



October 20, 2023

Our File Ref.: 220536

Unpoised Architecture Inc.

5-16 Sweetland Ave.
Ottawa, ON
K1N 7T6

Attention: Sam Cox

**Subject: Slope Stability Analysis – Proposed Automotive Dealership and Body Shop
5254 Bank Street
Ottawa, Ontario**

Pursuant to your request, LRL Associates Ltd. (LRL) completed a slope stability analysis at the above referenced location. The purpose of this analysis was to evaluate the proposed construction pertaining to the site development, and to ensure the construction will not negatively affect the site stability in short term (drained), long term (undrained), and seismic condition.

This report only considered overall slope stability. It shall be noted, once the retaining wall design is complete, LRL shall perform a “Global Stability Analysis” on the retaining wall sections.

Furthermore, this report shall be read in conjunction with the “Geotechnical Investigation – Proposed Automotive Dealership and Body Shop”, generated by LRL (File # 220536), dated July 6, 2023.

1 SITE AND PROJECT DESCRIPTION

The site under investigation is currently used for residential purposes. The site consists of a single-storey residential dwelling, a detached double car garage, and multiple storage buildings at the rear portion of the property. The site is rectangular in shape, having a total surface area of about 1,740 m². The general topography of the eastern portion of the site is considered to be relatively flat. An approximate 3.5 m high slope is present in the north-south direction at the middle of the site. Access to the site comes by way of Bank Street, and is civically located at 5254 Bank Street, Ottawa, Ontario.

It is understood that the new development will consist of a proposed four (4) bay Automotive Dealership and Body Shop, which each bay having a surface area of +/- 90 m². A section of the site is proposed to be raised in order to provide a flat area to construct the bays. The grade raise is proposing to be retained by a retaining wall.



2 PROCEDURE

Two (2) site visits were carried out by a member of our geotechnical team; October 8, 2019, and June 9, 2023. During these site visits, boreholes were drilled across the site to determine the surficial soil of the slope and surrounding site.

A total of eight (8) boreholes were drilled across the site, and labelled BH1 through BH8. All boreholes were advanced until practical auger refusal; at depths ranging between 0.7 and 3.7 m below ground surface (bgs).

3 SLOPE DESCRIPTION

The slope under review herein is located at the approximate mid-point of the site, running in the north-south direction, and sloping downwards towards the west. Currently the slope has a profile of about 3.5 Horizontal to 1 Vertical (3.5H:1.0V), and a height of about 3.5 m.

Based on observations made during the site visit, no signs of current or former slope failure appeared within the slope or its surroundings.

4 SUBSURFACE CONDITIONS

A review of local surficial geology maps provided by the Department of Energy, Mines and Resources Canada suggest that the surficial geology for this area consists of bedrock. The bedrock is of the Oxford Formation, consisting of dolomite and limestone.

The boreholes indicate the site is comprised of a thin layer of silt and fill material, overlying bedrock.

No groundwater was encountered during our subsurface investigation. However, it should be noted that groundwater level can vary and is subject to seasonal fluctuation in response to major changes to weather events.

5 SLOPE STABILITY ANALYSES

The slope modelling program, Slide 5.0 (Rocscience), was used to implement the Bishop simplified method of slices. The slope profile chosen to be ran in the modelling was obtained from a cross-section from the project's "Grading and Drainage Plan", generated by LRL. The approximate location of the cross-section (labelled A-A) that was taken and ran in the modelling is shown on the above-mentioned drawing, attached to this report. The slope was analyzed under the undrained (short-term), drained (long-term), and seismic condition. However, it shall be noted that the drained and undrained parameters for the soil encountered on this site are the same. Therefore, the drained and undrained conditions are considered to be equivalent.

The seismic analysis was performed by incorporating the seismic coefficient (k_h) into the modelling. The peak ground acceleration (PGA) for this area is equal to 0.32 for the 2% in 50 year probability of exceedance as per the NBC 2015. The value for k_h was taken as 50% of the PGA, which equates to 0.16.

The field measurements from the borehole drilling in conjunction with known published data of the materials within the region were used for selection of appropriate soil modelling parameters in the slope stability analyses.

The results of the analyses are potentially dependent on the assumption of groundwater conditions. During the development of this report, no information on the groundwater level was available throughout the year. However, as a conservative approach the analysis was completed assuming full saturation throughout the slope.

