

Stormwater Management Report and Servicing Brief

Proposed 8- Storey Multi-Unit Building 424 Churchill Avenue, Ottawa, ON

Prepared for:

Churchill Properties Inc. 145 Select Avenue Unit 5, Toronto ON M1V 5M8

Attention: Jemmy Taing

LRL File No.: 220224

Rev. Oct 18, 2024 July 16, 2024

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1 INTRODUCTION AND SITE DESCRIPTION

LRL Associates Ltd. was retained by Churchill Properties Inc to complete a Stormwater Management Analysis and Servicing Brief for the development of a 7-storey condo building with 2 level of underground garage parking. Part of the work will include the demolition of a one-storey commercial building located on the site.

The subject property consists of one (1) lot with an existing one-storey commercial building. The lot is legally described as being part of Lot 1 and Part of Lot 2 (South Danforth Avenue) Registered Plan 204, in the City of Ottawa. The subject lot is zoned TM H (24) (Traditional Mainstreet Zone).



Figure 1: Aerial View of Subject Lands

The subject property is irregular shaped and measures approximately 55m in frontage along Danforth Avenue, 25.5m along Churchill Avenue and 50m along Byron Avenue. The total site area is approximately **0.101 Ha**.

The proposed development will be constructed in a single phase, which includes the demolition of the existing one-storey commercial building and the construction of the 7-storey condo building. Refer to *Site Plan* included in *Appendix F* for more details.

This report has been prepared in consideration of the terms and conditions noted above and with the civil drawings prepared for the new development. Should there be any changes in the design features, which may relate to the stormwater and servicing considerations, LRL Associates Ltd. should be advised to review the report recommendations.

2 EXISTING SITE AND DRAINAGE DESCRIPTION

The subject site measures **0.101 ha** and currently consists of a one-storey commercial building with associated asphalt parking and entrances, located along Byron Avenue and Churchill Avenue. The asphalt surface of the site is generally flat and slopes towards the North and East property lines. At the Northwest corner of the site there is a steep slope with tree cover that slopes down to Danforth Avenue. There is a drop of approximately 1m along the East property line, from the Southeast site corner and sloping down along Churchill Avenue towards Danforth Avenue. There is also a drop of approximately 6m along the northwest property line of the site, from the North property line down to Danforth Avenue. To accommodate for this drop there is an existing retaining wall which wraps around the northeast corner of the site and runs primarily along the North property line of the site. Part of the retaining wall is located just outside of the property line and part of it runs across the site along the treed area.

Sewer and watermain mapping, along with as-built information collected from the City of Ottawa indicate the following existing infrastructure located within the adjacent right-of-ways:

Churchill Avenue N:

- 300mm PVC sanitary sewer (2010)
- 300mm CONC storm sewer (2010)
- 400mm PVC watermain (2010)

Danforth Avenue:

- 225mm CONC sanitary sewer (1940)
- 150mm DI watermain (1984)

3 SCOPE OF WORK

As per applicable guidelines, the scope of work includes the following:

Stormwater management

- Calculate the allowable stormwater release rate.
- Calculate the anticipated post-development stormwater release rates.
- Demonstrate how the target quantity objectives will be achieved.

Water services

- Calculate the expected water supply demand at average and peak conditions.
- Calculate the required fire flow as per the Fire Underwriters Survey (FUS) method.
- Confirm the adequacy of water supply and pressure during peak flow and fire flow.
- Describe the proposed water distribution network and connection to the existing system.

Sanitary services

- Describe the existing sanitary sewers available to receive wastewater from the building.
- Calculate peak flow rates from the development.

- Describe the proposed sanitary sewer system.
- Review impact of increased sanitary flow on downstream sanitary sewer.

4 **REGULATORY APPROVALS**

An MECP Environmental Compliance Approval is not expected to be required for installation of the proposed storm and sanitary sewers within the site. A Permit to Take Water is not anticipated to be required for pumping requirements for sewer installation. The Rideau Valley Conservation Authority will need to be consulted to obtain municipal approval for site development. No other approval requirements from other regulatory agencies are anticipated.

5 WATER SUPPLY AND FIRE PROTECTION

5.1 Existing Water Supply Services and Fire Hydrant Coverage

The subject property lies within the City of Ottawa 1W water distribution network pressure zone. There is an existing 400 mm PVC watermain within Churchill Avenue N and a 150mm PVC watermain in Danforth Avenue. There are currently seven (7) existing fire hydrants within proximity to the subject property. Refer to *Appendix B* for the location of fire hydrants.

5.2 Water Supply Servicing Design

According to the City of Ottawa Water Distribution Guidelines (Technical Bulletin ISDTB-2014-02), since the subject site is anticipated to house more than 50 residential units, it is required to be serviced by two water service laterals, separated by an isolation valve, for redundancy and to avoid creation of a vulnerable service area. Additionally, considering the presence of automatic sprinkler system inside the building and a recommended size to service the sprinkler system, the subject property is proposed to be serviced via two (2) 150 mm diameter service laterals connected to the existing 406mm PVC watermain within Churchill Ave and the 152mm DI watermain located in Danforth Ave. Refer to *Site Servicing Plan* C.401 in *Appendix E* for servicing layout and connection points.

We have analyzed the water demand requirements for the proposed 7-storey condo building. The residential water demands, and anticipated population were determined using Appendix 4-A, Table 4.1 and Table 4.2 from the *City of Ottawa Water Distribution Design Guidelines* and Table 3-3 from the *MOE Design Guidelines for Drinking Water Systems*.

Through reviewing the architectural floor plans of the proposed building, it was determined that the building will have a total combined floorspace of **7,818 m**², **58** residential units, **1,670 m**² of amenity space and **3** office spaces.

The water supply requirements for the residential units, office spaces and amenity space in the proposed development have been calculated using the following formulas:

 $Q = (q \times P \times M)$, for the residential and office spaces and $Q = (q \times A \times M)$, for the amenity space.

Where:

q = average water consumption (L/capita/day) or (L/ha/day)
 P = design population (capita)
 M = Peak factor

A = area (ha)

Residential

The proposed building will include **52** one-bedroom units and **6** two-bedroom units. Based on the City of Ottawa Design guidelines for population projection, this translates to approximately **85.4** residents. *Table 1* below summarizes the proposed residential population count as interpreted using Table 4-1 from the City of Ottawa Water Distribution Design Guideline.

| Proposed Unit Type | Persons Per Unit | Number of Units | Total Population | |
|--------------------|------------------|-----------------|------------------|--|
| 1 Bedroom | 1.4 | 52 | 72.8 | |
| 2 Bedroom | 2.1 | 6 | 12.6 | |
| | Total | 58 | 85.4 | |

Table 1: Development Residential Population Estimate

With reference to *Table 4.1 of the City of Ottawa Water Distribution Design Guidelines*, an average water consumption rate of 280 L/c/d was used. With reference to Table 3-3 of the MOE *Design Guidelines for Drinking Water Systems* a Maximum Daily Demand Factor and Maximum Hour Demand Factor were calculated to be 7.2 and 10.9, respectively. The anticipated residential demands were calculated as follows:

- > Average daily domestic water demand is **0.28** L/s,
- > Maximum daily demand is 2.00 L/s, and
- > Maximum hourly demand is **3.01** L/s.

Commercial/Institutional

Appendix 4-A and *Table 4.2 of the City of Ottawa Water Distribution Design Guidelines* were used to determine the consumption rates and peak factors of the amenity and office spaces. A water consumption rate of 75L/p/d was used for office employees and a consumption rate of 28,000L/ha/d was used for the amenity space. The Maximum Daily Demand Factor and the Maximum Hourly Demand Factor were 1.5 and 1.8 respectively. *Table 2* below summarizes the proposed institutional/ commercial demands.

| Property Type | Unit | Rate | Units | Demand (L/d) |
|---------------|--------|--------|-----------|--------------|
| Office | 75 | L/p/d | 3 people | 225.0 |
| Amenity Space | 28,000 | L/ha/d | 0.0167 ha | 467.6 |

| Table 2: Institutional/ | Commercial Demands |
|-------------------------|--------------------|
|-------------------------|--------------------|

Using the peak factors, the anticipated institutional and commercial demands were calculated as follows:

- > Average daily domestic water demand is **0.008** L/s,
- > Maximum daily demand is **0.012** L/s, and
- > Maximum hourly demand is **0.022**L/s.

Combined - Residential/Commercial/Institutional

The combined peak factors for the site are anticipated to equal the following:

- > Average daily domestic water demand is 0.28 L/s,
- > Maximum daily demand is **2.01** L/s, and
- > Maximum hourly demand is **3.03** L/s.

Refer to *Appendix B* for water demand calculations.

The City of Ottawa was contacted to obtain boundary conditions associated with the estimated water demand, as indicated in the boundary request correspondence included in *Appendix B*. *Table 3* below summarizes boundary conditions for the proposed development.

| Design Parameter | Anticipated | Boundary Conditions @ Churchill Ave & Danforth Ave | | |
|---|--------------|---|---------------------------------|--|
| | Demand (L/s) | Connection 1* (m H2O / kPa) | Connection 2** (m H2O / kPa) | |
| Average Daily Demand | 0.28 | 41.21 / 404.13 | 44.04 / 431.88 | |
| Max Day + Max Fire Flow (per FUS) | 2.01 + 216.7 | 35.61 / 349.22 | 15.04 / 147.49 | |
| Peak Hour | 3.03 | 35.01 / 343.33 | 37.84 / 371.08 | |
| *Ground Elevation assumed at 73.69m for Connection 1 @ Churchill Ave | | | | |
| ** Ground Elevation assumed at 70.86m for Connection 2 @ Danforth Ave | | | | |

Table 3: Summary of Boundary Conditions

As indicated in Table 3, pressures in all scenarios meet the required pressure range stated in the City of Ottawa Design Guidelines – Water Distribution (Section 4.2.2). Refer to *Appendix B* for Boundary Conditions.

The estimated fire flow for the proposed buildings was calculated in accordance with *ISTB-2018-02*. The following parameters were provided by the Architect:

- Type of construction Non-combustible construction
- Occupancy type Limited Combustible
- Sprinkler Protection Fully Automatic Sprinkler System

The estimated fire flow demand was estimated to be **13,000** L/min, see Appendix B for details.

There are six (6) existing fire hydrants in proximity to the proposed buildings that are available to provide the required fire flow demands of 13,000 L/min. Refer to **Appendix G** for fire hydrant locations. The proposed development has been reviewed in the context of the location of the surrounding fire hydrants. Given the surrounding layout of the fire hydrants, these hydrants are accessible to fight fire at the subject property. Table 4 below summarizes the aggregate fire flow of the contributing hydrants in proximity to the proposed development based on Table 18.5.4.3 of *ISTB-2018-02*.

| | Max. Fire | Fire | Fire | Available |
|-----------------------------|-------------|-------------|-------------|--|
| | Flow Demand | Hydrants(s) | Hydrant(s) | Combined Fire |
| | (L/min) | within 75m | within 150m | Flow (L/min) |
| Contemplated Development | 13,000 | 2 | 4 | (2 x 5678) + (4 x 3785) = 26,496 |

 Table 4: Fire Protection Summary Table

The total available fire flow from contributing hydrants is equal to **26,496 L/min** which is sufficient to provide adequate fire flow for the proposed development. A certified fire protection system specialist will need to be employed to design the building's fire suppression system and confirm the actual fire flow demand.

The proposed water supply design conforms to all relevant City Guidelines and Policies.

6 SANITARY SERVICE

6.1 Existing Sanitary Sewer Services

There is an existing 300mm PVC Sanitary sewer located in Churchill Ave N and a 225mm CONC Sanitary Sewer located in Danforth Ave. It is anticipated that the contemplated development will be connected to the existing 3000mm PVC sanitary sewer located within Churchill Ave N, to be connected to the proposed building.

6.2 Sanitary Sewer Servicing Design

The proposed development will be serviced via a 150 mm dia. sanitary service connected to the existing 300mm diameter sanitary sewer within Churchill Avenue N. Refer to LRL drawing C.401, included in **Appendix F**, for the proposed sanitary servicing.

The parameters used to calculate the anticipated sanitary flows are residential average population per unit of 1.4 person for single units, 2.1 persons for two-bedroom units and a residential daily demand of 280 L/p/day, a residential peaking factor of 3.5 and a total infiltration rate of 0.33 L/s/ha. Based on these parameters and the total site area of 0.101 ha, the total anticipated wet wastewater flow was estimated to be **1.04 L/s**. Refer to *Appendix C* for the site sanitary sewer design sheet.

As requested in the pre-consultation with City staff, the calculated sanitary demands for the proposed development were coordinated with the City of Ottawa to confirm there is sufficient capacity in the downstream municipal sewers. As per correspondence attached, see *Appendix C*, the downstream municipal sewers can sufficiently accommodate the increase in sanitary flows from the proposed development.

7 STORMWATER MANAGEMENT

7.1 Existing Stormwater Infrastructure

The subject property is tributary to the Ottawa River West sub-watershed. Stormwater runoff from the subject property is tributary to the City of Ottawa sewer system as such, approvals for the proposed development within this area are under the approval authority of the City of Ottawa.

There is an existing 300mm CONC storm sewer available in Churchill Avenue N. In the predevelopment conditions, drainage from the subject lot is depicted by existing watershed EWS-01 (0.101ha), which drains towards the North and West property lines. Refer to plan C701 included in **Appendix E** for pre-development drainage characteristics. Refer to **Appendix D** for predevelopment and post-development watershed information.

7.2 Design Criteria

The stormwater management criteria for this development are based on the pre-consultation with City of Ottawa officials, the City of Ottawa Sewer Design Guidelines including City of Ottawa Stormwater Management Design Guidelines, 2012 (City standards), as well as the Ministry of the Environment's Stormwater Management Planning and Design Manual, 2003 (SWMP Manual).

7.2.1 Water Quality

The subject property lies within the Ottawa River West sub-watershed and is therefore subject to review by the Rideau Valley Conservation Authority (RVCA). It was determined that water quality controls would not be required on this site as treatment would be handled by municipal infrastructure. Correspondence with RVCA is included in *Appendix A*.

7.2.2 Water Quantity

Based on pre-consultation with the City, correspondence included in *Appendix A*, the following stormwater management requirements were identified for the subject site:

- Meet an allowable release rate based on a Rational Method Coefficient of 0.50, employing the City of Ottawa IDF parameters for a 2-year storm with a calculated time of concentration equal to 10 minutes; and
- > Attenuate all storms up to and including the City of Ottawa 100-year storm event on site.
- Water quality treatment will not be required on this site as the water being collected and conveyed to the storm system is rooftop water.

As per the pre-application consultation meeting with the City of Ottawa, it was recommended that it would be acceptable to control only the roof portion of the building up to the 100-year storm event, to a 2-year pre-development level and that the remainder of the site could be left uncontrolled as long as the uncontrolled portion is directed towards the right of way. Based on these stormwater objectives for the subject site, it was determined that the allowable release rate for the site is **10.81 L/s** for all storms up to and including the 100-year storm. Refer to **Appendix D** for calculations.

7.3 Method of Analysis

The Modified Rational Method has been used to calculate the runoff rate from the site to quantify the detention storage required for quantity control of the development. Refer to *Appendix D* for storage calculations.

7.4 Proposed Stormwater Quantity Controls

The proposed stormwater management quantity control for this development will be accomplished using rooftop storage and roof drains with controls. A proposed 250mm diameter PVC storm sewer pipe will outlet stormwater flows from the site to the existing 300mm PVC storm sewer located within Churchill Avenue N. An additional 150mm diameter PVC storm sewer is proposed to outlet stormwater flows from the foundation drain directly to the existing 300mm PVC storm sewer located within Churchill Avenue N. The foundation drain outlet will have a backflow prevention device at the connection to the building and will be equipped with a sump pump as well as a backup pump and backup power source to ensure flow from the foundation level reaches elevation at the city sewer. Pumping details are to be designed by the mechanical engineer and provided at the Building permit stage. The proposed servicing layout and connection points are shown on drawing C.401 in *Appendix E*, and detailed calculations can be found in *Appendix D*.

The site has been analyzed and six (6) post-development watersheds have been allocated.

WS-01 to WS-05 (0.070 ha) consist of the proposed building's roof envelope and will be captured via roof drains with controls.

WS-06 (0.031 ha) is uncontrolled and consists of the remainder of the site that is not part of the roof. Runoff from this area will be directed to the City Right of Way.

Refer to C601, Stormwater Management Plan and C702, Post-Development Watershed Plan C702 in *Appendix E* for reference.

Table 5 below summarizes post-development drainage areas. Calculations can be seen in *Appendix D.*

| WATERSHED C = 0.90 Building Area/ Asphalt & Concrete (m ²) | Total Area (ha) | Weighted Runoff Coefficient (C) |
|---|-----------------|------------------------------------|
|---|-----------------|------------------------------------|

| WS-01(ROOF) | 116.29 | 0.012 | 0.90 |
|--------------------------|--------|-------|------|
| WS-02 (ROOF) | 141.44 | 0.014 | 0.90 |
| WS-03 (ROOF) | 248.09 | 0.025 | 0.90 |
| WS-04 (ROOF) | 62.07 | 0.006 | 0.90 |
| WS-05 (ROOF) | 130.54 | 0.013 | 0.90 |
| WS-06(UN- CONTROLLED) | 313.97 | 0.031 | 0.90 |
| TOTAL | 1012.4 | 0.101 | 0.90 |

The proposed building's rooftop was analysed, and it was determined that there would be $33.53m^3$ of roof storage available. A total of **ten (10)** roof drains would be used, each roof drain would have a restricted discharge rate of **0.63L/s**, resulting in a total release rate from the roof of **6.30 L/s** with a proposed head of 0.15m. The proposed roof drains are to be fully closed WATTS Adjustable Accutrol RD-100-A1. For calculations for available area of rooftop storage and for more information regarding the selected roof drain and flow restrictor, refer to **Appendix D**. For additional details on the roof storage areas refer to drawing *C.601* in **Appendix E**.

Table 6 below summarizes the release rates and storage volumes required to meet the allowable release rate of **10.81 L/s** for 100-year flow rates.

| CATCHMENT AREAS | DRAINAGE AREAS (ha) | 100-YEAR RELEASE RATE (L/s) | 100-YEAR REQUIRED STORAGE (m ³) | TOTAL AVAILABLE STORAGE (m ³) |
|----------------------|------------------------|--------------------------------|--|--|
| WS-01(ROOF) | 0.012 | 1.26 | 3.15 | 6.03 |
| WS-02 (ROOF) | 0.014 | 1.26 | 4.23 | 4.55 |
| WS-03 (ROOF) | 0.025 | 1.26 | 9.46 | 13.17 |
| WS-04 (ROOF) | 0.006 | 1.26 | 1.09 | 3.14 |
| WS-05 (ROOF) | 0.013 | 1.26 | 3.76 | 6.64 |
| TOTAL CONTROLLED | 0.070 | 6.30 | 21.69 | 33.53 |
| WS-06 (UNCONTROLLED) | 0.031 | 15.59 | 0 | 0 |
| TOTAL UNCONTROLLED | 0.031 | 15.59 | 0.00 | 0.00 |
| TOTAL | 0.101 | 21.89 | 21.68 | 33.53 |

Table 6: Stormwater Release Rate & Storage Volume Summary (100 Year)

To attenuate flows to the allowable release rate of **10.81 L/s**, it is calculated that a total of **19.53** m^3 of storage will be required on the roof top. The required storage is proposed to be met via the building rooftop ponding. The total required storage, storage available and allowable release rate is the following;

- 19.53 m³ is required for rooftop storage in WS-01 corresponding to a maximum restricted flow of 6.30 L/s via roof drain controls;
- > There is **33.53** m^3 of available rooftop storage.

The 100-year maximum ponding extents can be found on drawing "C601 – Stormwater Management Plan" in *Appendix E*.

8 EROSION AND SEDIMENT CONTROL

During construction, erosion and sediment controls will be provided primarily via a sediment control fence to be erected along the perimeter of the site where runoff has the potential of leaving the site. Inlet sediment control devices are also to be provided in any catch basin and/or manholes in and around the site that may be impacted by the site construction. Construction and maintenance requirements for erosion and sediment controls are to comply with Ontario Provincial Standard Specification OPSS 577. For more details refer to drawing C101 Erosion and Sediment Control Plan in *Appendix E*.

9 CONCLUSION

This Stormwater Management and Servicing Report for the development proposed at 424 Churchill Avenue N presents the rationale and details for the servicing requirements for the subject property.

In accordance with the report objectives, the servicing requirements for the development are summarized below:

Water Service

- The maximum required fire flow was calculated to be **13,000 L/min** using the FUS method.
- There are six (6) existing fire hydrants available to service the proposed development. They will provide a combined fire flow of **26,496 L/min** to the site.
- The new development will be serviced via two (2) 150mm diameter services connected to the existing 406mm PVC watermain within Churchill Ave N and the 152mm DI watermain located in Danforth Ave.
- Boundary conditions received from the City of Ottawa indicate that sufficient pressure is available to service the proposed site.

Sanitary Service

- The total calculated wet wastewater flow from the proposed development is 1.04 L/s.
- The proposed development will discharge **1.04 L/s** to the existing 300 mm PVC sanitary sewer within Churchill Avenue N via a proposed 150mm PVC sanitary service lateral.

Stormwater Management

- The stormwater release rates from the proposed development will meet the calculated allowable release rate of **10.81L/s.**
- As per the pre-application consultation meeting with the City of Ottawa, only the roof portion of the building will be controlled up to the 100-year storm event, to a 2-year predevelopment level and the remainder of the site will be left uncontrolled and will be directed towards the right of way
- The site stormwater quantity control objectives will be met through ponding on the roof. 21.69m³ of storage will be required and there will be **33.53m³** of available rooftop storage.

Ten (10) area drains will be used to control the flows to 0.63L/s each, which when combined will produce a controlled 100-year release rate of 6.30L/s.

• The roof drains will each be WATTS Adjustable Accutrol RD-100-A1 that are fully closed.

10 REPORT CONDITIONS AND LIMITATIONS

The report conclusions are applicable only to this specific project described in the preceding pages. Any changes, modifications or additions will require a subsequent review by LRL Associates Ltd. to ensure the compatibility with the recommendations contained in this document.

If you have any questions or comments, please contact the undersigned.

Prepared by: LRL Associates Ltd.

Tamara Harb, EIT, SPESC-IT Civil Designer



Virginia Johnson, P. Eng. Civil Engineer

APPENDIX A

Pre-consultation / Correspondance

Tamara Harb

| From: | Bakhit, Reza <reza.bakhit@ottawa.ca></reza.bakhit@ottawa.ca> |
|--------------|--|
| Sent: | September 22, 2022 7:37 AM |
| То: | Tamara Harb |
| Cc: | Amr Salem |
| Subject: | RE: LRL220224 - CIV 7-Storey Condo Redevelopment Boundary Conditions Request (Water and Sanitary) |
| Attachments: | 424 Churchill Avenue September 2022.pdf |

Hi,

The following are boundary conditions, HGL, for hydraulic analysis at 424 Churchill Avenue (zone 1W) assumed to be connected to the 406 mm watermain on Churchill Avenue and the 152 mm on Danforth Avenue (see attached PDF for location).

Both Connections:

Minimum HGL: 108.7 m

Maximum HGL: 114.9 m

Max Day + Fire Flow (216.7 L/s): 109.3 m (Churchill Connection) and 85.9 m (Danforth connection)

These are for current conditions and are based on computer model simulation.

Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation.

Reza Bakhit, P.Eng, C.E.T Project Manager Planning, Real Estate and Economic Development Department / Direction générale de la planification, des biens immobiliers et du développement économique Development Review - Centeral Branch City of Ottawa | Ville d'Ottawa 110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1 613.580.2424 ext./poste 19346, <u>reza.bakhit@ottawa.ca</u> Please note: Given the current pandemic, I will be working from home until further notice; reaching me by email is the easiest. I will be checking my voicemail, just not as frequently as I normally would be.

From: Tamara Harb <tharb@lrl.ca>
Sent: Wednesday, September 07, 2022 11:03 AM
To: Bakhit, Reza <reza.bakhit@ottawa.ca>
Cc: Amr Salem <asalem@lrl.ca>
Subject: LRL220224 - CIV 7-Storey Condo Redevelopment Boundary Conditions Request (Water and Sanitary)

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Tamara Harb

| From: | Bakhit, Reza <reza.bakhit@ottawa.ca></reza.bakhit@ottawa.ca> |
|----------|--|
| Sent: | September 19, 2022 7:36 AM |
| То: | Tamara Harb |
| Cc: | Amr Salem |
| Subject: | RE: LRL220224 - CIV 7-Storey Condo Redevelopment Boundary Conditions Request (Water and Sanitary) |

Hi Tamara,

Not sure if I sent you this email, but just in case, please note that there is no concern with the proposed SAN flow .

Thanks,

Reza Bakhit, P.Eng, C.E.T Project Manager Planning, Real Estate and Economic Development Department / Direction générale de la planification, des biens immobiliers et du développement économique Development Review - Centeral Branch City of Ottawa | Ville d'Ottawa 110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1 613.580.2424 ext./poste 19346, <u>reza.bakhit@ottawa.ca</u> Please note: Given the current pandemic, I will be working from home until further notice; reaching me by email is the easiest. I will be checking my voicemail, just not as frequently as I normally would be.

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Sent: Wednesday, September 07, 2022 11:03 AM
To: Bakhit, Reza <reza.bakhit@ottawa.ca>
Cc: Amr Salem <asalem@lrl.ca>
Subject: LRL220224 - CIV 7-Storey Condo Redevelopment Boundary Conditions Request (Water and Sanitary)

CAUTION: This email originated from an External Sender. Please do not click links or open attachments unless you recognize the source.

ATTENTION : Ce courriel provient d'un expéditeur externe. Ne cliquez sur aucun lien et n'ouvrez pas de pièce jointe, excepté si vous connaissez l'expéditeur.

Good morning Reza,

I would like to request boundary conditions for the development of a 7-storey condo building located at 424 Churchill Ave, Ottawa ON.

Water Connection

We are proposing two water service laterals connected to the existing 400mm municipal watermain in Churchill Avenue and the existing 150mm municipal watermain in Danforth Avenue. Please provide the boundary conditions for the proposed building using the following proposed development demands:

• Type of development: 7 Storey condo building with 2 levels of underground parking and 58 units

(52 one-bedroom & 6 two-bedroom)

| From: | Bakhit, Reza |
|--------------|---|
| То: | Gauthier, Steve |
| Subject: | PC2022-0016 Pre-application Consultation Meeting 424 Churchill Avenue N |
| Date: | Tuesday, March 8, 2022 4:48:37 PM |
| Attachments: | oledata.mso |
| | image021.png |
| | image001.emz |
| | image003.png |

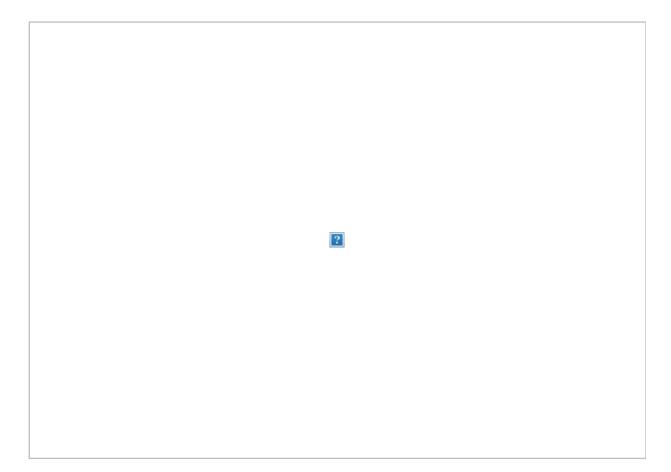
Hi Steve

Please forward the below information to the applicant regarding a development proposal at **424 Churchill Avenue N, Ottawa for the 9 story apartment building.** Note that the information is considered **preliminary** and the assigned Development Review Project Manager may modify and/or add additional requirements and conditions upon review of an application if deemed necessary.

General:

- It is the sole responsibility of the consultant to investigate the location of existing underground utilities in the proposed servicing area and submit a request for locates to avoid conflict(s). The location of existing utilities and services shall be documented on an Existing Conditions Plan.
- Any easements on the subject site shall be identified and respected by any development proposal and shall adhere to the conditions identified in the easement agreement. A legal survey plan shall be provided and all easements shall be shown on the engineering plans.
- A deep excavation and dewatering operations have the potential to cause damages to the neighboring adjacent buildings/ City infrastructure. Document that construction activities (excavation, dewatering, vibrations associated with construction, etc.) will not have an impact on any adjacent buildings and infrastructure.
- A Record of Site Condition (RSC) in accordance with O.Reg. 153/04 will be required to be filed and acknowledged by the Ministry prior to issuance of a building permit due to a change to a more sensitive property use.
- 0. Reference documents for information purposes :
 - Ottawa Sewer Design Guidelines (October 2012)
 - Technical Bulletin PIEDTB-2016-01
 - Technical Bulletins ISTB-2018-01, ISTB-2018-02 and ISTB-2018-03.
 - Ottawa Design Guidelines Water Distribution (2010)
 - Technical Bulletin ISTB-2021-03
 - Geotechnical Investigation and Reporting Guidelines for Development Applications in the City of Ottawa (2007)
 - City of Ottawa Slope Stability Guidelines for Development Applications (revised 2012)
 - City of Ottawa Environmental Noise Control Guidelines (January 2016)
 - City of Ottawa Accessibility Design Standards (2012) (City recommends development be in accordance with these standards on private property)
 - Ottawa Standard Tender Documents (latest version)
 - Ontario Provincial Standards for Roads & Public Works (2013)
 - Record drawings and utility plans are also available for purchase from the City (Contact the City's Information Centre by email at <u>InformationCentre@ottawa.ca</u> or by phone at (613) 580-424 x.44455).

Please note that this is the applicant responsibility to refer to the latest applicable guidelines while preparing reports and studies.



Disclaimer:

The City of Ottawa does not guarantee the accuracy or completeness of the data and information contained on the above image(s) and does not assume any responsibility or liability with respect to any damage or loss arising from the use or interpretation of the image(s) provided. This image is for schematic purposes only.

Stormwater Management Criteria and Information:

- Water Quantity Control: In the absence of area specific SWM criteria please control postdevelopment runoff from the subject site, up to and including the 100-year storm event, to a 2-year pre-development level. The pre-development runoff coefficient will need to be determined as per existing conditions but in no case more than 0.5. [If 0.5 applies it needs to be clearly demonstrated in the report that the pre-development runoff coefficient is greater than 0.5]. The time of concentration (T_c) used to determine the pre-development condition should be calculated. *Tc should not be less than 10 min. since IDF curves become unrealistic at less than 10 min; T_c of 10 minutes shall be used for all post-development calculations].*
- Any storm events greater than the established 2-year allowable release rate, up to and including the 100-year storm event, shall be detained on-site. The SWM measures required to avoid impact on downstream sewer system will be subject to review.
- Please note that foundation drainage is to be independently connected to sewer main unless being pumped with appropriate back up power, sufficient sized pump and back flow prevention. It is recommended that the foundation drainage system be drained by a sump pump connection to the storm sewer to minimize risk of basement flooding as it will provide the best protection from the uncontrolled sewer system compared to relying on the backwater valve.

Water Quality Control: Please consult with the local conservation authority (RVCA) regarding water quality criteria prior to submission of a Site Plan Control Proposal application to establish any water quality control restrictions, criteria and measures for the site. Correspondence and clearance shall be provided in the Appendix of the report.

- Please note that as per Technical Bulletin PIEDTB-2016-01 section 8.3.11.1 (p.12 of 14) there shall be no surface ponding on private parking areas during the 5-year storm rainfall event.
- If Underground Storage proposed: Please note that the Modified Rational Method for storage computation in the Sewer Design Guidelines was originally intended to be used for above ground storage (i.e. parking lot) where the change in head over the orifice varied from 1.5 m to 1.2 m (assuming a 1.2 m deep CB and a max ponding depth of 0.3 m). This change in head was small and hence the release rate fluctuated little, therefore there was no need to use an average release rate.

When underground storage is used, the release rate fluctuates from a maximum peak flow based on maximum head down to a release rate of zero. This difference is large and has a significant impact on storage requirements. We therefore require that an average release rate equal to 50% of the peak allowable rate shall be applied to estimate the required volume. Alternatively, the consultant may choose to use a submersible pump in the design to ensure a constant release rate.

In the event that there is a disagreement from the designer regarding the required storage, The City will require that the designer demonstrate their rationale utilizing dynamic modelling, that will then be reviewed by City modellers in the Water Resources Group.

Please provide information on UG storage pipe. Provide required cover over pipe and details, chart of storage values, capacity etc. How will this pipe be cleaned of sediment and debris?

Provide information on type of underground storage system including product name and model, number of chambers, chamber configuration, confirm invert of chamber system, top of chamber system, required cover over system and details, interior bottom slope (for self-cleansing), chart of storage values, length, width and height, capacity, entry ports (maintenance) etc.

Provide a cross section of underground chamber system showing invert and obvert/top, major and minor HWLs, top of ground, system volume provided during major and minor events. UG storage to provide actual 2- and 100-year event storage requirements.

In regard to all proposed UG storage, ground water levels (and in particular HGW levels) will need to be reviewed to ensure that the proposed system does not become surcharged and thereby ineffective.

Modeling can be provided to ensure capacity for both storm and sanitary sewers for the proposed development by City's Water Distribution Dept. – Modeling Group, through PM and upon request.

- Please note that the minimum orifice dia. for a plug style ICD is 83mm and the minimum flow rate from a vortex ICD is 6 L/s in order to reduce the likelihood of plugging.
- Post-development site grading shall match existing property line grades in order to minimize disruption to the adjacent residential properties. A topographical plan of survey shall be provided as part of the submission and a note provided on the plans.
- Please provide a Pre-Development Drainage Area Plan to define the pre-development drainage areas/patterns. Existing drainage patterns shall be maintained and discussed as part of the proposed SWM solution.
- If rooftop control and storage is proposed as part of the SWM solutions sufficient details (Cl. 8.3.8.4) shall be discussed and document in the report and on the plans. Roof drains are to be connected downstream of any incorporated ICDs within the SWM system and not to the

foundation drain system. Provide a **Roof Drain Plan** as part of the submission.

- Considering the size of the site, it would be acceptable to control the roof portion only (100-year storm event, to a 2-year pre-development level) and leave the remainder of the site uncontrol as long as the uncontrolled portion is directed towards the right of way. This approach should be discussed in the SWM report. Also, the grading plan should clearly demonstrate that the runoff from the uncontrolled portion of the site will be directed towards the ROW
- If Window wells are proposed, they are to be indirectly connected to the footing drains. A
 detail of window well with indirect connection is required, as is a note at window well location
 speaking to indirect connection.
- There must be at least 15cm of vertical clearance between the spill elevation and the ground elevation at the building envelope that is in proximity of the flow route or ponding area. The exception in this case would be at reverse sloped loading dock locations. At these locations, a minimum of 15cm of vertical clearance must be provided below loading dock openings. Ensure to provide discussion in report and ensure grading plan matches if applicable.

Storm Sewer:

• A 300mm dia. CONC storm sewer (2010) is available within Churchill Avenue N.

Sanitary Sewer Maclaren St:

- A 250 mm dia. PVC Sanitary sewer (2010) is available within Churchill Avenue N.
- A 225 mm dia. CONC Sanitary sewer (1940) is available within Danforth Avenue.
- Please provide the new Sanitary sewer discharge and we confirm if sanitary sewer main has the capacity. An analysis and demonstration that there is sufficient/adequate residual capacity to accommodate any increase in wastewater flows in the receiving and downstream wastewater system is required to be provided. Needs to be demonstrated that there is adequate capacity to support any increase in wastewater flow.
- Please apply the wastewater design flow parameters in Technical Bulletin PIEDTB-2018-01.
- Sanitary sewer monitoring maintenance hole is required to be installed at the property line (on the private side of the property) as per City of Ottawa Sewer-Use By-Law 2003-514 (14) *Monitoring Devices*.
- A backwater valve is required on the sanitary service for protection.

Water :

- A 406 mm dia. PVC watermain (2010) is available within Churchill Avenue N.
- A 152 mm dia. DI watermain (1984) is available within Danforth Avenue.
- Existing residential service to be blanked at the main.
- Water Supply Redundancy: Residential buildings with a basic day demand greater than 50m³/day (0.57 L/s) are required to be connected to a minimum of two water services separated by an isolation valve to avoid a vulnerable service area as per the Ottawa Design Guidelines Water Distribution, WDG001, July 2010 Clause 4.3.1 Configuration.
- Please review Technical Bulletin ISTB-2018-0, maximum fire flow hydrant capacity is provided in Section 3 Table 1 of Appendix I. A hydrant coverage figure shall be provided and demonstrate there is adequate fire protection for the proposal. Two or more public hydrants are anticipated to be required to handle fire flow.
- Boundary conditions are required to confirm that the require fire flows can be achieved as well as availability of the domestic water pressure on the City street in front of the development. Use Table 3-3 of the MOE Design Guidelines for Drinking-Water System to determine Maximum Day and Maximum Hour peaking factors for 0 to 500 persons and use Table 4.2 of

the Ottawa Design Guidelines, Water Distribution for 501 to 3,000 persons. Please provide the following information to the City of Ottawa via email to request water distribution network boundary conditions for the subject site. Please note that once this information has been provided to the City of Ottawa it takes approximately 5-10 business days to receive boundary conditions.

- 0. Type of Development and Units
- 1. Site Address
- 2. A plan showing the proposed water service connection location.
- 3. Average Daily Demand (L/s)
- 4. Maximum Daily Demand (L/s)
- 5. Peak Hour Demand (L/s)
- 6. Fire Flow (L/min)

[Fire flow demand requirements shall be based on **Fire Underwriters Survey (FUS)** Water Supply for Public Fire Protection 1999]

[Fire flow demand requirements shall be based on ISTB-2021-03]

<u>Note: The OBC method can be used if the fire demand for the private property is less than 9,000</u> <u>L/min. If the OBC fire demand reaches 9000 L/min, then the FUS method is to be used</u>. Exposure separation distances shall be defined on a figure to support the FUS calculation and required fore flow (RFF).

7. Hydrant capacity shall be assessed to demonstrate the RFF can be

achieved. Please identify which hydrants are being considered to meet the RFF on a fire hydrant coverage plan as part of the boundary conditions request.

Snow Storage:

0. Any portion of the subject property which is intended to be used for permanent or temporary snow storage shall be as shown on the approved site plan and grading plan. Snow storage shall not interfere with approved grading and drainage patters or servicing. Snow storage areas shall be setback from the property lines, foundations, fencing or landscaping a minimum of 1.5m. Snow storage areas shall not occupy driveways, aisles, required parking spaces or any portion of a road allowance. If snow is to be removed from the site please indicate this on the plan(s).

Gas pressure regulating station

A gas pressure regulating station may be required depending on HVAC needs (typically for 12+ units). Be sure to include this on the Grading, Site Servicing, SWM and Landscape plans. This is to ensure that there are no barriers for overland flow routes (SWM) or conflicts with any proposed grading or landscape features with installed structures and has nothing to do with supply and demand of any product.

Regarding Quantity Estimates:

Please note that external Garbage and/or bicycle storage structures are to be added to QE under Landscaping as it is subject to securities. In addition, sump pumps for Sanitary and Storm laterals and/or cisterns are to be added to QE under Hard items as it is subject to securities, even though it is internal and is spoken to under SWM and Site Servicing Report and Plan.

CCTV sewer inspection

CCTV sewer inspection required for pre and post construction conditions to ensure no damage to City Assets surrounding site.

Pre-Construction Survey

Pre-Construction (Piling/Hoe Ramming or close proximity to City Assets) and/or Pre-Blasting (if applicable) Survey required for any buildings/dwellings in proximity of 75m of site and circulation of notice of vibration/noise to residents within 150 m of site. Conditions for Pre-Construction/ Pre-Blast Survey & Use of Explosives will be applied to agreements. Refer to City's Standard S.P. No. F-1201 entitled Use of Explosives, as amended.

Road Reinstatement

Where servicing involves three or more service trenches, either a full road width or full lane width 40 mm asphalt overlay will be required, as per amended Road Activity By-Law 2003-445 and City Standard Detail Drawing R10. The amount of overlay will depend on condition of roadway and width of roadway(s).

