

**ROADWAY TRAFFIC NOISE
ASSESSMENT**

1299 Richmond Road
Ottawa, Ontario

REPORT: 23-057 – Traffic Noise



October 31st, 2023

PREPARED FOR

Brigil

98 Lois Street
Gatineau, QC J8Y 3R7

PREPARED BY

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EXECUTIVE SUMMARY

This report describes a roadway traffic noise assessment undertaken in support of concurrent Zoning By-law Amendment (ZBLA) and Site Plan Control Application (SPA) submissions for a proposed development located 1299 Richmond Road in Ottawa, Ontario. The proposed development features two rectangular towers, Towers A and B, rising 28 and 32-storeys, respectively, atop a 4-storey shared podium. The primary sources of roadway traffic noise are Richmond Road and Sir John A. Macdonald Parkway. Figure 1 illustrates a complete site plan with surrounding context.

The assessment is based on (i) theoretical noise prediction methods that conform to the Ministry of the Environment, Conservation and Parks (MECP) and City of Ottawa requirements; (ii) noise level criteria as specified by MECP's and the City of Ottawa's Environmental Noise Control Guidelines (ENCG); (iii) future vehicular traffic volumes based on the City of Ottawa's Official Plan roadway classifications; and (iv) architectural drawings provided by Quadrangle Architects Limited, provided in May 2023.

The results of the current analysis indicate that Plane-of-Window noise levels will range between 63 and 68 dBA during the daytime period (07:00-23:00) and between 55 and 60 dBA during the nighttime period (23:00-07:00). The highest noise level (68 dBA) occurs at the south façade, which is closest and most exposed to Richmond Road. Building components with a higher Sound Transmission Class (STC) rating will be required where exterior noise levels exceed 65 dBA, as indicated in Figure 3.

Results of the calculations also indicate that the development will require central air conditioning, which will allow occupants to keep windows closed and maintain a comfortable living environment. A Type D Warning Clause will be required on all Lease, Purchase, and Sale Agreements. Additionally, noise levels at receptor 5 (Pool Area), marginally exceeds 55 dBA. As such, a Type A Warning Clause will be required on Lease, Purchase, and Sale Agreements. Both clauses are summarized in section 6.

Stationary noise impacts from the surroundings onto the proposed development are expected to be negligible as the building is not in proximity to any large mechanical equipment. The setback distance between the proposed development and mechanical equipment servicing neighboring buildings is expected to be sufficient in attenuating noise.



With regard to stationary noise impacts of the development on the surroundings and itself, a stationary noise study is recommended for the site during the detailed design once mechanical plans for the proposed building become available. The stationary noise study would assess impacts of stationary noise from rooftop mechanical units serving the proposed building on surrounding noise-sensitive areas. Noise impacts can generally be minimized by judicious selection and placement of the equipment.



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1. INTRODUCTION

Gradient Wind Engineering Inc. (Gradient Wind) was retained by Brigil to undertake a roadway traffic noise assessment in support of concurrent Zoning By-law Amendment (ZBLA) and Site Plan Control Application (SPA) submissions for a proposed development located 1299 Richmond Road in Ottawa, Ontario. This report summarizes the methodology, results, and recommendations related to the assessment of exterior and interior noise levels generated by local roadway traffic.

Our work is based on theoretical noise calculation methods conforming to the City of Ottawa¹ and Ministry of the Environment, Conservation and Parks (MECP)² noise guidelines. Noise calculations were based on architectural drawings provided by Quadrangle Architects Ltd., in May 2023, with future traffic volumes corresponding to the City of Ottawa's Official Plan (OP) roadway classifications.

2. TERMS OF REFERENCE

The subject site is located at 1299 Richmond Road in Ottawa; situated at the northeast corner of Richmond Road and Assaly Road, and bordered by Richmond Road to the southeast, Assaly Road to the southwest, and Starflower Lane to the northeast and northwest. Throughout this report, Richmond Road is referred to as Project South. The proposed development comprises two towers of 32 and 28 storeys, identified as Tower A and Tower B, raising atop a 4-storey podium with a nominally rectangular planform, to the west and east of the subject site, respectively.

At the ground floor, the proposed development comprises residential main entrances to the north and south, indoor amenity space to the north and at the northwest corner, residential space at the northeast corner, elevator cores to the east and west, and retail space throughout the remainder of the space. Access to below grade parking is provided by a ramp via Starflower Lane to the northeast, an outdoor amenity is located central to the subject site along the north elevation, and private patios are located at the northeast corner. Additionally, a park land area is proposed along the west elevation of the proposed development. Levels 2-4 are reserved for residential use, and the building steps back from the north

¹ City of Ottawa Environmental Noise Control Guidelines, January 2016

² Ontario Ministry of the Environment and Climate Change – Environmental Noise Guidelines, Publication NPC-300, Queens Printer for Ontario, Toronto, 2013



elevation at Level 2 to accommodate private terraces. Level 5 includes lounge and bar space to the west, a central indoor pool, a gym and yoga room to the east, and residential space throughout the remainder of the level. Also, the building steps back from all elevations at Level 5 to accommodate private terraces and common amenity terraces. The common amenity terraces at Level 5 are located central to the north, and to the southeast and southwest, adjacent to the indoor pool. Levels 6-32 of Tower A and Levels 6-28 of Tower B are reserved for residential use. The MPH level of Tower A includes a party room to the east, a games room to the north, and mechanical room to the southeast. Tower A is served by two common amenity balconies to the north and south of the MPH Level.

The near-field surroundings, defined as an area within 200 m of the subject site, includes two high-rise residential buildings to the immediate east, a cluster of high-rise buildings to the northeast, a cluster of mid- and high-rise residential buildings to the south across Richmond Road, two isolated high-rise buildings to the west-southwest, and a mix of primarily low-rise massing and green space from the northwest clockwise to the southeast.

Stationary noise impacts from the surroundings onto the proposed development are expected to be negligible as the building is not in proximity to any large mechanical equipment. The setback distance between the proposed development and mechanical equipment servicing neighboring buildings is expected to be sufficient in attenuating noise.

The primary sources of noise impacting the development are the major roadways of Richmond Road (Arterial), and Sir John A. Macdonald Parkway (federally owned parkway). The new LRT system is more than 250 m to the east of the development; therefore, it is not considered a significant source of noise and vibrations.

3. OBJECTIVES

The principal objectives of this study are to (i) calculate the future noise levels on the study buildings produced by local roadway traffic, and (ii) ensure that interior and exterior noise levels do not exceed the allowable limits specified by the City of Ottawa's Environmental Noise Control Guidelines and the MECP Guidelines as outlined in Section 4.2 of this report.

4. METHODOLOGY

4.1 Background

Noise can be defined as any obtrusive sound. It is created at a source, transmitted through a medium, such as air, and intercepted by a receiver. Noise may be characterized in terms of the power of the source or the sound pressure at a specific distance. While the power of a source is characteristic of that particular source, the sound pressure depends on the location of the receiver and the path that the noise takes to reach the receiver. Measurement of noise is based on the decibel unit, dBA, which is a logarithmic ratio referenced to a standard noise level (2×10^{-5} Pascals). The 'A' suffix refers to a weighting scale, which better represents how the noise is perceived by the human ear. With this scale, a doubling of power results in a 3 dBA increase in measured noise levels and is just perceptible to most people. An increase of 10 dBA is often perceived to be twice as loud.

