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**141 George Street**

**Servicing and Stormwater Management Report**



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**141 George Street**  
**City of Ottawa**  
**Servicing and Stormwater Management Report**

Prepared By:

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September 24<sup>th</sup>, 2024

Novatech File: 112142  
Ref: R-2023-103



September 24, 2024

City of Ottawa  
Planning, Infrastructure and Economic Development Department  
Planning and Infrastructure Approvals Branch  
110 Laurier Avenue West, 4<sup>th</sup> Floor  
Ottawa ON, K1P 1J1

**Attention: Vincent Duquette, Infrastructure Project Manager**

**Reference: 141 George Street  
Servicing and Stormwater Management Report  
Our File No.: 112142**

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Please find enclosed the 'Servicing and Stormwater Management Report' for the above noted development located in the City of Ottawa. This report is being submitted in support of a revised site plan application for 141 George to include the complete underground parking structure between York Street and George Street. The above grade building for 110 York and 116 York will be submitted under separate applications (OPA, Zoning and Site Plan).

Should you have any questions or require additional information, please contact the undersigned.

Yours truly,

**NOVATECH**



Greg MacDonald, P. Eng.  
Director, Land Development and Public Sector Infrastructure



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## 1.0 INTRODUCTION

Novatech has been retained to prepare a Servicing and Stormwater Management Report for the proposed site plan located at 141 George Street within the City of Ottawa. The purpose of this report is to support a revised site plan application for 141 George to include the complete underground parking structure between York Street and George Street. The above grade building for 110-116 York will be submitted under separate applications (OPA, Zoning and Site Plan). **Figure 1** Key Plan shows the site location.

### 1.1 Existing Conditions

The subject site is generally bound by York Street to the north, George Street to the south, the Andaz Hotel to the west and 118 York Street to the east. The total area comprises of approximately 0.44 hectares.

Presently the site contains the existing Whiskey Bar, addressed 112 York Street, along the York Street frontage. The remainder of the site presently consists of an aboveground asphalt parking area, with access to Dalhousie and George Street.

The site primarily drains from the south to the north with a +/- 1.56m grade differential across the site. **Figure 2** shows the existing site conditions.

Previous and relevant reports pertaining to the development of this site include:

#### **110 York and 141 George Street Serviceability Memo, by Novatech dated March 12, 2024**

This memo assessed the serviceability of the development based on a concept which included the following:

- 141 George with 295 residential units and 679 m<sup>2</sup> of commercial area
- 110 York Street with 106 hotel rooms and 793 m<sup>2</sup> of commercial space

#### **Residential / Hotel Development 141 George Street/ 325 Dalhousie Street/110 York Street, Ottawa, Ontario, Servicing Design Brief', by Novatech Engineering dated April 12, 2018**

This memo assessed the serviceability of the development based on a concept which included the following:

- 141 George with 282 residential units and 1097 m<sup>2</sup> of commercial area
- 110 York Street with 128 hotel rooms with connection to the existing Andaz Hotel

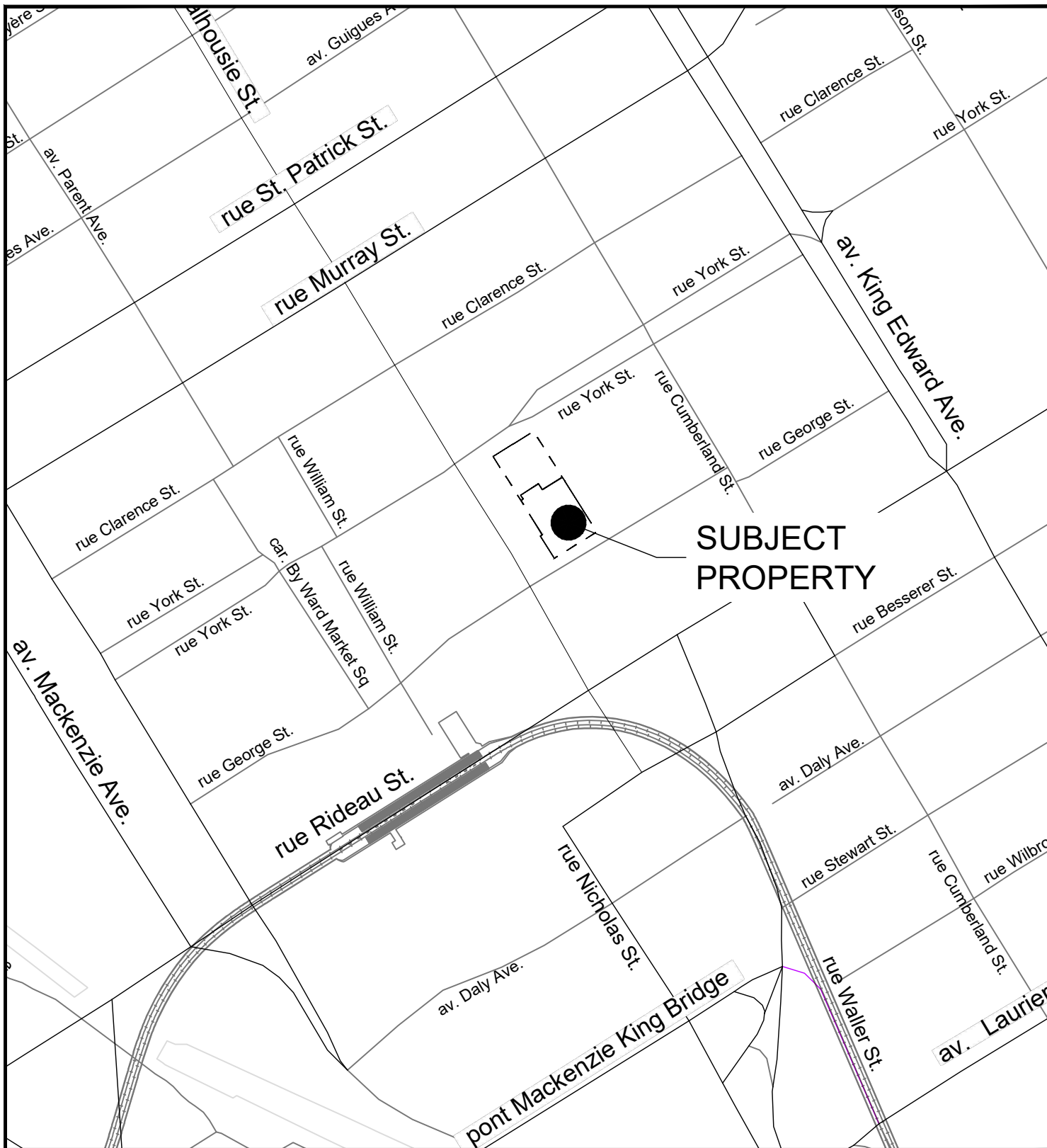
#### **Residential / Hotel Development 141 George Street/ 325 Dalhousie Street/, Ottawa, Ontario, Servicing Design Brief (Incl. Interim Condition) by Novatech dated February 14, 2014**

This memo assessed the serviceability of the development based on a concept which included the following:

- 141 George with 282 residential units and 1079 m<sup>2</sup> of commercial area



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CITY OF OTTAWA  
141 GEORGE STREET

## KEY PLAN

SCALE

N.T.S

DATE

SEPT 2024

JOB

112142

FIGURE

FIGURE 1



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LEGEND

----- SITE BOUNDARY



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CITY OF OTTAWA  
141 GEORGE STREET

EXISTING CONDITIONS

SCALE 1 : 1000 0 10 20 30 40

DATE SEPT 2024 JOB 112142 FIGURE 2



- 325 Dalhousie Street (current Andaz Hotel) with 187 hotel rooms and 292m<sup>2</sup> of commercial space

Site plan approval for the 141 George Street was received based on a 22-storey building with 295 residential units, 679m<sup>2</sup> of commercial area and 288 underground parking spaces on 4 levels of parking within the 141 George Street property.

## 1.2 Proposed Development

This report is submitted in support of a revised site plan application for the approved 141 George Street project. Plans are to build-out the complete underground parking for both 141 George Street and 110 – 116 York Street. The above grade building at 110-116 York Street will be subject to future development applications (OPA, Zoning and Site Plan) and will not be built at this time. However, proposed services for the building will be assessed and extended to the building and capped for future connection.

The proposed development at 141 George Street will change slightly as follows;

- 297 residential units and 525 m<sup>2</sup> of commercial area

The proposed future 110-116 York Building will consist of 154 hotel rooms and 1400 m<sup>2</sup> of commercial space connected to the existing Andaz Hotel.

Access to the proposed underground parking structure will be provided from George Street and Dalhousie Street. The proposed parking structure will have three (3) levels of parking beneath the development of 141 George and 110-116 York. An access will be provided off Dalhousie Street. Once the site plan is approved for 110-116 York Street the entire parking garage will have access from both Dalhousie Street and 141 George Street.

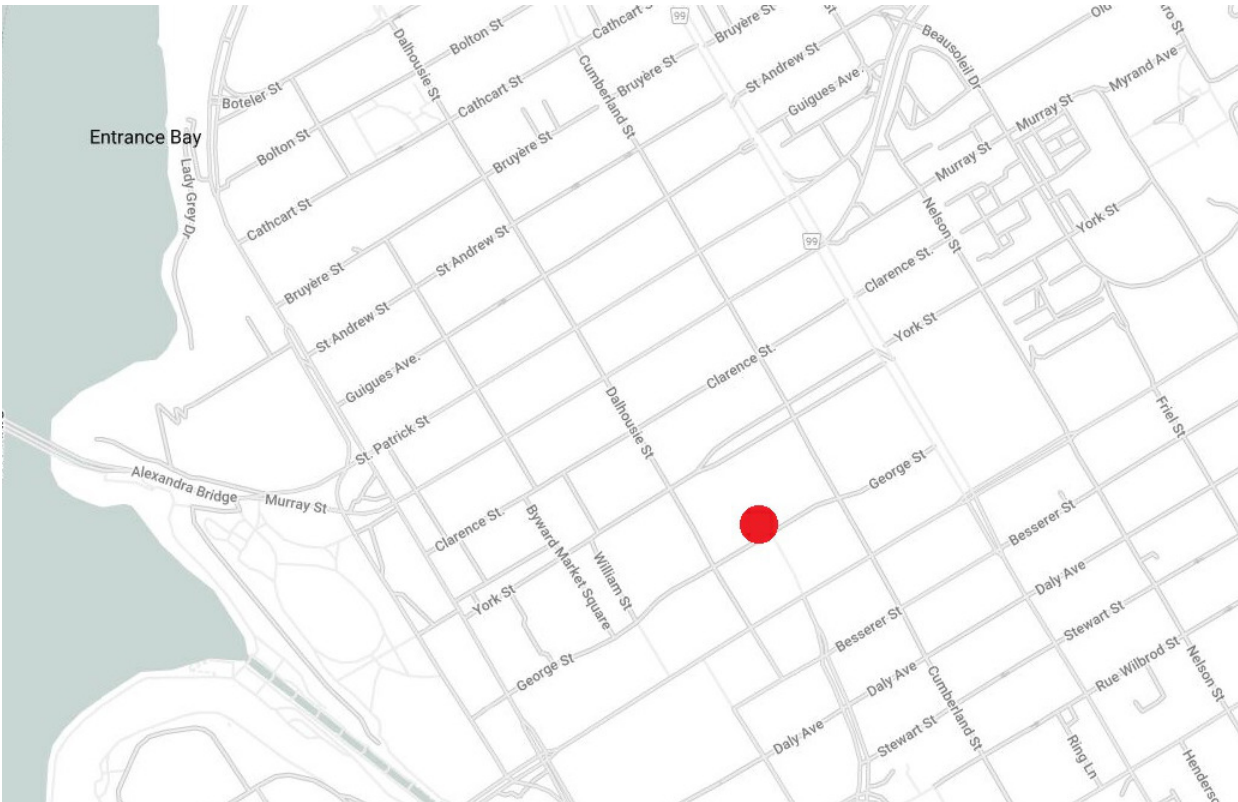
**Figure 3** shows the site plan for the proposed development.

## 2.0 GEOTECHNICAL INVESTIGATION

A geotechnical investigation was completed for the development, and a report prepared entitled 'Geotechnical Investigation', Proposed High-Rise Building, 141 George Street, Ottawa, Ontario prepared by Paterson Group Inc. dated March 20, 2023 (PG2733-3.). The following is a summary of the findings of the report:

- The long-term groundwater table can be expected at a depth of approximately 2.5 to 4.5 m throughout the subject site. It should be noted that groundwater levels are subject to seasonal fluctuations. Therefore, the groundwater levels could vary at the time of construction.
- Practical auger refusal was encountered on the bedrock surface at approximate depths ranging from 3.5 to 5.6 m. Based on the recovered rock core samples, the bedrock was observed to consist of grey limestone, which is poor to good in quality in the upper 1 to 1.5 m, generally becoming excellent in quality with depth.
- Existing foundation walls and other construction debris should be entirely removed from within the building perimeter and within the lateral support zones of the foundation. Under paved areas, existing construction remnants, such as foundation walls, should be excavated to a minimum of 1 m below final grade.





- NOTES
- FOR EXISTING SITE CONDITIONS. SEE SURVEY PLAN BY ANNIS, OSULLIVAN, VOLLEBEKK LTD. SUBMITTED SEPERATELY.
  - FOR NEW GRADES AND SITE SERVICES. SEE CIVIL ENGINEERING PLANS BY NOVATECH ENGINEERING CONSULTANTS, SUBMITTED SEPERATELY.
  - ZONING GFA INCLUDES AREA MEASURED FROM THE INTERIOR FACE OF EXTERIOR WALLS TO THE EXTERIOR FACE OF PARTY WALLS SEPARATING DIFFERENT USES, AS DEFINED IN CITY OF OTTAWA ZONING BY-LAW DEFINITION (2008-250).

OCCUPANCY	UNITS / STOREYS	PROPOSED ZONING GFA
Residential (Rental)	297 units / Ground to 21st floors	Ground = 1 caretaker unit = 93.9m <sup>2</sup> (excluded) 2 <sup>nd</sup> = 16 unit = 949m <sup>2</sup> 3 <sup>rd</sup> = 16 unit = 946m <sup>2</sup> 4 <sup>th</sup> - 11 <sup>th</sup> = 15 units/floor = 934m <sup>2</sup> / floor 12 <sup>th</sup> = 15 units = 932m <sup>2</sup> 13 <sup>th</sup> - 17 <sup>th</sup> = 15 units/floor = 934m <sup>2</sup> / floor 18 <sup>th</sup> = 14 units = 876m <sup>2</sup> 19 <sup>th</sup> & 20 <sup>th</sup> = 14 units = 851m <sup>2</sup> 21 <sup>st</sup> = 12 units = 772m <sup>2</sup>  TOTAL = 18,309m <sup>2</sup> (without Ground)
	Minimum 15% (44 units) required to be Barrier-Free (BF) to be distributed throughout residential storeys.	8 x Studios (18F units = 15%) 191 x 1 Bedroom (318F units = 16%) 98 x 2 Bedroom (158F units = 15%)  478F units = 15%
Commercial	Ground	Commercial = 453m <sup>2</sup> Office = 72m <sup>2</sup>
TOTAL		18,834m <sup>2</sup>

MIXED-USE WITH GROUND FLOOR COMMERCIAL - ZONING - MD2 (2031) S307		
ZONING RULE	REQUIREMENT	PROVIDED
Minimum lot area	No minimum	3,109.10m <sup>2</sup>
Minimum lot width	No minimum	42.45m on George Street. 40.40 on back portion.
Minimum front yard	No minimum, 1m maximum.	0.72m on George Street
Minimum interior side yard	No minimum	0.70m on West side of building. 1.94m on East side of building.
Minimum rear yard	No minimum	6.29m to one storey volume. 5.47m to 4th to 17th floor overhang.
Maximum building height	70m as per Schedule 307. No projections permitted beyond building height.	70m all inclusive.
Maximum floor space index	Not applicable	Not applicable
Minimum width of landscape area	No minimum except that where a yard is provided and not used for required driveways, aisles, parking, loading spaces, or outdoor commercial patio, the whole yard must be landscaped	Whole yard to be landscaped.
Provisions for buildings 10 storeys and higher (By-law 2019-353)	Minimum lot area for an interior lot: 1350m <sup>2</sup>  Minimum interior side and rear yard setback for a tower: 7.5m  Minimum separation distance between towers on the same lot: 15m.	Minimum lot area met.  Site Plan Approval received.  Not applicable.
Parking Garage permission	100% of ground floor fronting a street (excluding mechanical room, pedestrian and vehicular access) for a minimum depth of 3m, must be occupied by permitted use..	100% of ground fronting George Street for a minimum depth of 3m, is occupied by permitted Commercial use and Office use.
Ground floor use	100% of ground floor fronting a street (excluding lobby area, mechanical room and access to other floors) for a minimum depth of 3m, must be occupied by select uses.  Total gross area of lobbies, mechanical rooms and access to other floors must not exceed 50% of ground floor gross area.  Min. 50% of ground floor to be occupied by permitted use subject to a separate and direct access to abutting street.	100% of ground fronting George Street for a minimum depth of 3m, is occupied by permitted Commercial use.  Total gross area of lobbies, mechanical rooms and access to other floors does not exceed 50% of ground floor gross area.  Area of permitted Commercial use exceeds 50% of gross floor area and has separate direct access to George Street.

AMENITY AND PARKING REQUIREMENTS ZONING - MD2 (2031) S307 (COMBINED WITH 110 YORK STREET)		
ZONING MECHANISM	REGULATION	PROPOSED
Residential Parking	None Required 6m drive aisle required.	P2 31 spaces P3 12 spaces 6.0m drive aisle provided.
Visitor Parking (6m drive aisle)	Residential Area Z (By-law 2016-249): no more than 30 visitor spaces are required per building. Exception #2031: 0.063 spaces x 297 units = 25 visitor parking spaces 6m drive aisle required.	P3 25 spaces 6.0m drive aisle provided.
Commercial Parking	None Required 6.7m drive aisle required.	P2 5 spaces 6.0m drive aisle provided.
Hotel Parking	None Required 6m drive aisle required.	P1 26 spaces 6.0m drive aisle provided.
Barrier-Free Parking	Requires 1 barrier-free spaces (Traffic and Parking By-Law 2017-301)	Total: 99 spaces P2 1 space P3 1 space Total 2 barrier-free spaces
Minimum bicycle parking	Residential: 0.5 spaces x 297 units = 149 bicycle parking spaces Retail: 1 space per 250m <sup>2</sup> of GFA 460m <sup>2</sup> GFA / 250m <sup>2</sup> = 2 bicycle parking spaces Minimum 50% to be horizontal racks.	Residential: 86 (P1) (Indoor) 36 (P2) 37 (P3) Retail: 5 (Exterior) Total: 179 bicycle spaces 75 (42%) vertical mount.
Maximum parking	1.5 per dwelling unit. Limited to 446 space for 297 units. (combined with visitor) 1 per 100m <sup>2</sup> of Commercial gross area. Limited to 5 spaces.	Total parking spaces is under the limit. Commercial parking spaces maximized.
Minimum driveway width	6m	6m
Minimum aisle width	6m	6m
Loading	Exception #2031: None Required.	NA
Amenities Areas	Amenity Area - 6m <sup>2</sup> per unit = 297 units x 6m <sup>2</sup> = 1,782m <sup>2</sup> Communal Amenity Area : Exception #2031: minimum 40% off the required Total Amenity Area = 1,782m <sup>2</sup> x 0.4 = minimum 713m <sup>2</sup> Layout of Communal Amenity Area - aggregated into areas up to 54m <sup>2</sup>	Combined Balcony Areas = 1,734m <sup>2</sup> Ground = 7m <sup>2</sup> 2nd = 110m <sup>2</sup> 3rd = 113m <sup>2</sup> 4th = 95m <sup>2</sup> 5th to 17th = 82m <sup>2</sup> / floor 18th = 80m <sup>2</sup> 19th = 97m <sup>2</sup> 20th = 84m <sup>2</sup> 21st = 82m <sup>2</sup>  Combined Communal Areas = 773m <sup>2</sup> Ground floor = 432m <sup>2</sup> 22nd = 341m <sup>2</sup> Total = 2,507m <sup>2</sup>

SOLID WASTE COLLECTION REQUIREMENTS		
ZONING MECHANISM	REGULATION	PROPOSED
Residential Waste	Garbage (Compacted) = 0.053y <sup>3</sup> /unit Require 16y <sup>3</sup> Recycling (GMP) = 0.018y <sup>3</sup> /unit Require 5y <sup>3</sup> Recycling (Fibres) = 0.038y <sup>3</sup> /unit Require 12y <sup>3</sup> Organics = 240L container/50 units Require 5 containers	Garbage (Compacted) = 6 x 3y <sup>3</sup> containers Total = 18y <sup>3</sup> Recycling (GMP) = 2 x 3y <sup>3</sup> containers Total = 6y <sup>3</sup> Recycling (Fibres) = 4 x 3y <sup>3</sup> containers Total = 12y <sup>3</sup> Organics = 7 x 240L containers Total = 1680L

- GENERAL NOTES
- These architectural documents are the exclusive property of NEUF architect(e)s inc. and cannot be used, copied, or reproduced without written pre-authorisation.
  - The contractor is responsible for checking and verifying all dimensions with respect to the project. Any discrepancy shall be reported to the architect.
  - The architect must be notified of all errors, omissions, and discrepancies between these documents and those of the other professionals.
  - Do not scale drawings. The dimensions on these documents must be read and not measured.
  - These drawings are to be read in conjunction with all material relevant to the project.

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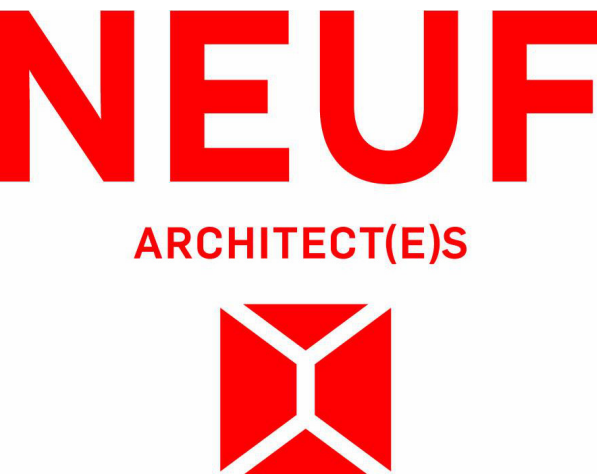
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Seal



Project  
**141 GEORGE STREET**

Location  
**OTTAWA**

No.  
**12810**

NO	REVISION	DATE (yyyy.mm.dd)
Y	FOR COORDINATION	2023.10.02
DD	FOR COORDINATION	2023.11.02
FF	FOR COORDINATION	2023.11.13
JJ	FOR COORDINATION	2023.11.27
KK	FOR COORDINATION	2023.12.04
LL	FOR COORDINATION	2023.12.15
MM	FOR PERMIT	2023.12.21
OO	FOR COORDINATION	2024.01.23
PP	FOR COORDINATION	2024.02.28
VV	RE-ISSUED FOR PERMIT	2024.04.16
WW	FOR COORDINATION	2024.05.02
XX	FOR COORDINATION	2024.05.09
YY	FOR COORDINATION	2024.05.14
ZZ	RE-ISSUED FOR SITE PLAN APPROVAL	2024.05.16
CCC	FOR TENDER	2024.05.23

Drawn by  
**SJ**

Checked by  
**LH**

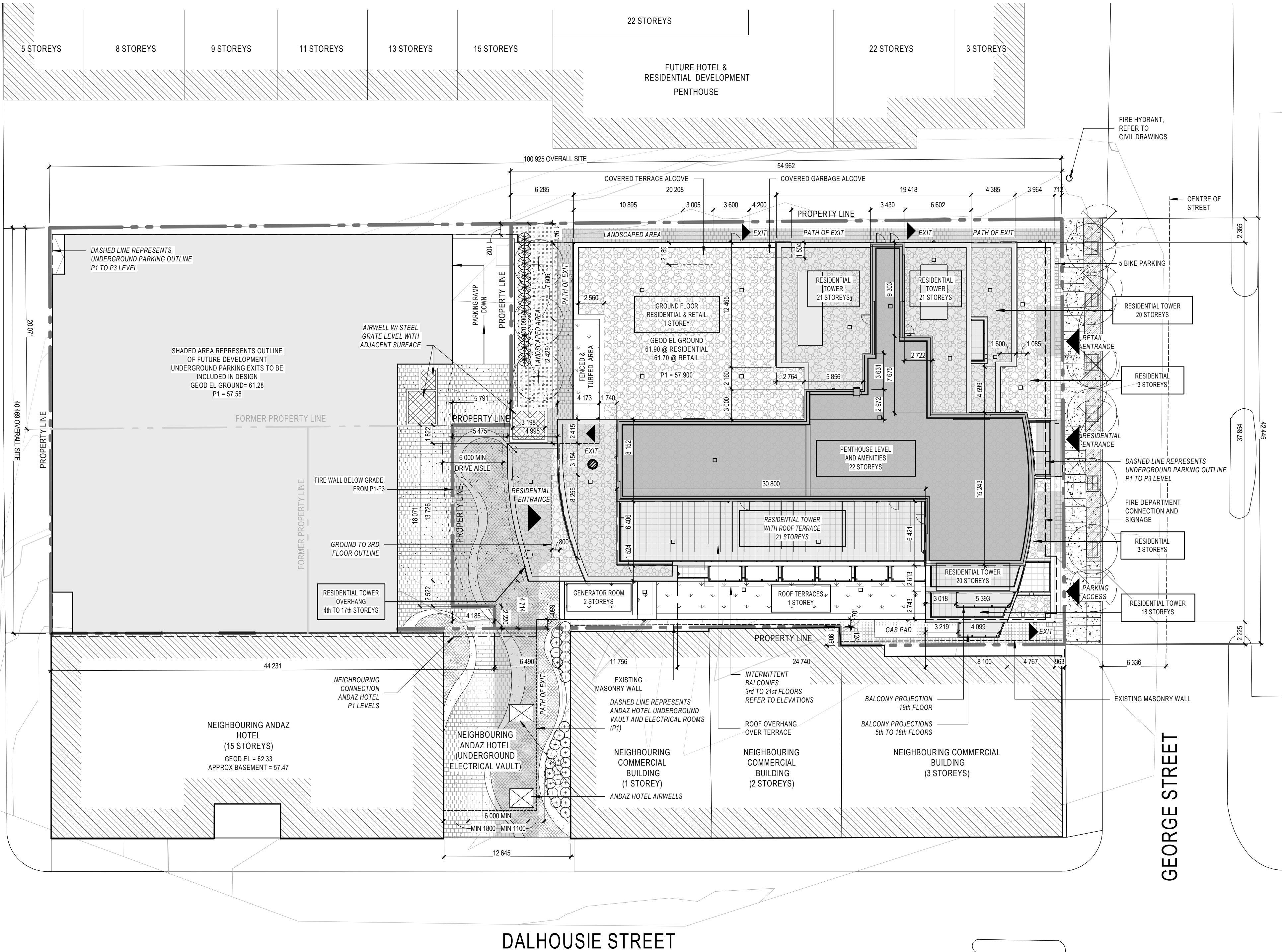
DATE (aa.mm.jj)  
**FEB 2023**

Scale  
**As indicated**

Drawing Title  
**SITE PLAN**

Revision  
**CCC**

Dwg Number  
**A100**



SITE PLAN

1 : 250

1  
A100



- The excavation side slopes above the groundwater level extending to a maximum depth of 3 m should be cut back at 1H:1V or flatter. The flatter slope is required for excavation below groundwater level. The subsurface soil is considered to be mainly a Type 2 and Type 3 soil according to the Occupational Health and Safety Act and Regulations for Construction Projects. Slopes in excess of 3 m in height should be periodically inspected by the geotechnical consultant.
- A temporary Ministry of Environment, Conservation and Parks (MECP) permit to take water (PTTW) may be required if more than 400,000 L/day of ground and/or surface water are to be pumped during the construction phase.
- For typical ground or surface water volumes being pumped during the construction phase, typically between 50,000 to 400,000 L/day, it is required to register on the Environmental Activity and Sector Registry (EASR).

### 3.0 WATER SERVICING

There are existing City watermains in all rights-of-way fronting the proposed site. There is an existing 200mm diameter (dia.) watermain within York Street, a 300mm (dia.) watermain in Dalhousie Street, and a 300mm (dia.) watermain within George Street.

Each building will have its own individual water entry, and servicing. It is proposed to service 141 George Street with two (2) individual 200mm diameter services. Two (2) services will connect to the existing 300mm diameter watermain within the George Street right-of-way. Additionally, two (2) 200mm diameter services will connect to the existing 200mm diameter watermain within the York Street right-of-way which will service the future 110-116 York Building. The proposed services will be separated by the existing isolation valves within the rights-of-way providing redundancy, as per the City of Ottawa standards.

The buildings will be sprinkled and equipped with a siamese connections located near the main entrance within 45m of a fire hydrant. Refer to the General Plan of Services drawing (112142-GP) for servicing details.

Water demand calculations have been calculated using criteria from Section 4 of the City of Ottawa Water Distribution Guidelines and the Ontario Building Code as follows:

- Average Day Demand = 280L/cap/day
- 1 Bedroom Apartment = 1.4 Persons/unit
- 2 Bedroom Apartment = 2.1 Persons/unit
- 3 Bedroom Apartment = 3.1 Persons/unit
- Office = 75L/9.3m<sup>2</sup>/day
- Bar/Cocktail Lounge = 70 L/day/seat
- Restaurant = 125 L/seat/day
- Residential Peaking Factors
  - Maximum Day = 2.5 x Avg Day
  - Peak Hour = 2.2 x Max Day
- Commercial Peaking Factors
  - Maximum Day = 1.5
- Peak Hour = 1.8



The required fire demand was calculated using the OBC and compared to Fire Underwriters Survey 2020 (FUS) Guidelines. Through correspondence with the architect, it is understood that the proposed building is residential occupancy (Limited Combustible), composed of fire resistive construction (2 hrs.), and will contain a fully supervised sprinkler system designed as per NFPA 13. The building has a podium footprint of 1720m<sup>2</sup>, and a maximum tower footprint of 350m<sup>2</sup>.

The water demand calculations, fire flow calculations and correspondence are provided in **Appendix B** for reference. A summary of the water demand and fire flows for both 141 George Street and 110-116 York Street is provided in **Table 3.1** and **Table 3.2**.

**Table 3.1: Water Demand Summary (141 George Street)**

Population	Commercial Area (m <sup>2</sup> )	Ave. Daily Demand (L/s)	Max. Daily Demand (L/s)	Peak Hour Demand (L/s)	Fire Flow (L/s)	Fire Flow (L/s) - OBC
502	670	2.03	4.68	10.04	100	150

**Table 3.2: Water Demand Summary (110-116 York Street)**

Population	Commercial Area (m <sup>2</sup> )	Ave. Daily Demand (L/s)	Max. Daily Demand (L/s)	Peak Hour Demand (L/s)	Fire Flow (L/s) - FUS	Fire Flow (L/s) - OBC
278	1420	0.94	2.31	5.07	117	150

Note as per ITSB 2018-02 the fire flow was distributed among several surrounding hydrants during modelling as outlined in **Table 3.3**.

**Table 3.3: Maximum Flow to be considered from a given hydrant.**

Hydrant Class	Distance to building (m)	Contribution to Fire Flow	
		(L/min)	(L/s)
AA	≤75	5700	95
	>75 and ≥150	3800	63.33
A	≤75	3800	63.33
	>75 and ≥150	2850	47.50
B	≤75	1900	31.67
	>75 and ≥150	1500	25.00
C	≤75	800	13.33
	>75 and ≥150	800	13.33

For the purpose of the analysis, and in light of the available pressures, it was assumed off-site hydrants would be rated as Class AA. As the fire flow is calculated as 100 L/s, two (2) hydrants will be required to achieve the required flow. There are presently 2 existing class AA hydrants



within the boulevards of George Street within 75m of the proposed building capable of providing a maximum flow of 190L/s as per **Table 3.3**. Both hydrants are within 45m of the proposed Siamese connection. Refer to **Appendix B** for calculations and the hydrant coverage figure.

Fire hydrant coverage for the proposed 110-116 York Building is shown in **Appendix B** as well.

The above water demand information for 141 George Street was submitted to the City for boundary conditions from the City's water model. These boundary conditions were used for analyzing the performance of the proposed and existing watermain systems for three theoretical conditions:

- 1) High Pressure check under Average Day conditions
- 2) Peak Hour demand
- 3) Maximum Day + Fire Flow demand.

Refer to **Table 3.4**, for a summary of the proposed boundary conditions and hydraulic analysis.

**Table 3.4: Water Boundary Conditions Response (141 George Street)**

Criteria	Head (m)	Pressure <sup>1</sup> (m)	Pressure (PSI)	Pressure Requirements
<b>Connection (George Street)</b>				
Min HGL	106.3	44.4	63.08	> 40psi
Max HGL	115.4	53.5	76.01	< 80psi
Max Day + Fire Flow	109.0	47.1	66.91	> 20psi

<sup>1</sup>Pressure based on a Finished Floor elevation of 61.90m

When the 110-116 York Street project proceeds to site plan, boundary conditions will be requested. However, it is expected that adequate pressures and flows are available in York Street for this development.

The hydraulic analysis indicates that the system can provide adequate pressures and flow to meet the domestic and fire flow requirements for the site. Refer to **Appendix B** for detailed water demand calculations, and City of Ottawa boundary conditions.

#### 4.0 SANITARY SERVICING

There are existing City sanitary sewers in all rights-of-way fronting the proposed site. There is an existing 1200mm sanitary sewer within York Street right-of-way, a 250mm sanitary sewer within Dalhousie Street right-of-way, and a 1980x1500 brick sanitary sewer (horseshoe shape) within George Street right-of-way.

It is proposed to service the George Building with a 200mm sanitary service connection to the existing 1280x1500 brick sanitary within the George Street right-of-way.

Additionally, it is proposed to service the future 110-116 York Building with a 200mm sanitary service connection to the existing 1200mm sanitary within the York Street right-of-way.



Sanitary flows for the proposed developments were calculated using criteria from Section 4 of the City of Ottawa Sewer Design Guidelines and the Ontario Building Code as follows:

- Residential Average Flow = 280 L/capita/day
- 1 Bed apartment = 1.4 Person/unit
- 2 Bed apartment = 2.1 Person/unit
- 3 Bed apartment = 3.1 Person/unit
- Professional Office flow = 75 L/9.3m<sup>3</sup>/day
- Retail Restaurant flow = 125 L/seat/day
- Bar / Cocktail Lounge flow = 70 L/seat/day (1 Seat / 2m<sup>2</sup>)
- Residential Peaking Factor = Harmon Equation (max peaking factor = 4.0)
- Commercial Peaking Factor = 1.0
- Peak Extraneous Flows (Infiltration) = 0.33L/s/ha

The peak sanitary flow including infiltration for 141 George Street was calculated to be **5.91 L/s**. Detailed sanitary flow calculations are provided in **Appendix C** for reference.

The anticipated peak sanitary flow including infiltration for 110-116 York Street was calculated to be **3.22 L/s**. Detailed sanitary flow calculations are provided in **Appendix C** for reference.

## 5.0 STORM SERVICING

There is a 675m storm sewer located within the York Street right-of-way, a 450mm storm sewer located in Dalhousie Street right of-way and a 900mm storm sewer within the George Street right-of-way fronting the proposed development.

It is proposed to service the proposed 141 George development with one (1) 250mm storm service connections to the existing 900m storm sewer within the George Street right-of-way. The storm service will convey the uncontrolled foundation drain and the controlled flows from the internal stormwater cistern within the parking garage. Through correspondence with the City it is understood that the existing 100-year HGL within George Street is at an elevation of 60.6m during the 100-yr storm event. The proposed services will be installed complete with backflow prevention as the 100-year HGL is higher than the proposed service inverts. Additionally, a test port will be provided to give access to City personnel. Refer to the General Plan of Services drawing (112142 - GP) for details.

Additionally, as part of this application it is proposed to service the proposed development with one (1) 250mm storm service connections to the existing 675m storm sewer within the York Street right-of-way. The storm service will convey the uncontrolled foundation drain and the controlled flows from the internal stormwater cistern within the parking garage. Through correspondence with the City it is understood that the existing 100-year HGL within York Street is at an elevation of approximately 60.1m during the 100-yr storm event. The proposed storm services are set to be above the frequent storm event for the foundation drain, and the cistern services, respectively. The proposed services will be installed complete with backflow prevention as the 100-year HGL is higher than the proposed service inverts. Additionally, a test port will be provided to give access to City personnel. Refer to the General Plan of Services drawing (112142 - GP) for details.



The design criteria used in sizing the storm sewers are summarized below in **Table 5.1**.

**Table 5.1: Storm Sewer Design Parameters**

Parameter	Design Criteria
Local Roads	2 Year Return Period
Storm Sewer Design	Rational Method
IDF Rainfall Data	Ottawa Sewer Design Guidelines
Initial Time of Concentration (Tc)	20 min
Allowable Runoff Coefficient (C)	0.5
Minimum Velocity	0.8 m/s
Maximum Velocity	3.0 m/s
Minimum Diameter	250 mm

Refer to **Appendix D** for detailed storm drainage area plans and storm sewer design sheets.

## **6.0 STORM DRAINAGE AND STORMWATER MANAGEMENT (141 GEORGE, 110-116 YORK)**

### **6.1 Design Criteria**

Through correspondence with the City of Ottawa, and our knowledge of development requirements in the area, the following criteria have been adopted to control post-development stormwater discharge from the site:

- Control proposed development flows, up to and including the 100-year storm event, to a 5 year allowable release rate calculated using a runoff coefficient (C) of 0.50 and a time of concentration (Tc) of 20 minutes;
- Provide source controls which are in conformity with the City of Ottawa requirements, where possible;
- Limit ponding to 0.15 m for all rooftop storage areas and 0.30 m for all parking storage areas; and
- Provide guidelines to ensure that site preparation and construction is in accordance with the current Best Management Practices for Erosion and Sediment Control.

The approach to the stormwater management design is to determine the allowable release rate for the site, calculate the uncontrolled flow, and ensure that the remaining flow, in combination with the uncontrolled flow, does not exceed the allowable release rate. All proposed development runoff in excess of the allowable release rate, will be attenuated on-site prior to being released into the storm sewers within George Street and York Street.



## 6.2 Quantity Control

The allowable release rate for the 0.438 ha site was calculated to be 42.8 L/s based on the SWM criteria provided by the City of Ottawa.

### Design Storms

The design storms are based on City of Ottawa design storms. Design storms were used for the 5-year and 100-year return periods (i.e. storm events).

### Model Parameters

Post-development catchments were modelled based on the proposed site plan and grading as shown on **Drawing 112142-SWM** within **Appendix D**. The building roofs were assumed to have no depression storage.

The site has been divided into sixteen (16) areas for the post development condition. The drainage areas are as follows:

#### **Area R-01 to R-10:**

- Stormwater from the building roof will be captured and controlled by flow control roof drains prior to releasing to the existing storm sewer servicing the development. The ponding will be limited to 0.15m in depth with overflow scuppers provided for emergencies. Storage of stormwater will be provided for storms up to and including the 100-year event. Further detailed calculations will be provided once a roof plan has been established for the 110 York development. Assumptions; 10 drains and 1 L/s of flow per drain.

#### **Area D-01:**

- Stormwater from the small area fronting George Street will flow uncontrolled to the George Street right-of-way.

#### **Area D-02:**

- Stormwater from the area North-East of the proposed building will flow uncontrolled to the George Street right-of-way.

#### **Area A-01:**

- Stormwater from the area north-west of the proposed George building to the property line fronting Dalhousie Street will be captured by an area drain to the York cistern.

#### **Area A-02:**

- Stormwater from the area north of the proposed George building, outside of the ground floor units with private access will be captured by an area drain. These flows will be conveyed through the underground parking garage by the internal mechanical plumbing to the proposed George cistern.

#### **Area A-03:**

- Stormwater from the area above parking structure within the York building ramp will be captured with a trench drain. These flows will be conveyed through the underground parking garage by the internal mechanical plumbing to the proposed York cistern.



Table **6.1 below** summarizes the flow, storage required, and storage provided for each of the site drainage areas.



Table 6.1: Post-Development Stormwater Management Summary

Area ID	Area (ha)	1:5 Year Weighted Cw	1:100 Year Weighted Cw	Control Device	Outlet Location	2 Year Storm Event				5 Year Storm Event				100 Year Storm Event			
						Release (L/s)	Ponding Depth (m)	Req'd Vol (cu.m)	Max. Vol. Provided (cu.m.)	Release (L/s)	Ponding Depth (m)	Req'd Vol (cu.m)	Max. Vol. Provided (cu.m.)	Release (L/s)	Ponding Depth (m)	Req'd Vol (cu.m)	Max. Vol. Provided (cu.m.)
D-01	0.011	0.90	1.00	N/A	George Street	2.20	N/A	N/A	N/A	2.90	N/A	N/A	N/A	5.60	N/A	N/A	N/A
D-02	0.011	0.90	1.00	N/A	George Street	2.00	N/A	N/A	N/A	2.80	N/A	N/A	N/A	5.30	N/A	N/A	N/A
R-01	0.015	0.90	1.00	Watts Roof Drain	York Street	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD
R-02	0.015	0.90	1.00	Watts Roof Drain	York Street	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD
R-03	0.015	0.90	1.00	Watts Roof Drain	York Street	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD
R-04	0.015	0.90	1.00	Watts Roof Drain	York Street	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD
R-05	0.015	0.90	1.00	Watts Roof Drain	York Street	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD
R-06	0.015	0.90	1.00	Watts Roof Drain	York Street	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD
R-07	0.015	0.90	1.00	Watts Roof Drain	York Street	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD
R-08	0.015	0.90	1.00	Watts Roof Drain	York Street	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD
R-09	0.015	0.90	1.00	Watts Roof Drain	York Street	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD
R-10	0.015	0.90	1.00	Watts Roof Drain	York Street	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD
A-03 / AD-01 (A-01)	0.075	0.84	0.94	Pump	York Street	10.60	TBD	2.31	26.00	10.60	TBD	4.69	26.00	10.60	TBD	15.78	26.00
R-00 / AD-02 (A-02)	0.193	0.90	1.00	Pump	George Street	11.30	0.485	16.60	79.64	11.30	0.875	27.17	79.64	11.30	2.385	69.68	79.64
Post-Development Flow						36.1	-	18.9	105.6	37.6	-	31.9	105.6	42.8	-	85.5	105.6
Total Allowable Release Rate						42.8				42.8				42.8			

**Notes:**  
D-01 and D-02 are uncontrolled flows from 141 George to George Street  
AD-02 (A-02) and R-00 are flows to Geroge Cistern  
A-03 and AD-01 (A-01) are flows to York cistern  
R-01 to R-10 are controlled flows to to service the future building at 110-116 York which will discharge directly to storm sewer on York

**Interim Conditon 110-116 York**  
In the interim , e.g. pending the construction of 110-116 York and the roof top controls & cistern, it is proposed to sheet drain the area to a catch basin which will connect to the York Street Sewer. The catch basin will be incorporated into the future cistern. As the exisitng area is hard surface and curently drains to York post-development will not exceed predevelopment, per below.  
Qpre (Asphalt Current);  $2.78 \times 0.223 \times 178.56 \times 0.90 = 58.1$  L/sec (5-Year).  $2.78 \times 0.223 \times 104.16 \times 0.90 = 99.4$  L/sec (100-Year)  
Qpost (Gravel Interim);  $2.78 \times 0.223 \times 178.56 \times 0.75 = 48.4$  L/sec (5-Year),  $2.78 \times 0.223 \times 104.16 \times 0.75 = 82.8$  L/sec (100-Year)

Refer to **Appendix D** for Rational Method calculations and **Drawing SWM**-Stormwater Management Plan.



### **6.3 Major Overland Flow Route**

A major overland flow route will be provided for storms greater than the 100-year storm event. Stormwater will be directed to the surrounding rights-of-way. The major overland system is shown on the Grading Plan (drawing 112142-GR).

## **7.0 EROSION AND SEDIMENT CONTROL**

Temporary erosion and sediment control measures will be implemented on-site during construction in accordance with the Best Management Practices for Erosion and Sediment Control. This includes the following temporary measures:

- Filter socks (catchbasin inserts) will be placed in existing and proposed catchbasins and catchbasin manholes, and will remain in place until vegetation has been established and construction is completed;
- Silt fencing will be placed along the surrounding construction limits;
- Mud mats will be installed at the site entrances;
- Strawbale or rock check dams will be installed in swales and ditches;
- The contractor will be required to perform regular street sweeping and cleaning as required, to suppress dust and to provide safe and clean roadways adjacent to the construction site;

Erosion and sediment control measures should be inspected daily and after every rain event to determine maintenance, repair or replacement requirements. Sediments or granulars that enter site sewers shall be removed immediately by the contractor. These measures will be implemented prior to the commencement of construction and maintained in good order until vegetation has been established. Refer to the Erosion and Sediment Control Plan (drawing 112142-ESC) for additional information.



## 8.0 CONCLUSIONS AND RECOMMENDATIONS

### Watermain

The analysis of the existing and proposed watermain network confirms the following:

- The proposed dual 200mm dia. watermain service which connects to the existing 300mm in George Street can service the proposed development.
- The proposed 200mm dia. watermain service which connects to the existing 200mm in York Street can service the proposed development.
- There are adequate pressures in the existing watermain infrastructure to meet the required domestic demands for the development.
- There is adequate flow to service the proposed fire protections system.

### Sanitary Servicing

The analysis of the existing and proposed sanitary system confirms the following:

- It is proposed to service the development with a proposed 200mm Sanitary service which will connect to existing sewers within the George Street Avenue right-of-way.
- Additionally, It is proposed to service the development with a proposed 200mm Sanitary service which will connect to existing sewers within the York Street Avenue right-of-way.
- It is anticipated there is adequate capacity within the existing sanitary infrastructure to service.

### Stormwater Management

The following provides a summary of the storm sewer and stormwater management system:

- The proposed storm sewer system is to connect to the storm sewers within in the George Street and York Street right-of-way.
- Stormwater control is to be provided by two cisterns within the P1 parking level.
- Storm flows will be attenuated through the implementation of a pump.
- As per existing conditions a major overland flow routes have been provided to the surrounding rights-of-way.

### Erosion and Sediment control

- Erosion and sediment control measures (i.e. filter fabric, catch basin inserts, silt fences, etc.) will be implemented prior to construction and are to remain in place until vegetation is established.



## 9.0 CLOSURE

The preceding report is respectfully submitted for review and approval. Please contact the undersigned should you have questions or require additional information.

