

# Geotechnical Investigation

## Proposed Sortation Facility

Project X Development

99 Bill Laethem Drive, 2 & 20 Leikin Drive and 11 Beckstead Road  
Ottawa, Ontario

Prepared for Broccolini

Report PG5876-2 Revision 1 dated September 11, 2024

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## 1.0 Introduction

Paterson Group (Paterson) was commissioned by Broccolini to conduct a geotechnical investigation for the proposed Project X Development to be located at 99 Bill Leathem Drive, 2 & 20 Leikin Drive & 11 Beckstead Road in the City of Ottawa, Ontario (reference should be made to Figure 1 - Key Plan in Appendix 2 of this report for the general site location).

The objectives of the geotechnical investigation were to:

- Determine the subsoil and groundwater conditions at this site by means of test holes, and to
- Provide geotechnical recommendations pertaining to design of the proposed development including construction considerations which may affect the design.

The following report has been prepared specifically and solely for the aforementioned project which is described herein. It contains our findings and includes geotechnical recommendations pertaining to the design and construction of the subject development as they are understood at the time of writing this report.

Investigating the presence or potential presence of contamination on the subject property was not part of the scope of work of the present investigation. Therefore, the present report does not address environmental issues.

## 2.0 Proposed Development

Based on the available drawings, it is understood that the proposed development will consist of a multi-storey sortation facility building with a slab-on-grade and an approximate footprint of 60,000 m<sup>2</sup>. The proposed building will be immediately surrounded by loading bays, access lanes and parking areas.

The proposed development will also include the construction of a sanitary alignment connected between Leathem Drive and Merivale Road, which is to be located south of the proposed building.

## **3.0 Method of Investigation**

### **3.1 Field Investigation**

#### **Field Program**

The field program for the current investigation was conducted between July 25 and August 7, 2024 and consisted of advancing a total of 32 boreholes to a maximum depth of 14.3 m below the existing grade.

These boreholes were advanced using a low clearance, track-mounted drill rig operated by a two-person crew. The drilling procedure consisted of augering to the required depths at the selected locations and sampling the overburden soils. All fieldwork was conducted under the full-time supervision of our personnel under the direction of a senior engineer from our geotechnical department.

Previous geotechnical investigations were completed by others in June to July 2023, and April to May 2021. During those investigations, a total of 18 boreholes, 68 test pits and 28 cone-penetration tests (CPTs) were advanced throughout the subject site to a maximum depth of 28.3 m below the existing ground surface. Additional historical boreholes were completed by others between June 1990 and October 1991, at which time 10 boreholes were drilled to a maximum depth of 22.7 m below the ground surface.

The test hole locations were distributed in a manner to provide general coverage of the subject site and taking into consideration underground utilities and site features. The locations of the test holes are shown on Drawing PG5876-1 - Test Hole Location Plan in Appendix 2.

The subsurface profiles are presented on the Test Hole Logs and Cone Penetration Testing (CPT) Logs by Others in Appendix 1.

#### **Sampling and In Situ Testing**

Soil samples collected from the boreholes were either recovered directly from the auger flights (AU) or collected using a 50 mm diameter split-spoon (SS) sampler. All samples were initially classified on site and subsequently placed in sealed plastic bags and transported to our laboratory for further examination and classification. The depths at which the auger and split spoon samples were recovered from the boreholes are shown as AU and SS, respectively, on the Soil Profile and Test Data Sheets presented in Appendix 1.

The Standard Penetration Test (SPT) was conducted in conjunction with the recovery of the split spoon samples. The SPT results are recorded as "N" values on the Soil Profile and Test Data sheets. The "N" value is the number of blows required to drive the split spoon sampler 300 mm into the soil after a 150 mm initial penetration using a 63.5 kg hammer falling from a height of 760 mm.

Undrained shear strength testing was conducted at regular intervals in cohesive soils (clay) where encountered, using a field vane apparatus.

The overburden thickness was evaluated by a dynamic cone penetration test (DCPT) completed at boreholes BH 1-24 to BH 17-24, BH 20-24, BH 21-24, and BH 30-24 to BH 32-24. The DCPT consists of driving a steel drill rod, equipped with a 50 mm diameter cone at the tip, using a 63.5 kg hammer falling from a height of 760 mm. The number of blows required to drive the cone into the soil is recorded for each 300 mm increment.

The subsurface conditions observed in the boreholes were recorded in detail in the field. The soil profiles are logged on the Soil Profile and Test Data sheets and Cone Penetration Testing (CPT) Logs, by others, presented in Appendix 1.

## **Groundwater**

Boreholes BH 18-24, BH 22-24 to BH 25-24, BH 29-24 and BH 32-24 were fitted with 51 mm diameter PVC groundwater monitoring wells. Boreholes BH 5-24, BH 9-24, BH 11-24, BH 14-24 and BH 15-24 were fitted with flexible polyethylene standpipes to permit monitoring of the groundwater levels subsequent to the completion of the sampling program. The groundwater observations are discussed in Subsection 4.3 and presented in the Soil Profile and Test Data sheets in Appendix 1.

Typical monitoring well construction details are described below:

- Slotted 51 mm diameter PVC screen at the base of each borehole.
- 51 mm diameter PVC riser pipe from the top of the screen to the ground surface.
- No.3 silica sand backfill within annular space around screen.
- Bentonite hole plug directly above PVC slotted screen.
- Clean backfill from top of bentonite plug to the ground surface.

Reference should be made to the Soil Profile and Test Data sheets presented in Appendix 1 for specific well construction details.

## **3.2 Field Survey**

The test hole locations and ground surface elevation at each test hole location were surveyed by Paterson using a high precision, handheld GPS and referenced to a geodetic datum. The location of the test holes and ground surface elevation at each the test hole location are presented on Drawing PG5876-1 - Test Hole Location Plan presented in Appendix 2.

## **3.3 Laboratory Review**

Soil samples were recovered from the subject site and visually examined in our laboratory to review the results of the field logging. A total of 2 Atterberg limits tests were completed on selected soil samples obtained from the current investigation. Moisture content was completed on all retrieved soil samples. The results of the testing are discussed in Section 4.2 and are provided in Appendix 1.

### **Sample Storage**

All samples from the current investigation will be stored in the laboratory for a period of 1 month after issuance of this report. They will then be discarded unless we are otherwise directed.

## **3.4 Analytical Testing**

One (1) soil sample was submitted for analytical testing to assess the corrosion potential for exposed ferrous metals and the potential of sulphate attacks against subsurface concrete structures by Paterson. The sample was submitted to determine the concentration of sulphate and chloride, the resistivity, and the pH of the sample. The results are discussed further in Section 6.7 and presented in Appendix 1.

## 4.0 Observations

### 4.1 Surface Conditions

The majority of the subject site currently consists of agricultural fields. The existing ground surface was observed to be relatively flat at approximate geodetic elevation 90.5 m, although it has been noted that an approximately 5 m high stockpile of fill had been placed within the southwest portion of the subject site.

The site is bordered to the west and north by agricultural land, to the south by Bill Leathem Drive and a three-storey manufacturing facility on Paragon Avenue, and to the east by Leikin Drive. The subject site is at grade with the surrounding roadways.

### 4.2 Subsurface Profile

#### Overburden

Generally, the subsurface profile consists of topsoil underlain by a deep deposit of silty clay, followed by a glacial till deposit.

The silty clay deposit was observed to consist of a layer of hard to very stiff, brown silty clay crust extending to depths ranging between 2.9 and 4.5 m below ground surface. The brown silty clay layer was observed to be underlain by a firm to stiff, grey silty clay deposit extending to depths ranging between 9.0 and 17.0 m below the ground surface.

The silty clay deposit was underlain by a compact to very dense glacial till deposit. The fine matrix of the glacial till was observed to consist of either silty clay or silty sand, along with varying amounts of gravel, cobbles and boulders.

Practical refusal to DCPT was observed at depths ranging between 17.4 and 23.6 m below ground surface.

Reference should be made to the Soil Profile and Test Data sheets presented in Appendix 1 for details of the soil profile encountered at each borehole location.

#### Bedrock

Based on available geological mapping, the bedrock in the subject area consists of interbedded sandstone and dolomite of the March formation, with an overburden drift thickness of 15 to 25 m depth.



The bedrock was cored by others throughout the subject site at depths ranging between 19.3 and 25.4 m below the ground surface, and was observed to consist of a fair to good quality dolomite.

### Atterberg Limit and Shrinkage Tests

Atterberg limits testing, as well as associated moisture content testing, were completed on the recovered silty clay samples at selected locations throughout the subject site. The results of the Atterberg limits tests are presented in Table 1 and on the Atterberg Limits Results by Others in Appendix 1.

<b>Table 1 - Atterberg Limits Results</b>						
<b>Test Hole and Sample</b>	<b>Depth (m)</b>	<b>LL (%)</b>	<b>PL (%)</b>	<b>PI (%)</b>	<b>w (%)</b>	<b>Classification</b>
BH 4-24 SS2	0.7-1.3	61	25	36	38.6	CH
BH 16-24 SS3	1.5-2.1	40	19	21	34.0	CL
Notes: LL: Liquid Limit; PL: Plastic Limit; PI: Plasticity Index; w: water content; CH: Inorganic Clay of High Plasticity CL: Lean Clay of Low Plasticity ML: Silt						

Atterberg limits testing were also completed following previous investigations by others. The results of the Atterberg Limits testing completed by others are summarized in Table 2 and on the Laboratory Results by Others included in Appendix 1.

<b>Table 2 - Atterberg Limits Results by Others</b>						
<b>Test Hole and Sample</b>	<b>Depth (m)</b>	<b>LL (%)</b>	<b>PL (%)</b>	<b>PI (%)</b>	<b>w (%)</b>	<b>Classification</b>
BH-01 ST-5	3.05	52	21	31	45	CH
BH-01 SS-11	9.15	50	24	26	68	CH
BH-02 ST-7	4.57	47	22	25	54	CL
BH-02 SS-3	1.52	38	17	21	27	CL
BH-02 SS-11	9.15	27	22	5	25	CL-ML
BH-02 SS-14	11.43	14	12	2	8	SM
BH-02 SS-19	15.24	13	11	2	8	SM
BH-03 SS-11	8.23	48	23	25	66	CL
BH-03 SS-14	12.19	26	18	8	39	CL
BH-03 SS-18	18.29	15	13	2	9	SM

Test Hole and Sample	Depth (m)	LL (%)	PL (%)	PI (%)	w (%)	Classification
BH-03 ST-13	10.67	41	22	19	58	CL
BH 101-23 SS-06	3.05-3.66	43	19	24	33	CL
BH 101-23 SS-08	4.57-5.18	46	21	25	50	CL
BH 101-23 SS-10	6.09-6.70	51	25	26	62	CH
BH 101-23 SS-12	7.62-8.23	48	23	25	63	CL
BH 102-23 SS-12	7.62-8.23	39	19	20	33	CL
BH 102-23 SS-14	10.1-10.7	44	20	24	52	CL
BH 102-23 SS-16	13.1-13.7	65	22	43	62	CH
BH 102-23 SS-17	14.6-15.3	43	21	22	51	CL

Notes: LL: Liquid Limit; PL: Plastic Limit; PI: Plasticity Index; w: water content;  
 CH: Inorganic Clay of High Plasticity CL: Lean Clay of Low Plasticity ML: Inorganic Silt

### Grain Size Distribution and Hydrometer Testing

Grain size distribution was completed by others on 11 soil samples. The grain-size analysis results are summarized in Table 3 below, and also in Appendix 1.

Test Hole	Sample	Gravel (%)	Sand (%)	Silt (%)	Clay (%)
BH 01	ST 5	0	7	93	
BH 01	SS 11	0	7	93	
BH 02	SS 3	0	10	90	
BH 02	SS 11	0	2	98	
BH 02	SS 14	22	42	36	
BH 02	SS 19	26	40	34	
BH 03	SS 11	0	4	96	
BH 03	SS 14	0	6	67	27
BH 03	SS 18	25	45	23	7
BH 101-23	SS 12	0	0.7	99.3	
BH 101-23	SS 17	0	0.5	99.5	
BH 101-23	SS 18	0	0.5	99.5	
BH 102-23	SS 12	0	3.6	96.4	

### 4.3 Groundwater

Groundwater levels were measured on August 13, 2024 within the installed monitoring wells and piezometers. The measured groundwater levels are presented in Table 4 below and on the Soil Profile and Test Data Sheet in Appendix 1.

<b>Table 4 – Summary of Groundwater Levels (Paterson – 2024 Investigation)</b>					
<b>Borehole Number</b>	<b>Observation Method</b>	<b>Ground Surface Elevation (m)</b>	<b>Measured Groundwater Level</b>		<b>Date Recorded</b>
			<b>Depth (m)</b>	<b>Elevation (m)</b>	
BH 5-24	Piezometer	90.56	1.15	89.41	August 13, 2024
BH 9-24	Piezometer	90.43	1.02	89.41	August 13, 2024
BH 11-24	Piezometer	90.52	1.02	89.50	August 13, 2024
BH 14-24	Piezometer	90.38	0.92	89.46	August 13, 2024
BH 15-24	Piezometer	90.46	0.63	89.83	August 13, 2024
BH 18-24	Monitoring Well	90.61	1.26	89.35	August 13, 2024
BH 22-24	Monitoring Well	90.37	1.08	89.29	August 13, 2024
BH 23-24	Monitoring Well	90.37	0.88	89.49	August 13, 2024
BH 24-24	Monitoring Well	90.25	0.45	89.80	August 13, 2024
BH 25-24	Monitoring Well	90.44	1.26	89.18	August 13, 2024
BH 29-24	Monitoring Well	90.34	1.33	89.01	August 13, 2024
BH 32-24	Monitoring Well	90.06	4.97	85.09	August 13, 2024

Long-term groundwater levels can also be estimated based on the observed colour and consistency of the subsurface profile. Based on these observations, the long-term groundwater table can be expected at a depth ranging between 2.5 to 3.5 m below the existing ground surface.

However, it should be noted that groundwater levels are subject to seasonal fluctuations. Therefore, the groundwater levels could vary at the time of construction.

## 5.0 Discussion

### 5.1 Geotechnical Assessment

From a geotechnical perspective, the subject site is considered suitable for the proposed development. Based on preliminary foundation loads provided by the structural engineer, it is understood that the foundation loads will vary from approximately 5,000 to 8,000 kN. Accordingly, it is recommended that foundation support for the proposed building consist of one of the following:

- conventional spread footings bearing on the undisturbed, stiff silty clay in conjunction with significant lightweight fill placed under the building floor slab, or
- end-bearing piles driven to refusal on the bedrock surface

Due to the presence of a silty clay layer, the site is subjected to a permissible grade raise restriction. The permissible grade raise recommendations are discussed in Section 5.3.

Based on the anticipated excavation depth and the nature of the overburden, a temporary excavation support system is expected to be required for the construction of the proposed sanitary alignment.

The above and other considerations are discussed in the following sections.

### 5.2 Site Grading and Preparation

#### Stripping Depth

Topsoil and deleterious fill, such as those containing significant organic materials, should be stripped from under any buildings, paved areas, pipe bedding and other settlement sensitive structures.

Care should be taken not to disturb adequate bearing soils below the founding level during site preparation activities. Disturbance of the subgrade may result in sub-excavating the disturbed material and the placement of additional suitable fill material.

## Fill Placement

Fill used for grading beneath the building area should consist, unless otherwise specified, of clean imported granular fill, such as Ontario Provincial Standard Specifications (OPSS) Granular A or Granular B Type II. The imported fill material should be tested and approved by Paterson personnel prior to delivery to site. The fill should be placed in lifts no greater than 300 mm thick and compacted using suitable compaction equipment for the lift thickness. Fill placed beneath the building footprint should be compacted to a minimum of 98% of the standard Proctor maximum dry density (SPMDD).

Non-specified existing fill along with site-excavated soil can be used as general landscaping fill where settlement of the ground surface is of minor concern. The material should be spread in thin lifts with a maximum thickness of 300 mm and at least compacted by the tracks of the spreading equipment to minimize voids.

If excavated brown silty clay, free of organics and deleterious materials, is to be used to build up the subgrade level for areas to be paved, it is recommended that the material be placed under dry conditions and above freezing temperatures. The silty clay should be compacted in thin lifts using suitable compaction equipment to a minimum density of 95% of its respective SPMDD.

## 5.3 Foundation Design

### Conventional Spread Footings

Pad footings, up to 8 m wide, and strip footings up to 2.5 m wide, placed on the undisturbed, stiff silty clay can be designed using a bearing resistance value at serviceability limit states (SLS) of **150 kPa** and a factored bearing resistance value at ultimate limit states (ULS) of **225 kPa**. A geotechnical resistance factor of 0.5 was applied to the above-noted bearing resistance value at ULS.

It should be noted that these bearing resistance values and footing sizes can only be used in conjunction with a reduced permissible grade raise restriction within the building footprint. This is discussed further below in the “Permissible Grade Raise Recommendations” subsection.

An undisturbed soil bearing surface consists of a surface from which all topsoil and deleterious materials, such as loose, frozen or disturbed soil, whether in situ or not, have been removed, in the dry, prior to the placement of concrete for footings.

Footings placed on the undisturbed, stiff silty clay and designed using the bearing resistance values at SLS given above will be subjected to potential post construction total and differential settlements of 25 and 20 mm, respectively.

## Pile Foundation

As an alternative to conventional spread footings and a reduced permissible grade raise restriction within the building footprint, a deep foundation consisting of end-bearing steel pipe piles could be employed.

Concrete filled steel pipe piles driven to refusal are a typical deep foundation option in Ottawa. Applicable pile resistance at serviceability limit states (SLS) and ultimate limit states (UL) are provided in Table 5 below. Additional resistance values can be provided if available pile sizes vary from those detailed in Table 5. Note that these are all geotechnical axial resistance values.

The geotechnical pile resistance values were estimated calculating the Hiley dynamic formula. The piles should be confirmed during pile installation with a program of dynamic monitoring. For this project, the dynamic monitoring of four piles is recommended. This is considered to be the minimum monitoring program, as the piles under shear walls may be required to be driven using the maximum recommended driving energy to achieve the greatest factored resistance at ULS values.

<b>Table 5 - Pile Foundation Design Data</b>				
<b>Pile Outside Diameter (mm)</b>	<b>Pile Wall Thickness (mm)</b>	<b>Geotechnical Axial Resistance</b>	<b>Final Set (blows/12 m)</b>	<b>Transferred Hammer Energy (kJ)</b>
		<b>Factored at ULS (kN)</b>		
245	9	1090	10	28.5
245	11	1260	10	34.2
245	13	1500	10	40.7

The minimum centre-to-centre pile spacing is 2.5 times the pile diameter. The closer the piles are spaced, however, the more potential that the driving of subsequent piles in a group could have influence on piles in the group that have already been driven. These effects, primarily consisting of uplift of previously driven piles, are checked as part of the field review of the pile driving operations.

Accordingly, re-striking of all piles, at least once, will also be required after at least 48 hours have elapsed since initial driving.

A full-time field review program carried out by Paterson personnel should be conducted during the pile driving operations, which is required under the Ontario Building Code (OBC) 2012 to record the pile lengths, and to ensure that the refusal criteria is met, and that piles are driven within the location tolerances (within 75 mm of proper location and within 2% of vertical).

Prior to the commencement of production pile driving, a limited number of indicator piles should be installed across the site. It is recommended that each indicator pile be dynamically load tested to evaluate pile stresses, hammer efficiency, pile load transfer, and end-of-driving criteria for end-bearing in the bedrock.

### Down Drag Loads

Due to the presence of silty clay below the subject site and proposed grade raises at the site, down drag loads should be considered during the final design of the piles. Based on the available subsurface information, it is expected that the piles will be driven through approximately 21 to 26 m of stiff to soft silty clay. The silty clay generally has a cohesion of 30 to 70 kPa. Assigning an adhesion factor of 1.0 to 0.5 (as per the Canadian Foundation Engineering Manual), the silty clay can be taken to have an ultimate adhesion of 20 kPa against the sides of the piles.

The down drag load is effectively applied to each pile at the location of the “neutral plane,” where negative (i.e., down drag) skin friction becomes positive shaft resistance. In the case of the end-bearing piles at this site, the neutral plane will be located near the bedrock surface.

The down drag load is a structural pile capacity criterion and does not affect the geotechnical capacity of the piles. The structural axial capacity of the pile is governed by its structural strength at the neutral plane when subjected to the permanent load plus the down drag load. Transient live load is not to be included. At or below the pile cap, the structural strength of the embedded pile is determined as a short column subjected to the permanent load plus the transient live load, but down drag load is to be excluded.

At the depth of the neutral plane where the down drag load is applied, the pile structure is well confined. The 4th edition of the Canadian Foundation Engineering Manual recommends that the allowable structural axial capacity of piles at the neutral plane, for resisting permanent load plus the down drag load, can be determined by applying a factor of safety of 1.5 to the pile material strength (steel yield and concrete 28 day compressive strength).

## Foundation Lateral Load Resistance

Lateral loads on the foundations can be resisted using passive resistance on the sides of the foundations. For Limit States Design, the resistance factor to be applied to the ultimate lateral resistance, including passive pressure, is 0.50. The total lateral resistance will be comprised of the individual contributions from up to several material layers.

Geotechnical parameters for the native silty clay and glacial till, and for typical backfill materials, compacted to 98% of SPMDD in 300 mm lift thicknesses, are provided in Table 6 below. In addition, earth pressure coefficients are provided in Table 6 for the horizontal resistance calculated for pile caps or grade beams under lateral loads. Friction factors between concrete and the various subgrade materials are also provided in Table 6, where normal loads allow them to be used.

Where granular soils and/or granular backfill materials are present, the passive pressure can be calculated using a triangular distribution equal to  $K_P \cdot \gamma \cdot H$  where:

$K_P$  = factored passive earth pressure coefficient of the applicable retained soil  
 $\gamma$  = unit weight of the fill of the applicable retained soil (kN/m<sup>3</sup>)  
 $H$  = height of the equivalent wall or footing side (m)

Note that for cases where the depth to the top of the structure pushing against the soil does not exceed 50% of the depth to the base of the structure, the effective value of  $H$  in the above noted relationship will be the overall depth to the base of the structure. There will also be “edge effects” where the effective width of soil providing the resistance can be increased by 50% of the effective depth on each side of the pushing structural component.

Note that where the foundation extends below the groundwater level, the effective unit weight should be utilized for the saturated portion of the soil or fill.

Should additional passive resistance be required, the horizontal component of the axial resistance of battered piles (up to 1H:3V inclination), or anchors can be used in the building foundation design. This resistance would be considered in conjunction with additional sources of lateral load resistance considered for the structure.

## Foundation Uplift Resistance

Uplift forces on the proposed foundations can be resisted using the dead weight of the concrete foundations, the weight of the materials overlying the foundations, and the submerged weight of the piles. Unit weights of materials are provided in Table 6.



For soil above the groundwater level, uplift forces should be calculated using the drained unit weight. For calculations below groundwater level, the effective unit weight should be used. Backfilled excavations in low permeability soils can be expected to fill with water. Then, effective unit weights should be used if drainage of the anchor footings is not allowed.

As noted above, the piles will be mostly located below the groundwater level, so the submerged, or effective, weights of the piles, where used, will be available to contribute to the uplift resistance. Considering that this is a reliable uplift resistance, and is counteracting a dead load, it is our opinion that a resistance factor of 0.9 is applicable for the ULS weight component. Should the pile uplift resistance capacities be insufficient for the foundation uplift loads, rock anchors should be utilized if a deadman anchor is not considered economical (i.e., dead weight of buried concrete foundation members). Detailed design recommendations for rock anchors can be provided upon request, if needed.

A sieve analysis and standard Proctor test should be completed on each of the fill materials proposed to obtain an accurate soil density to be expected, so the applicable unit weights can be estimated.

<b>Table 6 – Geotechnical Parameters for Uplift and Lateral Resistance Design</b>							
<b>Material Description</b>	<b>Unit Weight (kN/m<sup>3</sup>)</b>		<b>Internal Friction Angle (°) <math>\phi'</math></b>	<b>Friction Factor, <math>\tan \delta</math></b>	<b>Earth Pressure Coefficients</b>		
	<b>Drained <math>\gamma_{dr}</math></b>	<b>Effective <math>\gamma'</math></b>			<b>Active <math>K_A</math></b>	<b>At-Rest <math>K_0</math></b>	<b>Passive <math>K_p</math></b>
OPSS Granular A (Crushed Stone)	22.0	13.7	38	0.60	0.22	0.36	8.80
OPSS Granular B Type II (Well-Graded Sand-Gravel)	21.5	13.4	36	0.55	0.26	0.41	7.50
In-Situ Silty Clay	17.0	10.0	33	0.40	0.30	0.45	3.40
In-Situ Glacial Till	20.0	12.0	33	0.50	0.29	0.46	3.39

**Notes:**

- Properties for fill materials are for condition of 98% of standard Proctor maximum dry density.
- The earth pressure coefficients provided are for horizontal backfill profile.
- Passive pressure coefficients incorporate wall friction of  $0.5 \phi'$ .

## Permissible Grade Raise Recommendations

If the proposed building is supported on conventional spread footings bearing on the undisturbed stiff silty clay, a reduced permissible grade raise restriction of **0.4 m** is required inside and within 3 m of the building footprint. With this permissible grade raise restriction and the available preliminary grading for the site, it is expected that significant lightweight fill (about 1.0 m thickness or more) would be required below the slab-on-grade.

If the proposed building is supported on end-bearing piles, a permissible grade raise restriction of **1.5 m** is applicable inside and within 3 m of the building footprint.

A permissible grade raise restriction of **2.0 m** may be considered throughout the remainder of the subject site, regardless of the foundation type of the proposed building.

As noted above, if higher than permissible grade raises are required, lightweight fill and/or other measures should be investigated to reduce the risks of unacceptable long-term post construction total and differential settlements.

However, once detailed grading plans have been finalized for the subject development, Paterson should complete a review of the proposed grades for the subject site to ensure they are suitable from a geotechnical perspective, and to specify lightweight fill thicknesses, where required.

## 5.4 Design for Earthquakes

The site class for seismic site response can be taken as **Class D** for foundations constructed at the subject site. The soils underlying the subject site are not susceptible to liquefaction. Reference should be made to the latest revision of the 2012 Ontario Building Code for a full discussion of the earthquake design requirements.

## 5.5 Slab-on-Grade Construction

With the removal of all topsoil and fill within the footprint of the proposed building, the native and undisturbed silty clay deposit will be considered to be an acceptable subgrade upon which to commence backfilling for floor slab construction.

The upper 300 mm of sub-slab fill is recommended to consist of OPSS Granular A crushed stone. All backfill material within the footprint of the proposed building should be placed in maximum 300 mm thick loose lifts and compacted to a minimum of 98% of its SPMDD.

If the top of the slab-on-grade extends above the permissible grade raise restriction, then lightweight fill (LWF) would be required under the 300 mm thickness of OPSS Granular A crushed stone. The specific thickness of LWF would depend on the final elevation of the slab-on-grade.

## 5.6 Pavement Design

Car only parking areas, access lanes, heavy truck parking areas, and concrete aprons are anticipated at this site. The proposed pavement structures are presented in Tables 7 to 9 below.

<b>Table 7 – Recommended Light Duty Pavement Structure for Car Only Parking Areas</b>	
<b>Thickness (mm)</b>	<b>Material Description</b>
50	<b>Wear Course</b> - HL-3 or Superpave 12.5 Asphaltic Concrete
150	<b>BASE</b> - OPSS Granular A Crushed Stone
450	<b>SUBBASE</b> - OPSS Granular B Type II
Separation Layer	<b>Woven Geotextile</b> - Terrafix 200W or equivalent
<b>SUBGRADE</b> – Either approved fill, in-situ soil, or OPSS Granular B Type I or II material placed on in-situ soil or fill.	

<b>Table 8 - Recommended Flexible Pavement Structure for Access Lanes and Heavy Truck Parking Areas</b>	
<b>Thickness (mm)</b>	<b>Material Description</b>
40	<b>Wear Course</b> - HL-3 or Superpave 12.5 Asphaltic Concrete
50	<b>Upper Binder Course</b> - HL-8 or Superpave 19.0 Asphaltic Concrete
50	<b>Lower Binder Course</b> - HL-8 or Superpave 19.0 Asphaltic Concrete
150	<b>BASE</b> - OPSS Granular A Crushed Stone
550	<b>SUBBASE</b> - OPSS Granular B Type II
Separation Layer	<b>Woven Geotextile</b> - Terrafix 200W or equivalent
<b>SUBGRADE</b> - Either approved fill, in-situ soil, or OPSS Granular B Type I or II material placed on in-situ soil or fill.	

<b>Table 9 - Recommended Rigid Structure for Concrete Aprons</b>	
<b>Thickness (mm)</b>	<b>Material Description</b>
Specified by Others	Reinforced Concrete Slab
150	<b>BASE</b> - OPSS Granular A Crushed Stone
600	<b>SUBBASE</b> - OPSS Granular B Type II
100	HI-40 Rigid Insulation
<b>SUBGRADE</b> - Either approved fill, in-situ soil, or OPSS Granular B Type I or II material placed on in-situ soil or fill.	

The pavement granular base and subbase should be placed in maximum 300 mm thick lifts and compacted to a minimum of 100% of the material's SPMDM using suitable compaction equipment. If soft spots develop in the subgrade during compaction or due to construction traffic, the affected areas should be excavated and replaced with OPSS Granular B Type II material.

### **Grade Raise Fill for Paved Areas**

It is anticipated the cut and fill operation throughout the subject site will result in portions of the paved areas to be located over grade raise fill. This fill may consist of a workable brown silty clay material generated by site excavations. It should be noted that grey or wet/saturated portions of the silty clay will not be considered suitable for this purpose. If additional material will be imported to accommodate the proposed grades, the geotechnical consultant should review the additional material at the source prior to being delivered to site to assess its suitability for this purpose.

Site-approved grade raise fill should be spread in maximum 300 mm thick loose lifts and compacted using a suitably sized vibratory sheepsfoot roller. It is anticipated the material may be compacted by several passes of the suitably sized equipment (i.e.- 5 to 6 passes and as deemed appropriate by the geotechnical consultant at the time of construction). The material should be placed in **dry and above-freezing conditions**. Frozen material may not be considered for this purpose.

Surfaces should be shaped to minimize ponding of water and promote sheet drainage of rain. Areas exposed to heavy rainfall events should be given a sufficient period to dry to avoid over-wetting of the surface and potential for soft spots to develop throughout the fill. Compaction efforts and placement of site-generated fill should be reviewed by the geotechnical consultant at the time of construction to ensure the placement of grade raise fill is carried out satisfactorily.

## **Paving Timeline**

It is recommended to delay paving over the grade raise fill areas by a minimum of one freeze-thaw seasons (i.e.- raise subgrade with suitable fill prior to winter and freezing temperatures, pave the following summer or fall. It is not recommended to carry out paving within the early-spring in consideration of the thawing of soils affected by frost migration.

## **Frost Tapers**

For utility trenches and other subgrade structures backfilled with non-frost susceptible granular material or at the interface between the concrete apron and flexible pavement structure, consideration should be given to installing a 1V:5H frost tapers in hard landscaped areas and below pavement structures to lessen the effects of differential frost heaving. Consideration could also be given to installing rigid insulation which requires tapering with various insulation thicknesses.

## **Rigid Pavement Apron - Frost Protection and Taper Recommendations**

To improve the long-term performance of the concrete apron and lessen the effects of frost penetration and movement, the following insulation detail is suggested:

- Insulation type required.....HI-40 or equivalent
- HI-40 Insulation thickness (directly under the concrete apron) .....100 mm
- HI-40 Insulation thickness (0 to 1.2 m beyond the edge of the apron).....75 mm
- HI-40 Insulation thickness (1.2 to 2.4 m beyond the edge of the apron)..50 mm
- HI-40 Insulation thickness (2.4 to 3.6 m beyond the edge of the apron)..25 mm

## **Pavement Structure Drainage**

The pavement structure performance is dependent on the moisture condition at the contact zone between the subgrade material and granular base. Failure to provide adequate drainage under conditions of heavy wheel loading could result in the subgrade fines pumped into the stone subbase voids, thereby reducing the load bearing capacity.

Due to the impervious nature of the subgrade materials and transitions between various pavement structures, consideration should be provided to installing subdrains during the pavement construction. At transition zones between various pavement structures, subdrains will be installed longitudinally to drain any potential water trapped in the granular layers. This recommendation should be considered at the transition between rigid aprons against the building footprints and the flexible pavement structure. The subdrains at catch basins should extend in four orthogonal directions and longitudinally when placed along a curb.

The clear crushed stone surrounding the drainage lines or the pipe, should be wrapped with suitable filter cloth. The subdrain inverts should be approximately 300 mm below subgrade level. The subgrade surface should be shaped to promote water flow to the drainage lines. Discharge of the subdrains should be directed by gravity to storm sewers or deeper drainage ditches.

## **6.0 Design and Construction Precautions**

### **6.1 Foundation Drainage and Backfill**

#### **Foundation Drainage**

It is recommended that a perimeter foundation drainage system be provided for the proposed structure. The system should consist of a 150 mm diameter, perforated and corrugated plastic pipe which is wrapped in a geosock and surrounded by 150 mm of 19 mm clear crushed stone, placed at the footing level around the exterior perimeter of the structure. The 19 mm clear crushed stone should be wrapped in a non-woven geotextile. The pipes should have a positive outlet, such as a gravity connection to storm sewer or sump pump.

#### **Foundation Backfill**

Backfill against the exterior sides of the foundation walls should consist of free-draining, non-frost susceptible granular materials. Foundation backfill located below pavement structures and hard landscaped areas should be spread in 300 mm thick loose lifts and compacted to a minimum of 95% of the materials SPMDD.

#### **Sidewalks and Walkways**

To avoid differential settlement within proposed sidewalks adjacent to the building, it is recommended that the upper 600 mm of backfill placed below concrete sidewalk and walkways adjacent to the proposed building footprint consist of free draining, non-frost susceptible material, such as OPSS Granular A or Granular B Type II.

The granular material should be shaped to promote positive drainage towards the building perimeter drainage system. The granular material should be placed in maximum 300 mm thick loose lifts and compacted to at least 98% of the materials SPMDD under dry and above-freezing conditions, and using suitable compaction equipment. Consideration could be given to placing a rigid insulation layer below the granular fill layer to prevent frost heave issues at the building entrance.

### **6.2 Protection of Footings Against Frost Action**

Perimeter footings and pile caps of heated structures are required to be insulated against the deleterious effects of frost action. A minimum 1.5 m thick soil cover, or a combination of soil cover in conjunction with insulation, should be provided in this regard.

Exterior unheated foundations, such as those for isolated exterior piers, are more prone to deleterious movement associated with frost action than the exterior walls of the heated structure. These structures require additional protection, such as 2.1 m of soil cover or an equivalent combination of soil cover and rigid insulation.

### **6.3 Excavation Side Slopes and Temporary Shoring**

The side slopes of excavations at the subject site should be cut back at acceptable slopes from the start of the excavation until structures are backfilled. It is expected that sufficient room will be available for excavations to be undertaken by open-cut methods.

However, if insufficient room is available to permit the proposed sanitary alignment excavation to be constructed by open-cut methods (i.e., unsupported excavations), then a temporary shoring system would be required.

#### **Unsupported Excavations**

The excavation side slopes above the groundwater level extending to a maximum depth of 3 m should be cut back at 1H:1V or flatter. The flatter slope is required for excavation below groundwater level. The subsurface soil is mainly a Type 2 and 3 soil according to the Occupational Health and Safety Act and Regulations for Construction Projects. Excavated soil should not be stockpiled directly at the top of excavations and heavy equipment should maintain safe working distance from the excavation sides.

Slopes in excess of 3 m in height should be periodically inspected by the geotechnical consultant in order to detect if the slopes are exhibiting signs of distress.

Excavated soil and other material should not be stockpiled directly at the top of excavations and heavy equipment should be kept away from the excavation sides.

It is recommended that a trench box be used at all times to protect personnel working in trenches with steep or vertical sides. It is expected that services will be installed by “cut and cover” methods and excavations will not be left open for extended periods of time.

#### **Temporary Shoring**

Temporary shoring may be required for support of the overburden soils to complete the required excavations for the installation of the sanitary alignment, where insufficient room is available for open cut methods.



If a temporary shoring system is required, the design and implementation of these temporary systems will be the responsibility of the excavation contractor and their design team. The shoring requirements, designed by a structural engineer specializing in those works, will depend on the depth of the excavation, the proximity of the adjacent structures, and the elevation of the adjacent building foundations and underground services. The design and implementation of these temporary systems will be the responsibility of the excavation contractor and their design team. Inspections and approval of the temporary system will also be the responsibility of the designer.

Geotechnical information provided below is to assist the designer in completing a suitable and safe shoring system. The designer should take into account the impact of a significant precipitation event and designate design measures to ensure that precipitation will not negatively impact the shoring system or soils supported by the system. Any changes to the approved shoring design system should be reported immediately to the owner's structural design prior to implementation.

The temporary system could consist of soldier pile and lagging system or interlocking steel sheet piling.

Any additional loading due to street traffic, construction equipment, adjacent structures and facilities, etc., should be included to the earth pressures described below. These systems could be cantilevered, anchored or braced. Generally, it is expected that the shoring systems will be provided with tie-back rock anchors to ensure their stability. The shoring system is also recommended to be adequately supported to resist toe failure and inspected to ensure that the sheet piles extend well below the excavation base.

The earth pressures acting on the shoring system may be calculated with the following parameters.

<b>Table 10 – Soil Parameters for Shoring System Design</b>	
<b>Parameters</b>	<b>Values</b>
Active Earth Pressure Coefficient ( $K_a$ )	0.33
Passive Earth Pressure Coefficient ( $K_p$ )	3
At-rest Earth Pressure Coefficient ( $K_o$ )	0.5
Total Unit Weight ( $\gamma$ ), kN/m <sup>3</sup>	20
Submerged Unit Weight ( $\gamma'$ ), kN/m <sup>3</sup>	13

The active earth pressure should be calculated where wall movements are permissible while the at-rest pressure should be calculated if no movement is permissible. The dry unit weight should be calculated above the groundwater level while the effective unit weight should be calculated below the groundwater level.

The hydrostatic groundwater pressure should be included to the earth pressure distribution wherever the effective unit weights are calculated for earth pressures. If the groundwater level is lowered, the dry unit weight for the soil/bedrock should be calculated full weight, with no hydrostatic groundwater pressure component.

### **Excavation Base Stability**

Excavation base stability for the deep sanitary alignment should be reviewed based on the final invert elevations.

The base of supported excavations can fail by 3 general modes:

- Shear failure within the ground caused by inadequate resistance to loads imposed by grade difference inside and outside of the excavation,
- Piping from water seepage through granular soils, and
- Heave of layered soils due to water pressures confined by intervening low permeability soils.

The factor of safety with respect to base heave,  $FS_b$ , is:

$$FS_b = N_b s_u / \sigma_z$$

where:

$N_b$  - stability factor dependent upon the geometry of the excavation and given in the figure on the following page.

$s_u$  - undrained shear strength of the soil below the base level.

$\sigma_z$  - total overburden and surcharge pressures at the bottom of the excavation.

Shear failure of excavation bases is typically rare in granular soils if adequate lateral support is provided. Inadequate dewatering can cause instability in excavations made through granular or layered soils. The potential for base heave in cohesive soils should be determined for stability of flexible retaining systems.

As a preliminary precaution, service trench excavations exceeding 4 to 5 m in depth should be assessed for excavation base stability during the design phase to verify the suitability of conventional cut-and-cover excavation techniques.

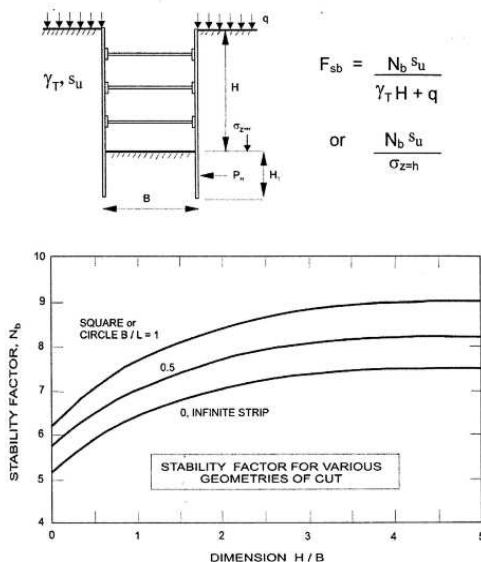


Figure for Stability Factor  $N_b$

## 6.4 Pipe Bedding and Backfill

Bedding and backfill materials should be in accordance with the most recent Material Specifications and Standard Detail Drawings from the Department of Public Works and Services, Infrastructure Services Branch of the City of Ottawa.

At least 150 mm of OPSS Granular A should be used for pipe bedding for sewer and water pipes when placed on a soil subgrade. If the bedding subgrade consists of grey silty clay, the thickness of the bedding should be increased to 300 mm for sewer pipes. The bedding should also extend to the spring line of the pipe.

Cover material, from the spring line to at least 300 mm above the obvert of the pipe, should consist of OPSS Granular A or Granular B Type II with a maximum size of 25 mm. The bedding and cover materials should be placed in maximum 225 mm thick lifts compacted to 99% of the material's SPMDD.

It should generally be possible to re-use the site materials above the cover material if the operations are carried out in dry weather conditions.

Where hard surface areas are considered above the trench backfill, the trench backfill material within the frost zone (about 1.8 m below finished grade) should match the soils exposed at the trench walls to minimize differential frost heaving. The trench backfill should be placed in maximum 300 mm thick loose lifts and compacted to a minimum of 95% of the material's SPMDD.

To reduce long-term lowering of the groundwater level at this site, clay seals should be provided in the service trenches. The seals should be at least 1.5 m long and should extend from trench wall to trench wall. Generally, the seals should extend from the frost line and fully penetrate the bedding, sub-bedding and cover material. The barriers should consist of relatively dry and compactable brown silty clay placed in maximum 225 mm thick loose lifts and compacted to a minimum of 95% of the material's SPMDD. The clay seals should be placed at the site boundaries and at no more than 60 m intervals in the service trenches.

## **6.5 Groundwater Control**

### **Groundwater Control for Building Construction**

It is anticipated that groundwater infiltration into the excavations should be controllable using open sumps. The contractor should be prepared to direct water away from all bearing surfaces and subgrades, regardless of the source, to prevent disturbance to the founding medium.

#### **Dewatering Permit**

A temporary Ministry of Environment, Conservation and Parks (MECP) permit to take water (PTTW) may be required if more than 400,000 L/day of ground and/or surface water are to be pumped during the construction phase. At least 4 to 5 months should be allowed for completion of the application and issuance of the permit by the MECP.

For typical ground or surface water volumes being pumped during the construction phase, typically between 50,000 to 400,000 L/day, it is required to register on the Environmental Activity and Sector Registry (EASR). A minimum of two to four weeks should be allotted for completion of the EASR registration and the Water Taking and Discharge Plan to be prepared by a Qualified Persons as stipulated under O.Reg. 63/16.

## **6.6 Winter Construction**

Precautions must be taken if winter construction is considered for this project.

The subsoil conditions at this site consist of frost susceptible materials. In the presence of water and freezing conditions, ice could form within the soil mass with potentially intolerable settlement upon thawing.

In the event of construction during below zero temperatures, the founding stratum should be protected from freezing temperatures by propane heaters and tarpaulins or other suitable means. Additional means may consist of backfilling the foundation with an appropriate thickness of fill extending above and beyond the base of the footing. It would be further recommended to mitigate heavy-truck traffic in proximity to the foundation and across the insulating soil to minimize the effect of compressing frost-affected soils against sufficiently insulated soils.

The base of the excavations should be insulated from sub-zero temperatures immediately upon exposure and until such time as heat is adequately supplied to the building and the footings are protected with sufficient soil cover to prevent freezing at founding level.

Trench excavations and pavement construction are difficult activities to complete during freezing conditions without introducing frost in the subgrade or in the excavation walls and bottoms. Precautions should be considered if such activities are to be completed during freezing conditions. Additional information could be provided, if required.

## **6.7 Corrosion Potential and Sulphate**

The results of analytical testing show that the sulphate content is less than 0.1%. This result is indicative that Type 10 Portland cement (normal cement) would be appropriate for this site. The chloride content and the pH of the sample indicate that they are not significant factors in creating a corrosive environment for exposed ferrous metals at this site, whereas the resistivity is indicative of a non-aggressive to slightly aggressive corrosive environment.

## **6.8 Tree Planting Restrictions**

Paterson completed a soils review of the site to determine the applicable tree planting setbacks, in accordance with the City of Ottawa's "Tree Planting in Sensitive Marine Clay Soils (2017 Guidelines)". Atterberg limits testing was completed for selected silty clay samples. Sieve analysis testing was also completed on selected soil samples. The results of the testing are presented in Tables 1, 2, and 3 in Section 4.2 and included in Appendix 1.

Based on the results of our review, the plasticity index of the silty clay deposit at the subject site does not exceed 40%. Therefore, the following tree planting setbacks are recommended for the silty clay deposit. Large trees (mature height over 14 m) can be planted within the silty clay areas provided a tree to foundation setback equal to the full mature height of the tree can be provided (e.g., in a park or other green space).

Tree planting setback limits may be reduced to **4.5 m** for small (mature height up to 7.5 m) and medium size trees (mature tree height 7.5 to 14 m), provided that the conditions noted below are met.

- The underside of footing (USF) is 2.1 m or greater below the lowest finished grade must be satisfied for footings within 10 m from the tree, as measured from the centre of the tree trunk and verified by means of the Grading Plan as indicated procedural changes below.
- A small tree must be provided with a minimum 25 m<sup>3</sup> of available soil volume while a medium tree must be provided with a minimum of 30 m<sup>3</sup> of available soil volume, as determined by the Landscape Architect. The developer is to ensure that the soil is generally un-compacted when backfilling in street tree planting locations.
- The tree species must be small (mature tree height up to 7.5 m) to medium size (mature tree height 7.5 m to 14 m) as confirmed by the Landscape Architect.
- The foundation walls are to be reinforced at least nominally (minimum of two upper and two lower 15M bars in the foundation wall).
- Grading surrounding the tree must promote drainage to the tree root zone (in such a manner as not to be detrimental to the tree).

It is well documented in the literature, and is our experience, that fast-growing trees located near buildings founded on cohesive soils that shrink on drying can result in long-term differential settlements of the structures. Tree varieties that have the most pronounced effect on foundations are seen to consist of poplars, willows, and some maples (i.e., Manitoba Maples) and, as such, they should not be considered in the landscaping design.

## 7.0 Recommendations

It is a requirement for the foundation design data provided herein to be applicable that a material testing and observation program be performed by the geotechnical consultant. The following aspects of the program should be performed by the geotechnical consultant:

- Review detailed grading plan(s) from a geotechnical perspective.
- Observation of all bearing surfaces prior to the placement of concrete.
- Sampling and testing of the concrete and fill materials.
- Periodic observation of the condition of unsupported excavation side slopes in excess of 3 m in height, if applicable.
- Observation of all subgrades prior to backfilling.
- Field density tests to determine the level of compaction achieved.
- Sampling and testing of the bituminous concrete including mix design reviews.

All excess soils, with the exception of engineered crushed stone fill, generated by construction activities that will be transported on-site or off-site should be handled as per *Ontario Regulation 406/19: On-Site and Excess Soil Management*.

A report confirming that these works have been conducted in general accordance with our recommendations could be issued upon the completion of a satisfactory inspection program by the geotechnical consultant.

## 8.0 Statement of Limitations

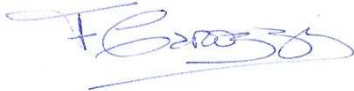
The recommendations provided are in accordance with the present understanding of the project. Paterson requests permission to review the recommendations when the drawings and specifications are completed.

A soils investigation is a limited sampling of a site. Should any conditions at the site be encountered which differ from those at the test locations, Paterson requests immediate notification to permit reassessment of our recommendations.

The recommendations provided herein should only be used by the design professionals associated with this project. They are not intended for contractors bidding on or undertaking the work. The latter should evaluate the factual information provided in this report and determine the suitability and completeness for their intended construction schedule and methods. Additional testing may be required for their purposes.

The present report applies only to the project described in this document. Use of this report for purposes other than those described herein or by person(s) other than Broccolini or their agents is not authorized without review by Paterson for the applicability of our recommendations to the alternative use of the report.

### Paterson Group Inc.



Fernanda Carrozzi, PhD. Geoph.



Scott S. Dennis, P.Eng.

### Report Distribution:

- Broccolini (digital copy)
- Paterson Group (1 copy)



# APPENDIX 1

SOIL PROFILE AND TEST DATA SHEETS

SYMBOLS AND TERMS

TEST HOLE LOGS BY OTHERS

ATTERBERG LIMITS TESTING RESULTS

LABORATORY TESTING RESULTS BY OTHERS

ANALYTICAL TESTING RESULTS

COORD. SYS.: MTM ZONE 9      EASTING: 366796.64      NORTHING: 5017980.42      ELEVATION: 90.61

PROJECT: Project X Development      FILE NO.: **PG5876**

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: July 25, 2024      HOLE NO.: **BH 1-24**

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, Cur (kPa)					
							▲ PEAK SHEAR STRENGTH, Cu (kPa)					
PL (%)		WATER CONTENT (%)		LL (%)								
GROUND SURFACE		0										
<b>TOPSOIL</b> 0.25m [90.36m]		0	SS 1	100	2-3-5-6 8	23.45	○			90		
Hard to very stiff, brown <b>SILTY CLAY</b>		1	SS 2	100	3-3-4-5 7	33.51	○			89		
2.13m [88.48m]		2	SS 3	100	1-1-2-2 3	34.81	○			89		
Dynamic Cone Penetration Test commenced at 2.13 m depth		2				41.73	○			88		
		3								87		
		4								86		
		5								85		
		6								84		
		7								83		
		8								82		
		9								81		
		10								80		
		11								79		
		12								78		
		13								78		

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							△ REMOULDED SHEAR STRENGTH, $C_{ur}$ (kPa)					
							▲ PEAK SHEAR STRENGTH, $C_u$ (kPa)					
PL (%)		WATER CONTENT (%)		LL (%)								
GROUND SURFACE		13									77	
		14									76	
		15									75	
		16									74	
		17									73	
		18									72	
		19									71	
19.76m [ 70.85m ]		20									70	
End of Borehole		21									69	
Cone pushed up to 18.59 m depth. Practical refusal to DCPT at 19.76 m depth.		22									68	
		23									67	
		24									66	
		25									65	
		26									65	

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COORD. SYS.: MTM ZONE 9      EASTING: 366763.67      NORTHING: 5018024.57      ELEVATION: 90.58

PROJECT: Project X Development      FILE NO.: **PG5876**

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: July 25, 2024      HOLE NO.: **BH 2-24**

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, Cur (kPa)					
							▲ PEAK SHEAR STRENGTH, Cu (kPa)					
PL (%)		WATER CONTENT (%)		LL (%)								
GROUND SURFACE		0										
<b>TOPSOIL</b> 0.23m [90.35m]		0	SS 1	90	2-2-4-6 6	21.6	○			90		
Hard to very stiff, brown <b>SILTY CLAY</b>		1	SS 2	90	4-3-5-4 8	30.72	○			89		
		2	SS 3	70	5-2-2-2 4	38.67	○			88		
2.13m [88.45m]		2				26.76	○			87		
Dynamic Cone Penetration Test commenced at 2.13 m depth		3								86		
		4								85		
		5								84		
		6								83		
		7								82		
		8								81		
		9								80		
		10								79		
		11								78		
		12								78		
		13								78		

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COORD. SYS.: MTM ZONE 9      EASTING: 366763.67      NORTHING: 5018024.57      ELEVATION: 90.58

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SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
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							△ REMOULDED SHEAR STRENGTH, $C_{ur}$ (kPa)					
							▲ PEAK SHEAR STRENGTH, $C_u$ (kPa)					
PL (%)		WATER CONTENT (%)		LL (%)								
GROUND SURFACE		13								77		
		14								76		
		15								75		
		16								74		
		17								73		
		18								72		
		19								71		
		20								70		
20.45m [ 70.13m ]		21								69		
End of Borehole		22								68		
		23								67		
		24								66		
		25								65		
		26								65		

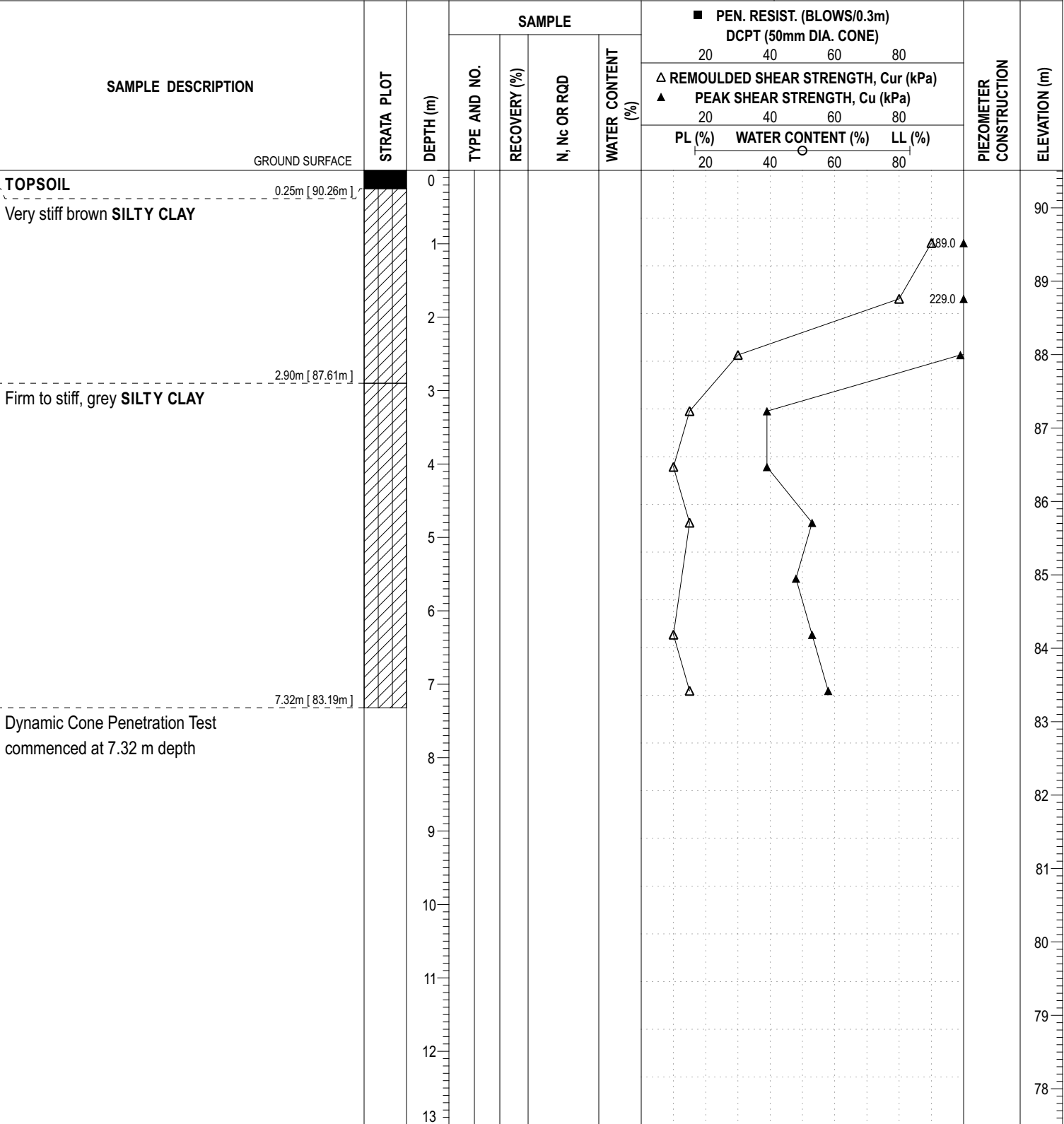
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COORD. SYS.: MTM ZONE 9      EASTING: 366721.56      NORTHING: 5018070.21      ELEVATION: 90.51

PROJECT: Project X Development      FILE NO.: **PG5876**

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: July 25, 2024      HOLE NO.: **BH 3-24**



P:/AutoCAD Drawings/Test Hole Data Files/PG5876/data/sqlite\_2024-09-10\_17:11 Paterson\_Template\_AA

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**COORD. SYS.:** MTM ZONE 9      **EASTING:** 366721.56      **NORTHING:** 5018070.21      **ELEVATION:** 90.51

**PROJECT:** Project X Development      **FILE NO. :** PG5876

**BORINGS BY:** CME 55 Low Clearance Drill

**REMARKS:**      **DATE:** July 25, 2024      **HOLE NO. :** BH 3-24

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, $C_{ur}$ (kPa) ▲ PEAK SHEAR STRENGTH, $C_u$ (kPa)					
			PL (%)		WATER CONTENT (%)		LL (%)					
GROUND SURFACE		13								77		
		14								76		
		15								75		
		16								74		
		17								73		
		18								72		
		19								71		
19.74m [ 70.77m ]		20								70		
End of Borehole		21								69		
Cone pushed up to 17.63 m depth.		22								68		
Practical refusal to DCPT at 19.74 m depth.		23								67		
		24								66		
		25								65		
		26								65		

P:/AutoCAD Drawings/Test Hole Data Files/PG5876/data/sqlite 2024-09-10, 17:11 Paterson\_Template AA

COORD. SYS.: MTM ZONE 9      EASTING: 366657.86      NORTHING: 5018035.99      ELEVATION: 90.54

PROJECT: Project X Development      FILE NO.: **PG5876**

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: July 26, 2024      HOLE NO.: **BH 4-24**

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, Cur (kPa)					
							▲ PEAK SHEAR STRENGTH, Cu (kPa)					
PL (%)		WATER CONTENT (%)		LL (%)								
GROUND SURFACE		0										
<b>TOPSOIL</b> Very stiff brown <b>SILTY CLAY</b>		0 to 2.13								90.54 to 88.41		
		0	SS 1	70	2-2-4-5 6	23.66						
		1	SS 2	100	3-4-5-4 9	27.53						
		2	SS 3	100	2-1-2-2 3	39.95						
		2				29.8						
Dynamic Cone Penetration Test commenced at 7.32 m depth		2.13 to 13								88.41 to 78		

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COORD. SYS.: MTM ZONE 9      EASTING: 366657.86      NORTHING: 5018035.99      ELEVATION: 90.54

PROJECT: Project X Development      FILE NO.: **PG5876**

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: July 26, 2024      HOLE NO.: **BH 4-24**

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, $C_{ur}$ (kPa)	▲ PEAK SHEAR STRENGTH, $C_u$ (kPa)	PL (%)			WATER CONTENT (%)
GROUND SURFACE												
		13									77	
		14									76	
		15									75	
		16									74	
		17									73	
		18									72	
		19									71	
19.61m [ 70.93m ]												
End of Borehole		20									70	
Cone pushed up to 13.87 m depth. Practical refusal to DCPT at 19.61 m depth.		21									69	
		22									68	
		23									67	
		24									66	
		25									65	
		26									65	

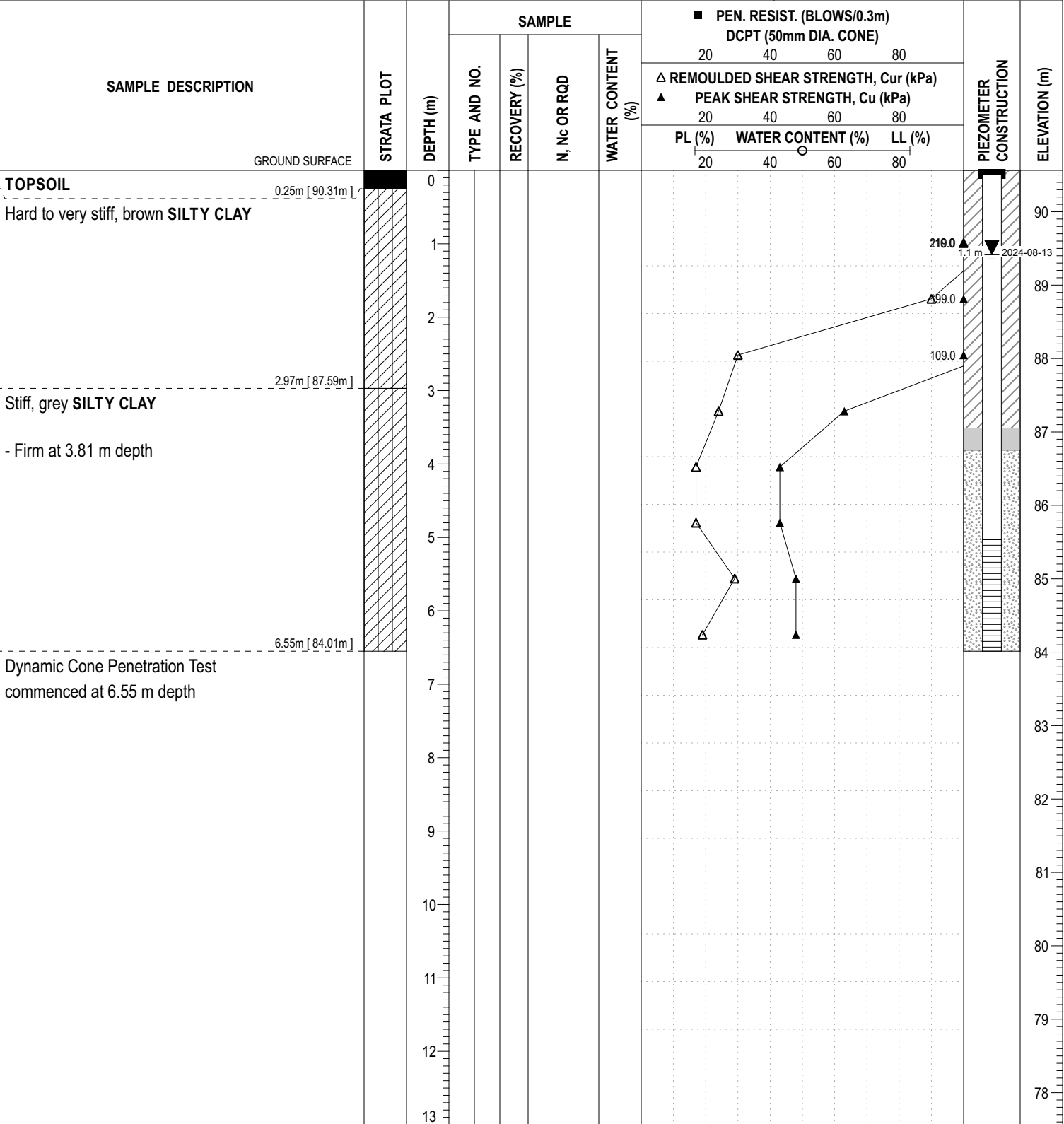
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COORD. SYS.: MTM ZONE 9      EASTING: 366644.70      NORTHING: 5017962.75      ELEVATION: 90.56

PROJECT: Project X Development      FILE NO.: **PG5876**

BORINGS BY: CME 55 Low Clearance Drill      HOLE NO.: **BH 5-24**

REMARKS:      DATE: July 26, 2024



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**COORD. SYS.:** MTM ZONE 9      **EASTING:** 366644.70      **NORTHING:** 5017962.75      **ELEVATION:** 90.56

**PROJECT:** Project X Development      **FILE NO. :** PG5876

**BORINGS BY:** CME 55 Low Clearance Drill

**REMARKS:**      **DATE:** July 26, 2024      **HOLE NO. :** BH 5-24

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, Cur (kPa) ▲ PEAK SHEAR STRENGTH, Cu (kPa)					20
			PL (%)		WATER CONTENT (%)		LL (%)					
GROUND SURFACE												
		13									77	
		14									76	
		15									75	
		16									74	
		17									73	
		18									72	
		19									71	
		20									70	
		21									69	
End of Borehole		21									69	
Cone pushed up to 15.19 m depth.		22									68	
Practical refusal to DCPT at 20.96 m depth.		23									67	
(GWL at 1.15 m depth - August 13, 2024)		24									66	
		25									65	
		26									65	

20.96m [ 69.60m ]

P:/AutoCAD Drawings/Test Hole Data Files/PG5876\data.sqlite 2024-09-10, 17:11 Paterson\_Template AA

COORD. SYS.: MTM ZONE 9      EASTING: 366682.93      NORTHING: 5017929.77      ELEVATION: 90.46

PROJECT: Project X Development      FILE NO.: **PG5876**

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: July 26, 2024      HOLE NO.: **BH 6-24**

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20    40    60    80				
							△ REMOULDED SHEAR STRENGTH, Cur (kPa)				
							▲ PEAK SHEAR STRENGTH, Cu (kPa)				
		PL (%)		WATER CONTENT (%)		LL (%)					
		20    40    60    80									
GROUND SURFACE		0								90.46	
TOPSOIL 0.25m [90.21m]		0	SS 1	60	2-3-4-6 7	29.87	○			90	
Very stiff brown SILTY CLAY		1	SS 2	100	2-4-5-6 9	29.63	○			89	
		2	SS 3	100	1-2-2-2 4	29.44	○			88	
Dynamic Cone Penetration Test commenced at 2.13 m depth		2.13m [88.33m]				32.89	○			88	
		3								87	
		4								86	
		5								85	
		6								84	
		7								83	
		8								82	
		9								81	
		10								80	
		11								79	
		12								78	
		13								77	

P:/AutoCAD Drawings/Test Hole Data Files/PG5876/data/sqlite 2024-09-10, 17:11 Paterson\_Template AA

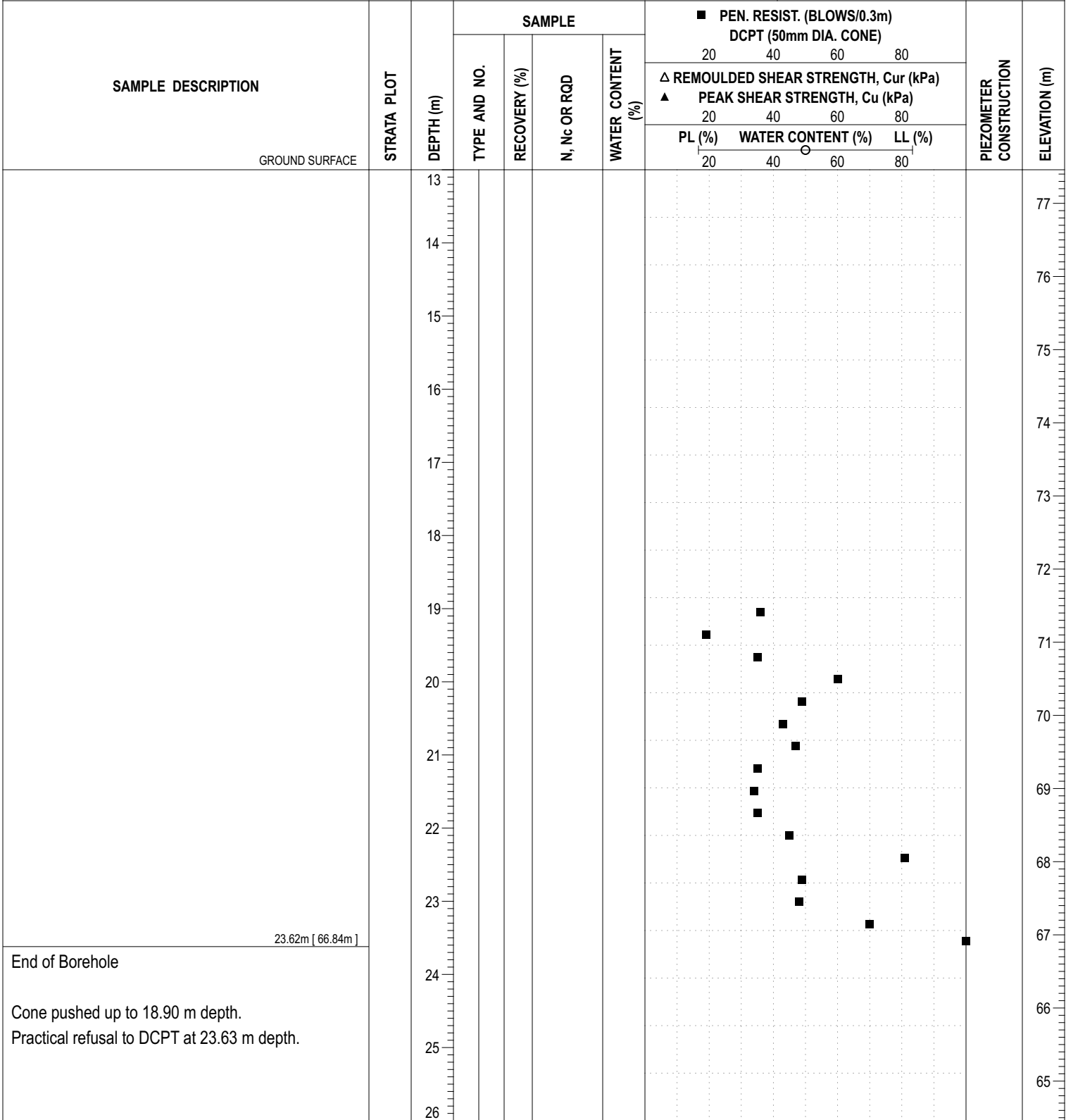
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COORD. SYS.: MTM ZONE 9      EASTING: 366682.93      NORTHING: 5017929.77      ELEVATION: 90.46

PROJECT: Project X Development      FILE NO.: **PG5876**

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: July 26, 2024      HOLE NO.: **BH 6-24**



P:/AutoCAD Drawings/Test Hole Data Files/PG5876/data/sqlite 2024-09-10, 17:11 Paterson\_Template AA

**COORD. SYS.:** MTM ZONE 9      **EASTING:** 366749.06      **NORTHING:** 5017944.55      **ELEVATION:** 90.45

**PROJECT:** Project X Development      **FILE NO. :** PG5876

**BORINGS BY:** CME 55 Low Clearance Drill

**REMARKS:**      **DATE:** July 26, 2024      **HOLE NO. :** BH 7-24

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, Cur (kPa) ▲ PEAK SHEAR STRENGTH, Cu (kPa)					
			PL (%)		WATER CONTENT (%)		LL (%)					
GROUND SURFACE		0										
TOPSOIL 0.28m [90.17m]		0	SS 1	50	1-2-4-5 6	23.2				90		
Very stiff brown SILTY CLAY		1	SS 2	100	2-4-5-6 9	30.11				89		
		2	SS 3	100	1-1-2-2 3	33.87				88		
Dynamic Cone Penetration Test commenced at 2.13 m depth		2				30.88				87		
		3								86		
		4								85		
		5								84		
		6								83		
		7								82		
		8								81		
		9								80		
		10								79		
		11								78		
		12								77		
		13								76		

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**COORD. SYS.:** MTM ZONE 9      **EASTING:** 366749.06      **NORTHING:** 5017944.55      **ELEVATION:** 90.45

**PROJECT:** Project X Development      **FILE NO. :** PG5876

**BORINGS BY:** CME 55 Low Clearance Drill

**REMARKS:**      **DATE:** July 26, 2024      **HOLE NO. :** BH 7-24

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	△ REMOULDED SHEAR STRENGTH, Cur (kPa)	▲ PEAK SHEAR STRENGTH, Cu (kPa)	○ PL (%)			
							20	40	60			80
						WATER CONTENT (%)			LL (%)			
						20	40	60	80			
GROUND SURFACE		13									77	
		14									76	
		15									75	
		16									74	
		17									73	
		18									72	
		19									71	
		20									70	
20.19m [ 70.26m ]		21									69	
End of Borehole		22									68	
Cone pushed up to 15.34 m depth.		23									67	
Practical refusal to DCPT at 20.19 m depth.		24									66	
		25									65	
		26									65	

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COORD. SYS.: MTM ZONE 9      EASTING: 366712.80      NORTHING: 5017973.11      ELEVATION: 90.53

PROJECT: Project X Development      FILE NO.: **PG5876**

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: July 29, 2024      HOLE NO.: **BH 8-24**

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20    40    60    80				
							△ REMOULDED SHEAR STRENGTH, $C_{ur}$ (kPa)				
							▲ PEAK SHEAR STRENGTH, $C_u$ (kPa)				
		PL (%)		WATER CONTENT (%)		LL (%)					
		20    40    60    80		20    40    60    80		20    40    60    80					
GROUND SURFACE		0								90.53	
TOPSOIL 0.20m [90.33m]		0	SS 1	50	2-2-3-3 5	23.74					
Hard to very stiff, brown SILTY CLAY		1	SS 2	50	3-5-4-4 9	32.22				90	
		2	SS 3	60	3-2-3-3 5	45.79				89	
2.13m [88.40m]		2				26.74				88	
Dynamic Cone Penetration Test commenced at 2.13 m depth		3								87	
		4								86	
		5								85	
		6								84	
		7								83	
		8								82	
		9								81	
		10								80	
		11								79	
		12								78	
		13								78	

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**COORD. SYS.:** MTM ZONE 9      **EASTING:** 366712.80      **NORTHING:** 5017973.11      **ELEVATION:** 90.53

**PROJECT:** Project X Development      **FILE NO. :** PG5876

**BORINGS BY:** CME 55 Low Clearance Drill

**REMARKS:**      **DATE:** July 29, 2024      **HOLE NO. :** BH 8-24

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, Cur (kPa) ▲ PEAK SHEAR STRENGTH, Cu (kPa)					20
			PL (%)		WATER CONTENT (%)		LL (%)					
GROUND SURFACE												
		13									77	
		14									76	
		15									75	
		16									74	
		17									73	
		18									72	
		19									71	
		19.89m [ 70.64m ]									71	
End of Borehole		20									70	
Cone pushed up to 14.17 m depth. Practical refusal to DCPT at 19.89 m depth.		21									69	
		22									68	
		23									67	
		24									66	
		25									65	
		26									65	

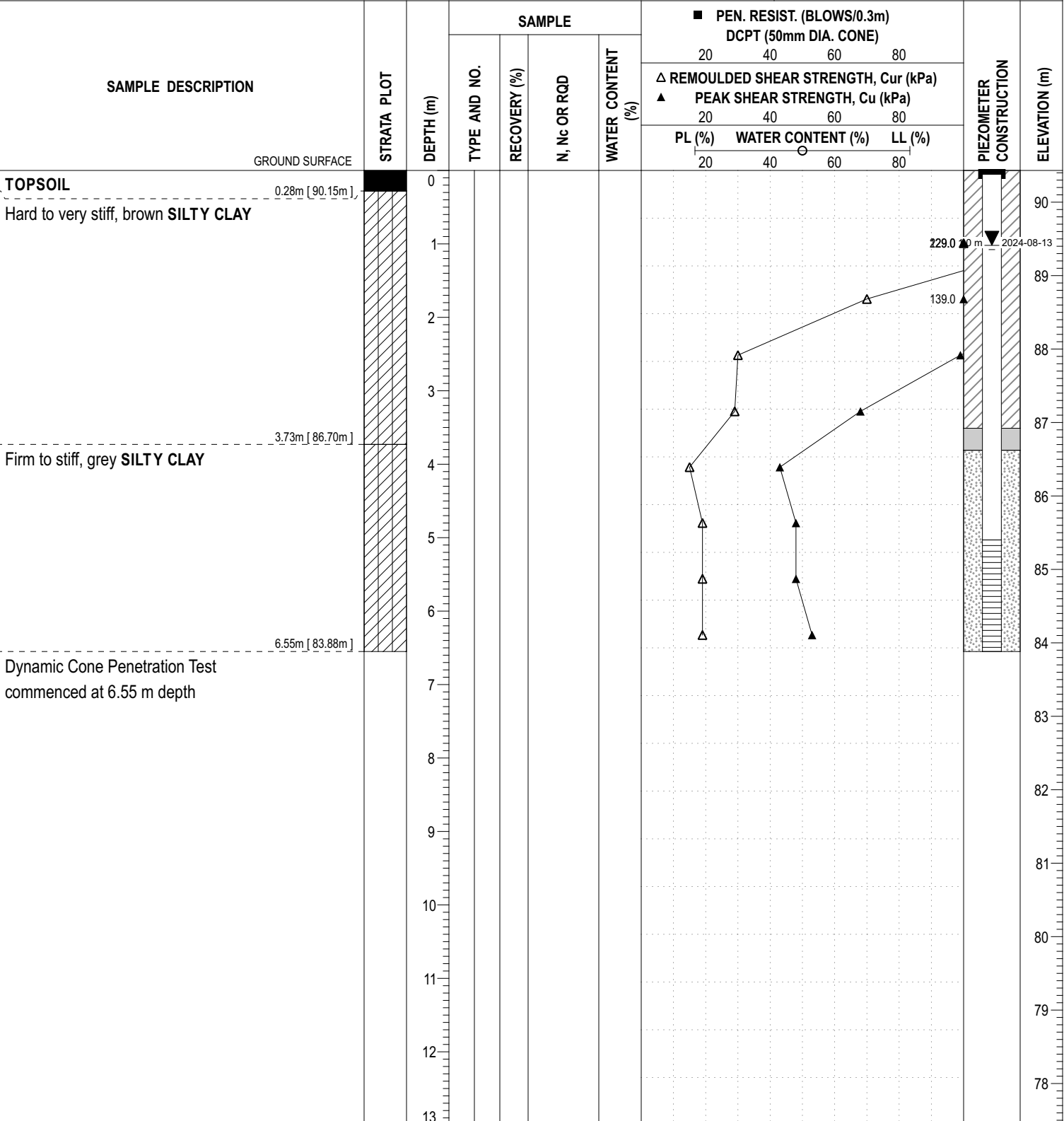
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COORD. SYS.: MTM ZONE 9      EASTING: 366708.14      NORTHING: 5018020.56      ELEVATION: 90.43

PROJECT: Project X Development      FILE NO.: **PG5876**

BORINGS BY: CME 55 Low Clearance Drill      HOLE NO.: **BH 9-24**

REMARKS:      DATE: July 29, 2024



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**COORD. SYS.:** MTM ZONE 9      **EASTING:** 366708.14      **NORTHING:** 5018020.56      **ELEVATION:** 90.43

**PROJECT:** Project X Development      **FILE NO. :** PG5876

**BORINGS BY:** CME 55 Low Clearance Drill

**REMARKS:**      **DATE:** July 29, 2024      **HOLE NO. :** BH 9-24

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, Cur (kPa) ▲ PEAK SHEAR STRENGTH, Cu (kPa)					
			PL (%)		WATER CONTENT (%)		LL (%)					
GROUND SURFACE												
		13									77	
		14									76	
		15									75	
		16									74	
		17									73	
		18									72	
		19									71	
		20									70	
		21									69	
End of Borehole		21.01m [ 69.42m ]									68	
Cone pushed up to 14.05 m depth. Practical refusal to DCPT at 21.01 m depth.											67	
(GWL at 1.02 m depth - August 13, 2024)											66	
											65	
											64	
											63	
											62	
											61	
											60	
											59	
											58	
											57	
											56	
											55	
											54	
											53	
											52	
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											30	
											29	
											28	
											27	
											26	

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**COORD. SYS.:** MTM ZONE 9      **EASTING:** 366626.06      **NORTHING:** 5017875.49      **ELEVATION:** 90.52

**PROJECT:** Project X Development      **FILE NO.:** PG5876

**BORINGS BY:** CME 55 Low Clearance Drill

**REMARKS:**      **DATE:** July 29, 2024      **HOLE NO.:** BH 10-24

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, Cur (kPa) ▲ PEAK SHEAR STRENGTH, Cu (kPa)					
			PL (%)		WATER CONTENT (%)		LL (%)					
GROUND SURFACE		0										
FILL: Brown silty sand, with crushed stone and gravel 0.08m [90.44m]		0	SS 1			3-6-4-3 10	8.57 31.55 22.85	○	○		90	
TOPSOIL 0.30m [90.22m]		1	SS 2	70		2-5-7-7 12	34.35		○		89	
Hard to very stiff, brown SILTY CLAY 2.13m [88.39m]		2	SS 3	100		2-3-3-3 6	29.1		○		88	
Dynamic Cone Penetration Test commenced at 2.13 m depth		3									87	
		4									86	
		5									85	
		6									84	
		7									83	
		8									82	
		9									81	
		10									80	
		11									79	
		12									78	
		13									78	

P:/AutoCAD Drawings/Test Hole Data Files/PG5876/data/sqlite 2024-09-10, 17:11 Paterson\_Template AA

**COORD. SYS.:** MTM ZONE 9      **EASTING:** 366626.06      **NORTHING:** 5017875.49      **ELEVATION:** 90.52

**PROJECT:** Project X Development      **FILE NO. :** PG5876

**BORINGS BY:** CME 55 Low Clearance Drill

**REMARKS:**      **DATE:** July 29, 2024      **HOLE NO. :** BH 10-24

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, $C_{ur}$ (kPa) ▲ PEAK SHEAR STRENGTH, $C_u$ (kPa)					
			PL (%)		WATER CONTENT (%)		LL (%)					
GROUND SURFACE		13								77		
		14								76		
		15								75		
		16								74		
		17								73		
		18								72		
		19								71		
		20								70		
		21								69		
		22								68		
		23								67		
		24								66		
		25								65		
		26								65		

22.68m [ 67.84m ]

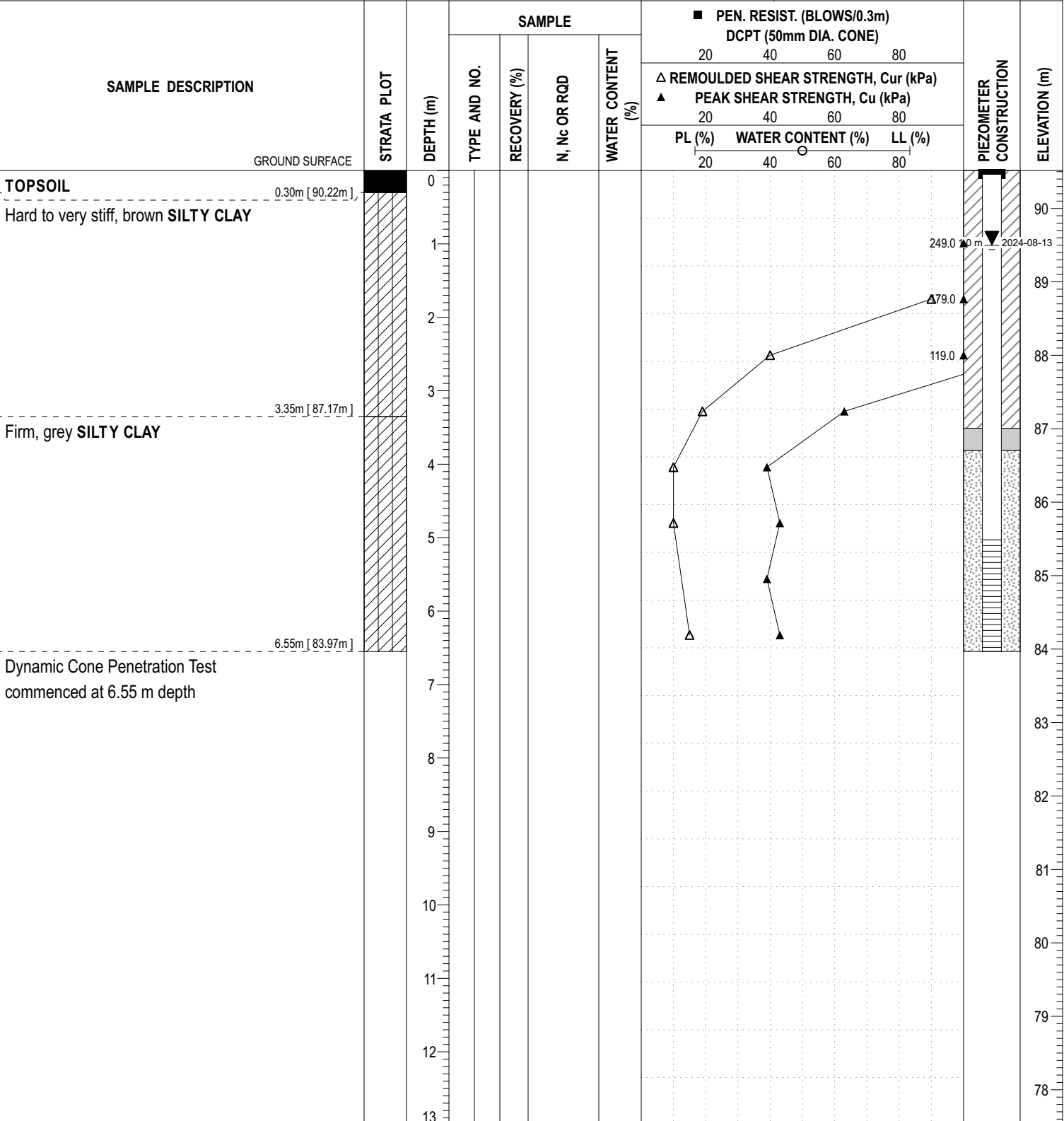
End of Borehole  
 Cone pushed up to 19.91 m depth.  
 Practical refusal to DCPT at 22.68 m depth.

