Z.V. Holdings Corporation

Preliminary Geotechnical Investigation

1881/1883 Merivale and Adjacent Lot, Ottawa



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Preliminary Geotechnical Investigation

1881/1883 Merivale and Adjacent Lot, Ottawa, Ontario

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Acronyms and Abbreviations

Arcadis	Arcadis Canada Inc.
AST	Aboveground Storage Tank
BVL	Bureau Veritas Laboratories
COPE	Construction, Occupancy, Protection, Exposure
CSA	Canadian Standards Association
ESA	Environmental Site Assessment
FIP	Fire Insurance Plan
HASP	Health and Safety Plan
LDPE	Low-density polyethylene
masl	metres above sea level
mald	metres above local datum
mbgs	metres below ground surface
MECP	Ontario Ministry of the Environment, Conservation and Parks
PCA	Potentially Contaminating Activity
PHC	Petroleum hydrocarbons
PVC	Polyvinyl chloride
QA/QC	Quality assurance/quality control
RDL	Reportable detection limit
RPD	Relative percent difference
SCS	Site Condition Standards
SLS	Serviceability Limit State
SPMDD	Standard Proctor Maximum Dry Density
TOC	Top of Casing
ULS	Ultimate Limit State
VOCs	Volatile Organic Compound

Executive Summary

Arcadis Canada Inc. (Arcadis) was retained by Z.V. Holdings Corporation to conduct a Preliminary Geotechnical Investingation in conjunction with Phase One and Two Environmental Site Assessment (ESA) updates of the properties at 1881 and 1883 Merivale Road and Adjacent Lot, Ottawa, ON (the Site). The Preliminary Geotechnical Assessment was required to develop preliminary designs and evaluate alternatives for the proposed new construction. The proposed new construction includes two raised, one-storey, office/warehouse space buildings; Building A of 3540m² and Building B of 3070m², across a total site area of 14,113m² under zoning designation IG – General Industrial zone.

It was understood that the objectives of the Preliminary Geotechnical Investigation were to determine the subsoil and groundwater conditions at the property by means of advancing boreholes and taking soil samples for geotechnical testing. The objective of the investigation was to then provide geotechnical recommendations for design of the proposed development, including construction considerations which may affect the design process.

Arcadis carried out the borehole drilling program on 15 and 16 September 2022, with a return visit to the site to measure groundwater levels on 11 October 2022. The investigation consisted of the advancement of boreholes at nine locations to a typical depth of 5m below existing ground surface (mbgs). Three of the boreholes were completed as piezometers to measure static groundwater levels. One borehole (BH22-10) was advanced using a dynamic cone to a maximum depth of 10.9 metres below surface (mbgs). Selected soil samples obtained were analyzed for grain size distribution and corrosivity parameters.

Generally, the subsurface profile encountered at borehole locations consists of a layer of sand fill at surface underlain by native fine sand with silt/silty sand. The surface fill layer along Jamie Avenue consisted of gravel fill while a medium to coarse sand (often characterized as topsoil when organics were noted) was encountered at other locations. No bedrock was encountered at any borehole locations.

SPT values in the overburden at a depth of 1.5 to 2.5mbgs ranged from 9 to 28 per 0.3m with an average SPT of 16 over the nine boreholes reviewed (BH22-2 to BGH22-10); indicative of a compact relative density. Borehole BH22-10 was advanced beyond 5m depth using a dynamic cone to an eventual depth of 10.9mbgs. SPT values from the cone were 15 at 5.6mbgs and increased with depth. No indications of voids or any very soft overburden materials were observed.

Soil samples submitted for analytical testing to assess the corrosion potential for exposed ferrous metals and the potential of sulphate attacks against subsurface concrete structures found no concerns related to potentially aggressive/ corrosive environment and GU cement was considered suitable for use.

Geotechnical recommendations were provided for slab on grade as well as strip or spread shallow footing construction.

It is also recommended that a professional engineering firm be retained during construction to perform a) observation of and verification of all bearing surfaces prior to the placement of foundation concrete; b) sampling and testing of the concrete and fill materials used; c) periodic observation of the condition of unsupported excavation side slopes in excess of 3m in height, if applicable; d) observation of all subgrades prior to backfilling; e) field density tests to determine the level of compaction achieved; f) sampling and testing of the bituminous concrete including mix design reviews.

1 Introduction

Arcadis Canada (Arcadis) was commissioned by the Z.V. Holdings Corporation to conduct a Preliminary Geotechnical Investigation for the properties located at 1881-1883 Merivale Road, in the City of Ottawa, Ontario (the Site, refer to Figure 1 attached to this report). It is understood that two raised, one-storey warehouse buildings are proposed for the Site. The objectives of the investigation were to provide preliminary geotechnical information to guide design and potential construction of the proposed development.

The scope of work for the preliminary geotechnical investigation included:

- Completion of a field investigation consisting of nine borehole advanced across the Site;
- Water level measurements taken from installed monitoring wells;
- Specified laboratory index testing;
- Geotechnical engineering analyses; and
- Preparation of a preliminary geotechnical engineering report.

The following report has been prepared specifically and solely for the aforementioned project which is described herein. It contains our preliminary findings and geotechnical recommendations pertaining to the design and construction of the subject development as they are understood at the time of writing this report. We note that the recommendations provided in this report are intended solely for the preliminary planning of this development. Geotechnical recommendations may change with proposed design changes. Further investigation will be required before detailed geotechnical parameters can be provided.

This report does not address environmental concerns associated with the Site. Please reference the Arcadis Phase One and Two ESA reports completed for these properties, as provided under separate cover.

1.1 Site Description

Address #1: 1881 and 1883 Merivale Road, Ottawa, Ontario

Location: The site is surrounded by mixed residential and commercial properties. It is located on the east side of Merivale Road and south side of Jamie Avenue in the City of Ottawa, Ontario. Refer to **Figure 1** following the text.

Latitude and Longitude: 45° 19' 57.8244" N, 75° 43' 19.7508" W (centroid)

Zoning: IG- General Industrial Use

Site Area: 14,113 m²

The subject site is currently occupied by an undeveloped grass field with a graveled school bus parking lot adjacent to the Jamie street property access. Grass covered areas and mature bushes/trees are found on the periphery of the property. The existing ground surface at the site is relatively flat with a gentle downslope towards the west.

1.2 Physical Setting

The subject property is situated in an urban area zoned for institutional land use. The subject area is relatively flat and generally level with surrounding grades having an approximate elevation of 91masl. Based on site observations and topographic maps, both 1881 and 1883 Merivale properties slope from east to west towards Merivale Road. Based on site observations and topographic maps both 1881 and 1883 Merivale slope from east to west towards Merivale Road. Generally, 1883 Merivale Road is at a higher elevation than 1881 Merivale Road, which is at a slightly higher elevation than 6 and 12 Jamie Avenue. Site drainage was not observed, no ditches were observed on either site. The site surface stormwater would be expected to flow from east to west towards Merivale Road. The regional topography is relatively flat. A depiction of the site is shown on **Figure 2**.

1.3 Local Geology and Hydrogeology

Bedrock geology mapping for the Site indicates that local bedrock is described as the Rockcliffe Formation comprising shale with lenses of sandstone (Geological Survey of Canada Map 1058A Generalized Bedrock Geology Ottawa, Ontario and Quebec).

The surficial geology mapping referenced describes surface soils as: Deltaic and Estuarine deposits, medium to fine grained sand, in some place fossiliferous; lying outside abandoned channels; most common deposit is a combined strip delta-sand plain that developed as fluvial water levels fell (Geological Survey of Canada Map 1056A Surficial Geology Ottawa, Ontario and Quebec).

Borehole logs and figures from surrounding properties were also referenced for surficial soil geology from records returned in the ERIS Ecolog search. According to the data contained in logs for wells advanced in close proximity to the property, the soils were generally characterized as sand and/or medium sand from surface to a depth ranging from 10.67 to 15.2 metres below ground surface (mbgs) before encountering bedrock.

Regional shallow groundwater may be directed westwards towards surficial water bodies in the Pinhey Forest but it is expected that deep groundwater flow may be in a northeasterly direction towards the Rideau River, based on a review of local topographical features and drainage patterns. Immediate area groundwater flow may be influenced by local features such as the presence of utilities and site facilities.

1.4 Proposed Development

The specific study area is located at 1881-1883 Merivale Road in Ottawa, Ontario. The proposed new construction includes two raised, one-storey buildings; Building A of 3540m² area and Building B of 3070m² area office/warehouse space, across a total site area of 14, 113m² under zoning designation IG – General Industrial zone.

1.5 Previous Reporting

Arcadis completed previous reporting for this subject property, which included the following reports: *Phase I and II Environmental Site Assessment, Arcadis – dated 17 December 2019.*

2 Scope of Work

The scope of work for the preliminary geotechnical investigation, conducted concurrently with the Phase One and Two ESA Updates for the Site, included the following:

- i. Development of a Site Specific Health and Safety Plan governing all site activities;
- ii. Performance of Utility OneCall clearances as well as borehole location clearances performed by a private utility locator;
- iii. Advancement of nine boreholes to depths ranging from 5.18 to 10.67mbgs (refer to Figure 2 for locations);
- iv. Installation of monitoring wells in three of the advanced boreholes;
- v. Selection of soil samples obtained for geotechnical analyses and submission to an accredited laboratory for testing;
- vi. Return to site and measurement of water levels, where possible;
- vii. Survey of all boreholes and monitoring wells to a temporary, local benchmark; and
- viii. Preparation of a preliminary geotechnical report summarizing the results of the onsite investigation and providing basic geotechnical recommendations to inform the proposed design and construction.

3 Method of Investigation

3.1 General

The field work for this investigation was carried out on 15 and 16 September (with a subsequent site visit on 11 October) under the supervision of Mr. Lennart DeGroot, B.Sc. of Arcadis. Nine boreholes were drilled on the subject property at the locations shown on **Figure 2**. Borehole locations were selected to correspond with the proposed building footprints as shown on the preliminary site layout drawings provided to Arcadis.

The Site area and all test locations were cleared for buried utilities prior to the start of the field investigation program. Ontario OneCall was contacted to determine the location of public utilities, and USL-1 was contracted to clear private utilities.

Standard field procedures are summarized in the following sections.

3.2 Borehole Drilling

Nine boreholes (BH22-2 through -10) were advanced on 15 and 16 September 2022 as shown on **Figure 2**. Borehole depths ranged from 5.18mbgs to 10.67mbgs. Descriptions of the soil stratigraphy encountered are presented on the borehole logs included as **Appendix A**.

The boreholes were advanced using a truck-mounted CME-55 auger drill rig (with hollow stem augers) operated by a two-person crew from Downing Estate Drilling. All fieldwork was conducted under the full-time supervision of Arcadis personnel, under the direction of a senior engineer. The proposed borehole at location BH22-1 was not able to be advanced due to safety concerns associated with heavy traffic at that location. Boreholes were backilled with bentonite clay chips at the end of site operations, with the exception of three boreholes (BH22-2, -4, and -6) which were outfitted as monitoring wells for purposes of evaluating water table elevation measurement and groundwater sampling.

3.1.2 Soil Sampling and In-Situ Testing

Soil samples were collected from the boreholes using a 51mm diameter, 0.6m long split-spoon (SS) sampler on a continuous basis to 3mbgs, then at intervals of 1.6m thereafter. Standard penetration testing (SPT) was performed, and "N" values were recorded at the time of sample collection to assess soil density conditions.

All soil samples were visually inspected and initially classified on site. The split-spoon samples were placed in sealed plastic bags or jars and logged in the field for soil type, moisture content, colour, structure, and visual evidence of potential contamination, then transferred to the Arcadis laboratory for further evaluation. Borehole logs were prepared on the basis of sample and drilling process observations in the field describing the encountered strata and are presented in **Appendix A**. Site photographs are presented in **Appendix B**. Samples were selected and submitted to ALS in Ottawa, Ontario, for the selected geotechnical testing.

All samples will be stored at the laboratory for a period of one month after the issue date of this report. They will then be discarded unless we are otherwise directed. All excess soil cuttings were used as backfill when reinstating boreholes.

3.3 Groundwater Monitoring Well Installation and Groundwater Elevation Measurement

Three boreholes were finished as groundwater monitoring wells – BH22-2, -4, and -6 – to permit monitoring of the groundwater levels at Site. The monitoring wells comprised 50mm diameter Schedule 40 PVC Triloc riser pipes with a 3.05m long No. 10 slot intake zone (well screen). Silica sand was placed around the piping to a height of at least 300mm above the top of the well screen as filter pack. The remaining annular space was filled with a bentonite clay seal. A protective aluminum flushmount casing was then cemented in place at the top of the well.

In accordance with O.Reg. 903, well records were submitted to the MECP for the monitoring wells installed at the Site. The well tag and well record was submitted by the subcontracted licenced well drillers (Downing) who performed the installation.

A dedicated WaTerra inertial pump was installed in each monitoring well. The well was developed by handpumping the WaTerra sampler to ensure that at least three well volumes of water were removed (or until the well ran dry) to reduce the potential effects of foreign material introduced through drilling and to maximize the responsiveness of the surrounding geological materials.

Groundwater table monitoring was completed on 11 October 2022 at all wells within the same time period to ensure that the results are representative of conditions across the Site. Any unusual weather conditions and modifying features were noted on the log.

3.4 Field Survey

The test holes and monitoring wells installed on Site were located and surveyed in the field by Arcadis personnel during the initial fieldwork. Elevations were surveyed using a TopCon laser-level unit to a local datum, where the top of the concrete NE corner of the residential building used as the Diver's Wearhouse was assigned an elevation of 100.00m. The borehole location northing and easting coordinates were determined using a handheld GPS. The borehole locations are presented on **Figure 2** and the ground surface elevations are shown on each borehole log (**Appendix A**).

4 Geotechnical Laboratory Testing Program

Geotechnical laboratory testing was carried out on representative samples recovered from the boreholes, to effectively classify the soil strata observed in the field. This program included:

- Natural moisture content on all recovered samples where feasible;
- Grain size (sieve and hydrometer) testing on two samples;
- Coarse/fine material analyses on four samples; and
- Corrosivity suite testing on three samples.

The results of the testing program have been summarized in tabular format following the text of this report. Samples subjected to geotechnical testing have been identified on the borehole logs presented as **Appendix A**. Where applicable, the results of the index testing have been included on the borehole logs.

Additional soil and groundwater analytical results are reported in the corresponding Phase II ESA report prepared by Arcadis, presented under a separate cover. Environmental results and potential liabilities are not discussed in this report, unless where specifically noted.

The laboratory certificates of analyses are presented in Appendix C.

5 Subsurface Conditions

Generally, the subsurface profile encountered at borehole locations consists of a layer of gravel fill or topsoil underlain by native silty sand/sandy silt units. grading to light brown fine sand with depth. The surface fill layer along Jamie Avenue consisted of gravel fill while a medium to coarse sandy topsoil was encountered at other locations. No bedrock was encountered at any borehole location.

Reference should be made to the borehole logs in **Appendix A** for specific details of the soil profiles encountered at each borehole location.

5.1 Fill Soils

Fill soils were encountered at each borehole location onsite.

5.1.1 Gravel/Sand Fill

Gravel or sand fill (parking lot surfacing, at some locations) was encountered at borehole locations BH22-2, -3, -5 and -8 at surface and extended to depths ranging from 0.3 to 1.2mbgs. This unit was generally described as light grey and dry, with some to trace sand. The natural water content was measured at 0-8% - moisture content was not measured at each location if the sample was considered too dry. The SPT values obtained in this strata ranged from 5-18 blows per 300mm, indicating a loose to compact (medium dense) soil.

5.1.2 Topsoil

Topsoil was encountered at borehole locations that were not in areas used as parking space; BH22-4, -6, -7, -9, and -10. This unit was encountered at surface and extended to depths ranging from 0.3 to 0.6mbgs. This stratum was generally described as moist and brown to black organic material and medium to coarse sand, with or without organic lenses, trace roots and grass debris. The natural water content was measured at 10-16%. SPT values in this unit ranged from 2-4, indicating a loose to very loose soil.

5.2 Native Soils

5.2.1 Silty Sand/Silt with Sand

Silty sand/sand with silt was encountered at each borehole location, underlying the surficial fill units. This unit was general described as dry to moist, light to dark brown or grey fine sand with silt. Some lenses of coarser sand material were noted, as well as mottled texture in BH22-9. The natural water content was measured at 2-19%, with an average of 8%. The SPT values in this stratum ranged from 9-33, indicating a loose to dense soil.

5.2.2 Sand

Native sand was encountered in BH22-7 at a depth of 2.4mbgs and continuing to borehole termination at 5.18mbgs. This stratum was described as moist, light brown to light grey fine to coarse sand with some silt. The natural water

content was measured at 5%. SPT values in this unit ranged from 23-38, indicating a compact (medium dense) to dense soil.

5.3 Bedrock

The bedrock surface was not encountered in any of the borehole locations advanced. The cone penetration test performed at BH22-10 was terminated at a depth of 10.67mbgs.

5.4 Groundwater

Groundwater levels were measured at the monitoring wells in the borehole locations on 11 October 2022. The measured groundwater levels in monitoring wells are presented in **Table 2** following the text of this report – of the three wells, only one was observed to have collected liquid. Borehole logs indicated the presence of a wet soil at depths ranging from 2.5 to 4.5mbgs. Capillary action in the silty native soils may tend to wick moisture upwards. Based on these observations, the long-term shallow groundwater table is anticipated to vary seasonally between 3.5 to 5.5m depth below grade. It is anticipated that groundwater elevations may vary between the monitoring time and the time of construction.

