

Minto Communities

Arcadia Commercial Site

Design Brief

April 30, 2025

Arcadia Commercial Site - Design Brief November 13, 2024 Revised April 30, 2025

Arcadia Commercial Site

Design Brief City of Ottawa

Development Application File: D07-12-24-0148

April 30, 2025

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Version Control (optional)

Issue	Revision No.	Date Issued	Page No.	Description	Reviewed By
1	-	2024-11-13		Issued for Site Plan Approval	RM/DY
2	-	2025-01-23		Revised per City Comments	RM/WZ
3	-	2025-03-07		Revised per City Comments	RM/WZ
4	-	2025-04-16		Revised per City Comments	RM/WZ
5		2025-04-30		Revised per City & MVCA Comments	RM/WZ

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1 Introduction

1.1 Scope

Arcadis Professional Services (Canada) Inc., hereinafter referred to as "Arcadis", has been retained by Minto Communities to prepare the necessary engineering plans, specifications and documents to support the proposed Site Plan Application for the subject lands, following the policies set out by the Planning and Development Branch of the City of Ottawa. This Brief will present a detailed grading and servicing scheme to support the development of the property and will include sections on water supply, wastewater management, minor and major stormwater management, site grading and erosion and sediment control. Minto Communities intends to sever a small portion of the remaining undeveloped lands of its 370 Huntmar Road site for use as its Sales and Design Centre.

This parcel of land is part of the proponent's larger "Arcadia" development lands, which are currently being developed. This subject parcel is referred to as Stage 5 in other previously approved Minto reports, including "Conceptual Site Servicing Arcadia Stages 1, 2, 5 and 8", and "Arcadia Interim SWMF", which provide details related to the construction and operation of the downstream infrastructure which will service these lands. The subject lands were previously Site Plan Approved (circa 2014), and subsequently severed for the Microtel Hotel. The public road portion of the original Site Plan Application (Country Glen Way), has been constructed and is in service.

This report was prepared in accordance with the Servicing Study Guidelines for Development Applications in the City of Ottawa. **Appendix A** contains a customized copy of the City's checklist which can be used as a quick reference for the location within this study report of each of the checklist items.

1.2 Background

In 2002, the City of Ottawa expanded its urban area to include the lands currently known as Kanata West. In March 2003, the Ottawa City Council approved the general land use and development principles of the Kanata West Concept Plan (KWCP). The plan is a mixed-use community with a population of about 17,000 persons in 6,300 households, 24,000 jobs and approximately 1 million square meters of commercial space. After approval of the KWCP, several supporting technical documents, including the Kanata West Master Servicing Study (KWSS), were prepared. The KWSS provided a master servicing plan for the entire KWCP, including major infrastructure such as water supply, wastewater disposal and stormwater management.

As mentioned, the site was previously Site Plan Approved (D07-12-14-0014). IBI Group (now Arcadis) prepared the Site Servicing Brief and Engineering Drawings to support the original SPA. The approval has since lapsed. This report aims to follow the principles established in the original site plan approval and engineering drawings, and provide adjustments to suit the new severance.

1.3 Subject Site

The Arcadia Commercial Site is located at 370 Huntmar Road, at the East intersection of Campeau Drive and Huntmar Drive in Ottawa, to the northeast of Tanger Outlets, and is part of the Kanata West Business Park

(KWBP). The KWBP is proposed to include several types of non-residential uses including Prestige Business Park, High Profile Employment and Extensive Employment.

The subject site severance is approximately 0.46 ha and consists of a two-storey Office and Showroom building as a small phase of a larger future commercial development.

Refer to **Figure 1**, below, for more information regarding the site location.



Figure 1 Subject Site Location

The site's natural topography, with the existing grade sloping from west to east, the proposed concept aims to seamlessly integrate the proposed two-storey building into the existing natural slope while taking the future design of the more significant commercial site into consideration to ensure there are no potential conflicts with future work. The building's facades will be maintained at an accessible grade to permit entry into the main levels of the building.

The primary vehicular and pedestrian access to the site is located off Campeau Drive and provides unimpeded access to the site office through a parking area to the South of the building. Two entrances with pedestrian access will be provided to the north of the building.

This project will consist of the construction of a two-storey office and showroom building. The site will also contain vehicular access routes for future commercial area, dedicated parking spaces, Tactile Walking Surface Indicators (TWSI) and landscaping areas. A site plan of the proposed development is included in **Appendix A**.

1.4 Previous Studies

1. Kanata West Concept Plan

The Kanata West Concept Plan (KWCP) was approved by the City of Ottawa in 2003. The plan provides a framework for the current and future development of the Kanata West lands. It also provides the guidelines and requirements for concept planning, the recommended concept plan, and an implementation strategy. The plan focuses on development of the urban lands with mix uses including office, housing, retail, institutional, entertainment and leisure activities.

2. Kanata West Servicing Study

The Kanata West Servicing Study (KWSS) was completed by the City of Ottawa in 2006. That study provided detailed guidelines for provision of major municipal infrastructure in support of the Kanata West Concept Plan. Among other things it provided guidelines and criteria for water supply, wastewater collection and stormwater management.

3. Third Party Review

The Third Party Review (TPR) was completed after potential omissions in the stormwater management model for KWSS were identified. The TPR was commissioned to be an arm's length review of the model to ensure that it was property calibrated and validated.

4. Signature Ridge Pump Station Hydraulic Grade Line Analysis

A March 2012 report by IBI Group was completed for Minto Properties and completed an update to the Signature Ridge Pump Station sanitary hydraulics. The report predicted HGL's for several scenarios for the tributary sewers including the sanitary sewer servicing the subject parcel. The HGL analysis was further refined in September 2012 based on current overflow proposals by the City.

5. Implementation Plan – Kanata West Development Area

This Plan was prepared for the City of Ottawa and the Kanata West Land Owners Group. The Implementation Plan recognizes that Kanata West is a large planning area which will take years to fully develop and therefore includes a mixture of short and long-term development plans and the associated infrastructure requirements to support them. The Plan builds on the framework of the KWCP and KWSS and provides updated comments for future approvals and the actions that would bring about the approval requirements. The Plan further reviews actions that would be conducted if "triggered" by an event or set of circumstances, while allowing sufficient flexibility to ensure that appropriate changes to the undertaking(s), once identified, are made.

6. Conceptual Site Servicing Arcadia Stages 1, 2, 5 & 8 Kanata West - Minto Communities

This IBI Group report, completed in September 2012, provided a high-level conceptual site servicing plan specifically for Minto Arcadia Lands, including the subject site which is Stage 5 of the report. The report focused on details related to water supply, wastewater disposal and stormwater management.

7. Arcadia Interim Stormwater Management Facility Design Brief June 2012

This IBI Group report outlines the design of the interim SWM Facility to service Minto's Arcadia development lands, including these commercial lands, until such time as the ultimate stormwater management facility is constructed.

8. Arcadia Commercial, 370 Huntmar Drive Design Brief October 2014

This IBI Group report provides a detailed servicing scheme to support the development of the Arcadia commercial site.

An engineering pre-consultation with the City of Ottawa was held in August, 2024 regarding the proposed development. Notes from this meeting are included in **Appendix A**.

1.5 Geotechnical Considerations

Paterson Group Inc. was retained to prepare a geotechnical investigation for the site. The objectives of the investigation were to prepare a report to:

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- Determine the subsoil and groundwater conditions at the site by means of boreholes
- To provide geotechnical recommendations pertaining to the design of the proposed development including construction considerations

The geotechnical investigation report PG7168-LET.01 Rev 2 Dated December 19, 2024 confirmed that the site consists of thick layer of silty clay underlain by glacial till overlying the bedrock surface. Based on the presence of the silty clay layer, a varying permissible grade raise plan was provided. The permissible grade raise of 2.0m is recommended for grading within 5m of the proposed buildings and 3.0m grade raise for the parking areas and access lanes.

The report contains recommendations which include but are not limited to the following:

- Fill used for grading beneath the proposed development to meet OPSS Granular 'A' or Granular 'B' Type II placed in lifts no greater than 300 mm compacted to 98% SPMDD
- Pavement Structures as identified below:

Table 1-1 Pavement Structure – Car Only Parking Areas

Local Road – Parking Areas	Thickness
12.5 Asphaltic Concrete	50 mm
OPSS Granular A Base	150 mm
OPSS Granular B Type II Subbase	300 mm

Table 1-2 Pavement Structure – Heavy Truck Parking Areas and Access Lanes

Local Road	Thickness
12.5 Asphaltic Concrete	40 mm
19.0 Asphaltic Concrete	50 mm
OPSS Granular A Base	150 mm
OPSS Granular B Type II Subbase	400 mm

The report contains recommendations which include but are not limited to the following:

- Pipe bedding and cover: The pipe bedding for sewer and water pipes should consist of at least 150 mm of OPSS Granular A crushed stone. The material should be placed in maximum 225 mm thick lifts and compacted to a minimum of 99% of its SPMDD. The cover material, which should consist of OPSS Granular A, should extend from the spring line of the pipe to at least 300 mm above the obvert of the pipe.
- The excavation side slopes above the groundwater level extending to a maximum depth of 3 m should be cut back at 1H:1V or flatter. The flatter slope is required for excavation below groundwater level.

2 Water Supply

2.1 Existing Conditions

As previously noted, the 0.46 ha office and showroom building site is surrounded by Huntmar Drive to the southwest, Campeau Drive to the northwest, and undeveloped land in the remaining surrounding area. An existing PVC 203 mm diameter watermain stub from Campeau Drive was previously installed and is located at the property line to the proposed site. This watermain falls within the City of Ottawa's pressure district Pressure Zone 3W which will provide the water supply to the site.

2.2 Design Criteria

2.2.1 Water Demands

Water demands have been calculated for this proposed site. This site consists of a two-storey office and showroom building. Siamese connections will be provided for this building. Consumption rates are taken from Tables 4.1 and 4.2 at the Ottawa Design Guidelines – Water Distribution and are summarized as follows:

•	Commercial Shopping Center	2500 l/1000m ² /day
•	Other Commercial	28,000 l/gross ha/day
•	ICI Average Day Demand	28,000 l/gross ha/day
•	ICI peak Daily Demand	42,000 l/gross ha/day
•	ICI Peak Hour Demand	75,600 l/gross ha/day

A watermain demand calculation sheet is included in **Appendix B** and the total water demands are summarized as follows:

Average Day
 Maximum Day
 Peak Hour
 0.03 l/s
 0.04 l/s
 0.07 l/s

2.2.2 System Pressure

The Ottawa Design Guidelines – Water Distribution (WDG001), July 2010, City of Ottawa, Clause 4.2.2 states that the preferred practice for design of a new distribution system is to have normal operating pressures range between 345 kPa (50 psi) and 480 kPa (80 psi) under maximum daily flow conditions. Other pressure criteria identified in Clause 4.2.2 of the guidelines are as follows:

Minimum Pressure Minimum	system pressure un	der peak hour demand	conditions shall not be less
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than 276 kPa (40 psi)

Fire Flow During the period of maximum day demand, the system pressure shall not be less

than 140 kPa (20 psi) during a fire flow event.

Maximum Pressure In accordance with the Ontario Building/Plumbing Code, the maximum pressure

should not exceed 552 kPa (80 psi). Pressure reduction controls will be required

for buildings where it is not possible/feasible to maintain the system pressure below 552 kPa.

2.2.3 Fire Flow Rates

The proposed site plan contains one commercial building, with automatic sprinkler systems. The building will fall under OBC Section 3.10, F-2 or F3 occupancy and combustibility. The sprinkler system will be designed and installed in accordance with NFPA-13 requirements. The sprinkler system will be supplied from the city water connection and the demand will be calculated using the hazard classification plus the appropriate inside/outside hose allowances.

Calculations using the Fire Underwriting Survey (FUS version 2020) were conducted to determine the fire flow requirement for the site. Results of the analysis provides a maximum fire flow rate of 5,000 l/min or 83.3 l/s is required which is used in the hydraulic analysis. A copy of the FUS calculations is included in **Appendix B**.

2.2.4 Boundary Conditions

The City of Ottawa has provided the hydraulic boundary conditions at the site. A copy of the boundary conditions is included in **Appendix B** and summarized as follows:

Table 2-1 Hydraulic Boundary Conditions

Criteria	Hydraulic Head	Pressure
Max HGL (Basic Day)	160.7 m	88.8 psi
Peak Hour	156.5 m	82.8 psi
Max Day + Fire Flow (5,000 L/m)	155.4 m	81.2 psi

Ground elevation: 127.5 m

2.2.5 Hydraulic Model

A computer model for the subject site has been developed using the InfoWater Pro program by Autodesk. The model includes the existing watermain and boundary condition at Campeau Drive.

2.3 Proposed Water Plan

2.3.1 Proposed Water Plan

This site will be serviced by connecting to an existing 200mm diameter watermain extending from Campeau Drive. The building will be serviced by a lateral service connection from the proposed watermain. There is one hydrant proposed on site located at the east side of the proposed parking area, within 45m of the proposed building.

Refer to the general plan of services **Drawing C-001** for detailed watermain layout for the subject site.

2.3.2 Hydraulic Analysis

The hydraulic model was run under basic day conditions to determine the maximum pressure for the site. The minimum pressure for the site is determined in the peak hour analysis using the provided boundary condition. Results of the analysis for the site are summarized in Section 2.3.2 and the water model schematic and model results are included in **Appendix B**.

2.3.3 Modeling Results

The hydraulic model was run under basic day, maximum day with fire flows and under peak hour conditions. Results of the hydraulic model are included in **Appendix B** and summarized as follows:

Basic Day (Max HGL) Pressure Range (kPa)
Peak Hour (Min HGL) Pressure Range (kPa)
553.36 – 557.09

Fire Flow @ 5,000 L/min Residual Pressure (kPa)
Residual Pressure @ 140 kPa Available Fire Flow (l/s)
283.83

A comparison of the results and design criteria is summarized as follows:

Maximum Pressure All nodes in basic day scenario exceed 552 kPa (80 psi), therefore pressure reducing

control is required for the proposed building in this development.

Minimum Pressure All nodes in the model exceed the minimum value of 276 kPa (40 psi).

Fire Flow The minimum design fire flow under maximum day conditions with minimum system

pressure of 140 kPa is 283.83 l/s for retail which exceeds the requirement of 83.3 l/s (5,000

I/min) from Section 2.3.3.

3 Wastewater Disposal

3.1 Existing Conditions

There is an existing 375mm diameter sanitary sewer along Campeau Drive, which flows east along Campeau Drive and flows ultimately to the Ottawa Wastewater Treatment Plant at 395 Terry Fox Drive. There is an existing 200mm sanitary cap from existing MH301 to the property line in anticipation of this development. This sewer has been designed to provide wastewater service to the subject development site.

3.2 Previous Studies

The October, 2014 IBI Group Design Brief for Arcadia Commercial provided the wastewater servicing plan for the Arcadia Retail Development, including the subject site. The detailed sanitary sewer design sheets and related sanitary drainage area plan 35355 - C-501 are included in **Appendix C**.

3.3 Design Criteria

The sanitary sewers for the subject site will be based on the City of Ottawa design criteria. It should be noted that the sanitary sewer design for this study incorporates the latest City of Ottawa design parameters identified in Technical Bulletin ISTB-2018-01. Some of the key criteria will include the following:

Average commercial flow = 28,000 l/s/ha

• Peak ICI flow factor = 1.5 if ICI area is > 20% total area

1.0 if ICI area is ≤ 20% total area

Inflow and Infiltration Rate = 0.33 l/s/ha
 Minimum Full Flow Velocity = 0.60 m/s

Maximum Full Flow Velocity = 3.0 m/s

Minimum Pipe Size = 200 mm diameter

3.4 Recommended Wastewater Plan

The on-site sanitary system will consist of 200mm PVC sewer installed at standard depth and slope and will provide 150mm service connections to the proposed building. The sewers have been designed using the criteria noted above in section 3.2 and outlet via the existing sanitary stub connection to the sanitary sewer to Campeau Drive.

As noted in the pre-consultation meeting with the City of Ottawa, a monitoring maintenance hole was included just inside the property line of the subject site. The July 2012 Site Servicing Report 'Arcadia – Kanata West Ph 1' by IBI Group identified conceptually the servicing for the 9.84 Ha parcel of land south of Campeau Drive. This site comprises approximately 1.79 Ha of that area. The Campeau Drive sewer was designed and constructed assuming 0.85 Ha of commercial lands connecting to MH301A, with peak flows of 0.98 l/s. This site generates approximately 1.47 l/s to MH 301A. The minor (0.49 l/s) increase in flow to MH 301A has negligible impact on the system as it has over 34 l/s spare capacity up to MH 303A.

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This site is comprised of slab on grade construction (no basements). The minor (0.49 l/s) increase in flow from MH 301A to 303A will not negatively impact this site. Sanitary design sheet from 'Arcadia – Kanata West Ph 1' site servicing report, which demonstrates the capacity in the receiving and downstream wastewater system is included in **Appendix C**.

As identified in the Arcadia Commercial Design Brief, there are existing houses along Campeau Drive and the current freeboard between the HGL and USF is approximately 1.18 m at MH301A. It is anticipated that any minor HGL adjustment (1 to 2 cm) due to the 0.49 l/s increase at this MH will leave these units within excess of 1 m of freeboard.

A copy of the sanitary sewer design sheet can be found in **Appendix C.** Please refer to the General Plan of Services **Drawing C-001** for further details.

4 Site Stormwater Management

4.1 Existing Conditions

The undeveloped subject lands currently drain east away from Campeau Drive and Huntmar Drive intersection to the recently developed Country Glen Way. There is an existing 825mm diameter downstream storm sewer along Campeau Drive with a 600mm storm stub from the existing MH301 to the property line with an allocation of flows from this development previously taken into consideration.

The Arcadia Commercial Site Plan was allocated a total 100-year release rate of 240L/s/Ha. The original site plan approval included two separate outlets, one to Campeau Drive and one to Country Glen Way. Based on the original site area draining to Campeau, of 0.8Ha, the theoretical maximum release rate is 192.00L/s. However, the site stormwater management plan identified a release rate to Outlet #2 (MH 301 in Campeau Drive) of 125.94 L/s. This report aims to meet the more restrictive target to MH301 established in the Site Plan. An excerpt from the Arcadia Commercial Stormwater Management Calculations has been provided in Appendix D.

4.2 Design Criteria

The stormwater system was designed following the principles of dual drainage, making accommodations for both major and minor flow. The on-site minor system design criteria identified below are consistent with the current City of Ottawa Sewer Design Guidelines.

Some of the key criteria include the following:

Design Storm 1:2year return (Ottawa)

Rational Method Sewer Sizing

Initial Time of Concentration
 10 minutes

Runoff Coefficients

Landscaped Areas
 Asphalt/Concrete
 Roof
 C = 0.20
 C = 0.90
 C = 0.90

Pipe Velocities
 Minimum Pipe Size
 250 mm diameter
 (200 mm CB Leads)

4.3 Proposed Minor System

Where possible, the minor system storm sewers for the subject site will be sized based on the rational method and the City of Ottawa 2-year event. Minor storm flow to the downstream storm sewer network will be controlled by Inlet Control Devices (ICDs) to limit flow and prevent sewer surcharging downstream.

Due to the severance area and the need to maintain maximum flexibility for future development opportunities within the existing site, a rebalancing of tributary areas to Campeau has been completed. General Areas 122, 123, 110A and Roof Areas BLK700 and BLK800 (as identified on the original site plan) have been removed from the tributary outletting to Campeau. The sum of the areas removed from Outlet #2 is 0.30Ha. This has permitted an expansion

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of the parking lot area adjacent to the proposed sales Center drain into the Campeau outlet without constructing services through the remainder of the site, as originally intended. The sum of the area added to Outlet #2 is 0.23Ha. An overall drainage area plan has been provided in **Appendix D** which demonstrates the areas removed (in red) and the areas added (in green).

The proposed minor storm sewer will range between 300 mm diameter and 600 mm diameter. Catch basin lead pipes will be 200 mm in diameter. The minor storm sewer outlet will be via the 600 mm diameter pipe which is proposed to connect to the existing 825 mm diameter storm sewer in Campeau Drive.

An allocation has been provided in the minor system for future flows to the east. This includes Future Building Block 600 and future parking lot area 120, as were identified on the original site plan approval.

A detailed storm sewer design sheet and the associated storm sewer drainage area plan is included in **Appendix D**. The General Plan of Services, depicting all on-site storm sewers can be found in **Appendix A**.

4.4 Stormwater Management

As previously noted, the overall site release rate was determined based on a level of service of 240 L/s/Ha. However, the original SWM concept for the approved site plan had adjusted the overall release rate between the two outlets, and Outlet #2 (MH301 to Campeau) is slightly overcontrolled relative to the level of service for the whole site. The intent is to maintain the outlet dispersion with **125.94** L/s as the maximum permissible release rate to Campeau.

At certain locations within the site, the opportunity to capture and/or store runoff is limited due to grading constraints and site plan geometry. These locations are generally located at the site's perimeter, where it is necessary to tie into public ROWs and adjacent properties or in areas where ponding stormwater is undesirable. These "uncontrolled" areas – 0.064 hectares in total, have a C value of 0.20 and increased by 25% during 100-year events (as per City SDG). It should be noted that the total uncontrolled areas are based on the uncontrolled areas identified in the original site plan SWM concept and are all located adjacent to future development areas. All areas within the severed parcel are captured and controlled.

4.5 Inlet Control

Per the original stormwater management calculations provided for the entire site, the restricted flow rate was used for the Campeau outlet is:

Q_{restricted} = 125.94 L/s

As noted in Section 4.4, a small, landscaped area along the west property line will drain offsite uncontrolled.

Based on a 100-year event, the flow from the 0.063 Ha uncontrolled area (including storm drainage area UNC1, future UNC1B, UNC1C and UNC1D) can be determined as:

 $Q_{uncontrolled} = 2.78 \times C \times i_{100yr} \times A$ where:

C = Average runoff coefficient of uncontrolled area = 0.20 x 1.25

i_{100yr} = Intensity of 100-year storm event (mm/hr)

= $1735.688 \times (T_c + 6.014)^{0.820} = 178.56 \text{ mm/hr}$; where $T_c = 10 \text{ minutes}$

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Therefore, the uncontrolled release rate can be determined as:

Quncontrolled =
$$2.78 \times 1.25C \times i_{100yr} \times A$$

= $2.78 \times 1.25 \times 0.020 \times 178.56 \times 0.063$
= 7.82 L/s

The higher roof top area of 0.027 ha will be uncontrolled due to difficulty of maintenance. The total flow from the uncontrolled roof area UNC2 can be determined as:

The maximum allowable release rate to Campeau Drive (Outlet #2/MH301) can then be determined as:

Based on the flow allowance at the various inlet locations, various sizes of inlet control devices (ICDs) were chosen in the design. The design of the inlet control devices is unique to each drainage area and is determined based on various factors, including hydraulic head and allowable release rate. Ponding locations and elevations are summarized on the Ponding Plan **Drawing C-600**, and included in **Appendix D**.

4.6 On-Site Detention

The site was designed to limit runoff to the allowable release rate up to the 2-year post-development storm event. Flows exceeding the maximum allowable release rate will be contained on-site via underground and surface storage at strategic locations. Orifices are proposed in manholes, catch basins and roof drains to control runoff from the site. The modified rational method determined the storage volumes during a 2-year and 100-year storm event. Available surface ponding volumes at each inlet were determined using CAD surface volume tools. As per the Ottawa SDG, when underground storage is considered available storage, the ICD release rate is to be reduced by 50% to determine the storage requirements.

The proposed roof is partially flat and partially peaked. The drainage area plan considers the roof structure of this building. The flat roof area has accounted for ponding storage with depths not exceeding 150mm per the OBC, and there are five roof drains. Watts roof drain flow control weirs are proposed on each inlet, set to 2 L/s or 30GPM each.

Major flow up to the 100-year storm is contained on-site and is gradually released to the minor system. Apart from the small uncontrolled areas, major flow does not leave the site via overland flow.

The site's stormwater management has ensured that surface ponding will not occur during the 2-year storm event.

Stormwater management and on-site underground storage volume calculations, and manufacturers spec sheets are included in **Appendix D**.

A summary of the ICD type for each drainage area and corresponding storage details is provided in Table 4.1 below.

Table 4-1 Post-Development Storage Summary Table

Location	ICD Type	Drainage Area (Ha)	Restricted / Storage Uncontrolled Required Flow (L/s) (m³)		Storage Provided (m³)		
			2 - Year	2 - Year	Surface	UGS	Total
Controlled S	torm Sewer S	ystem					
FUT 600	-	0.06	2	7.22	33.75	0	33.75
FUT 120	-	0.11	15	4.18	33.99	0	33.99
ROOF	WATTS	0.07	10	2.38	18.15	0	18.15
110	IPEX MHF	0.12	28	0	8.49	0	8.49
102	IPEX MHF	0.24	25	20.49	23.30	68.80	92.10
MH100B	IPEX MHF	0.04	24	0	1.57	0	1.57
Total		0.64	104	34.27	119.25	68.80	188.05

The area Future 120 has identified surface level ponding during the 2-year event. The drainage area and release rate have been carried form the original site plan SWM concept. Future site plan development will need to address 2-year ponding in this area.

Area 102 identifies a 20.49m3 storage required during the 2-year event. 68.80m3 of storage is provided underground, therefore there will be no surface ponding during the 2-year event.

4.7 100-Year Overflow

A review of the 100-year event, and overflow depth has been performed using the modified rational method. The calculations are included in the modified rational stormwater management sheets **Appendix D**.

A summary of the required storage volumes and overflow balances is provided below.

Table 4-2 Post-Development 100yr Storage Summary Table

Drainage Area	ICD Restricted Flow (L/s)	100 Year Storage Required (m³)	Total Storage Provided* (m3)	Upsteam Overflow (m³)	100 – Year Overflow (m³)
FUT 600	2	26.48	33.75	0	0

November 13, 2024 Revised April 30, 2025

Drainage Area	ICD Restricted Flow (L/s)	100 Year Storage Required (m³)	Total Storage Provided* (m3)	Upsteam Overflow (m³)	100 – Year Overflow (m³)
FUT 120	15	26.10	33.99	0	0
ROOF	10	15.64	18.15	0	0
110	28	7.96	8.49	0	0
102	25	90.65	92.10	0	0
MH100B	24	0.20	1.57	0	0
Total	104	167.03	188.05	0	0

^{*}includes surface storage and underground storage. For building Areas, it includes rooftop storage.

The 100-year flow from all areas within the proposed site plan is contained on-site, with no overland flow offsite or to other areas.

4.8 100-Year + 20% Stress Test

A cursory review of the 100-year event + 20% has been performed using the modified rational method. The peak flow from each area during a 100-year event has increased by 20%. The calculations have been included in **Appendix D.**

A summary of the require storage volumes, and overflow balances is provided below.

Table 4-3 Post-Development 100yr+20% Stress Test Storage Summary Table

Drainage Area	ICD Restricted Flow (L/s)	100 Year + 20% Storage Required (m³)	Total Storage Provided	Upsteam Overflow (m³)	100 Year + 20% Overflow (m³)
FUT 600	2	33.48	33.75	0	0
FUT 120	15	34.56	33.99	0	0.57
ROOF	10	20.80	18.15	0	2.65
110	28	11.57	8.49	0	3.08
102	25	115.68	92.10	2.65	26.23
MH100B	24	0.53	1.57	0	0
Total	104		188.05		

The overland flow from 110 is directed to Campeau Drive. The 100yr +20% overflow volume from Area 110 is **3.08** m3 at peak. Based on a peak Tc of 6 minutes, the volume can be reverse calculated to **8.55** L/s. A channel depth

conveyance calculation has been provided to determine the overflow depth of **0.02m** above the static ponding elevation.

The overland flow from the area tributary to 102 is directed south to future development lands. The 100yr +20% overflow volume from Area 102, including upstream roof contribution (2.65 m3), is **26.23** m3 at peak. Based on a peak Tc of 46 minutes, this volume can be reverse calculated to **9.50 L/s**. A channel depth conveyance calculation has been provided to determine the overflow depth of **0.03m** above static ponding elevation. These stress test flows will need to be considered in future SWM analysis.

4.9 Underground Storage

Due to the site's constraints and the stormwater management plan, underground storage was deemed the best option to contain the 100-year storm event on site. The table below summarizes underground storage, and additional information about the underground storage structures is found in **Appendix D**.

Table 4-3 Underground Storage Summary Table

Storage Name	Structure Type	Storage Provided (m³)
CB102	Stormtech DC-780 or approved equivalent	68.80

4.10 Quality Control

As noted in the Arcadia Commercial Design Brief, flows from the subject site discharged into the Arcadia Interim SWM facility, which provided an interim quality and quantity control facility for the Arcadia community. We understand that the ultimate SWM facility has been constructed and is operational.

4.11 Hydraulic Grade Line

As identified in the Arcadia Commercial Design Brief, as part of the original site plan approval, the storm Hydraulic Grading Line (HGL) is dictated by downstream infrastructure. The storm HGL within the existing storm sewer on Campeau Drive is at 96.05m at existing MH's 301. The sewers are not surcharged at these points, since the internal sewers are restricted to meet the downstream system design requirements and sized to accommodate the restricted flow. The onsite sewers will not be surcharged, and as such, the HGL will follow the obvert of the pipes. Additionally, this is a slab on grade development, and the City requirement for 0.3 m freeboard to USF to protect basements from flooding is not applicable. The minimum freeboard from the onsite HGL (obvert of storm sewer) to the finished floor elevation is 1.51 m.

5 Grading and Roads

5.1 Site Grading

The existing grades within portions of the proposed development lands vary significantly due to the existing topography of the site. The grading plan will require the balancing of various requirements including but not limited to geotechnical constraints, minimum/maximum slopes, overland routing of stormwater, all to ensure the site is graded following municipal and accessibility standards.

Special consideration is needed for the building, where elevated foundation walls are required along the west façade to maintain the grade. A minimum of 150mm foundation exposure is required around the perimeter of the building. Internal and external steps will also be required to match grades. The main entrance has been designed to provide barrier-free access to the parking areas.

The parking areas have been designed to meet accessibility requirements, with slopes ranging between 0.5% along curbs to a maximum of 5%.

Refer to the grading plan provided in Appendix E.

5.2 Road Network

No public roads are proposed through the site. A minimum 8.0m wide drive aisle has been provided, as shown on the Site Plan in **Appendix A.** An internal Fire route has been shown where fire truck access is required, as determined by the site architect.

There are 39 parking stalls provided on the site, of which two are barrier-free.

Pedestrian access facilities and multiple connections to Campeau Drive and Huntmar are provided.

A bicycle parking facility has been proposed adjacent to each building entrance.

Noise attenuation features and indoor noise clause provisions will not be required for commercial use lands for road noise generated by the adjacent roads.

6 Source Controls

6.1 General

Since an end-of-pipe treatment facility is already provided for the development lands, stormwater site management for the subject lands will focus on the site level or source control management of runoff. Such controls or mitigative measures are proposed for this development not only for final development but also during construction and build-out. Some of these measures are:

- Flat site grading where possible
- Vegetation planting
- Groundwater recharge in landscaped areas

6.2 Lot Grading

Where possible, all of the proposed blocks within the development will make use of gentle surface slopes on hard surfaces such as asphalt and concrete. In accordance with local municipal standards, all grading will be between 0.5 and 5.0 percent for hard surfaces and 2.0 and 7.0 percent for all landscaped areas. Significant grade changes will be accomplished through the use of terracing (3:1 max slope), ramps and/or retaining walls. All street and parking lot catchbasins shall be equipped with 3.0m subdrains on opposite sides of a curbside catchbasin running parallel to the curb, and with 3.0m subdrains extending out from all 4 sides of parking lot catchbasins.

6.3 Vegetation

As with most site plans, the developer will be required to complete a vegetation and planting program. Vegetation throughout the development including planting along roadsides and within the individual blocks provides opportunities to re-create lost vegetation.

6.4 Groundwater Recharge

Groundwater recharge targets have not been identified for this site. Perforated sub-drain systems will be implemented at capture locations in all vegetated areas. This will promote increased infiltration during low flow events before water is collected by the storm sewer system.

7 Conveyance Controls

7.1 Generals

Besides source controls, the development also proposes to use several conveyance control measures to improve runoff quality. These will include:

- Vegetated swales
- Catchbasin sumps and manhole sumps

7.2 Catchbasins and Maintenance Hole Sumps

All catchbasins within the development, either rear yard or street, will be constructed with minimum 600 mm deep sumps. These sumps trap pollutants, sand, grit and debris which can be mechanically removed prior to being flushed into the minor pipe system. Both rear yard and street catchbasins will be to OPSD 705.02. All storm sewer maintenance holes serving local sewers less than 900 mm diameter shall be constructed with a 300 mm sump as per City standards.

