SIX (6) STOREY APARTMENT BUILDING SITE

LOT 1

R-PLAN 268160

917 MERIVALE ROAD

CITY OF OTTAWA

SERVICEABILITY REPORT

REPORT No. R-823-102A

T.L. MAK ENGINEERING CONSULTANTS LTD.

AUGUST 2024

REFERENCE FILE NUMBER 823-102

Introduction

The developer of this property is proposing to redevelop the existing residential lot described as Lot 1 Registered Plan 268160 City of Ottawa by constructing a six (6) storey residential apartment building plus a basement consisting of twenty (20)-units, including ten (1)-bedroom units and ten (10) bachelor units.

The municipal address of this property is referenced as 917 Merivale Road and it is located in the City Ward (16 - River). The site is situated on the east side of Merivale Road, south of Crerar Avenue and north of Anna Avenue, see site plan and legal survey plan in Appendix A for details.

The area of this property is ±0.0482 hectares. In addition to the six (6) storey residential building, the other development features will comprise of an interlock paver access to the front entrance plus a concrete sidewalk access along the south side yard to the waste storage and one vehicular entrance asphalt access road, parking areas and an amenity area is also located in the rear yard including landscaped areas along the north side of the site, etc., to meet the City of Ottawa's site plan requirements.

A site geotechnical report was prepared by the owner's soils engineer Yuri Mendez Engineering entitled "Subsurface Investigation Report" 917 Merivale Road (Report No. 63-SPD-R0) dated September 27, 2023 for this proposed development property.

This serviceability report will provide the City of Ottawa with our serviceability brief to address the proposed servicing scheme for this site.

Existing Site Conditions and Servicing

This property is presently occupied by one and one half ($1\,\%$) storey wooden sided residential building. The existing house is located near the front centre on this property with existing gazebo structures located at the rear yard, asphalt surface along the south side yard and gravel plus interlock walkway located along the north side of the property limit which currently provides pedestrian access to the gazebos. For additional details of the site's pre-development conditions, refer to the coloured Google Image (2023) and aerial photography from (GeoOttawa 2022) in Appendix B.

Approximately one half of this site is currently permeable surface covered and consisting of grass/landscaped areas with the remaining areas being roof area, concrete steps, gravel and asphalt surfaces. Presently, most of the landscape areas are concentrated at the rear of lot and at the front yard.

The topography of the land is found to be graded primarily to drain from rear to the front of the lot (east to west). The existing gradient of the property is sloping approximately 1.9% from back to front.

Water and sanitary service lateral currently servicing the existing dwelling on 917 Merivale Road will be removed. The existing water services shall be blanked at the main and the existing house laterals shall be capped at the front property line for re-development of this lot.

As for the availability of underground municipal services, there are existing municipal services along Merivale Road in front of this property consisting of a 450mm diameter storm sewer, a 375mm diameter sanitary sewer, and a 300mm diameter watermain for development of this property. Refer to the City of Ottawa Merivale Road UCC drawing and As-Built plan and profile drawing included in Appendix C for details.

Because the site will be connecting to and outletting into the separated Merivale Road storm sewer located within the Merivale Road road right of way in the City of Ottawa, therefore, the approval exemption under Ontario Regulations 525/98 would apply since storm water discharges from this site will outlet flow into a downstream storm sewer. Thus, an Environmental Compliance Approval (ECA) application will not be required to be submitted to the Ministry.

Proposed Residential Apartment Building Site

A vehicle entrance located at the northwest corner of the lot is proposed to provide vehicular access to this property along with an access roadway from this entranceway to direct vehicular traffic in and out of the site. Vehicular parking will be available at the rear of the site, east of the proposed building.

A. Water Supply

The proposed building located within Pressure Zone 2W at 917 Merivale Road is a 6-storey residential multiunit building with a basement. The building contains twenty (20) total units, ten (10) 1-bedroom, and ten (10) bachelor units. Each floor covers an average area of around 218 m^2 , for a gross floor area of 1,310 m² (excluding the basement).

The building is to be serviced by the 300 mm diameter watermain along Merivale Road. The ground elevation along Merivale Road is approximately 77.9 m.

Demand Projections

The domestic demands were calculated using the City of Ottawa's Water Design Guidelines, where the residential consumption rate of 280 L/cap/d was used to estimate average day

demands (AVDY). Persons per unit (PPU) for each unit were estimated based on the City of Ottawa's Water Design Guidelines.

Following discussions with the City, peaking factors are to be estimated from Table 3-3 of the MECP Design Guidelines for Drinking-Water Systems, given that the proposed development population is less than 500 people. Maximum day (MXDY) demands were calculated by multiplying AVDY demands by a factor of 9.5. Peak hour (PKHR) demands were calculated by multiplying AVDY by a factor of 14.3. **Table 1** shows the estimated domestic demands of the proposed building.

Table 1: Estimated Domestic Demand

Unit Type	Unit	PPU	Concumption	AV	DY	MXE	Y	PKH	R
ome Type	Count	PPU	Consumption	L/d	L/s	L/d	L/s	L/d	L/s
Apartment, 1- Bedroom	10	1.4	000	3,920	0.05	37,240	0.43	56,056	0.65
Apartment, Bachelor	10	1.4	280	3,920	0.05	37,240	0.43	56,056	0.65
Total	20			7,840	0.09	74,480	0.86	112,112	1.30

The fire flow required was determined following the Fire Underwriter Survey (FUS) method and is provided in the attached worksheet. The proposed building will be of wood frame construction. It is understood that the building will be equipped with sprinklers, and that the basement is more than 50% below ground level. The resulting required fire flow is 11,000 L/min (183 L/s) for a duration of 2.25 hours.

Details are provided in the attached **Fire Flow Calculations** (See Appendix D). Furthermore, **Figure 1** found in Appendix D provides separation distances for the FUS calculations. The proposed **Site Plan** attached in Appendix D was used to determine distances from the proposed building to the property lines.

In summary, the estimated water demands for the proposed building are as follows:

- AVDY = 7,840 L/d (0.09 L/s)
- MXDY = 74,480 L/d (0.86 L/s);
- PKHR = 112,112 L/d (1.30 L/s); and,
- Fire Flow (FUS) = 11,000 L/min (183 L/s).

Boundary Conditions

The hydraulic gradeline (HGL) boundary conditions for 917 Merivale Road, as presented in **Table 2**, were provided by the City on May 2, 2024 (see attached **Water Boundary Conditions Email** in Appendix D). Note that slight architectural changes to the buildings were made

following the reception of the boundary conditions, resulting in slightly less water demands. As such, the received boundary conditions are considered conservative and applicable).

Table 2: Boundary Conditions

Demand Scenario	Head (m)
Minimum HGL (Peak Hour)	124.4
Maximum HGL (Average Day)	132.8
Available Fire Flow @ Residual 20 psi	118.0

Hydraulic Analysis

Peak Hour & Average Day

During peak hour demands, the resulting minimum hydraulic gradeline of 124.4 m corresponds to a peak hour pressure of 456 kPa (66 psi). This value is above the minimum pressure objective of 276 kPa (40 psi) for residential buildings up to two storeys. Adding 5 psi per floor above two stories, to account for headloss due to elevation and pipe losses, a minimum pressure of 413 kPa (60 psi) would be required for the sixth floor. The peak hour pressure at ground level is above this objective and therefore considered acceptable.

During average day demands, the resulting maximum hydraulic gradeline of 132.8 m corresponds to a maximum pressure of 538 kPa (78 psi). This value is less than the maximum pressure objective of 552 kPa (80 psi) and therefore considered acceptable.

Supporting hydraulic calculations are attached in Appendix D.

Maximum Day + Fire Flow

A maximum day plus fire flow (11,000 L/min) hydraulic gradeline of 118.0 m corresponds to a residual pressure of 393 kPa (57 psi) at this location, which is above the minimal residual pressure requirement of 140 kPa (20 psi).

Based on Table 1 of Appendix I of the City of Ottawa Technical Bulletin ISTB-2018-02 and a desktop review (i.e., Google Street View) to confirm hydrant class, four (4) hydrants are located in the vicinity of the proposed building. One (1) Class AA hydrants is within 75 m, both with a capacity contribution of up to 5,700 L/min. Three (3) other Class AA hydrants are within 150 m from the site, both with a capacity contribution of up to 3,800 L/min. The combined hydrant flow coverage for 917 Merivale Road is therefore 17,100 L/min, which is above the RFF obtained from the FUS (11,000 L/min) method.

The hydrant coverage is illustrated in Figure 2 attached in Appendix D. A breakdown of the hydrant coverage is summarized in Table 3 below.

Table 3: Fire Hydrant Coverage

				Fire Hydrar	nts		Combined
Building	Fire Flow Demand	11. 1. 1	Witl	nin 75 m	Between 7	6 m and 150 m	Hydrant
Building	(L/min)	Hydrant Class	Quantity	Contribution to RFF	Quantity	Contribution to RFF	Flow Coverage (L/min)
		AA	1	5,700	3	3,800	
917 Merivale	11 000	Α					
Road	11,000	В					17,100
		С					

Conclusion

In conclusion, based on the boundary condition provided, 300 mm diameter watermain along Merivale Road provides adequate fire flow capacity, as per the Fire Underwriters Survey (FUS) method, to the proposed development 917 Merivale Road. Resulting pressures during anticipated demand flows meet the pressure objectives during average and peak demand conditions, as per the City of Ottawa's Drinking Water Design Guidelines.

B. Sanitary Flow

The peak sanitary flow for the 20 units, which comprise of ten (1)-bedroom and ten (10) bachelor apartment units, is estimated at Q = 0.34 L/s with an infiltration rate of 0.02 L/s. Refer to Appendix E sheet 1 of 1 regarding sanitary flow calculations. This flow will enter the existing 375 mm diameter sanitary sewer on Merivale Road via the proposed 150 mm diameter PVC sanitary service lateral from the six (6)-storey residential apartment building.

The existing peak sanitary flow of the site for single detached dwelling unit is Q = 0.06 L/s with an infiltration rate of 0.02 L/s. The net increase in flow from this proposed development is 0.28 L/s which is not expected to negatively impact the existing 375 mm dia. sanitary sewer.

Waste water from this site outlets into the Merivale Road 375 mm dia. sanitary sewer then continues to outlet north along Merivale Road into the existing downstream 1050 mm dia. concrete sanitary collector sewer located north of Carling Avenue which further direct sewage flow northward crossing Island Park Drive into the Geneva Street 1050 mm dia. sanitary collector sewer.

C. Storm Flow

Stormwater outlet for this proposed development property will be the existing 450 mm dia. storm sewer located on Merivale Road. The proposed residential apartment building has a rooftop that is partially flat and will be able to provide on-site stormwater management (SWM)

storage. Roof water from the building will be drained and controlled by two (2) roof drains which then outlets directly into the existing Merivale Road 450 mm dia. storm sewer via the proposed 300 mm dia. PVC storm sewer from the site.

On-site drainage shall be graded and drained into (2) catch basin manholes where they are interconnected by oversized underground 600 mm dia. storm sewer stormwater flow here will be controlled by the specified ICD located in CB/MH#1 to a rate of 6.0 L/s (min.) permitted by the City.

The building foundation weeping tile drainage system shall have its own separate gravity flow pipe where weeping tile water is outletted via a 150 mm dia. storm pipe to the existing Merivale Road storm sewer. The stormwater outlet for the rooftop water from roof drains will also be a separately designated proposed 150 mm dia. PVC pipe that will also be outletted into the existing Merivale Road storm sewer.

Two (2) roof drains are proposed for this residential building to restrict flow to a rate of 2.84 L/s (1.26 L/s + 1.58 L/s) into the existing municipal storm sewer.

Based on the residential site plan from the owner's architect, the average post-development runoff coefficient is estimated at C = 0.82 and A = 0.0482 hectares.

An estimation of the pre-development flow condition was carried out using the criteria accepted by the City of Ottawa. If post-development C valve exceeds the lesser of the $C_{pre} = 0.59$ then SWM is required. Because $C_{post} = 0.82$ for this site exceeds $C_{pre} = 0.59$ then SWM measures are required.

Therefore, based on our calculation, on-site retention is required for this proposed residential development site, because the site post-development C value of 0.82 is greater than the $C_{pre} = 0.59$.

The storage volume for the five (5)-Year and up to the 100-Year storm event attenuation will be stored by means of flat rooftop of the proposed residential building and by the oversized underground storm drainage pipe and structures on-site. Also refer to the site storm drainage report (Report No. R-823-102) for further details.

Conclusion

To develop this proposed residential site (±0.0482 ha. in size) and in controlling the 5-Year stormwater release rate off-site to an allowable rate of 5.17 L/s, a calculated site storage volume of approximately 5.26 m³ (min.) is required during the 5-Year event. We estimate that the required storage volume is 1.69 m³ (min.) from rooftop storage and 3.57 m³ (min.) from the

site underground drainage system are necessary to attenuate the 5-Year storm event. Refer to the Storm Drainage Report (Report No. R-823-102) for details.

