00   | 1.0000 | 6hr-100yr | CBMH_18   |
| Area_5    | 0.15 | 50.00  | 90.00   | 1.0000 | 6hr-100yr | CB_27     |
| Area_6    | 0.15 | 50.00  | 90.00   | 1.0000 | 6hr-100yr | CB_28     |
| Area_7    | 0.04 | 13.33  | 90.00   | 1.0000 | 6hr-100yr | CBMH_19   |
| Area_8    | 0.12 | 40.00  | 90.00   | 1.0000 | 6hr-100yr | CBMH_21   |
| Area_9    | 0.12 | 40.00  | 90.00   | 1.0000 | 6hr-100yr | CBMH_22   |

\*\*\*\*\*  
Node Summary  
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| Name    | Type     | Invert Elev. | Max. Depth | Ponded Area | External Inflow |
|---------|----------|--------------|------------|-------------|-----------------|
| CB_10   | JUNCTION | 65.33        | 1.41       | 10.0        |                 |
| CB_23   | JUNCTION | 66.20        | 0.93       | 10.0        |                 |
| CB_27   | JUNCTION | 65.48        | 1.34       | 10.0        |                 |
| CB_28   | JUNCTION | 65.39        | 1.52       | 10.0        |                 |
| CB_29   | JUNCTION | 64.11        | 2.43       | 0.0         |                 |
| CB_5    | JUNCTION | 65.11        | 1.63       | 10.0        |                 |
| CBMH_11 | JUNCTION | 63.58        | 2.16       | 10.0        |                 |
| CBMH_12 | JUNCTION | 64.06        | 1.68       | 10.0        |                 |
| CBMH_14 | JUNCTION | 64.11        | 2.21       | 10.0        |                 |
| CBMH_15 | JUNCTION | 64.47        | 1.85       | 10.0        |                 |
| CBMH_18 | JUNCTION | 64.05        | 2.54       | 0.0         |                 |
| CBMH_19 | JUNCTION | 64.88        | 2.38       | 10.0        |                 |
| CBMH_2  | JUNCTION | 64.06        | 2.94       | 10.0        |                 |
| CBMH_21 | JUNCTION | 65.17        | 1.87       | 10.0        |                 |
| CBMH_22 | JUNCTION | 65.53        | 1.51       | 10.0        |                 |
| CBMH_3  | JUNCTION | 64.42        | 2.58       | 10.0        |                 |



|           |          |       |      |      |
|-----------|----------|-------|------|------|
| CBMH_4    | JUNCTION | 64.78 | 2.22 | 10.0 |
| CBMH_6    | JUNCTION | 63.91 | 2.73 | 10.0 |
| CBMH_7    | JUNCTION | 64.27 | 2.73 | 10.0 |
| CBMH_8    | JUNCTION | 64.63 | 2.37 | 10.0 |
| CBMH_9    | JUNCTION | 64.99 | 2.01 | 10.0 |
| DCB_16    | JUNCTION | 64.80 | 1.52 | 10.0 |
| J1        | JUNCTION | 63.75 | 3.27 | 0.0  |
| J13       | JUNCTION | 63.54 | 3.10 | 10.0 |
| J2        | JUNCTION | 63.24 | 3.33 | 0.0  |
| MH_20     | JUNCTION | 64.99 | 2.30 | 0.0  |
| MH_24     | JUNCTION | 64.13 | 2.50 | 10.0 |
| MH_25     | JUNCTION | 64.42 | 2.63 | 0.0  |
| MH_26     | JUNCTION | 64.56 | 2.70 | 0.0  |
| MH_27     | JUNCTION | 63.89 | 2.02 | 0.0  |
| MH_30     | JUNCTION | 63.73 | 3.08 | 0.0  |
| MH_44     | JUNCTION | 63.51 | 3.51 | 0.0  |
| MH_45     | JUNCTION | 63.11 | 3.46 | 0.0  |
| OGS_1     | JUNCTION | 63.04 | 3.34 | 0.0  |
| OGS_2     | JUNCTION | 63.47 | 3.01 | 0.0  |
| Humber_P1 | OUTFALL  | 62.48 | 0.38 | 0.0  |
| OF1       | OUTFALL  | 63.41 | 0.38 | 0.0  |
| OF2       | OUTFALL  | 0.00  | 0.00 | 0.0  |
| SU_N      | STORAGE  | 63.75 | 3.04 | 0.0  |
| SU_S      | STORAGE  | 63.24 | 3.33 | 0.0  |