Required Engineering Plans and Studies:

PLANS:

- Existing Conditions and Removals Plan
- Site Servicing Plan
- Grade Control and Drainage Plan
- Erosion and Sediment Control Plan
- Roof Drainage Plan (When rooftop storage is proposed)
- Topographical survey

REPORTS:

- Site Servicing and Stormwater Management Report (is required per section 4.7.1, policy 6 and section 4.7.1, policy 23 of the OP
- Geotechnical Study/Investigation (including sensitive marine clays and unstable slopes) is required per section 10.1.4 of OP
- Noise Control Study required as per section 10.2.1
- Phase I ESA 4) A Phase 1 and, where required, a Phase 2 ESA are required per section 10.1.6 OP
- Phase II ESA (Depending on recommendations of Phase I ESA). It appears the site is contaminated.
- RSC (Record of the site Conditions)
- Site lighting certificate
- Wind analysis
- Shadow Study

Please refer to the **City of Ottawa Guide to Preparing Studies and Plans [Engineering]:** Specific information has been incorporated into both the <u>Guide to Preparing Studies and Plans</u> for a site plan. The guide outlines the requirement for a statement to be provided on the plan about where the property boundaries have been derived from.

Added to the general information for servicing and grading plans is a note that an **O.L.S**. should be engaged when reporting on or relating information to property boundaries or existing conditions. The importance of engaging an O.L.S. for development projects is emphasized.

Phase One Environmental Site Assessment:

• A Phase I ESA is required to be completed in accordance with Ontario Regulation 153/04 in

support of this development proposal to determine the potential for site contamination. Depending on the Phase I recommendations a Phase II ESA may be required.

- The Phase I ESA shall provide all the required Environmental Source Information as required by O. Reg. 153/04. ERIS records are available to public at a reasonable cost and need to be included in the ESA report to comply with O.Reg. 153/04 and the Official Plan. The City will not be in a position to approve the Phase I ESA without the inclusion of the ERIS reports.
- Official Plan Section 4.8.4:

https://ottawa.ca/en/city-hall/planning-and-development/official-plan-and-master-plans/officialplan/volume-1-official-plan/section-4-review-development-applications#4-8-protection-health-andsafety

RSC (Record of the site Conditions)

 A RSC is required when changing the land use (zoning) of a property to a more sensitive land use.

Submitting a record of site condition | Ontario.ca

Geotechnical Investigation:

- A Geotechnical Study/Investigation shall be prepared in support of this development proposal.
- Reducing the groundwater level in this area can lead to potential damages to surrounding structures due to excessive differential settlements of the ground. The impact of groundwater lowering on adjacent properties needs to be discussed and investigated to ensure there will be no short term and long term damages associated with lowering the groundwater in this area.
- Geotechnical Study shall be consistent with the Geotechnical Investigation and Reporting Guidelines for Development Applications.

https://documents.ottawa.ca/sites/documents/files/geotech_report_en.pdf

Noise Study:

- A Transportation Noise Assessment is required as the subject development is located within 100m proximity of an Arterial Road
- A Stationary Noise Assessment is required in order to assess the noise impact of the proposed sources of stationary noise (mechanical HVAC system/equipment) of the development onto the surrounding residential area to ensure the noise levels do not exceed allowable limits specified in the City Environmental Noise Control Guidelines.

https://documents.ottawa.ca/sites/default/files/documents/enviro_noise_guide_en.pdf

Wind analysis:

0. A wind analysis must be prepared, signed and stamped by an engineer who specializes in pedestrian level wind evaluation. Where a wind analysis is prepared by a company which do not have extensive experience in pedestrian level wind evaluation, an independent peer review may be required at the expense of the proponent.

Terms of Reference: Wind Analysis (ottawa.ca)

Shadow Study

When greater than 9 storey in height, a Shadow Study required for all buildings/dwellings.

Exterior Site Lighting:

 Any proposed light fixtures (both pole-mounted and wall mounted) must be part of the approved Site Plan. All external light fixtures must meet the criteria for Full Cut-off Classification as recognized by the Illuminating Engineering Society of North America (IESNA or IES), and must result in minimal light spillage onto adjacent properties (as a guideline, 0.5 fc is normally the maximum allowable spillage). In order to satisfy these criteria, the please provide the City with a **Certification (Statement) Letter** from an acceptable professional engineer stating that the design is compliant.

Fourth (4th) Review Charge:

Please be advised that additional charges for each review, after the 3rd review, will be applicable to each file. There will be no exceptions.

Construction approach – Please contact the Right-of-Ways Permit Office <u>TMconstruction@ottawa.ca</u> early in the Site Plan process to determine the ability to construct site and copy File Lead <u>Steve.Gauthier@ottawa.ca</u> on this request.

Please note that these comments are considered <u>preliminary based on the information available</u> to date and therefore maybe amended as additional details become available and presented to the City. It is the responsibility of the applicant to <u>verify the above information</u>. The applicant may contact me for follow-up questions related to engineering/infrastructure prior to submission of an application if necessary.

If you have any questions or require any clarification, please let me know.

Regards,

Reza Bakhit, P.Eng, C.E.T

Project Manager

Planning, Real Estate and Economic Development Department / Direction générale de la planification, des biens immobiliers et du développement économique

Development Review - Centeral Branch

City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1

613.580.2400 ext./poste 19346, reza.bakhit@ottawa.ca

Please note: Given the current pandemic, I will be working from home until further notice; reaching me by email is the easiest. I will be checking my voicemail, just not as frequently as I normally would be.

APPENDIX B

Water Supply Calculations



Water Supply Calculations

LRL File No. 220224 2022-09-07 Prepared by Tamara Harb

Water Demand based on the City of Ottawa Design Guidelines-Water Distribution, 2010

Date

| | Domestic Deman | d | |
|---------------------|------------------|-----------------|------------|
| Unit Type | Persons Per Unit | Number of Units | Population |
| 1 Bedroom Apartment | 1.4 | 52 | 72.8 |
| 2 Bedroom Apartment | 2.1 | 6 | 12.6 |
| | Total | 58 | 85.4 |

*Based on a daily demand of 280L/day per person as identified by Appendix 4-A of the Sewer design guidelines.

| Average Water Consumption Rate | 280 L/ | _/c/d |
|--------------------------------|------------|---------------------------------|
| Average Day Demand | 23,912 L/ | L/d 0.28 L/s |
| Maximum Day Factor | 7.2 | Table (3-3) MOE Peaking Factors |
| Maximum Daily Demand | 172,910 L/ | L/d 2.00 L/s |
| Peak Hour Factor | 10.9 | Table (3-3) MOE Peaking Factors |
| Maximum Hour Demand | 260,015 L/ | L/d 3.01 L/s |

| | Institutional / Commercial / Industria | al Demand | |
|---------------|--|-----------|-----------------|
| Property Type | Unit Rate | Units | Demand (L/d) |
| Office | 75 L/p/d | 3 people | 225.0 |
| Amenities | 28000 L/ha/d | 0.0167 ha | 467.6 |

| Average Day Demand | 693 | L/d | 0.008 | L/s |
|----------------------|---------|------------|----------------------|---------------------|
| Maximum Day Factor | 1.5 | (Design G | uidelines-Water Dist | ribution Table 4.2) |
| Maximum Daily Demand | 1,039 | L/d | 0.012 | L/s |
| Peak Hour Factor | 1.8 | (Design G | uidelines-Water Dist | ribution Table 4.2) |
| Maximum Hour Demand | 1,870 | L/d | 0.022 | L/s |
| | TOTAL I | DEMAND | | |

| Average Day Demand | 24,605 L/d | 0.28 | L/s | |
|----------------------|-------------|------|-----|--|
| Maximum Daily Demand | 173,949 L/d | 2.01 | L/s | |
| Maximum Hour Demand | 261,885 L/d | 3.03 | L/s | |

Water Service Pipe Sizing

Q = VA

Where: V = velocity A = area of pipe Q = flow rate

Assuming a maximum velocity of 1.8m/s, the diameter of pipe is calculated as:

| Minimum pipe diameter (d) = | (4Q/πV) ^{1/2} | |
|------------------------------|------------------------|--------|
| = | 0.046 | m |
| = | 46 | mm |
| Proposed pipe diameter (d) = | 150 | mm |
| = = | 6 | Inches |
| | | |



Fire Flow Calculations

| LRL File No. | 220224 |
|--------------|--------------------------------|
| Date | September 8, 2022 |
| Method | Fire Underwriters Survey (FUS) |
| Prepared by | Tamara Harb |

| Step | Task | Term | Options | Options Multiplier Cho | | Value | Unit | Fire Flow |
|------|------------------------------------|---|--|------------------------|---------------------------------------|-----------------|---|-----------|
| | | | Structural Framing Material | | | | | |
| | | | Wood Frame | 1.5 | | | | |
| | Choose frame used for | Coofficient C | Ordinary Construction | 1.0 | | | | |
| 1 | | related to the type of construction | Non-combustible construction | 0.8 | Non-combustible construction | 0.8 | | |
| | | | Fire resistive construction <2 hrs | 0.7 | | | | |
| | | | Fire resistive construction >2 hrs | | | | | |
| | | | Floor Space Area (A) | | | | | |
| 2 | | | Total area | | | 6,961 | m ² | |
| 3 | Obtain fire flow before reductions | Required fire flow (rounded to nearest 1,000 L/min) | Fire I | Flow = 220 x C | x A ^{0.5} | | 31 m² 31 m² L/min 1 % L/min 1 % L/min 7 % L/min 1 % L/min 1 | 15,000 |
| | : | | Reductions or surcharge due to factors aff | fecting burning |] | | | |
| | | | Non-combustible | -25% | | | | |
| | Chasses combustibility | Occupancy hazard reduction or | Limited combustible | -15% | | | | |
| 4 | | surcharge | Combustible | 0% | Limited combustible | -15% | L/min | 12,750 |
| | | | Free burning | 15% | | | | |
| | | | Rapid burning | 25% | | | | |
| | | | Full automatic sprinklers | -30% | True | -30% | | |
| 5 | Choose reduction for sprinklers | Sprinkler reduction | Water supply is standard for both the system and fire department hose lines | -10% | True | -10% | L/min | 7,650 |
| | | | Fully supervised system | -10% | False | 0% | | |
| | | | North side | >30m | 0% | | | |
| 6 | building relation 2 | Exposure distance between units | West side | 0 to 3m | 25% 10% | | l /min | 13 388 |
| | | | East side | 20.1 to 30m | | | L/11111 | 13,300 |
| | | | South side | 20.1 to 30m | 10% | 45% | | |
| | | | Net required fire flow | | | | | |
| | Obtain fire flow | | | Minimum | required fire flow rate (rounded to n | , | | 13,000 |
| 7 | | | | | Minimum required | | | 216.7 |
| | | | | | Required duration | on of fire flow | 1 m ² 1 m ² L/min 15,00 L/min 12,75 L/min 12,75 L/min 12,75 L/min 13,35 L/min 13,00 L/min 13,00 L/min 13,00 L/min 13,00 L/min 13,00 | 2.75 |

APPENDIX C

Wastewater Collection Calculations



| | | LRL File No Project: Location: Date: | | 220224 CIV 7 Store 424 Church September | ill Avenue | • | ent | | | Light Indu Heavy Ind Maximum | ustrial Flow dustrial Flow n Resident | w = 35000 ow = 5500 tial Peak f | low = 2800) L/ha/day)0 L/ha/da Factor = 4 eak Facto | 00 L/ha y .0 | - | sign Para | Average Daily Flov Industrial | w for Plac Peak Fac | • | oloyment = er Append | = 75L/p/day dix 4-B = 7 | | | Minin | | ity = 0.60 n n = 0.013 |
|--------------------|-------------|---|--------------|--|----------------------|-----------------|---------------|-----------------------|--------------|------------------------------------|---|---------------------------------------|---|---------------------------|--------------|-----------------------|-------------------------------------|------------------------|--------------------------|-------------------------|----------------------------|------------------|---|------------|-------------------------|---------------------------|
| LOC | CATION | | | RESIDENT | IAL AREA | | JLATION | | COMME | ERCIAL | IN | IDUSTRI | AL | 0 | FICE | C+I+I | INF | FILTRATI | ON | TOTAL | | | F | PIPE | | |
| STREET FF | ROM | то | AREA (Ha) | POP. | CUMM AREA (Ha) | ULATIVE POP. | PEAK FACT. | PEAK FLOW (l/s) | AREA (Ha) | ACCU. AREA (Ha) | AREA (Ha) | ACCU. AREA (Ha) | PEAK FACT. | POP | ACCU. POP | PEAK FLOW (l/s) | TOTAL AREA (Ha) | ACCU. AREA (Ha) | INFILT. FLOW (I/s) | TOTAL FLOW (I/s) | LENGT H (m) | DIA. (mm) | SLOPE (%) | MATERIAL | CAP. (FULL) (I/s) | VEL. (FULL) (m/s) |
| Churchill E Ave | Bldg | PROP SAN MH01 | 0.101 | 85.4 | 0.101 | 85.4 | 3.6 | 1.00 | 0.017 | 0.017 | 0.00 | 0.00 | 7.0 | 3.0 | 3.0 | 0.01 | 0.101 | 0.101 | 0.03 | 1.04 | 13.1 | 150 | 2.00% | PVC | 21.54 | 1.22 |
| NOTES Existin | ing inverts | and slopes a | re estima | ted. They are | e to be cor | nfirmed on-si | ite. | | | | |] | | Desigr Check Dwg. I | ТН | • | File Ref.: | | · | • | | torey Cor LOC | OJECT: ndo Rede CATION: rchil Aver | evelopment | | Shee |

APPENDIX D

Stormwater Management Calculations Watts Roof Drain Specification

| | LRL File No. | 220224 |
|--------------------------|--------------------|-----------------------------|
| | Project: | CIV 7-Storey Condo Building |
| | Location: | 424 Churchill Avenue |
| | Date: | April 9, 2023 |
| | Designed: | Tamara Harb |
| ENGINEERING INGÉNIERIE | Drawing Reference: | C701/C702 |

Pre-Development Catchments

| WATERSHED | C = 0.2 | C=0.7 | C = 0.90 | Total Area (m ²) | Total Area (ha) | Combined C |
|-----------|---------|-------|----------|------------------------------|-----------------|------------|
| EWS-01 | 119.4 | 0.0 | 893.0 | 1012.4 | 0.101 | 0.82 |
| TOTAL | 119.4 | 0.0 | 893.0 | 1012.4 | 0.101 | 0.82 |

Post-Development Catchments

| WATERSHED | C = 0.20 | C = 0.70 | C = 0.90 | Total Area (m ²) | Total Area (ha) | Combined C |
|----------------------|----------|----------|----------|------------------------------|-----------------|------------|
| WS-01(ROOF) | 0.00 | 0.00 | 116.29 | 116.29 | 0.012 | 0.90 |
| WS-02 (ROOF) | 0.00 | 0.00 | 141.44 | 141.44 | 0.014 | 0.90 |
| WS-03 (ROOF) | 0.00 | 0.00 | 248.09 | 248.09 | 0.025 | 0.90 |
| WS-04 (ROOF) | 0.00 | 0.00 | 62.07 | 62.07 | 0.006 | 0.90 |
| WS-05 (ROOF) | 0.00 | 0.00 | 130.54 | 130.54 | 0.013 | 0.90 |
| WS-06(UN-CONTROLLED) | 0.00 | 0.00 | 313.97 | 313.97 | 0.031 | 0.90 |
| TOTAL | 0.0 | 0.0 | 1012.4 | 1012.4 | 0.101 | 0.90 |



LRL File No. Project: Location: Date: 220224 CIV 7-Storey Condo Building 424 Churchilll Ave April 9, 2023 Tamara Harb C601 Date: Designed: Drawing Ref.:

Stormwater Management Design Sheet-100 Year

Runoff Equation

- Q = 2.78CIA (L/s) C = Runoff coefficient I = Rainfall intensity (mm/hr) A = Area (ha) = A / (Td + C)^B
- T_c = Time of concentration (min)

Pre-development Stormwater Management - 2 Year Storm

| 2 year storm | = 732.95 / (Td | + 6.199) ^{0.81} a = 732.951 b = 0.810 C = 6.199 |
|--------------|----------------|--|
| C | = 0.50 | max of 0.5 as per City of Ottawa |
| | = 76.8 | mm/hr |
| То | = 10 | min |
| Total Area | = 0.101 | ha |

Allowable Release Rate= 10.81 L/s

Post-development Stormwater Management

| | | | | | ∑R _{2&5} | ∑R ₁₀₀ |
|---------------|-----------------------|-------|----|-----|-----------------------|-------------------|
| | Total Site Area = | 0.070 | ha | ∑R= | | |
| | WS-01(ROOF) | 0.012 | ha | R= | 0.90 | 1.00 |
| | WS-02 (ROOF) | 0.014 | ha | R= | 0.90 | 1.00 |
| Controlled | WS-03 (ROOF) | 0.025 | ha | R= | 0.90 | 1.00 |
| Controlled | WS-04 (ROOF) | 0.006 | ha | R= | 0.90 | 1.00 |
| | WS-05 (ROOF) | 0.013 | ha | R= | 0.90 | 1.00 |
| | Total Controlled | 0.070 | ha | ∑R= | 0.90 | 1.00 |
| Un-controlled | WS-06 (UNCONTROLLED) | 0.031 | ha | R= | 0.90 | 1.00 |
| Un-controlled | Total Un-Controlled = | 0.031 | ha | ∑R= | 0.90 | 1.00 |

| | | | Pos | st-development Stormwa | ter Management (Uncon | rolled Catchment W | <u>/S-06)</u> | |
|-----------------------|---------------------------|----------|-----------------------------|-------------------------|--------------------------|--------------------|---------------|-----------|
| 100 Year Storm Event: | | | | | | | | |
| | I ₁₀₀ = 1735.6 | 88 / (Tc | i + 6.014) ^{0.820} | | a = | 1735.688 | b = 0.820 | C = 6.014 |
| | Inter | nsity | Uncontrolled | Controlled Release Rate | | | | |
| Time (min) | (mm | ı/hr) | Runoff (L/s) | Constant (L/s) | Total Release Rate (L/s) | | | |
| 10 | 178 | 8.6 | 15.59 | 0.00 | 15.59 | | | |
| | | | | • | | | | |



LRL File No. 2202 Project: CIV Location: 424 Date: April Designed: Tam Drawing Ref.: C60

220224 CIV 7-Storey Condo Building 424 Churchilli Ave April 9, 2023 Tamara Harb C601

| Ir | 735.688 / (To Intensity (mm/hr) 178.6 142.9 120.0 103.8 91.9 | L + 6.014) ^{0.820} Controlled Runoff (L/s) | | a = | 1735.688 | h = | 0.820 | 0 - 0 044 |
|--|--|--|--|--|--|---|-------------------------|-----------|
| Time (min) (10 10 15 20 25 30 35 40 45 50 60 70 80 60 | (mm/hr) 178.6 142.9 120.0 103.8 | | | | 1755.000 | D - | 0.820 | C = 6.014 |
| Time (min) (10 10 15 20 25 30 35 40 45 50 60 70 80 60 | (mm/hr) 178.6 142.9 120.0 103.8 | | Storage Required | d Controlled Release Rate | | Total Dalage | 7 | |
| 15 20 25 30 35 40 45 50 60 70 80 | 142.9 120.0 103.8 | | Storage Volume (m ³) | Constant (L/s) | Uncontrolled Runoff (L/s) | Total Release Rate (L/s) | | |
| 20 25 30 35 40 45 50 60 70 80 | 120.0 103.8 | 5.77 | 2.71 | 1.26 | 0.00 | 1.26 | - | |
| 25 30 35 40 45 50 60 70 80 | 103.8 | 4.62 | 3.02 | 1.26 | 0.00 | 1.26 | | |
| 30 35 40 45 50 60 70 80 | | 3.88 | 3.14 | 1.26 | 0.00 | 1.26 | - | |
| 35 40 45 50 60 70 80 | | 3.36 2.97 | <u>3.15</u> 3.08 | 1.26 1.26 | 0.00 | 1.26 1.26 | | |
| 40 45 50 60 70 80 | 82.6 | 2.97 | 2.96 | 1.20 | 0.00 | 1.20 | - | |
| 50 60 70 80 | 75.1 | 2.43 | 2.81 | 1.26 | 0.00 | 1.26 | | |
| 60 70 80 | 69.1 | 2.23 | 2.63 | 1.26 | 0.00 | 1.26 | | |
| 70 80 | 64.0 | 2.07 | 2.42 | 1.26 | 0.00 | 1.26 | | |
| 80 | 55.9 | 1.81 | 1.97 | 1.26 | 0.00 | 1.26 | _ | |
| | 49.8 45.0 | 1.61 1.45 | 1.47 0.93 | 1.26 1.26 | 0.00 | 1.26 | 4 | |
| | 45.0 | 1.45 | 0.93 | 1.20 | 0.00 | 1.26 | 1 | |
| 100 | 37.9 | 1.23 | 0.00 | 1.26 | 0.00 | 1.26 | 1 | |
| 110 | 35.2 | 1.14 | 0.00 | 1.26 | 0.00 | 1.26 |] | |
| 120 | 32.9 | 1.06 | 0.00 | 1.26 | 0.00 | 1.26 | | |
| Maximum Require | ired Roof Sto | Summary of Root prage (100 Year) = Proposed Head = pontrol Flow/Drain = | 3.15 150 0.63 | m ³ mm L/s | *An Emergency over | flow scupper is prov | ided above this height. | |
| | | er of Roof Drains = | 2 | | | | | |
| | | from Roof Drain = | 1.26 | L/s | | | | |
| | | ble Roof Surface = | 116.28 | m ² | | | | |
| | R | oof Drain Model = | WATTS adjustable roof dra | in w/ weir opening-closed | | | | |
| | Total St | orage Required = | 3.15 | m³ | | | | |
| | Availab | e Roof Storage = | 6.03 | m ³ | refer to LRL Plan C6 | 01 | | |
| ar Storm Event: | | | | | | | | |
| | 735.688 / (Td | l + 6.014) ^{0.820} | | a = | 1735.688 | b = | 0.820 | C = 6.014 |
| I ₁₀₀ = 173 | | | Storage Required | d | Ţ | | 0.820 | C = 6.014 |
| I ₁₀₀ = 173 | 735.688 / (Td Intensity (mm/hr) | l + 6.014) ^{0.820} Controlled Runoff (L/s) | Storage Required | | 1735.688 Uncontrolled Runoff (L/s) | b = Total Release Rate (L/s) | 0.820 | C = 6.014 |
| I ₁₀₀ = 173 Time (min) (10 | Intensity (mm/hr) 178.6 | Controlled Runoff (L/s) 7.02 | Storage Volume (m ³) 3.46 | d Controlled Release Rate Constant (L/s) 1.26 | Uncontrolled Runoff (L/s) 0.00 | Total Release Rate (L/s) 1.26 | 0.820 | C = 6.014 |
| I ₁₀₀ = 173 Time (min) (10 15 | Intensity (mm/hr) 178.6 142.9 | Controlled Runoff (L/s) 7.02 5.62 | Storage Volume (m ³) 3.46 3.92 | d Controlled Release Rate Constant (L/s) 1.26 1.26 | Uncontrolled Runoff (L/s) 0.00 0.00 | Total Release Rate (L/s) 1.26 1.26 | 0.820 | C = 6.014 |
| I ₁₀₀ = 173 Time (min) (10 15 20 | Intensity (mm/hr) 178.6 142.9 120.0 | Controlled Runoff (L/s) 7.02 5.62 4.72 | Storage Volume (m ³) 3.46 3.92 4.15 | d Controlled Release Rate Constant (L/s) 1.26 1.26 1.26 | Uncontrolled Runoff (L/s) 0.00 0.00 0.00 | Total Release Rate (L/s) 1.26 1.26 1.26 | 0.820 | C = 6.014 |
| I ₁₀₀ = 173 Time (min) (10 15 20 25 | Intensity (mm/hr) 178.6 142.9 120.0 103.8 | Controlled Runoff (L/s) 7.02 5.62 4.72 4.08 | Storage Volume (m ³) 3.46 3.92 4.15 4.23 | d Controlled Release Rate Constant (L/s) 1.26 1.26 1.26 1.26 | Uncontrolled Runoff (L/s) 0.00 0.00 0.00 0.00 | Total Release Rate (L/s) 1.26 1.26 1.26 1.26 | 0.820 | C = 6.014 |
| I ₁₀₀ = 173 | Intensity (mm/hr) 178.6 142.9 120.0 103.8 91.9 | Controlled Runoff (L/s) 7.02 5.62 4.72 4.08 3.61 | Storage Volume (m³) 3.46 3.92 4.15 4.23 | d Controlled Release Rate Constant (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 | Uncontrolled Runoff (L/s) 0.00 0.00 0.00 0.00 0.00 | Total Release Rate (L/s) 1.26 1.26 1.26 1.26 1.26 | 0.820 | C = 6.014 |
| I ₁₀₀ = 173 Time (min) (10 15 20 25 | Intensity (mm/hr) 178.6 142.9 120.0 103.8 | Controlled Runoff (L/s) 7.02 5.62 4.72 4.08 | Storage Volume (m ³) 3.46 3.92 4.15 4.23 | d Controlled Release Rate Constant (L/s) 1.26 1.26 1.26 1.26 | Uncontrolled Runoff (L/s) 0.00 0.00 0.00 0.00 | Total Release Rate (L/s) 1.26 1.26 1.26 1.26 | 0.820 | C = 6.014 |
| I ₁₀₀ = 173 | Intensity (mm/hr) 178.6 142.9 120.0 103.8 91.9 82.6 | Controlled Runoff (L/s) 7.02 5.62 4.72 4.08 3.61 3.25 | Storage Volume (m ³) 3.46 3.92 4.15 4.23 4.23 4.17 | d Controlled Release Rate Constant (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 | Uncontrolled Runoff (L/s) 0.00 0.00 0.00 0.00 0.00 0.00 | Total Release Rate (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 1.26 | 0.820 | C = 6.014 |
| I ₁₀₀ = 173 | Intensity (mm/hr) 178.6 142.9 120.0 103.8 91.9 82.6 75.1 69.1 64.0 | Controlled Runoff (L/s) 7.02 5.62 4.72 4.08 3.61 3.25 2.95 2.72 2.51 | Storage Volume (m³) 3.46 3.92 4.15 4.23 4.23 4.17 4.07 3.93 3.76 | d Controlled Release Rate Constant (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 | Uncontrolled Runoff (L/s) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0. | Total Release Rate (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 | 0.820 | C = 6.014 |
| I ₁₀₀ = 173 | Intensity (mm/hr) 178.6 142.9 120.0 103.8 91.9 82.6 75.1 69.1 69.1 64.0 55.9 | Controlled Runoff (L/s) 7.02 5.62 4.72 4.08 3.61 3.25 2.95 2.72 2.72 2.51 2.20 | Storage Volume (m ³) 3.46 3.92 4.15 4.23 4.23 4.17 4.07 3.93 3.76 3.38 | d Controlled Release Rate Constant (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 | Uncontrolled Runoff (L/s) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0. | Total Release Rate (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 | 0.820 | C = 6.014 |
| Item Irent 10 (1) 15 (2) 20 (2) 30 (3) 35 (4) 40 (4) 50 (6) 70 (1) | Intensity (mm/hr) 178.6 142.9 120.0 103.8 91.9 82.6 75.1 69.1 64.0 55.9 49.8 | Controlled Runoff (L/s) 7.02 5.62 4.72 4.08 3.61 3.25 2.95 2.72 2.51 2.25 2.20 1.96 | Storage Volume (m ³) 3.46 3.92 4.15 4.23 4.23 4.17 4.07 3.93 3.76 3.38 2.93 | d Controlled Release Rate Constant (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 | Uncontrolled Runoff (L/s) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0. | Total Release Rate (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 | 0.820 | C = 6.014 |
| L ₁₀₀ = 173 | Intensity (mm/hr) 178.6 142.9 120.0 103.8 91.9 82.6 75.1 69.1 64.0 55.9 49.8 45.0 | Controlled Runoff (L/s) 7.02 5.62 4.72 4.08 3.61 3.25 2.95 2.75 2.77 2.51 2.20 1.96 1.77 | Storage Volume (m ³) 3.46 3.92 4.15 4.23 4.23 4.17 4.07 3.93 3.76 3.38 2.93 2.44 | d Controlled Release Rate Constant (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 | Uncontrolled Runoff (L/s) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0. | Total Release Rate (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 | 0.820 | C = 6.014 |
| Interference Interference 10 10 15 20 25 25 30 35 40 45 50 60 70 80 90 90 | Intensity (mm/hr) 178.6 142.9 120.0 103.8 91.9 82.6 75.1 69.1 64.0 55.9 49.8 45.0 41.1 | Controlled Runoff (L/s) 7.02 5.62 4.72 4.08 3.61 3.25 2.95 2.72 2.51 2.20 1.96 1.77 1.62 | Storage Volume (m ³) 3.46 3.92 4.15 4.23 4.23 4.23 4.17 4.07 3.93 3.76 3.38 2.93 2.44 1.93 | d Controlled Release Rate Constant (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 | Uncontrolled Runoff (L/s) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0. | Total Release Rate (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 | 0.820 | C = 6.014 |
| L ₁₀₀ = 173 | Intensity (mm/hr) 178.6 142.9 120.0 103.8 91.9 82.6 75.1 69.1 64.0 55.9 49.8 45.0 | Controlled Runoff (L/s) 7.02 5.62 4.72 4.08 3.61 3.25 2.95 2.75 2.77 2.51 2.20 1.96 1.77 | Storage Volume (m ³) 3.46 3.92 4.15 4.23 4.23 4.17 4.07 3.93 3.76 3.38 2.93 2.44 | d Controlled Release Rate Constant (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 | Uncontrolled Runoff (L/s) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0. | Total Release Rate (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 | 0.820 | C = 6.014 |
| Time (min) Ir 10 (1) 15 (2) 20 (2) 30 (2) 35 (2) 40 (2) 45 (2) 50 (2) 60 (2) | Intensity (mm/hr) 178.6 142.9 120.0 103.8 91.9 82.6 75.1 69.1 64.0 55.9 49.8 | Controlled Runoff (L/s) 7.02 5.62 4.72 4.08 3.61 3.25 2.95 2.72 2.51 2.25 2.20 1.96 | Storage Volume (m ³) 3.46 3.92 4.15 4.23 4.23 4.17 4.07 3.93 3.76 3.38 2.93 | d Controlled Release Rate Constant (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 | Uncontrolled Runoff (L/s) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0. | Total Release Rate (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 | 0.820 | C = 6.014 |



LRL File No. 2 Project: C Location: 4 Date: A Designed: T Drawing Ref.: C

220224 CIV 7-Storey Condo Building 424 Churchilli Ave April 9, 2023 Tamara Harb C601

Post-development Stormwater Management (WS-03 ROOF)

Stormwater Management Design Sheet-100 Year

| | | l + 6.014) ^{0.820} | | a = | 1735.688 | b = 0.820 | C = 6.014 |
|------------|-------------------|---|----------------------------------|----------------------------|----------------------|------------------------------|------------------|
| | ŕ | | | | т | | |
| | Intensity | Controlled | Storage Require | Controlled Release Rate | Uncontrolled | Total Release | |
| Time (min) | (mm/hr) | Runoff (L/s) | Storage Volume (m ³) | Constant (L/s) | Runoff (L/s) | Rate (L/s) | |
| 10 | 178.6 | 12.32 | 6.63 | 1.26 | 0.00 | 1.26 | |
| 15 | 142.9 | 9.86 | 7.74 | 1.26 | 0.00 | 1.26 | |
| 20 | 120.0 | 8.27 | 8.42 | 1.26 | 0.00 | 1.26 | |
| 25 | 103.8 | 7.16 | 8.85 | 1.26 | 0.00 | 1.26 | |
| 30 | 91.9 | 6.34 | 9.14 | 1.26 | 0.00 | 1.26 | |
| 35 | 82.6 | 5.70 | 9.31 | 1.26 | 0.00 | 1.26 | |
| 40 | 75.1 | 5.18 | 9.41 | 1.26 | 0.00 | 1.26 | |
| 45 | 69.1 | 4.76 | 9.46 | 1.26 | 0.00 | 1.26 | |
| 50 | 64.0 | 4.41 | 9.45 | 1.26 | 0.00 | 1.26 | |
| 60 | 55.9 | 3.86 | 9.34 | 1.26 | 0.00 | 1.26 | |
| 70 | 49.8 | 3.43 | 9.13 | 1.26 | 0.00 | 1.26 | |
| 80 | 45.0 | 3.10 | 8.85 | 1.26 | 0.00 | 1.26 | |
| 90 | 41.1 | 2.84 | 8.51 | 1.26 | 0.00 | 1.26 | |
| 100 | 37.9 | 2.61 | 8.13 | 1.26 | 0.00 | 1.26 | |
| 110 | 35.2 | 2.43 | 7.71 | 1.26 | 0.00 | 1.26 | |
| 120 | 32.9 | 2.27 | 7.26 | 1.26 | 0.00 | 1.26 | |
| Maximum | Required Roof Sto | <u>Summary of Roof</u> prage (100 Year) = Proposed Head = | 9.46 | m ³ | *An Emergency cycr | flow scupper is provided abo | ave this height |
| | | ntrol Flow/Drain = | | L/s | , at Emergency over | souppor is provided abt | ste alle height. |
| | | r of Roof Drains = | | L-0 | | | |
| | | from Roof Drain = | | L/s | | | |
| | | ble Roof Surface = | | m ² | | | |
| | | | | ain w/ weir opening-closed | | | |
| | Total St | orage Required = | 9.46 | m ³ | | | |
| | | le Roof Storage = | 13.17 | m ³ | refer to LRL Plan C6 | 01 | |

| I ₁ | ₀₀ = 1735.688 / (To | d + 6.014) ^{0.820} | a = 1735.688 | | | b = 0.820 | | C = 6.014 |
|----------------|--------------------------------|-----------------------------|----------------------------------|-------------------------|--------------------|-------------------------|-----------------------|-----------|
| | | | Storage Require | d | ſ | | | |
| | Intensity | Controlled | | Controlled Release Rate | Uncontrolled | Total Release | | |
| Time (min) | (mm/hr) | Runoff (L/s) | Storage Volume (m ³) | Constant (L/s) | Runoff (L/s) | Rate (L/s) | | |
| 10 | 178.6 | 3.08 | 1.09 | 1.26 | 0.00 | 1.26 | | |
| 15 | 142.9 | 2.47 | 1.09 | 1.26 | 0.00 | 1.26 | | |
| 20 | 120.0 | 2.07 | 0.97 | 1.26 | 0.00 | 1.26 | | |
| 25 | 103.8 | 1.79 | 0.80 | 1.26 | 0.00 | 1.26 | | |
| 30 | 91.9 | 1.59 | 0.59 | 1.26 | 0.00 | 1.26 | | |
| 35 | 82.6 | 1.42 | 0.35 | 1.26 | 0.00 | 1.26 | | |
| 40 | 75.1 | 1.30 | 0.09 | 1.26 | 0.00 | 1.26 | | |
| 45 | 69.1 | 1.19 | 0.00 | 1.26 | 0.00 | 1.26 | | |
| 50 | 64.0 | 1.10 | 0.00 | 1.26 | 0.00 | 1.26 | | |
| 60 | 55.9 | 0.96 | 0.00 | 1.26 | 0.00 | 1.26 | | |
| 70 | 49.8 | 0.86 | 0.00 | 1.26 | 0.00 | 1.26 | | |
| 80 | 45.0 | 0.78 | 0.00 | 1.26 | 0.00 | 1.26 | | |
| 90 | 41.1 | 0.71 | 0.00 | 1.26 | 0.00 | 1.26 | | |
| 100 | 37.9 | 0.65 | 0.00 | 1.26 | 0.00 | 1.26 | | |
| 110 | 35.2 | 0.61 | 0.00 | 1.26 | 0.00 | 1.26 | | |
| 120 | 32.9 | 0.57 | 0.00 | 1.26 | 0.00 | 1.26 | | |
| | | Summary of Roo | f Storage | | | | | |
| Maximum | Required Roof Ste | orage (100 Year) = | 1.09 | m ³ | | | | |
| | | Proposed Head = | 150 | mm | *An Emergency over | rflow scupper is provid | ded above this height | |
| | | ontrol Flow/Drain = | 0.63 | L/s | | | | |
| | | er of Roof Drains = | 2 | | | | | |
| | Total Flow | from Roof Drain = | 1.26 | L/s | | | | |
| | Availal | ble Roof Surface = | 62.07 | m ² | | | | |



LRL File No. Project: Location: Date: Designed: Drawing Ref.:

220224 CIV 7-Storey Condo Building 424 Churchilli Ave April 9, 2023 Tamara Harb C601

Post-development Stormwater Management (WS-05 ROOF)

Stormwater Management Design Sheet-100 Year

| I ₁ | ₁₀₀ = 1735.688 / (To | d + 6.014) ^{0.820} | | a = | = 1735.688 | b = | 0.820 | C = 6.014 |
|----------------|---------------------------------|-----------------------------|----------------------------------|----------------------------------|--------------------|------------------------|-----------------------|-----------|
| | | | Storage Require | d | Т | | | |
| | Intensity | Controlled | | Controlled Release Rate | Uncontrolled | Total Release | | |
| Time (min) | (mm/hr) | Runoff (L/s) | Storage Volume (m ³) | Constant (L/s) | Runoff (L/s) | Rate (L/s) | | |
| 10 | 178.6 | 6.48 | 3.13 | 1.26 | 0.00 | 1.26 | | |
| 15 | 142.9 | 5.19 | 3.53 | 1.26 | 0.00 | 1.26 | | |
| 20 | 120.0 | 4.35 | 3.71 | 1.26 | 0.00 | 1.26 | | |
| 25 | 103.8 | 3.77 | 3.76 | 1.26 | 0.00 | 1.26 | | |
| 30 | 91.9 | 3.33 | 3.73 | 1.26 | 0.00 | 1.26 | | |
| 35 | 82.6 | 3.00 | 3.65 | 1.26 | 0.00 | 1.26 | | |
| 40 | 75.1 | 2.73 | 3.52 | 1.26 | 0.00 | 1.26 | | |
| 45 | 69.1 | 2.51 | 3.36 | 1.26 | 0.00 | 1.26 | | |
| 50 | 64.0 | 2.32 | 3.18 | 1.26 | 0.00 | 1.26 | | |
| 60 | 55.9 | 2.03 | 2.77 | 1.26 | 0.00 | 1.26 | | |
| 70 | 49.8 | 1.81 | 2.30 | 1.26 | 0.00 | 1.26 | | |
| 80 | 45.0 | 1.63 | 1.79 | 1.26 | 0.00 | 1.26 | | |
| 90 | 41.1 | 1.49 | 1.25 | 1.26 | 0.00 | 1.26 | | |
| 100 | 37.9 | 1.38 | 0.69 | 1.26 | 0.00 | 1.26 | | |
| 110 | 35.2 | 1.28 | 0.12 | 1.26 | 0.00 | 1.26 | | |
| 120 | 32.9 | 1.19 | 0.00 | 1.26 | 0.00 | 1.26 | | |
| Maximum | | Summary of Roof | <u>Storage</u> 3.76 | m ³ | | | | |
| IVIAXIIIIUII | r required roor ou | Proposed Head = | 150 | mm | *An Emergency over | flow scupper is provid | ded above this heid | ht |
| | C | ontrol Flow/Drain = | 0.63 | L/s | An Emergency over | | aca above tills neigi | |
| | | er of Roof Drains = | 2 | | | | | |
| | | from Roof Drain = | 1.26 | L/s | | | | |
| | | ble Roof Surface = | 131 | m ² | | | | |
| | | | | ain w/ weir opening-closed | | | | |
| | | Roof Drain Model = | WATTS adjustable root dra | | | | | |
| | | Roof Drain Model = | WATTS adjustable root dra | | | | | |
| | F | Roof Drain Model = | 3.76 | m ³ m ³ | | | | |

| CATCHMENT AREAS | DRAINAGE AREAS (ha) | 100-YEAR RELEASE RATE | 100-YEAR REQUIRED STORAGE (m3) | TOTAL AVAILABLE STORAGE (m3) |
|----------------------|------------------------|--------------------------|-----------------------------------|---------------------------------|
| WS-01(ROOF) | 0.012 | 1.26 | 3.15 | 6.03 |
| WS-02 (ROOF) | 0.014 | 1.26 | 4.23 | 4.55 |
| WS-03 (ROOF) | 0.025 | 1.26 | 9.46 | 13.17 |
| WS-04 (ROOF) | 0.006 | 1.26 | 1.09 | 3.14 |
| WS-05 (ROOF) | 0.013 | 1.26 | 3.76 | 6.64 |
| TOTAL CONTROLLED | 0.070 | 6.30 | 21.69 | 33.53 |
| WS-06 (UNCONTROLLED) | 0.031 | 15.59 | 0 | 0 |
| TOTAL UNCONTROLLED | 0.031 | 15.59 | 0.00 | 0.00 |
| TOTAL | 0.101 | 21.89 | 21.69 | 33.53 |