8 Sediment and Erosion Control Plan

8.1 General

During construction, existing stream and conveyance systems can be exposed to significant sediment loadings. Although construction is only a temporary situation, it is proposed to possibly introduce a number of mitigative construction techniques to reduce unnecessary construction sediment loadings. These may include:

- Until the local storm sewer is constructed, groundwater in construction trenches shall be pumped into a filter mechanism prior to release to the environment
- Vegetated swale sediment capture filter socks will remain on open surface structures such as maintenance holes and catchbasins until these structures are commissioned and put into use
- Silt fence on the site perimeter will be installed

8.2 Trench Dewatering

Any trench dewatering using pumps will be discharged into a filter trap made up of geotextile filters and straw bales similar in design to the OPSD 219.240 Dewatering Trap. These will be constructed in a bowl shape with the fabric forming the bottom and the straw bales forming the sides. Any pumped groundwater will be filtered prior to release to the existing surface runoff. The contractor will inspect and maintain the filters as needed, including sediment removal and disposal and material replacement as needed. It should be noted that that the contractor will be responsible for the design and management of the trap(s).

8.3 Seepage Barriers

In order to further reduce sediment loading to the stormwater management facility, seepage barriers will be installed on any surface water courses at appropriate locations that may become evident during construction. These barriers will be Light Duty Straw Bale Barriers per OPSD 219.100 and Heavy-Duty Silt Fence Barriers per OPSD 219.130; locations are shown on the Sediment and Erosion Control Plan included in **Appendix E**. They are typically made of layers of straw bales or geotextile fabric staked in place. All seepage barriers will be inspected and maintained as needed.

8.4 Surface Structure Filters

All catchbasins, and to a lesser degree, manholes, convey surface water to sewers. Until streets are asphalted and curbed, all catchbasins and manholes will be constructed with sediment capture inserts or equivalent located between the structure frame and cover. These will stay in place and be maintained during construction and build until it is appropriate to remove same.

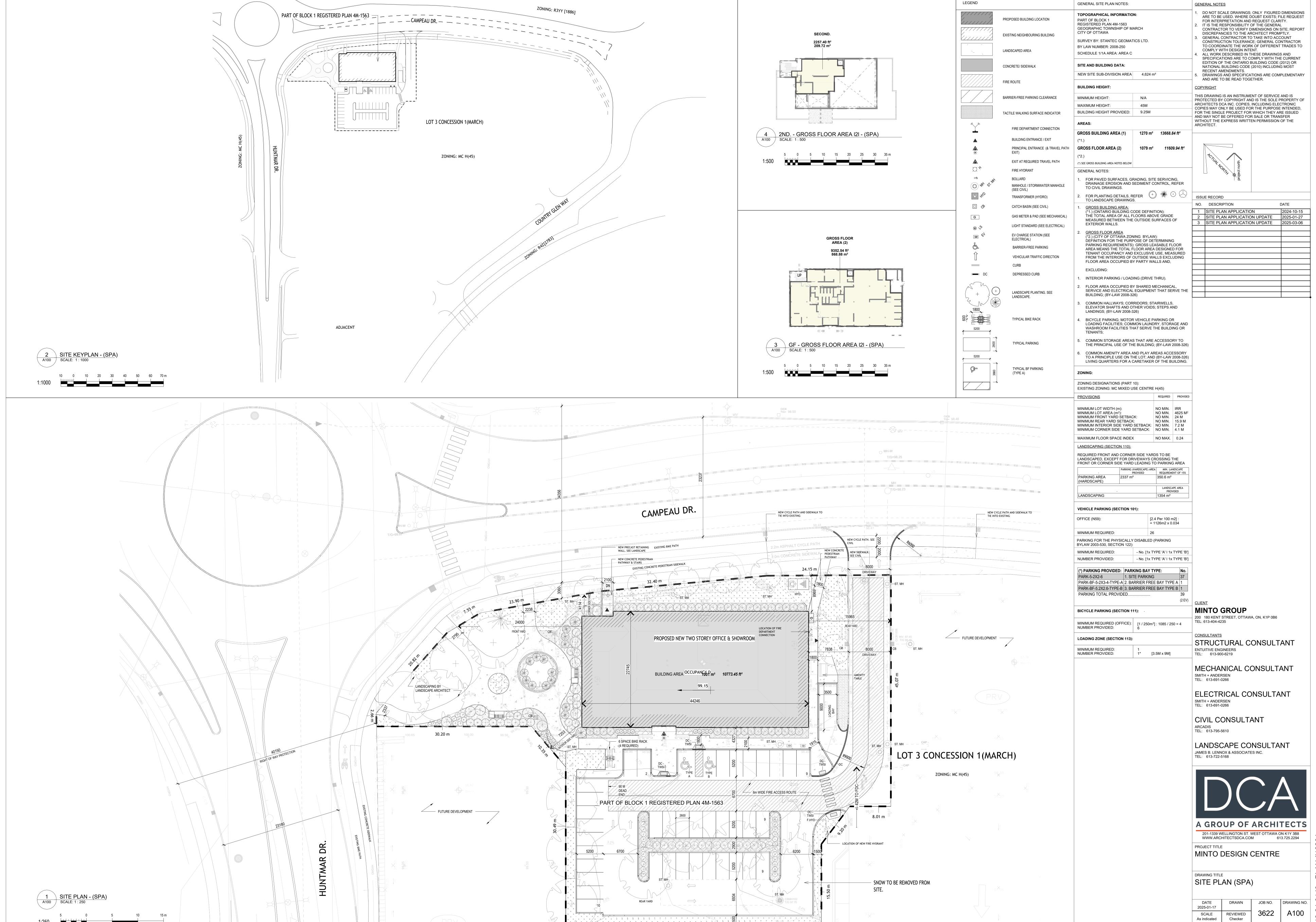
9 Conclusion

This report has illustrated that the proposed two-storey office and showroom development can be serviced via existing municipal services. The water network will be extended to provide necessary service. All sanitary and storm sewer designs for this development will be completed in conformance with City of Ottawa standards while acknowledging downstream constraints. By limiting flow into the minor storm sewer system as per the applicable local stormwater management criteria and allowing for excess surface storage on-site, all stormwater management requirements will be met. Adherence to the Sediment and Erosion Control Plan during construction will minimize harmful impacts on surface water.

Based on the information provided within this report, the plans prepared for the subject development can be serviced to meet City of Ottawa requirements.

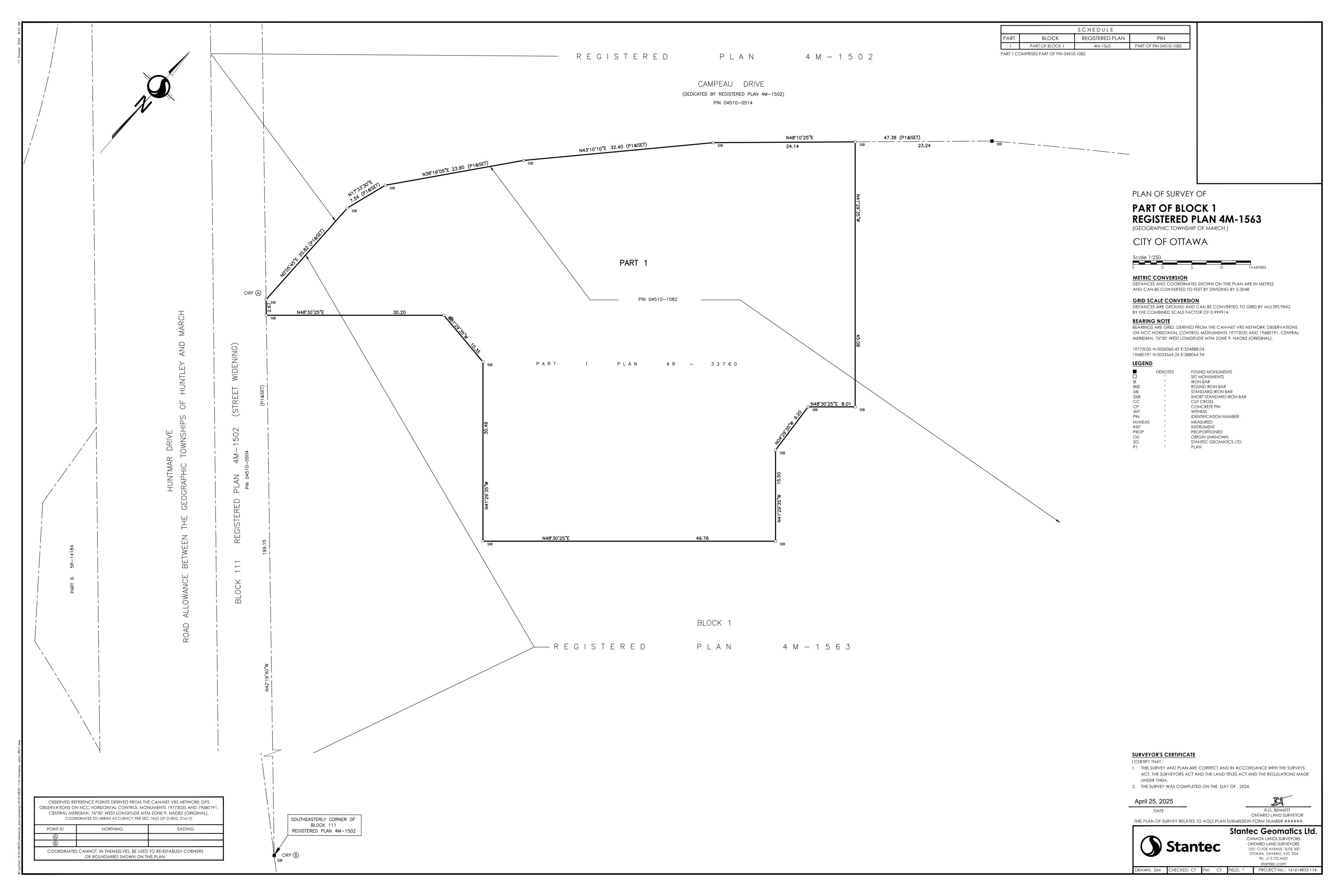
Appendix A

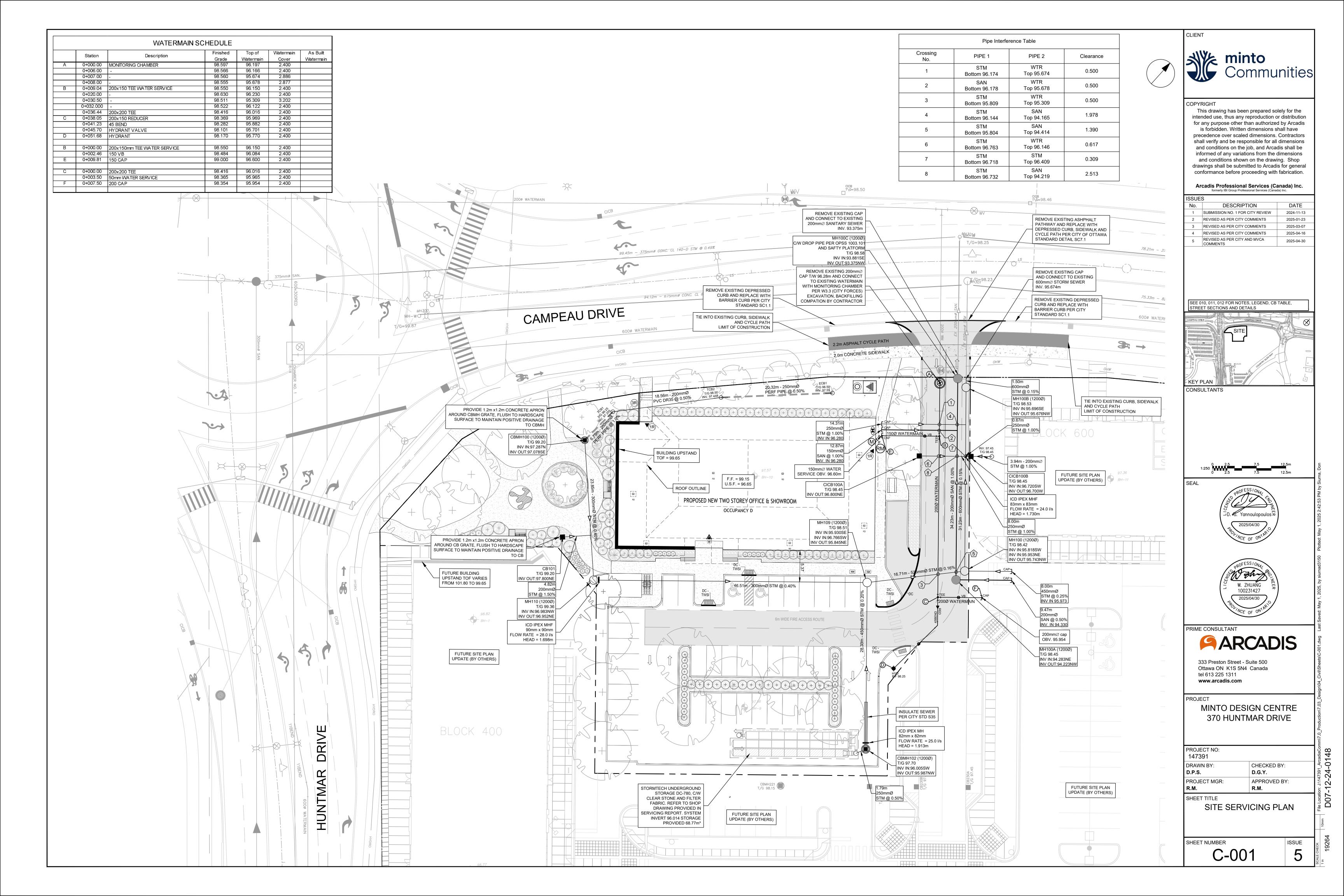
- Site Plan
- Stantec Plan of Survey
- Site Servicing Plan 147391-C-001
- Arcadia Site Servicing Plan 35355-C-100
- Pre-Consultation City Comments
- Study and Plan Identification List

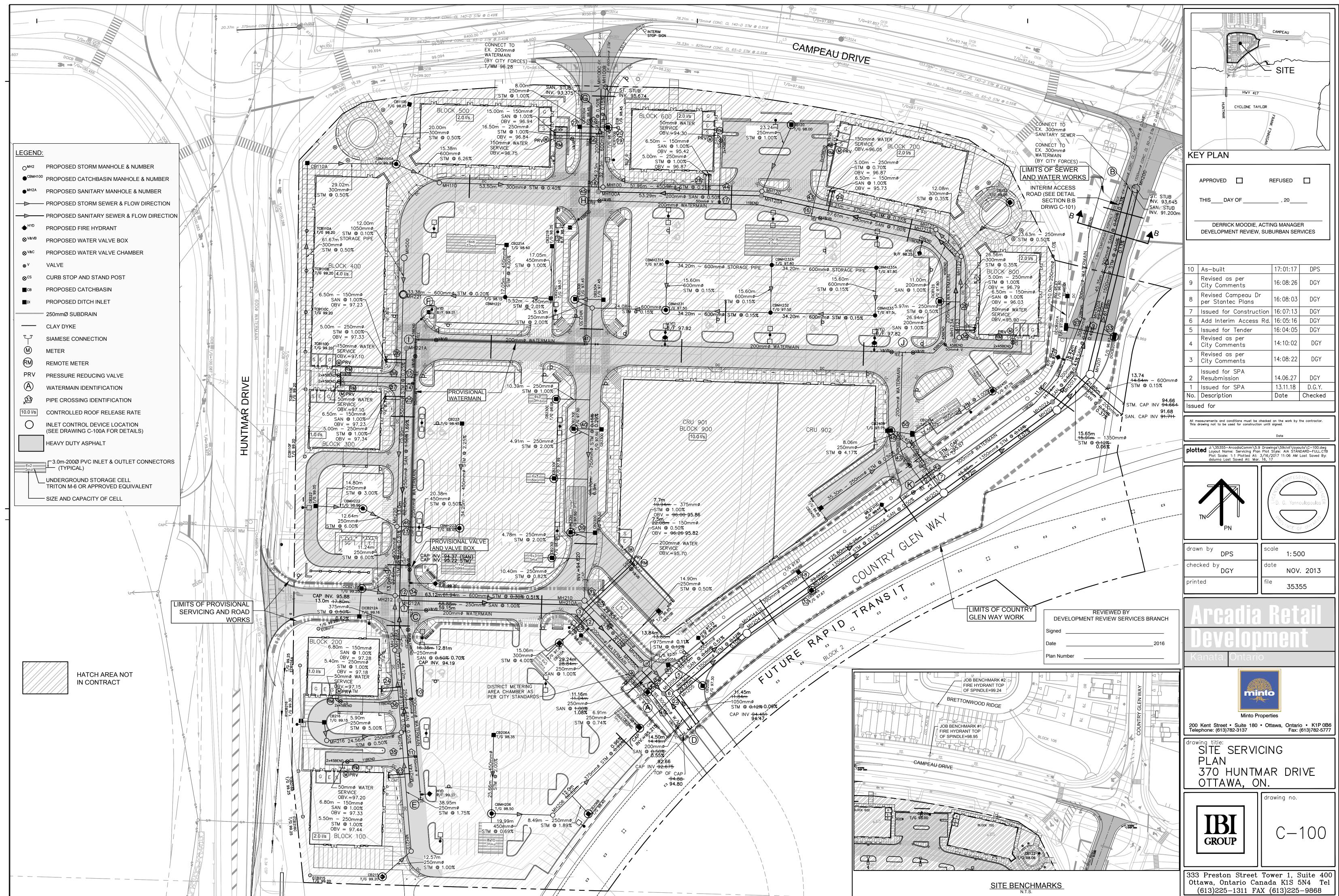


49.76 m

ARCHITECTURAL







D07-12-14-0014



File No.: PC2024-0304

August 21, 2024

Kevin Harper Minto Communities Inc.

Via email: kharper@minto.com

Subject: Pre-Consultation: Meeting Feedback

Proposed Site Plan Control Application – 370 Huntmar Drive

Please find below information regarding next steps as well as consolidated comments from the above-noted pre-consultation meeting held on August 13, 2024.

Pre-Consultation Preliminary Assessment

1 □	2 □	3 □	4 □	5 ⋈
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One (1) indicates that considerable major revisions are required while five (5) suggests that the proposal appears to meet the City's key land use policies and guidelines. This assessment is purely advisory and does not consider technical aspects of the proposal or in any way guarantee application approval.

Next Steps

- 1. A review of the proposal and materials submitted for the above-noted preconsultation has been undertaken.
- 2. In your subsequent submission, please ensure that all comments or issues detailed herein are addressed. A detailed cover letter stating how each issue has been addressed must be included with the submission materials. Please coordinate the numbering of your responses within the cover letter with the comment number(s) herein.
- 3. Please note, if your development proposal changes significantly in scope, design, or density before the next submission, you may be requested to repeat the preconsultation process before filing an Official application.

Supporting Information and Material Requirements

- 1. The attached **Study and Plan Identification List** outlines the information and material that has been identified, during this phase of pre-consultation, as either required (R) or advised (A) as part of a future complete application submission.
 - a. The required plans and studies must meet the City's Terms of Reference (ToR) and/or Guidelines, as available on Ottawa.ca. These ToR and Guidelines outline



the specific requirements that must be met for each plan or study to be deemed adequate.

Consultation with Technical Agencies

1. You are encouraged to consult with technical agencies early in the development process and throughout the development of your project concept. A list of technical agencies and their contact information is enclosed.

Planning

Comments:

- 1. The following policies apply to the site:
 - a. The site is designated Minor Corridor on Schedule B5 Suburban (West) Transect.
 - b. Huntmar Drive and Campeau Drive are both identified as Arterial Roads on Schedule C4 Urban Road Network.
 - c. The site is subject to Area-Specific Policy 2 Kanata West, per Annex 5 Urban and Rural aras Subject to Area-Specic Policies. Refer to Volume 2C for applicable policies.
- 2. It is understood that the owner no longer intends to proceed with the previously approved commercial development on the site (File No. D07-12-14-0014) has lapsed and the owner no longer intends to proceed.
 - a. Please ensure this is clear on any plans submitted in support of the proposed development. The current plans showing the proposal in the context of the previously approved development may be misleading to staff, technical agencies, public, etc. in future reviews.
 - b. Is there an intention to release the registered site plan agreement (Instrument No. OC1817302) on the subject site and surrounding lands?
- 3. Provide further details on the use(s) of the proposed building. Staff understand that there is an intention to have offices, a combined sales and design centre, as well as showroom space in the building. Zoning interpretation have confirmed that more information is required to confirm whether there is a "retail" component to the use.

4. Landscaping

a. Please ensure that the minimum landscaping requirements identified in Section 110(1) of the Zoning By-law are met. Please note that a landscaped



buffer with a minimum width of 1.5 metres must be provided between the permitter of the parking lot and a lot line not abutting a street, per Table 110(b). It appears that there are deficiencies along the west, south and east lot line.

- b. Consider opportunities for additional trees and landscaping in the development. It appears that parking is being provided above the minimum zoning requirements – consider removing excess parking spaces to meet minimum landscaping buffer requirements and allow for the introduction of additional landscaped islands within the surface parking lot. Refer to Policy 11 of Section 4.1.4 of the Official Plan for additional direction on surface parking lot design.
- 5. Consider opportunities to visually screen the loading dock from the sightline of the front lot line. Policy 3 of Section 4.6.5 of the Official Plan directs development along corridors shall improve the attractiveness of the realm by internalizing loading areas and visually screening surface parking.
- 6. Explore opportunities to provide additional bicycle parking on-site to promote active transportation.
- 7. Required Applications
 - a. Site Plan Control (Standard) more information on the process can be found here.
 - b. If required, zoning relief can be sought through a Minor Variance or Minor Zoning By-law Amendment application.
 - i. Minor Variance more information on the process can be found here.
 - ii. Zoning By-law Amendment (Minor) more information on the process can be found here.
 - c. Consent for Severance more information on this process can be found <u>here</u>. Please continue to engage with <u>Elizabeth King</u>, Planner I (DRAW), on the proposed severance.

Feel free to contact Colette Gorni, Planner II (DR West), for follow-up questions.

<u>Urban Design</u>

Comments:

8. An Urban Design Brief is not required as the project ties into the larger approved Site Plan Control Application for the site.



- 9. Urban Design staff require an architectural package which includes a Site Plan and Building Elevations, as well as a Landscape Plan as part of the Applicant's submission.
- 10. Urban Design staff look forward to seeing the planting strategy and would encourage the Applicant to explore opportunities for tree planting.

Feel free to contact Kadri Nader (kadri.nader@ottawa.ca), Urban Design Planner, for follow-up questions.

Engineering

Comments:

11. Water Design

a.	A water boundary condition request should be made for this development.
	Please provide the following information including supporting calculations:

I.	Location of service
ii.	Type of development
iii.	Amount of fire flow required.
iv.	Average daily demand: l/s.
٧.	Maximum daily demand:l/s.
vi.	Maximum hourly daily demand: l/s

- b. A 203mm PVC watermain is available at the site propoerty line
- c. Submission to include watermain system analysis demonstrating adequate pressure as per section 4.2.2 of the Water Distribution Guidelines.
- d. Demonstrate adequate hydrant coverage for fire protection. Please review Technical Bulletin ISTB-2018-02, Appendix I table 1 maximum flow to be considered from a given hydrant.
- e. Any proposed emergency route (to be satisfactory to Fire Services).

12. Sanitary Design

- a. A 200mm sanitary sewer is available at the site property line
- b. A monitoring maintenance hole is required just inside the property line for the proposed development.



- c. Please apply the wastewater design flow parameters in Technical Bulletin PIEDTB-2018-01.
- d. Demonstrate that there is adequate residual capacity in the receiving and downstream wastewater system

13. Storm Design

- a. There is access to a 600mm storm sewer at the site property line
- IDF information derived from the Meteorological Services of Canada rainfall data, taken from the MacDonald Cartier Airport, collected 1966 to 1997 must be applied
- c. The pre-development runoff shall be the lower of the existing coefficient or a maximum equivalent 'C' of 0.5, whichever is less (§ 8.3.7.3).
- d. Time of concentration: to be calculated, min Tc = 10mins
- e. Design storm for receiving sewer: 5-year design storm
- f. Allowable release rate: 240L/s/Ha.
- g. Storm sewer outlets should not be submerged.
- h. Proovide information on the monitoring manhole should be located in an accessible location on private property near the property line (ie. Not in a parking area).
- 14. An MECP Environmental Compliance Approval [Private Sewage Works] will be required should the proposed storm system collect off-site drainage. An exemption to review the application under City's Transfer of Review may be granted for the proposed development provided that specific criteria are met.

15. Geotechnical

 Sensitive Marine Clay (SMC) is widely found across Ottawa- geotechnical reports should include Atterberg Limits, consolidation testing, sensitivity values, and vane

16. Additional Notes

- a. No road moratorium that would impact the application has been identified
- b. Any easement identified should be shown on all plans
- c. For any proposed exterior light fixtures, please provide certification from a licensed professional engineer confirming lighting has been designed only using fixtures that meet the criteria for full cut-off classification as



recognized by the Illuminating Engineering Society of North America and result in minimal light spillage onto adjacent properties (maximum allowable spillage is 0.5 fc). Additionally, include in the submission the location of the fixtures, fixture type (make, model, part number and mounting height.

Feel free to contact Abibatou Dieme (<u>abibatou.dieme@ottawa.ca</u>), Infrastructure Project Manager, for follow-up questions.

Noise

Comments:

17. Not required for sales office.

Feel free to contact Mike Giampa (mike.giampa@ottawa.ca), Transportation Project Manager, for follow-up questions.

Transportation

Comments:

- 18. Right-of-way protection (if required)
 - a. See Schedule C16 of the Official Plan.
 - b. Any requests for exceptions to ROW protection requirements <u>must</u> be discussed with Transportation Planning and concurrence provided by Transportation Planning management.
- 19. A TIA is not required.

Feel free to contact Mike Giampa (mike.giampa@ottawa.ca), Transportation Project Manager, for follow-up questions.

Environment

Comments:

- 20. There are no natural heritage features, surface water features, or species-at-risk habitat on or near the site that would trigger the need for an Environmental Impact Statement (EIS). An EIS is not required as part of this application.
- 21. Please consider additional tree plantings wherever possible to help meet the City's urban forest canopy goals and to help mitigation the impacts of the urban heat island effect and climate change. Please note that the City prefers that all plantings be of native and non-invasive species.



Feel free to contact Mark Elliott (mark.elliot@ottawa.ca), Environmental Planner, for follow-up questions.

Forestry

Comments:

22. Tree Conservation Report

- a. Please confirm whether any trees >10cm in diameter exist on site or of any size in the ROW; if yes, a Tree Conservation Report is required, in accordance with Schedule E of the Tree Protection By-law. Ownership of all trees on the subject site and with Critical Root Zones extending onto the subject site must be determined, and plans must show how they will be protected from proposed works.
- b. A permit is required prior to removal of any protected trees on site. The tree permit will be released upon site plan approval. Please contact the planner associated with the file or the Planning Forester, Nancy Young (Nancy.young@ottawa.ca) for information on obtaining the tree permit.
- c. To ensure that no harm is caused to breeding birds, tree removal and vegetation clearing should be avoided during the migratory bird season (April 15 – August 15) as specified by The City of Ottawa's Environmental Impact Study Guidelines.

23. Landscape Plan

- a. A Landscape Plan is required with this application and must address all requirements within the Landscape Plan Terms of Reference https://documents.ottawa.ca/sites/documents/files/landscape_tor_en.pdf, including the projection of canopy cover toward the target of 40%, and confirmation of adequate soil volumes to support any proposed trees.
- b. The Landscape Plan must show the soil volumes and setback distances between proposed and existing trees to buildings and underground structures to ensure that both the above and below-ground space proposed is sufficient for tree planting in the Right of Way and other landscaped areas.
- c. The Official Plan section 4.8.2, sub 3 provides the following direction related to tree planting related to site plans:
 - i. Preserve and provide space for mature, healthy trees on private and public property, including the provision of adequate volumes of high-quality soil as recommended by a Landscape Architect;



- ii. On urban properties subject to site plan control or community planning permits, development shall create tree planting areas within the site and in the adjacent boulevard, as applicable, that meet the soil volume requirements in any applicable City standards or best management practices or in accordance with the recommendation of a Landscape Architect
- d. It is a Best Management Practice to plant one tree for every 5 parking spaces to help address the urban heat island effect created by paved areas, and also to work toward the Official Plan target of 40% canopy cover.
- e. Consider increasing the size of the landscape buffers and/or parking lot islands to create plantable spaces with sufficient soil volumes.

Feel free to contact Nancy Young (nancy,young@ottawa.ca), Planning Forester, for follow-up questions.

Parkland

Comments:

- 24. The amount of parkland dedication that is required is to be calculated as per the City of Ottawa Parkland Dedication By-law No 2022-280. For commercial and Industrial development, parkland dedication is required to be provided at the rate of 2% the gross land area.
- 25. Parks & Facilities Planning is requesting **Cash in Lieu** of for this proposal. The value of the property will be determined by market appraisal approved by the City prior to planning approval for the site plan.
- 26. Please provide the City with a surveyor's area certificate/memo which specifies the exact gross land area of the property parcel being developed.
- 27. If parkland dedication for the parcel has been satisfied previously, please provide Parks & Facilities Planning with the supporting documentation.
- 28. Please note that the park comments are preliminary and will be finalized (and subject to change) upon receipt of the development application and the requested supporting documentation. Additionally, if the proposed residential product or land use changes, then the parkland dedication requirement be reevaluated accordingly.

Feel free to contact Anissa McAlpine (anissa.mcalpine@ottawa.ca), Parks Planner, for follow-up questions.



<u>Other</u>

- 29. The High-Performance Development Standard (HPDS) is a collection of voluntary and required standards that raise the performance of new building projects to achieve sustainable and resilient design. The HPDS was passed by Council on April 13, 2022.
 - a. At this time, the HPDS is not in effect and Council has referred the 2023 HPDS Update Report back to staff with direction to bring forward an updated report to Committee with recommendations for revised phasing timelines, resource requirements and associated amendments to the Site Plan Control By-law by no later than Q1 2024.
 - b. Please refer to the HPDS information attached and ottawa.ca/HPDS for more information.

Should there be any questions, please do not hesitate to contact myself or the contact identified for the above areas / disciplines.

Yours Truly, Colette Gorni, Planner II (DR West)

c.c. Nishant Dave, Planner I (DR West)
Kadri Nader, Urban Design
Abibatou Dieme, Infrastructure Project Manager
Mike Giampa, Transportation Project Manager
Nancy Young, Planning Forester
Mark Elliot, Environmental Planner
Anissa McAlpine, Parks Planner
Elizabeth King, Planner I (DRAW)



APPLICANT'S STUDY AND PLAN IDENTIFICATION LIST

Proposed Site Plan Control Application – 370 Huntmar Drive – PC2024-0304

Legend: **R** = Required, the study or plan is required with application submission

A = Advised, the study or plan is advised to evaluate the application or satisfy a condition of approval/draft approval

1 - OPA, 2 - ZBA, 3 - Plan of Subdivision, 4 - Plan of Condominium, 5 - SPC

Core studies required for certain applications all the time (Remaining studies are site specific)

For information and guidance on preparing required studies and plans refer here:

R	٨	Study/ Plan Name	Description		Wh	en Requi	red		Applicable Study Components	
n	Α	Study/ Flail Name	Description	1	2	3	4	5	& Other Comments	
		1. Environmental Site	Ensures development only takes place on sites where the	\boxtimes	\boxtimes	\boxtimes	\boxtimes	\boxtimes	Record of Site Condition	
		Assessment (Phase 1 & Phase 2)	environmental conditions are suitable for the proposed use	Study Tr All cases	rigger Deta s	ails:			Yes □ No ⊠	
			Geotechnical design	\boxtimes	\boxtimes	\boxtimes	\boxtimes	\boxtimes		
		2. Geotechnical Study	requirements for the subsurface conditions	Study Tr All cases	rigger Deta s	ails:				
		3. Grading and	Grading relationships between connecting (or abutting)			\boxtimes		\boxtimes		
		Drainage Plan	properties and surface runoff control	Study Tr All cases	rigger Deta	ails:				
			A scientific study or evaluation			\boxtimes	\boxtimes	\boxtimes	Reasonable Use Study	
		4. Hydrogeological and Terrain Analysis	that includes a description of the ground and surface hydrology, geology, terrain, affected landform and its susceptibility	Study Trigger Details: When developing on private services or who urban development is in close proximity to existing private serviced development					Yes □ No □ Groundwater Impact Study Yes □ No □	
			Detential impacts of naise on a				\boxtimes	\boxtimes	· Vibration Study	
		5. Noise Control Study	Potential impacts of noise on a development	Study Trigger Details: See Terms of Reference for full details.					Yes □ No □	

				\boxtimes	\boxtimes	\boxtimes		
	6. Rail Proximity Study	Development on land adjacent to all Protected Transportation Corridors and facilities shown on Schedule C2 of the Official Plan, to follow rail safety and risk mitigation best practices	Within the existing a corridors on land a Transport	igger Deta le Develop and future s, as show adjacent to rtation Col dule C2 of	ment Zor rapid trar n on Anne all Prote rridors and	nsit station ex 2 of the cted d facilities	s and OP OR	Rail Safety Report Yes □ No □ O-Train Network Proximity Study Yes □ No □
				\boxtimes	\boxtimes	\boxtimes	\boxtimes	Fluvial Geomorphological Report Yes □ No ⊠
	7. Site Servicing Study	Provides servicing details based on proposed scale of development with an engineering overview taking into consideration surrounding developments and connections.	Study Tr All cases	igger Deta	ails:			Assessment of Adequacy of Public Services Yes No C Servicing Options Report Yes No S Erosion and Sediment Control Plan / Brief Yes No C Hydraulic Water Main Analysis Yes No C Stormwater Management Report and Detailed Design Brief Yes No C
		Assessment of slope stability and		\boxtimes	\boxtimes	\boxtimes	\boxtimes	
	8. Slope Stability Study	measures to provide safe set- back.		igger Deta ne potentia		ard Lands	exists	Retrogressive Landslide Analysis Yes □ No □
				\boxtimes	\boxtimes	\boxtimes	\boxtimes	
	9. Transportation Impact Assessment	Identify on and off-site measures to align a development with City transportation objectives.	Study Trigger Details: If the development generates 60 person-trips or more; or if the development is located in a Location Trigger; or if the development has a Safety Trigger.					Roadway Modification Functional Design Yes No

				\boxtimes	\boxtimes	\boxtimes	\boxtimes		
	10. Water Budget Assessment	Identify impact of land use changes on the hydrologic cycle and post-development mitigation targets.	May be application and / or sensitive required assessm	Study Trigger Details: May be required for site plan control applications for sites with private servicing and / or proximity to hydrogeologically-sensitive areas. Draft plans of subdivision are equired to integrate water budget assessments into supporting stormwater management plans and analysis for the study area.					
	11. Wellhead Protection Study	Delineate a Wellhead Protection Area (WHPA) and characterize vulnerability for new communal residential drinking water well systems, in accordance with Technical Rules under Clean	Required drinking municipa (small w Respons	igger Deta d for all ne water well al wells, ne ater works sibility Agre	ails: w commu I systems; ew private s) that requeement (N	nal reside including communa uire a Mur IRA), exp	ential new al wells nicipal ansions		
		Water Act.	municipa	nunicipal wells, new private communal wells small water works) that require a Municipal Responsibility Agreement (MRA), expansions or increased water takings from an existing municipal well or existing private communal well and new private communal wells.					

