HYDROGEOLOGICAL STUDY

Wateridge Village – Phase 4 Ottawa, Ontario

CO947.02

FINAL REPORT

Project Date: September 18, 2024 Revised: February 10, 2025 Revised: March 7, 2025

Prepared for:

ROHIT COMMUNITIES, 15 FITZGERALD RD., SUITE 200 OTTAWA, ONTARIO

TERRAPEX

90 Scarsdale Road Toronto, Ontario, M3B 2R7 Telephone: (416) 245-0011 Service Line Email www.terrapex.com

TABLE OF CONTENTS

1.0	E>	(ECUTIVE SUMMARY	3
2.0	BA	ACKGROUND	4
3.0	รเ	JBJECT AREA AND PHYSICAL CONTEXT	5
	3.1 3.2 3.3	SUBJECT AREA AND PROPOSED CONDITIONS	5 5 5
4.0	M	ETHODOLOGY	6
	4.1 4.2	GROUNDWATER MONITORING WELL CONSTRUCTION	6 6
5.0	Cł	HARACTERIZATION OF GROUNDWATER	7
	5.1 5.2 5.3 5.4	WATER LEVEL MONITORING GROUNDWATER FLOW DIRECTION	7 7 8 8
6.0	VI	BRATION ATTENUATION ASSESSMENT	9
7.0	รเ	JMMARY OF KEY FINDINGS10	0
8.0	CL	_OSURE1 [,]	1



TABLES

Table 1: Groundwater Monitoring Well Construction Specifications	.6
Table 2: Relevant Groundwater Monitoring Well Measurements	.7
Table 3: Summary of Hydraulic Conductivity Estimates	. 8

FIGURES

Figure 1	General Site Layout
Figure 2	Groundwater Contour Map

APPENDICES

Appendix I	Borehole Log Reports
Appendix II	Hydraulic Analyses
Appendix III	Appended Assessments



1.0 EXECUTIVE SUMMARY

Terrapex Environmental Ltd. (Terrapex) has been retained by Rohit to carry out a hydrogeological study to address the City of Ottawa request to determine if a full Hydrogeological Impact Assessment (HIA) is necessary.

The Fairhaven Area is located approximately 0.5 kms to the south of the Subject Areas defined as Block 4 (1275 Hemlock Rd), Block 5 (1255 Hemlock Road), and Block 6 (Building B – 125 Oshedina St; Building C – 135 Oshedina St). Hydrogeological investigations carried out by Terrapex observed that groundwater flowed from the subject area toward the Ottawa River, and away from the Fairhaven Area. Topography on the Subject Area was also noted to direct surface water away from the Fairhaven Area, and toward the Ottawa River. Depths of anticipated excavations would not be sufficient to create a dewatering Zone of Influence of significance to the Fairhaven Area. The Fairhaven Area is essentially 'upstream' from groundwater and surface water influence.

As such, based on the topography, direction of groundwater flow, vibration attenuation assessment, and the proposed depths of the planned excavations for the Rohit development, it is the opinion of Terrapex that a full HIA is not required for this project.



2.0 BACKGROUND

Terrapex Environmental Ltd. (Terrapex) has been retained by Rohit to carry out a hydrogeological study to address the City of Ottawa request to determine if a full Hydrogeological Impact Assessment (HIA) is necessary.

This review herein was prepared in accordance with the Ontario Water Resources Act, and Ontario Regulation 387/04. In addition, it is intended to satisfy the August 2018 edition of the hydrological requirements of the City of Ottawa that define hydrogeological aspects, as part of the development application process.

A concurrent geotechnical study for the Site was undertaken by Terrapex, which has been submitted under separate cover.



3.0 SUBJECT AREA AND PHYSICAL CONTEXT

3.1 SUBJECT AREA AND PROPOSED CONDITIONS

The subject area is irregular in shape and is located in north of Hemlock Road at 1076 Hemlock Private, Wateridge Community, Ottawa, Ontario. The subject area studied consists of the areas defined as Block 4 (1275 Hemlock Rd), Block 5 (1255 Hemlock Road), and Block 6 (Building B – 125 Oshedina St; Building C – 135 Oshedina St). The subject area is approximately 5.05 acres in area. A visual representation, including the monitoring well locations, is provided as **Figure 1** and **Figure 2**.

3.2 PHYSIOLOGY AND DRAINAGE

The ground surface elevations at the locations of the boreholes and monitoring wells were established by Terrapex using a Topcon Hiper V Global Navigation Satellite System (GNSS) Receiver. The accuracy of the Topcon unit is in the centimetre scale. The ground surface elevation of the monitoring wells ranged between 82.82 masl (MW6-1) and 88.41 (MW4-1). Topography is generally highest at the south part of the subject area, and lowest at the north part of the subject area.

The nearest surface water body is identified as the Ottawa River, located approximately 0.75 km to the north of the subject area.

3.3 GEOLOGY

Available mapping indicates that the subject area is situated over fine-textured glacio-marine deposits, over shallow bedrock.

Block 5 - 1255 Hemlock Rd Block 6, Building B - 125 Oshedina St and Building C - 135 Oshedina St. Block 4 - 1275 Hemlock Rd



4.0 METHODOLOGY

4.1 GROUNDWATER MONITORING WELL CONSTRUCTION

Drilling operations were carried out as part of historical investigations and drilled in 2023. Groundwater monitoring well construction dates are provided in **Table 1**, below.

4.2 ENCOUNTERED SUBSURFACE CONDITIONS

Review of the borehole reports generated from the cumulative drilling events, indicates that the encountered overburden is generally comprised of sandy silt to silty clay materials overlying bedrock. The relevant borehole logs are provided in **Appendix I**.

