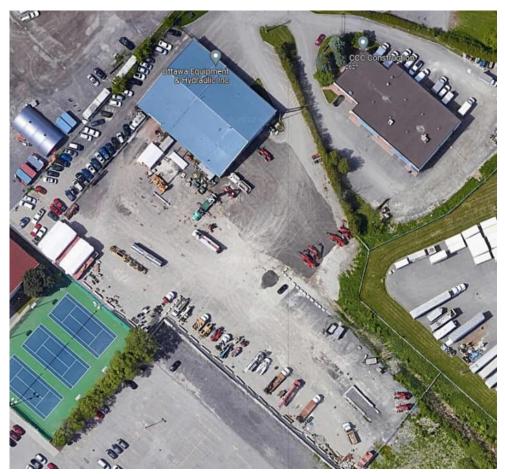
SERVICING & STORMWATER MANAGEMENT REPORT 2628 EDINBURGH PLACE



Project No.: CCO-22-2058

City File No.: D07-12-22-0184

Prepared for:

BBS Construction Ltd 1805 Woodward Drive Ottawa, ON K2C 0P9

Prepared by:

McIntosh Perry Consulting Engineers Ltd. 115 Walgreen Road Carp, ON K0A 1L0

December 5th, 2022

Rev02: April 28th, 2023

McINTOSH PERRY

TABLE OF CONTENTS

1.0	PROJECT DESCRIPTION	1
1.1	Purpose	1
1.2	Ste Description	1
1.3	Proposed Development and Statistics	2
1.4	Existing Conditions and Infrastructures	2
1.5	Approvals	2
2.0	BACKROUND STUDIES, STANDARDS, AND REFERENCES	3
2.1	Background Reports / Reference Information	3
2.2	Applicable Guidelines and Standards	3
3.0	PRE-CONSULTATION SUMMARY	4
4.0	WATERMAIN	5
4.1	Existing Watermain	5
4.2	Proposed Watermain	5
5.0	SANITARY DESIGN	7
5.1	Existing Sanitary Sewer	7
5.2	Proposed Sanitary Sewer	7
6.0	STORM SEWER DESIGN	9
6.1	Existing Storm Sewers	9
6.2	Proposed Storm Sewers	9
7.0	PROPOSED STORM WATER MANAGEMENT	10
7.1	Design Criteria and Methodology	10
7.2	Runoff Calculations	10
7.3	Pre-Development Drainage	11
7.4	Post-Development Drainage	11
7.5	Quality Control	12
8.0	EROSION AND SEDIMENT CONTROL	13
8.1	Temporary Measures	13
8.2	Permanent Measures	13

MCINTOSH PERRY

9.0	SUMMARY	14
10.0	RECOM M ENDATION	15
11.0	STATEM ENT OF LIMITATIONS	16

LIST OF TABLES

Table 1: Water Supply Design Criteria	. 5
Table 2: Summary of Estimated Water Demand	. 6
Table 3: Fire Protection Confirmation	. 6
Table 4: Sanitary Design Criteria	. 7
Table 5: Summary of Estimated Sanitary Flow	. 7
Table 6: Pre-Development Runoff Summary	11
Table 7: Required Restricted Flow	11
Table 8: Post-Development Runoff Summary	11

APPENDICES

Appendix A: Ste Location Plan Appendix B: Background Documents Appendix C: Watermain Calculations Appendix D: Sanitary Calculations Appendix E: Pre-Development Drainage Plan Appendix F: Post-Development Drainage Plan Appendix G: Stormwater Management Calculations Appendix H: Oty of Ottawa Design Checklist

MCINTOSH PERRY

1.0 PROJECT DESCRIPTION

1.1 Purpose

McIntosh Perry (MP) has been retained by BBS Construction LTD to prepare this Servicing and Stormwater Management Report in support of the Ste Plan Control process for the proposed development located at 2628 Edinburgh Place within the City of Ottawa.

The main purpose of this report is to present a servicing and stormwater management design for the development in accordance with the recommendations and guidelines provided by the City of Ottawa (City), the Rideau Valley Conservation Authority (RVCA), and the Ministry of the Environment, Conservation and Parks (MECP). This report will address the water, sanitary and storm sewer servicing for the development, ensuring that existing and available services will adequately service the proposed development.

This report should be read in conjunction with the following drawings:

- CCO-22-2058, C101 Erosion, Sediment Control, Grading and Drainage Plan
- CCO-22-2058, C102 Site Servicing Plan
- CCO-22-2058, PRE Pre-Development Drainage Area Plan (Appendix E)
- CCO-22-2058, POST Post-Development Drainage Area Plan (Appendix F)

1.2 Site Description

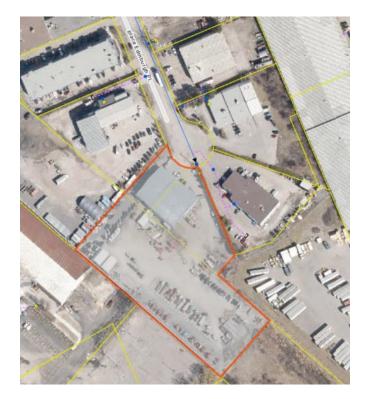


Figure 1: Ste Map

The subject property, herein referred to as the site, is located at 2628 Edinburgh Place within the Alta Vista ward. The site covers approximately 1.34 ha and is located at the end of Edinburgh Place. The site is zoned for Heavy Industrial Use (IH) and Light Industrial use (IL). See Ste Location Plan in Appendix 'A' for more details.

1.3 Proposed Development and Statistics

The proposed development consists of a 1003 m² addition to the existing building. The proposed addition will contain a sales area, service bays, storage areas, and a staff amenity area. Parking and drive aisles will be reconfigured as part of the development. Development is proposed within 1.33 ha of the site. Refer to Ste Plan (SP1) prepared by GJA Inc. and included in Appendix B for further details.

1.4 Existing Conditions and Infrastructures

The site is currently developed containing an existing 1-storey commercial/industrial building with asphalt and gravel parking areas, and gravel storage areas in the rear yard. The existing building is serviced via a 150 mm sanitary service connected to the 250 mm diameter concrete sanitary sewer located within Edinburgh Place. Water servicing is assumed to be connected to the 305 mm diameter watermain within Edinburgh Place.

Sewer and watermain mapping collected from the City of Ottawa indicate that the following services exist across the property frontages within the adjacent municipal rights-of-way(s):

- Edinburgh Place
 - 305 mm diameter DI watermain, and
 - 450 mm diameter concrete storm sewer tributary to Green's Creek, and
 - 250 mm diameter concrete sanitary sewer, tributary to the Innes Road trunk sewer.

1.5 Approvals

The proposed development is subject to the City of Ottawa site plan control approval process. Site plan control requires the City to review, provided concurrence and approve the engineering design package. Permits to construct can be requested once the City has issued a site plan agreement.

An Environmental Compliance Approval (ECA) through the Ministry of Environment, Conservation and Parks (MECP) is not anticipated to be required since the proposed storm sewer system services one parcel of land and is not tributary to a combined sewershed. ECA requirements to be further discussed with City staff due to the heavy industrial zoning.

2.0 BACKROUND STUDIES, STANDARDS, AND REFERENCES

2.1 Background Reports / Reference Information

As-built drawings of existing services, provided by the City of Ottawa Information centre, within the vicinity of the proposed site were reviewed in order to identify infrastructure available to service the proposed development.

A topographic survey (22676-22) of the site was completed by Annis, O'Sullivan, Vollebekk Ltd. and dated March 9th, 2022.

The Ste Plan (SP1) was prepared by GJA Inc. and dated April 28th, 2023 (Ste Plan).

A geotechnical report was completed by Paterson Group and dated August 17th, 2022.

2.2 Applicable Guidelines and Standards

City of Ottawa:

- Ottawa Sewer Design Guidelines, City of Ottawa, SDG002, October 2012. (Ottawa Sewer Guidelines)
 - Technical Bulletin ISTB-2014-01 City of Ottawa, February 2014. (ISTB-2014-01)
 - Technical Bulletin PIEDTB-2016-01 City of Ottawa, September 2016. (PIEDTB-2016-01)
 - Technical Bulletin ISTB-2018-01 City of Ottawa, January 2018. (ISTB-2018-01)
 - Technical Bulletin ISTB-2018-04 City of Ottawa, March 2018. (ISTB-2018-04)
 - Technical Bulletin ISTB-2019-02 City of Ottawa, February 2019. (ISTB-2019-02)
- Ottawa Design Guidelines Water Distribution City of Ottawa, July 2010. (Ottawa Water Guidelines)
 - Technical Bulletin ISD-2010-2 City of Ottawa, December 15, 2010. (ISD-2010-2)
 - Technical Bulletin ISDTB-2014-02 City of Ottawa, May 2014. (ISDTB-2014-02)
 - Technical Bulletin ISTB-2018-02 City of Ottawa, March 2018. (ISTB-2018-02)
 - Technical Bulletin ISTB-2021-03 City of Ottawa, August 2021. (ISTB-2021-03)

Ministry of Environment, Conservation and Parks:

- Stormwater Planning and Design Manual, Ministry of the Environment, March 2003. (MECP Stormwater Design Manual)
- Design Guidelines for Sewage Works, Ministry of the Environment, 2008. (MEOP Sewer Design Guidelines)

Other:

• Water Supply for Public Fire Protection, Fire Underwriters Survey, 2020. (FUS Guidelines)

3.0 PRE-CONSULTATION SUMMARY

A pre-consultation meeting was held with City staff on September 15th, 2021, regarding the proposed site servicing. Specific design parameters to be incorporated within this design include the following:

- Pre-development and post-development flows shall be calculated using a time of concentration (Tc) no less than 10 minutes.
- Control 5 through 100-year post-development flows to the 5-year pre-development flows with a combined C value to a maximum of 0.50.
- Quality control requirements to be provided by the Rideau Valley Conservation Authority (RVCA).

4.0 WATERMAIN

4.1 Existing Watermain

The site is located within the 1E pressure zone, as per the Water Distribution System mapping included in Appendix C. There are two public fire hydrants along Edinburgh Place available to service the development.

4.2 Proposed Watermain

It is proposed to service the proposed building addition through the existing building. A mechanical consultant will need to review and confirm whether upgrades to the existing building are required to accommodate the addition.

Table 1, below, summarizes the water supply design criteria obtained from the Ottawa Water Guidelines and utilized for the water analysis.

Table 1: Water Supply Design Criteria

Ste Area	1.34 ha	
Commercial Area	28,000 L/ gross ha/ day	
Max Day Peaking Factor	1.5 x avg. day	
Peak Hour Peaking Factor	1.8 x max. day	

The Fire Underwriters Survey 2020 (FUS) method was utilized to estimate the required fire flow for the site. Fire flow requirements were calculated per City of Ottawa Technical Bulletin ISTB-2018-02. The following parameters were assumed for the FUS calculation:

- Type of construction Non-Combustible Construction
- Occupancy Type Combustible
- Sprinkler Protection No Sprinkler System

The results of the calculations yielded a required fire flow of 9,000 L/min (150 L/s). The detailed calculations for the FUS can be found in Appendix C.

The city provided the estimated water pressures at both the average day scenario, peak hour scenario, and the max day plus fire flow scenario for the demands indicated by the correspondence in Appendix C. The resulting pressures for the boundary conditions results are shown in Table 2, below.

Scenario	Proposed Demands (L/ S)	Connection 1 HGL (m H₂O)* / kPa		
Average Day Demand	0.44	51.8 / 507.7		
Maximum Daily + Fire Flow Demand (FUS)	150.65	32.3 / 316.4		
Maximum Daily + Fire Flow Demand (OBC)	150.65	32.3 / 316.4		
Peak Hourly Demand	1.17	43.8 / 429.2		
* Adjusted for an estimated ground elevation of 68.48m above the connection point.				

The normal operating pressure range is anticipated to be 429.2 kPa to 507.7 kPa and will not be less than 275 kPa (40 psi) or exceed 689 kPa (100 psi). The proposed watermains will meet the minimum required 20 psi (140 kPa) from the Ottawa Water Guidelines at the ground level under maximum day demand and fire flow conditions.

To confirm the adequacy of fire flow to protect the proposed development, public fire hydrants within 150 m of the proposed building were analysed per City of Ottawa ISTB 2018-02 Appendix I Table 1. The results are summarized below.

Table 3: Fire Protection Confirmation

Building	Fire How Demand (L/ min.)	Fire Hydrant(s) within 75m (5,700 L/ min)	Fire Hydrant(s) within 150m (3,800 L/ min)	Combined Fire Flow (L/ min.)
2628 Edinburgh Place	9,000	1 Public	1 Public	9,500

Based on City guidelines (ISTB-2018-02), the existing hydrants provide adequate protection for the proposed development. A hydrant coverage figure can be found in Appendix C.

5.0 SANITARY DESIGN

5.1 Existing Sanitary Sewer

There is an existing 150 mm diameter service connection to the 250mm diameter concrete sanitary sewer located within Edinburgh Place, which is tributary to the Innes Road trunk sewer. No changes are proposed to the existing sanitary sewer system.

5.2 Proposed Sanitary Sewer

It is proposed to service the proposed building addition through the existing building. A mechanical consultant will need to review and confirm whether upgrades to the existing building are required to accommodate the addition.

Table 4, below, summarizes the wastewater design criteria identified by the Ottawa Sewer Guidelines.

Design Parameter	Value
Ste Area	1.34 ha
Commercial Area	2211 m ²
Commercial Peaking Factor	1.5
Extraneous Row Allowance	0.33 L/ s/ ha

Table 4: Sanitary Design Criteria

Table 5 below, summarizes the estimated wastewater flow from the proposed development. Refer to Appendix D for detailed calculations.

Table 5: Summary of Estimated Sanitary Row

Design Parameter	Total How (L/s)
Total Estimated Average Dry Weather Flow	0.14
Total Estimated Peak Dry Weather Flow	0.17
Total Estimated Peak Wet Weather Flow	0.55

As noted above, the development is proposed to be serviced via the existing 150 mm sanitary service connection to the 250 mm concrete sanitary sewer within Edinburgh Place. Due to the complexity of the downstream network the City will need to advise of any downstream constraints.

The full flowing capacity of a 150 mm diameter service at a 1.0% slope is estimated to be 15.89 L/s. Per Table 5, a peak wet weather flow of 0.55 L/s will be conveyed within the 150 mm diameter service, therefore the existing sanitary service is sufficiently sized for the development.

6.0 STORM SEWER DESIGN

6.1 Existing Storm Sewers

There is an existing 450 mm diameter storm sewer within Edinburgh Place that is available to service the site. The existing sewer is tributary to Green's Creek approximately 1.6 km downstream.