### NOVATECH

**Prepared by:**



**Curtis Ferguson, E.I.T.**  
**Land Development Engineering**

**Reviewed by:**



**Greg MacDonald, P.Eng**  
**Director, Land Development and Public**  
**Sector Infrastructure**



## **Appendix A**

### **Pre-Consultation**





File No.: PC2024-0200

June 5, 2024

Vincent Denomme  
Claridge Homes(George St) Inc.  
Via email: [vincent.denomme@claridgehomes.com](mailto:vincent.denomme@claridgehomes.com)

**Subject: Pre-Consultation: Meeting Feedback  
Proposed Site Plan Control Revision Application – 137, 141 George  
Street and 110-116 York Street**

Please find below information regarding next steps as well as consolidated comments from the above-noted pre-consultation meeting held on May 28, 2024.

### **Pre-Consultation Preliminary Assessment**

1 <input type="checkbox"/>	2 <input type="checkbox"/>	3 <input checked="" type="checkbox"/>	4 <input type="checkbox"/>	5 <input type="checkbox"/>
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One (1) indicates that considerable major revisions are required while five (5) suggests that the proposal appears to meet the City's key land use policies and guidelines. This assessment is purely advisory and does not consider technical aspects of the proposal or in any way guarantee application approval.

### **Next Steps**

1. A review of the proposal and materials submitted for the above-noted pre-consultation has been undertaken. Please proceed to complete a Phase 3 Pre-consultation Application Form and submit it together with the necessary studies and/or plans to [planningcirculations@ottawa.ca](mailto:planningcirculations@ottawa.ca).
2. In your subsequent pre-consultation submission, please ensure that all comments or issues detailed herein are addressed. A detailed cover letter stating how each issue has been addressed must be included with the submission materials. Please coordinate the numbering of your responses within the cover letter with the comment number(s) herein.
3. Please note, if your development proposal changes significantly in scope, design, or density before the Phase 3 pre-consultation, you may be required to complete or repeat the Phase 2 pre-consultation process.

### **Supporting Information and Material Requirements**

1. The attached **Study and Plan Identification List** outlines the information and material that has been identified, during this phase of pre-consultation, as either required (R) or advised (A) as part of a future complete application submission.



- a. The required plans and studies must meet the City's Terms of Reference (ToR) and/or Guidelines, as available on [Ottawa.ca](http://Ottawa.ca). These ToR and Guidelines outline the specific requirements that must be met for each plan or study to be deemed adequate.

### **Consultation with Technical Agencies**

1. You are encouraged to consult with technical agencies early in the development process and throughout the development of your project concept. A list of technical agencies and their contact information is enclosed.

### **Planning**

Comments:

1. From a construction and efficiency perspective, we agree that building this garage all together at once is logical; however, we will want some protections in place because it is premature to what is happening above-grade. We have some concerns with permitting this high volume of parking on such a downtown site in advance of the redevelopment approval at 110 and 116 York Street; and therefore, any approved drawings should essentially close-off the section of parking on 110 and 116 York Street. Punch-out walls can effectively temporarily close off this section of the parking garage as an interim measure. We do not want any functioning parking taking place on 110 and 116 York Street in advance of the Site Plan Approval for that property.
2. We wish to flag the risk to the Owner/applicant that constructing the footings (during the parking garage construction) in advance of the SPC approval for 110 and 116 York Street. The risk is that through the OPA/ZBLA/SPC process, the proposed building is still subject to change throughout the application processes. Should a change be required that affects the footings, it will be the Owner's responsibility to adjust or potentially rebuild accordingly.
3. Please ensure clear communication and the same floor plans are shared between City of Ottawa departments working on this project; namely, Building Permit Office (attn: Terri Hunt) and Right-Of-Way Approvals Office (attn: Tyler McQuillen).
4. In the Scoped Planning Rationale/Planning Cover Letter, clarify the Ownership, easements, and intended users
  - a. Clarify the intent of ownership over the parking garage. There is a Part Lot Control application (D07-08-23-0036) to adjust lot line adjustments between 137, 141 George St and 110 York St that is currently on hold. This application does not need to be re-initiated in tandem with this application, but please provide an explanation outlining the general intent



in terms of who will own and operate this shared parking garage and clarify if any easements are anticipated to allow for this shared ownership.

- b. It is understood from the pre-con meeting that the garage is intended to be used by visitors to the hotel Andaz (existing and future addition) as well as the people renting within the 137, 141 George St building. It is understood that the first level of underground parking will be for the hotel use and level 2 and 3 will be gated to allow the renters of 137, 141 George St to use their fobs through this restricted access to park. It is also understood there is commercial at grade at 137, 141 George. Please confirm this understanding is correct and outline how this parking garage will function and address any requirements of each use within the Scoped Planning Rationale.

5. Parking calculations:

- a. It is understood that the same number of parking spaces are being proposed through this application as was previously approved through the SPC application at 137, 141 George St (D07-12-12-0199). In the Scoped Planning Rationale, please outline the numbers and layout of what was previously approved (X number of spaces, 6 levels?) compared to what it is now (X number of spaces, 3 levels?).
- b. Provide a chart that has a breakdown of the required and proposed vehicular and bike parking and accessible spaces provided for all developments sharing this underground parking garage. The chart should:
  - i. Provide a total for the entire garage of vehicular spaces, bike parking spaces, accessible spaces
  - ii. Breakdown the total under associated address and also use within that address.
- c. It is understood that the redevelopment proposal and it's associated unit count at 110 and 116 York St is still subject to change through the future OPA/ZBLA/SPC applications.

6. Illustrate and label on submitted floor plans:

- a. Clearly show and label all property lines on the floor plans
- b. Identify municipal addresses of applicable areas of the plan (understanding the property boundaries may be subject to change through the associated Part Lot Control application)
- c. Punch-out walls. The City wants a punch-out wall on the property line for 110 and 16 York Street. This needs to be built alongside the parking garage to ensure the portion located on 110 and 116 York Street is not



accessible/used in advance of a redevelopment approval (associated OPA, ZBLA, and SPC approval).

- d. Dimension parking spaces, drive aisle widths, turning radius', access etc. to ensure compliance with the Zoning By-law Part 4
7. Clarify if any above-grade soft landscaping will be impacted by the location/height of the underground parking garage at specifically 110 and 116 York Street.
8. Speak to any changes (or whether there are no changes) to the vehicular access or underground vehicular circulation.
9. Provide a Zoning Confirmation Report citing the underground parking garage is in compliance with Part 4 – Parking, Queuing and Loading Provisions of the Zoning By-law.
10. For Phase 3 Pre-con and application, in addition to any other staff requirements outlined in the SPIL, please provide the following:
  - a. Floor Plans for each level of underground parking (addressing comments above)
  - b. Scoped Planning Rationale / Planning Cover letter (addressing comments above)
  - c. Zoning Confirmation Report (only for the underground parking garage)
  - d. Plan of Survey (if easily available for all properties in question)

## **Engineering**

Comments:

11. The Stormwater Management Criteria, for the subject site, is to be based on the following:
  - a. Please update the SWM calculations to account for the added parcel at 116 York.
  - b. Demonstrate the servicing strategy is consistent with the studies and plans previously approved under the existing SPC agreement.
  - c. Please provide a Pre-Development Drainage Area Plan to define the pre-development drainage areas/patterns. Existing drainage patterns shall be maintained and discussed as part of the proposed SWM solution.



## 12. General Servicing

- a. Provide existing servicing information and the recommended location for the proposed connections. Services should ideally be grouped in a common trench to minimize the number of road cuts.
- b. Where servicing involves three or more service trenches, either a full road width or full lane width 40 mm asphalt overlay will be required, as per amended Road Activity By-Law 2003-445 and City Standard Detail Drawing R10. The extent of the overlay must be shown on the grading plan or a road reinstatement plan.
- c. CCTV sewer inspection of city infrastructure is required to record pre and post construction conditions and ensure there is no damage to City

## 13. Storm Sewer

- a. A 675mm dia. concrete storm sewer (1991) is available within York Street.
- b. A storm sewer monitoring maintenance hole is required to be installed at the property line (on the private side of the property) as per City of Ottawa Sewer-Use By-Law 2003-514 (14) Monitoring Devices. If there is no space to accommodate a monitoring maintenance hole, a test port giving access to the city personnel shall be provided.

## 14. Sanitary Sewer

- a. A 1200 mm dia. concrete Sanitary sewer (1934) is available within York Street.
- b. Please provide the estimated new Sanitary sewer discharge and we will confirm if sanitary sewer main has the capacity.
- c. Please apply the wastewater design flow parameters in Technical Bulletin PIEDTB-2018-01.
- d. Sanitary sewer monitoring maintenance hole is required to be installed at the property line (on the private side of the property) as per City of Ottawa Sewer-Use By-Law 2003-514 (14) Monitoring Devices. If there is no space to accommodate a monitoring maintenance hole, a test port giving access to the city personnel shall be provided.
- e. A backwater valve is required on the sanitary service for protection.

## 15. Water:

- a. A 200 mm dia. Ductile Iron watermain (1989) is available within York Street.



- b. The pre-installation of water service laterals for future use is not typically permitted. For this specific situation we will allow the installation of the pre-installation of the water services, however the connection to the main and commissioning will not be permitted until SPC approval for the hotel addition is obtained.
- c. Existing water services are to be blanked at the watermain.
- d. Water Supply Redundancy: As per ISTB-2021-03, Industrial, commercial, institutional service areas with a basic day demand greater than 50 m<sup>3</sup>/day and residential areas serving 50 or more dwellings shall be connected with a minimum of two watermains, separated by an isolation valve, to avoid the creation of a vulnerable service area. Individual residential facilities with a basic day demand greater than 50 m<sup>3</sup>/day shall be connected with a minimum of two water services, each their own meter and separated by an isolation valve, to avoid the creation of a vulnerable service area.
- e. Water Boundary condition requests must include the location of the service (map or plan with connection location(s) indicated) and the expected loads required by the proposed development, including calculations. Please provide the following information:
  - i. Plan showing the proposed location of service(s).
  - ii. Type of development and the amount of fire flow required (L/min).  
Note: The OBC method can be used if the fire demand for the private property is less than 9,000 L/min. If the OBC fire demand reaches 9000 L/min, then the FUS method is to be used. Fire flow demand requirements are to be based on ISTB-2021-03. Exposure separation distances shall be defined on a figure to support the FUS calculation and required fire flow (RFF).
  - iii. Average daily demand: \_\_L/s.
  - iv. Maximum daily demand: \_\_L/s.
  - v. Maximum hourly daily demand: \_\_L/s.
  - vi. Note: Use Table 3-3 of the MOE Design Guidelines for Drinking-Water System to determine Maximum Day and Maximum Hour peaking factors for 0 to 500 persons and use Table 4.2 of the Ottawa Design Guidelines, Water Distribution for 501 to 3,000 persons.
- f. Please review Technical Bulletin ISTB-2018-02, maximum fire flow hydrant capacity is provided in Section 3 Table 1 of Appendix I. A hydrant coverage figure shall be provided and demonstrate there is adequate fire





protection for the proposal. Two or more public hydrants are anticipated to be required to handle fire flow.

- g. A Water Data Card will have to be submitted to size the water meter.

#### 16. Grading and Erosion

- a. Post-development site grading shall match existing property line grades in order to minimize disruption to the adjacent residential properties. A topographical plan of survey shall be provided as part of the submission and a note provided on the plans.
- b. Erosion and sediment control plan must be provided.

#### 17. Environmental

- a. A Phase I ESA is required to be completed in accordance with Ontario Regulation 153/04 to determine the potential for site contamination of the added parcel at 116 York St. Depending on the Phase I recommendations a Phase II ESA may be required.
- b. The Phase I ESA shall provide all the required Environmental Source Information as required by O. Reg. 153/04. ERIS records are available to public at a reasonable cost and need to be included in the ESA report to comply with O.Reg. 153/04 and the Official Plan. The City will not be in a position to approve the Phase I ESA without the inclusion of the ERIS reports.
- c. [Official Plan: Section 10. Protection of Health and Safety \(ottawa.ca\)](#)

#### 18. Environmental Compliance Approval

- a. An Environmental Compliance Approval (ECA) for Private Sewage Works is not required at this stage. However, consideration shall be taken to evaluate the proposed SWM works with respect to the future severance of the site as Stormwater management works servicing more than one parcel of land requires an ECA from the Ministry of the Environment, Conservation and Parks.
- b. [Environmental Compliance Approval | Ontario.ca](#)

#### 19. Geotechnical

- a. A Geotechnical Study/Investigation shall be prepared in support of this development proposal for the added parcel at 116 York St. The geotechnical study shall also be updated to address the proposed changes regarding the depth of excavation and founding depth.



- b. Geotechnical Study shall be consistent with the Geotechnical Investigation and Reporting Guidelines for Development Applications. [Geotechnical Investigation and Reporting \(ottawa.ca\)](http://ottawa.ca/GeotechnicalInvestigationandReporting)

## 20. Pre-Construction Survey

- a. Pre-Construction (Piling/Hoe Ramming or close proximity to City Assets) and/or Pre-Blasting (if applicable) Survey required for any buildings/dwellings in proximity of 75m of site and circulation of notice of vibration/noise to residents within 150 m of site. Conditions for Pre-Construction/ Pre-Blast Survey & Use of Explosives will be applied to agreements. Refer to City's Standard S.P. No. F-1201 entitled Use of Explosives, as amended.

Please refer to the City of Ottawa Guide to Preparing Studies and Plans [Engineering]: [Planning application submission information and materials](#). The guide outlines the requirement for a statement to be provided on the plan about where the property boundaries have been derived from

Feel free to contact Vincent Duquette, Infrastructure Project Manager, for follow-up questions.

## **Noise**

Comments:

## 21. Noise requirements

- a. A Transportation Noise Assessment is not required at this stage. It will be requested during SPC/ZBLA application for the hotel addition seeing as the subject development is located within 100m proximity of Dalhousie Street.

Feel free to contact Vincent Duquette, Infrastructure Project Manager, for follow-up questions.

## **Transportation**

Comments:

## 22. Right-of-way protection.

- a. See [Schedule C16 of the Official Plan](#).
- b. Any requests for exceptions to ROW protection requirements must be discussed with Transportation Planning and concurrence provided by Transportation Planning management.





23. The Screening Form has indicated that TIA Triggers have been met. Please proceed with the TIA Step 3– Forecasting Report. The consultant is to address how they plan to enable and encourage travel by sustainable modes (i.e., to make walking, cycling, transit, carpooling and telework more convenient, accessible, safe, and comfortable). Please complete the City of Ottawa’s TDM Measures Checklist.
24. Please provide your response to the previous Transportation comments submitted under PC2024-0101 (Ph1 precon for OPA/ZBLA/SPC for 110, 116 York).

Feel free to contact **Wally Dubyk**, Transportation Project Manager, for follow-up questions.

### **Submission Requirements and Fees**

1. A Site Plan Control Revision Application (to D07-12-12-0199) – Standard is required.
  - a. Additional information regarding fees related to planning applications can be found [here](#).
2. The attached **Study and Plan Identification List** outlines the information and material that has been identified as either required (R) or advised (A) as part of a future complete application submission.
  - a. The required plans and studies must meet the City’s Terms of Reference (ToR) and/or Guidelines, as available on [Ottawa.ca](http://Ottawa.ca). These ToR and Guidelines outline the specific requirements that must be met for each plan or study to be deemed adequate.
3. All of the above comments or issues should be addressed to ensure the effectiveness of the application submission review.

Should there be any questions, please do not hesitate to contact myself or the contact identified for the above areas / disciplines.

Yours Truly,  
Ann O’Connor

Encl. Study and Plan Identification List (SPIL)

c.c. Vincent Duquette  
John Wu  
Wally Dubyk

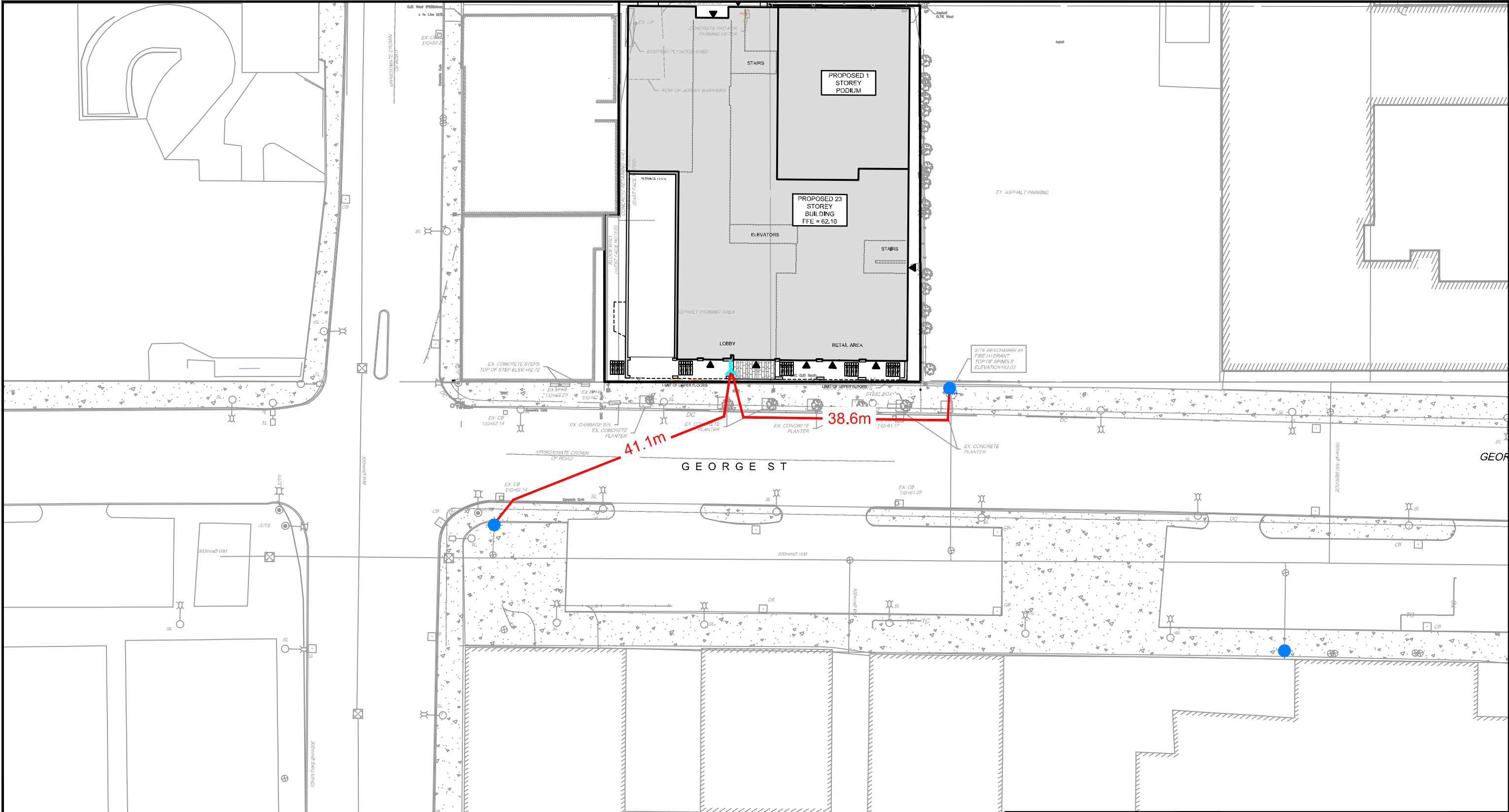


## **Appendix B**

### **Water Servicing**

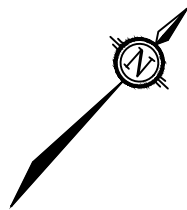


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**LEGEND**

- PROPERTY LINE
- Y PROPOSED SIAMESE CONNECTION
- EXISTING CLASS AA HYDRANT
- DISTANCE FROM HYDRANT TO SIAMESE CONNECTION/ BUILDING ENTRANCE



**NOVATECH**

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Website [www.novatech-eng.com](http://www.novatech-eng.com)

CITY OF OTTAWA  
141 GEORGE STREET

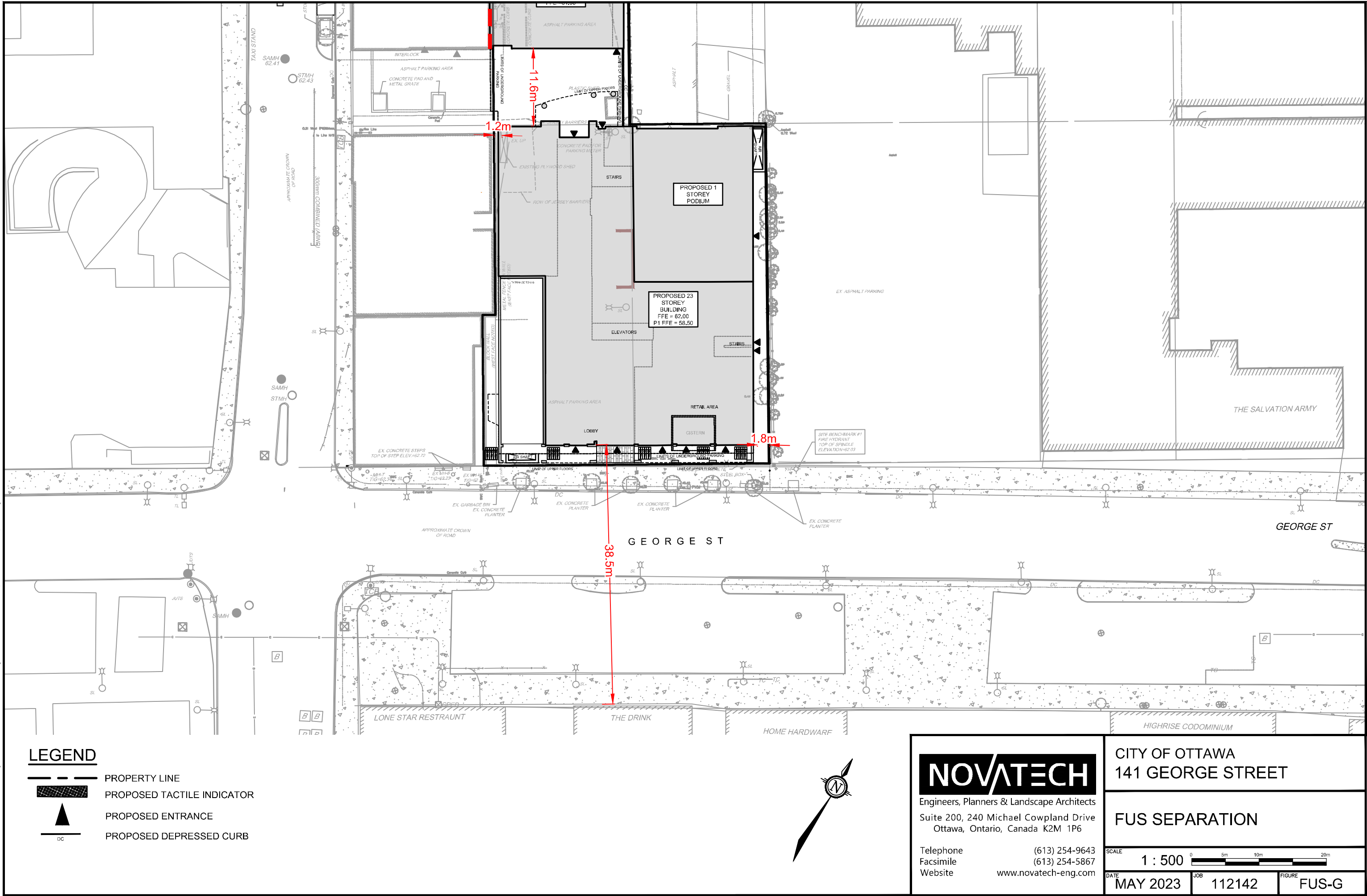
**COVERAGE PLAN**

SCALE 1 : 500 0 5m 10m 20m

DATE APRIL 2023 JOB 112142 FIGURE COV-G



M:\2012\11\12142\PHASE 2\CAD\Civil\Figures\FUS\112142-FUS SEP.dwg, SEP-141 GEORGE Apr 26, 2023 - 3:34pm, cferguson





# FUS - Fire Flow Calculations

As per 2020 Fire Underwriter's Survey Guidelines



Engineers, Planners & Landscape Architects

Novatech Project #: 112142  
 Project Name: 141 George Street  
 Date: 5/1/2023  
 Input By: Curtis Ferguson, E.I.T.  
 Reviewed By: Anthony Mestwarp, P.Eng

Legend

Input by User  
 No Information or Input Required

Building Description: 21 Storey Mixed-Use with Ground Floor Commercial  
 Type I - Fire resistive construction (2 hrs)

Step			Choose		Value Used	Total Fire Flow (L/min)	
<b>Base Fire Flow</b>							
1	<b>Construction Material</b>  <b>Coefficient related to type of construction</b> <b>C</b>	Type V - Wood frame		1.5	0.6		
		Type IV - Mass Timber		Varies			
		Type III - Ordinary construction		1			
		Type II - Non-combustible construction		0.8			
		Type I - Fire resistive construction (2 hrs)	Yes	0.6			
2	<b>Floor Area</b>  <b>A</b>	Podium Level Footprint (m <sup>2</sup> )	1759				
		Total Floors/Storeys (Podium)	1				
		Tower Footprint (m <sup>2</sup> )	1220				
		Total Floors/Storeys (Tower)	20				
		Protected Openings (1 hr)	Yes				
		A, Total Effective Floor Area (m <sup>2</sup> )					2,369
	<b>F</b>	<b>Base fire flow without reductions</b> <b>F = 220 C (A)<sup>0.5</sup></b>				6,000	
<b>Reductions or Surcharges</b>							
3	<b>Occupancy hazard reduction or surcharge</b>  <b>(1)</b>	FUS Table 3	<b>Reduction/Surcharge</b>		-15%	5,100	
		Non-combustible		-25%			
		Limited combustible	Yes	-15%			
		Combustible		0%			
		Free burning		15%			
4	<b>Sprinkler Reduction</b>  <b>(2)</b>	FUS Table 4	<b>Reduction</b>			-2,040	
		Adequately Designed System (NFPA 13)	Yes	-30%			-30%
		Standard Water Supply	Yes	-10%			-10%
		Fully Supervised System	Yes	-10%			-10%
		<b>Cumulative Sub-Total</b>		<b>-50%</b>			
		<b>Area of Sprinklered Coverage (m<sup>2</sup>)</b>	20927.2	80%			
		<b>Cumulative Total</b>		<b>-40%</b>			
5	<b>Exposure Surcharge per</b>  <b>(3)</b>	FUS Table 5	<b>Surcharge</b>			3,315	
		North Side	10.1 - 20 m				15%
		East Side	0 - 3 m				25%
		South Side	>30m				0%
		West Side	0 - 3 m				25%
<b>Cumulative Total</b>		<b>65%</b>					
<b>Results</b>							
6	<b>(1) + (2) + (3)</b>	<b>Total Required Fire Flow, rounded to nearest 1000L/min</b>			<b>L/min</b>	<b>6,000</b>	
		(2,000 L/min < Fire Flow < 45,000 L/min)		or	<b>L/s</b>	<b>100</b>	
				or	<b>USGPM</b>	<b>1,585</b>	
7	<b>Storage Volume</b>	Required Duration of Fire Flow (hours)			Hours	2	
		Required Volume of Fire Flow (m <sup>3</sup> )			m <sup>3</sup>	720	



# OBC Water Supply for Firefighting Calculation

Based on OBC 2012 (Div. B, Article 3.2.5.7)

References: [Ontario Fire Marshal - OBC Fire Fighting Water Supply](#)  
[Ontario Building Code 2012, Appendix A, Vol 2., A-3.2.5.7](#)



**Novatech Project #:** 112142  
**Project Name:** 141 George Street  
**Date:** 9/24/2024  
**Input By:** Curtis Ferguson, E.I.T.  
**Reviewed By:** Greg MacDonald, P.Eng.

Legend

Input by User

No Input Required

**Building Description:** 17 + Penthouse Storey Mixed-Use Building

Step	Calculation Inputs	Calculation Notes	Value
<b>Minimum Fire Protection Water Supply Volume</b>			
1	<b>Water Supply Coefficient</b>		
	Building Classification = <b>Water Supply Coefficient - K =</b>	From Table 3.1.2.1 From Table 1 (A3.2.5.7)	<b>18</b>
2	<b>Total Building Volume</b>		
	Building Width - W	37.70 m	
	Building Length - L	47.18 m	Area (W * L) = 1779 m <sup>2</sup>
	Building Height - H	64.5 m	
	<b>Total Building Volume - V =</b>	W * L * H	<b>114725 m<sup>3</sup></b>
3	<b>Spatial Coefficient Value</b>		
	<b>Exposure Distances:</b> (Exterior building face to property/lot line, to street centre, or to mid-point between proposed building and another building on same lot)	<b>Spatial Coefficients:</b> From Figure 1 (Spatial Coefficient vs Exposure Distance)	
	North	11.60 m	Sside 1 = 0.00
	East	1.80 m	Sside 2 = 0.50
	South	38.50 m	Sside 3 = 0.00
	West	1.20 m	Sside 4 = 0.50
	<b>Total of Spacial Coefficient Values - S-Tot</b> as obtained from the formula =	1.0 + (Sside 1 + Sside 2 + Sside 3 + Sside 4) (Max. value = 2.0)	<b>2.00</b>
4	<b>Minimum Fire Protection Water Supply Volume</b>		
	<b>Q =</b>	<b>K * V * S<sub>Tot</sub></b>	<b>4,130,109 L</b>
<b>Required Minimum Water Supply Flow Rate</b>			
5	<b>Minimum Water Supply Flow Rate</b>		
	<b>=</b>	From Table 2 (For water supply from a municipal or industrial water supply system, min. pressure is 140 kPa) or	<b>9,000 L/min</b> <b>150 L/s</b>
<b>Minimum Fire Protection Water Supply Volume for 30 minutes</b>			
6	<b>Q =</b>	<b>= Minimum Water Supply Flow Rate (L/min) * 30 minutes</b>	<b>270,000 L</b>
<b>Required Fire Protection Water Supply Volume</b>			
7	<b>Q =</b>	Highest volume out of (4) and (6)	<b>4,130,109 L</b>
Notes			



**Proposed Development Conditions - 141 George Street**

	<b>21-Storey Mixed-Use</b>
Studio	25
1 Bed Apartment	147
2 Bed Apartment/ 1 Bed+ Den	123
3 Bed Apartment/ 2 Bed + Den	1
Number of units	296
<b>Total Residential Population</b>	<b>502</b>
<b>Total Residential Daily Flow (L/day)</b>	<b>140616</b>
Office Area (m <sup>2</sup> )	72.70
Restaurant Area (m2)	477.00
Party/Meeting Room (m2)	130.00
<b>Total Commercial Daily Flow (L/day)</b>	<b>34948.79</b>
Avg Day Demand (L/s)	2.03
Max Day Demand (L/s)	4.68
Peak Hour Demand (L/s)	10.04

\* Rental Office  
 \* Commercial area on 1st floor  
 \* 2nd floor communal amenities

**Design Parameters**

<b>Use</b>	<b>Daily Demand Volume</b>		<b>Source</b>
Studio	1.4	Person/unit	City of Ottawa Sewer Design Guidelines
1 Bed Apartment	1.4	Person/unit	
2 Bed Apartment	2.1	Person/unit	
3 Bed Apartment	3.1	Person/unit	
Bar/ Cocktail Lounge (meeting/party room)	70	L/day/seat (1 seat/ 2m2)	City of Ottawa Water Distribution Guidelines
Average Residential Flow	280	L/c/day	
Professional Office	75	L/9.3m2/day	Daily Demands from OBC Table 8.2.1.3
Retail - Restaurant	125	L/2m2/day	

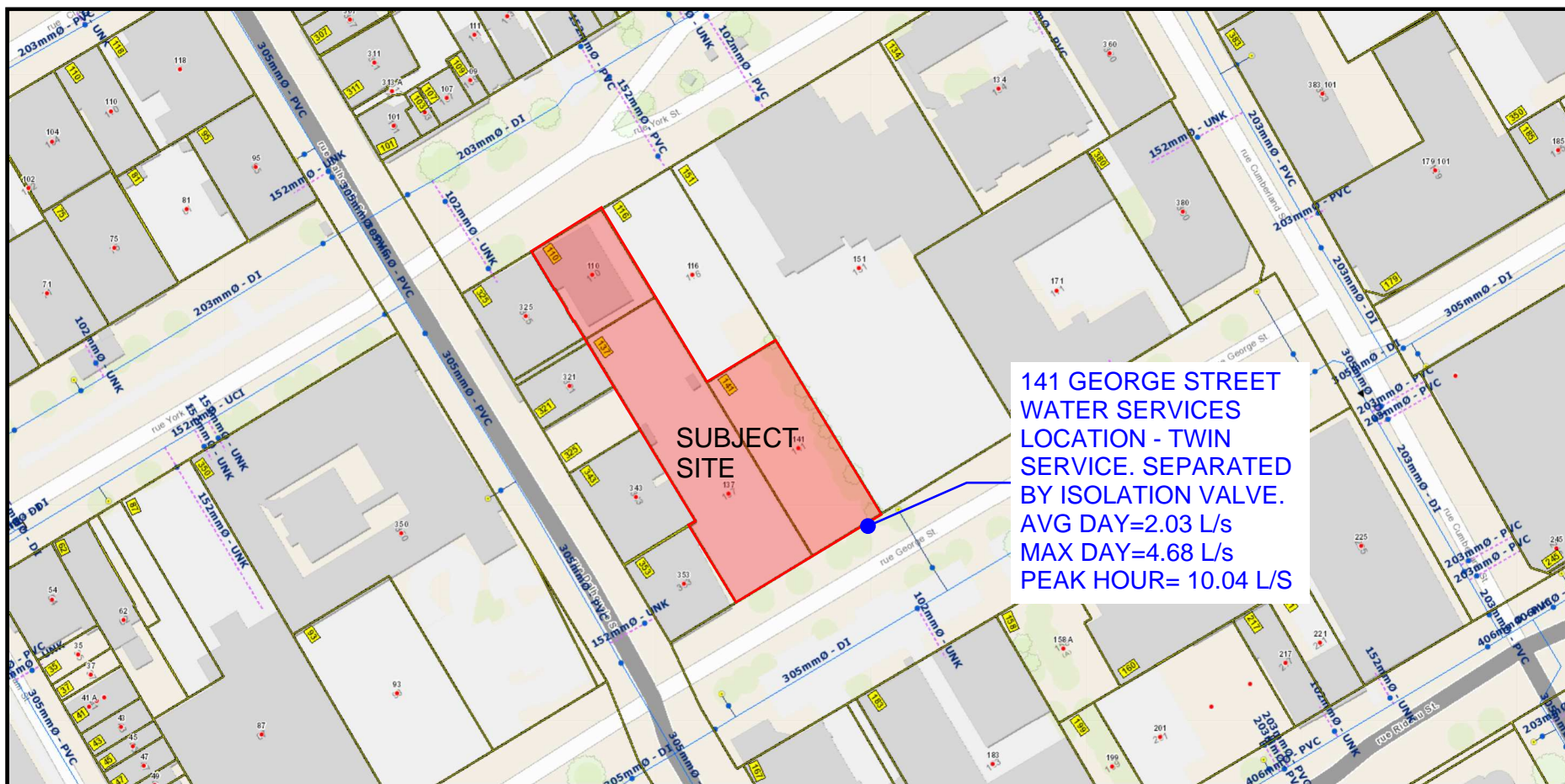
**Residential Peaking Factors City of Ottawa Water Distribution Guidelines:**

Conditions	Peaking Factor	
Maximum Day	2.5	x avg day
Peak Hour	2.2	x max day

**Commercial Peaking Factors City of Ottawa Water Distribution Guidelines**

Conditions	Peaking Factor	
Maximum Day	1.5	x avg day
Peak Hour	1.8	x max day





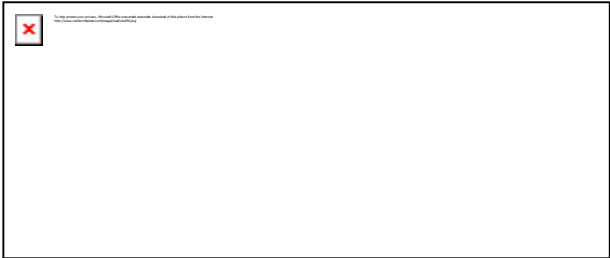
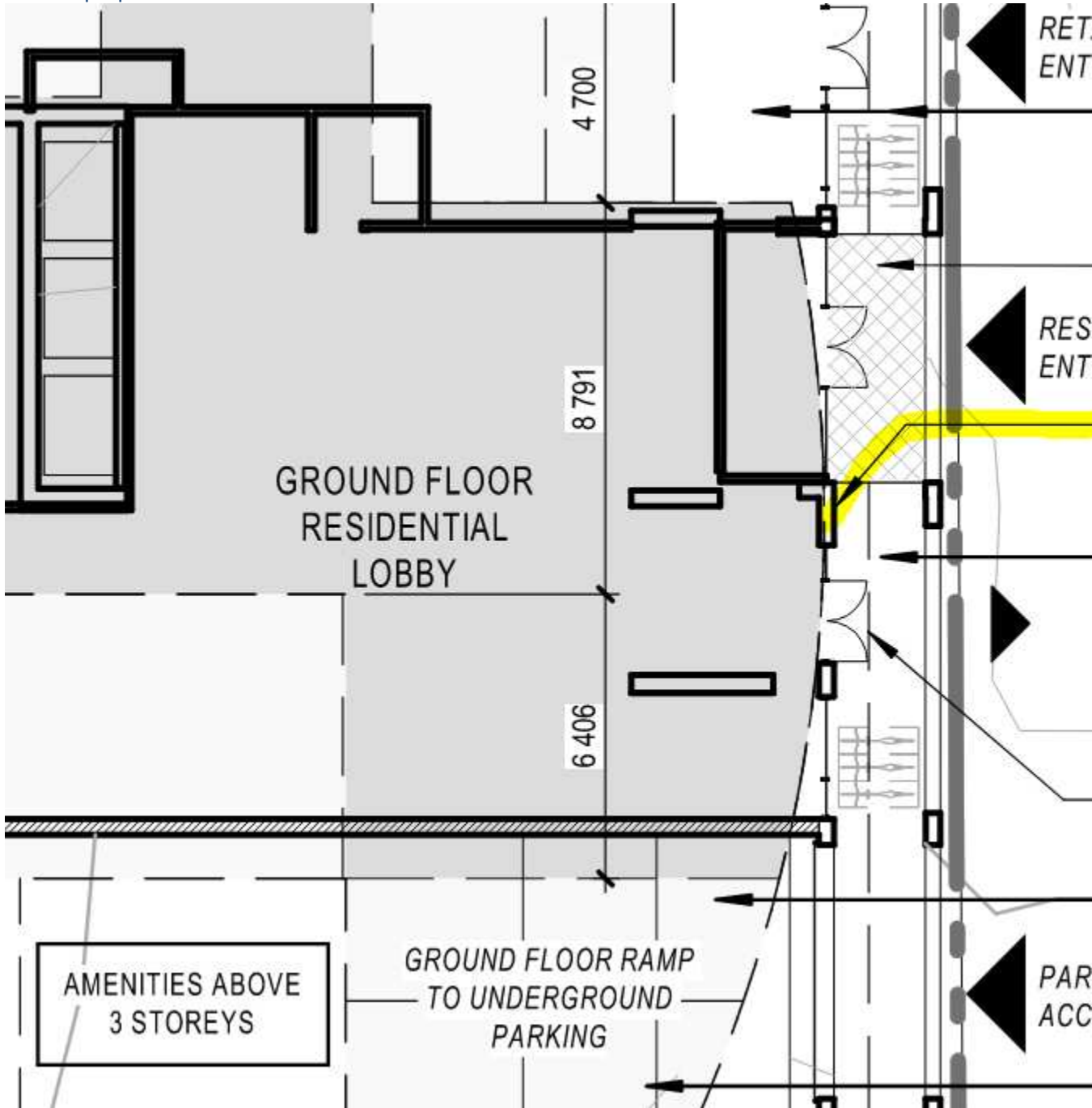


Curtis Ferguson

From: Evelyne Cardinal <ecardinal@neufarchitectes.com>  
Sent: Tuesday, April 25, 2023 10:09 AM  
To: Curtis Ferguson; Dinesh Jain  
Cc: Anthony Mestwarp  
Subject: RE: 141 George Street (112142)

Adding Dinesh Jain, mechanical engineer to the email.

- 1) Type 1: concrete construction = fire resistive construction 2hr
- 2) Yes to all three, but mechanical to confirm
- 3) Current proposed location:



**EVELYNE CARDINAL, OAA, OAQ**  
Directrice du bureau d'Ottawa . Ottawa Office Director  
T 613 234 2274 #288 F 514 847 2287 C 613 809 3042  
47 Clarence Street, suite 406, Ottawa (ON) K1N 9K1  
**NEUF ARCHITECTES INC.** Confidentialité + Transmission  
Montréal. Ottawa. Toronto

50 ANS ET TOUJOURS NEUF . 50 YEARS AND STILL NEUF

De : Curtis Ferguson <c.ferguson@novatech-eng.com>  
Envoyé : April 25, 2023 9:52 AM  
À : Evelyne Cardinal <ecardinal@neufarchitectes.com>



Cc : Anthony Mestwarp <a.mestwarp@novatech-eng.com>  
Objet : RE: 141 George Street (112142)

Good Morning Evelyne,

Few more questions pertaining to 141 George and 110 York;

1) Construction Material (one of the following);

Type V - Wood frame
Type IV - Mass Timber
Type III - Ordinary construction
Type II - Non-combustible construction
Type I - Fire resistive construction (2 hrs)

2) Sprinkler Reduction (YES or NO);

- a. Adequately Designed System (NFPA 13) – Y OR N
- b. Standard Water Supply – Y OR N
- c. Fully Supervised System – Y OR N

3) Location of Siamese Connections

Thanks,  
Curtis Ferguson, B.A.Sc., E.I.T. | Land Development

**NOVATECH**  
Engineers, Planners & Landscape Architects  
240 Michael Cowpland Drive, Suite 200, Ottawa, ON, K2M 1P6 | Tel: 613.254.9643 EXT: 331  
The information contained in this email message is confidential and is for exclusive use of the addressee.

From: Curtis Ferguson  
Sent: Monday, April 24, 2023 4:31 PM  
To: Evelyne Cardinal <ecardinal@neufarchitectes.com>  
Cc: Anthony Mestwarp <a.mestwarp@novatech-eng.com>  
Subject: RE: 141 George Street (112142)

Evelyne,  
  
Perfect, thanks.

Keep me updated on the changes. Will need to include the “Retail Office” space in our Water / Sanitary calculations as well.

- In the interment I’ll assume;
- 5000 ft^2 Commercial (use to be determined - conservative assumptions until confirmed use [I.E. Café, Office, Retail etc..]).
  - 1000 ft^2 Retail Office Space.

Thanks,  
Curtis Ferguson, B.A.Sc., E.I.T. | Land Development

**NOVATECH**  
Engineers, Planners & Landscape Architects  
240 Michael Cowpland Drive, Suite 200, Ottawa, ON, K2M 1P6 | Tel: 613.254.9643 EXT: 331  
The information contained in this email message is confidential and is for exclusive use of the addressee.

From: Evelyne Cardinal <ecardinal@neufarchitectes.com>  
Sent: Monday, April 24, 2023 4:13 PM  
To: Pascal Vendette <pascal@neufarchitectes.com>; Curtis Ferguson <c.ferguson@novatech-eng.com>  
Cc: Anthony Mestwarp <a.mestwarp@novatech-eng.com>  
Subject: RE: 141 George Street (112142)

.... And the CAD.





**EVELYNE CARDINAL**, OAA, OAQ  
Directrice du bureau d'Ottawa . Ottawa Office Director  
T 613 234 2274 #288 F 514 847 2287 C 613 809 3042  
47 Clarence Street, suite 406, Ottawa (ON) K1N 9K1  
**NEUF ARCHITECTES** INC. Confidentialité + Transmission  
Montréal. Ottawa. Toronto

**50 ANS ET TOUJOURS NEUF . 50 YEARS AND STILL NEUF**

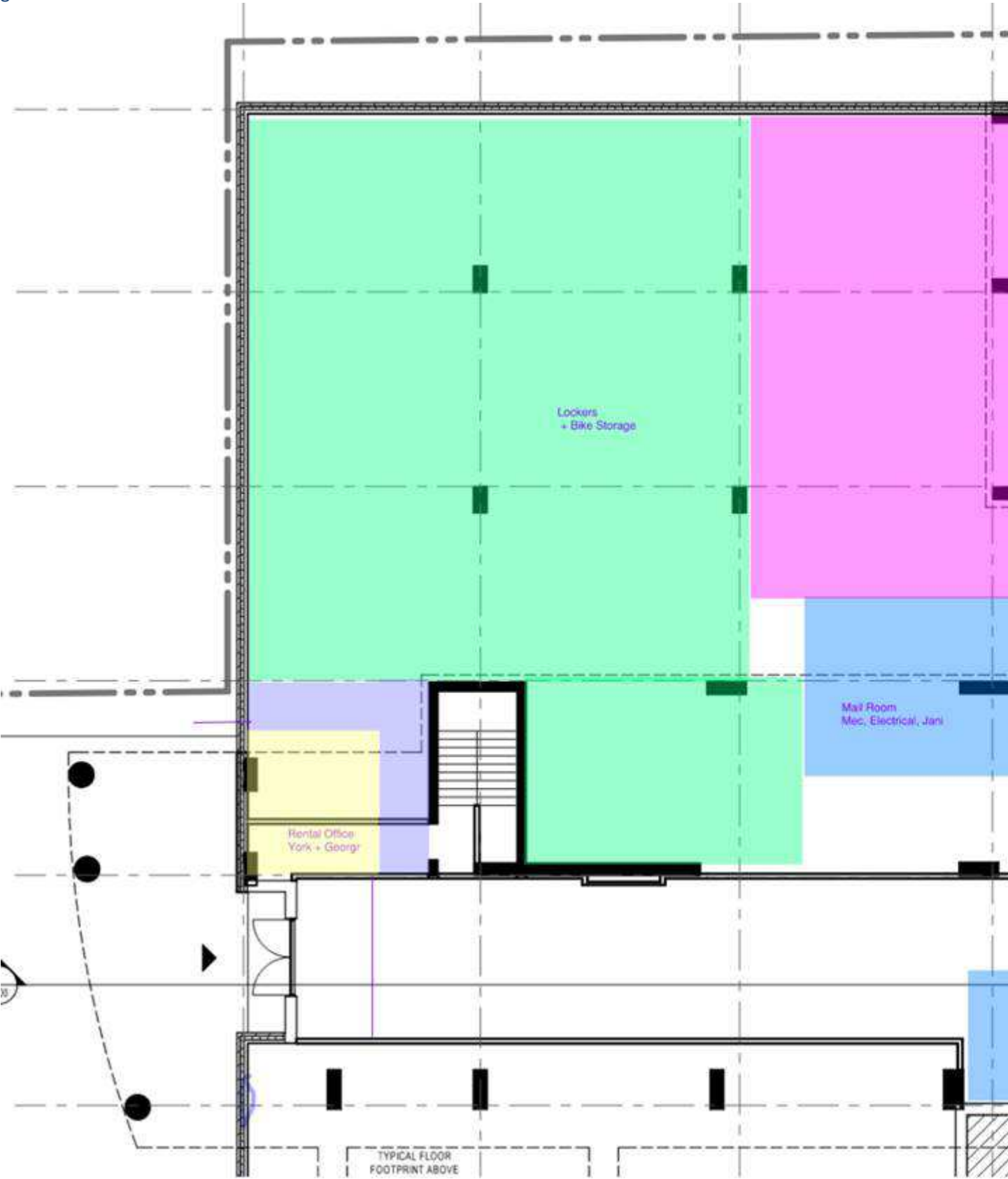
---

**De :** Evelyne Cardinal  
**Envoyé :** April 24, 2023 4:13 PM  
**À :** Pascal Vendette <[pascal@neufarchitectes.com](mailto:pascal@neufarchitectes.com)>; Curtis Ferguson <[c.ferguson@novatech-eng.com](mailto:c.ferguson@novatech-eng.com)>  
**Cc :** Anthony Mestwarp <[a.mestwarp@novatech-eng.com](mailto:a.mestwarp@novatech-eng.com)>  
**Objet :** RE: 141 George Street (112142)

Hi Curtis,  
We recently got information that the retail space will be cut down to 5000 sq.ft. as shown in this pink area. There's a second 1000sq.ft. pink area at the bottom that will most likely become the retail offices. Shawn is working on this right now, so if there are any changes, I will let you know.