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Link Summary  
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| Name | From Node | To Node   | Type    | Length | %Slope  | Roughness |
|------|-----------|-----------|---------|--------|---------|-----------|
| C1   | SU_N      | MH_44     | CONDUIT | 2.5    | 1.0001  | 0.0090    |
| C10  | CB_28     | MH_26     | CONDUIT | 30.4   | 1.0001  | 0.0110    |
| C11  | CB_27     | MH_26     | CONDUIT | 32.8   | 1.0001  | 0.0110    |
| C12  | MH_26     | MH_25     | CONDUIT | 16.5   | 0.4970  | 0.0110    |
| C13  | MH_24     | CBMH_18   | CONDUIT | 4.8    | 0.5000  | 0.0110    |
| C14  | CB_23     | CBMH_22   | CONDUIT | 51.5   | 1.0001  | 0.0110    |
| C15  | CBMH_22   | CBMH_21   | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C16  | CBMH_21   | MH_20     | CONDUIT | 24.5   | 0.5020  | 0.0110    |
| C17  | MH_20     | CBMH_19   | CONDUIT | 10.4   | 0.5000  | 0.0110    |
| C18  | CBMH_19   | MH_24     | CONDUIT | 46.5   | 0.5011  | 0.0110    |
| C19  | CB_10     | CBMH_9    | CONDUIT | 52.5   | 0.4991  | 0.0110    |
| C2   | MH_44     | OGS_2     | CONDUIT | 11.6   | 0.3707  | 0.0110    |
| C20  | CBMH_9    | CBMH_8    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C21  | CBMH_8    | CBMH_7    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C22  | CBMH_7    | CBMH_6    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C23  | CBMH_6    | J13       | CONDUIT | 29.9   | 0.5017  | 0.0110    |
| C24  | J13       | SU_S      | CONDUIT | 4.0    | 0.5000  | 0.0110    |
| C25  | CB_5      | CBMH_4    | CONDUIT | 52.5   | 0.4991  | 0.0110    |
| C26  | CBMH_4    | CBMH_3    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C27  | CBMH_3    | CBMH_2    | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C28  | CBMH_2    | MH_30     | CONDUIT | 53.4   | 0.4963  | 0.0110    |
| C29  | CBMH_12   | CBMH_11   | CONDUIT | 50.0   | 0.5700  | 0.0110    |
| C3   | J1        | MH_44     | CONDUIT | 2.5    | 0.4800  | 0.0110    |
| C30  | MH_30     | J13       | CONDUIT | 9.3    | 0.4839  | 0.0110    |
| C31  | MH_27     | CBMH_11   | CONDUIT | 8.2    | 0.5000  | 0.0110    |
| C32  | CBMH_11   | SU_S      | CONDUIT | 13.2   | 0.5000  | 0.0110    |
| C33  | OGS_1     | Humber_P1 | CONDUIT | 4.0    | 14.1135 | 0.0110    |
| C34  | OGS_2     | OF1       | CONDUIT | 8.7    | 0.6782  | 0.0110    |
| C35  | MH_25     | MH_24     | CONDUIT | 44.2   | 0.5000  | 0.0110    |
| C36  | CBMH_18   | SU_N      | CONDUIT | 3.9    | 0.5128  | 0.0110    |
| C37  | CB_29     | MH_27     | CONDUIT | 32.9   | 0.4985  | 0.0110    |
| C4   | SU_S      | MH_45     | CONDUIT | 9.4    | 1.0001  | 0.0090    |
| C5   | J2        | MH_45     | CONDUIT | 9.4    | 0.5000  | 0.0110    |
| C6   | MH_45     | OGS_1     | CONDUIT | 3.1    | 0.4839  | 0.0110    |
| C7   | DCB_16    | CBMH_15   | CONDUIT | 54.4   | 0.5000  | 0.0110    |
| C8   | CBMH_15   | CBMH_14   | CONDUIT | 60.0   | 0.5000  | 0.0110    |
| C9   | CBMH_14   | SU_N      | CONDUIT | 15.2   | 0.5000  | 0.0110    |
| OR1  | SU_S      | J2        | ORIFICE |        |         |           |
| OR2  | SU_N      | J1        | ORIFICE |        |         |           |

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Cross Section Summary  
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| Conduit | Shape    | Full Depth | Full Area | Hyd. Rad. | Max. Width | No. of Barrels | Full Flow |
|---------|----------|------------|-----------|-----------|------------|----------------|-----------|
| C1      | CIRCULAR | 0.20       | 0.03      | 0.05      | 0.20       | 1              | 0.05      |
| C10     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.34      |
| C11     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.34      |
| C12     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C13     | CIRCULAR | 0.60       | 0.28      | 0.15      | 0.60       | 1              | 0.51      |
| C14     | CIRCULAR | 0.38       | 0.11      | 0.09      | 0.38       | 1              | 0.21      |
| C15     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C16     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C17     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C18     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C19     | CIRCULAR | 0.45       | 0.16      | 0.11      | 0.45       | 1              | 0.24      |
| C2      | CIRCULAR | 0.38       | 0.11      | 0.09      | 0.38       | 1              | 0.13      |
| C20     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C21     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C22     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C23     | CIRCULAR | 0.53       | 0.22      | 0.13      | 0.53       | 1              | 0.36      |
| C24     | CIRCULAR | 0.75       | 0.44      | 0.19      | 0.75       | 1              | 0.93      |

|     |          |      |      |      |      |   |      |
|-----|----------|------|------|------|------|---|------|
| C25 | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C26 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C27 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C28 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C29 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.16 |
| C3  | CIRCULAR | 0.30 | 0.07 | 0.07 | 0.30 | 1 | 0.08 |
| C30 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.50 |
| C31 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.15 |
| C32 | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C33 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.78 |
| C34 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.17 |
| C35 | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |
| C36 | CIRCULAR | 0.75 | 0.44 | 0.19 | 0.75 | 1 | 0.94 |
| C37 | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.15 |
| C4  | CIRCULAR | 0.20 | 0.03 | 0.05 | 0.20 | 1 | 0.05 |
| C5  | CIRCULAR | 0.30 | 0.07 | 0.07 | 0.30 | 1 | 0.08 |
| C6  | CIRCULAR | 0.38 | 0.11 | 0.09 | 0.38 | 1 | 0.14 |
| C7  | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C8  | CIRCULAR | 0.53 | 0.22 | 0.13 | 0.53 | 1 | 0.36 |
| C9  | CIRCULAR | 0.60 | 0.28 | 0.15 | 0.60 | 1 | 0.51 |

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NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
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\*\*\*\*\*  
Analysis Options  
\*\*\*\*\*  
Flow Units ..... CMS  
Process Models:  
  Rainfall/Runoff ..... YES  
  RDII ..... NO  
  Snowmelt ..... NO  
  Groundwater ..... NO  
  Flow Routing ..... YES  
  Ponding Allowed ..... NO  
  Water Quality ..... NO  
Infiltration Method ..... HORTON  
Flow Routing Method ..... DYNWAVE  
Surcharge Method ..... EXTRAN  
Starting Date ..... 12/11/2020 00:00:00  
Ending Date ..... 12/21/2020 00:00:00  
Antecedent Dry Days ..... 0.0  
Report Time Step ..... 00:01:00  
Wet Time Step ..... 00:01:00  
Dry Time Step ..... 00:01:00  
Routing Time Step ..... 1.00 sec  
Variable Time Step ..... YES  
Maximum Trials ..... 8  
Number of Threads ..... 6  
Head Tolerance ..... 0.001500 m

