HYDROGEOLOGICAL STUDY

Wateridge Village – Phase 4 Ottawa, Ontario



TERRAPEX

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1.0 EXECUTIVE SUMMARY

Terrapex Environmental Ltd. (Terrapex) has been retained by Rohit to carry out a hydrogeological study to address the City of Ottawa request to determine if a full Hydrogeological Impact Assessment (HIA) is necessary.

The Fairhaven Area is located approximately 0.5 kms to the south of the Subject Areas defined as Block 4 (1275 Hemlock Rd), Block 5 (1255 Hemlock Road), and Block 6 (Building B – 125 Oshedina St; Building C – 135 Oshedina St). Hydrogeological investigations carried out by Terrapex observed that groundwater flowed from the subject area toward the Ottawa River, and away from the Fairhaven Area. Topography on the Subject Area was also noted to direct surface water away from the Fairhaven Area, and toward the Ottawa River. Depths of anticipated excavations would not be sufficient to create a dewatering Zone of Influence of significance to the Fairhaven Area. The Fairhaven Area is essentially 'upstream' from groundwater and surface water influence.

As such, based on the topography, direction of groundwater flow, vibration attenuation assessment, and the proposed depths of the planned excavations for the Rohit development, it is the opinion of Terrapex that a full HIA is not required for this project.



2.0 BACKGROUND

Terrapex Environmental Ltd. (Terrapex) has been retained by Rohit to carry out a hydrogeological study to address the City of Ottawa request to determine if a full Hydrogeological Impact Assessment (HIA) is necessary.

This review herein was prepared in accordance with the Ontario Water Resources Act, and Ontario Regulation 387/04. In addition, it is intended to satisfy the August 2018 edition of the hydrological requirements of the City of Ottawa that define hydrogeological aspects, as part of the development application process.

A concurrent geotechnical study for the Site was undertaken by Terrapex, which has been submitted under separate cover.



3.0 SUBJECT AREA AND PHYSICAL CONTEXT

3.1 SUBJECT AREA AND PROPOSED CONDITIONS

The subject area is irregular in shape and is located in north of Hemlock Road at 1076 Hemlock Private, Wateridge Community, Ottawa, Ontario. The subject area studied consists of the areas defined as Block 4 (1275 Hemlock Rd), Block 5 (1255 Hemlock Road), and Block 6 (Building B – 125 Oshedina St; Building C – 135 Oshedina St). The subject area is approximately 5.05 acres in area. A visual representation, including the monitoring well locations, is provided as **Figure 1** and **Figure 2**.

3.2 PHYSIOLOGY AND DRAINAGE

The ground surface elevations at the locations of the boreholes and monitoring wells were established by Terrapex using a Topcon Hiper V Global Navigation Satellite System (GNSS) Receiver. The accuracy of the Topcon unit is in the centimetre scale. The ground surface elevation of the monitoring wells ranged between 82.82 masl (MW6-1) and 88.41 (MW4-1). Topography is generally highest at the south part of the subject area, and lowest at the north part of the subject area.

The nearest surface water body is identified as the Ottawa River, located approximately 0.75 km to the north of the subject area.

3.3 GEOLOGY

Available mapping indicates that the subject area is situated over fine-textured glacio-marine deposits, over shallow bedrock.

Block 5 - 1255 Hemlock Rd

Block 6, Building B - 125 Oshedina St and Building C - 135 Oshedina St.

Block 4 - 1275 Hemlock Rd



4.0 METHODOLOGY

4.1 GROUNDWATER MONITORING WELL CONSTRUCTION

Drilling operations were carried out as part of historical investigations and drilled in 2023. Groundwater monitoring well construction dates are provided in **Table 1**, below.

4.2 ENCOUNTERED SUBSURFACE CONDITIONS

Review of the borehole reports generated from the cumulative drilling events, indicates that the encountered overburden is generally comprised of sandy silt to silty clay materials overlying bedrock. The relevant borehole logs are provided in **Appendix I**.

TABLE 1: GROUNDWATER MONITORING WELL CONSTRUCTION SPECIFICATIONS

		Loc	ximate ation Cone 17)	Approximate Ground Surface Elevation	Top of Pipe	Approximate Screened Interval	Soils Reported at	SPT N- Value at
Well	Construction	Easting	Northing				Screened	Screened
ID	Date	(m)	(m)	(masl)	(masl)	(mbg)	Interval	Interval
MW4-1	Aug 11, 2023	450268	5033514	88.14	89.105	2.7 to 4.7	Bedrock	-
MW5-1	Aug 11, 2023	450192	5033509	87.71	88.624	2.5 to 4.4	Bedrock	-
MW5-2	Aug 11, 2023				88.108		Bedrock	RQD =
						2.7 to 4.6		32% to
		450216	5033464	86.90				79%
MW6-1	Aug 10, 2023				83.802		Bedrock	RQD =
						2.7 to 4.7		15% to
		450070	5033727	82.82				45%
MW6-3	Sept 11, 2023				86.688		Bedrock	RQD =
						2.7 to 4.7		16% to
		450119	5033677	85.7				30%
MW6-6	Oct 11, 2023				86.85		Bedrock	RQD =
						2.7 to 4.7		74% to
		450125	5033580	85.87				84%

masl - indicates Metres Above Sea Level



5.0 CHARACTERIZATION OF GROUNDWATER

5.1 WATER LEVEL MONITORING

Groundwater elevations were measured at five monitoring events carried out in November of 2023 and July of 2024.

TABLE 2: RELEVANT GROUNDWATER MONITORING WELL MEASUREMENTS

	Ground				Grou	ındwater Measuı	rements	
	Surface	Well		2023		20	24	
	Elevation	Stickup	Bottom of Well	Nov 16	July 19	July 22	July 23	July 24
			mbTOP	mbTOP	mbTOP	mbTOP	mbTOP	mbTOP
Well ID	(masl)	(masl)	(masl)	(masl)	(masl)	(masl)	(masl)	(masl)
MW4-1	00 1 /	90.10	5.56	4.99	5.07	5.07	5.05	5.06
101004-1	88.14	89.10	(82.58)	(84.44)	(84.03)	(84.03)	(84.05)	(84.04)
MW5-1	87.71	00.60	5.29	4.98	4.98	5.19	dn	dn
IVIVVO-1	07.71	88.62	(82.42)	(83.64)	(83.64)	(83.43)	dry	dry
MANA/E O	96.00	00.10	5.74	4.59	4.70	4.75	4.76	4.77
MW5-2	86.90	88.10	(81.16)	(83.52)	(83.40)	(83.36)	(83.35)	(83.34)
MW6-1	82.82	83.80	5.54	5.21	4.92	5.08	5.03	5.14
IVIVVO- I	02.02	03.00	(77.28)	(78.56)	(78.88)	(78.72)	(78.77)	(78.66)
MW6-3	85.70	86.68	5.54	4.32	dostroved	dostrovod	dootroved	dostroved
101000-3	65.70	00.00	(80.16)	(82.37)	destroyed	destroyed	destroyed	destroyed
MANGG	05.07	00.05	5.54	4.49	4.46	4.46	4.46	4.49
MW6-6	85.87	86.85	(80.33)	(82.36)	(82.39)	(82.39)	(82.39)	(82.36)

DNE - indicates that the well did not exist at that time

NC - indicates 'not constructed at that time'

Shaded cells indicate groundwater high and groundwater low levels.

