

Minto Communities

Arcadia Commercial Site

Design Brief

March 5th, 2025

Arcadia Commercial Site

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1 Introduction

1.1 Scope

Arcadis Professional Services (Canada) Inc., hereinafter referred to as "Arcadis", has been retained by Minto Communities to prepare the necessary engineering plans, specifications and documents to support the proposed Site Plan Application for the subject lands, following the policies set out by the Planning and Development Branch of the City of Ottawa. This Brief will present a detailed grading and servicing scheme to support the development of the property and will include sections on water supply, wastewater management, minor and major stormwater management, site grading and erosion and sediment control. Minto Communities intends to sever a small portion of the remaining undeveloped lands of its 370 Huntmar Road site for use as its Sales and Design Centre.

This parcel of land is part of the proponent's larger "Arcadia" development lands, which are currently being developed. This subject parcel is referred to as Stage 5 in other previously approved Minto reports, including "Conceptual Site Servicing Arcadia Stages 1, 2, 5 and 8", and "Arcadia Interim SWMF", which provide details related to the construction and operation of the downstream infrastructure which will service these lands. The subject lands were previously Site Plan Approved (circa 2014), and subsequently severed for the Microtel Hotel. The public road portion of the original Site Plan Application (Country Glen Way), has been constructed and is in service.

This report was prepared in accordance with the Servicing Study Guidelines for Development Applications in the City of Ottawa. **Appendix A** contains a customized copy of the City's checklist which can be used as a quick reference for the location within this study report of each of the checklist items.

1.2 Background

In 2002, the City of Ottawa expanded its urban area to include the lands currently known as Kanata West. In March 2003, the Ottawa City Council approved the general land use and development principles of the Kanata West Concept Plan (KWCP). The plan is a mixed-use community with a population of about 17,000 persons in 6,300 households, 24,000 jobs and approximately 1 million square meters of commercial space. After approval of the KWCP, several supporting technical documents, including the Kanata West Master Servicing Study (KWSS), were prepared. The KWSS provided a master servicing plan for the entire KWCP, including major infrastructure such as water supply, wastewater disposal and stormwater management.

As mentioned, the site was previously Site Plan Approved (D07-12-14-0014). IBI Group (now Arcadis) prepared the Site Servicing Brief and Engineering Drawings to support the original SPA. The approval has since lapsed. This report aims to follow the principles established in the original site plan approval and engineering drawings, and provide adjustments to suit the new severance.

1.3 Subject Site

The Arcadia Commercial Site is located at 370 Huntmar Road, at the East intersection of Campeau Drive and Huntmar Drive in Ottawa, to the northeast of Tanger Outlets, and is part of the Kanata West Business Park

(KWBP). The KWBP is proposed to include several types of non-residential uses including Prestige Business Park, High Profile Employment and Extensive Employment.

The subject site severance is approximately 0.46 ha and consists of a two-storey Office and Showroom building as a small phase of a larger future commercial development.

Refer to Figure 1, below, for more information regarding the site location.



Figure 1 Subject Site Location

The site's natural topography, with the existing grade sloping from west to east, the proposed concept aims to seamlessly integrate the proposed two-storey building into the existing natural slope while taking the future design of the more significant commercial site into consideration to ensure there are no potential conflicts with future work. The building's facades will be maintained at an accessible grade to permit entry into the main levels of the building.

The primary vehicular and pedestrian access to the site is located off Campeau Drive and provides unimpeded access to the site office through a parking area to the South of the building. Two entrances with pedestrian access will be provided to the north of the building.

This project will consist of the construction of a two-storey office and showroom building. The site will also contain vehicular access routes for future commercial area, dedicated parking spaces, Tactile Walking Surface Indicators (TWSI) and landscaping areas. A site plan of the proposed development is included in **Appendix A**.

1.4 **Previous Studies**

1. Kanata West Concept Plan

The Kanata West Concept Plan (KWCP) was approved by the City of Ottawa in 2003. The plan provides a framework for the current and future development of the Kanata West lands. It also provides the guidelines and requirements for concept planning, the recommended concept plan, and an implementation strategy. The plan focuses on development of the urban lands with mix uses including office, housing, retail, institutional, entertainment and leisure activities.

2. Kanata West Servicing Study

The Kanata West Servicing Study (KWSS) was completed by the City of Ottawa in 2006. That study provided detailed guidelines for provision of major municipal infrastructure in support of the Kanata West Concept Plan. Among other things it provided guidelines and criteria for water supply, wastewater collection and stormwater management.

3. Third Party Review

The Third Party Review (TPR) was completed after potential omissions in the stormwater management model for KWSS were identified. The TPR was commissioned to be an arm's length review of the model to ensure that it was property calibrated and validated.

4. Signature Ridge Pump Station Hydraulic Grade Line Analysis

A March 2012 report by IBI Group was completed for Minto Properties and completed an update to the Signature Ridge Pump Station sanitary hydraulics. The report predicted HGL's for several scenarios for the tributary sewers including the sanitary sewer servicing the subject parcel. The HGL analysis was further refined in September 2012 based on current overflow proposals by the City.

5. Implementation Plan – Kanata West Development Area

This Plan was prepared for the City of Ottawa and the Kanata West Land Owners Group. The Implementation Plan recognizes that Kanata West is a large planning area which will take years to fully develop and therefore includes a mixture of short and long-term development plans and the associated infrastructure requirements to support them. The Plan builds on the framework of the KWCP and KWSS and provides updated comments for future approvals and the actions that would bring about the approval requirements. The Plan further reviews actions that would be conducted if "triggered" by an event or set of circumstances, while allowing sufficient flexibility to ensure that appropriate changes to the undertaking(s), once identified, are made.

6. Conceptual Site Servicing Arcadia Stages 1, 2, 5 & 8 Kanata West – Minto Communities

This IBI Group report, completed in September 2012, provided a high-level conceptual site servicing plan specifically for Minto Arcadia Lands, including the subject site which is Stage 5 of the report. The report focused on details related to water supply, wastewater disposal and stormwater management.

7. Arcadia Interim Stormwater Management Facility Design Brief June 2012

This IBI Group report outlines the design of the interim SWM Facility to service Minto's Arcadia development lands, including these commercial lands, until such time as the ultimate stormwater management facility is constructed.

8. Arcadia Commercial, 370 Huntmar Drive Design Brief October 2014

This IBI Group report provides a detailed servicing scheme to support the development of the Arcadia commercial site.

An engineering pre-consultation with the City of Ottawa was held in August, 2024 regarding the proposed development. Notes from this meeting are included in **Appendix A**.

1.5 Geotechnical Considerations

Paterson Group Inc. was retained to prepare a geotechnical investigation for the site. The objectives of the investigation were to prepare a report to:

www.arcadis.com

https://arcadiso365.sharepoint.com/sites/Projects5/147391/Internal Documents/6.0_Technical/6.04_Civil/03_Reports/Submission No. 3/CTR_Arcadia-Comm_Design_Brief_2025-03-05.docx

- Determine the subsoil and groundwater conditions at the site by means of boreholes
- To provide geotechnical recommendations pertaining to the design of the proposed development including construction considerations

The geotechnical investigation report PG7168-LET.01 Rev 2 Dated December 19, 2024 confirmed that the site consists of thick layer of silty clay underlain by glacial till overlying the bedrock surface. Based on the presence of the silty clay layer, a varying permissible grade raise plan was provided. The permissible grade raise of 2.0m is recommended for grading within 5m of the proposed buildings and 3.0m grade raise for the parking areas and access lanes.

The report contains recommendations which include but are not limited to the following:

- Fill used for grading beneath the proposed development to meet OPSS Granular 'A' or Granular 'B' Type II placed in lifts no greater than 300 mm compacted to 98% SPMDD
- Pavement Structures as identified below:

Table 1-1 Pavement Structure – Car Only Parking Areas

Local Road – Parking Areas	Thickness
12.5 Asphaltic Concrete	50 mm
OPSS Granular A Base	150 mm
OPSS Granular B Type II Subbase	300 mm

Table 1-2 Pavement Structure – Heavy Truck Parking Areas and Access Lanes

Local Road	Thickness
12.5 Asphaltic Concrete	40 mm
19.0 Asphaltic Concrete	50 mm
OPSS Granular A Base	150 mm
OPSS Granular B Type II Subbase	400 mm

The report contains recommendations which include but are not limited to the following:

- Pipe bedding and cover: The pipe bedding for sewer and water pipes should consist of at least 150 mm of OPSS Granular A crushed stone. The material should be placed in maximum 225 mm thick lifts and compacted to a minimum of 99% of its SPMDD. The cover material, which should consist of OPSS Granular A, should extend from the spring line of the pipe to at least 300 mm above the obvert of the pipe.
- The excavation side slopes above the groundwater level extending to a maximum depth of 3 m should be cut back at 1H:1V or flatter. The flatter slope is required for excavation below groundwater level.

2 Water Supply

2.1 Existing Conditions

As previously noted, the 0.46 ha office and showroom building site is surrounded by Huntmar Drive to the southwest, Campeau Drive to the northwest, and undeveloped land in the remaining surrounding area. An existing PVC 203 mm diameter watermain stub from Campeau Drive was previously installed and is located at the property line to the proposed site. This watermain falls within the City of Ottawa's pressure district Pressure Zone 3W which will provide the water supply to the site.

2.2 Design Criteria

2.2.1 Water Demands

Water demands have been calculated for this proposed site. This site consists of a two-storey office and showroom building. Siamese connections will be provided for this building. Consumption rates are taken from Tables 4.1 and 4.2 at the Ottawa Design Guidelines – Water Distribution and are summarized as follows:

•	Commercial Shopping Center	2500 l/1000m²/day
•	Other Commercial	28,000 l/gross ha/day
•	ICI Average Day Demand	28,000 l/gross ha/day
•	ICI peak Daily Demand	42,000 l/gross ha/day
•	ICI Peak Hour Demand	75,600 l/gross ha/day

A watermain demand calculation sheet is included in **Appendix B** and the total water demands are summarized as follows:

•	Average Day	0.03 l/s
•	Maximum Day	0.04 l/s
•	Peak Hour	0.07 l/s

2.2.2 System Pressure

The Ottawa Design Guidelines – Water Distribution (WDG001), July 2010, City of Ottawa, Clause 4.2.2 states that the preferred practice for design of a new distribution system is to have normal operating pressures range between 345 kPa (50 psi) and 480 kPa (80 psi) under maximum daily flow conditions. Other pressure criteria identified in Clause 4.2.2 of the guidelines are as follows:

Minimum Pressure	Minimum system pressure under peak hour demand conditions shall not be less than 276 kPa (40 psi)
Fire Flow	During the period of maximum day demand, the system pressure shall not be less than 140 kPa (20 psi) during a fire flow event.
Maximum Pressure	In accordance with the Ontario Building/Plumbing Code, the maximum pressure should not exceed 552 kPa (80 psi). Pressure reduction controls will be required

for buildings where it is not possible/feasible to maintain the system pressure below 552 kPa.

2.2.3 Fire Flow Rates

The proposed site plan contains one commercial building, with automatic sprinkler systems. The building will fall under OBC Section 3.10, F-2 or F3 occupancy and combustibility. The sprinkler system will be designed and installed in accordance with NFPA-13 requirements. The sprinkler system will be supplied from the city water connection and the demand will be calculated using the hazard classification plus the appropriate inside/outside hose allowances.

Calculations using the Fire Underwriting Survey (FUS version 2020) were conducted to determine the fire flow requirement for the site. Results of the analysis provides a maximum fire flow rate of 5,000 l/min or 83.3 l/s is required which is used in the hydraulic analysis. A copy of the FUS calculations is included in **Appendix B**.

2.2.4 Boundary Conditions

The City of Ottawa has provided the hydraulic boundary conditions at the site. A copy of the boundary conditions is included in **Appendix B** and summarized as follows:

Criteria	Hydraulic Head	Pressure
Max HGL (Basic Day)	160.7 m	88.8 psi
Peak Hour	156.5 m	82.8 psi
Max Day + Fire Flow (5,000 L/m)	155.4 m	81.2 psi

Table 2-1 Hydraulic Boundary Conditions

Ground elevation: 127.5 m

2.2.5 Hydraulic Model

A computer model for the subject site has been developed using the InfoWater Pro program by Autodesk. The model includes the existing watermain and boundary condition at Campeau Drive.

2.3 Proposed Water Plan

2.3.1 Proposed Water Plan

This site will be serviced by connecting to an existing 200mm diameter watermain extending from Campeau Drive. The building will be serviced by a lateral service connection from the proposed watermain. There is one hydrant proposed on site located at the east side of the proposed parking area, within 45m of the proposed building.

Refer to the general plan of services Drawing C-001 for detailed watermain layout for the subject site.

2.3.2 Hydraulic Analysis

The hydraulic model was run under basic day conditions to determine the maximum pressure for the site. The minimum pressure for the site is determined in the peak hour analysis using the provided boundary condition. Results of the analysis for the site are summarized in Section 2.3.2 and the water model schematic and model results are included in **Appendix B**.

2.3.3 Modeling Results

The hydraulic model was run under basic day, maximum day with fire flows and under peak hour conditions. Results of the hydraulic model are included in **Appendix B** and summarized as follows:

•	Basic Day (Max HGL) Pressure Range (kPa)	608.24 - 611.96
•	Peak Hour (Min HGL) Pressure Range (kPa)	553.36 - 557.09
•	Fire Flow @ 5,000 L/min Residual Pressure (kPa)	514.42
•	Residual Pressure @ 140 kPa Available Fire Flow (I/s)	283.83

A comparison of the results and design criteria is summarized as follows:

Maximum Pressure	All nodes in basic day scenario exceed 552 kPa (80 psi), therefore pressure reducing control is required for the proposed building in this development.
Minimum Pressure	All nodes in the model exceed the minimum value of 276 kPa (40 psi).
Fire Flow	The minimum design fire flow under maximum day conditions with minimum system pressure of 140 kPa is 283.83 l/s for retail which exceeds the requirement of 83.3 l/s (5,000 l/min) from Section 2.3.3.

3 Wastewater Disposal

3.1 Existing Conditions

There is an existing 375mm diameter sanitary sewer along Campeau Drive, which flows east along Campeau Drive and flows ultimately to the Ottawa Wastewater Treatment Plant at 395 Terry Fox Drive. There is an existing 200mm sanitary cap from existing MH301 to the property line in anticipation of this development. This sewer has been designed to provide wastewater service to the subject development site.

3.2 Previous Studies

The October, 2014 IBI Group Design Brief for Arcadia Commercial provided the wastewater servicing plan for the Arcadia Retail Development, including the subject site. The detailed sanitary sewer design sheets and related sanitary drainage area plan 35355 - C-501 are included in **Appendix C**.

3.3 Design Criteria

The sanitary sewers for the subject site will be based on the City of Ottawa design criteria. It should be noted that the sanitary sewer design for this study incorporates the latest City of Ottawa design parameters identified in Technical Bulletin ISTB-2018-01. Some of the key criteria will include the following:

Average commercial flow = 28,000 l/s/ha
Peak ICI flow factor = 1.5 if ICI area is > 20% total area 1.0 if ICI area is ≤ 20% total area = 0.33 l/s/ha
Inflow and Infiltration Rate = 0.33 l/s/ha
Minimum Full Flow Velocity = 0.60 m/s
Maximum Full Flow Velocity = 3.0 m/s
Minimum Pipe Size = 200 mm diameter

3.4 Recommended Wastewater Plan

The on-site sanitary system will consist of 200mm PVC sewer installed at standard depth and slope and will provide 150mm service connections to the proposed building. The sewers have been designed using the criteria noted above in section 3.2 and outlet via the existing sanitary stub connection to the sanitary sewer to Campeau Drive.

As noted in the pre-consultation meeting with the City of Ottawa, a monitoring maintenance hole was included just inside the property line of the subject site. The July 2012 Site Servicing Report 'Arcadia – Kanata West Ph 1' by IBI Group identified conceptually the servicing for the 9.84 Ha parcel of land south of Campeau Drive. This site comprises approximately 1.79 Ha of that area. The Campeau Drive sewer was designed and constructed assuming 0.85 Ha of commercial lands connecting to MH301A, with peak flows of 0.98 l/s. This site generates approximately 1.47 l/s to MH 301A. The minor (0.49 l/s) increase in flow to MH 301A has negligible impact on the system as it has over 34 l/s spare capacity up to MH 303A.

This site is comprised of slab on grade construction (no basements). The minor (0.49 l/s) increase in flow from MH 301A to 303A will not negatively impact this site. Sanitary design sheet from 'Arcadia – Kanata West Ph 1' site servicing report, which demonstrates the capacity in the receiving and downstream wastewater system is included in **Appendix C**.

As identified in the Arcadia Commercial Design Brief, there are existing houses along Campeau Drive and the current freeboard between the HGL and USF is approximately 1.18 m at MH301A. It is anticipated that any minor HGL adjustment (1 to 2 cm) due to the 0.49 l/s increase at this MH will leave these units within excess of 1 m of freeboard.

A copy of the sanitary sewer design sheet can be found in **Appendix C**. Please refer to the General Plan of Services **Drawing C-001** for further details.

4 Site Stormwater Management

4.1 Existing Conditions

The undeveloped subject lands currently drain east away from Campeau Drive and Huntmar Drive intersection to the recently developed Country Glen Way. There is an existing 825mm diameter downstream storm sewer along Campeau Drive with a 600mm storm stub from the existing MH301 to the property line with an allocation of flows from this development previously taken into consideration.

The Arcadia Commercial Site Plan was allocated a total 100-year release rate of 240L/s/Ha. The original site plan approval included two separate outlets, one to Campeau Drive and one to Country Glen Way. Based on the original site area draining to Campeau, of 0.8Ha, the theoretical maximum release rate is 192.00L/s. However, the site stormwater management plan identified a release rate to Outlet #2 (MH 301 in Campeau Drive) of **125.94 L/s**. This report aims to meet the more restrictive target to MH301 established in the Site Plan. An excerpt from the Arcadia Commercial Stormwater Management Calculations has been provided in **Appendix D**.

4.2 Design Criteria

The stormwater system was designed following the principles of dual drainage, making accommodations for both major and minor flow. The on-site minor system design criteria identified below are consistent with the current City of Ottawa Sewer Design Guidelines.

Some of the key criteria include the following:

•	Design Storm	1:2year return (Ottawa)
•	Rational Method Sewer Sizing	
•	Initial Time of Concentration	10 minutes
•	Runoff Coefficients	
	 Landscaped Areas 	C = 0.20
	 Asphalt/Concrete 	C = 0.90
	– Roof	C = 0.90
•	Pipe Velocities	0.80 m/s to 6.0 m/s
•	Minimum Pipe Size	250 mm diameter
		(200 mm CB Leads)

4.3 Proposed Minor System

Where possible, the minor system storm sewers for the subject site will be sized based on the rational method and the City of Ottawa 2-year event. Minor storm flow to the downstream storm sewer network will be controlled by Inlet Control Devices (ICDs) to limit flow and prevent sewer surcharging downstream.

Due to the severance area and the need to maintain maximum flexibility for future development opportunities within the existing site, a rebalancing of tributary areas to Campeau has been completed. General Areas 122, 123, 110A and Roof Areas BLK700 and BLK800 (as identified on the original site plan) have been removed from the tributary outletting to Campeau. The sum of the areas removed from Outlet #2 is 0.30Ha. This has permitted an expansion

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https://arcadiso365.sharepoint.com/sites/Projects5/147391/Internal Documents/6.0_Technical/6.04_civil/03_Reports/Submission No. 3/CTR_Arcadia-Comm_Design_Brief_2025-03-05.docx

of the parking lot area adjacent to the proposed sales Center drain into the Campeau outlet without constructing services through the remainder of the site, as originally intended. The sum of the area added to Outlet #2 is 0.23Ha. An overall drainage area plan has been provided in **Appendix D** which demonstrates the areas removed (in red) and the areas added (in green).

The proposed minor storm sewer will range between 300 mm diameter and 600 mm diameter. Catch basin lead pipes will be 200 mm in diameter. The minor storm sewer outlet will be via the 600 mm diameter pipe which is proposed to connect to the existing 825 mm diameter storm sewer in Campeau Drive.

An allocation has been provided in the minor system for future flows to the east. This includes Future Building Block 600 and future parking lot area 120, as were identified on the original site plan approval.

A detailed storm sewer design sheet and the associated storm sewer drainage area plan is included in **Appendix D**. The General Plan of Services, depicting all on-site storm sewers can be found in **Appendix A**.

4.4 Stormwater Management

As previously noted, the overall site release rate was determined based on a level of service of 240 L/s/Ha. However, the original SWM concept for the approved site plan had adjusted the overall release rate between the two outlets, and Outlet #2 (MH301 to Campeau) is slightly overcontrolled relative to the level of service for the whole site. The intent is to maintain the outlet dispersion with **125.94 L/s** as the maximum permissible release rate to Campeau.

At certain locations within the site, the opportunity to capture and/or store runoff is limited due to grading constraints and site plan geometry. These locations are generally located at the site's perimeter, where it is necessary to tie into public ROWs and adjacent properties or in areas where ponding stormwater is undesirable. These "uncontrolled" areas – 0.064 hectares in total, have a C value of 0.20 and increased by 25% during 100-year events (as per City SDG). It should be noted that the total uncontrolled areas are based on the uncontrolled areas identified in the original site plan SWM concept and are all located adjacent to future development areas. All areas within the severed parcel are captured and controlled.

4.5 Inlet Control

Per the original stormwater management calculations provided for the entire site, the restricted flow rate was used for the Campeau outlet is:

Qrestricted = 125.94 L/s

As noted in Section 4.4, a small, landscaped area along the west property line will drain offsite uncontrolled.

Based on a 100-year event, the flow from the 0.063 Ha uncontrolled area UNC1 can be determined as:

Quncontrolled	= 2.78 x C x i _{100yr} x A where:
С	= Average runoff coefficient of uncontrolled area = 0.20 x 1.25
İ _{100yr}	= Intensity of 100-year storm event (mm/hr)
	= 1735.688 x (T _c + 6.014) ^{0.820} = 178.56 mm/hr; where T _c = 10 minutes
Α	= Uncontrolled Area = 0.063 Ha

Therefore, the uncontrolled release rate can be determined as:

 $Q_{uncontrolled} = 2.78 \times 1.25C \times i_{100yr} \times A$ $= 2.78 \times 1.25 \times 0.020 \times 178.56 \times 0.063$ = 7.82 L/s

The higher roof top area of 0.027 ha will be uncontrolled due to difficulty of maintenance. The total flow from the uncontrolled roof area UNC2 can be determined as:

$$\begin{aligned} \mathbf{Q}_{uncontrolled} &= \mathbf{2.78} \times \mathbf{1.25C} \times \mathbf{i}_{100yr} \times \mathbf{A} \\ &= 2.78 \times 1.0 \times 178.56 \times 0.0269 \\ &= \mathbf{13.35} \text{ L/s} \end{aligned}$$

The maximum allowable release rate to Campeau Drive (Outlet #2/MH301) can then be determined as:

Q_{max allowable} = Q_{restricted} - Q_{uncontrolled} = 125.94 L/s - 7.82 L/s - 13.35 L/s = 104.77 L/s

Based on the flow allowance at the various inlet locations, various sizes of inlet control devices (ICDs) were chosen in the design. The design of the inlet control devices is unique to each drainage area and is determined based on various factors, including hydraulic head and allowable release rate. Ponding locations and elevations are summarized on the Ponding Plan **Drawing C-600**, and included in **Appendix D**.

4.6 **On-Site Detention**

The site was designed to limit runoff to the allowable release rate up to the 2-year post-development storm event. Flows exceeding the maximum allowable release rate will be contained on-site via underground and surface storage at strategic locations. Orifices are proposed in manholes, catch basins and roof drains to control runoff from the site. The modified rational method determined the storage volumes during a 2-year and 100-year storm event. Available surface ponding volumes at each inlet were determined using CAD surface volume tools. As per the Ottawa SDG, when underground storage is considered available storage, the ICD release rate is to be reduced by 50% to determine the storage requirements.

The proposed roof is partially flat and partially peaked. The drainage area plan considers the roof structure of this building. The flat roof area has accounted for ponding storage with depths not exceeding 150mm per the OBC, and there are five roof drains. Watts roof drain flow control weirs are proposed on each inlet, set to 2 L/s or 30GPM each.

Major flow up to the 100-year storm is contained on-site and is gradually released to the minor system. Apart from the small uncontrolled areas, major flow does not leave the site via overland flow.

The site's stormwater management has ensured that surface ponding will not occur during the 2-year storm event.

Stormwater management and on-site underground storage volume calculations, and manufacturers spec sheets are included in **Appendix D**.

A summary of the ICD type for each drainage area and corresponding storage details is provided in Table 4.1 below.

Table 4-1 Post-Development Storage Summary Table

Location	ІСД Туре	Drainage Area (Ha)	Restricted / Uncontrolled Flow (L/s)	Storage Required (m³)	Storage Provided (m ³)		
			2 - Year	2 - Year	Surface	UGS	Total
Controlled S	torm Sewer S	ystem					
FUT 600	-	0.06	2	7.22	33.75	0	33.75
FUT 120	-	0.11	15	4.18	33.99	0	33.99
ROOF	WATTS	0.07	10	2.38	18.15	0	18.15
110	IPEX MHF	0.12	28	0	8.49	0	8.49
102	IPEX MHF	0.24	25	20.49	25.20	68.80	94.00
MH100B	IPEX MHF	0.04	24	0	1.57	0	1.57
Total		0.64	104	34.27	121.15	68.80	189.95

The area Future 120 has identified surface level ponding during the 2-year event. The drainage area and release rate have been carried form the original site plan SWM concept. Future site plan development will need to address 2-year ponding in this area.

Area 102 identifies a 20.49m3 storage required during the 2-year event. 68.80m3 of storage is provided underground, therefore there will be no surface ponding during the 2-year event.

4.7 100-Year Overflow

A review of the 100-year event, and overflow depth has been performed using the modified rational method. The calculations are included in the modified rational stormwater management sheets **Appendix D**.

A summary of the required storage volumes and overflow balances is provided below.

Drainage Area	ICD Restricted Flow (L/s)	100 Year Storage Required (m³)	Total Storage Provided* (m3)	Upsteam Overflow (m³)	100 – Year Overflow (m³)
FUT 600	2	26.48	33.75	0	0

Drainage Area	ICD Restricted Flow (L/s)	100 Year Storage Required (m³)	Total Storage Provided* (m3)	Upsteam Overflow (m³)	100 – Year Overflow (m³)
FUT 120	15	26.10	33.99	0	0
ROOF	10	15.64	18.15	0	0
110	28	7.96	8.49	0	0
102	25	90.65	94.00	0	0
MH100B	24	1.41	1.57	0	0
Total	104	168.23	189.95	0	0

*includes surface storage and underground storage. For building Areas, it includes rooftop storage.

The 100-year flow from all areas within the proposed site plan is contained on-site, with no overland flow offsite or to other areas.

4.8 100-Year + 20% Stress Test

A cursory review of the 100-year event + 20% has been performed using the modified rational method. The peak flow from each area during a 100-year event has increased by 20%. The calculations have been included in **Appendix D.**

A summary of the require storage volumes, and overflow balances is provided below.

Table 4-3 Post-Development 100yr+20% Stress Test Storage Summary Table

Drainage Area	ICD Restricted Flow (L/s)	100 Year + 20% Storage Required (m ³)	Total Storage Provided	Upsteam Overflow (m³)	100 Year + 20% Overflow (m³)
FUT 600	2	33.48	33.75	0	0
FUT 120	15	34.56	33.99	0	0.57
ROOF	10	20.80	18.15	0	2.65
110	28	11.57	8.49	0	3.08
102	25	115.68	94.00	2.65	24.33
MH100B	24	2.55	1.57	0.57	1.55
Total	104		189.95		

The overland flow from 110 is directed to Campeau Drive. The 100yr +20% overflow volume from Area 110 is **3.08** m3 at peak. Based on a peak Tc of 6 minutes, the volume can be reverse calculated to **8.55** L/s. A channel depth

conveyance calculation has been provided to determine the overflow depth of **0.02m** above the static ponding elevation.

The overland flow from the area tributary to 102 is directed south to future development lands. The 100yr +20% overflow volume from Area 102, including upstream roof contribution (2.65 m3), is **24.33** m3 at peak. Based on a peak Tc of 46 minutes, this volume can be reverse calculated to **8.82** L/s. A channel depth conveyance calculation has been provided to determine the overflow depth of **0.03m** above static ponding elevation. These stress test flows will need to be considered in future SWM analysis.

The overland flow from the area tributary to MH100B is directed to Campeau Drive. The volume of overflow from MH100B is **1.55**m3 at peak. Based on a peak Tc of 3 minutes, this volume can be reverse calculated to **8.62 L/s**. A channel depth conveyance calculation has been provided to determine the overflow depth of **0.04m** above static ponding elevation.

4.9 Underground Storage

Due to the site's constraints and the stormwater management plan, underground storage was deemed the best option to contain the 100-year storm event on site. The table below summarizes underground storage, and additional information about the underground storage structures is found in **Appendix D**.

Table 4-3 Underground Storage Summary Table

Storage Name	Structure Type	Storage Provided (m ³)
CB102	Stormtech DC-780 or approved equivalent	68.80

4.10 Quality Control

www.arcadis.com

As noted in the Arcadia Commercial Design Brief, flows from the subject site discharged into the Arcadia Interim SWM facility, which provided an interim quality and quantity control facility for the Arcadia community. We understand that the ultimate SWM facility has been constructed and is operational.

4.11 Hydraulic Grade Line

As identified in the Arcadia Commercial Design Brief, as part of the original site plan approval, the storm Hydraulic Grading Line (HGL) is dictated by downstream infrastructure. The storm HGL within the existing storm sewer on Campeau Drive is at 96.05m at existing MH's 301. The sewers are not surcharged at these points, since the internal sewers are restricted to meet the downstream system design requirements and sized to accommodate the restricted flow. The onsite sewers will not be surcharged, and as such, the HGL will follow the obvert of the pipes. Additionally, this is a slab on grade development, and the City requirement for 0.3 m freeboard to USF to protect basements from flooding is not applicable. The minimum freeboard from the onsite HGL (obvert of storm sewer) to the finished floor elevation is 1.51 m.

5 Grading and Roads

5.1 Site Grading

The existing grades within portions of the proposed development lands vary significantly due to the existing topography of the site. The grading plan will require the balancing of various requirements including but not limited to geotechnical constraints, minimum/maximum slopes, overland routing of stormwater, all to ensure the site is graded following municipal and accessibility standards.

Special consideration is needed for the building, where elevated foundation walls are required along the west façade to maintain the grade. A minimum of 150mm foundation exposure is required around the perimeter of the building. Internal and external steps will also be required to match grades. The main entrance has been designed to provide barrier-free access to the parking areas.

The parking areas have been designed to meet accessibility requirements, with slopes ranging between 0.5% along curbs to a maximum of 5%.

Refer to the grading plan provided in Appendix E.

5.2 Road Network

No public roads are proposed through the site. A minimum 8.0m wide drive aisle has been provided, as shown on the Site Plan in **Appendix A.** An internal Fire route has been shown where fire truck access is required, as determined by the site architect.

There are 39 parking stalls provided on the site, of which two are barrier-free.

Pedestrian access facilities and multiple connections to Campeau Drive and Huntmar are provided.

A bicycle parking facility has been proposed adjacent to each building entrance.

Noise attenuation features and indoor noise clause provisions will not be required for commercial use lands for road noise generated by the adjacent roads.

6 Source Controls

6.1 General

Since an end-of-pipe treatment facility is already provided for the development lands, stormwater site management for the subject lands will focus on the site level or source control management of runoff. Such controls or mitigative measures are proposed for this development not only for final development but also during construction and build-out. Some of these measures are:

- Flat site grading where possible
- Vegetation planting
- Groundwater recharge in landscaped areas

6.2 Lot Grading

Where possible, all of the proposed blocks within the development will make use of gentle surface slopes on hard surfaces such as asphalt and concrete. In accordance with local municipal standards, all grading will be between 0.5 and 5.0 percent for hard surfaces and 2.0 and 7.0 percent for all landscaped areas. Significant grade changes will be accomplished through the use of terracing (3:1 max slope), ramps and/or retaining walls. All street and parking lot catchbasins shall be equipped with 3.0m subdrains on opposite sides of a curbside catchbasin running parallel to the curb, and with 3.0m subdrains extending out from all 4 sides of parking lot catchbasins.

6.3 Vegetation

As with most site plans, the developer will be required to complete a vegetation and planting program. Vegetation throughout the development including planting along roadsides and within the individual blocks provides opportunities to re-create lost vegetation.

6.4 Groundwater Recharge

Groundwater recharge targets have not been identified for this site. Perforated sub-drain systems will be implemented at capture locations in all vegetated areas. This will promote increased infiltration during low flow events before water is collected by the storm sewer system.

7 **Conveyance Controls**

7.1 Generals

Besides source controls, the development also proposes to use several conveyance control measures to improve runoff quality. These will include:

- Vegetated swales
- Catchbasin sumps and manhole sumps

7.2 Catchbasins and Maintenance Hole Sumps

All catchbasins within the development, either rear yard or street, will be constructed with minimum 600 mm deep sumps. These sumps trap pollutants, sand, grit and debris which can be mechanically removed prior to being flushed into the minor pipe system. Both rear yard and street catchbasins will be to OPSD 705.02. All storm sewer maintenance holes serving local sewers less than 900 mm diameter shall be constructed with a 300 mm sump as per City standards.

8 Sediment and Erosion Control Plan

8.1 General

During construction, existing stream and conveyance systems can be exposed to significant sediment loadings. Although construction is only a temporary situation, it is proposed to possibly introduce a number of mitigative construction techniques to reduce unnecessary construction sediment loadings. These may include:

- Until the local storm sewer is constructed, groundwater in construction trenches shall be pumped into a filter mechanism prior to release to the environment
- Vegetated swale sediment capture filter socks will remain on open surface structures such as maintenance holes and catchbasins until these structures are commissioned and put into use
- Silt fence on the site perimeter will be installed

8.2 Trench Dewatering

Any trench dewatering using pumps will be discharged into a filter trap made up of geotextile filters and straw bales similar in design to the OPSD 219.240 Dewatering Trap. These will be constructed in a bowl shape with the fabric forming the bottom and the straw bales forming the sides. Any pumped groundwater will be filtered prior to release to the existing surface runoff. The contractor will inspect and maintain the filters as needed, including sediment removal and disposal and material replacement as needed. It should be noted that that the contractor will be responsible for the design and management of the trap(s).