During the 5-Year storm event for the flat rooftop storage, the ponding depth of rooftop is estimated at 120 mm at Roof Drain No. 1 and Roof Drain No. 2 and 0 mm at the roof perimeter, assuming a 2.0% (min.) roof pitch to the roof drains. The rooftop storage available at Roof Area No. 1 is $1.17 \, \text{m}^3$ and Roof Area No. 2 is $1.38 \, \text{m}^3$, for a total of $2.55 \, \text{m}^3$, which is greater than the required volume of $1.69 \, \text{m}^3$.

As for the remaining storage volume of 3.57 m³ (min.) required from the site development area for the 5-Year storm event, the estimated H.W.L. of 76.48 m will provide a total available underground storage volume of 4.0 m³ consisting of the proposed underground storm piping and drainage structures. In total, the 5-Year available site storage volume is approximately 4.0 m³ which is greater than the required site storage volume of 3.57 m³. See Appendix E for details.

In order to control the 100-Year stormwater release rate off-site to an allowable rate of 5.17 L/s, a calculated site storage volume of approximately 13.37 m 3 (min.) is required during the 100-Year event. We estimate that the required storage volume of 4.65 m 3 (min.) of rooftop storage and 8.72 m 3 (min.) from the site underground drainage system are necessary to attenuate the 5-Year storm event. See Table 4 to 6 inclusive

During the 100-year storm event for the flat rooftop storage, the ponding depth on this rooftop is estimated at 150 mm at Roof Drain No. 1 and Roof Drain No. 2 and 0 mm at the roof perimeter assuming a 2.0% (min.) roof pitch to the drains. The rooftop storage available at Roof Area No. 1 is 2.35 m^3 and Roof Area No. 2 is 2.69 m^3 for a total of 5.04 m^3 which is greater than the required volume of 4.65 m^3 .

As for the remaining storage volume of 8.72 m³ (min.) required from the site development area for the 100-Year storm event, the estimated H.W.L. of 77.18 m will provide a total available underground storage volume of 8.90 m³ consisting of the proposed underground storm piping and drainage structures. In total, the 100-Year available site storage volume is approximately 8.90 m³ which is greater than the required site storage volume of 8.72 m³. See Appendix E for details.

Therefore, by means of flat building rooftop storage, grading the site to the proposed grades and constructing the proposed underground storm piping and drainage system as shown on the Proposed Site Grading and Servicing Plan (Dwg. No. 823-102, G-1) the desirable 5-Year and 100-Year storm event attenuation volume of 4.0 m³ and 8.90 m³ respectively will be available on-site.

In order to control the release flow rate off-site from the controlled drainage are of the lot, an inlet control device (ICD) will be installed at the outlet of CB/MH#1 in the 300 mm diameter storm pipe (outlet pipe) with Q = 6.0 L/s under a head of 1.0 m. A rooftop drain with a maximum release rate of 1.26 L/s will be installed at Roof Drain No. 1 and a maximum release rate of 1.58 L/s will be installed at Roof Drain No. 2 under a head of 150 mm at the proposed apartment building flat rooftop as depicted on (Dwg. No. 823-102, G-1).

A specified inlet control device (ICD) will be installed at the outlet of CB/MH#1 in the 300 mm diameter storm pipe (outlet pipe) with Q = 6.0 L/s under a head of 1.0 m. The ICD type recommended is a Hydrovex Regulator (75-VHV-1) or equivalent. The specified ICD at 6.0 L/s is the lowest flow ICD permitted by the City of Ottawa for maintenance purposes.

The building weeping tile drainage will outlet via its separate 150mm diameter PVC storm lateral. The roof drains will be outletted also via a separate 150mm PVC storm lateral from the apartment building whereupon both laterals "wye" into the proposed 300 mm dia. storm pipe due to one (1) connection to the existing Merivale Road storm sewer is permitted. Therefore, both storm laterals and the site storm sewer all outlets to the existing Merivale Road 450 mm diameter storm sewer with only one (1) storm pipe connection. The City of Ottawa recommends that pressurized drain pipe material be used in the building for the roof drain leader pipe in the event of surcharging on the City storm sewer system. Refer to the proposed site grading and servicing plan Dwg. 823-102 G-1 for details.

To achieve a minimum of 80 percent TSS removal, a Stormceptor structure (Model EFO-4) is proposed to be installed for the site development of this property. This Stormceptor structure shall be located downstream of the proposed CB/MH#1, which houses the site's inlet control device (ICD). Based on the Stormceptor system that is proposed for this site, size of the lot, and impervious ratio, a greater than 80 percent TSS removal is estimated for all rainfall events including large storms. (See Appendix D of the Storm Drainage Report {Report No. R-823-102} for details).

Erosion and Sediment Control

The contractor shall implement Best Management Practices to provide for protection of the receiving storm sewer during construction activities. These practices are required to ensure no sediment and/or associated pollutants are released to the receiving watercourse. These practices include installation of a "siltsack" catch basin sediment control device or equal in catch basins as recommended by manufacturer on-site and off-site within the Merivale Road road right of way adjacent to this property. Siltsack shall be inspected every 2 to 3 weeks and after major storm. The deposits will be disposed of as per the requirements of the contract. See Dwg. #823-102 ESC-1 for details.

Refer to Appendix F for the summary of the Development Servicing Study Checklist that is applicable to this development.

PREPARED BY T.L. MAK ENGINEERING CONSULTANTS LTD.

TONY L. MAK, P.ENG

SIX (6) STOREY APARTMENT BUILDING SITE

LOT 1

R-PLAN 268160

917 MERIVALE ROAD

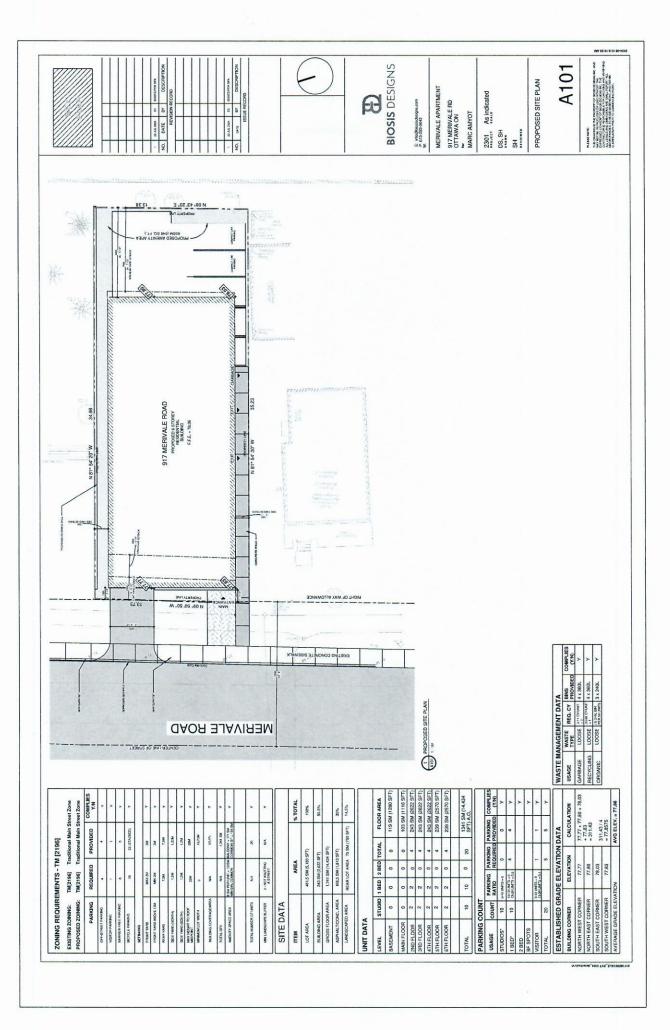
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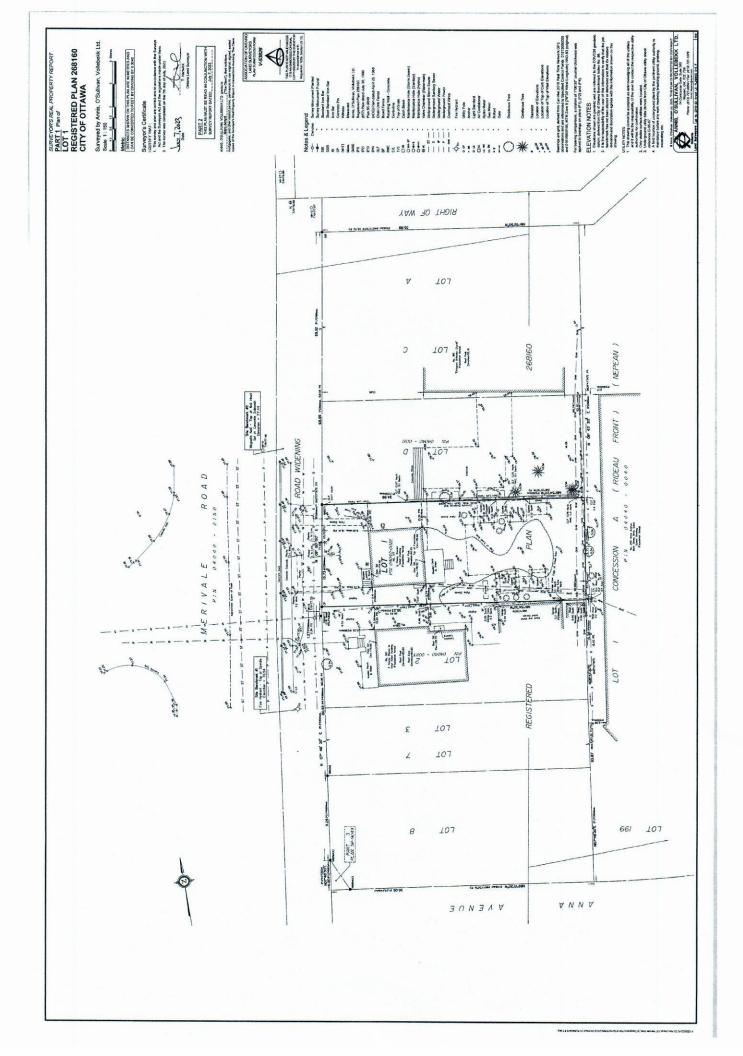
APPENDIX A