6.2 Proposed Storm Sewers

The proposed development will be serviced through an on-site storm sewer network connected to the existing 450 mm diameter storm sewer within Edinburgh Place.

Runoff from the proposed roof, parking, storage, and landscaped areas will be directed towards catch basins and catch basins maintenance holes. The storm flow will be treated for quality, stored, and controlled. Storm flows will be controlled by an inlet control device (ICD) to limit the flow to the specified allowable release rate.

See CCO-22-2058 - POST include in Appendix F of this report for more details. The Stormwater Management design for the subject property will be outlined in Section 7.0 of this report.

7.0 PROPOSED STORM WATER MANAGEMENT

7.1 Design Criteria and Methodology

As per Section 6.2, stormwater management for the proposed development will be provided by catch basin flow attenuation and surface storage. The controlled stormwater flow will be directed to the existing 450 mm diameter storm sewer within Edinburgh Place.

In summary, the following design criteria have been employed in developing the stormwater management design for the site as directed by the RVCA and City:

Quality Control

• Based on coordination with the RVCA, quality controls, up to an enhanced level of treatment, are required for the development.

Quantity Control

- Any storm events greater than the 5-year, up to 100-year, and including 100-year storm event must be detained on site.
- Post-development to be restricted to the 5-year storm event, based on a calculated time of concentration of at least 10 minutes and a maximum combined maximum rational method coefficient of 0.50. Refer to Section 7.2 for further details.

7.2 Runoff Calculations

Runoff calculations presented in this report are derived using the Rational Method, given as:

		Q = 2.78 CIA (L/s)
Where:	С	= Runoff coefficient
	I	= Rainfall intensity in mm/hr (City of Ottawa IDF curves)
	А	= Drainage area in hectares

It is recognized that the Pational Method tends to overestimate runoff rates. As a result, the conservative calculation of runoff ensures that any SWM facility sized using this method is expected to function as intended. The following coefficients were used to develop an average C for each area:

Roofs/Concrete/Asphalt	0.90
Undeveloped and Grass	0.20

As per the City of Ottawa - Sewer Design Guidelines, the 5-year balanced 'C' value must be increased by 25% for a 100-year storm event to a maximum of 1.0.

7.3 Pre-Development Drainage

It has been assumed that the development area contains no stormwater management controls for flow attenuation. The estimated pre-development peak flows for the 5- and 100-year events are summarized below in Table 6. See CCO-22-2058 - PRE in Appendix E and Appendix G for calculations.

Dusiasas	A	С		Q (L/ s)	
Drainage Area	Area (ha)	5-Year	100-Year	5-Year	100-Year
A1	1.33	0.70	0.83	269.41	547.83

Table 6: Pre-Development Runoff Summary

Table 7, below, summarizes the required restricted flow.

Table 7: Required Restricted Flow

Drainage	Area	C	Q (L/ s)
Area	(ha)	(5-Year)	5-Year
A1	1.33	0.50	192.47

7.4 Post-Development Drainage

To meet the stormwater objectives, the development will contain flow attenuation via surface storage.

Based on the criteria listed in Section 7.1, the development will be required to restrict flow to the 5-year storm event. It is estimated that the target release rate during the 100-year event will be 192.47 L/s. See Appendix G for calculations.

The proposed site drainage limits are demonstrated on the Post-Development Drainage Area Plan. See CCO-22-2058 - POST in Appendix F of this report for more details. A summary of the postdevelopment runoff calculations can be found below.

Drainage Area	Area (ha)	5-year Peak How (L∕ s)	100-year Peak Row (L∕ s)	100-year Storage Required (m³)	100-year Storage Available (m³)
B1	1.25	167.65	173.85	187.8	188.0
B2	0.08	7.17	15.36	-	-
Total	1.33	175.45	189.81	187.48	187.97

Table 8: Post-Development Runoff Summary

The flow from Area B2 will be discharged without restriction and will be compensated for in areas with attenuation.

Runoff for area B2 will flow overland towards the proposed catch basin systems. Stormwater will be restricted by a 264 mm ICD to a maximum release rate of 173.85 L/s. The ICD will be located at the outlet of CBMH1 at an invert elevation of 67.07. The catch basin system will provide 188.0 m³ of surface storage.

7.5 Quality Control

As noted in Section 7.1, quality controls are required for the development. Per drawing C102, a Hydro International FD-4HC (or approved equivalent) is proposed to be installed at the downstream end of the proposed storm servicing. The oil & grit separator structure will provide an enhanced level of treatment (80% TSS removal) for the parking lot, roof, and landscaped areas. Refer to Appendix G for OGS sizing and TSS removal calculations.

Storm runoff from area B2 will consist of runoff from landscaped areas and will maintain existing drainage patterns.

8.0 EROSION AND SEDIMENT CONTROL

8.1 Temporary Measures

Before construction begins, temporary silt fence, straw bale or rock flow check dams will be installed at all-natural runoff outlets from the property. It is crucial that these controls be maintained throughout construction and inspection of sediment and erosion control will be facilitated by the Contractor or Contract Administration staff throughout the construction period.

SIt fences will be installed where shown on the final engineering plans, specifically along the downstream property limits. The Contractor, at their discretion or at the instruction of the City, Conservation Authority or the Contract Administrator shall increase the quantity of sediment and erosion controls on-site to ensure that the site is operating as intended and no additional sediment finds its way off site. The rock flow, straw bale & silt fence check dams and barriers shall be inspected weekly and after rainfall events. Care shall be taken to properly remove sediment from the fences and check dams as required. Fibre roll barriers are to be installed at all existing curb inlet catch basins and filter fabric is to be placed under the grates of all existing catch basins and manholes along the frontage of the site and any new structures immediately upon installation. The measures for the existing/ proposed structures are to be removed only after all areas have been paved. Care shall be taken at the removal stage to ensure that any silt that has accumulated is properly handled and disposed of. Removal of silt fences without prior removal of the sediments shall not be permitted.

Although not anticipated, work through winter months shall be closely monitored for erosion along sloped areas. Should erosion be noted, the Contractor shall be alerted and shall take all necessary steps to rectify the situation. Should the Contractor's efforts fail at remediating the eroded areas, the Contractor shall contact the City and/or Conservation Authority to review the site conditions and determine the appropriate course of action. As the ground begins to thaw, the Contractor shall place silt fencing at all required locations as soon as ground conditions warrant. Please see the Ste Grading, Drainage and Sediment & Erosion Control Plan for additional details regarding the temporary measures to be installed and their appropriate OPSD references.

8.2 Permanent Measures

It is expected that the Contractor will promptly ensure that all disturbed areas receive topsoil and seed/sod and that grass be established as soon as possible. Any areas of excess fill shall be removed or levelled as soon as possible and must be located a sufficient distance from any watercourse to ensure that no sediment is washed out into the watercourse. As the vegetation growth within the site provides a key component to the control of sediment for the site, it must be properly maintained once established. Once the construction is complete, it will be up to the landowner to maintain the vegetation and ensure that the vegetation is not overgrown or impeded by foreign objects.

9.0 SUMMARY

- A new 1003 m² building addition is proposed to be constructed at 2628 Edinburgh Place. The development is proposed within 1.33 ha of the site.
- It is proposed to service the new building through the existing service connection for water and sanitary. A new storm service is proposed to collect and control drainage within the development area.
- It is proposed to service the development area via surface storage with a series of catch basins. The storm system will connect to the existing 450 mm diameter concrete storm sewer located south of the site.
- Storage for the 5- through 100-year storm events will be provided by surface storage.
- Quality controls will be provided up to an enhanced level of treatment via an Oil and Grit separator.

10.0 RECOMMENDATION

Based on the information presented in this report, we recommend that City of Ottawa approve this Servicing and Stormwater Management report in support of the proposed development at 2628 Edinburgh Place.

This report is respectfully being submitted for approval.

Regards,

McIntosh Perry Consulting Engineers Ltd.



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Francis Valent

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11.0 STATEMENT OF LIMITATIONS

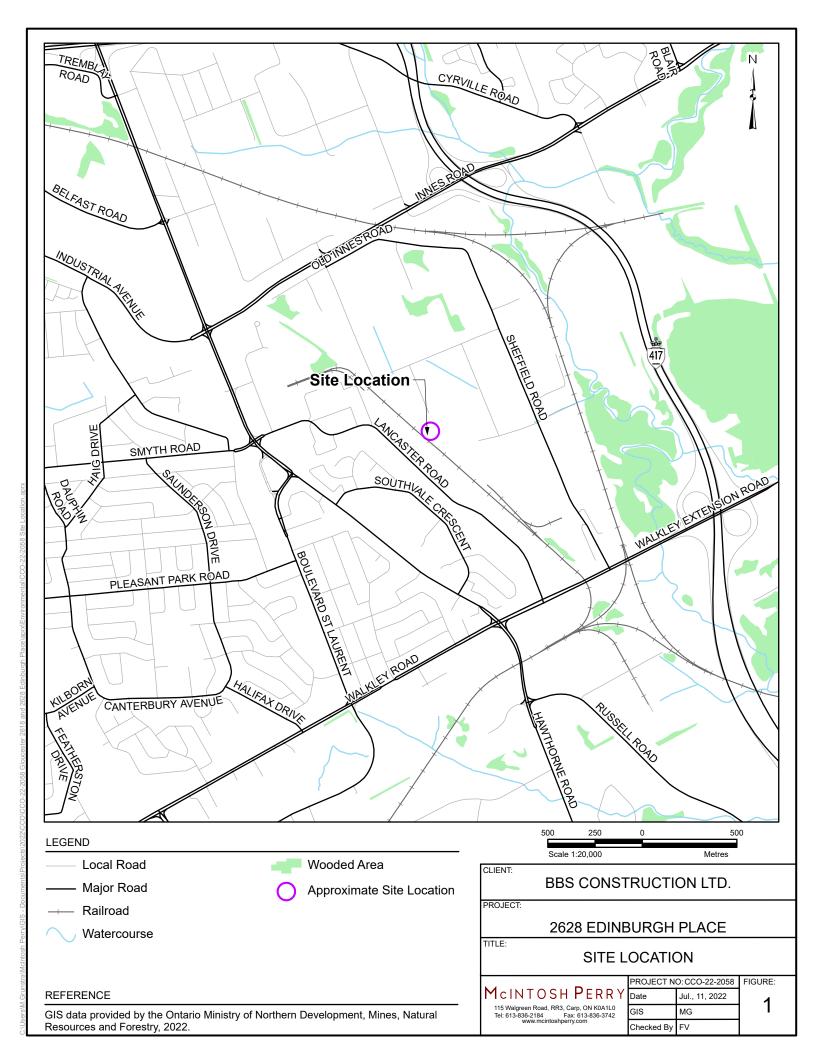
This report was produced for the exclusive use of <u>BBSConstruction LTD</u>. The purpose of the report is to assess the existing stormwater management system and provide recommendations and designs for the post-construction scenario that are in compliance with the guidelines and standards from the Ministry of the Environment, Parks and Climate Change, City of Ottawa, and local approval agencies. McIntosh Perry reviewed the site information and background documents listed in Section 2.0 of this report. While the previous data was reviewed by McIntosh Perry and site visits were performed, no field verification/measures of any information were conducted.

Any use of this review by a third party, or any reliance on decisions made based on it, without a reliance report is the responsibility of such third parties. McIntosh Perry accepts no responsibility for damages, if any, suffered by any third party as a result of decisions or actions made based on this review.

The findings, conclusions and/or recommendations of this report are only valid as of the date of this report. No assurance is made regarding any changes in conditions subsequent to this date. If additional information is discovered or becomes available at a future date, McIntosh Perry should be requested to re-evaluate the conclusions presented in this report, and provide amendments, if required.

APPENDIX A KEY PLAN

McINTOSH PERRY



APPENDIX B BACKGROUND DOCUMENTS

McINTOSH PERRY

2628 Edinburgh Place

Meeting Summary Notes Sept 15, 2021. Online Teams Meeting

Attendees:

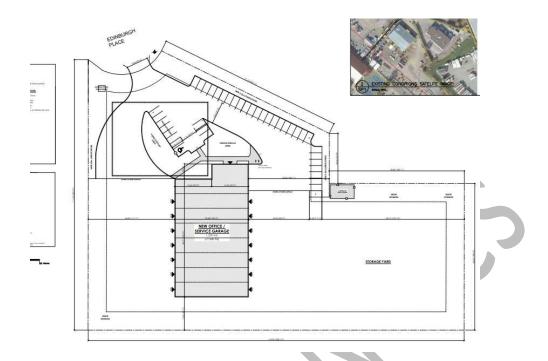
- Michel Pouliot, Co-Owner, Ottawa Equipment & Hydraulics Inc.
- Mark Kauhanen, Applicant, BBS Construction (Ontario) Ltd.
- Matthew co owner
- Scott Bosman, BBS Construction
- Bridgette Alchawa, McIntosh Perry
- Curtis Melanson, McIntosh Perry
- Tyler Cassidy, Kelsey Charie (Project Manager/EIT, City of Ottawa)
- Adrian vanWyk (Urban Designer, Architect, City of Ottawa)
- Katie Morphet (File Lead, Planner, City of Ottawa)
- Matthew Hayley (Environmental Planner)
- Jeannette Krabicka (Parks Planner)
- Penelope Horn (Planning Student)
- Tracey Scaramozzino (Planner, City of Ottawa)

Not in Attendance:

- Mark Richardson (City Forester)
- Wally Dubyk (Transportation Project Manager, City of Ottawa)
- Jamie Batchelor (RVCA)

Issue of Discussion:

- Site Plan Control for a new 1-storey 17,000 ft2 service garage/office bldg. and future demolition of existing 13,000 ft2 bldg
- New service connection for water, sani and storm to Edinburgh Place



1. Official Plan

a. Designated "Urban Employment Lands".