8.3 Seepage Barriers

In order to further reduce sediment loading to the stormwater management facility, seepage barriers will be installed on any surface water courses at appropriate locations that may become evident during construction. These barriers will be Light Duty Straw Bale Barriers per OPSD 219.100 and Heavy-Duty Silt Fence Barriers per OPSD 219.130; locations are shown on the Sediment and Erosion Control Plan included in **Appendix E**. They are typically made of layers of straw bales or geotextile fabric staked in place. All seepage barriers will be inspected and maintained as needed.

8.4 Surface Structure Filters

All catchbasins, and to a lesser degree, manholes, convey surface water to sewers. Until streets are asphalted and curbed, all catchbasins and manholes will be constructed with sediment capture inserts or equivalent located between the structure frame and cover. These will stay in place and be maintained during construction and build until it is appropriate to remove same.

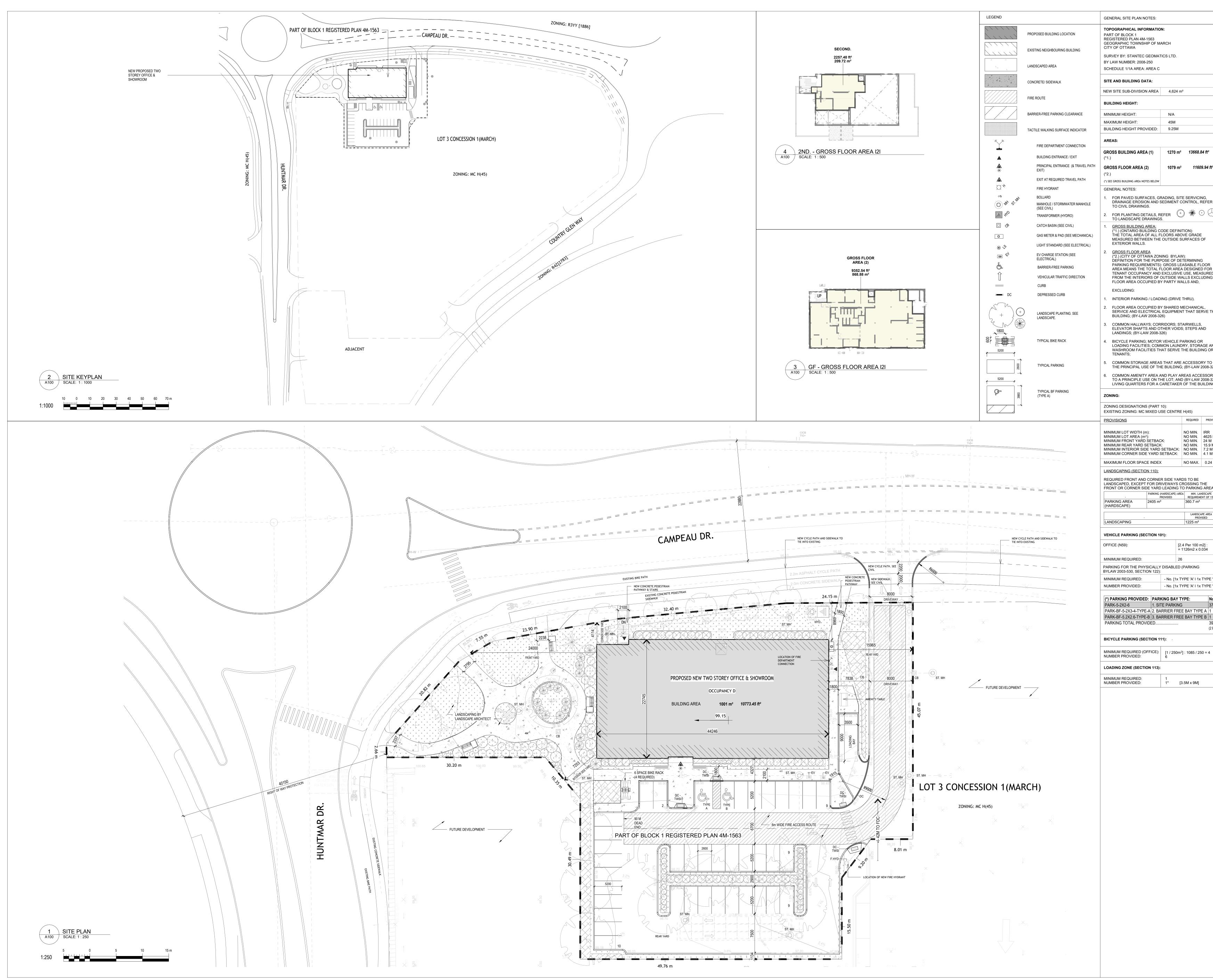
9 Conclusion

This report has illustrated that the proposed two-storey office and showroom development can be serviced via existing municipal services. The water network will be extended to provide necessary service. All sanitary and storm sewer designs for this development will be completed in conformance with City of Ottawa standards while acknowledging downstream constraints. By limiting flow into the minor storm sewer system as per the applicable local stormwater management criteria and allowing for excess surface storage on-site, all stormwater management requirements will be met. Adherence to the Sediment and Erosion Control Plan during construction will minimize harmful impacts on surface water.

Based on the information provided within this report, the plans prepared for the subject development can be serviced to meet City of Ottawa requirements.

Appendix A

Site Plan AOV Legal Plan Site Servicing Plan 147391-C-001 Arcadia Site Servicing Plan 35355-C-100 Pre-Consultation City Comments Study and Plan Identification List



	 GENERAL NOTES 1. DO NOT SCALE DRAWINGS; ONLY FIGURED ARE TO BE USED. WHERE DOUBT EXISTS; F FOR INTERPRETATION AND REQUEST CLAR 2. IT IS THE RESPONSIBILITY OF THE GENERAL CONTRACTOR TO VERIFY DIMENSIONS ON S DISCREPANCIES TO THE ARCHITECT PROMI 3. GENERAL CONTRACTOR TO TAKE INTO ACC CONSTRUCTION TOLERANCE; GENERAL CO TO COORDINATE THE WORK OF DIFFERENT COMPLY WITH DESIGN INTENT. 4. ALL WORK DESCRIBED IN THESE DRAWINGS SPECIFICATIONS ARE TO COMPLY WITH THE EDITION OF THE ONTARIO BUILDING CODE (NATIONAL BUILDING CODE (2010) INCLUDING RECENT AMENDMENTS. 	ILE REQUEST ITY. SITE; REPORT PTLY. COUNT NTRACTOR TRADES TO S AND E CURRENT 2012) OR G MOST
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	TEL: 613-691-0266 ELECTRICAL CONSULTA SMITH + ANDERSEN	NT
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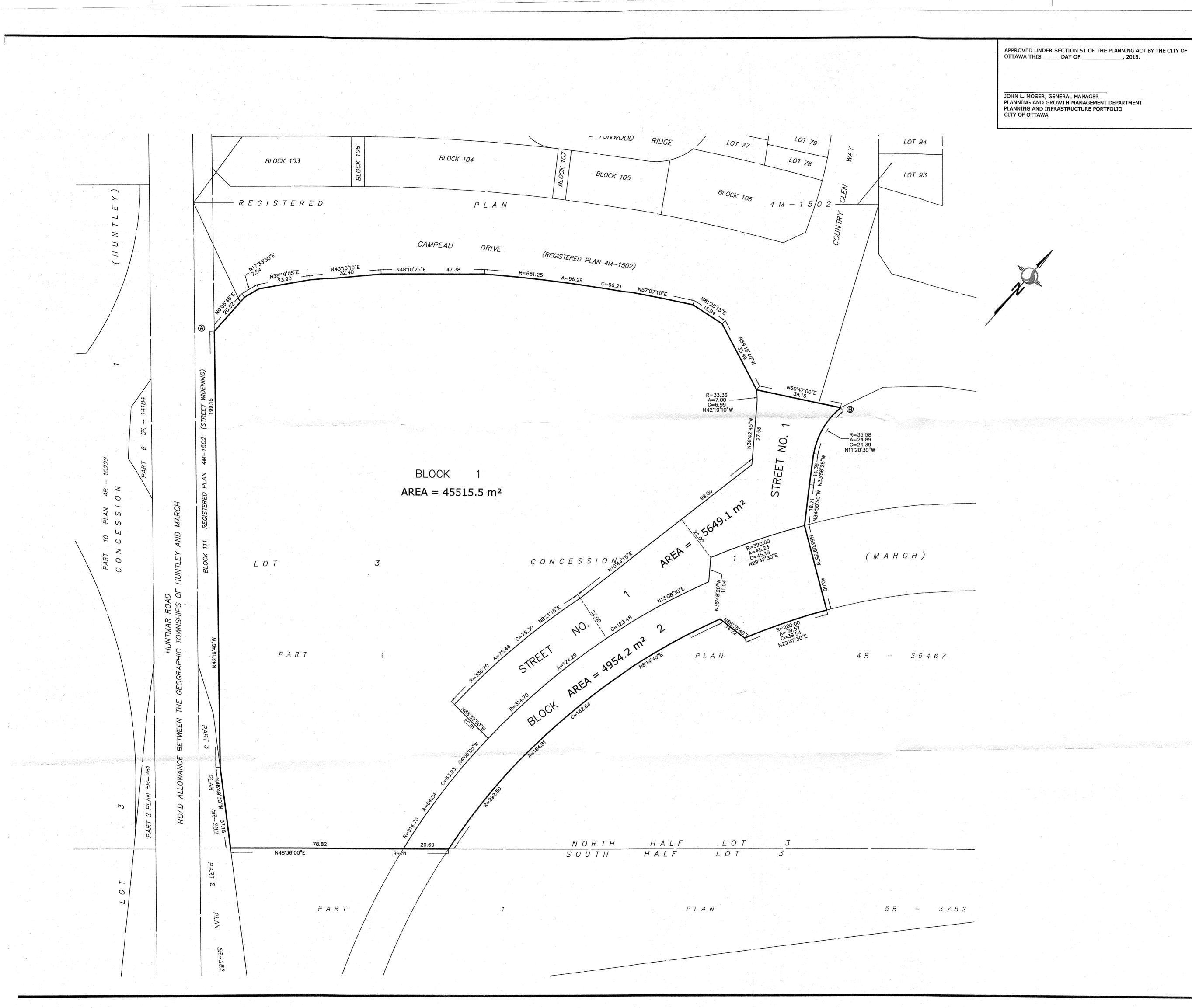
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CERTIFICATE OF REGISTRATION PLAN 4M-____

I CERTIFY THAT THIS PLAN IS REGISTERED IN THE LAND REGISTRY OFFICE FOR THE LAND TITLES DIVISION OF OTTAWA-CARLETON NO.4 AT___O'CLOCK ON THE _____ DAY OF , 2013 AND ENTERED IN THE PARCEL REGISTER FOR PROPERTY IDENTIFIER _____, AND THAT THE REQUIRED CONSENTS ARE REGISTERED AS

PLAN DOCUMENT NUMBER

REPRESENTATIVE FOR THE LAND REGISTRAR

THIS PLAN COMPRISES ALL THE LAND IDENTIFIED BY PIN XXXXX-XXXX.

PLAN OF SUBDIVISION of

PART OF LOT 3 **CONCESSION 1** GEOGRAPHIC TOWNSHIP OF MARCH CITY OF OTTAWA

Stantec Geomatics Ltd.

Scale 1:750

METRIC CONVERSION

DISTANCES AND COORDINATES SHOWN ON THIS PLAN ARE IN METRES AND CAN BE CONVERTED TO FEET BY DIVIDING BY 0.3048

GRID SCALE CONVERSION

DISTANCES ARE GROUND AND CAN BE CONVERTED TO GRID BY MULTIPLYING BY THE COMBINED SCALE FACTOR OF 0.999914.

BEARING NOTE

BEARINGS HEREON ARE GRID BEARINGS DERIVED FROM THE CAN-NET VRS NETWORK MONUMENT - OTTAWA - (N 5036741.327, E 327757.614) AND FITZROY (N 5036741.327, E 327757.614) AND ARE REFERRED TO THE CENTRAL MERIDIAN 76° 30' WEST LONGITUDE OF THE 3° MTM ONTARIO COORDINATE SYSTEM, NAD83 (CSRS) ZONE 9.

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COORDINATES CANNOT, IN THEMSELVES, BE USED TO RE-ESTABLISH CORNERS OR BOUNDARIES SHOWN ON THIS PLAN.			

SURVEYOR'S CERTIFICATE

I CERTIFY THAT :

- 1. THIS SURVEY AND PLAN ARE CORRECT AND IN ACCORDANCE WITH THE SURVEYS ACT, THE SURVEYORS ACT AND THE LAND TITLES ACT AND THE REGULATIONS MADE UNDER THEM.
- 2. THE SURVEY WAS COMPLETED ON THE _ _ DAY OF _ _ _ _ , 2013.

DATE	BRIAN J. WEBSTER ONTARIO LAND SURVEYOR
	UNTAKIO LAND SUKVETOK

OWNER'S CERTIFICATE

THIS IS TO CERTIFY THAT :

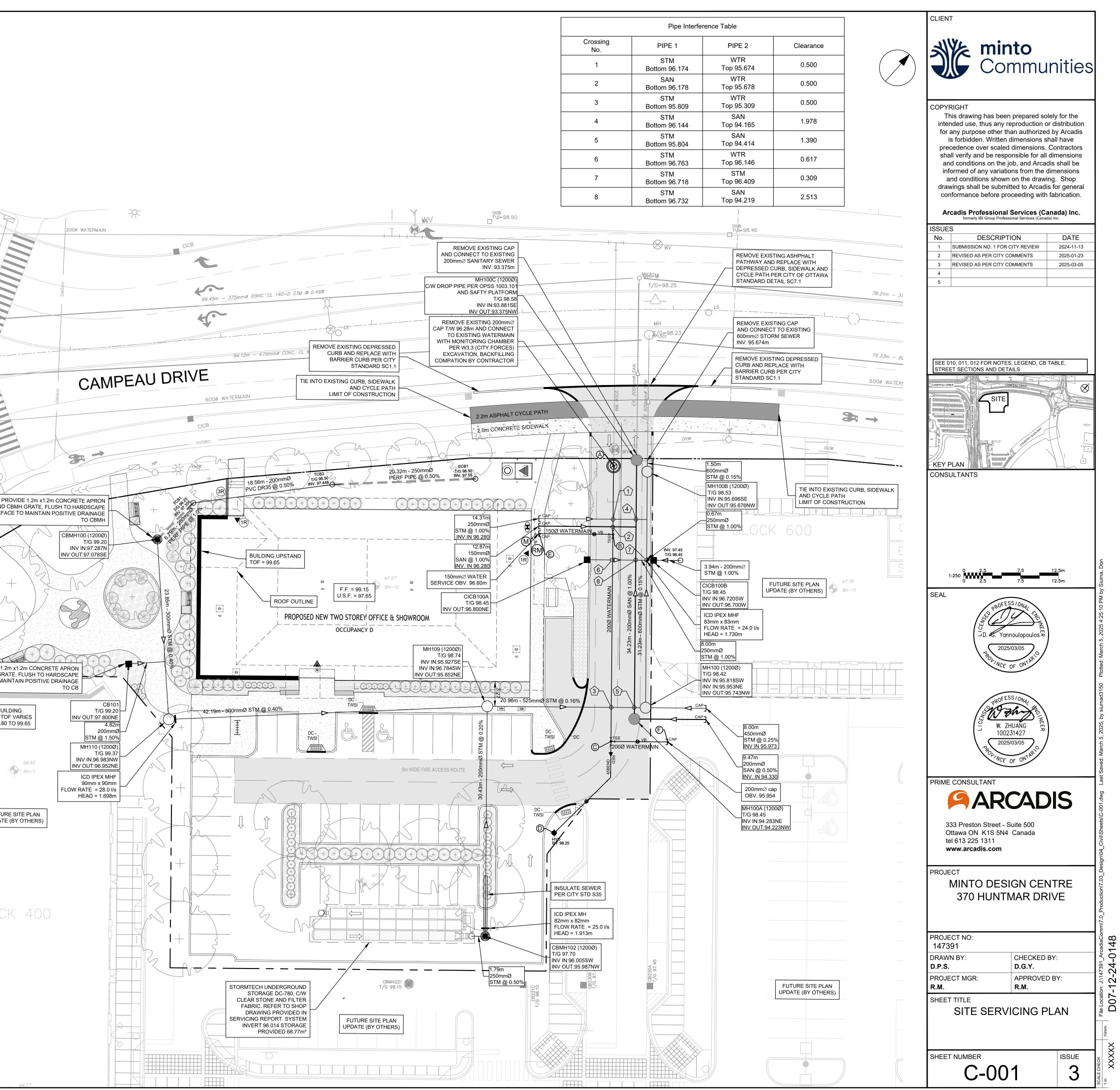
- 1. BLOCKS 1 AND 2 INCLUSIVE, THE STREET, NAMELY STREET NO. 1 HAVE BEEN LAID OUT IN ACCORDANCE WITH OUR INSTRUCTIONS.
- 2. THE STREET AND STREET WIDENING ARE DEDICATED AS PUBLIC HIGHWAYS.

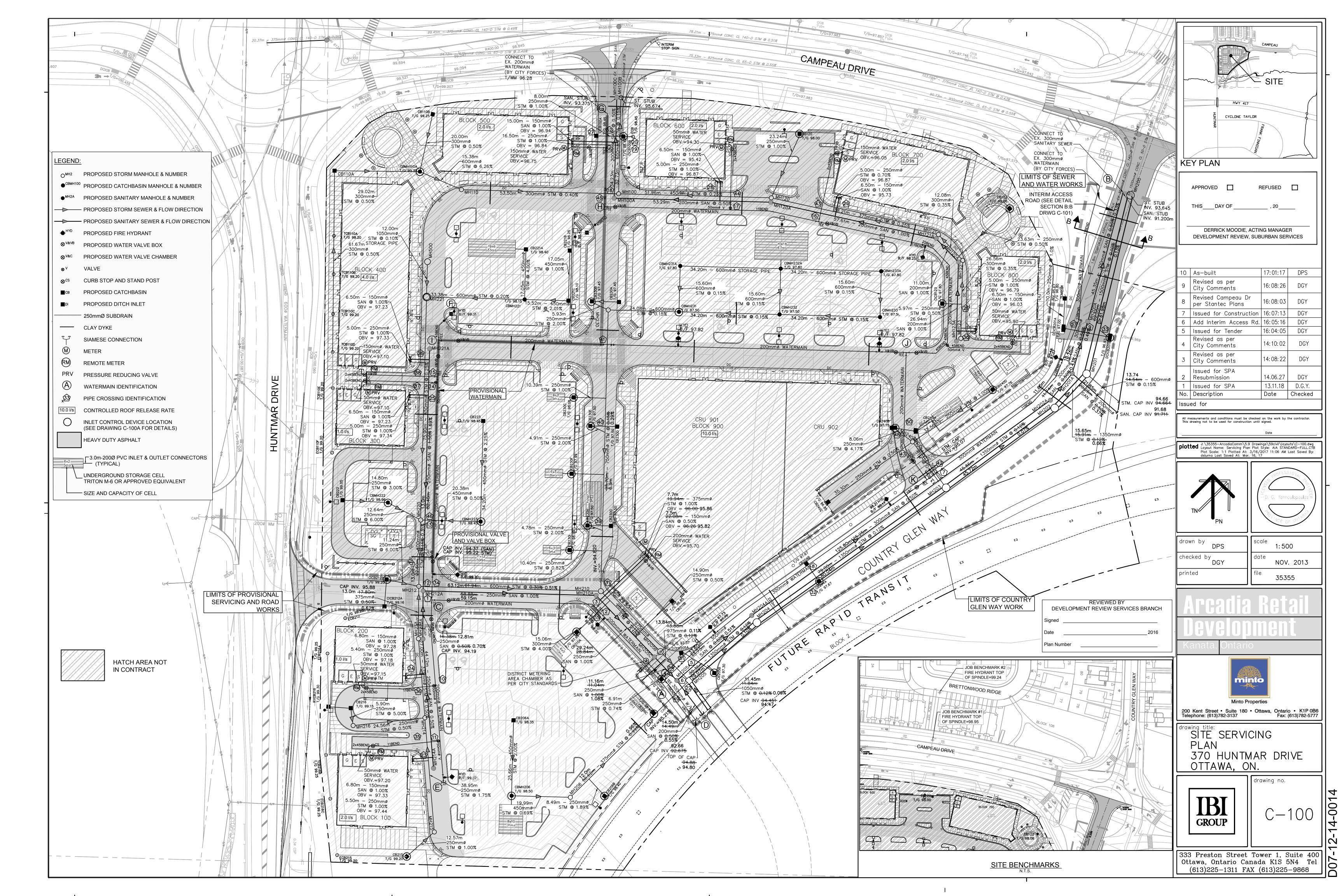
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Stantec Geomatics Ltd. Ontario Land Surveyors Canada Lands Surveyors 1331 CLYDE AVENUE, SUITE 400, OTTAWA, ON. K2C 3G4 PHONE (613)722-4420 FAX (613)722-0789 brian.webster@stantec.com Stantec stantec.com DRAWN BY:CEC CHECKED BY: * PM: BW FIELD: * PROJECT No.: 161613058-132

PLANNING AND INFRASTRUCTURE PORTFOLIO

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August 21, 2024

Kevin Harper Minto Communities Inc. Via email: <u>kharper@minto.com</u>

Subject: Pre-Consultation: Meeting Feedback Proposed Site Plan Control Application – 370 Huntmar Drive

Please find below information regarding next steps as well as consolidated comments from the above-noted pre-consultation meeting held on August 13, 2024.

Pre-Consultation Preliminary Assessment

1 🗆 2 🗆 3 🗆 4 🗆 5 🖂

One (1) indicates that considerable major revisions are required while five (5) suggests that the proposal appears to meet the City's key land use policies and guidelines. This assessment is purely advisory and does not consider technical aspects of the proposal or in any way guarantee application approval.

Next Steps

- 1. A review of the proposal and materials submitted for the above-noted preconsultation has been undertaken.
- 2. In your subsequent submission, please ensure that all comments or issues detailed herein are addressed. A detailed cover letter stating how each issue has been addressed must be included with the submission materials. Please coordinate the numbering of your responses within the cover letter with the comment number(s) herein.
- 3. Please note, if your development proposal changes significantly in scope, design, or density before the next submission, you may be requested to repeat the preconsultation process before filing an Official application.

Supporting Information and Material Requirements

- 1. The attached **Study and Plan Identification List** outlines the information and material that has been identified, during this phase of pre-consultation, as either required (R) or advised (A) as part of a future complete application submission.
 - a. The required plans and studies must meet the City's Terms of Reference (ToR) and/or Guidelines, as available on <u>Ottawa.ca</u>. These ToR and Guidelines outline



the specific requirements that must be met for each plan or study to be deemed adequate.

Consultation with Technical Agencies

1. You are encouraged to consult with technical agencies early in the development process and throughout the development of your project concept. A list of technical agencies and their contact information is enclosed.

<u>Planning</u>

Comments:

- 1. The following policies apply to the site:
 - a. The site is designated Minor Corridor on Schedule B5 Suburban (West) Transect.
 - b. Huntmar Drive and Campeau Drive are both identified as Arterial Roads on Schedule C4 – Urban Road Network.
 - c. The site is subject to Area-Specific Policy 2 Kanata West, per Annex 5 Urban and Rural aras Subject to Area-Specic Policies. Refer to Volume 2C for applicable policies.
- 2. It is understood that the owner no longer intends to proceed with the previously approved commercial development on the site (File No. D07-12-14-0014) has lapsed and the owner no longer intends to proceed.
 - a. Please ensure this is clear on any plans submitted in support of the proposed development. The current plans showing the proposal in the context of the previously approved development may be misleading to staff, technical agencies, public, etc. in future reviews.
 - b. Is there an intention to release the registered site plan agreement (Instrument No. OC1817302) on the subject site and surrounding lands?
- 3. Provide further details on the use(s) of the proposed building. Staff understand that there is an intention to have offices, a combined sales and design centre, as well as showroom space in the building. Zoning interpretation have confirmed that more information is required to confirm whether there is a "retail" component to the use.
- 4. Landscaping
 - a. Please ensure that the minimum landscaping requirements identified in Section 110(1) of the Zoning By-law are met. Please note that a landscaped



buffer with a minimum width of 1.5 metres must be provided between the permitter of the parking lot and a lot line not abutting a street, per Table 110(b). It appears that there are deficiencies along the west, south and east lot line.

- b. Consider opportunities for additional trees and landscaping in the development. It appears that parking is being provided above the minimum zoning requirements consider removing excess parking spaces to meet minimum landscaping buffer requirements and allow for the introduction of additional landscaped islands within the surface parking lot. Refer to Policy 11 of Section 4.1.4 of the Official Plan for additional direction on surface parking lot design.
- 5. Consider opportunities to visually screen the loading dock from the sightline of the front lot line. Policy 3 of Section 4.6.5 of the Official Plan directs development along corridors shall improve the attractiveness of the realm by internalizing loading areas and visually screening surface parking.
- 6. Explore opportunities to provide additional bicycle parking on-site to promote active transportation.
- 7. Required Applications
 - a. Site Plan Control (Standard) more information on the process can be found <u>here</u>.
 - b. If required, zoning relief can be sought through a Minor Variance or Minor Zoning By-law Amendment application.
 - i. Minor Variance more information on the process can be found <u>here</u>.
 - ii. Zoning By-law Amendment (Minor) more information on the process can be found <u>here</u>.
 - c. Consent for Severance more information on this process can be found <u>here</u>. Please continue to engage with <u>Elizabeth King</u>, Planner I (DRAW), on the proposed severance.

Feel free to contact Colette Gorni, Planner II (DR West), for follow-up questions.

<u>Urban Design</u>

Comments:

8. An Urban Design Brief is not required as the project ties into the larger approved Site Plan Control Application for the site.



- 9. Urban Design staff require an architectural package which includes a Site Plan and Building Elevations, as well as a Landscape Plan as part of the Applicant's submission.
- 10. Urban Design staff look forward to seeing the planting strategy and would encourage the Applicant to explore opportunities for tree planting.

Feel free to contact Kadri Nader (kadri.nader@ottawa.ca), Urban Design Planner, for follow-up questions.

Engineering

Comments:

- 11. Water Design
 - a. A water boundary condition request should be made for this development. Please provide the following information including supporting calculations:
 - i. Location of service
 - ii. Type of development
 - iii. Amount of fire flow required.
 - iv. Average daily demand: _____ l/s.
 - v. Maximum daily demand: ____l/s.
 - vi. Maximum hourly daily demand: ____ l/s.
 - b. A 203mm PVC watermain is available at the site propoerty line
 - c. Submission to include watermain system analysis demonstrating adequate pressure as per section 4.2.2 of the Water Distribution Guidelines.
 - d. Demonstrate adequate hydrant coverage for fire protection. Please review Technical Bulletin ISTB-2018-02, Appendix I table 1 maximum flow to be considered from a given hydrant.
 - e. Any proposed emergency route (to be satisfactory to Fire Services).
- 12. Sanitary Design
 - a. A 200mm sanitary sewer is available at the site property line
 - b. A monitoring maintenance hole is required just inside the property line for the proposed development.



- c. Please apply the wastewater design flow parameters in Technical Bulletin PIEDTB-2018-01.
- d. Demonstrate that there is adequate residual capacity in the receiving and downstream wastewater system
- 13. Storm Design
 - a. There is access to a 600mm storm sewer at the site property line
 - b. IDF information derived from the Meteorological Services of Canada rainfall data, taken from the MacDonald Cartier Airport, collected 1966 to 1997 must be applied
 - c. The pre-development runoff shall be the lower of the existing coefficient or a maximum equivalent 'C' of 0.5, whichever is less (§ 8.3.7.3).
 - d. Time of concentration: to be calculated, min Tc = 10 mins
 - e. Design storm for receiving sewer: 5-year design storm
 - f. Allowable release rate: 240L/s/Ha.
 - g. Storm sewer outlets should not be submerged.
 - h. Proovide information on the monitoring manhole should be located in an accessible location on private property near the property line (ie. Not in a parking area).
- 14. An MECP Environmental Compliance Approval [Private Sewage Works] will be required should the proposed storm system collect off-site drainage. An exemption to review the application under City's Transfer of Review may be granted for the proposed development provided that specific criteria are met.
- 15. Geotechnical
 - a. Sensitive Marine Clay (SMC) is widely found across Ottawa- geotechnical reports should include Atterberg Limits, consolidation testing, sensitivity values, and vane
- 16. Additional Notes
 - a. No road moratorium that would impact the application has been identified
 - b. Any easement identified should be shown on all plans
 - c. For any proposed exterior light fixtures, please provide certification from a licensed professional engineer confirming lighting has been designed only using fixtures that meet the criteria for full cut-off classification as



recognized by the Illuminating Engineering Society of North America and result in minimal light spillage onto adjacent properties (maximum allowable spillage is 0.5 fc). Additionally, include in the submission the location of the fixtures, fixture type (make, model, part number and mounting height.

Feel free to contact Abibatou Dieme (<u>abibatou.dieme@ottawa.ca</u>), Infrastructure Project Manager, for follow-up questions.

<u>Noise</u>

Comments:

17. Not required for sales office.

Feel free to contact Mike Giampa (mike.giampa@ottawa.ca), Transportation Project Manager, for follow-up questions.

Transportation

Comments:

- 18. Right-of-way protection (if required)
 - a. See <u>Schedule C16 of the Official Plan</u>.
 - b. Any requests for exceptions to ROW protection requirements <u>must</u> be discussed with Transportation Planning and concurrence provided by Transportation Planning management.
- 19. A TIA is not required.

Feel free to contact Mike Giampa (mike.giampa@ottawa.ca), Transportation Project Manager, for follow-up questions.

Environment

Comments:

- 20. There are no natural heritage features, surface water features, or species-at-risk habitat on or near the site that would trigger the need for an Environmental Impact Statement (EIS). An EIS is not required as part of this application.
- 21. Please consider additional tree plantings wherever possible to help meet the City's urban forest canopy goals and to help mitigation the impacts of the urban heat island effect and climate change. Please note that the City prefers that all plantings be of native and non-invasive species.



Feel free to contact Mark Elliott (mark.elliot@ottawa.ca), Environmental Planner, for follow-up questions.

Forestry

Comments:

- 22. Tree Conservation Report
 - a. Please confirm whether any trees >10cm in diameter exist on site or of any size in the ROW; if yes, a Tree Conservation Report is required, in accordance with Schedule E of the Tree Protection By-law. Ownership of all trees on the subject site and with Critical Root Zones extending onto the subject site must be determined, and plans must show how they will be protected from proposed works.
 - b. A permit is required prior to removal of any protected trees on site. The tree permit will be released upon site plan approval. Please contact the planner associated with the file or the Planning Forester, Nancy Young (Nancy.young@ottawa.ca) for information on obtaining the tree permit.
 - c. To ensure that no harm is caused to breeding birds, tree removal and vegetation clearing should be avoided during the migratory bird season (April 15 – August 15) as specified by The City of Ottawa's Environmental Impact Study Guidelines.
- 23. Landscape Plan
 - a. A Landscape Plan is required with this application and must address all requirements within the Landscape Plan Terms of Reference <u>https://documents.ottawa.ca/sites/documents/files/landscape_tor_en.pdf</u>, including the projection of canopy cover toward the target of 40%, and confirmation of adequate soil volumes to support any proposed trees.
 - b. The Landscape Plan must show the soil volumes and setback distances between proposed and existing trees to buildings and underground structures to ensure that both the above and below-ground space proposed is sufficient for tree planting in the Right of Way and other landscaped areas.
 - c. The Official Plan section 4.8.2, sub 3 provides the following direction related to tree planting related to site plans:
 - i. Preserve and provide space for mature, healthy trees on private and public property, including the provision of adequate volumes of high-quality soil as recommended by a Landscape Architect;



- ii. On urban properties subject to site plan control or community planning permits, development shall create tree planting areas within the site and in the adjacent boulevard, as applicable, that meet the soil volume requirements in any applicable City standards or best management practices or in accordance with the recommendation of a Landscape Architect
- d. It is a Best Management Practice to plant one tree for every 5 parking spaces to help address the urban heat island effect created by paved areas, and also to work toward the Official Plan target of 40% canopy cover.
- e. Consider increasing the size of the landscape buffers and/or parking lot islands to create plantable spaces with sufficient soil volumes.

Feel free to contact Nancy Young (nancy,young@ottawa.ca), Planning Forester, for follow-up questions.

Parkland

Comments:

- 24. The amount of parkland dedication that is required is to be calculated as per the City of Ottawa Parkland Dedication By-law No 2022-280. For commercial and Industrial development, parkland dedication is required to be provided at the rate of 2% the gross land area.
- 25. Parks & Facilities Planning is requesting **Cash in Lieu** of for this proposal. The value of the property will be determined by market appraisal approved by the City prior to planning approval for the site plan.
- 26. Please provide the City with a surveyor's area certificate/memo which specifies the exact gross land area of the property parcel being developed.
- 27. If parkland dedication for the parcel has been satisfied previously, please provide Parks & Facilities Planning with the supporting documentation.
- 28. Please note that the park comments are preliminary and will be finalized (and subject to change) upon receipt of the development application and the requested supporting documentation. Additionally, if the proposed residential product or land use changes, then the parkland dedication requirement be re-evaluated accordingly.

Feel free to contact Anissa McAlpine (anissa.mcalpine@ottawa.ca), Parks Planner, for follow-up questions.



<u>Other</u>

- 29. The High-Performance Development Standard (HPDS) is a collection of voluntary and required standards that raise the performance of new building projects to achieve sustainable and resilient design. The HPDS was passed by Council on April 13, 2022.
 - a. At this time, the HPDS is not in effect and Council has referred the 2023 HPDS Update Report back to staff with direction to bring forward an updated report to Committee with recommendations for revised phasing timelines, resource requirements and associated amendments to the Site Plan Control By-law by no later than Q1 2024.
 - b. Please refer to the HPDS information attached and ottawa.ca/HPDS for more information.

Should there be any questions, please do not hesitate to contact myself or the contact identified for the above areas / disciplines.

