

MEMORANDUM

DATE: JULY 28, 2023
TO: ABI DIEME (CITY OF OTTAWA)
FROM: DREW BLAIR
RE: 5000 ROBERT GRANT AVENUE
SITE SERVICING – MULTIPLE SERVICE CONNECTIONS
PRECON #: PC2023-0046
NOVATECH #: 117151
CC: F. LEPINE, A. LALONDE (LEPINE), A. WENDZICH (NEUF), S. EZZIO (CITY)

Novatech has been retained to prepare a site servicing and stormwater management report to support the site plan application for the property located at 5000 Robert Grant Avenue within the City of Ottawa. The subject site is a vacant lot with a total site area of approximately 2.02 hectares. The site plan application proposes three new residential mid to high-rise towers (ranging between 4 and 18-stories) to be built on top of a single common podium structure for the on-site underground parking. The proposed site entrance off Robert Grant Avenue will provide access to all buildings at the ground level as well as access to the underground parking structure via a ramp near the south-west corner of the site. The Livery Street site entrance will provide access to the underground parking garage only and is to be located near the south-east corner of the subject site.

This technical memorandum is being submitted in support of the site plan application process for the justification of multiple service connections to the adjacent municipal infrastructure. The City of Ottawa previously identified that multiple sanitary and storm outlet sewers are available for connecting the proposed site servicing. While the City typically allows one sanitary and one storm sewer connection per property, it was stated in the pre-consultation meeting that multiple servicing connections may be permitted on a case-by-case basis.

Multiple Sanitary Service Outlets

As part of the Fernbank Crossing Subdivision, the original concept for the subject site was to develop the lands as a commercial/mixed use residential area. A 250mm diameter sanitary service stub connected to Livery Street was installed as part of the Fernbank Crossing Subdivision works near the north-east corner of the site. The approved design flow from the subject site to the existing Livery Street sanitary sewer was approximately 3.3 L/s via the existing 250mm service stub. Refer to the sanitary sewer design sheet and drainage area plan in **Appendix A** for details of the approved sanitary site flows and sewer pipe capacities in the downstream system along Livery Street in Fernbank Crossing. The site was Block 203 (labelled as Area A4-3) in the Fernbank Crossing drainage area plan and design sheet.

The current site development proposal contains high density residential buildings with anticipated sanitary flows greater than originally accounted for in the downstream Livery Street sanitary sewer

system. Peak sanitary flows for the entire site will be in the order of 10.8 L/s and are summarized in **Table 1** below:

Table 1: Proposed Sanitary Peak Flow Summary

Proposed Use	Unit Count / Area	Peaking Factor ⁽¹⁾	Peak Design Flow (L/s)
Building A			
Residential Tower	113	3.52	2.32
Extraneous Infiltration (ha)	0.68	-	0.22
Building A	-	-	2.5
Building B			
Residential Tower	153	3.47	3.11
Extraneous Infiltration (ha)	0.67	-	0.22
Building B	-	-	3.3
Building C			
Residential Tower	238	3.41	4.74
Commercial/Retail Space (m ²)	157	1.5	0.01
Extraneous Infiltration (ha)	0.67	-	0.22
Building C	-	-	5.0
Site Totals	504 / 157	-	10.8

⁽¹⁾ Peaking Factor for industrial and commercial areas as per Section 3.2.1

Refer to the sanitary design sheets in **Appendix A** for details of the theoretical site flows generated by the full site development.

Upon review of the downstream sanitary sewers, it is noted that there is one section of sewer within the Westpark Phase 1 sanitary sewer system that is near capacity. The sanitary sewer design sheet for the Westpark Phase 1 development, prepared by IBI, indicates that the existing 375mm diameter sewer on Oxford Place (between MH 103A and MH 202A) is currently operating at 92% with 6.57 L/s of available capacity. This sewer is downstream of Livery Street in Fernbank Crossing and is shown on the IBI West Park General Plan of Services provided in **Appendix A**.

The proposed site will generate sanitary flows greater than the original design flows (10.8 L/s versus 3.3 L/s), and as noted above, there are capacity limitations in the downstream sanitary sewer within the Westpark Phase 1 development, so it would be beneficial to split post-development sanitary flows between two separate sanitary service outlets.

As indicated in the pre-consultation meeting with the City, there is an existing 250mm diameter PVC sanitary sewer accessible in the Robert Grant Avenue right-of-way (ROW). The existing 250mm diameter PVC sanitary sewer in the Robert Grant Avenue ROW outlets directly to the municipal 750mm diameter Stittsville sanitary trunk sewer on the north side of the hydro corridor. This segment of the 250mm diameter sewer was constructed at a slope of 0.35% and has an approximate capacity of 36.7 L/s. The theoretical sanitary flow from the upstream tributary area (including the future residential build-out area) is approximately 14.5 L/s, leaving approximately 22.2 L/s of available flow capacity in the pipe segment downstream of the subject site. Refer to **Appendix A** for details of the anticipated off-site flows and sewer pipe capacities in the downstream system along Robert Grant Avenue.

In the post-development condition, the subject site may be serviced by the 250mm diameter sanitary sewer in the Robert Grant Avenue ROW with the anticipated peak sanitary flow of 8.3 L/s from Towers 'B' and 'C'. The remaining 2.5 L/s of sanitary flow from Tower 'A' will outlet to the existing sanitary servicing stub on Livery Street. The sanitary flow to Livery Street will be less than the approved allowable release rate and the available capacity in the municipal system.

The internal mechanical plumbing will benefit from splitting flows to reduce the lengths and sizes of the internal runs and still be able to service all of the residential units through the use of gravity sewers. Reducing or avoiding pumping sanitary flows will increase the reliability and the safety of the system for the long-term maintenance of the system.