Otherwise, I forgot to include the ground floor roof plan. I've attached the second floor, there's a roof space between grid 8-5 and G-D.



**EVELYNE CARDINAL, OAA, OAQ**  
Directrice du bureau d'Ottawa . Ottawa Office Director  
T 613 234 2274 #288 F 514 847 2287 C 613 809 3042  
47 Clarence Street, suite 406, Ottawa (ON) K1N 9K1  
**NEUF ARCHITECTES INC.** Confidentialité + Transmission  
Montréal. Ottawa. Toronto

50 ANS ET TOUJOURS NEUF . 50 YEARS AND STILL NEUF

De : Pascal Vendette <[pascal@neufarchitectes.com](mailto:pascal@neufarchitectes.com)>  
Envoyé : April 24, 2023 2:46 PM  
À : Curtis Ferguson <[c.ferguson@novatech-eng.com](mailto:c.ferguson@novatech-eng.com)>  
Cc : Anthony Mestwarp <[a.mestwarp@novatech-eng.com](mailto:a.mestwarp@novatech-eng.com)>; Evelyn Cardinal <[ecardinal@neufarchitectes.com](mailto:ecardinal@neufarchitectes.com)>  
Objet : RE: 141 George Street (112142)



Hi Curtis.  
Evelyne Cardinal is the main contact for 141 George & 110 York.  
I cc'ed her to this email ... + see below for contact info.

**EVELYNE CARDINAL**, OAA, OAQ  
Directrice du bureau d'Ottawa . Ottawa Office Director  
T 613 234 2274 #288 F 514 847 2287 C 613 809 3042  
47 Clarence Street, suite 406, Ottawa (ON) K1N 9K1  
**NEUF ARCHITECTES INC.** Confidentialité + Transmission  
Montréal. Ottawa. Toronto



**PASCAL VENDETTE**  
Technologue senior en architecture . Senior architectural technologist  
T 514 847 1117 #269 F 514 847 2287 C 514 833 6005  
630, boul. René-Lévesque O. 32<sup>e</sup> étage, Montréal (QC) H3B 1S6  
**NEUF ARCHITECTES INC.** Confidentialité + Transmission  
Montréal. Ottawa. Toronto

**50 ANS ET TOUJOURS NEUF . 50 YEARS AND STILL NEUF**

---

**De :** Curtis Ferguson <[c.ferguson@novatech-eng.com](mailto:c.ferguson@novatech-eng.com)>  
**Envoyé :** 24 avril 2023 13:55  
**À :** Pascal Vendette <[pascal@neufarchitectes.com](mailto:pascal@neufarchitectes.com)>  
**Cc :** Anthony Mestwarp <[a.mestwarp@novatech-eng.com](mailto:a.mestwarp@novatech-eng.com)>  
**Objet :** 141 George Street (112142)

Good Afternoon Pascal,

Hope you're doing well.

Assuming you're on Claridge - 141 George Street? If not, please forward to correct contact.

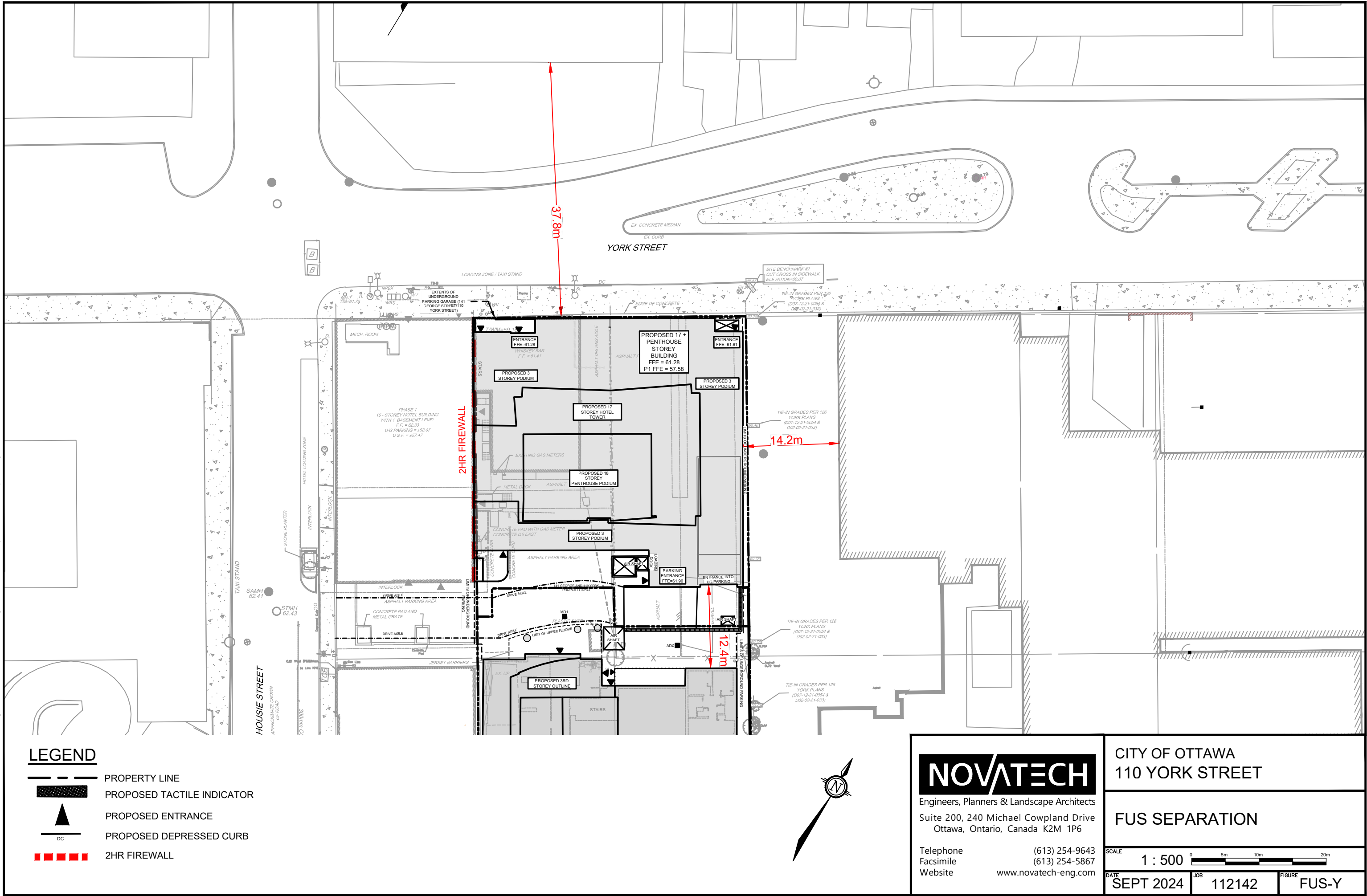
Do we have confirmation of retail area size (m2) for 141 George Street? I could take the area from CAD but figured I'd check for true value. Also under the assumption York Street component contains no retail. Please confirm.

Thanks,  
**Curtis Ferguson**, B.A.Sc., E.I.T. | Land Development

**NOVATECH**  
Engineers, Planners & Landscape Architects  
240 Michael Cowpland Drive, Suite 200, Ottawa, ON, K2M 1P6 | Tel: 613.254.9643 EXT: 331  
The information contained in this email message is confidential and is for exclusive use of the addressee.

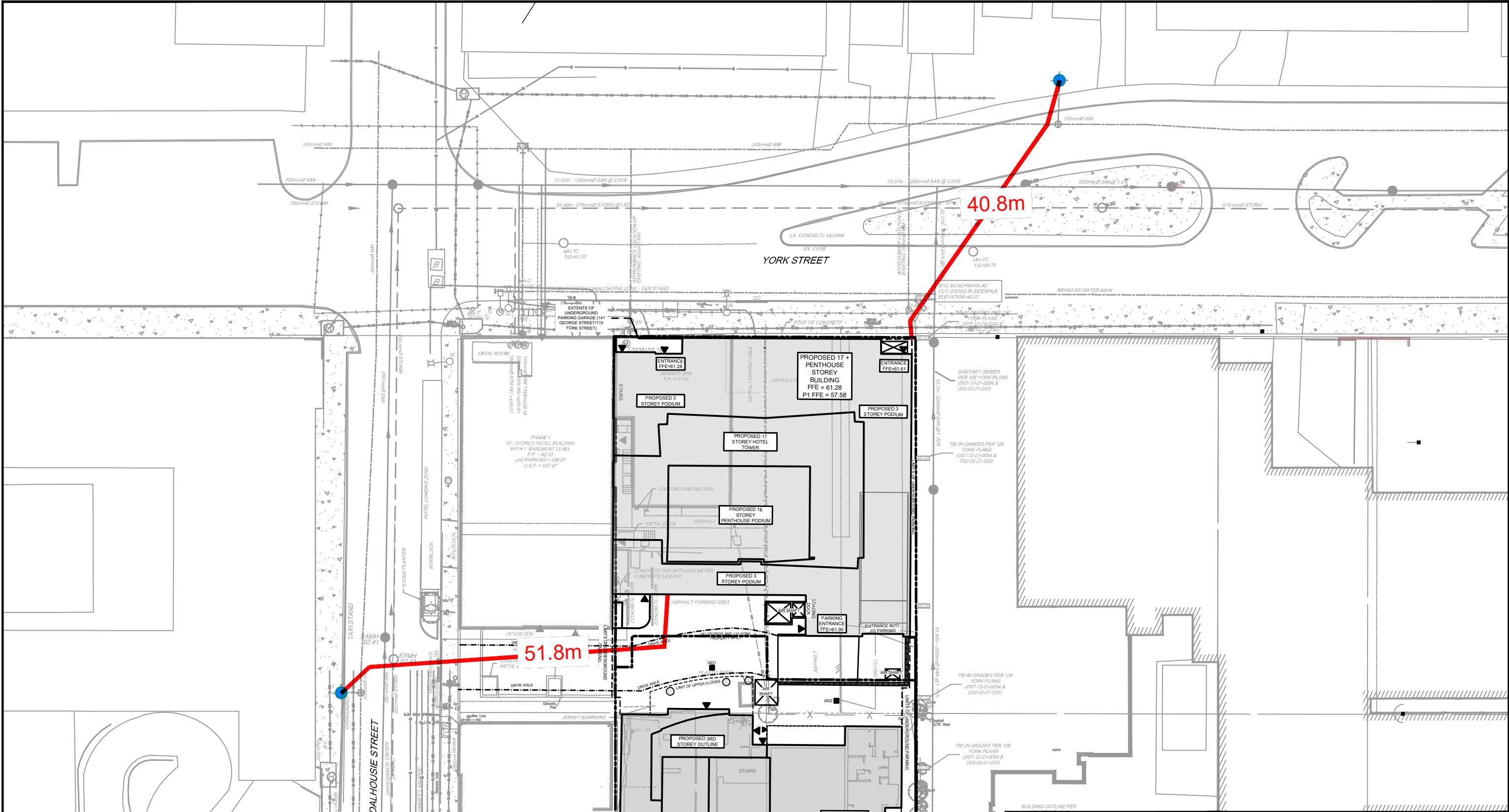


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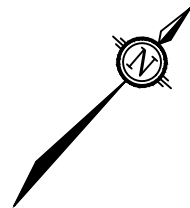


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## LEGEND

- PROPERTY LINE
- PROPOSED SIAMESE CONNECTION
- EXISTING CLASS AA HYDRANT
- PROPOSED HYDRANT
- DISTANCE FROM HYDRANT TO SIAMESE CONNECTION/ BUILDING ENTRANCE



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Telephone (613) 254-9643  
Facsimile (613) 254-5867  
Website [www.novatech-eng.com](http://www.novatech-eng.com)

CITY OF OTTAWA  
110 YORK STREET

## COVERAGE PLAN

SCALE 1 : 500

DATE SEPT 2024 JOB 112142 FIGURE COV-Y



# Water Demand Design Sheet

## Boundary Condition Request

**Novatech Project #:** 112142  
**Project Name:** 110 York Street  
**Date:** 9/20/2024  
**Input By:** Curtis Ferguson, E.I.T.  
**Reviewed By:** Greg MacDonald, P.Eng  
**Drawing Reference:**

**Legend:** Input by User No Input Required

Calculated Cells →

**Reference:** Ottawa Design Guidelines - Water Distribution (2010 and TBs)  
MOE Design Guidelines for Drinking-Water Systems (2008)  
Fire Underwriter's Survey Guideline (2020)  
Ontario Building Code, Part 3 (2012)

**Small System =** NO

	# of Dwellings	Area (ha.)	Pop. Equiv.	Average Day Demand (L/s)	Maximum Day Demand (L/s)	Peak Hour Demand (L/s)
<b>Residential Input</b>						
Singles			0.00	0.00	0.00	0.00
Semis / Townhomes			0.00	0.00	0.00	0.00
Apartments (2-BR)			0.00	0.00	0.00	0.00
Apartments (1-BR)			0.00	0.00	0.00	0.00
Hotel Rooms(Avg)	154		277.20	0.90	2.25	4.94
<b>Industrial / Commercial / Institutional (ICI) Input</b>						
Industrial Area - Light				0.00	0.00	0.00
Industrial Area - Heavy				0.00	0.00	0.00
Commercial Area		0.14		0.05	0.07	0.12
Institutional Area				0.00	0.00	0.00
Other Area				0.00	0.00	0.00
<b>Totals</b>	<b>154</b>	<b>0.14</b>	<b>277.20</b>	<b>0.94</b>	<b>2.31</b>	<b>5.07</b>

## Summary

i. Type of Development and Units:	
ii. Site Address:	
iii. Proposed Water Service Connection Location(s):	
Sketch	
iv. Average Day Flow Demand:	0.94 L/s
v. Peak Hour Flow Demand:	5.07 L/s
vi. Maximum Day Flow Demand:	2.31 L/s
vii. Required Fire Flow #1:	7000 L/min
viii. Required Fire Flow #2:	L/min
ix. Required Fire Flow #3:	L/min



## Design Parameters

Residential					
Unit Type Population Equiv.	Singles	Semis/ Towns	Apts (2-BR)	Apts (1-BR)	Hotel Room (Avg)
	3.4	2.7	2.1	1.4	1.8
Daily Demand	L/per person/day				
Average Demand	280				
Basic Demand	200				

Residential Peaking Factors		Max Day (x Avg Day)	Peak Hour (x Avg Day)
Small System (If Applicable)  <i>Modified</i>	Pop.		
	0	9.50	14.30
	30	9.50	14.30
	150	4.90	7.40
	300	3.60	5.50
	450	3.00	5.50
	500	2.90	5.50
Large System (Default)	> 500	2.50	5.50

Institutional / Commercial / Industrial				
Industrial		Commercial	Institutional	Other Use
Light	Heavy			
L/gross ha/day				L/m²/day
35,000	55,000	28,000	28,000	5
10,000	17,000	17,000	17,000	3

ICI Peaking Factors	Max Day (x Avg Day)	Peak Hour (x Avg Day)
	1.50	2.70



# FUS - Fire Flow Calculations

As per 2020 Fire Underwriter's Survey Guidelines



Engineers, Planners & Landscape Architects

Novatech Project #: 112142

Project Name: 110-116 York

Date: 9/25/2024

Input By: Curtis Ferguson, E.I.T.

Reviewed By: Anthony Mestwarp, P.Eng

Legend

Input by User

No Information or Input Required

Building Description: 17 + Penthouse Storey Mixed-Use Building

Type I - Fire resistive construction (2 hrs)

Step		Choose		Value Used	Total Fire Flow (L/min)
<b>Base Fire Flow</b>					
1	<b>Construction Material</b>		<b>Multiplier</b>		
	<b>Coefficient related to type of construction</b> <b>C</b>	Type V - Wood frame		1.5	0.6
		Type IV - Mass Timber		Varies	
		Type III - Ordinary construction		1	
		Type II - Non-combustible construction		0.8	
		Type I - Fire resistive construction (2 hrs)	Yes	0.6	
2	<b>Floor Area</b>				
	<b>A</b>	Podium Level Footprint (m <sup>2</sup> )	1427.95		
		Total Floors/Storeys (Podium)	2		
		Tower Footprint (m <sup>2</sup> )	615.04		
		Total Floors/Storeys (Tower)	15		
		Protected Openings (1 hr)	No		
		A, Total Effective Floor Area (m <sup>2</sup> )		5,316	
	<b>F</b>	<b>Base fire flow without reductions</b>			10,000
		<b>F = 220 C (A)<sup>0.5</sup></b>			
<b>Reductions or Surcharges</b>					
3	<b>Occupancy hazard reduction or surcharge</b>		<b>FUS Table 3</b>	<b>Reduction/Surcharge</b>	
	<b>(1)</b>	Non-combustible		-25%	-15%
		Limited combustible	Yes	-15%	
		Combustible		0%	
		Free burning		15%	
		Rapid burning		25%	
4	<b>Sprinkler Reduction</b>		<b>FUS Table 4</b>	<b>Reduction</b>	
	<b>(2)</b>	Adequately Designed System (NFPA 13)	Yes	-30%	-4,250
		Standard Water Supply	Yes	-10%	
		Fully Supervised System	Yes	-10%	
		<b>Cumulative Sub-Total</b>		-50%	
		<b>Area of Sprinklered Coverage (m<sup>2</sup>)</b>	12081.5	100%	
5	<b>Exposure Surcharge per</b>		<b>FUS Table 5</b>	<b>Surcharge</b>	
	<b>(3)</b>	North Side	>30m	0%	2,550
		East Side	10.1 - 20 m	15%	
		South Side	10.1 - 20 m	15%	
		West Side	>30m	0%	
		<b>Cumulative Total</b>		30%	
<b>Results</b>					
6	<b>(1) + (2) + (3)</b>	<b>Total Required Fire Flow, rounded to nearest 1000L/min</b>		<b>L/min</b>	<b>7,000</b>
		(2,000 L/min < Fire Flow < 45,000 L/min)		L/s	117
				USGPM	1,849
7	<b>Storage Volume</b>	Required Duration of Fire Flow (hours)		Hours	2
		Required Volume of Fire Flow (m <sup>3</sup> )		m <sup>3</sup>	840



# OBC Water Supply for Firefighting Calculation

Based on OBC 2012 (Div. B, Article 3.2.5.7)

References: [Ontario Fire Marshal - OBC Fire Fighting Water Supply](#)  
[Ontario Building Code 2012, Appendix A, Vol 2., A-3.2.5.7](#)



**Novatech Project #:** 112142  
**Project Name:** 110-116 York Street  
**Date:** 9/24/2024  
**Input By:** Curtis Ferguson, E.I.T.  
**Reviewed By:** Greg MacDonald, P.Eng.

Legend

Input by User

No Input Required

**Building Description:** 17 + Penthouse Storey Mixed-Use Building

Step	Calculation Inputs	Calculation Notes	Value
<b>Minimum Fire Protection Water Supply Volume</b>			
1	<b>Water Supply Coefficient</b> Building Classification = <b>Water Supply Coefficient - K =</b>	C From Table 3.1.2.1 From Table 1 (A3.2.5.7)	18
2	<b>Total Building Volume</b> Building Width - W Building Length - L Building Height - H <b>Total Building Volume - V =</b>	39.92 m 39.90 m 52.4 m W * L * H	83463 m <sup>3</sup>
3	<b>Spatial Coefficient Value</b> <b>Exposure Distances:</b> (Exterior building face to property/lot line, to street centre, or to mid-point between proposed building and another building on same lot) North East South West <b>Total of Spatial Coefficient Values - S-Tot</b> as obtained from the formula =	<b>Spatial Coefficients:</b> From Figure 1 (Spatial Coefficient vs Exposure Distance) Sside 1 = 0.00 Sside 2 = 0.00 Sside 3 = 0.00 Sside 4 = 0.00 1.0 + (Sside 1 + Sside 2 + Sside 3 + Sside 4) (Max. value = 2.0)	1.00
4	<b>Minimum Fire Protection Water Supply Volume</b> <b>Q =</b>	<b>K * V * S<sub>Tot</sub></b>	1,502,337 L
<b>Required Minimum Water Supply Flow Rate</b>			
5	<b>Minimum Water Supply Flow Rate</b> <b>=</b>	From Table 2 (For water supply from a municipal or industrial water supply system, min. pressure is 140 kPa) or	9,000 L/min 150 L/s
<b>Minimum Fire Protection Water Supply Volume for 30 minutes</b>			
6	<b>Q =</b>	<b>= Minimum Water Supply Flow Rate (L/min) * 30 minutes</b>	270,000 L
<b>Required Fire Protection Water Supply Volume</b>			
7	<b>Q =</b>	Highest volume out of (4) and (6)	1,502,337 L
Notes			

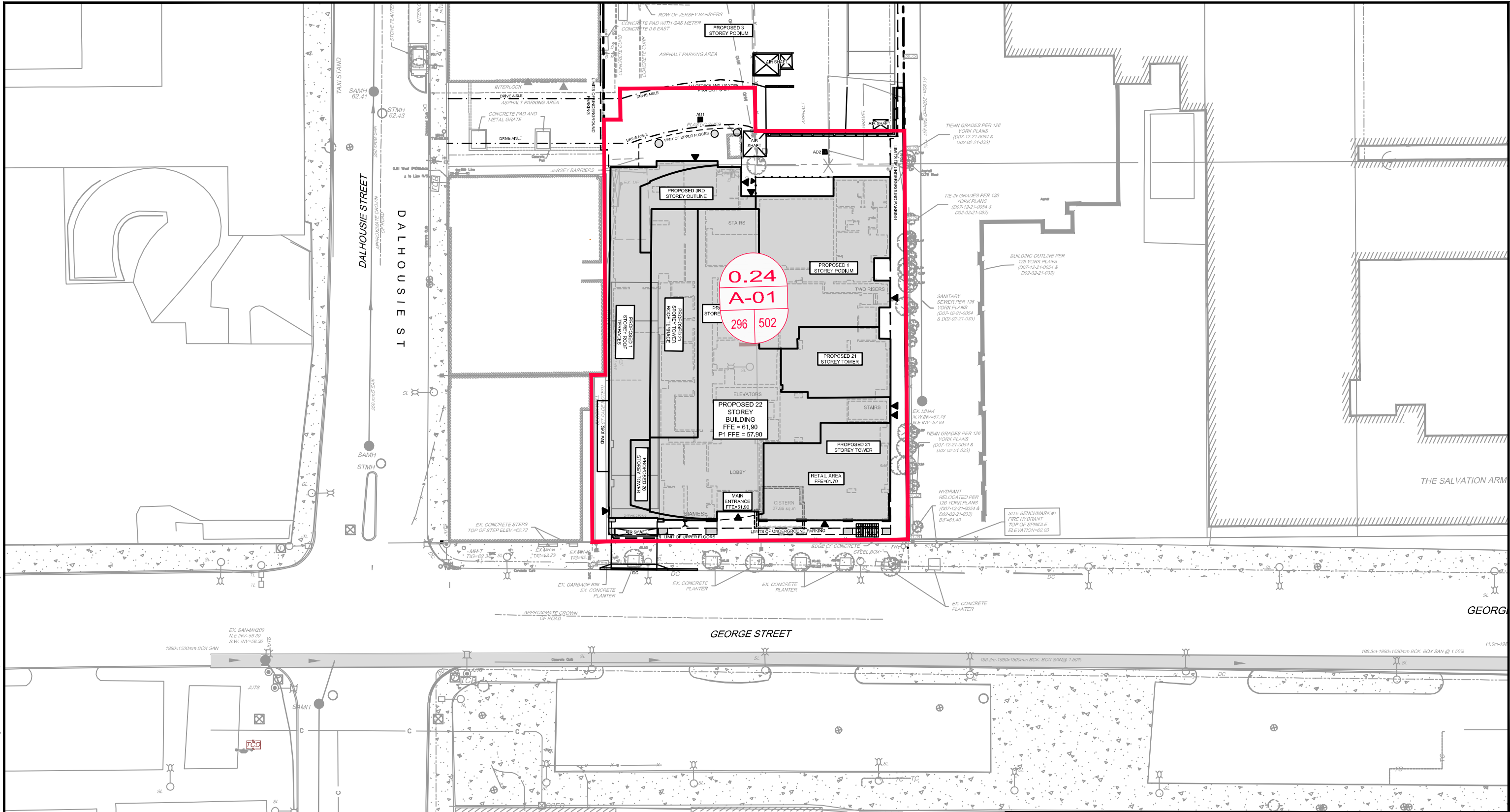


## **Appendix C**

### **Sanitary Servicing**



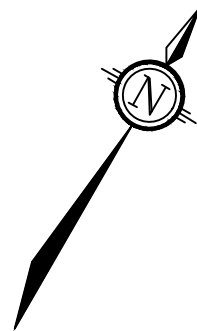
M:\2012\11\12142\141 GEORGE-110 YORK\CAD\Civil\112142-SAN-2.dwg, 112142-SAN, Sep 20, 2024 - 3:14pm, cferguson



- LEGEND**
- PROPERTY LINE
  - PROPOSED SANITARY SEWER AND MANHOLE
  - SAN MH* ● EXISTING SANITARY MANHOLE & SEWER
  - SANITARY SEWER DRAINAGE AREA BOUNDARY

0.47  
20A-19A  
71 128

DRAINAGE AREA (ha)  
SAN SEWER PIPE RUN  
NO. UNITS/POPULATION



**NOVATECH**  
Engineers, Planners & Landscape Architects  
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Ottawa, Ontario, Canada K2M 1P6  
Telephone (613) 254-9643  
Facsimile (613) 254-5867  
Website www.novatech-eng.com

141 GEORGE STREET  
**SANITARY DRAINAGE  
AREA PLAN**  
SCALE 1 : 500  
DATE SEPT 2024 JOB 112142 FIGURE SAN



Project Name: 141 George Street  
Date Prepared: 5/25/2023  
Date Revised: 9/24/2024  
Input By: Curtis Ferguson, E.I.T.  
Reviewed By: Greg MacDonald, P.Eng  
Drawing Reference: 112142 - SAN - 141 George Street

USER DESIGN INPUT  
CUMULATIVE CELL  
CALCULATED DESIGN CELL OUTPUT



Engineers, Planners & Landscape Architects

LOCATION			DEMAND										DESIGN CAPACITY															
AREA	FROM MH	TO MH	RESIDENTIAL FLOW									COMMERCIAL FLOW					EXTRANEOUS FLOW				PROPOSED SEWER PIPE SIZING / DESIGN							
			Studio	1 Bed Apartment	2 Bed / 1 Bed + Den Apartment	3 Bed / 2 Bed + Den Apartment	POPULATIO N (in 1000's)	CUMULATIVE POPULATION (in 1000's)	PEAK FACTOR M	AVG POPULATION FLOW (L/s)	PEAKED DESIGN POP FLOW (L/s)	COMMERICAL Area	CUMULATIVE COMMERICAL Area	DESIGN COMMERICAL FLOW (L/s)	COMMERICAL PEAK FACTOR	PEAKED COMMERCIAL FLOW	Total Area (ha.)	Accum. Area (ha.)	DESIGN EXTRAN. FLOW (L/s)	TOTAL DESIGN FLOW (L/s)	PIPE LENGTH (m)	PIPE SIZE (mm) AND MATERIAL	PIPE ID ACTUAL (m)	ROUGH. (n)	DESIGN GRADE (%)	CAPACITY (L/s)	FULL FLOW VELOCITY (m/s)	Qpeak Design Qcap
George Street																												
A-02	Stub	EX. 1980mm x 1500mm SAN	25	147	123	1	0.502	0.502	3.38	1.63	5.50	525.700	525.700	0.33	1.00	0.33	0.24	0.24	0.08	5.91	6.4	250 PVC	0.254	0.013	2.00	87.7	1.73	6.7%
TOTAL			25	147	123	1	0.502	0.502				525.700	525.700				0.24											

7. Commercial Flow

141 George

Use	Area (m2)	Use	Daily Demand Volume	Source
Office Area	72.70	Professional Office	75	L/9.3m2/day
Restaurant Area	453.00	Retail Restaurant	125	L/2m2/day
		Bar/ Cocktail Lounge (meeting/party room)	70	L/day/seat (1 seat/ 2m2)
Total Com Area	525.70	City of Ottawa Sewer Design Guidelines		
Total Com Daily Volume (L/s)	28898.79			

Design Parameters:							
1. Residential Flows				CAPACITY EQUATION			
-1 Bed Apartment / Studio	1.4	Person/ Unit		Q full= (1/n) A R^(2/3)So^(1/2)			
-2 Bed Apartment	2.1	Person/ Unit					
-3 Bed Apartment	3.1	Person/ Unit					
2. Commercial Flow				Where :	Q full = Capacity (L/s)		
-Restaurant/Lounge	125	L/day/seat					
3. q Avg capita flow	280	L/per/day					
4. M = Harmon Formula (maximum of 4.0)					n = Manning coefficient of roughness (0.013)		
5. K =	0.8				A = Flow area (m <sup>2</sup> )		
6. Commercial Peak Factor					R = Wetter perimenter (m)		
-area > 20% of development	1.5				So = Pipe Slope/gradient		
-area < 20% of development	1.0						
7. Extraneous Flows =	0.33	L/sec/ha					



Project Name: 110 York Street  
Date Prepared: 10/13/2023  
Date Revised: 9/25/2024  
Input By: Curtis Ferguson, E.I.T.  
Reviewed By: Greg MacDonald, P.Eng  
Drawing Reference: 112142 - SAN - 110 York Street

USER DESIGN INPUT  
CUMULATIVE CELL  
CALCULATED DESIGN CELL OUTPUT

LOCATION			DEMAND											DESIGN CAPACITY											
AREA	FROM MH	TO MH	RESIDENTIAL FLOW					COMMERCIAL FLOW					EXTRANEIOUS FLOW				PROPOSED SEWER PIPE SIZING / DESIGN								
			HOTEL ROOMS	POPULATION (in 1000's)	CUMULATIVE POPULATION (in 1000's)	PEAK FACTOR M	AVG POPULATION FLOW (L/s)	PEAKED DESIGN POP FLOW (L/s)	COMMERICAL Area	CUMULATIVE COMMERICAL Area	DESIGN COMMERICAL FLOW (L/s)	COMMERICAL PEAK FACTOR	PEAKED COMMERCIAL FLOW	Total Area (ha.)	Accum. Area (ha.)	DESIGN EXTRAN. FLOW (L/s)	TOTAL DESIGN FLOW (L/s)	PIPE LENGTH (m)	PIPE SIZE (mm) AND MATERIAL	PIPE ID ACTUAL (m)	ROUGH. (n)	DESIGN GRADE (%)	CAPACITY (L/s)	FULL FLOW VELOCITY (m/s)	Qpeak Design / Qcap
York Street																									
A-01	Stub	EX. 1200mm SAN	154	0.277	0.277	3.47	0.72	2.51	793.000	793.000	0.69	1.00	0.69	0.08	0.08	0.03	3.22	6.4	250 PVC	0.254	0.013	2.00	87.7	1.73	3.7%
TOTAL			154	0.277	0.277				793.000	793.000				0.08											

7. Commercial Flow					
110 York Street					
Use	Area (m2)	Use	Daily Demand Volume	Source	
Dance Hall (c/w restaurant & bar)	793.00	Dance Hall (c/w restaurant & bar)	150	L/day/patron (1 patron/ 2m2)	City of Ottawa Sewer Design Guidelines
Total Com Area	793.00				
Total Com Daily Volume (L/s)	59475.00				

Design Parameters:							
1. Residential Flows			CAPACITY EQUATION				
-Hotel Room	1.8	Person/ Unit	Q full= (1/n) A R^(2/3)So^(1/2)				
2. Commercial Flow			Where : Q full = Capacity (L/s)				
-Dance hall (c/w restaurant & bar)	150	L/day/patron					
3. q Avg Hotel flow ( With Full Housekeeping facilities	225	L/per/day					
4. M = Harmon Formula (maximum of 4.0)			n = Manning coefficient of roughness (0.013)				
5. K =	0.8		A = Flow area (m²)				
6. Commercial Peak Factor			R = Wetter perimenter (m)				
-area > 20% of development	1.5		So = Pipe Slope/gradient				
-area < 20% of development	1.0						
7. Extraneous Flows =	0.33	L/sec/ha					



## **Appendix D**

### **Storm Servicing**



**From:** Duquette, Vincent <[Vincent.Duquette@ottawa.ca](mailto:Vincent.Duquette@ottawa.ca)>

**Sent:** Friday, May 5, 2023 4:51 PM

**To:** Anthony Mestwarp <[a.mestwarp@novatech-eng.com](mailto:a.mestwarp@novatech-eng.com)>

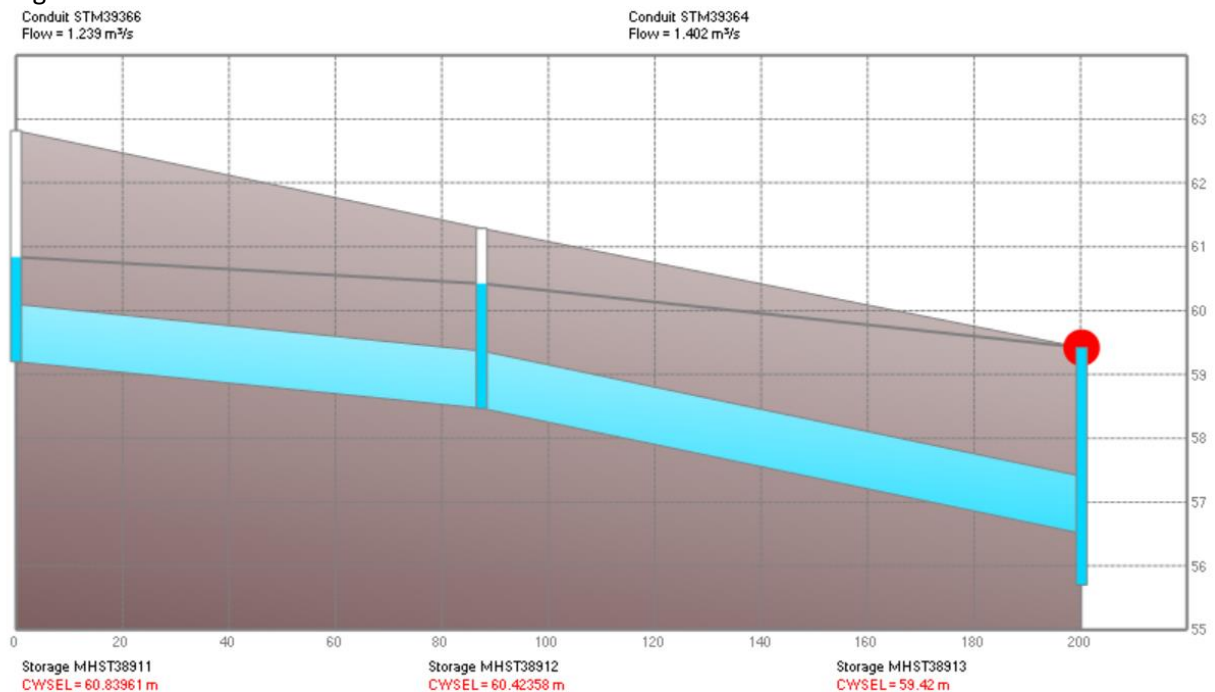
**Cc:** Mottalib, Abdul <[Abdul.Mottalib@ottawa.ca](mailto:Abdul.Mottalib@ottawa.ca)>; Wu, John <[John.Wu@ottawa.ca](mailto:John.Wu@ottawa.ca)>; Greg MacDonald <[g.Macdonald@novatech-eng.com](mailto:g.Macdonald@novatech-eng.com)>; Curtis Ferguson <[c.ferguson@novatech-eng.com](mailto:c.ferguson@novatech-eng.com)>

**Subject:** RE: 141 George Street - Phase 2 (112142)

Hi Anthony,

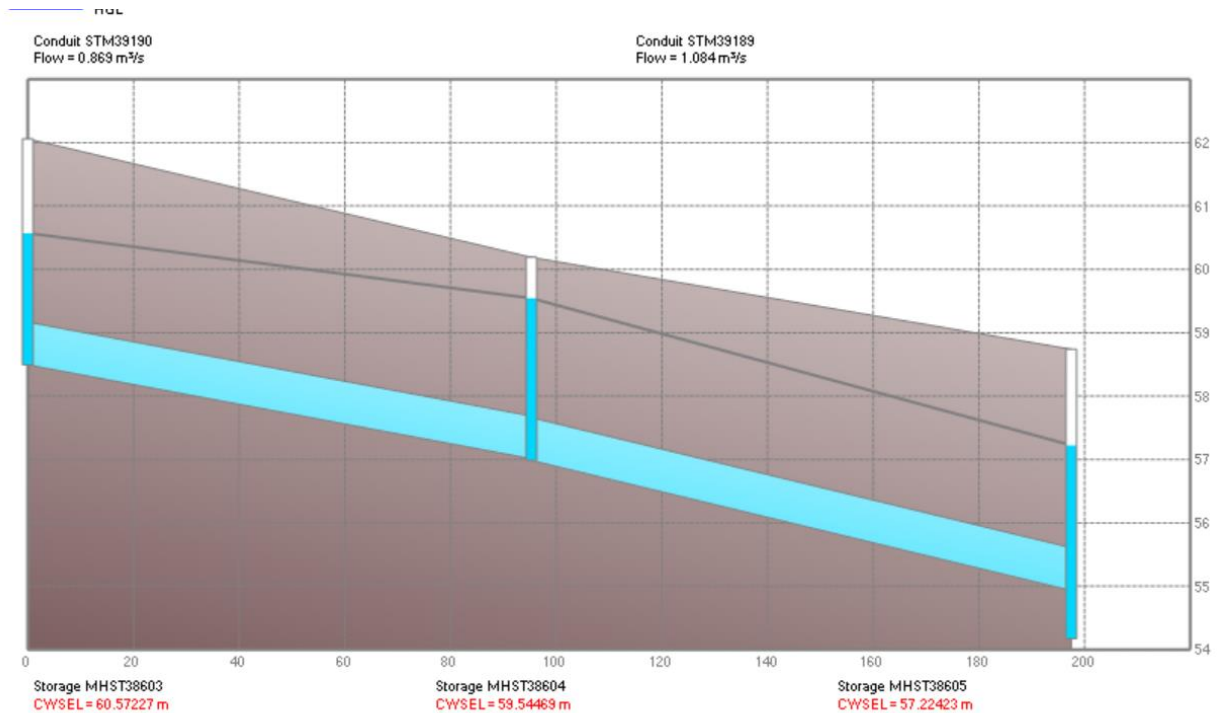
Please see below HGL requested. In these old uncontrolled systems, the 100-year HGL is expected to break out at the surface.

#### George between Dalhousie and Cumberland



#### York between Dalhousie and Cumberland





Best Regards,

**Vincent Duquette, E.I.T**

Project Manager, Infrastructure Approvals

Planning, Real Estate and Economic Development Department – Direction général de la planification,  
des biens immobilier et du développement économique

Development Review – Central Branch

City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1

613.580.2424 ext./poste 14048, [vincent.duquette@ottawa.ca](mailto:vincent.duquette@ottawa.ca)

**From:** Anthony Mestwarp <[a.mestwarp@novatech-eng.com](mailto:a.mestwarp@novatech-eng.com)>

**Sent:** April 28, 2023 5:20 PM

**To:** Duquette, Vincent <[Vincent.Duquette@ottawa.ca](mailto:Vincent.Duquette@ottawa.ca)>

**Cc:** Mottalib, Abdul <[Abdul.Mottalib@ottawa.ca](mailto:Abdul.Mottalib@ottawa.ca)>; Wu, John <[John.Wu@ottawa.ca](mailto:John.Wu@ottawa.ca)>; Greg MacDonald <[g.Macdonald@novatech-eng.com](mailto:g.Macdonald@novatech-eng.com)>; Curtis Ferguson <[c.ferguson@novatech-eng.com](mailto:c.ferguson@novatech-eng.com)>

**Subject:** RE: 141 George Street - Phase 2 (112142)

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Hi Vincent,

The requested PDF is attached.



I hope you have a good weekend.

Regards,

**Anthony Mestwarp**, P.Eng., Project Engineer | Land Development Engineering  
**NOVATECH**

Engineers, Planners & Landscape Architects

240 Michael Cowpland Drive, Suite 200, Ottawa, ON, K2M 1P6 | Tel: 613.254.9643 Ext. 216

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**From:** Duquette, Vincent <[Vincent.Duquette@ottawa.ca](mailto:Vincent.Duquette@ottawa.ca)>

**Sent:** Friday, April 28, 2023 4:13 PM

**To:** Anthony Mestwarp <[a.mestwarp@novatech-eng.com](mailto:a.mestwarp@novatech-eng.com)>

**Cc:** Mottalib, Abdul <[Abdul.Mottalib@ottawa.ca](mailto:Abdul.Mottalib@ottawa.ca)>; Wu, John <[John.Wu@ottawa.ca](mailto:John.Wu@ottawa.ca)>; Greg MacDonald <[g.Macdonald@novatech-eng.com](mailto:g.Macdonald@novatech-eng.com)>; Curtis Ferguson <[c.ferguson@novatech-eng.com](mailto:c.ferguson@novatech-eng.com)>

**Subject:** RE: 141 George Street - Phase 2 (112142)

Hi Anthony,

I will be reviewing this file in John's absence. Can you please forward me the pdf file highlighting the pipe segments that is mentioned in your previous email. I will then circulate it to asset management to obtain the HGL requested.

Best Regards,

**Vincent Duquette, E.I.T**

Project Manager, Infrastructure Approvals

Planning, Real Estate and Economic Development Department – Direction général de la planification, des biens immobilier et du développement économique

Development Review – Central Branch

City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1

613.580.2424 ext./poste 14048, [vincent.duquette@ottawa.ca](mailto:vincent.duquette@ottawa.ca)

**From:** Mottalib, Abdul <[Abdul.Mottalib@ottawa.ca](mailto:Abdul.Mottalib@ottawa.ca)>

**Sent:** April 28, 2023 10:59 AM

**To:** Duquette, Vincent <[Vincent.Duquette@ottawa.ca](mailto:Vincent.Duquette@ottawa.ca)>

**Cc:** Wu, John <[John.Wu@ottawa.ca](mailto:John.Wu@ottawa.ca)>; Greg MacDonald <[g.Macdonald@novatech-eng.com](mailto:g.Macdonald@novatech-eng.com)>; Curtis Ferguson <[c.ferguson@novatech-eng.com](mailto:c.ferguson@novatech-eng.com)>; Anthony Mestwarp <[a.mestwarp@novatech-eng.com](mailto:a.mestwarp@novatech-eng.com)>; Mottalib, Abdul <[Abdul.Mottalib@ottawa.ca](mailto:Abdul.Mottalib@ottawa.ca)>

**Subject:** RE: 141 George Street - Phase 2 (112142)

Hi Vincent ,

Please review it.



--

Thanks,

Abdul  
Mohammad Abdul Mottalib, P. Eng.  
Extension: 27798

**From:** Anthony Mestwarp <[a.mestwarp@novatech-eng.com](mailto:a.mestwarp@novatech-eng.com)>  
**Sent:** April 28, 2023 10:15 AM  
**To:** Mottalib, Abdul <[Abdul.Mottalib@ottawa.ca](mailto:Abdul.Mottalib@ottawa.ca)>  
**Cc:** Wu, John <[John.Wu@ottawa.ca](mailto:John.Wu@ottawa.ca)>; Greg MacDonald <[g.Macdonald@novatech-eng.com](mailto:g.Macdonald@novatech-eng.com)>; Curtis Ferguson <[c.ferguson@novatech-eng.com](mailto:c.ferguson@novatech-eng.com)>  
**Subject:** FW: 141 George Street - Phase 2 (112142)

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Hi Abdul,

I understand that John is currently out of the office.

Can you please review the below?

Thanks,

**Anthony Mestwarp**, P.Eng., Project Engineer | Land Development Engineering  
**NOVATECH**

Engineers, Planners & Landscape Architects

240 Michael Cowpland Drive, Suite 200, Ottawa, ON, K2M 1P6 | Tel: 613.254.9643 Ext. 216

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**From:** Anthony Mestwarp  
**Sent:** Friday, April 28, 2023 10:10 AM  
**To:** Wu, John <[John.Wu@ottawa.ca](mailto:John.Wu@ottawa.ca)>  
**Cc:** Greg MacDonald <[g.Macdonald@novatech-eng.com](mailto:g.Macdonald@novatech-eng.com)>; Curtis Ferguson <[c.ferguson@novatech-eng.com](mailto:c.ferguson@novatech-eng.com)>  
**Subject:** 141 George Street - Phase 2 (112142)

Hi John,

We are working on the design of 141 George Street Phase 2 and would like to confirm the existing storm sewer HGL within the city infrastructure neighboring the site, to ensure there will not be any backflow issues on the proposed connections.



