City Of Ottawa

Lansdowne Park Event Centre - Ottawa, ON

Stormwater Management Report

September 13, 2024

Confidential







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Project No.: CA0033920.1056 Date: September 13, 2024

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REVISION 2				
FINAL				

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Date

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TABLE OF CONTENTS

1	INTRODUCTION	1
1.1	Scope	1
1.2	Site Location	1
1.3	Design Criteria	1
2	EXISTING CONDITIONS	2
2.1	General	2
2.2	Rainfall Information	2
2.3	Modelling Methodology	2
∩ 4	Existing Conditions Model Results	4
2.4		4
2.4 <mark>3</mark>	POST DEVELOPMENT CONDITIONS	
	-	5
3	POST DEVELOPMENT CONDITIONS	5
<mark>3</mark> 3.1	POST DEVELOPMENT CONDITIONS	5
<mark>3</mark> 3.1 3.2	POST DEVELOPMENT CONDITIONS General Minor System	5 5 5
<mark>3</mark> 3.1 3.2 3.3	POST DEVELOPMENT CONDITIONS General Minor System Major System	5 5 5 5

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Tables

- Table 2.1:
 Existing Condition Storage Results4
- Table 2.2:
 Existing Condition Peak Flows4
- Table 3.1:
 Proposed Condition Storage Results ..6
- Table 3.2:Proposed Condition Peak Flows6

Appendices

- A City NCC Comments
- **B** Existing Conditions
- B-1 Stantec 2012 Existing Drainage Plan
- B-2 As Built Drawings
- B-3 Stantec 2012 Existing Storm Sewer Design Sheet
- B-4 Stantec 2012 Storm Drainage Schematic
- B-5 PCSWMM Output
- **C** Proposed Conditions
- C-1 Storm Sewer Design Sheet
- C-2 PCSWMM Output
- C-3 ADS Treatment Train Sizing

1 INTRODUCTION

1.1 Scope

Following the Zoning By-Law Amendment submission in September 2023, the Lansdowne Park redevelopment project (Lansdowne 2.0) entered the Site Plan Control Application stage. WSP was again retained by the City of Ottawa to provide servicing, grading and stormwater management design services for the phase 1 (Event Centre) development of the project for Site Plan Control Application.

1.2 Site Location

The Lansdowne site is home to many commercial, residential, and leisure facilities. This includes TD place Stadium, Aberdeen Pavilion, Horticultural Building, mixed-use retail/office/residential, and a subsurface parking lot. The overall site is approximately 15.4 ha, and borders Bank Street to the west, Holmwood Ave to the north, and Queen Elizabeth Drive to the south and east.

1.3 Design Criteria

The existing stormwater management system is outlined in the Stormwater Management Design Report for Lansdowne Urban Park, February 2012, by Stantec Consulting Ltd. The design criteria for the proposed development will follow the same criteria outlined in the Stantec 2012.

- Peak flow rate of 616 L/s to O'Connor Street sewer for all events from the 2-year to the 100-year return period
- Stormwater shall be treated to MOE "enhanced" standard (80% TSS removal)
- The "first flush" (i.e. 10mm event) shall be directed to the O'Connor Street sewer for the entire site drainage area.
- Outflow to O'Connor Street Sewer will be restricted if the downstream system surcharges and will be cut off when the receiving sewer HGL is higher than the onsite HGL.
- Minor system shall be design for a 5-year level of service with minimal surface ponding.
- Major system shall provide a 100-year level of service while minimizing outflow to the canal.

2 EXISTING CONDITIONS

2.1 General

The existing conditions on the Lansdowne site are as designed in the Stantec Stormwater Management Design Report – Lansdowne Urban Park (2012). The primary site stormwater outlet is to the storm sewer on O'Connor Street, which discharges to a combined sewer at the intersection with Fifth Street. During large storm events (i.e. greater than the 5-year return period) runoff is directed to the Rideau Canal through an overflow pipe.

Based on the 2012 Stantec report and Survey runoff from O'Connor Street flows south to a sag in the road next to Syliva Holden Park.

2.2 Rainfall Information

The stormwater management system consists of two subsurface storage tanks, surface storage on the Great Lawn, outlet controls, and quality control structures. The two underground storage tanks provide 600 m³ in Basin 1 and 2200 m³ in Basin 2, with 700 m³ provided in pipe storage (total of 3500 m³ subsurface storage). A minimum storage volume of 3000 m³ is also provided on the surface of the Great Lawn.

A schematic of the existing stormwater management strategy is included in Appendix B.

A PCSWMM model was created to represent the existing conditions on the site based on the documentation provided in the Stantec 2012 report and the As-Built servicing drawings, included in Appendix B.

2.3 Modelling Methodology

A PCSWMM model of existing conditions was created as a baseline with which to compare the proposed design.

- Catchment Areas: Catchment areas were delineated based on the Stantec catchment area plan (C03). Sub-catchment imperviousness was determined by creating a land use shapefile and using the PCSWMM spatial weighting tool. Subcatchment parameters are included in Appendix B.
- Storm Sewers: Storm sewers were modelled as conduits with their size and inverts based on the as-built servicing drawing. A roughness coefficient of 0.013 and average loss coefficient of 0.2 was used.

- Weirs: Weirs were used to direct runoff to the major flow route when storm sewer capacity is exceeded. Weirs are also used within the underground storm chamber inlet/outlet structures.
- Orifices: An orifice was modelled at the quantity control structure with a discharge coefficient of 0.62. Orifices were also used in the model to represent the 450 mm backflow preventers within the underground storage chamber inlet/outlet structures.
- Storage: Underground storage chambers were modelled using storage nodes with storage curves based on their storage area. The Great Lawn was modelled as a storage node with storage defined as the average area available for storage. Roof storage was also modelled based on the documentation in the DSEL FSR report (2012).
- Ditches: Ditches shown in the Stantec grading plan were modelled as conduits.
 Ditches were connected to storm sewers with a catch basin and discharge curve as per MTO design chart 4.19.
- Rainfall: The 3-hour Chicago storm using the IDF parameters from the Ottawa Sewer Design Guidelines was used in the analysis.
- Tailwater Conditions: Tailwater conditions at O'Connor Street were set as a timeseries with a peak at the 5-year peak HGL of 65.2 m. The timeseries was calibrated to produce similar results to those shown in the Stantec report. This tailwater condition will be revised as more information becomes available.

The results of the existing conditions PCSWMM model are not expected to exactly match those of the Stantec 2012 report due to the following:

- Data regarding tailwater condition In the Stantec analysis, they were provided with the City of Ottawa Infoworks model for the Holmwood and O'Connor sewer system so were able to incorporate a dynamic tailwater condition at the site outlet. The PCSWMM model can be refined as more information becomes available.
- Infoworks Model Stantec modelling for the existing site was completed in Infoworks. WSP has requested this model to review catchment parameters and model setup. Without the model or detailed documentation, differences in modelling parameters and methodology are inevitable leading to variations in model results.
- 3. SWMM Engines Developments in stormwater management modelling software engines have been made since 2012, which affects the ability to replicate results.

The focus of this analysis is on the comparison between storage and outflows in the existing conditions PCSWMM model versus the proposed conditions PCSWMM model.

The design intent is to match the outflows from the existing conditions PCSWMM model. PCSWMM modelling output is included in Appendix B.

2.4 Existing Conditions Model Results

The existing conditions PCSWMM model was run for the 5-year and the 100-year events. Storage volumes for Basin 1, Basin 2, and the Great Lawn are shown in Table 2.1, and peak flows at the outfalls in Table 2.2.

Table 2.1: Existing Condition Storage Results

	5-year		100-year	
	Peak Volume (m ³)	Peak HGL (m)	Peak Volume (m ³)	Peak HGL (m)
Basin 1	630	64.47	632	64.67
Basin 2	2236	64.47	2238	64.65
Great Lawn	215	64.43	2040	64.65

Table 2.2: Existing Condition Peak Flows

Outlet Location	5-year Peak Flow (m³/s)	100-year Peak Flow (m³/s)
O'Connor Sewer	0.524	0.590
Rideau Canal	0.0	0.131

Please note that the 2012 Stantec report and infoworks model resulted in a 100-year release rate of 0.616 m³/s. The recreated PCSWMM model presented above in Table 2.2 shows a lower flow rate. An allowable release rate of 0.616 m³/s is used for the purpose of this report.

3 POST DEVELOPMENT CONDITIONS

3.1 General

Under proposed conditions the majority of the site land use remains as it is under existing conditions, except for the new event centre. The new event centre requires some rerouting of storm sewers and encroaches on the surface storage previously provided in the Great Lawn. The proposed design involves routing storm sewers south of the new event centre and installing subsurface storage beneath the Great Lawn to account for the additional storage required from the change in land use and elimination of storage available on the surface.

3.2 Minor System

The subject site will be serviced by a storm sewer system designed in accordance with the amendment to the storm sewer and stormwater management elements of the Ottawa Design Guidelines. The minor system has been designed to convey the 5-year storm without ponding on the surface. Storm sewer design sheets are included in Appendix C. A hydraulic analysis report prepared by the trench drain supplier, ACO, demonstrates that the trench drains can collect and convey the 100-year runoff rate without over topping, the report is included in Appendix C.

3.3 Major System

The major system will remain similar to how it is in existing conditions. The site is graded toward to Great Lawn where trench drains around the perimeter will intercept overland runoff and direct it to the underground storm chamber under the Great Lawn. Emergency overland flow is directed toward the Rideau Canal during extreme events exceeding the 100-year design storm. There is no pipe outlet to the Rideau Canal.

3.4 Quantity Control

Additional storage is required to account for the addition of the new event centre and the removal of surface storage on the Great Lawn. The proposed storm system was modelled in PCSWMM according to the same methodology presented in Section 2.3. Sub-catchment areas and parameters were modified based on the proposed development. To size of the new underground storage chamber (Basin 3) it was

modelled iteratively to determine the required area and volume to match the existing conditions PCSWMM model results.

The new underground storage chamber beneath the Great Lawn will have a volume of 4777 m³. A specification drawing from the supplier is included in Appendic-C3. Replacing the surface storage with underground storage will improve the useability of the Great Lawn for recreation and events as the ground surface will no longer be used to pond runoff. Overland flow directed to the Great Lawn will be captured by trench drains around the perimeter, and the lawn will be graded to avoid ponding. In events greater than the 100-year storm flow will be directed overland to the Rideau Canal.

Storage volumes and peak HGL during the 5-year and 100-year events for Basin 1, Basin 2, and the new Basin 3 are shown in Table 3.1. Peak flows are shown in Table 3.2.

	5-year		100-year	
	Peak Volume (m ³)	Peak HGL (m)	Peak Volume (m ³)	Peak HGL (m)
Basin 1	530	63.91	630	64.46
Basin 2	1289	63.67	2237	64.47
Great Lawn/ Basin 3	2614	63.67	4648	64.47

Table 3.1: Proposed Condition Storage Results

Table 3.2: Proposed Condition Peak Flows

Outlet Location	5-year Peak Flow (m³/s)	100-year Peak Flow (m³/s)	100-year Allowable Release Rate (m³/s)
O'Connor Sewer	0.315	0.581	0.616
Overland to Rideau Canal	0.0	0.0	0.0

3.5 Quality Control

As noted in Section 1.3, the water quality criteria requires the long-term removal of 80% TSS on an annual loading basis. To achieve the required water quality requirement a treatment train approach is proposed.

Runoff directed to the proposed underground storage will be treated by an OGS and the Isolator® Row Plus provided in the chamber system.

An Isolator® Row Plus shall be proposed at each storm inlet to provide water quality control with easy access for maintenance. The Isolator® Row Plus is the first row of StormTech chambers covered in a non-woven geotextile fabric with a single layer of proprietary woven fabric at the bottom that serves as a filter strip, providing surface area for infiltration and runoff reduction with enhanced suspended solids and pollutant removal. The open-bottom chambers allow stormwater to flow out of the chambers, while sediment is captured in the Isolator® Row Plus.

The Isolator® Row Plus is designed to capture the "first flush" and offers the versatility to be sized on a volume basis or a flow-rate basis. An upstream manhole not only provides access to the Isolator® Row Plus but includes a flow splitter such that stormwater flow rates or volumes that exceed the capacity of the Isolator® Row Plus bypass through a manifold to the other chambers. This creates a differential between the Isolator® Row Plus and the manifold, thus allowing for settlement time in the Isolator® Row Plus. After Stormwater flows through the Isolator® Row Plus and into the rest of the StormTech chamber system, it is passed at a controlled rate through an outlet manifold and outlet control structure.

The Isolator Row® Plus was verified by Environmental Technology Verification (ETV) in July 2020, with an average 82% removal efficiency of Total Suspended Solids (TSS). Refer to Appendix C for ETV verification statement.

The net annual removal efficiency of the proposed OGS and Isolator Row® Plus is provided in Appendix C.

4 CONCLUSIONS

The Ottawa Sport and Entertainment Group in collaboration with the City of Ottawa are proposed to demolish the existing Civic Arena and North Stands. The proposed Lansdowne 2.0 will include a new 5,500 seat Event Centre, a new 11,200 to 12,000 seat spectator North Stadium Stands and the addition of rental and owned residential units with approx. 1199 units, and associated subsurface parking, as well as the significant landscaping east of the new Event Centre.

Water Quantity

The site will be required by the City to limit the discharge of stormwater to the existing conditions peak flow rate, with stormwater up to the post-development 100yr storm stored on-site. Preliminary estimates of the runoff rates lead to an approximate maximum site discharge rate of 581 L/s to the O'Connor Street sewer, with additional required storage of 4648 m³.

Water Quality

A treatment train comprised of an OGS and isolator row are proposed to in order to ensure 80% TSS removal for the site.

APPENDIX





File Number: D01-01-23-0009 D02-02-23-0047

August 3, 2023

Patricia Warren Fotenn Planning + Design Via email: <u>warren@fotenn.com</u>

Subject: Official Plan and Zoning By-law Amendment Application – 945 & 1015 Bank Street – Formal Review Comments

Please find below the consolidated comments from the formal review of the above noted applications.

1. Planning

Comments:

- 1.1. Generally, the proposal is in keeping with the Official Plan adopted by Council.
- 1.2. The Policy team is supportive of the proposed OPA, but requested that a minor change be made.

"Rather than stating that the Special District policies supersede the Greenspace designation, it would be more appropriate to simply list in the areaspecific policy the desired permitted uses on lands designated as Greenspace within the Special District (i.e., an event centre with a green roof etc.).

The preamble in Section 6.6 – Special Districts of the Official Plan states: "[...] They are distinct areas that transcend the role and function of Hubs, Corridors and Neighbourhoods, and warrant unique planning approaches." Notably, Greenspaces are not included in this list as they are intended to maintain their original function within the Special Districts.

It would be more appropriate to expand what is permitted rather than risk setting a precedent that allows for OPAs to effectively eliminate the greenspace function in other Special Districts."

1.3. Please see the draft OPA and ZBA details attached for review and comment.

2. Engineering

Comments:

Functional Servicing & Stormwater Management Study, prepared by WSP, May 25, 2023

2.1. General



Section 1.3 of the report states "the minutes for the Pre-Application Consultation Meeting for this Zoning By Law Amendment is provided for reference in Appendix A". Meeting minutes could not be found in appendix A please revise.

2.2. Storm

PCSWMM models are under review by City of Ottawa staff, comments will be provided upon receipt.

The underground storm water storage tank (approx. 4100m3) proposed within the great lawn as part of the study requires technical foundation design based off a geotechnical investigation of the subsurface profile. Please coordinate with the geotechnical engineering consultant Parsons to ensure that the geotechnical study considers this aspect of the design and speak to this in the report.

2.3. Sanitary

Provide detailed calculations used to determine the existing sanitary flows, and the anticipated sanitary flows.

2.4. Water

Table 2-2 Water Demand and Boundary Conditions Existing Conditions does not match the required fire flow or water demand calculations in Appendix A please clarify and revise.

Provide boundary condition email correspondence with the City of Ottawa in the Appendix of the study.

Please modify section 2.3 (Domestic Supply and pressure) to reference technical bulletin ISD-2010-0

<u>Geotechnical Investigation Proposed Lansdowne Rink and Towers, prepared by</u> Paterson Group, June 28, 2023, Report: PG5792-1

2.5. The project consists of significant underground storm water storage tank (approx. 4100m3) proposed within the great lawn as part of the functional servicing and storm water management study prepared by WSP. Please confirm and coordinate with WSP's consulting team to ensure that the geotechnical study considers this aspect of the design and speaks to this in the report. The geotechnical investigation should speak to the foundation of the storage tank and determine if additional investigation of the subsurface within the great lawn is required for this proposed structure. For more information, please consult the study prepared by WSP.

Roadway Traffic Noise Feasibility Assessment, prepared by Gradient Wind Engineering Inc., June 16, 2023, Report: 23-053-Traffic noise feasibility.

2.6. During 10. Bank street is divided Arterial not undivided in front of the project, so traffic volume count should be 35,000 instead of 30,000, please clarify. In addition, Queen Elizabeth Drive roadway classification is not listed within the city of Ottawa official plan and Transportation master plan please provide source of Queen Elizabeth Drive roadway classification.



- 2.7. In section 4.2.3 of the assessment, it is unclear if the listed parameters used for the noise prediction calculations were imputed for the STAMSON model, the Predictor-Lima model, or both. Please clarify in the body of the report.
- 2.8. The noise feasibility assessment is required to be modeled using the City of Ottawa approved STAMSON modeling program. Additionally, the STAMSON results shown in the report have shown consistently higher results therefore it is possible the STAMSON model is more conservative. Please provide significant justification for the use of the Predictor-Lima software over the approved STAMSON software.
- 2.9. Have noise impacts from the stadium been factored into the assessment for the predicted noise levels of the outdoor living areas?
- 2.10.Additional information is required for the analysis of the proposed event center. Quantify the predicted noise levels, and to what extent will the proposed 'room within a room' design mitigate the anticipated noise. Similarly, quantifiable information and assessment of the noise generated from pedestrians congregating at the event center is required to be investigated. What are the potential sound levels generated by the congregating pedestrians, will this impact the residential units as well as the outdoor amenity areas of the proposed towers?
- 2.11. The STAMSON calculations for receptor 3 and receptor 4 use different barrier heights, please clarify.
- 2.12.The STAMSON calculations for receptor 3 use a receiver source distance of 80m where receptor 4 uses a receiver source distance of 76m. Based on figure-3 it appears that receptor 3 is closer to the noise source please clarify.
- 2.13.As per the noise feasibility assessment the following construction is proposed for the event center east of the proposed towers "the floor could be isolated, jack up slab, the interior walls would be built of double row studs with the first row of studs built on top of the isolation slab. The second row of studs would be on the surrounding structure. A suspended ceiling would be hung using isolation hangers". Please confirm and coordinate with the geotechnical consultant, Parsons Group, that this type of construction is feasible within the geotechnical constraints of the site. Please speak to this within the assessment.

Phase I & Phase II Environmental Site Assessment

2.14.It has been confirmed with City staff that a Phase I & Phase II environmental site assessment is not required for the Zoning By-law Amendment or The Official Plan Amendment. A phase I and phase II environmental site assessment will be required for the subsequent Site Plan Control application.

Pedestrian Level Wind Study, prepared by Gradient Wind Engineering Inc., June 15, 2023

2.15.It has been confirmed with City staff that the pedestrian level wind study is under review by the urban design.



3. Corporate Real Estate Office

Comments:

- 3.1. A new Phase One Environmental Site Assessment (ESA) will be required at the time of Site Plan. Should the Phase One identify any Areas of Potential Environmental Concern, a Phase Two ESA will also be required.
- 3.2. A Record of Site Condition (RSC) will have to be filed with the Ministry of Environment, Conservation and Parks in order to permit the more sensitive residential land use in the area currently occupied by the north side stands and arena structure. This can also be addressed with conditions at the time of Site Plan Approval.

4. Transportation

Comments are forthcoming.

5. Urban Design

Comments:

Clarification questions and additional information requested:

- 5.1. The zoning schedule permits 38m heights and has a notch close to the Aberdeen Pavilion (Please see the Appendix 1, image 1- area circled in red color). The podium of Tower 3 appears to extend the permitted 38m beyond the zoning line. Does the 'tail' of the proposed building fall within the area with a 6m height max (see Appendix 1, image 2– blue line is estimated as the location of the zoning line). Please provide a drawing that overlays the zoning lines with the proposed building footprint to provide clarity.
- 5.2. During games or festival times, it is essential to have a well-thought-out plan to handle the crowd effectively, including crowd interface with vehicular circulation and parking. Please clarify:
 - 5.2.1. What are the assumptions regarding pedestrian volumes?
 - 5.2.2. What calculations were used to determine volumes for the commercial areas, when there are events and / or multiple events on site, during different seasons etc.?
 - 5.2.3. Were the edges of the public realm determined by pedestrian volumes or by the limits of easements and building footprints?
- 5.3. Please clarify:
 - 5.3.1. Which vehicles can drive down to the Exhibition Way as far as the Aberdeen Pavilion.
 - 5.3.2. Is there residential drop-off / delivery all the way to Tower 3?
 - 5.3.3. Are there alternate locations for the servicing / loading function?
- 5.4. What is the current amount of useable park / great lawn space and what is the size of the park in the proposed concept? Additional dimensioned plans and



section drawings of the berm and grade transition from parkland to Event Centre should be provided.

- 5.5. The Design Brief TOR noted the need to provide both streetscape cross-sections and a conceptual landscape plan. Neither requirement has been met. These drawings are required to evaluate how the public spaces around Aberdeen, Tower 3, and Event Centre, in particular, will work. The drawings should focus on the proposed public realm and indicate, at minimum:
 - 5.5.1. The locations for pedestrian and vehicular movement.
 - 5.5.2. The size and location of pedestrian gathering points and plazas.
 - 5.5.3. The area available for outdoor staging (current versus proposed).
 - 5.5.4. The room available for tree planting.
 - 5.5.5. the space available for street furniture.
- 5.6. Streetscape cross-sections and a conceptual landscape plan are required with the second UDRP submission.
- 5.7. Updated wind and shadow studies are required with the second UDRP submission, based on any proposed revisions.
- Building Massing and Public Spaces:
- 5.8. As noted in previous comments and by the UDRP, tower floorplates shall adhere to the City's High-Rise Building Design Guidelines. Therefore, the floorplates, including balconies, cannot exceed 750m2.
- 5.9. For towers up to 30-storeys, the minimum separation distance between towers is 23m. For towers over 30-storeys, the minimum separation distance is 25m. Greater tower separations should be provided when tower floorplates exceed 750m².
- 5.10. The wind and shadow studies provided show negative impacts on the public realm. Specifically, the shadow study shows that Exhibition Way and the Aberdeen Pavilion are in shadow for large amounts of the day. The wind study shows that Exhibition Way and the plaza spaces around the Pavilion were comfortable for sitting, but with new development these comfortable areas will be reduced. The approach to massing and tower placement should re-considered to minimize the impacts of shadowing and wind on the public realm.
- 5.11.Tower 3 takes away from the experience of the Aberdeen Pavilion; it shifts views and emphasis away from the Pavilion and blocks certain views of the Pavilion. Additionally, it creates significant shadow and wind impacts on the public realm. Urban Design's position is that Tower 3, and the associated podium, should be eliminated (Please see attached Appendix 1, image 3,4 and 5) and the redevelopment of this site should, at maximum, include only two towers.
- 5.12. Urban Design believes that there should be no building where the Tower 3 podium / base is shown. The space should remain open, at grade, public space in order to: (1) enhance the experience of the Aberdeen Pavilion as seen from the south



side stands, (2) allow for enlarged gathering spaces around the Pavilion and entrance to the Event Center (see Public Space comments below) which will be particularly important when there are events / concurrent events, (3) create more opportunities for tree planting and seating areas, and (4) Provide additional public realm on-site.

- 5.13. The attached Appendix 1, images 3,4 and 5 shows the positive impacts on the open space and Aberdeen Pavilion with the removal of the tower 3 and its podium. The removal of this podium and tower also creates clear sight lines from north to south, creating a stronger visual connection between the Event Centre and the existing Lansdowne commercial/mixed use development and associated public realm. This space should remain free and clear of any buildings, including if a three- tower solution be pursued,
- 5.14.Should a three-tower scenario be pursued, the towers are to have a maximum 750m2 floor plate (including balconies) with appropriate separations indicated above, and be located above the north side stands. The attached Appendix 2 illustrates a few conceptual three-tower options.
- 5.15.In a three-tower scenario towers should be of different heights generally. Taller building / higher density should be positioned closest to Bank Street, while the lower can be placed closer to the Aberdeen Pavilion to better integrate with the historical context of the site (see attached Appendix 2).
- 5.16.In a two-tower scenario, which is preferred, a twin-tower design may be appropriate. Appendix 3 compares the shadow impacts of the 3-tower scenario and a 2 -tower scenario.
- 5.17.As currently shown, the Event Centre interrupts the open space and the current slope from the lawn to roof appears to be too steep. Event Centre must be sunk further into the landscape and that the roof must be green and accessible, in order to create a continuous lawn as an extension of the public realm.
- 5.18.It appears as though there will be significant vehicular circulation on the west end of Exhibition Way. There will also be significant pedestrian circulation. The truck entrance to underground parking in front of the Aberdeen Pavilion will also cross a significant pedestrian space. Alternative solutions should be considered to address the potential conflicts where pedestrians and vehicles cross paths.

Key Recommendations:

- 5.19. The Urban Design recommends a zoning envelope for this site be produced by way of a schedule for the final proposed podium and tower(s). In the absence of a zoning schedule, the RFO / RFP process to follow should include the following requirements for the redevelopment:
 - 5.19.1. A maximum tower floor plate, including balconies, of 750m2.
 - 5.19.2. A minimum separation distance of 23m between towers up to 30-storeys and 25m between towers above 30-storeys.
 - 5.19.3. No building where Podium / Tower 3 is currently proposed.



- 5.19.4. Towers to be of different heights (unless in Tower 2 scenario the twintower may be appropriate)
- 5.19.5. Direction regarding podium design and height
- 5.19.6. An Event Center with a publicly accessible, green roof that functions as a useable extension of the public open space.
- 5.19.7. The maximum footprint of the Event Centre

6. Urban Design Review Panel

Key Recommendations:

- 6.1. The Panel recommends designing the site both for event days and the everyday experience of locals.
- 6.2. The Panel recommends the focus of this next phase of development should be to ensure established qualities are not compromised by the new development.
 - 6.2.1. The Panel recommends year-round success of the pedestrian realm must be achieved and enhanced.
 - 6.2.2. The Panel recommends the pedestrian accessibility of the site needs to be maintained for events such as the Farmer's Market and future large gatherings around the proposed event space.
- 6.3. The Panel supports opening up Exhibition Way to further pedestrian activity.
- 6.4. The Panel has concerns with the proposed event centre being too high in the landscape.
 - 6.4.1. The Panel strongly recommends lowering the event centre further into the ground and providing pedestrian access to the rooftop greenspace as a continuation of the park lawn.
 - 6.4.1.1.Consider the overall pedestrian accessibility to the event space, and the potential for large gatherings.
- 6.5. The Panel strongly recommends the towers follow the City's guidelines of a 750sq.m. floorplate.
 - 6.5.1. The Panel recommends further investigating a single-tower or two-tower concept to allow for the 750-sq.m floorplates to be achieved.
 - 6.5.2. The Panel suggests doing so will improve the porosity of the site and maintain north-south views across Lansdowne Park, while minimizing wind and shadow impacts on the public realm.
- 6.6. The Panel has concerns with the orientation and location of Tower 'C' and its tight condition with the Aberdeen Pavilion.
 - 6.6.1. Consider forgoing a three-tower approach.
- 6.7. The Panel recommends that the future design of the podium consider using masonry to best relate to the Bank Street frontage and neighbourhood character.



Site Design & Public Realm:

- 6.8. The Panel appreciates and understands all the challenges with funding and the complexity of adding users, servicing, access, and new stands, etc.
- 6.9. The Panel suggests locating the truck entrance in front of the Aberdeen Pavilion is problematic and would create a lot of challenges.
 - 6.9.1. Consider consolidating servicing to avoid conflicts.
 - 6.9.2. Consider locating the servicing between the podium and the bleachers, preferably with access from west side closer to Bank Street to mitigate trucks driving further into the site.
- 6.10. The Panel appreciates the existing amenities of Lansdowne and how it has maintained amenities that are multi-generational, with a good balance of commercial uses and public spaces/events. Consider reinforcing this aspect of the site.
- 6.11. The Panel appreciates that the site could support additional density to help animate Lansdowne Park. However, the Panel has concerns with Lansdowne Park's ability to provide space that is pedestrian friendly and pedestrian focused, which are central to Lansdowne Park's success—and transformative for Ottawa.
 - 6.11.1. The Panel recommends that this unique characteristic of Lansdowne as a pedestrian space and as a city outdoor public amenity must be protected and enhanced. Any diminishment of that would be a concern.
- 6.12. The Panel has concerns with the lack of porosity north-south.
 - 6.12.1. Consider increasing the porosity between the buildings in the north-south direction.
- 6.13.The Panel has concerns with the relationship between Tower 'C' and Aberdeen Pavilion.
 - 6.13.1. The Panel has concerns with how Tower 'C' seems to significantly obstruct the Aberdeen Pavilion and the event centre.
 - 6.13.2. The Panel suggests that Tower 'C' obstructs the connectivity and accessibility of the site and negatively affects the north-south access in front of Aberdeen Pavilion.
- 6.14. The Panel has questions and concerns with the location and orientation of Tower 'C'.
 - 6.14.1. Consider re-orientation to align with the street grid.
- 6.15. The Panel appreciates that the views from the Rideau Canal have been maintained. However, Tower 'C' shifts the views away from the heritage of Aberdeen Pavilion and is much too prominent in the view planes.
 - 6.15.1. The Panel recommends enhancing the entrance to the event centre and protecting the views of Aberdeen Pavilion by removing Tower 'C'.



- 6.16. The Panel recommends at a minimum to incorporate a 23-meter separation between Tower 'C' and the Aberdeen Pavilion.
- 6.17.The Panel has concerns with the proposal's large impact on the pedestrian realm, and outdoor eating and patio spaces.
 - 6.17.1. The Panel recommends a single tower and podium approach that minimizes the wind and shadowing effects of the tower on the pedestrian realm.
- 6.18. The Panel appreciates that there are various elements of the proposal that are being connected through the site by the promenade behind the stands and the ceremonial stairway, however these may not be the priority to preserve in the grand scheme.
- 6.19.The Panel recommends any redevelopment of Lansdowne ensures that it remains a great destination in the city for Ottawans and visitors.

Sustainability:

6.20.The Panel strongly recommends and emphasizes that it is an important task to adhere to the sustainability standards and urban design guidelines that the City has implemented or is planning on implementing.

<u>Sustainability</u>:

- 6.21. The Panel strongly recommends and emphasizes that it is an important task to adhere to the sustainability standards and urban design guidelines that the City has implemented or is planning on implementing.
- 6.22. The Panel appreciates the aspirations and objectives of the project and the rejuvenation of the stands and site.
 - 6.22.1. The Panel understands the economic model of the project and the neutral cost aspect.
- 6.23.The Panel strongly recommends adhering to the City's high-rise design guidelines for this City-led project.
 - 6.23.1. The Panel strongly recommends that the guideline's 750-sq.m. floorplate should be followed.
 - 6.23.1.1. Views from the entrance off Queen Elizabeth Driveway (11), from the Bank Street bridge (13), and from Sunnyside/Bristol (7) are all significantly improved with a smaller floorplate design.
 - 6.23.2. The Panel strongly recommends the massing be adjusted with slender towers that meet the 750-sq.m. floorplates and separation distances of the guidelines. Doing so would result in much better views of Lansdowne from afar, and reduce the shadow and wind impacts on the pedestrian realm.
- 6.24.The Panel recommends that more slender towers and protecting important sky views will greatly improve the proposal.



- 6.25.The Panel recommends staggering the heights of the towers with the goal of making the high-rise portion seem less like a barrier.
- 6.26.The Panel recommends designing the project with a brick and stone material palette to help create a cohesive sense of a precinct and to strengthen the character of the area.
 - 6.26.1. The Panel recommends the final product pick up on the prominent use of brick as a character element of Bank Street.
 - 6.26.2. The Panel appreciates the articulation of the podium, however, recommends the materiality should be more tactile and more residential in nature rather than having a glazed commercial appearance.
 - 6.26.3. The Panel recommends the final product should be a residential brick and stone palette, especially on the podium, to enhance the character of Bank.
- 6.27.The Panel has concerns with the event centre in terms of how it blocks and interrupts the pedestrian experience of the site.
 - 6.27.1. The Panel encourages the applicant to consider alternate sectional studies and provide further analysis to better inform the end result.
 - 6.27.2. The Panel strongly recommends lowering the event centre into the ground and seamlessly connecting the park with its roof to create a park space for public enjoyment, despite additional cost.
- 6.28.The Panel encourages the applicant to consider alternate sectional studies and provide further analysis to better inform the end result.
 - 6.28.1. Consider other amenities instead to highlight the 'highline' effects. Residential units facing the bleachers should not be an option.
- 6.29.The Panel appreciates the decision to setback the podium and open up space on the south side of Exhibition Way.
- 6.30.The Panel recommends further developing the ceremonial stairway. Consideration needs to be given to accessibility standards.
- 6.31.The Panel recommends pursuing a two-tower approach instead of the three-tower proposal.

7. Heritage

Comments:

7.1. Heritage Context and Background

Existing Context

The Lansdowne Park is the site of the former Central Canada Exhibition Association fairground (1888 – 2009). It is bounded by Bank Street to the west, Holmwood Avenue to the north, and the Queen Elizabeth Driveway (QED) and



the Rideau Canal, National Historic Site of Canada, Canadian Heritage River and UNESCO World Heritage Site to the east and south.

The site contains the Aberdeen Pavilion and Horticulture Building, both of which are designated under Part IV of the Ontario Heritage Act. The Aberdeen Pavilion - a structural steel and pressed metal late-Victorian exhibition hall – was designed by architect Moses C. Edey and constructed in 1898. It is designated a National Historic Site and is also designated by the City of Ottawa under Section 29 of the Ontario Heritage Act (Bylaw No. 22-84). The Prairie-style two-storey brick Horticulture Building opened in 1914 and its design is attributed to architects Francis C. Sullivan (1882-1929) and Allan Keefer (1883-1952).

Permissions, Applications and Review

Part of the site, including the Aberdeen Pavilion and Horticulture Building, are subject to a 2012 Heritage Conservation Easement Agreement between the City of Ottawa and the Ontario Heritage Trust, which includes protected view corridors, and delineated framing and setting lands. Permission will be required from the Ontario Heritage Trust for any construction within the Easement.

The Site is subject to the 1993 Parks Canada and City of Ottawa Cost-Share Agreement and accompanying (1990) Aberdeen Pavilion Conservation Report that identifies the importance of maintaining clear vistas at each of the four entries to the Pavilion.

In accordance with Section 33 (1) of the Ontario Heritage Act, a heritage permit is not required as the proposed alterations will not impact the heritage attributes of the Aberdeen Pavilion and Horticulture building as set out in the designating bylaw. This document has been prepared by Heritage Planning staff at the City of Ottawa as the formal comments on the Official Plan and Zoning By-law Amendments for Lansdowne Park.

Section 4.5.2.1 of the City's Official Plan states that when reviewing development applications properties on, or adjacent to a designated property, the City will ensure that the proposal is compatible by respecting and conserving the cultural heritage value and attributes of the heritage property as defined by the associated designation bylaw and having regard for the Standards and Guidelines for the Conservation of Historic Places in Canada. This will be accomplished through the adaptation of the mitigative measures in the HIA and through the consideration and implementation of Heritage Staff's comments.

7.2. Heritage Impact Assessment:

Heritage Staff generally concur with the findings, recommendations, and conclusions in the HIA provided by ERA Architects Inc. dated June 29,2023. Some of the key impacts identified include:

- The visibility of the proposed towers beyond the silhouette of the Aberdeen Pavilion from the east having some visual impact
- Impact to the dynamic views of the site from the Rideau Canal and adjacent landscapes



- The shadow impact on existing built heritage resources
- The proposed new event centre and extended berm will encroach into the framing lands and Great Lawn south of the Aberdeen Pavilion.

The report concludes that:

The proposed development generally conserves the cultural heritage value of the Site, while allowing for its revitalization. New construction is sited to the southwest portion of the Site, where high-density contemporary structures are currently located. The existing built heritage resources will be retained and rehabilitated as part of ongoing City-initiated programs. Other existing land uses and the spatial organization of the Site will remain unchanged. The proposed development has been designed and situated to minimize impact on the protected HCEA and Parks Canada Cost-Share Agreement views, the setting and framing lands, the Aberdeen Pavilion, and the Horticulture Building. Though protecting the silhouette of the Aberdeen Pavilion is not an express objective of the HCEA, the proposed towers will be visible beyond the silhouette of the Aberdeen Pavilion, creating some visual impact

Mitigative Measures

The mitigative measures identified in the HIA should be implemented and used as guiding principles through the next stages of planning and design for the project. These measure include;

- Design the new retail podium to enhance views to and experience of the Aberdeen Pavilion;
- Enhance the public realm surrounding the new retail podium along Exhibition Way and design for year-round usability;
- Consider the form, massing and materiality of the high-rise towers to complement the new backdrop setting of the Aberdeen Pavilion;
- Consider the high-rise tower shape, placement and articulation to minimize shadow impact; and
- Design the new event centre and berm to minimize visual impact on the south elevation of the Aberdeen Pavilion, while enhancing the Great Lawn open space.
- The commemoration and interpretation of Frank Clair Stadium and Ottawa Civic Centre

Conservation Design Parameters

Similarly, the HIA has detailed Conservation Design Parameters, which are intended to establish a set of conservation objectives and design guidelines for the following areas: Exhibition Way, Event Centre and Southeastern Edge and Tower Design. The Conservation Design Parameters (CDPs) should be implemented to help guide the overall design and maintain the cultural heritage value of the site.



Heritage staff recommend the implementation of the Conservation Design Parameters be included as part of the framework for the RFP of the air rights.

7.3. Additional Heritage Issues /Concerns

Aberdeen Pavillion and the East Tower

Heritage staff have concerns with the proposed eastern tower on the site and its potential impact on the Aberdeen Pavilion. The revitalization of Lansdowne Park offers an opportunity to further highlight the Aberdeen Pavilion as the heart of Lansdowne, efforts should be made to highlight this landmark building and improve the existing condition between the Aberdeen Pavilion and the new building.

The proposed east tower is adjacent to the Aberdeen Pavilion. The HIA identifies that the proposed development will have an adverse impact on the visual prominence of the Aberdeen Pavilion from certain vantage points within and adjacent to the Site. The 2022 Council-approved (in principle) Lansdowne 2.0 Concept Plan tower heights and massing create a shadow impact on the Aberdeen Pavilion by obscuring heritage features from late morning to early afternoon during the fall and winter months. Character-defining attributes including the central cupola and clerestory windows are cast in new shadow during the September and December test dates. Potential at-grade impacts may include pedestrian and vehicular congestion as well as potential impact during construction. The measures identified in in the HIA will help mitigate these impacts and should be implemented.

Heritage Staff suggest that alternative option(s) be considered, such as reducing the floor plate and/or height of the eastern tower and/or removing the tower. Further to the appendices provided with comments from the Public Realm and Urban Design Branch, heritage staff encourage the elimination of the third tower or if three towers are to be considered, moving the tower west towards Bank Street so that all three towers are oriented towards Exhibition Way. As shown in these documents, this will mitigate the negative shadow impacts of the current proposal.



Event Centre



The proposed event centre and relocated berm to the east of the TD Place Stadium will encroach in the framing lands as identified within the Ontario Heritage Trust Easement.



Heritage staff support the Conservation Design Parameter in the HIA that states that: The location and design of the event centre should be further refined to minimize visual impact on the south elevation of the Aberdeen Pavilion, while allowing for continued public use of the Great Lawn.

Any alterations to the property within the boundaries of this easement area requires consultation with and approval from the Ontario Heritage Trust.

Public Realm

The open space surrounding the Aberdeen Pavilion contributes to the legibility and prominence of the building. Recommendations to improve the public realm should be explored in coordination with the Council-approved Guiding Principles for the Transformation of Lansdowne and the City of Ottawa's Strategic Investment Plan for the Urban Park and Public Realm.

Heritage Staff encourage the removal of the proposed parking entrance closest to the Aberdeen Pavilion. If required, it should be limited to use as service access.

7.4. Zoning Specific Recommendations– Heritage

Heritage staff recommend that the following be considered through the proposed Zoning By-Law Amendment and Official Plan Amendment.

7.4.1. Reduce potential impacts on the Aberdeen Pavilion

- For the towers, locate the taller height closer to Bank Street and reduce the height and/or building floor plate of the east tower
- 7.4.2. Protection and enhancement of views of Aberdeen Pavilion
 - Establish an increased setback along the southern portion of Exhibition Way to increase the visibility of the Aberdeen pavilion and ensure both spires of the pavilion are visible from Bank Street.
- 7.4.3. Define and relate the podium height to the Aberdeen Pavilion
 - Limit the height of the podium along Exhibition Way to provide a 3-4 storey streetwall height to ensure compatibility with the Aberdeen Pavilion and the original stadium/grandstand.



- 7.4.4. Provide a maximum height of the event centre
 - Limit the height of the event centre to ensure that the dynamic view of the upper portions of the Aberdeen Pavillion, as defined in the OHT easement, are maintained
- 7.4.5. Public Realm enhancements to conserve and highlight the Aberdeen Pavilion
 - Ensure that the zoning considers the role of open space surrounding the pavilion to maintain its prominence and maintain the established protected views



7.5. Additional Plans and Studies for Site Plan

The following additional plans and studies should be required at site plan:

- HIA Addendum: to look at the more detailed design, including architectural detailing.
- Heritage Interpretation Plan
- Documentation and Salvage Plan for Frank Clair Stadium.
- Heritage Protection Plan for the site which includes:
 - Pre-construction building condition survey and documentation;
 - Vibration and crack monitoring;
 - o Implementation of physical protection for the designated buildings;
 - o Management of construction dust, debris etc.; and
 - Post-construction building condition survey and documentation.

Heritage Planning Staff can assist in the creation and establishment of the terms of reference for these studies and plans.

8. Ontario Heritage Trust

Comments:



8.1. Building Heights

Towers of the height proposed in the ZBA would impose a negative impact on nearby cultural heritage, by:

- Altering the background of protected views of the Aberdeen Pavilion;
- Placing the Pavilion, Park, and adjacent portions of the Canal in shadow;
- Introducing an abrupt transition of building scale, particularly with respect to proposed Tower 3.

The OHT offers this summary assessment while recognizing that the proposed tower locations are not contained within the boundaries of the provincial easement.

8.2. Event Centre

OHT staff have seen conceptual depictions of the proposed Event Centre pass through several iterations. Previously we have indicated that the heritage impact, though negative, appeared manageable.

The iteration contained in these applications, while understood to be still conceptual, appears to have grown significantly in scale (both the building scale and hardscaping). Its impact would be more considerable than that of previous iterations:

- All iterations of the proposed Event Centre would negatively impact protected views of the Aberdeen Pavilion. The iteration associated with this application appears to have grown in height, and therefore in visual impact;
- All iterations would involve construction within identified zones of archaeological potential;
- This iteration shows hardscape extending further into the Park, and in general, a potentially significant reduction of green space within the easement boundaries;
- The current iteration, unlike previous ones, would appear also to disrupt current community uses of this green space. OHT staff have requested that community uses be integrated.

Recognizing again the conceptual state of progress, the design associated with these applications raises new concerns about impact. The OHT looks forward to continuing discussions with the City.

9. Ottawa Public Health

Comments:

9.1. We note that the provision of 1200 bicycle parking spaces exceeds the current Zoning By-law requirements, however, given that many units will be occupied by more than one person, would recommend increasing this. Unsecure bike parking



would be a significant disincentive to using cycling as a primary mode. This would support OP policies 2.2.4, and 4.1 that seek to incentivize active transportation and make cycling the healthy and easy choice.

9.2. Could there be integration of the High Performance Development Standards (HPDS) in this application, given this is on City lands?

10. Climate Change and Resiliency

Comments:

- 10.1. While the HPDS has not come into effect, given that this is a City-owned site, it would be appropriate to push this development to apply the HPDS to the fullest extent possible as a showcase example of a City-led project that advances sustainable and resilient design. In my quick review of the Planning Rationale, I see that:
 - The project will seek a "high level of sustainable design" as part of the future Site Plan Control application, including:
 - alternative energy and energy-efficient measures, including electric and solar energy sources
 - o alternatives to fuel-dependent vehicles
 - The proposed concept will aim for LEED Silver certification and will follow the City's Corporate Green Building Policy
 - Consideration of a green roof for the event centre.

Here is the link to the Tier 1 and Tier 2 of the HPDS: <u>High Performance</u> <u>Development Standards (HPDS) | City of Ottawa</u>

11. Accessibility Committee

Comments:

- 11.1. The UDRP package only includes the word accessibility once. Given the scope and application of this work, it should be more explicit in the vision and design objectives.
- 11.2.Overall, the site should include many accessible rest areas in both active and green spaces.
- 11.3.Renderings:
 - 11.3.1. Should include people with various disabilities. This shows the disability community that they are considered and included in our work.
 - 11.3.2. Ensure TWSIs are not shown as being obstructed. This is something that should be a strong consideration as the Lansdowne space is reimagined. As constructed, they are not serving their intended purpose.
 - 11.3.3. Ensure a clear pedestrian path of travel (unobstructed by bikes, A-frames, patios, etc.)- the City requires 2 m which won't be demonstrated accurately in a rendering, however, it can demonstrate a clear path



- 11.3.4. Patios are required to be delineated. This should be shown in renderings.
- 11.4. How many of the 739 parking spaces will be accessible?
- 11.5. How many visitor parking spaces will be accessible?
- 11.6. Are the ceremonial stairs a primary entrance to the buildings or do they serve a strictly decorative purpose?
- 11.7. Lansdowne has a designated "on-street" accessible parking space above ground will more of these be included?

12. Rideau Valley Conservation Authority

Comments:

12.1. The RVCA has reviewed the above noted Official Plan and Zoning By-law Amendment application for the Lansdowne 2.0 project to permit building heights up to 40 storeys and facilitate a new stand-alone Event Centre at the east end of TD Place stadium and have no objections.

13. National Capital Commission

Comments are forthcoming.

14. Parks Canada

Comments are forthcoming.

15. Enbridge Gas

Comments:

- 15.1. Enbridge Gas does not object to the proposed application(s) however, we reserve the right to amend or remove development conditions.
- 15.2. The applicant will contact Enbridge Gas Customer Service at 1-877-362-7434 prior to any site construction activities to determine if existing piping facilities need to be relocated or abandoned.

16. Telecon

Comments:

16.1. EXTREME CAUTION! TELUS HAS CABLE IN FOREIGN UTILITY'S LEASED DUCTS AND VAULTS, close to the proposed route. Please call for locates.

17. Ottawa Catholic School Board

Comments:

17.1. The Ottawa Catholic School Board has no objection to the proposed zoning amendments and the site plan control proposal for the property located at 945, 1015 Bank Street. However, since new residential developments have an impact on enrolment, transportation routes and attendance boundaries, we would like to



be notified of all decisions pertaining to this application, including notice of public meetings, street name dedications and approval status.

18. Ottawa Catholic School Board

Comments:

18.1.The Planning staff has reviewed the above-noted Official Plan & Zoning By-Law Amendment application. It is understood that the proposed development will have the North stadium stands removed and reconstructed as a standalone structure, which will be the new event centre for Lansdown Park. The proposed development also includes three high-rise residential towers with a maximum height of 40 storeys to be established and will have up to 1,200 residential units.

It is our understanding that the City seeks to amend Area-Specific Policy of the Lansdown Special District designation through an Official Plan Amendment to clarify the City's Official Plan with the following amendments:

- Confirm that the Lansdowne Special District policies supersede the Greenspace and Mainstreet
- Corridor functional designations that are shown on Schedule B2 of the Official Plan.
- Allow for a maximum building height of 40 storeys on the site.
- Allow for a portion of the existing greenspace on the site to be repurposed for a new event centre.

The Zoning By-Law application seeks to rezone a portion of the subject site to permit the new event centre, as well as increase the maximum permitted building height to allow for the proposed 40 storeys and a maximum proposed height of 15.05 meters for the event centre.

Please be advised that our response to your request for comments regarding the proposed development is as follows:

The Ottawa-Carleton District School Board (OCDSB) has no concerns against the proposed Official Plan & Zoning By-Law Amendment. The city is seeking to increase intensification within the urban boundary, and the OCDSB recognizes that new dwellings will generate new students to our local schools.

We would also like to note that the owner be required to inform prospective purchasers that school accommodation pressures exist in the Ottawa-Carleton District School Board schools designated to serve this development which are

19. Councillor and Community issues

Comments:

19.1.Please see summary of community comments (Document 2) attached for review and comment. A public meeting was held on July 13, 2023, with approximately 150 people in attendance.



- 19.2.At this time, planning staff have not received formal comments from Councillor Menard.
- 19.3. Staff received approximately 175 public comments during the comment period. Approximately 60 percent of respondent was opposed to the development while 40 percent are either in support or indifferent.

Please review the following comments and provide a response for each theme.

Building height

- Increase of up to 40 storeys from current limit of 20 storeys is selfish and dangerous
- General opposition to Zoning By-law amendment to increase height
- Tall buildings are an eye sore
- The request to increase the maximum height restriction from 38 metres to 127 is excessive and over three times the existing height.
- These heights are out of place for the neighbourhood and the surrounding heritage buildings
- No building should be taller vs. what is there today
- A set of mid-rise residential buildings, with a more fitting aesthetic for the area, would be much more appealing to Glebe residents

Transition to Adjacent Low-rise neighbourhood

- The high-rises are out of place in comparison to the rest of the Glebe
- Completely out of scale with the charm of the surrounding neighbourhood.
- The Glebe has always had an old-world (aka low-rise) feel. This changes the landscape of this beautiful old community,
- This is an iconic Ottawa site, and to propose 40 story towers, which are so shockingly out of proportion with the surrounding cityscape and the site is outrageous.
- The imposing presence of these buildings not only clashes with the surrounding Glebe aesthetic, it also invades the sight lines of Glebe residents, shoppers, and seasonal event goers

Wind impact

- The towers will cause a wind tunnel that will make walking on Marché very unbearable in winter months.
- The wind study as presented, lacks significant information for an assessment to be made as to its validity and appropriateness in the



current context. If anything, it may underestimate the wind climate problems which could occur were this development to be built.

Shadow impact

- The 3 residential towers proposed will be too tall and will provide too much shade on the Aberdeen Pavilion and the existing structures at Lansdowne
- Three high-rise towers will overwhelm the site especially at 40 stories. They will block the sun and cast long shadows. They will destroy the character of the surrounding area.
- The towers will create large shadows and wind tunnels that will cause the very popular patios on Marché Way to lose most of their sunlight.
- 40 stories will shade so much it will reduce quality of life and enjoyment in the whole area.
- Not only will much of the Lansdowne site be covered by shadow, but also neighboring streets in the Glebe as far as 1st Ave, the canal and streets in Old Ottawa South (across the canal!)
- The angled tower next to the Aberdeen Pavilion is particularly egregious and should be eliminated entirely as it over-shadows the Pavilion
- Eliminating all the sunlight for businesses on exhibition way would be a travesty.

<u>Traffic</u>

- The congestion and confusion in the neighbourhood when events are on now (and even when they aren't) will only be exacerbated by the existence of so many new residential units and the additional events.
- Traffic needs to be addressed to public, and discussions need to be had early on for solving traffic related issues
- Please do whatever is possible to deter more vehicular traffic. It's already a disaster in this regard for anyone living nearby or trying to get to/from that area

Active Transportation (Bicycle and Pedestrian connectivity/safety)

- The active transportation along Bank Street and the Queen Elizabeth Driveway needs to be improved.
- The addition of up to 1200 new units will clog up Bank Street and the nearby neighbourhoods and reduce the ability for pedestrians and cyclists to enjoy the canal and Lansdowne itself.
- Need to widen the Bank Street sidewalks and create properly separated bike lanes



• Increase the transit service to and from the park on Bank Street with a dedicated lane. Get bike lanes on Bank Street and create new and safe bicycling infrastructure to and through the site

<u>Transit</u>

- Insufficient transit options for the site, the busses are insufficient and will only get worse upon development
- How will all of the new residents and visitors get to and from the site.
- Transit for all the events at Lansdowne does not work, building this without implementing better busses or the O-Train will not work

Parking

- 739 parking spaces for 1200 units will be woefully insufficient and 400 cars will try to park in surrounding streets
- unless there is a spot per unit, there will be a spillover to the local neighbourhood
- That a number of dedicated disabled parking spots be implemented in this area would be welcomed.
- Adding 739 vehicles to this space seems designed to create traffic chaos on the site and affected roads.

<u>Density</u>

- Increased density makes sense if there is increased greenspace
- Clearly, the city center is already overcrowded and adding the traffic density expected from thousands of new residents will further degrade the residential environment
- The density of this project will have a negative impact on traffic, transportation, servicing, and greenspace

Loss of Greenspace

- Loss of greenspace will negatively affect the residents on Holmwood
 Ave
- Replacing the arena and moving it to the green space park is a terrible and costly idea. The lawn is well used and enjoyed by many, and will be needed even more to serve the local population if it increases with the towers
- It is obviously a bad idea to add 1200+ yard-free occupants to the site and eliminate greenspace.
- Lansdowne already has very little green space. None of the green space should be lost, especially to build an arena that is not needed. With this loss of green space, Lansdowne will not have enough green



space to hold music festivals. Also, Lansdowne will be even more of a concrete jungle.

- The plan for 35, 40 and 46 storey towers removes whatever pretext remains for calling Landsdowne a park.
- Make the green roof on the new arena accessible to the public. Doing so would help to offset much of the usable greenspace being lost by relocating the arena.
- The overall design of the project should enhance the site with green space and fit in with some aspect of historical respect for the look of the canal site
- Lansdowne is a park and should be kept as such. Should not be developed on and should be enjoyed by all residents of the city.
- Please save all the green area possible in the inner city lest it become a wasteland.

<u>Housing</u>

- The plan is trying to fit in more residential units than are appropriate for the space
- 40-story condominium buildings at Landsdowne will generate very good property tax revenue for the City but does nothing to address the affordable housing shortage. If you were making affordable or public housing this would be acceptable, but it is not.
- We need more affordable housing, and this project will not be, why aren't we seeing proposals for 5-10 storey buildings lining streets instead?
- If housing is to be added to Lansdowne Park, it should be rent-toincome only. I don't feel like subsidizing rich people's access to pricey condos overlooking the sports fields. I can't afford to buy at Lansdowne. Many people cannot.
- These towers would be better used with 2 and 3 bedroom units -Ottawa already has enough bachelor and one bedroom towers, we need to be thinking of more affordable options for families.

Land Use

- People WANT a park -- not an event space, not an arena, but a PARK. A place for leisure, walking, meeting friends
- The proposed three towers would render this end of the Glebe almost unlivable
- This is not a "partnership" (public, private) but handover of public, precious land to satisfy and expand commercial interests.



- Should not be building 40 storey towers in what is supposed to be a park
- Plant some trees, preserve what little green space is left, build peoplefriendly sized buildings with affordable housing
- Why aren't we redeveloping the St Laurent shopping centre into high density and putting the stadium there? It's right on the transit way and the freeway

<u>Heritage</u>

- The towers are also in no way in respect to the beauty and heritage of the UNESCO Rideau Canal and the two heritage buildings on site; the Aberdeen Pavillon and the Horticulture Building. Imagine the city of Rome allowing towers such as proposed to be built beside the Colosseum or beside the Pantheon. We need to honor and respect our heritage buildings and not pollute them with 40 story condo buildings.
- This project will fundamentally change the area by overshadowing the historic Aberdeen Pavilion

<u>Sustainability</u>

- There is waste in destroying the recently built podium.
- Force the developers to use only green technologies to lower Lansdowne's carbon footprint. How about increasing rooftop green space use by planting garden beds and vertical gardens?
- Concrete and steel consumption contribute greatly to carbon emissions. It would be irresponsible to dispose of what's already been built, only to replace it with more concrete and steel.
- putting an arena where some of the limited current green space exists seems contrary to all city policies and guidance for greater green space, and inconsistent with fighting climate change.

<u>Noise</u>

- The increased noise, commotion will absolutely kill The Glebe.
- Please revise to lower density and noise

General Inquiries and comments:

- What failed in financial model of 1.0, and how is that being addressed/prevented in 2.0
- The time to complete this large project of this size would be years. Trying to keep the businesses already in place here running during extensive construction will be very difficult



- Saddling the tax payers of Ottawa for years with billions of dollars of debt to finance the proposal and to line the pockets of OSEG members is criminal.
- Where will the kids go to school? Where will they go to the Doctor/Dentist?
- Lack of public consultation

Positive Comments:

- Full support of application in their current state
- This looks great. I was expecting more of the green space to be used so that more people could live in this desirable neighborhood, but there's not much to object with on the modest proposal
- Density and building heights are good, and keeping the arena within Lansdowne is key to the continued success of the area
- I am in full support of densification. This is essential to improving affordability in the city and reducing our environmental impact.
- I think the towers add good density to an attractive site, and bring a critical mass of residents to increase the vibrancy of Lansdowne.
- I LOVE the proposal for Lansdowne 2.0!! We NEED housing. We NEED a football stadium. We NEED a hockey arena for 67s. PLEASE build this as presented. The 3 towers are in the PERFECT PLACE!!! BUILD THIS PLEASE!!! Thank you.
- Review the financials but as for the development as proposed please approve.
- As a homeowner in the Glebe, I'm trilled to hear that the Glebe will be further densified by this development, as it rightly should be. These new towers will provide valuable housing to this supply-constrained market, will provide many people the opportunity to live in one of the best parts of Ottawa, and will bring tons of business to the local businesses.
- I support the project for 945 and 1015 bank St and I think there should be even more apartments.
- I'm a resident of Centretown, frequenting the Glebe/Lansdowne, and I am 100% in favour of this application moving forward. As someone who has lived inner-city in various cities across Canada, I have witnessed first-hand the good that density like this whether it be market-rate homes for ownership or rental and/or social/affordable homes does for a community. In my view, intensification makes areas vibrant it supports businesses, creates walkable areas, helps cut down on our environmental impact, and fosters a sense of community.



• I am in support. This project will make Ottawa a more competitive city for events and will provide more apartments for people to live in.

Should there be any other questions, please do not hesitate to contact me.

Sincerely,

Krishon Walker

cc. Sean Moore, Director, Lansdowne Park Redevelopment Project Simon Deiaco, Senior Planner Abdul Mottalib, Infrastructure Project Manager Mike Giampa, Transportation Project Manager

National Capital Commission Comments

Thank you for circulating the National Capital Commission (NCC) on applications for Official Plan Amendment and Zoning By-law Amendment for 945 and 1015 Bank Street (D01-01-23-0009 / D02-02-23-0047), "Lansdowne 2.0". The Lansdowne 2.0 initiative presents an opportunity to think boldly about Lansdowne, QED, and broader Capital-building and City-building perspectives. We present the below comments (paired with an attached Appendix in response to the 'Lessons Learned' report) in a spirit of openminded discussion and collaboration on this exciting initiative.

<u>Context</u>

- The current process leading to the redevelopment of Lansdowne began in 2007 as the City sought to replace the existing south-side stands and revitalize the site with new development.
- Lansdowne is bounded to the east and south by the NCC-owned Queen Elizabeth Drive (QED) and Capital Urban Greenspace beside the Rideau Canal.
- The Rideau Canal is owned and managed by Parks Canada, and is a UNESCO World Heritage Site.
- The NCC has been a collaborative stakeholder in the redevelopment of Lansdowne, including approving improvements to pedestrian connectivity from the Rideau Canal Capital Pathway, participating in the Lansdowne Transportation Monitoring and Operations Committee (LTMOC), and permitting by agreement the use of QED for park-and-ride shuttles for major events.

Proposed Development

- The proposal comprises:
 - three high-rise residential towers with up to 1,200 new dwelling units and 739 new parking spaces;
 - replacing the current 3,809 square metres of retail space attached to the arena/stadium complex along Exhibition Way with 9,290 square metres of new mixed-use retail space in the podium of the new residential towers;
 - replacing the north-side stadium stands;
 - a new 1,500-person music hall; and
 - o a new 5,500 seat multipurpose event centre.

<u>Comments</u>

1. Queen Elizabeth Drive

- a. The NCC shares the City's goal of re-imagining Queen Elizabeth Driveway to reduce the road's importance as a commuter route in favour of active mobility and the public realm. The QED is a capital parkway designed for its experiential quality, and not intended as a principal commuting transportation route.
- b. The NCC's guiding principles for Queen Elizabeth Driveway emphasize sustainable and active modes of mobility over private motor vehicle use of the roadway, consistent with the overall vision for NCC parkways as scenic connections between major national areas of significance while providing opportunities for recreational purposes.

QED is a federal parkway under the jurisdiction of the NCC. Since 1970 the NCC has hosted bike days, including periodic full closures of Colonel By Drive. Since 2020 the NCC has expanded this program to other parkways so they are periodically reserved for active use and not for use by vehicles and QED is seasonally reserved for active use from May to October on varying days.

We remain concerned that the TIA analysis does not reflect the reality of regular periods when QED is not available for private vehicle use. We provided feedback on the draft TIA and requested that it evaluate a range of scenarios – different levels of intensity of events at Lansdowne with different formats of QED use. There is a wide range of options and level of impact, wherein QED could be reserved for active use, or opened to shuttles at events of certain sizes. Similarly, the impacts of each option vary by the size of events at Lansdowne: the 1,500-person music venue, the 5,500-seat event venue, events at the Aberdeen Pavilion, and the stadium itself – as each venue is added to a concurrent peak demand, the ways that QED could be used vary.

The TIA and associated studies did not evaluate these more nuanced options to inform the conversation about QED access, instead relying on "our assumption is that the QED will, generally, remain as a viable secondary vehicular access point to Lansdowne". The response provided in the Lessons Learned states that "If the assumptions are not valid, then the integrity of the Lansdowne 2.0 program (and likely current Lansdowne operations) would be severely compromised from a transportation perspective." This generalization lacks nuance – there are levels of intensity of activity at Lansdowne wherein QED access is more critical than others.

Lacking a study of those different levels of intensity and QED access as was requested leaves the applications relying on broad assumptions.

Note: The NCC is currently reviewing its Parkway Policy which will provide direction for future use and evolution of QED. We look forward to working with the City to support sustainable mobility while protecting QED's unique capital vocation.

c. The transportation challenges of Lansdowne will not be solved by prioritizing access by personal vehicles. Where access to Lansdowne is needed for major events, Queen Elizabeth Drive has proven successful at efficiently moving large numbers of people through the shuttle program. Improving access to Lansdowne must prioritize increasing capacity and mobility through making transit and other sustainable modes the preferred choice.

These modes will be the preferred choice not only by requiring the attendees of ticketed events to pay for their transit by providing a transit fare with every ticket, but also on a day-to-day basis making access to Lansdowne by transit and other sustainable modes competitively preferable to personal vehicles in cost, time, and convenience. Keeping QED open to personal vehicles at all times undermines this effort.

2. Capital Urban Greenspace

- a. The *Strategic Investment Plan for the Urban Park and Public Realm* identifies potential projects on adjacent NCC-owned lands:
 - a. Redesigned entrance to Lansdowne at Queen Elizabeth Driveway to better accommodate cyclists and pedestrians with the possibility of a signalized crosswalk.
 - b. Forestry and floral plantings along QED
 - c. Additional signage of speed limit along QED
 - d. A new pedestrian crossing of QED at the site's southeast edge
 - e. A two-way accessible link from Colonel By Drive to Bank via Echo Street

Note: We are supportive of improvements to active transportation connectivity and enhancements to animation of the QED corridor, when they are in keeping with its heritage and cultural significance. A <u>Federal</u>

Land Use Design and Transaction Approval (FLUDTA) will be required for any work that is proposed on federal land.

3. Transportation

- a. It is essential that the transportation plans associated with Lansdowne 2.0 adequately explore the necessary bold sustainable transportation initiatives, projects and investments and site access improvements to reach the City's and the NCC's objectives. Whether identifying issues through the Transportation Impact Assessment for Lansdowne or proposing new projects for the Transportation Master Plan, these processes must work in tandem to improve mobility and access to this important destination.
- b. As noted, the NCC is currently reviewing its Parkway Policy. This initiative, combined with Lansdowne 2.0, presents the opportunity to discuss bold exploratory ideas such as, but not limited to:
 - Piloting conversion of QED & Colonel By Drive to one-way streets while reducing the number of lanes to provide more space for active use;
 - ii. Realigning a portion QED to provide a dedicated access to Lansdowne; and/or
 - iii. Exploring limiting access to QED to major event shuttles, emergency vehicles, and active modes on an ongoing basis by design.
- c. As discussed in Item 1 above, it needs to be understood how Lansdowne 2.0 and the surrounding transportation network will function under a day-today scenario (no medium, major or mega events occurring) with QED closed for active use programming. If it is hypothesized that any long-term, frequent closure of QED will negatively impact the viability of events at Lansdowne, it needs to be understood at what point, in terms of event size programming, does this negative situation occur.
- d. To support a viable Lansdowne at all times, TDM activities must strive for a transit mode share that strives beyond the targets set for Lansdowne 1.0; applying the status quo is not a target.
 - i. It is important to plan for a transit mode share greater than 10% and an auto mode share lower than 75%, even for events below 10,000 persons in attendance. The smaller events with attendance levels of 5,000 or less occur more frequently at Lansdowne. Of the 161 events

expected in 2024 at Lansdowne, approximately 128 (79%) will be under 5,000.

- ii. The Official Plan calls for by 2046, the majority of trips in the city will be made by sustainable transportation. Planning for a 10% transit modal share for 79% of events at Lansdowne will not achieve this objective.
- iii. There is inconsistency in the modal share targets. Table 2 indicates a Transit & Shuttle target of 50-55% for Minor Events. Table 4 indicates a target of 10%.
- iv. The TIA remains based on forecasted trip generation rates and modal splits. We believe back-casting to identify what actions (built form, TDM, parking supply, transit service, pricing) are needed to reach a desired future scenario is more likely to achieve transportation goals.
- v. The growth of automotive mode share should be considered constrained by existing and anticipated conditions on the network including active-use programs on QED.
- vi. The TDM report assumes 8,225 person trips as the cap on automotive mode share based on an existing on-street parking supply of 2,175 spaces and on-site of 600 spaces. This appears to presume on-street spaces are available for Lansdowne users despite numerous competing demands for on-street spaces.
- vii. Providing capacity to Lansdowne needs to be addressed through high-capacity transportation modes such as shuttles and transit; reliance on the private vehicle will not address the capacity needed.
- e. Identifying alternative off-site parking locations is a good approach to intercepting and diverting traffic from Bank. However, consideration should be given to providing shuttle service for locations located further away (i.e. 30-40 minute walk from Lansdowne). For some event goers, the walk may be longer than their drive to the off-site parking location. Park & ride locations that see low usage on evening and weekends present such an opportunity.
- f. The inclusion of the concept of a "Fare Free" zone on Bank Street such as is employed in downtown Calgary can support local businesses, including Lansdowne, and reduce the reliance on auto travel while supportive the evolution of Bank Street into a 24/7 transit priority corridor. This is a positive idea that merits serious consideration.

- g. To incentivize the use of transit and support a lasting change in commuting behaviour, consideration should be given to providing a preloaded PRESTO card with a 6-month or 1 year transit pass to new residents. A similar type of incentive should be developed for businesses and offered to their employees.
- h. In addition to the continuance of bicycle workshops (recommended in the report for the spring), it is recommended that a second workshop be introduced in the fall to provide information on winter cycling. Currently, the multi-use pathways along QED and Colonel By Drive, as well as the cycling facilities on O'Connor St. and Fifth Ave. (QED to O'Connor) are winter maintained routes. Lansdowne 2.0 should take advantage of its proximity to these year-round cycling facilities.

Although the City is only beginning discussion on a City-wide, City-led bike share program, could a Lansdowne specific bike share program be implemented that would serve the residents of both the new and existing towers? Potentially this program could be managed by the TMA.

- i. During the planning process for Lansdowne 1.0, City Staff were directed to retain two qualified transit and transportation planning professionals from outside Ottawa to undertake an independent peer review of the Lansdowne Transportation Impact and Assessment Study and TDM Plan. We suggest a similar peer review be required to provide an independent third-party opinion.
- j. The Lansdowne 2.0 proposal includes 739 additional parking spaces for 1,200 new dwelling units, while the zoning by-law requires a minimum rate of 0.5 spaces per dwelling unit. There is no rationale provided for why parking in excess of the minimum is proposed to be provide. Indeed there is no analysis of why a lower rate than the minimum was not considered. Each parking space constructed is a sunk cost into vehicular use that will be paid for by the future residents and users of the site, and by residents surrounding the site through additional traffic generation.
- k. The <u>Capital Pathways Strategic Plan</u> is the NCC's principal guiding document for the Capital Pathway network. Based on the thresholds set by the Plan, the Rideau Canal West pathway adjacent to QED exceeds its peak capacity and does not provide the level of high-quality comfortable experience intended for users, nor does the existing pathway width support

ongoing growth of active transportation users. More room for active transportation users is required, especially given ongoing intensification in the inner urban area such as that proposed by Lansdowne 2.0.

4. Civil

a. We understand the existing stormwater management system for Lansdowne includes subsurface storage, surface storage, conveyance sewers, quality control structures and outlet controls. Lansdowne's stormwater management (SWM) discharges to the O'Connor Street combined sewer, and the Rideau Canal sewer functions as a relief sewer, but only once the underground storage system is full and major storm drainage flows enter the Great Lawn (i.e. for events greater than the 5-year event).

SWM runoff to the Rideau Canal is a pressing concern – it not only carries nutrients and sediment that can impact the aquatic ecosystem, but also salt that impacts the ability of the Canal to freeze and be used for skating. Ongoing NCC research in collaboration with Carleton University also identifies warm winter meltwater as exacerbating challenges of establishing and maintaining the Canal's frozen surface for winter skating. It is important that any development brings net improvements to the SWM approach and further avoids directing runoff to the Rideau Canal.

It appears that the proposed Major Event Centre will impact the existing Great Lawn, Berm, and associated SWM storage area. The proposed Major Event Centre is also located on top of the existing Rideau Canal SWM outlet pipe.

We request the City through future detailed design ensure no increase in runoff volume to the Rideau Canal, and evaluate opportunities to reduce or eliminate existing runoff.

Appendix A: Lessons Learned Report Response

In May 2023 the NCC was invited to submit comments on 'Lessons Learned' from experiences of transportation effects of Lansdowne 1.0 (2014-2020). The Lessons Learned document prepared by OSEG (June 2023) contains input from members of the community, the NCC, City Traffic Services, and the Glebe BIA. In preparing the Lessons Learned document, OSEG on behalf of the City, elected to only provide responses to the comments of the NCC. The below comments are further responses.

1. NCC Comment (May 2023): The location of the principal parking garage access at the east end of the site adjacent to the QED forces an unfortunate choice between the impacts to the QED and the vehicular ingress across the quasi- pedestrianized core of Lansdowne.

OSEG Response: Based on parking garage data, as well as updated turning movement count data. The QED access functions as an important secondary access point to the site, as intended, and accommodates approximately 35% of vehicular access to Lansdowne. The Bank Street garage ramp functions as the primary access point during regular non-event days. It is noted that the QED access plays a vital role in balancing transportation demands and access arrangements, including during major events when vehicular access from Bank Street is restricted to safely accommodate pedestrian and transit passenger demands from the 450- series shuttle service.

NCC Response (July 2023): Vehicular ingress across the quasi-pedestrianized core of Lansdowne is an acknowledged challenge. Despite being designed as a 'shared street', post-development Princess Patricia Way internal to Lansdowne was restricted to pedestrians only, and vehicle traffic was routed through the site via Marché Way. The May 2022 'Lansdowne Partnership Sustainability Plan and Implementation Report' contains extensive discussion of the challenges of the design of Aberdeen Square and the internal streets of Lansdowne, and recommends investment to 'improve on-site safety for all users and reduce conflict between transportation modes.' The location of the parking garage access at the east end of the site adjacent to the QED forces an unfortunate choice between the impacts to the QED and the vehicular ingress across the quasi- pedestrianized core of Lansdowne.

- 2. NCC Comment (May 2023): Assumptions of unfettered access to the federal parkways from major transportation demand generators, such as was the case for Lansdowne 1.0, led to under-planning for other modes of travel and dissatisfaction when access is not available.
 - a) NCC staff flagged this issue in 2011. Quote May 2011 NCC staff comments to the City regarding the then-draft *Transit Service and Shuttle Services and Off-Site Parking Plan Technical Report,* which discussed whether to focus shuttles on QED or Bank, and which heavily favored QED: "[The report] must be written in neutral language without prejudice, and cannot be seen to be 'prejudging'

outcomes in advance of the findings and conclusions of the pilot project. The outcomes cannot be predicted, and it is unfair to present opinions on one option as the sure success, and the other as a failure. As was mentioned, the City and OSEG have to make the Bank Street shuttle route work, as the QED will not be available for shuttles for all Lansdowne events. So why not make the best effort, devise the best plan, put the best foot forward for the Bank Street option?" [emphasis added].

OSEG Response: One of the key achievements of the TDM program since its implementation in 2014 is the gradual reduction of Park & Shuttle buses operating on QED during major events. As of 2022, the number of Park & Shuttle buses operating on QED has been reduced to an average of 30 - 60 inbound bus trips per major event. This is significantly lower than the original number of bus trips estimated in the 2011 TDM Plan, which is upwards of 100 buses per hour on QED (upwards of +200 bus trips for inbound service). Currently, the majority of Park & Shuttle customers are utilizing the 450-series shuttles with service provided on Bank Street.

This achievement is consistent with the ideal long-term objective outlined in the **City of Ottawa – NCC Letter of Intent for Special Event Shuttle Service Pilot Project**, which envisioned a reduction in the number of shuttle buses operating on QED over time.

It is noted that under a future scenario where no shuttle services are operating on QED, the parkway continues to play a crucial role in supporting a balanced, safe and efficient access program to Lansdowne, particularly during major events.

During major events, vehicular access to Lansdowne is temporarily restricted on Bank Street to safely accommodate the large number of transit passengers, pedestrians and cyclists accessing Lansdowne from Bank Street. During these temporary closures, vehicular access to the underground garage and TNC drop- offs (i.e. Uber and Lyft) is accommodated at the QED access. Under a full QED closure scenario during major events, the expected traffic impacts would be extremely severe and the viability of running events safely with minimal impact to the community would be severely compromised.

NCC Response (July 2023): The reduction in shuttles on QED is an accomplishment in line with the Letter of Intent for the Pilot Project. This does not diminish that the NCC has been consistent in the feedback (as quoted above) that 'the QED will not be available for shuttles for all Lansdowne events' and that development of the site cannot rely on the assumption of unfettered vehicular access.

The NCC provided feedback during the preparation of the TIA, requesting that it model certain scenarios to understand the transportation impacts of different forms of QED access amidst different levels of intensity of Lansdowne programming. No such modeling took place, leaving the analysis of the true impacts of the Lansdowne 2.0 proposal under-informed. The NCC similarly provided detailed comments on the TIA's analysis of MMLOS, transit capacity, and exemptions, among other elements, but received no response.

The NCC has not determined to close QED during major events but rather has continued to collaborate with the City and OSEG to ensure major events function well. However, we note our 2011 comment that "[The report] must be written in neutral language without prejudice" and that comments such as "the expected traffic impacts would be extremely severe" without the benefit of the requested analysis of such a scenario are premature.

b) NCC Comment (May 2023): The NCC reiterated that it "will continue (and retains full rights) to close the parkways at its own discretion for its own requirements and third party events" in a June 2015 letter to OSEG and the City of Ottawa.

OSEG Response: It is acknowledged that QED is a federal parkway under the jurisdiction of the NCC. It is recognized that the NCC closes QED to vehicular traffic for the staging of Capital events, which historically averages between 15 to 20 days annually. These closures, which occur from time to time as we understand, are successfully coordinated in a collaborative fashion between the NCC, City of Ottawa and OSEG for events such as Winterlude and the Ottawa Race Weekend. OSEG has indicated, for example, that closures that occur in the morning of events, where QED is returned to full operations two hours before events, generally work well.

NCC Response (July 2023): Major Events (i.e. Ottawa RedBlacks games at the stadium) only constitute 10 to 12 events per year. We continue to coordinate with the City and OSEG to facilitate their successful operation. To suggest that QED should be available to vehicles over the course of the year due to events that occur 10 to 12 times would drastically prioritize vehicular access for a limited number of peak demand events.

c) NCC Comment (May 2023): This mirrors our earlier comment that Lansdowne 2.0's studies cannot rely on the assumption that QED will be available upon demand.

OSEG Response: It is acknowledged that QED is a federal parkway under the jurisdiction of the NCC Irrespective of Lansdowne 2.0, QED is an integral part of the city's transportation network and plays a crucial role in supporting a balanced, safe and efficient access program to Lansdowne, particularly during major events. As previously stated, our assumption is that the QED will, generally, remain as a viable secondary vehicular access point to Lansdowne. If the assumptions is not valid, then the integrity of the Lansdowne 2.0 program (and likely current Lansdowne operations) would be severely compromised from a transportation perspective.