It is proposed to split flows and utilize the available downstream sewer capacities of both the Livery Street and Robert Grant Avenue municipal sanitary sewer systems with the additional sanitary connection (i.e.: two (2) sanitary connections in total for this site).

Multiple Storm Service Outlets

The Fernbank Crossing Subdivision design proposed a storm service from the subject site to outlet to the existing 1200mm/1350mm diameter concrete storm trunk sewer within the on-site City easement along the north side of the site. The approved design included approximately 440 L/s from the subject site outletting to the 1200mm/1350mm diameter storm sewer segments which drains to Pond 6 providing quality control of stormwater for a portion of the Fernbank Crossing Subdivision. The site's allowable release rate, as defined in the pre-consultation notes from the City, is significantly less than the modelled system capacity and has been calculated to be 353 L/s.

Under post-development conditions, it is proposed that stormwater from the majority of the site will be controlled using two (2) internal storage tanks. One internal tank will outlet to the existing maintenance hole on the 1350mm storm trunk sewer next to the north-east corner of Building A. The second internal tank will outlet to the existing maintenance hole on the 1200mm storm trunk sewer located midway within the easement along the northern edge of the site.

The proposed development will require some direct runoff towards the municipal ROW's and the hydro corridor in order to match the existing elevations surrounding the site. The actual flows directed to the municipal storm sewer system will be significantly less than the allowable (approximately 165 L/s outlet from the internal storage tanks to the 1200mm/1350mm storm trunk sewer system).

To protect the south building façade from off-site drainage that currently slopes towards the subject site and self-contain stormwater within the site area, a diversion berm is proposed to direct off-site stormwater runoff to the existing catchbasin near the south-east property corner (as intended in the approved Fernbank Crossing design for stormwater flowing from the adjacent site). The on-site diversion berm and swale will protect the building from flooding and provide storage for the controlled stormwater flows prior to outletting to the proposed additional storm connection to the local 375mm diameter storm sewer on Livery Street. These external storm flows and a portion of the access ramp to the underground parking garage would need to be taken internally into the building (which is not desirable or encouraged) to outlet on the east side of the site on Livery Street. The existing 375mm diameter storm sewer in Livery Street is currently operating at 65% with approximately 35 L/s of available capacity. Therefore, it is proposed to have a small portion of the post-development storm flows outlet separately from the main building services to the additional Livery Street storm sewer connection. Refer to **Appendix B** for details of the sewer pipe capacities in the downstream storm sewer system along Livery Street.

The internal mechanical plumbing will benefit from splitting flows and having three (3) storm service connections to the municipal system to reduce the lengths and sizes of the internal runs as intake of exterior storm flow to be conveyed and stored is reduced. Reducing the pumping of stormwater will increase the reliability and the safety of the system for the long-term maintenance of the system.

It is proposed to split flows and utilize the available downstream sewer capacities of both the 1200mm/1350mm storm trunk sewer along the north side of the site and the Livery Street municipal storm sewer system with the additional storm service connections (i.e.: three (3) storm service connections in total for this site).

Conclusion

In order to meet the allowable release rates and available downstream capacities in the municipal sanitary and storm sewer systems, it is proposed to service the subject site with more than one each for the sanitary and storm service connections. Multiple sanitary and storm service outlets for the proposed development at 5000 Robert Grant Avenue will provide a beneficial design in the follow aspects:

- Splitting sanitary flows to meet existing downstream sewer capacities in the municipal systems.
- Reduction of the length and sizes of internal sanitary and storm plumbing to increase reliability and safety of the internal systems.
- Allows the internal sanitary and storm plumbing systems to maximize gravity servicing of the large podium and multiple towers while minimizing the amount of pumping required.

We trust this justifies the site requirements for multiple sanitary and storm connections to service the proposed development. Should you have any questions or require additional information, please contact the undersigned.

Yours truly,

NOVATECH



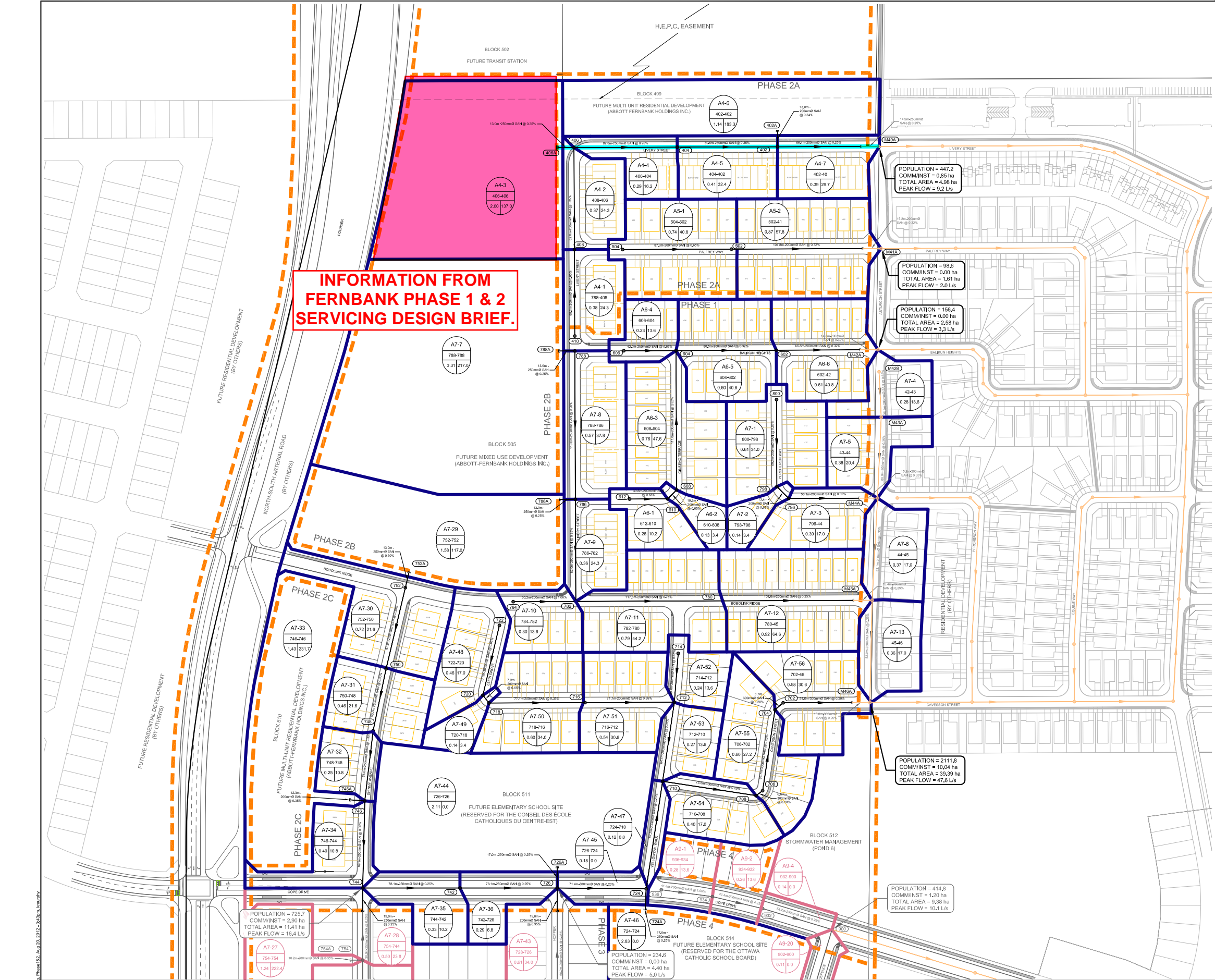
Drew Blair, P. Eng.
Senior Project Manager