Yours Truly, Colette Gorni, Planner II (DR West)

c.c. Nishant Dave, Planner I (DR West) Kadri Nader, Urban Design Abibatou Dieme, Infrastructure Project Manager Mike Giampa, Transportation Project Manager Nancy Young, Planning Forester Mark Elliot, Environmental Planner Anissa McAlpine, Parks Planner Elizabeth King, Planner I (DRAW)



APPLICANT'S STUDY AND PLAN IDENTIFICATION LIST

Proposed Site Plan Control Application – 370 Huntmar Drive – PC2024-0304

Legend: \mathbf{R} = Required, the study or plan is required with application submission

A = Advised, the study or plan is advised to evaluate the application or satisfy a condition of approval/draft approval

1 - OPA, 2 - ZBA, 3 - Plan of Subdivision, 4 - Plan of Condominium, 5 - SPC

Core studies required for certain applications all the time (Remaining studies are site specific)

For information and guidance on preparing required studies and plans refer here:

R	•	Study/ Plan Name	Description		Wh	en Requi	red		Applicable Study Components
n	A	Study/ Plan Name	Description	1	2	3	4	5	& Other Comments
		1. Environmental Site	Ensures development only takes	\boxtimes	\boxtimes	\boxtimes	\boxtimes	\boxtimes	Record of Site Condition
		Assessment (Phase 1 & Phase 2)	place on sites where the environmental conditions are suitable for the proposed use	<u>Study Tr</u> All cases	rigger Deta s	<u>ails</u> :			Yes □ No ⊠
			Geotechnical design	\boxtimes	\boxtimes	\boxtimes	\boxtimes	\boxtimes	
\boxtimes		2. Geotechnical Study	requirements for the subsurface conditions	<u>Study Tr</u> All cases	rigger Deta s	<u>ails</u> :	I	I	
		3. Grading and	Grading relationships between connecting (or abutting)			\boxtimes		\boxtimes	
\boxtimes		Drainage Plan	properties and surface runoff control	<u>Study Tr</u> All cases	rigger Deta s	<u>ails</u> :	I	I	
			A scientific study or evaluation			\boxtimes	\boxtimes	\boxtimes	Reasonable Use Study
		4. Hydrogeological and Terrain Analysis	that includes a description of the ground and surface hydrology, geology, terrain, affected landform and its susceptibility	When de	rigger Deta eveloping evelopmer private se	on private nt is in clos	se proxim	ity to	Yes I No I Groundwater Impact Study Yes I No I
				\boxtimes	\boxtimes	\boxtimes	\boxtimes	\boxtimes	Vibration Otvolv
		5. Noise Control Study	Potential impacts of noise on a development	<u>Study Trigger Details</u> : See Terms of Reference for full details.					Vibration Study Yes □ No □

				\boxtimes	\boxtimes	\boxtimes	X	
	6. Rail Proximity Study	Development on land adjacent to all Protected Transportation Corridors and facilities shown on Schedule C2 of the Official Plan, to follow rail safety and risk mitigation best practices	Study Tr Within th existing corridors on land a Transpo	igger Deta te Develop and future and show adjacent to rtation Co dule C2 of	<u>ails</u> : oment Zor rapid trar n on Anne o all Prote rridors and	ne of Influe nsit statior ex 2 of the cted d facilities	ence for ns and e OP OR	Rail Safety Report Yes D No D O-Train Network Proximity Study Yes D No D
	7. Site Servicing Study	Provides servicing details based on proposed scale of development with an engineering overview taking into consideration surrounding developments and connections.	Study Tr All cases	igger Deta	⊠ ails:			Fluvial Geomorphological Report Yes No ⊠ Assessment of Adequacy of Public Services Yes ⊠ No □ Servicing Options Report Yes □ No ⊠ Erosion and Sediment Control Plan / Brief Yes ⊠ No □ Hydraulic Water Main Analysis Yes ⊠ No □ Stormwater Management Report and Detailed Design Brief Yes ⊠ No □
	8. Slope Stability Study	Assessment of slope stability and measures to provide safe set- back.		igger Deta ne potentia		⊠ ard Lands	⊠ exists	Retrogressive Landslide Analysis Yes □ No □
	9. Transportation Impact Assessment	Identify on and off-site measures to align a development with City transportation objectives.	If the der or more;	igger Deta velopment or if the d Trigger; c rigger.	t generate evelopme	ent is locat	ed in a	Roadway Modification Functional Design Yes □ No □

				\boxtimes	\boxtimes	\boxtimes	\boxtimes
	10. Water Budget Assessment	Identify impact of land use changes on the hydrologic cycle and post-development mitigation targets.	May be r applicati and / or sensitive required assessm	Study Trigger Details: May be required for site plan control applications for sites with private servicing and / or proximity to hydrogeologically- sensitive areas. Draft plans of subdivision a required to integrate water budget assessments into supporting stormwater management plans and analysis for the stud area.			/- ision are iter
				\boxtimes	\boxtimes	\boxtimes	\boxtimes
	11. Wellhead Protection Study	Delineate a Wellhead Protection Area (WHPA) and characterize vulnerability for new communal residential drinking water well systems, in accordance with Technical Rules under <i>Clean</i> <i>Water Act.</i>	Required drinking municipa (small w Respons or increa municipa	d for all ne water well al wells, ne ater works sibility Agro	w commu systems w private that req eement (N takings fi xisting pri	; including commun uire a Muu MRA), exp rom an ex ivate com	new al wells nicipal ansions isting munal

				PLANNIN	IG				
	•	Ctudu/Dian Name	Description		Wh	en Requi	red		Applicable Study Components
R	A	Study/Plan Name	Description	1	2	3	4	5	& Other Comments
				\boxtimes					
		12. Agrology and Soil Capability Study	Confirm or recommend alterations to mapping of agricultural lands in the City.	For the e identifica through is demor	rigger Deta expansion ation of a r a compre nstrated th irements f	of a settle new settle hensive re nat the lar	ment area eview; or v id does no	a where it ot meet	
					\boxtimes	\boxtimes	\boxtimes	\boxtimes	
		13. Archaeological Assessment	Discover any archaeological resources on site, evaluate cultural heritage value and conservation strategies	When th archaeo archaeo Archaeo Study in outside of any a	rigger Deta le land has logical site logical site logical Re dicates ar of the hist rchaeolog stion in the	s either: a e; or the p es; or whe esource P chaeologi oric core; ical resou	otential to re the Cit otential M cal poten or upon d rce during	y's apping tial, liscovery	
				\boxtimes	\boxtimes			\boxtimes	
		14. Building Elevations	Visual of proposed development to understand facing of building including direction of sunlight, height, doors, and windows.	 <u>Study Trigger Details</u>: Site Plan: for residential buildings with 25 or more residential units; or for residential buildings with less than 25 residential units, if the units are within the Urban area or the High-performance Development Standard threshold in the rural area. Official Plan or Zoning By-law: if staff deem it necessary to determine compliance with OP policies, the Zoning By-law or City of Ottawa Urban Design Guidelines. 					

				\boxtimes	\boxtimes	\boxtimes	\boxtimes	
	15. Heritage Impact Assessment	Determine impacts of proposed development on cultural heritage resources.	Where of the Onta adjacen 30 metro for any of Canal U	rigger Deta developme ario Heritag t to, across es of a pro developme NESCO W ped buffer	nt or an a ge Act is p s the stree tected he ent adjace Vorld Heri	proposed et from or ritage pro nt to the F	on, within perty; or Rideau	Conservation Plan Yes □ No □
	16. Heritage Act Acknowledgement Report	A submission requirement to demonstrate that the <i>Ontario</i> <i>Heritage Act</i> requirements have been satisfied, to ensure that multiple applications are considered currently.	Where t Heritage submit a (designa Heritage to demo	rigger Deta he subject e Register a Heritage ated herita e Register) lish or rem ted proper r).	property and the a Permit Ap ge proper or provid	pplicant m oplication ty listed o e notice c Iding (nor	nust n the of intent 1-	Heritage Permit Application Yes No Notice of Intent to Demolish Yes No
		Mineral aggregate extraction activities; and to protect	\boxtimes	\boxtimes	\boxtimes	\boxtimes	\boxtimes	
	17. Impact Assessment Study – Mineral Aggregate	known high quality mineral aggregate resources from development and activities that would preclude or hinder their existence (ability to be extracted) or expansion.	New De within th metres of	rigger Deta velopment ie Bedrock of lands wi ce Area Ov	t within 50 Overlay thin the S	, or within	300	
		To identify or confirm known mineral deposits or petroleum	\boxtimes	\boxtimes	\boxtimes	\boxtimes	\boxtimes	
	18. Impact Assessment Study – Mining Hazards	resources and significant areas of mineral potential. To protect mineral and petroleum resources from development and activities which would preclude or hinder the establishment of new operations or access to the resources.		rigger Deta pplications ins.		nity to mir	ning	

		To identify or confirm known						
	19. Impact Assessment Study – Waste Disposal Sites / Former Landfill Sites	To ensure issues of public health, public safety and environmental impact are addressed.	For the e Disposa an opera develop	rigger Deta establishm I Site or fo ating Solid ment withi g or non-c	nent of any or a footpri I Waste D n three ki	nt expans isposal Si ometers c	sion of te; or of an	
			\boxtimes	\boxtimes	\boxtimes	\boxtimes	\boxtimes	
	20. <mark>Landscape Plan</mark>	A plan to demonstrate how the canopy cover, urban design, health, and climate change objectives of Official Plan will be met through tree planting and other site design elements.	Site Plar Condom it is dem compone review o A high-le be requi	rigger Deta n, Plan of ninium: alw onstrated ent of a pr f the appli evel conce red to sup Plan Amer	Subdivision vays requi- that the la roject is no- cation. eptual Lan oport Zonir			
				\boxtimes				
	21. Mature Neighbourhood Streetscape Character Analysis	In the Mature Neighbourhoods a Streetscape Character Analysis is required to determine the applicable zoning requirements.	Zoning E areas co zoning o develop	rigger Deta By-law am overed by overlay for ment of fo 2, R3, or F	endment the Matur applicatic ur storeys	e Neighbo	ourhoods idential	
		Provincial land use planning						
	22. Minimum Distance Separation	tool that determines setback distances between livestock barns, manure storages or anaerobic digesters and surrounding land uses, with the objective of minimizing land use conflicts and nuisance complaints related to odour.	<u>Study Trigger Details</u> : Applications in the Rural Area, outside of a village.					

		A tool to assess the			\boxtimes	\boxtimes		
	23. Parking Plan	sufficiency of on-street parking in plans of subdivision.		rigger Deta or revised reets.		subdivisio	on with	
		A Plan of Survey depicts legal	\boxtimes	\boxtimes	\boxtimes	\boxtimes	\boxtimes	
	24. <mark>Plan of Survey</mark>	boundaries and is a specialized map of a parcel of land and it delineates boundary locations, building locations, physical features and other items of spatial importance.		rigger Deta d for all <i>Pl</i>				
	25. Plan of Subdivision	Proposed subdivision layout to be used for application approval	Always	rigger Deta required w vision app	ith the sul	omission		
			Amendn	uired with nent applic nse to ena	ZBLA is			
		Proposed condominium				\boxtimes		
	26. Plan of Condominium	layout to be used for application approval		rigger Deta submissio on.		of condo	minium	
		Provides the planning	\boxtimes	\boxtimes	\boxtimes			
	27. Planning Rationale	justification in support of the <i>Planning Act</i> application and to assist staff and the public in the review of the proposal.	For all C	rigger Deta Official Plar endment, c ons.	n amendr		Integrated Environmental Review Summary Yes No	
		A checklist that shows a			\boxtimes		\boxtimes	
	28. Preliminary Construction Management Plan	development proposal's anticipated impacts to all modes of transportation and all elements in the right of way during construction.	all n and t of t of					

			\boxtimes	\boxtimes	\boxtimes	\boxtimes	\boxtimes	
	29. Public Consultation Strategy	Proposal to reach and collect public input as part of development application.	Study Tr Official F Amendm required Condom Site Plar lead in c	igger Deta Plan Amen hent and S	uils: dment, Zo oubdivision cant Land scretion o n with the	oning By- n: Always only of the City Business	law 's file	
	30. Shadow Analysis	A visual model of how the proposed development will cast its shadow.	 When the massing commercial commercial commercial commercial commercial commercial commercial commeters and the second commeters and the	igger Deta ere is an in proposed cial or offic gers: the Greer ment is over and/or may to a shace analysis m de the Green ment is over and is in c area. Wh ment is not sensitive a ment) the t is over 5 s	ncrease in for a resi ce use. hbelt: prop er 5 store opment propo assing an low sensi hay be rec enbelt: pr er 3 store lose prox ere a pro t in close area (e.g. rigger for	dential, bosed ys in heig roposal is sing an in d is in clo tive area, quested. oposed ys in heig imity to a posed proximity industrial a shadov	ht (≤15 5 icrease a ht (≤9 shadow to a	
	31. <mark>Site Plan</mark>	A Site Plan is a visual drawing that illustrates the proposed development of a site in two dimensions.	Site Plar	igger Deta n: All		the	Site Plan Yes ⊠ No □ Concept Plan Yes □ No □	

			densities provides sites pro with mul- more bu and/or a sites with (such as vehicula sites who adjacent	alm, buildi s or massin posing mu tiple lando ildings, on new publi h proposed active tra r circulatio ere the de properties integrated	ng of the plan to the plan ultiple lanc wners; sit -site park c or privat d changes nsportatio n or acce velopmen s may be	proposal nned cont I uses; sit es with tw dedicatio te street(s s to conne s to conne s to trans t potentia impacted	ext; es vo or n, s); ectivity (s, sit); I on by or	Facility Fit Plan Yes □ No □
	32. Urban Design Brief	Illustrate how a development proposal represents high- quality and context sensitive design that implements policies of the Official Plan, relevant secondary plans, and Council approved plans and guidelines.	For all O law ame applicati For SPC residenti residenti residenti Urban an Develop area who	igger Deta fficial Plar ndment, a ons. application al building al units, of al building al units, if rea or the ment Stan ere OP Po dential ano	nd plan of ons: propo is with 25 r for propo is with les the units High-perfo dard three licy 11.3 (f subdivision or more osals for s than 25 are within ormance shold in th (3) is relev	the ne rural vant; for	
	33. Urban Design Review Panel Report	Demonstrates that a development proposal has attended an Urban Design Review Panel formal review meeting, received, and responded to the associated recommendations, if applicable	Required subject t	igger Deta d for all pla o UDRP ro P Panel T	anning act eview, in a	accordanc	e with	
	34. Wind Analysis	A visual model and a written evaluation of how a proposed development will impact pedestrian-level wind conditions.	Applicati and/or m building(igger Deta ons seekin nassing wh s), 10 stor that is mo	ng an incr nich is eith reys or mo	ier: a tall pre or a pr	oposed	

			five store existing	t existing b eys in heig or planned aces, wate areas.	ht and is d low rise	adjacent i developm	to 1ent,	
		The purpose of the Zoning Confirmation Report (ZCR) is		\boxtimes			\boxtimes	
	35. <mark>Zoning Confirmation</mark> Report	to identify all zoning compliance issues, if any, at the outset of a planning application.		rigger Deta d for all SF		BLA applic	cations.	

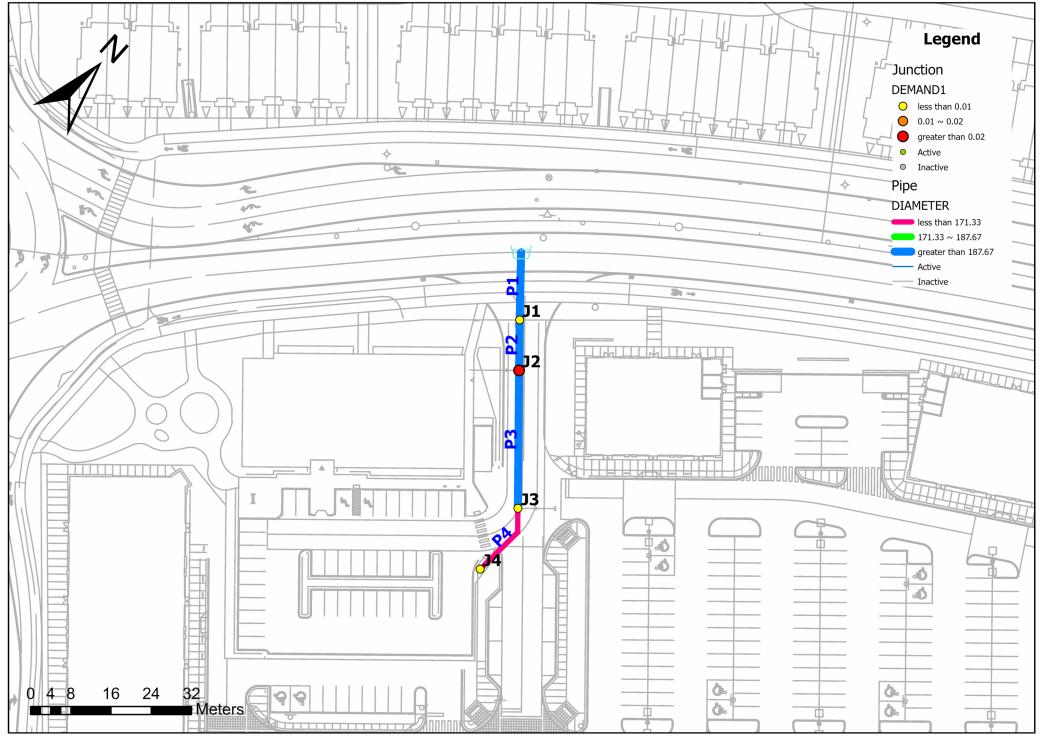
R	Α	Study / Plan Name	Description		Wh	en Requi	red		Applicable Study Components
n	A		Description	1	2	3	4	5	& Other Comments
			Includes a community						
		36. Community Energy Plan	energy analysis, alongside mitigation measures, and other associated information. The community energy analysis refers to the overall assessment process to identify on and off-site measures to align the design of the development with City climate objectives.	NOT I	MPLEMEI	NTED & N	IOT REQI	UIRED	
			The Energy Modeling						
		37. Energy Modelling Report	Report is a Site Plan Control application submission requirement to show how climate change mitigation, and energy objectives will be met through exterior building design elements.	NOT I	MPLEME	NTED & N	IOT REQ	UIRED	
			Assessment of environmental impacts of a	\boxtimes	\boxtimes	\boxtimes		\boxtimes	Assessment of Landform Features
		38. Environmental Impact Study	project and documents the existing natural features, identifies the potential environmental impacts,	Is requir	rigger Deta ed when c n is propos	levelopme			Yes I No I Integrated Environmental Review Yes I No I

		recommends ways to avoid and reduce the negative impacts, and proposes ways to enhance natural features and functions.	designat the City' hazardo The EIS Environr provides features EIS is re	d distance ted lands, s Natural I us forest ty Decision mental Imp a checklis and adjac equired to s ons under	natural he Heritage S ypes for w Tool (App pact Study st of the n cent areas support de	eritage fea System, or vildland fir pendix 2 of y Guideline atural heri s within wh evelopmer	e. the es) itage iich an	Protocol for Wildlife Protection during Construction Yes No Significant Woodlands Guidelines for Identification, Evaluation, and Impact Assessment Yes No D
	39. Environmental Management Plan	A comprehensive environmental planning document that identifies, evaluates, and mitigates the potential impacts of proposed development on the natural environment and its ecological functions at local planning stage.	Official F (area-sp where: th condition based; th planned subdivis impact of subdivis applicab	rigger Deta Plan amen becific polic here is sig ns upon wi here are p infrastruct ion that wo on the infra ion within ile Class E I has expir	dments for cy or seconificant cl hich the o roposed o ture need bould have the EMP s invironme	ndary plau hange in th original stu changes to ed to servi a significa needs of a study area	n, ne dy was ice a ant another a, or the	
		A collection of voluntary and required standards that raise						
	40. High-performance Development Standard	performance of new building projects to achieve sustainable and resilient design	NOT I	MPLEME	NTED & N	NOT REQU	JIRED	
		Demonstrates how tree			\boxtimes	\boxtimes	\boxtimes	
	41. Tree Conservation Report	cover will be retained and protected on the site, including mature trees, stands of trees, and hedgerows.	Where the diameter is a tree Root Zoo	rigger Deta here is a tr r or greate on an adja ne (CRZ) o ment site.	ree of 10 o or on the s acent site	ite and/or that has a	if there	



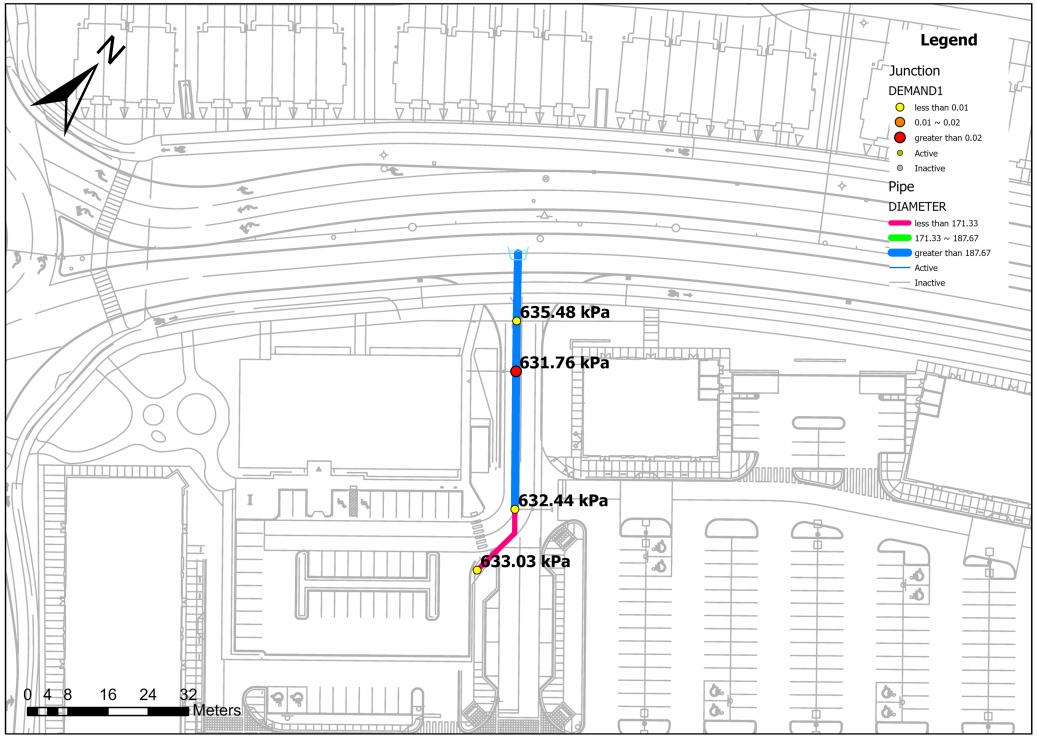
Watermain Boundary Conditions Water Demand Calculations FUS Calculations Water Model Results

Junctions and Pipes Layout



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Average Day Pressures

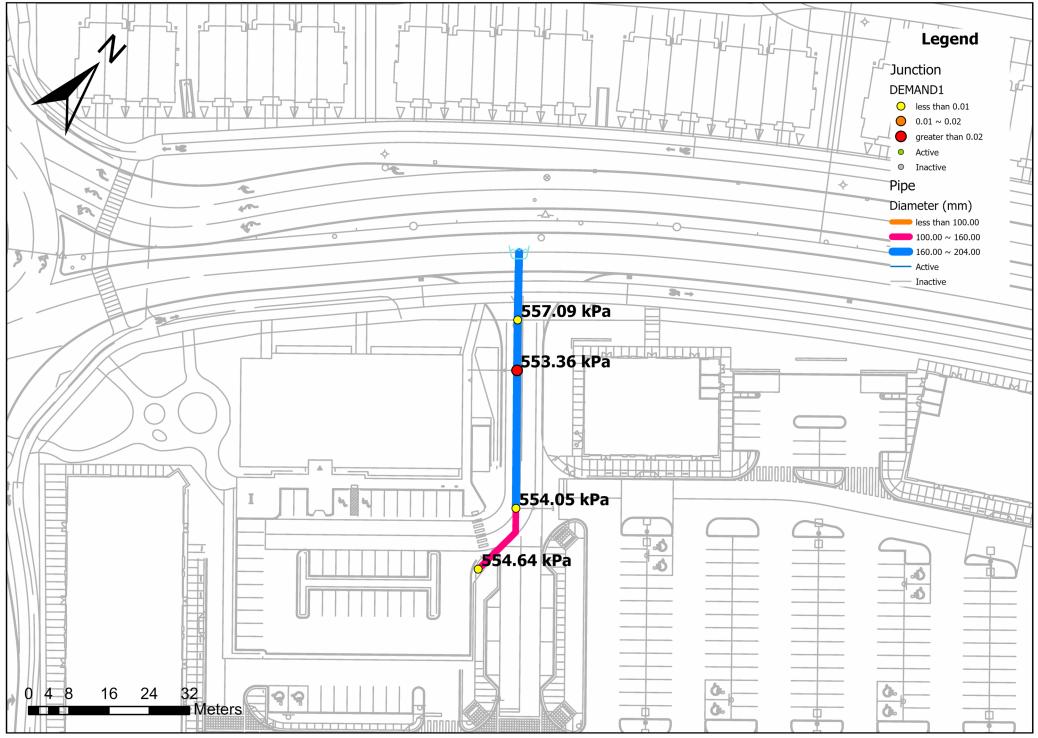


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Average Day Pressures

	ID	Demand (L/s)	Elevation (m)	Head (m)	Pressure (kPa)
1	J1	0.00	98.25	160.70	611.96
2	J2	0.03	98.63	160.70	608.24
3	J3	0.00	98.56	160.70	608.92
4	J4	0.00	98.50	160.70	609.51

Peak Hour Pressures

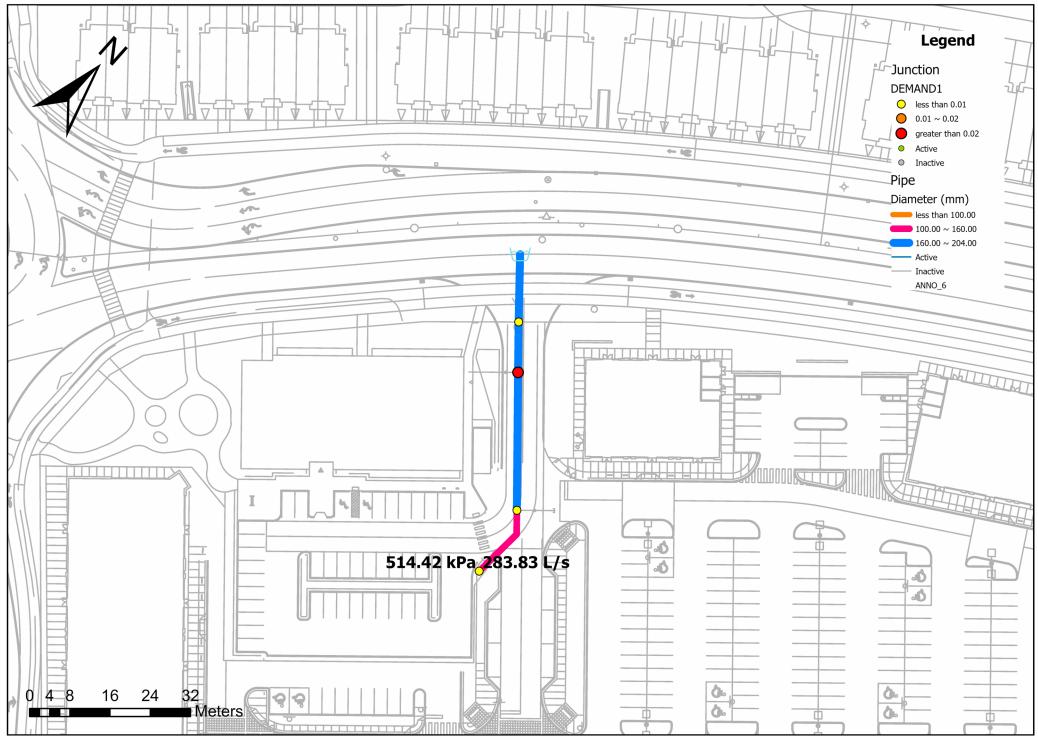


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Peak Hour Pressures

	ID	Demand (L/s)	Elevation (m)	Head (m)	Pressure (kPa)
1	J1	0.00	98.25	155.10	557.09
2	J2	0.07	98.63	155.10	553.36
3	J3	0.00	98.56	155.10	554.05
4	J4	0.00	98.50	155.10	554.64

Max Day + Fire Flow



Max Day + Fire Flow

		ID	Static Demand (L/s)	Static Pressure (kPa)	Static Head (m)	Fire-Flow Demand (L/s)	Residual Pressure (kPa)	Hydrant Available Flow (L/s)	Hydrant Pressure at Available Flow (kPa)
-	\Box	J4	0.00	557.58	155.40	83.33	514.42	283.83	140.0

Boundary Conditions 370 Huntmar Drive

Provided Information

Scenario	Dem	nand
Scenario	L/min	L/s
Average Daily Demand	2	0.03
Maximum Daily Demand	2	0.04
Peak Hour	4	0.07
Fire Flow Demand #1	5,000	83.33
Fire Flow Demand #2	6,000	100.00

Location



Results

Connection Option 1 – Campeau Dr.

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	160.7	88.8
Peak Hour	156.5	82.8
Max Day plus Fire Flow #1	155.4	81.2
Max Day plus Fire Flow #2	154.6	80.1
	134.0	00.1

¹ Ground Elevation = 127.5 m

Notes

- 1. As per the Ontario Building Code in areas that may be occupied, the static pressure at any fixture shall not exceed 552 kPa (80 psi.) Pressure control measures to be considered are as follows, in order of preference:
 - If possible, systems to be designed to residual pressures of 345 to 552 kPa (50 to 80 psi) in all occupied areas outside of the public right-of-way without special pressure control equipment.
 - Pressure reducing valves to be installed immediately downstream of the isolation valve in the home/ building, located downstream of the meter so it is owner maintained.
- 2. Demands for proposed Connection 1 at existing stub off Campeau Drive were assigned to upstream junction at Campeau Drive off the public looped watermains. The engineer must calculate headloss off the dead-end main.

Disclaimer

The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation. Fire Flow analysis is a reflection of available flow in the watermain; there may be additional restrictions that occur between the watermain and the hydrant that the model cannot take into account.

ARCADIS ARCADIS IBI GROUP

500-333 Preston Street

Ottawa, Ontario K1S 5N4 Canada **IBI GROUP** arcadis.com

WATERMAIN DEMAND CALCULATION SHEET

Arcadia Commercial Site | Minto 147391 -6.0 | Rev #0 | 2024-11-13 Prepared By: MP | Checked By: RM

		RESIDI	ENTIAL		NON	-RESIDENTIAL	. (ICI)	AVERAG	E DAILY DEM	AND (l/s)	MAXIMU	IM DAILY DEM	AND (I/s)	MAXIMUN	HOURLY DE	MAND (l/s)	FIRE
NODE	Towns	Medium Density		POPULATION	INDUST. (ha)	COMM. (ha)	INSTIT. (ha)	RESIDENTIAL	ICI	TOTAL	RESIDENTIAL	ICI	TOTAL	RESIDENTIAL	ICI	TOTAL	DEMAND (l/min)
Arcadia						0.090			0.03	0.03		0.04	0.04		0.07	0.07	5,000
TOTAL						0.09				0.03			0.04			0.07	

			ASS	UMPTIONS		
POPULATION DENSITY		WATER DEMAND RATES		PEAKING FACTORS FOR POP. O	F 501 TO 3000	FIRE DEMANDS
Townhouse	2.7 persons/unit	Residential	280 l/cap/day	Maximum Daily		Single Family 10,000 I/min (166.7 I/s)
				Residential	2.5 x avg. day	
Medium Density (Stacks)	1.8 persons/unit			Commercial	1.5 x avg. day	Semi Detached
		Commercial Shopping Center	2,500 L/(1000m2)/day	Maximum Hourly		& Townhouse 12,000 I/min (200.0 I/s)
				Residential	2.2 x max. day	
				Commercial	1.8 x max. day	Medium Density 15,000 I/min (250.0 I/s)



IBI GROUP

ARCADIS IBI GROUP

500-333 Preston Street Ottawa, Ontario K1S 5N4 Canada arcadis.com

FIRE UNDERWRITERS SURVEY

Arcadia Commercial Site | Minto 147391-6.0 | Rev #0 | 2024-11-13 Prepared By: MP | Checked By: RM

STEP	Contents	Description		Adjustment Fa	actor	Resu	ult
1	Floor Area Total Storey Total Effective Floor Area	Arcadia Commercial Site				997 2 1994	m2 storey m2
2	Type of Construction	Type V Wood Frame Type III Ordinary Construction Type II Noncombustible Construction Type I Fire Resistive Construction	1.5 1.0 0.8 0.6	Noncombustible Construction	0.8		
3	Required Fire Flow	RFF = 220C√A				8000	L/min
4	Occupancy and Contents	Noncombustible Contents Limited Combustible Contents Combustible Contents Free Burning Contents Rapid Burning Contents	-25% -15% 0% 15% 25%	Limited Combustible Contents	-15%	-1200	L/min
	Fire Flow					6800	L/min
5	Automatic Sprinkler Protection	Automatic Sprinkler Conforming to NFPA 13 Standard Water Supply for both the system and Fire Department Hose Lines Fully Supervised System	-30% -10% -10%	Yes No No	-30%	0 -2040	L/min L/min
	Fire Flow					-2040	L/min
	Exposure Adjustment	Based on Table 6 Exposure Adjustement Ch	arges for	Subject Building			
0	East (Future)	Separation (m) Length X Height Factor (m.storeys) Construction Type	24.07 20 Type II	Without unprotected opening	0%	0	L/min
6	South-West (Future)	Separation (m) Length X Height Factor (m.storeys) Construction Type	10.6 64 Type II	Without unprotected opening	6%	408	L/min
	Fire Flow		* •			408	L/min
7	Total Required Fire Flow					5168	
1	rotar Required i lie Flow	Rounded to Nearest 1000 L/min				5000	L/min

Notes 1. Fire flow calculation are based on Fire Underwriters Survey version 2020.