TABLE 1: GROUNDWATER MONITORING WELL CONSTRUCTION SPECIFICATIONS

				Approximate			-	
		Appro	oximate	Ground		Approximate	Soils	
		Loc	ation	Surface	Top of	Screened	Reported	SPT N-
		(UTM Zone 17)		Elevation	Pipe	Interval	at	Value at
Well	Construction	Easting	Northing				Screened	Screened
ID	Date	(m)	(m)	(masl)	(masl)	(mbg)	Interval	Interval
MW4-1	Aug 11, 2023	450268	5033514	88.14	89.105	2.7 to 4.7	Bedrock	-
MW5-1	Aug 11, 2023	450192	5033509	87.71	88.624	2.5 to 4.4	Bedrock	-
MW5-2	Aug 11, 2023				88.108		Bedrock	RQD =
						2.7 to 4.6		32% to
		450216	5033464	86.90				79%
MW6-1	Aug 10, 2023				83.802		Bedrock	RQD =
						2.7 to 4.7		15% to
		450070	5033727	82.82				45%
MW6-3	Sept 11, 2023				86.688		Bedrock	RQD =
						2.7 to 4.7		16% to
		450119	5033677	85.7				30%
MW6-6	Oct 11, 2023				86.85		Bedrock	RQD =
						2.7 to 4.7		74% to
		450125	5033580	85.87				84%

masl – indicates Metres Above Sea Level



5.0 CHARACTERIZATION OF GROUNDWATER

5.1 WATER LEVEL MONITORING

Groundwater elevations were measured at five monitoring events carried out in November of 2023 and July of 2024.

	Ground				Groundwater Measurements									
	Surface	Well		2023		20	2024							
	Elevation	Stickup	Bottom of Well	Nov 16	July 19	July 22	July 23	July 24						
			mbTOP	mbTOP	mbTOP	mbTOP	mbTOP	mbTOP						
Well ID	(masl)	(masl)	(masl)	(masl)	(masl)	(masl)	(masl)	(masl)						
	99 1/	80.10	5.56	4.99	5.07	5.07	5.05	5.06						
101004-1	00.14	09.10	(82.58)	(84.44)	(84.03)	(84.03)	(84.05)	(84.04)						
	97 71	88 62	5.29	4.98	4.98	5.19	dny	dny						
101003-1	07.71	00.02	(82.42)	(83.64)	(83.64)	(83.43)	ury	ury						
	96.00	00 10	5.74	4.59	4.70	4.75	4.76	4.77						
101003-2	80.90	00.10	(81.16)	(83.52)	(83.40)	(83.36)	(83.35)	(83.34)						
	82.82	83.80	5.54	5.21	4.92	5.08	5.03	5.14						
101000-1	02.02	03.00	(77.28)	(78.56)	(78.88)	(78.72)	(78.77)	(78.66)						
	95 70	96 69	5.54	4.32	destroyed	destroyed	destroyed	deatroyed						
10100-3	85.70	00.00	(80.16)	(82.37)	uesiioyeu	uesii0yeu	uesiioyeu	uesiioyeu						
	05 07	00.05	5.54	4.49	4.46	4.46	4.46	4.49						
0-044141	05.67	86.85	(80.33)	(82.36)	(82.39)	(82.39)	(82.39)	(82.36)						

TABLE 2: RELEVANT GROUNDWATER MONITORING WELL MEASUREMENTS

DNE - indicates that the well did not exist at that time

NC – indicates 'not constructed at that time'

Shaded cells indicate groundwater high and groundwater low levels.

As summarized in **Table 2**, groundwater elevations ranged from approximately 78.56 masl to 84.44 masl (roughly equivalent to 3.94 mbg to 4.07 mbg). These values are within the bedrock, but it is worth noting that groundwater may exist periodically, flowing over the bedrock/overburden interface in the direction of bedrock topography (northward).

5.2 **GROUNDWATER FLOW DIRECTION**

Groundwater flow directions were estimated using manual piezometric head measurements recorded on July 22, 2024, as referenced in **Table 2.** Based on these measurements, the groundwater is interpreted to be generally flowing from the south toward the north.

The horizontal gradient was estimated to be 0.0001 m/m. It is noted that groundwater within bedrock does not strictly follow a horizontal gradient, because groundwater flow is controlled by fracture systems, and not porosity.



5.3 HYDRAULIC CONDUCTIVITY TESTING

Hydraulic conductivity is a parameter for quantifying the ability of a soil unit to transmit water. This parameter is necessary for predicting the rate of seepage into excavations to be intercepted or collected by dewatering efforts during construction.

To estimate the hydraulic conductivity (K) of the soil materials adjacent to the screened intervals at the tested monitoring wells, single well response tests were carried out at locations MW4-1, MW5-2, and MW6-1.

The tests were carried out by rapidly adding a volume of water from a well (Falling Head Test) and monitoring the subsequent water level recovery to the static water level conditions. The Bouwer and Rice (1976) method was applied to test data, using the unconfined solution. The data was analyzed using the AQTESOLV[™] (v. 4.50). A summary of the single well response tests carried out is presented below in **Table 3**, below, and Single Well Response Test Reports are provided in **Appendix II**.

Well ID	Screened Interval (mbg)	Soils at Screened Interval	Hydraulic Conductivity (m/s)
MW4-1	2.7 to 4.7	Bedrock	1.9 x 10 ⁻⁶
MW5-2	2.7 to 4.6	Bedrock RQD = 32% to 79%	1.06 x 10 ⁻⁶
MW6-1	2.7 to 4.7	Bedrock RQD = 15% to 45%	4.02 x 10 ⁻⁷

TABLE 3: SUMMARY OF HYDRAULIC CONDUCTIVITY ESTIMATES

Based on the tests carried out at the three locations , *in-situ* hydraulic conductivities ranged from 1.02×10^{-7} m/s to 1.9×10^{-6} m/s. For the purposes of flow rate estimates, the "fastest" hydraulic conductivity is of 1.9×10^{-6} m/s was used.