COORD. SYS.: MTM ZONE 9      EASTING: 366567.02      NORTHING: 5017860.06      ELEVATION: 90.52

PROJECT: Project X Development      FILE NO.: **PG5876**

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: July 29, 2024      HOLE NO.: **BH 11-24**



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**COORD. SYS.:** MTM ZONE 9      **EASTING:** 366567.02      **NORTHING:** 5017860.06      **ELEVATION:** 90.52

**PROJECT:** Project X Development      **FILE NO. :** PG5876

**BORINGS BY:** CME 55 Low Clearance Drill

**REMARKS:**      **DATE:** July 29, 2024      **HOLE NO. :** BH 11-24

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, $C_{ur}$ (kPa) ▲ PEAK SHEAR STRENGTH, $C_u$ (kPa)					
			PL (%)	WATER CONTENT (%)	LL (%)							
GROUND SURFACE												
		13								77		
		14								76		
		15								75		
		16								74		
		17								73		
		18								72		
		19								71		
		20								70		
		21								69		
		22								68		
		23								67		
		24								66		
		25								65		
		26								65		

21.84m [ 68.68m ]

End of Borehole

Cone pushed up to 19.18 m depth.  
 Practical refusal to DCPT at 21.84 m depth.

(GWL at 1.02 m depth - August 13, 2024)

COORD. SYS.: MTM ZONE 9      EASTING: 366521.69      NORTHING: 5017840.31      ELEVATION: 90.53

PROJECT: Project X Development      FILE NO.: **PG5876**

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: July 29, 2024      HOLE NO.: **BH 12-24**

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, $C_{ur}$ (kPa) ▲ PEAK SHEAR STRENGTH, $C_u$ (kPa)					
			PL (%)		WATER CONTENT (%)		LL (%)					
GROUND SURFACE		0										
TOPSOIL 0.25m [90.28m]		0	SS 1	60	2-5-6-7 11	19.96						
Hard to very stiff, brown SILTY CLAY  2.13m [88.40m]	[Hatched Pattern]	1	SS 2	100	3-5-5-6 10	33.56						
		2	SS 3	100	1-2-2-3 4	38.05						
						36.41						
Dynamic Cone Penetration Test commenced at 2.13 m depth		3										
		4										
		5										
		6										
		7										
		8										
		9										
		10										
		11										
		12										
		13										

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**COORD. SYS.:** MTM ZONE 9      **EASTING:** 366521.69      **NORTHING:** 5017840.31      **ELEVATION:** 90.53

**PROJECT:** Project X Development      **FILE NO. :** PG5876

**BORINGS BY:** CME 55 Low Clearance Drill

**REMARKS:**      **DATE:** July 29, 2024      **HOLE NO. :** BH 12-24

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, $C_{ur}$ (kPa) ▲ PEAK SHEAR STRENGTH, $C_u$ (kPa)					
			PL (%)		WATER CONTENT (%)		LL (%)					
GROUND SURFACE		13								77		
		14								76		
		15								75		
		16								74		
		17								73		
		18								72		
		19								71		
		20								70		
End of Borehole		20								70		
		21								69		
		22								68		
		23								67		
		24								66		
		25								65		
		26								65		

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COORD. SYS.: MTM ZONE 9      EASTING: 366818.35      NORTHING: 5017939.97      ELEVATION: 90.57

PROJECT: Project X Development      FILE NO.: **PG5876**

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: July 30, 2024      HOLE NO.: **BH 13-24**

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, Cur (kPa) ▲ PEAK SHEAR STRENGTH, Cu (kPa)					
			PL (%)		WATER CONTENT (%)		LL (%)					
GROUND SURFACE		0										
TOPSOIL		0	SS 1	60	1-2-3-5	24.24						
Hard to very stiff, brown SILTY CLAY		1	SS 2	60	3-5-8-8	33.07				90		
		2	SS 3	100	2-2-3-2	34.29				89		
		2			5	32.03				88		
Dynamic Cone Penetration Test commenced at 2.13 m depth		3								87		
		4								86		
		5								85		
		6								84		
		7								83		
		8								82		
		9								81		
		10								80		
		11								79		
		12								78		
		13								78		

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**COORD. SYS.:** MTM ZONE 9      **EASTING:** 366818.35      **NORTHING:** 5017939.97      **ELEVATION:** 90.57

**PROJECT:** Project X Development      **FILE NO. :** PG5876

**BORINGS BY:** CME 55 Low Clearance Drill

**REMARKS:**      **DATE:** July 30, 2024      **HOLE NO. :** BH 13-24

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)					
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	△ REMOULDED SHEAR STRENGTH, $C_{ur}$ (kPa)	▲ PEAK SHEAR STRENGTH, $C_u$ (kPa)	○ PL (%)							
							20	40	60			80	20	40	60	80
							WATER CONTENT (%)					LL (%)				
GROUND SURFACE																
		13								77						
		14								76						
		15								75						
		16								74						
		17								73						
		18								72						
		19								71						
19.61m [ 70.96m ]		20								70						
End of Borehole		21								69						
Cone pushed up to 14.33 m depth.		22								68						
Practical refusal to DCPT at 19.61 m depth.		23								67						
		24								66						
		25								65						
		26								65						

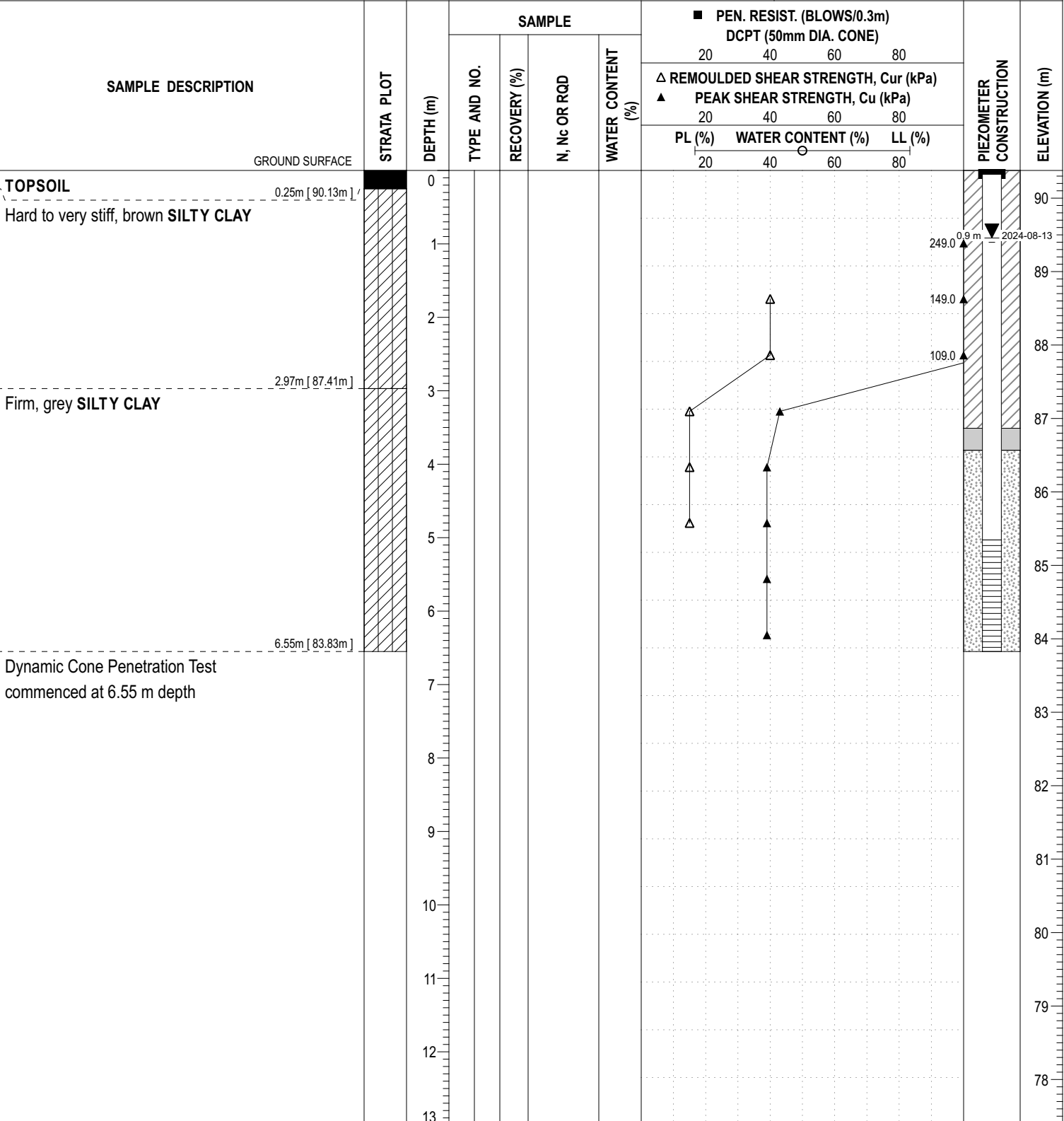
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COORD. SYS.: MTM ZONE 9      EASTING: 366739.01      NORTHING: 5017875.54      ELEVATION: 90.38

PROJECT: Project X Development      FILE NO.: **PG5876**

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: July 30, 2024      HOLE NO.: **BH 14-24**



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**COORD. SYS.:** MTM ZONE 9      **EASTING:** 366739.01      **NORTHING:** 5017875.54      **ELEVATION:** 90.38

**PROJECT:** Project X Development      **FILE NO. :** PG5876

**BORINGS BY:** CME 55 Low Clearance Drill

**REMARKS:**      **DATE:** July 30, 2024      **HOLE NO. :** BH 14-24

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, $C_{ur}$ (kPa)					
							▲ PEAK SHEAR STRENGTH, $C_u$ (kPa)					
PL (%)		WATER CONTENT (%)		LL (%)								
GROUND SURFACE		13								77		
		14								76		
		15								75		
		16								74		
		17								73		
		18								72		
		19								71		
End of Borehole		19.02m [ 71.36m ]								71		
Cone pushed up to 19.02 m depth. Practical refusal to DCPT at 14.63 m depth.		20								70		
(GWL at 0.92 m depth - August 13, 2024)		21								69		
		22								68		
		23								67		
		24								66		
		25								65		
		26								65		

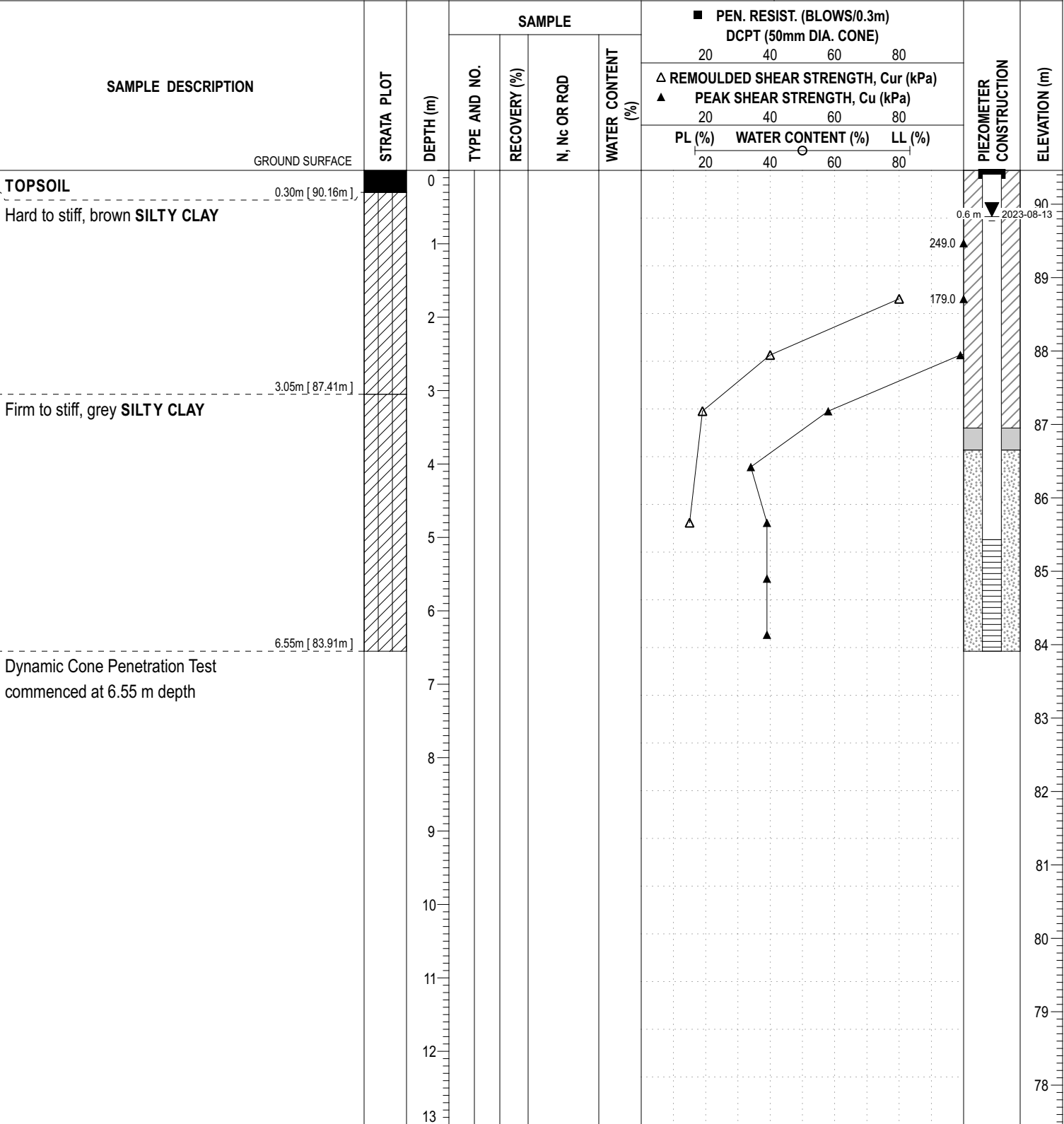
P:/AutoCAD Drawings/Test Hole Data Files/PG5876\data\splite 2024-09-10, 17:11 Paterson\_Template AA

COORD. SYS.: MTM ZONE 9      EASTING: 366681.92      NORTHING: 5017868.47      ELEVATION: 90.46

PROJECT: Project X Development      FILE NO.: **PG5876**

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: July 30, 2024      HOLE NO.: **BH 15-24**



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COORD. SYS.: MTM ZONE 9      EASTING: 366681.92      NORTHING: 5017868.47      ELEVATION: 90.46

PROJECT: Project X Development      FILE NO.: **PG5876**

BORINGS BY: CME 55 Low Clearance Drill      HOLE NO.: **BH 15-24**

REMARKS:      DATE: July 30, 2024

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, $C_{ur}$ (kPa)	▲ PEAK SHEAR STRENGTH, $C_u$ (kPa)	PL (%)			WATER CONTENT (%)
							20	40	60			80
GROUND SURFACE		13									77	
		14									76	
		15									75	
		16									74	
		17									73	
		18									72	
		19									71	
		20									70	
		21									69	
		22									68	
End of Borehole		22.00m [ 68.46m ]									68	
Cone pushed up to 15.24 m depth. Practical refusal to DCPT at 22.00 m depth.		23									67	
(GWL at 0.63 m depth - August 13, 2024)		24									66	
		25									65	
		26									65	

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**COORD. SYS.:** MTM ZONE 9      **EASTING:** 366608.67      **NORTHING:** 5017827.16      **ELEVATION:** 90.38

**PROJECT:** Project X Development      **FILE NO.:** PG5876

**BORINGS BY:** CME 55 Low Clearance Drill

**REMARKS:**      **DATE:** July 30, 2024      **HOLE NO.:** BH 16-24

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, $C_{ur}$ (kPa) ▲ PEAK SHEAR STRENGTH, $C_u$ (kPa)					
			PL (%)		WATER CONTENT (%)		LL (%)					
GROUND SURFACE		0										
TOPSOIL 0.25m [90.13m]		0	SS 1	60	1-3-3-6 6	29.64					90	
Very stiff, brown SILTY CLAY		1	SS 2	100	2-4-5-5 9	33.03					89	
2.13m [88.25m]		2	SS 3	100	1-2-2-2 4	38.36					88	
Dynamic Cone Penetration Test commenced at 2.13 m depth		3				34.04					87	
		4									86	
		5									85	
		6									84	
		7									83	
		8									82	
		9									81	
		10									80	
		11									79	
		12									78	
		13									78	

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**COORD. SYS.:** MTM ZONE 9      **EASTING:** 366608.67      **NORTHING:** 5017827.16      **ELEVATION:** 90.38

**PROJECT:** Project X Development      **FILE NO. :** PG5876

**BORINGS BY:** CME 55 Low Clearance Drill

**REMARKS:**      **DATE:** July 30, 2024      **HOLE NO. :** BH 16-24

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, $C_{ur}$ (kPa) ▲ PEAK SHEAR STRENGTH, $C_u$ (kPa)					
			PL (%)		WATER CONTENT (%)		LL (%)					
GROUND SURFACE		13								77		
		14								76		
		15								75		
		16								74		
		17								73		
		18								72		
		19								71		
		20								70		
		21								69		
End of Borehole		21								69		
Cone pushed up to 15.24 m depth.		22								68		
Practical refusal to DCPT at 21.18 m depth.		23								67		
		24								66		
		25								65		
		26								65		

21.18m [ 69.20m ]

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**COORD. SYS.:** MTM ZONE 9      **EASTING:** 366552.75      **NORTHING:** 5017783.74      **ELEVATION:** 90.29

**PROJECT:** Project X Development      **FILE NO.:** PG5876

**BORINGS BY:** CME 55 Low Clearance Drill

**REMARKS:**      **DATE:** July 30, 2024      **HOLE NO.:** BH 17-24

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, $C_{ur}$ (kPa) ▲ PEAK SHEAR STRENGTH, $C_u$ (kPa)					
			PL (%)		WATER CONTENT (%)		LL (%)					
GROUND SURFACE		0									90	
<b>TOPSOIL</b> Very stiff, brown <b>SILTY CLAY</b>		0	SS 1	70	1-2-3-3 5	33.35						90
		1	SS 2	100	3-4-5-5 9	37.61						89
		2	SS 3	100	2-2-3-3 5	35.13						88
Dynamic Cone Penetration Test commenced at 2.13 m depth		2.13										88
		3										87
		4										86
		5										85
		6										84
		7										83
		8										82
		9										81
		10										80
		11										79
		12										78
		13										78

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**COORD. SYS.:** MTM ZONE 9      **EASTING:** 366552.75      **NORTHING:** 5017783.74      **ELEVATION:** 90.29

**PROJECT:** Project X Development      **FILE NO. :** PG5876

**BORINGS BY:** CME 55 Low Clearance Drill

**REMARKS:**      **DATE:** July 30, 2024      **HOLE NO. :** BH 17-24

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, Cur (kPa) ▲ PEAK SHEAR STRENGTH, Cu (kPa)					20
			PL (%)		WATER CONTENT (%)		LL (%)					
GROUND SURFACE												
		13									77	
		14									76	
		15									75	
		16									74	
		17									73	
		18									72	
		19									71	
		20									70	
End of Borehole		20									70	
Cone pushed up to 15.24 m depth. Practical refusal to DCPT at 19.86 m depth.		21									69	
		22									68	
		23									67	
		24									66	
		25									65	
		26									65	

19.86m [ 70.43m ]

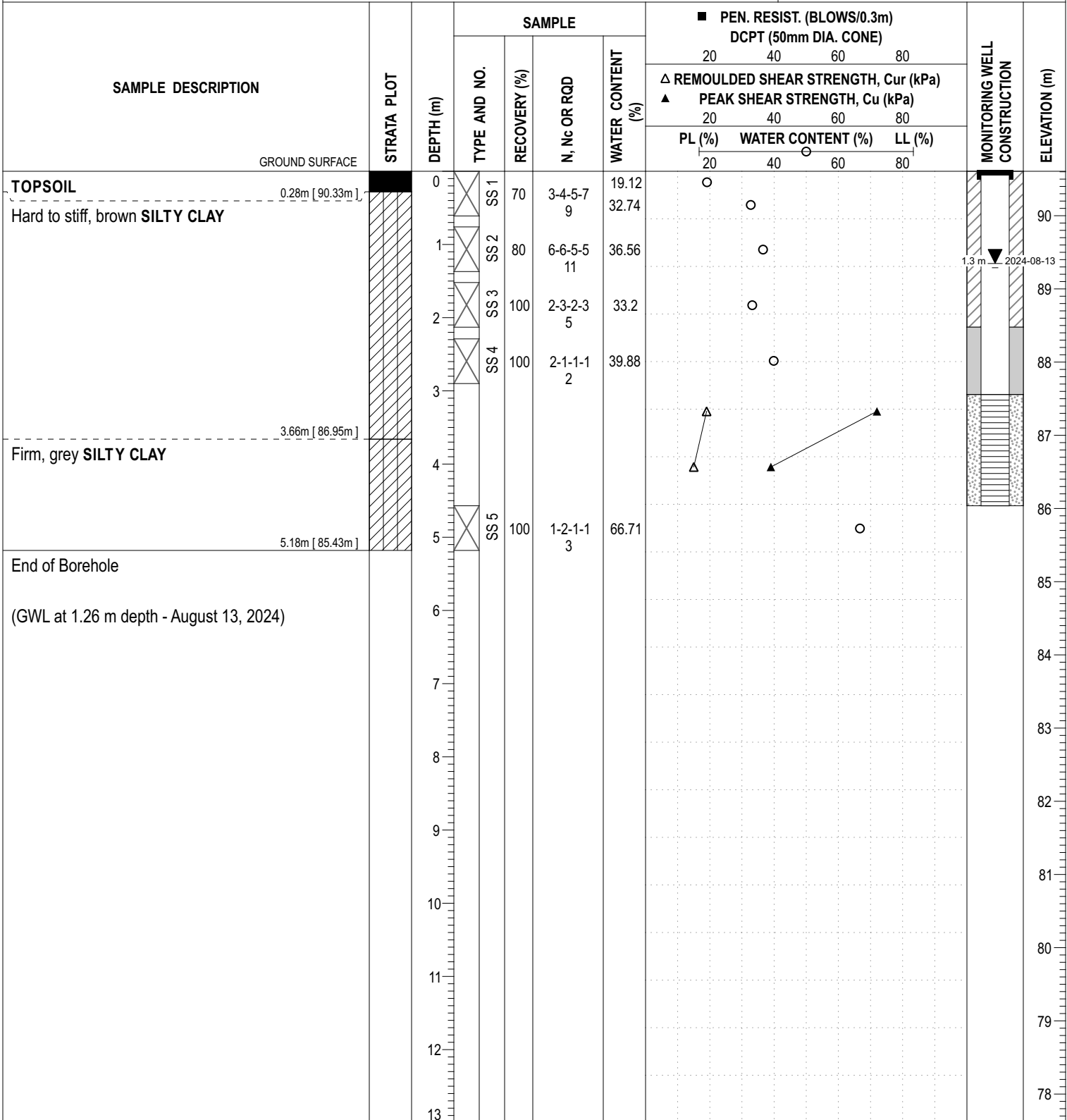
P:/AutoCAD Drawings/Test Hole Data Files/PG5876/data/sqlite 2024-09-10, 17:11 Paterson\_Template AA

**COORD. SYS.:** MTM ZONE 9      **EASTING:** 366298.58      **NORTHING:** 5017778.70      **ELEVATION:** 90.61

**PROJECT:** Project X Development      **FILE NO.:** PG5876

**BORINGS BY:** CME 55 Low Clearance Drill

**REMARKS:**      **DATE:** July 31, 2024      **HOLE NO.:** BH 18-24

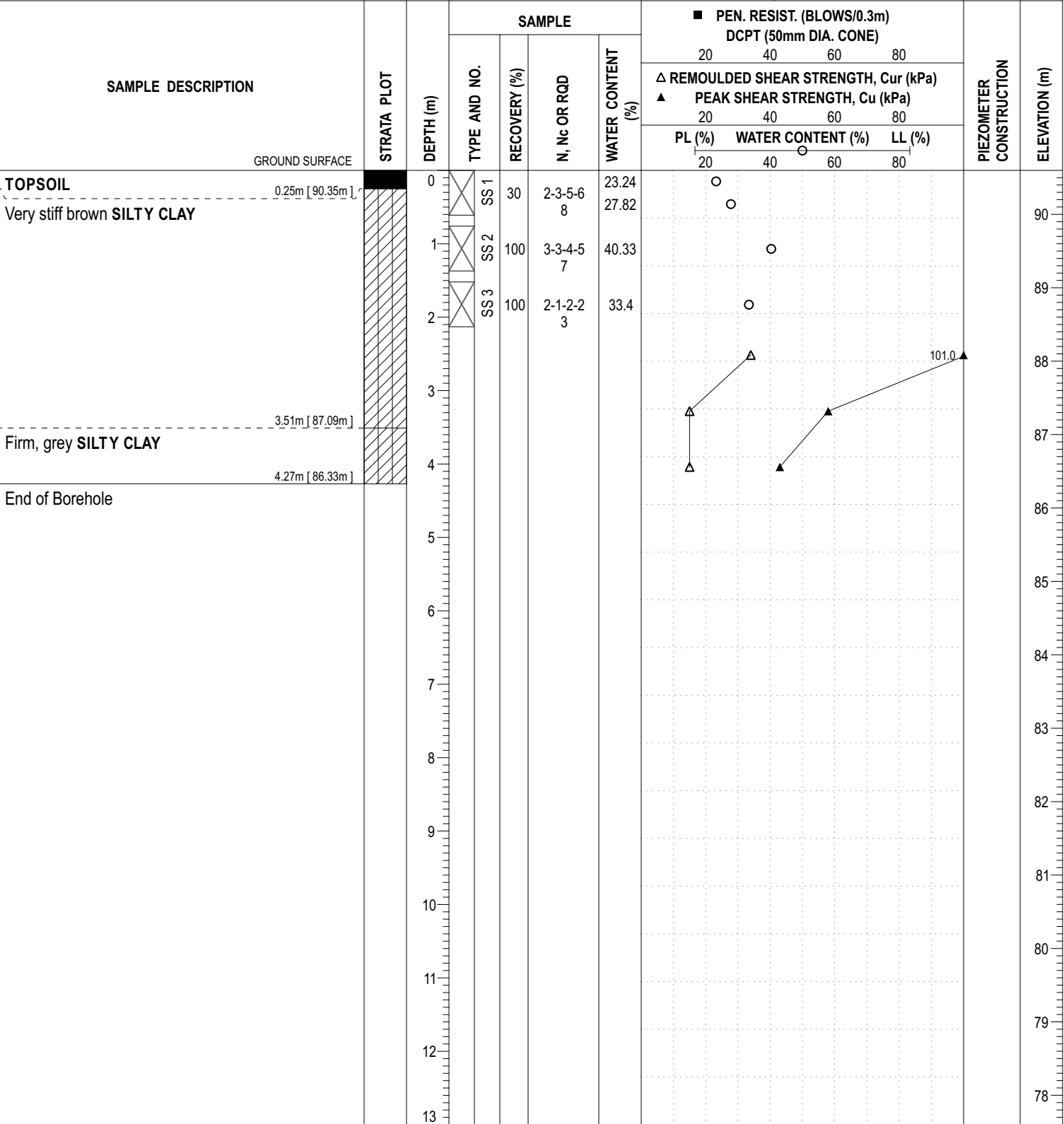


COORD. SYS.: MTM ZONE 9      EASTING: 366342.71      NORTHING: 5017902.32      ELEVATION: 90.60

PROJECT: Project X Development      FILE NO.: **PG5876**

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: July 31, 2024      HOLE NO.: **BH 19-24**



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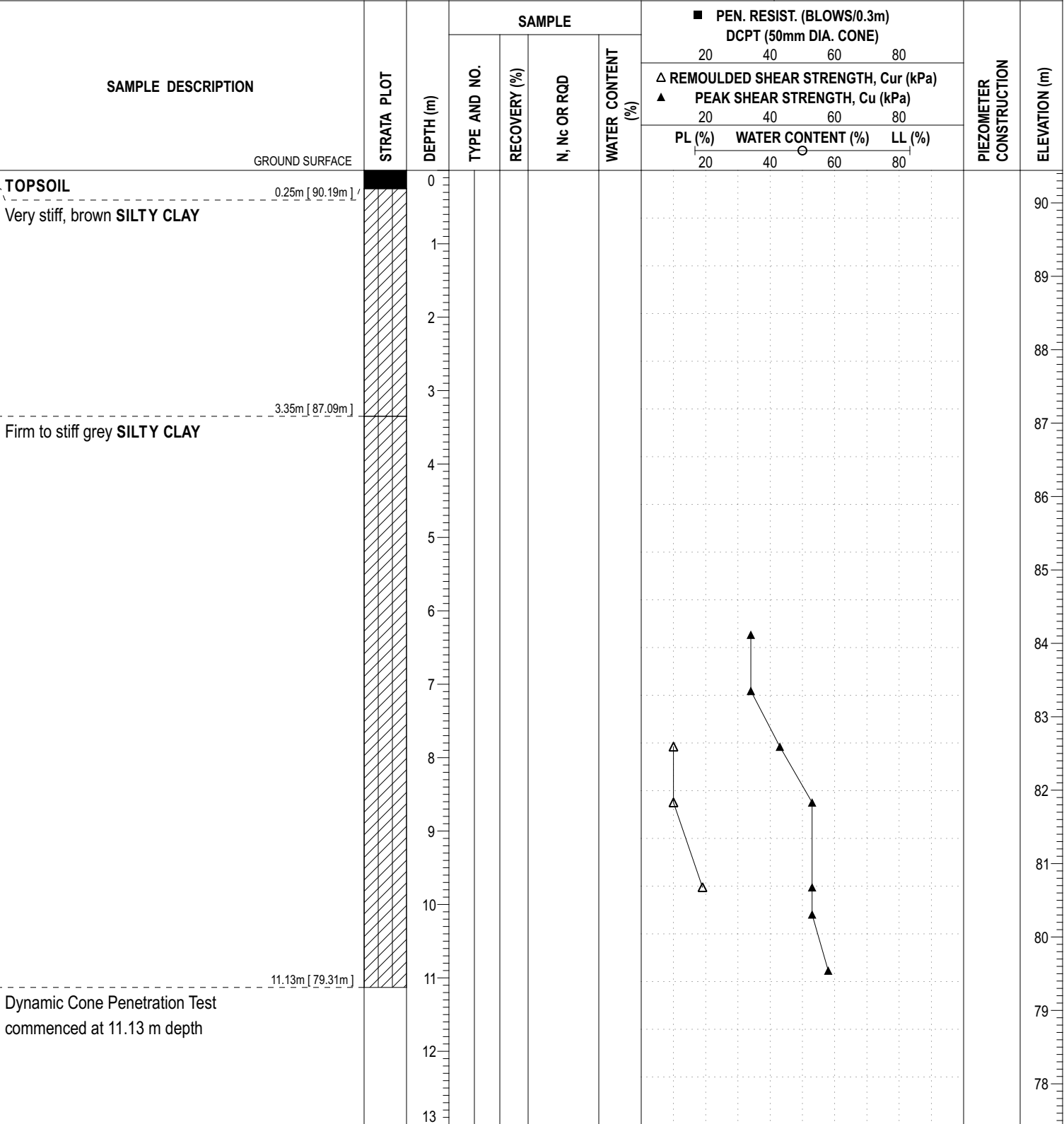
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COORD. SYS.: MTM ZONE 9      EASTING: 366496.91      NORTHING: 5017771.92      ELEVATION: 90.44

PROJECT: Project X Development      FILE NO.: **PG5876**

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: July 31, 2024      HOLE NO.: **BH 20-24**



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COORD. SYS.: MTM ZONE 9      EASTING: 366496.91      NORTHING: 5017771.92      ELEVATION: 90.44

PROJECT: Project X Development      FILE NO.: PG5876

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: July 31, 2024      HOLE NO.: BH 20-24

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, $C_{ur}$ (kPa)					
							▲ PEAK SHEAR STRENGTH, $C_u$ (kPa)					
PL (%)		WATER CONTENT (%)		LL (%)								
GROUND SURFACE		13								77		
		14								76		
		15								75		
		16								74		
		17								73		
		18								72		
		19								71		
		20								70		
20.35m [ 70.09m ]												
End of Borehole		21								69		
Cone pushed up to 17.37 m depth.		22								68		
Practical refusal to DCPT at 20.35 m depth.		23								67		
		24								66		
		25								65		
		26								65		

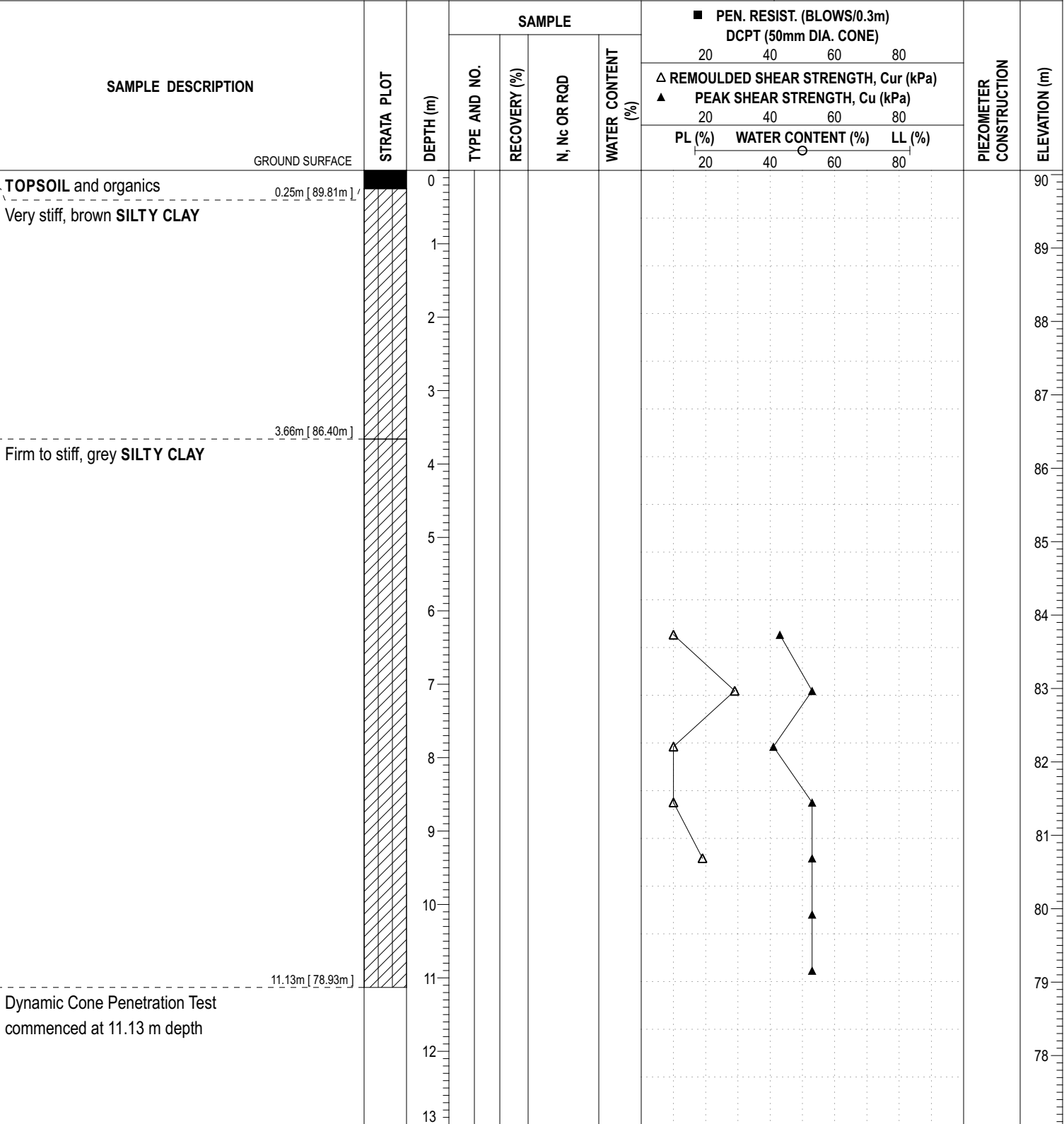
P:/AutoCAD Drawings/Test Hole Data Files/PG5876\data\splite 2024-09-10, 17:11 Paterson\_Template AA

COORD. SYS.: MTM ZONE 9      EASTING: 366644.01      NORTHING: 5017774.89      ELEVATION: 90.06

PROJECT: Project X Development      FILE NO.: PG5876

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: August 01, 2024      HOLE NO.: BH 21-24



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COORD. SYS.: MTM ZONE 9      EASTING: 366644.01      NORTHING: 5017774.89      ELEVATION: 90.06

PROJECT: Project X Development      FILE NO. : PG5876

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: August 01, 2024      HOLE NO. : BH 21-24

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, $C_{ur}$ (kPa) ▲ PEAK SHEAR STRENGTH, $C_u$ (kPa)					
			PL (%)		WATER CONTENT (%)		LL (%)					
GROUND SURFACE												
		13									77	
		14									76	
		15									75	
		16									74	
		17									73	
		18									72	
		19									71	
		20									70	
20.45m [ 69.61m ]												
End of Borehole												
Cone pushed up to 14.17 m depth. Practical refusal to DCPT at 20.45 m depth.												
		21									69	
		22									68	
		23									67	
		24									66	
		25									65	
		26									65	

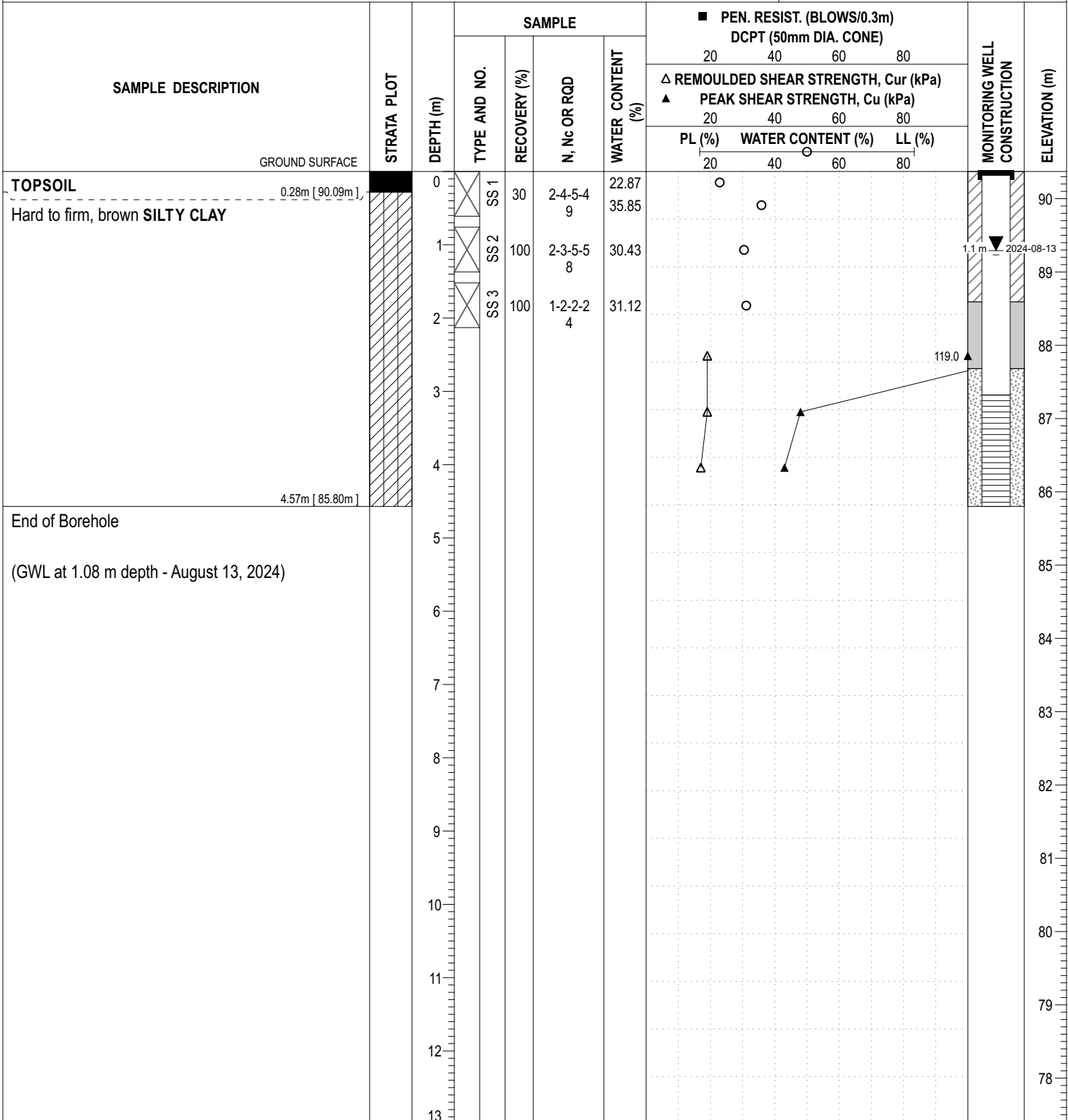
P:/AutoCAD Drawings/Test Hole Data Files/PG5876\data\sqliite 2024-09-10, 17:11 Paterson\_Template AA

COORD. SYS.: MTM ZONE 9      EASTING: 366590.72      NORTHING: 5017655.28      ELEVATION: 90.37

PROJECT: Project X Development      FILE NO.: **PG5876**

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: August 01, 2024      HOLE NO.: **BH 22-24**

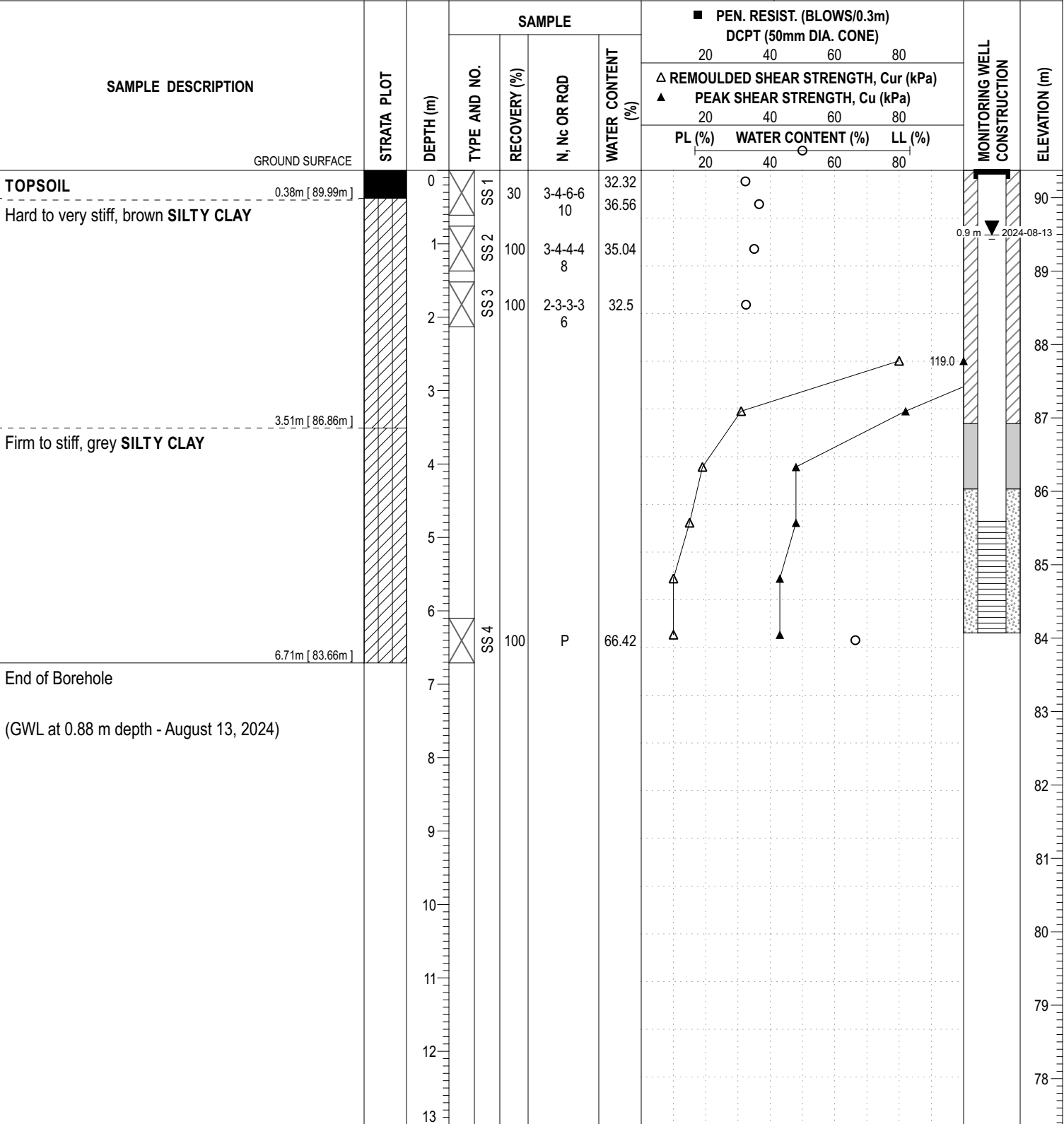


COORD. SYS.: MTM ZONE 9      EASTING: 366775.72      NORTHING: 5017808.64      ELEVATION: 90.37

PROJECT: Project X Development      FILE NO.: PG5876

BORINGS BY: CME 55 Low Clearance Drill      HOLE NO.: BH 23-24

REMARKS:      DATE: August 01, 2024



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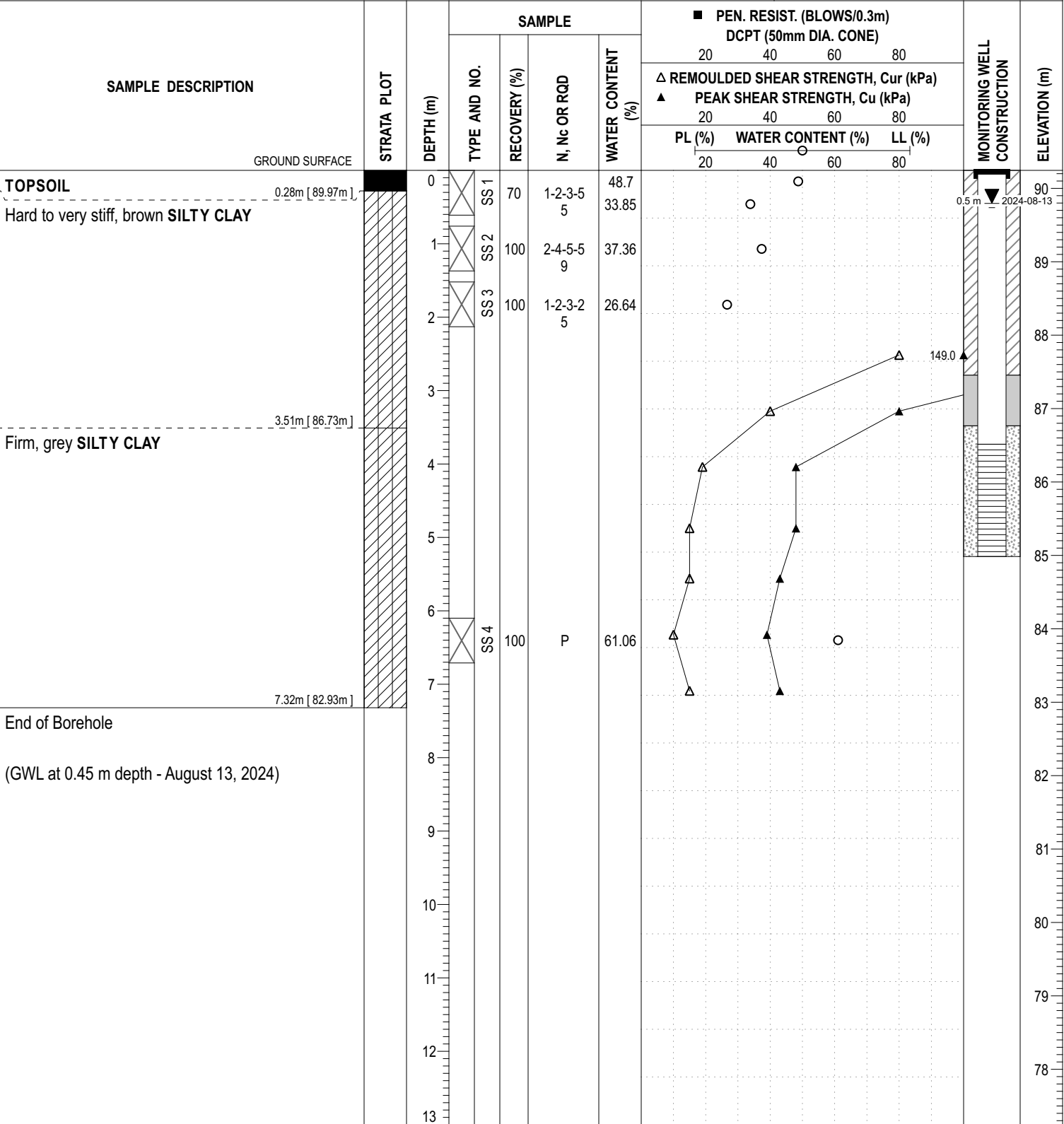
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COORD. SYS.: MTM ZONE 9      EASTING: 366832.58      NORTHING: 5017838.09      ELEVATION: 90.25

PROJECT: Project X Development      FILE NO.: **PG5876**

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: August 02, 2024      HOLE NO.: **BH 24-24**



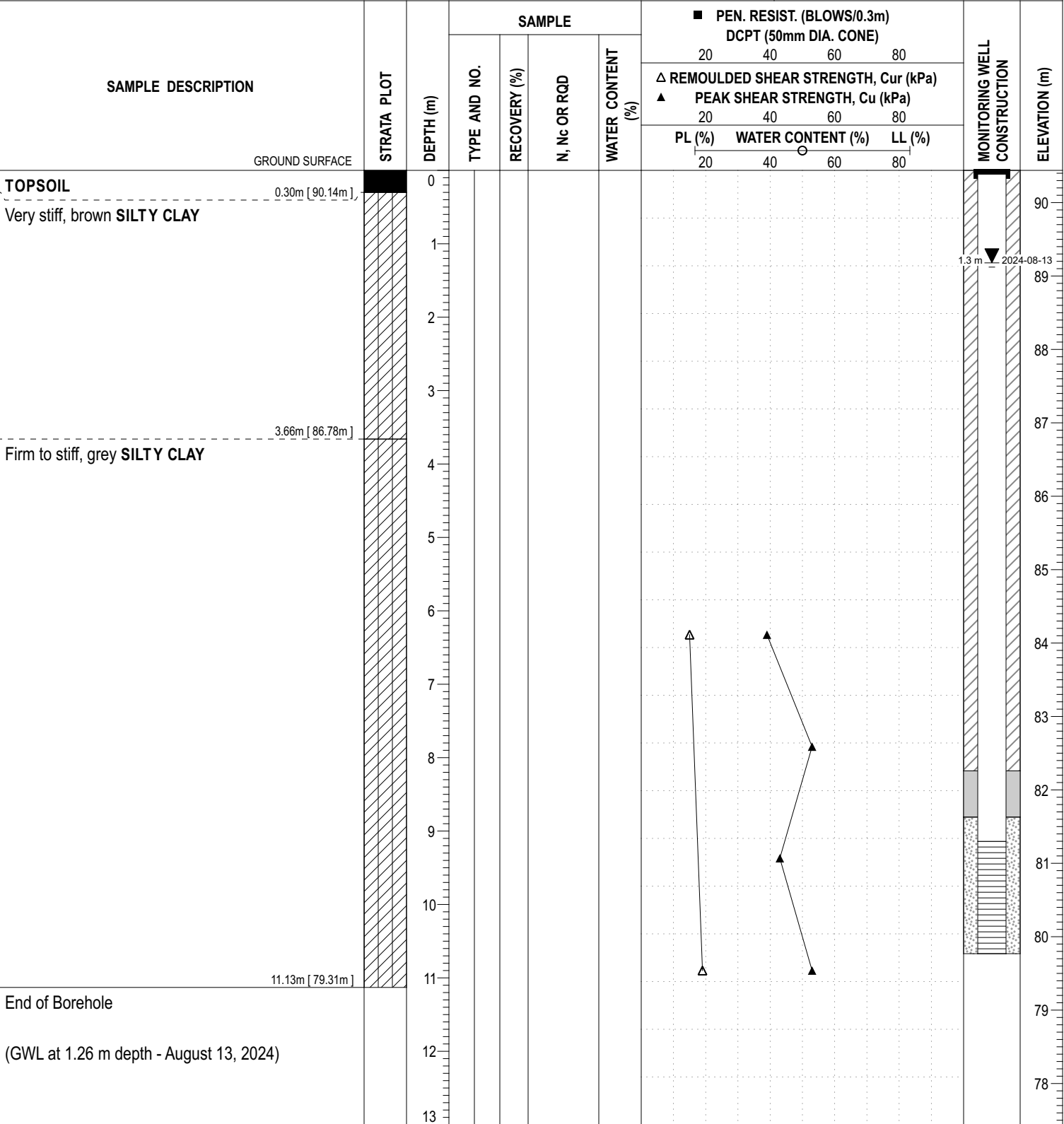
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COORD. SYS.: MTM ZONE 9      EASTING: 366792.13      NORTHING: 5017856.33      ELEVATION: 90.44

PROJECT: Project X Development      FILE NO.: **PG5876**

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: August 02, 2024      HOLE NO.: **BH 25-24**



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COORD. SYS.: MTM ZONE 9      EASTING: 366921.89      NORTHING: 5017932.86      ELEVATION: 90.32

PROJECT: Project X Development      FILE NO. : PG5876

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: August 02, 2024      HOLE NO. : BH 26-24

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, $C_{ur}$ (kPa) ▲ PEAK SHEAR STRENGTH, $C_u$ (kPa)					
			PL (%)	WATER CONTENT (%)	LL (%)							
GROUND SURFACE		0								90		
TOPSOIL		0										
0.25m [ 90.07m ]		0.25										
Hard to very stiff, brown SILTY CLAY		0.25 - 3.66										
3.66m [ 86.66m ]		3.66										
Firm to stiff, grey SILTY CLAY		3.66 - 11.89										
11.89m [ 78.43m ]		11.89										
End of Borehole		11.89										

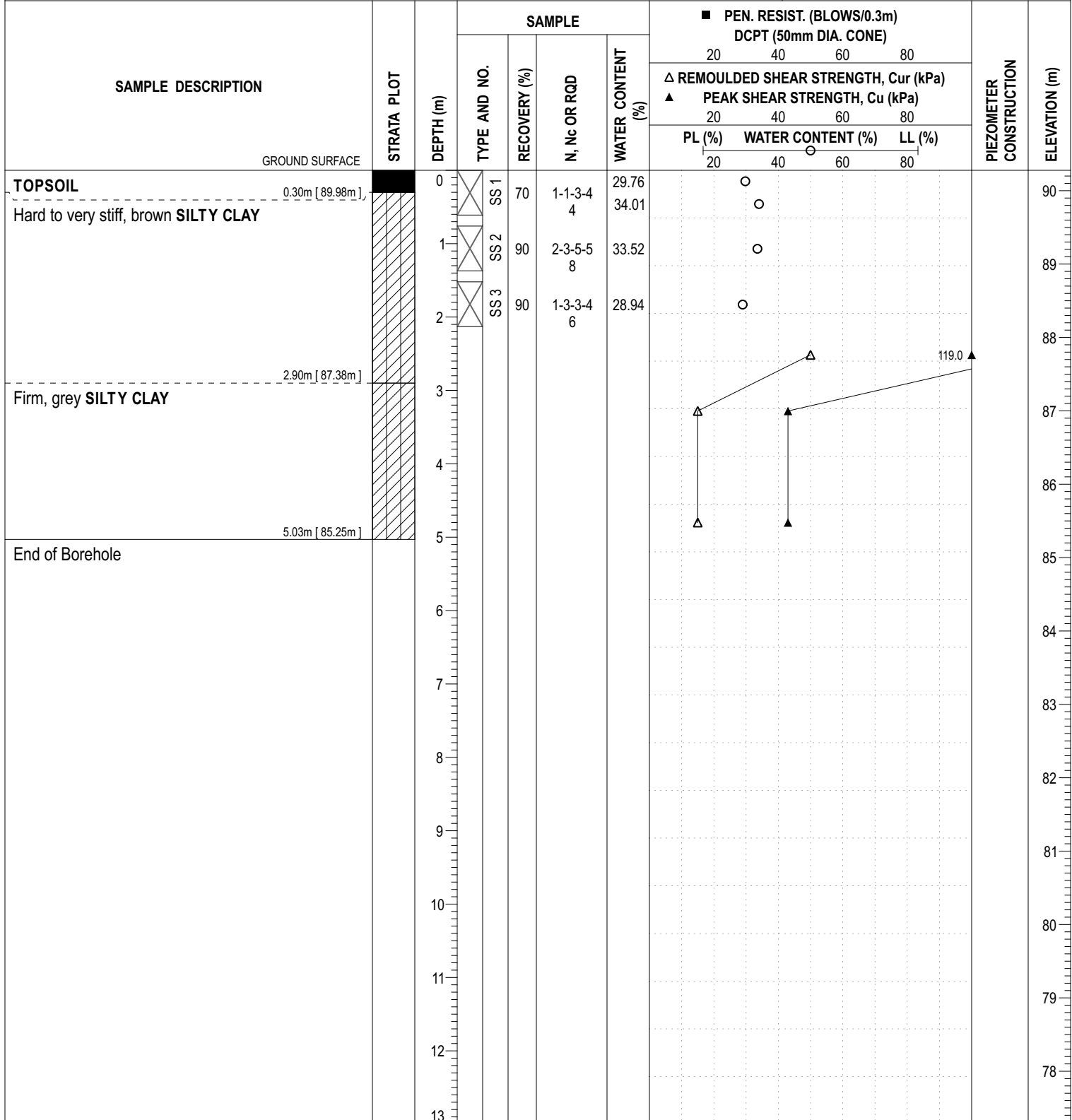
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COORD. SYS.: MTM ZONE 9      EASTING: 366935.39      NORTHING: 5017999.30      ELEVATION: 90.28

PROJECT: Project X Development      FILE NO.: **PG5876**

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: August 06, 2024      HOLE NO.: **BH 27-24**



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COORD. SYS.: MTM ZONE 9      EASTING: 366899.03      NORTHING: 5018108.15      ELEVATION: 90.59

PROJECT: Project X Development      FILE NO.: **PG5876**

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: August 06, 2024      HOLE NO.: **BH 28-24**

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, $C_{ur}$ (kPa)					
							▲ PEAK SHEAR STRENGTH, $C_u$ (kPa)					
PL (%)		WATER CONTENT (%)		LL (%)								
GROUND SURFACE		0										
<b>TOPSOIL</b> 0.25m [90.34m]		0	SS 1	50	3-6-7-8 13	25.63				90		
Hard to very stiff, brown <b>SILTY CLAY</b>		1	SS 2	100	2-3-4-4 7	27.78				89		
		2	SS 3	100	1-1-1-2 2	39.72				88		
		3				36.02				87		
3.05m [87.54m]		3								86		
Firm, grey <b>SILTY CLAY</b>		4								85		
		5								84		
5.03m [85.56m]		5								83		
End of Borehole		6								82		
		7								81		
		8								80		
		9								79		
		10								78		
		11										
		12										
		13										

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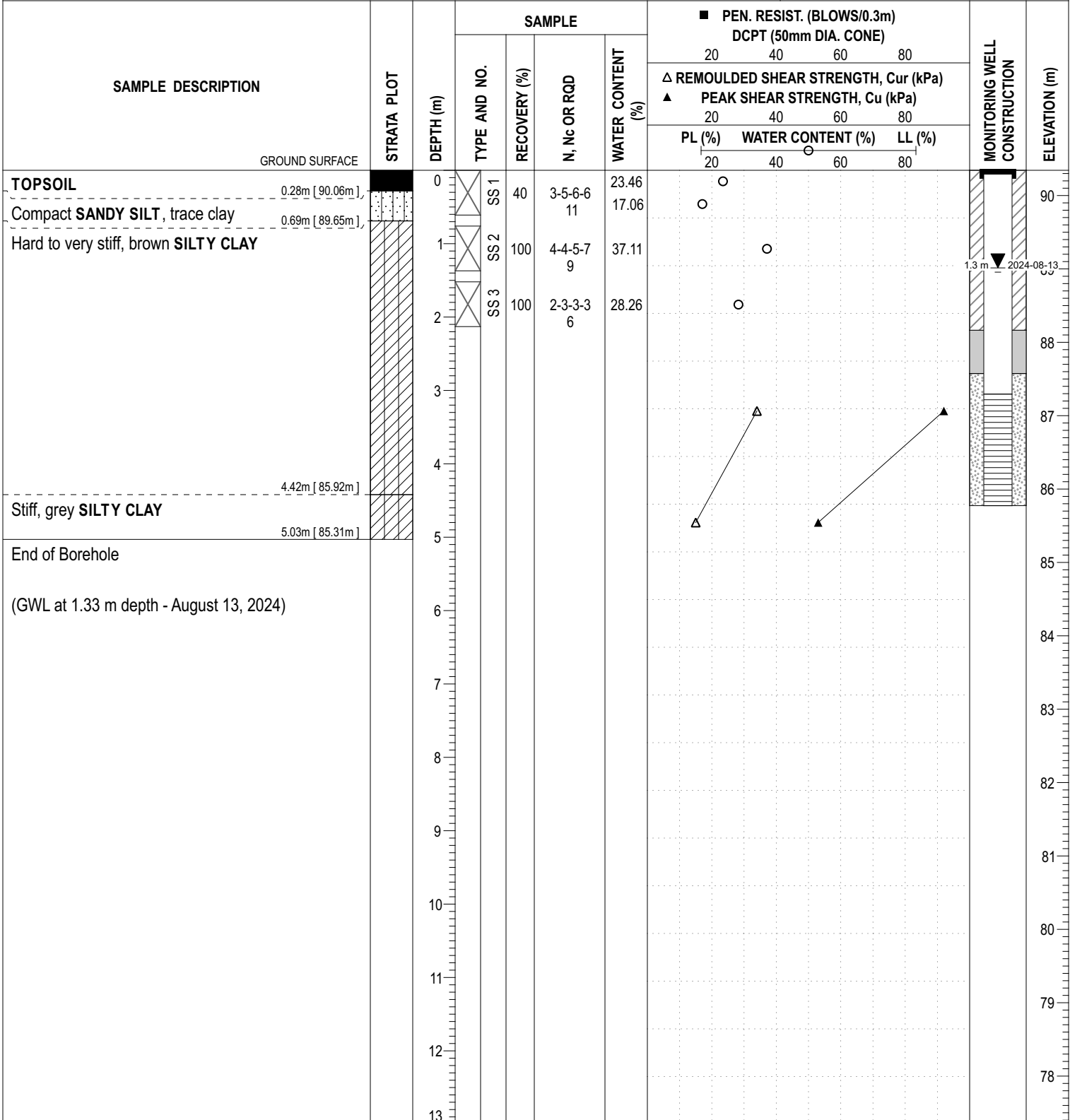


**COORD. SYS.:** MTM ZONE 9      **EASTING:** 366989.29      **NORTHING:** 5018132.77      **ELEVATION:** 90.34

**PROJECT:** Project X Development      **FILE NO.:** PG5876

**BORINGS BY:** CME 55 Low Clearance Drill

**REMARKS:**      **DATE:** August 06, 2024      **HOLE NO.:** BH 29-24



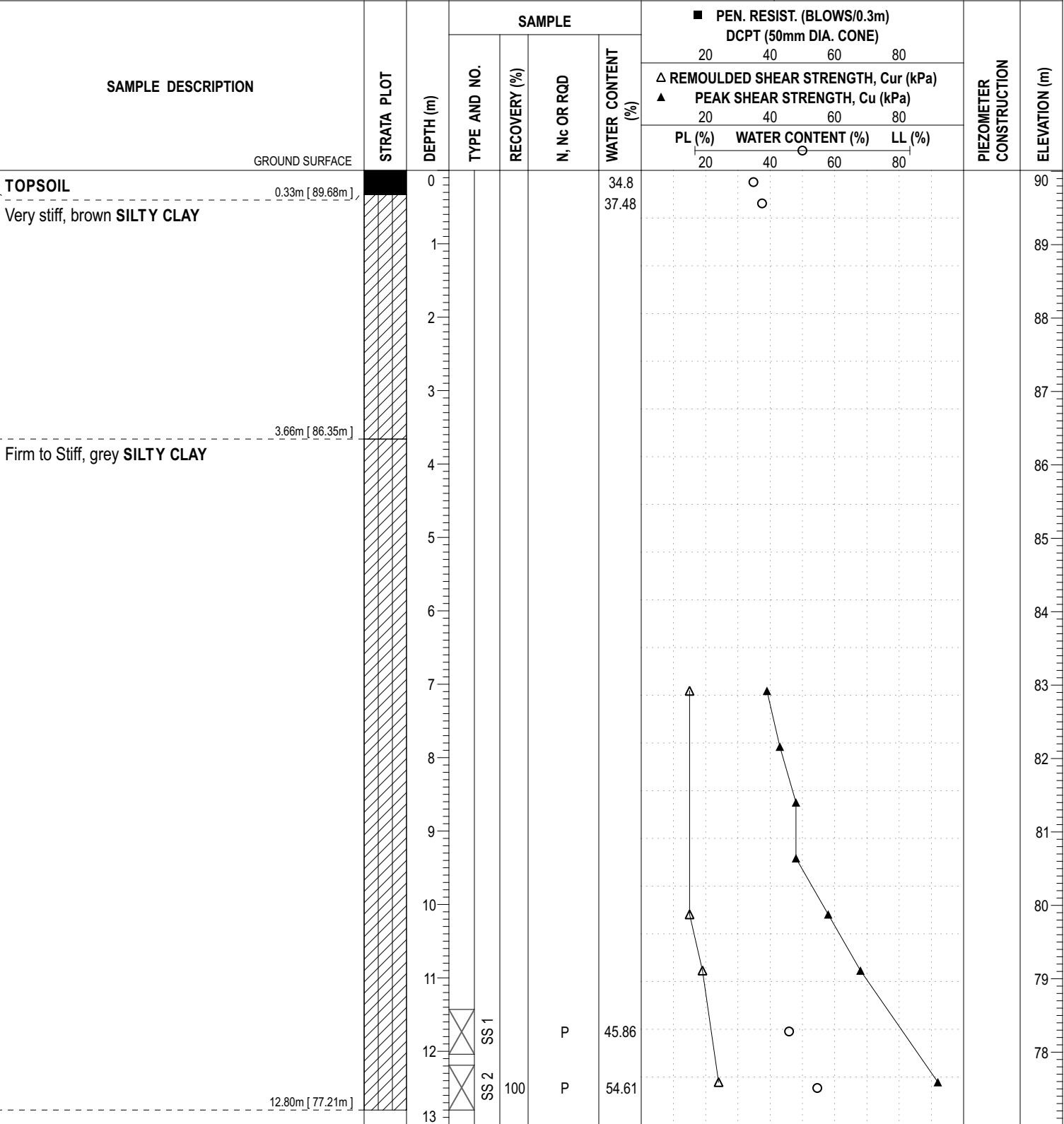
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COORD. SYS.: MTM ZONE 9      EASTING: 367033.99      NORTHING: 5017996.72      ELEVATION: 90.01