4.2 Roadway Traffic Noise

4.2.1 Criteria for Roadway Traffic Noise

For surface roadway traffic noise, the equivalent sound energy level, L_{eq} , provides a measure of the time varying noise levels, which is well correlated with the annoyance of sound. It is defined as the continuous sound level, which has the same energy as a time varying noise level over a period of time. For roadways, the L_{eq} is commonly calculated on the basis of a 16-hour (L_{eq16}) daytime (07:00-23:00) / 8-hour (L_{eq8}) nighttime (23:00-07:00) split to assess its impact on residential buildings. The City of Ottawa's Environmental Noise Control Guidelines (ENCG) specifies that the recommended indoor noise limit range (that is relevant to this study) is 50, 45 and 40 dBA for living rooms and sleeping quarters respectively for roadway as listed in Table 1. Based on Gradient Wind's experience, more comfortable indoor noise levels should be targeted, towards 42, 37, and 32 dBA, respectively, to control peak noise and deficiencies in building envelope construction.

TABLE 1: INDOOR SOUND LEVEL CRITERIA (ROAD)³

Type of Space	Time Period	L _{eq} (dBA)
General offices, reception areas, retail stores , etc.	07:00 – 23:00	50
Living/dining/den areas of residences , hospitals, schools, nursing/retirement homes, day-care centres, theatres, places of worship, libraries, individual or semi-private offices, conference rooms, etc.	07:00 – 23:00	45
Sleeping quarters of hotels/motels	23:00 – 07:00	45
Sleeping quarters of residences , hospitals, nursing/retirement homes, etc.	23:00 – 07:00	40

Predicted noise levels at the plane of window (POW) dictate the action required to achieve the recommended sound levels. An open window is considered to provide a 10 dBA reduction in noise, while a standard closed window is capable of providing a minimum 20 dBA noise reduction⁴. A closed window due to a ventilation requirement will bring noise levels down to achieve an acceptable indoor environment⁵. Therefore, where noise levels exceed 55 dBA daytime and 50 dBA nighttime, the ventilation for the building should consider the need for having windows and doors closed, which triggers the need for forced air heating with provision for central air conditioning. Where noise levels exceed 65 dBA daytime and 60 dBA nighttime, air conditioning will be required and building components will require higher levels of sound attenuation⁶.

4.2.2 Theoretical Roadway Noise Predictions

Noise predictions were performed with the aid of the MECP computerized noise assessment program, STAMSON 5.04, for road analysis. Appendix A includes the STAMSON 5.04 input and output data.

³ Adapted from ENCG 2016 – Tables 2.2b and 2.2c

⁴ Burberry, P.B. (2014). Mitchell’s Environment and Services. Routledge, Page 125

⁵ MOECP, Environmental Noise Guidelines, NPC 300 – Part C, Section 7.8

⁶ MOECP, Environmental Noise Guidelines, NPC 300 – Part C, Section 7.1.3

Roadway traffic noise calculations were performed by treating each roadway segment as separate line sources of noise. In addition to the traffic volumes summarized in Table 2, theoretical noise predictions were based on the following parameters:

- Truck traffic on all roadways was assumed to comprise 5% heavy trucks and 7% medium trucks, as per ENCG requirements for noise level predictions.
- The day/night split for all streets was taken to be 92%/8%, respectively.
- Ground surfaces were taken to be reflective due to the presence of hard (paved) ground.
- Topography was assumed to be a flat/gentle slope surrounding the study building.
- Noise receptors were placed at 7 locations around the study area (see Figure 2).
- Receptor distances and exposure angles are illustrated in Figures A1 and A2.

4.2.3 Roadway Traffic Volumes

The ENCG dictates that noise calculations should consider future sound levels based on a roadway’s classification at the mature state of development. Therefore, traffic volumes are based on the roadway classifications outlined in the City of Ottawa’s Official Plan (OP) and Transportation Master Plan⁷ which provide additional details on future roadway expansions. Average Annual Daily Traffic (AADT) volumes are then based on data in Table B1 of the ENCG for each roadway classification. Table 2 (below) summarizes the AADT values used for each roadway included in this assessment.

TABLE 2: ROADWAY TRAFFIC DATA

Segment	Roadway Traffic Data	Speed Limit (km/h)	Traffic Volumes
Richmond Road	2-Lane Urban Arterial (2-UAU)	50	15,000
Sir John A. Macdonald Parkway	4-Lane Urban Arterial Divided (2-UAD)	60	35,000

⁷ City of Ottawa Transportation Master Plan, November 2013

4.3 Indoor Noise Calculations

The difference between outdoor and indoor noise levels is the noise attenuation provided by the building envelope. According to common industry practice, complete walls and individual wall elements are rated according to the Sound Transmission Class (STC). The STC ratings of common residential walls built in conformance with the Ontario Building Code (2020) typically exceed STC 35, depending on exterior cladding, thickness and interior finish details. For example, brick veneer walls can achieve STC 50 or more. Standard commercially sided exterior metal stud walls have around STC 45. Standard good quality double-glazed non-operable windows can have STC ratings ranging from 25 to 40, depending on the window manufacturer, pane thickness and inter-pane spacing.

As per Section 4.2, when daytime noise levels from road sources at the plane of the window exceed 65 dBA, calculations must be performed to evaluate the sound transmission quality of the building components to ensure acceptable indoor noise levels. The calculation procedure⁸ considers:

- Indoor sound level criteria, which varies according to the intended use of a space
- Window type and total area as a percentage of total room floor area
- Exterior wall type and total area as a percentage of the total room floor area
- Acoustic absorption characteristics of the room
- Outdoor noise source type and approach geometry

Based on published research⁹, exterior walls possess specific sound attenuation characteristics that are used as a basis for calculating the required STC ratings of windows in the same partition. Due to the limited information available at the time of the study detailed floor layouts and building elevations have not been finalized; therefore, detailed STC calculations could not be performed at this time. As a guideline, the anticipated STC requirements for windows have been estimated based on the overall noise reduction required for each intended use of space (STC = outdoor noise level – targeted indoor noise levels).

⁸ Building Practice Note: Controlling Sound Transmission into Buildings by J.D. Quirt, National Research Council of Canada, September 1985

⁹ CMHC, Road & Rail Noise: Effects on Housing

5. RESULTS AND DISCUSSION

5.1 Roadway Traffic Noise Levels

The results of the roadway traffic noise calculations are summarized in Table 3 below. A complete set of input and output data from all STAMSON 5.04 calculations are available in Appendix A.

TABLE 3: EXTERIOR NOISE LEVELS DUE TO ROAD TRAFFIC

Receptor Number	Receptor Height Above Grade (m)	Receptor Location	STAMSON 5.04 Noise Level (dBA)	
			Day	Night
1	98.4	POW / Tower B, South Façade, Level 32	68	60
2	98.4	POW / Tower B, West Façade, Level 32	65	57
3	98.4	POW / Tower B, East Façade, Level 32	64	57
4	86.5	POW / Tower A, East Façade, Level 28	63	55
5	21.0	OLA / Level 5 Outdoor Amenity Area (Pool Area)	56	N/A
6	6.5	OLA / Level 2 Private Terraces	45	N/A
7	1.5	OLA / Ground Level Outdoor Amenity	44	N/A

*Noise levels during the nighttime are not considered as per ENCG

The results of the current analysis indicate that Plane-of-Window noise levels will range between 63 and 68 dBA during the daytime period (07:00-23:00) and between 55 and 60 dBA during the nighttime period (23:00-07:00). The highest noise level (68 dBA) occurs at the south façade, which is closest and most exposed to Richmond Road.

Noise levels at receptor 5 (Pool Area) identified as an Outdoor Living Area (OLAs), marginally exceeds 55 dBA. As such, a Warning Clause will be required on Lease, Purchase, and Sale Agreements, as summarized in Section 6.