NCC Response (July 2023): As previously stated, the NCC provided feedback during the preparation of the TIA, requesting that it model certain scenarios to understand the transportation impacts of different forms of QED access amidst different levels of intensity of Lansdowne programming. No such modeling took place. The assumption

of ongoing QED access was refuted by the NCC in 2011 and consistently since then. Such access is not a binary question of no restrictions or complete closures – there are forms of QED access for different modes, and levels of intensity of programming at Lansdowne. To state that 'the integrity of the Lansdowne 2.0 program (and likely current Lansdowne operations) would be severely compromised from a transportation perspective' is over-broad and lacks nuance or qualification.

- 3. NCC Comment (May 2023): Transportation Demand Management has not been consistently supported.
 - a) As the Office of the Auditor General: Audit of the Management of the Lansdowne Contract report noted that while OSEG employed a TDM coordinator from 2014 to 2017, despite being required to do so by the site plan agreement "*effective January 1, 2017, OSEG no longer has a dedicated TDM Coordinator, thereby increasing the risk that the effectiveness of the TDM program may be negatively impacted.*"
 - b) The 12 November 2020 Lansdowne Annual Report to Finance and Economic Development Committee noted that OSEG did not have a dedicated TDM Coordinator.
 - c) The 2021-2022 Lansdowne Annual Report makes no mention of whether this gap has been filled.

OSEG Response: Administering the TDM program on-site remains a key component to the success of the TDM program at Lansdowne through the planning and delivery of the various event services and supplementary programming, and support for workplaces and residents at Lansdowne. Currently, the coordination of the TDM program at Lansdowne is administered through a full team that is comprised of individuals within OSEG. This includes the VP, Guest Relations and Operation, and the Director of Safety, Security and Guest Services, who oversee the TDM program and are responsible for the annual TDM reports, in addition to various OSEG staff within Guest Relations and Marketing.

NCC Response (July 2023): The 2011 Transportation Demand Management Plan identified the role of a dedicated, on-site TDM Coordinator as key to achieving target modal shares, particularly related to special events. While mode share targets have been met for many events, new TDM initiatives have lagged with the lack of a dedicated TDM coordinator whose responsibilities are not divided with other matters; car sharing is no longer provided, and recommendations related to carpool preferential parking spaces were not implemented. If Lansdowne is to intensify in its residential development and frequency of events, further efforts of TDM will be required.

4. NCC Comment (May 2023): In the first months and years following the opening of

Lansdowne's first revitalization, transit was heavily and proactively emphasized as the best way to reach Lansdowne, in marketing material and in direct communications to sports fans. It is our observation that there has been a decline in such promotion in recent years.

OSEG Response: The inclusion of free transit for all ticketed events at Lansdowne continues to be provided on the TD Place website, as well as through e-mail communications with all event ticketholders. Information is also shared on social media periodically. By example, the inclusion of free transit and enhanced park and shuttle service information is shared on "Know Before You Go" videos that are broadcasted at the start of each season.

5. NCC Comment (May 2023): Lack of clarity on the threshold for enhanced, free, and discounted transit service outside of major event days at the stadium has led to Lansdowne not achieving as high a transit modal share as would be the case if it were commonly known that attending any event at Lansdowne entitled an attendee to ride transit for free.

OSEG Response: One of the hallmarks of the TDM program for events at Lansdowne is the inclusion of free transit for all ticketed events at Lansdowne with all costs for enhanced public transportation and shuttles paid for by OSEG. This is provided for all events, irrespective of the size of the event. Promotion of free transit service is shared on the TD Place website and shared on social media and promotional materials. The current messaging on the TD Place website for events and concerts states:

- a) The April 2022 "Lansdowne Partnership Sustainability Plan and Implementation Report" dismissed any consideration of free transit to Lansdowne, writing "Before an assessment of free transit can be undertaken, an identified funding mechanism is needed."
- b) The report stated that" The concept of free transit, and its implications, was considered by Transportation Committee as a Motion ACS2021-OCC-TRC-0032 on December 1, 2021." The December 2021 response to the motion was regarding free transit being studied through the TMP, not regarding Lansdowne and its redevelopment.
- c) The entire premise of Lansdowne 2.0 is funding a major civic project (the replacement of the north stands and the new Event Centre) through the sale of air rights, property tax uplift, and ticket surcharge revenues. The Lansdowne 2.0 analysis should identify the range of costs of providing discount or free transit and the funding mechanisms available to provide this (e.g. further sale of air rights, property tax uplift, and ticket surcharge revenues).

OSEG Response: As stated earlier, ticketholders to all events at Lansdowne currently have access to free transit and shuttle service for events. The incremental costs of enhancing transit service and providing free transit is paid for by OSEG.

NCC Response (July 2023): Ticketholders are not provided with free transit, they purchase their transit ride with their ticket cost. The 2012 Site Plan Agreement requires OSEG to include "the cost of enhanced transportation services such as transit, off-site parking and shuttle services and the cost to provide secure temporary on-site bicycle parking corrals **in the ticket price**" [emphasis added].

Despite the continued comment that ticketholders to all events have access to transit, the transit modal share target for Lansdowne 2.0 for minor events (less than 10,000 attendees) is only 10%. This modal share target is low and it appears additional efforts are required to increase transit ridership to minor events and reduce reliance on the private auto (target modal share is 75%).

The analysis of the TIA shows the existing TLOS along Bank at Lansdowne at F. Requiring ticketholders to purchase a transit fare with their ticket may assist with events, but everyday conditions outside of major event days demonstrate the need for improved transit at all times.

6. **NCC Comment (May 2023):** The event size increments for TDM measures is large, which may suggest that implementing more discrete TDM measures commensurate with the size of a wider variety of events should be analyzed

OSEG Response: The TDM program in place at Lansdowne has been a successful in meetings its goals. Much experience has been gained by City of Ottawa Traffic Services, OC Transpo, and OSEG on a complex program that changes due to factors such as day of the week, time of day, and time of year.

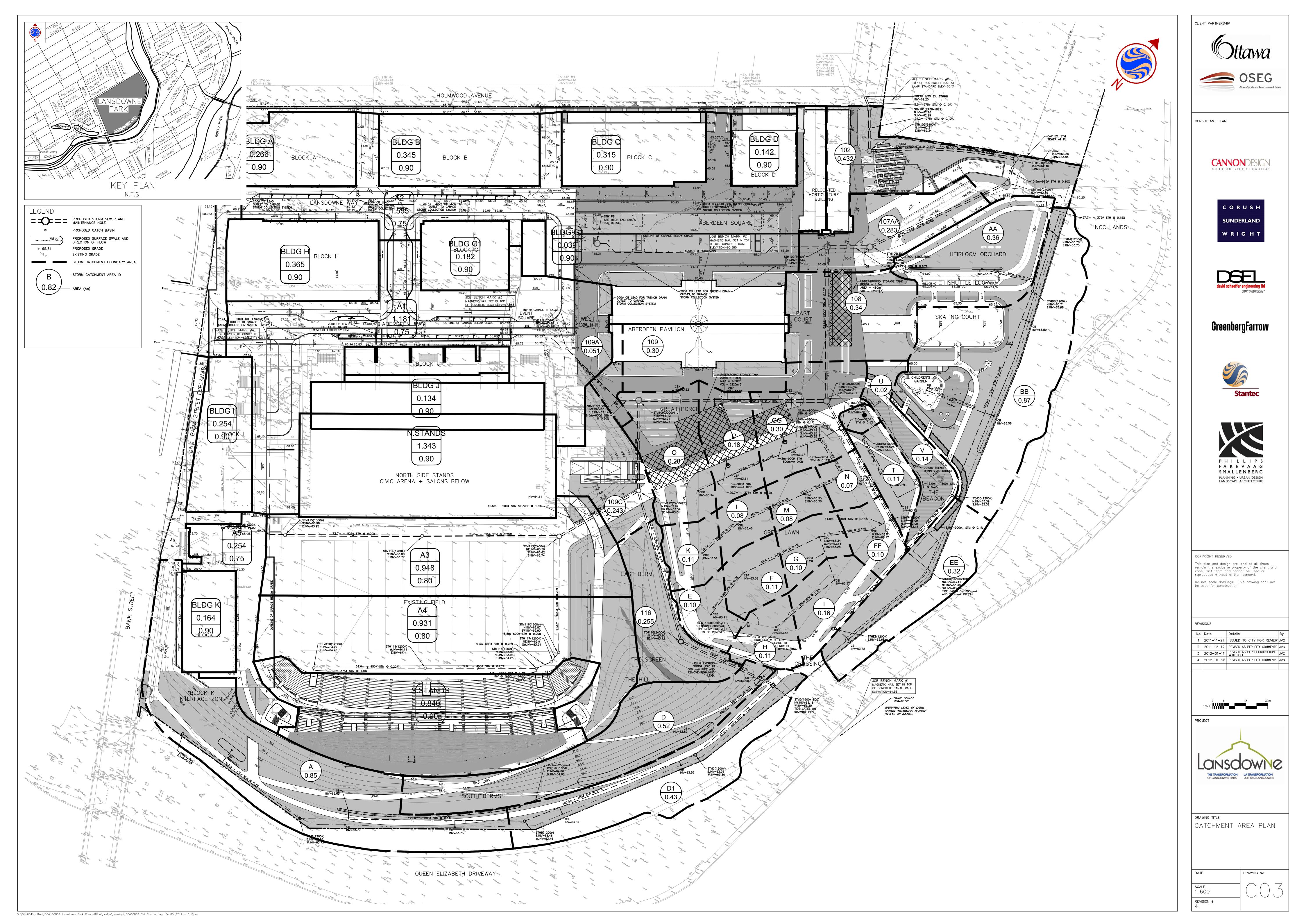
The management of these factors within the revised attendance levels: less than 5,000, 5,000 to 15,000, 15,000 to 25,000, 25,000 to 40,000, and over 40,000 have proven to be effective. Also, as stated previously, the size of average events at TD Place has proven smaller than initially anticipated. OSEG expects 78% of events held this year to be below 5,000.

NCC Response (July 2023): It is good to see the TDM Report identify updated thresholds of minor and major events, and the growth of public and non-ticketed events that may occur concurrently with other events.

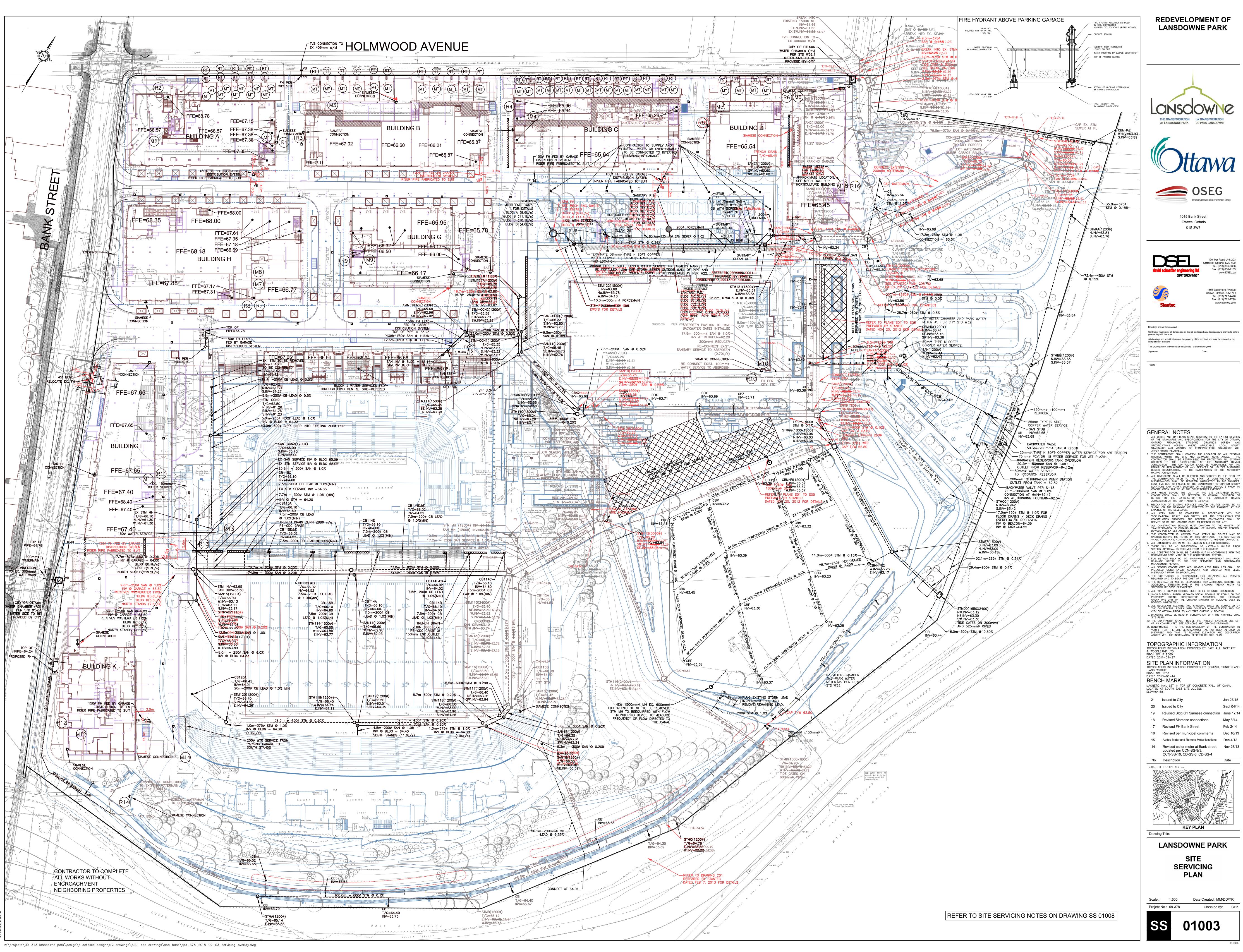
APPENDIX











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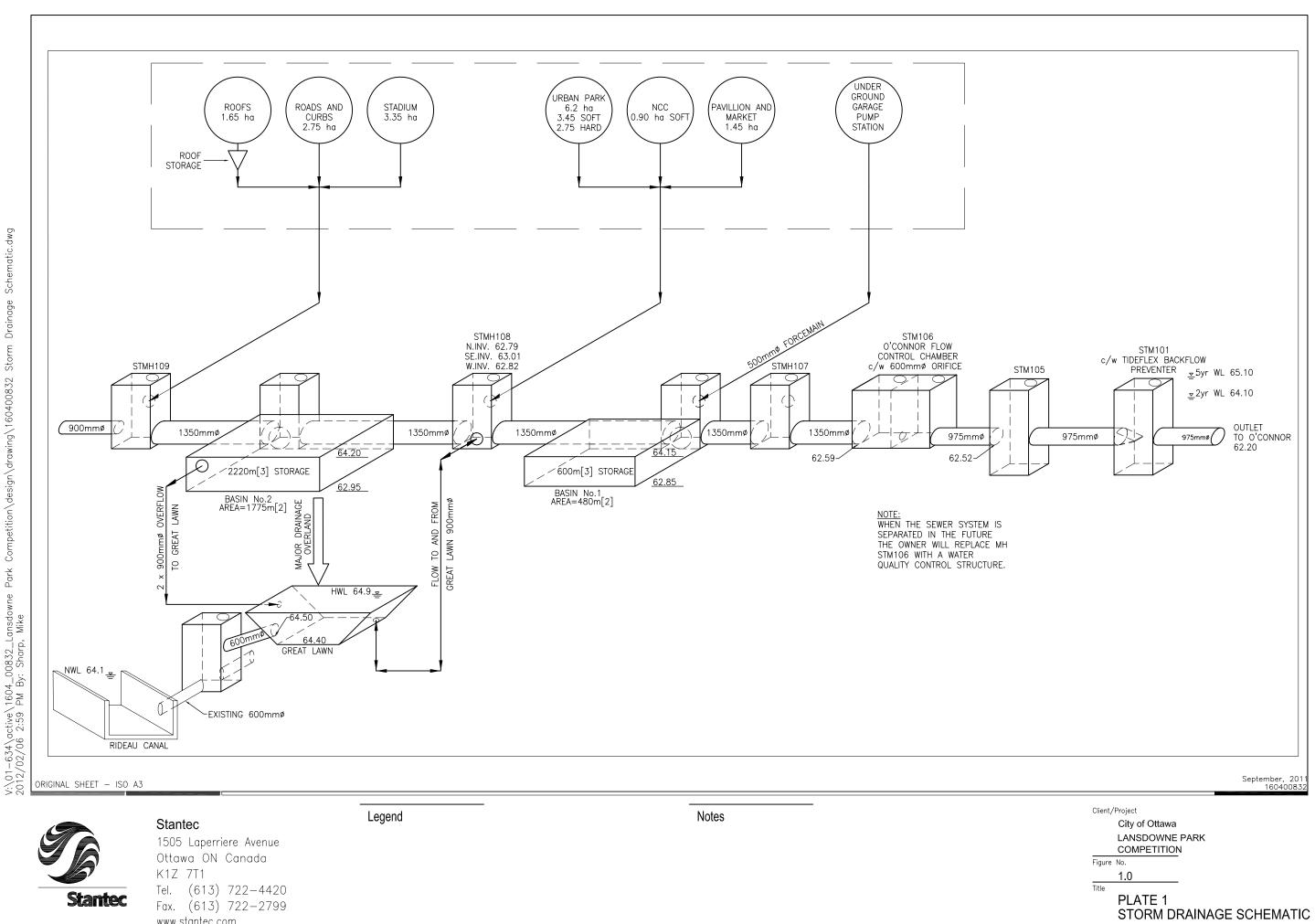
Storm Sewer Calculation Sheet Lansdowne Park Re-Development

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120	110 9	6. Stands	106.0	106.0			0.00	0.00	20.0	70.3	0.0	106.0	450	0.20	59.6	0.159	0.113	0.80	127.5	1.2	0.83
120	119 3	5. Stanus	106.0	106.0			0.00	0.00	20.0		0.0	106.0	450		59.6 59.6	0.159	0.113		127.5		0.83
118		S. Stands	106.0	212.0			0.00	0.00	22.5		0.0	212.0	600	0.20	8.7	0.283	0.150		274.6		0.00
117	116			212.0			0.00	0.00	22.6		0.0	212.0	600	0.20	3.8	0.283	0.150		274.6		0.77
116	113			212.0			0.00	0.00	22.7 23.8		0.0	212.0	600	0.20	62.4	0.283	0.150	0.97	274.6	1.1	0.77
115	114 .	K, N.STANDS	232.6	232.6 A3, A4, A5	2.133	0.80	1.71	1.71	20.0	70.3	333.0	565.6	825	0.20	73.7	0.535	0.206	1.20	641.9	1.0	0.88
114	113	,		232.6			0.00	1.71	21.0 22.0	68.1	322.7	555.4	825	0.20	73.0	0.535	0.206				
113	112			444.6			0.00	1.71	23.8		298.4	743.0	1050	0.10	47.8	0.866	0.263	1.00	863.5	0.8	0.86
113	112			444.0			0.00	1.71	23.8		298.4	743.0	1050	0.10	47.8	0.866	0.263	1.00	863.5	0.8	0.86
A	В			0.0	0.870	0.35		0.30	15.0		70.7	70.7	600	0.10	100.0	0.283	0.150		194.2		0.36
В	С			0.0	0.430	0.35		0.46	17.4		96.6	96.6	600	0.10	100.0	0.283	0.150				0.50
C D	D D1			0.0	0.520	0.35	0.00	0.46	19.9 21.2		89.2 119.7	89.2 119.7	600 900	0.10 0.10	57.0 55.8	0.283	0.150		194.2 572.5		0.46 0.21
D1	112			0.0	0.320	0.35		0.64	21.2		137.8	137.8	900	0.10	55.8 85.0	0.636	0.225		572.5		0.21
				0.0	0.010	0.00	0.12	0.70	23.8		107.0	10710		0.10	00.0	0.000	0.220	0.00	072.0		
112	109			444.6			0.00	2.46	24.6	61.6	421.4	866.0	1200	0.10	46.8	1.131	0.300	1.09	1232.9	0.7	0.70
									25.3												
111	110 н,	, G1, G2, J	23.1	23.1 A1	1.181	0.75	0.89	0.89	20.0	70.3	172.8	196.0	600	0.20	39.6	0.283	0.150	0.97	274.6	0.7	0.71
110	109			23.1			0.00	0.89	20.7 20.8		169.3	192.4	600	0.20	8.5	0.283	0.150	0.97	274.6	0.1	0.70
									20.8												
109	108			467.8			0.00	3.35	25.3 26.7		562.3	1030.0	1350	0.10	99.8	1.431	0.338	1.18	1687.8	1.4	0.61
				0.0	0.400	0.00	0.00	0.00			50.0	50.0	075	0.15	114.0	0.110	0.004	0.01	07.0	0.1	0.00
CB1A AA	AA BB			0.0	0.430	0.60		0.26	15.0 18.1	83.6 74.7	59.9 79.7	59.9 79.7	375 450		114.0 35.0	0.110 0.159	0.094		67.9 98.8		0.88 0.81
BB	CC			0.0	0.870	0.35		0.69	19.0		138.6	138.6	525	0.12	120.0	0.135	0.131		210.7		0.66
CC	DD			0.0			0.00	0.69	21.1 21.7	68.0	130.0	130.0	525	0.24	38.0	0.216	0.131		210.7		0.62
EE	DD			0.0	0.220	0.25	0.11	0.11			26.0	26.0	300	0.40	59.0	0.071	0.075	0.97	61.0		
				0.0	0.320	0.35	0.11	0.11	15.0 16.1		26.0	20.0	300	0.40	59.0	0.071	0.075	0.87	61.2	1.1	0.43
DD	FF			0.0			0.00	0.80	21.7	66.7	148.2	148.2	900	0.10	31.0	0.636	0.225	0.90	572.5	0.6	0.26
									22.3												
Н	G			0.0	0.270	0.35		0.09	15.0		21.9	21.9	300		66.0	0.071	0.075		43.2		
G	J	-		0.0	0.310	0.35		0.20	16.8	78.2	44.1	44.1	375		30.0	0.110	0.094		67.9		0.65
J	FF			0.0	0.100	0.35	0.04	0.24	17.6 17.8		50.2	50.2	600	0.15	12.0	0.283	0.150	0.84	237.8	0.2	0.21
FF	GG			0.0			0.00	1.04	22.3	65.6	189.1	189.1	900	0.10	57.0	0.636	0.225	0.90	572.5	1.1	0.33
									23.4												
K	М			0.0	0.270	0.35		0.09	15.0		21.9	21.9	300		65.0		0.075		43.2		0.51
М	R			0.0	0.070	0.35	0.02	0.12	16.8 18.1		25.9	25.9	300	0.20	47.0	0.071	0.075	0.61	43.2	1.3	0.60

Storm Sewer Calculation Sheet Lansdowne Park Re-Development

															Ś	Sewer Data	1			
Up	Down BLDG ID		Q _{BLDG TOT} AREA ID	Area	С	Indiv AxC	Acc AxC	Tc	I	Q	Q _{TOT}	DIA	Slope	Length	A _{hydraulic}	R	Velocity	Qcap	Time Flow	Q / Q full
		(L/s)	(L/s)	(ha)	(-)			(min)	(mm/hr)	(L/s)	(L/s)	(mm)	(%)	(m)	(m ²)	(m)	(m/s)	(L/s)	(min)	(-)
0	Р		0.0	0.280	0.60	0.17	0.17	15.0	83.6	39.0	39.0	375	0.12	21.0	0.110	0.094	0.55	60.7	0.6	0.64
Р	Q		0.0	0.180	0.60	0.11	0.28	15.6	81.6	62.5	62.5	375	0.10	34.0	0.110	0.094	0.50	55.4	1.1	1.13
Q	R		0.0	0.300	0.60	0.18	0.46	16.8	78.3	99.1	99.1	375	0.12	18.0	0.110	0.094	0.55	60.7	0.5	1.63
R	GG		0.0			0.00	0.58	17.3	76.8	122.6	122.6	600	0.10	13.0	0.283	0.150	0.69	194.2	0.3	0.63
								17.6												
S	U		0.0	0.130	0.60	0.08	0.08	15.0	00.6	18.1	18.1	450	0.20	20.0	0 150	0 1 1 2	0.80	127.5	0.6	0.14
U	GG		0.0	0.130	0.60			15.0 15.6	83.6 81.6	36.7	36.7	450 525	0.20	30.0 17.0	0.159 0.216	0.113				0.14
0	GG		0.0	0.140	0.60	0.08	0.16	15.6	01.0	30.7	30.7	525	0.10	17.0	0.216	0.131	0.63	136.0	0.5	0.27
								10.1												
GG	108		0.0			0.00	1.78	17.6	75.9	374.5	374.5	900	0.10	22.0	0.636	0.225	0.90	572.5	0.4	0.65
								18.0												
108	107		0.0	0.340	0.60	0.20		26.7	58.3	863.2	863.2	1350	0.10	81.4	1.431	0.338	1.18	1687.8		0.51
107	106 A, B, C, D	34.4	502.2 A2	1.555	0.75	1.17	6.49	27.8	56.7	1023.0	1525.1	1350	0.10	20.7	1.431	0.338	1.18	1687.8	0.3	0.90
								28.1												
CONTROLL	ED ELOW																			
106	105	616.0	616.0			0.00	0.00	27.8	56.7	0.0	616.0	975	0.10	80.2	0.747	0.244	0.95	708.7	1.4	0.87
105	104	010.0	616.0			0.00		29.2	54.9	0.0	616.0	975	0.10	12.1	0.747	0.244	0.95	708.7	0.2	0.87
104	103		616.0			0.00		29.5	54.6	0.0	616.0	975	0.10	19.2	0.747	0.244	0.95	708.7	0.3	0.87
103	102		616.0			0.00		29.8	54.2	0.0	616.0	975	0.10	54.2	0.747	0.244	0.95	708.7	1.0	0.87
102	101		616.0			0.00		30.7	53.0	0.0	616.0	975	0.10	24.2	0.747	0.244	0.95	708.7	0.4	0.87
101	EX		616.0			0.00	0.00	31.2	52.5	0.0	616.0	975	0.10	5.8	0.747	0.244	0.95	708.7	0.1	0.87
								31.3												







Schematic.dwg

Drainage

Storm

Competition\design\drawing\160400832

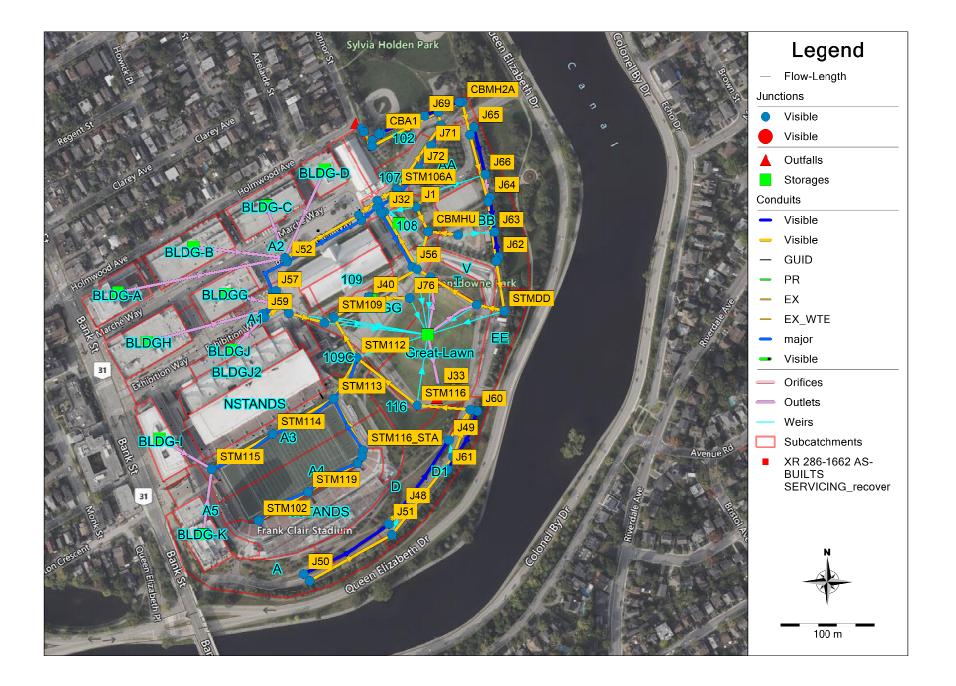
Park

www.stantec.com



PCSWMM Catchment Parameters	– Existing Conditions
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	Area		<u> </u>		
Name	(ha)	Width (m)	Flow Length (m)	Slope (%)	Imperv. (%)
102	0.444	44.4	100.14	0.5	64.2
107AA	0.270	176.7	15.28	0.5	86.3
108	0.344	162.7	21.16	0.5	68.5
109	0.288	88.9	32.42	0.5	87.5
109C	0.254	52.3	48.58	0.5	66.5
116	0.212	66.8	31.67	10	13.9
А	0.733	37.9	193.25	0.5	43.3
A1	1.028	236.0	43.57	0.5	98.5
A2	1.578	358.2	44.06	0.5	97.9
A3	0.931	263.1	35.38	0.5	90.3
A4	0.832	227.3	36.59	2	84.6
A5	0.246	30.9	79.59	0.5	99.9
AA	0.370	72.8	50.84	0.5	54.4
BB	0.891	50.5	176.24	0.5	41.1
BLDG-A	0.254	254.2	10.00	0.5	100.0
BLDG-B	0.363	362.6	10.00	0.5	100.0
BLDG-C	0.299	299.3	10.00	0.5	100.0
BLDG-D	0.138	138.0	10.00	0.5	100.0
BLDGG	0.243	242.9	10.00	0.5	100.0
BLDGH	0.371	370.9	10.00	0.5	100.0
BLDG-I	0.226	225.6	10.00	0.5	100.0
BLDGJ	0.137	137.1	10.00	0.5	100.0
BLDGJ2	0.389	388.5	10.00	0.5	100.0
BLDG-K	0.247	247.3	10.00	0.5	100.0
D	0.584	56.5	103.36	0.5	30.0
D1	0.479	271.3	17.65	0.5	32.5
EE	0.347	38.6	89.83	0.5	15.3
Great-					
Lawn	1.013	164.4	61.62	0.5	26.5
NSTANDS	0.756	97.2	77.76	2	100.0
OPGG	0.813	147.5	55.14	0.5	59.6
SSTANDS	0.799	165.3	48.34	10	100.0
Т	0.131	75.9	17.24	0.5	27.8
V	0.158	167.8	9.40	0.5	96.6



	ATED MAN	CEMENI	MODEL -	VPDC	ION 5	1 (5	nild 5	1 01	15)		
03:	negative	e offse	et ignored	for	Link	C18_	1				
03:	negative	e offse	et ignored	for	Link	C18_	2				
03:	negative	e offse	et ignored	for	Link	C27	2				
03:	negative	e offse	et ignored	for	Link	C42					
03:	negative	e offse	et ignored	for	Link	C43					
03:	negative	e offse	et ignored	for	Link	C44					
04:	minimum	elevat	ion drop	used	for (Condu	it C46				
04:	minimum	elevat	ion drop	used	for (Condu	it C64				
03:	negative	e offse	et ignored	for	Link	C27	1				
							-				
							invort	for	rogulator	Tink	ыл
								TOT	regulator	LIIK	Wa
							10				
02:	maximum	depth	increased	for	Node	STMI	05				
02:	maximum	depth	increased	for	Node	STMI	06A				
02:	maximum	depth	increased	for	Node	STMI	06B				
02:	maximum	depth	increased	for	Node	STMI	07				
02:	maximum	depth	increased	for	Node	STMI	.08				
02:	maximum	depth	increased	for	Node	STMI	0.9				
02:	maximum	depth	increased	for	Node	STMI	10				
02:	maximum	depth	increased	for	Node	STMI	11				
02:			increased								
	mawimum	depth	increased								
			increased	for	Node	STME	3B				
02:	maximum	depth	increased increased								
02:02:	maximum maximum	depth depth		for	Node	STMO	2				
02: 02: 02:	maximum maximum maximum	depth depth depth	increased	for for	Node Node	STM0 STM0	e ec				
	03: 03: 03: 03: 03: 03: 03: 03: 02: 02: 02: 02: 02: 02: 02: 02: 02: 02	<pre>03: negativy 03: negativy 04: mininum 03: negativy 04: mininum 02: maxinum 02:</pre>	Ol: negative offss Ol: crest elevatic Ol: crest elevatic Ol: crest elevatic Ol: maximum depth Ol: maximum depth	01: negative offset ignored 03: negative offset ignored 03: negative offset ignored 03: negative offset ignored 03: negative offset ignored 04: minimum elevation drop 04: minimum elevation drop 05: negative offset ignored 05: negative offset ignored 07: crest elevation raised 07: crest elevation raised 08: maximum depth increased 07: ma	03: negative offset ignored for 03: negative offset ignored for 04: minimum elevation drop used 04: minimum elevation drop used 03: negative offset ignored for 03: negative offset ignored for 03: negative offset ignored for 04: minimum elevation raised to d 10: crest elevation for elevation d 10: maximum depth increased for 10: maximum depth increased	03: negative offset ignored for Link 03: negative offset ignored for Link 04: minimum elevation drop used for: 04: minimum elevation drop used for: 05: negative offset ignored for Link 03: negative offset ignored for Link 04: minimum depth increased for Node 02: maximum depth increased for	03: negative offset ignored for Link C1 03: negative offset ignored for Link C2 03: negative offset ignored for Link C2 03: negative offset ignored for Link C2 03: negative offset ignored for Link C4 04: minimum elevation drop used for Cond 04: minimum elevation drop used for Cond 05: negative offset ignored for Link C4 05: negative offset ignored for Link C4 05: negative offset ignored for Link C4 07: negative offset ignored for Lond C4 07: negative offset ignored for Lond C4 07: neximum depth increased for Node C54 07: maximum depth increased for Node C4 07: maximum depth increased for Node J3 07: maximum depth increased for Node J4 07: maximum depth increased for Node S74 07: maximu	03: negative offset ignored for Link Cl1 03: negative offset ignored for Link Cl8_1 03: negative offset ignored for Link Cl8_2 03: negative offset ignored for Link Cd3_2 03: negative offset ignored for Link Cd4 03: negative offset ignored for Link Cd4 04: minimum elevation drop used for Conduit Cd4 04: minimum elevation drop used for Conduit Cd4 03: negative offset ignored for Link Cd7_1 03: negative offset ignored for Link Cd7_1 04: rest elevation raised to downstream invert 10: crest elevation raised to downstream invert 10: maximum depth increased for Node CBA1 12: maximum depth increased for Node J19 12: maximum depth increased for Node J17 12: maximum depth increased for Node J17 12: maximum depth increased for Node J17 12: maximum depth increased for Node STM102 12: maximum depth increased for Node STM102 12: maximum depth increased for Node STM106 12: maximum depth increased for Node STM107 12: maximum depth increased for Node STM108 12: maximum depth increased for Node STM108 12: maximum depth increased for Node STM110 12: maximum depth increased for Node STM114 12: maximum depth increased	03: negative offset ignored for Link Cl1 03: negative offset ignored for Link Cl8_1 03: negative offset ignored for Link Cl8_2 03: negative offset ignored for Link C43 03: negative offset ignored for Link C43 03: negative offset ignored for Link C43 04: minimum elevation drop used for Conduit C46 04: minimum elevation drop used for Conduit C46 03: negative offset ignored for Link C47_1 03: negative offset ignored for Link C42 10: crest elevation raised to downstream invert for 10: crest elevation raised to Mode J1 10: maximum depth increased for Node J1 10: maximum depth increased for Node J1 10: maximum depth increased for Node STM102 10: maximum depth increased for Node STM102 10: maximum depth increased for Node STM105 10: maximum depth increased for Node STM105 10: maximum depth increased for Node STM106 10: maximum depth increased for Node STM106 10: maximum depth increased for Node STM110 10: maximum depth increased for Node STM111 10: maximum depth increased for Node STM111 10: maximum depth increased for Node STM114 10: maximum depth increased for Node STM114 10: maximum depth increased for Node STM114 10: maximum depth increased for Node STM116 10: maximum depth increased for Node STM116 10: maximum depth increased for Node STM118 10: maximum dep	03: negative offset ignored for Link C18_1 03: negative offset ignored for Link C17_2 03: negative offset ignored for Link C47 04: minimum elevation foro used for Conduit C46 05: negative offset ignored for Link C47 06: negative offset ignored for Link C47 07: negative offset ignored for Link C47 08: negative offset ignored for Link C47 09: negative offset ignored for Link C47 09: negative offset ignored for Link C47 10: crest elevation raised to downstream invert for regulator 10: maximum depth increased for Node CBMHU 10: maximum depth increased for Node J19 10: maximum depth increased for Node J19 10: maximum depth increased for Node J37 10: maximum depth increased for Node J37 10: maximum depth increased for Node STM102 10: maximum depth increased for Node STM103 10: maximum depth increased for Node STM105 10: maximum depth increased for Node STM106 10: maximum depth increased for Node STM116 10: maximum depth increased for Node STM116 10: maximum depth increased for Node STM118 10: maximum depth increased for Node STM118 10: maximum depth increased for Node STM116 10: maximum depth increased for Node STM116	03: negative offset ignored for Link Cl1 03: negative offset ignored for Link Cl8_1 03: negative offset ignored for Link Cl8_2 03: negative offset ignored for Link Cd2 03: negative offset ignored for Link Cd2 03: negative offset ignored for Link Cd3 04: minimum elevation drop used for Conduit Cd6 04: minimum elevation drop used for Conduit C64 05: negative offset ignored for Link Cd2 10: negative offset ignored for Link Cd2 10: negative offset ignored for Link Cd2 10: crest elevation raised to downstream invert for regulator Link 10: crest elevation raised to downstream invert for regulator Link 10: crest elevation raised to downstream invert for regulator Link 10: crest elevation raised to downstream invert for regulator Link 10: crest elevation raised to downstream invert for regulator Link 10: crest elevation raised to downstream invert for regulator Link 10: crest elevation raised to downstream invert for regulator Link 10: crest elevation raised for Node CBM12 12: maximum depth increased for Node CBM12 12: maximum depth increased for Node J19 12: maximum depth increased for Node J37 12: maximum depth increased for Node J37 12: maximum depth increased for Node STM102 12: maximum depth increased for Node STM102 12: maximum depth increased for Node STM105 12: maximum depth increased for Node STM105 12: maximum depth increased for Node STM105 12: maximum depth increased for Node STM106 12: maximum depth increased for Node STM107 12: maximum depth increased for Node STM106 12: maximum depth increased for Node STM107 12: maximum depth increased for Node STM108 12: maximum depth increased for Node STM110 12: maximum depth increased for Node STM113 12: maximum depth increased for Node STM114 12: maximum depth increased for Node STM114 12: maximum depth incr

109C	0.25	52.31	66.54	0.5000	100yr_3hr_Chicago
STM112 116	0.21	66.78	13.91	10.0000	100yr_3hr_Chicago
STM116 A	0.73	37.91	43.28	0.5000	100yr_3hr_Chicago
J50 A1	1.03	236.01	98.55	0.5000	100yr_3hr_Chicago
J58 A2	1.58	358.18	97.91	0.5000	100yr_3hr_Chicago
J52 A3	0.93	263.12	90.26	0.5000	100yr_3hr_Chicago
STM114 A4	0.83	227.29	84.59	2.0000	100yr 3hr Chicago
STM119 A5	0.25	30.92	99.94	0.5000	100yr 3hr Chicago
STM115 AA	0.37	72.80	54.39	0.5000	100yr 3hr Chicago
J37					
BB J63	0.89	50.53	41.05		100yr_3hr_Chicago
BLDG-A S-BLDG-A	0.25	254.20	100.00	0.5000	100yr_3hr_Chicago
BLDG-B S-BLDG-B	0.36	362.60	100.00	0.5000	100yr_3hr_Chicago
BLDG-C S-BLDG-C	0.30	299.30	100.00	0.5000	100yr_3hr_Chicago
BLDG-D S-BLDG-D	0.14	138.00	100.00	0.5000	100yr_3hr_Chicago
BLDGG S-BLDG-G	0.24	242.90	100.00	0.5000	100yr_3hr_Chicago
BLDGH S-BLDG-H	0.37	370.90	100.00	0.5000	100yr_3hr_Chicago
BLDG-I	0.23	225.60	100.00	0.5000	100yr_3hr_Chicago
S-BLDG-I BLDGJ	0.14	137.10	100.00	0.5000	100yr_3hr_Chicago
S-BLDG-J BLDGJ2	0.39	388.50	100.00	0.5000	100yr_3hr_Chicago
STM-CCN2 BLDG-K	0.25	247.30	99.99	0.5000	100yr_3hr_Chicago
S-BLDG-K D	0.58	56.48	30.02	0.5000	100yr_3hr_Chicago
J48 D1	0.48	271.32	32.46	0.5000	100yr_3hr_Chicago
J61 EE	0.35	38.57	15.30	0.5000	100yr_3hr_Chicago
STMDD Great-Lawn	1.01	164.38	26.54	0.5000	100yr_3hr_Chicago
STMFF NSTANDS	0.76	97.25	100.00	2.0000	100yr_3hr_Chicago
STM113 OPGG	0.81	147.51	59.59	0.5000	100yr_3hr_Chicago
STMGG SSTANDS	0.80	165.31	99.95	10.0000	100yr_3hr_Chicago
STM119 T	0.13	75.86	27.76	0.5000	100yr_3hr_Chicago
STMGG V	0.16	167.82	96.59	0.5000	100yr_3hr_Chicago
STMFF					

			0.000		
WARNING 02: maximum	donth ingroace				
WARNING 02: maximum WARNING 02: maximum					
WARNING 02: maximum WARNING 02: maximum					
WARNING 02: maximum WARNING 02: maximum					
WARNING UZ: Maximum	depth increase	a tot Not	ie SimGG		

Element Count					
* * * * * * * * * * * *					
Number of rain gage:	s 18				
Number of subcatchm	ents 33				
Number of nodes					
Number of links	134				
Number of pollutant:	s O				
Number of land uses	0				

Raingage Summary					

				Data	Recording
Name	Data Source				Interval
100yr 3hr Chicago				INTENSITY	
100yr 3hr Chicago C					
0 min.					
100yr 6hr Chicago	100yr 6hr Chi	cago		INTENSITY	10 min.
100vr 6hr Chicago C	limate Change l	00vr 6hr	Chicago :	Increase 20	Opercent INTENSI
100yr_6hr_Chicago_C 0 min.	limate_Change 1	00yr_6hr_	Chicago_	Increase_20	Opercent INTENSI
				-	Opercent INTENSII
0 min. 100yr-SCS_12hr_Type 100yr-SCS_24hr_Type	_II 100yr-SCS_1 II 100yr-SCS_2	2hr_Type 4hr Type	II		
0 min. 100yr-SCS_12hr_Type 100yr-SCS_24hr_Type	_II 100yr-SCS_1 II 100yr-SCS_2	2hr_Type 4hr Type	II	INTENSI INTENSI INTENSITY	<pre>FY 6 min. FY 15 min. 10 min.</pre>
0 min. 100yr-SCS_12hr_Type 100yr-SCS_24hr_Type	_II 100yr-SCS_1 II 100yr-SCS_2	2hr_Type 4hr Type	II	INTENSI INTENSI INTENSITY	<pre>FY 6 min. FY 15 min. 10 min.</pre>
0 min. 100yr-SCS_12hr_Type 100yr-SCS_24hr_Type	_II 100yr-SCS_1 II 100yr-SCS_2	2hr_Type 4hr Type	II II	INTENSI INTENSI	<pre>TY 6 min. TY 15 min. 10 min. 10 min.</pre>
0 min. 100yr-SCS_12hr_Type 100yr-SCS_24hr_Type	_II 100yr-SCS_1 II 100yr-SCS_2	2hr_Type 4hr Type	II	INTENSI INTENSI INTENSITY INTENSITY INTENSITY	<pre>FY 6 min. FY 15 min. 10 min. 10 min. 10 min.</pre>
0 min. 100yr-SCS_12hr_Type 100yr-SCS_24hr_Type 10yr_3hr_Chicago 10yr_6hr_Chicago 25mm_3hr_Chicago 25mm dhr Chicago	II 100yr-SCS_1 II 100yr-SCS_2 10yr_3hr_Chic 10yr_6hr_Chic 25mm_3hr_Chic 25mm_4hr_Chic	2hr_Type 4hr_Type ago ago ago ago ago	II II	INTENSI INTENSI INTENSITY INTENSITY INTENSITY INTENSITY	<pre>TY 6 min. TY 15 min. 10 min. 10 min. 10 min. 10 min.</pre>
0 min. 100yr-SCS_12hr_Type 100yr-SCS_24hr_Type 10yr_3hr_Chicago 10yr_6hr_Chicago 25mm_3hr_Chicago 25mm dhr Chicago	II 100yr-SCS_1 II 100yr-SCS_2 10yr_3hr_Chic 10yr_6hr_Chic 25mm_3hr_Chic 25mm_4hr_Chic	2hr_Type 4hr_Type ago ago ago ago ago	II II	INTENSIT INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY	<pre>FY 6 min. FY 15 min. 10 min. 10 min. 10 min. 10 min. 10 min.</pre>
0 min. 100yr-SCS_12hr_Type 100yr-SCS_24hr_Type 10yr_3hr_Chicago 10yr_6hr_Chicago 25mm_3hr_Chicago 25mm dhr Chicago	II 100yr-SCS_1 II 100yr-SCS_2 10yr_3hr_Chic 10yr_6hr_Chic 25mm_3hr_Chic 25mm_4hr_Chic	2hr_Type 4hr_Type ago ago ago ago ago	II	INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY	<pre>FY 6 min. FY 15 min. 10 min. 10 min. 10 min. 10 min. 10 min. 10 min.</pre>
0 min. 100yr-SCS_12hr_Type 100yr-SCS_24hr_Type 10yr_3hr_Chicago 10yr_6hr_Chicago 25mm_3hr_Chicago 25mm dhr Chicago	II 100yr-SCS_1 II 100yr-SCS_2 10yr_3hr_Chic 10yr_6hr_Chic 25mm_3hr_Chic 25mm_4hr_Chic	2hr_Type 4hr_Type ago ago ago ago ago	II	INTENSI INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY	<pre>FY 6 min. FY 15 min. 10 min. 10 min. 10 min. 10 min. 10 min. 10 min.</pre>
<pre>D min. 100yr-SCS_12hr_Type 100yr-SCS_24hr_Type 10yr_3hr_Chicago 25mm_3hr_Chicago 25mm_3hr_Chicago 25yr_3hr_Chicago 2yr_3hr_Chicago 2yr_5hr_Chicago</pre>	II 100yr-SCS 1 II 100yr-SCS 2 10yr_3hr_Chic 10yr_6hr_Chic 25mm_3hr_Chic 25yr_3hr_Chic 25yr_6hr_Chic 2yr_3hr_Chica 2yr_6hr_Chica 2yr_6hr_Chica	2hr_Type 4hr_Type ago ago ago ago ago ago go go	II	INTENSI INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY	<pre>FY 6 min. FY 15 min. 10 min. 10 min. 10 min. 10 min. 10 min. 10 min. 10 min.</pre>
0 min. 100yr-SCS_12hr_Type, 100yr_SCS_24hr_Type, 10yr_3hr_Chicago 25mm_3hr_Chicago 25yr_3hr_Chicago 25yr_3hr_Chicago 2yr_3hr_Chicago 2yr_3hr_Chicago 2yr_3hr_Chicago 2yr_3hr_Chicago 2yr_3hr_Chicago	II 100yr-SCS 1 II 100yr-SCS 2 10yr_3hr_Chic 25mm_3hr_Chic 25mm_3hr_Chic 25yr_3hr_Chic 25yr_3hr_Chic 25yr_6hr_Chic 2yr_3hr_Chic 2yr_6hr_Chica	2hr_Type 4hr_Type ago ago ago ago ago go go go go	II	INTENSI INTENS	<pre>FY 6 min. IV 15 min. 10 min. 10 min. 10 min. 10 min. 10 min. 10 min. 10 min. 10 min. 10 min.</pre>
0 min. 100yr-SCS_12hr_Type, 100yr_SCS_24hr_Type, 10yr_3hr_Chicago 25mm_3hr_Chicago 25yr_3hr_Chicago 25yr_3hr_Chicago 2yr_3hr_Chicago 2yr_3hr_Chicago 2yr_3hr_Chicago 2yr_3hr_Chicago 2yr_3hr_Chicago	II 100yr-SCS 1 II 100yr-SCS 2 10yr_3hr_Chic 25mm_3hr_Chic 25mm_3hr_Chic 25yr_3hr_Chic 25yr_3hr_Chic 25yr_6hr_Chic 2yr_3hr_Chic 2yr_6hr_Chica	2hr_Type 4hr_Type ago ago ago ago ago go go go go	II	INTENSI INTENS	<pre>TY 6 min. TY 15 min. 10 min. 10 min. 10 min. 10 min. 10 min. 10 min. 10 min. 10 min. 10 min.</pre>
<pre>D min</pre>	II 100yr-SCS 1 II 100yr-SCS 2 10yr 3hr Chic 25mm 3hr Chic 25mm 3hr Chic 25yr 3hr Chic 25yr 3hr Chic 25yr 3hr Chic 2yr 6hr Chic 30yr 3hr Chic 50yr 3hr Chic 50yr 6hr Chic 50yr 6hr Chic	2hr_Type 4hr_Type ago ago ago ago ago go go go ago ago go go go	II	INTENSI INTENS	<pre>TY 6 min. 10 min.</pre>
0 min. 100yr-SCS_12hr_Type, 100yr_SCS_24hr_Type, 10yr_Shr_Chicago 25mm_Ahr_Chicago 25yr_3hr_Chicago 25yr_Shr_Chicago 2yr_Shr_Chicago 2yr_Shr_Chicago 2yr_Shr_Chicago 2yr_Shr_Chicago	II 100yr-SCS 1 II 100yr-SCS 2 10yr_3hr_Chic 25mm_3hr_Chic 25mm_3hr_Chic 25yr_3hr_Chic 25yr_3hr_Chic 25yr_6hr_Chic 2yr_3hr_Chic 2yr_6hr_Chica	2hr_Type 4hr_Type ago ago ago ago ago go go go ago ago go go go	II	INTENSI INTENS	<pre>TY 6 min. 10 min.</pre>
0 min. 100yr-SCS_12hr_Type 100yr-SCS_24hr_Type 10yr_Shr_Chicago 10yr_Ghr_Chicago 25mr_Shr_Chicago 25yr_Ghr_Chicago 2yr_Ghr_Chicago 2yr_Ghr_Chicago 50yr_Ghr_Chicago 50yr_Shr_Chicago 50yr_Shr_Chicago 5yr_Shr_Chicago	II 100yr-sCS 1 II 100yr-sCS 2 10yr_shc_chic 25mm_3hr_chic 25yr_shr_chic 25yr_shr_chic 2yr_3hr_chica 2yr_3hr_chica 50yr_3hr_chica 50yr_shr_chica 5yr_shr_chica	2hr_Type 4hr_Type ago ago ago ago ago go go go ago ago go go go	II	INTENSI INTENS	<pre>TY 6 min. 10 min.</pre>
<pre>0 min. 0 min. 100yr-SCS 12hr Type 100yr-SCS 24hr Type 10yr_Ghr_Chicago 25mm_Ghr_Chicago 25mm_Ghr_Chicago 25yr_Ghr_Chicago 2yr_Ghr_Chicago 50yr_Ghr_Chicago 50yr_Ghr_Chicago 5yr_Ghr_Chicago 5yr_Ghr_Chicago</pre>	II 100yr=862 1 II 100yr=862 2 10yr_3hr_Chic 25mm_3hr_Chic 25yr_3hr_Chic 2yr_3hr_Chica 2yr_3hr_Chica 50yr_3hr_Chica 50yr_3hr_Chica 5yr_3hr_Chica	2hr_Type 4hr_Type ago ago ago ago ago go go go ago ago go go go	II	INTENSI INTENS	<pre>TY 6 min. 10 min.</pre>
0 min. 100yr-SCS_12hr_Type 100yr-SCS_24hr_Type 10yr_SCF_Chicago 10yr_chr_Chicago 25mm_Shr_Chicago 25yr_Shr_Chicago 2yr_Ghr_Chicago 2yr_Ghr_Chicago 50yr_Ghr_Chicago 50yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago	II 100yr-868 1 II 100yr-868 2 10yr_3hr_Chic 25mm_3hr_Chic 25mr_3hr_Chic 25yr_6hr_Chic 25yr_6hr_Chic 50yr_6hr_Chic 50yr_3hr_Chice 5yr_6hr_Chice 5yr_6hr_Chice	2hr_Type 4hr_Type ago ago ago ago ago go go go ago ago go go go	II	INTENSI INTENS	<pre>TY 6 min. 10 min.</pre>
<pre>0 min. 100yr-SCS 12hr Type 100yr-SCS 24hr Type 10yr_SCS 24hr Type 10yr_chr_Chicago 25mm_dhr_Chicago 25yr_chr_Chicago 25yr_chr_Chicago 2yr_5hr_Chicago 50yr_chr_Chicago 50yr_shr_Chicago 5yr_shr_Chicago 5yr_shr_Chicago</pre>	II 100yr-868 1 II 100yr-868 2 10yr 3hr Chic 25mm 3hr Chic 25yr 3hr Chic 25yr 3hr Chic 29yr 3hr Chica 50yr 3hr Chica 50yr 3hr Chica 5yr 3hr Chica	2hr_Type 4hr_Type ago ago ago ago ago ago ago go go go go go	II	INTENSIT INTENSIT INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY	<pre>TY 6 min. TY 15 min. 10 min.</pre>
0 min. 100yr-SCS_12hr_Type 100yr-SCS_24hr_Type 10yr_SCS_24hr_Type 10yr_6hr_Chicago 25mm_Shr_Chicago 25yr_Shr_Chicago 2yr_Shr_Chicago 2yr_Shr_Chicago 50yr_Shr_Chicago 50yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago	II 100yr-868 1 II 100yr-868 2 10yr 3hr Chic 25mm 3hr Chic 25yr 3hr Chic 25yr 3hr Chic 29yr 3hr Chica 50yr 3hr Chica 50yr 3hr Chica 5yr 3hr Chica	2hr_Type 4hr_Type ago ago ago ago ago ago ago go go go go go	II	INTENSI INTENS	<pre>TY 6 min. TY 15 min. 10 min.</pre>
<pre>0 min. 100yr-SCS_12hr_Type 100yr-SCS_24hr_Type 10yr_SCS_24hr_Type 10yr_chr_Chicago 25mm_4hr_Chicago 25mm_4hr_Chicago 25yr_6hr_Chicago 2yr_6hr_Chicago 50yr_6hr_Chicago 50yr_6hr_Chicago 5yr_6hr_Chicago 5yr_6hr_Chicago 5yr_6hr_Chicago 5yr_6hr_Chicago</pre>	II 100yr-868 1 II 100yr-868 2 10yr_3hr_Chic 25mr_3hr_Chic 25yr_3hr_Chic 25yr_3hr_Chic 2yr_3hr_Chica 50yr_3hr_Chica 50yr_3hr_Chica 5yr_3hr_Chica y * Y *	2hr_Type 4hr_Type ago ago ago ago ago go go go go go go go	%Imperv	INTENSIT INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY	<pre>TY 6 min. TY 15 min. 10 min. 10 min. 10 min. 10 min. 10 min. 10 min. 10 min. 10 min. 10 min.</pre>
0 min. 100yr-SCS_12hr_Type 100yr-SCS_24hr_Type 10yr_SCS_24hr_Type 10yr_6hr_Chicago 25mm_Shr_Chicago 25yr_Shr_Chicago 25yr_Shr_Chicago 2yr_Shr_Chicago 50yr_Shr_Chicago 50yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago	II 100yr-86S 1 II 100yr-86C 2 10yr_3hr_Chic 10yr_6hr_Chic 25mm_3hr_Chic 25yr_3hr_Chic 25yr_3hr_Chica 50yr_6hr_Chica 5yr_6hr_Chica 5yr_6hr_Chica yr_Shr_Chica yr_Shr_Chica yr_Shr_Chica	2hr_Type 4hr_Type ago ago ago ago ago go go go go go go go	%Imperv	INTENSIT INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY	<pre>TY 6 min. TY 15 min. 10 min. 10 min. 10 min. 10 min. 10 min. 10 min. 10 min. 10 min. 10 min.</pre>
<pre>0 min. 0 min. 100yr-SCS_12hr_Type 100yr-SCS_24hr_Type 10yr_SCF_Chicago 25mm_Ahr_Chicago 25mm_Ahr_Chicago 25yr_Ghr_Chicago 2yr_Ghr_Chicago 50yr_Ghr_Chicago 50yr_Ghr_Chicago 5yr_Ghr_Chicago 5yr_Ghr_Chicago 5yr_Ghr_Chicago yr_Ghr_Chicago yr_Ghr_Chicago yr_Ghr_Chicago yr_Ghr_Chicago</pre>	II 100yr-868 1 II 100yr-868 2 10yr 3hr Chic 25mr 3hr Chic 25yr 3hr Chic 2yr 5hr Chic 2yr 5hr Chic 2yr 3hr Chica 50yr 3hr Chica 5yr 3hr Chica yr 6hr Chica yr 7hr 7hr 7hr 7hr 7hr 7hr 7hr 7hr 7hr 7h	2hr_Type 4hr_Type ago ago ago ago ago go go go go go go	%Imperv	INTENSIT INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY	<pre>TY 6 min. TY 15 min. 10 min.</pre>
0 min. 100yr-SCS_12hr_Type 100yr-SCS_24hr_Type 10yr_SCS_Chicago 10yr_Ghr_Chicago 25mm_Shr_Chicago 25yr_Shr_Chicago 2yr_Ghr_Chicago 2yr_Ghr_Chicago 50yr_Ghr_Chicago 50yr_Ghr_Chicago 50yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 1002	II 100yr-86S 1 II 100yr-86C 2 10yr_3hr_Chic 10yr_6hr_Chic 25mm_3hr_Chic 25yr_3hr_Chic 25yr_3hr_Chica 50yr_6hr_Chica 5yr_6hr_Chica 5yr_6hr_Chica yr_Shr_Chica yr_Shr_Chica yr_Shr_Chica	2hr_Type 4hr_Type ago ago ago ago ago go go go go go go go	%Imperv	INTENSIT INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY	<pre>TY 6 min. TY 15 min. 10 min. 10 min. 10 min. 10 min. 10 min. 10 min. 10 min. 10 min. 10 min.</pre>
0 min. 100yr-SCS_12hr_Type 100yr-SCS_24hr_Type 10yr_SCS_Chicago 10yr_Ghr_Chicago 25mm_Shr_Chicago 25yr_Shr_Chicago 2yr_Ghr_Chicago 2yr_Ghr_Chicago 50yr_Ghr_Chicago 50yr_Ghr_Chicago 50yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago 1002	II 100yr-868 1 II 100yr-868 2 10yr 3hr Chic 25mr 3hr Chic 25yr 3hr Chic 25yr 3hr Chic 2yr 3hr Chica 5yr 3hr Chica 5yr 3hr Chica 5yr 3hr Chica yr 4 x Xrea	2hr_Type 4hr_Type ago ago ago ago ago go go go go Width 	%Imperv 64.22	INTENSIT INTENSIT INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY	<pre>TY 6 min. TY 15 min. 10 min.</pre>
0 min 100yr-SCS_12hr_Type 100yr-SCS_24hr_Type 10yr_SCS_24hr_Type 10yr_6hr_Chicago 25mm_3hr_Chicago 25mm_4hr_Chicago 25yr_3hr_Chicago 2yr_6hr_Chicago 2yr_6hr_Chicago 50yr_6hr_Chicago 50yr_6hr_Chicago 5yr_6hr_Chicago 5yr_6hr_Chicago 5yr_6hr_Chicago 5yr_6hr_Chicago 5yr_6hr_Chicago 5yr_6hr_Chicago 5yr_6hr_Chicago 5yr_6hr_Chicago 5yr_6hr_Chicago 5yr_6hr_Chicago 1000000000000000000000000000000000000	II 100yr-868 1 II 100yr-868 2 10yr_3hr_Chic 25mr_3hr_Chic 25yr_3hr_Chic 25yr_3hr_Chic 2yr_3hr_Chica 5yr_3hr_Chica 5yr_3hr_Chica 5yr_3hr_Chica	2hr_Type 4hr_Type ago ago ago ago go go go go go 44.37 176.73	%Imperv 64.22 86.34	INTENSIT INTENSIT INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY OC.5000 0.5000	<pre>TY 6 min. TY 15 min. 10 min.</pre>
0 min. 100yr-SCS_12hr_Type 100yr-SCS_24hr_Type 10yr_SCS_Chicago 10yr_Ghr_Chicago 25mm_Shr_Chicago 25yr_Ghr_Chicago 2yr_Ghr_Chicago 2yr_Ghr_Chicago 50yr_Ghr_Chicago 50yr_Ghr_Chicago 50yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago yr_Shr_Chicago yr_Shr_Chicago 100 100 100 100 100 100 100 10	II 100yr-868 1 II 100yr-868 2 10yr_3hr_Chic 25mr_3hr_Chic 25yr_3hr_Chic 25yr_3hr_Chic 2yr_3hr_Chica 5yr_3hr_Chica 5yr_3hr_Chica 5yr_3hr_Chica	2hr_Type 4hr_Type ago ago ago ago go go go go go 44.37 176.73	%Imperv 64.22 86.34	INTENSIT INTENSIT INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY OC.5000 0.5000	<pre>TY 6 min. TY 15 min. 10 min.</pre>
0 min 100yr-SCS_12hr_Type 100yr-SCS_24hr_Type 10yr_SCS_24hr_Type 10yr_Chr_Chicago 25mm_4hr_Chicago 25yr_3hr_Chicago 2yr_Shr_Chicago 2yr_Shr_Chicago 50yr_Shr_Chicago 50yr_Shr_Chicago 5yr_Shr_Chicago 5yr_Shr_Chicago yr_Shr_Chicago yr_Shr_Chicago 1000000000000000000000000000000000000	II 100yr-868 1 II 100yr-868 2 10yr 3hr Chic 25mr 3hr Chic 25yr 3hr Chic 2yr 5hr Chic 2yr 3hr Chica 2yr 5hr Chica 5yr 3hr Chica 5yr 3hr Chica y Area	2hr_Type 4hr_Type ago ago ago go go go go go go go go 176.73 162.73	\$Imperv 64.22 86.34 68.53	INTENSIT INTENSIT INTENSIT INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY INTENSITY 0.5000 0.5000	<pre>TY 6 min. TY 15 min. 10 min.</pre>

**********		Invort	Max	Ponded	Extern
Name	Type	Elev.	Depth	Area	Inflow
CBA1	JUNCTION				
CBMH2A	JUNCTION	63.89	2.31	0.0	
CBMHU	JUNCTION	63.36	2.64		
J1	JUNCTION	63.56	2.79	0.0	
J19	JUNCTION	63.62	2.08 3.44 3.00	720.0	
J32	JUNCTION	62.76	3.44	0.0	
J33	JUNCTION	63.09	3.00	0.0	
J37	JUNCTION	63.68	2.42	466.0	
J40	JUNCTION	63.68 62.91 64.69	2.21		
J48	TUNCTION	64.69	3.00		
.749	JUNCTION	64.40	3.00		
J50	JUNCTION	65.08	3.00		
J51	JUNCTION				
J52	JUNCTION	65.35 65.31	3.00		
J53	JUNCTION	65.25	3.00		
J54	JUNCTION				
J55	JUNCTION	65.25 65.20	3.00		
		65.20	3.00		
J56	JUNCTION	64.95 65.30	3.00		
J57	JUNCTION		3.00	0.0	
J58	JUNCTION	65.35	3.00		
J59	JUNCTION	65.58	3.00		
J60	JUNCTION	64.65	3.00		
J61	JUNCTION	64.30 64.70	3.00		
J62	JUNCTION				
J63	JUNCTION	64.50	3.00		
J64	JUNCTION	64.65	3.00		
J65	JUNCTION	65.10	3.00		
J66	JUNCTION	64.50	3.00	0.0	
J67	JUNCTION	65.17	3.00		
J68	JUNCTION	65.00	3.00	0.0	
J69	JUNCTION	65.43	3.00	0.0	
J70	JUNCTION	65.20	3.00	0.0	
J71	JUNCTION	65.70	3.00	0.0	
J72	JUNCTION	65.70 65.30	3.00	0.0	
J73	JUNCTION			0.0	
J74	JUNCTION	64.93 65.01	3.00	0.0	
J75	JUNCTION	65.89	3.00		
J76	JUNCTION	62.95	2.45		
STM101	JUNCTION	62.25	2.88	0.0	
STM101A	TUNCTION	62.29			
STM102	JUNCTION	64.26	3.14		
STM102A	TUNCTION	62.35	3.65		
STM104	JUNCTION	62.49	2.88		
STM104	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	62.53	4.36		
STM106A	JUNCTION	62.64	3.29		
STM106A STM106B	TUNCTION				
STM106B STM107	TUNCTION	62.64 62.72	3.29		
STM107 STM108	JUNCTION	62.00	3.03		
		b∠.00	3.95		
STM109	JUNCTION	62.91	3.32	0.0	
STM110	JUNCTION	63.14	3.10	0.0	
STM111	JUNCTION	63.28	3.17	0.0	