PROJECT: Project X Development      FILE NO.: PG5876

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: August 06, 2024      HOLE NO.: BH 30-24



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**COORD. SYS.:** MTM ZONE 9      **EASTING:** 367033.99      **NORTHING:** 5017996.72      **ELEVATION:** 90.01

**PROJECT:** Project X Development      **FILE NO. :** PG5876

**BORINGS BY:** CME 55 Low Clearance Drill

**REMARKS:**      **DATE:** August 06, 2024      **HOLE NO. :** BH 30-24

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, $C_{ur}$ (kPa) ▲ PEAK SHEAR STRENGTH, $C_u$ (kPa)					
			PL (%)	WATER CONTENT (%)		LL (%)						
GROUND SURFACE												
Dynamic Cone Penetration Test commenced at 12.8 m depth		13									77	
		14									76	
		15									75	
		16									74	
		17									73	
		18									72	
		19									71	
		20									70	
		21									69	
21.44m [ 68.57m ]												
End of Borehole		22									68	
Cone pushed up to 19.91 m depth.		23									67	
Practical refusal to DCPT at 21.44 m depth.		24									66	
		25									65	
		26									65	

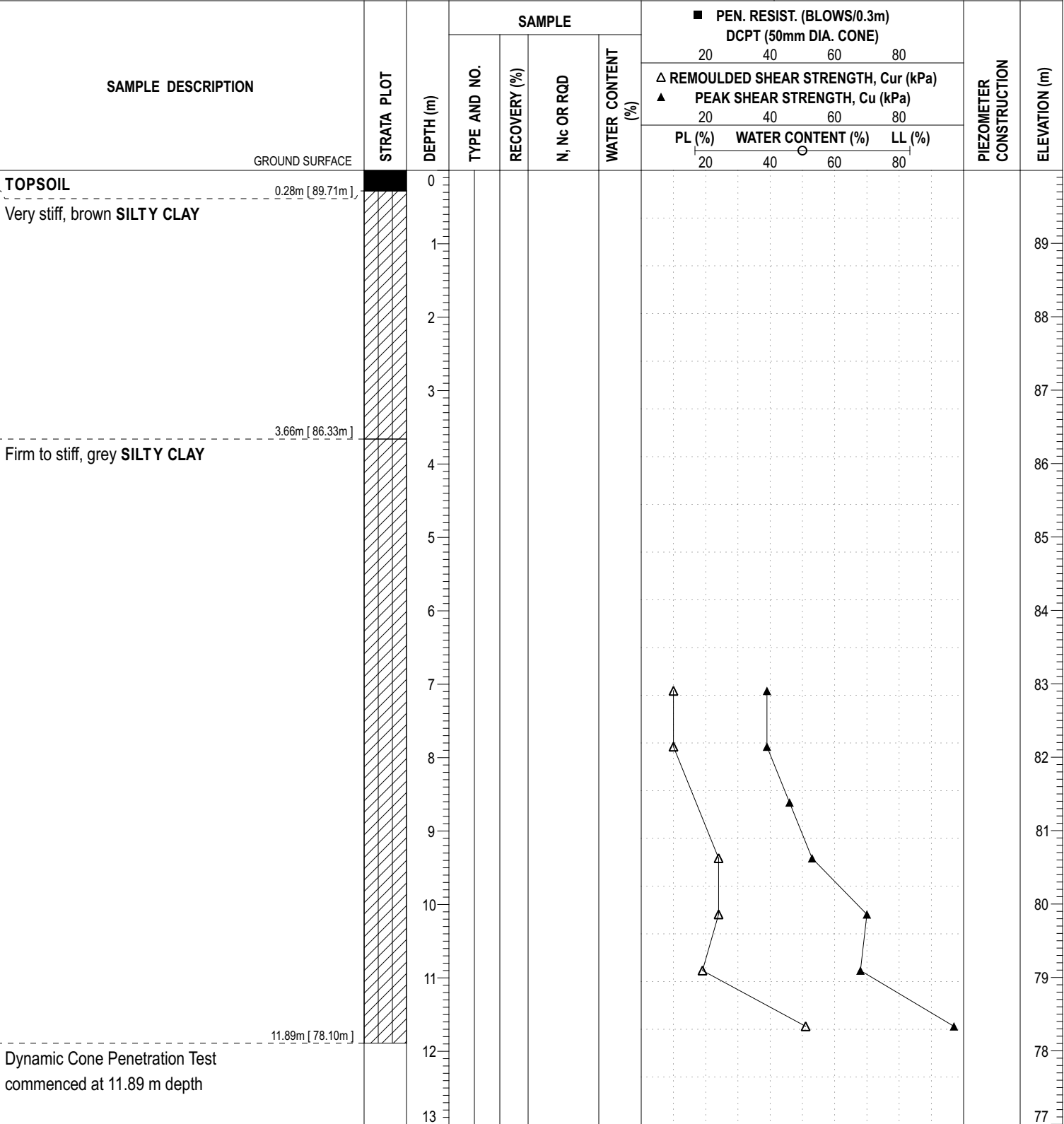
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COORD. SYS.: MTM ZONE 9      EASTING: 367067.25      NORTHING: 5018068.19      ELEVATION: 89.99

PROJECT: Project X Development      FILE NO.: **PG5876**

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: August 07, 2024      HOLE NO.: **BH 31-24**



P:\AutoCAD Drawings\Test Hole Data Files\PG5876\data\splite 2024-09-10, 17:11 Paterson\_Template AA

**COORD. SYS.:** MTM ZONE 9      **EASTING:** 367067.25      **NORTHING:** 5018068.19      **ELEVATION:** 89.99

**PROJECT:** Project X Development      **FILE NO. :** PG5876

**BORINGS BY:** CME 55 Low Clearance Drill

**REMARKS:**      **DATE:** August 07, 2024      **HOLE NO. :** BH 31-24

SAMPLE DESCRIPTION	STRATA PLOT	DEPTH (m)	SAMPLE				■ PEN. RESIST. (BLOWS/0.3m) DCPT (50mm DIA. CONE)			PIEZOMETER CONSTRUCTION	ELEVATION (m)	
			TYPE AND NO.	RECOVERY (%)	N, Nc OR RQD	WATER CONTENT (%)	20	40	60			80
							△ REMOULDED SHEAR STRENGTH, $C_{ur}$ (kPa)					
			▲ PEAK SHEAR STRENGTH, $C_u$ (kPa)				20	40	60			80
				PL (%)	WATER CONTENT (%)		LL (%)					
GROUND SURFACE												
		13										
		14									76	
		15									75	
		16									74	
		17									73	
		18									72	
		18.90m [ 71.09m ]									71	
End of Borehole		19									71	
Cone pushed up to 18.85 m depth. Practical refusal to DCPT at 18.90 m depth.		20									70	
		21									69	
		22									68	
		23									67	
		24									66	
		25									65	
		26									64	

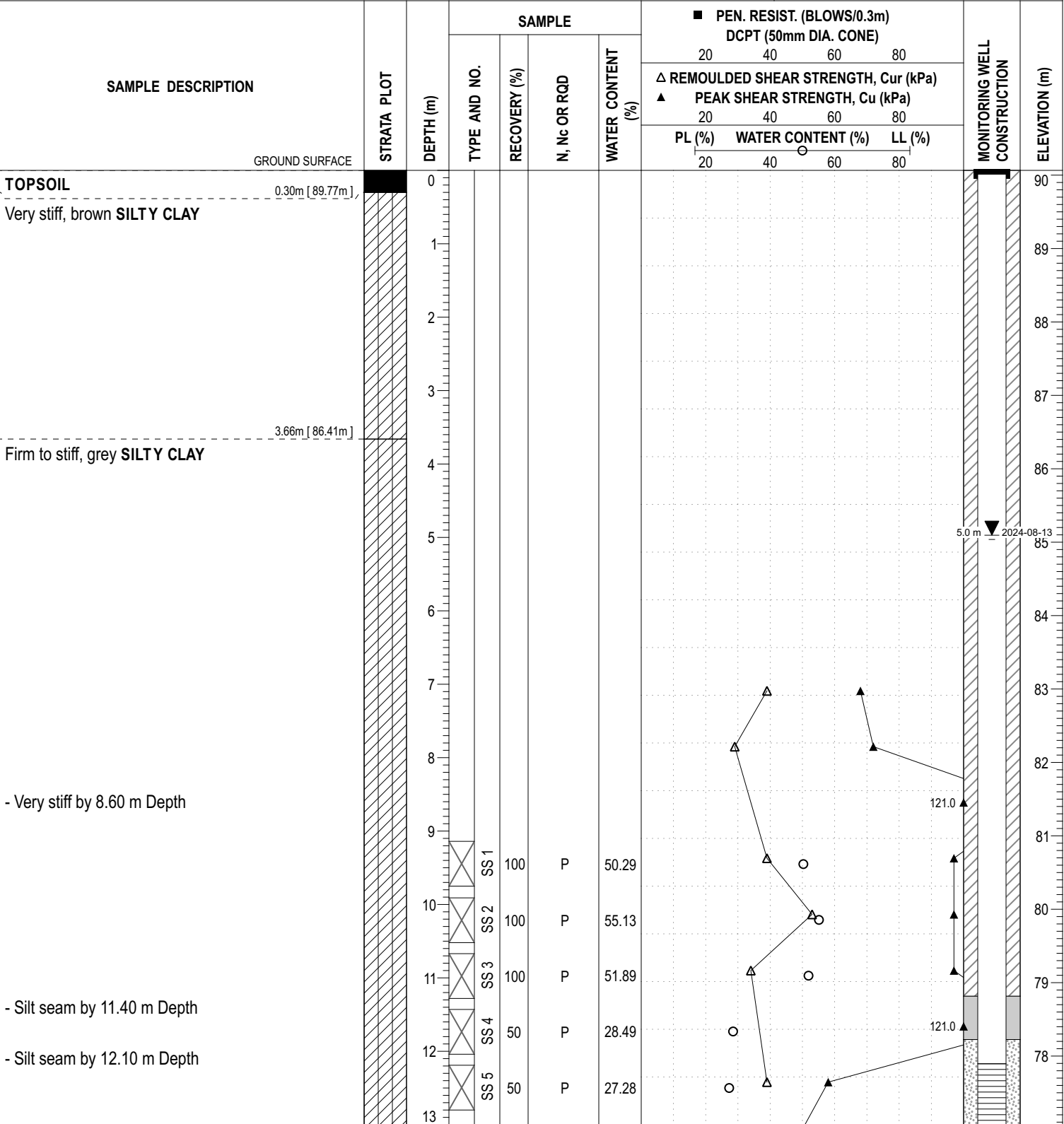
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COORD. SYS.: MTM ZONE 9      EASTING: 367157.38      NORTHING: 5018138.45      ELEVATION: 90.06

PROJECT: Project X Development      FILE NO.: PG5876

BORINGS BY: CME 55 Low Clearance Drill

REMARKS:      DATE: August 07, 2024      HOLE NO.: BH 32-24



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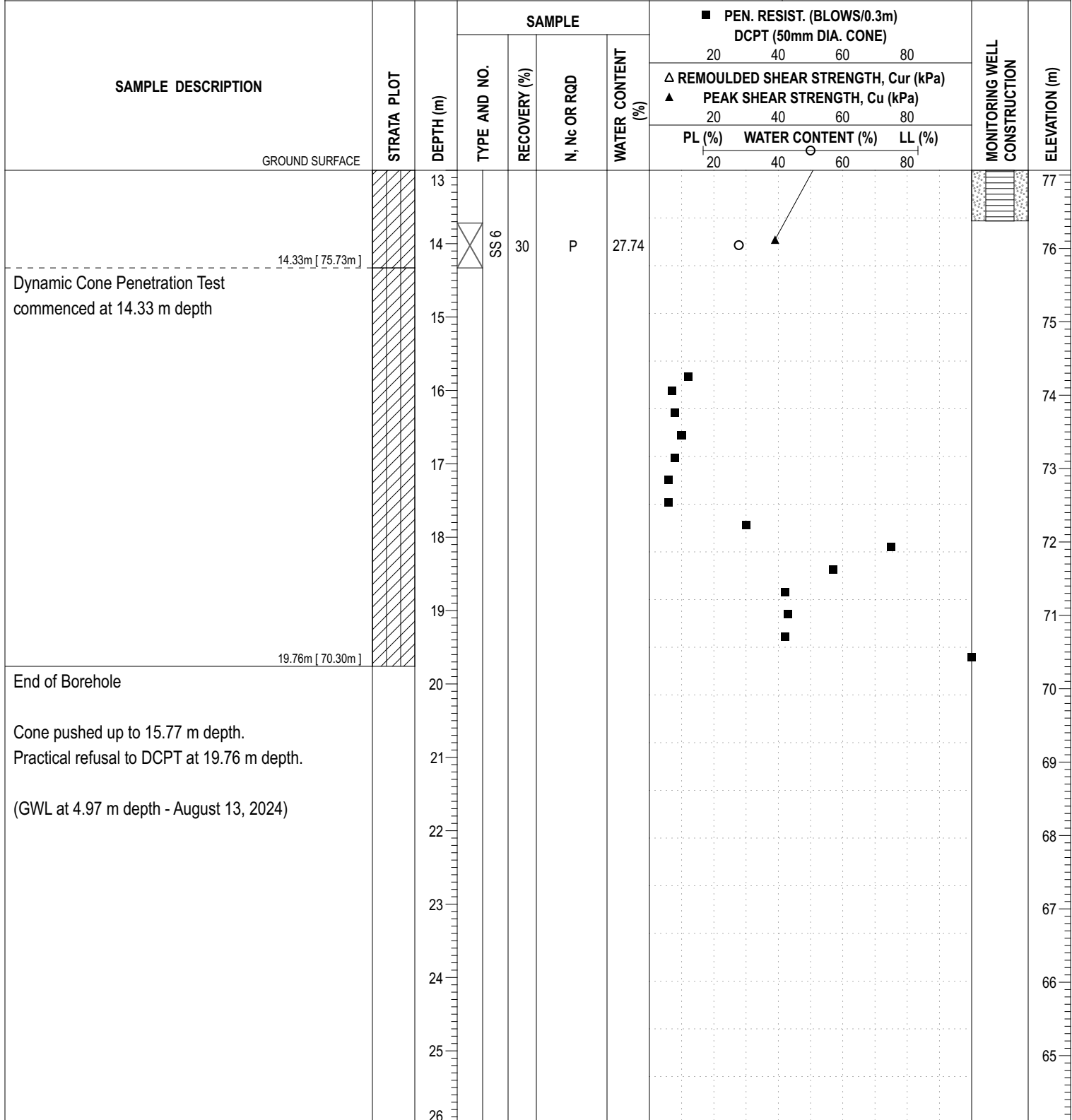
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**COORD. SYS.:** MTM ZONE 9      **EASTING:** 367157.38      **NORTHING:** 5018138.45      **ELEVATION:** 90.06

**PROJECT:** Project X Development      **FILE NO. :** PG5876

**BORINGS BY:** CME 55 Low Clearance Drill

**REMARKS:**      **DATE:** August 07, 2024      **HOLE NO. :** BH 32-24



P:/AutoCAD Drawings/Test Hole Data Files/PG5876/data/sqlite 2024-09-10, 17:14 Paterson\_Template AA

# SYMBOLS AND TERMS

## SOIL DESCRIPTION

Behavioural properties, such as structure and strength, take precedence over particle gradation in describing soils. Terminology describing soil structure are as follows:

Desiccated	-	having visible signs of weathering by oxidation of clay minerals, shrinkage cracks, etc.
Fissured	-	having cracks, and hence a blocky structure.
Varved	-	composed of regular alternating layers of silt and clay.
Stratified	-	composed of alternating layers of different soil types, e.g. silt and sand or silt and clay.
Well-Graded	-	Having wide range in grain sizes and substantial amounts of all intermediate particle sizes (see Grain Size Distribution).
Uniformly-Graded	-	Predominantly of one grain size (see Grain Size Distribution).

The standard terminology to describe the strength of cohesionless soils is the relative density, usually inferred from the results of the Standard Penetration Test (SPT) 'N' value. The SPT N value is the number of blows of a 63.5 kg hammer, falling 760 mm, required to drive a 51 mm O.D. split spoon sampler 300 mm into the soil after an initial penetration of 150 mm.

Relative Density	'N' Value	Relative Density %
Very Loose	<4	<15
Loose	4-10	15-35
Compact	10-30	35-65
Dense	30-50	65-85
Very Dense	>50	>85

The standard terminology to describe the strength of cohesive soils is the consistency, which is based on the undisturbed undrained shear strength as measured by the in situ or laboratory vane tests, penetrometer tests, unconfined compression tests, or occasionally by Standard Penetration Tests.

Consistency	Undrained Shear Strength (kPa)	'N' Value
Very Soft	<12	<2
Soft	12-25	2-4
Firm	25-50	4-8
Stiff	50-100	8-15
Very Stiff	100-200	15-30
Hard	>200	>30



## SYMBOLS AND TERMS (continued)

### SOIL DESCRIPTION (continued)

Cohesive soils can also be classified according to their "sensitivity". The sensitivity is the ratio between the undisturbed undrained shear strength and the remoulded undrained shear strength of the soil.

Terminology used for describing soil strata based upon texture, or the proportion of individual particle sizes present is provided on the Textural Soil Classification Chart at the end of this information package.

### ROCK DESCRIPTION

The structural description of the bedrock mass is based on the Rock Quality Designation (RQD).

The RQD classification is based on a modified core recovery percentage in which all pieces of sound core over 100 mm long are counted as recovery. The smaller pieces are considered to be a result of closely-spaced discontinuities (resulting from shearing, jointing, faulting, or weathering) in the rock mass and are not counted. RQD is ideally determined from NXL size core. However, it can be used on smaller core sizes, such as BX, if the bulk of the fractures caused by drilling stresses (called "mechanical breaks") are easily distinguishable from the normal in situ fractures.

<b>RQD %</b>	<b>ROCK QUALITY</b>
90-100	Excellent, intact, very sound
75-90	Good, massive, moderately jointed or sound
50-75	Fair, blocky and seamy, fractured
25-50	Poor, shattered and very seamy or blocky, severely fractured
0-25	Very poor, crushed, very severely fractured

### SAMPLE TYPES

SS	-	Split spoon sample (obtained in conjunction with the performing of the Standard Penetration Test (SPT))
TW	-	Thin wall tube or Shelby tube
PS	-	Piston sample
AU	-	Auger sample or bulk sample
WS	-	Wash sample
RC	-	Rock core sample (Core bit size AXT, BXL, etc.). Rock core samples are obtained with the use of standard diamond drilling bits.

## SYMBOLS AND TERMS (continued)

### GRAIN SIZE DISTRIBUTION

MC%	-	Natural moisture content or water content of sample, %
LL	-	Liquid Limit, % (water content above which soil behaves as a liquid)
PL	-	Plastic limit, % (water content above which soil behaves plastically)
PI	-	Plasticity index, % (difference between LL and PL)
Dxx	-	Grain size which xx% of the soil, by weight, is of finer grain sizes These grain size descriptions are not used below 0.075 mm grain size
D10	-	Grain size at which 10% of the soil is finer (effective grain size)
D60	-	Grain size at which 60% of the soil is finer
Cc	-	Concavity coefficient = $(D_{30})^2 / (D_{10} \times D_{60})$
Cu	-	Uniformity coefficient = $D_{60} / D_{10}$

Cc and Cu are used to assess the grading of sands and gravels:

Well-graded gravels have:  $1 < Cc < 3$  and  $Cu > 4$

Well-graded sands have:  $1 < Cc < 3$  and  $Cu > 6$

Sands and gravels not meeting the above requirements are poorly-graded or uniformly-graded.

Cc and Cu are not applicable for the description of soils with more than 10% silt and clay (more than 10% finer than 0.075 mm or the #200 sieve)

### CONSOLIDATION TEST

$p'_o$	-	Present effective overburden pressure at sample depth
$p'_c$	-	Preconsolidation pressure of (maximum past pressure on) sample
Ccr	-	Recompression index (in effect at pressures below $p'_c$ )
Cc	-	Compression index (in effect at pressures above $p'_c$ )
OC Ratio		Overconsolidation ratio = $p'_c / p'_o$
Void Ratio		Initial sample void ratio = volume of voids / volume of solids
Wo	-	Initial water content (at start of consolidation test)

### PERMEABILITY TEST

k	-	Coefficient of permeability or hydraulic conductivity is a measure of the ability of water to flow through the sample. The value of k is measured at a specified unit weight for (remoulded) cohesionless soil samples, because its value will vary with the unit weight or density of the sample during the test.
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## SYMBOLS AND TERMS (continued)

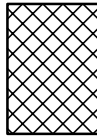
### STRATA PLOT



Topsoil



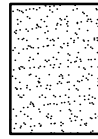
Asphalt



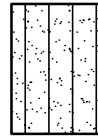
Fill



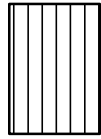
Peat



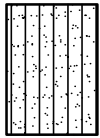
Sand



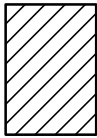
Silty Sand



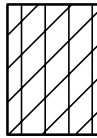
Silt



Sandy Silt



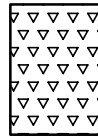
Clay



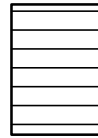
Silty Clay



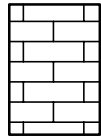
Clayey Silty Sand



Glacial Till



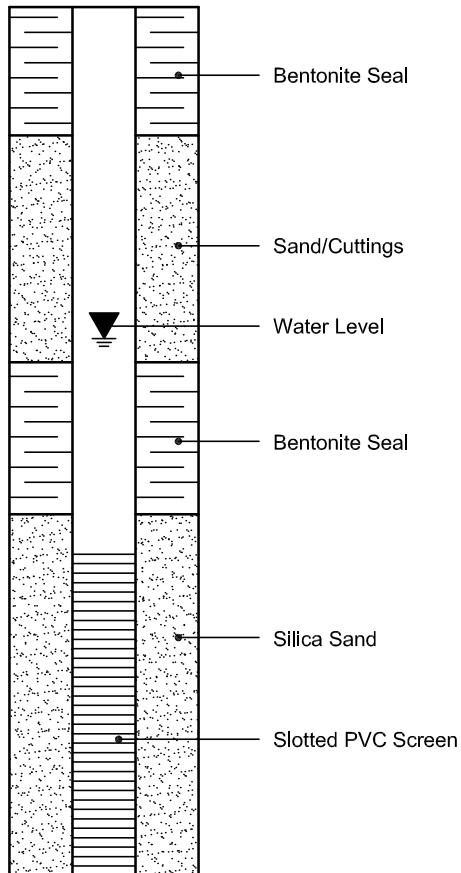
Shale



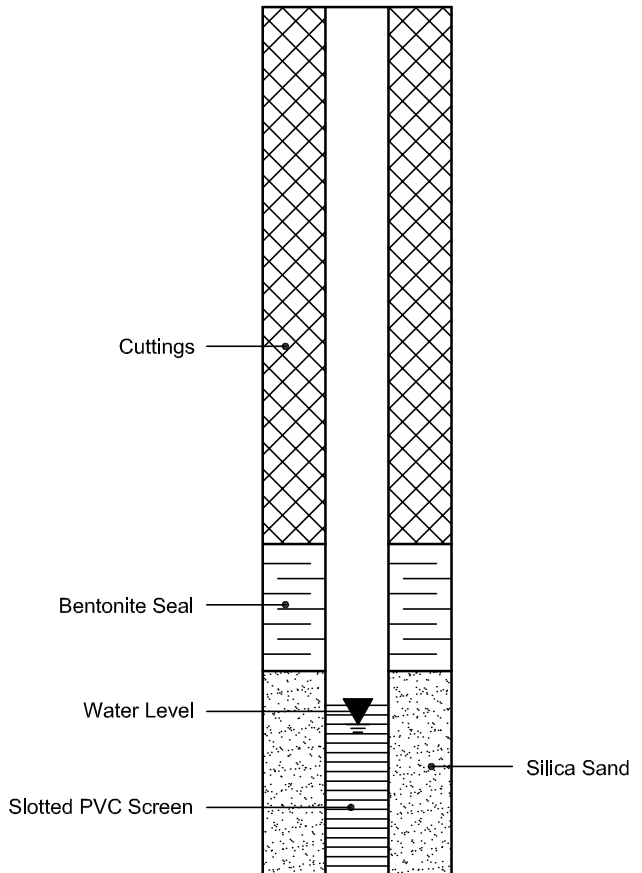
Bedrock

### MONITORING WELL AND PIEZOMETER CONSTRUCTION

#### MONITORING WELL CONSTRUCTION



#### PIEZOMETER CONSTRUCTION





# BOREHOLE REPORT

Reference No.: 12615684-A1

Borehole No.

**BH-101-23**

Client : **Medusa Limited Partnership**

Geodetic Coordinates

X: **366614.6**

Project : **Geotechnical Investigation - Proposed Distribution Center**

MTM-9 (NAD-1983)

Y: **5017753.8**

Z: **90.67**

Location : **Bill Leathem Drive, Ottawa, Ontario**

**Preliminary**

Date (Start) :

**2023-07-03**

Drilling Contractor : **George Downing Estate Drilling Limited**

Date (Finish) :

**2023-07-06**

Borehole Type : **Auger and Casing**

Borehole Depth (m):

**28.30**

Borehole Diameter : **200 mm & 76 mm**

Core Bit Size : **NQ**

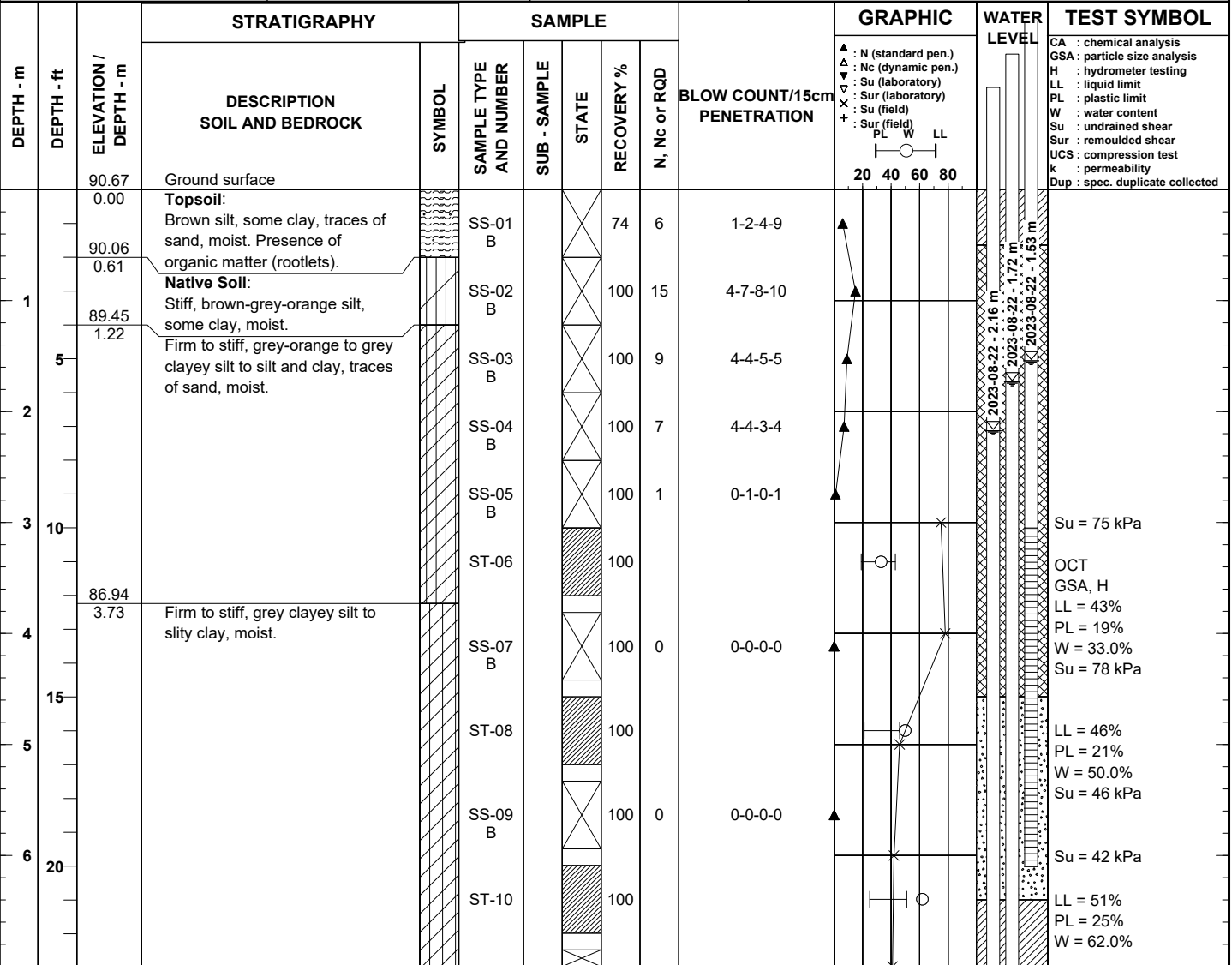
Location Plan No.:

**FIGURE 1**

Described by : **David Vincent, Tech.**

Verified by : **Keshini Rangasamy, CEP**

SAMPLE TYPE	TERMINOLOGY	BEDROCK QUALITY INDEX	COMPACTNESS INDEX "N"	WATER LEVEL
SS(E) : Split Spoon (Environment) RC : Rock diamond core GS(E) : Grab sample (Environment) AU(E) : Auger (Environment) TEE : Sample tube environment ST : Shelby tube	"traces" 1-10% "some" 10-20% "adjective" (...y) 20-35% "and" 35-50%	% RQD QUALIFYING 0-25 Very poor 25-50 Poor 50-75 Fair 75-90 Good 90-100 Excellent	Very loose 0-4 Loose 4-10 Compact 10-30 Dense 30-50 Very dense >50	Date: 2023-08-22 Date: 2023-07-20 Depth: Depth:
SAMPLE STATE	SYMBOLS	CLASSIFICATION (UNIFIED SYSTEM)	CONSISTENCY	SHEAR RESISTANCE (Su)
Remoulded Intact Lost Diamond drilling	N: Standard penetration index R: Refusal (N > 100) R.Q.D.: Rock Quality Designation % R.Q.D. $\geq \frac{\text{Core} > 4 \text{ in. (10 cm)}}{\text{drilled length}}$	< 0.002 mm Clay 0.002 - 0.075 mm Silt 0.075 - 4.75 mm Sand 4.75 - 75 mm Gravel 75 - 300 mm Cobbles > 300 mm Boulders	Very soft Soft Firm Stiff Very stiff Hard	<12 kPa 12-25 kPa 25-50 kPa 50-100 kPa 100-200 kPa >200 kPa



Remark(s) : OCT: Oedometer Consolidation Test

Borehole - standard.sty



# BOREHOLE REPORT

Reference No.: 12615684-A1

Borehole No.

**BH-101-23**

DEPTH - m	DEPTH - ft	ELEVATION / DEPTH - m	STRATIGRAPHY		SAMPLE				BLOW COUNT/15cm PENETRATION	GRAPHIC	WATER LEVEL	TEST SYMBOL
			DESCRIPTION SOIL AND BEDROCK	SYMBOL	SAMPLE TYPE AND NUMBER	SUB - SAMPLE	STATE	RECOVERY %				
25	8				SS-11 B			100	0	0-0-0-0		Su = 41 kPa
					ST-12			100				OCT GSA LL = 48% PL = 23% W = 63.0% Su = 37 kPa
30	9				SS-13 B			100	0	0-0-0-0		Su = 42 kPa
					SS-14 B			100	0	0-0-0-0		Su = 44 kPa
35	11				SS-15 B			100	0	0-0-0-0		Su = 43 kPa
					SS-16 B			100	0	0-0-0-0		Su = 42 kPa
40	12				SS-16 B			100	0	0-0-0-0		Su = 42 kPa
45	14	77.72 12.95		Firm to stiff, grey clayey silt, traces of sand, moist.	SS-17 B			74	1	0-1-0-1		Su = 47 kPa GSA Su = 59 kPa
50	15				SS-18 B			82	2	1-1-1-0		GSA Su = 58 kPa
55	16	74.52 16.15		Loose to compact, grey silty sand, some gravel, some to traces of clay, moist.	SS-18 B							
60	17				SS-19 B			49	8	4-5-3-4		GSA
65	18				SS-20 B			25	16	6-8-8-7		
70	19	71.62 19.05		becoming with presence of cobbles and/or boulders								

Borehole - standard.sty



# BOREHOLE REPORT

Reference No.: 12615684-A1

Borehole No.

**BH-101-23**

DEPTH - m	DEPTH - ft	ELEVATION / DEPTH - m	STRATIGRAPHY		SAMPLE				BLOW COUNT/15cm PENETRATION	GRAPHIC	WATER LEVEL	TEST SYMBOL	
			DESCRIPTION SOIL AND BEDROCK	SYMBOL	SAMPLE TYPE AND NUMBER	SUB - SAMPLE	STATE	RECOVERY %					N, Nc or RQD
20					SS-21 B			57	26	23-12-14-19			
21													
22	70				RC-22 NQ			100	0				
23	75				RC-23 NQ			42	0				
24													
25	80				RC-24 NQ			22	0				
26	85	65.24 25.43		<b>Bedrock:</b> Grey dolomite, excellent quality.		A							
27					RC-25 NQ	B		91	91				
28	90												
29					RC-26 NQ			95	95				
30	100	62.37 28.30		End of borehole									
31													
32	105												

Borehole - standard.sty



# BOREHOLE REPORT

Reference No.: 12615684-A1

**Borehole No. BH-102-23**

Client : **Medusa Limited Partnership**  
 Project : **Geotechnical Investigation - Proposed Distribution Center**  
 Location : **Bill Leathem Drive, Ottawa, Ontario**  
 Drilling Contractor : **George Downing Estate Drilling Limited**  
 Borehole Type : **Auger and Casing**  
 Borehole Diameter : **200 mm**  
 Described by : **David Vincent, Tech.**  
 Core Bit Size :  
 Verified by : **Keshini Rangasamy, CEP**

Geodetic Coordinates X: **366511.8**  
 Y: **5017682.3**  
 Z: **95.18**  
 Date (Start) : **2023-07-10**  
 Date (Finish) : **2023-07-11**  
 Borehole Depth (m): **22.90**  
 Location Plan No.: **FIGURE 1**

**Preliminary**

<b>SAMPLE TYPE</b> SS(E) : Split Spoon (Environment) RC : Rock diamond core GS(E) : Grab sample (Environment) AU(E) : Auger (Environment) TEE : Sample tube environment ST : Shelby tube	<b>TERMINOLOGY</b> "traces" 1-10% "some" 10-20% "adjective" (...y) 20-35% "and" 35-50%	<b>BEDROCK QUALITY INDEX</b> % RQD QUALIFYING 0-25 Very poor 25-50 Poor 50-75 Fair 75-90 Good 90-100 Excellent	<b>COMPACTNESS INDEX "N"</b> Very loose 0-4 Loose 4-10 Compact 10-30 Dense 30-50 Very dense >50	<b>WATER LEVEL</b> Date: _____ Date: _____ Depth: _____ Depth: _____
<b>SAMPLE STATE</b> Remoulded Intact Lost Diamond drilling	<b>SYMBOLS</b> N: Standard penetration index R: Refusal (N > 100) R.Q.D.: Rock Quality Designation % R.Q.D. $\geq$ Core > 4 in. (10 cm) drilled length	<b>CLASSIFICATION (UNIFIED SYSTEM)</b> Clay < 0.002 mm Silt 0.002 - 0.075 mm Sand 0.075 - 4.75 mm Gravel 4.75 - 75 mm Cobbles 75 - 300 mm Boulders > 300 mm	<b>CONSISTENCY</b> Very soft Soft Firm Stiff Very stiff Hard	<b>SHEAR RESISTANCE (Su)</b> <12 kPa 12-25 kPa 25-50 kPa 50-100 kPa 100-200 kPa >200 kPa

DEPTH - m	DEPTH - ft	ELEVATION / DEPTH - m	STRATIGRAPHY		SAMPLE				BLOW COUNT/15cm PENETRATION	GRAPHIC	WATER LEVEL	TEST SYMBOL
			DESCRIPTION SOIL AND BEDROCK	SYMBOL	SAMPLE TYPE AND NUMBER	SUB - SAMPLE	STATE	RECOVERY %				
		95.18	Ground surface									
		0.00	<b>Topsoil:</b> Brown silt, some clay, traces of sand, moist. Presence of organic matter (rootlets).		SS-01 B			61	10	3-4-6-7		
1		94.57 0.61	<b>Fill:</b> Brown-grey clayey silt, traces of sand, moist. Presence of organic matter (rootlets).		SS-02 B			74	11	4-5-6-6		
	5				SS-03 B			66	9	2-4-5-6		
2		93.35 1.83	Grey-brown to grey clayey silt, traces of sand, moist. Presence of organic matter (rootlets).		SS-04 B			66	13	5-6-7-7		
					SS-05 B			66	7	1-3-4-5		
3	10				SS-06 B			66	7	2-3-4-6		
4					SS-07 B			0	10	2-4-6-7		
	15				SS-08 B			66	12	3-4-8-7		
5					SS-09 B			66	19	7-8-11-13		
		89.69 5.49	Grey-orange clayey silt, moist.		SS-10 B			100	13	2-6-7-10		
6	20				SS-11 B			100	8	2-3-5-5		Su = 70 kPa

Remark(s) : OCT: Oedometer Consolidation Test

Borehole - standard.sty



# BOREHOLE REPORT

Reference No.: 12615684-A1

Borehole No.

**BH-102-23**

DEPTH - m	DEPTH - ft	ELEVATION / DEPTH - m	STRATIGRAPHY		SAMPLE				BLOW COUNT/15cm PENETRATION	GRAPHIC	WATER LEVEL	TEST SYMBOL
			DESCRIPTION SOIL AND BEDROCK	SYMBOL	SAMPLE TYPE AND NUMBER	SUB - SAMPLE	STATE	RECOVERY %				
		88.01 7.17	Native Soil: Firm to stiff, grey clayey silt, traces of sand, moist.	[diagonal lines]	ST-12			100				Su = 80 kPa
25	8											
		86.76 8.42	Firm to stiff, grey clayey silt to silty clay, moist.	[diagonal lines]	SS-13 B			100	0	0-0-0-0		LL = 39% PL = 19% W = 33.0% Su = 58 kPa
9	30											
			Firm to stiff, grey clayey silt, traces of sand, moist.	[diagonal lines]	ST-14			82				LL = 44% PL = 20% W = 52.0% Su = 46 kPa
10	35											
			Firm to stiff, grey clayey silt, traces of sand, moist.	[diagonal lines]	SS-15 B			100	0	0-0-0-0		Su = 43 kPa
12	40											
			Firm to stiff, grey clayey silt, traces of sand, moist.	[diagonal lines]	ST-16			100				LL = 43% PL = 21% W = 51.0% Su = 48 kPa
13	45											
			Firm to stiff, grey clayey silt, traces of sand, moist.	[diagonal lines]	ST-17			100				
15	50											
			Firm to stiff, grey clayey silt, traces of sand, moist.	[diagonal lines]	SS-18 B			100	0	0-0-0-0		
16	55											
		77.90 17.28	Firm to stiff, grey clayey silt, traces of sand, moist.	[diagonal lines]	SS-19 B			0	2	0-1-1-1		
17	60											
			Firm to stiff, grey clayey silt, traces of sand, moist.	[diagonal lines]	SS-20			100	8	2-3-5-3		
18	60											
19												

Borehole - standard.sty





# BOREHOLE REPORT

Reference No.: 12615684-A1

Borehole No.

**BH-102-23**

DEPTH - m	DEPTH - ft	ELEVATION / DEPTH - m	STRATIGRAPHY		SAMPLE				BLOW COUNT/15cm PENETRATION	GRAPHIC	WATER LEVEL	TEST SYMBOL
			DESCRIPTION SOIL AND BEDROCK	SYMBOL	SAMPLE TYPE AND NUMBER	SUB - SAMPLE	STATE	RECOVERY %				
20					B							
21					SS-21 B			90	9	4-3-6-6		
22												
23		72.28 22.90			SS-22 B			16	3	1-2-1-2		
			End of borehole									
24												
25												
26												
27												
28												
29												
30												
31												
32												

▲ : N (standard pen.)  
 △ : Nc (dynamic pen.)  
 ▽ : Su (laboratory)  
 ∇ : Sur (laboratory)  
 × : Su (field)  
 + : Sur (field)  
 PL W LL

- TEST SYMBOL**  
 CA : chemical analysis  
 GSA : particle size analysis  
 H : hydrometer testing  
 LL : liquid limit  
 PL : plastic limit  
 W : water content  
 Su : undrained shear  
 Sur : remoulded shear  
 UCS : compression test  
 k : permeability  
 Dup : spec. duplicate collected

Borehole - standard.sty



# BOREHOLE REPORT

Reference No.: 12615684-A1

Borehole No.

**BH-103-23**

Client : **Medusa Limited Partnership**

Geodetic Coordinates  
MTM-9 (NAD-1983)

X: **366472.6**  
Y: **5017591.4**  
Z: **90.66**

Project : **Geotechnical Investigation - Proposed Distribution Center**

**Preliminary**

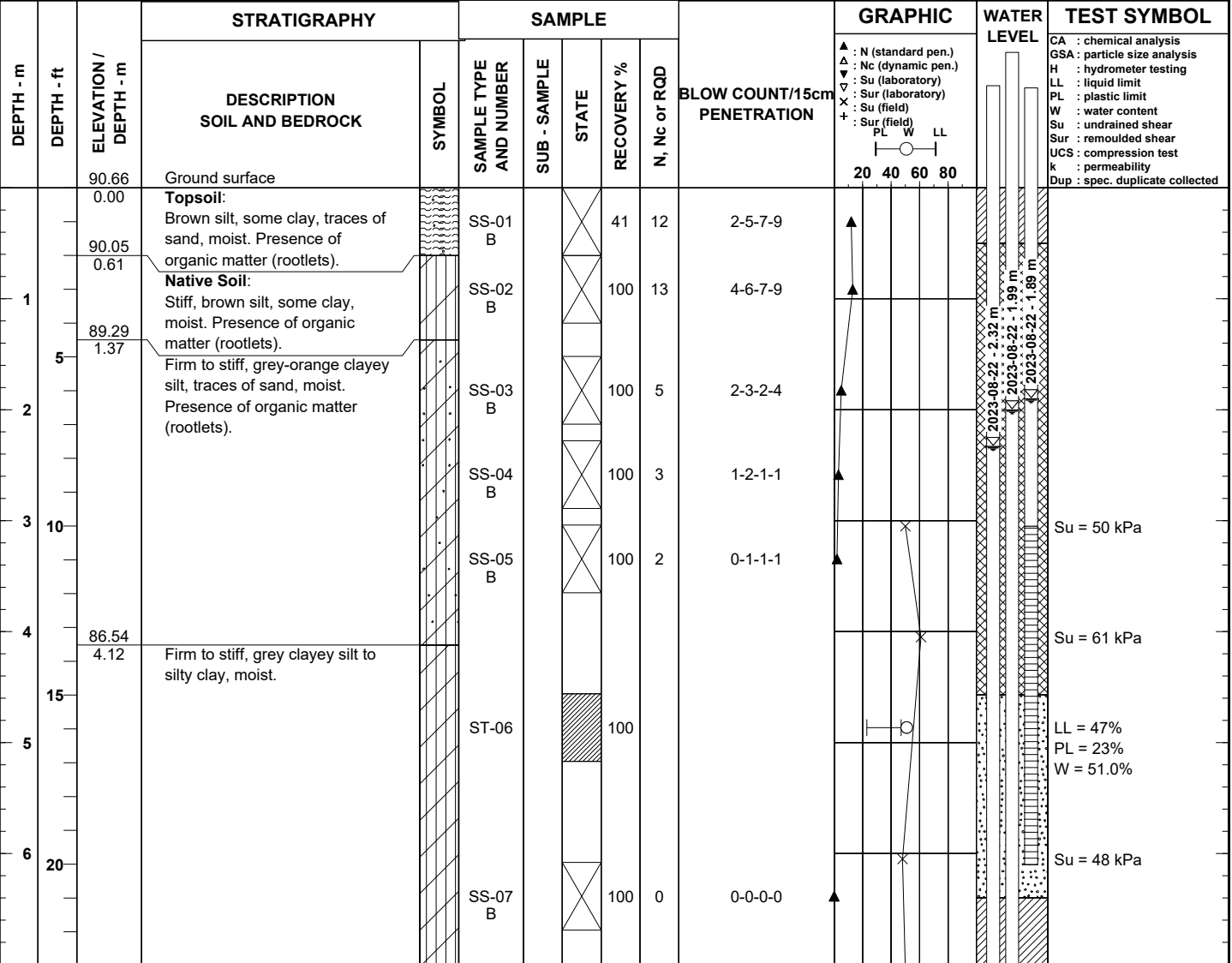
Location : **Bill Leathem Drive, Ottawa, Ontario**  
Drilling Contractor : **George Downing Estate Drilling Limited**  
Borehole Type : **Auger and Casing**  
Borehole Diameter : **200 mm & 76 mm**  
Described by : **David Vincent, Tech.**

Date (Start) : **2023-07-06**  
Date (Finish) : **2023-07-10**  
Borehole Depth (m): **25.25**  
Location Plan No.: **FIGURE 1**

Core Bit Size : **NQ**  
Verified by : **Keshini Rangasamy, CEP**

SAMPLE TYPE	TERMINOLOGY	BEDROCK QUALITY INDEX	COMPACTNESS INDEX "N"	WATER LEVEL
SS(E) : Split Spoon (Environment) RC : Rock diamond core GS(E) : Grab sample (Environment) AU(E) : Auger (Environment) TEE : Sample tube environment ST : Shelby tube	"traces" 1-10% "some" 10-20% "adjective" (...y) 20-35% "and" 35-50%	% RQD 0-25 Very poor 25-50 Poor 50-75 Fair 75-90 Good 90-100 Excellent	Very loose 0-4 Loose 4-10 Compact 10-30 Dense 30-50 Very dense >50	Date: 2023-08-22 Date: 2023-07-20 Depth: Depth:

SAMPLE STATE	SYMBOLS	CLASSIFICATION (UNIFIED SYSTEM)	CONSISTENCY	SHEAR RESISTANCE (Su)
Remoulded Intact Lost Diamond drilling	N: Standard penetration index R: Refusal (N > 100) R.Q.D.: Rock Quality Designation % R.Q.D. $\geq$ Core > 4 in. (10 cm) drilled length	< 0.002 mm Clay 0.002 - 0.075 mm Silt 0.075 - 4.75 mm Sand 4.75 - 75 mm Gravel 75 - 300 mm Cobbles > 300 mm Boulders	Very soft Soft Firm Stiff Very stiff Hard	<12 kPa 12-25 kPa 25-50 kPa 50-100 kPa 100-200 kPa >200 kPa



Remark(s) :

Borehole - standard.sty



# BOREHOLE REPORT

Reference No.: 12615684-A1

Borehole No.

**BH-103-23**

DEPTH - m	DEPTH - ft	ELEVATION / DEPTH - m	STRATIGRAPHY		SAMPLE				BLOW COUNT/15cm PENETRATION	GRAPHIC	WATER LEVEL	TEST SYMBOL
			DESCRIPTION SOIL AND BEDROCK	SYMBOL	SAMPLE TYPE AND NUMBER	SUB - SAMPLE	STATE	RECOVERY %				
25	8				ST-08			100				
30	9				SS-09 B			100	0	0-0-0-0		LL = 54% PL = 23% W = 58.0% Su = 52 kPa
35	10				ST-10			100				Su = 48 kPa
79.36	11	11.30	Firm to stiff, grey clayey silt, traces of sand, moist.		ST-11			0				LL = 52% PL = 21% W = 58.0%
40	12				SS-12 B			100	2	2-1-1-0		Su = 52 kPa
76.32	14	14.34	Very loose to loose, grey sandy silt, some clay, traces of gravel, moist.		SS-13 B			100	3	1-1-2-2		Su = 58 kPa
50	15				SS-14 B			0	8	8-4-4-3		
73.28	17	17.38	Compact to dense, grey silty sand, some gravel and clay, moist.		SS-15 B			0	17	10-6-11-19		
60	18											
19												

Borehole - standard.sty



# BOREHOLE REPORT

Reference No.: 12615684-A1

Borehole No.

**BH-103-23**

DEPTH - m	DEPTH - ft	ELEVATION / DEPTH - m	STRATIGRAPHY		SAMPLE				BLOW COUNT/15cm PENETRATION	GRAPHIC	WATER LEVEL	TEST SYMBOL	
			DESCRIPTION SOIL AND BEDROCK	SYMBOL	SAMPLE TYPE AND NUMBER	SUB - SAMPLE	STATE	RECOVERY %					N, Nc or RQD
20													
21													
70					SS-16 B			X	90	47	11-20-27-34		GSA
22													
75		68.03 22.63			<b>Bedrock:</b> Brown-grey dolomite, poor quality.								
23					RC-17 NQ				100	44			
24		66.91 23.75			becoming grey, excellent quality								
25					RC-18 NQ				95	95			
80													
25		65.41 25.25			End of borehole								
26													
85													
27													
90													
28													
29													
95													
30													
100													
31													
32													
105													

Borehole - standard.sty



# BOREHOLE REPORT

Reference No.: 12615684-A1

**Borehole No. BH-104-23**

Client : **Medusa Limited Partnership**  
 Project : **Geotechnical Investigation - Proposed Distribution Center**

Geodetic Coordinates X: **366549.1**  
 MTM-9 (NAD-1983) Y: **5017733.7**  
 Z: **91.01**

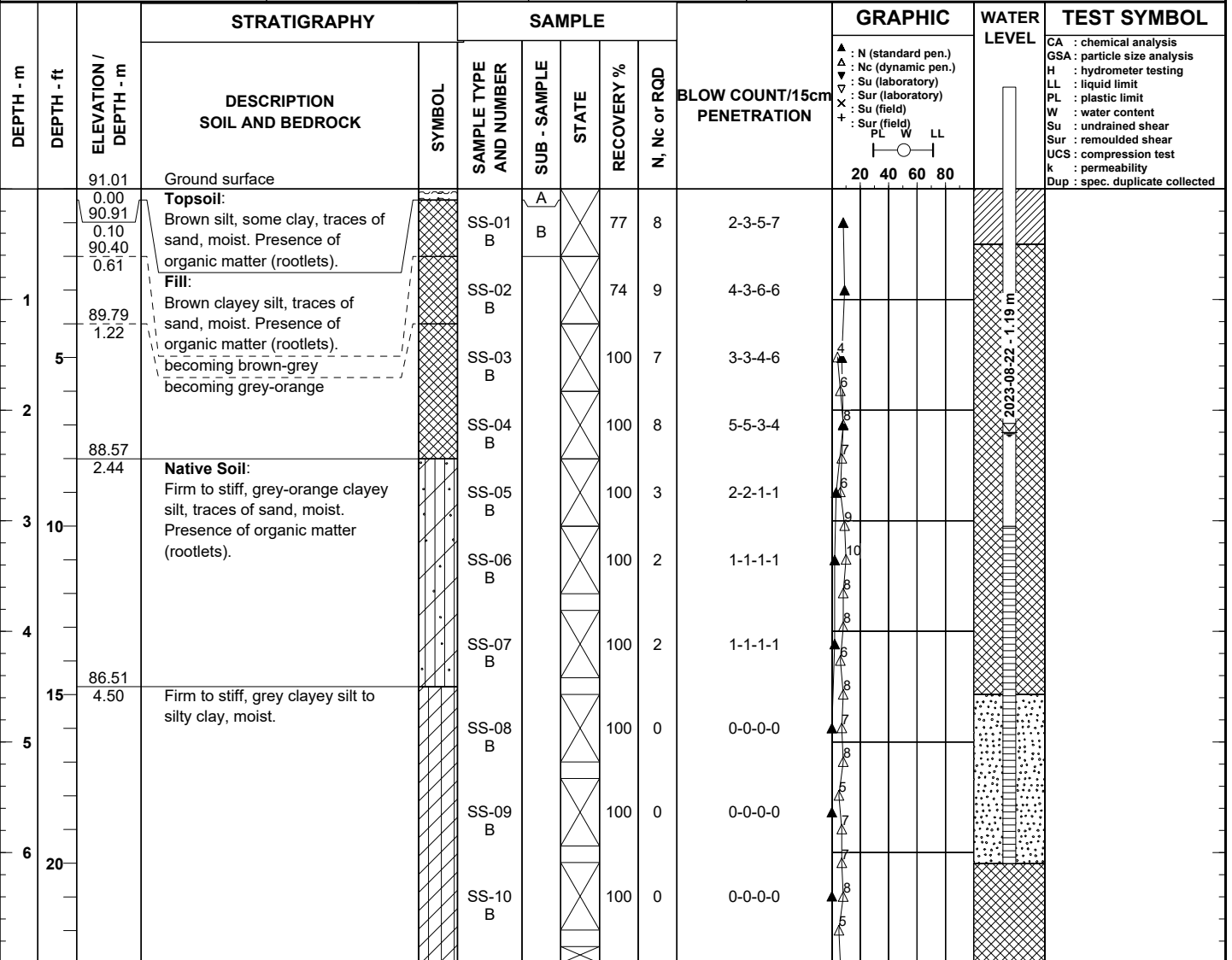
Location : **Bill Leathem Drive, Ottawa, Ontario**  
 Drilling Contractor : **George Downing Estate Drilling Limited**  
 Borehole Type : **Auger and Casing**  
 Borehole Diameter : **200 mm**  
 Described by : **David Vincent, Tech.**

**Preliminary**

Date (Start) : **2023-06-29**  
 Date (Finish) : **2023-06-29**  
 Borehole Depth (m): **22.33**  
 Location Plan No.: **FIGURE 1**

Core Bit Size :  
 Verified by : **Keshini Rangasamy, CEP**

<b>SAMPLE TYPE</b> SS(E) : Split Spoon (Environment) RC : Rock diamond core GS(E) : Grab sample (Environment) AU(E) : Auger (Environment) TEE : Sample tube environment ST : Shelby tube	<b>TERMINOLOGY</b> "traces" 1-10% "some" 10-20% "adjective" (...y) 20-35% "and" 35-50%	<b>BEDROCK QUALITY INDEX</b> % RQD QUALIFYING 0-25 Very poor 25-50 Poor 50-75 Fair 75-90 Good 90-100 Excellent	<b>COMPACTNESS INDEX "N"</b> Very loose 0-4 Loose 4-10 Compact 10-30 Dense 30-50 Very dense >50	<b>WATER LEVEL</b> Date: 2023-08-22 Date: 2023-07-20 Depth: 1.19 Depth: 1.83
<b>SAMPLE STATE</b> Remoulded Intact Lost Diamond drilling	<b>SYMBOLS</b> N: Standard penetration index R: Refusal (N > 100) R.Q.D.: Rock Quality Designation % R.Q.D. $\geq$ Core > 4 in. (10 cm) drilled length	<b>CLASSIFICATION (UNIFIED SYSTEM)</b> Clay < 0.002 mm Silt 0.002 - 0.075 mm Sand 0.075 - 4.75 mm Gravel 4.75 - 75 mm Cobbles 75 - 300 mm Boulders > 300 mm	<b>CONSISTENCY</b> Very soft Soft Firm Stiff Very stiff Hard	<b>SHEAR RESISTANCE (Su)</b> <12 kPa 12-25 kPa 25-50 kPa 50-100 kPa 100-200 kPa >200 kPa



Remark(s) :

Borehole - standard.sty



# BOREHOLE REPORT

Reference No.: 12615684-A1

Borehole No.

**BH-104-23**

DEPTH - m	DEPTH - ft	ELEVATION / DEPTH - m	STRATIGRAPHY		SAMPLE				BLOW COUNT/15cm PENETRATION	GRAPHIC	WATER LEVEL	TEST SYMBOL					
			DESCRIPTION SOIL AND BEDROCK	SYMBOL	SAMPLE TYPE AND NUMBER	SUB - SAMPLE	STATE	RECOVERY %					N, Nc or RQD				
					SS-11 B		X	100	0	0-0-0-0	▲						
8	25				SS-12 B		X	100	0	0-0-0-0	▲						
9	30				SS-13 B		X	100	0	0-0-0-0	▲						
10	35				SS-14 B		X	100	0	0-0-0-0	▲						
					SS-15 B		X	100	0	0-0-0-0	▲						
11					SS-16 B		X	100	0	0-0-0-0	▲						
12	40				SS-17 B		X	90	0	0-0-0-0	▲						
13		77.77 13.24	becoming with traces of sand								▲						
14	45				SS-18 B		X	100	0	0-0-0-0	▲						
15	50				SS-19 B		X	100	0	0-0-0-0	▲						
16		75.19 15.82	End of sampling								▲						
17	55										▲						
18	60										▲						
19											▲						

Borehole - standard.sty



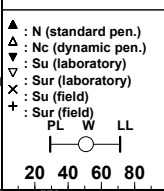
# BOREHOLE REPORT

Reference No.: 12615684-A1

Borehole No.

**BH-104-23**

DEPTH - m	DEPTH - ft	ELEVATION / DEPTH - m	STRATIGRAPHY		SAMPLE					BLOW COUNT/15cm PENETRATION	GRAPHIC	WATER LEVEL	TEST SYMBOL	
			DESCRIPTION SOIL AND BEDROCK	SYMBOL	SAMPLE TYPE AND NUMBER	SUB - SAMPLE	STATE	RECOVERY %	N, Nc or RQD					
20														
21														
22		68.68 22.33	End of dynamic penetration test End of borehole											
23														
24														
25														
26														
27														
28														
29														
30														
31														
32														



- TEST SYMBOL**
- CA : chemical analysis
  - GSA : particle size analysis
  - H : hydrometer testing
  - LL : liquid limit
  - PL : plastic limit
  - W : water content
  - Su : undrained shear
  - Sur : remoulded shear
  - UCS : compression test
  - k : permeability
  - Dup : spec. duplicate collected

Borehole - standard.sty



# BOREHOLE REPORT

Reference No.: 12615684-A1

**Borehole No. BH-105-23**

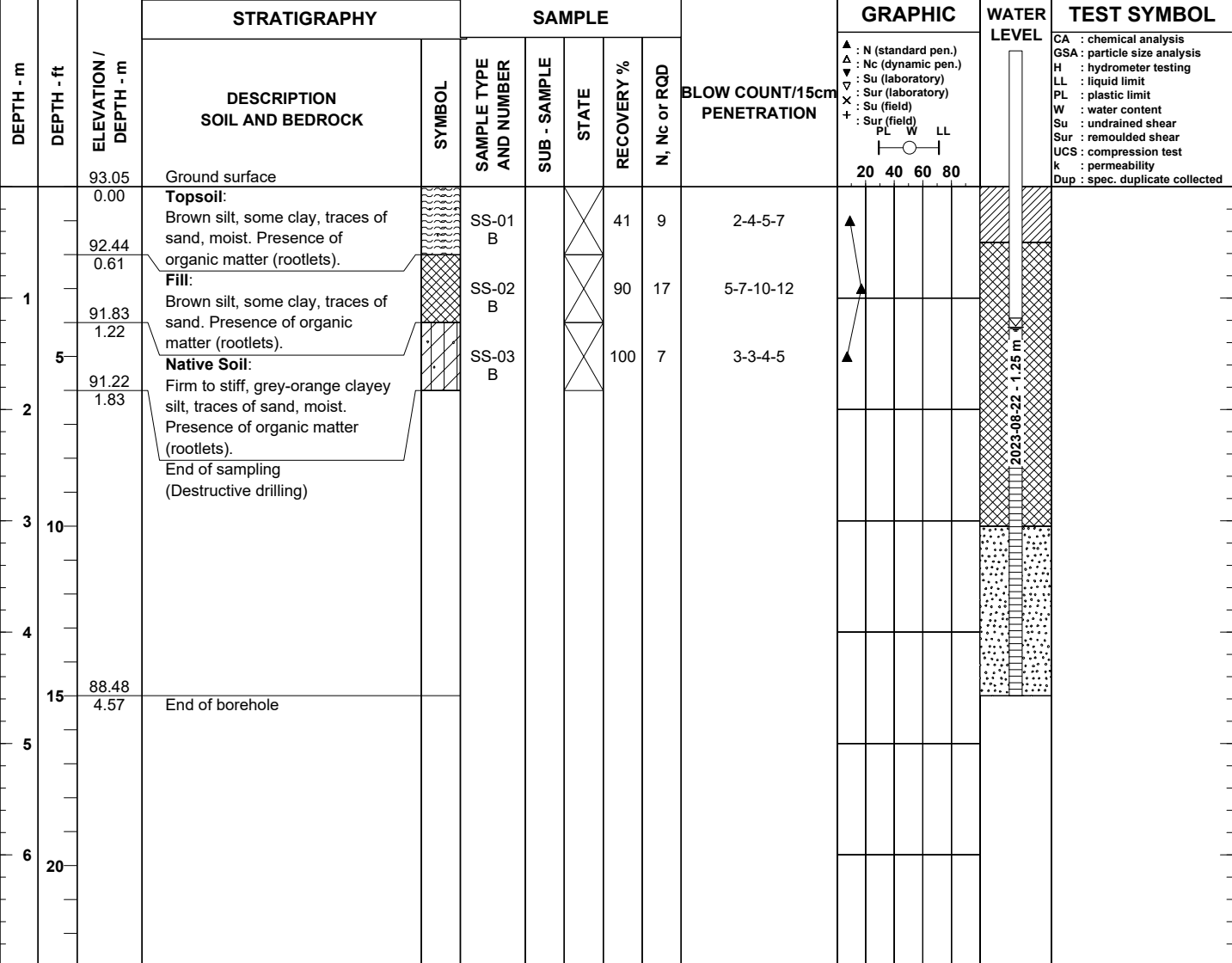
Client : **Medusa Limited Partnership**  
 Project : **Geotechnical Investigation - Proposed Distribution Center**  
 Location : **Bill Leathem Drive, Ottawa, Ontario**  
 Drilling Contractor : **George Downing Estate Drilling Limited**  
 Borehole Type : **Auger**  
 Borehole Diameter : **200 mm**  
 Described by : **David Vincent, Tech.**  
 Core Bit Size :  
 Verified by : **Keshini Rangasamy, CEP**

Geodetic Coordinates X: **366555.1**  
 Y: **5017688.8**  
 Z: **93.05**  
 Date (Start) : **2023-07-11**  
 Date (Finish) : **2023-07-11**  
 Borehole Depth (m): **4.57**  
 Location Plan No.: **FIGURE 1**

**Preliminary**

<b>SAMPLE TYPE</b> SS(E) : Split Spoon (Environment) RC : Rock diamond core GS(E) : Grab sample (Environment) AU(E) : Auger (Environment) TEE : Sample tube environment ST : Shelby tube	<b>TERMINOLOGY</b> "traces" 1-10% "some" 10-20% "adjective" (...y) 20-35% "and" 35-50%	<b>BEDROCK QUALITY INDEX</b> % RQD QUALIFYING 0-25 Very poor 25-50 Poor 50-75 Fair 75-90 Good 90-100 Excellent		<b>COMPACTNESS INDEX "N"</b> Very loose 0-4 Loose 4-10 Compact 10-30 Dense 30-50 Very dense >50	<b>WATER LEVEL</b> Date: 2023-08-22 Date: 2023-07-20 Depth: 1.25 Depth: 1.77
		<b>SAMPLE STATE</b> Remoulded Intact Lost Diamond drilling	<b>SYMBOLS</b> N: Standard penetration index R: Refusal (N > 100) R.Q.D.: Rock Quality Designation % R.Q.D. $\geq$ Core > 4 in. (10 cm) drilled length	<b>CLASSIFICATION (UNIFIED SYSTEM)</b> Clay < 0.002 mm Silt 0.002 - 0.075 mm Sand 0.075 - 4.75 mm Gravel 4.75 - 75 mm Cobbles 75 - 300 mm Boulders > 300 mm	

<b>SAMPLE STATE</b> Remoulded Intact Lost Diamond drilling	<b>SYMBOLS</b> N: Standard penetration index R: Refusal (N > 100) R.Q.D.: Rock Quality Designation % R.Q.D. $\geq$ Core > 4 in. (10 cm) drilled length	<b>CLASSIFICATION (UNIFIED SYSTEM)</b> Clay < 0.002 mm Silt 0.002 - 0.075 mm Sand 0.075 - 4.75 mm Gravel 4.75 - 75 mm Cobbles 75 - 300 mm Boulders > 300 mm	<b>CONSISTENCY</b> Very soft Soft Firm Stiff Very stiff Hard	<b>SHEAR RESISTANCE (Su)</b> <12 kPa 12-25 kPa 25-50 kPa 50-100 kPa 100-200 kPa >200 kPa
--	--	---	--	--



Remark(s) :

Borehole - standard.sty





Photographic Report of Rock Samples

Project : 12615684-A1

Client : Medusa Limited Partnership

Borehole Date : July 3-6, 2023

Site : Ottawa, Ontario

Depth : 25.43 to 28.30 m

Borehole : BH-101-23

Elevation : 65.24 to 62.37 m

Photograph of Dry Rock



Photograph of Wet Rock





Photographic Report of Rock Samples

Project : 12615684-A1

Client : Medusa Limited Partnership

Borehole Date : July 6-10, 2023

Site : Ottawa, Ontario

Depth : 22.63 to 25.25 m

Borehole : BH-103-23

Elevation : 68.03 to 65.41 m

**Photograph of Dry Rock**



**Photograph of Wet Rock**



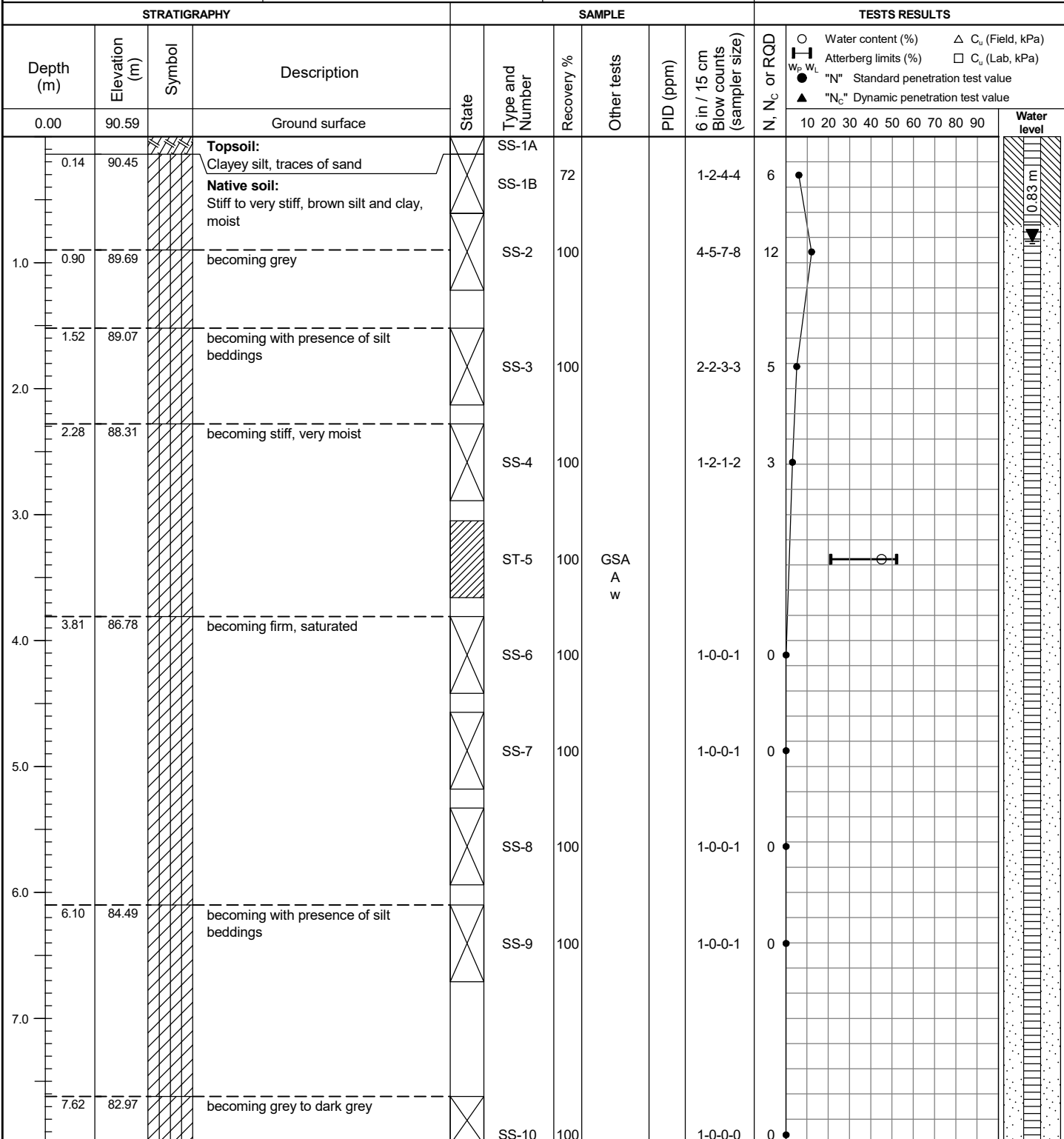


# BOREHOLE REPORT

**Borehole No. BH-01**

CLIENT: MEDUSA LP PROJECT: PROPOSED SORTATION FACILITY LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO DESCRIBED BY: F. ARGUIN VERIFIED BY: M.-A. RICHARD / A. FIORILLI	GEODETIC COORDINATES (MTM, NAD-83) (m) X : 366477.6 Y : 5017942.8 Z : 90.59	▼ - WATER LEVEL Date : 2021-05-19 Depth (m) : 0.83 Location plan : 11220797-A1-1
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Borehole type : Auger Core bit size : B Hammer type : Automatic Energy ratio : Date (start) : 2021-04-19 Date (finish) : 2021-04-19	<b>SAMPLE TYPE</b>	SS(E) - Split Spoon (Environment) RC(E) - Rock diamond core AU(E) - Auger TEE - Sampling Tube Environment ST - Shelby tube GS(E) - Grab sample	<b>SAMPLE STATE</b>	☒ Remoulded ▨ Intact ◻ Diamond drilling ■ Lost	<b>TEST SYMBOL</b>	GSA: grain size analysis CA: chemical analysis w <sub>l</sub> : liquid limit w <sub>p</sub> : plastic limit w: water content C <sub>u</sub> : undrained shear strength S <sub>r</sub> : sensitivity Dup: duplicate sample
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See the attached explicative note for the complete list of symbols and abbreviations



# BOREHOLE REPORT

**Borehole No. BH-01**

CLIENT: MEDUSA LP PROJECT: PROPOSED SORTATION FACILITY LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO DESCRIBED BY: F. ARGUIN      VERIFIED BY: M.-A. RICHARD / A. FIORILLI	GEODETIC COORDINATES (MTM, NAD-83) (m) X : 366477.6 Y : 5017942.8 Z : 90.59	▼ - WATER LEVEL Date : 2021-05-19 Depth (m) : 0.83 Location plan : 11220797-A1-1
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Borehole type : Auger Core bit size : B Hammer type : Automatic Energy ratio : Date (start) : 2021-04-19 Date (finish) : 2021-04-19	<b>SAMPLE TYPE</b>	SS(E) - Split Spoon (Environment) RC(E) - Rock diamond core AU(E) - Auger TEE - Sampling Tube Environment ST - Shelby tube GS(E) - Grab sample	<b>SAMPLE STATE</b>	<input checked="" type="checkbox"/> Remoulded <input checked="" type="checkbox"/> Intact <input type="checkbox"/> Diamond drilling <input checked="" type="checkbox"/> Lost	<b>TEST SYMBOL</b>	GSA: grain size analysis CA: chemical analysis w <sub>l</sub> : liquid limit w <sub>p</sub> : plastic limit w: water content C <sub>u</sub> : undrained shear strength S <sub>r</sub> : sensitivity Dup: duplicate sample
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STRATIGRAPHY				SAMPLE						TESTS RESULTS	
Depth (m)	Elevation (m)	Symbol	Description	State	Type and Number	Recovery %	Other tests	PID (ppm)	6 in / 15 cm Blow counts (sampler size)	N, N <sub>c</sub> or RQD	○ Water content (%)      △ C <sub>u</sub> (Field, kPa) □ Atterberg limits (%)      □ C <sub>u</sub> (Lab, kPa) ● "N" Standard penetration test value ▲ "N <sub>c</sub> " Dynamic penetration test value
8.00	82.59		Ground surface	X							10 20 30 40 50 60 70 80 90
9.76	80.83		End of sampling Beginning of dynamic penetration test	X	SS-11	100	GSA A w		1-0-0-0	0	
9.0											
10.0											
11.0											
12.0											
13.0											
14.0											
15.0											

See the attached explicative note for the complete list of symbols and abbreviations



# BOREHOLE REPORT

**Borehole No. BH-01**

CLIENT: MEDUSA LP PROJECT: PROPOSED SORTATION FACILITY LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO DESCRIBED BY: F. ARGUIN      VERIFIED BY: M.-A. RICHARD / A. FIORILLI	GEODETIC COORDINATES (MTM, NAD-83) (m) X : 366477.6 Y : 5017942.8 Z : 90.59	▼ - WATER LEVEL Date : 2021-05-19 Depth (m) : 0.83 Location plan : 11220797-A1-1
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Borehole type : Auger Core bit size : B Hammer type : Automatic Energy ratio : Date (start) : 2021-04-19 Date (finish) : 2021-04-19	<b>SAMPLE TYPE</b>	SS(E) - Split Spoon (Environment) RC(E) - Rock diamond core AU(E) - Auger TEE - Sampling Tube Environment ST - Shelby tube GS(E) - Grab sample	<b>SAMPLE STATE</b>	<input checked="" type="checkbox"/> Remoulded <input checked="" type="checkbox"/> Intact <input type="checkbox"/> Diamond drilling <input checked="" type="checkbox"/> Lost	<b>TEST SYMBOL</b>	GSA: grain size analysis CA: chemical analysis w <sub>l</sub> : liquid limit w <sub>p</sub> : plastic limit w : water content C <sub>u</sub> : undrained shear strength S <sub>r</sub> : sensitivity Dup: duplicate sample
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STRATIGRAPHY				SAMPLE						TESTS RESULTS									
Depth (m)	Elevation (m)	Symbol	Description	State	Type and Number	Recovery %	Other tests	PID (ppm)	6 in / 15 cm Blow counts (sampler size)	N, N <sub>c</sub> or RQD	w <sub>p</sub>	w <sub>L</sub>	Atterberg limits (%)	"N" Standard penetration test value	"N <sub>c</sub> " Dynamic penetration test value	C <sub>u</sub> (Field, kPa)	C <sub>u</sub> (Lab, kPa)	Water level	
16.00	74.59		Ground surface																
21.16	69.43		End of dynamic penetration test End of borehole																

Depth (m)	Dynamic Penetration Test Value (N <sub>c</sub> )
16.00	4
16.50	5
17.00	4
17.50	3
18.00	5
18.50	3
19.00	3
19.50	2
20.00	5
20.50	4
21.00	3
21.16	8

See the attached explicative note for the complete list of symbols and abbreviations

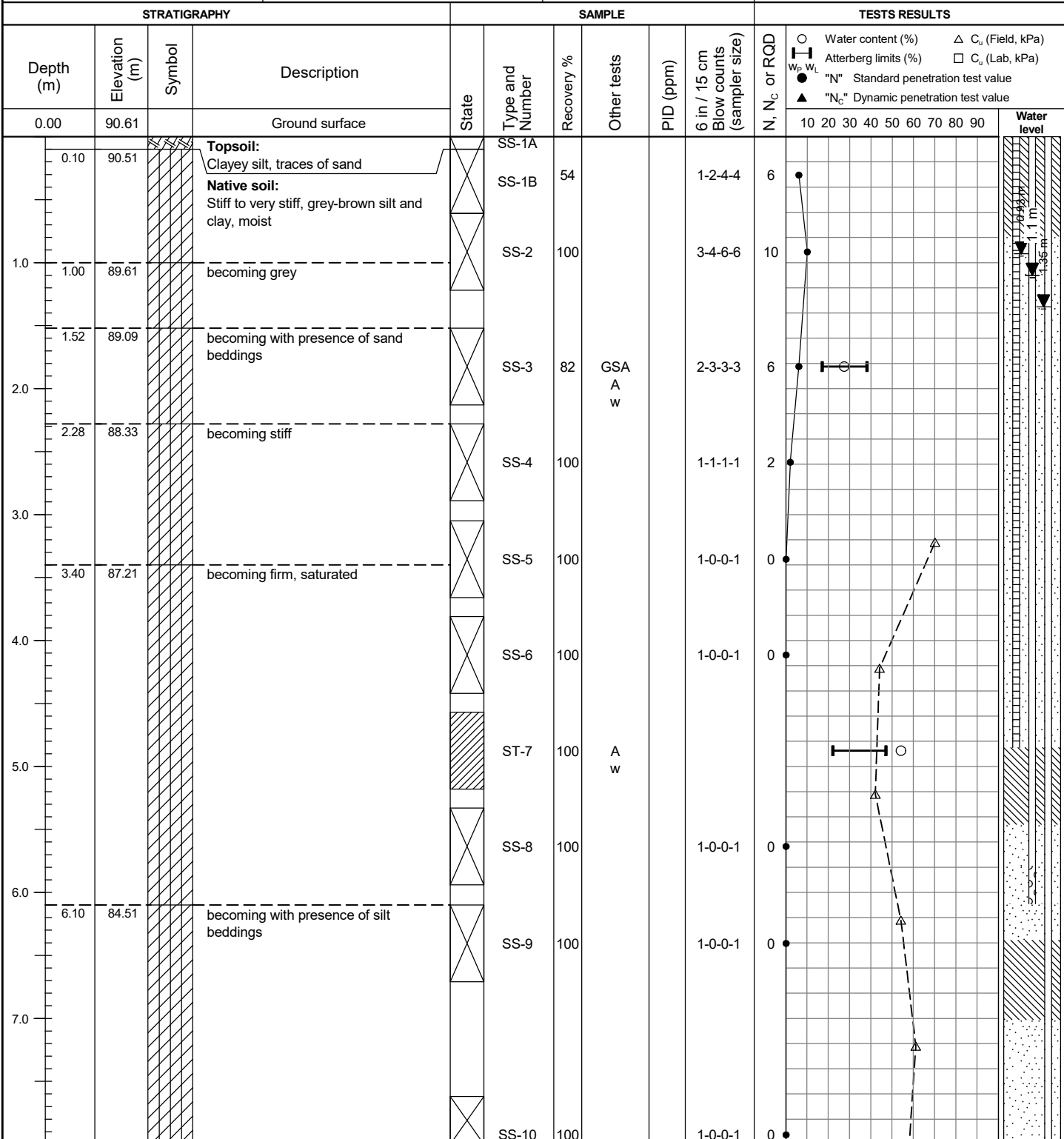


# BOREHOLE REPORT

Borehole No. **BH-02**

CLIENT: MEDUSA LP PROJECT: PROPOSED SORTATION FACILITY LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO DESCRIBED BY: F. ARGUIN VERIFIED BY: M.-A. RICHARD / A. FIORILLI	GEODETIC COORDINATES (MTM, NAD-83) (m) X : 366599.6 Y : 5018011.4 Z : 90.61	- WATER LEVEL Date : 2021-05-19 Depth (m) : 1.1 0.93 ; 1.35 Location plan : 11220797-A1-1
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Borehole type : Auger + Casing Core bit size : B+NQ Hammer type : Automatic Energy ratio : Date (start) : 2021-04-21 Date (finish) : 2021-04-22	<b>SAMPLE TYPE</b> SS(E) - Split Spoon (Environment) RC(E) - Rock diamond core AU(E) - Auger TEE - Sampling Tube Environment ST - Shelby tube GS(E) - Grab sample	<b>SAMPLE STATE</b> <input checked="" type="checkbox"/> Remoulded <input checked="" type="checkbox"/> Intact <input type="checkbox"/> Diamond drilling <input type="checkbox"/> Lost	<b>TEST SYMBOL</b> GSA: grain size analysis CA: chemical analysis w <sub>l</sub> : liquid limit w <sub>p</sub> : plastic limit w : water content C <sub>u</sub> : undrained shear strength S <sub>r</sub> : sensitivity Dup: duplicate sample
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See the attached explicative note for the complete list of symbols and abbreviations



# BOREHOLE REPORT

Borehole No.