List of Appendices:

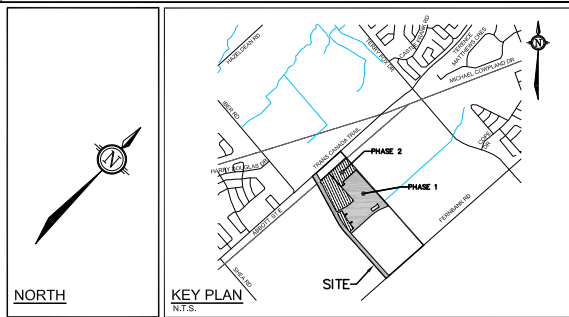
Appendix A: Sanitary Flow Calculations and Sewer Capacities
Appendix B: Storm Drainage Areas and Sewer Capacities
Appendix C: Proposed Servicing Sketch

APPENDIX A

Sanitary Flow Calculations and Sewer Capacities



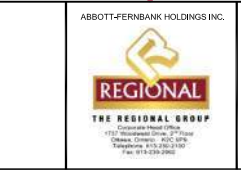
INFORMATION FROM FERNBANK PHASE 1 & 2 SERVICING DESIGN BRIEF.



LEGEND

	AREA ID		FUTURE AREA ID
	MANHOLE TO MANHOLE		FUTURE MANHOLE TO MANHOLE
	POPULATION EQUIVALENT		FUTURE POPULATION EQUIVALENT
	AREA IN HECTARES		FUTURE AREA IN HECTARES
	SANITARY DRAINAGE AREA BOUNDARY		FUTURE SANITARY DRAINAGE AREA BOUNDARY
	PHASE BOUNDARY LINE		FUTURE DIRECTION OF FLOW
	DIRECTION OF FLOW		FUTURE PROPOSED SANITARY SEWER AND MANHOLE
	PROPOSED SANITARY SEWER AND MANHOLE		

NOTE:
THE POSITION OF ALL POLE LINES, CONDUITS, WATERMANS, SEWERS AND OTHER UNDERGROUND AND OVERGROUND UTILITIES AND STRUCTURES IS NOT NECESSARILY SHOWN ON THE CONTRACT DRAWINGS, AND WHERE SHOWN, THE ACCURACY OF THE POSITION OF SUCH UTILITIES AND STRUCTURES IS NOT GUARANTEED, BEFORE STARTING WORK, DETERMINE THE EXACT LOCATION OF ALL SUCH UTILITIES AND STRUCTURES AND ASSUME ALL LIABILITY FOR DAMAGE TO THEM.



No.	REVISION	DATE	BY
3.	ISSUED FOR APPROVAL (PHASE 1&2)	AUG 17/12	KJM
2.	ISSUED FOR APPROVAL (PHASE 1&2)	JUN 21/12	KJM
1.	ISSUED FOR APPROVAL	MAR 9/12	KJM

SCALE	
1:1250	
1:1250	
0 10 20 30 40 50	

DESIGN	CHECKED	DRAWN	APPROVED
KJM	MAB	RCH	KJM
			MAB

FOR REVIEW ONLY

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CITY OF OTTAWA
FERNBANK CROSSING