As summarized in **Table 2**, groundwater elevations ranged from approximately 78.56 masl to 84.44 masl (roughly equivalent to 3.94 mbg to 4.07 mbg). These values are within the bedrock, but it is worth noting that groundwater may exist periodically, flowing over the bedrock/overburden interface in the direction of bedrock topography (northward).

5.2 GROUNDWATER FLOW DIRECTION

Groundwater flow directions were estimated using manual piezometric head measurements recorded on July 22, 2024, as referenced in **Table 2.** Based on these measurements, the groundwater is interpreted to be generally flowing from the south toward the north.

The horizontal gradient was estimated to be 0.0001 m/m. It is noted that groundwater within bedrock does not strictly follow a horizontal gradient, because groundwater flow is controlled by fracture systems, and not porosity.



5.3 HYDRAULIC CONDUCTIVITY TESTING

Hydraulic conductivity is a parameter for quantifying the ability of a soil unit to transmit water. This parameter is necessary for predicting the rate of seepage into excavations to be intercepted or collected by dewatering efforts during construction.

To estimate the hydraulic conductivity (K) of the soil materials adjacent to the screened intervals at the tested monitoring wells, single well response tests were carried out at locations MW4-1, MW5-2, and MW6-1.

The tests were carried out by rapidly adding a volume of water from a well (Falling Head Test) and monitoring the subsequent water level recovery to the static water level conditions. The Bouwer and Rice (1976) method was applied to test data, using the unconfined solution. The data was analyzed using the AQTESOLV™ (v. 4.50). A summary of the single well response tests carried out is presented below in **Table 3**, below, and Single Well Response Test Reports are provided in **Appendix II**.

TABLE 3: SUMMARY OF HYDRAULIC CONDUCTIVITY ESTIMATES

Well ID	Screened Interval (mbg)	Soils at Screened Interval	Hydraulic Conductivity (m/s)
MW4-1	2.7 to 4.7	Bedrock	1.9 x 10 ⁻⁶
MW5-2	2.7 to 4.6	Bedrock RQD = 32% to 79%	1.06 x 10 ⁻⁶
MW6-1	2.7 to 4.7	Bedrock RQD = 15% to 45%	4.02 x 10 ⁻⁷

Based on the tests carried out at the three locations , *in-situ* hydraulic conductivities ranged from 1.02×10^{-7} m/s to 1.9×10^{-6} m/s. For the purposes of flow rate estimates, the "fastest" hydraulic conductivity is of 1.9×10^{-6} m/s was used.

5.4 HYDRAULIC ZONE OF INFLUENCE

Based on the hydraulic conductivity, flow direction and hydraulic gradient provided above, groundwater was interpreted to be flowing toward the northwest at a rate of approximately $2.91 \text{ m}^3/\text{s}$, with a linear velocity of $2.85 \times 10^{-4} \text{ m/year}$.



6.0 VIBRATION ATTENUATION ASSESSMENT

In response to comments provided to Terrapex by the City of Ottawa (dated December 20. 2024), an assessment of the Peak Particle Velocity (PPV) for a distance of 500 metres from the subject property was requested of M-ROC to address the 'Zone of Influence' for anticipated blasting operations to be carried out as part of construction operations. M-ROC is a specialist drilling and blasting contractor, located in Ottawa and Internationally. The assessment was provided to Terrapex by M-ROC, and is included in **Appendix III** of this report.

Theoretical PPV (mm/s) were predicted at distances of 100 m, 200 m, 400 m, and 500 m from the epicentre of the project. PPV levels at 500 metres distance were estimated to be 0.03 mm/s to 0.06 mm/s. For the purposes of context, it is understood that the typical Peak Particle Velocity for background vehicles vibration (passive over calming road humps) are in the range of 0.1 mm/s to 2 mm/s (source: https://www.campbell-associates.co.uk/post/peak-particle-velocity-why-dower-monitor-it). Based on the report provided by M-ROC, the PPV anticipated from the proposed blasting operations would be analogous to background vehicle vibration approximately 400 metres from the site epicentre.



7.0 SUMMARY OF KEY FINDINGS

The following points summarize the key findings of this hydrogeological peer review:

• **Groundwater elevations** ranged from approximately 78.56 masl to 84.44 masl (roughly equivalent to 3.94 mbg to 4.07 mbg). These values are within the bedrock, but it is worth noting that groundwater may exist periodically, flowing over the bedrock/overburden interface in the direction of bedrock topography (northward).

- **Groundwater flow direction** is interpreted to be generally flowing from the southeast toward the northwest with a horizontal gradient of approximately 0.0001 m/m. It is noted that groundwater within bedrock does not strictly follow a gradient, because groundwater flow is controlled by fracture systems, and not porosity.
- Based on the tested locations, *in-situ* hydraulic conductivities ranged from 1.02 x 10⁻⁷ m/s to 1.9 x 10⁻⁶ m/s. For the purposes of flow rate estimates, the "fastest" hydraulic conductivity is of 1.9 x 10⁻⁶ m/s was used.

Hydraulic zone of influence was assessed using the groundwater elevations, groundwater flow direction, and hydraulic conductivities.

Based on the information, groundwater is interpreted to be flowing generally northward at a rate of approximately 2.91 m³/s, with a linear velocity of 2.85 x 10⁻⁴ m/year.

 A Vibration Attenuation Assessment was carried out by M-ROC consultants. Based on the report provided by M-ROC, the PPV anticipated from the proposed blasting operations would be analogous to background vehicle vibration approximately 400 metres from the site epicentre.