5.2 Noise Control Measures

The noise levels predicted due to roadway traffic exceed the criteria listed in Section 4.2 for building components. As discussed in Section 4.3, the anticipated STC requirements for windows have been estimated based on the overall noise reduction required for each intended use of space (STC = outdoor

noise level – targeted indoor noise levels). As per city of Ottawa requirements, detailed STC calculations will be required to be completed prior to building permit application for each unit type. The STC requirements for the windows are summarized below for various units within the development (see Figure 3):

- **Bedroom Windows**

- (i) Bedroom windows facing south will require a minimum STC of 31.
- (i) All other bedroom windows are to satisfy Ontario Building Code (OBC 2020) requirements.

- **Living Room Windows**

- (i) Living Room windows facing south will require a minimum STC of 26.
- (ii) All other living room windows are to satisfy Ontario Building Code (OBC 2020) requirements.

- **Exterior Walls**

- (i) Exterior wall components on the north and east façades will require a minimum STC of 45, which will be achieved with brick cladding or an acoustical equivalent according to NRC test data¹⁰

The STC requirements apply to windows, doors, spandrel panels and curtainwall elements. Exterior wall components on these façades are recommended to have a minimum STC of 45, where a window/wall system is used. A review of window supplier literature indicates that the specified STC ratings can be achieved by a variety of window systems having a combination of glass thickness and inter-pane spacing. We have specified an example window configuration, however several manufacturers and various combinations of window components, such as those proposed, will offer the necessary sound attenuation rating. The specified STC requirements also apply to swinging and/or sliding patio doors.

Results of the calculations also indicate that the development will require central air conditioning, which will allow occupants to keep windows closed and maintain a comfortable living environment. In addition to ventilation requirements, Warning Clauses will also be required in all Agreements of Purchase and Sale and Lease Agreements, as summarized in Section 6.

¹⁰ J.S. Bradley and J.A. Birta. Laboratory Measurements of the Sound Insulation of Building Façade Elements, National Research Council October 2000.

6. CONCLUSIONS AND RECOMMENDATIONS

The results of the analysis indicate that Plane-of-Window noise levels will range between 63 and 68 dBA during the daytime period (07:00-23:00) and between 55 and 60 dBA during the nighttime period (23:00-07:00). The highest noise level (68 dBA) occurs at the south façade, which is closest and most exposed to Richmond Road. Building components with a higher Sound Transmission Class (STC) rating will be required where exterior noise levels exceed 65 dBA, as indicated in Figure 3. Results of the calculations also indicate that the development will require central air conditioning, which will allow occupants to keep windows closed and maintain a comfortable living environment. A Type D Warning Clause will be required on all Lease, Purchase, and Sale Agreements, as seen below:

Type D:

"This dwelling unit has been supplied with a central air conditioning system which will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the sound level limits of the Municipality and the Ministry of the Environment."

Noise levels at receptor 5 (Pool Area) identified as an Outdoor Living Area (OLA), marginally exceeds 55 dBA. As such, a Warning Clause will be required on Lease, Purchase, and Sale Agreements, as summarized below:

Type A

"Purchasers/tenants are advised that sound levels due to increasing road traffic may occasionally interfere with some activities of the dwelling occupants as the sound levels exceed the sound level limits of the Municipality and the Ministry of the Environment."

Stationary noise impacts from the environment onto the proposed development are expected to be negligible as the building is not in proximity to any large mechanical equipment. The setback distance between the proposed development and mechanical equipment servicing neighboring buildings is expected to be sufficient in attenuating noise.

With regard to stationary noise impacts of the development on the surroundings and itself, a stationary noise study is recommended for the site during the detailed design once mechanical plans for the



proposed building become available. The stationary noise study would assess impacts of stationary noise from rooftop mechanical units serving the proposed building on surrounding noise-sensitive areas. Noise impacts can generally be minimized by judicious selection and placement of the equipment.

This concludes our roadway traffic noise assessment and report. If you have any questions or wish to discuss our findings, please advise us. In the interim, we thank you for the opportunity to be of service.

Sincerely,

Gradient Wind Engineering Inc.

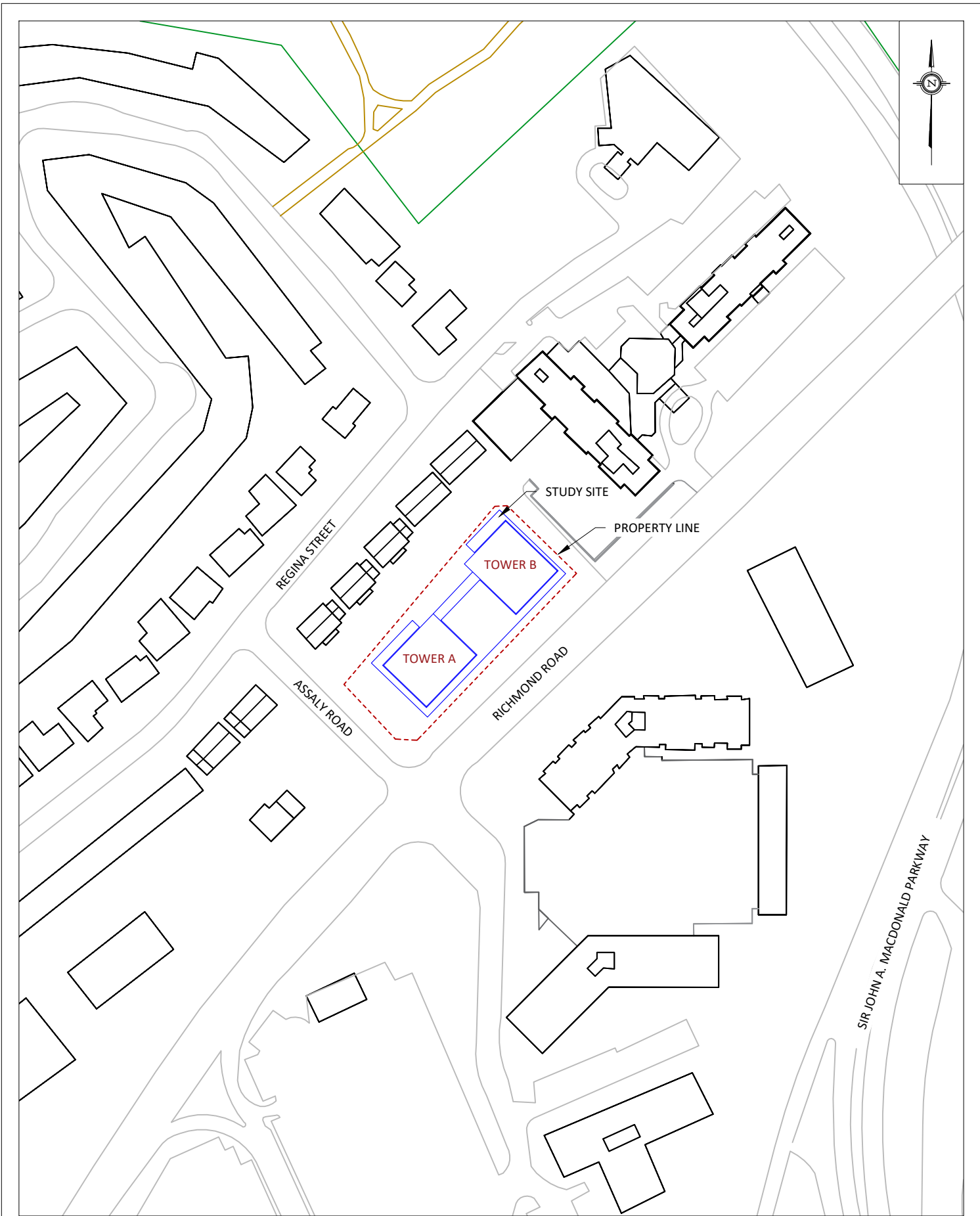


Essraa Alqassab, B.A.Sc.
Junior Environmental Scientist

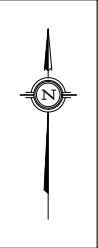


Joshua Foster, P.Eng.
Lead Engineer

Gradient Wind File #23-057-Traffic Noise



PROJECT	1299 RICHMOND ROAD, OTTAWA ROADWAY TRAFFIC NOISE ASSESSMENT	
SCALE	1:2000 (APPROX.)	DRAWING NO. GW23-057-1
DATE	MAY 11, 2023	DRAWN BY E.A.