Can you please confirm who would be the engineering reviewer for this project, and if required forward this email to the appropriate contact.

**York Street:**

Can you please confirm the existing HGL within the 675mm concrete storm sewer within York street between manholes MHST38603 and MHST38604 as highlighted on the attached PDF.

**George Street:**

Can you please confirm the existing HGL within the 900mm concrete storm sewer within York street between manholes MHST38911 and MHST38912 as highlighted on the attached PDF.

Thanks,

**Anthony Mestwarp**, P.Eng., Project Engineer | Land Development Engineering

**NOVATECH**

Engineers, Planners & Landscape Architects

240 Michael Cowpland Drive, Suite 200, Ottawa, ON, K2M 1P6 | Tel: 613.254.9643 Ext. 216

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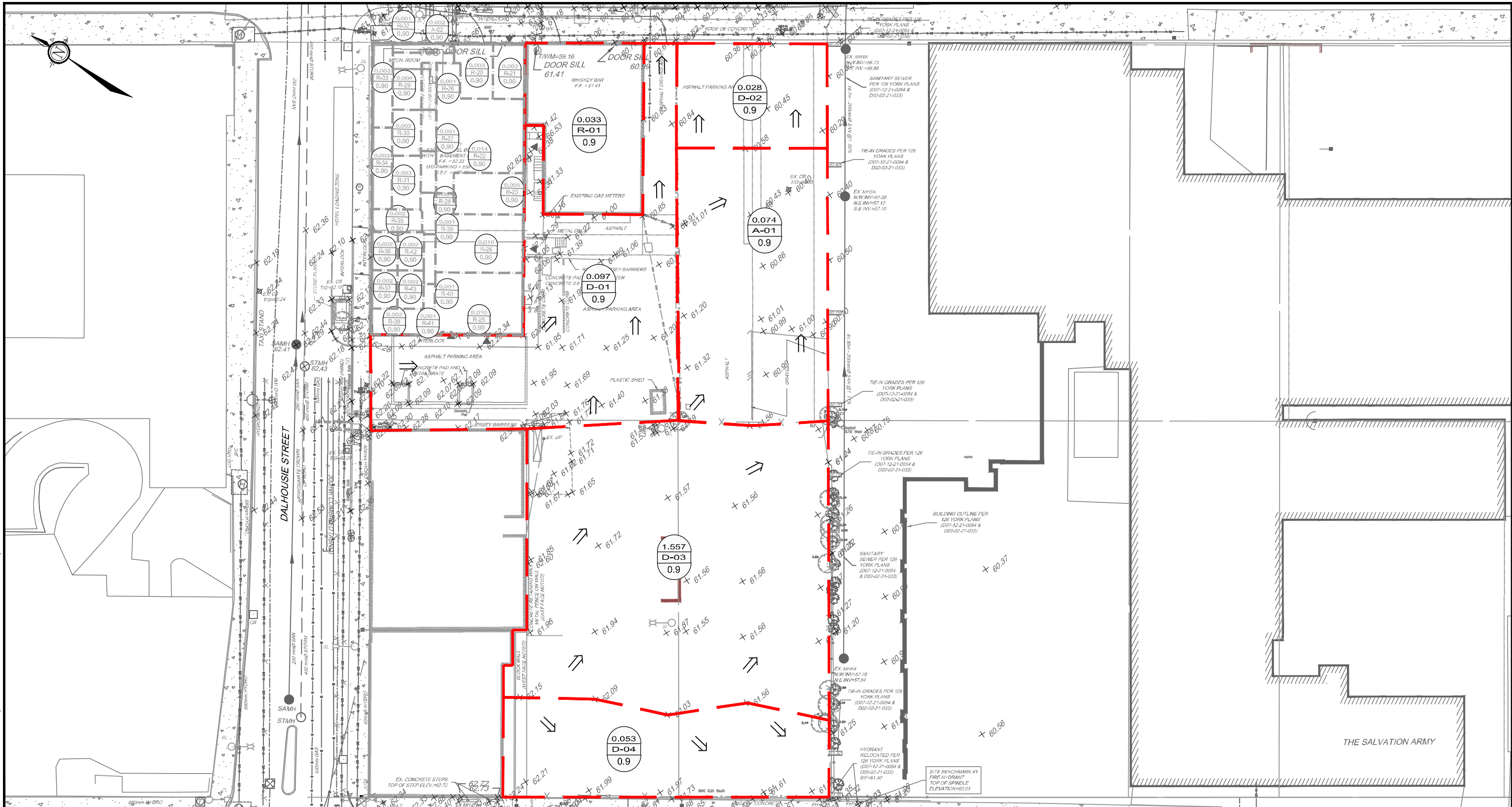
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,



M:\2012\112142\_110 GEORGE-110 YORK\CAD\Civil\112142-2-PRESTIM-Y.dwg, PRE FLOWS, Sep 19, 2024 - 2:35pm, cferguson



## LEGEND

<div><div>0.03</div><div>R-01</div><div>0.9</div></div>	DRAINAGE AREA
<div><div>0.03</div><div>R-01</div><div>0.9</div></div>	AREA ID
<div><div>0.03</div><div>R-01</div><div>0.9</div></div>	C VALUE
<div><div>0.03</div><div>R-01</div><div>0.9</div></div>	PROPOSED STORM DRAINAGE AREA
<div><div>0.03</div><div>R-01</div><div>0.9</div></div>	EXISTING CATCHBASIN
<div><div>0.03</div><div>R-01</div><div>0.9</div></div>	EXISTING GRADES

**NOVATECH**

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Facsimile (613) 254-5867  
Website [www.novatech-eng.com](http://www.novatech-eng.com)

141 GERGE, 110 & 116  
YORK

PRE DEVELOPMENT  
DRAINAGE FLOWS

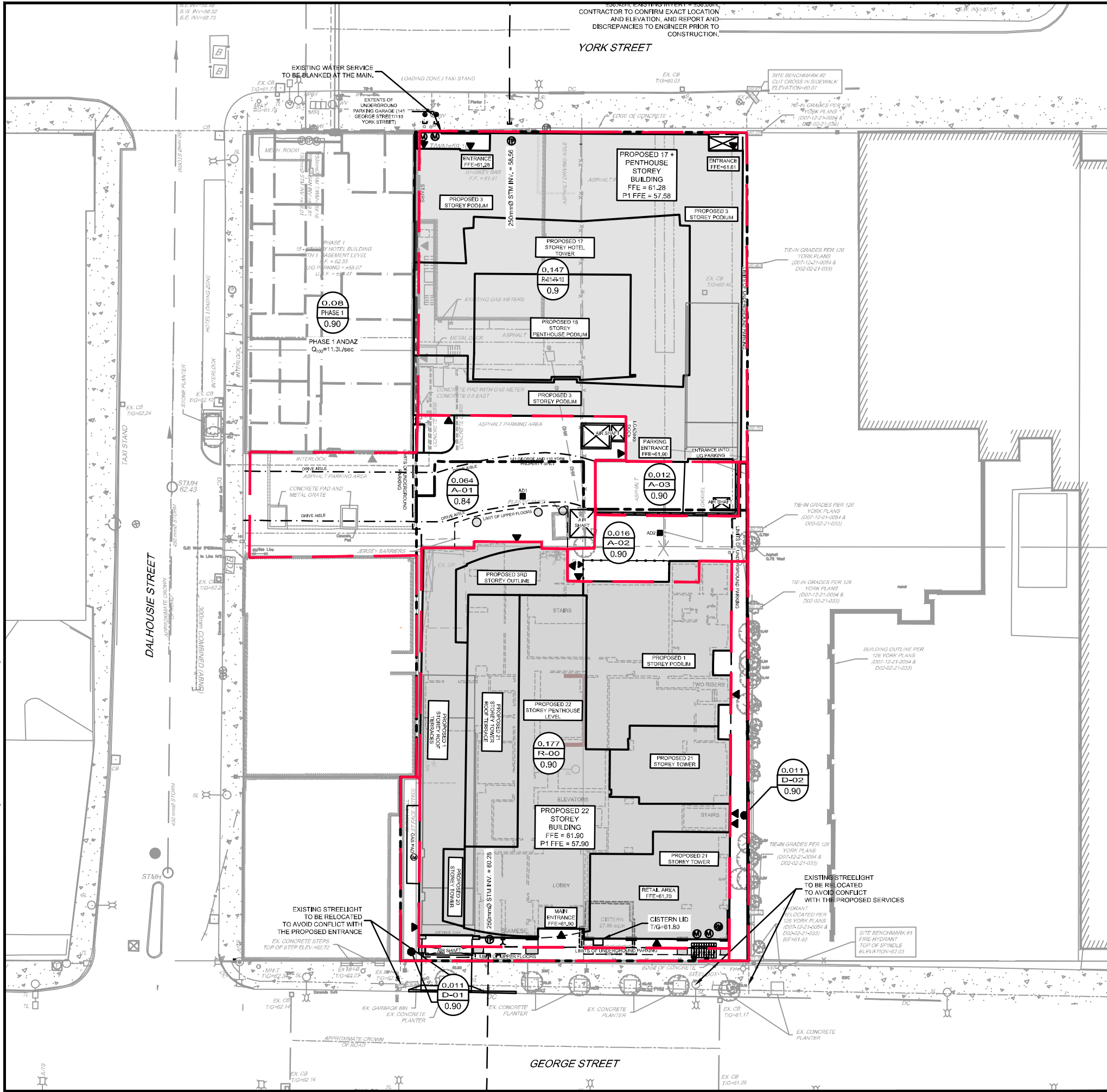
SCALE 1 : 500

DATE SEP 2024 JOB 112142 FIGURE PRE-STIM

SUT11Y17 DWG 270mm X 122mm

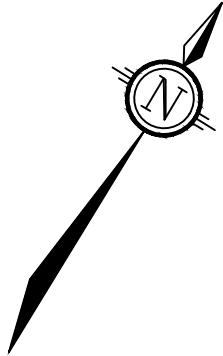


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LEGEND

- DRAINAGE AREA LIMITS
- DRAINAGE AREA (ha)  
DRAINAGE AREA ID  
RUNOFF COEFFICIENT
- PROPERTY LINE
- PROPOSED CURB
- PROPOSED DEPRESSED CURB
- PROPOSED RETAINING WALL C/W GUARD RAIL
- PROPOSED STORM SEWER AND MANHOLE
- PROPOSED AREA DRAIN
- PROPOSED TRENCH DRAIN
- PROPOSED BUILDING ENTRANCE
- EXISTING STORM MANHOLE & SEWER
- EXISTING CATCHBASIN



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Ottawa, Ontario, Canada K2M 1P6

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Facsimile (613) 254-5867  
Website www.novatech-eng.com

CITY OF OTTAWA  
141 GEORGE STREET & 110 YORK

POST-DEVELOPMENT  
STORMWATER MANAGEMENT PLAN

SCALE 1 : 500

DATE SEPT 2024 JOB 112142 FIGURE SWM



TABLE 1A: Allowable Runoff Coefficient "C"

Area*	"C"
Total	0.50
0.438	

TABLE 1B: Allowable Flows

Outlet Options	Area (ha)	"C"	Tc (min)	Q <sub>5 Year</sub> (L/s)	Q <sub>ALLOW</sub> (L/s)
George Street / York Street	0.438	0.50	20	42.8	42.8

Time of Concentration	Tc=	20	min
Intensity (2 Year Event)	I <sub>2</sub> =	52.03	mm/hr
Intensity (5 Year Event)	I <sub>5</sub> =	70.25	mm/hr
Intensity (100 Year Event)	I <sub>100</sub> =	119.95	mm/hr

100 year Intensity =  $1735.688 / (\text{Time in min} + 6.014)^{0.820}$   
5 year Intensity =  $998.071 / (\text{Time in min} + 6.053)^{0.814}$

Equations:  
Flow Equation  
 $Q = 2.78 \times C \times I \times A$   
Where:  
C is the runoff coefficient  
I is the rainfall intensity, City of Ottawa IDF  
A is the total drainage area



**TABLE 2A: Post-Development Runoff Coefficient "C" - D-01 - Uncontrolled Flow**

Area	Surface	Ha	"C"	C <sub>avg</sub>	*C <sub>100</sub>	Runoff Coefficient Equation
Total	Hard	0.011	0.90	0.90	1.00	$C = (A_{hard} \times 0.9 + A_{soft} \times 0.2) / A_{Tot}$ * Runoff Coefficient increases by 25% up to a maximum value of 1.00 for the 100-Year event
0.011	Soft	0.000	0.20			

**TABLE 2B: Post-Development D-01 Flows**

Outlet Options	Area (ha)	C <sub>avg</sub>	Tc (min)	Q <sub>2 Year</sub> (L/s)	Q <sub>5 Year</sub> (L/s)	Q <sub>100 Year</sub> (L/s)
George Street	0.011	0.90	10	2.2	2.9	5.6

Time of Concentration Tc= 10 min  
 Intensity (2 Year Event) I<sub>2</sub>= 76.81 mm/hr  
 Intensity (5 Year Event) I<sub>5</sub>= 104.19 mm/hr  
 Intensity (100 Year Event) I<sub>100</sub>= 178.56 mm/hr

Equations:  
 Flow Equation  
 $Q = 2.78 \times C \times I \times A$

Where:  
 C is the runoff coefficient  
 I is the rainfall intensity, City of Ottawa IDF  
 A is the total drainage area

100 year Intensity =  $1735.688 / (\text{Time in min} + 6.014)^{0.820}$   
 5 year Intensity =  $998.071 / (\text{Time in min} + 6.053)^{0.814}$   
 2 year Intensity =  $732.951 / (\text{Time in min} + 6.199)^{0.810}$



**TABLE 3A: Post-Development Runoff Coefficient "C" - D-02 - Uncontrolled Flow**

Area	Surface	Ha	"C"	C <sub>avg</sub>	*C <sub>100</sub>	Runoff Coefficient Equation
Total	Hard	0.011	0.90	0.90	1.00	$C = (A_{\text{hard}} \times 0.9 + A_{\text{soft}} \times 0.2) / A_{\text{Tot}}$ * Runoff Coefficient increases by 25% up to a maximum value of 1.00 for the 100-Year event
0.011	Soft	0.000	0.20			

**TABLE 3B: Post-Development D-01 Flows**

Outlet Options	Area (ha)	C <sub>avg</sub>	Tc (min)	Q <sub>2 Year</sub> (L/s)	Q <sub>5 Year</sub> (L/s)	Q <sub>100 Year</sub> (L/s)
George Street	0.011	0.90	10	2.0	2.8	5.3

Time of Concentration Tc= 10 min  
 Intensity (2 Year Event) I<sub>2</sub>= 76.81 mm/hr  
 Intensity (5 Year Event) I<sub>5</sub>= 104.19 mm/hr  
 Intensity (100 Year Event) I<sub>100</sub>= 178.56 mm/hr

Equations:  
 Flow Equation  
 $Q = 2.78 \times C \times I \times A$

Where:  
 C is the runoff coefficient  
 I is the rainfall intensity, City of Ottawa IDF  
 A is the total drainage area

100 year Intensity =  $1735.688 / (\text{Time in min} + 6.014)^{0.820}$   
 5 year Intensity =  $998.071 / (\text{Time in min} + 6.053)^{0.814}$   
 2 year Intensity =  $732.951 / (\text{Time in min} + 6.199)^{0.810}$



**TABLE 6A: Post-Development Runoff Coefficient "C" - A-01,A-03**

Area	Surface	Ha	5 Year Event		100 Year Event	
			"C"	C <sub>avg</sub>	"C" + 25%	*C <sub>avg</sub>
Total	Hard	-0.007	0.90	0.84	1.00	0.94
0.075	Roof	0.076	0.90		1.00	
	Soft	0.006	0.20		0.25	

**TABLE 6B: 2 YEAR EVENT QUANTITY STORAGE REQUIREMENT - A-01,A-03**

0.075 =Area (ha)

0.84 = C

Return Period	Time (min)	Intensity (mm/hr)	Flow Q (L/s)	Allowable Runoff (L/s)	Net Flow to be Stored (L/s)	Storage Req'd (m <sup>3</sup> )
2 YEAR	-5	632.75	111.84	10.6	101.24	-30.37
	0	167.22	29.56	10.6	18.96	0.00
	5	103.57	<b>18.31</b>	<b>10.6</b>	<b>7.71</b>	<b>2.31</b>
	10	76.81	13.58	10.6	2.98	1.79
	15	61.77	10.92	10.6	0.32	0.29

**TABLE 6C: 5 YEAR EVENT QUANTITY STORAGE REQUIREMENT - A-01,A-03**

0.075 =Area (ha)

0.84 = C

Return Period	Time (min)	Intensity (mm/hr)	Flow Q (L/s)	Allowable Runoff (L/s)	Net Flow to be Stored (L/s)	Storage Req'd (m <sup>3</sup> )
5 YEAR	0	230.48	40.74	10.6	30.14	0.00
	5	141.18	24.95	10.6	14.35	4.31
	10	<b>104.19</b>	<b>18.42</b>	<b>10.6</b>	<b>7.82</b>	<b>4.69</b>
	15	83.56	14.77	10.6	4.17	3.75
	20	70.25	12.42	10.6	1.82	2.18

**TABLE 6D: 100 YEAR EVENT QUANTITY STORAGE REQUIREMENT - A-01,A-03**

0.075 =Area (ha)

0.94 = C

Return Period	Time (min)	Intensity (mm/hr)	Flow Q (L/s)	Allowable Runoff (L/s)*	Net Flow to be Stored (L/s)	Storage Req'd (m <sup>3</sup> )
100 YEAR	5	242.70	47.77	10.6	37.17	11.15
	10	178.56	35.15	10.6	24.55	14.73
	15	<b>142.89</b>	<b>28.13</b>	<b>10.6</b>	<b>17.53</b>	<b>15.78</b>
	20	119.95	23.61	10.6	13.01	15.61
	25	103.85	20.44	10.6	9.84	14.76

**Equations:**

Flow Equation

$$Q = 2.78 \times C \times I \times A$$

Where:

C is the runoff coefficient

I is the rainfall intensity, City of Ottawa IDF

A is the total drainage area

Runoff Coefficient Equation

$$C_s = (A_{\text{hard}} \times 0.9 + A_{\text{soft}} \times 0.2) / A_{\text{Tot}}$$

$$C_{100} = (A_{\text{hard}} \times 1.0 + A_{\text{soft}} \times 0.25) / A_{\text{Tot}}$$



TABLE 6F: Structure information - A-01, A-03

Structures	Size Dia.(mm)	Area (m <sup>2</sup> )	T/G	Bottom of Tank
Tank	-	10.00	60.66	58.07

TABLE 6G: Storage Provided - A-01,A-03

Storage Table		
Elevation (m)	System Depth (m)	Tank Volume (m <sup>3</sup> )
58.07	0.00	0.00
58.165	0.10	1.00
58.265	0.20	2.00
58.365	0.30	3.00
58.465	0.40	4.00
58.565	0.50	5.00
58.665	0.60	6.00
58.765	0.70	7.00
58.865	0.80	8.00
58.965	0.90	9.00
59.065	1.00	10.00
59.165	1.10	11.00
59.265	1.20	12.00
59.365	1.30	13.00
59.465	1.40	14.00
59.565	1.50	15.00
59.665	1.60	16.00
59.765	1.70	17.00
59.865	1.80	18.00
59.965	1.90	19.00
60.065	2.00	20.00
60.165	2.10	21.00
60.265	2.20	22.00
60.365	2.30	23.00
60.465	2.40	24.00
60.565	2.50	25.00
60.665	2.60	26.00
60.765	2.70	27.00
60.865	2.80	28.00
60.965	2.90	29.00
61.065	3.00	30.00
61.165	3.10	31.00
61.265	3.20	32.00

Top of Tank

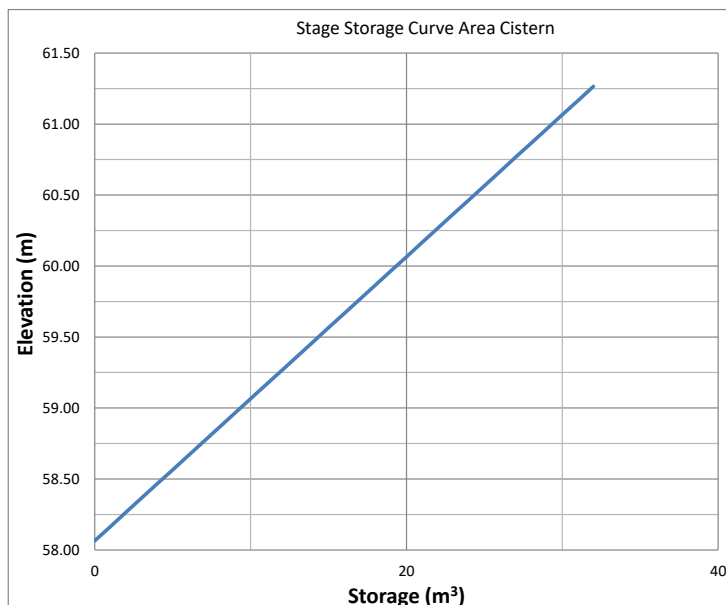


TABLE 3G: Orifice Sizing information - A-01, A-03

Control Device					
Pump					
Design Event	Flow (L/S)	Head (m)	Elev (m)	Outlet dia. (mm)	Volume (m³)
1:2 Year	10.6	TBD	TBD	250.00	2.31
1:5 Year	10.6	TBD	TBD	250.00	4.69
1:100 Year	10.6	TBD	TBD	250.00	15.78

\*\*The design Head is calculated based on the centre of the pipe



**TABLE 4A: Post-Development Runoff Coefficient "C" - A-02,R-00 - George Cistern**

Area	Surface	Ha	5 Year Event		100 Year Event	
			"C"	C <sub>avg</sub>	"C" + 25%	*C <sub>avg</sub>
Total	Hard	0.016	0.90	0.90	1.00	1.00
0.193	Roof	0.177	0.90		1.00	
	Soft	0.000	0.20		0.25	

**TABLE 4B: 2 YEAR EVENT QUANTITY STORAGE REQUIREMENT - A-02,R-01**

0.193 =Area (ha)  
 0.90 = C

Return Period	Time (min)	Intensity (mm/hr)	Flow Q (L/s)	Allowable Runoff (L/s)	Net Flow to be Stored (L/s)	Storage Req'd (m <sup>3</sup> )
2 YEAR	10	76.81	37.10	11.3	25.80	15.48
	15	61.77	29.84	11.3	18.54	16.68
	<b>20</b>	<b>52.03</b>	<b>25.13</b>	<b>11.3</b>	<b>13.83</b>	<b>16.60</b>
	25	45.17	21.82	11.3	10.52	15.78
	30	40.04	19.34	11.3	8.04	14.48

**TABLE 4C: 5 YEAR EVENT QUANTITY STORAGE REQUIREMENT - A-02,R-01**

0.193 =Area (ha)  
 0.90 = C

Return Period	Time (min)	Intensity (mm/hr)	Flow Q (L/s)	Allowable Runoff (L/s)	Net Flow to be Stored (L/s)	Storage Req'd (m <sup>3</sup> )
5 YEAR	15	83.56	40.36	11.3	29.06	26.16
	20	70.25	33.94	11.3	22.64	27.16
	<b>25</b>	<b>60.90</b>	<b>29.42</b>	<b>11.3</b>	<b>18.12</b>	<b>27.17</b>
	30	53.93	26.05	11.3	14.75	26.55
	35	48.52	23.44	11.3	12.14	25.49

**TABLE 4D: 100 YEAR EVENT QUANTITY STORAGE REQUIREMENT - A-02,R-01**

0.193 =Area (ha)  
 1.00 = C

Return Period	Time (min)	Intensity (mm/hr)	Flow Q (L/s)	Allowable Runoff (L/s)*	Net Flow to be Stored (L/s)	Storage Req'd (m <sup>3</sup> )
100 YEAR	30	91.87	49.31	11.3	38.01	68.42
	35	82.58	44.32	11.3	33.02	69.35
	<b>40</b>	<b>75.15</b>	<b>40.33</b>	<b>11.3</b>	<b>29.03</b>	<b>69.68</b>
	45	69.05	37.06	11.3	25.76	69.56
	50	63.95	34.33	11.3	23.03	69.08

**Equations:**

Flow Equation  
 $Q = 2.78 \times C \times I \times A$

Where:

C is the runoff coefficient  
 I is the rainfall intensity, City of Ottawa IDF  
 A is the total drainage area

**Runoff Coefficient Equation**

$$C_s = (A_{\text{hard}} \times 0.9 + A_{\text{soft}} \times 0.2) / A_{\text{Tot}}$$

$$C_{100} = (A_{\text{hard}} \times 1.0 + A_{\text{soft}} \times 0.25) / A_{\text{Tot}}$$

George Street Flow - Reference "Technical Memorandum 110 York Street & 141 George Street Serviceability Memo", Revised: March 12th, 2023  
 Note: Runoff / pump rate was increased by 1.3L/s to accommodate additional stormwater runoff from 116 York.

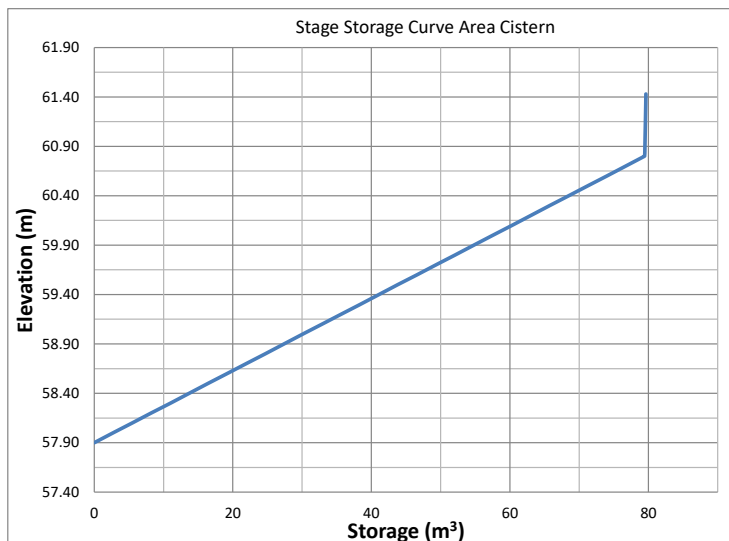


TABLE 4F: Structure information - A-02,R-01

Structures	Size Dia.(mm)	Area (m <sup>2</sup> )	T/G	Bottom of Tank
Tank	-	27.40	61.80	57.90

TABLE 4G: Storage Provided - A-02,R-01

Storage Table		
Elevation (m)	System Depth (m)	Tank Volume (m <sup>3</sup> )
57.90	0.00	0.00
58.000	0.10	2.74
58.100	0.20	5.48
58.200	0.30	8.22
58.300	0.40	10.96
58.400	0.50	13.70
58.500	0.60	16.44
58.600	0.70	19.18
58.700	0.80	21.92
58.800	0.90	24.66
58.900	1.00	27.40
59.000	1.10	30.14
59.100	1.20	32.88
59.200	1.30	35.62
59.300	1.40	38.36
59.400	1.50	41.10
59.500	1.60	43.84
59.600	1.70	46.58
59.700	1.80	49.32
59.800	1.90	52.06
59.900	2.00	54.80
60.000	2.10	57.54
60.100	2.20	60.28
60.200	2.30	63.02
60.300	2.40	65.76
60.400	2.50	68.50
60.500	2.60	71.24
60.600	2.70	73.98
60.700	2.80	76.72
60.800	2.90	79.46
60.830	2.93	79.47
60.930	3.03	79.50
61.030	3.13	79.53
61.130	3.23	79.55
61.230	3.33	79.58
61.330	3.43	79.61
61.430	3.53	79.64



Top of Tank (underside)

TABLE 4G: Orifice Sizing information - A-02,R-01

Control Device					
PUMP					
Design Event	Flow (L/S)	Head (m)	Elev (m)	Outlet dia. (mm)	Volume (m³)
1:2 Year	11.3	0.48	58.51	250.00	16.60
1:5 Year	11.3	0.88	58.90	250.00	27.17
1:100 Year	11.3	2.39	60.41	250.00	69.68

\*\*The design Head is calculated based on the centre of the pipe

George Street Flow - Reference "Technical Memorandum 110 York Street & 141 George Street Serviceability Memo", Revised: March 12th, 2024

Note: Runoff / pump rate was increased by 1.3L/s to accomdate additional stromwater runoff from 116 York.



Table 6.1: Post-Development Stormwater Management Summary

Area ID	Area (ha)	1:5 Year Weighted Cw	1:100 Year Weighted Cw	Control Device	Outlet Location	2 Year Storm Event				5 Year Storm Event				100 Year Storm Event			
						Release (L/s)	Ponding Depth (m)	Req'd Vol (cu.m)	Max. Vol. Provided (cu.m.)	Release (L/s)	Ponding Depth (m)	Req'd Vol (cu.m)	Max. Vol. Provided (cu.m.)	Release (L/s)	Ponding Depth (m)	Req'd Vol (cu.m)	Max. Vol. Provided (cu.m.)
D-01	0.011	0.90	1.00	N/A	George Street	2.20	N/A	N/A	N/A	2.90	N/A	N/A	N/A	5.60	N/A	N/A	N/A
D-02	0.011	0.90	1.00	N/A	George Street	2.00	N/A	N/A	N/A	2.80	N/A	N/A	N/A	5.30	N/A	N/A	N/A
R-01	0.015	0.90	1.00	Watts Roof Drain	York Street	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD
R-02	0.015	0.90	1.00	Watts Roof Drain	York Street	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD
R-03	0.015	0.90	1.00	Watts Roof Drain	York Street	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD
R-04	0.015	0.90	1.00	Watts Roof Drain	York Street	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD
R-05	0.015	0.90	1.00	Watts Roof Drain	York Street	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD
R-06	0.015	0.90	1.00	Watts Roof Drain	York Street	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD
R-07	0.015	0.90	1.00	Watts Roof Drain	York Street	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD
R-08	0.015	0.90	1.00	Watts Roof Drain	York Street	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD
R-09	0.015	0.90	1.00	Watts Roof Drain	York Street	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD
R-10	0.015	0.90	1.00	Watts Roof Drain	York Street	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD	1.00	TBD	TBD	TBD
A-03 / AD-01 (A-01)	0.075	0.84	0.94	Pump	York Street	10.60	TBD	2.31	26.00	10.60	TBD	4.69	26.00	10.60	TBD	15.78	26.00
R-00 / AD-02 (A-02)	0.193	0.90	1.00	Pump	George Street	11.30	0.485	16.60	79.64	11.30	0.875	27.17	79.64	11.30	2.385	69.68	79.64
<b>Post-Development Flow</b>						<b>36.1</b>	<b>-</b>	<b>18.9</b>	<b>105.6</b>	<b>37.6</b>	<b>-</b>	<b>31.9</b>	<b>105.6</b>	<b>42.8</b>	<b>-</b>	<b>85.5</b>	<b>105.6</b>
<b>Total Allowable Release Rate</b>						<b>42.8</b>				<b>42.8</b>				<b>42.8</b>			

**Notes:**

D-01 and D-02 are uncontrolled flows from 141 George to George Street  
AD-02 (A-02) and R-00 are flows to Geroge Cistern  
A-03 and AD-01 (A-01) are flows to York cistern  
R-01 to R-10 are controlled flows to service the future building at 110-116 York which will discharge directly to storm sewer on York

**Interim Condition 110-116 York**

In the interim , e.g. pending the construction of 110-116 York and the roof top controls & cistern, it is proposed to sheet drain the area to a catch basin which will connect to the York Street Sewer. The catch basin will be incorporated into the future cistern. As the existng area is hard surface and curently drains to York post-development will not exceed predevelopment, per below.

Qpre (Asphalt Current);  $2.78 \times 0.223 \times 178.56 \times 0.90 = 58.1$  L/sec (5-Year),  $2.78 \times 0.223 \times 104.16 \times 0.90 = 99.4$  L/sec (100-Year)

Qpost (Gravel Interim);  $2.78 \times 0.223 \times 178.56 \times 0.75 = 48.4$  L/sec (5-Year),  $2.78 \times 0.223 \times 104.16 \times 0.75 = 82.8$  L/sec (100-Year)



## **Appendix E**

### **Recent and Relevant Reports**



**"110 York Street & 141 George Street Serviceability Memo", by Novatech Engineering, dated March 12th, 2024**

**"Residential / Hotel Development 141 Geroge Street / 325 Dalhousie Street/110 York Street, Ottawa, Ontario, Servicing Design Brief", by Novatech Engineering, dated April 12th, 2018**

**"Residential / Hotel Development 141 Geroge Street / 325 Dalhousie Street/110 York Street, Ottawa, Ontario, Servicing Design Brief (Incl. Interim Condition)", by Novatech Engineering, dated February 14th, 2014**



# TECHNICAL MEMORANDUM

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**DATE:** OCTOBER 16TH, 2023  
**REVISED:** MARCH 12TH, 2024  
**TO:** MR. JOHN WU  
**FROM:** GREG MACDONALD, P.ENG & CURTIS FERGUSON, E.I.T.  
**RE:** 110 YORK STREET & 141 GEORGE STREET  
SERVICEABILITY MEMO  
112142  
**CC:** VINCENT DENOMME (CLARIDGE HOMES), STEPHEN  
POON (CLARIDGE HOMES),

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Novatech has been retained by Claridge Homes to prepare a Servicing Memo for the proposed site plan located at 141 George Street & 110 York Street within the City of Ottawa.

The following technical memorandum will review the water, sanitary and storm servicing of the proposed development to determine the serviceability of the development.

## **141 George Street**

### **Sanitary Sewer**

There is an existing 1980x1500mm horseshoe sanitary sewer within the George Street right-of-way.

### **Design Criteria**

Sanitary flows for the proposed development were calculated using criteria from Section 4 of the City of Ottawa Sewer Design Guidelines and the Ontario Building Code as follows:

- Residential Average Flow = 280 L/capita/day
- Studio Apartment = 1.4 Person/unit
- 1 Bed apartment = 1.4 Person/unit
- 2 Bed / 1 Bed + Den apartment = 2.1 Person/unit
- 3 Bed / 2 Bed + Den apartment = 3.1 Person/unit
- Professional Office = 75 L/9.3m<sup>2</sup>/day
- Retail / Restaurant = 125 L/2m<sup>2</sup>/day
- Bar / Cocktail Lounge = 70 L/day/seat (assumed 1 seat per 2m<sup>2</sup>)
- Residential Peaking Factor = Harmon Equation (max peaking factor = 4.0)
- Commercial Peaking Factor = 1.0
- Peak Extraneous Flows (Infiltration) = 0.33L/s/ha



### Sanitary Servicing

The tower is proposed to be serviced by a 200mm dia. sanitary sewer. The proposed service will connect to the existing 1980x1500mm sanitary sewer within the George Street right-of-way. It was confirmed through correspondence with the City that the existing sanitary sewer in George Street has adequate capacity for the development. The peak sanitary flow including infiltration for the site development was calculated to be **6.03 L/s**. Detailed sanitary flow calculations, and correspondence can be found in **Appendix A**.

The detailed design of the Andaz Hotel (Phase 1) was completed by Novatech with details provided within the Andaz Servicing Report. The previous design assumed that the George Building was to consist of a 22-storey condominium with 282 units, and 1097m<sup>2</sup> of commercial. The resultant assumed flow for the site was **9.32L/s**. Additionally, the projected flow from George Street was calculated to be **5.62 L/s**. The assumed design flow was lower than currently proposed, approximately a 7 percent increase in flow from the previous design.

### Storm Sewer

There is an existing 900mm dia. concrete sewer within George Street right-of-way.

### Design Criteria

Storm Sewer Design Parameters

Parameter	Design Criteria
Local Roads	2 Year Return Period
Storm Sewer Design	Rational Method
IDF Rainfall Data	Ottawa Sewer Design Guidelines
Initial Time of Concentration (Tc)	20 min
Minimum Velocity	0.8 m/s
Maximum Velocity	3.0 m/s
Minimum Diameter	250 mm

### Storm Servicing

It is proposed to service the proposed development with one (1) 250mm storm service connections to the existing 900mm storm sewer within the George Street right-of-way. The service will convey the uncontrolled foundation drain and the controlled flows from the internal stormwater cistern within the parking garage. Through correspondence with the City it is understood that the existing 100-year HGL within George Street is at an elevation of 60.6m during the 100-yr storm event. The proposed services will be installed complete with backflow prevention as the 100-year HGL is close to the proposed service inverts (60.28).



## Water

There is an existing 300mm dia. watermain within George Street right-of-way.

## Design Criteria

Water demand calculations have been calculated using criteria from Section 4 of the City of Ottawa Water Distribution Guidelines and the Ontario Building Code as follows:

- Average Domestic Flow = 280L/cap/day
- 1 Bedroom Apartment = 1.4 Persons/unit
- 2 Bedroom Apartment = 2.1 Persons/unit
- 3 Bedroom Apartment = 3.1 Persons/unit
- Office = 75L/9.3m<sup>2</sup>/day
- Bar/Cocktail Lounge = 70 L/day/seat
- Restaurant = 125 L/seat/day
- Residential Peaking Factors
  - Maximum Day = 2.5 x Avg Day
  - Peak Hour = 2.2 x Max Day
- Commercial Peaking Factors
  - Maximum Day = 1.5
- Peak Hour = 1.8

The required fire demand was calculated using the Fire Underwriters Survey 2020 (FUS) Guidelines. Through correspondence with the architect, it is understood that the proposed building is residential occupancy (Limited Combustible), composed of fire resistive construction (2 hrs.), and will contain a fully supervised sprinkler system designed as per NFPA 13.

## Water Servicing

**Domestic Water Demand Summary (George Building)**

Population	Commercial Area (m <sup>2</sup> )	Ave. Daily Demand (L/s)	Max. Daily Demand (L/s)	Peak Hour Demand (L/s)	Fire Flow (L/s)
502	670	2.03	4.68	10.04	100

## **Water Boundary Conditions Response (141 George Street)**

Criteria	Head (m)	Pressure <sup>1</sup> (m)	Pressure (PSI)	Pressure Requirements
<b>Connection (George Street)</b>				
Min HGL	106.3	44.4	63.08	> 40psi
Max HGL	115.4	53.5	76.01	< 80psi
Max Day + Fire Flow	109.0	47.1	66.91	> 20psi

<sup>1</sup>Pressure based on a Finished Floor elevation of 61.90m



The hydraulic analysis indicates that the system can provide adequate pressures and flow to meet the domestic and fire flow requirements for the site.

It is proposed to service the George Building with two (2) individual 200mm diameter services. Two (2) services will connect to the existing 300mm diameter watermain within the George Street right-of-way by way of a TVS connection. A valve will be placed on the 300mm main between the two services for redundancy.

### **110 York Street**

#### **Sanitary Sewer**

There is an existing 1200mm dia. sanitary sewer within the York Street right-of-way.

#### **Design Criteria**

Sanitary flows for the proposed development were calculated using criteria from Section 4 of the City of Ottawa Sewer Design Guidelines and the Ontario Building Code as follows:

- Average Hotel Flow (full housekeeping facilities) = 225 L/capita/day
- Hotel Room = 1.8 person/unit
- Dance Hall (plus restaurant & bar) = 150 L/day/patron (assumed 1 patron per 2m<sup>2</sup>)
- Residential Peaking Factor = Harmon Equation (max peaking factor = 4.0)
- Commercial Peaking Factor = 1.0
- Peak Extraneous Flows (Infiltration) = 0.33L/s/ha

#### **Sanitary Servicing**

The building is proposed to be serviced by a 200mm dia. sanitary sewer. The proposed service will connect to the existing 1200mm dia. sanitary sewer within the York Street right-of-way. It was confirmed through correspondence with the City that the existing sanitary sewer in York Street has adequate capacity for the development. The peak sanitary flow including infiltration for the site development was calculated to be **3.13 L/s**. Detailed sanitary flow calculations, and correspondence are attached can be found in **Appendix A**.

#### **Storm Sewer**

There is an existing 675mm dia. concrete sewer within George Street right-of-way.

#### **Design Criteria**

##### Storm Sewer Design Parameters

Parameter	Design Criteria
Local Roads	2 Year Return Period
Storm Sewer Design	Rational Method
IDF Rainfall Data	Ottawa Sewer Design Guidelines
Initial Time of Concentration (T <sub>c</sub> )	20 min
Minimum Velocity	0.8 m/s
Maximum Velocity	3.0 m/s
Minimum Diameter	250 mm



### Storm Servicing

It is proposed to service the proposed development with two (2) 250mm storm service connections to the existing 675mm storm sewer within the York Street right-of-way. One (1) storm service will convey the uncontrolled foundation drain while the second service will convey the controlled flows from the internal stormwater cistern within the parking garage. Through correspondence with the City it is understood that the existing 100-year HGL within York Street is at an elevation of approximately 60.1m during the 100-yr storm event. The proposed services will be installed complete with backflow prevention as the 100-year HGL is higher than the proposed service inverts.

### Water

There is an existing 200mm dia. watermain within York Street right-of-way.

### Design Criteria

Water demand calculations have been calculated using criteria from Section 4 of the City of Ottawa Water Distribution Guidelines and the Ontario Building Code as follows:

- Average Hotel Flow (full housekeeping facilities) = 225 L/capita/day
- Hotel Room = 1.8 Persons/unit
- Dance Hall (plus restaurant & bar) = 150 L/day/patron (assumed 1 patron per 2m<sup>2</sup>)
- Residential Peaking Factors
  - Maximum Day = 2.5 x Avg Day
  - Peak Hour = 2.2 x Max Day
- Commercial Peaking Factors
  - Maximum Day = 1.5
- Peak Hour= 1.8

The required fire demand was calculated using the Fire Underwriters Survey 2020 (FUS) Guidelines. Through correspondence with the architect, it is understood that the proposed building is residential occupancy (Limited Combustible), composed of fire resistive construction (2 hrs.), and will contain a fully supervised sprinkler system designed as per NFPA 13.

**Domestic Water Demand Summary (York Building)**

Population	Commercial Area (m <sup>2</sup> )	Ave. Daily Demand (L/s)	Max. Daily Demand (L/s)	Peak Hour Demand (L/s)	Fire Flow (L/s)
191	793	1.31	2.58	5.26	67

It is proposed to service the York Building with two (2) individual 200mm diameter services. Two (2) services will connect to the existing 200mm diameter watermain within the York Street right-of-way by way of a TVS connection. A valve will be added to the 300mm main between the services to provide redundancy.

Boundary conditions have been requested from the City. We do not anticipate any pressure issues and expect proposed flows to meet the domestic and fire flow requirements for the site.



## **Stormwater Management 141 George & 110 York**

### **Design Criteria**

Through correspondence with the City of Ottawa, and our knowledge of development requirements in the area, the following criteria have been adopted to control post-development stormwater discharge from the site:

- Control proposed development flows, up to and including the 100-year storm event, to a 5 year allowable release rate calculated using a runoff coefficient (C) of 0.50 and a time of concentration (Tc) of 20 minutes;
- Provide source controls which are in conformity with the City of Ottawa requirements, where possible;
- Limit ponding to 0.15 m for all rooftop storage areas and 0.30 m for all parking storage areas; and
- Provide guidelines to ensure that site preparation and construction is in accordance with the current Best Management Practices for Erosion and Sediment Control.

The approach to the stormwater management design is to determine the allowable release rate for the site, calculate the uncontrolled flow, and ensure that the remaining flow, in combination with the uncontrolled flow, does not exceed the allowable release rate. All proposed development runoff in excess of the allowable release rate, will be attenuated on-site prior to being released into the storm sewers within George Street and York Street.

### **Quantity Control**

The allowable release rate for the 0.419 ha site was calculated to be 40.9 L/s based on the SWM criteria provided by the City of Ottawa, and the Andaz Servicing Report. The Andaz Hotel (Phase 1) consumed 11.3 L/s which leaves an allowable of 29.6 L/s for the remaining development during the 100-year event.

### **Design Storms**

The design storms are based on City of Ottawa design storms. Design storms were used for the 5, and 100 return periods (i.e. storm events).

### **Model Parameters**

Post-development catchments were modelled based on the proposed site plan and grading as shown on **Drawing 112142-SWM** within **Appendix A**. The building roofs were assumed to have no depression storage.

Post development Stormwater Management Summary can be found below.



Table 15: Post-Development Stormwater Management Summary

Area ID	Area (ha)	1:5 Year Weighted Cw	1:100 Year Weighted Cw	Control Device	Outlet Location	2 Year Storm Event				5 Year Storm Event				100 Year Storm Event			
						Release (L/s)	Ponding Depth (m)	Req'd Vol (cu.m)	Max. Vol. Provided (cu.m.)	Release (L/s)	Ponding Depth (m)	Req'd Vol (cu.m)	Max. Vol. Provided (cu.m.)	Release (L/s)	Ponding Depth (m)	Req'd Vol (cu.m)	Max. Vol. Provided (cu.m.)
D-01	0.011	0.90	1.00	N/A	George Street	2.20	N/A	N/A	N/A	2.90	N/A	N/A	N/A	5.60	N/A	N/A	N/A
D-02	0.011	0.90	1.00	N/A	George Street	2.00	N/A	N/A	N/A	2.80	N/A	N/A	N/A	5.30	N/A	N/A	N/A
D-03	0.004	0.90	1.00	N/A	York Street	0.70	N/A	N/A	N/A	1.00	N/A	N/A	N/A	1.90	N/A	N/A	N/A
Cistern (York)	0.125	0.87	0.96	Pump	York Street	6.80	0.240	10.61	75.99	6.80	0.470	17.26	75.99	6.80	1.380	44.00	75.99
Cistern (George)	0.185	0.90	1.00	Pump	George Street	10.00	0.545	16.96	89.11	10.00	0.955	27.36	89.11	10.00	2.615	69.07	89.11
Post-Development Flow						21.7	-	27.6	165.1	23.5	-	44.6	165.1	29.6	-	113.1	165.1
Total Allowable Release Rate						29.6				29.6				29.6			



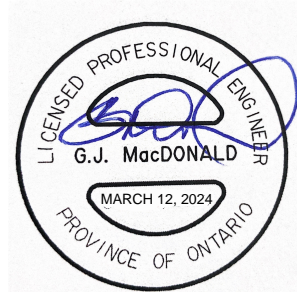
**NOVATECH**

**Prepared by:**



**Curtis Ferguson, E.I.T.**  
**Land Development Engineering**

**Reviewed by:**



**Greg MacDonald, P.Eng**  
**Director, Land Development and Public**  
**Sector Infrastructure**



## Appendix A



**From:** Duquette, Vincent <Vincent.Duquette@ottawa.ca>  
**Sent:** Tuesday, October 10, 2023 2:22 PM  
**To:** Curtis Ferguson  
**Cc:** Wu, John; Anthony Mestwarp; Greg MacDonald  
**Subject:** RE: 141 George Street / 110 York Street - Sanitary HGL (112142)

Hi Curtis,

Asset Management confirmed there is no capacity concerns for the proposed sanitary flows at 110 York St. and 141 George St.