R	Α	Study/Plan Name	Description		Wh	en Requi	red	_	Applicable Study Components
n	^	Study/Flail Name	Description	1	2	3	4	5	& Other Comments
			Confirm or recommend		rigger Deta	ails:	ment are	D Or	
		12. Agrology and Soil Capability Study	alterations to mapping of agricultural lands in the City.	identifica through is demoi	ation of a r a comprel nstrated th	new settle hensive re nat the lan for an Agr	ment area eview; or v d does no	a where it ot meet	
				\boxtimes	\boxtimes	\boxtimes	\boxtimes	\boxtimes	
		13. Archaeological Assessment	Discover any archaeological resources on site, evaluate cultural heritage value and conservation strategies	When the archaeo archaeo Archaeo Study in outside of any archaeo	logical site logical site logical Redicates are the hister chaeolog	ails: s either: a e; or the p es; or whe esource Po chaeologi oric core; ical resou e City's his	otential to re the Cit otential M cal potent or upon d rce during	y's apping tial, liscovery	
				\boxtimes	\boxtimes			\boxtimes	
\boxtimes		14. Building Elevations	Visual of proposed development to understand facing of building including direction of sunlight, height, doors, and windows.	Site Plar more res buildings the units High-per threshold Official F necessa policies,	sidential us with less are within formance d in the ruplan or Zory to dete	dential bui nits; or for s than 25 r n the Urba Developr ral area. ning By-la rmine con	residenti esidentia an area or ment Stan aw: if staff apliance v	al I units, if the dard deem it vith OP	

				\boxtimes	\boxtimes		\boxtimes	
	15. Heritage Impact Assessment	Determine impacts of proposed development on cultural heritage resources.	Where of the Onta adjacen 30 metro for any of Canal U	rigger Det developme ario Herita t to, acros es of a pro developme NESCO V oed buffer	ent or an a ge Act is p s the stree stected he ent adjace Vorld Heri	oroposed et from or ritage proent to the f	on, within perty; or Rideau	Conservation Plan Yes □ No □
				\boxtimes	\boxtimes	\boxtimes	\boxtimes	
	16. Heritage Act Acknowledgement Report	A submission requirement to demonstrate that the <i>Ontario Heritage Act</i> requirements have been satisfied, to ensure that multiple applications are considered currently.	Where t Heritage submit a (designa Heritage to demo	rigger Det he subject e Register a Heritage ated herita e Register lish or ren ted proper	t property and the a Permit Ap ge proper or provide nove a bu	pplicant noplication ty listed of le notice	nust on the of intent n-	Heritage Permit Application Yes □ No □ Notice of Intent to Demolish Yes □ No □
		Mineral aggregate extraction activities; and to protect	×	\boxtimes	\boxtimes	\boxtimes	\boxtimes	
	17. Impact Assessment Study – Mineral Aggregate	known high quality mineral aggregate resources from development and activities that would preclude or hinder their existence (ability to be extracted) or expansion.	New De within the metres of	rigger Det velopmen e Bedrock of lands w ee Area O	t within 50 c Overlay ithin the S	, or within	300	
		To identify or confirm known mineral deposits or petroleum		\boxtimes	\boxtimes	\boxtimes	\boxtimes	
	18. Impact Assessment Study – Mining Hazards	resources and significant areas of mineral potential. To protect mineral and petroleum resources from development and activities which would preclude or hinder the establishment of new operations or access to the resources.		rigger Det pplication ns.		nity to mir	ning	

		To identify or confirm known	\boxtimes	\boxtimes		\boxtimes	\boxtimes		
	19. Impact Assessment Study – Waste Disposal Sites / Former Landfill Sites	proximity of existing or former waste disposal sites. To ensure issues of public health, public safety and environmental impact are addressed.	aste disposal sites. De ensure issues of public ealth, public safety and environmental impact are addressed. Study Trigger Details: For the establishment of any new Solid Waste Disposal Site or for a footprint expansion of an operating Solid Waste Disposal Site; or development within three kilometers of an operating or non-operating Waste Disposal Site.						
			\boxtimes	\boxtimes	\boxtimes	\boxtimes	\boxtimes		
	20. <mark>Landscape Plan</mark>	A plan to demonstrate how the canopy cover, urban design, health, and climate change objectives of Official Plan will be met through tree planting and other site design elements.	Site Plai Condom it is dem compon review of A high-le be requi	ninium: alv constrated ent of a profession of the applaced evel concestred to sup	Subdivision vays requining that the land the la	red, exce andscape of relevan dscape P ng By-law	pt where t to the lan may and		
				\boxtimes					
	21. Mature Neighbourhood Streetscape Character Analysis	In the Mature Neighbourhoods a Streetscape Character Analysis is required to determine the applicable zoning requirements.	Study Trigger Details: Zoning By-law amendment application in areas covered by the Mature Neighbourhoods zoning overlay for applications of residential development of four storeys or less located in a R1, R2, R3, or R4 zone.						
		Provincial land use planning			\boxtimes	\boxtimes			
	22. Minimum Distance Separation	tool that determines setback distances between livestock barns, manure storages or anaerobic digesters and surrounding land uses, with the objective of minimizing land use conflicts and nuisance complaints related to odour.		rigger Det ions in the	<u>ails</u> : e Rural Ard	ea, outsid	e of a		

		A tool to assess the			\boxtimes			
	23. Parking Plan	sufficiency of on-street parking in plans of subdivision.		igger Deta or revised reets.		subdivisio	n with	
		A Plan of Survey depicts legal boundaries and is a	\boxtimes	\boxtimes	\boxtimes	\boxtimes	\boxtimes	
\boxtimes	24. Plan of Survey	specialized map of a parcel of land and it delineates boundary locations, building locations, physical features and other items of spatial importance. Study Trigger Details: Required for all Planning Act applications.						
				\boxtimes	\boxtimes			
	25. Plan of Subdivision	Proposed subdivision layout to be used for application approval	Study Trigger Details: Always required with the submission of plan of subdivision application.					
		арріоча	Amendn	uired with nent applic nse to ena	cation, wh	ere such 2	ZBLA is	
		Proposed condominium				\boxtimes		
	26. Plan of Condominium	layout to be used for application approval		igger Deta submissio on.		of condor	ninium	
		Provides the planning	\boxtimes	\boxtimes	\boxtimes			
	27. Planning Rationale	justification in support of the <i>Planning Act</i> application and to assist staff and the public in the review of the proposal.	Study Trigger Details: For all Official Plan amendment, Zoning Bylaw amendment, or plan of subdivision applications.					Integrated Environmental Review Summary Yes □ No □
		A checklist that shows a			\boxtimes		\boxtimes	
	28. Preliminary Construction Management Plan	development proposal's anticipated impacts to all modes of transportation and all elements in the right of way during construction.	Study Trigger Details: For all Site Plan and plan of subdivision applications.				on	

			\boxtimes	\boxtimes	\boxtimes	\boxtimes	\boxtimes	
	29. Public Consultation Strategy	Proposal to reach and collect public input as part of development application.	Official F Amendm required Condom Site Plar lead in c	rigger Deta Plan Amer nent and S inium: Va in: At the d onsultatio al Support	ndment, Zo Gubdivision cant Land iscretion on with the	n: Always only of the City Business	's file s and	
	30. Shadow Analysis	A visual model of how the proposed development will cast its shadow.	When th massing commerce to the massing commerce to the massing commerce to the massing commerce to the massing commeters). Storeys of in height proximity shadow the massing commeters to the massing commeters to the massing commeters to the massing commeters to the massing commence to the mass	igger Deta ere is an i proposed cial or office gers: the Gree ment is over le a devel or less, but and/or may to a shad analysis not de the Gree ment is over and is in oft e area. When ment is not sensitive a ment) the is over 5	ncrease in I for a resince use. Inbelt: proper 5 store opment proper is proporassing an adow sensing an adow sensing the store store a proper a pr	posed ys in heig roposal is sing an in d is in clo tive area, quested. roposed ys in heig imity to a posed proximity industrial a shadov	ht (≤15 5 crease se a ht (≤9 shadow to a	
	31. Site Plan	A Site Plan is a visual drawing that illustrates the proposed development of a site in two dimensions.	Site Plar	igger Deta		⊠ layout of	⊠ the	Site Plan Yes ⊠ No □ Concept Plan Yes □ No □

			densities provides sites pro with mul more bu and/or a sites with (such as vehicula sites whadjacent	ealm, build s or massi s changes posing mu tiple lando ildings, or new publ h propose s active tra r circulatio ere the de t propertie e integrate	ng of the part to the plan ultiple land owners; site park ic or privard changes ansportation or acceptelopments may be	oroposal nned confiduses; sit dedication te street(s to conner networks to tranut potential impacted	Facility Fit Plan Yes □ No □	
	32. Urban Design Brief	Illustrate how a development proposal represents high-quality and context sensitive design that implements policies of the Official Plan, relevant secondary plans, and Council approved plans and guidelines.	For all C law ame applicati For SPC residenti residenti residenti Urban ai Develop area who	rigger Deta Difficial Plane endment, a cons. Capplication ial building ial units, o ial building ial units, if rea or the ment Star ere OP Po dential an	n amendment of the property of the units of	sals for or more osals for s than 25 are within ormance shold in th (3) is relev	the ne rural vant; for	
	33. Urban Design Review Panel Report	Demonstrates that a development proposal has attended an Urban Design Review Panel formal review meeting, received, and responded to the associated recommendations, if applicable	Required subject t	rigger Deta d for all pla to UDRP r RP Panel T	anning act	accordano	ce with	
	34. Wind Analysis	A visual model and a written evaluation of how a proposed development will impact pedestrian-level wind conditions.	Application and/or model building(rigger Deta ions seeki nassing wl (s), 10 sto that is mo	ng an incr nich is eith reys or mo	ner: a tall ore or a pi	roposed	

			five store	existing to existing to exist in height or planned aces, water areas.	ght and is d low rise	o ent,		
		The purpose of the Zoning Confirmation Report (ZCR) is		\boxtimes			\boxtimes	
\boxtimes	35. Zoning Confirmation Report	to identify all zoning compliance issues, if any, at the outset of a planning application.		igger Deta d for all SF				

R	٨	Study / Blan Nama	Description		Wh	en Requi	red		Applicable Study Components	
n	Α	Study / Plan Name	Description	1	2	3	4	5	& Other Comments	
			Includes a community energy analysis, alongside							
		36. Community Energy Plan	mitigation measures, and other associated information. The community energy analysis refers to the overall assessment process to identify on and off-site measures to align the design of the development with City climate objectives.	itigation measures, and her associated formation. The community nergy analysis refers to the verall assessment process identify on and off-site easures to align the esign of the development						
			The Energy Modeling							
		37. Energy Modelling Report	Report is a Site Plan Control application submission requirement to show how climate change mitigation, and energy objectives will be met through exterior building design elements.	NOT I	MPLEMEI	NTED & N	IOT REQI	JIRED		
			Assessment of environmental impacts of a	\boxtimes	\boxtimes	\boxtimes		\boxtimes	Assessment of Landform Features	
		38. Environmental Impact Study	project and documents the existing natural features, identifies the potential environmental impacts,	Is require	rigger Deta ed when on is propos	levelopme			Yes □ No □ Integrated Environmental Review Yes □ No □	

		recommends ways to avoid and reduce the negative impacts, and proposes ways to enhance natural features and functions.	designate the City' hazardo The EIS Environre provides features EIS is re	d distance ted lands, s Natural I us forest to Decision mental Imparant and adjace quired to sons under	natural he Heritage S ypes for w Tool (Approact Study st of the nate ent areas support de	eritage fea System, or vildland fir endix 2 of Guidelina atural her within whevelopme	f the es) itage nich an	Protocol for Wildlife Protection during Construction Yes □ No □ Significant Woodlands Guidelines for Identification, Evaluation, and Impact Assessment Yes □ No □
	39. Environmental Management Plan	A comprehensive environmental planning document that identifies, evaluates, and mitigates the potential impacts of proposed development on the natural environment and its ecological functions at local planning stage.	Official If (area-sp where: t condition based; t planned subdivis impact c subdivis applicab	rigger Deta Plan amen pecific police here is signs upon where are pointrastruct ion that we note infrastruct ion within ale Class E I has expir	dments for secondificant chair the or roposed could have a structure the EMP structure the EMP structure.	ndary pla nange in the riginal stuchanges to ed to serve a signification needs of study area	n, he ldy was cice a ant another a, or the	
	40. High-performance Development Standard	A collection of voluntary and required standards that raise performance of new building projects to achieve sustainable and resilient design	NOT I	MPLEME	□ □ NTED & N	OT REQ	UIRED	
\boxtimes	41. Tree Conservation Report	Demonstrates how tree cover will be retained and protected on the site, including mature trees, stands of trees, and hedgerows.	Where to diamete is a tree Root Zo	rigger Deta here is a tr r or greate on an adja ne (CRZ) of ment site.	ree of 10 c or on the si acent site	ite and/or that has a	if there	

Appendix B

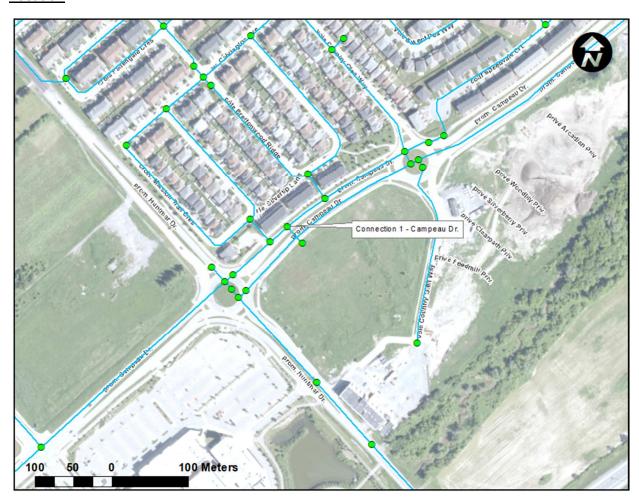
- Watermain Boundary Conditions
- Water Demand Calculations
- FUS Calculations
- Water Model Results

Boundary Conditions 370 Huntmar Drive

Provided Information

Scenario	De	mand
Scenario	L/min	L/s
Average Daily Demand	2	0.03
Maximum Daily Demand	2	0.04
Peak Hour	4	0.07
Fire Flow Demand #1	5,000	83.33
Fire Flow Demand #2	6,000	100.00

Location



Results

Connection Option 1 - Campeau Dr.

Demand Scenario	Head (m)	Pressure ¹ (psi)
Maximum HGL	160.7	88.8
Peak Hour	156.5	82.8
Max Day plus Fire Flow #1	155.4	81.2
Max Day plus Fire Flow #2	154.6	80.1

¹ Ground Elevation = 127.5 m

Notes

- 1. As per the Ontario Building Code in areas that may be occupied, the static pressure at any fixture shall not exceed 552 kPa (80 psi.) Pressure control measures to be considered are as follows, in order of preference:
 - If possible, systems to be designed to residual pressures of 345 to 552 kPa (50 to 80 psi) in all occupied areas outside of the public right-of-way without special pressure control equipment.
 - Pressure reducing valves to be installed immediately downstream of the isolation valve in the home/ building, located downstream of the meter so it is owner maintained.
- 2. Demands for proposed Connection 1 at existing stub off Campeau Drive were assigned to upstream junction at Campeau Drive off the public looped watermains. The engineer must calculate headloss off the dead-end main.

Disclaimer

The boundary condition information is based on current operation of the city water distribution system. The computer model simulation is based on the best information available at the time. The operation of the water distribution system can change on a regular basis, resulting in a variation in boundary conditions. The physical properties of watermains deteriorate over time, as such must be assumed in the absence of actual field test data. The variation in physical watermain properties can therefore alter the results of the computer model simulation. Fire Flow analysis is a reflection of available flow in the watermain; there may be additional restrictions that occur between the watermain and the hydrant that the model cannot take into account.

ARCADIS ARCADIS IBI GROUP

500-333 Preston Street

arcadis.com

IBI GROUP

Ottawa, Ontario K1S 5N4 Canada

WATERMAIN DEMAND CALCULATION SHEET

Arcadia Commercial Site | Minto 147391 -6.0 | Rev#0 | 2024-11-13 Prepared By: MP | Checked By: RM

		RESID	ENTIAL		NON	-RESIDENTIAL	(ICI)	AVERAG	E DAILY DEM	AND (I/s)	MAXIMU	JM DAILY DEM	AND (I/s)	MAXIMUM	HOURLY DE	MAND (I/s)	FIRE
NODE	Towns	Medium Density		POPULATION	INDUST. (ha)	COMM. (ha)	INSTIT. (ha)	RESIDENTIAL	ICI	TOTAL	RESIDENTIAL	ICI	TOTAL	RESIDENTIAL	ICI	TOTAL	DEMAND (I/min)
<u>Arcadia</u>						0.090			0.03	0.03		0.04	0.04		0.07	0.07	5,000
<u>TOTAL</u>						0.09				0.03			0.04			0.07	

			ASS	UMPTIONS		
POPULATION DENSITY		WATER DEMAND RATES		PEAKING FACTORS FOR POP. OF	F 501 TO 3000	FIRE DEMANDS
Townhouse	2.7 persons/unit	Residential	280 l/cap/day	Maximum Daily		Single Family 10,000 l/min (166.7 l/s)
				Residential	2.5 x avg. day	
Medium Density (Stacks)	1.8 persons/unit			Commercial	1.5 x avg. day	Semi Detached
		Commercial Shopping Center	2,500 L/(1000m2)/day	Maximum Hourly		& Townhouse 12,000 I/min (200.0 I/s)
				Residential	2.2 x max. day	
				Commercial	1.8 x max. day	Medium Density 15,000 I/min (250.0 I/s)



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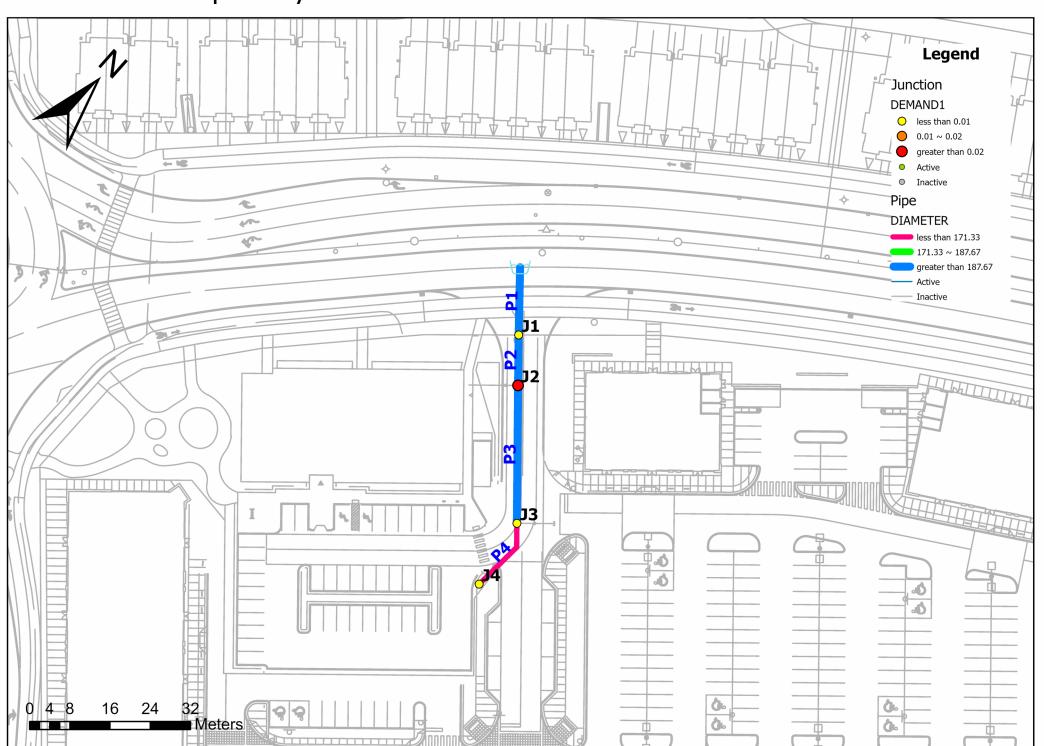
FIRE UNDERWRITERS SURVEY

Arcadia Commercial Site | Minto 147391-6.0 | Rev #0 | 2024-11-13 Prepared By: MP | Checked By: RM

STEP	Contents	Description		Adjustment Fa	actor	Resu	ılt
1	Floor Area Total Storey Total Effective Floor Area	Arcadia Commercial Site				997 2 1994	m2 storey m2
2	Type of Construction	Type V Wood Frame Type III Ordinary Construction Type II Noncombustible Construction Type I Fire Resistive Construction	1.5 1.0 0.8 0.6	Noncombustible Construction	0.8		
3	Required Fire Flow	RFF = 220C√A				8000	L/min
4	Occupancy and Contents	Noncombustible Contents Limited Combustible Contents Combustible Contents Free Burning Contents Rapid Burning Contents	-25% -15% 0% 15% 25%	Limited Combustible Contents	-15%	-1200	L/min
	Fire Flow					6800	L/min
5	Automatic Sprinkler Protection	Automatic Sprinkler Conforming to NFPA 13 Standard Water Supply for both the system and Fire Department Hose Lines Fully Supervised System	-30% -10% -10%	Yes No No	-30%	-2040	L/min L/min
	Fire Flow		<u>u</u>			-2040	L/min
	Exposure Adjustment	Based on Table 6 Exposure Adjustement Ch	narges for	Subject Building			
0	East (Future)	Separation (m) Length X Height Factor (m.storeys) Construction Type	24.07 20 Type II	Without unprotected opening	0%	0	L/min
6	South-West (Future)	Separation (m) Length X Height Factor (m.storeys) Construction Type	10.6 64 Type II	Without unprotected opening	6%	408	L/min
	Fire Flow	<u>'</u>	۷.			408	L/min
7	Total Baguirad Fire Flaw					5168	
1	Total Required Fire Flow	Rounded to Nearest 1000 L/min				5000	L/min

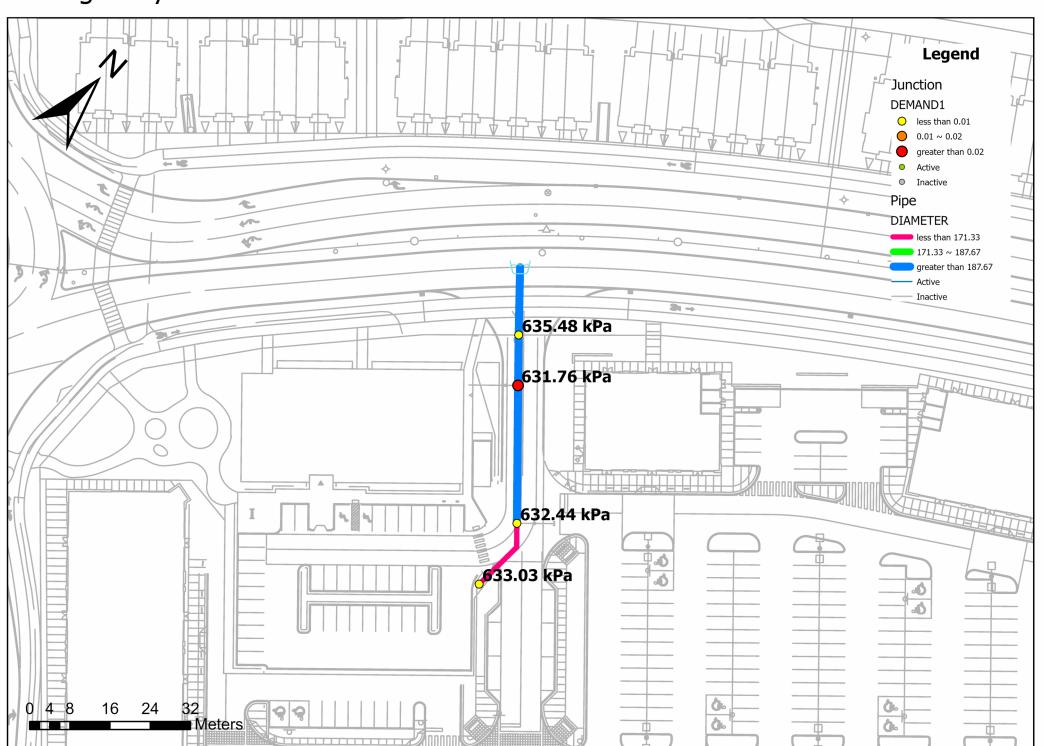
Notes 1. Fire flow calculation are based on Fire Underwriters Survey version 2020.

Junctions and Pipes Layout



Date Printed: 2024-11-13 9:46 AM

Average Day Pressures



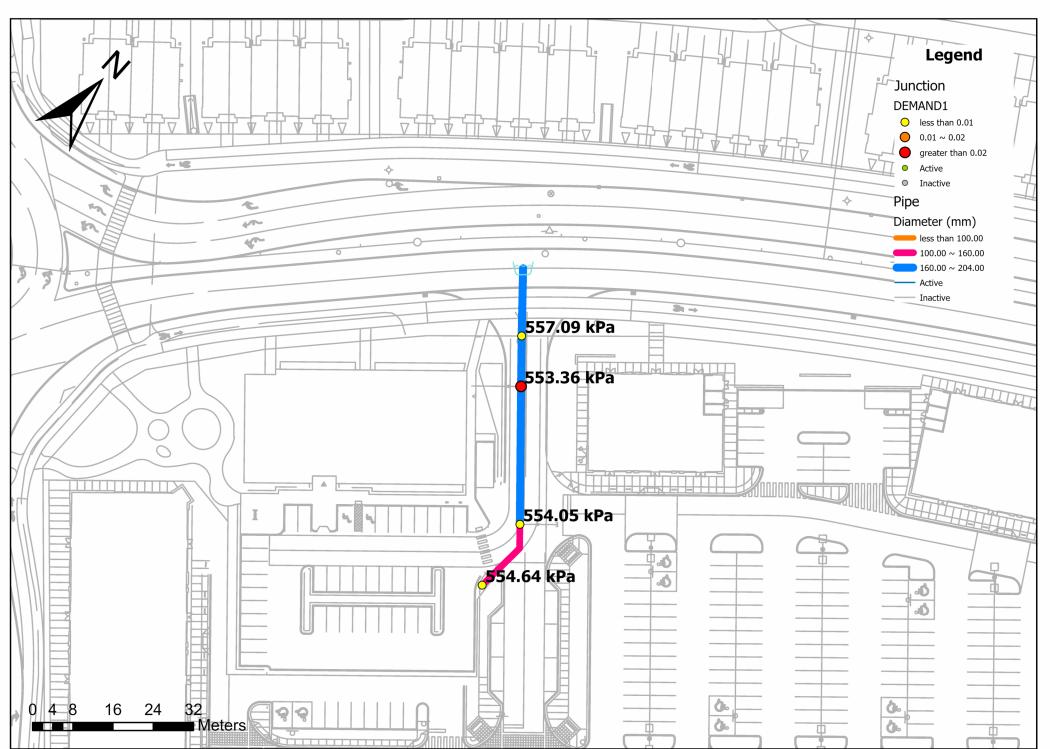
Date Printed: 2024-11-13 9:50 AM

Average Day Pressures

	ID	Demand (L/s)	Elevation (m)	Head (m)	Pressure (kPa)
1	J1	0.00	98.25	160.70	611.96
2	J2	0.03	98.63	160.70	608.24
3	J3	0.00	98.56	160.70	608.92
4	J4	0.00	98.50	160.70	609.51

Date: Wednesday, November 13, 2024, Time: 09:45:14, Page 1

Peak Hour Pressures



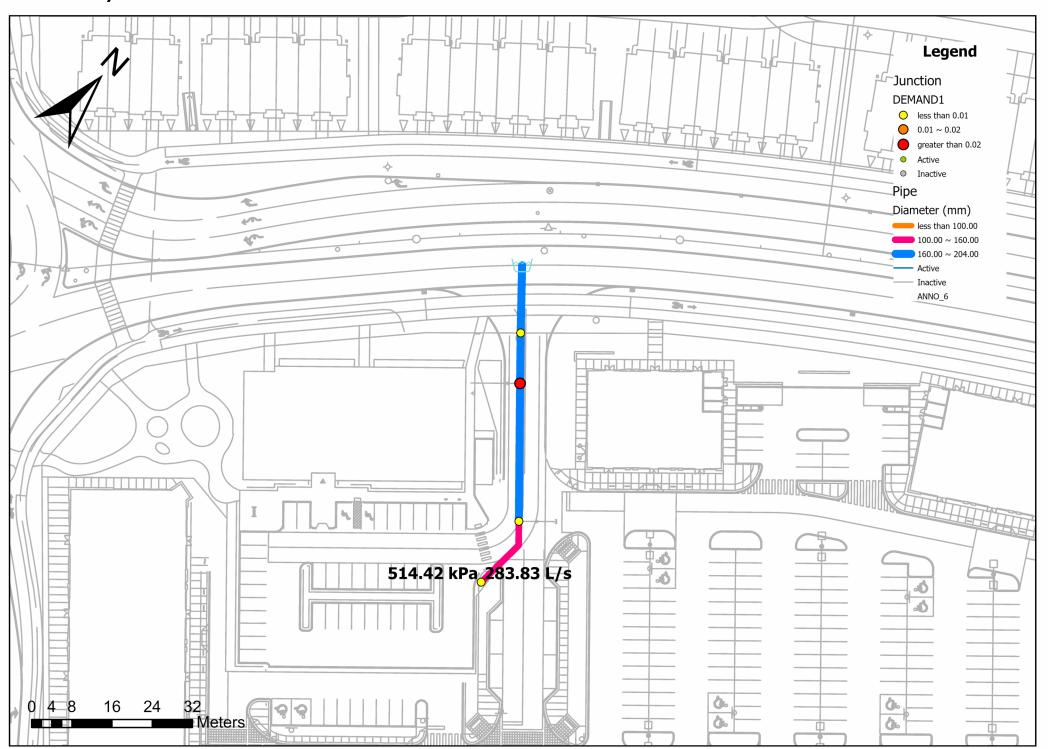
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Peak Hour Pressures

	ID	Demand (L/s)	Elevation (m)	Head (m)	Pressure (kPa)
1	J1	0.00	98.25	155.10	557.09
2	J2	0.07	98.63	155.10	553.36
3	J3	0.00	98.56	155.10	554.05
4	J4	0.00	98.50	155.10	554.64

Date: Wednesday, November 13, 2024, Time: 09:51:55, Page 1

Max Day + Fire Flow



Date Printed: 2025-02-26 2:58 PM

Max Day + Fire Flow

	ID	Static Demand (L/s)	Static Pressure (kPa)	Static Head (m)	Fire-Flow Demand (L/s)	Residual Pressure (kPa)	Hydrant Available Flow (L/s)	Hydrant Pressure at Available Flow (kPa)
1	J4	0.00	557.58	155.40	83.33	514.42	283.83	140.0