It is understood that the Fairhaven Area is located approximately 0.5 kms to the south of the subject area. As such, based on the topography, direction of groundwater flow assessed above, the Vibration Attenuation Assessment, and the proposed depths of the planned excavations for the Rohit development, the proposed development is not anticipated to impact the general groundwater conditions or quality at Fairhaven Area. Therefore, it is the opinion of Terrapex that a full HIA is not required for this project.



8.0 CLOSURE

This report has been completed in accordance with the terms of reference for this project as agreed upon by Rohit Communities (the Client) and Terrapex Environmental Ltd. (Terrapex) and generally accepted hydrogeological consulting practices in this area.

The reported information is believed to provide a reasonable representation of the general hydrogeological conditions at the site; however, studies of this nature have inherent limitations. The data were collected at specific locations and conditions may vary at other locations, or with the passage of time. Where applicable, the assessment of the environmental quality of groundwater was limited to a study of those chemical parameters specifically addressed in this report.

Terrapex has relied in good faith on information and representations obtained from the Client and third parties and, except where specifically identified, has made no attempt to verify such information. Terrapex accepts no responsibility for any deficiency or inaccuracy in this report as a result of any misstatement, omission, misrepresentation, or fraudulent act of those providing information. Terrapex shall not be responsible for conditions or consequences arising from relevant facts that were concealed, withheld, or not fully disclosed at the time of the study.

This report has been prepared for the sole use of Rohit Communities. Terrapex accepts no liability for claims arising from the use of this report, or from actions taken or decisions made as a result of this report, by parties other than Rohit Communities.

Respectfully submitted.

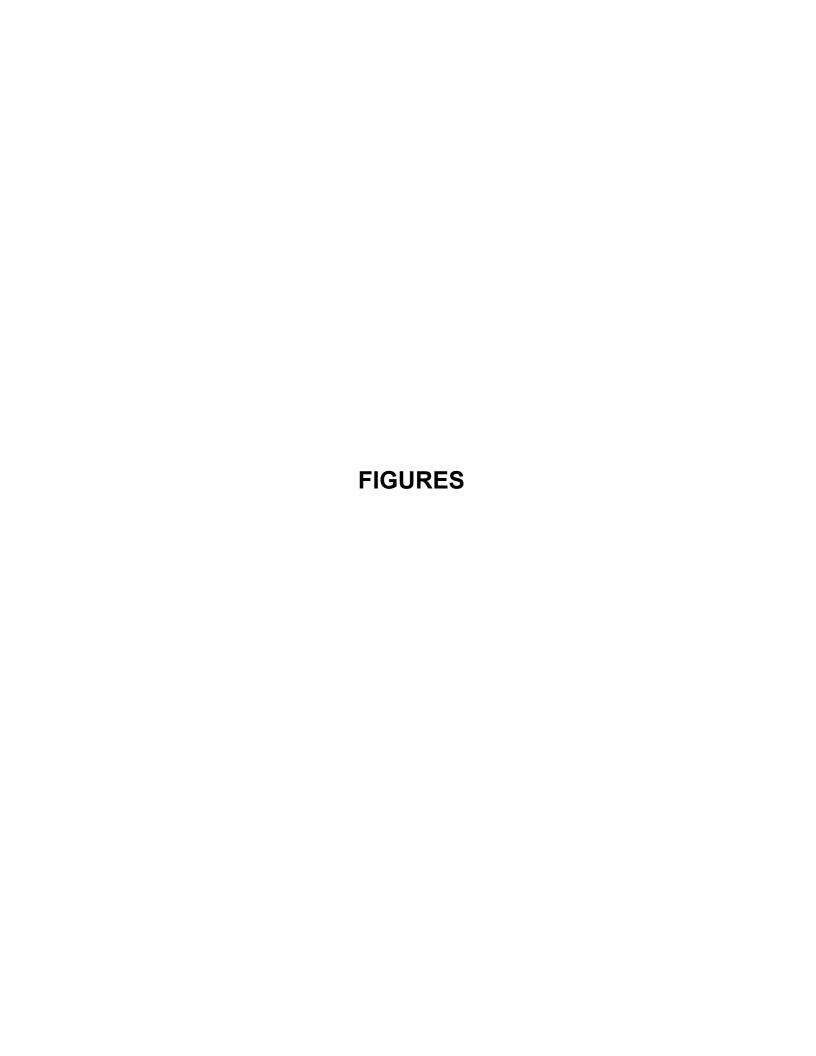
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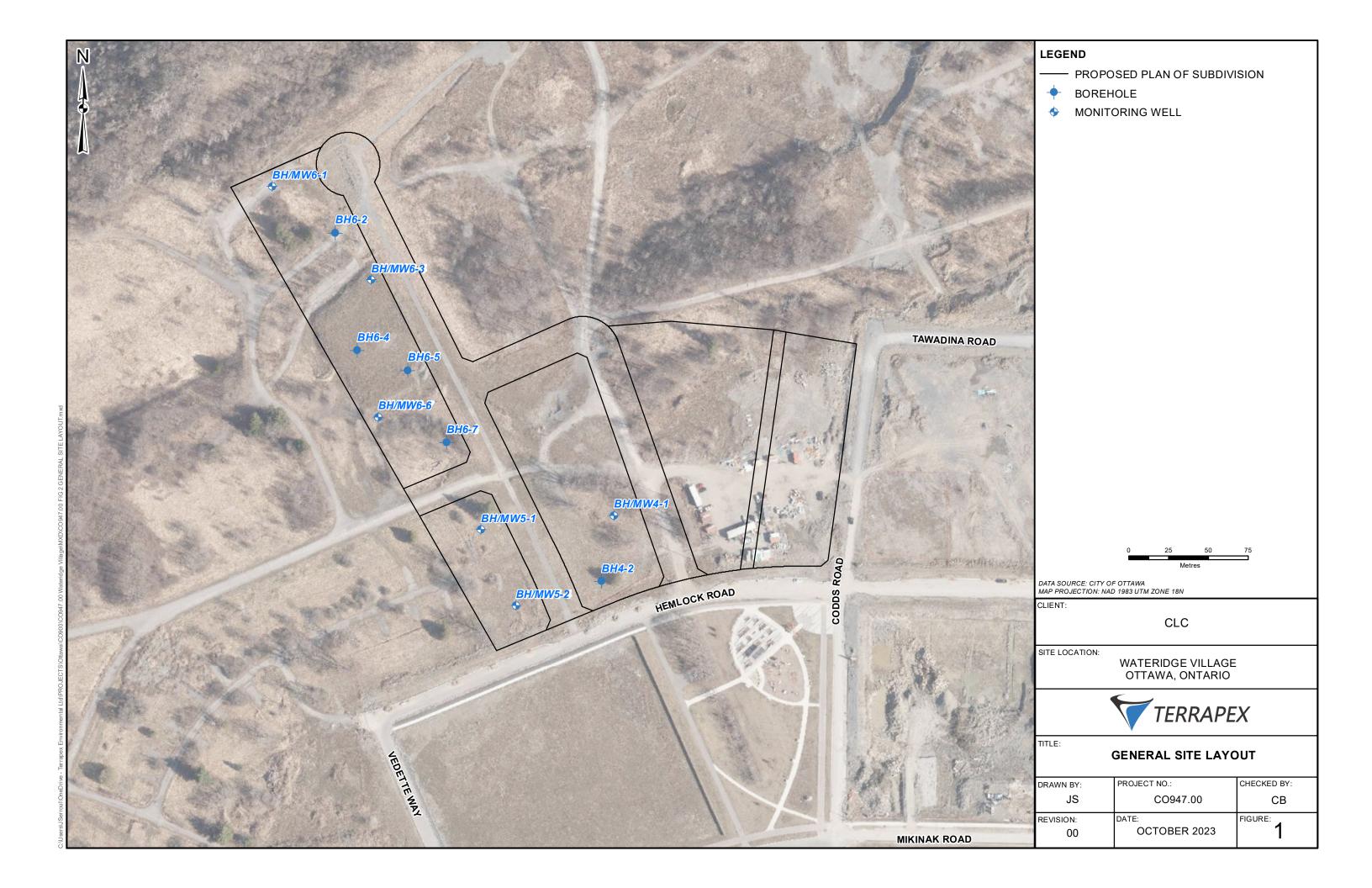
Andrew Durbano, M.Sc., P.Geo.