Appendix C

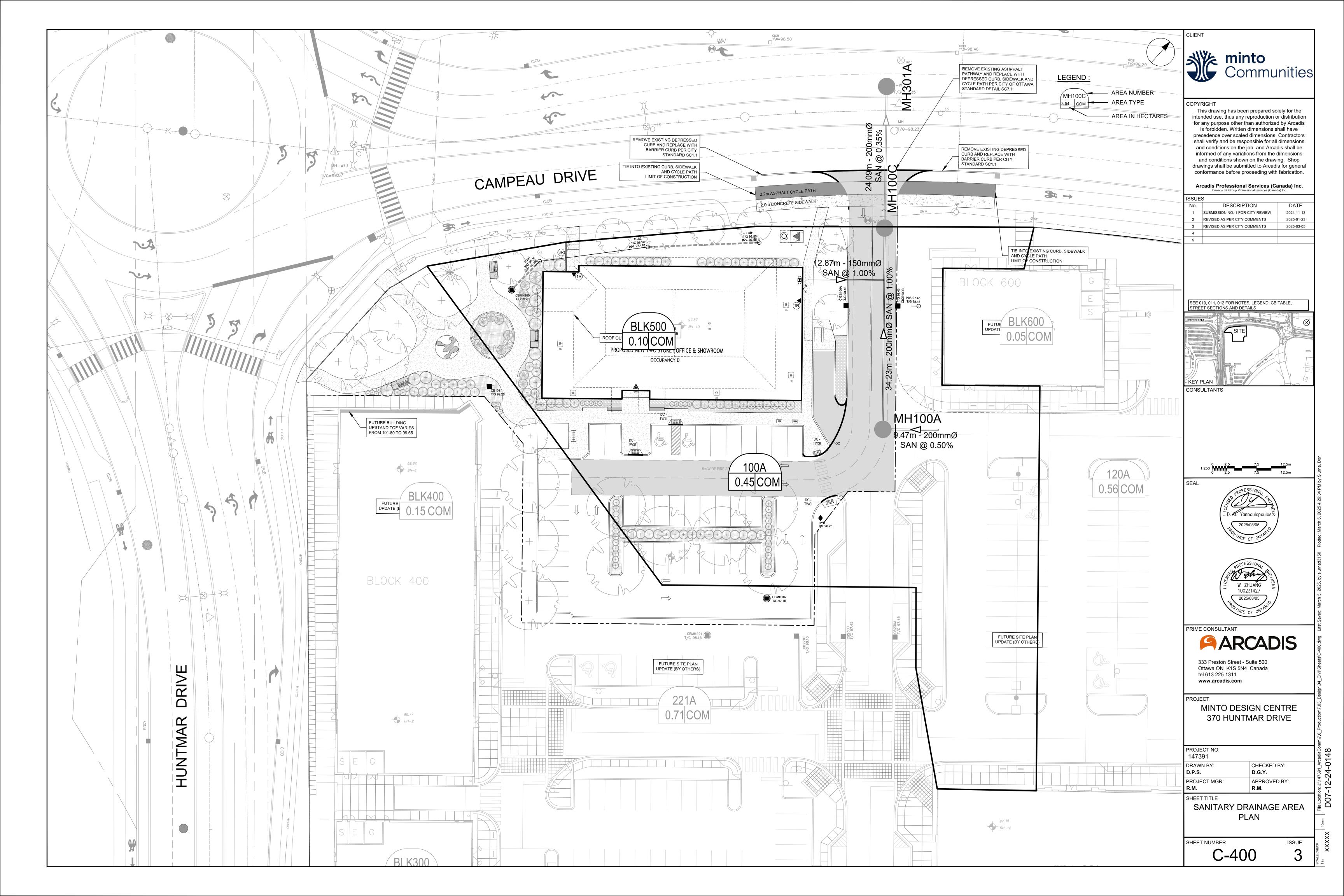
Sanitary Sewer Design Sheet Sanitary Drainage Area Plan 147391-C-400 Sanitary Sewer Design Sheet 35355 Sanitary Drainage Area Plan 35355-C-501 Sanitary Sewer Design Sheet – Kanata West Servicibility Study

ARCADIS 400-333 Preston Street 400-333 Preston Street Ottawa, Ontario K1S 5N4 Canada tel 613 225 1311 fax 613 225 9868 arcadis.com

	1.00	CATION							RESIDE	NTIAL								ICI A	REAS				INFILT	RATION ALL	OWANCE		LOW (L/s)	TOTAL			PROPO	SED SEWER I	DESIGN		
	LU	CATION	1		AREA		UNIT	TYPES		AREA	POPU	ATION	RES	PEAK				A (Ha)			ICI	PEAK	ARE	A (Ha)	FLOW	FIXED F	LOW (L/S)	FLOW	CAPACITY	LENGTH	DIA	SLOPE	VELOCITY	AVAIL	
STREET	A	REA ID	FROM MH	ТО МН	w/ Units (Ha)	SF	TH/SD	APT	OTHER	w/o Units (Ha)	IND	CUM	PEAK FACTOR	FLOW (L/s)	INSTITU	CUM		ERCIAL CUM	INDUS IND	TRIAL CUM	PEAK FACTOR	FLOW (L/s)	IND	СЛМ	(L/s)	IND	CUM	(L/s)	(L/s)	(m)	(mm)	(%)	(full) (m/s)	CAPA L/s	(%)
Arcadia Comm	nercial Site																																		
SITE PLAN			CAP	MH100A							0.0	0.0	3.80	0.00		0.00	1.24	1.24		0.00	1.50	0.60	1.24	1.24	0.41		0.00	1.01	24.19	9.47	200	0.50	0.746	23.18	95.82%
SITE FLAN			CAF	MITTUUA							0.0	0.0	3.00	0.00		0.00	1.24	1.24		0.00	1.50	0.00	1.24	1.24	0.41		0.00	1.01	24.19	9.47	200	0.50	0.740	23.10	95.62 %
	В	3LK500	BLDG SVC	SEWER							0.0	0.0	3.80	0.00		0.00	0.10	1.34		0.00	1.50	0.65	0.10	1.34	0.44		0.00	1.09	19.46	12.87	150	1.50	1.067	18.37	94.38%
			MH100A	MH100C		_					0.0	0.0	3.80	0.00		0.00	0.45	1.79		0.00	1.50	0.87	0.45	1.79	0.59		0.00	1.46	34.22	34.23	200	1.00	1.055	32.76	95.73%
																															200				
																									-	-									
					Notes:								Berland					N.,							Revision								Date		
Design Parameters:	•				1. Mannings	coefficier	nt (n) =		0.013				Designed:					No.						Submissi	on No. 1 for Cit	v Review							2024-11-13		
Residential		I	CI Areas		2. Demand (L/day	200	L/day							2							on No. 2 for Cit								2025-01-23		
SF 3.4 p/p	o/u				3. Infiltration			0.33	L/s/Ha		-		Checked:												-										
TH/SD 2.7 p/p			0 L/Ha/day		4. Residentia			4//4./0/400																											
APT 1.8 p/p	u COM		0 L/Ha/day 0 L/Ha/day	MOE Chart			Formula = 1+(1 = 0.8 Correctio		JU)^U.5))0.8				Dwa. Refe	rence:	147391-40	0																			
Other 60 p/p/			0 L/Ha/day				titutional Peak		ed on total a	rea.			Ding. Itele		147 03 1-40	•		F	le Referenc	e:						Date:							Sheet No:		
							20%, otherwise												7391-6.04.							2024-11-							1 of 1		

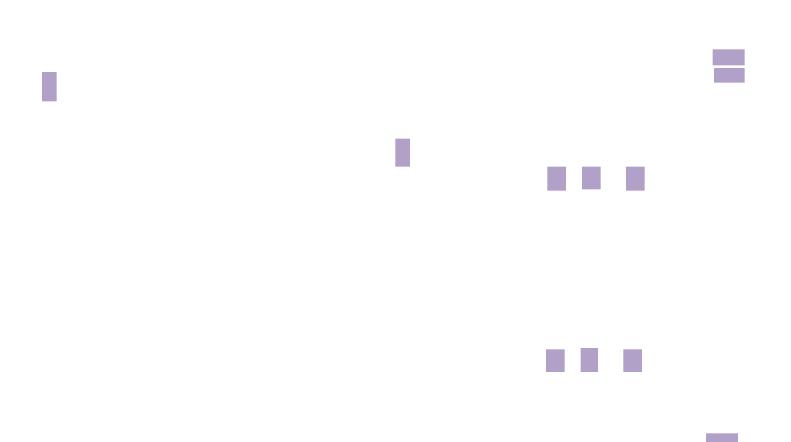
SANITARY SEWER DESIGN SHEET

147391 - Arcadia Commercial Site CITY OF OTTAWA Minto Communities





	1001-1011						RESIDENTIAL							ICI AREAS			INFIL	TRATION ALLO	NANCE	TOTAL				PROPOSED S	EWER DESIGN			
	LOCATION				UNIT TYPES		AREA	POPULAT	ION	PEAK	PEAK		ARE	A (Ha)		PEAK	ARE	A (Ha)	FLOW	FLOW	CAPACITY	LENGTH	DIA	SLOPE	VELOCITY	VELOCITY	AVAI	LABLE
STREET	AREA ID	FROM	то	CE C	D TH	APT	(Ha)	IND	CUM	FACTOR	FLOW I	NSTITUTIONAL	COM	MERCIAL	INDUSTRIAL	FLOW	IND	CUM	(1/s)	(1/c)	(1/s)	(m)	(mm)	(%)	(full)	(actual)	CAPA	ACITY
		МН	МН	3F 3		AFT	(па)	IND	COIVI		(L/s) II	ND CUM	IND	CUM	IND CUM	(L/s)	IND	CON	(L/ S)	(L/3)	(L/s)	(m)	(1111)	(78)	(m/s)	(m/s)	L/s	(%)
	BLK800	BLK800A	MAIN					0.0	0.0	4.00	0.00	0.00	0.06	0.06	0.00	0.05	0.06	0.06	0.02	0.07	15.89	6.50	150	1.00	0.871		15.82	99.57
	1224	N4U122A	N411122A					0.0	0.0	4.00	0.00	0.00	0.20	0.25	0.00	0.20	0.20	0.25	0.10	0.40	24.22	26.04	200	1.00	1.055		22.01	09.93
	123A	MH123A	MH122A						0.0			0.00	0.29	0.35	0.00	0.30	0.29	0.35	0.10	0.40	34.22	26.94	200	1.00	1.055		33.81	98.83
	122A	MH122A	MH121A					0.0	0.0	4.00	0.00	0.00	0.09	0.44	0.00	0.38	0.09	0.44	0.12	0.51	34.22	11.00	200	1.00	1.055		33.71	98.52
	BLK700	BLK700A	MAIN			-		0.0	0.0	4.00	0.00	0.00	0.10	0.10	0.00	0.09	0.10	0.10	0.03	0.11	15.89	6.50	150	1.00	0.871		15.77	99.28
	DER/00	BERYOOA	MAIN					0.0	0.0	4.00	0.00	0.00	0.10	0.10	0.00	0.05	0.10	0.10	0.05	0.11	15.65	0.50	150	1.00	0.071		15.77	55.28
	121A	MH121A	MH120A					0.0	0.0	4.00	0.00	0.00	0.08	0.62	0.00	0.54	0.08	0.62	0.17	0.71	34.22	57.61	200	1.00	1.055		33.50	97.92
																					_							
	BLK600	BLK600A	MAIN					0.0	0.0	4.00	0.00	0.00	0.06	0.06	0.00	0.05	0.06	0.06	0.02	0.07	15.89	6.50	150	1.00	0.871		15.82	99.57
	120A	MH120A	MH100A					0.0	0.0	4.00	0.00	0.00	0.56	1.24	0.00	1.08	0.56	1.24	0.35	1.42	24.19	53.29	200	0.50	0.746		22.77	94.12
	BLK500	BLK500A	MAIN				4	0.0	0.0	4.00	0.00	0.00	0.09	0.09	0.00	0.08	0.09	0.09	0.03	0.10	15.89	15.00	150	1.00	0.871		15.78	99.35
											0.00			4 = 0					0.50									01 51
	100A	MH100A	MH100C					0.0	0.0	4.00	0.00	0.00	0.46	1.79	0.00	1.55	0.46	1.79	0.50	2.06	24.19	34.23	200	0.50	0.746		22.14	91.51
		MH100C	EXMH301A					0.0	0.0				0.00	1.79		1.55	0.00	1.79	0.50	2.06	24.19	23.50	200	0.50	0.746		<u>22.14</u>	91.51
														<u> </u>	<u> </u>						+	+					- Eg	
<u> </u>	BLK400	BLK400A	MAIN				+ +	0.0	0.0	4.00	0.00	0.00	0.15	0.15	0.00	0.13	0.15	0.15	0.04	0.17	15.89	6.50	150	1.00	0.871		15.72	98.92
	BLK300	BLK300A	MAIN					0.0	0.0	4.00	0.00	0.00	0.15	0.05	0.00	0.13	0.05	0.05	0.01	0.06	15.89	6.50	150	1.00	0.871		15.83	99.64
	DEROOO	DEROCOR							0.0		0.00	0.00	0.00	0.05			0.05	0.00	0.01	0.00	10100	0.50		1.00			13.00	
	221A	MH221A	MH212A					0.0	0.0	4.00	0.00	0.00	0.71	0.91	0.00	0.79	0.71	0.91	0.25	1.04	75.98	82.40	250	1.50	1.500	0.522	74.94	98.63
	BLK100	BLK100A	MAIN					0.0	0.0	4.00	0.00	0.00	0.06	0.06	0.00	0.05	0.06	0.06	0.02	0.07	15.89	6.85	150	1.00	0.871		15.82	99.57
	BLK200	BLK200A	MAIN					0.0	0.0	4.00	0.00	0.00	0.05	0.05	0.00	0.04	0.05	0.05	0.01	0.06	15.89	6.75	150	1.00	0.871		15.83	99.64
	214A	MH214A	MH213A					0.0	0.0	4.00	0.00	0.00	0.42	0.53	0.00	0.46	0.42	0.53	0.15	0.61	43.87	44.12	250	0.50	0.866	0.301	43.26	98.61
	213A	MH213A	MH212A				+	0.0	0.0	4.00	0.00	0.00	0.13	0.66	0.00	0.57	0.13	0.66	0.18	0.76	43.87	16.38	250	0.50	0.866	0.325	43.11	98.27
	212A	MH212A	MH210A					0.0	0.0	4.00	0.00	0.00	0.21	1 99	0.00	1.62	0.31	1 99	0.52	2 16	62.04	E0 00	250	1.00	1.224	0.551	59.88	96.52
	212A		IVINZ10A					0.0	0.0	4.00	0.00	0.00	0.31	1.88	0.00	1.63	0.51	1.88	0.53	2.16	62.04	58.88	250	1.00	1.224	0.551	59.00	96.52
	BLK900	BLK900A	MAIN					0.0	0.0	4.00	0.00	0.00	0.47	0.47	0.00	0.41	0.47	0.47	0.13	0.54	11.23	22.08	150	0.50	0.616		10.69	95.20
	DEROOO	DERSOON							0.0		0.00	0.00					0.17	0.17	0.10	0.01				0.50			10:05	35.20
	210A	MH210A	MH205C					0.0	0.0	4.00	0.00	0.00	0.32	2.67	0.00	2.32	0.32	2.67	0.75	3.07	62.04	28.84	250	1.00	1.224	0.633	58.97	95.06
		MH205C	MH205A					0.0	0.0	4.00	0.00	0.00	0.19	2.86	0.00	2.48	0.19	2.86	0.80	3.28	62.04	11.04	250	1.00	1.224	0.633	58.76	94.71
																												-5
nal South mixed	EXT 2	STUB	MH205A					0.0	0.0	4.00	0.00	0.00		0.00	0.00	3.01	2.82	2.82	0.79	3.80	24.19	14.51	200	0.50	0.746		20.39	84.29
																												- 8
try Glen Way	205A	MH205A	MH204A					0.0	0.0	4.00	0.00	0.00		2.94	0.00	5.56	0.08	5.76	1.61	7.18	71.33	33.73	300	0.50	0.978	0.620	64.16	89.94
try Glen Way	204A	MH204A	MH202A					0.0	0.0	4.00	0.00	0.00	0.32	3.26	0.00	5.84	0.32	6.08	1.70	7.54	71.33	125.25	300	0.50	0.978	0.628	63.79	89.43
ry Glen Way	202A	MH202A	MH201A		<u> </u>			0.0	0.0	4.00	0.00	0.00	0.04	3.30	0.00	5.87	0.04	6.12	1.71	7.59	71.33	11.74	300	0.50	0.978	0.633	63.75	89.36
nal East Mix	EXT-1	Stub	MH201A				+	0.0	0.0	4.00	0.00	0.00		0.00	0.00	0.79	0.74	0.74	0.21	1.00	24.19	20.27	200	0.50	0.746		23.19	95.87
		Jub	WIII 201A				+ +					0.00		0.00		0.73	5.74	0.74	0.21	1.00	27.13		200	0.50	0.740		23.15	55.07
ry Glen Way	201A	MH201A	MH200A				1 1	0.0	0.0	4.00	0.00	0.00	0.10	3.40	0.00	6.75	0.10	6.96	1.95	8.70	71.33	18.49	300	0.50	0.978	0.659	62.63	87.80
try Glen Way	200A	MH200A	EX CAP					0.0	0.0	4.00	0.00	0.00		3.40	0.00	6.75	0.00	6.96	1.95	8.70	58.82	45.35	300	0.34	0.806	0.630	50.12	85.20
eau Dr			EXMH303A					0.0	0.0			00 0.00	0.00	3.40	0.00 0.00	6.75	0.00	6.96	1.95	8.70	58.82	20.50	300	0.34	0.806	0.630	50.12	85.20
																												- 8 _
Parameters:				Notes:					[Designed:	RM			No.				Revision							Da	ate		
				1. Mannings coeffi			0.013							1.				Issued for S								-11-15		
Residential		ICI Areas		2. Demand (per ca			0 L/day	300 L/0		-				2.				sed as per City								-06-24		<u> </u>
3.4 p/p/u				3. Infiltration allow		0.2	8 L/s/Ha	0.4 L/s	s/Ha	Checked:	DY			3.				sed as per City								-08-22		
SD 2.7 p/p/u		000 L/Ha/day		4. Residential Peak	0	1 4 // 4 . 5 4 5 5 1								4.			Revi	ised as per City	Comments				 		2014-	-10-02		
T 1.8 p/p/u er 60 p/p/Ha		000 L/Ha/day	1.5		on Formula = 1+(1				Ļ		400.0	F 01																
u bu b/b/Ha		000 L/Ha/day 000 L/Ha/day	MOE Chart	where	e P = population ir	i thousands			ľ	Dwg. Referer	nce: 1234	0-501			ile Reference:				Date:							et No:		
	A 7 A								1										11210						Shoo			

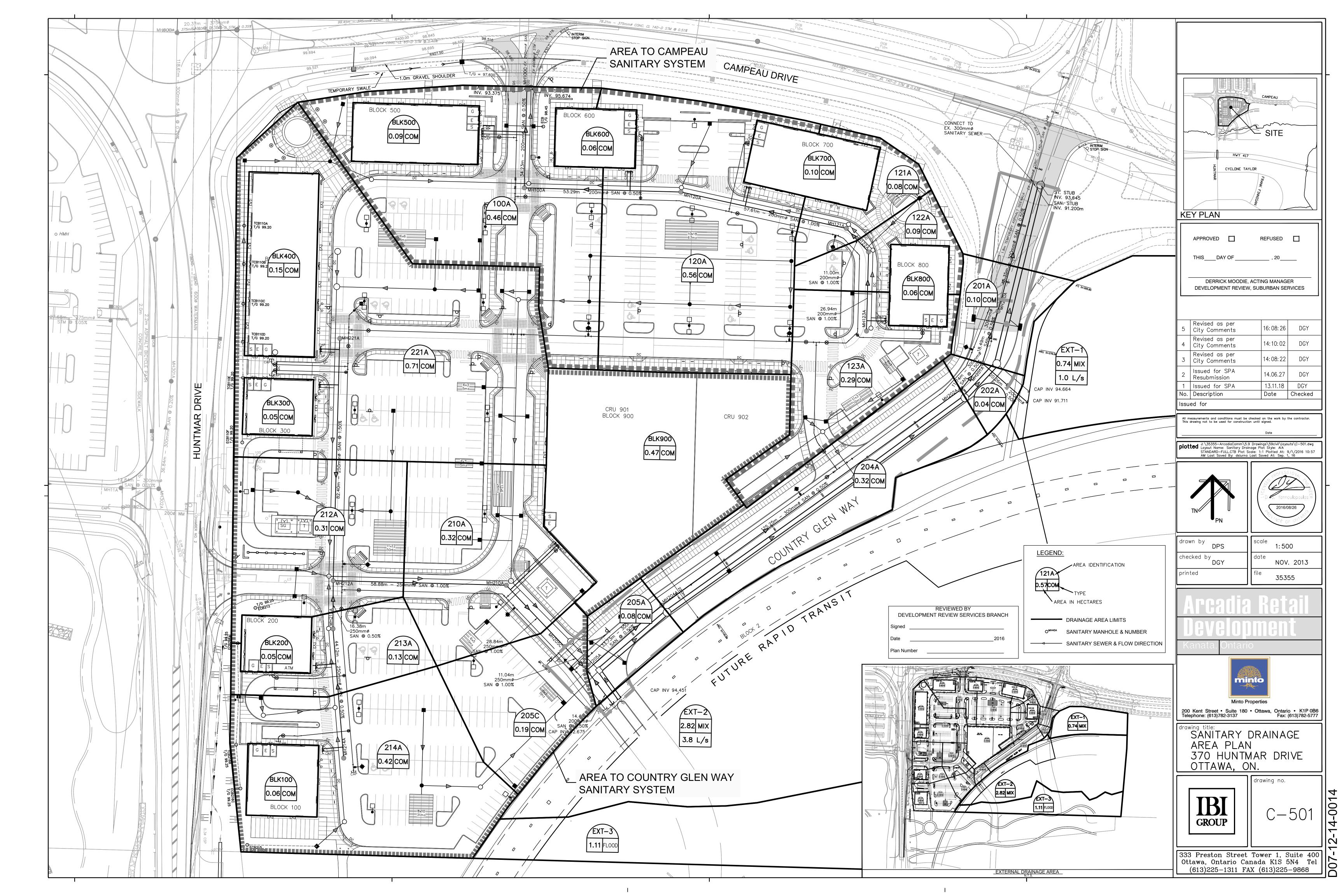


https://arcadiso365.sharepoint.com/sites/Projects5/147391/Internal Documents/6.0_Technical/6.04_Civil/04_Design-Analysis/CCS_35355_sanitarysewers_2014-10-02

SANITARY SEWER DESIGN SHEET

-

PROJECT: NAME OF PROJECT LOCATION: CITY OF OTTAWA CLIENT: NAME OF CLIENT



SANITARY SEWER DESIGN SHEET PROJECT : Kanata West Servicibility Study LOCATION : CITY OF OTTAWA

				25						population	based criter	a.ici simu	dianaous per		All minimized	S PARKOPE	SPACES	1		INFILTRA	TION		TOTAL		ROPOSED	SEWER	min a	oning	AVAIL,	HARMON	ACTUAL	va/Vf	ACTU
				TOTAL				IDENTIAL					EMPLOY	MENT/RET	FLOW	SS PARIOFEI	AK FLOW		A	REA (Ha)		PEAK	FLOW	CAPACITY	VELOCITY	LGTH.	PIPE	GRADE	CAP.	PF	q/Q		VELOC
	OCATI	UN I		AREA	APPLIC	UNIT/Ha	TOTAL	POPUL				APPLIC	ACCUM	AREA	RATE		ACCUM	TOTAL	INDIV	CUMUL	TOTAL	FLOW			(full)		1			- rr	- uu		(m/s
STREET	ROM	то		22.	AREA	17.55001.04-308	UNITS	INDIV J	ACCUM	FACTOR	FLOW	AREA	AREA (Ha)	(Ha)	(VHa/d)	(1/s)	(Vs)	(1/s)	dana seo	())	CUMUL	(1/s)	(l/s)	l/s	m/s	(m)	(mm)	%	(%)				4000
	MH	MH		(Ha)	(Ha)			-			(1/5)	(Ha)	(ria)	Inaj	Interest	ALC: N																	
	MUS	mail										10.11	20.44		35000	23.16	23.16		38.11	38.11													
P. J., Pauls Parent	1	2	Area 1 (PBP)	38.11								38.11	38.11 65.40		35000	16.58	39.74		27.29	65.40													
npeau Drive Trunk Sewer			Area 2 (PBP)	27.29								27,29	All and a second se		50000	12.20	51.94		14.05	79.45						1 196.0	525	0.40	69.44%		0.306	0.730	
			Area 3 Ext Employment	14.05								14.05		90.38		9.49	61.42	61.42	10.93	90.38	90.38	25.31	86,73	283.79	1.27	525.0	2421	0.40	42.4473	3,65			
	-		Area 4 HP Employment	10.93								10.93	90.38		30000		10111	61.42	29.19	29.19						700.0	600	0.20	54.93%	4.44	0.451	0.830	-
			Area S Residential	29.19	29.19	19	555	1664	1664	3.65	24.58		8,45	90.38 98.83	50000	7.34	7.34	68.76	8.45	128.02	128.02	35.85	129.18	286,61	0.98	8 700.0	600	0.20	34.9390		0,701	0.00	<u> </u>
	2		Area 9 Ext Employment	8.45							24.58	8.45	and the second second			14.45	14.45		16.65	16.65					14				82.92%		0.171	0.630	
		-	Area 6/8 Ext Employment.	16.65			194 - L					16.65			50000	4.76	19.21	19.21	5,48	22.13	22.13	6.20	25.41	148,74		1 910.0				1.65	0.394	0.790	
and the second	14		Area 7 HP Employment	-5.48	0				(C)			5.48				0.00	0.00	87.97	0.00	0.00	150.15	42.04	154.59	392.29		6 300.0			the second se	165	0.211	0,650	
-			Juca / In Langier Junio						1664			0.00	0.00	120.96		0,00			27.86	27,86	27.86	7.80	31.36	148.74		1 750.0	450			3.38	0.481	0.840	
	3	4	Area 10 Residential	27.86	27.86	19	529	1588	1588	3.66	23.55		C			1.44	1.44	89.41	4.13	4.13	182.14	51,00	188.58	392.29	1.00	6 450.0	675	0.20	51.93%	3.30	0,401	0.040	-
	4A	4	14 Mixed Use	4.13	1.76				3515	3.38	48.17	2.37						1.96	6.35												0.507	0.040	
	4	5	the second se	6.35								6.35				3.86	3,86	7.98	11.80	18.15	18.15	5.08	24.88	43.88	. 0.8	7 420.0	250	0,50	43.31%	3.86	0.567	0.860	-
9	teensway	5	Area 13 Community Retail	11.80	5.02	50	251	752	752	3.88	11.81	6,79	And and a design of the local division of the local division of the local division of the local division of the	13.14			1.78	1.20	3.88											3,31	0.450	0.040	-
•			Area 11/12 Mixed Use	. 3.88	5.04			0	4267	3.31	57.19	3.88			35000	2.36	17.88	115.27	25.54	29,42	229.71	64.32	236.77	519.43	1,14	4 300.0	750	0.20	54.42%		0,456	0.830	-
	5	5A	Area 15 Community Retail	25.54							57.19	25,54	29.42	165.89	35000	15.52	17,88		43.34	23.94		64.32	236,77										-
nst Line Road Sewer			Area 44								\$7.19							115.27				United the	and the		•					3.23			-
71				229.71	00.00	10	1714	5141	5141	3.23	67.35	0.00							05.00	95.08	95.08	26.62	98.21						(-
gnature Ridge		5A	Area 100 Residential	90.20	90,20	19	1/14	2141			67.35	4,88	4.88	4,88	50000	4.24	4,24	4.24	95.08	95.00	35.04	40,04	65 00		12. 11								
gnature Ridge		5A	Area 100 Non-Residential	4,88					-		AL MAR					-					791.00	00.04	399.98	580.53	. 1.2	7 30.0	750	0.25	31.10%	2.98	0.689	0.940	
tersticial Lands & Broughton/Richardson		5A			1 1 1 1 1 1		212/		9409		124.54	170.77						. 119.51			324.79	90.94	399.90	330.33	A.44					1			
otal To SRPS	5A	SRPS		324.79	154.02		3136		9409		- AA4.54						1	1.1.1						+			1			1			1
																														1			1
													57.03		50000	49.51	49.51		57.03						10	-						100	1
U. U. Dalas Brack Savar	6	7	Area 32 (FBP)	57.03								57.03	and the second division in which the second division in the second din the second division in the second division		0	0.00	49.51		8.34							-	-						1
dladium Drive Trunk Sewer			Area 32A Park	8.34								8.34 54.85			50000	47.61	97.12	- 97.12	54,85	120.22	120.22				0	12 020	0 675	0.27	57.69%	3.53	0.423	0.810	
			Area 33/34 Ext Employment	54.85												18.32	18.32	115.44	36,70	36,70	156.92	43,94	192.85	455.83	1.2	13 925.0	0/5	0.27	51.0378	3.53			1
	7	8	Arcs 37 Mixed Use	36.70	15.60	50	780	2340				21.10	and the second se	141.32	50000	a second		115.44			156.92	43.94	192.85					<u> </u>		1			1-
		0	10 00 V 10 10 10 10 10 10 10 10 10 10 10 10 10	156.92	15.60		780		2340		33.47	141.33			20000	3.15	3.15	and a state of the	6.05			Ĩ				-				()			1-
			Area 35 HP Employment	6.05	1							6.05	6.05		30000	3.13	2.10					30.00				-	1	↓ ′		(—)			+
Corel Centre Etc. (Existing Sewer) *		16	Area 36 (Corel Centre)	1	1					1.000				-	14400	5.04	8.19	8.19	20.15	26.20	26.20	7,34	45.52				Relating	<u> </u>		()			-
		16	Area 38 Exten Employment	20.15	-					1		20.1		and the second division of the local divisio		8.87	8.87	0.17	14.59	the state of the s				54			1 1						1
		16		14:59								14.55			35000		16.14		11.97					i		1	1 0	1 /					1-
first Line Road Sewer	15	16	Area 40 Employment	11.97	1	1						11.9			35000	7,17			20.66							-	James I	J		(<u> </u> '	0.001	0.74	-
			Area 41 Employment	20.66								20.6			35000	12.55	28.69	46.25			76.11	21.31	67.56	224.35		00 525.					0.301	. 0.73	
	-		Area 42 Employment	20.00	-		-		1			28.8				17.55		46.23			102.31	28.65	113.08	286.61		98 400.				3.53			
		-	Area 43 Employment	102.31	15.6	0	780		2340	3.53	33,47	102,3				0.00	54.44		0.00		259.23	109.92		579.95	1.0	05 550.	0 825	0,15	47.25%	3.53	0.528	0.86	1
Carp River Trunk	16		Nothing To Add		15.6		780		2340		33,47	0.0	0 0.00	243.63		0.00	0.00	169.87	0.00	122.01	ALC: Y LAND												-
Carp River Trunk	8	10A	Nothing To Add	259.23	13.61		100												1 12.00	23.34			1							3.72			-
						1 0	10	1250	1330		i								23.34		102.66	28.74	132.56	405.11	1.3	39 775.	.0 600	0.40	67.28%	3.03	0.327	0.74	0
Marle Grove Road Trunk Sewer	9	10	Area 18/19 Exist. Residential	23.34	23.3		0 2380	7139	9 8465	3.03	103.82	1					-	_	79.32	104.00	*04/00	AGUTA					1						-
	1.000		Area 22/26/27 Residential	79.32	19.3		100	1133				1							00.01	00.01										3.20			_
				-	-	1 0	1 1901	5644	4 5644	3.20	73.06			1					99.01														-
Hazeldean/Huntmar Trunk Sewer	11	12	Area 16/20 Residential	99.01	99.0	1 1	9 1881	3044	1	0.40	10140	33.5	0 33.50	33.50	50000	29.08	29.08	29.08					1.000										-
			Area 16/20 Commercial	33.50								14.1							14.13			42.02	146.26	\$54.82	1.2	50 775	.0 675	5 0.40	73,64%	4	0.264	0.70	0
			Area 16/20 Open Space	14.13 8		++					73.06			36.9		2.09	31.17	31.17			and the second se	44.02	140.20										
			Area 17 Ex. Commercial	3,44							1,5144	10.8			50000	9.45	9.45		10.89														
	12	10	Area 21 Exist. Employment	16.89	-	-			0			1					9.45		6.63														_
			Area 19A Exist Residential	6.63	6.6	3 1	9 126	5 37	0			17.6	1 28.5	0 28.5	35000	10.70	20.15	51.32				59.45	214.49	519.43	1.	14 950	.0 750	0 0.20	58.71%	3.03	0.413	0.80	0
			Ares 23/24 Community Retail	17.61					9 846	3.0	103.72	0.0						51.32			. 212.31	39.43	A14,42	1									
· · · · · · · · · · · · · · · · · · ·	-		Area 28/30 Residential	27.10	27.1		0 813		and the second se	3.4.	103./1	12.1			9 35000	7.38	7.38	58.71				98.31	368.56	669,89	1	21 1000	.0 82.5	5 0.20	44.98%	6 2.66	0,550	0.87	0
Marle Grove Road Trunk Sewer	10	10A	Area 39 Mixed Use	21.13	8.5		0 449		10.00	7 2.6	6 211.54	14.1	40,1					58.71			351.10	98,31	305.30	607.89				1	T	1			
SHOTE MORE ALLER OFTIG			Area 29 Residential	15.00	15.0	10 3	0 450	0 135	0 1962	2.0	411.34	30.7	24 20.2	4 20.2	4 35000	12.30	12.30	12.30	20,24				76.61	320.17	1	10 1000	600	0 0.25	5 76.07%	3.39	0.239	0.68	0
Garp River Trunk Sewer	13	10A	Area 25 Community Retail	20.24			-				47.80		40.2		-	1	4	12.30				16.51	And and a second se			72 100				1	0.023		0
SAVE THUR DEWEL		140	Area 31 residential	38.72	38.1	72 3	10 1162	2 348	348	5 3,3	47.80	0,5	75 0.7	5 0.7	5 50000	0.65	0.65	0.6	s 0.75	0.75	0.75	0.21	0.86	36.69		100	430			11	1	1	1
91 ³		10A	Area 31A (PBP)	0.75								4,1	0.1		-						-					10	0 1050	0.7/	40.39%	2.55	0.596	0.90	
12		in							1									241.53	5		670.04	224.95	759.29	1273.71	1.4	43 30.	U 1050	0 0.20	40.39%	2.5	0.096	0,90	-
Den 1 di di ante ante	101	Trume		670:04	313.7	0	8484	\$	2545	1	292.82	356.3	4					242100					1.2.2		+	1.2	10	-		-			-
Pumping Station 2 to KWPS	10A	KWPS		070.04			-		1		1	1								1					Logi -		_			241			1
												1 100		1									the second second	_									
TUDY TOTALS				994.83	467.3	73	11620	0	3486	0		527.	11		_								Revision No	o. 1: April 01	1-2005	Revisio	HI NO. 6:	Oct. 14, 24	005				