The following soil parameters were used as part of the analyses.

| Soil Type | Effective cohesion (c') - KPa | Angle of internal friction (ϕ') - degrees | Bulk unit weight (γ_B) – KN/m ³ |
|--|----------------------------------|---|--|
| Drained/Undrained Parameters (Long/Short Term) | | | |
| Silt | 0 | 35 | 17.5 |
| In-situ Fill | 1 | 33 | 18.5 |
| Imported Fill | 1 | 35 | 19.0 |
| Retaining Wall | - | - | 24.0 |
| Bedrock | - | - | 24.0 |

The factor of safety (FoS) against slope failure was run with the loading for the proposed garage bays for the drained/undrained and seismic conditions.

A typical value of 75 kPa for the structures was assumed and included within the modelling.

The FoS against slope failure for the proposed slope profile was determined to be 4.51. A FoS of 1.50 or greater is considered to be safe with regards to slope stability.

The FoS in the seismic condition was determined to be 1.98. The minimum FoS with regards to seismic condition is 1.10.

These results indicate that the proposed construction will not negatively affect the slope, and it will remain stable in the long and short term, and in the event of any seismic activity.

The model results are attached for your reference.

6 SETBACK REQUIREMENTS

The Limit of Hazard Land consists of three components as follows:

Limit of Hazard land = Stable Slope Allowance + Toe Erosion Allowance + Erosion Access Allowance.

The Stable Slope Allowance is the area where a factor of safety is less than 1.5 against overall rotational failure. As indicated in the enclosed figures, the slope stability analysis indicated the factor of safety equal to or greater than 1.5 against failure. Therefore, stable slope allowance can be omitted.

Based on our field observation no sign or indication of toe erosion was observed, therefore no Toe Erosion Allowance is required at this site.

An Erosion Access Allowance is intended to provide a corridor of sufficient width that allows equipment to access the site to undertake a repair for any future unforeseen slope failure. A typical setback value of 6.0 m can be taken for this site. Based on the proposed site development, the setback distance will be greater than 6.0 m.

7 CONCLUSIONS/RECOMMENDATIONS

The following recommendations should be adhered to during the construction and post construction to ensure the long-term stability of the slope.

- Once the site-specific retaining wall design is made available, LRL shall check the wall for Global Stability.
- Any site drainage should be diverted away from the slope/retaining wall. Drainage outlets, if any, shall be protected with riprap over approved geotextile to eliminate erosion in the slope.

- If the site grading changes from what is illustrated in the Grading and Drainage Plan, dated September 25, 2023; LRL shall be consulted to ensure the contents of this reports are still valid.

8 GENERAL COMMENTS AND LIMITATIONS OF REPORT

The conclusion and recommendations are provided in this report are based on subsoil properties at the boreholes' locations. The material reflected in this report are best judgement in light of information obtained from localized auger holes and information available with LRL at the time of report preparation.

This report is prepared for and is intended solely for its client and authorized engineers. Unless otherwise agreed in writing, no portion of this report, or any part thereof may be used for decisions made based on it by separate entity, are the responsibility of such entity. LRL accepts no responsibility for damage, if any, suffered by any separate entity as a result of decisions made or suffered from illegal use of this report. The findings are relevant for the date of the site investigation and any changes on the ground profile or subsurface condition at later date, LRL should be retained to review and for further recommendations.

We trust this report provides sufficient information for your present purposes. If you have any questions concerning this report or if we may be of further services to you, please do not hesitate to contact our office.

Yours truly,

LRL Associates Ltd.