Runoff Equation

 LRL File No.
 220224

 Project:
 CIV 7-Storey Condo Building

 Location:
 424 Churchill Ave

 Date:
 April 9, 2023

 Designed:
 Tamara Harb

 Drawing Ref.:
 C601

Stormwater Management Design Sheet 5-YR

_

Q = 2.78CIA (L/s) C = Runoff coefficient I = Rainfall intensity (mm/hr) = A / (Td + C)^B A = Area (ha) T_c = Time of concentration (min) Pre-development Stormwater Management - 2 Year Storm

| 2 year storm | 12 = 7 | 32.95 / (Td · | + 6.199) ^{0.81} a | a = 732.951 | b = 0.810 | C = | 6.199 |
|--------------|--------|---------------|----------------------------------|-------------|-----------|-----|-------|
| | C = | 0.50 | max of 0.5 as per City of Ottawa | | | | |
| | = | 76.8 | mm/hr | | | | |
| | Tc = | 10 | min | | | | |
| Total | Area = | 0.101 | ha | | | | |
| | | | | | | | |

Allowable Release Rate= 10.81 L/s

Post-development Stormwater Management

| | | | | | ∑R _{2&5} |
|---------------|-----------------------|-------|----|-----|-----------------------|
| | Total Site Area = | 0.070 | ha | ∑R= | |
| | WS-01(ROOF) | 0.012 | ha | R= | 0.90 |
| | WS-02 (ROOF) | 0.014 | ha | R= | 0.90 |
| Controlled | WS-03 (ROOF) | 0.025 | ha | R= | 0.90 |
| Controlled | WS-04 (ROOF) | 0.006 | ha | R= | 0.90 |
| | WS-05 (ROOF) | 0.013 | ha | R= | 0.90 |
| | Total Controlled | 0.070 | ha | ∑R= | 0.90 |
| Un-controlled | WS-06 (UNCONTROLLED) | 0.031 | ha | R= | 0.90 |
| Un-controlled | Total Un-Controlled = | 0.031 | ha | ∑R= | 0.90 |

| | | Pos | st-development Stormwa | Post-development Stormwater Management (Uncontrolled Catchment WS-06) | | | | | | | | | | | | |
|---------------------|---------------------|---------------------------|-------------------------|---|---------|-----------|-----|-------|--|--|--|--|--|--|--|--|
| 5 Year Storm Event: | | | | | | | | | | | | | | | | |
| | ls = 998.071/ (Td - | + 6.053) ^{0.814} | | a = | 998.071 | b = 0.814 | C = | 6.053 | | | | | | | | |
| | Intensity | Uncontrolled | Controlled Release Rate | | 1 | | | | | | | | | | | |
| Time (min) | (mm/hr) | Runoff (L/s) | Constant (L/s) | Total Release Rate (L/s) | | | | | | | | | | | | |
| 10 | 104.2 | 8.18 | 0.00 | 8.18 | 1 | | | | | | | | | | | |



LRL File No.220Project:CIVLocation:42Date:ApDesigned:TaiDrawing Ref.:C6

220224 CIV 7-Storey Condo Building 424 Churchilli Ave April 9, 2023 Tamara Harb C601

| | | | Post-developmen | t Stormwater Managemei | nt (WS-01 ROOF) | | | | |
|---|--|--|---|--|--|--|---------------------------------|-----|-------|
| | | | | | | | | | |
| ear Storm Event: | | | | | | | | | |
| ls | = 998.071/ (Td + | 6.053) ^{0.814} | | a = | 998.071 | b = | 0.814 | C = | 6.053 |
| | | | Storage Require | d | T | | | | |
| Time (min) | Intensity (mm/hr) | Controlled Runoff (L/s) | Storage Volume (m ³) | Controlled Release Rate | Uncontrolled | Total Release | | | |
| Time (min) 10 | 104.2 | 3.03 | Storage Volume (m ³) 1.06 | Constant (L/s) 1.26 | Runoff (L/s) 0.00 | Rate (L/s) 1.26 | | | |
| 15 | 83.6 | 2.43 | 1.05 | 1.26 | 0.00 | 1.26 | | | |
| 20 | 70.3 | 2.04 | 0.94 | 1.26 | 0.00 | 1.26 | | | |
| 25 | 60.9 | 1.77 | 0.77 | 1.26 | 0.00 | 1.26 | | | |
| 30 35 | 53.9 48.5 | 1.57 1.41 | 0.56 | 1.26 1.26 | 0.00 | 1.26 1.26 | | | |
| 40 | 44.2 | 1.29 | 0.06 | 1.26 | 0.00 | 1.26 | | | |
| 45 | 40.6 | 1.18 | 0.00 | 1.26 | 0.00 | 1.26 | | | |
| 50 | 37.7 | 1.10 | 0.00 | 1.26 | 0.00 | 1.26 | | | |
| 60 70 | 32.9 29.4 | 0.96 | 0.00 | 1.26 | 0.00 | 1.26 1.26 | | | |
| 80 | 26.6 | 0.03 | 0.00 | 1.20 | 0.00 | 1.20 | | | |
| 90 | 24.3 | 0.71 | 0.00 | 1.26 | 0.00 | 1.26 | | | |
| 100 | 22.4 | 0.65 | 0.00 | 1.26 | 0.00 | 1.26 | | | |
| 110 | 20.8 | 0.61 | 0.00 | 1.26 | 0.00 | 1.26 | | | |
| 120 | 19.5 | 0.57 | 0.00 | 1.26 | 0.00 | 1.26 | | | |
| Maximum F | Co Numbe | Summary of Roof prage (100 Year) = Proposed Head = portrol Flow/Drain = er of Roof Drains = from Roof Drain = | Storage 1.06 150 0.63 2 1.26 | m ³ mm L/s | *An Emergency over | flow scupper is provid | ded above this height. | | |
| | | ble Roof Surface = | 116.28 | m ² | | | | | |
| | Availai | Je Roor Sunace - | | | | | | | |
| | | | WATTS adjustable roof dra | ain w/ weir opening-closed | | | | | |
| | F | | WATTS adjustable roof dra 1.06 | m ³ | | | | | |
| | F Total St | Roof Drain Model = | | | refer to LRL Plan C6 | 01 | | | |
| | F Total St | coof Drain Model = | 1.06 6.03 | m ³ | | 01 | | | _ |
| ear Storm Event: | F Total St | coof Drain Model = | 1.06 6.03 | m ³ m ³ | | 01 | | _ | _ |
| | F Total St | koof Drain Model = orage Required = le Roof Storage = | 1.06 6.03 | m ³ m ³ t Stormwater Managemen | | | 0.814 | C = | 6.053 |
| | F Total St Availab | koof Drain Model = orage Required = le Roof Storage = | 1.06 6.03 Post-developmen | m ³ m ³ <u>t Stormwater Managemen</u> a = | nt (WS-02 ROOF) | | 0.814 | C = | 6.053 |
| ls | F Total St Availab | koof Drain Model = orage Required = le Roof Storage = + 6.053) ^{0.814} | 1.06 6.03 Post-developmen Storage Require | m ³ m ³ t Stormwater Managemen a = d Controlled Release Rate | nt (WS-02 ROOF) 998.071 Uncontrolled | b = Total Release | 0.814 | C = | 6.053 |
| ls Time (min) | F Total St Availab | koof Drain Model = orage Required = le Roof Storage = + 6.053) ^{0.814} Controlled Runoff (L/s) | 1.06 6.03 Post-developmen Storage Require Storage Volume (m ³) | m ³ m ³ <u>t Stormwater Managemen</u> a = d <u>Controlled Release Rate</u> Constant (L/s) | nt (WS-02 ROOF) 998.071 Uncontrolled Runoff (L/s) | b = Total Release Rate (L/s) | 0.814 | C = | 6.053 |
| Is Time (min) 10 | F Total St Availab | koof Drain Model = orage Required = le Roof Storage = + 6.053) ^{0.814} Controlled Runoff (L/s) 3.69 | 1.06 6.03 Post-developmen Storage Require Storage Volume (m ³) 1.46 | m ³ m ³ t Stormwater Managemen a = d Controlled Release Rate Constant (L/s) 1.26 | nt (WS-02 ROOF) 998.071 Uncontrolled | b = Total Release Rate (L/s) 1.26 | 0.814 | C = | 6.053 |
| ls Time (min) | F Total St Availab | koof Drain Model = orage Required = le Roof Storage = + 6.053) ^{0.814} Controlled Runoff (L/s) | 1.06 6.03 Post-developmen Storage Require Storage Volume (m ³) | m ³ m ³ <u>t Stormwater Managemen</u> a = d <u>Controlled Release Rate</u> Constant (L/s) | 998.071 Uncontrolled Runoff (L/s) 0.00 | b = Total Release Rate (L/s) | 0.814 | C = | 6.053 |
| Is Time (min) 10 15 20 25 | F Total St Availab | koof Drain Model = orage Required = le Roof Storage = + 6.053) ^{0.814} Controlled Runoff (L/s) 3.69 2.96 2.49 2.16 | 1.06 6.03 Post-developmen Storage Require Storage Volume (m ³) 1.46 1.53 1.47 1.34 | m ³ m ³ t Stormwater Management t Stormwater Management a = d Controlled Release Rate Constant (L/s) 1.26 1.26 1.26 1.26 | 998.071 Uncontrolled Runoff (L/s) 0.00 0.00 0.00 0.00 | b = Total Release Rate (L/s) 1.26 1.26 1.26 1.26 | 0.814 | C = | 6.053 |
| Is Time (min) 10 15 20 25 30 | F Total St Availab | koof Drain Model = orage Required = le Roof Storage = + 6.053) ^{0.814} Controlled Runoff (L/s) 3.69 2.96 2.49 2.16 1.91 | 1.06 6.03 Post-developmen Storage Require Storage Volume (m ³) 1.46 1.53 1.47 1.34 1.17 | m ³ m ³ t Stormwater Managemen a = d Controlled Release Rate Constant (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 | 998.071 998.071 Uncontrolled Runoff (L/s) 0.00 0.00 0.00 0.00 0.00 | b = Total Release Rate (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 | 0.814 | C = | 6.053 |
| Is Time (min) 10 15 20 25 30 35 | F Total St Availab | koof Drain Model = orage Required = le Roof Storage = - 6.053) ^{0.814} Controlled Runoff (L/s) 3.69 2.96 2.96 2.49 2.16 1.91 1.72 | 1.06 6.03 Post-developmen Storage Require Storage Volume (m ³) 1.46 1.53 1.47 1.34 1.17 0.96 | m ³ m ³ t Stormwater Managemen a = d Controlled Release Rate Constant (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 | 998.071 998.071 Uncontrolled Runoff (L/s) 0.00 0.00 0.00 0.00 0.00 0.00 | b = Total Release Rate (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 | 0.814 | C = | 6.053 |
| Is Time (min) 10 15 20 25 30 35 40 | F Total St Availab | koof Drain Model = orage Required = le Roof Storage = + 6.053) ^{0.814} Controlled Runoff (L/s) 3.69 2.96 2.49 2.49 2.16 1.91 1.72 1.56 | 1.06 6.03 Post-developmen Storage Require Storage Volume (m ³) 1.46 1.53 1.47 1.34 1.17 0.96 0.73 | m ³ m ³ t Stormwater Management t Stormwater Management a = d Controlled Release Rate Constant (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 | 998.071 998.071 Uncontrolled Runoff (L/s) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | b = Total Release Rate (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 | 0.814 | C = | 6.053 |
| Is Time (min) 10 15 20 25 30 35 | F Total St Availab | koof Drain Model = orage Required = le Roof Storage = - 6.053) ^{0.814} Controlled Runoff (L/s) 3.69 2.96 2.96 2.49 2.16 1.91 1.72 | 1.06 6.03 Post-developmen Storage Require Storage Volume (m ³) 1.46 1.53 1.47 1.34 1.17 0.96 | m ³ m ³ t Stormwater Managemen a = d Controlled Release Rate Constant (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 | 998.071 998.071 Uncontrolled Runoff (L/s) 0.00 0.00 0.00 0.00 0.00 0.00 | b = Total Release Rate (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 | 0.814 | C = | 6.053 |
| Is Time (min) 10 15 20 25 30 35 40 45 50 60 | F Total St Availab | koof Drain Model = orage Required = le Roof Storage = b 6.053) ^{0.814} Controlled Runoff (L/s) 3.69 2.96 2.49 2.49 2.16 1.91 1.72 1.56 1.44 1.33 1.17 | 1.06 6.03 Post-developmen Storage Require Storage Volume (m ³) 1.46 1.53 1.47 1.34 1.17 0.96 0.73 0.48 0.22 0.00 | m ³ m ³ t Stormwater Management t Stormwater Management a = d Controlled Release Rate Constant (L/s) 1.26 | 998.071 998.071 Uncontrolled Runoff (L/s) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | b = Total Release Rate (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 | 0.814 | C = | 6.053 |
| Is Time (min) 10 15 20 25 30 35 40 45 50 60 70 | F Total St Availab | koof Drain Model = orage Required = le Roof Storage = + 6.053) ^{0.814} Controlled Runoff (L/s) 3.69 2.96 2.49 2.16 1.91 1.72 1.56 1.44 1.33 1.17 1.04 | 1.06 6.03 Post-developmen Storage Require Storage Volume (m ³) 1.46 1.53 1.47 1.34 1.17 0.96 0.73 0.48 0.22 0.00 0.00 | m ³ m ³ t Stormwater Management t Stormwater Management a = d Controlled Release Rate Constant (L/s) 1.26 | 998.071 998.071 Uncontrolled Runoff (L/s) 0.00 0. | b = Total Release Rate (L/s) 1.26 | 0.814 | C = | 6.053 |
| Is Time (min) 10 15 20 25 30 35 40 45 50 60 70 80 | F Total St Availab | koof Drain Model = orage Required = le Roof Storage = le Roof Storage = controlled Runoff (L/s) 3.69 2.96 2.96 2.96 2.96 1.91 1.72 1.56 1.44 1.33 1.17 1.04 0.94 | 1.06 6.03 Post-developmen Storage Require Storage Volume (m ³) 1.46 1.53 1.47 1.34 1.17 0.96 0.73 0.48 0.22 0.00 0.00 | m ³ m ³ t Stormwater Management t Stormwater Management a = d Controlled Release Rate Constant (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 | 998.071 Uncontrolled Runoff (L/s) 0.00 | b = Total Release Rate (L/s) 1.26 | 0.814 | C = | 6.053 |
| Is Time (min) 10 15 20 25 30 25 40 45 50 60 70 80 90 | F Total St Availab | koof Drain Model = orage Required = le Roof Storage = be 6.053) ^{0.814} Controlled Runoff (L/s) 3.69 2.96 2.49 2.49 2.16 1.91 1.72 1.56 1.44 1.33 1.17 1.04 0.94 0.86 | 1.06 6.03 Post-developmen Storage Require Storage Volume (m ³) 1.46 1.53 1.47 1.34 1.17 0.96 0.73 0.48 0.22 0.00 0.00 0.00 0.00 | m ³ m ³ t Stormwater Management t Stormwater Management a = d Controlled Release Rate Constant (L/s) 1.26 | 998.071 998.071 Uncontrolled Runoff (L/s) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0. | b = Total Release Rate (L/s) 1.26 | 0.814 | C = | 6.053 |
| Is Time (min) 10 15 20 25 30 35 40 45 50 60 70 80 90 100 | F Total St Availab | koof Drain Model = orage Required = le Roof Storage = + 6.053) ^{0.814} Controlled Runoff (L/s) 3.669 2.96 2.49 2.16 1.91 1.72 1.56 1.44 1.33 1.17 1.04 0.94 0.86 0.79 | 1.06 6.03 Post-developmen Storage Require Storage Volume (m ³) 1.46 1.53 1.47 1.34 1.17 0.96 0.73 0.48 0.22 0.00 0.00 0.00 0.00 0.00 | m ³ m ³ t Stormwater Management a = d Controlled Release Rate Constant (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 | 998.071 998.071 Uncontrolled Runoff (L/s) 0.00 0. | b = Total Release Rate (L/s) 1.26 | 0.814 | C = | 6.053 |
| Is Time (min) 10 15 20 25 30 35 40 45 50 60 70 80 90 | F Total St Availab | koof Drain Model = orage Required = le Roof Storage = be 6.053) ^{0.814} Controlled Runoff (L/s) 3.69 2.96 2.49 2.49 2.16 1.91 1.72 1.56 1.44 1.33 1.17 1.04 0.94 0.86 | 1.06 6.03 Post-developmen Storage Require Storage Volume (m ³) 1.46 1.53 1.47 1.34 1.17 0.96 0.73 0.48 0.22 0.00 0.00 0.00 0.00 | m ³ m ³ t Stormwater Management t Stormwater Management a = d Controlled Release Rate Constant (L/s) 1.26 | 998.071 998.071 Uncontrolled Runoff (L/s) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0. | b = Total Release Rate (L/s) 1.26 | 0.814 | C = | 6.053 |
| Is Time (min) 10 15 20 25 30 35 40 45 50 60 70 80 90 100 110 | F Total St Availab = 998.071/ (Td - Intensity (mm/hr) 104.2 83.6 70.3 60.9 53.9 53.9 53.9 53.9 48.5 44.2 40.6 37.7 32.9 48.5 44.2 40.6 37.7 32.9 48.5 44.2 40.6 37.7 32.9 4 8.5 40.6 2.0 8 | koof Drain Model = orage Required = le Roof Storage = le Roof Storage = controlled Runoff (L/s) 3.69 2.96 2.96 2.96 2.96 1.91 1.72 1.56 1.44 1.33 1.17 1.04 0.94 0.86 0.79 0.74 | 1.06 6.03 Post-developmen Storage Require Storage Volume (m ³) 1.46 1.53 1.47 1.34 1.17 0.96 0.73 0.48 0.22 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | m³ m3 t Stormwater Management t Stormwater Management a = d Controlled Release Rate Constant (L/s) 1.26 1. | (WS-02 ROOF) (WS-02 ROOF) (Uncontrolled Runoff (L/s) 0.00 | b = Total Release Rate (L/s) 1.26 | 0.814 | C = | 6.053 |
| Is Time (min) 10 15 20 25 30 35 40 45 50 60 70 80 90 100 110 | F Total St Availab | koof Drain Model = orage Required = le Roof Storage = le Roof Storage = controlled Runoff (L/s) 3.69 2.96 2.96 2.96 2.96 1.91 1.72 1.56 1.44 1.33 1.17 1.04 0.94 0.86 0.79 0.74 | 1.06 6.03 Post-developmen Storage Require Storage Volume (m ³) 1.46 1.53 1.47 1.34 1.17 0.96 0.73 0.48 0.22 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | m³ m3 t Stormwater Management t Stormwater Management a = d Controlled Release Rate Constant (L/s) 1.26 1. | (WS-02 ROOF) (WS-02 ROOF) (Uncontrolled Runoff (L/s) 0.00 | b = Total Release Rate (L/s) 1.26 | 0.814 | C = | 6.053 |
| Is Time (min) 10 15 20 25 30 35 40 45 50 60 70 80 90 100 110 120 | F Total St Availab | koof Drain Model = orage Required = le Roof Storage = be 6.053) ^{0.814} Controlled Runoff (L/s) 3.69 2.96 2.49 2.49 2.49 1.62 1.91 1.72 1.56 1.44 1.33 1.17 1.04 0.94 0.86 0.79 0.74 0.69 Summary of Roof | 1.06 6.03 Post-developmen Storage Require Storage Volume (m ³) 1.46 1.53 1.47 1.34 1.17 0.96 0.73 0.48 0.22 0.00 0.0 | m³ m³ t Stormwater Management t Stormwater Management a = d Controlled Release Rate Constant (L/s) 1.26 1. | (WS-02 ROOF) (WS-02 ROOF) (Uncontrolled Runoff (L/s) 0.00 | b = Total Release Rate (L/s) 1.26 | 0.814 | C = | 6.053 |
| Is Time (min) 10 15 20 25 30 35 40 45 50 60 70 80 90 100 110 120 | F Total St Availab | koof Drain Model = orage Required = le Roof Storage = - 6.053) ^{0.814} Controlled Runoff (L/s) 3.69 2.96 2.16 1.91 1.56 1.44 1.33 1.17 1.04 0.94 0.86 0.79 0.74 0.69 Summary of Roof orage (100 Year) = | 1.06 6.03 Post-developmen Storage Require Storage Volume (m ³) 1.46 1.53 1.47 1.34 1.17 0.96 0.73 0.48 0.22 0.00 0.0 | m ³ t Stormwater Management t Stormwater Management a = d Controlled Release Rate Constant (L/s) 1.26 1.2 | 998.071 998.071 Uncontrolled Runoff (L/s) 0.00 0. | b = Total Release Rate (L/s) 1.26 | | C = | 6.053 |
| Is Time (min) 10 15 20 25 30 35 40 45 50 60 70 80 90 100 110 120 | F Total St Availab = 998.071/ (Td - Intensity (mm/hr) 104.2 83.6 70.3 60.9 53.9 48.5 44.2 40.6 37.7 32.9 29.4 20.4 20.4 20.4 20.8 19.5 Required Roof St | koof Drain Model = orage Required = le Roof Storage = be 6.053) ^{0.814} Controlled Runoff (L/s) 3.69 2.96 2.49 2.49 2.49 1.62 1.91 1.72 1.56 1.44 1.33 1.17 1.04 0.94 0.86 0.79 0.74 0.69 Summary of Roof | 1.06 6.03 Post-developmen Storage Require Storage Volume (m ³) 1.46 1.53 1.47 1.34 1.17 0.96 0.73 0.48 0.22 0.00 0.0 | m³ m³ t Stormwater Management t Stormwater Management a = d Controlled Release Rate Constant (L/s) 1.26 1. | 998.071 998.071 Uncontrolled Runoff (L/s) 0.00 0. | b = Total Release Rate (L/s) 1.26 | 0.814 ded above this height. | C = | 6.053 |
| Is Time (min) 10 15 20 25 30 35 40 45 50 60 70 80 90 100 110 120 | F Total St Availab a 998.071/ (Td - Intensity (mm/hr) 104.2 83.6 70.3 60.9 53.9 53.9 53.9 48.5 44.2 40.6 37.7 32.9 48.5 44.2 40.6 22.4 20.8 19.5 Required Roof Str Ca Numbr | toof Drain Model = orage Required = le Roof Storage = le Roof Storage = - 6.053) ^{0.814} Controlled Runoff (L/s) 3.69 2.96 2.96 2.16 1.91 1.56 1.44 1.33 1.17 1.04 0.94 0.669 0.74 0.69 Summary of Roof portor Flow/Drain = of Orajan = | 1.06 6.03 Post-developmen Storage Require Storage Volume (m ³) 1.46 1.53 1.47 1.34 1.17 0.96 0.73 0.48 0.22 0.00 0.03 0.05 0.03 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.0 | m ³ m ³ t Stormwater Management a = d Controlled Release Rate Constant (L/s) 1.26 1.26 1.26 1.26 1.26 1.26 1.26 1.26 | 998.071 998.071 Uncontrolled Runoff (L/s) 0.00 0. | b = Total Release Rate (L/s) 1.26 | | C = | 6.053 |
| Is Time (min) 10 15 20 25 30 35 40 45 50 60 70 80 90 100 110 120 | F Total St Availab = 998.071/ (Td - 104.2 83.6 70.3 60.9 53.9 48.5 44.2 40.6 37.7 32.9 48.5 44.5 44.5 40.6 20.4 20.4 20.4 20.4 20.4 20.8 19.5 Required Roof Sta CC Number Total Flow | toof Drain Model = orage Required = le Roof Storage = le Roof Storage = controlled Runoff (L/s) 3.69 2.96 2.96 2.96 2.96 1.91 1.72 1.56 1.44 0.33 1.17 0.66 0.79 0.74 0.69 Summary of Roof orage (100 Year) = Proposed Head = of Orains = roof Roof Drains = | 1.06 6.03 Post-developmen Storage Require Storage Volume (m ³) 1.46 1.53 1.47 1.34 1.17 0.96 0.73 0.48 0.22 0.00 0.0 | m ³ t Stormwater Managemen t Stormwater Managemen a = d Controlled Release Rate Constant (L/s) 1.26 1.25 1.26 | 998.071 998.071 Uncontrolled Runoff (L/s) 0.00 0. | b = Total Release Rate (L/s) 1.26 | | C = | 6.053 |
| Is Time (min) 10 15 20 25 30 35 40 45 50 60 70 80 90 100 110 120 | F Total St Availab = 998.071/ (Td - Intensity (mm/hr) 104.2 83.6 70.3 60.9 53.9 44.5 44.2 40.6 70.3 60.9 53.9 44.5 44.2 40.6 20.4 20.4 20.8 19.5 Required Roof Str Numbe Total Flow Availab | koof Drain Model = orage Required = le Roof Storage = le Roof Storage = controlled Runoff (L/s) 3.69 2.96 2.49 2.16 1.91 1.72 1.56 1.44 0.94 0.86 0.74 0.69 Summary of Roof proposed Heag = ontrol Flow/Drain = ro Roof Drains = le Roof Surface = | 1.06 6.03 Post-developmen Storage Require Storage Volume (m ³) 1.46 1.53 1.47 1.34 1.17 0.96 0.73 0.48 0.22 0.00 0.03 0.05 0.03 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.0 | m ³ t Stormwater Management t Stormwater Management a = d Controlled Release Rate Constant (L/s) 1.26 1.2 | 998.071 998.071 Uncontrolled Runoff (L/s) 0.00 0. | b = Total Release Rate (L/s) 1.26 | | C = | 6.053 |
| Is Time (min) 10 15 20 25 30 35 40 45 50 60 70 80 90 100 110 120 | F Total St Availab = 998.071/ (Td - Intensity (mm/hr) 104.2 83.6 70.3 60.9 53.9 53.9 53.9 48.5 44.2 40.6 37.7 32.9 48.5 44.5 44.2 20.4 20.4 20.8 19.5 Required Roof Sta CC Number Total Flow Availab | koof Drain Model = orage Required = le Roof Storage = le Roof Storage = controlled Runoff (L/s) 3.69 2.96 2.49 2.16 1.91 1.72 1.56 1.44 0.94 0.86 0.74 0.69 Summary of Roof proposed Heag = ontrol Flow/Drain = ro Roof Drains = le Roof Surface = | 1.06 6.03 Post-developmen Storage Require Storage Volume (m ³) 1.46 1.53 1.47 1.34 1.17 0.96 0.73 0.48 0.22 0.00 0.63 2 1.26 141 | m ³ t Stormwater Management t Stormwater Management a = d Controlled Release Rate Constant (L/s) 1.26 1.2 | 998.071 998.071 Uncontrolled Runoff (L/s) 0.00 0. | b = Total Release Rate (L/s) 1.26 | | C = | 6.053 |



LRL File No. Project: Location: Date: Designed: Drawing Ref.:

220224 CIV 7-Storey Condo Building 424 Churchilli Ave April 9, 2023 Tamara Harb C601

Post-development Stormwater Management (WS-03 ROOF)

| | l₅ = 998.071/ (Td + | 6.053) ^{0.814} | | a = | 998.071 | b = 0 | .814 | C = | 6.0 |
|------------|---|--|----------------------------------|-------------------------|----------------------|-------------------------|------------------|--------|-----|
| |] | | Storage Require | d | T | | | | |
| | Intensity | Controlled | | Controlled Release Rate | Uncontrolled | Total Release | | | |
| Time (min) | (mm/hr) | Runoff (L/s) | Storage Volume (m ³) | Constant (L/s) | Runoff (L/s) | Rate (L/s) | | | |
| 10 | 104.2 | 6.47 | 3.12 | 1.26 | 0.00 | 1.26 | | | |
| 15 | 83.6 | 5.19 | 3.53 | 1.26 | 0.00 | 1.26 | | | |
| 20 | 70.3 | 4.36 | 3.72 | 1.26 | 0.00 | 1.26 | | | |
| 25 | 60.9 | 3.78 | 3.78 | 1.26 | 0.00 | 1.26 | | | |
| 30 | 53.9 | 3.35 | 3.76 | 1.26 | 0.00 | 1.26 | | | |
| 35 | 48.5 | 3.01 | 3.68 | 1.26 | 0.00 | 1.26 | | | |
| 40 | 44.2 | 2.74 | 3.56 | 1.26 | 0.00 | 1.26 | | | |
| 45 | 40.6 | 2.52 | 3.41 | 1.26 | 0.00 | 1.26 | | | |
| 50 | 37.7 | 2.34 | 3.23 | 1.26 | 0.00 | 1.26 | | | |
| 60 | 32.9 | 2.04 | 2.83 | 1.26 | 0.00 | 1.26 | | | |
| 70 | 29.4 | 1.82 | 2.37 | 1.26 | 0.00 | 1.26 | | | |
| 80 | 26.6 | 1.65 | 1.87 | 1.26 | 0.00 | 1.26 | | | |
| 90 | 24.3 | 1.51 | 1.34 | 1.26 | 0.00 | 1.26 | | | |
| 100 | 22.4 | 1.39 | 0.79 | 1.26 | 0.00 | 1.26 | | | |
| 110 | 20.8 | 1.29 | 0.21 | 1.26 | 0.00 | 1.26 | | | |
| 120 | 19.5 | 1.21 | 0.00 | 1.26 | 0.00 | 1.26 | | | |
| | | Summary of Roo | f Storage | | | | | | |
| | Required Roof Sto | orage (100 Year) = | 3.78 | m ³ | | | | | |
| Maximum | | | | mm | *An Emergency over | flow scupper is provide | ed above this he | eight. | |
| Maximum | | Proposed Head = | 150 | 11011 | An Emergency over | | | | |
| Maximum | | Proposed Head = ontrol Flow/Drain = | 0.63 | L/s | An Emergency over | | | | |
| Maximum | Co | | | | | | | | |
| Maximum | Co | ntrol Flow/Drain = | 0.63 | L/s L/s | An Emergency over | | | | |
| Maximum | Co Numbe Total Flow | ntrol Flow/Drain = r of Roof Drains = | 0.63 2 | L/s | , an Emergency over | | | | |
| Maximum | Cc Numbe Total Flow Availab | ntrol Flow/Drain = r of Roof Drains = from Roof Drain = le Roof Surface = | 0.63 2 1.26 | L/s m ² | The Emergency over | | | | |
| Maximum | Cc Numbe Total Flow Availab R | ntrol Flow/Drain = r of Roof Drains = from Roof Drain = le Roof Surface = | 0.63 2 1.26 248 | L/s m ² | , ur Enleigency over | | | | |

| | | | Post-developmer | t Stormwater Managemen | t (WS-04 ROOF) | | | | |
|----------------|--------------------|--|------------------------------------|--|----------------------|------------------------|----------------------|-----|-------|
| | | | | | | | | | |
| r Storm Event: | | | | | | | | | |
| l | 5 = 998.071/ (Td + | 6.053) ^{0.814} | | a = | 998.071 | b = | 0.814 | C = | 6.053 |
| | | | Storage Require | d | r | | | | |
| | Intensity | Controlled | | Controlled Release Rate | Uncontrolled | Total Release |] | | |
| Time (min) | (mm/hr) | Runoff (L/s) | Storage Volume (m ³) | Constant (L/s) | Runoff (L/s) | Rate (L/s) | - | | |
| 10 | 104.2 | 1.62 | 0.21 | 1.26 | 0.00 | 1.26 | - | | |
| 15 | 83.6 | 1.30 | 0.03 | 1.26 | 0.00 | 1.26 | - | | |
| 20 | 70.3 | 1.09 | 0.00 | 1.26 | 0.00 | 1.26 | 4 | | |
| 25 | 60.9 | 0.95 | 0.00 | 1.26 | 0.00 | 1.26 | - | | |
| 30 | 53.9 | 0.84 | 0.00 | 1.26 | 0.00 | 1.26 | - | | |
| 35 | 48.5 | 0.75 | 0.00 | 1.26 | 0.00 | 1.26 | | | |
| 40 | 44.2 | 0.69 | 0.00 | 1.26 | 0.00 | 1.26 | | | |
| 45 | 40.6 | 0.63 | 0.00 | 1.26 | 0.00 | 1.26 | | | |
| 50 | 37.7 | 0.58 | 0.00 | 1.26 | 0.00 | 1.26 | | | |
| 60 | 32.9 | 0.51 | 0.00 | 1.26 | 0.00 | 1.26 | | | |
| 70 | 29.4 | 0.46 | 0.00 | 1.26 | 0.00 | 1.26 | | | |
| 80 | 26.6 | 0.41 | 0.00 | 1.26 | 0.00 | 1.26 | | | |
| 90 | 24.3 | 0.38 | 0.00 | 1.26 | 0.00 | 1.26 | | | |
| 100 | 22.4 | 0.35 | 0.00 | 1.26 | 0.00 | 1.26 | | | |
| 110 | 20.8 | 0.32 | 0.00 | 1.26 | 0.00 | 1.26 | | | |
| 120 | 19.5 | 0.30 | 0.00 | 1.26 | 0.00 | 1.26 | | | |
| | | Summary of Roo | | m³ | | | | | |
| Maximum I | | orage (100 Year) = | | | | | | | |
| | | Proposed Head = | | | An Emergency over | rflow scupper is provi | ded above this heigh | nt. | |
| | | ontrol Flow/Drain = | | L/s | | | | | |
| | | er of Roof Drains = | | | | | | | |
| | | from Roof Drain = | | L/s | | | | | |
| | | ole Roof Surface = Roof Drain Model = | 62.07 WATTS adjustable roof dra | m ² ain w/ weir opening-closed | | | | | |
| | Total St | orage Required = | 0.21 | m ³ | | | | | |
| | | le Roof Storage = | | | refer to LRL Plan C6 | | | | |

Stormwater Management Design Sheet 5-YR



LRL File No. Project: Location: Date: Designed: Drawing Ref.:

220224 CIV 7-Storey Condo Building 424 Churchilli Ave April 9, 2023 Tamara Harb C601

Post-development Stormwater Management (WS-05 ROOF)

Stormwater Management Design Sheet 5-YR

| | ls = 998.071/ (Td · | + 6.053) ^{0.814} | | a = | 998.071 | b = | 0.814 | C = | 6 |
|------------------|---------------------|---------------------------|--|--|----------------------|--------------------------|--|-------|---|
| | | | Storage Require | d | ĺ | | Total Release Rate (L/s) 1.26 | | |
| Time (min) | Intensity | Controlled | | Controlled Release Rate | Uncontrolled | | | | |
| Time (min) 10 | (mm/hr) 104.2 | Runoff (L/s) 3.40 | Storage Volume (m ³) 1.29 | Constant (L/s) 1.26 | Runoff (L/s) 0.00 | | | | |
| 10 | 83.6 | 2.73 | 1.32 | 1.26 | 0.00 | | | | |
| 20 | 70.3 | 2.73 | 1.24 | 1.26 | 0.00 | | | | |
| 20 | 60.9 | 1.99 | 1.09 | 1.26 | 0.00 | | | | |
| 30 | 53.9 | 1.99 | 0.90 | 1.20 | 0.00 | | | | |
| 35 | 48.5 | 1.58 | 0.90 | 1.20 | 0.00 | | | | |
| 40 | 40.5 | 1.44 | 0.00 | 1.26 | 0.00 | | | | |
| 45 | 40.6 | 1.33 | 0.44 | 1.26 | 0.00 | | | | |
| 50 | 37.7 | 1.23 | 0.00 | 1.26 | 0.00 | | | | |
| 60 | 32.9 | 1.08 | 0.00 | 1.26 | 0.00 | | | | |
| 70 | 29.4 | 0.96 | 0.00 | 1.26 | 0.00 | | | | |
| 80 | 26.6 | 0.87 | 0.00 | 1.26 | 0.00 | | | | |
| 90 | 24.3 | 0.79 | 0.00 | 1.26 | 0.00 | | | | |
| 100 | 22.4 | 0.73 | 0.00 | 1.26 | 0.00 | | | | |
| 110 | 20.8 | 0.68 | 0.00 | 1.26 | 0.00 | | | | |
| 120 | 19.5 | 0.64 | 0.00 | 1.26 | 0.00 | 1.26 | | | |
| | | Summary of Roo | f Storage | | | | | | |
| Maximum | Required Roof St | orage (100 Year) = | 1.32 | m ³ | | | | | |
| | | Proposed Head = | | mm | *An Emergency ove | orflow scupper is provid | ded above this he | ight. | |
| | C | ontrol Flow/Drain = | 0.63 | L/s | | | | | |
| | Numbe | er of Roof Drains = | 2 | | | | | | |
| | Total Flow | from Roof Drain = | 1.26 | L/s | | | | | |
| | TOLAT FIOW | | 131 | m ² | | | | | |
| | | ble Roof Surface = | | | | | | | |
| | Availa | | WATTS adjustable roof dra | in w/ weir opening-closed | | | | | |
| | Availa F | | WATTS adjustable roof dra | in w/ weir opening-closed m ³ | | | | | |

| SUN | IMARY OF R | ELEASE RATES | AND STORAGE VOLUME | ES |
|----------------------|------------------------|------------------------|---------------------------------|---------------------------------|
| CATCHMENT AREAS | DRAINAGE AREAS (ha) | 5-YEAR RELEASE RATE | 5-YEAR REQUIRED STORAGE (m3) | TOTAL AVAILABLE STORAGE (m3) |
| WS-01(ROOF) | 0.012 | 1.26 | 1.06 | 6.03 |
| WS-02 (ROOF) | 0.014 | 1.26 | 1.53 | 4.55 |
| WS-03 (ROOF) | 0.025 | 1.26 | 3.78 | 13.17 |
| WS-04 (ROOF) | 0.006 | 1.26 | 0.21 | 3.14 |
| WS-05 (ROOF) | 0.013 | 1.26 | 1.32 | 6.64 |
| TOTAL CONTROLLED | 0.070 | 6.30 | 7.91 | 33.53 |
| WS-06 (UNCONTROLLED) | 0.031 | 8.18 | 0 | 0 |
| TOTAL UNCONTROLLED | 0.031 | 8.18 | 0.00 | 0.00 |
| TOTAL | 0.101 | 14.48 | 7.91 | 33.53 |

LRL Associates Ltd. Storm Design Sheet



 LRL File No.
 220224

 Project:
 CIV 7-Storey Condo Building

 Location:
 424 Churchill Avenue

 Date:
 April 9, 2023

 Designed:
 Tamara Harb

 Drawing Reference:
 C.401

| | Storm Design P | rs |
|--|------------------------|--|
| Rational Method Q = 2.78CIA | | Ottawa Macdonald-Cartier International Airport IDF curve |
| | | equation (10 year event, intensity in mm/hr) |
| Q = Peak flow in litres per second (L/s) | Runoff Coefficient (C) | l100 = 1735.688 / (Td + 6.014)0.820 |
| A = Drainage area in hectares (ha) | Grass 0.2 | Min. velocity = 0.80 m/s |
| C = Runoff coefficient | Gravel 0.7 | Manning's "n" = 0.013 |
| I = Rainfall intensity (mm/hr) | Asphalt / rooftop 0.9 | |

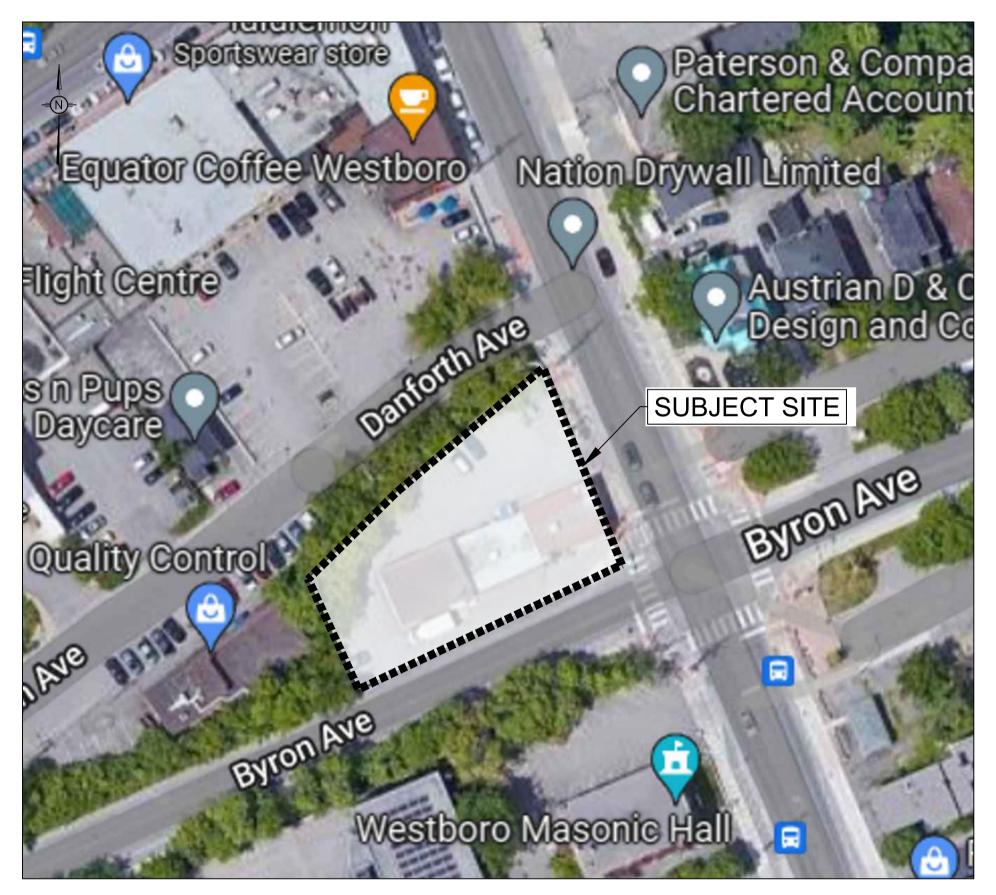
| LO | CATION | | | AREA (ha) | ha) FLOW | | | | | | | ç | STORM S | EWER | | | | | |
|-----------------------|----------|------------------|----------|-----------|----------|------------------|------------------|----------------------------|----------------------------------|----------------------|-------------------------------|--------------------------|---------|-----------|---------------|------------------------|---------------------------|---------------------------|---------------------------------|
| WATERSHED / STREET | From MH | To MH | C = 0.20 | C = 0.70 | C = 0.90 | Indiv. 2.78AC | Accum. 2.78AC | Time of Conc. (min.) | Rainfall Intensity (mm/hr) | Peak Flow Q (L/s) | Controlled Flow Q (L/s) | Pipe Diameter (mm) | Туре | Slope (%) | Length (m) | Capacity Full (L/s) | Velocity Full (m/s) | Time of Flow (min.) | Ratio (Q/Q _{FULL}) |
| WS-01 to WS-05 | Building | PROP STM MH01 | 0.000 | 0.000 | 0.070 | 0.175 | 0.175 | 10.00 | 178.6 | 31.28 | 6.30 | 250 | PVC | 2.00% | 11.6 | 84.1 | 1.71 | 0.11 | 0.37 |
| | | | | | | | | | | | | | | | | | | | |

APPENDIX E

Civil Engineering Drawings

PROPOSED 8 STOREY MULTI-UNIT BUILDING 424 CHURCHILL AVE, OTTAWA ON

REVISION 05



KEY PLAN (N.T.S.)