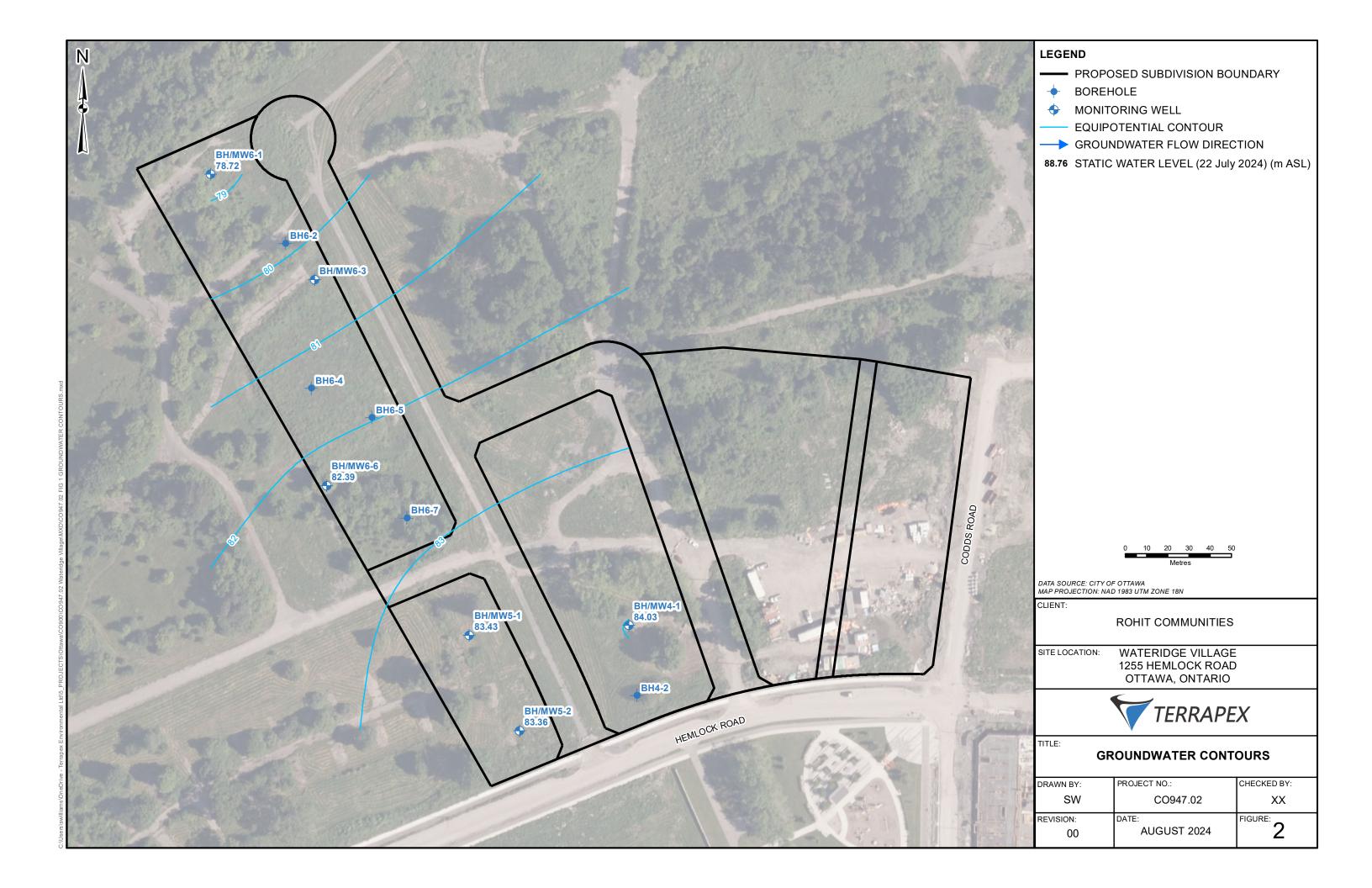
Hydrogeologist

Zen Keizars, P.Geo., FGC. Senior Hydrogeologist









APPENDIX I Borehole Log Reports

CLIEN	NT: Rohit Communities				PRO	DJECT NO.:	CO947	.00		R	ECO	RD OF:
ADDR	RESS: Wateridge Village / Hemlo	ock Road Area	1		STA	ATION:				В	H/N	/IW4-1
	PROVINCE: Ottawa, ON			NORTHING ((m): 50	033514.04	EAS	ΓING (m):	45026	7.99	ELEV	. (m) 88.15
	RACTOR: George Downing Est				THOD:		_					
	EHOLE DIAMETER (cm): 20	WELL DIAME	7			SLOT #: 10		D TYPE:				:: Bentonite
	PLE TYPE AUGER	DRIVEN	_	RING SHEAR STRE	NGTH	YNAMIC CO WATER	₹	SHEL			IT SPC	OON GRAB
GWL (m) SOIL SYMBOL	SOIL DESCRIPTIOI	У	ELEVATION (m)	(kPa) 40 80 120 N-VALU (Blows/300	0 160 E mm)	CONTEN (%) PL W.C.	LL	SAMPLE NO. SAMPLE TYPE RECOVERY (%)	CSV/TOV (ppm or %LEL)	LABORATORY TESTING	WELL INSTALLATION	REMARKS
	FILL hard, brown, moist sandy silty clay trace organics Bedrock Cored to depth of 4.63 n	0.5	88 - 87.5 - 87 - 86.5 - 85.5 - 85.5 - 84.5 - 84 - 84 -	20 40 60	75 •	18	F	3		∑#.	№ 2	Bentonite 50 mm monitoring well was installed and the water level measured on November 24, 2023: 4.0 mbgs Sand Screen + Sand
	END OF BOREHOLE	4.5										END OF BOREHOLE: 4.65 mbgs ELEV.(m) = 83.5
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CITY/	PROVINCE: Ottawa, ON			NORTHI	NG (ı	m): 50	03348	31.01		EAST	ING	(m):	45027	71.84	ELEV.	(m)	87.91	
CONT	RACTOR: George Downing Estate Drillin	g Ltd			MET	HOD:												
BORE	HOLE DIAMETER (cm): WELL DI	_	7		SCF	REEN S	SLOT	#:		SANE	_			SEALAN	T TYPE:			
SAMF	LE TYPE AUGER DRIVEN			RING	CTDE		YNAI			L	S	HEL	BY	SPL	IT SPO	ON	GRA	λB
GWL (m) SOIL SYMBOL	SOIL DESCRIPTION	DЕРТН (m)	ELEVATION (m)	SHEAR (40 80 N-1 (Blows	kPa) 0 120 VALUE s/300r	160 E nm)	P	WAT CONT (% L W.0	ENT) C. LL	0 0	SAMPLE NO.	RECOVERY (%)	CSV/TOV (ppm or %LEL)	LABORATORY TESTING	WELL INSTALLATION		REMARK	S
	FILL firm to hard, dark brown, moist sandy silty clay trace gravel, trace organics Gr=8.7%, Sa=33.5%, Si=35.9%, CI=21.9% LL=49.8%, PI=21. Bedrock END OF BOREHOLE	- 0 - - - 0.5 - - - - - 1	87.5 — 87.5 — 87 —	6	57		14.7	6			2	100				1.32	OF BORI	
	END OF BOILEROLE															ELEV	//(m) = 8	5.6
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BORE	HOLE DIAMETER (cm): 20	WELL DI		7): 5 SC	REEN S	SLOT#	: 10	SA	ND 1	YPE:	2	SEALAN	Г ТҮРЕ	: Bentonite
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8				╗	20 40 6			40 60		SA	SA	88	₹#	ĕ≌	Rontonito
	FILL compact to very dense, brown sandy silt some sand, some clay, trace organics Gr=9.0%, Sa=13.0%, Si=66.5%, Ci crushed rock pieces Bedrock Cored to depth of 4.39 m	gravel, =11.5%	- 0.5 1.5 1.5 2.5 3.5	87.5 – 87 – 86.5 – 85.5 – 85.5 – 84.5 –	36 10 57		25.4 4.9			1 2 3 R1 R2	100	0			Bentonite 50 mm monitoring well was installed and the water level measured on November 24, 2023: 4.24 mbgs Sand Screen + Sand