|                            | Volume    | Depth  |
|----------------------------|-----------|--------|
| Runoff Quantity Continuity | hectare-m | mm     |
| Total Precipitation        | 0.580     | 82.325 |
| Evaporation Loss           | 0.000     | 0.000  |
| Infiltration Loss          | 0.018     | 2.506  |
| Surface Runoff             | 0.563     | 79.876 |
| Final Storage              | 0.000     | 0.000  |
| Continuity Error (%)       | -0.069    |        |

|                         | Volume    | Volume   |
|-------------------------|-----------|----------|
| Flow Routing Continuity | hectare-m | 10^6 ltr |
| Dry Weather Inflow      | 0.000     | 0.000    |
| Wet Weather Inflow      | 0.563     | 5.630    |
| Groundwater Inflow      | 0.000     | 0.000    |
| RDII Inflow             | 0.000     | 0.000    |
| External Inflow         | 0.000     | 0.000    |
| External Outflow        | 0.563     | 5.633    |
| Flooding Loss           | 0.000     | 0.000    |
| Evaporation Loss        | 0.000     | 0.000    |
| Exfiltration Loss       | 0.000     | 0.000    |
| Initial Stored Volume   | 0.000     | 0.000    |
| Final Stored Volume     | 0.000     | 0.000    |
| Continuity Error (%)    | -0.048    |          |

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Time-Step Critical Elements  
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Link C33 (4.38%)

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Highest Flow Instability Indexes  
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Link C2 (5)

Link OR2 (1)  
 Link OR1 (1)

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 Routing Time Step Summary  
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Minimum Time Step : 0.50 sec  
 Average Time Step : 0.98 sec  
 Maximum Time Step : 1.00 sec  
 Percent in Steady State : -0.00  
 Average Iterations per Step : 2.00  
 Percent Not Converging : 0.01  
 Time Step Frequencies :  
 1.000 - 0.871 sec : 95.79 %  
 0.871 - 0.758 sec : 0.30 %  
 0.758 - 0.660 sec : 0.29 %  
 0.660 - 0.574 sec : 0.83 %  
 0.574 - 0.500 sec : 2.79 %

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 Subcatchment Runoff Summary  
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| Subcatchment | Total Precip<br>mm | Total Runon<br>mm | Total Evap<br>mm | Total Infil<br>mm | Imperv Runoff<br>mm | Perv Runoff<br>mm | Total Runoff<br>mm | Total Runoff<br>10 <sup>6</sup> ltr | Peak Runoff<br>CMS | Runoff Coeff |
|--------------|--------------------|-------------------|------------------|-------------------|---------------------|-------------------|--------------------|-------------------------------------|--------------------|--------------|
| Area_1       | 82.33              | 0.00              | 0.00             | 2.58              | 74.16               | 5.66              | 79.82              | 0.20                                | 0.12               | 0.970        |
| Area_10      | 82.32              | 0.00              | 0.00             | 2.58              | 74.16               | 5.66              | 79.82              | 0.06                                | 0.04               | 0.970        |
| Area_101     | 82.32              | 0.00              | 0.00             | 1.30              | 78.24               | 2.82              | 81.06              | 1.11                                | 0.65               | 0.985        |
| Area_102     | 82.32              | 0.00              | 0.00             | 1.30              | 78.24               | 2.82              | 81.06              | 0.92                                | 0.53               | 0.985        |
| Area_11      | 82.33              | 0.00              | 0.00             | 2.58              | 74.16               | 5.66              | 79.82              | 0.10                                | 0.06               | 0.970        |
| Area_12      | 82.32              | 0.00              | 0.00             | 2.58              | 74.16               | 5.66              | 79.82              | 0.13                                | 0.08               | 0.970        |
| Area_13      | 82.32              | 0.00              | 0.00             | 2.58              | 74.16               | 5.66              | 79.82              | 0.13                                | 0.08               | 0.970        |
| Area_14      | 82.32              | 0.00              | 0.00             | 2.58              | 74.16               | 5.66              | 79.82              | 0.14                                | 0.08               | 0.970        |
| Area_15      | 82.33              | 0.00              | 0.00             | 2.58              | 74.16               | 5.66              | 79.82              | 0.07                                | 0.04               | 0.970        |
| Area_16      | 82.33              | 0.00              | 0.00             | 2.58              | 74.16               | 5.66              | 79.82              | 0.12                                | 0.07               | 0.970        |
| Area_17      | 82.32              | 0.00              | 0.00             | 2.58              | 74.16               | 5.66              | 79.82              | 0.14                                | 0.08               | 0.970        |
| Area_18      | 82.32              | 0.00              | 0.00             | 2.58              | 74.16               | 5.66              | 79.82              | 0.14                                | 0.08               | 0.970        |
| Area_19      | 82.32              | 0.00              | 0.00             | 2.58              | 74.16               | 5.66              | 79.82              | 0.14                                | 0.08               | 0.970        |
| Area_2       | 82.32              | 0.00              | 0.00             | 2.58              | 74.16               | 5.66              | 79.82              | 0.13                                | 0.08               | 0.970        |
| Area_20      | 82.33              | 0.00              | 0.00             | 2.58              | 74.16               | 5.66              | 79.82              | 0.22                                | 0.14               | 0.970        |
| Area_2001    | 82.33              | 0.00              | 0.00             | 21.03             | 20.60               | 40.72             | 61.31              | 0.04                                | 0.01               | 0.745        |
| Area_2002    | 82.33              | 0.00              | 0.00             | 2.63              | 74.12               | 5.61              | 79.73              | 0.17                                | 0.10               | 0.969        |
| Area_2003    | 82.32              | 0.00              | 0.00             | 2.65              | 74.13               | 5.59              | 79.72              | 0.13                                | 0.08               | 0.968        |
| Area_2004    | 82.32              | 0.00              | 0.00             | 25.10             | 4.12                | 53.14             | 57.25              | 0.01                                | 0.01               | 0.695        |
| Area_2005    | 82.32              | 0.00              | 0.00             | 25.10             | 4.12                | 53.14             | 57.25              | 0.02                                | 0.01               | 0.695        |
| Area_21      | 82.33              | 0.00              | 0.00             | 2.58              | 74.16               | 5.66              | 79.82              | 0.17                                | 0.10               | 0.970        |
| Area_22      | 82.32              | 0.00              | 0.00             | 2.58              | 74.16               | 5.66              | 79.82              | 0.26                                | 0.16               | 0.970        |
| Area_23      | 82.32              | 0.00              | 0.00             | 2.58              | 74.16               | 5.66              | 79.82              | 0.13                                | 0.08               | 0.970        |
| Area_3       | 82.33              | 0.00              | 0.00             | 2.58              | 74.16               | 5.66              | 79.82              | 0.29                                | 0.18               | 0.970        |
| Area_4       | 82.33              | 0.00              | 0.00             | 2.58              | 74.16               | 5.66              | 79.82              | 0.22                                | 0.14               | 0.970        |
| Area_5       | 82.33              | 0.00              | 0.00             | 2.58              | 74.16               | 5.66              | 79.82              | 0.12                                | 0.07               | 0.970        |
| Area_6       | 82.33              | 0.00              | 0.00             | 2.58              | 74.16               | 5.66              | 79.82              | 0.12                                | 0.07               | 0.970        |
| Area_7       | 82.32              | 0.00              | 0.00             | 2.58              | 74.16               | 5.66              | 79.82              | 0.03                                | 0.02               | 0.970        |
| Area_8       | 82.33              | 0.00              | 0.00             | 2.58              | 74.16               | 5.66              | 79.82              | 0.10                                | 0.06               | 0.970        |
| Area_9       | 82.33              | 0.00              | 0.00             | 2.58              | 74.16               | 5.66              | 79.82              | 0.10                                | 0.06               | 0.970        |