Furthermore, dropping into the 1200mm dia. sanitary sewer on York St. would be acceptable.

Best Regards,

**Vincent Duquette, E.I.T**

Project Manager, Infrastructure Approvals

Planning, Real Estate and Economic Development Department – Direction général de la planification, des biens immobilier et du développement économique

Development Review – Central Branch

City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1

613.580.2424 ext./poste 14048, [vincent.duquette@ottawa.ca](mailto:vincent.duquette@ottawa.ca)

---

**From:** Curtis Ferguson <[c.ferguson@novatech-eng.com](mailto:c.ferguson@novatech-eng.com)>

**Sent:** October 03, 2023 3:28 PM

**To:** Duquette, Vincent <[Vincent.Duquette@ottawa.ca](mailto:Vincent.Duquette@ottawa.ca)>

**Cc:** Wu, John <[John.Wu@ottawa.ca](mailto:John.Wu@ottawa.ca)>; Anthony Mestwarp <[a.mestwarp@novatech-eng.com](mailto:a.mestwarp@novatech-eng.com)>; Greg MacDonald <[g.Macdonald@novatech-eng.com](mailto:g.Macdonald@novatech-eng.com)>

**Subject:** RE: 141 George Street / 110 York Street - Sanitary HGL (112142)

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Hi Vincent,

141 George Street *Sanitary Design Sheet* is attached.

Anticipated for 110 York (building layout coordination is on-going):

- 84 1 Bed Apartments.
- ~ 200m<sup>2</sup> of commercial area anticipated.
- Total Design Flow = 1.79 L/s.

Let me know if you require anything further.

**Curtis Ferguson**, B.A.Sc., E.I.T. | Land Development



## NOVATECH

Engineers, Planners & Landscape Architects

240 Michael Cowpland Drive, Suite 200, Ottawa, ON, K2M 1P6 | Tel: 613.254.9643 EXT: 331

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**From:** Duquette, Vincent <[Vincent.Duquette@ottawa.ca](mailto:Vincent.Duquette@ottawa.ca)>

**Sent:** Tuesday, October 3, 2023 2:46 PM

**To:** Curtis Ferguson <[c.ferguson@novatech-eng.com](mailto:c.ferguson@novatech-eng.com)>

**Cc:** Wu, John <[John.Wu@ottawa.ca](mailto:John.Wu@ottawa.ca)>; Anthony Mestwarp <[a.mestwarp@novatech-eng.com](mailto:a.mestwarp@novatech-eng.com)>; Greg MacDonald <[g.Macdonald@novatech-eng.com](mailto:g.Macdonald@novatech-eng.com)>

**Subject:** RE: 141 George Street / 110 York Street - Sanitary HGL (112142)

Hi Curtis,

Can you provide calculations showing the anticipated peak sanitary flows going to each sewer and a unit breakdown for the proposed development.

Best Regards,

**Vincent Duquette, E.I.T**

Project Manager, Infrastructure Approvals

Planning, Real Estate and Economic Development Department – Direction général de la planification, des biens immobilier et du développement économique

Development Review – Central Branch

City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1

613.580.2424 ext./poste 14048, [vincent.duquette@ottawa.ca](mailto:vincent.duquette@ottawa.ca)

---

**From:** Curtis Ferguson <[c.ferguson@novatech-eng.com](mailto:c.ferguson@novatech-eng.com)>

**Sent:** September 28, 2023 2:12 PM

**To:** Duquette, Vincent <[Vincent.Duquette@ottawa.ca](mailto:Vincent.Duquette@ottawa.ca)>

**Cc:** Wu, John <[John.Wu@ottawa.ca](mailto:John.Wu@ottawa.ca)>; Anthony Mestwarp <[a.mestwarp@novatech-eng.com](mailto:a.mestwarp@novatech-eng.com)>; Greg MacDonald <[g.Macdonald@novatech-eng.com](mailto:g.Macdonald@novatech-eng.com)>

**Subject:** 141 George Street / 110 York Street - Sanitary HGL (112142)

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Good Afternoon Vincent,

Inquiring to see if there is capacity issues for the sanitary system fronting both 110 York Street (MHSA38588 to MHSA60171)/ 141 George Street (MHSA38588 to MHSA60171)? Would setting the invert above the obvert of the sanitary in York (1200mm DIA.) function or would there be surcharging issues in the area?



Thanks,

**Curtis Ferguson**, B.A.Sc., E.I.T. | Land Development

**NOVATECH**

Engineers, Planners & Landscape Architects

240 Michael Cowpland Drive, Suite 200, Ottawa, ON, K2M 1P6 | Tel: 613.254.9643 EXT: 331

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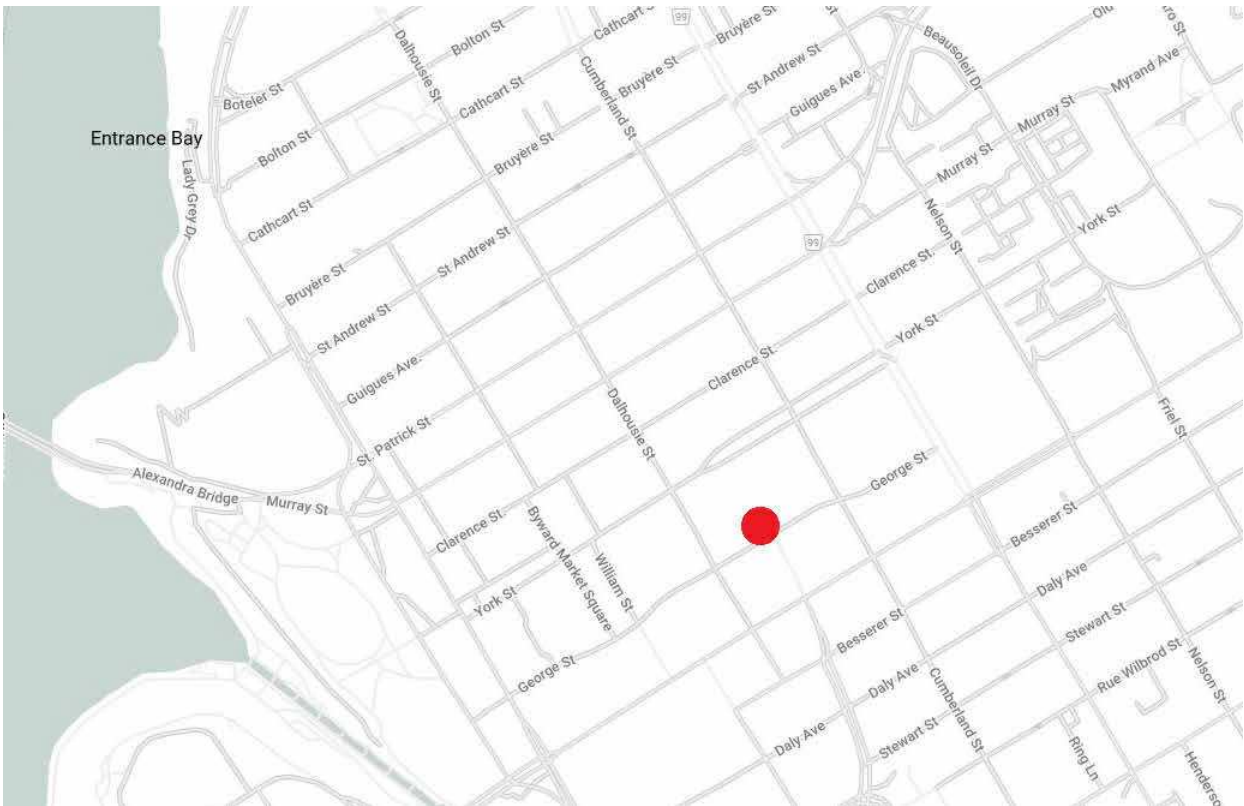
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NOTES		
<ul style="list-style-type: none"><li>FOR EXISTING SITE CONDITIONS, SEE SURVEY PLAN BY ANNIS, O'SULLIVAN, VOLLEBEKK LTD., SUBMITTED SEPERATELY.</li><li>FOR NEW GRADES AND SITE SERVICES, SEE CIVIL ENGINEERING PLANS BY NOVATECH ENGINEERING CONSULTANTS, SUBMITTED SEPERATELY.</li></ul>		
OCCUPANCY	UNITS / STOREYS	PROPOSED ZONING GFA
Residential (Rental)	297 units / Ground to 21st floors	Ground = 227m <sup>2</sup> 2 <sup>nd</sup> = 807m <sup>2</sup> 3 <sup>rd</sup> = 1,222m <sup>2</sup> 4 <sup>th</sup> - 17 <sup>th</sup> = 927m <sup>2</sup> / floor 12 <sup>th</sup> = 925m <sup>2</sup> 18 <sup>th</sup> = 869m <sup>2</sup> 19 <sup>th</sup> & 20 <sup>th</sup> = 849m <sup>2</sup> 21 <sup>st</sup> = 772m <sup>2</sup>  TOTAL = 18,571m <sup>2</sup>
	Minimum 15% (44 units) required to be Barrier-Free (BF) to be distributed throughout residential storeys.	7 x Studios (1BF units = 15%) 193 x 1 Bedroom (31BF units = 16%) 97 x 2 Bedroom (15BF units = 15%)  47BF units = 15%
Commercial	Ground	Commercial = 455m <sup>2</sup> Office = 73m <sup>2</sup>
	<b>TOTAL</b>	<b>19,099m<sup>2</sup></b>

MIXED-USE WITH GROUND FLOOR COMMERCIAL - ZONING - MD2 (2031) S307		
ZONING RULE	REQUIREMENT	PROVIDED
Minimum lot area	No minimum	3,109.10m <sup>2</sup>
Minimum lot width	No minimum	42.45m on George Street. 20.19m on back portion.
Minimum front yard	No minimum	1.51m on George Street
Minimum interior side yard	No minimum	0.45m on West side of building. 0.00m on East side of building.
Minimum rear yard	No minimum	0.15m to one storey volume. 19.92m to 4th to 17th floor overhang.
Maximum building height	70m as per Schedule 307. No projections permitted beyond building height.	70m all inclusive.
Maximum floor space index	Not applicable	Not applicable
Minimum width of landscape area	No minimum except that where a yard is provided and not used for required driveways, aisles, parking, loading spaces, or outdoor commercial patio, the whole yard must be landscaped	Whole yard to be landscaped.
Provisions for buildings 10 storeys and higher (By-law 2019-353)	Minimum lot area for an interior lot: 1350m <sup>2</sup>  Minimum interior side and rear yard setback for a tower: 7.5m  Minimum separation distance between towers on the same lot: 15m.	Minimum lot area met.  Site Plan Approval received.  Not applicable.
Parking Garage permission	100% of ground floor fronting a street (excluding mechanical room, pedestrian and vehicular access) for a minimum depth of 3m, must be occupied by permitted use..	100% of ground fronting George Street for a minimum depth of 3m, is occupied by permitted Commercial use and Office use.
Ground floor use	100% of ground floor fronting a street (excluding lobby area, mechanical room and access to other floors) for a minimum depth of 3m, must be occupied by select uses.  Total gross area of lobbies, mechanical rooms and access to other floors must not exceed 50% of ground floor gross area.  Min. 50% of ground floor to be occupied by permitted use subject to a separate and direct access to abutting street.	100% of ground fronting George Street for a minimum depth of 3m, is occupied by permitted Commercial use.  Total gross area of lobbies, mechanical rooms and access to other floors does not exceed 50% of ground floor gross area.  Area of permitted Commercial use exceeds 50% of gross floor area and has separate direct access to George Street.

AMENITY AND PARKING REQUIREMENTS ZONING - MD2 (2031) S307 (COMBINED WITH 110 YORK STREET)		
ZONING MECHANISM	REGULATION	PROPOSED
Residential Parking	None Required  Minimum 50% to be horizontal racks.	P2 19 spaces P3 51 spaces P4 52 spaces P5 51 spaces  84 horizontal & 67 vertical mount.
Visitor Parking	Residential Area Z (By-law 2016-249); no more than 30 visitor spaces are required per building.  Exception #2031: 0.063 spaces x 297 units = 25 visitor parking spaces	P2 30 spaces
Commercial Parking	None Required	P1 5 spaces
Hotel Parking	None Required	P1 27 spaces
Barrier-Free Parking	Requires 3 barrier-free spaces (Traffic and Parking By-Law 2017-301)	P1 to P5 2 spaces per floor Total 10 barrier-free spaces
		<b>Total: 245 spaces</b>
Minimum bicycle parking	Residential: 0.5 spaces x 297 units = 149 bicycle parking spaces  Retail: 1 space per 250m <sup>2</sup> of GFA 470m <sup>2</sup> GFA / 250m <sup>2</sup> = 2 bicycle parking spaces	Residential: 16 (P1) 64 (P2) 66 (P3) 5 (Exterior)  Total: 151 bicycle spaces
Maximum parking	1.5 per dwelling unit Limited to 445 spaces for 297 units. (combined with visitor) 1 per 100m <sup>2</sup> of Commercial gross area. Limited to 5 spaces.	Total parking spaces is under the limit. Commercial parking spaces maximized.
Minimum driveway width	6m	6m
Minimum aisle width	6m	6m
Loading	Exception #2031, None Required.	NA
Amenities Areas	Amenity Area - 6m <sup>2</sup> per unit = 297 units x 6m <sup>2</sup> = 1,782m <sup>2</sup> Require 16y <sup>3</sup> Recycling (GMP) = 0.018y <sup>3</sup> /unit Require 6y <sup>3</sup> Recycling (Fibres) = 0.038y <sup>3</sup> /unit Require 19y <sup>3</sup> Organics = 240L container/50 units Require 6 containers  Communal Amenity Area : Exception #2031; minimum 40% off the required total Amenity Area = 1,782m <sup>2</sup> x 0.4 = minimum 713m <sup>2</sup> Layout of Communal Amenity Area - aggregated into areas up to 54m <sup>2</sup>	Combined Balcony Areas = 1,555m <sup>2</sup> Ground = 35m <sup>2</sup> Total = 20y <sup>3</sup> Recycling (GMP) = 2 x 3y <sup>3</sup> containers Total = 6y <sup>3</sup> Recycling (Fibres) = 3 x 4y <sup>3</sup> containers Total = 12y <sup>3</sup> Organics = 7 x 240L containers Total = 1680L  Combined Communal Areas = 729m <sup>2</sup> Ground = 220m <sup>2</sup> 2 <sup>nd</sup> = 195m <sup>2</sup> 21 <sup>st</sup> = 314m <sup>2</sup>  Total = 2,284m <sup>2</sup>

SOLID WASTE COLLECTION REQUIREMENTS		
ZONING MECHANISM	REGULATION	PROPOSED
Residential Waste	Garbage (Compacted) = 0.053y <sup>3</sup> /unit Require 16y <sup>3</sup> Recycling (GMP) = 0.018y <sup>3</sup> /unit Require 6y <sup>3</sup> Recycling (Fibres) = 0.038y <sup>3</sup> /unit Require 19y <sup>3</sup> Organics = 240L container/50 units Require 6 containers	Garbage (Compacted) = 5 x 4y <sup>3</sup> containers Total = 20y <sup>3</sup> Recycling (GMP) = 2 x 3y <sup>3</sup> containers Total = 6y <sup>3</sup> Recycling (Fibres) = 3 x 4y <sup>3</sup> containers Total = 12y <sup>3</sup> Organics = 7 x 240L containers Total = 1680L

## SITE PLAN

1 : 250

1  
A100

### GENERAL NOTES

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- The dimensions on these documents must be read and not measured.

### Mechanical - Electrical Engineer

#### JAIN

2405 East Dandora Crescent, 2nd Floor Mississauga, Ontario, L5N 6P8  
T 905 285 9900 jainconsultants.com

### Structural Engineer

#### Goodeve Structural Inc.

18-77 Aunga Drive, Ottawa ON K2E 7Z7  
T 613 226 4555 goodevestructural.ca

### Landscape Architect

#### James B. Lennox & Associates

3332, Carling Avenue, Ottawa, ON, K2H 5A8  
T 613 722 5166 jba.ca

### Civil

#### Novatech Eng. Consultants Ltd.

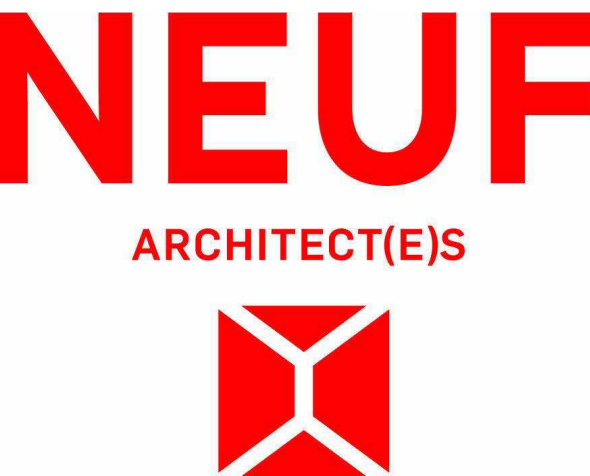
240, Michael Cowland Drive, Suite 200, Ottawa ON K2M 1P6  
T 613 234 9643 novatech-eng.com

### Architect

#### NEUF Architectes INC.

630 Ave. René-Lévesque O. 32e Etage, Montréal QC H3B 1S6  
T 514 847 1117 NEUFarchitectes.com

### Seal



### Client



CLARIDGE  
HOMES

### Project

**141 GEORGE STREET**

### Location

OTTAWA

### No.

12810

### NO REVISION

### DATE (yyyy.mm.dd)

F	FOR CLIENT COMMENTS	2023.03.03
G	FOR COORDINATION	2023.03.03
H	FOR COORDINATION	2023.04.17
J	FOR COORDINATION	2023.05.17
N	RE-ISSUED FOR SITE PLAN APPROVAL	2023.06.06
O	FOR COORDINATION	2023.06.09
Q	RE-ISSUED FOR SITE PLAN APPROVAL	2023.07.06
R	FOR COORDINATION	2023.07.07
V	FOR COORDINATION	2023.09.11

### Drawn by

SJ

### Checked by

LH

DATE (aa.mm.jj)

FEB 2023

Scale

As indicated

### Drawing Title

**SITE PLAN**

### Revision

V

### Dwg Number

A100



**From:** Vincent Denomme <vincent.denomme@claridgehomes.com>

**Sent:** Wednesday, October 4, 2023 2:32 PM

**To:** Curtis Ferguson <c.ferguson@novatech-eng.com>

**Cc:** Stephen Poon <stephen.poon@claridgehomes.com>

**Subject:** 110 York

Hi Curtis,

As discussed. Please remove any reference to servicing 110 York on the George Plans.

Also, please prepare a Servicing memo indicating there is sufficient capacity for both projects.

Attached is the site plan prepared for 110 York, there are 106 Hotel rooms. The ground floor has a ball room with back of house/kitchen etc.



Project Name: 141 George Street  
Date Prepared: 5/25/2023  
Date Revised: 10/13/2023  
Input By: Curtis Ferguson, E.I.T.  
Reviewed By: Greg MacDonald, P.Eng  
Drawing Reference: 112142 - SAN - 141 George Street

USER DESIGN INPUT  
CUMULATIVE CELL  
CALCULATED DESIGN CELL OUTPUT



Engineers, Planners & Landscape Architects

LOCATION			DEMAND										DESIGN CAPACITY															
AREA	FROM MH	TO MH	RESIDENTIAL FLOW								COMMERCIAL FLOW					EXTRANEOUS FLOW				PROPOSED SEWER PIPE SIZING / DESIGN								
			Studio	1 Bed Apartment	2 Bed / 1 Bed + Den Apartment	3 Bed / 2 Bed + Den Apartment	POPULATIO N (in 1000's)	CUMULATIVE POPULATION (in 1000's)	PEAK FACTOR M	AVG POPULATION FLOW (L/s)	PEAKED DESIGN POP FLOW (L/s)	COMMERICAL Area	CUMULATIVE COMMERCIAL Area	DESIGN COMMERCIAL FLOW (L/s)	COMMERICAL PEAK FACTOR	PEAKED COMMERCIAL FLOW	Total Area (ha.)	Accum. Area (ha.)	DESIGN EXTRAN. FLOW (L/s)	TOTAL DESIGN FLOW (L/s)	PIPE LENGTH (m)	PIPE SIZE (mm) AND MATERIAL	PIPE ID ACTUAL (m)	ROUGH. (n)	DESIGN GRADE (%)	CAPACITY (L/s)	FULL FLOW VELOCITY (m/s)	Qpeak Design Qcap
George Street																												
A-02	Stub	EX. 1980mm x 1500mm SAN	25	147	123	1	0.502	0.502	3.38	1.63	5.50	679.700	679.700	0.40	1.00	0.40	0.39	0.39	0.13	6.03	6.4	250 PVC	0.254	0.013	2.00	87.7	1.73	6.9%
TOTAL			25	147	123	1	0.502	0.502				679.700	679.700				0.39											

7. Commercial Flow

141 George

Use	Area (m2)	Use	Daily Demand Volume	Source
Office Area	72.70	Professional Office	75 L/9.3m2/day	Daily Demands from OBC Table 8.2.1.3
Restaurant Area	477.00	Retail Restaurent	125 L/2m2/day	
Bar/Cocktail Lounge	130.00	Bar/ Cocktail Lounge (meeting/party room)	70 L/day/seat (1 seat/ 2m2)	City of Ottawa Sewer Design Guidelines
Total Com Area	679.70			
Total Com Daily Volume (L/s)	34948.79			

Design Parameters:							
1. Residential Flows				CAPACITY EQUATION			
-1 Bed Apartment / Studio	1.4	Person/ Unit		Q full= (1/n) A R^(2/3)So^(1/2)			
-2 Bed Apartment	2.1	Person/ Unit					
-3 Bed Apartment	3.1	Person/ Unit					
2. Commercial Flow				Where :	Q full = Capacity (L/s)		
-Restaurant/Lounge	125	L/day/seat					
3. q Avg capita flow	280	L/per/day					
4. M = Harmon Formula (maximum of 4.0)					n = Manning coefficient of roughness (0.013)		
5. K =	0.8				A = Flow area (m <sup>2</sup> )		
6. Commercial Peak Factor					R = Wetter perimenter (m)		
-area > 20% of development	1.5				So = Pipe Slope/gradient		
-area < 20% of development	1.0						
7. Extraneous Flows =	0.33	L/sec/ha					



Project Name: 110 York Street  
Date Prepared: 10/13/2023  
Date Revised: 10/13/2023  
Input By: Curtis Ferguson, E.I.T.  
Reviewed By: Greg MacDonald, P.Eng  
Drawing Reference: 112142 - SAN - 110 York Street

USER DESIGN INPUT  
CUMULATIVE CELL  
CALCULATED DESIGN CELL OUTPUT



LOCATION			DEMAND												DESIGN CAPACITY										
AREA	FROM MH	TO MH	RESIDENTIAL FLOW					COMMERCIAL FLOW					EXTRANEOUS FLOW				PROPOSED SEWER PIPE SIZING / DESIGN								
			HOTEL ROOMS	POPULATION (in 1000's)	CUMULATIVE POPULATION (in 1000's)	PEAK FACTOR M	AVG POPULATION FLOW (L/s)	PEAKED DESIGN POP FLOW (L/s)	COMMERICAL Area	CUMULATIVE COMMERICAL Area	DESIGN COMMERICAL FLOW (L/s)	COMMERICAL PEAK FACTOR	PEAKED COMMERCIAL FLOW	Total Area (ha.)	Accum. Area (ha.)	DESIGN EXTRAN. FLOW (L/s)	TOTAL DESIGN FLOW (L/s)	PIPE LENGTH (m)	PIPE SIZE (mm) AND MATERIAL	PIPE ID ACTUAL (m)	ROUGH. (n)	DESIGN GRADE (%)	CAPACITY (L/s)	FULL FLOW VELOCITY (m/s)	Qpeak Design / Qcap
York Street																									
A-01	Stub	EX. 1200mm SAN	106	0.191	0.191	3.52	0.50	1.75	793.000	793.000	0.69	1.00	0.69	0.80	0.80	0.26	2.70	6.4	250 PVC	0.254	0.013	2.00	87.7	1.73	3.1%
TOTAL			106	0.191	0.191				793.000	793.000				0.80											

7. Commercial Flow					
110 York Street					
Use	Area (m2)	Use	Daily Demand Volume	Source	
Dance Hall (c/w restaurant & bar)	793.00	Dance Hall (c/w restaurant & bar)	150	L/day/patron (1 patron/ 2m2)	City of Ottawa Sewer Design Guidelines
Total Com Area	793.00				
Total Com Daily Volume (L/s)	59475.00				

Design Parameters:							
1. Residential Flows			CAPACITY EQUATION				
-Hotel Room	1.8	Person/ Unit	Q full= (1/n) A R^(2/3)So^(1/2)				
2. Commercial Flow			Where : Q full = Capacity (L/s)				
-Dance hall (c/w restaurant & bar)	150	L/day/patron					
3. q Avg Hotel flow ( With Full Housekeeping facilities	225	L/per/day					
4. M = Harmon Formula (maximum of 4.0)			n = Manning coefficient of roughness (0.013)				
5. K =	0.8		A = Flow area (m²)				
6. Commercial Peak Factor			R = Wetter perimeter (m)				
-area > 20% of development	1.5		So = Pipe Slope/gradient				
-area < 20% of development	1.0						
7. Extraneous Flows =	0.33	L/sec/ha					



**From:** Duquette, Vincent <[Vincent.Duquette@ottawa.ca](mailto:Vincent.Duquette@ottawa.ca)>

**Sent:** Friday, May 5, 2023 4:51 PM

**To:** Anthony Mestwarp <[a.mestwarp@novatech-eng.com](mailto:a.mestwarp@novatech-eng.com)>

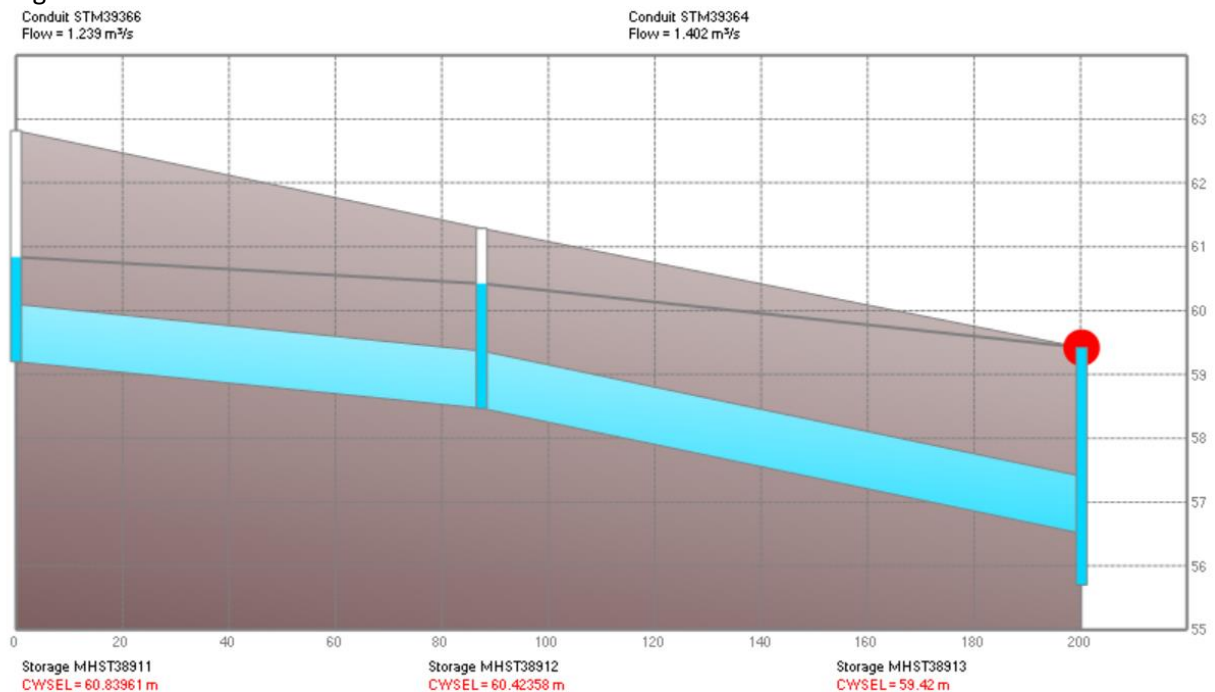
**Cc:** Mottalib, Abdul <[Abdul.Mottalib@ottawa.ca](mailto:Abdul.Mottalib@ottawa.ca)>; Wu, John <[John.Wu@ottawa.ca](mailto:John.Wu@ottawa.ca)>; Greg MacDonald <[g.Macdonald@novatech-eng.com](mailto:g.Macdonald@novatech-eng.com)>; Curtis Ferguson <[c.ferguson@novatech-eng.com](mailto:c.ferguson@novatech-eng.com)>

**Subject:** RE: 141 George Street - Phase 2 (112142)

Hi Anthony,

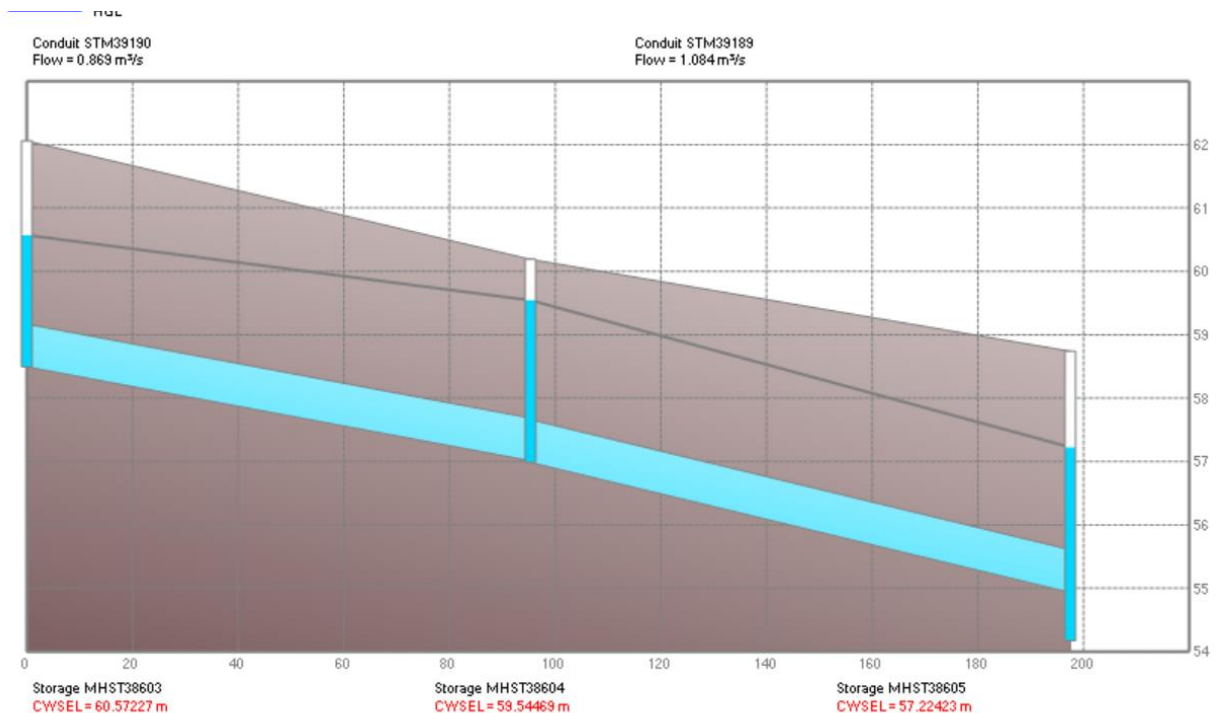
Please see below HGL requested. In these old uncontrolled systems, the 100-year HGL is expected to break out at the surface.

#### George between Dalhousie and Cumberland



#### York between Dalhousie and Cumberland





Best Regards,

**Vincent Duquette, E.I.T**

Project Manager, Infrastructure Approvals

Planning, Real Estate and Economic Development Department – Direction général de la planification,  
des biens immobilier et du développement économique

Development Review – Central Branch

City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1

613.580.2424 ext./poste 14048, [vincent.duquette@ottawa.ca](mailto:vincent.duquette@ottawa.ca)

**From:** Anthony Mestwarp <[a.mestwarp@novatech-eng.com](mailto:a.mestwarp@novatech-eng.com)>

**Sent:** April 28, 2023 5:20 PM

**To:** Duquette, Vincent <[Vincent.Duquette@ottawa.ca](mailto:Vincent.Duquette@ottawa.ca)>

**Cc:** Mottalib, Abdul <[Abdul.Mottalib@ottawa.ca](mailto:Abdul.Mottalib@ottawa.ca)>; Wu, John <[John.Wu@ottawa.ca](mailto:John.Wu@ottawa.ca)>; Greg MacDonald <[g.Macdonald@novatech-eng.com](mailto:g.Macdonald@novatech-eng.com)>; Curtis Ferguson <[c.ferguson@novatech-eng.com](mailto:c.ferguson@novatech-eng.com)>

**Subject:** RE: 141 George Street - Phase 2 (112142)

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Hi Vincent,

The requested PDF is attached.



I hope you have a good weekend.

Regards,

**Anthony Mestwarp**, P.Eng., Project Engineer | Land Development Engineering  
**NOVATECH**

Engineers, Planners & Landscape Architects

240 Michael Cowpland Drive, Suite 200, Ottawa, ON, K2M 1P6 | Tel: 613.254.9643 Ext. 216

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**From:** Duquette, Vincent <[Vincent.Duquette@ottawa.ca](mailto:Vincent.Duquette@ottawa.ca)>

**Sent:** Friday, April 28, 2023 4:13 PM

**To:** Anthony Mestwarp <[a.mestwarp@novatech-eng.com](mailto:a.mestwarp@novatech-eng.com)>

**Cc:** Mottalib, Abdul <[Abdul.Mottalib@ottawa.ca](mailto:Abdul.Mottalib@ottawa.ca)>; Wu, John <[John.Wu@ottawa.ca](mailto:John.Wu@ottawa.ca)>; Greg MacDonald <[g.Macdonald@novatech-eng.com](mailto:g.Macdonald@novatech-eng.com)>; Curtis Ferguson <[c.ferguson@novatech-eng.com](mailto:c.ferguson@novatech-eng.com)>

**Subject:** RE: 141 George Street - Phase 2 (112142)

Hi Anthony,

I will be reviewing this file in John's absence. Can you please forward me the pdf file highlighting the pipe segments that is mentioned in your previous email. I will then circulate it to asset management to obtain the HGL requested.

Best Regards,

**Vincent Duquette, E.I.T**

Project Manager, Infrastructure Approvals

Planning, Real Estate and Economic Development Department – Direction général de la planification, des biens immobilier et du développement économique

Development Review – Central Branch

City of Ottawa | Ville d'Ottawa

110 Laurier Avenue West Ottawa, ON | 110, avenue. Laurier Ouest. Ottawa (Ontario) K1P 1J1

613.580.2424 ext./poste 14048, [vincent.duquette@ottawa.ca](mailto:vincent.duquette@ottawa.ca)

**From:** Mottalib, Abdul <[Abdul.Mottalib@ottawa.ca](mailto:Abdul.Mottalib@ottawa.ca)>

**Sent:** April 28, 2023 10:59 AM

**To:** Duquette, Vincent <[Vincent.Duquette@ottawa.ca](mailto:Vincent.Duquette@ottawa.ca)>

**Cc:** Wu, John <[John.Wu@ottawa.ca](mailto:John.Wu@ottawa.ca)>; Greg MacDonald <[g.Macdonald@novatech-eng.com](mailto:g.Macdonald@novatech-eng.com)>; Curtis Ferguson <[c.ferguson@novatech-eng.com](mailto:c.ferguson@novatech-eng.com)>; Anthony Mestwarp <[a.mestwarp@novatech-eng.com](mailto:a.mestwarp@novatech-eng.com)>; Mottalib, Abdul <[Abdul.Mottalib@ottawa.ca](mailto:Abdul.Mottalib@ottawa.ca)>

**Subject:** RE: 141 George Street - Phase 2 (112142)

Hi Vincent ,

Please review it.



--

Thanks,

Abdul  
Mohammad Abdul Mottalib, P. Eng.  
Extension: 27798

**From:** Anthony Mestwarp <[a.mestwarp@novatech-eng.com](mailto:a.mestwarp@novatech-eng.com)>  
**Sent:** April 28, 2023 10:15 AM  
**To:** Mottalib, Abdul <[Abdul.Mottalib@ottawa.ca](mailto:Abdul.Mottalib@ottawa.ca)>  
**Cc:** Wu, John <[John.Wu@ottawa.ca](mailto:John.Wu@ottawa.ca)>; Greg MacDonald <[g.Macdonald@novatech-eng.com](mailto:g.Macdonald@novatech-eng.com)>; Curtis Ferguson <[c.ferguson@novatech-eng.com](mailto:c.ferguson@novatech-eng.com)>  
**Subject:** FW: 141 George Street - Phase 2 (112142)

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Hi Abdul,

I understand that John is currently out of the office.

Can you please review the below?

Thanks,

**Anthony Mestwarp**, P.Eng., Project Engineer | Land Development Engineering  
**NOVATECH**

Engineers, Planners & Landscape Architects

240 Michael Cowpland Drive, Suite 200, Ottawa, ON, K2M 1P6 | Tel: 613.254.9643 Ext. 216

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**From:** Anthony Mestwarp  
**Sent:** Friday, April 28, 2023 10:10 AM  
**To:** Wu, John <[John.Wu@ottawa.ca](mailto:John.Wu@ottawa.ca)>  
**Cc:** Greg MacDonald <[g.Macdonald@novatech-eng.com](mailto:g.Macdonald@novatech-eng.com)>; Curtis Ferguson <[c.ferguson@novatech-eng.com](mailto:c.ferguson@novatech-eng.com)>  
**Subject:** 141 George Street - Phase 2 (112142)

Hi John,

We are working on the design of 141 George Street Phase 2 and would like to confirm the existing storm sewer HGL within the city infrastructure neighboring the site, to ensure there will not be any backflow issues on the proposed connections.



Can you please confirm who would be the engineering reviewer for this project, and if required forward this email to the appropriate contact.

**York Street:**

Can you please confirm the existing HGL within the 675mm concrete storm sewer within York street between manholes MHST38603 and MHST38604 as highlighted on the attached PDF.

**George Street:**

Can you please confirm the existing HGL within the 900mm concrete storm sewer within York street between manholes MHST38911 and MHST38912 as highlighted on the attached PDF.

Thanks,

**Anthony Mestwarp**, P.Eng., Project Engineer | Land Development Engineering

**NOVATECH**

Engineers, Planners & Landscape Architects

240 Michael Cowpland Drive, Suite 200, Ottawa, ON, K2M 1P6 | Tel: 613.254.9643 Ext. 216

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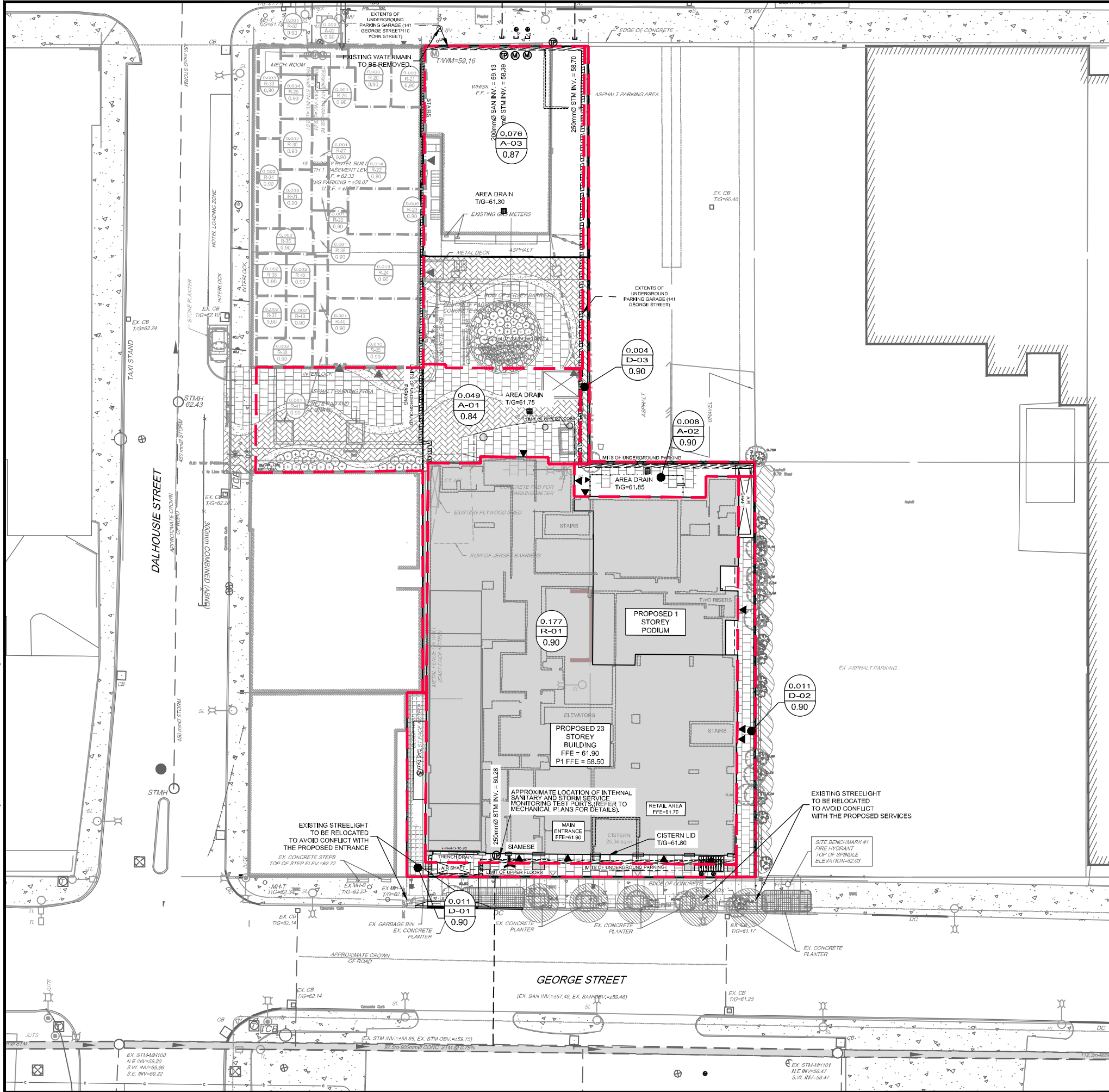
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,

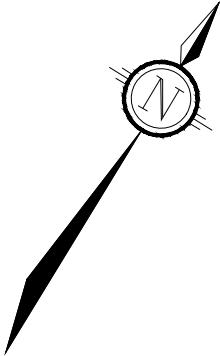


M:\2012\112142\141 GEORGE-110 YORKCAD\Civil\112142-2-SWM.dwg, SWM, Oct 17, 2023 - 1:43pm, cferguson



LEGEND

- DRAINAGE AREA LIMITS
- DRAINAGE AREA (ha)  
DRAINAGE AREA ID  
RUNOFF COEFFICIENT
- PROPERTY LINE
- PROPOSED CURB
- PROPOSED DEPRESSED CURB
- PROPOSED CURB CUT
- PROPOSED RETAINING WALL C/W GUARD RAIL
- PROPOSED CAP
- PROPOSED STORM SEWER AND MANHOLE
- PROPOSED AREA DRAIN
- PROPOSED TRENCH DRAIN
- PROPOSED BUILDING ENTRANCE
- PROPOSED FIREWALL
- DIRECTION OF FLOW
- EXISTING STORM MANHOLE & SEWER
- EXISTING CATCHBASIN



N VATECH

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Facsimile (613) 254-5867  
Website www.novatech-eng.com

CITY OF OTTAWA  
141 GEORGE STREET

STORMWATER  
MANAGEMENT PLAN

SCALE	1 : 500	0 5m 10m 20m
DATE	MARCH 2024	JOB 112142
FIGURE	SWM	





Engineers, Planners & Landscape Architects

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Development  
  
Municipal  
Infrastructure  
  
Environmental /  
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#### Planning

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Planning Application  
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Municipal Planning  
Documents &  
Studies  
  
Expert Witness  
(OMB)  
  
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Residential  
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Institutional Sites  
  
Environmental  
Restoration



## Residential / Hotel Development 141 George Street / 325 Dalhousie Street / 110 York Street Ottawa, Ontario

### Servicing Design Brief

Engineering excellence. Planning precision. Inspired landscapes.



**RESIDENTIAL / HOTEL DEVELOPMENT  
141 GEORGE STREET / 325 DALHOUSIE STREET / 110 YORK STREET  
OTTAWA, ONTARIO**

**SERVICING DESIGN BRIEF**

**Prepared by:**

**NOVATECH**

240 Michael Cowpland Drive  
Ottawa, Ontario  
K2M 1P6

December 07, 2012 (R-2012-171)

February 28, 2013 (R-2013-019)

February 14, 2014

**Revised April 12, 2018**

**File No.: 112142**

**Report Reference No.: R-2014-020**



April 12, 2018

City of Ottawa  
Planning and Growth Management Department  
Development Review (Urban) Services Branch  
Infrastructure Approvals Division  
110 Laurier Avenue West, 4<sup>th</sup> Floor  
Ottawa ON, K1P 1J1

**Attention: Mr. Richard Buchanan**

Dear Sir:

**Reference: Residential / Hotel Development  
141 George Street / 325 Dalhousie Street  
Servicing Design Brief  
Our File No.: 112142**

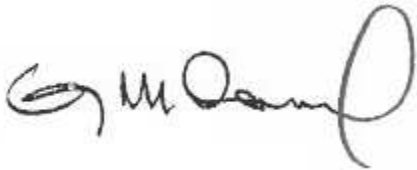
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Enclosed herein is the revised Servicing Design Brief for the proposed Residential / Hotel development at 141 George Street / 325 Dalhousie Street / 110 York Street, located east of Dalhousie Street between York Street and George Street. This brief is submitted in support of the zoning amendment for the site and outlines how the site will be serviced with sanitary, storm and watermain.