- 1 OLA RECEPTOR
- 1 POW RECEPTOR

PROJECT	1299 RICHMOND ROAD, OTTAWA ROADWAY TRAFFIC NOISE ASSESSMENT	
SCALE	1:2000 (APPROX.)	DRAWING NO. GW23-057-2
DATE	MAY 11, 2023	DRAWN BY E.A.



 BEDROOM/LIVING ROOM WINDOWS: STC 31/26

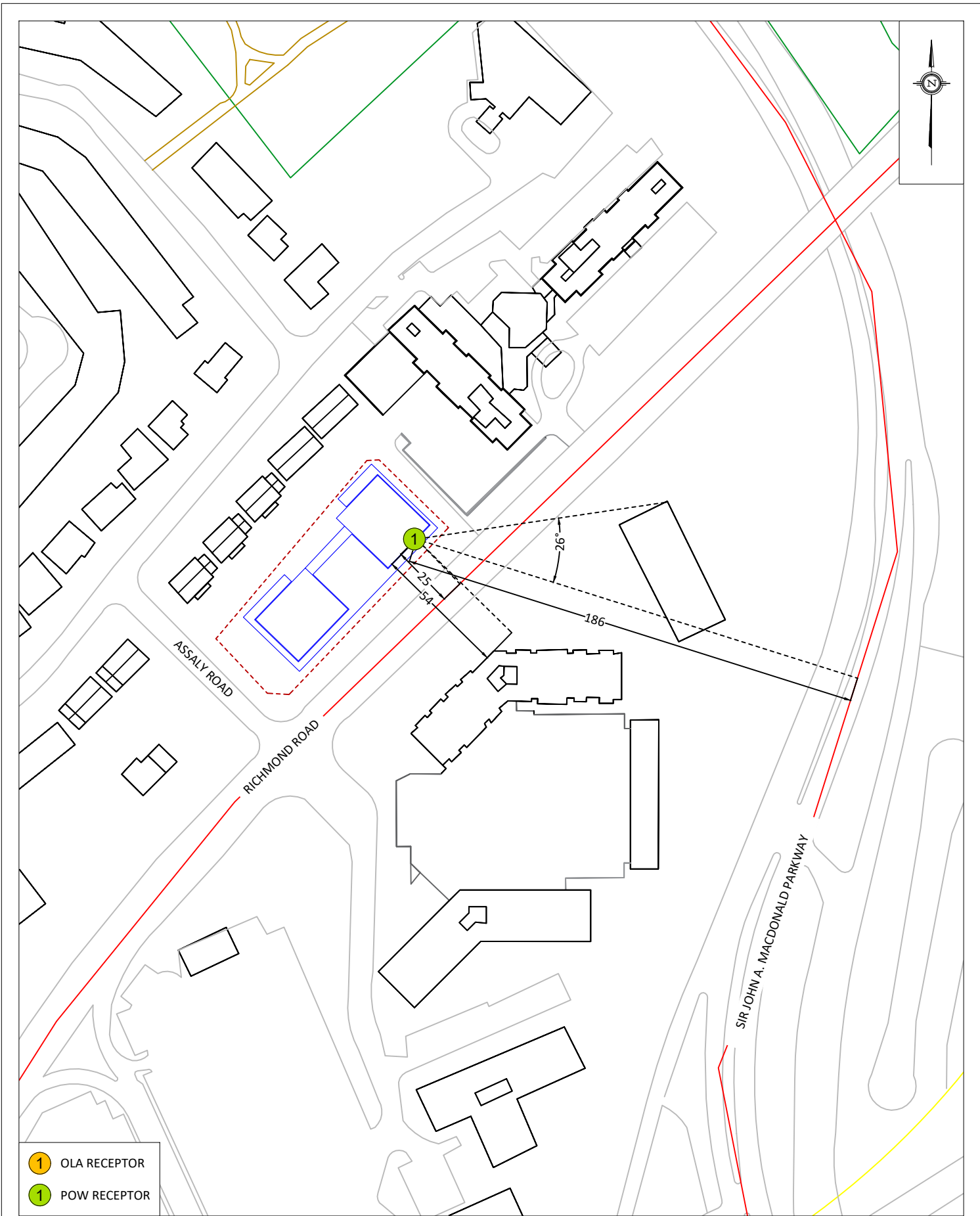
GRADIENTWIND ENGINEERS & SCIENTISTS 127 WALGREEN ROAD, OTTAWA, ON 613 836 0934 • GRADIENTWIND.COM	PROJECT 1299 RICHMOND ROAD, OTTAWA ROADWAY TRAFFIC NOISE ASSESSMENT		DESCRIPTION FIGURE 3: WINDOW STC RECOMMENDATIONS
	SCALE 1:200 (APPROX.)	DRAWING NO. GW23-057-3	
	DATE MAY 11, 2023	DRAWN BY E.A.	

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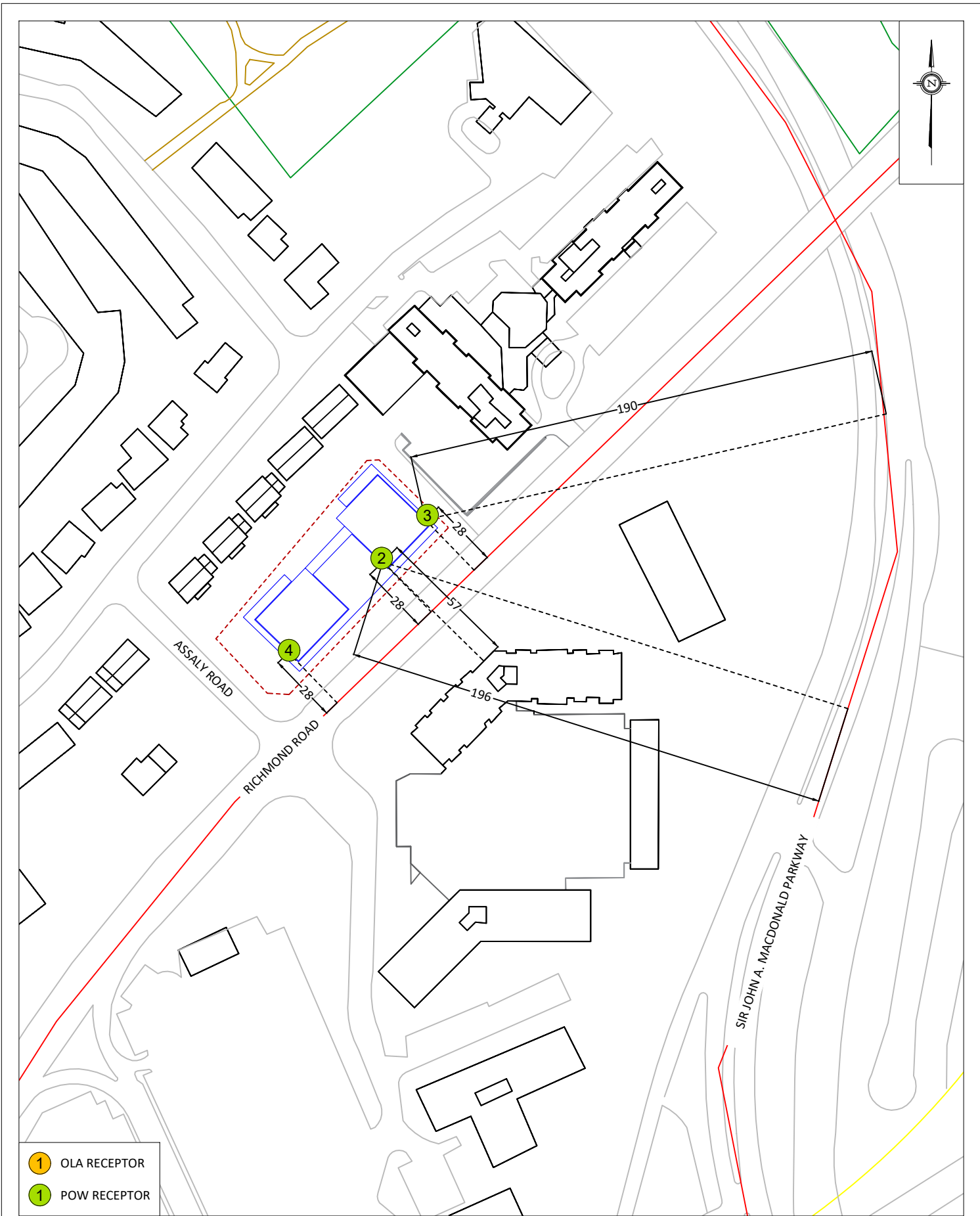
APPENDIX A STAMSON CALCULATIONS