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 Strings Daily Per capita Flow Rate =
 350 V/cap/d

 Offrigin Allowance Flow Rate =
 0.28 V/sec/Ha

 Strings Daily Per capita Flow Rate =
 0.28 V/sec/Ha

 Strings Daily Per capita Flow Rate =
 0.28 V/sec/Ha

 Strings Pactor = 1+(14/(4+(P^0_5))), P=Pop. in 1000's, Max of 4

 Strings Daily Per capita Flow Rate =
 3.00

 Strings Pactor = 1+(14/(4+(P^0_5))), P=Pop. in 1000's, Max of 4

 Strings Pactor = 1+(14/(4+(P^0_5))), P=Pop. in 1000's, Max of 4

 Strings Pactor = 1-(15)

 Strings Pactor = 1.50

 antml:image>data:image/s3,anthropic-data-us-east-2/u/marker_images/sfishman-markermapper-09261316/ea4a4bd0ab0d9a6381a74759c685a5cf.jpeg</antml:image>

Revision No. 2: April 11, 2005 Revision No. 3: April 21, 2005 Revision No. 4: June 07, 2005 Revision No. 5: August 10, 2005

PAGE 1 OF 1 PROJECT: 3599-LD-03 DATE: April 2005 DESIGN: J1M FILE: 3598LD.sewers.XLS

 Revision No. 7:
 Nov. 10, 2005

 Revision No. 8:
 Nov. 11, 2005

 Revision No. 9:
 Apr. 19, 2006

FIG. 4.2-1

SANITARY SEWER DESIGN SHEET PROJECT : Kanata West Servicibility Stury LOCATION : CITY OF OTTAWA

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PHASE 1 SIGNATURE RIDGE (population based criteria..ICI simultaneous peaking)

LOCATI STREET FROM MH Campeau Drive Trunk Sewer 1 2 14	то мн 2 3	Area 1 (PBP) Area 2 (PBP) Area 3 Ext Employment Area 4 HP Employment Area 5 Residential	TOTAL AREA (Ha) 0.00 0.00 0.00	APPLIC AREA (Ha)	UNIT/Ha				PEAK FACTOR	PEAK FLOW (Vs)	APPLIC AREA (Ha)	ACCUM AREA (Ha)	TOTAL AREA	FLOW RATE	INDIV	PEAK FLOW	TOTAL		REA (Ha) CUMUL	TOTAL	PEAK FLOW	FLOW	CAPACITY	VELOCITY (full)	LGTH.			AVAIL. CAP.
Zampeau Drive Trunk Sewer 1		Area 2 (PBP) Area 3 Ext Employment Area 4 HP Employment Area 5 Residential	(Ha) 0.00 0.00 0.00 0.00	AREA						FLOW	AREA	AREA		RATE			TOTAL	INDIV	CUMUL	TOTAL	FLOW	1 1		(full)			-	CAP.
Zampeau Drive Trunk Sewer 1		Area 2 (PBP) Area 3 Ext Employment Area 4 HP Employment Area 5 Residential	0.00 0.00 0.00 0.00	1 11 1 1 1					2				(11-)															
Campeau Drive Trunk Sewer 1	2	Area 2 (PBP) Area 3 Ext Employment Area 4 HP Employment Area 5 Residential	0.00 0.00 0.00 0.00					*	. V.		and a second		(Ha)	(l/Ha/d)	(l/s)	(Vs)	(I/s)			CUMUL	(1/s)	(l/s)	1/s	mis	(m)	(mm)	%	(%)
2	23	Area 2 (PBP) Area 3 Ext Employment Area 4 HP Employment Area 5 Residential	0.00 0.00 0.00																				[]				-	
2	3	Area 3 Ext Employment Area 4 HP Employment Area 5 Residential	0,00 0,00								0,00	0.00		35000	0.00			0.00	0.00				F					<u></u>
	3	Area 4 HP Employment Area 5 Residential	0,00								0.00			35000	0.00			0.00	0.00				F					1
	3	Area 5 Residential									0.00			50000	0.00			0.00	0.00		0.00	0.00	283.79	1.27	500.0	525	0.40	100.00%
	3										0.00	0.00		50000	0,00	0.00	0.00		0.00	and the second se	. 0.00	0.00	403.17	1.27	500.0	125	0.40	100.00%
14			29.19	29.19	19	555	' 1664	1664	3.65				0.00			121	0.00		29.19		0.10	20.00	286.61	0.98	700.0	600	0.20	88.57%
14		Area 9 Ext Employment	0,00							24.58				50000	0.00		0.00		0.00		8.17	in the second se	1	0.98	100.0	000	0,20	
	3 8	Area 5/8 Ext Employment	0.00								0.00			50000	0.00		0.00		0.00		• 0.00	0.00	148.74	0.91	920,0	450	0.00	L00.00%
		Area 7 HP Employment	0.00								0.00			50000	0.00		0.00		0.00		1				920.0		0.25	83,68%
3	4				•			1664				0.00	0.00		0.00	0.00	0.00		0.00		8.17				750.0			7,76%
44	4	Area 10 Residential	27.86	27.86	19	529	1588	1588										27.86	27,86		• 7.80				600.0		0.25	66.74%
	5	14 Mixed Use	4.13	1.76	50	88	263	3 3515	3.38	48.17				35000	1.44		1.44		4.13	61.18	17.13	66.74	200.07	0.90	000.0	750	0.20	00.747
Corel Centre Etc. (Existing Sewer)	15	Area 35 HP Employment	6.05								6.05	6.05		30000	3,15	3.15		6.05				[]	[]	ł				
		Area 36 (Corel Centre)	1																	0.000	30.00		↓	ł		Existing		
		Area 38 Exten Employment	20.15								20.15				5.04		8.19	in the second se	26.20		1.39	43.32	(<u> </u>	(`	Childrig		
First Line Road Sewer	15	Area 40 Employment	14.59				S				14.59			35000	8.87			14.59	14.59			[]	[]	·				
		Area 41 Employment	11.97					1			11.97			35000	7.27			11.97	26.56			[]	<u> </u>					
		Area 42 Employment	20.66					5.			20.66			35000	12.55	28.69		20.66	47.22 76.11		21.31	67.56	100.21	0.88	694.0	375	0.30	32.59%
		Area 43 Employment	28.89	1							28.89	76.11	76.11	35000	17.55	46.25	46.25		70.11	102.31	58.65				230.0		0.47	44.54%
Totals South Of Ousensway To SRPS 15	5A		102.31	0.00		0		0		0.00	102.31						54.44	the second s			36,03	113,00	203.30	4,61	200.0	4.50		99.097
Queensway	5	Area 13 Community Retail	6.35								6.35			35000	3.86	58.29		6.35	6.35		63.73	137.96	203.90	1.24	420.0	450	0.47	32,3496
		Area 11/12 Mixed Use	11.80	5.02	50	251	752	2 753	3.88	11.8	6.79		and the second se	35000	4.12	to an	62.42		18.15		03,73	137.90	203.90	1.49	430.0	420	0.42	38,3470
5	5A	Area 15 Community Retail	3.88								3,88			35000	2.36			3.88	124.34		89.10	230.81	519.43	111	300.0	750	0.20	55.56%
		Area 44	25.54							59.91	25.54	144.87	268.20	35000	15.52	81.73	81.73	25.54	149.88	211.00				1.14	200.0	750	0.20	33.307
			149.88			(1								63.73	63.73		[]		-		
Heritage Hills	纳	Area 100 Residential	90.20	90.20	19	1714	\$14	1 5141	3.2	67.3					1000 C			90.20			26.62	00.01	[]					
Heritage Hills	SA.	Area 100 Non-Residential	4.88							67.3	4.88	4.88	4.88	50000	4.24	4.24	4.24	4.88	95,08	95.08	20.02	98.21	<u></u>					
Broughton-Richardson / Interstitial	5A					4																		1.00	10.0	770	0.00	25 020
	SRPS		306.14	154.03		3136		9409		127.33	152.12						85.97	10-01-0-1-0-1-0-1-0-1-0-1-0-1-0-1-0-1-0	-	306.14	115.72	394.02	625.68	the second s	A	750	0.29 pril 11, 2005	37.03%

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Average Daily Per capita Flow Rate = 350 Voap/d Infiltration Allowance Flow Rate = 0.28 Veco/Ha Residential Peaking Factor = 1+(14/(4+(P^0.5))), P=Pop. in 1000's, Max of 4 Population density per unit = 3.00 P. F. For Employment/Retail/Business Park = 1.50 Mixed Uses Assumes: 15% Community Retail, 42.5% Business Park and 42.5% Residential

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Note: Sewer from node 5 to SRPS is existing and is to be replaced.

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Revision No. 1.	Mptu 11, 2003
Revision No. 2;	April 20, 2005
Revision No. 3:	June 07, 2005
Revision No. 4:	Oct. 14, 2005
Revision No. 5:	Feb. 15, 2006

FIG. 4.2-2

Appendix D

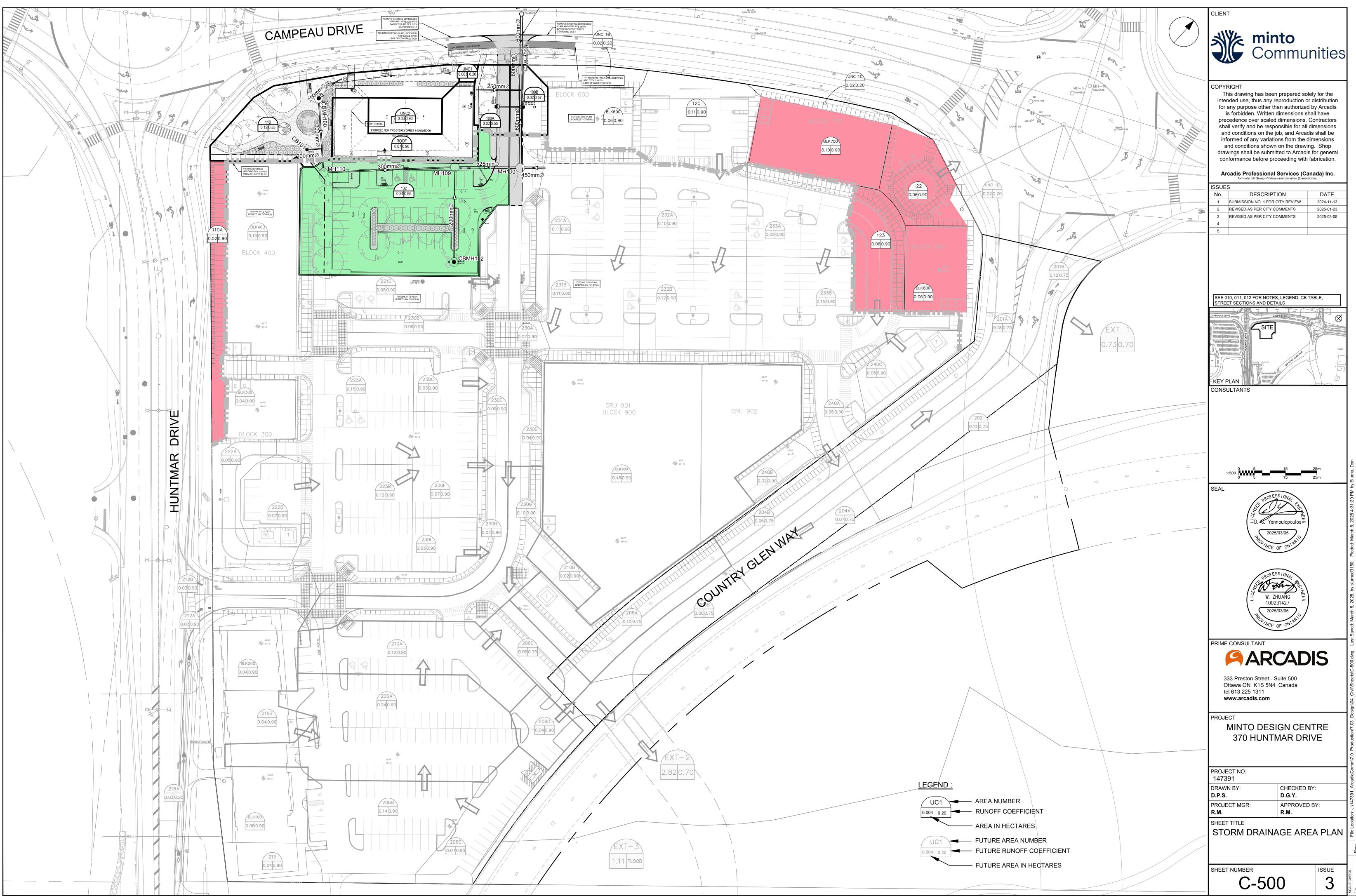
Storm Sewer Design Sheet Storm Drainage Area Plan 147391-C-500 Ponding Plan 147391-C-600 Storm Water Management Sheet Orifice Sizing Calculations Overflow Depth Calculations Runoff Coefficient Calculations Stormtech Chamber Specifications Watts Adjustable Flow Control for Roof Drains Storm Sewer Design Sheet 35355 Storm Drainage Area Plan 35355-C-500



	LOCATION							AREA	A (Ha)												RATION	NAL DESIG	FLOW											SEW	ER DATA			
				C=	C=	C=	C=	C=	C=	C= (C= C:	= C=	= IND) CUI	INLE	TIME	Е ТОТИ	∖L i(2)	i (5)	i (10)	i (100)	2vr PEAK	5vr PEAK	10vr PEAK	100yr PEAK	FIXED	FLOW	DESIGN	CAPACIT	Y LENGTH		PIPE SIZE	E (mm)	SLOPE	VELOCITY	AVAIL 0	CAP (2yr)
STREET	AREA ID	FROM	то	0.20	0.25	0.40	0.50	0.55	0.57	0.69 0	.70 0.8	85 0.9	0 2.78	AC 2.78	AC (min	IN PIF	PE (min) (mm	/hr) (r	mm/hr)	(mm/hr)	(mm/hr)	FLOW (L/s)	FLOW (L/s)	FLOW (L/s	FLOW (L/s)			FLOW (L/s)		(m)		A W	Ú	Н (%)	(m/s)	(L/s)	
Arcadia Comme	ercial Site																																					
SITE PLAN	110	MH111	MH110	-				0.12					0.1	8 0.1	3 10.00	0.45	10.4	5 76	01 1	104 10	122.14	178.56	14.00	19.12	22.41	32.76	0.00	0.00	14.09	63.80	23.85	300			0.40	0.874	49.71	77.91%
OTLIEAN	110		MH109					0.12				0.1		5 0.4		0.40						174.51		44.17	51.77		0.00	0.00	32.57	63.80	42.19	300			0.40	0.874	31.23	
		CBMH102	2 MH109								0.2	24	0.5	7 0.5	7 10.00	0.63	10.6	3 76	81 1	104.19	122.14	178.56	43.56	59.09	69.27	101.26	0.00	0.00	43.56	133.02	30.43	450)		0.20	0.810	89.46	67.25%
	102	MUIAOO	MH100										0.0	0 10	0 11.26	0.44	11.6	0 70	20	07.00	444.00	167.82	70.05	98.06	114.92	167.95	0.00	0.00	72.35	179.46	20.96	525	-		0.40	0.803	407.40	59.69%
	102	MH109	MH100										0.0	0 1.0	J 11.20	0.44	11.0	9 72	29	97.98	114.83	167.82	72.35	98.06	114.92	167.95	0.00	0.00	72.35	179.46	20.96	525	>		0.16	0.803	107.12	59.69%
-		CAP	MH100									0.1	7 0.4	3 0.4	3 10.00	0.15	10.1	5 76	81 1	104.19	122.14	178.56	32.67	44.32	51.95	75.95	0.00	0.00	32.67	148.72	8.00	450)		0.25	0.906	116.05	78.03%
		BLDG	SEWEF	2									0.0	0.0	0 10.00	0.19	10.1	9 76	81 1	104.19	122.14	178.56	0.00	0.00	0.00	0.00	0.00	0.00	0.00	62.04	14.31	250)		1.00	1.224	62.04	100.00%
		MU100	MH100E	,									0.0	0 1.4	3 11.69	0.61	12.3	1 70	96	96.02	112.52	164.43	101.06	136.94	160.47	234.50	0.00	0.00	101.06	248.09	31.23	600	<u>`</u>		0.15	0.850	147.03	59.27%
		IVIH I UU	IVIH TUUE	>									0.0	0 1.4	5 11.0	0.01	12.3	1 70	00	90.02	112.52	104.43	101.06	130.94	100.47	234.50	0.00	0.00	101.06	240.09	31.23	600	,		0.15	0.650	147.03	59.27%
	100A, 100B	MH100B	EX CAP					0.02	0.02				0.0	6 1.4	9 12.3	0.03	12.3	4 68	96	93.41	109.44	159.91	102.63	139.03	162.90	238.01	0.00	0.00	102.63	248.09	1.50	600)		0.15	0.850	145.45	58.63%
																																600)					
Definitions:				Notes:											Design	d:						No.						Rev	ision							Date		
Q = 2.78CiA, where:				1. Mar	nnings c	oefficien	nt (n) =	0.013														1					Submission	No. 1 for	City Review							2024-11-13		
Q = Peak Flow in Litre					-																	2					Submission		- ,							2025-01-23		
A = Area in Hectares															Checke	d:						3					Submission	No. 3 for	City Review							2025-03-05		
	n millimeters per hour																																					
[i = 732.951 / (TC+ [i = 998.071 / (TC+		2 YEAR 5 YEAR													Dwg R	ference:	147391	- 500																				
[i = 1174.184 / (TC		10 YEAR													Bwg. R		147.551	000					File Re	ference:					Dat	te:						Sheet No:		
[i = 1735.688 / (TC		100 YEAF																						-6.04.04					2024-							1 of 1		

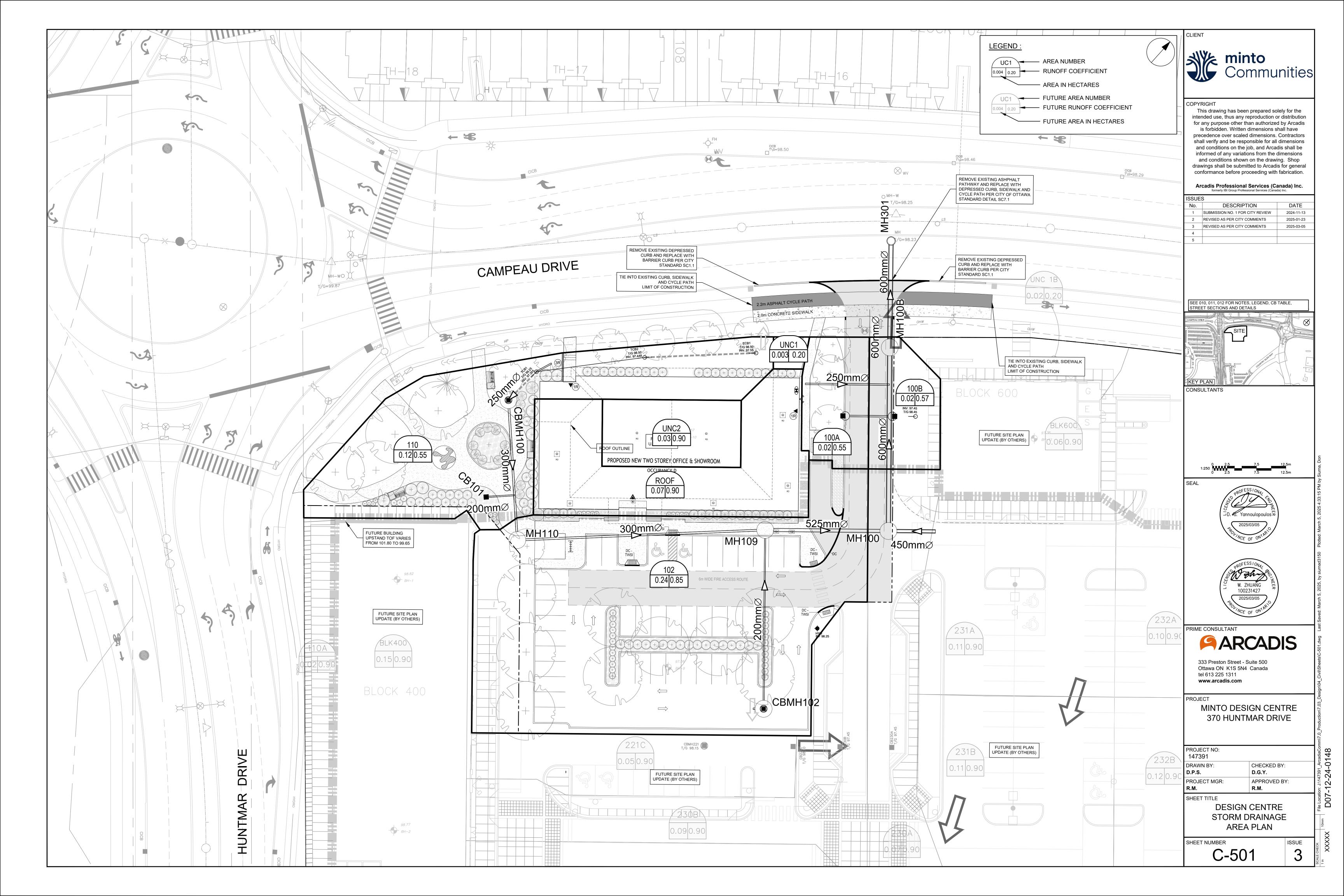
STORM SEWER DESIGN SHEET

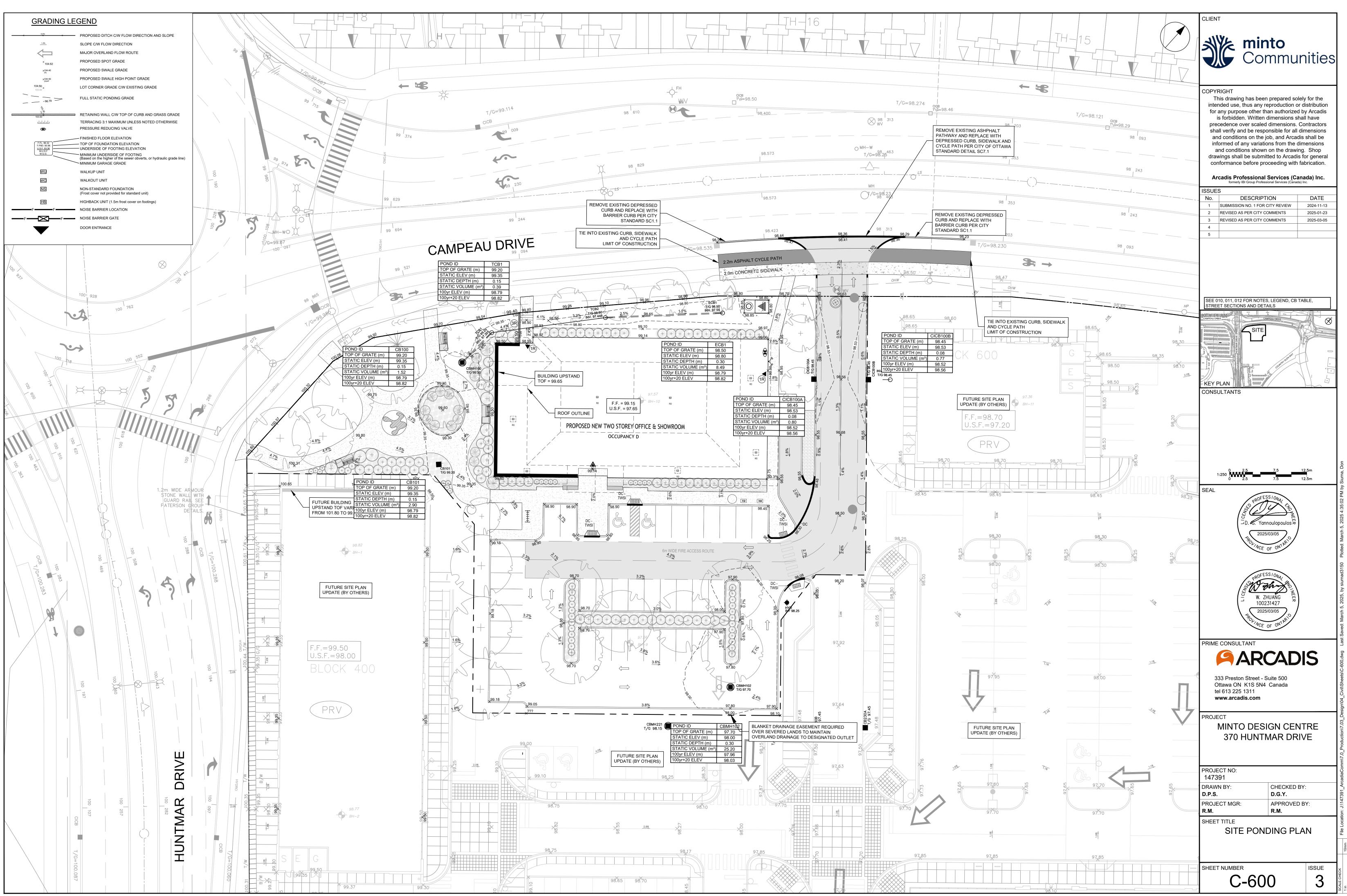
147391 - Arcadia Commercial Site CITY OF OTTAWA Minto Properties



 CHECK
 File Location: J:/147391_ArcadiaComm/7.0_Production/7.03_Design/04_Civil/Sheets/C-500.dwg
 Last Saved: March 5, 2025, by siumad3150
 Plotted: March 5, 2025.

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 File Location: J:/147391_ArcadiaComm/7.0_Production/7.03_Design/04_Civil/Sheets/C-600.dwg
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Formulas and Descriptions

i_{2vr} = 1:2 year Intensity = 732.951 / (T_c+6.199)^{0.810}

 i_{5vr} = 1:5 year Intensity = 998.071 / $(T_c + 6.053)^{0.814}$

 i_{100yr} = 1:100 year Intensity = 1735.688 / (T_c+6.014)^{0.820}

 T_c = Time of Concentration (min)

C = Average Runoff Coefficient

A = Area (Ha)

OO

Q = Flow = 2.78CiA (L/s)

Maximum Allowable Release Rate

Restricted Flowrate

Per the previously completed SWM calculations for the overall commercial site development, the total flow to Outlet #2 (Ex. MH301) is calculated at 125.94 L/s.

Q_{restricted} = 125.94 L/s

Uncontrolled Release (Q_{uncontrolled} = 2.78*C*i_{100vr} *A_{uncontrolled})

for 100-yr storm event

10 min

178.56 mm/hr

0.027 Ha

13.35 L/s

Uncontrolled Area UNC	1	Uncontrolled Roof A	rea UNC2
C ₁₀₀ =	0.25	C ₁₀₀ =	1.0
$T_c =$	10 min	$T_c =$	10
i _{100yr} =	178.56 mm/hr	i _{100yr} =	178.56
$A_{uncontrolled} =$	0.063 Ha	$A_{uncontrolled} =$	0.027
$Q_{uncontrolled 1} =$	7.82 L/s	$Q_{uncontrolled 2} =$	13.35
Q _{uncontrolled} =	21.17 L/s		

Maximum Allowable Release Rate (Q_{max allowable} = Q_{restricted} - Q_{uncontrolled})

104.77 L/s Q_{max allowable} =

STORMWATER MANAGEMENT

Arcadia Comm | Minto Properties 147391-6.0 | Rev #3 | 2025-03-05 Prepared By: MP | Checked By: RM/WZ



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MODIFIED RATIONAL METHOD (100-Year, 5-Year & 2-Year Ponding)

Drainage Area	FUT 600	T							Drainage Area	FUT 600	1			
Area (Ha)	0.06	Restricted Flow ICD	_{Actual} (L/s)=	2.00					Area (Ha)	0.06	1			
C =	1.00	Restricted Flow Q _{r for}	_{swm calc} (L/s)=	2.00	50% reduction if su	ıb-surface storage			C =	0.90	Restricted Flow Q_r (′L/s)=	2.00	
		100-Year Pond	ing			100-Y	ear +20% Po	nding			2-Year Ponding	9		
T _c Variable	i _{100yr}	Peak Flow Q _p =2.78xCi _{100yr} A	Q,	Q _p - Q _r	Volume 100yr	100YRQ _p 20%	Qp - Qr	Volume 100+20	T _c Variable	i _{2yr}	Peak Flow Q _p =2.78xCi _{2yr} A	Q _r	Q _p -Q _r	Volume 2yr
(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m ³)	(L/s)	(L/s)	(m ³)	(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m³)
69	50.33	8.40	2.00	6.40	26.48				27	42.95	6.45	2.00	4.45	7.21
70	49.79	8.30	2.00	6.30	26.48				28	41.93	6.29	2.00	4.29	7.21
71	49.26	8.22	2.00	6.22	26.48	9.86	7.86	33.48	29	40.96	6.15	2.00	4.15	7.22
72	48.74	8.13	2.00	6.13	26.48				30	40.04	6.01	2.00	4.01	7.22
73	48.23	8.05	2.00	6.05	26.48				31	39.17	5.88	2.00	3.88	7.22

	S	torage (m ³)				100+20		
Overflow	Required	Surface	Sub-surface	Balance	Overflow	Required	Balance	Overflow
0.00	26.48	33.75	0	0.00	0.00	33.48	0.00	0.00
					convert to flo	w with peak Tc (L/s)	0.00	
			. .					

overflows to: FUT 120

Calculations for future block 600 taken from overall Arcadia Commercial site plan swm calculations

Drainage Area	FUT 120								Drainage Area	FUT 120				
Area (Ha)	0.11	Restricted Flow ICD	_{Actual} (L/s)=	15.00					Area (Ha)	0.11				
; =	1.00	Restricted Flow Q _{r for}	_{swm calc} (L/s)=	15.00	50% reduction if su	b-surface storage			C =	0.90	Restricted Flow Q_r (′L/s)=	15.00	
		100-Year Pondi	ing		•	100-Y	ear +20% Po	nding			2-Year Ponding	9		
T _c Variable	i _{100yr}	Peak Flow Q _p =2.78xCi _{100yr} A	Qr	Q _p - Q _r	Volume 100yr	100YRQ _p 20%	Qp - Qr	Volume 100+20	T _c Variable	i _{2yr}	Peak Flow Q _p =2.78xCi _{2yr} A	Q _r	Q _p - Q _r	Volume 2yr
(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m ³)	(L/s)	(L/s)	(m³)	(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m³)
16	137.55	42.06	15.00	27.06	25.98				5	103.57	28.50	15.00	13.50	4.05
17	132.63	40.56	15.00	25.56	26.07				6	96.64	26.60	15.00	11.60	4.17
18	128.08	39.17	15.00	24.17	26.10	47.00	32.00	34.56	7	90.66	24.95	15.00	9.95	4.18
19	123.87	37.88	15.00	22.88	26.08				8	85.46	23.52	15.00	8.52	4.09
20	119.95	36.68	15.00	21.68	26.02				9	80.87	22.26	15.00	7.26	3.92

	St	torage (m ³)				100+20			Sto	orage (m ³)		
Overflow	Required	Surface	Sub-surface	Balance	Overflow	Required	Balance	Overflow	Required	Surface	Sub-surface	Balance
0.00	26.10	33.99	0	0.00	0.00	34.56	0.57	0.00	4.18	61.88	0	0.00
					convert to flow	w with peak Tc (L/s)	0.53					
			overflows to:	offsite							overflows to:	offsite

Calculations for future block 120 taken from overall Arcadia Commercial site plan swm calculations

STORMWATER MANAGEMENT

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Storage (I	m^3)
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Required	Surface	Sub-surface	Balance
7.22	33.75	0	0.00

overflows to: FUT 120

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Drainage Area	ROOF				_				Drainage Area	ROOF	-			
rea (Ha)	0.07	Restricted Flow ICD A	_{Actual} (L/s)=	10.00					Area (Ha)	0.07	7			
; =	1.00) Restricted Flow Q _{r for s}	_{swm calc} (L/s)=	10.00	50% reduction if su	ıb-surface storage			C =	0.90	0 Restricted Flow Q _r (L	/s)=	10.00	
		100-Year Pond	ing			100-Y	ear +20% Po	onding			2-Year Ponding]		
T _c Variable	i _{100yr}	Peak Flow Q _p =2.78xCi _{100yr} A	Q,	Q _p -Q _r	Volume 100yr	100YRQ _p 20%	Qp - Qr	Volume 100+20	T _c Variable	i _{2yr}	Peak Flow Q _p =2.78xCi _{2yr} A	Q,	Q _p - Q _r	Volume 2yr
(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m ³)	(L/s)	(L/s)	(m ³)	(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m ³)
15	142.89	27.29	10.00	17.29	15.56				4	111.72	19.20	10.00	9.20	2.21
16	137.55	26.27	10.00	16.27	15.62				5	103.57	17.80	10.00	7.80	2.34
17	132.63	25.33	10.00	15.33	15.64	30.40	20.40	20.80	6	96.64	16.61	10.00	6.61	2.38
18	128.08	24.46	10.00	14.46	15.62				7	90.66	15.58	10.00	5.58	2.35
19	123.87	23.66	10.00	13.66	15.57				8	85.46	14.69	10.00	4.69	2.25

	S	storage (m°)				100+20			
Overflow	Required	Surface	Sub-surface	Balance	Overflow	Required	Balance	-	Overflow
0.00	15.64	18.15	0	0.00	0.00	20.80	2.65		0.00
					convert to flo	w with peak Tc (L/s)	2.60		

overflows to: 102

Note: The roof storage volume was calculated by taking the following into consideration: Flat roof area = 363m2 with no obstructions (i.e. 100% of usable area), max ponding depth of 0.15m