The groundwater levels measured in 2019 are noted on **Figure 3**. These are not necessarily considered representative of current conditions but may be used as a reference when discussing construction methodology.

6 Geotechnical Discussion and Recommendations

It is understood that the site is intended to be developed as warehouse space, with two raised, single-storey warehouse buildings occupying the proposed footprints as shown on **Figure 2** at the rear of this report. Further geotechnical engineering analyses and/or investigation work may be required if the design changes beyond what has been proposed.

From a geotechnical perspective, the subject site condition is satisfactory for the construction of the proposed two buildings. It is recommended that the proposed building be founded on conventional shallow foundations placed over competent native silty sands. The geotechnical recommendations provided herein to assist preliminary foundation and building design are general in nature as limited details are available regarding the proposed structures. The recommendations should be reviewed by Arcadis prior to final design and construction to assess their applicability to the proposed structure. Further engineering, analyses and investigation work may be required once the final building parameters and configuration is known.

It is assumed that the proposed buildings would be no more than one raised storey in height. On the basis of the results of the field investigation program carried out during this study, the following geotechnical recommendations are provided.

6.1 Foundation Considerations

6.1.1 Shallow Foundations

The subsurface conditions encountered at the site are considered suitable for support for the proposed warehouse buildings on spread or strip footings, provided that they can be designed using the bearing resistance values provided below. Due to the presence of competent soils at shallow depths, deep foundations involving piles or caissons is not considered necessary or cost-effective. All existing fill, topsoil, organics, humus, reworked fill and any other deleterious material should be excavated and removed and the spread or strip footings founded on the underlying competent native silty sands/sands.

The maximum bearing resistance for spread or strip foundations up to 1.5m in width founded on the undisturbed native silty sands may be designed using a net allowable serviceability limit states (SLS) bearing capacity of 100kPa and a factored bearing resistance value at ultimate limit states (ULS) of 200 kPa. The maximum bearing resistance for pad footings up to 4m in width may be taken as the same.

Exterior wall support structures placed on undisturbed compact silty sand can be designed using a bearing resistance value SLS of 100kPa and a factored bearing resistance at ULS of 200kPa. All founding surfaces must be proof rolled by adequately sized compaction equipment making several passes under dry conditions and above freezing temperatures.

A geotechnical resistance factor of 0.5 was applied to the reported bearing resistance values at ULS.

In the proposed warehouse building footprint areas, the surface of undisturbed native silty fine sand stratum is located 0.6 to 1.8 m below grade. Total and differential settlements of properly designed and installed foundations are estimated to not exceed 25mm.

Proof-rolling and geotechnical inspection is required to ensure that founding surfaces are of acceptable undisturbed, native soils prior to placing crushed stone, engineered fill or concrete.

6.1.2 Slabs-on-Grade

It is anticipated that slab-on-grade floor construction may be required for the main floor of the buildings. The surficial topsoil/humus layer is considered unsuitable for support of building floor slabs due to its compressible nature and should be excavated and removed. Any underlying reworked overburden is considered adequate for support of building floor slabs. The underlying native silty sands, if exposed during regrading of the site, are also considered suitable for slab-on-grade floor support. Exposed surfaces of the reworked or undisturbed sandy soil should be proof rolled to identify soft spots, which should be repaired through excavation and backfilled with OPSS Granular B fill material compacted to not less than 95% SPMDD.

Any building floor slabs should typically be constructed to be independent of building foundation walls, or any other part of the structure founded on different soils/foundations to minimize differential settlement.

A minimum 150 mm-thick layer of compacted, free-draining granular or crushed stone material should be placed between the subgrade and the building floor slab to provide proper sub-slab drainage, moisture migration and support. If reworked overburden or native fill options are used, given the variable subgrade soil gradation potentially present it is recommended that a non-woven geotextile layer (Terrafix 270R or equivalent) be placed to separate crushed stone from the subgrade.

Proof-rolling and geotechnical inspection is required to ensure that founding surfaces are of acceptable undisturbed, native soils prior to placing crushed stone, engineered fill or concrete.

6.1.3 Frost Protection

All exterior foundations should be provided with a minimum of 1.5m soil cover, or equivalent, to provide frost protection. Frost protection should also be provided for any slabs exposed to the elements. The silty or fine sand stratum is considered to be frost susceptible. Due to its freezing potential, the silty or fine sand material is not recommended as backfill to exterior building walls.

Trench excavations and pavement construction are difficult activities to complete during freezing conditions without introducing frost in the sub-grade or in the excavation walls and bottoms. Precautions should be taken if such activities are to be carried out during freezing conditions.

6.2 Site Grading and Preparation

6.2.1 Recommendations for Soil Removal

Asphalt, topsoil, and deleterious fill, such as material containing high content of organic materials or construction remnants, should be stripped entirely from under the proposed building footprint and other settlement sensitive structures (e.g. pavement structures). All overburden at the subject property within the proposed building footprints are expected to be removed. Further geotechnical analyses on the stratum will be required if the fill is to be considered for construction use (founding surface, backfill, etc.) on site.

6.2.2 Engineered and Native Fill

Fill used for grading beneath the proposed building should consist of clean imported granular fill, such as Ontario Provincial Standard Specifications (OPSS) Granular A or Granular B Type II. This material should be tested and approved prior to delivery to the site. The fill should be placed in lifts no greater than 300mm thick and compacted using suitable compaction equipment for the lift thickness. Load-bearing fill soils placed beneath the building footings and paved areas should be compacted to at least 98% of the material's standard Proctor maximum dry density (SPMDD).

Topsoil and humus excavated throughout the site may be stockpiled for future use on site. Reworked native soils excavated during the course of foundation installation are considered to be frost susceptible and as such are not recommended for use as load-bearing material. The material may be reused on site as general upfill as required for berms or landscaping.

Non-specified existing fill, along with site-excavated soil, can be used as general landscaping fill where settlement of the ground surface is of minor concern. This material should be spread in thin lifts and at least compacted by the tracks of the spreading equipment to minimize voids. If this material is to be used to build up the subgrade level for areas to be paved, it should be compacted in thin lifts to at least 98% of the material's SPMDD (this will require Proctor testing).

Non-specified existing fill and site excavated soils are not suitable for use as backfill against foundation walls unless used in conjunction with a composite drainage membrane. Further geotechnical testing and analyses on this material to confirm consistency and suitability is required before it is approved for construction use such as this.

6.2.1 Excess Soils

The removal of any excess soil from the site should follow the requirements of O.Reg. 406/19- *On-Site and Excess Soil Management*.

6.3 Seismic Considerations

6.3.1 Seismic Hazard

The Ottawa area falls within the Western Quebec Seismic Zone (WQSZ), according to the Geological Survey of Canada. Based on a review of Ontario Geological Survey maps (map 431A), the project Site is not underlain by any known faults. Under the 2015 Ontario Building Code, a seismic hazard with a 2% probability of exceedance in 50 years has been retained for design of the building structure. The design earthquake magnitude retained for this event is 6.1, and represents the mean magnitude of the de-aggregation of the PGA seismic hazard for Ottawa.

6.3.2 Liquefaction Assessment

Liquefaction is a seismically induced phenomenon that can cause soil densification and excess pore pressures which then can lead to potentially large surface settlements and sudden temporary losses in bearing strength. These then can cause lateral spreading and catastrophic soil failures (or flow slides) which are often observed

alongside rivers or shorelines. The shallow overburden present at the subject site is not considered to be potentially liquifiable.

6.3.3 Seismic Classification

At this preliminary stage, the site class for seismic site response can be taken as **Class D** (stiff soil) for the foundations bearing on soil profile materials with an average N_{60} between 15 to 50.

Seismic classifications should be verified during the subsequent detailed geotechnical investigation(s) using field MASW/ESPAC and seismic refraction methods.

6.4 Pavement Recommendations

Founding soils for pavements structure must be proof-rolled and inspected by qualified personnel prior to pavement structure construction. Where required at the subject site, the recommended pavement structures for parking areas and access lanes are shown below:

Thickness (mm)	Material Description				
50	Wear Course: HL-3 or Superpave 12.5 Asphaltic Concrete				
150	Base: OPSS Granular A Crushed Stone base				
300	Subbase: OPSS Granular B Type II				
Subgrade: Either fill, competent in-situ soil or OPSS Granular B Type I or II material placed over competent in- situ soil or fil.					

Table 6-1: Recommended Pavement Structure-Car Only Parking Areas

Table 6-2: Recommended Pavement Structure- Access Lanes and Heavy Truck Parking/Loading Areas

Thickness (mm)	Material Description			
40	Wear Course: HL-3 or Superpave 12.5 Asphaltic Concrete			
50	Binder Course: HL-8 or Superpave 19.0 Asphaltic Concrete			
150	Base: OPSS Granular A Crushed Stone base			
450	Subbase: OPSS Granular B Type II			
Subgrade: Either fill, in-situ soil or OPSS Granular B Type I or II material placed over in-situ soil or fil.				

Minimum Performance Graded (PG) 58-34 asphalt cement is recommended for this project.

If soft spots develop in the subgrade during compaction or due to construction traffic, the affected areas should be excavated and replaced with compacted OPSS Granular B Type II material. Weak subgrade conditions may be

experienced over service trench fill materials. This may require the use of a geotextile, such as Terrafix 270R or equivalent, thicker subbase or other measures that can be recommended at the time of construction as part of the field observation program.

The pavement granular base and subbase should be placed in maximum 300mm thick lifts and compacted to a minimum of 100% of the material's SPMDD using suitable vibratory equipment.

7 Design and Construction Precautions

7.1 Temporary Excavations

Temporary excavations are expected to be shallow and must conform to the stipulations made in O.Reg. 213/91 promulgated under the Occupational Health and Safety Act. Most soils that will be encountered in temporary excavations are anticipated to be Type 3, as defined under the Regulation. Therefore, open cut side slopes would need to be cut back at an inclination of no steeper than 1 horizontal to 1 vertical (1H:1V). For slopes which are unsupported in the longer term, and might experience free-thaw cycles, flatter side slope inclinations could be required. It is not anticipated that excavations would extend below the groundwater table, but any soils below such would be considered Type 4 and require 3H:1V slopes

7.2 Foundation Drainage and Backfill

Based on the amount of silt present in native soils on site, it is recommended that a perimeter foundation drainage system be provided for the proposed structure. The system should consist of a 100 mm diameter perforated corrugated plastic pipe, surrounded on all sides by 100mm of 19mm clear crushed stone which is placed at the footing level around the exterior perimeter of the structure. The perimeter drainage pipe system should direct water to a suitable outlet.

7.3 Pipe Bedding and Backfill

Bedding and backfill materials should be in accordance with the most recent Material Specifications & Standard Detail Drawings from the Department of Public Works and Services, Infrastructure Services Branch of the City of Ottawa.

A minimum of 150mm of OPSS Granular A should be placed for bedding for sewer or water pipes when placed on soil subgrade. If the bedding is placed on bedrock, the thickness of the bedding should be increased to 300 mm for sewer pipes. The bedding should extend to the spring line of the pipe. The material should be placed in a maximum 300mm thick loose lifts and compacted to a minimum of 95% of its SPMDD.

The cover material, which should consist of OPSS Granular A, should extend from the springline of the pipe to at least 300mm above the obvert of the pipe. The material should be placed in a maximum 300 mm thick loose lifts and compacted to a minimum of 95% of its SPMDD.

Where hard surface areas are considered above the trench backfill, the trench backfill material within the frost zone (to about 1.8 m below finished grade) should match the soils exposed at the trench walls to minimize differential frost heaving. The trench backfill should be placed in a maximum 300 mm thick loose lifts and compacted to a minimum of 95% of the material's SPMDD.

If required, frost depth protection can be provided to duct banks or similar using an overlay of Styrofoam SM insulation. Insulation overlay design and backfill parameters can be provided by Arcadis once embedment depths have been confirmed.

7.4 Groundwater Control

6.4.1 Groundwater Control for Building Construction

Based on our observations, it is anticipated that groundwater infiltration into the excavations should be negligible given use of shallow spread or strip footings under summer conditions. Pumping from open sumps should be sufficient to control the groundwater influx through the sides of shallow excavations under summer conditions.

The contractor should be prepared to direct water away from all bearing surfaces and subgrades, regardless of the source, to prevent disturbance to the founding medium. Discharged water should be subject to filtering before discharge. A municipal permit will be required if impounded water is pumped into the sewer. Any sewer discharges should be conducted to meet City of Ottawa sewer discharge bylaw standards.

The finished exterior surface grades of the proposed structure should be sloped away from the building to prevent surface ponding and infiltration immediately adjacent to the building exterior walls. Backfill adjacent to all exterior walls should comprise compacted, free-draining granular materials (OPSS Granular B or equivalent).

6.4.2 Permit to Take Water/ EASR

It is unlikely that a Ministry of the Environment, Conservation and Parks (MECP) permit to take water (PTTW) is required for this site (typically required if more than 400,000 L/day of ground and/or surface water is to be pumped during the construction phase). For typical ground or surface water volumes being pumped during the construction phase, typically between 50,000 to 400,000 L/day, it is required to register on the Environmental Activity and Sector Registry (EASR). A minimum of two to four weeks should be allotted for the completion of the EASR registration and the Water Taking and Discharge Plan to be prepared by a Qualified Person as stipulated under O. Reg. 63/16.

Neither a PTTW or an EASR is expected to be required for this site given the shallow nature of the proposed foundation footings and the inferred depth of water table across the site.

7.5 Winter Construction

The subsoil fill conditions at this site mostly consist of frost susceptible materials. In presence of water and freezing conditions, ice could form within the soil mass. Heaving upon freezing and settlement upon thawing could occur. Precautions should be taken if winter construction is considered for this project.

In the event of construction during below zero temperatures, the founding stratum should be protected from freezing temperatures by the use of straw, propane heaters, tarpaulins or other suitable means. In this regard, the base of the excavations should be insulated from sub-zero temperatures immediately upon exposure and until such time as heat is adequately supplied to the building and the footings are protected with sufficient soil cover to prevent freezing at founding level.

Any trench excavations should be carried out in a manner that will avoid the introduction of frozen materials into the trenches. As well, pavement construction is difficult during winter. The subgrade consists of frost susceptible soil which will experience total and differential frost heaving as the work takes place. In addition, the introduction of frost, snow or ice into the pavement materials, which is difficult to avoid, could adversely affect the performance

of the pavement structure. Additional information and recommendations can be provided during the design and construction project phases if requested.

7.6 Corrosion Potential

Three soil samples were submitted for corrosivity testing, from BH22-3, -5, and -6. The results of analytical corrosivity testing on soil are summarized in Table 4 following the text of this report.

The laboratory results on soil indicate that the sulphate content was non-detect in samples submitted, indicating a non-corrosive environment. As The threshold for chloride content requiring amended concrete is 0.2%, while the maximum concentration observed was at $41\mu g/g$ (or 0.0041%), which is acceptable. The neutral pH levels (from 7.5 to 6.6) of the three samples analyzed indicate that this is not a contributing factor in creating a corrosive environmental for exposed ferrous metals at this site.

Based on the National Corrugated Steel Pipe Association, a low soil resistivity relates to increased potential corrosion activity and is governed by the content of electrolytes, which consist of moisture, minerals and dissolved salts which can vary throughout the seasons. Typically, the lower the resistivity, the higher will be the soil corrosivity. Corrosive soil environments occur with a resistivity between 30 and 50 Ohm-m while even lower values are highly corrosive. Based on the soil samples tested with a resulting minimum resistivity of 4950 Ohm-cm (or 49.5 Ohm-m), the corrosion rating for the subject property soil classifies it essentially a non-corrosive environment.

Uncontaminated, high quality concrete normally provides excellent corrosion protection for reinforcing steel. The high pH environment of the concrete (greater than 12.5) keeps the reinforcing steel in a non-active corrosion state. Intrusion of chlorides into the concrete through contact with chloride-contaminated soil, water or marine atmosphere, however, may lead to corrosion of the embedded reinforcing steel. Sulphate attack can cause extensive cracking, expansion and loss of bonds between the cement paste and aggregates. Type GU Portland cement should therefore be suitable for use in concrete at this site based on the results as reported by the laboratory.

8 Future Recommendations

8.1 Detailed Geotechnical Investigation

The geotechnical recommendations provided herein are preliminary in nature. It is recommended that a detailed geotechnical investigation be performed once the new building design has been finalized and once proposed footing alignments and depths are known. Recommendations for future geotechnical work on site and in the laboratory to support the building design process should include, but are not limited to:

- Further geotechnical testing (additional grain size analyses, Proctor testing) of any onsite fill/ soil
 materials proposed for reuse;
- A soil management plan be developed with the aim of handling soils suitable as native fill, as well as excess soils generated during the construction process, in an efficient and cost-effective manner; and
- Confirmatory boreholes to confirm soil types, distributions and depths to bedrock at defined intervals across the proposed building footprint and especially at proposed corners, anticipated footing locations, etc.

8.2 Geotechnical Consultation During Design Process

The preliminary geotechnical recommendations provided herein to assist foundation and building design are general in nature as specifics of the structure have yet to be determined. These recommendations should be reviewed by Arcadis prior to final design and construction to assess their applicability to the proposed structure. Site-specific foundation design recommendations will be required for components of the proposed structure.