- 1 OLA RECEPTOR
- 1 POW RECEPTOR

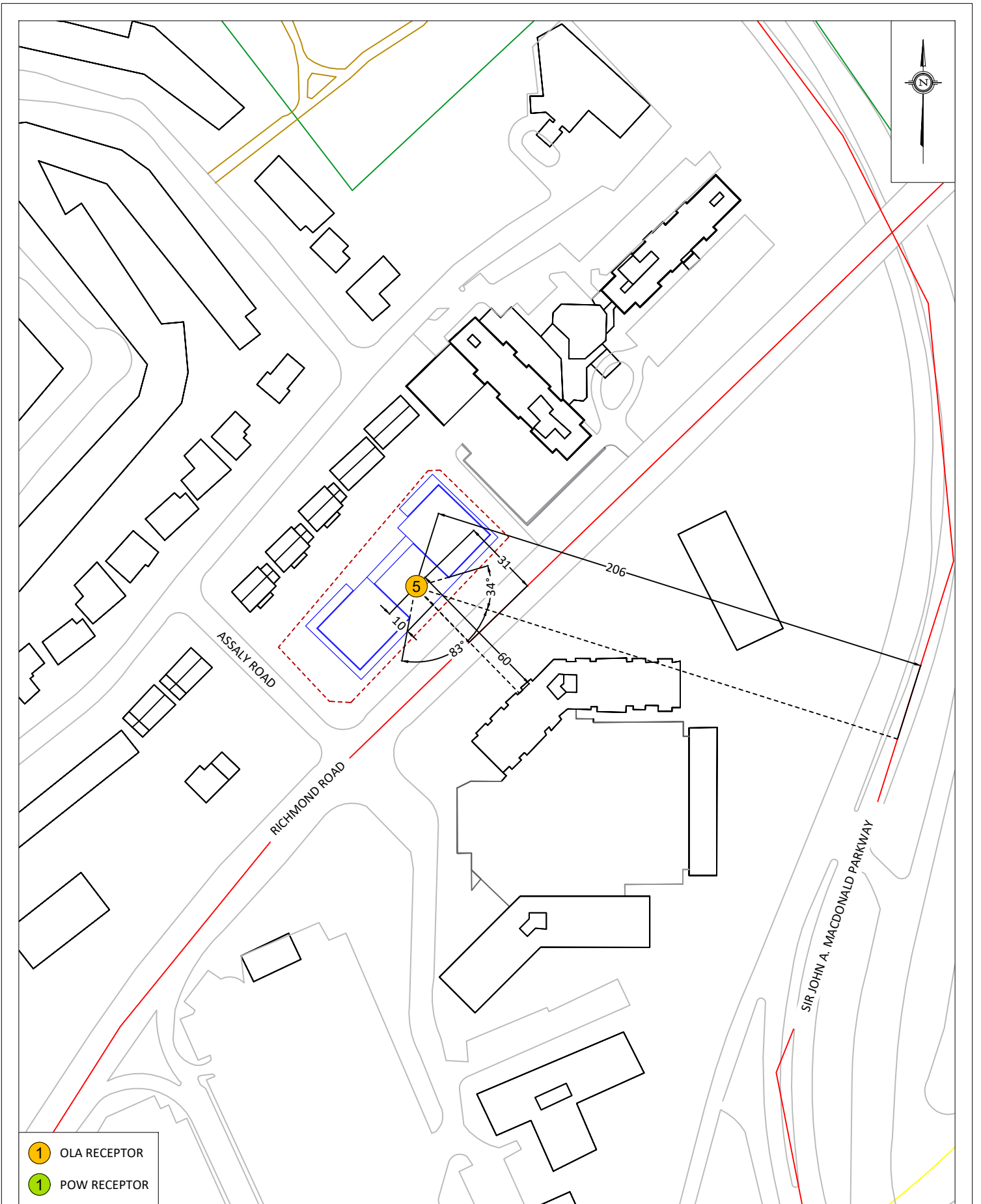
<p>GRADIENTWIND ENGINEERS & SCIENTISTS</p> <p>127 WALGREEN ROAD, OTTAWA, ON 613 836 0934 • GRADIENTWIND.COM</p>	PROJECT	1299 RICHMOND ROAD, OTTAWA ROADWAY TRAFFIC NOISE ASSESSMENT		DESCRIPTION	
	SCALE	1:2000 (APPROX.)	DRAWING NO.		GW23-057-A1
	DATE	MAY 11, 2023	DRAWN BY		E.A.

FIGURE A1:
STAMSON PARAMETERS (1/4)