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 Node Depth Summary  
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| Node    | Type     | Average Depth<br>Meters | Maximum Depth<br>Meters | Maximum HGL<br>Meters | Time of Max Occurrence<br>days hr:min | Reported Max Depth<br>Meters |
|---------|----------|-------------------------|-------------------------|-----------------------|---------------------------------------|------------------------------|
| CB_10   | JUNCTION | 0.00                    | 0.16                    | 65.49                 | 0 02:10                               | 0.16                         |
| CB_23   | JUNCTION | 0.00                    | 0.11                    | 66.31                 | 0 02:10                               | 0.11                         |
| CB_27   | JUNCTION | 0.00                    | 0.48                    | 65.96                 | 0 02:10                               | 0.45                         |
| CB_28   | JUNCTION | 0.00                    | 1.39                    | 66.77                 | 0 02:09                               | 0.54                         |
| CB_29   | JUNCTION | 0.02                    | 0.93                    | 65.04                 | 0 02:07                               | 0.67                         |
| CB_5    | JUNCTION | 0.00                    | 0.16                    | 65.28                 | 0 02:10                               | 0.16                         |
| CBMH_11 | JUNCTION | 0.06                    | 1.20                    | 64.78                 | 0 02:50                               | 1.20                         |
| CBMH_12 | JUNCTION | 0.02                    | 1.45                    | 65.50                 | 0 02:03                               | 0.93                         |
| CBMH_14 | JUNCTION | 0.05                    | 1.15                    | 65.26                 | 0 02:32                               | 1.15                         |
| CBMH_15 | JUNCTION | 0.02                    | 1.57                    | 66.04                 | 0 02:13                               | 0.80                         |
| CBMH_18 | JUNCTION | 0.05                    | 1.21                    | 65.26                 | 0 02:31                               | 1.21                         |
| CBMH_19 | JUNCTION | 0.00                    | 0.39                    | 65.26                 | 0 02:30                               | 0.39                         |
| CBMH_2  | JUNCTION | 0.02                    | 0.73                    | 64.78                 | 0 02:50                               | 0.72                         |
| CBMH_21 | JUNCTION | 0.00                    | 0.27                    | 65.44                 | 0 02:10                               | 0.27                         |
| CBMH_22 | JUNCTION | 0.00                    | 0.20                    | 65.73                 | 0 02:10                               | 0.20                         |
| CBMH_3  | JUNCTION | 0.01                    | 0.37                    | 64.78                 | 0 02:50                               | 0.36                         |
| CBMH_4  | JUNCTION | 0.00                    | 0.23                    | 65.01                 | 0 02:10                               | 0.23                         |
| CBMH_6  | JUNCTION | 0.03                    | 0.87                    | 64.78                 | 0 02:50                               | 0.87                         |
| CBMH_7  | JUNCTION | 0.01                    | 0.51                    | 64.78                 | 0 02:50                               | 0.51                         |
| CBMH_8  | JUNCTION | 0.00                    | 0.30                    | 64.93                 | 0 02:10                               | 0.30                         |
| CBMH_9  | JUNCTION | 0.00                    | 0.23                    | 65.22                 | 0 02:10                               | 0.23                         |
| DCB_16  | JUNCTION | 0.01                    | 0.47                    | 65.27                 | 0 02:29                               | 0.47                         |
| J1      | JUNCTION | 0.01                    | 0.24                    | 63.99                 | 0 02:31                               | 0.24                         |
| J13     | JUNCTION | 0.07                    | 1.24                    | 64.78                 | 0 02:51                               | 1.24                         |