8.3 Geotechnical Supervision During Construction

Development of the subject site will require movement of a variety of soil types and potentially specialized foundation installations. It is recommended that a qualified geotechnical engineer be retained to inspect and approve the subgrade prior to placement of utility lines, watermain thrust blocks, pavement structures, building floor slab/foundations or to supervise the installation of foundations. Geotechnical supervision should also be provided to ensure that engineered fill placed beneath floor slabs, roadways and parking areas is properly compacted and that any weak soil layers are properly removed. Geotechnical inspection of the bearing conditions for the proposed foundation system should also be carried out.

Geotechnical site supervision and review is required during future construction activities. It is recommended that the following material testing and observation program be performed by a licensed geotechnical engineering consultant during construction operations:

- · Observation of all bearing surfaces prior to the placement of concrete/crushed stone/engineered fill;
- · Sampling and testing of the concrete and fill materials used;
- Periodic observation of the condition of unsupported excavation side slopes in excess of 3m in height, if applicable;
- Observation of all subgrades prior to backfilling;

- · Field density tests to determine the level of compaction achieved; and
- Sampling and testing of the bituminous concrete including mix design reviews.

A report confirming that these construction works have been conducted in general accordance with geotechnical recommendations would then be issued following the completion of a satisfactory material testing and observation program by the geotechnical consultant. It is recommended that all footing excavations be inspected by competent geotechnical personnel to ensure that a proper bearing surface has been attained and that foundation designs are suited to site conditions.

8.4 Existing Wells

The groundwater wells installed at this site will require decommissioning at the time of construction in accordance with O.Reg. 461/19 protocols.

9 Closure

The field work and reporting for this investigation was carried out by Mr. Lennart de Groot, B.Sc. and Mr. Justin Cameron, B.Sc., working under the direction and final review of Mr. Troy Austrins, P.Eng., PMP and Mr. Ryan Janzen, P. Eng.

We trust that the contents of this report are sufficient for your present purposes. If you have any questions, please call.

Respectfully submitted,

Arcadis Canada Inc.

Ryan Janzen, P.Eng. Project Engineer

SERVICE FILM

Troy Austrins, P.Eng., PMP Team Lead

10 Statement of Limitations

This report, prepared for the Z.V. Holdings Corporation, does not provide certification or warranty, expressed or implied, that the investigation conducted by Arcadis uncovered all potential geotechnical constraints at the site. The conclusions and recommendations presented in this geotechnical investigation report are based on the information determined at the borehole locations. The information contained within this report in no way reflects the environmental aspect of the site or soil, unless specifically reported upon. Subsurface and groundwater conditions between and beyond the test locations may differ from those encountered at the specific locations tested, and conditions may be encountered during construction which were not detected and could not be anticipated at the time of the site investigation. It is recommended that Arcadis be retained during construction to confirm that the subsurface conditions throughout the subject property do not differ materially from those conditions in this report were used to establish relative elevation differences between the test locations and should not be used for other purposes, such as grading, excavating, planning, development, etc.

The design recommendations provided in this report are applicable only to the project described in the text and then only if constructed substantially in accordance with the details stated in this report. Since all details of the design may not have been available at the time this report was prepared, it is recommended that a qualified engineering consultant be retained during future stages of the design process to verify that the design is consistent with the recommendations of this report, and that the assumptions made in the analyses contained in this report are still valid. The need for additional subsurface investigation work and laboratory testing should be reviewed by the retained qualified engineering consultant during the course of the detailed design work.

The comments given in this report on potential construction problems and possible methods of construction are intended only for the guidance of the designer. The number of boreholes/ groundwater wells may not be sufficient to determine all of the factors that may affect construction methods and costs (e.g., the thickness of surficial topsoil and fill layers can vary markedly and unpredictably). Contractors bidding on the project or undertaking the construction should, therefore, make their own interpretations of the factual information in this report and draw their own conclusions as to how the subsurface conditions may affect their bid or work.

Furthermore, this report was prepared by Arcadis for Z.V. Holdings Corporation. The material in it reflects the best judgement of Arcadis based on the information available at the time of preparation, Sept./Oct. 2022. Changes to soil and/or groundwater quality in the areas investigated can occur following the date of testing. Any use which a third party makes of the report, or reliance on, or decisions to be based on it, is the responsibility of such third parties. Arcadis accepts no liability, whether in negligence, contract or arising on any other basis for damages or from indemnification arising from decisions or actions by others based on this report. Please note that the recommendations provided in this report are intended solely for the preliminary planning of this development. Further geotechnical investigation will be required before detailed geotechnical parameters can be established.

Tables



Table 1Elevations Summary

Borehole Number	Borehole Co-ordinates Number		Ground Surface Elevation	Borehole Depth (mbgs)	Borehole Base Elevation	Depth to Well Screen (mbgs)	Well Screen Elevation	Depth to bedrock (mbgs)	Bedrock Elevation (local)
	Ν	E	(local)		(local)	(11083)	(iocal)		
BH22-2	45°20.011'	075°43.315'	98.98	5.18	93.80	2.13	96.85		
BH22-3	45°19.988'	075°43.303'	98.96	5.18	93.78				
BH22-4	45°19.976'	075°43.332'	98.97	5.18	93.79	2.13	96.84		
BH22-5	45°19.996'	075°43.338'	98.81	5.18	93.63				
BH22-6	45°19.968'	075°43.324'	99.04	5.61	93.43	2.56	96.48		
BH22-7	45°19.947'	075°43.306'	99.86	5.18	94.68				
BH22-8	45°19.934'	075°43.335'	99.48	5.18	94.30				
BH22-9	45°19.957'	075°43.351'	99.15	5.18	93.97				
BH22-10	45°19.952'	075°43.306'	99.86	10.67	89.19			10.67	89.19

Notes: - All screen intervals are 3.05m. Elevation given is the top of the screen.

- Bedrock was not proved during this investigation, depth given is the inferred bedrock surface.

- A local datum was used, with the catchbasin present at the northwestern corner given as 100.00m elevation.



Borehole / MW Number	Ground Surface Elevation (m)	Depth to Water (m) 2022.10.11	Water Elevation (m) 2022.10.11
BH22-2	98.98	4.85	94.13
BH22-4	98.97	dry	
BH22-6	98.04	dry	

Notes: - Water levels were measured using an oil-water interface probe.



Table 3Grain Size Analyses Results

Borehole Number	Sample	Gravel	Sand	Silt	Clay	Classification
BH22-3	2	0%	67%	30%	3%	Silty SAND, fine grained.
BH22-4	2	0%	69%	27%	4%	Silty SAND, fine grained.
BH22-5	2	0%	47%	46%	6%	SAND-SILT, trace clay.
BH22-6	2	0%	78%	18%	4%	SAND, fine-grained, some silt.
BH22-7	5	0%	84%	15%	1%	SAND, fine-grained, some silt.
BH22-10	2	0%	38%	56%	6%	SAND-SILT, trace clay.

Notes: - Grain size analyses were performed by ALS.

- Laboratory certificates are provided in the report appendices.

Table 4Results of Corrosivity Suite Analyses



Borehole Number	Sample	Depth (mbgs)	Sulphide (µg/g)	Chloride (20:1) (µg/g)	Sulphate (20:1) (µg/g)	pH (pH units)	Electrical Conductivity (µS/cm)	Resistivity (ohm.cm)	Redox Potential (mV)
BH22-3	2	1.80	<20	30	<20	7.54	202	4950	486
BH22-5	3	1.80	<20	41	<20	7.52	194	5150	457
BH22-6	3	1.80	<20	<5	<20	6.63	40.2	24900	409

Notes: - Chloride and Sulphate were determined on the extract obtained from the 20:1 leaching procedure.

- All tests were performed by ALS, a CALA accredited laboratory.

- Laboratory certificates are provided in the report appendices.





	-		
NW SW S SE		SITE BOUNDARY LOT LINES PROPOSED BUILDI	NG FOOTPRINT
2			
	15 Title:	0 0 1:800 KEY PLAN	15 30
34	Project: 1881 & 18 Client:	GEOTECHNICAL INVEST 883 MERIVALE RD and 6 8 OTTAWA, ONTAR Z.V.HOLDINGS	GATION 12 JAMIE AVENUE IO CORP. Date: Octobor 2022
C		RCADIS	FIGURE 1

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N	LEGEND				
W SW SE E		SITE BOUNDARY			
		LOT LINES			
de l	\oplus	BOREHOLE LOCAT	ION		
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ne.	Title: BOREHOLE LOCATION PLAN				
	Project: GEOTECHNICAL INVESTIGATION 1881 & 1883 MERIVALE RD and 6 & 12 JAMIE AVENUE				
5	OTTAWA, ONTARIO Client: Z.V.HOLDINGS CORP.				
State .			Date: October 2022		
Contraction of the	A	RCADIS	FIGURE 2		

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	LEGEND ↓ (4.81)	SITE BOUNDARY LOT LINES BOREHOLE LOCAT MONITORING WELL GROUNDWATER T/ (OCTOBER 2019)	ION L LOCATION ABLE DEPTH	
		10 0 Metres 10 1 1.750	10 20	
1	Title: GROUNDWATER TABLE DEPTHS (OCTOBER 2019)			
N.C.F.	Project: GEOTECHNICAL INVESTIGATION 1881 & 1883 MERIVALE RD and 6 & 12 JAMIE AVENUE OTTAWA, ONTARIO			
-	Client: Z.V.HOLDINGS CORP.			
			Date: October 2022	
STALLY -	A	RCADIS	FIGURE 3	


Borehole Logs

Lc	go	Arcadis Canada Inc. 1050 Morrison Drive, Suite 201 Ottawa, ON Telephone: 613-721-0555			BC	DRIN	NG NUN	MBE	ER E	3H2	2-2	(M) PAC	N22 6E 1	2-2) OF 1
CLIEN	T ZV	Holdings	PRO.	ECT	NAN	/IE _1	881-1883 M	erivale	Geote	ech				
PROJ	ECT NI	JMBER _ 30127480	PRO.	ЕСТ	LOC	CATIO	N _1881 Me	rivale l	Road,	Ottawa	a, ON			
DATE	STAR	COMPLETED 22-9-15	GROUND	ELE	VAT	ION _	98.98 m	ł	HOLE	SIZE	15cm	1		
DRILL	ING CO	DNTRACTOR Downing Estate Drilling	GROUND	WA.	TER	LEVE	LS:							
DRILL	ING M	ETHOD HSA	AT	тім	e of	DRIL	LING							
LOGO	GED BY	LDeGroot CHECKED BY RJanzen		ENC	O OF	DRILL	.ING							
NOTE	s		⊥¥ AF	TER	DRIL	LING	4.85 m / E	lev 94	.13 m					
DEPTH (m)	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE	NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (kPa)	DRY UNIT WT. (Mg/m ³)	MOISTURE CONTENT (%)	LIQUID LIMIT	LERBE LIMIT LIMIT LIMIT		FINES (%)
		WELL GRADED GRAVEL, SANDY, light gray, angular, fine t grained, dry, very dense (GRAVEL FILL) SILTY SAND, light brown, fine grained, moist, loose to mediu dense, trace gravel	o coarse		SS 1	50	35-55-25-12 (80)							
				\mathbb{N}	SS 2	75	8-8-9-10 (17)			8				
				\mathbb{N}	SS 3	67	4-5-4-50 (9)			3				
2		Sand becomes fine to coarse			SS 4	92	5-5-4-11 (9)			3	-			
- ·		Colour becomes brown to grey			SS 5	83	6-8-9-9 (17)			8				
		Becomes wet ⊈		\mathbb{N}	SS 6	50	3-7-9-12 (16)			6				
	·	Bottom of borehole at 5.20 meters.		<u> </u>										



Borehole Logs

Lc	go	Arcadis Canada Inc. 1050 Morrison Drive, Suite 201 Ottawa, ON Telephone: 613-721-0555			BC	DRIN	NG NUN	MBE	ER E	3H2	2-2	(M) PAC	N22 6E 1	2-2) OF 1
CLIEN	T ZV	Holdings	PRO.	ECT	NAN	/IE _1	881-1883 M	erivale	Geote	ech				
PROJ	ECT NI	JMBER _ 30127480	PRO.	ЕСТ	LOC	CATIO	N _1881 Me	rivale l	Road,	Ottawa	a, ON			
DATE	STAR	COMPLETED 22-9-15	GROUND	ELE	VAT	ION _	98.98 m	ł	HOLE	SIZE	15cm	1		
DRILL	ING CO	DNTRACTOR Downing Estate Drilling	GROUND	WA.	TER	LEVE	LS:							
DRILL	ING M	ETHOD HSA	AT	тім	e of	DRIL	LING							
LOGO	GED BY	LDeGroot CHECKED BY RJanzen		ENC	O OF	DRILL	.ING							
NOTE	s		⊥¥ AF	TER	DRIL	LING	4.85 m / E	lev 94	.13 m					
DEPTH (m)	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE	NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (kPa)	DRY UNIT WT. (Mg/m ³)	MOISTURE CONTENT (%)	LIQUID LIMIT	LERBE LIMIT LIMIT LIMIT		FINES (%)
		WELL GRADED GRAVEL, SANDY, light gray, angular, fine t grained, dry, very dense (GRAVEL FILL) SILTY SAND, light brown, fine grained, moist, loose to mediu dense, trace gravel	o coarse		SS 1	50	35-55-25-12 (80)							
				\mathbb{N}	SS 2	75	8-8-9-10 (17)			8				
				\mathbb{N}	SS 3	67	4-5-4-50 (9)			3				
2		Sand becomes fine to coarse			SS 4	92	5-5-4-11 (9)			3	-			
- ·		Colour becomes brown to grey			SS 5	83	6-8-9-9 (17)			8				
		Becomes wet ⊈		\mathbb{N}	SS 6	50	3-7-9-12 (16)			6				
	·	Bottom of borehole at 5.20 meters.		<u> </u>										

Lo	go	Arcadis Canada Inc. 1050 Morrison Drive, Suite 201 Ottawa, ON Telephone: 613-721-0555					BC	DRIN	IG I	NUN	ЛВЕ	PAC	3 H2 5E 1	2-3 OF 1
CLIEN	IT _ZV	Holdings	PROJ	EC.		ME _1	<u>881-1883 M</u>	erivale	Geote	ech				
PROJ	ECT NI	JMBER	PROJ	EC.		CATIO	N <u>1881 Me</u>	rivale	Road,	Ottawa	a, ON			
DATE	STAR	TED 22-9-16 COMPLETED 22-9-16	GROUND	EL	EVAT	ION _	98.96 m	I	HOLE	SIZE	15cm	۱		
DRILL	ING CO	DNTRACTOR Downing Estate Drilling	GROUND	WA	TER	LEVE	LS:							
DRILL	ING MI	ETHOD HSA	AT	TIN	ie of	DRIL	LING							
LOGO	GED BY	LDeGroot CHECKED BY RJanzen	AT	EN	d of	DRILL	_ING							
NOTE	S		AF	TEF	R DRII	LLING								
DEPTH (m)	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPI E TVDE	NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (kPa)	DRY UNIT WT. (Mg/m ³)	MOISTURE CONTENT (%)	TA LIMIT	LERBE LIMIT LIMIT LIMIT		FINES (%)
		WELL GRADED GRAVEL, SANDY, light gray, angular, fine t grained, dry, loose to medium dense some dark brown topsoi (GRAVEL FILL)	o coarse I	\mathbb{N}	SS 0	75	18-12-6-2 (18)							
					SS 1	75	2-2-5-3 (7)			6				
		SILTY SAND, light brown, fine grained, moist, medium dense gravel	e, trace	\mathbb{N}	SS 2	75	6-8-10-10 (18)			10				33
2		Colour becomes light grey		\mathbb{N}	SS 3	75	4-7-8-6 (15)			8				
				\mathbb{N}	SS 4	75	4-8-8-10 (16)			14				
4														
		Becomes wet		\mathbb{N}	SS 5	75	6-9-6-7 (15)	-						
		Bottom of borehole at 5.20 meters.				·		<u>.</u>	·		<u>.</u>	·		<u>.</u>

L	_0	go	Arcadis Canada Inc. 1050 Morrison Drive, Suite 201 Ottawa, ON Telephone: 613-721-0555			BC	DRII	ng nui	MBE	ERI	BH2	2-4	PAC	N22 ∋∈1 (2-4) OF 1
CL	IEN'	T_Z∖	/ Holdings	PRO	JEC		ME _1	881-1883 M	erivale	e Geote	ech				
PR	OJE		JMBER _ 30127480	PRO	JEC	TLO	CATIO	N <u>1881 Me</u>	rivale	Road,	Ottawa	a, ON			
DA	TE	STAR	TED _22-9-15 COMPLETED _22-9-15	GROUNE) EL	EVA1		98.97 m		HOLE	SIZE	15cm	า		
DR		NG C	ONTRACTOR Downing Estate Drilling	GROUNE	w	ATER	LEVE	LS:							
DR		NG M	ETHOD HSA	AT	TI	ME OF	- DRIL	LING							
LO	GG	ED BY	LDeGroot CHECKED BY RJanzen	A	EN	ID OF	DRILI	ING							
NO	TES	s		AF	ΤE	r Dri	LLING								
DEPTH	(m)	GRAPHIC LOG	MATERIAL DESCRIPTION			SAMPLE IYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (kPa)	DRY UNIT WT. (Mg/m ³)	MOISTURE CONTENT (%)	AT LIMIT LIMIT	LIMITS LIMITS LIMIT LIMIT		FINES (%)
-			ORGANIC SOIL WITH SAND, dark brown, medium to coarse grained, moist, very loose, some organics, and roots (TOPSO	: IL)		SS 0	50	1-1-1-1 (2)			10				
1			SILTY SAND, light brown, fine grained, moist, medium dense gravel	, trace	$\left \right\rangle$	SS 1	58	5-11-13-16 (24)			5				31
-						SS 2	25	5-11-11-11 (22)			5				
1.GDT 22-11-22	2		Becomes wet at 2 5mbos			SS 3	5000	4-7-9-8 (16)			3	-			
STD CANADA LAB	3					SS 4	92	6-8-7-7 (15)			14	-			
	- - -														
S 3012 7480 1881 MERIVAL GE	-		Becomes light grey, wet and fine to medium grained			SS 5	83	4-12-13-16 (25)							
GEOLECH BH COLUM			Bottom of borehole at 5.20 meters.												