Trusting this report is adequate for your purposes. Should you have any questions, or require additional information, please contact us.

Yours truly,

**NOVATECH**



Greg MacDonald, P.Eng.  
Director | Land Development and Public-Sector Infrastructure



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Appendix B: Servicing Study Guidelines Checklist



## 1.0 INTRODUCTION

This Servicing Design Brief has been prepared in support of a Zoning By-Law Amendment Application of the property located at 110 York Street. A previous Servicing Design Brief was completed on February 14, 2014 in support of a Zoning By-Law Amendment Application for 141 George Street and 325 Dalhousie Street. The proposed development at that time included a 15-storey hotel with 200 rooms and a 22-storey residential condominium with 282 units with approximately 1097 m<sup>2</sup> of commercial floorspace on the ground floor. This report addresses the proposed hotel expansion on 110 York Street, which will add another 128 hotel rooms.

The subject site is located in the Byward Market, east of Dalhousie Street between York Street and George Street in the City of Ottawa. The existing properties are currently occupied by commercial spaces at 110 York Street (The Whiskey Bar), a 15-story hotel building at 325 Dalhousie Street (constructed in 2015), and a privately-owned surface parking lot. Aerial view of the subject is provided in **Figure 1**.

The proposed development of the site will consist of an 18-storey hotel addition at 110 York Street with 128 units and a 22-storey tower at 141 George Street with 282 condominium units. The condominium building will include approximately 1097 m<sup>2</sup> of commercial floor space located on the ground floor. A total of approximately 288 underground parking spaces will be provided on 4 levels of underground parking. Refer to **Figure 2** for details.

As identified in the City of Ottawa's Zoning By-Law, the site is currently designated as Mixed-Use Downtown (MD2). The minor zoning by-law amendment will revise the site's current designation for the proposed development to deal with building height, parking requirements and any applicable zoning provisions that cannot be met. The specific details regarding the changes proposed to the zoning of the subject site are provided in a Planning Rationale submitted as part of the Zoning By-Law Amendment application.

The subject site is approximately 0.42 ha in area. This servicing design brief will outline how the site will be serviced with sanitary, storm and watermain, and will demonstrate that adequate municipal capacity is available within the existing infrastructure to service the development.

## 2.0 SANITARY SEWER

The existing Dalhousie Street hotel is serviced by a 200 mm dia. sanitary service that connects to the existing 1200 mm dia. sanitary sewer on York Street. The proposed York Street hotel addition will have a separate 200 mm dia. sanitary service that will connect to the existing 1200 mm dia. sanitary sewer on York Street. The existing 200 mm dia. sanitary service for the 110 York Street property will be abandoned. The proposed condominium development will be serviced by a 200 mm dia. sanitary service that will connect to the existing 1980x1500 mm dia. sanitary sewer on George Street. Refer to **Figure 3** for details.

The proposed development flows are based on the City of Ottawa Sewer Design Guidelines. The calculated sanitary flow estimates for existing and proposed buildings on site will be compared to design flows based on current zoning.





Engineers, Planners & Landscape Architects  
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Website [www.novatech-eng.com](http://www.novatech-eng.com)

CITY OF OTTAWA  
141 GEORGE STREET / 325 DALHOUSIE  
STREET / 110 YORK STREET

## AERIAL PHOTO

SCALE

N.T.S

DATE

APR 2018

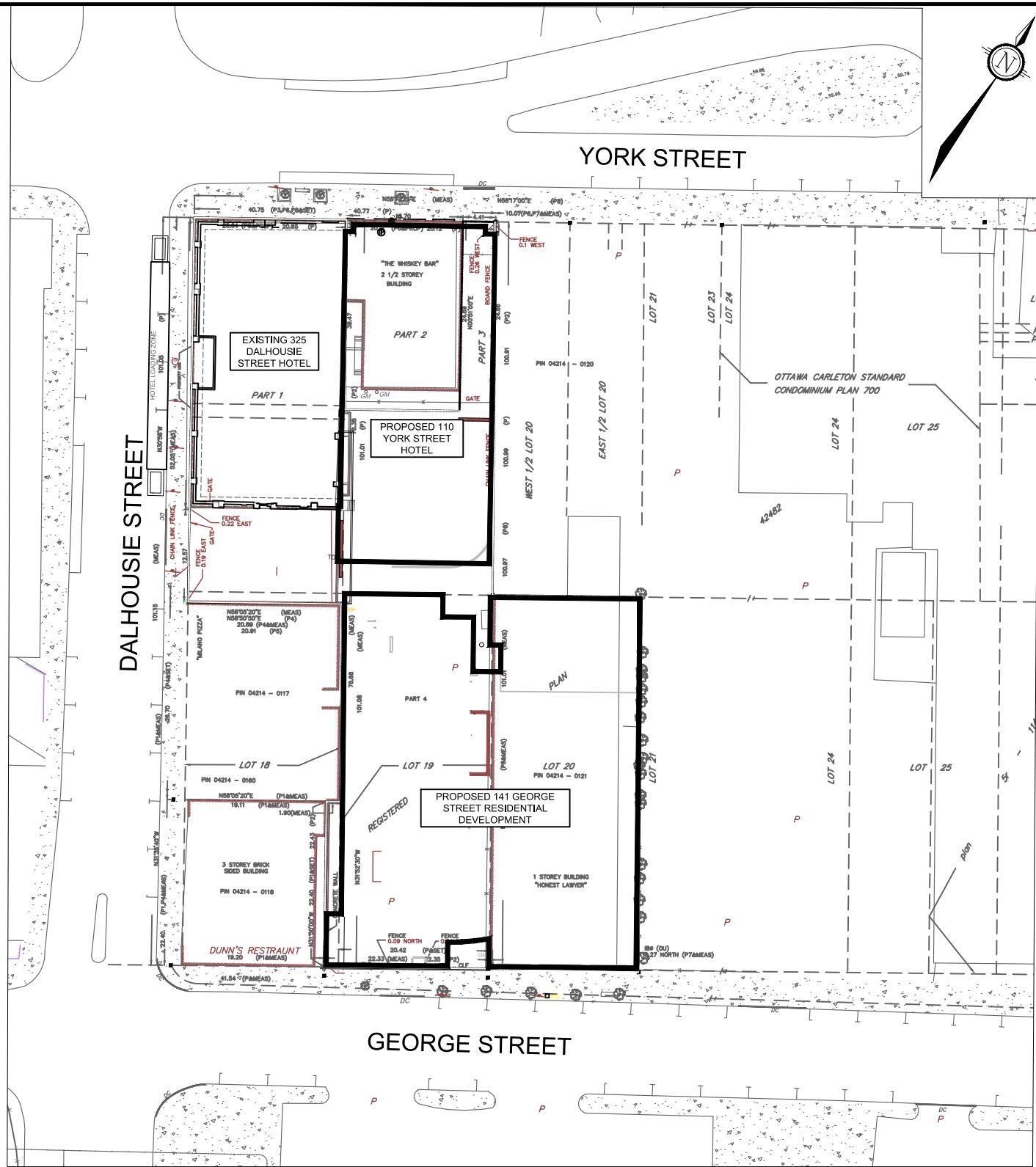
JOB

112142

FIGURE

FIGURE 1





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Website [www.novatech-eng.com](http://www.novatech-eng.com)

CITY OF OTTAWA  
141 GEORGE STREET / 325 DALHOUSIE  
STREET / 110 YORK STREET

## CONCEPTUAL SITE PLAN

SCALE

N.T.S

DATE

APR 2018

JOB

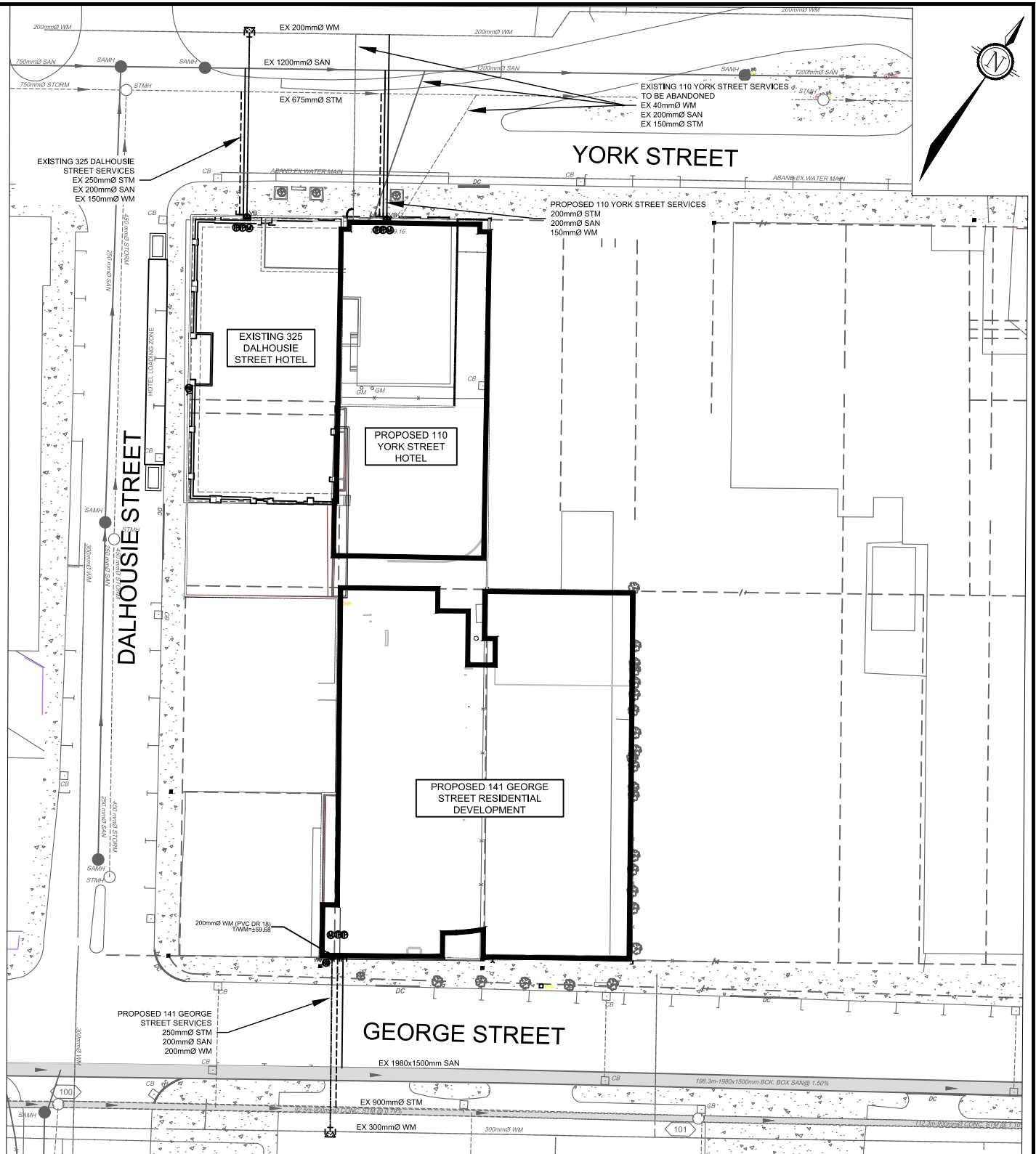
112142

FIGURE

FIGURE 2



M:\2012\112142\CAD\Design\Figures\Design Brief\112142 - SITEPLAN 2018.dwg, Figure 3, Apr 10, 2018 - 12:41pm, jmaruccio



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 Suite 200, 240 Michael Cowpland Drive  
 Ottawa, Ontario, Canada K2M 1P6

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 Facsimile (613) 254-5867  
 Website [www.novatech-eng.com](http://www.novatech-eng.com)

CITY OF OTTAWA  
 141 GEORGE STREET / 325 DALHOUSIE  
 STREET / 110 YORK STREET

## CONCEPTUAL SITE SERVICING PLAN

SCALE

N.T.S

DATE

APR 2018

JOB

112142

FIGURE

FIGURE 3



**Sanitary Flows Under Proposed Development****Existing Hotel (Dalhousie Street)****Average Sanitary Flow:**

Residential:  $Q_{SAN} = 200 \text{ units} \times 1.1 \text{ persons/unit} \times 225 \text{ L/cap/day} = 49,500 \text{ L/day} = 0.57 \text{ L/s}$

Restaurant/Bar:  $Q_{SAN} = 100 \text{ seats} \times 125 \text{ L/seat/day} = 12,500 \text{ L/day} = 0.14 \text{ L/s}$

Rooftop Bar:  $Q_{SAN} = 50 \text{ seats} \times 70 \text{ L/seat/day} = 3,500 \text{ L/day} = 0.04 \text{ L/s}$

Staff:  $Q_{SAN} = 20 \text{ staff} \times 40 \text{ L/staff/day} = 800 \text{ L/day} = 0.01 \text{ L/s}$

Total Average Residential Flow = 0.57 L/s

Total Average Commercial Flow = 0.14 L/s + 0.04 L/s + 0.01 L/s = 0.19 L/s

Total Average Sanitary Flow = 0.57 L/s + 0.19 L/s = 0.76 L/s

**Peak Sanitary Flow:**

Residential Peaking Factor (Harmon Equation) = 3.51

Total Peak Residential Flow = 0.57 L/s  $\times$  3.51 = 2.00 L/s

Commercial Peaking Factor = 1.0

Total Peak Commercial Flow = 0.19 L/s  $\times$  1.0 = 0.19 L/s

Total Peak Sanitary Flow = 2.00 L/s + 0.19 L/s = 2.19 L/s

*\* Based on predominantly one person per room (business travel).*

**Proposed Hotel (York Street)****Average Sanitary Flow:**

Residential:  $Q_{SAN} = 128 \text{ units} \times 1.1 \text{ persons/unit} \times 225 \text{ L/cap/day} = 31,680 \text{ L/day} = 0.37 \text{ L/s}$

Ballroom/Bar:  $Q_{SAN} = 50 \text{ seats} \times 70 \text{ L/seat/day} = 3,500 \text{ L/day} = 0.04 \text{ L/s}$

Staff:  $Q_{SAN} = 20 \text{ staff} \times 40 \text{ L/staff/day} = 800 \text{ L/day} = 0.01 \text{ L/s}$

Total Average Residential Flow = 0.37 L/s

Total Average Commercial Flow = 0.04 L/s + 0.01 L/s = 0.05 L/s

Total Average Sanitary Flow = 0.37 L/s + 0.05 L/s = 0.42 L/s

**Peak Sanitary Flow:**

Residential Peaking Factor (Harmon Equation) = 3.56

Total Peak Residential Flow = 0.37 L/s  $\times$  3.56 = 1.32 L/s

Commercial Peaking Factor = 1.0

Total Peak Commercial Flow = 0.05 L/s  $\times$  1.0 = 0.05 L/s

Total Peak Sanitary Flow = 1.32 L/s + 0.05 L/s = 1.37 L/s

*\* Based on predominantly one person per room (business travel).*

**Proposed Condominium (George Street)****Average Sanitary Flow:**

Residential:  $Q_{SAN} = 282 \text{ units} \times 1.8 \text{ persons/unit} \times 280 \text{ L/cap/day} = 142,128 \text{ L/day} = 1.65 \text{ L/s}$

Commercial:  $Q_{SAN} = 0.1097 \text{ ha} (1097 \text{ m}^2) \times 28,000 \text{ L/ha/d} = 3072 \text{ L/day} = 0.04 \text{ L/s}$



$$\text{Total Average Sanitary Flow} = 1.65 \text{ L/s} + 0.04 \text{ L/s} = 1.69 \text{ L/s}$$

**Peak Sanitary Flow:**

$$\text{Residential Peaking Factor (Harmon Equation)} = 3.38$$

$$\text{Total Peak Residential Flow} = 1.65 \text{ L/s} \times 3.38 = 5.58 \text{ L/s}$$

$$\text{Commercial Peaking Factor} = 1.0$$

$$\text{Total Peak Commercial Flow} = 0.04 \text{ L/s} \times 1.0 = 0.04 \text{ L/s}$$

$$\text{Total Peak Sanitary Flow} = 5.58 \text{ L/s} + 0.04 \text{ L/s} = 5.62 \text{ L/s}$$

**Infiltration – Site**

$$\text{Total Site Area} = 0.42 \text{ ha}$$

$$\text{Infiltration Flow} = 0.33 \text{ L/s/ha} \times 0.42 \text{ ha} = 0.14 \text{ L/s}$$

**Site Total**

$$\text{Total Average Sanitary Flow} = \mathbf{2.87 \text{ L/s}}$$

$$\text{Total Peak Sanitary Flow (including infiltration)} = \mathbf{9.32 \text{ L/s}}$$

**Sanitary Flows Under Current Zoning**

Currently, the site is zoned as MD2 – Mixed-Use Downtown. The current zoning by-law permits hotel and a restaurant component as well as residential mid to high use development and a commercial component ancillary to residential. Based on this, sanitary flows are calculated below.

**Existing Hotel (Dalhousie Street)**

$$\text{Average Sanitary Flow} = 0.76 \text{ L/s}^*$$

$$\text{Peak Sanitary Flow} = 2.19 \text{ L/s}^*$$

*\*See calculations in previous section.*

**Existing 110 York Street (The Whiskey Bar)****Average Sanitary Flow:**

$$\text{Bar: } Q_{\text{SAN}} = 170 \text{ seats} \times 70 \text{ L/seat/day} = 11,900 \text{ L/day} = 0.14 \text{ L/s}$$

$$\text{Staff: } Q_{\text{SAN}} = 6 \text{ staff} \times 40 \text{ L/staff/day} = 240 \text{ L/day} = 0.003 \text{ L/s}$$

$$\text{Total Average Sanitary Flow} = 0.14 \text{ L/s} + 0.003 \text{ L/s} = 0.14 \text{ L/s}$$

**Total Peak Sanitary Flow:**

$$\text{Commercial Peaking Factor} = 1.5$$

$$\text{Total Peak Sanitary Flow} = 0.14 \text{ L/s} \times 1.5 = 0.21 \text{ L/s}$$

**Future Residential Development (George Street)****Average Sanitary Flow:**

$$\text{Total Site Area} = 0.42 \text{ ha}$$

$$\text{Area Designated for Future Residential Development} = 0.21 \text{ ha}$$



$$\text{Population} = 0.21 \text{ ha} \times 1800 \text{ persons/ha} = 378 \text{ persons}$$

$$\text{Total Average Sanitary Flow} = 378 \text{ persons} \times 280 \text{ L/cap/day} = 105,840 \text{ L/day} = 1.23 \text{ L/s}$$

Peak Sanitary Flow:

$$\text{Residential Peaking Factor (Harmon Equation)} = 3.43$$

$$\text{Total Peak Residential Flow} = 1.23 \text{ L/s} \times 3.43 = 4.22 \text{ L/s}$$

#### Infiltration – Site

$$\text{Total Site Area} = 0.42 \text{ ha}$$

$$\text{Infiltration Flow} = 0.33 \text{ L/s/ha} \times 0.42 \text{ ha} = 0.14 \text{ L/s}$$

#### Site Total

$$\text{Total Average Sanitary Flow} = \mathbf{2.13 \text{ L/s}}$$

$$\text{Total Peak Sanitary Flow (including infiltration)} = \mathbf{6.76 \text{ L/s}}$$

The sanitary flows from the proposed development are in close proximity to the flows calculated under the existing zoning. The existing receiving sewers are a 1200 mm dia. sanitary sewer at  $\pm 2.0\%$  slope on York Street with a capacity of approximately 5,750 L/s and a 1500 mm dia. sanitary sewer at  $\pm 1.5\%$  slope on George Street with a capacity of approximately 11,650 L/s. Therefore, the proposed development will have negligible impact on the existing municipal sanitary sewer system.

### **3.0 STORMWATER**

Stormwater flows from the site are currently conveyed to the existing storm sewer system via on-site catchbasins and overland flows to York Street, Dalhousie Street, and George Street. The stormwater from the Dalhousie Street hotel as well as the existing building at 110 & 112 York Street is captured by roof drains and outlet through their respective existing service connections. As part of this development, all stormwater will be controlled on site prior to being discharged to the storm system.

The proposed York Street hotel development will be serviced by a new 250 mm dia. storm service that will connect to the existing 675 mm dia. storm sewer on York Street; therefore, the existing 150 mm dia. storm service that is currently connected to the existing 675 mm dia. storm sewer on York Street will need to be abandoned. The new storm service connection to the building will be equipped with a backwater valve.

Furthermore, the proposed condominium development will be serviced by a 250 mm dia. storm service that will connect to the existing 900 mm dia. storm sewer on George Street. The proposed storm service connection to the building will be equipped with a backwater valve. Refer to **Figure 3** for details.

The City will require that on-site stormwater management be implemented to control post-development stormwater discharge for both the 5 & 100 year storm events based on an allowable runoff coefficient (C) of 0.50, a time of concentration ( $t_c$ ) of 20 minutes, and a 5-year storm control. Stormwater management will be achieved through the use of rooftop controls and surface ponding (as required). Should surplus storage be required, stormwater management



alternatives such as storage tanks or super-pipes will be implemented. Temporary storage will be provided at the surface as required to supply the necessary release rate during all phases until full build out is achieved with underground systems.

The site will be graded such that flows in excess of the 100-year storm event will be conveyed overland to York Street, Dalhousie Street and George Street. Erosion and sediment control measures will be implemented during all phases of construction and inspected regularly.

## 4.0 WATERMAIN

### 4.1 Domestic Water Demand

The existing Dalhousie Street hotel is serviced by a 150mm dia. water service that is connected to the existing 200mm dia. watermain in York Street. The proposed York Street hotel development will be serviced by a separate 150 mm dia. water service that will connect to the existing 200 mm dia. watermain on York Street. The existing water service for the 110 York Street property will need to be blanked at the City watermain and abandoned. The proposed condominium development will be serviced by a 200mm dia. water service that will connect to the existing 300 mm dia. watermain on George Street. Refer to **Figure 3** for details.

Estimated domestic daily water demands for the development are roughly the same as the proposed development sanitary flows listed above in Section 2.0:

#### Existing Hotel (Dalhousie Street)

Residential Average Day Demand = 0.57 L/s

Residential Maximum Day Demand (2.5 x avg. day) = 1.43 L/s

Residential Peak Hour Demand (2.2 x max. day) = 3.15 L/s

Commercial Average Day Demand (Restaurant + Bar + Staff) = 0.19 L/s

Commercial Maximum Day Demand (1.5 x avg. day) = 0.29 L/s

Commercial Peak Hour Demand (1.8 x max. day) = 0.52 L/s

Total Average Day Demand = 0.76 L/s

Total Maximum Day Demand = 1.72 L/s

Total Peak Hour Demand = 3.67 L/s

#### Proposed Hotel (York Street)

Residential Average Day Demand = 0.37 L/s

Residential Maximum Day Demand (2.5 x avg. day) = 0.93 L/s

Residential Peak Hour Demand (2.2 x max. day) = 2.05 L/s

Commercial Average Day Demand (Ballroom/Bar + Staff) = 0.05 L/s

Commercial Maximum Day Demand (1.5 x avg. day) = 0.08 L/s

Commercial Peak Hour Demand (1.8 x max. day) = 0.14 L/s

Total Average Day Demand = 0.42 L/s

Total Maximum Day Demand = 1.01 L/s

Total Peak Hour Demand = 2.19 L/s



Condominium (George Street)

Residential Average Day Demand = 1.65 L/s

Residential Maximum Day Demand (2.5 x avg. day) = 4.13 L/s

Residential Peak Hour Demand (2.2 x max. day) = 9.09 L/s

Commercial Average Day Demand = 0.04 L/s

Commercial Maximum Day Demand (1.5 x avg. day) = 0.06 L/s

Commercial Peak Hour Demand (1.8 x max. day) = 0.11 L/s

Total Average Day Demand = 1.69 L/s

Total Maximum Day Demand = 4.19 L/s

Total Peak Hour Demand = 9.20 L/s

Based on the data provided by the City, the existing watermain in the area are adequate to service this development. According to hydrant test results, the watermain in the street can deliver in the range of approximately 1000 igpm ( $\pm 75.8$  L/s) at a dynamic pressure greater than 56 psi. A copy of the watermain data is attached in **Appendix A**.

#### 4.2 Fire Demand

Section 4.2.11 of the City of Ottawa Water Design Guidelines reads:

“When calculating the fire flow requirements and affected pipe sizing, designers shall use the method developed by the Fire Underwriters Survey.”, and

“The requirements for levels of fire protection on private property are covered in Section 7.2.11 of the Ontario Building Code.”

The Fire Underwriters Survey is used to assess the performance of the water distribution system on a “City Block” basis rather than an individual building basis. The Ontario Building Code governs the assessment of fire demand for individual buildings.

Section 7.2.11.1 of the Ontario Building Codes states that the design, construction, installation and testing of fire service mains and water service pipe combined with fire service mains shall be in conformance with NFPA 24.

NFPA 24 is the standard for the “Installation of Private Fire Service Mains and their Appurtenances”. Chapter 13 of NFPA 24 discusses sizing the private service fire mains for fire protection systems which shall be approved by the authority having jurisdiction, considering the following factors:

- Construction and Occupancy of the building
- Fire Flow and Pressure of the Water Required
- Adequacy of the Water Supply

Specific to this project the buildings will be sprinklered per Section 3.2.2.45 of the Ontario Building Code (OBC). Section 3.2.5.7 of the OBC requires that an adequate water supply for fire fighting be provided to each building, and references Appendix A of the OBC. Sentence 3 of Section A 3.2.5.7 of the OBC (Appendix A) states that NFPA 13 be used for determining both sprinkler and hose stream demands for a sprinklered building.



The design of the sprinkler system is completed by a Fire Protection Engineer, or typically computed by the sprinkler contractor and approved by the Fire Protection Engineer. The process involves detailed hydraulic calculations based on building layout, pipe runs, head losses, fire pump requirements, etc. At this stage in the development process, these details are not available. However, using Chapter 7 of NFPA 13, it is possible to provide a fairly accurate estimate of the fire demand for the building. This estimate is provided below.

**NFPA Chapter 7 Calculation**

22 Storey Residential Building – Light Hazard

15 Storey Hotel Building – Light Hazard [incl. restaurant - Ordinary Hazard (Group 1)]

18-Storey Hotel Building – Light Hazard

4 Level Underground Parking (under residential building - serve both) - Ordinary Hazard (Group 1)

Section 7.2.3 of NFPA 13, “Water Demand Requirements – Hydraulic Calculation Methods” is used to estimate the hose stream demand and the sprinkler demand. The water demand for sprinklers is estimated using the most remote area in the building. Figure 7.2.3.1.2 – Area/Density Curves is used for the worst case scenario, which in this case is the Ordinary Hazard Classification in the underground parking garage. For this classification, Figure 7.2.3.1.2 provides a density of 0.15 gpm/ft<sup>2</sup> using a coverage of 1500 ft<sup>2</sup>, or 225 gpm (US).

Table 7.2.3.1.1 is used to determine the hose stream demand. For Ordinary Hazard a total combined inside and outside hose stream demand of 250 gpm is required. Typically, 150 gpm would be drawn off the hydrant and 100 gpm off the hose cabinets.

Therefore, total estimated demand would be 225 gpm + 250 gpm = 475 gpm. Adding an allowance for head losses through out the sprinkler system, an estimated fire demand of between 550 – 600 gpm, or say 600 USgpm (2,270 L/min) would be required. According to the fire hydrant data provided by the City, the 200 mm and 300 mm watermains on York Street and George Street respectively can deliver in the range of 1,000 l gpm (1,200 USgpm) under normal conditions and 2,100 l gpm (2,500 USgpm) at 20 psi residual. The building will also be equipped with a fire pump, if necessary, to provide the minimum residual pressure at the sprinkler heads.

Reference material from NFPA 13 is contained in **Appendix A**.



## 5.0 CONCLUSIONS

Based on the foregoing, adequate sanitary, storm and water services are available to support this development.

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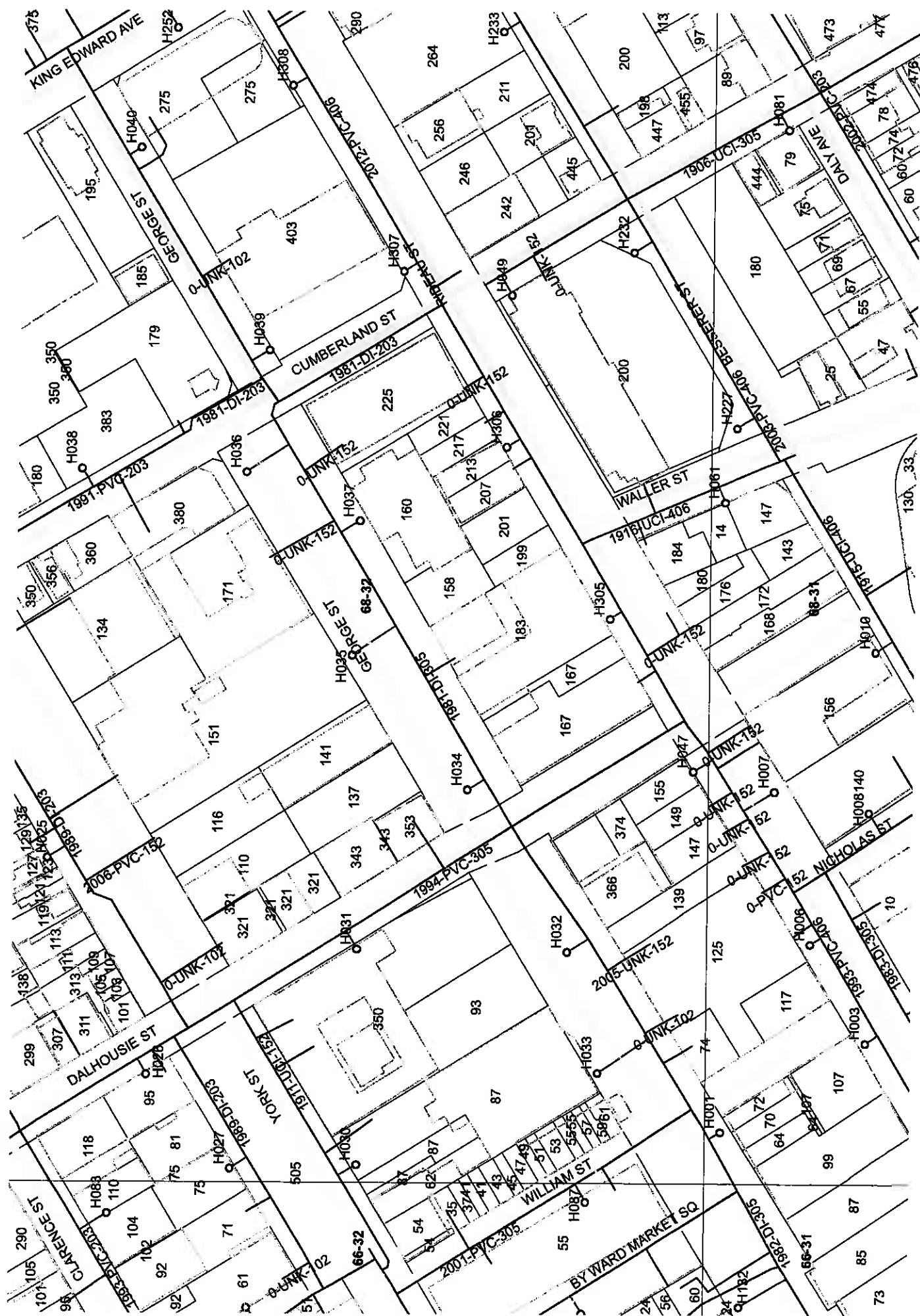
## **APPENDIX A**

### **Hydrant Flow Data/Fire Fighting Information**



**6350**







**6-4.5.9\*** For individual fasteners, the loads determined in 6-4.5.6 shall not exceed the allowable loads provided in Figure 6-4.5.9.

The type of fasteners used to secure the bracing assembly to the structure shall be limited to those shown in Figure 6-4.5.9. For connections to wood, through bolts with washers on each end shall be used. Holes for through bolts shall be  $\frac{1}{16}$  in. (1.6 mm) greater than the diameter of the bolt.

*Exception No. 1: Where it is not practical to install through bolts due to the thickness of the member or inaccessibility, lag screws shall be permitted. Holes shall be pre-drilled  $\frac{1}{8}$  in. (3.2 mm) smaller than the maximum root diameter of the lag screw.*

*Exception No. 2: Other fastening methods are acceptable for use if certified by a registered professional engineer to support the loads determined in accordance with the criteria in 6-4.5.9. Calculations shall be permitted where required by the authority having jurisdiction.*

**6-4.5.10** Sway bracing assemblies shall be listed for a maximum load rating. The loads shall be reduced as shown in Table 6-4.5.10 for loads that are less than 90 degrees from vertical.

*Exception: Where sway bracing utilizing pipe, angles, flats, or rods as shown in Table 6-4.5.8 is used, the components do not require listing. Bracing fittings and connections used with those specific materials shall be listed.*

**Table 6-4.5.10 Allowable Horizontal Load on Brace Assemblies Based on the Weakest Component of the Brace Assembly**

Brace Angle	Allowable Horizontal Load
30-40 degrees from vertical	Listed load rating divided by 2.000
45-59 degrees from vertical	Listed load rating divided by 1.414
60-89 degrees from vertical	Listed load rating divided by 1.155
90 degrees from vertical	Listed load rating

**6-4.5.11** Bracing shall be attached directly to feed and cross mains. Each run of pipe between changes in direction shall be provided with both lateral and longitudinal bracing.

*Exception: Pipe runs less than 12 ft (3.6 m) in length shall be permitted to be supported by the braces on adjacent runs of pipe.*

**6-4.5.12** A length of pipe shall not be braced to sections of the building that will move differentially.

#### **6-4.6 Restraint of Branch Lines.**

**6-4.6.1\*** Restraint is considered a lesser degree of resisting loads than bracing and shall be provided by use of one of the following:

- (1) A listed sway brace assembly
- (2) A wraparound U-hook satisfying the requirements of 6-4.5.3, Exception No. 3
- (3) No. 12, 440-lb (200-kg) wire installed at least 45 degrees from the vertical plane and anchored on both sides of the pipe
- (4) Other approved means

Wire used for restraint shall be located within 2 ft (610 mm) of a hanger. The hanger closest to a wire restraint shall be of a type that resists upward movement of a branch line.

**6-4.6.2** The end sprinkler on a line shall be restrained against excessive vertical and lateral movement.

**6-4.6.3\*** Where upward or lateral movement would result in an impact against the building structure, equipment, or finish materials, branch lines shall be restrained at intervals not exceeding 30 ft (9 m).

**6-4.6.4\*** Sprig-ups 4 ft (1.2 m) or longer shall be restrained against lateral movement.

#### **6-4.7 Hangers and Fasteners Subject to Earthquakes.**

**6-4.7.1** C-type clamps (including beam and large flange clamps) used to attach hangers to the building structure in areas subject to earthquakes shall be equipped with a restraining strap. The restraining strap shall be listed for use with a C-type clamp or shall be a steel strap of not less than 16 gauge thickness and not less than 1 in. (25.4 mm) wide for pipe diameters 8 in. (203 mm) or less and 14 gauge thickness and not less than  $1\frac{1}{4}$  in. (31.7 mm) wide for pipe diameters greater than 8 in. (203 mm). The restraining strap shall wrap around the beam flange not less than 1 in. (25.4 mm). A lock nut on a C-type clamp shall not be used as a method of restraint. A lip on a "C" or "Z" purlin shall not be used as a method of restraint.

Where purlins or beams do not provide an adequate lip to be secured by a restraining strap, the strap shall be through-bolted or secured by a self-tapping screw.

**6-4.7.2** C-type clamps (including beam and large flange clamps), with or without restraining straps, shall not be used to attach braces to the building structure.

**6-4.7.3** Powder-driven fasteners shall not be used to attach braces to the building structure.

*Exception: Powder-driven fasteners shall be permitted where they are specifically listed for service in resisting lateral loads in areas subject to earthquakes.*

**6-4.7.4** Powder-driven fasteners shall not be used to attach hangers to the building structure where the systems are required to be protected against earthquakes using a horizontal force factor exceeding  $0.50 W_p$ , where  $W_p$  is the weight of the water-filled pipe.

*Exception: Powder-driven fasteners shall be permitted where they are specifically listed for horizontal force factors in excess of  $0.50 W_p$ .*

## **Chapter 7 Design Approaches**

### **7-1 General.**

**7-1.1** Water demand requirements shall be determined from the occupancy hazard fire control approach of Section 7-2.

*Exception: Special design approaches as permitted in Section 7-9.*

**7-1.2** For buildings with two or more adjacent occupancies that are not physically separated by a barrier or partition capable of delaying heat from a fire in one area from fusing sprinklers in the adjacent area, the required sprinkler protection for the more demanding occupancy shall extend 15 ft (4.6 m) beyond its perimeter.



## 7-2 Occupancy Hazard Fire Control Approach.

### 7-2.1 Occupancy Classifications.

**7-2.1.1** Occupancy classifications for this standard relate to sprinkler installations and their water supplies only. They shall not be used as a general classification of occupancy hazards.

**7-2.1.2** Occupancies or portions of occupancies shall be classified according to the quantity and combustibility of contents, the expected rates of heat release, the total potential for energy release, the heights of stockpiles, and the presence of flammable and combustible liquids, using the definitions contained in Section 1-4. Classifications are as follows:

Light hazard

Ordinary hazard (Groups 1 and 2)

Extra hazard (Groups 1 and 2)

Special occupancy hazard (*see Section 7-10*)

### 7-2.2 Water Demand Requirements — Pipe Schedule Method.

**7-2.2.1** Table 7-2.2.1 shall be used in determining the minimum water supply requirements for light and ordinary hazard occupancies protected by systems with pipe sized according to the pipe schedules of Section 8-5. Pressure and flow requirements for extra hazard occupancies shall be based on the hydraulic calculation methods of 7-2.3. The pipe schedule method shall be permitted only for new installations of 5000 ft<sup>2</sup> (465 m<sup>2</sup>) or less or for additions or modifications to existing pipe schedule systems sized according to the pipe schedules of Section 8-5. Table 7-2.2.1 shall be used in determining the minimum water supply requirements.

*Exception No. 1: The pipe schedule method shall be permitted for use in systems exceeding 5000 ft<sup>2</sup> (465 m<sup>2</sup>) where the flows required in Table 7-2.2.1 are available at a minimum residual pressure of 50 psi (3.4 bar) at the highest elevation of sprinkler.*

*Exception No. 2: The pipe schedule method shall be permitted for additions or modifications to existing extra hazard pipe schedule systems.*

**7-2.2.2** The lower duration value of Table 7-2.2.1 shall be acceptable only where remote station or central station water-flow alarm service is provided.

**7-2.2.3\*** The residual pressure requirement of Table 7-2.2.1 shall be met at the elevation of the highest sprinkler. (*See the Exceptions to 7-2.2.1*).

**7-2.2.4** The lower flow figure of Table 7-2.2.1 shall be permitted only where the building is of noncombustible construction or the potential areas of fire are limited by building size or compartmentation such that no open areas exceed 3000 ft<sup>2</sup> (279 m<sup>2</sup>) for light hazard or 4000 ft<sup>2</sup> (372 m<sup>2</sup>) for ordinary hazard.

**Table 7-2.2.1 Water Supply Requirements for Pipe Schedule Sprinkler Systems**

Occupancy Classification	Minimum Residual Pressure Required (psi)	Acceptable Flow at Base of Riser (Including Hose Stream Allowance) (gpm)	Duration (minutes)
Light hazard	15	500–750	30–60
Ordinary hazard	20	850–1500	60–90

For SI units, 1 gpm = 3.785 L/min; 1 psi = 0.0689 bar.

### 7-2.3 Water Demand Requirements — Hydraulic Calculation Methods.

#### 7-2.3.1 General.

**7-2.3.1.1\*** The minimum water supply requirements for a hydraulically designed occupancy hazard fire control sprinkler system shall be determined by adding the hose stream demand from Table 7-2.3.1.1 to the water supply for sprinklers determined in 7-2.3.1.2. This supply shall be available for the minimum duration specified in Table 7-2.3.1.1.

*Exception No. 1: An allowance for inside and outside hose shall not be required where tanks supply sprinklers only.*

*Exception No. 2: Where pumps taking suction from a private fire service main supply sprinklers only, the pump need not be sized to accommodate inside and outside hose. Such hose allowance shall be considered in evaluating the available water supplies.*

**7-2.3.1.2** The water supply for sprinklers only shall be determined either from the area/density curves of Figure 7-2.3.1.2 in accordance with the method of 7-2.3.2 or be based upon the room design method in accordance with 7-2.3.3, at the discretion of the designer. For special areas under consideration, as described in 7-2.3.4, separate hydraulic calculations shall be required in addition to those required by 7-2.3.2 or 7-2.3.3.



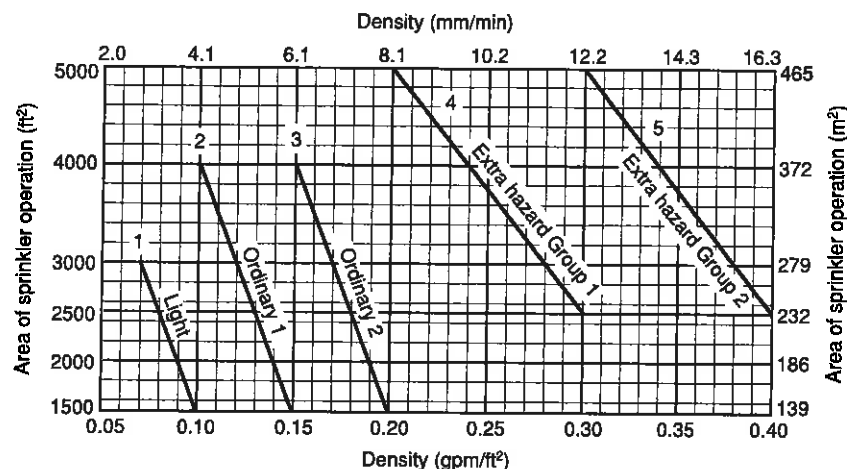
**Table 7-2.3.1.1† Hose Stream Demand and Water Supply Duration Requirements for Hydraulically Calculated Systems**

Occupancy or Commodity Classification	Inside Hose (gpm)	Total Combined Inside and Outside Hose (gpm)	Duration (minutes)
Light hazard	0, 50, or 100	100	30
Ordinary hazard	0, 50, or 100	250	60-90
Extra hazard	0, 50, or 100	500	90-120
Rack storage, Class I, II, and III commodities up to 12 ft (3.7 m) in height	0, 50, or 100	250	90
Rack storage, Class IV commodities up to 10 ft (3.1 m) in height	0, 50, or 100	250	90
Rack storage, Class IV commodities up to 12 ft (3.7 m) in height	0, 50, or 100	500	90
Rack storage, Class I, II, and III commodities over 12 ft (3.7 m) in height	0, 50, or 100	500	90
Rack storage, Class IV commodities over 12 ft (3.7 m) in height and plastic commodities	0, 50, or 100	500	120
General storage, Class I, II, and III commodities over 12 ft (3.7 m) up to 20 ft (6.1 m)	0, 50, or 100	500	90
General storage, Class IV commodities over 12 ft (3.7 m) up to 20 ft (6.1 m)	0, 50, or 100	500	120
General storage, Class I, II, and III commodities over 20 ft (6.1 m) up to 30 ft (9.1 m)	0, 50, or 100	500	120
General storage, Class IV commodities over 20 ft (6.1 m) up to 30 ft (9.1 m)	0, 50, or 100	500	150
General storage, Group A plastics ≤ 5 ft (1.5 m)	0, 50, or 100	250	90
General storage, Group A plastics over 5 ft (1.5 m) up to 20 ft (6.1 m)	0, 50, or 100	500	120
General storage, Group A plastics over 20 ft (6.1 m) up to 25 ft (7.6 m)	0, 50, or 100	500	150

For SI units, 1 gpm = 3.785 L/min.



Figure 7-2.3.1.2 Area/density curves.



**7-2.3.1.3** Regardless of which of the two methods is used, the following restrictions shall apply:

(a) For areas of sprinkler operation less than 1500 ft<sup>2</sup> (139 m<sup>2</sup>) used for light and ordinary hazard occupancies, the density for 1500 ft<sup>2</sup> (139 m<sup>2</sup>) shall be used. For areas of sprinkler operation less than 2500 ft<sup>2</sup> (232 m<sup>2</sup>) for extra hazard occupancies, the density for 2500 ft<sup>2</sup> (232 m<sup>2</sup>) shall be used.

(b) \*For buildings having unsprinklered combustible concealed spaces (as described in 5-13.1.1 and 5-13.7), the minimum area of sprinkler operation shall be 3000 ft<sup>2</sup> (279 m<sup>2</sup>).

*Exception No. 1: Combustible concealed spaces filled entirely with noncombustible insulation.*

*Exception No. 2: \*Light or ordinary hazard occupancies where noncombustible or limited combustible ceilings are directly attached to the bottom of solid wood joists so as to create enclosed joist spaces 160 ft<sup>3</sup> (4.8 m<sup>3</sup>) or less in volume.*

*Exception No. 3: \*Concealed spaces where the exposed surfaces have a flame spread rating of 25 or less and the materials have been demonstrated to not propagate fire in the form in which they are installed in the space.*

(c) Water demand of sprinklers installed in racks or water curtains shall be added to the ceiling sprinkler water demand at the point of connection. Demands shall be balanced to the higher pressure. (See Chapter 8.)

(d) Water demand of sprinklers installed in concealed spaces or under obstructions such as ducts and cutting tables need not be added to ceiling demand.

(e) Where inside hose stations are planned or are required, a total water allowance of 50 gpm (189 L/min) for a single hose station installation or 100 gpm (378 L/min) for a multiple hose station installation shall be added to the sprinkler requirements. The water allowance shall be added in 50-gpm (189-L/min) increments beginning at the most remote hose station, with each increment added at the pressure required by the sprinkler system design at that point.

(f) When hose valves for fire department use are attached to wet pipe sprinkler system risers in accordance with 5-15.5.2, the water supply shall not be required to be added to standpipe demand as determined from NFPA 14, *Standard for the Installation of Standpipe and Hose Systems*.

*Exception No. 1: Where the combined sprinkler system demand and hose stream allowance of Table 7-2.3.1.1 exceeds the requirements of NFPA 14, Standard for the Installation of Standpipe and Hose Systems, this higher demand shall be used.*

*Exception No. 2: For partially sprinklered buildings, the sprinkler demand, not including hose stream allowance, as indicated in Table 7-2.3.1.1 shall be added to the requirements given in NFPA 14, Standard for the Installation of Standpipe and Hose Systems.*

(g) Water allowance for outside hose shall be added to the sprinkler and inside hose requirement at the connection to the city water main or a yard hydrant, whichever is closer to the system riser.