DRAWING INDEX

TITLE PAGE

SEDIMENT AND EROSION CONTROL PLAN

DEMOLITION PLAN

GRADING AND DRAINAGE PLAN

SERVICING PLAN

STORMWATER MANAGEMENT PLAN

PRE-DEVELOPMENT WATERSHED PLAN

POST-DEVELOPMENT WATERSHED PLAN

CONSTRUCTION DETAIL PLAN



ENGINEERING | INGÉNIERIE

5430 Canotek Road | Ottawa, ON, K1J 9G2 www.lrl.ca | (613) 842-3434

| C101 | |
|------|--|
| C102 | |
| C301 | |
| C401 | |
| C601 | |
| C701 | |
| C702 | |
| C901 | |
| | |





GENERAL NOTES

- 1. ALL WORKS MATERIALS SHALL CONFIRM TO THE LAST REVISION OF THE STANDARDS AND SPECIFICATIONS FOR THE CITY OF OTTAWA, ONTARIO PROVINCIAL STANDARD DRAWINGS (OPSD) AND SPECIFICATIONS (OPSS), WHERE APPLICABLE. LOCAL UTILITY STANDARDS AND MINISTRY OF TRANSPORTATION STANDARDS WILL APPLY WHERE REQUIRED.
- 2. THE CONTRACTORS SHALL CONFIRM THE LOCATION OF ALL EXISTING UTILITIES WITHIN THE SITE AND ADJACENT WORK AREAS. THE CONTRACTORS SHALL BE RESPONSIBLE FOR PROTECTING ALL EXISTING UTILITIES TO THE SATISFACTION OF THE AUTHORITY HAVING JURISDICTION. THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE REPAIR OR REPLACEMENT OF ANY SERVICES OR UTILITIES DISTURBED DURING CONSTRUCTION, TO THE SATISFACTION OF THE AUTHORITY HAVING JURISDICTION.
- 3. ALL DIMENSIONS SHALL BE CHECKED AND VERIFIED IN THE FIELD BY THE CONTRACTOR PRIOR TO THE START OF CONSTRUCTION, ANY DISCREPANCIES SHALL BE REPORTED IMMEDIATELY TO THE ENGINEER. LOST TIME DUE TO FAILURE OF THE CONTRACTORS TO CONFIRM UTILITY LOCATIONS AND NOTIFY ENGINEER OF POSSIBLE CONFLICTS PRIOR TO CONSTRUCTION WILL BE AT CONTRACTORS EXPENSE. 4. ANY AREA BEYOND THE LIMIT OF THE SITE DISTURBED DURING CONSTRUCTION SHALL BE RESTORED TO ORIGINAL CONDITION OR
- BETTER TO THE SATISFACTION OF THE AUTHORITY HAVING JURISDICTION AT THE CONTRACTOR'S EXPENSE RELOCATING OF EXISTING SERVICES AND/OR UTILITIES SHALL BE AS SHOWN ON THE DRAWINGS OR DETECTED BY THE ENGINEER AT THE EXPENSE OF DEVELOPERS
- 5. ALL WORK SHALL BE COMPLETED IN ACCORDANCE WITH THE 'OCCUPATIONAL HEALTH AND SAFETY ACT AND REGULATIONS FOR CONSTRUCTION PROJECTS'. THE GENERAL CONTRACTORS SHALL BE DEEMED TO BE THE 'CONTRACTOR' AS DEFINED IN THE ACT. 6. ALL THE CONSTRUCTION SIGNAGE MUST CONFIRM TO THE MINISTRY OF TRANSPORTATION OF ONTARIO MANUAL OF UNIFORM TRAFFIC
- CONTROL DEVICES PER LATEST AMENDMENT 7. THE CONTRACTOR IS ADVISED THAT WORKS BY OTHERS MAY BE ONGOING DURING THE PERIOD OF THE CONTRACT. THE CONTRACTOR SHALL COORDINATE CONSTRUCTION ACTIVITIES TO PREVENT CONFLICTS.
- 8. ALL DIMENSIONS ARE IN METRES UNLESS SPECIFIED OTHERWISE.
- 9. THERE WILL BE NO SUBSTITUTION OF MATERIALS UNLESS PRIOR WRITTEN APPROVAL IS RECEIVED FROM THE ENGINEER. 10. ALL CONSTRUCTION SHALL BE CARRIED OUT IN ACCORDANCE WITH THE RECOMMENDATIONS MADE IN THE GEOTECHNICAL REPORT
- 11. FOR DETAILS RELATING TO STORMWATER MANAGEMENT AND ROOF DRAINAGE REFER TO THE SITE SERVICING AND STORMWATER MANAGEMENT REPORT
- 12. ALL SEWERS CONSTRUCTED WITH GRADES LESS THAN 1.0% SHALL BE INSTALLED USING LASER ALIGNMENT AND CHECKED WITH LEVEL INSTRUMENT PRIOR TO BACKFILLING.
- 13. THE CONTRACTOR IS RESPONSIBLE FOR OBTAINING ALL PERMITS REQUIRED AND TO BEAR THE COST OF THE SAME. 14. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ADDITIONAL BEDDING, OR ADDITIONAL STRENGTH PIPE IF THE MAXIMUM TRENCH WIDTH AS
- SPECIFIED BY OPSD IS EXCEEDED.
- 15. ALL PIPE/CULVERT SECTION SIZES REFER TO INSIDE DIMENSIONS. 16. SHOULD DEEPLY BURIED ARCHAEOLOGICAL REMAINS BE FOUND ON THE PROPERTY DURING CONSTRUCTION ACTIVITIES. THE HERITAGE OPERATIONS UNIT OF THE ONTARIO MINISTRY OF CULTURE MUST BE NOTIFIED IMMEDIATELY.
- 17. ALL NECESSARY CLEARING AND GRUBBING SHALL BE COMPLETED BY THE CONTRACTOR. REVIEW WITH CONTRACT ADMINISTRATOR AND THE CITY OF OTTAWA PRIOR TO ANY TREE CUTTING/REMOVAL. 18. DRAWINGS SHALL BE READ ON CONJUNCTION WITH ARCHITECTURAL SITE PLAN.
- 19. THE CONTRACTOR SHALL PROVIDE THE PROJECT ENGINEER ON SET OF AS CONSTRUCTED SITE SERVICING AND GRADING DRAWINGS. 20.BENCHMARKS: IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO VERIFY THAT THE SITE BENCHMARK(S) HAS NOT BEEN ALTERED OR DISTURBED AND THAT ITS RELATIVE ELEVATION AND DESCRIPTION AGREES WITH THE INFORMATION DEPICTED ON THIS PLAN.

EROSION AND SEDIMENT CONTROL NOTES

GENERAL

THE CONTRACTOR SHALL IMPLEMENT BEST MANAGEMENT PRACTICES, TO PROVIDE FOR PROTECTION OF THE AREA DRAINAGE SYSTEM AND THE RECEIVING WATERCOURSE. DURING CONSTRUCTION ACTIVITIES. THE CONTRACTOR ACKNOWLEDGES THAT FAILURE TO IMPLEMENT APPROPRIATE EROSION AND SEDIMENT CONTROL MEASURES MAY BE SUBJECT TO PENALTIES IMPOSED BY ANY APPLICABLE REGULATORY AGENCY.

THE CONTRACTOR ACKNOWLEDGES THAT SURFACE EROSION AND SEDIMENT RUNOFF RESULTING FROM THEIR CONSTRUCTION OPERATIONS HAS POTENTIAL TO CAUSE A DETRIMENTAL IMPACT TO ANY DOWNSTREAM WATERCOURSE OR SEWER. AND THAT ALL CONSTRUCTION OPERATIONS THAT MAY IMPACT UPON WATER QUALITY SHALL BE CARRIED OUT IN MANNER THAT STRICTLY MEETS THE REQUIREMENT OF ALL APPLICABLE LEGISLATION AND REGULATIONS.

AS SUCH, THE CONTRACTOR SHALL BE RESPONSIBLE FOR CARRYING OUT THEIR OPERATIONS, AND SUPPLYING AND INSTALLING ANY APPROPRIATE CONTROL MEASURES, SO AS TO PREVENT SEDIMENT LADEN RUNOFF ENTERING ANY SEWER OR WATERCOURSE WITHIN OR DOWNSTREAM OF THE WORKING AREA.

THE CONTRACTOR ACKNOWLEDGES THAT NO ONE MEASURE IS LIKELY TO BE 100% EFFECTIVELY FOR EROSION PROTECTION AND CONTROLLING SEDIMENT RUNOFF AND DISCHARGES FROM THE SITE. THEREFORE, WHERE NECESSARY THE CONTRACTOR SHALL IMPLEMENT ADDITIONAL MEASURES ARRANGED IN SUCH MANNER AS TO MITIGATE SEDIMENT RELEASE FROM THE CONSTRUCTION OPERATIONS AND ACHIEVE SPECIFIC MAXIMUM PERMITTED CRITERIA WHERE APPLICABLE. SUGGESTED ON-SITE MEASURES MAY INCLUDE, BUT SHALL NOT BE LIMITED TO, THE FOLLOWING METHODS: FILTER BAGS, PUMP FILTERS, SILT FENCE, FILTER CLOTHS, CATCH BASIN FILTERS, AND/OR OTHER RECOGNIZED TECHNOLOGIES AND METHOD AVAILABLE AT THE TIME OF CONSTRUCTION. SPECIFIC MEASURES SHALL BE INSTALLED IN ACCORDANCE WITH REQUIREMENTS OF OPSS 805 WHERE APPROPRIATE, OR IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATIONS.

WHERE, IN THE OPINION OF THE CONTRACT ADMINISTRATOR OR REGULATORY AGENCY, THE INSTALLED CONTROL MEASURES FAIL TO PERFORM ADEQUATELY, THE CONTRACTOR SHALL SUPPLY AND INSTALL ADDITIONAL OR ALTERNATIVE MEASURES AS DIRECTED BY THE CONTRACT ADMINISTRATOR OR REGULATORY AGENCY, AS SUCH, THE CONTRACTOR SHALL HAVE ADDITIONAL CONTROL MATERIALS ON SITE AT ALL TIME WHICH ARE EASILY ACCESSIBLE AND MAY BE IMPLEMENTED BY HIM AT THE MOMENT'S NOTICE.

PRIOR TO COMMENCING WORK, THE CONTRACTOR SHALL SUBMIT TO THE CONTRACT ADMINISTRATOR SIX COPIES OF A DETAILED EROSION AND SEDIMENT CONTROL PLAN (ESCP). THE ESCP WILL CONSIST OF WRITTEN DESCRIPTION AND DETAILED DRAWINGS INDICATING THE ON-SITE ACTIVITIES AND MEASURES TO BE USED TO CONTROL EROSION AND SEDIMENT MOVEMENT FOR EACH STEP OF THE WORK.

CONTRACTOR'S RESPONSIBILITIES

THE CONTRACTOR SHALL ENSURE THAT ALL WORKERS, INCLUDING SUB-CONTRACTOR, IN THE WORKING ARE ARE AWARE OF THE IMPORTANCE OF THE EROSION AND SEDIMENT CONTROL MEASURES AND INFORMED OF THE CONSEQUENCES OF THE FAILURE TO COMPLY WITH THE REQUIREMENTS OF ALL REGULATORY AGENCIES.

THE CONTRACTOR SHALL PERIODICALLY, AND WHEN REQUESTED BY THE CONTRACT ADMINISTRATOR, CLEAN OUT ACCUMULATED SEDIMENT DEPOSITS AS REQUIRED AT THE SEDIMENT CONTROL DEVICES, INCLUDING THOSE DEPOSITS THAT MAY ORIGINATE FROM OUTSIDE THE CONSTRUCTION AREA. ACCUMULATED SEDIMENT SHALL BE REMOVED IN SUCH A MANNER THAT PREVENTS THE DEPOSITION OF THIS MATERIAL INTO THE SEWER WATERCOURSE AND AVOIDS DAMAGE TO CONTROL MEASURES. THE SEDIMENT SHALL BE REMOVED FROM THE SITE AT THE CONTRACTOR'S EXPENSE AND MANAGED IN COMPLIANCE WITH REQUIREMENTS FRO EXCESS EARTH MATERIAL, AS SPECIFIED ELSEWHERE IN THE CONTRACT.

THE CONTRACTOR SHALL IMMEDIATELY REPORT TO THE CONTRACT ADMINISTRATOR ANY ACCIDENTAL DISCHARGES OF SEDIMENT MATERIAL INTO EITHER THE WATERCOURSE OR THE STORM SEWER SYSTEM. FAILURE TO REPORT WILL BE CONSTITUTE A BRACH OF THIS SPECIFICATION AND THE CONTRACTOR MAY ALSO BE SUBJECT TO THE PENALTIES IMPOSED BY THE APPLICABLE REGULATORY AGENCY. APPROPRIATE RESPONSE MEASURES, INCLUDING ANY REPAIRS TO EXISTING CONTROL MEASURES OR THE IMPLEMENTATION OF ADDITIONAL CONTROL MEASURES, SHALL BE CARRIED OUT BY THE CONTRACTOR WITHOUT DELAY.

THE SEDIMENT CONTROL MEASURES SHALL ONLY BE REMOVED WHEN, IN THE OPINION OF THE CONTRACT ADMINISTRATOR, THE MEASURE OR MEASURES, IS NO LONGER REQUIRED. NO CONTROL MEASURE MAY BE PERMANENTLY REMOVED WITHOUT PRIOR AUTHORIZATION FROM THE CONTRACT ADMINISTRATOR. ALL SEDIMENT AND EROSION CONTROL MEASURES SHALL BE REMOVED IN A MANNER THAT AVOIDS THE ENTRY OF ANY EQUIPMENT, OTHER THAN HAND-HELD EQUIPMENT, INTO ANY WATERCOURSE, AND PREVENTS THE RELEASE OF ANY SEDIMENT OR DEBRIS INTO ANY SEWER OR WATERCOURSE WITHIN OR DOWNSTREAM OF THE WORKING AREA. ALL ACCUMULATED SEDIMENT SHALL BE REMOVED FROM THE WORKING AREA AT THE CONTRACTOR'S EXPENSE AND MANAGED IN COMPLIANCE WITH THE REQUIREMENTS FOR EXCESS EARTH MATERIAL

WHERE, IN THE OPINION OF EITHER THE CONTRACT ADMINISTRATOR OR A REGULATORY AGENCY, ANY OF THE TERMS SPECIFIED HEREIN HAVE NOT BEEN COMPLIED WITH OR PERFORMED IN A SUITABLE MANNER, OR TAT ALL, THE CONTRACTOR ADMINISTRATOR OR A REGULATORY AGENCY HAS THE RIGHT TO IMMEDIATELY WITHDRAW ITS PERMISSION TO CONTINUE THE WORK BUT MAY RENEW ITS PERMISSION UPON BEING SATISFIED THAT THE DEFAULTS OR DEFICIENCIES IN THE PERFORMANCE OF THIS SPECIFICATION BY THE CONTRACTOR HAVE BEEN REMEDIED.

SPILL CONTROL NOTES

- 1. ALL CONSTRUCTION EQUIPMENT SHALL BE RE-FUELED, MAINTAINED, AND STORED NO LESS THAN 30 METRES FROM WATERCOURSE, STEAMS, CREEKS, WOODLOTS, AND ANY ENVIRONMENTALLY SENSITIVE AREAS, OR AS OTHERWISE SPECIFIED. 2. THE CONTRACTOR MUST IMPLEMENT ALL NECESSARY MEASURES IN ORDER TO PREVENT LEAKS, DISCHARGES OR SPILLS OF POLLUTANTS,
- DELETERIOUS MATERIALS, OR OTHER SUCH MATERIALS OR SUBSTANCES WHICH WOULD OR COULD CAUSE AN ADVERSE IMPACT TO THE NATURAL ENVIRONMENT
- 3. IN THE EVENT OF A LEAK, DISCHARGE OR SPILL OF POLLUTANT, DELETERIOUS MATERIAL OR OTHER SUCH MATERIAL OR SUBSTANCE WHICH WOULD OR COULD CAUSE AN ADVERSE IMPACT TO THE NATURAL ENVIRONMENT, THE CONTRACTOR SHALL: 3.1. IMMEDIATELY NOTIFY APPROPRIATE FEDERAL, PROVINCIAL, AND LOCAL GOVERNMENT MINISTRIES, DEPARTMENTS, AGENCIES, AND
- AUTHORITIES OF THE INCIDENT IN ACCORDANCE WITH ALL CURRENT LAWS, LEGISLATION, ACTS, BY-LAWS, PERMITS, APPROVALS, ETC 3.2. TAKE IMMEDIATE MEASURES TO CONTAIN THE MATERIAL OR SUBSTANCE, AND TO TAKE SUCH MEASURES TO MITIGATE AGAINST
- ADVERSE IMPACTS TO THE NATURAL ENVIRONMENT 3.3. RESTORE THE AFFECTED AREA TO THE ORIGINAL CONDITION OR BETTER TO THE SATISFACTION OF THE AUTHORITIES HAVING JURISDICTION

MUD MAT NOTES

- 1. THE GRANULAR MATERIAL WILL REQUIRE PERIODIC REPLACEMENT AS IT BECOMES CONTAMINATED BY VEHICLE TRAFFIC.
- 2. SEDIMENT SHALL BE CLEANED FROM PUBLIC ROADS AT THE END OF EACH DAY. 3. SEDIMENT SHALL BE REMOVED FROM PUBLIC ROADS BY SHOVELING OR SWEEPING AND DISPOSED OR PROPERLY IN A CONTROLLED SEDIMENT DISPOSAL AREA.

SITE GRADING NOTES

- EROSION CONTROL PLAN
- RECOMMENDATIONS
- OF CONSTRUCTION.
- AND OPSS 310
- 7. SUB-EXCAVATE SOFT AREAS AND FILL WITH GRANULAR 'B' COMPACTED IN MAXIMUM 300MM LIFTS.
- REQUIRED BY THE MUNICIPALITY.
- SYMBOLS SHALL BE APPLIED WITH A MINIMUM OF TWO COATS OF ORGANIC SOLVENT PAINT.
- 11. REFER TO ARCHITECTURAL SITE PLAN FOR DIMENSIONS AND SITE DETAILS.
- STANDARDS
- 15. ROADWORK TO BE COMPLETED IN ACCORDANCE WITH GEOTECHNICAL REPORT.
- AND STOCK PILLED ON SITE AS DIRECTED BY NATIONAL MUNICIPALITY.

SANITARY, FOUNDATION DRAIN, STORM SEWER AND WATERMAIN NOTES

<u>GENERAL</u>

- 1. LASER ALIGNMENT CONTROL TO BE UTILIZED ON ALL SEWER INSTALLATIONS. AND AT 60M INTERVALS IN THE SERVICE TRENCHES.
- PROCTOR DENSITY, A MINIMUM OF 300MM AROUND STRUCTURES.
- ADJUSTING UNITS ON THE OUTSIDE ONLY.
- 6. SAFETY PLATFORMS SHALL BE PER OPSD 404.02.
- 7. DROP STRUCTURES SHALL BE IN ACCORDANCE WITH OPSD 1003.01, IF APPLICABLE.
- SATISFACTION OF THE ENGINEER

SANITARY

- STANDARD DRAWINGS (OPSD). AND SPECIFICATIONS (OPSS).
- AMENDMENT, UNLESS SPECIFIED OTHERWISE
- OTHERWISE.
- 16. SANITARY MAINTENANCE STRUCTURES SHALL BE BENCHED PER OPSD 701.021.
- DRAWING SSP-1

<u>STORM</u>

- GASKETS AS PER CSA A257.3, OR LATEST AMENDMENT.

- 21. CATCH BASIN SHALL BE IN ACCORDANCE WITH OPSD 705.010.
- 23. ALL CATCH BASINS SHALL HAVE 600MM SUMPS, UNLESS SPECIFIED OTHERWISE.
- 24. ALL CATCH BASIN LEAD INVERTS TO BE 1.5M BELOW FINISHED GRADE UNLESS SPECIFIED OTHERWISE. 25. THE STORM SEWER CLASSES HAVE BEEN DESIGNED BASED ON BEDDING CONDITIONS SPECIFIED ABOVE. WHERE THE SPECIFIED TRENCH WIDTH IS
- EXCEEDED , THE CONTRACTOR IS REQUIRED TO PROVIDE AND SHALL BE RESPONSIBLE FOR EXTRA TEMPORARY AND/OR PERMANENT REPAIRS MADE NECESSARY BY THE WIDENED TRENCH.
- 26. ALL ROAD AND PARKING LOT CATCH BASINS TO BE INSTALLED WITH ORTHOGONALLY PLACED SUBDRAINS IN ACCORDANCE WITH DETAIL.
- PERFORATED SUBDRAIN FOR ROAD AND PARKING LOT CATCH BASIN SHALL BE INSTALLED PER CITY STD R1 UNLESS OTHERWISE NOTED. 27. PERFORATED SUBDRAIN FOR REAR YARD AND LANDSCAPING APPLICATIONS SHALL BE INSTALLED PER CITY STD S29, S30 AND S31, WHERE
- APPLICABLE
- 28. RIP-RAP TREATMENT SEWER AND CULVERT OUTLETS PER OPSD 810.010. 29. ALL STORM SEWER/ CULVERTS TO BE INSTALLED WITH FROST TREATMENT PER OPSD 803.031 WHERE APPLICABLE.
- 30. ALL STORM MANHOLES WITH PIPE LESS THAN 900MM IN DIAMETER SHALL BE CONSTRUCTED WITH A 300MM SUMP AS PER SDG, CLAUSE 6.2.6.

WATERMAIN

- 31. ALL WATERMAIN INSTALLATION SHALL CONFORM TO THE LATEST REVISIONS OF THE CITY OF OTTAWA AND THE ONTARIO PROVINCIAL STANDARD
- DRAWINGS (OPSD) AND SPECIFICATIONS (OPSS).
- 32. ALL PVC WATERMAINS SHALL BE AWWA C-900 CLASS 150, SDR 18 OR APPROVED EQUIVALENT. 33. ALL WATER SERVICES LESS THAN OR EQUAL TO 50MM IN DIAMETER TO BE TYPE 'K' COPPER.
- 34. WATERMAIN TRENCH AND BEDDING SHALL BE IN ACCORDANCE WITH CITY OF OTTAWA STANDARD W17. UNLESS SPECIFIED OTHERWISE. BEDDING AND COVER MATERIAL SHALL BE SPECIFIED BY THE PROJECT GEOTECHNICAL ENGINEER.
- 35. ALL PVC WATERMAINS, SHALL BE INSTALLED WITH A 10 GAUGE STRANDED COPPER TWU OR RWU TRACER WIRE IN ACCORDANCE WITH CITY OF OTTAWA STD. W.36
- 36. CATHODIC PROTECTION IS REQUIRED ON ALL METALLIC FITTINGS PER CITY OF OTTAWA STD.25.5 AND W25.6.
- 37. VALVE BOXES SHALL BE INSTALLED PER CITY OF OTTAWA STD W24. 38. WATERMAIN IN FILL AREAS TO BE INSTALLED WITH RESTRAINED JOINTS PER CITY OF OTTAWA STD.25.5 AND W25.6.
- 39. THRUST BLOCKING OF WATERMAINS TO BE INSTALLED PER CITY OF OTTAWA STD. W25.3 AND W25.4. 40. THE CONTRACTOR SHALL PROVIDE ALL TEMPORARY CAPS, PLUGS, BLOW-OFFS, AND NOZZLES REQUIRED FOR TESTING AND DISINFECTION OF THE
- WATERMAIN
- 2 4 M
- WATER PIPE SHALL BE CENTERED AT THE POINT OF CROSSING TO ENSURE THAT THE JOINTS WILL BE EQUIDISTANT AND AS FAR AS POSSIBLE FROM THE SEWER
- 45. GENERAL WATER PLANT TO UTILITY CLEARANCE AS PER STD DWG R20.

BACK FROM STUB.

41. WATERMAIN CROSSING OVER AND BELOW SEWERS SHALL BE IN ACCORDANCE WITH THE CITY OF OTTAWA STD. W25,2 AND W25, RESPECTIVELY. 42. WATER SERVICES ARE TO BE INSULATED PER CITY STD. W23 WHERE SEPARATION BETWEEN SERVICES AND MAINTENANCE HOLES ARE LESS THAN 43. THE MINIMUM VERTICAL CLEARANCE BETWEEN WATERMAIN AND SEWER/UTILITY IS 0.5M PER MOE GUIDELINES. FOR CROSSING UNDER SEWERS, ADEQUATE STRUCTURAL SUPPORT FOR THE SEWER IS REQUIRED TO PREVENT EXCESSIVE DEFLECTION OF JOINTS AND SETTLING. THE LENGTH OF

44. ALL WATERMAINS SHALL HAVE A MINIMUM COVER OR 2.4M, OTHERWISE THERMAL INSULATION IS REQUIRED AS PER STD DWG W22.

46. FIRE HYDRANT INSTALLATION AS PER STD DWG W19, ALL BOTTOM OF HYDRANT FLANGE ELEVATIONS TO BE INSTALLED 0.10M ABOVE PROPOSED FINISHED GRADE AT HYDRANT; FIRE HYDRANT LOCATION AS PER STD DWG W18. 47. BUILDING SERVICE TO BE CAPPED 1.0M OFF THE FACE OF THE BUILDING UNLESS OTHERWISE NOTED AND MUST BE RESTRAINED A MINIMUM OF 12M

48. ALL WATERMAINS SHALL BE HYDROSTATICALLY TESTED IN ACCORDANCE WITH THE CITY OF OTTAWA AND ONTARIO GUIDELINES UNLESS OTHERWISE DIRECTED. PROVISIONS FOR FLUSHING WATER LINE PRIOR TO TESTING, ETC. MUST BE PROVIDED. 49. ALL WATERMAINS SHALL BE BACTERIOLOGICALLY TESTED IN ACCORDANCE WITH THE CITY OF OTTAWA AND ONTARIO GUIDELINES. ALL

CHLORINATED WATER TO BE DISCHARGED AND PRETREATED TO ACCEPTABLE LEVELS PRIOR TO DISCHARGE. ALL DISCHARGED WATER MUST BE CONTROLLED AND TREATED SO AS NOT TO ADVERSELY EFFECT ENVIRONMENT. IT IS RESPONSIBILITY OF THE CONTRACTOR TO ENSURE THAT ALL MUNICIPAL AND/OR PROVINCIAL REQUIREMENTS ARE FOLLOWED.

50. ALL WATERMAIN STUBS SHALL BE TERMINATED WITH A PLUG AND 50MM BLOW OFF UNLESS OTHERWISE NOTED.

20. ALL PVC STORM SEWERS ARE TO BE SDR 35 APPROVED PER C.S.A. B182.2 OR LATEST AMENDMENT, UNLESS OTHERWISE SPECIFIED. 22. CATCH BASIN LEADS SHALL BE IN 200MM DIA. AT 1% SLOPE (MIN) UNLESS SPECIFIED OTHERWISE

SPECIFIED. BEDDING AND COVER MATERIAL SHALL BE SPECIFIED BY PROJECT GEOTECHNICAL ENGINEER.

19. ALL STORM SEWER TRENCH AND BEDDING SHALL BE IN ACCORDANCE WITH THE CITY OF OTTAWA STD. S6 AND S7 CLASS 'B' UNLESS OTHERWISE

CONCRETE STORM SEWER PIPE SHALL BE IN ACCORDANCE WITH CSA A257.1, OR LATEST AMENDMENT. PIPE SHALL BE JOINED WITH STD. RUBBER

18. ALL REINFORCED CONCRETE STORM SEWER PIPE SHALL BE IN ACCORDANCE WITH CSA A257.2, OR LATEST AMENDMENT. ALL NON-REINFORCED

17. 100MM THICK HIGH-DENSITY GRADE 'A' POLYSTYRENE INSULATION TO BE INSTALLED IN ACCORDANCE WITH CITY STD W22 WHERE INDICATED ON

15. SANITARY MAINTENANCE STRUCTURE FRAME AND COVERS SHALL BE PER CITY OF OTTAWA STD. S24 AND S25.

13. EXISTING MAINTENANCE STRUCTURES TO BE RE-BENCHED WHERE A NEW CONNECTION IS MADE. 14. SANITARY GRAVITY SEWER TRENCH AND BEDDING SHALL BE PER CITY OF OTTAWA STD. S6 AND S7 CLASS 'B' BEDDING, UNLESS SPECIFIED

11. ALL SANITARY SEWER INSTALLATION SHALL CONFORM TO THE LATEST REVISIONS OF THE CITY OF OTTAWA AND THE ONTARIO PROVINCIAL 12. ALL SANITARY GRAVITY SEWER SHALL BE PVC SDR 35, IPEX 'RING-TITE' (OR APPROVED EQUIVALENT) PER CSA STANDARD B182.2 OR LATEST

ENTIRE WIDTH OF THE CITY'S ROAD SURFACE, CURB TO CURB; ENSURING A MIN. 50mm ASPHALT OVERLAY TO MEET CITY STANDARDS.

9. CONTRACTOR SHALL PERFORM LEAKAGE TESTING, IN THE PRESENCE OF THE CONSULTANT, FOR SANITARY SEWERS IN ACCORDANCE WITH OPSS 407. CONTRACTOR SHALL PERFORM VIDEO INSPECTION OF ALL SEWERS. A COPY OF THE VIDEO AND INSPECTION REPORT SHALL BE SUBMITTED TO THE CONSULTANT FOR REVIEW AND APPROVAL PRIOR TO PLACEMENT OF WEAR COURSE ASPHALT 10. FOLLOWING INSTALLATION/ CONNECTION OF SERVICES WITHIN THE CITY'S RIGHT-OF-WAY. THE CONTRACTOR MUST ENSURE AND REPAVE THE

VIDEO RECORDING IN A FORMAT ACCEPTABLE TO ENGINEER. ALL SEWER ARE TO BE FLUSHED PRIOR TO CAMERA INSPECTION. ASPHALT WEAR COURSE SHALL NOT BE PLACED UNTIL THE VIDEO INSPECTION OF SEWERS AND NECESSARY REPAIRS HAVE BEEN COMPLETED TO THE

8. THE CONTRACTOR IS TO PROVIDE CCTV CAMERA INSPECTIONS OF ALL SEWERS, INCLUDING PICTORIAL REPORT, ONE (1) CD COPY AND TWO (2)

5. "MODULOC" OR APPROVED PRE-CAST MAINTENANCE STRUCTURE AND CATCH BASIN ADJUSTERS TO BE USED IN LIEU OF BRICKING. PARGE

3. SERVICES TO BUILDING TO BE TERMINATED 1.0M FROM THE OUTSIDE FACE OF BUILDING UNLESS OTHERWISE NOTED. 4. ALL MAINTENANCE STRUCTURE AND CATCH BASIN EXCAVATIONS TO BE BACKFILLED WITH GRANULAR MATERIAL COMPACTED TO 98% STANDARD

2. CLAY SEALS TO BE INSTALLED AS PER CITY STANDARD DRAWING S8. THE SEALS SHOULD BE AT LEAST 1.5M LONG (IN THE TRENCH DIRECTION) AND SHOULD EXTEND FROM TRENCH WALL TO TRENCH WALL. THE SEALS SHOULD EXTEND FROM THE FROST LINE AND FULLY PENETRATE THE BEDDING, SUB-BEDDING, AND COVER MATERIAL. THE BARRIERS SHOULD CONSIST OF RELATIVELY DRY AND COMPATIBLE BROWN SILTY CLAY PLACED IN MAXIMUM 225MM LIFTS AND COMPACTED TO A MINIMUM OF 95% SPMDD. THE CLAY SEALS SHOULD BE PLACED AT THE SITE BOUNDARIES

16. ALL TOPSOIL AND ORGANIC MATERIAL SHALL BE STRIPPED WITHIN THE ROAD ALLOWANCE PRIOR TO THE COMMENCEMENT OF CONSTRUCTION 17. SUB-EXCAVATE SOFT AREAS AND FILL WITH GRANULAR 'A', TYPE II COMPACTED IN MAXIMUM 300MM LIFTS.

14. WHERE APPLICABLE THE CONTRACTOR IS TO SUBMIT SHOP DRAWINGS TO THE ENGINEER FOR APPROVAL PRIOR TO CONSTRUCTION. SHOP DRAWINGS MUST BE SITE SPECIFIC, SIGNED AND SEALED BY A LICENSED STRUCTURAL ENGINEER. THE CONTRACTOR WILL ALSO BE REQUIRED TO SUPPLY AND GEOTECHNICAL CERTIFICATION OF THE AS-CONSTRUCTED RETAINING WALL TO THE ENGINEER PRIOR TO FINAL ACCEPTANCE.

12. STEP JOINTS ARE TO BE USED WHERE PROPOSED ASPHALT MEETS EXISTING ASPHALT, ALL JOINTS MUST BE SEALED. 13. SIDEWALKS TO BE 13MM & BEVELED AT 2:1 OR 6MM WITH NO BEVEL REQUIRED BELOW THE FINISHED FLOOR SLAB ELEVATION AT ENTRANCES REQUIRED TO BE BARRIER-FREE, UNLESS OTHERWISE NOTED. ALL IN ACCORDANCE WITH OBC 3.8.1.3 & OTTAWA ACCESSIBILITY DESIGN

10. ALL PAVEMENT MARKING FEATURES AND SITE SIGNAGE SHALL BE PLACED PER ARCHITECTURAL SITE PLAN. LINE PAINTING AND DIRECTIONAL

9. CONTRACTOR TO OBTAIN A ROAD OCCUPANCY PERMIT 48 HOURS PRIOR TO COMMENCING ANY WORK WITHIN THE MUNICIPAL ROAD ALLOWANCE, IF

6. GRANULAR 'A' SHALL BE PLACED TO A MINIMUM THICKNESS OF 300MM AROUND ALL STRUCTURES WITHIN THE PAVEMENT AREA. 8. ALL WORK ON THE MUNICIPAL RIGHT OF WAY AND EASEMENTS TO BE INSPECTED BY THE MUNICIPALITY PRIOR BACKFILLING.

4. CONCRETE CURB SHALL BE IN ACCORDANCE WITH THE CITY OF OTTAWA STD. SC1.1 OR OPSD 600.110. PROVISION SHALL BE MADE OR CURB DEPRESSIONS AS INDICATED ON ARCHITECTURAL SITE PLAN. CONCRETE SIDEWALK SHALL BE IN ACCORDANCE WITH CITY OF OTTAWA STD SC1.4. ALL CURBS, CONCRETE ISLANDS, AND SIDEWALKS SHOWN ON THIS DRAWING ARE TO BR PRICED IN SITE WORKS PORTION OF THE CONTRACT. 5 PAVEMENT REINSTATEMENT FOR SERVICE AND UTILITY CUTS SHALL BE IN ACCORDANCE WITH THE CITY OF OTTAWA STD R10 AND OPSD 509 010

3. ALL TOPSOIL AND ORGANIC MATERIAL SHALL BE STRIPPED WITHIN THE ROAD AND PARKING AREAS ALLOWANCE PRIOR TO THE COMMENCEMENT

1. PRIOR TO THE COMMENCEMENT OF THE SITE GRADING WORKS, ALL SILTATION CONTROL DEVICES SHALL BE INSTALLED AND OPERATIONAL PER 2. ALL GRANULAR AND PAVEMENT FOR ROADS/PARKING AREAS SHALL BE CONSTRUCTED IN ACCORDANCE WITH GEOTECHNICAL ENGINEER'S

USE AND INTERPRETATION OF DRAWINGS

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IN THE EVENT THE CLIENT, THE CLIENT'S CONTRACTORS OR SUBCONTRACTORS, OF

UNAUTHORIZED CHANGES:

ANYONE FOR WHOM THE CLIENT IS LEGALLY LIABLE MAKES OR PERMITS TO BI ADE ANY CHANGES TO ANY REPORTS, PLANS, SPECIFICATIONS OR OTH CONSTRUCTION DOCUMENTS PREPARED BY LRL ASSOCIATES LTD. (LRL) WITHOUT OBTAINING LRL'S PRIOR WRITTEN CONSENT, THE CLIENT SHALL ASSUME F RESPONSIBILITY FOR THE RESULTS OF SUCH CHANGES. THEREFORE THE CLIENT AGREES TO WAIVE ANY CLAIM AGAINST LRL AND TO RELEASE LRL FROM ANY IABILITY ARISING DIRECTLY OR INDIRECTLY FROM SUCH UNAUTHORIZED CHANGES.