Drainage Area	110	1							Drainage Area	110	1			
Area (Ha)	0.12	Restricted Flow ICD A	_{Actual} (L/s)=	28.00					Area (Ha)	0.12				
C =	0.69	Restricted Flow Q _{r for s}	_{swm calc} (L/s)=	28.00	50% reduction if su	ıb-surface storage			C =	0.55	Restricted Flow Q _r (L	/s)=	28.00	
		100-Year Pond	ing			100-Y	ear +20% Po	nding			2-Year Ponding	J		
T _c Variable	i _{100yr}	Peak Flow Q _p =2.78xCi _{100yr} A	Q _r	Q _p -Q _r	Volume 100yr	100YRQ _p 20%	Qp - Qr	Volume 100+20	T _c Variable	i _{2yr}	Peak Flow Q _p =2.78xCi _{2vr} A	Q,	Q _p - Q _r	Volume 2yr
(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m ³)	(L/s)	(L/s)	(m ³)	(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m ³)
4	262.41	58.18	28.00	30.18	7.24				8	85.46	15.16	28.00	-12.84	-6.16
5	242.70	53.81	28.00	25.81	7.74				9	80.87	14.34	28.00	-13.66	-7.37
6	226.01	50.11	28.00	22.11	7.96	60.13	32.13	11.57	10	76.81	13.62	28.00	-14.38	-8.63
7	211.67	46.93	28.00	18.93	7.95				11	73.17	12.98	28.00	-15.02	-9.92
8	199.20	44.16	28.00	16.16	7.76				12	69.89	12.40	28.00	-15.60	-11.23

	S	torage (m ³)				100+20			St	orage (m ³)		
Overflow	Required	Surface	Sub-surface	Balance	Overflow	Required	Balance	Overflow	Required	Surface	Sub-surface	Balance
0.00	7.96	8.49	0	0.00	0.00	11.57	3.08	0.00	0.00	8.49	0	0.00
					convert to flo	w with peak Tc (L/s)	8.55					
			overflows to:	Composu Drive	0						overflows to:	Composu Drivo

overflows to: Campeau Drive

STORMWATER MANAGEMENT

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Sto	orage (m ³)		
Required	Surface	Sub-surface	Balance
2.38	18.15	0	0.00

overflows to: 102.00

15.47

Storage	(m^3)

overflows to: Campeau Drive



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Drainage Area	102								Drainage Area	102				
rea (Ha)	0.24	1 Restricted Flow ICD A	_{actual} (L/s)=	25.00					Area (Ha)	0.24	1			
=	1.00	Restricted Flow Q _{r for s}	_{swm calc} (L/s)=	12.50	50% reduction if su	ıb-surface storage			C =	0.85	5 Restricted Flow Q _r (L	_/s)=	12.50	
100-Year Ponding 100-Year +20% Pc							% Ponding 2-Year Ponding							
T _c Variable	i _{100yr}	Peak Flow Q _p =2.78xCi _{100yr} A	Q _r	$Q_p - Q_r$	Volume 100yr	100YRQ _p 20%	Qp - Qr	Volume 100+20	T _c Variable	i _{2yr}	Peak Flow Q _p =2.78xCi _{2vr} A	Q,	Q _p -Q _r	Volume 2yr
(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m³)	(L/s)	(L/s)	(m ³)	(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m³)
44	70.18	46.82	12.50	34.32	90.62				16	59.50	33.75	12.50	21.25	20.40
45	69.05	46.07	12.50	33.57	90.64				17	57.42	32.56	12.50	20.06	20.46
46	67.96	45.34	12.50	32.84	90.65	54.41	41.91	115.68	18	55.49	31.47	12.50	18.97	20.49
47	66.91	44.64	12.50	32.14	90.64				19	53.70	30.45	12.50	17.95	20.47
48	65.89	43.96	12.50	31.46	90.61				20	52.03	29.51	12.50	17.01	20.41

	S	Storage (m ³)				100+20			St	orage (m³)		
Overflow	Required	Surface	Sub-surface	Balance	Overflow	Required	Balance	 Overflow	Required	Surface	Sub-surface	Balance
0.00	90.65	25.20	68.80	0.00	2.65	118.33	24.33	0.00	20.49	25.20	68.8	0.00
		convert to fl	low with peak Tc (L/s)	0.00	convert to flo	w with peak Tc (L/s)	8.82					
			a ,	ee							a ,	cc

overflows to: offsite

Drainage Area	MH100B	CICB100A, CICB100)B						Drainage Area	MH100B	1			
Area (Ha)	0.04	4 Restricted Flow ICD	_{Actual} (L/s)=	24.00					Area (Ha)	0.04				
C =	1.00) Restricted Flow Q _{r for}	_{swm calc} (L/s)=	24.00	50% reduction if su	ıb-surface storage			C =	0.90	Restricted Flow Q _r (L			
100-Year Ponding 100-Year +20% Ponding								onding			2-Year Ponding	g		
T _c Variable	İ _{100yr}	Peak Flow Q _p =2.78xCi _{100yr} A	Q _r	Q _p - Q _r	Volume 100yr	100YRQ _p 20%	Qp - Qr	Volume 100+20	T _c Variable	i _{2yr}	Peak Flow Q _p =2.78xCi _{2yr} A	Q _r	Q _p -Q _r	Volume 2yr
(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m³)	(L/s)	(L/s)	(m ³)	(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m ³)
1	351.38	39.07	24.00	15.07	0.90				8	85.46	8.55	24.00	-15.45	-7.41
2	315.00	35.03	24.00	11.03	1.32				9	80.87	8.09	24.00	-15.91	-8.59
3	286.05	31.81	24.00	7.81	1.41	38.17	14.17	2.55	10	76.81	7.69	24.00	-16.31	-9.79
4	262.41	29.18	24.00	5.18	1.24				11	73.17	7.32	24.00	-16.68	-11.01
5	242.70	26.99	24.00	2.99	0.90				12	69.89	6.99	24.00	-17.01	-12.24

	Storage (m ³) 100+20								St	orage (m ³)		
Overflow	Required	Surface	Sub-surface	Balance	Overflow	Required	Balance	Overflow	Required	Surface	Sub-surface	Balance
0.00	1.41	1.57	0	0.00	0.57	3.12	1.55	0.00	0.00	1.57	0	0.00
		convert to fl	low with peak Tc (L/s)	0.00	convert to flo	w with peak Tc (L/s)	8.62					
			overflows to: o	offsite							overflows to:	offsite

STORMWATER MANAGEMENT

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overflows to: offsite



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	Stormwater Management Summary Table												
Drainage Area	ICD Restricted Flow (L/s)	2 Year Storage Required (m3)	100 Year Storage Required (m3)	Storage Provided									
FUT 600	2.00	7.22	26.48	33.75									
FUT 120	15.00	4.18	26.10	33.99									
ROOF	10.00	2.38	15.64	18.15									
110	28.00	0.00	7.96	8.49									
102	25.00	20.49	90.65	94.00									
MH100B	24.00	0.00	1.41	1.57									
TOTAL	104.00	34.27	168.23	189.95									

100-yr Overflow: 100-yr Total Release Rate: 100-yr Max. Allowable Rate:

0.00 L/s 104.00 L/s 104.77 L/s TRUE

STORMWATER MANAGEMENT

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IBIGROUP ibigroup.com

500-333 Preston Street Ottawa, Ontario K1S 5N4 Canada **ORIFICE SIZING**

Arcadia Commercial Site | Minto Communities 147391-6.0 | Rev #2 | 2025-01-23 Prepared By: MP | Checked By: RM/WZ

 $Q = C_v \times A \times \sqrt{2gH}$

Orifice coefficients Cv = 0.60

		-					The	oretical	Recor	nmended
	Invert	Diameter	Centre ICD	Max. Pond Elevation	Hydraulic Slope	Target Flow	Orifice	Actual Flow	Orifice	Actual Flow
	(m)	(mm)	(m)	(m)	(m)	(l/s)	(m)	(I/s)	(m)	(l/s)
Area 110	96.952	300	97.102	98.800	1.698	28.00	0.090	28.00	0.090	28.00
Area 102	95.987	200	96.087	98.000	1.913	25.00	0.082	25.00	0.082	25.00
MH100B	96.700	200	96.800	98.530	1.730	24.00	0.083	24.00	0.083	24.00
							*Diamond Shap	e		
						77.00				77.00



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OVERFLOW DEPTH CALCULATIONS

Arcadia Comm | Minto Properties 147391-6.0 | Rev #3 | 2025-03-05 Prepared By: WZ | Checked By: RM

Overflow Area 110		_								
New Flow Section Required 1:					l/s	or		Cu m/sec		
New Flow Section Required 1:		+ 20%	o flow		., -	or		Cu m/sec		
Overflow Slope					Overflow X-S		n		Overflow Cap	
Length =	8.79	m		Side Slope 1 =	1.10				From Seelye n =	0.040 (Channels)
Up Stream Ground Elev =	98.80	m		Side Slope 2 =	1.30					2
Down Stream Ground Elev =	98.56	m		Bottom Width =	0.00				100 Year Q =	m³/s
Difference =	0.24	m			100 Yea		100 Year +		100 Year Velocity =	m/s
Ditch Slope =	2.73	%		Water depth =	0.000		0.02	m		
				X-Sect. Area =	0.00	m²	0.04	m ²	100 Y +20% Q =	0.009 m³/s
				Wetted Per. =	0.00	m	3.86	m	100 Y + 20% Velocity =	0.21 m/s
Q = A*(1.0/n)*R^2/3*S^1/2				where:	A = cross sec					
					n = friction co					
					R = hydraulic	radius	= A/wetted per	imetre (wp) i	n m	
Overflow Area 102	100	0			1/			0 /		
New Flow Section Required 1:	100 year	flow =	£1		l/s	or		Cu m/sec		
New Flow Section Required 1:		+ 20%	o TIOW			or		Cu m/sec		
Overflow Slope					Overflow X-S		n		Overflow Cap	
Length =	-	m		Side Slope 1 =	3.80				From Seelye n =	0.040 (Channels)
Up Stream Ground Elev = Down Stream Ground Elev =	-	m		Side Slope 2 = Bottom Width =	1.33				100 V 0	3,
Down Stream Ground Elev =	-	m		Bottom Width =	0.00 100 Yea		100 Year +	000/	100 Year Q =	m³/s m/s
	-	m) (/ _ +]				-	100 Year Velocity =	m/s
Ditch Slope =	1.00			Water depth =	0.000		0.03	m		
	Estimate	d		X-Sect. Area =	0.00	m²		m²	100 Y +20% Q =	0.009 m³/s
				Wetted Per. =	0.00	m	3.35	m	100 Y + 20% Velocity =	0.16 m/s
Q = A*(1.0/n)*R^2/3*S^1/2				where:	A = cross sec		•			
					n = friction co					
Owerflow Area MU400D					R = hydraulic	radius	= A/wetted per	imetre (wp) i	n m	
Overflow Area MH100B	100	0			1/			0 /		
New Flow Section Required 1: New Flow Section Required 1:					l/s	or		Cu m/sec Cu m/sec		
		+ 20%	DIIOW		-	or		Cu m/sec	0	
Overflow Slope Length =	20.00	m		Side Slope 1 =	<u>2.00 2.00 2.00</u>		11		Overflow Cap From Seelye n =	0.040 (Channels)
Up Stream Ground Elev =	20.00 98.53	m		Side Slope 1 =	2.00	% %			1 Iom Seerye II -	0.040 (Channels)
Down Stream Ground Elev =	98.23			Bottom Width =	0.00				100 Year Q =	m ³ /s
Down Stream Ground Elev =	98.23 0.30	m		BOLLOM VVIath =	100 Yea		100 Year +	20%	100 Year Q = 100 Year Velocity =	
		m %		Watar danth -				-	100 real velocity =	m/s
Ditch Slope =	1.50	70		Water depth =	0.000	m 2	0.04	m 2	400.14 0004 0	

Q = A*(1.0/n)*R^2/3*S^1/2

Wetted Per. = where:

X-Sect. Area =

A = cross sectional area in Sq. m

n = friction coefficient

0.00 m²

0.00 m

R = hydraulic radius = A/wetted perimetre (wp) in m

0.04 m²

2.06 m 100 Y +20% Q =

100 Y + 20% Velocity =

0.009 m³/s

0.22 m/s



ARCADIS IBI GROUP

500-333 Preston Street Ottawa, Ontario K1S 5N4 Canada ibigroup.com

IBI GROUP

Ave. Runoff

	110			102			100A			100B			ROOF			UNC1	
GRASS	ROOF	ASPHALT	GRASS	ROOF	ASPHALT	GRASS	ROOF	ASPHALT	GRASS	ROOF	ASPHALT	GRASS	ROOF	ASPHALT	GRASS	ROOF	ASPHAL
676.46	279.77	291.25	164.21		2194.73	116.22		117.65	118.26		129.88		857.86		37.25		
																	-
676.46	279.77	291.25	164.21	0.00	2194.73	116.22	0.00	117.65	118.26	0.00	129.88	0.00	857.86	0.00	37.25	0.00	0 0.
	1247.48			2358.94			233.87			248.14			857.86			37.25	
0.2	0.9	0.9	0.2	0.9	0.9	0.2	0.9	0.9	0.2	0.9	0.9	0.2	0.9	0.9	0.2	0.9	0.9
	0.52			0.85			0.55			0.57						0.20	
	676.46	GRASS ROOF 676.46 279.77	GRASS ROOF ASPHALT 676.46 279.77 291.25	GRASS ROOF ASPHALT GRASS 676.46 279.77 291.25 164.21	GRASS ROOF ASPHALT GRASS ROOF 676.46 279.77 291.25 164.21	GRASS ROOF ASPHALT GRASS ROOF ASPHALT 676.46 279.77 291.25 164.21 2194.73	GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS 676.46 279.77 291.25 164.21 2194.73 116.22 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 <td>GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF 676.46 279.77 291.25 164.21 2194.73 116.22 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1<</td> <td>GRASS ROOF ASPHALT GRASS Info <thinfo< th=""> <thinfo< th=""> <thinfo< th=""></thinfo<></thinfo<></thinfo<></td> <td>GRASS ROOF ASPHALT GRASS III.20 III.25 III.26 II</td> <td>GRASS ROOF ASPHALT GRASS ROOF 676.46 279.77 291.25 164.21 2194.73 116.22 117.65 118.26 1</td> <td>GRASS ROOF ASPHALT GRASS ROOF ASPHALT III6.22 III7.65 II8.26 129.88 </td> <td>GRASS ROOF ASPHALT GRASS 676.46 279.77 291.25 164.21 2194.73 116.22 117.65 118.26 129.88 129.88 </td> <td>GRASS ROOF ASPHALT GRASS ROOF 676.46 279.77 291.25 164.21 2194.73 116.22 117.65 118.26 129.88 857.86 </td> <td>GRASS ROOF ASPHALT GRASS ROOF ASPHALT</td> <td>GRASS ROOF ASPHALT GRASS ROOF ASPHALT</td> <td>GRASS ROOF ASPHALT GRASS ROOF ASPHALT</td>	GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF 676.46 279.77 291.25 164.21 2194.73 116.22 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1<	GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT Grass Info Info <thinfo< th=""> <thinfo< th=""> <thinfo< th=""></thinfo<></thinfo<></thinfo<>	GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS III.20 III.25 III.26 II	GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF 676.46 279.77 291.25 164.21 2194.73 116.22 117.65 118.26 1	GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT III6.22 III7.65 II8.26 129.88	GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS 676.46 279.77 291.25 164.21 2194.73 116.22 117.65 118.26 129.88 129.88	GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF ASPHALT GRASS ROOF 676.46 279.77 291.25 164.21 2194.73 116.22 117.65 118.26 129.88 857.86	GRASS ROOF ASPHALT GRASS ROOF ASPHALT	GRASS ROOF ASPHALT GRASS ROOF ASPHALT	GRASS ROOF ASPHALT GRASS ROOF ASPHALT

Runoff Coefficient Used(C):	0.52	0.85	0.55	0.57	0.90	0.20
	0.52	0.00	0.00	0.57	0.00	0.20

RUN-OFF COEFFICIENTS

Arcadia Comm | Minto Properties 147391-6.0 | Rev #1 | 2024-11-13 Prepared By: MP | Checked By: RM

PROJECT INFORMATION

ENGINEERED PRODUCT MANAGER	
ADS SALES REP	
PROJECT NO.	



ARCADIACOMM OTTAWA, ON, CANADA

DC-780 STORMTECH CHAMBER SPECIFICATIONS

- 1 CHAMBERS SHALL BE STORMTECH DC-780.
- 2. CHAMBERS SHALL BE ARCH-SHAPED AND SHALL BE MANUFACTURED FROM VIRGIN, IMPACT-MODIFIED POLYPROPYLENE COPOLYMERS
- CHAMBERS SHALL BE CERTIFIED TO CSA B184, "POLYMERIC SUB-SURFACE STORMWATER MANAGEMENT STRUCTURES", AND MEET 3 THE REQUIREMENTS OF ASTM F2418, "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 4. CHAMBER ROWS SHALL PROVIDE CONTINUOUS, UNOBSTRUCTED INTERNAL SPACE WITH NO INTERNAL SUPPORTS THAT WOULD IMPEDE FLOW OR LIMIT ACCESS FOR INSPECTION.
- THE STRUCTURAL DESIGN OF THE CHAMBERS. THE STRUCTURAL BACKFILL, AND THE INSTALLATION REQUIREMENTS SHALL ENSURE 5. THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET FOR: 1) LONG-DURATION DEAD LOADS AND 2) SHORT-DURATION LIVE LOADS, BASED ON THE CSA S6 CL-625 TRUCK AND THE AASHTO DESIGN TRUCK WITH CONSIDERATION FOR IMPACT AND MULTIPLE VEHICLE PRESENCES.
- CHAMBERS SHALL BE DESIGNED, TESTED AND ALLOWABLE LOAD CONFIGURATIONS DETERMINED IN ACCORDANCE WITH ASTM F2787, 6 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS". LOAD CONFIGURATIONS SHALL INCLUDE: 1) INSTANTANEOUS (<1 MIN) AASHTO DESIGN TRUCK LIVE LOAD ON MINIMUM COVER 2) MAXIMUM PERMANENT (75-YR) COVER LOAD AND 3) ALLOWABLE COVER WITH PARKED (1-WEEK) AASHTO DESIGN TRUCK.
- REQUIREMENTS FOR HANDLING AND INSTALLATION: 7.
 - TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING. CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS.
 - TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL, THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 50 mm (2").
 - TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION, a) THE ARCH STIFFNESS CONSTANT AS DEFINED IN SECTION 6.2.8 OF ASTM F2418 SHALL BE GREATER THAN OR EQUAL TO 550 LBS/FT/%. AND b) TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES (ABOVE 23° C / 73° F), CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS.
- ONLY CHAMBERS THAT ARE APPROVED BY THE SITE DESIGN ENGINEER WILL BE ALLOWED. UPON REQUEST BY THE SITE DESIGN 8 ENGINEER OR OWNER, THE CHAMBER MANUFACTURER SHALL SUBMIT A STRUCTURAL EVALUATION FOR APPROVAL BEFORE DELIVERING CHAMBERS TO THE PROJECT SITE AS FOLLOWS:
 - THE STRUCTURAL EVALUATION SHALL BE SEALED BY A REGISTERED PROFESSIONAL ENGINEER.
 - THE STRUCTURAL EVALUATION SHALL DEMONSTRATE THAT THE SAFETY FACTORS ARE GREATER THAN OR EQUAL TO 1.95 FOR DEAD LOAD AND 1.75 FOR LIVE LOAD, THE MINIMUM REQUIRED BY ASTM F2787 AND BY SECTIONS 3 AND 12.12 OF THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS FOR THERMOPLASTIC PIPE.
 - THE TEST DERIVED CREEP MODULUS AS SPECIFIED IN ASTM F2418 SHALL BE USED FOR PERMANENT DEAD LOAD DESIGN EXCEPT THAT IT SHALL BE THE 75-YEAR MODULUS USED FOR DESIGN.
- CHAMBERS AND END CAPS SHALL BE PRODUCED AT AN ISO 9001 CERTIFIED MANUFACTURING FACILITY.
- MANIFOLD SIZE TO BE DETERMINED BY SITE DESIGN ENGINEER. SEE TECH NOTE #6.32 FOR MANIFOLD SIZING GUIDANCE. DUE TO THE 10. ADAPTATION OF THIS CHAMBER SYSTEM TO SPECIFIC SITE AND DESIGN CONSTRAINTS, IT MAY BE NECESSARY TO CUT AND COUPLE ADDITIONAL PIPE TO STANDARD MANIFOLD COMPONENTS IN THE FIELD.
- ADS DOES NOT DESIGN OR PROVIDE MEMBRANE LINER SYSTEMS. TO MINIMIZE THE LEAKAGE POTENTIAL OF LINER SYSTEMS, THE MEMBRANE 11. LINER SYSTEM SHOULD BE DESIGNED BY A KNOWLEDGEABLE GEOTEXTILE PROFESSIONAL AND INSTALLED BY A QUALIFIED CONTRACTOR.

IMPORTANT - NOTES FOR THE BIDDING AND INSTALLATION OF THE DC-780 CHAMBER SYSTEM

- STORMTECH DC-780 CHAMBERS SHALL NOT BE INSTALLED UNTIL THE MANUFACTURER'S REPRESENTATIVE HAS COMPLETED A PRE-CONSTRUCTION MEETING WITH THE INSTALLERS.
- STORMTECH DC-780 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE". 2
- CHAMBERS ARE NOT TO BE BACKFILLED WITH A DOZER OR AN EXCAVATOR SITUATED OVER THE CHAMBERS. 3. STORMTECH RECOMMENDS 3 BACKFILL METHODS:
 - STONESHOOTER LOCATED OFF THE CHAMBER BED
 - BACKFILL AS ROWS ARE BUILT USING AN EXCAVATOR ON THE FOUNDATION STONE OR SUBGRADE.
 - BACKFILL FROM OUTSIDE THE EXCAVATION USING A LONG BOOM HOE OR EXCAVATOR.
- THE FOUNDATION STONE SHALL BE LEVELED AND COMPACTED PRIOR TO PLACING CHAMBERS. 4.
- JOINTS BETWEEN CHAMBERS SHALL BE PROPERLY SEATED PRIOR TO PLACING STONE. 5.
- 6 MAINTAIN MINIMUM - 150 mm (6") SPACING BETWEEN THE CHAMBER ROWS.
- 7. 467. 5. 56. OR 57
- 8. THE CONTRACTOR MUST REPORT ANY DISCREPANCIES WITH CHAMBER FOUNDATION MATERIALS BEARING CAPACITIES TO THE SITE DESIGN ENGINEER.
- ADS RECOMMENDS THE USE OF "FLEXSTORM CATCH IT" INSERTS DURING CONSTRUCTION FOR ALL INLETS TO PROTECT THE SUBSURFACE 9. STORMWATER MANAGEMENT SYSTEM FROM CONSTRUCTION SITE RUNOFF.

NOTES FOR CONSTRUCTION EQUIPMENT

- STORMTECH DC-780 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE". 1
- THE USE OF CONSTRUCTION EQUIPMENT OVER DC-780 CHAMBERS IS LIMITED: 2
 - NO EQUIPMENT IS ALLOWED ON BARE CHAMBERS.
 - WITH THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE".
 - WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT CAN BE FOUND IN THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE".
- 3. FULL 900 mm (36") OF STABILIZED COVER MATERIALS OVER THE CHAMBERS IS REQUIRED FOR DUMP TRUCK TRAVEL OR DUMPING.

USE OF A DOZER TO PUSH EMBEDMENT STONE BETWEEN THE ROWS OF CHAMBERS MAY CAUSE DAMAGE TO THE CHAMBERS AND IS NOT AN ACCEPTABLE BACKFILL METHOD. ANY CHAMBERS DAMAGED BY THE "DUMP AND PUSH" METHOD ARE NOT COVERED UNDER THE STORMTECH STANDARD WARRANTY.

CONTACT STORMTECH AT 1-800-821-6710 WITH ANY QUESTIONS ON INSTALLATION REQUIREMENTS OR WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT.

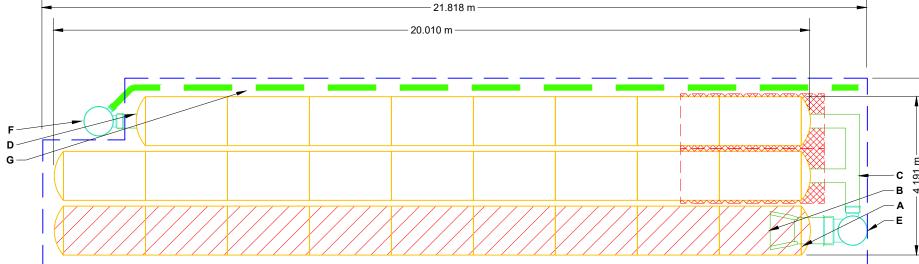




EMBEDMENT STONE SURROUNDING CHAMBERS MUST BE A CLEAN, CRUSHED, ANGULAR STONE OR RECYCLED CONCRETE; AASHTO M43 #3, 357, 4,

NO RUBBER TIRED LOADERS, DUMP TRUCKS, OR EXCAVATORS ARE ALLOWED UNTIL PROPER FILL DEPTHS ARE REACHED IN ACCORDANCE

	PROPOSED LAYOUT	CONCEPTUAL ELEVATIONS:				
26	STORMTECH DC-780 CHAMBERS	MAXIMUM ALLOWABLE GRADE (TOP OF PAVEMENT/UNPAVED):	4.648	PART TYPE	ITEM ON	DESCRIPTION
152	STORMTECH DC-780 END CAPS STONE ABOVE (mm)	MINIMUM ALLOWABLE GRADE (UNPAVED WITH TRAFFIC): MINIMUM ALLOWABLE GRADE (UNPAVED NO TRAFFIC):		PREFABRICATED EZ END CAP	Δ	600 mm BOTTOM PREFABRICATED EZ END CAP, PART#: SC740ECE; BOTTOM CONNECTIONS AND ISOLATOR PLUS ROWS
	STONE BELOW (mm) STONE VOID INSTALLED SYSTEM VOLUME (m ³)	MINIMUM ALLOWABLE GRADE (TOP OF RIGID CONCRETE PAVEMENT): MINIMUM ALLOWABLE GRADE (BASE OF FLEXIBLE PAVEMENT): TOP OF STONE:	1.448	FLAMP MANIFOLD PIPE CONNECTION		INSTALL FLAMP ON 600 mm ACCESS PIPE / PART#: SC74024RAMP 300 mm x 300 mm TOP MANIFOLD, ADS N-12
68.8	(PERIMETER STONE INCLUDED) (COVER STONE INCLUDED)	TOP OF STORE: TOP OF DC-780 CHAMBER: 300 mm x 300 mm TOP MANIFOLD INVERT:	0.991	PIPE CONNECTION NYLOPLAST (INLET W/ ISO		
105.2	(BASE STONE INCLUDED)	300 mm BOTTOM CONNECTION INVERT: 600 mm ISOLATOR ROW PLUS INVERT:	0.259	PLUS ROW) NYLOPLAST (OUTLET)		750 mm DIAMETER (610 mm SUMP MIN) 750 mm DIAMETER (DESIGN BY ENGINEER)
	SYSTEM PERIMÈTÉR (m)	BOTTOM OF DC-780 CHAMBER:	0.229	UNDERDRAIN	G	150 mm ADS N-12 DUAL WALL PERFORATED HDPE UNDERDRAIN
		UNDERDRAIN INVERT: BOTTOM OF STONE:	0.000			





PLACE MINIMUM 3.810 m OF ADSPLUS625 WOVEN GEOTEXTILE OVER BEDDING STONE AND UNDERNEATH CHAMBER FEET FOR SCOUR PROTECTION AT ALL CHAMBER INLET ROWS

- BED LIMITS

NOTES
THE SITE DESIGN ENGINEER MUST REVIEW ELEVATIONS AND IF NECESSARY ADJUST GRADING TO ENSURE THE CHAMBER OF NOT FOR CONSTRUCTION: THIS LAYOUT IS FOR DIMENSIONAL PURPOSES ONLY TO PROVE CONCEPT & THE REQUIRED STOP

*INVERT ABC	OVE BASE	E OF CHAMBER			z
	INVERT*	MAX FLOW			RUCTIO
CEZ / TYP OF ALL 600 mm	3 mm				
Р	318 mm		ΣĮ	MP	CHECKED: N/A
	30 mm		NO NO	N, CANADA DRAWN: MP	
		130 L/s IN	IAC	DR/	
		57 L/s OUT	AD	NA, C	FORL
			ARCADIACOMM	DATE: 11/05/2024 DRAWN: MI	PROJECT #:
					ATECH.COM DATE DRW CHK DESCRIPTION PROJECT #: CHECKED: N/ ON 0F THE PROJECT'S ENGINEER OF RECOMD (FOR.) OF OTHER PROJECT REPRESENTATIVE THIS DRAWING IS NOT INTENDED FOR USE IN BIDDING OR CO
					CHK SPD ("EOR") OR
					DRW
				+	
					DATE s enginee
4.0833 E 6.9833			StormTech®	Chamber System	SCALE = 1 : 100 1-800-821-6710 WWW.STORMTECH.COM DATE DRW CHK DESCRIPTION PROJECT #: CHECKED: N/A HIS DRAWING HAS BEEN PREPARED BASED ON INFORMATION PROVIDED TO ADSIGNANTICEH UNDER THE PROJECT SEGNING FOR DEEP PROJECT REPRESENTATIVE THIS DRAWING SNOT INTENDED FOR USE IN BIDDING OF ONSTRUCTION
			4640 TRUEMAN BLVD HILLIARD, OH 43026 1-800-733-7473		SCALE = 1 : 100 1-800-821-6710 WWW.STORN HIS DRAWING HAS BEEN PREPARED BASED ON INFORMATION PROVIDED OF DADSSTORMECH UNDER THE DRECTI
				SHEE	
OVER REQUIREMENTS ARE MET. RAGE VOLUME CAN BE ACHIEVED			2	OF	6

ACCEPTABLE FILL MATERIALS: STORMTECH DC-780 CHAMBER SYSTEMS

	MATERIAL LOCATION	DESCRIPTION	AASHTO MATERIAL CLASSIFICATIONS	COMPA
D	FINAL FILL: FILL MATERIAL FOR LAYER 'D' STARTS FROM THE TOP OF THE 'C' LAYER TO THE BOTTOM OF FLEXIBLE PAVEMENT OR UNPAVED FINISHED GRADE ABOVE. NOTE THAT PAVEMENT SUBBASE MAY BE PART OF THE 'D' LAYER	ANY SOIL/ROCK MATERIALS, NATIVE SOILS, OR PER ENGINEER'S PLANS. CHECK PLANS FOR PAVEMENT SUBGRADE REQUIREMENTS.	N/A	PREPARE INSTALL
C	INITIAL FILL: FILL MATERIAL FOR LAYER 'C' STARTS FROM THE TOP OF THE EMBEDMENT STONE ('B' LAYER) TO 18" (450 mm) ABOVE THE TOP OF THE CHAMBER. NOTE THAT PAVEMENT SUBBASE MAY BE A PART OF THE 'C' LAYER.	GRANULAR WELL-GRADED SOIL/AGGREGATE MIXTURES, <35% FINES OR PROCESSED AGGREGATE. MOST PAVEMENT SUBBASE MATERIALS CAN BE USED IN LIEU OF THIS LAYER.	AASHTO M145 ¹ A-1, A-2-4, A-3 OR AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57, 6, 67, 68, 7, 78, 8, 89, 9, 10	BEGIN COM THE CHAMBE 6" (150 mm) WELL GRA PROCES VEHICLE WE
D	EMBEDMENT STONE: FILL SURROUNDING THE CHAMBERS FROM THE FOUNDATION STONE ('A' LAYER) TO THE 'C' LAYER ABOVE.	CLEAN, CRUSHED, ANGULAR STONE OR RECYCLED CONCRETE⁵	AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57	
~	FOUNDATION STONE: FILL BELOW CHAMBERS FROM THE SUBGRADE UP TO THE FOOT (BOTTOM) OF THE CHAMBER.	CLEAN, CRUSHED, ANGULAR STONE OR RECYCLED CONCRETE⁵	AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57	PLATE CON

PLEASE NOTE:

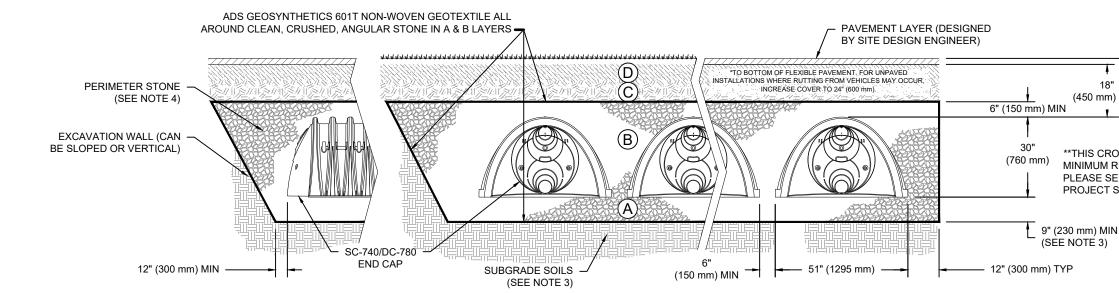
1. THE LISTED AASHTO DESIGNATIONS ARE FOR GRADATIONS ONLY. THE STONE MUST ALSO BE CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR NO. 4 (AASHTO M43) STONE".

2. STORMTECH COMPACTION REQUIREMENTS ARE MET FOR 'A' LOCATION MATERIALS WHEN PLACED AND COMPACTED IN 9" (230 mm) (MAX) LIFTS USING TWO FULL COVERAGES WITH A VIBRATORY COMPACTOR.

3. WHERE INFILTRATION SURFACES MAY BE COMPROMISED BY COMPACTION, FOR STANDARD DESIGN LOAD CONDITIONS, A FLAT SURFACE MAY BE ACHIEVED BY RAKING OR DRAGGING WITHOUT COMPACTION EQUIPMENT. FOR SPECIAL LOAD DESIGNS, CONTACT STORMTECH FOR COMPACTION REQUIREMENTS.