SITE PLAN

AND

LEGAL SURVEY PLAN





SIX (6) STOREY APARTMENT BUILDING SITE

LOT 1

R-PLAN 268160

917 MERIVALE ROAD

CITY OF OTTAWA

APPENDIX B

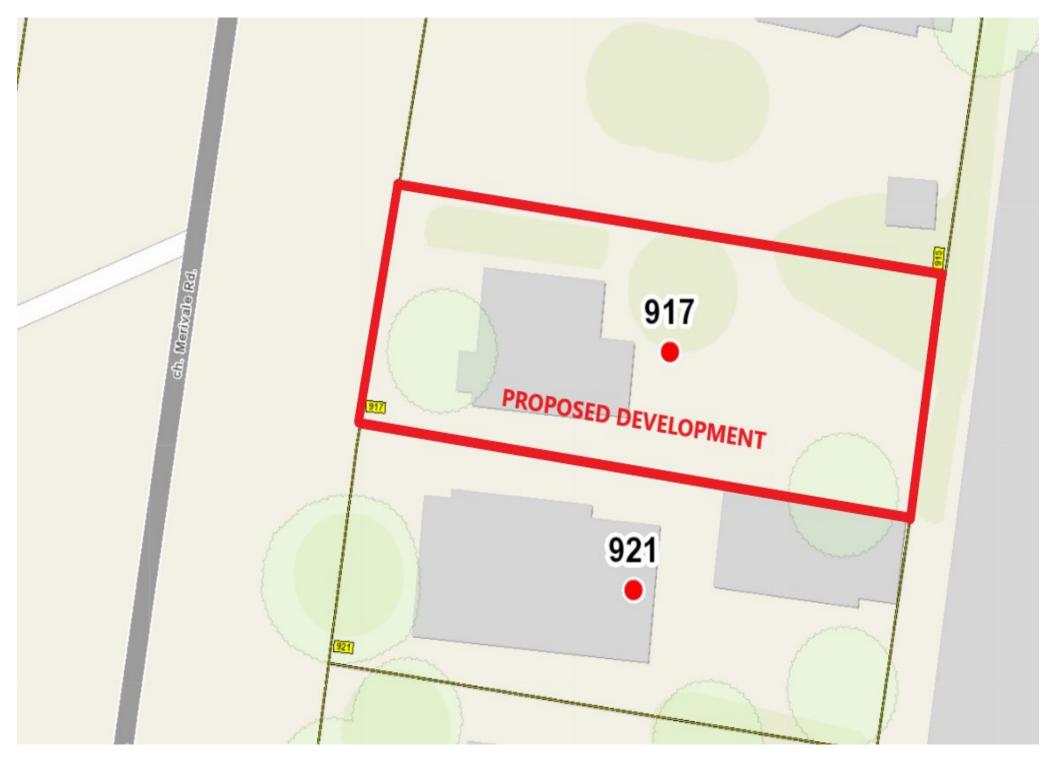
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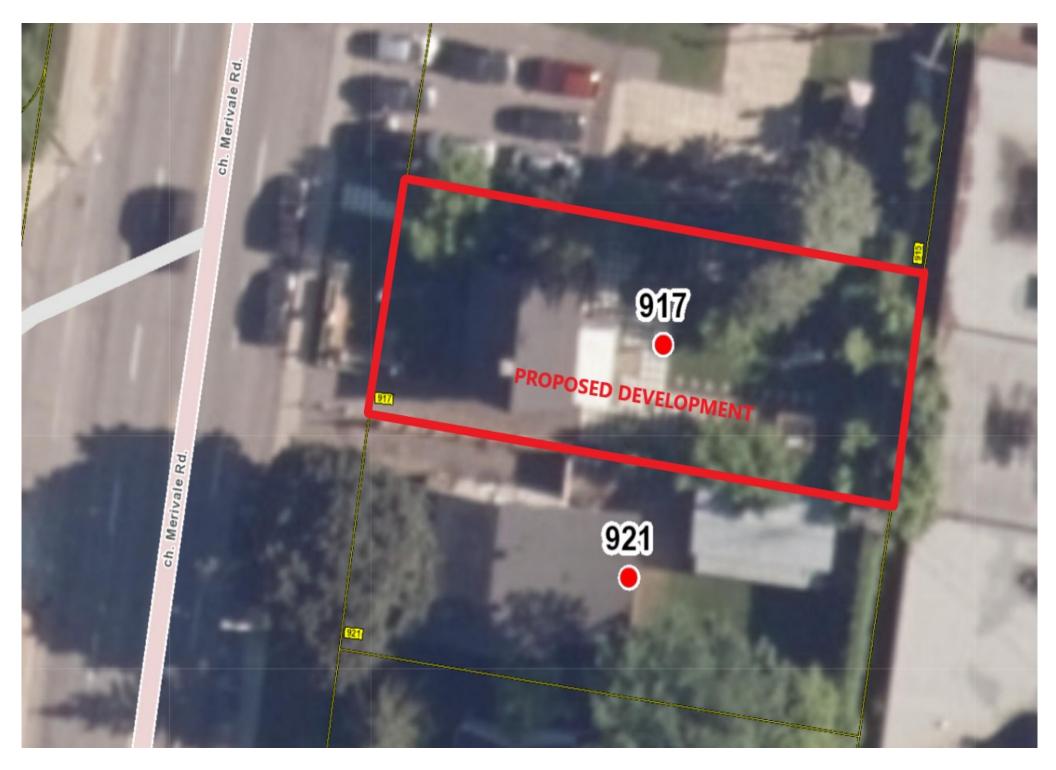
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SIX (6) STOREY APARTMENT BUILDING SITE

LOT 1

R-PLAN 268160

917 MERIVALE ROAD

CITY OF OTTAWA

APPENDIX C

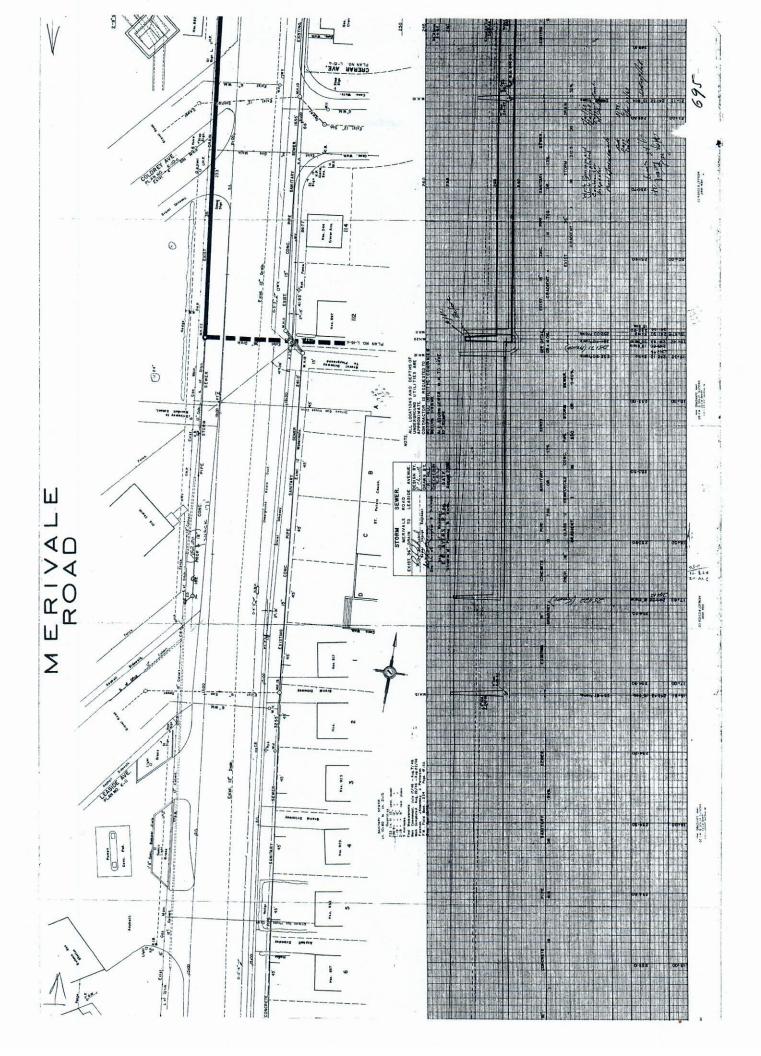
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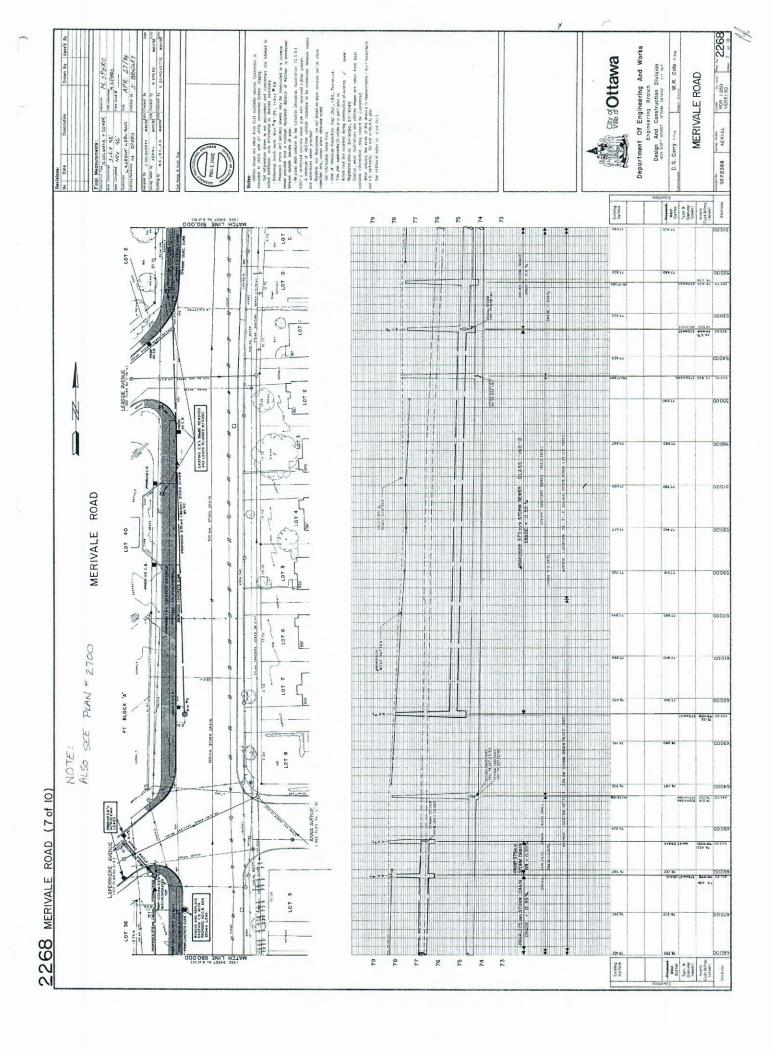
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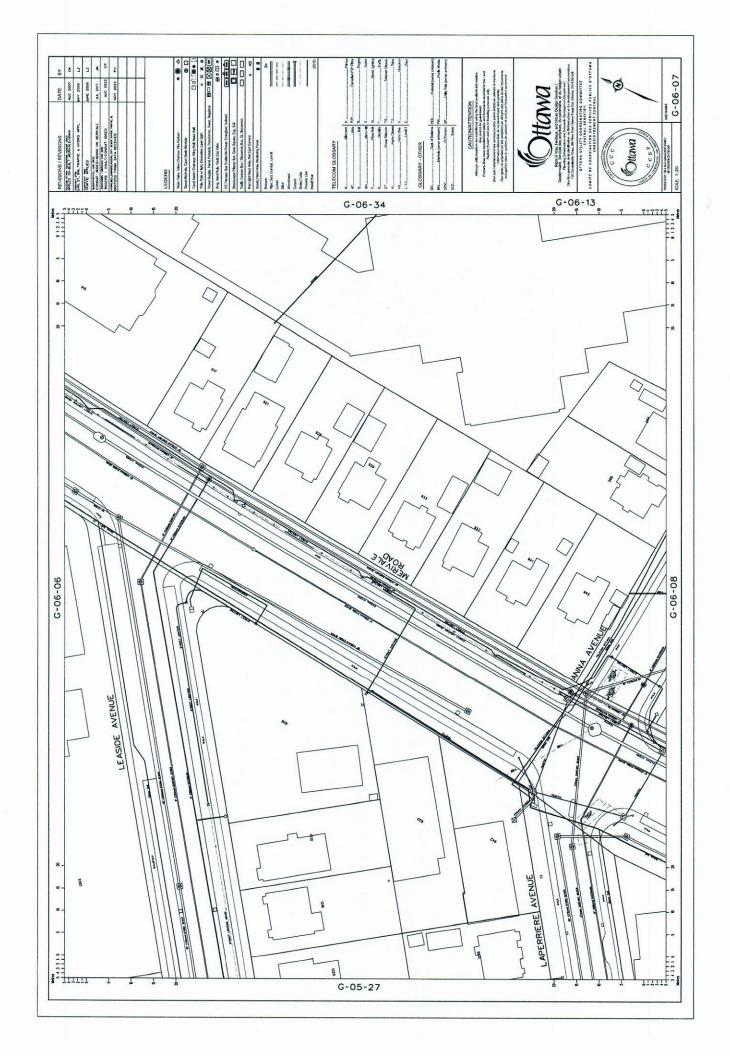
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SIX (6) STOREY APARTMENT BUILDING SITE

LOT 1

R-PLAN 268160

917 MERIVALE ROAD

CITY OF OTTAWA

APPENDIX D

CITY OF OTTAWA

- SITE PLAN AND ARCHITECTURAL DRAWINGS
- WATER BOUNDARY CONDITIONS E-MAIL
- FUS FIRE FLOW CALCULATION
- FUS EXPOSURE DISTANCES FIGURE 1
- SUPPORTING HYDRAULIC CALCULATIONS
- HYDRANT SPACING FIGURE 2