2. Zoning Information

- a. Split Zoning: Heavy Industrial (IH) and Light Industrial (IL)
- b. IL Section 203 (5):
 - 3. Except in the case of the storage of motor vehicles associated with an automobile dealership and automobile rental establishment, outdoor storage is prohibited. (By-law 2017-302)
- c. The uses (heavy equipment and vehicles sales, servicing, rental; office; parking lot) are permitted, except that as per section 203 (5), accessory outdoor storage of the heavy equipment is NOT permitted for this use in the IL zone

3. Infrastructure/Servicing (Tyler Cassidy)

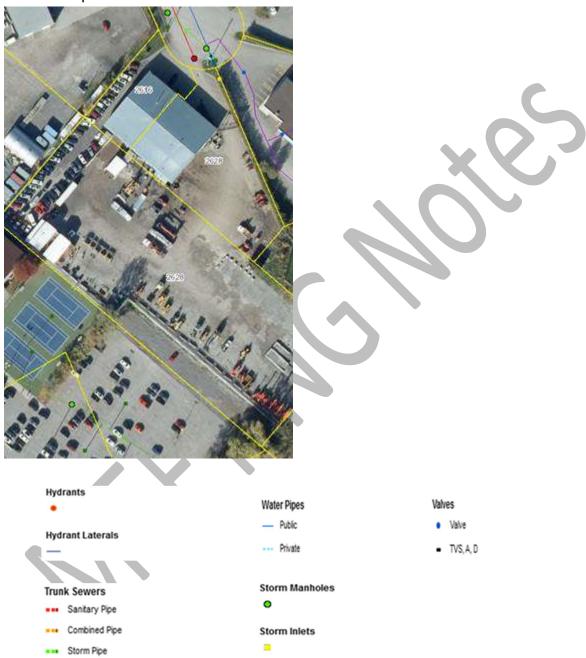
Please note the following information regarding the engineering design submissions for the above noted site:

a. The Servicing Study Guidelines for Development Applications are available at the following address:

https://ottawa.ca/en/city-hall/planning-and-development/how-developproperty/development-application-review-process-2/guide-preparing-studies-andplans

- b. Servicing and site works shall be in accordance with the following documents:
 - Ottawa Sewer Design Guidelines (October 2012) and all the Technical Bulletins including, Technical Bulletin PIEDTB-2016-01 and ISTB-2018-01
 - Ottawa Design Guidelines Water Distribution (2010) and Technical Bulletins
 ISD-2010-2, ISDTB-2014-02 and ISTB-2018-02
 - Geotechnical Investigation and Reporting Guidelines for Development Applications in the City of Ottawa (2007)
 - City of Ottawa Slope Stability Guidelines for Development Applications (revised 2012)
 - City of Ottawa Environmental Noise Control Guidelines (January, 2016)
 - City of Ottawa Park and Pathway Development Manual (2012)
 - City of Ottawa Accessibility Design Standards (2012)
 - Ottawa Standard Tender Documents (latest version)
 - Ontario Provincial Standards for Roads & Public Works (2013)
- c. Record drawings and utility plans are also available for purchase from the City (Contact the City's Information Centre by email at <u>InformationCentre@ottawa.ca</u> or by phone at (613) 580-2424 x 44455
- d. The Stormwater Management Criteria, for the subject site, is to be based on the following (as established in the Citigate Centre Site Servicing Report):
 - The pre-development runoff coefficient or a maximum equivalent 'C' of 0.5, whichever is less (§ 8.3.7.3).
 - Flows to the storm sewer in excess of the 5-year storm release rate, up to and including the 100-year storm event, must be detained on site (based on sewer age, 1989)
 - Ensure no overland flow for all storms up to and including the 100-year event.
 - The 2-yr storm or 5-yr storm event using the IDF information derived from the Meteorological Services of Canada rainfall data, taken from the MacDonald Cartier Airport, collected 1966 to 1997.
 - A calculated time of concentration (Cannot be less than 10 minutes).
 - Quality control requirements to be provided by Rideau Valley Conservation Authority (RVCA)

- This property is located within the Green's Creek subwatershed. Please verify any subwatershed specific SWM criteria with the RVCA.
- e. Deep Services:



- *i.* A plan view of the approximate services may be seen above. Services should ideally be grouped in a common trench to minimize the number of road cuts. The sizing of available future services is:
 - a. Connections (Edinburgh Place):

- i. Existing 450 mm dia. STM (Conc.)
- ii. Existing 305 mm dia. Watermain (DI)
- iii. Existing 250 mm dia. SAN (Conc.)
- *ii.* Provide existing servicing information and the recommended location for the proposed connections. Services should ideally be grouped in a common trench to minimize the number of road cuts.
- iii. Provide information on the monitoring manhole requirements should be located in an accessible location on private property near the property line (ie. Not in a parking area).
- iv. Provide information on the type of connection permitted

Sewer connections to be made above the springline of the sewermain as per:

- a. Std Dwg S11.1 for flexible main sewers connections made using approved tee or wye fittings.
- *b.* Std Dwg S11 (For rigid main sewers) *lateral must be less that 50% the diameter of the sewermain,*
- *c.* Std Dwg S11.2 (for rigid main sewers using bell end insert method) for larger diameter laterals where manufactured inserts are not available; lateral must be less that 50% the diameter of the sewermain,
- *d.* Connections to manholes permitted when the connection is to rigid main sewers where the lateral exceeds 50% the diameter of the sewermain. Connect obvert to obvert with the outlet pipe unless pipes are a similar size.
- e. No submerged outlet connections.
- f. Civil consultant must request boundary conditions from the City's assigned Project Manager prior to first submission. Water Boundary condition requests must include the location of the service and the expected loads required by the proposed development. Please provide the following information:
 - i. Location of service(s)
 - ii. Type of development and the amount of fire flow required (as per FUS, 1999).

- iii. Average daily demand: ____ l/s.
- iv. Maximum daily demand: ____l/s.
- v. Maximum hourly daily demand: ____ l/s.
- vi. Hydrant location and spacing to meet City's Water Design guidelines.
- vii. Water supply redundancy will be required for more than 50 m3/day water demand.
- g. Phase 1 ESAs and Phase 2 ESAs must conform to clause 4.8.4 of the Official Plan that requires that development applications conform to Ontario Regulation 153/04.
- h. If applicable, MECP ECA Requirements -

All development applications should be considered for an Environmental Compliance Approval (ECA) by the Ministry of the Environment, Conservation, and Parks (MECP);

- a. Consultant determines if an approval for sewage works under Section 53 of OWRA is required. Consultant then determines what type of application is required and the City's project manager confirms. (If the consultant is not clear if an ECA is required, they will work with the City to determine what is required. If the consultant it is still unclear or there is a difference of opinion only then will the City PM approach the MECP.
- b. The project will be either transfer of review (standard), transfer of review (additional), direct submission, or exempt as per O. Reg. 525/98.
 - . Standard Works ToR Draft ECA's are sent to the local MECP office (<u>moeccottawasewage@ontario.ca</u>) for information only
- d. Additional ToR draft ECAs require a project summary/design brief and require a response from the local MECP (10 business day window)
- e. Site plan Approval, or Draft Approval, is required before an application is sent to the MECP

4. Initial Planning Comments (Katie Morphet)

a. IL permits "Heavy Equipment and vehicle sales, rental and servicing"

We have been able to confirm with Zoning Interpretation that the proposed accessory outdoor storage is not permitted in the IL zone (as per section 203 (5)) and must be contained and kept to the side of the lot that is zoned Heavy Industrial. Alternatively a Zoning By-law Amendment could be sought to permit the use on the entire property.

- b. Please submit a survey plan to help clarify property boundary.
- c. Please update the zoning table on the Site Plan to show the correct zones and zoning information. Please include all relevant zoning information such as parking spaces, bicycle parking and loading.

5. Urban Design Comments (Adrian van Wyk)

- a. Please see the attached Design Brief Submission Requirements. A scoped Design Brief will be required, which may be combined with a Planning Rationale.
- b. Landscaping
 - It is recommended that hard surfaces be kept to a minimum, except where required for parking, storage, or vehicle circulation.
 - A soft landscaped buffer is recommended along the rear and side lot lines.
 - It is recommended that new softscape and shrubs/trees be introduced where possible.
- c. <u>Pedestrian and bicycle circulation</u>
 - It is recommended that pedestrian circulation be carefully considered, and options explored to provide a connection between the proposed building and Edinburgh Place.
- d. <u>Sustainability</u>
 - It is recommended that the applicant consider introducing sustainable design features, such as light coloured materials, swales, etc.

6. Parks (Jeanette Krabicka)

1. Parkland Dedication:

- a. The amount of parkland dedication that is required is to be calculated as per the City of Ottawa Parkland Dedication By-law No 2009-95. Parkland requirement for commercial uses is calculated as 2% of the gross land area of the site being developed.
- b. Section 14 (2) (b) of the By-law states that no conveyance of land or payment of money in-lieu is required for a change of use from commercial or industrial to another commercial or industrial use, or for the alteration of an existing

building resulting in a change of use from commercial or industrial to another commercial or industrial use.

- c. The 'front' property parcel (located to the north-east) which contains the existing building is currently developed with a commercial/industrial use. The proposed development is also for a commercial/industrial use. Therefore, no additional parkland dedication is required for the front property parcel.
- d. The 'rear' property parcel has not been developed to date and is therefore subject to parkland dedication for the proposed development.
- e. The approximate gross land area of the rear property parcel is 9,378 sq.m. The approximate parkland dedication requirement is calculated as:
 - 9,378 m2 x 2% = 188 sq.m.
- f. Please provide the City with a surveyor's area certificate/memo which specifies the exact gross land area of the rear property parcel of 2628 Edinburgh Place.
- g. If parkland dedication for the rear parcel has been satisfied previously, please provide Parks & Facilities Planning with the supporting documentation.
- h. Please note that the park comments are preliminary and will be finalized (and subject to change) upon receipt of the development application and the requested supporting documentation.

Additionally, if the proposed commercial product or land use changes, then the parkland dedication

requirement be re-evaluated accordingly.

- 2. Form of Parkland Dedication:
 - a. Parks & Facilities Planning will be requesting Cash-in-Lieu of Parkland for this Site Plan proposal.

7. Trees (Mark Richardson)

a. No comments as there are no trees on site.

8. Environment (Matthew Hayley)

a. Bird Safe Design

Given the proposal will need to review and incorporate bird safe design elements. Some of the risk factors include glass and related design traps such as corner glass and fly-through conditions, ventilation grates and open pipes, landscaping, light pollution. More guidance and solutions are available in the guidelines which can be found here: <u>https://ottawa.ca/en/planning-</u> development-and-construction/developing-property/development-applicationreview-process/development-application-submission/guide-preparing-studiesand-plans.

- b. Site Plan Applications: medium to large scale commercial / industrial / institutional:
 - Bird-safe glass or integrated protection measures may be required through conditions of site plan approval for projects involving large expanses of glazing. However, it is important that the Bird-Safe Design Guidelines do not have a significant impact on the affordability or timelines of the respective project. The City recognize that corporate standards or other design requirements may limit or preclude use of bird-safe glass or integrated protection measures in cases of small-scale commercial buildings (e.g. restaurant, retail pads).

9. Conservation Authority (RVCA)

a. Comments not received yet.

10. Transportation (Wally Dubyk)

- a. The development site proposes an additional 4,000 ft2 service garage with 40 parking spaces. This development would not generate sufficient traffic to warrant a TIA report.
- b. Edinburgh Place is classified as a Local road. There are no additional protected ROW limits identified in the OP.
- c. The proponent shall comply with the Private Approach By-Law 2003-447
- d. No private approach intended for two-way vehicular traffic shall exceed 9.0 metres in width at the roadway edge, and in no case shall the width exceed 50% of the frontage on which the approach or approaches are located.
- e. The closure of an existing private approach shall reinstate the sidewalk, shoulder, curb and boulevard to City standards.
- f. No private approach shall be constructed within 0.3 metres of any adjacent property measured at the highway line, and at the curb line or roadway edge.
- g. The Tactile Walking Surface Indicator (TWSI) should be provided at pedestrian crossings. Under the Integrated Accessibility Standards of the Accessibility for Ontarians with Disabilities Act, 2005, and the City of Ottawa Accessibility Design Standards, TWSI's are required for new construction and the redevelopment of elements in public spaces, such as for exterior paths of travel (e.g. sidewalks and at the top of stairs).

h. Bicycle parking spaces are required as per Section 111 of the Ottawa Comprehensive Zoning By-law. Bicycle parking spaces should be located in safe, secure places near main entrances and preferably protected from the weather.

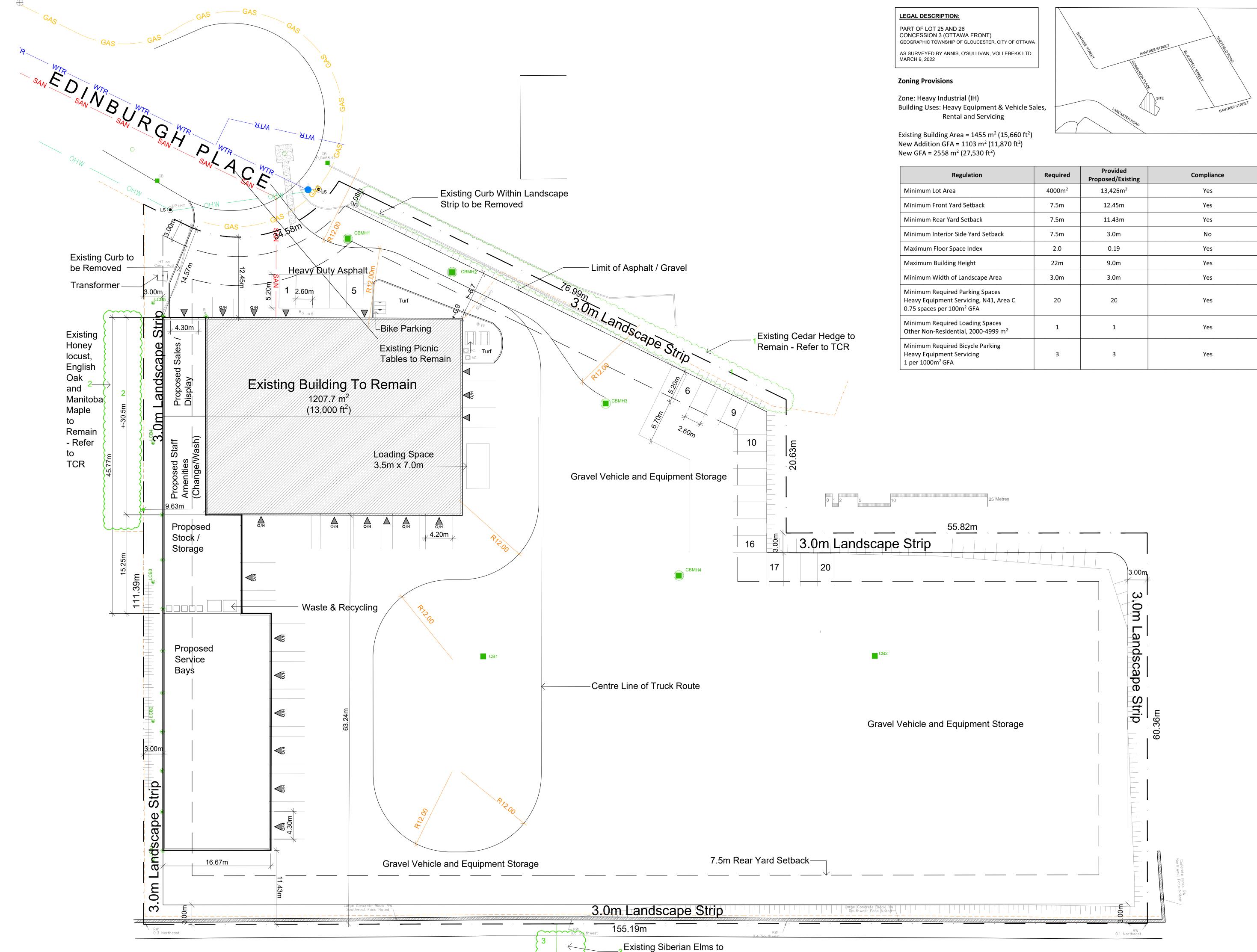
11.Waste Collection

This facility will not be on City Collection.