1A 2	JUNCTION JUNCTION	63.76 62.99	2.54 3.13	0.0		0	C15 .2126	0.0130	STM-CCN1	STM111	CONDUIT	
3	JUNCTION JUNCTION	63.59 63.77	3.83 2.78	0.0		0	C16 .2785	0.0130	STM111	STM110	CONDUIT	
5	JUNCTION JUNCTION	63.95 63.14	3.10 2.73	0.0		0	C17 0.1770	0.0130	STM110	STM109	CONDUIT	
6_STA 7	JUNCTION JUNCTION	63.87 63.91	3.64 3.51	0.0		0	C18 0.0992	0.0130	STMDD	STMFF	CONDUIT	
8 9	JUNCTION JUNCTION	63.96 64.11	3.51 3.00	0.0		0	C18_1	0.0130	STM109	J40	CONDUIT	
1	JUNCTION JUNCTION	63.31 63.68	2.94	0.0			C18_2 .1265	0.0130	J40	STM108	CONDUIT	
	JUNCTION	63.56	2.58	0.0			C19 0.0526	0.0130	STMFF	STMGG	CONDUIT	
	JUNCTION	63.76 63.44	2.64	0.0		0	C2 .1975	0.0130	STM102	STM119	CONDUIT	
	JUNCTION JUNCTION	63.57 63.35	2.83 2.21	0.0		6	C20 5.1921	0.0130	STMGG	STM108	CONDUIT	
CN1	JUNCTION JUNCTION	63.42 63.32	2.78 3.03	0.0		0	C21 .2247	0.0130	STMCC	STMDD	CONDUIT	
CN2	JUNCTION JUNCTION	63.79 63.18	2.79	0.0		0	C21_1 0.0599	0.0130	STM108	J32	CONDUIT	
	JUNCTION JUNCTION	63.12 63.09	2.93 2.82	0.0			C21_2 .0565	0.0130	J32	STM107	CONDUIT	
_Outlet	JUNCTION OUTFALL	63.03 62.58	2.85	0.0		0	C22 .5029	0.0130	J19	CBMHU	CONDUIT	
1	OUTFALL STORAGE	62.22 62.81	0.97	0.0			C23 .5054	0.0130	CBMHU	STM108	CONDUIT	
2	STORAGE	62.95	2.19	0.0		0	C24 .3752	0.0130	STM122	STM121	CONDUIT	
-Lawn-Stor G-A	STORAGE	64.40 100.00	0.50	0.0			C25	0.0130	STM121	STM107	CONDUIT	
-в -с	STORAGE	100.00	0.15	0.0			C26	0.0130	STM107	STM106A	CONDUIT	
- D - G	STORAGE STORAGE	100.00	0.15	0.0			C27	0.0130	STMBB	STMCC	CONDUIT	
l I	STORAGE STORAGE	100.00	0.15	0.0			C27_2	0.0130	STM106B	STM105	CONDUIT	
J	STORAGE STORAGE	100.00	0.15	0.0			C28	0.0130	STM105	STM104	CONDUIT	
	SIURAGE	100.00	0.10	0.0			C29		STM104	STM102A	CONDUIT	
***							C3	0.0130	STM119	STM118	CONDUIT	
mmary *****							C30	0.0130	STM102A	STM101A	CONDUIT	
hness	From Node	To Node	Туре	Length	8	0	C31	0.0130	STM101A	STM101	CONDUIT	
						0	C32	0.0130	STM101	J28	CONDUIT	
0.0130	STM115	STM114	CONDUIT	75.0		0	C33	0.0130	J37	J1	CONDUIT	
	STMC	SIMD	CONDUIT	53.4		0	C34	0.0130	J1	CBMHU	CONDUIT	
0.0130	STMD	STM116	CONDUIT	56.4		0	C34 C35	0.0130	STMA	STMB	CONDUIT	
0.0130	STM116	STM112	CONDUIT	81.9		0	.0999	0.0130				
0.0130	STM-CCN2	STM-CCN1	CONDUIT	24.3		0	C36 0.0761	0.0130	STMB	STMC	CONDUIT	
0.0130	STM111A	STM-CCN1	CONDUIT	17.9	0.50		C37 0.8418	0.0130	J33	Canal_Outlet	CONDUIT	
					0.50							
0.0130	STMAA	STMBB	CONDUIT	73.4		0	C7 0.2004	0.0130	STM114	STM113	CONDUIT	
.0130	CBMH2A	STMAA	CONDUIT	73.4 35.7			C8	0.0130 0.0130	STM113	STM112	CONDUIT	
.0130	CBMH2A STM118	STMAA STM117	CONDUIT	73.4 35.7 8.8		0	C8 C9 C9 C9 C1015	0.0130 0.0130 0.0130	STM113 STM112	STM112 STM109	CONDUIT	
.0130	CBMH2A	STMAA	CONDUIT	73.4 35.7		0	C8 C9 C9	0.0130	STM113	STM112	CONDUIT	
0.0130 0.0130 0.0130	CBMH2A STM118	STMAA STM117	CONDUIT	73.4 35.7 8.8		0 0 0	0.2004 C8 0.0999 C9 0.1015 W24	0.0130	STM113 STM112	STM112 STM109	CONDUIT	
.0130 .0130 .0130 .0350	CBMH2A STM118 CBA1 J48 J49	STMAA STM117 CBMH2A	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	73.4 35.7 8.8 92.3 88.2 39.4		0 0 0	0.2004 C8 0.0999 C9 0.1015 W24 0.6623 W25	0.0130 0.0130 0.0100	STM113 STM112 STM115 STM114 STM113	STM112 STM109 STM114 STM113 STM112	CONDUIT CONDUIT CONDUIT	
.0130 .0130 .0130 .0350 .0130	CBMH2A STM118 CBA1 J48	STMAA STM117 CEMH2A J49	CONDUIT CONDUIT CONDUIT CONDUIT	73.4 35.7 8.8 92.3 88.2	-	0 0 0 0).2004 C8).0999 C9).1015 W24).6623 W25).1974 W26	0.0130 0.0130 0.0100 0.0130	STM113 STM112 STM115 STM114	STM112 STM109 STM114 STM113	CONDUIT CONDUIT CONDUIT CONDUIT	
.0130 .0130 .0130 .0350 .0130 .0350	CBMH2A STM118 CBA1 J48 J49	STMAA STM117 CBMH2A J49 STMD	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	73.4 35.7 8.8 92.3 88.2 39.4		0 0 0 0 0 0).2004 C8).0999 C9).1015 W24).6623 W25).1974 W26).5495 W27).4727 W28	0.0130 0.0130 0.0100 0.0130 0.0130	STM113 STM112 STM115 STM114 STM113	STM112 STM109 STM114 STM113 STM112	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	
0.0130 0.0130 0.0130 0.0350 0.0130 0.0350 0.0350 0.0240	CBMH2A STM118 CBA1 J48 J49 J50	STMAA STM117 CBMH2A J49 STMD J51	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	73.4 35.7 8.8 92.3 88.2 39.4 105.0		0 0 0 0 0 3	0.2004 C8 0.0999 C9 0.1015 W24 0.6623 W25 0.1974 W26 0.5495 W27 0.4727 W28 8.5105 W29	0.0130 0.0130 0.0100 0.0130 0.0100 0.0130 0.0100	STM113 STM112 STM115 STM114 STM113 STM102	STM112 STM109 STM114 STM113 STM112 STM119	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	
0.0130 0.0130 0.0130 0.0350 0.0350 0.0350 0.0240 0.0130 0.0130	CBMH2A STM118 CBA1 J48 J49 J50 J51	STMAA STM117 CEMH2A J49 STMD J51 J48	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	73.4 35.7 8.8 92.3 88.2 39.4 105.0 21.6		0 0 0 0 3 2).2004 C8 0.0999 C9 0.1015 W25 0.6623 W25 0.5495 W27 0.4727 W28 0.5105 W28 0.5105 W29 0.5105 W29 0.5307 W30	0.0130 0.0130 0.0100 0.0130 0.0100 0.0130 0.0100 0.0130	STM113 STM112 STM115 STM114 STM113 STM102 STM119	STM112 STM109 STM114 STM113 STM112 STM119 STM118	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	
0.0130 0.0130 0.0350 0.0350 0.0350 0.0350 0.0240 0.0240 0.0130	CBMH2A STM118 CBA1 J48 J49 J50 J51 J52	STMAA STM117 CEMH2A J49 STMD J51 J48 J53	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	73.4 35.7 8.8 92.3 88.2 39.4 105.0 21.6 90.8		0 0 0 0 3 22	0.2004 C8 0.0999 C9 0.1015 W24 0.6623 W25 0.1974 W26 0.5495 W27 W28 0.4727 W28 0.4727 W28 0.4727 W29 0.4727 W30 0.2411 W31	0.0130 0.0130 0.0100 0.0130 0.0130 0.0130 0.0130 0.0130	STM113 STM112 STM115 STM114 STM113 STM102 STM119 STM118	STM112 STM109 STM114 STM113 STM112 STM119 STM118 STM117	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	
0.0130 0.0130 0.0350 0.0350 0.0350 0.0350 0.0240 0.0130 0.0130	CBMH2A STM118 CBA1 J48 J49 J50 J51 J52 J53	STMAA STM117 CEMH2A J49 STMD J51 J48 J53 J54	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	73.4 35.7 8.8 92.3 88.2 39.4 105.0 21.6 90.8 22.0		0 0 0 0 3 22).2004 C8 C9 C9 W24).1015 W25).1974 W26 S.5495 W27 0.4727 W28 S.5105 W29 S.4307 W30 S.2411 W31 0.2411 W31 C27_1	0.0130 0.0130 0.0100 0.0130 0.0100 0.0130 0.0100 0.0130	STM113 STM112 STM115 STM114 STM113 STM102 STM119 STM118 STM117 STM116_STA STM106A	STM112 STM109 STM114 STM113 STM112 STM119 STM118 STM116_STA STM116_STA STM113	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT ORIFICE	
0.0130 0.0130 0.0130 0.0350 0.0130 0.0240 0.0130 0.0130 0.0130 0.0130	CBMH2A STM118 CBA1 J48 J49 J50 J51 J52 J53 J54	STMAA STM117 CBMH2A J49 STMD J51 J48 J53 J54 J55	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	73.4 35.7 8.8 92.3 88.2 39.4 105.0 21.6 90.8 22.0 7.7		0 0 0 0 3 22).2004 C8 C9 C9 W24 W24 V26 W25 V25 V25 V27 W28 V26 V27 W28 V29 V4727 W28 V29 V4727 W29 V4727 W29 V4727 W29 V4727 W29 V4747 V477 W29 V4777 V477 V477 V477 V477 V477 V477 V4	0.0130 0.0130 0.0100 0.0130 0.0130 0.0130 0.0130 0.0130	STM113 STM112 STM115 STM114 STM102 STM119 STM119 STM118 STM117 STM116_STA STM106A BASIN1	STM112 STM109 STM114 STM113 STM112 STM119 STM116 STM116_STA STM113 STM106B J40 J32	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT ORIFICE ORIFICE	
).0130).0130).0350).0350).0350).0350).0350).0240).0130).0130).0130).0130	CBMH2A STM118 CBA1 J48 J49 J50 J51 J52 J53 J54 J55	STMAA STM117 CBMH2A J49 J51 J51 J48 J53 J54 J55 J56	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	73.4 35.7 8.8 92.3 88.2 39.4 105.0 21.6 90.8 22.0 7.7 65.7		0 0 0 0 3 22).2004 C8 C9 C9 C9 W24 W25).1015 W24 W25).1974 W26 0.5495 W27 W28 S.5105 W29 5.5405 W29 5.5405 W29 1.4727 W28 S.5105 W29 1.4727 W28 S.5105 W29 C9 C9 C9 C9 C9 C9 C9 C9 C9 C	0.0130 0.0130 0.0100 0.0130 0.0130 0.0130 0.0130 0.0130	STW113 STW112 STM115 STM114 STM102 STM102 STM105 STW116_STA STW106A BASIN2 EASIN1 STW102A STW102A STW102A	STM112 STM1109 STM114 STM113 STM112 STM119 STM118 STM117 STM116_STA STM113 STM1106B J40 J32 J68 J48	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT ORIFICE ORIFICE ORIFICE WEIR	
0.0130 0.0130 0.0350 0.0350 0.0240 0.0130 0.0130 0.0130 0.0130 0.0130	CBMH2A STM118 CBA1 J48 J50 J51 J52 J53 J54 J55 J59	STMAA STM117 CBMH2A J49 J51 J51 J48 J53 J54 J55 J56 J58	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	73.4 35.7 8.8 92.3 88.2 39.4 105.0 21.6 90.8 22.0 7.7 65.7 18.0		0 0 0 0 3 22).2004 C8 .0999 C9 .1015 W24 .6623 W25 .5495 W27 .4727 W28 .5105 W29 .54307 W30 .2411 W31 .1417 C27_1 OR1 OR1 OR16	0.0130 0.0130 0.0100 0.0130 0.0130 0.0130 0.0130 0.0130	STM113 STM112 STM115 STM114 STM113 STM102 STM105 STM117 STM116_STA STM106A BASIN2 BASIN2 BASIN1 STM102A	STM112 STM1109 STM114 STM113 STM112 STM119 STM116 STM116_STA STM116_STA STM106B J40 J40 J32 J68	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT ORIFICE ORIFICE WEIR	
0.0130 0.0130 0.0350 0.0350 0.0240 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130	CBMH2A STM118 CBA1 J48 J49 J50 J51 J52 J53 J54 J55 J59 STM117	STMAA STM117 CBMH2A J49 STMD J51 J48 J53 J54 J55 J56 J58 STM116_STA	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	73.4 35.7 8.8 92.3 88.2 39.4 105.0 21.6 90.8 22.0 7.7 65.7 18.0 6.7		0 0 0 0 3 22).2004 C8 .0999 C9 .1015 W24 W26 .5495 W27 .4727 W20 W27 .4727 W28 .5105 W29 .2411 W31 .2411 W31 .2411 W31 .1417 C27_1 OR1 OR2 OL16 W10 W11 W13	0.0130 0.0130 0.0100 0.0130 0.0130 0.0130 0.0130 0.0130	STM113 STM112 STM115 STM114 STM113 STM102 STM102 STM19 STM18 STM17 STM16_STA STM16_STA STM16A BASIN2 BASIN2 BASIN1 STM10A STM10A STM13A	STM112 STM109 STM114 STM113 STM112 STM119 STM118 STM116 STM116_STA STM116E J40 J40 J40 J40 J40 J40 J49	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	
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).0130).0130).0130).0350).0350).0130).0130).0130).0130).0130).0130	CBMH2A STM118 CBA1 J48 J50 J51 J52 J53 J54 J55 J59 STM117 J58 J57 J50	STMAA STM117 CEMH2A J49 STMD J51 J48 J53 J54 J55 J56 J58 STM116_STA J57 J52 J52	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	73.4 35.7 8.8 92.3 88.2 39.4 105.0 21.6 90.8 22.0 7.7 65.7 18.0 6.7 14.2 47.6 70.3	-	0 0 0 0 3 22).2004 C8 C8 C9 .1015 w24 .6623 w25 .1974 w26 .5495 w27 .4727 w28 .5105 w29 .4727 w28 .5105 w29 .4727 w20 .4411 w31 .1417 C27_1 OR1 OR2 OL6 W31 .1417 W31 W11 W12 W13 W14 W15 W15 W15 W17	0.0130 0.0130 0.0100 0.0130 0.0130 0.0130 0.0130 0.0130	STM113 STM112 STM115 STM114 STM102 STM102 STM105 STM105 STM116_STA STM105 STM105A EASIN1 STM102A STM0 STM02A STM0 STM102A STM102A STM113 STM05 STM113	STW112 STW109 STW114 STW113 STW112 STW119 STW116 STW116_STM STW106B J40 J40 J49 J50 Great-Lawn-Stor J60 Great-Lawn-Stor J52 J53	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT WEIR WEIR WEIR WEIR WEIR WEIR WEIR	
0130 0130 0350 0350 0240 0130 0130 0130 0130 0130 0130 0130	CBMH2A STM118 CBA1 J49 J50 J51 J52 J53 J54 J55 J59 STM117 J58 J57 J59 STM117 J58 J57	STMAA STM117 CEMH2A J49 STMD J51 J48 J53 J54 J55 J56 J56 STM116_STA J57 J52 J52 J61 J63	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	73.4 35.7 8.8 92.3 88.2 39.4 105.0 21.6 90.8 22.0 7.7 65.7 18.0 6.7 14.2 47.6 70.3 26.8	-	0 0 0 0 3 22).2004 C8 C8 C9 J01015 W24 J.6623 W25 J.25495 W27 W26 J.5105 W29 J.4727 W28 J.5105 W29 J.4727 W28 J.5105 W29 J.4727 W20 J.4727 W20 W14 W12 W14 W16 W16	0.0130 0.0130 0.0100 0.0130 0.0130 0.0130 0.0130 0.0130	STM113 STM112 STM115 STM114 STM102 STM102 STM102 STM105 STM106A BASIN2 BASIN1 STM106A BASIN2 BASIN1 STM106A BASIN1 STM106A BASIN1 STM106A BASIN1 STM106A BASIN1 STM106A BASIN1 STM106A BASIN1 STM106A BASIN1 STM106A BASIN1 STM106A BASIN1 STM106A BASIN1 STM106A BASIN1 STM106A BASIN1 STM106A BASIN1 STM106A STM107	STM112 STM114 STM113 STM112 STM112 STM119 STM116 STM116_STA STM116_STA STM116 J40 J40 J40 J40 J40 J50 Great-Lawn-Stor J52	CONDUIT CONDUIT	
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B-BLOC-O SHD22 Grad-Lawn-Bucarge JJJ DUTLET OUTLET OUTLET OUTLET Full Full Rud. Max. No. of Full Full Rud. Max. No. of Imare Dept Area Red. Witeb Dertes CHCULAR O.42 O.53 O.21 O.40 1 CHCULAR O.40 O.28 O.15 O.40 1 CHCULAR O.40 O.28 O.50 I.40 I.40 CHCULAR O.40 O.40 O.50 I.40 I.40	Width Barrels 0.82 1 0.60 1 0.90 1 0.90 1 0.25 1 0.60 1 0.60 1 0.60 1 0.60 1 0.60 1 0.60 1 0.60 1 0.60 1 0.60 1 0.90 1 1.35 1 0.90 1 8.00 1 8.00 1 8.00 1 8.00 1 7.00 1 7.00 1 7.00 1 6.00 1 8.00 1 8.00 1 8.00 1 8.00 1 8.00 1 8.00 1 8.00 1 8.00 1 <td>22 OUTLET</td> <td>C25 CIRCULAR 0.68 0.36 0.17 0. 0.53</td>	22 OUTLET	C25 CIRCULAR 0.68 0.36 0.17 0. 0.53
CHERCY-LEARN-SCREER JOILET Full Full Rull Max. Mas. Ms. of Shape Depth Area Rad. Kidth Barzela CIRCULAR 0.60 0.33 0.21 0.40 1 CIRCULAR 0.60 0.23 0.40 1 CIRCULAR 0.90 0.64 0.23 0.90 1 CIRCULAR 0.90 0.64 0.23 0.40 1 CIRCULAR 0.90 0.64 0.23 0.40 1 CIRCULAR 0.40 0.28 0.15 0.60 1 CIRCULAR 0.40 0.28 0.15 0.40 1 CIRCULAR 0.40 0.28 0.41 1.35 1 CIRCULAR 0.40 0.28 0.40 1.35 1 CIRCULAR 0.40 0.40 0.40 1.35 1 CIRCULAR 0.40 0.40 0.40 1.35 1	Width Barrels 0.82 1 0.60 1 0.90 1 0.90 1 0.25 1 0.60 1 0.60 1 0.60 1 0.60 1 0.60 1 0.60 1 0.60 1 0.60 1 0.60 1 0.90 1 1.35 1 0.90 1 8.00 1 8.00 1 8.00 1 8.00 1 8.00 1 7.00 1 7.00 1 6.00 1 8.00 1 8.00 1 8.00 1 8.00 1 8.00 1 8.00 1 8.00 1 8.00 1 <td>22 OUTLET</td> <td>C26 CIRCULAR 1.35 1.43 0.34 1. 2.20</td>	22 OUTLET	C26 CIRCULAR 1.35 1.43 0.34 1. 2.20
TRUE Full Full Full Hyd. Mas. Rot. of Shape Begth Area Rad. Nid. Barto CIRCULAR 0.42 0.53 0.21 0.49 1 CIRCULAR 0.40 0.23 0.40 1.21 1 CIRCULAR 0.40 0.23 0.40 1.23 1 CIRCULAR 0.23 0.05 0.64 0.23 1 CIRCULAR 0.23 0.15 0.60 1 1 CIRCULAR 0.40 0.23 0.13 1 1 CIRCULAR 0.40 0.23 0.40 1.33 1 CIRCULAR 1.35 1.43 0.40 1.33 1 CIRCULAR 0.25 0.44 0.23 0.40 1 RECTOREN 1.00 8.00 0.40 1.33 1 RECTOREN 1.00 8.00 0.40 1.40 1 RECTOREN 1	WidthBarrels0.8210.6010.9010.2510.6010.6010.6010.6010.70011.3510.9011.3510.9018.0018.0018.0018.0018.0018.0018.0018.0017.0017.0017.0016.0018.00 </td <td></td> <td>C27 CIRCULAR 0.53 0.22 0.13 0. 0.21</td>		C27 CIRCULAR 0.53 0.22 0.13 0. 0.21
Full Full Full Full Keit Name Name shape Deet Area Rad Nich Barzet CIRCULAR 0.42 0.53 0.21 0.42 1 CIRCULAR 0.40 0.23 0.40 0.44 0.23 0.40 1 CIRCULAR 0.20 0.64 0.23 0.40 1.21 1 CIRCULAR 0.20 0.64 0.23 0.40 1.21 1 CIRCULAR 0.40 0.23 0.40 1.23 1.41 0.40 1.21 1 CIRCULAR 0.40 0.41 0.43 1.43 1.43 1.41 1.45 1 CIRCULAR 0.45 0.44 0.23 0.40 1 1 CIRCULAR 0.45 0.44 0.23 0.40 1 1 CIRCULAR 0.45 0.44 0.23 0.40 1 1 CIRCULAR 0.45 0.4<	Width Barrels 0.82 1 0.60 1 0.90 1 0.90 1 0.25 1 0.60 1 0.60 1 0.60 1 0.60 1 0.60 1 0.60 1 0.60 1 0.60 1 0.60 1 0.60 1 0.60 1 0.90 1 1.35 1 0.90 1 8.00 1 8.00 1 8.00 1 8.00 1 8.00 1 8.00 1 6.00 1 8.00 1 8.00 1 8.00 1 8.00 1 8.00 1 8.00 1 8.00 1 <td></td> <td>C27_2 CIRCULAR 0.97 0.75 0.24 0.</td>		C27_2 CIRCULAR 0.97 0.75 0.24 0.
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	0.4589 0.5987 0.7551 0.9284	0.4855 0.6287 0.7884 0.9598	0.5128 0.6593 0.8223 0.9822	0.5408 0.6906 0.8570 0.9956	0.5694 0.7225 0.8923 1.0000		0.6902 0.7930 0.8958 0.9923	0.7107 0.8135 0.9153 0.8333	0.7313 0.8341 0.9345 0.5556	0.7519 0.8547 0.9538 0.2778	0.7724 0.8752 0.9730 0.0000
	0.0372 0.2365 0.4324 0.6298 0.8288 1.0266 1.2191 1.4056 1.5879 1.7432	0.0761 0.2767 0.4727 0.6707 0.8684 1.0657 1.2568 1.4423 1.6237 1.4768	0.1167 0.3160 0.5123 0.7109 0.9079 1.1045 1.2943 1.4789 1.6580 1.2801	0.1577 0.3545 0.5513 0.7506 0.9473 1.1430 1.3316 1.5153 1.6923 1.1258	0.1971 0.3926 0.5899 0.7899 0.9872 1.3687 1.5517 1.7266 1.0000	Shape 1.03 Area:	30_1 0.0011 0.1137 0.2272 0.3409 0.4545 0.5681 0.6818 0.7954	0.0036 0.0348 0.1363 0.2499 0.3636 0.4772 0.5909 0.7045 0.8182	0.0070 0.0512 0.1590 0.2727 0.3863 0.5000 0.6136 0.7272 0.8409	0.0115 0.0715 0.1817 0.2954 0.4090 0.5227 0.6363 0.7500 0.8636	0.0170 0.0924 0.2045 0.3181 0.4318 0.5454 0.6591 0.7727 0.8864
	0.0402 0.1958 0.3244 0.4380 0.5392 0.6327 0.7235 0.8143 0.9051 0.9876	0.0771 0.2219 0.3474 0.4582 0.5585 0.6509 0.7417 0.8325 0.9235 0.7397	0.1097 0.2480 0.3704 0.4785 0.5776 0.6691 0.7599 0.8506 0.9428 0.4917	0.1387 0.2741 0.3935 0.4987 0.5964 0.6872 0.7780 0.8688 0.9622 0.2445	0.1678 0.3002 0.4165 0.5189 0.6146 0.7054 0.7962 0.8870 0.9816 0.0000	Hrad:	0.9091 0.0314 0.1620 0.2745 0.5046 0.7284 0.9360 1.1291 1.3091 1.4773	0.9318 0.0635 0.1324 0.3125 0.5507 0.7712 0.9758 1.1661 1.3436 1.5096	0.9545 0.0926 0.1419 0.3616 0.5962 0.8133 1.0149 1.2026 1.3777 1.5415	0.9773 0.1201 0.1823 0.4100 0.6410 0.8548 1.0535 1.2386 1.4113 1.5730	1.0000 0.1455 0.2297 0.4577 0.6850 0.8957 1.0916 1.2741 1.4445 1.6041
	_3 0.0005 0.0170 0.0559 0.1165 0.1985 0.3018 0.4254 0.5689 0.7323 0.7323	0.0019 0.0230 0.0663 0.1312 0.2175 0.3250 0.4525 0.6000 0.7673 0.9516	0.0043 0.0299 0.0776 0.1467 0.2373 0.3489 0.4804 0.6319 0.8031 0.9785	0.0076 0.0377 0.0897 0.1631 0.2580 0.3736 0.5091 0.6645 0.8396 0.9946	0.0119 0.0464 0.1027 0.1804 0.2795 0.3991 0.5386 0.6980 0.8769 1.0000	Width:	1.6348 0.0832 0.3361 0.9547 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	1.6651 0.1290 0.6079 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	1.6950 0.1738 0.8354 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	1.7246 0.2192 0.9071 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	1.0001 0.2684 0.9283 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000
	0.0376 0.2280 0.4180 0.6063 0.7928 0.9819 1.1744 1.3639 1.5516 1.7455	0.0752 0.2657 0.4559 0.6437 0.8300 1.0207 1.2125 1.4016 1.5904 1.5679	0.1127 0.3033 0.4937 0.6811 0.8671 1.0593 1.2505 1.4392 1.6294 1.3259	0.1518 0.3414 0.5313 0.7183 0.9042 1.0978 1.2884 1.4767 1.6682 1.1446	0.1901 0.3798 0.5689 0.7555 0.9429 1.1362 1.3262 1.5142 1.7069 1.0000	Shape 1.0 Area:	0.0006 0.0246 0.0687 0.1257 0.1973 0.2893 0.3991 0.5241	0.0025 0.0324 0.0791 0.1388 0.2142 0.3100 0.4229 0.5510	0.0059 0.0407 0.0900 0.1524 0.2318 0.3313 0.4473 0.5787	0.0111 0.0495 0.1014 0.1667 0.2503 0.3532 0.4723 0.6077	0.0174 0.0589 0.1133 0.1815 0.2694 0.3758 0.4978 0.6381
	0.0248 0.1440 0.2574 0.3684 0.4793 0.5874	0.0496 0.1672 0.2796 0.3905 0.5015 0.6079	0.0744 0.1904 0.3018 0.4127 0.5236 0.6285	0.0976 0.2131 0.3240 0.4349 0.5458 0.6490	0.1208 0.2352 0.3462 0.4571 0.4571 0.6696	Hrad:	0.6695 0.8421 0.0439 0.2771 0.5611 0.8054	0.7019 0.8797 0.0784 0.3374 0.6132 0.8484	0.7354 0.9185 0.1169 0.3949 0.6640 0.8912	0.7699 0.9586 0.1600 0.4523 0.7137 0.9337	0.8055 1.0000 0.2149 0.5075 0.7620 0.9723
Vidth:	0.9801 1.1656 1.3842 1.6056 1.7156 1.8607 0.0272 0.1778 0.2408	1.0115 1.2075 1.4302 1.6451 1.7430 1.8918 0.0632 0.1913 0.2529	1.0497 1.2511 1.4758 1.6692 1.7713 1.9130 0.1025 0.2046 0.2650	1.0882 1.2946 1.5212 1.6678 1.8004 1.9355 0.1394 0.2167 0.2771	1.1268 1.3380 1.5663 1.6891 1.8302 1.0000 0.1631 0.2288 0.2894	Hrad:	0.1075 0.1960 0.2975 0.4121 0.5669 0.7649 0.9028 0.9808 0.0375	0.1242 0.2153 0.3193 0.4366 0.6113 0.7973 0.9232 0.9892 0.1240	0.1414 0.2350 0.3417 0.4616 0.6533 0.8273 0.9412 0.9952 0.1851	0.1591 0.2553 0.3646 0.4882 0.6929 0.8548 0.9568 0.9988 0.2523	0.1773 0.2761 0.3881 0.5202 0.7301 0.8800 0.9700 1.0000 0.3182
hape 1.030_	0.3036 0.3912 0.4829 0.5598 0.6325 0.7597 0.8840	0.3178 0.4118 0.4993 0.5739 0.6491 0.7846 0.9088	0.3320 0.4296 0.5148 0.5879 0.6724 0.8094 0.9392	0.3462 0.4473 0.5304 0.6020 0.7082 0.8343 0.9696	0.3619 0.4651 0.5458 0.6160 0.7349 0.8591 1.0000		0.3831 0.6223 0.9393 1.2166 1.4680 1.0362 1.1479 1.1494 1.0842	0.4393 0.6900 0.9973 1.2688 1.5160 1.0707 1.1552 1.1407 1.0654	0.4740 0.7553 1.0539 1.3201 1.5558 1.0984 1.1587 1.1297 1.0450	0.4912 0.8185 1.1093 1.3700 1.5322 1.1200 1.1586 1.1165 1.0232	0.5519 0.8798 1.1635 1.4193 0.9940 1.1364 1.1554 1.1013 1.0000
	0.0028 0.0401 0.0943 0.1624 0.2451 0.3425 0.4543 0.5804 0.7203 0.8711	0.0081 0.0498 0.1068 0.1777 0.2634 0.3637 0.4784 0.6073 0.7496 0.9025	0.0149 0.0600 0.1199 0.2823 0.3855 0.5030 0.6348 0.7794 0.9343	0.0226 0.0709 0.1335 0.2102 0.3018 0.4079 0.5282 0.6628 0.8096 0.9668	0.0310 0.0824 0.1476 0.2274 0.3219 0.4308 0.5540 0.6913 0.6913 0.8402 1.0000	Width:	0.1024 0.2082 0.3390 0.4468 0.5017 0.9429 0.6948 0.4467 0.1985	0.1194 0.2276 0.3498 0.4037 0.4575 0.5128 0.8933 0.6452 0.3970 0.1489	0.1520 0.2610 0.3606 0.4144 0.4684 0.5273 0.8437 0.5955 0.3474 0.0993	0.1734 0.3080 0.3713 0.4252 0.4795 0.5728 0.7940 0.5459 0.2978 0.0496	0.1922 0.3282 0.3821 0.4360 0.9926 0.7444 0.4963 0.2481 0.0000
	0.0451 0.2899 0.5176 0.7195 0.9031 1.0834 1.2612 1.4356 1.6213	0.0901 0.3377 0.5606 0.7569 0.9390 1.1193 1.2964 1.4702 1.6633	0.1398 0.3838 0.6026 0.7939 0.9747 1.1550 1.3313 1.5050 1.7049	0.1923 0.4285 0.6435 0.8306 1.0109 1.1906 1.3662 1.5431 1.7462	0.2412 0.4737 0.6617 0.8670 1.0473 1.2260 1.4010 1.5809 1.7871	Shape 1170 Area:	0_2 0.0005 0.0169 0.0551 0.1144 0.2367 0.3742 0.5117	0.0018 0.0230 0.0652 0.1311 0.2642 0.4017 0.5393	0.0041 0.0298 0.0762 0.1544 0.2917 0.4292 0.5668	0.0074 0.0374 0.0879 0.1817 0.3192 0.4567 0.5943	0.0117 0.0459 0.1005 0.2092 0.3467 0.4842 0.6218
Width:	1.8279 0.1283 0.2801	1.8683 0.1844 0.2978 0.3811	1.8978 0.2182 0.3155 0.3971	1.9230 0.2395 0.3330 0.4134	1.0000 0.2610 0.3490 0.4311	Hrad:	0.6493 0.7868 0.9244 0.0316	0.6768 0.8143 0.9519 0.0626	0.7043 0.8418 0.9780 0.0953	0.7318 0.8693 0.9945 0.1241	0.7593 0.8968 1.0000 0.1548
	0.3651 0.4488 0.5374 0.6242 0.7092 0.7943 0.8703 0.9292	0.4666 0.5552 0.6412 0.7262 0.8113 0.8821 0.9410	0.4843 0.5729 0.6582 0.7432 0.8281 0.8939 0.9589	0.5020 0.5901 0.6752 0.7603 0.8427 0.9057 0.9794	0.5197 0.6071 0.6922 0.7773 0.8574 0.9174 1.0000		0.1901 0.3530 0.4832 0.5636 0.8061 1.0065 1.1747	0.2251 0.3837 0.4225 0.6161 0.8492 1.0424 1.2052	0.2588 0.4152 0.4104 0.6665 0.8907 1.0772 1.2347	0.2916 0.4465 0.4516 0.7149 0.9307 1.1108 1.2633	0.3223 0.4776 0.5088 0.7614 0.9692 1.1433 1.2911

0.6349 0.6609 0.6870 0.7131 0.7392 0.7653 0.7914 0.8174 0.8435 0.8696 0.8957 0.9218 0.9478 0.9739 1.0000 d:	0.5375 0.5500 0.5625 0.5750 0.5876 0.6001 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000
d: 0.05599 0.1132 0.1636 0.2129 0.2593 0.3031 0.3448 0.3846 0.4229 0.4598 0.4956 0.5303 0.5641 0.4010 0.4344 0.4810 0.5308 0.5795 0.6270 0.6734 0.7189 0.7633 0.8069 0.8496 0.8908 0.8013 0.8477 0.8930 0.9374 0.9808 1.0233 1.0649 1.1057 1.1456 1.1847 1.2230 1.2605 1.2973 1.3334 1.3688 1.4025 1.4375 1.4709 1.5037 1.5339 1.5674 1.5984 1.6289 1.6588 1.0000 th: 0.3138 0.3286 0.3419 0.3552 0.3655 0.3180 0.3910 0.0484 0.7054 0.7522 0.7596 0.7759 0.7822 0.7866 0.7949 0.8012 0.8075 0.8138 0.8201 0.8274 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	NOTE: The summary statistics displayed in this report are based on results from dat every computational time step, not just on results from each reporting time step. Analysis Options The Units
pe 3235 a: 0.0097 0.0196 0.0299 0.0405 0.0513 0.0625 0.0740 0.0857 0.1978 0.1101 0.1228 0.1357 0.1490 0.1625 0.1764 0.1905 0.2141 0.2379 0.2617 0.2855 0.3094 0.3332 0.3570 0.3808 0.4046 0.4244 0.4523 0.4761 0.4999 0.5237 0.5475 0.5713 0.5951 0.6199 0.6428 0.6666 0.6904 0.7142 0.7380 0.7618 0.6666 0.6904 0.7142 0.7380 0.7618 0.7857 0.8095 0.8333 0.8571 0.8809 0.9047 0.9286 0.9524 0.9762 1.0000	Flow Routing Method DYWWAVE Surcharge Method EXTRAN Starting Date
Volume Depth off Quantity Continuity hectare-m mm al Precipitation 1.159 71.677 poration Loss 0.000 0.000 iltration Loss 0.225 13.897 face Runoff 0.923 57.120 al Storage 0.019 1.165 tinuity Error (%) -0.705 Weather Inflow 0.923 5.234 undwater Inflow 0.923 5.234 undwater Inflow 0.000 0.000 Inflow 0.000 0.000 ernal Outflow 0.200 7.204	Minimum Time Step : 0.50 sec Average Time Step : 0.98 sec Maximum Time Step : 1.00 sec Percent in Steady State : -0.00 Average lecarions per Step : 6.11 Percent Not Converging : 17.95 Time Step Frequencies : 1.000 - 0.871 sec : 94.92 % 0.871 - 0.758 sec : 1.61 % 0.758 - 0.560 sec : 1.42 % 0.660 - 0.574 sec : 0.97 % 0.574 - 0.500 sec : 1.09 %
oding Loss 0.000 0.000 poration Loss 0.000 0.000 litration Loss 0.000 0.000 tial Stored Volume 0.000 0.005 al Stored Volume 0.141 1.411 tinuity Error (%) 6.779	Total Total Total Imperv Perv Total Total Perk Runoff Total Total Imperv Perv Total Precip Runon Evap Infil Runoff Runoff Runoff Runoff Runoff Coeff mm 10/6 11 CMS 10/2 71.66 0.00 0.00 20.12 45.43
hest Continuity Errors e J40 (6.39%) e BASIN2 (2.87%) e J60 (2.28%) e STM119 (1.4%) e J50 (1.38%)	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
e-Step Critical Elements k C64 (6.56%)	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
	2.89 66.67 0.62 0.45 0.930 A4 71.68 0.00 0.00 6.76 59.59

3	71.68	0	.00	0.00	0.00	70.32	J51	JUNCTION	0.00	0.00	65.35	0 00:00
70.32 C	0.25 0	0	.00	0.00	0.00	70.32	J52 J53	JUNCTION JUNCTION	0.01 0.01	0.18 0.12		0 01:10 0 01:10
70.32	71.68		.00	0.00	0.00	70.32	J54 J55	JUNCTION JUNCTION	0.00	0.05	65.30 65.26	0 01:10 0 01:11
70.32	0.10 0	0	.00	0.00	0.00	70.32	J56 J57	JUNCTION	0.01	0.23	65.18 65.49	0 01:13 0 01:10
70.32	0.17 (71.68	0	.00	0.00	0.00	70.32	J58 J59	JUNCTION	0.00	0.15	65.50 65.60	0 01:10 0 01:10
-I 70.32	0.26 0.16	0	.00	0.00	0.00	70.32	J60 J61	JUNCTION	0.00	0.09	64.74 64.74	0 01:27 0 01:28
70.32 J 70.32	0.10 71.68	0	.00	0.00	0.00	70.32	J62 J63	JUNCTION JUNCTION	0.00	0.02		0 01:30 0 01:31
70.32 J2 70.32	0.10 71.68	0	.00	0.00	0.00	70.32	J64 J65	JUNCTION	0.00	0.07	64.72	0 01:30
-K 70.32	71.68	0	.00	0.00	0.00	70.31	J66 J67	JUNCTION JUNCTION	0.03	0.23	64.73 65.17	0 01:32 0 00:00
31.67	71.68 0.18	0	.00	0.00	39.90	21.21	J68 J69	JUNCTION	0.00	0.00	65.00 65.43	0 00:00
39.40	71.68 0.19	0.14 0	.00 .550	0.00	32.49	22.80	J70 J71	JUNCTION JUNCTION	0.00	0.00	65.20 65.70	0 00:00
25.25	71.68 0.09	0.03 0	.00	0.00	46.41	10.77	J72 J73	JUNCTION	0.00	0.00		0 00:00 0 01:12
:-Lawn 32.37 NDS	71.68 0.33 71.68	0.13 0	.00 .452 .00	0.00	39.27	18.70	J74 J75	JUNCTION JUNCTION	0.00	0.18	65.89	0 01:12 0 00:00
70.70	0.53 0	.37 0.		0.00	18.99	42.11	J76 STM101	JUNCTION	0.79	1.79	64.67	0 01:21 0 03:06
52.28 NDS	0.43 71.68	0.29 0	.729	0.00	0.02	70.30	STM101A STM102	JUNCTION	1.38	2.39		0 03:09 0 01:04
70.32	0.56 0	0.40 0.9 0	981 .00	0.00	32.90	19.50	STM102A STM104	JUNCTION	1.32	2.30	64.65 64.69	0 03:06 0 02:49
38.95	0.05	0.04 0	.543 .00	0.00	1.48	67.90	STM105 STM106A	JUNCTION	1.15	2.12	64.65 64.66	0 03:09 0 01:29
69.03	0.11 0						STM106B STM107	JUNCTION	1.05	2.02	64.67	0 03:12 0 01:29
****************************	У						STM108 STM109 STM110 STM111	JUNCTION JUNCTION JUNCTION JUNCTION	1.72 0.84 0.61 0.48	2.67 1.79 1.60 1.45		0 01:29 0 01:24 0 01:21 0 01:21
							STM111A STM112	JUNCTION JUNCTION	0.26	1.65 1.71	65.41 64.70	0 01:10 0 01:24
				Maximum	Time of Max Occurrence	Reported	STM113 STM114	JUNCTION JUNCTION	0.31 0.25	1.13 1.04	64.72 64.81	0 01:24 0 01:23
	Туре	Meters	Meters	Meters	days hr:min	Meters	STM115 STM116	JUNCTION JUNCTION	0.19 0.61	0.88	64.83 64.74	0 01:23 0 01:24
2A	JUNCTION	0.15	0.82	64.89 64.88	0 01:13 0 01:14	0.80	STM116_STA STM117	JUNCTION JUNCTION	0.22 0.21	1.26	65.13 65.22	0 01:12 0 01:12
	JUNCTION	0.41	1.77	65.13 65.18	0 01:13	1.75	STM118 STM119	JUNCTION JUNCTION	0.20	1.36 2.05	65.32 66.16	0 01:12 0 01:09
	JUNCTION	0.29	1.15	64.77 64.66	0 01:13	1.15	STM121 STM122	JUNCTION JUNCTION	0.45	1.45 1.32		0 01:23 0 01:11
	JUNCTION JUNCTION	0.99	1.44	64.53 65.21	0 00:00		STMA STMAA	JUNCTION	0.31	1.21	64.77 64.77	0 01:29 0 01:14
	JUNCTION	0.84	1.89	64.79 64.81	0 01:21 0 01:20	1.76	STMB STMBB	JUNCTION JUNCTION	0.35 0.31	1.32 1.16	64.76 64.73	0 01:25 0 01:31
	JUNCTION	0.06	0.34	64.74 65.25	0 01:27	0.33	STMC STMCC	JUNCTION JUNCTION	0.41 0.36	1.39 1.30	64.74 64.72	0 01:27 0 01:31
2CN1	JUNCTION	0.44	1.45	64.77	0 01:21		J49 0.198 0.757	JUNCTION	0.000	0.148	0 01:21	5
20N1 20N2	JUNCTION JUNCTION	0.25	1.90 1.56	65.69 64.74	0 01:10 0 01:26	1.90 1.53		JUNCTION	0.000 0.066	0.148 0.066	0 01:2: 0 01:2:	
	JUNCTION	0.25	1.90	65.69	0 01:10	1.90 1.53 1.55 1.58	0.198 0.757 J50					5 0.25
12	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION OUTFALL	0.25 0.57 0.63 0.66 0.72 1.50	1.90 1.56 1.56 1.58 1.64 1.50	65.69 64.74 64.68 64.67 64.67 64.08	0 01:10 0 01:29 0 01:29 0 01:29 0 01:29 0 01:29 0 01:29	1.90 1.53 1.55 1.58 1.63 1.50	0.198 0.757 J50 0.258 1.403 J51 0 0.000 ltr J52 1.46 -0.001	JUNCTION JUNCTION JUNCTION	0.066 0.000 0.776	0.066 0.000 1.109	0 01:2: 0 00:0 0 01:1	5 0.25 0 0 1.
	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.25 0.57 0.63 0.66 0.72	1.90 1.56 1.56 1.58 1.64	65.69 64.74 64.68 64.67 64.67	0 01:10 0 01:29 0 01:29 0 01:29 0 01:29	1.90 1.53 1.55 1.58 1.63 1.50 2.98 1.86	0.198 0.757 J50 0.258 1.403 J51 0 0.000 ltr J52 1.46 -0.001 J53 1.23 0.001	JUNCTION JUNCTION JUNCTION JUNCTION	0.066 0.000 0.776 0.000	0.066 0.000 1.109 0.964	0 01:22 0 00:00 0 01:10 0 01:10	5 0.25 0 1. 0
N2 Outlet	JUNCTION JUNCTION JUNCTION JUNCTION OUTFALL OUTFALL STORAGE STORAGE	0.25 0.57 0.63 0.66 0.72 1.50 1.60 0.92	1.90 1.56 1.58 1.64 1.50 2.98 1.86	65.69 64.74 64.68 64.67 64.67 64.08 65.20 64.67	0 01:10 0 01:29 0 01:29 0 01:29 0 01:29 0 00:00 0 03:00 0 01:29	1.90 1.53 1.55 1.58 1.63 1.50 2.98 1.86 1.70 0.25	0.198 0.757 J50 0.238 1.403 J51 0 0.000 ltr J52 1.46 -0.001 J53 1.23 0.001 J54 1.05 -0.006	JUNCTION JUNCTION JUNCTION JUNCTION	0.066 0.000 0.776 0.000 0.000	0.066 0.000 1.109 0.964 0.883	0 01:22 0 00:00 0 01:11 0 01:11 0 01:11	5 0.25 0 1. 0 0
2 utlet awn-Storag A	JUNCTION JUNCTION JUNCTION JUNCTION OUTFALL OUTFALL STORAGE STORAGE TORAGE	0.25 0.57 0.63 0.66 0.72 1.50 1.60 0.92 0.79 0.06	1.90 1.56 1.56 1.58 1.64 1.50 2.98 1.86 1.83 0.25	65.69 64.74 64.68 64.67 64.67 64.08 65.20 64.67 64.78 64.65	0 01:10 0 01:26 0 01:29 0 01:29 0 01:29 0 01:29 0 00:00 0 03:00 0 01:29 0 01:21 0 03:15	1.90 1.53 1.55 1.58 1.63 1.50 2.98 1.86 1.70 0.25 0.07 0.08	0.198 0.757 J50 0.238 1.403 J51 0 0.000 ltr J52 1.46 -0.001 J53 1.23 0.001 J54 1.05 -0.006 J55 0.418 -0.007	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.066 0.000 0.776 0.000 0.000 0.000	0.066 0.000 1.109 0.964 0.883 0.347	0 01:22 0 00:00 0 01:10 0 01:11 0 01:11	5 0.25 0 1. 0 1. 1
tlet wn-Storag	JUNCTION JUNCTION JUNCTION JUNCTION OUTFALL STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE	0.25 0.57 0.63 0.66 0.72 1.50 1.60 0.92 0.79 0.06 0.01 0.02	1.90 1.56 1.58 1.64 1.50 2.98 1.86 1.83 0.25 0.07 0.08	65.69 64.74 64.68 64.67 64.67 64.67 64.78 64.67 64.78 64.65 100.07 100.08 100.07 100.08	0 01:10 0 01:20 0 01:29 0 01:29 0 00:00 0 03:00 0 01:21 0 03:10 0 01:52 0 01:52 0 01:52 0 01:52 0 01:52	1,90 1,53 1,55 1,58 1,63 1,50 2,98 1,86 1,50 2,98 1,86 1,50 0,25 0,07 0,08 0,07 0,08 0,09	0.198 0.757 J50 0.258 1.403 J51 0 0.000 ltr J52 1.46 -0.001 J53 1.23 0.001 J54 J55	JUNCTION JUNCTION JUNCTION JUNCTION	0.066 0.000 0.776 0.000 0.000	0.066 0.000 1.109 0.964 0.883	0 01:22 0 00:00 0 01:11 0 01:11 0 01:11	5 0.25 0 1. 0 1. 1
2 utlet A B C D G H I I	JUNCTION JUNCTION JUNCTION JUNCTION UNCTION OUTFALL STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE	0.25 0.57 0.63 0.66 0.72 1.50 1.60 0.92 0.79 0.06 0.01 0.02 0.01 0.02 0.02 0.02	1.90 1.56 1.58 1.64 1.50 2.98 1.86 1.83 0.25 0.07 0.08 0.07 0.08 0.09 0.08 0.09	65.69 64.74 64.68 64.67 64.67 64.08 65.20 64.67 64.78 64.65 100.07 100.08 100.09 100.08 100.09	0 01:10 0 01:20 0 01:29 0 01:29 0 00:00 0 01:29 0 00:00 0 01:29 0 01:21 0 01:20 0 01:21 0 01:52 0 01:53 0 02:11 0 01:54 0 01:55	1.90 1.53 1.55 1.58 1.58 1.50 2.98 1.60 2.98 1.80 0.25 0.07 0.08 0.07 0.08 0.07	0.198 0.757 350 0.258 1.403 351 0 0.000 ltr 352 1.46 -0.001 353 1.23 0.001 354 1.05 -0.006 355 0.418 -0.007 356 0.383 0.000 357 0.647 0.001 358	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.066 0.000 0.776 0.000 0.000 0.000	0.066 0.000 1.109 0.964 0.883 0.347 0.321	0 01:2: 0 00:00 0 01:10 0 01:11 0 01:11 0 01:11 0 01:11	5 0.25 0 1. 0 1. 1 1 0
	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION OUTFALL OUTFALL STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE	0.25 0.57 0.63 0.66 0.72 1.50 1.60 0.92 0.79 0.06 0.01 0.02 0.01 0.01 0.01 0.02 0.01 0.02 0.02	1.90 1.56 1.55 1.64 1.80 1.83 0.25 0.07 0.08 0.07 0.08 0.07 0.08 0.09 0.08	65.69 64.74 64.68 64.67 64.08 65.20 64.67 64.78 64.65 100.07 100.08 100.07 100.08 100.09 100.08	0 01:10 0 01:29 0 01:29 0 01:29 0 00:00 0 03:00 0 03:00 0 01:21 0 03:15 0 01:52 0 01:52 0 01:52 0 01:53 0 01:54 0 01:54	1,90 1,53 1,55 1,58 1,50 1,50 1,50 2,98 1,86 1,70 0,07 0,08 0,07 0,08 0,07 0,08 0,07 0,08 0,07 0,08 0,07 0,08 0,07 0,08	$\begin{array}{c} 0.198 \\ 350 \\ 350 \\ 350 \\ 351 \\ 0 \\ 352 \\ 1.46 \\ 353 \\ 353 \\ 353 \\ 353 \\ 354 \\ 355 \\ 0.418 \\ 355 \\ 0.418 \\ -0.007 \\ 355 \\ 0.418 \\ -0.007 \\ 355 \\ 0.418 \\ 0.383 \\ 0.000 \\ 357 \\ 0.647 \\ 0.001 \\ 357 \\ 0.647 \\ 0.001 \\ 358 \\ 0.75 \\ -0.002 \\ 359 \\ \end{array}$	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.066 0.000 0.776 0.000 0.000 0.000 0.000 0.000	0.066 0.000 1.109 0.964 0.883 0.347 0.321 0.470	0 01:2: 0 00:00 0 01:10 0 01:11 0 01:11 0 01:11 0 01:11 0 01:11	5 0.25 0 1. 0 1. 1 0 0 0.72
n-Storag	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION UUTFALL OUTFALL STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE	0.25 0.57 0.63 0.66 0.72 1.50 0.92 0.79 0.06 0.01 0.02 0.01 0.01 0.02 0.02 0.02 0.02	1.90 1.56 1.56 1.58 1.64 1.83 0.25 0.07 0.08 0.07 0.08 0.07 0.08 0.09 0.08 0.09	65.69 64.74 64.68 64.67 64.07 64.07 64.08 64.78 64.78 64.78 100.07 100.08 100.09 100.08 100.07	0 01:10 0 01:26 0 01:29 0 01:29 0 01:29 0 00:00 0 01:29 0 01:25 0 01:25 0 01:52 0 01:52 0 01:55 0 01:54 0 01:54 0 01:54 0 01:54	1,90 1,53 1,55 1,58 1,50 1,50 1,50 2,98 1,86 1,70 0,07 0,08 0,07 0,08 0,07 0,08 0,07 0,08 0,07 0,08 0,07 0,08 0,07 0,08	$\begin{array}{c} 0.198 & 0.757 \\ 350 \\ 0.258 & 1.403 \\ 351 \\ 0 \\ 0.000 \ 1 tr \\ 353 \\ 1.23 \\ 0.001 \\ 353 \\ 1.23 \\ 0.001 \\ 354 \\ 1.05 \\ -0.006 \\ 355 \\ 0.418 \\ -0.007 \\ 356 \\ 0.383 \\ 0.000 \\ 357 \\ 0.647 \\ 0.001 \\ 358 \\ 0.75 \\ -0.002 \\ 359 \\ 0.0284 \\ 0.010 \\ 360 \\ \end{array}$	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.066 0.000 0.776 0.000 0.000 0.000 0.000 0.000 0.506	0.066 0.000 1.109 0.964 0.883 0.347 0.347 0.321 0.470 0.576	0 01:2: 0 00:00 0 01:11 0 01:11 0 01:11 0 01:11 0 01:11 0 01:11 0 01:11	5 0.25 0 1. 0 1. 1 1 0 0.72 0
2 stlet A 3 2 2 5 4 4 5 5 4 4 5 5 4 5 5 5 4 5 5 5 5	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION UUTFALL OUTFALL STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE	0.25 0.57 0.63 0.66 0.72 1.50 0.92 0.79 0.06 0.01 0.02 0.01 0.01 0.02 0.02 0.02 0.02	1.90 1.56 1.56 1.58 1.64 1.83 0.25 0.07 0.08 0.07 0.08 0.07 0.08 0.09 0.08 0.09	65.69 64.74 64.68 64.67 64.07 64.07 64.08 64.78 64.78 64.78 100.07 100.08 100.09 100.08 100.07	0 01:10 0 01:26 0 01:29 0 01:29 0 01:29 0 00:00 0 01:29 0 01:25 0 01:25 0 01:52 0 01:52 0 01:55 0 01:54 0 01:54 0 01:54 0 01:54	1,90 1,53 1,55 1,58 1,50 1,50 1,50 2,98 1,86 1,70 0,07 0,08 0,07 0,08 0,07 0,08 0,07 0,08 0,07 0,08 0,07 0,08 0,07 0,08	0.198 0.757 30 0.258 1.403 352 1.46 -0.001 tr 353 1.23 0.001 354 1.05 -0.006 355 0.418 -0.007 356 0.383 0.000 357 0.647 0.001 356 0.647 0.001 358 0.647 0.001 359 0.6284 0.010 359 0.0284 0.010 359 0.028 0.0000 0.000 0.000 0.000 0.0000 0.000 0.000 0.000 0.0000000000	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.066 0.000 0.776 0.000 0.000 0.000 0.506 0.506	0.066 0.000 1.109 0.964 0.883 0.347 0.321 0.470 0.576 0.070	0 01:2: 0 00:00 0 01:10 0 01:11 0 01:11 0 01:11 0 01:11 0 01:11 0 01:11	5 0.25 0 1. 0 1 1 0 0 0 0.72 5
tlet wn-Storag	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION UUTFALL OUTFALL STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE	0.25 0.57 0.63 0.66 0.72 1.50 0.92 0.79 0.06 0.01 0.02 0.01 0.01 0.02 0.02 0.02 0.02	1.90 1.56 1.56 1.58 1.64 1.83 0.25 0.07 0.08 0.07 0.08 0.07 0.08 0.09 0.08 0.09	65.69 64.74 64.68 64.67 64.07 64.07 64.08 64.78 64.78 64.78 100.07 100.08 100.09 100.08 100.07	0 01:10 0 01:26 0 01:29 0 01:29 0 01:29 0 00:00 0 01:29 0 01:25 0 01:25 0 01:52 0 01:52 0 01:55 0 01:54 0 01:54 0 01:54 0 01:54	1,90 1,53 1,55 1,58 1,50 1,50 1,50 2,98 1,86 1,70 0,07 0,08 0,07 0,08 0,07 0,08 0,07 0,08 0,07 0,08 0,07 0,08 0,07 0,08	0.198 0.757 350 0.258 1.403 351 0 0.000 ltr 352 1.46 -0.001 353 1.23 0.001 354 1.05 -0.006 355 0.418 -0.007 356 0.383 0.000 357 0.647 0.001 358 0.75 -0.002 359 0.0284 0.010 359 0.0284 0.010 350 0.000 359 0.0284 0.010 350 0.000 350 0.000 359 0.0284 0.010 360 0.000 0.0000 0.000 0.000 0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.00000 0.00000 0.00000 0.000000 0.00000000	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.066 0.000 0.776 0.000 0.000 0.000 0.506 0.000 0.000	0.066 0.000 1.109 0.964 0.883 0.347 0.321 0.470 0.576 0.070 0.063	0 01:23 0 00:01 0 01:11 0 01:11 0 01:11 0 01:12 0 01:12 0 01:11 0 01:11 0 01:11 0 01:11 0 01:12	5 0.25 0 1. 0 1 1 0 0.72 0 5 4 0.18
tlet wn-Storag low Summa	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION UUTFALL OUTFALL STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE	0.25 0.57 0.63 0.66 0.72 1.50 1.60 0.92 0.79 0.06 0.01 0.02 0.01 0.02 0.02 0.02 0.03	1.90 1.56 1.58 1.64 1.60 2.98 1.86 1.83 0.25 0.07 0.08 0.07 0.08 0.07 0.08 0.07	65.69 64.74 64.68 64.67 64.67 64.67 64.08 65.20 64.67 100.08 100.07 100.08 100.07 100.08 100.09 100.08 100.01	0 01:10 0 01:22 0 01:29 0 01:29 0 01:29 0 00:29 0 00:20 0 01:29 0 01:22 0 01:22 0 01:22 0 01:22 0 01:52 0 01:53 0 02:12 0 01:55 0 02:20	1.90 1.53 1.55 1.58 1.63 1.50 2.98 1.86 1.86 1.80 0.25 0.07 0.08 0.07 0.08 0.09 0.08 0.07 0.08 0.07 0.08 0.07 0.08 0.07 0.08 0.07 0.08 0.07 0.08 0.07 0.08 0.07 0.08 0.07 0.08 0.09 0.08 0.09 0.08 0.09 0.08 0.09 0.08 0.09 0.08 0.09 0.08 0.09 0.08 0.09 0.09 0.08 0.09 0	$\begin{array}{c} 0.198 \\ 0.258 \\ 0.258 \\ 0.258 \\ 0.258 \\ 1.403 \\ 0.000 \ \mathrm{tr} \\ 352 \\ 1.46 \\ 0.001 \\ 353 \\ 0.011 \\ 354 \\ 0.355 \\ 0.418 \\ 0.355 \\ 0.418 \\ 0.355 \\ 0.418 \\ 0.355 \\ 0.418 \\ 0.355 \\ 0.418 \\ 0.355 \\ 0.418 \\ 0.006 \\ 0.355 \\ 0.258 \\ 0.000 \\ 0.002 \\ 0.002 \\ 0.002 \\ 0.002 \\ 0.002 \\ 0.000 \\ 0.0057 \\ 0.000 \\ 0.0057 \\ 0.000 \\ 0.00072 \\ 0.13 \\ 0.000 \\ 0.00072 \\ 0.000 \\ 0.00072 \\ 0.000 \\ 0.00072 \\ 0.3 \\ 0.00072 \\ 0.000 \\ 0.00072 \\ 0.000 \\ 0.00072 \\ 0.000 \\ 0.00072 \\ 0.000 \\$	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.066 0.000 0.776 0.000 0.000 0.000 0.506 0.000 0.000 0.000 0.000	0.066 0.000 1.109 0.964 0.883 0.347 0.321 0.470 0.576 0.070 0.063 0.252	0 01:23 0 00:01 0 01:11 0 01:11 0 01:11 0 01:12 0 01:11 0 01:11 0 01:11 0 01:11 0 01:11 0 01:12 0 01:22 0 01:22	5 0.25 0 1. 0 1 1 0 0.72 0 5 4 0.18 0
tlet wn-Storag low Summa	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION OUTFALL STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE	0.25 0.57 0.63 0.66 0.72 1.50 0.92 0.79 0.06 0.01 0.02 0.01 0.02 0.01 0.02 0.03	1.90 1.56 1.58 1.64 1.50 2.98 1.86 1.83 0.25 0.07 0.08 0.09 0.08 0.09 0.08 0.09 0.08 0.10	65.69 64.74 64.68 64.67 64.67 64.67 64.78 64.78 64.78 64.78 64.78 100.07 100.08 100.09 100.08 100.07 100.08 100.10	0 01:10 0 01:22 0 01:29 0 01:29 0 01:29 0 00:00 0 01:29 0 01:22 0 01:22 0 01:22 0 01:22 0 01:25 0 01:55 0 01:55 0 01:55 0 02:12 0 02:20 0 02:20	eral	$\begin{array}{c} 0.198 \\ 350 \\ 350 \\ 350 \\ 0.258 \\ 1.40 \\ 351 \\ 0 \\ 0.000 \ \mathrm{ltr} \\ 352 \\ 1.46 \\ -0.001 \\ 353 \\ 0.353 \\ 0.001 \\ 354 \\ 0.355 \\ 0.418 \\ 0.355 \\ 0.418 \\ 0.355 \\ 0.418 \\ 0.355 \\ 0.418 \\ 0.355 \\ 0.418 \\ 0.355 \\ 0.418 \\ 0.006 \\ 0.355 \\ 0.364 \\ 0.000 \\ 355 \\ 0.647 \\ 0.001 \\ 356 \\ 0.364 \\ 0.000 \\ 357 \\ 0.647 \\ 0.001 \\ 356 \\ 0.002 \\ 359 \\ 0.0284 \\ 0.000 \\ 359 \\ 0.0284 \\ 0.000 \\ 359 \\ 0.0284 \\ 0.000 \\ 359 \\ 0.002 \\ 359 \\ 0.00072 \\ 0.36 \\ 0.00072 \\ 1.3 \\ 363 \\ 0.402 \\ 0.229 \\ 364 \\ \end{array}$	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.066 0.000 0.000 0.000 0.000 0.000 0.506 0.000 0.000 0.143 0.000	0.066 0.000 1.109 0.964 0.883 0.347 0.321 0.470 0.576 0.070 0.063 0.252 0.004	0 01:23 0 00:01 0 01:11 0 01:11 0 01:12 0 01:13 0 01:13 0 01:14 0 0	5 0.25 0 1. 0 1. 0 1 1 0 0 0.72 0 5 4 0.18 0 7 0.30
n-Storag ********* ow Summa ********* Flow	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION OUTFALL STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE	0.25 0.57 0.63 0.66 0.72 1.60 0.92 0.79 0.06 0.01 0.02 0.01 0.02 0.02 0.03	1.90 1.56 1.58 1.58 1.64 1.80 2.98 1.86 1.83 0.07 0.08 0.09 0.08 0.07 0.08 0.10 0.08 0.10	65.69 64.74 64.62 64.67 64.67 64.67 64.70 64.70 64.70 64.70 100.08 100.07 100.08 100.07 100.08 100.07 100.08 100.10	0 01:10 0 01:22 0 01:22 0 01:23 0 00:02 0 01:23 0 00:02 0 01:22 0 01:22 0 01:22 0 01:22 0 01:22 0 01:25 0 01:55 0 01:55 0 02:11 0 01:55 0 02:20	<pre>1.90</pre>	$\begin{array}{c} 0.198 \\ 350 \\ 350 \\ 350 \\ 0.258 \\ 1.40 \\ 351 \\ 0 \\ 0.000 \ 1 {\rm tr} \\ 352 \\ 1.46 \\ -0.001 \\ 353 \\ 0.353 \\ 0.001 \\ 354 \\ 0.355 \\ 0.418 \\ -0.007 \\ 355 \\ 0.418 \\ 0.353 \\ 0.000 \\ 355 \\ 0.418 \\ 0.363 \\ 0.000 \\ 355 \\ 0.647 \\ 0.001 \\ 356 \\ 0.383 \\ 0.000 \\ 357 \\ 0.647 \\ 0.001 \\ 358 \\ 0.75 \\ -0.002 \\ 359 \\ 0.0284 \\ 0.000 \\ 359 \\ 0.0284 \\ 0.000 \\ 359 \\ 0.0284 \\ 0.000 \\ 359 \\ 0.00072 \\ 1.3 \\ 360 \\ 0.00072 \\ 1.3 \\ 363 \\ 0.402 \\ -0.229 \\ 364 \\ 0.00203 \\ 1.20 \\ 365 \\ \end{array}$	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.066 0.000 0.776 0.000 0.000 0.000 0.000 0.506 0.000 0.000 0.143 0.000 0.143	0.066 0.000 1.109 0.964 0.883 0.347 0.321 0.470 0.576 0.070 0.063 0.252 0.004 0.119	0 01:23 0 00:01 0 01:11 0 01:11 0 01:12 0 01:12 0 01:12 0 01:11 0 01:11 0 01:11 0 01:12 0 01:22 0 01:22 0 01:23 0 01:24	5 0.25 0 1. 0 1. 0 1 1 0 0 0.72 0 5 4 0.18 0 7 0.30 5
Storag	JUNCTION JUNCTION JUNCTION JUNCTION OUTFALL STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE	0.25 0.57 0.63 0.66 0.72 1.50 0.92 0.79 0.06 0.01 0.02 0.01 0.02 0.01 0.02 0.03 0.03 0.03	1.90 1.56 1.55 1.58 1.64 1.80 2.98 1.86 1.83 0.07 0.08 0.09 0.08 0.07 0.08 0.10 0.08 0.10	65.69 64.74 64.62 64.67 64.67 64.67 64.70 64.70 64.70 64.70 100.08 100.07 100.08 100.07 100.08 100.07 100.08 100.10	0 01:10 0 01:22 0 01:22 0 01:23 0 01:23 0 01:23 0 01:23 0 01:23 0 01:23 0 01:23 0 01:23 0 01:23 0 01:25 0 01:55 0 01:55 0 01:55 0 02:20 Variable Construction Lat Max Innence Vo	eral	$\begin{array}{ccccccc} 0.198 & 0.757 \\ 350 \\ 0.258 & 1.403 \\ 351 \\ 0 & 0.000 \ 1 {\rm tr} \\ 352 \\ 1.46 & -0.001 \\ 353 \\ 0.353 \\ 0.354 \\ 1.05 & -0.006 \\ 355 \\ 0.418 & -0.007 \\ 355 \\ 0.418 & -0.007 \\ 355 \\ 0.418 & 0.000 \\ 355 \\ 0.383 & 0.000 \\ 357 \\ 0.647 & 0.001 \\ 356 \\ 0.383 & 0.000 \\ 357 \\ 356 \\ 0.284 & 0.010 \\ 359 \\ 0.0284 & 0.010 \\ 359 \\ 0.0284 & 0.010 \\ 359 \\ 0.0284 & 0.010 \\ 359 \\ 0.00672 & 2.32 \\ 361 \\ 0.00672 & 1.3 \\ 362 \\ 0.000472 & 1.3 \\ 363 \\ 0.402 & -0.229 \\ 364 \\ 0.00203 & 1.20 \\ 366 \\ 0 & 0.000 \ 1 {\rm tr} \\ 366 \\ \end{array}$	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.066 0.000 0.776 0.000 0.000 0.000 0.000 0.506 0.000 0.000 0.143 0.000 0.143 0.000	0.066 0.000 1.109 0.964 0.883 0.347 0.321 0.470 0.576 0.070 0.063 0.252 0.004 0.119 0.012	0 01:23 0 00:01 0 01:11 0 01:11 0 01:12 0 01:13 0 01:13 0 01:13 0 01:14 0 01:14 0 01:14 0 01:14 0 01:14 0 01:14 0 01:25 0 01:14 0 0	5 0.25 0 1. 0 1. 1 0 0 0.72 0 5 4 0.18 0 7 0.30 5 0
-Storag ******* * Summa ****** Flow alance Error ent	JUNCTION JUNCTION JUNCTION JUNCTION OUTFALL STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE	0.25 0.57 0.63 0.66 0.72 1.60 0.92 0.79 0.06 0.01 0.02 0.01 0.02 0.02 0.03	1.90 1.56 1.58 1.58 1.64 1.80 2.98 1.86 1.83 0.07 0.08 0.09 0.08 0.07 0.08 0.07 0.08 0.10 0.08 0.10	65.69 64.74 64.68 64.67 64.69 64.67 64.70 64.70 64.70 64.70 100.08 100.07 100.08 100.07 100.08 100.07 100.08 100.010	0 01:10 0 01:22 0 01:23 0 01:25 0 01:55 0 01:55 0 01:55 0 01:55 0 01:55 0 01:55 0 02:120 0 01:23 0 02:20 Lat Max In ence VC :min 10^6	eral	$\begin{array}{c} 0.198 \\ 0.258 \\ 350 \\ 0.258 \\ 1.403 \\ 351 \\ 0 \\ 0.000 \ 1 tr \\ 352 \\ 1.46 \\ 0.000 \ 1 tr \\ 353 \\ 0.001 \\ 354 \\ 0.355 \\ 0.418 \\ 0.355 \\ 0.418 \\ 0.355 \\ 0.418 \\ 0.355 \\ 0.418 \\ 0.000 \\ 355 \\ 0.418 \\ 0.361 \\ 0.361 \\ 0.361 \\ 0.000 \\ 0.000 \\ 356 \\ 0.000 \ 1 tr \\ 360 \\ 360 \\ 0.000 \ 1 tr \\ 360 \\ 0.000 \ 1 tr \\ 360 \\ 0.000 \ 1 tr \\ 360 \\ 360 \\ 0.000 \ 1 tr \\ 360 \\ 360 \\ 0.000 \ 1 tr \\ 360 \\ 360 \\ 0.000 \ 1 tr \\ 360 \\ 360 \\ 0.000 \ 1 tr \\ 360 \\ 360 \\ 0.000 \ 1 tr \\ 360 \\ 360 \\ 360 \\ 0.000 \ 1 tr \\ 360 \\ 360 \\ 360 \\ 0.000 \ 1 tr \\ 360 \\ 360 \\ 360 \\ 0.000 \ 1 tr \\ 360 \\$	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.066 0.000 0.776 0.000 0.000 0.000 0.000 0.506 0.000 0.000 0.143 0.000 0.082 0.082	0.066 0.000 1.109 0.964 0.883 0.347 0.321 0.470 0.576 0.070 0.063 0.252 0.004 0.119 0.012 0.000	0 01:23 0 00:01 0 01:11 0 01:11 0 01:12 0 01:13 0 01:13 0 01:14 0 01:14 0 01:14 0 01:14 0 01:14 0 01:14 0 01:14 0 01:12 0 01:23 0 01:24 0 01:23 0 01:23 0 01:23 0 01:24 0 01:23 0 01:23 0 01:24 0 01:23 0 01:23 0 01:24 0 01:23 0 01:23 0 01:23 0 01:24 0 01:23 0 01:24 0 01:23 0 01:24 0 01:24 0 01:24 0 01:24 0 01:24 0 01:25 0 00:25 0 0	5 0.25 0 1. 0 1. 1 0 0 0 0.72 0 5 7 0.30 5 0 1
-Storag ******** Summa Summa Flow alance Error ent	JUNCTION JUNCTION JUNCTION JUNCTION OUTFALL STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE	0.25 0.57 0.57 1.60 0.92 0.92 0.06 0.01 0.02 0.01 0.02 0.01 0.02 0.03 0.02 0.03 Maximum Lateral Inflow CMS	1.90 1.56 1.58 1.58 1.64 1.80 2.98 1.86 1.83 0.07 0.08 0.07 0.08 0.07 0.08 0.07 0.08 0.10 0.08 0.10 0.08 0.10	65.69 64.74 64.68 64.67 64.67 64.67 64.70 64.70 64.70 64.70 100.08 100.07 100.08 100.07 100.08 100.07 100.08 100.07 100.08 100.07	0 01:10 0 01:22 0 01:23 0 01:25 0 01:55 0 02:20	eral	$\begin{array}{cccccccc} 0.198 & 0.757 \\ 350 \\ 0.258 & 1.403 \\ 351 \\ 0 & 0.000 \ 1 {\rm tr} \\ 352 \\ 1.46 & -0.001 \\ 353 \\ 0.233 & 0.001 \\ 354 \\ 1.05 & -0.006 \\ 355 \\ 0.418 & -0.007 \\ 355 \\ 0.418 & -0.007 \\ 355 \\ 0.418 & 0.000 \\ 355 \\ 0.418 & -0.001 \\ 356 \\ 0.383 & 0.000 \\ 357 \\ 0.647 & 0.001 \\ 356 \\ 0.383 & 0.000 \\ 359 \\ 0.0284 & 0.010 \\ 359 \\ 0.0284 & 0.010 \\ 359 \\ 0.0284 & 0.010 \\ 359 \\ 0.00672 & 2.32 \\ 350 \\ 350 \\ 0.00072 & 1.3 \\ 360 \\ 0.000472 & 1.3 \\ 360 \\ 0.000472 & 1.3 \\ 363 \\ 0.000012 & 1.20 \\ 364 \\ 0.0000 \ 1 {\rm tr} \\ 365 \\ 0 & 0.000 \ 1 {\rm tr} \\ 368 \\ 367 \\ 0 & 0.000 \ 1 {\rm tr} \\ 368 \\ \end{array}$	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.066 0.000 0.776 0.000 0.000 0.000 0.000 0.506 0.000 0.000 0.143 0.000 0.082 0.000 0.000	0.066 0.000 1.109 0.964 0.883 0.347 0.321 0.470 0.576 0.070 0.063 0.252 0.004 0.119 0.012 0.001	0 01:23 0 00:01 0 01:11 0 01:11 0 01:12 0 01:12 0 01:12 0 01:12 0 01:11 0 01:11 0 01:12 0 01:22 0 01:23 0 01:24 0 01:22 0 01:23 0 0	5 0.22 0 1. 0 1. 0 0 1. 0 0 0.72 0 5 5 7 0.30 5 5 0 1 0
-Storag	JUNCTION JUNCTION JUNCTION JUNCTION OUTFALL STORAGE ST	0.25 0.57 0.53 0.66 0.72 1.50 1.60 0.92 0.79 0.06 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.03 0.03 Maximum Lateral Inflow CMS	1.90 1.56 1.58 1.58 1.64 1.86 1.88 1.86 1.83 0.07 0.08 0.07 0.08 0.07 0.08 0.07 0.08 0.07 0.08 0.10 0.08 0.10 0.08 0.10	65.69 64.74 64.68 64.67 64.67 64.67 64.70 64.70 64.70 64.73 64.73 100.07 100.08 100.07 100.08 100.07 100.08 100.07 100.08 100.07 100.08 100.07	0 01:10 0 01:25 0 01:55 0 0	<pre>1.90</pre>	$\begin{array}{ccccccc} 0.198 & 0.757 \\ 350 \\ 0.258 & 1.403 \\ 351 \\ 0 & 0.000 \ 1 {\rm tr} \\ 352 \\ 1.46 & -0.001 \\ 353 \\ 1.23 & 0.001 \\ 354 \\ 1.05 & -0.006 \\ 355 \\ 0.418 & -0.007 \\ 355 \\ 0.418 & -0.007 \\ 355 \\ 0.418 & -0.007 \\ 356 \\ 0.383 & 0.000 \\ 357 \\ 0.647 & 0.001 \\ 356 \\ 0.383 & 0.000 \\ 357 \\ 0.647 & 0.001 \\ 358 \\ 0.75 & -0.002 \\ 359 \\ 0.0284 & 0.010 \\ 359 \\ 0.0284 & 0.010 \\ 358 \\ 0.00672 & 2.32 \\ 356 \\ 0.00072 & 1.3 \\ 360 \\ 0.0000472 & 1.3 \\ 363 \\ 0.402 & -0.229 \\ 364 \\ 0.00001r \\ 365 \\ 0 & 0.000 \ 1 {\rm tr} \\ 369 \\ 0 & 0.000 \ 1 {\rm tr} \\ 369 \\ 0 & 0.000 \ 1 {\rm tr} \\ 369 \\ \end{array}$	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.066 0.000 0.776 0.000 0.000 0.000 0.000 0.506 0.000 0.000 0.143 0.000 0.143 0.000 0.082 0.000 0.000	0.066 0.000 1.109 0.964 0.347 0.321 0.470 0.576 0.070 0.063 0.252 0.004 0.119 0.012 0.000 0.143 0.000	0 01:23 0 00:01 0 01:11 0 01:11 0 01:12 0 01:13 0 01:13 0 01:14 0 01:14 0 01:14 0 01:14 0 01:14 0 01:14 0 01:22 0 01:23 0 00:23 0 00:23 0 00:23 0 00:00 0 0	5 0.25 0 1. 0 1. 0 0 1. 0 0 0.72 0 5 0 1 7 0.30 5 0 1 0 0 0
n-Storag .ow Summa Flow Balance Error :cent	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION UUTFALL OUTFALL STORAGE S	0.25 0.57 0.63 0.66 0.62 0.92 1.50 0.92 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.03 0.03 Maximum Lateral Inflow CMS	1.90 1.56 1.56 1.58 1.64 1.83 0.25 0.07 0.08 0.07 0.08 0.07 0.08 0.07 0.08 0.07 0.08 0.07 0.08 0.07 0.08 0.10 Maximum Total Inflow CMS	65.69 64.74 64.68 64.67 64.68 65.20 64.67 64.08 64.65 100.07 100.08 100.07 100.08 100.08 100.08 100.08 100.08 100.01 100.08 100.01 100.08 100.01 100.02 100.02 Time of Occurred days hr 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.0	0 01:10 0 01:25 0 01:25 0 01:25 0 01:25 0 00:05 0 01:25 0 01:25 0 01:25 0 01:25 0 01:25 0 01:25 0 01:55 0 01:5	eral flow eral flow eral flow	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.066 0.000 0.776 0.000 0.000 0.000 0.000 0.000 0.000 0.143 0.000 0.143 0.000 0.082 0.000 0.000 0.000	0.066 0.000 1.109 0.964 0.347 0.321 0.470 0.576 0.070 0.063 0.252 0.004 0.119 0.012 0.000 0.143 0.000	0 01:23 0 00:01 0 01:11 0 01:11 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:22 0 01:23 0 00:23 0 00:25 0 0	5 0.22 0 1. 0 1. 0 0 1. 0 0 0.72 0 5 5 0 1 7 0.30 5 0 1 0 0 0 0 0 0
n-Storag	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION UUTFALL OUTFALL STORAGE S	0.25 0.57 0.63 0.66 0.72 1.50 0.92 0.79 0.06 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.03 0.03 Maximum Lateral Inflow CMS 0.000 0.113 0.000	1.90 1.56 1.56 1.58 1.83 0.25 0.07 0.08 0.09 0.08 0.09 0.08 0.09 0.09 0.0000000000	65.69 64.74 64.68 64.67 64.08 65.20 64.67 64.08 64.65 100.07 100.08 100.07 100.08 100.09 100.08 100.09 100.08 100.01 100.08 100.01 100.01 100.02 100.01 00.0100.01 00.00000000	0 01:10 0 01:25 0 01:55 0 0	eral flow flow eral flow	0.198 0.757 350 0.258 1.403 351 0 0.000 ltr 353 1.23 0.001 353 0.418 -0.001 355 -0.006 355 -0.006 355 0.418 0.3647 0.001 359 0.002 359 0.000 0.3647 0.001 359 0.00072 0.32 361 0.057 362 0.057 363 -0.057 363 0.000 363 0.000 363 0.000 ltr 366 0 11 -1.038 367 0 0 0.000 ltr 368 0 0 0.000 ltr 368 0 0 0.000 ltr 369 0 0 0.000 ltr	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.066 0.000 0.776 0.000 0.000 0.000 0.000 0.506 0.000 0.000 0.143 0.000 0.082 0.000 0.000 0.000 0.000 0.000	0.066 0.000 1.109 0.964 0.347 0.321 0.470 0.576 0.070 0.063 0.252 0.004 0.119 0.012 0.000 0.143 0.000 0.000	0 01:23 0 00:01 0 01:11 0 01:11 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:22 0 01:23 0 00:01 0 00:01 0 00:23 0 00:01 0 00:01 0 00:23 0 00:01 0 0	5 0.22 0 1. 0 1. 0 0 1. 0 0 0.72 0 5 5 0 1 0 0.30 5 0 1 0 0 0 0 0 0
n-Storag ov Summa Flow Balance Error 0.430 0.542 0.027	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION UUTFALL OUTFALL STORAGE S	0.25 0.57 0.63 0.66 0.62 0.92 1.50 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.03 0.03 Maximum Lateral Inflow CMS 0.000 0.113 0.000	1.90 1.56 1.56 1.58 1.81 0.298 1.83 0.25 0.07 0.08 0.022 0.022 0.022 0.02200000000000	65.69 64.74 64.68 64.67 64.68 65.20 64.67 64.08 64.65 100.07 100.08 100.07 100.08 100.09 100.08 100.08 100.01 100.08 100.01 100.08 100.01 100.08 100.01 100.02 100.02 100.01 0 0 0 0 0 0 0 0 0 0	0 01:10 0 01:25 0 01:55 0 0	eral flow flow eral flow flow eral flow	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	JUNCTION JUNCTION	0.066 0.000 0.776 0.000 0.000 0.000 0.000 0.000 0.000 0.143 0.000 0.082 0.000 0.000 0.000 0.000 0.000 0.000	0.066 0.000 1.109 0.964 0.347 0.321 0.470 0.576 0.070 0.063 0.252 0.004 0.119 0.012 0.000 0.143 0.000 0.000	0 01:23 0 00:01 0 01:11 0 01:11 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:22 0 01:23 0 00:01 0 00:01 0 00:23 0 00:01 0 0	5 0.25 0 1. 0 1. 1 0 0.72 0 0.72 0 5 0. 7 0.30 5 0 1 0 0 0. 0 0 0. 0 0 0. 0 0 0.
tlet wn-Storag low Summa Flow Balance Error rcent 0.430 0.542	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION UUTFALL OUTFALL STORAGE S	0.25 0.57 0.63 0.66 0.72 1.50 0.92 0.79 0.06 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.03 0.03 Maximum Lateral Inflow CMS 0.000 0.113 0.000 0.000	1.90 1.56 1.56 1.58 1.83 0.298 1.83 0.29 0.07 0.08 0.07 0.029 0.010 0.029 0.010 0.029 0.010 0.029 0.0210 0.0200000000	65.69 64.74 64.68 64.67 64.68 65.20 64.67 64.08 64.67 100.08 100.07 100.08 100.09 100.08 100.09 100.08 100.01 100.08 100.01 100.01 100.08 100.01 100.01 00.00000000	0 01:10 0 01:25 0 01:55 0 0	eral fflow 1.27 0.227 0 0 0 0 0 0 0 0 0 0 0 0 0	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	JUNCTION JUNCTION	0.066 0.000 0.776 0.000 0.000 0.000 0.000 0.000 0.143 0.000 0.143 0.000 0.082 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.066 0.000 1.109 0.964 0.347 0.321 0.470 0.576 0.070 0.063 0.252 0.004 0.119 0.012 0.000 0.143 0.000 0.000 0.000	0 01:23 0 00:01 0 01:11 0 01:11 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:22 0 01:23 0 01:22 0 01:23 0 01:22 0 01:23 0 00:01 0 0	5 0.22 0 1. 0 1. 1 0 0 0 0.72 0 5 5 0 1 0.36 5 0 1 0 0 0 0 0 0 0 0 0
n-Storag ov Summa Flow Balance Error 0.430 0.542 0.027 -0.072	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION UUTFALL OUTFALL STORAGE S	0.25 0.57 0.63 0.66 0.62 0.92 1.50 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.03 0.03 0.03 Maximum Lateral Inflow CMS 0.000 0.113 0.000 0.000 0.000	1.90 1.56 1.56 1.58 1.81 0.298 1.83 0.25 0.07 0.08 0.07 0.029 0.013 0.029 0.03 0.029 0.03113 0.122 0.034 0.034 0.034 0.034 0.034 0.032 0.034	65.69 64.74 64.68 64.67 64.68 65.20 64.67 64.08 64.67 100.08 100.07 100.08 100.09 100.08 100.08 100.09 100.08 100.01 100.08 100.01 100.08 100.01 100.08 100.01 00.00 00 00 00 00 00 00 00 00 00 00 00	0 01:10 0 01:25 0 01:55 0 0	<pre>1 .90 . 1.53 . 1.55 . 1.58 . 1.63 . 1.63 . 2.98 . 1.86 . 0.07 . 0.08 . 0.07 . 0.08 . 0.08 . 0.08 . 0.08 . 0.08 . 0.08 . 0.10 . 0.8</pre>	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	JUNCTION JUNCTION	0.066 0.000 0.776 0.000 0.000 0.000 0.000 0.000 0.000 0.143 0.000 0.082 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.066 0.000 1.109 0.964 0.883 0.347 0.321 0.470 0.576 0.070 0.063 0.252 0.004 0.119 0.012 0.000 0.143 0.000 0.000 0.000 0.000	0 01:23 0 00:01 0 01:11 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:22 0 01:22 0 01:23 0 01:22 0 01:23 0 01:22 0 01:23 0 01:23 0 01:23 0 01:23 0 01:23 0 01:23 0 01:23 0 01:23 0 01:23 0 01:12 0 01:00 0 01:12 0 00:00 0 0	5 0.25 0 0 1. 0 1 0 0 0 0 5 5 4 0.18 0 7 0.30 5 0 1 0 0 0 0 0 0 0 0 1
	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION UUTFALL OUTFALL STORAGE S	0.25 0.57 0.63 0.66 0.72 1.50 0.92 0.79 0.06 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.03 0.03 Maximum Lateral Inflow CMS 0.000 0.113 0.000 0.000 0.000	1.90 1.56 1.56 1.58 1.83 0.298 1.83 0.27 0.08 0.07 0.09 0.029 0.013 0.022 0.034 0.122 0.034	65.69 64.74 64.68 64.67 64.68 65.20 64.67 64.08 100.07 100.08 100.07 100.08 100.09 100.08 100.08 100.09 100.08 100.01 100.08 100.01 100.01 100.08 100.01 00.00 00.01 00.00000000	0 01:10 0 01:25 0 01:55 0 0	<pre>1 .90 . 1.53 . 1.55 . 1.58 . 1.63 . 1.63 . 2.98 . 1.86 . 0.07 . 0.08 . 0.07 . 0.08 . 0.08 . 0.08 . 0.08 . 0.08 . 0.08 . 0.08 . 0.10 . 0.8 . 0.1</pre>	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	JUNCTION JUNCTION		0.066 0.000 1.109 0.964 0.883 0.347 0.321 0.470 0.576 0.070 0.063 0.252 0.004 0.119 0.012 0.001 0.143 0.000 0.000 0.000 0.000 0.000 0.000	0 01:23 0 00:01 0 01:11 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:22 0 01:22 0 01:23 0 01:12 0 01:12 0 01:12 0 00:01 0 0	5 0.25 0 0 1. 0 1 1 0 0 0 5 5 4 0.18 0 7 0.30 5 0 1 0 0 0 0 0 0 0 0 1 0 0 0 0 0 0 0
-Storag w Summa w Summa w Summa alance Error o.430 0.542 0.027 0.072 0.007 .358 .096	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION UUTFALL OUTFALL STORAGE S	0.25 0.57 0.63 0.66 0.72 1.50 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.03 0.03 0.02 0.03 0.03 0.03 0.03	1.90 1.56 1.56 1.58 1.81 0.298 1.83 0.25 0.07 0.08 0.07 0.029 0.013 0.022 0.034 0.122 0.0344 0.0344 0.0344 0.0344 0.0344 0.03444 0.03444 0.03444 0.03444 0.03444 0.03444 0.034444 0.034444 0.034444 0.034444 0.034444 0.034444 0.0344444 0.034444444444	65.69 64.74 64.68 64.67 64.68 65.20 64.67 64.08 64.67 100.08 100.07 100.08 100.08 100.08 100.08 100.08 100.08 100.08 100.01 100.08 100.01 100.08 100.01 00.0	0 01:10 0 01:25 0 01:55 0 01:55 1 00:55 0 01:55 1 00:55 0 01:55 1 00:55 0 01:55 1 00:55 0 01:55 1 00:55 0 01:55 1 00:55 1 0	<pre>1.90 .1.93 .1.55 .1.58 .1.63 .1.63 .1.63 .2.98 .1.8607080708080808080808080801080801080801080800</pre>	0.198 0.757 350 0.258 1.403 351 0 0.000 ltr 352 1.46 -0.001 353 0.233 0.001 355 -0.006 355 0.418 -0.007 355 0.418 -0.007 356 0.333 0.000 357 0.002 359 0.0284 0.010 360 0.00672 2.32 359 0.0284 0.010 360 0.00672 1.3 361 0.0057 362 0.000472 1.3 363 0.402 -0.229 364 0.0000 ltr 365 0 0.000 ltr 368 0 0.000 ltr 369 0 0.000 ltr 370 0 0.000 ltr 371 0 0.000 ltr 373 0 0.000 ltr 373 0 0.000 ltr 374 375 0 0.000 ltr 373 0 0.000 ltr 373 0 0.000 ltr 374 0 0.000 ltr 374 0 0.000 ltr 375 0 0.000 ltr 375 0 0.000 ltr 375 0 0.000 ltr 375 0 0.000 ltr 375 0 0.000 ltr 375 0 0.000 ltr 374 375 0 0.000 ltr 375 0 0.000 ltr 3	JUNCTION JUNCTION		0.066 0.000 1.109 0.964 0.883 0.347 0.321 0.470 0.576 0.070 0.063 0.252 0.004 0.119 0.012 0.001 0.143 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.501 0.514 0.001 0.514	0 01:23 0 00:01 0 01:11 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:22 0 00:01 0 0	5 0.25 0 0 1. 0 1 1 0 0 0 5 5 4 0.18 0 7 0.30 5 0 1 0 0 0 0 0 0 0 0 0 0 0 1 0 0 1 0 0 1 0 0 1 1 0 0 0 0 1. 0 0 0 1. 0 0 0 1. 0 0 0 1. 0 0 0 1. 0 0 0 0
-Storag w Summa Flow alance Error 0.430 0.0542 0.027 0.072 -0.007 .358	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION UUTFALL OUTFALL STORAGE S	0.25 0.57 0.63 0.66 0.72 1.50 0.92 0.79 0.06 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.03 0.03 Maximum Lateral Inflow CMS 0.000 0.113 0.000 0.000 0.000	1.90 1.56 1.56 1.58 1.83 0.298 1.83 0.27 0.08 0.07 0.09 0.029 0.013 0.022 0.034 0.122 0.034	65.69 64.74 64.68 64.67 64.68 65.20 64.67 64.08 100.07 100.08 100.07 100.08 100.09 100.08 100.08 100.09 100.08 100.01 100.08 100.01 100.01 100.08 100.01 00.00 00.01 00.00000000	0 01:10 0 01:25 0 01:55 0 01:55 1 00:55 0 01:55 1 00:55 0 01:55 1 00:55 0 01:55 1 00:55 0 01:55 1 00:55 0 01:55 1 00:55 1 0	<pre>1 .90 . 1.53 . 1.55 . 1.58 . 1.63 . 1.63 . 2.98 . 1.86 . 0.07 . 0.08 . 0.07 . 0.08 . 0.08 . 0.08 . 0.08 . 0.08 . 0.08 . 0.08 . 0.10 . 0.8 . 0.1</pre>	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	JUNCTION JUNCTION		0.066 0.000 1.109 0.964 0.883 0.347 0.321 0.470 0.576 0.070 0.063 0.252 0.004 0.119 0.012 0.001 0.143 0.000 0.000 0.000 0.000 0.000 0.501 0.514 0.000	0 01:23 0 00:01 0 01:11 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:22 0 00:00 0 0	5 0.22 0 1. 0 1. 0 0 1. 0 0 0.72 0 5 0. 1 0 0.30 5 0 0.30 0 0 0. 0 0 0 0. 1 0 0 0. 1 0 0 0. 1 1

STM102	0.175	JUNCTION	0.000	0.059	0	01:04	0
STM102A	0.645	JUNCTION	0.000	0.647	0	01:11	0
STM104 5.62 0	.599	JUNCTION	0.000	0.647	0	01:11	0
STM105	0.533	JUNCTION	0.000	0.593	0	01:11	0
STM106A	.595	JUNCTION	0.131	0.659	0	01:10	0.175
STM106B 5.75 0	0.318	JUNCTION	0.000	0.627	0	01:10	0
STM107 6.28	.196	JUNCTION	0.000	0.698	0	01:08	0
STM108	0.611	JUNCTION	0.000	1.546	0	01:11	0
STM109 4.91 (.376	JUNCTION	0.138	2.113	0	01:10	0.189
STM110 1.17 (0.106	JUNCTION	0.000	0.380	0	01:06	0
STM111 1.17 (.160	JUNCTION	0.000	0.382	0	01:06	0
STM111A 0.293	0.193	JUNCTION	0.000	0.141	0	01:05	0
STM112 3.7 0.	123	JUNCTION	0.086	1.657	0	01:10	0.135
STM113 2.75 (0.419	JUNCTION	0.374	1.400	0	01:10	0.535
STM114 1.14 (0.036	JUNCTION	0.451	0.549	0	01:09	0.621
STM115 0.513 -	0.146	JUNCTION	0.119	0.229	0	01:22	0.174
STM116	1.104	JUNCTION	0.072	0.346	0	01:03	0.0695
STM116_STA		JUNCTION	0.000	0.552	0	01:13	0
STM117 1.09 -0	.047	JUNCTION	0.000	0.563	0	01:11	0
STM118 1.09 -0	.376	JUNCTION	0.000	0.801	0	01:09	0
STM119	.465	JUNCTION	0.796	0.813	0	01:09	1.1
STM121 1.15 (0.064	JUNCTION	0.000	0.431	0	01:11	0
STM122 0.968	0.108	JUNCTION	0.000	0.297	0	01:10	0
STMA 0.276	0.079	JUNCTION	0.000	0.155	0	01:06	0
STMAA	0.026	JUNCTION	0.000	0.095	0	01:14	0
STMB	0.119	JUNCTION	0.000	0.223	0	01:05	0
STMBB	-0.061	JUNCTION	0.000	0.241	0	01:14	0
STMC 0.752	0.239	JUNCTION	0.000	0.296	0	01:38	0
STMCC 0.692	0.194	JUNCTION	0.000	0.261	0	01:16	0
STM-CCN1	0.051	JUNCTION	0.000	0.384	0	01:06	0

STM-CCN2		JUNCTION	0.193	0.197	0	01:10	0.27
0.37	0.467						
STMD		JUNCTION	0.000	0.283	0	01:16	
.827	0.458						
STMDD		JUNCTION	0.027	0.290	0	01:16	0.087
0.753	0.388						
STMFF		JUNCTION	0.185	0.445	0	01:15	0.43
2.36	0.381						
STMGG		JUNCTION	0.328	0.657	0	01:13	0.47
3.63	0.208						
Canal Out	let	OUTFALL	0.000	0.444	0	00:00	
1.67 -	0.000						
J28		OUTFALL	0.000	0.725	0	01:11	
5.54	0.000						
BASIN1		STORAGE	0.151	1.921	0	01:08	0.19
2.59 -	0.024						
BASIN2		STORAGE	0.000	3.418	0	01:11	
4.02	2.954						
Great-Law	n-Storage	STORAGE	0.000	0.845	0	01:29	
	0.350						
S-BLDG-A		STORAGE	0.126	0.126	0	01:10	0.17
0.179	0.005						
S-BLDG-B		STORAGE	0.180	0.180	0	01:10	0.25
0.255	0.005						
S-BLDG-C		STORAGE	0.148	0.148	0	01:10	0.2
0.21	0.005						
S-BLDG-D		STORAGE	0.068	0.068	0	01:10	0.09
0.097	0.005						
S-BLDG-G		STORAGE	0.120	0.120	0	01:10	0.17
0.171	0.005						
S-BLDG-H		STORAGE	0.184	0.184	0	01:10	0.26
	0.005						
S-BLDG-I		STORAGE	0.112	0.112	0	01:10	0.15
0.159	0.005						
S-BLDG-J		STORAGE	0.068	0.068	0	01:10	0.096
0.0964	0.005				-		
S-BLDG-K		STORAGE	0 123	0.123	0	01:10	0.17
		01010401	0.120	0.120			0.17

Surcharging occurs when water rises above the top of the highest conduit.