**BH-02**

CLIENT: MEDUSA LP	PROJECT: PROPOSED SORTATION FACILITY	LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO	DESCRIBED BY: F. ARGUIN	VERIFIED BY: M.-A. RICHARD / A. FIORILLI	GEODETIC COORDINATES (MTM, NAD-83) (m) X : 366599.6 Y : 5018011.4 Z : 90.61	- WATER LEVEL Date : 2021-05-19 Depth (m) : 1.1 0.93 ; 1.35 Location plan : 11220797-A1-1
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Borehole type : Auger + Casing Core bit size : B+NQ Hammer type : Automatic Energy ratio : Date (start) : 2021-04-21 Date (finish) : 2021-04-22	<b>SAMPLE TYPE</b> SS(E) - Split Spoon (Environment) RC(E) - Rock diamond core AU(E) - Auger TEE - Sampling Tube Environment ST - Shelby tube GS(E) - Grab sample	<b>SAMPLE STATE</b> <input checked="" type="checkbox"/> Remoulded <input checked="" type="checkbox"/> Intact <input type="checkbox"/> Diamond drilling <input checked="" type="checkbox"/> Lost	<b>TEST SYMBOL</b> GSA: grain size analysis CA: chemical analysis w <sub>L</sub> : liquid limit w <sub>p</sub> : plastic limit w: water content C <sub>u</sub> : undrained shear strength S <sub>r</sub> : sensitivity Dup: duplicate sample
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STRATIGRAPHY			SAMPLE					TESTS RESULTS										
Depth (m)	Elevation (m)	Symbol	Description	State	Type and Number	Recovery %	Other tests	PID (ppm)	6 in / 15 cm Blow counts (sampler size)	N, N <sub>c</sub> or RQD	○ Water content (%)    △ C <sub>u</sub> (Field, kPa) □ Atterberg limits (%)    □ C <sub>u</sub> (Lab, kPa) ● "N" Standard penetration test value ▲ "N <sub>c</sub> " Dynamic penetration test value							
8.00	82.61		Ground surface															
9.15	81.46		Stiff, grey clayey silt, traces of sand, saturated		SS-11	49	GSA A w		1-0-0-0	0								
10.0					SS-12	51			4-3-2-2	5								
10.67	79.94		Loose to very loose, grey silty and gravelly sand, traces of clay, saturated		SS-13	100			1-2-2-2	4								
12.0					SS-14	71	GSA A w		1-1-4-1	5								
13.0					SS-15	100			2-1-0-3	1								
14.0					SS-16	57			3-1-1-2	2								
15.0					SS-17	100			1-1-1-3	2								
					SS-18	13			1-1-0-1	1								
					SS-19	72	GSA A w		1-5-1-1	6								

See the attached explicative note for the complete list of symbols and abbreviations

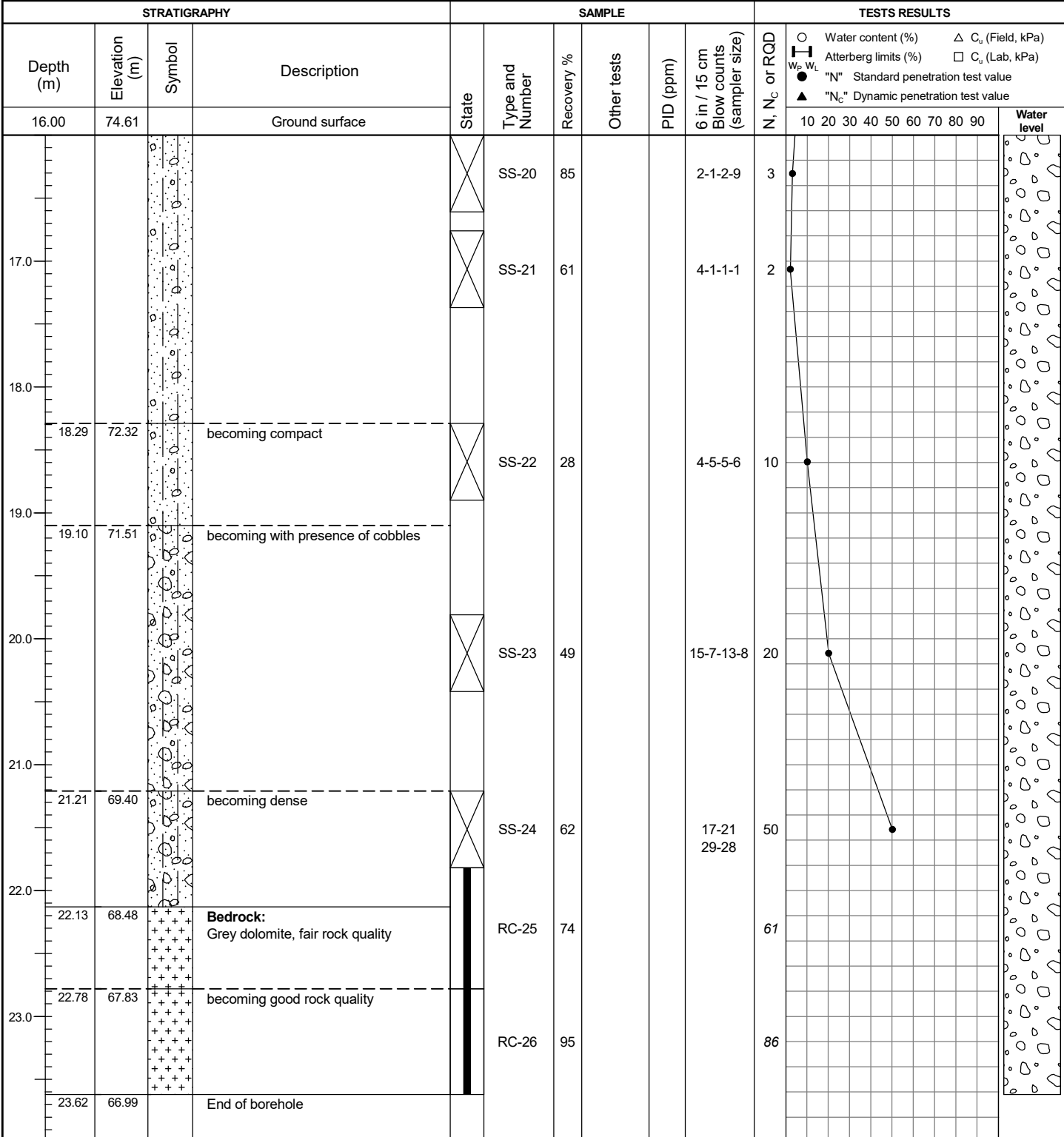


# BOREHOLE REPORT

**Borehole No. BH-02**

CLIENT: MEDUSA LP PROJECT: PROPOSED SORTATION FACILITY LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO DESCRIBED BY: F. ARGUIN      VERIFIED BY: M.-A. RICHARD / A. FIORILLI	GEODETIC COORDINATES (MTM, NAD-83) (m) X : 366599.6 Y : 5018011.4 Z : 90.61	▼ - WATER LEVEL Date : 2021-05-19 Depth (m) : 1.1    0.93 ; 1.35 Location plan : 11220797-A1-1
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Borehole type : Auger + Casing Core bit size : B+NQ Hammer type : Automatic Energy ratio : Date (start) : 2021-04-21 Date (finish) : 2021-04-22	<b>SAMPLE TYPE</b>	SS(E) - Split Spoon (Environment) RC(E) - Rock diamond core AU(E) - Auger TEE - Sampling Tube Environment ST - Shelby tube GS(E) - Grab sample	<b>SAMPLE STATE</b>	<input checked="" type="checkbox"/> Remoulded <input checked="" type="checkbox"/> Intact <input type="checkbox"/> Diamond drilling <input type="checkbox"/> Lost	<b>TEST SYMBOL</b>	GSA: grain size analysis CA: chemical analysis w <sub>l</sub> : liquid limit w <sub>p</sub> : plastic limit w : water content C <sub>u</sub> : undrained shear strength S <sub>r</sub> : sensitivity Dup: duplicate sample
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See the attached explicative note for the complete list of symbols and abbreviations





Photo 1 : BH-02 Core box – Dry rock



Photo 2 : BH-02 Core box – Wet rock

## Borehole No. BH-02

Proposed Sortation Facility  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario



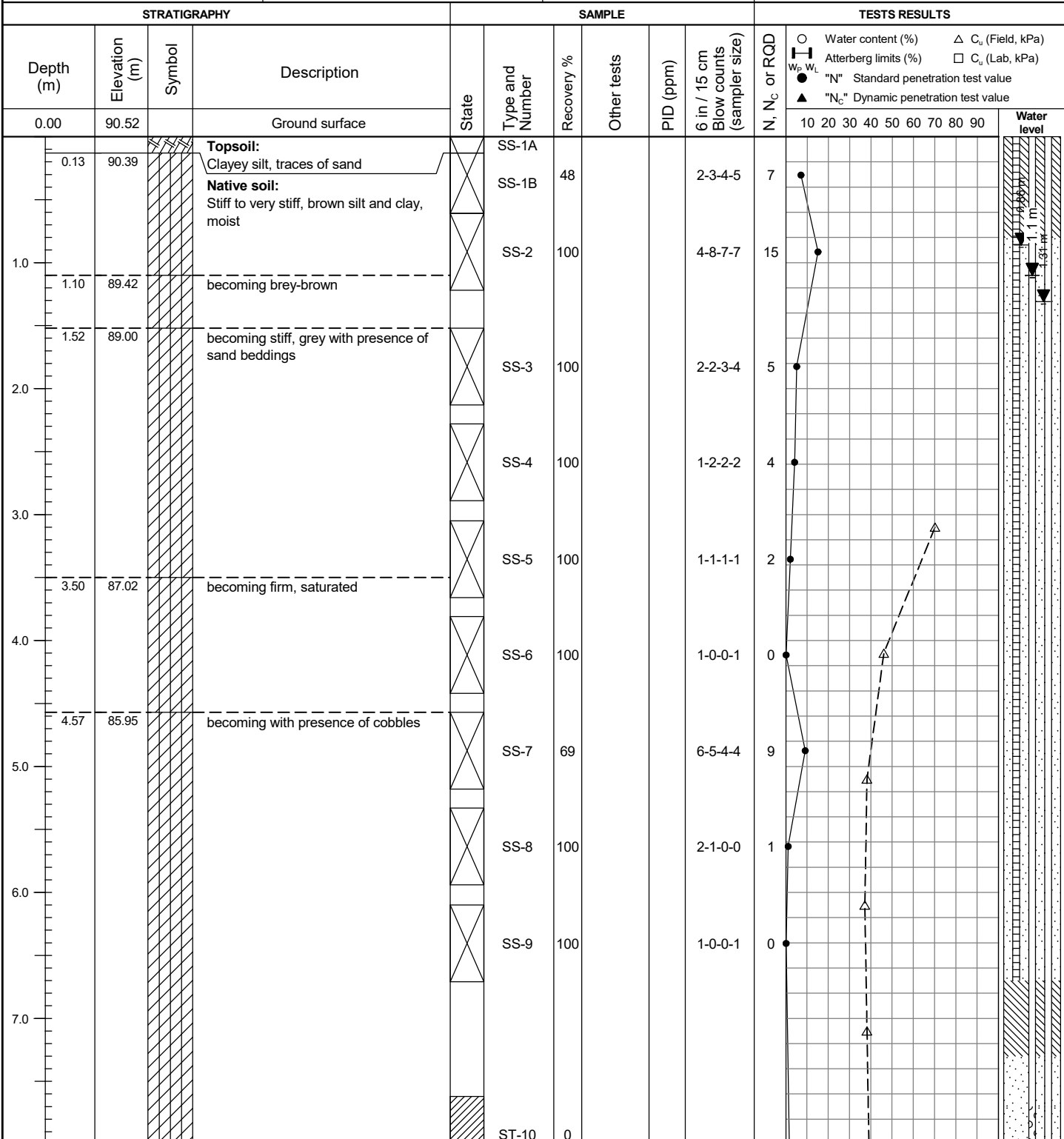


# BOREHOLE REPORT

**Borehole No. BH-03**

CLIENT: MEDUSA LP PROJECT: PROPOSED SORTATION FACILITY LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO DESCRIBED BY: F. ARGUIN      VERIFIED BY: M.-A. RICHARD / A. FIORILLI	GEODETIC COORDINATES (MTM, NAD-83) (m) X : 366427.8 Y : 5017867.9 Z : 90.52	▼ - WATER LEVEL Date : 2021-05-19 Depth (m) : 1.1    0.86 ; 1.31 Location plan : 11220797-A1-1
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Borehole type : Auger + Casing Core bit size : B+NQ Hammer type : Automatic Energy ratio : Date (start) : 2021-04-19 Date (finish) : 2021-04-20	<b>SAMPLE TYPE</b> SS(E) - Split Spoon (Environment) RC(E) - Rock diamond core AU(E) - Auger TEE - Sampling Tube Environment ST - Shelby tube GS(E) - Grab sample	<b>SAMPLE STATE</b> <input checked="" type="checkbox"/> Remoulded <input checked="" type="checkbox"/> Intact <input type="checkbox"/> Diamond drilling <input type="checkbox"/> Lost	<b>TEST SYMBOL</b> GSA: grain size analysis CA: chemical analysis w <sub>l</sub> : liquid limit w <sub>p</sub> : plastic limit w : water content C <sub>u</sub> : undrained shear strength S <sub>r</sub> : sensitivity Dup: duplicate sample
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See the attached explicative note for the complete list of symbols and abbreviations



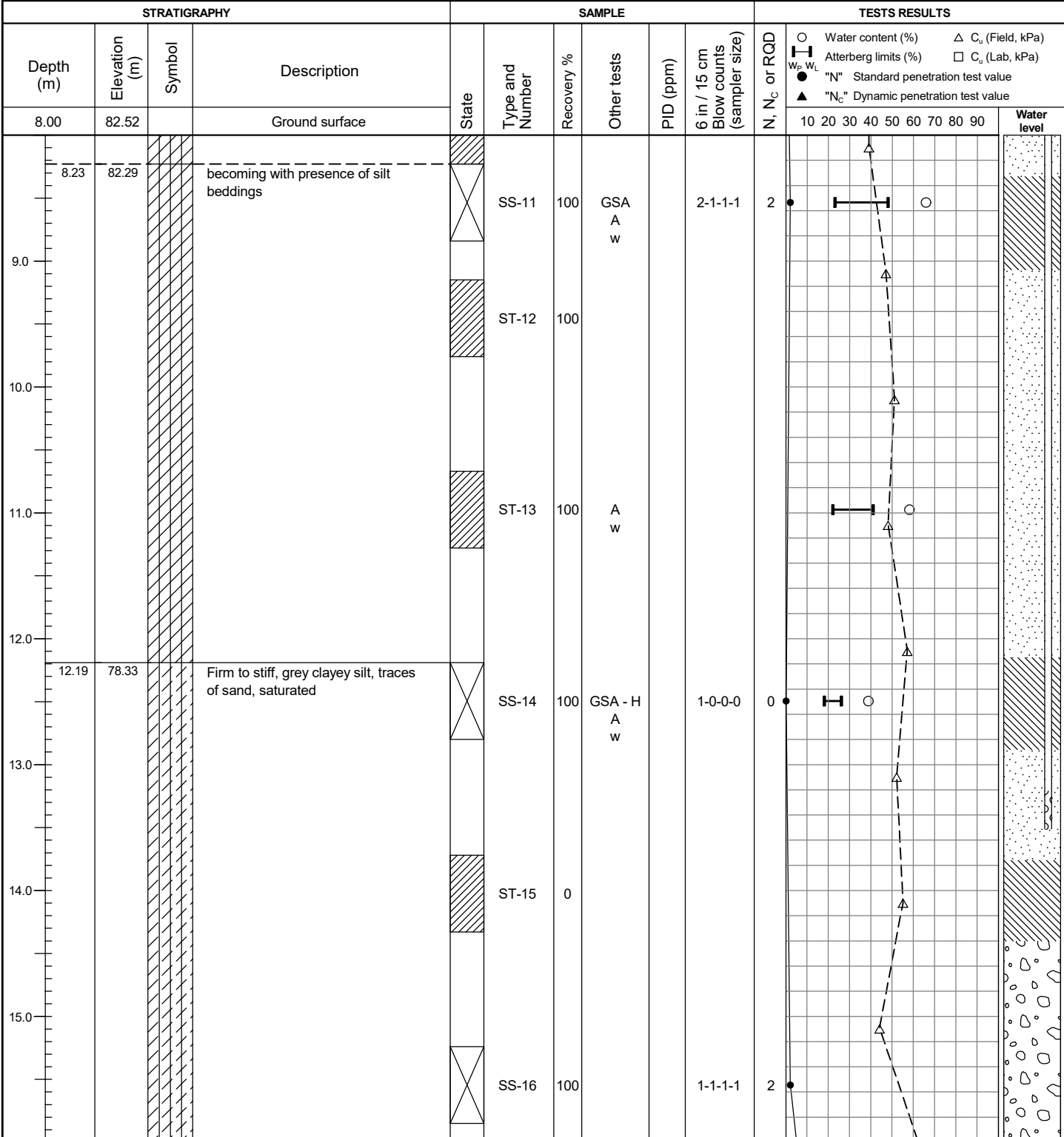
# BOREHOLE REPORT

Borehole No.

**BH-03**

CLIENT: MEDUSA LP	GEODETIC COORDINATES (MTM, NAD-83) (m)	▼ - WATER LEVEL Date : 2021-05-19 Depth (m) : 1.1 0.86 ; 1.31
PROJECT: PROPOSED SORTATION FACILITY	X : 366427.8 Y : 5017867.9 Z : 90.52	
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO	DESCRIBED BY: F. ARGUIN	VERIFIED BY: M.-A. RICHARD / A. FIORILLI

Borehole type : Auger + Casing	SAMPLE TYPE	SS(E) - Split Spoon (Environment)	SAMPLE STATE	☒ Remoulded	TEST SYMBOL	GSA: grain size analysis
Core bit size : B+NQ		RC(E) - Rock diamond core		☒ Intact		CA: chemical analysis
Hammer type : Automatic		AU(E) - Auger		☐ Diamond drilling		w <sub>l</sub> : liquid limit
Energy ratio :		TEE - Sampling Tube Environment		■ Lost		w <sub>p</sub> : plastic limit
Date (start) : 2021-04-19		ST - Shelby tube				w : water content
Date (finish) : 2021-04-20		GS(E) - Grab sample				C <sub>u</sub> : undrained shear strength



See the attached explicative note for the complete list of symbols and abbreviations



# BOREHOLE REPORT

**Borehole No. BH-03**

CLIENT: MEDUSA LP PROJECT: PROPOSED SORTATION FACILITY LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO DESCRIBED BY: F. ARGUIN      VERIFIED BY: M.-A. RICHARD / A. FIORILLI	GEODETIC COORDINATES (MTM, NAD-83) (m) X : 366427.8 Y : 5017867.9 Z : 90.52	▼ - WATER LEVEL Date : 2021-05-19 Depth (m) : 1.1    0.86 ; 1.31 Location plan : 11220797-A1-1
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Borehole type : Auger + Casing Core bit size : B+NQ Hammer type : Automatic Energy ratio : Date (start) : 2021-04-19 Date (finish) : 2021-04-20	<b>SAMPLE TYPE</b>	SS(E) - Split Spoon (Environment) RC(E) - Rock diamond core AU(E) - Auger TEE - Sampling Tube Environment ST - Shelby tube GS(E) - Grab sample	<b>SAMPLE STATE</b>	<input checked="" type="checkbox"/> Remoulded <input checked="" type="checkbox"/> Intact <input type="checkbox"/> Diamond drilling <input type="checkbox"/> Lost	<b>TEST SYMBOL</b>	GSA: grain size analysis CA: chemical analysis w <sub>l</sub> : liquid limit w <sub>p</sub> : plastic limit w : water content C <sub>u</sub> : undrained shear strength S <sub>r</sub> : sensitivity Dup: duplicate sample
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STRATIGRAPHY				SAMPLE					TESTS RESULTS				
Depth (m)	Elevation (m)	Symbol	Description	State	Type and Number	Recovery %	Other tests	PID (ppm)	6 in / 15 cm Blow counts (sampler size)	N, N <sub>c</sub> or RQD	○ Water content (%)    △ C <sub>u</sub> (Field, kPa) □ Atterberg limits (%)    □ C <sub>u</sub> (Lab, kPa) ● "N" Standard penetration test value ▲ "N <sub>c</sub> " Dynamic penetration test value	10 20 30 40 50 60 70 80 90	Water level
16.00	74.52		Ground surface										
16.20	74.32		Compact to loose, grey gravelly and silty sand, traces of clay, saturated										
17.0					SS-17	59			2-6-6-7	12			
18.0					SS-18	64	GSA - H A w		3-3-6-7	9			
19.0					SS-19	43				R			
20.0	19.97	70.55	<b>Bedrock:</b> Grey dolomite, good rock quality						27 50/8cm				
21.0			- joint from 20.75 to 20.76m		RC-20	97				79			
22.0			- fractured from 21.26 to 21.36m		RC-21	92				76			
23.0	22.81	67.71	End of borehole										

See the attached explicative note for the complete list of symbols and abbreviations



Photo 3 : BH-03 Core box – Dry rock



Photo 4 : BH-03 Core box – Wet rock

### Borehole No. BH-03

Proposed Sortation Facility  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario



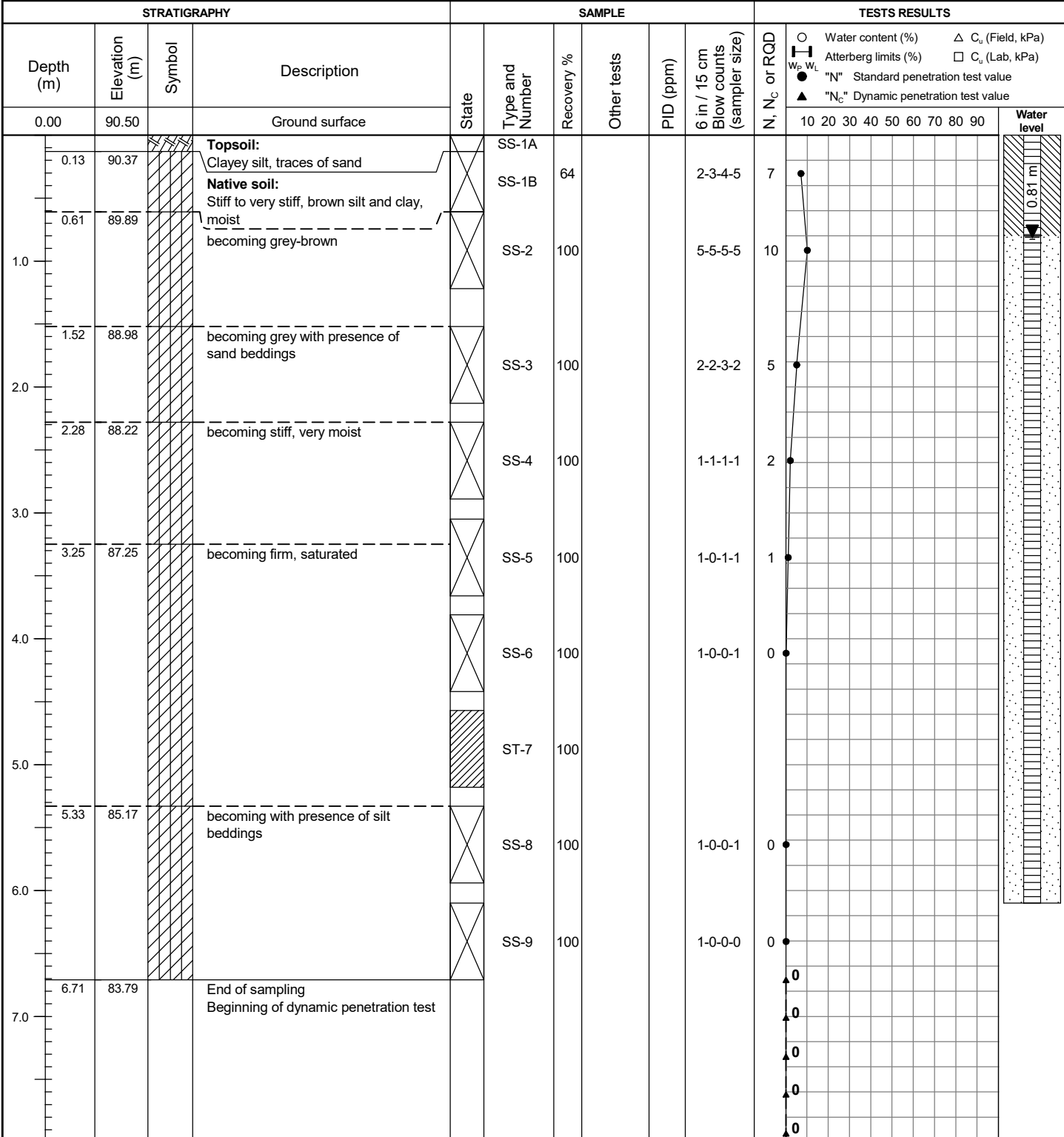


# BOREHOLE REPORT

Borehole No. **BH-04**

CLIENT: MEDUSA LP	GEODETIC COORDINATES (MTM, NAD-83) (m)	▼ - WATER LEVEL Date : 2021-05-19 Depth (m) : 0.81
PROJECT: PROPOSED SORTATION FACILITY	X : 366567.3 Y : 5017946.1 Z : 90.50	
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO	DESCRIBED BY: F. ARGUIN	VERIFIED BY: M.-A. RICHARD / A. FIORILLI

Borehole type : Auger	SAMPLE TYPE	SS(E) - Split Spoon (Environment)	SAMPLE STATE	☒ Remoulded	TEST SYMBOL	GSA: grain size analysis
Core bit size : B		RC(E) - Rock diamond core		☒ Intact		CA: chemical analysis
Hammer type : Automatic	AU(E) - Auger	TEE - Sampling Tube Environment	☐ Diamond drilling	w <sub>l</sub> : liquid limit	w <sub>p</sub> : plastic limit	w : water content
Energy ratio :	ST - Shelby tube	GS(E) - Grab sample	■ Lost	C <sub>u</sub> : undrained shear strength	S <sub>r</sub> : sensitivity	Dup: duplicate sample
Date (start) : 2021-04-19						
Date (finish) : 2021-04-19						



See the attached explicative note for the complete list of symbols and abbreviations





# BOREHOLE REPORT

**Borehole No. BH-04**

CLIENT: MEDUSA LP PROJECT: PROPOSED SORTATION FACILITY LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO DESCRIBED BY: F. ARGUIN      VERIFIED BY: M.-A. RICHARD / A. FIORILLI	GEODETIC COORDINATES (MTM, NAD-83) (m) X : 366567.3 Y : 5017946.1 Z : 90.50	▼ - WATER LEVEL Date : 2021-05-19 Depth (m) : 0.81 Location plan : 11220797-A1-1
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Borehole type : Auger Core bit size : B Hammer type : Automatic Energy ratio : Date (start) : 2021-04-19 Date (finish) : 2021-04-19	<b>SAMPLE TYPE</b>	SS(E) - Split Spoon (Environment) RC(E) - Rock diamond core AU(E) - Auger TEE - Sampling Tube Environment ST - Shelby tube GS(E) - Grab sample	<b>SAMPLE STATE</b>	<input checked="" type="checkbox"/> Remoulded <input checked="" type="checkbox"/> Intact <input type="checkbox"/> Diamond drilling <input checked="" type="checkbox"/> Lost	<b>TEST SYMBOL</b>	GSA: grain size analysis CA: chemical analysis w <sub>l</sub> : liquid limit w <sub>p</sub> : plastic limit w: water content C <sub>u</sub> : undrained shear strength S <sub>r</sub> : sensitivity Dup: duplicate sample
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STRATIGRAPHY				SAMPLE						TESTS RESULTS									
Depth (m)	Elevation (m)	Symbol	Description	State	Type and Number	Recovery %	Other tests	PID (ppm)	6 in / 15 cm Blow counts (sampler size)	N, N <sub>c</sub> or RQD	W <sub>p</sub>	W <sub>L</sub>	Atterberg limits (%)	"N" Standard penetration test value	"N <sub>c</sub> " Dynamic penetration test value	C <sub>u</sub> (Field, kPa)	C <sub>u</sub> (Lab, kPa)	Water level	
16.00	74.50		Ground surface																
23.0	22.73	67.77	End of dynamic penetration test End of borehole																

Depth (m)	Dynamic Penetration Test Value (N <sub>c</sub> )
16.00	5
16.50	6
17.00	23
17.50	15
18.00	12
18.50	8
19.00	9
19.50	11
20.00	8
20.50	8
21.00	8
21.50	9
22.00	13
22.50	10
23.00	11
23.50	11
24.00	13
24.50	15
25.00	18
25.50	34
26.00	45
26.50	100

See the attached explicative note for the complete list of symbols and abbreviations



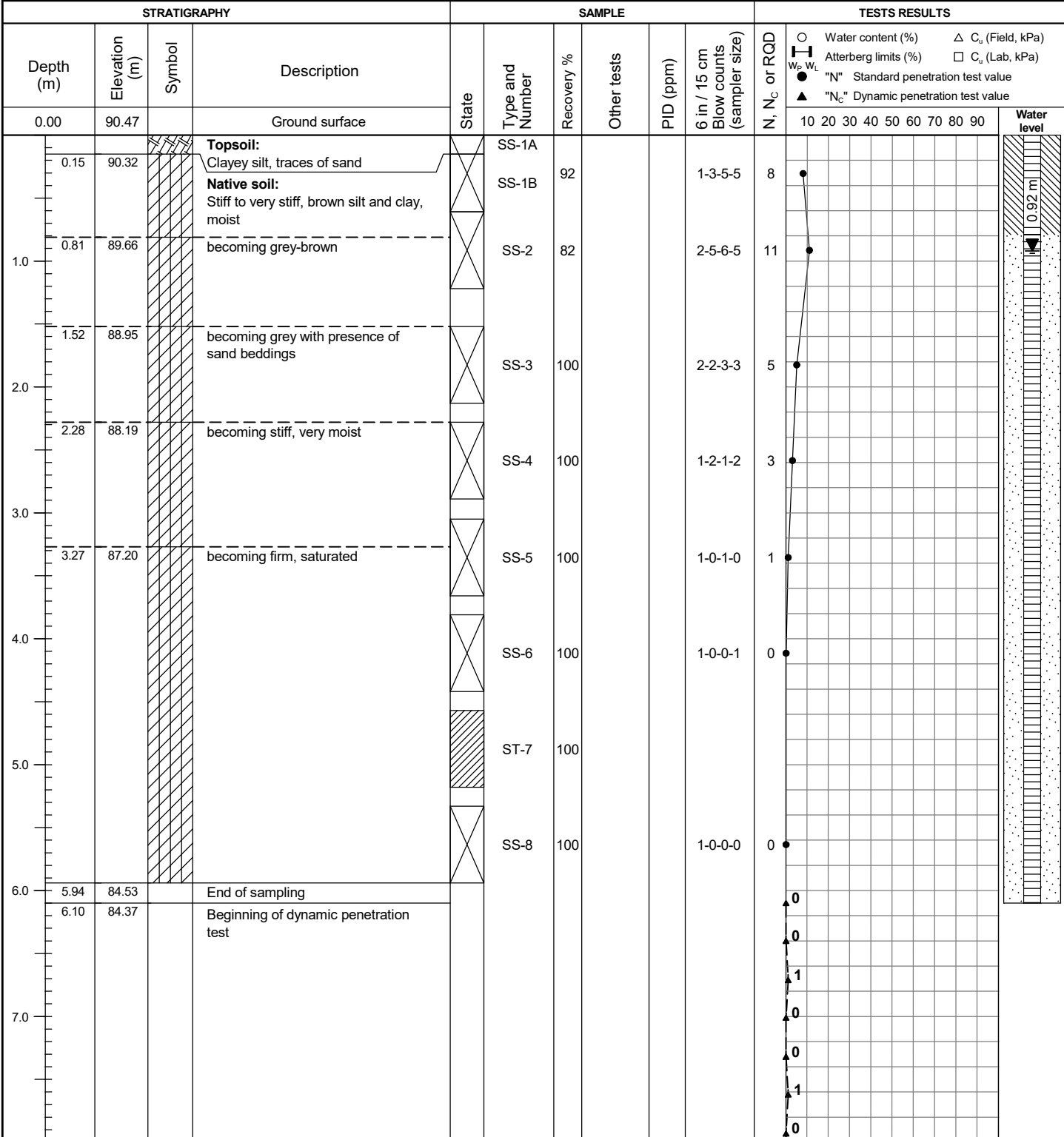


# BOREHOLE REPORT

**Borehole No. BH-05**

CLIENT: MEDUSA LP PROJECT: PROPOSED SORTATION FACILITY LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO DESCRIBED BY: F. ARGUIN      VERIFIED BY: M.-A. RICHARD / A. FIORILLI	GEODETIC COORDINATES (MTM, NAD-83) (m) X : 366518.8 Y : 5017869.4 Z : 90.47	▼ - WATER LEVEL Date : 2021-05-19 Depth (m) : 0.92 Location plan : 11220797-A1-1
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Borehole type : Auger Core bit size : B Hammer type : Automatic Energy ratio : Date (start) : 2021-04-28 Date (finish) : 2021-04-28	<b>SAMPLE TYPE</b>	SS(E) - Split Spoon (Environment) RC(E) - Rock diamond core AU(E) - Auger TEE - Sampling Tube Environment ST - Shelby tube GS(E) - Grab sample	<b>SAMPLE STATE</b>	<input checked="" type="checkbox"/> Remoulded <input checked="" type="checkbox"/> Intact <input type="checkbox"/> Diamond drilling <input checked="" type="checkbox"/> Lost	<b>TEST SYMBOL</b>	GSA: grain size analysis CA: chemical analysis w <sub>l</sub> : liquid limit w <sub>p</sub> : plastic limit w: water content C <sub>u</sub> : undrained shear strength S <sub>r</sub> : sensitivity Dup: duplicate sample
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See the attached explicative note for the complete list of symbols and abbreviations



# BOREHOLE REPORT

**Borehole No. BH-05**

CLIENT: MEDUSA LP PROJECT: PROPOSED SORTATION FACILITY LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO DESCRIBED BY: F. ARGUIN      VERIFIED BY: M.-A. RICHARD / A. FIORILLI	GEODETIC COORDINATES (MTM, NAD-83) (m) X : 366518.8 Y : 5017869.4 Z : 90.47	▼ - WATER LEVEL Date : 2021-05-19 Depth (m) : 0.92 Location plan : 11220797-A1-1
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Borehole type : Auger Core bit size : B Hammer type : Automatic Energy ratio : Date (start) : 2021-04-28 Date (finish) : 2021-04-28	<b>SAMPLE TYPE</b>	SS(E) - Split Spoon (Environment) RC(E) - Rock diamond core AU(E) - Auger TEE - Sampling Tube Environment ST - Shelby tube GS(E) - Grab sample	<b>SAMPLE STATE</b>	<input checked="" type="checkbox"/> Remoulded <input checked="" type="checkbox"/> Intact <input type="checkbox"/> Diamond drilling <input checked="" type="checkbox"/> Lost	<b>TEST SYMBOL</b>	GSA: grain size analysis CA: chemical analysis w <sub>l</sub> : liquid limit w <sub>p</sub> : plastic limit w : water content C <sub>u</sub> : undrained shear strength S <sub>v</sub> : sensitivity Dup: duplicate sample
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STRATIGRAPHY				SAMPLE						TESTS RESULTS									
Depth (m)	Elevation (m)	Symbol	Description	State	Type and Number	Recovery %	Other tests	PID (ppm)	6 in / 15 cm Blow counts (sampler size)	N, N <sub>c</sub> or RQD	w <sub>p</sub>	w <sub>L</sub>	Atterberg limits (%)	"N" Standard penetration test value	"N <sub>c</sub> " Dynamic penetration test value	C <sub>u</sub> (Field, kPa)	C <sub>u</sub> (Lab, kPa)	Water level	
8.00	82.47		Ground surface																
9.0																			
10.0																			
11.0																			
12.0																			
13.0																			
14.0																			
15.0																			

See the attached explicative note for the complete list of symbols and abbreviations



# BOREHOLE REPORT

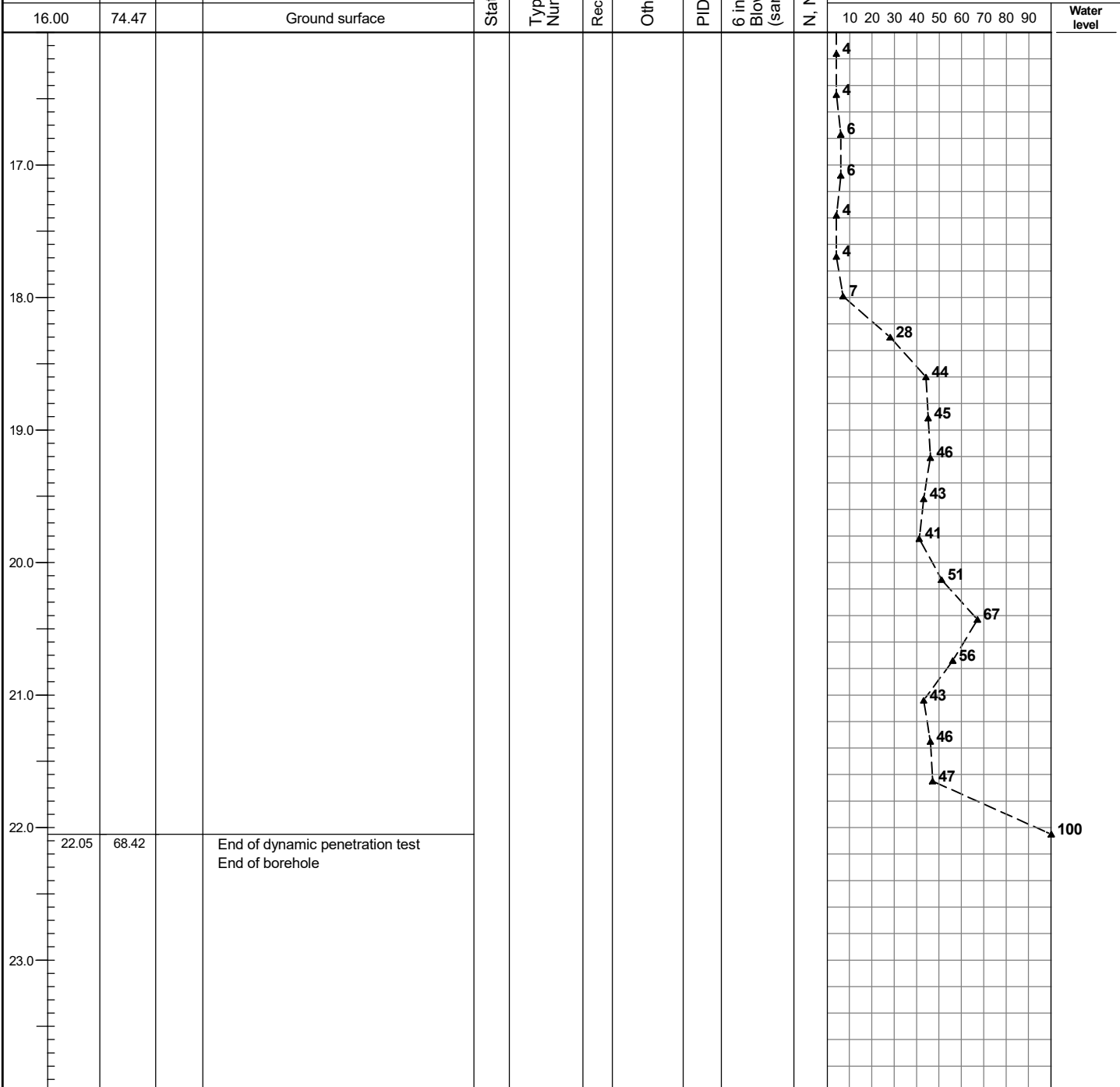
Borehole No.

**BH-05**

CLIENT: MEDUSA LP	GEODETIC COORDINATES (MTM, NAD-83) (m)	▼ - WATER LEVEL Date : 2021-05-19 Depth (m) : 0.92
PROJECT: PROPOSED SORTATION FACILITY	X : 366518.8 Y : 5017869.4 Z : 90.47	
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO	DESCRIBED BY: F. ARGUIN	VERIFIED BY: M.-A. RICHARD / A. FIORILLI

Borehole type : Auger	SAMPLE TYPE	SS(E) - Split Spoon (Environment)	SAMPLE STATE	<input checked="" type="checkbox"/> Remoulded	TEST SYMBOL	GSA: grain size analysis
Core bit size : B		RC(E) - Rock diamond core		<input checked="" type="checkbox"/> Intact		CA: chemical analysis
Hammer type : Automatic		AU(E) - Auger		<input type="checkbox"/> Diamond drilling		w <sub>l</sub> : liquid limit
Energy ratio :		TEE - Sampling Tube Environment		<input type="checkbox"/> Lost		w <sub>p</sub> : plastic limit
Date (start) : 2021-04-28		ST - Shelby tube				w : water content
Date (finish) : 2021-04-28		GS(E) - Grab sample				C <sub>u</sub> : undrained shear strength

STRATIGRAPHY				SAMPLE						TESTS RESULTS										
Depth (m)	Elevation (m)	Symbol	Description	State	Type and Number	Recovery %	Other tests	PID (ppm)	6 in / 15 cm Blow counts (sampler size)	N, N <sub>c</sub> or RQD	○ Water content (%)    Δ C <sub>u</sub> (Field, kPa) □ Atterberg limits (%)    □ C <sub>u</sub> (Lab, kPa) ● "N" Standard penetration test value ▲ "N <sub>c</sub> " Dynamic penetration test value									



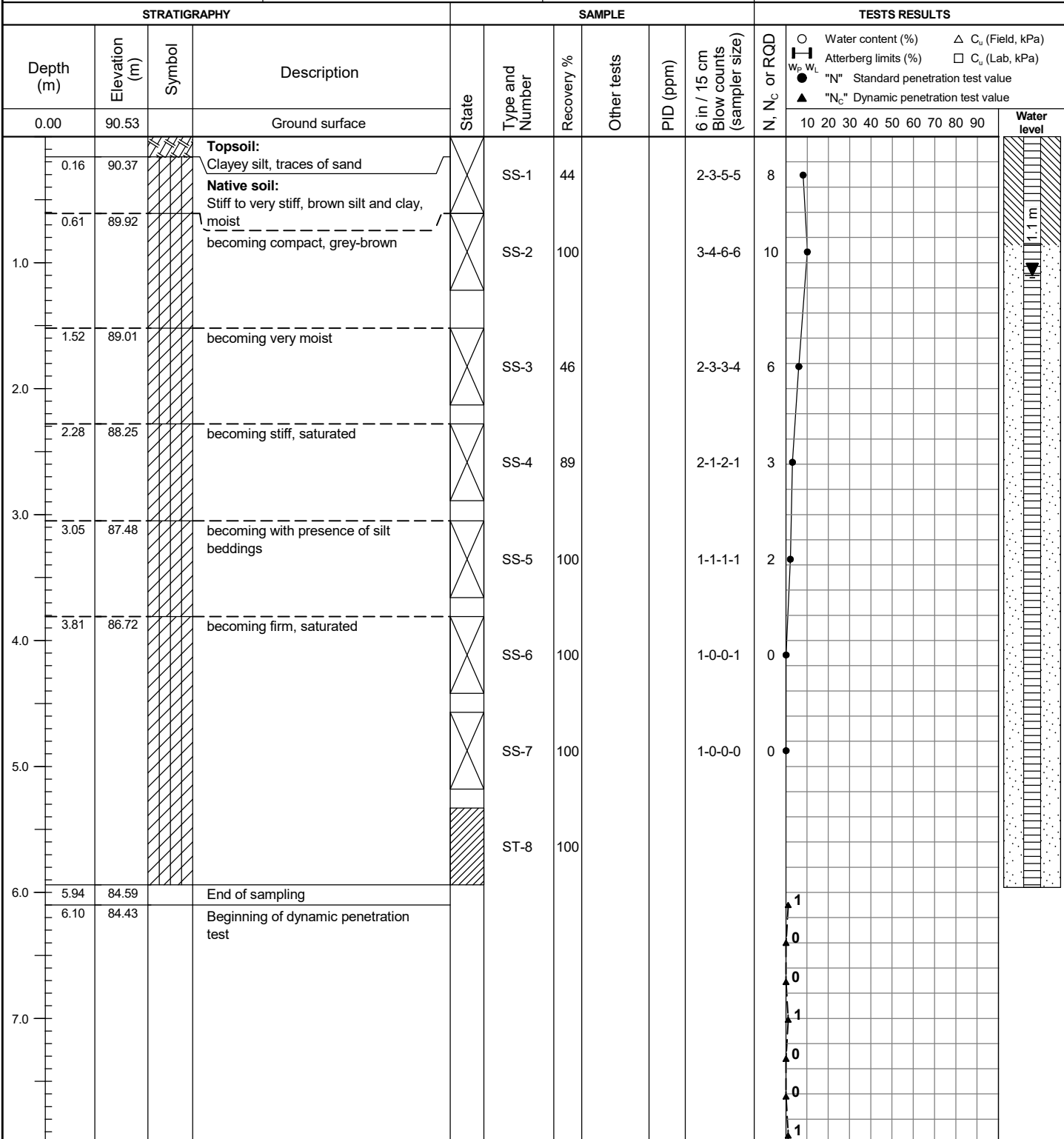


# BOREHOLE REPORT

Borehole No. **BH-06**

CLIENT: MEDUSA LP PROJECT: PROPOSED SORTATION FACILITY LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO DESCRIBED BY: F. ARGUIN      VERIFIED BY: M.-A. RICHARD / A. FIORILLI	GEODETIC COORDINATES (MTM, NAD-83) (m) X : 366640.1 Y : 5017937.4 Z : 90.53	▼ - WATER LEVEL Date : 2021-05-19 Depth (m) : 1.1 Location plan : 11220797-A1-1
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Borehole type : Auger Core bit size : B Hammer type : Automatic Energy ratio : Date (start) : 2021-04-28 Date (finish) : 2021-04-28	<b>SAMPLE TYPE</b>	SS(E) - Split Spoon (Environment) RC(E) - Rock diamond core AU(E) - Auger TEE - Sampling Tube Environment ST - Shelby tube GS(E) - Grab sample	<b>SAMPLE STATE</b>	<input checked="" type="checkbox"/> Remoulded <input checked="" type="checkbox"/> Intact <input type="checkbox"/> Diamond drilling <input type="checkbox"/> Lost	<b>TEST SYMBOL</b>	GSA: grain size analysis CA: chemical analysis w <sub>l</sub> : liquid limit w <sub>p</sub> : plastic limit w: water content C <sub>u</sub> : undrained shear strength S <sub>r</sub> : sensitivity Dup: duplicate sample
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See the attached explicative note for the complete list of symbols and abbreviations



# BOREHOLE REPORT

**Borehole No.**

**BH-06**

<p>CLIENT: MEDUSA LP                  PROJECT: PROPOSED SORTATION FACILITY                  LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO                  DESCRIBED BY: F. ARGUIN      VERIFIED BY: M.-A. RICHARD / A. FIORILLI</p>	<p>GEODETIC COORDINATES (MTM, NAD-83) (m)                  X : 366640.1                  Y : 5017937.4                  Z : 90.53</p>	<p>▼ - WATER LEVEL                  Date : 2021-05-19                  Depth (m) : 1.1                  Location plan : 11220797-A1-1</p>
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<p>Borehole type : Auger                  Core bit size : B                  Hammer type : Automatic                  Energy ratio :                  Date (start) : 2021-04-28                  Date (finish) : 2021-04-28</p>	<p><b>SAMPLE TYPE</b></p> <p>SS(E) - Split Spoon (Environment)                  RC(E) - Rock diamond core                  AU(E) - Auger                  TEE - Sampling Tube Environment                  ST - Shelby tube                  GS(E) - Grab sample</p>	<p><b>SAMPLE STATE</b></p> <p><input checked="" type="checkbox"/> Remoulded  <input checked="" type="checkbox"/> Intact  <input type="checkbox"/> Diamond drilling  <input type="checkbox"/> Lost</p>	<p><b>TEST SYMBOL</b></p> <p>GSA: grain size analysis                  CA: chemical analysis                  w<sub>L</sub>: liquid limit                  w<sub>p</sub>: plastic limit                  w: water content                  C<sub>u</sub>: undrained shear strength                  S<sub>r</sub>: sensitivity                  Dup: duplicate sample</p>
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STRATIGRAPHY				SAMPLE						TESTS RESULTS										
Depth (m)	Elevation (m)	Symbol	Description	State	Type and Number	Recovery %	Other tests	PID (ppm)	6 in / 15 cm Blow counts (sampler size)	N, N <sub>c</sub> or RQD	○ Water content (%)      Δ C <sub>u</sub> (Field, kPa) □ Atterberg limits (%)      □ C <sub>u</sub> (Lab, kPa) ● "N" Standard penetration test value ▲ "N <sub>c</sub> " Dynamic penetration test value									
8.00	82.53		Ground surface								10	20	30	40	50	60	70	80	90	Water level
9.0																				
10.0																				
11.0																				
12.0																				
13.0																				
14.0																				
15.0																				

See the attached explicative note for the complete list of symbols and abbreviations



# BOREHOLE REPORT

**Borehole No. BH-06**

CLIENT: MEDUSA LP PROJECT: PROPOSED SORTATION FACILITY LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO DESCRIBED BY: F. ARGUIN      VERIFIED BY: M.-A. RICHARD / A. FIORILLI	GEODETIC COORDINATES (MTM, NAD-83) (m) X : 366640.1 Y : 5017937.4 Z : 90.53	▼ - WATER LEVEL Date : 2021-05-19 Depth (m) : 1.1 Location plan : 11220797-A1-1
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Borehole type : Auger Core bit size : B Hammer type : Automatic Energy ratio : Date (start) : 2021-04-28 Date (finish) : 2021-04-28	<b>SAMPLE TYPE</b>	SS(E) - Split Spoon (Environment) RC(E) - Rock diamond core AU(E) - Auger TEE - Sampling Tube Environment ST - Shelby tube GS(E) - Grab sample	<b>SAMPLE STATE</b>	<input checked="" type="checkbox"/> Remoulded <input checked="" type="checkbox"/> Intact <input type="checkbox"/> Diamond drilling <input checked="" type="checkbox"/> Lost	<b>TEST SYMBOL</b>	GSA: grain size analysis CA: chemical analysis w <sub>l</sub> : liquid limit w <sub>p</sub> : plastic limit w: water content C <sub>u</sub> : undrained shear strength S <sub>r</sub> : sensitivity Dup: duplicate sample
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STRATIGRAPHY				SAMPLE						TESTS RESULTS										
Depth (m)	Elevation (m)	Symbol	Description	State	Type and Number	Recovery %	Other tests	PID (ppm)	6 in / 15 cm Blow counts (sampler size)	N, N <sub>c</sub> or RQD	○ Water content (%)      △ C <sub>u</sub> (Field, kPa) □ Atterberg limits (%)      □ C <sub>u</sub> (Lab, kPa) ● "N" Standard penetration test value ▲ "N <sub>c</sub> " Dynamic penetration test value									
16.00	74.53		Ground surface								10 20 30 40 50 60 70 80 90 <b>Water level</b>									
17.0										4	4									
										5	5									
										6	6									
										5	5									
										5	5									
										3	3									
										5	5									
18.0										7	7									
										5	5									
										6	6									
										11	11									
										13	13									
										8	8									
										13	13									
										14	14									
										17	17									
21.0										21	21									
										16	16									
										22	22									
22.0	21.97	68.56	End of dynamic penetration test End of borehole								100									
23.0																				

See the attached explicative note for the complete list of symbols and abbreviations

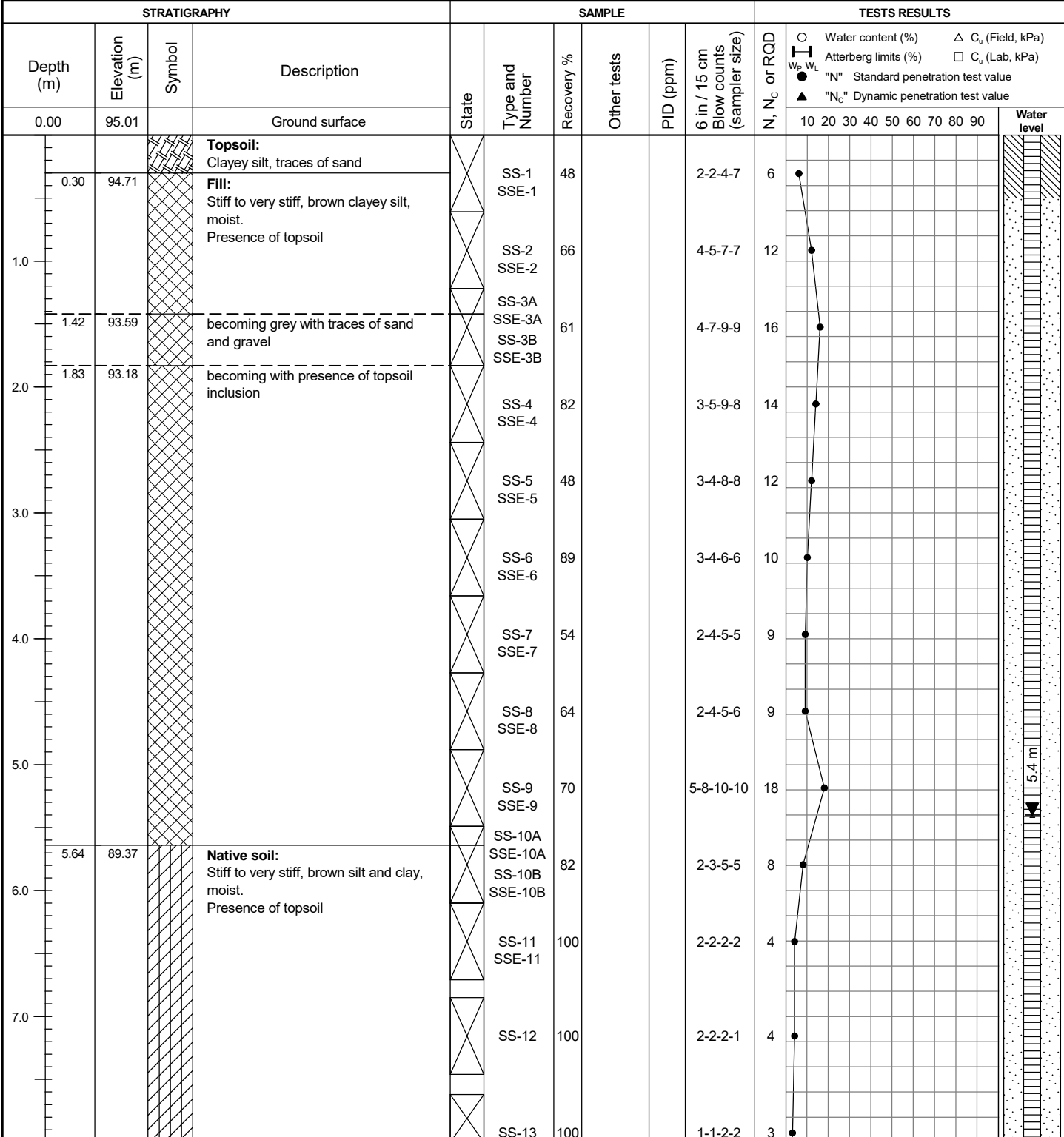


# BOREHOLE REPORT

**Borehole No. BH-11**

CLIENT: MEDUSA LP PROJECT: PROPOSED SORTATION FACILITY LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO DESCRIBED BY: F. ARGUIN      VERIFIED BY: M.-A. RICHARD / A. FIORILLI	GEODETIC COORDINATES (MTM, NAD-83) (m) X : 366474.0 Y : 5017740.7 Z : 95.01	▼ - WATER LEVEL Date : 2021-05-19 Depth (m) : 5.4 Location plan : 11220797-A1-1
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Borehole type : Auger Core bit size : B Hammer type : Automatic Energy ratio : Date (start) : 2021-04-29 Date (finish) : 2021-04-29	<b>SAMPLE TYPE</b> SS(E) - Split Spoon (Environment) RC(E) - Rock diamond core AU(E) - Auger TEE - Sampling Tube Environment ST - Shelby tube GS(E) - Grab sample	<b>SAMPLE STATE</b> <input checked="" type="checkbox"/> Remoulded <input checked="" type="checkbox"/> Intact <input type="checkbox"/> Diamond drilling <input type="checkbox"/> Lost	<b>TEST SYMBOL</b> GSA: grain size analysis CA: chemical analysis w <sub>L</sub> : liquid limit w <sub>p</sub> : plastic limit w: water content C <sub>u</sub> : undrained shear strength S <sub>r</sub> : sensitivity Dup: duplicate sample
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See the attached explicative note for the complete list of symbols and abbreviations



# BOREHOLE REPORT

**Borehole No. BH-11**

CLIENT: MEDUSA LP	GEODETIC COORDINATES (MTM, NAD-83) (m)	▼ - WATER LEVEL Date : 2021-05-19 Depth (m) : 5.4
PROJECT: PROPOSED SORTATION FACILITY	X : 366474.0 Y : 5017740.7 Z : 95.01	
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO	VERIFIED BY: M.-A. RICHARD / A. FIORILLI	Location plan : 11220797-A1-1
DESCRIBED BY: F. ARGUIN		

Borehole type : Auger	<b>SAMPLE TYPE</b>	SS(E) - Split Spoon (Environment)	<b>SAMPLE STATE</b>	<input checked="" type="checkbox"/> Remoulded	<b>TEST SYMBOL</b>	GSA: grain size analysis
Core bit size : B		RC(E) - Rock diamond core		<input checked="" type="checkbox"/> Intact		CA: chemical analysis
Hammer type : Automatic		AU(E) - Auger		<input type="checkbox"/> Diamond drilling		w <sub>l</sub> : liquid limit
Energy ratio :		TEE - Sampling Tube Environment		<input type="checkbox"/> Lost		w <sub>p</sub> : plastic limit
Date (start) : 2021-04-29		ST - Shelby tube				w : water content
Date (finish) : 2021-04-29		GS(E) - Grab sample				C <sub>u</sub> : undrained shear strength
				S <sub>r</sub> : sensitivity	Dup: duplicate sample	

STRATIGRAPHY				SAMPLE					TESTS RESULTS		
Depth (m)	Elevation (m)	Symbol	Description	State	Type and Number	Recovery %	Other tests	PID (ppm)	6 in / 15 cm Blow counts (sampler size)	N, N <sub>c</sub> or RQD	Water level
8.00	87.01		Ground surface								
8.33	86.68		becoming stiff, very moist with presence of beddings of sand		SS-14	100			1-1-2-1	3	
9.0					ST-15	100					
10.0					SS-16	100			1-0-0-1	0	
10.51	84.50		End of borehole								
11.0											
12.0											
13.0											
14.0											
15.0											

See the attached explicative note for the complete list of symbols and abbreviations





# BOREHOLE REPORT

Borehole No.