SANITARY DRAINAGE AREA PLAN
PHASE 1 & 2

PROJECT NO.: 108180-10
REV #3
DRAWING NO.: 108180-SAN1

Fernbank Crossing - Sanitary Sewer Design Sheet

FLOW ALLOTTED FROM BLOCK 203

AREA			RESIDENTIAL											ICI				INFILTRATION			Total Flow (l/s)	PIPE						
ID	From	To	SINGLES		TOWNS			MIXED USE		TOTAL				Commercial Area (ha)	Institutional Area (ha)	Accum. Area (ha)	Peak Flow (l/s)	Total Area (ha)	Accum. Area (ha)	Infiltr. Flow (l/s)		Size (mm)	Slope (%)	Length (m)	Capacity (l/s)	Full Flow Vel. (m/s)	Q/Q _{full} (%)	
			Units	Pop.	Units	Pop.	Area	Pop.	Net Area (ha)	Pop.	Pop.	Accum. Pop.	Peak Factor								Peak Flow (l/s)							
Outlet 400																												
4-1	410	408	0	0.0	9	24.3	0.0	0.0	0.00	0.0	24.3	24.3	4.0	0.4	0.00	0.00	0.00	0.0	0.38	0.38	0.1	0.5	200	0.65	69.3	27.6	0.85	1.8%
4-2	408	406	0	0.0	9	24.3	0.0	0.0	0.00	0.0	24.3	48.6	4.0	0.8	0.00	0.00	0.00	0.0	0.37	0.75	0.2	1.0	200	0.35	82.0	20.2	0.62	4.9%
4-3	406A	406	0	0.0	0	0.0	0.0	0.0	1.70	137.0	137.0	137.0	4.0	2.2	0.85	0.00	0.85	0.5	2.00	2.00	0.6	3.3	250	0.25	11.0	31.0	0.61	10.6%
4-4	406	404	0	0.0	6	16.2	0.0	0.0	0.00	0.0	16.2	201.8	4.0	3.3	0.00	0.00	0.85	0.5	0.29	3.04	0.9	4.6	250	0.25	82.8	31.0	0.61	14.9%
4-5	404	402	0	0.0	12	32.4	0.0	0.0	0.00	0.0	32.4	234.2	4.0	3.8	0.00	0.00	0.85	0.5	0.41	3.45	1.0	5.3	250	0.25	80.5	31.0	0.61	17.0%
4-6	402A	402	0	0.0	0	0.0	1.1	183.3	0.00	0.0	183.3	183.3	4.0	3.0	0.00	0.00	0.00	0.0	1.14	1.14	0.3	3.3	200	0.35	11.0	20.2	0.62	16.3%
4-7	402	40A	0	0.0	11	29.7	0.0	0.0	0.00	0.0	29.7	447.2	4.0	7.2	0.00	0.00	0.85	0.5	0.39	4.98	1.4	9.2	250	0.25	81.3	31.0	0.61	29.5%
Outlet 500																												
5-1	504	502	12	40.8	0	0.0	0.0	0.0	0.00	0.0	40.8	40.8	4.0	0.7	0.00	0.00	0.00	0.0	0.74	0.74	0.2	0.9	200	0.65	87.3	27.6	0.85	3.2%
5-2	502	41A	17	57.8	0	0.0	0.0	0.0	0.00	0.0	57.8	98.6	4.0	1.6	0.00	0.00	0.00	0.0	0.87	1.61	0.5	2.0	200	0.32	120.0	19.4	0.60	10.6%
Outlet 600																												
6-1	612	610	3	10.2	0	0.0	0.0	0.0	0.00	0.0	10.2	10.2	4.0	0.2	0.00	0.00	0.00	0.0	0.26	0.26	0.1	0.2	200	0.65	30.6	27.6	0.85	0.9%
6-2	610	608	1	3.4	0	0.0	0.0	0.0	0.00	0.0	3.4	13.6	4.0	0.2	0.00	0.00	0.00	0.0	0.13	0.39	0.1	0.3	200	0.65	10.2	27.6	0.85	1.2%
6-3	608	604	14	47.6	0	0.0	0.0	0.0	0.00	0.0	47.6	61.2	4.0	1.0	0.00	0.00	0.00	0.0	0.76	1.14	0.3	1.3	200	0.32	111.8	19.4	0.60	6.8%
6-4	606	604	4	13.6	0	0.0	0.0	0.0	0.00	0.0	13.6	13.6	4.0	0.2	0.00	0.00	0.00	0.0	0.23	0.23	0.1	0.3	200	0.65	42.0	27.6	0.85	1.0%
6-5	604	602	12	40.8	0	0.0	0.0	0.0	0.00	0.0	40.8	115.6	4.0	1.9	0.00	0.00	0.00	0.0	0.60	1.97	0.6	2.4	200	0.32	80.5	19.4	0.60	12.5%
6-6	602	42A	12	40.8	0	0.0	0.0	0.0	0.00	0.0	40.8	156.4	4.0	2.5	0.00	0.00	0.00	0.0	0.61	2.58	0.7	3.3	200	0.32	81.6	19.4	0.60	16.8%
Outlet 700																												
7-1	800	798	10	34.0	0	0.0	0.0	0.0	0.00	0.0	34.0	34.0	4.0	0.6	0.00	0.00	0.00	0.0	0.61	0.61	0.2	0.7	200	0.65	69.9	27.6	0.85	2.6%
7-2	798	796	1	3.4	0	0.0	0.0	0.0	0.00	0.0	3.4	37.4	4.0	0.6	0.00	0.00	0.00	0.0	0.14	0.75	0.2	0.8	200	0.65	13.4	27.6	0.85	3.0%
7-3	796	44A	5	17.0	0	0.0	0.0	0.0	0.00	0.0	17.0	54.4	4.0	0.9	0.00	0.00	0.00	0.0	0.39	1.14	0.3	1.2	200	0.35	71.3	20.2	0.62	5.9%
7-4	42B	43A	4	13.6	0	0.0	0.0	0.0	0.00	0.0	13.6	13.6	4.0	0.2	0.00	0.00	0.00	0.0	0.28	0.28	0.1	0.3	200	0.65	36.5	27.6	0.85	1.1%
7-5	43A	44A	6	20.4	0	0.0	0.0	0.0	0.00	0.0	20.4	34.0	4.0	0.6	0.00	0.00	0.00	0.0	0.38	0.66	0.2	0.7	200	0.35	65.0	20.2	0.62	3.6%
7-6	44A	45A	5	17.0	0	0.0	0.0	0.0	0.00	0.0	17.0	105.4	4.0	1.7	0.00	0.00	0.00	0.0	0.37	2.17	0.6	2.3	200	0.35	82.1	20.2	0.62	11.4%
7-7	788A	788	0	0.0	0	0.0	0.0	0.0	2.68	217.0	217.0	217.0	4.0	3.5	1.34	0.00	1.34	0.8	3.31	3.31	0.9	5.3	250	0.25	11.0	31.0	0.61	17.0%
7-8	788	786	0	0.0	14	37.8	0.0	0.0	0.00	0.0	37.8	254.8	4.0	4.1	0.00	0.00	1.34	0.8	0.57	3.89	1.1	6.0	250	0.25	119.0	31.0	0.61	19.4%
7-9	786	782	0	0.0	9	24.3	0.0	0.0	0.00	0.0	24.3	279.1	4.0	4.5	0.00	0.00	1.34	0.8	0.36	4.25	1.2	6.5	250	0.25	82.0	31.0	0.61	21.0%
7-10	784	782	4	13.6	0	0.0	0.0	0.0	0.00	0.0	13.6	13.6	4.0	0.2	0.00	0.00	0.00	0.0	0.30	0.30	0.1	0.3	200	1.00	50.2	34.2	1.06	0.9%
7-11	782	780	13	44.2	0	0.0	0.0	0.0	0.00	0.0	44.2	336.9	4.0	5.5	0.00	0.00	1.34	0.8	0.80	5.35	1.5	7.8	250	0.75	117.8	53.7	1.06	14.5%
7-12	780	45A	19	64.6	0	0.0	0.0	0.0	0.00	0.0	64.6	401.5	4.0	6.5	0.00	0.00	1.34	0.8	0.93	6.28	1.8	9.1	250	0.25	120.0	31.0	0.61	29.3%
7-13	45A	46A	5	17.0	0	0.0	0.0	0.0	0.00	0.0	17.0	523.9	4.0	8.4	0.00	0.00	1.34	0.8	0.36	8.81	2.5	11.7	250	0.25	82.0	31.0	0.61	37.7%