	ogo	Arcadis Canada Inc. 1050 Morrison Drive, Suite 201 Ottawa, ON					BC	RIN	IG I	NUN	/ BE	PAC	3 H2 : ∋∈ 1 0	2-5 OF 1
	U	Telephone: 613-721-0555												
CLIE	NT _ Z\	/ Holdings	PROJ	EC	T NAI	ME _1	881-1883 M	erivale	Geote	ech				
PRO	JECT N	UMBER _30127480	PROJ	EC	T LOO		N <u>1881 Me</u>	rivale l	Road,	Ottawa	a, ON			
DAT		TED 22-9-16 COMPLETED 22-9-16	GROUND	EL	EVAT	'ION _	<u>98.81 m</u>	ł	HOLE	SIZE	15cm	1		
DRIL	LING C	ONTRACTOR Downing Estate Drilling	GROUND	w/	ATER	LEVE	LS:							
			AI				LING							
NOT	GED BI	LDegroot CHECKED BY KJanzen		EN	ID OF		_ING							
			Ar						1					
DEPTH (m)	GRAPHIC LOG	MATERIAL DESCRIPTION			SAMPLE 17FE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (kPa)	DRY UNIT WT. (Mg/m ³)	MOISTURE CONTENT (%)		LERBE LIMIT LIMIT LIMIT		FINES (%)
-		WELL GRADED GRAVEL, SANDY, light gray, angular, fine t grained, dry, medium dense (GRAVEL FILL)	to coarse	\mathbb{N}	SS 1	50	18-4-7-7 (11)							
- 1		SILT WITH SAND, dark brown to black, well graded, fine to c grained, moist, loose to medium dense, some organics, trace pockets of organic material	oarse clay	\mathbb{N}	SS 2	67	7-7-7-7 (14)			14				52
-					SS 3	50	5-5-5-5 (10)			17				
2		SILTY SAND, light gray to brown, fine grained, moist, mediun trace gravel	n dense,	\mathbb{N}	SS 4	83	6-12-14-10 (26)			5				
		Colour becomes only grey		\mathbb{N}	SS 5	92	7-10-13-14 (23)			4				
1 001/2100 00 5		Becomes wet at 4.5mbgs		\mathbb{N}	SS 6	75	7-12-14-14 (26)			5				
		Bottom of borehole at 5.20 meters.												

Lo	go	Arcadis Canada Inc. 1050 Morrison Drive, Suite 201 Ottawa, ON Telephone: 613-721-0555			БС	JRII	NG NUI	VIB	=R I	382	2-0	PAC	GE 1	2-6) OF 1
CLIEN	IT _ZV	Holdings	PRO	JEC		ME _1	1881-1883 M	erivale	e Geote	ech				
PROJ	ECT NU	JMBER _ 30127480	PRO	JEC	T LOO	CATIO	N <u>1881 Me</u>	rivale	Road,	Ottawa	a, ON			
DATE	STAR	COMPLETED 22-9-15	GROUNE) EL	EVAT		99.04 m	I	HOLE	SIZE	15cm	۱		
DRILL	ING CO	DNTRACTOR Downing Estate Drilling	GROUNE	w	ATER	LEVE	LS:							
DRILL	ING M	ETHOD HSA	AT	TI	NE OF	DRIL	LING							
LOGG	ED BY	LDeGroot CHECKED BY RJanzen	A	EN	id of	DRILI	LING							
NOTE	s		AF	TE	r Drii	LLING	i <u></u>							
E_	с НС				- Н К П П	:RY % О)	UE) UE)	PEN.	т WT. ³)	URE IT (%)	AT	TERBE LIMITS	RG }	S.
DEP1 (m)	GRAPI	MATERIAL DESCRIPTION			SAMPLE NUMB	RECOVE (RQI	BLO' COUN (N VAL	POCKET (kPa	DRY UNI (Mg/n	MOISTI	LIQUID	PLASTIC LIMIT	PLASTICIT INDEX	FINE (%)
		ORGANIC SOIL WITH SAND, light brown, well graded, fine to grained, moist, very loose, some organics, trace roots and gra debris (TOPSOIL)	o coarse ss	X	SS 1	50	1-1-2-2 (3)			12				
 		POORLY GRADED SAND, light gray, fine grained, moist, loos medium dense, some silt	se to		SS 2	75	6-10-12-11 (22)			5				
 				\mathbb{N}	SS 3	100	4-8-9-8 (17)			6				22
2					SS 4	67	3-5-5-5 (10)			11				
 _ 3		Becoming wet at 2.8mbgs			SS 5	67	3-3-7-6 (10)			19				
 4 														
 5 -					SS 6	83	6-15-18-21 (33)							
		Define of hereinstein at 5.04 meters												
		Bottom of borehole at 5.61 meters.												

L	.og	0	Arcadis Canada Inc. 1050 Morrison Drive, Suite 201 Ottawa, ON					BC	RIN	IG I	NUN	/IBE	PAC	3H2 5E 1	2-7 OF 1
			Telephone: 613-721-0555	PPO	EC			001 1002 M	orivolo	Coot	a ah				
		<u></u> T NII	INGER 30127480	PROJ			יים שוע העדור	N 1881 Ma	rivale	Road					
			ED 22.0.15 COMPLETED 22.0.15					00.96 m				<u>15 or</u>			
	1 E 31		ED <u>22-9-13</u> COMPLETED <u>22-9-13</u>	GROUND				99.00 m	'	IOLE	SIZE	TOCH	1		
				GROUND	VV/										
				A1 AT			י וופח								
		, DI				יוס טי וופח כ									
DEPTH	GRAPHIC	DOL	MATERIAL DESCRIPTION			NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (kPa)	DRY UNIT WT. (Mg/m ³)	MOISTURE CONTENT (%)	AT LIMIT	LERBE LIMITS LIMIT LIMIT		FINES (%)
-		<u>x</u>	ORGANIC SOIL WITH SAND, light brown to black, well grade to coarse grained, moist, loose, some organics, trace gravel (TOPSOIL)	ed, fine	\mathbb{N}	SS 1	50	1-2-2-1 (4)			11				
1			POORLY GRADED SAND, light brown, fine grained, moist, n dense, some silt	nedium	\mathbb{N}	SS 2	75	4-7-10-8 (17)			6				
-					\mathbb{N}	SS 3	92	3-7-8-9 (15)			6				
2					\mathbb{N}	SS 4	83	4-8-10-13 (18)			5				
			WELL GRADED SAND, light brown, fine to coarse grained, n medium dense to dense, some silt	noist,	\mathbb{N}	SS 5	83	7-12-11-10 (23)			5				16
			Colour becomes light grey		\mathbb{N}	SS 6	67	4-17-21-16 (38)							
			Bottom of borehole at 5.20 meters.		/ \										
GEOLECH BH COLU															

Lc	ogo	Arcadis Canada Inc. 1050 Morrison Drive, Suite 201 Ottawa, ON Telephone: 613-721-0555					BC	RIN	NG I	NUN	/IBE	PAC	3H2 5E 1	2-8 OF 1
CLIEN	NT ZV	/ Holdings	PROJ	EC.		ME _1	<u>881-1883 M</u>	erivale	Geote	ech				
PROJ	ECT NI	JMBER	PROJ	EC.	T LOO	CATIO	N <u>1881 Me</u>	rivale	Road,	Ottawa	a, ON			
DATE	STAR	TED 22-9-16 COMPLETED 22-9-16	GROUND	ELI	EVAT	ION _	99.48 m	I	HOLE	SIZE	15cm	1		
DRILL	-ING CO	DOWNING Estate Drilling	GROUND	WA	TER	LEVE	LS:							
DRILL		ETHOD HSA	AT	TIN			LING							
	GED BY S	LDeGroot CHECKED BY RJanzen	AT AF	EN TFF			_ING							
HTH (m)	APHIC OG	MATERIAL DESCRIPTION		I E TVDE	MBER L	VERY % (QD)	-OW UNTS ALUE)	ET PEN. (Pa)	JNIT WT. g/m ³)	STURE ENT (%)	AT		RG ≻LIX	NES (%)
	GR			CAMPI	NUN	RECO (R	(N < OI	POCK	DRY L (M	MOIS	LIQUIT	PLASTI	PLASTIC	Ē
		WELL GRADED GRAVEL, SANDY, light gray, angular, fine t grained, dry, loose (GRAVEL FILL)	to coarse	X	SS 1	33	11-3-1-2 (4)							
- ·		WELL GRADED SAND, brown, fine to coarse grained, loose FILL)	(SAND		SS 2	92	5-3-2-4 (5)			8				
		SILTY SAND, brown, medium to coarse grained, moist, medi dense	ium		SS 3	83	3-9-11-11 (20)			7				
2		Sand becomes fine, colour becomes grey			SS 4	75	4-8-9-11 (17)			4				
					SS 5	83	5-11-11-10 (22)			9				
5		Colour becomes dark grey		\mathbb{N}	SS 6	83	6-12-13-9 (25)							
		Bottom of borehole at 5.20 meters.												

	Lo	go	Arcadis Canada Inc. 1050 Morrison Drive, Suite 201 Ottawa, ON					BC	RIN	IG I	NUN	/ BE	PAC	3H2 5E 1 (2-9 OF 1
			Telephone: 613-721-0555	000		-		004 4000 M		Cent					
	LIEN RO II		Holdings	PRO	IEC		ME _1	<u>881-1883 M</u> N 1881 Me	erivale	e Geote Road	ech Ottawa				
		STAR	COMPLETED 22-9-16	GROUND	FI	FVAT		99 15 m		HOLF	SIZE	15cm			
	RILL	ING CO	DNTRACTOR Downing Estate Drilling	GROUND	w	ATER	LEVE	LS:	_ '	IULL		10011	•		
D	RILL	ING MI	ETHOD HSA	AT	TIN	/IE OF	DRIL	LING							
	OGG	ED BY	LDeGroot CHECKED BY RJanzen	AT	EN	d of	DRILI	_ING							
N	OTE	s		AF	TE	r Drii	LLING								
7	E	с П				- H - H - H	RY %))	V TS UE)	PEN.	т WT. 1 ³)	JRE T (%)	AT	TERBE LIMITS	RG ≻	S
	(m)	GRAP	MATERIAL DESCRIPTION			NUMBI	RECOVE (RQE	BLOV COUN (N VAL	POCKET (kPa	DRY UNI' (Mg/m	MOISTU	LIQUID	PLASTIC LIMIT	PLASTICIT INDEX	FINE (%)
-	-		ORGANIC SOIL WITH SAND, light brown to black, well grade to coarse grained, moist, very loose, some organics, trace gra (TOPSOIL)	ed, fine vel	\mathbb{N}	SS 1	83	1-1-2-1 (3)			16				
-	- 1		SILTY SAND, dark brown to light gray, fine grained, moist, me dense	edium		SS 2	92	4-9-12-11 (21)			8	-			
-	-		Colour become grey		\mathbb{N}	SS 3	92	6-10-15-13 (25)			9	-			
27-11-22 10	2		Coarse sand lenses		\mathbb{N}	SS 4	100	5-9-10-9 (19)			8				
					\mathbb{N}	SS 5	100	4-10-12-15 (22)			6				
	-														
	4														
3012/480 1001 14151	- - 5		Sand becomes fine to coarse			SS 6	75	5-8-11-10 (19)							
		<u>µ. 1 </u>	Bottom of borehole at 5.20 meters.		<u>/ </u>		1	1							

Lo	go	Arcadis Canada Inc. 1050 Morrison Drive, Suite 201 Ottawa, ON Telephone: 613-721-0555				BOF	RINC	g N	UMI	BEF	R BI PAC	H22 GE 1	- 10 OF 1
CLIEN	T_ZV	/ Holdings	PRO	JECT NA	ME _1	881-1883 M	lerival	e Geo	tech				
PROJ		UMBER _ 30127480	PRO	JECT LO	CATIO	N <u>1881 Me</u>	erivale	Road	, Ottav	va, ON	١		
DATE	STAR	TED 22-9-16 COMPLETED 22-9-16	GROUNE	ELEVAT		99.86 m	I	HOLE	SIZE	15cn	n		
DRILL	ING C	ONTRACTOR Downing Estate Drilling	GROUNE	WATER	LEVE	LS:							
DRILL	ING M	ETHOD HSA	AT		DRIL	LING							
LOGG	ED BY	LDeGroot CHECKED BY RJanzen	AT	END OF	DRILI	ING							
NOTE	s		AF	TER DRI	LLING								
DEPTH (m)	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (kPa)	DRY UNIT WT. (Mg/m ³)	MOISTURE CONTENT (%)	TA FIGUID FIMIT	LERBE LIMIT LIMIT		FINES (%)
	<u>17</u> 77 77 77 77	ORGANIC SOIL WITH SAND, dark brown to black, well gra fine to coarse grained, moist, very loose, some organics, tra roots (TOPSOIL)	aded, ace	SS 0	33	1-1-1-1 (2)							
		SILT WITH SAND, light gray, fine grained, moist, loose to r dense	nedium	SS 1	67	1-1-8-14 (9)			14				
				SS 2	83	5-10-9-10 (19)			12				
2		Some mottling visible			50	9-9-9-11 (18)			15				62
				SS 4	67	5-13-12-12 (25)			2	_			
 - 4		Trace gravel, mottled texture											
				5	75	(22)							
		SPT cone test begins at 5.18mbgs.		SPT		7-8-18-18 (26)							
6				SPT		17-17-17- 18 (34)							
				SPT		18-19-23- 23 (42)							
				SPT		22-23-22- 23 (45)							
8				SPT		14-15-10-9 (25)							
				SPT		(30)							
				SPT		29 (51) 26-26-27							
10				SPT		20-20-27- 28 (53) 27-27-18-							
		Borehole ends.		SPT		18 (45)							
		Bottom of borehole at 10.67 meters.											



Photo Log



Project Photographs

Preliminary Geotechnical Investigation - 1881/1883 Merivale and Adjacent Lot, Ottawa, ON



Photo: 1

Date: 16 September 2022

Description:

View of the drilling of borehole location MW22-6 at the northeast portion of the 6/12 Jamie Avenue bus parking lot. Looking northeast.



Photo: 2

Date: 16 September 2022

Description:

View of the drilling of borehole location BH22-5 at the southwest portion the 6/12 Jamie Avenue bus parking lot. Looking northeast.



Project Photographs

Preliminary Geotechnical Investigation - 1881/1883 Merivale and Adjacent Lot, Ottawa, ON



Photo: 3

Date: 16 September 2022

Description:

View of the drilling of borehole location BH22-8 at the southwest portion of 1881 Merivale Road, looking northeast. The scuba divers' warehouse is visible.

Photo: 4

Date: 16 September 2022

Description:

View of the drilling of borehole location MW22-4 at the northern portion of 1881 Merivale Road, looking north.





Project Photographs

Preliminary Geotechnical Investigation - 1881/1883 Merivale and Adjacent Lot, Ottawa, ON



Photo: 5

Date: 16 September 2022

Description:

View of a split spoon containing the typical light brown fine sand observed at most areas on the property.



Laboratory Certificates of Analysis

ALS Canada Ltd.



	CERTIFICATE OF ANALYSIS										
Work Order	: WT2214822	Page	: 1 of 10								
Amendment	: 1										
Client	: Arcadis Canada Inc.	Laboratory	: Waterloo - Environmental								
Contact	: Lennart DeGroot	Account Manager	: Emily Smith								
Address	: 1050 Morrison Drive Suite 201	Address	: 60 Northland Road, Unit 1								
	Ottawa ON Canada K2H 1L1		Waterloo ON Canada N2V 2B8								
Telephone	: 613 721 0555	Telephone	: +1 519 886 6910								
Project	: 30127480	Date Samples Received	: 19-Sep-2022 14:55								
PO		Date Analysis Commenced	: 21-Sep-2022								
C-O-C number	:	Issue Date	: 31-Oct-2022 10:15								
Sampler	:										
Site											
Quote number	: Waterloo 2022 Price List										
No. of samples received	: 42										
No. of samples analysed	: 42										

This report supersedes any previous report(s) with this reference. Results apply to the sample(s) as submitted. This document shall not be reproduced, except in full.

This Certificate of Analysis contains the following information:

- General Comments
- Analytical Results

Additional information pertinent to this report will be found in the following separate attachments: Quality Control Report, QC Interpretive report to assist with Quality Review and Sample Receipt Notification (SRN).

Signatories

This document has been electronically signed by the authorized signatories below. Electronic signing is conducted in accordance with US FDA 21 CFR Part 11.

Signatories	Position	Laboratory Department
Amanda Ganouri-Lumsden	Department Manager - Microbiology and Prep	Centralized Prep, Waterloo, Ontario
Hedy Lai	Team Leader - Inorganics	Inorganics, Saskatoon, Saskatchewan
Hedy Lai	Team Leader - Inorganics	Sask Soils, Saskatoon, Saskatchewan
Jon Fisher	Department Manager - Inorganics	Inorganics, Waterloo, Ontario
Joseph Scharbach		Centralized Prep, Waterloo, Ontario
Niral Patel		Centralized Prep, Waterloo, Ontario



General Comments

The analytical methods used by ALS are developed using internationally recognized reference methods (where available), such as those published by US EPA, APHA Standard Methods, ASTM, ISO, Environment Canada, BC MOE, and Ontario MOE. Refer to the ALS Quality Control Interpretive report (QCI) for applicable references and methodology summaries. Reference methods may incorporate modifications to improve performance.