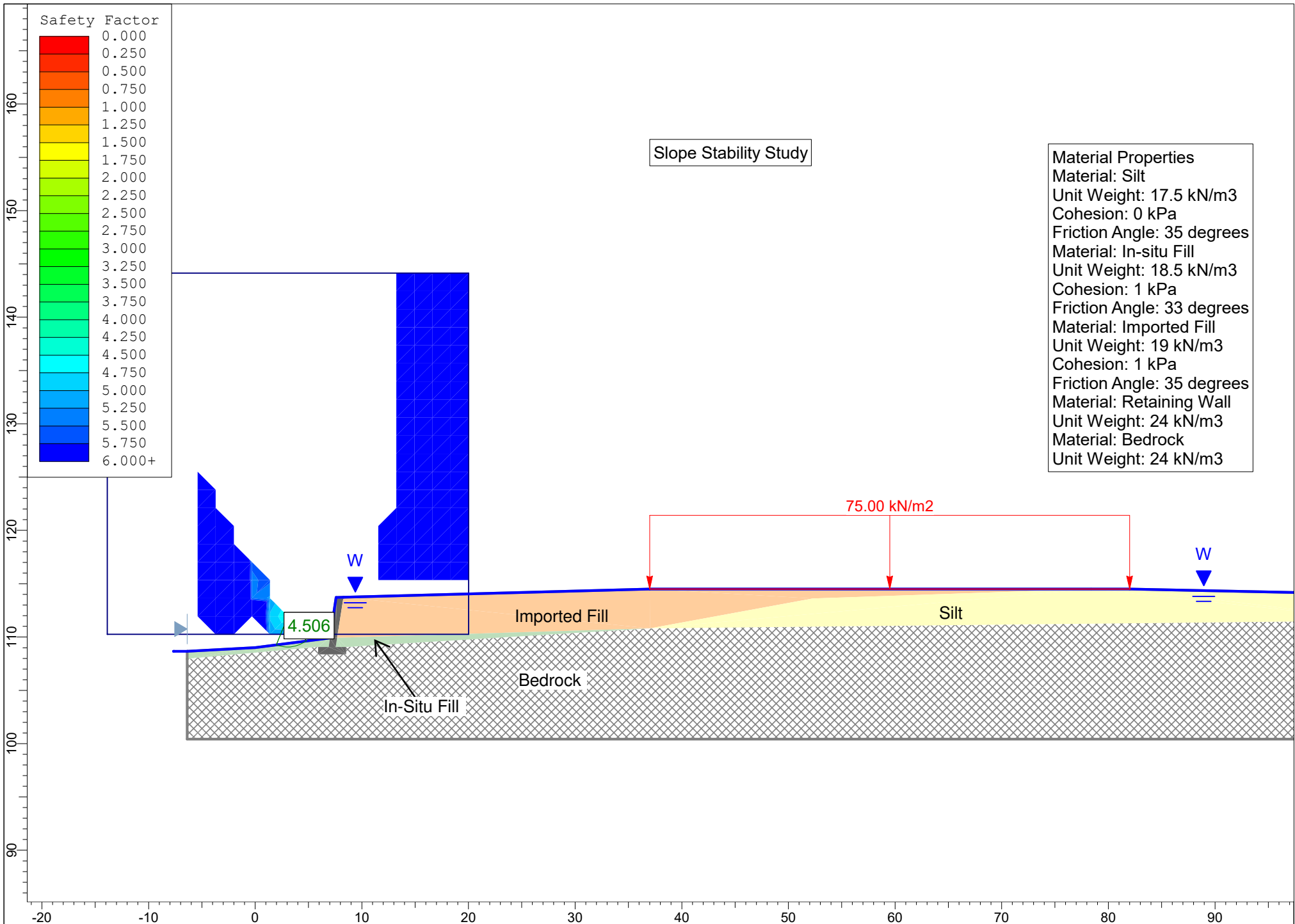


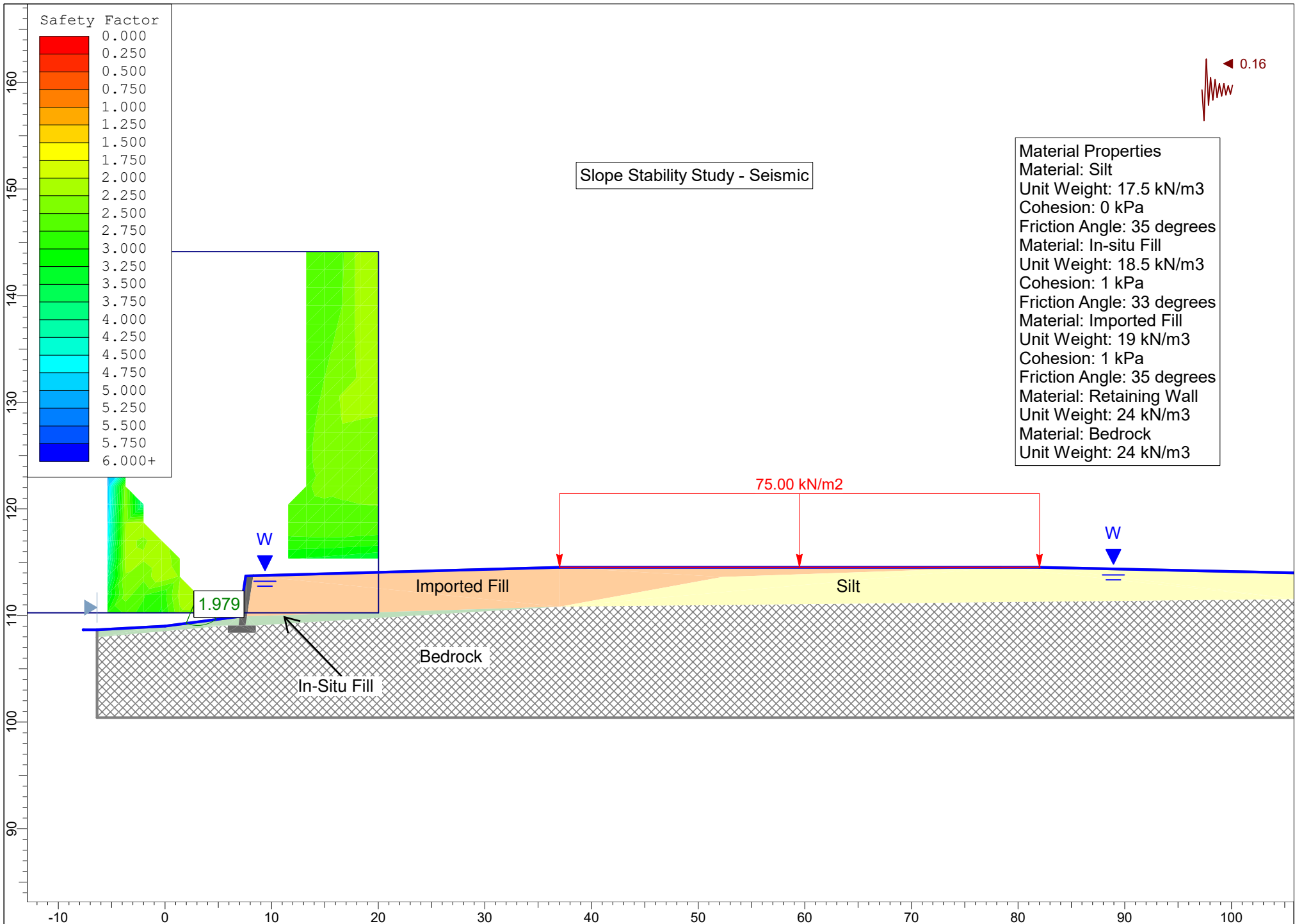
Brad Johnson, P. Eng.
Geotechnical Engineer



Encl. Slope Stability Analysis Results
Cross-section Location







GENERAL NOTES

- 1. ALL WORKS MATERIALS SHALL CONFIRM TO THE LAST REVISION OF THE STANDARDS AND SPECIFICATIONS FOR THE CITY OF OTTAWA... 2. THE CONTRACTORS SHALL CONFIRM THE LOCATION OF ALL EXISTING UTILITIES... 3. ALL DIMENSIONS SHALL BE CHECKED AND VERIFIED IN THE FIELD BY THE CONTRACTOR PRIOR TO THE START OF CONSTRUCTION... 4. ANY AREA BEYOND THE LIMIT OF THE SITE DISTURBED DURING CONSTRUCTION SHALL BE RESTORED TO ORIGINAL CONDITION OR BETTER TO THE SATISFACTION OF THE AUTHORITY... 5. ALL SEWERS CONSTRUCTED WITH GRADES LESS THAN 1.0% SHALL BE INSTALLED USING LASER ALIGNMENT... 6. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL PERMITS REQUIRED AND TO BEAR THE COST OF THE SAME... 7. ALL NECESSARY CLEARING AND GRUBBING SHALL BE COMPLETED BY THE CONTRACTOR... 8. THE CONTRACTOR SHALL PROVIDE THE PROJECT ENGINEER ON SET OF AS CONSTRUCTED SITE SERVING AND GRADING DRAWINGS... 9. BENCHMARKS: IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO VERIFY THAT THE SITE BENCHMARK(S) HAS NOT BEEN ALTERED OR DISTURBED AND THAT ITS RELATIVE ELEVATION AND DESCRIPTION AGREES WITH THE INFORMATION DEPICTED ON THIS PLAN.