Node	Туре	Hours Surcharged	Max. Height Above Crown Meters	Min. Depth Below Rim Meters
J33	JUNCTION	24.00	0.844	1.556
J40	JUNCTION	6.35	0.445	0.317
STM101	JUNCTION	23.08	1.430	0.455
STM101A	JUNCTION	23.06	1.378	0.447
STM104	JUNCTION	7.02	1.192	0.683

No nodes were flooded.

	Average	Avg	Evap	Exfil	Maximum	Max	Time
of Max Maximum	17-1	Deet	Deet	Deet	Volume	Deet	
Occurrence Outflow	vorume	PCIIC	PCIIC	PCIIC	vorume	PCIIC	
Storage Unit	1000 m3	Full	Loss	Loss	1000 m3	Full	days
hr:min CMS							
BASIN1	0.380	60	0	0	0.632	99	0
01:29 0.433							
BASIN2 01:21 0.734	1.216	54	0	0	2.240	100	0
	0.491	12	0	0	2.040	50	0
03:15 0.405			-	-			-
S-BLDG-A	0.017	4	0	0	0.121	24	0
01:52 0.009 S-BLDG-B	0.028	4	0	0	0.176	27	0
01:54 0.011	0.028	4	0	0	0.176	21	0
S-BLDG-C	0.021	3	0	0	0.142	24	0
01:52 0.011							
S-BLDG-D 01:53 0.005	0.010	4	0	0	0.066	25	0
S-BLDG-G	0.024	7	0	0	0.125	38	0
02:11 0.006							
S-BLDG-H	0.027	4	0	0	0.179	27	0
01:54 0.012 S-BLDG-I	0.015	3	0	0	0.106	23	0
01:50 0.008	0.015	3	U	U	0.106	23	U
S-BLDG-J	0.010	4	0	0	0.066	26	0
01:54 0.004							
S-BLDG-K 02:20 0.005	0.028	9	0	0	0.130	42	0
02.20 0.005							

Outfall Loading Summary

	Flow	Avg	Max	Total
	Freq	Flow	Flow	Volume
Outfall Node	Pent	CMS	CMS	10^6 ltr
Canal Outlet	25.26	0.075	0.444	1.671
J28	74.97	0.092	0.725	5.536
System	50.12	0.167	0.725	7.207

	_	Maximum Flow	Time Occu	of Max rrence	Maximum Veloc m/sec	Max/ Full	Max Ful
Link 	Туре	CMS	days	hr:min	m/sec	Flow	Dept
C1	CONDUIT CONDUIT CONDUIT CONDUIT	0.183	0	01:22	0.37	0.28	1.0
C10	CONDUIT	0.227	0	01:16	0.80	1.21	1.0
C11	CONDUIT	0.294	0	01:16	0.46	0.61	1.0
C12	CONDUIT	0.347	0	01:16	0.55	0.48	1.0
C13	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	0.145	0	01:03	2.95 2.76 1.35 1.34 1.33	3.47	1.0
C14	CONDUIT	0.135	0	01:05	2.76	3.21	1.0
C15	CONDUIT	0.382	0	01:06	1.35	1.35	1.0
C16	CONDUIT	0.380	0	01:06	1.34	1.17	1.0
C17	CONDUIT	0.376	0	01:06	1.33	1.46	1.0
C18	CONDUIT	0.291	0	01:15	0.46	0.51	1.0
C18_1	CONDUIT	2.094	0	01:10	1.50	1.10	1.0
C18 2	CONDUIT	1.550	0	01:11	1.08	0.82	1.
C19	CONDUIT	0.455	0	01:15	0.72	1.10	1.
C2	CONDUIT	0.059	0	01:04	0.37	0.47	1.
C20	CONDUIT	0.654	0	01:13	1.03	0.15	1.
C21	CONDUIT	0.263	0	01:16	1.22	1.29	1.
C21 1	CONDUIT	1.087	0	01:08	0.77	0.83	1.
C21_1 C21_2	CONDUIT	0.687	0	01:08	0.70	0.54	1.
C22	CONDUIT	0.034	0	01:13	1.09	1.47	1.
C23	CONDUIT	0.085	0	01:09	1.73	2.01	1.
C24	CONDUIT	0.352	0	01:11	0.98	0.68	1.
C25	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	0.549	0	01:11	1.53	1.04	1.
C26	CONDUIT	0.577	0	08:01	0.73	0.26	1.
C27	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	0.155	0	01:16	0.72	0.74	1.
C27 2	CONDUIT	0.593	0	01:11	0.81	0.80	1.
C28	CONDUIT	0.647	0	01:11	0.87	1.08	1.
C29	CONDUIT	0.647	0	01:11	0.87	0.77	1.
С3	CONDUIT	0.464	0	01:04	2.93	3.66	1.
C30	CONDUIT	0.723	0	01:11	0.97	0.96	1.
C31	CONDUIT CONDUIT	0.725	0	01:11	0.97 0.97	0.49	1.
C32	CONDUIT	0.725	0	01:11	0.97	0.53	1.
C33	CONDUIT	0.069	0	01:06	1.41	1.74	1.
C34	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	0.057	0	01:07	0.97 1.41 1.17 0.71 0.89	1.34	1.
C35	CONDUIT	0.155	0	01:06	0.71	0.80	1.
C36	CONDUTT	0.223	0	01:05	0.89	1.32	1.
C37	CONDUTT	0.444	0	00:00	2.00	0.79	1.
C38	CONDUTT	0.096	0	01:14	0.61	0.87	1.
C39	CONDULT	0 095	0	01.14	0.92	1 44	1
C4	CONDUIT	0.563	ő	01:11	1.99	1.92	1.
C40	CONDULT	0 029	0	01.10	0.27	0 42	1
C41	CONDUIT	0.058	0	01:20	0.33	0.01	<u>.</u>
C42	CONDULT	0.060	0	01.20	1 02	0 47	1
C43	CONDUTT	0.000	0	00:00	0.00	0.00	0
C45	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	0.000	0	00.00	0.00	0.00	0.
C45	CONDUTT	0.000	0	01.10	0.00	0.00	0
C45 C46	CONDUIT	0.964	0	01.10	1.20	0.07	0.
		0.883	U	01:10	1.20	0.45	U.

C48 C49 C5 C50 C51 C52 C54 C55 C56 C57 C56 C56 C57 C66 C61 C61 C61 C61 C62 C63 C64 C7 C8 C9 W24 W25 W25 W26 W25 W25 W26 W25 W26 W22 C9 C7 C7 C8 C9 W21 C7 C7 C7 C7 C7 C7 C7 C7 C7 C7 C7 C7 C7	CONDUIT 0.321 0 01:11 0.35 0.01 0.14 CONDUIT 0.669 0 01:10 0.11 0.00 0.08 CONDUIT 0.522 0 01:13 1.95 2.32 1.00 CONDUIT 0.552 0 01:10 0.23 0.04 0.19 CONDUIT 0.633 0 01:25 0.17 0.01 0.26 CONDUIT 0.043 0 01:20 0.02 0.00 0.12 CONDUIT 0.040 0 01:20 0.00 0.00 0.12 CONDUIT 0.040 0 01:00 0.00 0.00 0.00 CONDUIT 0.040 0 00:00 0.00 0.00 0.00 CONDUIT 0.040 0 00:00 0.00 0.00 0.00 CONDUT 0.050 0 00:00 0.00 0.00 0.00 CONDUT 0.558 0 0.113 1.77	W39 W4 W40 W41 W42 W43 W45 W5 W6 W7 W8 W9 OL1 OL1 OL1 OL1 OL1 OL1 OL1 OL1 OL1 OL1	ation Summary	0.169 0.147 0.000 0.000 0.009 0.011	0 01 0 00 0 01 0 00 0 01	13 00 12 21 12 21 11 00 00 00 00 24 00 00 00 24 00 00 00 24 00 00 00 24 03 00 00 07 03 1 15 00 00 07 00 07 00 06 00 00 00 00 00 00 00 00 12 21 21 21 21 21 21 21 21 21 21 21 21			0.00 0.07 0.26 0.26 0.26 0.24 0.14 0.14 0.00 0.00 0.00 0.00 0.00 0.0
W11 W12	WEIR 0.063 0 01:25 0.18 WEIR 0.066 0 01:25 0.11		**************						
W13 W14 W15	WEIR 0.000 0 0:00 0.00 WEIR 0.000 0 0:00 0.00 WEIR 0.000 0 0:00 0.00		Adjusted		Fract:	on of Tin	ne in Flo	ow Clas	s
W16 W17	WEIR 0.108 0 01:10 0.18 WEIR 0.080 0 01:10 0.12	Inlet	/Actual		Down				
W18 W19	WEIR 0.022 0 01:10 0.05 WEIR 0.025 0 01:11 0.06	Conduit Ctrl	Length	Dry Dr					
W2 W20 W21	WEIR 3.418 0 0.1:11 1.00 WEIR 0.197 0 0.1:13 0.23 WEIR 0.070 0 0.11 1	 C1	1.00	0.01 0.	00 0.00	0.33 0.	0.00	0.65	0.03
W22 W23	WEIR 0.102 0 01:10 0.15 WEIR 0.141 0 01:05 0.19	0.00 C10 0.00	1.00	0.01 0.	00 0.00	0.96 0.	0.00	0.02	0.00
W3 W32 W33	WEIR 1.777 0 01:08 1.00 WEIR 0.000 0 00:00 0.00	C11 0.00		0.02 0.					
W33 W34 W35	WEIR 0.000 0 0:00 0.00 WEIR 0.000 0 0:00 0.00 WEIR 0.000 0 0:00 0.00	C12 0.00 C13		0.02 0.					
W36 W37	WEIR 0.000 0 00:00 0.00 WEIR 0.092 0 01:13 0.18	0.00 C14		0.02 0.					
615		C18	1.00	0.02 0.	0.00	0.33 0.1	10 0.00	0.65	0.01
0.00 C15 C16	1.00 0.01 0.00 0.00 0.96 0.00 0.00 0.02 0.00 1.00 0.01 0.00 0.00 0.96 0.00 0.00 0.02 0.00	C38 0.00 C39		0.02 0. 0.01 0.					
0.00 C16 0.00 C17		0.00 C39 0.00 C4	1.00		00 0.00	0.31 0.	0.00	0.68	0.01
0.00 C16 0.00	1.00 0.01 0.00 0.00 0.96 0.00 0.00 0.02 0.00	0.00 C39 0.00	1.00	0.01 0. 0.01 0.	00 0.00	0.31 0.	00 0.00	0.68 0.68	0.01
0.00 C16 0.00 C17 0.00 C18 0.00 C18 0.00 C18_1 0.00	1.00 0.01 0.00 0.00 0.96 0.00 0.00 0.02 0.00 1.00 0.02 0.00 0.00 0.96 0.00 0.00 0.02 0.00 1.00 0.02 0.00 0.96 0.00 0.00 0.02 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00	0.00 C39 0.00 C4 0.00 C40 0.00 C41 0.00	1.00 1.00 1.00	0.01 0. 0.01 0. 0.02 0. 0.04 0.	00 0.00 00 0.00 02 0.00 34 0.00	0.31 0.1 0.30 0.1 0.30 0.1 0.62 0.1	00 0.00 00 0.00 00 0.00 00 0.00	0.68 0.68 0.65 0.00	0.01 0.00 0.02 0.95
0.00 C16 0.00 C17 0.00 C18 0.00 C18_1 0.00 C18_2 0.00 C19	1.00 0.01 0.00 0.00 0.96 0.00 0.00 0.02 0.00 1.00 0.02 0.00 0.00 0.96 0.00 0.02 0.00 1.00 0.02 0.00 0.96 0.00 0.00 0.02 0.00 1.00 0.00 0.02 0.00 0.98 0.00 0.00 0.00	0.00 C39 0.00 C4 0.00 C40 0.00 C41 0.00 C42 0.00 C43	1.00 1.00 1.00	0.01 0. 0.01 0. 0.02 0. 0.04 0.	00 0.00 00 0.00 02 0.00	0.31 0.1 0.30 0.1 0.30 0.1 0.62 0.1 0.33 0.1	00 0.00 00 0.00 00 0.00 00 0.00	0.68 0.68 0.65 0.00 0.63	0.01 0.00 0.02 0.95 0.06
0.00 C16 0.00 C17 0.00 C18 0.00 C18 0.00 C18_2 0.00 C19 0.00 C2	1.00 0.01 0.00 0.00 0.00 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.00 0.00 0.00 0.02 0.00 1.00 0.02 0.00 0.96 0.00 0.00 0.02 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.97 0.00 0.00 0.00 0.00	0.00 C39 0.00 C4 0.00 C40 0.00 C41 0.00 C42 0.00 C42 0.00 C43 0.00 C43 0.00 C43 0.00 C44	1.00 1.00 1.00 1.00	0.01 0. 0.01 0. 0.02 0. 0.04 0. 0.04 0.	00 0.00 00 0.00 02 0.00 34 0.00 00 0.00	0.31 0.1 0.30 0.1 0.30 0.1 0.62 0.1 0.33 0.1 0.00 0.1	00 0.00 00 0.00 00 0.00 00 0.00 00 0.00	0.68 0.65 0.00 0.63 0.00	0.01 0.00 0.02 0.95 0.06 0.00
0.00 C16 0.00 C17 0.00 C18 0.00 $C18_{-}1$ 0.00 $C19_{-}2$ 0.00 C19 0.00 C29 0.00 C20 0.00 C20 0.0	1.00 0.01 0.00 <th< td=""><td>$egin{array}{cccc} 0.00\\ C39\\ 0.00\\ C4\\ 0.00\\ C40\\ 0.00\\ C41\\ 0.00\\ C41\\ 0.00\\ C42\\ 0.00\\ C42\\ 0.00\\ C43\\ 0.00\\ C44\\ 0.00\\ C44\\ 0.00\\ C45\\ 0.00\\ \end{array}$</td><td>1.00 1.00 1.00 1.00 1.00 1.00 1.00</td><td>0.01 0. 0.01 0. 0.02 0. 0.04 0. 0.04 0. 0.04 0. 0.38 0. 0.01 0.</td><td>00 0.00 00 0.00 02 0.00 34 0.00 00 0.00 96 0.00 62 0.00 02 0.00</td><td>0.31 0.1 0.30 0.1 0.30 0.1 0.62 0.1 0.33 0.1 0.00 0.1 0.00 0.1</td><td>0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00</td><td>0.68 0.65 0.00 0.63 0.00 0.00 0.00</td><td>0.01 0.00 0.95 0.06 0.00 0.00 0.93</td></th<>	$egin{array}{cccc} 0.00\\ C39\\ 0.00\\ C4\\ 0.00\\ C40\\ 0.00\\ C41\\ 0.00\\ C41\\ 0.00\\ C42\\ 0.00\\ C42\\ 0.00\\ C43\\ 0.00\\ C44\\ 0.00\\ C44\\ 0.00\\ C45\\ 0.00\\ \end{array}$	1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.01 0. 0.01 0. 0.02 0. 0.04 0. 0.04 0. 0.04 0. 0.38 0. 0.01 0.	00 0.00 00 0.00 02 0.00 34 0.00 00 0.00 96 0.00 62 0.00 02 0.00	0.31 0.1 0.30 0.1 0.30 0.1 0.62 0.1 0.33 0.1 0.00 0.1 0.00 0.1	0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00	0.68 0.65 0.00 0.63 0.00 0.00 0.00	0.01 0.00 0.95 0.06 0.00 0.00 0.93
0.00 C16 0.00 C17 0.00 C18 0.00 C18_1 0.00 C19_1 0.00 C19_2 0.00 C20 0.00 C20 0.00 C20 0.00 C20 0.00 C20 0.00 C21 0.00 C12 0.00 C20 C20 0.00 C20 C20 C20 C20 C20 C20 C20 C	1.00 0.01 0.00 0.00 0.96 0.00 0.00 0.02 0.00 1.00 0.02 0.00 0.00 0.96 0.00 0.00 0.02 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.97 0.00 0.00 0.00 0.00 1.00 0.00 0.00 0.97 0.00 0.03 0.00 1.00 0.01 0.00 0.01 0.00 0.00 0.01 0.01 1.00 0.02 0.01 0.00 0.00 0.00 0.02 0.58	$egin{array}{ccccc} 0.00\\ C39\\ 0.00\\ C4\\ 0.00\\ C40\\ 0.00\\ C41\\ 0.00\\ C42\\ 0.00\\ C42\\ 0.00\\ C42\\ 0.00\\ C43\\ 0.00\\ C44\\ 0.00\\ C45\\ 0.00\\ C46\\ 0.00\\ C46\\ 0.00\\ \end{array}$	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.01 0. 0.01 0. 0.02 0. 0.04 0. 0.04 0. 0.04 0. 0.38 0. 0.01 0. 0.02 0.	00 0.00 01 0.00 02 0.00 034 0.00 000 0.00 04 0.00 05 0.00 06 0.00 06 0.00 07 0.00 08 0.00 09 0.00 00 0.00	0.31 0.1 0.30 0.1 0.62 0.1 0.33 0.1 0.33 0.1 0.00 0.1 0.00 0.1 0.97 0.1	0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00	0.68 0.65 0.00 0.63 0.00 0.00 0.00 0.00	0.01 0.02 0.95 0.06 0.00 0.93 0.00
0.00 c16 0.00 c17 0.00 c18 0.00 c18-1 0.00-1 c18-2 0.00-1 c19-2 0.00-2 c19-2 0.00 c20-2 0.00 c20-2 0.00 c21-2 0.00-2 0.00-2 0.0	1.00 0.01 0.00 <th< td=""><td>0.00 C39 0.00 C4 0.00 C41 0.00 C41 0.00 C42 0.00 C43 0.00 C43 0.00 C44 0.00 C45 0.00 C45 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C46 0.00 C46 0.00 C47 0.00 C48 C47 0.00 C48</td><td>1.00 1.00 1.00 1.00 1.00 1.00 1.00</td><td>0.01 0. 0.01 0. 0.02 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0.</td><td>00 0.00 00 0.00 02 0.00 34 0.00 00 0.00 96 0.00 62 0.00 02 0.00</td><td>0.31 0.1 0.30 0.1 0.30 0.1 0.62 0.1 0.33 0.1 0.00 0.1 0.00 0.1 0.97 0.1 0.97 0.1 0.40 0.1</td><td>00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 01 0.00</td><td>0.68 0.65 0.00 0.63 0.00 0.00 0.00 0.00 0.00</td><td>0.01 0.02 0.95 0.06 0.00 0.00 0.93 0.00 0.39</td></th<>	0.00 C39 0.00 C4 0.00 C41 0.00 C41 0.00 C42 0.00 C43 0.00 C43 0.00 C44 0.00 C45 0.00 C45 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C46 0.00 C46 0.00 C47 0.00 C48 C47 0.00 C48	1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.01 0. 0.01 0. 0.02 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0.	00 0.00 00 0.00 02 0.00 34 0.00 00 0.00 96 0.00 62 0.00 02 0.00	0.31 0.1 0.30 0.1 0.30 0.1 0.62 0.1 0.33 0.1 0.00 0.1 0.00 0.1 0.97 0.1 0.97 0.1 0.40 0.1	00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 01 0.00	0.68 0.65 0.00 0.63 0.00 0.00 0.00 0.00 0.00	0.01 0.02 0.95 0.06 0.00 0.00 0.93 0.00 0.39
0.00 C16 0.00 C17 0.00 C18 0.00 C18 0.00^{-1} $C18_{-1}$ 0.00^{-1} $C19_{-2}$ 0.00^{-1} C20 0.00^{-1} C20 0.00^{-1} C20 0.00^{-1} C20 0.00^{-1} $C21^{-1}$ 0.00^{-1} $C21^{-1}$ 0.00^{-1} $C22^{-1}$ 0.00^{-1} $C2^{-1}$ 0.00^{-1} $C2^{-1}$ 0.00^{-1} $C2^{-1}$ 0.00^{-1} $C2^{-1}$ 0.00^{-1} $C2^{-1}$ 0.00^{-1} $C2^{-1}$ 0.00^{-1} $C2^{-1}$ 0.00^{-1} $C2^{-1}$ 0.00^{-1} $C2^{-1}$ 0.00^{-1} $C2^{-1}$ 0.00^{-1} 0.	1.00 0.01 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.00 0.00 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.00 0.97 0.00 0.00 0.00 0.00 1.00 0.00 0.00 0.97 0.00 0.00 0.00 0.00 1.00 0.01 0.00 0.01 0.00 0.00 0.00 0.00 1.00 0.02 0.01 1.00 0.00 0.00 0.00 0.00	0.00 C39 0.00 C4 0.00 C4 0.00 C41 0.00 C42 0.00 C42 0.00 C43 0.00 C44 0.00 C44 0.00 C45 0.00 C45 0.00 C46 0.00 C44 0.00 C42 0.00 C43 0.00 C43 0.00 C44 0.00 C43 0.00 C44 0.00 C42 0.00 C42 0.00 C43 0.00 C44 0.00 C43 0.00 C44 0.00 C44 0.00 C42 0.00 C44 0.00 C44 0.00 C42 0.00 C44 0.00 C48 0.00 C48 0.00 C48 0.00 C48 0.00 C49	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.01 0. 0.01 0. 0.02 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0.	00 0.00 01 0.00 02 0.00 34 0.00 00 0.00 04 0.00 05 0.00 06 0.00 02 0.00 02 0.00 02 0.00 02 0.00 02 0.00 02 0.00 03 0.00	0.31 0.1 0.30 0.1 0.30 0.1 0.62 0.1 0.33 0.1 0.00 0.1 0.97 0.1 0.40 0.1 0.51 0.1	00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 01 0.00 01 0.00 01 0.00	0.68 0.65 0.00 0.63 0.00 0.00 0.00 0.00 0.00 0.00	0.01 0.02 0.95 0.06 0.00 0.93 0.00 0.39 0.39
0.00 C16 0.00 C17 0.00 C18 0.00 C18 0.00^{-1} $C18_{-1}$ 0.00^{-1} $C19_{-2}$ 0.00^{-1} $C20_{-2}$ 0.00^{-1} $C20_{-2}$ 0.00^{-1} $C21_{-2}$ 0.00^{-1} $C22_{-2}$ 0.00^{-1}	1.00 0.01 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.00 0.00 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.97 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.00 0.97 0.00 0.00 0.00 0.00 1.00 0.00 0.00 0.97 0.00 <t< td=""><td>0.00 C39 0.00 C4 0.00 C4 0.00 C41 0.00 C42 0.00 C43 0.00 C44 0.00 C44 0.00 C45 0.00 C45 0.00 C45 0.00 C46 0.00 C45 0.00 C55 C46 0.00 C55 C55 C55 C55 C55 C55 C55 C</td><td>1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00</td><td>0.01 0. 0.01 0. 0.02 0. 0.04 0. 0.04 0. 0.04 0. 0.05 0. 0.04 0. 0.05 0. 0.04 0. 0.04 0. 0.05 0. 0.04 0. 0.05 0. 0.04 0. 0.04 0. 0.05 0.</td><td>00 0.00 01 0.00 02 0.00 34 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 01 0.00 02 0.00 03 0.00 04 0.00</td><td>0.31 0.1 0.30 0.1 0.30 0.1 0.42 0.1 0.33 0.1 0.00 0.1 0.97 0.1 0.40 0.1 0.51 0.1 0.02 0.1</td><td>00 0.00 01 0.00 02 0.00 03 0.00 04 0.00 05 0.00 06 0.00 07 0.00 08 0.00 09 0.00 09 0.00 09 0.00 09 0.00 09 0.00 09 0.00 09 0.00</td><td>0.68 0.65 0.00 0.63 0.00 0.00 0.00 0.00 0.00 0.00</td><td>0.01 0.02 0.95 0.06 0.00 0.00 0.93 0.00 0.39 0.92 0.96</td></t<>	0.00 C39 0.00 C4 0.00 C4 0.00 C41 0.00 C42 0.00 C43 0.00 C44 0.00 C44 0.00 C45 0.00 C45 0.00 C45 0.00 C46 0.00 C45 0.00 C55 C46 0.00 C55 C55 C55 C55 C55 C55 C55 C	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.01 0. 0.01 0. 0.02 0. 0.04 0. 0.04 0. 0.04 0. 0.05 0. 0.04 0. 0.05 0. 0.04 0. 0.04 0. 0.05 0. 0.04 0. 0.05 0. 0.04 0. 0.04 0. 0.05 0.	00 0.00 01 0.00 02 0.00 34 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 01 0.00 02 0.00 03 0.00 04 0.00	0.31 0.1 0.30 0.1 0.30 0.1 0.42 0.1 0.33 0.1 0.00 0.1 0.97 0.1 0.40 0.1 0.51 0.1 0.02 0.1	00 0.00 01 0.00 02 0.00 03 0.00 04 0.00 05 0.00 06 0.00 07 0.00 08 0.00 09 0.00 09 0.00 09 0.00 09 0.00 09 0.00 09 0.00 09 0.00	0.68 0.65 0.00 0.63 0.00 0.00 0.00 0.00 0.00 0.00	0.01 0.02 0.95 0.06 0.00 0.00 0.93 0.00 0.39 0.92 0.96
0.00 C16 0.00 C17 0.00 C18 0.00 $C18_{-1}$ 0.00^{-1} 0.00^{-2} 0.00 0	1.00 0.01 0.00 0.00 0.96 0.00 0.00 0.02 0.00 1.00 0.02 0.00 0.00 0.96 0.00 0.00 0.02 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.97 0.00 0.00 0.00 0.00 1.00 0.02 0.01 0.00 0.97 0.00 0.00 0.00 0.00 1.00 0.02 0.01 0.00 0.31 0.00 0.00 0.01 0.01 1.00 0.02 0.01 0.00 0.31 0.00 0.00 0.00 0.01 1.00 0.02 0.01 0.00 0.98 0.00 0.00 0.00	0.00 C39 0.00 C4 0.00 C40 0.00 C41 0.00 C42 0.00 C42 0.00 C43 0.00 C44 0.00 C45 0.00 C45 0.00 C45 0.00 C44 0.00 C45 0.00 C44 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C47 0.00 C45 0.00 C47 0.00 C45 0.00 C47 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C47 0.00 C45 0.00 C47 0.00 C47 0.00 C55 0.00 C55 0.00 0.00 C55 0.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.01 0. 0.02 0. 0.04 0. 0.05 0. 0.04 0. 0.05 0. 0.01 0. 0.02 0. 0.04 0. 0.05 0. 0.04 0. 0.05 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.05 0. 0.02 0. 0.02 0. 0.01 0.	00 0.00 010 0.00 02 0.00 034 0.00 040 0.00 052 0.00 052 0.00 052 0.00 052 0.00 052 0.00 053 0.00 054 0.00 053 0.00 054 0.00 054 0.00	0.31 0.1 0.30 0.1 0.62 0.1 0.33 0.1 0.40 0.1 0.30 0.1 0.33 0.1 0.00 0.1 0.97 0.1 0.97 0.1 0.40 0.1 0.51 0.1 0.32 0.1 0.33 0.1 0.31 0.1	00 0.00 01 0.00 02 0.00 030 0.00 040 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 051 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00	0.68 0.65 0.00 0.63 0.00 0.00 0.00 0.00 0.00 0.00	0.01 0.02 0.95 0.06 0.00 0.00 0.93 0.00 0.39 0.92 0.96 0.00 0.95
0.00 c16 c17 c17 0.00 c18 1.00 c18 0.00 c18 2.00 c19 0.00 c22 0.00 c21 0.00 c22 0.00 c21 0.00 c22 0.00 c21 0.00 c22 0.00 c23 0.00 c25 0.00 c23 0.00 c25 0.00	1.00 0.01 0.00 0.00 0.00 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.00 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.97 0.00 0.00 0.00 0.00 1.00 0.02 0.01 0.00 0.97 0.00 0.00 0.01 0.00 1.00 0.02 0.01 0.00 0.31 0.00 0.00 0.01 0.01 1.00 0.02 0.01 0.00 0.31 0.00 0.00 0.03 0.01 1.00 0.02 0.01 0.00 0.98 0.00 0.00 0.00 0.00	0.00 C39 0.00 C4 0.00 C40 0.00 C41 0.00 C41 0.00 C42 0.00 C42 0.00 C43 0.00 C44 0.00 C45 0.00 C45 0.00 C44 0.00 C44 0.00 C45 0.00 C44 0.00 C45 0.00 C45 0.00 C44 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C47 0.00 C47 0.00 C47 0.00 C45 0.00 C47 0.00 C45 0.00 C47 0.00 C45 0.00 C47 0.00 C47 0.00 C50 0.00 C50 0.00 C50 0.00 C50 0.00 C50 0.00 C50 0.00 C50 0.00 C50 0.00 C50 0.00 C50 0.00 C50 0.00 0.00 C50 0.00 0.00 C50 0.00 0.00 C50 0.00 0.00 0.00 C50 0.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.01 0. 0.02 0. 0.04 0. 0.05 0. 0.04 0. 0.05 0. 0.01 0. 0.02 0. 0.04 0. 0.05 0. 0.04 0. 0.05 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.05 0. 0.01 0. 0.01 0.	00 0.00 010 0.00 02 0.00 034 0.00 040 0.00 052 0.00 052 0.00 052 0.00 052 0.00 052 0.00 052 0.00 053 0.00 054 0.00 050 0.00 050 0.00	0.31 0.1 0.30 0.1 0.30 0.1 0.62 0.1 0.33 0.1 0.00 0.1 0.00 0.1 0.97 0.1 0.44 0.1 0.51 0.1 0.33 0.1 0.45 0.1 0.55 0.1 0.85 0.1	00 0.00 01 0.00 02 0.00 03 0.00 04 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00	0.68 0.68 0.65 0.00 0.63 0.00 0.00 0.00 0.00 0.00 0.00	0.01 0.02 0.95 0.06 0.00 0.00 0.93 0.90 0.92 0.96 0.96 0.95 0.84
0.00 C16 C17 C17 0.00 C18 0.00 C18 0.00 C18 0.00 C18 0.00 C21 0.00 C22 0.00 C21 0.00 C21 0.00 C21 0.00 C21 0.00 C21 0.00 C22 C22 0.00 C22 C22 C22 C22 C22 C22 C22 C	1.00 0.01 0.00 0.00 0.96 0.00 0.00 0.02 0.00 1.00 0.02 0.00 0.00 0.96 0.00 0.00 0.02 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.97 0.00 0.00 0.00 0.00 1.00 0.02 0.01 0.00 0.97 0.00 0.00 0.00 0.00 1.00 0.02 0.01 0.00 0.31 0.00 0.00 0.01 0.01 1.00 0.02 0.01 0.00 0.31 0.00 0.00 0.00 0.00 1.00 0.02 0.01 0.00 0.98 0.00 0.00 0.00	0.00 C39 0.00 C4 0.00 C41 0.00 C41 0.00 C42 0.00 C43 0.00 C44 0.00 C44 0.00 C45 0.00 C44 0.00 C45 0.00 C44 0.00 C45 0.00 C44 0.00 C45 0.00 C45 0.00 C44 0.00 C45 0.00 C55 0.000 C55 0.0000 C55 0.0000 C55 0	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.01 0. 0.02 0. 0.04 0. 0.05 0. 0.04 0. 0.05 0. 0.06 0. 0.01 0. 0.02 0. 0.04 0. 0.05 0. 0.06 0. 0.015 0. 0.010 0. 0.011 0. 0.012 0.	00 0.00 010 0.00 02 0.00 034 0.00 040 0.00 052 0.00 052 0.00 052 0.00 052 0.00 052 0.00 053 0.00 054 0.00 053 0.00 054 0.00 054 0.00	0.31 0. 0.30 0. 0.30 0. 0.62 0. 0.33 0. 0.00 0. 0.00 0. 0.01 0. 0.02 0. 0.33 0. 0.40 0. 0.51 0. 0.31 0. 0.33 0. 0.34 0. 0.35 0. 0.97 0.	00 0.00 01 0.00 02 0.00 030 0.00 040 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 051 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00	0.68 0.65 0.00 0.63 0.00 0.00 0.00 0.00 0.00 0.00	0.01 0.02 0.95 0.06 0.00 0.00 0.93 0.90 0.93 0.92 0.96 0.95 0.84 0.26
0.00 c16 c17 c17 0.00 c18 0.00 c18 1.00 c18 0.00 c18 1.00 c18 2.00 c18 2.00 c19 0.00 c20 0.00 c21 0.00 c22 0.00 c21 0.00 c21 0.00 c22 0.00 c27 0	1.00 0.01 0.00 0.00 0.00 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.00 0.96 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.98 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.97 0.00 0.00 0.00 0.00 1.00 0.02 0.01 0.00 0.97 0.00 0.00 0.00 1.00 0.02 0.01 0.00 0.31 0.00 0.00 0.01 1.00 0.02 0.01 0.00 0.31 0.00 0.00 0.01 0.01 1.00 0.02 0.01 0.00 0.98 0.00 0.00 0.00 1.00 <td>0.00 C39 0.00 C4 0.00 C4 0.00 C41 0.00 C41 0.00 C42 0.00 C43 0.00 C44 0.00 C45 0.00 C45 0.00 C44 0.00 C45 0.00 C45 0.00 C44 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C55 0.00 0.00 C55 0.00</td> <td>1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00</td> <td>0.01 0. 0.02 0. 0.04 0. 0.05 0. 0.04 0. 0.05 0. 0.01 0. 0.02 0. 0.04 0. 0.05 0. 0.04 0. 0.05 0. 0.04 0. 0.05 0. 0.04 0. 0.05 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0.</td> <td>00 0.00 010 0.00 02 0.00 034 0.00 040 0.00 052 0.00 052 0.00 052 0.00 052 0.00 052 0.00 053 0.00 054 0.00</td> <td>0.31 0. 0.30 0. 0.30 0. 0.62 0. 0.33 0. 0.00 0. 0.00 0. 0.01 0. 0.02 0. 0.33 0. 0.40 0. 0.51 0. 0.31 0. 0.33 0. 0.34 0. 0.35 0. 0.365 0. 0.50 0.</td> <td>00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 01 0.00 01 0.00 01 0.00 01 0.00 01 0.00 010 0.00 010 0.00 010 0.00 010 0.00 010 0.00 010 0.00 010 0.00 010 0.00 010 0.00</td> <td>0.68 0.65 0.00 0.63 0.00 0.00 0.00 0.00 0.00 0.00</td> <td>0.01 0.02 0.95 0.06 0.00 0.00 0.93 0.92 0.96 0.92 0.95 0.84 0.26 0.93</td>	0.00 C39 0.00 C4 0.00 C4 0.00 C41 0.00 C41 0.00 C42 0.00 C43 0.00 C44 0.00 C45 0.00 C45 0.00 C44 0.00 C45 0.00 C45 0.00 C44 0.00 C45 0.00 C45 0.00 C45 0.00 C45 0.00 C55 0.00 0.00 C55 0.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.01 0. 0.02 0. 0.04 0. 0.05 0. 0.04 0. 0.05 0. 0.01 0. 0.02 0. 0.04 0. 0.05 0. 0.04 0. 0.05 0. 0.04 0. 0.05 0. 0.04 0. 0.05 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0.	00 0.00 010 0.00 02 0.00 034 0.00 040 0.00 052 0.00 052 0.00 052 0.00 052 0.00 052 0.00 053 0.00 054 0.00	0.31 0. 0.30 0. 0.30 0. 0.62 0. 0.33 0. 0.00 0. 0.00 0. 0.01 0. 0.02 0. 0.33 0. 0.40 0. 0.51 0. 0.31 0. 0.33 0. 0.34 0. 0.35 0. 0.365 0. 0.50 0.	00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 00 0.00 01 0.00 01 0.00 01 0.00 01 0.00 01 0.00 010 0.00 010 0.00 010 0.00 010 0.00 010 0.00 010 0.00 010 0.00 010 0.00 010 0.00	0.68 0.65 0.00 0.63 0.00 0.00 0.00 0.00 0.00 0.00	0.01 0.02 0.95 0.06 0.00 0.00 0.93 0.92 0.96 0.92 0.95 0.84 0.26 0.93
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0.00 c16 c17 c17 c18 c18 c18 c19 c19 c19 c20 c20 c20 c20 c20 c20 c20 c20	1.00 0.01 0.00 0.00 0.00 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.00 0.99 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.99 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.99 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.99 0.00 0.00 0.00 0.00 1.00 0.02 0.00 0.00 0.97 0.00 0.00 0.00 1.00 0.00 0.00 0.97 0.00 0.00 0.00 1.00 0.00 0.00 0.97 0.00 0.00 0.01 0.01 1.00 0.00 0.00 0.31 0.00 0.00 0.00 0.01 0.01 1.00 0.01 0.00 0.98 0.00 0.00 0.00 0.00 0.00 1.00 <td>0.00 C39 0.00 C4 0.00 C41 0.00 C41 0.00 C41 0.00 C42 0.00 C42 0.00 C43 0.00 C43 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C45 0.00 C47 0.00 C47 0.00 C55 0.00 C51 0.00 C53 0.00 C53 0.00 C53 0.00 C53 0.00 C53 0.00 C53 0.00 C53 0.00 C55 0.00 0.00 C55 0.00 0.00 C55 0.00</td> <td>1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00</td> <td>0.01 0. 0.02 0. 0.04 0. 0.05 0. 0.04 0. 0.05 0. 0.06 0. 0.07 0. 0.01 0. 0.02 0. 0.04 0. 0.05 0. 0.06 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0.</td> <td>00 0.00 010 0.00 02 0.00 02 0.00 034 0.00 040 0.00 052 0.00 052 0.00 052 0.00 052 0.00 053 0.00 054 0.00 055 0.00 056 0.00 057 0.00 057 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00</td> <td>0.31 0. 0.30 0. 0.30 0. 0.62 0. 0.33 0. 0.00 0. 0.00 0. 0.01 0. 0.02 0. 0.33 0. 0.40 0. 0.51 0. 0.31 0. 0.33 0. 0.34 0. 0.35 0. 0.55 0. 0.50 0. 0.12 0. 0.27 0. 0.000 0.</td> <td>0 0.00 0 0.00</td> <td>0.68 0.68 0.65 0.00 0.00 0.00 0.00 0.00 0.00 0.00</td> <td>0.01 0.02 0.95 0.06 0.00 0.93 0.00 0.93 0.92 0.96 0.92 0.94 0.95 0.84 0.26 0.93 0.25 0.00</td>	0.00 C39 0.00 C4 0.00 C41 0.00 C41 0.00 C41 0.00 C42 0.00 C42 0.00 C43 0.00 C43 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C45 0.00 C47 0.00 C47 0.00 C55 0.00 C51 0.00 C53 0.00 C53 0.00 C53 0.00 C53 0.00 C53 0.00 C53 0.00 C53 0.00 C55 0.00 0.00 C55 0.00 0.00 C55 0.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.01 0. 0.02 0. 0.04 0. 0.05 0. 0.04 0. 0.05 0. 0.06 0. 0.07 0. 0.01 0. 0.02 0. 0.04 0. 0.05 0. 0.06 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0.	00 0.00 010 0.00 02 0.00 02 0.00 034 0.00 040 0.00 052 0.00 052 0.00 052 0.00 052 0.00 053 0.00 054 0.00 055 0.00 056 0.00 057 0.00 057 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00	0.31 0. 0.30 0. 0.30 0. 0.62 0. 0.33 0. 0.00 0. 0.00 0. 0.01 0. 0.02 0. 0.33 0. 0.40 0. 0.51 0. 0.31 0. 0.33 0. 0.34 0. 0.35 0. 0.55 0. 0.50 0. 0.12 0. 0.27 0. 0.000 0.	0 0.00 0 0.00	0.68 0.68 0.65 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.01 0.02 0.95 0.06 0.00 0.93 0.00 0.93 0.92 0.96 0.92 0.94 0.95 0.84 0.26 0.93 0.25 0.00
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).00 C16 C17 C17 C18 C18 C18 C18 C18 C19 C19 C19 C20 C20 C20 C20 C20 C21 C21 C21 C21 C22 C21 C22 C21 C22 C22	1.000.010.000.000.000.000.000.000.000.001.000.020.000.000.000.000.000.000.000.001.000.020.000.000.980.000.000.000.000.001.000.020.000.980.000.000.000.000.001.000.020.000.970.000.000.000.001.000.000.000.970.000.000.010.001.000.000.000.970.000.000.010.011.000.000.000.970.000.000.010.011.000.000.000.970.000.000.000.011.000.000.000.970.000.000.000.011.000.000.000.980.000.000.000.011.000.020.010.000.980.000.000.001.000.020.000.980.000.000.000.001.000.020.000.980.000.000.020.001.000.010.000.980.000.000.020.001.000.010.000.980.000.000.010.001.000.010.000.980.000.000.010.001.000.01<	0.00 C39 0.00 C4 0.00 C4 0.00 C41 0.00 C41 0.00 C42 0.00 C43 0.00 C44 0.00 C45 0.00 C44 0.00 C45 0.00 C44 0.00 C45 0.00 C44 0.00 C45 0.00 C45 0.00 C55 0.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.01 0. 0.02 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.05 0. 0.06 0. 0.07 0. 0.01 0. 0.02 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.72 0. 0.73 0. 1.00 0. 1.00 0. 1.00 0.	00 0.00 010 0.00 02 0.00 02 0.00 034 0.00 040 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 051 0.00 052 0.00 053 0.00 054 0.00 055 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00	0.31 0.1 0.30 0.1 0.30 0.1 0.62 0.1 0.00 0.1 0.00 0.1 0.00 0.1 0.00 0.1 0.97 0.1 0.97 0.1 0.33 0.1 0.31 0.1 0.85 0.1 0.97 0.1 0.97 0.1 0.27 0.1 0.27 0.1 0.00 0.2 0.00 0.1 0.00 0.1 0.00 0.1 0.00 0.1 0.00 0.1 0.00 0.1 0.00 0.1 0.00 0.1 0.00 0.1	0 0.00 0 0.00	0.68 0.68 0.65 0.00 0.63 0.00 0.00 0.00 0.00 0.00 0.00	0.01 0.02 0.95 0.06 0.00 0.93 0.00 0.93 0.92 0.94 0.92 0.96 0.95 0.84 0.25 0.24 0.00 0.00 0.00 0.00
0.00 c16 c17 0.00 c17 0.00 c18 0.00 c18 0.00 c18 0.00 c19 0.00 c20 0.00 c21 0.00 c21 0.00 c22 0.00 c23 0.00 c23 0.00 c23 0.00 c23 0.00 c23 0.00 c23 0.00 c23 0.00 c23 0.00 c30 0.00 c31 0.00 c31 c31 c31 c31 c32 c32 c32 c32 c32 c32 c32 c32	1.000.010.000.000.000.000.000.000.000.001.000.020.000.000.980.000.000.000.000.001.000.020.000.980.000.000.000.000.001.000.020.000.980.000.000.000.001.000.020.000.970.000.000.000.001.000.020.010.000.970.000.000.010.001.000.020.010.000.970.000.000.010.011.000.020.010.000.970.000.000.010.011.000.020.010.000.310.000.000.020.031.000.020.010.000.970.000.000.000.011.000.020.010.000.980.000.000.000.011.000.020.010.000.980.000.000.000.011.000.020.000.980.000.000.000.000.011.000.010.000.980.000.000.020.001.000.010.000.980.000.000.020.001.000.010.000.980.000.000.010.001.000.010.000.980	0.00 C39 0.00 C4 0.00 C4 0.00 C41 0.00 C41 0.00 C42 0.00 C43 0.00 C43 0.00 C44 0.00 C45 0.00 C44 0.00 C45 0.00 C44 0.00 C45 0.00 C45 0.00 C44 0.00 C45 0.00 C45 0.00 C55 0.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.01 0. 0.02 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.05 0. 0.04 0. 0.05 0. 0.01 0. 0.02 0. 0.03 0. 0.04 0. 0.05 0. 0.01 0. 0.01 0. 0.01 0. 0.72 0. 0.73 0. 1.00 0. 1.00 0. 1.00 0. 1.00 0.	00 0.00 010 0.00 02 0.00 02 0.00 034 0.00 040 0.00 052 0.00 052 0.00 052 0.00 052 0.00 053 0.00 053 0.00 054 0.00 055 0.00 050 0.00 051 0.00 052 0.00 053 0.00 054 0.00 055 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00 050 0.00	0.31 0.1 0.30 0.1 0.30 0.1 0.62 0.1 0.00 0.1 0.00 0.1 0.00 0.1 0.00 0.1 0.97 0.1 0.97 0.1 0.31 0.1 0.85 0.1 0.97 0.1 0.97 0.1 0.97 0.1 0.97 0.1 0.97 0.1 0.97 0.1 0.97 0.1 0.97 0.1 0.97 0.1 0.97 0.1 0.97 0.1 0.97 0.1 0.97 0.1 0.90 0.1 0.90 0.1 0.90 0.1 0.90 0.1 0.90 0.1 0.90 0.1 0.90 0.1 0.90 0.1 0.90 0.1 0.90 0.1	0 0.000 0 0.000	0.68 0.68 0.65 0.00 0.63 0.00 0.00 0.00 0.00 0.00 0.00	0.01 0.02 0.95 0.06 0.00 0.93 0.00 0.93 0.92 0.94 0.92 0.96 0.95 0.84 0.25 0.25 0.00 0.00 0.00 0.00 0.00 0.00
0.00 c16 0.00 c17 0.00 c17 0.00 c18 0.00 c18 0.00 c18 0.00 c19 0.00 c20 0.00 c21 0.00 c21 0.00 c21 0.00 c21 0.00 c22 0.00 c23 0.00 c23 0.00 c23 0.00 c23 0.00 c30 c30 c30 c30 c30 c30 c30 c	1.000.010.000.000.000.000.000.000.000.001.000.020.000.000.000.000.000.000.000.001.000.020.000.000.980.000.000.000.001.000.020.000.000.980.000.000.000.001.000.020.000.000.970.000.000.000.001.000.000.000.000.970.000.000.010.001.000.000.000.010.000.000.000.010.011.000.000.000.010.000.000.000.000.011.000.020.010.000.970.000.000.000.011.000.020.010.000.310.000.000.000.011.000.020.010.000.970.000.000.000.011.000.020.010.000.980.000.000.000.011.000.020.010.000.980.000.000.000.001.000.020.000.980.000.000.000.001.000.010.000.980.000.000.000.001.000.010.000.980.000.000.000.001.000.010	0.00 C39 0.00 C4 0.00 C4 0.00 C41 0.00 C41 0.00 C42 0.00 C43 0.00 C45 0.00 C44 0.00 C45 0.00 C44 0.00 C45 0.00 C45 0.00 C44 0.00 C45 0.00 C45 0.00 C55 0.00 C60 0.00 C60 0.00 C61 0.00 0.00 0.00 C61 0.00 0.0	1.00 1.00	0.01 0. 0.02 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.05 0. 0.06 0. 0.07 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.01 0. 0.02 0. 0.03 0. 0.04 0. 0.05 0. 1.00 0. 1.00 0. 0.02 0. 0.03 0. 0.04 0. 0.05 0. 0.06 0. 0.07 0.	00 0.00 01 0.00 02 0.00 02 0.00 02 0.00 02 0.00 02 0.00 02 0.00 02 0.00 02 0.00 02 0.00 03 0.00 044 0.00 05	0.31 0.1 0.30 0.1 0.30 0.1 0.33 0.1 0.00 0.1 0.00 0.1 0.97 0.1 0.97 0.1 0.31 0.1 0.31 0.1 0.35 0.1 0.36 0.1 0.37 0.1 0.38 0.1 0.397 0.1 0.31 0.1 0.27 0.1 0.30 0.1 0.400 0.1 0.301 0.1 0.400 0.1 0.500 0.1 0.000 0.1 0.000 0.1 0.322 0.1 0.322 0.1 0.321 0.1	0 0.00 0 0.00	0.68 0.68 0.65 0.00 0.63 0.00 0.00 0.00 0.00 0.00 0.00	0.01 0.02 0.95 0.06 0.00 0.93 0.00 0.93 0.92 0.94 0.92 0.94 0.95 0.84
0.00 c16 c17 c17 0.00 c18 c18 0.00 c18 c18 0.00 c18 c19 0.00 c21 0.00 c22 0.00 c21 0.00 c21 0.00 c21 0.00 c21 0.00 c22 0.00 c23 0.00 c33 0.00 c33 0.00 c33 0.00 c33 0.00 c33 0.00 c33 0.00 c33 0.00 c33 0.00 c33 0.00 c33 0.00 c33 0.00 c33 0.00 c33 0.00 c33 0.00 c33 0.00 c33 0.00 c35 0.00 c3	1.000.010.000.000.000.000.000.000.000.001.000.020.000.000.000.000.000.000.000.001.000.020.000.000.980.000.000.000.001.000.020.000.000.980.000.000.000.001.000.020.000.000.970.000.000.010.001.000.020.010.000.970.000.000.010.011.000.020.010.000.310.000.000.000.011.000.020.010.000.310.000.000.000.011.000.020.010.000.310.000.000.000.011.000.020.010.000.980.000.000.000.011.000.020.010.000.980.000.000.000.011.000.020.010.000.980.000.000.000.011.000.020.000.980.000.000.000.000.011.000.010.000.980.000.000.000.001.000.010.000.980.000.000.000.011.000.010.000.980.000.000.010.001.000.010	0.00 C39 0.00 C4 0.00 C4 0.00 C41 0.00 C41 0.00 C42 0.00 C43 0.00 C44 0.00 C45 0.00 C44 0.00 C44 0.00 C44 0.00 C44 0.00 C45 0.00 C44 0.00 C45 0.00 C44 0.00 C45 0.00 C45 0.00 C46 0.00 C45 0.00 C55 0.00 C66 0.00 C61 0.00 C62 0.00 C61 0.00 C62 0.00 C61 0.00 C62 0.00 C61 0.00 C62 0.00 C62 0.00 C61 0.00 C62 0.00 0.0	1.00 1.00	0.01 0. 0.02 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.05 0. 0.06 0. 0.07 0. 0.01 0. 0.02 0. 0.01 0. 0.02 0. 0.72 0. 0.73 0. 1.00 0. 1.00 0. 0.02 0. 0.03 0. 0.04 0. 0.05 0. 0.06 0. 0.07 0. 0.08 0. 0.09 0. 0.09 0. 0.00 0. 0.00 0. 0.00 0. 0.00	00 0.00 01 0.00 02 0.00 02 0.00 02 0.00 02 0.00 02 0.00 02 0.00 02 0.00 02 0.00 02 0.00 03 0.00 044 0.00 05 0.00 02 0.00 03 0.00 04 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05	0.31 0.1 0.30 0.1 0.30 0.1 0.33 0.1 0.00 0.1 0.00 0.1 0.97 0.1 0.97 0.1 0.31 0.1 0.35 0.1 0.37 0.1 0.38 0.1 0.397 0.1 0.31 0.1 0.35 0.1 0.31 0.1 0.27 0.1 0.30 0.1 0.400 0.1 0.31 0.1 0.32 0.1 0.33 0.1 0.400 0.1 0.32 0.1 0.32 0.1 0.32 0.1	0 0.00 0 0.00	0.68 0.68 0.65 0.00 0.63 0.00 0.00 0.00 0.00 0.00 0.00	0.01 0.02 0.95 0.06 0.00 0.93 0.00 0.93 0.92 0.94 0.92 0.94 0.95 0.84 0.25 0.00 0.00 0.00 0.00 0.00 0.00 0.00
0.00 c16 c17 c17 0.00 c18 c18 0.00 c18 c18 0.00 c18 c19 0.00 c21 0.00 c22 0.00 c21 0.00 c21 0.00 c22 0.00 c23 0.00 c23 0.00 c33 0.00 c33 0.00 c33 0.00 c34 0.00 c3	1.000.010.000.000.000.000.000.000.000.001.000.020.000.000.000.000.000.000.000.001.000.020.000.000.980.000.000.000.001.000.020.000.000.980.000.000.000.001.000.020.000.000.970.000.000.000.001.000.000.000.000.970.000.000.010.001.000.000.000.000.310.000.000.010.011.000.000.000.000.310.000.000.000.011.000.000.000.970.000.000.000.010.011.000.020.010.000.310.000.000.000.031.000.020.010.000.980.000.000.000.011.000.020.010.000.980.000.000.000.011.000.020.000.980.000.000.000.000.011.000.010.000.980.000.000.020.001.000.010.000.980.000.000.000.011.000.010.000.980.000.000.010.001.000.010	0.00 C39 0.00 C4 0.00 C4 0.00 C41 0.00 C41 0.00 C42 0.00 C43 0.00 C44 0.00 C45 0.00 C44 0.00 C44 0.00 C45 0.00 C44 0.00 C45 0.00 C45 0.00 C46 0.00 C47 0.00 C55 0.00 C56 0.00 C60 C60 C60 C60 C60 C61 0.00 C62 C52 C55 C55 0.00 C61 0.00 C62 C52 C55 C55 0.00 C61 0.00 C62 C52 C55 0.00 C62 C52 C55 C55 C55 0.00 C61 C52 C55 C55 C55 0.00 C61 C52 C55 C55 C55 0.00 C61 C62 C55 C5	1.00 1.00	0.01 0. 0.02 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.04 0. 0.05 0. 0.06 0. 0.07 0. 0.01 0. 0.02 0. 0.01 0. 0.02 0. 0.72 0. 0.73 0. 1.00 0. 1.00 0. 0.02 0. 0.03 0. 0.04 0. 0.05 0. 0.06 0. 0.07 0. 0.08 0. 0.09 0. 0.09 0. 0.00 0. 0.00 0. 0.00 0. 0.00	00 0.00 01 0.00 02 0.00 02 0.00 02 0.00 02 0.00 02 0.00 02 0.00 02 0.00 02 0.00 02 0.00 03 0.00 044 0.00 05 0.00 02 0.00 03 0.00 04 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05 0.00 05	0.31 0.1 0.30 0.1 0.30 0.1 0.33 0.1 0.00 0.1 0.00 0.1 0.97 0.1 0.97 0.1 0.31 0.1 0.35 0.1 0.37 0.1 0.38 0.1 0.397 0.1 0.31 0.1 0.35 0.1 0.31 0.1 0.27 0.1 0.30 0.1 0.400 0.1 0.31 0.1 0.32 0.1 0.33 0.1 0.400 0.1 0.32 0.1 0.32 0.1 0.32 0.1 0.32 0.1 0.32 0.1	0 0.00 0 0.00	0.68 0.68 0.65 0.00 0.63 0.00 0.00 0.00 0.00 0.00 0.00	0.01 0.02 0.95 0.06 0.00 0.93 0.00 0.93 0.92 0.94 0.92 0.94 0.95 0.84 0.25 0.00 0.00 0.00 0.00 0.00 0.00 0.00

C7	1.00	0.01	0.00	0.00	0.39	0.00	0.00	0.59	0.02
0.00 C8	1.00	0.01	0.00	0.00	0.35	0.00	0.00	0.64	0.00
0.00 C9	1.00	0.01	0.00	0.00	0.98	0.00	0.00	0.00	0.00
0.00 W24	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00 W25	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00 W26	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00 W27		0.99	0.01	0.00	0.00		0.00		0.00
0.00									
W28 0.00					0.01			0.00	
W29 0.00	1.00	0.02	0.98	0.00	0.00	0.00	0.00	0.00	0.00
W30 0.00	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
W31 0.00	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

				Hours	Hours
		Hours Full		Above Full	Capacity
				Normal Flow	
C1	0.01	0.01	2.61	0.01	0.01
C10				0.08	
C11	7.00	7.00	7.10	0.01	0.02
C12	7.10	7.10	7.39	0.01	0.01
C13	7.14	7.18	7.38	0.48	0.35
C14	7.20	7.21	7.38	0.44	0.41
C15	7.38	7.38	7.42	0.17	0.20
C16	7.47	7.47	7.70	0.14	0.16
C17	7.76	7.76	7.80	0.19	
C18	7.12	7.12	7.19	0.01	0.01
C18_1	6.52	6.52	6.62	0.03	0.07
C18_2	6.62	6.62	6.73	0.01	0.01
C19	7.19	7.19	7.25	0.11	0.16
C2		0.62			0.01
C20	7.32	7.32	23.39	0.01	0.01
C21	7.29	7.29	7.57	0.15	0.16
C21_1	6.79	6.79	6.86	0.01	0.01
C21_2	6.86	6.86	6.88	0.01	0.02
C22	7.58	7.58	7.92	0.19	0.01
C23	8.05	8.05	9.72	0.38	0.38
C24	6.39	6.39	7.10	0.01	0.01
C25	7.17	7.17	7.40	0.01	0.02
C26	6.95	6.95	7.05	0.01	0.01
C27	6.94	6.94	7.29	0.01	0.01
C27_2	6.94	6.94	7.00	0.01	0.01

C28	7.01	7.02	7.02	0.01	1
C29	7.37	7.37	23.05	0.01	0
C3	6.18	6.24	6.54	0.53	0
C30	23.06	23.06	23.06	0.01	(
C31	23.08	23.08	23.08	0.01	1
C32	23.08	23.08	24.00	0.01	(
C33	7.36	7.36	7.55	0.16	0
C34	7.61	7.61	7.92	0.08	0
C35	6.84	6.84	7.04	0.01	(
C36	7.08	7.08	7.27	0.05	0
C37	24.00	24.00	24.00	0.01	(
C38	6.70	6.70	6.93	0.01	(
C39	6.65	6.65	6.69	0.21	0
C 4	6.16	6.16	6.29	0.30	(
C40	6.43	6.43	6.61	0.01	0
C42	0.18	0.18	7.19	0.01	(
C5	6.39	6.39	6.41	0.32	0
C 6	6.46	6.47	6.62	0.28	0
C64	7.35	7.35	7.35	0.48	1
C7	4.80	4.80	6.36	0.01	0
C8	1.52	1.52	5.03	0.22	(
C 9	6.74	6.74	6.85	0.17	0
W28	0.01	0.01	22.86	0.01	(

Analysis begun on: Thu Aug 8 19:48:32 2024 Analysis ended on: Thu Aug 8 19:48:39 2024 Total elapsed time: 00:00:07

APPENDIX





STORM SEWER DESIGN SHEET LANSDOWNE 2.0 REDEVELOPMENT CITY OF OTTAWA Project: CA0033920.1056 Date: August, 2024

		LOCATION			ARE	EA (Ha)								RATIONAL	DESIGN FLOW						PROPS	SOED SEWER D	ΑΤΑ		
BLDG FLOW	AREA ID	FROM	то	C=	C= C=	C=	C= C=	IND	CUM		TOTAL	i (2)	i (5)	i (100)	BLDG 2yr PEAK		100yr PEAK ICD FIXED DESIGN				OPE LENGTH	CAPACITY VE			
				0.20	0.35 0.75	0.80	0.90 1.00	2.78AC	2.78 AC	(min)	(min)	(mm/hr)	(mm/hr)	(mm/hr)	FLOW (L/s) FLOW (L/s)) FLOW (L/s)	FLOW (L/s) FLOW (L/s) FLOW (L/s)	6) DESIGN FLOW (L/s	PIPE	(mm) (%	%) (m)	(I/s)	(m/s) IN	PIPE (L/s)	(%)
				- I - I				-				Lansd	lowne 2.0						1					<u> </u>	
+106 l/s	S. STANDS	Ex. STM 120	Ex. STM 119					0.000	0.000	20.00	21.24	52.03	70.25	119.95		0.00	0.00	106.00			20 59.60	127.63	0.80	1.24 21.63 1	6.95%
+106 l/s		Ex. STM 119 Ex. STM 118	Ex. STM 118 Ex. STM 117					0.000			22.48 22.63	50.12 48.36	67.64 65.24	115.46 111.33		0.00	0.00	106.00 212.00		450.0 0.2 600.0 0.2				1.24 21.63 1 0.15 62.87 2	
+1001/5		EX. 5111110	Ex. 31101117					0.000	0.000	22.40	22.03	40.30	05.24	111.55		0.00	0.00	212.00	CONC	000.0 0.2	20 0.70	274.07	0.97	0.15 02.87 2	2.07 %
		Ex. STM 117	STMH 208					0.000	0.000	22.63	22.68	48.16	64.97	110.85		0.00	0.00	212.00	CONC	600.0 0.2	20 3.00	274.87	0.97	0.05 62.87 2	2.87%
A3	3, A4, A5, BLDG I, K,							_																	
+232.6 l/s	N STANDS	Ex. STM 115	Ex. STM 114	1.118			0.399	1.620	_		21.02	52.03	70.25	119.95		113.80	113.80	346.40			20 73.70	642.59		1.02 296.19 4	
		Ex. STM 114	STMH 209					0.000	1.620	21.02	22.06	50.44	68.08	116.22		110.29	110.29	342.89	CONC	825.0 0.2	20 74.50	642.59	1.20	1.03 299.71 4	<u>3.64%</u>
	Half of NEC Area	STMH 209	STMH 208	0.000			0.486	1.215	2.835	22.06	23.27	48.94	66.04	112.69		187.19	187.19	419.79	CONC	900.0 0.1	10 65.64	573.05	0.90	1.22 153.26 20	6.74%
Q _{bldg Tot} = 444.6																									
I/s		STMH 208	STMH 207					0.000	2.835	23.27	23.58	47.30	63.80	108.84		180.85	180.85	625.45	CONC	1050.0 0.	10 18.55	864.40	1.00	0.31 238.95 2 ⁻	7.64%
			CTMUL 000					0.000	0.005	00.50	00.07	40.00	<u> </u>	107.01		170.01	170.01	C00.01	00N0	1050.0	10 00 14	004.40	1.00		7.000/
		STMH 207	STMH 206					0.000	2.835	23.58	23.97	46.90	63.26	107.91		179.31	179.31	623.91	CONC	1050.0 0.	10 23.14	864.40	1.00 (0.39 240.49 2	/.82%
	A6	STMH 206	STMH 205	0.048			0.025	0.089	2.924	23.97	24.61	46.41	62.59	106.77		183.01	183.01	627.61	CONC	1050.0 0. ⁻	10 38.05	864.40	1.00	0.64 236.79 2	7.39%
		STMH 205	STMH 204					0.000	2.924	24.61	25.10	45.64	61.53	104.94		179.92	179.92	624.52	CONC	1050.0 0. ⁻	10 29.50	864.40	1.00).49 239.89 2	7.75%
	Half of NEC Area	STMH 204	STMH 203	0.000			0.486	1.215	4.139	25.10	25.55	45.05	60.74	103.58		251.38	251.38	695.98	CONC	1050.0 0. ⁻	10 27.14	864.40	1.00 (0.45 168.43 1) .48%
	Great Lawn 5	STMH 203	CBMH 202	0.089			0.026	0.115	4.253	25.55	26.25	44.53	60.03	102.36		255.31	255.31	699.91	CONC	1050.0 0.1	10 41.65	864.40	1.00	0.70 164.49 1	9.03%
Gre	eat Lawn 6, A, D, D1,							_																	
	D2	Ex. STMD	CBMH 210	1.237			0.542	2.044	2.044	20.00	20.83	52.03	70.25	119.95		143.58	143.58		CONC	600.0 0. ⁻	10 34.40	194.36	0.69	0.83 50.78 2	6.13%
	Great Lawn 4	CBMH 210	CBMH 202	0.160			0.024	0 1 4 9	2.193	20.83	21.27	50.73	68.47	116.88		150.15	150.15		CONC	600.0	10 22.20	194.36	0.69).54 44.22 23	2 75%
	Gleat Lawit 4	OBMIN 210		0.100			0.024	0.149	2.195	20.03	21.57	50.75	00.47	110.00		150.15	130.13		CONC	000.0 0.	10 22.20	194.30	0.09	0.04 44.22 2	2.75%
$Q_{\text{bldg Tot}} = 444.6$								0.000	0.440	00.05	00.05	40.75	50.07	100 54		000.45	000.45	004 75		-			DEGLONI		
I/S		CBMH 202	CHAMBER / Ex. Chamber					0.000	6.446	26.25	26.25	43.75	58.97	100.54		380.15	380.15	824.75				STORMTECH	DESIGN		
				0.000			0.404	0.455	0.004	00.05	00.05	40.75	50.07	100 54		400.05	400.05	054.55	1	•					
Or	PGG5, Great Lawn 3	CHAMBER / Ex. Chamber	Ex. 1350 PIPE	0.228			0.131	0.455	6.901	26.25	26.25	43.75	58.97	100.54		406.95	406.95	851.55				STORMTECH	DESIGN		
	, BLDGS H, G, J, J1,																								
+23.1 l/s	J2	Ex. STM-CCN1 NEW STMH 212	NEW STMH 212 NEW STMH 211	0.019			0.938	2.357 0.000			20.21 20.72		70.25 69.80	119.95 119.18		165.61 164.55	165.61 164.55	<u>188.71</u> 187.65	CONC CONC	600.0 0.2 600.0 0.2	20 12.03 20 30.00			0.2186.1630.5187.223	
		NEW STMH 211	Ex. STM 110					0.000	2.357	20.72	20.91	50.90	68.71	117.29		161.97	161.97	185.07	CONC	600.0 0.2	20 11.00	274.87	0.97	0.19 89.80 3	2.67%
Q _{bldg Tot} = 467.7	OPGG1, OPGG4	Ex. STM 110	Ex. STM 109	0.015			0.160	0.409	2.766	20.91	21.11	50.61	68.31	116.62		188.97	188.97	212.07	CONC	600.0 0.2	20 11.70	274.87	0.97	0.20 62.81 2	2.85%
l/s	OPGG2	Ex. STM 109	Ex. STM 108	0.020			0.251	0.639	10.306	26.25	27.49	43.75	58.97	100.54		607.77	607.77	1075.47	CONC	1350.0 0.1	13 99.80	1926.37	1.34	1.24 850.90 4	4.17%
	102, AA, BB, EE	Ex. STMDD	Ex. STMFF	1 410			0.594	0.070	0.070	01.70	00.07	40.45	66.70	110.00		151.40	151.40		CONC		10 21 00	E70.0E	0.00		0.579/
	102, AA, BB, EE	EX. STMDD	EX. STMFF	1.410			0.594	2.270	2.270	21.70	22.27	49.45	66.73	113.88		151.48	151.48		CONC	900.0 0.	10 31.00	573.05	0.90	0.57 421.57 73	3.57%
Gi	ireat Lawn 1 & 2, T1,		5. 07400	0.500			0.005	1 001	0.001	00.07	00.00	40.04	05.00	444.00		045.05	015.05		00110		10 57.00	570.05	0.00		0.000/
	T2, V1, V2	Ex. STMFF	Ex. STMGG	0.508			0.295	1.021	3.291	22.27	23.33	48.64	65.62	111.98		215.95	215.95		CONC	900.0 0.1	10 57.00	573.05	0.90	1.06 357.10 6	2.32%
		Ex. STMGG	Ex. STM 108					0.000	3.291	23.33	23.74	47.23	63.70	108.67		209.61	209.61		CONC	900.0 0.	10 22.00	573.05	0.90	0.41 363.43 6	3.42%
$Q_{bldg Tot} = 467.7$								+																	
I/s	OPGG3, 108	Ex. STM 108	Ex. STM 107	0.167			0.316	0.883	14.480	27.49	28.64	42.45	57.20	97.49		828.21	828.21	1295.91	CONC	1350.0 0.	10 81.40	1689.54	1.18	1.15 393.63 2	3.30%
+34.4 l/s, Qbldg				+		$\left \right $																			
Tot = 502.1 l/s A2	2, BLDGS A, B, C, D	Ex. STM 107	Ex. STM 106	0.032			1.555	3.908	18.388	28.64	28.93	41.31	55.65	94.82		1023.27	1023.27	1525.37	CONC	1350.0 0.	10 20.70	1689.54	1.18	0.29 164.17 9).72%
l		Ex. STM 106	Ex. STM 105	+		$\left \right $		_									616.00		CONC	975.0 0	10 80.20	709.40	0.95	1.41 93.40 1	3 17%
	-	Ex. STM 105	Ex. STM 104														616.00		CONC	975.0 0.1	10 12.10	709.40	0.95	0.21 93.40 1	3.17%
Controlle	ed Flow	Ex. STM 104	Ex. STM 103														616.00		CONC	975.0 0.1	10 19.20	709.40	0.95	0.34 93.40 1	3.17%
		Ex. STM 103 Ex. STM 102	Ex. STM 102 Ex. STM 101			+											616.00 616.00				10 54.20 10 24.20			0.9593.40130.4293.4013	
ļ		Ex. STM 101	Ex. STM MH (O'Connnor)											1			616.00				10 5.80			0.10 93.40 1	
Definition:				Notes:										Designed:	Z.A.		No.		Revision					Date	
Q=2.78CiA, where:					gs coefficient (n) =	0.013		Concentratio						- signour	/ \·		1.	City Su	bmission No. 1					2023-05-25	
Q = Peak Flow in Litres	,							ation: t (min	,	-	-			Chasked	D D Y		2.		bmission No. 2					2023-09-22	
A = Area in Hectares (H i = Rainfall Intensity in	ma) millimeters per hour (mi	m/hr)					wnere: L	Longest Wat	Runof	ff Coef.C =	, , , ,	Impervious		Checked:	D.B.Y.		J.	City St	bmission No. 3					2024-08-07	
i = 732.951/(TC+6.1	199)^0.810		2 Year					No.	L (m)																
i = 1174.184/(TC+6 i = 1735.688/(TC+6			5 Year 100 Year								#DIV/0!	J		Dwg. Referer	F2		File Reference			Dat	e:			Sheet No:	
/ 00.000/(10+0																	CA0002045.0622			2023-0				1 of 1	
																									the second se



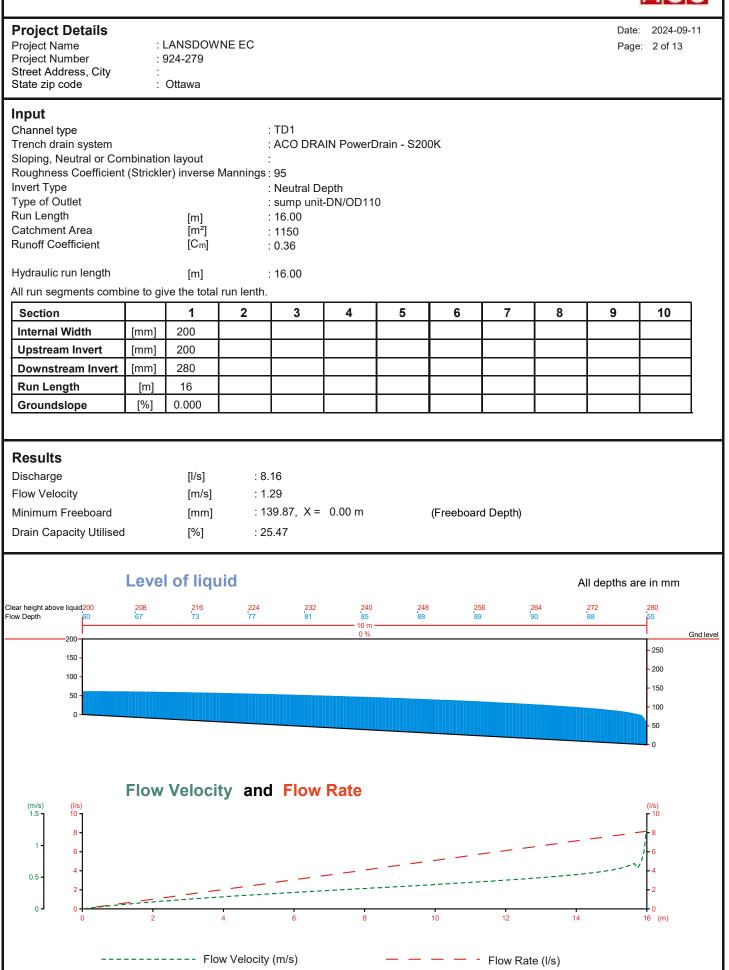


												ACO
Project Project	Number Address, City	: LANSDC : 924-279 : : Ottawa		C								te: 2024-09-11 ge: 1 of 13
	iny it Name Address, City											
Input Locatio		: Ottawa										
	Catchment Desc			Area [m²]		с	D [min]	F [a]	l [mm/hr]	Catchn	nent Surface Type	Installatio
1	CB02 to TD1			1150.	0 0.3	36	0	0	71			
2	CB03 to TD2			545.0	_		0	0	355			
3	CB05 to TD3			2420.			0	0	160			
4	CB06 to TD4			3190.	0 0.	56	0	0	110			
5	CB07 to TD5			1840.	0 0.:	29	0	0	50			
6	CB08 to TD6			2500.	0 0.:	26	0	0	35			
Channe	el type		Catch	ment (s)		hmen a [m²]		m	Total run l [m]	ength	Applica	ition
TD1			1			50.00		.36	16.00			
TD2			2		54	5.00	0	.90	13.50			
TD3			3		242	20.00	0	.39	12.50			
TD4			4			90.00		.56	21.50			
TD5			5			40.00		.29	22.00			
TD6			6		250	00.00	0	.26	25.00			

ACO Systems Ltd.