12. General Information

a. Ensure that all plans and studies are prepared as per City guidelines – as available online...

https://ottawa.ca/en/city-hall/planning-and-development/informationdevelopers/development-application-review-process/developmentapplication-submission/guide-preparing-studies-and-plans



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Remain - Refer to TCR

+	Povicion	Date
# 0	Revision REVIEW/COORDINATION	OCTOBER 2022
1	FIRST SUBMISSION SPC	DECEMBER 19 2022
2	SECOND SUBMISSION SPC	APRIL 28 2023
		AN LEGEND
	Existi	ng Building(s)
	Propos	ed Building(s)
	F	Property Lines
	;	Setback Lines
		Fence
	—— Proposed (Concrete Curb
		Slope at 3:1
	Un	less Specified
	∧ Existing	Exterior Door
	('O/H' indica	ates Overhead Door)
	· · ·	Exterior Door ates Overhead Door)
	·	Retaining Wall
		Fire Hydrant
		Standard Base
		er Downspout
	Ŭ	asin Man Hole
		Catch Basin e Catch Basin
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Required	Provided Proposed/Existing	Compliance
4000m ²	13,426m ²	Yes
7.5m	12.45m	Yes
7.5m	11.43m	Yes
7.5m	3.0m	Νο
2.0	0.19	Yes
22m	9.0m	Yes
3.0m	3.0m	Yes
20	20	Yes
1	1	Yes
3	3	Yes

APPENDIX C WATERMAIN CALCULATIONS

McINTOSH PERRY

000-22-2058 - 2628 Edinburgh Place - Water Demands

Project:	2628 Edinburgh Place		
Project No.:	000-22-2058		
Designed By:	FV		
Checked By:	AG		
Date:	November 23, 2022		
Ste Area:	1.34	grossha	
Commercial Area	13425.00	m2	28,000

L/gross ha/d

AVERAGE DAILY DEM AND

DEMAND TYPE	AMOUNT	UNITS]
Residential	280	L/c/d]
Industrial - Light	35,000	L/grossha/d	
Industrial - Heavy	55,000	L/grossha/d	
Shopping Centres	2,500	L/ (1000m² /d	
Hospital	900	L/(bed/day)	
Schools	70	L/(Student/d)	
Trailer Park with no Hook-Ups	340	L/(space/d)	
Trailer Park with Hook-Ups	800	L/(space/d)	
Campgrounds	225	L/ (campsite/d)	
Mobile Home Parks	1,000	L/ (Space/d)	
Motels	150	L/ (bed-space/d)	
Hotels	225	L/ (bed-space/d)	
Tourist Commercial	28,000	L/ gross ha/ d	
Other Commercial	28,000	L/ gross ha/ d	
	Residential	0.00	L/s
AVERAGE DAILY DEMAND	Commercial/Industrial		
	/Institutional	0.44	Ľs

MAXIMUM DAILY DEMAND

DEMAND TYPE	AMOUNT		UNITS	
Residential	9.5	x avg. day	L/c/d	
Industrial	1.5	x avg. day	L/grossha/d	
Commercial	1.5	x avg. day	L/grossha/d	
Institutional	1.5	x avg. day	L/grossha/d	
	Residential	0.00	L∕s	
MAXIMUM DAILY DEMAND	Commercial/Industrial			
	/Institutional	0.65	L∕ s	

MAXIMUM HOUR DEMAND

DEMAND TYPE	AMOUNT		UNITS	
Residential	14.3	x avg. day	L/c/d	
Industrial	1.8	x max. day	L/grossha/d	
Commercial	1.8	x max. day	L/grossha/d	
Institutional	1.8	x max. day	L/grossha/d	
	Residential	0.00	L∕s	
MAXIMUM HOUR DEMAND	Commercial/Industrial			
	/Institutional	1.17	L∕s	

WATER DEMAND DESIGN FLOWS PER UNIT COUNT

CITY OF OTTAWA - WATER DISTRIBUTION GUIDELINES, JULY 2010

AVERAGE DAILY DEMAND	0.44	L/ s
MAXIMUM DAILY DEMAND	0.65	L/s
MAXIMUM HOUR DEMAND	1.17	L/s

000-22-2058 - 2628 Edinburgh Place - OBC Fire Calculations

Project:	2628 Edinburgh Place
Project No.:	000-22-2058
Designed By:	FV
Checked By:	AG
Date:	November 23, 2022

Ontario 2006 Building Code Compendium (Div. B - Part 3)

Water Supply for Fire-Fighting - Store/ Office & Warehouse Building

 Building is classified as Group :
 D, E, and F2 up to 2 Storeys
 (from table 3.2.2.55)

 Building is of noncombustible construction with fire separations and fire-resistance ratings provided in accordance with subsections
 3.2.2., including loadbearing walls, columns and arches

From Div. B A-3.2.5.7. of the Ontario Building Code - 3. Building On-Ste Water Supply:

(a) $Q = K \times V \times Stot$

where:

Q = minimum supply of water in litres

K = water supply coefficient from Table 1

V = total building volume in cubic metres

Stot = total of spatial coefficient values from the property line exposures on all sides as obtained from the formula:

Stot = 1.0 + [Side1+Side2+Side3+..etc.]

К	17	(from Table 1 pg A-31) (Worst case occupancy {E/ F2} 'K' value used)			F	rom Figure
V	16,012	(Total building volume in m ³ .)				1 (A-32)
Stot	1.5	(From figure 1 pg A-32)	Shorth	12.49	m	0.0
Q =	408,298.3	6 L	Seast	24.24	m	0.0
			Scouth	11.44	m	0.0
From Table 2: Required Minimum	Water Supply Row	Rate (L/s)	Swest	3	m	0.5
			* ap	pproximate	distar	nces

 9000
 L/min
 if Q > 270,000 L

 2378
 gpm

000-22-2058 - 2628 Edinburgh Place - Fire Underwriters Survey

Project:	2628 Edinburgh Place
Project No .:	000-22-2058
Designed By:	FV
Checked By:	AG
Date:	November 23, 2022

From the Fire Underwriters Survey (2020)

From Part II – Guide for Determination of Required Fire Flow Copyright I.SO.: City of Ottawa Technical Bulletin ISTB-2018-02 Applied Where Applicable

	QUIREMENT (Rounded to $20 \times C \times \sqrt{A}$ Where:		nin) flow in liters per minute				
F = 24	20 X C X VA Where:		elated to the type of construction				
				Ig all storey's, but excluding basemen	ts at least	50 percent belo	w grade) in
		the building beir					gradd) m
	Construction T	ype Non-Combustibl	e Construction				
			0.8				
		С		A	2,211.0) m ²	
			Total Roor Area (per the 202	0 FUS Page 20 - Total Effective Area)	2,211.0	0 m ²	* Unprotected Vertical Openi
Calcu	lated Fire Flow				8.275.7	7 L/ min	
Galloc) L/min	
		E (No Dounding)					
	ON FOR OCCUPANCY TYP						
FIOII	Page 24 of the Fire Under Combust			0%			
	Combusi	lible		078			
Fire F	Vol				8,000.0) L/min	
C. REDUCTI	ON FOR SPRINKLER TYPE	(No Rounding)					
	N. 0 111			201			
	Non-Sprinkle	ered		0%			
Bedu	ction				0.0) I/min	
Redu					0.0) L/ min	
	ction E FOR EXPOSURE (No Rou	unding)			0.0) L∕ min	
D. INCREAS	E FOR EXPOSURE (No Rou	unding)		Length Exposed	0.0 Height		ł
D. INCREAS		unding)	Cons.of Exposed Wall	Length Exposed Adjacent Wall (m)		Length-Height	
D. INCREAS	E FOR EXPOSURE (No Rou Separation Distance (m) Over 30 m	unding)	Wood frame	Adjacent Wall (m) N/A	Height (Stories) N/A	Length-Height Factor N/ A	0%
D. INCREAS posure 1 posure 2	E FOR EXPOSURE (No Rou Separation Distance (m) Over 30 m 20.1 to 30	unding)	Wood frame Wood frame	Adjacent Wall (m) N/A 43.6	Height (Stories) N/A 2	Length-Height Factor N/A 87.2	0% 8%
D. INCREAS posure 1 posure 2 posure 3	EFOR EXPOSURE (No Rou Separation Distance (m) Over 30 m 20.1 to 30 Over 30 m	unding)	Wood frame Wood frame Wood frame	Adjacent Wall (m) N/ A 43.6 N/ A	Height (Stories) N/A 2 N/A	Length-Height Factor N/ A 87.2 N/ A	0% 8% 0%
D. INCREAS posure 1 posure 2	E FOR EXPOSURE (No Rou Separation Distance (m) Over 30 m 20.1 to 30	unding)	Wood frame Wood frame	Adjacent Wall (m) N/A 43.6	Height (Stories) N/A 2	Length-Height Factor N/A 87.2	0% 8% 0% 0%

E Total Fire How (Rounded to the Nearest 1000 L/min)

Fire How8,640.0 L/ minFire How Required**9,000.0 L/ min

 * In accordance with Part II, Section 4, the Increase for separation distance is not to exceed 75%

 ** In accordance with Section 4 the Fire flow is not to exceed 45,000 L/min or be less than 2,000 L/min

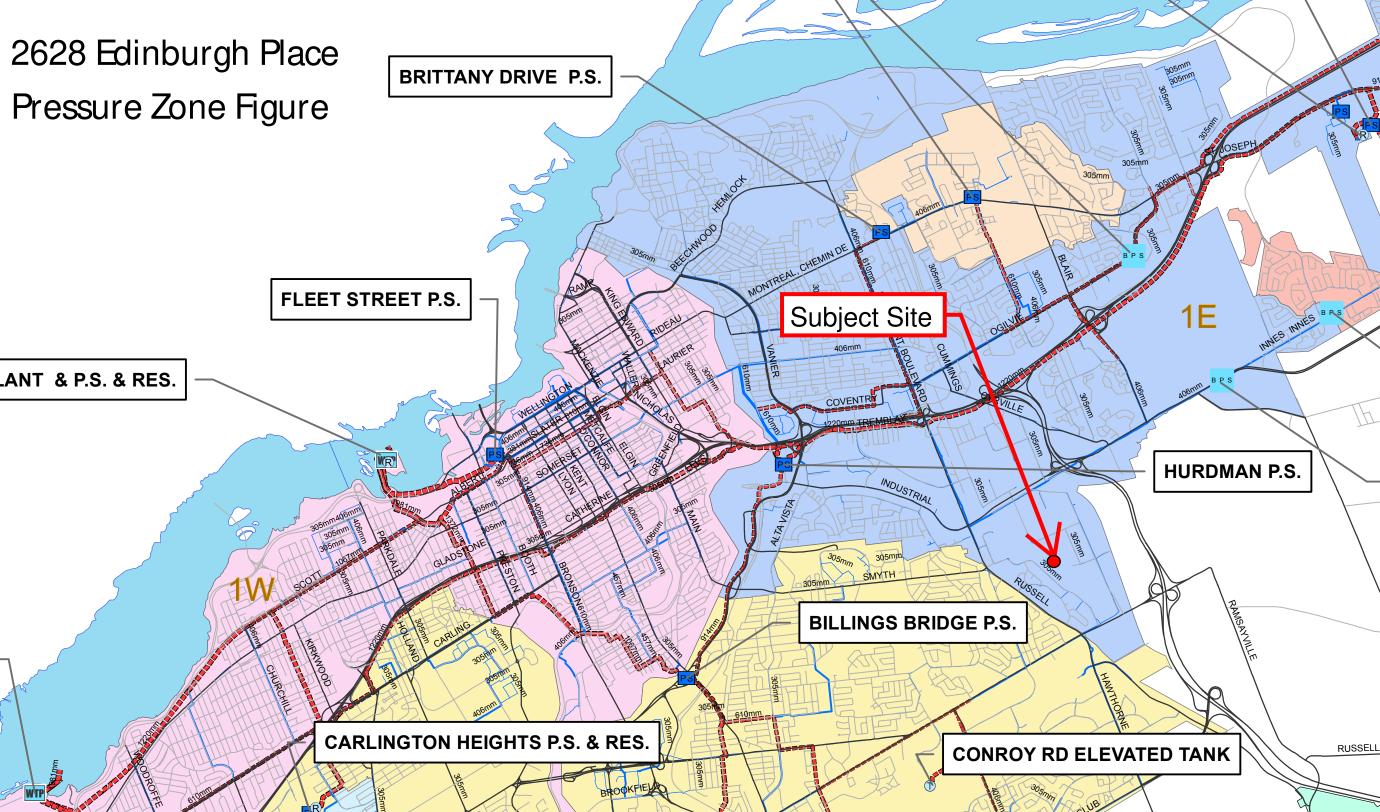
000-22-2058 - 2628 Edinburgh Place - Boundary Condition Unit Conversion

Project:	2628 Edinburgh Place
Project No .:	000-22-2058
Designed By:	FV
Checked By:	AG
Date:	November 23, 2022

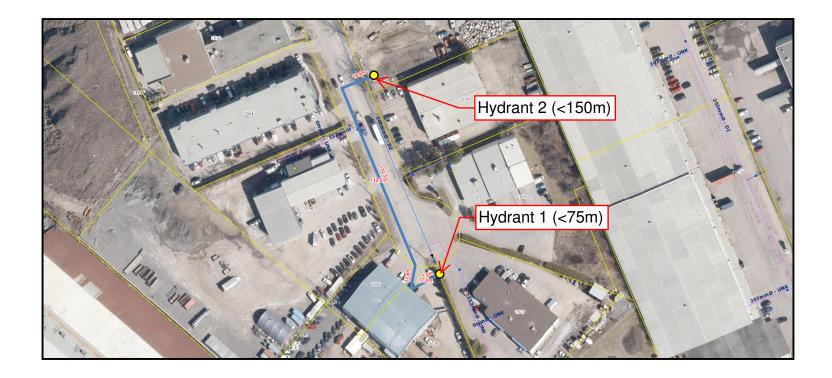
Boundary Conditions Unit Conversion

Edinburgh Place

Scenario	Height (m)	Elevation (m)	m H₂O	PSI	kPa
Avg. DD	117.9	66.2	51.8	73.6	507.7
Max Day + Fire Flow (150.0 L/s)	98.4	66.2	32.3	45.9	316.4
Peak Hour	109.9	66.2	43.8	62.2	429.2



2628 Edinburgh Place Hydrant Coverage Figure



Francis Valenti

From:	Charie, Kelsey <kelsey.charie@ottawa.ca></kelsey.charie@ottawa.ca>
Sent:	August 11, 2022 11:58 AM
То:	Cassidy, Tyler; Francis Valenti
Cc:	Alison Gosling
Subject:	RE: 22-2058 - Boundary Condition Request - 2628 Edinburgh Place
Attachments:	2628 Edinburgh Place August 2022.pdf

Hi Francis,

Here is the water boundary conditions from our water resources department:

The following are boundary conditions, HGL, for hydraulic analysis at 2628 Edinburgh Place (zone 1E) assumed to be connected to the 305 mm watermain on Edinburgh Place (see attached PDF for location).