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| 05 | RE-ISSUED FOR APPROVAL | S.V. | 18 OCT 2024 |
|-----|------------------------|------|--------------|
| 04 | RE-ISSUED FOR APPROVAL | S.V. | 16 JULY 2024 |
| 03 | RE-ISSUED FOR APPROVAL | S.V. | 03 MAY 2024 |
| 02 | RE-ISSUED FOR APPROVAL | Т.Н. | 14 APR 2023 |
| 01 | ISSUED FOR APPROVAL | Т.Н. | 11 OCT 2022 |
| No. | REVISIONS | BY | DATE |
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GSI PROPERTIES

APPROVED BY Т.Н. V.J. Т.Н.

PROJECT PROPOSED 8-STOREY MULTI-UNIT BUILDING 424 CHURCHILL AVE

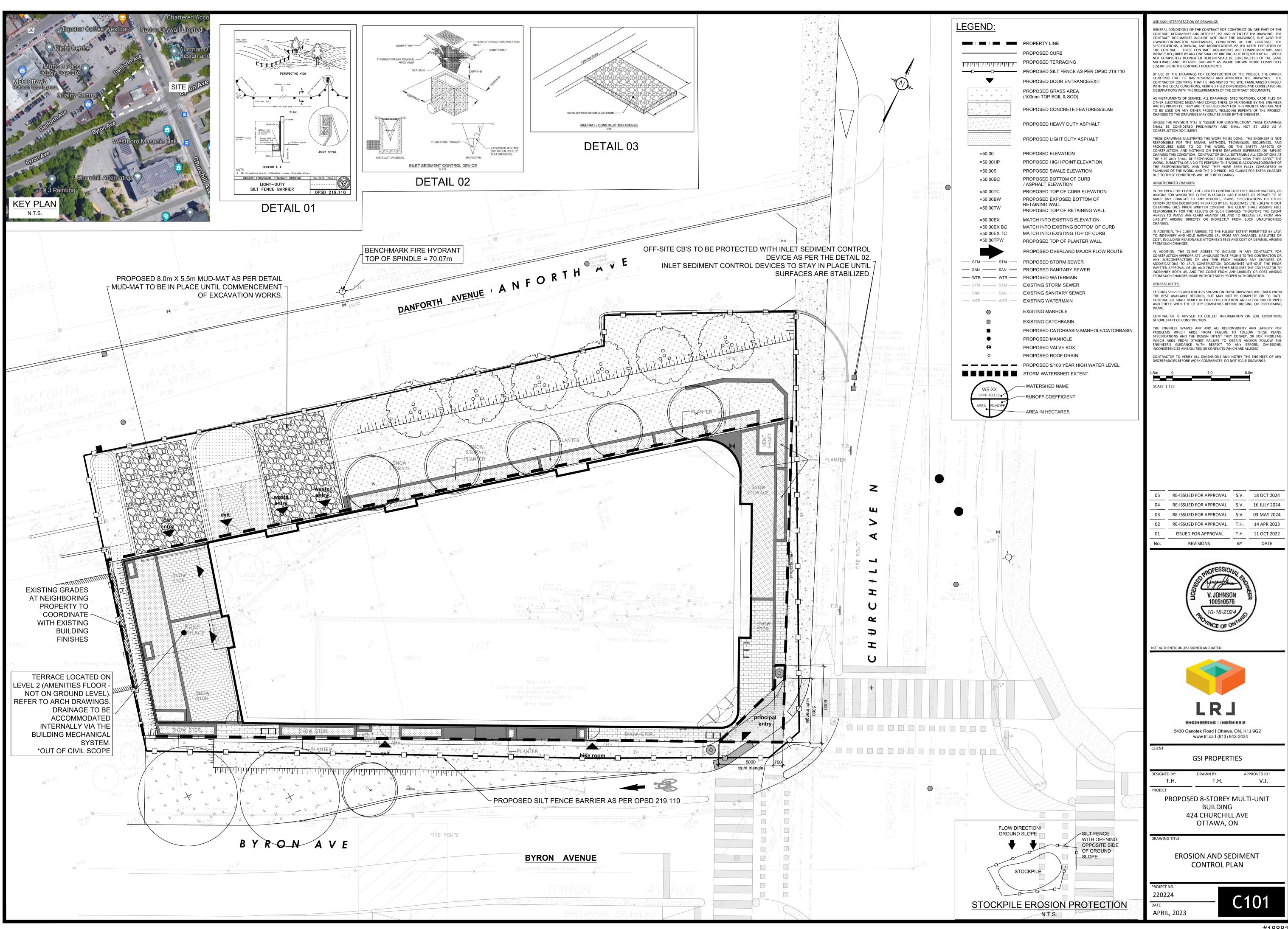
OTTAWA, ON

GENERAL NOTES

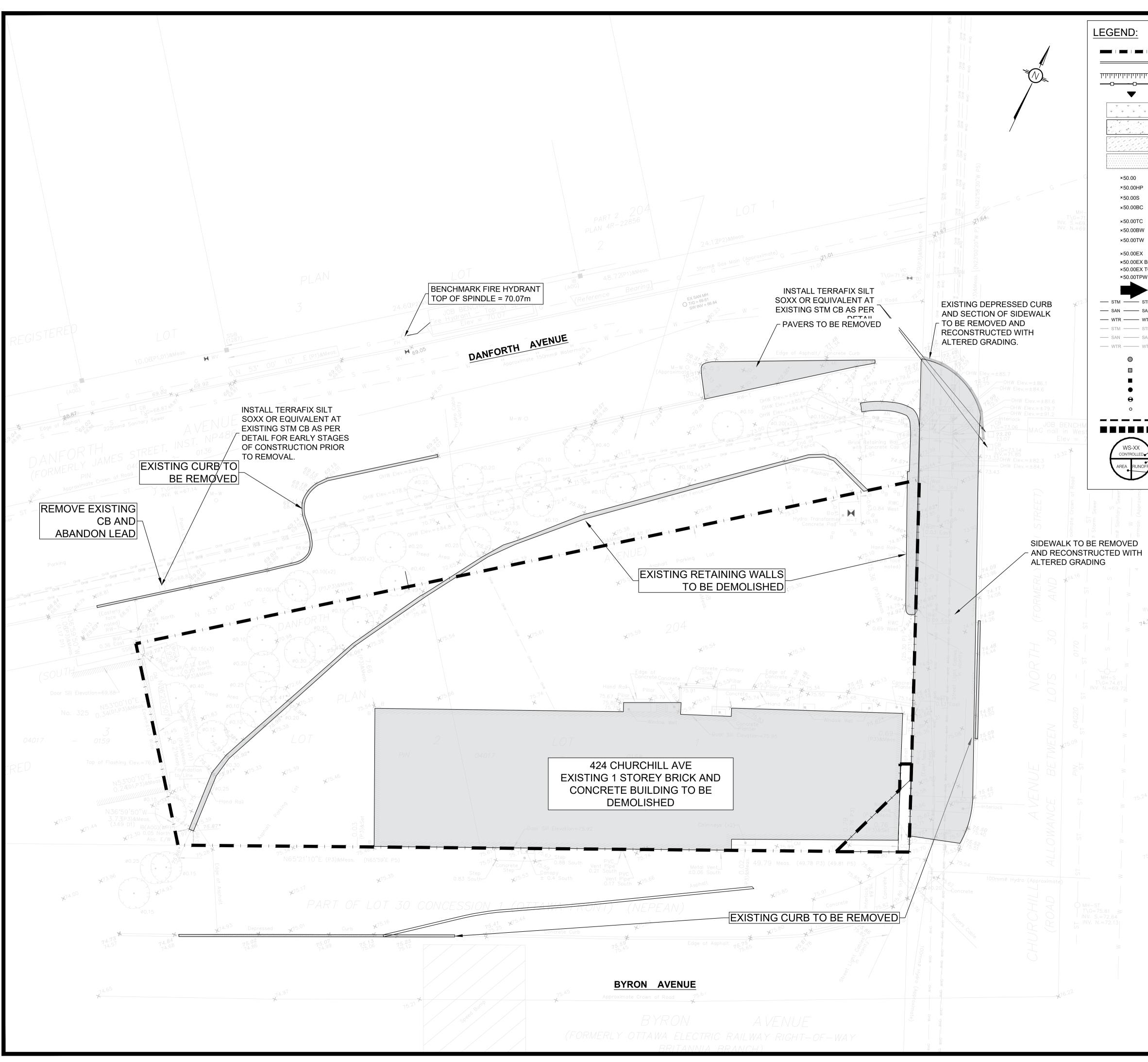
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APRIL, 2023

DRAWING TITLE



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PROPOSED CURB PROPOSED TERRACING PROPOSED SILT FENCE AS PER OPSD 219.110 PROPOSED DOOR ENTRANCE/EXIT PROPOSED GRASS AREA (100mm TOP SOIL & SOD) PROPOSED CONCRETE FEATURES/SLAB PROPOSED HEAVY DUTY ASPHALT PROPOSED LIGHT DUTY ASPHALT PROPOSED ELEVATION PROPOSED HIGH POINT ELEVATION PROPOSED SWALE ELEVATION PROPOSED BOTTOM OF CURB / ASPHALT ELEVATION PROPOSED TOP OF CURB ELEVATION PROPOSED EXPOSED BOTTOM OF RETAINING WALL PROPOSED TOP OF RETAINING WALL MATCH INTO EXISTING ELEVATION MATCH INTO EXISTING BOTTOM OF CURB MATCH INTO EXISTING TOP OF CURB PROPOSED TOP OF PLANTER WALL PROPOSED OVERLAND MAJOR FLOW ROUTE PROPOSED STORM SEWER PROPOSED SANITARY SEWER PROPOSED WATERMAIN EXISTING STORM SEWER EXISTING SANITARY SEWER EXISTING WATERMAIN EXISTING MANHOLE EXISTING CATCHBASIN PROPOSED CATCHBASIN-MANHOLE/CATCHBASIN PROPOSED MANHOLE PROPOSED VALVE BOX PROPOSED ROOF DRAIN PROPOSED 5/100 YEAR HIGH WATER LEVEL STORM WATERSHED EXTENT - WATERSHED NAME -RUNOFF COEFFICIENT - AREA IN HECTARES

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SCALE: 1:125

____ 05 RE-ISSUED FOR APPROVAL S.V. 18 OCT 2024 RE-ISSUED FOR APPROVAL S.V. 16 JULY 2024 04 RE-ISSUED FOR APPROVAL S.V. 03 MAY 2024 03 RE-ISSUED FOR APPROVAL T.H. 14 APR 2023 02 ISSUED FOR APPROVAL T.H. 11 OCT 2022 01 DATE REVISIONS BY



NOT AUTHENTIC UNLESS SIGNED AND DATE



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GSI PROPERTIES

APPROVED BY: DRAWN B Т.Н. V.J. T.H.

PROJECT **PROPOSED 8-STOREY MULTI-UNIT** BUILDING

424 CHURCHILL AVE OTTAWA, ON

DRAWING TITLE

DESIGNED B

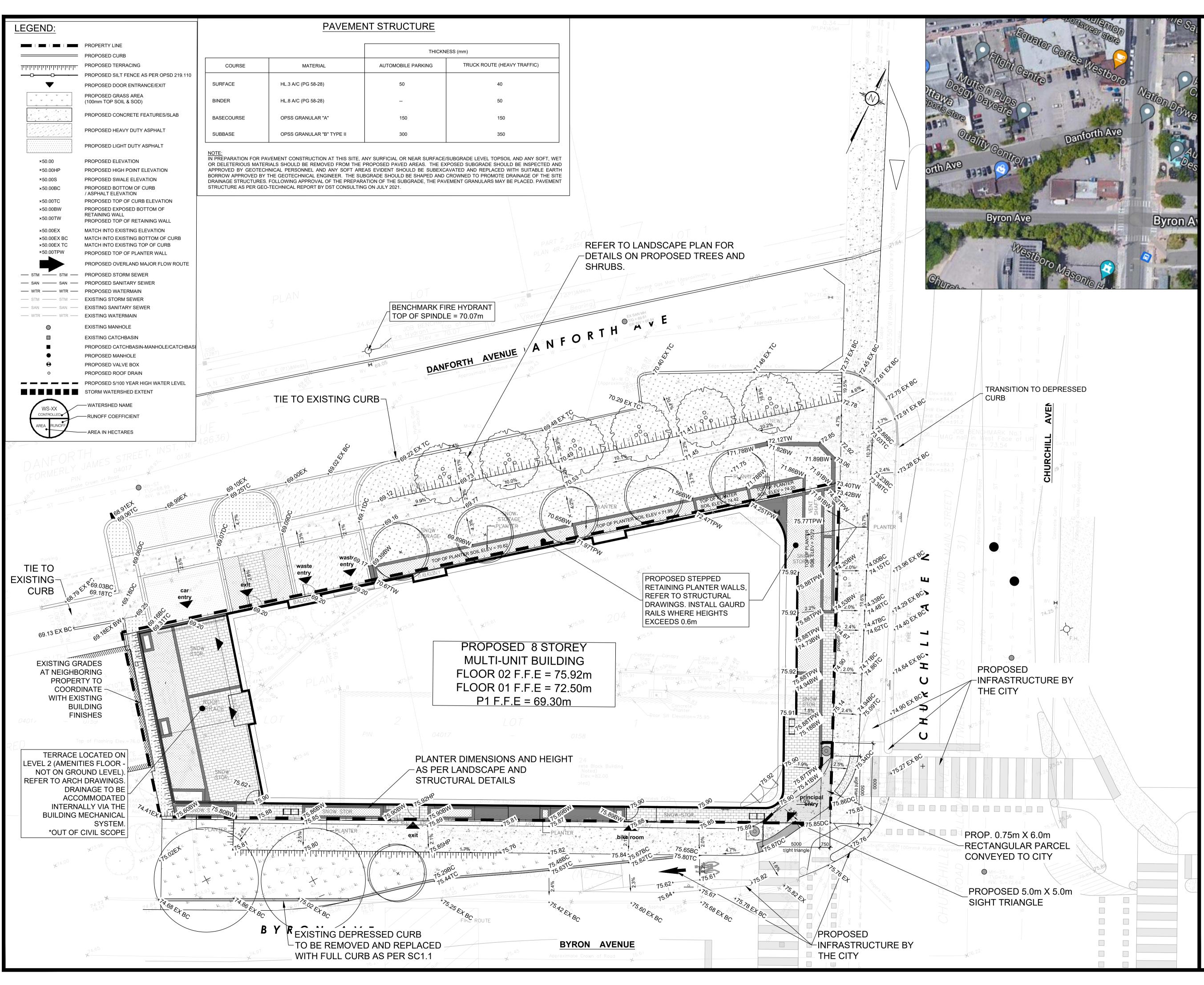
DEMOLITION PLAN

PROJECT NO. 220224 DATE

APRIL, 2023



#18881



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5430 Canotek Road | Ottawa, ON, K1J 9G2 www.lrl.ca | (613) 842-3434

GSI PROPERTIES

DESIGNED BY: DRAWN BY: APPROVED BY: T.H. T.H. V.J. PROJECT

PROPOSED 8-STOREY MULTI-UNIT BUILDING 424 CHURCHILL AVE OTTAWA, ON

DRAWING TITLE

GRADING AND DRAINAGE PLAN

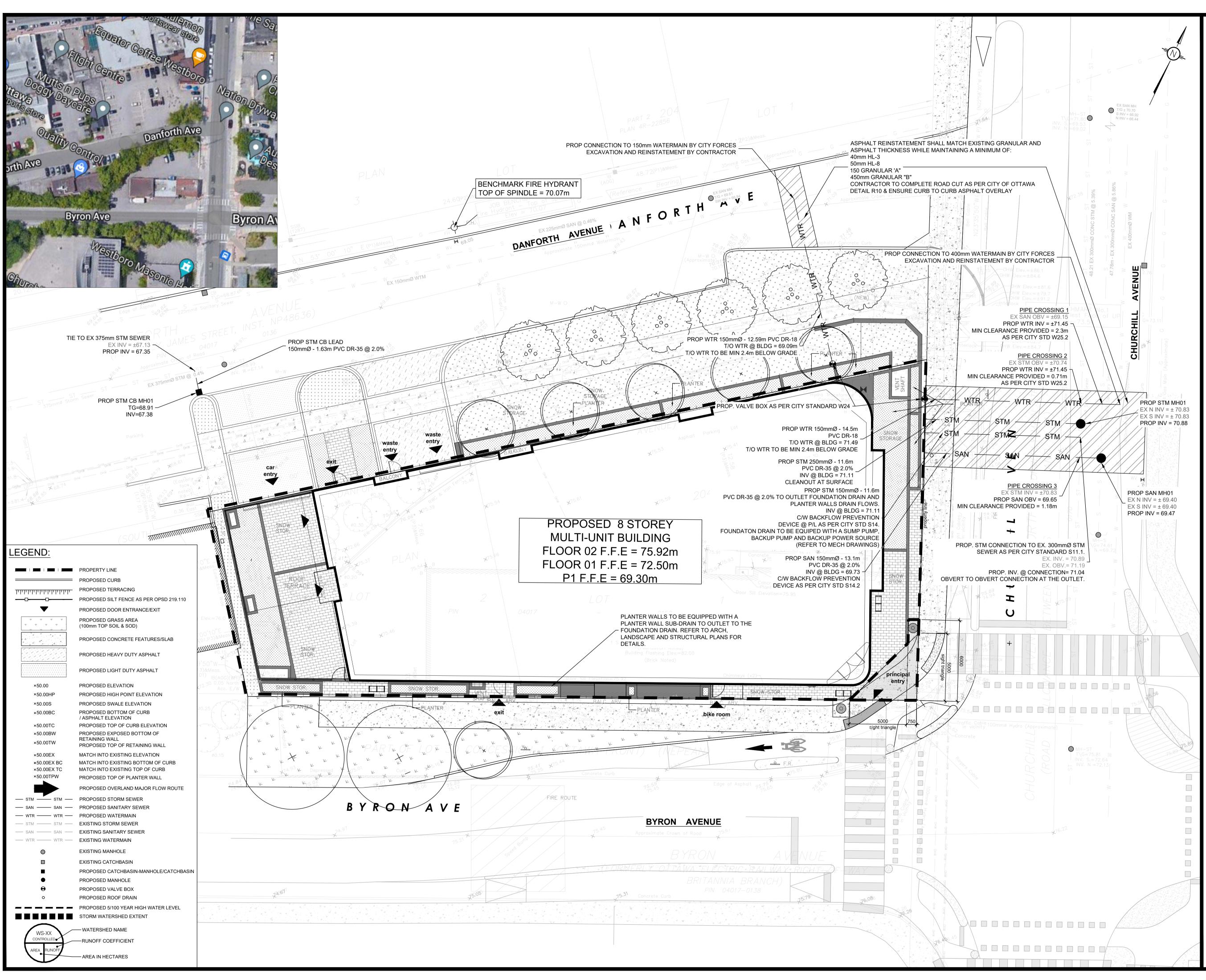
PROJECT NO.
220224
DATE

APRIL, 2023

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PROJECT

PROPOSED 8-STOREY MULTI-UNIT BUILDING 424 CHURCHILL AVE OTTAWA, ON

DRAWING TITLE

PROJECT NO.

220224

APRIL, 2023

DATE

SERVICING PLAN



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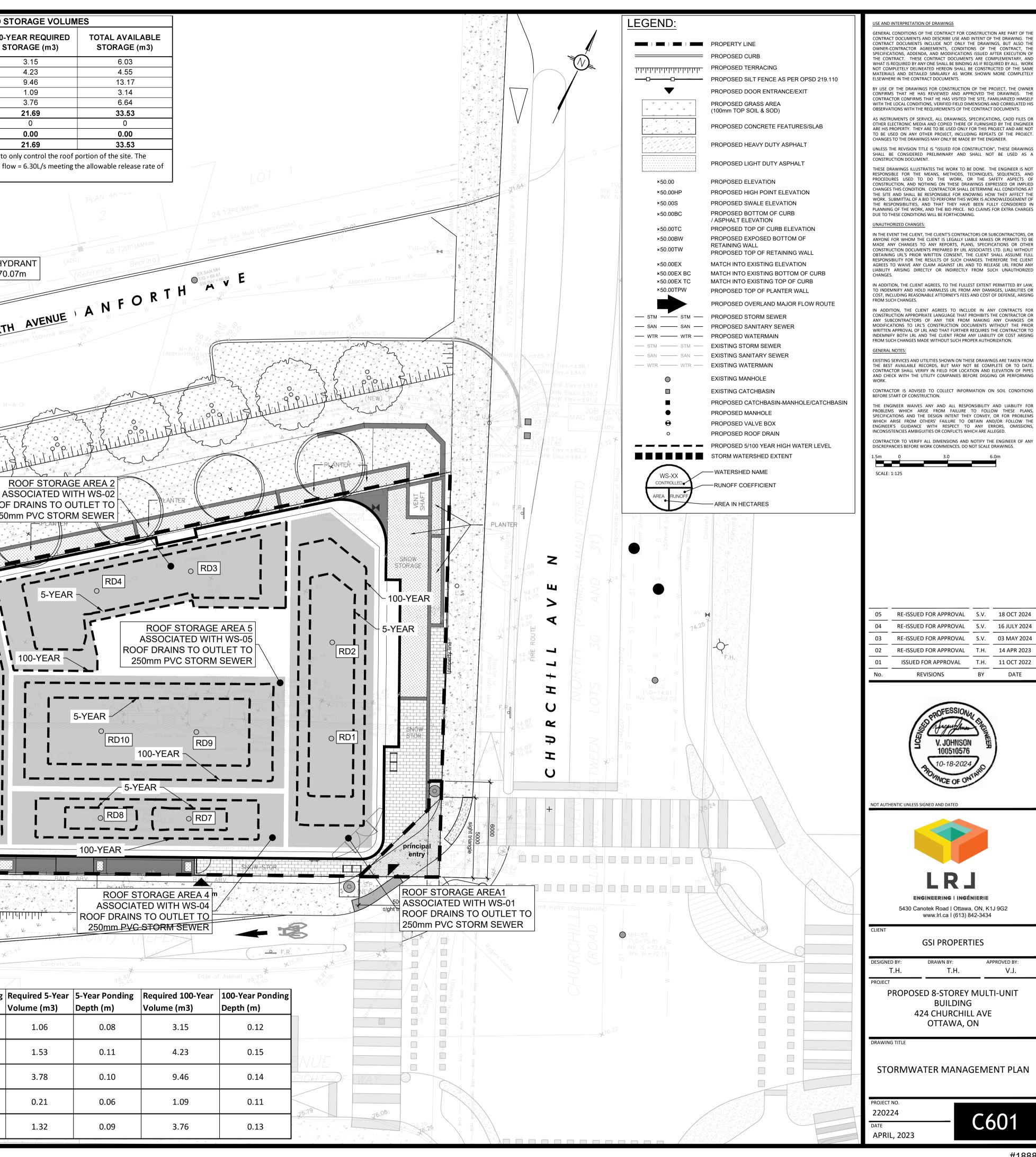
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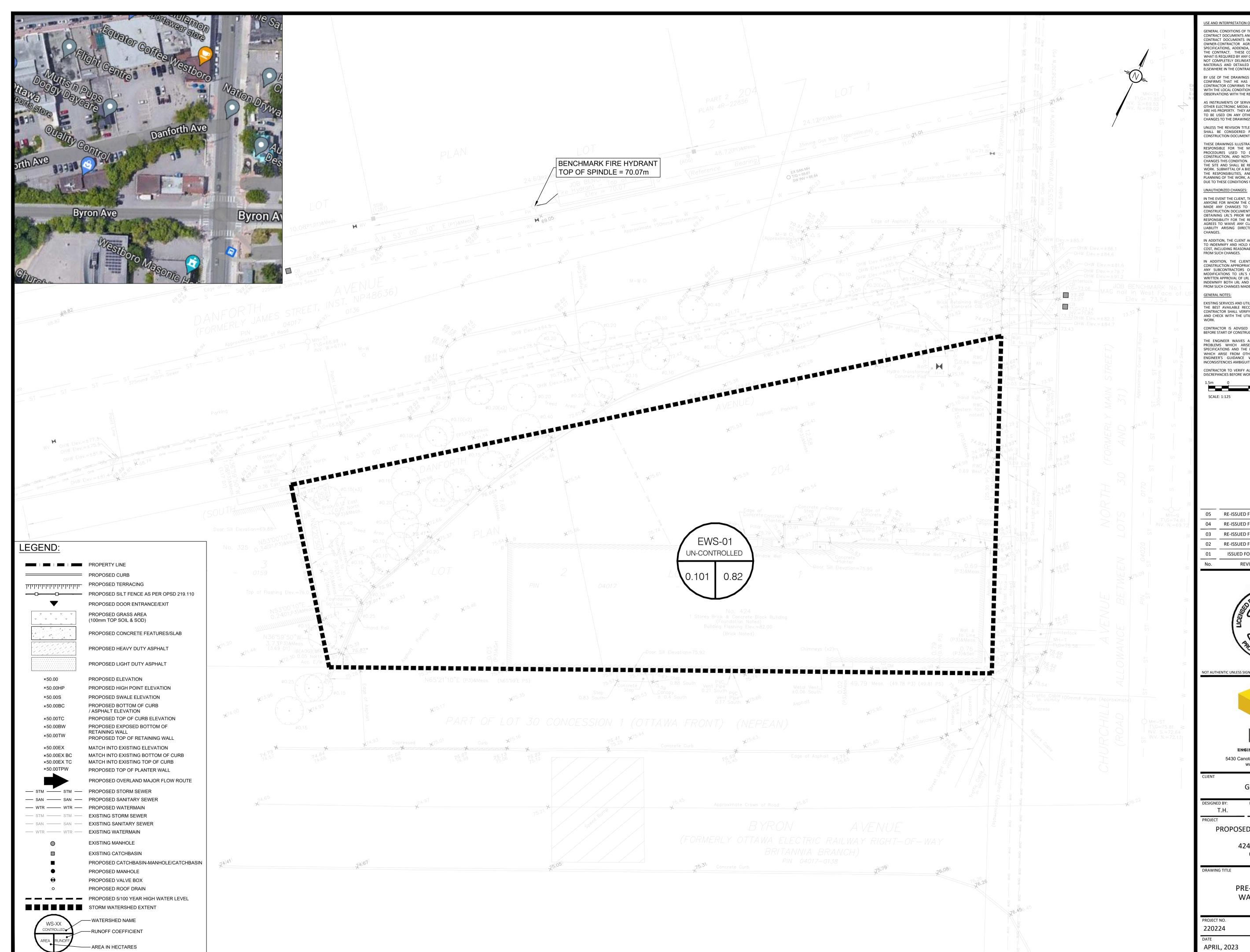
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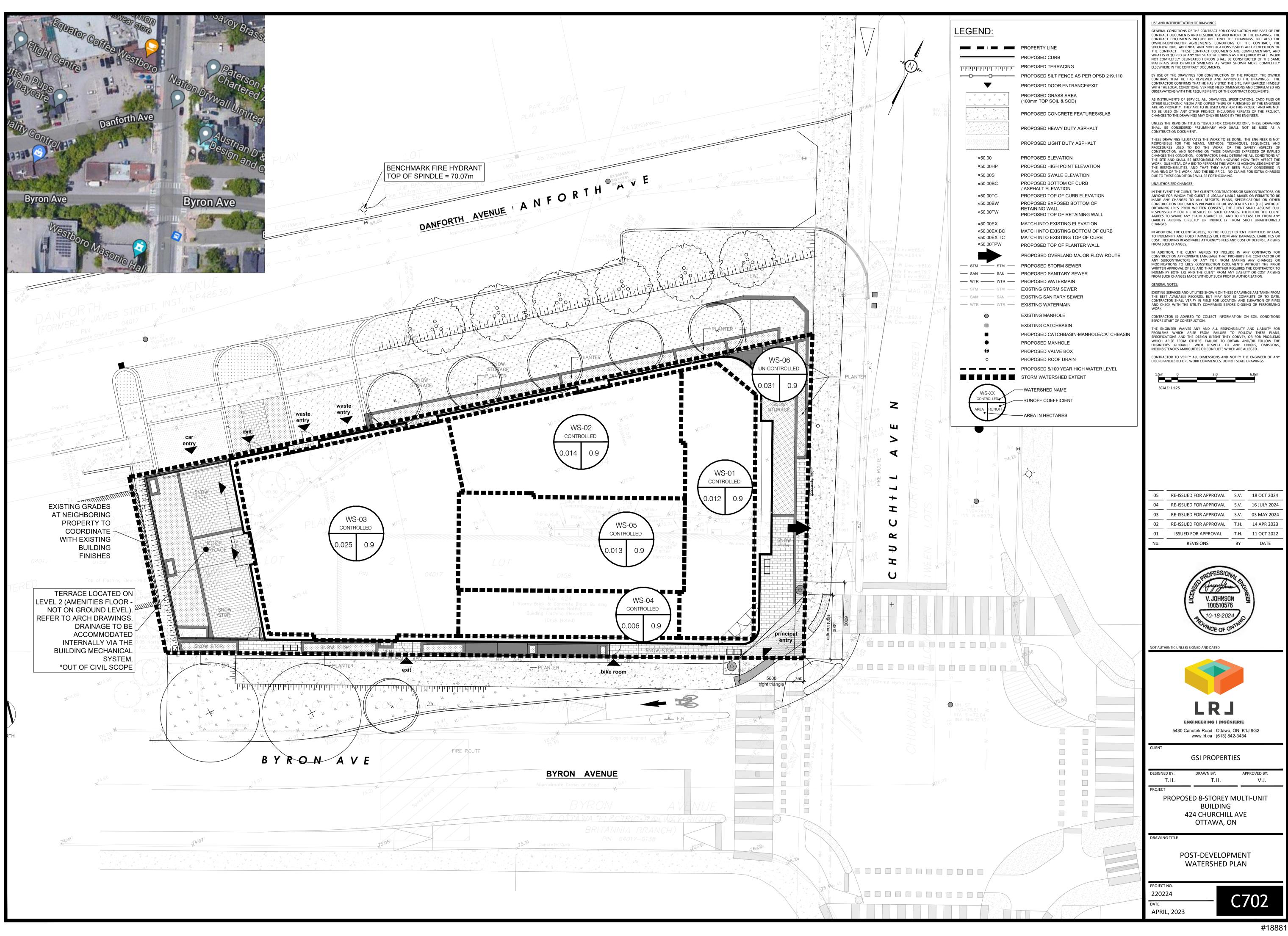
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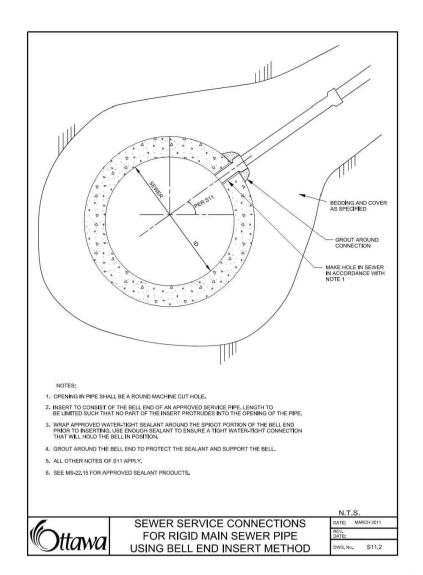
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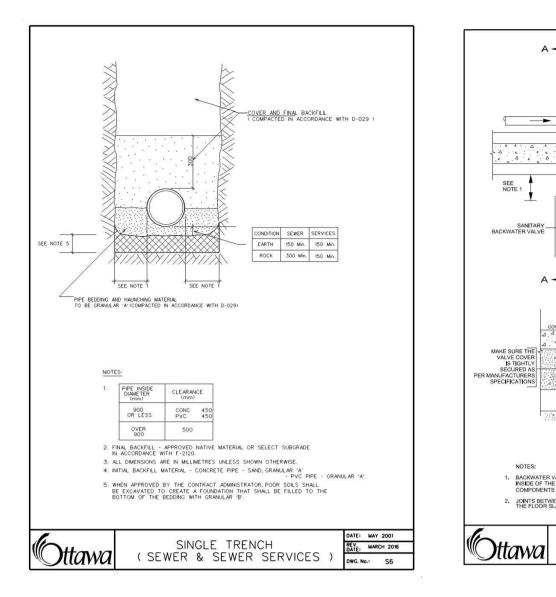
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PRE-DEVELOPMENT WATERSHED PLAN

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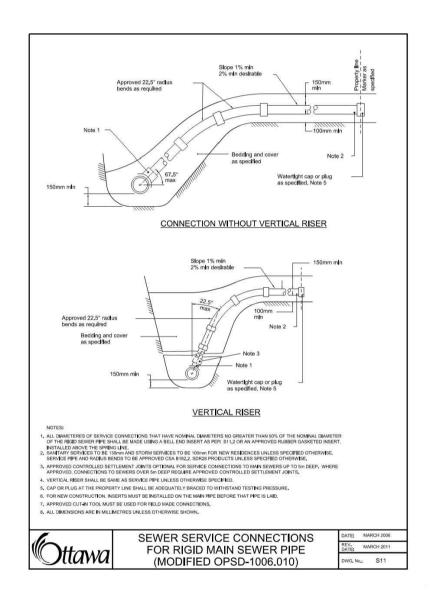


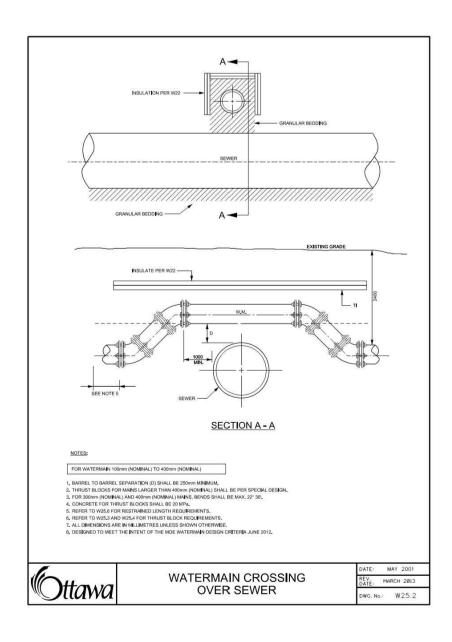


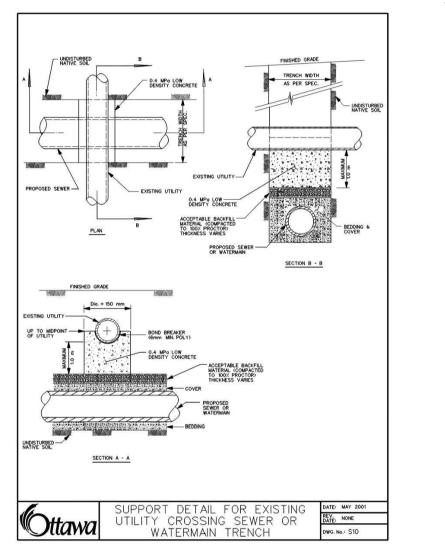


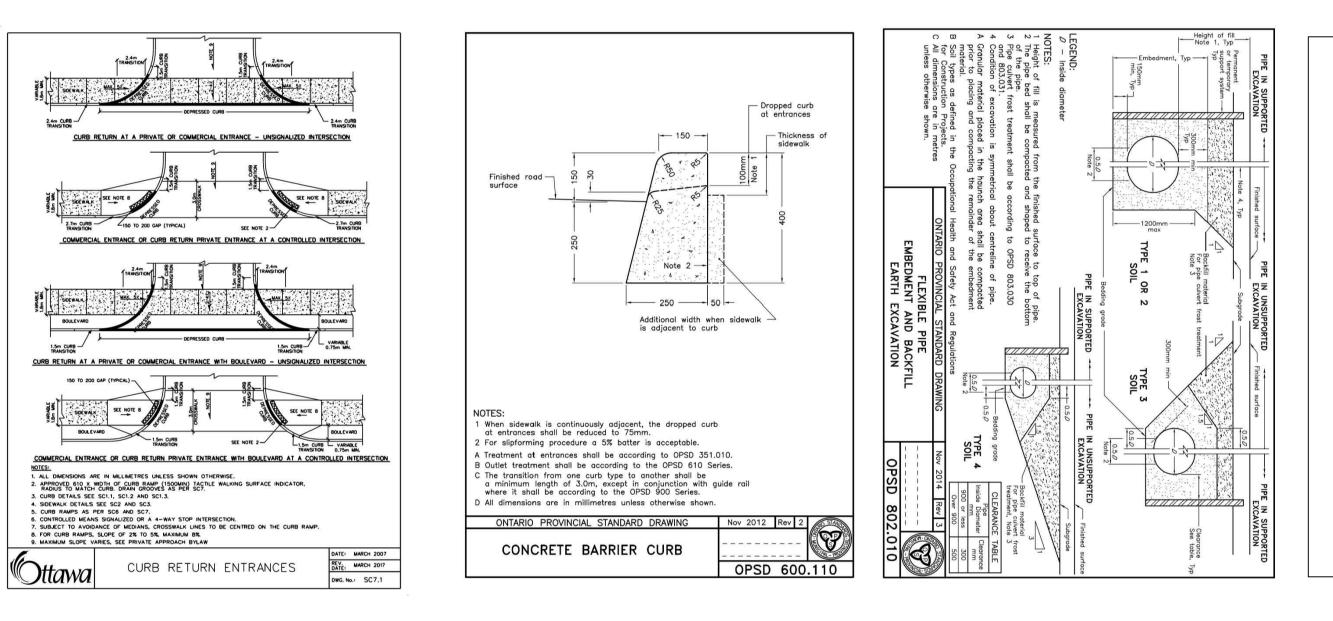
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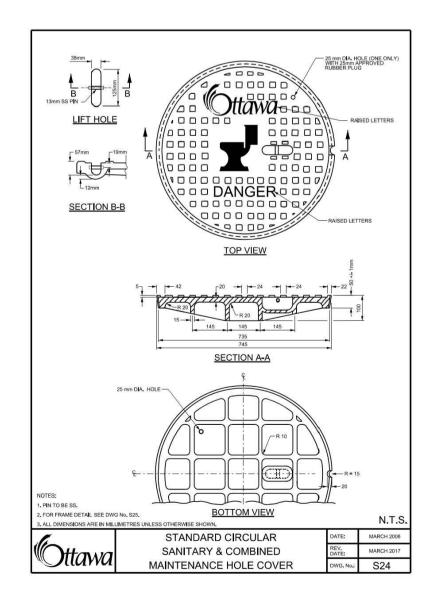
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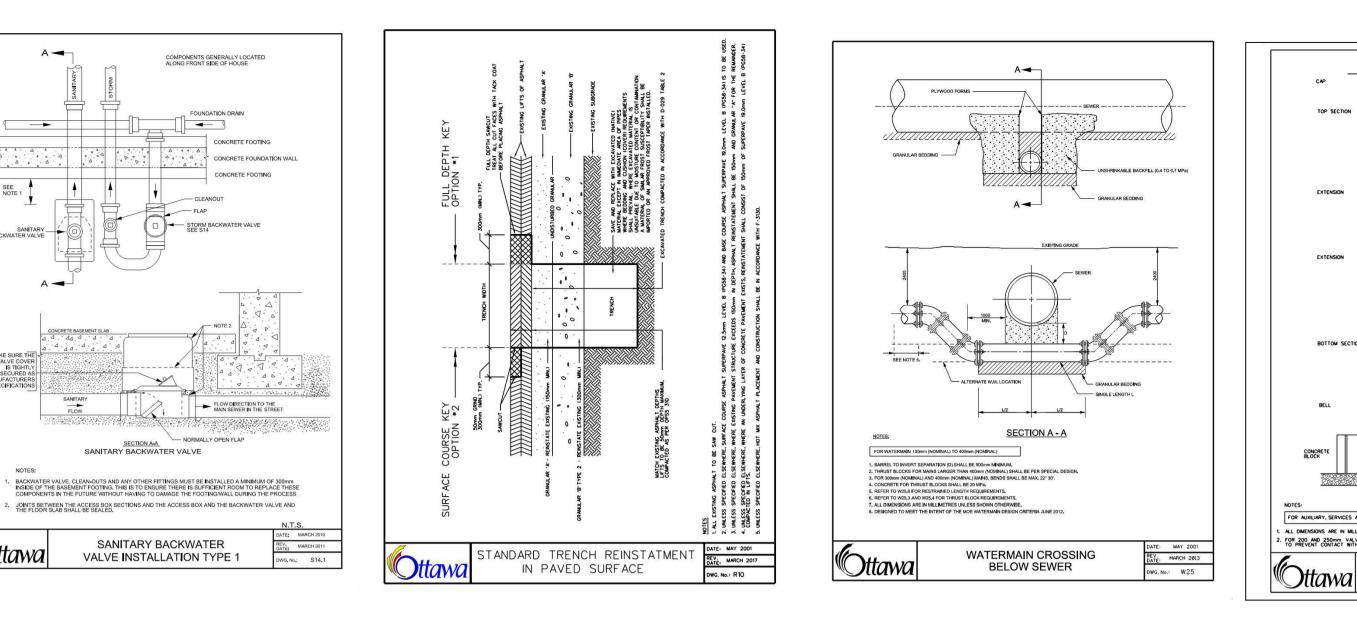