ATTACHMENT	Γ1: SITE PLA	N AND ARC	HITECTUR	AL DRAWINGS

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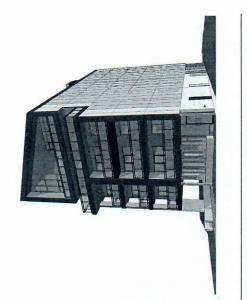
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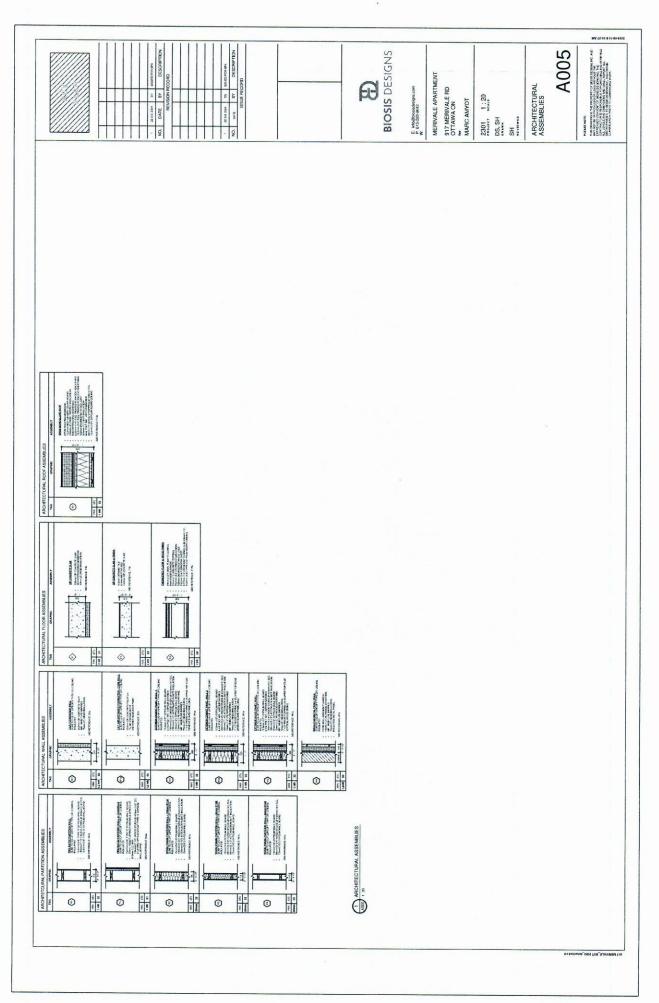
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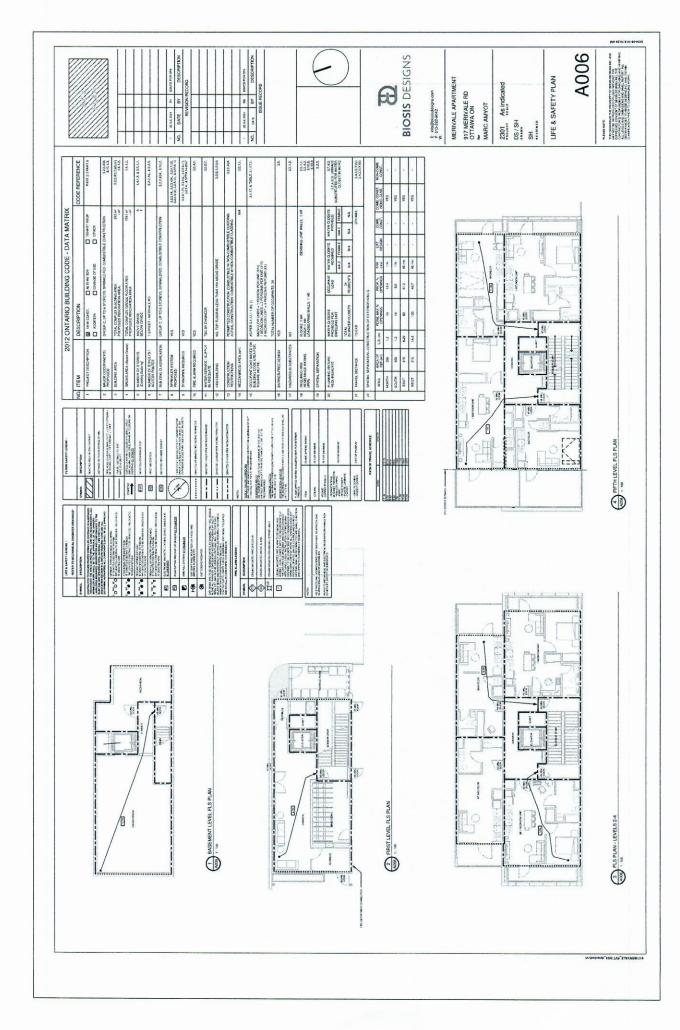
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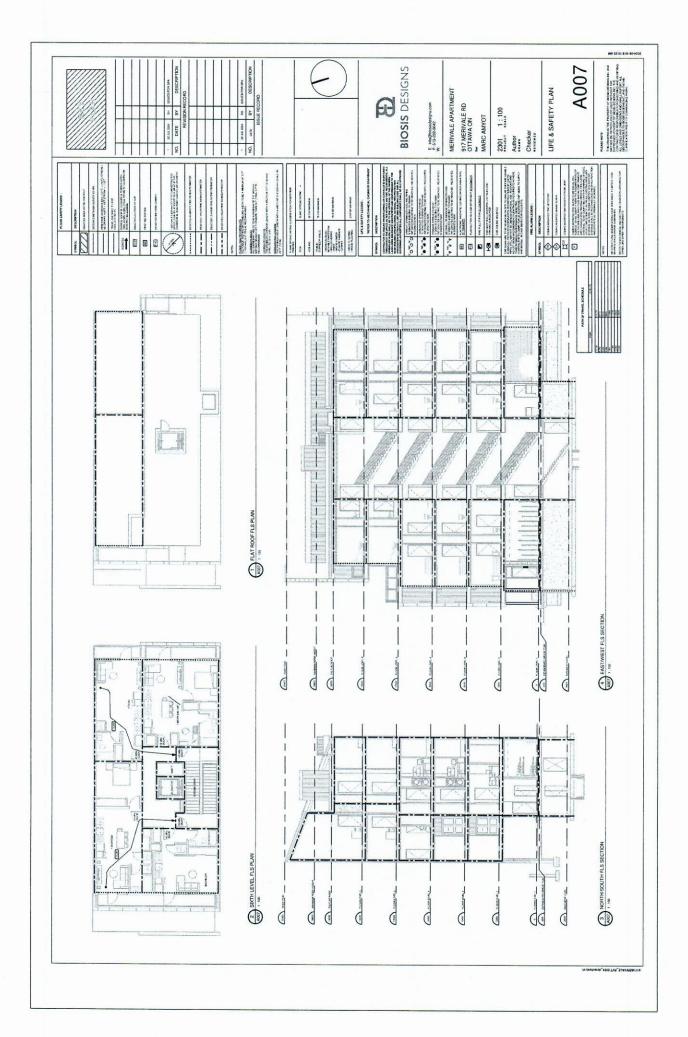


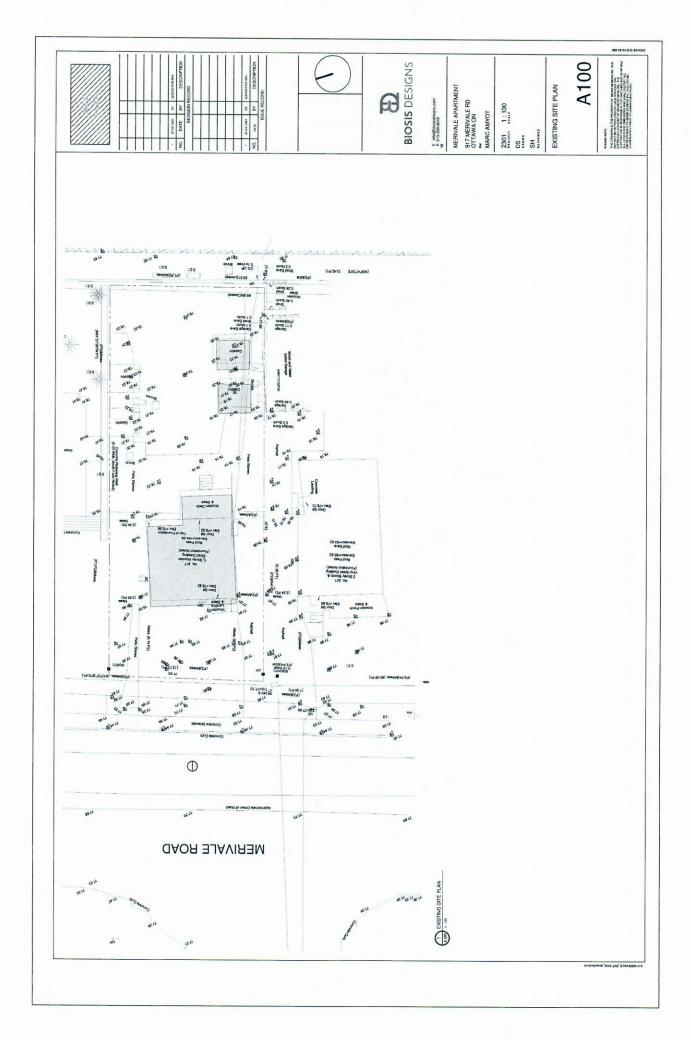
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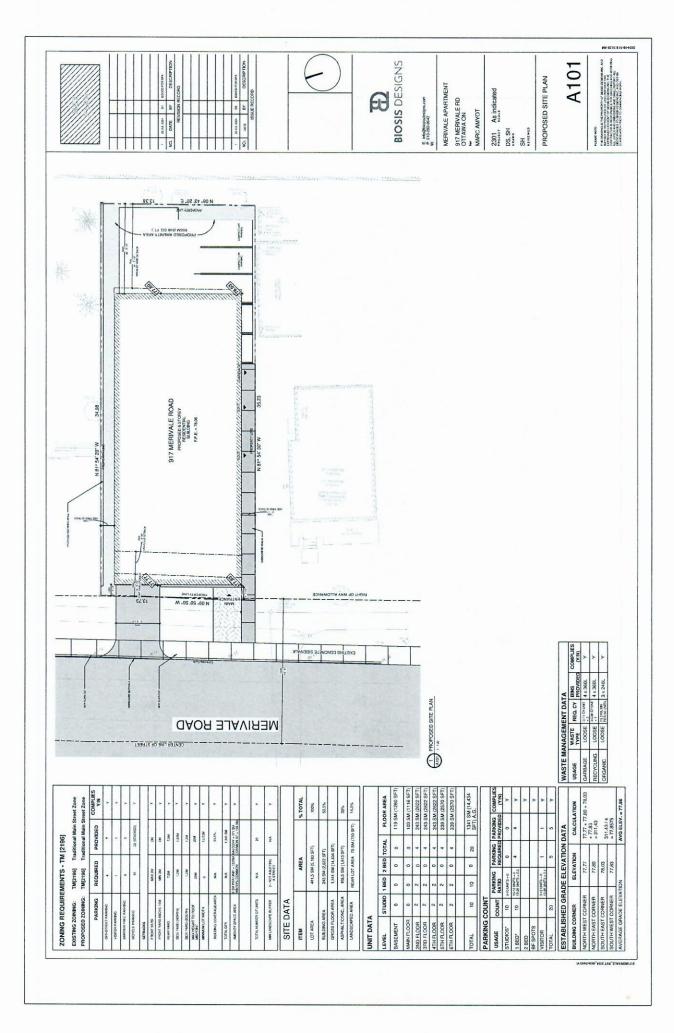
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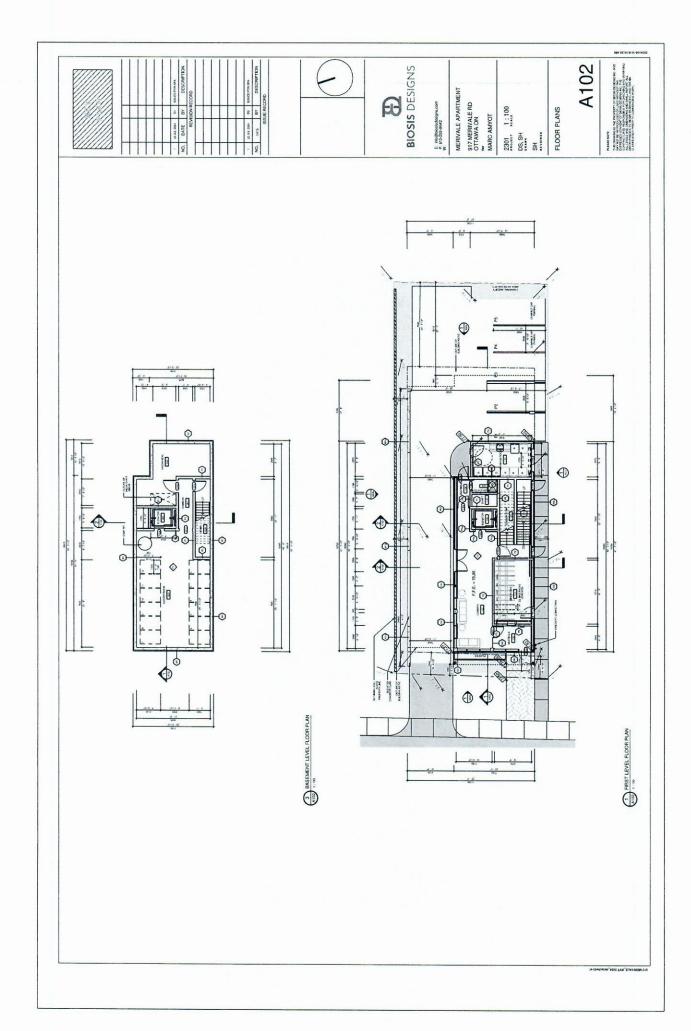