5.4 HYDRAULIC ZONE OF INFLUENCE

Based on the hydraulic conductivity, flow direction and hydraulic gradient provided above, groundwater was interpreted to be flowing toward the northwest at a rate of approximately 2.91 m^3 /s, with a linear velocity of $2.85 \times 10^{-4} \text{ m/year}$.



6.0 VIBRATION ATTENUATION ASSESSMENT

In response to comments provided to Terrapex by the City of Ottawa (dated December 20. 2024), an assessment of the Peak Particle Velocity (PPV) for a distance of 500 metres from the subject property was requested of M-ROC to address the 'Zone of Influence' for anticipated blasting operations to be carried out as part of construction operations. M-ROC is a specialist drilling and blasting contractor, located in Ottawa and Internationally. The assessment was provided to Terrapex by M-ROC, and is included in **Appendix III** of this report.

Theoretical PPV (mm/s) were predicted at distances of 100 m, 200 m, 400 m, and 500 m from the epicentre of the project. PPV levels at 500 metres distance were estimated to be 0.03 mm/s to 0.06 mm/s. For the purposes of context, it is understood that the typical Peak Particle Velocity for background vehicles vibration (passive over calming road humps) are in the range of 0.1 mm/s to 2 mm/s (source: https://www.campbell-associates.co.uk/post/peak-particle-velocity-why-do-we-monitor-it). Based on the report provided by M-ROC, the PPV anticipated from the proposed blasting operations would be analogous to background vehicle vibration approximately 400 metres from the site epicentre. As such, proposed blasting operations are not anticipated to loosen materials into the existing water supply wells.



7.0 SUMMARY OF KEY FINDINGS

The following points summarize the key findings of this hydrogeological peer review:

- **Groundwater elevations** ranged from approximately 78.56 masl to 84.44 masl (roughly equivalent to 3.94 mbg to 4.07 mbg). These values are within the bedrock, but it is worth noting that groundwater may exist periodically, flowing over the bedrock/overburden interface in the direction of bedrock topography (northward).
- **Groundwater flow direction** is interpreted to be generally flowing from the southeast toward the northwest with a horizontal gradient of approximately 0.0001 m/m. It is noted that groundwater within bedrock does not strictly follow a gradient, because groundwater flow is controlled by fracture systems, and not porosity.
- Based on the tested locations, *in-situ* hydraulic conductivities ranged from 1.02 x 10⁻⁷ m/s to 1.9 x 10⁻⁶ m/s. For the purposes of flow rate estimates, the "fastest" hydraulic conductivity is of 1.9 x 10⁻⁶ m/s was used.

Hydraulic zone of influence was assessed using the groundwater elevations, groundwater flow direction, and hydraulic conductivities.

Based on the information, groundwater is interpreted to be flowing generally northward at a rate of approximately 2.91 m³/s, with a linear velocity of 2.85 x 10⁻⁴ m/year.

 A Vibration Attenuation Assessment was carried out by M-ROC consultants. Based on the report provided by M-ROC, the PPV anticipated from the proposed blasting operations would be analogous to background vehicle vibration approximately 400 metres from the site epicentre. As such, vibration associated with blasting operations would not be anticipated to loosen materials into existing water supply wells.

It is understood that the Fairhaven Area is located approximately 0.5 kms to the south of the subject area. As such, based on the topography, direction of groundwater flow assessed above, the Vibration Attenuation Assessment, and the proposed depths of the planned excavations for the Rohit development, the proposed development is not anticipated to impact the general groundwater conditions or quality at Fairhaven Area. Therefore, it is the opinion of Terrapex that a full HIA is not required for this project.



8.0 CLOSURE

This report has been completed in accordance with the terms of reference for this project as agreed upon by Rohit Communities (the Client) and Terrapex Environmental Ltd. (Terrapex) and generally accepted hydrogeological consulting practices in this area.

The reported information is believed to provide a reasonable representation of the general hydrogeological conditions at the site; however, studies of this nature have inherent limitations. The data were collected at specific locations and conditions may vary at other locations, or with the passage of time. Where applicable, the assessment of the environmental quality of groundwater was limited to a study of those chemical parameters specifically addressed in this report.

Terrapex has relied in good faith on information and representations obtained from the Client and third parties and, except where specifically identified, has made no attempt to verify such information. Terrapex accepts no responsibility for any deficiency or inaccuracy in this report as a result of any misstatement, omission, misrepresentation, or fraudulent act of those providing information. Terrapex shall not be responsible for conditions or consequences arising from relevant facts that were concealed, withheld, or not fully disclosed at the time of the study.

This report has been prepared for the sole use of Rohit Communities. Terrapex accepts no liability for claims arising from the use of this report, or from actions taken or decisions made as a result of this report, by parties other than Rohit Communities.

Respectfully submitted,

TERRAPEX ENVIRONMENTAL LTD.