|           |          |      |      |       |   |       |      |
|-----------|----------|------|------|-------|---|-------|------|
| J2        | JUNCTION | 0.02 | 0.15 | 63.38 | 0 | 02:51 | 0.15 |
| MH_20     | JUNCTION | 0.00 | 0.27 | 65.26 | 0 | 02:30 | 0.27 |
| MH_24     | JUNCTION | 0.04 | 1.13 | 65.26 | 0 | 02:31 | 1.13 |
| MH_25     | JUNCTION | 0.02 | 1.26 | 65.67 | 0 | 02:09 | 1.10 |
| MH_26     | JUNCTION | 0.01 | 1.59 | 66.15 | 0 | 02:09 | 1.35 |
| MH_27     | JUNCTION | 0.03 | 0.89 | 64.78 | 0 | 02:50 | 0.89 |
| MH_30     | JUNCTION | 0.04 | 1.05 | 64.78 | 0 | 02:50 | 1.05 |
| MH_44     | JUNCTION | 0.02 | 0.47 | 63.99 | 0 | 02:31 | 0.47 |
| MH_45     | JUNCTION | 0.02 | 0.27 | 63.38 | 0 | 02:51 | 0.27 |
| OGS_1     | JUNCTION | 0.01 | 0.10 | 63.14 | 0 | 02:51 | 0.10 |
| OGS_2     | JUNCTION | 0.02 | 0.38 | 63.85 | 0 | 02:31 | 0.38 |
| Humber_P1 | OUTFALL  | 0.00 | 0.00 | 62.48 | 0 | 00:00 | 0.00 |
| OF1       | OUTFALL  | 0.01 | 0.34 | 63.75 | 0 | 02:31 | 0.34 |
| OF2       | OUTFALL  | 0.00 | 0.00 | 0.00  | 0 | 00:00 | 0.00 |
| SU_N      | STORAGE  | 0.10 | 1.51 | 65.26 | 0 | 02:31 | 1.51 |
| SU_S      | STORAGE  | 0.12 | 1.54 | 64.78 | 0 | 02:51 | 1.54 |

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Node Inflow Summary  
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| Node      | Type     | Maximum Lateral Inflow<br>CMS | Maximum Total Inflow<br>CMS | Time of Max Occurrence<br>days hr:min | Lateral Inflow Volume<br>10^6 ltr | Total Inflow Volume<br>10^6 ltr | Flow Balance Error<br>Percent |
|-----------|----------|-------------------------------|-----------------------------|---------------------------------------|-----------------------------------|---------------------------------|-------------------------------|
| CB_10     | JUNCTION | 0.064                         | 0.064                       | 0 02:10                               | 0.104                             | 0.104                           | -0.010                        |
| CB_23     | JUNCTION | 0.039                         | 0.039                       | 0 02:10                               | 0.0638                            | 0.0638                          | -0.006                        |
| CB_27     | JUNCTION | 0.074                         | 0.074                       | 0 02:10                               | 0.12                              | 0.12                            | 0.440                         |
| CB_28     | JUNCTION | 0.074                         | 0.074                       | 0 02:10                               | 0.12                              | 0.12                            | 0.379                         |
| CB_29     | JUNCTION | 0.079                         | 0.079                       | 0 02:10                               | 0.128                             | 0.128                           | 0.499                         |
| CB_5      | JUNCTION | 0.074                         | 0.074                       | 0 02:10                               | 0.12                              | 0.12                            | -0.011                        |
| CBMH_11   | JUNCTION | 0.637                         | 0.874                       | 0 02:10                               | 1.08                              | 1.47                            | 0.034                         |
| CBMH_12   | JUNCTION | 0.158                         | 0.158                       | 0 02:10                               | 0.255                             | 0.255                           | 0.284                         |
| CBMH_14   | JUNCTION | 0.123                         | 0.377                       | 0 02:06                               | 0.2                               | 0.612                           | -0.406                        |
| CBMH_15   | JUNCTION | 0.079                         | 0.258                       | 0 02:08                               | 0.128                             | 0.413                           | -0.081                        |
| CBMH_18   | JUNCTION | 0.138                         | 1.080                       | 0 02:10                               | 0.223                             | 1.86                            | 0.005                         |
| CBMH_19   | JUNCTION | 0.020                         | 0.177                       | 0 02:10                               | 0.0319                            | 0.287                           | 0.775                         |
| CBMH_2    | JUNCTION | 0.084                         | 0.325                       | 0 02:10                               | 0.136                             | 0.523                           | 0.118                         |
| CBMH_21   | JUNCTION | 0.059                         | 0.158                       | 0 02:10                               | 0.0958                            | 0.255                           | 0.120                         |
| CBMH_22   | JUNCTION | 0.059                         | 0.099                       | 0 02:10                               | 0.0958                            | 0.16                            | 0.027                         |
| CBMH_3    | JUNCTION | 0.084                         | 0.241                       | 0 02:10                               | 0.136                             | 0.39                            | 0.533                         |
| CBMH_4    | JUNCTION | 0.084                         | 0.158                       | 0 02:10                               | 0.136                             | 0.255                           | 0.562                         |
| CBMH_6    | JUNCTION | 0.044                         | 0.349                       | 0 02:10                               | 0.0718                            | 0.562                           | -0.377                        |
| CBMH_7    | JUNCTION | 0.084                         | 0.305                       | 0 02:10                               | 0.136                             | 0.493                           | 0.562                         |
| CBMH_8    | JUNCTION | 0.079                         | 0.222                       | 0 02:10                               | 0.128                             | 0.358                           | 0.432                         |
| CBMH_9    | JUNCTION | 0.079                         | 0.143                       | 0 02:10                               | 0.128                             | 0.231                           | 0.306                         |
| DCB_I6    | JUNCTION | 0.177                         | 0.177                       | 0 02:10                               | 0.287                             | 0.287                           | 0.838                         |
| J1        | JUNCTION | 0.000                         | 0.014                       | 0 02:23                               | 0                                 | 1.02                            | -0.004                        |
| J13       | JUNCTION | 0.138                         | 0.801                       | 0 02:07                               | 0.223                             | 1.31                            | -0.203                        |
| J2        | JUNCTION | 0.000                         | 0.015                       | 0 02:51                               | 0                                 | 1.28                            | -0.003                        |
| MH_20     | JUNCTION | 0.000                         | 0.158                       | 0 02:10                               | 0                                 | 0.255                           | -0.069                        |
| MH_24     | JUNCTION | 0.000                         | 0.963                       | 0 02:10                               | 0                                 | 1.63                            | -0.450                        |
| MH_25     | JUNCTION | 0.000                         | 0.787                       | 0 02:10                               | 0                                 | 1.35                            | 0.228                         |
| MH_26     | JUNCTION | 0.647                         | 0.787                       | 0 02:10                               | 1.11                              | 1.35                            | 0.049                         |
| MH_27     | JUNCTION | 0.000                         | 0.080                       | 0 02:07                               | 0                                 | 0.127                           | -0.483                        |
| MH_30     | JUNCTION | 0.000                         | 0.327                       | 0 02:09                               | 0                                 | 0.523                           | -0.712                        |
| MH_44     | JUNCTION | 0.000                         | 0.223                       | 0 02:31                               | 0                                 | 2.48                            | 0.011                         |
| MH_45     | JUNCTION | 0.000                         | 0.132                       | 0 02:51                               | 0                                 | 2.78                            | 0.000                         |
| OGS_1     | JUNCTION | 0.000                         | 0.132                       | 0 02:51                               | 0                                 | 2.78                            | -0.000                        |
| OGS_2     | JUNCTION | 0.000                         | 0.223                       | 0 02:31                               | 0                                 | 2.48                            | -0.009                        |
| Humber_P1 | OUTFALL  | 0.019                         | 0.135                       | 0 02:44                               | 0.0344                            | 2.82                            | 0.000                         |
| OF1       | OUTFALL  | 0.077                         | 0.236                       | 0 02:30                               | 0.128                             | 2.6                             | 0.000                         |
| OF2       | OUTFALL  | 0.111                         | 0.111                       | 0 02:10                               | 0.21                              | 0.21                            | 0.000                         |
| SU_N      | STORAGE  | 0.000                         | 1.428                       | 0 02:10                               | 0                                 | 2.48                            | -0.069                        |
| SU_S      | STORAGE  | 0.000                         | 1.642                       | 0 02:09                               | 0                                 | 2.78                            | -0.074                        |