Minimum HGL: 109.9 m

Maximum HGL: 117.9 m

Max Day + FF (150.0 L/s): 98.4 m

These are for current conditions and are based on computer model simulation.

Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation.

Please let me know if there is anything you wish to discuss further,

Kelsey Charie, EIT Engineering Intern Planning, Real Estate and Economic Development Department - Direction générale de la planification, des biens immobiliers et du développement économique Development Review - South Branch City of Ottawa | Ville d'Ottawa 110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1 613.580.2424 ext./poste 22551, <u>kelsey.charie@ottawa.ca</u>

From: Cassidy, Tyler <tyler.cassidy@ottawa.ca>
Sent: August 02, 2022 2:28 PM
To: Francis Valenti <F.Valenti@McIntoshPerry.com>; Charie, Kelsey <kelsey.charie@ottawa.ca>
Cc: Alison Gosling <a.gosling@mcintoshperry.com>
Subject: RE: 22-2058 - Boundary Condition Request - 2628 Edinburgh Place

Hi Francis,

I've sent the request to our Water Resources group. Please allow for up to 10 business days for them to provide boundary conditions.

Please reach out to Kelsey Charie if you do not receive them before then.

Thank you,

Please note that I am anticipated to be Out of Office for 5 weeks starting August 8th, 2022. For any inquiries please contact Kelsey Charie at Kelsey.Charie@Ottawa.ca .

Tyler Cassidy, P.Eng Infrastructure Project Manager, Planning, Real Estate and Economic Development Department / Direction générale de la planification, des biens immobiliers et du développement économique - South Branch City of Ottawa | Ville d'Ottawa 110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1 613.580.2424 ext./poste 12977, <u>Tyler.Cassidy@ottawa.ca</u>

From: Francis Valenti <<u>F.Valenti@McIntoshPerry.com</u>>
Sent: August 02, 2022 11:32 AM
To: Cassidy, Tyler <<u>tyler.cassidy@ottawa.ca</u>>; Charie, Kelsey <<u>kelsey.charie@ottawa.ca</u>>
Cc: Alison Gosling <<u>a.gosling@mcintoshperry.com</u>>
Subject: RE: 22-2058 - Boundary Condition Request - 2628 Edinburgh Place

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Hi Tyler,

The water demand calculations have been revised to consider the entire lot area as commercial. The revised demands are listed below:

- The estimated fire flow is 9,000 L/min based on the OBC method
- The estimated fire flow is 9,000 L/min based on the FUS method
- Average Daily Demand (combined): 0.44 L/s
- Maximum Daily Demand (combined): 0.65 L/s
- Maximum hourly daily demand (combined): 1.17 L/s

Please find attached calculations prepared for the demands listed above.

Regards,

From: Cassidy, Tyler <<u>tyler.cassidy@ottawa.ca</u>>
Sent: August 2, 2022 9:09 AM
To: Francis Valenti <<u>F.Valenti@McIntoshPerry.com</u>>; Charie, Kelsey <<u>kelsey.charie@ottawa.ca</u>>
Cc: Alison Gosling <<u>a.gosling@mcintoshperry.com</u>>
Subject: RE: 22-2058 - Boundary Condition Request - 2628 Edinburgh Place

Hi Francis,

I'm reviewing the water demand calculations from your email below and they look a little low. Can you please double check the calculations and confirm what your Average Daily Demand, Max Daily Demand, and Max Hourly Daily Demand rates are? Note that Average Daily Demand is calculated with the site's gross area (1.34 gross ha x 28,000 L/gross ha/day) and reduced down to L/s.

Thank you,

Please note that I am anticipated to be Out of Office for 5 weeks starting August 8th, 2022. For any inquiries please contact Kelsey Charie at <u>Kelsey.Charie@Ottawa.ca</u>.

Tyler Cassidy, P.Eng

Infrastructure Project Manager, Planning, Real Estate and Economic Development Department / Direction générale de la planification, des biens immobiliers et du développement économique - South Branch City of Ottawa | Ville d'Ottawa 110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1 613.580.2424 ext./poste 12977, <u>Tyler.Cassidy@ottawa.ca</u>

From: Francis Valenti <<u>F.Valenti@McIntoshPerry.com</u>>
Sent: July 28, 2022 4:24 PM
To: Cassidy, Tyler <<u>tyler.cassidy@ottawa.ca</u>>; Charie, Kelsey <<u>kelsey.charie@ottawa.ca</u>>
Cc: Alison Gosling <<u>a.gosling@mcintoshperry.com</u>>
Subject: 22-2058 - Boundary Condition Request - 2628 Edinburgh Place

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Good afternoon,

We would like to request boundary conditions for the proposed development at 2628 Edinburgh Place. The proposed development includes a 1-storey rear addition with gravel vehicle & equipment storage areas. The proposed connection (single) will be to the existing 305 mm dia. watermain located within Edinburgh Place.

- The estimated fire flow is 9,000 L/min based on the OBC method
- The estimated fire flow is 9,000 L/min based on the FUS method
- Average Daily Demand (combined): 0.07 L/s
- Maximum Daily Demand (combined): 0.11 L/s
- Maximum hourly daily demand (combined): 0.19 L/s

Please find attached a map showing the proposed connection location and calculations prepared for the demands listed above.

Regards,

Francis Valenti, EIT

Engineering Intern, Land Development

T. 613.714.6895 | C. 613.808.2123 F.Valenti@McIntoshPerry.com | www.mcintoshperry.com

MCINTOSH PERRY

Turning Possibilities Into Reality

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Platinum member

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APPENDIX D SANITARY CALCULATIONS

000-22-2058 - 2628 Edinburgh Pl - Existing Sanitary Demands

Project:	2628 Edinburgh Pl		
Project No.:	000-22-2058		
Designed By:	FV		
Checked By:	AG		
Date:	Jun-22		
Ste Area	1.34 Gross ha		
Commercial Area	1207.70 m ²		

DESIGN PARAMETERS

Institutional/Commercial Peaking Facto	1.5	
Mannings coefficient (n)	0.013	
Demand (per capita)	280	L/day
Infiltration allowance	0.33	L/s/Ha

EXTRANEOUS FLOW ALLOWANCES

Infiltration / Inflow	How (L∕s)	
Dry	0.07	
Wet	0.38	
Total	0.44	

AVERAGE DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS	POPULATION / AREA	Flow (L/s)
Residential	280	L/c/d	0	0.00
Industrial - Light**	35,000	L/gross ha/d		0
Industrial - Heavy* *	55,000	L/gross ha/d		0
Commercial / Amenity	2,800	L/(1000m ² /d)	1207.70	0.04
Hospital	900	L/ (bed/day)		0
Schools	70	L/(Student/d)		0
Trailer Parks no Hook-Ups	340	L/ (space/d)		0
Trailer Park with Hook-Ups	800	L/ (space/d)		0
Campgrounds	225	L/(campsite/d)		0
Mobile Home Parks	1,000	L/ (Space/d)		0
Motels	150	L/ (bed-space/d)		0
Hotels	225	L/ (bed-space/d)		0
Office	75	L/7.0m ² /d		0
Tourist Commercial	28,000	L/gross ha/d		0
Other Commercial	28,000	L/gross ha/d		0

AVERAGE RESIDENTIAL FLOW PEAK RESIDENTIAL FLOW		Ľs Ľs
AVERAGE ICI FLOW	0.04	L/s
PEAK INSTITUTIONAL/ COMMERCIAL FLOW	0.06	L/s
PEAK INDUSTRIAL FLOW	0.00	L/s
TOTAL PEAK ICI FLOW	0.06	L∕s

TOTAL SANITARY DEMAND

TOTAL ESTIMATED AVERAGE DRY WEATHER FLOW	0.11	L∕s
TOTAL ESTIMATED PEAK DRY WEATHER FLOW	0.13	L∕s
TOTAL ESTIMATED PEAK WET WEATHER FLOW	0.50	L/s

000-22-2058 - 2628 Edinburgh PI - Proposed Sanitary Demands

Project:	2628 Edinburgh Pl		
Project No.:	000-22-2058		
Designed By:	FV		
Checked By:	AG		
Date:	Jun-22		
Ste Area	1.34 Gross ha		
Commercial Area	2210.76 m ²		

DESIGN PARAMETERS

Institutional/Commercial Peaking Factor	1.5	
Mannings coefficient (n)	0.013	
Demand (per capita)	280	L/day
Infiltration allowance	0.33	L/s/Ha

EXTRANEOUS FLOW ALLOWANCES

Infiltration / Inflow	How (L∕s)
Dry	0.07
Wet	0.38
Total	0.44

AVERAGE DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS	POPULATION / AREA	How (L/s)
Residential	280	L/c/d	0	0.00
Industrial - Light**	35,000	L/gross ha/d		0
Industrial - Heavy* *	55,000	L/gross ha/d		0
Commercial / Amenity	2,800	L/ (1000m² /d)	2210.76	0.07
Hospital	900	L/ (bed/day)		0
Schools	70	L/ (Student/d)		0
Trailer Parks no Hook-Ups	340	L/(space/d)		0
Trailer Park with Hook-Ups	800	L/(space/d)		0
Campgrounds	225	L/ (campsite/d)		0
Mobile Home Parks	1,000	L/ (Space/d)		0
Motels	150	L/ (bed-space/d)		0
Hotels	225	L/ (bed-space/d)		0
Office	75	L/7.0m ² /d		0
Tourist Commercial	28,000	L/gross ha/d		0
Other Commercial	28,000	L/gross ha/d		0

AVERAGE RESIDENTIAL FLOW PEAK RESIDENTIAL FLOW	0.00 0.00	∐/s ∐/s
	0.00	L 5
AVERAGE ICI FLOW	0.07	L∕s
PEAK INSTITUTIONAL/ COMMERCIAL FLOW	0.11	L∕s
PEAK INDUSTRIAL FLOW	0.00	L∕s
TOTAL PEAK ICI FLOW	0.11	L∕s

TOTAL SANITARY DEMAND

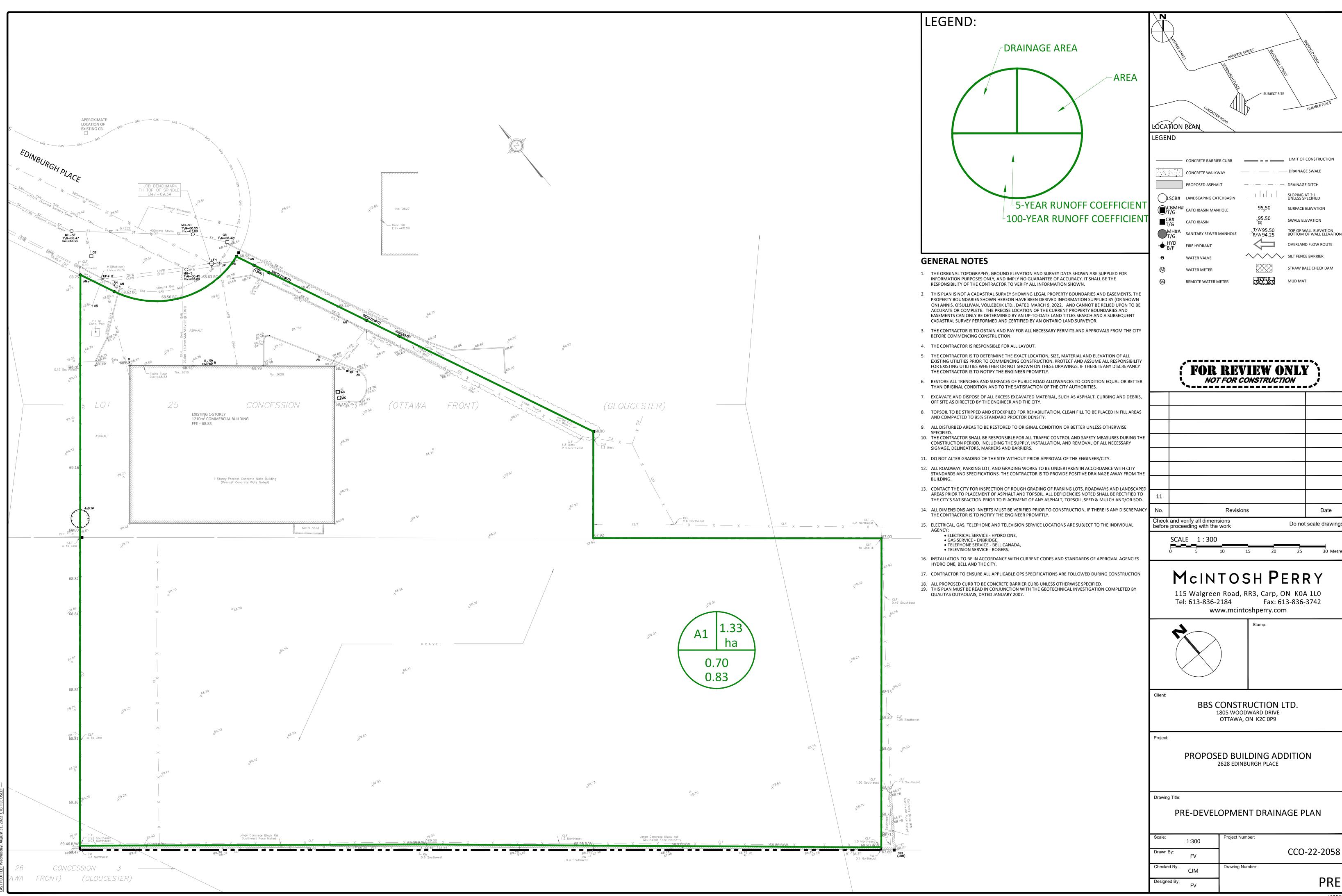
TOTAL ESTIMATED AVERAGE DRY WEATHER FLOW	0.14	L∕s
TOTAL ESTIMATED PEAK DRY WEATHER FLOW	0.17	L∕s
TOTAL ESTIMATED PEAK WET WEATHER FLOW	0.55	L∕s