Andrew Durbano, M.Sc., P.Geo. Hydrogeologist

Zen Keizars, P.Geo., FGC. Senior Hydrogeologist





FIGURES









APPENDIX I Borehole Log Reports

CLIENT: Rohit Communities			PROJECT NO.: (CO947.00	0 RECORD OF:			
ADDRESS: Wateridge Village / Hemlock Road A	Area		STATION:		BH	H/MW4-1		
CITY/PROVINCE: Ottawa, ON	I	NORTHING (m): 5033514.04	EASTING (m):	450267.99 E	ELEV. (m) 88.15		
CONTRACTOR: George Downing Estate Drilling	Ltd	ME	THOD:					
BOREHOLE DIAMETER (cm): 20 WELL DIAM	METER (cm)): 5 SCF	REEN SLOT #: 10	SAND TYPE:	2 SEALANT T	TYPE: Bentonite		
SAMPLE TYPE _ AUGER _ DRIVEN		RING	DYNAMIC COI	NE SHEL		SPOON GRAB		
SOIL DESCRIPTION	DEPTH (m) ELEVATION (m	(kPa) 40 80 120 N-VALUI (Blows/300) 20 40 60	CONTEN (%) E mm)▲ PL W.C. 80 20 40 60	08 T A SAMPLE NO. SAMPLE TYPE RECOVERY (%	CSV/TOV (ppm or %LEL) LABORATORY TESTING	REMARKS REMARKS		
FILL 0 hard, brown, moist 1 sandy silty clay 0 trace organics 0 Bedrock 1 Cored to depth of 4.63 m. 1 2 2 3 2 4 2 4 2 4 2 5 3 4 4	0 88 0.5 87.5 - 1 87.5 - 1 87.5 - 1 87.5 - 1 87.5 - 2 86.5 - 2 86.5 - 3 85.5 - 3 85.5 - 3 85.5 - 4 84.5 - 4 84 -		75 18	1 100 R1 R2 R3		Bentonite 50 mm monitoring well was installed and the water level measured on November 24, 2023: 4.0 mbgs		
END OF BOREHOLE	4.5		LOGGED BY: UB		LLING DATE: 08-	END OF BOREHOLE: 4.65 mbgs ELEV.(m) = 83.5		
TEDDADEV		F				24-11-2023		
		F	REVIEWED BY: T	Y PAG	E 1 OF 1			

CLIENT: Rohit Communities			PROJECT NO.:	CO947.00	0 RECORD OF:			
ADDRESS: Wateridge Village / Hemlock Road	Area		STATION:		BH4-2			
CITY/PROVINCE: Ottawa, ON		NORTHING	(m): 5033481.01	EASTING (r	m): 450271.84	ELEV. (m) 87.91		
CONTRACTOR: George Downing Estate Drillin	ng Ltd	ME	THOD:	1				
BOREHOLE DIAMETER (cm): WELL D	IAMETER (cr	n): SC	REEN SLOT #:	SAND TYPE	E: SEALA	NT TYPE:		
SAMPLE TYPE AUGER DRIVEN				NE SH		PLIT SPOON GRAB		
SOIL DESCRIPTION	DEPTH (m) ELEVATION (m)	(kPa) 40 80 12 N-VALU (Blows/300 20 40 60	ENGTH WATER CONTEN 0 160 (%) //E PL W.C. 0 80 20 40 60	08 T SAMPLE NO. 21 SAMPLE TYPE	RECOVERY (%) CSV/TOV (ppm or %LEL) LABORATORY TESTING	NOLTALLA KEWARKS		
FILL firm to hard, dark brown, moist sandy silty clay trace gravel, trace organics Gr=8.7%, Sa=33.5%, Si=35.9%, Cl=21.9% LL=49.8%, PI=21.	0.5 0.5 1 1	57 Å	23.6 14.7	1	100			
Bedrock END OF BOREHOLE						END OF BOREHOLE: 1.32 mbgs ELEV.(m) = 86.6		
		F	LOGGED BY: UB	B [[DRILLING DATE:	08-11-2023		
		ŀ				16.		

CLIEN	IT: Rohit Communities				PROJECT NO.: CO947.00					00 RECORD OF:				
ADDR	ESS: Wateridge Village / Hemlo	ock Road Are	a		STA	ATION:						B	H/N	IW5-1
CITY/	PROVINCE: Ottawa, ON			NORTHING	(m): 50	033509	9.37	EAST	ring ((m):	450192	.60	ELEV.	(m) 87.72
CONT	RACTOR: George Downing Est	ate Drilling Lt	td	ME	THOD:									
BORE	HOLE DIAMETER (cm): 20	WELL DIAME	ETER (cm): 5 SCI	REEN	SLOT #	t: 10	SAN	D TYF	PE: 2	SE		TYPE:	Bentonite
SAMF	PLE TYPE AUGER	DRIVEN		RING		DYNAM	IC CON	NE	s		BY		T SPO	ON GRAB
GWL (m) SOIL SYMBOL	SOIL DESCRIPTIOI	DEPTH (m)	ELEVATION (m)	(kPa) 40 80 12 N-VALU (Blows/300	0 160 E mm)	C PL 20	ONTEN (%) W.C.	T LL	SAMPLE NO. SAMPLE TYPE	RECOVERY (%	CSV/TOV (ppm or %LEL)	LABORATORY TESTING	WELL INSTALLATION	REMARKS
	FILL compact to very dense, browr sandy silt some sand, some clay, trace trace organics Gr=9.0%, Sa=13.0%, Si=66.5%, C crushed rock pieces Bedrock Cored to depth of 4.39 n	n, moist gravel, -0.5 -1 l=11.5% - -1 -1.5% - -1.5% -	87.5 87- 86.5 86.5 86.5 88.5 88.5 88.5 88.5 88.5			20 25.4 4.9 ■ 7.5	1	BU F	3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	100		1		Bentonite 50 mm monitoring well was installed and the water level measured on November 24, 2023 4.24 mbgs Sand Screen + Sand
	END OF BOREHOLE													END OF BOREHOLE: 4.39 mbgs ELEV.(m) = 83.3
							Y: UB			DRIL	LING DA	ATE: 08	3-11-2	023
	TERR/	APEX		Ļ	INPU	IT BY:	RR			MON	ITORING	G DATE	: 24-1	11-2023
1	¥				REVI	IEWED	BY: T	Y		PAG	E 1 OF 1			