4. ONCE LAYER 'C' IS PLACED, ANY SOIL/MATERIAL CAN BE PLACED IN LAYER 'D' UP TO THE FINISHED GRADE. MOST PAVEMENT SUBBASE SOILS CAN BE USED TO REPLACE THE MATERIAL REQUIREMENTS OF LAYER 'C' OR 'D' AT THE SITE DESIGN ENGINEER'S DISCRETION

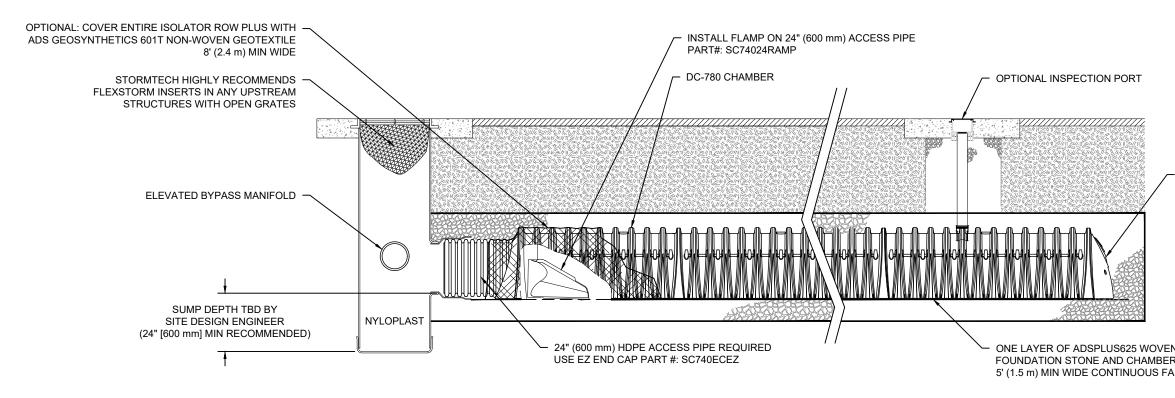
5. WHERE RECYCLED CONCRETE AGGREGATE IS USED IN LAYERS 'A' OR 'B' THE MATERIAL SHOULD ALSO MEET THE ACCEPTABILITY CRITERIA OUTLINED IN TECHNICAL NOTE 6.20 "RECYCLED CONCRETE STRUCTURAL BACKFILL".



NOTES:

- 1. CHAMBERS SHALL MEET THE REQUIREMENTS OF ASTM F2418, "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 2. DC-780 CHAMBERS SHALL BE DESIGNED IN ACCORDANCE WITH ASTM F2787 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 3. THE SITE DESIGN ENGINEER IS RESPONSIBLE FOR ASSESSING THE BEARING RESISTANCE (ALLOWABLE BEARING CAPACITY) OF THE SUBGRADE SOILS AND THE DEPTH OF FOUNDATION STONE WITH
- CONSIDERATION FOR THE RANGE OF EXPECTED SOIL MOISTURE CONDITIONS. REFERENCE STORMTECH DESIGN MANUAL FOR BEARING CAPACITY GUIDANCE.
- 4. PERIMETER STONE MUST BE EXTENDED HORIZONTALLY TO THE EXCAVATION WALL FOR BOTH VERTICAL AND SLOPED EXCAVATION WALLS.
- 5. REQUIREMENTS FOR HANDLING AND INSTALLATION:
 - TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING, CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS.
 - TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL, THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 2".
 - TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION, a) THE ARCH STIFFNESS CONSTANT SHALL BE GREATER THAN OR EQUAL TO 550 LBS/FT/%. THE ASC IS DEFINED IN SECTION 6.2.8 OF ASTM F2418. AND b) TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES (ABOVE 73° F / 23° C), CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS.

2024 DRAWN: MP CHECKED: N ARCADIACOMM PACTION / DENSITY REQUIREMENT ARE PER SITE DESIGN ENGINEER'S PLANS. PAVED LLATIONS MAY HAVE STRINGENT MATERIAL AND PREPARATION REQUIREMENTS. MPACTIONS AFTER 12" (300 mm) OF MATERIAL OVER 11/05/2024 BERS IS REACHED. COMPACT ADDITIONAL LAYERS IN n) MAX LIFTS TO A MIN. 95% PROCTOR DENSITY FOR RADED MATERIAL AND 95% RELATIVE DENSITY FOR ESSED AGGREGATE MATERIALS, ROLLER GROSS PROJE DATE: WEIGHT NOT TO EXCEED 12,000 lbs (53 kN). DYNAMIC FORCE NOT TO EXCEED 20,000 lbs (89 kN). NO COMPACTION REQUIRED. COMPACT OR ROLL TO ACHIEVE A FLAT SURFACE.^{2,3} SCRIPT Ш ㅎ DRW DATE 12' HCHL 18' (3.7 m) (450 mm) MIN* MAX **StormTech[®]** **THIS CROSS SECTION DETAIL REPRESENTS Chamber System MINIMUM REQUIREMENTS FOR INSTALLATION. PLEASE SEE THE LAYOUT SHEET(S) FOR PROJECT SPECIFIC REQUIREMENTS. 4640 TRUEMAN BLVD HILLIARD, OH 43026 1-800-733-7473 4640 HILLI SHEET 3 OF 6



DC-780 ISOLATOR ROW PLUS DETAIL

NTS

INSPECTION & MAINTENANCE

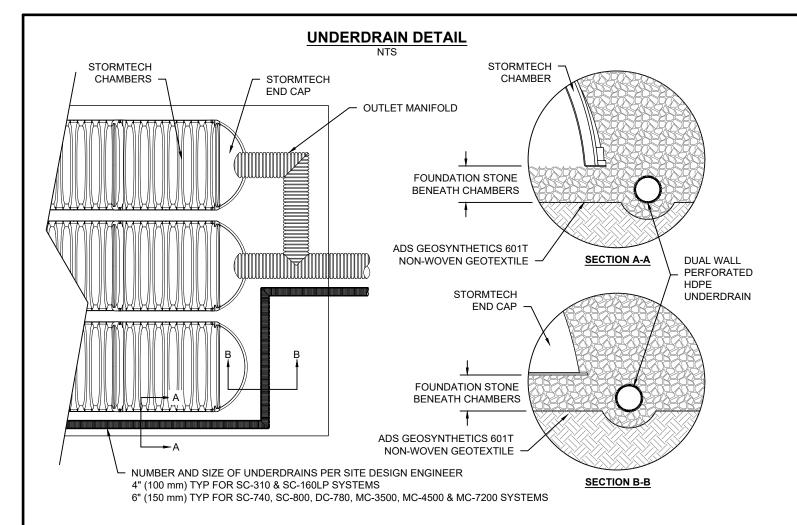
STEP 1) INSPECT ISOLATOR ROW PLUS FOR SEDIMENT

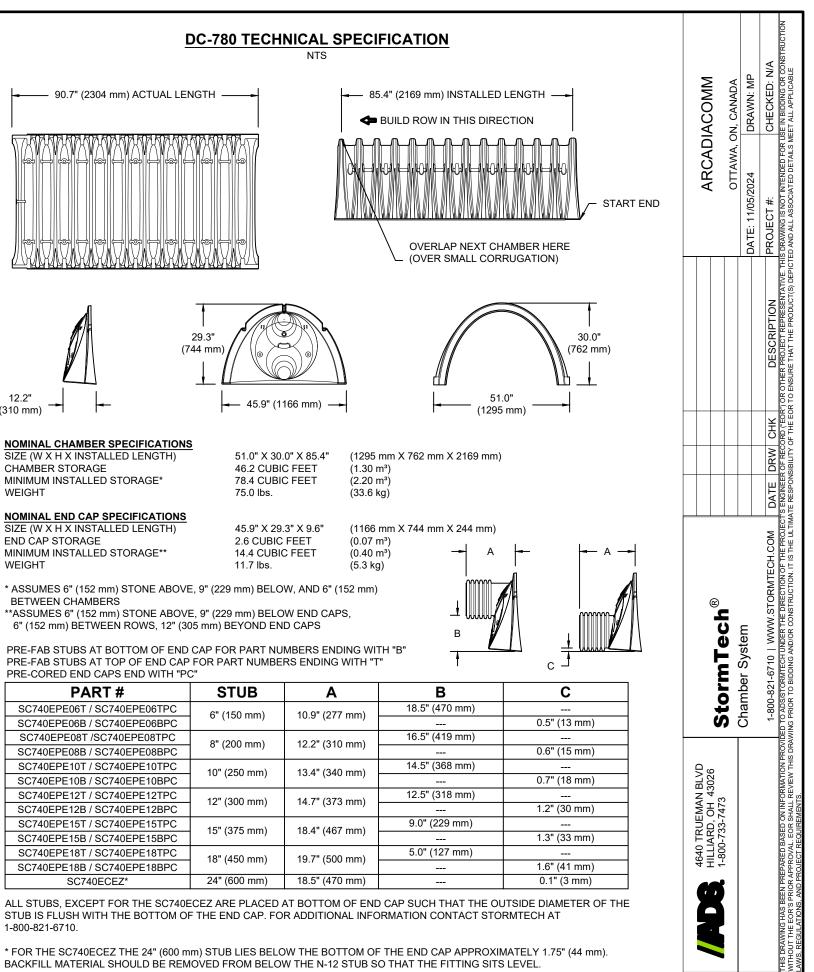
- A. INSPECTION PORTS (IF PRESENT)
 - A.1. REMOVE/OPEN LID ON NYLOPLAST INLINE DRAIN
 - REMOVE AND CLEAN FLEXSTORM FILTER IF INSTALLED A.2.
 - USING A FLASHLIGHT AND STADIA ROD, MEASURE DEPTH OF SEDIMENT AND RECORD ON MAINTENANCE LOG LOWER A CAMERA INTO ISOLATOR ROW PLUS FOR VISUAL INSPECTION OF SEDIMENT LEVELS (OPTIONAL) A.3.
 - A.4.
 - A.5. IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2, IF NOT, PROCEED TO STEP 3.
- B. ALL ISOLATOR PLUS ROWS
- B.1. REMOVE COVER FROM STRUCTURE AT UPSTREAM END OF ISOLATOR ROW PLUS
- USING A FLASHLIGHT, INSPECT DOWN THE ISOLATOR ROW PLUS THROUGH OUTLET PIPE B.2.
 - i) MIRRORS ON POLES OR CAMERAS MAY BE USED TO AVOID A CONFINED SPACE ENTRY ii) FOLLOW OSHA REGULATIONS FOR CONFINED SPACE ENTRY IF ENTERING MANHOLE
- B.3. IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3.
- STEP 2) CLEAN OUT ISOLATOR ROW PLUS USING THE JETVAC PROCESS
 - A. A FIXED CULVERT CLEANING NOZZLE WITH REAR FACING SPREAD OF 45" (1.1 m) OR MORE IS PREFERRED
 - APPLY MULTIPLE PASSES OF JETVAC UNTIL BACKFLUSH WATER IS CLEAN Β.
 - C. VACUUM STRUCTURE SUMP AS REQUIRED
- STEP 3) REPLACE ALL COVERS, GRATES, FILTERS, AND LIDS; RECORD OBSERVATIONS AND ACTIONS.
- STEP 4) INSPECT AND CLEAN BASINS AND MANHOLES UPSTREAM OF THE STORMTECH SYSTEM.

NOTES

- INSPECT EVERY 6 MONTHS DURING THE FIRST YEAR OF OPERATION. ADJUST THE INSPECTION INTERVAL BASED ON PREVIOUS 1. OBSERVATIONS OF SEDIMENT ACCUMULATION AND HIGH WATER ELEVATIONS.
- 2. CONDUCT JETTING AND VACTORING ANNUALLY OR WHEN INSPECTION SHOWS THAT MAINTENANCE IS NECESSARY.

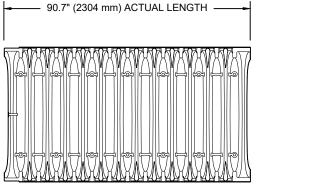
		S BRIC WITHOUT SEAMS	GEOTEXTILE BETWEEN	DC-780/SC-740 END CAP
4640 TRUEMAN BLVD HILLIARD, OH 43026 1-800-733-7473 1-800-733-7473 1-800-733-7473 1-800-733-7473	StormTech® Chamber System 1-800-821-6710 www.STORMTECH.COM 1-800-821-6710 www.STORMTECH.COM	DATE DRW CHK	DESCRIPTION DESCRIPTION	Attal Trueman BLVD Attal Attal Attal Attal HILLIARD, OH 43026 HILLIARD, OH 43026 Attal Attal Attal 1-800-733-7473 1-800-733-7473 Attal Attal Attal Attal 1-800-733-7473 Attal Attal Attal Attal Attal 1-800-733-7473 Attal Attal

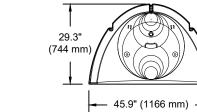




SHEET

5 OF 6





NOMINAL CHAMBER SPECIFICATIONS

12.2"

(310 mm)

SIZE (W X H X INSTALLED LENGTH) CHAMBER STORAGE MINIMUM INSTALLED STORAGE* WEIGHT	51.0" X 30.0" X 85.4" 46.2 CUBIC FEET 78.4 CUBIC FEET 75.0 lbs.	(1295 mr (1.30 m ³) (2.20 m ³) (33.6 kg)
NOMINAL END CAP SPECIFICATIONS		
SIZE (W X H X INSTALLED LENGTH)	45.9" X 29.3" X 9.6"	(1166 mr
END CAP STORAGE	2.6 CUBIC FEET	(0.07 m ³)
MINIMUM INSTALLED STORAGE**	14.4 CUBIC FEET	(0.40 m ³)
WEIGHT	11.7 lbs.	(5.3 kg)

* ASSUMES 6" (152 mm) STONE ABOVE, 9" (229 mm) BELOW, AND 6" (152 mm) BETWEEN CHAMBERS

**ASSUMES 6" (152 mm) STONE ABOVE, 9" (229 mm) BELOW END CAPS,

6" (152 mm) BETWEEN ROWS, 12" (305 mm) BEYOND END CAPS

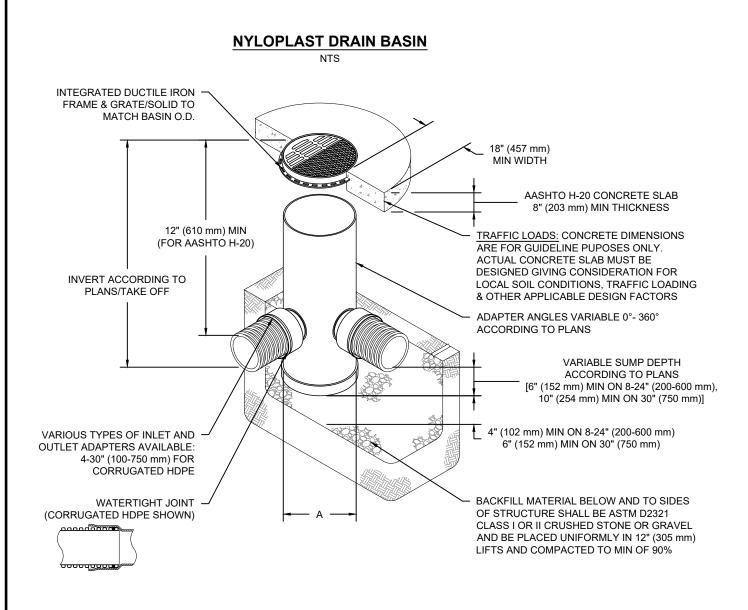
PRE-FAB STUBS AT BOTTOM OF END CAP FOR PART NUMBERS ENDING WITH "B" PRE-FAB STUBS AT TOP OF END CAP FOR PART NUMBERS ENDING WITH "T" PRE-CORED END CAPS END WITH "PC"

STUB	Α	
6" (150 mm)	10.0" (277 mm)	
0 (130 mm)	10.9 (277 1111)	
8" (200 mm)	12.2" (210 mm)	
8 (200 mm)	12.2 (310 1111)	
10" (250 mm)	13 /" (3/0 mm)	
	13.4 (340 1111)	
12" (200 mm)	14.7" (272 mm)	
	14.7 (373 1111)	
15" (275 mm)	19 /" (/67 mm)	
15 (375 mm)	10.4 (407 11111)	
18" (450 mm)	10.7" (500 mm)	
	13.7 (300 11111)	
24" (600 mm)	18.5" (470 mm)	
	6" (150 mm) 8" (200 mm) 10" (250 mm) 12" (300 mm) 15" (375 mm) 18" (450 mm)	6" (150 mm) 10.9" (277 mm) 8" (200 mm) 12.2" (310 mm) 10" (250 mm) 13.4" (340 mm) 12" (300 mm) 14.7" (373 mm) 15" (375 mm) 18.4" (467 mm) 18" (450 mm) 19.7" (500 mm)

1-800-821-6710.

BACKFILL MATERIAL SHOULD BE REMOVED FROM BELOW THE N-12 STUB SO THAT THE FITTING SITS LEVEL.

NOTE: ALL DIMENSIONS ARE NOMINAL

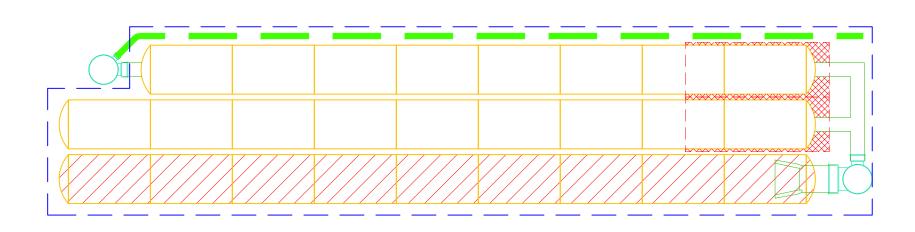


NOTES

- 1. 8-30" (200-750 mm) GRATES/SOLID COVERS SHALL BE DUCTILE IRON PER ASTM A536 GRADE 70-50-05
- 12-30" (300-750 mm) FRAMES SHALL BE DUCTILE IRON PER ASTM A536 GRADE 70-50-05
 DRAIN BASIN TO BE CUSTOM MANUFACTURED ACCORDING TO PLAN DETAILS
- DRAINAGE CONNECTION STUB JOINT TIGHTNESS SHALL CONFORM TO ASTM D3212 4.
- FOR CORRUGATED HDPE (ADS & HANCOR DUAL WALL) & SDR 35 PVC 5. FOR COMPLETE DESIGN AND PRODUCT INFORMATION: WWW.NYLOPLAST-US.COM
- 6. TO ORDER CALL: 800-821-6710

Α	PART #	GRATE/S	GRATE/SOLID COVER OPTIONS					
8" (200 mm)	2808AG	PEDESTRIAN LIGHT DUTY	STANDARD LIGHT DUTY	SOLID LIGHT DUTY				
10" (250 mm)	2810AG	PEDESTRIAN LIGHT DUTY	STANDARD LIGHT DUTY	SOLID LIGHT DUTY				
12"	2812AG	PEDESTRIAN	STANDARD AASHTO	SOLID				
(300 mm)		AASHTO H-10	H-20	AASHTO H-20				
15"	2815AG	PEDESTRIAN	STANDARD AASHTO	SOLID				
(375 mm)		AASHTO H-10	H-20	AASHTO H-20				
18"	2818AG	PEDESTRIAN	STANDARD AASHTO	SOLID				
(450 mm)		AASHTO H-10	H-20	AASHTO H-20				
24"	2824AG	PEDESTRIAN	STANDARD AASHTO	SOLID				
(600 mm)		AASHTO H-10	H-20	AASHTO H-20				
30"	2830AG	PEDESTRIAN	STANDARD AASHTO	SOLID				
(750 mm)		AASHTO H-20	H-20	AASHTO H-20				

ARCADIACOMM		OTTAWA, ON, CANADA	/2024 DRAWN: MP	CHECKED: N/A	" INTENDED FOR USE IN BIDDING OR CONSTRUCTION :IATED DETAILS MEET ALL APPLICABLE
			DATE: 11/05/2024	PROJECT #:	THIS DRAWING IS NOT CTED AND ALL ASSOC
				DESCRIPTION	DR OTHER PROJECT REPRESENTATIVE. ¹ TO ENSURE THAT THE PRODUCT(S) DEPI
				W CHK	RECORD ("EOK") (ITY OF THE EOR 1
				DATE DR	"S ENGINEER OF F ATE RESPONSIBILI
	Nvioniaet [®]			770-932-2443 WWW.NYLOPLAST-US.COM DATE DRW CHK	HIS DRAWING HAS BEEN PREPARED BASED ON INFORMATION PROVIDED TO ADS/STORMTECH UNDER THE DIRECTION OF THE PROJECT" SENGINEER OF RECORD ("EOR") OR OTHER PROJECT REPRESENTATIVE. THIS DRAWING IS NOT INTENDED FOR USE IN BIDDING OR CONSTRUCTION WITHOUT THE EOR'S PRIOR APPROVAL. EOR SHALL REVIEW THIS DRAWING PRIOR TO BIDDING AND/OR CONSTRUCTION. IT IS THE ULTIMATE RESPONSIBILITY OF THE EOR TO ENSURE THAT THE PRODUCT(S) DEPICTED AND ALL ASSOCIATED DETAILS MEET ALL APPLICABLE AWS. REGULATIONS, AND PROJECT REQUIREMENTS.
4640 TRUEMAN BLVD					THIS DRAWING HAS BEEN PREPARED BASED ON INFORMATION PROV WITHOLT THE EOR'S PRIOR APPROVAL. EOR SHALL REVIEW THIS DR. LAWS, REGULATIONS, AND PROJECT REQUIREMENTS.
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WATTS	Adjustable Accutrol Weir Tag:	Adjustable Flow Control for Roof Drains
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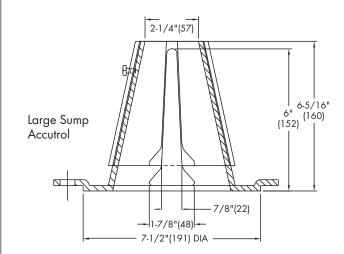
ADJUSTABLE ACCUTROL (for Large Sump Roof Drains only)

For more flexibility in controlling flow with heads deeper than 2", Watts Drainage offers the Adjustable Accutrol. The Adjustable Accutrol Weir is designed with a single parabolic opening that can be covered to restrict flow above 2" of head to less than 5 gpm per inch, up to 6" of head. To adjust the flow rate for depths over 2" of head, set the slot in the adjustable upper cone according to the flow rate required. Refer to Table 1 below. Note: Flow rates are directly proportional to the amount of weir opening that is exposed.

EXAMPLE:

For example, if the adjustable upper cone is set to cover 1/2 of the weir opening, flow rates above 2"of head will be restricted to 2-1/2 gpm per inch of head.

Therefore, at 3" of head, the flow rate through the Accutrol Weir that has 1/2 the slot exposed will be: [5 gpm (per inch of head) x 2 inches of head] + 2-1/2 gpm (for the third inch of head) = 12-1/2 gpm.



Wain Opening	1"	2"	3"	4"	5"	6"	
Weir Opening Exposed	Flow Rate (gallons per minute)						
Fully Exposed	5	10	15	20	25	30	
3/4	5	10	13.75	17.5	21.25	25	
1/2	5	10	12.5	15	17.5	20	
1/4	5	10	11.25	12.5	13.75	15	
Closed	5	5	5	5	5	5	

Job Name

Job Location

Engineer

Contractor's P.O. No.

Representative ____

Contractor _

Watts product specifications in U.S. customary units and metric are approximate and are provided for reference only. For precise measurements, please contact Watts Technical Service. Watts reserves the right to change or modify product design, construction, specifications, or materials without prior notice and without incurring any obligation to make such changes and modifications on Watts products previously or subsequently sold.

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A Watts Water Technologies Company



Ottawa, Ontario

K1S 5N4

	1101.4		-					WER DATA		114									ATIONAL DES	К							REA (Ha)					LOCATION
FF**		ed upstre				VELOCITY	SLOPE		PE SIZE (mm)				DESIGN	ICD FIXED	100yr PEAK	10yr PEAK	5yr PEAK	i (100)	1 (10)	I (5)	TOTAL	TIME	INLET	CUM	IND	C=	= C=	C= (то	FROM	
m	rt m	obve	pipe	(%)	(L/s)	{m/s}	(%)	н		DIA	(m)	(L/s)	FLOW (L/s)	FLOW (L/s)	FLOW (L/s)	FLOW (L/s)	FLOW (L/s)	(mm/hr)	(mm/hr)	(mm/hr)	(min)	IN PIPE	(min)	2.78AC	2.78AC	0.90	70 0.75	0.20 0		мн	мн	AREA ID
98.30	96.79			74.79%	46.40	1.224	1.00			250	5.00	62.04	15.64				15.64	178.56	122.14	104.19	10.07	0.07	10.00		0.15	0.00			-			
																	20101	210120		104.15		0.07	10.00	0.10	0.15	0.00	_			WAIN	BLK800	BLK800
				64.34%	28.23	0.866	0.50			250	5.97	43.87	15.64				15.64	178.56	122.14	104.19	10.11	0.11	10.00	0.15	0.15	0.06				-MAIN	CICB123	123
	9 96.79	96.7	no	47.76%	28.51	0.818	0.35			300	26.56	59,68	31.18				31.18	177.94	121.72	103.83	10.65	0.54	10.07	0.70	- A HA			_		MH122	the first of the	
																				105.05	10.01	0.34			17/012					MH122	MH123	
				64.34%	28.23	0.866	0.50			250	23.63	43.87	15.64				15.64	178.56	122.14	104.19	10:45	0.45	10.00	0.15	0.15	0.06		<u> </u>	N I	MAIN	CB122	122
	7 96.67	96.6	no	23.72%	14.16	0.818	0.35			300	12.08	59.68	45.52				45.52	173.18	118.48	101.08	10.85	0.25	10.51	0.45	0.00	-		_		MH121	MH122	
																						0120		0.40			_			INITIAGA	(MILLING)	•
98.45	96.63			49.78%	25.84	1.024	0.70			250	5.00	51.91	26.07				26.07	178.56	122.14	104.19	10.08	0.08	10.00	0.25	0.25	0.10			V	MAIN	BLK700	BLK700
	3 96.63	96.6	no	23.49%	21.48	0.802	0.25			375	58.21	91.46	69.97				69.97	171.10	117.06	99.88	12.06	1.21	10.86	0.70	0.00	-			0	MH120	MH121	
				F2 70%	22.26	1.004	4.00																		- Cristo					WHILED	WITHEA	
				53.78%	33.36	1.224	1.00			250	23.24	62.04	28.68				28.68	178.56	122.14	104.19	10.32	0.32	10.00	0.28	0.28	0.11			20	MH120	CB120	120
98.70	96.45			74.79%	46.40	1.224	1.00			250	5.00	62.04	15.64				15.64	178.56	122.14	104.19	10.07	0.07	10.00	0.15	0.15	0.06			N	MAIN	BLK600	BLK600
	5 96,45	96.4	no	28.52%	42,41	0,906	0.25			450	51.96	148.72	106.31				106.31	161.66	110.52													
	00110	••••				0.000	0.00			430	31.50	140.72	100.51				100.31	101.00	110.63	94.42	13.02	0.96	12.05	1.13	0.00				0	MH100	MH120	*
				70.76%	50.48	0.978	0.50			300	29.02	71.33	20.86				20.86	178.56	122.14	104.19	10.49	0.49	10.00	0.20	0.20	0.08			10A	CBMH110	CB110A	110
				85.38%	60.91	0.978	0.50			300	20.00	71.33	10.43				10.43	178.56	122.14	104.19	10.34	0.34	10.00	0.10	0.10	0.04			10A	CBMH110	CB110B	
				89.35%	255.95	0.982	0.20			600	15.38	286.47	30.52				30.52	174.16	119,15	101.65	10.76	0.26	10.49	0.30	0.00		_		10	MH110	CBMH110A	
	4 96.54	96.5	no	52.77%	33.67	0.874	0.40			300	53.50	63.80	30.13				30.13	171.93	117.63	100.36	11.78	1.02	10.75	0.30	0.00		_		10	MH100	MH110	
99.15	96.32			62.18%	38.58	1.224	1.00			250	16.50	62.04	02.46																			
33.13	50.32	_		02,10%	30.30	1.224	1.00	_		250	16.50	62.04	23.46				23.46	178.56	122.14	104.19	10.22	0.22	10.00	0.23	0.23	0.09	-	_	N	MAIN	BLK500	BLK500
				87.39%	54.22	1.224	1.00			250	8.00	62.04	7.82				7.82	178.56	122.14	104.19	10.11	0.11	10.00	0.08	0.08	0.03	_		ов	CICB100E	CICB100A	100A
				74.93%	46.48	1.224	1.00			250	0.74	62.04	15.56				15.56	177.57	121.47	103.62	10.12	0.01	10.11	0.15	0.08	0.03			N	MAIN	CICB100B	1008
	2 96.32	96.3	no	34,25%	84.97	0.850	0.15			600	32.73	248.09	163.12				163.12	154.97	106.08	90.55	13.66	0.64	13.02	1.80	0.00	-	_	_	08	MH1008	MH100	
			no	36.00%	89.30	0.850	0.15			600	16.00	248.09	158.78				158.78	150.81	103.25	88.14	13.98	0.31	11-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	1.80	0.00	-				100000000000000000000000000000000000000	MH100B	EXISTING
	5 96.052	96.2	по																		1000	0.51	15.00			0.72	00 0.00	0.00		EAIVITISUS	IVIT1008	EXISTING

STORM SEWER DESIGN SHEET

PROJECT: Arcadia Commercial

LOCATION: CITY OF OTTAWA

CLIENT: Minto Development Group

*HGL at obvert of pipe if plpe is not surcharged
** Finished floor for slab on grade commercial building
***Freeboard is from upstream MH HGL to FF



Ottawa, Ontario

K1S 5N4

	LOCATION	1		-	-	A (Ha)					1	1	-	RATIONAL D			1	1				1			SEWER DATA	-								
ET	AREA ID	FROM	то	C=		C=				INLET	TIME		1 (5)	i (10)			10yr PEAK							PIPE SIZE (mm	1)	•	VELOCITY	AVAIL	CAP (5yr)	surcharged	d upstream	HGL*	FF**	Free
		мн	мн	0.20	0.70	0.75	0.90	2.78AC	2.78AC	(min)	IN PIPE	(mín)	(mm/hr)	(mm/hr)	(mm/hr)	FLOW (L/s)	(L/s)	(m)	DIA	W	H	(%)	{m/s}	(L/s)	(%)	pipe	obvert	m	m					
	1114	C0040122224	CD14112222				0.00	0.33	0.22	10.00	0.21	10.21	104.10	122.14	170 50	22.40				12.40		48.48											÷	
	233A 233B	CBMH233A CBMH233	CBMH233 CBMH232	-						10.00			104.19									15.60				0.15	0.850		90.54%	4			4	
	2330	CDIVINZ33	CDIVINZ52				0.15	0.56	0.00	10.31	0.07	10:20	102.00	120.27	1/5.01	01.01				61.61	248.09	34.20	600			0.15	0.850	186.48	75.17%	4			4	
	232A	CBMH232A	CBMH232		-		0.10	0.25	0.25	10.00	0.31	10.31	104.19	122.14	178.56	26.07				26.07	248.09	15.60	600			0.15	0.850	222.02	89.49%	4				
																					210105	13100	000			0.15	0.030	444.02	03.43/0	1			(N)	
	232B	CBMH232	CBMH231				0.12	0.30	1.15	10.98	0.67	11.65	99.30	116.38	170.10	114.29				114.29	248.09	34.20	600			0.15	0.850	133.80	53.93%	1			4	
								if in																						1			4	
	231A	CBMH231A	C8MH231				0.11	0.28	0.28	10.00	0.31	10.31	104.19	122.14	178.56	28.68				28.68	248.09	15.60	600			0.15	0.850	219.41	88.44%					
		100000000000			-				100 100 4																					1				
	231B	CBMH231	MH230				0.11	0.28	1.70	11.65	0.47	12.12	96.23	112.76	164.79	163.72				163.72	248.09	24.08	600	<u> </u>		0.15	0.850	84.37	34.01%	4				
	230A	CICB230A	CICB230B	<u> </u>		-	0.05	0.15	0.15	10.00	0.11	10.11	104.19	122.14	178.56	15.64				15.64	62.04	0.04	350			1.00	4.834	15.10		4				
	230B	CICB230B	MH230							10.00			104.19		_					49.26		8.04 5.93	250			1.00	1.224		74.79%	4				
		COLUM	ALCONT OF	1	1		0.13	0.55	Sec. 1	10.11	0.00		TOULDE	1	1.1.50		-			73.69	07.74	3.33	2.0			2.00	1./21	38.48	43.80%	1				
	230C	CB230C	MAIN				0.03	0.08	0.08	10.00	0.14	10.14	104.19	122.14	178.56	7.82				7.82	62.04	10.39	250			1.00	1.224	54.22	87.39%	1				
			·																											1				
	230D	CB230D	CB230E		<u> </u>					10.00			104.19							10.43	62.04	7.95	250			1.00	1.224	51.61	83.19%	1				
	230E	CB230E	MAIN				0.09	0.23	0.33	10.11	0.05	10.16	103.62	121.47	177.58	33.70				33.70	87.74	4.91	250			2.00	1.731	54.03	61.58%	1				
	230F	CB230F	MAIN	-			0.07	0.10	0.10	10.00	0.17	10.17	104.10	122.14	178.56	18.25				10.05	62.04	40.50								1				
	230F	CB2SUF	ORALO	-			0.07	0.18	0.19	10.00	0.17	49.47	104.19	122.14	1/8.30	18.25				18.25	62.04	12.50	250			1.00	1.224	43.79	70.59%	1			1	
	230G	CB230G	CB230H		-		0.10	0.25	0.25	10.00	0.11	10.11	104.19	122.14	178.56	26.07				26.07	62.04	8.00	250			1.00	1.224	35.97	57.98%	1			1	
	230H	CB230H	MAIN							10.11			103.62	-						44.07		4.78				2.00	1.731	43.66		1			1	
																														1			1	
	2301	CB2301	MAIN				0.03	0.08	0.08	10.00	0.12	10.12	104.19	122.14	178.56	7.82				7.82	62.04	8.57	250			1.00	1.224	54.22	87.39%	1			1	
		_							-	18.18		All Property lies						·												1			1	
		MH230	MH210					0.00		12.12	1.62	13.76	94.19	110.36	161.26	306.36				306.36	449.81	95.70	750			0.15	0.986	143.45	31.89%	no	95.70	95.70	1	
	221A	CB221A	CBMH221				0.16	0.40	0.40	10.00	0.11	10.11	104 19	122.14	178 56	41.71	-			41.71	420.62	17.05	450			1.00	2.562	270.02	00.000/	1			1	
		COLLIA					0.10	0.40		10.00	0.11	407.44	104.15	122.14	170.30	41.71				41.71	420.05	17.05	430			2.00	2.302	378.92	90.08%	1			1	
	221B	CB221B	CB221C				0.03	0.08	0.08	10.00	0.16	10.16	104.19	122.14	178.56	7.82				7.82	297.43	17.05	450			1.00	1.812	289.61	97.37%	1			1	
	2210	CB221C	CBMH221				0.02	0.05	0.13	10.16	0.09	10.24	103.37	121.17	177.14	12.93				12.93		15.52					2.977		97.35%	í -			1	
						-						-																		i			1	
	221D	CBMH221	MH221		-	-	0.08	0.20	0.73	10.24	0.57	10.81	102.92	120.65	176.36	74.68				74.68	286.47	33.38	600			0.20	0.982	211.79	73.93%	i			1	
	BLK400	BLK400	MAIN	-			0.15	0.20	0.24	10.00	0.07	- 10.07	104.10	133.14	170 54	39.10				20.10	(2.04	F 00	050							L			L	
	BLK400	BLK400	DISIN'	-			0.15	0.58	0.30	10.00	0.07	10.07	104.19	122.14	178.56	39.10				39.10	62.04	5.00	250			1.00	1.224	22.94	36.97%			96.03	99.50	
	BLK300	BLK300	MAIN		-		0.04	0.10	0.10	10.00	0.07	10.07	104.19	122.14	178.56	10.43		-		10.43	62.04	5.00	250			1.00	1.224	51 61	83.19%			06.02	00.50	
			III MARKAN	1	1							- Contraction		-	1.0.00					20175	VEIUT	5100	230			1.00	1.224	31.01	03.13%			96.03	99.50	
		MH500	MH221				0.00	0.00	0.00	10.00	0.20	10.20	104.19	122.14	178.56	0.00				0.00	900.87	12.00	1050			0.10	1.008	900.87	100.00%	i			ł.	
								_							1															i			1	
	3	MHZZ3	MH220					0.00	1.20	10.51	1.40	12.21	100.10	117.32	171.47	120.21				120.21	148.72	75.90	450			0.25	0.906	28.50	19.17%	no	96.03	96.03	1	
		(1993)	COMUNICA	-			0.05	0.40	0.42	10.00	0.43	40.45	104.40	122.44	470.54	10.05					107.45	44.00											1	
	222A	CB222	CBMH222		-					10.00		10.12		-						13.03		14.80					2.121			1			1	
	222B	CBMH222	MH220				0.07	0.18	0.30	10.12	0.07	10.19	103.58	121.42	177.50	31.10				31.10	151.96	12.64	250	a		6.00	2.999	120.86	79.53%	7			ŧ.	