Appendix C

- Sanitary Sewer Design Sheet
- Sanitary Drainage Area Plan 147391-C-400
- Sanitary Sewer Design Sheet 35355
- Sanitary Drainage Area Plan 35355-C-501
- Sanitary Sewer Design Sheet Kanata West Servicibility Study

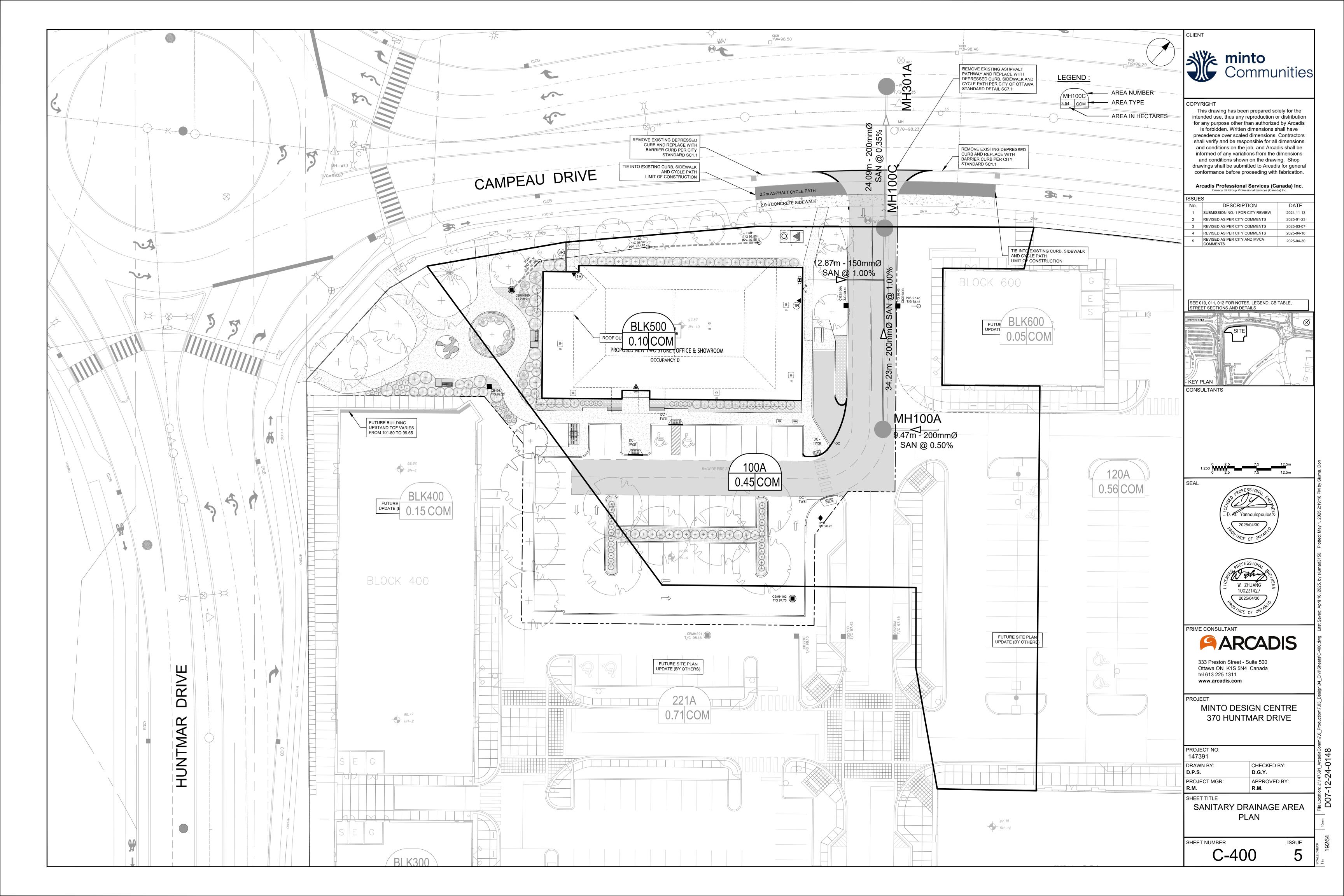
SANITARY SEWER DESIGN SHEET



ARCADIS 400-333 Preston Street 400-333 Preston Street
Ottawa, Ontario K1S 5N4 Canada tel 613 225 1311 fax 613 225 9868 arcadis.com

147391 - Arcadia Commercial Site CITY OF OTTAWA Minto Communities

							RES	DENTIAL								ICI A	REAS			INFIL1	TRATION ALL	OWANCE			TOTAL			PROPO	SED SEWER	DESIGN		
	LOCATION			AREA		UNIT 1	TYPES	AREA	POPUI	LATION	RES	PEAK			ARE	A (Ha)		ICI	PEAK	ARE	EA (Ha)	FLOW	FIXED	LOW (L/s)	FLOW	CAPACITY	LENGTH	DIA	SLOPE	VELOCITY	AVAI	ILABLE
STREET	AREA ID	FROM	TO	w/ Units	SF	TUOD	APT OTHE		i inib	01114	PEAK	FLOW	INSTIT	JTIONAL	COMM	ERCIAL	INDUSTRIAL	PEAK	FLOW	IND	O. Inc	(1, 1-)	INID	01114	41.4-3	(1.1-)	()	()	(0/)	(full)	CAP	PACITY
SIREEI	AREA ID	МН	МН	(Ha)	51	TH/SD	API OTHE	(Ha)	IND	CUM	FACTOR	(L/s)	IND	CUM	IND	CUM	IND CUM	FACTOR	(L/s)	IND	CUM	(L/s)	IND	CUM	(L/s)	(L/s)	(m)	(mm)	(%)	(m/s)	L/s	(%)
Arcadia Commerci	al Site																															+
SITE PLAN		CAP	MH100A						0.0	0.0	3.80	0.00		0.00	1.24	1.24	0.00	1.50	0.60	1.24	1.24	0.41		0.00	1.01	24.19	9.47	200	0.50	0.746	22.10	95.82%
SITE FLAIN			WITTOUA						0.0	0.0	3.60	0.00		0.00	1.24	1.24	0.00	1.50	0.00	1.24	1.24	0.41		0.00	1.01	24.19	9.41	200	0.50	0.740	23.10	93.82%
	BLK500	BLDG SVC	SEWER						0.0	0.0	3.80	0.00		0.00	0.10	1.34	0.00	1.50	0.65	0.10	1.34	0.44		0.00	1.09	19.46	12.87	150	1.50	1.067	18.37	94.38%
		MH100A	MH100C						0.0	0.0	3.80	0.00		0.00	0.45	1.79	0.00	1.50	0.87	0.45	1.79	0.59		0.00	1.46	34.22	34.23	200	1.00	1.055	32.76	95.73%
																												200				
																																+
																																-
																																+
Design Parameters:				Notes: 1. Mannings		(m) =	0.013				Designed:					No.					Cubasissi	Revision on No. 1 for Cit	. Devieus							Date 2024-11-13		
Residential		ICI Areas		Demand (280 L/day	20	00 L/day							2						on No. 2 for Cit								2025-01-23		
SF 3.4 p/p/u				3. Infiltration			0.33 L/s/Ha				Checked:																					
TH/SD 2.7 p/p/u APT 1.8 p/p/u		3,000 L/Ha/day 3,000 L/Ha/day		4. Residentia			14/(4+(P/1000)^0.5))0).8																								
	IND 35	5,000 L/Ha/day	MOE Chart		where K =	0.8 Correctio	n Factor				Dwg. Refer	rence:	147391-40	0																		
Other 60 p/p/Ha	1	7000 L/Ha/day				tutional Peak 20%. otherwise	Factors based on tot e 1.0	al area,									ile Reference: 47391-6.04.04						Date: 2024-11-							Sheet No: 1 of 1		

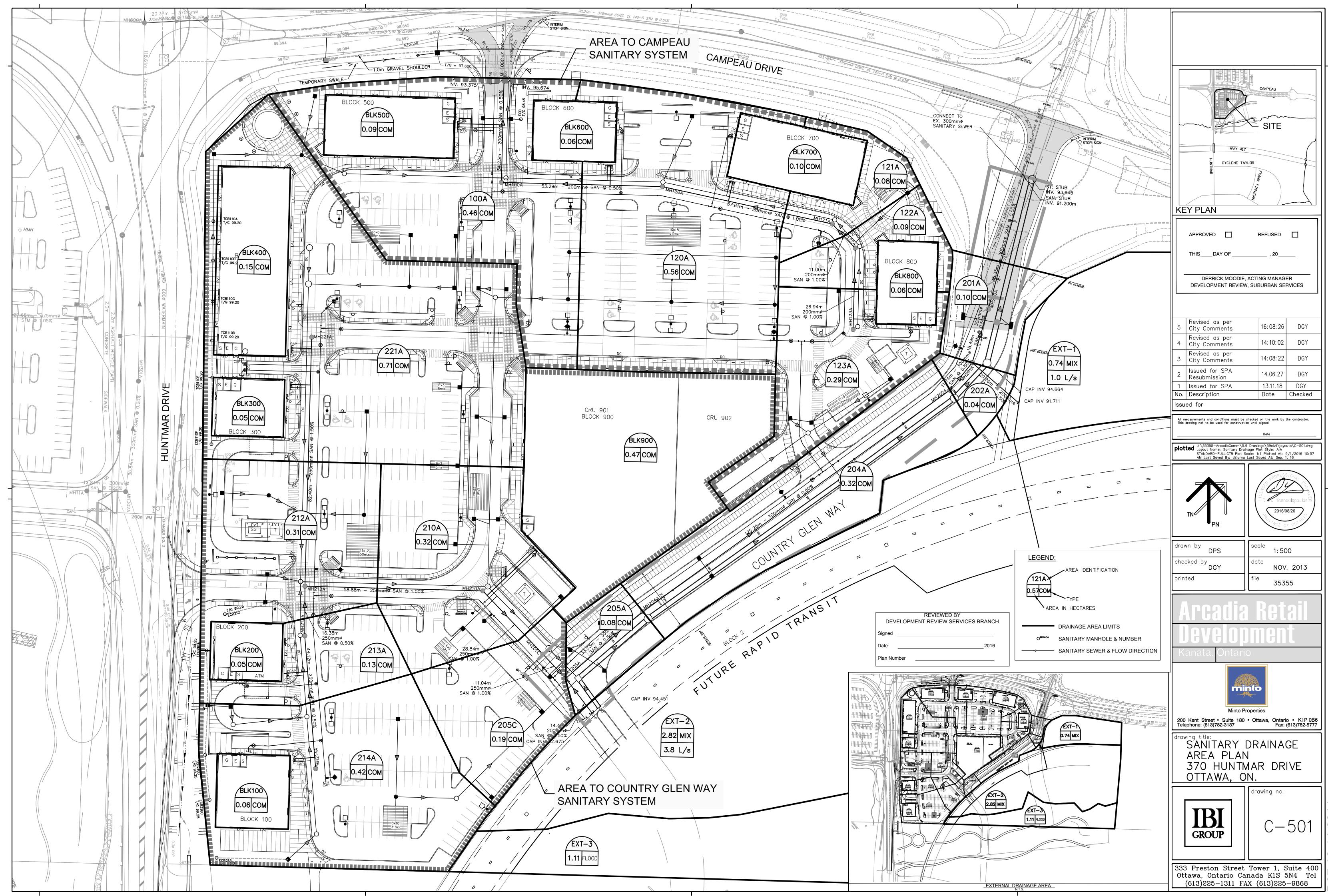




SANITARY SEWER DESIGN SHEET

PROJECT: NAME OF PROJECT **LOCATION:** CITY OF OTTAWA **CLIENT:** NAME OF CLIENT

								RESIDENTIA	4L							ICI AREAS			INFILT	RATION ALLO	DWANCE	TOTAL				PROPOSED S	SEWER DESIGN			
	LOCATION		ŀ		UNIT TY	YPES		AREA		ILATION	PEAK	PEAK			AREA			PEAK	AREA		FLOW	FLOW	CAPACITY	LENGTH	DIA	SLOPE	VELOCITY	VELOCITY	AVA	ILABLE
		FROM	то								FACTOR	FLOW	INSTITUTION	VAL	COMM	<u> </u>	INDUSTRIAL	FLOW			–	()					(full)	(actual)		ACITY
STREET	AREA ID	МН	МН	SF	SD	TH	APT	(Ha)	IND	CUM		(L/s)		CUM	IND	CUM	IND CUM	(L/s)	IND	CUM	(L/s)	(L/s)	(L/s)	(m)	(mm)	(%)	(m/s)	(m/s)	L/s	(%)
	DIKOOO	DI KOOOA	DAAIN						0.0	0.0	4.00	0.00		0.00	0.00	0.00	0.00	0.05	0.00	0.00	0.02	0.07	45.00	6.50	150	1.00	0.074		45.02	00.57
	BLK800	BLK800A	MAIN					-	0.0	0.0	4.00	0.00		0.00	0.06	0.06	0.00	0.05	0.06	0.06	0.02	0.07	15.89	6.50	150	1.00	0.871	+	15.82	99.57
	123A	MH123A	MH122A					1	0.0	0.0	4.00	0.00		0.00	0.29	0.35	0.00	0.30	0.29	0.35	0.10	0.40	34.22	26.94	200	1.00	1.055		33.81	98.83
	122A	MH122A	MH121A						0.0	0.0	4.00	0.00		0.00	0.09	0.44	0.00	0.38	0.09	0.44	0.12	0.51	34.22	11.00	200	1.00	1.055		33.71	98.52
	DI KZ00	D1 1/700 A	DAAIN						0.0	0.0	4.00	0.00		0.00	0.10	0.10	0.00	0.00	0.10	0.10	0.02	0.11	45.00	6.50	150	1.00	0.074		45.77	00.20
	BLK700	BLK700A	MAIN						0.0	0.0	4.00	0.00		0.00	0.10	0.10	0.00	0.09	0.10	0.10	0.03	0.11	15.89	6.50	150	1.00	0.871	+	15.77	99.28
	121A	MH121A	MH120A						0.0	0.0	4.00	0.00		0.00	0.08	0.62	0.00	0.54	0.08	0.62	0.17	0.71	34.22	57.61	200	1.00	1.055		33.50	97.92
	BLK600	BLK600A	MAIN					-	0.0	0.0	4.00	0.00	1	0.00	0.06	0.06	0.00	0.05	0.06	0.06	0.02	0.07	15.89	6.50	150	1.00	0.871		15.82	99.57
	120A	MH120A	MH100A						0.0	0.0	4.00	0.00		0.00	0.56	1.24	0.00	1.08	0.56	1.24	0.35	1.42	24.19	53.29	200	0.50	0.746		22.77	94.12
		-																												
	BLK500	BLK500A	MAIN						0.0	0.0	4.00	0.00		0.00	0.09	0.09	0.00	0.08	0.09	0.09	0.03	0.10	15.89	15.00	150	1.00	0.871		15.78	99.35
	100A	MH100A	MH100C						0.0	0.0	4.00	0.00		0.00	0.46	1.79	0.00	1.55	0.46	1.79	0.50	2.06	24.19	34.23	200	0.50	0.746		22.14	91.51
	1000	MH100C	EXMH301A						0.0	0.0	4.00	0.00		0.00	0.00	1.79	0.00	1.55	0.00	1.79	0.50	2.06	24.19	23.50	200	0.50	0.746	 	22.14	91.51
	DLKAOO	DI KAOOA	DAAIN						0.0	0.0	4.00	0.00		0.00	0.45	0.45	0.00	0.12	0.45	0.45	0.04	0.47	45.00	6.50	150	1.00	0.074		45.72	
	BLK400 BLK300	BLK400A BLK300A	MAIN MAIN						0.0	0.0	4.00	0.00		0.00 0.00	0.15 0.05	0.15 0.05	0.00	0.13	0.15 0.05	0.15 0.05	0.04	0.17 0.06	15.89 15.89	6.50 6.50	150 150	1.00	0.871 0.871		15.72 15.83	98.92 99.64
	DENGOO	BERGOOA	WAIN						0.0	1 0.0	4.00	0.00		0.00	0.03	0.03	0.00	0.04	0.03	0.03	0.01	0.00	13.03	0.50	130	1.00	0.071		13.03	33.0
	221A	MH221A	MH212A						0.0	0.0	4.00	0.00		0.00	0.71	0.91	0.00	0.79	0.71	0.91	0.25	1.04	75.98	82.40	250	1.50	1.500	0.522	74.94	98.63
	DI 1/4 00	DI K100A	DAAIN						0.0	0.0	4.00	0.00		0.00	0.00	0.00	0.00	0.05	0.00	0.00	0.03	0.07	15.00	C 05	150	1.00	0.074		45.02	00.5
	BLK100 BLK200	BLK100A BLK200A	MAIN MAIN						0.0	0.0	4.00	0.00		0.00 0.00	0.06 0.05	0.06 0.05	0.00	0.05	0.06 0.05	0.06 0.05	0.02	0.07 0.06	15.89 15.89	6.85 6.75	150 150	1.00 1.00	0.871 0.871		15.82 15.83	99.57 99.64
	DEIXEGO	BEIGEORY	in the							1 0.0	1.00	0.00		0.00	0.05	0.03	0.00	0.01	0.03	0.05	1 0.01	0.00	15.05	0.75	150	1.00	0.072		15.55	33.0
	214A	MH214A	MH213A						0.0	0.0	4.00	0.00		0.00	0.42	0.53	0.00	0.46	0.42	0.53	0.15	0.61	43.87	44.12	250	0.50	0.866	0.301	43.26	98.61
	213A	N/11212A	N411242A						0.0	0.0	4.00	0.00		0.00	0.12	0.66	0.00	0.57	0.12	0.66	0.19	0.76	42.07	16.20	250	0.50	0.866	0.335	42.11	98.27
	213A	MH213A	MH212A						0.0	0.0	4.00	0.00		0.00	0.13	0.66	0.00	0.57	0.13	0.66	0.18	0.76	43.87	16.38	250	0.50	0.800	0.325	43.11	98.27
	212A	MH212A	MH210A						0.0	0.0	4.00	0.00		0.00	0.31	1.88	0.00	1.63	0.31	1.88	0.53	2.16	62.04	58.88	250	1.00	1.224	0.551	59.88	96.52
	211/222	211/222														2.5						^	44.00	22.22	4=0		2 212		10.00	27.00
	BLK900	BLK900A	MAIN						0.0	0.0	4.00	0.00		0.00	0.47	0.47	0.00	0.41	0.47	0.47	0.13	0.54	11.23	22.08	150	0.50	0.616		10.69	95.20
	210A	MH210A	MH205C						0.0	0.0	4.00	0.00		0.00	0.32	2.67	0.00	2.32	0.32	2.67	0.75	3.07	62.04	28.84	250	1.00	1.224	0.633	58.97	95.06
		MH205C	MH205A						0.0	0.0	4.00	0.00		0.00	0.19	2.86	0.00	2.48	0.19	2.86	0.80	3.28	62.04	11.04	250	1.00	1.224	0.633	58.76	94.71
al Cauth minad	EVT 2	CTUD	B 41120E A						0.0	0.0	4.00	0.00		0.00		0.00	0.00	2.04	2.02	2.02	0.70	2.00	24.40	44.54	200	0.50	0.746		20.20	04.20
nal South mixed	EXT 2	STUB	MH205A						0.0	0.0	4.00	0.00	'	0.00		0.00	0.00	3.01	2.82	2.82	0.79	3.80	24.19	14.51	200	0.50	0.746		20.39	84.29
ry Glen Way	205A	MH205A	MH204A						0.0	0.0	4.00	0.00		0.00	0.08	2.94	0.00	5.56	0.08	5.76	1.61	7.18	71.33	33.73	300	0.50	0.978	0.620	64.16	89.94
ry Glen Way	204A	MH204A	MH202A						0.0	0.0	4.00	0.00		0.00	0.32	3.26	0.00	5.84	0.32	6.08	1.70	7.54	71.33	125.25	300	0.50	0.978	0.628	63.79	89.43
ry Glen Way	202A	MH202A	MH201A					+	0.0	0.0	4.00	0.00		0.00	0.04	3.30	0.00	5.87	0.04	6.12	1.71	7.59	71.33	11.74	300	0.50	0.978	0.633	63.75	89.36
nal East Mix	EXT-1	Stub	MH201A						0.0	0.0	4.00	0.00		0.00		0.00	0.00	0.79	0.74	0.74	0.21	1.00	24.19	20.27	200	0.50	0.746		23.19	95.87
																														_
ry Glen Way	201A 200A	MH201A MH200A	MH200A EX CAP						0.0	0.0	4.00	0.00		0.00	0.10	3.40 3.40	0.00	6.75	0.10 0.00	6.96 6.96	1.95	8.70 8.70	71.33 58.82	18.49 45.35	300 300	0.50 0.34	0.978 0.806	0.659 0.630	62.63 50.12	87.80 85.20
try Glen Way eau Dr	ZUUA	EX CAP	EX CAP EXMH303A						0.0	0.0	4.00	0.00		0.00	0.00	3.40	0.00 0.00	6.75	0.00	6.96	1.95 1.95	8.70 <i>8.70</i>	58.82 58.82	20.50	300	0.34	0.806	0.630	50.12	85.20 85.20
- '														- -																
n Parameters:				Notes:		<u> </u>					Designed:		RM			No.				Revisio								ate		
Residential		ICI Areas		 Mannings coef Demand (per c) =	20	0.013 50 L/day	200	J I /day						1.			Povis	Issued for ed as per City								3-11-15 1-06-24		-
3.4 p/p/u		ICI AI Ed3	Peak Factor	3. Infiltration allo				28 L/s/Ha		O L/day 4 L/s/Ha	Checked:		DY			3.				ed as per City								1-06-24 1-08-22		
5D 2.7 p/p/u	INST 50,00	0 L/Ha/day		4. Residential Pea		tor:	0.2		0	, 5, 110	J					4.				ed as per City								l-10-02		
T 1.8 p/p/u	COM 50,00	0 L/Ha/day	1.5	Harm	on Formu	nula = 1+(14/)												1										
er 60 p/p/Ha		0 L/Ha/day 0 L/Ha/day	MOE Chart	wher	e P = pop	pulation in th	housands				Dwg. Refer	rence:	12345-501				File Defense				Data							-1 NI -		
	1700	u I/Ha/day									1						File Reference:				Date:						She	et No:		



SANITARY SEWER DESIGN SHEET
PROJECT: Kanata West Servicibility Study
LOCATION: CITY OF OTTAWA

PAGE 1 OF 1

PROJECT: 3598-LD-03

DATE: April 2005

DESIGN: JiM

FILE: 3598LD.24wers.XLS

				19				MODEL 1 U	LTIMATE	(population	based crite	riaICI simi	dianeous p	eaking)		DO BARKIO	DEN COACEC			INFILTR	ATION		TOTAL		PROPOSED:	SEWER				*******	A OTHER		ACTUAL
	0015	10.11		TOTAL				SIDENTIAL					EMPLO	YMEN I/RE	TAILBUSINE	SS PARKIO	PEN SPACES PEAK FLOW			AREA (Ha)		PEAK	FLOW	CAPACITY	VELOCITY	LGTH.	PIPE	GRADE	AVAIL.	HARMON PF	a/Q	va/Vf	VELOCITY
	OCAT	ION		AREA	APPLIC	UNIT/Ha		POPULA	NOITA	PEAK		APPLIC	ACCUM	TOTAL	FLOW	INDIV	ACCUM	TOTAL	INDIV	CUMUL	TOTAL	FLOW		N4-176.5022.77.00	(full)	6-3	- Immiral		(%)	rr	-44		(m/s)
STREET	FROM	то		12	AREA	L 100000114 - LAS	UNITS	INDIV A	ACCUM	FACTOR	FLOW	AREA (Ha)	AREA (Ha)		(VHa/d)	(1/s)	(Vs)	(Vs)	MARKED .	14.00000.Hz	CUMUL	(lis)	(l/s)	Us	m/s	(m)	(mm)	%	(70)		_		- Arra-ay
314221	MH	MH		(Ha)	(Ha)						(1/5)	(rta)	Ariaj	hin	To record											-	-						
	*****							-				38.11	38.11		35000	23.16			38.1							-	-						
ampesu Drive Trude Sewer	1	2	Area 1 (PBP)	38.11								27,29			35000	16.58			27,2														
			Area 2 (PBP)	27.29					_			14.05			50000	12.20			14.0		90.38	25.31	86,73	283.79	1.27	525.0	525	0.40	69,44%		0.308	0,730	0.927
			Area 3 Ext Employment	14.05								10.93		90.38	50000	9.45	61.42	61.42	10.9			23.31	60,73	40000						3,85			
			Area 4 HP Employment	10.93	29.19	19	555	1664	1664	3,65	24.58			90.38				68,76	29.1			35,85	129,18	286.61	0.98	700.0	0 600	0.20	54.93%		0.451	0.830	0,815
	2	3	Area 5 Residential	29.19 8.45	29.15	19	222	1001	1391		24.58	8.45				7.3		68.76				35,65		- 513/15	26								0.757
			Area 9 Ext Employment	16.65		_						16.65			50000	14,4		19.21	16.6			6.20	25,41	148,74	0.91	910.	0 450	0.25			0.171	0.630	
	14	3	Area 6/8 Ext Employment	-5.48		1						5.48				4.7								392.29	1,00	6 300.	0 675			1.65		0.790	
			Area 7 HP Employment	-5,40				-	1664	3.65	- 24.58	0.00	0.00	120.9	5	0.0	0.00	67.7	27.8					148.74		750.				166		0.660	
	3		A to Besidential	27.86	27.80	19	529	1588	1588	3.66	23.55					- 17	1.44	89.4						392.29	1.00	6 450.	0 675	0.20	51.93%	3.38	0.481	0.840	0.692
	4A		Area 10 Residential	4.13	1.76				3515	3.38	48.17	2.37				1.4		3.9	6.3											200	0.507	0.940	0,762
	4	5	Area 13 Community Ratail	6.35	1							6.33				3.8 4.1		7.9			18.15	5.08	24.88	43.88	8.0	7 420.	0 250	0,50	43.31%	3.88		0.860	V,/02
	Queenswa	5	Area 13 Community Ferent	11.80	5.00	2 50	251	752	752			6.75		13.14		2.3		1,0	3.8									4.74	£1 4007	3,31	0,456	0.830	0.945
	-		Area 15 Community Retail	. 3.88	1			0	4267	3.31	57.19	3.88		1000	35000	15.5		115.2	25.5		229.71	64,32	236.77	519.43	1,1	4 300.	0 750	0.20	54.42%		0,430	0.030	0,840
	5	5A	Area 44	25.54	3						57.19	25,5	29.4	165.8	35000	13.3	17,00	115.2				64.32	236,77			-	-			3.23			
First Line Road Sewer			ALVA TT	229.71							57.19				-			113.2		1						-	_			173			
		CA.	Area 100 Residential	90.20	90.2	0 19	1714	5141	5141	3.2		0.00			8 50000	4.2	4 4.24	4.2	95.0	8 95.08	95.08	26,62				-	-	-					
Signature Ridge	-	5A 5A	Area 100 Non-Residential	4,88	- 2000					1.5	67.35	4,8	4.8	8 4.8	30000	4.2	*124	7,2					65.00						21.100	200	0.689	0.940	1.197
Signature Ridge		5A	Area 100 (101/Acquisition									10000000	-	-	-		-	119.5			324.79	90.94	399.98	580.53	. 1.2	7 30.	0 750	0.25	31.10%	2.98	0.689	0.940	1.157
Intersticial Lands & Broughton/Richardson				324.79	154.02	2	3136		9409		124.54	170.77					-	ALJ.O.	-	-			1										-
Total To SRPS	5A	SRPS		- Davis	29,111	_													_	-													
				-	_	_										40.0	1 49.51		57.0	3 57.03											-		
			Ares 32 (PBP)	57.03		1						57.0			50000	49.5			8.3											-			
Palladium Drive Trunk Sewer	6	7	Area 32 (FOF)	8.34								8,3			2 50000			- 97.1				2			1 2				49 101	3.53	0.423	0,810	1.000
	_	-	Area 33/34 Ext Employment	54.85								54.8										2 43.94			1.2	3 925	.0 675	0.27	57.69%	3.53		0.010	1.000
	-	-	Area 37 Mixed Use	36.70	15.6	0 50	780	2340	2340	3.5				0 141.3	2 30000	1.0-2	10.52	115.4			156.93	43.94	192.85	5					_	3.53			-
	1	8	ACC 37 MARCH COL	156.92	15.6		780		2340)	33.47				20000	3.1	5 3.15	- IIII	6.0														
		10	Area 35 HP Employment	6.05								6.0	5 6.0	5	30000	3.5	4-200					30.00				-		_					
Corel Centre Etc. (Existing Sewer) *	_	16	Area 36 (Corel Centre)									L	- 000	0 26.7	0 14400	5.0	8,19	8.1	9 20.	15 26.20	26.2	7.34	45.5	2		-	Relating	-					
	-	16	Area 38 Exten Employment	20.15								20.1			35000				14.	59 14.59				S.	1							$\overline{}$	
	15		Area 40 Employment	14:59								14.5			35000				11.5	97 26.56	5			1	1	1	1	1	1 1				
First Line Road Sewer	13	10	Area 41 Employment	11.97								11.9			35000				20.	66 47.22	2					00 525	5.0 525	0.2	69,89%	-	0.301	0.730	0.733
			Area 42 Employment	20.66								20.6							28.	89 76.11							0.0 600		The second second	3.53			
			Area 43 Employment	28.89				-	-							0.		54.4	4 0.	00 102.31							0.0 82			3.53			
Care Birms Touris	16	8	Nothing To Add	102.31	15.6		78		2346							0.		169.8	7 0.	00 139.01	259.2	3 109.9	305.9	579.9	1.0	05 530	1,U 82.	9,1	77.2270	1		-	
Carp River Trunk Carp River Trunk		10A	Nothing To Add	259.23	15.0	50	78	0	234	0	33,4	0.0	0.0	2737	-				1				1	10	-1		4	1		3.72			7
Carp River Trunk	·						0.00	2000	1999								1		23.		4			6 405.1		39 775	5.0 60	0 0.4	67.28%	3.03		0.740	1.027
Marle Grove Road Trunk Sewer	9	10	Area 18/19 Exist. Residential	23.34	23.		9 44		846	9 3.0	3 103.8	1	+	_					79.	32 102.60	6 102.6	6 28.7	4 132.5	403.1	1	110	- 00						A COLUMN
TOTAL CHOICE HOLD HOLD DAVID			Area 22/26/27 Residential	79.32	79.	32 3	0 238	0 7139	840	3,0	103.0	1-	_									_	-							3.20		/	
									564	4 3.3	73.0	6					P		99.			_	-	-									
Hazeldean/Huntmar Trunk Sewer	11	12	Area 16/20 Residential	99,01	99.	01 1	9 188	1 5644	304	4 3.,	75.0	33.5	50 33.5	50 33.	50000	29.	08 29.01	29.				-	-	-	_								
- The state of the			Area 16/20 Commercial	33,50			-		_	-		14.							14.			8 42.0	2 146.2	6 554.8	2 1.	50 775	5.0 67	5 0.4	0 73,64%		0.264	0.700	0 1.051
g -			Area 16/20 Open Space	14.13 %	*	+	-	-	-	-	73.0	-0		94 36.						44 150.0	-	44.0	170.0	1									
			Area 17 Ex. Commercial	3,44	-		-	-	_		1	10.		89 10.	89 50000	9.				.89 10.8 .63 17.5		-					336						
	12	10	Area 21 Exist. Employment	10.89	-	ć1 ·	9 12	16 378									9,4		_	61 35.1		-	1	1							-		0.00
			Area 19A Exist Residential	6.63	- 0.	63	- 12	370	1			17.				10.	70 20.1:	51.		.10 62.2		59.4	5 214.4	9 519.4	3 1.	14 95	0.0 75	0 0.2	0 58.71%	3.03	0.413	0.800	0.91
			Area 23/24 Community Retail	27.10	27.	10	81	3 2435	846	50 3.	03 103.7	2 0.		00 65,						.13	-								1				4 46
	-		Area 28/30 Residential	21.13		98	100	19 134				12.	15 12.	15 77.	59 35000	7	38 7.31	58.		.00 36.1	3 351.1	0 98,3	1 368.5	669.8	9 1.	21 100	0.0 82	5 0.2	0 44.98%	2.66	0,550	0.87	1.05
Marie Grove Road Trunk Sewer	10	10A	Area 39 Mixed Use	15.00			10 4			27 2.	66 211.5				**		10 17.1			.24			1				200				0.000	0.00	0 0.74
	-		Area 29 Residential	20.24	_							20.	24 20.	24 20.	24 35000	0 12	30 12.3	12.		.72 58.9	6 58.5	16.5	76.6	320.1		10 100				3.35	0.239		
Garp River Trunk Sewer	13	10A	Area 25 Community Retail Area 31 residential	38.72		.72	30 116	62 348	5 348	85 3.	39 47.8			-	25 50000	0	65 0.6			.75 0.7			0.5	36.6	9 3 0.	.72 10	0.0 25	0.3	5 97.65%		0.023	0.34	0,24
	-	177	Area 31 A (PBP)	0.75			1					0,	75 0.	75 0.	75 50000	-	9.0	1						- 2			_					\vdash	-
20	-	10A	Vice 31 V (191)	0.13										_		-		241.5	(3		670.0	4 224.9	5 759.2	9 1273.7	1 1.	43 30	0.0 105	0 0.2	0 40.39%	2,55	0.598	0.90	0 1.283
# ************************************	-	-		670:04	4 313.	70	848	4	2545	1	292.8	2 356.3	14					241.3	70	-			-										
Pumping Station 2 to KWPS	104	KWP	5	0.70:04	313.	70	U-10	-	1												+									2.4			
Section 1						1	_1					527				1		1		1								Ort 14					

| Verage Daily Per capita Flow Rate = 350 Vcap/d | Vcap/d

rccl/IBI

Revision No. 1: April 01; 2005 Revision No. 6: Oct. 14, 2005 Revision No. 7: Nov. 10, 2005
Revision No. 8: Nov. 11, 2005
Revision No. 9: Apr. 19, 2006 Revision No. 2: April 11, 2005 Revision No. 3: April 21, 2005