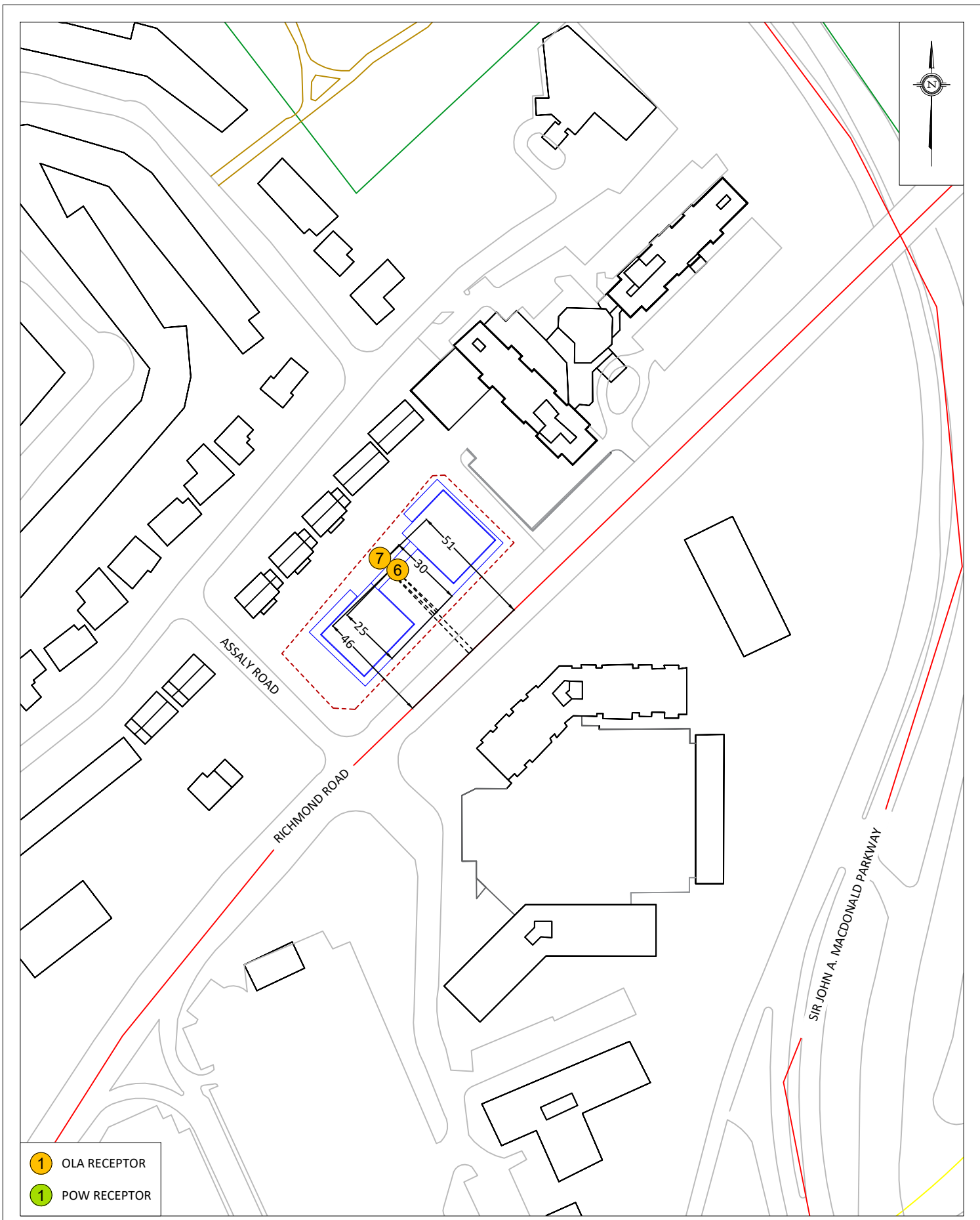
- 1 OLA RECEPTOR
- 1 POW RECEPTOR

<p>GRADIENTWIND ENGINEERS & SCIENTISTS</p> <p>127 WALGREEN ROAD, OTTAWA, ON 613 836 0934 • GRADIENTWIND.COM</p>	<p>PROJECT 1299 RICHMOND ROAD, OTTAWA ROADWAY TRAFFIC NOISE ASSESSMENT</p>	<p>DESCRIPTION</p>	
	<p>SCALE 1:2000 (APPROX.)</p>	<p>DRAWING NO. GW23-057-A2</p>	<p>FIGURE A2: STAMSON PARAMETERS (2/4)</p>
	<p>DATE MAY 11, 2023</p>	<p>DRAWN BY E.A.</p>	



- 1 OLA RECEPTOR
- 1 POW RECEPTOR

GRADIENTWIND ENGINEERS & SCIENTISTS 127 WALGREEN ROAD, OTTAWA, ON 613 836 0934 • GRADIENTWIND.COM	PROJECT 1299 RICHMOND ROAD, OTTAWA ROADWAY TRAFFIC NOISE ASSESSMENT	DESCRIPTION FIGURE A3: STAMSON PARAMETERS (3/4)	
	SCALE 1:2000 (APPROX.)	DRAWING NO. GW23-057-A3	
	DATE MAY 11, 2023	DRAWN BY E.A.	



- 7 OLA RECEPTOR
- 1 POW RECEPTOR

<p>GRADIENTWIND ENGINEERS & SCIENTISTS</p> <p>127 WALGREEN ROAD, OTTAWA, ON 613 836 0934 • GRADIENTWIND.COM</p>	<p>PROJECT: 1299 RICHMOND ROAD, OTTAWA ROADWAY TRAFFIC NOISE ASSESSMENT</p>	<p>DESCRIPTION:</p> <p style="text-align: center;">FIGURE A4: STAMSON PARAMETERS (4/4)</p>	
	<p>SCALE: 1:2000 (APPROX.)</p>	<p>DRAWING NO.: GW23-057-A4</p>	
	<p>DATE: MAY 11, 2023</p>	<p>DRAWN BY: E.A.</p>	

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STAMSON 5.0 NORMAL REPORT Date: 11-05-2023 17:11:00
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r1.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: Richmond Rd (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: Richmond Rd (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 25.00 / 25.00 m
Receiver height : 98.40 / 98.40 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

Road data, segment # 2: SJAM Parkway (day/night)

Car traffic volume : 28336/2464 veh/TimePeriod *
Medium truck volume : 2254/196 veh/TimePeriod *
Heavy truck volume : 1610/140 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 35000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00



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Medium Truck % of Total Volume      :    7.00
Heavy Truck  % of Total Volume      :    5.00
Day (16 hrs) % of Total Volume      :   92.00
  
```

Data for Segment # 2: SJAM Parkway (day/night)

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-----
Angle1  Angle2      : -90.00 deg   90.00 deg
Wood depth          :          0   (No woods.)
No of house rows   :          0 / 0
Surface            :          2   (Reflective ground surface)
Receiver source distance : 186.00 / 186.00 m
Receiver height    :   98.40 / 98.40 m
Topography         :          2   (Flat/gentle slope; with barrier)
Barrier angle1     : -26.00 deg   Angle2 : 90.00 deg
Barrier height     :   11.00 m
Barrier receiver distance : 54.00 / 54.00 m
Source elevation   :    0.00 m
Receiver elevation :    0.00 m
Barrier elevation  :    0.00 m
Reference angle    :    0.00
  
```

Results segment # 1: Richmond Rd (day)

Source height = 1.50 m

ROAD (0.00 + 66.26 + 0.00) = 66.26 dBA

SubLeq	Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

66.26	-90	90	0.00	68.48	0.00	-2.22	0.00	0.00	0.00	0.00
-------	-----	----	------	-------	------	-------	------	------	------	------

Segment Leq : 66.26 dBA

Results segment # 2: SJAM Parkway (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	98.40	70.27	70.27



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ROAD (58.25 + 60.83 + 0.00) = 62.74 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--									
-90	-26	0.00	73.68	0.00	-10.93	-4.49	0.00	0.00	0.00
58.25									

--									
-26	90	0.00	73.68	0.00	-10.93	-1.91	0.00	0.00	-0.00
60.83*									

-26	90	0.00	73.68	0.00	-10.93	-1.91	0.00	0.00	0.00
60.83									

* Bright Zone !

Segment Leq : 62.74 dBA

Total Leq All Segments: 67.86 dBA

Results segment # 1: Richmond Rd (night)

Source height = 1.50 m

ROAD (0.00 + 58.66 + 0.00) = 58.66 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--									
-90	90	0.00	60.88	0.00	-2.22	0.00	0.00	0.00	0.00
58.66									

Segment Leq : 58.66 dBA

Results segment # 2: SJAM Parkway (night)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
-----	-----	-----	-----



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1.50 ! 98.40 ! 70.27 ! 70.27

ROAD (50.65 + 53.24 + 0.00) = 55.15 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

SubLeq	-----									
--										
50.65	-90	-26	0.00	66.08	0.00	-10.93	-4.49	0.00	0.00	0.00

--										
53.23*	-26	90	0.00	66.08	0.00	-10.93	-1.91	0.00	0.00	-0.00
53.24	-26	90	0.00	66.08	0.00	-10.93	-1.91	0.00	0.00	0.00

--										

* Bright Zone !