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Node Surcharge Summary  
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Surcharging occurs when water rises above the top of the highest conduit.

| Node    | Type     | Hours Surcharged | Max. Height Above Crown<br>Meters | Min. Depth Below Rim<br>Meters |
|---------|----------|------------------|-----------------------------------|--------------------------------|
| CB_27   | JUNCTION | 0.01             | 0.027                             | 0.868                          |
| CB_28   | JUNCTION | 0.02             | 0.938                             | 0.136                          |
| CB_29   | JUNCTION | 2.73             | 0.554                             | 1.498                          |
| CBMH_11 | JUNCTION | 4.80             | 0.560                             | 0.957                          |
| CBMH_12 | JUNCTION | 3.15             | 1.070                             | 0.237                          |
| CBMH_14 | JUNCTION | 3.66             | 0.553                             | 1.061                          |
| CBMH_15 | JUNCTION | 1.04             | 0.987                             | 0.282                          |
| CBMH_18 | JUNCTION | 2.32             | 0.459                             | 1.331                          |
| CBMH_2  | JUNCTION | 1.01             | 0.065                             | 2.218                          |
| CBMH_6  | JUNCTION | 2.56             | 0.285                             | 1.858                          |
| J13     | JUNCTION | 4.22             | 0.493                             | 1.860                          |
| MH_24   | JUNCTION | 0.90             | 0.167                             | 1.369                          |
| MH_25   | JUNCTION | 1.31             | 0.660                             | 1.365                          |
| MH_26   | JUNCTION | 0.05             | 0.545                             | 1.108                          |
| MH_27   | JUNCTION | 4.00             | 0.459                             | 1.127                          |

MH\_30                    JUNCTION            3.32            0.389            2.029  
 OGS\_2                   JUNCTION            0.31            0.007            2.629

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 Node Flooding Summary  
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No nodes were flooded.

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 Storage Volume Summary  
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| Storage Unit | Average<br>Volume<br>1000 m3 | Avg<br>Pcnt<br>Full | Evap<br>Pcnt<br>Loss | Exfil<br>Pcnt<br>Loss | Maximum<br>Volume<br>1000 m3 | Max<br>Pcnt<br>Full | Time of Max<br>Occurrence<br>days hr:min | Maximum<br>Outflow<br>CMS |
|--------------|------------------------------|---------------------|----------------------|-----------------------|------------------------------|---------------------|--|---------------------------|
| SU_N         | 0.075                        | 3                   | 0                    | 0                     | 1.371                        | 53                  | 0 02:31                                  | 0.223                     |
| SU_S         | 0.118                        | 3                   | 0                    | 0                     | 1.748                        | 51                  | 0 02:51                                  | 0.132                     |

\*\*\*\*\*  
 Outfall Loading Summary  
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| Outfall Node | Flow<br>Freq<br>Pcnt | Avg<br>Flow<br>CMS | Max<br>Flow<br>CMS | Total<br>Volume<br>10^6 ltr |
|--------------|----------------------|--------------------|--------------------|-----------------------------|
| Humber_Pl    | 30.07                | 0.017              | 0.135              | 2.818                       |
| OF1          | 24.82                | 0.020              | 0.236              | 2.605                       |
| OF2          | 5.74                 | 0.007              | 0.111              | 0.210                       |
| System       | 20.21                | 0.043              | 0.402              | 5.633                       |