Revision No. 4: June 07, 2005

Revision No. 5: August 10, 2005

FIG. 4.2-1

SANITARY SEWER DESIGN SHEET

PROJECT : Kanata West Servicibility Stury

LOCATION : CITY OF OTTAWA

PAGE 1 OF 1 PROJECT: 3588-LD-03 DATE: Apr 2005 DESIGN: JIM FILE: 3598LD,sewers.XLS

				TOTAL				SIDENTIA		RE RIDGE (- Option of		EMPLO	YMENT/RE	TAIL/BUSIN	ESS PARK/OF	PEN SPACES			INFILT	RATION		TOTAL		PROPOSED S				
	LOCA	TION			ADDITIO	UNIT/Ha		POPUL		PEAK	PEAK	APPLIC		TOTAL	FLOW		PEAK FLOW			AREA (Ha	1	PEAK	FLOW	CAPACITY	VELOCITY	LGTH.	PIPE	GRADE	AVAIL.
		1		AREA	AREA		UNITS			FACTOR		AREA	AREA	AREA	RATE	INDIV	ACCUM	TOTAL	INDIV	CUMUL	TOTAL	FLOW			(full)				CAP.
STREET	FROM	TO MH		(Ha)	(Ha)	-	UNITS	INDIV	ACCOM	PACION	(IIs)	(Ha)	(Ha)	(Ha)	(VHa/d)	(l/s)	(Vs)	(lis)			CUMUL	(l/s)	(lis)	1/s	mis	(m)	(mm)	%	(%)
				1	3				-	72																			
Campeau Drive Trunk Sower	1	2	Area 1 (PBP)	0.00								0,00			35000				0.00	0.00									
			Area 2 (PBP)	0.00	V							0.00			35000				0.00	0.00			1				-		
			Area 3 Ext Employment	0.00								0.00			50000		0.00		0.00	0.00		0.00	0.00	283.79	1.27	500.0	525	0.40	100,009
			Area 4 HP Employment	0,00								0.00	0.00	0,00	50000	0,00	0.00					. 0.00	0.00	203.17	1.27	300.0	323	0.40	100.00
	2	3	Area 5 Residential	29.19	29.19	9 19	555	1664	1664	3.65				0,00			171	0.00		29,19		8.17	32.75	286.61	0.98	700.0	600	0.20	88,579
			Area 9 Ext Employment	0,00							24.58				50000					0.00			-		0.70	700.0	000	0,20	80,37
	14	3	Area 5/8 Ext Employment	0.00								0.00			50000					0.00		0,00	0.00	148.74	0.91	920,0	450	0.25	100.009
			Area 7 HP Employment	0,00								0,00			50000					0.00		8.17	32.75						83,689
	3	4		J					1664				0.00	0.00		0.00	0.00	0.00	4115	0.00									7,769
	4A	4	Area 10 Residential	27,86	27.8	6 19	529	1588	1588										27.86	27,86		-		1					66.749
	4	5	14 Mixed Use	4.13	1.7	6 50	88	263	3515	3.38	48.17	2.37								4,13	61.18	17.13	00.74	200.67	0.90	000.0	730	0.20	00.747
Corel Centre Etc. (Existing Sewer)		15	Area 35 HP Employment	6,05								6.05	6.05		30000	3,15	3.15		6.05			22.00					-	\rightarrow	
			Area 36 (Corel Centre)																			30.00					Existing	\rightarrow	
			Area 38 Exten Employment	20.15								20.15						and the second second		26.20		7.34	45.52	1			Extrung		
First Line Road Sewer		15	Area 40 Employment	14.59				- S				14,59			35000				14.59	14.59							-		
2.00			Area 41 Employment	11.97								11.97			35000				11.97	26,56			ļ	-			-	\rightarrow	
			Area 42 Employment	20.66								20.66			35000				20.66	47.22		21.31	67,56	100.21	0.88	694.0	375	0.30	32.599
			Area 43 Employment	28.89								28.89	76.11	76.11	35000	17,55	46.25			76.11					*****				44.549
Totals South Of Queensway To SRPS	15	5A		102.31	0.0	0	0		0		0.0	102.31						54.44	- marine	Travale.	102.31	38,03	113,08	203.90	1,24	230.0	450	0.47	44,547
	Queensway	5	Area 13 Community Retail	6.35								6.35			35000	3.86			6.35	6.35		(2.72	137.96	203.90	1.24	420.0	450	0.47	32,349
			Area 11/12 Mixed Use	11.80	5.0	2 50	251	752	753	3.88	11.8	6.79	115.45	115,45	-	4.12		62.42		18.15		63.73	137.90	203,90	1.24	420.0	430	0.47	32,347
	- 5	5A	Area 15 Community Retail	3.88								3,88			35000				3.88	124,34			600.0	519.43	1.14	2000	750	200	55.569
			Area 44	25.54							59.9	25,54	144.87	268.20	35000	15.52	2 81.73	81.73	25.54	149.88	211.00		()		1.14	300.0	730	0.20	33,307
	1			149.88																		63.73	63.73					-	
Heritage Hills		9 A	Area 100 Residential	90.20	90.2	10 19	1714	5141	5141	3.23	67,3	0.00							90.20			1	00.0				1	\rightarrow	
Heritage Hills		\$A	Area 100 Non-Residential	4.88							67.3	4.88	4.88	4.88	50000	4.24	4 4.24	4.24	4,88	95,08	95.0	26.62	98.21	1		-	-	\rightarrow	
Broughton-Richardson / Interstitial		5A					1																		- 4.55		1 220		
Total To SRPS	5A	SRPS		306.14	154.0	3	3136		9409		127.33	152.12						85.97			306.14	115.72	394.02	625.68	1.37	THE RESIDENCE	ale constant	STATE OF THE PARTY	37.03%
TOTAL TO DICE D	JA	DIGID		230124	10410					-	OCOCAL III	December 1	ALCOHOL: USA	-	-					- 2 00 1.0						Revision	No. 1:	April 11, 200	5

Aversge Daily Per capits Flow Rate = 350 1/cap/d
Infiltration Allowance Flow Rate = 0.28 1/sec/Ha
Residential Peaking Factor = 1+(14/(4+(P^0.5))), P=Pop. in 1000's, Max of 4
Population density per unit = 3.00
P. F. For Employment/Retail/Business Park = 1.50
Mixed Uses Assumes: 15% Community Retail, 42.5% Business Park and 42.5% Residential

Note: Sewer from node 5 to SRPS is existing and is to be replaced.

Revision No. 1: April 11, 2005 Revision No. 2: April 20, 2005 Revision No. 3: June 07, 2005 Revision No. 4: Oct. 14, 2005 Revision No. 5: Feb. 15, 2006



FIG. 4.2-2

Appendix D

- Storm Sewer Design Sheet
- Storm Drainage Area Plan 147391-C-500, C-501, C-502
- Ponding Plan 147391-C-600
- Storm Water Management Calculations
- Orifice Sizing Calculations
- Overflow Depth Calculations
- Runoff Coefficient Calculations
- Stormtech Chamber Specifications
- Watts Adjustable Flow Control for Roof Drains
- Storm Sewer Design Sheet & SWM Design Summary 53533
- Storm Drainage Area Plan 53533-C-500

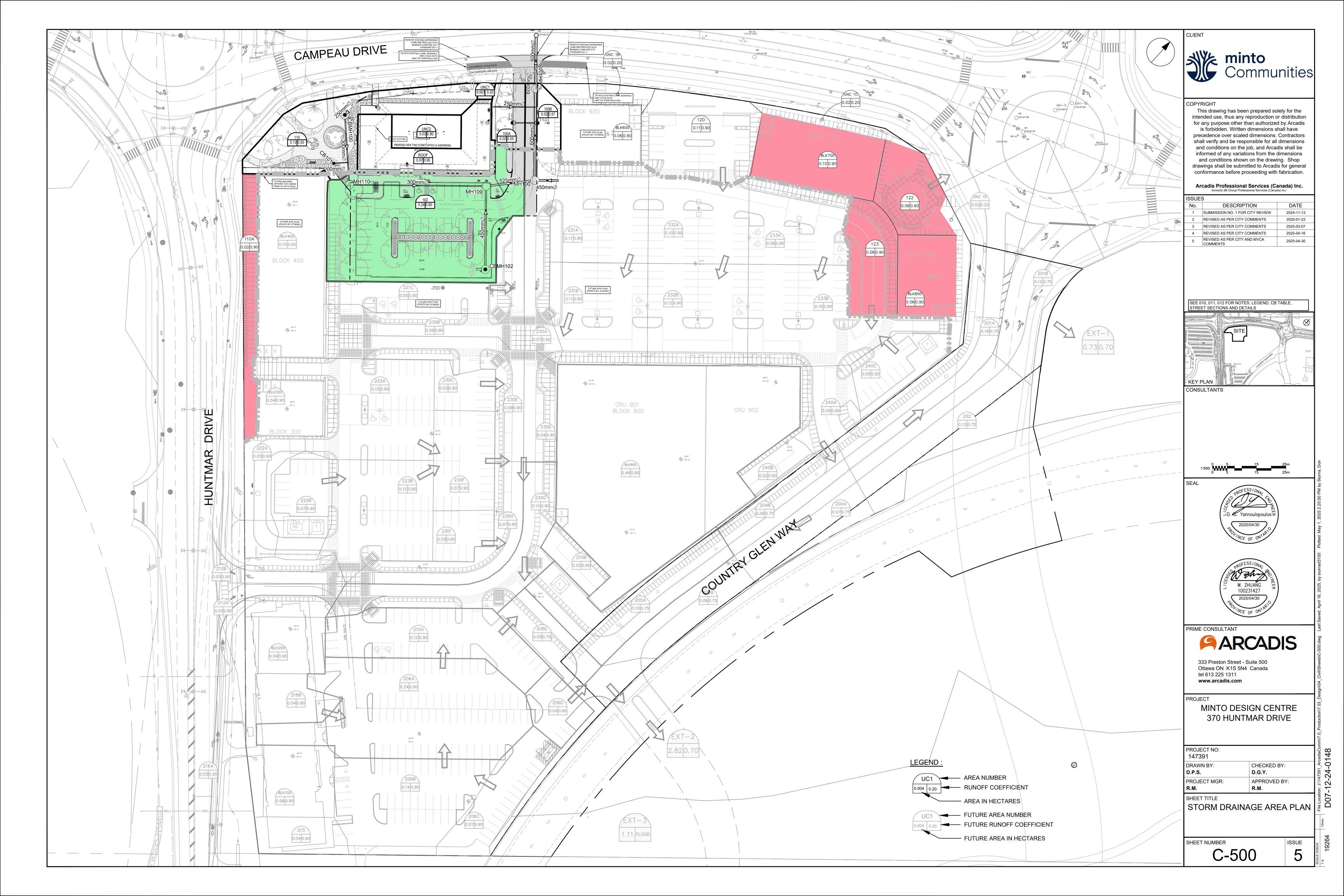
STORM SEWER DESIGN SHEET

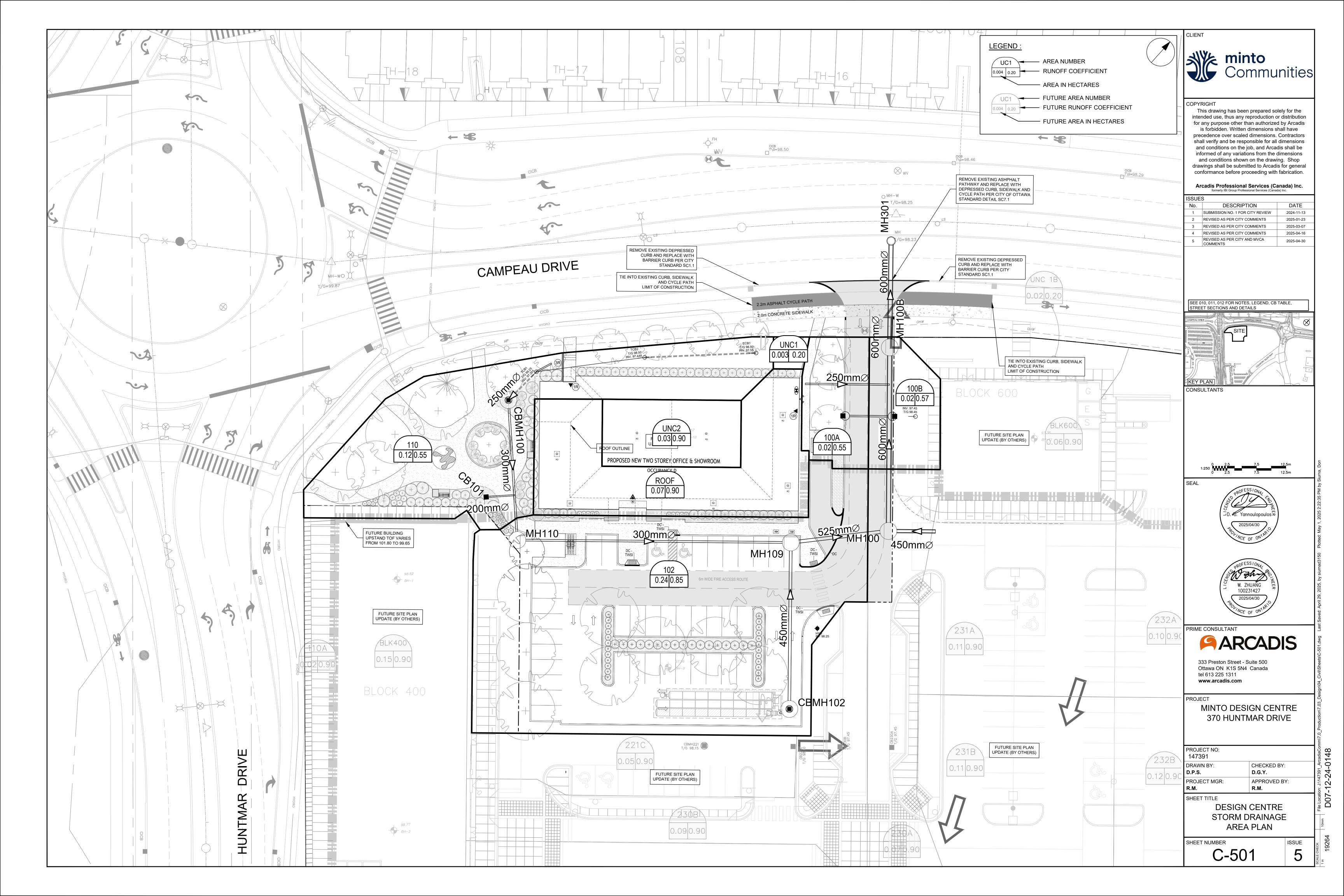
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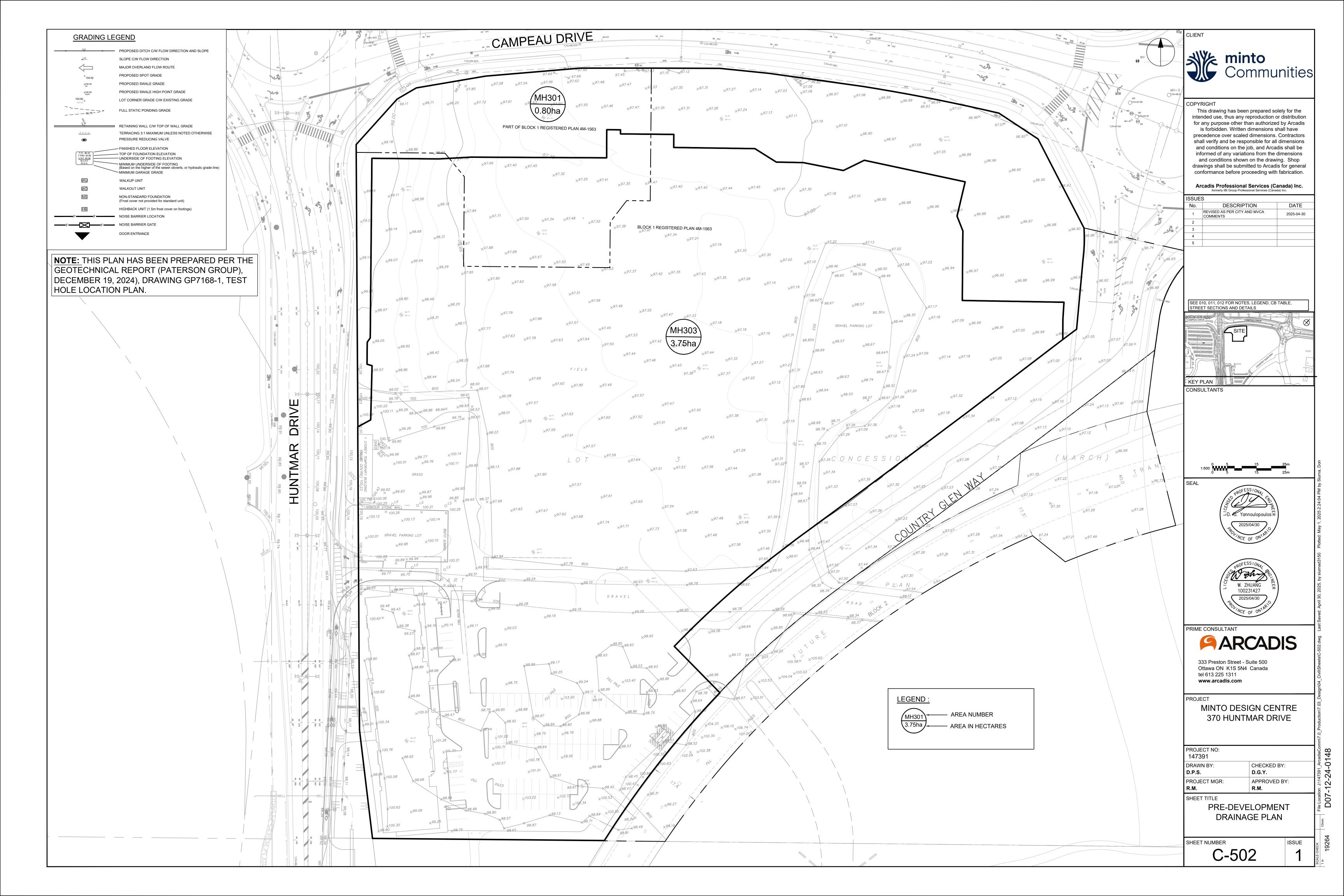
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Ottawa, Ontario k1S 5N4 Canada
tel 613 225 1311 fax 613 225 9868
arcadis.com

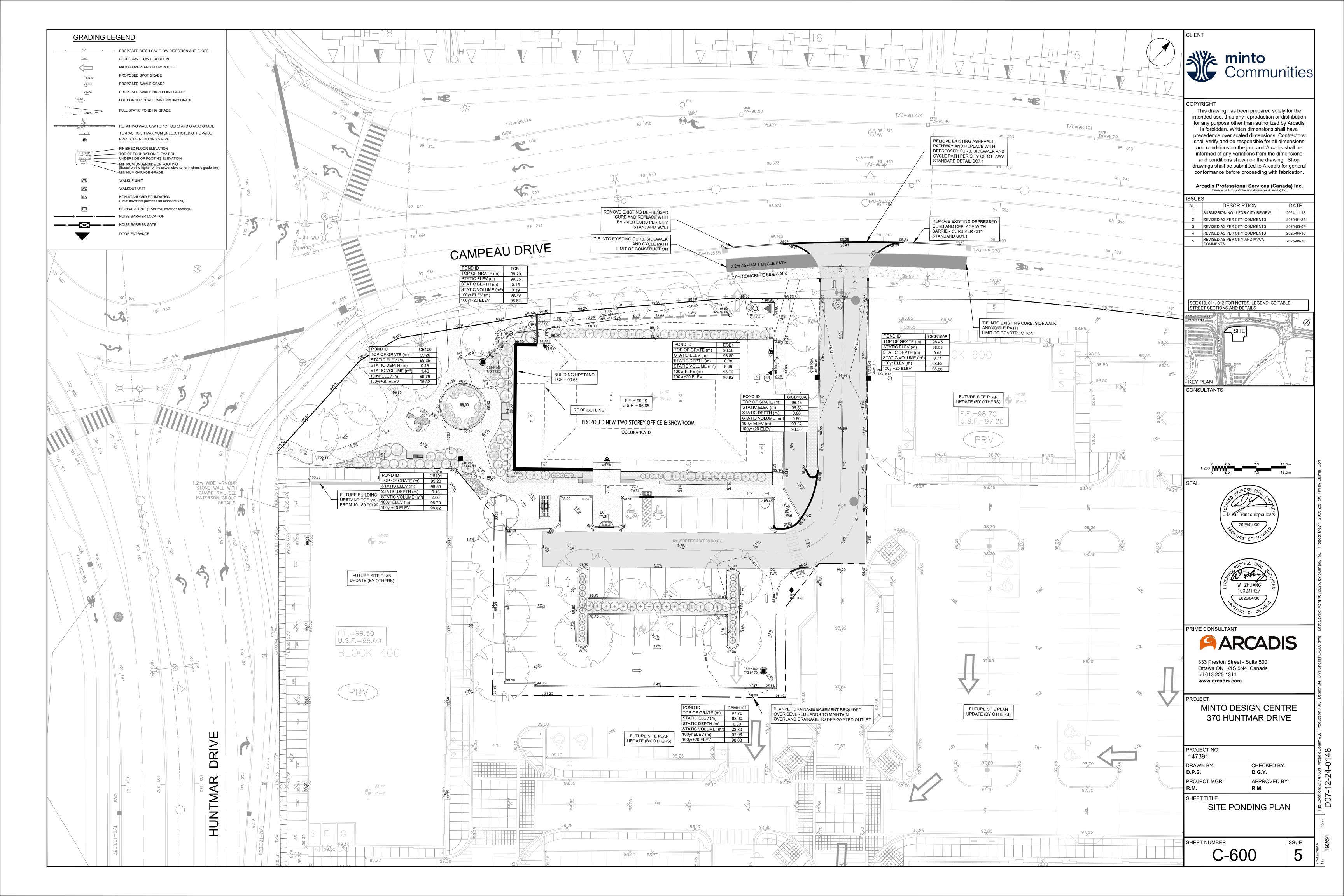
147391 - Arcadia Commercial Site CITY OF OTTAWA Minto Properties

LOCATION						AREA (H	la)										RATIO	NAL DESIG	N FLOW							SEWER DATA									
070557	DE 4 ID			C= C:	= C=	C=	C= (C= C=	C=	C=	C= INI	CUM	INLET	TIME	TOTAL	i (2)	i (5)	i (10)	i (100)	2yr PEAK	5yr PEAK	10yr PEAK	100yr PEAK	FIXED	FLOW	DESIGN	CAPACITY	LENGTH	F	PIPE SIZE (mn	n) S	LOPE VEI	LOCITY	AVAIL C	AP (2yr)
STREET AF	REA ID	FROM	то	0.20 0.2	25 0.40	0.50	0.55 0	.57 0.69	0.70	0.85	0.90 2.78	C 2.78AC	(min)	IN PIPE	(min)		(mm/hr)	(mm/hr)	(mm/hr)	FLOW (L/s	FLOW (L/s)	FLOW (L/s	FLOW (L/s)	IND	CUM	FLOW (L/s)	(L/s)	(m)	DIA	W	Н	(%)	(m/s)	(L/s)	(%)
Arcadia Commercial S	Site																																		
SITE PLAN	110	CBMH110					0.12					0.18		0.45	10.45	76.81					19.12	22.41	32.76	0.00	0.00	14.09	63.80	23.85	300				0.874		77.91%
		MH110	MH109								0.10 0.2	0.43	10.45	0.89	11.34	75.10	101.85	119.38	174.51	32.57	44.17	51.77	75.68	0.00	0.00	32.57	63.80	46.51	300			0.40	0.874	31.23	48.95%
		CBMH102	MH109							0.24	0.5	0.57	10.00	0.58	10.58	76.81	104.19	122.14	178.56	43.56	59.09	69.27	101.26	0.00	0.00	43.56	133.02	28.33	450			0.20	0.810	89.46	67.25%
	102	MH109	MH100								0.0	1.00	11.34	0.35	11.69	72.01	97.61	114.38	167.16	72.07	97.68	114.48	167.30	0.00	0.00	72.07	179.46	16.71	525			0.16	0.803	107.39	59.84%
		CAP	MH100							1	0.17 0.4	0.43	10.00	0.15	10.15	76.81	104.19	122.14	178.56	32.67	44.32	51.95	75.95	0.00	0.00	32.67	148.72	8.00	450			0.25	0.906	116.05	78.03%
		BLDG	SEWER								0.0	0.00	10.00	0.19	10.19	76.81	104.19	122.14	178.56	0.00	0.00	0.00	0.00	0.00	0.00	0.00	62.04	14.31	250			1.00 1	1.224	62.04	100.00%
		MH100	MH100B								0.0	1.43	11.69	0.61	12.30	70.88	96.05	112.55	164.47	101.08	136.98	160.51	234.56	0.00	0.00	101.08	248.09	31.23	600			0.15	0.850	147.00	59.25%
100.	0A, 100B	MH100B	EX CAP				0.02 0	.02			0.0	1.49	12.30	0.03	12.33	68.97	93.43	109.47	159.95	102.66	139.07	162.94	238.07	0.00	0.00	102.66	248.09	1.50	600			0.15	0.850	145.43	58.62%
																													600						<u> </u>
Definitions:				Notes:									Designed:						No.						Rev	ision							Date		
Q = 2.78CiA, where: Q = Peak Flow in Litres per Sec				1. Manning	s coefficie	nt (n) =	0.013												1						n No. 1 for (24-11-13 25-01-23		
A = Area in Hectares (Ha)	econa (L/S)												Checked:						3						n No. 2 for 0 n No. 3 for 0								25-03-07		
i = Rainfall intensity in millimeter [i = 732.951 / (TC+6.199)^0.8		(mm/hr) 2 YEAR											Oncorou.						4						n No. 4 for 0								25-04-16		
[i = 998.071 / (TC+6.053)^0.8	.814]	5 YEAR											Dwg. Refe	rence:	147391 - 5	500																			
[i = 1174.184 / (TC+6.014)^0 [i = 1735.688 / (TC+6.014)^0		10 YEAR 100 YEAR																			eference: 1-6.04.04					Date 2024-1							eet No: 1 of 1		











500-333 Preston Street Ottawa, Ontario K1S 5N4 Canada arcadis.com

STORMWATER MANAGEMENT

Arcadia Comm | Minto Properties 147391-6.0 | Rev #4R | 2025-04-25 Prepared By: MP | Checked By: RM/WZ

Formulas and Descriptions

 i_{2yr} = 1:2 year Intensity = 732.951 / $(T_c+6.199)^{0.810}$ i_{5yr} = 1:5 year Intensity = 998.071 / $(T_c+6.053)^{0.814}$

 i_{100yr} = 1:100 year Intensity = 1735.688 / $(T_c+6.014)^{0.820}$

T_c = Time of Concentration (min)

C = Average Runoff Coefficient

A = Area (Ha)

Q = Flow = 2.78CiA (L/s)

Maximum Allowable Release Rate

Restricted Flowrate

Per the previously completed SWM calculations for the overall commercial site development, the total flow to Outlet #2 (Ex. MH301) is calculated at 125.94 L/s.