(h) The lower duration values in Table 7-2.3.1.1 shall be permitted where remote station or central station waterflow alarm service is provided.

(i) Where pumps, gravity tanks, or pressure tanks supply sprinklers only, requirements for inside and outside hose need not be considered in determining the size of such pumps or tanks.

**7-2.3.1.4** Total system water supply requirements shall be determined in accordance with the hydraulic calculation procedures of Section 8-4.

### 7-2.3.2 Area/Density Method.

**7-2.3.2.1** The water supply requirement for sprinklers only shall be calculated from the area/density curves in Figure 7-2.3.1.2 or from Section 7-10 where area/density criteria is specified for special occupancy hazards. When using Figure 7-2.3.1.2, the calculations shall satisfy any single point on the appropriate area/density curve as follows:

- (1) Light hazard area/density curve 1
- (2) Ordinary hazard (Group 1) area/density curve 2
- (3) Ordinary hazard (Group 2) area/density curve 3
- (4) Extra hazard (Group 1) area/density curve 4
- (5) Extra hazard (Group 2) area/density curve 5

It shall not be necessary to meet all points on the selected curve.

*Exception: Sprinkler demand for storage occupancies as determined in Sections 7-3 through 7-8.*

**7-2.3.2.2** For protection of miscellaneous storage, miscellaneous tire storage, and storage up to 12 ft (3.7 m) in height, the discharge criteria in Table 7-2.3.2.2 shall apply.



Table A-1-4.11 Typical Cotton Bale Types and Approximate Sizes

Bale Type	Dimensions		Average Weight		Volume		Density	
	in.	mm	lb	kg	ft <sup>3</sup>	m <sup>3</sup>	lb/ft <sup>3</sup>	kg/m <sup>3</sup>
Gin, flat	55 × 45 × 28	1397 × 1143 × 711	500	226.8	40.1	1.13	12.5	201
Modified gin, flat	55 × 45 × 24	1397 × 1143 × 610	500	226.8	34.4	0.97	14.5	234
Compressed, standard	57 × 29 × 23	1448 × 736 × 584	500	226.8	22.0	0.62	22.7	366
Gin, standard	55 × 31 × 21	1397 × 787 × 533	500	226.9	20.7	0.58	24.2	391
Compressed, universal	58 × 25 × 21	1475 × 635 × 533	500	226.8	17.6	0.50	28.4	454
Gin, universal	55 × 26 × 21	1397 × 660 × 533	500	226.8	17.4	0.49	28.7	463
Compressed, high density	58 × 22 × 21	1473 × 559 × 533	500	226.8	15.5	0.44	32.2	515

## A-1-4.11 Baled Cotton. See Table A-1-4.11.

**A-1-4.12 Array, Standard (Paper).** The occasional presence of partially used rolls on top of columns of otherwise uniform diameter rolls does not appreciably affect the burning characteristics.

**A-1-4.12 Roll Paper Storage, Wrapped.** Rolls that are completely protected with a heavyweight kraft wrapper on both sides and ends are subject to a reduced degree of fire hazard. Standard methods for wrapping and capping rolls are outlined in Figure A-1-4.12.

In some cases, rolls are protected with laminated wrappers, using two sheets of heavy kraft with a high-temperature wax laminate between the sheets. Where using this method, the overall weight of wax-laminated wrappers should be based on the basis weight per 1000 ft<sup>2</sup> (92.9 m<sup>2</sup>) of the outer sheet only, rather than on the combined basis weight of the outer and inner laminated wrapper sheets. A properly applied wrapper can have the effect of changing the class of a given paper to essentially that of the wrapper material. The effect of applying a wrapper to tissue has not been determined by test.

**A-1-4.12 Roll Paper Storage Height.** The size of rolls and limitations of mechanical handling equipment should be considered in determining maximum storage height.

**A-2-1** Occupancy examples in the listings as shown in the various hazard classifications are intended to represent the norm for those occupancy types. Unusual or abnormal fuel loadings or combustible characteristics and susceptibility for changes in these characteristics, for a particular occupancy, are considerations that should be weighed in the selection and classification.

The light hazard classification is intended to encompass residential occupancies; however, this is not intended to preclude the use of listed residential sprinklers in residential occupancies or residential portions of other occupancies.

**A-2-1.1** Light hazard occupancies include occupancies having uses and conditions similar to the following:

Churches

Clubs

Eaves and overhangs, if of combustible construction with no combustibles beneath

Figure A-1-4.12 Wrapping and capping terms and methods.

**Wrapper**

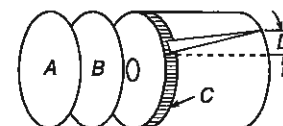
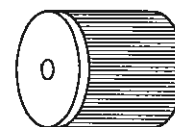
Exterior wrapper  
Body wrapper

General term for protective wrapping of sides and ends on roll.

**Body wrap**

Sleeve wrap  
Wrap — do not cap

Wrapper placed around circumference of roll. No heads or caps needed.

**Heads**

Headers

Protection applied to the ends of the rolls (A and B). Heads do not lap over the end of the roll.

Inside heads

Protection applied to the ends of the rolls next to the roll itself (B). The wrapper of the rolls is crimped down over these heads.

Outside heads

Protection applied to the ends of the rolls on the outside (A). This head is applied after the wrapper is crimped.

**Edge protectors**

Edge bands

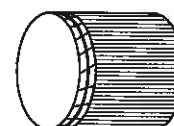
Refers to extra padding to prevent damage to roll edges (C).

Overwrap

The distance the body wrap or wrapper overlaps itself (D).

**Roll cap**

A protective cover placed over the end of a roll. Edges of cap lap over the end of the roll and are secured to the sides of the roll.





Educational  
Hospitals  
Institutional  
Libraries, except large stack rooms  
Museums  
Nursing or convalescent homes  
Offices, including data processing  
Residential  
Restaurant seating areas  
Theaters and auditoriums, excluding stages and prosceniums  
Unused attics

**A-2-1.2.1** Ordinary hazard occupancies (Group 1) include occupancies having uses and conditions similar to the following:

Automobile parking and showrooms  
Bakeries  
Beverage manufacturing  
Canneries  
Dairy products manufacturing and processing  
Electronic plants  
Glass and glass products manufacturing  
Laundries  
Restaurant service areas

**A-2-1.2.2** Ordinary hazard occupancies (Group 2) include occupancies having uses and conditions similar to the following:

Cereal mills  
Chemical plants — ordinary  
Confectionery products  
Distilleries  
Dry cleaners  
Feed mills  
Horse stables  
Leather goods manufacturing  
Libraries — large stack room areas  
Machine shops  
Metal working  
Mercantile  
Paper and pulp mills  
Paper process plants  
Piers and wharves  
Post offices  
Printing and publishing  
Repair garages  
Resin application area  
Stages  
Textile manufacturing  
Tire manufacturing  
Tobacco products manufacturing  
Wood machining  
Wood product assembly

**A-2-1.3.1** Extra hazard occupancies (Group 1) include occupancies having uses and conditions similar to the following:

Aircraft hangars (except as governed by NFPA 409, *Standard on Aircraft Hangars*)  
Combustible hydraulic fluid use areas  
Die casting

Metal extruding  
Plywood and particle board manufacturing  
Printing [using inks having flash points below 100°F (38°C)]  
Rubber reclaiming, compounding, drying, milling, vulcanizing  
Saw mills  
Textile picking, opening, blending, garnetting, or carding, combining of cotton, synthetics, wool shoddy, or burlap  
Upholstering with plastic foams

**A-2-1.3.2** Extra hazard occupancies (Group 2) include occupancies having uses and conditions similar to the following:

Asphalt saturating  
Flammable liquids spraying  
Flow coating  
Manufactured home or modular building assemblies (where finished enclosure is present and has combustible interiors)  
Open oil quenching  
Plastics processing  
Solvent cleaning  
Varnish and paint dipping

**A-2-1.4** Other NFPA standards contain design criteria for fire control or fire suppression (*see 2-1.4 and Chapter 13*). While these can form the basis of design criteria, this standard describes the methods of design, installation, fabrication, calculation, and evaluation of water supplies that should be used for the specific design of the system.

Other NFPA standards contain sprinkler system design criteria for fire control or suppression of specific hazards. This information has been either referenced or copied into Chapters 5 and 7 using NFPA's extract policy.

**A-2-2** Specification of the type, amount, and arrangement of combustibles for any commodity classification is essentially an attempt to define the potential fire severity, based on its burning characteristics, so the fire can be successfully controlled by the prescribed sprinkler protection for the commodity class. In actual storage situations, however, many storage arrays do not fit precisely into one of the fundamental classifications; therefore, the user needs to make judgments after comparing each classification to the existing storage conditions. Storage arrays consist of thousands of products, which make it impossible to specify all the acceptable variations for any class. As an alternative, a variety of common products are classified in this appendix based on judgment, loss experience, and fire test results.

Table A-2-2 provides examples of commodities not addressed by the classifications in Section 2-2.

Table A-2-2.3 is an alphabetized list of commodities with corresponding classifications.

Tables A-2-2.3.1 through A-2-2.3.4 and A-2-2.4.1 provide examples of commodities within a specific class.

**Table A-2-2 Examples of Commodities Not Addressed by the Classifications in Section 2-2**

Boxes, Crates
- Empty, wood slatted
Lighters (butane)
- Loose in large containers (Level 3 aerosol)

\*Should be treated as idle pallets.



## **APPENDIX B**

### **Servicing Study Guidelines Checklist**



**Development Servicing Study Checklist**

<b>4.1 General Content</b>	<b>Addressed (Y/N/NA)</b>	<b>Comments</b>
Executive Summary (for larger reports only).	NA	
Date and revision number of the report.	Y	
Location map and plan showing municipal address, boundary, and layout of proposed development.	Y	Figure 1
Plan showing the site and location of all existing services.	Y	Figure 3
Development statistics, land use, density, adherence to zoning and official plan, and reference to applicable subwatershed and watershed plans that provide context to which individual developments must adhere.	Y	Refer to Site Plan
Summary of Pre-consultation Meetings with City and other approval agencies.	N	
Reference and confirm conformance to higher level studies and reports (Master Servicing Studies, Environmental Assessments, Community Design Plans), or in the case where it is not in conformance, the proponent must provide justification and develop a defensible design criteria.	NA	
Statement of objectives and servicing criteria.	Y	
Identification of existing and proposed infrastructure available in the immediate area.	Y	
Identification of Environmentally Significant Areas, watercourses and Municipal Drains potentially impacted by the proposed development (Reference can be made to the Natural Heritage Studies, if available).	NA	
Concept level master grading plan to confirm existing and proposed grades in the development. This is required to confirm the feasibility of proposed stormwater management and drainage, soil removal and fill constraints, and potential impacts to neighboring properties. This is also required to confirm that the proposed grading will not impede existing major system flow paths.	N/A	
Identification of potential impacts of proposed piped services on private services (such as wells and septic fields on adjacent lands) and mitigation required to address potential impacts.	NA	
Proposed phasing of the development, if applicable.	NA	
Reference to geotechnical studies and recommendations concerning servicing.	NA	
All preliminary and formal site plan submissions should have the following information:		
Metric scale	Y	
North arrow (including construction North)	Y	
Key plan	Y	Figure 1
Name and contact information of applicant and property owner	N	
Property limits including bearings and dimensions	Y	Figures 2 & 3
Existing and proposed structures and parking areas	Y	Figures 2 & 3
Easements, road widening and rights-of-way	Y	
Adjacent street names	Y	



**Development Servicing Study Checklist**

<b>4.2 Water</b>	<b>Addressed (Y/N/NA)</b>	<b>Comments</b>
Confirm consistency with Master Servicing Study, if available.	N/A	
Availability of public infrastructure to service proposed development.	Y	Figure 3
Identification of system constraints.	NA	
Identify boundary conditions.	Y	
Confirmation of adequate domestic supply and pressure.	Y	
Confirmation of adequate fire flow protection and confirmation that fire flow is calculated as per the Fire Underwriter's Survey. Output should show available fire flow at locations throughout the development.	Y	
Provide a check of high pressures. If pressure is found to be high, an assessment is required to confirm the application of pressure reducing valves.	NA	
Definition of phasing constraints. Hydraulic modeling is required to confirm servicing for all defined phases of the project including the ultimate design.	NA	
Address reliability requirements such as appropriate location of shut-off valves.	NA	
Check on the necessity of a pressure zone boundary modification.	NA	
Reference to water supply analysis to show that major infrastructure is capable of delivering sufficient water for the proposed land use. This includes data that shows that the expected demands under average day, peak hour and fire flow conditions provide water within the required pressure range.	Y	
Description of the proposed water distribution network, including locations of proposed connections to the existing system, provisions for necessary looping, and appurtenances (valves, pressure reducing valves, valve chambers, and fire hydrants) including special metering provisions.	Y	
Description of off-site required feeder mains, booster pumping stations, and other water infrastructure that will be ultimately required to service proposed development, including financing, interim facilities, and timing of implementation.	NA	
Confirmation that water demands are calculated based on the City of Ottawa Design Guidelines.	Y	
Provision of a model schematic showing the boundary conditions locations, streets, parcels, and building locations for reference.	NA	



**Development Servicing Study Checklist**

<b>4.3 Wastewater</b>	<b>Addressed (Y/N/NA)</b>	<b>Comments</b>
Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitored flow data from relatively new infrastructure cannot be used to justify capacity requirements for proposed infrastructure).	Y	
Confirm consistency with Master Servicing Study and/or justifications for deviations.	NA	
Consideration of local conditions that may contribute to extraneous flows that are higher than the recommended flows in the guidelines. This includes groundwater and soil conditions, and age and condition of sewers.	NA	
Description of existing sanitary sewer available for discharge of wastewater from proposed development.	Y	
Verify available capacity in downstream sanitary sewer and/or identification of upgrades necessary to service the proposed development. (Reference can be made to previously completed Master Servicing Study if applicable)	NA	
Calculations related to dry-weather and wet-weather flow rates from the development in standard MOE sanitary sewer design table (Appendix 'C') format.	NA	
Description of proposed sewer network including sewers, pumping stations, and forcemains.	Y	
Discussion of previously identified environmental constraints and impact on servicing (environmental constraints are related to limitations imposed on the development in order to preserve the physical condition of watercourses, vegetation, soil cover, as well as protecting against water quantity and quality).	NA	
Pumping stations: impacts of proposed development on existing pumping stations or requirements for new pumping station to service development.	NA	
Forcemain capacity in terms of operational redundancy, surge pressure and maximum flow velocity.	NA	
Identification and implementation of the emergency overflow from sanitary pumping stations in relation to the hydraulic grade line to protect against basement flooding.	NA	
Special considerations such as contamination, corrosive environment etc.	NA	



**Development Servicing Study Checklist**

<b>4.4 Stormwater</b>	<b>Addressed (Y/N/NA)</b>	<b>Comments</b>
Description of drainage outlets and downstream constraints including legality of outlet (i.e. municipal drain, right-of-way, watercourse, or private property).	Y	
Analysis of the available capacity in existing public infrastructure.	NA	
A drawing showing the subject lands, its surroundings, the receiving watercourse, existing drainage patterns and proposed drainage patterns.	NA	
Water quantity control objective (e.g. controlling post-development peak flows to pre-development level for storm events ranging from the 2 or 5 year event (dependent on the receiving sewer design) to 100 year return period); if other objectives are being applied, a rationale must be included with reference to hydrologic analyses of the potentially affected subwatersheds, taking into account long-term cumulative effects.	Y	
Water Quality control objective (basic, normal or enhanced level of protection based on the sensitivities of the receiving watercourse) and storage requirements.	N/A	
Description of stormwater management concept with facility locations and descriptions with references and supporting information.	Y	
Set-back from private sewage disposal systems.	NA	
Watercourse and hazard lands setbacks.	NA	
Record of pre-consultation with the Ontario Ministry of Environment and the Conservation Authority that has jurisdiction on the affected watershed.	NA	
Confirm consistency with sub-watershed and Master Servicing Study, if applicable study exists.	NA	
Storage requirements (complete with calcs) and conveyance capacity for 5 yr and 100 yr events.	N	Will be addressed during detailed design for Site Plan application.
Identification of watercourse within the proposed development and how watercourses will be protected, or, if necessary, altered by the proposed development with applicable approvals.	NA	
Calculate pre and post development peak flow rates including a description of existing site conditions and proposed impervious areas and drainage catchments in comparison to existing conditions.	N	Will be addressed during detailed design for Site Plan application.
Any proposed diversion of drainage catchment areas from one outlet to another.	NA	
Proposed minor and major systems including locations and sizes of stormwater trunk sewers, and SWM facilities.	Y	
If quantity control is not proposed, demonstration that downstream system has adequate capacity for the post-development flows up to and including the 100-year return period storm event.	NA	
Identification of municipal drains and related approval requirements.	NA	
Description of how the conveyance and storage capacity will be achieved for the development.	Y	
100 year flood levels and major flow routing to protect proposed development from flooding for establishing minimum building elevations (MBE) and overall grading.	N	Will be addressed during detailed design for Site Plan application.
Inclusion of hydraulic analysis including HGL elevations.	NA	
Description of approach to erosion and sediment control during construction for the protection of receiving watercourse or drainage corridors.	N	Will be addressed during detailed design for Site Plan application.
Identification of floodplains – proponent to obtain relevant floodplain information from the appropriate Conservation Authority. The proponent may be required to delineate floodplain elevations to the satisfaction of the Conservation Authority if such information is not available or if information does not match current conditions.	NA	
Identification of fill constraints related to floodplain and geotechnical investigation.	NA	



**Development Servicing Study Checklist**

<b>4.5 Approval and Permit Requirements</b>	<b>Addressed (Y/N/NA)</b>	<b>Comments</b>
Conservation Authority as the designated approval agency for modification of floodplain, potential impact on fish habitat, proposed works in or adjacent to a watercourse, cut/fill permits and Approval under Lakes and Rivers Improvement Act. The Conservation Authority is not the approval authority for the Lakes and Rivers Improvement Act. Where there are Conservation Authority regulations in place, approval under the Lakes and Rivers Improvement Act is not required, except in cases of dams as defined in the Act.	NA	
Application for Certificate of Approval (CofA) under the Ontario Water Resources Act.	N	
Changes to Municipal Drains.	N	
Other permits (National Capital Commission, Parks Canada, Public Works and Government Services Canada, Ministry of Transportation etc.)	NA	

<b>4.6 Conclusion</b>	<b>Addressed (Y/N/NA)</b>	<b>Comments</b>
Clearly stated conclusions and recommendations.	Y	
Comments received from review agencies including the City of Ottawa and information on how the comments were addressed. Final sign-off from the responsible reviewing agency.	N	
All draft and final reports shall be signed and stamped by a professional Engineer registered in Ontario.	Y	



**RESIDENTIAL / HOTEL DEVELOPMENT  
141 GEORGE STREET / 325 DALHOUSIE STREET  
OTTAWA, ONTARIO**

**SERVICING DESIGN BRIEF  
(INCL. INTERIM CONDITION)**

**Prepared by:**

**NOVATECH ENGINEERING CONSULTANTS LTD.  
240 Michael Cowpland Dr. - Suite 200  
Ottawa, Ontario  
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**File No.: 112142  
Report Reference No.: R-2014-020  
December 07, 2012 (R-2012-171)  
February 28, 2013 (R-2013-019)  
Revised February 14, 2014**





February 14, 2014

City of Ottawa  
Planning and Growth Management Department  
Development Review (Urban) Services Branch  
Infrastructure Approvals Division  
110 Laurier Avenue West, 4<sup>th</sup> Floor  
Ottawa ON, K1P 1J1

**Attention: Mr. John Wu, P. Eng.**

Dear Sir:

**Reference: Residential / Hotel Development  
141 George Street / 325 Dalhousie Street  
Servicing Design Brief (Incl. Interim Condition)  
Our File No.: 112142**

---

Enclosed herein is the revised Servicing Design Brief (including interim condition) for the proposed Residential / Hotel development at 141 George Street / 325 Dalhousie Street, located east of Dalhousie Street between York Street and George Street. This brief is submitted in support of the zoning amendment and site plan application for the site and outlines how the site will be serviced with sanitary, storm and watermain.

Trusting this report is adequate for your purposes. Should you have any questions, or require additional information, please contact us.

Yours truly,

**NOVATECH ENGINEERING CONSULTANTS LTD.**

A handwritten signature in black ink, appearing to read "John Riddell", is written over a horizontal line.

John Riddell, P.Eng.  
President

JAG/jag



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 Appendix C: Correspondence  
 Appendix D: Servicing Study Guidelines Checklist

### List of Attached Drawings

161612779v-111-Claridge-325 Dalhousie-rev 1      Topographical Survey



## 1.0 INTRODUCTION

The proposed Residential / Hotel (141 George Street / 325 Dalhousie Street) development is located in the Byward Market, east of Dalhousie Street between York Street and George Street in the City of Ottawa, as shown in Figure 1a – Aerial Photo and Figure 1b – Key Plan. The existing properties are currently occupied by the Honest Lawyer bar/restaurant, the 11-storey Union du Canada office building as well as privately-owned surface parking lots which serve the office building. The proposed re-development of the site will consist of a 15-storey hotel with 187 units and a 22-storey tower with 282 condominium units (Ph. 1 – 156 & Ph. 2 – 126) to be constructed in three phases. The hotel building will include a rooftop pool as well as approximately 3,145 ft<sup>2</sup> of commercial floor space and the condominium building will include approximately 11,810 ft<sup>2</sup> of commercial floor space (Ph. 1 – ±1,505 ft<sup>2</sup> & Ph. 2 – ±10,300 ft<sup>2</sup>), both located on the ground floor. Also, a total of approximately 227 underground parking spaces will be provided on 4 levels of underground parking and 5 surface parking spaces. Refer to Figure 2 – Site Plan for details.

**Figure 1a: Aerial Photo of Subject Site**

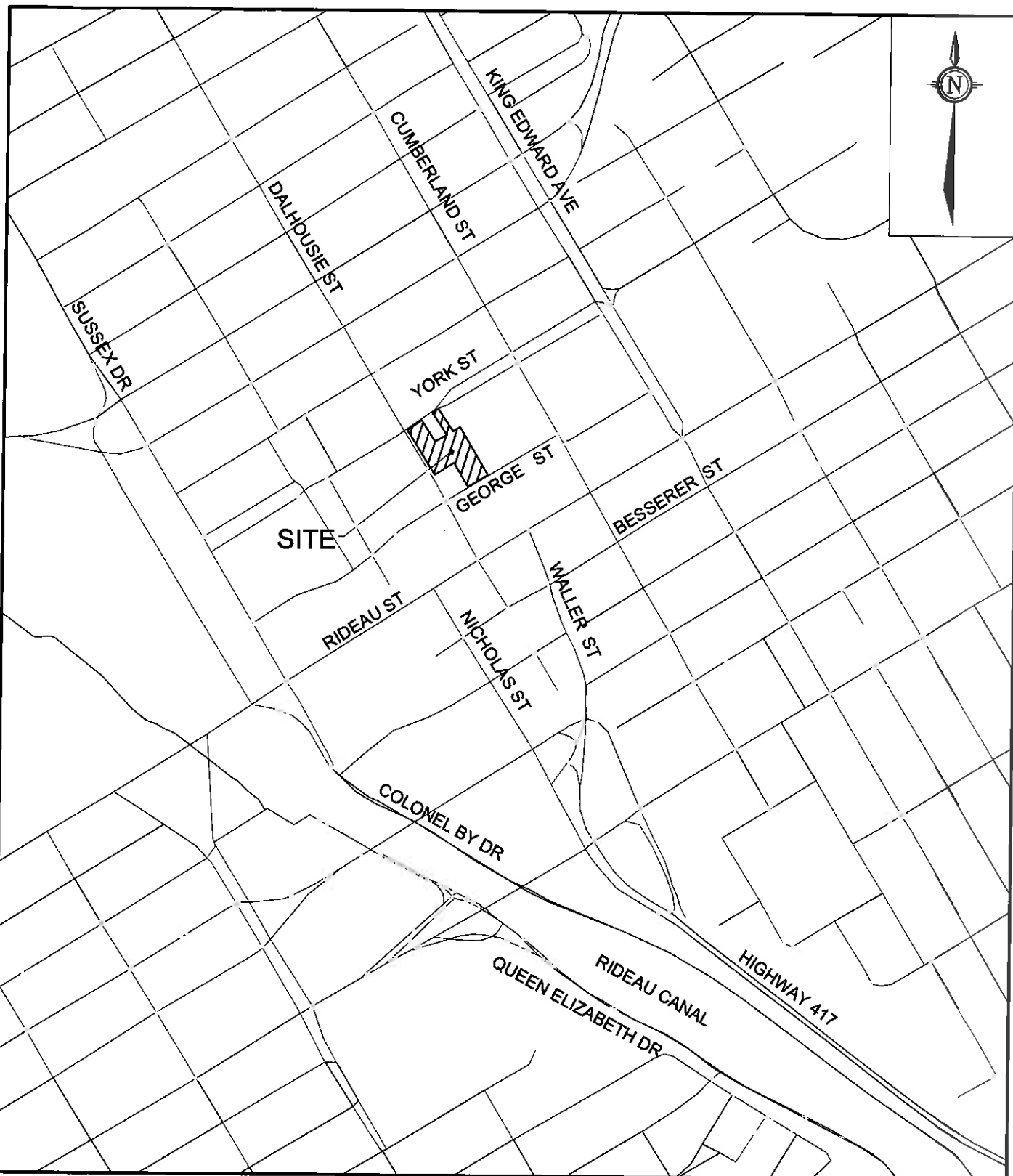


Photo courtesy of [www.bing.com/maps](http://www.bing.com/maps)

As identified in the City of Ottawa's Zoning By-law (ZBL), this site is currently designated as both MD2 S74 – Mixed-Use Downtown (325 Dalhousie Street) and R5R[235] S76 – Residential Fifth Density (141 George Street). The minor zoning by-law amendment will revise the site's current designation for the proposed development to deal with building height, parking requirements and any applicable zoning provisions that cannot be met. The specific details regarding the changes proposed to the zoning of the subject site are provided in a Planning Rationale submitted as part of the ZBL Amendment application.

The subject site is approximately 0.42 ha in area. The development will have a single two-way ramp access to the underground parking garage located on George Street, mid-block between Dalhousie Street and Cumberland Street. The pick-up/drop-off area outside the main entrance to the hotel/condominiums will be accessed from the existing access driveway at 321 Dalhousie





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**CITY OF OTTAWA**

**325 DALHOUSIE STREET &  
141 GEORGE STREET**

**KEY PLAN**

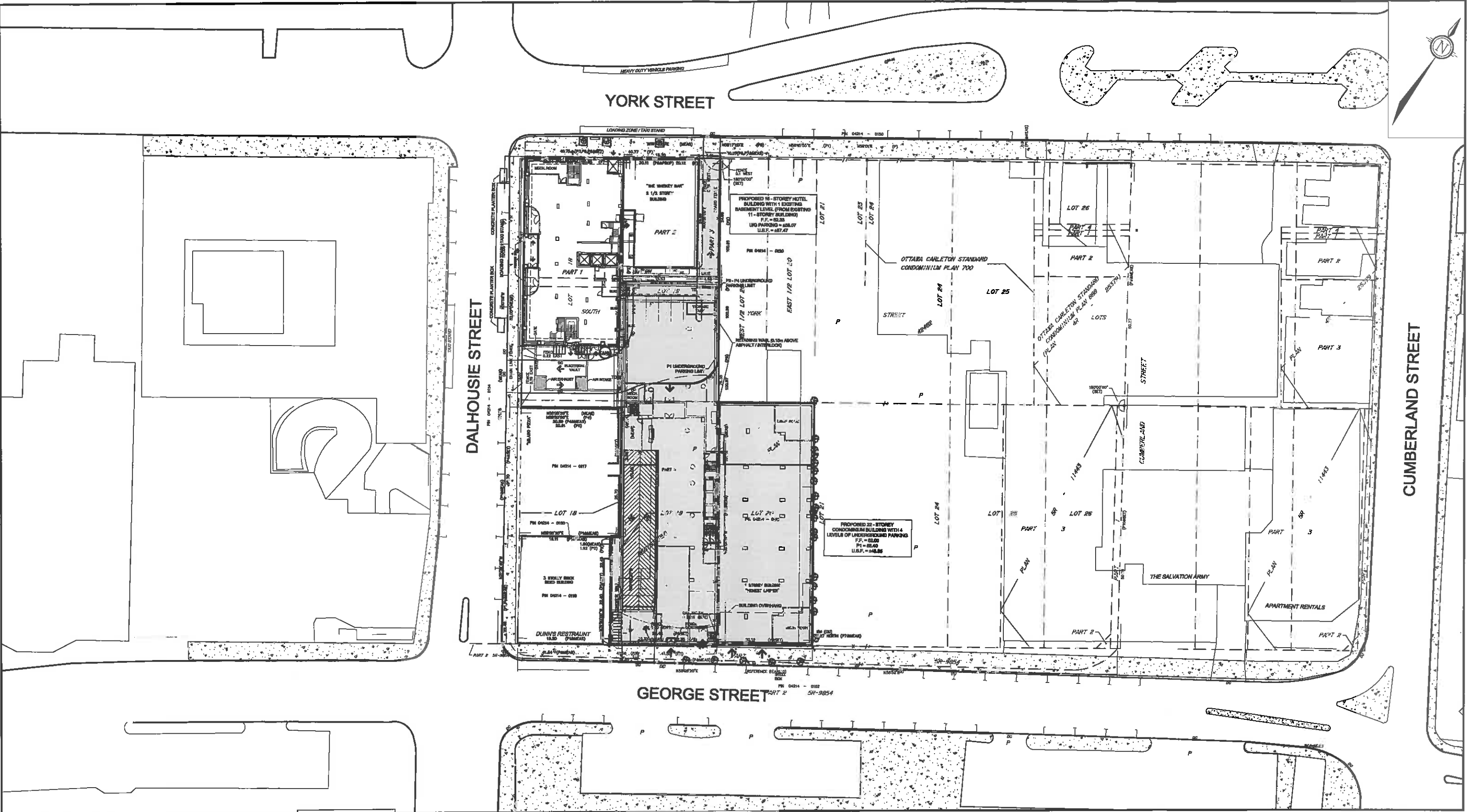
**JAN 2014**

**112142**

**FIGURE # 1B**



M:\2012\112142\CAD\Design\Figures\Design Brief\112142 - SITEPLAN.dwg, FIGURE-3 (2), Feb 10, 2014 - 9:58am, bthurber



LEGEND

- SITE PLAN AREA
- ON STREET PARKING
- PROPOSED FUTURE DEVELOPMENT (PHASE 2 & 3)

NTS

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CITY OF OTTAWA  
325 DALHOUSIE STREET &  
141 GEORGE STREET  
**SITE PLAN**  
JAN 2014 112142 **FIGURE 2**



Street, mid-block between George Street and York Street (adjacent to the Union du Canada office building). A secondary right-out egress only will also be provided at 110 York Street, immediately east of The Whiskey Bar. A copy of the topographical survey which shows the property outline is included in the back of this report. Refer to Figure 3 – Existing Conditions. The construction schedule for the proposed development is as follows:

- Phase 1 (hotel) starting in June 2013, build-out expected in 2014;
- Phase 2 (condo ph.1) scheduled for completion in 2015;
- Phase 3 (condo ph. 2) scheduled for completion in 2017 (subject to market demand).

This servicing design brief will outline how the site will be serviced with sanitary, storm and watermain; and will demonstrate that adequate municipal capacity is available within the existing infrastructure to service the development.

## 2.0 SANITARY SEWER

The proposed hotel development will be serviced by a 200 mm dia. sanitary service that will connect to the existing 1200 mm dia. sanitary sewer on York Street; therefore the existing 200 mm dia. sanitary service that is currently connected to the existing 1200 mm dia. sanitary sewer on York Street will need to be abandoned. The new sanitary service connection to the building will be equipped with a full-port backwater valve. It is to be noted that the attached neighboring 2 ½ storey property has its own existing sanitary service (approx. 200 mm dia.) that also connects to the existing 1200 mm dia. sanitary sewer on York Street (was previously interconnected, but is currently separated).

The hotel will have a rooftop pool with controlled deck drains and the pool drains will be directed to a pump. Both will drain through a dedicated pipe within the building until it connects to the main service prior to exiting the building.

Furthermore, the proposed condominium development will be serviced by a 200 mm dia. sanitary service that will connect to the existing 1980x1500 mm dia. sanitary sewer on George Street. The proposed sanitary service connection to the building will be equipped with a full-port backwater valve.

The proposed development flows are based on the City of Ottawa Sewer Design Guidelines (refer to Appendix A). The flows are comprised of residential, retail, and office space as presented below and are compared to the design flows based on current zoning.

### Sanitary Flows Under Proposed Development

#### Hotel

Residential:  $Q_{SAN} = 187 \text{ units} \times 1.1 \text{ persons/unit} \times 350 \text{ L/cap/day} = 71,995.0 \text{ L/day}$

Restaurant:  $Q_{SAN} = 0.02922 \text{ ha} (3,145 \text{ ft}^2) \times 50,000 \text{ L/ha/d} = 1,461.0 \text{ L/day}$

Average Sanitary Flow = 73,456 L/day = 0.85 L/sec

Peak Sanitary Flow = 3.43 L/sec (with Res. PF = 4.14  $\therefore$  use 4.0  $\Rightarrow$  max, Comm. PF = 1.5)

\* Based on predominantly one person per room (business travel).

#### Condominium – Phase 1

Residential:  $Q_{SAN} = 156 \text{ units} \times 1.8 \text{ persons/unit} \times 350 \text{ L/cap/day} = 98,280.0 \text{ L/day}$

Commercial:  $Q_{SAN} = 0.01398 \text{ ha} (1,505 \text{ ft}^2) \times 50,000 \text{ L/ha/d} = 699.0 \text{ L/day}$





# LEGEND



SITE PLAN AREA



PROPOSED FUTURE DEVELOPMENT (PHASE 2 & 3)

ON STREET PARKING

NTS

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CITY OF OTTAWA

325 DALHOUSIE STREET &  
141 GEORGE STREET

EXISTING CONDITIONS

JAN 2014

112142

FIGURE 3

SHT11X:7.DWG - 278m x 43.1m



Average Sanitary Flow = 98,979 L/day = 1.15 L/sec

Peak Sanitary Flow = 4.56 L/sec (with Res. PF = 4.09  $\therefore$  use 4.0  $\Rightarrow$  max, Comm. PF = 1.5)

### Condominium – Phase 2

Residential:  $Q_{SAN} = 126 \text{ units} \times 1.8 \text{ persons/unit} \times 350 \text{ L/cap/day} = 79,380.0 \text{ L/day}$

Commercial:  $Q_{SAN} = 0.09569 \text{ ha} (10,300 \text{ ft}^2) \times 50,000 \text{ L/ha/d} = 4,784.5 \text{ L/day}$

Average Sanitary Flow = 84,164.5 L/day = 0.97 L/sec

Peak Sanitary Flow = 3.76 L/sec (with Res. PF = 4.13  $\therefore$  use 4.0  $\Rightarrow$  max, Comm. PF = 1.5)

Infiltration Flow = 0.28 L/s/ha  $\times$  0.42 ha = 0.12 L/s

Therefore,

Total Average Sanitary Flow = 3.09 L/sec

Total Peak Sanitary Flow = 11.87 L/sec (with PF)

### Hotel Rooftop Pool

As per discussion with the pool designers, the pool will use cartridge filters and therefore eliminating the need for backwashes. The only flow from the pool will be when it needs to be emptied for maintenance/closure and from the surrounding roof drains during a rainfall event. This will slightly increase the flows to the sanitary sewer; consequently, this would have negligible impact on the existing City sanitary sewer system.

Pool Drainage Flow = 3.0m  $\times$  9.75m  $\times$  1.0m\* per day = 29.25m<sup>3</sup>/day  
= 0.34 L/s for that day only

\* Approximate depth of water in pool.

### Sanitary Flows Under Current Zoning

Currently, the site is zoned as both MD2 S74 – Mixed-Use Downtown (325 Dalhousie Street) and R5R[235] S76 – Residential Fifth Density (141 George Street). The current zoning by-law permits hotel and a restaurant component as well as residential mid to high use development and a commercial component ancillary to residential. Based on this, sanitary flows are calculated below. (Zoning flows are calculated using the City's general population densities from Table 4.1 of the City of Ottawa Sewer Design Guidelines)

Site Area = 0.42 ha (0.21 ha each MD and R5 zones)

Commercial Area = 0.21 ha

Existing building = 8,999.73 m<sup>2</sup> (11-storey: 818.16)

$Q_{ave} = (8,999.73 \text{ m}^2 + 1,281.84 \text{ m}^2) \times 5 \text{ L/m}^2 = 51,407.85 \text{ L/day} = 0.59 \text{ L/sec}$

$Q_{peak} = 0.59 \text{ L/sec} \times 1.5 = 0.89 \text{ L/sec}$

Residential Area = 0.21 ha

Population density = 1800 persons/ha

$Q_{ave} = 0.21 \text{ ha} \times 1800 \text{ persons/ha} \times 350 \text{ L/person/day} = 132,300 \text{ L/day} = 1.53 \text{ L/sec}$



$$P.F. = 1 + \frac{14}{4 + \left(\frac{378}{1000}\right)^{1/2}} = 4.03 \therefore \text{use } 4.0 \Rightarrow \text{max}$$

$$Q_{\text{peak}} = 1.53 \text{ L/sec} * 4.0 = 6.12 \text{ L/sec}$$

$$\text{Infiltration Flow} = 0.28 \text{ L/s/ha} \times 0.42 \text{ ha} = 0.12 \text{ L/s}$$

Therefore,

$$\text{Total Average Sanitary Flow} = 2.24 \text{ L/sec}$$

$$\text{Total Peak Sanitary Flow} = 7.13 \text{ L/sec (with PF)}$$

Therefore, the development sanitary flows under the proposed development are in close proximity to the flows calculated under the existing zoning (note that the existing zoning permits more than what has been accounted for, which would offset the variation); consequently, this would have negligible impact on the existing City sanitary sewer system.

### **Sanitary Flows Under Existing Conditions**

The site in question which is currently occupied by two existing buildings and surface parking lots would generate the following approximate flows:

$$\text{Existing building at 325 Dalhousie} = 8,999.73 \text{ m}^2 \text{ (11-storey: 818.16)}$$

$$Q_{\text{ave}} = 8,999.73 \text{ m}^2 * 5 \text{ L/m}^2 = 44,998.65 \text{ L/day} = 0.52 \text{ L/sec}$$

$$Q_{\text{peak}} = 0.52 \text{ L/sec} * 1.5 = 0.78 \text{ L/sec}$$

$$\text{Existing building at 141 George Street} = 1,128.71 \text{ m}^2 \text{ (1-storey: 1,128.71)}$$

$$Q_{\text{ave}} = (1,128.71 \text{ m}^2) * 5 \text{ L/m}^2 = 5,643.55 \text{ L/day} = 0.07 \text{ L/sec}$$

$$Q_{\text{peak}} = 0.07 \text{ L/sec} * 1.5 = 0.11 \text{ L/sec}$$

$$\text{Infiltration Flow} = 0.28 \text{ L/s/ha} \times 0.42 \text{ ha} = 0.12 \text{ L/s}$$

Therefore,

$$\text{Total Average Sanitary Flow} = 0.71 \text{ L/sec}$$

$$\text{Total Peak Sanitary Flow} = 1.01 \text{ L/sec (with PF)}$$

Development sanitary flows under proposed zoning are greater than the flows under existing conditions; but as mentioned previously, the existing zoning permits greater development. Also, the existing receiving sewers are a 1200 mm dia. sanitary sewer at  $\pm 2.0\%$  slope on York Street with a capacity of approximately 5,750 L/s and a 1500 mm dia. sanitary sewer at  $\pm 1.5\%$  slope on George Street with a capacity of approximately 11,650 L/s. Consequently, this would have negligible impact on the existing City sanitary sewer system.

### **3.0 STORMWATER**

Stormwater flows from the site are currently conveyed to the existing storm sewer system via on-site catchbasins and overland flows to York Street, Dalhousie Street as well as George Street. The stormwater from the existing building at 325 Dalhousie Street as well as 110 York Street is captured by roof drains and outlet through their respective existing service connection. As for stormwater from the existing building at 141 George Street, approximately half is captured by roof



drains whereas the balance of the building has a pitched roof. As part of this development, all stormwater will be controlled on site prior to being discharged to the storm system.

The proposed hotel development will be serviced by a new 150 mm dia. storm service that will connect to the existing 675 mm dia. storm sewer on York Street; therefore the existing 150 mm dia. storm service that is currently connected to the existing 675 mm dia. storm sewer on York Street will need to be abandoned. The new storm service connection to the building will be equipped with a backwater valve. Also, a portion of the roof will be directed to sanitary due to the rooftop pool (refer to sanitary section for further details). It is to be noted that the attached neighboring 2 ½ storey property has its own existing storm service (approx. 150 mm dia.) that also connects to the existing 675 mm dia. storm sewer on York Street (was previously interconnected, but is currently separated).

Furthermore, the proposed condominium development will be serviced by a 250 mm dia. storm service that will connect to the existing 900 mm dia. storm sewer on George Street. The proposed storm service connection to the building will be equipped with a backwater valve.

The City will require that on-site stormwater management be implemented to control post-development stormwater discharge for both the 5 & 100 year storm events based on an allowable runoff coefficient (C) of 0.50, a time of concentration ( $t_c$ ) of 20 minutes, and a 5-year storm control. Stormwater management will be achieved through the use of rooftop controls and surface ponding (as required). Should surplus storage be required, stormwater management alternatives such as storage tanks or super-pipes will be implemented. Temporary storage will be provided at the surface as required to supply the necessary release rate during all phases until full build out is achieved with underground systems.

The site will be graded such that flows in excess of the 100-year storm event will be conveyed overland to York Street, Dalhousie Street and George Street. Erosion and sediment control measures will be implemented during all phases of construction and inspected regularly.

A detailed stormwater management report addressing these requirements is also submitted under separate cover as part of the site plan application.

## **4.0 WATERMAIN**

### **4.1 Domestic Water Demand**

The proposed hotel development will be serviced by a 150 mm dia. water service that will connect to the existing 200 mm dia. watermain on York Street, therefore the existing 150 mm dia. water service that is currently connected to the existing 200 mm dia. watermain on York Street will need to be abandoned. An existing shut off valve is present within the right of way outside the property line of the site as per old City of Ottawa Specifications for the existing service, but a new shut off valve will be provided at the property line of the site as per City of Ottawa Specifications for the new service. The existing water meter is located in the basement level mechanical room of the building (replace in new location as required, refer to mechanical). Similarly, a remote receptacle will be located at the surface near the entrance to the building on the exterior. It is to be noted that the attached neighboring 2 ½ storey property now has its own 40 mm dia. water service that is also connected to the existing 200 mm dia. watermain on York Street (it was previously interconnected). An existing shut off valve is present within the right of way outside the property line of the site as per old City of Ottawa Specifications.



Furthermore, the proposed condominium development will be serviced by a 200 mm dia. water service that will connect to the existing 300 mm dia. watermain on George Street. A shut off valve will be provided at the property line of the site as per City of Ottawa Specifications. The water meter will be located in the basement level mechanical room of the building. Similarly, a remote receptacle will be located at the surface near the entrance to the building on the exterior.

Estimated domestic water demands for the development are roughly the same as the proposed development sanitary flows listed above in Section 2.0.

#### Hotel

Average daily demand (L/sec):  $Q_{\text{WATER}} = 73,456.0 \text{ L/day} \div 86,400 \text{ sec/day} = 0.85 \text{ L/sec}$

Using a peak factor of 2.5, the required maximum daily demand yields:  $Q_{\text{WATER}} = 2.13 \text{ L/sec}$

Using a peak factor of 2.2, the required maximum hour demand yields:  $Q_{\text{WATER}} = 4.69 \text{ L/sec}$

#### Condominium – Phase 1

Average daily demand (L/sec):  $Q_{\text{WATER}} = 98,979.0 \text{ L/day} \div 86,400 \text{ sec/day} = 1.15 \text{ L/sec}$

Using a peak factor of 2.5, the required maximum daily demand yields:  $Q_{\text{WATER}} = 2.88 \text{ L/sec}$

Using a peak factor of 2.2, the required maximum hour demand yields:  $Q_{\text{WATER}} = 6.34 \text{ L/sec}$

#### Condominium – Phase 2

Average daily demand (L/sec):  $Q_{\text{WATER}} = 84,164.5 \text{ L/day} \div 86,400 \text{ sec/day} = 0.97 \text{ L/sec}$

Using a peak factor of 2.5, the required maximum daily demand yields:  $Q_{\text{WATER}} = 2.43 \text{ L/sec}$

Using a peak factor of 2.2, the required maximum hour demand yields:  $Q_{\text{WATER}} = 5.35 \text{ L/sec}$

Based on the data provided by the City, the existing watermain in the area are adequate to service this development. According to hydrant test results, the watermain in the street can deliver in the range of approximately 1000 igpm ( $\pm 75.8 \text{ L/sec}$ ) at a dynamic pressure greater than 56 psi. A copy of the watermain data is attached in Appendix B.

## **4.2 Fire Demand**

Section 4.2.11 of the City of Ottawa Water Design Guidelines reads:

“When calculating the fire flow requirements and affected pipe sizing, designers shall use the method developed by the Fire Underwriters Survey.”, and

“The requirements for levels of fire protection on private property are covered in Section 7.2.11 of the Ontario Building Code.”

The Fire Underwriters Survey is used to assess the performance of the water distribution system on a “City Block” basis rather than an individual building basis. The Ontario Building Code governs the assessment of fire demand for individual buildings.

Section 7.2.11.1 of the Ontario Building Codes states that the design, construction, installation and testing of fire service mains and water service pipe combined with fire service mains shall be in conformance with NFPA 24.

NFPA 24 is the standard for the “Installation of Private Fire Service Mains and their Appurtenances”. Chapter 13 of NFPA 24 discusses sizing the private service fire mains for fire protection systems which shall be approved by the authority having jurisdiction, considering the following factors:

- Construction and Occupancy of the building



- Fire Flow and Pressure of the Water Required
- Adequacy of the Water Supply

Specific to this project the buildings will be sprinklered per Section 3.2.2.45 of the Ontario Building Code (OBC). Section 3.2.5.7 of the OBC requires that an adequate water supply for fire fighting be provided to each building, and references Appendix A of the OBC. Sentence 3 of Section A 3.2.5.7 of the OBC (Appendix A) states that NFPA 13 be used for determining both sprinkler and hose stream demands for a sprinklered building.