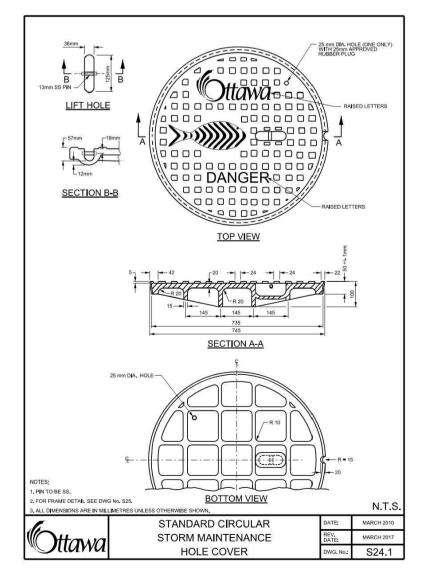


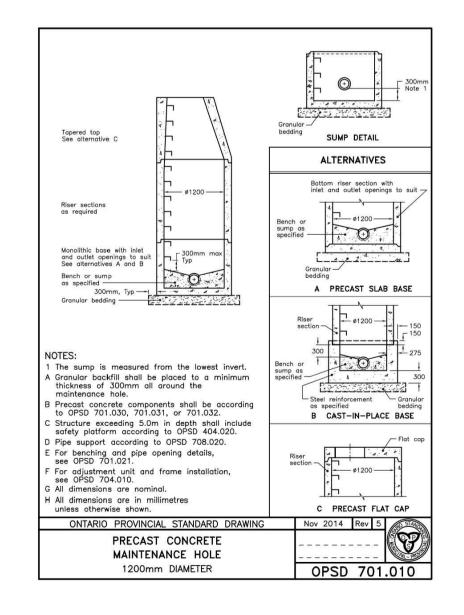


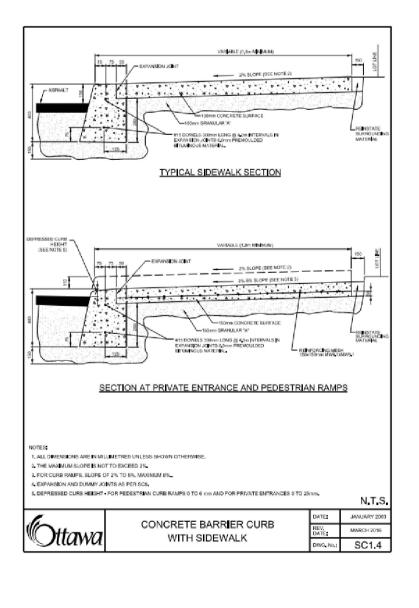


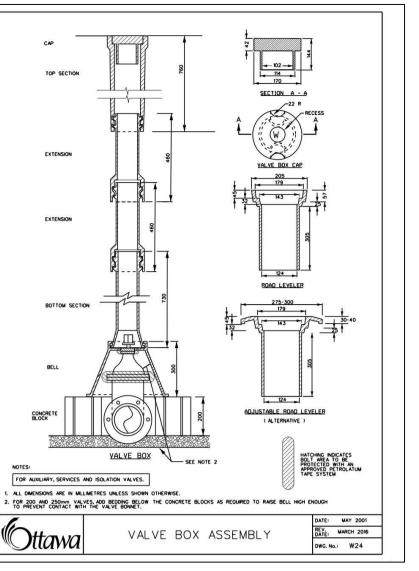


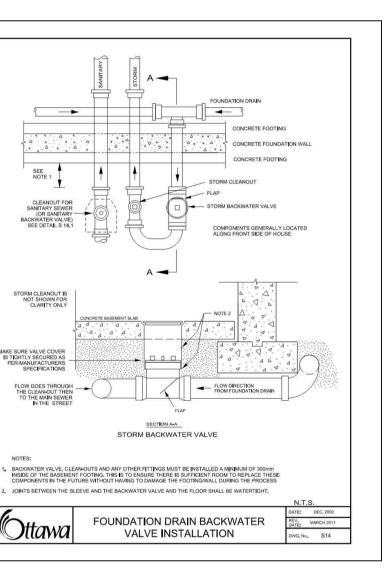












USE AND INTERPRETATION OF DRAWINGS

GENERAL CONDITIONS OF THE CONTRACT FOR CONSTRUCTION ARE PART OF THE CONTRACT DOCUMENTS AND DESCRIBE USE AND INTENT OF THE DRAWING. TH CONTRACT DOCUMENTS INCLUDE NOT ONLY THE DRAWINGS, BUT ALSO THI WNER-CONTRACTOR AGREEMENTS, CONDITIONS OF THE CONTRACT, TH SPECIFICATIONS, ADDENDA, AND MODIFICATIONS ISSUED AFTER EXECUTION OF THE CONTRACT. THESE CONTRACT DOCUMENTS ARE COMPLEMENTARY, AND WHAT IS REQUIRED BY ANY ONE SHALL BE BINDING AS IF REQUIRED BY ALL. WORK NOT COMPLETELY DELINEATED HEREON SHALL BE CONSTRUCTED OF THE SAME MATERIALS AND DETAILED SIMILARLY AS WORK SHOWN MORE COMPLETELY ELSEWHERE IN THE CONTRACT DOCUMENTS.

BY USE OF THE DRAWINGS FOR CONSTRUCTION OF THE PROJECT, THE OWNER CONFIRMS THAT HE HAS REVIEWED AND APPROVED THE DRAWINGS. THE CONTRACTOR CONFIRMS THAT HE HAS VISITED THE SITE, FAMILIARIZED HIMSELF WITH THE LOCAL CONDITIONS, VERIFIED FIELD DIMENSIONS AND CORRELATED HIS DBSERVATIONS WITH THE REQUIREMENTS OF THE CONTRACT DOCUMENTS.

AS INSTRUMENTS OF SERVICE, ALL DRAWINGS, SPECIFICATIONS, CADD FILES OR AS INSTRUMENTS OF SERVICE, ALL DRAWINGS, SECURIONS, CADD FILES OF OTHER ELECTRONIC MEDIA AND COPIED THERE OF FURNISHED BY THE ENGINEER ARE HIS PROPERTY. THEY ARE TO BE USED ONLY FOR THIS PROJECT AND ARE NOT TO BE USED ON ANY OTHER PROJECT, INCLUDING REPEATS OF THE PROJECT. CHANGES TO THE DRAWINGS MAY ONLY BE MADE BY THE ENGINEER.

UNLESS THE REVISION TITLE IS "ISSUED FOR CONSTRUCTION", THESE DRAWINGS SHALL BE CONSIDERED PRELIMINARY AND SHALL NOT BE USED AS A CONSTRUCTION DOCUMENT.

THESE DRAWINGS ILLUSTRATES THE WORK TO BE DONE. THE ENGINEER IS NOT RESPONSIBLE FOR THE MEANS, METHODS, TECHNIQUES, SEQUENCES, AND PROCEDURES USED TO DO THE WORK, OR THE SAFETY ASPECTS OF CONSTRUCTION, AND NOTHING ON THESE DRAWINGS EXPRESSED OR IMPLIED CHANGES THIS CONDITION. CONTRACTOR SHALL DETERMINE ALL CONDITIONS AT THE SITE AND SHALL BE RESPONSIBLE FOR KNOWING HOW THEY AFFECT THE WORK. SUBMITTAL OF A BID TO PERFORM THIS WORK IS ACKNOWLEDGEMENT OF THE RESPONSIBILITES, AND THAT THEY HAVE BEEN FULLY CONSIDERED IN PLANNING OF THE WORK, AND THE BID PRICE. NO CLAIMS FOR EXTRA CHARGES DUE TO THESE CONDITIONS WILL BE FORTHCOMING. UNAUTHORIZED CHANGES:

IN THE EVENT THE CLIENT, THE CLIENT'S CONTRACTORS OR SUBCONTRACTORS, OR ANYONE FOR WHOM THE CLIENT IS LEGALLY LIABLE MAKES OR PERMITS TO BE

MADE ANY CHANGES TO ANY REPORTS, PLANS, SPECIFICATIONS OR OTHER CONSTRUCTION DOCUMENTS PREPARED BY LRL ASSOCIATES LTD. (LRL) WITHOUT OBTAINING LRL'S PRIOR WRITTEN CONSENT, THE CLIENT SHALL ASSUME FULL RESPONSIBILITY FOR THE RESULTS OF SUCH CHANGES. THEREFORE THE CLIENT AGREES TO WAIVE ANY CLAIM AGAINST LRI AND TO RELEASE LRI FROM ANY LIABILITY ARISING DIRECTLY OR INDIRECTLY FROM SUCH UNAUTHORIZED CHANGES.

IN ADDITION, THE CLIENT AGREES, TO THE FULLEST EXTENT PERMITTED BY LAW, TO INDEMNIFY AND HOLD HARMLESS LRL FROM ANY DAMAGES, LIABILITIES OR COST, INCLUDING REASONABLE ATTORNEY'S FEES AND COST OF DEFENSE, ARISING FROM SUCH CHANGES.

IN ADDITION, THE CLIENT AGREES TO INCLUDE IN ANY CONTRACTS FOR CONSTRUCTION APPROPRIATE LANGUAGE THAT PROHIBITS THE CONTRACTOR OR ANY SUBCONTRACTORS OF ANY TIER FROM MAKING ANY CHANGES OR MODIFICATIONS TO LRL'S CONSTRUCTION DOCUMENTS WITHOUT THE PRIOR WRITTEN APPROVAL OF LRL AND THAT FURTHER REQUIRES THE CONTRACTOR TO INDEMNIFY BOTH LRL AND THE CLIENT FROM ANY LIABILITY OR COST ARISING FROM SUCH CHANGES MADE WITHOUT SUCH PROPER AUTHORIZATION. GENERAL NOTES:

EXISTING SERVICES AND UTILITIES SHOWN ON THESE DRAWINGS ARE TAKEN FROM HE BEST AVAILABLE RECORDS, BUT MAY NOT BE COMPLETE OR TO DATE. CONTRACTOR SHALL VERIFY IN FIELD FOR LOCATION AND ELEVATION OF PIPES AND CHECK WITH THE UTILITY COMPANIES BEFORE DIGGING OR PERFORMING WORK.

CONTRACTOR IS ADVISED TO COLLECT INFORMATION ON SOIL CONDITIONS BEFORE START OF CONSTRUCTION. THE ENGINEER WAIVES ANY AND ALL RESPONSIBILITY AND LIABILITY FOR PROBLEMS WHICH ARISE FROM FAILURE TO FOLLOW THESE PLANS, SPECIFICATIONS AND THE DESIGN INTENT THEY CONVEY, OR FOR PROBLEMS WHICH ARISE FROM OTHERS' FAILURE TO OBTAIN AND/OR FOLLOW THE

ENGINEER'S GUIDANCE WITH RESPECT TO ANY ERRORS, OMISSIONS NCONSISTENCIES AMBIGUITIES OR CONFLICTS WHICH ARE ALLEGED. CONTRACTOR TO VERIFY ALL DIMENSIONS AND NOTIFY THE ENGINEER OF ANY DISCREPANCIES BEFORE WORK COMMENCES. DO NOT SCALE DRAWINGS.

| 05 | RE-ISSUED FOR APPROVAL | S.V. | 18 OCT 2024 |
|-----|------------------------|------|--------------|
| 04 | RE-ISSUED FOR APPROVAL | S.V. | 16 JULY 2024 |
| 03 | RE-ISSUED FOR APPROVAL | S.V. | 03 MAY 2024 |
| 02 | RE-ISSUED FOR APPROVAL | Т.Н. | 14 APR 2023 |
| 01 | ISSUED FOR APPROVAL | Т.Н. | 11 OCT 2022 |
| No. | REVISIONS | BY | DATE |
| | | | |



NOT AUTHENTIC UNLESS SIGNED AND DATED



5430 Canotek Road | Ottawa, ON, K1J 9G2 www.lrl.ca I (613) 842-3434

GSI PROPERTIES

DRAWN B APPROVED BY: DESIGNED BY Т.Н. V.J. Т.Н.

PROJECT **PROPOSED 8-STOREY MULTI-UNIT** BUILDING

424 CHURCHILL AVE OTTAWA, ON

DRAWING TITLE

CLIENT

CONSTRUCTION DETAIL PLAN

PROJECT NO. 220224

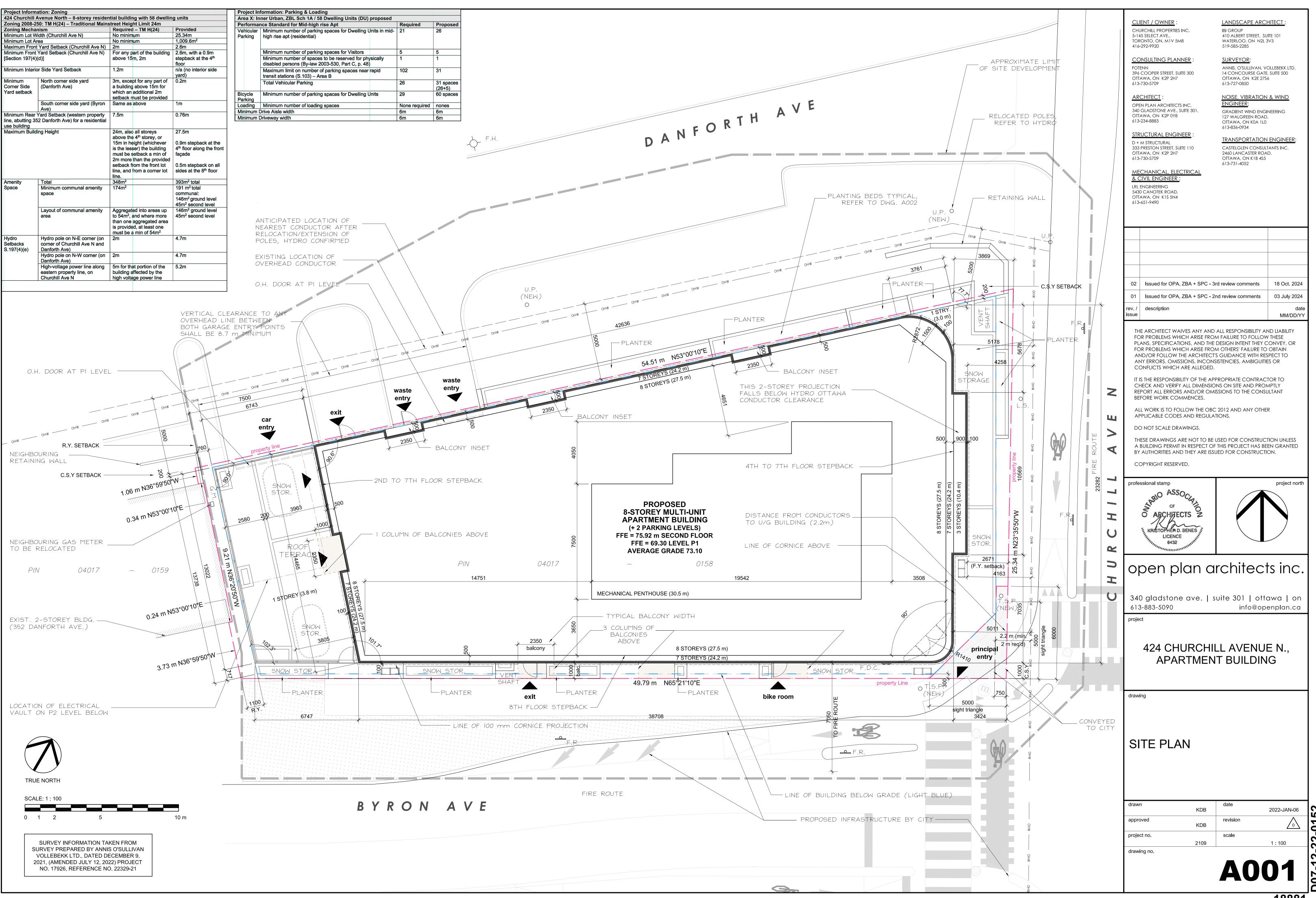
APRIL, 2023

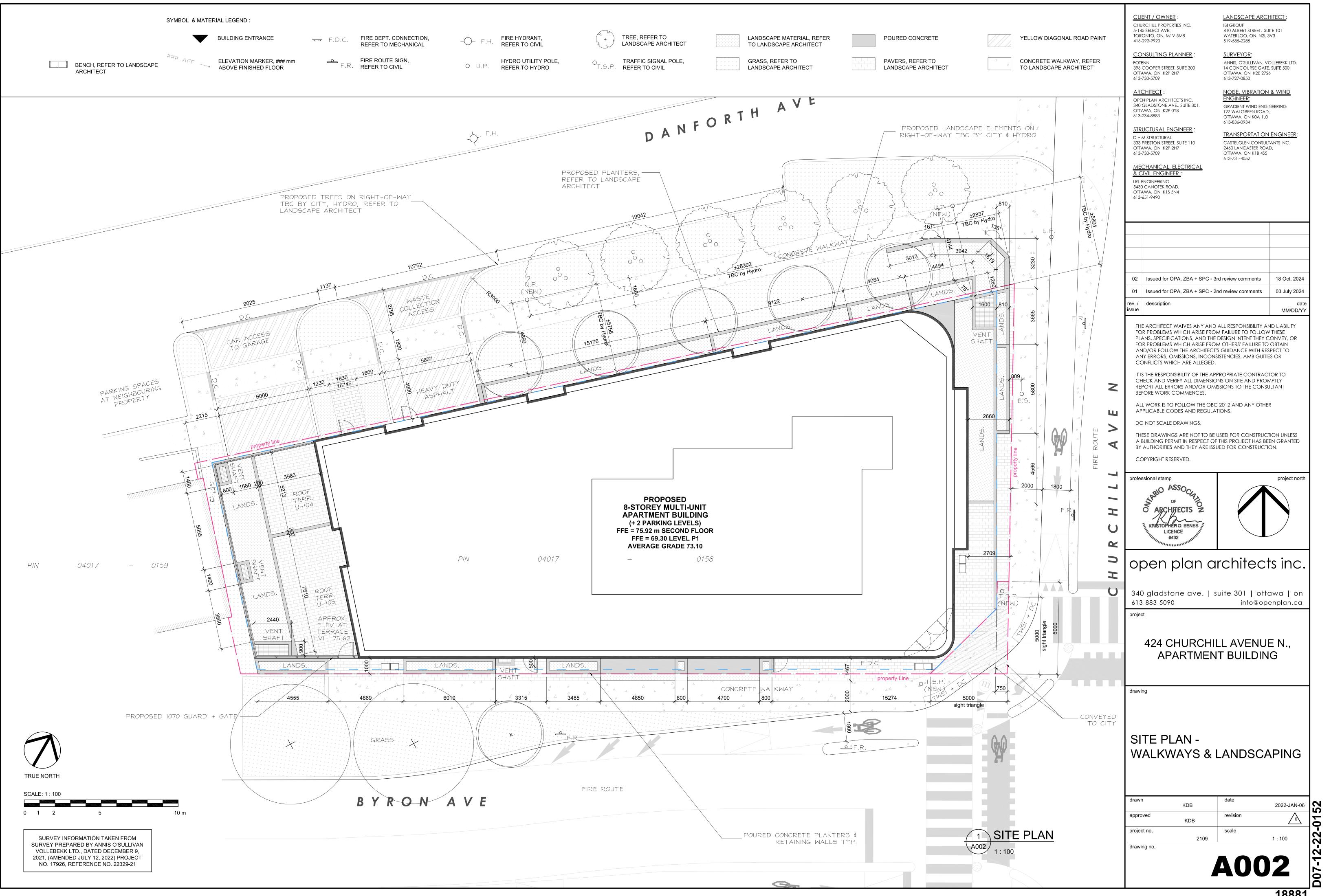


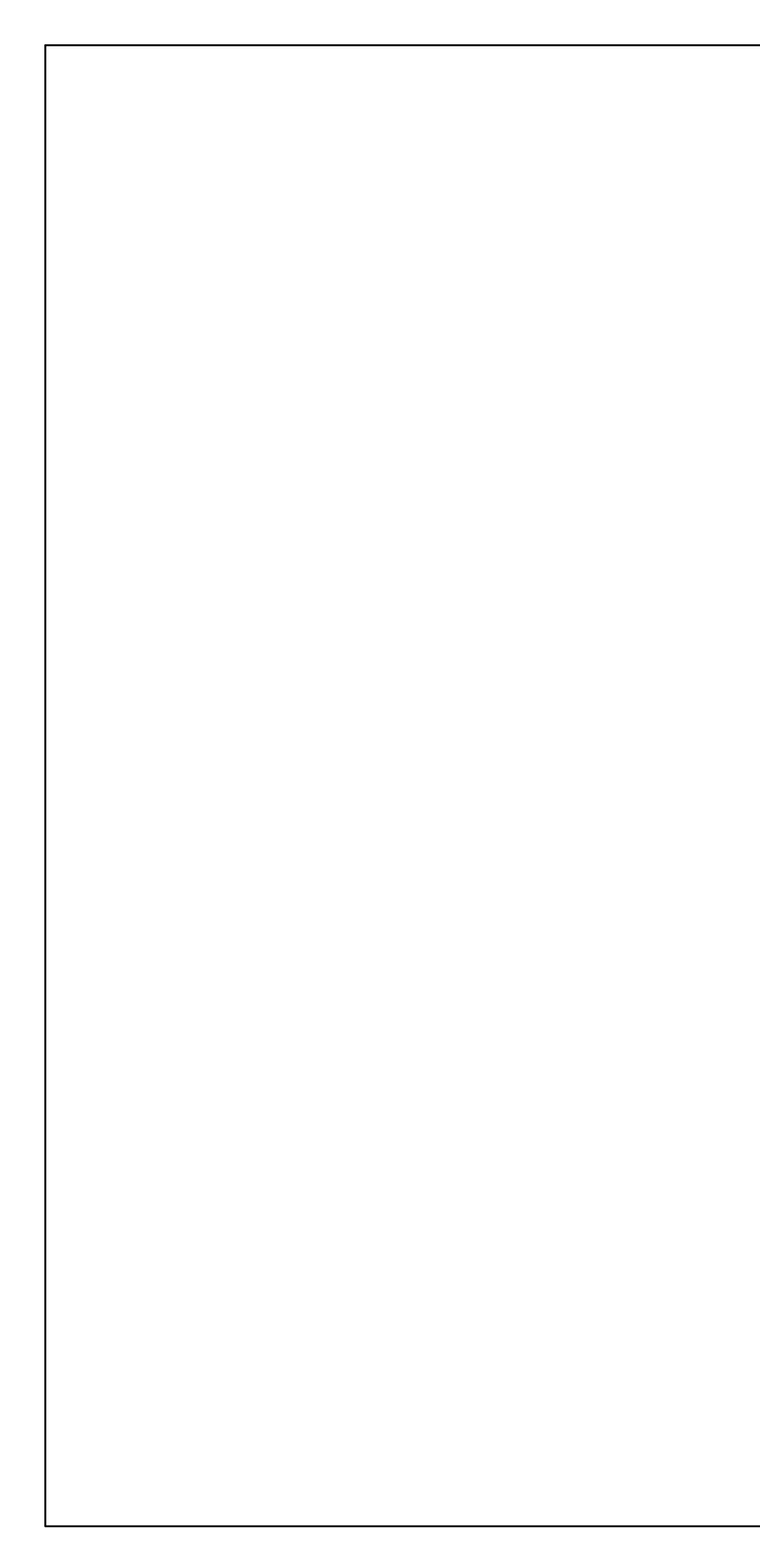
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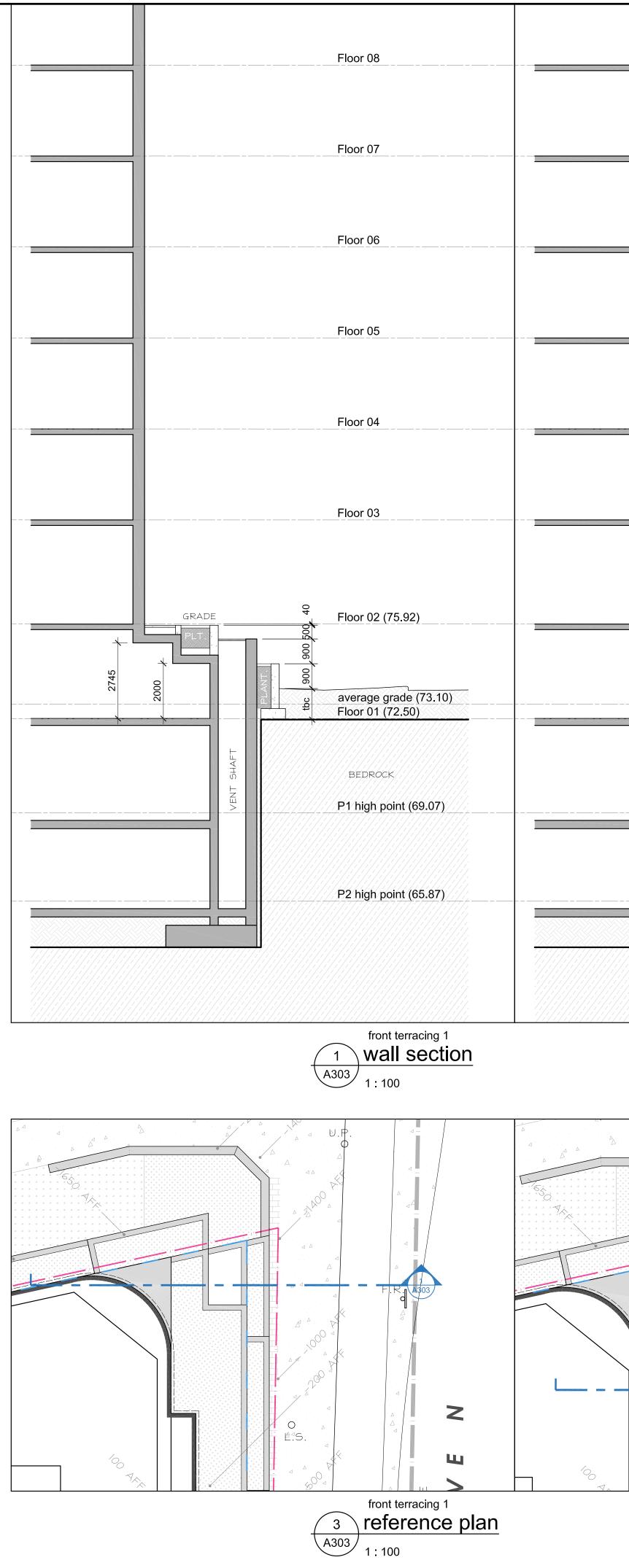
APPENDIX F

Proposed Site Plan Legal Survey As-builts

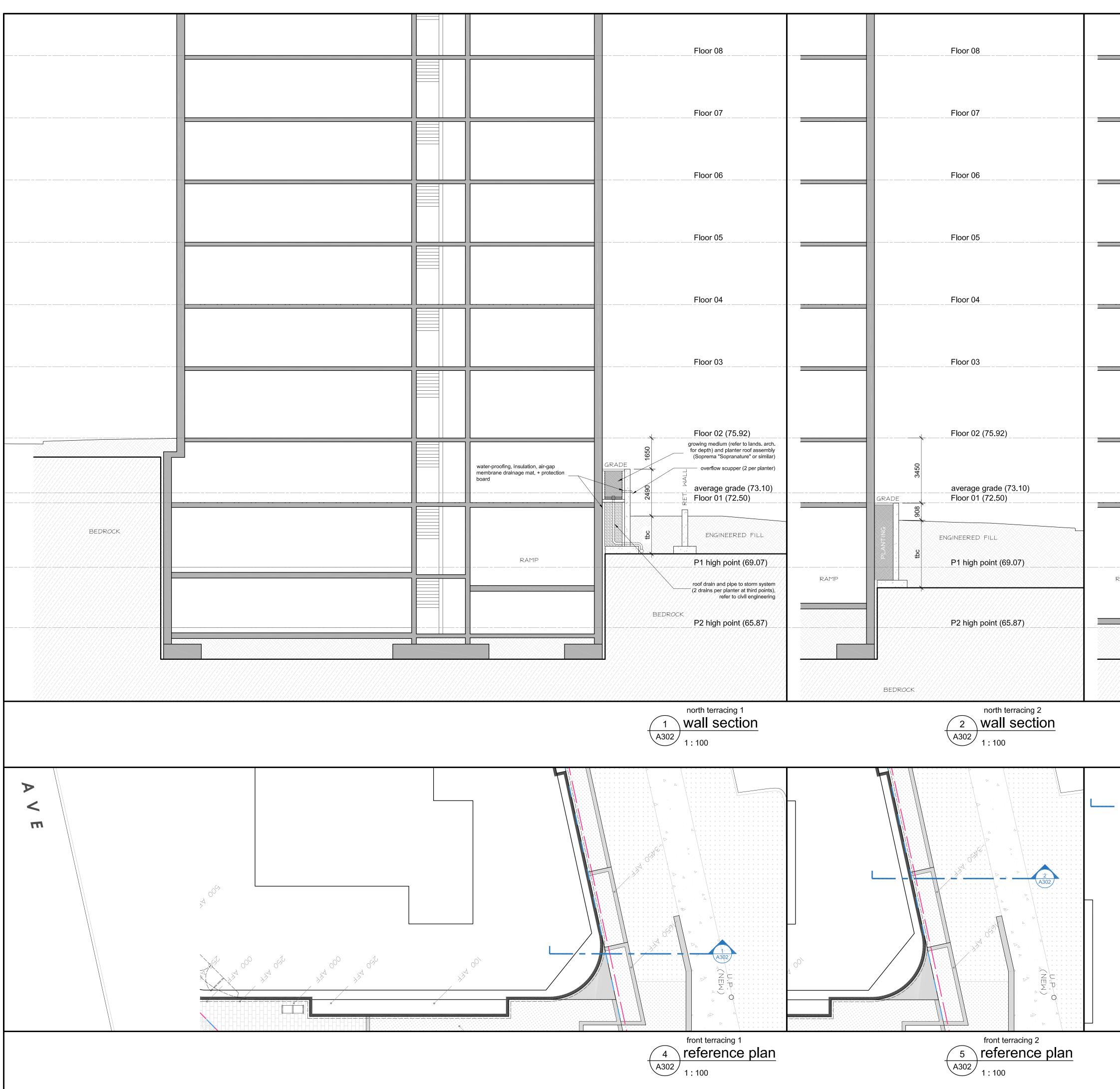




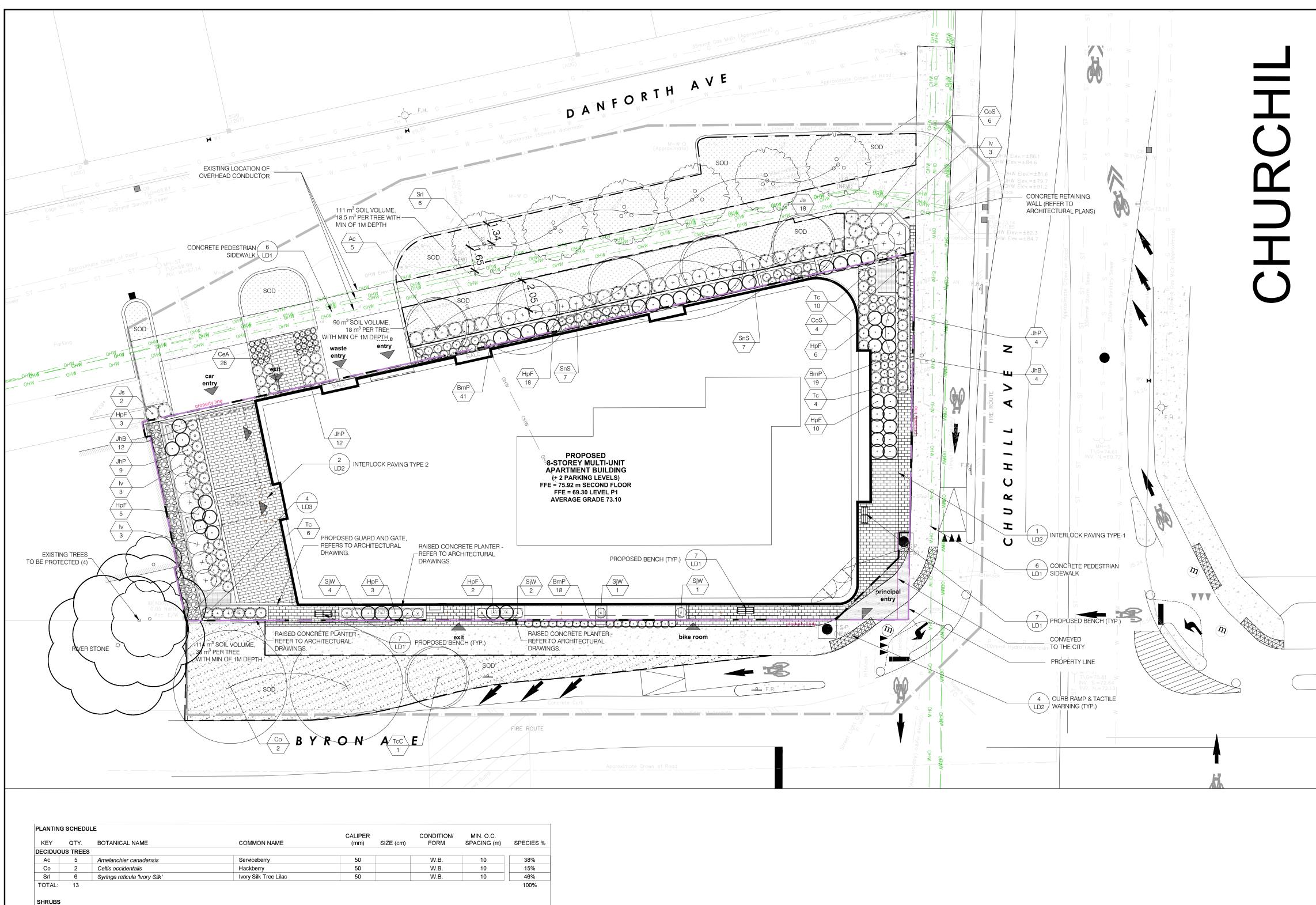




| | Floor 08 | CHU 5-14 TOR | ENT / OWNER : JRCHILL PROPERTIES INC. 15 SELECT AVE., 20NTO, ON, M1V 5M8 | LANDSCAPE ARC IBI GROUP 410 ALBERT STREET, S WATERLOO, ON N2L | UITE 101 |
|---|---|--|--|---|--|
|] | Floor 07 | <u>СС</u> FOT 396 ОТТ 613- 613- СРЕ 340 | -292-9920 <u>ONSULTING PLANNER</u> : ENN COOPER STREET, SUITE 300 AWA, ON K2P 2H7 -730-5709 <u>CHITECT</u> : EN PLAN ARCHITECTS INC. GLADSTONE AVE., SUITE 301, | 519-585-2285 <u>SURVEYOR</u> : ANNIS, O'SULLIVAN, N 14 CONCOURSE GAT OTTAWA, ON K2E 27 613-727-0850 <u>NOISE, VIBRATIOI</u> <u>ENGINEER</u> : GRADIENT WIND ENC | e, suite 500 S6 <u>N & WIND</u> |
| | Floor_06 | 613 <u>STR</u> D + 333 ΟΠ 613 | AWA, ON K2P 0Y8 -234-8883 RUCTURAL ENGINEER : M STRUCTURAL PRESTON STREET, SUITE 110 AWA, ON K2P 2H7 -730-5709 | 127 WALGREEN ROA OTTAWA, ON KOA 116 613-836-0934 <u>TRANSPORTATIO</u> CASTELGLEN CONSU 2460 LANCASTER RO OTTAWA, ON K1B 455 613-731-4052 | d, d n <u>engineer</u> : ltants inc. ad, |
| 1 | Floor 05 | & C LRL 543 | CHANICAL, ELECTRICAL CIVIL ENGINEER : ENGINEERING 0 CANOTEK ROAD, AWA, ON K1S 5N4 -651-9490 | | |
| 1 | Floor 04 | _ | | | |
| | Floor 03 | 02 | Issued for OPA, ZBA + SPC - Issued for coordination description | 3rd review comments | 18 Oct. 2024 02 Oct. 2024 date |
| GRADE | Floor 02 (75.92) | FC PL FC At | E ARCHITECT WAIVES ANY AN DR PROBLEMS WHICH ARISE FR ANS, SPECIFICATIONS, AND TH DR PROBLEMS WHICH ARISE FR ND/OR FOLLOW THE ARCHITEC NY ERRORS, OMISSIONS, INCOI DNFLICTS WHICH ARE ALLEGED | OM FAILURE TO FOLLO IE DESIGN INTENT THEY OM OTHERS' FAILURE TO T'S GUIDANCE WITH RE NSISTENCIES, AMBIGUIT | w These Convey, Or D Obtain Spect To |
| 5000 | average grade (73.10) Floor 01 (72.50) | IT IS THE RESPONSIBILITY OF THE APPROPRIATE CONTRACTOR TO CHECK AND VERIFY ALL DIMENSIONS ON SITE AND PROMPTLY REPORT ALL ERRORS AND/OR OMISSIONS TO THE CONSULTANT BEFORE WORK COMMENCES. ALL WORK IS TO FOLLOW THE OBC 2012 AND ANY OTHER APPLICABLE CODES AND REGULATIONS. | | | PMPTLY SULTANT |
| | BEDROCK P1 high point (69.07) | DO NOT SCALE DRAWINGS. THESE DRAWINGS ARE NOT TO BE USED FOR CONSTRUCTION UN A BUILDING PERMIT IN RESPECT OF THIS PROJECT HAS BEEN GRA BY AUTHORITIES AND THEY ARE ISSUED FOR CONSTRUCTION. COPYRIGHT RESERVED. | | EEN GRANTED | |
| | P2 high point (65.87) | _ | SSIONAL STAMP | | project north |
| | | | oen plan c | architec | ts inc. |
| | 2 A303 1 : 100 front terracing 2 Wall section | |) gladstone ave. 3-883-5090 ¤ | | awa on penplan.ca |
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| | | <u> </u> | | | 18881 |



| | Floor 08 | CLIENT / OWNER : CHURCHILL PROPERTIES INC. 5-145 SELECT AVE., TORONTO, ON, M1V 5M8 416-292-9920 | LANDSCAPE ARCH IBI GROUP 410 ALBERT STREET, SUI WATERLOO, ON N2L 3' 519-585-2285 | TE 101 |
|------|--|---|---|--|
| | Floor 07 | CONSULTING PLANNER : FOTENN 396 COOPER STREET, SUITE 300 OTTAWA, ON K2P 2H7 613-730-5709 | <u>SURVEYOR</u> : ANNIS, O'SULLIVAN, VC 14 CONCOURSE GATE, OTTAWA, ON K2E 2756 613-727-0850 | SUITE 500 |
| | | ARCHITECT : OPEN PLAN ARCHITECTS INC. 340 GLADSTONE AVE., SUITE 301, OTTAWA, ON K2P 0Y8 613-234-8883 | NOISE, VIBRATION ENGINEER: GRADIENT WIND ENGIN 127 WALGREEN ROAD, OTTAWA, ON K0A 1L0 613-836-0934 | |
| | Floor 06 | STRUCTURAL ENGINEER : D + M STRUCTURAL 333 PRESTON STREET, SUITE 110 OTTAWA, ON K2P 2H7 613-730-5709 | TRANSPORTATION CASTELGLEN CONSULT, 2460 LANCASTER ROAE OTTAWA, ON K1B 4S5 613-731-4052 | ants inc. |
| | Floor 05 | MECHANICAL, ELECTRICAL & CIVIL ENGINEER : LRL ENGINEERING 5430 CANOTEK ROAD, OTTAWA, ON K1S 5N4 613-651-9490 | | |
| | Floor 04 | | | |
| | Floor 03 | 02 Issued for OPA, ZBA + SPC - 3 01 Issued for coordination rev. / description issue | 3rd review comments | 18 Oct. 2024 02 Oct. 2024 date MM/DD/YY |
| | Floor 02 (75.92) | THE ARCHITECT WAIVES ANY ANE FOR PROBLEMS WHICH ARISE FRO PLANS, SPECIFICATIONS, AND THE FOR PROBLEMS WHICH ARISE FRO AND/OR FOLLOW THE ARCHITEC ANY ERRORS, OMISSIONS, INCON CONFLICTS WHICH ARE ALLEGED | om Failure to follow E design intent they co om others' failure to t's guidance with resi isistencies, ambiguitie | THESE ONVEY, OR OBTAIN PECT TO |
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| RAMP | P1 high point (69.07) | DO NOT SCALE DRAWINGS. THESE DRAWINGS ARE NOT TO BE A BUILDING PERMIT IN RESPECT O BY AUTHORITIES AND THEY ARE ISS COPYRIGHT RESERVED. | F THIS PROJECT HAS BEE | N GRANTED |
| | P2 high point (65.87) | professional stamp OF ARCHITECTS KRISTOPHER D. BENES LICENCE 6432 | | project north |
| | BEDROCK | open plan c | L Irchitect | s inc. |
| | north terracing 33Wall sectionA3021 : 100 | 340 gladstone ave. 613-883-5090 | | iwa on enplan.ca |
| | | 424 CHURCHI APARTMEN | | |
| | | drawing | s - landsca | ipe |
| | front terracing 3 | drawn KDB approved KDB project no. 2119 | date revision scale | 2024 |
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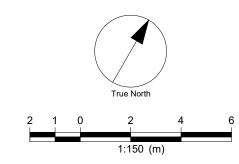
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BmP Buxus microphylla 'Pincushion Pincushion Boxwood CoS Spiral Hinoki cypress 3 Gal. Chamaecyparis obtusa 'Spiralis' 3 Gal. HpF Hydrangea paniculata 'Fire Light Tidbit' Fire Light Tidbit Hydrangea 3 Gal. llex verticillata Winterberry 3 Gal. SiW Little Princess Spirea Spiraea japonica 'Little Princess SnS Spiraea nipponica 'Snowmound' Snowmound Spirea 14 3 Gal Juniperus sabina Juniperus sabina Js 20 JhB 16 Juniperus horizontalis 'Blue Chip 3 Gal. Creeping Juniper JhP Juniperus horizontalis 'Plumosa Compacta Compact Andorra Juniper 3 Gal. 25 Тс 3 Gal. 20 Taxus canadensis Canada Yew TOTAL: 247 GRASSE CeA Bowles Golden Sedge 1 Gal. 0.3 28 Carex elata 'Aurea' TOTAL: 28 LANDSCAPE ITEMS QTY. UNIT DESCRIPTION 798 m² Kentucky Blue Grass Sod



LANDSCAPE NOTES:

- 1. ALL WORK TO BE CARRIED OUT IN ACCORDANCE WITH BY-LAWS AND CODES HAVING JURISDICTION OVER SITE LOCATION.
- 2. COMPLETE ALL WORK TO THE SATISFACTION OF THE LANDSCAPE ARCHITECT. 3. REPORT ANY CHANGES, DISCREPANCIES OR SUBSTITUTIONS TO THE LANDSCAPE
- ARCHITECT FOR REVIEW. OBTAIN APPROVAL FROM THE LANDSCAPE ARCHITECT BEFORE PROCEEDING. 4. IT IS THE CONTRACTOR'S RESPONSIBILITY TO DETERMINE EXISTING SERVICE LOCATIONS.
- EXACT LOCATIONS OF PLANT MATERIAL WILL BE DETERMINED BY PLACEMENT OF SITE SERVICES SUCH AS HYDRO VAULTS, METERS, UTILITIES ROOF RAIN WATER LEADERS, DRIVEWAYS, LIGHT STANDARDS, ETC.
- ALL PLANT MATERIAL LOCATIONS TO BE STAKED OR MARKED OUT AND APPROVED BY LANDSCAPE ARCHITECT PRIOR TO INSTALLATION.
 SUPPLY ALL PLANT MATERIAL IN ACCORDANCE WITH THE CANADIAN STANDARDS FOR NURSERY STOCK (8th Ed.).
- 8. INSTALL PLANT MATERIAL ACCORDING TO DETAILS SHOWN.
- DISTURBED SOIL AREAS AROUND TREES AND SHRUBS ARE TO BE COVERED WITH

SHREDDED CONIFER BARK MULCH SUCH AS 'CANADA RED' OR 'GRO-BARK' SPM MULCH, OR APPROVED EQUIVALENT. ALTERNATIVE MULCHES MUST BE APPROVED BY THE LANDSCAPE ARCHITECT.