2910 Brighton Rd L6H 5S3 Oakville





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Project Details

Project Details Project Name Project Number Street Address, City State zip code		: LANSDOWNE EC : 924-279 : : Ottawa	Date: Page	2024-09-11 3 of 13
Channel type		: TD1		
Trench drain system		: ACO DRAIN PowerDrain - S200K		
Sloping, Neutral or Comb	ination layout	:		
Type of Outlet		: sump unit-DN/OD110		
Run Length	[m]	: 16.00		
Hydraulic run length	[m]	: 16.00		

Notes

Installation

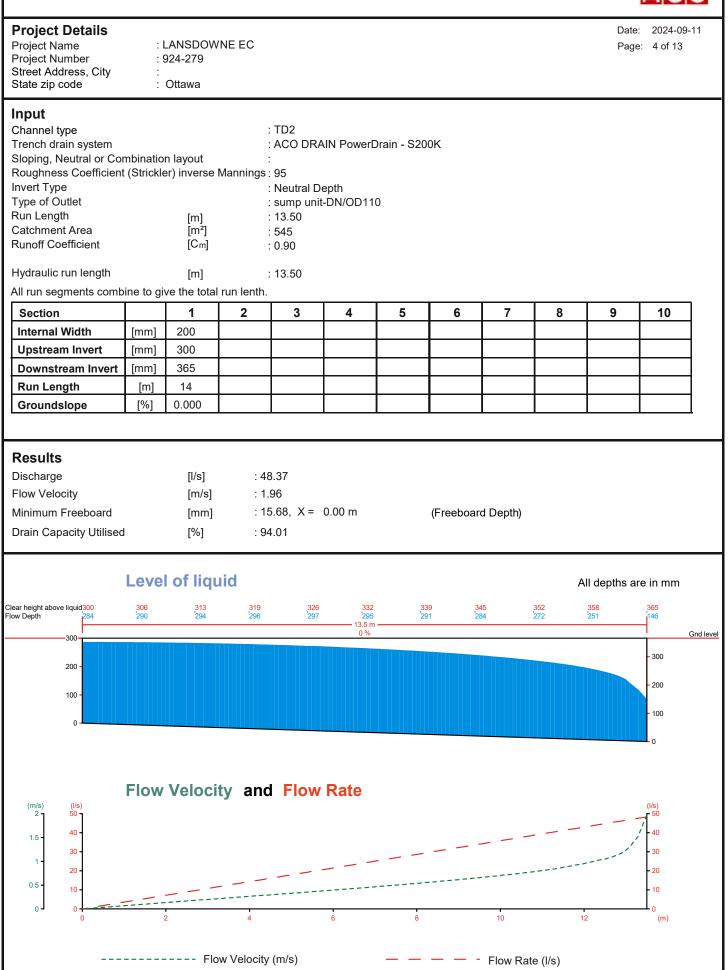
Legend LC = Load Class according to EN1433 (A15; B125; C250; D400; E600; F900)

SU = Catch Basin

SU = Catch Basin AU = Access Unit VO = Vertical Outlet FO = Free Outflow EO = End Outlet LO = Lateral Outlet A = Adapter B = Pieto

P = Plate





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Project Details

Project Details Project Name Project Number Street Address, City State zip code		: LANSDOWNE EC : 924-279 : : Ottawa	Date Page	: 2024-09-11 : 5 of 13
Channel type		: TD2		
Trench drain system		: ACO DRAIN PowerDrain - S200K		
Sloping, Neutral or Comb	ination layout	:		
Type of Outlet		: sump unit-DN/OD110		
Run Length	[m]	: 13.50		
Hydraulic run length	[m]	: 13.50		

Notes

Installation

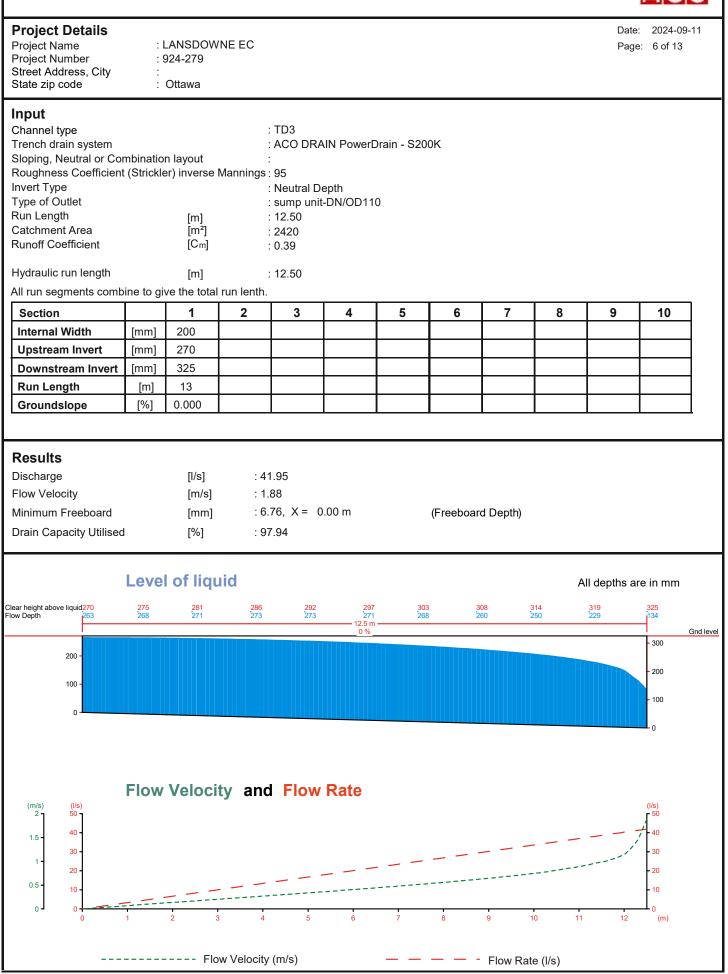
Legend LC = Load Class according to EN1433 (A15; B125; C250; D400; E600; F900)

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P = Plate





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Project Details

Project Details Project Name Project Number Street Address, City State zip code		: LANSDOWNE EC : 924-279 : : Ottawa	Date: 2024-09-11 Page: 7 of 13
Channel type		: TD3	
Trench drain system		: ACO DRAIN PowerDrain - S200K	
Sloping, Neutral or Combi	ination layout	:	
Type of Outlet		: sump unit-DN/OD110	
Run Length	[m]	: 12.50	
Hydraulic run length	[m]	: 12.50	

Notes

Installation

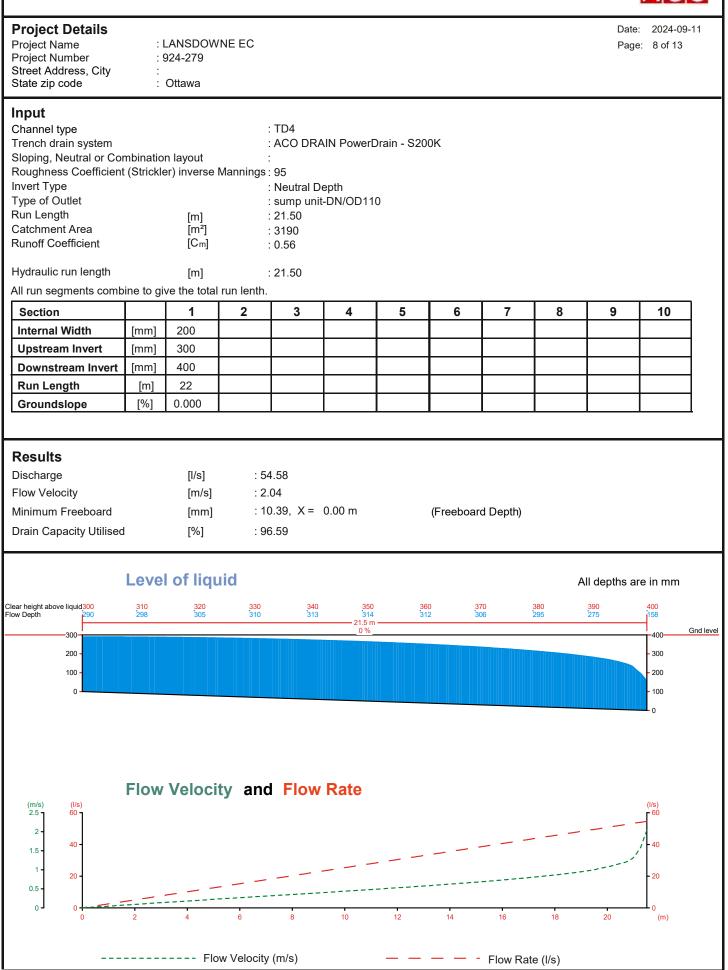
Legend LC = Load Class according to EN1433 (A15; B125; C250; D400; E600; F900)

SU = Catch Basin

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P = Plate





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Project Details

Project Details Project Name Project Number Street Address, City State zip code		: LANSDOWNE EC : 924-279 : : Ottawa	Date: Page	2024-09-11 9 of 13
Channel type		: TD4		
Trench drain system		: ACO DRAIN PowerDrain - S200K		
Sloping, Neutral or Combi	ination layout	:		
Type of Outlet		: sump unit-DN/OD110		
Run Length	[m]	: 21.50		
Hydraulic run length	[m]	: 21.50		

Notes

Installation

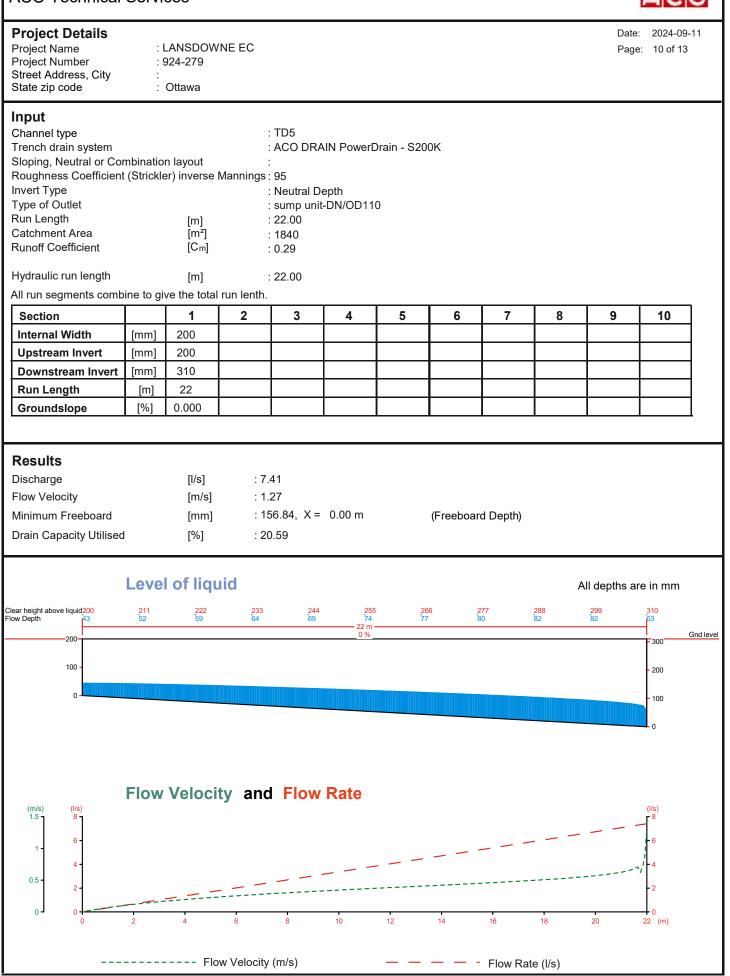
Legend LC = Load Class according to EN1433 (A15; B125; C250; D400; E600; F900)

SU = Catch Basin

SU = Catch Basin AU = Access Unit VO = Vertical Outlet FO = Free Outflow EO = End Outlet LO = Lateral Outlet A = Adapter B = Pieto

P = Plate





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Project Details

Project Details Project Name Project Number Street Address, City State zip code		: LANSDOWNE EC : 924-279 : : Ottawa	Da Pa	te: 2024-09-11 ge: 11 of 13
Channel type		: TD5		
Trench drain system		: ACO DRAIN PowerDrain - S200K		
Sloping, Neutral or Combin	nation layout	:		
Type of Outlet		: sump unit-DN/OD110		
Run Length	[m]	: 22.00		
Hydraulic run length	[m]	: 22.00		

Notes

Installation

Legend LC = Load Class according to EN1433 (A15; B125; C250; D400; E600; F900)

SU = Catch Basin

SU = Catch Basin AU = Access Unit VO = Vertical Outlet FO = Free Outflow EO = End Outlet LO = Lateral Outlet A = Adapter B = Pieto

P = Plate



Project Details Date: 2024-09-11 Project Name : LANSDOWNE EC Page: 12 of 13 Project Number : 924-279 Street Address, City State zip code Ottawa Input Channel type : TD6 : ACO DRAIN PowerDrain - S200K Trench drain system Sloping, Neutral or Combination layout Roughness Coefficient (Strickler) inverse Mannings: 95 Invert Type : Neutral Depth Type of Outlet : sump unit-DN/OD110 Run Length : 25.00 [m] Catchment Area [m²] : 2500 **Runoff Coefficient** [Cm] : 0.26 Hydraulic run length [m] : 25.00 All run segments combine to give the total run lenth. 1 2 3 4 5 6 7 8 9 10 Section Internal Width 200 [mm] **Upstream Invert** [mm] 200 325 **Downstream Invert** [mm] 25 **Run Length** [m] Groundslope [%] 0.000 **Results** Discharge [l/s] : 6.32 Flow Velocity [m/s] : 1.23 Minimum Freeboard : 165.77, X = 0.00 m (Freeboard Depth) [mm] Drain Capacity Utilised [%] : 16.61 Level of liquid All depths are in mm Clear height above liquid200 Flow Depth 212 225 237 55 262 64 275 68 287 71 300 312 74 325 250 60 19 Gnd leve 0 % 200 300 100 200 0 100 Flow Velocity and Flow Rate (m/s)(l/s) (l/s)1.5 6 4 0.5 2. 10 12 14 16 18 20 22 24 (m) ----- Flow Velocity (m/s) Flow Rate (I/s) -

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Project Details

Project Details Project Name Project Number Street Address, City State zip code		: LANSDOWNE EC : 924-279 : : Ottawa	Dat Paç	e: 2024-09-11 ge: 13 of 13
Channel type		: TD6		
Trench drain system		: ACO DRAIN PowerDrain - S200K		
Sloping, Neutral or Combi	nation layout	:		
Type of Outlet		: sump unit-DN/OD110		
Run Length	[m]	: 25.00		
Hydraulic run length	[m]	: 25.00		

Notes

Installation

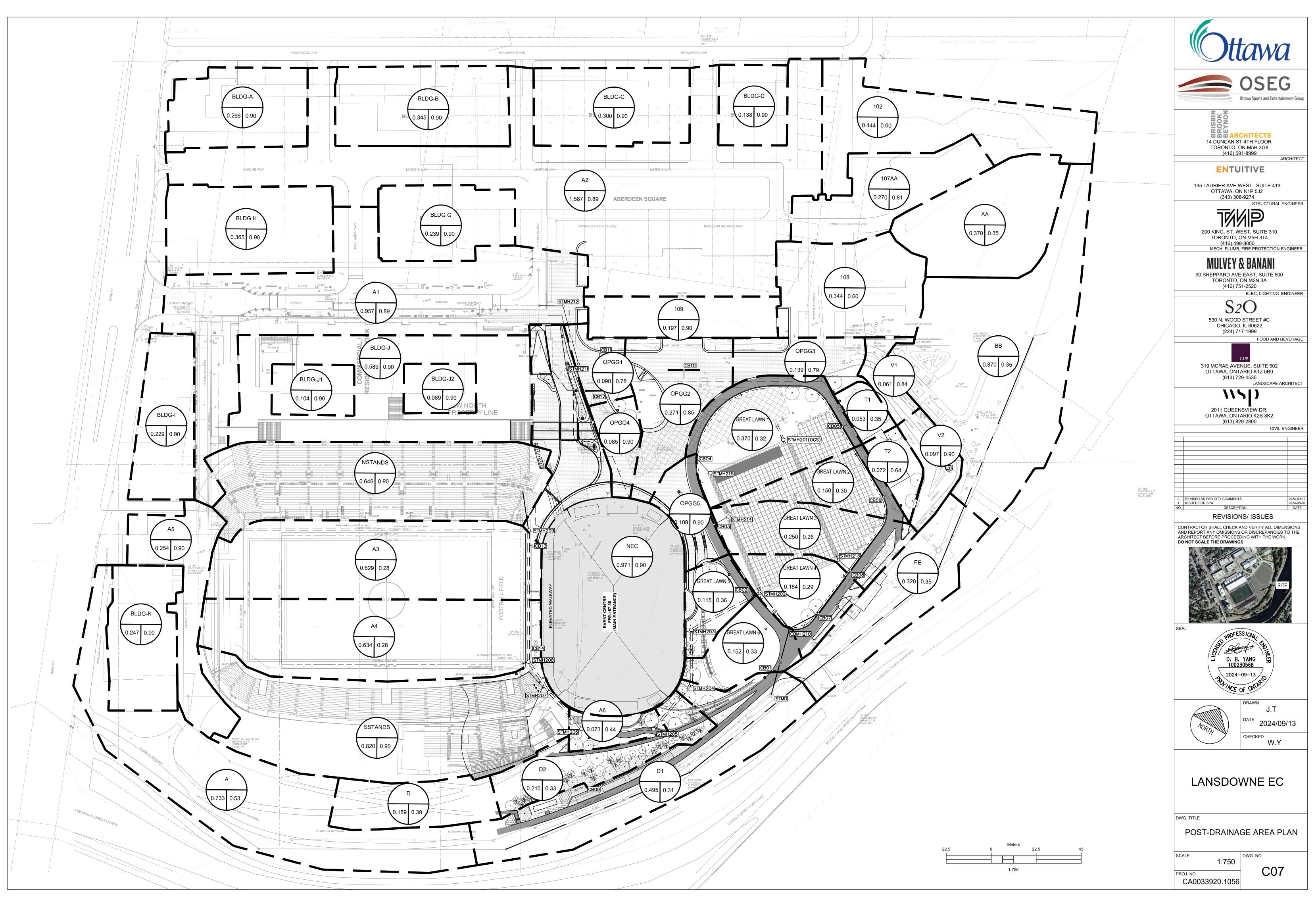
Legend LC = Load Class according to EN1433 (A15; B125; C250; D400; E600; F900)

SU = Catch Basin

SU = Catch Basin AU = Access Unit VO = Vertical Outlet FO = Free Outflow EO = End Outlet LO = Lateral Outlet A = Adapter B = Pieto

P = Plate

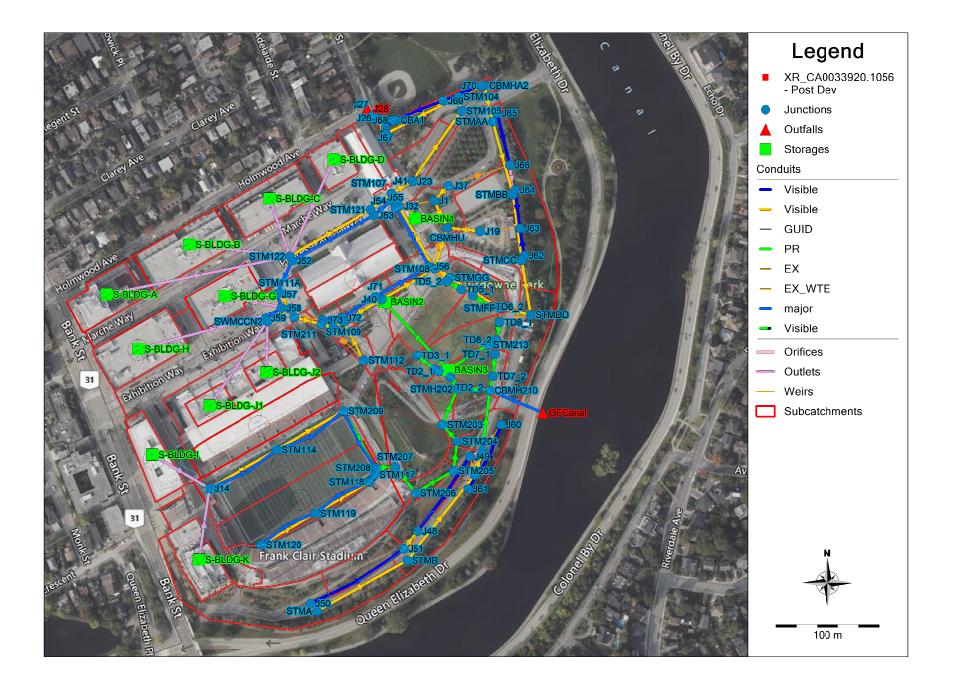




DATE PLOTTE

			Flow Length	Slope	Imperv.
Name	Area (ha)	Width (m)	(m)	(%)	(%)
102	0.444	44.4	100.14	0.5	64.2
107AA	0.270	176.7	15.28	0.5	86.3
108	0.344	162.7	21.16	0.5	68.5
109	0.198	88.9	22.24	0.5	87.5
A	0.733	43.0	170.37	0.5	47.4
A1	0.957	234.9	40.75	0.5	98.5
A2	1.578	358.2	44.06	0.5	97.9
A3	0.770	217.1	35.45	0.5	100.0
A4	0.623	170.2	36.59	2	100.0
A5	0.246	30.9	79.59	0.5	99.9
A6	0.073	14.9	49.23	0.5	44.0
AA	0.370	72.8	50.84	0.5	54.4
BB	0.891	50.5	176.24	0.5	41.1
BLDG-A	0.254	254.2	10.00	0.5	100.0
BLDG-B	0.363	362.6	10.00	0.5	100.0
BLDG-C	0.299	299.3	10.00	0.5	100.0
BLDG-D	0.138	138.0	10.00	0.5	100.0
BLDGG	0.243	242.9	10.00	0.5	100.0
BLDGH	0.371	370.9	10.00	0.5	100.0
BLDG-I	0.226	225.6	10.00	0.5	100.0
BLDG-J	0.604	604.4	10.00	0.5	100.0
BLDG-J1	0.104	103.9	10.00	0.5	100.0
BLDG-J2	0.089	89.2	10.00	0.5	100.0
BLDG-K	0.247	247.3	10.00	0.5	100.0
D	0.189	38.7	48.90	0.5	27.1
D_2	0.210	38.7	54.30	0.5	19.1
D1	0.495	271.3	18.25	0.5	15.2
EE	0.353	38.6	91.52	0.5	15.3
Great-Lawn_1	0.370	75.0	49.33	0.5	17.0
Great-Lawn_2	0.150	46.0	32.61	0.5	15.0
Great-Lawn_3	0.250	41.0	61.05	0.5	9.0
Great-Lawn_4	0.184	49.7	37.08	0.5	13.0
Great-Lawn_5	0.115	45.5	25.20	0.5	23.0
 Great-Lawn_6	0.152	40.0	38.05	0.5	18.0
 Great-Lawn_9	0.000	135.1	0.00	0.5	19.0
 NEC1	0.486	247.7	19.62	10	99.0
NEC2	0.486	247.7	19.62	10	99.0
NSTANDS	0.472	62.2	75.86	2	100.0
OPGG 1	0.090	42.8	20.94	0.5	83.0
OPGG 2	0.273	83.0	32.86	0.5	93.0
OPGG 3	0.139	67.0	20.70	0.5	84.0
OPGG 4	0.085	47.0	18.00	0.5	99.0

OPGG5	0.109	42.0	25.95	0.5	99.0
SSTANDS	0.786	162.6	48.34	10	100.0
Т	0.131	75.9	17.24	0.5	27.8
V_1	0.061	167.8	3.62	0.5	96.6
V_2	0.097	167.8	5.77	0.5	96.6



EPA STORM WATER MANA												
WARNING 03: negative					Raingage Sur ***********							
ARNING 03: negative ARNING 10: crest el				rt for regulator Link W26	Name	D	ata Source			Data	Record	
RNING 02: maximum	depth increased	d for Node (CBA1	te for regulator blink wro								
NING 02: maximum NING 02: maximum					100yr_3hr_Ch 100yr_3hr_Ch					INTENSIT Increase		
NING 02: maximum NING 02: maximum					10 min. 100yr 6hr Cb							
NING 02: maximum	depth increased	d for Node 3	J14		100yr_6hr_Ch				_Chicago_		Y 10 m: 20percent	
RNING 02: maximum RNING 02: maximum					10 min. 100yr-SCS_12	hr Type II	100vr-SCS	12hr Type		INTENS	ITY 6	min.
RNING 02: maximum	depth increased	d for Node 3	J37		100yr-SCS_24	hr_Type_II	100yr-SCS	24hr_Type		INTENS	ITY 15	min.
RNING 02: maximum RNING 02: maximum					10yr_3hr_Ch 10yr_6hr_Ch		0yr_3hr_Ch: 0yr_6hr_Ch:			INTENSIT INTENSIT	Y 10 m: Y 10 m:	
RNING 02: maximum	depth increased	d for Node S	STM112		25mm_3hr_Ch:	icago 25	5mm_3hr_Ch:	icago		INTENSIT	Y 10 m:	in.
ARNING 02: maximum ARNING 02: maximum					25mm_4hr_Ch: 25yr_3hr_Ch:	icago 25	5mm_4hr_Ch: 5yr_3hr_Ch:			INTENSIT INTENSIT	Y 10 m:	in.
ARNING 02: maximum ARNING 02: maximum					25yr_6hr_Chi 2yr_3hr_Chi	Lcago 25	5yr_6hr_Ch: yr_3hr_Chio	icago		INTENSIT INTENSIT		
ARNING 02: maximum	depth increased	d for Node S	STM120		2yr_6hr_Chic	ago 23	yr_6hr_Chio	cago		INTENSIT	Y 10 m:	in.
RNING 02: maximum RNING 02: maximum					50yr_3hr_Ch: 50yr_6hr_Ch:		0yr_3hr_Ch: 0yr 6hr Ch:			INTENSIT INTENSIT		
RNING 02: maximum	depth increased	d for Node S	STM209		5yr_3hr_Chic	cago 5y	yr_3hr_Chio	cago		INTENSIT	Y 10 m:	in.
RNING 02: maximum RNING 02: maximum					5yr_6hr_Chio	ago 53	yr_6hr_Chio	cago		INTENSIT	Y 10 m:	1n.
RNING 02: maximum RNING 02: maximum					*********	*******						
RNING 02: maximum	depth increased	d for Node S	STMC		Subcatchment							
RNING 02: maximum RNING 02: maximum					**************************************	*******	Area	Width	%Imperv	%S1op	e Rain Ga	arre
RNING 02: maximum	depth increased	d for Node S	STMDD		Outlet							
RNING 02: maximum RNING 02: maximum												
RNING 02: maximum	depth increased	d for Node 🤅	TD2_1		102 J67		0.44	44.37	64.22	0.500	0 100yr_:	3hr_C
RNING 02: maximum RNING 02: maximum	depth increased	d for Node 1	TD3_2		107AA		0.27	176.73	86.34	0.500	0 100yr_:	3hr_C
RNING 02: maximum RNING 02: maximum	depth increased	d for Node 1	TD5_1		J23 108		0.34	162.73	68.53	0.500	0 100yr_:	3hr C
RNING 02: maximum	depth increased	d for Node 1	TD6_2		BASINI							
RNING 02: maximum RNING 02: maximum	depth increased	d for Node 🤅	TD7_1		STM109		0.20	88.92	87.49		0 100yr_3	_
RNING 02: maximum	depth increased	d for Node 1	TD8 1		A J50		0.73	43.00	47.40	0.500	0 100yr_:	3hr_C
RNING 02: maximum	depth increased	d for Node ?	TD8_2		A1 J59		0.96	234.86	98.54	0.500	0 100yr_:	3hr_0
* * * * * * * * * * *					A2		1.58	358.18	97.91	0.500	0 100yr_:	3hr_0
ement Count ******					J52 A3		0.77	217.10	100.00		0 100yr_:	
mber of rain gages					STM114							
mber of subcatchme mber of nodes	106				A4 STM119		0.62	170.22	100.00		0 100yr_3	
mber of links mber of pollutants					A5 J14		0.25	30.92	99.94	0.500	0 100yr_:	3hr_0
mber of pollutants mber of land uses					A6 STM206		0.07	14.87	44.00	0.500	0 100yr_:	3hr_0
4	0.37	72.80	54.39	0.5000 100yr_3hr_Chicago	OPGG5 TD3 1		0.11	42.00	99.00	0.500	0 100yr_:	3hr_C
3	0.37 0.89		54.39 41.05	0.5000 100yr_3hr_Chicago 0.5000 100yr_3hr_Chicago	TD3_1 SSTANDS		0.11 0.79	42.00	99.00 99.99		0 100yr_: 0 100yr_:	-
DG-A		50.53			TD3_1 SSTANDS STM119 T1					10.000		- 3hr_C
3 LDG-A LDG-A	0.89	50.53 254.20	41.05 100.00	0.5000 l00yr_3hr_Chicago 0.5000 l00yr_3hr_Chicago	TD3_1 STANDS STM119 T1 TD5_1		0.79	162.57 71.00	99.99 24.40	10.000 0.500	0 100yr_3	- 3hr_0 3hr_0
DG-A DG-A DG-B DG-B	0.89 0.25 0.36	50.53 254.20 362.60	41.05 100.00 100.00	0.5000 100yr_3hr_Chicago 0.5000 100yr_3hr_Chicago 0.5000 100yr_3hr_Chicago	TD3_1 STTANDS STMI19 T1 TD5_1 T2 TD6_1		0.79 0.05 0.08	162.57 71.00 75.86	99.99 24.40 27.76	10.000 0.500 0.500	0 100yr_3 0 100yr_3 0 100yr_3	3hr_C 3hr_C 3hr_C
B LDG-A LDG-B LDG-B LDG-C	0.89 0.25 0.36	50.53 254.20 362.60	41.05 100.00	0.5000 l00yr_3hr_Chicago 0.5000 l00yr_3hr_Chicago	TD3_1 STANDS STM119 T1 TD5_1 T2		0.79	162.57 71.00	99.99 24.40	10.000 0.500 0.500	0 100yr_3	3hr_C 3hr_C 3hr_C
3 LDG-A LDG-B LDG-B LDG-C LDG-C LDG-C LDG-C	0.89 0.25 0.36	50.53 254.20 362.60 299.30	41.05 100.00 100.00	0.5000 100yr_3hr_Chicago 0.5000 100yr_3hr_Chicago 0.5000 100yr_3hr_Chicago	TD3_1 SSTANDS STMN19 T1 TD5_1 T2 TD6_1 V_1 TD5_2 V_2 V_2		0.79 0.05 0.08	162.57 71.00 75.86	99.99 24.40 27.76	10.000 0.500 0.500 0.500	0 100yr_3 0 100yr_3 0 100yr_3	3hr_C 3hr_C 3hr_C 3hr_C 3hr_C
DG-A DG-B DG-B DG-C DG-C DG-C DG-D DG-D DGG	0.89 0.25 0.36 0.30	50.53 254.20 362.60 299.30 138.00	41.05 100.00 100.00 100.00	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago	TD3_1 SSTANDS STMI13 T1 TD5_1 T2 TD5_1 V_1 V_1 TD5_2		0.79 0.05 0.08 0.06	162.57 71.00 75.86 78.30	99.99 24.40 27.76 96.59	10.000 0.500 0.500 0.500	0 100yr_3 0 100yr_3 0 100yr_3 0 100yr_3	3hr_C 3hr_C 3hr_C 3hr_C 3hr_C
DG-A DG-A DG-B DG-B DG-C DG-C DG-C DG-C DG-D DG-G DG-G DG-H DG-H	0.89 0.25 0.36 0.30 0.14	50.53 254.20 362.60 299.30 138.00 242.90	41.05 100.00 100.00 100.00 100.00	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago	TD3_1 SSTANDS STMN19 T1 TD5_1 T2 TD6_1 V_1 TD5_2 V_2 V_2		0.79 0.05 0.08 0.06	162.57 71.00 75.86 78.30	99.99 24.40 27.76 96.59	10.000 0.500 0.500 0.500	0 100yr_3 0 100yr_3 0 100yr_3 0 100yr_3	3hr_C 3hr_C 3hr_C 3hr_C 3hr_C
DG-A DG-B DG-B DG-C DG-C DG-C DG-D DG-D DG-D DG-G DG-G	0.89 0.25 0.36 0.30 0.14 0.24	50.53 254.20 3 362.60 3 138.00 3 242.90 3 370.90 3	41.05 100.00 100.00 100.00 100.00	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago	TD3_1 SSTANDS STM19 T1 TD5_1 T2 TD6_1 V_1 TD5_2 V_1 TD5_2 V_2 TD6_1	7	0.79 0.05 0.08 0.06	162.57 71.00 75.86 78.30	99.99 24.40 27.76 96.59	10.000 0.500 0.500 0.500	0 100yr_3 0 100yr_3 0 100yr_3 0 100yr_3	3hr_C 3hr_C 3hr_C 3hr_C 3hr_C
DG-A DG-B DG-B DG-C DG-C DG-C DG-C DG-C DG-D DG-G DG-G	0.89 0.25 0.36 0.30 0.14 0.24 0.37 0.23	50.53 254.20 3 362.60 3 138.00 3 242.90 3 370.90 3	41.05 100.00 100.00 100.00 100.00 100.00 100.00	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago	TD3_1 SSTANDS STMNI9 T1 TD5_1 T2 TD6_1 V_1 TD5_2 V_2 TD6_1	Ž.	0.79 0.05 0.08 0.06 0.10	162.57 71.00 75.86 78.30 167.82	99.99 24.40 27.76 96.59 96.59	10.000 0.500 0.500 0.500 0.500	0 100yr_: 0 100yr_: 0 100yr_: 0 100yr_: 0 100yr_: Ponded	
DG-A DG-B DG-B DG-C DG-C DG-C DG-C DG-D DG-D DG-G DG-G	0.89 0.25 0.36 0.30 0.14 0.24 0.37 0.23 0.60	50.53 254.20 2 362.60 2 138.00 2 370.90 2 225.60 2 604.40 2	41.05 100.00 100.00 100.00 100.00 100.00 100.00 100.00	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago	TD3_1 SSTANDS STMID9 T1 TD5_1 T2 TD6_1 V_1 TD5_2 V_2 TD6_1 	Ύ Τ	0.79 0.05 0.08 0.06	162.57 71.00 75.86 78.30 167.82	99.99 24.40 27.76 96.59 96.59	10.000 0.500 0.500 0.500	0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_	
DG-A DG-B DG-B DG-C DG-C DG-C DG-C DG-D DG-D DG-D DG-D	0.89 0.25 0.36 0.30 0.14 0.24 0.37 0.23	50.53 254.20 2 362.60 2 138.00 2 370.90 2 225.60 2 604.40 2	41.05 100.00 100.00 100.00 100.00 100.00 100.00	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago	TD3_1 SSTANDS STM119 T1 TD5_1 T2 TD6_1 V_1 TD5_2 V_2 TD6_1 	Г тъ л.	0.79 0.05 0.08 0.06 0.10 ype	162.57 71.00 75.86 78.30 167.82 I	99.99 24.40 27.76 96.59 96.59 96.59 96.59	10.000 0.500 0.500 0.500 0.500 Max. Depth	0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ Ponded Area 0.0	
YG-A YG-B YG-C YG-C YG-C YG-C YG-D YG-G YG-G YG-H YG-G YG-H YG-J YG-J1 YG-J2	0.89 0.25 0.36 0.30 0.14 0.24 0.37 0.23 0.60	50.53 254.20 2 362.60 2 138.00 2 370.90 2 225.60 2 604.40 2 103.90 2	41.05 100.00 100.00 100.00 100.00 100.00 100.00 100.00	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago	TD3_1 SSTANDS STMN19 T1 TD5_1 T2 TD6_1 V_1 TD5_2 V_2 TD6_1 	T) JU	0.79 0.05 0.08 0.10 0.10 ype	162.57 71.00 75.86 78.30 167.82 I	99.99 24.40 27.76 96.59 96.59 96.59	10.000 0.500 0.500 0.500 0.500 0.500 1.93 2.80	0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ Ponded Area	
۱/۵-A ۱/۵-B ۱/۵-B ۱/۵-C ۱	0.89 0.25 0.36 0.30 0.14 0.24 0.37 0.23 0.60 0.10	50.53 254.20 2 362.60 2 138.00 2 370.90 2 225.60 2 604.40 2 103.90 2	41.05 100.00 100.00 100.00 100.00 100.00 100.00 100.00	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago	TD3_1 SSTANDS STMN19 T1 TD5_1 T2 TD6_1 V_1 TD5_2 V_2 TD6_1 	דע זע זע זע זע זע	0.79 0.05 0.08 0.06 0.10 UNCTION UNCTION UNCTION	162.57 71.00 75.86 78.30 167.82 I	99.99 24.40 27.76 96.59 96.59 96.59 96.59 96.59 63.59 63.18 63.89 63.36	10.000 0.500 0.500 0.500 0.500 0.500 0.500 1.93 2.80 2.31 2.64	0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 0.00 0.0 0.0	
G-A GC-B GC-C GC-T GC-T <	0.89 0.25 0.36 0.14 0.24 0.37 0.23 0.60 0.10 0.09 0.25	50.53 254.20 3 362.60 3 299.30 3 242.90 3 370.90 3 225.60 3 604.40 3 103.90 3 247.30 3	41.05 100.00 100.00 100.00 100.00 100.00 100.00 100.00 100.00 99.99	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago	TD3_1 SSTANDS STMN19 T1 TD5_1 T2 TD6_1 V_1 TD5_2 V_2 V_2 TD6_1 Node Summar CBA1 CBMHA210 CBMHA2	י דג זר זר זר זר זר זר זר	0.79 0.05 0.08 0.06 0.10 UNCTION UNCTION UNCTION	162.57 71.00 75.86 78.30 167.82 I	99.99 24.40 27.76 96.59 96.59 96.59 96.59 	10.000 0.500 0.500 0.500 0.500 0.500 1.93 2.80 2.31	0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 0.00 0.0	
NG-A NG-B NG-B NG-C NG-C NG-C NG-D NG-D NG-D NG-D NG-G NG-H NG-H NG-H NG-H NG-T NG-T NG-J NG-J NG-J NG-J NG-J NG-J C-S NG-J C-K NG-J C-K NG-S C-K NG-S NG-S NG-S NG-S NG-S NG-S NG-S NG-S	0.89 0.25 0.36 0.30 0.14 0.24 0.37 0.23 0.60 0.10 0.09 0.25 0.19	50.53 254.20 3 362.60 3 299.30 3 242.90 3 370.90 3 225.60 3 103.90 3 247.730 3	41.05 100.00 100.00 100.00 100.00 100.00 100.00 100.00 99.99 27.10	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago	TD3_1 SSTANDS STMN19 T1 TD5_1 T2 TD6_1 V_1 TD5_2 V_2 TD6_1 Node Summary Node Summary CBA1 CBMH210 CBMH210 CBMH22 CBMH24 J1 J1 J1 J1 J19	י דע זר זר זר זר זר זר זר זר זר זר זר זר זר	0.79 0.05 0.08 0.06 0.10 UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION	162.57 71.00 75.86 78.30 167.82 I	99.99 24.40 27.76 96.59 96.59 96.59 96.59 96.59 64.07 63.18 63.89 63.36 63.56 63.56 63.62	10.000 0.500 0.500 0.500 0.500 0.500 0.500 0.500 2.80 2.31 2.80 2.31 2.80 2.31 2.79 3.10 2.08	0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 0.00 0.	
IG-A IG-B IG-B IG-C IG-C IG-C IG-C IG-C IG-C IG-C IG-C	0.89 0.25 0.36 0.14 0.24 0.37 0.23 0.60 0.10 0.09 0.25	50.53 254.20 3 362.60 3 299.30 3 242.90 3 370.90 3 225.60 3 604.40 3 103.90 3 247.30 3	41.05 100.00 100.00 100.00 100.00 100.00 100.00 100.00 100.00 99.99	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago	TD3_1 SSTANDS STMNI9 T1 TD5_1 T2 TD6_1 V_1 TD5_2 V_2 TD6_1 Node Summar CBA1 CBMH210 CBMH20 CBMH20 GBHU J1 J14	ר דע זר זר זר זר זר זר זר זר זר זר זר זר זר	0.79 0.05 0.08 0.06 0.10 UNCTION UNCTION UNCTION UNCTION UNCTION	162.57 71.00 75.86 78.30 167.82 I	99.99 24.40 27.76 96.59 96.59 96.59 96.59 63.59 63.89 63.89 63.36 63.59	10.000 0.500 0.500 0.500 0.500 0.500 0.500 0.500 2.30 2.80 2.31 2.64 2.79 3.10	0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 0 00 0.0 0.0 0.0 0.0 0.0	
NG-A DG-B DG-B DG-C DG-C DG-C DG-C DG-D DG-D DG-D DG-G DG-H DG-H DG-H DG-H	0.89 0.25 0.36 0.30 0.14 0.24 0.37 0.23 0.60 0.10 0.09 0.25 0.19	50.53 254.20 3 362.60 3 299.30 3 242.90 3 225.60 3 225.60 3 89.20 3 247.30 3	41.05 100.00 100.00 100.00 100.00 100.00 100.00 100.00 99.99 27.10	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago	TD3_1 SSTANDS STMNI9 T1 TD5_1 T2 TD6_1 T55_2 V_1 T05_2 V_2 T06_1 	י די די זר זר זר זר זר זר זר זר זר זר זר זר זר	0.79 0.05 0.08 0.06 0.10 UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION	162.57 71.00 75.86 78.30 167.82 I	99.99 24.40 27.76 96.59 96.59 96.59 96.59 64.07 63.18 63.88 63.36 63.36 63.36 63.36 63.36 63.55 63.65 63.25 63.62 63.25	10.000 0.500 0.500 0.500 0.500 0.500 1.93 2.80 2.31 2.64 2.79 3.10 2.08 2.30 2.28	0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 0 00 0	
NG-A NG-B NG-B NG-C NG-C NG-C NG-D NG-D NG-D NG-G NG-G NG-T NG-T NG-T NG-T NG-T NG-T	0.89 0.25 0.36 0.30 0.14 0.24 0.37 0.23 0.60 0.10 0.09 0.25 0.19 0.21	50.53 254.20 3 362.60 3 299.30 3 242.90 3 225.60 3 225.60 3 0.04.40 3 247.30 3 38.69 3	41.05 100.00 100.00 100.00 100.00 100.00 100.00 100.00 99.99 27.10 19.10	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago	TD3_1 SSTANDS STMNI9 T1 TD5_1 T2 TD6_1 V_1 TD5_2 V_2 TD6_1 Node Summary CBA1 CBMH210 CBMH210 CBMH22 CBMHU J1 J14 J19 J23 J26 J27 J32 J37	רד דע זת זת זת זת זת זת זת זת זת זת זת זת זת	0.79 0.05 0.08 0.06 0.10 UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION	162.57 71.00 75.86 78.30 167.82 I	99.99 24.40 27.76 96.59 96.59 96.59 96.59 96.59 63.18 63.88 63.36 63.36 63.36 63.36 63.95 63.65 63.95 63.25 62.25 62.25 62.25 62.25	10.000 0.500 0.500 0.500 0.500 0.500 1.93 2.80 2.31 2.64 2.73 2.64 2.79 2.08 2.30 2.84	0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 0 00 0.0 0.0 0.0 0.0 0.0 720.0 1000.0 0.0	
G-A G-B G-B G-C G-C G-C G-D G-D G-G G-G G-G G-I G-J G-J G-J G-J G-J G-K G-K G-K	0.89 0.25 0.36 0.30 0.14 0.24 0.37 0.23 0.60 0.10 0.25 0.19 0.21 0.50 0.35	50.53 254.20 2 362.60 2 299.30 2 138.00 2 242.90 2 225.60 2 604.40 2 103.90 2 247.30 3 38.69 2 271.32 3 38.57 3	41.05 100.00 100.00 100.00 100.00 100.00 100.00 100.00 100.00 99.99 27.10 19.10 15.20 15.30	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago	TD3_1 SSTANDS STMN19 T1 TD5_1 T2 TD6_1 V_1 TD5_2 V_2 TD6_1 	י די ג ג ג ג ג ג ג ג ג ג ג ג ג ג ג ג ג ג	0.79 0.05 0.08 0.06 0.10 UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION	162.57 71.00 75.86 78.30 167.82 I	99.99 24.40 27.76 96.59 96.59 96.59 96.59 63.63 63.56 63.18 63.86 63.56 63.36 63.95 63.62 63.29 62.29 62.29 62.29 62.29 62.29	10.000 0.500 0.500 0.500 0.500 1.93 2.80 2.31 2.64 2.79 3.10 2.08 2.30 2.24 2.88 3.44 2.88 3.44 2.88	Ponded Area 0.000yr_0 0.000yr_0 0.000yr_0 0.00 0.00 0.00 0.00 720.0 1000.0 0.00 0.00 0.00 0.00 0.00 0.0	
G-A G-B G-B G-C G-C G-D G-D G-G G-G G-G G-G G-I G-J G-J G-J G-J G-J G-J G-K G-K G-K G-K	0.89 0.25 0.36 0.30 0.14 0.24 0.37 0.23 0.60 0.10 0.25 0.19 0.21 0.50 0.33 0.37	50.53 254.20 2 362.60 2 299.30 2 138.00 2 242.90 2 270.90 2 209.30 2 200.90 2 225.60 2 200.90 2 242.90 2 200.90 2 210.30 2 38.69 2 21.32 3 38.57 7	41.05 100.00 100.00 100.00 100.00 100.00 100.00 100.00 100.00 99.99 27.10 19.10 15.20 15.30 17.00	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago	TD3_1 SSTANDS STMN19 T1 TD5_1 T2 TD6_1 V_1 TD5_2 V_2 TD6_1 	(0.79 0.05 0.08 0.06 0.10 VPP VNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION	162.57 71.00 75.86 78.30 167.82 I	99.99 24.40 27.76 96.59 96.59 96.59 96.59 64.63 63.95 63.63 63.95 63.36 63.95 63.95 63.95 63.95 62.59 62.29 62.25 62.25 62.25 62.85 62.85 62.85	10.000 0.500 0.500 0.500 0.500 1.90 2.80 2.31 2.64 2.79 3.10 2.68 2.31 2.64 2.79 3.10 2.08 2.31 2.64 2.28 3.44 2.26 2.30 3.44	Ponded Area 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 0 00 0	
G-A GC-B GC-B GC-C GC-C GC-C GC-C GC-C GC-C	0.89 0.25 0.36 0.30 0.14 0.24 0.37 0.23 0.60 0.10 0.25 0.19 0.21 0.50 0.35	50.53 254.20 2 362.60 2 299.30 2 138.00 2 242.90 2 225.60 2 604.40 2 103.90 2 247.30 3 38.69 2 271.32 3 38.57 3	41.05 100.00 100.00 100.00 100.00 100.00 100.00 100.00 100.00 99.99 27.10 19.10 15.20 15.30	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago	TD3_1 SSTANDS STMNI9 STM19 T1 TD5_1 T2 TD6_1 T05_2 V_1 TD5_2 V_2 TD6_1 Node Summary CBA1 CBMH210 CBMHA2 CBMHU J1 J14 J14 J19 J23 J26 J27 J37 J40 J41 J49	۲۲ ۲ ח ח ח ח ח ח ח ח ח ח ח ח ח ח ח ח ח	0.79 0.05 0.08 0.06 0.10 UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION	162.57 71.00 75.86 78.30 167.82 I	99.99 24.40 27.76 96.59 96.59 96.59 96.59 63.63 63.95 63.95 63.95 63.95 63.95 63.95 63.95 63.95 63.95 63.62 62.29 62.25 62.25 62.25 62.25 62.59 62.59 62.59 62.59 62.85 62.59	10.000 0.500 0.500 0.500 0.500 0.500 1.93 2.80 2.31 2.64 2.79 3.10 2.08 2.31 2.68 2.30 2.84 2.88 3.44 2.88 3.44 2.26 2.30 3.58	0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
0G-A 0G-B 0G-B 0G-C 0G-C 0G-C 0G-D 0G-D 0G-D 0G-H 0G-T 0G-T 0G-T 0G-T 0G-T 0G-J	0.89 0.25 0.36 0.30 0.14 0.24 0.37 0.23 0.60 0.10 0.25 0.19 0.21 0.50 0.33 0.37	50.53 254.20 2 362.60 2 299.30 2 138.00 2 242.90 2 270.90 2 209.30 2 200.90 2 225.60 2 200.90 2 242.90 2 200.90 2 210.30 2 38.69 2 21.32 3 38.57 7	41.05 100.00 100.00 100.00 100.00 100.00 100.00 100.00 100.00 99.99 27.10 19.10 15.20 15.30 17.00	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago	TD3_1 SSTANDS STMNI9 STM19 T1 TD5_1 T2 TD6_1 T05_2 V_1 TD5_2 V_2 TD6_1 Node Summary CBA1 CBMH210 CBMHA2 CBMH210 CBMH42 J1 J1 J1 J1 J23 J26 J27 J37 J40 J41 J49 J50 J51	۲ ۲ ۲ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳	0.79 0.05 0.08 0.06 0.10 UNCTION	162.57 71.00 75.86 78.30 167.82 I	99.99 24.40 27.76 96.59 96.59 96.59 96.59 63.08 64.08 64.08 64.08 64.08 64.08 64.08 64.08 64.08 64.08 64.08 64.08 64.08 64.08 64.08 65.080	10.000 0.500 0.500 0.500 0.500 0.500 0.500 2.80 2.31 2.64 2.79 3.10 2.08 2.31 2.64 2.79 3.10 2.08 2.31 2.68 2.30 2.84 2.88 3.44 2.42 2.26 2.30 3.58 3.347	Ponded Area Ponded Area Ponded Area 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	
DG-A DG-B DG-B DG-C DG-C DG-C DG-C DG-C DG-D DG-D DG-D	0.89 0.25 0.36 0.14 0.24 0.37 0.23 0.60 0.10 0.09 0.25 0.19 0.21 0.50 0.35 0.37 0.35	50.53 254.20 2 362.60 2 299.30 2 138.00 2 242.90 2 25.60 2 200.00 2 242.90 2 200.00 2 242.90 2 200.00 2 200.00 2 200.00 2 200.00 2 38.69 2 271.32 3 38.57 7 75.00 4 46.00 4	41.05 100.00 100.00 100.00 100.00 100.00 100.00 100.00 100.00 99.99 27.10 19.10 15.20 15.30 17.00	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago	TD3_1 SSTANDS STMN19 STM19 T1 TD5_1 T2 TD6_1 V_1 TD5_2 V_2 TD6_1 Node Summar CBM210 CBMH210 CBM10 CDM10 CDM10 CDM10 CBM10 CDM10 CBM10 CDM10 CDM10 CBM10 CDM10	۲ ۲ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳	0.79 0.05 0.08 0.06 0.10 VPP VPP VNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION UNCTION	162.57 71.00 75.86 78.30 167.82 I	99.99 24.40 27.76 96.59 96.59 96.59 96.59 63.63 63.63 63.56 63.36 63.56 63.36 63.56 63.95 63.62 62.59 62.25 62.25 62.25 62.25 62.25 62.85	10.000 0.500 0.500 0.500 0.500 0.500 1.93 2.64 2.79 3.00 2.64 2.30 2.64 2.30 2.64 2.30 2.88 3.44 2.26 2.30 3.44 2.26 2.30 3.00 3.300	Ponded Area 0 100yr_: 0 100yr_: 0 100yr_: 0 100yr_: 0 100yr_: 0 100yr_: 0 0 00yr_: 0 0 00 0	
B DG-A DG-A DG-B DG-B DG-C DG-C DG-C DG-C DG-C DG-C DG-G DG-G DG-H DG-H DG-H DG-H DG-H DG-J DG-J DG-J DG-J DG-J DG-J DG-J DG-J DG-J CNU DG-J DG-J DG-J CNU DG-J DG-K	0.89 0.25 0.36 0.14 0.24 0.37 0.23 0.60 0.10 0.09 0.25 0.19 0.21 0.50 0.35 0.37 0.35 0.37	50.53 254.20 2 362.60 2 299.30 2 138.00 2 242.90 2 25.60 2 200.00 2 242.90 2 200.00 2 242.90 2 200.00 2 200.00 2 200.00 2 200.00 2 38.69 2 271.32 3 38.57 7 75.00 4 46.00 4	41.05 100.00 100.00 100.00 100.00 100.00 100.00 100.00 100.00 99.99 27.10 19.10 15.20 15.30 17.00 15.00 9.00	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago	TD3_1 SSTANDS STMN19 STM19 T1 TD5_1 T2 TD6_1 V_1 TD5_2 V_2 TD6_1 	۲۰ ۳۵ ۳۵ ۳۵ ۳۵ ۳۵ ۳۵ ۳۵ ۳۵ ۳۵ ۳۵ ۳۵ ۳۵ ۳۵	0.79 0.05 0.08 0.06 0.10 VPP VPP VPP VPP VPP VPP VPP VPP VPP VP	162.57 71.00 75.86 78.30 167.82	99.99 24.40 27.76 96.59 96.59 96.59 96.59 63.02 63.02 63.03 63.05 63.05 63.05 63.05 63.05 62.29 62.25 62.25 62.25 62.62 62.85 62.85 62.85 62.85 62.85 62.85 62.85 62.85 62.85 62.85 62.85 63.68 63.68 63.68 63.68 65.25	Max. Depth 1.93 2.64 2.79 3.10 2.88 3.44 2.28 2.30 2.88 3.44 2.28 3.44 2.28 3.00 3.00 3.00 3.00 3.00	Ponded Area 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 0 00yr_ 0	
NG-A NG-B NG-B NG-B NG-C NG-C NG-C NG-D NG-D NG-D NG-J NG-J NG-J1 NG-J1 NG-J1 NG-J1 NG-J2 NG-Z	0.89 0.25 0.36 0.30 0.14 0.24 0.37 0.23 0.60 0.10 0.09 0.25 0.19 0.21 0.50 0.35 0.37 0.15 0.35 0.37 0.15 0.25 0.18 0.11	50.53 254.20 2 362.60 2 299.30 2 38.00 2 242.90 2 25.60 2 201.00 2 242.90 2 370.90 2 242.90 2 25.60 2 201.01 2 38.69 2 271.32 3 38.57 7 75.00 4 41.00 4 49.70 4	41.05 100.00 100	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago	TD3_1 SSTANDS STANDS STM19 T1 TD5_1 T2 TD6_1 V 1 TD5_2 V 2 TD6_1 	۲ ۲ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳	0.79 0.05 0.08 0.06 0.10 UNCTION	162.57 71.00 75.86 78.30 167.82 I	99.99 24.40 27.76 96.59 96.59 96.59 96.59 63.18 63.89 63.36 63.95 63.95 63.95 63.95 63.95 63.25 62.29 62.25 62.25 64.69 63.82 65.08 65.25	Max. Depth 1.93 2.80 2.31 2.64 2.79 3.10 2.08 2.31 2.64 2.80 2.28 2.80 2.31 2.64 2.28 3.44 2.42 2.88 3.44 2.42 3.58 3.60 3.58 3.00 3.58	Ponded Area 0 100yr_1 0 100yr_1 0 100yr_1 0 100yr_1 0 100yr_1 0 100yr_1 0 100yr_1 0	
B DDG-A DDG-A DDG-B DDG-B DDG-C DDG-C DDG-C DDG-C DDG-G DDG-G DDG-H DDG-H DDG-H DDG-H DDG-J DDG-K DDG-J DDG-K DDG-J DDG-K	0.89 0.25 0.36 0.30 0.14 0.24 0.37 0.23 0.60 0.10 0.09 0.25 0.19 0.21 0.50 0.35 0.35 0.37 0.15 0.25 0.18 0.11 0.15	50.53 254.20 2 362.60 2 299.30 2 38.00 2 242.90 2 370.90 2 25.60 2 604.40 2 103.90 2 247.30 2 38.69 2 271.32 3 38.57 7 75.00 4 40.00 4	41.05 100.00 100	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago	TD3_1 SSTANDS STANDS STM19 T1 TD5_1 T2 TD6_1 V 1 TD5_2 V 2 TD6_1 	۲ ۲ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳	0.79 0.05 0.08 0.06 0.10 0.10 0.10 0.010 0.010 0.00100 0.00100 0.00000000	162.57 71.00 75.86 78.30 167.82 I	99.99 24.40 27.76 96.59 96.59 96.59 96.59 96.59 63.18 63.36 63.36 63.36 63.36 63.36 63.36 63.36 63.29 62.29 62.25 62.29 62.25 62.29 62.28 62.85 62.85 62.85 62.85 62.85 63.25 65.25 65.25	10.000 0.500 0.500 0.500 0.500 1.93 2.80 2.31 2.80 2.31 2.80 2.31 2.82 2.83 2.30 2.84 2.88 3.44 2.42 2.88 3.44 2.88 3.44 2.88 3.44 2.88 3.44 2.88 3.44 2.88 3.44 3.50 3.00 3.50 3.00 3.00 3.00 3.00 3.00	Ponded Area 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
DG-A DG-B DG-B DG-B DG-C DG-C DG-C DG-C DG-C DG-C DG-C DG-T DG-T DG-T DG-T DG-T DG-T DG-T DG-T	0.89 0.25 0.36 0.30 0.14 0.24 0.37 0.23 0.60 0.10 0.09 0.25 0.19 0.21 0.50 0.35 0.37 0.15 0.35 0.37 0.15 0.25 0.18 0.11	50.53 254.20 2 362.60 2 299.30 2 38.00 2 242.90 2 25.60 2 201.00 2 242.90 2 370.90 2 242.90 2 25.60 2 201.01 2 38.69 2 271.32 3 38.57 7 75.00 4 41.00 4 49.70 4	41.05 100.00 100	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago	TD3_1 SSTANDS STMN19 STM19 T1 TD5_1 T2 TD6_1 V_1 TD5_2 V_2 TD6_1 Name CBA1 CBMH210 CBMH20 CBMH20 CBMH210 CBM120 C	۲۰ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳	0.79 0.05 0.08 0.06 0.10 VPP VPP VNTION VNCTION	162.57 71.00 75.86 78.30 167.82 I	99.99 24.40 27.76 96.59 96.59 96.59 96.59 96.59 64.05 63.62 63.63 63.56 63.56 63.56 63.95 62.25 62.25 62.25 62.25 62.25 62.25 62.68 62.81 63.81 65.31 65.25 65.31 65.25 65.25	Max. Depth 1.93 2.80 2.31 2.80 2.31 2.80 2.31 2.80 2.31 2.80 2.31 2.80 2.31 2.80 2.31 2.80 2.31 2.80 2.31 2.80 2.31 2.80 2.31 2.80 3.44 2.26 2.30 3.44 2.28 3.44 2.28 3.44 2.28 3.44 2.26 3.50 3.00	Ponded Area 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 0 00 0	
A DDG-A DDG-B DDG-B DDG-B DDG-C DDG-C DDG-C DDG-C DDG-C DDG-T	0.89 0.25 0.36 0.30 0.14 0.24 0.37 0.23 0.60 0.10 0.09 0.25 0.19 0.21 0.50 0.35 0.35 0.37 0.15 0.25 0.18 0.11 0.15	50.53 254.20 2 362.60 2 299.30 2 38.00 2 242.90 2 370.90 2 25.60 2 604.40 2 103.90 2 247.30 2 38.69 2 271.32 3 38.57 7 75.00 4 40.00 4	41.05 100.00 100	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago	TD3_1 SSTANDS STMN19 STM19 T1 TD5_1 T2 TD6_1 V_1 TD5_2 V_2 TD6_1 Node Summary Name 	۲۰ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳	0.79 0.05 0.08 0.10 0.10 Vype Vype Vype Vype Vype Vype Vype Vype	162.57 71.00 75.86 78.30 167.82 I	99.99 24.40 27.76 96.59 96.59 96.59 96.59 96.59 64.07 63.18 63.36 63.36 63.36 63.36 63.95 63.62 62.25 62.25 62.25 62.25 62.25 62.25 63.68 62.25 63.82 63.82 65.31 65.25 65.25 65.25 65.25 65.35 65.35 65.35 65.35 65.35	Max. Depth 1.93 2.80 2.31 2.80 2.31 2.80 2.31 2.80 2.31 2.80 2.31 2.80 2.31 2.80 2.31 2.80 2.31 2.80 2.31 2.80 2.31 2.80 2.31 2.80 3.44 2.26 2.30 3.44 2.26 3.44 2.26 3.44 2.26 3.44 2.26 3.44 2.26 3.44 2.26 3.44 2.26 3.44 2.26 3.44 2.80 3.44 2.80 3.44 2.80 3.44 2.80 3.44 2.80 3.44 2.80 3.64 3.60 3.60 3.00	Ponded 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 0 000 0	
G-A G-B G-B G-C G-C G-D G-D G-D G-G-C G-G-C G-T G-T G-T G-T G-T G-T G-J G-J G-J G-J G-J G-J G-J G-J G-J G-J	0.89 0.25 0.36 0.30 0.14 0.24 0.37 0.23 0.60 0.10 0.09 0.25 0.19 0.21 0.50 0.35 0.37 0.15 0.35 0.37 0.15 0.25 0.18 0.11 0.15 0.49	50.53 254.20 2 362.60 2 2 138.00 2 2 242.90 2 2 370.90 2 2 103.90 2 2 209.30 2 2 103.90 2 2 247.30 2 2 38.69 2 2 38.69 2 2 38.57 7 5.00 46.00 4 4 40.00 2 4	41.05 100.00 100	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago	TD3_1 SSTANDS STMNI9 STM19 T1 TD5_1 T2 TD6_1 V_1 TD5_2 V_2 TD6_1 Node Summary CBA1 CBMH210 CBMH210 CBMH210 CBMH210 CBMH210 CBMH210 CBMH210 CBMH210 J1 J14 J14 J14 J14 J14 J19 J23 J26 J27 J37 J37 J37 J37 J37 J37 J37 J37 J37 J3	۲۰ ۳۲ ۳۳ ۳۳ ۳۳ ۳۳ ۳۳ ۳۳ ۳۳ ۳۳ ۳۳ ۳۳ ۳۳ ۳۳	0.79 0.05 0.08 0.10 0.10 WTTION WATION	162.57 71.00 75.86 78.30 167.82 I	99.99 24.40 27.76 96.59 96.59 96.59 96.59 96.59 63.61 63.18 63.36 63.36 63.36 63.36 63.36 63.36 63.95 63.62 62.25 62.25 62.25 62.25 62.25 62.25 63.68 63.82 63.85 63.82 63.85 63.82 63.85 65.85	Max. Depth 1.93 2.80 2.31 2.64 2.79 3.00 2.81 2.64 2.79 3.20 2.24 2.26 2.30 2.24 2.26 2.30 2.28 3.44 2.28 3.44 2.28 3.44 2.26 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.0	Donded 0 100yr_0 0 100yr_0 0 100yr_0 0 100yr_0 0 100yr_0 0 100yr_0 0 0 000 0	
G-A G-B G-B G-B G-C G-C G-C G-C G-C G-C G-C G-C G-C G-C	0.89 0.25 0.36 0.30 0.14 0.24 0.37 0.23 0.60 0.10 0.09 0.25 0.19 0.21 0.50 0.35 0.35 0.35 0.35 0.35 0.35 0.49 0.49 0.49 0.47	50.53 254.20 2 362.60 2 299.30 2 38.00 2 242.90 2 370.90 2 25.60 2 103.90 2 247.30 2 247.30 2 38.69 2 38.69 2 38.57 7 75.00 4 40.00 2 49.70 4 40.00 2 247.73 2	41.05 100.00 100	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_c	TD3_1 SSTANDS STMN19 T1 TD5_1 T2 TD6_1 V_1 TD5_2 V_2 TD6_1 Node Summary CBA1 CBMH210 CBMH20	۲ ۲ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳	0.79 0.05 0.08 0.06 0.10 VPP UNCTION	162.57 71.00 75.86 78.30 167.82 I	99.99 24.40 27.76 96.59 96.59 96.59 96.59 64.59 63.63 63.63 63.56 63.62 63.95 63.36 63.95 63.36 63.95 63.36 63.95 63.25 62.25 62.25 62.25 62.25 62.25 62.25 63.68 64.69 65.31 65.25 65.30 65.35 65.35 65.35 65.35 64.40 65.35 65.35 64.40 65.35 64.50	10.000 0.500 0.500 0.500 0.500 1.93 2.80 2.31 2.64 2.79 3.10 2.08 2.31 2.64 2.28 2.30 2.84 2.26 2.30 3.54 2.26 2.30 3.47 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.0	Ponded Area Ponded Area Ponded Area 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 0 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
G-A G-B G-B G-C G-C G-C G-D G-D G-D G-G-G G-G-G G-G-G G-J1 G-J1 G-J1 G-J2 G-J2 G-J2 G-J2 G-G-K at-Lawn_1 at-Lawn_4 at-Lawn_6 10 1 4 2 2 4 4 2 5 4 5 9 9 G_1	0.89 0.25 0.36 0.30 0.14 0.24 0.37 0.23 0.60 0.10 0.09 0.25 0.19 0.21 0.50 0.35 0.35 0.35 0.35 0.35 0.35 0.35	50.53 254.20 2 362.60 2 138.00 2 242.90 2 370.90 2 225.60 2 103.90 2 247.30 2 247.30 2 38.69 2 271.32 3 38.57 7 75.00 4 40.00 2 247.73 2 247.73 2 25.57 2	41.05 100.00 100	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 10.0000 100yr_3hr_chicago 10.0000 100yr_3hr_chicago 2.0000 100yr_3hr_chicago	TD3_1 SSTANDS STM19 T1 TD5_1 T2 TD6_1 V_1 TD5_2 V_2 TD6_1 Node Summary TD6_1 Node Summary TD6_1 CBM1210 CBMH210 CBM	۲۰ ۳۵ ۳۵ ۳۵ ۳۵ ۳۵ ۳۵ ۳۵ ۳۵ ۳۵ ۳۵ ۳0 ۳0 ۳0 ۳0 ۳0 ۳0 ۳0 ۳0 ۳0 ۳0 ۳0 ۳0 ۳0	0.79 0.05 0.08 0.06 0.10 VPP VPC VPC VPC VPC VPC VPC VPC VPC VPC	162.57 71.00 75.86 78.30 167.82 I	99.99 24.40 27.76 96.59 96.59 96.59 96.59 96.59 63.63 63.76 65.75 75 75 75 75 75 75 75 75 75 75 75 75 7	10.000 0.500 0.500 0.500 0.500 1.500 2.500 2.500 2.84 2.80 2.31 2.80 2.31 2.82 2.31 2.83 2.31 2.98 2.34 2.26 2.30 2.26 2.30 3.58 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.0	Ponded Ponded Ponded Area 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 0 00yr_ 0 0 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
G-A G-B G-B G-B G-C G-C G-C G-C G-C G-C G-C G-C G-C G-T G-T G-T G-T G-T G-T G-T G-T G-T G-T	0.89 0.25 0.36 0.30 0.14 0.24 0.37 0.23 0.60 0.10 0.09 0.25 0.19 0.21 0.50 0.35 0.35 0.35 0.35 0.35 0.35 0.49 0.49 0.49 0.47	50.53 254.20 2 362.60 2 299.30 2 370.90 2 225.60 2 103.90 2 242.90 2 103.90 2 247.30 2 247.30 2 38.69 2 38.69 2 38.57 7 75.00 4 40.00 2 247.73 2 247.73 2 247.73 2 247.73 2 38.69 2 38.69 2 38.69 2 271.32 3 46.00 2 42.80 2 42.280 2 42.80 3 38.00 3	41.05 100.00 100	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 10.0000 100yr_3hr_chicago 10.0000 100yr_3hr_chicago 2.0000 100yr_3hr_chicago 2.0000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago	TD3_1 SSTANDS STMNI9 T1 TD5_1 T2 TD6_1 V_1 TD5_2 V_2 TD6_1 Node Summary CBA1 CBMH210 CBMH210 CBMH22 CBMHU J1 J14 J14 J19 J23 J26 J27 J37 J37 J40 J41 J41 J44 J49 J23 J26 J27 J37 J37 J40 J41 J41 J49 J23 J26 J27 J37 J37 J40 J41 J41 J49 J55 J55 J55 J55 J55 J55 J55 J55 J55 J5	۲ ۲ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳	0.79 0.05 0.08 0.10 0.10 UNCTION	162.57 71.00 75.86 78.30 167.82 I	99.99 24.40 27.76 96.59 96.59 96.59 96.59 96.59 96.59 63.68 63.36 63.36 63.36 63.36 63.36 63.36 63.36 63.36 63.36 63.25 62.25 62.25 62.25 62.25 62.25 62.25 63.82 65.25 64.88 65.31 65.35 65.25 65.25 65.35 65.35 65.35 65.35 65.35 65.35 65.35 65.35 65.35 65.35 65.46 65.35	Max. Depth Depth 1.93 2.80 2.31 2.64 2.79 3.44 2.79 3.44 2.30 2.88 3.44 2.26 2.30 3.44 2.30 3.44 2.30 3.44 2.30 3.44 3.44 3.44 3.44 3.44 3.44 3.44 3.44 3.44 3.44 3.44 3.44 3.44 3.44 3.60 3.00	0 100yr_1 0 100yr_2 0 0 <	
B DG-A DG-A DG-B DG-B DG-C DG-C DG-C DG-C DG-C DG-C DG-G DG-G DG-H DG-H DG-H DG-H DG-J DG-K DG-J DG-K DG-J DG-K DG-K DG-K DG-K DG-K DG-Z DG-K DG-K DG-K DG-Z DG-K DG-K DG-Z DG-K DG-K DG-Z DG-K DG-Z DG-K DG-K DG-Z DG-K DG-Z DG-K DG-Z DG-K DG-Z DG-K DG-Z DG-K DG-Z DG-K DG-Z DG-K DG-K DG-Z DG-K DG-	0.89 0.25 0.36 0.30 0.14 0.24 0.37 0.23 0.60 0.10 0.09 0.25 0.19 0.21 0.50 0.35 0.35 0.35 0.35 0.35 0.35 0.35	50.53 254.20 2 362.60 2 138.00 2 242.90 2 370.90 2 225.60 2 103.90 2 247.30 2 247.30 2 38.69 2 271.32 3 38.57 7 75.00 4 40.00 2 247.73 2 247.73 2 25.57 2	41.05 100.00 100	0.5000 100yr_3hr_chicago 0.5000 100yr_3hr_chicago 10.0000 100yr_3hr_chicago 10.0000 100yr_3hr_chicago 2.0000 100yr_3hr_chicago	TD3_1 SSTANDS STM19 T1 TD5_1 T2 TD6_1 V_1 TD5_2 V_2 TD6_1 Node Summary TD6_1 Node Summary TD6_1 CBM1210 CBMH210 CBM	۲ ۲ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳ ۳	0.79 0.05 0.08 0.06 0.10 VPP VPC VPC VPC VPC VPC VPC VPC VPC VPC	162.57 71.00 75.86 78.30 167.82 I	99.99 24.40 27.76 96.59 96.59 96.59 96.59 96.59 63.63 63.76 65.75 75 75 75 75 75 75 75 75 75 75 75 75 7	10.000 0.500 0.500 0.500 0.500 1.500 2.500 2.500 2.84 2.80 2.31 2.80 2.31 2.82 2.31 2.83 2.31 2.98 2.34 2.26 2.30 2.26 2.30 3.58 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.0	Ponded Ponded Ponded Area 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 100yr_ 0 0 00yr_ 0 0 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	3hr_C 3hr_C 3hr_C 3hr_C 3hr_C