Where a reported less than (<) result is higher than the LOR, this may be due to primary sample extract/digestate dilution and/or insufficient sample for analysis.

Where the LOR of a reported result differs from standard LOR, this may be due to high moisture content, insufficient sample (reduced weight employed) or matrix interference. Please refer to Quality Control Interpretive report (QCI) for information regarding Holding Time compliance.

Key : CAS Number: Chemical Abstracts Services number is a unique identifier assigned to discrete substances LOR: Limit of Reporting (detection limit).

Unit	Description
-	No Unit
%	percent
μS/cm	Microsiemens per centimetre
mg/kg	milligrams per kilogram
mV	millivolts
ohm cm	ohm centimetre (resistivity)
pH units	pH units

<: less than.

>: greater than.

Surrogate: An analyte that is similar in behavior to target analyte(s), but that does not occur naturally in environmental samples. For applicable tests, surrogates are added to samples prior to analysis as a check on recovery.

Test results reported relate only to the samples as received by the laboratory.

UNLESS OTHERWISE STATED on SRN or QCI Report, ALL SAMPLES WERE RECEIVED IN ACCEPTABLE CONDITION.

Sample Comments

Sample	Client Id	Comment
WT2214822-007	BH22-3-2	Sample(s) XXX: Limited sample was available for PSA (100g minimum is standard). Measurement Uncertainty for PSA results may be higher than usual.
WT2214822-020	MW22-4-2	Sample(s) XXX: Limited sample was available for PSA (100g minimum is standard). Measurement Uncertainty for PSA results may be higher than usual.
WT2214822-025	BH22-5-2	Sample(s) XXX: Limited sample was available for PSA (100g minimum is standard). Measurement Uncertainty for PSA results may be higher than usual.
WT2214822-030	MW22-6-2	Sample(s) XXX: Limited sample was available for PSA (100g minimum is standard). Measurement Uncertainty for PSA results may be higher than usual.
WT2214822-038	BH22-7-5	Sample(s) XXX: Limited sample was available for PSA (100g minimum is standard). Measurement Uncertainty for PSA results may be higher than usual.

Page Work Order Client Project	:	3 of 10 WT2214822 Amendment 1 Arcadis Canada Inc. 30127480		ALS
WT2214	822-040	BH22-10-2	Sample(s) XXX: Limited sample was available for PSA (100g minimum is standard). Measurement Uncertainty for PSA results may be higher than usual.	



Sub-Matrix: Soil/Solid			Ci	lient sample ID	MW22-2-1	MW22-2-2	MW22-2-3	MW22-2-4	MW22-2-5
(Matrix: Soil/Solid)									
			Client samp	oling date / time	16-Sep-2022 09:00	16-Sep-2022 09:00	16-Sep-2022 09:00	16-Sep-2022 09:00	16-Sep-2022 09:00
Analyte	CAS Number	Method	LOR	Unit	WT2214822-001	WT2214822-002	WT2214822-003	WT2214822-004	WT2214822-005
					Result	Result	Result	Result	Result
Physical Tests									
moisture		E144	0.25	%	8.08	3.28	3.22	8.18	6.09

Please refer to the General Comments section for an explanation of any qualifiers detected.

Analytical Results

Sub-Matrix: Soil/Solid			Cli	ient sample ID	BH22-3-1	BH22-3-2	BH22-3-3	BH22-3-4	BH22-8-1
(Matrix: Soil/Solid)									
			Client samp	ling date / time	16-Sep-2022 12:00	16-Sep-2022 12:00	16-Sep-2022 12:00	16-Sep-2022 12:00	16-Sep-2022 14:00
Analyte	CAS Number	Method	LOR	Unit	WT2214822-006	WT2214822-007	WT2214822-008	WT2214822-009	WT2214822-010
					Result	Result	Result	Result	Result
Physical Tests									
conductivity (1:2 leachate)		E100-L	5.00	μS/cm		202			
moisture		E144	0.25	%	5.84	9.93	7.95	13.5	8.06
oxidation-reduction potential [ORP]		E125	0.10	mV		486			
pH (1:2 soil:CaCl2-aq)		E108A	0.10	pH units		7.54			
resistivity		EC100R	100	ohm cm		4950			
Particle Size									
passing (9.5 mm)		E181	1.0	%		100			
passing (4.75 mm)		E181	1.0	%		100			
passing (19 mm)		E181	1.0	%		100			
passing (25.4 mm)		E181	1.0	%		100			
passing (38.1 mm)		E181	1.0	%		100			
passing (50.8 mm)		E181	1.0	%		100			
passing (76.2 mm)		E181	1.0	%		100			
passing (1.0 mm)		E182	1.0	%		100			
passing (0.841 mm)		E182	1.0	%		100			
passing (0.50 mm)		E182	1.0	%		99.8			
passing (0.420 mm)		E182	1.0	%		99.7			



Sub-Matrix: Soil/Solid			Cl	ient sample ID	BH22-3-1	BH22-3-2	BH22-3-3	BH22-3-4	BH22-8-1
(Matrix: Soil/Solid)									
			Client samp	ling date / time	16-Sep-2022 12:00	16-Sep-2022 12:00	16-Sep-2022 12:00	16-Sep-2022 12:00	16-Sep-2022 14:00
Analyte	CAS Number	Method	LOR	Unit	WT2214822-006	WT2214822-007	WT2214822-008	WT2214822-009	WT2214822-010
					Result	Result	Result	Result	Result
Particle Size									
passing (0.250 mm)		E182	1.0	%		95.9			
passing (0.149 mm)		E182	1.0	%		75.6			
passing (0.125 mm)		E182	1.0	%		61.8			
passing (0.075 mm)		E182	1.0	%		33.1			
passing (0.063 mm)		E182	1.0	%		22.7			
passing (0.05 mm)		E182	1.0	%		13.4			
passing (0.0312 mm)		E183	1.0	%		7.8			
passing (0.020 mm)		E183	1.0	%		4.5			
passing (0.005 mm)		E183	1.0	%		3.4			
passing (0.004 mm)		E183	1.0	%		3.0			
passing (0.002 mm)		E183	1.0	%		2.2			
grain size curve		E185	-	-		See			
passing (2.0 mm)		E181	1.0	%		Attached 100			
Inorganic Parameters									
sulfides, acid volatile		E396-L	0.20	mg/kg		<0.20			
Leachable Anions & Nutrients									
chloride, soluble ion content	16887-00-6	E236.CI	5.0	mg/kg		29.8			
sulfate, soluble ion content	14808-79-8	E236.SO4	20	mg/kg		<20			



Sub-Matrix: Soil/Solid			CI	lient sample ID	BH22-8-2	BH22-8-3	BH22-8-4	BH22-9-1	BH22-9-2
(Matrix: Soil/Solid)									
			Client samp	oling date / time	16-Sep-2022 14:00	16-Sep-2022 14:00	16-Sep-2022 14:00	16-Sep-2022 13:00	16-Sep-2022 13:00
Analyte	CAS Number	Method	LOR	Unit	WT2214822-011	WT2214822-012	WT2214822-013	WT2214822-014	WT2214822-015
					Result	Result	Result	Result	Result
Physical Tests									
moisture		E144	0.25	%	7.19	4.09	8.75	15.9	7.82

Please refer to the General Comments section for an explanation of any qualifiers detected.

Analytical Results

Sub-Matrix: Soil/Solid			Cl	ient sample ID	BH22-9-3	BH22-9-4	BH22-9-5	MW22-4-1	MW22-4-2
(Matrix: Soil/Solid)									
			Client samp	ling date / time	16-Sep-2022 13:00	16-Sep-2022 13:00	16-Sep-2022 13:00	15-Sep-2022 15:45	15-Sep-2022 15:45
Analyte	CAS Number	Method	LOR	Unit	WT2214822-016	WT2214822-017	WT2214822-018	WT2214822-019	WT2214822-020
					Result	Result	Result	Result	Result
Physical Tests									
moisture		E144	0.25	%	9.34	7.60	6.48	10.1	4.59
Particle Size									
sand (>0.075mm)		E178	1.0	%					69.3
fines (<0.075mm)		E178	1.0	%					30.6
texture class		E178	-	-					Coarse



Sub-Matrix: Soil/Solid			Cl	ient sample ID	MW22-4-3	MW22-4-4	MW22-4-5	BH22-5-1	BH22-5-2
(Matrix: Soil/Solid)									
		Madaad	Client sampling date / time		15-Sep-2022 15:45	15-Sep-2022 15:45	15-Sep-2022 15:45	16-Sep-2022 08:50	16-Sep-2022 08:50
Analyte CAS N	umber	Method	LOR	Unit	W12214822-021	W12214822-022	W12214822-023	W12214822-024	W12214822-025
					Result	Result	Result	Result	Result
Physical lests		E144	0.25	0/	5.44	2.00	12.0	14.2	16.0
moisture		E 144	0.25	70	5.44	2.00	13.0	14.5	10.9
Particle Size		Elot	1.0	N					100
passing (9.5 mm)		E181	1.0	%					100
passing (4.75 mm)		E181	1.0	%					100
passing (19 mm)		E181	1.0	%					100
passing (25.4 mm)		E181	1.0	%					100
passing (38.1 mm)		E181	1.0	%					100
passing (50.8 mm)		E181	1.0	%					100
passing (76.2 mm)		E181	1.0	%					100
passing (1.0 mm)		E182	1.0	%					94.3
passing (0.841 mm)		E182	1.0	%					93.2
passing (0.50 mm)		E182	1.0	%					80.7
passing (0.420 mm)		E182	1.0	%					77.9
passing (0.250 mm)		E182	1.0	%					74.3
passing (0.149 mm)		E182	1.0	%					66.6
passing (0.125 mm)		E182	1.0	%					61.9
passing (0.075 mm)		E182	1.0	%					52.2
passing (0.063 mm)		E182	1.0	%					43.4
passing (0.05 mm)		E182	1.0	%					33.8
passing (0.0312 mm)		E183	1.0	%					21.5
passing (0.020 mm)		E183	1.0	%					14.9
passing (0.005 mm)		E183	1.0	%					6.4
passing (0.004 mm)		E183	1.0	%					5.7
passing (0.002 mm)		E183	1.0	%					4.8
grain size curve		E185	-	-					See Attached
passing (2.0 mm)		E181	1.0	%					99.4



Sub-Matrix: Soil/Solid			Cl	lient sample ID	BH22-5-3	BH22-5-4	BH22-5-5	MW22-6-1	MW22-6-2
(Matrix: Soil/Solid)									
			Client samp	ling date / time	16-Sep-2022 08:50	16-Sep-2022 08:50	16-Sep-2022 08:50	15-Sep-2022 11:15	15-Sep-2022 11:15
Analyte	CAS Number	Method	LOR	Unit	WT2214822-026	WT2214822-027	WT2214822-028	WT2214822-029	WT2214822-030
					Result	Result	Result	Result	Result
Physical Tests									
conductivity (1:2 leachate)		E100-L	5.00	µS/cm	194				
moisture		E144	0.25	%	4.82	4.42	5.22	11.9	5.34
oxidation-reduction potential [ORP]		E125	0.10	mV	457				
pH (1:2 soil:CaCl2-aq)		E108A	0.10	pH units	7.52				
resistivity		EC100R	100	ohm cm	5150				
Particle Size									
sand (>0.075mm)		E178	1.0	%					78.5
fines (<0.075mm)		E178	1.0	%					21.5
texture class		E178	-	-					Coarse
Inorganic Parameters									
sulfides, acid volatile		E396-L	0.20	mg/kg	<0.20				
Leachable Anions & Nutrients									
chloride, soluble ion content	16887-00-6	E236.CI	5.0	mg/kg	40.5				
sulfate, soluble ion content	14808-79-8	E236.SO4	20	mg/kg	<20				



Sub-Matrix: Soil/Solid			Cl	ient sample ID	MW22-6-3	MW22-6-4	MW22-6-5	BH22-7-1	BH22-7-2
(Matrix: Soil/Solid)									
Analyte CAS Number Method			Client sampling date / time		15-Sep-2022 11:15	15-Sep-2022 11:15	15-Sep-2022 11:15	15-Sep-2022 13:00	15-Sep-2022 13:00
Analyte	CAS Number	Method	LOR	Unit	WT2214822-031	WT2214822-032	WT2214822-033	WT2214822-034	WT2214822-035
					Result	Result	Result	Result	Result
Physical Tests									
conductivity (1:2 leachate)		E100-L	5.00	µS/cm	40.2				
moisture		E144	0.25	%	5.90	10.6	19.4	10.6	5.59
oxidation-reduction potential [ORP]		E125	0.10	mV	409				
pH (1:2 soil:CaCl2-aq)		E108A	0.10	pH units	6.63				
resistivity		EC100R	100	ohm cm	24900				
Inorganic Parameters									
sulfides, acid volatile		E396-L	0.20	mg/kg	<0.20				
Leachable Anions & Nutrients									
chloride, soluble ion content	16887-00-6	E236.CI	5.0	mg/kg	<5.0				
sulfate, soluble ion content	14808-79-8	E236.SO4	20	mg/kg	<20				

Please refer to the General Comments section for an explanation of any qualifiers detected.

Analytical Results

Sub-Matrix: Soil/Solid Client sample ID					BH22-7-3	BH22-7-4	BH22-7-5	BH22-10-1	BH22-10-2
(Matrix: Soil/Solid)									
		Client sampling date / time		15-Sep-2022 13:00	15-Sep-2022 13:00	15-Sep-2022 13:00	15-Sep-2022 14:10	15-Sep-2022 14:10	
Analyte	CAS Number	Method	LOR	Unit	WT2214822-036	WT2214822-037	WT2214822-038	WT2214822-039	WT2214822-040
					Result	Result	Result	Result	Result
Physical Tests									
moisture		E144	0.25	%	6.03	4.98	4.63	14.4	12.0
Particle Size									
sand (>0.075mm)		E178	1.0	%			83.9		38.1
fines (<0.075mm)		E178	1.0	%			16.1		61.9
texture class		E178	-	-			Coarse		Fine



Sub-Matrix: Soil/Solid	Client sample ID				BH22-10-3	BH22-10-4	 	
(Matrix: Soil/Solid)								
			Client samp	ling date / time	15-Sep-2022 14:10	15-Sep-2022 14:10	 	
Analyte	CAS Number	Method	LOR	Unit	WT2214822-041	WT2214822-042	 	
					Result	Result	 	
Physical Tests								
moisture		E144	0.25	%	14.6	1.99	 	



	QUALITY CONTROL INTERPRETIVE REPORT										
Work Order	:WT2214822	Page	: 1 of 15								
Amendment	:1										
Client	Arcadis Canada Inc.	Laboratory	: Waterloo - Environmental								
Contact	: Lennart DeGroot	Account Manager	: Emily Smith								
Address	: 1050 Morrison Drive Suite 201	Address	60 Northland Road, Unit 1								
	Ottawa ON Canada K2H 1L1		Waterloo, Ontario Canada N2V 2B8								
Telephone	613 721 0555	Telephone	: +1 519 886 6910								
Project	: 30127480	Date Samples Received	: 19-Sep-2022 14:55								
PO		Issue Date	: 31-Oct-2022 10:15								
C-O-C number	:										
Sampler	:										
Site											
Quote number	: Waterloo 2022 Price List										
No. of samples received	:42										
No. of samples analysed	:42										

This report is automatically generated by the ALS LIMS (Laboratory Information Management System) through evaluation of Quality Control (QC) results and other QA parameters associated with this submission, and is intended to facilitate rapid data validation by auditors or reviewers. The report highlights any exceptions and outliers to ALS Data Quality Objectives, provides holding time details and exceptions, summarizes QC sample frequencies, and lists applicable methodology references and summaries.

Key

Anonymous: Refers to samples which are not part of this work order, but which formed part of the QC process lot.

CAS Number: Chemical Abstracts Service number is a unique identifier assigned to discrete substances.

DQO: Data Quality Objective.

LOR: Limit of Reporting (detection limit).

RPD: Relative Percent Difference.

Workorder Comments

Holding times are displayed as "---" if no guidance exists from CCME, Canadian provinces, or broadly recognized international references.

Summary of Outliers Outliers : Quality Control Samples

- No Method Blank value outliers occur.
- No Duplicate outliers occur.
- No Laboratory Control Sample (LCS) outliers occur
- No Test sample Surrogate recovery outliers exist.

Outliers: Reference Material (RM) Samples

• No Reference Material (RM) Sample outliers occur.

Outliers : Analysis Holding Time Compliance (Breaches) <u>No</u> Analysis Holding Time Outliers exist.

Outliers : Frequency of Quality Control Samples • No Quality Control Sample Frequency Outliers occur.



Analysis Holding Time Compliance

This report summarizes extraction / preparation and analysis times and compares each with ALS recommended holding times, which are selected to meet known provincial and /or federal requirements. In the absence of regulatory hold times, ALS establishes recommendations based on guidelines published by organizations such as CCME, US EPA, APHA Standard Methods, ASTM, or Environment Canada (where available). Dates and holding times reported below represent the first dates of extraction or analysis. If subsequent tests or dilutions exceeded holding times, qualifiers are added (refer to COA).