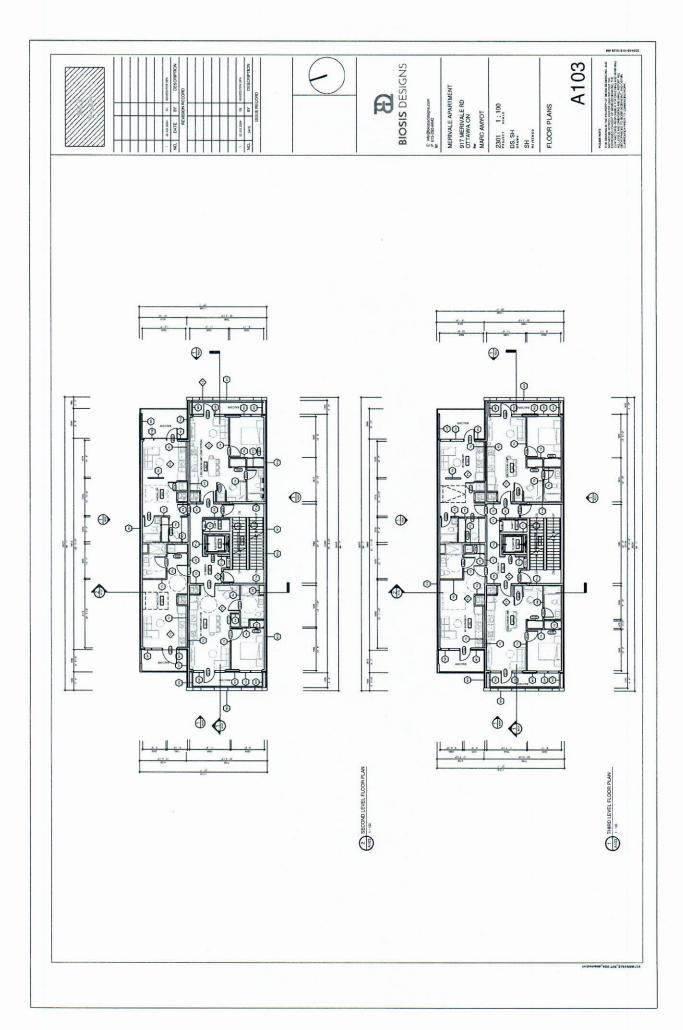


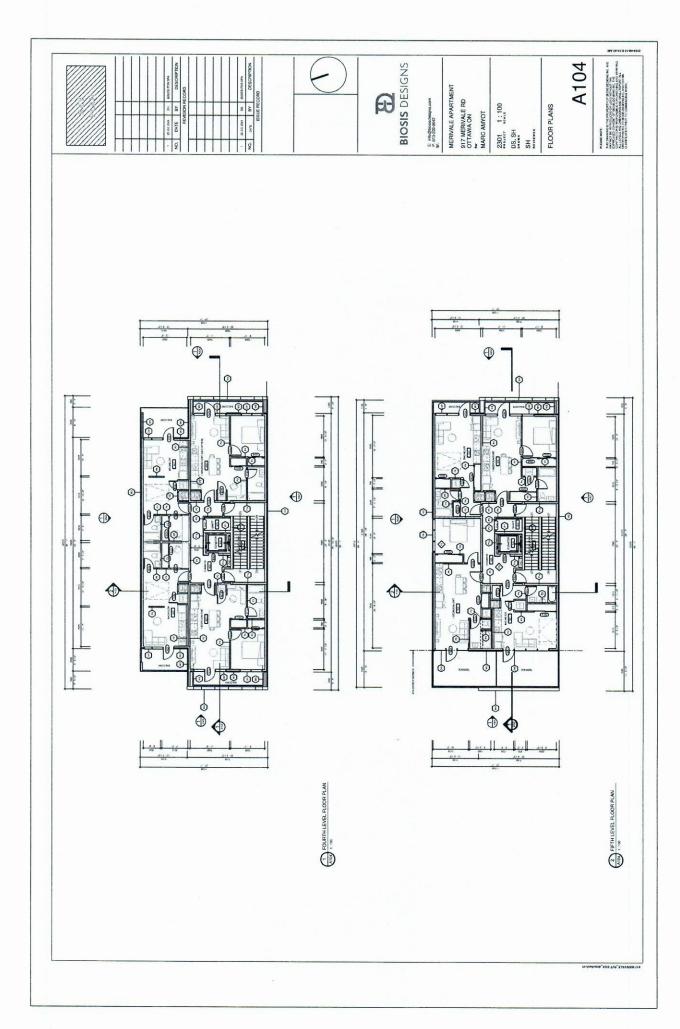


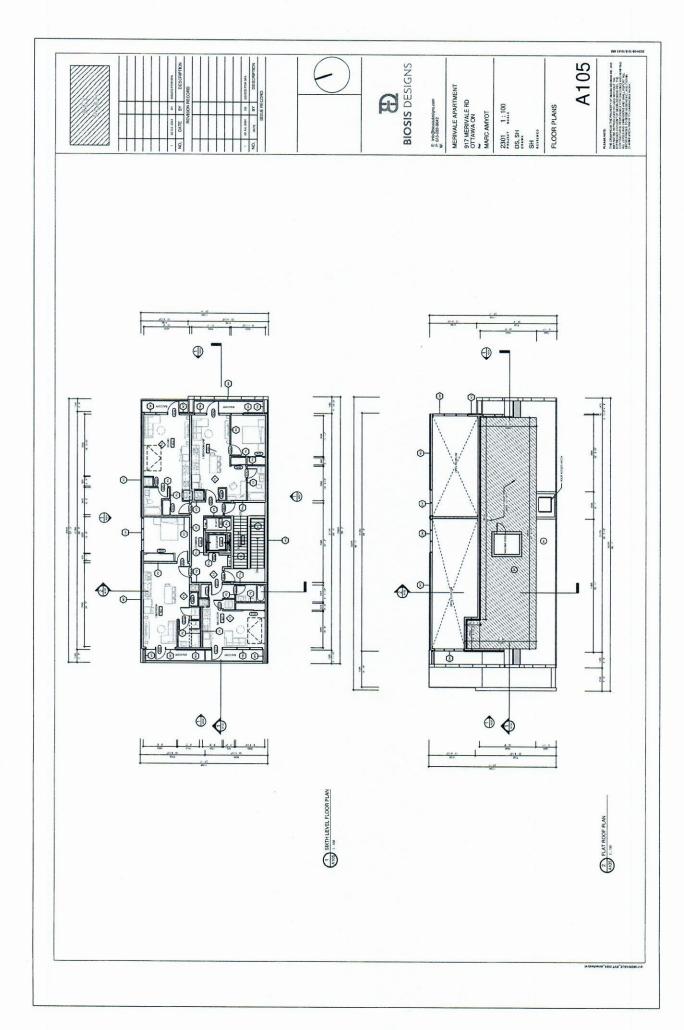


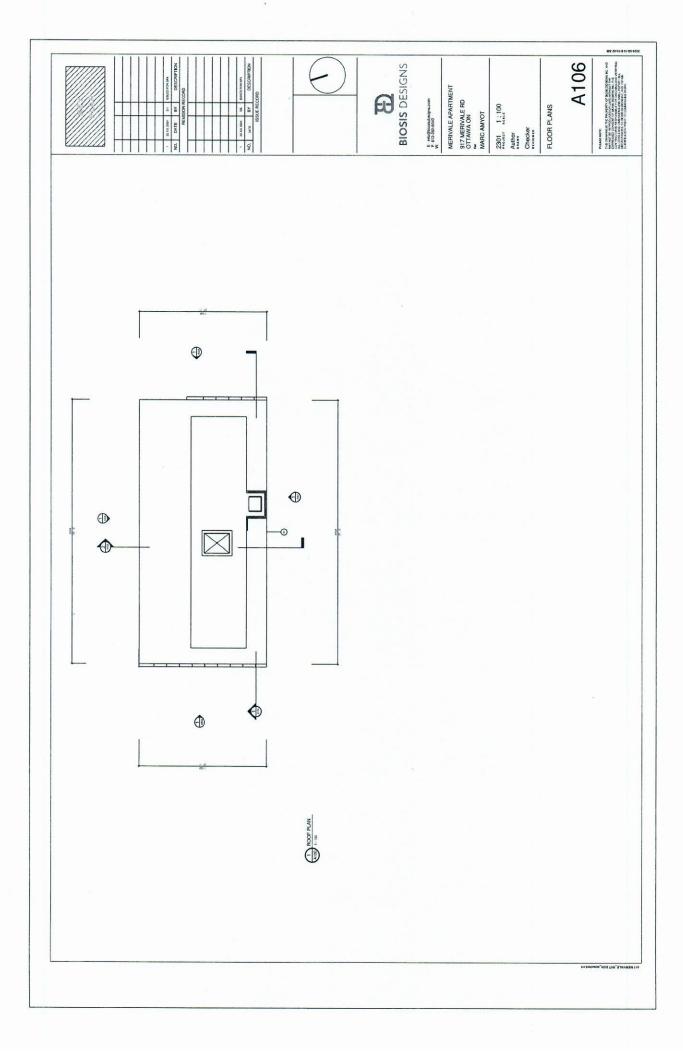


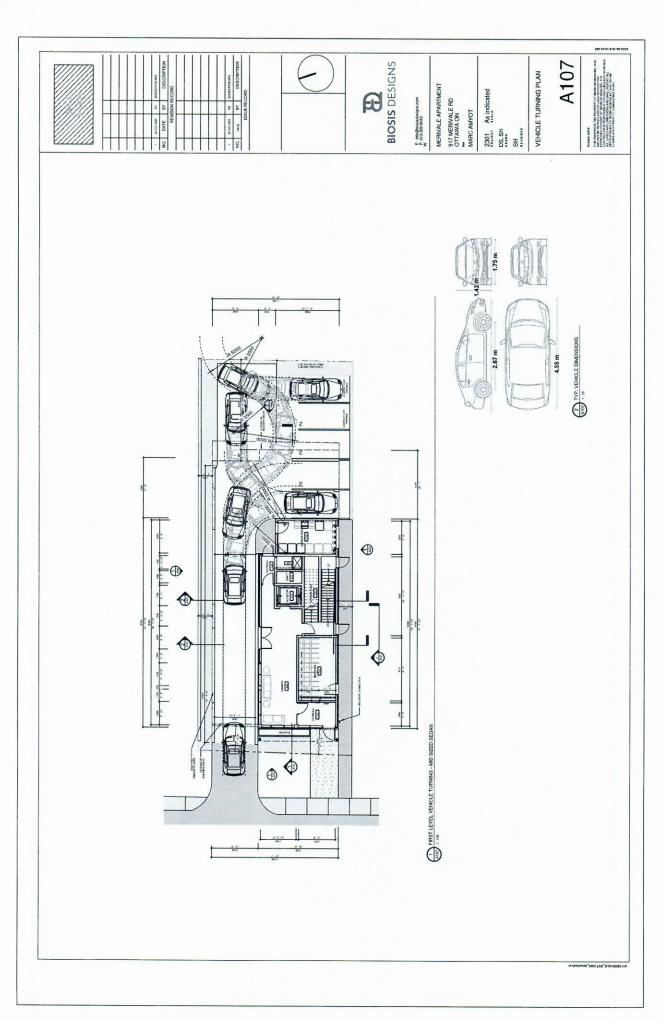


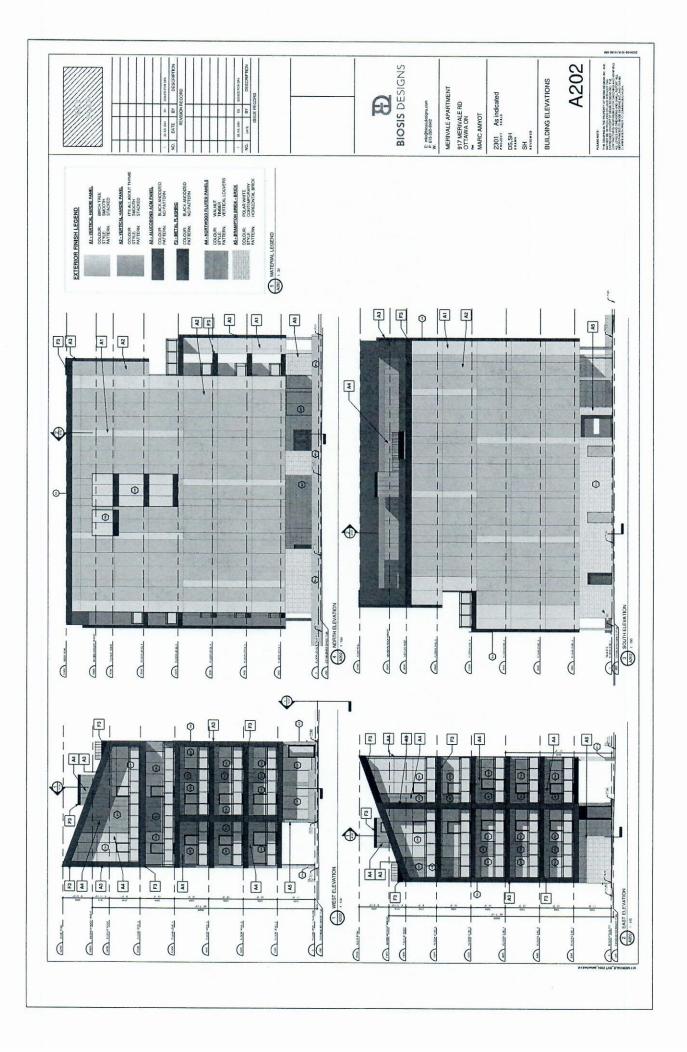


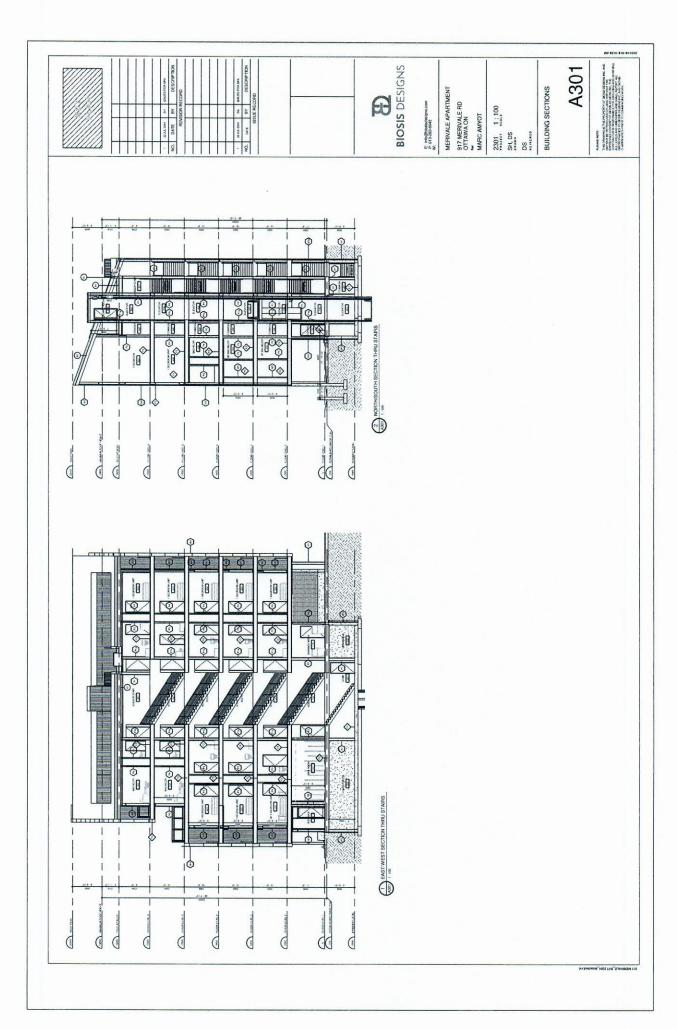


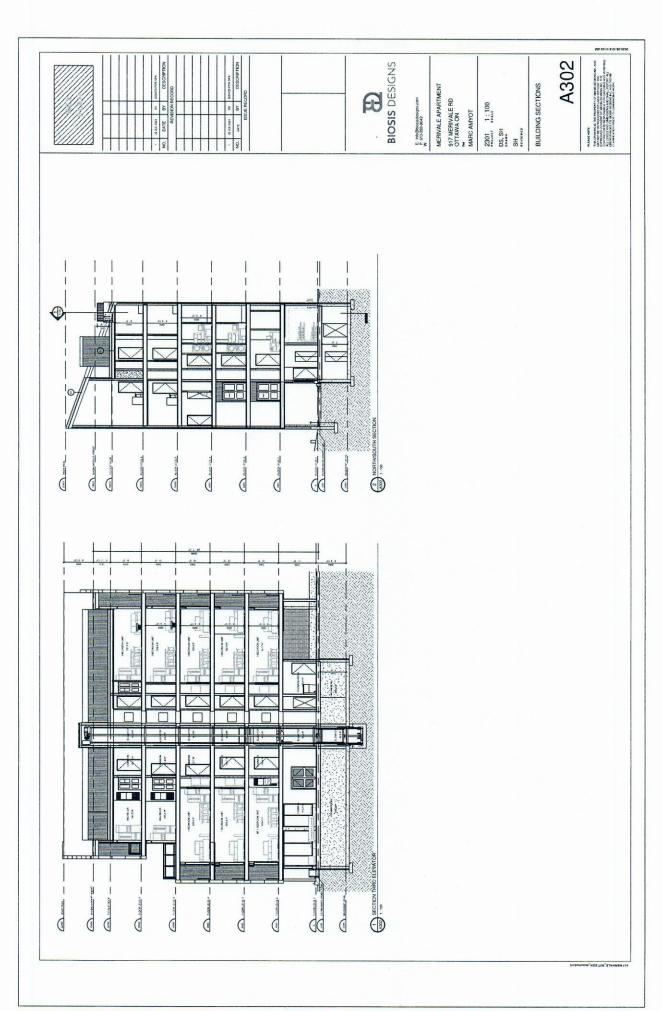


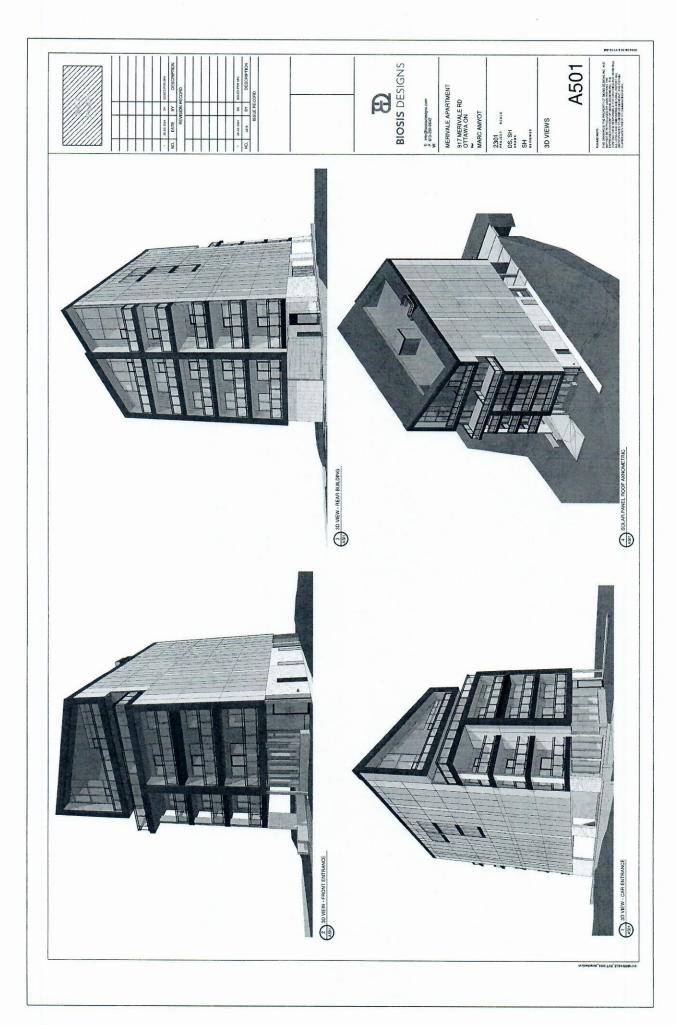












ATTACHMENT 2: WATER BOUNDARY CONDITIONS E-MAIL

Mineault-Guitard, Alexandre

From:

TL MaK <tlmakecl@bellnet.ca>

Sent: To:

Friday, May 3, 2024 11:01 AM Mineault-Guitard, Alexandre

Cc:

Alemany, Kevin

Subject:

RE: 917 Merivale Road - Water Boundary Conditions Request

Attachments:

917 Merivale Road April 2024.pdf

Hi Alex,

Attached please find the Water Boundary Conditions received from the City on May 2, 2024 for your calculation use.

Have a good weekend.

Thank you,

Tony Mak

T.L. Mak Engineering Consultants Ltd. 1455 Youville Drive, Suite 218 Ottawa, ON. K1C 6Z7

Tel. 613-837-5516 | Fax: 613-837-5277

E-mail: tlmakecl@bellnet.ca

From: Adams, Reed [mailto:reed.adams@ottawa.ca]

Sent: May 2, 2024 2:50 PM

To: TL MaK

Subject: RE: 917 Merivale Road - Water Boundary Conditions Request

Hi Tony,

Here are the boundary conditions for 917 Merivale:

The following are boundary conditions, HGL, for hydraulic analysis at 917 Merivale Road (zone 2W2C) assumed to be connected to the 305 mm watermain on Merivale Road (see attached PDF for location).

Min HGL: 124.4 m Max HGL: 132.8 m

Max Day + Fire Flow (183 L/s): 118.0 m

These are for current conditions and are based on computer model simulation.

Disclaimer: The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation.

Thanks,

Reed

From: Adams, Reed

Sent: April 18, 2024 1:59 PM
To: TL MaK <tlmakecl@bellnet.ca>

Subject: RE: 917 Merivale Road - Water Boundary Conditions Request

Hi Tony,

I've sent the request to our water resources group and should get a response back in two weeks max.

Thanks,

Reed

From: TL MaK < tlmakecl@bellnet.ca>

Sent: April 18, 2024 1:41 PM

To: Adams, Reed < reed.adams@ottawa.ca>

Subject: 917 Merivale Road - Water Boundary Conditions Request

CAUTION: This email originated from an External Sender. Please do not click links or open attachments unless you recognize the source.

ATTENTION : Ce courriel provient d'un expéditeur externe. Ne cliquez sur aucun lien et n'ouvrez pas de pièce jointe, excepté si vous connaissez l'expéditeur.

Hi Reed,