	END OF BOREHOLE			83.5											END OF BOREHOLE: 4.39 mbgs ELEV.(m) = 83.3
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	TRACTOR: George Downing Estate Drilling				THOD:			=						
	EHOLE DIAMETER (cm): 20 WELL D		7			SLOT #: 10		SAND						: Bentonite
SAME	PLE TYPE AUGER DRIVEN		_	RING SHEAR STRE	ENGTH	YNAMIC C	ER			HELE			IT SPC	OON GRAB
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NOS	BEGGIAII TIGIT		ELE	N-VALU (Blows/300 20 40 60	mm)) 80	PL W.0 20 40		SAN	SAN	REC	CSV (ppn	LAB	WEL	
	FILL very dense, brown, moist sandy silt trace clay, trace organics	0 - - - - 0.5	86.5	50/125		17.4		1		100				Bentonite 50 mm monitoring well was installed and the
	Bedrock Cored to depth of 4.57 m.	- - - 1	86 -						V					water level measured on November 24, 2023: 3.52 mbgs
	TCR(1) = 100% RQD(1) = 32%	- - - 1.5	85.5					R1	M					
		-2 -2	85 -											
	TCR(2) = 100% RQD(2) = 79%	- 2.5 2.5	84.5					R2	M				H II	Sand
		-3 -3 -	84 -						$/\!\!/$					Screen + Sand
	TCR(3) = 100%	-3.5 - - - - -4	83 -					R3						
	RQD(3) = 72%	- 4 - - - - 4.5	82.5					K						
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	HOLE DIAMETER (cm): 20 WELL D): 5 SC	REEN S	SLOT #:	10	SAI	ND T	YPE:		SEALAN	T TYPE	: Bentonite
SAMP	LE TYPE AUGER DRIVEN	<u> </u>	7	RING SHEAR STRE		YNAMI	C CON	E	Ц		LBY		IT SPC	OON GRAB
GWL (m) SOIL SYMBOL	SOIL DESCRIPTION	DЕРТН (m)	ELEVATION (m)	(kPa) 40 80 12 N-VALU (Blows/300	0 160 IE	CC PL	ONTENT (%) W.C. L	L	SAMPLE NO.	SAMPLE TYPE	CSV/TOV (ppm or %LEL)	LABORATORY TESTING	WELL INSTALLATION	REMARKS
	FILL stiff, grey, moist sandy silty clay, trace gravel & organics	_ 0 -	82.5 - 82.5 - 81.5 - 81.5 - 80	(Blows/300 20 40 60 12 53	(mm)** () 80		W.C. L		1A 1B 2 3 R1	100 January 100 Ja	0	LABO		Bentonite 50 mm monitoring well was installed and the water level measured on November 24, 2023: 4.30 mbgs Sand Screen + Sand END OF BOREHOLE: 4.67 mbgs ELEV.(m) = 78.1
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CONT	RACTOR: George Downing Estate Drilling	ng Ltd		ı	METH	HOD:											
BORE	HOLE DIAMETER (cm): WELL D	IAMET	ER (cm): {	SCRE	EN S	SLOT	Г#:		SA	AND T	TYPE	Ξ:	5	SEALAN	TYPE	:
SAMF	LE TYPE AUGER DRIVEN		COF	RING			YNA				Ш	SH	IELI	BY	SPL	IT SPO	ON GRAB
GWL (m) SOIL SYMBOL	SOIL DESCRIPTION	DEPTH (m)	ELEVATION (m)	40 80	Pa) P 120 ALUE /300mi	160 m) [▲]		CON		T LL	SAMPLE NO.	SAMPLE TYPE	RECOVERY (%)	CSV/TOV (ppm or %LEL)	LABORATORY TESTING	WELL INSTALLATION	REMARKS
	FILL compact to dense, grey, moist sandy silty clay trace gravel, trace oxidation Bedrock Cored to depth of 1.15 m.	- 0.5 1	84 -	30	60		■ 8.0		60	80	1A 1B 2	ш	50		71		END OF BOREHOLE:
	END OF BOREHOLE																END OF BOREHOLE: 1.15 mbgs ELEV.(m) = 83.0
		•	•			LOG	GED	BY:	UB		,		RIL	LING [DATE: 1	0-11-2	023
	TERRAPEX					INPU	IT BY	′: RI	R			l N	/ON	IITORII	NG DATI	≣:	
	▼					REVI	EWE	D B	Y: T	Υ		P	AG	E 1 OF	1		