If samples are identified below as having been analyzed or extracted outside of recommended holding times, measurement uncertainties may be increased, and this should be taken into consideration when interpreting results.

Where actual sampling date is not provided on the chain of custody, the date of receipt with time at 00:00 is used for calculation purposes.

Where only the sample date without time is provided on the chain of custody, the sampling date at 00:00 is used for calculation purposes.

Matrix: Soil/Solid					E١	aluation: × =	Holding time excee	edance ; 🔹		Holding Time
Analyte Group	Method	Sampling Date	Ext	raction / Pr	eparation		Analysis			
Container / Client Sample ID(s)			Preparation	Holding	g Times	Eval	Analysis Date	Holding Times		Eval
			Date	Rec	Actual			Rec	Actual	
Inorganic Parameters : Acid Volatile Sulfide in Soil by Colourimetry (0.2 mg/kg)										
Glass soil jar/Teflon lined cap BH22-3-2	E396-L	16-Sep-2022	21-Sep-2022	14 dave	5 days	~	21-Sep-2022	7 days	0 days	*
lucurania Devenatare : Acid Valatila Cultida in Cail hu: Calaurimater: (A.2 ma//re)				uays						
Glass soil jar/Teflon lined can										
BH22-5-3	E396-L	16-Sep-2022	21-Sep-2022	14 davs	5 days	*	21-Sep-2022	7 days	0 days	*
Inorganic Parameters : Acid Volatile Sulfide in Soil by Colourimetry (0.2 mg/kg)				,						
Glass soil jar/Teflon lined cap										
MW22-6-3	E396-L	15-Sep-2022	21-Sep-2022	14 days	6 days	~	21-Sep-2022	7 days	0 days	*
Leachable Anions & Nutrients : Water Extractable Chloride by IC										
Glass soil jar/Teflon lined cap BH22-3-2	E236.CI	16-Sep-2022	26-Sep-2022	30 days	10 days	✓	28-Sep-2022	28 days	2 days	*
Leachable Anions & Nutrients : Water Extractable Chloride by IC										
Glass soil jar/Teflon lined cap BH22-5-3	E236.CI	16-Sep-2022	26-Sep-2022	30 days	10 days	~	28-Sep-2022	28 days	2 days	4
Leachable Anions & Nutrients : Water Extractable Chloride by IC										
Glass soil jar/Teflon lined cap MW22-6-3	E236.CI	15-Sep-2022	26-Sep-2022	30 days	11 days	✓	28-Sep-2022	28 days	2 days	*
Leachable Anions & Nutrients : Water Extractable Sulfate by IC										
Glass soil jar/Teflon lined cap BH22-3-2	E236.SO4	16-Sep-2022	26-Sep-2022	30 days	10 days	✓	28-Sep-2022	28 days	2 days	*



Matrix: Soil/Solid					Ev	aluation: × =	Holding time exce	edance ; 🗸	<pre>< = Within</pre>	Holding Time
Analyte Group	Method	Sampling Date	Ext	raction / Pr	eparation			Analys	is	
Container / Client Sample ID(s)			Preparation Date	Holding Rec	g Times Actual	Eval	Analysis Date	Holding Rec	Times Actual	Eval
Leachable Anions & Nutrients : Water Extractable Sulfate by IC										
Glass soil jar/Teflon lined cap BH22-5-3	E236.SO4	16-Sep-2022	26-Sep-2022	30 days	10 days	✓	28-Sep-2022	28 days	2 days	✓
Leachable Anions & Nutrients : Water Extractable Sulfate by IC										
Glass soil jar/Teflon lined cap MW22-6-3	E236.SO4	15-Sep-2022	26-Sep-2022	30 days	11 days	√	28-Sep-2022	28 days	2 days	√
Particle Size : CCME fine/coarse Particle Size Analysis by wet sieve										
Glass soil jar/Teflon lined cap BH22-10-2	E178	15-Sep-2022					30-Sep-2022	180 days	15 days	✓
Particle Size : CCME fine/coarse Particle Size Analysis by wet sieve										
Glass soil jar/Teflon lined cap BH22-7-5	E178	15-Sep-2022					30-Sep-2022	180 days	15 days	✓
Particle Size : CCME fine/coarse Particle Size Analysis by wet sieve										
Glass soil jar/Teflon lined cap MW22-4-2	E178	15-Sep-2022					30-Sep-2022	180 days	15 days	✓
Particle Size : CCME fine/coarse Particle Size Analysis by wet sieve										
Glass soil jar/Teflon lined cap MW22-6-2	E178	15-Sep-2022					30-Sep-2022	180 days	15 days	√
Particle Size : Grain Size Report (Attachment) Hydrometer/Sieve Method										
Glass soil jar/Teflon lined cap BH22-3-2	E185	16-Sep-2022					29-Sep-2022			
Particle Size : Grain Size Report (Attachment) Hydrometer/Sieve Method										
Glass soil jar/Teflon lined cap BH22-5-2	E185	16-Sep-2022					29-Sep-2022			
Particle Size : Particle Size Analysis - Hydrometer										
Glass soil jar/Teflon lined cap BH22-3-2	E183	16-Sep-2022	23-Sep-2022				23-Sep-2022	365 days	7 days	✓



Matrix: Soil/Solid					Ev	aluation: × =	Holding time excee	edance ; 🖌	<pre>/ = Within</pre>	Holding Time
Analyte Group	Method	Sampling Date	Ext	traction / Pi	reparation			Analys	is	
Container / Client Sample ID(s)			Preparation Date	Holdin Rec	g Times Actual	Eval	Analysis Date	Holding Rec	Times Actual	Eval
Particle Size : Particle Size Analysis - Hydrometer										
Glass soil jar/Teflon lined cap BH22-5-2	E183	16-Sep-2022	23-Sep-2022				23-Sep-2022	365 days	7 days	√
Particle Size : Particle Size Analysis - Sieve <2mm					1					
Glass soil jar/Teflon lined cap BH22-3-2	E182	16-Sep-2022	23-Sep-2022				23-Sep-2022	365 days	7 days	V
Particle Size : Particle Size Analysis - Sieve <2mm										
Glass soil jar/Teflon lined cap BH22-5-2	E182	16-Sep-2022	23-Sep-2022				23-Sep-2022	365 days	7 days	~
Particle Size : Particle Size Analysis - Sieve >2mm										
Glass soil jar/Teflon lined cap BH22-3-2	E181	16-Sep-2022	23-Sep-2022				23-Sep-2022	365 days	7 days	√
Particle Size : Particle Size Analysis - Sieve >2mm										
Glass soil jar/Teflon lined cap BH22-5-2	E181	16-Sep-2022	23-Sep-2022				23-Sep-2022	365 days	7 days	V
Physical Tests : Conductivity in Soil (1:2 Soil:Water Extraction) (Low Level)										
Glass soil jar/Teflon lined cap BH22-3-2	E100-L	16-Sep-2022	28-Sep-2022				28-Sep-2022	30 days	12 days	V
Physical Tests : Conductivity in Soil (1:2 Soil:Water Extraction) (Low Level)										
Glass soil jar/Teflon lined cap BH22-5-3	E100-L	16-Sep-2022	28-Sep-2022				28-Sep-2022	30 days	12 days	~
Physical Tests : Conductivity in Soil (1:2 Soil:Water Extraction) (Low Level)										
Glass soil jar/Teflon lined cap MW22-6-3	E100-L	15-Sep-2022	28-Sep-2022				28-Sep-2022	30 days	13 days	~
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap BH22-10-1	E144	15-Sep-2022					22-Sep-2022			



Matrix: Soil/Solid					Ev	aluation: × =	Holding time excee	edance ; •	🗸 = Within	Holding Time
Analyte Group	Method	Sampling Date	Ex	traction / Pi	reparation			Analysis		
Container / Client Sample ID(s)			Preparation	Holdin	g Times	Eval	Analysis Date	Holding	g Times	Eval
			Date	Rec	Actual			Rec	Actual	
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap										
BH22-10-2	E144	15-Sep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry				1				1	-	
Glass soil jar/Teflon lined cap		45.0 0000								
BH22-10-3	E144	15-Sep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry		1			1				1	
Glass soil jar/Teflon lined cap	E144	15 Son 2022					22 Son 2022			
BH22-10-4	⊏144	15-5ep-2022					22-3ep-2022			
Physical Tests : Moisture Content by Gravimetry										
BH22-3-1	F144	16-Sen-2022					22-Sen-2022			
		10 000 2022					22 000 2022			
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap										
BH22-3-2	E144	16-Sep-2022					21-Sep-2022			
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap										
BH22-3-3	E144	16-Sep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap										
BH22-3-4	E144	16-Sep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap	E 444	40.0					00.0			
BH22-5-1	E144	16-Sep-2022					22-Sep-2022			
	I									
Physical Tests : Moisture Content by Gravimetry										
Glass soli jar/Tetion lined cap	F144	16-Sen-2022					22-Sen-2022			
		10-000-2022					22-06p-2022			



Matrix: Soil/Solid					Ev	aluation: × =	Holding time excee	dance ; •	= Within	Holding Time
Analyte Group	Method	Sampling Date	Ext	raction / Pr	eparation			Analysis		
Container / Client Sample ID(s)			Preparation	Holding	g Times	Eval	Analysis Date	Holding	g Times	Eval
			Date	Rec	Actual			Rec	Actual	
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap										
BH22-5-3	E144	16-Sep-2022					21-Sep-2022			
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap										
BH22-5-4	E144	16-Sep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap	F 444	40.0-= 0000					00.0-= 0000			
BH22-5-5	E144	16-Sep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry				1						
Glass soil jar/letion lined cap	E144	15 Son 2022					22 Son 2022			
BH22-1-1	L 144	10-0ep-2022					22-3ep-2022			
Physical Tests : Moisture Content by Gravimetry										
BH22-7-2	F144	15-Sep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap										
BH22-7-3	E144	15-Sep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap										
BH22-7-4	E144	15-Sep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap										
BH22-7-5	E144	15-Sep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap		16 8 - 0000					00.0 0000			
BH22-0-1	⊏144	10-Sep-2022					22-Sep-2022			



Matrix: Soil/Solid					Ev	aluation: × =	Holding time excee	edance ; •	🗸 = Within	Holding Time
Analyte Group	Method	Sampling Date	Ext	traction / Pi	reparation			Analysis		
Container / Client Sample ID(s)			Preparation	Holdin	g Times	Eval	Analysis Date	Holding	g Times	Eval
			Date	Rec	Actual			Rec	Actual	
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap										
BH22-8-2	E144	16-Sep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap										
BH22-8-3	E144	16-Sep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry				1						
Glass soil jar/Teflon lined cap										
BH22-8-4	E144	16-Sep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap										
BH22-9-1	E144	16-Sep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap		40.0 0000								
BH22-9-2	E144	16-Sep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap	E 444	40.0					00.0.0000			
BH22-9-3	E144	16-Sep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry									1	
Glass soil jar/Teflon lined cap	E144	16 San 2022					22 San 2022			
BH22-9-4	⊏144	16-Sep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry		1 1					1			
Glass soil jar/letion lined cap	E144	16 Son 2022					22 San 2022			
DH22-9-3	L 144	10-3ep-2022					22-3ep-2022			
Physical Tests : Moisture Content by Gravimetry										
	F144	16-Sep-2022					22-Sen-2022			
WITTLE-2-1	L (77	10 000-2022					22-00p-2022			



Matrix: Soil/Solid					Ev	aluation: × =	Holding time excee	edance ; •	🗸 = Withir	Holding Time
Analyte Group	Method	Sampling Date	Ex	traction / Pi	reparation			Analysis		
Container / Client Sample ID(s)			Preparation	Holdin	g Times	Eval	Analysis Date	Holding	g Times	Eval
			Date	Rec	Actual			Rec	Actual	
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap										
MW22-2-2	E144	16-Sep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap										
MW22-2-3	E144	16-Sep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap	E 444	40.0					00.0.0000			
MW22-2-4	E144	16-Sep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry					1					
Glass soil jar/Teflon lined cap	E144	16 Son 2022					22 San 2022			
WVV22-2-5	C 144	10-3ep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry							1			
	E144	15-Sen-2022					22-Sen-2022			
1010022-4-1	L 144	10-069-2022					22-069-2022			
Research Testers Meisters Constant has Constant for										
Physical Tests : Molsture Content by Gravimetry										
MW22-4-2	E144	15-Sep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap										
MW22-4-3	E144	15-Sep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry							1			
Glass soil jar/Teflon lined cap										
MW22-4-4	E144	15-Sep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap										
MW22-4-5	E144	15-Sep-2022					22-Sep-2022			
	1									


Matrix: Soil/Solid					Ev	/aluation: × =	Holding time exce	edance ; 🗸	<pre>/ = Within</pre>	Holding Time
Analyte Group	Method	Sampling Date	Extraction / Preparation				Analys	sis		
Container / Client Sample ID(s)			Preparation	Holdin	g Times	Eval	Analysis Date	Holding	g Times	Eval
			Date	Rec	Actual			Rec	Actual	
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap										
MW22-6-1	E144	15-Sep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap										
MW22-6-2	E144	15-Sep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap										
MW22-6-3	E144	15-Sep-2022					21-Sep-2022			
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap										
MW22-6-4	E144	15-Sep-2022					22-Sep-2022			
Physical Tests : Moisture Content by Gravimetry										
Glass soil jar/Teflon lined cap										
MW22-6-5	E144	15-Sep-2022					22-Sep-2022			
Physical Tests : ORP by Electrode										
Glass soil jar/Teflon lined cap										
BH22-3-2	E125	16-Sep-2022	22-Sep-2022				22-Sep-2022	180	6 days	✓
								days		
Physical Tests : ORP by Electrode										
Glass soil jar/Teflon lined cap										
BH22-5-3	E125	16-Sep-2022	22-Sep-2022				22-Sep-2022	180	6 days	✓
								days		
Physical Tests : ORP by Electrode										
Glass soil jar/Teflon lined cap										
MW22-6-3	E125	15-Sep-2022	22-Sep-2022				22-Sep-2022	180	7 days	✓
								days		
Physical Tests : pH by Meter (1:2 Soil:0.01M CaCl2 Extraction) - As Received										
Glass soil jar/Teflon lined cap										
BH22-3-2	E108A	16-Sep-2022	22-Sep-2022				22-Sep-2022	30 days	6 days	✓



Matrix: Soil/Solid Evaluation: **×** = Holding time exceedance ; **✓** = Within Holding Time Extraction / Preparation Sampling Date Analysis Analyte Group Method Container / Client Sample ID(s) Holding Times Eval Preparation Holding Times Eval Analysis Date Rec Actual Rec Actual Date Physical Tests : pH by Meter (1:2 Soil:0.01M CaCl2 Extraction) - As Received Glass soil jar/Teflon lined cap 22-Sep-2022 BH22-5-3 E108A 16-Sep-2022 22-Sep-2022 30 days 6 days ✓ --------Physical Tests : pH by Meter (1:2 Soil:0.01M CaCl2 Extraction) - As Received Glass soil jar/Teflon lined cap 22-Sep-2022 30 days 7 days ✓ MW22-6-3 E108A 15-Sep-2022 22-Sep-2022 --------

Legend & Qualifier Definitions

Rec. HT: ALS recommended hold time (see units).



Quality Control Parameter Frequency Compliance

The following report summarizes the frequency of laboratory QC samples analyzed within the analytical batches (QC lots) in which the submitted samples were processed. The actual frequency should be greater than or equal to the expected frequency.

Matrix: Soil/Solid	Evaluation: × = QC frequency outside specification; ✓ = QC frequency within spec							
Quality Control Sample Type		unt	Frequency (%)					
Analytical Methods	Method	QC Lot #	QC	Regular	Actual	Expected	Evaluation	
Laboratory Duplicates (DUP)								
Acid Volatile Sulfide in Soil by Colourimetry (0.2 mg/kg)	E396-L	657907	1	4	25.0	4.7	1	
CCME fine/coarse Particle Size Analysis by wet sieve	E178	674236	1	8	12.5	5.0	✓	
Conductivity in Soil (1:2 Soil:Water Extraction) (Low Level)	E100-L	659587	1	19	5.2	5.0	✓	
Moisture Content by Gravimetry	E144	659122	4	70	5.7	5.0	1	
ORP by Electrode	E125	659317	1	3	33.3	5.0	✓	
Particle Size Analysis - Hydrometer	E183	663154	1	5	20.0	5.0	✓	
Particle Size Analysis - Sieve <2mm	E182	663153	1	5	20.0	5.0	✓	
pH by Meter (1:2 Soil:0.01M CaCl2 Extraction) - As Received	E108A	659219	1	20	5.0	5.0	✓	
Water Extractable Chloride by IC	E236.Cl	659594	1	3	33.3	5.0	1	
Water Extractable Sulfate by IC	E236.SO4	659593	1	3	33.3	5.0	✓	
Laboratory Control Samples (LCS)								
Acid Volatile Sulfide in Soil by Colourimetry (0.2 mg/kg)	E396-L	657907	1	4	25.0	4.7	✓	
CCME fine/coarse Particle Size Analysis by wet sieve	E178	674236	1	8	12.5	5.0	✓	
Conductivity in Soil (1:2 Soil:Water Extraction) (Low Level)	E100-L	659587	2	19	10.5	10.0	✓	
Moisture Content by Gravimetry	E144	659122	4	70	5.7	5.0	✓	
ORP by Electrode	E125	659317	1	3	33.3	5.0	✓	
Particle Size Analysis - Hydrometer	E183	663154	1	5	20.0	5.0	✓	
Particle Size Analysis - Sieve <2mm	E182	663153	1	5	20.0	5.0	1	
Particle Size Analysis - Sieve >2mm	E181	663152	1	5	20.0	5.0	✓	
pH by Meter (1:2 Soil:0.01M CaCl2 Extraction) - As Received	E108A	659219	1	20	5.0	5.0	✓	
Water Extractable Chloride by IC	E236.Cl	659594	2	3	66.6	10.0	✓	
Water Extractable Sulfate by IC	E236.SO4	659593	2	3	66.6	10.0	✓	
Method Blanks (MB)								
Acid Volatile Sulfide in Soil by Colourimetry (0.2 mg/kg)	E396-L	657907	1	4	25.0	4.7	1	
Conductivity in Soil (1:2 Soil:Water Extraction) (Low Level)	E100-L	659587	1	19	5.2	5.0	✓	
Moisture Content by Gravimetry	E144	659122	4	70	5.7	5.0	1	
Water Extractable Chloride by IC	E236.Cl	659594	1	3	33.3	5.0	1	
Water Extractable Sulfate by IC	E236.SO4	659593	1	3	33.3	5.0	1	



Methodology References and Summaries

The analytical methods used by ALS are developed using internationally recognized reference methods (where available), such as those published by US EPA, APHA Standard Methods, ASTM, ISO, Environment Canada, BC MOE, and Ontario MOE. Reference methods may incorporate modifications to improve performance (indicated by "mod").