- 10. CONTRACTOR TO UTILIZE LAYOUT DIMENSIONS WHERE PROVIDED.
- 11. PROVIDE PLANTING BED AREA AS NOTED ON THE DRAWING OR TO ACCOMMODATE MATURE SIZE OF PLANT MATERIAL.
- ALL SUPPORT SYSTEMS MUST BE REMOVED BY THE CONTRACTOR AT TIME OF FINAL ACCEPTANCE. NO EXTRAS WILL BE PAID TO COMPLETE THIS WORK.
 SUPPLY AND PLACE TOPSOIL IN ACCORDANCE WITH OPSS 570 TO A MINIMUM DEPTH OF
- 150MM UNLESS OTHERWISE SPECIFIED. 14. SUPPLY AND PLACE SOD IN ACCORDANCE WITH OPSS 571 UNLESS OTHERWISE SPECIFIED.
- 15. SUPPLY AND PLACE SEED IN ACCORDANCE WITH OPSS 572 UNLESS OTHERWISE SPECIFIED. ALL 5:1 OR GREATER SLOPES TO BE SEEDED WITH TACIFIER. CONTRACTOR TO PROVIDE NECESSARY EROSION CONTROL PROTECTION AS REQUIRED TO ENSURE SOIL STABILIZATION AND PROPER SEED GERMINATION.
- 16. ALL DIMENSIONS IN METRES UNLESS OTHERWISE NOTED.
 17. IF DISCREPANCIES ARISE BETWEEN PLANT MATERIAL COUNT SHOWN ON DRAWING AND PLANT LIST, THE DRAWING SHALL BE CONSIDERED CORRECT.
 18. CONTRACTOR TO PROVIDE MINIMUM TWO (2) YEAR WARRANTY FROM DATE ACCEPTED ON
- ALL WORK UNLESS OTHERWISE SPECIFIED. 19. ANY SITE PLAN OR GRADING AND SERVICING SHOWN IS FOR INFORMATION ONLY. REFER TO APPROVED DRAWINGS.
- 20.NOT FOR CONSTRUCTION UNLESS STAMPED, SIGNED AND DATED BY LANDSCAPE ARCHITECT.21.DRAWINGS NOT TO BE REPRODUCED WITHOUT WRITTEN CONSENT FROM LANDSCAPE
- ARCHITECT. 22.APPROVAL OF LANDSCAPE PLAN TO BE OBTAINED FROM MUNICIPALITY.
- 23.FOR GRADING AND SERVICING INFORMATION REFER TO THE CONSULTING ENGINEER'S DRAWINGS.24.FOR LIGHTING INFORMATION AND POWER DISTRIBUTION REFER TO THE ELECTRICAL CONSULTANT'S DRAWINGS.

PLANTING NOTES

- 1. THE CONTRACTOR MUST NOTIFY THE LANDSCAPE ARCHITECT PRIOR TO THE COMMENCEMENT OF ANY PLANTING. THE CONTRACTOR SHALL SUPPLY ALL PLANTS AND MATERIALS IN QUANTITIES SUFFICIENT TO COMPLETE THE WORK SHOWN ON THIS DRAWING. ANY DISCREPANCIES BETWEEN QUANTITIES SHALL BE REPORTED TO THE LANDSCAPE ARCHITECT.
- 2. ALL LANDSCAPE WORKS WILL BE WARRANTIED FOR A PERIOD OF TWO YEARS FOLLOWING INSPECTION AND WRITTEN NOTICE OF START OF WARRANTY PERIOD AS DETERMINED AND PROVIDED BY THE LANDSCAPE ARCHITECT. PLANT MATERIAL, WHICH IS NOT IN A HEALTHY, VIGOROUS GROWING CONDITION AT THE END OF THE WARRANTY PERIOD, SHALL BE REPLACED TO THE SATISFACTION OF THE LANDSCAPE ARCHITECT / OWNER.
- 3. THE LANDSCAPE ARCHITECT RESERVES THE RIGHT TO EXTEND CONTRACTOR'S WARRANTY RESPONSIBILITIES FOR AN ADDITIONAL YEAR IF, AT THE END OF INITIAL WARRANTY PERIOD, LEAF DEVELOPMENT AND GROWTH IS NOT SUFFICIENT TO ENSURE FUTURE SURVIVAL AS DETERMINED BY THE LANDSCAPE ARCHITECT.
- 4. THE CONTRACTOR IS TO IDENTIFY WITH LANDSCAPE ARCHITECT/OWNER ANY MAINTENANCE REQUIREMENTS NECESSARY FOR WARRANTY PURPOSES.
- 5. PLANT MATERIALS SPECIFIED FOR THIS PROJECT WILL CONFORM TO THE CANADIAN NURSERY LANDSCAPE ASSOCIATION (C.N.L.A.) FOR SIZE, VARIETY AND CONDITION AS INDICATED ON THE PLANT SCHEDULE SHOWN ON THESE DRAWINGS. ANY PLANT MATERIALS WHICH DO NOT CONFORM WILL BE PROMPTLY REMOVED FROM THE SITE AND REPLACED BY THE CONTRACTOR AT NO ADDITIONAL COST TO THE PROJECT.
- 6. THE LANDSCAPE ARCHITECT IS TO BE CONTACTED FOR INSPECTION AND WRITTEN APPROVAL PRIOR TO PLANT MATERIAL ARRIVING ON SITE. THE LANDSCAPE ARCHITECT RESERVED THE RIGHT TO REJECT ANY PLANT MATERIALS THAT HAVE NOT BEEN INSPECTED AND APPROVED.
- 7. THE LANDSCAPE ARCHITECT RESERVES THE RIGHT TO REFUSE ACCEPTANCE OF ANY PLANT DISPLAYING POOR GROWTH HABITS, INJURY OR DISEASE. ANY PLANT MATERIAL THAT IS REJECTED BY THE LANDSCAPE ARCHITECT WILL BE PROMPTLY REMOVED FROM THE SITE AND REPLACED WITH MATERIAL OF ACCEPTABLE QUALITY AT NO ADDITIONAL CHARGE TO THE PROJECT.
- 8. PLANT MATERIALS COLLECTED FROM WILD SOURCES WILL NOT BE ACCEPTED WITHOUT WRITTEN APPROVAL OF THE LANDSCAPE ARCHITECT. THE LANDSCAPE ARCHITECT RESERVES THE RIGHT TO REQUIRE THAT SUPPLIER INVOICES BE SUBMITTED FOR INSPECTION AND APPROVAL PRIOR TO ACCEPTANCE.
- 9. ON-SITE LAYOUT OF THE PLANT MATERIALS TO BE APPROVED BY THE LANDSCAPE ARCHITECT PRIOR TO INSTALLATION. MINOR FIELD ADJUSTMENTS TO PLANT MATERIAL LOCATIONS MAY BE NECESSARY TO RESPOND TO THE LOCATIONS OF EXISTING PLANTS AND SITE CONDITIONS. THE CONTRACTOR TO REVIEW WITH LANDSCAPE ARCHITECT WHERE RELOCATIONS ARE NECESSARY. THE CONTRACTOR MUST RECEIVE APPROVAL FROM LANDSCAPE ARCHITECT PRIOR TO INSTALLATION.
- 10. PLANTS ARE NOT TO BE INSTALLED DURING EXTREME HEAT, DROUGHT, OR OTHER UNDESIRABLE CONDITIONS. THOROUGHLY WATER ALL PLANTS IMMEDIATELY AFTER INSTALLATION. THE CONTRACTOR SHALL REGULARLY MONITOR SITE CONDITIONS AND WATER AS REQUIRED TO ENSURE HEALTHY GROWTH CONDITIONS THROUGHOUT THE DURATION OF THE WARRANTY PERIOD.
- 11. DO NOT PLANT DIRECTLY IN CENTERLINE OF DRAINAGE SWALES OR DEPRESSION AREAS. WHERE PROPOSED PLANTING LOCATIONS CONFLICT WITH CONSTRUCTED SWALES OR LOW-LYING WET AREAS, CONTACT LANDSCAPE ARCHITECT FOR DIRECTION.
- 12. ALL PLANTS ARE TO BE PLANTED IN ACCORDANCE WITH THE PLANTING DETAILS SHOWN ON THIS DRAWING. ALL PLANTS ARE TO BE INSTALLED VERTICAL AND PLUMB, REGARDLESS OF GROUND SLOPE.
- 13. SUPPLY AND PLACE TOPSOIL IN ACCORDANCE WITH OPSS 802 TO A MINIMUM DEPTH OF 150MM IN SEED/SOD AREAS AND 600MM IN PLANTING BEDS UNLESS OTHERWISE SPECIFIED. EACH SOURCE OF TOPSOIL, IMPORTED OR NATIVE TO BE APPROVED BY LANDSCAPE ARCHITECT PRIOR TO USE. SUBMIT TOPSOIL ANALYSIS/TEST RESULTS TO LANDSCAPE ARCHITECT PRIOR TO ORDER OR DELIVERY TO SITE. TESTING TO BE IN ACCORDANCE WITH CONTRACT SPECIFICATIONS. PREPARED TOPSOIL SHALL BE 4 PARTS TOPSOIL TO ONE PART WELL-ROTTED COMPOST.
- 14. MULCH: TO BE SPREAD UNIFORMLY AROUND THE BASE OF TREES AND SHRUBS TO A MINIMUM DEPTH OF 100 MM. DO NOT PLACE MULCH IN DIRECT CONTACT WITH TRUNK OR STEM(S). ALLOW A 100 MM MULCH FREE ZONE AT TRUNK/STEMS. SHRUBS TO BE IN CONTINUOUSLY MULCHED PLANTING BEDS UNLESS OTHERWISE SPECIFIED.
- 15. SUPPLY AND PLACE SEED IN ACCORDANCE WITH OPSS 804 UNLESS OTHERWISE SPECIFIED. ALL 5:1 OR GREATER SLOPES TO BE SEEDED WITH TACKIFIER. ALL SLOPES GREATER THAN 3:1 SHALL BE MATTED WITH AN EROSION CONTROL BLANKET. SUPPLY AND PLACE SOD IN ACCORDANCE WITH OPSS 803 UNLESS OTHERWISE SPECIFIED.
- 16. THE CONTRACTOR IS TO REMOVE DEAD OR DAMAGED BRANCHES ON TREES OR SHRUBS. ALL PRUNING SHALL BE PERFORMED IN ACCORDANCE WITH STANDARD HORTICULTURAL PRACTICES AND APPROPRIATE TIMING FOR EACH SPECIES.
- 17. ALL STAKES AND ASSOCIATED TIES ARE TO BE REMOVED AFTER THE FIRST FULL GROWING SEASON. RODENT GUARDS ARE TO BE REMOVED AT THE CONCLUSION OF THE WARRANTY PERIOD. IF UTILIZED, GATORBAGS ARE TO BE REMOVED FOR WINTER MONTHS.

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| PROJECT NO: 139413 | |
|----------------------------|---------------------|
| DRAWN BY: E.L | CHECKED BY: E.L |
| PROJECT MGR: M.P | APPROVED BY: T.O |
| SHEET TITLE LANDSCA | APE PLAN |

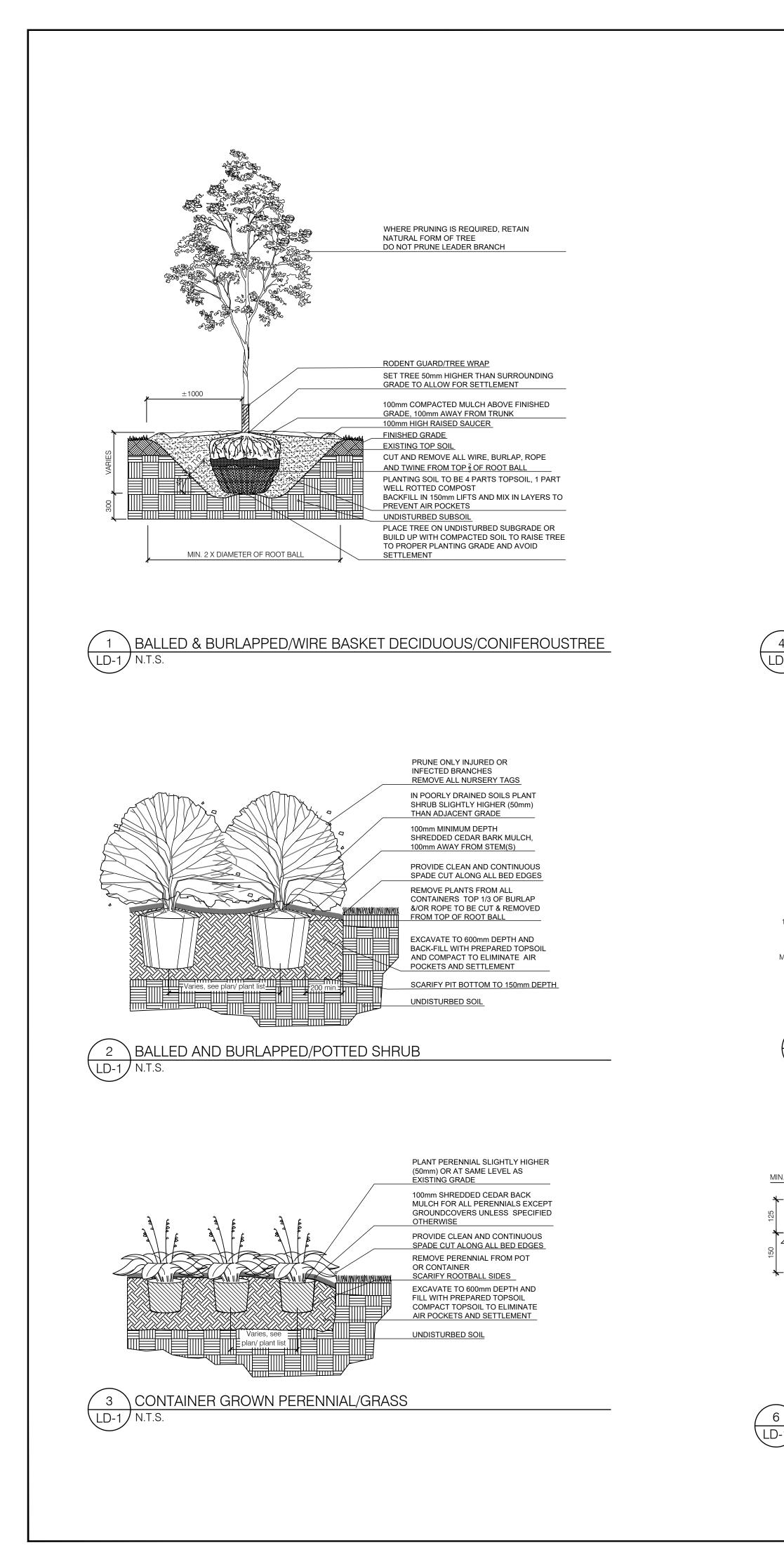
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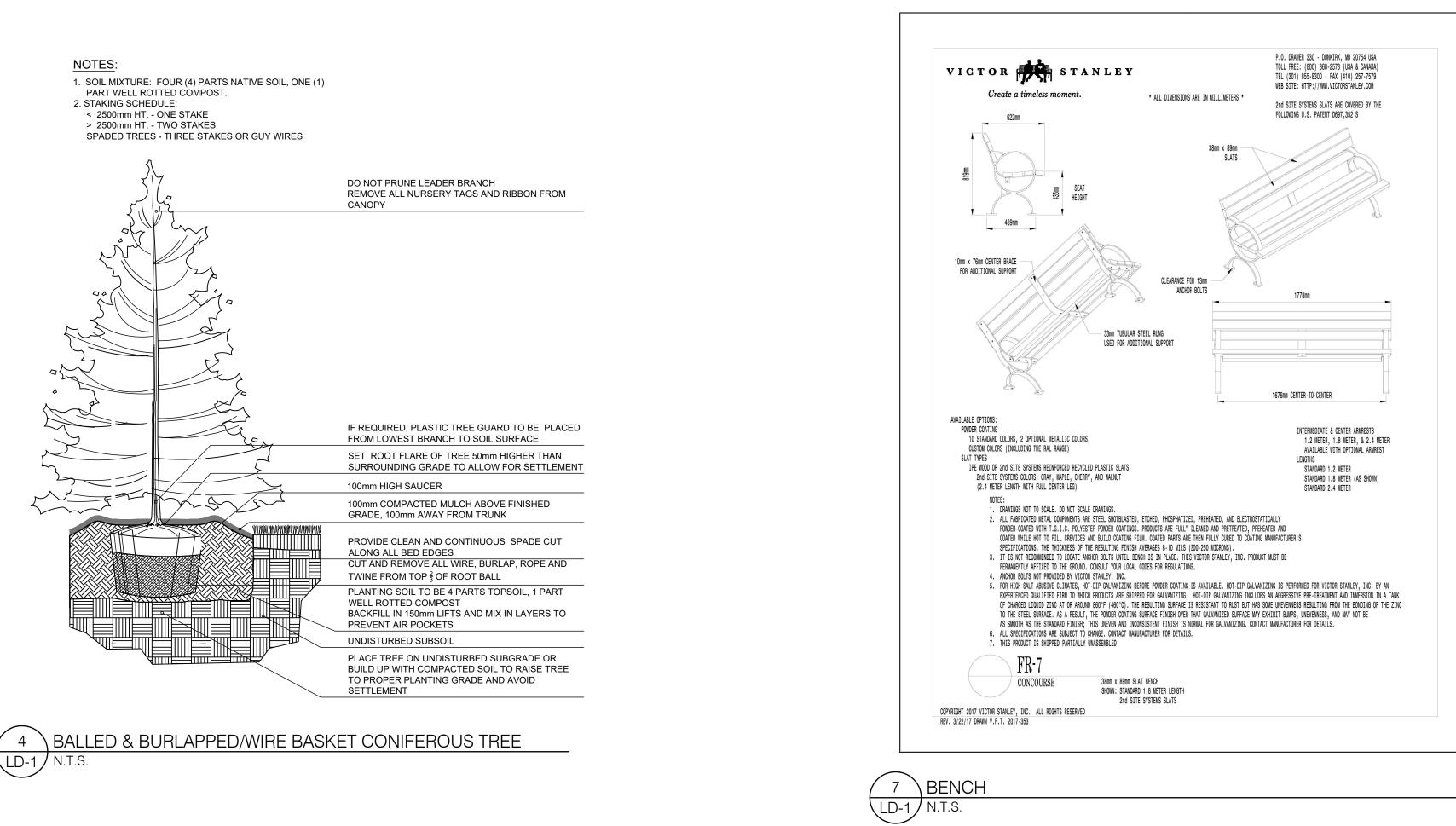
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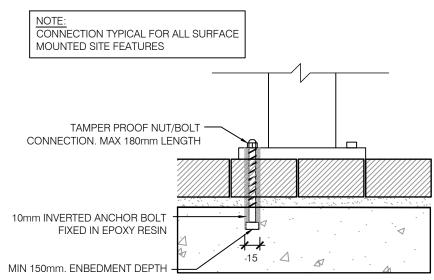
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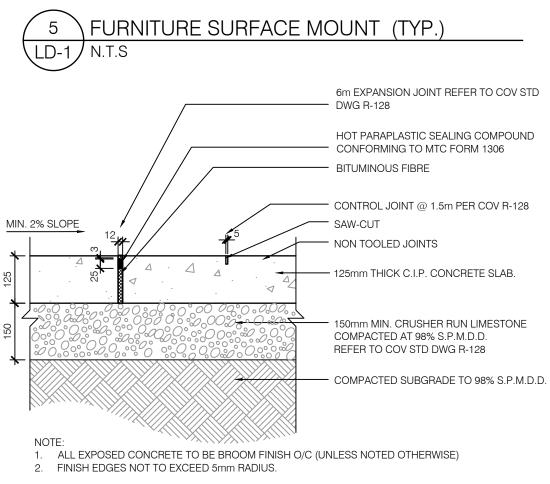
ISSUE

4





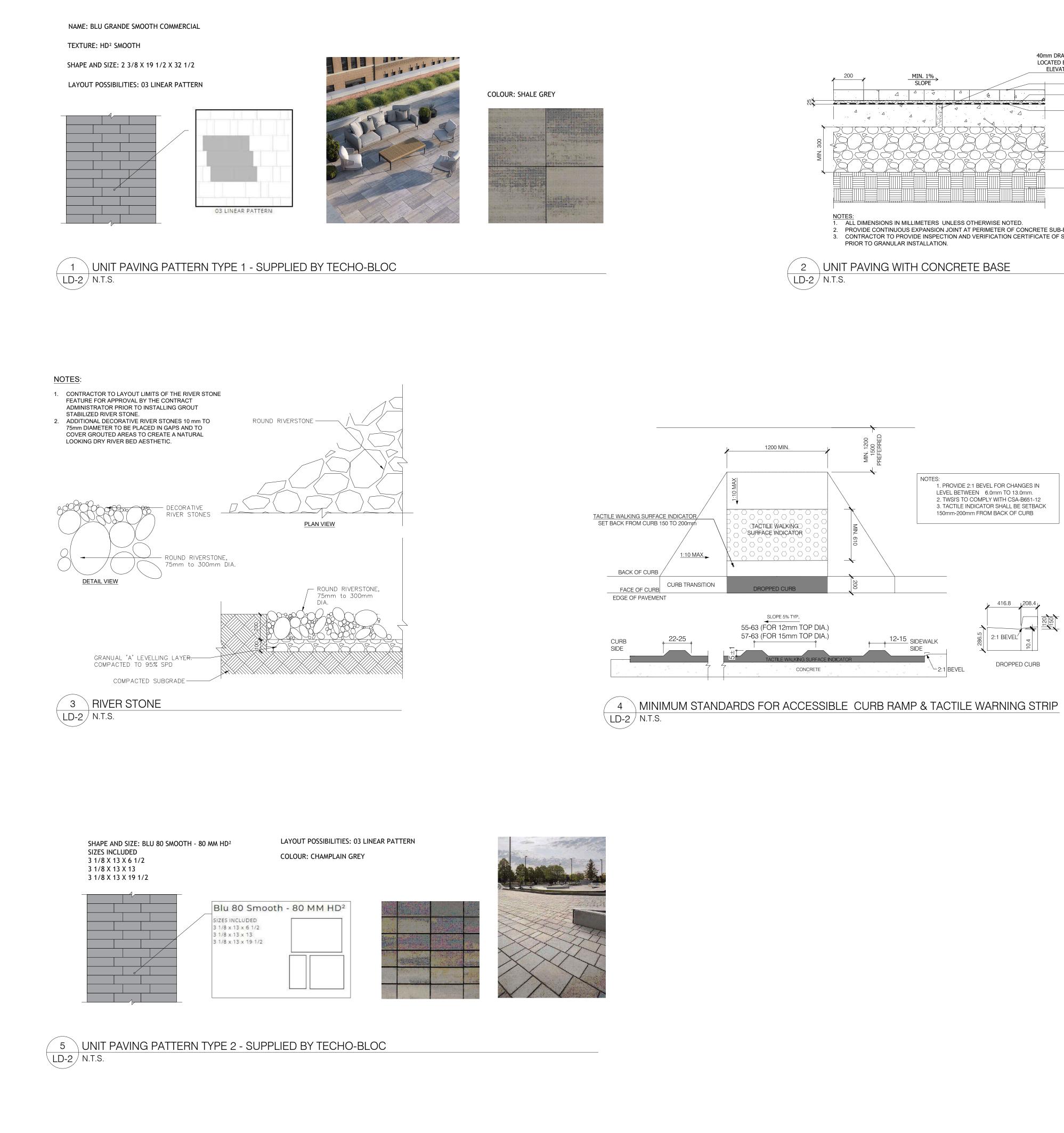


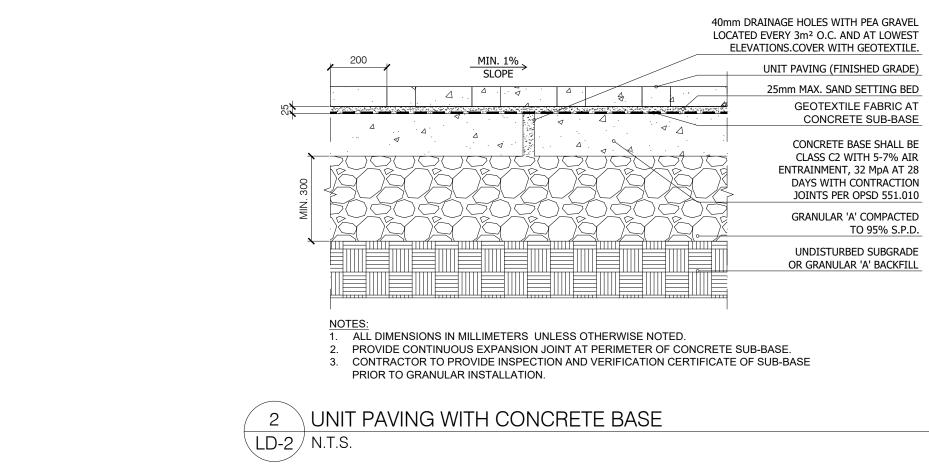




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| ISSUES No. DESCRIPTION | DATE | | | |
| 1 ISSUED FOR ZBA & SPA REVIEW 2 ISSUED FOR ZBA & SPA REVIEW 3 ISSUED FOR ZBA & SPA REVIEW 4 ISSUED FOR ZBA & SPA REVIEW | 2022-10-21 2023-03-24 2024-08-12 2024-10-11 | | | |
| | | | | |
| | | | | |
| SEAL | | | | |
| | S | | | |
| PRIME CONSULTANT PRIME CONSULTANT 410 Albert Street - Suite 101 Waterloo ON N2L 3V3 Canada tel 519 585 2255 www.arcadis.com | S | | | |
| PROJECT 424 Churchill Ave | | | | |
| | | | | |
| 139413 CHECKED BY: E.L E.L | | | | |
| PROJECT MGR: APPROVED B' M.P T.O | Y: | | | |
| SHEET TITLE LANDSCAPE DETAIL | S | | | |
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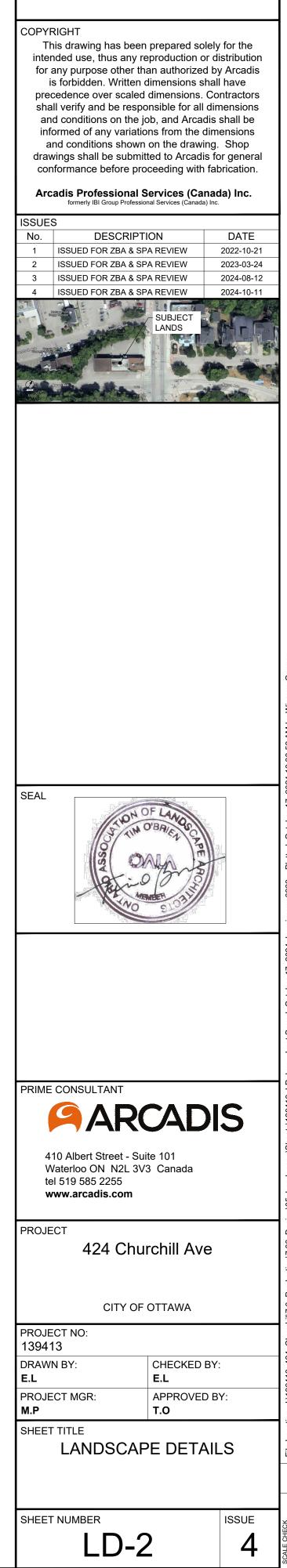
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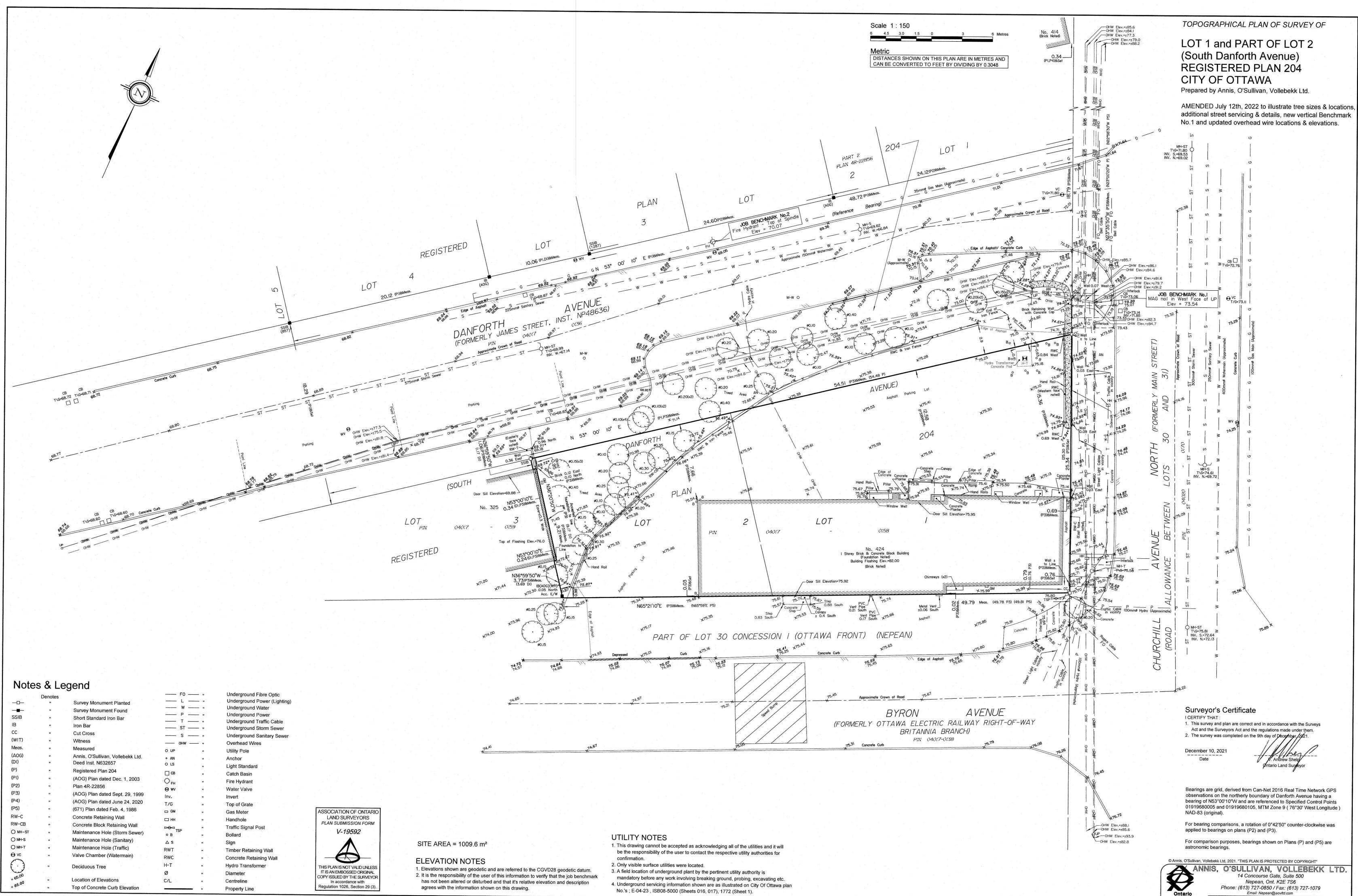




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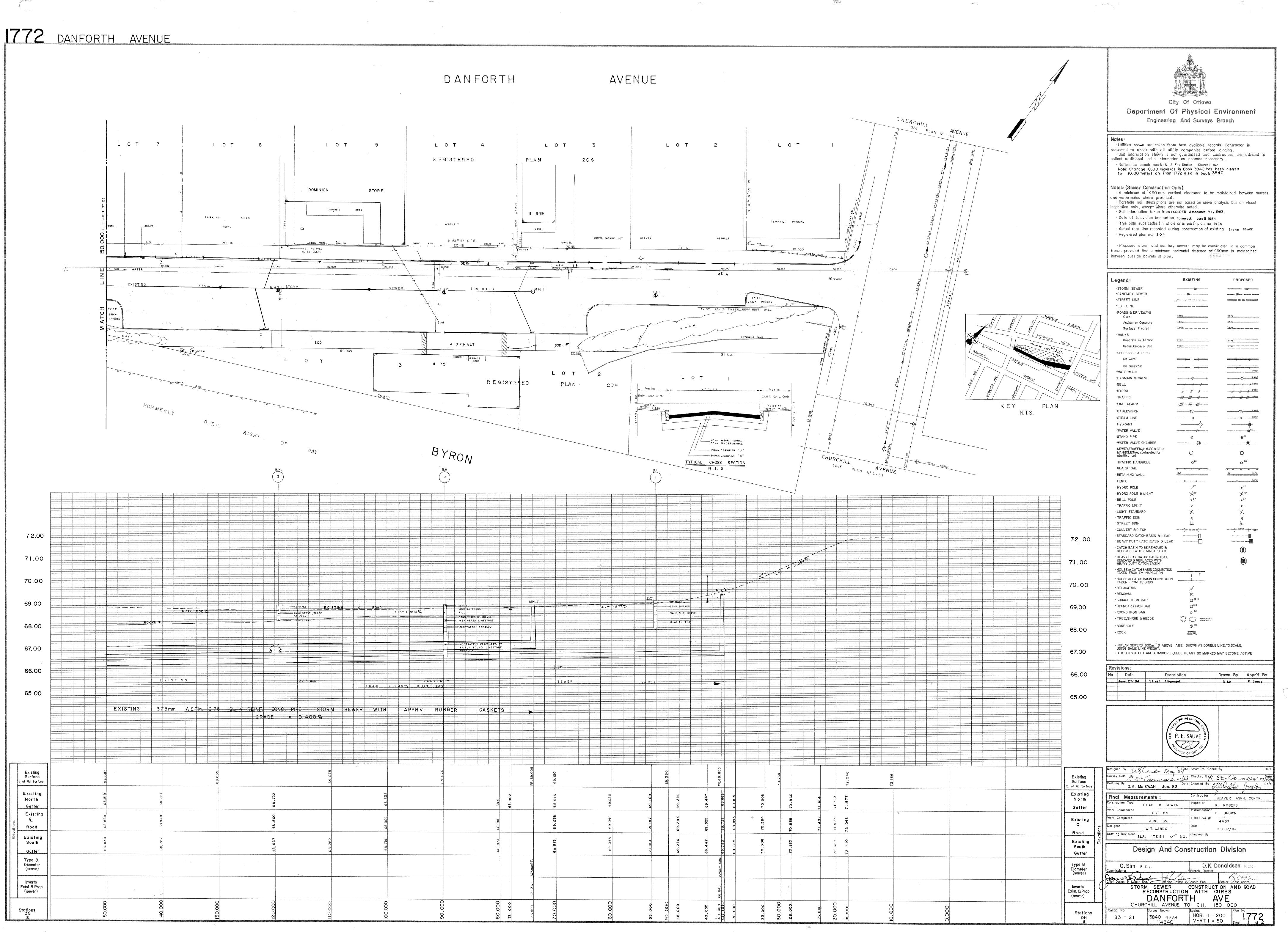


| | Denotes | | —— F0 — | n | Underground F |
|------------------------|---------|---|-----------|-----------|------------------|
| | n | Survey Monument Planted | — L — | — · · · · | Underground F |
| · · · · · | н | Survey Monument Found | — w — | <u> </u> | Underground V |
| SSIB | | Short Standard Iron Bar | —— P — | | Underground F |
| IB | | Iron Bar | — T — | | Underground T |
| CC | u | Cut Cross | ST | - " | Underground S |
| (WIT) | | Witness | S | - " | Underground S |
| Meas. | | Measured | OHW | - " | Overhead Wire |
| (AOG) | U. | | O UP | 0 | Utility Pole |
| (DI) | u | Annis, O'Sullivan, Vollebekk Ltd. Deed Inst. N632657 | • AN | н 2 | Anchor |
| (D) | | | O LS | н | Light Standard |
| | | Registered Plan 204 | СВ | | Catch Basin |
| (PI) | | (AOG) Plan dated Dec. 1, 2003 | OFH | a | Fire Hydrant |
| (P2) | н. | Plan 4R-22856 | €9 WV | u . | Water Valve |
| (P3) | н | (AOG) Plan dated Sept. 29, 1999 | Inv. | | Invert |
| (P4) | U. | (AOG) Plan dated June 24, 2020 | T/G | | Top of Grate |
| (P5) | y | (671) Plan dated Feb. 4, 1986 | GM | u | Gas Meter |
| RW-C | Ü. | Concrete Retaining Wall | — — нн | | Handhole |
| RW-CB | | Concrete Block Retaining Wall | | | |
| O MH-ST | | Maintenance Hole (Storm Sewer) | Den TSP | | Traffic Signal P |
| O MH-S | ü | Maintenance Hole (Sanitary) | оB | u. | Bollard |
| Омн-т | | Maintenance Hole (Traffic) | Δs | | Sign |
| ⊖ vc | | | RWT | н | Timber Retainir |
| 0 VC | | Valve Chamber (Watermain) | RWC | | Concrete Retai |
| $\left\{\cdot\right\}$ | н | Deciduous Tree | H-T | н | Hydro Transfor |
| Y AND | | | Ø | | Diameter |
| + 65.00 | н | Location of Elevations | C/L | н | Centreline |
| + 6 ^{5.00} | | Top of Concrete Curb Elevation | - | n | Property Line |
| | | | | | |

- No.'s ; E-04-23 , ISB08-5000 (Sheets 016, 017), 1772 (Sheet 1).