STORM SEWER DESIGN SHEET

PROJECT: Arcadla Commercial

LOCATION: CITY OF OTTAWA

CLIENT: Minto Development Group

*HGL at obvert of pipe if pipe is not surcharged **Finished floor for slab an grade commercial building ***Freeboard is from upstream MH HGL to FF



Ottawa, Ontario

K1S 5N4

	LOCATION			1	APE	A (Ha)								RATIONAL D																***Freeboard	is from upstrea	IM MH HGL to I	F	
		FROM	то	C=		C=	C=	IND	СЛМ	INLET	TIME	TOTAL	1 (5)	(10)	1 (100)	Euro DEAK	10	100yr PEAK		DECION	CARACITY	Leveru			SEWER DATA		T			1.0				
STREET	AREA ID	MH	мн					2.78AC			IN PIPE							FLOW (L/s)				(m)	DIA	PIPE SIZE (mn	n) H	(%)	VELOCITY (m/s)		CAP (Syr)	-	upstream		FF**	Freeboa
				1		-						Print?		1	1 may my	100010404	1.1011 (1.) 0)	1000 10,07	10011 [2] 3]	10011 [0/3]	14/3/	1.07		~~		[70]	(m/s)	(L/S)	(%)	pipe	obvert	m		n
	223A	CB223	CBMH223	1	1		0.15	0.38	0.38	10.00	0.21	10.21	104.19	122.14	178.56	39.10				39.10	446.15	34.20	450			2.25	2 710	407.05	01.044					
	223B	CBMH223	MH220			<u> </u>				10.21	0.27					69.65				69.65		20.38				0.50	2.718	407.05	91.24%					
				1											1					05105	LIVISE	20.50	450			0.30	1.201	140.67	66.88%	-			1	
		MH220	MH212					0.00	22:38	12.21	0.44	11221651	93.82	109.93	160.62	204.22				204.22	248.09	22.60	600			0.15	0.850	43.86	17.68%	-	05.94	05.04		
																										0.10	0.030	43.00	17.00%	no	95.84	95.84		
	212A	CICB212A	CICB212B				0.03	0.08	0.08	10.00	0.12	10.12	104.19	122.14	178.56	7.82				7.82	62.04	8.61	250			1.00	1.224	54.22	87.39%					
	212B	CICB212B	MH212				0.03	0.08	0.15	10.12	0.06	10.18	103.58	121.42	177.49	15.55				15.55	151.96	11.24	250			6.00	2.999		89.77%	-				
															<u> </u>			· · · · · · · · · · · · · · · · · · ·						1						7				
	215	CB215	MH215				0.04	0.10	0.10	10.00	0.17	10.17	104.19	122.14	178.56	10.43				10.43	62.04	12.57	250			1.00	1.224	51.61	83.19%				1	
			1 - www.	-					100000000				-												((
	BLK100	BLK100	MAIN	-			0.06	0.15	0.15	10.00	0.07	10.07	104.19	122.14	178.56	15.64				15.64	62.04	5.50	250			1.00	1.224	46.40	74.79%			97.23	99.60	2.3
	2	ANDAR	No. of Concession, Name	-				0.00	ALC: NOT	10.12	0.40	1000	402.20	124.00	477.04																			
	·	MH215	MH214				-	0.00	0.23	10.17	0.40	10.57	103.30	121.09	177.01	25.85				25.85	82.07	38.95	250			1.75	1.620	56.22	68.51%	no	97.23	97.23		
	216A	RYCB216	CB216	0.03				0.02	0.02	10.00	0.05	10.05	104.19	122.14	178.56	1.74				1.74	124.00	7.40	350											
	216A	CB216	MH216	0.03	1	-	0.04			10.00	0.05	of the local division of the local divisiono			-	1./4				1.74	124.08	7.40	250			4.00	2.449		98.60%	-				
	LIUU	COLIO	CONTINUED.	-			0.04	0.10	U.A.S.	10.00	0.04	40104	104.15	166.14	178.30	12.17				12.17	138.72	5.90	250			5.00	2.738	126.56	91.23%					
		MH216	MH234					0.00	0.12	10.05	0.47	10.52	103.93	121.83	178.10	12.13				12.13	43.87	24.56	250			0.50	0.866	24.72	70.040/	-			1	
																				12.15	43.07	24.50	2.50			0.50	0.806	31./3	72.34%	no	97.07	97.07		
	BLK200	BLK200	MAIN				0.04	0.10	0.10	10.00	0.07	10.07	104.19	122.14	178.56	10.43				10.43	62.04	5.40	250			1.00	1.224	51.61	83.19%	-		00.55	00.55	
				-																						100	1.224	51.01	03:13/8			96.55	99.55	3.0
		MH234	MH213				_	0.00	0.47	20.57	0.40	10.97	101.27	118.69	173.49	47.30				47.30	129.34	27.00	375			0.50	1,134	82.04	63.43%	1 10	96.55	96.55		
	*	MH213	MHRIR					0.00	0.47	10.97	0.26	11.23	99.34	116.43	170.16	46.40				46.40	129.34	17.80	375			0.50	1.134		64.13%	no	96.39	96.39		
																														1	20100	00.00		
		MH212	MH210					D.DO	2/19.(08 11 33	0.86	17.09	98.12	114.98	168.05	274.12				274.12	350.85	61.94	600			0.30	1.202	76.72	21.87%	no	95.74	95.74		
		-	-	-					-			and the second sec																		1				
	210A	CB210A	MAIN				0.12	0.30	10.10	10.00	0.09	10.09	104.19	122.14	178.56	31.28				31.28	201.76	15.06	300			4.00	2.765	170.48	84.50%	1				
	BLK900	BLK900	- MAIN	-			0.45	1.15	Terren (10.00	0.71	10.21	104.10	122.14	178.56	119.92				440.00					-									
	BLK900	BLKSOU	- Burden				0.40	1.15	the state of the second second second second second second second second second second second second second se	10.00	0.21	10.61	104.19	122.14	178.56	119.92				119.92	182.91	19.94	375			1.00	1.604	62.99	34.44%			95.56	98.10	2.54
PRESSED LOADING	2108	CB210B	MANN	-			0.02	0.05	0.05	10.00	0.29	10.29	104.19	122.14	178.56	5.21				5.21	43.87	14.90	250		_	0.50								
							- OIOL	0.05		10100	ULLS	Course of the Area	104.15	112.14	170.50	5.21				5.21	43.07	14.90	250			0.50	0.866	38.65	88.11%	{				
		MH210	MH205B					0.00	7.55	33.24	0.41	14.15	87.88	102.93	150.35	663.26				663.26	905.48	28.86	975			0.15	1.175	242.22	36 759/					
										and and a second second second second second second second second second second second second second second se										200140	505145	20.00	575	· · · · · · · · · · · · · · · · · · ·		0.10	1.175	242.23	20./3%	no	92.26	95.56		
	206E	CICB206D	MAIN			0.09		0.19	0.19	10.00	0.02	10.02	104.19	122.14	178.56	19.55				19.55	87.74	2.57	250			2.00	1.731	68.18	77.72%					
																												oprac	13012/0					
	•	MH205B	MH205					0.00	7.74 -	- 14.15	0.20	14.8	86.42	101.22	147.84	668.51				668.51	905.48	13,88	975			0.15	1.175	236.97	26.17%	no	95.50	95.50		
				-	-		-																									33.39		
	206A	CB206A	CBMH206	-				0.60			0.17				178.56	62.57				62.57	420.63	25.66	450			2.00	2.562	358.07	85.13%	1				
	206B	CBMH206	MH206	-			0.14	0.35	0.95	10.17	0.26	10,43	103.32	121.11	177.05	98.23				98.23	210.32	19.99	450			0.50	1.281	112.09	53.29%					
	2000	CD30CD					0.07	0.40				1000																						
	206C 206D	CB206B	MAIN					0.18			0.08	10.08	104.19	122.14	-	18.25				18.25	85.29	8.49	250			1.89	1.683	67.04						
	2060	CB206C	MAIN				0.04	0.10	0.10	10.00	0.02	10.02	104.19	122.14	178.56	10.43				10.43	87.74	2.32	250			2.00	1.731	77.31	88.11%					
		MH206	MH205	-				0.00	3.33	10.43	0.59	11.02	101.00	110 57	174.75	125.04				435.04	402.04								_					
		PHILIPPIN	(and share)	-				0.00	1.63	10,93	0.59	41.07	101.99	119.55	1/4./5	125.04				125.04	182.91	56.62	375			1.00	1.604	57.87	31.64%	no	96.05	96.05		
ernal South	EXT-2	STUB	MH205		2.82			5.49	5.49	12.00	0.17	212.12	94.70	110.96	167.12	519.66				E10.66	096.95	11.55	1050			0.42								
	Act 1 1 2	51.00			2.02	-		3.73	and a state of the	12.00	0.17	Contraction of the	34.10	110.30	102.13	313.00				519.66	986.85	11.55	1050			0.12	1.104	467.19	47.34%	по	95.50	95.50		

STORM SEWER DESIGN SHEET

PROJECT: Arcadia Commercial

LOCATION: CITY OF OTTAWA

CLIENT: Minto Development Group

*HGL at obvert of pipe if pipe is not surcharged ** Finished floor for slab on grade commercial building ***Freeboard is from upstream MH HGL to FF



Ottawa, Ontario

K1S 5N4

	LOCATION				ARE	EA (Ha)							W	RATIONAL D	ESIGN FLOW										SEWER DAT	A				1			
CTREET		FROM	то	C=	C=	C=	C=	IND	CUM	INLET	TIME	TOTAL	1 (5)	i (10)	i (100)	5yr PEAK	10yr PEAK	100yr PEAI	ICD FIXED	DESIGN	CAPACITY	LENGTH		PIPE SIZE (m	ากา)	SLOPE	VELOCITY	AVAIL	CAP (5yr)	surcharged	upstream	HGL*	FF** Freeboar
STREET	AREA ID	мн	мн		0.70		0.90	2.78AC	2.78AC	(min)	IN PIPE	(min)	(mm/hr)	(mm/hr)	(mm/hr)	FLOW (L/s)	FLOW (L/s)) FLOW (L/s	FLOW (L/s	FLOW (L/s	(L/s)	(m)	DIA	W	Н	(%)	(m/s)	(L/s)	(%)	pipe	obvert	m	m m
	205A	CICB205A	CICB205B		1	0.10		0.21	0.21	10.00	0.16	10.16	104.19	122.14	178.56	21.72				21.72	62.04	11.97	250			1.00	1.224	40.31	64.98%				
	205B	CICB205B	MAIN			0.06		0.13	0.38	10.00	0.01	10.01	104.19	122.14	178.56	34.76				34.76	87.74	0.64	250			2.00	1.731	52.98	60.38%	1			(
													V	1																1			1
treet 1	22	MIR205	MH204					0.00	14.78	14:34	0.39	14.73	85,74	100.42	146.67	1,267.51				1,267.51	1,928.87	30.36	1350			0.12	1.305	661.36	34.29%	no	95.48	95.48	1
					1	i T										1								1						1			1
treet 1	204B	CICB204B	CICB204A			0.06		0.13	0.13	10.00	0.12	10.12	104.19	122.14	178.56	13.03			0	13.03	62.04	9.00	250			1.00	1.224	49.00	78.99%	1			1
treet 1	204A	CICB204A	MAIN	1		0.07		0.15	0.27	10.12	0.02	10.14	103.55	121.38	177.45	28.07			C	28.07	87.74	2.34	250			2.00	1.731	59.67	68.01%	1			1
															_											1]			1
	(a)	MH204	MH203					0.00	15.05	14.73	1.01	35.74	84.44	98.89	144.42	1,271.12				1,271.12	1,928.87	79.00	1350			0.12	1.305	657.75	34.10%	no	95.43	95.43	1
																														1			1
	240A	CICB240A	CICB240B	-	_				0.00		0.14			122.14		0.00				0.00	62.04	10.23	250			1.00	1.224	62.04	100.00%	1			1
	2407	CICB240B	MHZ40	2			0.05	0.13	0.13	10.14	0.16	10.30	103.46	121.28	177.30	12.94	1	_		12.94	87.74	16.81	250			2.00	1.731	74.79	85.25%	1			1
				_	_	_						-			_															1			1
EPRESSED LOADING	240B	CB240C	MH240	1	_	_	0.02	0.05	0.05	10.00	0.68	10.68	104.19	122.14	178.56	5.21				5.21	43.87	35.30	250			0.50	0.866	38.65	88.11%	1			1
					_	-						-							-						· · · · · · · · · · · · · · · · · · ·				· · · · · · · · · · · · · · · · · · ·				1
	240C	CB240D	MHZ40		_		0.05	0.13	0.13	10.00	0.44	10.44	104.19	122.14	178.56	13.03				13.03	62.04	32,56	250		-	1.00	1.224	49.00	78.99%				
					-	-	-	-	-					440.07	170.70										-			-					0
	25	MH240	MH203		-	-	-	0.00	0,30	10.68	0.37	11.05	100.74	118.07	172.58	30.24		-		30.24	63.80	19.34	300		_	0.40	0.874	33.56	52.60%	no	95.39	95.39	1
				1		_			10.00			46.00	01.04	05.42	120.00	4 747 47				1 347 43	1 030 07	45.86	1250		-	0.13	4.005	004.14	-	1			1
reet 1	100	MH203	MH202	-					15.35		0.59					1,247.42				1,247.42	1,928.87	45.86	1350			0.12	1.305		35.33%	no	95.31	95.31	1
treet 1		MH202	MH201		_			0.00	15.35	16.32	0.20	16,53	79.51	93.09	135,91	1,220.78				1,220.78	1,928.87	15.91	1350	-	-	0.12	1.305	708.09	36.71%	по	95.23	95.23	1
								0.00	0.00	12.00	0.20	12.20	94.70	110.96	162.13	36.59		_		36.59	62.04	14.74	250			1.00	1.224	25.45	41.02%				
treet 1	201A	DCICB201A		0.02		0.18			0.39	12.00	0.20	12.20				83.98				83.98	87.74	3.43	250		-	2.00	1.731	25.45	41.02%				
treet 1	201B, 202	DCICB201B	MAIN	-		0.24		0.50	0.89	12.00	0.03	12.05	94.70	110.96	102.15	85.98		-		03.90	67.74	5.45	230			2.00	1./31	3.70	4.28%				1
xternal East	EXT-1	CAP	MH201		0.73		-	1.42	1.42	10.00	0.29	10.29	104.19	122.14	178.56	148.01	-			148.01	248.09	14.54	600			0.15	0.850	100.07	40,34%	no	95.23	95.23	
xternal East	EXI-1	CAP	INIMEOT	-	0.75	-		1.42	774%	10.00	0.25	1042	104.10	122.14	170.30	140.01				140.01	240.05	14.54	000			0.15	0.030	100.07	40.3470	1 110	53.23	95.25	/
treet 1	i i i i i i i i i i i i i i i i i i i	MH201	CAP	-	-		-	0.00	17.66	16.53	0.82	17.34	78.93	92.41	134.90	1,393.95				1.393.95	2,332.02	62.55	1500			0.10	1.278	938.07	40.23%	no	95.21	95.21	1
treet 1	existing	Ex CAP	EXMH303							17.34		17.66			131.03	1.354.27	·			1.354.27	2.332.02		1500			0.10	1.278	977.75	41.93%	no	55.21	55.21	
treet 1	existing	EXILAT	EXIVITISUS	0.05	2.55	0.00	3.62			11.54	0.52	47.00	70100			1,55 1127				1 400 1121	ajoo Lio L	21130	1000			0120	1.270	577.75	41.5576	по	95.17	95.088	
				0.05	3,33	0.80	5.02	17.00	TROL						+					· · · · · ·									-	110	55.17	33.088	
		-		-	APEA	A CHECK	-								+			_					1					1					
				-		and the second second	A 8.02	-							+															1			
				-			A 3.55	-	-				1																	1			
				-	LATER	T	4.47		-																					1			
					-	-		-		-			-				1													1			
efinitions:		1.	J	Notes:		-	_			Designed:		RM			No.		1.1.1.1.1	- 19 A	A States	Revision	13 10 10 10 10	17 - 18 M	100 1000	11-12-12-12	1.	1.200	Date	1.8121.00.00	100				
= 2.78CiA, where:					nnings co	pefficient	t (n) =								1.					ssued for SPA							11/15/201	3					
= Peak Flow in Litres per	Second (L/s)				Ba co										2				Revised	per City Com	ments				la		6/27/2014						
= Area in Hectares (Ha)										Checked:		DY			3				Revised	per City Com	ments						8/22/2014						
= Rainfall intensity in mil		/hr)																		per City Com							10/2/2014			1			
[i = 998.071 / (TC+6.053		5 YEAR																		<u> </u>													
[i = 1174.184 / (TC+6.01		10 YEAR								Dwg. Refer	ence:	31855-500			1																		
[i = 1735.688 / (TC+6.01		100 YEAR										100			Newson	File Reference	e:	States and the	1000	1123	Date:	CA TABLE P	7.14.00.00	Contraction of the	Statements of	0.000	Sheet No:	1	College March				
[1 = 1/00.000 / (10+0.01		100 ILMN													1.	31855.5.7.1		10121			11/15/2013				10000		3 of 3						

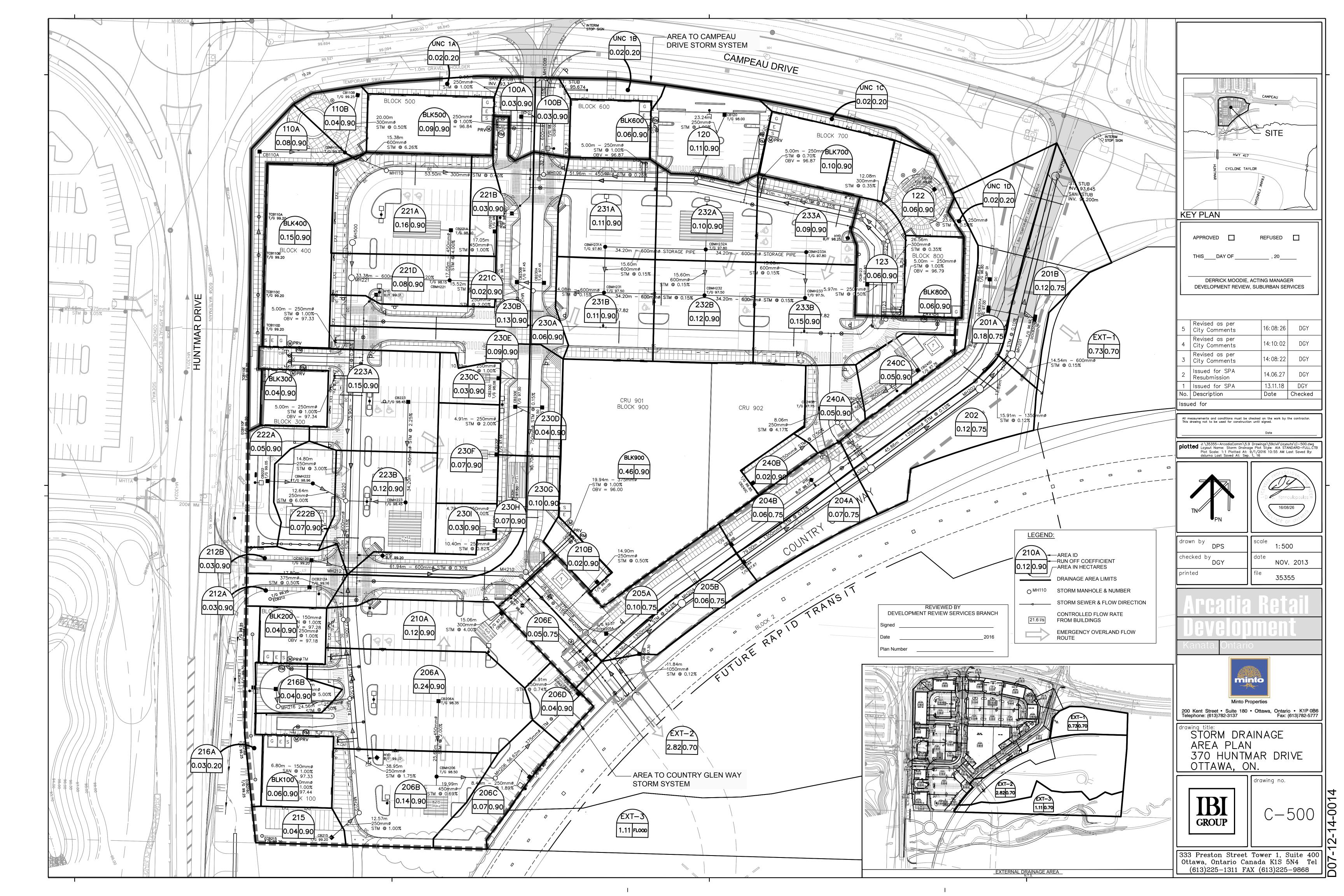
STORM SEWER DESIGN SHEET

PROJECT: Arcadia Commercial

LOCATION: CITY OF OTTAWA

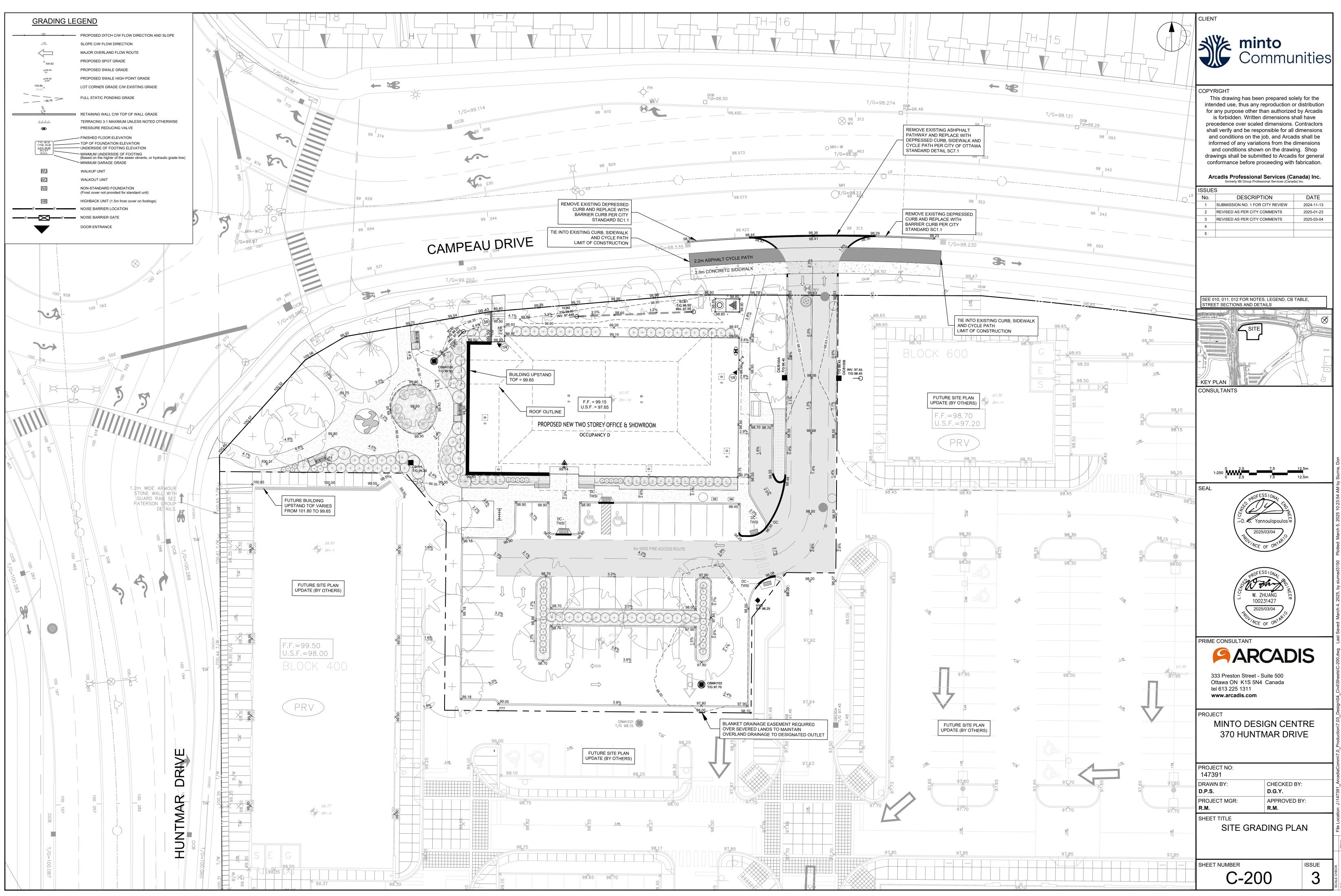
CLIENT: Minto Development Group

*HGL at obvert of pipe if pipe is not surcharged ** Finished floor for slab on grade commercial building ***Freeboard is from upstream MH HGL to FF

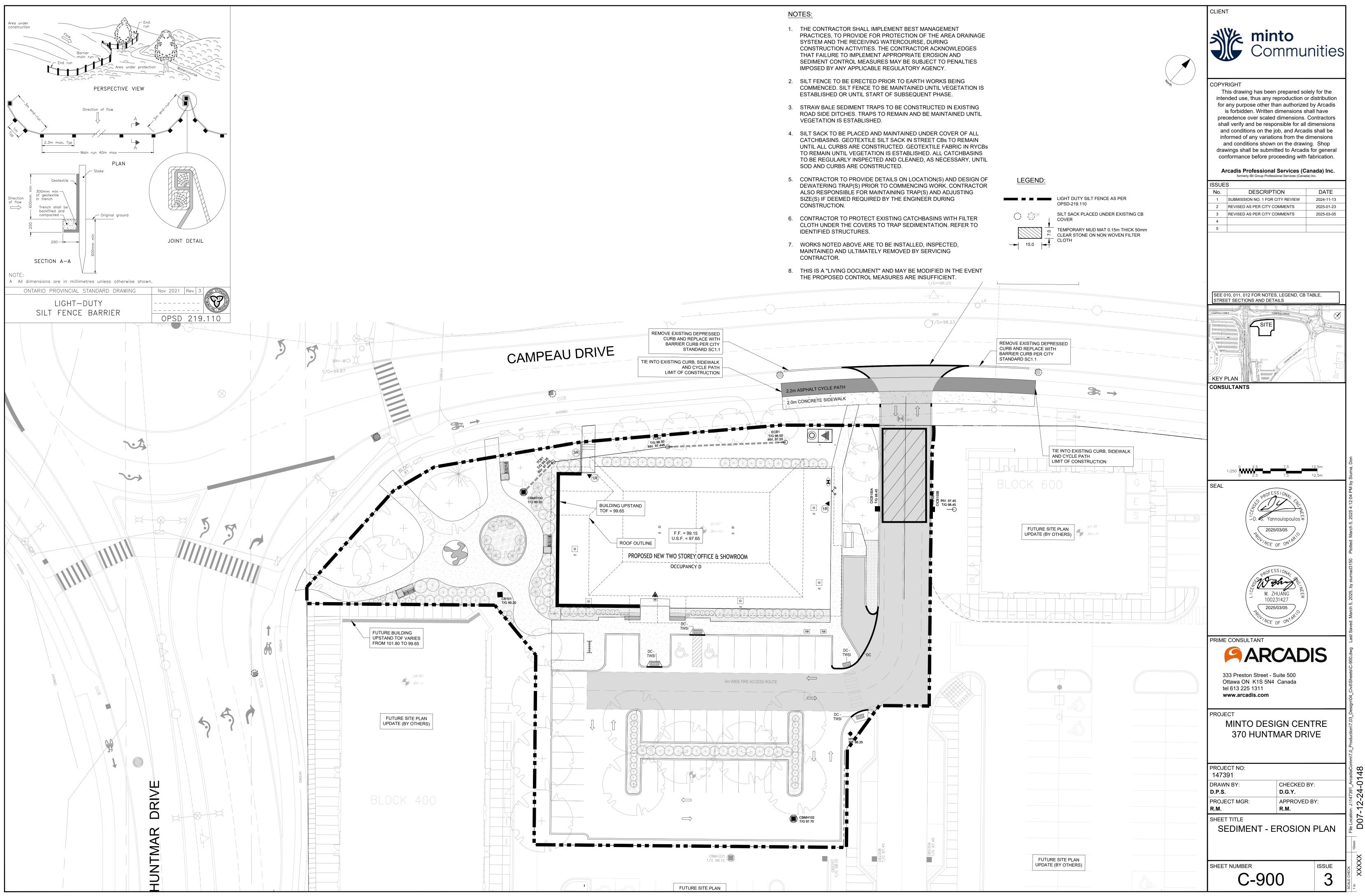


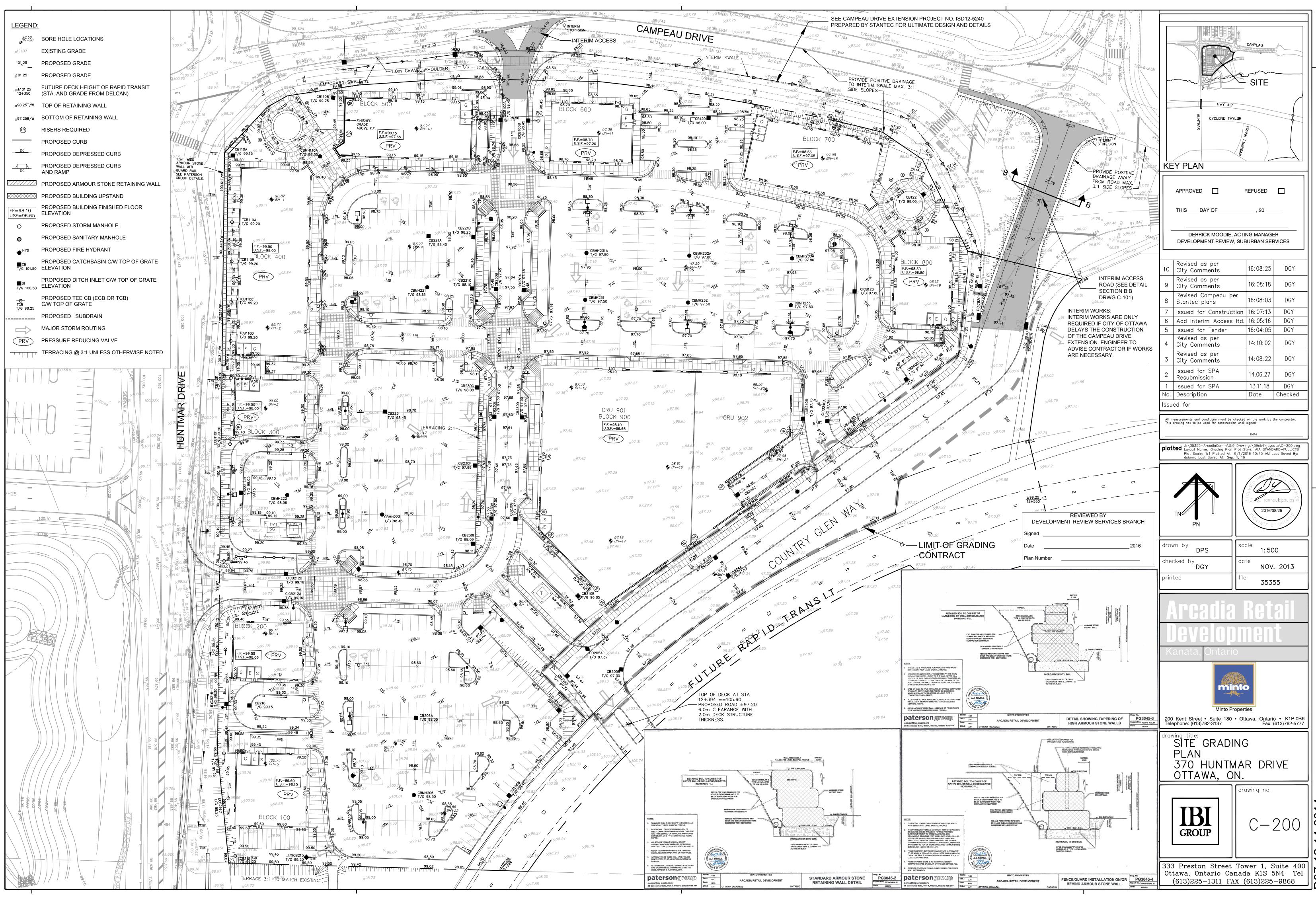


Grading Plan 147391-C-200 Erosion and Sediment Control Plan 147391-C-900 Grading Plan 35355-C-200



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007-12-14-0014

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