Analytical Methods	Method / Lab	Matrix	Method Reference	Method Descriptions
Conductivity in Soil (1:2 Soil:Water Extraction) (Low Level)	E100-L Waterloo - Environmental	Soil/Solid	CSSS Ch. 15 (mod)/APHA 2510 (mod)	Conductivity, also known as Electrical Conductivity (EC) or Specific Conductance, is measured by immersion of a conductivity cell with platinum electrodes into a soil sample that has been added in a defined ratio of soil to deionized water, then shaken well and allowed to settle. Conductance is measured in the fluid that is observed in the upper layer.
pH by Meter (1:2 Soil:0.01M CaCl2 Extraction) - As Received	E108A Waterloo - Environmental	Soil/Solid	MOEE E3137A	pH is determined by potentiometric measurement with a pH electrode, and is conducted at ambient laboratory temperature (normally $20 \pm 5^{\circ}$ C) and is carried out in accordance with procedures described in the Analytical Protocol (prescriptive method). A minimum 10g portion of the sample, as received, is extracted with 20mL of 0.01M calcium chloride solution by shaking for at least 30 minutes. The aqueous layer is separated from the soil by centrifuging, settling, or decanting and then analyzed using a pH meter and electrode.
ORP by Electrode	E125 Waterloo - Environmental	Soil/Solid	APHA 2580 (mod)	Oxidation Redution Potential (ORP) is reported as the oxidation-reduction potential of the platinum metal-reference electrode employed in the analysis, measured in mV.
Moisture Content by Gravimetry	E144 Waterloo - Environmental	Soil/Solid	CCME PHC in Soil - Tier 1	Moisture is measured gravimetrically by drying the sample at 105°C. Moisture content is calculated as the weight loss (due to water) divided by the wet weight of the sample, expressed as a percentage.
CCME fine/coarse Particle Size Analysis by wet sieve	E178 Saskatoon - Environmental	Soil/Solid	CCME Vol 4 Analytical Methods	An air-dried sample is reduced to < 2 mm size and mixed with a dispersing agent (sodium hexametaphosphate). The sample is washed through a 200 mesh (0.075 mm) sieve. The retained mass of sample is used to determine % sand fraction. If the percentage of sand is >50%, the soil is considered to be coarse textured soil. If the percentage of sand is <50% the soil is considered to be fine textured.
Particle Size Analysis - Sieve >2mm	E181 Saskatoon - Environmental	Soil/Solid	ASTM D6913-17 (mod)	Soil samples are disaggregated and sieved through a 2mm sieve. Material retained on the sieve is then further sieved through a series of sieves. The amount passing through the sieves is measured gravimetrically.
Particle Size Analysis - Sieve <2mm	E182 Saskatoon - Environmental	Soil/Solid	ASTM D6913-17 (mod)	Soil samples are disaggregated and sieved through a 2mm sieve. Material passed through the sieve is then further disaggregated using calgon solution and passed through a series of sieves. The amount passing through the sieves is measured gravimetrically.
Particle Size Analysis - Hydrometer	E183 Saskatoon - Environmental	Soil/Solid	ASTM D7928-21 (mod)	Soil material is separated from coarse material (>2mm). A specimen is then disaggregated through mixing with Calgon solution. The material is then suspended in solution wherein regular hydrometer readings are taken at specific time intervals. The principles of Stokes' Law are applied to determine the amount of material remaining in solution as well as the maximum particle size remaining in solution at the specified time.

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Analytical Methods	Method / Lab	Matrix	Method Reference	Method Descriptions
Grain Size Report (Attachment)	E185	Soil/Solid	ASTM D6913/D7928	A grain size curve is a graphical representation of the particle sizing of a sample
Hydrometer/Sieve Method				representing the percent passing against the effective particle size.
	Saskatoon -			
	Environmental			
Water Extractable Chloride by IC	E236.CI	Soil/Solid	EPA 300.1	Inorganic anions are analyzed by Ion Chromatography with conductivity and /or UV
				detection using a soil sample that has been added in a defined ratio of soil to deionized
	Waterloo -			water, then shaken well and allowed to settle. Anions are measured in the fluid that is
	Environmental			observed in the upper layer.
Water Extractable Sulfate by IC	E236.SO4	Soil/Solid	EPA 300.1	Inorganic anions are analyzed by Ion Chromatography with conductivity and /or UV detection using a soil sample that has been added in a defined ratio of soil to deionized
	Waterloo -			water, then shaken well and allowed to settle. Anions are measured in the fluid that is
	Environmental			observed in the upper layer.
Acid Volatile Sulfide in Soil by Colourimetry	E396-L	Soil/Solid	APHA 4500S2J	This analysis is carried out in accordance with the method described in APHA 4500
(0.2 mg/kg)				S2-J. After extraction the Acid Volatile Sulphide is determined colourimetrically.
	Waterloo -			
	Environmental			
Resistivity Calculation for Soil Using E100-L	EC100R	Soil/Solid	APHA 2510 B	Soil Resistivity (calculated) is determined as the inverse of the conductivity of a 2:1
				water:soil leachate (dry weight). This method is intended as a rapid approximation for
	Waterloo -			Soil Resistivity. Where high accuracy results are required, direct measurement of Soil
	Environmental			Resistivity by the Wenner Four-Electrode Method (ASTM G57) is recommended.
Preparation Methods	Method / Lab	Matrix	Method Reference	Method Descriptions
Preparation Methods Leach 1:2 Soil:Water for pH/EC	Method / Lab EP108	<i>Matrix</i> Soil/Solid	Method Reference BC WLAP METHOD: PH. ELECTROMETRIC.	Method Descriptions The procedure involves mixing the dried (at <60°C) and sieved (No. 10 / 2mm) sample with deionized/distilled water at a 1:2 ratio of sediment to water.
Preparation Methods Leach 1:2 Soil:Water for pH/EC	<i>Method / Lab</i> EP108 Waterloo -	<i>Matrix</i> Soil/Solid	Method Reference BC WLAP METHOD: PH, ELECTROMETRIC, SOIL	Method Descriptions The procedure involves mixing the dried (at <60°C) and sieved (No. 10 / 2mm) sample with deionized/distilled water at a 1:2 ratio of sediment to water.
Preparation Methods Leach 1:2 Soil:Water for pH/EC	<i>Method / Lab</i> EP108 Waterloo - Environmental	<i>Matrix</i> Soil/Solid	Method Reference BC WLAP METHOD: PH, ELECTROMETRIC, SOIL	Method Descriptions The procedure involves mixing the dried (at <60°C) and sieved (No. 10 / 2mm) sample with deionized/distilled water at a 1:2 ratio of sediment to water.
Preparation Methods Leach 1:2 Soil:Water for pH/EC Leach 1:2 Soil : 0.01CaCl2 - As Received for	Method / Lab EP108 Waterloo - Environmental EP108A	Matrix Soil/Solid Soil/Solid	Method Reference BC WLAP METHOD: PH, ELECTROMETRIC, SOIL MOEE E3137A	Method Descriptions The procedure involves mixing the dried (at <60°C) and sieved (No. 10 / 2mm) sample with deionized/distilled water at a 1:2 ratio of sediment to water.
Preparation Methods Leach 1:2 Soil:Water for pH/EC Leach 1:2 Soil : 0.01CaCl2 - As Received for pH	Method / Lab EP108 Waterloo - Environmental EP108A	Matrix Soil/Solid Soil/Solid	Method Reference BC WLAP METHOD: PH, ELECTROMETRIC, SOIL MOEE E3137A	Method Descriptions The procedure involves mixing the dried (at <60°C) and sieved (No. 10 / 2mm) sample with deionized/distilled water at a 1:2 ratio of sediment to water.
Preparation Methods Leach 1:2 Soil:Water for pH/EC Leach 1:2 Soil : 0.01CaCl2 - As Received for pH	Method / Lab EP108 Waterloo - Environmental EP108A Waterloo -	Matrix Soil/Solid Soil/Solid	Method Reference BC WLAP METHOD: PH, ELECTROMETRIC, SOIL MOEE E3137A	Method Descriptions The procedure involves mixing the dried (at <60°C) and sieved (No. 10 / 2mm) sample with deionized/distilled water at a 1:2 ratio of sediment to water.
Preparation Methods Leach 1:2 Soil:Water for pH/EC Leach 1:2 Soil : 0.01CaCl2 - As Received for pH	Method / Lab EP108 Waterloo - Environmental EP108A Waterloo - Environmental	Matrix Soil/Solid Soil/Solid	Method Reference BC WLAP METHOD: PH, ELECTROMETRIC, SOIL MOEE E3137A	Method Descriptions The procedure involves mixing the dried (at <60°C) and sieved (No. 10 / 2mm) sample with deionized/distilled water at a 1:2 ratio of sediment to water.
Preparation Methods Leach 1:2 Soil:Water for pH/EC Leach 1:2 Soil : 0.01CaCl2 - As Received for pH Preparation of ORP by Electrode	Method / Lab EP108 Waterloo - Environmental EP108A Waterloo - Environmental EP125	Matrix Soil/Solid Soil/Solid Soil/Solid	Method Reference BC WLAP METHOD: PH, ELECTROMETRIC, SOIL MOEE E3137A APHA 2580 (mod)	Method Descriptions The procedure involves mixing the dried (at <60°C) and sieved (No. 10 / 2mm) sample with deionized/distilled water at a 1:2 ratio of sediment to water.
Preparation Methods Leach 1:2 Soil:Water for pH/EC Leach 1:2 Soil : 0.01CaCl2 - As Received for pH Preparation of ORP by Electrode	Method / Lab EP108 Waterloo - Environmental EP108A Waterloo - Environmental EP125 Waterloo -	Matrix Soil/Solid Soil/Solid Soil/Solid	Method Reference BC WLAP METHOD: PH, ELECTROMETRIC, SOIL MOEE E3137A APHA 2580 (mod)	Method Descriptions The procedure involves mixing the dried (at <60°C) and sieved (No. 10 / 2mm) sample with deionized/distilled water at a 1:2 ratio of sediment to water.
Preparation Methods Leach 1:2 Soil:Water for pH/EC Leach 1:2 Soil : 0.01CaCl2 - As Received for pH Preparation of ORP by Electrode	Method / Lab EP108 Waterloo - Environmental EP108A Waterloo - Environmental EP125 Waterloo - Environmental	Matrix Soil/Solid Soil/Solid Soil/Solid	Method Reference BC WLAP METHOD: PH, ELECTROMETRIC, SOIL MOEE E3137A APHA 2580 (mod)	Method Descriptions The procedure involves mixing the dried (at <60°C) and sieved (No. 10 / 2mm) sample with deionized/distilled water at a 1:2 ratio of sediment to water.
Preparation Methods Leach 1:2 Soil:Water for pH/EC Leach 1:2 Soil : 0.01CaCl2 - As Received for pH Preparation of ORP by Electrode Anions Leach 1:10 Soil:Water (Dry)	Method / Lab EP108 Waterloo - Environmental EP108A Waterloo - Environmental EP125 Waterloo - Environmental EP236	Matrix Soil/Solid Soil/Solid Soil/Solid	Method Reference BC WLAP METHOD: PH, ELECTROMETRIC, SOIL MOEE E3137A APHA 2580 (mod) EPA 300.1	Method Descriptions The procedure involves mixing the dried (at <60°C) and sieved (No. 10 / 2mm) sample with deionized/distilled water at a 1:2 ratio of sediment to water.
Preparation Methods Leach 1:2 Soil:Water for pH/EC Leach 1:2 Soil : 0.01CaCl2 - As Received for pH Preparation of ORP by Electrode Anions Leach 1:10 Soil:Water (Dry)	Method / Lab EP108 Waterloo - Environmental EP108A Waterloo - Environmental EP125 Waterloo - Environmental EP236	Matrix Soil/Solid Soil/Solid Soil/Solid	Method Reference BC WLAP METHOD: PH, ELECTROMETRIC, SOIL MOEE E3137A APHA 2580 (mod) EPA 300.1	Method Descriptions The procedure involves mixing the dried (at <60°C) and sieved (No. 10 / 2mm) sample with deionized/distilled water at a 1:2 ratio of sediment to water.
Preparation Methods Leach 1:2 Soil:Water for pH/EC Leach 1:2 Soil : 0.01CaCl2 - As Received for pH Preparation of ORP by Electrode Anions Leach 1:10 Soil:Water (Dry)	Method / Lab EP108 Waterloo - Environmental EP108A Waterloo - Environmental EP125 Waterloo - Environmental EP236 Waterloo -	Matrix Soil/Solid Soil/Solid Soil/Solid	Method Reference BC WLAP METHOD: PH, ELECTROMETRIC, SOIL MOEE E3137A APHA 2580 (mod) EPA 300.1	Method Descriptions The procedure involves mixing the dried (at <60°C) and sieved (No. 10 / 2mm) sample with deionized/distilled water at a 1:2 ratio of sediment to water.
Preparation Methods Leach 1:2 Soil:Water for pH/EC Leach 1:2 Soil : 0.01CaCl2 - As Received for pH Preparation of ORP by Electrode Anions Leach 1:10 Soil:Water (Dry)	Method / Lab EP108 Waterloo - Environmental EP108A Waterloo - Environmental EP125 Waterloo - Environmental EP236 Waterloo - Environmental	Matrix Soil/Solid Soil/Solid Soil/Solid	Method Reference BC WLAP METHOD: PH, ELECTROMETRIC, SOIL MOEE E3137A APHA 2580 (mod) EPA 300.1	Method Descriptions The procedure involves mixing the dried (at <60°C) and sieved (No. 10 / 2mm) sample with deionized/distilled water at a 1:2 ratio of sediment to water.
Preparation Methods Leach 1:2 Soil:Water for pH/EC Leach 1:2 Soil : 0.01CaCl2 - As Received for pH Preparation of ORP by Electrode Anions Leach 1:10 Soil:Water (Dry) Distillation for Acid Volatile Sulfide in Soil	Method / Lab EP108 Waterloo - Environmental EP108A Waterloo - Environmental EP125 Waterloo - Environmental EP125 Waterloo - Environmental EP236 Waterloo - Environmental EP396-L	Matrix Soil/Solid Soil/Solid Soil/Solid Soil/Solid	Method Reference BC WLAP METHOD: PH, ELECTROMETRIC, SOIL MOEE E3137A APHA 2580 (mod) EPA 300.1 APHA 4500S2J	Method Descriptions The procedure involves mixing the dried (at <60°C) and sieved (No. 10 / 2mm) sample with deionized/distilled water at a 1:2 ratio of sediment to water.
Preparation Methods Leach 1:2 Soil:Water for pH/EC Leach 1:2 Soil : 0.01CaCl2 - As Received for pH Preparation of ORP by Electrode Anions Leach 1:10 Soil:Water (Dry) Distillation for Acid Volatile Sulfide in Soil	Method / Lab EP108 Waterloo - Environmental EP108A Waterloo - Environmental EP125 Waterloo - Environmental EP236 Waterloo - Environmental EP236 Waterloo - Environmental EP396-L	Matrix Soil/Solid Soil/Solid Soil/Solid Soil/Solid	Method Reference BC WLAP METHOD: PH, ELECTROMETRIC, SOIL MOEE E3137A APHA 2580 (mod) EPA 300.1 APHA 4500S2J	Method Descriptions The procedure involves mixing the dried (at <60°C) and sieved (No. 10 / 2mm) sample with deionized/distilled water at a 1:2 ratio of sediment to water.
Preparation Methods Leach 1:2 Soil:Water for pH/EC Leach 1:2 Soil : 0.01CaCl2 - As Received for pH Preparation of ORP by Electrode Anions Leach 1:10 Soil:Water (Dry) Distillation for Acid Volatile Sulfide in Soil	Method / Lab EP108 Waterloo - Environmental EP108A Waterloo - Environmental EP125 Waterloo - Environmental EP236 Waterloo - Environmental EP396-L Waterloo - Waterloo -	Matrix Soil/Solid Soil/Solid Soil/Solid Soil/Solid	Method Reference BC WLAP METHOD: PH, ELECTROMETRIC, SOIL MOEE E3137A APHA 2580 (mod) EPA 300.1 APHA 4500S2J	Method Descriptions The procedure involves mixing the dried (at <60°C) and sieved (No. 10 / 2mm) sample with deionized/distilled water at a 1:2 ratio of sediment to water.