INFORMATION FROM FERNBANK PHASE 1 & 2 SERVICING DESIGN BRIEF.

Fernbank Crossing - Sanitary Sewer Design Sheet

AREA			RESIDENTIAL											ICI				INFILTRATION			PIPE								
ID	From	To	SINGLES		TOWNS				MIXED USE		TOTAL				Commercial Area (ha)	Institutional Area (ha)	Accum. Area (ha)	Peak Flow (l/s)	Total Area (ha)	Accum. Area (ha)	Infiltr. Flow (l/s)	Total Flow (l/s)	Size (mm)	Slope (%)	Length (m)	Capacity (l/s)	Full Flow Vel. (m/s)	Q/Q _{full} (%)	
			Units	Pop.	Units	Pop.	Area	Pop.	Net Area (ha)	Pop.	Pop.	Accum. Pop.	Peak Factor	Peak Flow (l/s)															
Future		744	101	343.4	0	0.0	2.4	382.3	0.00	0.0	725.7	725.7	3.9	11.4	0.00	2.90	2.90	1.8	11.41	11.41	3.2	16.4							
7-29	752A	752	0	0.0	0	0.0	0.0	1.45	117.0	117.0	117.0	4.0	1.9	0.73	0.00	0.73	0.4	1.58	1.58	0.4	2.8	250	0.30	11.0	34.0	0.67	8.2%		
7-30	752	750	0	0.0	8	21.6	0.0	0.0	0.00	0.0	21.6	138.6	4.0	2.2	0.00	0.00	0.73	0.4	0.72	2.30	0.6	3.3	250	0.30	67.0	34.0	0.67	9.8%	
7-31	750	748	0	0.0	8	21.6	0.0	0.0	0.00	0.0	21.6	160.2	4.0	2.6	0.00	0.00	0.73	0.4	0.44	2.74	0.8	3.8	250	0.30	51.6	34.0	0.67	11.2%	
7-32	748	746	0	0.0	4	10.8	0.0	0.0	0.00	0.0	10.8	171.0	4.0	2.8	0.00	0.00	0.73	0.4	0.23	2.97	0.8	4.0	250	0.30	55.9	34.0	0.67	11.9%	
7-33	746A	746	0	0.0	0	0.0	1.4	231.7	0.00	0.0	231.7	231.7	4.0	3.8	0.00	0.00	0.00	0.0	1.43	1.43	0.4	4.2	200	0.35	10.2	20.2	0.62	20.5%	
7-34	746	744	0	0.0	4	10.8	0.0	0.0	0.00	0.0	10.8	413.5	4.0	6.7	0.00	0.00	0.73	0.4	0.40	4.80	1.3	8.5	250	0.30	69.9	34.0	0.67	25.0%	
7-35	744	742	3	10.2	0	0.0	0.0	0.0	0.00	0.0	10.2	1149.3	3.8	17.5	0.00	0.00	3.76	2.3	0.33	16.54	4.6	24.4	250	0.25	78.1	31.0	0.61	78.7%	
7-36	742	726	2	6.8	0	0.0	0.0	0.0	0.00	0.0	6.8	1156.1	3.8	17.6	0.00	0.00	3.76	2.3	0.29	16.83	4.7	24.6	250	0.25	78.1	31.0	0.61	79.3%	
Future		726	69	234.6	0	0.0	0.0	0.0	0.00	0.0	234.6	234.6	4.0	3.8	0.00	0.00	0.00	0.0	4.40	4.40	1.2	5.0							
7-44	726A	726	0	0.0	0	0.0	0.0	0.0	0.00	0.0	0.0	0.0	4.0	0.0	0.00	2.12	2.12	1.3	2.12	2.12	0.6	1.9	250	0.25	15.0	31.0	0.61	6.1%	
7-45	726	724	0	0.0	0	0.0	0.0	0.0	0.00	0.0	0.0	1390.7	3.7	20.9	0.00	0.00	5.87	3.6	0.18	23.53	6.6	31.0	300	0.20	71.4	45.1	0.62	68.7%	
7-46	724A	724	0	0.0	0	0.0	0.0	0.0	0.00	0.0	0.0	0.0	4.0	0.0	0.00	2.83	2.83	1.7	2.83	2.83	0.8	2.5	250	0.25	15.0	31.0	0.61	8.1%	
7-47	724	710	0	0.0	0	0.0	0.0	0.0	0.00	0.0	0.0	1390.7	3.7	20.9	0.00	0.00	8.70	5.3	0.11	26.47	7.4	33.6	300	0.20	87.2	45.1	0.62	74.4%	
7-48	722	720	5	17.0	0	0.0	0.0	0.0	0.00	0.0	17.0	17.0	4.0	0.3	0.00	0.00	0.00	0.0	0.46	0.46	0.1	0.4	200	0.65	57.6	27.6	0.85	1.5%	