SANITARY SEWER DESIGN SHEET

PROJECT:	CCO-22-2058
LOCATION:	2628 Edinburgh Place
CLIENT:	BBS Construction LTD

	LOC	ATION							RESIDENTIA	L							ICI AREAS				INFILTR	ATION ALLO	WANCE	FLOW				SEWER DAT	A	
1	2	3	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30 31
						UNIT	TYPES		AREA	POPU	LATION		PEAK			ARE	A (ha)		•	PEAK	AREA	A (ha)	FLOW	DESIGN	CAPACITY	LENGTH	DIA	SLOPE	VELOCITY	AVAILABLE
STREET	AREA	ID FRC	ом	то	SF	SD	тн	АРТ	(ha)	INID	сим	PEAK	FLOW	INSTITU	JTIONAL	COMM	IERCIAL	INDU	STRIAL	FLOW	IND	сим	(1.4.)	FLOW	(L/s)	()	(mm)	(0/)	(full)	CAPACITY
		м	н	MH	55	50	1	APT	(na)	IND	COIM	FACTOR	(L/s)	IND	CUM	IND	CUM	IND	CUM	(L/s)	IND	COM	(L/s)	(L/s)	(L/S)	(m)	(mm)	(%)	(m/s)	L/s (%)
Edinburgh Place		Ex. E	Bldg	Ex. Main												0.22	0.22			0.11	1.34	1.34	0.44	0.55	15.89	29.60	150	1.00	0.871	15.34 96.54
														51/								<u> </u>								
Design Parameters:					Notes:	<i>.</i>						Designed:		FV			No.					Revision							Date	
						gs coefficien			0.013								1.													
Residential		ICI Area			4	(per capita	-) L/day																					
SF 3.4 p/p/u				Peak Factor	4	on allowanc		0.33	B L/s/Ha			Checked:		AG																
TH/SD 2.7 p/p/u	INST	28,000 L/Ha/da				tial Peaking																								
APT 2.3 p/p/u	COM	28,000 L/Ha/da	ау	1.5		Harmon Fo	rmula = 1+(14/(4+P^0.5	5)*0.8)																					
Other 60 p/p/Ha	IND	35,000 L/Ha/da	ау	MOE Chart		where P = p	population i	n thousands	i			Project No.	:	CCO-22-20	58					_										
																													Sheet No:	
																													1 of 1	

APPENDIX E PRE-DEVELOPMENT DRAINAGE PLAN



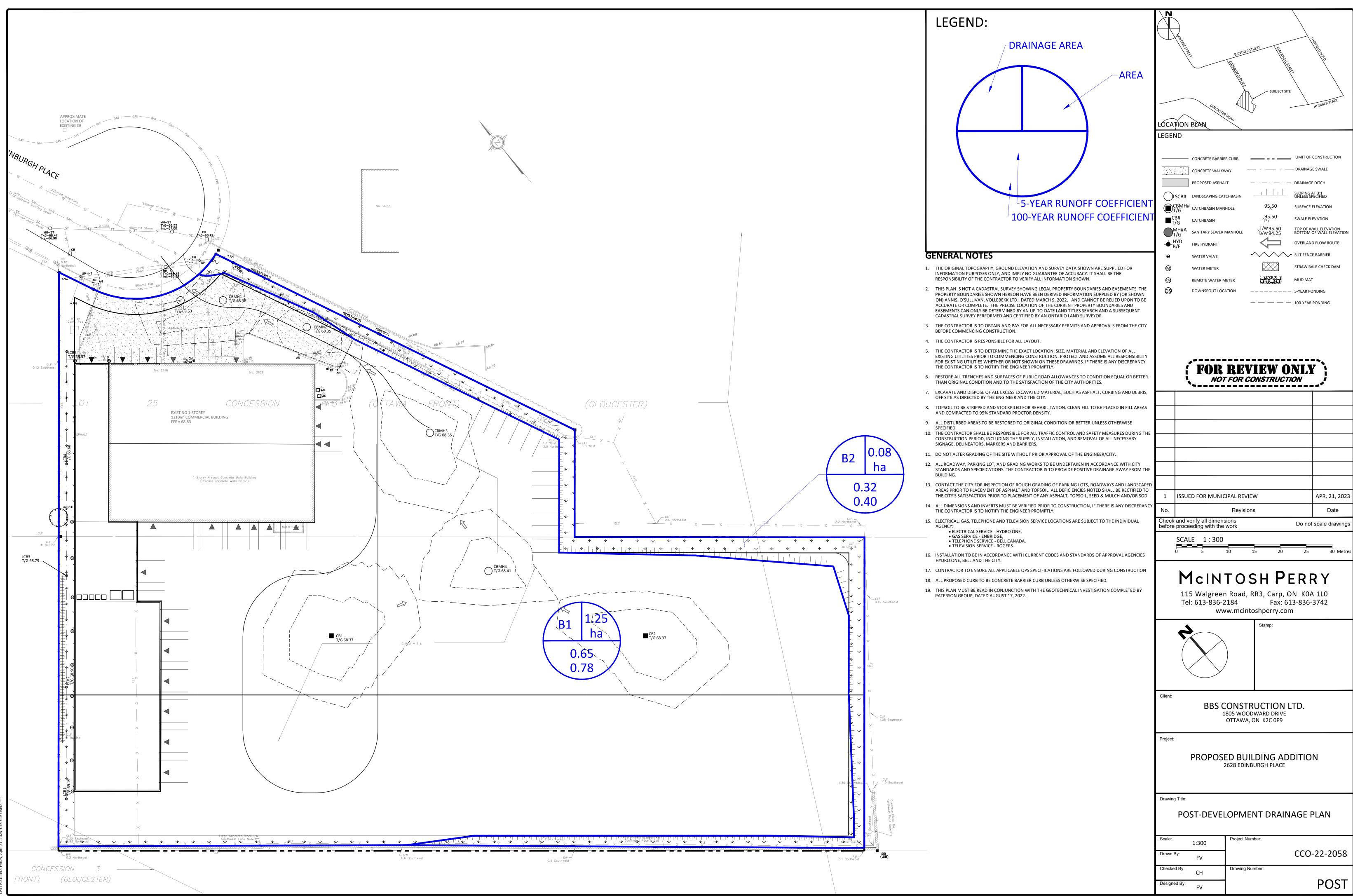
Fax: 613-836-3742

CCO-22-2058 PRE

#XXXXX

30 Metr

APPENDIX F POST-DEVELOPMENT DRAINAGE PLAN



#XXXXX

APPENDIX G STORIVWATER MANAGEMENT CALCULATIONS

CO-22-2058 - 2628 Edinburgh Place

Tc (min)		nsity n/hr)				
(11111)	5-Year	100-Year			C-Va	alues
20	70.3	120.0]	Impervious	0.90
13	90.6	155.1]	Gravel	0.60
10	104.2	178.6		-	Pervious	0.20

Pre-Development Runoff Coefficient

Drainage	Impervious	Gravel	Pervious Area	Average C	Average C
Area	Area (m ²)	(m²)	(m ²)	(5-year)	(100-year)
A1	4,722	8,344	223	0.70	0.83

Pre-Development Runoff Calculations

Drainage	Area	C	С	Tc	Q (L/ s)
Area	(ha)	5-Year	100-Year	(min)	5-Year	100-Year
A1	1.33	0.70	0.83	10	269.41	547.83
Total	1.33				269.41	547.83

Post-Development Runoff Coefficient

Drainage Area	Impervious Area (m ²)	Gravel (m²)	Pervious Area (m²)	Average C (5-year)	Average C (100-year)	
B1	2,589	9,468	467	0.65	0.78	Restricted
B2	0	236	529	0.32	0.40	Unrestricted

Post-Development Runoff Calculations

Drainage	Area	С	С	Тс	Q (L/ s)	
Area	(ha)	5-Year	100-Year	(min)	5-Year	100-Year	
B1	1.25	0.65	0.78	10	234.75	486.81	Restricted
B2	0.08	0.32	0.40	10	7.17	15.36	Unrestricted
Total	1.33				241.92	502.17]

Required Restricted How

Drainage	Area	С	Тс	Q (L/ s)
Area	(ha)	5-Year	(min)	5-Year
A1	1.33	0.50	10	192.47

Post-Development Restricted Runoff Calculations

Drainage Area	(L/ S)		Restricted How (ƯS)		Storage Re	quired (m ³)	Storage Provided (m ³)		
Area	5-year	100-Year	5-Year	100-Year	5-Year	100-Year	5-Year	100-Year	
B1	234.75	486.81	167.65	173.85	40.3	187.8	42.7	188.0	
B2	7.17	15.36	7.17	15.36					
Total	241.92	502.17	174.82	189.21	40.3	187.8	42.7	188.0	

1 of 3

CO-22-2058 - 2628 Edinburgh Place

Storage Req 5-Year Storm	uirements for	Area B1			
Tc (min)	l (mm/ hr)	Runoff (L∕ s) B1	Allowable Outflow (L/s)	Runoff to be Stored (L/s)	Storage Required (m ³)
10	104.2	234.77	167.65	67.12	40.27
20	70.3	158.39	167.65	-9.26	-11.11
	Maximum S	atorage Requi	red 5-year =	40	m ³
100-Year Sto	orm Event				
Tc (min)	l (mm/ hr)	Runoff (L/ s) B1	Allowable Outflow (L/s)	Runoff to be Stored (L/ s)	Storage Required (m ³)
10	178.6	486.92	173.85	313.07	187.84
20	120.0	327.16	173.85	153.31	183.97
	Maximum Sto n Event Storag	je Summary		188	m ³
La catta a	TIO		er ⊟ev. (m) =		.53
Location CBMH1	T/ G 68.38	INV. (out) 67.07	Depth (m) 0.15	Head (m) 1.33	Volume (m 42.7
				Storage Av	ailable (m³) = 42.7 quired (m³) = 40.3
Tuu-rear ac	orm Event Stor		y er ⊟ev. (m) =	68	.63
Location	T/ G	INV. (out)	Depth (m)	Head (m)	Volume (m
CBMH1	68.38	67.07	0.25	1.43	188.0
					ailable (m³) = 188 guired (m³) = 187

* Available Storage calculated from AutoCAD

2 of 3

CO-22-2058 - 2628 Edinburgh Place

For Orifice Flow, C= For Weir Flow, C=	0.60 1.84					3 of
		Orifice 1	Orifice 2	Weir 1	Weir 2	
inv	vert elevation	67.07				
center of cr	est elevation	67.20				
orifice width	/ weir length	264 mm				
	weir height					
orit	fice area (m²)	0.055				

Bevation Discharge Table - Storm Routing

Bevation	Orit	ice 1	Ori	fice 2	W	eir 1	W	eir 2	Total	
	H[m]	Q [m ³ /s]	Q [L/ s]							
68.35	1.15	0.16							155.87	7
68.36	1.16	0.16							156.55	
68.37	1.17	0.16							157.22	7
68.38	1.18	0.16							157.90	7
68.39	1.19	0.16							158.57	
68.40	1.20	0.16							159.23	1
68.41	1.21	0.16							159.89	
68.42	1.22	0.16							160.55	
68.43	1.23	0.16							161.21	1
68.44	1.24	0.16							161.87	7
68.45	1.25	0.16							162.52	1
68.46	1.26	0.16							163.17	1
68.47	1.27	0.16							163.82	7
68.48	1.28	0.16							164.46	1
68.49	1.29	0.17							165.10	7
68.50	1.30	0.17							165.74	7
68.51	1.31	0.17							166.38	7
68.52	1.32	0.17							167.02	7
68.53	1.33	0.17							167.65	5-Year
68.54	1.34	0.17							168.28	
68.55	1.35	0.17							168.91	7
68.56	1.36	0.17							169.53	7
68.57	1.37	0.17							170.15	7
68.58	1.38	0.17							170.77	7
68.59	1.39	0.17							171.39	7
68.60	1.40	0.17							172.01	7
68.61	1.41	0.17							172.62	7
68.62	1.42	0.17							173.24	7
68.63	1.43	0.17				1			173.85	100-Year

Notes: 1. For Orifice How, User is to Input an Elevation Higher than Crown of Orifice.

2. Orifice Equation: $Q = cA(2gh)^{1/2}$

3. Weir Equation: $Q = QLH^{3/2}$

4. These Computations Do Not Account for Submergence Effects Within the Pond Riser.

5. H for orifice equations is depth of water above the centroide of the orifice.

6. H for weir equations is depth of water above the weir crest.

CO-22-2058 - 2628 Edinburgh Place

Storage Requirements for Area B1

2-Year Storm Event

Tc (min)	l (mm/ hr)	Runoff (L/ s) B1	Allowable Outflow* (L/s)	Runoff to be Stored (L/s)	Storage Required (m ³)
10	76.8	173.04	155.87	17.17	10.30
12	69.9	157.47	155.87	1.60	1.15
	M	aximum Storage Re	10.30	m ³	

* Outflow based on flow rate of proposed 264mm Orifice at lowest T/ G Elevation (68.35)

Storage within Pipes:

Pipe (Start - End)	Inner Diameter (m)	Cross-Sectional Area (m2)	Pipe Length (m)	Volume (m3)
CB1-CBM H4	0.375	0.11	32.71	3.61
CB2-CBM H4	0.375	0.11	32.74	3.62
CBM H4-CBM H3	0.450	0.16	28.90	4.60
CBM H3-CBM H2	0.525	0.22	31.25	6.76
CBM H2-CBM H1	0.525	0.22	16.93	3.66
Total	-	-	-	22.25

Storage Required within Storm System (m3):	10.30
Storage Available within Storm System (m3):	22.25

Based on the calculations above, the proposed storm system has sufficient capacity to contain excess flow during the 2-year event.