J71 J72 J73 STM102 STM104 STM105 STM107 STM108 STM109 STM110 STM1110 STM1112 STM112	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	65.18 64.75 65.45 62.34 62.52 62.72 62.00 62.96 63.10 63.76 63.03 63.77	3.00 3.00 2.32 2.90 3.05 3.53 3.95 1.79 2.35 1.54 3.42 3.00	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0		BASIN2 BASIN3 S-BLDG-1 S-BLDG-1 S-BLDG-1 S-BLDG-2 S-BLDG-3 S-BLDG-3 S-BLDG-3 S-BLDG-4	B C G H J J J J 2	STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE STORAGE	62.95 62.86 100.00 100.00 100.00 100.00 100.00 100.00 100.00 100.00 100.00	2.19 1.68 0.15 0.15 0.15 0.15 0.15 0.15 0.15 0.15	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	
STM117 STM118 STM119 STM120 STM121 STM122	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	63.91 63.96 64.11 64.26 63.31 63.68	3.51 3.51 3.34 3.14 2.94 1.63	0.0 0.0 0.0 0.0 0.0 0.0		Link Sur ******** Name lope Roug	nmary ****	From Node	To Node	Туре	Length	8
STM203 STM204 STM205	JUNCTION JUNCTION JUNCTION	63.19 63.24 63.29	5.07 8.26 4.76	0.0 0.0 0.0		C1		J14	STM114	CONDUIT	75.0	
STM206 STM207	JUNCTION JUNCTION	63.35 63.40	5.36 5.43	0.0		C10	0.0130	STMH202	BASIN3	CONDUIT	20.5	
STM208 STM209 STM211	JUNCTION JUNCTION JUNCTION	63.44 63.58 63.22	4.07 3.84 2.23	0.0 0.0 0.0		C10_1	0.0130	STMC	STMD	CONDUIT	25.1	
STM211 STM212 STM213	JUNCTION JUNCTION	63.22 63.29 63.09	2.23 3.16 1.95	0.0	0.	C11 .1017	0.0130	STMD	CBMH210	CONDUIT	34.4	
SIMA SIMA	JUNCTION	63.56 63.76	2.58	0.0	0.		0.0100	CBMH210 SWMCCN2	OFCanal SWMCCN1	CONDUIT	55.8	
STMB STMBB	JUNCTION	63.44 63.57	2.58	0.0	0.	C13 .5217 C14	0.0130	STM111A	SWMCCN1	CONDUIT	23.0	
STMC STMCC	JUNCTION JUNCTION	63.35 63.42	2.21 2.78	0.0	0.	.5037 C15	0.0130	SWMCCN1	STM212	CONDUIT	8.2	
STMD STMDD	JUNCTION JUNCTION	63.24 63.12	2.66 2.93	0.0		C16	0.0130	STM212	STM211	CONDUIT	30.0	
STMFF STMGG	JUNCTION JUNCTION	63.09 63.03	2.82	0.0		.1667 C17	0.0130	STM110	STM109	CONDUIT	11.3	
STMH202 SWMCCN1	JUNCTION JUNCTION	63.06 63.32	2.33 2.03	0.0		.1770 C18 .0992	0.0130	STMDD	STMFF	CONDUIT	30.2	
SWMCCN2 TD2_1 TD2_2	JUNCTION JUNCTION JUNCTION	63.79 65.38 64.01	1.79 0.28 1.57	0.0 0.0 0.0		C18_1 .2542	0.0130	STM109	J40	CONDUIT	43.3	
TD3_1 TD3_2	JUNCTION JUNCTION	65.98 64.19	0.36	0.0	0.	C18_2 .0337	0.0130	J40	STM108	CONDUIT	59.3	
TD5_1 TD5_2	JUNCTION	64.64 63.74	0.33	0.0	0.	C19 .0526 C2	0.0130	STMFF STM120	STMGG STM119	CONDUIT	57.0	
TD6_1 TD6_2	JUNCTION JUNCTION	64.71 63.76	0.40	0.0	0.		0.0130	SIMIZO	STM108	CONDUIT	16.7	
TD7_1 TD7_2	JUNCTION JUNCTION	64.71 63.69	0.31	0.0	6.		0.0130	STMCC	STMDD	CONDUIT	53.4	
TD8_1 TD8_2	JUNCTION	64.70 63.19	0.33	0.0		C21_1	0.0130	STM108	J32	CONDUIT	70.1	
J28 OFCanal BASIN1	OUTFALL OUTFALL STORAGE	62.22 64.50 62.81	0.97 1.00 2.39	0.0 0.0 0.0		C21 2	0.0130	J32	STM107	CONDUIT	14.2	
C22 0.5029 0.0130		СЕМНИ	CONDUIT	31.8	0.		0.0130	STM117	STM208	CONDUIT	6.7	
0.5029 0.0130 C23 0.5054 0.0130	CBMHU	STM108	CONDUIT	41.5	0.	.1504 C50 .3521	0.0130 0.0130	J58	J57	CONDUIT	14.2	
0.5029 0.0130 C23 0.5054 0.0130 C24 0.3752 0.0130 C25	CBMHU STM122 STM121				0. 0. 0.	.1504 C50 .3521 C51 .9741 C52	0.0130					
0.5029 0.0130 C23 0.5054 0.0130 C24 0.3752 0.0130 C25 0.3937 0.0130 C26	CBMHU STM122 STM121 STM107	STM108 STM121	CONDUIT	41.5 90.6	0. 0. 0.	.1504 C50 .3521 C51 .9741 C52 .4980 C53	0.0130 0.0130 0.0350	J58 STM213	J57 BASIN3	CONDUIT	14.2	
0.5029 0.0130 C23 0.5054 0.0130 C24 0.3752 0.0130 C25 0.3937 0.0130 C26 0.1932 0.0130 C27	CBMHU STM122 STM121 STM107 STMBB	STM108 STM121 STM107	CONDUIT CONDUIT CONDUIT	41.5 90.6 25.4	0. 0. 0. 0.	.1504 C50 .3521 C51 .9741 C52 .4980 C53 .7450 C54	0.0130 0.0130 0.0350 0.0350	J58 STM213 J60	J57 BASIN3 J61	CONDUIT CONDUIT CONDUIT	14.2 3.1 70.3	
0.5029 0.0130 C23 0.5054 0.0130 C24 0.3752 0.0130 C25 0.3937 0.0130 C26 0.1932 0.0130	CBMHU STM122 STM121 STM107 STMEB J41	STM108 STM121 STM107 J23	CONDUIT CONDUIT CONDUIT CONDUIT	41.5 90.6 25.4 20.7	0. 0. 0. 0. 0.	.1504 C50 .3521 C51 .9741 C52 .4980 C53 .7450 C54 .4039 C55	0.0130 0.0130 0.0350	J58 STM213 J60 J62	J57 BASIN3 J61 J63	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	14.2 3.1 70.3 26.8	
$\begin{array}{cccc} 0.5029 & 0.0130 \\ c23 \\ 0.5054 & 0.0130 \\ c24 \\ 0.3752 & 0.0130 \\ c26 \\ 0.1932 & 0.0130 \\ c27 \\ 0.2347 & 0.0130 \\ c27 \\ 0.0373 & 0.0130 \\ c27 \\ c28 \\ 0.0990 & 0.0130 \end{array}$	CBMHU STW122 STW121 STW107 STMBB J41 STM105	STM108 STM121 STM107 J23 STMCC STM105 STM104	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	41.5 90.6 25.4 20.7 63.9 80.2 10.1	0. 0. 0. 0. 1. 1.	.1504 C50 .3521 C51 .9741 C52 .4980 C53 .7450 C54 .4039 C55 .1643 C56 .6809	0.0130 0.0130 0.0350 0.0350 0.0350	J58 STM213 J60 J62 J64 J65 J67	J57 BASIN3 J61 J63 J66 J68	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	14.2 3.1 70.3 26.8 37.1 51.5 10.1	
$\begin{array}{ccc} 0.5029 & 0.0130 \\ c23 \\ 0.5054 & 0.0130 \\ c24 \\ 0.3752 & 0.0130 \\ c25 \\ 0.3937 & 0.0130 \\ c26 \\ 0.1932 & 0.0130 \\ c27 \\ 0.2347 & 0.0130 \\ c27 \\ 0.0873 & 0.0130 \\ c28 \\ 0.0990 & 0.0130 \\ c29 \\ 0.1394 & 0.0130 \end{array}$	CEMHU STW122 STW121 STM107 STMBB J41 STM105 STM104	STM108 STM121 STM107 J23 STMCC STM105 STM104 STM102	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	41.5 90.6 25.4 20.7 63.9 80.2 10.1 78.9	0. 0. 0. 0. 1. 1.	.1504 C50 .3521 C51 .9741 C52 .4980 C53 .7450 C53 .7450 C55 .1643 C55 .1643 C55 .6809 C57 .8247	0.0130 0.0130 0.0350 0.0350 0.0350 0.0350	358 STM213 J60 J62 J64 J65 J67 J69	J57 BASIN3 J61 J63 J66 J68 J68	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	14.2 3.1 70.3 26.8 37.1 51.5 10.1 52.1	
$\begin{array}{cccc} 0.5029 & 0.0130 \\ c23 \\ 0.5054 & 0.0130 \\ c24 \\ 0.3752 & 0.0130 \\ c25 \\ 0.3937 & 0.0130 \\ c26 \\ 0.1932 & 0.0130 \\ c27 \\ 0.2347 & 0.0130 \\ c27 \\ 0.0873 & 0.0130 \\ c28 \\ 0.0990 & 0.0130 \\ c29 \\ 0.1394 & 0.0130 \\ c3 \\ c3 \\ c30 \end{array}$	CBMHU STM122 STM121 STM107 STMBB J41 STM105 STM104 STM119 STM102	STM108 STM121 STM107 J23 STMCC STM105 STM104	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	41.5 90.6 25.4 20.7 63.9 80.2 10.1	0. 0. 0. 0. 1. 1. 0.	.1504 C50 .3521 C51 .9741 C52 .4980 C53 .4980 C54 .4039 C55 .6809 C57 .68247 C58 .5794 C59	0.0130 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350	J58 STM213 J60 J62 J64 J65 J67	J57 BASIN3 J61 J63 J66 J68	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	14.2 3.1 70.3 26.8 37.1 51.5 10.1	
$\begin{array}{cccc} 0.5029 & 0.0130 \\ c23 \\ 0.5054 & 0.0130 \\ c24 \\ 0.3752 & 0.0130 \\ c25 \\ 0.3937 & 0.0130 \\ c26 \\ 0.1932 & 0.0130 \\ c27 \\ 0.2347 & 0.0130 \\ c27 \\ 0.0873 & 0.0130 \\ c28 \\ 0.0990 & 0.0130 \\ c28 \\ 0.1394 & 0.0130 \\ c3 \\ c3 \\ 0.11976 & 0.0130 \\ c30 \\ c31 \\ \end{array}$	CBMHU STM122 STM121 STM107 STMBB J41 STM105 STM104 STM104 STM119 STM102 J26	STM108 STM121 STM107 J23 STMCC STM105 STM104 STM102 STM118	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	41.5 90.6 25.4 20.7 63.9 80.2 10.1 78.9 60.7	0. 0. 0. 0. 1. 1. 0. 0. 0.	1504 C50 3521 C51 9741 C52 4980 C53 7450 C54 4039 C55 1643 C56 6809 C55 8247 C58 8247 C58 .5794 C59 .0823 C6	0.0130 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350	J58 STM213 J60 J62 J64 J65 J67 J69 J69	J57 BASIN3 J61 J63 J66 J68 J68 J68 J70	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	14.2 3.1 70.3 26.8 37.1 51.5 10.1 52.1 39.7	
$\begin{array}{cccc} 0.5029 & 0.0130 \\ 0.23 \\ 0.5054 & 0.0130 \\ 0.24 \\ 0.3752 & 0.0130 \\ 0.25 \\ 0.3937 & 0.0130 \\ 0.26 \\ 0.1932 & 0.0130 \\ 0.277 \\ 0.2347 & 0.0130 \\ 0.277 \\ 0.0873 & 0.0130 \\ 0.278 \\ 0.0990 & 0.0130 \\ 0.28 \\ 0.0990 & 0.0130 \\ 0.23 \\ 0.1394 & 0.0130 \\ 0.33 \\ 0.1325 & 0.0130 \\ 0.31 \\ 0.4383 & 0.0130 \\ 0.32 \\ \end{array}$	CBMHU STM122 STM121 STM107 STMBB J41 STM105 STM104 STM104 STM119 STM102 J26 J27	STM108 STM121 STM107 J23 STMCC STM105 STM104 STM102 STM118 J26	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	41.5 90.6 25.4 20.7 63.9 80.2 10.1 78.9 60.7 17.8	0. 0. 0. 0. 1. 1. 0. 0. 0. 0. 0.	1504 C50 3521 C51 9741 C52 4980 C52 4980 C53 .7450 C54 4039 C55 .6809 C55 .8247 C58 .5794 C59 C5794 C59 C5794 C59 C622 C612 C57 C57 C57 C57 C54 C56 C57 C54 C56 C57 C54 C56 C56 C57 C54 C56 C57 C54 C56 C56 C57 C54 C56 C57 C54 C56 C57 C54 C56 C57 C57 C57 C56 C57 C57 C57 C57 C56 C57 C57 C57 C57 C57 C57 C57 C57	0.0130 0.0130 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0130	J58 STM213 J60 J62 J64 J65 J67 J69 J69 STM207	J57 BASIN3 J61 J63 J66 J68 J68 J70 STM206	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	14.2 3.1 70.3 26.8 37.1 51.5 10.1 52.1 39.7 24.3	
$\begin{array}{c} 0.5029 \\ 0.5029 \\ 0.5054 \\ 0.13752 \\ 0.3752 \\ 0.3937 \\ 0.13752 \\ 0.13937 \\ 0.1392 \\ 0.13937 \\ 0.1392 \\ 0.1392 \\ 0.1392 \\ 0.1392 \\ 0.0130 \\ 0.2347 \\ 0.0130 \\ 0.2347 \\ 0.0130 \\ 0.234 \\ 0.0130 \\ 0.1394 \\ 0.0130 \\ 0.3950 \\ 0.1394 \\ 0.0130 \\ 0.3950 \\ 0.132 \\ 0.1394 \\ 0.0130 \\ 0.334 \\ 0.1397 \\ 0.0130 \\ 0.334 \\ 0.1395 \\ 0.0130 \\ 0.333 \\ 0.4665 \\ 0.0130 \\ 0.330 \\ 0.4663 \\ 0.0130 \\ 0.3130 \\ 0.330 \\ 0.3695 \\ 0.0130 \\ 0.330 \\ 0.4663 \\ 0.0130 \\ 0.330 \\ 0.4663 \\ 0.0130 \\ 0.330 \\ 0.4663 \\ 0.0130 \\ 0.300 $	CBMHU STM122 STM121 STM107 STMBB J41 STM105 STM104 STM104 STM119 STM102 J26 J27 J37	STM108 STM121 STM107 J23 STMCC STM105 STM104 STM102 STM118 J26 J27	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	41.5 90.6 25.4 20.7 63.9 80.2 10.1 78.9 60.7 17.8 4.6		1504 C50 3521 C51 9741 C52 4980 C53 7450 C54 4039 C55 1643 C55 1643 C55 1643 C55 82247 C58 82247 C59 0.0823 C6 0.0914 C60 1109 C61 1016	0.0130 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350	J58 STM213 J60 J62 J64 J65 J67 J69 J69 STM207 STM209	J57 BASIN3 J61 J63 J66 J68 J68 J70 STM206 STM208	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	14.2 3.1 70.3 26.8 37.1 51.5 10.1 52.1 39.7 24.3 65.6 36.1 29.5	
$\begin{array}{c} 0.5029 \\ 0.5029 \\ 0.3752 \\ 0.3752 \\ 0.3752 \\ 0.3937 \\ 0.3752 \\ 0.3937 \\ 0.0130 \\ 0.25 \\ 0.1932 \\ 0.0130 \\ 0.2347 \\ 0.0130 \\ 0.2347 \\ 0.0130 \\ 0.2347 \\ 0.0130 $	CEMHU STM122 STM121 STM107 STMBB J41 STM105 STM104 STM119 STM102 J26 J27 J37 J1	STM108 STM121 STM107 J23 STMCC STM105 STM104 STM102 STM102 J26 J27 J28 J1 CBMHU	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	41.5 90.6 25.4 20.7 63.9 80.2 10.1 78.9 60.7 17.8 4.6 8.1 19.3 28.7		1504 C50 3521 C51 9741 C52 9741 C52 4980 C53 1643 C56 6809 C57 8247 C58 5794 C59 0823 C6 0914 C60 1100 C61 1016 C62	0.0130 0.0130 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0130 0.0130	J58 STM213 J60 J62 J64 J65 J67 J69 STM207 STM207 STM209 STM206 STM205 STM204	J57 BASIN3 J61 J63 J66 J68 J68 J68 J70 STM206 STM206 STM208 STM205 STM204 STM204	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	14.2 3.1 70.3 26.8 37.1 51.5 10.1 52.1 39.7 24.3 65.6 36.1 29.5 27.1	
$\begin{array}{c} 0.5029 \\ 0.5029 \\ 0.3752 \\ 0.3752 \\ 0.3752 \\ 0.3937 \\ 0.0130 \\ 0.25 \\ 0.1932 \\ 0.0130 \\ 0.27 \\ 0.2347 \\ 0.0130 \\ 0.27 \\ 0.2347 \\ 0.0130 \\ 0.27 \\ 0.0397 \\ 0.0130 \\ 0.0130 \\ 0.0990 \\ 0.0130 \\ 0.0100 \\ 0.0130 \\ 0.01$	CEMHU STM122 STM121 STM107 STMBB J41 STM105 STM104 STM19 STM102 J26 J27 J37 J1 STMA	STM108 STM121 STM107 J23 STMCC STM105 STM104 STM102 STM102 J26 J27 J28 J1 CBMHU STMB	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	41.5 90.6 25.4 20.7 63.9 80.2 10.1 78.9 60.7 17.8 4.6 8.1 19.3 28.7 100.1		1504 C50 3521 C51 9741 C52 9741 C52 07450 C54 4039 C55 0823 C56 0.0914 C66 0.0914 C62 C60 1109 C61 1105 C63 C64 C65 C64 C65 C66 C65 C66 C66 C66 C66 C66	0.0130 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0130 0.0130 0.0130	J58 STM213 J60 J62 J64 J65 J67 J69 J69 STM207 STM207 STM209 STM204 STM204 STM204 STM203	J57 BASIN3 J61 J63 J66 J68 J68 J68 J70 STM206 STM206 STM208 STM205 STM204 STM203 STM1202	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	14.2 3.1 70.3 26.8 37.1 51.5 10.1 52.1 39.7 24.3 65.6 36.1 29.5 27.1 41.6	
$\begin{array}{ccccc} 0.5029 & 0.0130 \\ c23 \\ 0.5054 & 0.0130 \\ c24 \\ 0.3752 & 0.0130 \\ c25 \\ 0.1932 & 0.0130 \\ c26 \\ 0.1932 & 0.0130 \\ c27 \\ 0.2347 & 0.0130 \\ c27 \\ 0.347 & 0.0130 \\ c27 \\ 0.0873 & 0.0130 \\ c28 \\ 0.0990 & 0.0130 \\ c30 \\ c31 \\ 0.1394 & 0.0130 \\ c31 \\ 0.1395 & 0.0130 \\ c31 \\ 0.4383 & 0.0130 \\ c33 \\ 0.3695 & 0.0130 \\ c33 \\ 0.4653 & 0.0130 \\ c34 \\ 0.5227 & 0.0130 \\ c35 \\ 0.0999 & 0.0130 \\ c36 \\ 0.0761 & 0.0130 \\ c36 \\ 0.0761 & 0.0130 \\ c36 \\ 0.0761 & 0.0130 \\ c31 \\ 0.0130 \\ c36 \\ 0.0761 & 0.0130 \\ c36 \\ 0.0761 & 0.0130 \\ c31 \\ c36 \\ 0.0761 & 0.0130 \\ c36 \\ 0.0761 & 0.0130 \\ c31 \\ c36 \\ c36 \\ c36 \\ c36 \\ c37 \\ c31 \\ c36 \\ c36 \\ c36 \\ c36 \\ c37 \\ c31 \\ c36 \\ c37 \\ c31 \\ c36 \\ c36 \\ c36 \\ c36 \\ c37 \\ c36 \\$	CEMHU STW122 STW121 STW107 STWBB J41 STW105 STW104 STW104 STW102 J26 J27 J37 J1 STWA STMA STMB	STM108 STM121 STM107 J23 STMCC STM105 STM104 STM102 STM108 J26 J27 J28 J1 CBMHU STMB STME	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	41.5 90.6 25.4 20.7 63.9 80.2 10.1 78.9 60.7 17.8 4.6 8.1 19.3 28.7 100.1 105.1		1504 C50 3521 C51 9741 C52 4980 C52 4980 C53 7450 C54 4039 C55 C55 C56 6257 C56 C56 C56 C5794 C594 C5794 C594 C5794 C594 C594 C594 C594 C594 C594 C594 C594 C594 C594 C594 C594 C594 C594 C595 C594 C694 C69	0.0130 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0130 0.0130 0.0130 0.0130	J58 STM213 J60 J62 J64 J65 J67 J69 J69 STM207 STM207 STM209 STM204 STM204 STM204 STM203 STM12	J57 BASIN3 J61 J63 J66 J68 J66 J68 J70 STM206 STM206 STM208 STM205 STM204 STM203 STM109	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	14.2 3.1 70.3 26.8 37.1 51.5 10.1 52.1 39.7 24.3 65.6 36.1 29.5 27.1 41.6 44.0	
$\begin{array}{cccc} 0.5029 & 0.0130 \\ 0.23 \\ 0.5054 & 0.0130 \\ 0.24 \\ 0.3752 & 0.0130 \\ 0.25 \\ 0.3937 & 0.0130 \\ 0.26 \\ 0.1932 & 0.0130 \\ 0.277 \\ 0.2347 & 0.0130 \\ 0.277 \\ 0.0873 & 0.0130 \\ 0.272 \\ 0.0873 \\ 0.0130 \\ 0.035 \\ 0.00761 \\ 0.0130 \\ 0.01$	CBMHU STM122 STM121 STM107 STMBB J41 STM105 STM104 STM104 STM102 J26 J27 J37 J1 STMA STMB J52 STMA	STM108 STM121 STM107 J23 STMCC STM105 STM104 STM102 STM102 J26 J27 J28 J1 CBMHU STMB	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	41.5 90.6 25.4 20.7 63.9 80.2 10.1 78.9 60.7 17.8 4.6 8.1 19.3 28.7 100.1		11504 C50 3521 C51 9741 C52 4980 C53 7450 C54 4039 C55 1643 C55 1643 C55 1643 C55 1643 C55 C56 6809 C57 8247 C55 C58 C59 0823 C6 0914 C60 0914 C62 C61 1016 C62 C61 1016 C62 C63 0962 C64 1136 C66 C66	0.0130 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130	J58 STM213 J60 J62 J64 J65 J67 J69 J69 STM207 STM207 STM209 STM204 STM204 STM204 STM203	J57 BASIN3 J61 J63 J66 J68 J68 J68 J70 STM206 STM206 STM208 STM205 STM204 STM203 STM1202	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	14.2 3.1 70.3 26.8 37.1 51.5 10.1 52.1 39.7 24.3 65.6 36.1 29.5 27.1 41.6	
$\begin{array}{cccc} 0.5029 & 0.0130 \\ 0.23 \\ 0.5054 & 0.0130 \\ 0.24 \\ 0.3752 & 0.0130 \\ 0.25 \\ 0.3937 & 0.0130 \\ 0.26 \\ 0.1932 & 0.0130 \\ 0.27 \\ 0.2347 & 0.0130 \\ 0.27 \\ 0.0873 & 0.0130 \\ 0.27 \\ 0.0873 & 0.0130 \\ 0.27 \\ 0.0873 & 0.0130 \\ 0.29 \\ 0.1394 & 0.0130 \\ 0.29 \\ 0.1394 & 0.0130 \\ 0.33 \\ 0.1976 & 0.0130 \\ 0.33 \\ 0.0130 \\ 0.33 \\ 0.33 \\ 0.3695 & 0.0130 \\ 0.33 \\ 0.33 \\ 0.3695 & 0.0130 \\ 0.33 \\ 0.35 \\ 0.035 \\ 0.0130 \\ 0.35 \\ 0.0130 \\ 0.35 \\ 0.0130 \\ 0.35 \\ 0.0130 \\ 0.35 \\ 0.0130 \\ 0.35 \\ 0.0130 \\ 0.35 \\ 0.0130 \\ 0.35 \\ 0.0130 \\ 0.35 \\ 0.0130 \\ 0.38 \\ 0.1498 & 0.0130 \\ 0.39 \\ 0.0130 \\ 0.39 \\ 0.0130 \\ 0.39 \\ 0.0130 \\ 0.39 \\ 0.0130 \\ 0.39 \\ 0.0130 \\ 0.39 \\ 0.0130 \\ 0.39 \\ 0.0130 \\$	CBMHU STM122 STM121 STM107 STMBB J41 STM105 STM104 STM104 STM102 J26 J27 J37 J1 STMA STMB J52 STMA CBMHA2	STM108 STM121 STM107 J23 STMCC STM105 STM104 STM102 STM102 STM118 J26 J27 J28 J1 CBMHU STMB STMC J57	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	41.5 90.6 25.4 20.7 63.9 80.2 10.1 78.9 60.7 17.8 4.6 8.1 19.3 28.7 100.1 105.1 35.4		11504 C50 3521 C51 9741 C52 4980 C53 7450 C54 4039 C55 1643 C55 1643 C55 1643 C55 1643 C55 C56 6809 C55 C57 8247 C58 C57 C58 C59 0823 C66 C60 1109 C62 C61 1016 C62 C63 0.962 C64 1136 C66 C66 C66 C66 C66 C66 C66 C	0.0130 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130	J58 STM213 J60 J62 J64 J65 J67 J69 J69 STM207 STM207 STM209 STM204 STM204 STM204 STM203 STM122 STM12	J57 BASIN3 J61 J63 J66 J68 J68 J68 J68 STM206 STM206 STM206 STM208 STM205 STM204 STM203 STM109 STM110	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	14.2 3.1 70.3 26.8 37.1 51.5 10.1 52.1 39.7 24.3 65.6 36.1 29.5 27.1 41.6 44.0 11.0	
$\begin{array}{cccc} 0.5029 & 0.0130 \\ 0.23 \\ 0.5054 & 0.0130 \\ 0.24 \\ 0.3752 & 0.0130 \\ 0.25 \\ 0.3937 & 0.0130 \\ 0.26 \\ 0.1932 & 0.0130 \\ 0.27 \\ 0.2347 & 0.0130 \\ 0.27 \\ 0.0873 & 0.0130 \\ 0.27 \\ 0.0873 & 0.0130 \\ 0.27 \\ 0.0873 & 0.0130 \\ 0.27 \\ 0.0873 & 0.0130 \\ 0.29 \\ 0.1394 & 0.0130 \\ 0.29 \\ 0.1394 & 0.0130 \\ 0.33 \\ 0.0130 \\ 0.33 \\ 0.3695 & 0.0130 \\ 0.33 \\ 0.3695 & 0.0130 \\ 0.33 \\ 0.3695 & 0.0130 \\ 0.33 \\ 0.35 \\ 0.035 \\ 0.0130 \\ 0.35 \\ 0.0130 \\ 0.35 \\ 0.0130 \\ 0.35 \\ 0.0130 \\ 0.35 \\ 0.0130 \\ 0.35 \\ 0.0130 \\ 0.35 \\ 0.0130 \\ 0.01$	CBMHU STM122 STM121 STM107 STMBB J41 STM105 STM104 STM104 STM102 J26 J27 J37 J1 STMA STMB J52 STMA STMB J52 STMAA CBMHA2 STM18	STM108 STM121 STM107 J23 STMCC STM105 STM104 STM102 STM102 STM118 J26 J27 J28 J1 CBMHU STMB STMC J57 STMBB	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	41.5 90.6 25.4 20.7 63.9 80.2 10.1 78.9 60.7 17.8 4.6 8.1 19.3 28.7 100.1 105.1 35.4 73.4		11504 C50 3521 C51 9741 C52 4980 C53 7450 C54 4039 C55 1643 C55 1643 C55 1643 C55 1643 C55 C56 6809 C57 8247 C55 0823 C6 0914 C60 0914 C62 C61 1016 C62 C61 1016 C62 C63 0962 C64 1135 C66 5000 C66 5000 C66 5000 C66 5000 C66 5000 C66 5000 C66 C66 C66 C66 C66 C66 C66	0.0130 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130	J58 STM213 J60 J62 J64 J65 J67 J69 J69 STM207 STM207 STM209 STM204 STM205 STM204 STM203 STM122 STM12 STM12 STM211 TD2_1	J57 BASIN3 J61 J63 J66 J68 J68 J68 J70 STM206 STM206 STM208 STM205 STM204 STM204 STM203 STM109 STM110 TD2_2	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	14.2 3.1 70.3 26.8 37.1 51.5 10.1 52.1 39.7 24.3 65.6 36.1 29.5 27.1 41.6 44.0 11.0 16.0	
$\begin{array}{cccc} 0.5029 & 0.0130 \\ c23 \\ 0.5054 & 0.0130 \\ c24 \\ 0.3752 & 0.0130 \\ c25 \\ 0.1932 & 0.0130 \\ c27 \\ 0.2347 & 0.0130 \\ c27 \\ 0.2347 & 0.0130 \\ c27 \\ 0.0873 & 0.0130 \\ c27 \\ 0.0873 & 0.0130 \\ c30 \\ 0.1976 & 0.0130 \\ c30 \\ c1125 & 0.0130 \\ c31 \\ c33 \\ c33 \\ c34 \\ c33 \\ c34 \\ c34 \\ c34 \\ c35 \\ c36 \\ c36 \\ c36 \\ c37 \\ c38 \\ c39 \\ 0.0130 \\ c31 \\ c36 \\ c31 \\ c33 \\ c36 \\ c34 \\ c35 \\ c36 \\ c36 \\ c36 \\ c36 \\ c37 \\ c38 \\ c39 \\ 0.0130 \\ c39 \\ c39 \\ 0.0130 \\ c39 \\ c31 \\ c39 \\ c39 \\ c39 \\ c39 \\ c39 \\ c31 \\ c39 \\ c39 \\ c39 \\ c31 \\ c39 \\ $	CBMHU STM122 STM121 STM107 STMBB J41 STM105 STM104 STM104 STM102 J26 J27 J37 J1 STMA STMB J52 STMA STMB J52 STMA CBMHA2 STM118 CBA1	STM108 STM121 STM107 J23 STMCC STM105 STM104 STM102 STM102 STM102 J26 J27 J28 J1 CBMHU STMB STMC J57 STMBB STMAA	CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT CONDUIT	41.5 90.6 25.4 20.7 63.9 80.2 10.1 78.9 60.7 17.8 4.6 8.1 19.3 28.7 100.1 105.1 35.4 73.4 35.8		11504 C50 3521 C51 9741 C52 4980 C53 7450 C54 4039 C55 1643 C55 1643 C55 1643 C55 1643 C55 C56 6809 C57 8247 C55 C58 C57 0823 C6 0914 C60 0914 C62 C61 1016 C62 C61 1016 C62 C63 0.0962 C64 1105 C64 1105 C66 C66 C66 C66 C66 C66 C66 C6	0.0130 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130	J58 STM213 J60 J62 J64 J65 J67 J69 STM207 STM207 STM209 STM204 STM204 STM203 STM204 STM203 STM112 STM112 STM211 TD2_1 TD2_2	J57 BASIN3 J61 J63 J66 J68 J68 J68 J70 STM206 STM206 STM206 STM205 STM204 STM203 STM109 STM110 TD2_2 STM1202	CONDUIT CONDUIT	14.2 3.1 70.3 26.8 37.1 51.5 10.1 52.1 39.7 24.3 65.6 36.1 29.5 27.1 41.6 44.0 11.0 16.0 5.8	
$\begin{array}{cccc} 0.5029 & 0.0130 \\ c23 \\ c24 \\ 0.3752 & 0.0130 \\ c24 \\ 0.3752 & 0.0130 \\ c25 \\ 0.1932 & 0.0130 \\ c27 \\ 0.2347 & 0.0130 \\ c27 \\ 0.2347 & 0.0130 \\ c27 \\ 0.0873 & 0.0130 \\ c27 \\ 0.0873 & 0.0130 \\ c30 \\ 0.1976 & 0.0130 \\ c31 \\ 0.1976 & 0.0130 \\ c31 \\ 0.3655 & 0.0130 \\ c33 \\ c34 \\ c33 \\ c36 \\ c34 \\ c35 \\ c36 \\ c36 \\ c37 \\ c38 \\ c39 \\ 0.0130 \\ c36 \\ c38 \\ c39 \\ 0.0130 \\ c36 \\ c31 \\ c31 \\ c31 \\ c31 \\ c31 \\ c33 \\ c36 \\ c33 \\ c36 \\ c33 \\ c36 \\ c37 \\ c38 \\ c39 \\ 0.0130 \\ c39 \\ 0.0130 \\ c39 \\ 0.0130 \\ c39 \\ c39 \\ 0.0130 \\ c40 \\ c40 \\ c41 \\ c327 & 0.0350 \\ c41 \\ c42 \\ c42 \\ c41 \\ c42 \\ c42 \\ c41 \\ c42 \\ c41 \\ c42 \\ c41 \\ c42 \\ c41 \\ c4$	CEMHU STM122 STM121 STM107 STMBB J41 STM105 STM104 STM19 STM102 J26 J27 J37 J1 STM102 J27 J37 J1 STM3 STM8 J52 STM3A CEMH32 STM18 CEM118 CEA1 J48	STM108 STM121 STM107 J23 STMCC STM105 STM104 STM102 STM102 STM118 J26 J27 J28 J1 CBMHU STM18 STMC J57 STMB STMC J57 STMBB STMAA STM117 CBMHA2 J49	CONDUIT CONDUIT	41.5 90.6 25.4 20.7 63.9 80.2 10.1 78.9 60.7 17.8 4.6 8.1 19.3 28.7 100.1 105.1 35.4 73.4 35.8 8.8 92.0 88.2		1504 C50 3521 C51 9741 C52 4980 C52 C54 4039 C55 1643 C556 C556 C557 C579 C5794 C5794 C5794 C5794 C58 C58 C6809 C68 C6809 C68 C69 C69 C69 C69 C69 C69 C69 C69	0.0130 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130	J58 STM213 J60 J62 J64 J65 J67 J69 STM207 STM209 STM207 STM208 STM204 STM203 STM204 STM211 TD2_1 TD2_2 TD3_1 TD2_2 STM114	J57 BASIN3 J61 J63 J66 J68 J68 J68 J70 STM206 STM206 STM206 STM208 STM204 STM203 STM100 TD2_2 STM109 STM110 TD2_2 STM1202 TD3_2 BASIN3 STM209	CONDUIT CONDUIT	14.2 3.1 70.3 26.8 37.1 51.5 10.1 52.1 39.7 24.3 65.6 36.1 29.5 27.1 41.6 44.0 11.0 16.0 5.8 14.0 8.2 74.9	
$\begin{array}{cccc} 0.5029 & 0.0130 \\ c23 \\ c24 \\ 0.3752 & 0.0130 \\ c24 \\ 0.3752 & 0.0130 \\ c25 \\ 0.3937 & 0.0130 \\ c26 \\ 0.1932 & 0.0130 \\ c27 \\ 0.2347 & 0.0130 \\ c27 \\ 0.0873 & 0.0130 \\ c27 \\ 0.0873 & 0.0130 \\ c27 \\ 0.0990 & 0.0130 \\ c30 \\ 0.1976 & 0.0130 \\ c31 \\ 0.1976 & 0.0130 \\ c31 \\ 0.3695 & 0.0130 \\ c33 \\ 0.3695 & 0.0130 \\ c34 \\ 0.5227 & 0.0130 \\ c36 \\ c36 \\ c37 \\ c38 \\ 0.01999 & 0.0130 \\ c36 \\ c39 \\ 0.01397 & 0.0130 \\ c36 \\ c37 \\ c38 \\ 0.1976 & 0.0130 \\ c39 \\ 0.0130 \\ c39 \\ 0.0130 \\ c44 \\ 0.5227 & 0.0130 \\ c36 \\ c37 \\ c38 \\ 0.1498 & 0.0130 \\ c39 \\ 0.1397 & 0.0130 \\ c40 \\ c40 \\ c41 \\ 0.3287 & 0.0350 \\ c43 \\ 0.1904 & 0.0350 \end{array}$	CEMHU STM122 STM121 STM107 STMBB J41 STM105 STM104 STM19 STM102 J26 J27 J37 J1 STM102 J27 J37 J1 STM4 STM8 STM8 CEMHA2 STM18 CEM118 CEA1 J48 J50	STM108 STM121 STM107 J23 STMCC STM105 STM104 STM102 STM102 STM102 J26 J27 J28 J1 CBMHU STM18 STM2 STM5 STM5 STM8 STM6 STM8 STM2 J49 J51	CONDUIT CONDUIT	41.5 90.6 25.4 20.7 63.9 80.2 10.1 78.9 60.7 17.8 4.6 8.1 19.3 28.7 100.1 105.1 35.4 73.4 35.8 8.8 92.0 88.2 105.0		1504 C50 3521 C51 9741 C52 4980 C52 C54 4039 C55 1643 C55 1643 C55 1643 C55 1643 C55 8247 C5794 C5794 C5794 C5794 C5794 C5794 C5794 C68 C5794 C69 C69 C61 1109 C61 1109 C61 1005 C62 C64 C69 C64 C69 C66 C69 C66 C69 C66 C69 C66 C69 C66 C69 C66 C69 C69	0.0130 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130	J58 STM213 J60 J62 J64 J65 J67 J69 STM207 STM209 STM207 STM209 STM205 STM204 STM203 STM112 STM211 TD2_1 TD2_1 TD3_1 TD3_2 STM114 TD5_1	J57 BASIN3 J61 J63 J66 J68 J68 J68 J70 STM206 STM206 STM206 STM208 STM205 STM204 STM203 STM100 TD2_2 STM109 STM110 TD2_2 STM1202 TD3_2 BASIN3 STM209 TD5_2	CONDUIT CONDUIT	14.2 3.1 70.3 26.8 37.1 51.5 10.1 52.1 39.7 24.3 65.6 36.1 29.5 27.1 41.6 44.0 11.0 16.0 5.8 14.0 8.2 74.9 12.5	
$\begin{array}{cccc} 0.5029 & 0.0130 \\ 0.23 \\ 0.5054 & 0.0130 \\ 0.24 \\ 0.3752 & 0.0130 \\ 0.26 \\ 0.1932 & 0.0130 \\ 0.2347 & 0.0130 \\ 0.2347 & 0.0130 \\ 0.27 \\ 0.2347 & 0.0130 \\ 0.27 \\ 0.0873 & 0.0130 \\ 0.27 \\ 0.0873 & 0.0130 \\ 0.29 \\ 0.1394 & 0.0130 \\ 0.29 \\ 0.1394 & 0.0130 \\ 0.29 \\ 0.1394 & 0.0130 \\ 0.33 \\ 0.0130 \\ 0.33 \\ 0.3695 & 0.0130 \\ 0.33 \\ 0.3695 & 0.0130 \\ 0.33 \\ 0.3695 & 0.0130 \\ 0.33 \\ 0.3695 & 0.0130 \\ 0.33 \\ 0.3695 & 0.0130 \\ 0.33 \\ 0.3695 & 0.0130 \\ 0.33 \\ 0.3695 & 0.0130 \\ 0.33 \\ 0.3695 & 0.0130 \\ 0.33 \\ 0.3695 & 0.0130 \\ 0.35 \\ 0.0761 & 0.0130 \\ 0.35 \\ 0.0761 & 0.0130 \\ 0.35 \\ 0.0761 & 0.0130 \\ 0.35 \\ 0.035 \\ 0.0130 \\ 0.37 \\ 0.0555 & 0.0130 \\ 0.37 \\ 0.0555 & 0.0130 \\ 0.37 \\ 0.0555 & 0.0130 \\ 0.37 \\ 0.0555 & 0.0130 \\ 0.37 \\ 0.0555 & 0.0130 \\ 0.37 \\ 0.0555 & 0.0130 \\ 0.39 \\ 0.1397 & 0.0130 \\ 0.39 \\ 0.1397 & 0.0130 \\ 0.3278 & 0.0350 \\ 0.44 \\ 0.2278 & 0.0350 \\ 0.44 \\ 0.3287 & 0.0350 \\ 0.44 \\ 0.3287 & 0.0350 \\ 0.44 \\ 0.3287 & 0.0350 \\ 0.44 \\ 0.0350 \\ 0.0$	CBMHU STM122 STM121 STM107 STMBB J41 STM105 STM104 STM104 STM102 J26 J27 J37 J1 STMA STMB J52 STMA STMB J52 STMA CBMHA2 STM118 CBA1 J48 J50 J51	STM108 STM121 STM107 J23 STMCC STM105 STM104 STM102 STM102 STM118 J26 J27 J28 J1 CBMHU STM18 STMC J57 STMB STMC J57 STMBB STMAA STM117 CBMHA2 J49	CONDUIT CONDUIT	41.5 90.6 25.4 20.7 63.9 80.2 10.1 78.9 60.7 17.8 4.6 8.1 19.3 28.7 100.1 105.1 35.4 73.4 35.8 8.8 92.0 88.2		11504 C50 3521 C51 9741 C52 4980 C53 7450 C54 4039 C55 1643 C55 1643 C55 1643 C55 C56 6809 C57 8247 C58 C57 0823 C6 0914 C60 0914 C60 0914 C62 C61 1016 C62 C61 1016 C62 C63 0962 C64 1105 C66 C64 1105 C66 C64 1105 C66 C64 1105 C66 C64 1105 C66 C64 C64 C64 C64 C64 C64 C64	0.0130 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130	J58 STM213 J60 J62 J64 J65 J67 J69 STM207 STM209 STM207 STM208 STM204 STM203 STM204 STM203 STM112 STM211 TD2_1 TD2_2 TD3_1 TD3_2 STM114 TD5_1 TD5_2	J57 BASIN3 J61 J63 J66 J68 J68 J70 STM206 STM206 STM206 STM205 STM204 STM202 STM100 TD2_2 STM109 STM110 TD2_2 STM1202 TD3_2 BASIN3 STM209 TD5_2 STM26	CONDUIT CONDUIT	14.2 3.1 70.3 26.8 37.1 51.5 10.1 52.1 39.7 24.3 65.6 36.1 29.5 27.1 41.6 44.0 11.0 16.0 5.8 14.0 8.2 74.9	
$\begin{array}{cccc} 0.5029 & 0.0136 \\ 0.23 \\ 0.5054 & 0.0136 \\ 0.24 \\ 0.3752 & 0.0136 \\ 0.25 \\ 0.3937 & 0.0136 \\ 0.26 \\ 0.1932 & 0.0136 \\ 0.27 \\ 0.2347 & 0.0136 \\ 0.27 \\ 0.0873 & 0.0136 \\ 0.27 \\ 0.0873 & 0.0136 \\ 0.29 \\ 0.1394 & 0.0136 \\ 0.29 \\ 0.1394 & 0.0136 \\ 0.29 \\ 0.1394 & 0.0136 \\ 0.29 \\ 0.1394 & 0.0136 \\ 0.33 \\ 0.0136 \\$	CBMHU STM122 STM121 STM107 STMBB J41 STM105 STM104 STM104 STM102 J26 J27 J37 J1 STMA STMB J52 STMA STMB J52 STMA CBMHA2 STM118 CBA1 J48 J50 J51 J52 STM1	STM108 STM121 STM107 J23 STMCC STM105 STM104 STM102 STM102 STM118 J26 J27 J28 J1 CBMHU STM18 STM17 CBMHU STMB STMAA STM117 CBMHA2 J49 J51	CONDUIT CONDUIT	41.5 90.6 25.4 20.7 63.9 80.2 10.1 78.9 60.7 17.8 4.6 8.1 19.3 28.7 100.1 105.1 35.4 73.4 35.8 8.8 92.0 88.2 105.0 21.6		11504 C50 3521 C51 9741 C52 4980 C52 4980 C53 7450 C54 4039 C55 1643 C55 1643 C55 1643 C55 1643 C55 C57 8247 C58 C57 0823 C6 0914 C60 0914 C62 C60 0914 C62 C61 1016 C62 C61 1016 C62 C63 0.0962 C64 1105 C66 C64 1105 C66 C62 2091 C66 C66 C60 C64 1105 C66 C62 C64 C62 C64 C64 C62 C64 C62 C64 C62 C64 C62 C64 C64 C62 C64 C64 C64 C62 C64 C64 C62 C64 C62 C64 C64 C66 C66 C66 C66 C66 C66	0.0130 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130	J58 STM213 J60 J62 J64 J65 J67 J69 STM207 STM209 STM207 STM209 STM205 STM204 STM203 STM112 STM211 TD2_1 TD2_1 TD3_1 TD3_2 STM114 TD5_1	J57 BASIN3 J61 J63 J66 J68 J68 J68 J70 STM206 STM206 STM206 STM208 STM205 STM204 STM203 STM100 TD2_2 STM109 STM110 TD2_2 STM1202 TD3_2 BASIN3 STM209 TD5_2	CONDUIT CONDUIT	14.2 3.1 70.3 26.8 37.1 51.5 10.1 52.1 39.7 24.3 65.6 36.1 29.5 27.1 41.6 44.0 11.0 16.0 5.8 14.0 8.2 74.9 12.5 3.0	
$\begin{array}{cccc} 0.5029 & 0.0130 \\ 0.23 \\ 0.5054 & 0.0130 \\ 0.24 \\ 0.3752 & 0.0130 \\ 0.25 \\ 0.3937 & 0.0130 \\ 0.26 \\ 0.1932 & 0.0130 \\ 0.27 \\ 0.2347 & 0.0130 \\ 0.27 \\ 0.0873 & 0.0130 \\ 0.27 \\ 0.0873 & 0.0130 \\ 0.29 \\ 0.1394 & 0.0130 \\ 0.29 \\ 0.1394 & 0.0130 \\ 0.29 \\ 0.1394 & 0.0130 \\ 0.33 \\ 0.0130 \\ 0.33 \\ 0.0130 \\ 0.33 \\ 0.0130 \\ 0.33 \\ 0.33 \\ 0.3655 & 0.0130 \\ 0.33 \\ 0.33 \\ 0.3665 & 0.0130 \\ 0.33 \\ 0.3665 & 0.0130 \\ 0.33 \\ 0.3665 & 0.0130 \\ 0.33 \\ 0.3665 & 0.0130 \\ 0.33 \\ 0.366 \\ 0.0761 & 0.0130 \\ 0.35 \\ 0.0399 & 0.0130 \\ 0.35 \\ 0.0761 & 0.0130 \\ 0.35 \\ 0.0761 & 0.0130 \\ 0.35 \\ 0.0761 & 0.0130 \\ 0.35 \\ 0.035 \\ 0.0130 \\ 0.1397 & 0.0130 \\ 0.44 \\ 0.2278 & 0.0130 \\ 0.44 \\ 0.3287 & 0.0350 \\ 0.44 \\ 0.3287 & 0.0350 \\ 0.44 \\ 0.3287 & 0.0350 \\ 0.44 \\ 0.0350 \\ 0.44 \\ 0.0350 \\ 0.44 \\ 0.0350 \\ 0.44 \\ 0.0350 \\ 0.44 \\ 0.0350 \\ 0.44 \\ 0.0350 \\ 0.44 \\ 0.0350 \\ 0.44 \\ 0.0350 \\ 0.44 \\ 0.0350 \\ 0.44 \\ 0.0350 \\ 0.44 \\ 0.0455 \\ 0.0130 \\ 0.0130 \\ 0.0130 \\ 0.035$	CBMHU STM122 STM121 STM107 STMBB J41 STM105 STM104 STM104 STM102 J26 J27 J37 J1 STMA STMB J52 STMA STMB J52 STMA CBMHA2 STM18 CBA1 J48 J50 J51 J52 STM18	STM108 STM121 STM107 J23 STMCC STM105 STM104 STM102 STM102 STM102 J26 J27 J28 J1 CBMHU STM18 STM2 STM2 STMB STM2 STMB STM2 J57 STMBB STMAA STM17 CBMHA2 J49 J51 J48 J53	CONDUIT CONDUIT	41.5 90.6 25.4 20.7 63.9 80.2 10.1 78.9 60.7 17.8 4.6 8.1 19.3 28.7 100.1 105.1 35.4 73.4 35.8 8.8 92.0 88.2 105.0 21.6 90.8		11504 C50 3521 C51 9741 C52 4980 C52 4980 C53 7450 C54 4039 C55 1643 C55 1643 C55 1643 C55 C56 6809 C57 8247 C58 C57 0823 C66 0914 C62 C60 0914 C62 C61 1016 C62 C61 1016 C62 C63 0.0962 C64 1105 C66 C62 2091 C66 C66 5000 C64 1105 C66 C64 1105 C66 C66 C62 C64 1105 C66 C66 C66 C66 C66 C66 C66 C6	0.0130 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130	J58 STM213 J60 J62 J64 J65 J67 J69 STM207 STM209 STM206 STM204 STM203 STM204 STM211 TD2_1 TD2_1 TD2_2 TD3_1 TD3_2 STM114 TD5_1 TD5_2 TD5_2 TD6_1	J57 BASIN3 J61 J63 J66 J68 J68 J70 STM206 STM206 STM206 STM208 STM205 STM204 STM202 STM100 TD2_2 STM109 STM110 TD2_2 STM1202 TD3_2 BASIN3 STM209 TD5_2 STM26 STM26 STM26 STM26 STM26 STM26 STM26 STM27	CONDUIT CONDUIT	14.2 3.1 70.3 26.8 37.1 51.5 10.1 52.1 39.7 24.3 65.6 36.1 29.5 27.1 41.6 44.0 11.0 16.0 5.8 14.0 8.2 74.9 12.5 3.0 21.5	
$\begin{array}{cccc} 0.5029 & 0.0130 \\ 0.23 \\ 0.5054 & 0.0130 \\ 0.24 \\ 0.3752 & 0.0130 \\ 0.25 \\ 0.3937 & 0.0130 \\ 0.26 \\ 0.1932 & 0.0130 \\ 0.27 \\ 0.2347 & 0.0130 \\ 0.27 \\ 0.0873 & 0.0130 \\ 0.27 \\ 0.0873 & 0.0130 \\ 0.29 \\ 0.1394 & 0.0130 \\ 0.29 \\ 0.1394 & 0.0130 \\ 0.29 \\ 0.1394 & 0.0130 \\ 0.33 \\ 0.0130 \\ 0.33 \\ 0.0130 \\ 0.33 \\ 0.0130 \\ 0.33 \\ 0.0130 \\ 0.33 \\ 0.0130 \\ 0.33 \\ 0.0130 \\ 0.33 \\ 0.0130 \\ 0.33 \\ 0.0130 \\ 0.33 \\ 0.0130 \\ 0.33 \\ 0.0130 \\ 0.33 \\ 0.0130 \\ 0.33 \\ 0.0130 \\ 0.33 \\ 0.0130 \\ 0.33 \\ 0.0130 \\ 0.33 \\ 0.0130 $	CBMHU STM122 STM121 STM107 STMBB J41 STM105 STM104 STM104 STM102 J26 J27 J37 J1 STMA STMB J52 STMA STMB J52 STMA CBMHA2 STM18 CBA1 J48 J50 J51 J52 STM18 STM18	STM108 STM121 STM107 J23 STMCC STM105 STM104 STM102 STM102 J26 J27 J28 J1 CBMHU STM18 STM18 STM2 STM2 STM8 STM8 STM6 STM8 STM17 CBMHA2 J49 J51 J48 J53 J54	CONDUIT CONDUIT	41.5 90.6 25.4 20.7 63.9 80.2 10.1 78.9 60.7 17.8 4.6 8.1 19.3 28.7 100.1 105.1 35.4 73.4 35.8 8.8 92.0 88.2 105.0 21.6 90.8 22.0 -		11504 C50 3521 C51 9741 C52 4980 C52 4980 C53 7450 C54 4039 C54 4039 C55 1643 C55 1643 C56 6809 C57 8247 C58 C57 0823 C66 0914 C66 C60 1109 C66 C61 1016 C62 C61 1016 C62 C64 1105 C64 1105 C66 C64 1105 C66 C64 1105 C66 C64 1105 C66 C64 1105 C66 C64 1105 C66 C64 1105 C66 C64 1105 C66 C64 1105 C66 C66 C60 C64 1105 C66 C66 C66 C67 2091 C66 C66 C66 C66 C66 C66 C66 C6	0.0130 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130	J58 STM213 J60 J62 J64 J65 J67 J69 STM207 STM209 STM206 STM205 STM204 STM203 STM112 STM211 TD2_1 TD2_1 TD2_1 TD3_1 TD3_2 STM114 TD5_1 TD5_1 TD5_2 TD6_1 TD6_2	J57 BASIN3 J61 J63 J66 J68 J68 J68 J70 STM206 STM206 STM206 STM208 STM205 STM204 STM202 STM100 TD2_2 STM109 STM110 TD2_2 STM1202 TD3_2 BASIN3 STM209 TD5_2 STM26 STM26 STM26 STM26 STM26 STM26 STM26 STM26 STM26 STM26 STM26 STM26 STM26 STM26 STM27 STM26 STM26 STM26 STM26 STM26 STM26 STM26 STM26 STM26 STM27 STM26 S	CONDUIT CONDUIT	14.2 3.1 70.3 26.8 37.1 51.5 10.1 52.1 39.7 24.3 65.6 36.1 29.5 27.1 41.6 44.0 11.0 16.0 5.8 14.0 8.2 74.9 12.5 3.0 21.5 1.9	
0.5029 0.0130 C23 0.5054 0.0130 C24 0.3752 0.0130 C25 0.3937 0.0130 C27 0.2347 0.0130 C27 0.2347 0.0130 C27 0.0873 0.0130 C27 0.0873 0.0130 C39 0.1394 0.0130 C31 0.1394 0.0130 C31 0.1394 0.0130 C31 0.4383 0.0130 C32 0.4383 0.0130 C33 0.4685 0.0130 C34 0.5227 0.0130 C35 0.0999 0.0130 C36 0.01365 0.0130 C37 0.0555 0.0130 C38 0.1397 0.0130 C39 0.1397 0.0130 C44 0.2278 0.0130 C41 0.3287 0.0350 C4 0.0350 0.0130 C4 0.0355 0.0130 C38 0.1397 0.0130 C4 0.0355 0.0130 C4 0.0350 0.0130 C4 0.0355 0.0130 C4 0.0350 0.0130 C4 0.0350 0.0130 C4 0.0355 0.0130 C4 0.0350 0.0130 C4 0.0400 0.0350 0.0130 C4 0.0400 0.0150 0.0130 C4 0.0400	CBMHU STM122 STM121 STM107 STMBB J41 STM105 STM105 STM104 STM19 STM19 J26 J27 J37 J1 STMA STMB J52 STMA STMB J52 STMA CBMHA2 STM18 CBA1 J48 J50 J51 J52 J53 J54 J55 J55 J59	STM108 STM121 STM107 J23 STMCC STM105 STM104 STM102 STM102 J26 J27 J28 J1 CBMHU STM18 STM18 STM2 STM2 STM8 STM8 STM6 STM8 STM8 STM8 STM17 CBMHA2 J49 J51 J48 J53 J54	CONDUIT CONDUIT	41.5 90.6 25.4 20.7 63.9 80.2 10.1 78.9 60.7 17.8 4.6 8.1 19.3 28.7 100.1 105.1 35.4 73.4 35.8 8.8 92.0 88.2 105.0 21.6 90.8 22.0 - 7.7		11504 C50 3521 C51 9741 C52 4980 C52 4980 C53 7450 C54 4039 C55 1643 C55 C54 4039 C55 1643 C55 C57 8247 C55 C58 C57 C58 C57 C58 C59 0823 C66 C59 0823 C66 C60 1109 C61 1016 C62 C63 0962 C64 1105 C66 C62 C64 1105 C66 C62 C64 1105 C66 C62 C64 C62 C64 C62 C64 C62 C64 C62 C64 C62 C64 C62 C64 C62 C64 C62 C64 C62 C64 C62 C64 C65 C66 C62 C64 C62 C64 C66 C66 C66 C66 C66 C66 C66	0.0130 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0350 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130 0.0130	J58 STM213 J60 J62 J64 J65 J67 J69 STM207 STM209 STM206 STM204 STM203 STM204 STM211 TD2_1 TD2_1 TD2_1 TD2_1 TD3_1 TD3_1 TD3_2 STM114 TD5_1 TD5_2 TD6_1 TD6_2 TD6_1	J57 BASIN3 J61 J63 J66 J68 J68 J70 STM206 STM206 STM206 STM208 STM204 STM203 STM100 TD2_2 STM109 STM110 TD2_2 STM109 STM110 TD2_2 TD3_2 BASIN3 STM209 TD5_2 STM26 TD5_2 STM26 TD5_2 STM26 TD5_2 STM27	CONDUIT CONDUIT	14.2 3.1 70.3 26.8 37.1 51.5 10.1 52.1 39.7 24.3 65.6 36.1 29.5 27.1 41.6 44.0 11.0 16.0 5.8 14.0 8.2 74.9 12.5 3.0 21.5 1.9 22.0	

277 278 278 279 279 279 285 279 280 2019 2013 280 2013 291 2014 2015	J72 J71 J71 STM208 J73 CBMH210 J14 STM114 STM114 STM120 STM119 STM118 STM117	STM213 J71 J56 STM207 J72 STM1202 STM114 STM209 STM119 STM118 STM117 STM208	CON CON CON CON CON CON CON	DUIT DUIT DUIT DUIT DUIT DUIT DUIT DUIT	8.1 38.9 59.7 18.4 18.4 22.2 75.5 76.0 61.3 61.3 10.4 8.3	-	W43 W5 W6 W7 W8 Q42 OL1 OL10 OL11 OL12 OL13 OL14 OL15 OL2 OL3 OL4 OL5 OL4 OL5 OL4 OL5 OL6 OL7 OL8 OL9	J73 J19 STMGG STMG8 J37 J49 J61 S-BLDG-H S-BLDG-G S-BLDG-G S-BLDG-K S-BLDG-K S-BLDG-K S-BLDG-J2 J63 J66 J70 S-BLDG-A S-BLDG-C S-BLDG-C S-BLDG-C S-BLDG-C	STM211 J63 TD5_2 TD5_2 J66 STMD STMC STMCCN1 J14 J14 SMMCCN2 STMCCN2 STMCCN2 STMCCN2 STME CBA1 CBMIA2 STM122 STM122 STM122	WE WE WE OU OU OU OU OU OU OU OU OU OU OU OU OU	IR IR IR IR IR TLET TLET TLET TLET TLET TLET TLET TLE		
N31 L417 0.010 N4 1499 0.013 227_1 DR1 DR2 N1 N10 N11	BASIN3 J23 BASIN2 BASIN1 BASIN1 STMB STMC	STM209 BASIN2 J41 J40 J32 J32 J48 J49	CON ORI ORI WEI WEI WEI	R	63.5		Cross Sectio Trull Conduit Flow	n Summary	Full Depth	Full Area	Hyd. Rad.	Max. Width	Ba
V12 V13 V14 V15 V16 V17 V18 V19	STMA STM212 STMD STMDD J52 STM121 STM107 J32 740	J50 J73 J60 TD8_1 STM122 J53 J54 J55 D56JN2	WEI WEI WEI WEI WEI WEI WEI	R R R R R R R			C1 0.64 C10 0.60 C10_1 0.19 C11 0.20 C12	CIRCULAR CIRCULAR CIRCULAR CIRCULAR RECT_OPEN	0.82 1.05 0.60 0.60 1.00	0.53 0.87 0.28 0.28 1.00	0.21 0.26 0.15 0.15 0.33	0.82 1.05 0.60 0.60 1.00	
N2 N20 N21 N22 N23 N26 N3 N3 N33 N33 N33 N33	J40 J56 J59 J58 J57 STM112 J32 STMAA J64	BASIN2 STM108 SWMCCN2 SWMCCN1 STM111A J73 BASIN1 J65 STMBB	WEI WEI WEI WEI WEI WEI WEI WEI	R R R R R R R			4.46 C13 0.04 C14 0.04 C15 0.30 C16	CIRCULAR CIRCULAR CIRCULAR CIRCULAR	0.25 0.25 0.60 0.60	0.05 0.05 0.28 0.28	0.06 0.06 0.15 0.15	0.25 0.25 0.60 0.60	
V35 V35 V36 V37 V38 V39 V41 V41	STMCC J1 CBMHU CBMH2 J72 J71	J62 J55 J56 J68 J70 STM109 J40	WEI WEI WEI WEI WEI WEI	R R R R R			0.25 C17 0.26 C18 0.57 C18_1 2.69 C18_2	CIRCULAR CIRCULAR CIRCULAR CIRCULAR	0.60 0.90 1.35 1.35	0.28 0.64 1.43 1.43	0.15 0.23 0.34 0.34	0.60 0.90 1.35 1.35	
							0.98						
12 22 13 220 51 221 20	CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR	0.90 0.45 0.90 0.53 1.35	0.64 0.16 0.64 0.22 1.43	0.23 0.11 0.23 0.13 0.34	0.90 0.45 0.90 0.53 1.35	1 1 1 1 1 1	C44 0.03 C45 13.63 C46 11.32 C47 42.85	CIRCULAR RECT_OPEN RECT_OPEN RECT_OPEN RECT_OPEN	0.25 1.00 1.00 1.00	0.05 8.00 8.00 8.00	0.06 0.80 0.80 0.80	0.25 8.00 8.00 8.00 8.00	
219 12 22 13 220 51 221 221 221 221 221 221 222 222 222	CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR	0.45 0.90 0.53 1.35 1.35 0.20 0.25 0.68 0.68	0.16 0.64 0.22 1.43 1.43 0.03 0.05 0.36 0.36	0.11 0.23 0.13 0.34 0.34 0.05 0.06 0.17 0.17	0.45 0.90 0.53 1.35 1.35 0.20 0.25 0.68 0.68	1 1 1 1 1 1 1 1 1	C44 0.03 C45 13.63 C46 11.32 C47 42.85 C48 32.71 C49 59.94 C5 0.24 C50 31.48 C51 0.06 C52 5.39	RECT_OPEN RECT_OPEN RECT_OPEN RECT_OPEN CIRCULAR RECT_OPEN CIRCULAR TRAPEZOIDAL	1.00 1.00 1.00 1.00 0.60 1.00 0.25 1.00	8.00 8.00 8.00 8.00 0.28 8.00 0.25 4.00	0.80 0.80 0.80 0.80 0.15 0.80 0.06 0.55	8.00 8.00 8.00 8.00 0.60 8.00 0.25 7.00	
12 22 23 33 20 31 20 20 21 21 22 21 21 22 22 22 22 22	CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR	0.45 0.90 0.53 1.35 1.35 0.20 0.25 0.68	0.16 0.64 0.22 1.43 1.43 0.03 0.05 0.36	0.11 0.23 0.13 0.34 0.34 0.05 0.06 0.17	0.45 0.90 0.53 1.35 1.35 0.20 0.25 0.68	1 1 1 1 1 1 1 1	C44 0.03 C45 13.63 C46 11.32 C47 42.85 C48 32.71 C49 59.94 C5 0.24 C50 31.48 C51 0.06 C52 C53 6.59 C53 6.59 C54 4.85 C55 8.24 C55 8.24 C55 8.24 C55 8.24 C55 8.24 C55 8.24 C55 8.24 C55 8.24 C55 8.24 C57 C57 C58	RECT_OPEN RECT_OPEN RECT_OPEN RECT_OPEN CIRCULAR RECT_OPEN CIRCULAR	1.00 1.00 1.00 1.00 0.60 1.00 0.25	8.00 8.00 8.00 8.00 0.28 8.00 0.05	0.80 0.80 0.80 0.80 0.80 0.15 0.80 0.06	8.00 8.00 8.00 8.00 0.60 8.00 0.25	
12 12 12 13 120 11 121 121 121 121 121 121 121 121 122 122 123 124 135 125 133 125 127 126 127 128 129 133 1330 75 131 1330 75 131 1330 1330 1331 14 1334	CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR	0.45 0.90 0.53 1.35 0.20 0.25 0.68 1.35 0.53 0.97 0.97	0.16 0.64 0.22 1.43 1.43 0.03 0.05 0.36 0.36 1.43 0.22 0.75 0.75 0.75	0.11 0.23 0.13 0.34 0.05 0.06 0.17 0.17 0.34 0.13 0.24 0.24	0.45 0.90 0.53 1.35 0.20 0.25 0.68 0.68 1.35 0.53 0.97 0.97 0.97	1 1 1 1 1 1 1 1 1 1 1 1 1 1	C44 0.03 C45 13.63 C46 11.32 C47 42.85 C48 32.71 C49 59.94 C49 59.94 C5 C50 C51 C51 C52 C53 C53 C53 C53 C54 4.85 C55 8.24 C55 C54 4.85 C55 C54 C55 C55 C54 C55 C55 C55 C55 C5	RECT_OPEN RECT_OPEN RECT_OPEN RECT_OPEN CIRCULAR RECT_OPEN CIRCULAR TRAPEZOIDAL TRAPEZOIDAL TRAPEZOIDAL TRAPEZOIDAL TRAPEZOIDAL	1.00 1.00 1.00 1.00 0.60 1.00 0.25 1.00 1.00 1.00 1.00	8.00 8.00 8.00 8.00 0.28 8.00 0.05 4.00 4.00 4.00 3.00	0.80 0.80 0.80 0.15 0.80 0.06 0.55 0.55 0.55 0.47 0.47	8.00 8.00 8.00 0.60 8.00 0.25 7.00 7.00 7.00 7.00 6.00	
12 22 23 33 20 51 20 20 21 21 21 22 22 22 22 22 22 22	CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR	0.45 0.90 0.53 1.35 0.20 0.25 0.68 1.35 0.53 0.97 0.97 0.97 0.97 0.97 0.97	0.16 0.64 0.22 1.43 1.43 0.03 0.05 0.36 1.43 0.22 0.75 0.75 0.75 0.75 0.75 0.75 0.75 0.75	0.11 0.23 0.13 0.34 0.34 0.05 0.06 0.17 0.17 0.34 0.24 0.24 0.24 0.24 0.24 0.24 0.24 0.2	0.45 0.90 0.53 1.35 0.20 0.25 0.68 0.68 1.35 0.53 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97		C44 0.03 C45 13.63 C46 11.32 C47 42.85 C48 32.71 C49 S9.94 C5 0.24 C50 31.48 C51 0.06 C52 S.39 C53 C54 4.85 C55 S.24 C55 S.24 C55 S.24 C55 S.24 C55 S.24 C55 C57 C57 C57 C57 C57 C57 C57 C57 C58 C55 C55 C55 C55 C55 C55 C55 C55 C55	RECT_OPEN RECT_OPEN RECT_OPEN RECT_OPEN CIRCULAR RECT_OPEN CIRCULAR TRAPEZOIDAL TRAPEZOIDAL TRAPEZOIDAL TRAPEZOIDAL TRAPEZOIDAL CIRCULAR CIRCULAR CIRCULAR	1.00 1.00 1.00 1.00 0.60 1.00 0.25 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.0	8.00 8.00 8.00 8.00 0.28 8.00 0.05 4.00 4.00 4.00 3.00 3.00 3.00 0.87 0.64 0.87	0.80 0.80 0.80 0.15 0.80 0.65 0.55 0.55 0.55 0.47 0.47 0.47 0.47 0.26 0.23 0.26	8.00 8.00 8.00 8.00 0.60 8.00 0.25 7.00 7.00 7.00 6.00 6.00 6.00 1.05 0.90 1.05	

71	CIRC	111.28	0.25	0.05	0.06	0.25	1		0.0326	0.0620	0.0927	0.1255	0.15
2		_OPEN	0.25	0.05	0.08	0.25	1		0.1941 0.4018	0.2345	0.2757 0.4860	0.3174 0.5280	0.157
3	CIRC		0.25	0.05	0.06	0.25	1		0.6191	0.6650	0.7103	0.7551	0.799
5 7 4		_OPEN	0.31	0.06	0.08	0.20	1		1.0552	1.0963	1.1369	1.1770	1.216
5	CIRC	ULAR	0.25	0.05	0.06	0.25	1		1.4465	1.4834	1.5199	1.5561	1.591
6 16	RECT	_OPEN	0.33	0.07	0.08	0.20	1	Width:	1.3366	1.2373	1.1497	1.0712	1.000
7	CIRC	ULAR	0.25	0.05	0.06	0.25	1		0.2699 0.8096	0.4300	0.5564	0.6554	0.7492
8	RECT	OPEN	1.00	8.00	0.80	8.00	1		0.9452	0.9640	0.9791	0.9940	1.0000
	RECT	OPEN	1.00	8.00	0.80	8.00	1		1.0000	1.0000	1.0000	1.0000	1.0000
_	CIRC	ULAR	1.05	0.87	0.26	1.05	1		1.0000	1.0000	1.0000	1.0000	1.0000
2	RECT	_OPEN	1.00	8.00	0.80	8.00	1		1.0000	1.0000	1.0000 0.2963	0.8889	0.740
	CIRC	ULAR	0.60	0.28	0.15	0.60	1	Shape 0.5					
1	RECT	_OPEN	1.00	14.00	0.87	14.00	1	Area:	-	0.0029	0.0063	0.0108	0.016
9		_OPEN	1.00	14.00	0.87	14.00	1		0.0230	0.0306	0.0392	0.0487 0.1097	0.059
		_OPEN	1.00	4.00	0.67	4.00	1		0.1399	0.1562	0.1733 0.2694	0.1911 0.2908	0.209
		_OPEN	1.00	4.00	0.67	4.00	1		0.3355 0.4589	0.3589	0.3829	0.4075	0.432
6		OPEN	1.00	4.00	0.67	4.00	1		0.5987	0.6287	0.6593	0.6906	0.722
		OPEN	1.00	4.00	0.67	4.00	1	Hrad:	0.9284	0.9598	0.9822	0.9956	1.0000
	CIRC	_OPEN	1.00	9.00	0.82	9.00	1		0.0372	0.0761	0.1167	0.1577 0.3545	0.1973
	CIRC	OLAR	0.90	0.64	0.23	0.90	1		0.4324 0.6298	0.4727	0.5123	0.5513	0.589
*****	****								0.8288	0.8684	0.9079	0.9473	0.987
pe Sur	mary								1.2191	1.2568	1.2943	1.3316	1.368
pe 0.5									1.5879	1.4423 1.6237 1.4768	1.6580	1.6923	1.726
a:	0.0040	0.0122	0.0237	0.0378	0.0541			Width:	0.0402	0.0771	0.1097	0.1387	0.1678
	0.0723	0.0915	0.1116	0.1323	0.1535				0.1958	0.2219	0.2480	0.2741 0.3935	0.3002
	0.2892	0.3125	0.3357	0.3589	0.3821 0.4981				0.4380 0.5392	0.4582	0.4785	0.4987	0.5189
	0.5213	0.5445	0.5677	0.5910	0.6142				0.6327	0.6509	0.6691	0.6872	0.705
	0.7534	0.7766	0.7998	0.8230	0.8462				0.8143 0.9051	0.8325	0.8506	0.8688	0.8870
			0.9931	0.9983	1.0000				0.9876	0.7397	0.4917	0.2445	0.0000
ad:	0.9725	0.9845											
rad:		0.9845											
ape 0.5	0.9725	0.9845							1.6348	1.6651	1.6950	1.7246	1.0000
pe 0.5	0.9725 510_3 0.0005	0.0019	0.0043	0.0076	0.0119			Width:	0.0832	0.1290	0.1738	0.2192	0.2684
pe 0.5	0.9725			0.0076 0.0377 0.0897	0.0119 0.0464 0.1027			Width:					0.268
pe 0.5	0.9725 510_3 0.0005 0.0170	0.0019 0.0230	0.0043 0.0299	0.0377	0.0464			Width:	0.0832 0.3361 0.9547 1.0000 1.0000	0.1290 0.6079	0.1738 0.8354	0.2192	0.268 0.928 1.000 1.000
pe 0.5	0.9725 510_3 0.0005 0.0170 0.0559 0.1165	0.0019 0.0230 0.0663 0.1312	0.0043 0.0299 0.0776 0.1467	0.0377 0.0897 0.1631	0.0464 0.1027 0.1804			Width:	0.0832 0.3361 0.9547 1.0000	0.1290 0.6079 1.0000 1.0000	0.1738 0.8354 1.0000 1.0000 1.0000 1.0000 1.0000	0.2192 0.9071 1.0000 1.0000 1.0000 1.0000 1.0000	0.268 0.928 1.000 1.000 1.000 1.000
pe 0.5	0.9725 10_3 0.0005 0.0170 0.0559 0.1165 0.1985 0.4254 0.5689 0.7323	0.0019 0.0230 0.0663 0.322 0.2175 0.3255 0.4525 0.6000 0.7673	0.0043 0.0299 0.0776 0.1467 0.2373 0.34894 0.4804 0.4804 0.6319	0.0377 0.0897 0.1631 0.2580 0.3736 0.5091 0.6645 0.8396	0.0464 0.1027 0.1804 0.2795 0.3991 0.5386 0.6980 0.8769			Width:	0.0832 0.3361 0.9547 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	0.1290 0.6079 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	0.1738 0.8354 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	0.2192 0.9071 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	0.268 0.928 1.000 1.000 1.000 1.000 1.000 1.000
e 0.5	0.9725 10_3 0.0005 0.0170 0.0559 0.1165 0.1995 0.3018 0.4254 0.5689 0.5689 0.4254 0.5689 0.9149	0.0019 0.0230 0.0663 0.1312 0.2175 0.3250 0.4525 0.6003 0.7673 0.7673	0.0043 0.0299 0.0776 0.2373 0.3469 0.4804 0.6319 0.8031 0.9785	0.0377 0.0897 0.1631 0.2580 0.3736 0.5091 0.6645 0.8396 0.9946	0.0464 0.1027 0.1804 0.2795 0.3991 0.5386 0.6980 0.8769 1.0000				0.0832 0.3361 0.9547 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	0.1290 0.6079 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	0.1738 0.8354 1.0000 1.0000 1.0000 1.0000 1.0000	0.2192 0.9071 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	0.268 0.928 1.000 1.000 1.000 1.000 1.000 1.000
pe 0.:	0.9725 0.0005 0.0170 0.0155 0.1185 0.4254 0.5689 0.7323 0.9149 0.0376 0.2280	0.0019 0.0230 0.0663 0.1312 0.2175 0.6000 0.4525 0.6000 0.7673 0.9516 0.0757	0.0043 0.0299 0.076 0.1467 0.2373 0.4804 0.6331 0.8031 0.8031 0.9785 0.1127 0.3033	0.0377 0.0897 0.1631 0.2580 0.3736 0.5091 0.6645 0.8396 0.9946 0.1518 0.3414	0.0464 0.1027 0.1804 0.2795 0.3991 0.5386 0.6980 0.8769 1.0000 0.1901 0.3798			Width: Shape 1.0 Area:	0.0832 0.3361 0.9547 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	0.1290 0.6079 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	0.1738 0.8354 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	0.2192 0.9071 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	0.268 0.928 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000
ape 0.:	0.9725 0.0005 0.0170 0.1165 0.1985 0.4254 0.5689 0.7323 0.9149 0.0376 0.2280 0.4180 0.6053	0.0019 0.0230 0.0663 0.1312 0.2175 0.3250 0.4525 0.4525 0.9525 0.9525 0.9525 0.9557 0.9552 0.9557 0.4559	0.0043 0.0299 0.076 0.1467 0.2373 0.4804 0.6319 0.8031 0.9782 0.1127 0.3033 0.4937 0.6814	0.0377 0.0897 0.1631 0.2580 0.3736 0.5091 0.6645 0.8396 0.9946 0.1518 0.3414 0.3414 0.5313 0.7183	0.0464 0.1027 0.1804 0.2795 0.3991 0.5386 0.6980 0.8769 1.0000 0.1901 0.3798 0.5689 0.7556			Shape 1.0	0.0832 0.3361 0.9547 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	0.1290 0.6079 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	0.1738 0.8354 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	0.2192 0.9071 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	0.268 0.928 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 0.017
ee 0.5	0.9725 0.0005 0.0170 0.0559 0.1165 0.1985 0.4254 0.5699 0.7323 0.9149 0.0376 0.2280 0.4180 0.2280 0.4180 0.6053 0.7928 0.9819	0.0019 0.0230 0.0663 0.1312 0.2175 0.3250 0.4525 0.4525 0.4525 0.4559 0.4559 0.6437 0.8559 0.6437	0.0043 0.0299 0.076 0.1467 0.2373 0.4804 0.6804 0.68031 0.9021 0.3033 0.4937 0.6811 0.8051 1.0553	0.0377 0.0897 0.1631 0.2580 0.3736 0.5091 0.6645 0.8396 0.9946 0.1518 0.3414 0.5313 0.7183 0.9042 1.0978	0.0464 0.1027 0.1804 0.2795 0.3991 0.5386 0.6980 0.8769 1.0000 0.1901 0.3798 0.5689 0.7556 0.9429 1.1362			Shape 1.0	0.0832 0.3361 0.9547 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 0.0006 0.0246 0.0246 0.0687 0.1257	0.1290 0.6079 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 0.0025 0.0324 0.0791 0.1388	0.1738 0.8354 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 0.00059 0.0407 0.0900 0.1524	0.2192 0.9071 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 0.0111 0.0495 0.1014 0.1667	0.2684 0.9281 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 0.0177 0.055 0.1133 0.1815
e 0.5	0.9725 0.0005 0.0170 0.0559 0.1165 0.1985 0.3018 0.4254 0.5699 0.7323 0.9149 0.0376 0.2280 0.4180 0.603 0.7928 0.9819 1.1744 1.3639	0.0019 0.0230 0.0663 0.3250 0.4525 0.4525 0.4525 0.6000 0.7673 0.9512 0.2657 0.4557 0.4637 0.6437 0.8457 0.8457 0.8457 0.8457 0.8457 0.8457 0.8457 0.8457 0.8457 0.8457 0.8457 0.8457 0.9457 0.8457 0.8457 0.8457 0.8457 0.94570 0.94570 0.9457000000000000000000000000000000000000	0.0043 0.0299 0.0776 0.2373 0.4804 0.4804 0.4804 0.4804 0.4803 0.4831 0.9782 0.3033 0.4937 0.6811 0.8611 0.8651 1.2505	0.0377 0.0897 0.1631 0.2580 0.3736 0.5091 0.6645 0.8396 0.9946 0.1518 0.3414 0.5313 0.7183 0.9042 1.0978 1.2884 1.4767	0.0464 0.1027 0.1804 0.2795 0.3991 0.5386 0.6980 0.8769 0.0000 0.1901 0.3798 0.5689 0.7556 0.9429 1.1362 1.3262 1.5142			Shape 1.0	0.0832 0.3361 0.9547 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 0.0246 0.0687 0.1257 0.1973 0.2893	0.1290 0.6079 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 0.0025 0.0324 0.0791 0.1388 0.2142 0.3100	0.1738 0.8354 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 0.0059 0.0407 0.0900 0.1524 0.2318 0.3313	0.2192 0.9071 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 0.0111 0.0495 0.1014 0.1667 0.2503 0.3532	0.268 0.928 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.00000 1.00000 1.00000000
De 0.5	0.9725 310_3 0.0005 0.0170 0.0559 0.10559 0.10559 0.3018 0.4254 0.5689 0.7323 0.9149 0.0376 0.2280 0.4180 0.6063 0.7928 0.9819 1.1744	0.0019 0.020 0.0663 0.1312 0.4525 0.6000 0.7673 0.9516 0.9516 0.4525 0.4525 0.4525 0.4525 0.4525 0.4537 0.4537 0.8300 0.8300 0.8300	0.0043 0.0299 0.2776 0.1467 0.2373 0.3489 0.6319 0.9785 0.1127 0.3978 0.9785 0.1127 0.3937 0.4804 0.4937 0.4937 0.4937 0.4937 0.8611 0.8611 0.8651 1.0553 1.2505	0.0377 0.1631 0.2580 0.3736 0.5091 0.6645 0.8396 0.9946 0.1518 0.3414 0.5313 0.7183 0.9042 1.0978 1.2884	0.0464 0.1027 0.1807 0.2795 0.3991 0.5386 0.6980 0.8769 1.0000 0.1901 0.3798 0.5689 0.7556 0.9429 1.362 1.3262			Shape 1.0	0.0832 0.3361 0.9547 1.0000 1.0000 1.0000 1.0000 1.0000 0.0006 0.0246 0.0246 0.02893 0.3991 0.5241	0.1290 0.6079 1.00000 1.00000 1.00000000	0.1738 0.8354 1.00000 1.00000 1.00000000	0.2192 0.9071 1.00000 1.00000 1.00000000	0.268 0.928 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 0.0174 0.058 0.113 0.181 0.269 0.375 0.375 0.4970 0.638
ad: ape 0.1	0.9725 0.0005 0.0170 0.0559 0.1165 0.3018 0.4254 0.5689 0.7323 0.9149 0.0376 0.2280 0.4180 0.6093 0.7928 0.9419 1.7455 0.0248	0.0019 0.0230 0.0663 0.1312 0.2175 0.4525 0.4525 0.4559 0.4559 0.4559 0.4559 0.4559 0.4559 0.4559 0.4559 0.4559 0.4559 0.4559 0.4559 0.4559 0.4559 0.4504 1.5679 0.0496	0.0043 0.0299 0.0776 0.1467 0.23739 0.4804 0.4804 0.4804 0.9785 0.1127 0.3033 0.9785 0.1127 0.6811 0.8611 1.0593 1.2505 1.4392 1.4392 1.4392 0.254	0.0377 0.1631 0.2500 0.37360 0.37360 0.5091 0.6645 0.8396 0.9946 0.1518 0.3414 0.5313 0.9042 1.0578 1.2874 1.4767 1.6662 1.1446 0.0976	0.0464 0.1027 0.1804 0.2795 0.3991 0.5386 0.6890 0.8769 1.0000 0.1901 0.3798 0.5890 0.7556 0.9429 1.3262 1.3262 1.3262 1.5142 1.7069 1.0000 0.1208			Shape 1.0 Area:	0.0832 0.3361 0.9547 1.0000 1.0000 1.0000 1.0000 1.0000 3.0000 0.0006 0.0246 0.0687 0.1257 0.1973 0.2893	0.1290 0.6079 1.0000 0.0324 0.1388 0.2142 0.14229	0.1738 0.8354 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 0.0407 0.0900 0.1524 0.2318 0.3313 0.4473	0.2192 0.9071 1.00000 1.00000000	0.268 0.928 1.00000 1.00000 1.00000000
ape 0.5	0.9725 0.0005 0.0170 0.0559 0.1165 0.1985 0.3018 0.4254 0.5699 0.7323 0.9149 0.0376 0.2280 0.4180 0.4180 0.4180 0.4180 0.4180 0.4180 0.4180 0.4180 0.4185 0.9819 1.1745 0.0248 0.1440 0.2574	0.0019 0.0203 0.1312 0.2175 0.3250 0.4525 0.4525 0.4525 0.4525 0.4525 0.4525 0.4557 0.4559 0.4559 0.4559 0.4559 0.4559 0.4559 0.4509 0.1207 1.2125 0.207 1.2125 0.207 1.2125 0.207 0.1579	0.0043 0.0299 0.0776 0.3489 0.4804 0.6319 0.9785 0.1127 0.3033 0.9785 0.4937 0.6811 1.0593 1.2505 0.8611 1.0593 1.2599 0.0744 0.3018	0.0377 0.1631 0.2580 0.37091 0.6645 0.5091 0.6645 0.8946 0.9946 0.3946 0.3946 0.3946 0.3946 0.3946 0.3944 1.4767 1.6682 1.1446 0.0976 0.3241 0.3241	0.0464 0.1027 0.1804 0.2795 0.3991 0.5386 0.6990 0.8769 1.0000 0.1901 0.3798 0.5569 0.7556 0.9429 1.3262 1.3262 1.3242 1.3242 1.3242 1.3242 0.0000 0.1208 0.2352 0.3662			Shape 1.0	0.0832 0.3361 0.000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 30_2 0.0066 0.0246 0.0687 0.1257 0.1257 0.1257 0.2893 0.2893 0.2893 0.2893 0.2893 0.3241 0.6655 0.6421	0.1290 0.6079 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 0.0025 0.0324 0.0791 0.1388 0.2142 0.2142 0.3100 0.4229 0.3100 0.4229 0.5510 0.7019 0.5797 0.784	0.1738 0.8354 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 0.0059 0.0407 0.0900 0.1524 0.3313 0.5787 0.7354 0.5315 0.5787	0.2192 0.9071 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 0.0111 0.4055 0.1014 0.4667 0.2503 0.4723 0.4752 0.4773 0.7699 0.9586 0.1600	0.268 0.928 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000000
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rad:	0.1905 0.3094 0.4284 0.5475 0.6666 0.7857 0.9047	0.2141 0.3332 0.4523 0.5713 0.6904 0.8095 0.9286	0.2379 0.3570 0.4761 0.5951 0.7142 0.8333 0.9524	0.2617 0.3808 0.4999 0.6190 0.7380 0.8571 0.9762	0.2855 0.4046 0.5237 0.6428 0.7618 0.8809 1.0000	We Dr Ro Va Ma Nu	et Time St ry Time St outing Tim ariable Ti aximum Tri umber of T	ep ep me Step als 'hreads	00:05 00:05 1.00 YES 20	:00 :00 sec		
nape 323 rea:	0.0097 0.0625 0.1228	0.0196 0.0740 0.1357	0.0299 0.0857 0.1490	0.0405 0.0978 0.1625	0.0513 0.1101 0.1764	Su St En An Re	urcharge M tarting Da nding Date ntecedent eport Time	lethod te Dry Days . Step	EXTRA 07/23 07/24 0.0 00:05	N /2009 00:03 /2009 00:03		
	0.2320 0.3153 0.3818 0.7696 0.8012 1.0000 1.0000 1.0000 1.0000 1.0000	0.2558 0.3286 0.3951 0.7759 0.8075 1.0000 1.0000 1.0000 1.0000 1.0000	0.2754 0.3419 0.4084 0.7822 0.8138 1.0000 1.0000 1.0000 1.0000 1.0000	0.2887 0.3552 0.7054 0.7886 0.8201 1.0000 1.0000 1.0000 1.0000 1.0000	0,3020 0,3685 0,7522 0,7549 0,8274 1,0000 1,0000 1,0000 1,0000	F1 Pr In	low Units rocess Mod Rainfall/ RDII Snowmelt Groundwat Flow Rout Ponding A Water Qua nfiltratio	Rels: Runoff er llowed lity n Method .	YES NO NO NO YES YES			
.dth:	0.8013 1.0233 1.2230 1.4035 1.5674	0.8477 1.0649 1.2605 1.4375 1.5984	0.8930 1.1057 1.2973 1.4709 1.6289	0.9374 1.1456 1.3334 1.5037 1.6588	0.9808 1.1847 1.3688 1.5359 1.0000	** ** An	ot just on ********** nalysis Op	**************************************	rom each re *********	porting tir	e step. **********	***
								-			-	
	0.1024 0.2082 0.3390 0.3929 0.4468 0.5017 0.9429	0.1194 0.2276 0.3498 0.4037 0.4575 0.5128 0.8933	0.1520 0.2610 0.3606 0.4144 0.4684 0.5273 0.8437	0.1734 0.3080 0.3713 0.4252 0.4795 0.5728 0.7940	0.1922 0.3282 0.3821 0.4360 0.4906 0.9926 0.7444	Hr	rad:	0.8957 0.0599 0.3031 0.4956 0.4810 0.7189	0.9218 0.1132 0.3448 0.5303 0.5308 0.7633	0.9478 0.1636 0.3846 0.5641 0.5795 0.8069	0.9739 0.2129 0.4229 0.4010 0.6270 0.8496	1.0000 0.2593 0.4598 0.4344 0.6734 0.8908
idth:	1.4680 1.0362 1.1479 1.1494 1.0842	1.5160 1.0707 1.1552 1.1407 1.0654	1.5558 1.0984 1.1587 1.1297 1.0450	1.5322 1.1200 1.1586 1.1165 1.0232	0.9940 1.1364 1.1554 1.1013 1.0000			0.1647 0.2672 0.3741 0.5045 0.6349 0.7653	0.1849 0.2881 0.4001 0.5305 0.6609 0.7914	0.2052 0.3093 0.4262 0.5566 0.6870 0.8174	0.2257 0.3306 0.4523 0.5827 0.7131 0.8435	0.2463 0.3521 0.4784 0.6088 0.7392 0.8696
ad:	0.0375 0.3831 0.6223 0.9393 1.2166	0.1240 0.4393 0.6900 0.9973 1.2688	0.1851 0.4740 0.7553 1.0539 1.3201	0.2523 0.4912 0.8185 1.1093 1.3700	0.3182 0.5519 0.8798 1.1635 1.4193		hape 2961 rea:	0.0057 0.0422 0.0876	0.0121 0.0506 0.0978	0.0191 0.0593 0.1082	0.0264 0.0684 0.1257	0.0341 0.0778 0.1448
	0.0401 0.1075 0.1960 0.2975 0.4121 0.5669 0.7649 0.9028 0.9808	0.0506 0.1242 0.2153 0.3193 0.4366 0.6113 0.7973 0.9232 0.9892	0.0624 0.1414 0.2350 0.3417 0.4616 0.6533 0.8273 0.9412 0.9952	0.0759 0.1591 0.2553 0.3646 0.4882 0.6929 0.8548 0.9568 0.9568	0.0914 0.1773 0.2761 0.5801 0.5202 0.7301 0.8800 0.9700 1.0000			0.2064 0.3523 0.5431 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	0.2344 0.3833 0.7533 1.0000 1.0000 1.0000 1.0000 1.0000	0.2623 0.4129 0.9431 1.0000 1.0000 1.0000 1.0000 0.8000	0.2904 0.4424 1.0000 1.0000 1.0000 1.0000 1.0000 0.4000	0.3214 0.4718 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 0.0000
hape 117 rea:	0.8703 0.9292 0_1 0.0018	0.8821 0.9410 0.0072	0.8939 0.9589 0.0137	0.9057 0.9794 0.0215	0.9174 1.0000	Wi	idth:	1.0065 1.1747 1.3180 1.4415	1.0424 1.2052 1.3441 1.4642 0.0679	1.0772 1.2347 1.3695 1.3515 0.0983	1.1108 1.2633 1.3942 1.1540 0.1370	1.1433 1.2911 1.4182 1.0000 0.1758
	0.2801 0.3651 0.4488 0.5374 0.6242 0.7092 0.7943	0.2978 0.3811 0.4666 0.5552 0.6412 0.7262 0.8113	0.3155 0.3971 0.4843 0.5729 0.6582 0.7432 0.8281	0.3330 0.4134 0.5020 0.5901 0.6752 0.7603 0.8427	0.3490 0.4311 0.5197 0.6071 0.6071 0.6922 0.7773 0.8574	Hr	rad:	0.0316 0.1901 0.3530 0.4832 0.5636 0.8061	0.0626 0.2251 0.3837 0.4225 0.6161 0.8492	0.0953 0.2588 0.4152 0.4104 0.6665 0.8907	0.1241 0.2916 0.4465 0.4516 0.7149 0.9307	0.1548 0.3223 0.4776 0.5088 0.7614 0.9692
idth:	0.7195 0.9031 1.0834 1.2612 1.4356 1.6213 1.8279 0.1283	0.7569 0.9390 1.1193 1.2964 1.4702 1.6633 1.8683 0.1844	0.7939 0.9747 1.1550 1.3313 1.5050 1.7049 1.8978 0.2182	0.8306 1.0109 1.1906 1.3662 1.5431 1.7462 1.9230 0.2395	0.8670 1.0473 1.2260 1.4010 1.5809 1.7871 1.0000 0.2610			0.0169 0.0551 0.1144 0.2367 0.3742 0.5117 0.6493 0.7868 0.9244	0.0230 0.0652 0.1311 0.2642 0.4017 0.5393 0.6768 0.8143 0.9519	0.0298 0.0762 0.1544 0.2917 0.4292 0.5668 0.7043 0.8418 0.9780	0.0374 0.0879 0.1817 0.3192 0.4567 0.5943 0.7318 0.8693 0.9945	0.0459 0.1005 0.2092 0.3467 0.4842 0.6218 0.7593 0.8968 1.0000
	0.0451 0.2899 0.5176	0.0901 0.3377 0.5606	0.1398 0.3838 0.6026	0.1923 0.4285 0.6435	0.2412 0.4737 0.6817		hape 1170_ rea:	0.0005	0.0018	0.0041	0.0074	0.0117