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Preparation Methods	Method / Lab	Matrix	Method Reference	Method Descriptions
Dry and Grind in Soil/Solid <60°C	EPP442	Soil/Solid	Soil Sampling and	After removal of any coarse fragments and reservation of wet subsamples a portion of
			Methods of Analysis,	homogenized sample is set in a tray and dried at less than 60°C until dry. The sample is
	Waterloo -		Carter 2008	then particle size reduced with an automated crusher or mortar and pestle, typically to
	Environmental			<2 mm. Further size reduction may be needed for particular tests.

ALS Canada Ltd.



	QUALITY CON	TROL REPORT	
Work Order	·WT2214822	Page	: 1 of 7
Amendment	:1		
Client	: Arcadis Canada Inc.	Laboratory	: Waterloo - Environmental
Contact	: Lennart DeGroot	Account Manager	: Emily Smith
Address	: 1050 Morrison Drive Suite 201 Ottawa ON Canada K2H 1I 1	Address	≑60 Northland Road, Unit 1 Waterloo, Ontario Canada N2V 2B8
Telephone	:	Telephone	:+1 519 886 6910
Project	: 30127480	Date Samples Received	: 19-Sep-2022 14:55
PO	:	Date Analysis Commenced	21-Sep-2022
C-O-C number	:	Issue Date	: 31-Oct-2022 10:15
Sampler	e13 721 0555		
Site	:		
Quote number	: Waterloo 2022 Price List		
No. of samples received	: 42		
No. of samples analysed	: 42		

This report supersedes any previous report(s) with this reference. Results apply to the sample(s) as submitted. This document shall not be reproduced, except in full. This Quality Control Report contains the following information:

- Laboratory Duplicate (DUP) Report; Relative Percent Difference (RPD) and Data Quality Objectives
- Reference Material (RM) Report; Recovery and Data Quality Objectives
- Method Blank (MB) Report; Recovery and Data Quality Objectives
- Laboratory Control Sample (LCS) Report; Recovery and Data Quality Objectives

Signatories

This document has been electronically signed by the authorized signatories below. Electronic signing is conducted in accordance with US FDA 21 CFR Part 11.

Signatories	Position	Laboratory Department
Amanda Ganouri-Lumsden	Department Manager - Microbiology and Prep	Waterloo Centralized Prep, Waterloo, Ontario
Hedy Lai	Team Leader - Inorganics	Saskatoon Inorganics, Saskatoon, Saskatchewan
Hedy Lai	Team Leader - Inorganics	Saskatoon Sask Soils, Saskatoon, Saskatchewan
Jon Fisher	Department Manager - Inorganics	Waterloo Inorganics, Waterloo, Ontario
Joseph Scharbach		Waterloo Centralized Prep, Waterloo, Ontario
Niral Patel		Waterloo Centralized Prep, Waterloo, Ontario



General Comments

The ALS Quality Control (QC) report is optionally provided to ALS clients upon request. ALS test methods include comprehensive QC checks with every analysis to ensure our high standards of quality are met. Each QC result has a known or expected target value, which is compared against predetermined Data Quality Objectives (DQOs) to provide confidence in the accuracy of associated test results. This report contains detailed results for all QC results applicable to this sample submission. Please refer to the ALS Quality Control Interpretation report (QCI) for applicable method references and methodology summaries.

Key :

Anonymous = Refers to samples which are not part of this work order, but which formed part of the QC process lot.

CAS Number = Chemical Abstracts Service number is a unique identifier assigned to discrete substances.

DQO = Data Quality Objective.

LOR = Limit of Reporting (detection limit).

RPD = Relative Percent Difference

= Indicates a QC result that did not meet the ALS DQO.

Workorder Comments

Holding times are displayed as "----" if no guidance exists from CCME, Canadian provinces, or broadly recognized international references.



Laboratory Duplicate (DUP) Report

A Laboratory Duplicate (DUP) is a randomly selected intralaboratory replicate sample. Laboratory Duplicates provide information regarding method precision and sample heterogeneity. ALS DQOs for Laboratory Duplicates are expressed as test-specific limits for Relative Percent Difference (RPD), or as an absolute difference limit of 2 times the LOR for low concentration duplicates within ~ 4-10 times the LOR (cut-off is test-specific).

Sub-Matrix: Soil/Solid					Laboratory Duplicate (DUP) Report						
Laboratory sample ID	Client sample ID	Analyte	CAS Number	Method	LOR	Unit	Original Result	Duplicate Result	RPD(%) or Difference	Duplicate Limits	Qualifier
Physical Tests (QC	Lot: 659122)										
WT2214822-001	MW22-2-1	moisture		E144	0.25	%	8.08	7.88	2.55%	20%	
Physical Tests (QC	Lot: 659123)										
WT2214822-010	BH22-8-1	moisture		E144	0.25	%	8.06	8.07	0.109%	20%	
Physical Tests (QC	Lot: 659219)										
TY2201744-003	Anonymous	pH (1:2 soil:CaCl2-aq)		E108A	0.10	pH units	7.56	7.69	1.70%	5%	
Physical Tests (QC	Lot: 659220)										
WT2214822-032	MW22-6-4	moisture		E144	0.25	%	10.6	10.2	3.74%	20%	
Physical Tests (QC	Lot: 659317)										
WT2214822-007	BH22-3-2	oxidation-reduction potential [ORP]		E125	0.10	mV	486	472	2.92%	25%	
Physical Tests (QC	Lot: 659587)										
WT2214860-003	Anonymous	conductivity (1:2 leachate)		E100-L	5.00	μS/cm	0.492 mS/cm	510	3.59%	20%	
Physical Tests (QC	Lot: 660485)										
WT2214804-001	Anonymous	moisture		E144	0.25	%	78.4	78.1	0.386%	20%	
Particle Size (QC L	ot: 663153)										
WT2214849-001	Anonymous	passing (0.05 mm)		E182	1.0	%	84.1	83.3	0.977%	15%	
		passing (0.063 mm)		E182	1.0	%	90.4	90.1	0.353%	15%	
		passing (0.075 mm)		E182	1.0	%	96.3	96.4	0.146%	15%	
		passing (0.125 mm)		E182	1.0	%	96.9	97.0	0.137%	15%	
		passing (0.149 mm)		E182	1.0	%	97.2	97.3	0.133%	15%	
		passing (0.250 mm)		E182	1.0	%	97.6	97.7	0.0742%	15%	
		passing (0.420 mm)		E182	1.0	%	98.0	98.0	0.0182%	15%	
		passing (0.50 mm)		E182	1.0	%	98.1	98.1	0.00625%	15%	
		passing (0.841 mm)		E182	1.0	%	98.5	98.4	0.0404%	15%	
		passing (1.0 mm)		E182	1.0	%	98.5	98.5	0.0361%	15%	
Particle Size (QC L	ot: 663154)										
WT2214849-001	Anonymous	passing (0.002 mm)		E183	1.0	%	27.4	28.4	3.70%	20%	
		passing (0.004 mm)		E183	1.0	%	45.0	47.2	4.84%	20%	
		passing (0.005 mm)		E183	1.0	%	51.9	53.8	3.66%	20%	
		passing (0.020 mm)		E183	1.0	%	75.0	74.1	1.19%	20%	
		passing (0.0312 mm)		E183	1.0	%	77.6	76.6	1.35%	20%	



Laboratory Duplicate (DUP) Report Sub-Matrix: Soil/Solid Laboratory sample ID CAS Number Method Client sample ID Analyte LOR Unit Original Duplicate RPD(%) or Duplicate Qualifier Result Result Difference Limits Particle Size (QC Lot: 674236) SK2205375-027 E178 Anonymous sand (>0.075mm) 1.0 % <1.0 <1.0 0 Diff <2x LOR --------Inorganic Parameters (QC Lot: 657907) WT2214267-003 E396-L Diff <2x LOR Anonymous 0.20 0.24 0.33 0.09 sulfides, acid volatile ---mg/kg ----Leachable Anions & Nutrients (QC Lot: 659593) WT2214822-007 BH22-3-2 sulfate, soluble ion content 14808-79-8 E236.SO4 20 <20 <20 0 Diff <2x LOR mg/kg ----Leachable Anions & Nutrients (QC Lot: 659594) WT2214822-007 BH22-3-2 16887-00-6 E236.Cl 5.0 Diff <2x LOR chloride, soluble ion content mg/kg 29.8 28.8 1.0 ----

Method Blank (MB) Report

A Method Blank is an analyte-free matrix that undergoes sample processing identical to that carried out for test samples. Method Blank results are used to monitor and control for potential contamination from the laboratory environment and reagents. For most tests, the DQO for Method Blanks is for the result to be < LOR.

Sub-Matrix: Soil/Solid

Analyte	CAS Number	Method	LOR	Unit	Result	Qualifier
Physical Tests (QCLot: 659122)						
moisture		E144	0.25	%	<0.25	
Physical Tests (QCLot: 659123)						
moisture		E144	0.25	%	<0.25	
Physical Tests (QCLot: 659220)						
moisture		E144	0.25	%	<0.25	
Physical Tests (QCLot: 659587)						
conductivity (1:2 leachate)		E100-L	5	μS/cm	<5.00	
Physical Tests (QCLot: 660485)						
moisture		E144	0.25	%	<0.25	
Inorganic Parameters (QCLot: 657907)						
sulfides, acid volatile		E396-L	0.2	mg/kg	<0.20	
Leachable Anions & Nutrients (QCLot: 6	59593)					
sulfate, soluble ion content	14808-79-8	E236.SO4	20	mg/kg	<20	
Leachable Anions & Nutrients (QCLot: 6	59594)					
chloride, soluble ion content	16887-00-6	E236.Cl	5	mg/kg	<5.0	



Laboratory Control Sample (LCS) Report

A Laboratory Control Sample (LCS) is an analyte-free matrix that has been fortified (spiked) with test analytes at known concentration and processed in an identical manner to test samples. LCS results are expressed as percent recovery, and are used to monitor and control test method accuracy and precision, independent of test sample matrix.

Sub-Matrix: Soil/Solid					Laboratory Control Sample (LCS) Report					
					Spike	Recovery (%)	Recovery	' Limits (%)		
Analyte	CAS Number	Method	LOR	Unit	Concentration	LCS	Low	High	Qualifier	
Physical Tests (QCLot: 659122)										
moisture		E144	0.25	%	50 %	100	90.0	110		
Physical Tests (QCLot: 659123)										
moisture		E144	0.25	%	50 %	100	90.0	110		
Physical Tests (QCLot: 659219)										
pH (1:2 soil:CaCl2-aq)		E108A		pH units	7 pH units	101	98.0	102		
Physical Tests (QCLot: 659220)										
moisture		E144	0.25	%	50 %	101	90.0	110		
Physical Tests (QCLot: 659587)										
conductivity (1:2 leachate)		E100-L	5	μS/cm	1409 µS/cm	105	90.0	110		
Physical Tests (QCLot: 660485)										
moisture		E144	0.25	%	50 %	101	90.0	110		
Inorganic Parameters (QCLot: 657907)										
sulfides, acid volatile		E396-L	0.2	mg/kg	2.536 mg/kg	99.4	70.0	130		
Leachable Anions & Nutrients (QCLot: 659593)										
sulfate, soluble ion content	14808-79-8	E236.SO4	20	mg/kg	5000 mg/kg	102	70.0	130		
Leachable Anions & Nutrients (QCLot: 659594)										
chloride, soluble ion content	16887-00-6	E236.CI	5	mg/kg	5000 mg/kg	101	80.0	120		



Reference Material (RM) Report

A Reference Material (RM) is a homogenous material with known and well-established analyte concentrations. RMs are processed in an identical manner to test samples, and are used to monitor and control the accuracy and precision of a test method for a typical sample matrix. RM results are expressed as percent recovery of the target analyte concentration. RM targets may be certified target concentrations provided by the RM supplier, or may be ALS long-term mean values (for empirical test methods).

Sub-Matrix:						Refere	nce Material (RM) Re	eport	
					RM Target	Recovery (%)	Recovery	Limits (%)	
Laboratory sample ID	Reference Material ID	Analyte	CAS Number	Method	Concentration	RM	Low	High	Qualifier
Physical Tests (QCLot: 659317)								
	RM	oxidation-reduction potential [ORP]		E125	475 mV	102	80.0	120	
Physical Tests (QCLot: 659587)								
	RM	conductivity (1:2 leachate)		E100-L	1031.5 µS/cm	111	70.0	130	
Particle Size (QC	CLot: 663152)								
	RM	passing (19 mm)		E181	100 %	100	90.0	110	
	RM	passing (2.0 mm)		E181	100 %	100	90.0	110	
	RM	passing (25.4 mm)		E181	100 %	100	90.0	110	
	RM	passing (38.1 mm)		E181	100 %	100	90.0	110	
	RM	passing (4.75 mm)		E181	100 %	100	90.0	110	
	RM	passing (50.8 mm)		E181	100 %	100	90.0	110	
	RM	passing (76.2 mm)		E181	100 %	100	90.0	110	
	RM	passing (9.5 mm)		E181	100 %	100	90.0	110	
Particle Size (QC	CLot: 663153)								
	RM	passing (0.05 mm)		E182	49.81 %	99.2	90.0	110	
	RM	passing (0.063 mm)		E182	54.27 %	98.6	90.8	109	
	RM	passing (0.075 mm)		E182	58.38 %	98.2	91.4	109	
	RM	passing (0.125 mm)		E182	68.06 %	99.3	92.7	107	
	RM	passing (0.149 mm)		E182	72.71 %	99.7	93.1	107	
	RM	passing (0.250 mm)		E182	85.38 %	99.2	94.1	106	
	RM	passing (0.420 mm)		E182	92.78 %	99.7	94.6	105	
	RM	passing (0.50 mm)		E182	93.78 %	99.7	94.7	105	
	RM	passing (0.841 mm)		E182	97.34 %	99.8	94.9	105	
	RM	passing (1.0 mm)		E182	97.77 %	99.8	94.9	105	
Particle Size (QC	CLot: 663154)								
	RM	passing (0.002 mm)		E183	21.14 %	89.0	76.0	124	
	RM	passing (0.004 mm)		E183	24.64 %	93.7	80.0	120	
	RM	passing (0.005 mm)		E183	25.91 %	96.3	82.0	118	
	RM	passing (0.020 mm)		E183	37.12 %	96.9	87.0	113	
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Page	:	7 of 7
Work Order	:	WT2214822 Amendment 1
Client	:	Arcadis Canada Inc.
Project	:	30127480



Sub-Matrix:						Refere	nce Material (RM) Re	port	
					RM Target	Recovery (%)	Recovery L	.imits (%)	
Laboratory sample ID	Reference Material ID	Analyte	CAS Number	Method	Concentration	RM	Low	High	Qualifier
Particle Size (QC	Lot: 663154) - continue	d							
	RM	passing (0.0312 mm)		E183	42.58 %	98.7	88.0	112	
Particle Size (QC	Lot: 674236)								
	RM	sand (>0.075mm)		E178	42.85 %	93.6	88.0	112	
Leachable Anions	s & Nutrients (QCLot: 6	59593)							
	RM	sulfate, soluble ion content	14808-79-8	E236.SO4	217 mg/kg	107	60.0	140	
Leachable Anions	s & Nutrients (QCLot: 6	59594)							
	RM	chloride, soluble ion content	16887-00-6	E236.CI	673 mg/kg	99.4	70.0	130	

819-58th Street, Saskatoon,SK

PARTICLE SIZE DISTRIBUTION CURVE

Client Name:WT2214822007Project Number:BH22-3-2Client Sample IDWT2214822007Lab Sample Received 00-Jan-00Test Completion Date: 28-Sep-22Analyst:SIH



819-58th Street, Saskatoon,SK

PARTICLE SIZE DISTRIBUTION CURVE

Client Name: WT2214822020 Project Number: Client Sample ID MW22-4-2 Lab Sample ID WT2214822020 Date Sample Received 00-Jan-00 Test Completion Date: 28-Sep-22 Analyst: SIH



819-58th Street, Saskatoon,SK

PARTICLE SIZE DISTRIBUTION CURVE

Client Name: WT2214822025 Project Number: Client Sample ID BH22-5-2 Lab Sample ID WT2214822025 Date Sample Received 00-Jan-00 Test Completion Date: 28-Sep-22 Analyst: SIH



819-58th Street, Saskatoon,SK

PARTICLE SIZE DISTRIBUTION CURVE

Client Name:WT2214822030Project Number:MW22-6-2Client Sample IDMW22-6-2Lab Sample IDWT2214822030Date Sample Received 00-Jan-00Test Completion Date:28-Sep-22Analyst:SIH



819-58th Street, Saskatoon,SK



Client Name:WT2214822038Project Number:BH22-7-5Client Sample IDBH22-7-5Lab Sample IDWT2214822038Date Sample Received 00-Jan-00OU-Jan-00Test Completion Date:28-Sep-22Analyst:SIH



819-58th Street, Saskatoon,SK

PARTICLE SIZE DISTRIBUTION CURVE

Client Name: WT2214822040 Project Number: Client Sample ID BH22-10-2 Lab Sample ID WT2214822040 Date Sample Received 00-Jan-00 Test Completion Date: 28-Sep-22 Analyst: SIH



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1. If any water samples are taken from a Regulated Drinking Water (DW) System, please submit using an Authorized DW COC form.

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Chain of Custody (COC) / Analytical Request Form

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