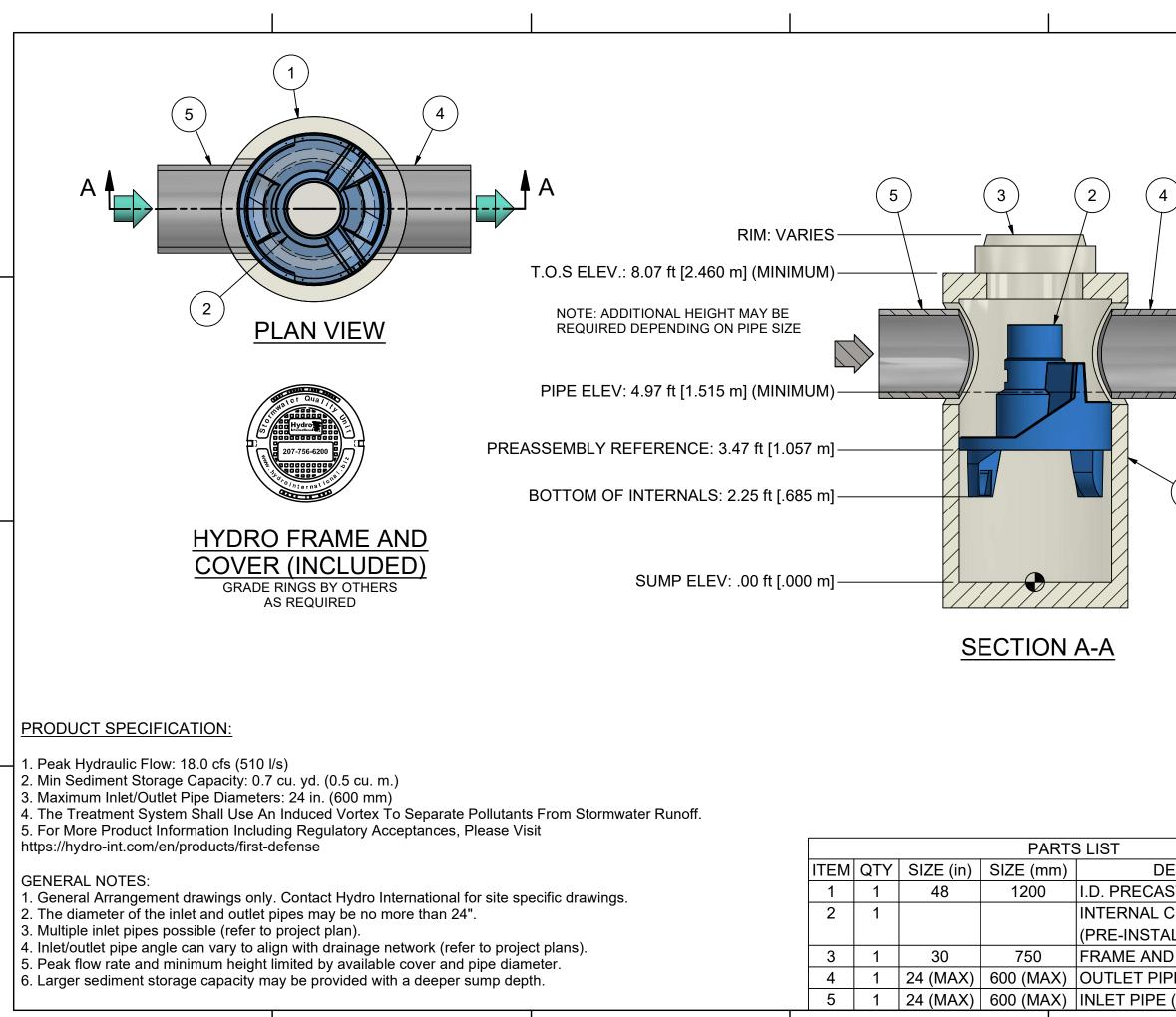
1 of 1

STORM SEWER DESIGN SHEET

PROJECT: CCO-22-2058 LOCATION: 2628 Edinburgh Place CLIENT: BBS Construction

	LOCATION				CONTRIBUTING AREA (ha	a)					RATIONAL D	ESIGN FLOW				SEWER DATA				ł		
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	19	20	21	22	25	26	27	28
STREET	AREA ID	FROM	TO	C-VALUE	AREA	INDIV	CUMUL	INLET	TIME	TOTAL	i (5)	i (10)	i (100)	5yr PEAK	DESIGN	CAPACITY	LENGTH	PIPESIZE (mm	SLOPE	VELOCITY	AVAILO	CAP (5yr)
SINEEI	ANEAID	MH	MH	GVALUE	ANDA	AC	AC	(min)	IN PIPE	(min)	(mm/hr)	(mm/hr)	(mm/hr)	FLOW (L/s)	FLOW (L/s)	(L/ s)	(m)	DIA	(%)	(m/s)	(L/ s)	(%)
	B1	LOB1	LOB2	0.65	0.15	0.09	0.09	10.00	0.41	10.41	104.19	122.14	178.56	27.45	27.45	43.87	21.50	250	0.50	0.866	16.42	37.42%
		LOB2	LOB3				0.09	10.41	0.41	10.83	102.06	119.62	174.86	26.89	26.89	43.87	21.50	250	0.50	0.866	16.98	38.71%
		LOB3	LOB4				0.09	10.83	0.41	11.24	100.01	117.22	171.33	26.35	26.35	43.87	21.50	250	0.50	0.866	17.52	39.93%
		LOB4	LOB5				0.09	11.24	0.42	11.66	98.06	114.92	167.95	25.84	25.84	43.87	21.64	250	0.50	0.866	18.03	41.11%
		LOB5	CBM H1				0.09	11.66	0.31	11.97	96.18	112.71	164.70	25.34	25.34	87.30	32.42	250	1.98	1.723	61.96	70.97%
	B1	CB1	CBM H4	0.65	0.43	0.28	0.28	10.00	0.68	10.68	104.19	122.14	178.56	80.99	80.99	91.46	32.71	375	0.25	0.802	10.46	11.44%
	B1	OB2	CBM H4	0.65	0.36	0.24	0.24	10.00	0.68	10.68	104.19	122.14	178.56	68.32	68.32	91.46	32.74	375	0.25	0.802	23.13	25.29%
																						<u> </u>
	B1	CBM H4	CBM H3	0.65	0.08	0.05	0.57	10.68	0.45	11.13	100.73	118.07	172.57	159.68	159.68	175.96	28.90	450	0.35	1.072	16.28	9.25%
	B1	CBM H3	CBM H2	0.65	0.11	0.07	0.64	11.13	0.60	11.72	98.58	115.53	168.85	175.01	175.01	195.57	31.25	525	0.19	0.875	20.55	10.51%
	B1	CBM H2	CBM H1	0.65	0.04	0.03	0.67	11.72	0.32	12.05	95.89	112.36	164.19	177.82	177.82	195.57	16.93	525	0.19	0.875	17.75	9.08%
	B1	CBM H1	OGS	0.65	0.09	0.06	0.82	11.72	0.13	11.85	95.89	112.36	164.19	218.16	218.16	237.41	8.17	525	0.28	1.062	19.25	8.11%
																						-
		OGS	EX. MH			0.00	0.82	11.72	0.21	11.93	95.89	112.36	164.19	218.16	218.16	237.41	13.34	525	0.28	1.062	19.25	8.11%
																						
										-												
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				N																		L
Definitions:				Notes:				Designed:					No.			Revision				Da		
Q = 2.780A, where:	0 1411			1. Mannings coefficient (n)	=		0.013	FV					1.			Revision 1				2023.	04.12	
Q = Peak Flow in Litres p	. ,																					
A = Area in Hectares (ha	/							Checked:														
i = Rainfall intensity in n		,						Checked:														
[i = 998.071 / (TC+6.0		5 YEAR																				
[i = 1174.184 / (TC+6.0		10 YEAR						Project No .:														
[i = 1735.688 / (TC+6.0	.014)^0.820]	100 YEAR						000-22-2058	3						Da					Shee		
															2015-	05-21				1 0	f 1	

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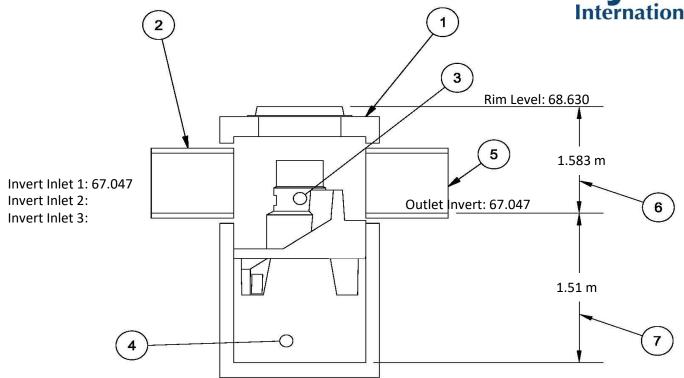


/	
	1. MANHOLE WALL AND SLAB THICKNESSES ARE NOT TO SCALE.
	2. CONTACT HYDRO INTERNATIONAL FOR A BOTTOM OF STRUCTURE ELEVATION PRIOR TO SETTING FIRST DEFENSE MANHOLE.
1	3. CONTRACTOR TO CONFIRM RIM, PIPE INVERTS, PIPE DIA. AND PIPE ORIENTATION PRIOR TO RELEASE OF UNIT TO FABRICATION.
	IF IN DOUBT ASK
	DATE: SCALE: 11/2/2021 1:30
	DRAWN BY: CHECKED BY: APPROVED BY ER MRJ
	Title 4-ft DIAMETER
	FIRST DEFENSE
	GENERAL ARRANGEMENT
	Hydro S.
SCRIPTION	hydro-int.com HYDRO INTERNATIONAL
ST MANHOLE	WEIGHT: MATERIAL:
OMPONENTS	
LLED)	STOCK NUMBER:
COVER (ROUND)	
E (BY OTHERS)	DRAWING NO.: FD GA-4 SHEET SIZE: SHEET: Rev:
	FD GA-4

Hydro First Defense [®] - HC)						Hy	
Rev. 12.6					Net	Annual Remo	val Model: FD-	4HC
Project Name: 22-2058 Street: 2628 Edinburgh Place Province: Ontario		4/18/2023 Ottawa Canada		Paste	Intensity ⁽¹⁾	Fraction of Rainfall ⁽¹⁾	FD-4HC Removal Efficiency ⁽²⁾	Weighted Net Annual Efficiency
Designer: Francis Valenti		F.Valenti@	McInto	shPerry.c	(mm/hr)	(%)	(%)	(%)
		πι			0.50	0.1%	100.0%	0.1%
Treatment Parameters:		DECUI	TS SUM		1.00	14.1%	95.9%	13.5%
Structure ID:		RESUL	13 3010	WARY	1.50	14.2%	92.3%	13.1%
TSS Goal: 80 % Removal		Model	TSS	Volume	2.00	14.1%	89.9%	12.7%
TSS Particle Size: Fine		FD-3HC	71.0%	>90%	2.50	4.2%	88.0%	3.7%
Area: 1.25 ha		FD-4HC	84.0%	>90%	3.00	1.5%	86.6%	1.3%
Percent Impervious: 65%		FD-5HC	89.0%	>90%	3.50	8.5%	85.3%	7.3%
Rational C value: 0,69 Calc. Cn		FD-6HC	91.0%	>90%	4.00	5.4%	84.3%	4.6%
Rainfall Station: Ottawa, ONT	MAP		95.0%	>90%	4.50	1.2%	83.4%	1.0%
Peak Storm Flow: 486.81 L/s		FD-10HC	97.0%	>90%	5.00	5.5%	82.5%	4.6%
annonina anno anno					6.00	4.3%	81.2%	3.5%
Model Specification:					7.00	4.5%	80.0%	3.6%
					8.00	3.1%	79.0%	2.4%
Model: FD-4HC					9.00	2.3%	78.2%	1.8%
Diameter: 1200 mm					10.00	2.6%	77.4%	2.0%
					20.00	9.2%	72.6%	6.7%
<i>Peak Flow Capacity:</i> 510.00 L/s					30.00	2.6%	69.9%	1.8%
Sediment Storage: 0.54 m ³					40.00	1.2%	68.0%	0.8%
Oil Storage: 723.00 L								
Installation Configuration: Placement: Online								<u> </u>
Outlet Pipe Size: 525 mm OK								
Inlet Pipe 1 Size: 525 mm OK					Total Net	Annual Remo	val Efficiency:	84.0%
Inlet Pipe 2 Size: mm OK						nual Runoff Vo		>90%
Inlet Pipe 3 Size: mm OK						0:2007, HLY03, Ottawa		
Rim Level:68.630 mCalc InvsOutlet Pipe Invert:67.047 mOKInvert Pipe 1:67.047 mOKInvert Pipe 2:mInvert Pipe 3:m					the STC Fine distribut	rty verified data and ap tion o 5 min peak intensity l		
Designer Notes:								

Hydro First Defense® - HC





All drawing elevations are metres.

FD-4HC Specification

1	Vortex Chamber Diameter	1200 mm
2	Inlet Pipe Diameter	525 mm
3	Oil Storage Capacity	723.00 L
4	Min. Provided Sediment Storage Capacity	0.54 m ³
5	Outlet Pipe Diameter	525 mm
6	Height(Final Grade to Outlet Invert)	1583 mm
7	Sump Depth(Outlet Invert to Sump)	1510 mm
	Total Depth	3093 mm

Notes:			



First Defense® High Capacity

A Simple Solution for your Trickiest Sites

Product Profile

The First Defense[®] High Capacity is an enhanced vortex separator that combines an effective stormwater treatment chamber with an integral peak flow bypass. It efficiently removes sediment total suspended solids (TSS), trash and hydrocarbons from stormwater runoff without washing out previously captured pollutants. The First Defense[®] High Capacity is available in several model configurations to accommodate a wide range of pipe sizes, peak flows and depth constraints (**Table 1**, next page).

Applications

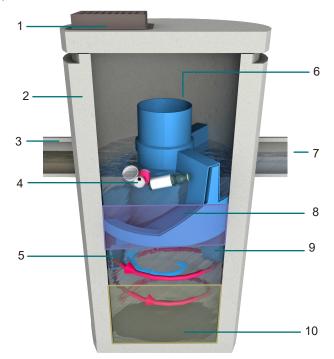
- Stormwater treatment at the point of entry into the drainage line
- Sites constrained by space, topography or drainage profiles with limited slope and depth of cover
- Retrofit installations where stormwater treatment is placed on or tied into an existing storm drain line
- · Pretreatment for filters, infiltration and storage

Advantages

- Inlet options include surface grate or multiple inlet pipes
- Integral high capacity bypass conveys large peak flows without the need for "offline" arrangements using separate junction manholes
- Proven to prevent pollutant washout at up to 450% of its treatment flow
- Long flow path through the device ensures a long residence time within the treatment chamber, enhancing pollutant settling
- Delivered to site pre-assembled and ready for installation

Verified by NJCAT and NJDEP

Fig.1 The First Defense[®] High Capacity has internal components designed to efficiently capture pollutants and prevent washout at peak flows.



Components

- 1. Inlet Grate (optional)
- 2. Precast chamber
- 3. Inlet Pipe (optional)
- Floatables Draw Off Slot (not pictured)
 Inlet Chute
- Internal Bypass
- Outlet pipe
 - 8. Oil and Floatables Storage
 - 9. Outlet chute
 - 10. Sediment Storage Sump

How it Works

The First Defense[®] High Capacity has internal components designed to remove and retain gross debris, total suspended solids (TSS) and hydrocarbons (Fig.1).