Regarding this site, we are requesting for water boundary conditions from the City of Ottawa to be provided for our hydraulic analysis. The particulars are as follows:

The proposed building located within Pressure Zone 2W at 917 Merivale Road is a 6-storey residential multi-unit building with a basement. The building contains twenty (20) total units, one (1) 2-bedroom, nine (9) 1-bedroom, and ten (10) bachelor units. Each floor covers an area of around 224 m², for a gross floor area of 1,341 m². The building is to be serviced by the 300 mm diameter watermain along Merivale Road.

The domestic demands were calculated using the City of Ottawa's Water Design Guidelines, where the residential consumption rate of 280 L/cap/d was used to estimate average day demands (AVDY). Persons per unit (PPU) for each unit were estimated based on the City of Ottawa's Water Design Guidelines. Following discussions with the City, peaking factors are to be estimated from Table 3-3 of the MECP Design Guidelines for Drinking-Water Systems, given that the proposed development population is less than 500 people. Maximum day (MXDY) demands were calculated by multiplying AVDY demands by a factor of 9.5. Peak hour (PKHR) demands were calculated by multiplying AVDY by a factor of 14.3. Table 1 shows the estimated domestic demands of the existing building.

Table 1: Estimated Domestic Demand

Unit Type	Unit Count	PPU	Consumption	AVDY		MXDY		PKHR	
Опт туре		PPU		L/d	L/s	L/d	L/s	L/d	L/s

Apartment, 2- Bedroom	1	2.1	_	588	0.01	5,586	0.06	8,408	0.10
Apartment, 1- Bedroom	9	1.4	280	3,528	0.04	33,516	0.39	50,450	0.58
Apartment, Bachelor	10	1.4		3,920	0.05	37,240	0.43	56,056	0.65
Total	20			8,036	0.09	76,342	0.88	114,915	1.33

The fire flow required was determined following the Fire Underwriter Survey (FUS) method and is provided in the attached worksheet. The proposed building will be of wood frame construction. It is understood that the building will be equipped with sprinklers, and that the basement is more than 50% below ground level. The resulting required fire flow is 11,000 L/min (183 L/s) for a duration of 2.25 hours.

In summary:

- AVDY = 8,036 L/d (0.09 L/s);
- MXDY = 76, 342 L/d (0.88 L/s);
- PKHR = 114,915 L/d (1.33 L/s); and,
- Fire Flow = 11,000 L/min (183 L/s).

The City is requested to provide boundary conditions for the Average Day, Maximum Day, Peak Hour and Fire Flow conditions indicated above.

Thank you for your prompt attention to this matter. Please forward the boundary conditions as soon as possible.

Have a good day.