CLIEN	IT: Rohit Communities				PRO	JECT NO.:	CO947	7.00				RD OF:
	ESS: Wateridge Village / Hemlock F	Road Area				TION:	1					W6-3
	PROVINCE: Ottawa, ON			NORTHING (33677.45	EAS	TING (m): 45	0119.58	ELEV.	(m) 85.70
	RACTOR: George Downing Estate DEHOLE DIAMETER (cm):	LL DIAMET	ED (cm		THOD: REEN S	LOT#:	SAN	D TYP		SEALAN	T TVDE:	
—		VEN	7	RING		YNAMIC CC	'		L. HELBY		IT SPOC	ON GRAB
GWL (m)	SOIL DESCRIPTION) DEPTH (m)	ELEVATION (m)	SHEAR STRE (kPa) 40 80 12 N-VALU (Blows/300	0 160	WATEI CONTEI (%)	R JT	SAMPLE NO. SAMPLE TYPE	^	(ppm or %LEL) LABORATORY TESTING	WELL	REMARKS
	FILL very stiff, brown, moist silty clay some gravel, some sand Bedrock Cored to depth of 3.50 m. TCR(1) = 100% RQD(1) = 16% TCR(2) = 30% END OF BOREHOLE	-1-0.5 -0.5 -1-1-5 -1.5 -2-1-3 -3.5 -4-4-5	86.5 - 86.5 - 85.5 - 85.5 - 83	20 40 60	0 80	20 40 60 24.8		1 R1 R2	50	NG DATE: (END OF BOREHOLE: 4.64 mbgs ELEV.(m) = 81.0
	TERRAPI	ļ	INPU	T BY: RR		ı		ORING DAT				
					v IL							

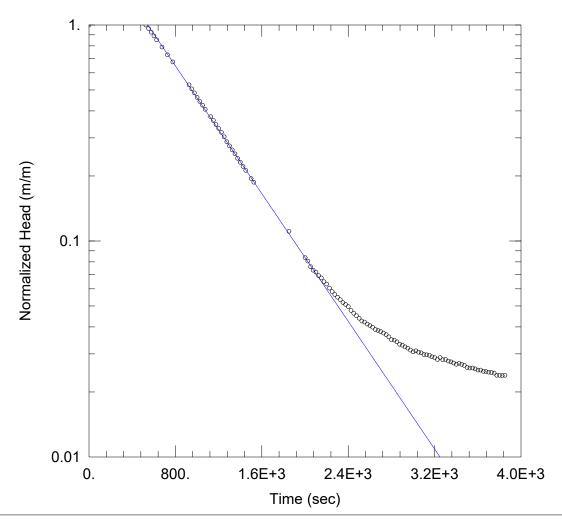
ADDRESS: Wateridge Village / Hemlock Roccity/PROVINCE: Ottawa, ON CONTRACTOR: George Downing Estate Dri BOREHOLE DIAMETER (cm): WELL SAMPLE TYPE AUGER DRIV	Iling Ltd	ER (cm			TATION: 5033626.1	16	EAS	\	10 /					l6-4
CONTRACTOR: George Downing Estate Dri BOREHOLE DIAMETER (cm): WELL	DIAMET	ER (cm			5033626.1	16	EAS	TIN	10 /	١ ٨				
BOREHOLE DIAMETER (cm): WELL	DIAMET	ER (cm		METHO	(m): 5033626.16 EASTING						45011	8.00	ELEV.	(m) 87.36
		_ `									\top	SEALAN1	- TVDE	
SAMPLE TIPE AUGER DRIV			i):	SCREEN	SLOT #: DYNAMIC	CON	SAN	ו טו		E: HELB				
SOIL SOIL DESCRIPTION	DEPTH (m)	ELEVATION (m)	SHEAR (40 80 N-V	STRENGTH kPa 0 120 160 VALUE s/300mm	H WA CON (*	TER ITENT %)	L	SAMPLE NO.		$\widehat{}$	(ppm or %LEL)	LABORATORY TESTING	WELL S INSTALLATION O	REMARKS
FILL soft to firm, grey, moist silty clay trace gravel, trace sand, trace organic Gr=6.0%, Sa=7.8%, Si=25.4%, Cl=60.8%. LL=58.3%, PI=28. END OF BOREHOLE	0	86.5 - 86.5 - 85.5 - 85 -	6	0 60 80	32.1 34.9		80	3 4		33 50 50				END OF BOREHOLE: 2.77 mbgs ELEV.(m) = 84.6
TERRAPE.	INF	GGED BY: PUT BY: RF VIEWED BY	R	· · · · · · · · · · · · · · · · · · ·		DRILLING DATE: 10-11-2023 MONITORING DATE: PAGE 1 OF 1					023			