7-49	720	718	1	3.4	0	0.0	0.0	0.0	0.00	0.0	3.4	20.4	4.0	0.3	0.00	0.00	0.00	0.0	0.14	0.60	0.2	0.5	200	0.65	7.9	27.6	0.85	1.8%	
7-50	718	716	10	34.0	0	0.0	0.0	0.0	0.00	0.0	34.0	54.4	4.0	0.9	0.00	0.00	0.00	0.0	0.60	1.20	0.3	1.2	200	0.35	75.7	20.2	0.62	6.0%	
7-51	716	712	9	30.6	0	0.0	0.0	0.0	0.00	0.0	30.6	85.0	4.0	1.4	0.00	0.00	0.00	0.0	0.54	1.74	0.5	1.9	200	0.35	73.1	20.2	0.62	9.2%	
7-52	714	712	4	13.6	0	0.0	0.0	0.0	0.00	0.0	13.6	13.6	4.0	0.2	0.00	0.00	0.00	0.0	0.23	0.23	0.1	0.3	200	0.65	39.4	27.6	0.85	1.0%	
7-53	712	710	4	13.6	0	0.0	0.0	0.0	0.00	0.0	13.6	112.2	4.0	1.8	0.00	0.00	0.00	0.0	0.28	2.25	0.6	2.4	200	0.35	64.1	20.2	0.62	12.1%	
7-54	710	708	5	17.0	0	0.0	0.0	0.0	0.00	0.0	17.0	1519.9	3.7	22.6	0.00	0.00	8.70	5.3	0.40	29.11	8.2	36.1	300	0.20	75.8	45.1	0.62	79.9%	
	708	706	0	0.0	0	0.0	0.0	0.0	0.00	0.0	0.0	1519.9	3.7	22.6	0.00	0.00	8.70	5.3	0.00	29.11	8.2	36.1	300	0.20	6.6	45.1	0.62	79.9%	
7-55	706	704	8	27.2	0	0.0	0.0	0.0	0.00	0.0	27.2	1547.1	3.7	23.0	0.00	0.00	8.70	5.3	0.60	29.71	8.3	36.6	300	0.20	65.7	45.1	0.62	81.1%	
	704	702	0	0.0	0	0.0	0.0	0.0	0.00	0.0	0.0	1547.1	3.7	23.0	0.00	0.00	8.70	5.3	0.00	29.71	8.3	36.6	300	0.20	8.7	45.1	0.62	81.1%	
7-56	702	46A	9	30.6	0	0.0	0.0	0.0	0.00	0.0	30.6	1577.7	3.7	23.4	0.00	0.00	8.70	5.3	0.58	30.29	8.5	37.2	300	0.20	69.6	45.1	0.62	82.4%	
	46A	31A	3	10.2	0	0.0	0.0	0.0	0.00	0.0	10.2	2111.8	3.6	30.5	0.00	0.00	10.04	6.1	0.29	39.39	11.0	47.6	300	0.65	82.0	81.3	1.11	58.6%	

Design Parameters: Avg Flow/Person = 350 l/day
 Comm./Inst. Flow = 35000 l/ha/day
 Infiltration = 0.28 l/s/ha
 Pipe Friction n = 0.013
 Residential Peaking Factor = Harmon Equation (max 4, min 2)
 Peaking Factor Comm./Inst. 1.5

Population Density: Mixed Use 1.80 ppl/unit
 Singles 3.40 ppl/unit
 Towns 2.70 ppl/unit

units/net ha: 90
 60

Project: Abbott-Fernbank (108180)
 Designed: KJM
 Checked: MAB
 Date: August 17, 2012

INFORMATION FROM
 FERNBANK CROSSING
 PHASE 1 & 2 DEVELOPMENT



5000 Robert Grant - Tower 'A' and Podium POST-DEVELOPMENT SANITARY FLOWS

Residential Flows		Post-Development	
Total Number of Units		113	
Average Number of Persons per Unit		1.8	
Design Population		204	
Average Daily Flow per Resident		280 L/c/day	
Peak Factor (Harmon Formula)		3.52	
Peak Residential Flow		2.32 L/s	
Commercial Flows			
Ground Floor Area		0 m ²	
Average Commercial Daily Demand		2.8 L/m ² /day	
Peaking Factor		1.5	
Peak Commercial Flows		0.00 L/s	
Extraneous Flow			
Site Area		0.68 ha	
Infiltration Allowance		0.33 L/s/ha	
Peak Extraneous Flow		0.22 L/s	
Total Peak Sanitary Flow		2.5 L/s	