The design of the sprinkler system is completed by a Fire Protection Engineer, or typically computed by the sprinkler contractor and approved by the Fire Protection Engineer. The process involves detailed hydraulic calculations based on building layout, pipe runs, head losses, fire pump requirements, etc. At this stage in the development process, e.g. Site Plan Submission, these details are not available. However, using Chapter 7 of NFPA 13, it is possible to provide a fairly accurate estimate of the fire demand for the building. This estimate is provided below.

#### **NFPA Chapter 7 Calculation**

22 Storey Residential Building - Light Hazard

15 Storey Hotel Building - Light Hazard [incl. restaurant - Ordinary Hazard (Group 1)]

4 Level Underground Parking (under residential building - serve both) - Ordinary Hazard (Group 1)

Section 7.2.3 of NFPA 13, "Water Demand Requirements – Hydraulic Calculation Methods" is used to estimate the hose stream demand and the sprinkler demand. The water demand for sprinklers is estimated using the most remote area in the building. Figure 7.2.3.1.2 – Area/Density Curves is used for the worst case scenario, which in this case is the Ordinary Hazard Classification in the underground parking garage. For this classification, Figure 7.2.3.1.2 provides a density of 0.15 gpm/ft<sup>2</sup> using a coverage of 1500 ft<sup>2</sup>, or 225 gpm (US).

Table 7.2.3.1.1 is used to determine the hose stream demand. For Ordinary Hazard a total combined inside and outside hose stream demand of 250 gpm is required. Typically, 150 gpm would be drawn off the hydrant and 100 gpm off the hose cabinets.

Therefore, total estimated demand would be 225 gpm + 250 gpm = 475 gpm. Adding an allowance for head losses through out the sprinkler system, an estimated fire demand of between 550 – 600 gpm, or say 600 USgpm (2,270 L/min) would be required. According to the fire hydrant data provided by the City, the 200 mm and 300 mm watermain on York Street and George Street respectively can deliver in the range of 1,000 lpm (1,200 USgpm) under normal conditions and 2,100 lpm (2,500 USgpm) at 20 psi residual. The building will also be equipped with a fire pump, if necessary, to provide the minimum residual pressure at the sprinkler heads.

Reference material from NFPA 13 is contained in Appendix B.



## 5.0 CONCLUSIONS

Based on the foregoing, adequate sanitary, storm and water services are available to support this development.

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**APPENDIX A**  
**Excerpts from Ottawa Sewer Design Guidelines**



## SECTION 4

## SANITARY SEWER SYSTEMS

specifically the downtown core. The construction of new combined sewer systems is no longer permitted in the City of Ottawa other than for the replacement of existing combined sewers within the City's defined Combined Sewer Area (see Section 5.1.6).

New storm drainage systems cannot be connected to existing combined sewers except as an interim measure where sewer separation is to be ultimately implemented or where circumstances allow no other alternative.

Section 5 discusses combined sewers in greater detail since their design must consider peak storm flows.

#### 4.2.4 Private Sanitary Servicing

Private servicing consists mainly of private sewage collection and treatment systems on individual lots and do not form part of these guidelines.

### 4.3 GENERAL POPULATION DENSITIES

**Pre-zoned Land** – When lands are zoned for a specific residential use and detailed information is not available, the following population densities shall apply:

**Table 4.1 Population Densities**

Unit Type (Min Lot Area M <sup>2</sup> )	Zoning (And all similar zonings)	Persons per unit <sup>1</sup>	Units per net ha avg. <sup>2</sup>	Persons (per net ha) <sup>3</sup>	Persons (per gross ha) <sup>4</sup>
Res-Single Family (600)	R1A-B*	3.4	16.7	57	34
Res-Single Family (501)	R1C-E*	3.4	20.0	68	41
Res-Single Family (441)	R1F-H*	3.4	22.7	77	47
Res-Single Family (360)	R1I-K*	3.4	27.8	94	57
Res-Single Family (270)	R1L-N*	3.4	37.1	126	76
Res-Single Family (197)	R1P-Q*	3.4	50.8	173	105
Res-Semi-detached (278)	R2A-B*	2.7	36.0	97	59
Res-Semi-detached (232)	R2C*	2.7	43.1	116	71
Res-Semi-detached (180)	R2D-E*, G*	2.7	55.6	150	91
Res-Semi-detached (135)	R2F*	2.7	74.1	200	121
Townhouse (170)	R3F*, R4A-B*	2.7	58.8	159	96
Townhouse (110)	R3M*	2.7	90.9	246	149
Res-Duplex (441)	R2A-C*	2.3	45.4	104	63
Res-Duplex (360)	R2D*, R3F-G*	2.3	55.6	128	77
Res-Duplex (270)	R2E-F*, R3K*	2.3	74.1	170	103
Res-Duplex (197)	R2G*, R4F*	2.3	101.6	234	141
Res-Triplex (557)	R3A-C*	2.3	53.9	124	75



## SECTION 4

## SANITARY SEWER SYSTEMS

Unit Type (Min Lot Area M <sup>2</sup> )	Zoning (And all similar zonings)	Persons per unit <sup>1</sup>	Units per net ha avg. <sup>2</sup>	Persons (per net ha) <sup>3</sup>	Persons (per gross ha) <sup>4</sup>
Res-Triplex (330)	R3D-E*, H-J*, L*, N*, R4C-E*	2.3	90.9	209	127
Apartments:					
Low Density		1.8	100	180	
Medium Density		1.8	300	540	
High Density		1.8	1000	1800	
Very High Density <sup>5</sup>		1.8	1000 +	1800 +	

\*) former City of Ottawa zoning designation.

1) from 1996 census data.

2) new suburban construction, 5-year average (1997-2001), except apartments data which is based on site plans & duplex density which is an assumed average.

3) "net ha" refers to population densities per hectare of purely residential land (i.e. area of the building lots only including private parking and roads but excluding all public road rights-of-way and all other non-residential uses such as parks, stormwater management facilities, commercial developments, schools, community centres, etc.).

4) "gross ha" refers to population densities per hectare of residential and all other non-residential land uses such as streets, schools and parks. Numbers provided apply to large subdivision situations. For smaller residential situations the persons per gross ha will be higher, about 75% of the persons per net ha.

5) apartment densities in the downtown have been as high as 4,000 units/net ha. Proposals with a units/net ha density greater than 1000 will be evaluated on a case-by-case basis.

**Development Proposed Land** – When the number and type of housing units within a proposed development are known, the calculation of population for the proposed development shall be based on the following:

**Table 4.2 Per Unit Populations**

Unit Type	Persons Per Unit
Single Family	3.4
Semi-detached	2.7
Duplex	2.3
Townhouse (row)	2.7
<b>Apartments:</b>	
Bachelor	1.4
1 Bedroom	1.4
2 Bedroom	2.1
3 Bedroom	3.1
Average Apt.	1.8



## SECTION 4

## SANITARY SEWER SYSTEMS

## 4.4.1 Calculation of Peak Design Flows

The formulae and parameters to be applied in the calculation of peak design flows (standard peak flow design parameters) for new or infill developments are illustrated in Figure 4.3 and described as follows:

Figure 4.3 Peak Flow Design Parameters Summary

**AVERAGE WASTEWATER FLOWS:**

<b>Residential Average Flow:</b>	350 L/c/day
<b>Commercial Average Flow:</b>	50,000 L/gross ha/d
<b>Institutional Average Flow:</b>	50,000 L/gross ha/d
<b>Average Light Industrial Flow:</b>	35,000 L/gross ha/d
<b>Average Heavy Industrial Flow:</b>	55,000 L/gross ha/d

**PEAKING FACTORS:**

**Residential Peak factor:** Harmon Equation

$$P.F. = 1 + \left( \frac{14}{4 + \left( \frac{P}{1000} \right)^{\frac{1}{2}}} \right) * K$$

where: P=Population

K=Correction Factor = 1

<b>Commercial Peak factor:</b>	1.5
<b>Institutional Peak factor:</b>	1.5
<b>Industrial Peak Factor:</b>	Per Figure in Appendix 4-B

**PEAK EXTRANEEOUS FLOWS: (design event)**

**Infiltration Allowance:** 0.28 L/s/effective gross ha (for all areas)

**Less than 10 ha**

**Foundation Drain Allowance:** 5.0 L/s/gross ha (if necessary for existing partially separated and combined areas only)

**10 ha – 100 ha**

**Foundation Drain Allowance:** 3.0 L/s/gross ha (if necessary for existing partially separated and combined areas only)

**Greater than 100 ha**

**Foundation Drain Allowance:** 2.0 L/s/gross ha (if necessary for existing partially separated and combined areas only)



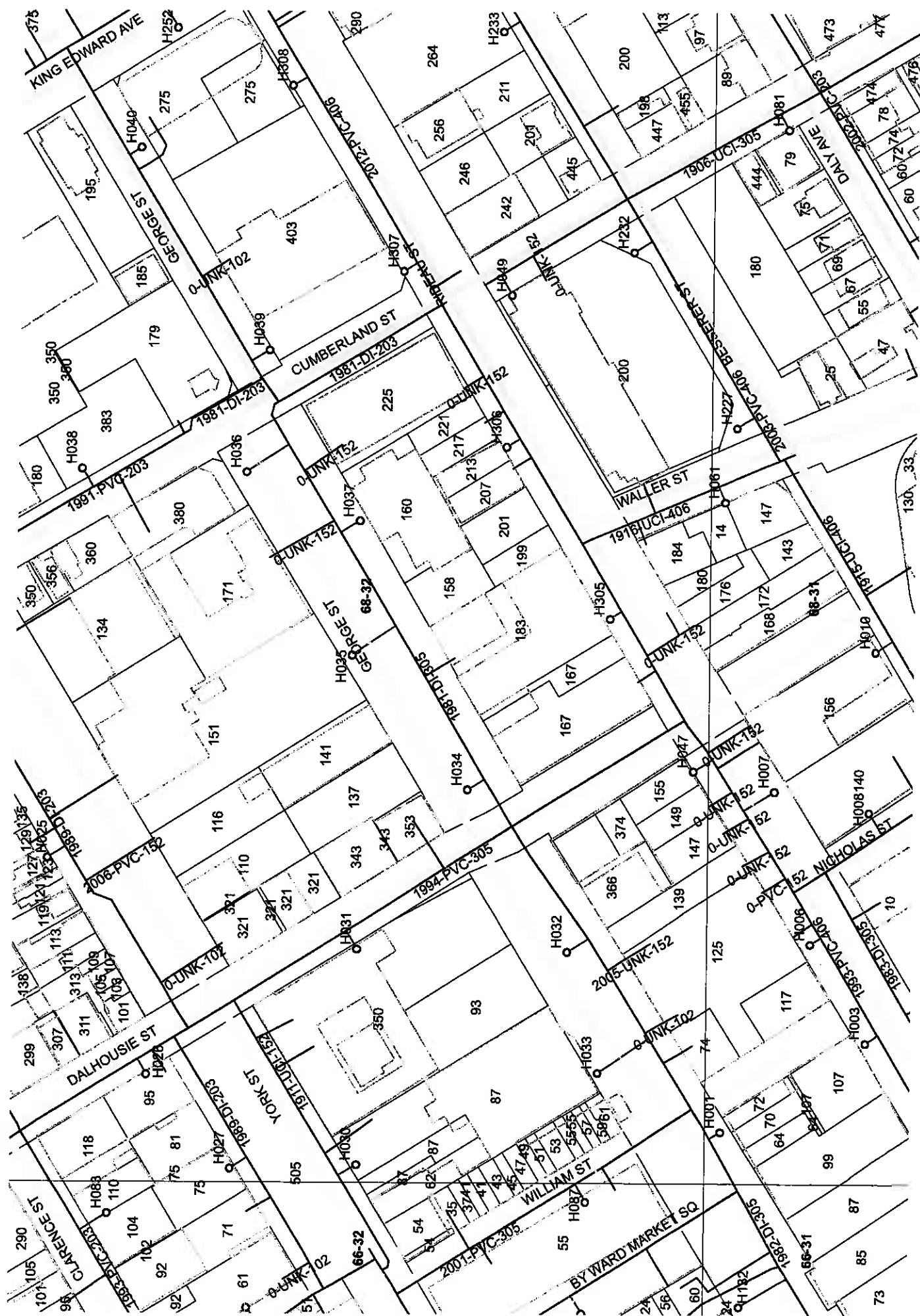
## **APPENDIX B**

### **Hydrant Flow Data/Fire Fighting Information**



## 6350







**6-4.5.9\*** For individual fasteners, the loads determined in 6-4.5.6 shall not exceed the allowable loads provided in Figure 6-4.5.9.

The type of fasteners used to secure the bracing assembly to the structure shall be limited to those shown in Figure 6-4.5.9. For connections to wood, through bolts with washers on each end shall be used. Holes for through bolts shall be  $\frac{1}{16}$  in. (1.6 mm) greater than the diameter of the bolt.

*Exception No. 1: Where it is not practical to install through bolts due to the thickness of the member or inaccessibility, lag screws shall be permitted. Holes shall be pre-drilled  $\frac{1}{8}$  in. (3.2 mm) smaller than the maximum root diameter of the lag screw.*

*Exception No. 2: Other fastening methods are acceptable for use if certified by a registered professional engineer to support the loads determined in accordance with the criteria in 6-4.5.9. Calculations shall be permitted where required by the authority having jurisdiction.*

**6-4.5.10** Sway bracing assemblies shall be listed for a maximum load rating. The loads shall be reduced as shown in Table 6-4.5.10 for loads that are less than 90 degrees from vertical.

*Exception: Where sway bracing utilizing pipe, angles, flats, or rods as shown in Table 6-4.5.8 is used, the components do not require listing. Bracing fittings and connections used with those specific materials shall be listed.*

**Table 6-4.5.10 Allowable Horizontal Load on Brace Assemblies Based on the Weakest Component of the Brace Assembly**

Brace Angle	Allowable Horizontal Load
30-40 degrees from vertical	Listed load rating divided by 2.000
45-59 degrees from vertical	Listed load rating divided by 1.414
60-89 degrees from vertical	Listed load rating divided by 1.155
90 degrees from vertical	Listed load rating

**6-4.5.11** Bracing shall be attached directly to feed and cross mains. Each run of pipe between changes in direction shall be provided with both lateral and longitudinal bracing.

*Exception: Pipe runs less than 12 ft (3.6 m) in length shall be permitted to be supported by the braces on adjacent runs of pipe.*

**6-4.5.12** A length of pipe shall not be braced to sections of the building that will move differentially.

#### **6-4.6 Restraint of Branch Lines.**

**6-4.6.1\*** Restraint is considered a lesser degree of resisting loads than bracing and shall be provided by use of one of the following:

- (1) A listed sway brace assembly
- (2) A wraparound U-hook satisfying the requirements of 6-4.5.3, Exception No. 3
- (3) No. 12, 440-lb (200-kg) wire installed at least 45 degrees from the vertical plane and anchored on both sides of the pipe
- (4) Other approved means

Wire used for restraint shall be located within 2 ft (610 mm) of a hanger. The hanger closest to a wire restraint shall be of a type that resists upward movement of a branch line.

**6-4.6.2** The end sprinkler on a line shall be restrained against excessive vertical and lateral movement.

**6-4.6.3\*** Where upward or lateral movement would result in an impact against the building structure, equipment, or finish materials, branch lines shall be restrained at intervals not exceeding 30 ft (9 m).

**6-4.6.4\*** Sprig-ups 4 ft (1.2 m) or longer shall be restrained against lateral movement.

#### **6-4.7 Hangers and Fasteners Subject to Earthquakes.**

**6-4.7.1** C-type clamps (including beam and large flange clamps) used to attach hangers to the building structure in areas subject to earthquakes shall be equipped with a restraining strap. The restraining strap shall be listed for use with a C-type clamp or shall be a steel strap of not less than 16 gauge thickness and not less than 1 in. (25.4 mm) wide for pipe diameters 8 in. (203 mm) or less and 14 gauge thickness and not less than  $1\frac{1}{4}$  in. (31.7 mm) wide for pipe diameters greater than 8 in. (203 mm). The restraining strap shall wrap around the beam flange not less than 1 in. (25.4 mm). A lock nut on a C-type clamp shall not be used as a method of restraint. A lip on a "C" or "Z" purlin shall not be used as a method of restraint.

Where purlins or beams do not provide an adequate lip to be secured by a restraining strap, the strap shall be through-bolted or secured by a self-tapping screw.

**6-4.7.2** C-type clamps (including beam and large flange clamps), with or without restraining straps, shall not be used to attach braces to the building structure.

**6-4.7.3** Powder-driven fasteners shall not be used to attach braces to the building structure.

*Exception: Powder-driven fasteners shall be permitted where they are specifically listed for service in resisting lateral loads in areas subject to earthquakes.*

**6-4.7.4** Powder-driven fasteners shall not be used to attach hangers to the building structure where the systems are required to be protected against earthquakes using a horizontal force factor exceeding  $0.50 W_p$ , where  $W_p$  is the weight of the water-filled pipe.

*Exception: Powder-driven fasteners shall be permitted where they are specifically listed for horizontal force factors in excess of  $0.50 W_p$ .*

## **Chapter 7 Design Approaches**

### **7-1 General.**

**7-1.1** Water demand requirements shall be determined from the occupancy hazard fire control approach of Section 7-2.

*Exception: Special design approaches as permitted in Section 7-9.*

**7-1.2** For buildings with two or more adjacent occupancies that are not physically separated by a barrier or partition capable of delaying heat from a fire in one area from fusing sprinklers in the adjacent area, the required sprinkler protection for the more demanding occupancy shall extend 15 ft (4.6 m) beyond its perimeter.



## 7-2 Occupancy Hazard Fire Control Approach.

### 7-2.1 Occupancy Classifications.

**7-2.1.1** Occupancy classifications for this standard relate to sprinkler installations and their water supplies only. They shall not be used as a general classification of occupancy hazards.

**7-2.1.2** Occupancies or portions of occupancies shall be classified according to the quantity and combustibility of contents, the expected rates of heat release, the total potential for energy release, the heights of stockpiles, and the presence of flammable and combustible liquids, using the definitions contained in Section 1-4. Classifications are as follows:

Light hazard

Ordinary hazard (Groups 1 and 2)

Extra hazard (Groups 1 and 2)

Special occupancy hazard (*see Section 7-10*)

### 7-2.2 Water Demand Requirements — Pipe Schedule Method.

**7-2.2.1** Table 7-2.2.1 shall be used in determining the minimum water supply requirements for light and ordinary hazard occupancies protected by systems with pipe sized according to the pipe schedules of Section 8-5. Pressure and flow requirements for extra hazard occupancies shall be based on the hydraulic calculation methods of 7-2.3. The pipe schedule method shall be permitted only for new installations of 5000 ft<sup>2</sup> (465 m<sup>2</sup>) or less or for additions or modifications to existing pipe schedule systems sized according to the pipe schedules of Section 8-5. Table 7-2.2.1 shall be used in determining the minimum water supply requirements.

*Exception No. 1: The pipe schedule method shall be permitted for use in systems exceeding 5000 ft<sup>2</sup> (465 m<sup>2</sup>) where the flows required in Table 7-2.2.1 are available at a minimum residual pressure of 50 psi (3.4 bar) at the highest elevation of sprinkler.*

*Exception No. 2: The pipe schedule method shall be permitted for additions or modifications to existing extra hazard pipe schedule systems.*

**7-2.2.2** The lower duration value of Table 7-2.2.1 shall be acceptable only where remote station or central station water-flow alarm service is provided.

**7-2.2.3\*** The residual pressure requirement of Table 7-2.2.1 shall be met at the elevation of the highest sprinkler. (*See the Exceptions to 7-2.2.1*).

**7-2.2.4** The lower flow figure of Table 7-2.2.1 shall be permitted only where the building is of noncombustible construction or the potential areas of fire are limited by building size or compartmentation such that no open areas exceed 3000 ft<sup>2</sup> (279 m<sup>2</sup>) for light hazard or 4000 ft<sup>2</sup> (372 m<sup>2</sup>) for ordinary hazard.

**Table 7-2.2.1 Water Supply Requirements for Pipe Schedule Sprinkler Systems**

Occupancy Classification	Minimum Residual Pressure Required (psi)	Acceptable Flow at Base of Riser (Including Hose Stream Allowance) (gpm)	Duration (minutes)
Light hazard	15	500–750	30–60
Ordinary hazard	20	850–1500	60–90

For SI units, 1 gpm = 3.785 L/min; 1 psi = 0.0689 bar.

### 7-2.3 Water Demand Requirements — Hydraulic Calculation Methods.

#### 7-2.3.1 General.

**7-2.3.1.1\*** The minimum water supply requirements for a hydraulically designed occupancy hazard fire control sprinkler system shall be determined by adding the hose stream demand from Table 7-2.3.1.1 to the water supply for sprinklers determined in 7-2.3.1.2. This supply shall be available for the minimum duration specified in Table 7-2.3.1.1.

*Exception No. 1: An allowance for inside and outside hose shall not be required where tanks supply sprinklers only.*

*Exception No. 2: Where pumps taking suction from a private fire service main supply sprinklers only, the pump need not be sized to accommodate inside and outside hose. Such hose allowance shall be considered in evaluating the available water supplies.*

**7-2.3.1.2** The water supply for sprinklers only shall be determined either from the area/density curves of Figure 7-2.3.1.2 in accordance with the method of 7-2.3.2 or be based upon the room design method in accordance with 7-2.3.3, at the discretion of the designer. For special areas under consideration, as described in 7-2.3.4, separate hydraulic calculations shall be required in addition to those required by 7-2.3.2 or 7-2.3.3.



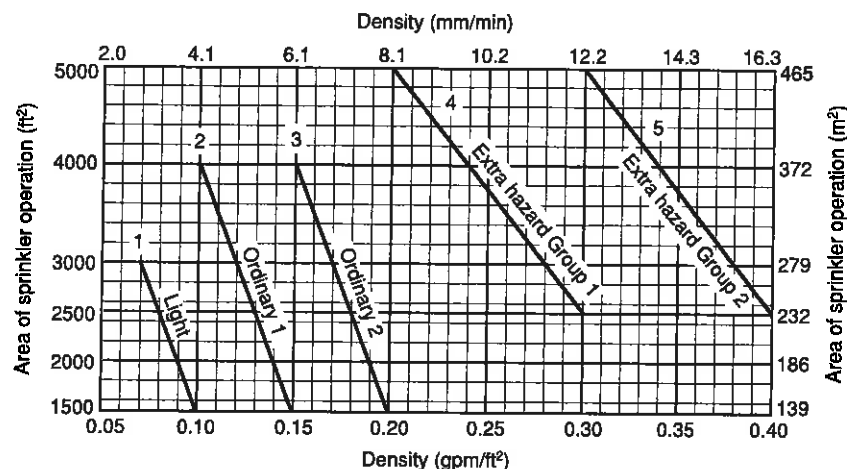
**Table 7-2.3.1.1† Hose Stream Demand and Water Supply Duration Requirements for Hydraulically Calculated Systems**

Occupancy or Commodity Classification	Inside Hose (gpm)	Total Combined Inside and Outside Hose (gpm)	Duration (minutes)
Light hazard	0, 50, or 100	100	30
Ordinary hazard	0, 50, or 100	250	60-90
Extra hazard	0, 50, or 100	500	90-120
Rack storage, Class I, II, and III commodities up to 12 ft (3.7 m) in height	0, 50, or 100	250	90
Rack storage, Class IV commodities up to 10 ft (3.1 m) in height	0, 50, or 100	250	90
Rack storage, Class IV commodities up to 12 ft (3.7 m) in height	0, 50, or 100	500	90
Rack storage, Class I, II, and III commodities over 12 ft (3.7 m) in height	0, 50, or 100	500	90
Rack storage, Class IV commodities over 12 ft (3.7 m) in height and plastic commodities	0, 50, or 100	500	120
General storage, Class I, II, and III commodities over 12 ft (3.7 m) up to 20 ft (6.1 m)	0, 50, or 100	500	90
General storage, Class IV commodities over 12 ft (3.7 m) up to 20 ft (6.1 m)	0, 50, or 100	500	120
General storage, Class I, II, and III commodities over 20 ft (6.1 m) up to 30 ft (9.1 m)	0, 50, or 100	500	120
General storage, Class IV commodities over 20 ft (6.1 m) up to 30 ft (9.1 m)	0, 50, or 100	500	150
General storage, Group A plastics ≤ 5 ft (1.5 m)	0, 50, or 100	250	90
General storage, Group A plastics over 5 ft (1.5 m) up to 20 ft (6.1 m)	0, 50, or 100	500	120
General storage, Group A plastics over 20 ft (6.1 m) up to 25 ft (7.6 m)	0, 50, or 100	500	150

For SI units, 1 gpm = 3.785 L/min.



Figure 7-2.3.1.2 Area/density curves.



**7-2.3.1.3** Regardless of which of the two methods is used, the following restrictions shall apply:

(a) For areas of sprinkler operation less than 1500 ft<sup>2</sup> (139 m<sup>2</sup>) used for light and ordinary hazard occupancies, the density for 1500 ft<sup>2</sup> (139 m<sup>2</sup>) shall be used. For areas of sprinkler operation less than 2500 ft<sup>2</sup> (232 m<sup>2</sup>) for extra hazard occupancies, the density for 2500 ft<sup>2</sup> (232 m<sup>2</sup>) shall be used.

(b) \*For buildings having unsprinklered combustible concealed spaces (as described in 5-13.1.1 and 5-13.7), the minimum area of sprinkler operation shall be 3000 ft<sup>2</sup> (279 m<sup>2</sup>).

*Exception No. 1: Combustible concealed spaces filled entirely with noncombustible insulation.*

*Exception No. 2: \*Light or ordinary hazard occupancies where noncombustible or limited combustible ceilings are directly attached to the bottom of solid wood joists so as to create enclosed joist spaces 160 ft<sup>3</sup> (4.8 m<sup>3</sup>) or less in volume.*

*Exception No. 3: \*Concealed spaces where the exposed surfaces have a flame spread rating of 25 or less and the materials have been demonstrated to not propagate fire in the form in which they are installed in the space.*

(c) Water demand of sprinklers installed in racks or water curtains shall be added to the ceiling sprinkler water demand at the point of connection. Demands shall be balanced to the higher pressure. (See Chapter 8.)

(d) Water demand of sprinklers installed in concealed spaces or under obstructions such as ducts and cutting tables need not be added to ceiling demand.

(e) Where inside hose stations are planned or are required, a total water allowance of 50 gpm (189 L/min) for a single hose station installation or 100 gpm (378 L/min) for a multiple hose station installation shall be added to the sprinkler requirements. The water allowance shall be added in 50-gpm (189-L/min) increments beginning at the most remote hose station, with each increment added at the pressure required by the sprinkler system design at that point.

(f) When hose valves for fire department use are attached to wet pipe sprinkler system risers in accordance with 5-15.5.2, the water supply shall not be required to be added to standpipe demand as determined from NFPA 14, *Standard for the Installation of Standpipe and Hose Systems*.

*Exception No. 1: Where the combined sprinkler system demand and hose stream allowance of Table 7-2.3.1.1 exceeds the requirements of NFPA 14, Standard for the Installation of Standpipe and Hose Systems, this higher demand shall be used.*

*Exception No. 2: For partially sprinklered buildings, the sprinkler demand, not including hose stream allowance, as indicated in Table 7-2.3.1.1 shall be added to the requirements given in NFPA 14, Standard for the Installation of Standpipe and Hose Systems.*

(g) Water allowance for outside hose shall be added to the sprinkler and inside hose requirement at the connection to the city water main or a yard hydrant, whichever is closer to the system riser.

(h) The lower duration values in Table 7-2.3.1.1 shall be permitted where remote station or central station waterflow alarm service is provided.

(i) Where pumps, gravity tanks, or pressure tanks supply sprinklers only, requirements for inside and outside hose need not be considered in determining the size of such pumps or tanks.

**7-2.3.1.4** Total system water supply requirements shall be determined in accordance with the hydraulic calculation procedures of Section 8-4.

### 7-2.3.2 Area/Density Method.

**7-2.3.2.1** The water supply requirement for sprinklers only shall be calculated from the area/density curves in Figure 7-2.3.1.2 or from Section 7-10 where area/density criteria is specified for special occupancy hazards. When using Figure 7-2.3.1.2, the calculations shall satisfy any single point on the appropriate area/density curve as follows:

- (1) Light hazard area/density curve 1
- (2) Ordinary hazard (Group 1) area/density curve 2
- (3) Ordinary hazard (Group 2) area/density curve 3
- (4) Extra hazard (Group 1) area/density curve 4
- (5) Extra hazard (Group 2) area/density curve 5

It shall not be necessary to meet all points on the selected curve.

*Exception: Sprinkler demand for storage occupancies as determined in Sections 7-3 through 7-8.*

**7-2.3.2.2** For protection of miscellaneous storage, miscellaneous tire storage, and storage up to 12 ft (3.7 m) in height, the discharge criteria in Table 7-2.3.2.2 shall apply.



Table A-1-4.11 Typical Cotton Bale Types and Approximate Sizes

Bale Type	Dimensions		Average Weight		Volume		Density	
	in.	mm	lb	kg	ft <sup>3</sup>	m <sup>3</sup>	lb/ft <sup>3</sup>	kg/m <sup>3</sup>
Gin, flat	55 × 45 × 28	1397 × 1143 × 711	500	226.8	40.1	1.13	12.5	201
Modified gin, flat	55 × 45 × 24	1397 × 1143 × 610	500	226.8	34.4	0.97	14.5	234
Compressed, standard	57 × 29 × 23	1448 × 736 × 584	500	226.8	22.0	0.62	22.7	366
Gin, standard	55 × 31 × 21	1397 × 787 × 533	500	226.9	20.7	0.58	24.2	391
Compressed, universal	58 × 25 × 21	1475 × 635 × 533	500	226.8	17.6	0.50	28.4	454
Gin, universal	55 × 26 × 21	1397 × 660 × 533	500	226.8	17.4	0.49	28.7	463
Compressed, high density	58 × 22 × 21	1473 × 559 × 533	500	226.8	15.5	0.44	32.2	515

#### A-1-4.11 Baled Cotton. See Table A-1-4.11.

**A-1-4.12 Array, Standard (Paper).** The occasional presence of partially used rolls on top of columns of otherwise uniform diameter rolls does not appreciably affect the burning characteristics.

**A-1-4.12 Roll Paper Storage, Wrapped.** Rolls that are completely protected with a heavyweight kraft wrapper on both sides and ends are subject to a reduced degree of fire hazard. Standard methods for wrapping and capping rolls are outlined in Figure A-1-4.12.

In some cases, rolls are protected with laminated wrappers, using two sheets of heavy kraft with a high-temperature wax laminate between the sheets. Where using this method, the overall weight of wax-laminated wrappers should be based on the basis weight per 1000 ft<sup>2</sup> (92.9 m<sup>2</sup>) of the outer sheet only, rather than on the combined basis weight of the outer and inner laminated wrapper sheets. A properly applied wrapper can have the effect of changing the class of a given paper to essentially that of the wrapper material. The effect of applying a wrapper to tissue has not been determined by test.

**A-1-4.12 Roll Paper Storage Height.** The size of rolls and limitations of mechanical handling equipment should be considered in determining maximum storage height.

**A-2-1** Occupancy examples in the listings as shown in the various hazard classifications are intended to represent the norm for those occupancy types. Unusual or abnormal fuel loadings or combustible characteristics and susceptibility for changes in these characteristics, for a particular occupancy, are considerations that should be weighed in the selection and classification.

The light hazard classification is intended to encompass residential occupancies; however, this is not intended to preclude the use of listed residential sprinklers in residential occupancies or residential portions of other occupancies.

**A-2-1.1** Light hazard occupancies include occupancies having uses and conditions similar to the following:

Churches

Clubs

Eaves and overhangs, if of combustible construction with no combustibles beneath

Figure A-1-4.12 Wrapping and capping terms and methods.

#### Wrapper

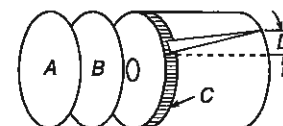
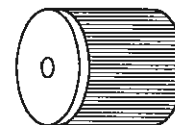
Exterior wrapper  
Body wrapper

General term for protective wrapping of sides and ends on roll.

#### Body wrap

Sleeve wrap  
Wrap — do not cap

Wrapper placed around circumference of roll. No heads or caps needed.



#### Heads

Headers

Protection applied to the ends of the rolls (A and B). Heads do not lap over the end of the roll.

Inside heads

Protection applied to the ends of the rolls next to the roll itself (B). The wrapper of the rolls is crimped down over these heads.

Outside heads

Protection applied to the ends of the rolls on the outside (A). This head is applied after the wrapper is crimped.

#### Edge protectors

Edge bands

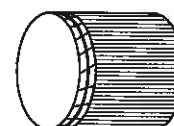
Refers to extra padding to prevent damage to roll edges (C).

Overwrap

The distance the body wrap or wrapper overlaps itself (D).

#### Roll cap

A protective cover placed over the end of a roll. Edges of cap lap over the end of the roll and are secured to the sides of the roll.





Educational  
Hospitals  
Institutional  
Libraries, except large stack rooms  
Museums  
Nursing or convalescent homes  
Offices, including data processing  
Residential  
Restaurant seating areas  
Theaters and auditoriums, excluding stages and prosceniums  
Unused attics

**A-2-1.2.1** Ordinary hazard occupancies (Group 1) include occupancies having uses and conditions similar to the following:

Automobile parking and showrooms  
Bakeries  
Beverage manufacturing  
Canneries  
Dairy products manufacturing and processing  
Electronic plants  
Glass and glass products manufacturing  
Laundries  
Restaurant service areas

**A-2-1.2.2** Ordinary hazard occupancies (Group 2) include occupancies having uses and conditions similar to the following:

Cereal mills  
Chemical plants — ordinary  
Confectionery products  
Distilleries  
Dry cleaners  
Feed mills  
Horse stables  
Leather goods manufacturing  
Libraries — large stack room areas  
Machine shops  
Metal working  
Mercantile  
Paper and pulp mills  
Paper process plants  
Piers and wharves  
Post offices  
Printing and publishing  
Repair garages  
Resin application area  
Stages  
Textile manufacturing  
Tire manufacturing  
Tobacco products manufacturing  
Wood machining  
Wood product assembly

**A-2-1.3.1** Extra hazard occupancies (Group 1) include occupancies having uses and conditions similar to the following:

Aircraft hangars (except as governed by NFPA 409, *Standard on Aircraft Hangars*)  
Combustible hydraulic fluid use areas  
Die casting

Metal extruding  
Plywood and particle board manufacturing  
Printing [using inks having flash points below 100°F (38°C)]  
Rubber reclaiming, compounding, drying, milling, vulcanizing  
Saw mills  
Textile picking, opening, blending, garnetting, or carding, combining of cotton, synthetics, wool shoddy, or burlap  
Upholstering with plastic foams

**A-2-1.3.2** Extra hazard occupancies (Group 2) include occupancies having uses and conditions similar to the following:

Asphalt saturating  
Flammable liquids spraying  
Flow coating  
Manufactured home or modular building assemblies (where finished enclosure is present and has combustible interiors)  
Open oil quenching  
Plastics processing  
Solvent cleaning  
Varnish and paint dipping

**A-2-1.4** Other NFPA standards contain design criteria for fire control or fire suppression (*see 2-1.4 and Chapter 13*). While these can form the basis of design criteria, this standard describes the methods of design, installation, fabrication, calculation, and evaluation of water supplies that should be used for the specific design of the system.

Other NFPA standards contain sprinkler system design criteria for fire control or suppression of specific hazards. This information has been either referenced or copied into Chapters 5 and 7 using NFPA's extract policy.

**A-2-2** Specification of the type, amount, and arrangement of combustibles for any commodity classification is essentially an attempt to define the potential fire severity, based on its burning characteristics, so the fire can be successfully controlled by the prescribed sprinkler protection for the commodity class. In actual storage situations, however, many storage arrays do not fit precisely into one of the fundamental classifications; therefore, the user needs to make judgments after comparing each classification to the existing storage conditions. Storage arrays consist of thousands of products, which make it impossible to specify all the acceptable variations for any class. As an alternative, a variety of common products are classified in this appendix based on judgment, loss experience, and fire test results.

Table A-2-2 provides examples of commodities not addressed by the classifications in Section 2-2.

Table A-2-2.3 is an alphabetized list of commodities with corresponding classifications.

Tables A-2-2.3.1 through A-2-2.3.4 and A-2-2.4.1 provide examples of commodities within a specific class.

**Table A-2-2 Examples of Commodities Not Addressed by the Classifications in Section 2-2**

Boxes, Crates
- Empty, wood slatted
Lighters (butane)
- Loose in large containers (Level 3 aerosol)

\*Should be treated as idle pallets.



## **APPENDIX C**

### **Correspondence**



## **APPENDIX D**

### **Servicing Study Guidelines Checklist**



**Development Servicing Study Checklist**

4.1 General Content	Addressed (Y/N/NA)	Section	Comments
Executive Summary (for larger reports only).	NA		
Date and revision number of the report.	Y	Cover	
Location map and plan showing municipal address, boundary, and layout of proposed development.	Y		Figures 1, 2 and 3
Plan showing the site and location of all existing services.	Y		Figures 2 and 3
Development statistics, land use, density, adherence to zoning and official plan, and reference to applicable subwatershed and watershed plans that provide context to which individual developments must adhere.	Y	1.0	
Summary of Pre-consultation Meetings with City and other approval agencies.	N		
Reference and confirm conformance to higher level studies and reports (Master Servicing Studies, Environmental Assessments, Community Design Plans), or in the case where it is not in conformance, the proponent must provide justification and develop a defensible design criteria.	Y	2.0 - 4.0	
Statement of objectives and servicing criteria.	Y		Addressed in Section 2.0, 3.0. 4.0.
Identification of existing and proposed infrastructure available in the immediate area.	Y		Figures 2 and 3
Identification of Environmentally Significant Areas, watercourses and Municipal Drains potentially impacted by the proposed development (Reference can be made to the Natural Heritage Studies, if available).	NA		
Concept level master grading plan to confirm existing and proposed grades in the development. This is required to confirm the feasibility of proposed stormwater management and drainage, soil removal and fill constraints, and potential impacts to neighboring properties. This is also required to confirm that the proposed grading will not impede existing major system flow paths.	N		Will be addressed in Site plan application.



**Development Servicing Study Checklist**

4.1 General Content	Addressed (Y/N/NA)	Section	Comments
Identification of potential impacts of proposed piped services on private services (such as wells and septic fields on adjacent lands) and mitigation required to address potential impacts.	NA		
Proposed phasing of the development, if applicable.	NA		
Reference to geotechnical studies and recommendations concerning servicing.	N		
All preliminary and formal site plan submissions should have the following information:			
Metric scale	Y	ALL	
North arrow (including construction North)	Y	ALL	
Key plan	Y	ALL	
Name and contact information of applicant and property owner	Y	ALL	
Property limits including bearings and	Y	ALL	
Existing and proposed structures and parking	Y	ALL	
Easements, road widening and rights-of-way	Y	ALL	
Adjacent street names	Y	ALL	



**Development Servicing Study Checklist**

4.2 Water	Addressed (Y/N/NA)	Section	Comments
Confirm consistency with Master Servicing Study, if available.	Y	5.0	Also refer to Appendix B for Hydrant Flow data.
Availability of public infrastructure to service proposed development.	Y		Figures 2 and 3
Identification of system constraints.	Y	4.0	
Identify boundary conditions.	Y	4.0	
Confirmation of adequate domestic supply and pressure.	Y	4.0	
Confirmation of adequate fire flow protection and confirmation that fire flow is calculated as per the Fire Underwriter's Survey. Output should show available fire flow at locations throughout the development.	Y	4.0	
Provide a check of high pressures. If pressure is found to be high, an assessment is required to confirm the application of pressure reducing valves.	Y	4.0	
Definition of phasing constraints. Hydraulic modeling is required to confirm servicing for all defined phases of the project including the ultimate design.	NA		
Address reliability requirements such as appropriate location of shut-off valves.	Y	4.0	
Check on the necessity of a pressure zone boundary modification.	NA		
Reference to water supply analysis to show that major infrastructure is capable of delivering sufficient water for the proposed land use. This includes data that shows that the expected demands under average day, peak hour and fire flow conditions provide water within the required pressure range.	Y	4.0	
Description of the proposed water distribution network, including locations of proposed connections to the existing system, provisions for necessary looping, and appurtenances (valves, pressure reducing valves, valve chambers, and fire hydrants) including special metering provisions.	Y	4.0	
Description of off-site required feeder mains, booster pumping stations, and other water infrastructure that will be ultimately required to service proposed development, including financing, interim facilities, and timing of implementation.	NA		
Confirmation that water demands are calculated based on the City of Ottawa Design Guidelines.	Y	4.0	
Provision of a model schematic showing the boundary conditions locations, streets, parcels, and building locations for reference.	N		Figure 3 shows main.



**Development Servicing Study Checklist**

4.3 Wastewater	Addressed (Y/N/NA)	Section	Comments
Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitored flow data from relatively new infrastructure cannot be used to justify capacity requirements for proposed infrastructure).	Y	2.0	
Confirm consistency with Master Servicing Study and/or justifications for deviations.	Y	2.0	
Consideration of local conditions that may contribute to extraneous flows that are higher than the recommended flows in the guidelines. This includes groundwater and soil conditions, and age and condition of sewers.	Y	2.0	
Description of existing sanitary sewer available for discharge of wastewater from proposed development.	Y	2.0	
Verify available capacity in downstream sanitary sewer and/or identification of upgrades necessary to service the proposed development. (Reference can be made to previously completed Master Servicing Study if applicable)	Y	2.0	
Calculations related to dry-weather and wet-weather flow rates from the development in standard MOE sanitary sewer design table (Appendix 'C') format.	Y	2.0	
Description of proposed sewer network including sewers, pumping stations, and forcemains.	Y	2.0	Figures 2 and 3
Discussion of previously identified environmental constraints and impact on servicing (environmental constraints are related to limitations imposed on the development in order to preserve the physical condition of watercourses, vegetation, soil cover, as well as protecting against water quantity and quality).	NA		
Pumping stations: impacts of proposed development on existing pumping stations or requirements for new pumping station to service development.	NA		
Forcemain capacity in terms of operational redundancy, surge pressure and maximum flow velocity.	NA		
Identification and implementation of the emergency overflow from sanitary pumping stations in relation to the hydraulic grade line to protect against basement flooding.	NA		
Special considerations such as contamination, corrosive environment etc.	NA		



**Development Servicing Study Checklist**

4.4 Stormwater	Addressed (Y/N/NA)	Section	Comments
Description of drainage outlets and downstream constraints including legality of outlet (i.e. municipal drain, right-of-way, watercourse, or private property).	Y	3.0	
Analysis of the available capacity in existing public infrastructure.	Y	3.0	
A drawing showing the subject lands, its surroundings, the receiving watercourse, existing drainage patterns and proposed drainage patterns.	Y		Figures 2 and 3
Water quantity control objective (e.g. controlling post-development peak flows to pre-development level for storm events ranging from the 2 or 5 year event (dependent on the receiving sewer design) to 100 year return period); if other objectives are being applied, a rationale must be included with reference to hydrologic analyses of the potentially affected subwatersheds, taking into account long-term cumulative effects.	Y	3.0	
Water Quality control objective (basic, normal or enhanced level of protection based on the sensitivities of the receiving watercourse) and storage requirements.	NA		
Description of stormwater management concept with facility locations and descriptions with references and supporting information.	Y	3.0	
Set-back from private sewage disposal systems.	NA		
Watercourse and hazard lands setbacks.	NA		
Record of pre-consultation with the Ontario Ministry of Environment and the Conservation Authority that has jurisdiction on the affected watershed.	NA		
Confirm consistency with sub-watershed and Master Servicing Study, if applicable study exists.	Y	3.0	
Storage requirements (complete with calcs) and conveyance capacity for 5 yr and 100 yr events.	Y	3.0	
Identification of watercourse within the proposed development and how watercourses will be protected, or, if necessary, altered by the proposed development with applicable approvals.	NA		
Calculate pre and post development peak flow rates including a description of existing site conditions and proposed impervious areas and drainage catchments in comparison to existing conditions.	Y	3.0	
Any proposed diversion of drainage catchment areas from one outlet to another.	NA		
Proposed minor and major systems including locations and sizes of stormwater trunk sewers, and SWM facilities.	Y	3.0	
If quantity control is not proposed, demonstration that downstream system has adequate capacity for the post-development flows up to and including the 100-year return period storm event.	NA		



**Development Servicing Study Checklist**

<b>4.4 Stormwater</b>	<b>Addressed (Y/N/NA)</b>	<b>Section</b>	<b>Comments</b>
Identification of municipal drains and related approval requirements.	NA		
Description of how the conveyance and storage capacity will be achieved for the development.	Y	3.0	
100 year flood levels and major flow routing to protect proposed development from flooding for establishing minimum building elevations (MBE) and overall grading.	Y	3.0	
Inclusion of hydraulic analysis including HGL elevations.	N		
Description of approach to erosion and sediment control during construction for the protection of receiving watercourse or drainage corridors.	Y	3.0	
Identification of floodplains – proponent to obtain relevant floodplain information from the appropriate Conservation Authority. The proponent may be required to delineate floodplain elevations to the satisfaction of the Conservation Authority if such information is not available or if information does not match current conditions.	NA		
Identification of fill constrains related to floodplain and geotechnical investigation.	NA		



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<b>4.5 Approval and Permit Requirements</b>	<b>Addressed (Y/N/NA)</b>	<b>Section</b>	<b>Comments</b>
Conservation Authority as the designated approval agency for modification of floodplain, potential impact on fish habitat, proposed works in or adjacent to a watercourse, cut/fill permits and Approval under Lakes and Rivers Improvement Act. The Conservation Authority is not the approval authority for the Lakes and Rivers Improvement Act. Where there are Conservation Authority regulations in place, approval under the Lakes and Rivers Improvement Act is not required, except in cases of dams as defined in the Act.	NA		
Application for Certificate of Approval (CofA) under the Ontario Water Resources Act.	N		
Changes to Municipal Drains.	N		
Other permits (National Capital Commission, Parks Canada, Public Works and Government Services Canada, Ministry of Transportation etc.)	NA		

<b>4.6 Conclusion</b>	<b>Addressed (Y/N/NA)</b>	<b>Section</b>	<b>Comments</b>
Clearly stated conclusions and recommendations.	Y	5.0	
Comments received from review agencies including the City of Ottawa and information on how the comments were addressed. Final sign-off from the responsible reviewing agency.	NA		
All draft and final reports shall be signed and stamped by a professional Engineer registered in Ontario.	Y	5.0	