CLIEN	NT: Rohit Communities		PROJECT NO.: CO947.00				7.00	0 RECORD OF:						
ADDR	RESS: Wateridge Village / Hemlo	ck Road Area			STA	ATION:						E	BH/N	1W5-2
CITY/	PROVINCE: Ottawa, ON			NORTHING (m): 50	033464.	36	EAS	STING	(m):	4502	16.33	ELEV	. (m) 86.91
CONT	RACTOR: George Downing Esta	te Drilling Ltd		ME	THOD:									
BORE	HOLE DIAMETER (cm): 20	WELL DIAMET	ER (cm): 5 SCI	REEN	SLOT #:	10	SAN		PE: 2	2			
SAMF	PLE TYPE AUGER			RING		DYNAMIC W/	CON ATER	NE	<u> </u>		3Y	_ <u>∏</u> SP I		OON GRAB
GWL (m)	SOIL DESCRIPTION	M HLG	EVATION (m	(kPa) 40 80 12 N-VALU (Blows/300	0 160 E mm)	PL V	NTEN ⁻ (%) W.C.	T	MPLE NO.	COVERY (%	sV/TOV om or %LEL)	BORATORY STING	ELL STALLATION	REMARKS
		<u>8</u>		20 40 60	80	20 40	<u> </u>	80	SA SA	R	S q	42	₿ž	Bentonite
	very dense, brown, mois	t Ľ		50/125	5	17.4			1	100				50 11 1 1
	sandy silt	- 0.5	86.5											was installed and the
	Bedrock													water level measured on November 24, 2023
	Cored to depth of 4.57 m	1	86 -											3.52 mbgs
	TCR(1) = 100%	-							R1					
	RQD(1) = 32%		85.5 -											
		- 1.5												
		-	85 -											
		-2												
	TCP(2) = 100%		84 5 -											
	RQD(2) = 79%	- 2.5							R2					
									1					Sand
		- 3	04											Screen + Sand
		-											l:≣:	
		- 3.5	83.5 -											
		-												
	TCR(3) = 100%	- 4	83-						R3					
	1(2) - 12/0	-												
		- 4.5	82.5											
	END OF BOREHOLE													END OF BOREHOLE: 4.57 mbgs
														ELEV.(m) = 82.3
					LOG	GED BY:	UB	-		DRIL	LING	DATE:	08-11-2	2023
	TFRR	PFX		F	INPU	IT BY: R	R			MON	ITORI	NG DAT	E:	
				-	REV	IEWED B	Y: T	Y		PAG	E 1 OF	= 1		

CLIEN	IT: Rohit Communities				PROJECT NO.: CO947.00				7.00	0 RECORD OF:				
ADDR	ESS: Wateridge Village / Hemloo	ck Road Area			STA	ATION:				BH/MW6-1				/IW6-1
CITY/	PROVINCE: Ottawa, ON			NORTHING	m): 50	033727.0	08	EAS	STING	i (m):	4500	70.46	ELEV	. (m) 82.82
CONT	RACTOR: George Downing Estat	te Drilling Ltd		ME	THOD:									
BORE	HOLE DIAMETER (cm): 20		ER (cm): 5 SC	REEN	SLOT #:	10	SAN	ID TY	PE: 2	2 :	SEALAN	IT TYPE	: Bentonite
SAMP	PLE TYPE AUGER			RING				E	ц	SHEL	BY	_∐_SP	LIT SPC	OON GRAB
GWL (m) SOIL SYMBOL	SOIL DESCRIPTION	DEPTH (m)	ELEVATION (m)	(kPa) 40 80 12 N-VALU (Blows/300 20 40 60	0 160 E mm) 80	CON (PL W 20 40	V.C. LI	L 80	SAMPLE NO.	RECOVERY (%	CSV/TOV (ppm or %LEL)	LABORATORY TESTING	WELL	REMARKS
	FILL stiff, grey, moist sandy silty clay, trace gravel & or Gr=8.7%,Sa=21.5%,Si=26.6% 43.2%. very dense, light brown, moi SILTY GRAVELLY SAND trace to some clay, rock piec Gr=29.2%, Sa=37.5%, Si=23.5%, Cl= Bedrock Cored to depth of 4.67 m. TCR(1) = 100% RQD(1) = 15%	rganics - 0.5 5,Cl= - 1 5es - 1.5 =9.8% 2 - 2.5 - 3 - 3.5 - 4	82.5 - 82 - 81.5 - 81.5 - 80.5 - 79.5 - 79.5 - 78.5 -	1 2 53 ▲ 50/125 ▲		20.7 16.8 10.7 ■ 11.5			1A 1B 2 3 R1 R2	50				Bentonite 50 mm monitoring well was installed and the water level measured on November 24, 2023: 4.30 mbgs Sand Screen + Sand
	END OF BOREHOLE													END OF BOREHOLE: 4.67 mbgs ELEV.(m) = 78.1
	TERRA	PEX			LOG	GED BY: IT BY: RI	UB R	· 1		DRII MON	LING	DATE: NG DAT	10-11-2 Е:	2023
	V				REVI	EWED B	Y: TY	,		PAG	E 1 OF	= 1		