SITE GRADING NOTES

- 1. ALL GRANULAR AND PAVEMENT FOR ROADS/PARKING AREAS SHALL BE CONSTRUCTED IN ACCORDANCE WITH GEOTECHNICAL ENGINEER'S RECOMMENDATIONS... 2. ALL TOPSOIL AND ORGANIC MATERIAL SHALL BE STRIPPED WITHIN THE ROAD AND PARKING AREAS ALLOWANCE PRIOR TO THE COMMENCEMENT OF CONSTRUCTION... 3. PAVEMENT REINSTATEMENT FOR SERVICE AND UTILITY CUTS SHALL BE IN ACCORDANCE WITH THE CITY OF OTTAWA STD. R10 AND OPS9 010 AND OPS9 310... 4. GRANULAR 'A' SHALL BE PLACED TO A MINIMUM THICKNESS OF 300MM AROUND ALL STRUCTURES WITHIN THE PAVEMENT AREA... 5. SUB-EXCAVATE SOFT AREAS AND FILL WITH GRANULAR 'B' COMPACTED IN MAXIMUM 300MM LIFTS... 6. ALL WORK ON THE MUNICIPAL RIGHT OF WAY AND EASEMENTS TO BE INSPECTED BY THE MUNICIPALITY PRIOR BACKFILLING... 7. CONTRACTOR TO OBTAIN A ROAD OCCUPANCY PERMIT 48 HOURS PRIOR TO COMMENCING ANY WORK WITHIN THE MUNICIPAL ROAD ALLOWANCE... 8. ALL PAVEMENT MARKING FEATURES AND SITE SIGNAGE SHALL BE PLACED PER ARCHITECTURAL SITE PLAN... 9. REFER TO ARCHITECTURAL SITE PLAN FOR DIMENSIONS AND SITE DETAILS... 10. STEP JOINTS ARE TO BE USED WHERE PROPOSED ASPHALT MEETS EXISTING ASPHALT... 11. WHERE APPLICABLE THE CONTRACTOR IS TO SUBMIT SHOP DRAWINGS TO THE ENGINEER FOR APPROVAL PRIOR TO CONSTRUCTION... 12. ROADWORK TO BE COMPLETED IN ACCORDANCE WITH GEOTECHNICAL REPORT... 13. ALL TOPSOIL AND ORGANIC MATERIAL SHALL BE STRIPPED WITHIN THE ROAD ALLOWANCE PRIOR TO THE COMMENCEMENT OF CONSTRUCTION... 14. THE SUBGRADE SHALL BE CROWNED AND SLOPED AT LEAST 2% AND PROOF ROLLED WITH HEAVY ROLLERS... 15. SUB-EXCAVATE SOFT AREAS AND FILL WITH GRANULAR 'A'; TYPE II COMPACTED IN MAXIMUM 300MM LIFTS... 16. GRANULAR FOR ROADS SHALL BE COMPACTED TO MINIMUM OF 100% STANDARD PROCTOR DENSITY MAXIMUM DRY DENSITY (SPMDD).

ROADWORK SPECIFICATIONS

- 12. ROADWORK TO BE COMPLETED IN ACCORDANCE WITH GEOTECHNICAL REPORT... 13. ALL TOPSOIL AND ORGANIC MATERIAL SHALL BE STRIPPED WITHIN THE ROAD ALLOWANCE PRIOR TO THE COMMENCEMENT OF CONSTRUCTION... 14. THE SUBGRADE SHALL BE CROWNED AND SLOPED AT LEAST 2% AND PROOF ROLLED WITH HEAVY ROLLERS... 15. SUB-EXCAVATE SOFT AREAS AND FILL WITH GRANULAR 'A'; TYPE II COMPACTED IN MAXIMUM 300MM LIFTS... 16. GRANULAR FOR ROADS SHALL BE COMPACTED TO MINIMUM OF 100% STANDARD PROCTOR DENSITY MAXIMUM DRY DENSITY (SPMDD).

PAVEMENT STRUCTURE

Table with 5 columns: COURSE, MATERIAL, THICKNESS (mm), AUTOMOBILE PARKING, TRUCK ROUTE (HEAVY TRAFFIC). Rows include SURFACE, BINDER, BASECOURSE, and SUBBASE with material specifications like HL.3 A/C (PG 58-28) and OPSS GRANULAR 'A'.