Regards,

Tony Mak

T.L. Mak Engineering Consultants Ltd. 1455 Youville Drive, Suite 218 Ottawa, ON. K1C 6Z7 Tel. 613-837-5516 | Fax: 613-837-5277 E-mail: tlmakecl@bellnet.ca

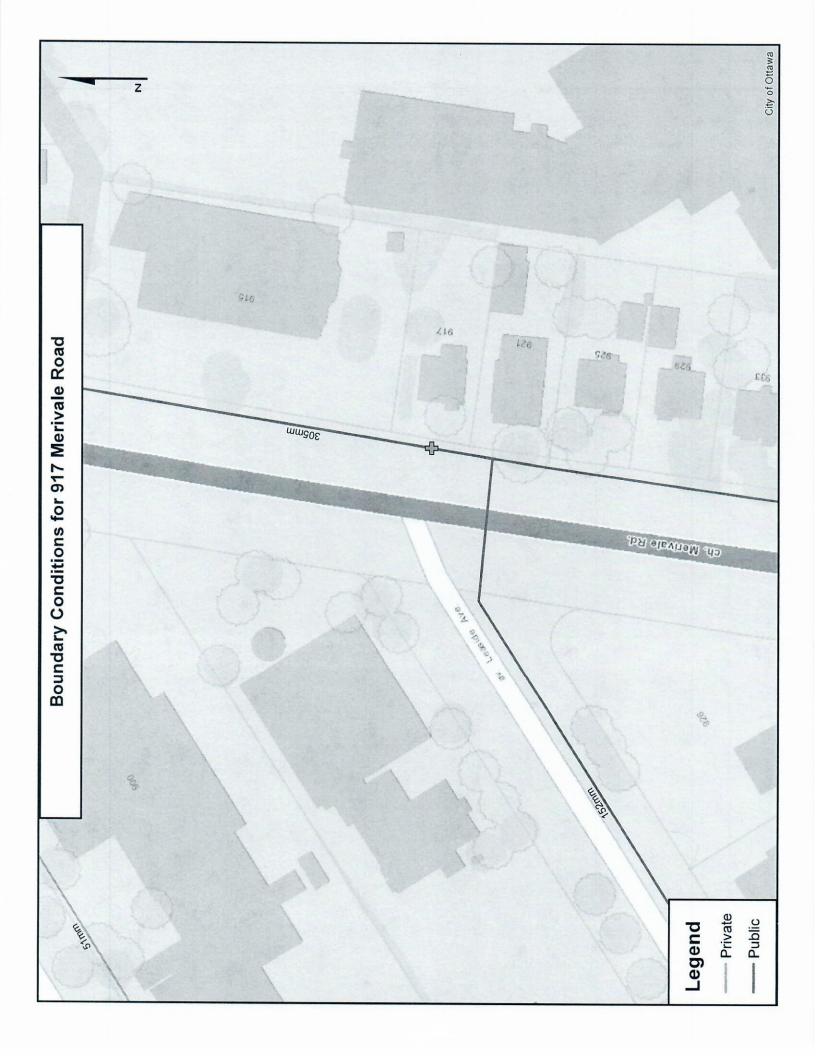
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ATTACHMENT 3: FUS FIRE FLOW CALCULATION



FUS Fire Flow Calculation - Long Method

Calculations based on: "Water Supply for Public Fire Protection" by Fire Underwriters' Survey, 2020

Stantec Project #: 163401084

Project Name: 917 Merivale Road

Fire Flow Calculation #: 1 Building Type/Description/Name: Residential

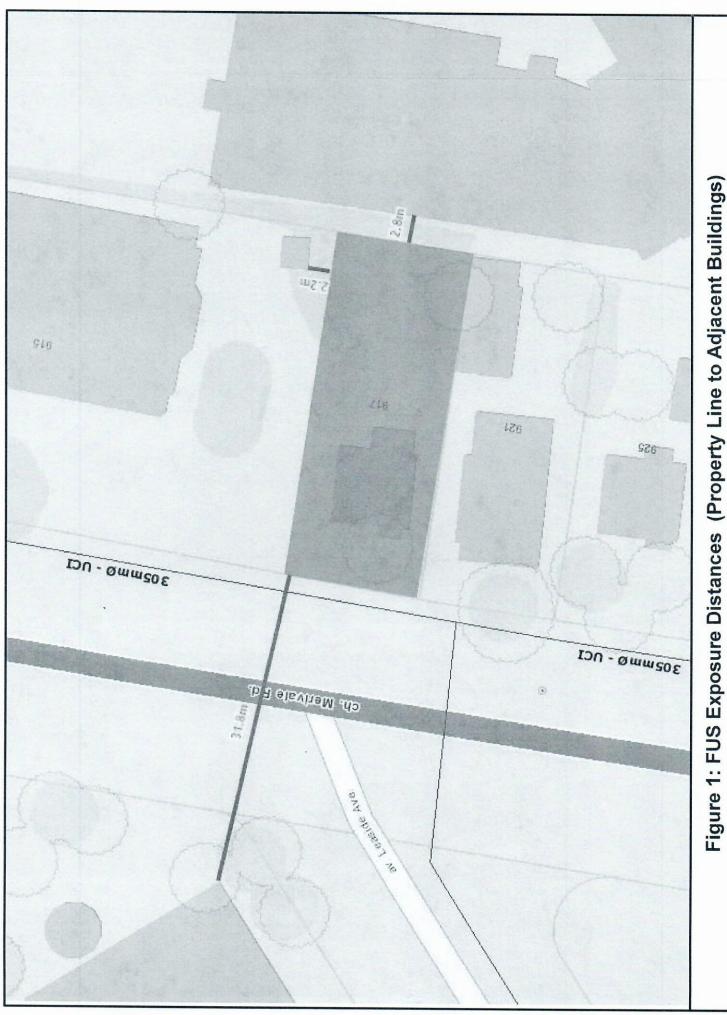
Date: August 14, 2024
Data inputted by: Melissa Nelson, EIT
Data reviewed by: Alexandre Mineault-Guitard, P.Eng

Notes: Wood frame, with sprinklers. 6-storey residential multi-unit building with a basement that is more than 50% below grade. The building contains twenty (20) total units, ten (10) 1-bedroom, and ten (10) bachelor units.

The average floor area is 218 sq.meters, for a gross floor area of 1,310 sq.meters.

	EST FINE			7/////					
Step	Task	Term	Options	Multiplier Associated with Option	Choose:	Value Used	Unit	Total Fire Flow (⊔min)	
			Little Control of the	Framing Materia	ı				
			Type V - Wood Frame	1.5		-			
	AND THE RESIDENCE OF THE PERSON OF THE PERSO		Type IV-A - Mass Timber	0.8					
1	Choose Frame Used		Type IV-B - Mass Timber	0.9					
1	for Construction of Unit	Coefficient related to	Type IV-C - Mass Timber	1	Type V - Wood Frame	1.5	m		
	Oilit	type of construction (C)	Type IV-D - Mass Timber	1.5	Type V - Wood Frame	1.5	l m		
			Type III - Ordinary construction	1				4	
			Type II - Non-combustible construction	0.8					
			Type I - Fire resistive construction	0.6					
	Choose Type of			Floor Space Are	а				
2	Housing (if TH, Enter Number of		Single Family	1	Other (Course led Ant				
	Units Per TH Block)	Type of Housing	Townhouse - indicate # of units	0	Other (Comm, Ind, Apt etc.)	20	Units		
			Other (Comm, Ind, Apt etc.)	20					
2.2	# of Storeys	Number of Floors/s	Storeys in the Unit (do not include basemen	t if 50% below grade):	6	6	Storeys		
3	Enter Ground Floor	Average Floor A	Area (A) based on total floor area of all floor	s for one unit (non-fire	218				
3	Area of One Unit			esistive construction):	Square Metres (m2)	218	Area in Square		
3.1	Obtain Total Effective Building Area	Total Effective Buildin	ng Area (# of Storeys x # of Units (if single f	amily or townhouse) x Average Floor Area):	1,310	M			
4	Obtain Required Fire Flow without Reductions	Required Fire Flow (without reductions or increases per FUS) (F = 220 * C * √A) Round to nearest 1,000 L/min					12,000		
5	Apply Factors	Reductions/Increases Due to Factors Affecting Burning							
-	Affecting Burning Choose		Non-combustible	-0.25					
		Occupancy Content Hazard Reduction or	Limited combustible	-0.15		-0.15	N/A		
5.1	Combustibility of		Combustible	0.10	Limited combustible			10,200	
	Building Contents	Surcharge	Free burning	0.15					
			Rapid burning	0.25					
		O-vielle- Bed of	Adequate Sprinkler conforms to NFPA13	-0.3	Adequate Sprinkler	100000	2000	110.000000	
		Sprinkler Reduction	None	0	conforms to NFPA13	-0.3	N/A	-3,060	
5.2	Choose Reduction Due to Presence of		Water Supply Credit	Water supply is standard for sprinkler and fire dept, hose line	-0.1	Water supply is standard for sprinkler	-0.1	N/A	-1,020
	оргинасто		Water supply is not standard or N/A Sprinkler system is fully supervised						
		Sprinkler Supervision Credit	Sprinkler system is fully supervised Sprinkler not fully supervised or N/A	-0.1	Sprinkler system is fully supervised	-0.1	N/A	-1,020	
_			Adequate sprinkler for exposures conform		Supervised				
		Sprinkler Conforms to NFPA13	None for exposures	S to INFFA 13	None for exposures		N/A		
F 0	Choose Presence of Sprinklers for Exposures within 30m	ose Presence of Water supply is standard for sprinkler and fire dept. hos		fire dept. hose line of	Water supply is not				
5.3		vvater Supply	Water supply is not standard or N/A for ex	posures	standard or N/A for exposures	0	N/A	0	
		Sprinkler Supervision		ervised	Sprinkler not fully supervised or N/A for		N/A		
			Sprinkler not fully supervised or N/A for ex	posures	exposures		14//		
		e Between Exposure Distance	Front Yard	30.1m or greater	0 0.2 0.15				
5.4			Right Side	3.1 to 10.0m		0.6	m	6,120	
			Rear Yard	10.1 to 20.0m		5.5		0,120	
		Left Side 0 to 3.0m 0.25 Total Required Fire Flow, rounded to nearest 1,000 L/min, with max/min limits applied:							
	Potential and the second		Total Required Fire Flow, r	rounded to neares	t 1,000 L/min, with m	ax/min li	mits applied:	11,000	
	Obtain Required				Total Required Fil	re Flow (a	bove) in L/s:	183	
6	Fire Flow. Duration								
6	Fire Flow, Duration & Volume	Was the same			Required Dura	tion of F	re Flow (hrs)	2.25	

ATTACHMENT 4 : FIGURE 1 – FUS EXPOSURE DISTANCES



Source: geoOttawa 2024; Contains information licensed under the Open Government License – City of Ottawa.

ATTACHMENT 5: SUPPORTING HYDRAULIC CALCULATIONS



Supporting Hydraulic Calculations

Stantec Project #: 163401084

Project Name: 917 Merivale Road

Date: May 9, 2024

Data inputted by: Alexandre Mineault-G, P.Eng. Data reviewed by: Alexandre Mineault-G, P.Eng.

Boundary Conditions provided by the City:

Scenario 1: Peak Hour (Min HGL): 124.4 m;

Scenario 2: Average Day (Max HGL): 132.8 m; and

Scenario 3: Maximum Day plus Fire Flow: 118.0 m.

Sample Calculations

HGL(m) = hp + hz

(1)

where: hp = Pressure Head (m); and hz = Elevation Head (m), estimated from topography.

For Scenario 1, we have:

HGL(m) = 124.4 and hz (m) = 77.9.

Rearranging Equation 1, we can calculate the Pressure Head (hp) as follow:

hp (m) = HGL - hz $\therefore hp = 124.4 - 77.9 \text{ m} = 46.5 \text{ m}.$

To convert from Pressure Head (m) to a pressure value (kPa), the following equation can be used:

P (kPa) = (p * g * hp) / 1000 (2)

where: ρ = density of water = 1000 kg/m³; and g = gravitational acceleration = 9.81 m/s².

Using Equation 2, we can calculate the Pressure Head (hp) as follow:

P (kPa) = (1000 * 9.81 * 46.5) / 1000

∴ P = 456 kPa.

Considering that 1 kPa = 0.145 psi, the pressure under Scenario 1 is equal to:

P = 66 psi.

Applying the same procedures, the pressures under Scenario 2 and Scenario 3 are calculated as follows: Scenario 2: P = 78 psi; and Scenario 3: P = 57 psi.