Highest Continuity Errors Node BASINI (7.88%) Node CASI (4.57%) Node (J2 (-1.22%) Time-Step Critical Elements Link C73 (4.77%) Link C73 (4.77%) Link C28 (1.37%) Highest Flew Instability Indexes Link C27 (46) Link C28 (26) Link C28 (26) Link C21 (25) Tommer Step Summary Time Step Summary Subcatchment Runoff Summary Time Step Summary Time Step Summary Subcatchment Runoff Summary	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
Maximum Time Step : 1.00 sec Percent in Steady State : 0.00 Average Iterations per Step : 4.74 Percent Not Converging : 8.36 Time Step Frequencies : 1.000 - 0.871 sec : 92.95 % 0.871 - 0.758 sec : 2.61 % 0.758 - 0.660 sec : 0.94 % 0.660 - 0.574 sec : 0.70 %	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
Subcatchment Runoff Summary	BLDG-K 71.68 0.00 0.00 70.31 0.00 70.32 0.17 0.12 0.981 D 71.68 0.00 0.00 38.21 19.08
Great-Lawn 2 71.68 0.00 0.00 42.23 10.53 19.65 23.65 0.04 0.02 0.414 Great-Lawn 3 71.68 0.00 0.00 47.25 6.32 Great-Lawn 4 71.68 0.00 0.00 43.48 9.13 8.38 28.38 0.05 0.02 0.396 0.00 38.28 16.15 Great-Lawn 5 71.68 0.00 0.00 41.45 12.64 0.36 30.36 0.02 0.424 0.974 69.49 133 69.82 0.34 0.24 0.974 69.49 NSTANDS 71.68 0.00 0.00 0.43 69.49 NSTANDS 71.68 0.00 0.00 7.48 58.50 0PGG_1 71.68 0.00 0.00 7.48 58.50 0PGG_2 71.68 0.00 0.00 7.03 59.20 0PGG_2 71.68 0.00 0.00 7.03 59.20 0PGG_2 71.68 0.00 0.00 7.3 59.20 <th>J40 JUNCTION 0.83 1.64 64.49 0 06:32 1.63 J41 JUNCTION 1.03 2.22 64.91 0 06:06 1.91 J48 JUNCTION 0.49 0.65 64.47 0 06:15 0.51 J50 JUNCTION 0.49 0.65 64.47 0 01:21 0.13 J51 JUNCTION 0.01 0.13 65:16 0 01:39 0.28 J52 JUNCTION 0.01 0.17 65:48 0 01:10 0.14 J53 JUNCTION 0.01 0.17 65:48 0 01:10 0.14 J54 JUNCTION 0.00 0.09 65:30 0 01:10 0.18 J55 JUNCTION 0.01 0.29 65:44 0 0.10 0.03 J56 JUNCTION 0.00 0.05 65:53 0 0.110 0.18 J57 JUNCTION 0.00</th>	J40 JUNCTION 0.83 1.64 64.49 0 06:32 1.63 J41 JUNCTION 1.03 2.22 64.91 0 06:06 1.91 J48 JUNCTION 0.49 0.65 64.47 0 06:15 0.51 J50 JUNCTION 0.49 0.65 64.47 0 01:21 0.13 J51 JUNCTION 0.01 0.13 65:16 0 01:39 0.28 J52 JUNCTION 0.01 0.17 65:48 0 01:10 0.14 J53 JUNCTION 0.01 0.17 65:48 0 01:10 0.14 J54 JUNCTION 0.00 0.09 65:30 0 01:10 0.18 J55 JUNCTION 0.01 0.29 65:44 0 0.10 0.03 J56 JUNCTION 0.00 0.05 65:53 0 0.110 0.18 J57 JUNCTION 0.00
Average Maximum Maximum Time of Max Reported Depth Depth HGL Occurrence Max Depth Node Type Meters Meters Meters Meters CBA1 JUNCTION 0.09 0.80 64.87 0 01:12 0.76 CBMHA2 JUNCTION 0.52 1.29 64.47 0 06:34 1.29 CBMHA2 JUNCTION 0.37 1.46 65.20 0 01:10 1.66 CBHHU JUNCTION 0.27 1.66 65.22 0 01:10 1.66 J14 JUNCTION 0.24 1.15 64.57 0 01:10 1.66 J14 JUNCTION 0.24 1.15 64.52 0 06:43 1.92 J26 JUNCTION 1.35 2.27 64.52 0 06:56 2.12 J27 JUNCTION 0.51 1.72 64.48 0 06:28 1.72	STM118 JUNCTION 0.12 0.54 64.50 0 01:12 0.51 STM119 JUNCTION 0.11 1.75 65.66 0 01:12 1.67 STM120 JUNCTION 0.06 1.60 65.66 0 01:12 1.57 STM121 JUNCTION 0.38 1.17 64.49 0 06:11 1.17 STM203 JUNCTION 0.52 1.30 64.49 0 06:25 0.61 STM203 JUNCTION 0.52 1.30 64.49 0 06:28 1.23 STM204 JUNCTION 0.43 1.20 64.49 0 06:11 1.28 STM205 JUNCTION 0.43 1.20 64.49 0 06:12 1.23 STM206 JUNCTION 0.33 1.07 64.47 0 06:28 1.23 STM208 JUNCTION 0.33 1.07 64.47 0 06:28 1.03 STM208 JUNCTION 0.25 0.91 64.47 0 06:44 1.25

	JUNCTION	0.24	0.91	64.48	0 07:07	0.90	CBMH.	0	JUNCTION	0.000	0.102	0 01:11	0
	JUNCTION	0.36	1.12	64.47	0 06:34	1.12	0.256	-0.369					0
	JUNCTION JUNCTION	0.29	1.06	64.47	0 06:38 0 06:23	1.05	CBMH 0.365	-0.009	JUNCTION	0.000	0.147	0 01:07	
	JUNCTION JUNCTION	0.57	1.36	64.48	0 06:32 0 06:32	1.35 1.38	J1 0.122 J14	0.007	JUNCTION	0.000	0.062	0 01:06	0.174
2	JUNCTION JUNCTION	0.65	1.44 1.43	64.49	0 06:47 0 06:25	1.44 1.41	0.507 J19	-0.084	JUNCTION	0.000	0.037	0 01:09	0.1/4
1 2	JUNCTION JUNCTION	0.38	1.23 0.83		0 01:10 0 01:10	1.23 0.83	0.056 J23	-0.000	JUNCTION	0.131	0.570	0 08:00	0.176
	JUNCTION JUNCTION	0.00	0.13		0 01:10 0 06:23	0.13 0.46	523 6.34 J26	0.576	JUNCTION				0.1/6
	JUNCTION JUNCTION	0.01	0.24	66.22	0 01:15	0.24 0.27	6.05	0.135		0.000	0.581	0 08:00	
	JUNCTION	0.01	0.32	64.96	0 01:10 0 06:47	0.32	J27 6.04	0.082	JUNCTION	0.000	0.581	0 08:00	0
	JUNCTION	0.01	0.34	65.05	0 01:10	0.34	J32 8.57	-1.302	JUNCTION	0.000	1.279	0 01:10	0
	JUNCTION	0.17	0.72	64.85	0 06:32 0 01:15	0.71 0.14	J37 0.179	0.219	JUNCTION	0.102	0.102	0 01:10	0.176
	JUNCTION JUNCTION	0.18	0.78		0 06:35 0 01:20	0.78 0.13	J40 9.86	4.789	JUNCTION	0.000	1.698	0 01:15	0
	JUNCTION OUTFALL	0.50	1.28 2.98		0 06:23 0 03:00	1.28 2.98	J41 6.18	0.601	JUNCTION	0.000	0.570	0 08:00	0
al 11	OUTFALL STORAGE	0.00	0.00 1.65		0 00:00 0 06:29	0.00 1.65	J48 0.32	0.276	JUNCTION	0.053	0.077	0 01:24	0.125
12 13	STORAGE STORAGE	0.73	1.53		0 07:10 0 06:34	1.52 1.61	J49 0.35	0.449	JUNCTION	0.000	0.087	0 04:42	0
DG-A DG-B	STORAGE STORAGE	0.01	0.07	100.07	0 01:52 0 01:54	0.07 0.08	J50 0.282	-0.486	JUNCTION	0.081	0.081	0 01:20	0.282
DG-C DG-D	STORAGE	0.01	0.07	100.07	0 01:52	0.07	J51 0.196	0.765	JUNCTION	0.000	0.047	0 01:21	0
DG-G	STORAGE STORAGE	0.02	0.09	100.09	0 02:11	0.09	J52 1.37	0.000	JUNCTION	0.776	0.986	0 01:10	1.1
DG-H DG-I	STORAGE STORAGE	0.02	0.08	100.07	0 01:54 0 01:50	0.08	J53 1.16	0.002	JUNCTION	0.000	0.849	0 01:10	0
DG-J1 DG-J2	STORAGE STORAGE	0.01	0.11 0.11	100.11	0 01:30 0 01:31	0.11 0.11	J54 0.935	0.000	JUNCTION	0.000	0.745	0 01:11	0
DG-K	STORAGE	0.03	0.10	100.10	0 02:20	0.10	J55 0.877	-0.002	JUNCTION	0.000	0.702	0 01:11	0
* * * * * * * * * * * * * * * * *							J56 0.946	0.003	JUNCTION	0.066	0.710	0 01:10	0.0887
Inflow Summary							J57 0.545	0.001	JUNCTION	0.000	0.358	0 01:10	0
							J58 0.639	0.001	JUNCTION	0.000	0.451	0 01:10	0
							J59 0.672	-0.005	JUNCTION	0.472	0.472	0 01:10	0.672
Flow		Maximum Lateral		Time of M:	Lateral Inflow		J60 0	0.000 ltr	JUNCTION	0.000	0.000	0 00:00	0
w Balance				Time of Max			J61 0.224	0.243	JUNCTION	0.113	0.135	0 06:34	0.159
e Error		Inflow	Inflow	Occurrence			J62 0	0.000 ltr	JUNCTION	0.000	0.000	0 00:00	0
le Percent	Type	CMS	CMS	days hr:min	10^6 ltr	10^6	J63 0.358	0.000 101	JUNCTION	0.000	0.115	0 01:20	0
							J64	-0.005	JUNCTION	0.082	0.082	0 01:20	0.308
													0
L 1.439	JUNCTION	0.000	0.112	0 01:10		0	0.308 J65 0	0.000 ltr	JUNCTION	0.000	0.000	0 00:00	
1						0	J65	0.000 ltr	JUNCTION	0.000	0.000	0 00:00	
1 1.439						0	J65	0.000 ltr	JUNCTION	0.000	0.000	0 00:00	
1.439					0.0462	0	J65		JUNCTION	0.000	0.000	0 00:00	0.333
1 1.439 H210	JUNCTION	0.022	0.255	0 01:17	0.0462	0	0 J65	09 0.180					
1.439 ;210 2.000	JUNCTION	0.022	0.255	0 01:17	0.0462	0	5TM2	99 0.180 -0.014	JUNCTION	0.233	0.705	0 01:10	0.333
1.439 2210 : 0.000 0.000 -0.002	JUNCTION	0.022	0.255 0.087 0.113	0 01:17 0 01:10 0 01:10	0.0462 0.228 0	0	5TM2 0 1.38 5TM2 1.4 5TM2 1.4 5TM2 1.4 5TM2	99 0.180 -0.014 .2 0.246 .3	JUNCTION	0.233 0.000	0.705 0.561	0 01:10 0 01:10	0.333
1.439 210 0.000 0.000 -0.002 0.000 ltr	JUNCTION JUNCTION JUNCTION JUNCTION	0.022 0.000 0.113 0.000	0.255 0.087 0.113 0.113	0 01:17 0 01:10 0 01:10 0 01:10	0.0462 0.228 0 0	0	5TM2 0 3TM2 1.38 5TM2 1.4 5TM2 1.4 5TM2 0.0636 5TM3 5TM2 5TM3 5TM3 5TM3 5TM3 5TM3 5TM3 5TM3 5TM3	99 0.180 .1 -0.014 .2 0.246 .3 0.290	JUNCTION JUNCTION JUNCTION	0.233 0.000 0.000	0.705 0.561 0.560	0 01:10 0 01:10 0 01:08	0.333 0 0
1 1.439 H210 2 0.000 0.000 -0.002	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.022 0.000 0.113 0.000 0.000	0.255 0.087 0.113 0.113 0.000	0 01:17 0 01:10 0 01:10 0 01:10 0 01:10 0 00:00	0.0462 0.228 0 0 0	0	5TM2 0 1.38 5TM2 1.38 5TM2 1.4 5TM2 1.4 5TM2 0.0636	09 0.180 -0.014 .2 0.246 3 0.290 0.329	JUNCTION JUNCTION JUNCTION JUNCTION	0.233 0.000 0.000 0.000	0.705 0.561 0.560 0.022	0 01:10 0 01:10 0 01:08 0 01:18	0.333 0 0 0
1 1.439 H210 2 0.000 0.000 -0.002 0.000 1tr 0.000 1tr -0.011	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.022 0.000 0.113 0.000 0.000 0.000	0.255 0.087 0.113 0.113 0.000 0.000	0 01:17 0 01:10 0 01:10 0 01:10 0 01:10 0 00:00 0 00:00	0.0462 0.228 0 0 0.185	0	5TM2 0 3TM2 1.38 3TM2 1.4 3TM2 1.4 3TM2 1.4 0.636 3TMA 0.103 3TMA 0.103 3TMA	09 0.180 -0.014 2 0.246 3 0.290 0.329 0.468	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.233 0.000 0.000 0.000 0.000 0.000	0.705 0.561 0.022 0.078	0 01:10 0 01:10 0 01:08 0 01:18 0 01:09	0.333 0 0 0 0
1 1.439 H210 2 0.000 0.000 -0.002 0.000 ltr 0.000 ltr -0.011 0.005	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.022 0.000 0.113 0.000 0.000 0.000 0.133	0.255 0.087 0.113 0.000 0.000 0.465	0 01:17 0 01:10 0 01:10 0 01:10 0 00:00 0 00:00 0 01:10	0.0462 0 0.228 0 0 0.185 0	0	5TM2 0 5TM2 1.38 5TM2 1.4 5TM2 1.4 5TM2 0.636 5TM3 0.103 5TM4 0.103 5TM4 0.158 5TM4 5TM2 5TM5 5TM5 5TM5 5TM5 5TM5 5TM5 5TM5	09 0.180 1 -0.014 2 0.246 3 0.290 0.329 0.468 -0.066	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.233 0.000 0.000 0.000 0.000 0.000 0.000	0.705 0.561 0.022 0.078 0.097	0 01:10 0 01:10 0 01:08 0 01:18 0 01:09 0 01:12	0.333 0 0 0 0 0 0
1.439 2. 0.000 0.000 -0.002 0.000 ltr 0.000 ltr -0.011 0.005 -0.005 0.02	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.022 0.000 0.113 0.000 0.000 0.000 0.133 0.000	0.255 0.087 0.113 0.000 0.000 0.465 0.459	0 01:17 0 01:10 0 01:10 0 01:10 0 01:10 0 00:00 0 00:00 0 01:10 0 01:10	0.0462 0 0.228 0 0 0.185 0 0.0569	0	5TM2 0 5TM2 1.38 5TM2 1.4 5TM2 1.4 5TM2 0.635 5TM3 0.103 5TM4 0.158 5TM4 0.158 5TM4 0.335 5TM4 0.335 5TM4 5TM2 5TM2 5TM2 5TM2 5TM2 5TM2 5TM2 5TM2	09 0.180 1 -0.014 2 0.246 3 0.290 0.329 0.468 -0.066 -0.060	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.233 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.705 0.561 0.522 0.078 0.097 0.113	0 01:10 0 01:10 0 01:08 0 01:18 0 01:09 0 01:12 0 01:08	0.333 0 0 0 0 0 0 0
1 1.439 H210 2 0.000 0.000 -0.002 0.000 ltr 0.000 ltr -0.011 0.005 9 -0.005 0.558 104	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.022 0.022 0.113 0.000 0.000 0.113 0.000 0.133 0.000 0.043	0.255 0.087 0.113 0.000 0.000 0.465 0.459 0.043	0 01:17 0 01:10 0 01:10 0 01:10 0 01:10 0 00:00 0 01:10 0 01:10 0 01:10	0.0462 0 0.228 0 0 0.185 0 0.0569 0	0	5TM2 0 5TM2 1.38 5TM2 1.4 5TM2 1.4 5TM2 0.0336 5TM8 0.103 5TM8 0.158 STM8 0.335 5TM8 0.335 5TM2 0.335 5 5TM2 0.335 5 5TM2 0.335 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	09 0.180 1 -0.014 2 0.246 3 0.290 0.329 0.468 -0.066 -0.609 -0.095	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.233 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.705 0.561 0.560 0.022 0.078 0.097 0.113 0.171	0 01:10 0 01:10 0 01:08 0 01:18 0 01:19 0 01:12 0 01:08 0 01:12	0.333 0 0 0 0 0 0 0 0 0 0
1.439 210 0.000 0.000 -0.002 0.000 ltr 0.000 ltr -0.011 0.005 0.588 04 0.529 05	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.022 0.022 0.113 0.000 0.000 0.133 0.000 0.133 0.000	0.255 0.087 0.113 0.000 0.000 0.465 0.459 0.043 0.580	0 01:17 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10	0.0462 0 0.228 0 0 0.185 0 0.0569 0 0.0559 0 0	0	5 TM2 0 1.18 5 TM2 1.38 5 TM2 1.4 1.4 2 0.0636 5 TM4 0.103 5 TM4 0.103 5 TM4 0.158 5 TM5 0.335 5 TM5 0.335 5 TM2 0.335 5 TM2 0.355 5 TM2 0.357 5 TM2 0 5 5 TM2 0 5 TM2 5 TM2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	09 0.180 -0.014 0.246 3 0.290 0.329 0.468 -0.066 -0.609 -0.095 0.077	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.233 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.705 0.561 0.560 0.022 0.078 0.097 0.113 0.171 0.154	0 01:10 0 01:10 0 01:08 0 01:18 0 01:19 0 01:12 0 01:12 0 01:12 0 01:14	0.333 0 0 0 0 0 0 0 0 0 0 0 0 0
1.439 210 0.000 0.000 -0.002 0.000 ltr 0.000 ltr -0.011 0.005 0.588 04 0.529 05 0.529 05 0.456 07	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.022 0.022 0.113 0.000 0.000 0.133 0.000 0.133 0.000 0.043 0.000	0.255 0.087 0.113 0.100 0.000 0.465 0.459 0.043 0.580 0.579	0 01:17 0 01:10 0 01:17 0 01:10 0 00:00 0 0	0.0462 0 0.228 0 0 0.185 0 0.0569 0 0.0559 0 0 0.0559	0	5 STM2 0 1.18 5 STM2 1.4 5 STM2 1.4 5 STM2 0.0636 5 STM2 0.103 5 STM2 0.158 5 STM5 0.158 5 STM5 0.335 5 STM5 0.335 5 STM5 0.335 5 STM5 5 STM5	09 0.180 1 -0.014 2 0.246 3 0.290 0.329 0.468 -0.066 -0.609 -0.095 0.077 -0.106	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.233 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.705 0.561 0.560 0.022 0.078 0.097 0.113 0.171 0.154 0.257	0 01:10 0 01:10 0 01:08 0 01:18 0 01:12 0 01:12 0 01:12 0 01:14 0 01:16	0.333 0 0 0 0 0 0 0 0 0 0 0 0 0 0
1 1.439 H210 2 0.000 0.000 -0.002 0.000 ltr 0.000 ltr -0.011 0.005 9 -0.005 10 0.588 104 0.529 105 0.456 0.179 108	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.022 0.022 0.113 0.000 0.000 0.000 0.133 0.000 0.043 0.000 0.000	0.255 0.087 0.113 0.100 0.000 0.465 0.459 0.043 0.580 0.579	0 01:17 0 01:10 0 01:17 0 01:10 0 00:00 0 0	0.0462 0 0.228 0 0 0.185 0 0.0569 0 0 0.0559 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0	5 STM2 0 1.18 5 STM2 1.38 5 STM2 1.4 1.4 2 0.0636 5 STM4 0.103 5 STM4 0.103 5 STM4 0.158 5 STM5 0.335 5 STM5 0.335 5 STM5 0.335 5 STM5 0.335 5 STM5 0.335 5 STM5 0.335 5 STM5 5 S	09 0.180 -0.014 0.246 3 0.290 0.329 0.468 -0.066 -0.609 -0.095 0.077 -0.106 0.357	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.233 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.705 0.561 0.560 0.022 0.078 0.097 0.113 0.171 0.154 0.257 0.207	0 01:10 0 01:10 0 01:08 0 01:18 0 01:12 0 01:12 0 01:12 0 01:14 0 01:16 0 01:17	0.333 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
1.439 210 0.000 0.000 -0.002 0.000 ltr 0.000 ltr 0.005 0.588 04 0.529 05 0.456 07 0.179 08 0.479 09	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.022 0.022 0.113 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.255 0.087 0.113 0.100 0.000 0.465 0.459 0.043 0.580 0.579 0.574 0.568	0 01:17 0 01:10 0 01:17 0 01:10 0 00:00 0 0	0.0462 0 0.228 0 0 0.185 0 0.0569 0 0 0.0559 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0	5 STM2 0 STM2 1.38 STM2 1.4 STM2 1.4 STM2 0.0636 STM3 0.103 STM4 0.266 STM4 0.335 STM4 0.335 STM4 0.335 STM4 0.335 STM4 0.335 STM4 0.335 STM4 0.335 STM4 0.335 STM4 0.335 STM4	09 0.180 -0.014 2 0.246 3 0.290 0.329 0.468 -0.069 -0.095 0.077 -0.106 0.357 0.913	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.233 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.028	0.705 0.561 0.560 0.022 0.078 0.113 0.171 0.154 0.257 0.207 0.287	0 01:10 0 01:10 0 01:08 0 01:18 0 01:12 0 01:12 0 01:12 0 01:12 0 01:14 0 01:16 0 01:17 0 01:18	0.333 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
1 1.439 H210 2 0.000 0.000 -0.002 0.000 1tr 0.000 1tr -0.011 0.005 9 -0.005 9 -0.005 9 -0.005 10 0.588 104 0.529 105 0.456 0.798 109 0.798	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.022 0.022 0.113 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.255 0.087 0.113 0.113 0.000 0.465 0.459 0.043 0.580 0.579 0.574 0.568 1.097	0 01:17 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 08:00 0 08:00 0 08:00 0 08:00 0 01:15	0.0462 0 0.228 0 0 0.185 0 0.0559 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0	5 STM2 0 STM2 1.38 STM2 1.4 STM2 1.4 STM2 0.0636 STM2 0.158 STM3 0.103 STM4 0.335 STM4 0.335 STM4 0.335 STM4 0.335 STM4 0.335 STM4 0.335 STM4 0.335 STM4 0.335 STM5	09 0.180 -0.014 2 0.246 3 0.290 0.329 0.468 -0.069 -0.095 0.077 -0.106 0.357 0.913 0.619	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.233 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.028 0.028 0.000	0.705 0.561 0.560 0.022 0.078 0.113 0.171 0.154 0.257 0.207 0.287 0.345	0 01:10 0 01:10 0 01:08 0 01:18 0 01:12 0 01:12 0 01:12 0 01:12 0 01:14 0 01:16 0 01:17 0 01:18 0 01:11	0.333 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
1 1.439 H210 2 0.000 0.000 -0.002 0.000 1tr 0.000 1tr 0.000 1tr -0.011 0.005 9 -0.005 9 -0.005 10 0.588 104 0.529 105 0.456 107 0.179 108 0.479 109 0.798 109 0.061 111A	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.022 0.022 0.113 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.255 0.087 0.113 0.113 0.000 0.465 0.459 0.043 0.580 0.579 0.574 0.568 1.097 0.883	0 01:17 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 08:00 0 08:00 0 08:00 0 08:00 0 08:00 0 01:15 0 01:11	0.0462 0 0.228 0 0 0.185 0 0.0559 0 0 0.0559 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0	5 STM2 0 STM2 1.38 STM2 1.4 STM2 1.4 STM2 0.0636 STM2 0.103 STM3 0.266 STM4 0.335 STM4 0.355 STM4 0.357 STM4 0.817 STM4 0.817 STM4 0.817 STM4 0.817 STM4 0.817 STM4 0.817 STM4 0.817 STM4 0.817 STM4 0.985 STM4 0.985 STM4 0.985 STM4 0.985 STM4 0.985 STM4 0.985 STM4 0.985 STM4 0.985 STM4 0.985 STM4 0.985 STM4 0.817	09 0.180 -0.014 2 0.246 3 0.290 0.329 0.468 -0.069 -0.095 0.077 -0.106 0.357 0.913 0.619 -0.033 N1	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.233 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.028 0.000 0.000 0.000	0.705 0.561 0.560 0.022 0.078 0.113 0.171 0.154 0.257 0.207 0.287 0.345 0.447	0 01:10 0 01:10 0 01:08 0 01:18 0 01:12 0 01:12 0 01:12 0 01:12 0 01:14 0 01:16 0 01:17 0 01:18 0 01:11 0 01:10	0.333 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
1.439 210 0.000 0.000 -0.002 0.000 ltr 0.000 ltr -0.011 0.005 0.588 04 0.529 05 0.456 07 0.179 05 0.456 07 0.179 08 0.479 09 0.798 10 0.0061 111 0.232	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.022 0.022 0.113 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.255 0.087 0.113 0.113 0.000 0.465 0.459 0.043 0.580 0.579 0.574 0.568 1.097 0.883 0.560	0 01:17 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 08:00 0 08:00 0 08:00 0 08:00 0 08:00 0 08:00 0 01:15 0 01:11 0 01:10	0.0462 0 0.228 0 0 0.185 0 0.0559 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		5 STM2 5 STM2 1.38 STM2 1.4 5 STM2 1.4 5 STM2 1.4 5 STM2 0.625 5 STM2 0.103 0.266 5 STM5 0.103 5 STM5 0.335 STM5 0.355 STM5 0.412 STM5 0.817 STM5 0.817 STM5 0.817 STM5 0.817 STM5 0.817 STM5 0.817 STM5 0.817 STM5 0.817 STM5 0.817 STM5 0.817 STM5 0.985 STM5	09 0.180 -0.014 2 0.246 3 0.290 0.329 0.468 -0.066 -0.609 -0.095 0.077 -0.106 0.357 0.913 0.619 -0.033 -0.131 -0.131	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.233 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.028 0.000 0.000 0.000 0.000	0.705 0.561 0.560 0.022 0.078 0.113 0.171 0.154 0.257 0.207 0.287 0.345 0.447 1.612	0 01:10 0 01:10 0 01:08 0 01:18 0 01:12 0 01:12 0 01:12 0 01:14 0 01:16 0 01:17 0 01:18 0 01:11 0 01:11 0 01:10 0 01:12	0.333 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
0.000 0.000 0.000 0.000 0.000 ltr 0.000 ltr 0.000 ltr 0.005 0.588 0.529 0.588 0.529 0.456 70 0.456 70 0.798 0.479 90 0.661 11 0.232 12 14 14 14 14 14 14 14 14 14 14	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.022 0.022 0.113 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.255 0.087 0.113 0.113 0.000 0.465 0.459 0.043 0.580 0.579 0.574 0.568 1.097 0.883 0.560 0.143	0 01:17 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 08:00 0 08:00 0 08:00 0 08:00 0 08:00 0 08:00 0 01:15 0 01:11 0 01:10	0.0462 0 0.228 0 0 0.185 0 0.0559 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0	5 STM2 0 STM2 1.38 STM2 1.4 STM2 1.4 STM2 0.625 STM4 0.103 STM4 0.103 STM4 0.103 STM4 0.335 STM5 0.355 STM5 0.335 STM5 0.335 STM5 STM5 STM5 0.335 STM5 S	09 0.180 -0.014 2 0.246 3 0.290 0.329 0.468 -0.066 -0.609 -0.095 0.077 -0.106 0.357 0.913 0.619 -0.033 -0.131 -0.131 -0.131 -0.131	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.233 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.028 0.000 0.028 0.000 0.000 0.000 0.000 0.000 0.000	0.705 0.561 0.560 0.022 0.078 0.113 0.171 0.154 0.257 0.207 0.287 0.287 0.345 0.447 1.612 0.559	0 01:10 0 01:10 0 01:08 0 01:18 0 01:12 0 01:12 0 01:12 0 01:12 0 01:14 0 01:14 0 01:16 0 01:17 0 01:18 0 01:11 0 01:10 0 01:12 0 01:12 0 01:12	0.333 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
0.000 0.000 0.000 0.000 -0.002 0.000 ltr 0.000 ltr 0.005 2 -0.005 2 -0.005 2 -0.005 2 0.058 4 0.529 5 0.456 7 0.179 8 0.479 9 0.798 0 0.661 1A 2 6.216 4 0.063	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.022 0.022 0.113 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.255 0.087 0.113 0.113 0.000 0.465 0.459 0.043 0.580 0.579 0.574 0.568 1.097 0.883 0.560 0.143 0.083	0 01:17 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 08:00 0 08:00 0 08:00 0 08:00 0 08:00 0 01:15 0 01:11 0 01:10 0 01:10	0.0462 0 0.228 0 0 0.185 0 0.0559 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		5 TM2 0 5 TM2 1.38 5 TM2 1.4 5 TM2 1.4 5 TM2 0.636 5 TM4 0.1636 5 TM4 0.158 0.158 5 TM4 0.158 5 TM4 0.177 5 TM4 0.177 5 TM4 0.177 5 TM4 0.172 5 T	09 0.180 1 -0.014 2 0.246 3 0.290 0.329 0.468 -0.066 -0.0095 0.077 -0.106 0.357 0.913 0.619 -0.033 -0.033 -0.031 0.131 0.137 0.000	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.233 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.028 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.300 0.300	0.705 0.561 0.560 0.022 0.078 0.113 0.171 0.154 0.257 0.207 0.287 0.287 0.287 0.345 0.447 1.612 0.559 0.032	0 01:10 0 01:10 0 01:08 0 01:18 0 01:18 0 01:12 0 01:12 0 01:12 0 01:12 0 01:14 0 01:14 0 01:16 0 01:17 0 01:18 0 01:11 0 01:11 0 01:12 0 01:10 8 0 01:10	0.333 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
0.000 0.000 0.000 0.000 0.000 0.000 10.005 0.000 10.005 0.005	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.022 0.022 0.113 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.255 0.087 0.113 0.113 0.000 0.465 0.459 0.043 0.580 0.579 0.574 0.568 1.097 0.883 0.560 0.143 0.083 0.496	0 01:17 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 08:00 0 08:00 0 08:00 0 08:00 0 08:00 0 01:15 0 01:11 0 01:10 0 01:10	0.0462 0 0.228 0 0 0.185 0 0 0.185 0 0 0.185 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		5 TM2 5 TM2 1.38 5 TM2 1.38 5 TM2 1.4 5 TM2 1.4 5 TM2 0.636 5 TM4 0.158 5 TM2 0.412 5 TM2 0.412 5 TM2 0.636 5 TM4 0.158 5 TM2 0.636 5 TM4 0.158 5 TM2 0.636 5 TM4 0.636 5 TM4 0.158 5 TM4 0.679 5 TM4 0.679 5 TM4 0.817 5 TM4 0.817 5 TM4 0.817 5 TM4 0.817 5 TM4 0.0365 5 TM4 0.035 5 TM4 0.035	09 0.180 -0.014 2 0.246 3 0.246 -0.066 -0.069 -0.095 0.077 -0.106 0.357 0.913 0.619 -0.033 -0.131 0.137 0.137 0.000 0.033	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.233 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.028 0.000 0.028 0.000 0.028 0.000 0.020 0.000 0.300 0.300 0.000 0.023	0.705 0.561 0.560 0.022 0.078 0.113 0.171 0.154 0.257 0.207 0.287 0.287 0.345 0.447 1.612 0.559 0.032 0.023	0 01:10 0 01:10 0 01:08 0 01:18 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:14 0 01:14 0 01:16 0 01:17 0 01:18 0 01:11 0 01:10 0 01:10	0.333 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
0.000 0.000 0.000 -0.002 0.000 ltr 0.000 ltr 0.001 ltr 0.005 2 -0.005 2 -0.005 2 0.529 5 0.529 5 0.456 7 0.456 7 0.456 7 0.179 8 0.479 9 0.798 0 0.061 1A 0.232 2 6.216 4 0.063 7 -0.043 8 -0.118	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.022 0.022 0.113 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.255 0.087 0.113 0.113 0.000 0.465 0.459 0.043 0.580 0.579 0.574 0.568 1.097 0.883 0.560 0.143 0.083 0.496 0.447	0 01:17 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 08:00 0 08:00 0 08:00 0 08:00 0 08:00 0 08:00 0 01:15 0 01:11 0 01:10 0 01:10 0 01:10	0.0462 0 0.228 0 0 0.185 0 0.0559 0 0 0.0559 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		5 TM2 0 5 TM2 1.38 5 TM2 1.4 5 TM2 1.4 5 TM2 0.636 5 TM4 0.158 0.178 0.679 0.679 0.0817 0.0817 0.082 0.036 0.172 0.036 0.	09 0.180 -0.014 2 0.246 3 0.246 -0.066 -0.069 -0.095 0.077 -0.106 0.357 0.913 0.619 -0.033 -0.131 0.137 0.137 0.000 0.033 -0.000	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.233 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.028 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.705 0.561 0.560 0.022 0.078 0.113 0.171 0.154 0.257 0.207 0.287 0.287 0.287 0.287 0.287 0.287 0.345 0.447 1.612 0.559 0.032 0.023 0.023	0 01:10 0 01:10 0 01:08 0 01:18 0 01:18 0 01:12 0 01:12 0 01:12 0 01:12 0 01:14 0 01:14 0 01:16 0 01:17 0 01:18 0 01:11 0 01:10 0 01:10 0 01:10	0.333 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
0.000 0.000 0.000 -0.002 0.000 ltr 0.000 ltr 0.001 ltr -0.011 0.005 0.005 0.005 0.005 0.058 0.456 0.059 0.588 0.456 0.529 0.588 0.456 0.529 0.588 0.456 0.79 0.059 0.59 0.59 0.59 0.529000000000000000000000	JUNCTION JUNCTION	0.022 0.022 0.113 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.001 0.000 0.001 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.000000	0.255 0.087 0.113 0.113 0.000 0.465 0.459 0.043 0.580 0.579 0.574 0.568 1.097 0.883 0.560 0.143 0.560 0.143 0.083 0.496 0.447 0.416 0.699	0 01:17 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 08:00 0 08:00 0 08:00 0 08:00 0 08:00 0 08:00 0 01:15 0 01:11 0 01:10 0 01:13 0 01:13 0 01:10	0.0462 0 0.228 0 0 0.185 0 0.0569 0 0 0.185 0 0 0.0593 0 0.0593 0.544 0 0.0593		5 TM2 0 5 TM2 1.38 5 TM2 1.4 5 TM2 1.4 5 TM2 1.4 5 TM2 1.4 5 TM2 0.636 5 TM4 0.158 5 TM4 0.679 5 TM4 0.817 5 TM4 0.0365 5 TM4 0.035 5 TM4 0.075 5 TM4 0.075	09 0.180 1 -0.014 2 0.246 3 0.246 0.329 0.468 -0.066 -0.009 0.0357 0.0131 0.131 0.137 0.131 0.137 0.000 0.000 0.0002	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.233 0.0000 0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.000000	0.705 0.561 0.560 0.022 0.078 0.113 0.171 0.154 0.257 0.207 0.287 0.287 0.247 1.612 0.559 0.032 0.023 0.023 0.054 0.054	0 01:10 0 01:10 0 01:08 0 01:18 0 01:18 0 01:12 0 01:12 0 01:12 0 01:12 0 01:14 0 01:16 0 01:17 0 01:18 0 01:11 0 01:10 0 01:10 0 01:10 0 01:10 0 01:15 0 01:15	0.333 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
1.439 210 . 0.000 0.000 -0.002 0.000 ltr 0.000 ltr 0.000 ltr 0.005 02 0.000 ltr 0.005 02 0.588 04 0.529 05 0.456 07 0.179 08 0.479 09 0.798 10 0.232 12 6.216 14 0.063 17 -0.043 18 -0.043 18 -0.118 19 0.828 20 0.119	JUNCTION JUNCTION	0.022 0.022 0.113 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.001 0.000 0.000 0.000	0.255 0.087 0.113 0.113 0.000 0.465 0.459 0.043 0.580 0.579 0.574 0.568 1.097 0.883 0.560 0.143 0.560 0.143 0.083 0.496 0.447 0.416 0.699 0.021	0 01:17 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 08:00 0 08:00 0 08:00 0 08:00 0 08:00 0 08:00 0 01:15 0 01:11 0 01:10 0 01:13 0 01:13 0 01:10 0 01:10	0.0462 0 0.228 0 0 0.185 0 0.0559 0 0 0.0559 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		5 TM2 0 5 TM2 1.38 5 TM2 1.4 5 TM2 1.4 5 TM2 1.4 5 TM2 1.4 5 TM2 0.636 5 TM4 0.158 5 TM4 0.158 5 TM4 0.158 5 TM4 0.158 5 TM4 0.636 5 TM4 0.158 5 TM4 0.636 5 TM4 0.158 5 TM4 0.158 5 TM4 0.636 5 TM4 0.158 5 TM4 0.0704 5 TM4 0.0704 5 TM4 0.0704 5 TM4 0.0704 5 TM4 0.0752 5 TM4 0.0365 5 TM4 0.0365 5 TM4 0.0365 5 TM4 0.0365 5 TM4 0.0375 5 TM4 0.0365 5 TM4 0.035 5 TM4 0.035 5 TM4 0.035 5 TM4 0.035 5 TM4 0.035 5 TM4 0.035 5 TM4 0.035 5 TM4 0.035 5 TM4 0.035	09 0.180 1 -0.014 2 0.246 3 0.290 0.329 0.468 -0.066 -0.009 0.0357 0.0131 0.131 0.137 0.131 0.137 0.000 0.002 -0.000	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.233 0.0000 0.000 0.000 0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.000000	0.705 0.561 0.560 0.022 0.078 0.113 0.171 0.154 0.257 0.207 0.287 0.287 0.247 1.612 0.559 0.032 0.023 0.023 0.054 0.054 0.054 0.054	0 01:10 0 01:10 0 01:08 0 01:18 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:14 0 01:16 0 01:17 0 01:18 0 01:11 0 01:10 0 01:10 0 01:10 0 01:15 0 01:15 0 01:10	0.333 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
1 1.439 3210 2.0.000 0.000 -0.002 0.000 ltr 0.000 ltr 0.000 ltr 0.000 ltr 0.005 9 -0.005 0.588 104 0.529 105 0.456 107 0.179 108 0.479 109 0.798 100 0.061 111 0.061 111 0.063 112 6.216 114 0.063 117 -0.043 118 -0.118 119 0.828 6 0.019 120 0.076	JUNCTION JUNCTION	0.022 0.022 0.113 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.255 0.087 0.113 0.113 0.000 0.465 0.459 0.043 0.580 0.579 0.574 0.568 1.097 0.574 0.568 1.097 0.883 0.560 0.143 0.683 0.496 0.447 0.416 0.699 0.021 0.226	0 01:17 0 01:17 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 08:00 0 08:00 0 08:00 0 08:00 0 08:00 0 08:00 0 01:15 0 01:11 0 01:10 0 01:13 0 01:13 0 01:10 0 01:12 0 01:12	0.0462 0 0.228 0 0 0.185 0 0.0569 0 0 0.0593 0 0.0593 0.544 0 0.0593 0.544 0 0.0593 0.544 0 0.0593		5 TM2 0 5 TM2 1.38 5 TM2 1.4 5 TM2 1.4 5 TM2 1.4 5 TM2 0.636 5 TM4 0.158 0.158 5 TM4 0.158 5 TM4 0.0704 5 TM4 0.0704 5 TM4 0.0704 5 TM4 0.0385 5 TM4 0.03	09 0.180 -0.014 2 0.246 3 0.246 -0.066 -0.069 -0.095 0.077 -0.106 0.357 0.913 0.619 -0.033 -0.131 0.137 0.137 0.000 2 0.000 0.002 -0.000 0.000	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.233 0.0000 0.000 0.000 0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.000000	0.705 0.561 0.560 0.022 0.078 0.113 0.171 0.154 0.257 0.207 0.287 0.287 0.345 0.447 1.612 0.559 0.032 0.023 0.023 0.023 0.054 0.054 0.054	0 01:10 0 01:0 0 01:0 0 01:18 0 01:18 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:14 0 01:16 0 01:17 0 01:18 0 01:11 0 01:10 0 01:10 0 01:10 0 01:15 0 01:10 0 01:10 0 01:10 0 01:15 0 01:10 0 01:10	0.333 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
1 1.439 3210 2.0.000 0.000 -0.002 0.000 ltr 0.000 ltr 0.000 ltr 0.000 ltr 0.005 9 -0.005 0.588 104 0.529 105 0.456 107 0.179 108 0.479 109 0.798 100 0.479 109 0.798 100 0.61 1111 0.232 122 6.216 144 0.063 177 -0.043 188 -0.118 199 0.828 6 0.119 121 0.076 122 0.087	JUNCTION JUNCTION	0.022 0.022 0.113 0.000 0.113 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.255 0.087 0.113 0.113 0.000 0.465 0.459 0.043 0.580 0.579 0.574 0.568 1.097 0.574 0.568 1.097 0.883 0.560 0.143 0.683 0.496 0.447 0.416 0.699 0.021 0.266 0.165	0 01:17 0 01:10 0 08:00 0 08:00 0 08:00 0 08:00 0 08:00 0 01:15 0 01:11 0 01:10 0 01:13 0 01:13 0 01:10 0 01:10 0 01:10	0.0462 0 0.228 0 0 0.185 0 0.0599 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		5 TM2 0 5 TM2 1.38 5 TM2 1.38 5 TM2 1.4 5 TM2 1.4 5 TM2 0.636 5 TM4 0.1636 5 TM4 0.1636 5 TM4 0.158 0.158 0.158 0.158 5 TM2 0.412 5 TM2 0.679 5 TM4 0.158 5 TM4 0.172 5 TM4 0.0365 5 TM4 0.0375 5 TM4	09 0.180 -0.014 2 0.246 3 0.246 -0.066 -0.609 -0.095 0.077 -0.106 0.357 0.913 0.619 -0.033 -0.131 0.137 0.137 0.000 2 0.000 -0.000 0.000 -0.000	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.233 0.0000 0.000 0.000 0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.000000	0.705 0.561 0.560 0.022 0.078 0.097 0.113 0.171 0.154 0.257 0.207 0.287 0.287 0.247 1.612 0.559 0.032 0.023 0.023 0.023 0.054 0.054 0.054 0.054 0.079 0.108 0.096	0 01:10 0 01:0 0 01:0 0 01:18 0 01:18 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:14 0 01:16 0 01:17 0 01:18 0 01:11 0 01:10 0 01:10 0 01:10 0 01:15 0 01:10 0 01:15 0 01:10 0 01:10 0 01:15 0 01:10 0 01:10 0 01:15 0 01:10 0 01:10 0 01:15 0 01:10 0 01:	0.333 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
1 1.439 H210 2 0.000 0.000 -0.002 0.000 ltr 0.000 ltr 0.000 ltr 0.001 0.588 104 0.529 105 0.588 104 0.529 105 0.456 107 0.798 104 0.798 104 0.798 105 0.479 109 0.798 101 0.061 114 0.023 114 0.063 117 0.078 101 0.798 101 0.798 101 0.798 101 0.798 101 0.798 101 0.078 102 0.798 101 0.061 114 0.023 114 0.063 117 0.003 118 -0.018 109 0.528 100 0.798 100 0.003 100 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0	JUNCTION JUNCTION	0.022 0.022 0.022 0.113 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.255 0.087 0.113 0.113 0.000 0.465 0.459 0.043 0.580 0.579 0.574 0.568 1.097 0.574 0.568 1.097 0.883 0.560 0.143 0.683 0.496 0.447 0.416 0.699 0.021 0.266 0.165 1.488	0 01:17 0 01:10 0 08:00 0 08:00 0 08:00 0 08:00 0 08:00 0 08:00 0 08:00 0 01:15 0 01:11 0 01:10 0 01:13 0 01:10 0 01:11 0 01:110 0 01:100 0 01:1	0.0462 0 0.228 0 0 0.185 0 0 0.185 0 0 0.0599 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		5 TM2 0 5 TM2 1.38 5 TM2 1.4 5 TM2 1.4 5 TM2 1.4 5 TM2 1.4 5 TM2 0.636 5 TM3 0.636 5 TM3 0.158 5 TM4 0.158 5 TM4 0.158 5 TM4 0.158 5 TM5 0.158 5 TM5 0.172 5 TM5 0.0386 5 TD2 0.0386 5 TD2	09 0.180 1 -0.014 2 0.246 3 0.290 0.329 0.468 -0.066 -0.009 0.0357 0.0131 0.131 0.131 0.137 0.131 0.137 0.000 2 0.002 -0.000 0.000 0.000 0.000 0.000	JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION JUNCTION	0.233 0.0000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.000000	0.705 0.561 0.560 0.022 0.078 0.097 0.113 0.171 0.154 0.257 0.207 0.287 0.287 0.247 1.612 0.559 0.032 0.023 0.023 0.023 0.054 0.054 0.054 0.054 0.096 0.096	0 01:10 0 01:08 0 01:10 0 01:18 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:14 0 01:16 0 01:16 0 01:11 0 01:12 0 01:11 0 01:12 0 01:12 0 01:12 0 01:10 0 01:10 0 01:10 0 01:15 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10	0.333 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
1 1.439 H210 0.000 0.000 0.000 0.000 1tr 0.000 0.588 004 0.529 005 0.456 007 0.179 0061 0.232 0061 0.061 00798 0.479 00798 0.479 00798 0.419 0061 0.061 0073 0.232 111 0.061 00798 0.118 109 0.828 00119 0.479 120 0.087 121 0.087 122 0.087 132 0.119 0.476 0.119	JUNCTION JUNCTION	0.022 0.022 0.113 0.0000 0.000 0.000 0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.000000	0.255 0.087 0.113 0.113 0.000 0.465 0.459 0.043 0.580 0.579 0.574 0.568 1.097 0.574 0.568 1.097 0.883 0.560 0.143 0.683 0.496 0.447 0.416 0.699 0.021 0.266 0.165 1.488 1.490	 0 01:17 0 01:10 0 01:11 0 01:10 0 01:12 0 01:13 0 01:13 0 01:13 0 01:13 0 01:14 0 01:10 0 11:10 	0.0462 0 0.228 0 0 0.185 0 0 0.185 0 0 0.0599 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		5 TM2 0 5 TM2 1.38 5 TM2 1.38 5 TM2 1.4 5 TM2 1.4 5 TM2 0.636 5 TM3 0.636 5 TM4 0.158 5 TM4 0.158 5 TM4 0.158 5 TM4 0.158 5 TM4 0.158 5 TM4 0.158 5 TM5 0.158 5 TM5 0.0704 5 TM5 0.0704 5 TM5 0.0704 5 TM5 0.0704 5 TM5 0.0386 5 TM5 0.0386 0.038	09 0.180 -0.014 2 0.246 3 0.246 -0.066 -0.069 -0.095 0.077 -0.106 0.357 0.913 0.619 -0.033 -0.131 0.137 0.137 0.000 2 0.000 -0.000 0.000 -0.000 0.000 -0.000 0.000 -0.000 0.000 -0.000 0.000 -0.000 0.000 -0.000 0.000 -0.000 0.000 -0.000 0.000 -0.000 0.000 -0.000 0.000 -0.000 0.000 -0.000 0.000 -0.000 0.000 -0.000 0.000 -0.000 0.000 -0.000 0.000 -0.000 -0.000 0.000 -0.0000 -0.0000 -0.0000 -0.0000 -0.0000 -0.0000 -0.0000 -0.000	JUNCTION JUNCTION	0.233 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.000000	0.705 0.561 0.560 0.022 0.078 0.097 0.113 0.171 0.154 0.257 0.207 0.287 0.287 0.247 0.345 0.447 1.612 0.559 0.032 0.023 0.023 0.054 0.054 0.054 0.096 0.096 0.096 0.024	0 01:10 0 01:08 0 01:08 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:14 0 01:16 0 01:16 0 01:11 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10	0.333 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
1.439 0.000 0.000 -0.002 0.000 ltr -0.011 0.000 ltr -0.011 0.005 12 0.588 14 0.529 15 0.456 17 0.529 15 0.456 17 0.222 16 0.221 16 0.222 17 0.061 11 0.222 16 0.216 17 0.222 17 0.061 11 0.222 16 0.061 11 0.232 17 0.043 18 0.118 19 0.538 10	JUNCTION JUNCTION	0.022 0.022 0.113 0.000 0.133 0.000 0.033 0.000 0.043 0.000 0.000 0.000 0.000 0.000 0.000 0.042 0.381 0.000 0.042 0.381 0.000 0.042 0.000 0.042 0.0000 0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.00000 0.000000	0.255 0.087 0.113 0.113 0.000 0.465 0.459 0.043 0.580 0.579 0.574 0.568 1.097 0.574 0.568 1.097 0.574 0.568 1.097 0.574 0.568 1.097 0.433 0.560 0.143 0.447 0.416 0.699 0.021 0.226 0.165 1.488 1.490 1.076	 0 01:17 0 01:10 0 01:11 0 01:10 0 01:11 0 11:10 0 11:10 0 11:11 0 11:10 0 11:11 0 11:11 0 11:12 0 11:12 0 11:10 0 11:12 0 11:10 0 11:10 0 11:10 0 11:11 0 11:12 0 11:12 0 11:10 0 11:11 0 11:11 0 11:11 0 11:12 	0.0462 0 0.228 0 0 0.185 0 0 0.0599 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		5 TM2 0 5 TM2 1.38 5 TM2 1.38 5 TM2 1.4 5 TM2 1.4 5 TM2 0.636 5 TM3 0.636 5 TM4 0.158 0.158 5 TM4 0.158 5 TM4 0.158 5 TM4 0.636 5 TM4 0.158 5 TM4 0.158 5 TM4 0.636 5 TM4 0.158 5 TM4 0.172 5 TM4 0.0365 5 TM4 0.0555 5 TM4 0.0555 0.05	09 0.180 -0.014 0.246 .3 0.290 0.329 0.468 -0.066 -0.095 -0.095 0.077 -0.131 0.317 -0.131 0.137 -0.000 0.0002 -0.000 0.0002 -0.000 0.0002 -0.000 0.0001 0.0001 0.0001 0.0001 0.0001	JUNCTION JUNCTION	0.233 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.000000	0.705 0.561 0.560 0.022 0.078 0.097 0.113 0.171 0.154 0.257 0.207 0.287 0.287 0.247 0.345 0.447 1.612 0.559 0.032 0.023 0.023 0.054 0.054 0.054 0.054 0.096 0.096 0.024 0.024	0 01:10 0 01:08 0 01:08 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:14 0 01:16 0 01:16 0 01:11 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:	0.333 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
1.439 0.000 0.000 -0.002 0.000 ltr 0.000 ltr 0.000 ltr 0.000 ltr 0.005 0.588 0.529 0.456 0.529 0.456 0.179 0.061 114 0.232 0.061 114 0.232 0.061 114 0.232 0.061 114 0.232 0.061 12 0.061 13 0.232 0.061 14 0.053 0.119 0.538 0.119 0.538 0.119 0.076 22 0.087 0.119 0.076 22 0.087 0.119 0.011 0.011 0.051 0.119 0.051 0.118 0.053 0.119 0.076 22 0.087 0.119 0.053 0.119 0.076 0.019 0.011 0.051 0.005 0.111 0.005 0.118 0.011 0.053 0.119 0.076 0.011 0.055 0.05	JUNCTION JUNCTION	0.022 0.022 0.113 0.000 0.133 0.000 0.033 0.000 0.043 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.042 0.381 0.000 0.042 0.381 0.000 0.042 0.381 0.000 0.042 0.000 0.000 0.000 0.042 0.0000 0.000 0.000 0.000 0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.0000 0.000000	0.255 0.087 0.113 0.113 0.000 0.465 0.459 0.043 0.579 0.574 0.568 1.097 0.574 0.568 1.097 0.574 0.568 1.097 0.540 0.447 0.416 0.699 0.021 0.266 0.165 1.488 1.490 1.076 1.072	 0 01:17 0 01:10 0 01:11 0 01:10 0 01:11 0 11:10 0 11:10 0 11:11 0 11:11 0 11:12 0 11:10 0 11:12 0 11:10 0 11:11 0 11:11 0 11:12 0 11:11 0 11:12 0 11:11 	0.0462 0 0.228 0 0 0.185 0 0.0599 0 0 0.0593 0.544 0 0.0593 0.544 0 0.0593 0.544 0 0.992 0 0.992 0 0.992 0 0 0.992 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		5 TM2 0 5 TM2 1.38 5 TM2 1.38 5 TM2 1.4 5 TM2 1.4 5 TM2 0.636 5 TM3 0.636 5 TM4 0.158 0.158 5 TM4 0.158 5 TM4 0.172 5 TM4 0.0365 5 TM4 0.0365 5 TM5 0.0365 5 TM5 0.0365 5 TM5 0.0365 5 TM5 0.0365 5 TM5 0.0365 5 TM6 0.0365 5 TM5 0.0365 5 TM5 0.0355 5 TM5 0.0555 5 TM5	09 0.180 -0.014 0.246 .3 0.290 0.329 0.468 -0.066 -0.095 -0.077 -0.106 0.357 0.913 0.4619 -0.033 -0.131 0.137 0.137 0.000 -0.000 0.002 -0.000 0.002 -0.000 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001	JUNCTION JUNCTION	0.233 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.000000	0.705 0.561 0.560 0.022 0.078 0.097 0.113 0.171 0.154 0.257 0.207 0.287 0.287 0.247 0.345 0.447 1.612 0.559 0.032 0.023 0.023 0.054 0.054 0.054 0.054 0.054 0.096 0.096 0.024 0.022	0 01:10 0 01:10 0 01:08 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:14 0 01:16 0 01:11 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:15 0 01:15 0	0.333 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
1.439 2. 0.000 0.000 -0.002 0.000 1tr 0.000 1tr 0.000 1tr 0.000 1tr 0.005 0.2 0.588 0.4 0.529 0.2 0.588 0.4 0.529 0.5 0.456 0.7 0.179 0.8 0.479 0.9 0.798 10 0.061 11 0.022 1.1 0.076 1.1 0.022 0.043 -0.118 1.9 0.828 0.119 1.0 0.63 -0.011 0.022 0.003 0.003 0.001 1.1 0.025 0.119 1.1 0.025 0.119 1.2 0.011 0.020 0.001 1.1 0.025 0.1 0.05 0.1 0.05 0.0 0.011 0.0 0.001 0.0 0.005 0.0 0.005 0.1 0.005 0.0 0.005 0	JUNCTION JUNCTION	0.022 0.022 0.113 0.000 0.133 0.000 0.033 0.000 0.043 0.000 0.000 0.000 0.000 0.000 0.000 0.042 0.381 0.000 0.042 0.381 0.000 0.042 0.000 0.042 0.0000 0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.000000	0.255 0.087 0.113 0.113 0.000 0.465 0.459 0.043 0.580 0.579 0.574 0.568 1.097 0.574 0.568 1.097 0.574 0.568 1.097 0.574 0.568 1.097 0.433 0.560 0.143 0.447 0.416 0.699 0.021 0.226 0.165 1.488 1.490 1.076	 0 01:17 0 01:10 0 01:11 0 01:10 0 01:11 0 11:10 0 11:10 0 11:11 0 11:10 0 11:11 0 11:11 0 11:12 0 11:12 0 11:10 0 11:12 0 11:10 0 11:10 0 11:10 0 11:11 0 11:12 0 11:12 0 11:10 0 11:11 0 11:11 0 11:11 0 11:12 	0.0462 0 0.228 0 0 0.185 0 0.0599 0 0 0.0599 0 0 0.0593 0.544 0 0 0.0593 0.544 0 0 0.992 0 0.992 0 0 0.992 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		J 55 0 STM2 1.38 STM2 1.4 STM2 1.4 STM2 0.6356 STM6 0.103 STM4 0.6356 STM5 0.138 STM5 0.138 STM6 0.138 STM6 0.412 STM6 0.412 STM6 0.412 STM6 0.412 STM6 0.412 STM6 0.412 STM6 0.412 STM6 0.412 STM6 0.412 STM6 0.412 STM6 0.412 STM6 0.412 STM6 0.412 STM6 0.412 STM6 0.412 STM6 0.412 STM6 0.412 STM6 0.545 STM6 0.412 STM6 0.412 STM6 0.545 STM6 0.545 STM6 0.412 STM6 0.545 STM6 0.545 STM6 0.545 STM6 0.158 STM6 0.158 STM6 0.158 STM6 0.158 STM6 0.122 0.0365 5.102 0.0365 STM6 0.985 STM6 0.0365 STM6 0.0365 STM6 0.0365 STM6 STM6 0.985 STM6	09 0.180 -0.014 0.246 .3 0.290 0.329 0.468 -0.066 -0.095 -0.077 -0.106 0.357 0.913 0.4619 -0.033 -0.131 0.137 0.137 0.000 -0.000 0.002 -0.000 0.002 -0.000 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001	JUNCTION JUNCTION	0.233 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.000000	0.705 0.561 0.560 0.022 0.078 0.097 0.113 0.171 0.154 0.257 0.207 0.287 0.287 0.247 0.345 0.447 1.612 0.559 0.032 0.023 0.023 0.054 0.054 0.054 0.054 0.096 0.096 0.024 0.024	0 01:10 0 01:08 0 01:08 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:14 0 01:16 0 01:16 0 01:11 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:12 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:10 0 01:	0.333 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