CLIEN	T: Rohit Communities				PROJECT NO.: CO947.00					RECORD OF:				
ADDR	ESS: Wateridge Village / Hemle	ock Road Area			STATION:					BH6-2				
CITY/F	PROVINCE: Ottawa, ON			NORTHING	6 (m): 5033694.44 EASTIN					G (m): 450105.97 ELEV. (m) 84.19				
CONT	RACTOR: George Downing Est	ate Drilling Ltd		ME										
BORE	HOLE DIAMETER (cm):	WELL DIAMET	ER (cm): SCI	REEN	SLOT	#:	SAN		PE:	5		T TYPE	:
SAMP	LE TYPE AUGER	DRIVEN		RING	NGTH	DYNA T	MIC CC	NE R	<u>ц</u> ;	SHEL	BY	SPI	LIT SPO	ON GRAB
GWL (m) GWL (m)	SOIL DESCRIPTIO	DEPTH (m)	ELEVATION (m	(kPa) 40 80 12 N-VALU (Blows/300 20 40 60	E mm) 80	F 20	CONTEN (%) PL W.C.	JT LL 80	SAMPLE NO.	RECOVERY (%	CSV/TOV (ppm or %LEL)	LABORATORY TESTING	WELL	REMARKS
	FILL compact to dense, grey, m sandy silty clay trace gravel, trace oxidati Bedrock Cored to depth of 1.15 n	noist 0.5	84 - 83.5 -	▲ 30	2	8.0 2.7			1A 1B 2	50				
	END OF BOREHOLE													END OF BOREHOLE: 1.15 mbgs ELEV.(m) = 83.0
					LOG	GED	BY: UE	3		DRIL	LING [DATE: 1	10-11-2	023
	TERR/	APEX			INPL	JT BY	RR			MON	ITORI	NG DAT	E:	
1	V				REV	IEWE	DBY:	ΓY		PAG	E 1 OF	1		

CLIEN	IT: Rohit Communities				PRC	DJECT NO.:	CO947.00	0	RECORD OF:			
ADDF	ESS: Wateridge Village / Hemlo	ock Road Area			STA	TION:		BH/MW6-3				
CITY/	PROVINCE: Ottawa, ON			NORTHING	(m): 50)33677.45	EASTIN	IG (m): 4	G (m): 450119.58 ELEV. (m) 85.70			
CONT	RACTOR: George Downing Est	ate Drilling Ltd		ME	THOD:		1					
BORE	HOLE DIAMETER (cm):	WELL DIAMET	ER (cm): SC	REEN S	SLOT #:	SAND 1	TYPE:	SEALAN	T TYPE:		
SAMF	PLE TYPE AUGER	DRIVEN		RING		YNAMIC CO WATEF		SHELE	BY <u>II</u> SPI		GRAB	
GWL (m) GWL (m)	SOIL DESCRIPTIOI		ELEVATION (m	(kPa) 40 80 12 N-VALU (Blows/300 20 40 60	0 160 IE Imm)	CONTEN (%) PL W.C. <u>20 40 60</u>	. TI SAMPLE NO. SAMPLE NO.	SAMPLE TYPE RECOVERY (%	CSV/TOV (ppm or %LEL) LABORATORY TESTING	WELL	REMARKS	
	FILL very stiff, brown, moist silty clay some gravel, some sand Bedrock Cored to depth of 3.50 n TCR(1) = 100% RQD(1) = 16% TCR(2) = 100% RQD(2) = 30% END OF BOREHOLE		86.5 86.5 86.5 85.5 84.5 84.5 83.5 83.5 82.5 82.5 82.5 82.5			24.8 24.8	1 R1 R2		CS CS CS CS CS CS CS CS CS CS		D OF BOREHOLE: 4 mbgs EV.(m) = 81.0	
							_ ;		LING DATE [、] (<u> </u>		
1	TFRR	APFX		-	INPU	<u>т вү:</u> RR		MON	ITORING DAT	E:		
				-	REVI	EWED BY: 1	ΓY	PAGE	E 1 OF 1			