Q _{restricted} =	125.94 L/s

Uncontrolled Release (Q uncontrolled = 2.78*C*i 100yr *A uncontrolled)

Q uncontrolled 1 =

for 100-yr storm event

Uncontrolled Roof Area UNC2

1.0

10 min

178.56 mm/hr 0.027 Ha

13.35 L/s

 $C_{100} =$

 $i_{100yr} =$

A uncontrolled =

 $Q_{uncontrolled 2} =$

 $T_c =$

Uncontrolled Area	UNC1, UNC1B	, UNC1C, UNC1D
-------------------	-------------	----------------

C ₁₀₀ =	0.25
$T_c =$	10 min
i _{100yr} =	178.56 mm/hr
A uncontrolled =	0.063 Ha

 $Q_{uncontrolled} = 21.17 \text{ L/s}$

Maximum Allowable Release Rate ($Q_{max allowable} = Q_{restricted} - Q_{uncontrolled}$)

Q _{max allowable}	=	104.77 L/s	

7.82 L/s

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STORMWATER MANAGEMENT

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MODIFIED RATIONAL METHOD (100-Year, 5-Year & 2-Year Ponding)

Drainage Area	FUT 600]						
Area (Ha)	0.06	Restricted Flow ICD	_{Actual} (L/s)=	2.00				
C =	1.00	Restricted Flow Q r for	r _{swm calc} (L/s)=	2.00	50% reduction if su			
		100-Year Pond	ling			100-Y	ear +20% Po	onding
T _c Variable	i _{100yr}	Peak Flow Q _p =2.78xCi _{100yr} A	Q_r	$Q_p - Q_r$	Volume 100yr	100YRQ _p 20%	Qp - Qr	Volume 100+20
(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m³)	(L/s)	(L/s)	(m ³)
69	50.33	8.40	2.00	6.40	26.48			
70	49.79	8.30	2.00	6.30	26.48			
71	49.26	8.22	2.00	6.22	26.48	9.86	7.86	33.48
72	48.74	8.13	2.00	6.13	26.48			
73	48.23	8.05	2.00	6.05	26.48			

C =	0.90		estricted Flow Q_r (L/s)= 2.00									
2-Year Ponding												
T _c Variable	i _{2yr}	Peak Flow Q _p =2.78xCi _{2yr} A	Q _r	$Q_p - Q_r$	Volume 2yr							
(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m³)							
27	42.95	6.45	2.00	4.45	7.21							
28	41.93	6.29	2.00	4.29	7.21							
29	40.96	6.15	2.00	4.15	7.22							
30	40.04	6.01	2.00	4.01	7.22							
31	39.17	5.88	2.00	3.88	7.22							

FUT 600

0.06

Drainage Area

Area (Ha)

	St	100+20						
Overflow	Required	Surface	Sub-surface	Balance	Overflow	Required	Balance	
0.00	26.48	33.75	0	0.00	0.00	33.48	0.00	
					convert to flor	w with peak Tc (L/s)	0.00	

overflows to: FUT 120

Storage (m^3) OverflowRequiredSurfaceSub-surfaceBalance0.007.2233.7500.00

overflows to: FUT 120

Calculations for future block 600 taken from overall Arcadia Commercial site plan swm calculations

Drainage Area	FUT 120	Ī										
Area (Ha)	0.11	Restricted Flow ICD	_{Actual} (L/s)=	15.00								
C =	1.00	Restricted Flow Q r for	_{swm calc} (L/s)=	15.00	50% reduction if sub-surface storage							
		100-Year Pond	ing			100-Y	ear +20% Pc	onding				
T _c Variable	i _{100yr}	Peak Flow Q _p =2.78xCi _{100yr} A	Q,	$Q_p - Q_r$	Volume 100yr	100YRQ _p 20%	Qp - Qr	Volume 100+20				
(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m³)	(L/s)	(L/s)	(m ³)				
16	137.55	42.06	15.00	27.06	25.98							
17	132.63	40.56	15.00	25.56	26.07							
18	128.08	39.17	15.00	24.17	26.10	47.00	32.00	34.56				
19	123.87	37.88	15.00	22.88	26.08							
20	119.95	36.68	15.00	21.68	26.02							

Drainage Area	FUT 120		
Area (Ha)	0.11		
C =	0.90	Restricted Flow Q_r (L/s)=	15
		2-Year Ponding	

	2-Year Politing												
T _c Variable	i _{2yr}	Peak Flow Q _p =2.78xCi _{2yr} A	Q_r	Q_p - Q_r	Volume 2yr								
(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m³)								
5	103.57	28.50	15.00	13.50	4.05								
6	96.64	26.60	15.00	11.60	4.17								
7	90.66	24.95	15.00	9.95	4.18								
8	85.46	23.52	15.00	8.52	4.09								
9	80.87	22.26	15.00	7.26	3.92								

	St	100+20						
Overflow	Required	Surface	Sub-surface	Balance	Overflow	Required	Balance	
0.00	26.10	33.99	0	0.00	0.00	34.56	0.57	
					convert to flow	w with peak Tc (L/s)	0.53	

Storage (m°)								
Overflow	Required	Surface	Sub-surface	Balance				
0.00	4.18	61.88	0	0.00				

overflows to: offsite

overflows to: offsite



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Drainage Area	ROOF	Ī						
Area (Ha)	0.07	Restricted Flow ICD ,	_{Actual} (L/s)=	10.00				
C =	1.00	Restricted Flow Q _{r for}	_{swm calc} (L/s)=	10.00	50% reduction if su	ub-surface storage		
		100-Year Pond	ling			100-Y	ear +20% Po	nding
T _c Variable	i _{100yr}	Peak Flow Q _p =2.78xCi _{100yr} A	Q_r	$Q_p - Q_r$	Volume 100yr	100YRQ _p 20%	Qp - Qr	Volume 100+20
(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m³)	(L/s)	(L/s)	(m³)
15	142.89	27.29	10.00	17.29	15.56			
16	137.55	26.27	10.00	16.27	15.62			
17	132.63	25.33	10.00	15.33	15.64	30.40	20.40	20.80
18	128.08	24.46	10.00	14.46	15.62			
19	123.87	23.66	10.00	13.66	15.57			

C =	0.90	Restricted Flow Q _r (L/s)=		10.00			
2-Year Ponding							
T _c Variable	i _{2yr}	Peak Flow Q _p =2.78xCi _{2yr} A	Q_r	Q_p - Q_r	Volume 2yr		
(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m ³)		
4	111.72	19.20	10.00	9.20	2.21		
5	103.57	17.80	10.00	7.80	2.34		
6	96.64	16.61	10.00	6.61	2.38		
7	90.66	15.58	10.00	5.58	2.35		
8	85.46	14.69	10.00	4.69	2.25		

Required

2.38

Storage (m³)

Surface

18.15

ROOF 0.07

Overflow

0.00

76.81

73.17

69.89

110 0.12

Drainage Area

Drainage Area

10 11

12

Area (Ha)

Area (Ha)

	Storage (m ³)					100+20	
Overflow	Required	Surface	Sub-surface	Balance	Overflow	Required	Balance
0.00	15.64	18.15	0	0.00	0.00	20.80	2.65
					convert to flow	w with peak Tc (L/s)	2.60

overflows to: 102

overflows to: 102.00

Balance

0.00

-8.63

-9.92

-11.23

Sub-surface

0

-14.38

-15.02

-15.60

Note: The roof storage volume was calculated by taking the following into consideration: Flat roof area = 363m2 with no obstructions (i.e. 100% of usable area), max ponding depth of 0.15m

15.47

Drainage Area	110							
∖rea (Ha)	0.12	Restricted Flow ICD Ad	_{ctual} (L/s)=	28.00				
C =	0.69	Restricted Flow Q _{r for so}	_{wm calc} (L/s)=	28.00	50% reduction if su	ub-surface storage		
		100-Year Pondi	ng			100-Y	ear +20% Po	nding
T _c Variable	i _{100yr}	Peak Flow Q _p = 2.78xCi _{100yr} A	Q _r	Q_p - Q_r	Volume 100yr	100YRQ _p 20%	Qp - Qr	Volume 100+20
(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m ³)	(L/s)	(L/s)	(m³)
4	262.41	58.18	28.00	30.18	7.24			
5	242.70	53.81	28.00	25.81	7.74			
6	226.01	50.11	28.00	22.11	7.96	60.13	32.13	11.57
7	211.67	46.93	28.00	18.93	7.95			
8	199.20	44.16	28.00	16.16	7.76			

C =	0.55	Restricted Flow Q_r (L/s)= 28.00						
2-Year Ponding								
T _c Variable	i _{2yr}	Peak Flow Q _p =2.78xCi _{2yr} A	Q,	$Q_p - Q_r$	Volume 2yr			
(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m ³)			
8	85.46	15.16	28.00	-12.84	-6.16			
9	80.87	14.34	28.00	-13.66	-7.37			

13.62

12.98

12.40

	S	torage (m³)				100+20	
Overflow	Required	Surface	Sub-surface	Balance	Overflow	Required	Balance
0.00	7.96	8.49	0	0.00	0.00	11.57	3.08
					convert to flo	w with peak Tc (L/s)	8.55
			overflows to:	Campeau Drive)		

_	Storage (m³)							
	Overflow	Required	Surface	Sub-surface	Balance			
	0.00	0.00	8.49	0	0.00			

28.00

28.00

28.00

overflows to: Campeau Drive

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STORMWATER MANAGEMENT

Arcadia Comm | Minto Properties 147391-6.0 | Rev #4R | 2025-04-25 Prepared By: MP | Checked By: RM/WZ

12.50

Drainage Area	102							
Area (Ha)	0.24	Restricted Flow ICD ,	_{Actual} (L/s)=	25.00				
C =	1.00	Restricted Flow Q _{r for}	_{swm calc} (L/s)=	12.50	50% reduction if su	ub-surface storage		
		100-Year Pond	ling			100-Y	ear +20% Po	nding
T _c Variable	i _{100yr}	Peak Flow Q _p =2.78xCi _{100yr} A	Q_r	$Q_p - Q_r$	Volume 100yr	100YRQ _p 20%	Qp - Qr	Volume 100+20
(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m³)	(L/s)	(L/s)	(m³)
44	70.18	46.82	12.50	34.32	90.62			
45	69.05	46.07	12.50	33.57	90.64			
46	67.96	45.34	12.50	32.84	90.65	54.41	41.91	115.68
47	66.91	44.64	12.50	32.14	90.64			
48	65.89	43.96	12.50	31.46	90.61		_	

	2-Year Ponding							
T _c Variable	i _{2yr}	Peak Flow Q _p =2.78xCi _{2yr} A	Q _r	Q _p -Q _r	Volume 2yr			
(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m³)			
16	59.50	33.75	12.50	21.25	20.40			
17	57.42	32.56	12.50	20.06	20.46			
18	55.49	31.47	12.50	18.97	20.49			
19	53.70	30.45	12.50	17.95	20.47			
20	52.03	29.51	12.50	17.01	20.41			

0.85 Restricted Flow Q_r (L/s)=

102 0.24

MH100B

73.17

69.89

Drainage Area

Drainage Area

11

Area (Ha)

Area (Ha)

	S	torage (m ³)				100+20		
Overflow	Required	Surface	Sub-surface	Balance	Overflow	Required	Balance	
0.00	90.65	23.30	68.80	0.00	2.65	118.33	26.23	
		convert to fl	ow with peak Tc (L/s)	0.00	convert to flo	w with peak Tc (L/s)	9.50	
			overflows to: o	offsite				

	Sto	orage (m³)		
Overflow	Required	Surface	Sub-surface	Balance
0.00	20.49	23.30	68.8	0.00

overflows to: offsite

Drainage Area	MH100B	CICB100A, CICB100	B (DA 100A, 10	00B)	_			
Area (Ha)	0.04	Restricted Flow ICD	_{Actual} (L/s)=	24.00	1			
C =	0.70	Restricted Flow Q _{r for}	swm calc (L/s)=	24.00	50% reduction if su	ub-surface storage		
		100-Year Pond	ling			100-Y	ear +20% Po	nding
T _c Variable	i _{100yr}	Peak Flow Q _p =2.78xCi _{100yr} A	Q _r	$Q_p - Q_r$	Volume 100yr	100YRQ _p 20%	Qp - Qr	Volume 100+20
(min)	(mm/hour)	(L/s)	(L/s)	(L/s)	(m ³)	(L/s)	(L/s)	(m ³)
0	398.62	31.03	24.00	7.03	0.00			
0.5	373.35	29.06	24.00	5.06	0.15			
1	351.38	27.35	24.00	3.35	0.20	32.82	8.82	0.53
1.5	332.09	25.85	24.00	1.85	0.17			
2	315.00	24.52	24.00	0.52	0.06			

C =	0.56	Restricted Flow Q _r (I		24.00	
T _c Variable (min)	i _{2yr} (mm/hour)	Peak Flow Q _p =2.78xCi _{2yr} A (L/s)	Q , (L/s)	Q _p -Q _r (L/s)	Volume 2yr (m³)
8	85.46	5.32	24.00	-18.68	-8.97
9	80.87	5.04	24.00	-18.96	-10.24
10	76.81	4.78	24.00	-19.22	-11.53

4.56

	S	torage (m ³)			100+20		
Overflow	Required	Surface	Sub-surface	Balance	Overflow	Required	Balance
0.00	0.20	1.57	0	0.00	0.57	1.10	0.00
		convert to fl	0.00	convert to flo	w with peak Tc (L/s)	0.00	
			overflows to: o	offsite			

	St	orage (m³)		
Overflow	Required	Surface	Sub-surface	Balance
0.00	0.00	1.57	0	0.00

24.00

24.00

overflows to: offsite

-19.44

-19.65

-12.83

-14.15



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STORMWATER MANAGEMENT

Arcadia Comm | Minto Properties 147391-6.0 | Rev #4R | 2025-04-25 Prepared By: MP | Checked By: RM/WZ

	Stormwater Management Summary Table								
Drainage Area	ICD Restricted Flow (L/s)	2 Year Storage Required (m3)	100 Year Storage Required (m3)	Storage Provided					
FUT 600	2.00	7.22	26.48	33.75					
FUT 120	15.00	4.18	26.10	33.99					
ROOF	10.00	2.38	15.64	18.15					
110	28.00	0.00	7.96	8.49					
102	25.00	20.49	90.65	92.10					
MH100B	24.00	0.00	0.20	1.57					
TOTAL	104.00	34.27	167.03	188.05					

 100-yr Overflow:
 0.00 L/s

 100-yr Total Release Rate:
 104.00 L/s

 100-yr Max. Allowable Rate:
 104.77 L/s

 TRUE



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ORIFICE SIZING

Arcadia Commercial Site | Minto Communities 147391-6.0 | Rev #3 | 2025-03-07 Prepared By: MP | Checked By: RM/WZ

Orifice coe	fficients
Cv =	0.60

 $Q=C_v\times A\times \sqrt{2gH}$

							The	oretical	Recor	nmended
	Invert	Diameter	Centre ICD	Max. Pond Elevation	Hydraulic Slope	Target Flow	Orifice	Actual Flow	Orifice	Actual Flow
	(m)	(mm)	(m)	(m)	(m)	(I/s)	(m)	(I/s)	(m)	(I/s)
Area 110	96.952	300	97.102	98.800	1.698	28.00	0.090	28.00	0.090	28.00
Area 102	95.987	450	96.212	98.000	1.788	25.00	0.084	25.00	0.084	25.00
MH100B	96.700	200	96.800	98.530	1.730	24.00	0.083	24.00	0.083	24.00
							*Diamond Shap	e		
						77.00				77.00



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OVERFLOW DEPTH CALCULATIONS

Arcadia Comm | Minto Properties 147391-6.0 | Rev #4R | 2025-04-25 Prepared By: WZ | Checked By: RM

Overflow Area 110

New Flow Section Required 1:1	100 year	flow =	=	0	l/s	or	0.000 Cu m	/sec		
New Flow Section Required 1:1	100 year	+ 209	% flow	8.55	l/s	or	0.009 Cu m	/sec		
Overflow Slope				C	verflow X-S	ectic	n		Overflow Cap	acity - Q
Length =	8.79	m		Side Slope 1 =	1.10	%			From Seelye n =	0.040 (Channels)
Up Stream Ground Elev =	98.80	m		Side Slope 2 =	1.30	%				
Down Stream Ground Elev =	98.56	m		Bottom Width =	0.00	m			100 Year Q =	m³/s
Difference =	0.24	m			100 Yea	ır	100 Year + 20%		100 Year Velocity =	m/s
Ditch Slope =	2.73	%		Water depth =	0.000	m	0.02 m			
				X-Sect. Area =	0.00	m ²	0.04 m ²	,	100 Y +20% Q =	$0.009 \text{ m}^3/\text{s}$
				Wetted Per. =	0.00	m	3.86 m		100 Y + 20% Velocity =	0.21 m/s

Q = A*(1.0/n)*R^2/3*S^1/2

where:

A = cross sectional area in Sq. m

n = friction coefficient

R = hydraulic radius = A/wetted perimetre (wp) in m

Overflow Area 102

New Flow Section Required 1	:100	year flow =	=	0	l/s		or	0.000 Cu m/s	ес		
New Flow Section Required 1	:100	year + 20%	6 flow	9.50	l/s		or	0.010 Cu m/s	ес		
Overflow Slope	9				Overflo	ow X-Se	ectio	n		Overflow Capa	acity - Q
Length =	-	m		Side Slope 1 =		3.80	%			From Seelye n =	0.040 (Channels)
Up Stream Ground Elev =	-	m		Side Slope 2 =		1.33	%				
Down Stream Ground Elev =	-	m		Bottom Width =		0.00	m			100 Year Q =	m³/s
Difference =	-	m			1	00 Year	r	100 Year + 20%		100 Year Velocity =	m/s
Ditch Slope =		1.00 %		Water depth =		0.000	m	0.03 m			
	Esti	imated		X-Sect. Area =		0.00	m ²	0.06 m ²		100 Y +20% Q =	0.010 m ³ /s
				Wetted Per. =		0.00	m	3.45 m		100 Y + 20% Velocity =	0.17 m/s

Q = A*(1.0/n)*R^2/3*S^1/2

where:

A = cross sectional area in Sq. m

n = friction coefficient

R = hydraulic radius = A/wetted perimetre (wp) in m



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RUN-OFF COEFFICIENTS

Arcadia Comm | Minto Properties 147391-6.0 | Rev #1 | 2024-11-13 Prepared By: MP | Checked By: RM

		110			102			100A			100B			ROOF			UNC1	
	GRASS	ROOF	ASPHALT	GRASS	ROOF	ASPHALT	GRASS	ROOF	ASPHALT	GRASS	ROOF	ASPHALT	GRASS	ROOF	ASPHALT	GRASS	ROOF	ASPHAL
	676.46	279.77	291.25	164.21		2194.73	116.22		117.65	118.26		129.88		857.86		37.25		
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TOTAL (m ²)	676.46		291.25	164.21		2194.73	116.22		117.65	118.26		129.88	0.00		0.00	37.25		
TOTAL (III)		1247.48			2358.94			233.87			248.14			857.86			37.25	
off Coefficient (C) :	0.2	0.9	0.9	0.2	0.9	0.9	0.2	0.9	0.9	0.2	0.9	0.9	0.2	0.9	0.9	0.2	0.9	0.9
off Coefficient (C):	U.Z	0.52	0.9	0.2	0.85	0.5	۷.۷	0.55	0.5	0.2	0.57	0.9	0.2	0.90	0.9	0.۷	0.9	0.8
anon Goenicient (G).		0.52			0.00			0.55			0.57			0.90			0.20	

Runoff Coefficient Used(C):	0.52	0.85	0.55	0.57	0.90	0.20

PROJECT INFORMATION					
ENGINEERED PRODUCT MANAGER					
ADS SALES REP					
PROJECT NO.					





ARCADIACOMM OTTAWA, ON, CANADA

DC-780 STORMTECH CHAMBER SPECIFICATIONS

- CHAMBERS SHALL BE STORMTECH DC-780.
- 2. CHAMBERS SHALL BE ARCH-SHAPED AND SHALL BE MANUFACTURED FROM VIRGIN, IMPACT-MODIFIED POLYPROPYLENE COPOLYMERS
- CHAMBERS SHALL BE CERTIFIED TO CSA B184, "POLYMERIC SUB-SURFACE STORMWATER MANAGEMENT STRUCTURES", AND MEET THE REQUIREMENTS OF ASTM F2418, "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 4. CHAMBER ROWS SHALL PROVIDE CONTINUOUS, UNOBSTRUCTED INTERNAL SPACE WITH NO INTERNAL SUPPORTS THAT WOULD IMPEDE FLOW OR LIMIT ACCESS FOR INSPECTION.
- 5. THE STRUCTURAL DESIGN OF THE CHAMBERS, THE STRUCTURAL BACKFILL, AND THE INSTALLATION REQUIREMENTS SHALL ENSURE THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET FOR: 1) LONG-DURATION DEAD LOADS AND 2) SHORT-DURATION LIVE LOADS, BASED ON THE CSA S6 CL-625 TRUCK AND THE AASHTO DESIGN TRUCK WITH CONSIDERATION FOR IMPACT AND MULTIPLE VEHICLE PRESENCES.
- 6. CHAMBERS SHALL BE DESIGNED, TESTED AND ALLOWABLE LOAD CONFIGURATIONS DETERMINED IN ACCORDANCE WITH ASTM F2787, "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS". LOAD CONFIGURATIONS SHALL INCLUDE: 1) INSTANTANEOUS (<1 MIN) AASHTO DESIGN TRUCK LIVE LOAD ON MINIMUM COVER 2) MAXIMUM PERMANENT (75-YR) COVER LOAD AND 3) ALLOWABLE COVER WITH PARKED (1-WEEK) AASHTO DESIGN TRUCK.</p>
- 7. REQUIREMENTS FOR HANDLING AND INSTALLATION:
 - TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING, CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS.
 - TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL, THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 50 mm (2").
 - TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION, a) THE ARCH STIFFNESS CONSTANT AS DEFINED IN SECTION 6.2.8 OF ASTM F2418 SHALL BE GREATER THAN OR EQUAL TO 550 LBS/FT/%. AND b) TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES (ABOVE 23° C / 73° F), CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS.
- 8. ONLY CHAMBERS THAT ARE APPROVED BY THE SITE DESIGN ENGINEER WILL BE ALLOWED. UPON REQUEST BY THE SITE DESIGN ENGINEER OR OWNER, THE CHAMBER MANUFACTURER SHALL SUBMIT A STRUCTURAL EVALUATION FOR APPROVAL BEFORE DELIVERING CHAMBERS TO THE PROJECT SITE AS FOLLOWS:
 - THE STRUCTURAL EVALUATION SHALL BE SEALED BY A REGISTERED PROFESSIONAL ENGINEER.
 - THE STRUCTURAL EVALUATION SHALL DEMONSTRATE THAT THE SAFETY FACTORS ARE GREATER THAN OR EQUAL TO 1.95 FOR
 DEAD LOAD AND 1.75 FOR LIVE LOAD, THE MINIMUM REQUIRED BY ASTM F2787 AND BY SECTIONS 3 AND 12.12 OF THE AASHTO
 LRFD BRIDGE DESIGN SPECIFICATIONS FOR THERMOPLASTIC PIPE.
 - THE TEST DERIVED CREEP MODULUS AS SPECIFIED IN ASTM F2418 SHALL BE USED FOR PERMANENT DEAD LOAD DESIGN EXCEPT THAT IT SHALL BE THE 75-YEAR MODULUS USED FOR DESIGN.
- 9. CHAMBERS AND END CAPS SHALL BE PRODUCED AT AN ISO 9001 CERTIFIED MANUFACTURING FACILITY.
- 10. MANIFOLD SIZE TO BE DETERMINED BY SITE DESIGN ENGINEER. SEE TECH NOTE #6.32 FOR MANIFOLD SIZING GUIDANCE. DUE TO THE ADAPTATION OF THIS CHAMBER SYSTEM TO SPECIFIC SITE AND DESIGN CONSTRAINTS, IT MAY BE NECESSARY TO CUT AND COUPLE ADDITIONAL PIPE TO STANDARD MANIFOLD COMPONENTS IN THE FIELD.
- 11. ADS DOES NOT DESIGN OR PROVIDE MEMBRANE LINER SYSTEMS. TO MINIMIZE THE LEAKAGE POTENTIAL OF LINER SYSTEMS, THE MEMBRANE LINER SYSTEM SHOULD BE DESIGNED BY A KNOWLEDGEABLE GEOTEXTILE PROFESSIONAL AND INSTALLED BY A QUALIFIED CONTRACTOR.

IMPORTANT - NOTES FOR THE BIDDING AND INSTALLATION OF THE DC-780 CHAMBER SYSTEM

- 1. STORMTECH DC-780 CHAMBERS SHALL NOT BE INSTALLED UNTIL THE MANUFACTURER'S REPRESENTATIVE HAS COMPLETED A PRE-CONSTRUCTION MEETING WITH THE INSTALLERS.
- 2. STORMTECH DC-780 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE".
- 3. CHAMBERS ARE NOT TO BE BACKFILLED WITH A DOZER OR AN EXCAVATOR SITUATED OVER THE CHAMBERS. STORMTECH RECOMMENDS 3 BACKFILL METHODS:
 - STONESHOOTER LOCATED OFF THE CHAMBER BED
 - BACKFILL AS ROWS ARE BUILT USING AN EXCAVATOR ON THE FOUNDATION STONE OR SUBGRADE.
 - BACKFILL FROM OUTSIDE THE EXCAVATION USING A LONG BOOM HOE OR EXCAVATOR.
- 4. THE FOUNDATION STONE SHALL BE LEVELED AND COMPACTED PRIOR TO PLACING CHAMBERS.
- 5. JOINTS BETWEEN CHAMBERS SHALL BE PROPERLY SEATED PRIOR TO PLACING STONE.
- 6. MAINTAIN MINIMUM 150 mm (6") SPACING BETWEEN THE CHAMBER ROWS.
- 7. EMBEDMENT STONE SURROUNDING CHAMBERS MUST BE A CLEAN, CRUSHED, ANGULAR STONE OR RECYCLED CONCRETE; AASHTO M43 #3, 357, 4, 467, 5, 56, OR 57.
- 3. THE CONTRACTOR MUST REPORT ANY DISCREPANCIES WITH CHAMBER FOUNDATION MATERIALS BEARING CAPACITIES TO THE SITE DESIGN ENGINEER.
- 9. ADS RECOMMENDS THE USE OF "FLEXSTORM CATCH IT" INSERTS DURING CONSTRUCTION FOR ALL INLETS TO PROTECT THE SUBSURFACE STORMWATER MANAGEMENT SYSTEM FROM CONSTRUCTION SITE RUNOFF.

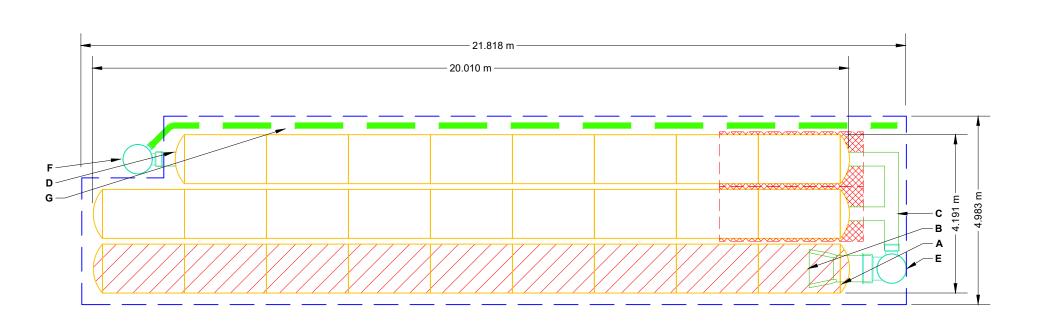
NOTES FOR CONSTRUCTION EQUIPMENT

- . STORMTECH DC-780 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE".
- THE USE OF CONSTRUCTION EQUIPMENT OVER DC-780 CHAMBERS IS LIMITED:
 - NO EQUIPMENT IS ALLOWED ON BARE CHAMBERS.
 - NO RUBBER TIRED LOADERS, DUMP TRUCKS, OR EXCAVATORS ARE ALLOWED UNTIL PROPER FILL DEPTHS ARE REACHED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE".
 - WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT CAN BE FOUND IN THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE".
- 3. FULL 900 mm (36") OF STABILIZED COVER MATERIALS OVER THE CHAMBERS IS REQUIRED FOR DUMP TRUCK TRAVEL OR DUMPING.

USE OF A DOZER TO PUSH EMBEDMENT STONE BETWEEN THE ROWS OF CHAMBERS MAY CAUSE DAMAGE TO THE CHAMBERS AND IS NOT AN ACCEPTABLE BACKFILL METHOD. ANY CHAMBERS DAMAGED BY THE "DUMP AND PUSH" METHOD ARE NOT COVERED UNDER THE STORMTECH STANDARD WARRANTY.

CONTACT STORMTECH AT 1-800-821-6710 WITH ANY QUESTIONS ON INSTALLATION REQUIREMENTS OR WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT.

	PROPOSED LAYOUT	CONCEPTUAL ELEVATIONS:				*INVERT	ABOVE BAS	E OF CHAMBER
26	STORMTECH DC-780 CHAMBERS	MAXIMUM ALLOWABLE GRADE (TOP OF PAVEMENT/UNPAVED):	4.648	PART TYPE	ITEM O		INVERT*	MAX FLOW
	STONE ABOVE (mm)	MINIMUM ALLOWABLE GRADE (UNPAVED WITH TRAFFIC): MINIMUM ALLOWABLE GRADE (UNPAVED NO TRAFFIC):		PREFABRICATED EZ END CAP	А	600 mm BOTTOM PREFABRICATED EZ END CAP, PART#: SC740ECEZ / TYP OF ALL 600 mm BOTTOM CONNECTIONS AND ISOLATOR PLUS ROWS	3 mm	
229 40	STONE BELOW (mm) STONE VOID	MINIMUM ALLOWABLE GRADE (TOP OF RIGID CONCRETE PAVEMENT): MINIMUM ALLOWABLE GRADE (BASE OF FLEXIBLE PAVEMENT):	1.448	FLAMP MANIFOLD	В	INSTALL FLAMP ON 600 mm ACCESS PIPE / PART#: SC74024RAMP 300 mm x 300 mm TOP MANIFOLD, ADS N-12	318 mm	
68.8	(PERIMETER STONE INCLUDED)	TOP OF STONE: TOP OF DC-780 CHAMBER:	1.143 0.991	PIPE CONNECTION NYLOPLAST (INLET W/ ISO		300 mm BOTTOM CONNECTION	30 mm	
	(BASE STONE INCLUDED)	300 mm x 300 mm TOP MANIFOLD INVERT: 300 mm BOTTOM CONNECTION INVERT:	0.259	PLUS ROW)	E	750 mm DIAMETER (610 mm SUMP MIN)		130 L/s IN
	` '	600 mm ISOLATOR ROW PLUS INVERT: BOTTOM OF DC-780 CHAMBER:	0.20.	NYLOPLAST (OUTLET) UNDERDRAIN	F G	750 mm DIAMETER (DESIGN BY ENGINEER) 150 mm ADS N-12 DUAL WALL PERFORATED HDPE UNDERDRAIN		57 L/s OUT
		UNDERDRAIN INVERT: BOTTOM OF STONE:	0.000 0.000				· · · · · ·	



ISOLATOR ROW PLUS (SEE DETAIL)

BED LIMITS

PLACE MINIMUM 3.810 m OF ADSPLUS625 WOVEN GEOTEXTILE OVER BEDDING STONE AND UNDERNEATH CHAMBER FEET FOR SCOUR PROTECTION AT ALL CHAMBER INLET ROWS

NOTES

THE SITE DESIGN ENGINEER MUST REVIEW ELEVATIONS AND IF NECESSARY ADJUST GRADING TO ENSURE THE CHAMBER COVER REQUIREMENTS ARE MET.

NOT FOR CONSTRUCTION: THIS LAYOUT IS FOR DIMENSIONAL PURPOSES ONLY TO PROVE CONCEPT & THE REQUIRED STORAGE VOLUME CAN BE ACHIEVED ON SITE.

DRW 3 OF RECC **StormTech**® Chamber System 4640 TRUEMAN BLVD HILLIARD, OH 43026 1-800-733-7473 : 100 П SCALE SHEET

2 OF 6

DATE: 11/05/2024 DRAWN: MP
PROJECT #: CHECKED: N/A
HIS DRAWING IS NOT INTENDED FOR USE IN BIDDING OR CONSTITED AND ALL ASSOCIATED DEFAULS MEET ALL APPLICABLE

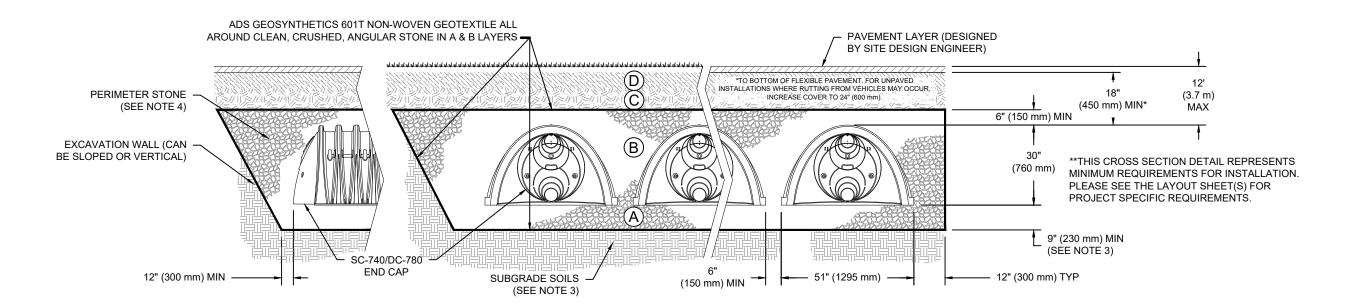
ARCADIACOMM

ACCEPTABLE FILL MATERIALS: STORMTECH DC-780 CHAMBER SYSTEMS

	MATERIAL LOCATION	DESCRIPTION	AASHTO MATERIAL CLASSIFICATIONS	COMPACTION / DENSITY REQUIREMENT
D	FINAL FILL: FILL MATERIAL FOR LAYER 'D' STARTS FROM THE TOP OF THE 'C' LAYER TO THE BOTTOM OF FLEXIBLE PAVEMENT OR UNPAVED FINISHED GRADE ABOVE. NOTE THAT PAVEMENT SUBBASE MAY BE PART OF THE 'D' LAYER	ANY SOIL/ROCK MATERIALS, NATIVE SOILS, OR PER ENGINEER'S PLANS. CHECK PLANS FOR PAVEMENT SUBGRADE REQUIREMENTS.	N/A	PREPARE PER SITE DESIGN ENGINEER'S PLANS. PAVED INSTALLATIONS MAY HAVE STRINGENT MATERIAL AND PREPARATION REQUIREMENTS.
С	INITIAL FILL: FILL MATERIAL FOR LAYER 'C' STARTS FROM THE TOP OF THE EMBEDMENT STONE ('B' LAYER) TO 18" (450 mm) ABOVE THE TOP OF THE CHAMBER. NOTE THAT PAVEMENT SUBBASE MAY BE A PART OF THE 'C' LAYER.	GRANULAR WELL-GRADED SOIL/AGGREGATE MIXTURES, <35% FINES OR PROCESSED AGGREGATE. MOST PAVEMENT SUBBASE MATERIALS CAN BE USED IN LIEU OF THIS LAYER.	AASHTO M145 ¹ A-1, A-2-4, A-3 OR AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57, 6, 67, 68, 7, 78, 8, 89, 9, 10	BEGIN COMPACTIONS AFTER 12" (300 mm) OF MATERIAL OVER THE CHAMBERS IS REACHED. COMPACT ADDITIONAL LAYERS IN 6" (150 mm) MAX LIFTS TO A MIN. 95% PROCTOR DENSITY FOR WELL GRADED MATERIAL AND 95% RELATIVE DENSITY FOR PROCESSED AGGREGATE MATERIALS. ROLLER GROSS VEHICLE WEIGHT NOT TO EXCEED 12,000 lbs (53 kN). DYNAMIC FORCE NOT TO EXCEED 20,000 lbs (89 kN).
В	EMBEDMENT STONE: FILL SURROUNDING THE CHAMBERS FROM THE FOUNDATION STONE ('A' LAYER) TO THE 'C' LAYER ABOVE.	CLEAN, CRUSHED, ANGULAR STONE OR RECYCLED CONCRETE ⁵	AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57	NO COMPACTION REQUIRED.
А	FOUNDATION STONE: FILL BELOW CHAMBERS FROM THE SUBGRADE UP TO THE FOOT (BOTTOM) OF THE CHAMBER.	CLEAN, CRUSHED, ANGULAR STONE OR RECYCLED CONCRETE ⁵	AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57	PLATE COMPACT OR ROLL TO ACHIEVE A FLAT SURFACE. ^{2,3}

DI EASE NOTE

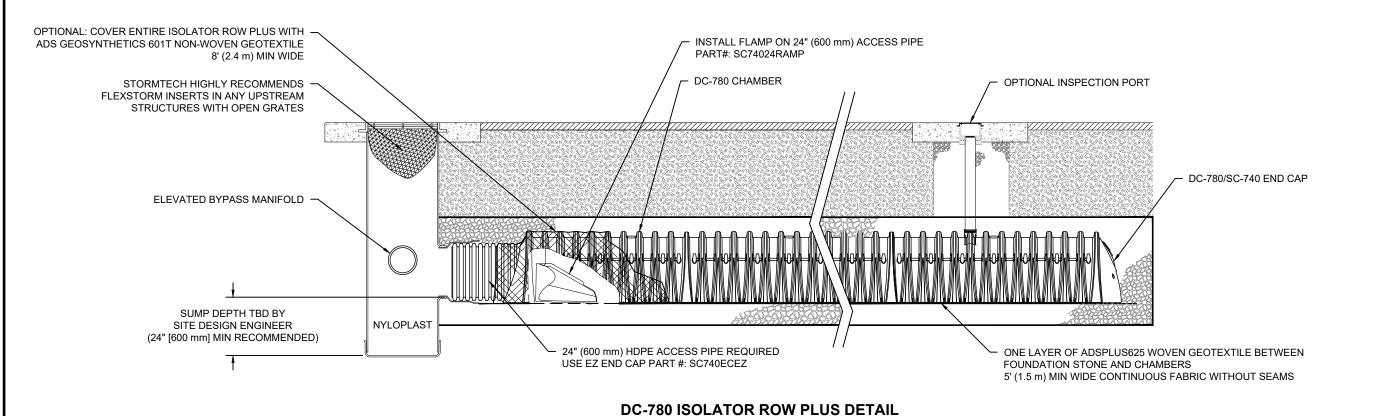
- 1. THE LISTED AASHTO DESIGNATIONS ARE FOR GRADATIONS ONLY. THE STONE MUST ALSO BE CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR NO. 4 (AASHTO M43) STONE".
- 2. STORMTECH COMPACTION REQUIREMENTS ARE MET FOR 'A' LOCATION MATERIALS WHEN PLACED AND COMPACTED IN 9" (230 mm) (MAX) LIFTS USING TWO FULL COVERAGES WITH A VIBRATORY COMPACTOR.
- 3. WHERE INFILTRATION SURFACES MAY BE COMPROMISED BY COMPACTION, FOR STANDARD DESIGN LOAD CONDITIONS, A FLAT SURFACE MAY BE ACHIEVED BY RAKING OR DRAGGING WITHOUT COMPACTION EQUIPMENT. FOR SPECIAL LOAD DESIGNS, CONTACT STORMTECH FOR COMPACTION REQUIREMENTS
- 4. ONCE LAYER 'C' IS PLACED, ANY SOIL/MATERIAL CAN BE PLACED IN LAYER 'D' UP TO THE FINISHED GRADE. MOST PAVEMENT SUBBASE SOILS CAN BE USED TO REPLACE THE MATERIAL REQUIREMENTS OF LAYER 'C' OR 'D' AT THE SITE DESIGN ENGINEER'S DISCRETION.
- 5. WHERE RECYCLED CONCRETE AGGREGATE IS USED IN LAYERS 'A' OR 'B' THE MATERIAL SHOULD ALSO MEET THE ACCEPTABILITY CRITERIA OUTLINED IN TECHNICAL NOTE 6.20 "RECYCLED CONCRETE STRUCTURAL BACKFILL".