5000 Robert Grant - Tower 'B' and Podium POST-DEVELOPMENT SANITARY FLOWS

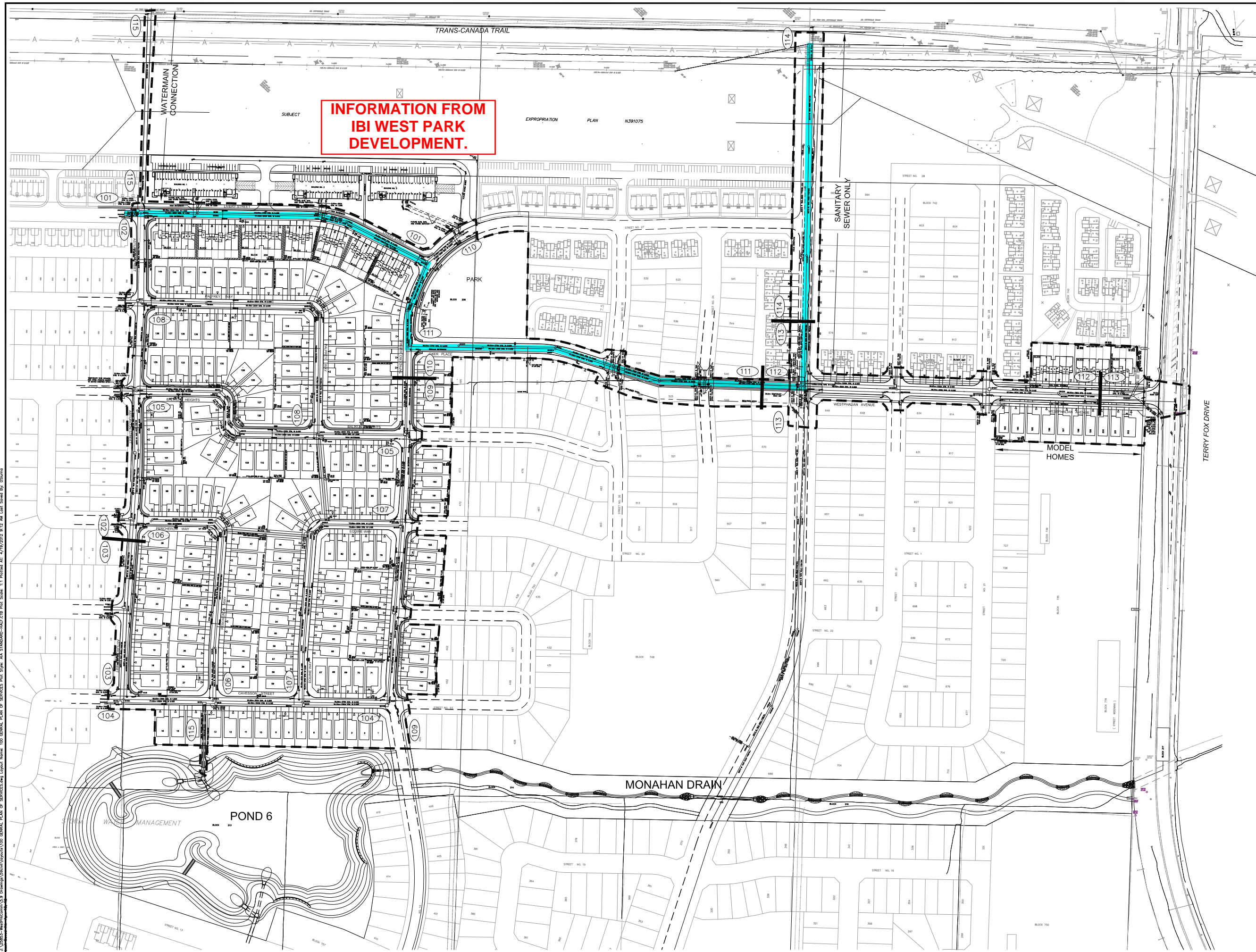
Residential Flows		Post-Development	
Total Number of Units		153	
Average Number of Persons per Unit		1.8	
Design Population		276	
Average Daily Flow per Resident		280 L/c/day	
Peak Factor (Harmon Formula)		3.47	
Peak Residential Flow		3.11 L/s	
Commercial Flows			
Ground Floor Area		0 m ²	
Average Commercial Daily Demand		2.8 L/m ² /day	
Peaking Factor		1.5	
Peak Commercial Flows		0.00 L/s	
Extraneous Flow			
Site Area		0.67 ha	
Infiltration Allowance		0.33 L/s/ha	
Peak Extraneous Flow		0.22 L/s	
Total Peak Sanitary Flow		3.3 L/s	

5000 Robert Grant - Tower 'C' and Podium POST-DEVELOPMENT SANITARY FLOWS

Residential Flows		Post-Development	
Total Number of Units		238	
Average Number of Persons per Unit		1.8	
Design Population		429	
Average Daily Flow per Resident		280 L/c/day	
Peak Factor (Harmon Formula)		3.41	
Peak Residential Flow		4.74 L/s	
Commercial Flows			
Ground Floor Area		157 m ²	
Average Commercial Daily Demand		2.8 L/m ² /day	
Peaking Factor		1.5	
Peak Commercial Flows		0.01 L/s	
Extraneous Flow			
Site Area		0.67 ha	
Infiltration Allowance		0.33 L/s/ha	
Peak Extraneous Flow		0.22 L/s	
Total Peak Sanitary Flow		5.0 L/s	

5000 Robert Grant - Towers A + B + C and Podium
SUBJECT SITE: SANITARY FLOW SUMMARY TABLE

Area	Allowable (to Livery) Peak Flow (L/s)	Available Capacity RGA 250 Sewer (L/s)	Post-Development Peak Flow (L/s)
Overall Site	3.3	22.2	-
Tower A	-	-	2.5
Tower B	-	-	3.3
Tower C	-	-	5.0
Totals	3.3	22.2	10.8