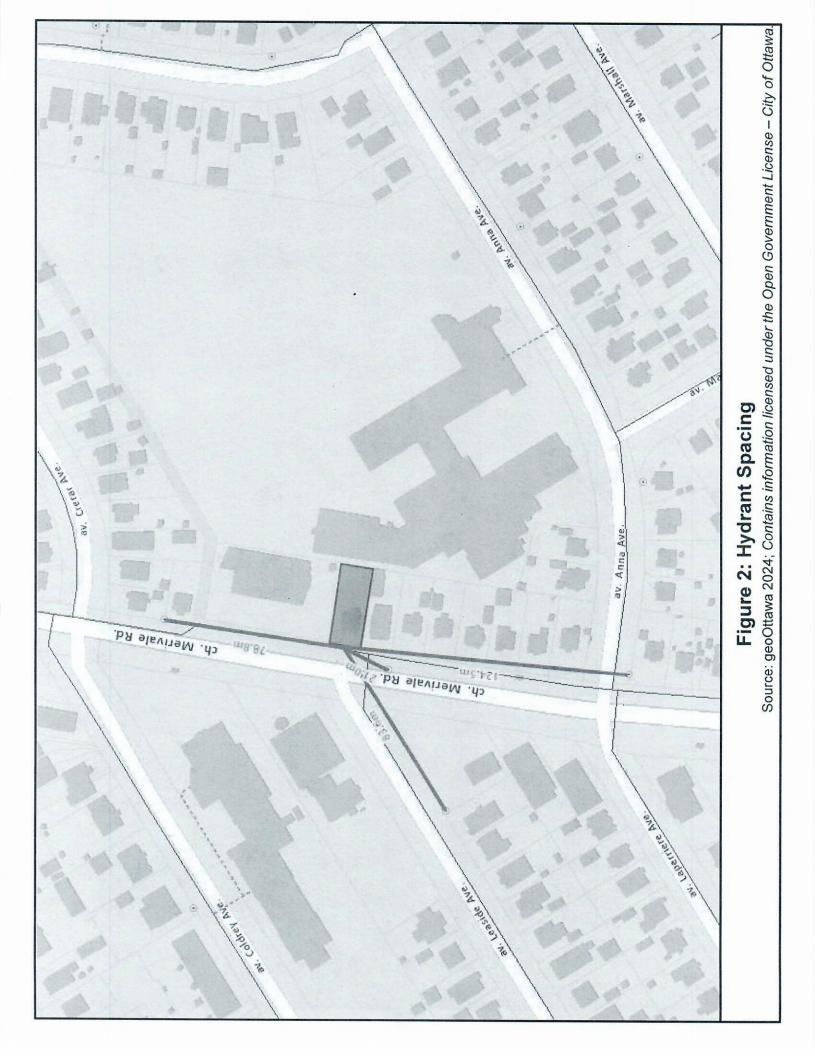
To summarize:

Scenario 1: Minimum Pressure under Peak Hour Demand: 456 kPa (66 psi)

Scenario 2: Maximum Pressure under Average Day Demand: 538 kPa (78 psi)

Scenario 3: Minimum Pressure under Maximum Day + Fire Flow Demand: 393 kPa (57 psi)

ATTACHMENT 6: FIGURE 2 - HYDRANT SPACING



PROPOSED

SIX (6) STOREY APARTMENT BUILDING SITE

LOT 1

R-PLAN 268160

917 MERIVALE ROAD

CITY OF OTTAWA

APPENDIX E

CITY OF OTTAWA

SANITARY SEWER DESIGN SHEET

SHEET No. 1 OF 1

:	1000's	Actual velocity at O(d)		SHEET NO.
	population in 1000). 8	Full flow velocity (m/s)	21-1	
		PROPOSED SEWER Type Grade CapacityFull flow / (L/A) velocity v		COAD ARMENIASA 1FOFFAWA
	g	Grade %		- SE SE SE SE SE SE SE SE SE SE SE SE SE
	$M = 1 + \frac{14}{4 + \sqrt{p}} \times \frac{14}{4 + \sqrt{p}}$ $Q(p) = \frac{pqM}{86.4} (L/s)$ $Q(l) = 1A (L/s) w$ $Q(d) = Q(p) + Q(l)$			SIX (6) STOREY ARM
ت	Q(p)	Pipe size (mm)		4 X X X X X X X X X X X X X X X X X X X
SHEET	•	Length (m)		1777
		Peak design Now Q(d)	9.3	
DESIGN		Peak extraneous (low Q(i) (L/s)	0.02	7024
		Pop. Ilow Q(p) (1./s)	0.93	773
WEF	. 1 \ \	Peaking Inclor M	of the second se	DESIGN CHECKED
SE	DENSITY BEPROOM BACHELOR	CUMULATIVE Area A Pop. (hectares)	0.048	0 5 6
SANITARY SEWER	- 2	CUMUL Pop.	82	(201
ANI		DUAL Area A	3ho.0	11E# 823-10
G)	ap, d)	NDIVIDUAL Area Pop. hectar	87.	#2717
		10	Sand Swift S	
	ask extransous flow (2) ask extransous flow (2) actor (2) (2) population flow (1/s) extransous flow (1/s) design flow	FROM	FESSION CONTRACTOR OF SECONDARY	
	q = average daily per capita flow (2) = unit of peak extransous flow (2) Mapeaking factor $A \subset M \times X \times X \times X \times X \times X \times X \times X \times X \times X \times$	STREET	MEGAWALE MACRAWA MACRA	

•

PROPOSED

THREE (3) STOREY APARTMENT BUILDING SITE

LOT 75

R-PLAN 263

370 ATHLONE AVENUE

CITY OF OTTAWA

APPENDIX F

DEVELOPMENT SERVICING STUDY CHECKLIST SUMMARY





Servicing study guidelines for development applications

4. Development Servicing Study Checklist

The following section describes the checklist of the required content of servicing studies. It is expected that the proponent will address each one of the following items for the study to be deemed complete and ready for review by City of Ottawa Infrastructure Approvals staff.

The level of required detail in the Servicing Study will increase depending on the type of application. For example, for Official Plan amendments and re-zoning applications, the main issues will be to determine the capacity requirements for the proposed change in land use and confirm this against the existing capacity constraint, and to define the solutions, phasing of works and the financing of works to address the capacity constraint. For subdivisions and site plans, the above will be required with additional detailed information supporting the servicing within the development boundary.

4.1 General Content

	Executive Summary (for larger reports only).
×	Date and revision number of the report.
×	Location map and plan showing municipal address, boundary, and layout of proposed development.
×	Plan showing the site and location of all existing services.
	Development statistics, land use, density, adherence to zoning and official plan, and reference to applicable subwatershed and watershed plans that provide context to which individual developments must adhere.
	Summary of Pre-consultation Meetings with City and other approval agencies.
	Reference and confirm conformance to higher level studies and reports (Master Servicing Studies, Environmental Assessments, Community Design Plans), or in the case where it is not in conformance, the proponent must provide justification and develop a defendable design criteria.
×	Statement of objectives and servicing criteria.
×	Identification of existing and proposed infrastructure available in the immediate area.
	Identification of Environmentally Significant Areas, watercourses and Municipal Drains potentially impacted by the proposed development (Reference can be made to the Natural Heritage Studies, if available).
	Concept level master grading plan to confirm existing and proposed grades in the development. This is required to confirm the feasibility of proposed stormwater management and drainage, soil removal and fill constraints, and potential impacts to neighbouring properties. This is also required to confirm that the proposed grading will not impede existing major system flow paths.
	Identification of potential impacts of proposed piped services on private services (such as wells and septic fields on adjacent lands) and mitigation required to address potential impacts.
	Proposed phasing of the development, if applicable.





- Reference to geotechnical studies and recommendations concerning servicing.
- ☑ All preliminary and formal site plan submissions should have the following information:
 - Metric scale
 - North arrow (including construction North)
 - Key plan
 - Name and contact information of applicant and property owner
 - Property limits including bearings and dimensions
 - Existing and proposed structures and parking areas
 - Easements, road widening and rights-of-way
 - · Adjacent street names

4.2 Development Servicing Report: Water

	Confirm consistency with Master Servicing Study, if available
×	Availability of public infrastructure to service proposed development
×	Identification of system constraints
×	Identify boundary conditions
×	Confirmation of adequate domestic supply and pressure
×	Confirmation of adequate fire flow protection and confirmation that fire flow is calculated as per the Fire Underwriter's Survey. Output should show available fire flow at locations throughout the development.
×	Provide a check of high pressures. If pressure is found to be high, an assessment is required to confirm the application of pressure reducing valves.
	Definition of phasing constraints. Hydraulic modeling is required to confirm servicing for all defined phases of the project including the ultimate design
	Address reliability requirements such as appropriate location of shut-off valves
×	Check on the necessity of a pressure zone boundary modification.
×	Reference to water supply analysis to show that major infrastructure is capable of delivering sufficient water for the proposed land use. This includes data that shows that the expected demands under

average day, peak hour and fire flow conditions provide water within the required pressure range





×	Description of the proposed water distribution network, including locations of proposed connections to the existing system, provisions for necessary looping, and appurtenances (valves, pressure reducing valves, valve chambers, and fire hydrants) including special metering provisions.
	Description of off-site required feedermains, booster pumping stations, and other water infrastructure that will be ultimately required to service proposed development, including financing, interim facilities, and timing of implementation.
×	Confirmation that water demands are calculated based on the City of Ottawa Design Guidelines.
	Provision of a model schematic showing the boundary conditions locations, streets, parcels, and building locations for reference.
	4.3 Development Servicing Report: Wastewater
×	Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitored flow data from relatively new infrastructure cannot be used to justify capacity requirements for proposed infrastructure).
	Confirm consistency with Master Servicing Study and/or justifications for deviations.
	Consideration of local conditions that may contribute to extraneous flows that are higher than the recommended flows in the guidelines. This includes groundwater and soil conditions, and age and condition of sewers.
×	Description of existing sanitary sewer available for discharge of wastewater from proposed development.
	Verify available capacity in downstream sanitary sewer and/or identification of upgrades necessary to service the proposed development. (Reference can be made to previously completed Master Servicing Study if applicable)
×	Calculations related to dry-weather and wet-weather flow rates from the development in standard MOE sanitary sewer design table (Appendix 'C') format.
	Description of proposed sewer network including sewers, pumping stations, and forcemains.
	Discussion of previously identified environmental constraints and impact on servicing (environmental constraints are related to limitations imposed on the development in order to preserve the physical condition of watercourses, vegetation, soil cover, as well as protecting against water quantity and quality).
	Pumping stations: impacts of proposed development on existing pumping stations or requirements for new pumping station to service development.
	Forcemain capacity in terms of operational redundancy, surge pressure and maximum flow velocity.
	Identification and implementation of the emergency overflow from sanitary pumping stations in relation to the hydraulic grade line to protect against basement flooding.
	Special considerations such as contamination, corrosive environment etc.





4.4 Development Servicing Report: Stormwater Checklist

×	Description of drainage outlets and downstream constraints including legality of outlets (i.e. municipal drain, right-of-way, watercourse, or private property)
	Analysis of available capacity in existing public infrastructure.
×	A drawing showing the subject lands, its surroundings, the receiving watercourse, existing drainage patterns, and proposed drainage pattern.
X	Water quantity control objective (e.g. controlling post-development peak flows to pre-development level for storm events ranging from the 2 or 5 year event (dependent on the receiving sewer design) to 100 year return period); if other objectives are being applied, a rationale must be included with reference to hydrologic analyses of the potentially affected subwatersheds, taking into account long-term cumulative effects.
	Water Quality control objective (basic, normal or enhanced level of protection based on the sensitivities of the receiving watercourse) and storage requirements.
×	Description of the stormwater management concept with facility locations and descriptions with references and supporting information.
	Set-back from private sewage disposal systems.
	Watercourse and hazard lands setbacks.
	Record of pre-consultation with the Ontario Ministry of Environment and the Conservation Authority that has jurisdiction on the affected watershed.
	Confirm consistency with sub-watershed and Master Servicing Study, if applicable study exists.
×	Storage requirements (complete with calculations) and conveyance capacity for minor events (1:5 year return period) and major events (1:100 year return period).
	Identification of watercourses within the proposed development and how watercourses will be protected, or, if necessary, altered by the proposed development with applicable approvals.
×	Calculate pre and post development peak flow rates including a description of existing site conditions and proposed impervious areas and drainage catchments in comparison to existing conditions.
	Any proposed diversion of drainage catchment areas from one outlet to another.
×	Proposed minor and major systems including locations and sizes of stormwater trunk sewers, and stormwater management facilities.
	If quantity control is not proposed, demonstration that downstream system has adequate capacity for the post-development flows up to and including the 100 year return period storm event.
	Identification of potential impacts to receiving watercourses
	Identification of municipal drains and related approval requirements.
×	Descriptions of how the conveyance and storage capacity will be achieved for the development.
×	100 year flood levels and major flow routing to protect proposed development from flooding for establishing minimum building elevations (MBE) and overall grading.

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	Inclusion of hydraulic analysis including hydraulic grade line elevations.
×	Description of approach to erosion and sediment control during construction for the protection of receiving watercourse or drainage corridors.
	Identification of floodplains – proponent to obtain relevant floodplain information from the appropriate Conservation Authority. The proponent may be required to delineate floodplain elevations to the satisfaction of the Conservation Authority if such information is not available or if information does not match current conditions.
	Identification of fill constraints related to floodplain and geotechnical investigation.
	4.5 Approval and Permit Requirements: Checklist
	The Servicing Study shall provide a list of applicable permits and regulatory approvals necessary for the proposed development as well as the relevant issues affecting each approval. The approval and permitting shall include but not be limited to the following:
	Conservation Authority as the designated approval agency for modification of floodplain, potential impact on fish habitat, proposed works in or adjacent to a watercourse, cut/fill permits and Approval under Lake and Rivers Improvement Act. The Conservation Authority is not the approval authority for the Lakes and Rivers Improvement Act. Where there are Conservation Authority regulations in place, approval under the Lakes and Rivers Improvement Act is not required, except in cases of dams as defined in the Act.
	Application for Certificate of Approval (CofA) under the Ontario Water Resources Act.
	Changes to Municipal Drains.
	Other permits (National Capital Commission, Parks Canada, Public Works and Government Services Canada, Ministry of Transportation etc.)
	4.6 Conclusion Checklist
	Clearly stated conclusions and recommendations Comments received from review agencies including the City of Ottawa and information on how the comments were addressed. Final sign-off from the responsible reviewing agency. All draft and final reports shall be signed and stamped by a professional Engineer registered in Ontario