CONTRACTOR: George Downing Estate Drilling Ltd METHOD.	CLIENT: Rohit Communities	PROJ	ECT NO.: (CO947	.00		RECORD OF:						
CONTRACTOR: George Downing Estate Drilling Ltd METHOD SCREEN SLOT #: SAND TYPE: SEALANT TYPE: SANPELT PRE	ADDRESS: Wateridge Village / Hemlo	STATI	ION:			BH6-5							
SORID SAMPLE TYPE			\perp			3612.15	EAS	TING	(m):	45014	6.62	ELEV.	(m) 87.34
SAMPLE TYPE			OT "	0.41	D. T./	DE		NEAL AND	- TVDE				
SOIL DESCRIPTION					·				$\overline{}$				
Second S			┯—	SHEAR STRE (kPa) 40 80 120 N-VALU (Blows/300	160 E mm)	WATER CONTEN (%) PL W.C.	T LL						
LOGGLD BT. OD DIVILLING DATE. 10-11-2023	FILL soft, grey, moist silty clay trace gravel, trace sand, trace o Gr=7.3%, Sa=7.5%, Si=24.6%, Cl=6 stiff Bedrock Core to depth of 2.97 m.	0 0 0.5 0.6% 1 - 1.5 - 2 - 2.5	86.5 - 86 - 85.5 -	2		32.8 34.6 32.9 30.5		2 3	58				ELEV.(m) = 84.5
TERRAPEX INPUT BY: RR MONITORING DATE: REVIEWED BY: TY PAGE 1 OF 1	TERRA	INPUT	BY: RR			MONITORING DATE:							

CLIENT: Rohit Communities						PRO	DJECT N	O.: C0	D947	.00		RECORD OF:					
ADDR	ADDRESS: Wateridge Village / Hemlock Road Area						ATION:					BH/MW6-6					
CITY/	PROVINCE: Ottawa, ON				NORTHING	G (m): 5033580.10 EASTING						G (m): 450125.25 ELEV. (m) 85.87					
CONT	RACTOR: George Downing Esta	ate Drillir	ng Ltd		ME	THOD:											
BOREHOLE DIAMETER (cm): 20 WELL DIAMETER (cm): 5 SCI						REENS	SLOT#:	10	SAN	D T	YPE:	2 8	SEALANT	TYPE	: Bentonite		
SAMPLE TYPE AUGER DRIVEN CORING						DYNAMIC CONE						BY	SPL	IT SPC	OON GRAB		
GWL (m) SOIL SYMBOL	SOIL DESCRIPTIO	V	DEPTH (m)	ELEVATION (m)	SHEAR STR (kPa) 40 80 12 N-VALI (Blows/30)	• 20 160	CON (ATER NTENT (%) V.C. LL		SAMPLE NO.	SAMPLE TYPE RECOVERY (%)	CSV/TOV (ppm or %LEL)	LABORATORY TESTING	WELL INSTALLATION	REMARKS		
S			O		20 40 6			60 8	0	SA	SA	CS (pp	LAE	N Z	Bentonite		
	FILL loose, grey, moist sandy silt some gravel, some clay, trace of some gravel, some clay, trace of some gravel, some clay, trace of gravel, some clay, trace of gravel, some gravel, some clay, trace of gravely some clay, trace of gravel, some clay, some clay, trace of gravely some clay,	CI=12.7%.	-0.5 -1.5 -2 -2.5	85.5 - 84.5 - 84.5 - 83	8		18.1			3 3	58				50 mm monitoring well was installed and the water level measured on November 24, 2023: 3.67 mbgs		
	TCR(2) = 100% RQD(2) = 74% END OF BOREHOLE		- 4 4 	82 - - - - - - 81.5 -						R2					END OF BOREHOLE:		
														0.44.5	4.64 mbgs ELEV.(m) = 81.2		
TERRAPEV							GED BY:			\dashv	DRILLING DATE: 10-11-2023 MONITORING DATE: 24-11-2023						
TERRAPEX							TBY: R			\dashv				: 24-	11-2023		
						KEVI	EWED B	Y: Y			PAGE 1 OF 1						

CLIENT: Rohit Communities						F	PROJECT NO.: CO947.00 RECORD													
ADDRESS: Wateridge Village / Hemlock Road Area							STATION:											BH	16-7	
CITY/	PROVINCE: Ottawa, ON			NOR	THI	NG	(m): 5033564.86 EASTIN						1G (m):	45016	3.18	ELEV.	(m) 86.75		
CONT	RACTOR: George Downing Estate Drilli	ng Ltd				ME	ETHOD:													
BORE	HOLE DIAMETER (cm): WELL D	IAMET	ER (cm):		SC	CREEN SLOT #: SAND 1					ГΥР	E:	5	SEALAN	ГТҮРЕ	:			
SAMF	PLE TYPE AUGER DRIVEN		COF	RING	;			D	YNA					П	S	HEL	BY	∭ SPL	IT SPO	ON GRAB
GWL (m) SOIL SYMBOL	SOIL DESCRIPTION	DЕРТН (m)	ELEVATION (m)	4(E) 0 80 N-\ Blows	kPa) 0 12 /ALU s/300	20 160 JE Omm)) A		CO PL \	MTE NTE (%)	NT LL	n	SAMPLE NO.	SAMPLE TYPE	RECOVERY (%)	CSV/TOV (ppm or %LEL)	LABORATORY TESTING	WELL INSTALLATION	REMARKS
	FILL very dense, brown, moist sand and gravel some silt, trace clay Bedrock Cored to depth of 1.80 m. END OF BOREHOLE	-0.5	86.5 — 86 — 85.5 — 85 —			50	0 800		19.		0 60	0 86	0	2		<u>~</u> 100	O)	2E	\$ 4	END OF BOREHOLE: 1.80 mbgs ELEV.(m) = 84.9
TERRAPEX							ED T BY			3			_			DATE: 0		023		
	*						RE	EVIE	EWE	DE	Y:	ΤY				PAG	E 1 OF	1		

APPENDIX II Hydrological Analyses



WELL TEST ANALYSIS

Data Set: C:\...\MW4 1 CO947.02.aqt

Date: 08/14/24 Time: 14:16:50

PROJECT INFORMATION

Company: Terrapex Environmental Limited

Client: Rohit Communities

Project: CO947.02

Location: Wateridge Village

Test Well: MW4-1

Test Date: July 23, 2024

AQUIFER DATA

Saturated Thickness: 0.996 m Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (MW4-1)