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 Link Flow Summary  
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| Link | Type    | Maximum<br> Flow <br>CMS | Time of Max<br>Occurrence<br>days hr:min | Maximum<br> Veloc <br>m/sec | Max/<br>Full<br>Flow | Max/<br>Full<br>Depth |
|------|---------|--------------------------|--|-----------------------------|----------------------|-----------------------|
| C1   | CONDUIT | 0.208                    | 0 02:31                                  | 6.63                        | 4.40                 | 1.00                  |
| C10  | CONDUIT | 0.078                    | 0 02:09                                  | 1.66                        | 0.23                 | 1.00                  |
| C11  | CONDUIT | 0.091                    | 0 02:10                                  | 1.67                        | 0.27                 | 1.00                  |
| C12  | CONDUIT | 0.787                    | 0 02:10                                  | 3.63                        | 2.20                 | 1.00                  |
| C13  | CONDUIT | 0.947                    | 0 02:10                                  | 3.35                        | 1.85                 | 1.00                  |
| C14  | CONDUIT | 0.039                    | 0 02:10                                  | 1.45                        | 0.19                 | 0.30                  |
| C15  | CONDUIT | 0.099                    | 0 02:10                                  | 1.40                        | 0.41                 | 0.45                  |
| C16  | CONDUIT | 0.158                    | 0 02:10                                  | 1.61                        | 0.66                 | 0.59                  |
| C17  | CONDUIT | 0.158                    | 0 02:10                                  | 1.60                        | 0.66                 | 0.67                  |
| C18  | CONDUIT | 0.177                    | 0 02:09                                  | 1.64                        | 0.74                 | 0.93                  |
| C19  | CONDUIT | 0.064                    | 0 02:10                                  | 1.28                        | 0.27                 | 0.35                  |
| C2   | CONDUIT | 0.223                    | 0 02:31                                  | 2.02                        | 1.76                 | 1.00                  |
| C20  | CONDUIT | 0.143                    | 0 02:10                                  | 1.52                        | 0.40                 | 0.45                  |
| C21  | CONDUIT | 0.221                    | 0 02:10                                  | 1.70                        | 0.62                 | 0.59                  |
| C22  | CONDUIT | 0.305                    | 0 02:10                                  | 1.86                        | 0.85                 | 0.99                  |
| C23  | CONDUIT | 0.347                    | 0 02:07                                  | 1.95                        | 0.96                 | 1.00                  |
| C24  | CONDUIT | 0.797                    | 0 02:07                                  | 2.36                        | 0.86                 | 1.00                  |
| C25  | CONDUIT | 0.074                    | 0 02:10                                  | 1.31                        | 0.21                 | 0.31                  |
| C26  | CONDUIT | 0.158                    | 0 02:10                                  | 1.59                        | 0.31                 | 0.38                  |
| C27  | CONDUIT | 0.241                    | 0 02:10                                  | 1.78                        | 0.47                 | 0.80                  |
| C28  | CONDUIT | 0.327                    | 0 02:09                                  | 1.91                        | 0.64                 | 1.00                  |
| C29  | CONDUIT | 0.158                    | 0 02:10                                  | 1.43                        | 1.01                 | 1.00                  |
| C3   | CONDUIT | 0.015                    | 0 02:43                                  | 0.84                        | 0.19                 | 0.81                  |
| C30  | CONDUIT | 0.319                    | 0 02:07                                  | 1.73                        | 0.63                 | 1.00                  |
| C31  | CONDUIT | 0.080                    | 0 02:07                                  | 0.97                        | 0.55                 | 1.00                  |
| C32  | CONDUIT | 0.874                    | 0 02:10                                  | 4.04                        | 2.43                 | 1.00                  |
| C33  | CONDUIT | 0.132                    | 0 02:51                                  | 5.24                        | 0.17                 | 0.28                  |
| C34  | CONDUIT | 0.223                    | 0 02:31                                  | 2.06                        | 1.30                 | 0.95                  |
| C35  | CONDUIT | 0.787                    | 0 02:10                                  | 2.78                        | 1.53                 | 1.00                  |
| C36  | CONDUIT | 1.079                    | 0 02:10                                  | 2.63                        | 1.15                 | 1.00                  |
| C37  | CONDUIT | 0.080                    | 0 02:07                                  | 1.20                        | 0.55                 | 1.00                  |
| C4   | CONDUIT | 0.117                    | 0 02:51                                  | 3.73                        | 2.47                 | 1.00                  |
| C5   | CONDUIT | 0.015                    | 0 02:52                                  | 0.82                        | 0.19                 | 0.57                  |
| C6   | CONDUIT | 0.132                    | 0 02:51                                  | 1.56                        | 0.92                 | 0.72                  |
| C7   | CONDUIT | 0.180                    | 0 02:08                                  | 1.62                        | 0.50                 | 0.95                  |
| C8   | CONDUIT | 0.255                    | 0 02:06                                  | 1.73                        | 0.71                 | 1.00                  |
| C9   | CONDUIT | 0.366                    | 0 02:07                                  | 1.89                        | 0.71                 | 1.00                  |
| OR1  | ORIFICE | 0.015                    | 0 02:51                                  |                             |                      | 1.00                  |
| OR2  | ORIFICE | 0.014                    | 0 02:23                                  |                             |                      | 1.00                  |