ADDRESS: Wateringer Ullage / Henrick: Road Area STATION: BHE-4 CITYPROPUNCE: Claws, ON MORTHING cpr: 503826.16 RASTING (nr): 450118.00 REEV (nr): 87.36 CONTRACTOR: Group Downing Estate Drilling Ltd MORTHING (nr): 450118.00 REEV (nr): 87.36 SOUTE: DEVICE: Only Net Soute Error Soute Er	CLIENT: Rohit Communities		PROJECT N	RECORD OF:						
CITUPREVNCE: CITURATION CONTINUE (m): SCATURA (m): ACTIVA (M):	ADDRESS: Wateridge Village / Hemlock Road	l Area		STATION:			BH6-4			
CONTRACTOR: Cederage Downing Estate Defining Lid METHOD: SAMPLE TYPE AUGER ORNON SCHENDLE DMARKER (m) SCHENDLE DMARKER (m)	CITY/PROVINCE: Ottawa, ON		NORTHING	m): 5033626.	.16 EAST	ING (m):	NG (m): 450118.00 ELEV. (m) 87.36			
BORENUCT BUNKTER (m): SERUNT TYPE: SAMPLE TYPE: SERUNT TYPE: SAMPLE TYPE: SERUNT TYPE: SOIL DOM: OF WINKING CONTENT SUBJECT ON GRAIN OF SOIL DOM: OF WINKING CONTENT SUBJECT TYPE: SERUNT TYPE: SOIL DOM: OF WINKING CONTENT SUBJECT ON GRAIN OF DESCRIPTION OF WINKING CONTENT SUBJECT ON GRAIN SOIL DOM: OF WINKING CONTENT SUBJECT ON GRAIN OF DESCRIPTION OF WINKING CONTENT SUBJECT ON GRAIN SOIL DOM: OF WINKING CONTENT SUBJECT ON GRAIN SOIL DOM: OF WINKING CONTENT SUBJECT ON GRAIN SOIL DOM: OF WINKING CONTENT SUBJECT ON GRAIN SUBJECT ON GRAIN OF ON GRAIN OF ON GRAIN SUBJECT ON GRAIN OF ON GRAIN SUBJECT ON GRAIN	CONTRACTOR: George Downing Estate Drillin	ME	THOD:							
SAMULE TYPE AUGER OPRIAN CORING OPVIAUUC CONE SHELEY PUTTOON GRAB SOUL SOUL SUBJECT SUBJECT<	BOREHOLE DIAMETER (cm): WELL D	IAMETER (cm	n): SCI	REEN SLOT #:	SAND	TYPE:	SEALAN			
Image: Solution Image: Sol	SAMPLE TYPE AUGER DRIVEN					SHEL		LIT SPOON GRAB		
Set of fm, grey, moist sity clay trace gravel, tace sand, tace organics Cr= 60%, Sar 7.8%, Si=25.4%, Cl=0.8%. 0 67 6 1 2 1 42 1 1 42 1 1 42 1 1 42 1 1 42 1 1 42 1 1 42 1 1 42 1 1 42 1 1 42 1 1 42 1 1 43 1<	(III) TO SOIL DESCRIPTION	DEPTH (m) ELEVATION (m)	SHEAR STRE (kPa) 40 80 12 N-VALU (Blows/300) 20 40 60	E mm) PL 0 80 20 40	ATER NTENT (%) W.C. LL 0 60 80	SAMPLE TYPE RECOVERY (%)	CSV/TOV (ppm or %LEL) LABORATORY TESTING	NOLTA REMARKS REMARKS		
END OF BOREHOLE	FILL soft to firm, grey, moist silty clay trace gravel, trace sand, trace organics Gr=6.0%, Sa=7.8%, Si=25.4%, CI=60.8%. LL=58.3%, PI=28.	0 0.5 0.5 1 86.5 1.5 85.5 2 85.5 2.5 85.5	7 7 6 4 1	29.4 32.1 34. 38	9 3 1 4			END OF BOREHOLE.		
LOGGED BY: UB DRILLING DATE: 10-11-2023 INPUT BY: RR MONITORING DATE:	END OF BOREHOLE							END OF BOREHOLE: 2.77 mbgs ELEV.(m) = 84.6		
			ŀ	LOGGED BY:	UB	DRIL		10-11-2023		
			F					E:		

CLIENT: Rohit Communities		PROJECT NO.:	CO947.00	RECORD OF:			
ADDRESS: Wateridge Village / Hemlock Road Area		STATION:	1	BH6-5			
CITY/PROVINCE: Ottawa, ON N	IORTHING (m): 5033612.15	EASTING (m): 450146.62	ELEV. (m) 87.34		
CONTRACTOR: George Downing Estate Drilling Ltd	MET	THOD:					
BOREHOLE DIAMETER (cm): WELL DIAMETER (cm):	SCF	REEN SLOT #:	SAND TYPE:	SEALAN			
	ING	DYNAMIC CO		ELBY <u>I</u> SP	LIT SPOON GRAB		
SOIL SOIL SOUL SAVIBOL SOIL SAVID SOIL SO	(kPa) <u>40 80 120</u> N-VALUI (Blows/300r 20 40 60	CONTEN 0 160 (%) E mm) PL W.C. 80 20 40 60	08 TT 11 SAMPLE NO. SAMPLE TYPE	CSV/TOV CSV/TOV (ppm or %LEL) LABORATORY TESTING	NOILEALIN KEMARKS		
0 FILL soft, grey, moist silty clay trace gravel, trace sand, trace organics 0 87		80 20 40 60 32.8 34.6 32.9 30.5			END OF BOREHOLE: 2.97 mbgs ELEV.(m) = 84.5		
TERRADEV	ŀ				10-11-2023		
	F	REVIEWED BY: T	TY P4	GE 1 OF 1	· •		

CLIENT: Rohit Communities	PR	OJECT NC	.: CO94	47.00	RECORD OF:							
ADDRESS: Wateridge Village / Hemlock Roa	d Area			ST	ATION:			BH/MW6-6				
CITY/PROVINCE: Ottawa, ON			NORTHING	6 (m): 5	033580.1	0 EA	STING	G (m):	450125.25	ELEV	. (m) 85.87	
CONTRACTOR: George Downing Estate Dril	ing Ltd		М	ETHOD	:							
BOREHOLE DIAMETER (cm): 20 WELL		ER (cm	i): 5 So		SLOT #: 1	0 SA		'PE: 2	SEALA	NT TYPE	: Bentonite	
SAMPLE TYPE AUGER DRIVE	N P		RING I SHEAR STE					SHEL	BY <u>I</u> S	PLIT SPC	OON GRAB	
	EPTH (m)	-EVATION (m)	(kPa 40 80 1 N-VAL (Blows/30	1)● 20 160 UE 00mm)▲	CONT (% PL W.	C. LL	AMPLE NO.	ECOVERY (%	SV/TOV pm or %LEL) ABORATORY ESTING	ELL STALLATION	REMARKS	
Image: Some gravel in the some gravel i	E 0 0.5 1.5 2.5 3.5 4.5 4.5	85.5 - 85 - 84.5 - 84.5 - 83.5 - 82.5 - 82.5 - 81.5 -		30 80	PL W. 20 40	C. LL 60 80	1 2 3 R1 R2		CSVT (pm c		Bentonite 50 mm monitoring well was installed and the water level measured on November 24, 2023: 3.67 mbgs Sand Screen + Sand END OF BOREHOLE: 4.64 mbgs ELEV.(m) = 81.2	
				LOG	GED BY:	UB		DRIL	LING DATE:	10-11-2	2023	
TERRAPE	(INPL	JT BY: R	2		MON	IITORING DA	TE: 24-	11-2023	
v				REV	IEWED BY	: TY		PAG	E 1 OF 1			