Initial Displacement: 1.252 m

Total Well Penetration Depth: 3.36 m

Casing Radius: 0.026 m

Static Water Column Height: 0.996 m

Screen Length: 0.996 m Well Radius: 0.033 m

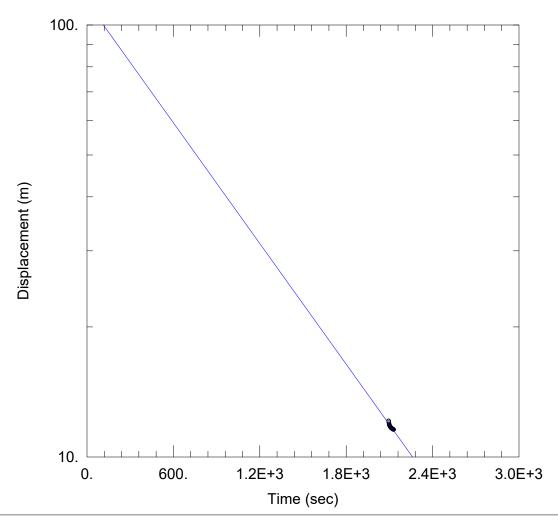
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 1.904E-6 m/sec

y0 = 3.159 m



WELL TEST ANALYSIS

Data Set: C:\...\MW5 2 CO947.02.aqt

Date: 08/14/24 Time: 13:05:18

PROJECT INFORMATION

Company: Terrapex Environmental Limited

Client: Rohit Communities

Project: CO947.02

Location: Wateridge Village

Test Well: MW5-2

Test Date: July 23, 2024

AQUIFER DATA

Saturated Thickness: 1.007 m Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (MW5-2)

Initial Displacement: 0.9199 m

Total Well Penetration Depth: 1.87 m

Casing Radius: 0.026 m

Static Water Column Height: 1.007 m

Screen Length: 1.87 m Well Radius: 0.033 m

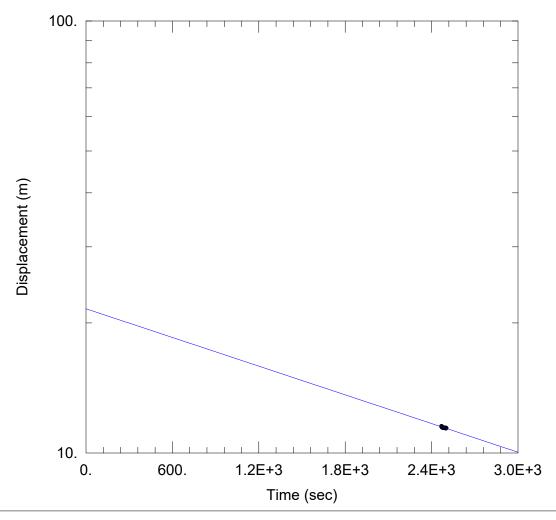
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 1.066E-6 m/sec

y0 = 113. m



WELL TEST ANALYSIS

Data Set: C:\...\MW6 1 CO947.02.aqt

Date: 08/14/24 Time: 14:17:49

PROJECT INFORMATION

Company: Terrapex Environmental Limited

Client: Rohit Communities

Project: CO947.02

Location: Wateridge Village

Test Well: MW6-1

Test Date: July 23, 2024

AQUIFER DATA

Saturated Thickness: 0.595 m Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (MW6-1)

Initial Displacement: 0.1683 m

Static Water Column Height: 0.595 m

Total Well Penetration Depth: 1.9 m Screen Length: 1.9 m Casing Radius: 0.026 m Well Radius: 0.033 m

SOLUTION

Aquifer Model: Unconfined Solution Method: Bouwer-Rice

K = 4.021E-7 m/secy0 = 21.57 m

APPENDIX III Appended Assessments





PPV Assessment R1 Wateridge Block 4, 5, & 6

Submitted by:

M-Roc Ltd 130 Spindrift Circle Ottawa, Ontario K4M 0G4

Phone: 613-791-9222 Jeff.corace@m-roc.ca Contact: Jeff Corace, P.Eng

Submission Date: November 26, 2024





BLAST PLAN 70 Richmond Road – Development Project

Scope of Work:

The following is a brief commentary on the predicted PPV levels expected to be encountered as part of the Wateridge Block 5, 6, & 7 development.

We have looked at the PPV levels predicted at 100m, 200m and 400m from the epicentre of the project, and have used the following expected rock depths.

Block 4 – Max of 2.0m Rock Cut – Max Charge weight of 5kg Block 5 – Max of 2.5m Rock Cut – Max Charge weight of 6.5kg Block 6 – Max of 3.5m Rock Cut – Max Charge weight of 11.5kg

Vibration Limits:

Blasting will be performed in compliance to City of Ottawa SP-F1201 as shown below.

Element	Frequency Hz	Peak Particle Velocity (PPV) mm/s
	≤ 40	20
Structures and Pipelines	> 40	50
Concrete and Grout < 72 hours from placement	N/A	10

Figure 1- F-1201 Vibration Limits

High frequency vibrations (Hz>40) are expected to be the guiding limit on this project due to the close proximity of the sensitive structures. Low total weight of explosives will contain sufficient high frequency energy to break the rock locally but will dissipate very quickly with distance. Typically, low frequency vibration occurs at greater distances and will largely not be the limiting factor for surrounding structures. Blasting will strive to be below both high frequency and low frequency vibration limits.





Vibration Prediction

Peak Particle Velocity (PPV) values may be approximated using the following propagation formula:

$$PPV = k(\frac{R}{\sqrt{W}})^{-e}$$

where:

k = 1730 (upper limit with heavy confinement)

e = -1.85 attenuation rate (typical for City of Ottawa)

W = charge weight/delay of powder (kg)

R = distance to blast (m)

Table 1 – Predicted PPV per Block												
Block	Distance (m)	PPV (mm/s)										
4	100	1.53										
4	200	0.42										
4	400	0.12										
4	500	0.03										
5	100	1.95										
5	200	0.54										
5	400	0.15										
5	500	0.03										
6	100	3.31										
6	200	0.92										
6	400	0.25										
6	500	0.06										

Conclusion:

We trust that the above satisfies the request for information regarding PPV assessment. However, should any additional information be required please do not hesitate to contact the undersigned at your convenience.

Jeff Corace, P.Eng.

M-Roc Ltd

Drilling and Blasting