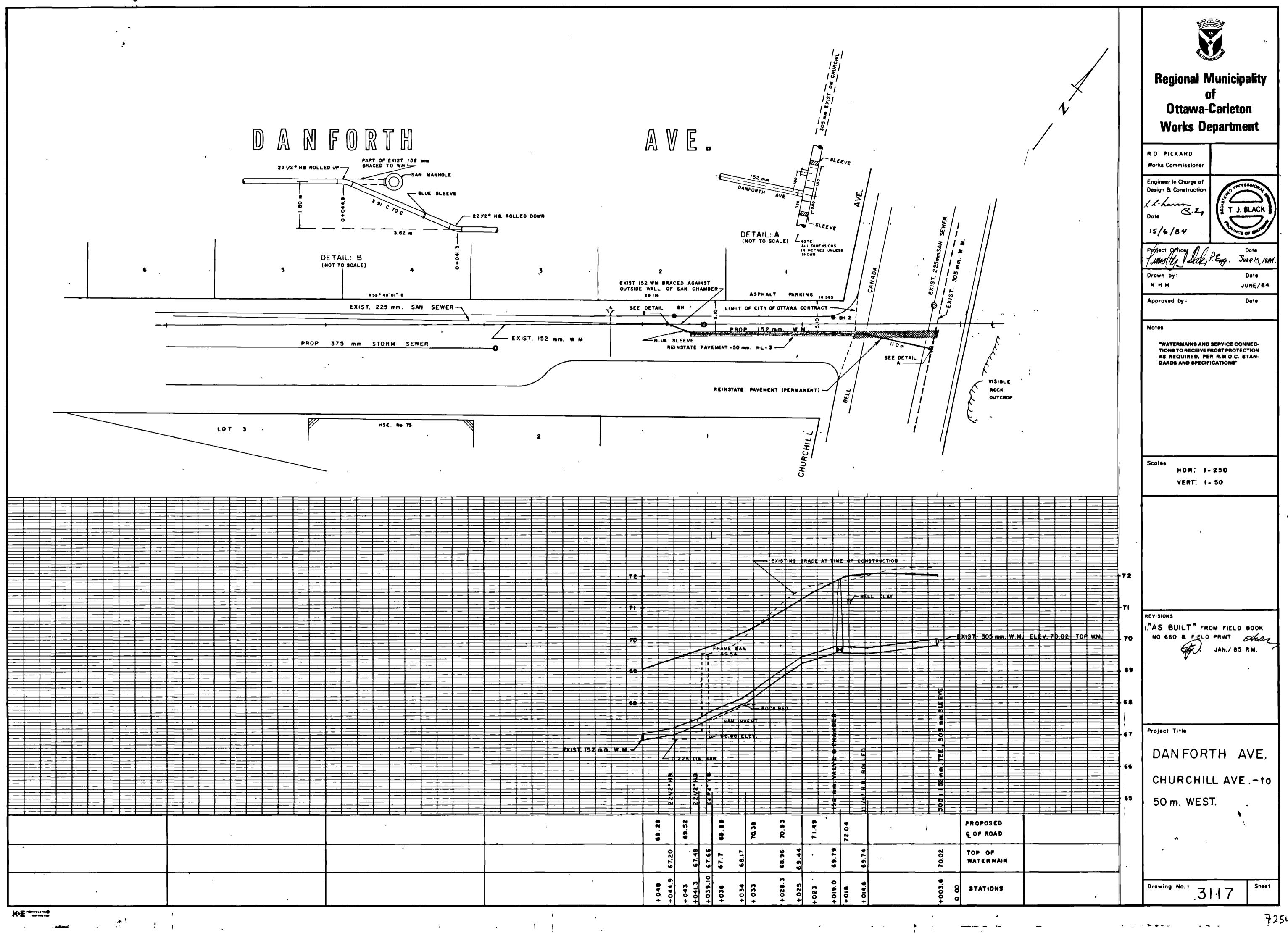
Land Surveyors Job No. 22329-21 (Amend) GSI Properties Pt. Lts 1,2 Pl.204 T F2 ns

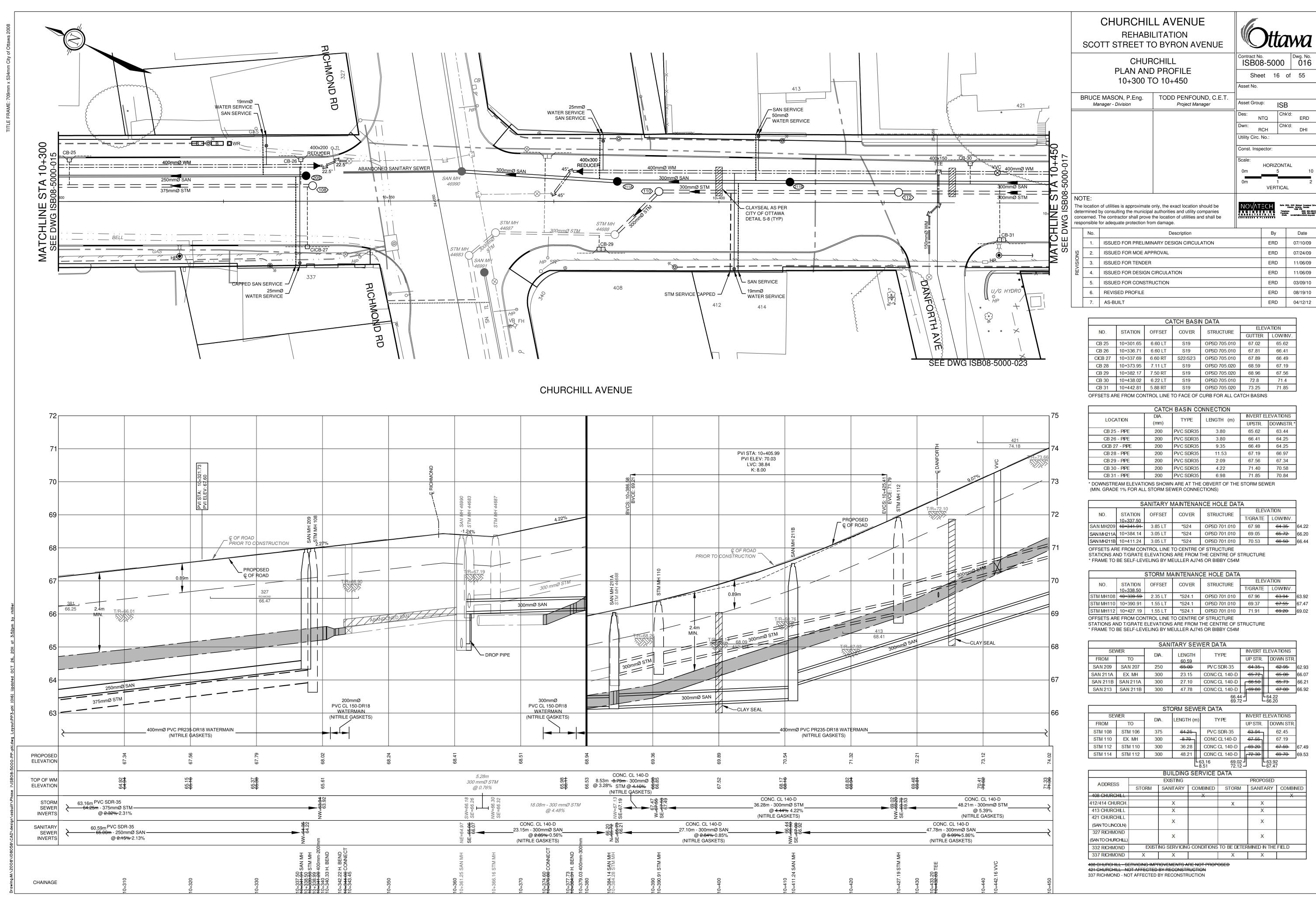




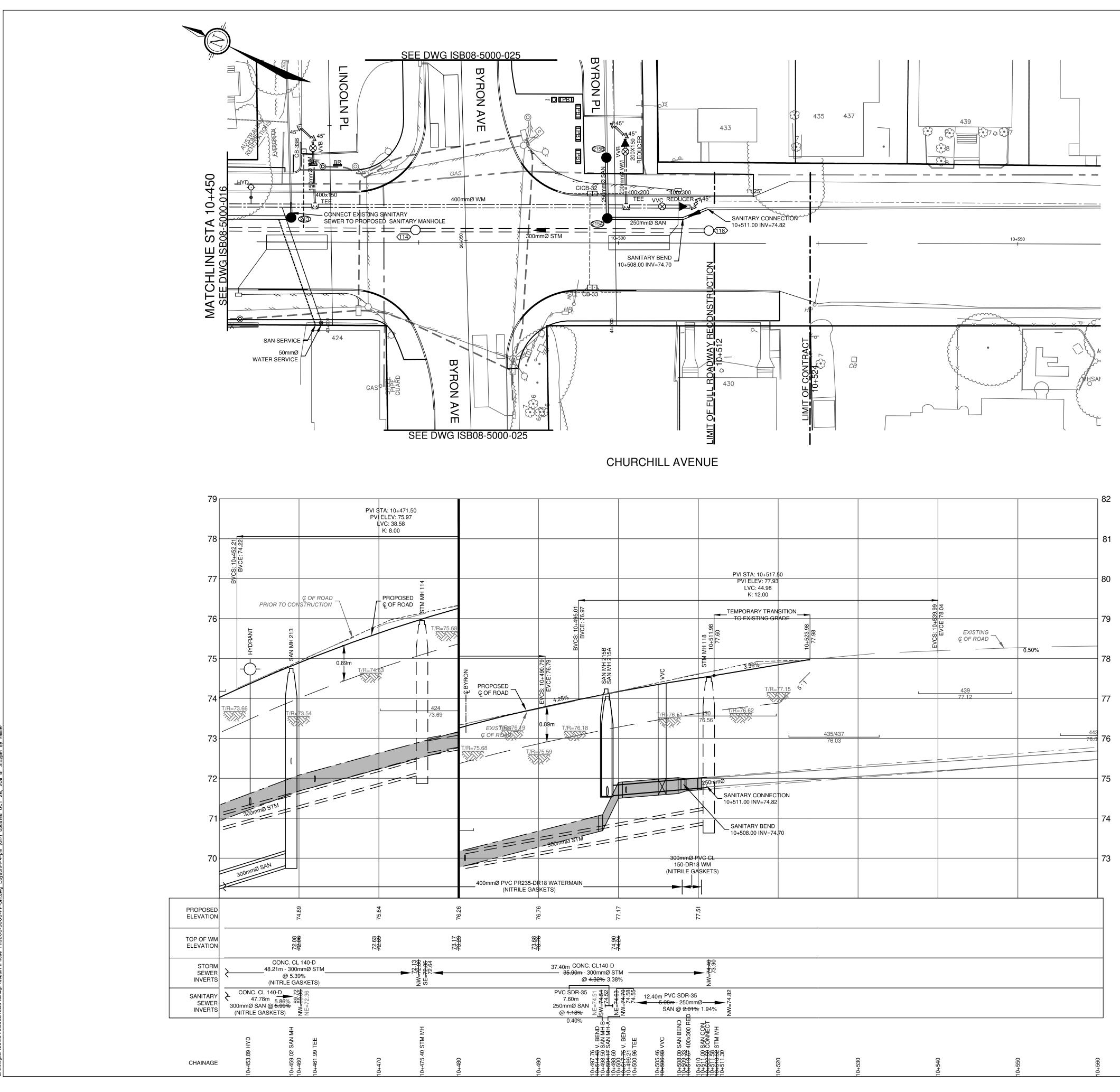
| | Existing Surface ६ of Rd. Surface | 69 085 | | t | | |
|--------|--|------------|---------|----------------------|--|-----|
| | Existing North Gutter | 68.81 9 | 68, 781 | | 68 722 | |
| ations | Existing (L Road Existing | 68,869 | 68.844 | | C B B B B B B B B B B B B B B B B B B B | • |
| | Existing South Gutter | 68.839 | 68,727 | | 68 627 | |
| | Type & Diameter (sewer) | | | | | ~~~ |
| | Inverts Exist.& Prop. (sewer) | | | | | |
| | Stations ON S. | 150.000 | 140.000 | | | |

. I A Martine





| | | TH OF | 408 | STM SERVICE CAPPED 412 | 414 | | | ANFORTH AVE SEE DWG |
|----------------|---|--|--|--|--|--|---|---|
| | | CHURCHIL | L AVENUE | | | | | |
| | | | 386.58 69,21 | | PVI STA: 10+405.99 PVI ELEV: 70.03 LVC: 38.84 K: 8.00 | | 425,41 1 71.79 | |
| | STM MH 446990 61:201 57M MH 44683 61:202 57M MH 44687 57M MH 44687 | 4.22% | A BVCS: 10+386.58 BVCE: 69.21 | PRIOR TO CO | © OF ROAD DNSTRUCTION | PRO QO PRO | PPOSED E BOY STM MH 112 STM MH 112 | T/R=72.10 |
| | | 300 mmØ STM | SAN MH 21 STM MH 21 STM MH 24 | 2.4m MIN. T/B | 0.89m 0.89m T/R=6 T/R=6 0.89m T/R=6 0.89m 0.80m 0. | 8.76 | 413 68.41 37.93 300mm@ SAN | 1 |
| | | 300mmØ PVC CL 150-DR18 WATERMAIN (NITRILE GASKETS) | 300mmø STM | 300mmØ SAN | CLAY SEAL | mmØ PVC PR235-DR18 WATI (NITRILE GASKETS) | ERMAIN | |
| 68 41 68 41 | 5.28m | | | | 70.54 | | | |
| | 300 mmØ STM @ 0.76% 2 NM= 69: 30 2 SE = 99: 30 2 SE = 99: 35 3 MM = 99: 35 3 SM= 90 3 SE = 99: 35 3 SM= 69: 3 | 8777 8787 8787 877 877 87 | (NITRLE GASKETS) (NITRLE GASKETS) (NITRL | © 000 000 000 000 000 000 000 000 | CONC. CL 14 36.28m - 300mm @ 4.44% (NITRLE GAS) AN % | 40-D nØ STM | NW = 69.02 SE = 69.73 69.53 69.48 | CONC. CL 140-E 48.2 (NI CONC. CL 140-E 47.78m - 300mmØ \$ @ 5.99% 5.8 (NITRLE GASKET |
| 10+360 | 25 SAN MH 16 STM MH | 10+3/0 10+3/0 10+3/4.60 10+3/4.60 10+3/7.73 10+3/7.73 10+379.03 10+379.03 10-380 10+379.03 10-380 10+379.03 10-380 10+370 10+370 10+370 10+370 10+370 10+370 10+370 10+370 10+370 10+370 10+370 10+370 10+370 10+370 10+370 10+370 10+377 10+370 10+300 10+370 | 10+384.14 SAN MH 10+384.28 STM MH 10+390 | 10+390.91 STM MH 10+400 | 10+410 | 24 SAN MH | 10+427.19 STM MH | 20 80 TEE |
| | | | | | | | | |



| | SCC | CHURCHIL REHABII | C |) tta | wa | |
|--------------|----------------------|------------------------------|--|---------------------------------------|--|---|
| | | CHUR PLAN AND 10+450 T | Contract No ISB08 Shee | 8-5000 | Dwg. No. 017 of 55 | |
| E | | E MASON, P.Eng. | Asset No. | ^{p:} ISE | 3 | |
| | | | | Dwn: | | ERD |
| | | | Const. Insp | | | |
| | | | | Om Om | HORIZONT 5 1 VERTICA | 10 2 |
| dete conc | location rmined l | by consulting the municipal | only, the exact location should be authorities and utility companies the location of utilities and shall be m damage. | | ECH Suite 2 RIN & Tologi T's LTR Feed CAUNERS | 200, 240 Michael Couplind Drive Kanete, Cetette, Canada Kall Pie ann (431 254-9843 de (431 254-9847 nevalafallinovatiech-seg.com |
| | No. | | Description | · · · · · · · · · · · · · · · · · · · | Ву | Date |
| S | 1. | ISSUED FOR PRELIMIN | IARY DESIGN CIRCULATION | | ERD | 07/10/09 |
| REVISIONS | 2. | ISSUED FOR MOE APP | PROVAL | | ERD | 07/24/09 |
| SIV18 | 3. | ISSUED FOR TENDER | | ERD | 11/06/09 | |
| ш | 4. | ISSUED FOR DESIGN (| | ERD | 11/06/09 | |
| | 5. | ISSUED FOR CONSTRU | ERD | 03/09/10 | | |
| | 6. | AS-BUILT | | | ERD | 04/12/12 |
| | | | | | | |

| | CATCH BASIN DATA | | | | | | | |
|---------|------------------|---------|---------|--------------|-----------|----------|--|--|
| NO. | STATION | OFFSET | COVER | STRUCTURE | ELEVATION | | | |
| NO. | UNTION | | | | GUTTER | LOW/INV. | | |
| CICB 32 | 10+496.72 | 5.88 LT | S22/S23 | OPSD 705.020 | 76.93 | 75.53 | | |
| CB 33 | 10+496.72 | 5.88 RT | S19 | OPSD 705.020 | 76.93 | 75.53 | | |
| | | | | | | | | |

OFFSETS ARE FROM CONTROL LINE TO FACE OF CURB FOR ALL CATCH BASINS

| | CATCH | BASIN CO | NNECTION | | |
|----------------|-------------------|-----------|------------|-------------------|-----------|
| LOCATION | DIA. (mm) TYPE | | LENGTH (m) | INVERT ELEVATIONS | |
| LUCATION | | | | UPSTR. | DOWNSTR.* |
| CICB 32 - PIPE | 200 | PVC SDR35 | 4.70 | 75.53 | 73.92 |
| CB 33 - PIPE | 200 | PVC SDR35 | 7.00 | 75.53 | 73.92 |

* DOWNSTREAM ELEVATIONS SHOWN ARE AT THE OBVERT OF THE STORM SEWER (MIN. GRADE 1% FOR ALL STORM SEWER CONNECTIONS)

| | | | | | | | _ | | | |
|-------------|--------------------------------|----------|-------|--------------|---------|------------------|-------|--|--|--|
| | SANITARY MAINTENANCE HOLE DATA | | | | | | | | | |
| NO. | STATION | OFFSET | COVER | STRUCTURE - | ELEV | ATION |] | | | |
| NO. | STATION | ULISEI | COVER | | T/GRATE | LOW/INV. | | | | |
| SAN MH213 | 10+459.02 | 3.05 LT | *S24 | OPSD 701.010 | 74.75 | 69.86 | 69.72 | | | |
| SAN MH215B | 10+498.47 | 10.67 LT | *S24 | OPSD 701.010 | 77.24 | 74.51 | | | | |
| SAN MH215A | 10+504.17 | 3.07 LT | *S24 | OPSD 701.010 | 77.27 | 74.63 | 74.55 | | | |
| SAN MIT-A | 10+515.65 | 3.07 LT | *S24 | OPSD 701.010 | 77.72# | 74.82 |] | | | |
| -SAN MH T-B | 10+521.49 | 4.38 LT | *\$24 | OPSD 701.010 | 77.88# | 74.90 | 1 | | | |

L 10+498.50 - 10+498.60

OFFSETS ARE FROM CONTROL LINE TO CENTRE OF STRUCTURE STATIONS AND T/GRATE ELEVATIONS ARE FROM THE CENTRE OF STRUCTURE * FRAME TO BE SELF-LEVELING BY MEULLER AJ745 OR BIBBY C54M # T/GRATE ELEVATION TO BE SET IN FEILD TO MATCH SURFACE ELEVATION IN TEMPORARY TRANSITION AREA

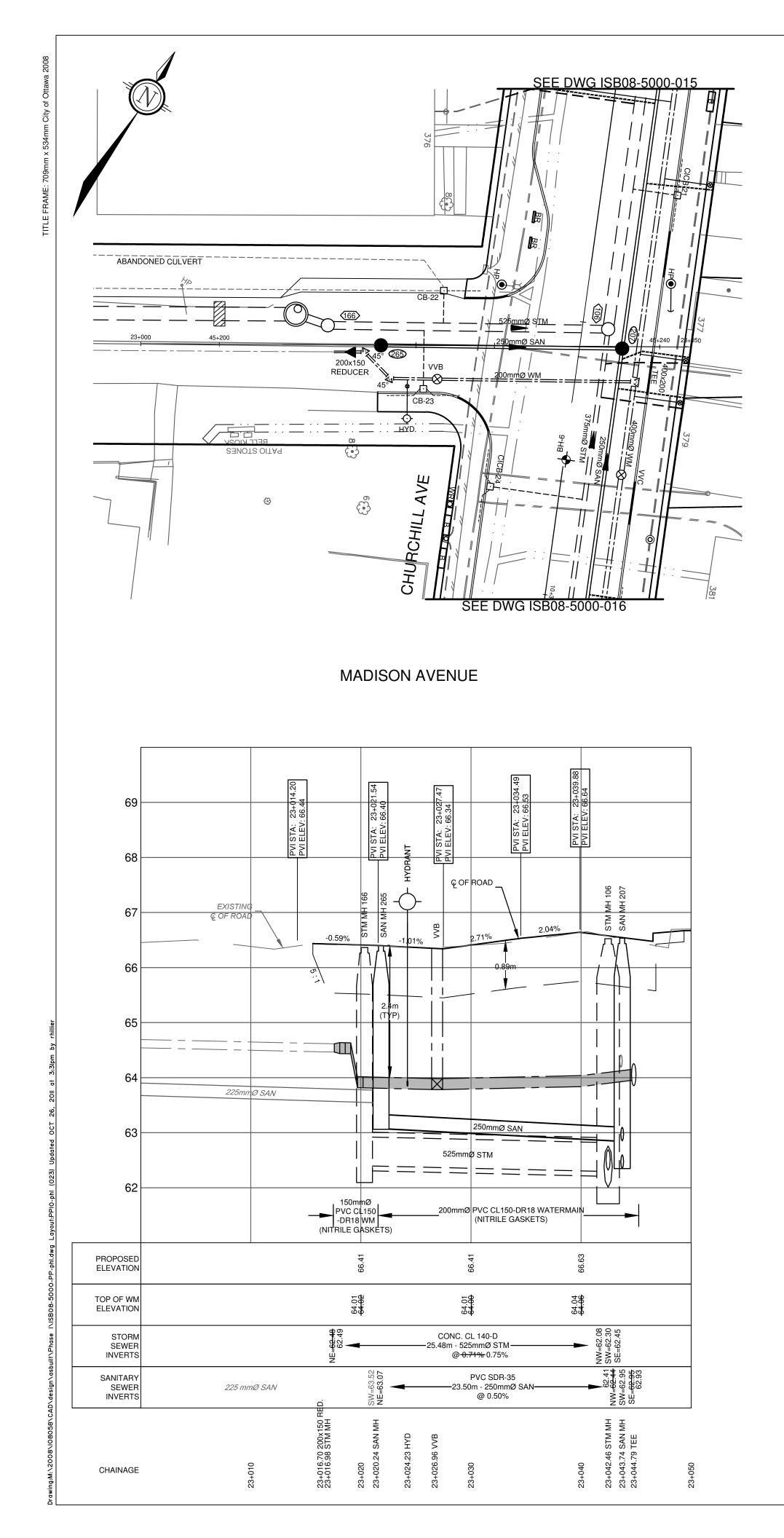
| STORM MAINTENANCE HOLE DATA | | | | | | | | |
|-----------------------------|----------------------|---------|-----------------|--------------|-----------|----------|-------|--|
| NO | STATION | OFFSET | COVER STRUCTURE | | ELEVATION | | | |
| NO. | JIATION | OTTOLI | COVER | SINCOLORE | T/GRATE | LOW/INV. | | |
| STM MH114 | 10+475.40 | 1.55 LT | *S24.1 | OPSD 701.010 | 75.95 | 72.30 | 72.12 | |
| STM MH118 | 10+518.52 | 1.57 LT | *S24.1 | OPSD 701.010 | 77.71# | 74.40 | 73.90 | |
| | 10.511.20 | | | | | | - | |

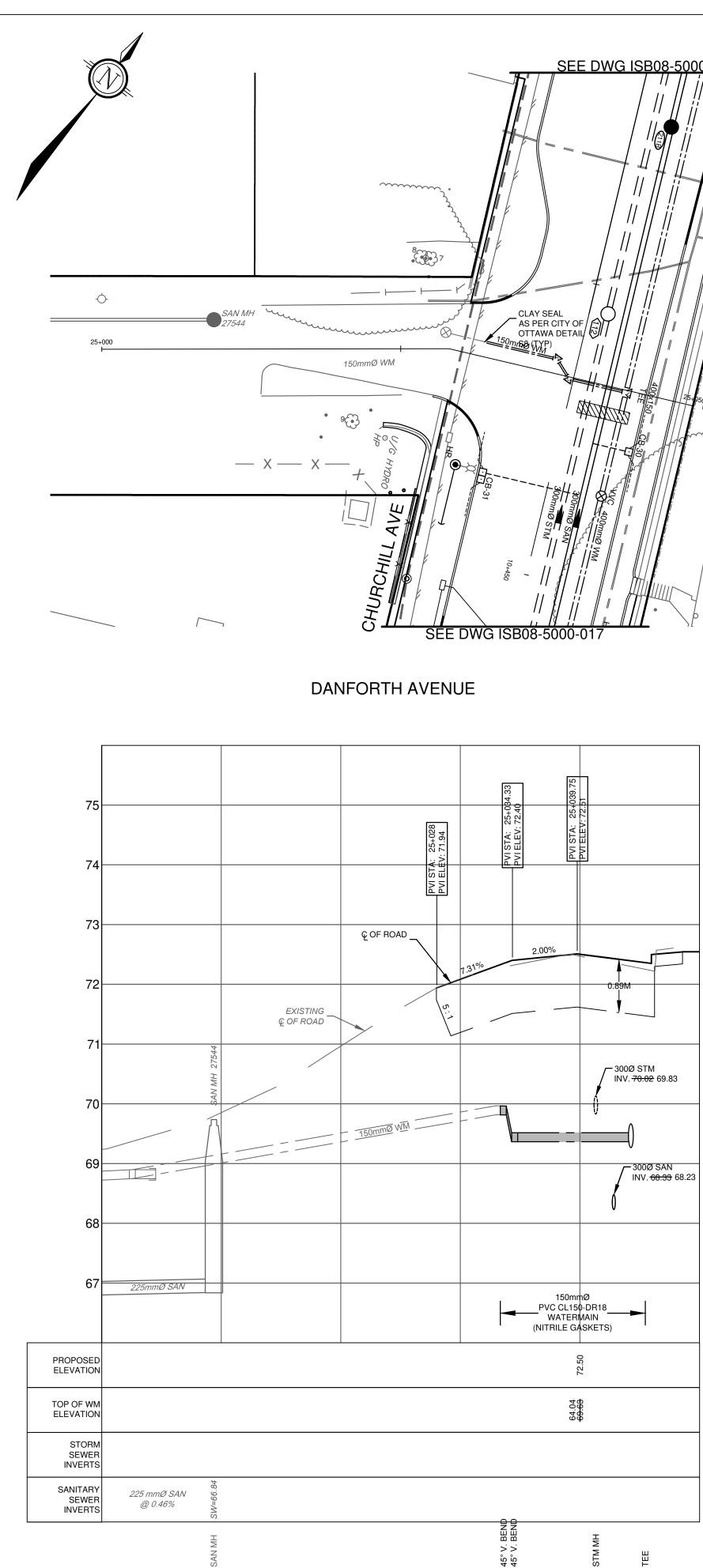
10+511.30 OFFSETS ARE FROM CONTROL LINE TO CENTRE OF STRUCTURE STATIONS AND T/GRATE ELEVATIONS ARE FROM THE CENTRE OF STRUCTURE * FRAME TO BE SELF-LEVELING BY MEULLER AJ745 OR BIBBY C54M # T/GRATE ELEVATION TO BE SET IN FEILD TO MATCH SURFACE ELEVATION IN TEMPORARY TRANSITION AREA

| SANITARY SEWER DATA | | | | | | | | |
|---------------------|----------|-------------|--------------------|---------------|------------------|------------------|-------|--|
| SEV | VER | DIA. LENGTH | | TYPE | INVERT EL | | | |
| FROM | TO | DVI. | LENGIN | 1116 | UP STR. | DOWN STR. | | |
| SAN 213 | SAN 211B | 300 | 47.78 | CONC CL 140-D | 69.86 | 67.00 | 66.92 | |
| -SAN 215A | SAN 215B | 250 | 9.50 | PVC SDR-35 | 74.63 | 74.54 | | |
| TEMP SAN A | SAN 215A | 250 | <mark>11.48</mark> | PVC SDR-35 | 74.82 | 74.66 | 74.58 | |
| TEMP SAN B | | 250 | <u>5.99</u> | PVC SDR-35 | 74.90 | 74.83 | | |
| | | L | 69.72 | - | | | | |

| STORM SEWER DATA | | | | | | | | |
|------------------|---------|-----|------------------|---------------|-------------------|------------------|------|--|
| SEV | SEWER | | LENGTH (m) | TYPE | INVERT ELEVATIONS | | | |
| FROM | TO | DA. | | ITTE | UP STR. | DOWN STR. | | |
| STM 114 | STM 112 | 300 | 48.21 | CONC CL 140-D | 72.30 | 69.70 | 69.5 | |
| STM 118 | STM 114 | 300 | 43.12 | CONC CL 140-D | 74.40 | 72.85 | 72.6 | |
| | | | 37.40 | | 73.90 L | 72.12 | _ | |

| BUILDING SERVICE DATA | | | | | | |
|-----------------------|----------|----------|----------|----------|----------|----------|
| ADDRESS | EXISTING | | | PROPOSED | | |
| ADDITEOU | STORM | SANITARY | COMBINED | STORM | SANITARY | COMBINED |
| 424 CHURCHILL | | Х | | | Х | |
| 430 CHURCHILL | | X | | | X | |





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CHAINAGE

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| | |

| | SCO | | L AVENUE LITATION O BYRON AVENUE | C |) tta | twa |
|---------------------|----------------------|-----------------------------|--|----------------------|---------------------------------|--|
| | | |) PROFILE 000 TO 23+050 | Contract No ISB08 |). 8-5000 | Dwg. No. 023 |
| | | | +000 TO 25+050 | Shee | et 23 | of 55 |
| E | | MASON, P.Eng. | TODD PENFOUND, C.E.T. Project Manager | Asset Ro. | ^{p:} IS | :D |
| | | | | Des: | | hk'd: |
| | | | | Dwn: | | ERD |
| | | | | R | CH | DHI |
| | | | | Utility Circ. | | |
| | | | | Const. Insp | ector: | |
| | | | | Scale: | HORIZON 5 | NTAL 10 |
| | | | | | VERTIC | _ |
| The dete cond | ermined I cerned. | by consulting the municipal | only, the exact location should be authorities and utility companies the location of utilities and shall be m damage. | | ECH RING TSLTR LANNERS | le 200, 240 Michael Couyland Driv Kanete, Onteria, Canede Kähl På (2013) Jaho (2013) Kanete (2013) Inda naveinfettioverlech-ang.com |
| | No. | | Description | | Ву | Date |
| S | 1. | ISSUED FOR PRELIMIN | IARY DESIGN CIRCULATION | | ERD | 07/10/09 |
| SNOISIVE | 2. | ISSUED FOR MOE APP | PROVAL | | ERD | 07/24/09 |
| SIV18 | 3. | ISSUED FOR TENDER | | | ERD | 11/06/09 |
| ш | 4. | ISSUED FOR DESIGN (| CIRCULATION | | ERD | 11/06/09 |
| | 5. | ISSUED FOR CONSTRI | JCTION | | ERD | 03/09/10 |
| | 6. | ADDED CB23 / REVISE | D PROFILE | | ERD | 08/19/10 |
| | 7. | AS-BUILT | | | ERD | 04/12/12 |

| | | CA | TCH BASI | N DATA | | |
|-------------|-----------|--------------|------------|--------------|--------|----------|
| NO | STATION | OFFSET | COVER | STRUCTURE | ELEV | ATION |
| NO. | JIAHON | OTTOLI | | OINCOTORE | GUTTER | LOW/INV. |
| CB 22 | 23+027.50 | 5.00 LT | S19 | OPSD 705.010 | 66.20 | 64.8 |
| CB 23 | 23+025.71 | 4.25 RT | S19 | OPSD 705.010 | 66.47 | 65.07 |
| OFFSET IS F | ROM CONTR | OL LINE TO C | ENTRE OF C | ATCHBASIN | | |

| | CATCH | BASIN CO | NNECTION | | |
|--|-------|-----------|------------|-----------|-----------|
| LOCATION | DIA. | TYPE | LENGTH (m) | INVERT EL | EVATIONS |
| LOGATION | (mm) | 1111 | | UPSTR. | DOWNSTR.* |
| CICB 22 - PIPE | 200 | PVC SDR35 | 3.20 | 64.94 | 62.95 |
| CICB 23 - PIPE | 200 | PVC SDR35 | 5.65 | 65.21 | 62.93 |
| * DOWNSTREAM ELEVATIONS SHOWN ARE AT THE OBVERT OF THE STORM SEWER | | | | | |

(MIN. GRADE 1% FOR ALL STORM SEWER CONNECTIONS)

| | S | ANITARY N | MAINTENA | NCE HOLE DAT | A | |
|-----------|-----------|-----------|-----------------|--------------|-------|----------|
| NO. | STATION | OFESET | COVER | STRUCTURE | ELEV. | ATION |
| NO. | OWNER | OFFOL | 00101 | ONCOTORE | | LOW/INV. |
| SAN MH265 | 23+020.24 | 0.01 RT | *S24 | OPSD 701.010 | 66.41 | 63.07 |
| | | - | | | | |

STATIONS AND T/GRATE ELEVATIONS ARE FROM THE CENTRE OF STRUCTURE * FRAME TO BE SELF-LEVELING BY MEULLER AJ745 OR BIBBY C54M

| | | STORM MA | INTENAN | CE HOLE DATA | | | |
|-----------|--|----------|---------|--------------|---------|----------|--|
| NO. | STATION | OFESET | COVER | STRUCTURE | ELEV | ATION | |
| NO. | JIATION | OFFOLI | 00101 | STRUCTURE | T/GRATE | LOW/INV. | |
| STM MH166 | 23+016.98 | 1.77 LT | *S24.1 | OPSD 701.010 | 66.39 | 62.48 | |
| | OFFSETS ARE FROM CONTROL LINE TO CENTRE OF STRUCTURE | | | | | | |

STATIONS AND T/GRATE ELEVATIONS ARE FROM THE CENTRE OF STRUCTURE * FRAME TO BE SELF-LEVELING BY MEULLER AJ745 OR BIBBY C54M

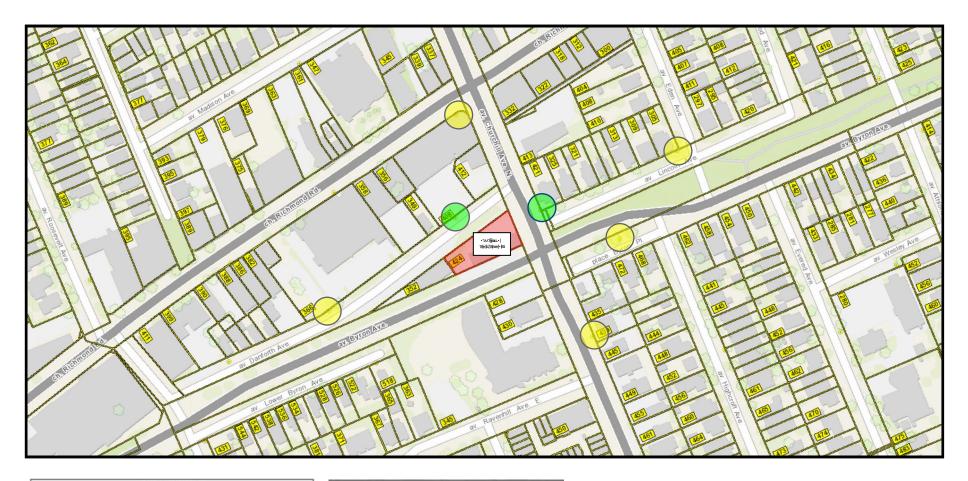
| | | SANI | TARY SEW | ER DATA | | |
|---------|---------|------|----------|-------------|-----------|-----------|
| SEWER | | DIA. | LENGTH | TYPE | INVERT EL | EVATIONS |
| FROM | TO | DIA. | LLINGTH | TTE | UP STR. | DOWN STR. |
| SAN 265 | SAN 207 | 250 | 23.50 | PV C SDR-35 | 63.07 | 62.95 |

| | | STO | ORM SEWE | R DATA | | |
|---------|---------|------|------------|---------------|-----------|-----------|
| SEWER | | DIA. | LENGTH (m) | TYPE | INVERT EL | EVATIONS |
| FROM | TO | UA. | | ITE | UP STR. | DOWN STR. |
| STM 166 | STM 106 | 525 | 25.48 | CONC CL 140-D | 62.48 | 62.30 |

APPENDIX G

Fire Hydrant Coverage

FIRE HYDRANT FIGURE



LEGEND Hydrants within 75m

 \bigcirc

Hydrants within 150m

| Distance to | Building ^a | Maximum Capacity ^b | | | |
|------------------------------|------------------------|-------------------------------|---------|--|--|
| (ft) | (m) | (gpm) | (L/min) | | |
| ≤ 250 | ≤ 76 | 1500 | 5678 | | |
| > 250 and ≤ 500 > 500 and | >76 and ≤ 152 | 1000 | 3785 | | |
| ≤ 1000 | > 152 and ≤ 305 | 750 | 2839 | | |

*Measured in accordance with 18.5.1.4 and 18.5.1.5. ^bMinimum 20 psi (139.9 kPa) residual pressure.