NOTE: IN PREPARATION FOR PAVEMENT CONSTRUCTION AT THIS SITE, ANY SURFICIAL OR NEAR SURFACE/SUBGRADE LEVEL TOPSOIL AND ANY SOFT, WET OR DELETERIOUS MATERIALS SHOULD BE REMOVED FROM THE PROPOSED PAVED AREAS... REFER TO GEOTECHNICAL INVESTIGATION REPORT PREPARED BY LRL ASSOCIATES DATED JULY 2021.

LEGEND:

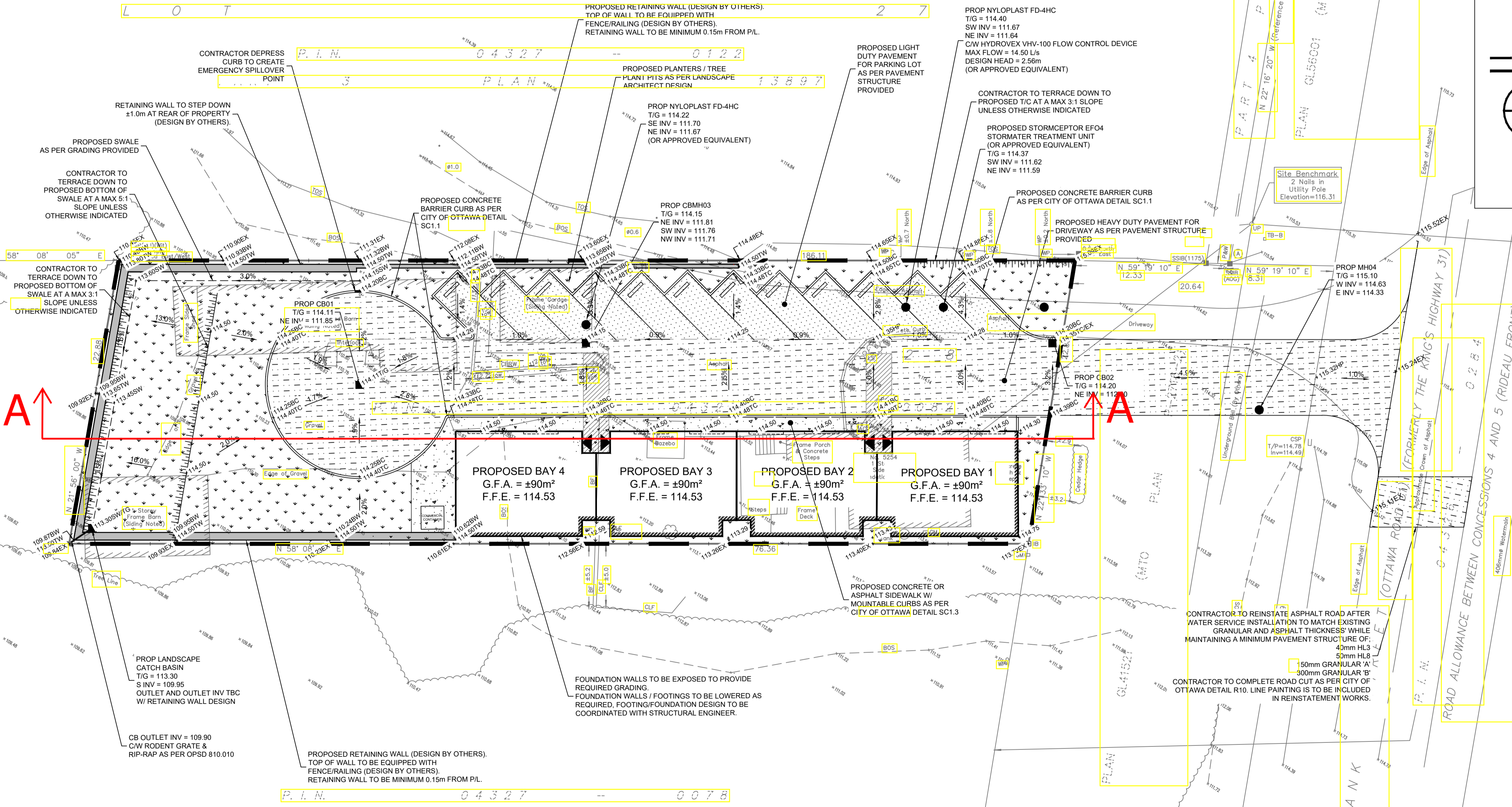
- EXISTING PROPERTY LINE TO REMAIN
PROPOSED CURB
PROPOSED DEPRESSED CURB
PROPOSED TERRACING (3:1 MIN.)
PROPOSED SILT FENCE AS PER OPSD 219.110
PROPOSED DOOR ENTRANCE/EXIT
PROPOSED GRASS AREA (100mm TOP SOIL & SOD)
PROPOSED CONCRETE FEATURES/SLAB
PROPOSED HEAVY DUTY ASPHALT
PROPOSED LIGHT DUTY ASPHALT
PROPOSED RIP RAP
PROPOSED ELEVATION
PROPOSED HIGH POINT ELEVATION
PROPOSED BOTTOM OF CURB / ASPHALT ELEVATION
PROPOSED TOP OF CURB ELEVATION
PROPOSED EXPOSED BOTTOM OF RETAINING WALL
PROPOSED TOP OF RETAINING WALL
MATCH INTO EXISTING ELEVATION
EXISTING ELEVATION
PROPOSED OVERLAND MAJOR FLOW ROUTE
PROPOSED STORM SEWER
PROPOSED SANITARY SEWER
PROPOSED WATERMAIN
EXISTING STORM SEWER
EXISTING SANITARY SEWER
EXISTING WATERMAIN
EXISTING CATCHBASIN-MANHOLE/MANHOLE
EXISTING CATCHBASIN
PROPOSED CATCHBASIN-MANHOLE/MANHOLE
PROPOSED CATCHBASIN
PROPOSED CURB STOP
PROPOSED 100 YEAR HIGH WATER LEVEL
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RUNOFF COEFFICIENT
AREA IN HECTARES