NOTES:

- 1. CHAMBERS SHALL MEET THE REQUIREMENTS OF ASTM F2418, "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 2. DC-780 CHAMBERS SHALL BE DESIGNED IN ACCORDANCE WITH ASTM F2787 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 3. THE SITE DESIGN ENGINEER IS RESPONSIBLE FOR ASSESSING THE BEARING RESISTANCE (ALLOWABLE BEARING CAPACITY) OF THE SUBGRADE SOILS AND THE DEPTH OF FOUNDATION STONE WITH CONSIDERATION FOR THE RANGE OF EXPECTED SOIL MOISTURE CONDITIONS. REFERENCE STORMTECH DESIGN MANUAL FOR BEARING CAPACITY GUIDANCE.
- 4. PERIMETER STONE MUST BE EXTENDED HORIZONTALLY TO THE EXCAVATION WALL FOR BOTH VERTICAL AND SLOPED EXCAVATION WALLS.
- 5. REQUIREMENTS FOR HANDLING AND INSTALLATION:
 - TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING, CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS.
 - TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL, THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 2".
 - TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION, a) THE ARCH STIFFNESS CONSTANT SHALL BE GREATER THAN OR EQUAL TO 550 LBS/FT/%. THE ASC IS DEFINED IN SECTION 6.2.8 OF ASTM F2418. AND b) TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES (ABOVE 73° F / 23° C), CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS.





INSPECTION & MAINTENANCE

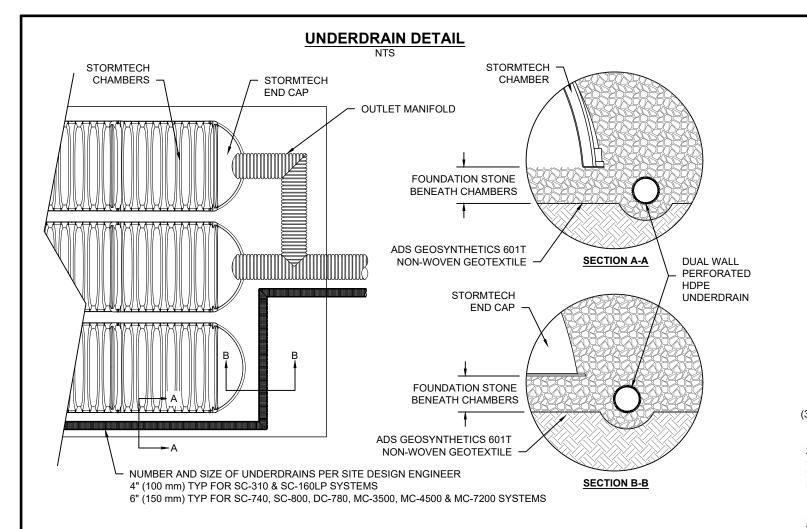
INSPECT ISOLATOR ROW PLUS FOR SEDIMENT

- A. INSPECTION PORTS (IF PRESENT)
- REMOVE/OPEN LID ON NYLOPLAST INLINE DRAIN
- REMOVE AND CLEAN FLEXSTORM FILTER IF INSTALLED
- USING A FLASHLIGHT AND STADIA ROD, MEASURE DEPTH OF SEDIMENT AND RECORD ON MAINTENANCE LOG LOWER A CAMERA INTO ISOLATOR ROW PLUS FOR VISUAL INSPECTION OF SEDIMENT LEVELS (OPTIONAL)
- IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2, IF NOT, PROCEED TO STEP 3.
- B. ALL ISOLATOR PLUS ROWS
- REMOVE COVER FROM STRUCTURE AT UPSTREAM END OF ISOLATOR ROW PLUS
- USING A FLASHLIGHT, INSPECT DOWN THE ISOLATOR ROW PLUS THROUGH OUTLET PIPE
 - i) MIRRORS ON POLES OR CAMERAS MAY BE USED TO AVOID A CONFINED SPACE ENTRY
 - ii) FOLLOW OSHA REGULATIONS FOR CONFINED SPACE ENTRY IF ENTERING MANHOLE
- IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3.
- CLEAN OUT ISOLATOR ROW PLUS USING THE JETVAC PROCESS
 - A. A FIXED CULVERT CLEANING NOZZLE WITH REAR FACING SPREAD OF 45" (1.1 m) OR MORE IS PREFERRED
 - APPLY MULTIPLE PASSES OF JETVAC UNTIL BACKFLUSH WATER IS CLEAN
 - C. VACUUM STRUCTURE SUMP AS REQUIRED
- REPLACE ALL COVERS, GRATES, FILTERS, AND LIDS; RECORD OBSERVATIONS AND ACTIONS.
- INSPECT AND CLEAN BASINS AND MANHOLES UPSTREAM OF THE STORMTECH SYSTEM. STEP 4)

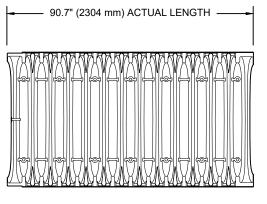
NOTES

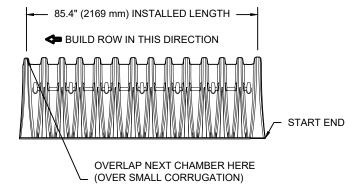
- INSPECT EVERY 6 MONTHS DURING THE FIRST YEAR OF OPERATION. ADJUST THE INSPECTION INTERVAL BASED ON PREVIOUS OBSERVATIONS OF SEDIMENT ACCUMULATION AND HIGH WATER ELEVATIONS.
- 2. CONDUCT JETTING AND VACTORING ANNUALLY OR WHEN INSPECTION SHOWS THAT MAINTENANCE IS NECESSARY.

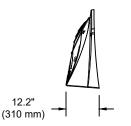


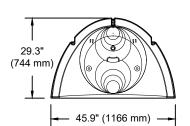


DC-780 TECHNICAL SPECIFICATION

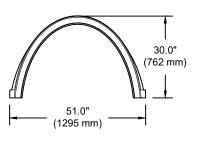








45.9" X 29.3" X 9.6"



NOMINAL CHAMBER SPECIFICATIONS

SIZE (W X H X INSTALLED LENGTH) CHAMBER STORAGE MINIMUM INSTALLED STORAGE* WEIGHT

51.0" X 30.0" X 85.4" (1295 mm X 762 mm X 2169 mm) 46.2 CUBIC FEET (1.30 m³) 78.4 CUBIC FEET (2.20 m³) 75.0 lbs. (33.6 kg)

(1166 mm X 744 mm X 244 mm)

NOMINAL END CAP SPECIFICATIONS

SIZE (W X H X INSTALLED LENGTH) **END CAP STORAGE** MINIMUM INSTALLED STORAGE** WEIGHT

2.6 CUBIC FEET (0.07 m^3) 14.4 CUBIC FEET (0.40 m^3) 11.7 lbs. (5.3 kg)

* ASSUMES 6" (152 mm) STONE ABOVE, 9" (229 mm) BELOW, AND 6" (152 mm) BETWEEN CHAMBERS

**ASSUMES 6" (152 mm) STONE ABOVE, 9" (229 mm) BELOW END CAPS, 6" (152 mm) BETWEEN ROWS, 12" (305 mm) BEYOND END CAPS

PRE-FAB STUBS AT BOTTOM OF END CAP FOR PART NUMBERS ENDING WITH "B" PRE-FAB STUBS AT TOP OF END CAP FOR PART NUMBERS ENDING WITH "T"

PART#	STUB	Α	В	С
SC740EPE06T / SC740EPE06TPC	6" (150 mm)	10.9" (277 mm)	18.5" (470 mm)	
SC740EPE06B / SC740EPE06BPC	0 (13011111)	10.9 (277 111111)		0.5" (13 mm)
SC740EPE08T /SC740EPE08TPC	8" (200 mm)	12.2" (310 mm)	16.5" (419 mm)	
SC740EPE08B / SC740EPE08BPC	0 (200 11111)	12.2 (310111111)		0.6" (15 mm)
SC740EPE10T / SC740EPE10TPC	10" (250 mm)	13.4" (340 mm)	14.5" (368 mm)	
SC740EPE10B / SC740EPE10BPC	10 (23011111)	13.4 (340 11111)		0.7" (18 mm)
SC740EPE12T / SC740EPE12TPC	12" (300 mm)	14.7" (373 mm)	12.5" (318 mm)	
SC740EPE12B / SC740EPE12BPC	12 (300 11111)	14.7 (373 11111)		1.2" (30 mm)
SC740EPE15T / SC740EPE15TPC	15" (375 mm)	18.4" (467 mm)	9.0" (229 mm)	
SC740EPE15B / SC740EPE15BPC	1 15 (3/5 111111)	10.4 (407 111111)		1.3" (33 mm)
SC740EPE18T / SC740EPE18TPC	18" (450 mm)	19.7" (500 mm)	5.0" (127 mm)	
SC740EPE18B / SC740EPE18BPC	10 (430 111111)	19.7 (500 11111)		1.6" (41 mm)
SC740ECEZ*	24" (600 mm)	18.5" (470 mm)		0.1" (3 mm)

ALL STUBS, EXCEPT FOR THE SC740ECEZ ARE PLACED AT BOTTOM OF END CAP SUCH THAT THE OUTSIDE DIAMETER OF THE STUB IS FLUSH WITH THE BOTTOM OF THE END CAP. FOR ADDITIONAL INFORMATION CONTACT STORMTECH AT 1-800-821-6710.

* FOR THE SC740ECEZ THE 24" (600 mm) STUB LIES BELOW THE BOTTOM OF THE END CAP APPROXIMATELY 1.75" (44 mm). BACKFILL MATERIAL SHOULD BE REMOVED FROM BELOW THE N-12 STUB SO THAT THE FITTING SITS LEVEL.

NOTE: ALL DIMENSIONS ARE NOMINAL

	ARCADIACOMM)	OTTAWA, ON, CANADA		DRAWN: MD	וווי .	CHECKED: N/A
	ARCADI		OTTAWA, O		DATE: 11/05/2024	CA1E. 1100/2024	PROJECT #:
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StormTech® Chamber System

4640 TRUEMAN BLVD HILLIARD, OH 43026 1-800-733-7473

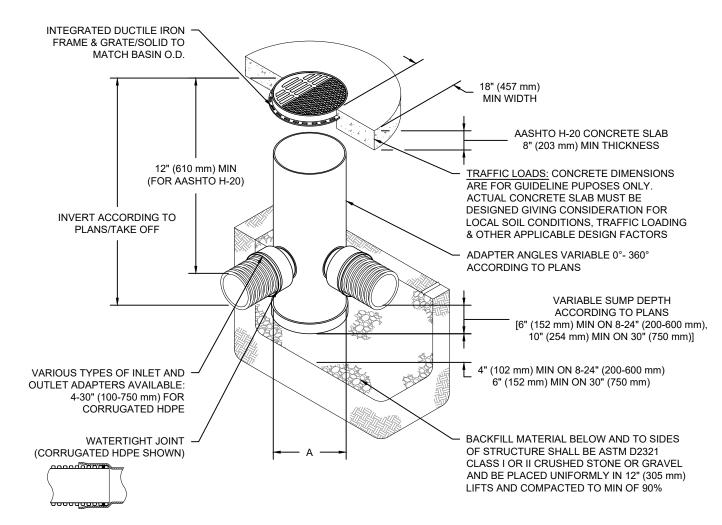


SHEET

5 OF 6

NYLOPLAST DRAIN BASIN

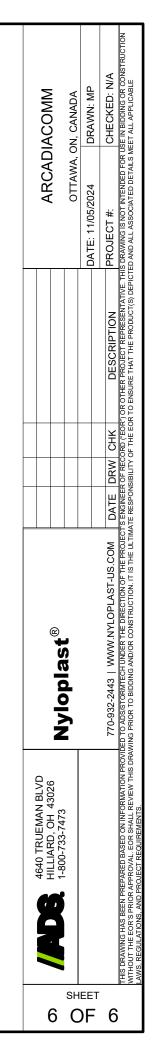
NTS

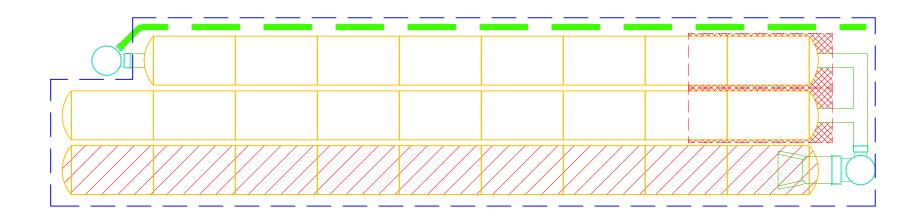


NOTES

- 1. 8-30" (200-750 mm) GRATES/SOLID COVERS SHALL BE DUCTILE IRON PER ASTM A536 GRADE 70-50-05
- 12-30" (300-750 mm) FRAMES SHALL BE DUCTILE IRON PER ASTM A536 GRADE 70-50-05
 DRAIN BASIN TO BE CUSTOM MANUFACTURED ACCORDING TO PLAN DETAILS
- DRAINAGE CONNECTION STUB JOINT TIGHTNESS SHALL CONFORM TO ASTM D3212
- 4. DRAINAGE CONNECTION STUB JOINT TIGHTNESS SHALL CONFORM TO ASTM D3212 FOR CORRUGATED HDPE (ADS & HANCOR DUAL WALL) & SDR 35 PVC
- 5. FOR COMPLETE DESIGN AND PRODUCT INFORMATION: WWW.NYLOPLAST-US.COM
- 6. TO ORDER CALL: 800-821-6710

Α	PART#	GRATE/S	SOLID COVER (OPTIONS
8" (200 mm)	2808AG	PEDESTRIAN LIGHT DUTY	STANDARD LIGHT DUTY	SOLID LIGHT DUTY
10" (250 mm)	2810AG	PEDESTRIAN LIGHT DUTY	STANDARD LIGHT DUTY	SOLID LIGHT DUTY
12"	2812AG	PEDESTRIAN	STANDARD AASHTO	SOLID
(300 mm)		AASHTO H-10	H-20	AASHTO H-20
15"	2815AG	PEDESTRIAN	STANDARD AASHTO	SOLID
(375 mm)		AASHTO H-10	H-20	AASHTO H-20
18"	2818AG	PEDESTRIAN	STANDARD AASHTO	SOLID
(450 mm)		AASHTO H-10	H-20	AASHTO H-20
24"	2824AG	PEDESTRIAN	STANDARD AASHTO	SOLID
(600 mm)		AASHTO H-10	H-20	AASHTO H-20
30"	2830AG	PEDESTRIAN	STANDARD AASHTO	SOLID
(750 mm)		AASHTO H-20	H-20	AASHTO H-20







Adjustable Accutrol Weir

Adjustable Flow Control for Roof Drains

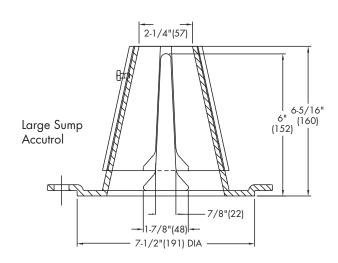
ADJUSTABLE ACCUTROL (for Large Sump Roof Drains only)

For more flexibility in controlling flow with heads deeper than 2", Watts Drainage offers the Adjustable Accutrol. The Adjustable Accutrol Weir is designed with a single parabolic opening that can be covered to restrict flow above 2" of head to less than 5 gpm per inch, up to 6" of head. To adjust the flow rate for depths over 2" of head, set the slot in the adjustable upper cone according to the flow rate required. Refer to Table 1 below. Note: Flow rates are directly proportional to the amount of weir opening that is exposed.

EXAMPLE:

For example, if the adjustable upper cone is set to cover 1/2 of the weir opening, flow rates above 2"of head will be restricted to 2-1/2 gpm per inch of head.

Therefore, at 3" of head, the flow rate through the Accutrol Weir that has 1/2 the slot exposed will be: [5 gpm (per inch of head) \times 2 inches of head] + 2-1/2 gpm (for the third inch of head) = 12-1/2 gpm.



Adjustable Upper Cone

Fixed Weir

1/2 Weir Opening Exposed Shown Above

TABLE 1. Adjustable Accutrol Flow Rate Settings

Wain Ononing	1"	2"	3"	4"	5"	6"
Weir Opening Exposed		Flow Ro	ate (galle	ons per	minute)	
Fully Exposed	5	10	15	20	25	30
3/4	5	10	13.75	17.5	21.25	25
1/2	5	10	12.5	15	17.5	20
1/4	5	10	11.25	12.5	13.75	15
Closed	5	5	5	5	5	5

Job Name	Contractor
lab l apation	Contractorio D.O. No
Job Location	Contractor's P.O. No.
Engineer	Representative
<u>e</u>	·

Watts product specifications in U.S. customary units and metric are approximate and are provided for reference only. For precise measurements, please contact Watts Technical Service. Watts reserves the right to change or modify product design, construction, specifications, or materials without prior notice and without incurring any obligation to make such changes and modifications on Watts products previously or subsequently sold.



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Latin America: Tel: (52) 81-1001-8600 • Fax: (52) 81-8000-7091 • Watts.com



STORM SEWER DESIGN SHEET

PROJECT: Arcadía Commercial LOCATION: CITY OF OTTAWA

CLIENT: Minto Development Group *HGL at obvert of pipe if

*HGL at obvert of pipe if plpe is not surcharged

** Finished floor for slab on grade commercial building

***Freeboard is from upstream MH HGL to FF

								EWER DATA	SE									SIGN FLOW	ATIONAL DE	R							AREA (Ha)					LOCATION
** Fre	HGL*	upstream	surcharged	CAP (5yr)	AVAIL	VELOCITY	SLOPE		IPE SIZE (mm)	P	LENGTH	CAPACITY	DESIGN	ICD FIXED	100vr PEAK	10vr PEAK	5vr PEAK	i (100)	1 (10)	1 (5)	TOTAL	TIME	INLET	CUM	IND	C=		C=	то		FROM	LOCATION
1	m	obvert	pipe	(%)	(L/s)	(m/s)	(%)	Н	w	DIA	(m)	(L/s)	FLOW (L/s)	FLOW (L/s)	FLOW (L/s)	FLOW (L/s)	FLOW (L/s)	(mm/hr)	(mm/hr)	(mm/hr)	(min)	IN PIPE			,	_	0.70 0.75	- 1	MH		MH	AREA ID
30	96,79			74,79%	46.40	1.224	1.00			250	5.00	62.04	15.64				15.64	178.56	122.14	104.19	10.07	0.07	10.00		0.45	0.00						
										2.50	3100	02.04	13.04				13.04	1/0.30	122.14	104.19	20.07	0.07	10.00	0.15	0.15	0.06	_	-	MAIN	0	BLK800	BLK800
				64.34%	28.23	0.866	0.50			250	5.97	43.87	15.64				15.64	178.56	122.14	104.19	10.11	0.11	10.00	0.15	0.15	0.06			MAIN	3	CICB123	123
	96.79	96.79	no	47.76%	28.51	0.818	0.35			300	20.50	50.00	24.40				21.12														-	
	30.73	30.73	no	47.70%	20.31	0.818	0.55			300	26.56	59,68	31.18				31.18	177.94	121.72	103.83	10.61	0.54	.10:07	0.30	0.00			_	MH122	30 04	MH123	
				64.34%	28.23	0.866	0.50			250	23.63	43.87	15.64				15.64	178.56	122.14	104.19	10:45	0.45	10.00	0.15	0.15	0.06		-	MAIN		CB122	122
	96.67	96.67		23.72%	14.16	0.818	0.35			200	42.00	50.00	40.50																Hermite			
	90.07	30.07	no	23.72%	14.10	0.010	0.33			300	12.08	59.68	45.52				45.52	173.18	118.48	101.08	10.86	0.25	10.81	0.45	0.00				MH121	2	WH122	*
45	96.63			49.78%	25.84	1.024	0.70			250	5.00	51.91	26.07				26.07	178.56	122.14	104.19	10.08	0.08	10.00	0.25	0.25	0.10			MAIN	0	BLK700	BLK700
	00.53	06.53		23.49%	21.40	0.002	0.25																						(FEFALL)		0.000	BEIGGO
	96.63	96.63	no	23.49%	21.48	0.802	0.25			375	58.21	91.46	69.97				69.97	171.10	117.06	99.88	12.06	1.21	10.86	0.70	0.00				MH120	1	MH121	
				53.78%	33.36	1.224	1.00			250	23.24	62.04	28.68				28.68	178.56	122.14	104.19	10.32	0.32	10.00	0.28	0.28	0.11	_	-	MH120	,	CB120	120
																							20300	GILO	1	0.22			WILLEA		CBIZO	120
70	96.45			74.79%	46.40	1.224	1.00			250	5.00	62.04	15.64				15.64	178.56	122.14	104.19	10.07	0.07	10.00	0.15	0.15	0.06			MAIN	0	BLK600	BLK600
	96.45	96.45	по	28.52%	42.41	0.906	0.25			450	51.96	148.72	106.31				106.31	161.66	110.63	94.42	13.02	0.96	12.05	1.13	0.00	+	_	-	MH100	0	MH120	
			į																					1.13	0.00				WINTED		MINAZO	
	- 1			70.76% 85.38%	50.48 60.91	0.978	0.50			300	29.02	71.33	20.86				20.86	178.56	122.14	104.19	10.49	0.49	10.00		0.20				BMH110A		CB110A	110
				89.35%	255.95	0.982	0.20			600	15.38	71.33 286.47	10.43 30.52				10.43 30.52	178.56 174.16	122.14 119.15	104.19	10.34	0.34	10.00		0.10	0.04	_		BMH110A	-	CB110B	U
										000	13.30	200.47	30.32				30.32	174.16	119,15	101.65	10.76	0.26	10.49	0.30	0.00		_		MH110	LOA	CBMH110A	
	96.54	96.54	no	52.77%	33.67	0.874	0.40			300	53.50	63.80	30.13				30.13	171.93	117.63	100.36	11.78	1.02	10.75	0.30	0.00				MH100	0	MH110	
15	96.32			62.18%	38.58	1.224	1.00			250	16.50	62.04	23.46			_	23,46	178.56	122.14	104.19	10.72	0.33	10.00	0.00	0.00				330000			
												94101	23170				23,40	176.30	142.14	104.13	10.22	0.22	10.00	0.23	0.23	0.09			MAIN	Ų .	BLK500	BLK500
			į.	87.39%	54.22	1.224	1.00			250	8.00	62.04	7.82				7.82	178.56	122.14	104.19	10.11	0.11	10.00	80.0	0.08	0.03			CICB100B	0A	CICB100A	100A
				74.93%	46.48	1.224	1.00			250	0.74	62.04	15.56				15.56	177.57	121.47	103.62	10.12	0.01	10.11	0.15	0.08	0.03			MAIN	0B	CICB100B	100B
	96.32	96.32	no		84.97	0.850	0.15			600	32.73	248.09	163.12				163.12	154.97	106.08	90.55	13.66	0.64	13.02	1.80	0.00	_			MH100B	0	MH100	
			no	36.00%	89.30	0.850	0.15			600	16.00	248.09	158.78				158.78	150.81	103.25	88.14	13.98	0.31	13.66	1.80	THE RESIDENCE OF THE PERSON NAMED IN				XMH301		MH100B	EXISTING
	96.052	96.25	no																								0.00 0.0			_		



STORM SEWER DESIGN SHEET

PROJECT: Arcadla Commercial LOCATION: CITY OF OTTAWA

CLIENT: Minto Development Group

*HGL at obvert of pipe if pipe is not surcharged

** Finished floor for siab on grade commercial building

***Freeboard is from upstream MH HGL to FF

	LOCATION			!	AREA (Ha)			_				-	RATIONAL DI		-									SEWER DATA	1								
EET	AREA ID	FROM	TO		C= C=					TIME	TOTAL		i (10)			10yr PEAK					LENGTH		PIPE SIZE (mn	n)	SLOPE	VELOCITY	AVAIL	CAP (5yr)	surcharged	upstream	HGL*	FF**	Free
		МН	MH	0.20	0.70 0.75	0.90	2.78AC	2.78AC	(min)	IN PIPE	(min)	(mm/hr)	(mm/hr)	(mm/hr)	FLOW (L/s)	FLOW (L/s)	FLOW (L/s)	FLOW (L/s)	FLOW (L/s)	(L/s)	(m)	DIA	W	Н	(%)	(m/s)		(%)	pipe	obvert	m	m	
	2224	CDBALL222A	CDMUIDIO			0.00	0.22	0.22	10.00	0.24	10.21	104.10	122.14	470.56	22.46				22.46	242.00	40.40												
	233A 233B	CBMH233A CBMH233	CBMH233 CBMH232					0.23	10.00	0.31	10.31	104.19	122.14	178.56 175.81	23.46 61.61	-			23.46	248.09	15.60	600	-		0.15	0.850		90.54%	(
	2330	CBIVITIZSS	CBIVIPIZSZ			0.15	0.38	0.60	10.31	0.67	10.98	102.60	120.27	1/5.81	61.61	<u> </u>			61.61	248.09	34.20	600			0.15	0.850	186.48	75.17%					
	232A	CBMH232A	CBMH232			0.10	0.25	0.25	10.00	0.31	10:31	104.19	122.14	178.56	26.07				26.07	248.09	15.60	600			0.15	0.850	222.02	89.49%					
	2328	CBMH232	CBMH231			0.12	0.30	1.15	10.98	0.67	11.65	99.30	116.38	170.10	114.29				114.29	248.09	34.20	600			0.15	0.850	133.80	53.93%					
	231A	CBMH231A	CBMH231			0.11	0.28	0.28	10.00	0.31	10.31	104.19	122 14	178.56	28.68	-			28.68	248.09	15.60	600			0.15	0.850	210.44	20.4404					
	2310	CDIVINIZGIA	Commercia			0.11	0.20	U.E.O.	10.00	0.51	50000	104.13	122.24	170.50	20.00				20.00	240.03	15.00	800			0.15	0.850	219.41	88.44%					
	231B	CBMH231	MH230			0.11	0.28	1.70	11.65	0.47	12.12	96.23	112.76	164.79	163.72				163.72	248.09	24.08	600			0.15	0.850	84.37	34.01%					
	230A 230B	CICB230A CICB230B	CICB230B MH230					0.15		0.11	10.11	104.19		178.56 177.56	15.64 49.26				15.64	62.04	8.04	250			1.00	1.224	-	74.79%					
	2300	CICB230B	WIHZ3U			0.13	0.33	U.45	10.11	0.06	10.17	103.62	121.47	1//.36	49.26				49.26	87.74	5.93	250			2.00	1.731	38.48	43.86%					
	230C	CB230C	MAIN			0.03	0.08	0.08	10.00	0.14	10.14	104.19	122.14	178.56	7.82				7.82	62.04	10.39	250			1.00	1,224	54.22	87.39%					
	230D	CB230D	CB230E					0.10	10.00	0.11	10.11			178.56	10.43				10.43	62.04	7.95	250			1.00	1.224	51.61						
	230E	CB230E	MAIN			0.09	0.23	0.33	10.11	0.05	10.16	103.62	121.47	177.58	33.70				33.70	87.74	4.91	250			2.00	1.731	54.03	61.58%					
	230F	CB230F	MAIN			0.07	0.18	0.18	10.00	0.17	10.17	104.19	122.14	178.56	18.25				18.25	62.04	12.50	250			1.00	1.224	43.79	70.59%					
																											10113	70.55%					
	230G	CB230G	CB230H					0.25	10.00	0.11	10.11								26.07	62.04	8.00	250			1.00	1.224	35.97	57.98%					
	230H	CB230H	MAIN			0.07	0.18	0.43	10.11	0.05	10.15	103.62	121.47	177.57	44.07				44.07	87.74	4.78	250			2.00	1.731	43.66	49.77%					
	2301	CB230I	MAIN			0.03	0.08	0.08	10.00	0.12	10.12	104.19	122.14	178.56	7.82				7.82	62.04	8.57	250		-	1.00	1.224	54 22	87.39%					
								1		7,355				-13100					7.02	02.01	0.51	250			1.00	1,224	37.22	07.33%					
	[Self	MH230	MH210				0.00	3.25	12.12	1.62	13.74	94.19	110.36	161.26	306.36				306.36	449.81	95.70	750			0.15	0.986	143.45	31.89%	no	95.70	95.70		
	221A	CD221A	CBMH221			0.15	0.40	0.40	10.00	0.11	10.44	104.10	122.14	170 50	41.71				44.74	420.52	47.05	450											
	221A	CB221A	COMPLET			0.16	0.40	0.40	10.00	0.11	10.11	104.19	122.14	178.56	41.71				41.71	420.63	17.05	450			2.00	2.562	378.92	90.08%					
	221B	CB221B	CB221C			0.03	0.08	0.08	10.00	0.16	10.16	104.19	122.14	178.56	7.82				7.82	297.43	17.05	450			1.00	1.812	289.61	97.37%					
	221C	CB221C	C8MH221					0.13	10.16	0.09	10.24	103.37	121.17	177.14	12.93				12.93	488.73		450			2.70	2.977	475.80	97.35%					
	2210	COLUMN	A11/22/2			0.00	0.25	10.00	10.04	0.57	10.01	402.00	120.65	476.76	74.50				74.60	200.45													
	221D	CBMH221	MH221			0.08	0.20	0.73	10.24	0.57	10.81	102.92	120.65	176.36	74.68			_	74.68	286.47	33.38	600	-		0.20	0.982	211.79	73.93%			- 1		
	BLK400	BLK400	MAIN			0.15	0.38	0.38	10.00	0.07	10.07	104.19	122.14	178.56	39.10				39.10	62.04	5.00	250			1.00	1.224	22.94	36.97%			96.03	99.50	_
																												55.57,0			30.03	33,30	_
	BLK300	BLK300	MAIN			0.04	0.10	0.10	10.00	0.07	10.07	104.19	122.14	178.56	10.43				10.43	62.04	5.00	250			1.00	1.224	51.61	83.19%			96.03	99.50	
_		MH500	MH221			0.00	0.00	0.00	10.00	0.20	10.20	104.19	122.14	178.56	0.00				0.00	900.87	12.00	1050			0.10	1.000	000.0=	400 000					
		14111300	MILES			0.00	0.00	WHOM	10.00	0.20	40.44	104.13	144.14	170.30	0.00		-		0.00	200.07	12.00	1020			0.10	1.008	900.87	100.00%			1		
		MH221	MH220				0.00	1.20	10.61	1.40	12.21	100.10	117.32	171.47	120.21				120.21	148.72	75.90	450			0.25	0.906	28.50	19.17%	no	96.03	96.03		
																											13117.55						
	222A	CB222	CBMH222					0.13		0.12	10.12	104.19	-		13.03				13.03	107.45	14.80	250			3.00	2.121		87.87%			- 1		
	222B	CBMH222	MH220			0.07	0.18	0.30	10.12	0.07	10.19	103.58	121.42	177.50	31.10				31.10	151.96	12.64	250			6.00	2.999	120.86	79.53%					