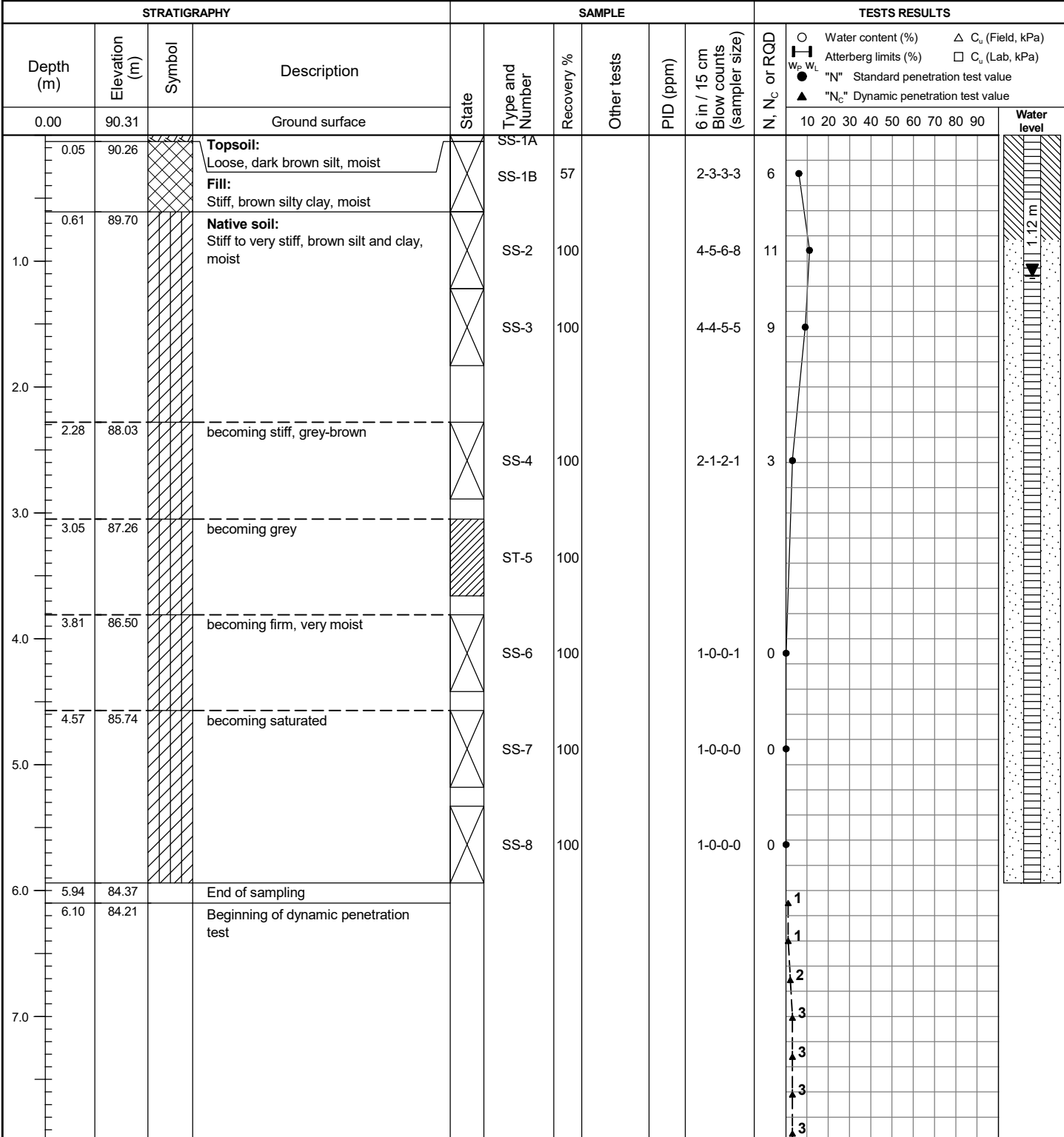
**BH-12**

CLIENT: MEDUSA LP  
 PROJECT: PROPOSED SORTATION FACILITY  
 LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO  
 DESCRIBED BY: F. ARGUIN VERIFIED BY: M.-A. RICHARD / A. FIORILLI

GEODETIC COORDINATES (MTM, NAD-83) (m)  
 X : 366605.0  
 Y : 5017606.5  
 Z : 90.31

▼ - WATER LEVEL  
 Date : 2021-05-19  
 Depth (m) : 1.12  
 Location plan : 11220797-A1-1

Borehole type : Auger	SAMPLE TYPE	SS(E) - Split Spoon (Environment)	SAMPLE STATE	☒ Remoulded	TEST SYMBOL	GSA: grain size analysis
Core bit size : B		RC(E) - Rock diamond core		☒ Intact		CA: chemical analysis
Hammer type : Automatic		AU(E) - Auger		☐ Diamond drilling		w <sub>l</sub> : liquid limit
Energy ratio :		TEE - Sampling Tube Environment		☐ Lost		w <sub>p</sub> : plastic limit
Date (start) : 2021-04-28		ST - Shelby tube				w : water content
Date (finish) : 2021-04-28		GS(E) - Grab sample				C <sub>u</sub> : undrained shear strength
						S <sub>r</sub> : sensitivity
						Dup: duplicate sample



See the attached explicative note for the complete list of symbols and abbreviations



# BOREHOLE REPORT

**Borehole No.**

**BH-12**

<p><b>CLIENT:</b> MEDUSA LP</p> <p><b>PROJECT:</b> PROPOSED SORTATION FACILITY</p> <p><b>LOCATION:</b> LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO</p> <p><b>DESCRIBED BY:</b> F. ARGUIN      <b>VERIFIED BY:</b> M.-A. RICHARD / A. FIORILLI</p>	<p><b>GEODETTIC COORDINATES</b> (MTM, NAD-83) (m)</p> <p>X : 366605.0 Y : 5017606.5 Z : 90.31</p>	<p><b>▼ - WATER LEVEL</b></p> <p>Date : 2021-05-19 Depth (m) : 1.12</p> <p>Location plan : 11220797-A1-1</p>
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<p>Borehole type : Auger Core bit size : B Hammer type : Automatic Energy ratio : Date (start) : 2021-04-28 Date (finish) : 2021-04-28</p>	<b>SAMPLE TYPE</b>	<p>SS(E) - Split Spoon (Environment) RC(E) - Rock diamond core AU(E) - Auger TEE - Sampling Tube Environment ST - Shelby tube GS(E) - Grab sample</p>	<b>SAMPLE STATE</b>	<p><input checked="" type="checkbox"/> Remoulded <input checked="" type="checkbox"/> Intact <input type="checkbox"/> Diamond drilling <input checked="" type="checkbox"/> Lost</p>	<b>TEST SYMBOL</b>	<p>GSA: grain size analysis CA: chemical analysis w<sub>l</sub>: liquid limit w<sub>p</sub>: plastic limit w: water content C<sub>u</sub>: undrained shear strength S<sub>r</sub>: sensitivity Dup: duplicate sample</p>
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STRATIGRAPHY				SAMPLE						TESTS RESULTS									
Depth (m)	Elevation (m)	Symbol	Description	State	Type and Number	Recovery %	Other tests	PID (ppm)	6 in / 15 cm Blow counts (sampler size)	N, N <sub>c</sub> or RQD	Water content (%)	Atterberg limits (%)	"N" Standard penetration test value	"N <sub>c</sub> " Dynamic penetration test value	C <sub>u</sub> (Field, kPa)	C <sub>u</sub> (Lab, kPa)	Water level		
8.00	82.31		Ground surface																
9.0										3 2 3 3 4 5 4 5 6 5 6 6 10 12 7 9 7 8 12 9 8 16 34 44 51 54									
10.0																			
11.0																			
12.0																			
13.0																			
14.0																			
15.0																			

See the attached explicative note for the complete list of symbols and abbreviations



# BOREHOLE REPORT

**Borehole No. BH-12**

CLIENT: MEDUSA LP PROJECT: PROPOSED SORTATION FACILITY LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO DESCRIBED BY: F. ARGUIN      VERIFIED BY: M.-A. RICHARD / A. FIORILLI	GEODETIC COORDINATES (MTM, NAD-83) (m) X : 366605.0 Y : 5017606.5 Z : 90.31	- WATER LEVEL Date : 2021-05-19 Depth (m) : 1.12 Location plan : 11220797-A1-1
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Borehole type : Auger Core bit size : B Hammer type : Automatic Energy ratio : Date (start) : 2021-04-28 Date (finish) : 2021-04-28	<b>SAMPLE TYPE</b>	SS(E) - Split Spoon (Environment) RC(E) - Rock diamond core AU(E) - Auger TEE - Sampling Tube Environment ST - Shelby tube GS(E) - Grab sample	<b>SAMPLE STATE</b>	<input checked="" type="checkbox"/> Remoulded <input checked="" type="checkbox"/> Intact <input type="checkbox"/> Diamond drilling <input type="checkbox"/> Lost	<b>TEST SYMBOL</b>	GSA: grain size analysis CA: chemical analysis w <sub>l</sub> : liquid limit w <sub>p</sub> : plastic limit w : water content C <sub>u</sub> : undrained shear strength S <sub>r</sub> : sensitivity Dup: duplicate sample
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STRATIGRAPHY				SAMPLE							TESTS RESULTS																																																																										
Depth (m)	Elevation (m)	Symbol	Description	State	Type and Number	Recovery %	Other tests	PID (ppm)	6 in / 15 cm Blow counts (sampler size)	N, N <sub>c</sub> or RQD	<div style="font-size: small; margin-bottom: 5px;">                     ○ Water content (%)      Δ C<sub>u</sub> (Field, kPa)                      ▭ Atterberg limits (%)      □ C<sub>u</sub> (Lab, kPa)                      ● "N" Standard penetration test value                      ▲ "N<sub>c</sub>" Dynamic penetration test value                 </div>																																																																										
16.00	74.31		Ground surface								<table border="1" style="width: 100%; border-collapse: collapse; font-size: x-small;"> <tr> <th style="width: 5%;">10</th><th style="width: 5%;">20</th><th style="width: 5%;">30</th><th style="width: 5%;">40</th><th style="width: 5%;">50</th><th style="width: 5%;">60</th><th style="width: 5%;">70</th><th style="width: 5%;">80</th><th style="width: 5%;">90</th><th style="width: 10%;">Water level</th> </tr> <tr> <td colspan="10"></td> <td style="text-align: center;">66</td> </tr> <tr> <td colspan="10"></td> <td style="text-align: center;">77</td> </tr> <tr> <td colspan="10"></td> <td style="text-align: center;">76</td> </tr> <tr> <td colspan="10"></td> <td style="text-align: center;">93</td> </tr> <tr> <td colspan="10"></td> <td style="text-align: center;">100</td> </tr> </table>										10	20	30	40	50	60	70	80	90	Water level											66											77											76											93											100
10	20	30	40	50	60	70	80	90	Water level																																																																												
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										76																																																																											
										93																																																																											
										100																																																																											
17.53	72.78		End of dynamic penetration test End of borehole																																																																																		
17.0																																																																																					
18.0																																																																																					
19.0																																																																																					
20.0																																																																																					
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23.0																																																																																					

See the attached explicative note for the complete list of symbols and abbreviations



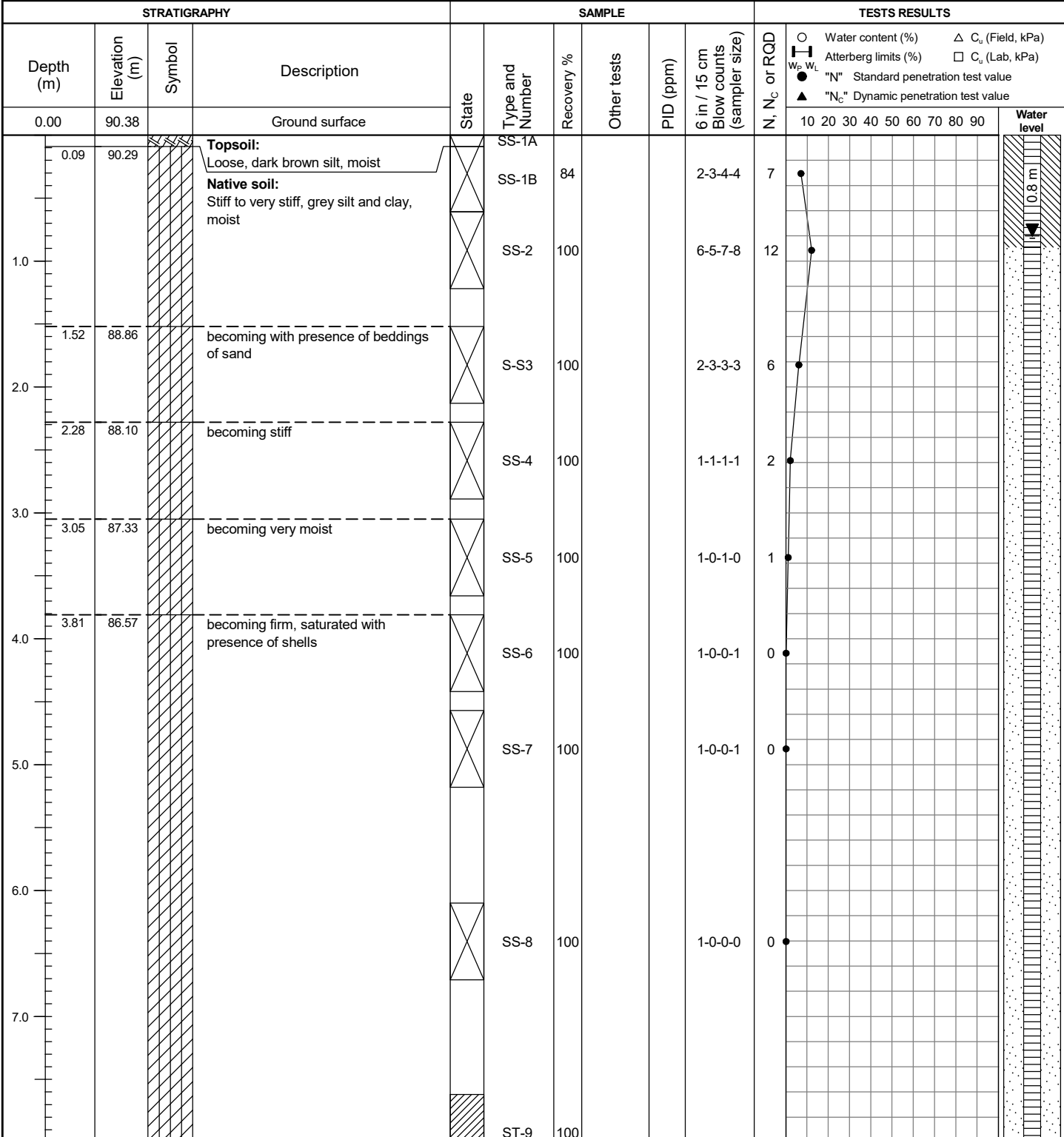
# BOREHOLE REPORT

**Borehole No.**

**BH-13**

<p><b>CLIENT:</b> MEDUSA LP  <b>PROJECT:</b> PROPOSED SORTATION FACILITY  <b>LOCATION:</b> LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO  <b>DESCRIBED BY:</b> F. ARGUIN <b>VERIFIED BY:</b> M.-A. RICHARD / A. FIORILLI</p>	<p><b>GEODETTIC COORDINATES</b>  (MTM, NAD-83) (m)  X : 366809.6  Y : 5017824.8  Z : 90.38</p>	<p><b>▼ - WATER LEVEL</b>  <b>Date :</b> 2021-05-19  <b>Depth (m) :</b> 0.8  <b>Location plan :</b> 11220797-A1-1</p>
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<p><b>Borehole type :</b> Auger  <b>Core bit size :</b> B  <b>Hammer type :</b> Automatic  <b>Energy ratio :</b>  <b>Date (start) :</b> 2021-04-29  <b>Date (finish) :</b> 2021-04-29</p>	<b>SAMPLE TYPE</b>	<p>SS(E) - Split Spoon (Environment)  RC(E) - Rock diamond core  AU(E) - Auger  TEE - Sampling Tube Environment  ST - Shelby tube  GS(E) - Grab sample</p>	<b>SAMPLE STATE</b>	<p><input checked="" type="checkbox"/> Remoulded  <input checked="" type="checkbox"/> Intact  <input type="checkbox"/> Diamond drilling  <input checked="" type="checkbox"/> Lost</p>	<b>TEST SYMBOL</b>	<p>GSA: grain size analysis  CA: chemical analysis  w<sub>l</sub>: liquid limit  w<sub>p</sub>: plastic limit  w: water content  C<sub>u</sub>: undrained shear strength  S<sub>r</sub>: sensitivity  Dup: duplicate sample</p>
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See the attached explicative note for the complete list of symbols and abbreviations



# BOREHOLE REPORT

**Borehole No. BH-13**

CLIENT: MEDUSA LP PROJECT: PROPOSED SORTATION FACILITY LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO DESCRIBED BY: F. ARGUIN      VERIFIED BY: M.-A. RICHARD / A. FIORILLI	GEODETIC COORDINATES (MTM, NAD-83) (m) X : 366809.6 Y : 5017824.8 Z : 90.38	- WATER LEVEL Date : 2021-05-19 Depth (m) : 0.8 Location plan : 11220797-A1-1
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Borehole type : Auger Core bit size : B Hammer type : Automatic Energy ratio : Date (start) : 2021-04-29 Date (finish) : 2021-04-29	<b>SAMPLE TYPE</b>	SS(E) - Split Spoon (Environment) RC(E) - Rock diamond core AU(E) - Auger TEE - Sampling Tube Environment ST - Shelby tube GS(E) - Grab sample	<b>SAMPLE STATE</b>	<input checked="" type="checkbox"/> Remoulded <input checked="" type="checkbox"/> Intact <input type="checkbox"/> Diamond drilling <input checked="" type="checkbox"/> Lost	<b>TEST SYMBOL</b>	GSA: grain size analysis CA: chemical analysis w <sub>l</sub> : liquid limit w <sub>p</sub> : plastic limit w: water content C <sub>u</sub> : undrained shear strength S <sub>r</sub> : sensitivity Dup: duplicate sample
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STRATIGRAPHY				SAMPLE						TESTS RESULTS								
Depth (m)	Elevation (m)	Symbol	Description	State	Type and Number	Recovery %	Other tests	PID (ppm)	6 in / 15 cm Blow counts (sampler size)	N, N <sub>c</sub> or RQD	○ Water content (%)      △ C <sub>u</sub> (Field, kPa) □ Atterberg limits (%)      □ C <sub>u</sub> (Lab, kPa) ● "N" Standard penetration test value ▲ "N <sub>c</sub> " Dynamic penetration test value							
8.00	82.38		Ground surface															
10.67	79.71		becoming with presence of beddings of silt		SS-10	100			1-0-0-0	0								
11.28	79.10		End of borehole Beginning of dynamic penetration test		SS-11	100			1-0-0-0	0								
12.0										1								
										2								
										3								
										3								
										2								
										3								
										9								
										8								
										8								
										11								
										27								
										20								
										13								
										17								
										14								
										17								

See the attached explicative note for the complete list of symbols and abbreviations



# BOREHOLE REPORT

**Borehole No. BH-13**

CLIENT: MEDUSA LP PROJECT: PROPOSED SORTATION FACILITY LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO DESCRIBED BY: F. ARGUIN      VERIFIED BY: M.-A. RICHARD / A. FIORILLI	GEODETIC COORDINATES (MTM, NAD-83) (m) X : 366809.6 Y : 5017824.8 Z : 90.38	▼ - WATER LEVEL Date : 2021-05-19 Depth (m) : 0.8 Location plan : 11220797-A1-1
--	--	--

Borehole type : Auger Core bit size : B Hammer type : Automatic Energy ratio : Date (start) : 2021-04-29 Date (finish) : 2021-04-29	<b>SAMPLE TYPE</b>	SS(E) - Split Spoon (Environment) RC(E) - Rock diamond core AU(E) - Auger TEE - Sampling Tube Environment ST - Shelby tube GS(E) - Grab sample	<b>SAMPLE STATE</b>	<input checked="" type="checkbox"/> Remoulded <input checked="" type="checkbox"/> Intact <input type="checkbox"/> Diamond drilling <input checked="" type="checkbox"/> Lost	<b>TEST SYMBOL</b>	GSA: grain size analysis CA: chemical analysis w <sub>l</sub> : liquid limit w <sub>p</sub> : plastic limit w : water content C <sub>u</sub> : undrained shear strength S <sub>r</sub> : sensitivity Dup: duplicate sample
--	--------------------	---	---------------------	--	--------------------	---

STRATIGRAPHY				SAMPLE						TESTS RESULTS									
Depth (m)	Elevation (m)	Symbol	Description	State	Type and Number	Recovery %	Other tests	PID (ppm)	6 in / 15 cm Blow counts (sampler size)	N, N <sub>c</sub> or RQD	W <sub>p</sub>	W <sub>L</sub>	Atterberg limits (%)	"N" Standard penetration test value	"N <sub>c</sub> " Dynamic penetration test value	C <sub>u</sub> (Field, kPa)	C <sub>u</sub> (Lab, kPa)	Water level	
16.00	74.38		Ground surface																
19.46	70.92		End of dynamic penetration test End of borehole																

Depth (m)	Blow counts	N	N <sub>c</sub>
16.5	17	17	17
16.8	25	25	25
17.2	39	39	39
17.5	44	44	44
17.8	50	50	50
18.2	52	52	52
18.5	40	40	40
19.2	100	100	100
19.5	93	93	93
19.8	87	87	87
20.0	100	100	100

See the attached explicative note for the complete list of symbols and abbreviations

O-A756 -A

# FONDEX

BOREHOLE NUMBER BH-91-3

PROJECT South Merivale Business Park

DRILLING DATE Oct 18/91

LOCATION Merivale Rd. & Highway 16, Nepean, Ont.

REPORT DATE Nov/91

DATUM Ass. Geodetic BOREHOLE TYPE CME-55, Hollow Stem

DRAWN BY M.K.

GEOLOGIC PROFILE		SAMPLES				DYNAMIC PENETRATION RESISTANCE BLOWS					CONSISTENCY:						
Elev. Depth (m)	DESCRIPTION	STRATIGRAPHY	NUMBER	TYPE	BLOWS (N)	% RECOVERY	RESISTANCE BLOWS					NATURAL MOISTURE CONTENT (W)					
							0	20	40	60	80	SHEAR STRENGTH kPa					
							FIELD VANE SHEAR					LIQUID LIMIT (W)					
							LAB VANE SHEAR					PLASTIC LIMIT (Wp)					
							0	50	100	150	200	250	0	20	40	60	80
0.00	<u>Silty Clay</u>																
1.00	-very stiff, brown, occasional oxidation stains and silty seams trace white shells, moist.																
2.00			1	SS	2												
3.00																	
4.00	-becoming, grey, stiff wet		2	SS	4												
5.00	-becoming, layered, with silty seams.		3	SS WH													
6.00																	
7.00			4	SS WH													
82.42																	
7.00	(continued on next page)																

● undisturbed  
○ remolded





O-A756 -A

# FONDEX

BOREHOLE NUMBER BH-91-4

PROJECT South Merivale Business Park

DRILLING DATE Oct 21/91

LOCATION Merivale Rd. & Highway 16, Nepean, Ont.

REPORT DATE Nov/91

DATUM Ass. Geodetic BOREHOLE TYPE CME-55, Hollow Stem

DRAWN BY M.K.

GEOLOGIC PROFILE		SAMPLES				DYNAMIC PENETRATION RESISTANCE BLOWS					CONSISTENCY:						
Elev. Depth (m)	DESCRIPTION	STRATIGRAPHY	NUMBER	TYPE	BLOWS (N)	% RECOVERY	RESISTANCE BLOWS					NATURAL MOISTURE CONTENT (W)					
							0	20	40	60	80	LIQUID LIMIT (W) PLASTIC LIMIT (Wp)					
							SHEAR STRENGTH kPa										
							FIELD VANE SHEAR										
							LAB VANE SHEAR										
							0 50 100 150 200 250					0 20 40 60 80 %					
89.70	0.00	Silty Clay															
	1.00	-very stiff, brown occasional oxidation stains and silty seams moist.															
	2.00	-becoming grey with occasional white shells	1	SS	5												
	3.00		2	SS	2												
	4.00	becoming stiff, wet with interbedded layered silty seams.															
	5.00		3	SS	WH												
	6.00		4	SS	WH												
82.70	7.00	(continued on next page)															
							●	undisturbed									
							○	remolded									

G.W.L. (elev. 85.3)



O-A756-A

# FONDEX

BOREHOLE NUMBER BH-91-5

PROJECT South Merivale Business Park  
 LOCATION Merivale Rd. & Highway 16, Nepean, Ont.  
 DATUM Ass. Geodetic BOREHOLE TYPE CME-55, Hollow Stem

DRILLING DATE Oct 21/91  
 REPORT DATE Nov/91  
 DRAWN BY M.K.

GEOLOGIC PROFILE		SAMPLES				DYNAMIC PENETRATION RESISTANCE BLOWS					CONSISTENCY:							
Elev. Depth (m)	DESCRIPTION	STRATIGRAPHY	NUMBER	TYPE	BLOWS (N)	% RECOVERY	RESISTANCE BLOWS					NATURAL MOISTURE CONTENT (W)						
							0	20	40	60	80	LIQUID LIMIT (W)						
							SHEAR STRENGTH kPa					PLASTIC LIMIT (Wp)						
							FIELD VANE SHEAR											
							LAB VANE SHEAR											
							0	50	100	150	200	250	0	20	40	60	80	%
89.76	0.00	Silty Clay																
	1.00	-Hard to stiff, brown, occasional oxidation stains, and silty seams moist																
	2.00		1	SS	5													
	3.00	-becoming grey, occasional white shells, wet																
	4.00		2	SS	1													
	5.00		3	SSWH														
	6.00	-becoming layered with silt seams																
	7.00		4	SSWH														
	82.76																	
	7.00	(continued on next page)																

G.W.L.  
(elev. 86.8)

● undisturbed  
 ○ remolded



O-A756-A

# FONDEX

BOREHOLE NUMBER BH-91-6

PROJECT South Merivale Business Park

DRILLING DATE Oct 21/91

LOCATION Merivale Rd. & Highway 16, Nepean, Ont.

REPORT DATE Nov/91

DATUM Ass. Geodetic BOREHOLE TYPE CME-55, Hollow Stem

DRAWN BY M.K.

GEOLOGIC PROFILE		SAMPLES			DYNAMIC PENETRATION RESISTANCE BLOWS					CONSISTENCY:							
Elev. Depth (m)	DESCRIPTION	STRATIGRAPHY	NUMBER	TYPE	BLOWS (N)	% RECOVERY	RESISTANCE BLOWS					NATURAL MOISTURE CONTENT (W)					
							0	20	40	60	80	0	20	40	60	80	
89.36							SHEAR STRENGTH kPa					LIQUID LIMIT (W)					
							FIELD VANE SHEAR					PLASTIC LIMIT (Wp)					
							LAB VANE SHEAR										
0.00	Silty Clay						0	50	100	150	200	250	0	20	40	60	80
1.00	very stiff, brown, occasional oxidation stains and silty seams moist		1	SS	5												
2.00																	
3.00	- becoming stiff, grey presence of white shells, wet		2	SS	2												
4.00																	
5.00	-becoming layered with silty seams.		3	SS	WH												
6.00																	
82.36			4	SS	WH												
7.00	(continued on next page)																

● undisturbed  
○ remolded



O-A756-A

# FONDEX

BOREHOLE NUMBER BH-91-7

PROJECT South Merivale Business Park

DRILLING DATE Oct 21/91

LOCATION Merivale Rd. & Highway 16, Nepean, Ont.

REPORT DATE Nov/91

DATUM Ass. Geodetic BOREHOLE TYPE CME-55, Hollow Stem

DRAWN BY M.K.

GEOLOGIC PROFILE		SAMPLES				DYNAMIC PENETRATION RESISTANCE BLOWS					CONSISTENCY:							
Elev. Depth (M)	DESCRIPTION	STRATIGRAPHY	NUMBER	TYPE	BLOWS (N)	% RECOVERY	RESISTANCE BLOWS					NATURAL MOISTURE CONTENT (W)						
							0	20	40	60	80	SHEAR STRENGTH kPa						
							FIELD VANE SHEAR					LIQUID LIMIT (W)						
							LAB VANE SHEAR					PLASTIC LIMIT (Wp)						
							0	50	100	150	200	250	0	20	40	60	80	%
88.97																		
0.00	Silty Clay																	
1.00	-very stiff, brown, occasional silty seams and oxidation stains, presence of white fossils, moist.																	
2.00			1	SS	3													
3.00																		
4.00	- becoming grey, stiff, wet		2	SS	3													
5.00																		
6.00	-becoming layered with silty seams		3	SS	WH													
81.97																		
7.00	(continued on next page)		4	SS	WH													

G.W.L. (Elev. 85.0)

● undisturbed  
○ remolded





O-A756

**FONDEX**

BOREHOLE NUMBER BH-1 (1 of 3)

PROJECT Geotechnical Investigation

DRILLING DATE June 22/90

LOCATION South Merivale Business Park

REPORT DATE July/90

DATUM Geodetic BOREHOLE TYPE CME-55

DRAWN BY M.T.W.

GEOLOGIC PROFILE		SAMPLES			DYNAMIC PENETRATION RESISTANCE BLOWS					CONSISTENCY:							
Elev. Depth	DESCRIPTION	STRATIGRAPHY	NUMBER	TYPE	BLOWS (IN)	RECOVERY %	RESISTANCE BLOWS					NATURAL MOISTURE CONTENT (w)					
							0	20	40	60	80	PLASTIC LIMIT (Wp) %					
							SHEAR STRENGTH kPa										
							FIELD VANE SHEAR										
							LAB. VANE SHEAR										
							50	100	150	200	250	20	40	60	80		
89.53	0.0																
	1.0		1	SS	9												
	2.0		2	SS	4												
	3.0		3	SS	2												
	3.81		4	SS	-												
	4.0		5	SS	-												
	5.0		6	ST	-												
	6.0		7	SS	-												
	6.71		8	SS	1												
	7.0		9	SS	1												
	8.0																
	9.0																
	10.0																

Corn and 330 mm clayey topsoil over

Silty Clay: occasional thin beds of silt and fine sand, trace shells; hard to stiff, olive-brown, moist

becoming firm to soft, grey, and wet

Trace charcoal-grey organic spots becoming stiff

Continued on next sheet

G.W.L. July 12/90 (piezo tip 'B')

G.W.L. July 12/90 (piezo. tip 'A')

in-situ re-moulded



O-A756

**FONDEX**

BOREHOLE NUMBER BH-1 (3 of 3)

PROJECT Geotechnical Investigation

DRILLING DATE June 25/90

LOCATION South Merivale Business Park

REPORT DATE July/90

DATUM Geodetic BOREHOLE TYPE CME-55

DRAWN BY M.T.W.

GEOLOGIC PROFILE		SAMPLES				DYNAMIC PENETRATION				CONSISTENCY:												
Elev Depth	DESCRIPTION	STRATIGRAPHY	NUMBER	TYPE	BLOWS (N)	% RECOVERY	RESISTANCE BLOWS				NATURAL MOISTURE											
							0	20	40	60	80	CONTENT (W)										
							SHEAR STRENGTH				LIQUID LIMIT (W)											
							FIELD VANE SHEAR				PLASTIC LIMIT (Wp)											
							LAB VANE SHEAR				%											
							kPa				*											
							X				%											
69.53	CONTINUED																					
20.0	Sandstone Bedrock horizontal bedding, sound, light grey. Becoming less sandy and more dolimitic with depth		13	RC55	89																	
21.0			14	RC	64	100																
22.0			15	RC	64	100																
66.82	End of Borehole																					
22.71																						

**Notes:**

- Two piezometer standpipes installed:  
 A) Piezometer tip 'A' installed at 18.3m;  
 B) Piezometer tip 'B' at 6.1 m;  
 C) 500 mm thick Bentonite Seals at 18.0 m, 6.7m, and 5.5 m.

**2. Water Level Record**

Time	Water Level (m)	
June 25/90	2.0 ( in augers)	
	A	B
June 26/90	13.3	4.1
July 6/90	7.9	2.5
July 12/90	9.0	2.4

**3.▲ Pocket Penetrometer Values**

- The low blow counts in values in the till may be attributed to saturated and disturbed conditions due to drilling

O-A756

# FONDEX

BOREHOLE NUMBER BH-7

PROJECT Geotechnical Investigation

DRILLING DATE June 22/90

LOCATION South Merivale Business Park

REPORT DATE July /90

DATUM Geodetic BOREHOLE TYPE CME-55

DRAWN BY M.T.W.

GEOLOGIC PROFILE		SAMPLES				DYNAMIC PENETRATION				CONSISTENCY:								
Elev. Depth	DESCRIPTION	STRATIGRAPHY	NUMBER	TYPE	BLOWS (m)	RECOVERY %	RESISTANCE BLOWS				NATURAL MOISTURE							
							0	20	40	60	80	CONTENT (w)						
							SHEAR STRENGTH				LIQUID LIMIT (W)							
							FIELD VANE SHEAR				PLASTIC LIMIT (W <sub>p</sub> )							
							LAB ONE BAR 150 200*				20 40 60 80 %							
90.07																		
0.0	Corn and 250 mm clayey topsoil over		1	SS	7													
1.0	Silty Clay occasional silt and fine sand lenses, trace shells, very stiff to stiff, olive-brown, moist		2	SS	3													
2.0			3	SS	2													
3.0			4	SS	2													
36.26	becoming firm to soft, grey, wet		5	SS	-													
3.81			6	SS	-													
4.0			7	SS	-													
5.0																		
6.0	Trace charcoal-grey organic spots																	
83.37																		
6.7	End of Borehole																	
Notes:																		
1. ▲ Pocket Penetrometer values																		
2. Standpipe piezometer installed to 6.1 m																		
3. Chemical Analysis performed on water sample obtained from 5 m depth																		
4. Water Level Record																		
Time Water Level (m)																		
on compl. 5.0 (in augers)																		
June 25/90 1.8																		
June 26/90 1.8																		
July 6/90 1.9																		

G.W.L. July 6/90

in-situ re-moulded

O-A756

**FONDEX**

BOREHOLE NUMBER **BH-8**

PROJECT Geotechnical Investigation

DRILLING DATE June 22/90

LOCATION South Merivale Business Park

REPORT DATE July/90

DATUM Geodetic BOREHOLE TYPE CME-55

DRAWN BY M.T.W.

GEOLOGIC PROFILE		SAMPLES				DYNAMIC PENETRATION RESISTANCE BLOWS					CONSISTENCY:						
Elev	DESCRIPTION	STRATIGRAPHY	NUMBER	TYPE	(N) BLOWS	RECOVERY %	RESISTANCE BLOWS					NATURAL MOISTURE CONTENT (w)					
Depth							0	20	40	60	80	SHEAR STRENGTH kPa				LIQUID LIMIT (w <sub>l</sub> )	
89.89							FIELD VANE SHEAR					PLASTIC LIMIT (w <sub>p</sub> )					
							LAB VANE SHEAR	50	100	150	200	20	40	60	80	%	
0.0	Corn and 275 mm clayey topsoil over																
1.0	Silty Clay: Trace fine sand, trace shells, very stiff to stiff, olive-brown, moist  becoming soft to firm, grey, wet		1	SS	6												
2.0			2	SS	3												
3.0				3	SS	2											
4.0				4	SS	1											
4.27				5	SS	1											
5.0				6	SS	-											
6.0		trace charcoal, grey organic spots		7	SS	-											
6.7	End of Borehole																
	Note:																
	1. ▲ Pocket Penetrometer Values																
	2. Standpipe Piezometer installed to 6.1 m.																
	3. Water Level Records																
	Time		Water Level (m)														
			on comp. dry (in augers)														
			June 25/90		2.3												
			June 26/90		2.3												
			July 6/90		2.3												

G.W.L. July 6/90

in situ re-moulded

O-A756

# FONDEX

BOREHOLE NUMBER BH-9 (1 of 3)

PROJECT Geotechnical Investigation

DRILLING DATE June 26/90


LOCATION South Merivale Business Park


REPORT DATE July/90

DATUM Geodetic BOREHOLE TYPE CME-55

DRAWN BY M.T.W.

GEOLOGIC PROFILE		SAMPLES				DYNAMIC PENETRATION					CONSISTENCY						
Elev. Depth	DESCRIPTION	STRATIGRAPHY	NUMBER	TYPE	BLOWS (IN)	RECOVERY %	RESISTANCE BLOWS					NATURAL MOISTURE					
							0	20	40	60	80	CONTENT (w)		LIQUID LIMIT (w <sub>L</sub> )		PLASTIC LIMIT (w <sub>p</sub> )	
							SHEAR STRENGTH kPa										
							FIELD VANE SHEAR										
							LAB VANE SHEAR										
							50	100	150	200	300	20	40	60	80	%	
90.65																	
0.0	Grass and 200 mm clayey topsoil over	)))															
1.0	<u>Silty Clay:</u> Trace fine sand and silt lenses occasional shells, very stiff to stiff, olive-brown, moist		1	SS	8												
2.0			2	SS	3												
3.0			3	SS	-												
37.65	becoming firm, grey and wet		4	SS	-												
3.0			5	SS	-												
86.84	Trace charcoal-grey organic spots to bottom of clay		6	SS	-												
3.81			7	SS	-												
4.0			8	ST	-												
5.0			9	SS	-												
6.0																	
7.0																	
8.0																	
9.0																	
10.0	Continued on next sheet																

G.W.L.   
 July 12/90  
 Piezo 'B'

G.W.L.   
 July 12/90  
 Piezo 'A'



O-A756

# FONDEX

BOREHOLE NUMBER BH-9 (3 of 3)

PROJECT Geotechnical Investigation

DRILLING DATE June 26/90

LOCATION South Merivale Business Park

REPORT DATE July/90

DATUM Geodetic BOREHOLE TYPE CME-55

DRAWN BY M. T. W.

GEOLOGIC PROFILE		SAMPLES				DYNAMIC PENETRATION RESISTANCE BLOWS					CONSISTENCY										
Elev. Depth	DESCRIPTION	STRATIGRAPHY	NUMBER	TYPE	BLOWS (N)	% RECOVERY	RESISTANCE BLOWS					NATURAL MOISTURE CONTENT (w)									
							0	20	40	60	80	PLASTIC LIMIT (Wp)									
							SHEAR STRENGTH kPa														
							FIELD VANE SHEAR *														
							LAB VANE SHEAR X														
												20	40	60	80	%					
70.65	Continued																				
20.0	Clay/Silt/Sand/Gravel Till : dense, grey, wet, occasional boulders (auger refusal at 20.7 m)	4	13	RC																	
21.0																					
68.91	Split spoon refusal																				
21.74	End of Borehole																				
Notes:																					
1. ▲ Pocket Penetrometer values																					
2. Two Piezometer standpipe installed.																					
A) Piezometer tip 'A' installed at 21.3 m																					
B) piezometer tip 'B' installed at 6.1 m																					
C) 500 mm thick Bentonite seals at 20.7 m, 6.4 m, and 5.5 m.																					
3. Water Level Record																					
Time																					
Water Level (m)																					
		'A'		'B'																	
July 6/90		3.0		1.5																	
July 12/90		3.1		1.7																	
4. 300 m of rock coring at a depth of 20.7 m (sample RC-13) confirmed the existence of a boulder																					





# TEST PIT REPORT

Reference No.: 12615684-A1

Test Pit No.: **TP-101-23**

Client : **Medusa Limited Partnership**

Geodetic Coordinates X : **366591**  
MTM-9 (NAD-1983) Y : **5017776**  
Z : **90.51**

Project : **Geotechnical Investigation - Proposed Distribution Center**

*Preliminary*

Location Plan No.: **FIGURE 1**

Location : **Bill Leathem Drive, Ottawa, Ontario**

Date (Start) : **2023-07-07**

Executed by : **Demolition Plus**

Date (Finish) : **2023-07-07**

Described by : **Mathieu Chénier, Tech.**

Verified by : **Keshini Rangasamy, CEP**

Test Pit Depth (m): **3.00**

DEPTH - m	ELEVATION / DEPTH - m	STRATIGRAPHY		SAMPLE		WATER INFILTRATION	TEST SYMBOL
		SOIL DESCRIPTION	SYMBOL	SAMPLE TYPE AND NUMBER	STATE		
	90.51	Ground Surface					
	0.00	<b>Topsoil:</b> Brown silt, some clay, traces of sand, moist. Presence of organic matter (rootlets) (1-5%).		GS-01	X		GSA, H LL = 70% PL = 31% W = 33.0%
0.5	89.91 0.60	<b>Native Soil:</b> Firm to stiff, grey clay and silt, traces of sand, moist. Presence of organic matter (rootlets) (1%).		GS-02	X		
1.0							
1.5	89.11 1.40	Firm to stiff, grey-orange clayey silt, traces of sand, moist.		GS-03	X		
2.0	88.41 2.10	Firm to stiff, grey clayey silt to silty clay, moist.		GS-04	X		
3.0	87.51 3.00	End of test pit (voluntary termination)					
3.5							
4.0							
4.5							
5.0							
5.5							

Remark(s) : Easy to excavate  
No water infiltration  
Stables walls  
The compactness / consistency is estimated



# TEST PIT REPORT

Reference No.: 12615684-A1

Test Pit No.: **TP-102-23**

Client : **Medusa Limited Partnership**

Geodetic Coordinates X : **366530**

MTM-9 (NAD-1983) Y : **5017774**

Project : **Geotechnical Investigation - Proposed Distribution Center**

Z : **90.77**

Location : **Bill Leatham Drive, Ottawa, Ontario**

*Preliminary*

Location Plan No.: **FIGURE 1**

Executed by : **Demolition Plus**

Date (Start) : **2023-07-07**

Described by : **Mathieu Chénier, Tech.**

Verified by : **Keshini Rangasamy, CEP**

Date (Finish) : **2023-07-07**

Test Pit Depth (m): **3.00**

DEPTH - m	ELEVATION / DEPTH - m	STRATIGRAPHY		SAMPLE		WATER INFILTRATION	TEST SYMBOL
		SOIL DESCRIPTION	SYMBOL	SAMPLE TYPE AND NUMBER	STATE		
	90.77	Ground Surface					GSA : Particle Size Analysis H : Hydrometer Testing CA : Chemical Analysis LL : Liquid Limit PL : Plastic Limit W : Water Content Dup : Duplicate Sample Taken OM : Organic Matter Content
	0.00	<b>Topsoil:</b> Brown silt, some clay, traces of sand, moist. Presence of organic matter (rootlets) (1-5%).			GS-01		
0.5	90.46 0.30	<b>Native Soil:</b> Firm to stiff, brown silt, some clay, traces of sand, moist. Presence of organic matter (rootlets) (1%).			GS-02		
1.0							
1.5	89.36 1.41	Firm to stiff, grey-orange silt, some clay to clayey, traces of sand, moist.			GS-03		
2.0							
2.5							
3.0	87.77 3.00	End of test pit (voluntary termination)					
3.5							
4.0							
4.5							
5.0							
5.5							

Remark(s) : Easy to excavate  
No water infiltration  
Stables walls  
The compactness / consistency is estimated



# TEST PIT REPORT

Reference No.: 12615684-A1

**Test Pit No.: TP-103-23**

Client : **Medusa Limited Partnership**

Geodetic Coordinates X : **366498**

MTM-9 (NAD-1983) Y : **5017740**

Project : **Geotechnical Investigation - Proposed Distribution Center**

Z : **93.33**

Location : **Bill Leatham Drive, Ottawa, Ontario**

Location Plan No.: **FIGURE 1**

Executed by : **Demolition Plus**

Date (Start) : **2023-07-07**

Described by : **Mathieu Chénier, Tech.**

Verified by : **Keshini Rangasamy, CEP**

Date (Finish) : **2023-07-07**

Test Pit Depth (m): **4.80**

Preliminary

DEPTH - m	ELEVATION / DEPTH - m	STRATIGRAPHY		SAMPLE		WATER INFILTRATION	TEST SYMBOL
		SOIL DESCRIPTION	SYMBOL	SAMPLE TYPE AND NUMBER	STATE		
	93.33	Ground Surface					GSA : Particle Size Analysis H : Hydrometer Testing CA : Chemical Analysis LL : Liquid Limit PL : Plastic Limit W : Water Content Dup : Duplicate Sample Taken OM : Organic Matter Content  GSA LL = 47% PL = 27% W = 22.0%
	0.00	<b>Fill:</b> Brown clayey silt, traces of sand, moist. Presence of organic matter (rootlets) (1-5%).			GS-01		
0.5	92.83	Loose to compact, brown silt, some sand, traces of clay and gravel, moist.			GS-02		
	0.50						
	92.53	Brown silt, some clay, traces of sand, moist. Presence of organic matter (rootlets) (1%).			GS-03		
1.0	0.80						
	91.53	Brown-grey clayey silt, traces of sand, moist. Presence of organic matter (rootletss) (1%).			GS-04		
2.0	1.80						
	90.73	Grey-brown silt, some clay to clayey, traces of sand, moist. Presence of organic matter (rootlets) (1%).			GS-05		
3.0	2.60						
	89.93	<b>Native Soil:</b> Firm to stiff, grey-orange clayey silt, traces of sand, moist.			GS-06		
3.5	3.40						
4.0							
4.5							
	88.53	End of test pit (voluntary termination)					
5.0	4.80						
5.5							

Remark(s) : Easy to excavate  
 No water infiltration  
 Stables walls  
 The compactness / consistency is estimated



# TEST PIT REPORT

Reference No.: 12615684-A1

**Test Pit No.: TP-104-23**

**Client : Medusa Limited Partnership**

Geodetic Coordinates X : **366619**  
 Y : **5017713**  
 Z : **90.41**

**Project : Geotechnical Investigation - Proposed Distribution Center**

*Preliminary*

**Location : Bill Leatham Drive, Ottawa, Ontario**

Location Plan No.: **FIGURE 1**

**Executed by : Demolition Plus**

Date (Start) : **2023-07-07**

**Described by : Mathieu Chénier, Tech.**

Verified by : **Keshini Rangasamy, CEP**

Date (Finish) : **2023-07-07**

Test Pit Depth (m): **3.00**

DEPTH - m	ELEVATION / DEPTH - m	STRATIGRAPHY		SAMPLE		WATER INFILTRATION	TEST SYMBOL
		SOIL DESCRIPTION	SYMBOL	SAMPLE TYPE AND NUMBER	STATE		
	90.41	Ground Surface					GSA : Particle Size Analysis H : Hydrometer Testing CA : Chemical Analysis LL : Liquid Limit PL : Plastic Limit W : Water Content Dup : Duplicate Sample Taken OM : Organic Matter Content
0.5	0.00	<b>Topsoil:</b> Brown silt, some clay, traces of sand, moist. Presence of organic matter (rootlets) (1-5%).			GS-01	X	
	89.71	<b>Native Soil:</b>					
1.0	0.70	Firm to stiff, grey-brown-orange silt, some clay, traces of sand, moist.			GS-02	X	
	89.31	Firm to stiff, grey-orange clayey silt, traces of sand, moist.					
1.5	1.10				GS-03	X	
2.0							
2.5					GS-04	X	
3.0	87.41	End of test pit (voluntary termination)					
	3.00						
3.5							
4.0							
4.5							
5.0							
5.5							

Remark(s) : Easy to excavate  
 No water infiltration  
 Stables walls  
 The compactness / consistency is estimated  
 SA: Soil Aggressiveness



# TEST PIT REPORT

Reference No.: 12615684-A1

Test Pit No.: **TP-105-23**

Client : **Medusa Limited Partnership**

Geodetic Coordinates X : **366489**

MTM-9 (NAD-1983) Y : **5017715**

Project : **Geotechnical Investigation - Proposed Distribution Center**

Z : **94.88**

Location : **Bill Leatham Drive, Ottawa, Ontario**

*Preliminary*

Location Plan No.: **FIGURE 1**

Executed by : **Demolition Plus**

Date (Start) : **2023-07-07**

Described by : **Mathieu Chénier, Tech.**

Verified by : **Keshini Rangasamy, CEP**

Date (Finish) : **2023-07-07**

Test Pit Depth (m): **5.50**

DEPTH - m	ELEVATION / DEPTH - m	STRATIGRAPHY		SAMPLE		WATER INFILTRATION	TEST SYMBOL
		SOIL DESCRIPTION	SYMBOL	SAMPLE TYPE AND NUMBER	STATE		
	94.88	Ground Surface					GSA : Particle Size Analysis H : Hydrometer Testing CA : Chemical Analysis LL : Liquid Limit PL : Plastic Limit W : Water Content Dup : Duplicate Sample Taken OM : Organic Matter Content
0.5	0.00	<b>Fill:</b> Brown silt, some clay, traces of sand, moist. Presence of organic matter (rootlets) (1-5%).		GS-01			
1.0				GS-02			
1.5	93.58 / 1.30	Grey silt, some clay to clayey, traces of sand, moist. Presence of organic matter (rootlets) (1%).		GS-03			
2.0				GS-04			
3.5				GS-05			
4.5	90.38 / 4.50	<b>Native Soil:</b> Firm to stiff, grey-orange clayey silt, traces of sand, moist.		GS-06		GSA LL = 56% PL = 27% W = 28.0%	
5.5	89.38 / 5.50	End of test pit (voluntary termination)					

Remark(s) : Easy to excavate  
No water infiltration  
Stables walls  
The compactness / consistency is estimated



# TEST PIT REPORT

Reference No.: 12615684-A1

**Test Pit No.: TP-106-23**

Client : **Medusa Limited Partnership**

Geodetic Coordinates X : **366454**

MTM-9 (NAD-1983) Y : **5017706**

Project : **Geotechnical Investigation - Proposed Distribution Center**

Z : **91.11**

Location : **Bill Leatham Drive, Ottawa, Ontario**

*Preliminary*

Location Plan No.: **FIGURE 1**

Executed by : **Demolition Plus**

Date (Start) : **2023-07-07**

Described by : **Mathieu Chénier, Tech.**

Verified by : **Keshini Rangasamy, CEP**

Date (Finish) : **2023-07-07**

Test Pit Depth (m): **3.00**

DEPTH - m	ELEVATION / DEPTH - m	STRATIGRAPHY		SAMPLE		WATER INFILTRATION	TEST SYMBOL
		SOIL DESCRIPTION	SYMBOL	SAMPLE TYPE AND NUMBER	STATE		
	91.11	Ground Surface					
	0.00	<b>Topsoil:</b> Brown silt, some clay, traces of sand, moist. Presence of organic matter (rootlets) (1-5%).		GS-01	X		
0.5	90.80 0.30	<b>Native Soil:</b> Firm to stiff, brown silt, some clay, traces of sand and gravel, moist. Presence of organic matter (rootlets) (1-5%).		GS-02	X		
1.0							
1.5	89.91 1.20	Firm to stiff, grey silt, some clay, traces of gravel and sand, moist.		GS-03	X		
2.0							
2.5	89.11 2.00	Firm to stiff, grey-orange clayey silt, traces of sand, moist.		GS-04	X		
3.0	88.11 3.00	End of test pit (voluntary termination)					
3.5							
4.0							
4.5							
5.0							
5.5							

LL = 45%  
PL = 18%  
W = 31.0%

Remark(s) : Easy to excavate  
No water infiltration  
Stables walls  
The compactness / consistency is estimated



# TEST PIT REPORT

Reference No.: 12615684-A1

Test Pit No.: **TP-107-23**

Client : **Medusa Limited Partnership**

Geodetic Coordinates X : **366586**

MTM-9 (NAD-1983) Y : **5017673**

Project : **Geotechnical Investigation - Proposed Distribution Center**

Z : **90.65**

Location : **Bill Leatham Drive, Ottawa, Ontario**

*Preliminary*

Location Plan No.: **FIGURE 1**

Executed by : **Demolition Plus**

Date (Start) : **2023-07-07**

Described by : **Mathieu Chénier, Tech.**

Verified by : **Keshini Rangasamy, CEP**

Date (Finish) : **2023-07-07**

Test Pit Depth (m): **3.00**

DEPTH - m	ELEVATION / DEPTH - m	STRATIGRAPHY		SAMPLE		WATER INFILTRATION	TEST SYMBOL
		SOIL DESCRIPTION	SYMBOL	SAMPLE TYPE AND NUMBER	STATE		
	90.65	Ground Surface					GSA : Particle Size Analysis H : Hydrometer Testing CA : Chemical Analysis LL : Liquid Limit PL : Plastic Limit W : Water Content Dup : Duplicate Sample Taken OM : Organic Matter Content
0.5	0.00	<b>Topsoil:</b> Brown silt, some clay, traces of sand, moist. Presence of organic matter (rootlets) (1-5%).			GS-01	X	
	89.95	<b>Native Soil:</b>				X	
1.0	0.70	Compact, brown-grey silt, some sand and clay, moist.			GS-02	X	
	89.55	Presence of organic matter (rootlets) (1%).				X	
1.5	1.10	Stiff, grey silt, some clay, moist.			GS-03	X	
2.0	88.65	Firm to stiff, grey-orange clayey silt, traces of sand, moist.				X	
2.5	2.00				GS-04	X	
3.0	87.65	End of test pit (voluntary termination)					
3.5	3.00						
4.0							
4.5							
5.0							
5.5							

Remark(s) : Easy to excavate  
No water infiltration  
Stables walls  
The compactness / consistency is estimated



# TEST PIT REPORT

Reference No.: 12615684-A1

Test Pit No.: **TP-108-23**

Client : **Medusa Limited Partnership**

Geodetic Coordinates X : **366455**

MTM-9 (NAD-1983) Y : **5017672**

Project : **Geotechnical Investigation - Proposed Distribution Center**

Z : **91.00**

Location : **Bill Leatham Drive, Ottawa, Ontario**

*Preliminary*

Location Plan No.: **FIGURE 1**

Executed by : **Demolition Plus**

Date (Start) : **2023-07-07**

Described by : **Mathieu Chénier, Tech.**

Verified by : **Keshini Rangasamy, CEP**

Date (Finish) : **2023-07-07**

Test Pit Depth (m): **3.00**

DEPTH - m	ELEVATION / DEPTH - m	STRATIGRAPHY		SAMPLE		WATER INFILTRATION	TEST SYMBOL
		SOIL DESCRIPTION	SYMBOL	SAMPLE TYPE AND NUMBER	STATE		
	91.00	Ground Surface					GSA : Particle Size Analysis H : Hydrometer Testing CA : Chemical Analysis LL : Liquid Limit PL : Plastic Limit W : Water Content Dup : Duplicate Sample Taken OM : Organic Matter Content
	0.00	<b>Topsoil:</b> Brown silt, some clay, traces of sand, moist. Presence of organic matter (rootlets) (1-5%).			GS-01	X	
0.5	0.40	<b>Native Soil:</b> Firm to stiff, grey-brown silt, some clay and sand, moist. Presence of cobbles (1-5%).			GS-02	X	
1.0	89.90	Firm to stiff, grey silt, some clay to clayey, traces of sand, moist.			GS-03	X	
1.5	1.10					X	
2.0	89.00	Firm to stiff, grey-orange clayey silt, traces of sand, moist.			GS-04	X	
2.5	2.00					X	
3.0	88.00	End of test pit (voluntary termination)					
3.0	3.00						
3.5							
4.0							
4.5							
5.0							
5.5							

Remark(s) : Easy to excavate  
No water infiltration  
Stables walls  
The compactness / consistency is estimated





# TEST PIT REPORT

Reference No.: 12615684-A1

**Test Pit No.: TP-109-23**

Client : **Medusa Limited Partnership**

Geodetic Coordinates X : **366605**  
 Y : **5017642**  
 Z : **90.81**

Project : **Geotechnical Investigation - Proposed Distribution Center**

*Preliminary*

Location : **Bill Leatham Drive, Ottawa, Ontario**

Location Plan No.: **FIGURE 1**

Executed by : **Demolition Plus**

Date (Start) : **2023-07-07**

Described by : **Mathieu Chénier, Tech.**

Verified by : **Keshini Rangasamy, CEP**

Date (Finish) : **2023-07-07**

Test Pit Depth (m): **3.00**

DEPTH - m	ELEVATION / DEPTH - m	STRATIGRAPHY		SAMPLE		WATER INFILTRATION	TEST SYMBOL
		SOIL DESCRIPTION	SYMBOL	SAMPLE TYPE AND NUMBER	STATE		
	90.81	Ground Surface					
	0.00	<b>Topsoil:</b> Brown silt, some clay, traces of sand, moist. Presence of organic matter (rootlets) (1-5%).			GS-01	X	LL = 69% PL = 26% W = 26.0%
0.5	90.51 / 0.30	<b>Native Soil:</b> Firm to stiff, brown silt, some clay, traces of sand, moist. Presence of cobbles (1-5%) and organic matter (rootlets) (1-5%).			GS-02	X	
1.0	89.91 / 0.90	Firm to stiff, brown silt, some clay, traces of sand, moist. Presence of organic matter (rootlets) (1%).			GS-03	X	
2.0	89.01 / 1.80	Firm to stiff, grey-orange silt, some clay, traces of sand, moist.			GS-04	X	
3.0	87.81 / 3.00	End of test pit (voluntary termination)					

Remark(s) : Easy to excavate  
 No water infiltration  
 Stables walls  
 The compactness / consistency is estimated



# TEST PIT REPORT

Reference No.: 12615684-A1

**Test Pit No.: TP-110-23**

Client : **Medusa Limited Partnership**

Geodetic Coordinates X : **366481**

MTM-9 (NAD-1983) Y : **5017640**

Project : **Geotechnical Investigation - Proposed Distribution Center**

Z : **90.51**

Location : **Bill Leathem Drive, Ottawa, Ontario**

Location Plan No.: **FIGURE 1**

Executed by : **Demolition Plus**

Date (Start) : **2023-07-07**

Described by : **Mathieu Chénier, Tech.**

Verified by : **Keshini Rangasamy, CEP**

Date (Finish) : **2023-07-07**

Test Pit Depth (m): **3.00**

*Preliminary*

DEPTH - m	ELEVATION / DEPTH - m	STRATIGRAPHY		SAMPLE		WATER INFILTRATION	TEST SYMBOL
		SOIL DESCRIPTION	SYMBOL	SAMPLE TYPE AND NUMBER	STATE		
	90.51	Ground Surface					
	0.00	<b>Topsoil:</b> Brown silt, some clay, traces of sand, moist. Presence of organic matter (rootlets) (1-5%).			GS-01	X	GSA : Particle Size Analysis H : Hydrometer Testing CA : Chemical Analysis LL : Liquid Limit PL : Plastic Limit W : Water Content Dup : Duplicate Sample Taken OM : Organic Matter Content  GSA, H LL = 45% PL = 18% W = 36.0%
0.5	90.20 0.30	<b>Native Soil:</b> Firm to stiff, brown-grey silt, some clay, traces of sand, moist. Presence of organic matter (rootlets) (1%).			GS-02	X	
1.0	89.31 1.20	Firm to stiff, grey silt, some clay, traces of sand, moist.			GS-03	X	
1.5	88.51 2.00	becoming grey-orange			GS-04	X	
2.0	87.51 3.00	End of test pit (voluntary termination)					
2.5							
3.0							
3.5							
4.0							
4.5							
5.0							
5.5							

Remark(s) : Easy to excavate  
 No water infiltration  
 Stables walls  
 The compactness / consistency is estimated



# TEST PIT REPORT

Reference No.: 12615684-A1

**Test Pit No.: TP-111-23**

Client : **Medusa Limited Partnership**

Geodetic Coordinates X : **366513**

MTM-9 (NAD-1983) Y : **5017631**

Project : **Geotechnical Investigation - Proposed Distribution Center**

Z : **90.52**

Location : **Bill Leatham Drive, Ottawa, Ontario**

Location Plan No.: **FIGURE 1**

Executed by : **Demolition Plus**

Date (Start) : **2023-07-07**

Described by : **Mathieu Chénier, Tech.**

Verified by : **Keshini Rangasamy, CEP**

Date (Finish) : **2023-07-07**

Test Pit Depth (m): **3.00**

Preliminary

DEPTH - m	ELEVATION / DEPTH - m	STRATIGRAPHY		SAMPLE		WATER INFILTRATION	TEST SYMBOL
		SOIL DESCRIPTION	SYMBOL	SAMPLE TYPE AND NUMBER	STATE		
	90.52	Ground Surface					GSA : Particle Size Analysis H : Hydrometer Testing CA : Chemical Analysis LL : Liquid Limit PL : Plastic Limit W : Water Content Dup : Duplicate Sample Taken OM : Organic Matter Content
	0.00	<b>Topsoil:</b> Brown silt, some clay, traces of sand, moist. Presence of organic matter (rootlets) (1-5%).			GS-01	X	
0.5	90.17 / 0.35	<b>Native Soil:</b> Firm to stiff, brown-grey silt, some clay, traces of sand, moist. Presence of organic matter (rootlets) (1%).			GS-02	X	
1.0	89.62 / 0.90	Firm to stiff, grey silt, some clay, traces of sand, moist. Presence of organic matter (rootlets) (1%).			GS-03	X	
2.0	88.72 / 1.80	Firm to stiff, grey-orange silt, some clay to clayey, traces of sand, moist.			GS-04	X	
3.0	87.52 / 3.00	End of test pit (voluntary termination)					

Remark(s) : Easy to excavate  
 No water infiltration  
 Stables walls  
 The compactness / consistency is estimated



# TEST PIT REPORT

Reference No.: 12615684-A1

**Test Pit No.: TP-112-23**

Client : **Medusa Limited Partnership**

Geodetic Coordinates X : **366582**

MTM-9 (NAD-1983) Y : **5017624**

Project : **Geotechnical Investigation - Proposed Distribution Center**

Z : **90.71**

Location : **Bill Leatham Drive, Ottawa, Ontario**

*Preliminary*

Location Plan No.: **FIGURE 1**

Executed by : **Demolition Plus**

Date (Start) : **2023-07-07**

Described by : **Mathieu Chénier, Tech.**

Verified by : **Keshini Rangasamy, CEP**

Date (Finish) : **2023-07-07**

Test Pit Depth (m): **3.00**

DEPTH - m	ELEVATION / DEPTH - m	STRATIGRAPHY		SAMPLE		WATER INFILTRATION	TEST SYMBOL
		SOIL DESCRIPTION	SYMBOL	SAMPLE TYPE AND NUMBER	STATE		
	90.71	Ground Surface					GSA : Particle Size Analysis H : Hydrometer Testing CA : Chemical Analysis LL : Liquid Limit PL : Plastic Limit W : Water Content Dup : Duplicate Sample Taken OM : Organic Matter Content
	0.00	<b>Topsoil:</b> Brown silt, some clay and sand, moist. Presence of organic matter (rootlets) (1-5%).			GS-01	X	
0.5	90.41 / 0.30	<b>Native Soil:</b> Firm to stiff, brown silt, some clay and sand, moist. Presence of organic matter (rootlets) (1%).			GS-02	X	
1.0	89.81 / 0.90	Firm to stiff, grey-orange clayey silt, traces of sand, moist.			GS-03	X	
2.0	88.71 / 2.00	Firm to stiff, grey clayey silt to silt and clay, moist.			GS-04	X	
3.0	87.71 / 3.00	End of test pit (voluntary termination)					
3.5							
4.0							
4.5							
5.0							
5.5							

Remark(s) : Easy to excavate  
 No water infiltration  
 Stables walls  
 The compactness / consistency is estimated



# TEST PIT REPORT

Reference No.: 12615684-A1

**Test Pit No.: TP-113-23**

Client : **Medusa Limited Partnership**

Geodetic Coordinates X : **366436**

MTM-9 (NAD-1983) Y : **5017625**

Project : **Geotechnical Investigation - Proposed Distribution Center**

Z : **90.56**

Location : **Bill Leatham Drive, Ottawa, Ontario**

*Preliminary*

Location Plan No.: **FIGURE 1**

Executed by : **Demolition Plus**

Date (Start) : **2023-07-07**

Described by : **Mathieu Chénier, Tech.**

Verified by : **Keshini Rangasamy, CEP**

Date (Finish) : **2023-07-07**

Test Pit Depth (m): **2.90**

DEPTH - m	ELEVATION / DEPTH - m	STRATIGRAPHY		SAMPLE		WATER INFILTRATION	TEST SYMBOL
		SOIL DESCRIPTION	SYMBOL	SAMPLE TYPE AND NUMBER	STATE		
	90.56	Ground Surface					
	0.00	<b>Topsoil:</b> Brown silt, some clay, traces of sand, moist. Presence of organic matter (rootlets) (1-5%).		GS-01	X		SA
0.5	90.21 / 0.35	<b>Native Soil:</b> Firm to stiff, brown silt, some clay, traces of sand, moist. Presence of organic matter (rootlets) (1-5%).		GS-02	X		
	89.81 / 0.75	Firm to stiff, grey silt, some clay, moist.		GS-03	X		
2.0	88.76 / 1.80	Firm to stiff, grey-orange clayey silt, traces of sand, moist.		GS-04	X		
3.0	87.66 / 2.90	End of test pit (voluntary termination)					

Remark(s) :  
 Easy to excavate  
 No water infiltration  
 Stables walls  
 The compactness / consistency is estimated  
 SA: Soil Aggressiveness



# TEST PIT REPORT

Reference No.: 12615684-A1

**Test Pit No.: TP-114-23**

Client : **Medusa Limited Partnership**

Geodetic Coordinates X : **366577**

MTM-9 (NAD-1983) Y : **5017568**

Project : **Geotechnical Investigation - Proposed Distribution Center**

Z : **90.27**

Location : **Bill Leatham Drive, Ottawa, Ontario**

*Preliminary*

Location Plan No.: **FIGURE 1**

Executed by : **Demolition Plus**

Date (Start) : **2023-07-07**

Described by : **Mathieu Chénier, Tech.**

Verified by : **Keshini Rangasamy, CEP**

Date (Finish) : **2023-07-07**

Test Pit Depth (m): **3.00**

DEPTH - m	ELEVATION / DEPTH - m	STRATIGRAPHY		SAMPLE		WATER INFILTRATION	TEST SYMBOL
		SOIL DESCRIPTION	SYMBOL	SAMPLE TYPE AND NUMBER	STATE		
	90.27	Ground Surface					GSA : Particle Size Analysis H : Hydrometer Testing CA : Chemical Analysis LL : Liquid Limit PL : Plastic Limit W : Water Content Dup : Duplicate Sample Taken OM : Organic Matter Content
	0.00	<b>Topsoil:</b> Brown-grey silt, some clay and sand, moist. Presence of organic matter (rootlets) (1-5%).			GS-01	X	
0.5	89.96 / 0.30	<b>Native Soil:</b> Firm to stiff, brown silt, some clay, traces of sand, moist. Presence of organic matter (rootlets) (1%).			GS-02	X	
1.0	89.37 / 0.90	Firm to stiff, grey-orange silt, some clay to clayey, traces of sand, moist.			GS-03	X	
2.0					GS-04	X	
3.0	87.27 / 3.00	End of test pit (voluntary termination)					SA

Remark(s) :  
 Easy to excavate  
 No water infiltration  
 Stables walls  
 The compactness / consistency is estimated  
 SA: Soil Aggressiveness



**TEST PIT REPORT**

**TEST PIT No.**

**TP-01**

CLIENT: MEDUSA LP	GEODETC COORDINATES (m) (MTM, NAD-83) X : 366239.2 Y : 5017861.2 Z : 90.67	← - INFILTRATION ▼ - WATER LEVEL
PROJECT: PROPOSED SORTATION FACILITY		
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type	Manual tests
DATE: 2021-05-03	CA : Chemical analysis PS : Proctor Sample	PA : Panda (q <sub>d</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )
DATE: 2021-05-03	RC : Rock core GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> ) GVT: Geonor Vane tester (C <sub>v</sub> )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	
					Type	▼
0,0	90.67					←
0.30	90.37		<b>Remoulded native soil / topsoil:</b> Clayey silt, traces of sand. Traces of roots and organics	GS-1 GSE-1	w = 33.0% Wl = 63.0% Wp = 26.0 %	←
0.5			<b>Native soil:</b> Stiff to very stiff, brown-grey silt and clay, very moist	GS-2		
0.80	89.87		becoming grey	GS-3		
1.5	89.17		becoming stiff, saturated	GS-4		
2.80	87.87		End of test pit  Note: Slight water infiltration at 2.80m			←

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-01 excavation.



Photo 2 : TP-01 materials.



**Test Pit No. TP-01**  
**Proposed Sortation Facility**  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario





**TEST PIT REPORT**

**TEST PIT No.**

**TP-02**

CLIENT: MEDUSA LP	GEODETIC COORDINATES (m) (MTM, NAD-83) X : 366350.8 Y : 5017942.4 Z : 90.59	← - INFILTRATION
PROJECT: PROPOSED SORTATION FACILITY		▼ - WATER LEVEL
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type		Manual tests	
DATE: 2021-05-03	CA : Chemical analysis	PS : Proctor Sample	PA : Panda (q <sub>d</sub> )	
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon	AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )	
DATE: 2021-05-03	RC : Rock core	GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> )	
			GVT: Geonor Vane tester (C <sub>v</sub> )	

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	
					Type	▼
0,0	90.59					←
0.30	90.29		<b>Remoulded native soil / topsoil:</b> Clayey silt, traces of sand. Traces of roots and organics	GS-1		
0.5			<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist	GS-2		
0.70	89.89		becoming grey			
1.0				GS-3		
1.5	89.09		becoming stiff, saturated			
2.0				GS-4		
3.0	87.59		End of test pit			
3.5			Note: No water infiltration			
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-02 excavation.



Photo 2 : TP-02 materials.



**Test Pit No. TP-02**  
**Proposed Sortation Facility**  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario



**TEST PIT REPORT**

**TEST PIT No.**

**TP-03**

CLIENT: MEDUSA LP	GEODETC COORDINATES (m) (MTM, NAD-83) X : 366431.0 Y : 5017938.4 Z : 90.52	← - INFILTRATION ▼ - WATER LEVEL
PROJECT: PROPOSED SORTATION FACILITY		
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type		Manual tests
DATE: 2021-05-03	CA : Chemical analysis	PS : Proctor Sample	PA : Panda (q <sub>d</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon	AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )
DATE: 2021-05-03	RC : Rock core	GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> ) GVT: Geonor Vane tester (C <sub>v</sub> )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	▼
					Type	
0,0	90.52					
			<b>Remoulded native soil / topsoil:</b> Clayey silt, traces of sand. Traces of roots and organics	GS-1		
0.30	90.22		<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist	GS-2		
0.5						
0.70	89.82		becoming grey, very moist			
1.0				GS-3		
1.5						
1.80	88.72		becoming stiff with traces of sand, saturated			
2.0				GS-4		
2.5						
3.0	2.90		End of test pit			
3.5			Note: No water infiltration			
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-03 excavation.



Photo 2 : TP-03 materials.



**Test Pit No. TP-04**  
**Proposed Sortation Facility**  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario

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**TEST PIT REPORT**

**TEST PIT No.**

**TP-04**

CLIENT: MEDUSA LP	GEODETTIC COORDINATES (m) (MTM, NAD-83) X : 366476.0 Y : 5018013.0 Z : 90.46	← - INFILTRATION ▼ - WATER LEVEL
PROJECT: PROPOSED SORTATION FACILITY		
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type	Manual tests
DATE: 2021-05-03	CA : Chemical analysis PS : Proctor Sample	PA : Panda (q <sub>d</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )
DATE: 2021-05-03	RC : Rock core GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> ) GVT: Geonor Vane tester (C <sub>v</sub> )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	▼
					Type	
0,0	90.46					
			<b>Remoulded native soil / topsoil:</b> Clayey silt, traces of sand. Traces of roots and organics	GS-1 GSE-1		
0.30	90.16		<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist	GS-2		
0.70	89.76		becoming very moist			
1.0				GS-3		
1.60	88.86		becoming stiff with traces of sand, grey, saturated			
2.0				GS-4		
2.5				GS-5		
3.0						
3.10	87.36		End of test pit  Note: Slight water infiltration at 3.10m			←
3.5						
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-04 excavation.



Photo 2 : TP-04 materials.



**Test Pit No. TP-04**  
**Proposed Sortation Facility**  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario

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**TEST PIT REPORT**

**TEST PIT No.**

**TP-05**

CLIENT: MEDUSA LP	GEODETTIC COORDINATES (m) (MTM, NAD-83) X : 366565.4 Y : 5018013.4 Z : 90.60	← - INFILTRATION
PROJECT: PROPOSED SORTATION FACILITY		▼ - WATER LEVEL
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type		Manual tests
DATE: 2021-05-03	CA : Chemical analysis	PS : Proctor Sample	PA : Panda (q <sub>d</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon	AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )
DATE: 2021-05-03	RC : Rock core	GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> )
			GVT: Geonor Vane tester (C <sub>v</sub> )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	
					Type	▼
0,0	90.60					←
			<b>Remoulded native soil / topsoil:</b> Clayey silt, traces of sand. Traces of roots and organics	GS-1		
0.30	90.30		<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist	GS-2		
0.5						
0.70	89.90		becoming grey, very moist			
1.0				GS-3		
1.5						
2.0				GS-4		
2.20	88.40		becoming stiff, saturated			
2.5				GS-5		
3.0	87.60		End of test pit			
			Note: No water infiltration			
3.5						
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations

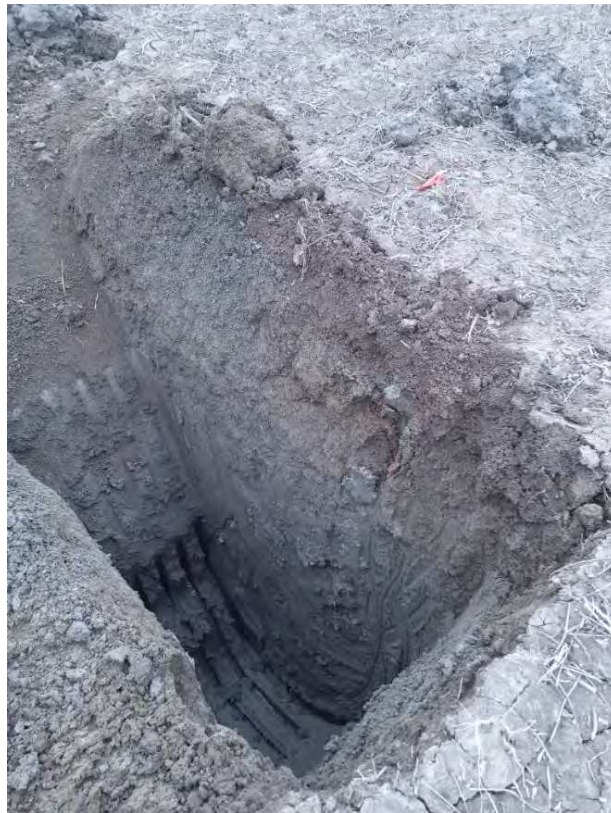


Photo 1 : TP-05 excavation.



Photo 2 : TP-05 materials.



**Test Pit No. TP-05**  
**Proposed Sortation Facility**  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario





### TEST PIT REPORT

TEST PIT No.

TP-06

CLIENT: MEDUSA LP	GEODETC COORDINATES (m) (MTM, NAD-83) X : 366603.7 Y : 5018084.5 Z : 90.61	← - INFILTRATION ▼ - WATER LEVEL
PROJECT: PROPOSED SORTATION FACILITY		
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type	Manual tests
DATE: 2021-05-04	CA : Chemical analysis PS : Proctor Sample	PA : Panda (q <sub>d</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )
DATE: 2021-05-04	RC : Rock core GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> ) GVT: Geonor Vane tester (C <sub>v</sub> )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	▼
					Type	
0,0	90.61					
0.30	90.31		<b>Remoulded native soil / topsoil:</b> Clayey silt, traces of sand. Traces of roots and organics	GS-1 GSE-1		
0.5			<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist	GS-2		
0.80	89.81		becoming grey, very moist			
1.0				GS-3		
1.5						
1.80	88.81		becoing stiff, saturated			
2.0				GS-4		
2.5						
3.0	87.61		End of test pit			
3.5			Note: No water infiltration			
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-06 excavation.



Photo 2 : TP-06 materials.



**Test Pit No. TP-06**  
**Proposed Sortation Facility**  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario



**TEST PIT REPORT**

**TEST PIT No.**

**TP-15**

CLIENT: MEDUSA LP	GEODETTIC COORDINATES (m) (MTM, NAD-83) X : 366292.5 Y : 5017826.9 Z : 90.65	← - INFILTRATION
PROJECT: PROPOSED SORTATION FACILITY		▼ - WATER LEVEL
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type		Manual tests
DATE: 2021-05-03	CA : Chemical analysis	PS : Proctor Sample	PA : Panda (q <sub>d</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon	AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )
DATE: 2021-05-03	RC : Rock core	GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> )
			GVT: Geonor Vane tester (C <sub>v</sub> )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	▼
					Type	
0,0	90.65					
			<b>Remoulded native soil / topsoil:</b> Clayey silt, traces of sand. Traces of roots and organics	GS-1		
0.30	90.35		<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist	GS-2		
0.5						
0.70	89.95		becoming grey, very moist			
1.0				GS-3		
1.5						
1.60	89.05		becoming stiff, saturated			
2.0				GS-4		
2.5						
2.80	87.85		End of test pit			
3.0			Note: Slight water infiltration at 2.80m			
3.5						
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-15 excavation.



Photo 1 : TP-15 materials.



**Test Pit No. TP-15**  
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**TEST PIT REPORT**

**TEST PIT No.**

**TP-16**

CLIENT: MEDUSA LP	GEODETTIC COORDINATES (m) (MTM, NAD-83) X : 366351.7 Y : 5017860.4 Z : 90.62	← - INFILTRATION ▼ - WATER LEVEL
PROJECT: PROPOSED SORTATION FACILITY		
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type	Manual tests
DATE: 2021-05-03	CA : Chemical analysis PS : Proctor Sample	PA : Panda (q <sub>d</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )
DATE: 2021-05-03	RC : Rock core GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> ) GVT: Geonor Vane tester (C <sub>v</sub> )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	▼
					Type	
0,0	90.62					
			<b>Remoulded native soil / topsoil:</b> Clayey silt, traces of sand. Traces of roots and organics	GS-1 GSE-1		
0.30	90.32		<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist	GS-2		
0.5						
0.80	89.82		becoming grey, very moist			
1.0				GS-3		
1.5	89.12		becoming stiff, saturated			
1.50				GS-4		
2.0						
2.5				GS-5		
3.0	87.62		End of test pit			
			Note: No water infiltration			
3.5						
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-16 excavation.



Photo 2 : TP-16 materials.



**Test Pit No. TP-16**  
**Proposed Sortation Facility**  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario

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**TEST PIT REPORT**

**TEST PIT No.**

**TP-17**

CLIENT: MEDUSA LP	GEODETTIC COORDINATES (m) (MTM, NAD-83)	< - INFILTRATION ▼ - WATER LEVEL
PROJECT: PROPOSED SORTATION FACILITY	X : 366450.1	
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO	Y : 5017904.3 Z : 90.59	

DESCRIBED BY: M. CHÉNIER	Sample type		Manual tests
DATE: 2021-05-03	CA : Chemical analysis	PS : Proctor Sample	PA : Panda (q <sub>d</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon	AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )
DATE: 2021-05-03	RC : Rock core	GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> ) GVT: Geonor Vane tester (C <sub>v</sub> )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	
					Type	▼
0,0	90.59					<
			<b>Remoulded native soil / topsoil:</b> Clayey silt, traces of sand. Traces of roots and organics	GS-1		
0.30	90.29		<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist	GS-2		
0.5						
0.80	89.79		becoming grey, very moist			
1.0				GS-3		
1.5	1.45		End of test pit  Note: No water infiltration			
2.0						
2.5						
3.0						
3.5						
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-17 excavation.



Photo 10 : TP-17 materials.



**Test Pit No. TP-17**  
**Proposed Sortation Facility**  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario





**TEST PIT REPORT**

**TEST PIT No.**

**TP-18**

CLIENT: MEDUSA LP	GEODETC COORDINATES (m) (MTM, NAD-83) X : 366524.8 Y : 5017946.2 Z : 90.55	← - INFILTRATION ▼ - WATER LEVEL
PROJECT: PROPOSED SORTATION FACILITY		
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type		Manual tests
DATE: 2021-05-03	CA : Chemical analysis	PS : Proctor Sample	PA : Panda (q <sub>d</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon	AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )
DATE: 2021-05-03	RC : Rock core	GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> ) GVT: Geonor Vane tester (C <sub>v</sub> )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	▼ ←
					Type	
0,0	90.55					
0.30	90.25		<b>Remoulded native soil / topsoil:</b> Clayey silt, traces of sand. Traces of roots and organics	GS-1		
0.5			<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist	GS-2		
0.90	89.65		becoming grey, very moist	GS-3		
1.5	89.05		End of test pit  Note: No water infiltration			
2.0						
2.5						
3.0						
3.5						
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-18 excavation.



Photo 2 : TP-18 materials.



**Test Pit No. TP-18**  
**Proposed Sortation Facility**  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario



**TEST PIT REPORT**

**TEST PIT No.**

**TP-19**

CLIENT: MEDUSA LP	GEODETC COORDINATES (m) (MTM, NAD-83) X : 366584.3 Y : 5017980.1 Z : 90.68	← - INFILTRATION ▼ - WATER LEVEL
PROJECT: PROPOSED SORTATION FACILITY		
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type		Manual tests
DATE: 2021-05-04	CA : Chemical analysis	PS : Proctor Sample	PA : Panda (q <sub>d</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon	AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )
DATE: 2021-05-04	RC : Rock core	GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> ) GVT: Geonor Vane tester (C <sub>v</sub> )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	
					Type	▼
0,0	90.68					←
			<b>Remoulded native soil / topsoil:</b> Clayey silt, traces of sand. Traces of roots and organics	GS-1 GSE-1		
0.30	90.38		<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist	GS-2		
0.5						
0.70	89.98		becoming grey, very moist			
1.0				GS-3		
1.5	89.18		End of test pit  Note: No water infiltration			
2.0						
2.5						
3.0						
3.5						
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-19 excavation.



Photo 1 : TP-19 materials.



**Test Pit No. TP-19**  
**Proposed Sortation Facility**  
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**TEST PIT REPORT**

**TEST PIT No.**

**TP-20**

CLIENT: MEDUSA LP	GEODETC COORDINATES (m) (MTM, NAD-83) X : 366653.2 Y : 5017996.1 Z : 90.52	← - INFILTRATION ▼ - WATER LEVEL
PROJECT: PROPOSED SORTATION FACILITY		
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type	Manual tests
DATE: 2021-05-04	CA : Chemical analysis PS : Proctor Sample	PA : Panda (q <sub>d</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )
DATE: 2021-05-04	RC : Rock core GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> ) GVT: Geonor Vane tester (C <sub>v</sub> )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	▼
					Type	
0,0	90.52					
0.30	90.22		<b>Remoulded native soil / topsoil:</b> Clayey silt, traces of sand. Traces of roots and organics	GS-1 GSE-1		
0.5			<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist	GS-2		
0.70	89.82		becoming grey, very moist			
1.0				GS-3		
1.40	89.12		becoming stiff with traces of sand, saturated			
2.0				GS-4		
2.5				GS-5		
3.0	87.52		End of test pit			
3.5			Note: Slight water infiltration at 3.0m			
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-20 excavation.



Photo 2 : TP-20 materials.



**Test Pit No. TP-20**  
**Proposed Sortation Facility**  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario

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**TEST PIT REPORT**

**TEST PIT No.**

**TP-24**

CLIENT: MEDUSA LP	GEODETIC COORDINATES (m) (MTM, NAD-83) X : 366263.6 Y : 5017757.8 Z : 90.68	← - INFILTRATION
PROJECT: PROPOSED SORTATION FACILITY		▼ - WATER LEVEL
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type		Manual tests	
DATE: 2021-05-03	CA : Chemical analysis	PS : Proctor Sample	PA : Panda (q <sub>d</sub> )	
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon	AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )	
DATE: 2021-05-03	RC : Rock core	GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> )	
			GVT: Geonor Vane tester (C <sub>v</sub> )	

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	
					Type	▼
0,0	90.68					←
0.5	90.18		<b>Remoulded native soil / topsoil:</b> Clayey silt, traces of sand. Traces of roots and organics	GS-1		
1.0	89.68		<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist becoming grey, very moist	GS-2		
1.5				GS-3		
2.0	88.68		becoming stiff, saturated	GS-4		
2.5						
3.0	87.68		End of test pit  Note: No water infiltration			
3.5						
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-24 excavation.



Photo 2 : TP-24 materials.



**Test Pit No. TP-24**  
**Proposed Sortation Facility**  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario





**TEST PIT REPORT**

**TEST PIT No.**

**TP-25**

CLIENT: MEDUSA LP	GEODETC COORDINATES (m) (MTM, NAD-83) X : 366327.0 Y : 5017764.9 Z : 90.71	← - INFILTRATION ▼ - WATER LEVEL
PROJECT: PROPOSED SORTATION FACILITY		
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type	Manual tests
DATE: 2021-05-03	CA : Chemical analysis PS : Proctor Sample	PA : Panda (q <sub>d</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )
DATE: 2021-05-03	RC : Rock core GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> )
		GVT: Geonor Vane tester (C <sub>v</sub> )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	
					Type	▼
0,0	90.71					←
			<b>Remoulded native soil / topsoil:</b> Clayey silt, traces of sand. Traces of roots and organics	GS-1 GSE-1		
0.30	90.41		<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist	GS-2		
0.70	90.01		becoming grey, very moist to saturated			
1.0						
1.5				GS-3	w = 37.0% Wl = 53.0% Wp = 24.0 %	
2.0						
2.10	88.61		Firm, grey sandy and clayey silt, saturated	GS-4		
2.5						
3.0	87.81		Stiff, grey clayey silt, saturated	GS-5		
3.30	87.41		End of test pit			
3.5			Note: No water infiltration			
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-25 excavation.



Photo 2 : TP-25 materials.