Segment Leq : 55.15 dBA

Total Leq All Segments: 60.26 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 67.86
 (NIGHT): 60.26



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STAMSON 5.0 NORMAL REPORT Date: 12-05-2023 08:49:46
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r2.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: Richmond (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: Richmond (day/night)

Angle1 Angle2 : 0.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 28.00 / 28.00 m
Receiver height : 98.40 / 98.40 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

Road data, segment # 2: SJAM Parkway (day/night)

Car traffic volume : 28336/2464 veh/TimePeriod *
Medium truck volume : 2254/196 veh/TimePeriod *
Heavy truck volume : 1610/140 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 35000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00



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```

Medium Truck % of Total Volume      :    7.00
Heavy Truck  % of Total Volume      :    5.00
Day (16 hrs) % of Total Volume      :   92.00
    
```

Data for Segment # 2: SJAM Parkway (day/night)

```

-----
Angle1  Angle2      :   0.00 deg   90.00 deg
Wood depth          :           0   (No woods.)
No of house rows   :           0 / 0
Surface            :           2   (Reflective ground surface)
Receiver source distance : 196.00 / 196.00 m
Receiver height    :   98.40 / 98.40 m
Topography         :           2   (Flat/gentle slope; with barrier)
Barrier angle1     :   0.00 deg   Angle2 : 90.00 deg
Barrier height     :   11.00 m
Barrier receiver distance : 57.00 / 57.00 m
Source elevation   :           0.00 m
Receiver elevation :           0.00 m
Barrier elevation  :           0.00 m
Reference angle    :           0.00
    
```

Results segment # 1: Richmond (day)

Source height = 1.50 m

ROAD (0.00 + 62.76 + 0.00) = 62.76 dBA

SubLeq	Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

62.76	0	90	0.00	68.48	0.00	-2.71	-3.01	0.00	0.00	0.00
-------	---	----	------	-------	------	-------	-------	------	------	------

Segment Leq : 62.76 dBA

Results segment # 2: SJAM Parkway (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	98.40	70.22	70.22



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ROAD (0.00 + 59.50 + 0.00) = 59.50 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

0	90	0.00	73.68	0.00	-11.16	-3.01	0.00	0.00	-0.00
59.50*									
0	90	0.00	73.68	0.00	-11.16	-3.01	0.00	0.00	0.00
59.50									

* Bright Zone !

Segment Leq : 59.50 dBA

Total Leq All Segments: 64.44 dBA

Results segment # 1: Richmond (night)

Source height = 1.50 m

ROAD (0.00 + 55.16 + 0.00) = 55.16 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

0	90	0.00	60.88	0.00	-2.71	-3.01	0.00	0.00	0.00
55.16									

Segment Leq : 55.16 dBA

Results segment # 2: SJAM Parkway (night)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	98.40	70.22	70.22

ROAD (0.00 + 51.91 + 0.00) = 51.91 dBA



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Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

SubLeq

--									
0	90	0.00	66.08	0.00	-11.16	-3.01	0.00	0.00	-0.00
51.90*									
0	90	0.00	66.08	0.00	-11.16	-3.01	0.00	0.00	0.00
51.91									

* Bright Zone !

Segment Leq : 51.91 dBA

Total Leq All Segments: 56.84 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 64.44
(NIGHT): 56.84



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STAMSON 5.0 NORMAL REPORT Date: 11-05-2023 17:14:06
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r3.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: Richmond (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: Richmond (day/night)

Angle1 Angle2 : -90.00 deg 0.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 28.00 / 28.00 m
Receiver height : 98.40 / 98.40 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

Road data, segment # 2: SJAM Parkway (day/night)

Car traffic volume : 28336/2464 veh/TimePeriod *
Medium truck volume : 2254/196 veh/TimePeriod *
Heavy truck volume : 1610/140 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 35000
Percentage of Annual Growth : 0.00



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```

Number of Years of Growth      : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume  : 5.00
Day (16 hrs) % of Total Volume : 92.00
    
```

Data for Segment # 2: SJAM Parkway (day/night)

```

-----
Angle1  Angle2      : -90.00 deg  0.00 deg
Wood depth      : 0 (No woods.)
No of house rows : 0 / 0
Surface         : 2 (Reflective ground surface)
Receiver source distance : 190.00 / 190.00 m
Receiver height : 98.40 / 98.40 m
Topography      : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00
    
```

Results segment # 1: Richmond (day)

Source height = 1.50 m

ROAD (0.00 + 62.76 + 0.00) = 62.76 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

```

-----
--
-90      0      0.00  68.48  0.00  -2.71  -3.01  0.00  0.00  0.00
62.76
-----
--
    
```

Segment Leq : 62.76 dBA

Results segment # 2: SJAM Parkway (day)

Source height = 1.50 m

ROAD (0.00 + 59.64 + 0.00) = 59.64 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

```

-----
--
-90      0      0.00  73.68  0.00 -11.03  -3.01  0.00  0.00  0.00
59.64
-----
--
    
```

Segment Leq : 59.64 dBA



Total Leq All Segments: 64.48 dBA

Results segment # 1: Richmond (night)

Source height = 1.50 m

ROAD (0.00 + 55.16 + 0.00) = 55.16 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

--									
-90	0	0.00	60.88	0.00	-2.71	-3.01	0.00	0.00	0.00
55.16									

--

Segment Leq : 55.16 dBA

Results segment # 2: SJAM Parkway (night)

Source height = 1.50 m

ROAD (0.00 + 52.04 + 0.00) = 52.04 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

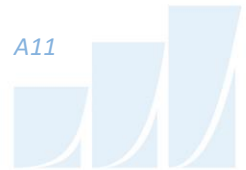
--									
-90	0	0.00	66.08	0.00	-11.03	-3.01	0.00	0.00	0.00
52.04									

--

Segment Leq : 52.04 dBA

Total Leq All Segments: 56.88 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 64.48
(NIGHT): 56.88



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STAMSON 5.0 NORMAL REPORT Date: 11-05-2023 10:47:54
 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r4.te Time Period: Day/Night 16/8 hours
 Description:

Road data, segment # 1: Richmond (day/night)

```
-----
Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)
```

* Refers to calculated road volumes based on the following input:

```
24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00
```

Data for Segment # 1: Richmond (day/night)

```
-----
Angle1 Angle2 : 0.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 28.00 / 28.00 m
Receiver height : 86.50 / 86.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00
```

Results segment # 1: Richmond (day)

Source height = 1.50 m

ROAD (0.00 + 62.76 + 0.00) = 62.76 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
--------	--------	-------	--------	-------	-------	-------	-------	-------	-------

SubLeq										
62.76	0	90	0.00	68.48	0.00	-2.71	-3.01	0.00	0.00	0.00



Segment Leq : 62.76 dBA

Total Leq All Segments: 62.76 dBA

Results segment # 1: Richmond (night)

Source height = 1.50 m

ROAD (0.00 + 55.16 + 0.00) = 55.16 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj
SubLeq

--
0 90 0.00 60.88 0.00 -2.71 -3.01 0.00 0.00 0.00
55.16

--

Segment Leq : 55.16 dBA

Total Leq All Segments: 55.16 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 62.76
(NIGHT): 55.16