STORM SEWER DESIGN SHEET

PROJECT: Arcadia Commercial
LOCATION: CITY OF OTTAWA

CLIENT: Minto Development Group

*HGL at obvert of pipe if pipe is not surcharged

** Finished floor for slab on grade commercial building

***Freeboard is from upstream MH HGL to FF

	LOCATION				AR	EA (Ha)	.01							RATIONAL D	ESIGN FLOW										SEWER DATA	1				7	is from upstrea	am win not to	rr	
STREET	AREA ID	FROM MH	TO MH	C= 0.20					CUM 2.78AC	INLET (min)	TIME IN PIPE	TOTAL (min)	(5) (mm/hr)	i (10) (mm/hr)	i (100) (mm/hr)	5yr PEAK FLOW (L/s)	10yr PEAK FLOW (L/s)	100yr PEAK FLOW (L/s)	ICD FIXED FLOW (L/s)	DESIGN FLOW (L/s)	CAPACITY [L/s]	LENGTH (m)	DIA	PIPE SIZE (mn	ROLLAND PARTITION	SLOPE (%)	VELOCITY (m/s)	AVAIL (L/s)	CAP (5yr) (%)	surcharged	upstream obvert	HGL*	FF**	Freeboard**
																										1707	1117.37	10/3/	(70)	pipe	obvert	m	 	m
	223A	CB223	CBMH223						0.38	10.00	0.21	10.21	104.19	122.14	178.56	39.10				39.10	446.15	34.20	450			2.25	2.718	407.05	91.24%					
	223B	CBMH223	MH220			+	0.12	0.30	0.68	10.21	0.27	10.47	103.10	120.85	176.66	69.65				69.65	210.32	20.38	450			0.50	1.281	140.67	66.88%					
	9	MH220	MH212					0.00	2.18	12.21	0.44	12.65	93.82	109.93	160.62	204.22				204.22	248.09	22.60	600			0.15	0.850	43.86	17.68%	no	95.84	95.84	1	
																											0.000	45.00	1710070		33.04	33.04		
	212A 212B	CICB212A CICB212B	CICB212B MH212	-	-	-			0.08	10.00	0.12	10.12	104.19			7.82				7.82	62.04		250			1.00	1.224	54.22	87.39%					
	2128	CICBZIZB	MILETE			1	0.03	0.08	0.35	10.12	0.06	10.18	103.58	121.42	177.49	15.55				15.55	151.96	11.24	250			6.00	2.999	136.41	89.77%				1	
	215	CB215	MH215				0.04	0.10	0.10	10.00	0.17	10.17	104.19	122.14	178.56	10.43				10.43	62.04	12.57	250			1.00	1.224	51.61	83.19%	1			ł	
	BLK100	BLK100	MAIN		-	+	0.06	0.15	0.15	10.00	0.07	10.07	104.19	122.14	178.56	15.64				45.54	52.04									1				
	BERTOO	BERTOO	IXIMIX				0.00	0.13	0:43	10.00	0.07	40.01	104.13	122.14	1/8.36	15.04				15.64	62.04	5.50	250			1.00	1.224	46.40	74.79%	-		97.23	99.60	2.37
		MH215	MH214					0.00	0.25	10.17	0.40	10,57	103.30	121.09	177.01	25.85				25.85	82.07	38.95	250			1.75	1.620	56.22	68.51%	no	97.23	97.23		
	216A	RYCB216	CB216	0.03	1-	1		0.03	0.02	10.00	0.05	10.05	104.10	122.14	130 50	4.74				4	40:00											_		
	216B	CB216	MH216	0.03	+		0.04		0.12	10.00	0.05	10.05	104.19			1.74 12.17				1.74	124.08		250			4.00	2.449	122.34	98.60%					
		COZIO	MATERIAL			1	0.04	0.10	UIAE	10.00	0.04	10,04	104.13	144.14	178.30	12.17				12.17	138.72	5.90	250			5.00	2.738	126.56	91.23%					
		MH216	MH214					0.00	0.12	10.05	0.47	10,52	103.93	121.83	178.10	12.13				12.13	43.87	24.56	250			0.50	0.866	31.73	72.34%	no	97.07	97.07	I	
	BLK200	BLK200	MAIN		-	+	0.04	0.10	0.30	10.00	0.07	10.07	104.19	122,14	178.56	10.43		ļ		10.43	62.04	E 40	350			4.00	4.844		202002200					
	52(1200	DENEGO	Michigan		1		0.04	0.10	MAN	10.00	0.07	- AMERICA	104.13	122,14	170.30	10.43				10.43	62.04	5.40	250			1.00	1.224	51.61	83.19%			96.55	99.55	3.00
		WHSZ4	MH213		1			0.00	0.47	10.57	0.40	10.97	101.27	118.69	173.49	47.30				47.30	129.34	27.00	375			0.50	1.134	82.04	63.43%	no	96.55	96.55	1	
	*	MH213	WHSTS	-	-	-		0.00	0,47	10.97	0.26	11.23	99.34	116.43	170.16	46.40				46.40	129.34	17.80	375			0.50	1.134	82.94	64.13%	no	96.39	96.39	l	
		MH212	WH210					0.00	2.79	N 41/23	0.86	17.09	98.12	114.98	168.05	274.12				274.12	350.85	61.94	600			0.30	1.202	76.72	21.87%	no no	95.74	95.74	l	
	210A	CB210A	MAIN		1	+	0.12	0.30	0.30	10.00	0.00	40 00	104.10	122.14	170.55	24.20														1	33174	33.74	ĺ	
	2104	CBZIUA	mala		1		0.12	0.30	10.90	10.00	0.09	10.09	104.19	122.14	178.56	31.28				31.28	201.76	15.06	300			4.00	2.765	170.48	84.50%	-				
	BLK900	BLK900	MAIN		1		0.46	1.15	1.35	10.00	0.21	10.21	104.19	122.14	178.56	119.92				119.92	182.91	19.94	375			1.00	1.604	62.99	34.44%			95.56	98.10	2.54
DEPRESSED LOADING	210B	CB210B	MAN		-		0.02	0.05	0.05	10.00	0.29	10.29	104.19	122.14	178.56	5.21				5.21	43.87	14.90	250			0.50	0.866	20.65	00.4404					
																5.22				3.21	43.67	14.30	230			0.50	0.800	38.65	88.11%	}				
		MH210	MH205B	-	-	-		0.00	7.55	11.74	0.41	14.15	87.88	102.93	150.35	663.26				663.26	905.48	28.86	975			0.15	1.175	242.23	26.75%	no	95.56	95.56		
	206E	CICB206D	MAIN			0.09		0.19	0.19	10.00	0.02	10.02	104.19	122.14	178.56	19.55				19.55	87.74	2.57	250			2.00	1.731	68.18	77.72%					
		MH205B	THE PROPERTY OF					0.00		110000																			1,1,1,1,1					
		MHZUSB	MH205				1	0.00	2.14	18,35	0.20	I MAE	86.42	101.22	147.84	668.51				668.51	905.48	13,88	975			0.15	1.175	236.97	26.17%	no	95.50	95.50		
	206A	CB206A	CBMH206						0.60		0.17	10.17		122.14	178.56	62.57				62.57	420.63	25.66	450			2.00	2.562	358.07	85.13%					
	206B	CBMH206	MH205			-	0.14	0.35	0.95	10.17	0.26	10,43	103.32	121.11	177.05	98.23				98.23	210.32	19.99	450			0.50	1.281	112.09	53.29%					
	206C	CB206B	MAIN				0.07	0.18	0.18	10.00	0.08	10.08	104.19	122.14	178.56	18.25				18.25	85.29	8.49	250			1.89	1.683	67.04	78.60%					
	206D	CB206C	MAIN					0.10		10.00	0.02	10.02	104.19	122.14	178.56	10.43				10.43	87.74		250			2.00	1.731	77.31	88.11%					
		MH206	7MH205		-			0.00	2.32	10.43	0.59	11:07	101.99	110 55	174.75	135.04				425.04	403.04													
		PHILIPSON	(timest)					tr.ta)	1169	.20,43	0.39	11.0%	101.99	119.55	174.75	125.04				125.04	182.91	56.62	375			1.00	1.604	57.87	31.64%	no	96.05	96.05		
external South	EXT-2	STUB	7614205		2.82			5.49	5.49	12.00	0.17	22,17	94.70	110.96	162.13	519.66				519.66	986.85	11.55	1050			0.12	1.104	467.19	47.34%	по	95.50	95.50		
																																22.22		



STORM SEWER DESIGN SHEET

PROJECT: Arcadia Commercial LOCATION: CITY OF OTTAWA

CLIENT: Minto Development Group *HGL at obvert of pipe if pipe

*HGL at obvert of pipe if pipe is not surcharged

** Finished floor for slab on grade commercial building

i mistico moor	to, aidb	On Brace	committercial	Dullull
***Freeboard is t	from up	stream M	H HGL to FF	

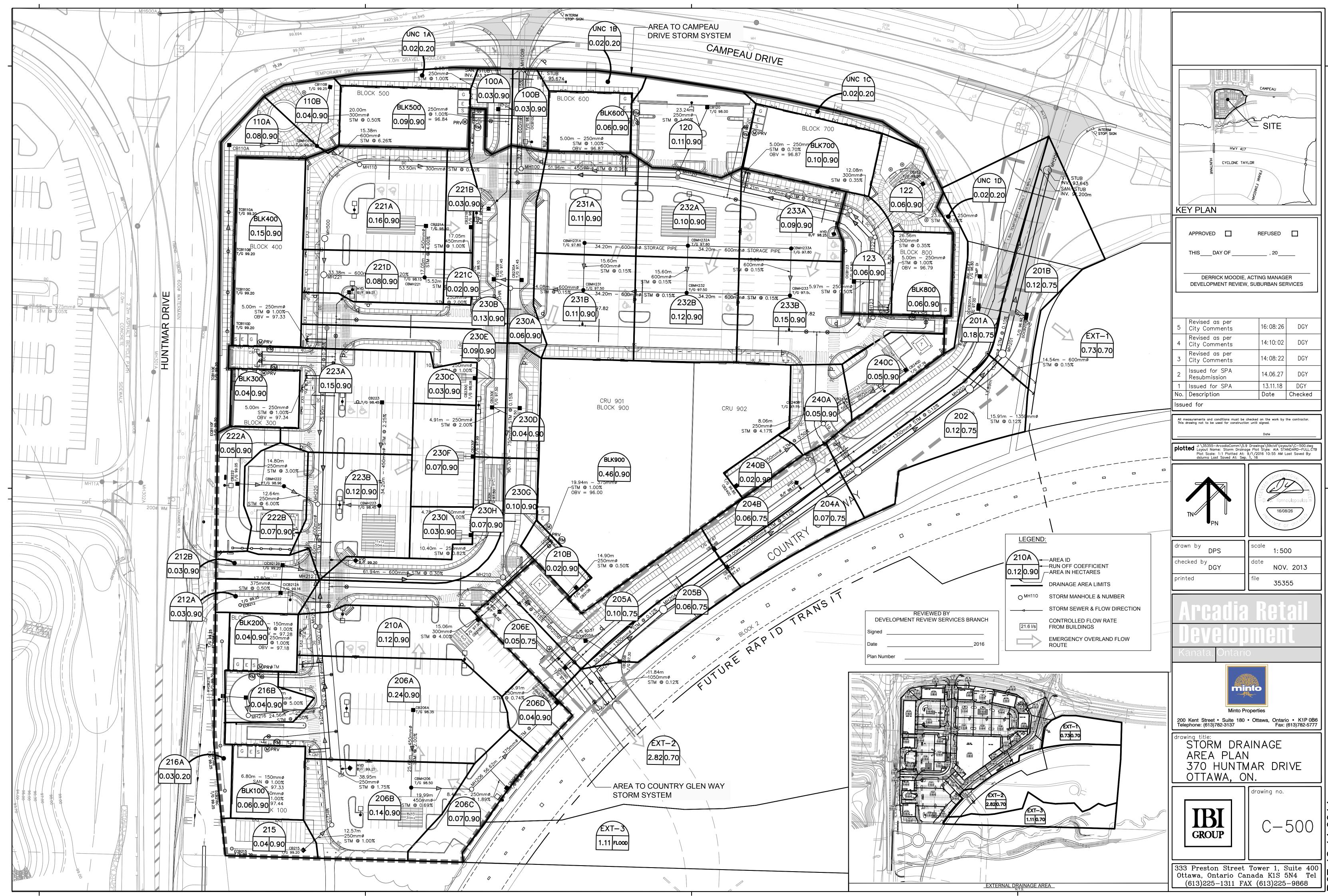
	LOCATION				AREA									RATIONAL DE		ri e						-			SEWER DAT									
STREET	AREA ID	FROM	то	C=	C=		C=	IND	CUM	INLET	TIME	TOTAL	1 (5)	i (10)	i (100)			100yr PEAK				LENGTH		PIPE SIZE (mm	A		VELOCITY		CAP (5yr)		upstream		FF**	Freeboa
JINGET	AIRENTO	MH	MH	0.20	0.70		0.90		2.78AC	(min)	IN PIPE	(min)	(mm/hr)	(mm/hr)	(mm/hr)	the sales	FLOW (L/s)	FLOW (L/s)	FLOW (L/s)		(L/s)	(m)	DIA	W	Н	[%]	(m/s)	(L/s)	(%)	pīpe	obvert	m	m	n
	205A	CICB205A	CICB205B			0.10			0.21	10.00	0.16	10.16	104.19	122.14	178.56	21.72				21.72	62.04	11.97	250			1.00	1.224	40.31	64.98%					
	205B	CICB205B	MAIN			0.06	_	0.13	0.33	10.00	0.01	10.01	104.19	122.14	178.56	34.76				34.76	87.74	0.64	250			2.00	1.731	52.98	60.38%					
						_		200			0.39	14.73	85.74	100.42	146.67	1,267.51				1.267.51	1,928.87	30.36	1350			0.12	1 205	661.36	24 2004		05.40	05.40		
treet 1	940	M19205	MH204			_	_	0.00	14.78	10:34	0.39	14:73	85,74	100.42	140.07	1,207.31		-		1,207.31	1,928.67	30.36	1350	 		0,12	1.305	661.36	34.29%	no	95.48	95.48		
treet 1	204B	CICB204B	CICB204A			0.06	_	0.13	0.13	10.00	0.12	10.12	104.19	122.14	178.56	13.03				13.03	62.04	9.00	250			1.00	1.224	49.00	78.99%	ŀ				
treet 1	204A	CICB204A	MAIN			0.07	\neg		0.27		0.02	10.14	103.55	121.38	177.45	28.07				28.07	87.74	2.34	250			2.00	1.731	59.67	68.01%					
			3340000																											i				
		MH204	MH203					0.00	15.05	14.73	1.01	15.74	84.44	98.89	144.42	1,271.12				1,271.12	1,928.87	79.00	1350			0.12	1.305	657.75	34.10%	no	95.43	95.43		
	240A	CICB240A	CICB240B						0.00	10.00	0.14	10.14	104.19	122.14	178.56	0.00				0.00	62.04	10.23	250			1.00	1.224	62.04	100.00%					
		CICB240B	MHZ40	_			0.05	0.13	0.13	10.14	0.16	10.30	103.46	121.28	177.30	12.94				12.94	87.74	16.81	250			2.00	1.731	74.79	85.25%	ł.				
	****	000400		_			0.00	0.05	0.00	10.00	0.00	10.50	104.19	122.14	178.56	5.21				5.21	43.87	35.30	250	-		0.50	0.866	20 CF	00.410/					
EPRESSED LOADING	240B	CB240C	MH240			-	0.02	0.05	0.05	10.00	0.68	10.68	104,19	122.14	1/0.30	3.21				5.21	43.07	33.30	230			0.50	0.800	38.65	88.11%					
	240C	CB240D	MH240				0.05	0.13	0.13	10.00	0.44	10.44	104.19	122.14	178.56	13.03				13.03	62.04	32,56	250			1.00	1.224	49.00	78.99%					
	2400	CDZ-40D	ATTICAL				UIUS	0125	10140	20100																			10.00%					
	·	MH240	WH203					0.00	0.30	10.68	0.37	11.05	100.74	118.07	172.58	30.24				30.24	63.80	19.34	300			0.40	0.874	33.56	52.60%	no	95.39	95.39		
treet 1	7.00	MH203	MH202						15.35	15.74	0.59	16.32	81.24	95.13	138.90	1,247.42				1,247.42	1,928.87	45.86	1350			0.12	1,305	681.46	35.33%	no	95.31	95.31		
treet 1		MH202	MH201				_	0.00	15.35	16.32	0.20	16.53	79.51	93.09	135,91	1,220.78		-		1,220.78	1,928.87	15.91	1350			0.12	1.305	708.09	36.71%	по	95.23	95.23		
				0.00		0.40	\rightarrow	0.00	0.20	12.00	0.70	12.20	94.70	110.96	162.13	36.59				36.59	62.04	14.74	250			1.00	1 224	25.45	41.020/					
treet 1	201A 201B, 202	DCICB201A DCICB201B	DCICB201B MAIN	0.02		0.18	\rightarrow		0.39	12.00 12.00	0.20	12.20 12.03	94.70	110.96	162.13	83.98				83.98	87.74	3.43	250			2.00	1.224	25.45 3.76	41.02%					
rreet 1	2018, 202	DCICB201B	MAIN	-		0.24		0.50	Uibb	12.00	0.03	12.05	34.70	110.30	102.13	03.50				05.50	07.74	3.43	230			2.00	1.731	3.70	4.20%					
kternal East	EXT-1	CAP	MH201		0.73			1,42	1.42	10.00	0.29	10.29	104.19	122.14	178.56	148.01				148.01	248.09	14.54	600			0.15	0.850	100.07	40,34%	no	95.23	95.23		
					377.5																													
reet 1		MH201	CAP					0.00	17.66	16.53	0.82	17.34	78.93	92.41	134.90	1,393.95				1,393.95	2,332.02	62.55	1500			0.10	1.278	938.07	40.23%	no	95.21	95.21		
reet 1	existing	Ex CAP	EXMH303					0.00	17.66	17.34	0.32	17.66	76.68	89.77	131.03	1,354.27				1,354.27	2,332.02	24.50	1500			0.10	1.278	977.75	41.93%	no				
				0.05	3.55	0.80	3.62	17.66	TRUE																					по	95.17	95.088		
							_											_																
				_	AREA C		0.00											_																
					EXTERNA	LAREA		_	-									1											_					
					EXTERINA	-	4.47																											
		-				-	7177																											
efinitions:				Notes:		_			-	Designed:		RM			No.			15.27		Revision			THE ST		1100		Date	STUATE	0					
) = 2.78CiA, where:					nings coef	ficient (n)) =			_					1.				Iss	ued for SPA							11/15/2013							
a = Peak Flow in Litres pe	er Second (L/s)				-										2					er City Comi							6/27/2014							
= Area in Hectares (Ha)										Checked:		DY			3					er City Com							8/22/2014							
= Rainfall intensity in m																			Revised p	er City Com	ments						10/2/2014							
[i = 998.071 / (TC+6.05		5 YEAR								6																								
[i = 1174.184 / (TC+6.0		10 YEAR								Dwg. Refere	ence:	31855-500			NAME OF STREET	File Defeater	Darbeit See		Total Section	10-0	Detai	EASTAN SECTION	V-10-4-10-10-10-1	III OF SHIP	1 march 1 m		Chant No.							
[i = 1735.688 / (TC+6.0	14)^0.820]	100 YEAR														File Reference 31855.5.7.1					Date: 11/15/2013			- C. C. C.			Sheet No: 3 of 3		250					

Outlet # 2 (MH301) SUMMARY

Outlet # 4 (Miliout) Committee	
Total Flow from Roofs=	8.00 l/s
Total Roof Area =	0.310 Ha
Average roof flow =	25.81 l/s/Ha
Volume Stored on Roofs	149.34 cm
Total Roof Storage rate	481.73 cm/Ha
Total flow from parking lot =	110.00 l/s
Total parking Lot area =	0.410 Ha
Average parking lot flow =	268.29 I/s/Ha
Volume Stored on Parking lot	80.59 cm
Total Parking lot Storage rate	196.56 cm/Ha
Total uncontrolled flow from site	7.94 l/s
Total uncontrolled area	0.080 Ha
Total flow	125.94 l/s
Total area	0.80 Ha
Average flow	157.43 I/s/Ha
Volume Stored	229.93 cm
Total Storage rate	287.41 cm/Ha

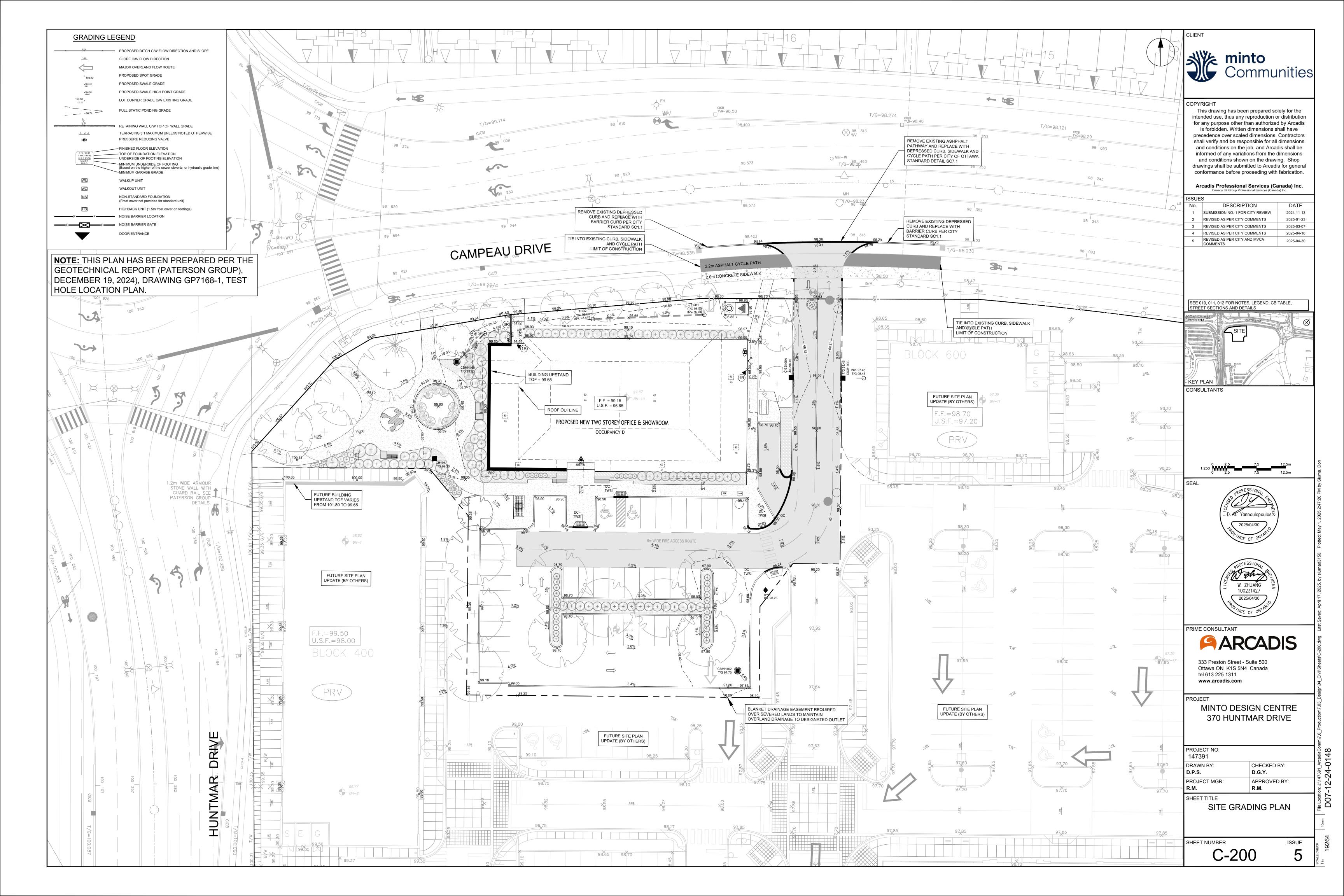
Outlet # 1 & 2 SUMMARY

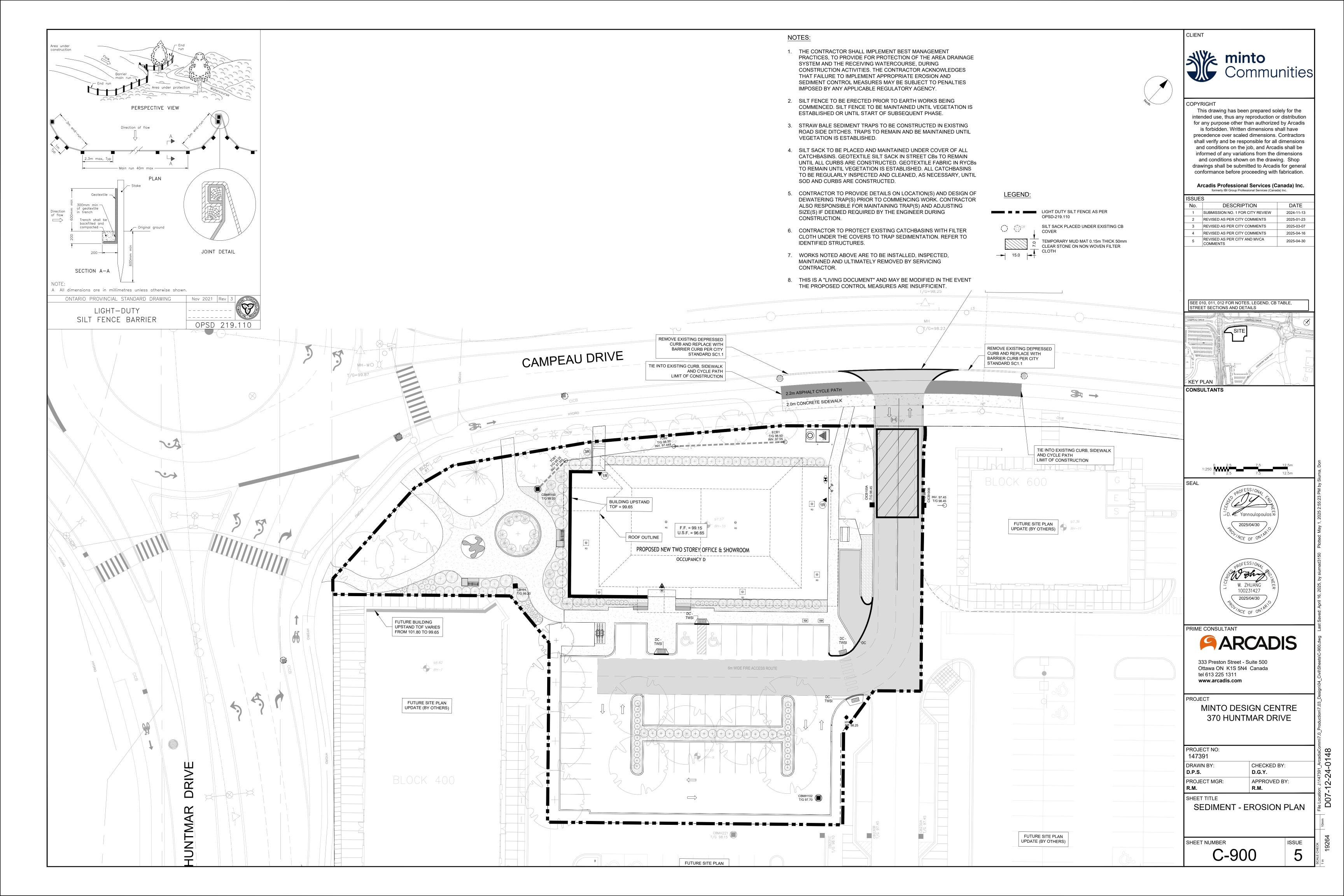
Outlet # 1 & 2 SUMMARY		
Total Flow from Roofs=	26.00	l/s
Total Roof Area =	1.06	На
Average roof flow =	24.53	I/s/Ha
Volume Stored on Roofs	516.49	cm
Total Roof Storage rate	487.25	cm/Ha
Total flow from parking lot =	1116.00	l/s
Total parking Lot area =	3.83	На
Average parking lot flow =	291.38	l/s/Ha
Volume Stored on Parking lot	895.67	cm
Total Parking lot Storage rate	233.86	cm/Ha
Total uncontrolled flow from site	46.66	l/s
Total uncontrolled area	0.190	На
Total flow	1188.66	l/s
Total area	5.080	На
Average flow	233.99	I/s/Ha
Volume Stored	1412.16	cm
Total Storage rate	277.98	cm/Ha

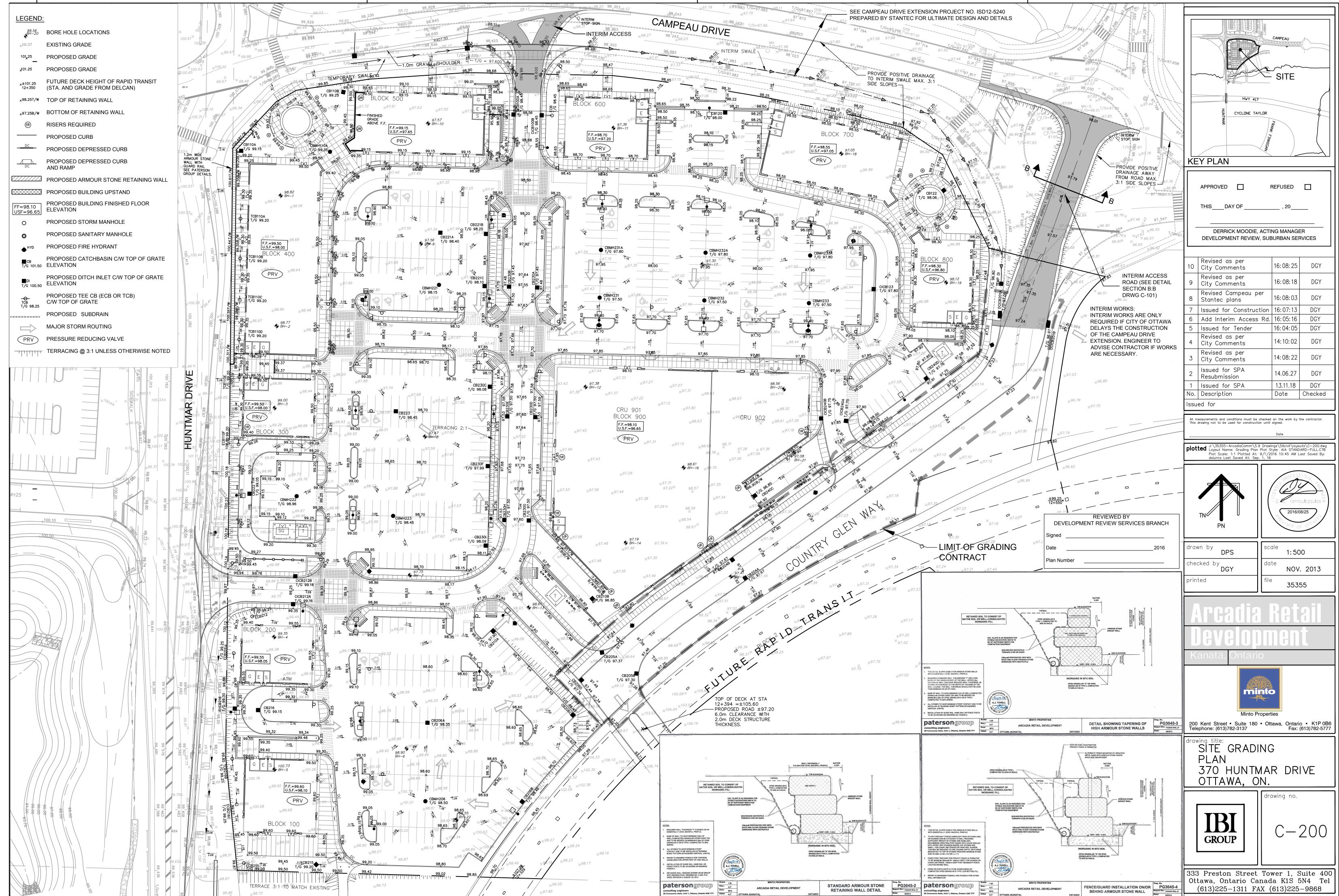


Appendix E

- Grading Plan 147391-C-200
- Erosion and Sediment Control Plan 147391-C-900
- Grading Plan 35355-C-200







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