**Test Pit No. TP-25**  
**Proposed Sortation Facility**  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario



**TEST PIT REPORT**

**TEST PIT No.**

**TP-26**

CLIENT: MEDUSA LP	GEODETIC COORDINATES (m) (MTM, NAD-83) X : 366386.2 Y : 5017798.3 Z : 90.68	← - INFILTRATION
PROJECT: PROPOSED SORTATION FACILITY		▼ - WATER LEVEL
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type		Manual tests
DATE: 2021-05-03	CA : Chemical analysis	PS : Proctor Sample	PA : Panda (q <sub>d</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon	AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )
DATE: 2021-05-03	RC : Rock core	GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> )
			GVT: Geonor Vane tester (C <sub>v</sub> )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	▼
					Type	
0,0	90.68					
			<b>Remoulded native soil / topsoil:</b> Clayey silt, traces of sand. Traces of roots and organics	GS-1		
0.30	90.38		<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist	GS-2		
0.5						
0.70	89.98		becoming grey, very moist			
1.0				GS-3		
1.5						
1.80	88.88		becoming stiff, saturated			
2.0				GS-4		
2.5						
3.0	2.90		End of test pit			
3.5			Note: No water infiltration			
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-26 excavation.



Photo 2 : TP-26 materials.



**Test Pit No. TP-26**  
**Proposed Sortation Facility**  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario

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**TEST PIT REPORT**

**TEST PIT No.**

**TP-27**

CLIENT: MEDUSA LP	GEODETC COORDINATES (m) (MTM, NAD-83) X : 366471.1 Y : 5017866.9 Z : 90.58	← - INFILTRATION ▼ - WATER LEVEL
PROJECT: PROPOSED SORTATION FACILITY		
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type		Manual tests
DATE: 2021-05-03	CA : Chemical analysis	PS : Proctor Sample	PA : Panda (q <sub>d</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon	AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )
DATE: 2021-05-03	RC : Rock core	GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> ) GVT: Geonor Vane tester (C <sub>v</sub> )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	▼ ←
					Type	
0,0	90.58					
0.30	90.28		<b>Remoulded native soil / topsoil:</b> Clayey silt, traces of sand. Traces of roots and organics	GS-1 GSE-1		
0.5			<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist	GS-2		
0.70	89.88		becoming grey, very moist			
1.0				GS-3		
1.5	89.08		End of test pit  Note: No water infiltration			
2.0						
2.5						
3.0						
3.5						
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-27 excavation.



Photo 2 : TP-27 materials.



**Test Pit No. TP-27**  
**Proposed Sortation Facility**  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario

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**TEST PIT REPORT**

**TEST PIT No.**

**TP-28**

CLIENT: MEDUSA LP	GEODETC COORDINATES (m) (MTM, NAD-83) X : 366545.7 Y : 5017908.9 Z : 90.71	← - INFILTRATION ▼ - WATER LEVEL
PROJECT: PROPOSED SORTATION FACILITY		
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type	Manual tests
DATE: 2021-05-03	CA : Chemical analysis PS : Proctor Sample	PA : Panda (q <sub>d</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )
DATE: 2021-05-03	RC : Rock core GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> ) GVT: Geonor Vane tester (C <sub>v</sub> )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	▼
					Type	
0,0	90.71					
0.30	90.41		<b>Remoulded native soil / topsoil:</b> Clayey silt, traces of sand. Traces of roots and organics	GS-1 GSE-1		
0.5			<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist	GS-2		
0.80	89.91		becoming grey, very moist			
1.0				GS-3		
1.5	89.21		End of test pit  Note: No water infiltration			
2.0						
2.5						
3.0						
3.5						
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-28 excavation.



Photo 2 : TP-28 materials.



**Test Pit No. TP-28**  
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**TEST PIT REPORT**

**TEST PIT No.**

**TP-29**

CLIENT: MEDUSA LP	GEODETIC COORDINATES (m) (MTM, NAD-83) X : 366605.4 Y : 5017942.6 Z : 90.72	← - INFILTRATION
PROJECT: PROPOSED SORTATION FACILITY		▼ - WATER LEVEL
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type		Manual tests	
DATE: 2021-05-04	CA : Chemical analysis	PS : Proctor Sample	PA : Panda (q <sub>d</sub> )	
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon	AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )	
DATE: 2021-05-04	RC : Rock core	GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> )	
			GVT: Geonor Vane tester (C <sub>v</sub> )	

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	
					Type	▼
0,0	90.72					←
			<b>Remoulded native soil / topsoil:</b> Clayey silt, traces of sand. Traces of roots and organics	GS-1		
0.30	90.42		<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist	GS-2		
0.5			becoming grey, very moist			
0.70	90.02					
1.0				GS-3		
1.5	1.45		End of test pit  Note: No water infiltration			
2.0						
2.5						
3.0						
3.5						
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-29 excavation.



Photo 2 : TP-29 materials.



**Test Pit No. TP-29**  
**Proposed Sortation Facility**  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario



**TEST PIT REPORT**

**TEST PIT No.**

**TP-30**

CLIENT: MEDUSA LP	GEODETTIC COORDINATES (m) (MTM, NAD-83) X : 366492.8 Y : 5017827.9 Z : 90.56	← - INFILTRATION
PROJECT: PROPOSED SORTATION FACILITY		▼ - WATER LEVEL
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type		Manual tests
DATE: 2021-05-03	CA : Chemical analysis	PS : Proctor Sample	PA : Panda (q <sub>d</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon	AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )
DATE: 2021-05-03	RC : Rock core	GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> )
			GVT: Geonor Vane tester (C <sub>v</sub> )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	
					Type	▼
0,0	90.56					←
			<b>Remoulded native soil / topsoil:</b> Clayey silt, traces of sand. Traces of roots and organics	GS-1 GSE-1		
0.30	90.26		<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist	GS-2		
0.5						
0.70	89.86		becoming grey, very moist			
1.0				GS-3		
1.5						
1.70	88.86		becoming stiff with traces of sand			
2.0				GS-4		
2.5						
2.60	87.96		Stiff, grey sandy and clayey silt, saturated	GS-5		
3.0	3.00	87.56	End of test pit			
			Note: No water infiltration			
3.5						
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-30 excavation.



Photo 2 : TP-30 materials.



**Test Pit No. TP-30**  
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**TEST PIT REPORT**

**TEST PIT No.**

**TP-31**

CLIENT: MEDUSA LP	GEODETC COORDINATES (m) (MTM, NAD-83) X : 366627.4 Y : 5017903.3 Z : 90.41	← - INFILTRATION ▼ - WATER LEVEL
PROJECT: PROPOSED SORTATION FACILITY		
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type	Manual tests
DATE: 2021-05-04	CA : Chemical analysis PS : Proctor Sample	PA : Panda (q <sub>d</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )
DATE: 2021-05-04	RC : Rock core GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> ) GVT: Geonor Vane tester (C <sub>v</sub> )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	▼
					Type	
0,0	90.41					
0.30	90.11		<b>Remoulded native soil / topsoil:</b> Clayey silt, traces of sand. Traces of roots and organics	GS-1 GSE-1		
0.5			<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist	GS-2		
0.80	89.61		becoming grey, very moist			
1.0				GS-3		
1.5						
1.70	88.71		becoming stiff with traces of sand, saturated			
2.0				GS-4		
2.5						
3.0	87.41		End of test pit			
3.5			Note: No water infiltration			
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-31 excavation.



Photo 2 : TP-31 materials.



**Test Pit No. TP-31**  
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**TEST PIT REPORT**

**TEST PIT No.**

**TP-35**

CLIENT: MEDUSA LP	GEODETIC COORDINATES (m) (MTM, NAD-83) X : 366558.2 Y : 5017809.8 Z : 90.46	< - INFILTRATION ▼ - WATER LEVEL
PROJECT: PROPOSED SORTATION FACILITY		
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type		Manual tests	
DATE: 2021-05-05	CA : Chemical analysis	PS : Proctor Sample	PA : Panda (q <sub>d</sub> )	PP : Portable penetrometer (C <sub>u</sub> ) DP: Dynamic penetrometer (E <sub>25</sub> ) GVT: Geonor Vane tester (C <sub>v</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon	AU: Auger		
DATE: 2021-05-05	RC : Rock core	GS(E) : Grab sample (environment)		

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	
					Type	
0,0	90.46					
0.30	90.16		<b>Topsoil:</b> Brown clayey silt, moist. Traces of roots and organics	GS-1		
0.5			<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist	GS-2		
0.70	89.76		becoming grey, very moist			
1.0						
1.5				GS-3	w = 30.0% Wl = 59.0% Wp = 25.0 %	
1.80	88.66		becoming stiff, very moist to saturated			
2.0						
2.5				GS-4		
3.0	87.46		End of test pit			
3.5			Note: No water infiltration			
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-35 excavation.



Photo 2 : TP-35 materials.



**Test Pit No. TP-35**  
**Proposed Sortation Facility**  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario





**TEST PIT REPORT**

**TEST PIT No.**

**TP-36**

CLIENT: MEDUSA LP	GEODETTIC COORDINATES (m) (MTM, NAD-83) X : 366701.1 Y : 5017889.7 Z : 90.34	← - INFILTRATION ▼ - WATER LEVEL
PROJECT: PROPOSED SORTATION FACILITY		
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type		Manual tests
DATE: 2021-05-05	CA : Chemical analysis	PS : Proctor Sample	PA : Panda (q <sub>d</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon	AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )
DATE: 2021-05-05	RC : Rock core	GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> )
			GVT: Geonor Vane tester (C <sub>v</sub> )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	▼
					Type	
0,0	90.34					
0.30	90.04		<b>Topsoil:</b> Brown clayey silt, moist. Traces of roots and organics	GS-1		
0.5			<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist	GS-2		
0.70	89.64		becoming stiff, grey, very moist to saturated			
1.0				GS-3		
1.5						
2.0						
2.5				GS-4		
3.0	87.34		End of test pit			
3.5			Note: No water infiltration			
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-36 excavation.



Photo 2 : TP-36 materials.



**Test Pit No. TP-36**  
**Proposed Sortation Facility**  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario



**TEST PIT REPORT**

**TEST PIT No.**

**TP-40**

CLIENT: MEDUSA LP	GEODETIC COORDINATES (m) (MTM, NAD-83) X : 366658.9 Y : 5017827.6 Z : 90.51	< - INFILTRATION ▼ - WATER LEVEL
PROJECT: PROPOSED SORTATION FACILITY		
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type		Manual tests
DATE: 2021-05-06	CA : Chemical analysis	PS : Proctor Sample	PA : Panda (q <sub>d</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon	AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )
DATE: 2021-05-06	RC : Rock core	GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> )
			GVT: Geonor Vane tester (C <sub>v</sub> )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	▼
					Type	
0,0	90.51					
0.5			<b>Topsoil:</b> Brown clayey silt, moist. Traces of roots and organics	GS-1 GSE-1		
0.60	89.91		<b>Native soil:</b> Stiff, grey silt and clay, very moist	GS-2		
1.0				GS-3		
1.5						
1.60	88.91		becoming stiff with traces of sand, very moist to saturated			
2.0				GS-4		
2.5						
3.0	87.51		End of test pit	GS-5		
3.5			Note: Slight water infiltration at 3.0m			
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 7 : TP-40 excavation.



Photo 8 : TP-40 materials.



**Test Pit No. TP-40**  
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**TEST PIT REPORT**

**TEST PIT No.**

**TP-43**

CLIENT: MEDUSA LP	GEODETIC COORDINATES (m) (MTM, NAD-83) X : 366526.6 Y : 5017723.1 Z : 93.75	← - INFILTRATION
PROJECT: PROPOSED SORTATION FACILITY		▼ - WATER LEVEL
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type		Manual tests	
DATE: 2021-05-05	CA : Chemical analysis	PS : Proctor Sample	PA : Panda (q <sub>d</sub> )	
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon	AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )	
DATE: 2021-05-05	RC : Rock core	GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> )	
			GVT: Geonor Vane tester (C <sub>v</sub> )	

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests		
					Type	▼	
0,0	93.75					←	
0.5	93.25	Fill: Stiff, brown clayey silt mixed with roots and organics, moist	Grey to brown clayey silt, moist	GS-1			
					GS-2		
1.0					GS-3		
1.5					GS-4		
2.0					GS-5		
2.5					GS-6		
3.0							
3.5	90.40		End of test pit				
			Note: No water infiltration				
4.0							
4.5							

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-43 excavation.



Photo 2 : TP-43 materials.



**Test Pit No. TP-43**  
**Proposed Sortation Facility**  
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**TEST PIT REPORT**

**TEST PIT No.**

**TP-44**

CLIENT: MEDUSA LP	GEODETIC COORDINATES (m) (MTM, NAD-83) X : 366587.9 Y : 5017715.6 Z : 90.55	< - INFILTRATION ▼ - WATER LEVEL
PROJECT: PROPOSED SORTATION FACILITY		
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type		Manual tests
DATE: 2021-05-05	CA : Chemical analysis	PS : Proctor Sample	PA : Panda ( $q_d$ )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon	AU: Auger	PP : Portable penetrometer ( $C_u$ )
DATE: 2021-05-05	RC : Rock core	GS(E) : Grab sample (environment)	DP: Dynamic penetrometer ( $E_{25}$ )
			GVT: Geonor Vane tester ( $C_u$ )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	▼ <
					Type	
0,0	90.55					
0.5	90.05		<b>Topsoil:</b> Brown clayey silt, moist. Traces of roots and organics	GS-1		
0.75	89.80		<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist becoming grey, very moist	GS-2		
1.80	88.75		becoming stiff with traces of sand	GS-3	w = 39.0% WI = 74.0% Wp = 34.0 %	
3.00	87.55		End of test pit  Note: No water infiltration	GS-4		
3.5						
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-44 excavation.



Photo 2 : TP-44 materials.



**Test Pit No. TP-44**  
**Proposed Sortation Facility**  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario





**TEST PIT REPORT**

**TEST PIT No.**

**TP-45**

CLIENT: MEDUSA LP	GEODETIC COORDINATES (m) (MTM, NAD-83) X : 366763.1 Y : 5017843.2 Z : 90.52	← - INFILTRATION ▼ - WATER LEVEL
PROJECT: PROPOSED SORTATION FACILITY		
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type		Manual tests
DATE: 2021-05-06	CA : Chemical analysis	PS : Proctor Sample	PA : Panda (q <sub>d</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon	AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )
DATE: 2021-05-06	RC : Rock core	GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> ) GVT: Geonor Vane tester (C <sub>v</sub> )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	▼ ←
					Type	
0,0	90.52					
0.30	90.22		<b>Topsoil:</b> Brown clayey silt, moist. Traces of roots and organics	GS-1 GSE-1		
0.5			<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist	GS-2		
0.60	89.92		becoming grey, very moist			
1.0				GS-3		
1.5						
1.60	88.92		becoming stiff with traces of sand, very moist to saturated	GS-4		
2.0						
2.5				GS-5		
3.0	87.52		End of test pit			
3.5			Note: No water infiltration			
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-45 excavation.



Photo 2 : TP-45 materials.



**Test Pit No. TP-45**  
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**TEST PIT REPORT**

**TEST PIT No.**

**TP-46**

CLIENT: MEDUSA LP	GEODETC COORDINATES (m) (MTM, NAD-83) X : 366877.5 Y : 5017907.6 Z : 90.36	← - INFILTRATION ▼ - WATER LEVEL
PROJECT: PROPOSED SORTATION FACILITY		
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type		Manual tests
DATE: 2021-05-06	CA : Chemical analysis	PS : Proctor Sample	PA : Panda (q <sub>d</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon	AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )
DATE: 2021-05-06	RC : Rock core	GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> ) GVT: Geonor Vane tester (C <sub>v</sub> )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	▼
					Type	
0,0	90.36					
0.30	90.06		<b>Topsoil:</b> Brown clayey silt, moist. Traces of roots and organics	GS-1 GSE-1		
0.5			<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist	GS-2		
0.70	89.66		becoming grey with traces of sand, very moist			
1.0				GS-3		
1.5						
1.60	88.76		becoing stiff very moist to saturated			
2.0				GS-4		
2.5						
3.0	3.00		End of test pit			
3.5			Note: No water infiltration			
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-46 excavation.



Photo 2 : TP-46 materials.



**Test Pit No. TP-46**  
**Proposed Sortation Facility**  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario

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**TEST PIT REPORT**

**TEST PIT No.**

**TP-47**

CLIENT: MEDUSA LP	GEODETC COORDINATES (m) (MTM, NAD-83) X : 366973.4 Y : 5017961.2 Z : 90.31	← - INFILTRATION ▼ - WATER LEVEL
PROJECT: PROPOSED SORTATION FACILITY		
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type	Manual tests
DATE: 2021-05-06	CA : Chemical analysis PS : Proctor Sample	PA : Panda (q <sub>d</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )
DATE: 2021-05-06	RC : Rock core GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> ) GVT: Geonor Vane tester (C <sub>v</sub> )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	▼
					Type	
0,0	90.31					
0.5			<b>Topsoil:</b> Brown clayey silt, moist. Traces of roots and organics	GS-1 GS-2		
0.60	89.71		<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist			
1.0				GS-3		
1.5						
1.70	88.61		becoming stiff with traces of sand, vert moist to saturated			
2.0				GS-4		
2.5						
3.0	87.31		End of test pit			
3.5			Note: No water infiltration			
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-47 excavation.



Photo 2 : TP-47 materials.



**Test Pit No. TP-47**  
**Proposed Sortation Facility**  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario



**TEST PIT REPORT**

**TEST PIT No.**

**TP-49**

CLIENT: MEDUSA LP	GEODETIC COORDINATES (m) (MTM, NAD-83) X : 366510.8 Y : 5017662.8 Z : 90.87	< - INFILTRATION ▼ - WATER LEVEL
PROJECT: PROPOSED SORTATION FACILITY		
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type		Manual tests
DATE: 2021-05-05	CA : Chemical analysis	PS : Proctor Sample	PA : Panda (q <sub>d</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon	AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )
DATE: 2021-05-05	RC : Rock core	GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> )
			GVT: Geonor Vane tester (C <sub>v</sub> )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	
					Type	▼
0.0	90.87					<
0.5			<b>Fill:</b> Brown clayey silt, moist. Presence of roots and organics	GS-1		
0.70	90.17		<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist	GS-2		
1.0						
1.30	89.57		becoming stiff, grey, very moist to saturated	GS-3		
1.5						
2.0						
2.5				GS-4		
3.0	3.00	87.87	End of test pit			
3.5			Note: No water infiltration			
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-49 excavation.



Photo 2 : TP-49 materials.



**Test Pit No. TP-49**  
**Proposed Sortation Facility**  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario

GHD | Geotechnical Investigation | 11227097-A1(1)





**TEST PIT REPORT**

**TEST PIT No. TP-49PILE**

CLIENT: MEDUSA LP	GEODETIC COORDINATES (m) (MTM, NAD-83) X : Y : Z : 92.90	< - INFILTRATION ▼ - WATER LEVEL
PROJECT: PROPOSED SORTATION FACILITY		
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type		Manual tests	
DATE: 2021-05-05	CA : Chemical analysis	PS : Proctor Sample	PA : Panda ( $q_d$ )	
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon	AU: Auger	PP : Portable penetrometer ( $C_u$ )	
DATE: 2021-05-05	RC : Rock core	GS(E) : Grab sample (environment)	DP: Dynamic penetrometer ( $E_{25}$ )	
			GVT: Geonor Vane tester ( $C_u$ )	

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	
					Type	▼
0,0	92.90					<
0.5		Fill: Brown clayey silt, moist		GS-1 GSE-1		
1.0				GS-2 GSE-2		
1.5				GS-3 GSE-3		
2.0				GS-4 GSE-4		
2.0	2.00 90.90		End of test pit  Note: No water infiltration			
2.5						
3.0						
3.5						
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-49-PILE excavation.



**Test Pit No. TP-49-PILE**  
**Proposed Sortation Facility**  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario

GHD | Geotechnical Investigation | 11227097-A1(1)



# TEST PIT REPORT

TEST PIT No.

TP-50

CLIENT: MEDUSA LP	GEODETIC COORDINATES (m) (MTM, NAD-83) X : 366472.0 Y : 5017605.6 Z : 90.55	← - INFILTRATION ▼ - WATER LEVEL
PROJECT: PROPOSED SORTATION FACILITY		
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type	Manual tests
DATE: 2021-05-05	CA : Chemical analysis PS : Proctor Sample	PA : Panda (q <sub>d</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )
DATE: 2021-05-05	RC : Rock core GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> )
		GVT: Geonor Vane tester (C <sub>v</sub> )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	▼
					Type	
0,0	90.55					
0.20	90.35		<b>Topsoil:</b> Brown clayey silt, moist. Traces of roots and organics	GS-1		
0.5			<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist	GS-2		
0.70	89.85		becoming grey, very moist			
1.0				GS-3		
1.5	89.05		becoming stiff, saturated			
2.0				GS-4		
2.5				GS-5		
3.0	87.55		End of test pit			
3.5			Note: Slight water infiltration at 3.0m			
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-50 excavation.



Photo 1 : TP-50 materials.



**Test Pit No. TP-50**  
**Proposed Sortation Facility**  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario

GHD | Geotechnical Investigation | 11227097-A1(1)



**TEST PIT REPORT**

**TEST PIT No.**

**TP-51**

CLIENT: MEDUSA LP	GEODETC COORDINATES (m) (MTM, NAD-83) X : 366550.3 Y : 5017657.8 Z : 90.42	← - INFILTRATION ▼ - WATER LEVEL
PROJECT: PROPOSED SORTATION FACILITY		
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type	Manual tests
DATE: 2021-05-05	CA : Chemical analysis PS : Proctor Sample	PA : Panda (q <sub>d</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )
DATE: 2021-05-05	RC : Rock core GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> ) GVT: Geonor Vane tester (C <sub>v</sub> )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	▼ ←
					Type	
0,0	90.42					
0.30	90.12		<b>Topsoil:</b> Brown clayey silt, moist. Traces of roots and organics	GS-1		
0.5			<b>Native soil:</b> Stiff to very stiff, brown silt and clay, moist	GS-2		
0.80	89.62		becoming grey			
1.0				GS-3		
1.5						
1.60	88.82		becoming stiff with traces of sand, moist to very moist			
2.0				GS-4		
2.5						
3.0	87.42		End of test pit			
3.5			Note: No water infiltration			
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-51 excavation.



**Test Pit No. TP-51**  
**Proposed Sortation Facility**  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario

GHD | Geotechnical Investigation | 11227097-A1(1)



**TEST PIT REPORT**

**TEST PIT No.**

**TP-52**

CLIENT: MEDUSA LP	GEODETIC COORDINATES (m) (MTM, NAD-83) X : 366538.8 Y : 5017605.5 Z : 92.69	< - INFILTRATION ▼ - WATER LEVEL
PROJECT: PROPOSED SORTATION FACILITY		
LOCATION: LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO		

DESCRIBED BY: M. CHÉNIER	Sample type		Manual tests
DATE: 2021-05-05	CA : Chemical analysis	PS : Proctor Sample	PA : Panda (q <sub>d</sub> )
VERIFIED BY: M.-A. RICHARD / A. FIORILLI	MSS: Manual split spoon	AU: Auger	PP : Portable penetrometer (C <sub>u</sub> )
DATE: 2021-05-05	RC : Rock core	GS(E) : Grab sample (environment)	DP: Dynamic penetrometer (E <sub>25</sub> )
			GVT: Geonor Vane tester (C <sub>v</sub> )

Depth (m)	Elevation (m)	Symbol	STRATIGRAPHY	Sample type & Number	Tests	
					Type	
0,0	92.69					
0.5			<b>Fill:</b> Brown clayey silt, moist	GS-1		
1.0				GS-2		
1.5				GS-3		
2.0				GS-4		
2.5				GS-5		
2.70	89.99		<b>Native soil:</b> Stiff, grey clayey silt, very moist	GS-6		
3.0						
3.32	89.37		End of test pit  Note: No water infiltration			
3.5						
4.0						
4.5						

See the attached explicative note for the complete list of symbols and abbreviations



Photo 1 : TP-52 excavation.

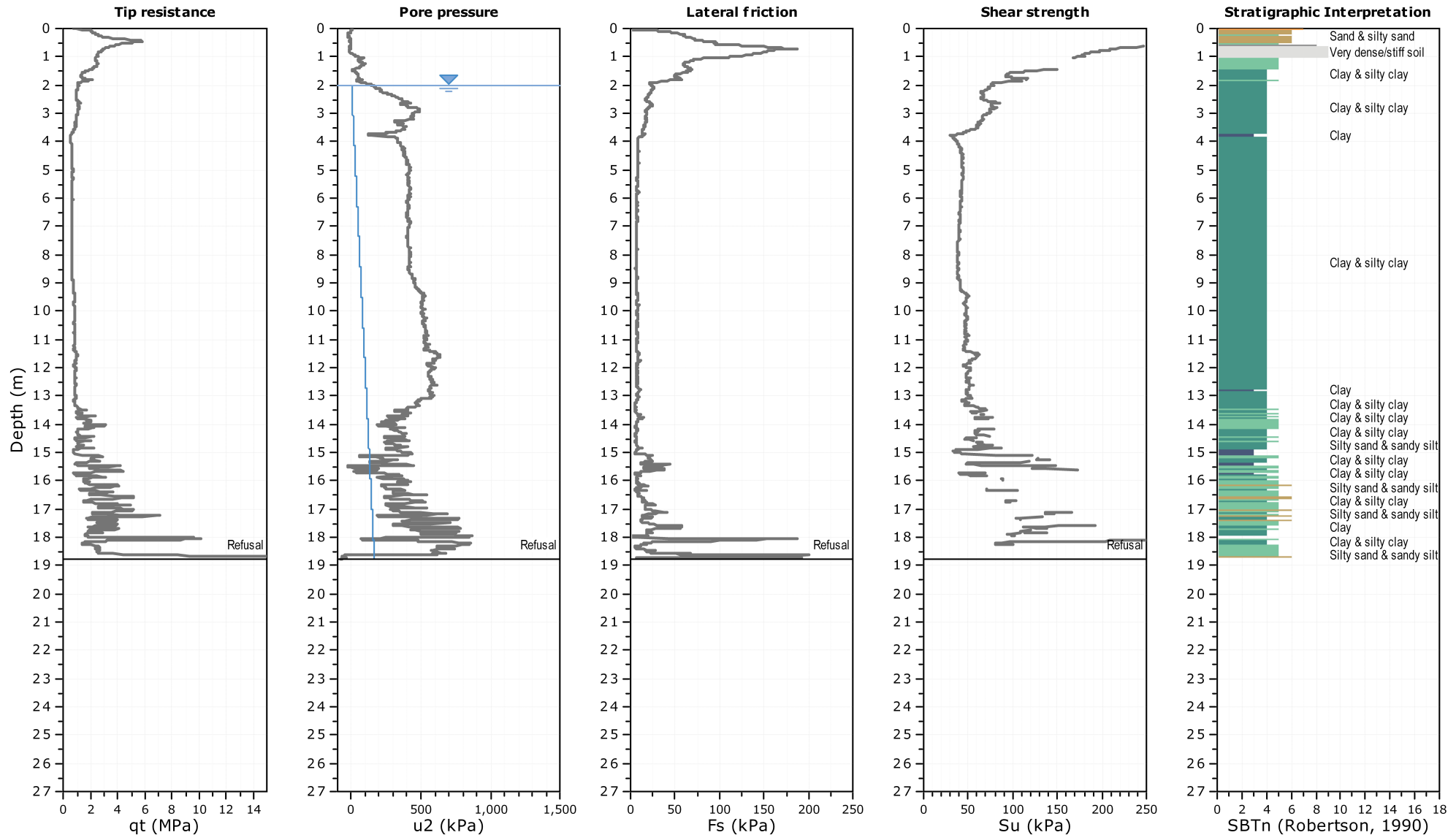


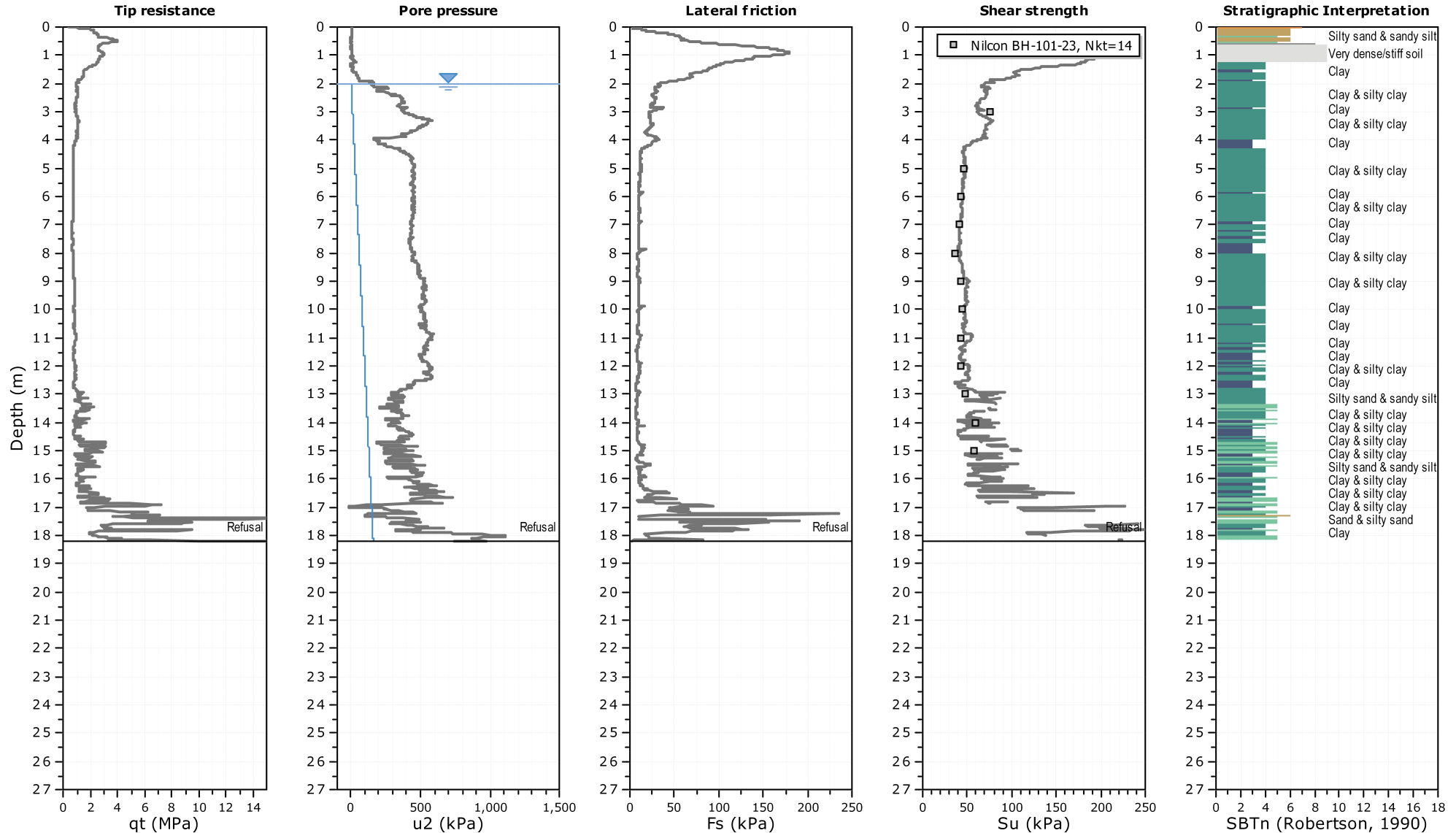
Photo 2 : TP-52 materials.

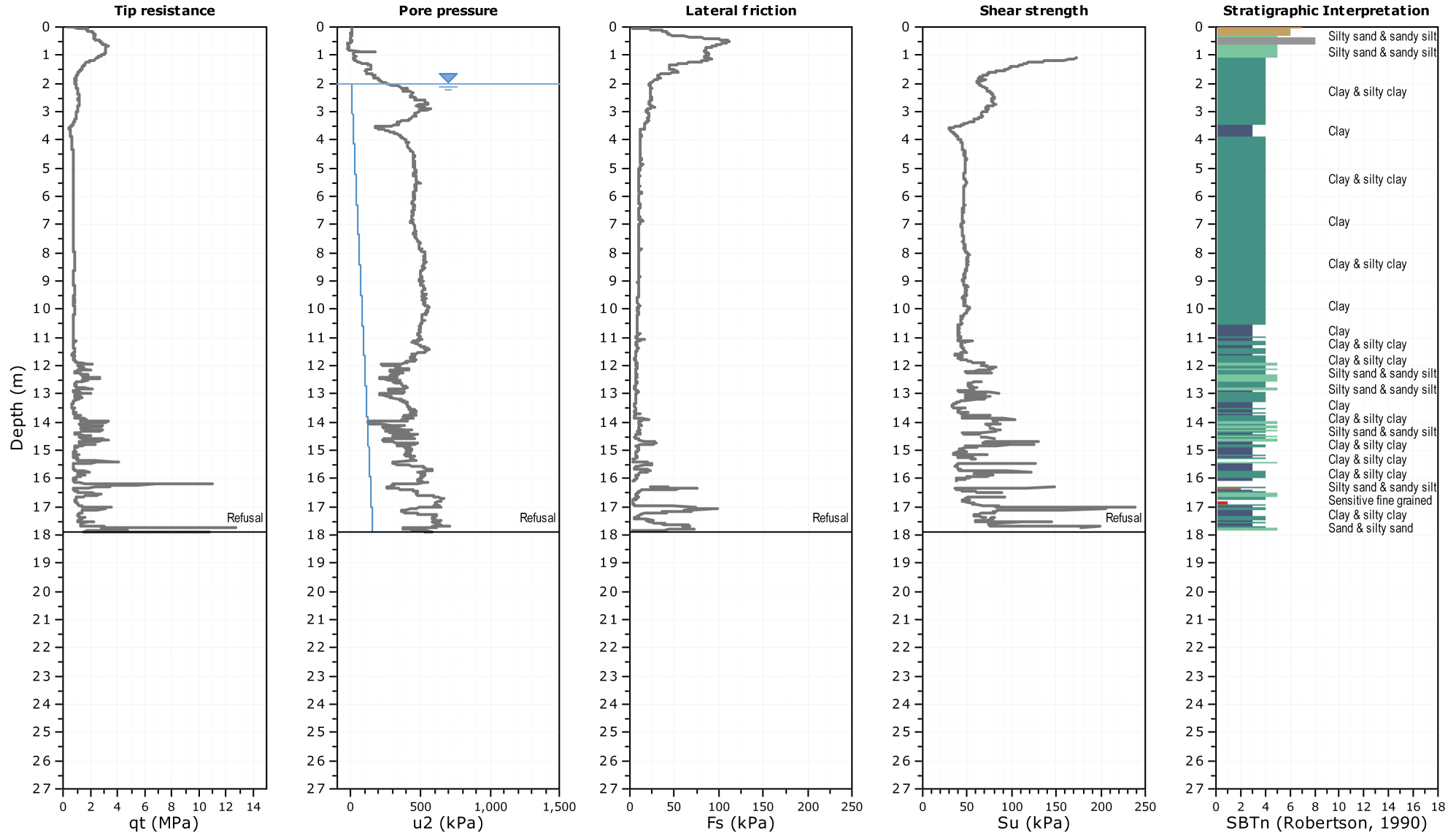


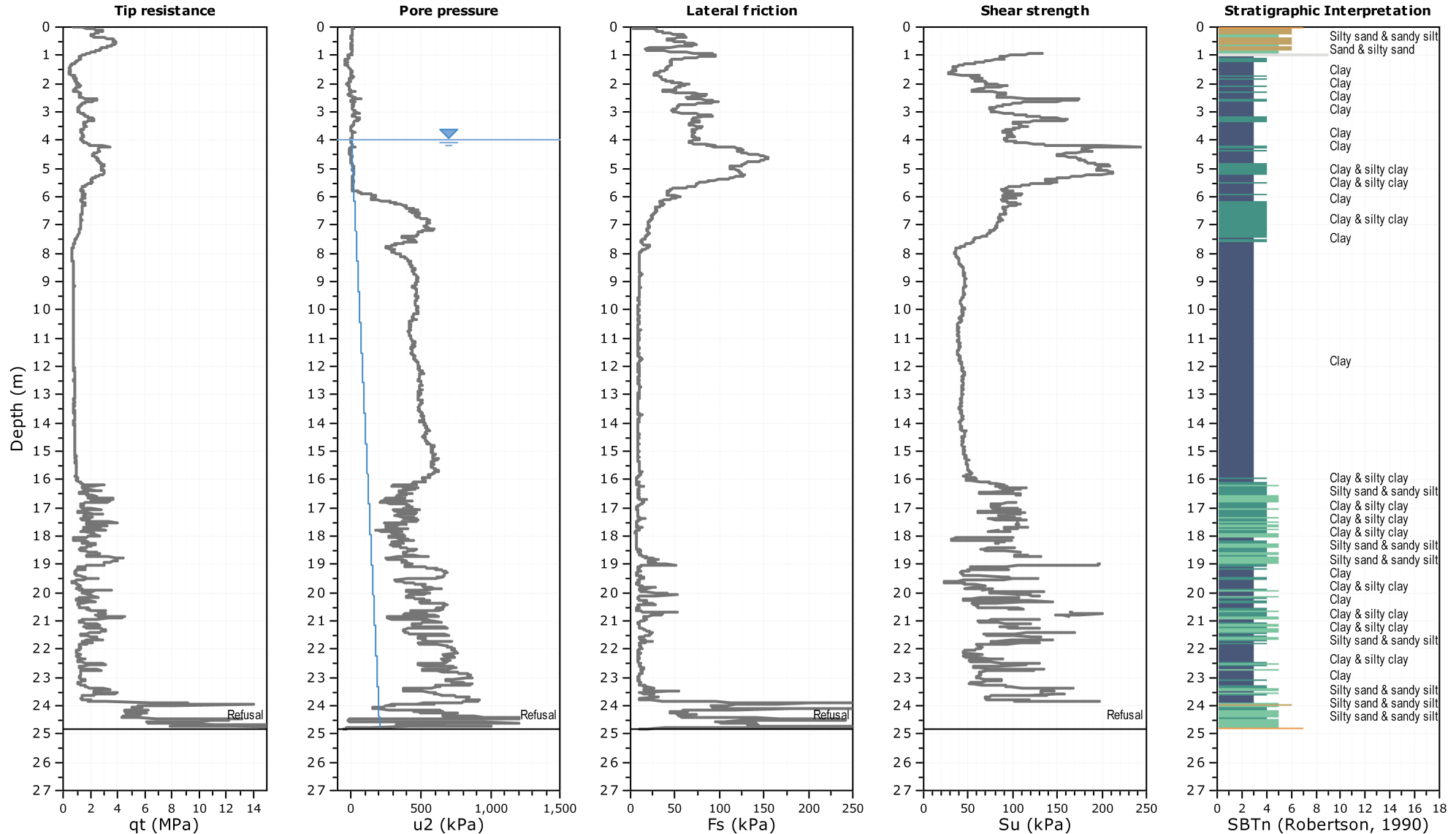
**Test Pit No. TP-52**  
**Proposed Sortation Facility**  
Leikin Drive and Merivale Road Intersection, Nepean, Ontario





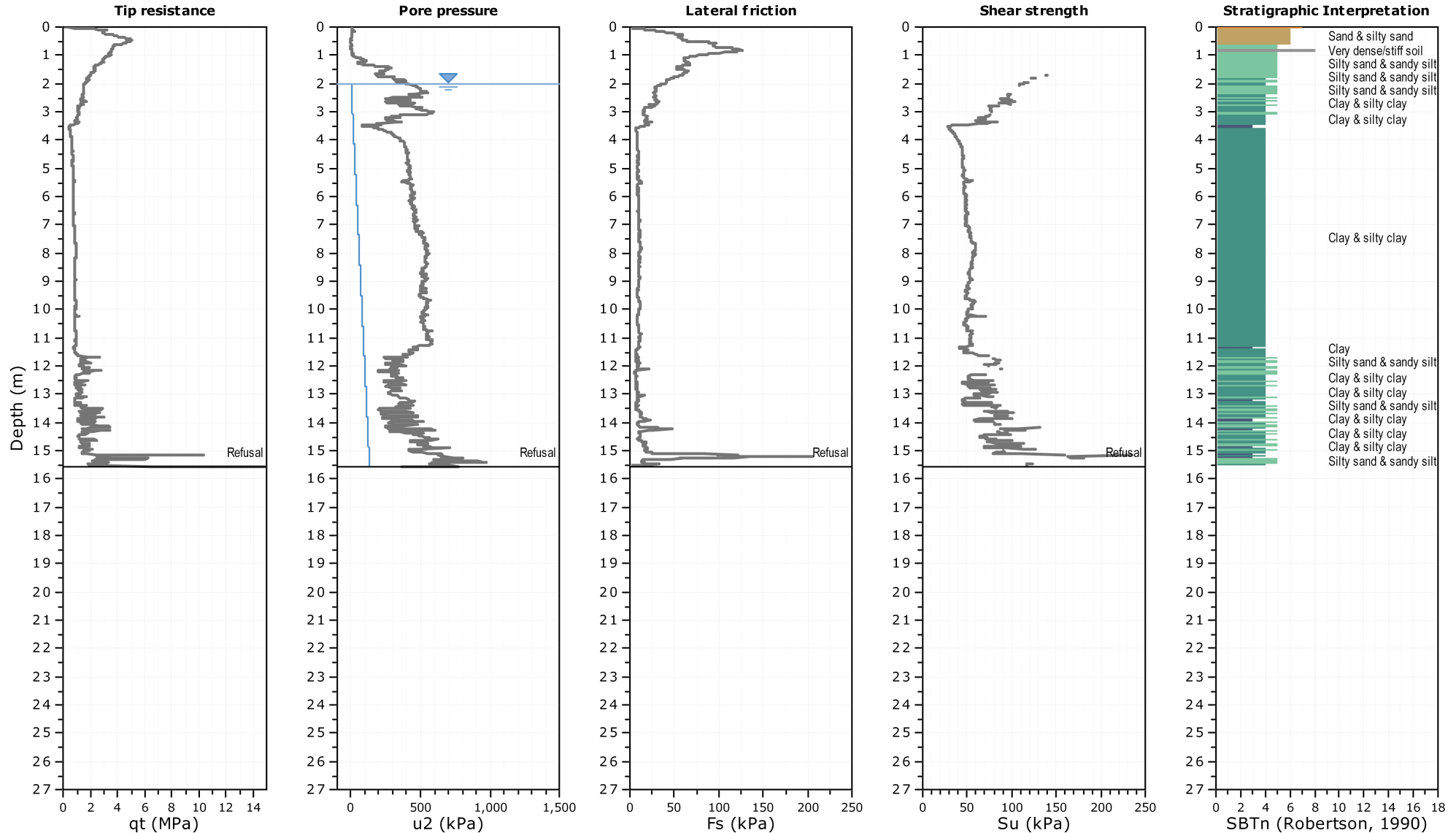


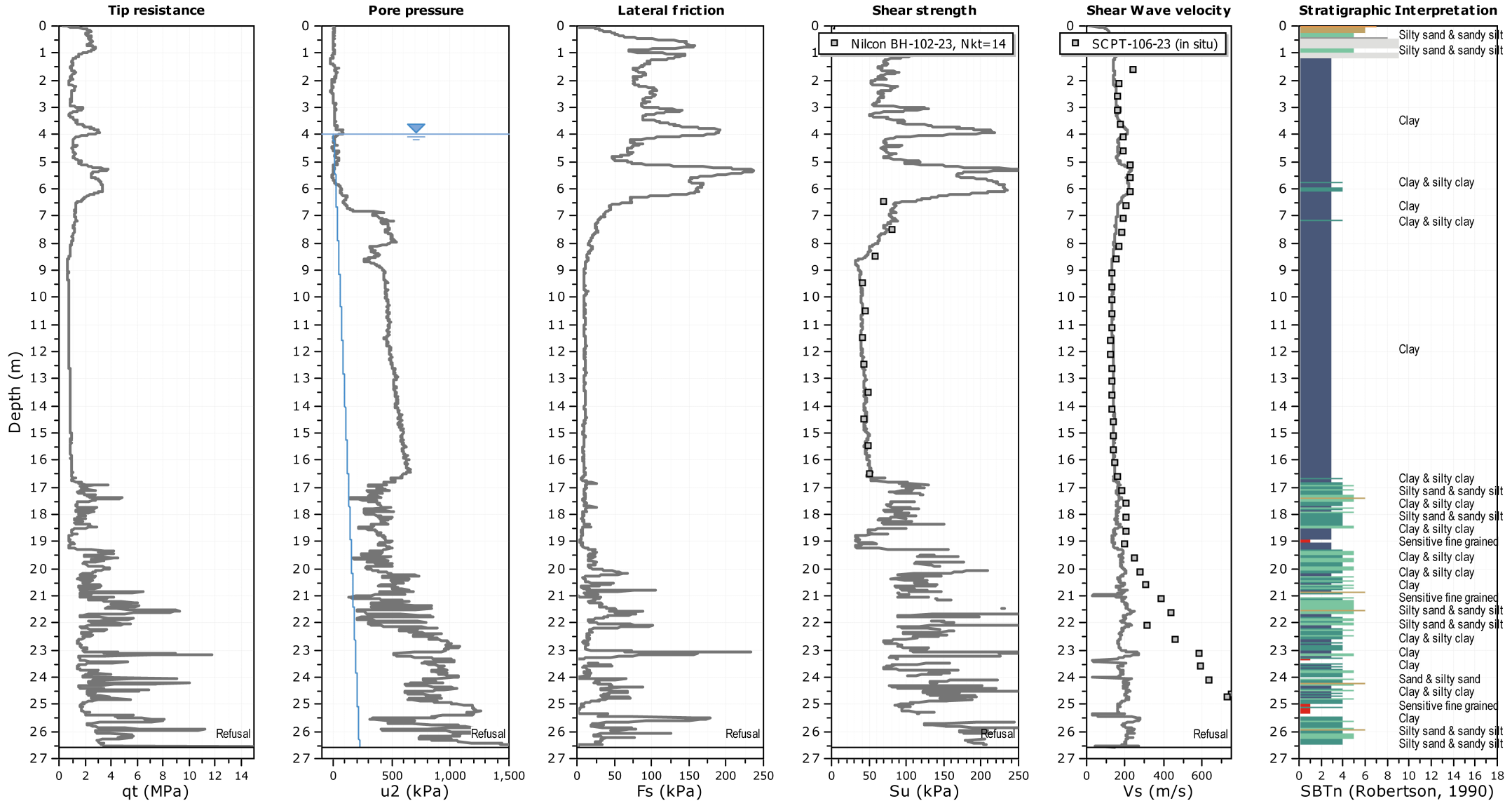






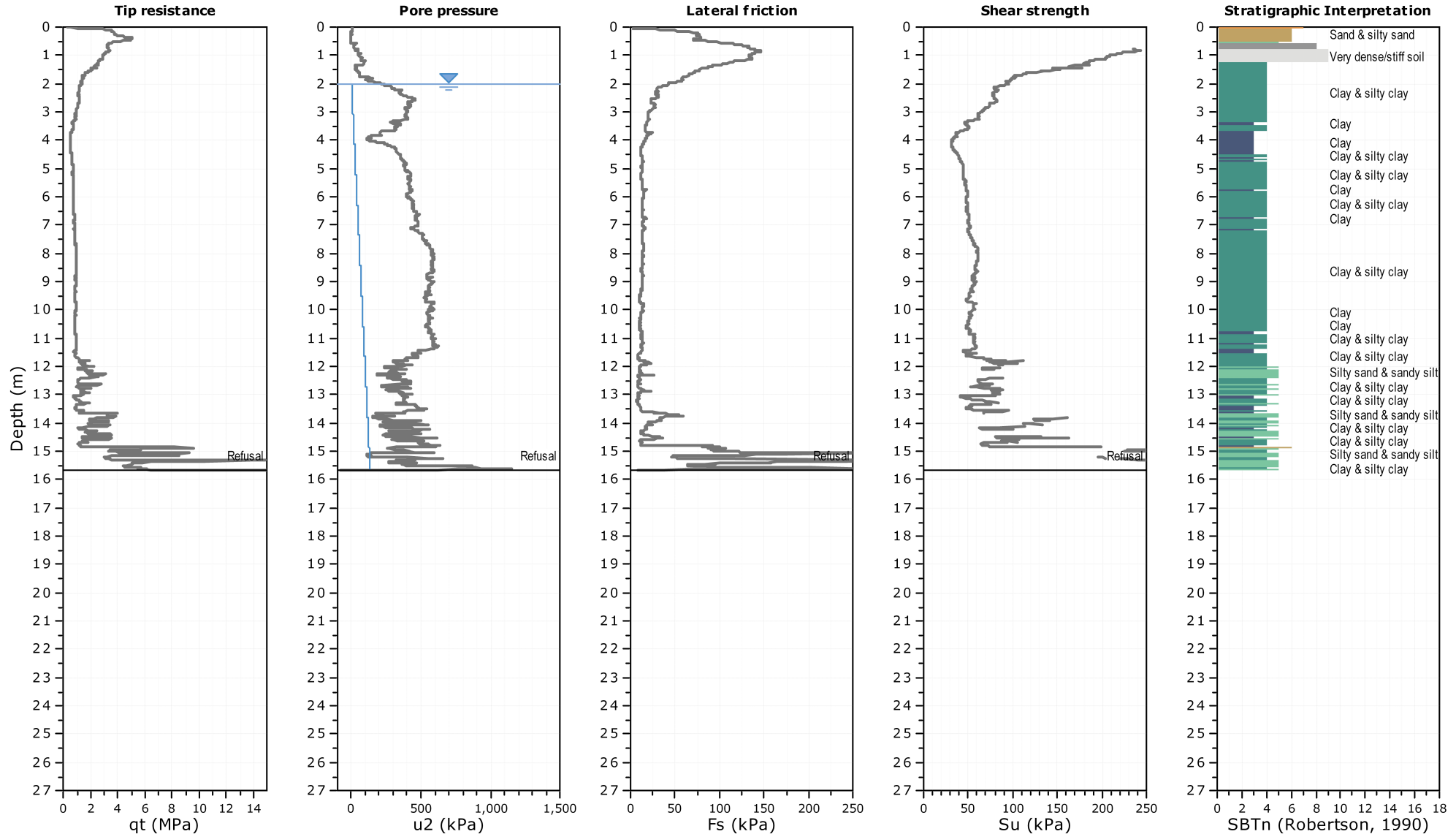
**Project: Proposed Distribution Center**  
**Location: Bill Leatham Drive, Ottawa, Ontario**

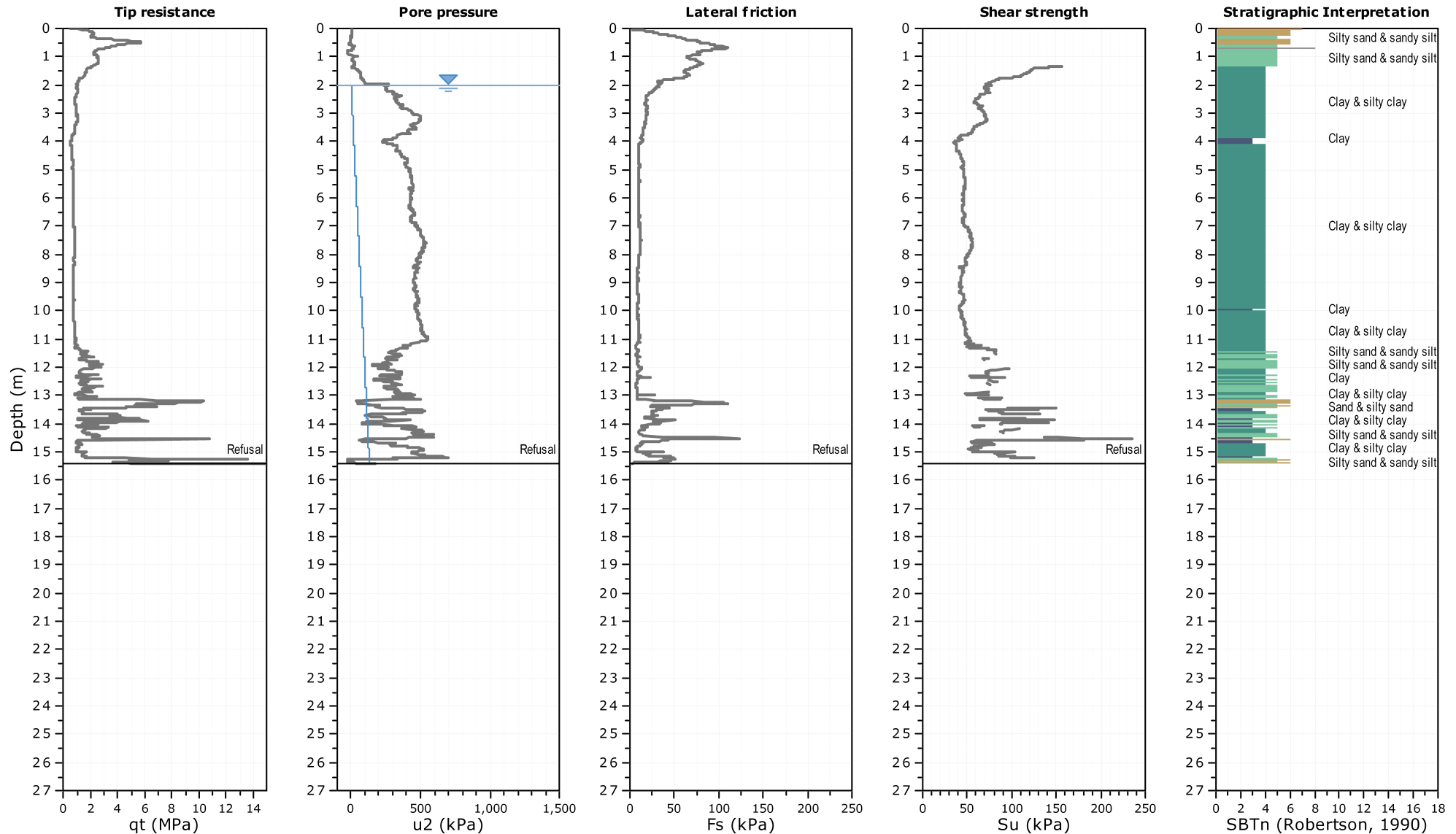




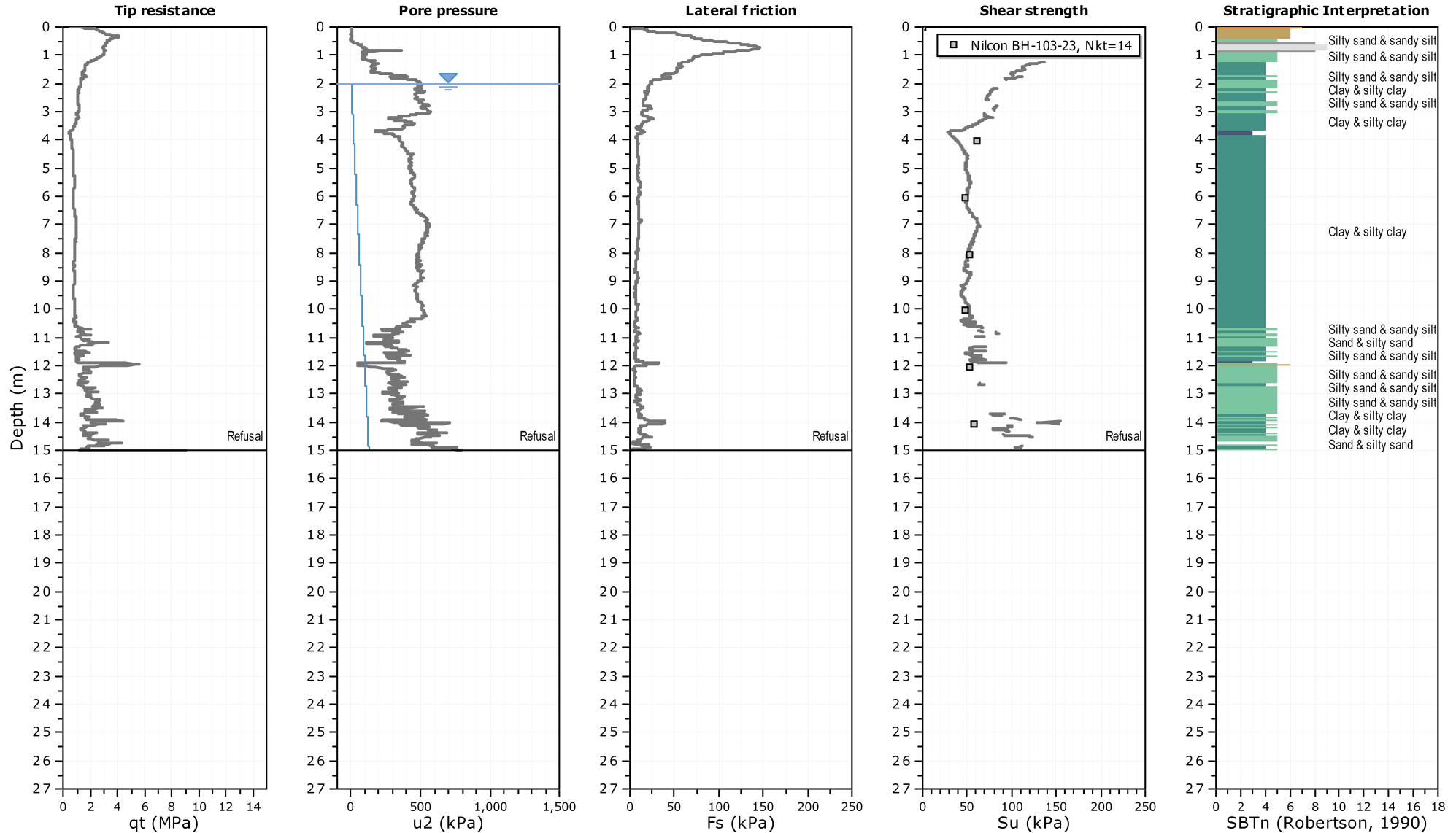


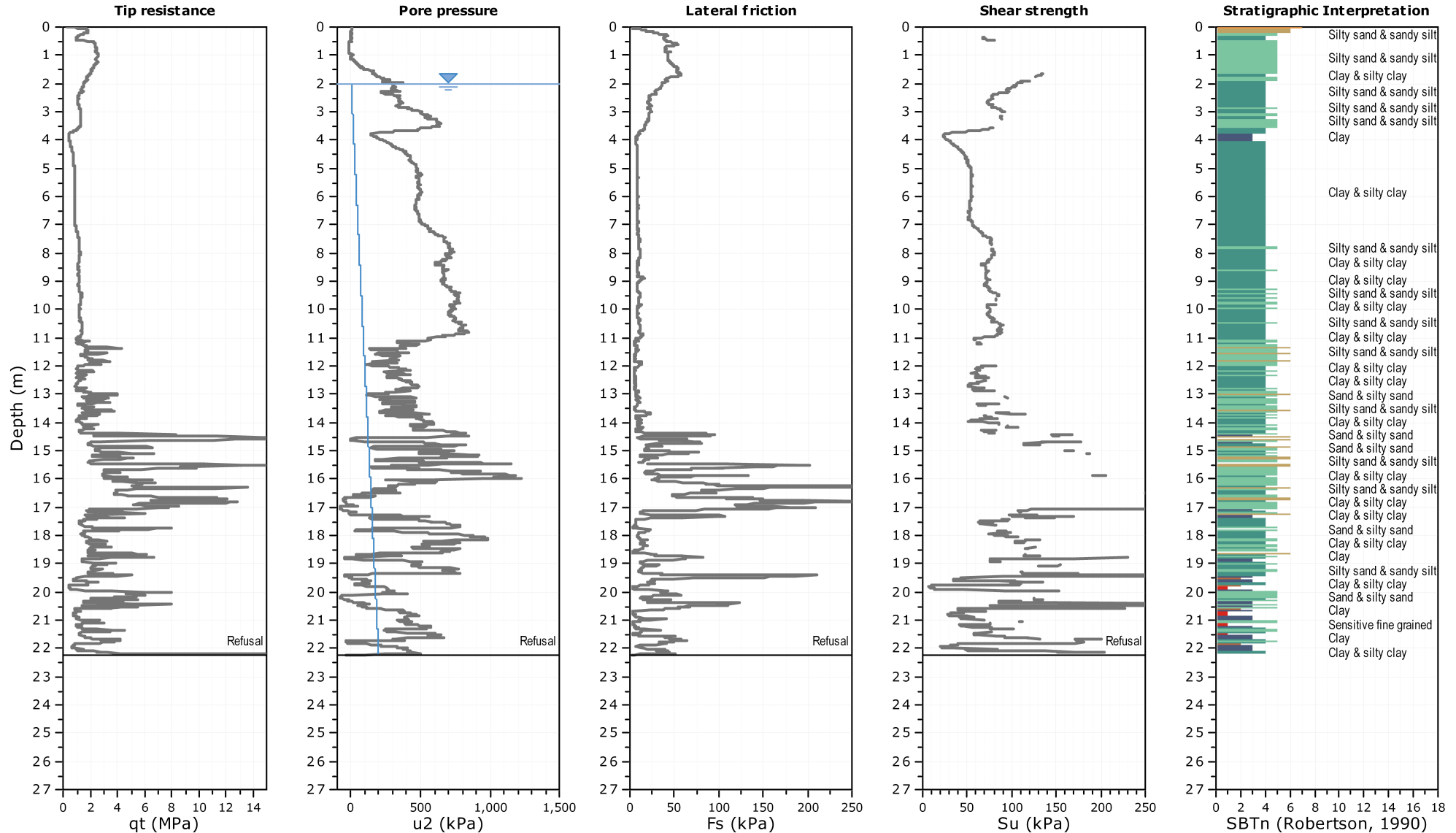
**Project: Proposed Distribution Center**  
**Location: Bill Leathem Drive, Ottawa, Ontario**













11227097-A1

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Interpreted by Marc-Andre Richard, ing. jr

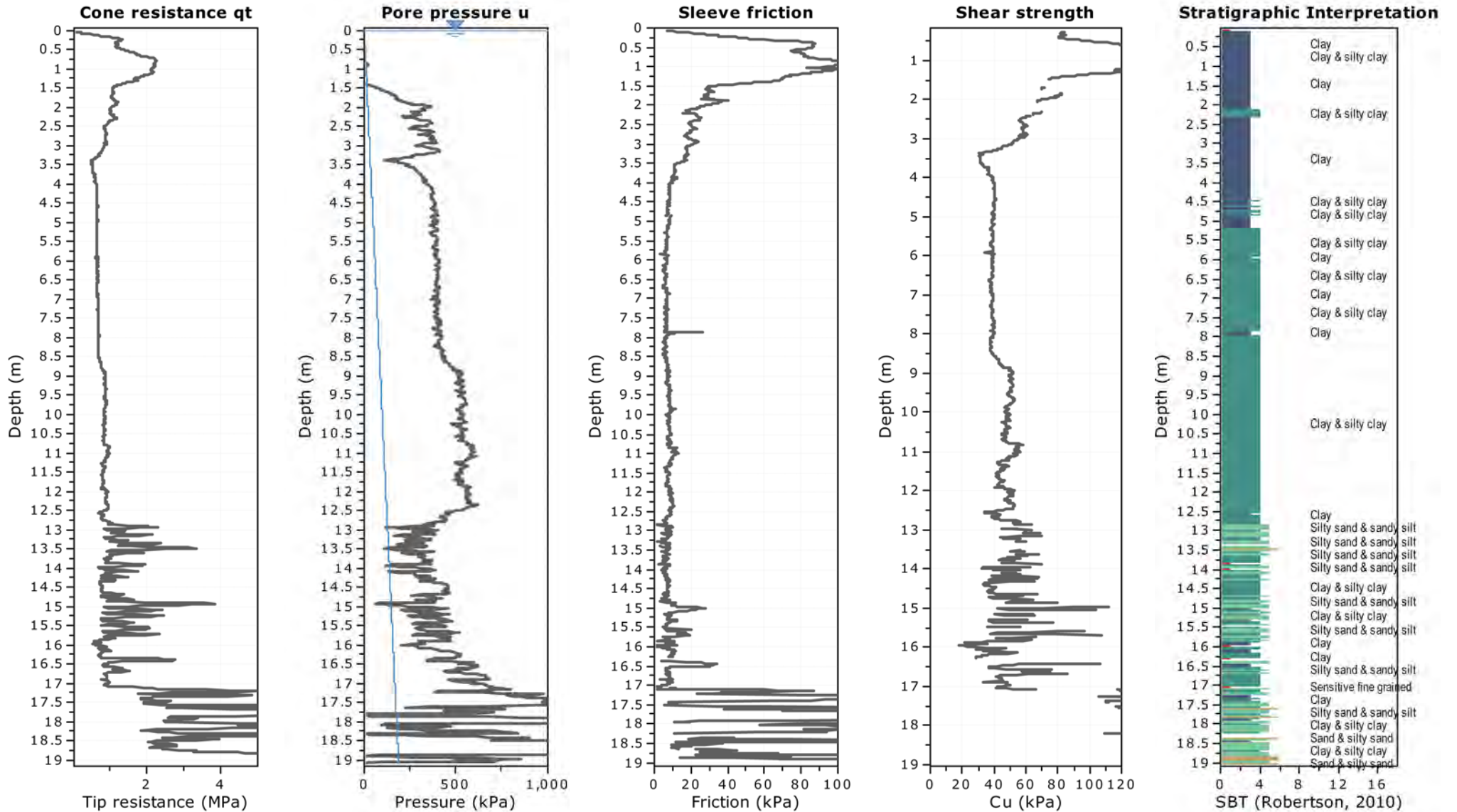
Verified by Kamel Hamouche, ing. Ph. D.

Project: Geotechnical Investigation - Proposed Sortation Facility

Location: Leikin Drive and Merival Road Intersection, Nepean, Ontario

CPT-01

Total depth: 19.08 m





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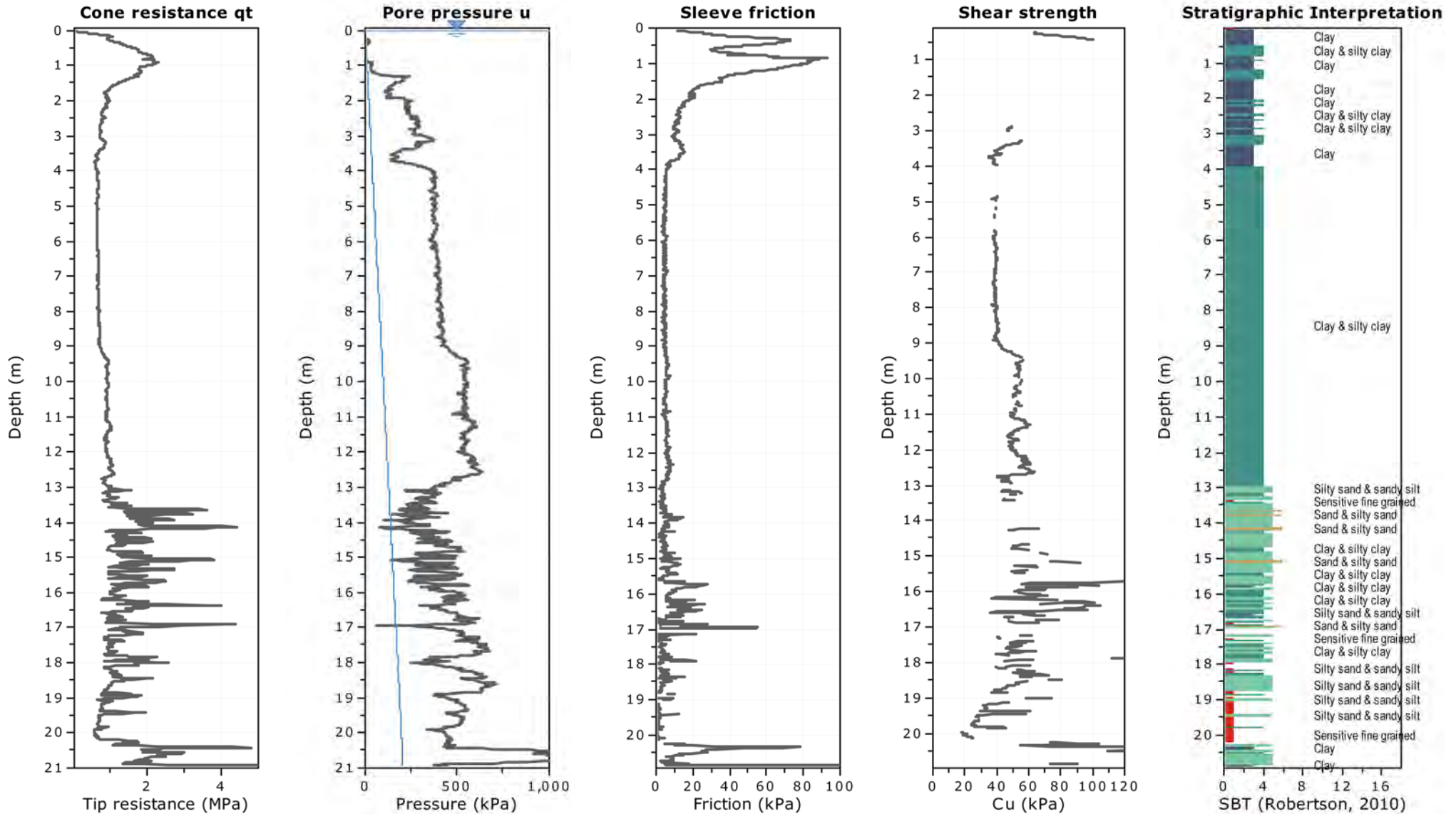
Verified by Kamel Hamouche, ing. Ph. D.

Project: Geotechnical Investigation - Proposed Sortation Facility

Location: Leikin Drive and Merival Road Intersection, Nepean, Ontario

CPT-02

Total depth: 20.92 m





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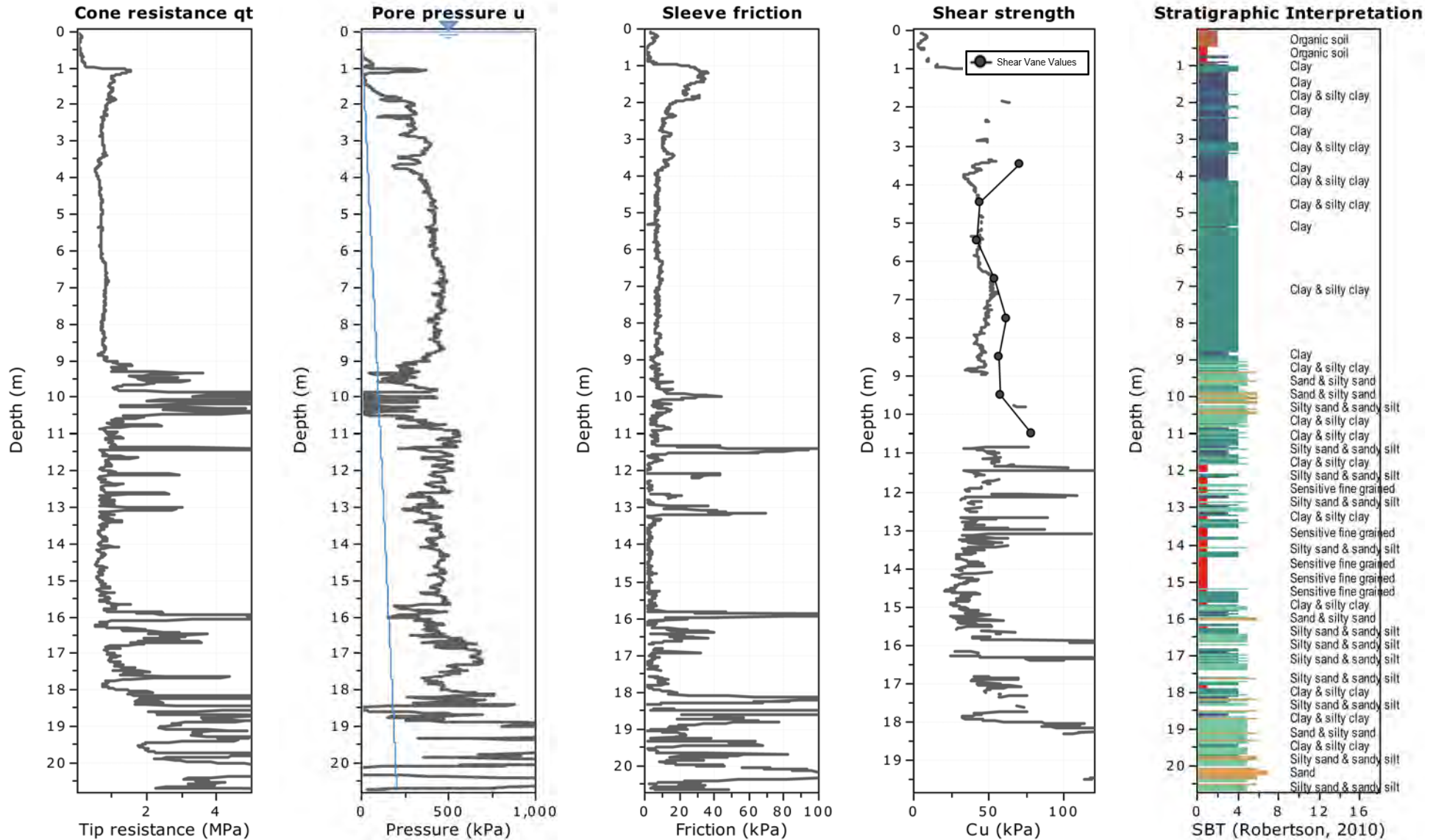
Verified by Kamel Hamouche, ing. Ph. D.