GRADIENTWIND

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STAMSON 5.0 NORMAL REPORT Date: 12-05-2023 08:51:15
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r5.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: Richmond (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: Richmond (day/night)

Angle1 Angle2 : -34.00 deg 83.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 31.00 / 31.00 m
Receiver height : 21.00 / 21.00 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -34.00 deg Angle2 : 83.00 deg
Barrier height : 19.50 m
Barrier receiver distance : 10.00 / 10.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Road data, segment # 2: SJAM Parkway (day/night)

Car traffic volume : 28336/2464 veh/TimePeriod *
Medium truck volume : 2254/196 veh/TimePeriod *
Heavy truck volume : 1610/140 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)



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* Refers to calculated road volumes based on the following input:

```

24 hr Traffic Volume (AADT or SADT): 35000
Percentage of Annual Growth          : 0.00
Number of Years of Growth           : 0.00
Medium Truck % of Total Volume      : 7.00
Heavy Truck % of Total Volume       : 5.00
Day (16 hrs) % of Total Volume      : 92.00
    
```

Data for Segment # 2: SJAM Parkway (day/night)

```

-----
Angle1   Angle2           : -34.00 deg   83.00 deg
Wood depth           : 0           (No woods.)
No of house rows    : 0 / 0
Surface             : 2           (Reflective ground surface)
Receiver source distance : 206.00 / 206.00 m
Receiver height      : 21.00 / 21.00 m
Topography          : 2           (Flat/gentle slope; with barrier)
Barrier angle1      : -34.00 deg   Angle2 : 83.00 deg
Barrier height      : 16.00 m
Barrier receiver distance : 60.00 / 60.00 m
Source elevation    : 0.00 m
Receiver elevation   : 0.00 m
Barrier elevation    : 0.00 m
Reference angle     : 0.00
    
```

Results segment # 1: Richmond (day)

Source height = 1.50 m

Barrier height for grazing incidence

```

-----
Source      ! Receiver      ! Barrier      ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.50 !      21.00 !      14.71 !      14.71
    
```

ROAD (0.00 + 47.37 + 0.00) = 47.37 dBA

```

Angle1 Angle2  Alpha RefLeq  P.Adj  D.Adj  F.Adj  W.Adj  H.Adj  B.Adj
SubLeq
    
```

```

-----
--
-34    83    0.00  68.48   0.00  -3.15  -1.87   0.00   0.00 -16.08
47.37
-----
--
    
```

Segment Leq : 47.37 dBA



Results segment # 2: SJAM Parkway (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	21.00	15.32	15.32

ROAD (0.00 + 55.21 + 0.00) = 55.21 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-34	83	0.00	73.68	0.00	-11.38	-1.87	0.00	0.00	-5.21

SubLeq

Segment Leq : 55.21 dBA

Total Leq All Segments: 55.87 dBA

Results segment # 1: Richmond (night)

Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	Receiver Height (m)	Barrier Height (m)	Elevation of Barrier Top (m)
1.50	21.00	14.71	14.71

ROAD (0.00 + 39.78 + 0.00) = 39.78 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
-34	83	0.00	60.88	0.00	-3.15	-1.87	0.00	0.00	-16.08

SubLeq



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Segment Leq : 39.78 dBA

Results segment # 2: SJAM Parkway (night)

 Source height = 1.50 m

Barrier height for grazing incidence

Source Height (m)	! Receiver ! Height (m)	! Barrier ! Height (m)	! Elevation of ! Barrier Top (m)
1.50	21.00	15.32	15.32

ROAD (0.00 + 47.62 + 0.00) = 47.62 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj
SubLeq									

 --
 -34 83 0.00 66.08 0.00 -11.38 -1.87 0.00 0.00 -5.21
 47.62

 --

Segment Leq : 47.62 dBA

Total Leq All Segments: 48.28 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 55.87
 (NIGHT): 48.28



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STAMSON 5.0 NORMAL REPORT Date: 11-05-2023 10:48:36
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r6.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: Richmond Rd (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: Richmond Rd (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 46.00 / 46.00 m
Receiver height : 6.50 / 6.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -90.00 deg Angle2 : 90.00 deg
Barrier height : 19.50 m
Barrier receiver distance : 25.00 / 25.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Results segment # 1: Richmond Rd (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source ! Receiver ! Barrier ! Elevation of



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```

Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.50 !          6.50 !          3.78 !          3.78
    
```

ROAD (0.00 + 44.85 + 0.00) = 44.85 dBA

```

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj
SubLeq
-----
    
```

```

--
-90      90      0.00  68.48   0.00  -4.87   0.00   0.00   0.00  -18.76
44.85
-----
    
```

Segment Leq : 44.85 dBA

Total Leq All Segments: 44.85 dBA

Results segment # 1: Richmond Rd (night)

Source height = 1.50 m

Barrier height for grazing incidence

```

Source      ! Receiver      ! Barrier      ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.50 !          6.50 !          3.78 !          3.78
    
```

ROAD (0.00 + 37.25 + 0.00) = 37.25 dBA

```

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj
SubLeq
-----
    
```

```

--
-90      90      0.00  60.88   0.00  -4.87   0.00   0.00   0.00  -18.76
37.25
-----
    
```

Segment Leq : 37.25 dBA

Total Leq All Segments: 37.25 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 44.85
(NIGHT): 37.25



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STAMSON 5.0 NORMAL REPORT Date: 12-05-2023 08:51:34
MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: r7.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: Richmond Rd (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: Richmond Rd (day/night)

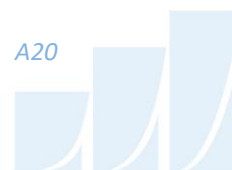
Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 2 (Reflective ground surface)
Receiver source distance : 51.00 / 51.00 m
Receiver height : 1.50 / 1.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -90.00 deg Angle2 : 90.00 deg
Barrier height : 19.50 m
Barrier receiver distance : 30.00 / 30.00 m
Source elevation : 0.00 m
Receiver elevation : 0.00 m
Barrier elevation : 0.00 m
Reference angle : 0.00

Results segment # 1: Richmond Rd (day)

Source height = 1.50 m

Barrier height for grazing incidence

Source ! Receiver ! Barrier ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)



GRADIENTWIND

ENGINEERS & SCIENTISTS

```

-----+-----+-----+-----
          1.50 !           1.50 !           1.50 !           1.50
ROAD (0.00 + 44.21 + 0.00) = 44.21 dBA
Angle1 Angle2  Alpha RefLeq  P.Adj  D.Adj  F.Adj  W.Adj  H.Adj  B.Adj
SubLeq
-----
--
-90      90      0.00  68.48   0.00  -5.31   0.00   0.00   0.00 -18.96
44.21
-----
--

```

Segment Leq : 44.21 dBA
Total Leq All Segments: 44.21 dBA

Results segment # 1: Richmond Rd (night)

Source height = 1.50 m

Barrier height for grazing incidence

```

-----+-----+-----+-----
Source      ! Receiver      ! Barrier      ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
-----+-----+-----+-----
          1.50 !           1.50 !           1.50 !           1.50
ROAD (0.00 + 36.61 + 0.00) = 36.61 dBA
Angle1 Angle2  Alpha RefLeq  P.Adj  D.Adj  F.Adj  W.Adj  H.Adj  B.Adj
SubLeq
-----
--
-90      90      0.00  60.88   0.00  -5.31   0.00   0.00   0.00 -18.96
36.61
-----
--

```

Segment Leq : 36.61 dBA
Total Leq All Segments: 36.61 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 44.21
(NIGHT): 36.61