Contaminated stormwater runoff enters the inlet chute from a surface grate and/or inlet pipe. The inlet chute introduces flow into the chamber tangentially to create a low energy vortex flow regime (magenta arrow) that directs sediment into the sump while oils, floating trash and debris rise to the surface.

Treated stormwater exits through a submerged outlet chute located opposite to the direction of the rotating flow (blue arrow). Enhanced vortex separation is provided by forcing the rotating flow within the vessel to follow the longest path possible rather than directly from inlet to outlet.

Higher flows bypass the treatment chamber to prevent turbulence and washout of captured pollutants. An internal bypass conveys infrequent peak flows directly to the outlet eliminating the need for, and expense of, external bypass control structures. A floatables draw off slot functions to convey floatables into the treatment chamber prior to bypass.

First Defense[®] High Capacity

Sizing & Design

This adaptable online treatment system works easily with large pipes, multiple inlet pipes, inlet grates and now, contains a high capacity bypass for the conveyance of large peak flows. Designed with site flexibility in mind, the First Defense[®] High Capacity allows engineers to maximize available site space without compromising treatment level.

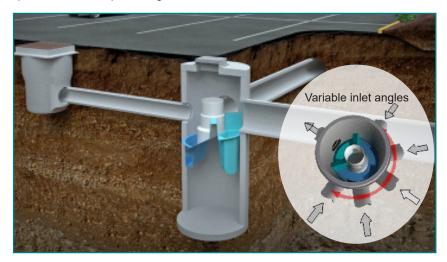


Fig 2. Works with multiple inlet pipes and grates

Inspection and Maintenance

Nobody maintains our systems better than we do. To ensure optimal, ongoing device performance, be sure to recommend Hydro International as a preferred service and maintenance provider to your clients.

Call **1 (800) 848-2706** to schedule an inspection and cleanout or learn more at **hydro-int.com/service**

Table 1. First Defense® High Capacity Design Criteria.

SIZING CALCULATOR FOR ENGINEERS



This simple online tool will recommend the best separatror, model size and online/offline arrangement based on site-specific data entered by the user.

Go to hydro-int.com/sizing to access the tool.



Fig 3. Maintenance is done with a vactor truck

First Defense® High Capacity	Diameter	Typical TSS Flow	S Treatment Rates	Peak Online	Maximum Pine Oil Storage		Pipe Oil Stora		Typical Sediment	Minimum Distance from	Standard Distance from Outlet
Model Number		NJDEP Certified	110µm	Flow Rate	Diameter ¹	Capacity	Storage Capacity ²	Outlet Invert to Top of Rim ³	Invert to Sump Floor		
	(ft / m)	(cfs / L/s)	(cfs / L/s)	(cfs / L/s)	(in / mm)	(gal / L)	(yd³ / m³)	(ft / m)	(ft / m)		
FD-3HC	3 / 0.9	0.84 / 23.7	1.06 / 30.0	15 / 424	18 / 457	125 / 473	0.4 / 0.3	2.0 - 3.5 / 0.6 - 1.0	3.71 / 1.13		
FD-4HC	4 / 1.2	1.50 / 42.4	1.88 / 53.2	18 / 510	24 / 600	191 / 723	0.7 / 0.5	2.3 - 3.9 / 0.7 - 1.2	4.97 / 1.5		
FD-5HC*	5 / 1.5	2.34 / 66.2	2.94 / 83.2	20 / 566	24 / 600	300 / 1135	1.1 / .84	2.5 - 4.5 / 0.7 - 1.3	5.19 / 1.5		
FD-6HC	6 / 1.8	3.38 / 95.7	4.23 / 119.8	32 / 906	30 / 750	496 / 1,878	1.6 / 1.2	3.0 - 5.1 / 0.9 - 1.6	5.97 / 1.8		
FD-8HC	8 / 2.4	6.00 / 169.9	7.52 / 212.9	50 / 1,415	48 / 1219	1120 / 4239	2.8 / 2.1	3.0 - 6.0 / 0.9 -1.8	7.40 / 2.2		

*Coming soon

¹Contact Hydro International when larger pipe sizes are required.

²Contact Hydro International when custom sediment storage capacity is required.

³Minimum distance for models depends on pipe diameter.

Hydro International, 94 Hutchins Drive, Portland, ME 04102 Tel: (207) 756-6200 Fax: (207) 756-6212 Email: stormwaterinquiry@hydro-int.com Web: www.hydro-int.com

APPENDIX H CITY OF OTTAWA DESIGN CHECKLIST

City of Ottawa

4. Development Servicing Study Checklist

The following section describes the checklist of the required content of servicing studies. It is expected that the proponent will address each one of the following items for the study to be deemed complete and ready for review by Oty of Ottawa Infrastructure Approvals staff.

The level of required detail in the Servicing Study will increase depending on the type of application. For example, for Official Plan amendments and re-zoning applications, the main issues will be to determine the capacity requirements for the proposed change in land use and confirm this against the existing capacity constraint, and to define the solutions, phasing of works and the financing of works to address the capacity constraint. For subdivisions and site plans, the above will be required with additional detailed information supporting the servicing within the development boundary.

4.1 General Content

Criteria	Location (if applicable)
Executive Summary (for larger reports only).	N/ A
Date and revision number of the report.	On Cover
Location map and plan showing municipal address, boundary, and layout of proposed development.	Appendix A
Plan showing the site and location of all existing services.	Ste Servicing Plan (C102)
Development statistics, land use, density, adherence to zoning and official plan, and reference to applicable subwatershed and	1.1 Purpose
watershed plans that provide context to which individual developments must adhere.	1.2 Ste Description
	6.0 Stormwater Management
Summary of pre-consultation meetings with City and other approval agencies.	Appendix B
Reference and confirm conformance to higher level studies and reports (Master Servicing Studies, Environmental Assessments,	1.1 Purpose
Community Design Plans), or in the case where it is not in conformance, the proponent must provide justification and	1.2 Ste Description
develop a defendable design criteria.	6.0 Stormwater Management
Statement of objectives and servicing criteria.	3.0 Pre-Consultation Summary

Identification of existing and proposed infrastructure available in the immediate area.	N/ A
 Identification of Environmentally Sgnificant Areas, watercourses and Municipal Drains potentially impacted by the proposed development (Reference can be made to the Natural Heritage Studies, if available). 	Ste Grading Plan (C101)
Concept level master grading plan to confirm existing and proposed grades in the development. This is required to confirm the feasibility of proposed stormwater management and drainage, soil removal and fill constraints, and potential impacts to neighbouring properties. This is also required to confirm that the proposed grading will not impede existing major system flow paths.	Ste Grading Plan (C101)
Identification of potential impacts of proposed piped services on private services (such as wells and septic fields on adjacent lands) and mitigation required to address potential impacts.	N/ A
Proposed phasing of the development, if applicable.	N/ A
Reference to geotechnical studies and recommendations concerning servicing.	Section 2.0 Background Studies, Standards and References
 All preliminary and formal site plan submissions should have the following information: Metric scale North arrow (including construction North) Key plan Name and contact information of applicant and property owner Property limits including bearings and dimensions Existing and proposed structures and parking areas Easements, road widening and rights-of-way Adjacent street names 	Ste Grading Plan (C101)

4.2 Development Servicing Report: Water

Oriteria	Location (if applicable)
Confirm consistency with Master Servicing Study, if available	N/ A
Availability of public infrastructure to service proposed development	N/ A
□ Identification of system constraints	N/A
□ Identify boundary conditions	Appendix C
Confirmation of adequate domestic supply and pressure	N/ A
 Confirmation of adequate fire flow protection and confirmation that fire flow is calculated as per the Fire Underwriter's Survey. Output should show available fire flow at locations throughout the development. 	Appendix C
Provide a check of high pressures. If pressure is found to be high, an assessment is required to confirm the application of pressure reducing valves.	N/ A
Definition of phasing constraints. Hydraulic modeling is required to confirm servicing for all defined phases of the project including the ultimate design	N/ A
Address reliability requirements such as appropriate location of shut-off valves	N/ A
Check on the necessity of a pressure zone boundary modification.	N/ A
Reference to water supply analysis to show that major infrastructure is capable of delivering sufficient water for the proposed land use. This includes data that shows that the expected demands under average day, peak hour and fire flow conditions provide water within the required pressure range	Appendix C, Section 4.2

Description of the proposed water distribution network, including locations of proposed connections to the existing system, provisions for necessary looping, and appurtenances (valves, pressure reducing valves, valve chambers, and fire hydrants) including special metering provisions.	Site Servicing Plan (C101)
Description of off-site required feedermains, booster pumping stations, and other water infrastructure that will be ultimately required to service proposed development, including financing, interim facilities, and timing of implementation.	N/ A
Confirmation that water demands are calculated based on the Oty of Ottawa Design Guidelines.	Appendix C
Provision of a model schematic showing the boundary conditions locations, streets, parcels, and building locations for reference.	N/ A

4.3 Development Servicing Report: Wastewater

Oriteria	Location (if applicable)
Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitored flow data from relatively new infrastructure cannot be used to justify capacity requirements for proposed infrastructure).	N/ A
Confirm consistency with Master Servicing Study and/or justifications for deviations.	N/ A
Consideration of local conditions that may contribute to extraneous flows that are higher than the recommended flows in the guidelines. This includes groundwater and soil conditions, and age and condition of sewers.	N/ A
Description of existing sanitary sewer available for discharge of wastewater from proposed development.	Section 5.2 Proposed Sanitary Sewer

 Verify available capacity in downstream sanitary sewer and/or identification of upgrades necessary to service the proposed development. (Reference can be made to previously completed Master Servicing Study if applicable) 	Section 5.3 Proposed Sanitary Design
Calculations related to dry-weather and wet-weather flow rates from the development in standard MOE sanitary sewer design table (Appendix 'C') format.	N/ A
Description of proposed sewer network including sewers, pumping stations, and forcemains.	Section 5.2 Proposed Sanitary Sewer
Discussion of previously identified environmental constraints and impact on servicing (environmental constraints are related to limitations imposed on the development in order to preserve the physical condition of watercourses, vegetation, soil cover, as well as protecting against water quantity and quality).	N/ A
Pumping stations: impacts of proposed development on existing pumping stations or requirements for new pumping station to service development.	N/ A
Forcemain capacity in terms of operational redundancy, surge pressure and maximum flow velocity.	N/ A
Identification and implementation of the emergency overflow from sanitary pumping stations in relation to the hydraulic grade line to protect against basement flooding.	N/ A
Special considerations such as contamination, corrosive environment etc.	N/A

4.4 Development Servicing Report: Stormwater Checklist

Criteria	Location (if applicable)
 Description of drainage outlets and downstream constraints including legality of outlets (i.e. municipal drain, right-of-way, watercourse, or private property) 	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
Analysis of available capacity in existing public infrastructure.	N/ A
A drawing showing the subject lands, its surroundings, the receiving watercourse, existing drainage patterns, and proposed drainage pattern.	Pre & Post-Development Plans
□ Water quantity control objective (e.g. controlling post- development peak flows to pre-development level for storm events ranging from the 2 or 5-year event (dependent on the receiving sewer design) to 100-year return period); if other objectives are being applied, a rationale must be included with reference to hydrologic analyses of the potentially affected subwatersheds, taking into account long-term cumulative effects.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
Water Quality control objective (basic, normal or enhanced level of protection based on the sensitivities of the receiving watercourse) and storage requirements.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
Description of the stormwater management concept with facility locations and descriptions with references and supporting information.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
Set-back from private sewage disposal systems.	N/ A
Watercourse and hazard lands setbacks.	N/ A
Record of pre-consultation with the Ontario Ministry of Environment and the Conservation Authority that has jurisdiction on the affected watershed.	N/ A
Confirm consistency with sub-watershed and Master Servicing Study, if applicable study exists.	N/ A
Storage requirements (complete with calculations) and conveyance capacity for minor events (1:5-year return period) and major events (1:100-year return period).	Appendix G

Identification of watercourses within the proposed development and how watercourses will be protected, or, if necessary, altered by the proposed development with applicable approvals.	Ste Grading Plan
Calculate pre-and post development peak flow rates including a description of existing site conditions and proposed impervious areas and drainage catchments in comparison to existing conditions.	Section 7.0 Proposed Stormwater Management Appendix G
Any proposed diversion of drainage catchment areas from one outlet to another.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
Proposed minor and major systems including locations and sizes of stormwater trunk sewers, and stormwater management facilities.	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
If quantity control is not proposed, demonstration that downstream system has adequate capacity for the post- development flows up to and including the 100-year return period storm event.	N/ A
□ Identification of potential impacts to receiving watercourses	N/ A
Identification of municipal drains and related approval requirements.	N/ A
 Descriptions of how the conveyance and storage capacity will be achieved for the development. 	Section 6.0 Stormwater Sewer Design & Section 7.0 Proposed Stormwater Management
100-year flood levels and major flow routing to protect proposed development from flooding for establishing minimum building elevations (MBE) and overall grading.	Ste Grading Plan (C101)
Inclusion of hydraulic analysis including hydraulic grade line elevations.	N/ A

Description of approach to erosion and sediment control during construction for the protection of receiving watercourse or drainage corridors.	Section 8.0 Sediment & Erosion Control
Identification of floodplains – proponent to obtain relevant floodplain information from the appropriate Conservation Authority. The proponent may be required to delineate floodplain elevations to the satisfaction of the Conservation Authority if such information is not available or if information does not match current conditions.	N/A
Identification of fill constraints related to floodplain and geotechnical investigation.	N/ A

4.5 Approval and Permit Requirements: Checklist

The Servicing Study shall provide a list of applicable permits and regulatory approvals necessary for the proposed development as well as the relevant issues affecting each approval. The approval and permitting shall include but not be limited to the following:

Oriteria	Location (if applicable)
Conservation Authority as the designated approval agency for modification of floodplain, potential impact on fish habitat, proposed works in or adjacent to a watercourse, cut/fill permits and Approval under Lakes and Rivers Improvement Act. The Conservation Authority is not the approval authority for the Lakes and Rivers Improvement Act. Where there are Conservation Authority regulations in place, approval under the Lakes and Rivers Improvement Act is not required, except in cases of dams as defined in the Act.	N/ A
Application for Certificate of Approval (CofA) under the Ontario Water Resources Act.	N/A
Changes to Municipal Drains.	N/A
 Other permits (National Capital Commission, Parks Canada, Public Works and Government Services Canada, Ministry of Transportation etc.) 	N/A

4.6 Conclusion Checklist

Oriteria	Location (if applicable)
□ Clearly stated conclusions and recommendations	Section 9.0 Summary
	Section 10.0 Recommendations
Comments received from review agencies including the City of Ottawa and information on how the comments were addressed. Final sign-off from the responsible reviewing agency.	All are stamped
All draft and final reports shall be signed and stamped by a professional Engineer registered in Ontario	All are stamped