USE AND INTERPRETATION OF DRAWINGS

GENERAL CONDITIONS OF THE CONTRACT FOR CONSTRUCTION ARE PART OF THE CONTRACT DOCUMENTS AND DESCRIBE USE AND INTENT OF THE DRAWING... THE CONTRACTOR SHALL VERIFY IN FIELD FOR LOCATION AND DEPTH OF PIPES AND CHECK WITH THE UTILITY COMPANIES BEFORE DIGGING OR PERFORMING WORK... CONTRACTOR TO VERIFY ALL DIMENSIONS AND NOTIFY THE ENGINEER OF ANY DISCREPANCIES BEFORE WORK COMMENCES.

SCALE: 1:200

NOT FOR CONSTRUCTION TENDER OR PERMIT



Topographical Information
Topographic information provided by Farley, Smith and Denis Surveying Ltd.
File No: 67-19
Date: April 24th, 2019

Metric Note
Distances and coordinates on this plan are in metres and can be converted to feet by dividing by 0.3048.

Distance Note
Distances shown on this plan are ground distances and can be converted to grid distances by multiplying by the combined scale factor of 0.99995.

Bearing Note
Bearings are NTM grid, derived from the Can-Net Real Time Network.
GPS observations on reference points A and B, shown hereon, having a bearing of N 22° 16' 20" W and are referred to the Central Meridian of NAD 83 (Original).

Elevation Notes
1. Elevations shown are geodetic and are referred to Geodetic Datum CGVD-1928-1978.
2. It is the responsibility of the user of this information to verify that the job benchmark has not been altered or disturbed and that its relative elevation and description agrees with the information shown on this drawing.

Utility Notes
1. This drawing cannot be accepted as acknowledging all of the utilities and it will be the responsibility of the user to contact the respective utility authorities for confirmation.
2. Only visible surface utilities were located.
3. Underground utility data derived from City of Ottawa utility sheet reference: 7123 (sheet 6).
4. A field location of underground plant by the pertinent utility authority is mandatory before any work involving breaking ground, probing, excavating etc.

Table with 4 columns: No., REVISIONS, BY, DATE. Rows 02, 01.

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UNPOISED ARCHITECTURE INC
DESIGNED BY: K.H. DRAWN BY: K.H. APPROVED BY: M.B.

PROPOSED MULTI-UNIT COMMERCIAL DEVELOPMENT
5254 BANK STREET, OTTAWA
GRADING AND DRAINAGE PLAN

PROJECT NO: 220536
DATE: JUNE 2022
C301