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 Flow Classification Summary  
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| Conduit | Adjusted<br>/Actual<br>Length | ----- Fraction of Time in Flow Class ----- |             |            |             |            |              |             |               |      |
|---------|-------------------------------|--|-------------|------------|-------------|------------|--------------|-------------|---------------|------|
|         |                               | Up<br>Dry                                  | Down<br>Dry | Sub<br>Dry | Sup<br>Crit | Up<br>Crit | Down<br>Crit | Norm<br>Ltd | Inlet<br>Ctrl |      |
| C1      | 1.00                          | 0.96                                       | 0.00        | 0.00       | 0.00        | 0.00       | 0.00         | 0.04        | 0.00          | 0.00 |
| C10     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.01        | 0.00       | 0.00         | 0.99        | 0.00          | 0.00 |
| C11     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.01        | 0.00       | 0.00         | 0.99        | 0.00          | 0.00 |
| C12     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.06        | 0.00       | 0.00         | 0.94        | 0.01          | 0.00 |
| C13     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.10        | 0.00       | 0.00         | 0.89        | 0.00          | 0.00 |
| C14     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.00        | 0.00       | 0.00         | 1.00        | 0.00          | 0.00 |
| C15     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.00        | 0.00       | 0.00         | 1.00        | 0.00          | 0.00 |
| C16     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.01        | 0.00       | 0.00         | 0.99        | 0.00          | 0.00 |
| C17     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.01        | 0.00       | 0.00         | 0.99        | 0.00          | 0.00 |
| C18     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.04        | 0.00       | 0.00         | 0.96        | 0.01          | 0.00 |
| C19     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.00        | 0.00       | 0.00         | 1.00        | 0.00          | 0.00 |
| C2      | 1.00                          | 0.00                                       | 0.09        | 0.00       | 0.76        | 0.15       | 0.00         | 0.00        | 0.77          | 0.00 |
| C20     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.00        | 0.00       | 0.00         | 0.99        | 0.00          | 0.00 |
| C21     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.03        | 0.00       | 0.00         | 0.97        | 0.01          | 0.00 |
| C22     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.07        | 0.00       | 0.00         | 0.93        | 0.03          | 0.00 |
| C23     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.10        | 0.00       | 0.00         | 0.90        | 0.03          | 0.00 |
| C24     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.14        | 0.00       | 0.00         | 0.86        | 0.01          | 0.00 |
| C25     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.00        | 0.00       | 0.00         | 1.00        | 0.00          | 0.00 |
| C26     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.02        | 0.00       | 0.00         | 0.98        | 0.01          | 0.00 |
| C27     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.04        | 0.00       | 0.00         | 0.95        | 0.02          | 0.00 |
| C28     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.09        | 0.00       | 0.00         | 0.91        | 0.04          | 0.00 |
| C29     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.10        | 0.00       | 0.00         | 0.90        | 0.05          | 0.00 |
| C3      | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.01        | 0.00       | 0.00         | 0.99        | 0.00          | 0.00 |
| C30     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.11        | 0.00       | 0.00         | 0.89        | 0.01          | 0.00 |
| C31     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.08        | 0.00       | 0.00         | 0.91        | 0.02          | 0.00 |
| C32     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.14        | 0.00       | 0.00         | 0.86        | 0.01          | 0.00 |
| C33     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.00        | 0.00       | 0.00         | 1.00        | 0.00          | 0.00 |
| C34     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.74        | 0.26       | 0.00         | 0.00        | 0.05          | 0.00 |
| C35     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.09        | 0.00       | 0.00         | 0.91        | 0.03          | 0.00 |
| C36     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.12        | 0.00       | 0.00         | 0.88        | 0.00          | 0.00 |
| C37     | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.07        | 0.00       | 0.00         | 0.93        | 0.03          | 0.00 |
| C4      | 1.00                          | 0.95                                       | 0.00        | 0.00       | 0.00        | 0.00       | 0.00         | 0.05        | 0.00          | 0.00 |
| C5      | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.03        | 0.00       | 0.00         | 0.96        | 0.00          | 0.00 |
| C6      | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.00        | 0.00       | 0.00         | 1.00        | 0.00          | 0.00 |
| C7      | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.05        | 0.00       | 0.00         | 0.95        | 0.03          | 0.00 |
| C8      | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.10        | 0.00       | 0.00         | 0.90        | 0.04          | 0.00 |
| C9      | 1.00                          | 0.00                                       | 0.00        | 0.00       | 0.11        | 0.00       | 0.00         | 0.88        | 0.01          | 0.00 |

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Conduit Surcharge Summary  
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| Conduit | ----- Hours Full ----- |          |          | Hours             | Hours            |
|---------|------------------------|----------|----------|-------------------|------------------|
|         | Both Ends              | Upstream | Dnstream | Above Normal Flow | Capacity Limited |
| C1      | 2.19                   | 2.32     | 2.19     | 2.65              | 2.19             |
| C10     | 0.02                   | 0.02     | 0.08     | 0.01              | 0.01             |
| C11     | 0.01                   | 0.01     | 0.05     | 0.01              | 0.01             |
| C12     | 1.11                   | 1.14     | 1.36     | 0.23              | 0.18             |
| C13     | 3.13                   | 3.17     | 3.56     | 0.18              | 0.09             |
| C18     | 0.01                   | 0.01     | 0.90     | 0.01              | 0.01             |
| C2      | 0.30                   | 0.89     | 0.30     | 1.57              | 0.30             |
| C22     | 0.01                   | 0.01     | 2.56     | 0.01              | 0.01             |
| C23     | 3.01                   | 3.01     | 4.22     | 0.01              | 0.01             |
| C24     | 4.22                   | 4.22     | 4.36     | 0.01              | 0.01             |
| C27     | 0.01                   | 0.01     | 1.01     | 0.01              | 0.01             |
| C28     | 1.48                   | 1.48     | 3.32     | 0.01              | 0.01             |
| C29     | 3.15                   | 3.15     | 5.89     | 0.05              | 0.05             |
| C30     | 3.84                   | 3.84     | 4.22     | 0.01              | 0.01             |
| C31     | 4.48                   | 4.48     | 4.80     | 0.01              | 0.01             |
| C32     | 7.02                   | 7.05     | 9.30     | 0.23              | 0.19             |
| C34     | 0.01                   | 0.30     | 0.01     | 1.05              | 0.01             |
| C35     | 1.25                   | 1.31     | 2.40     | 0.15              | 0.07             |
| C36     | 2.32                   | 2.32     | 2.53     | 0.10              | 0.03             |
| C37     | 2.73                   | 2.73     | 4.00     | 0.01              | 0.01             |
| C4      | 3.60                   | 4.12     | 3.60     | 4.36              | 3.60             |
| C7      | 0.01                   | 0.01     | 1.04     | 0.01              | 0.01             |
| C8      | 1.29                   | 1.29     | 4.08     | 0.01              | 0.01             |
| C9      | 3.65                   | 3.65     | 5.22     | 0.01              | 0.01             |

Analysis begun on: Wed Oct 5 21:20:59 2022  
Analysis ended on: Wed Oct 5 21:21:30 2022  
Total elapsed time: 00:00:31

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