Project: Geotechnical Investigation - Proposed Sortation Facility

Location: Leikin Drive and Merival Road Intersection, Nepean, Ontario

CPT-03

Total depth: 20.72 m





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Interpreted by Marc-Andre Richard, ing. jr

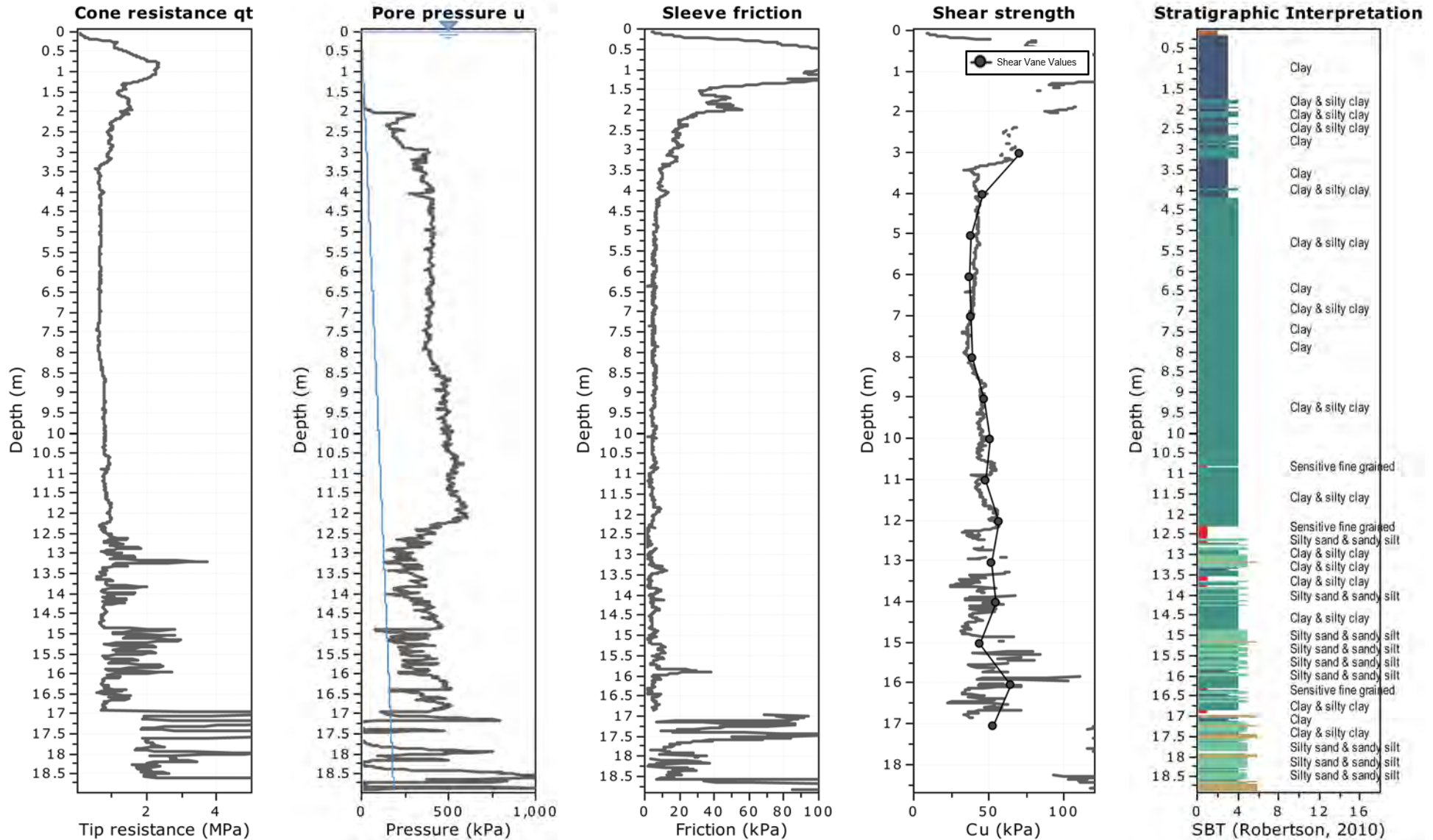
Verified by Kamel Hamouche, ing. Ph. D.

Project: Geotechnical Investigation - Proposed Sortation Facility

Location: Leikin Drive and Merival Road Intersection, Nepean, Ontario

CPT-04

Total depth: 18.89 m





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Interpreted by Marc-Andre Richard, ing. jr

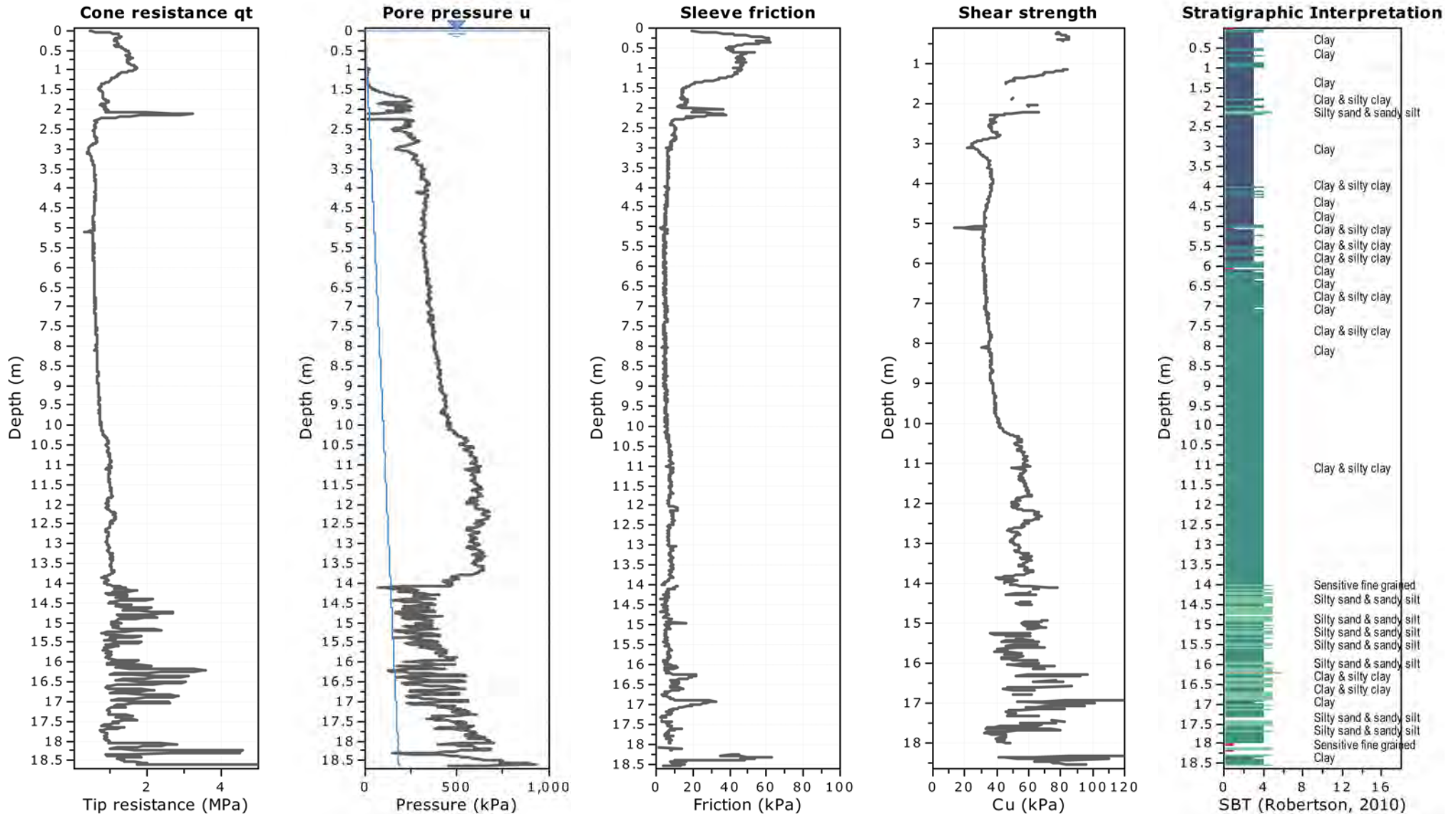
Verified by Kamel Hamouche, ing. Ph. D.

Project: Geotechnical Investigation - Proposed Sortation Facility

Location: Leikin Drive and Merival Road Intersection, Nepean, Ontario

CPT-05

Total depth: 18.63 m





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Interpreted by Marc-Andre Richard, ing. jr

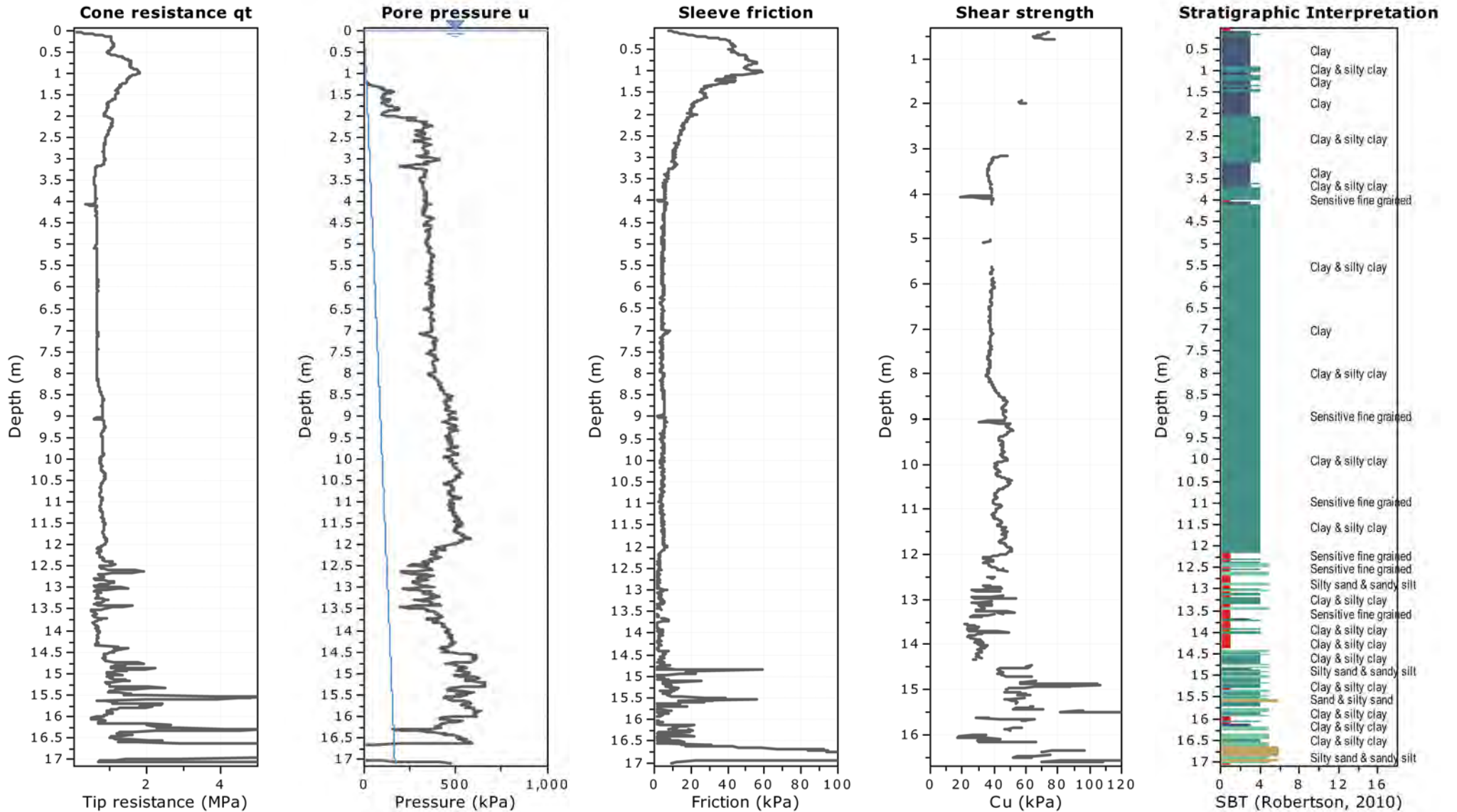
Verified by Kamel Hamouche, ing. Ph. D.

Project: Geotechnical Investigation - Proposed Sortation Facility

Location: Leikin Drive and Merival Road Intersection, Nepean, Ontario

CPT-06

Total depth: 17.10 m







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Interpreted by Marc-Andre Richard, ing. jr

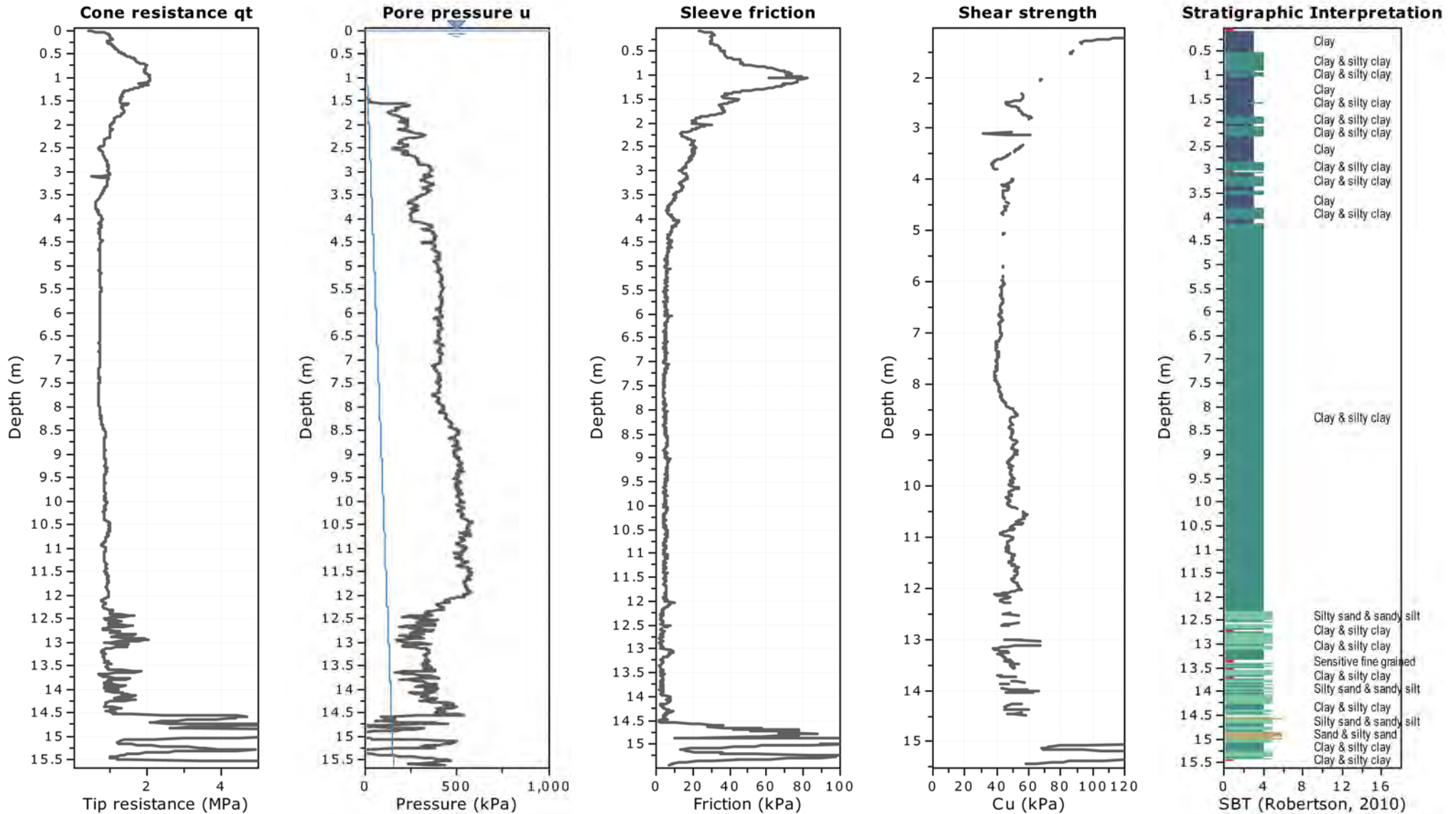
Verified by Kamel Hamouche, ing. Ph. D.

Project: Geotechnical Investigation - Proposed Sortation Facility

Location: Leikin Drive and Merival Road Intersection, Nepean, Ontario

CPT-07

Total depth: 15.62 m





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Interpreted by Marc-Andre Richard, ing. jr

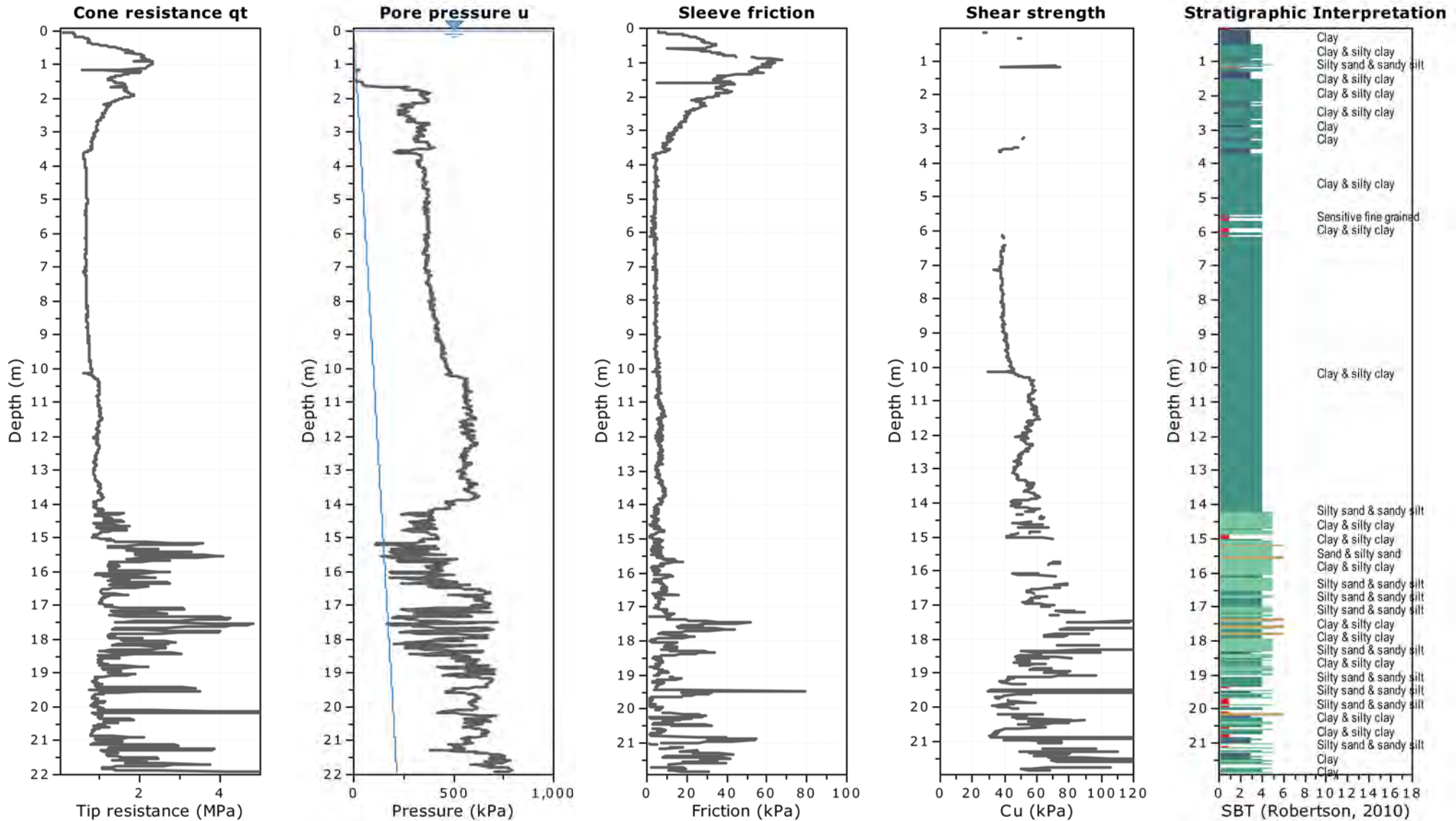
Verified by Kamel Hamouche, ing. Ph. D.

Project: Geotechnical Investigation - Proposed Sortation Facility

Location: Leikin Drive and Merival Road Intersection, Nepean, Ontario

CPT-08

Total depth: 21.93 m





11227097-A1

Performed by Stratum CPT

Interpreted by Marc-Andre Richard, ing. jr

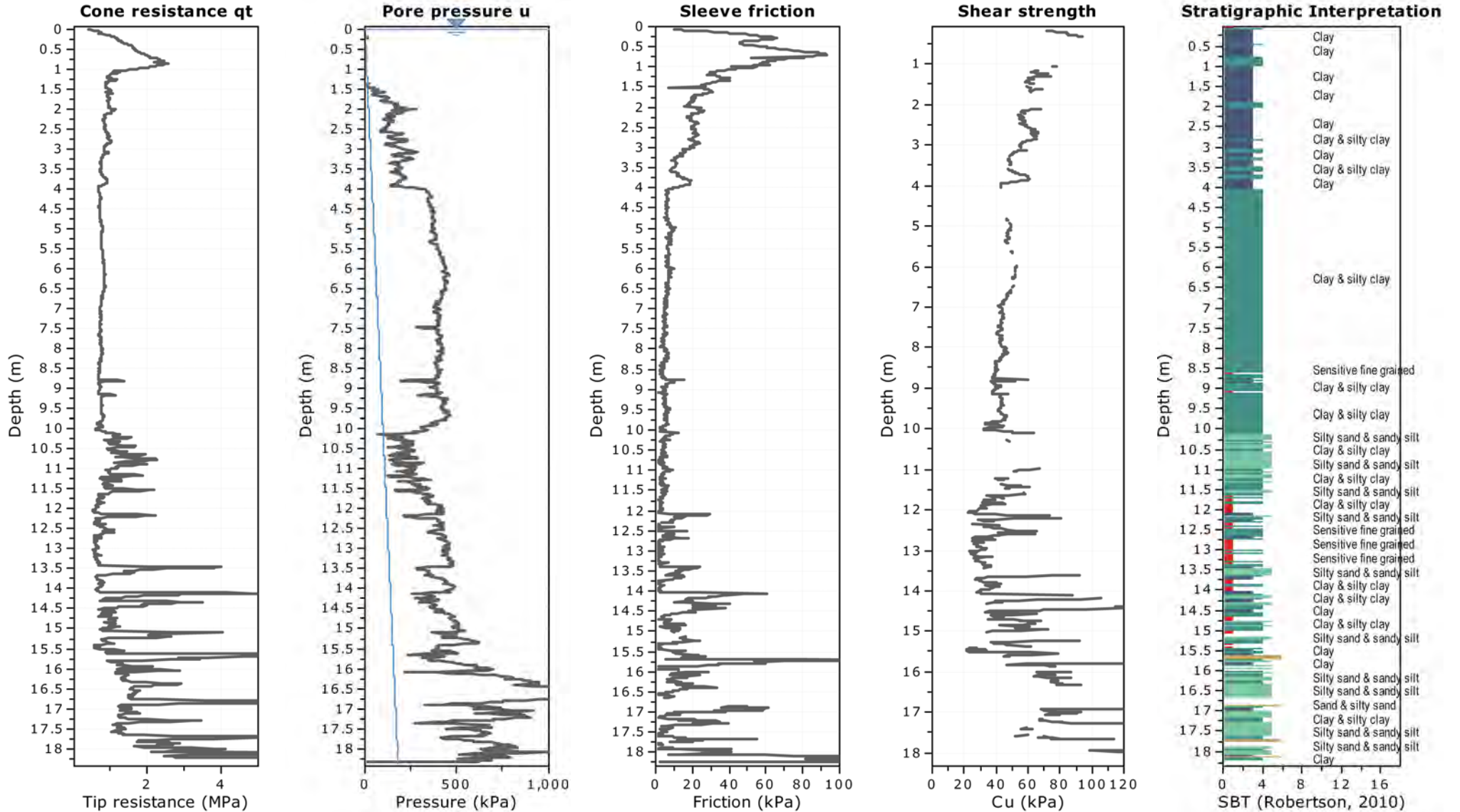
Verified by Kamel Hamouche, ing. Ph. D.

Project: Geotechnical Investigation - Proposed Sortation Facility

Location: Leikin Drive and Merival Road Intersection, Nepean, Ontario

CPT-14

Total depth: 18.37 m





11227097-A1

Performed by Stratum CPT

Interpreted by Marc-Andre Richard, ing. jr

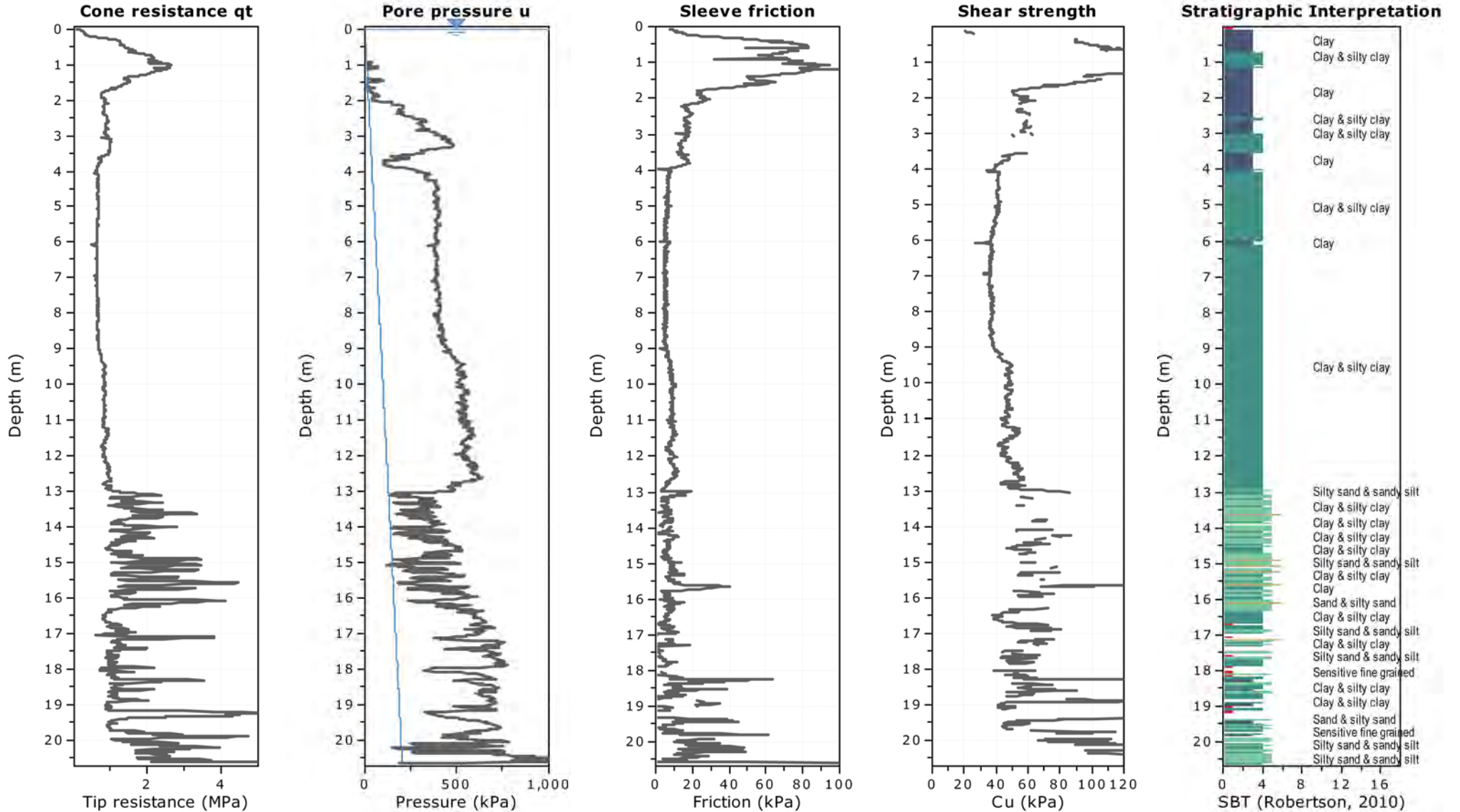
Verified by Kamel Hamouche, ing. Ph. D.

Project: Geotechnical Investigation - Proposed Sortation Facility

Location: Leikin Drive and Merival Road Intersection, Nepean, Ontario

CPT-16

Total depth: 20.66 m





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Performed by Stratum CPT

Interpreted by Marc-Andre Richard, ing. jr

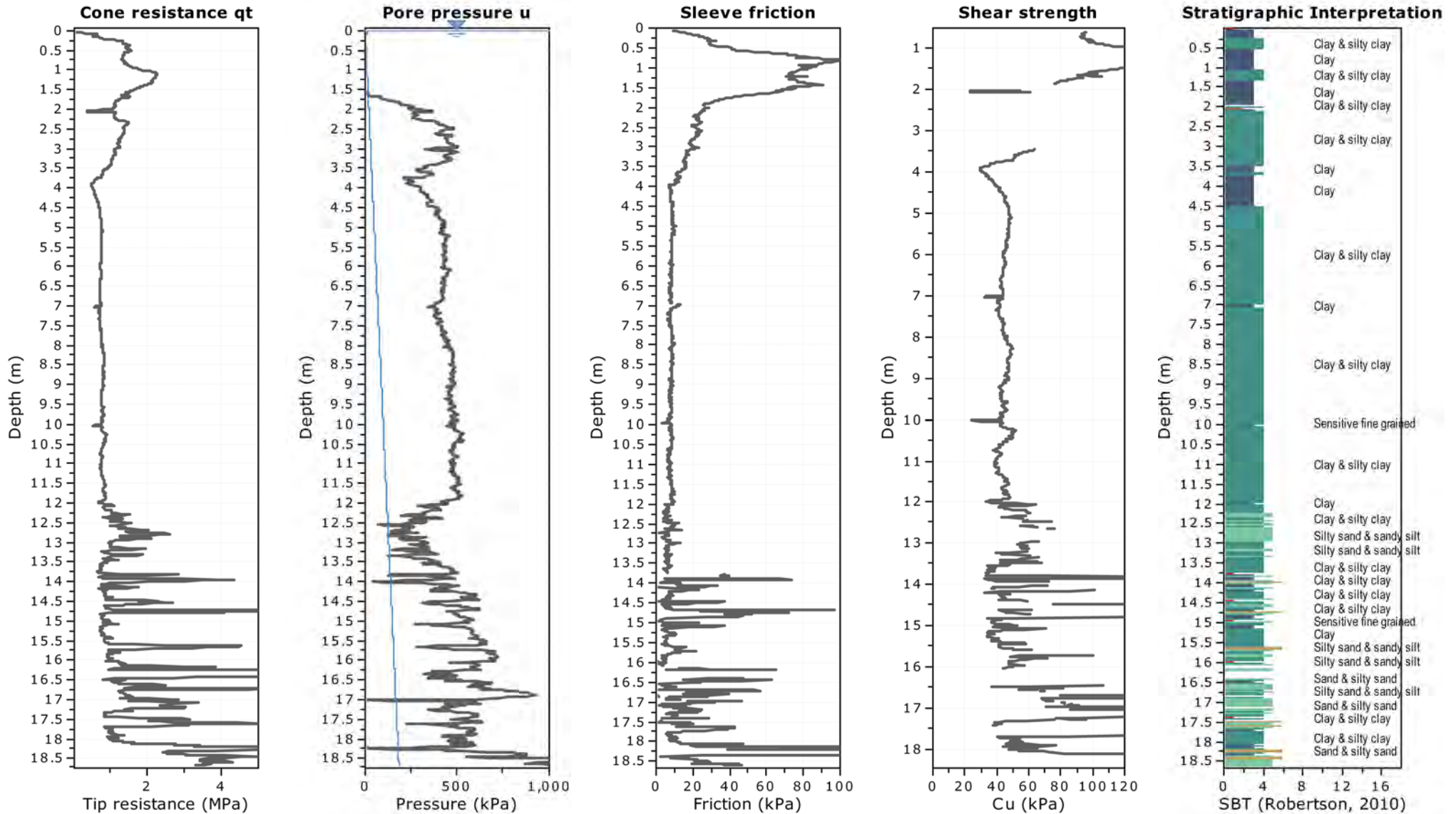
Verified by Kamel Hamouche, ing. Ph. D.

Project: Geotechnical Investigation - Proposed Sortation Facility

Location: Leikin Drive and Merival Road Intersection, Nepean, Ontario

CPT-18

Total depth: 18.66 m







# PLASTICITY CHART

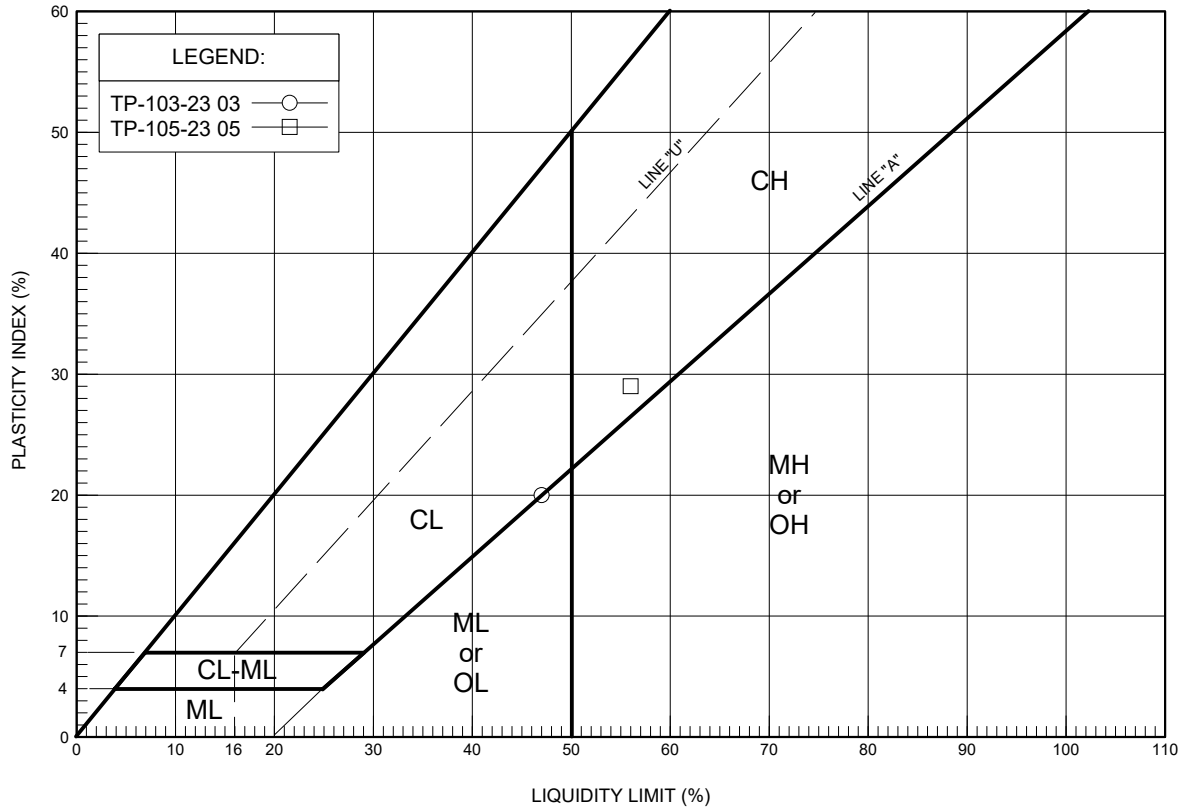
Client: **Medusa Limited Partnership**

Reference No.: 12615684-A1

Project: **Geotechnical Investigation - Proposed Distribution Center**

Location: **Bill Leatham Drive, Ottawa, Ontario**

## PLASTICITY CHART (ASTM D-2487 STANDARD)



### RESULTS INTERPRETATION AND WATER CONTENT

LEGEND	SOUNDING	SPL.	DEPTH (m)	DESCRIPTION	W	LL	PL	PI	LI	USCS
○	TP-103-23	03	0.80 - 1.80	Fill	22.0	47.0	27.0	20.0	-0.3	CL
□	TP-105-23	05	3.40 - 4.50	Fill	28.0	56.0	27.0	29.0	0.0	CH

Prepared by: Aman Azizi	Date : 2023-08-01	Verified by: Mark Gamboz	Date : 2023-08-01
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# PLASTICITY CHART

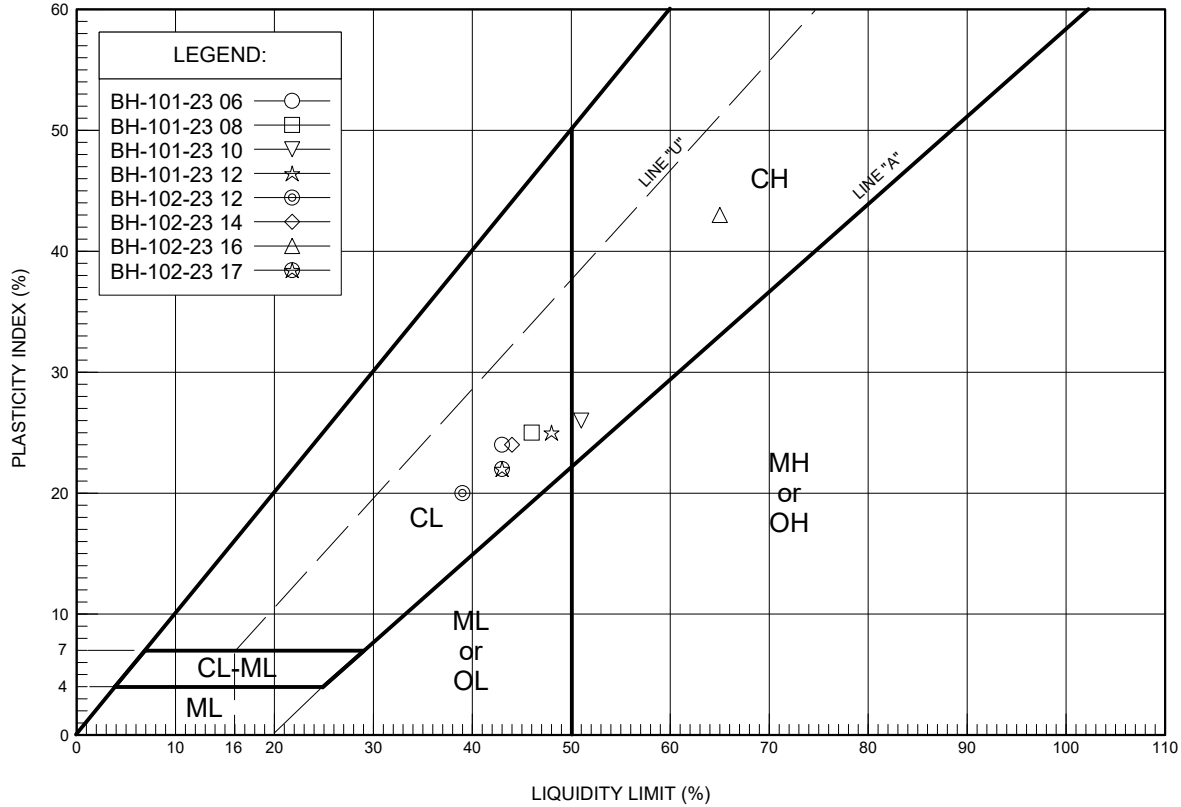
Client: **Medusa Limited Partnership**

Reference No.: 12615684-A1

Project: **Geotechnical Investigation - Proposed Distribution Center**

Location: **Bill Leatham Drive, Ottawa, Ontario**

## PLASTICITY CHART (ASTM D-2487 STANDARD)



### RESULTS INTERPRETATION AND WATER CONTENT

LEGEND	SOUNDING	SPL.	DEPTH (m)	DESCRIPTION	W	LL	PL	PI	LI	USCS
○	BH-101-23	06	3.05 - 3.66	Clayey Silt to Silty Clay Deposit	33.0	43.0	19.0	24.0	0.6	CL
□	BH-101-23	08	4.57 - 5.18	Clayey Silt to Silty Clay Deposit	50.0	46.0	21.0	25.0	1.2	CL
▽	BH-101-23	10	6.09 - 6.70	Clayey Silt to Silty Clay Deposit	62.0	51.0	25.0	26.0	1.4	CH
☆	BH-101-23	12	7.61 - 8.22	Clayey Silt to Silty Clay Deposit	63.0	48.0	23.0	25.0	1.6	CL
⊙	BH-102-23	12	7.62 - 8.23	Clayey Silt to Silty Clay Deposit	33.0	39.0	19.0	20.0	0.7	CL
◇	BH-102-23	14	10.13 - 10.74	Clayey Silt to Silty Clay Deposit	52.0	44.0	20.0	24.0	1.3	CL
△	BH-102-23	16	13.17 - 13.78	Clayey Silt to Silty Clay Deposit	62.0	65.0	22.0	43.0	0.9	CH
⊗	BH-102-23	17	14.69 - 15.30	Clayey Silt to Silty Clay Deposit	51.0	43.0	21.0	22.0	1.4	CL

Prepared by: Aman Azizi

Date: 2023-08-01

Verified by: Mark Gamboz

Date: 2023-08-01





# PLASTICITY CHART

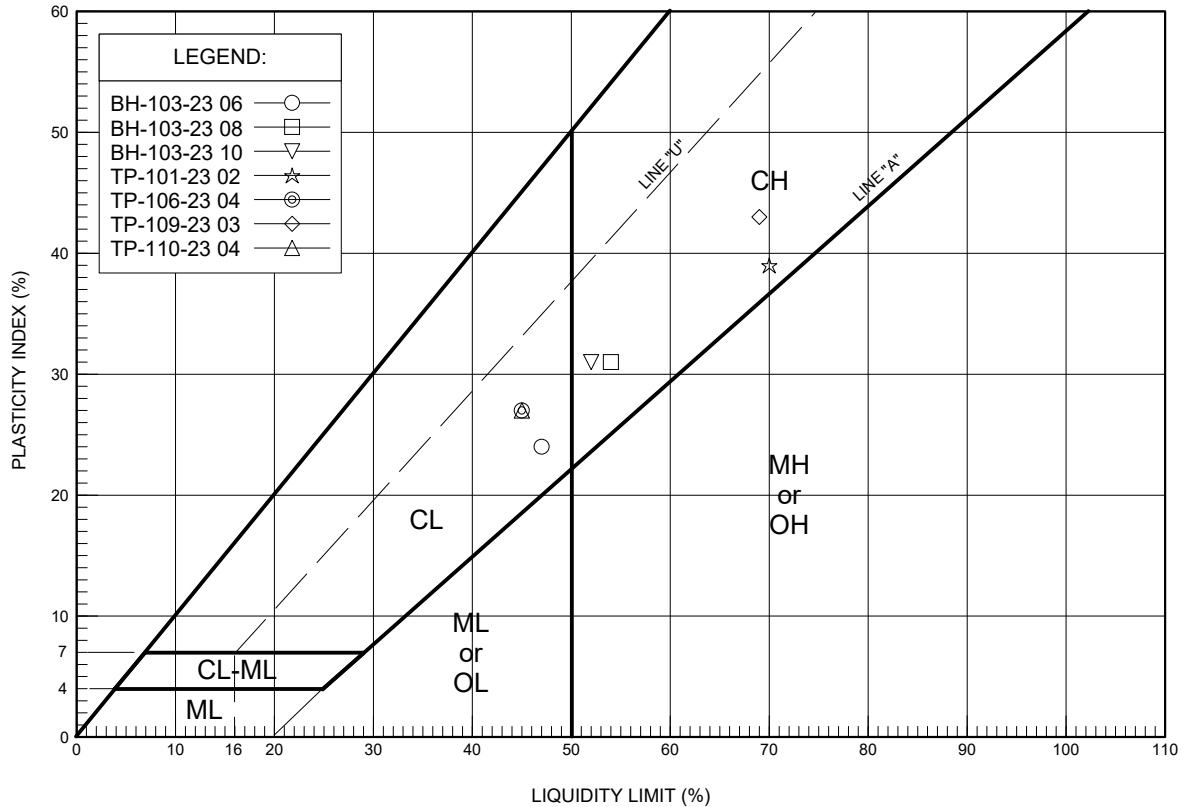
Client: **Medusa Limited Partnership**

Reference No.: 12615684-A1

Project: **Geotechnical Investigation - Proposed Distribution Center**

Location: **Bill Leathem Drive, Ottawa, Ontario**

## PLASTICITY CHART (ASTM D-2487 STANDARD)



### RESULTS INTERPRETATION AND WATER CONTENT

LEGEND	SOUNDING	SPL.	DEPTH (m)	DESCRIPTION	W	LL	PL	PI	LI	USCS
○	BH-103-23	06	4.56 - 5.17	Clayey Silt to Silty Clay Deposit	51.0	47.0	23.0	24.0	1.2	CL
□	BH-103-23	08	7.60 - 8.21	Clayey Silt to Silty Clay Deposit	58.0	54.0	23.0	31.0	1.1	CH
▽	BH-103-23	10	10.23 - 10.84	Clayey Silt to Silty Clay Deposit	58.0	52.0	21.0	31.0	1.2	CH
☆	TP-101-23	02	0.60 - 1.40	Clayey Silt to Silty Clay Deposit	33.0	70.0	31.0	39.0	0.1	CH
⊙	TP-106-23	04	2.00 - 3.00	Clayey Silt to Silty Clay Deposit	31.0	45.0	18.0	27.0	0.5	CL
◇	TP-109-23	03	0.90 - 1.80	Clayey Silt to Silty Clay Deposit	26.0	69.0	26.0	43.0	0.0	CH
△	TP-110-23	04	2.00 - 3.00	Clayey Silt to Silty Clay Deposit	36.0	45.0	18.0	27.0	0.7	CL

Prepared by: Aman Azizi

Date: 2023-08-01

Verified by: Mark Gamboz

Date: 2023-08-01



# CLASSIFICATION OF FINE GRAINED SOILS

REFERENCE No. : 11227097-A1

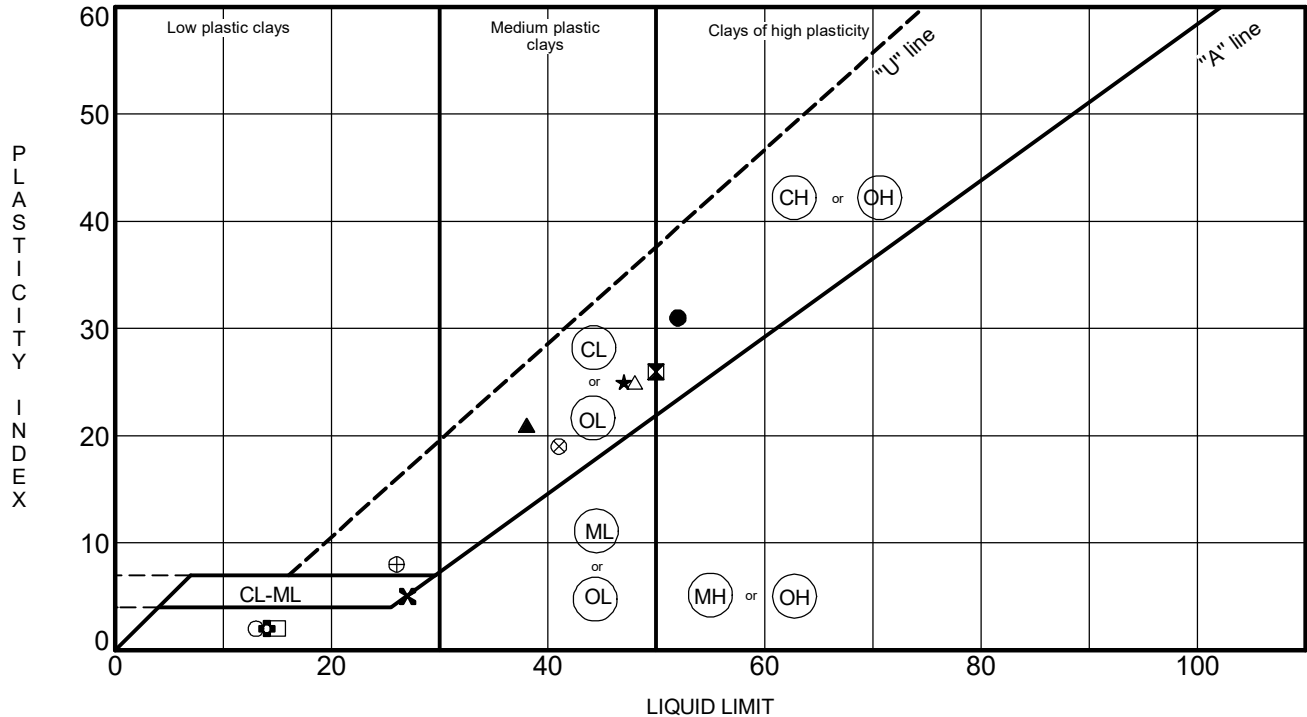
CLIENT : MEDUSA LP

LOCATION : LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO

PROJECT : PROPOSED SORTATION FACILITY

DATE : 5/11/2021

Plasticity Chart (ASTM D2487)



Bore No.	Sample	Depth	w	W <sub>L</sub>	W <sub>L-S</sub>	W <sub>P</sub>	I <sub>P</sub>	I <sub>L</sub>	C <sub>u</sub>	C <sub>ur</sub>	S <sub>T</sub>	Classification
●	BH-01	ST-5	45	52		21	31					CH
⊠	BH-01	SS-11	68	50		24	26					CH
▲	BH-02	SS-3	27	38		17	21					CL
★	BH-02	ST-7	54	47		22	25					CL
⊗	BH-02	SS-11	25	27		22	5					CL-ML
⊕	BH-02	SS-14	8	14		12	2					SM
○	BH-02	SS-19	8	13		11	2					SM
△	BH-03	SS-11	66	48		23	25					CL
⊗	BH-03	ST-13	58	41		22	19					CL
⊕	BH-03	SS-14	39	26		18	8					CL
□	BH-03	SS-18	9	15		13	2					SM

<b>Legend</b>	⊖ Inorganic clay of low plasticity	⊖ Inorganic silt	w : Water content (%)	I <sub>L</sub> : Liquidity index (%)
	⊖ Organic silt	⊖ Organic clay and organic silt	W <sub>L-S</sub> : Oven dried liquid limit (%)	C <sub>u</sub> : Intact undrained shear strength (kPa)
	⊖ Inorganic clay of high plasticity	⊖ Inorganic silt and very fine sand	W <sub>L</sub> : Liquid limit (%)	C <sub>ur</sub> : Remoulded undrained shear strength (kPa)
			W <sub>P</sub> : Plastic limit (%)	S <sub>T</sub> : Sensitivity
			I <sub>P</sub> : Plasticity index (%)	

Prepared by : Mark Gamboz, B.Sc. Geology

Verified by : Mark Gamboz, B.Sc. Geology



# CLASSIFICATION OF FINE GRAINED SOILS

REFERENCE No. : 11227097-A1

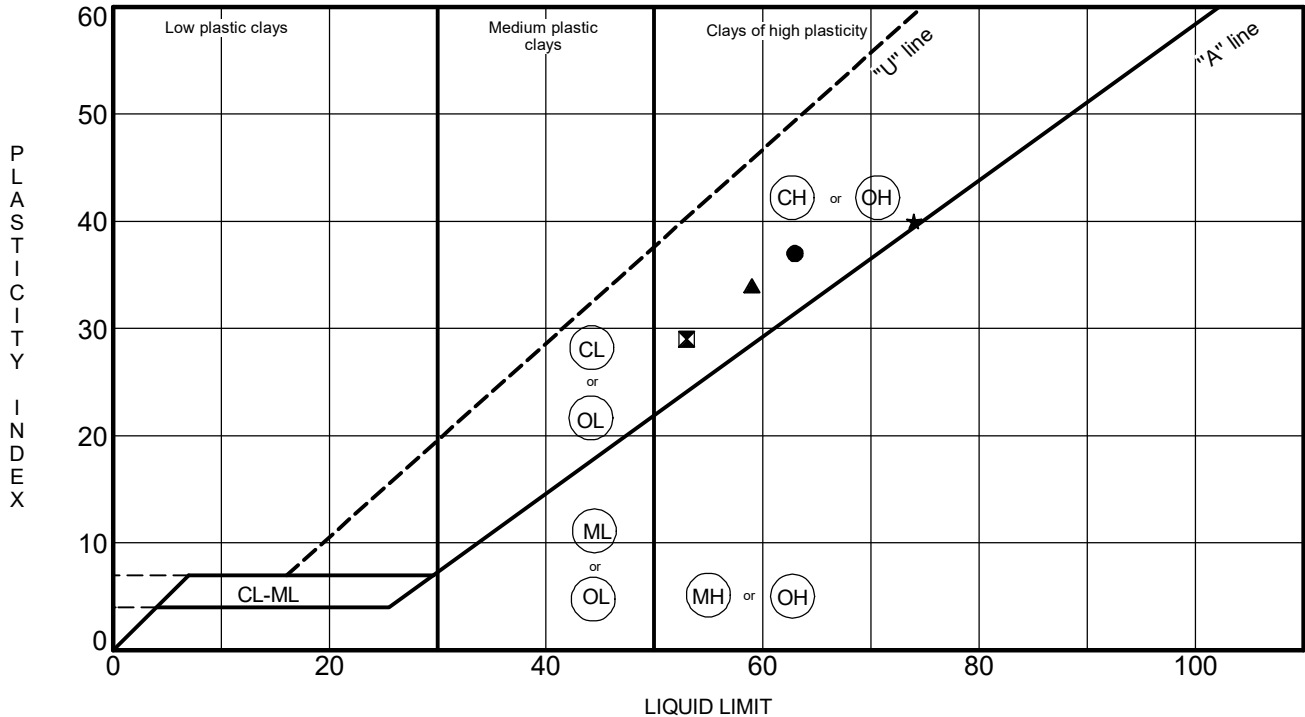
CLIENT : MEDUSA LP

LOCATION : LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO

PROJECT : PROPOSED SORTATION FACILITY

DATE : 5/31/2021

Plasticity Chart (ASTM D2487)



Bore No.	Sample	Depth	w	W <sub>L</sub>	W <sub>L-S</sub>	W <sub>P</sub>	I <sub>P</sub>	I <sub>L</sub>	C <sub>u</sub>	C <sub>ur</sub>	S <sub>T</sub>	Classification
● TP-01	GS-3	0.80	33	63		26	37					CH
⊠ TP-25	GS-3	0.70	37	53		24	29					CH
▲ TP-35	GS-3	0.70	30	59		25	34					CH
★ TP-44	GS-3	0.75	39	74		34	40					CH

<b>Legend</b>	Ⓞ (CL) Inorganic clay of low plasticity	Ⓞ (ML) Inorganic silt	w : Water content (%)	I <sub>L</sub> : Liquidity index (%)
	Ⓞ (OL) Organic silt	Ⓞ (OH) Organic clay and organic silt	W <sub>L-S</sub> : Oven dried liquid limit (%)	C <sub>i</sub> : Intact undrained shear strength (kPa)
	Ⓞ (CH) Inorganic clay of high plasticity	Ⓞ (MH) Inorganic silt and very fine sand	W <sub>L</sub> : Liquid limit (%)	C <sub>ur</sub> : Remoulded undrained shear strength (kPa)
			W <sub>P</sub> : Plastic limit (%)	S <sub>T</sub> : Sensitivity
			I <sub>P</sub> : Plasticity index (%)	

Prepared by : Mark Gamboz, B.Sc. Geology

Verified by : Mark Gamboz, B.Sc. Geology



# GRAIN SIZE ANALYSIS REPORT

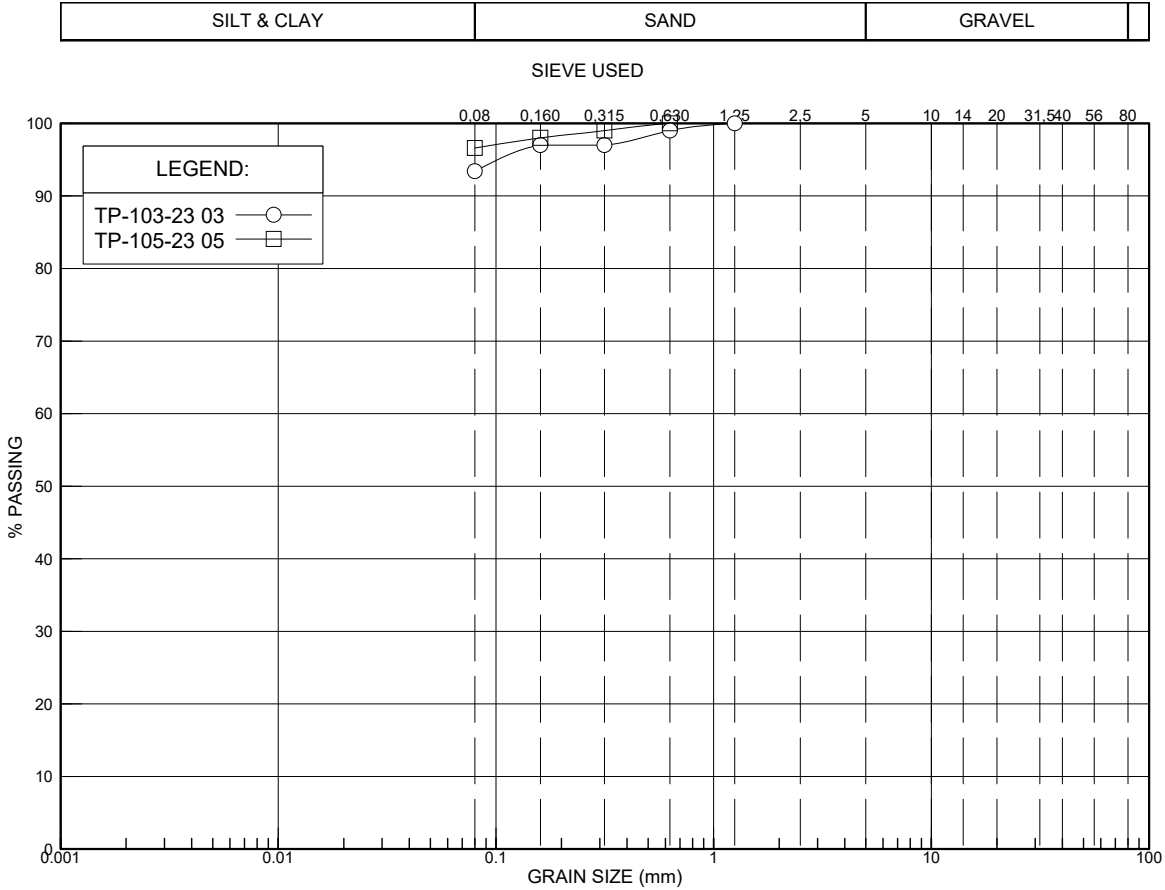
Client: **Medusa Limited Partnership**

Reference No.: 12615684-A1

Project: **Geotechnical Investigation - Proposed Distribution Center**

Location: **Bill Leathem Drive, Ottawa, Ontario**

## UNIFIED SOIL CLASSIFICATION



LEGEND	0.001 mm	0.01 mm	0.023 mm	0.051 mm	0.08 mm	0.16 mm	0.315 mm	0.630 mm	1.25 mm	2.5 mm	5 mm	10 mm	14 mm	20 mm	28 mm	31.5 mm
○	-	-	-	-	93.40	97.00	97.00	99.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
□	-	-	-	-	96.60	98.00	99.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00

### RESULTS INTERPRETATION AND WATER CONTENT

LEGEND	SOUNDING	SPL.	DEPTH (m)	DESCRIPTION	GRAVEL	SAND	SILT & CLAY	W	USCS
○	TP-103-23	03	0.80 - 1.80	Fill	0.0 %	6.6 %	93.4 %	22.0 %	CL
□	TP-105-23	05	3.40 - 4.50	Fill	0.0 %	3.4 %	96.6 %	28.0 %	CH

Prepared by: Aman Azizi

Date : 2023-08-01

Verified by: Mark Gamboz

Date : 2023-08-01



# GRAIN SIZE ANALYSIS REPORT

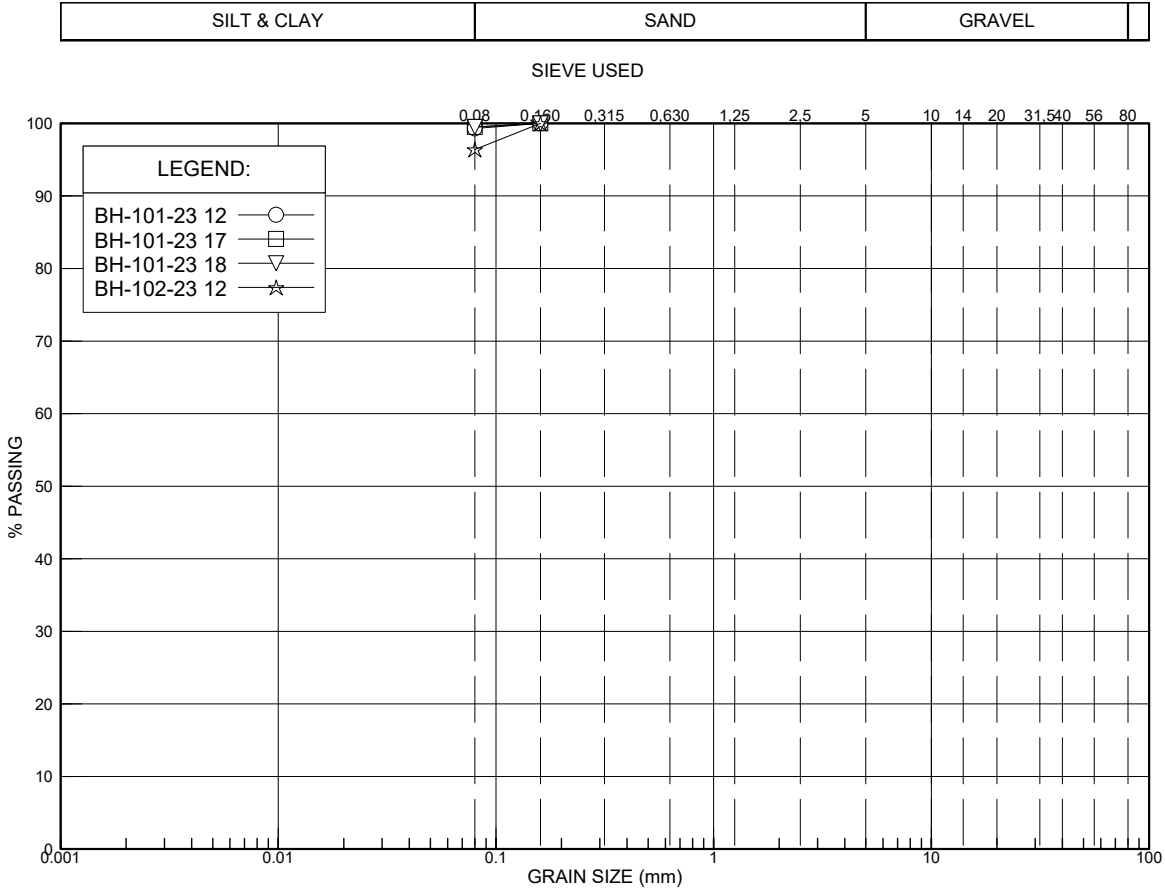
Client: **Medusa Limited Partnership**

Reference No.: 12615684-A1

Project: **Geotechnical Investigation - Proposed Distribution Center**

Location: **Bill Leatham Drive, Ottawa, Ontario**

## UNIFIED SOIL CLASSIFICATION



LEGEND	0.001 mm	0.01 mm	0.023 mm	0.051 mm	0.08 mm	0.16 mm	0.315 mm	0.630 mm	1.25 mm	2.5 mm	5 mm	10 mm	14 mm	20 mm	28 mm	31.5 mm
○	-	-	-	-	99.30	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
□	-	-	-	-	99.50	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
▽	-	-	-	-	99.50	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
☆	-	-	-	-	96.40	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00

### RESULTS INTERPRETATION AND WATER CONTENT

LEGEND	SOUNDING	SPL.	DEPTH (m)	DESCRIPTION	GRAVEL	SAND	SILT & CLAY	W	USCS
○	BH-101-23	12	7.61 - 8.22	Clayey Silt to Silty Clay Deposit	0.0 %	0.7 %	99.3 %	63.0 %	CL
□	BH-101-23	17	13.40 - 14.01	Clayey Silt to Silty Clay Deposit	0.0 %	0.5 %	99.5 %	-	-
▽	BH-101-23	18	14.92 - 15.53	Clayey Silt to Silty Clay Deposit	0.0 %	0.5 %	99.5 %	-	-
☆	BH-102-23	12	7.62 - 8.23	Clayey Silt to Silty Clay Deposit	0.0 %	3.6 %	96.4 %	33.0 %	CL

Prepared by: Aman Azizi

Date : 2023-08-01

Verified by: Mark Gamboz

Date : 2023-08-01



# HYDROMETER ANALYSIS REPORT

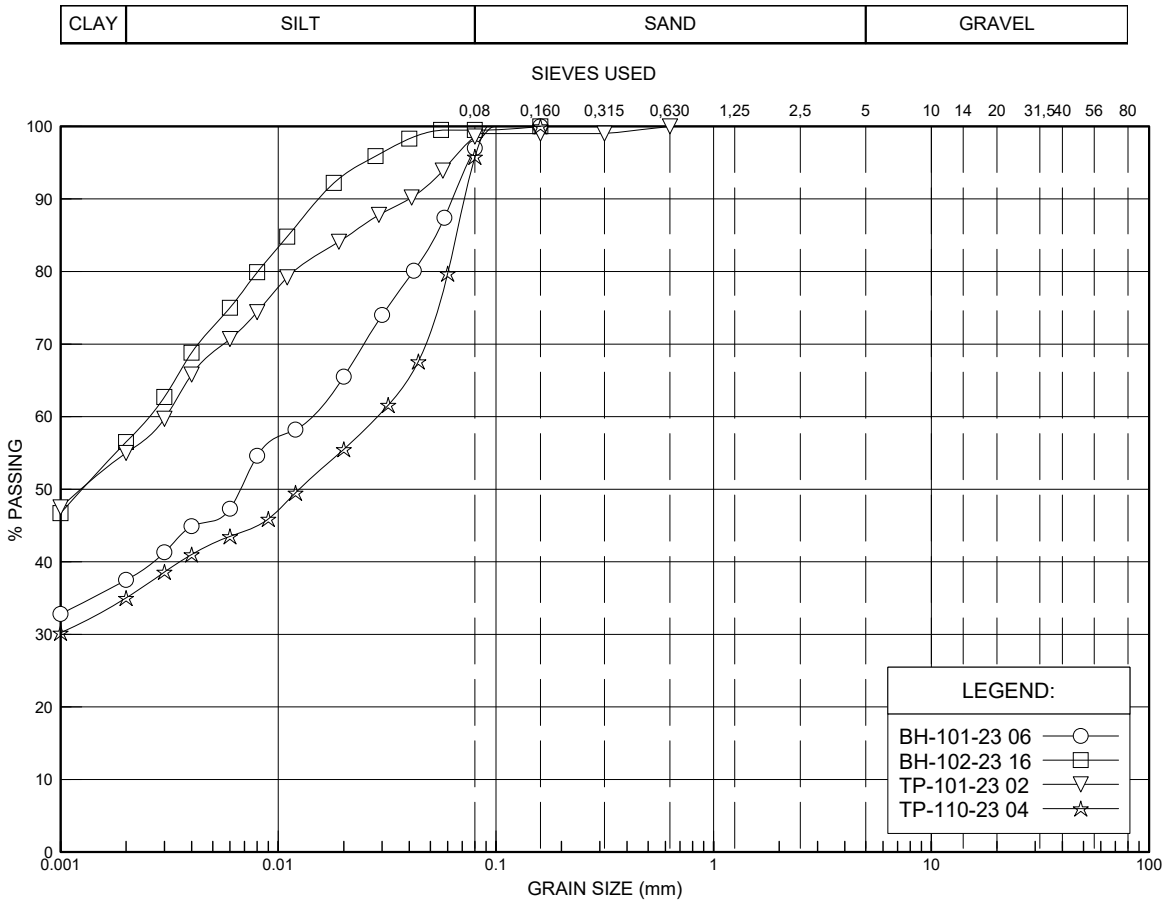
Client : **Medusa Limited Partnership**

Reference No.: 12615684-A1

Project : **Geotechnical Investigation - Proposed Distribution Center**

Location : **Bill Leathem Drive, Ottawa, Ontario**

## UNIFIED SOIL CLASSIFICATION



LEGEND	0.001 mm	0.01 mm	0.023 mm	0.051 mm	0.08 mm	0.16 mm	0.315 mm	0.630 mm	1.25 mm	2.5 mm	5 mm	10 mm	14 mm	20 mm	28 mm	31.5 mm
○	32.80	57.26	68.43	84.07	97.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
□	46.70	83.35	94.50	99.31	99.50	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
▽	47.50	77.86	85.81	92.43	98.59	99.01	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
☆	30.20	47.09	57.18	72.30	95.80	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00

### RESULTS INTERPRETATION AND WATER CONTENT

LEGEND	SOUNDING	SPL.	DEPTH (m)	DESCRIPTION	GRAVEL	SAND	SILT	CLAY	W	USCS
○	BH-101-23	06	3.05 - 3.66	Clayey Silt to Silty Clay Deposit	0.0 %	3.0 %	59.5 %	37.5 %	33.0 %	CL
□	BH-102-23	16	13.17 - 13.78	Clayey Silt to Silty Clay Deposit	0.0 %	0.5 %	43.0 %	56.5 %	62.0 %	CH
▽	TP-101-23	02	0.60 - 1.40	Clayey Silt to Silty Clay Deposit	0.0 %	1.4 %	43.6 %	55.0 %	33.0 %	CH
☆	TP-110-23	04	2.00 - 3.00	Clayey Silt to Silty Clay Deposit	0.0 %	4.2 %	60.8 %	35.0 %	36.0 %	CL

Prepared by: Aman Azizi

Date : 2023-08-01

Verified by: Mark Gamboz

Date : 2023-08-01

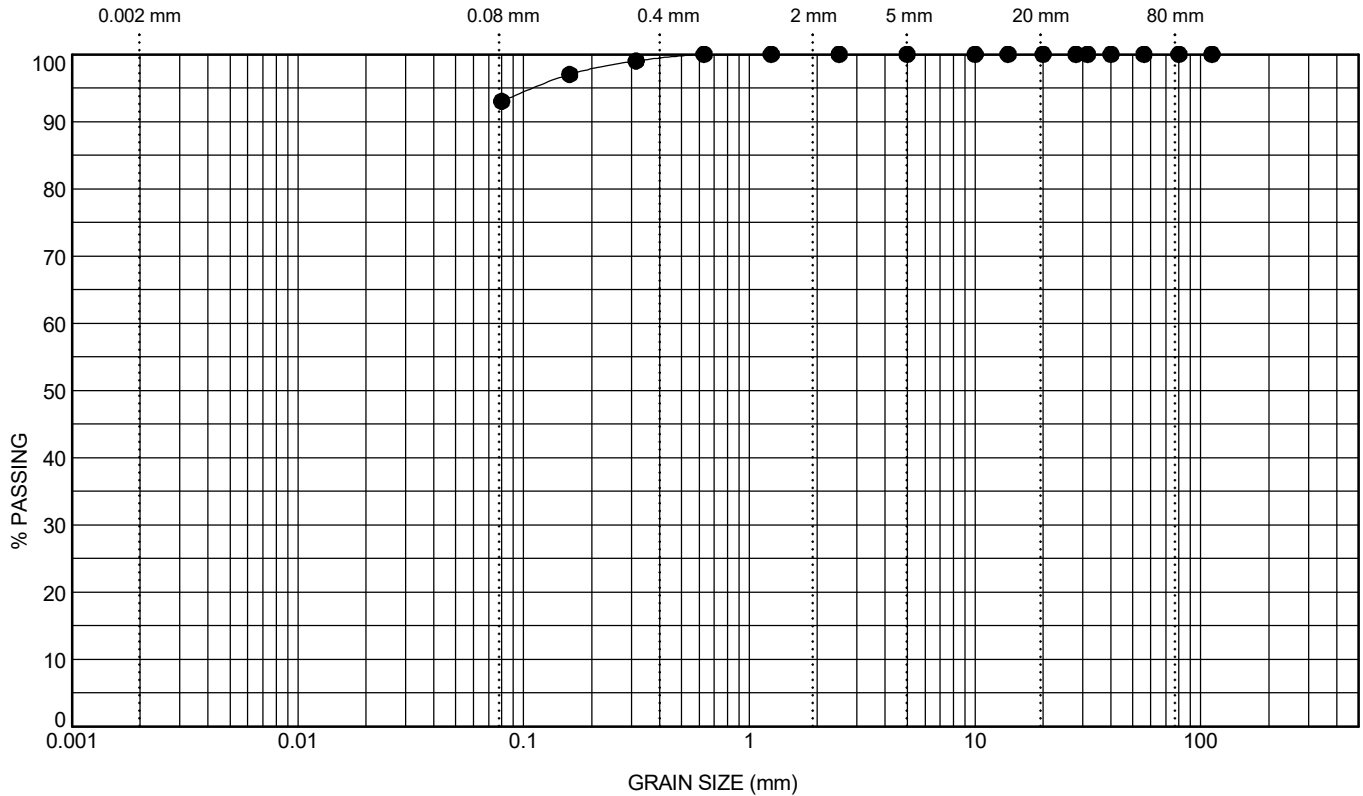


# GRAIN SIZE ANALYSIS REPORT

**CLIENT:** MEDUSA LP  
**PROJECT :** PROPOSED SORTATION FACILITY  
**LOCATION :** LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO

**REFERENCE No. :** 11227097-A1  
**BORING No. :** BH-01  
**SAMPLE No. :** ST-5  
**DEPTH :** 3.05 m      **DATE :** 5/11/2021

## UNIFIED SOIL CLASSIFICATION (BASED ON THE STANDARD LC 21-040)



CLAY	SILT	SAND			GRAVEL		COBBLES AND BOULDERS
		fine	medium	coarse	fine	coarse	

Description	w (%)	W <sub>L</sub> (%)	I <sub>p</sub> (%)	Classification (1)
Silt, traces of sand	45	52	31	CH

(1) USCS

% Gravel	% Sand	% Silt and % Clay	c <sub>u</sub>	c <sub>c</sub>	D85	D60	D50	D30	D15	D10
0	7	73								

Remarks :

Prepared by : Mark Gamboz, B.Sc. Geology

Verified by : Mark Gamboz, B.Sc. Geology

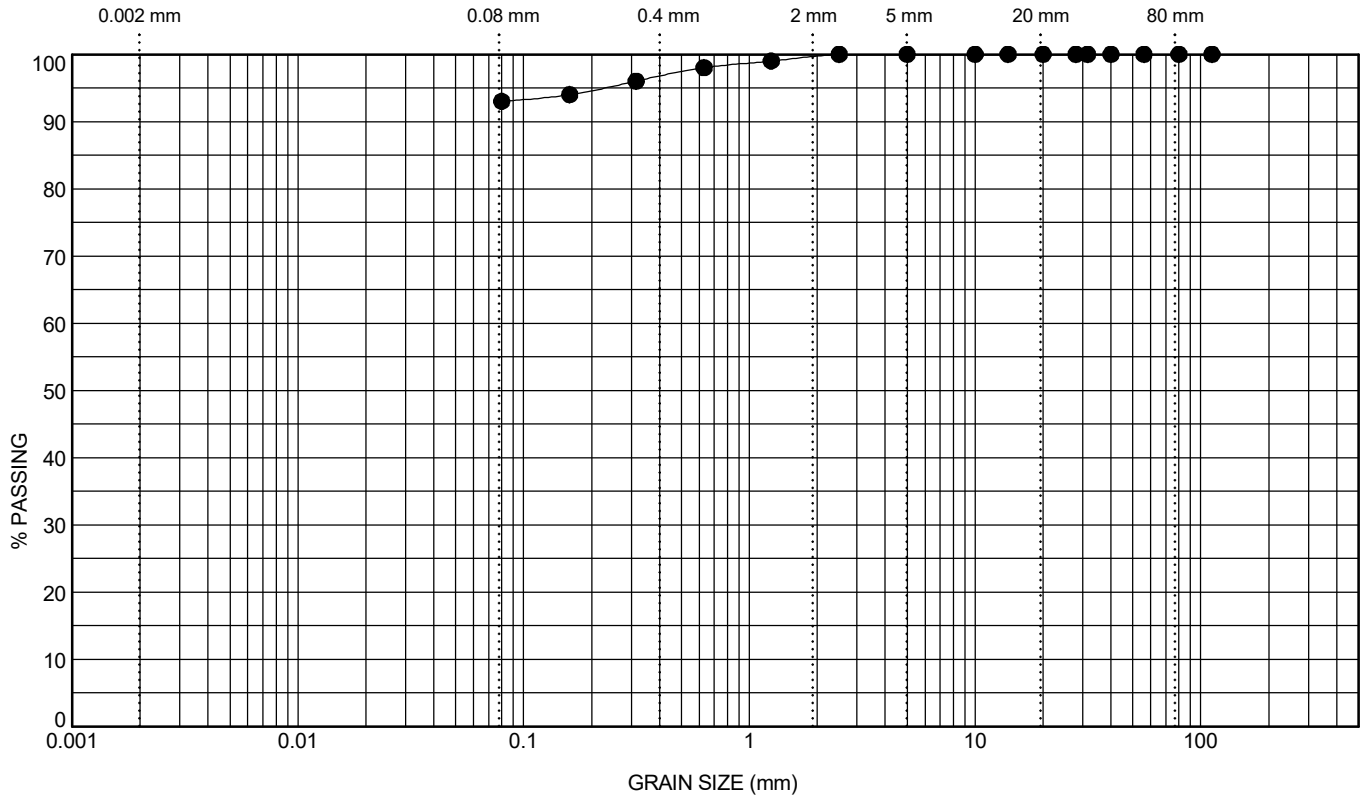


# GRAIN SIZE ANALYSIS REPORT

**CLIENT:** MEDUSA LP  
**PROJECT :** PROPOSED SORTATION FACILITY  
**LOCATION :** LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO

**REFERENCE No. :** 11227097-A1  
**BORING No. :** BH-01  
**SAMPLE No. :** SS-11  
**DEPTH :** 9.15 m      **DATE :** 5/11/2021

## UNIFIED SOIL CLASSIFICATION (BASED ON THE STANDARD LC 21-040)



CLAY	SILT	SAND			GRAVEL		COBBLES AND BOULDERS
		fine	medium	coarse	fine	coarse	

Description	w (%)	W <sub>L</sub> (%)	I <sub>p</sub> (%)	Classification (1)
Silt, traces of sand	68	50	26	CH

(1) USCS

% Gravel	% Sand	% Silt and % Clay	c <sub>u</sub>	c <sub>c</sub>	D85	D60	D50	D30	D15	D10
0	7	93								

Remarks :

Prepared by : Mark Gamboz, B.Sc. Geology

Verified by : Mark Gamboz, B.Sc. Geology



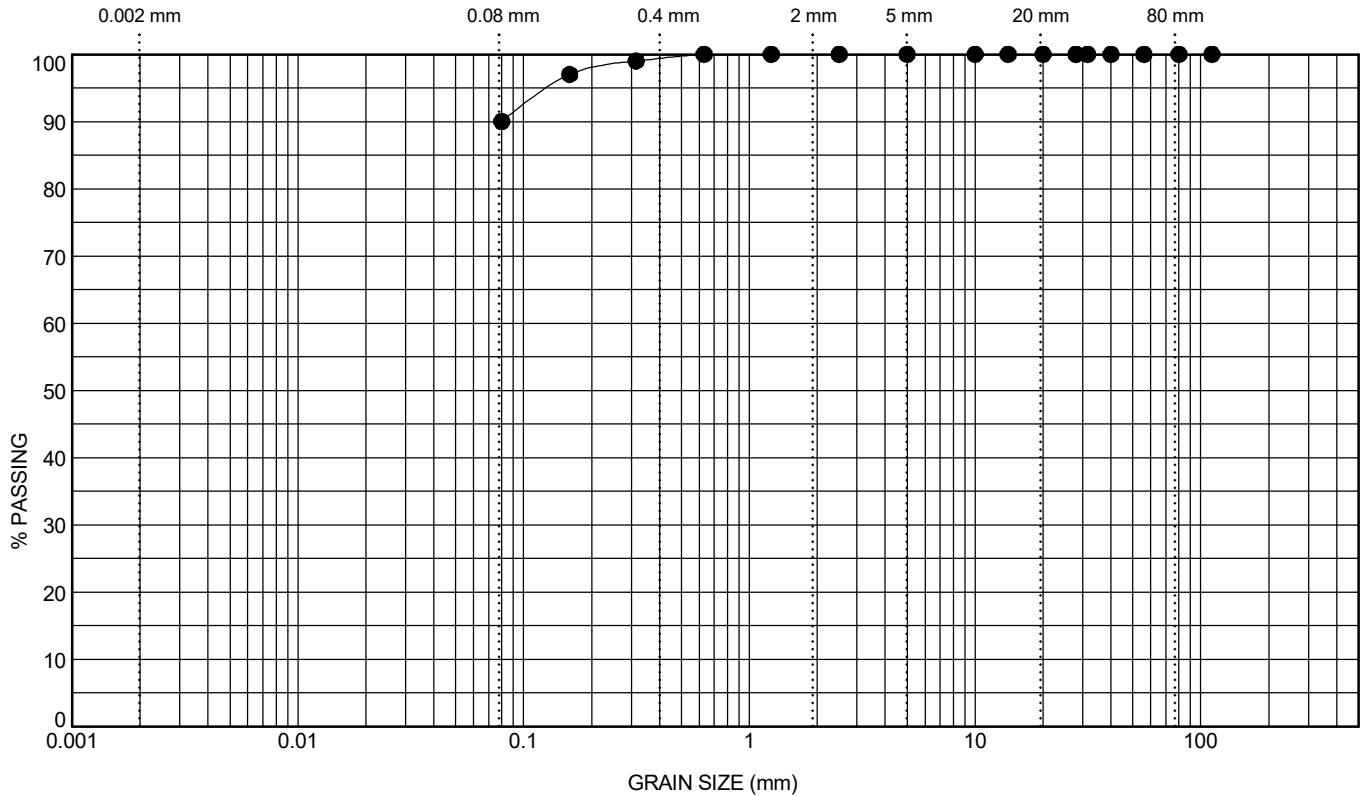


# GRAIN SIZE ANALYSIS REPORT

**CLIENT:** MEDUSA LP  
**PROJECT :** PROPOSED SORTATION FACILITY  
**LOCATION :** LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO

**REFERENCE No. :** 11227097-A1  
**BORING No. :** BH-02  
**SAMPLE No. :** SS-3  
**DEPTH :** 1.52 m **DATE :** 5/11/2021

## UNIFIED SOIL CLASSIFICATION (BASED ON THE STANDARD LC 21-040)



CLAY	SILT	SAND			GRAVEL		COBBLES AND BOULDERS
		fine	medium	coarse	fine	coarse	

Description	w (%)	W <sub>L</sub> (%)	I <sub>p</sub> (%)	Classification (1)
Silt, traces of sand	27	38	21	CL

(1) USCS

% Gravel	% Sand	% Silt and % Clay	c <sub>u</sub>	c <sub>c</sub>	D85	D60	D50	D30	D15	D10
0	10	90								

Remarks :

Prepared by : Mark Gamboz, B.Sc. Geology

Verified by : Mark Gamboz, B.Sc. Geology

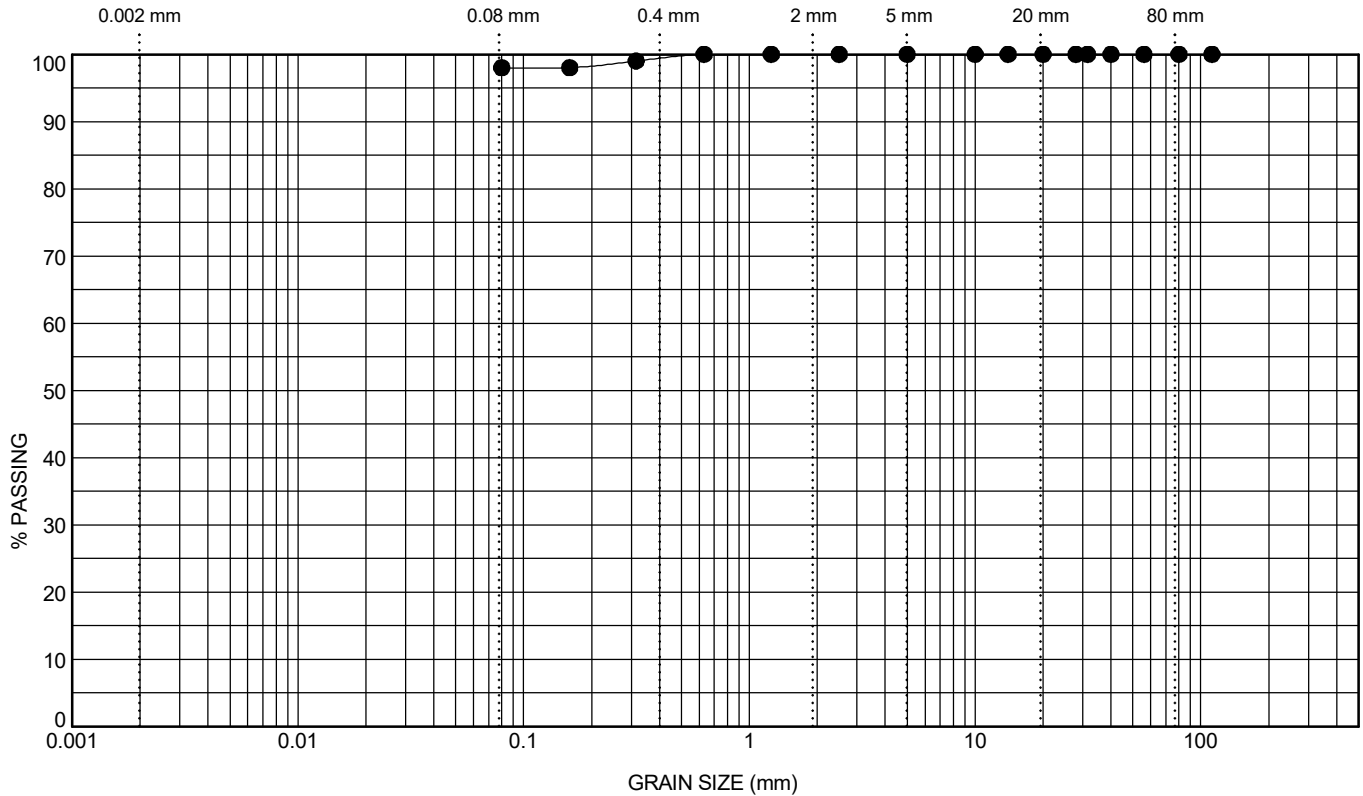


# GRAIN SIZE ANALYSIS REPORT

**CLIENT:** MEDUSA LP  
**PROJECT :** PROPOSED SORTATION FACILITY  
**LOCATION :** LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO

**REFERENCE No. :** 11227097-A1  
**BORING No. :** BH-02  
**SAMPLE No. :** SS-11  
**DEPTH :** 9.15 m      **DATE :** 5/11/2021

## UNIFIED SOIL CLASSIFICATION (BASED ON THE STANDARD LC 21-040)



CLAY	SILT	SAND			GRAVEL		COBBLES AND BOULDERS
		fine	medium	coarse	fine	coarse	

Description	w (%)	W <sub>L</sub> (%)	I <sub>p</sub> (%)	Classification (1)
Silt, traces of sand	25	27	5	CL-ML

(1) USCS

% Gravel	% Sand	% Silt and % Clay	c <sub>u</sub>	c <sub>c</sub>	D85	D60	D50	D30	D15	D10
0	2	98								

Remarks :

Prepared by : Mark Gamboz, B.Sc. Geology

Verified by : Mark Gamboz, B.Sc. Geology

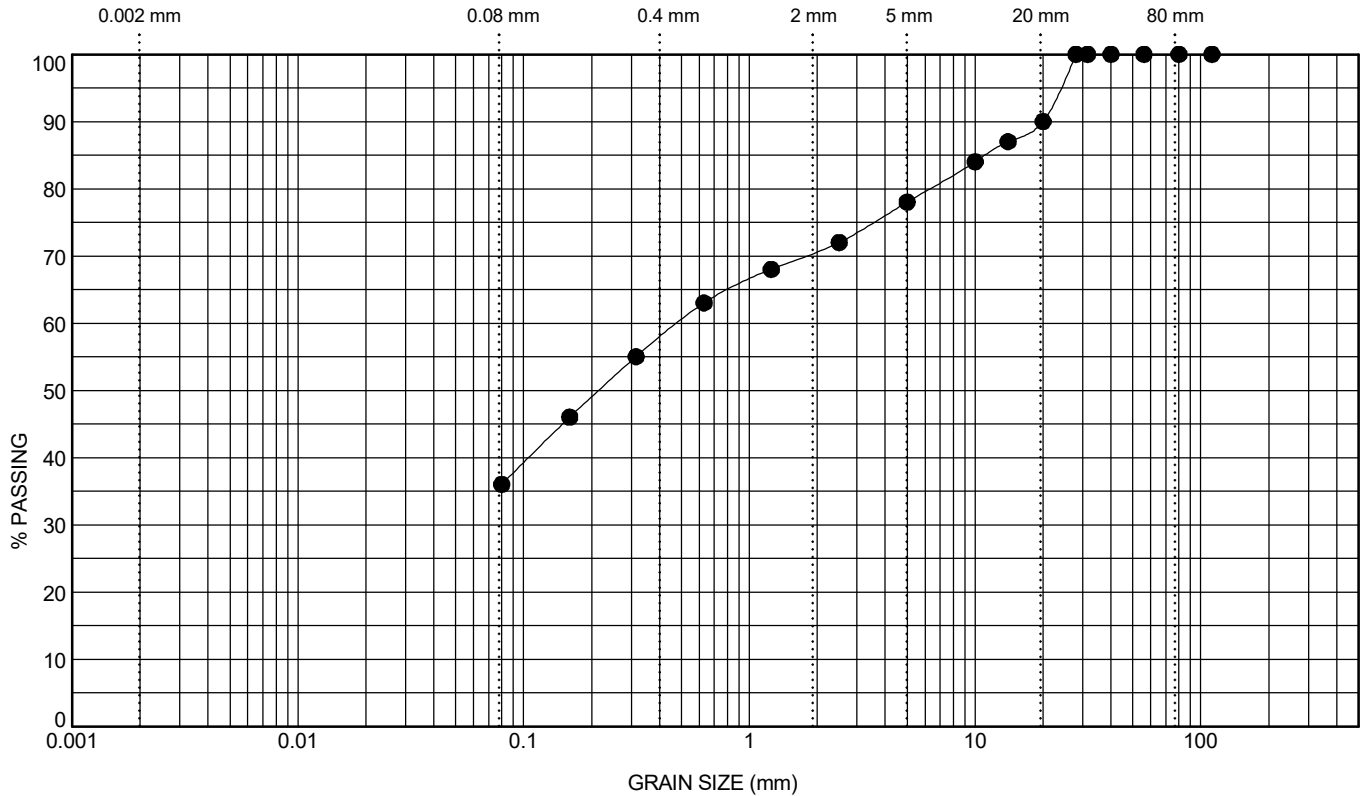


# GRAIN SIZE ANALYSIS REPORT

**CLIENT:** MEDUSA LP  
**PROJECT :** PROPOSED SORTATION FACILITY  
**LOCATION :** LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO

**REFERENCE No. :** 11227097-A1  
**BORING No. :** BH-02  
**SAMPLE No. :** SS-14  
**DEPTH :** 11.43 m **DATE :** 5/11/2021

## UNIFIED SOIL CLASSIFICATION (BASED ON THE STANDARD LC 21-040)



CLAY	SILT	SAND			GRAVEL		COBBLES AND BOULDERS
		fine	medium	coarse	fine	coarse	

Description	w (%)	W <sub>L</sub> (%)	I <sub>p</sub> (%)	Classification (1)
Gravelly sand and silt	8	14	2	SM

(1) USCS

% Gravel	% Sand	% Silt and % Clay	c <sub>u</sub>	c <sub>c</sub>	D85	D60	D50	D30	D15	D10
22	42	36								

Remarks :

Prepared by : Mark Gamboz, B.Sc. Geology

Verified by : Mark Gamboz, B.Sc. Geology

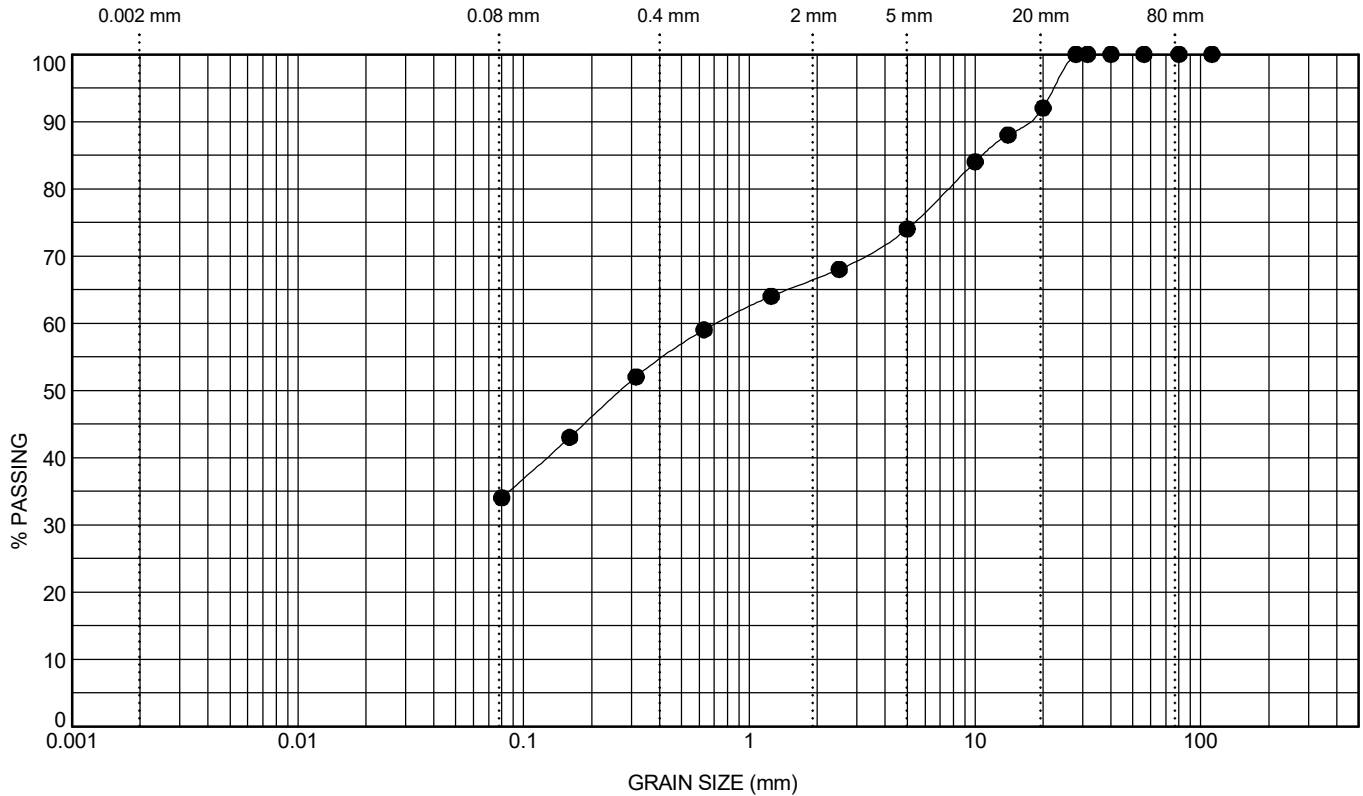


# GRAIN SIZE ANALYSIS REPORT

**CLIENT:** MEDUSA LP  
**PROJECT :** PROPOSED SORTATION FACILITY  
**LOCATION :** LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO

**REFERENCE No. :** 11227097-A1  
**BORING No. :** BH-02  
**SAMPLE No. :** SS-19  
**DEPTH :** 15.24 m **DATE :** 5/11/2021

## UNIFIED SOIL CLASSIFICATION (BASED ON THE STANDARD LC 21-040)



CLAY	SILT	SAND			GRAVEL		COBBLES AND BOULDERS
		fine	medium	coarse	fine	coarse	

Description	w (%)	W <sub>L</sub> (%)	I <sub>p</sub> (%)	Classification (1)
Silty and gravelly sand	8	13	2	SM

(1) USCS

% Gravel	% Sand	% Silt and % Clay	c <sub>u</sub>	c <sub>c</sub>	D85	D60	D50	D30	D15	D10
26	40	34								

Remarks :

Prepared by : Mark Gamboz, B.Sc. Geology

Verified by : Mark Gamboz, B.Sc. Geology

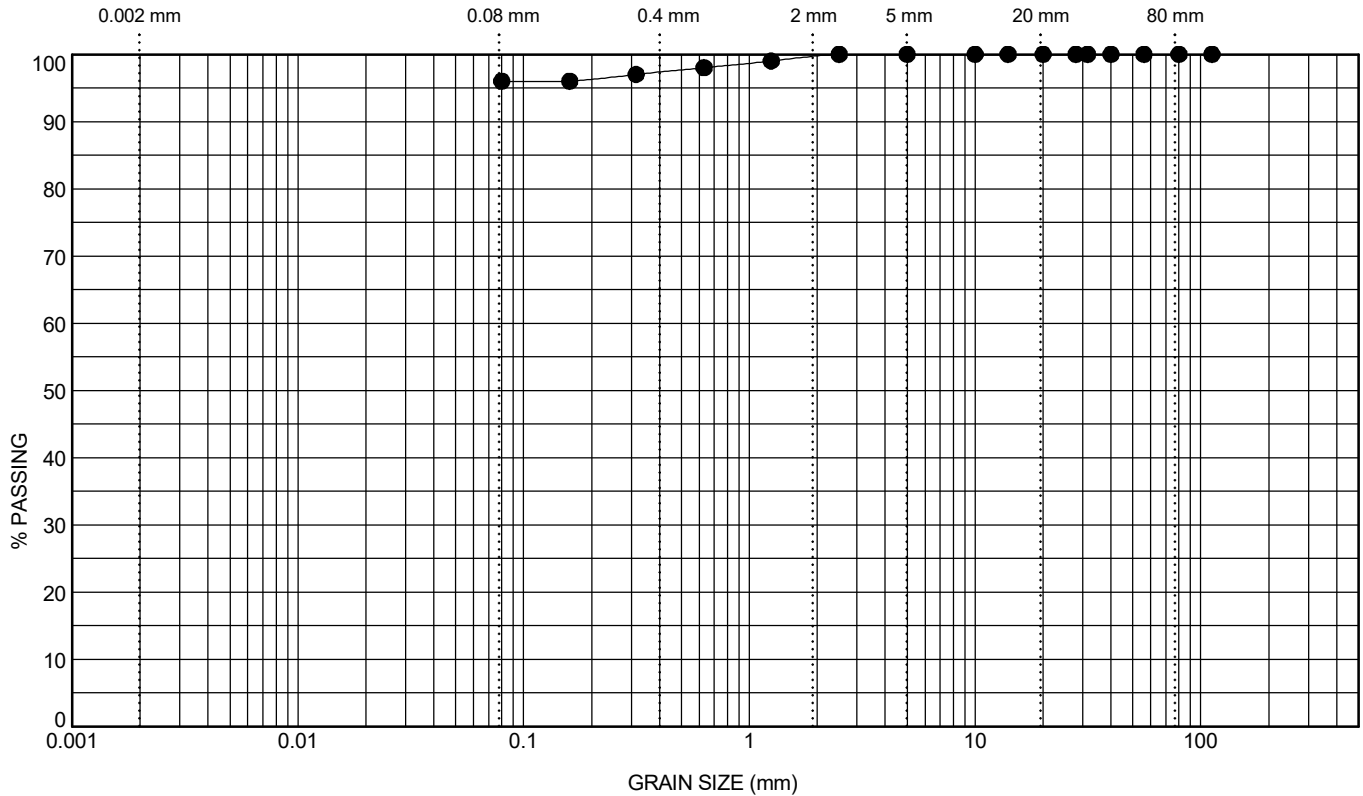


# GRAIN SIZE ANALYSIS REPORT

**CLIENT:** MEDUSA LP  
**PROJECT :** PROPOSED SORTATION FACILITY  
**LOCATION :** LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO

**REFERENCE No. :** 11227097-A1  
**BORING No. :** BH-03  
**SAMPLE No. :** SS-11  
**DEPTH :** 8.23 m      **DATE :** 5/11/2021

## UNIFIED SOIL CLASSIFICATION (BASED ON THE STANDARD LC 21-040)



CLAY	SILT	SAND			GRAVEL		COBBLES AND BOULDERS
		fine	medium	coarse	fine	coarse	

Description	w (%)	W <sub>L</sub> (%)	I <sub>p</sub> (%)	Classification (1)
Silt, traces of sand	66	48	25	CL

(1) USCS

% Gravel	% Sand	% Silt and % Clay	c <sub>u</sub>	c <sub>c</sub>	D85	D60	D50	D30	D15	D10
0	4	96								

Remarks :

Prepared by : Mark Gamboz, B.Sc. Geology

Verified by : Mark Gamboz, B.Sc. Geology

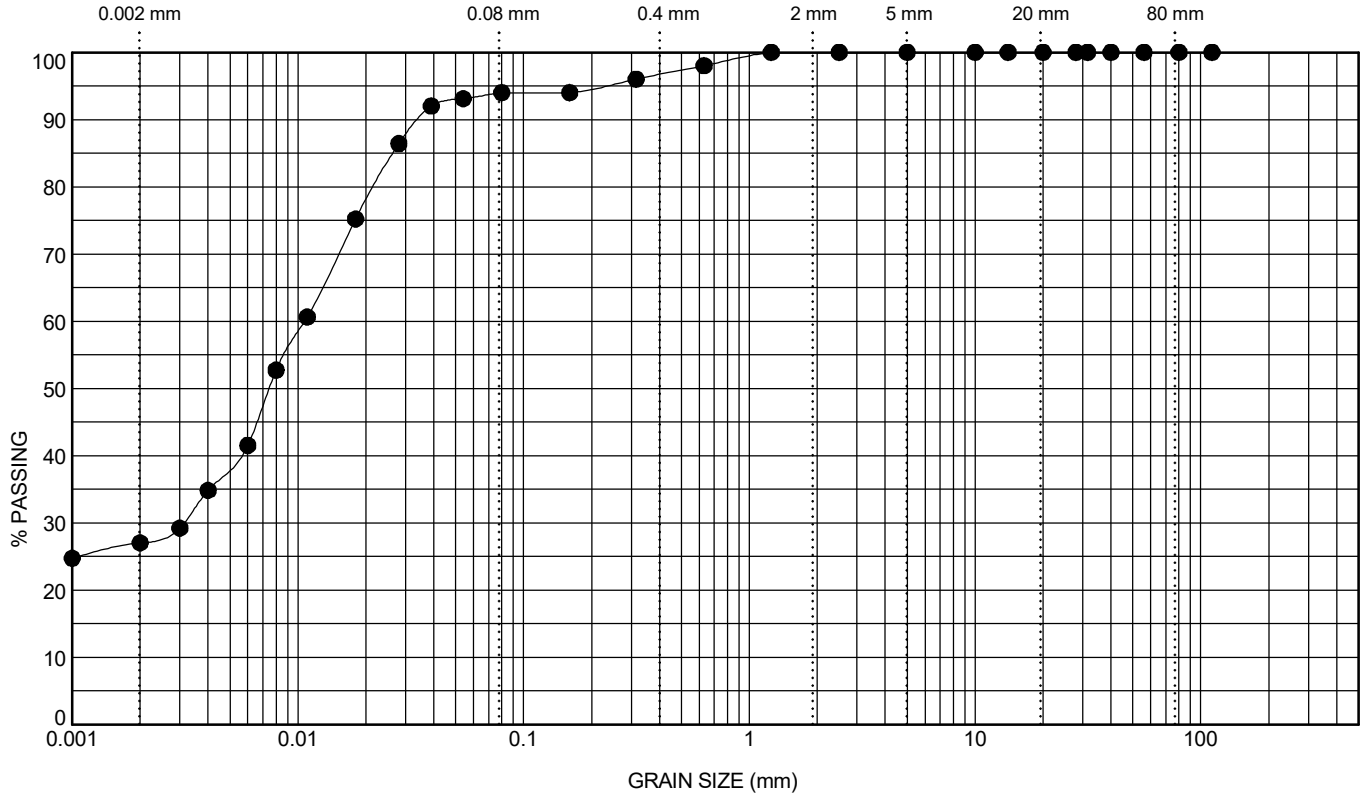


# GRAIN SIZE ANALYSIS REPORT (WITH SEDIMENTATION)

**CLIENT:** MEDUSA LP  
**PROJECT :** PROPOSED SORTATION FACILITY  
**LOCATION :** LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO

**REFERENCE No. :** 11227097-A1  
**BORING No. :** BH-03  
**SAMPLE No. :** SS-14  
**DEPTH :** 12.19 m **DATE :** 5/11/2021

## UNIFIED SOIL CLASSIFICATION (BASED ON THE STANDARD LC 21-040)



CLAY	SILT	SAND			GRAVEL		COBBLES AND BOULDERS
		fine	medium	coarse	fine	coarse	

Description	w (%)	W <sub>L</sub> (%)	I <sub>p</sub> (%)	Classification (1)
Clayey silt, traces of sand	39	26	8	CL

(1) USCS

% Gravel	% Sand	% Silt	% Clay	c <sub>u</sub>	c <sub>c</sub>	D85	D60	D50	D30	D15	D10
0	6	67	27								

Remarks :

Prepared by : Mark Gamboz, B.Sc. Geology

Verified by : Mark Gamboz, B.Sc. Geology

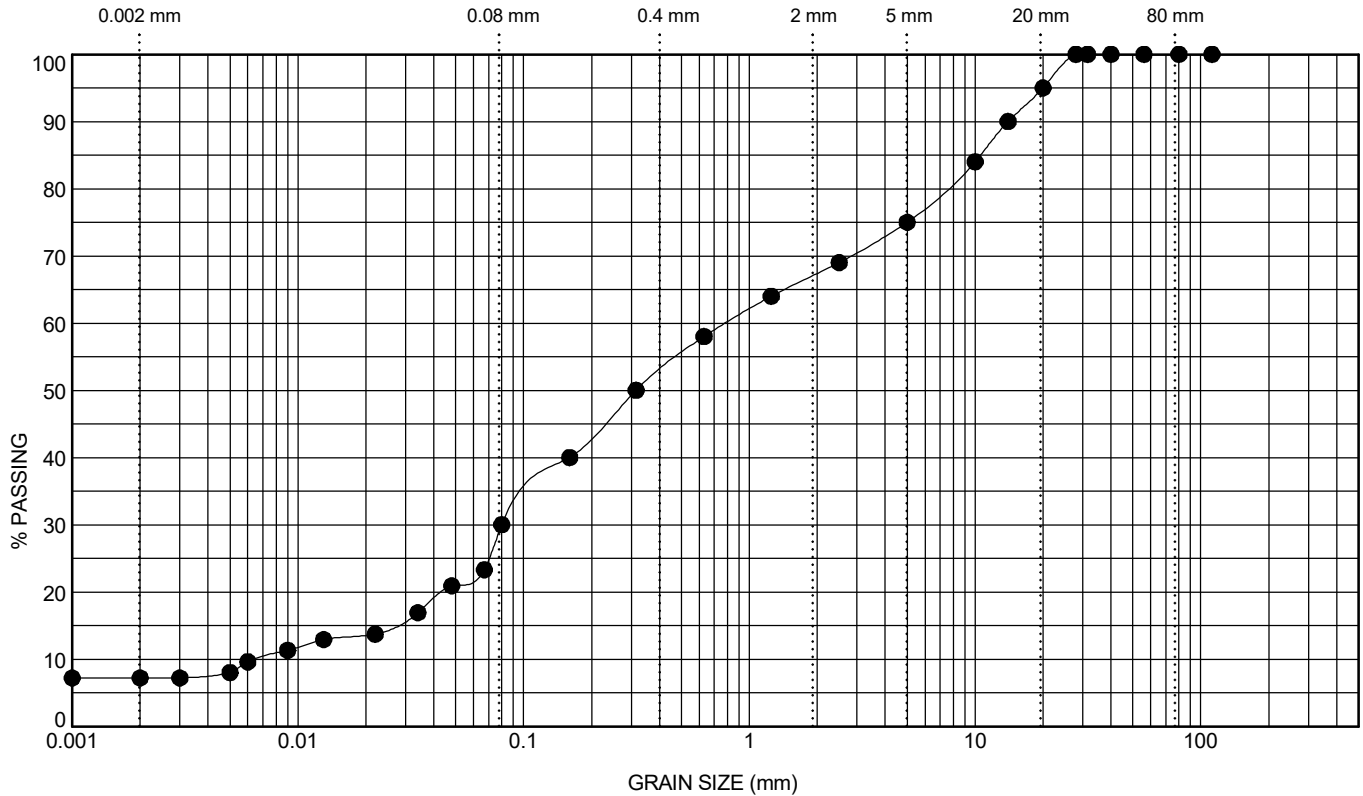


# GRAIN SIZE ANALYSIS REPORT (WITH SEDIMENTATION)

**CLIENT:** MEDUSA LP  
**PROJECT :** PROPOSED SORTATION FACILITY  
**LOCATION :** LEIKIN DRIVE AND MERIVALE ROAD INTERSECTION, NEPEAN, ONTARIO

**REFERENCE No. :** 11227097-A1  
**BORING No. :** BH-03  
**SAMPLE No. :** SS-18  
**DEPTH :** 18.29 m **DATE :** 5/11/2021

UNIFIED SOIL CLASSIFICATION (BASED ON THE STANDARD LC 21-040)



CLAY	SILT	SAND			GRAVEL		COBBLES AND BOULDERS
		fine	medium	coarse	fine	coarse	

Description	w (%)	W <sub>L</sub> (%)	I <sub>p</sub> (%)	Classification (1)
Gravelly and silty sand, traces of clay	9	15	2	SM

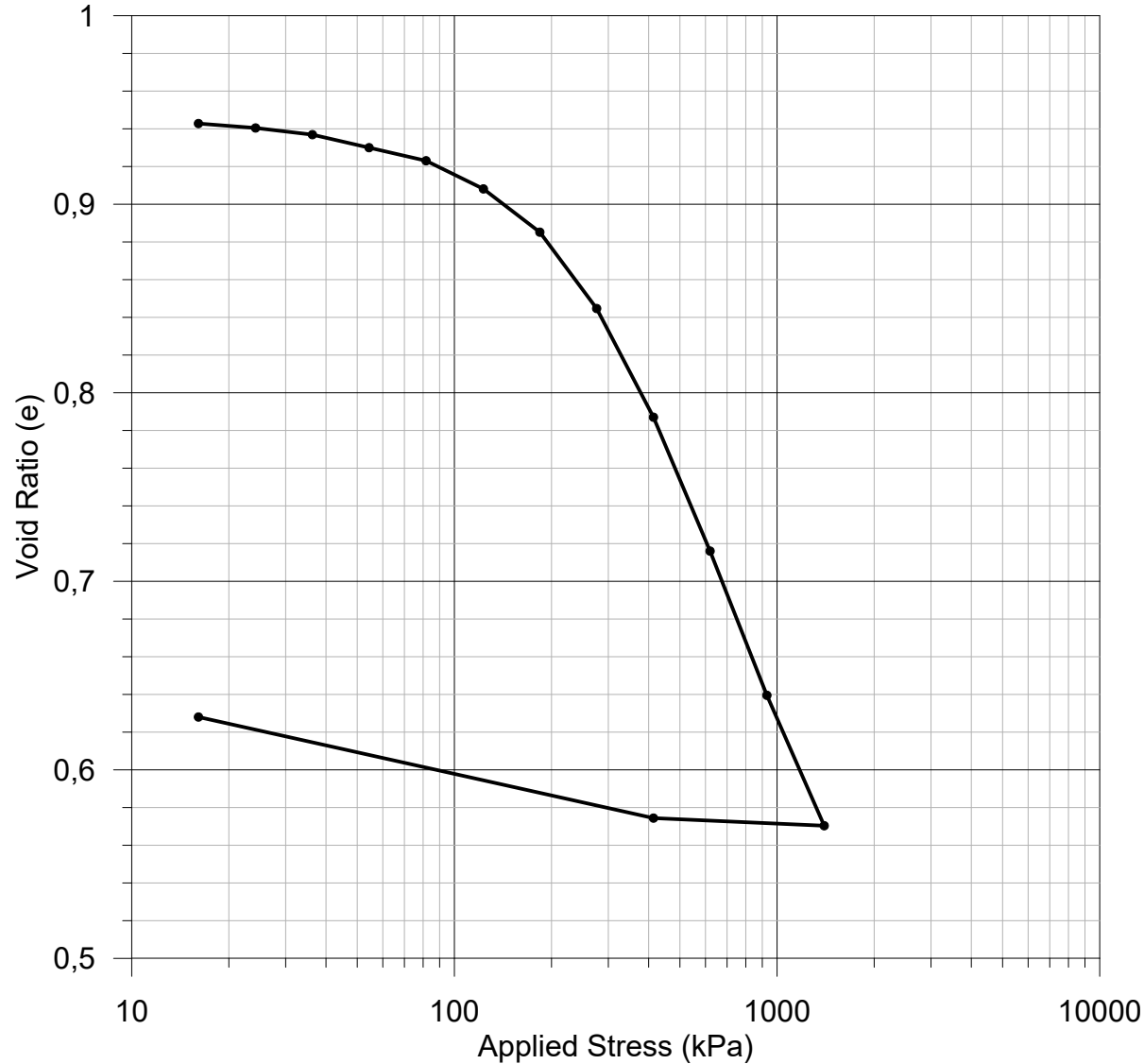
(1) USCS

% Gravel	% Sand	% Silt	% Clay	c <sub>u</sub>	c <sub>c</sub>	D85	D60	D50	D30	D15	D10
25	45	23	7								

Remarks :

Prepared by : Mark Gamboz, B.Sc. Geology Verified by : Mark Gamboz, B.Sc. Geology

# Oedometric Consolidation Test - BH-101-23 ST-06



## Sample Before Test

Diameter : 6,35 cm  
 Height : 2,56 cm  
 Unit Weight : 18,13 kN/m<sup>3</sup>  
 Water Content : 33,65%  
 Void Ratio : 0,95  
 Degree of Saturation : 95,38%  
 Specific Gravity : 2,70 (Assumed)

## Sample After Test

Water Content : 25,24%

## Sample Description (Visual)

Firm to stiff, grey silt and clay, traces of sand (CH)

## Test Results

Recompression Index ( $c_r$ )\* : 0,03  
 Compression Index ( $c_c$ ) : 0,39  
 Decompression Index ( $c_d$ ) : 0,03  
 Preconsolidation Pressure ( $\sigma'_p$ ) : 234 kPa  
 Preconsolidation Pressure ( $\sigma'_{p-min}$ ) : 150 kPa  
 Preconsolidation Pressure ( $\sigma'_{p-max}$ ) : 275 kPa

\* : Calculated in the first steps

**Loading Rate : 50%**

**Test Method Used :**

**ASTM D 2435-04**



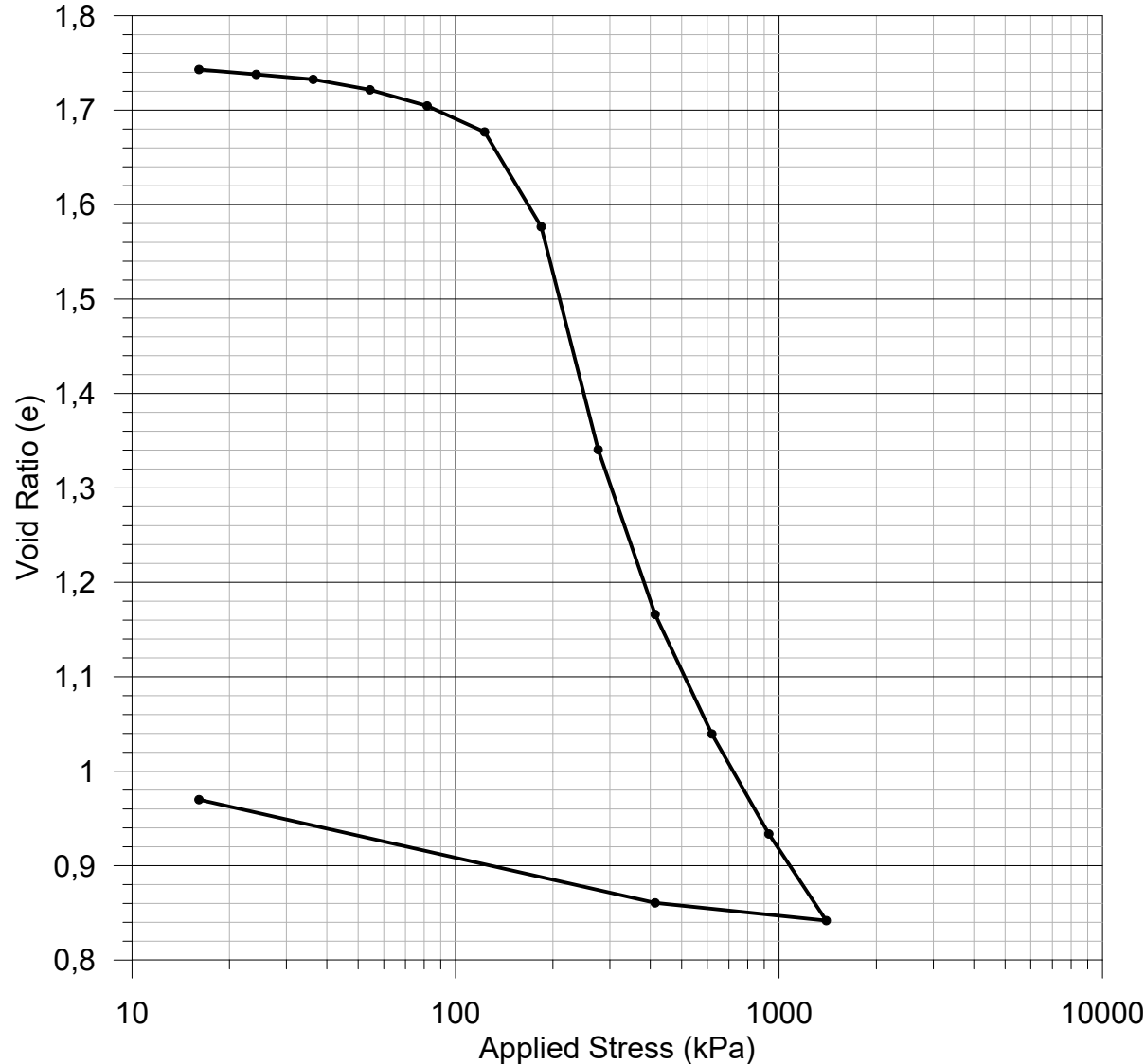
Borehole : BH-101-23  
 Sample : ST-06  
 Depth (m) : 3,42 to 3,52

Client: Medusa Limited Partnership  
 Project: Geotechnical Investigation - Proposed Distribution Center  
 Site: Bill Leathem Drive, Ottawa, Ontario  
 Date: 2023-08-08

Project No. : 12615684-A1  
 Laboratory No. : 2023-S092



# Oedometric Consolidation Test - BH-101-23 ST-12



### Sample Before Test

Diameter : 6,35 cm  
 Height : 2,55 cm  
 Unit Weight : 15,92 kN/m<sup>3</sup>  
 Water Content : 65,69%  
 Void Ratio : 1,76  
 Degree of Saturation : 100,97%  
 Specific Gravity : 2,70 (Assumed)

### Sample After Test

Water Content : 38,23%

### Sample Description (Visual)

Firm to stiff, grey clayey silt to silty clay (CH)

### Test Results

Recompression Index ( $c_r$ )\* : 0,06  
 Compression Index ( $c_c$ ) : 1,34  
 Decompression Index ( $c_d$ ) : 0,04  
 Preconsolidation Pressure ( $\sigma'_p$ ) : 162 kPa  
 Preconsolidation Pressure ( $\sigma'_{p-min}$ ) : 135 kPa  
 Preconsolidation Pressure ( $\sigma'_{p-max}$ ) : 183 kPa

\* : Calculated in the first steps

**Loading Rate : 50%**  
**Test Method Used :**  
**ASTM D 2435-04**

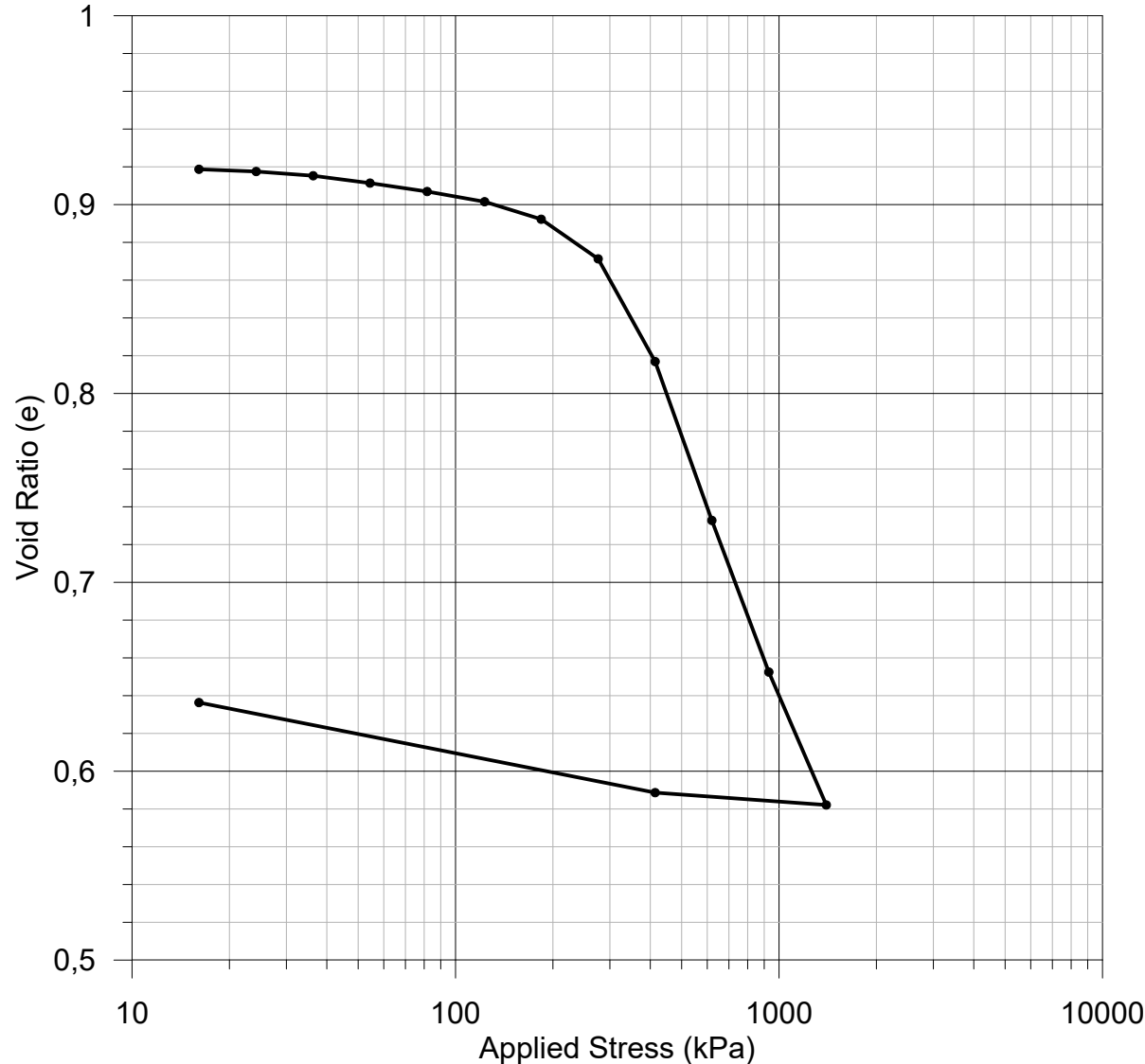


Borehole : BH-101-23  
 Sample : ST-12  
 Depth (m) : 7,98 to 8,08

Client: Medusa Limited Partnership  
 Project: Geotechnical Investigation - Proposed Distribution Center  
 Site: Bill Leathem Drive, Ottawa, Ontario  
 Date: 2023-08-08

Project No. : 12615684-A1  
 Laboratory No. : 2023-S092

# Oedometric Consolidation Test - BH-102-23 ST-12



## Sample Before Test

Diameter : 6,35 cm  
 Height : 2,56 cm  
 Unit Weight : 18,45 kN/m<sup>3</sup>  
 Water Content : 33,80%  
 Void Ratio : 0,92  
 Degree of Saturation : 99,08%  
 Specific Gravity : 2,70 (Assumed)

## Sample After Test

Water Content : 25,22%

## Sample Description (Visual)

Firm to stiff, grey clayey silt to silty clay (CL)

## Test Results

Recompression Index ( $c_r$ )\* : 0,02  
 Compression Index ( $c_c$ ) : 0,47  
 Decompression Index ( $c_d$ ) : 0,03  
 Preconsolidation Pressure ( $\sigma'_p$ ) : 336 kPa  
 Preconsolidation Pressure ( $\sigma'_{p-min}$ ) : 248 kPa  
 Preconsolidation Pressure ( $\sigma'_{p-max}$ ) : 411 kPa

\* : Calculated in the first steps

**Loading Rate : 50%**

**Test Method Used :**

**ASTM D 2435-04**

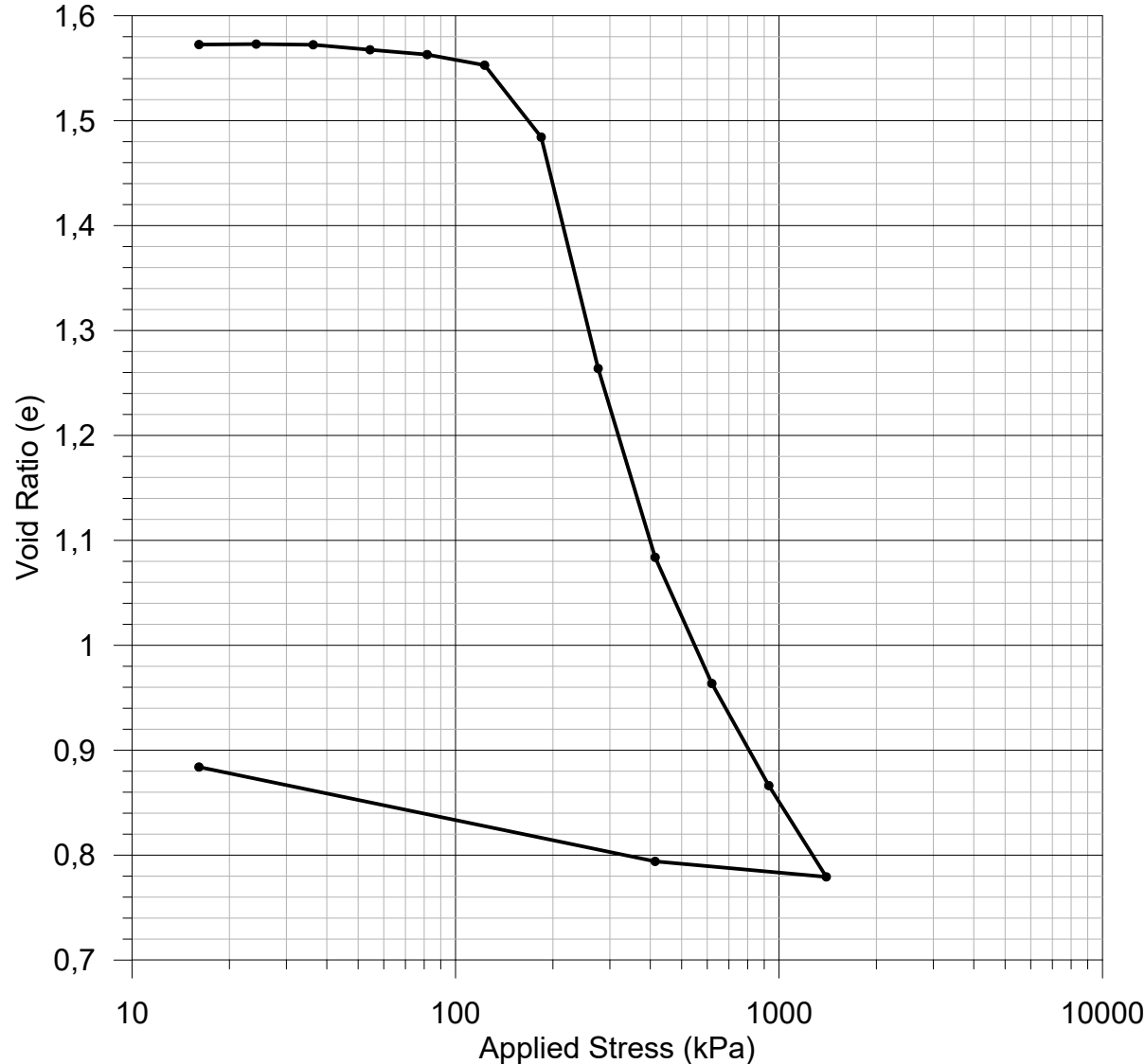


Borehole : BH-102-23  
 Sample : ST-12  
 Depth (m) : 7,99 to 8,09

Client: Medusa Limited Partnership  
 Project: Geotechnical Investigation - Proposed Distribution Center  
 Site: Bill Leathem Drive, Ottawa, Ontario  
 Date: 2023-08-11

Project No. : 12615684-A1  
 Laboratory No. : 2023-S092

# Oedometric Consolidation Test - BH-102-23 ST-16



## Sample Before Test

Diameter : 6,35 cm  
 Height : 2,55 cm  
 Unit Weight : 16,31 kN/m<sup>3</sup>  
 Water Content : 58,81%  
 Void Ratio : 1,58  
 Degree of Saturation : 100,59%  
 Specific Gravity : 2,70 (Assumed)

## Sample After Test

Water Content : 35,39%

## Sample Description (Visual)

Firm to stiff, grey clayey silt to silty clay (CH)

## Test Results

Recompression Index ( $c_r$ )\* : 0,03  
 Compression Index ( $c_c$ ) : 1,25  
 Decompression Index ( $c_d$ ) : 0,05  
 Preconsolidation Pressure ( $\sigma'_p$ ) : 169 kPa  
 Preconsolidation Pressure ( $\sigma'_{p-min}$ ) : 156 kPa  
 Preconsolidation Pressure ( $\sigma'_{p-max}$ ) : 183 kPa

\* : Calculated in the first steps

**Loading Rate : 50%**

**Test Method Used :**

**ASTM D 2435-04**



Borehole : BH-102-23  
 Sample : ST-16  
 Depth (m) : 13,49 to 13,59

Client: Medusa Limited Partnership  
 Project: Geotechnical Investigation - Proposed Distribution Center  
 Site: Bill Leathem Drive, Ottawa, Ontario  
 Date: 2023-08-11

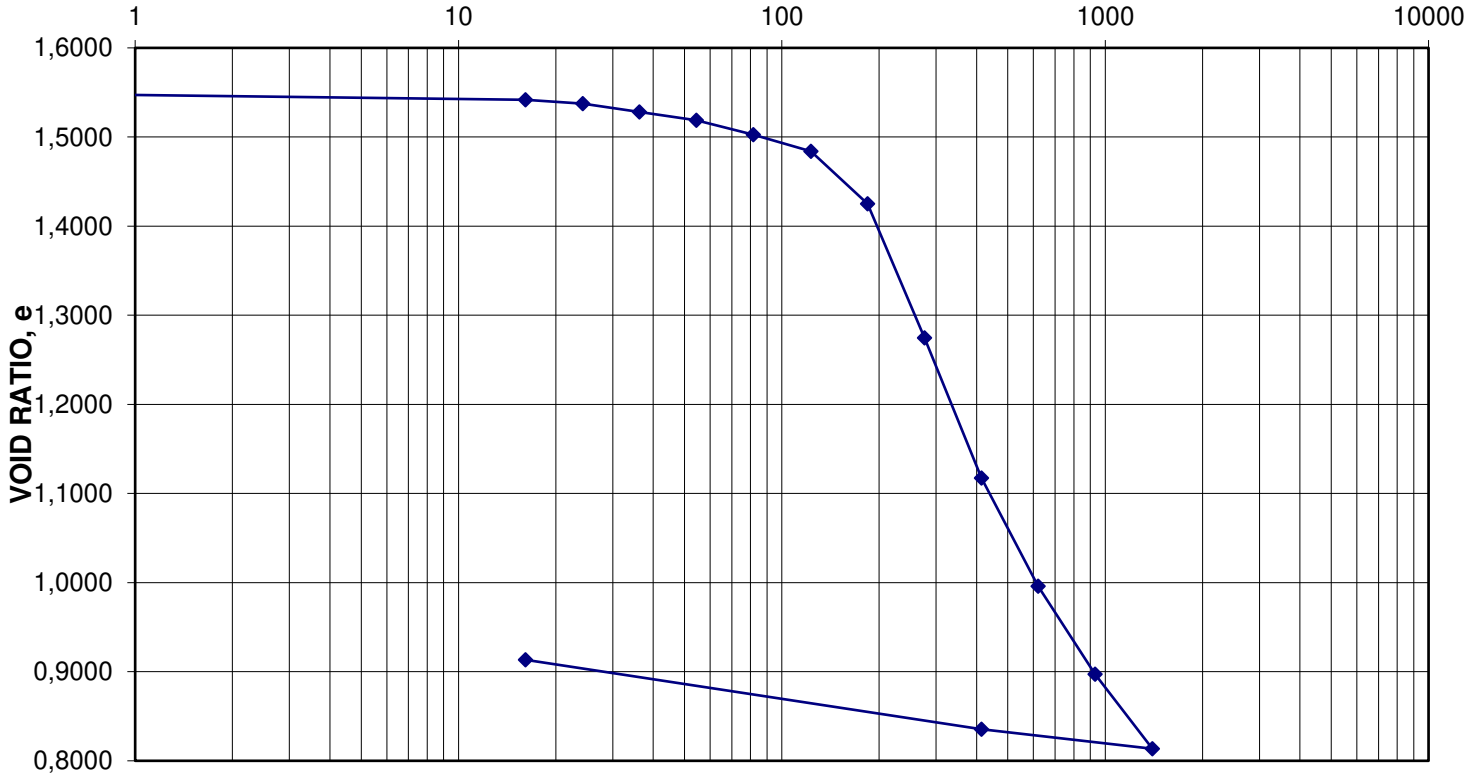
Project No. : 12615684-A1  
 Laboratory No. : 2023-S092



Client: Medusa LP Lab No: 2021-S0081  
 Project: Nepean, Ontario Project No: 11227097-A1

Borehole No: BH02 Sample No: TM7 Depth: 4,81-4,98 m  
 Description of Material: CL (medium)

APPLIED PRESSURE (kPa)



COMPRESSIBILITY PARAMETERS

$s'_p$ Preconsolidation pressure (kPa): <u>167</u>	$e_o$ Initial void ratio: <u>1,5606</u>
$s'_{vo}$ Effective pressure: <u>42</u>	$c_r$ Recompression index: <u>0,07</u>
$s'_p - s'_{vo}$ Overconsolidation: <u>125</u>	$c_c$ Compression index: <u>0,87</u>
Overconsolidation ratio ("OCR"): <u>4,0</u>	$c_s$ Swelling index: <u>0,04</u>
Size of Sample: Diameter (mm): <u>63,52</u>	Moisture Content (W) %
Height (mm): <u>25,48</u>	Initial: <u>58,0</u> Final: <u>35,7</u>

Notes: \_\_\_\_\_

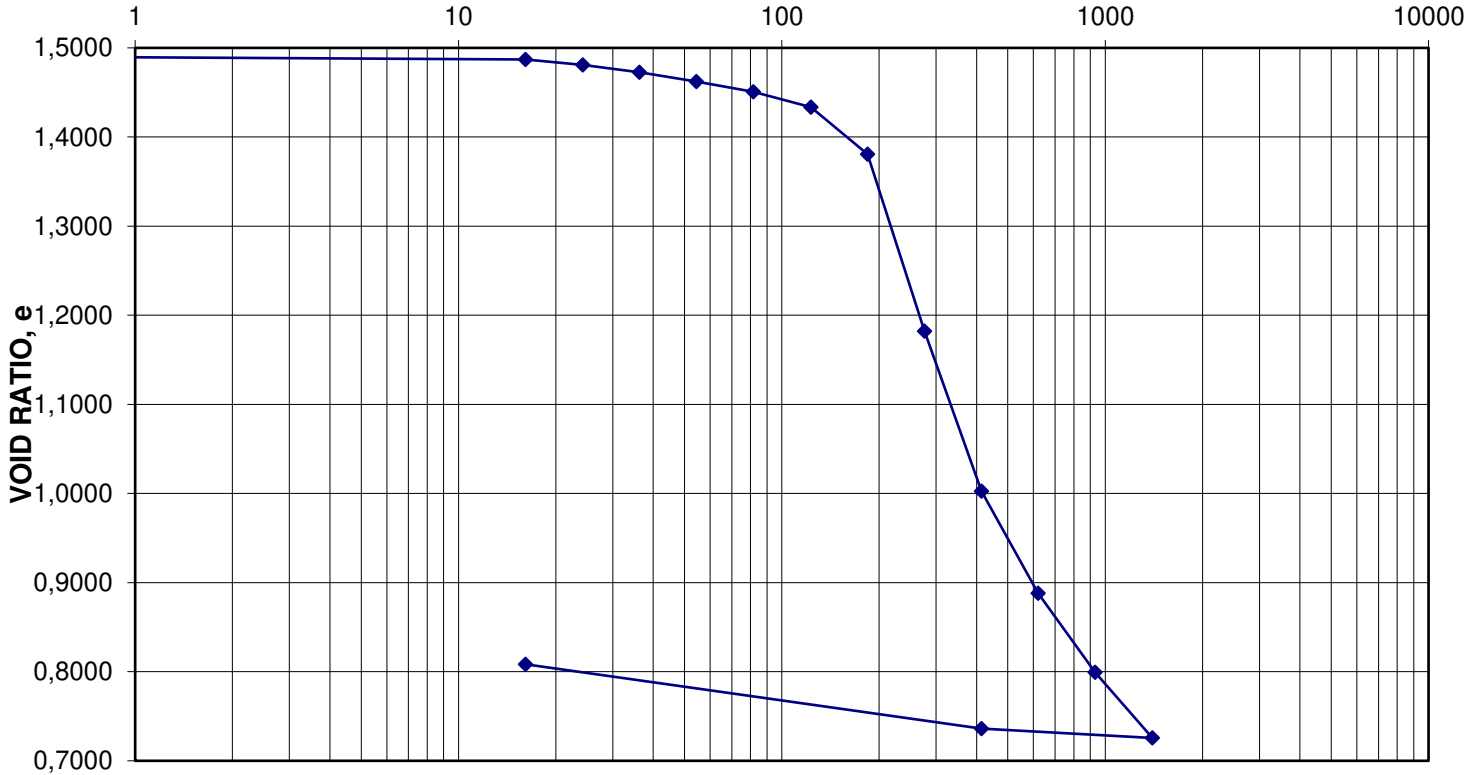
Performed By: A. Azizi Date: 2021-05-30  
 Checked By: M. Gamboz Date: 2021-06-04



Client: Medusa LP Lab No: 2021-S0081  
 Project: Nepean, Ontario Project No: 11227097-A1

Borehole No: BH03 Sample No: TM13 Depth: 10,87-11,02 m  
 Description of Material: CL (medium)

APPLIED PRESSURE (kPa)



COMPRESSIBILITY PARAMETERS

$S'_p$ Preconsolidation pressure (kPa): <u>176</u>	$e_o$ Initial void ratio: <u>1,4955</u>
$S'_{vo}$ Effective pressure: <u>81</u>	$c_r$ Recompression index: <u>0,06</u>
$S'_p - S'_{vo}$ Overconsolidation: <u>95</u>	$c_c$ Compression index: <u>1,13</u>
Overconsolidation ratio ("OCR"): <u>2,2</u>	$c_s$ Swelling index: <u>0,04</u>
Size of Sample: Diameter (mm): <u>63,52</u>	Moisture Content (W) %
Height (mm): <u>25,48</u>	Initial: <u>56,2</u> Final: <u>32,2</u>

Notes: \_\_\_\_\_

Performed By: A. Azizi Date: 2021-06-02  
 Checked By: M. Gamboz Date: 2021-06-07

Certificate of Analysis

Report Date: 22-Aug-2024

Client: **Paterson Group Consulting Engineers (Ottawa)**

Order Date: 16-Aug-2024

Client PO: 61024

Project Description: PG5876

<b>Client ID:</b>	BH6-24 SS3	-	-	-	-
<b>Sample Date:</b>	16-Aug-24 09:00	-	-	-	-
<b>Sample ID:</b>	2433647-01	-	-	-	-
<b>Matrix:</b>	Soil	-	-	-	-
<b>MDL/Units</b>					

**Physical Characteristics**

% Solids	0.1 % by Wt.	75.7	-	-	-	-
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**General Inorganics**

pH	0.05 pH Units	7.68	-	-	-	-
Resistivity	0.1 Ohm.m	69.5	-	-	-	-

**Anions**

Chloride	10 ug/g	<10	-	-	-	-
Sulphate	10 ug/g	<10	-	-	-	-



BUREAU  
VERITAS

Dossier Bureau Veritas: C340864

Date du rapport: 2023/08/31

GHD Consultants Ltée

Votre # du projet: 12615684-A1

Adresse du site: BROCCOLINI, NEPEAN

Votre # de commande: 762-003432

Initiales du préleveur: DV

### PARAMÈTRES CONVENTIONNELS (SOL)

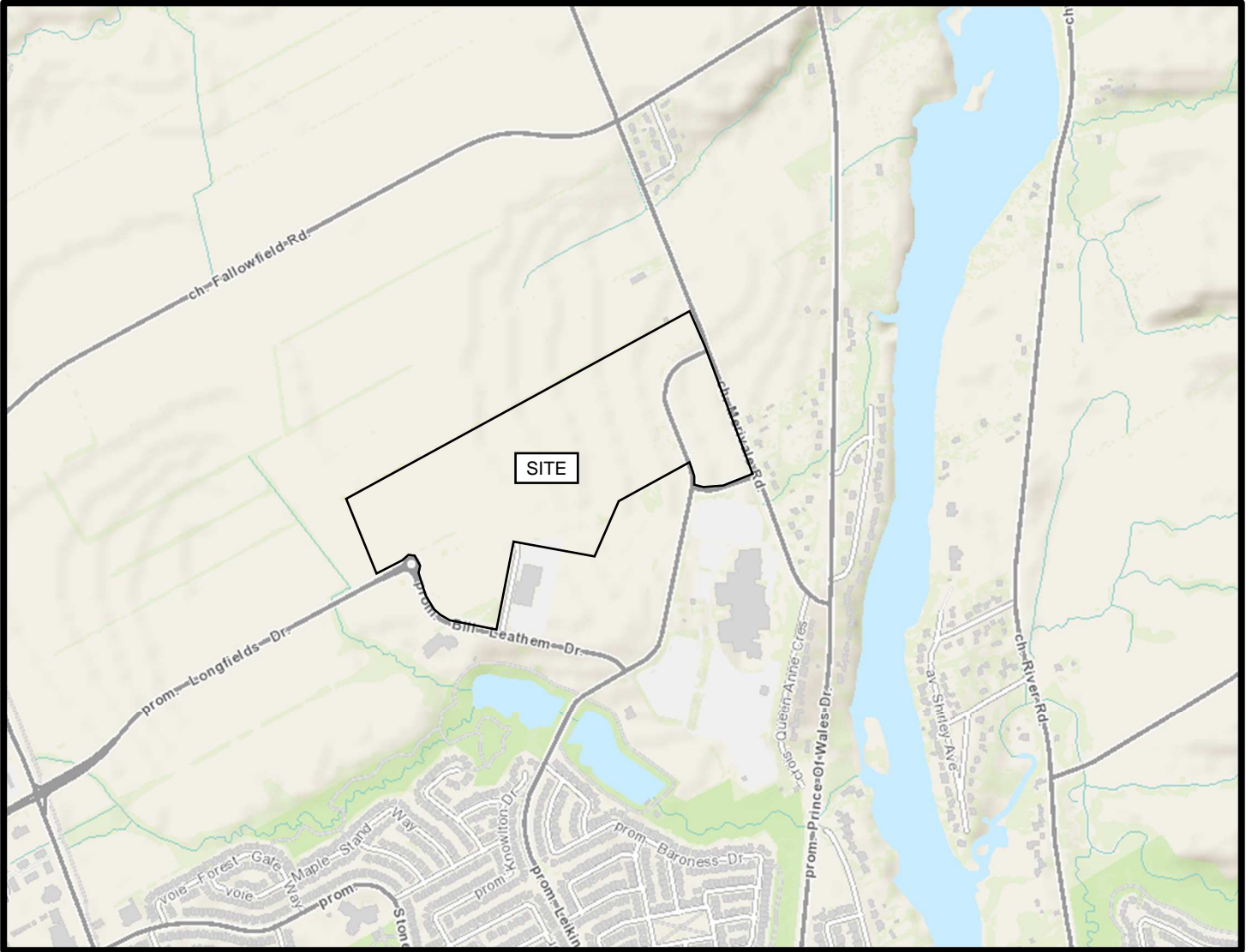
ID Bureau Veritas		MA7807	MA7808	MA7809		
Date d'échantillonnage		2023/07/07	2023/07/07	2023/07/07		
# Bordereau		N-A	N-A	N-A		
	<b>Unités</b>	<b>TP-104-23 VR-03 1,10-2,00</b>	<b>TP-113-23 VR-03 0,75-1,80</b>	<b>TP-114-23 VR-04 1,90 À 3,00</b>	<b>LDR</b>	<b>Lot CQ</b>
% HUMIDITÉ	%	23	26	26	N/A	N/A
<b>CONVENTIONNELS</b>						
Chlorures (Cl) †	mg/kg	1.2	3.1	2.3	1.0	2431102
Sulfates (SO4) †	mg/kg	8.4	15	9.2	5.0	2431102
LDR = Limite de détection rapportée						
Lot CQ = Lot contrôle qualité						
N/A = Non Applicable						
† Accréditation non existante pour ce paramètre						

# APPENDIX 2

FIGURE 1 - KEY PLAN

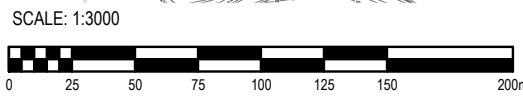
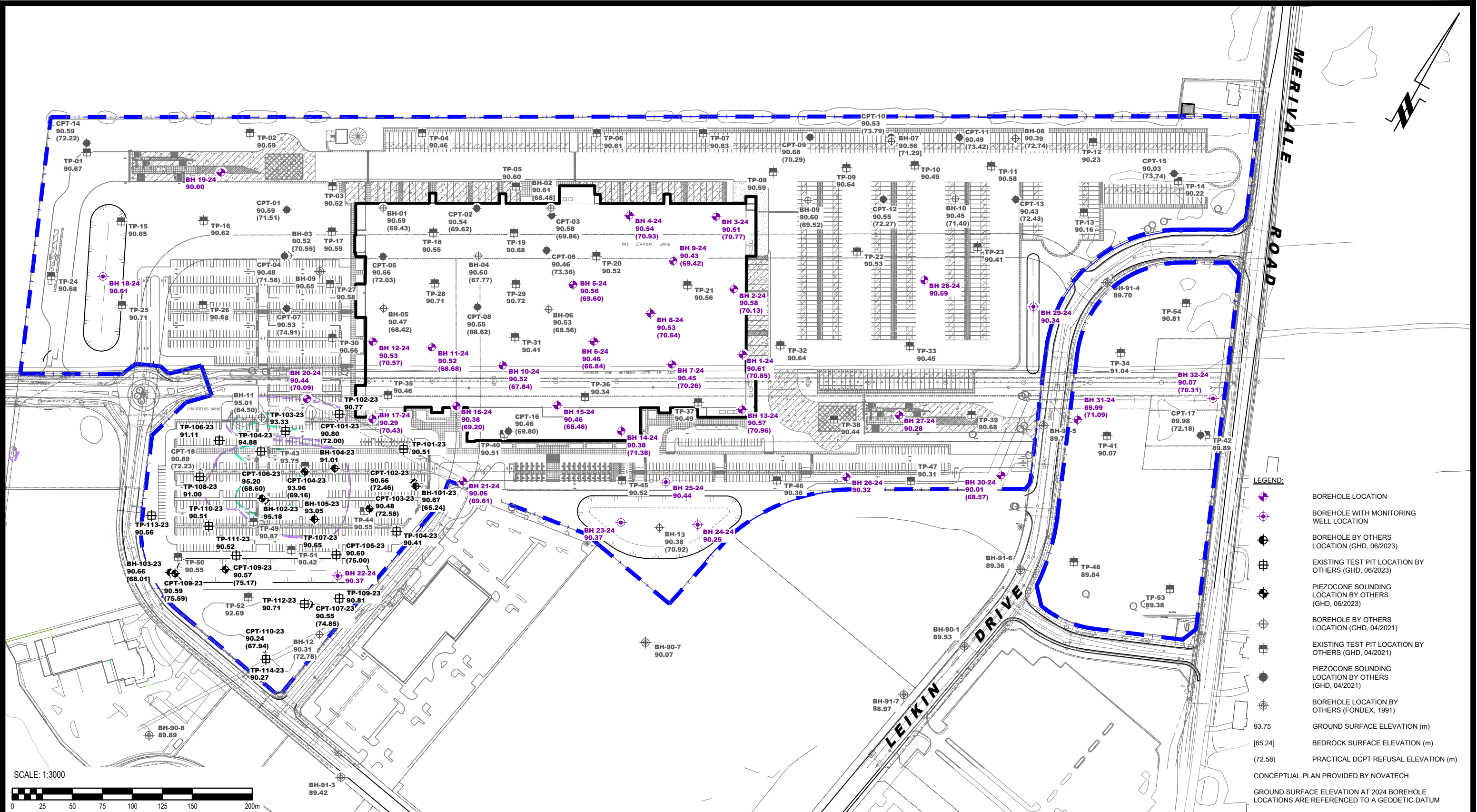
DRAWING PG5876-1 - TEST HOLE LOCATION PLAN





# FIGURE 1

## KEY PLAN



- LEGEND:**
- BOREHOLE LOCATION
  - BOREHOLE WITH MONITORING WELL LOCATION
  - BOREHOLE BY OTHERS LOCATION (GHD, 06/2023)
  - EXISTING TEST PIT LOCATION BY OTHERS (GHD, 06/2023)
  - PIEZOCONE SOUNDING LOCATION BY OTHERS (GHD, 06/2023)
  - BOREHOLE BY OTHERS LOCATION (GHD, 04/2021)
  - EXISTING TEST PIT LOCATION BY OTHERS (GHD, 04/2021)
  - PIEZOCONE SOUNDING LOCATION BY OTHERS (GHD, 04/2021)
  - BOREHOLE LOCATION BY OTHERS (FONDEX, 1991)
  - 93.75 GROUND SURFACE ELEVATION (m)
  - [65.24] BEDROCK SURFACE ELEVATION (m)
  - (72.58) PRACTICAL DCPT REFUSAL ELEVATION (m)
- CONCEPTUAL PLAN PROVIDED BY NOVATECH  
GROUND SURFACE ELEVATION AT 2024 BOREHOLE LOCATIONS ARE REFERENCED TO A GEODETIC DATUM

9 AURIGA DRIVE  
OTTAWA, ON  
K2E 7T9  
TEL: (613) 226-7381

NO.	REVISIONS	DD/MM/YYYY	INITIAL
2	2024 BOREHOLES ADDED TO PLAN UPDATED TO NEW CONCEPTUAL PLAN	30/08/2024	FC
1	AS PER REVISED SITE PLAN	16/07/2024	FC

**BROCCOLINI  
GEOTECHNICAL INVESTIGATION  
PROJECT X DEVELOPMENT - 90 BILL LEATHAM DRIVE,  
2 & 20 LEIKIN DRIVE & 11 BECKSTEAD ROAD**

**OTTAWA, ONTARIO**

**TEST HOLE LOCATION PLAN**

Scale:	1:3000	Date:	05/2021
Drawn by:	NFRV	Report No.:	PG5876-1
Checked by:	FC	Dwg. No.:	<b>PG5876-1</b>
Approved by:	DP	Revision No.:	2