OFCanal 0 0.000 ltr						
	OUTFALL 0.0	00 0.000	0 00:00	0	SWMCCN1 JUNCTION 4.12 0.226 0.804	
BASIN1	STORAGE 0.1	51 1.409	0 01:10	0.197		
1.81 8.551 BASIN2 7.73 0.103	STORAGE 0.0	00 1.843	0 01:15	0	**************************************	
BASIN3 5.39 -0.055	STORAGE 0.0	00 1.685	0 01:12	0	**********	
S-BLDG-A 0.179 0.007	STORAGE 0.1	26 0.126	0 01:10	0.179	Flooding refers to all water that overflows a node, whether it ponds or not	•
S-BLDG-B 0.255 0.007	STORAGE 0.1	80 0.180	0 01:10	0.255	Total Maximum Maximum Time of Max Flood Ponded	
S-BLDG-C 0.211 0.007	STORAGE 0.1	48 0.148	0 01:10	0.211	Hours Rate Occurrence Volume Depth Node Flooded CMS days hr:min 10^6 ltr Meters	
S-BLDG-D 0.0971 0.007	STORAGE 0.0	68 0.068	0 01:10	0.0971	STM111A 0.10 0.026 0 01:10 0.006 0.000	
S-BLDG-G 0.171 0.007	STORAGE 0.1		0 01:10	0.171		
S-BLDG-H 0.261 0.007	STORAGE 0.1		0 01:10	0.261	**************************************	
S-BLDG-I 0.159 0.007	STORAGE 0.1		0 01:10			
S-BLDG-J1 0.0731 0.008	STORAGE 0.0		0 01:10			
S-BLDG-J2 0.0627 0.008 S-BLDG-K	STORAGE 0.0 STORAGE 0.1		0 01:10	0.0627	Average Avg Evap Exfil Maximum Max of Max Maximum	Time
0.174 0.006	STORAGE 0.1	23 0.123	0 01:10	0.174	Volume Pcnt Pcnt Pcnt Volume Pcnt Occurrence Outflow Storage Unit 1000 m3 Full Loss Loss 1000 m3 Full	days
*****	****				hr:min CMS	
Node Surcharge Sum *****************					 BASIN1 0.382 60 0 0.630 99	0
Surcharging occurs	when water rises a	bove the top	of the highe	est conduit.	06:29 0.514 BASIN2 1.227 55 0 0 2.237 100	0
					07:10 0.774 BASIN3 2.466 52 0 0 4.649 97	0
Node	Hour Type Surcha	s Above		elow Rim Meters	06:34 0.409 S-BLDG-A 0.019 4 0 0 0.121 24	0
J23					01:52 0.009 S-BLDG-B 0.030 5 0 0.176 27 01:54 0.011	0
J26 J27	JUNCTION 2	2.99 3.01	1.216	0.609	01:54 0.011 S-BLDG-C 0.022 4 0 0 0.142 24 01:52 0.011	0
J40 J41	JUNCTION	3.69 6.90	0.137 1.213	0.625	0152 0.011 S-BLDG-D 0.011 4 0 0 0.066 25 0153 0.005	0
STM102 STM104	JUNCTION 2	2.97	1.155	0.150	S-BLDG-G 0.026 8 0 0.125 38 02:11 0.006	0
STM105 STM109	JUNCTION	6.92	0.995	1.050	S-BLDG-H 0.030 4 0 0.179 27 01:54 0.012	0
STM110 STM111A	JUNCTION	4.76	0.301	0.949	S-BLDG-I 0.016 3 0 0.106 23 01:50 0.008	0
STM203 STM204	JUNCTION	4.46	0.231 0.189	3.769	S-BLDG-J1 0.004 5 0 0.040 52 01:30 0.008	0
STM205 STM206		3.63	0.126	3.564	S-BLDG-J2 0.003 5 0 0.036 53 01:31 0.006	0
STM211 STM213	JUNCTION	4.63	0.276 1.133	0.951 0.547	S-BLDG-K 0.029 10 0 0.130 42 02:20 0.005	0
**************************************					C34 CONDUIT 0.042 0 01:06 0.93 0.97 1. C35 CONDUIT 0.065 0 01:09 0.48 0.34 1.	
Outfall Loading Su	mmary *****				C35 CONDUIT 0.065 0 01:09 0.48 0.34 1. C36 CONDUIT 0.113 0 01:08 0.64 0.67 1. C37 CONDUIT 0.222 0 01:11 0.17 0.02 0. C38 CONDUIT 0.093 0 01:13 0.74 0.85 1.	00 00 17 00
Outfall Loading Su	mmary ***** Flow Avg Freq Flow	Flow	Total Volume		C35 CONDUIT 0.065 0 01:09 0.48 0.34 1. C36 CONDUIT 0.113 0 01:08 0.64 0.67 1. C37 CONDUIT 0.222 0 01:11 0.17 0.02 0. C38 CONDUIT 0.093 0 01:13 0.74 0.85 1. C39 CONDUIT 0.097 0 01:12 0.99 1.48 1. C4 CONDUIT 0.447 0 1.78 1.53 0.	00 00 17 00 00 86
Outfall Loading Su	mmary ***** Flow Avg Freq Flow Pcnt CMS	Flow CMS	Volume 10^6 ltr		C35 CONDUT 0.065 0 0.109 0.48 0.34 1. C36 CONDUT 0.113 0 01:08 0.64 0.34 1. C37 CONDUT 0.222 0 01:11 0.17 0.022 0 C38 CONDUT 0.093 0 01:13 0.74 0.85 1. C39 CONDUT 0.097 0 01:12 0.9 1.48 1. C4 CONDUT 0.447 0 01:13 1.78 1.53 0. C40 CONDUT 0.1072 0 01:12 0.9 1.49 1. C41 CONDUT 0.1072 0 01:12 0.41 0.20 0.	00 00 17 00 00 86 00 13
Outfall Loading Su Outfall Node 	mmary ***** Flow Avg Freq Flow Pent CMS 32.22 0.222 0.00 0.000	Flow CMS 0.581 0.000	Volume 10^6 ltr 6.023 0.000		C35 CONDUIT 0.065 0 01:09 0.84 0.34 1. C36 CONDUIT 0.113 0 01:08 0.64 0.67 1. C37 CONDUIT 0.222 0 01:11 0.17 0.022 0 C38 CONDUIT 0.093 0 01:13 0.74 0.85 1. C39 CONDUT 0.093 0 01:13 0.74 0.85 1. C4 CONDUT 0.47 0 01:13 1.78 1.53 0. C40 CONDUT 0.102 0 01:11 0.93 1.49 1. C41 CONDUT 0.102 0 01:12 0.26 0. C43 CONDUT 0.075 0 01:29 0.41 0.02 0. C44 CONDUT 0.038 0 01:39 0.66 1.27 0.	00 00 17 00 00 86 00 13 20 87
Outfall Loading Su Outfall Node J28 OFCanal	mmary ***** Flow Avg Freq Flow Pent CMS 32.22 0.223	Flow CMS 0.581 0.000	Volume 10^6 ltr 6.023 0.000		C35 CONDUIT 0.065 0 01:09 0.84 0.34 1. C36 CONDUIT 0.113 0 01:08 0.64 0.67 1. C37 CONDUIT 0.222 0 01:11 0.17 0.62 0. C38 CONDUIT 0.093 0 01:13 0.74 0. 1.48 1. C39 CONDUT 0.093 0 01:13 0.74 0. 1.84 1. C4 CONDUT 0.47 0 01:13 1.78 1.53 0. C40 CONDUT 0.167 0 01:13 1.78 1.49 1. C41 CONDUT 0.047 0 01:29 0.41 0.02 0. C43 CONDUT 0.047 0 01:29 0.66 1.27 0. C44 CONDUT 0.038 0 01:10 0.66 0.06 0. C45 CONDUT 0.849<	00 00 17 00 00 86 00 13 20 87 16 12
Outfall Loading Su Outfall Node J28 OFCanal	mmary Flow Avç Freq Flow 22.22 0.222 0.00 0.000 16.11 0.223	Flow CMS 0.581 0.000	Volume 10^6 ltr 6.023 0.000		C35 CONDUIT 0.065 0 01:09 0.84 0.34 1. C36 CONDUIT 0.113 0 01:08 0.64 0.67 1. C37 CONDUIT 0.222 0 01:11 0.17 0.02 0. C38 CONDUIT 0.093 0 01:13 0.74 0. 0.85 1. C39 CONDUIT 0.093 0 01:13 0.74 0. 0.84 1. C4 CONDUIT 0.474 0 01:13 0.74 1.78 1.49 1. C40 CONDUT 0.447 0 01:13 1.78 1.49 1. C41 CONDUT 0.075 0 01:29 0.41 0.02 0. C43 CONDUT 0.047 0 01:20 0.26 0.01 0. C44 CONDUT 0.047 0 01:10 0.68 1.27 0. C45 CONDU	00 00 17 00 00 86 00 13 20 87 16 12 20 87 16 12 19
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Outfall Loading Su Outfall Node J28 OFCanal System Link Flow Summary Clo Clo Clo Clo Clo Clo Cl2 Cl3 Cl4 Cl5 Cl6 Cl7 Cl8 Cl8 Cl8 Cl8 Cl8 Cl8 Cl8 Cl9 C2 C20 C20 C21	<pre>mmary Flow Avg Freq Flow Pcnt CMS 32.22 0.222 0.00 0.000 16.11 0.223 Maximu [Flow Type CNDUIT 0.12 CONDUIT 0.12 CONDUIT 0.55 CONDUIT 0.55</pre>	Flow CMS CMS 0.581 0.000 0.581 0.000 0.581 0.000 0.581 0.000 0.581 0.000 0.011 0.000 0.001 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.000000	Volume 10^6 ltr 6.023 0.000 6.023 0.000 0.023 0.023 0.023 0.023 0.023 0.023 0.0280 0.0280 0.0280 0.0280 0.0280000000000	Max/ P Full F Flow De 0.21 0 0.83 1 1.07 1 0.00 0 0.79 1 3.09 1 1.84 1 2.23 1 1.84 1 2.23 1 0.51 1 0.51 1 0.33 1 1.11 1 0.88 1 0.0.81 1 1.11 1 1.28 1	C35 CONDUT 0.065 0 0.19 0.48 0.34 1.1 C36 CONDUT 0.113 0 0108 0.64 0.64 0.64 C37 CONDUT 0.222 0 01111 0.17 0.625 1. C38 CONDUT 0.093 0 01113 0.74 0.655 1. C4 CONDUT 0.447 0 01113 1.75 1.48 1. C40 CONDUT 0.477 0 01121 0.63 1.49 1. C41 CONDUT 0.047 0 0122 0.64 0.02 0. C43 CONDUT 0.745 0 01110 0.76 0. 0.22 0. C44 CONDUT 0.745 0 01111 0.77 0.77 0.77 0.77 0.77 0.77 0.77 0.77 0.77 0.77 0.74 0.74 0.74 0.74 0.77 0.74	00 00 17 10 00 00 00 00 86 87 11 12 20 87 14 00 00 99 94 16 00 99 94 16 00 99 94 16 00 00 99 94 16 00 99 94 16 00 00 00 00 00 00 00 00 00 00 00 00 00
Outfall Loading Su Outfall Node J28 OFCanal System Link Flow Summary Cl Cl Cl Cl Cl Cl Cl Cl Cl Cl	mmary Flow Avg Freq Flow Pcnt CMS 32.22 0.222 0.00 0.000 16.11 0.223 Maximu [Flow Type CN CONDUIT 0.12 CONDUIT 0.16 CONDUIT 0.61 CONDUIT 0.62 CONDUIT 0.62 CONDUIT 0.55 CONDUIT 0.55 CONDUIT 0.55 CONDUIT 0.55 CONDUIT 0.68 CONDUIT 0.68 CONDUIT 0.62 CONDUIT 0.68 CONDUIT 0.62 CONDUIT 0.64 CONDUIT 0.62 CONDUIT 0.65 CONDUIT 0.62 CONDUIT 0.65 CONDUIT 0.65 CONDUIT 0.65 CONDUIT 0.62 CONDUIT 0.62 CONDUIT 0.65 CONDUIT 0.62 CONDUIT 0.65 CONDUIT 0.62 CONDUIT 0.65 CONDUIT 0.65 CONDUIT 0.65 CONDUIT 0.62 CONDUIT 0.65 CONDUIT 0.6	Flow CMS CMS 0.581 0.000 0.581 0.59 0.591 0.59 0.591 0.59	Volume 10^6 ltr 6.023 6.023 6.023 7.025 7.027 7.027 7.027 7.025 7.027 7.027 7.027 7.027 7.025 7.027 7.	Max/ P Fulm F Flow D 0.21 C 2.67 1 1.07 1 0.00 C 0.79 1 1.84 1 2.23 1 0.51 1 0.53 1 1.11 0 0.88 1 0.17 1 0.17 1 0.62 1 0.62 1	C35 CONDUT 0.065 0 0.19 0.48 0.34 1.1 C36 CONDUT 0.113 0.170 0.47 0.42 1.1 C37 CONDUT 0.222 0 01111 0.17 0.42 0.42 C38 CONDUT 0.093 0 01113 0.178 0.48 1. C4 CONDUT 0.447 0 01113 1.78 1.53 0. C40 CONDUT 0.047 0 01129 0.41 0.22 0. C41 CONDUT 0.047 0 0129 0.46 0.22 0. C43 CONDUT 0.489 0 0110 0.66 0. C44 CONDUT 0.745 0 01111 0.46 0.02 0. C44 CONDUT 0.745 0 01111 0.46 0.02 0. C47 CONDUT 0.454 0 0113 1.90 1.	00 00 17 00 86 00 13 12 20 87 14 16 12 20 87 14 16 08 99 94 16 00 00 00 00 00 00 00 00 00 00 00 00 00
Outfall Loading Su Outfall Node J28 OFCanal J28 OFCanal Link Flow Summary Link Flow Summary Cl Cl0 Cl0 Cl0 Cl0 Cl0 Cl0 Cl2 Cl3 Cl4 Cl5 Cl6 Cl7 Cl8 Cl7 Cl8 Cl7 Cl8 Cl7 Cl8 Cl2 Cl0 Cl0 Cl0 Cl0 Cl0 Cl0 Cl0 Cl0	mmary Flow Avg Freq Flow Pcnt CM 32.22 0.223 0.00 0.000 16.11 0.223 ** ** ** ** ** ** ** CONDUIT 0.13 CONDUIT 0.13 CONDUIT 0.12 CONDUIT 0.12 CONDUIT 0.12 CONDUIT 0.12 CONDUIT 0.12 CONDUIT 0.12 CONDUIT 0.55 CONDUIT	<pre> Flow CMS CMS CMS 0.581 0.000 0.581 0.591</pre>	Volume 10^6 ltr 6.023 6.023 6.023 7.025 7.	Max/ P Full F Flow De 0.21 C 2.67 D 1.07 D 0.33 D 1.07 D 2.23 D 2.23 D 1.84 D 2.17 D 0.51 D 1.11 D 1.88 D 0.17 D 1.28 D 0.42 D 0.44 D 1.66 D	C35 CONDUIT 0.065 0 0.109 0.48 0.34 1. C36 CONDUIT 0.113 0 01:08 0.64 0.67 1. C37 CONDUIT 0.022 0 01:11 0.17 0.02 0. C38 CONDUIT 0.037 0 01:12 0.74 0.85 1. C40 CONDUIT 0.47 0 01:13 1.78 1.53 0. C41 CONDUIT 0.077 0 01:29 0.44 0.02 0. C43 CONDUIT 0.047 0 01:13 0.78 0.02 0. C44 CONDUIT 0.047 0 01:10 0.76 0.02 0. C44 CONDUIT 0.475 0 01:11 0.77 0.07 0. C44 CONDUIT 0.451 0 01:11 0.45 0.02 0. C45 CONDUIT 0.455 0	00 00 17 00 86 00 13 13 20 87 14 16 12 20 87 14 16 09 99 94 16 00 00 00 00 00 00 00 00 00 00 00 00 00
Outfall Loading Su Outfall Node J28 OFCanal J28 OFCanal Link Flow Summary Link Flow Summary Cl Cl Cl Cl Cl Cl Cl Cl Cl Cl	<pre>mmary Flow Avg Freq Flow Pcnt CMB 22.22 0.223 0.00 0.000 16.11 0.223 Massimu</pre>	<pre>Flow CMS CMS 0.581 0.000 Time of Ma 0.581 Construction Construc</pre>	Volume 10^6 ltr 6.023 6.023 6.023 7.025 7.	Max/ P Full F Flow De 0.21 C 2.67 1 0.83 1 1.07 1 0.03 1 1.07 1 2.267 1 0.33 1 1.64 1 2.23 1 0.51 1 0.51 1 0.17 1 0.88 1 0.10 1 1.28 1 0.62 1 0.44 1 1.60 1 0.36 1	C35 CONDUT 0.065 0 0.109 0.48 0.34 1. C36 CONDUT 0.122 0 01:01 0.17 0.022 0 C38 CONDUT 0.033 0 01:13 0.74 0.85 1. C39 CONDUT 0.097 0 01:13 0.74 0.12 C40 CONDUT 0.47 0 01:13 1.78 1.33 0. C41 CONDUT 0.075 0 01:29 0.44 0.02 0. C43 CONDUT 0.038 0 01:39 0.86 1.77 0. C44 CONDUT 0.745 0 01:11 0.74 0.07 0. C45 CONDUT 0.745 0 01:11 0.45 0.02 0. C46 CONDUT 0.745 0 01:11 0.45 0.02 0. 0.01 0. 0.07 0. 0.01 0. 0.01 <td>00 00 17 00 86 00 13 13 20 87 14 16 12 20 87 16 12 20 87 16 12 20 87 16 12 20 87 16 12 20 87 16 15 00 00 00 00 00 00 00 00 00 00 00 00 00</td>	00 00 17 00 86 00 13 13 20 87 14 16 12 20 87 16 12 20 87 16 12 20 87 16 12 20 87 16 12 20 87 16 15 00 00 00 00 00 00 00 00 00 00 00 00 00
Outfall Loading Su Outfall Node J28 OFCanal J28 OFCanal Link Flow Summary Link Flow Summary C1 C1 C10 C10 C10 C10 C10 C10	<pre>mmary</pre>	<pre> Flow</pre>	Volume 10°6 ltr 6.023 0.000 6.023 4.023 4.023 4.023 4.023 4.023 4.023 4.023 4.023 4.023 4.023 4.023 4.023 4.023 4.023 4.023 4.023 4.025 5.0.57	Max/ Full F Full F F D 0.21 C 2.67 D 1.07 1 D D 1.07 1 D D 3.09 1 D D 1.84 1 D D 0.51 1 D D 0.88 D D D 0.17 1 D D D 0.22 D D D D 0.44 1 D D D 0.366 1 D D D 0.364 1 D D D	C35 CONDUT 0.065 0 0.109 0.48 0.34 1. C36 CONDUT 0.122 0 01:11 0.17 0.022 0 C38 CONDUT 0.093 0 01:13 0.74 0.85 1. C40 CONDUT 0.497 0 01:13 0.78 1.33 1.34 1. C41 CONDUT 0.477 0 01:13 0.78 1.33 1.34 1. C41 CONDUT 0.077 0 01:29 0.44 0.22 0. C43 CONDUT 0.038 0 01:39 0.86 1.27 0. C44 CONDUT 0.745 0 01:11 0.76 0.022 0. C45 CONDUT 0.745 0 01:11 0.45 0.02 0. C46 CONDUT 0.754 0 01:11 0.45 0.02 0. 0.01 0. 0.01 0.<	00 00 17 00 86 00 13 20 87 14 16 12 20 99 94 43 16 09 99 94 16 00 99 94 16 00 99 94 16 00 99 94 16 00 99 94 16 00 99 94 16 00 99 95 90 00 00 00 99 99 90 00 00 00 00 99 99
Outfall Loading Su Outfall Node J28 OFCanal System Link Flow Summary Link Plow Summary Cl Cl Cl Cl Cl Cl Cl Cl Cl Cl	<pre>mmary Flow Avg Freq Flow Pcnt CMB 22.22 0.223 0.00 0.000 16.11 0.223 Maximu [Flow Type CN CONDUIT 0.13 CONDUIT 0.12 CONDUIT 0.12 CONDUIT 0.12 CONDUIT 0.12 CONDUIT 0.12 CONDUIT 0.12 CONDUIT 0.13 CONDUIT 0.55 CONDUIT</pre>	<pre>Flow CMS CMS 0.581 0.000 </pre>	Volume 10^6 ltr 6.023 0.000 6.023 4.023	Max / Full F Full E Flow De 0.21 C 2.67 D 1.07 1 1.07 D 1.07 1 2.23 D 2.23 1 2.23 D 1.84 1 2.23 D 1.84 1 0.53 D 1.84 1 0.33 D 1.88 D 0.17 D 0.262 D 0.44 D 1.2.37 1 0.66 D 0.54 1 0.54 D 0.24 1 0.687 D 0.877 1 0.877 D 0.872 D 0.872 D	C35 CONDUT 0.065 0 0.109 0.48 0.34 1. C37 CONDUT 0.122 0 01:11 0.17 0.022 0 C38 CONDUT 0.033 0 01:12 0.74 0.85 1. C40 CONDUT 0.477 0 01:13 0.74 0.12 C41 CONDUT 0.477 0 01:13 0.78 1.3 C41 CONDUT 0.077 0 01:29 0.44 0.22 0. C43 CONDUT 0.037 0 01:29 0.41 0.22 0. C44 CONDUT 0.038 0 01:13 0.26 0.01 0. C44 CONDUT 0.752 0 01:11 0.75 0.02 0. C44 CONDUT 0.754 0 01:11 0.454 0.01 0. C45 CONDUT 0.454 0 01:13 1.99 1	00 00 17 10 86 80 87 12 20 87 14 12 20 99 94 94 16 10 99 94 94 16 10 00 99 94 16 10 00 90 99 94 16 10 00 90 99 94 16 10 00 90 99 94 16 10 00 90 99 94 16 10 00 90 99 99 90 16 10 00 90 99 90 16 10 00 90 99 90 10 10 00 90 99 90 10 10 00 90 99 90 10 10 00 90 99 90 10 10 00 90 99 90 10 10 00 90 99 90 10 10 00 90 99 90 10 10 00 90 90 90 90 90 90 90 90 90 90 90 90
Outfall Loading Su Outfall Node J28 OFCanal System Link Flow Summary Link Flow Summary Cl Cl Cl Cl Cl Cl Cl Cl Cl Cl	<pre>mmary Flow Avg Freq Flow Pcnt CMS 32.22 0.223 0.00 0.000 16.11 0.223 ** ** ** ** ** ** ** ** ** ** ** ** **</pre>	<pre>Flow CMS CMS 0.581 0.000 0.581 0.581 0.000 COURTEN COURTE</pre>	Volume 10^6 ltr 6.023 6.023 6.023 7.0000 7.0000 7.0000 7.0000 7.0000 7.0000 7.0000 7.0000 7.0000 7.0000 7.0000 7.0000 7.0000 7.0000 7.00000 7.00000 7.00000 7.000000 7.00000000	Max/ b Max/ b Full E Flow De F	C35 CONDUT 0.065 0 0.19 0.48 0.34 1. C37 CONDUT 0.123 0 01:11 0.17 0.022 0 C38 CONDUT 0.093 0 01:11 0.17 0.022 0 C39 CONDUT 0.093 0 01:11 0.74 0.85 1. C4 CONDUT 0.477 0 01:13 1.78 1.33 0 C40 CONDUT 0.077 0 01:29 0.41 0.02 0 C41 CONDUT 0.038 0 01:39 0.66 1.27 0 C43 CONDUT 0.745 0 01:11 0.75 0 0.22 0 C44 CONDUT 0.745 0 01:11 0.75 0 0.111 0.75 0 01:11 0.75 0 0.111 0.45 0.02 0 0 0.02 0.02 0 0.02 <	00 00 17 17 00 86 00 13 13 20 87 16 12 20 87 16 12 20 87 16 12 20 87 16 12 20 87 16 16 09 99 94 16 00 00 00 00 00 00 00 00 00 00 00 00 00
Outfall Loading Su Outfall Node J28 OFCanal System Link Flow Summary Cl Cl Cl Cl Cl Cl Cl Cl Cl Cl	<pre>mmary</pre>	<pre>Flow CMS CMS 0.581 0.000 0.581 0.5910</pre>	Volume 10^61tr 6.023 6.023 6.023 6.023 7.025 7.0	Max/ b Max/ b Full E Flow De F	C35 CONDUT 0.065 0 0.109 0.48 0.34 1. C37 CONDUT 0.122 0 01:11 0.17 0.022 0 C38 CONDUT 0.093 0 01:11 0.17 0.022 0 C39 CONDUT 0.093 0 01:11 0.74 0.85 1. C4 CONDUT 0.477 0 01:13 1.78 1.33 0 C40 CONDUT 0.077 0 01:29 0.44 0.02 0 C43 CONDUT 0.038 0 01:39 0.66 1.27 0 C44 CONDUT 0.745 0 01:11 0.75 0 0.22 0 C44 CONDUT 0.745 0 01:11 0.45 0.02 0 C44 CONDUT 0.752 0 01:11 0.45 0.02 0 0 0.00 0.000 0.000 0.000	00 00 17 17 00 86 00 13 13 20 87 16 12 20 87 16 12 20 99 94 16 00 00 99 94 16 00 00 00 00 00 00 00 00 00 00 00 00 00
Outfall Loading Su 	<pre>mmary Flow Avg Freq Flow Pcnt CMS 32.22 0.222 0.00 0.000 16.11 0.223</pre>	<pre> Flow CMS CMS CMS 0.581 0.000 0.581 0.591</pre>	Volume 10°6 ltr 6.023 0.000 	Max/ b Ma	C35 CONDUT 0.065 0 0.199 0.48 0.34 1. C37 CONDUT 0.222 0 01:11 0.17 0.02 0.02 C38 CONDUT 0.222 0 01:11 0.17 0.02 0.02 C39 CONDUT 0.097 0 01:12 0.74 0.65 1. C40 CONDUT 0.447 0 01:13 1.78 1.33 0. C41 CONDUT 0.075 0 01:29 0.44 0.02 0. C43 CONDUT 0.038 0 01:39 0.66 1.27 0. C44 CONDUT 0.745 0 01:11 0.745 0.022 0. C45 CONDUT 0.745 0 01:11 0.464 0.022 0. C47 CONDUT 0.753 0 01:11 0.454 0.022 0. C45 CONDUT 0.454 0	00 00 17 17 00 00 88 80 87 13 13 14 16 12 20 87 99 94 16 00 89 99 94 16 00 80 99 99 94 16 00 80 99 99 94 16 00 80 99 99 94 16 00 80 99 99 94 16 00 80 99 99 94 16 00 80 99 99 90 17 17 18 00 80 99 99 14 00 80 99 99 14 00 80 99 99 14 00 80 99 99 14 00 80 99 99 14 00 80 99 99 14 00 80 99 99 14 00 80 99 99 14 00 80 99 99 14 00 80 99 99 14 16 00 80 99 99 14 16 00 80 99 99 14 10 90 99 99 14 10 90 99 99 14 10 99 99 14 10 99 99 14 10 99 99 14 10 99 99 14 10 99 99 10 10 10 10 10 10 10 10 10 10 10 10 10

W30 W31 W4 C27_1 OR1	CONDUIT CONDUIT CONDUIT ORIFICE ORIFICE	0.000 0.000 0.642 0.570 0.204	0 00:00 0 00:00 0 01:24 0 08:00 0 09:45	0.00 0.00 1.86	0.00 0.00 0.35	0.00 0.00 1.00 1.00 1.00		**************** Flow Classifica ****************	ation Summary ******								
OR2 W1	ORIFICE WEIR	0.066	0 01:14 0 01:14			1.00			Adjusted								s
W10 W11	WEIR WEIR	0.000	0 00:00			0.00			/Actual		Up	Down	Sub	Sup	Up	Down	Norm
W12 W13	WEIR WEIR	0.033	0 01:21 0 01:10			0.07		Inlet Conduit Ctrl	Length	Dry	Dry	Dry	Crit	Crit	Crit	Crit	Ltd
W14 W15	WEIR WEIR	0.000	0 00:00			0.00											
W16 W17	WEIR WEIR	0.129	0 01:10 0 01:10			0.17		C1 0.00	1.00	0.01	0.00	0.00	0.37	0.00	0.00	0.61	0.08
W18 W19 W2	WEIR WEIR WEIR		0 01:11 0 01:11			0.08		C10 0.00	1.00	0.01							
W20	WEIR	1.695	0 01:15			1.00		0.00	1.00	0.01							
W21 W22 W23	WEIR WEIR	0.020	0 01:10 0 01:10			0.05		0.00		0.02							
W25 W26 W3	WEIR WEIR WEIR	0.143 0.001 1.271	0 01:10 0 01:10 0 01:10			0.18 0.01 1.00		C12 0.00 C13		1.00							
W33	WEIR	0.000	0 00:00			0.00		0.00 C14	1.00	0.01					0.00		
W34 W35	WEIR WEIR	0.000	0 00:00			0.00		0.00 C15	1.00						0.00		
W36 W37	WEIR WEIR	0.000	0 00:00			0.00		0.00 C16	1.00	0.01							
W38 W39	WEIR WEIR	0.055	0 01:10 0 00:00			0.10		0.00 C17	1.00						0.00		
W41 W42	WEIR WEIR	0.348	0 01:14 0 01:10			0.33		0.00 C18	1.00						0.00		
W43 W5	WEIR WEIR	0.001	0 01:10 0 01:09			0.01		0.00 C18 1	1.00						0.00		
W 6 W 7	WEIR WEIR	0.000	0 00:00			0.00		0.00 - C18 2	1.00						0.00		
W 8 W 9	WEIR WEIR	0.000 0.087	0 00:00 0 01:10			0.00		0.00 C19	1.00	0.02	0.00	0.00	0.96	0.00	0.00	0.02	0.00
C42 OL1	DUMMY DUMMY	0.086	0 04:42 0 06:34					0.00 C2	1.00	0.02	0.01	0.00	0.34	0.00	0.00	0.63	0.07
OL10 OL11	DUMMY DUMMY	0.012	0 01:06 0 01:04					0.00 C20	1.00	0.01	0.00	0.00	0.98	0.00	0.00	0.00	0.02
OL12 OL13	DUMMY DUMMY	0.008	0 01:07 0 01:03					0.00 C21	1.00	0.02	0.00	0.00	0.96	0.00	0.00	0.02	0.50
OL14 OL15	DUMMY DUMMY	0.008	0 01:12 0 01:12					0.00 C21_1	1.00	0.02	0.01	0.00	0.98	0.00	0.00	0.00	0.00
OL2 OL3	DUMMY DUMMY	0.115 0.084	0 01:21 0 01:10					0.00 C21_2 0.00	1.00	0.02	0.00	0.00	0.98	0.00	0.00	0.00	0.00
OL4 OL5	DUMMY DUMMY	0.057	0 01:10 0 00:00					C22 0.00	1.00	0.04	0.00	0.00	0.42	0.00	0.00	0.53	0.61
OL6 OL7	DUMMY DUMMY	0.009	0 01:07 0 01:06					C23 0.00	1.00	0.02	0.00	0.00	0.96	0.00	0.00	0.02	0.00
OL8 OL9	DUMMY DUMMY	0.011 0.005	0 01:07 0 01:06					C24 0.00	1.00	0.01	0.00	0.00	0.96	0.00	0.00	0.02	0.62
								C25 0.00	1.00	0.01	0.00	0.00	0.96	0.00	0.00	0.03	0.00
C26 0.00 C27	1.00		0.00 0.97					C53 0.00 C54	1.00	0.77							
0.00 C27 2			0.00 0.98					0.00 C55	1.00						0.00		
0.00			0.00 0.97					0.00 C56		0.01							
0.00	1.00		0.00 0.97					0.00 C57	1.00						0.00		
0.00 C3	1.00		0.00 0.27					0.00 C58	1.00						0.00		
0.00	1.00	0.02 0.00	0.00 0.97	0.00 0.0	0 0.0	0.00		0.00 C59	1.00	0.02	0.00	0.00	0.97	0.00	0.00	0.01	0.42
0.00 C31	1.00	0.02 0.00	0.00 0.97	0.00 0.0	0 0.0	0.00		0.00 C6	1.00	0.01	0.00	0.00	0.47	0.00	0.00	0.52	0.03
0.00 C32 0.00	1.00	0.00 0.00	0.00 1.00	0.00 0.0	0 0.0	0.00		0.00 C60 0.00	1.00	0.01	0.00	0.00	0.98	0.00	0.00	0.01	0.00
C33 0.00	1.00	0.01 0.00	0.00 0.36	0.00 0.0	0 0.6	0.01		C61 0.00	1.00	0.02	0.00	0.00	0.98	0.00	0.00	0.00	0.00
C34 0.00	1.00	0.02 0.00	0.00 0.50	0.00 0.0	0 0.4	0.20		C62 0.00	1.00	0.01	0.00	0.00	0.98	0.00	0.00	0.01	0.00
C35 0.00	1.00	0.05 0.00	0.00 0.49	0.00 0.0	0 0.4	0.06		C63 0.00	1.00	0.01	0.00	0.00	0.95	0.00	0.00	0.04	0.00
C36 0.00	1.00		0.00 0.67					C64 0.00	1.00						0.00		
C37 0.00	1.00		0.00 0.13					C65 0.00	1.00						0.00		
C38 0.00	1.00		0.00 0.35					C66 0.00	1.00						0.00		
C39 0.00	1.00		0.00 0.33					C67 0.00	1.00						0.00		
C4 0.00 C40	1.00		0.00 0.29					C68 0.00 C69	1.00						0.00		
0.00 C41	1.00		0.00 0.32					0.00	1.00						0.00		
0.00 C43	1.00		0.00 0.12					0.00	1.00						0.00		
0.00 C44	1.00		0.00 0.87					0.00	1.00						0.00		
0.11 C45	1.00		0.00 0.99					0.00	1.00						0.00		
0.00 C46	1.00		0.00 0.00					0.00 C73	1.00						0.00		
0.00 C47	1.00		0.00 0.13					0.00 C74	1.00						0.00		
0.00 C48	1.00	0.02 0.74	0.00 0.25	0.00 0.0	0 0.0	0.97		0.00 C75	1.00	0.54	0.04	0.00	0.42	0.00	0.00	0.00	0.59
0.00	1.00	0.03 0.26	0.00 0.68	0.03 0.0	0 0.0	0.78		0.00	1.00						0.00		
0.00	1.00	0.02 0.00	0.00 0.27	0.00 0.0	0 0.7	0.00		0.00	1.00	0.04	0.00	0.00	0.95	0.00	0.00	0.01	0.00
0.00	1.00	0.02 0.03	0.00 0.95	0.00 0.0	0 0.0	0.95		0.00 C78	1.00	0.01	0.52	0.00	0.47	0.00	0.00	0.00	0.97
0.00 C51	1.00	0.04 0.00	0.00 0.95	0.00 0.0	0 0.0	0.00		0.00 C79 0.00	1.00	0.01	0.52	0.00	0.47	0.00	0.00	0.00	0.97
0.00 C52 0.00	1.00	0.68 0.32	0.00 0.00	0.00 0.0	0 0.0	0.00		0.00 C8 0.00	1.00	0.01	0.00	0.00	0.55	0.00	0.00	0.44	0.02
							1										

0	1.00 0.0	1 0.73	0.00 0.25	0.01 0.00	0.00 0.76
<u>.</u>	1.00 0.0		0.00 0.20	0.01 0.00	0.00 0.70
	1.00 0.0	0.00	0.00 0.98	0.00 0.00	0.00 0.00
	1.00 1.0		0 00 0 00	0.00 0.00	0 00 0 00
	1.00 1.0	0.00	0.00 0.00	0.00 0.00	0.00 0.00
	1.00 1.0	0.00	0.00 0.00	0.00 0.00	0.00 0.00
	1.00 0.0	01 0.99	0.00 0.00	0.00 0.00	0.00 0.00
8	1.00 0.0	0.98	0.00 0.00	0.00 0.00	0.00 0.00
9	1.00 0.0	0.98	0.00 0.00	0.00 0.00	0.00 0.00
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nduit Surcharge	e Summary				
*******	*****				
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nduit				Normal Flow	
0	5.47	5.47	5.54	0.47	0.58
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1 3	7.50	7.50 6.46	7.75	0.15	0.11 0.01
4	6.77	6.80	7.49	0.41	0.38
5	7.48	7.49	7.55	0.20	0.23
6	7.57	7.58	7.72	0.22	0.19
7	8.00	8.01	8.05	0.21	0.37
8	6.42	6.42	6.69	0.01	0.01
8_1	4.08	4.08	4.77	0.01	0.01
8_2 9	4.77	4.77 6.69	4.92 6.95	0.11 0.01	0.10
2	0.44	0.05	0.50	0.01	0.01
0	7.39	7.39	23.37	0.01	0.01
1	7.36	7.36	7.74	0.30	0.32
1_1	5.15	5.15	5.53	0.01	0.01
1_2	5.53 7.78	5.53 7.78	5.60 8.22	0.01	0.38
2	7.78 8.35	8.35	8.22	0.38	0.01
4	3.67	3.67	6.37	0.01	0.01
5	6.68	6.68	7.51	0.01	0.01
6	5.86	5.86	6.19	0.01	0.76
7	5.97	5.97	7.36	0.01	0.01
7_2	6.90	6.90	6.92	0.01	0.44
8 9	6.95 7.38	6.95 7.38	6.95 22.97	0.01	1.26
	/.38 0.15	7.38 0.52	22.97	0.64	0.01
	0.10	0.02	2.20	0.0.	0.10



PROJECT INFORMATION

ENGINEERED PRODUCT MANAGER	
ADS SALES REP	
PROJECT NO.	



LANSDOWNE 2.0 ADS OTTAWA, ON, CANADA

MC-3500 STORMTECH CHAMBER SPECIFICATIONS

- CHAMBERS SHALL BE STORMTECH MC-3500. 1
- 2. CHAMBERS SHALL BE ARCH-SHAPED AND SHALL BE MANUFACTURED FROM VIRGIN, IMPACT-MODIFIED POLYPROPYLENE COPOLYMERS
- CHAMBERS SHALL BE CERTIFIED TO CSA B184, "POLYMERIC SUB-SURFACE STORMWATER MANAGEMENT STRUCTURES", AND MEET 3 THE REQUIREMENTS OF ASTM F2418, "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS" CHAMBER CLASSIFICATION 45x76 DESIGNATION SS.
- 4. CHAMBER ROWS SHALL PROVIDE CONTINUOUS, UNOBSTRUCTED INTERNAL SPACE WITH NO INTERNAL SUPPORTS THAT WOULD IMPEDE FLOW OR LIMIT ACCESS FOR INSPECTION.
- THE STRUCTURAL DESIGN OF THE CHAMBERS. THE STRUCTURAL BACKFILL, AND THE INSTALLATION REQUIREMENTS SHALL ENSURE 5. THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET FOR: 1) LONG-DURATION DEAD LOADS AND 2) SHORT-DURATION LIVE LOADS, BASED ON THE CSA S6 CL-625 TRUCK AND THE AASHTO DESIGN TRUCK WITH CONSIDERATION FOR IMPACT AND MULTIPLE VEHICLE PRESENCES.
- CHAMBERS SHALL BE DESIGNED, TESTED AND ALLOWABLE LOAD CONFIGURATIONS DETERMINED IN ACCORDANCE WITH ASTM F2787, 6 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS". LOAD CONFIGURATIONS SHALL INCLUDE: 1) INSTANTANEOUS (<1 MIN) AASHTO DESIGN TRUCK LIVE LOAD ON MINIMUM COVER 2) MAXIMUM PERMANENT (75-YR) COVER LOAD AND 3) ALLOWABLE COVER WITH PARKED (1-WEEK) AASHTO DESIGN TRUCK.
- REQUIREMENTS FOR HANDLING AND INSTALLATION: 7.
 - TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING. CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS.
 - TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL, THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 75 mm (3")
 - TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION, a) THE ARCH STIFFNESS CONSTANT AS DEFINED IN SECTION 6.2.8 OF ASTM F2418 SHALL BE GREATER THAN OR EQUAL TO 450 LBS/FT/%. AND b) TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES (ABOVE 23° C / 73° F), CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS.
- ONLY CHAMBERS THAT ARE APPROVED BY THE SITE DESIGN ENGINEER WILL BE ALLOWED. UPON REQUEST BY THE SITE DESIGN 8 ENGINEER OR OWNER, THE CHAMBER MANUFACTURER SHALL SUBMIT A STRUCTURAL EVALUATION FOR APPROVAL BEFORE DELIVERING CHAMBERS TO THE PROJECT SITE AS FOLLOWS:
 - THE STRUCTURAL EVALUATION SHALL BE SEALED BY A REGISTERED PROFESSIONAL ENGINEER.
 - THE STRUCTURAL EVALUATION SHALL DEMONSTRATE THAT THE SAFETY FACTORS ARE GREATER THAN OR EQUAL TO 1.95 FOR DEAD LOAD AND 1.75 FOR LIVE LOAD, THE MINIMUM REQUIRED BY ASTM F2787 AND BY SECTIONS 3 AND 12.12 OF THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS FOR THERMOPLASTIC PIPE.
 - THE TEST DERIVED CREEP MODULUS AS SPECIFIED IN ASTM F2418 SHALL BE USED FOR PERMANENT DEAD LOAD DESIGN EXCEPT THAT IT SHALL BE THE 75-YEAR MODULUS USED FOR DESIGN.
- CHAMBERS AND END CAPS SHALL BE PRODUCED AT AN ISO 9001 CERTIFIED MANUFACTURING FACILITY. q
- MANIFOLD SIZE TO BE DETERMINED BY SITE DESIGN ENGINEER. SEE TECH NOTE #6.32 FOR MANIFOLD SIZING GUIDANCE. DUE TO THE 10. ADAPTATION OF THIS CHAMBER SYSTEM TO SPECIFIC SITE AND DESIGN CONSTRAINTS, IT MAY BE NECESSARY TO CUT AND COUPLE ADDITIONAL PIPE TO STANDARD MANIFOLD COMPONENTS IN THE FIELD.
- ADS DOES NOT DESIGN OR PROVIDE MEMBRANE LINER SYSTEMS. TO MINIMIZE THE LEAKAGE POTENTIAL OF LINER SYSTEMS, THE MEMBRANE 11. LINER SYSTEM SHOULD BE DESIGNED BY A KNOWLEDGEABLE GEOTEXTILE PROFESSIONAL AND INSTALLED BY A QUALIFIED CONTRACTOR.

IMPORTANT - NOTES FOR THE BIDDING AND INSTALLATION OF MC-3500 CHAMBER SYSTEM

- STORMTECH MC-3500 CHAMBERS SHALL NOT BE INSTALLED UNTIL THE MANUFACTURER'S REPRESENTATIVE HAS COMPLETED A 1 PRE-CONSTRUCTION MEETING WITH THE INSTALLERS.
- STORMTECH MC-3500 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH MC-3500/MC-4500 CONSTRUCTION GUIDE". 2.
- CHAMBERS ARE NOT TO BE BACKFILLED WITH A DOZER OR AN EXCAVATOR SITUATED OVER THE CHAMBERS. 3. STORMTECH RECOMMENDS 3 BACKFILL METHODS:
 - STONESHOOTER LOCATED OFF THE CHAMBER BED.
 - BACKFILL AS ROWS ARE BUILT USING AN EXCAVATOR ON THE FOUNDATION STONE OR SUBGRADE.
 - BACKFILL FROM OUTSIDE THE EXCAVATION USING A LONG BOOM HOE OR EXCAVATOR.
- THE FOUNDATION STONE SHALL BE LEVELED AND COMPACTED PRIOR TO PLACING CHAMBERS. 4
- JOINTS BETWEEN CHAMBERS SHALL BE PROPERLY SEATED PRIOR TO PLACING STONE. 5.
- 6. MAINTAIN MINIMUM - 150 mm (6") SPACING BETWEEN THE CHAMBER ROWS.
- 7. INLET AND OUTLET MANIFOLDS MUST BE INSERTED A MINIMUM OF 300 mm (12") INTO CHAMBER END CAPS.
- 8. EMBEDMENT STONE SURROUNDING CHAMBERS MUST BE A CLEAN, CRUSHED, ANGULAR STONE WELL GRADED BETWEEN 3/4" AND 2" (20-50 mm).
- 9. STONE MUST BE PLACED ON THE TOP CENTER OF THE CHAMBER TO ANCHOR THE CHAMBERS IN PLACE AND PRESERVE ROW SPACING.
- THE CONTRACTOR MUST REPORT ANY DISCREPANCIES WITH CHAMBER FOUNDATION MATERIALS BEARING CAPACITIES TO THE SITE DESIGN 10. ENGINEER.
- ADS RECOMMENDS THE USE OF "FLEXSTORM CATCH IT" INSERTS DURING CONSTRUCTION FOR ALL INLETS TO PROTECT THE SUBSURFACE 11 STORMWATER MANAGEMENT SYSTEM FROM CONSTRUCTION SITE RUNOFF.

NOTES FOR CONSTRUCTION EQUIPMENT

- 1. STORMTECH MC-3500 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH MC-3500/MC-4500 CONSTRUCTION GUIDE".
- THE USE OF EQUIPMENT OVER MC-3500 CHAMBERS IS LIMITED: 2
- NO EQUIPMENT IS ALLOWED ON BARE CHAMBERS.
 - NO RUBBER TIRED LOADER, DUMP TRUCK, OR EXCAVATORS ARE ALLOWED UNTIL PROPER FILL DEPTHS ARE REACHED IN ACCORDANCE WITH THE "STORMTECH MC-3500/MC-4500 CONSTRUCTION GUIDE".
 - WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT CAN BE FOUND IN THE "STORMTECH MC-3500/MC-4500 CONSTRUCTION GUIDE"
- 3. FULL 900 mm (36") OF STABILIZED COVER MATERIALS OVER THE CHAMBERS IS REQUIRED FOR DUMP TRUCK TRAVEL OR DUMPING.

BACKFILL METHOD. ANY CHAMBERS DAMAGED BY USING THE "DUMP AND PUSH" METHOD ARE NOT COVERED UNDER THE STORMTECH STANDARD WARRANTY.

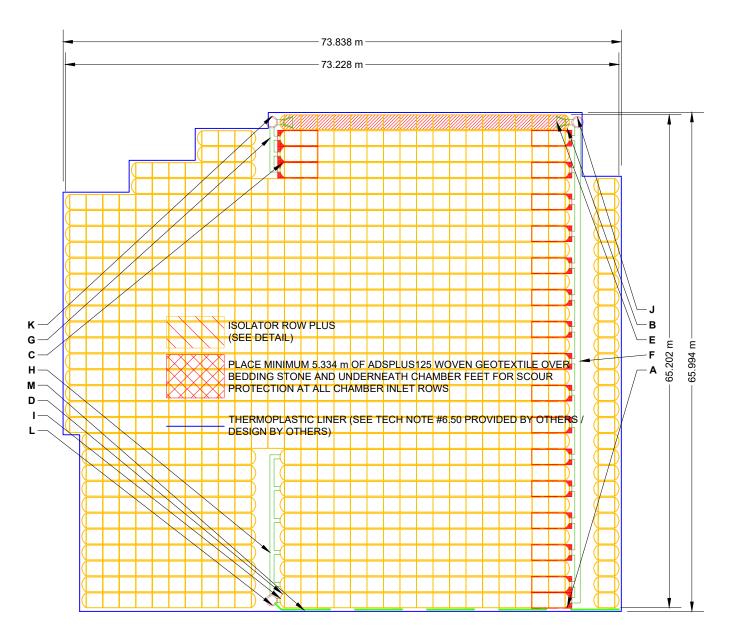
CONTACT STORMTECH AT 1-800-821-6710 WITH ANY QUESTIONS ON INSTALLATION REQUIREMENTS OR WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT.





- USE OF A DOZER TO PUSH EMBEDMENT STONE BETWEEN THE ROWS OF CHAMBERS MAY CAUSE DAMAGE TO CHAMBERS AND IS NOT AN ACCEPTABLE

	PROPOSED LAYOUT	PROPOSED ELEVATIONS:				
883	STORMTECH MC-3500 CHAMBERS	MAXIMUM ALLOWABLE GRADE (TOP OF PAVEMENT/UNPAVED):	66.670	PART TYPE	ITEM ON	DESCRIPTION
142		MINIMUM ALLOWABLE GRADE (UNPAVED WITH TRAFFIC):	64.842	PREFABRICATED END CAP		600 mm TOP CORED END CAP, PART#: MC3500IEPP24TC / TYP OF ALI
305	STONE ABOVE (mm)	MINIMUM ALLOWABLE GRADE (UNPAVED NO TRAFFIC):	64.68	1		600 mm BOTTOM CORED END CAP, PART#: MC3500IEPP24BC / TYP O
229	STONE BELOW (mm)	MINIMUM ALLOWABLE GRADE (TOP OF RIGID CONCRETE PAVEMENT):		PREFABRICATED END CAP		CONNECTIONS AND ISOLATOR PLUS ROWS
40	STONE VOID	MINIMUM ALLOWABLE GRADE (BASE OF FLEXIBLE PAVEMENT):	64.689			450 mm TOP CORED END CAP, PART#: MC3500IEPP18TC / TYP OF ALI
	INSTALLED SYSTEM VOLUME (m ³)	TOP OF STONE:	64.537		-	,
4777.1		TOP OF MC-3500 CHAMBER:	64.232	PREFABRICATED END CAP		450 mm BOTTOM CORED END CAP, PART#: MC3500IEPP18BC / TYP O
4///.1		450 mm x 450 mm TOP MANIFOLD INVERT:	63.597	7	_	
		600 mm x 600 mm TOP MANIFOLD INVERT:		FLAMP		INSTALL FLAMP ON 600 mm ACCESS PIPE / PART#: MCFLAMP (TYP 2
	SYSTEM AREA (m ²)	600 mm ISOLATOR ROW PLUS INVERT:	63.14	MANIFOLD		600 mm x 600 mm TOP MANIFOLD, ADS N-12
279.7		600 mm ISOLATOR ROW PLUS INVERT:	63.14	MANIFOLD	G	450 mm x 450 mm TOP MANIFOLD, ADS N-12
6096	THERMOPLASTIC LINER (m ²)	450 mm x 450 mm BOTTOM MANIFOLD INVERT:	63.134	MANIFOLD	Н	450 mm x 450 mm BOTTOM MANIFOLD, ADS N-12
0030	(20% OVERAGE)	450 mm BOTTOM CONNECTION INVERT:	63.134	PIPE CONNECTION		450 mm BOTTOM CONNECTION
		BOTTOM OF MC-3500 CHAMBER:	63.089	CONCRETE STRUCTURE	J	(DESIGN BY ENGINEER / PROVIDED BY OTHERS)
		UNDERDRAIN INVERT:	02.000	CONCRETE STRUCTURE	K	(DESIGN BY ENGINEER / PROVIDED BY OTHERS)
		BOTTOM OF STONE:	62.860	CONCRETE STRUCTURE	L	OCS (DESIGN BY ENGINEER / PROVIDED BY OTHERS)
				UNDERDRAIN	М	150 mm ADS N-12 DUAL WALL PERFORATED HDPE UNDERDRAIN



NOTES THE SITE DESIGN ENGINEER MUST REVIEW ELEVATIONS AND IF NECESSARY ADJUST GRADING TO ENSURE THE CHAMBER COV NOT FOR CONSTRUCTION: THIS LAYOUT IS FOR DIMENSIONAL PURPOSES ONLY TO PROVE CONCEPT & THE REQUIRED STORAGE

INVERT ABOVE BASE OF CHAMBER NVERT MAX FLOW ALL 600 mm TOP CONNECTIONS 368 mm 52 mm 509 mm OF ALL 600 mm BOTTOM 45 mm 45 mm 22 PLACES) 368 mm 509 mm 368 mm 45 mm 100 mm 45 mm 100 mm 100 mm 46 mm 100 mm 100 mm 47 mm 100 mm 100 mm 100 mm 100 mm <th>-</th>	-
ALL 600 mm TOP CONNECTIONS 368 mm S0	THIS DRAWING HAS BEEN PREPARED BASED ON INFORMATION PROVIDED TO ADS/STORMTECH UNDER THE DIRECTION OF THE PROJECT'S ENGINEER OF RECORD ("EOR") OR OTHER PROJECT REPRESENTATIVE. THIS DRAWING IS NOT INTENDED FOR USE IN BIDDING OR CONSTRUCTION AND COLTINE REPORT AND REPORT AND REVIEW THIS DRAWING PRIOR TO BIDDING AND/OR CONSTRUCTION. IT IS THE ULTIMATE RESPONSIBILITY OF THE EQR TO ENSURE THAT THE PRODUCT(S) DEPICTED AND ALL ASSOCIATED DETAILS MEET ALL APPLICABLE AND REPORT AND REPORT AND REPORT AND REVIEW THIS DRAWING PRIOR TO BIDDING AND/OR CONSTRUCTION. IT IS THE ULTIMATE RESPONSIBILITY OF THE EQR TO ENSURE THAT THE PRODUCT(S) DEPICTED AND ALL ASSOCIATED DETAILS MEET ALL APPLICABLE AND REPORT AND REPORT AND REPORT AND REPORTED AND AND AND AND AND AND AND AND AND AN
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OVER REQUIREMENTS ARE MET. AGE VOLUME CAN BE ACHIEVED ON SITE. 2 OF 5	

ACCEPTABLE FILL MATERIALS: STORMTECH MC-3500 CHAMBER SYSTEMS

	MATERIAL LOCATION	DESCRIPTION	AASHTO MATERIAL CLASSIFICATIONS	COMPA
D	FINAL FILL: FILL MATERIAL FOR LAYER 'D' STARTS FROM THE TOP OF THE 'C' LAYER TO THE BOTTOM OF FLEXIBLE PAVEMENT OR UNPAVED FINISHED GRADE ABOVE. NOTE THAT PAVEMENT SUBBASE MAY BE PART OF THE 'D' LAYER	ANY SOIL/ROCK MATERIALS, NATIVE SOILS, OR PER ENGINEER'S PLANS. CHECK PLANS FOR PAVEMENT SUBGRADE REQUIREMENTS.	N/A	PREPAR INSTALL
с	INITIAL FILL: FILL MATERIAL FOR LAYER 'C' STARTS FROM THE TOP OF THE EMBEDMENT STONE ('B' LAYER) TO 24" (600 mm) ABOVE THE TOP OF THE CHAMBER. NOTE THAT PAVEMENT SUBBASE MAY BE A PART OF THE 'C' LAYER.	GRANULAR WELL-GRADED SOIL/AGGREGATE MIXTURES, <35% FINES OR PROCESSED AGGREGATE. MOST PAVEMENT SUBBASE MATERIALS CAN BE USED IN LIEU OF THIS LAYER.	AASHTO M145 ¹ A-1, A-2-4, A-3 OR AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57, 6, 67, 68, 7, 78, 8, 89, 9, 10	BEGIN COM THE CHAMBI 12" (300 mm) WELL GRA
В	EMBEDMENT STONE: FILL SURROUNDING THE CHAMBERS FROM THE FOUNDATION STONE ('A' LAYER) TO THE 'C' LAYER ABOVE.	CLEAN, CRUSHED, ANGULAR STONE OR RECYCLED CONCRETE ⁵	AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57	
A	FOUNDATION STONE: FILL BELOW CHAMBERS FROM THE SUBGRADE UP TO THE FOOT (BOTTOM) OF THE CHAMBER.	CLEAN, CRUSHED, ANGULAR STONE OR RECYCLED CONCRETE ⁵	AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57	PLATE CO

PLEASE NOTE:

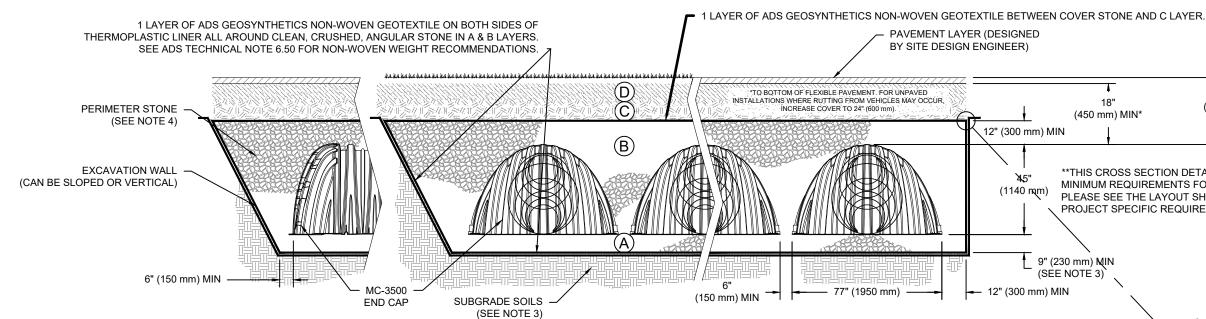
THE LISTED AASHTO DESIGNATIONS ARE FOR GRADATIONS ONLY. THE STONE MUST ALSO BE CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR NO. 4 (AASHTO M43) STONE".

STORMTECH COMPACTION REQUIREMENTS ARE MET FOR 'A' LOCATION MATERIALS WHEN PLACED AND COMPACTED IN 9" (230 mm) (MAX) LIFTS USING TWO FULL COVERAGES WITH A VIBRATORY COMPACTOR. 2

WHERE INFILTRATION SURFACES MAY BE COMPROMISED BY COMPACTION, FOR STANDARD DESIGN LOAD CONDITIONS, A FLAT SURFACE MAY BE ACHIEVED BY RAKING OR DRAGGING WITHOUT COMPACTION EQUIPMENT. FOR SPECIAL LOAD DESIGNS, CONTACT STORMTECH FOR 3 COMPACTION REQUIREMENTS.

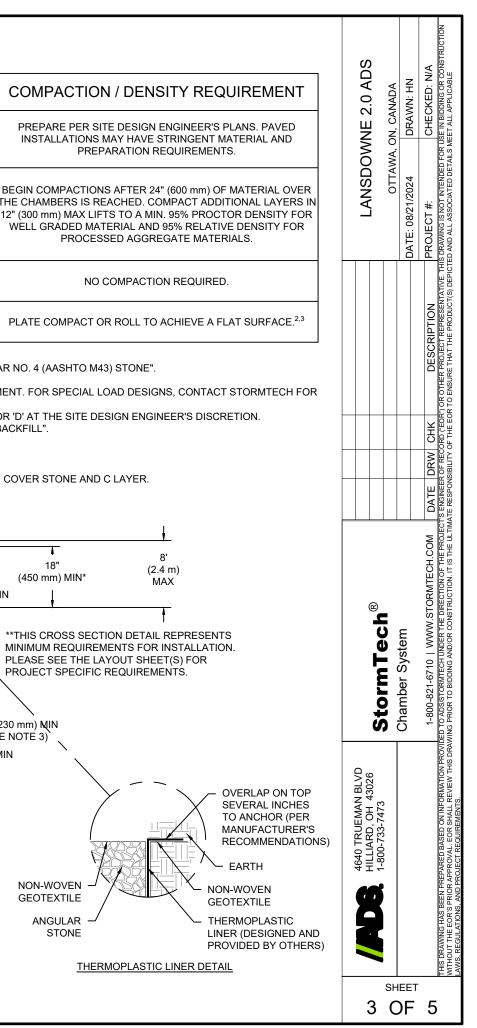
ONCE LAYER 'C' IS PLACED, ANY SOIL/MATERIAL CAN BE PLACED IN LAYER 'D' UP TO THE FINISHED GRADE. MOST PAVEMENT SUBBASE SOILS CAN BE USED TO REPLACE THE MATERIAL REQUIREMENTS OF LAYER 'C' OR 'D' AT THE SITE DESIGN ENGINEER'S DISCRETION

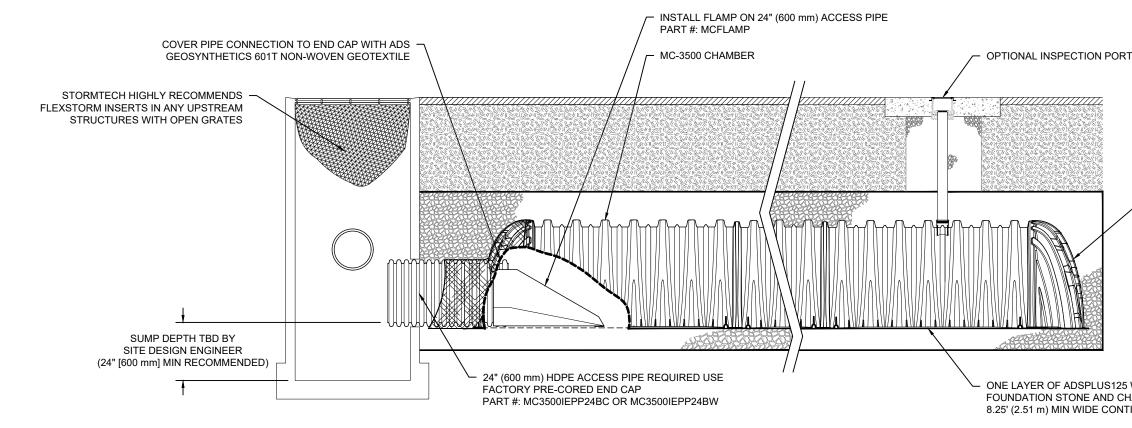
WHERE RECYCLED CONCRETE AGGREGATE IS USED IN LAYERS 'A' OR 'B' THE MATERIAL SHOULD ALSO MEET THE ACCEPTABILITY CRITERIA OUTLINED IN TECHNICAL NOTE 6.20 "RECYCLED CONCRETE STRUCTURAL BACKFILL".



NOTES:

- CHAMBERS SHALL MEET THE REQUIREMENTS OF ASTM F2418, "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS" CHAMBER CLASSIFICATION 45x76 1. DESIGNATION SS
- 2. MC-3500 CHAMBERS SHALL BE DESIGNED IN ACCORDANCE WITH ASTM F2787 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS"
- 3 THE SITE DESIGN ENGINEER IS RESPONSIBLE FOR ASSESSING THE BEARING RESISTANCE (ALLOWABLE BEARING CAPACITY) OF THE SUBGRADE SOILS AND THE DEPTH OF FOUNDATION STONE WITH CONSIDERATION FOR THE RANGE OF EXPECTED SOIL MOISTURE CONDITIONS. REFERENCE STORMTECH DESIGN MANUAL FOR BEARING CAPACITY GUIDANCE.
- 4. PERIMETER STONE MUST BE EXTENDED HORIZONTALLY TO THE EXCAVATION WALL FOR BOTH VERTICAL AND SLOPED EXCAVATION WALLS.
- 5. REQUIREMENTS FOR HANDLING AND INSTALLATION:
 - TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING, CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS.
 - TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL, THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 3".
 - TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION, a) THE ARCH STIFFNESS CONSTANT SHALL BE GREATER THAN OR EQUAL TO 450 LBS/FT/%. THE ASC IS DEFINED IN SECTION 6.2.8 OF ASTM F2418. AND b) TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES (ABOVE 73° F / 23° C), CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS.





MC-3500 ISOLATOR ROW PLUS DETAIL

NTS

INSPECTION & MAINTENANCE

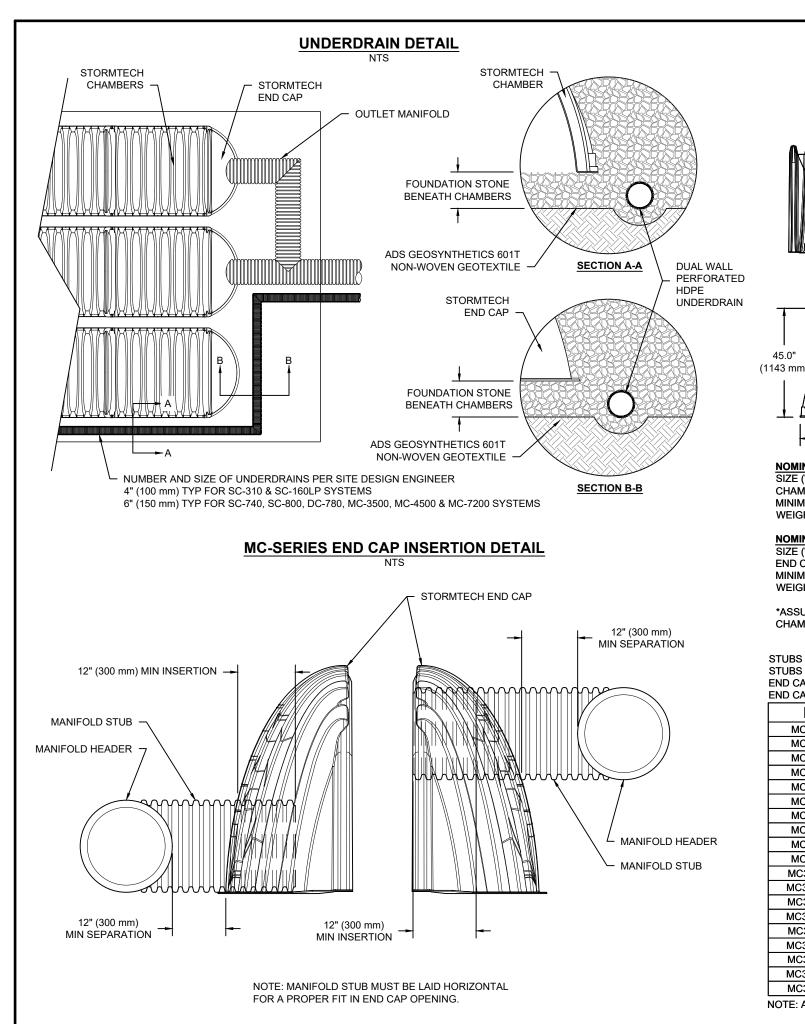
STEP 1) INSPECT ISOLATOR ROW PLUS FOR SEDIMENT

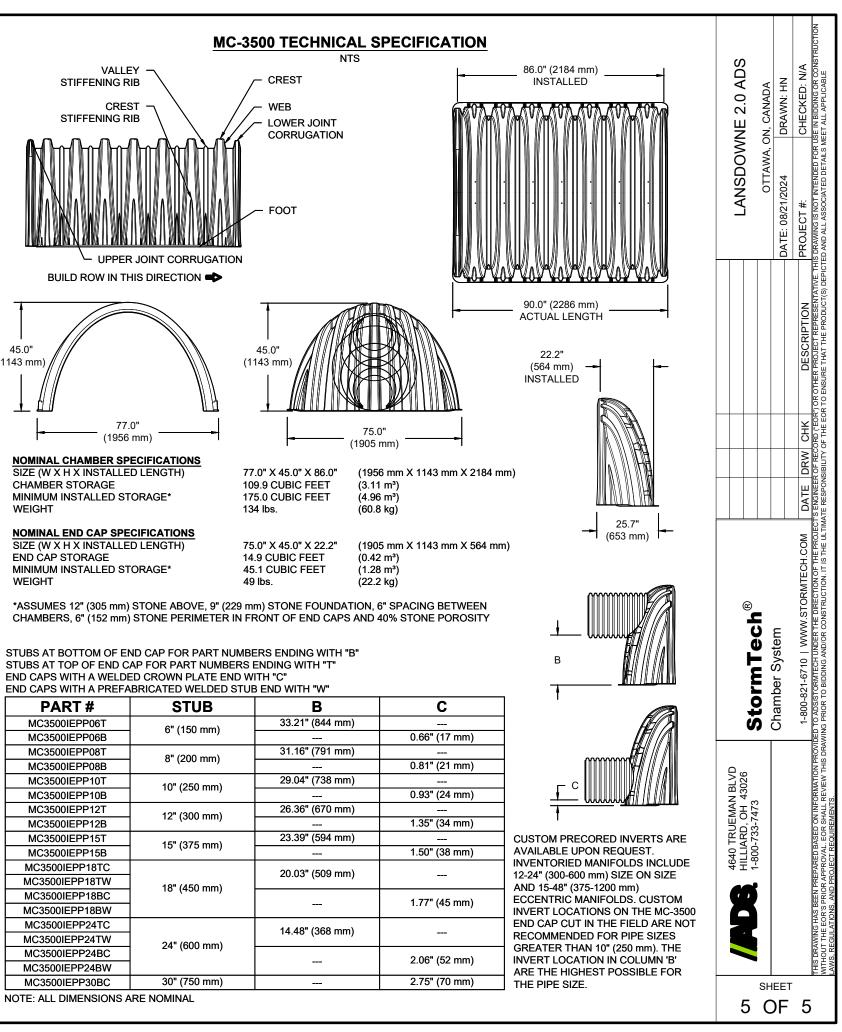
- A. INSPECTION PORTS (IF PRESENT)
 - A.1. REMOVE/OPEN LID ON NYLOPLAST INLINE DRAIN
 - REMOVE AND CLEAN FLEXSTORM FILTER IF INSTALLED A.2.
 - USING A FLASHLIGHT AND STADIA ROD, MEASURE DEPTH OF SEDIMENT AND RECORD ON MAINTENANCE LOG LOWER A CAMERA INTO ISOLATOR ROW PLUS FOR VISUAL INSPECTION OF SEDIMENT LEVELS (OPTIONAL) A.3.
 - A.4.
 - A.5. IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2, IF NOT, PROCEED TO STEP 3.
- B. ALL ISOLATOR PLUS ROWS
- B.1. REMOVE COVER FROM STRUCTURE AT UPSTREAM END OF ISOLATOR ROW PLUS
- USING A FLASHLIGHT, INSPECT DOWN THE ISOLATOR ROW PLUS THROUGH OUTLET PIPE B.2.
- i) MIRRORS ON POLES OR CAMERAS MAY BE USED TO AVOID A CONFINED SPACE ENTRY
- ii) FOLLOW OSHA REGULATIONS FOR CONFINED SPACE ENTRY IF ENTERING MANHOLE
- IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3. B.3.
- CLEAN OUT ISOLATOR ROW PLUS USING THE JETVAC PROCESS STEP 2)
 - A. A FIXED CULVERT CLEANING NOZZLE WITH REAR FACING SPREAD OF 45" (1.1 m) OR MORE IS PREFERRED
 - APPLY MULTIPLE PASSES OF JETVAC UNTIL BACKFLUSH WATER IS CLEAN Β.
 - C. VACUUM STRUCTURE SUMP AS REQUIRED
- REPLACE ALL COVERS, GRATES, FILTERS, AND LIDS; RECORD OBSERVATIONS AND ACTIONS. STEP 3)
- STEP 4) INSPECT AND CLEAN BASINS AND MANHOLES UPSTREAM OF THE STORMTECH SYSTEM.

NOTES

- INSPECT EVERY 6 MONTHS DURING THE FIRST YEAR OF OPERATION. ADJUST THE INSPECTION INTERVAL BASED ON PREVIOUS 1. OBSERVATIONS OF SEDIMENT ACCUMULATION AND HIGH WATER ELEVATIONS.
- 2. CONDUCT JETTING AND VACTORING ANNUALLY OR WHEN INSPECTION SHOWS THAT MAINTENANCE IS NECESSARY.

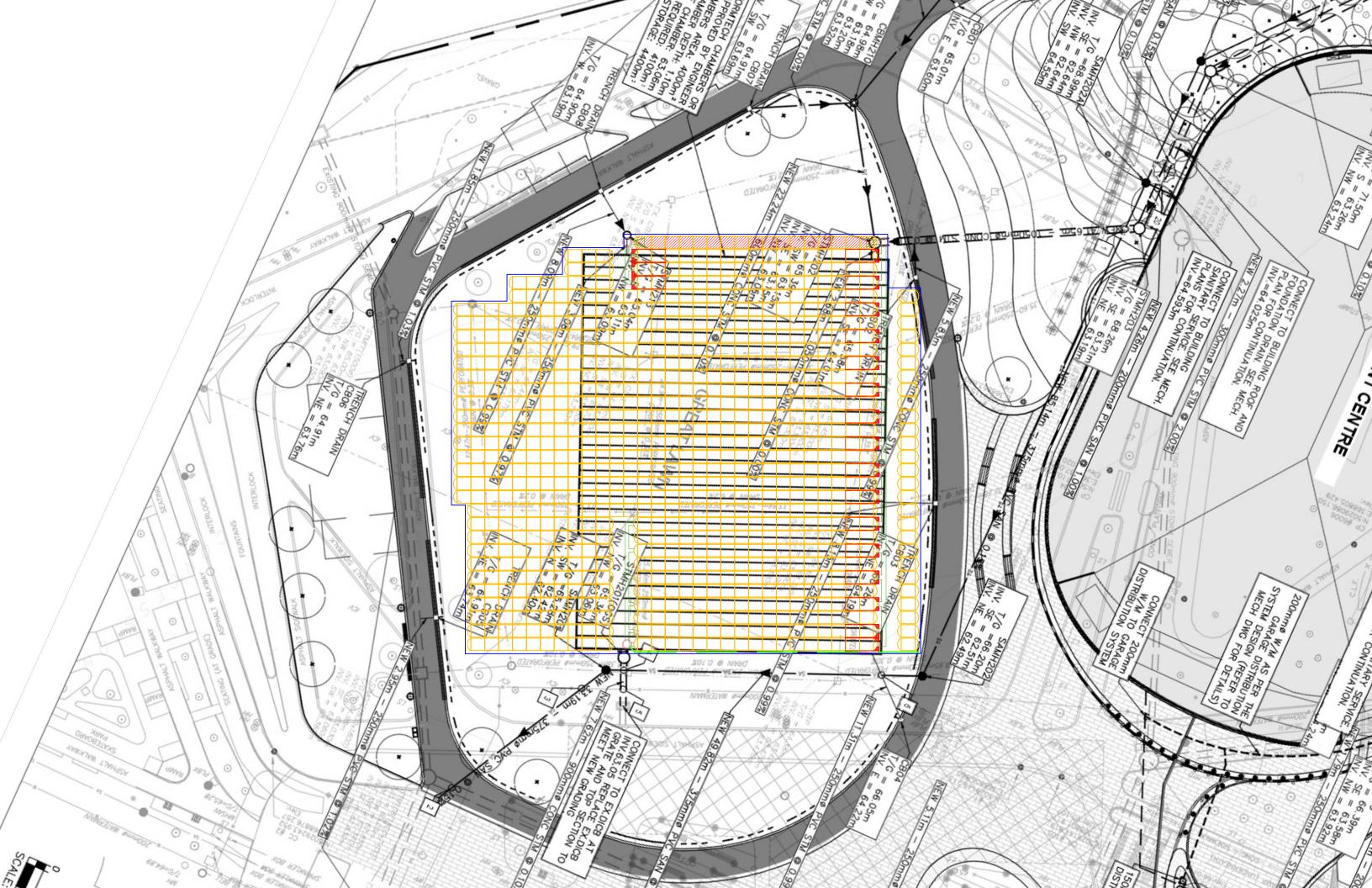
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Т	LANSDOWNE 2.0 ADS		, OIN, CAINADA	DRAWN: HN	CHECKED: N/A
MC-3500 END CAP	LANSDOV			DATE: 08/21/2024	PROJECT #: THIS DRAWING IS NOT INTENDED FOR
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		StormTech	Chamber System		1-800-821-6710 WWW.STORMTECH.COM DATE DRW CHK DESCRIPTION PROJECT #: CHECKED: N/A DESCRIPTION PROJECT #: CHECKED: N/A DESCRIPTION PROJECT PR
	HILLIARD, OH 43026	-			NG HAS BEEN PREPARED BASED ON INFORMATION PF
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STUBS AT TOP OF END CAP FOR PART NUMBERS ENDING WITH "T" END CAPS WITH A WELDED CROWN PLATE END WITH "C" END CAPS WITH A PREFABRICATED WELDED STUB END WITH "W"

PART #	STUB	В	
MC3500IEPP06T	6" (150 mm)	33.21" (844 mm)	
MC3500IEPP06B			0.66
MC3500IEPP08T	8" (200 mm)	31.16" (791 mm)	
MC3500IEPP08B	0 (200 mm)		0.81
MC3500IEPP10T	10" (250 mm)	29.04" (738 mm)	
MC3500IEPP10B			0.93
MC3500IEPP12T	12" (300 mm)	26.36" (670 mm)	
MC3500IEPP12B			1.35'
MC3500IEPP15T	15" (375 mm)	23.39" (594 mm)	
MC3500IEPP15B	13 (373 1111)		1.50
MC3500IEPP18TC		20.03" (509 mm)	
MC3500IEPP18TW	18" (450 mm)	20.03 (303 mm)	
MC3500IEPP18BC			1.77'
MC3500IEPP18BW			1.77
MC3500IEPP24TC		14.48" (368 mm)	
MC3500IEPP24TW	24" (600 mm)	14.40 (300 mm)	
MC3500IEPP24BC			2.06
MC3500IEPP24BW			2.00
MC3500IEPP30BC	30" (750 mm)		2.75
MC3500IEPP24BW	30" (750 mm)		



Project Name:	Lansdowne 2.0		
Consulting Engineer:	WSP		
Location:	Ottawa, Ontario		
Sizing Completed By:	Haider Nasrullah	Email:	haider.nasrullah@adspipe.com

Summary of Results					
Isolator Row PLUS TSS Removal:	80.1%				
FD-8HC TSS Removal:	29.0%				
Combined TSS Removal:	85.5%				
Total Volume Treated:	>90%				

Individual OGS Results					
Model	TSS Removal	Volume Treated			
FD-4HC	23.0%	>90%			
FD-5HC	25.0%	>90%			
FD-6HC	27.0%	>90%			
FD-8HC	29.0%	>90%			
FD-10HC	31.0%	>90%			

Overall System Capacities					
Total Sediment Storage Capacity:	12.37 m³				
Oil Storage Capacity:	4,239 L				
Max. OGS Pipe Diameter:	1,200 mm				
Peak OGS Flow Capacity:	1,415 L/s				
Peak Stormtech Inlet Flow Capacity:	311 L/s				
Peak IR PLUS Water Quality Flow:	323.8 L/s				

OGS Specifications					
Inlet Pipe Diameter (A):	450 mm				
Unit Diameter (B):	2,400 mm				
Outlet Pipe Diameter (C):	450 mm				
Rim Elevation (D):	100.00 m				
Bottom of Sump Elevation (E):	#N/A				
Inlet Pipe Elevation (F):	98.00 m				
Outlet Pipe Elevation (G):	98.00 m				

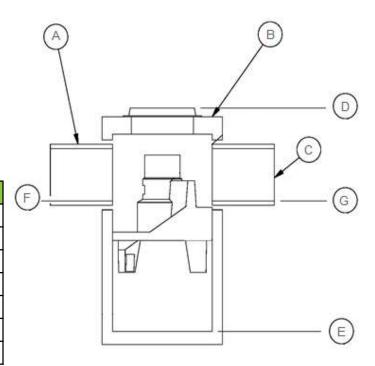
Site Details					
Site Area (ha):	6.94				
Rational C:	0.61				
Particle Size Distribution:	ETV				
Rainfall Station:	Ottawa, ONT				

Notes: OGS results based on ETV PSD and results from ETV testing protocols.

Stormtech Details					
Chamber Model:	MC-7200				
No. Chambers in Isolator Row PLUS:	25				
Volume Treated by Isolator Row PLUS:	98.6%				

Notes: Refer to Stormtech drawings for full IR+ configuration.

Isolator Row PLUS must include Flared End Ramp (FLAMP) for proper performance.



Notes:

Isolator Row PLUS removal efficiency based on verified ETV test report. For dimensions and configuration of Isolator Row PLUS, please see Stormtech drawing package.



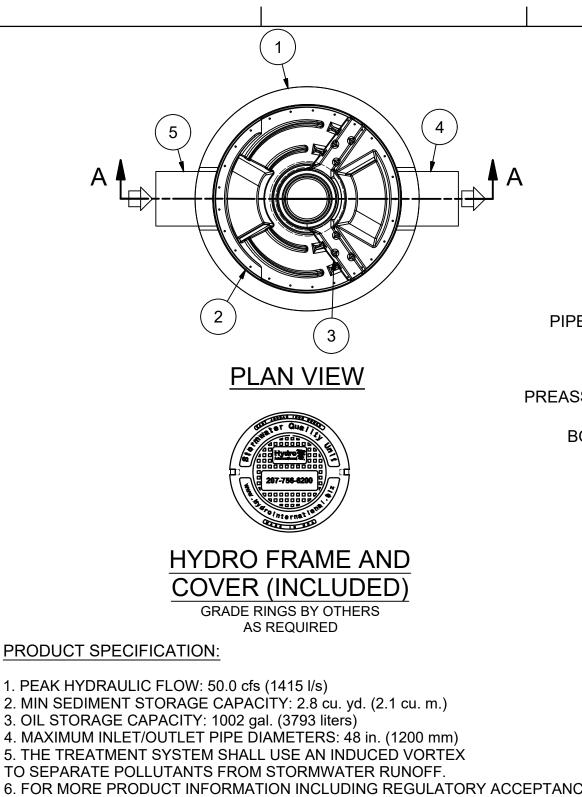
Lansdowne 2.0 WSP Ottawa, Ontario

Net Annual Removal Efficiency Summary

Rainfall Intensity	Fraction of	Removal	Efficiency	Combined	Combined Weighted
	Rainfall	FD-8HC	IR PLUS ⁽²⁾	Removal Efficiency	Removal Efficiency
mm/hr	%	%	%	%	%
0.50	0.1%	60.0%	81.2%	92.5%	0.1%
1.00	14.1%	55.0%	81.2%	91.5%	12.9%
1.50	14.2%	52.1%	81.2%	91.0%	12.9%
2.00	14.1%	50.0%	81.2%	90.6%	12.8%
2.50	4.2%	48.4%	81.2%	90.3%	3.8%
3.00	1.5%	47.1%	81.2%	90.1%	1.3%
3.50	8.5%	46.0%	81.2%	89.8%	7.7%
4.00	5.4%	0.0%	81.2%	81.2%	4.4%
4.50	1.2%	0.0%	81.2%	81.2%	0.9%
5.00	5.5%	0.0%	81.2%	81.2%	4.5%
6.00	4.3%	0.0%	81.2%	81.2%	3.5%
7.00	4.5%	0.0%	81.2%	81.2%	3.7%
8.00	3.1%	0.0%	81.2%	81.2%	2.5%
9.00	2.3%	0.0%	81.2%	81.2%	1.9%
10.00	2.6%	0.0%	81.2%	81.2%	2.1%
20.00	9.2%	0.0%	81.2%	81.2%	7.5%
30.00	2.6%	0.0%	74.5%	74.5%	2.0%
40.00	1.2%	0.0%	55.9%	55.9%	0.7%
50.00	0.5%	0.0%	44.7%	44.7%	0.2%
100.00	0.7%	0.0%	22.4%	22.4%	0.2%
150.00	0.1%	0.0%	14.9%	14.9%	0.0%
200.00	0.0%	0.0%	11.2%	11.2%	0.0%
		Total N	let Annual Ren	l noval Efficiency	85.5%
		Total Runoff Volume Treated			>90%

Notes:

- (1) Rainfall Data: 1960:2007, HLY03, Ottawa, ONT, 6105976 & 6105978.
- (2) IR PLUS removal based on ETV PSD and ETV protocols.
- (3) Rainfall adjusted to 5 min peak intensity based on hourly average.
- (4) Combined removal efficiencies calculated based on NCDENR Stormwater BMP Manual, Section 3.9.4, where Total Removal Efficiency = 1st BMP Efficiency + 2nd BMP Efficiency - (1st BMP Efficiency x 2nd BMP Efficiency)



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1. PEAK HYDRAULIC FLOW: 50.0 cfs (1415 l/s) 2. MIN SEDIMENT STORAGE CAPACITY: 2.8 cu. yd. (2.1 cu. m.) 3. OIL STORAGE CAPACITY: 1002 gal. (3793 liters) 4. MAXIMUM INLET/OUTLET PIPE DIAMETERS: 48 in. (1200 mm) 5. THE TREATMENT SYSTEM SHALL USE AN INDUCED VORTEX TO SEPARATE POLLUTANTS FROM STORMWATER RUNOFF. 6. FOR MORE PRODUCT INFORMATION INCLUDING REGULATORY ACCEPTA https://hydro-int.com/en/products/first-defense **GENERAL NOTES:**

1. General Arrangement drawings only. Contact Hydro International for site specific

2. The diameter of the inlet and outlet pipes may be no more than 48".

3. Multiple inlet pipes possible (refer to project plan).

4. Inlet/outlet pipe angle can vary to align with drainage network (refer to project pla

5. Peak flow rate and minimum height limited by available cover and pipe diameter

6. Larger sediment storage capacity may be provided with a deeper sump depth.

ANY WARRANTY GIVEN BY HYDRO INTERNATIONAL WILL APPLY ONLY TO THOSE ITEMS SUPPLIED BY IT. ACCORDINGLY HYDRO INTERNATIONAL PARTY. HYDRO INTERNATIONAL HAVE A POLICY OF CONTINUOUS DEVELOPMENT AND RESERVE THE RIGHT TO AMEND THE SPECIFICATION SPECIFICATION. HYDRO INTERNATIONAL OWNS THE COPYRIGHT OF THIS DRAWING, WHICH IS SUPPLIED IN CONFIDENCE. IT MUST NOT BE INTERNATIONAL

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