CLIENT: Rohit Communities						PROJECT NO.: CO947.00					0	RECORD OF:							
ADDRESS: Wateridge Village / He	nlock Roa	d Area				STATION:						BH6-7							
CITY/PROVINCE: Ottawa, ON				NORTHIN	IG (n	n): 50	0335	64.8	36	EA	STI	NG (m):	45016	63.18	ELEV	. (m)	86.75	
CONTRACTOR: George Downing	state Drilli	ng Ltd			MET	HOD:		- //					-						
					SCR			#:				I Y P						CRAR	
	DRIVE			SHEAR S		NGTH		WA				ы Ш	HEL (%)			z		GRAD	
	ON	DEPTH (m)	ELEVATION (40 80 N-VA (Blows/ 20 40	120 ALUE /300m 60	160 m) 80	- 	(PL W) 40	%) /.C. 60	LL 80	SAMPLE NO.	SAMPLE TYP	RECOVERY (CSV/TOV (ppm or %LEL	LABORATOR TESTING	WELL		REMARKS	
FILL very dense, brown, n sand and gravel some silt, trace cla	oist /	- 0.5	86.5 - 86 - 85.5 - 85.5 -	50/125 4	50		19. 8.9 ■	I 4			2		42				ENC	OF BOREHOLE	Ξ
Cored to depth of 1.8 END OF BOREHC	<u>) m.</u> _E																	mbgs V.(m) = 84.9	
						LOG	GED	BY:	UB				DRIL	LING	DATE: ()8-11-2	2023		
TER	RAPEX	•				INPL	IT BY	': RI	R				MON	IITORI	NG DAT	E:			
▼								פ ח	ν· Τ	~									

APPENDIX II Hydrological Analyses







APPENDIX III Appended Assessments



PPV Assessment R1 Wateridge Block 4, 5, & 6

Submitted by:

M-Roc Ltd 130 Spindrift Circle Ottawa, Ontario K4M 0G4 Phone: 613-791-9222 Jeff.corace@m-roc.ca Contact: Jeff Corace, P.Eng

> Submission Date: November 26, 2024





BLAST PLAN 70 Richmond Road – Development Project

Scope of Work:

The following is a brief commentary on the predicted PPV levels expected to be encountered as part of the Wateridge Block 5, 6, & 7 development.

We have looked at the PPV levels predicted at 100m, 200m and 400m from the epicentre of the project, and have used the following expected rock depths.

Block 4 – Max of 2.0m Rock Cut – Max Charge weight of 5kg Block 5 – Max of 2.5m Rock Cut – Max Charge weight of 6.5kg Block 6 – Max of 3.5m Rock Cut – Max Charge weight of 11.5kg

Vibration Limits:

Blasting will be performed in compliance to City of Ottawa SP-F1201 as shown below.

Element	Frequency Hz	Peak Particle Velocity (PPV) mm/s
	≤ 40	20
Structures and Pipelines	> 40	50
Concrete and Grout < 72 hours from placement	N/A	10

Figure 1- F-1201 Vibration Limits

High frequency vibrations (Hz>40) are expected to be the guiding limit on this project due to the close proximity of the sensitive structures. Low total weight of explosives will contain sufficient high frequency energy to break the rock locally but will dissipate very quickly with distance. Typically, low frequency vibration occurs at greater distances and will largely not be the limiting factor for surrounding structures. Blasting will strive to be below both high frequency and low frequency vibration limits.





130 SPINDRIFT CIRCLE OTTAWA, ONTARIO K4M 0G4 P. (613) 838-4666 C. (613) 791-9222 OFFICE@M-ROC.CA

Vibration Prediction

Peak Particle Velocity (PPV) values may be approximated using the following propagation formula:

$$PPV = k(\frac{R}{\sqrt{W}})^{-e}$$

where:

k = 1730 (upper limit with heavy confinement) e = -1.85 attenuation rate (typical for City of Ottawa) W = charge weight/delay of powder (kg) R = distance to blast (m)

Table 1 – Predicted PPV per Block								
Block	Distance (m)	PPV (mm/s)						
4	100	1.53						
4	200	0.42						
4	400	0.12						
4	500	0.03						
5	100	1.95						
5	200	0.54						
5	400	0.15						
5	500	0.03						
6	100	3.31						
6	200	0.92						
6	400	0.25						
6	500	0.06						

Conclusion:

We trust that the above satisfies the request for information regarding PPV assessment. However, should any additional information be required please do not hesitate to contact the undersigned at your convenience.

K

Jeff Corace, P.Eng. M-Roc Ltd Drilling and Blasting





⁴ R _i .	(Ottawa	
Ver		" Ri	rer

edicted PPV per Blo	DDV (mm/o)
	PPV (mm/s)
100	1.53
200	0.42
400	0.12
500	0.03
100	1.95
200	0.54
400	0.15
500	0.03
100	3.31
200	0.92
400	0.25
500	0.06

Leg	lend
- 🎝	Block 4 - 100m
- 🍰	Block 4 - 200m
- 🍰	Block 4 - 400m
0:20	Block 4 - 500m
	Block 5 - 100m
	Block 5 - 200m
- 🍰	Block 5 - 400m
- 🎝	Block 5 - 500m
- 🎝	Block 6 - 100m
- 🎝	Block 6 - 200m
- 🍰	Block 6 - 400m
- 🎝	Block 6 - 500m

Sir George=Étienne

cliffe Dr

A N