**INFORMATION FROM
IBI WEST PARK
DEVELOPMENT.**

- LEGEND:**
- SINGLE SERVICE LOCATION
 - DOUBLE SERVICE LOCATION
 - STACKED TOWNHOUSE DOUBLE SERVICE
 - DRIVEWAY LOCATION
 - STANDARD STREET CATCHBASIN *
 - REARYARD CB C/W TOP OF GRATE *
 - ELBOW OR TEE REARYARD CB C/W TOP OF GRATE
 - SINGLE CONNECTION BETWEEN PAIRS OF STREET CATCHBASINS
 - BARRIER CURB
 - MOUNTABLE CURB
 - PHASE LIMITS
 - DEPRESSED CURB
 - * REFER TO CATCHBASIN DATA TABLE ON DRAWING 25853-DETAILS 1 FOR TOP OF GRATE, LEAD INVERT, PIPE SIZE AND INLET CONTROL DEVICE INFORMATION
 - DRAWING NUMBER
 - MAIL BOX C/W 2.0m DEPRESSED CURB

14		
13		
12		
11		
10		
9		
8		
7		
6		
5		
4	ISSUED FOR MOE APPROVAL	LME 12:04:19
3	ISSUED FOR SUBMISSION #3	LME 12:03:29
2	ISSUED FOR SUBMISSION #2	LME 12:01:27
1	ISSUED FOR SUBMISSION #1	LME 11:09:22
No.	REVISIONS	By Date

IBI GROUP

333 Preston Street
Tower 1, Suite 400
Ottawa, Ontario
Canada K1S 5N4
Tel (613)225-1311
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Project Title

**WEST PARK
MONARCH - CARDELE
PHASE 1**

L. M. ERION
PROVINCE OF ONTARIO

Drawing Title

**GENERAL PLAN
OF SERVICES**

Scale

1 : 1500

Design	LME	Date	SEPT 2011
Drawn	D.D.	Checked	RWW
Project No.	25853	Drawing No.	100

J:\25853-WestParkMonarch\Layout\100 GENERAL PLAN OF SERVICES.dwg Layout Name: 100 GENERAL PLAN OF SERVICES Plot Size: A4 STANDARD-HALF C/B Plot Scale: 1:1 Plotted At: 4/17/2012 9:12 AM User Saved By: DBarne

**INFORMATION FROM IBI WEST
PARK DEVELOPMENT**



IBI Group
333 Preston Street - Suite 400
Ottawa, Ontario
K1S 5N4

SANITARY SEWER DESIGN SHEET

PROJECT: WEST PARK IN FERNBANK - PHASE 1
DEVELOPER: MONARCH CORPORATION

JOB #: 25853-5.7
DATE PRINTED: 01-May-12
DESIGN: LE

**FLOW FROM FERNBANK
CROSSING LIVERY STREET**

LOCATION			INDIVIDUAL				CUM. RES. FLOW			ICI				INFILTRATION			TOTAL DESIGN FLOW (l/s)	PROPOSED SEWER						FLOW DEPTH		
STREET	FROM MH	TO MH	RESID. UNITS			POP.	POP.	PEAK FACT.	PEAK FLOW (l/s)	COMM. AREA (Ha)	INSTIT. AREA (Ha)	CUM. AREA (Ha)	PEAK FLOW (l/s)	INCR. AREA (Ha)	CUM. AREA (Ha)	FLOW (l/s)		CAP. l/s	PIPE (mm)	LGTH. (m)	SLOPE %	VEL. (full) m/s	AVAIL. CAP. (l/s)	AVAIL. CAP. (%)	Flow qa/Qa	Depth da/Df
			Sngls	Towns Semis	Multi Res																					
Private Site	211 A	100 A			45	103.5	104	4.00	1.70					0.72	0.72	0.20	1.90	26.49	200	8.5	0.60	0.82	24.60	93%		
Tapadero Avenue	100 A	101 A				0.0	104	4.00	1.70					0.09	0.81	0.23	1.92	26.49	200	41.0	0.60	0.82	24.57	93%		
External	Stub	40 A				468.1	468	3.99	7.66					5.05	5.05	1.41	9.07	31.01	250	15.0	0.25	0.61	21.94	71%	0.29	0.37
Livery Street	40 A	90 A		6		16.2	484	3.98	7.91					0.22	5.27	1.48	9.38	70.74	250	51.1	1.30	1.40	61.36	87%	0.13	0.25
Private Site	240 A	90 A			56	128.8	129	4.00	2.11					0.49	0.49	0.14	2.25	34.21	200	9.5	1.00	1.06	31.96	93%		
Livery Street	90 A	91 A		16		43.2	656	3.91	10.52					0.55	6.31	1.77	12.29	39.22	250	111.5	0.40	0.77	26.93	69%	0.31	0.39
Private Site	241 A	91 A			45	103.5	104	4.00	1.70					0.43	0.43	0.12	1.82	34.21	200	9.5	1.00	1.06	32.40	95%		
Livery Street	91 A	92 A		3		8.1	768	3.87	12.19					0.11	6.85	1.92	14.11	62.02	250	27.0	1.00	1.22	47.92	77%	0.23	0.33
	92 A	101 A		10		27.0	795	3.86	12.59					0.39	7.24	2.03	14.61	53.71	250	83.0	0.75	1.06	39.10	73%	0.27	0.35
Tapadero Avenue	101 A	102 A				0.0	898	3.83	14.11					0.07	8.12	2.27	16.38	34.00	250	46.2	0.30	0.67	17.62	52%	0.48	0.49
	102 A	103 A		3		10.2	909	3.83	14.25					0.22	8.34	2.34	16.59	34.00	250	33.0	0.30	0.67	17.41	51%	0.49	0.49
Asturcon Street	42 B	43 A	4			13.6	14	4.00	0.22					0.28	0.28	0.08	0.30	27.60	200	36.5	0.65	0.85	27.30	99%		
Asturcon Street	43 A	44 A	7			23.8	37	4.00	0.61					0.38	0.66	0.18	0.80	20.24	200	65.0	0.35	0.62	19.44	96%		
External	Stub	44 A				52.8	53	4.00	0.87					1.14	1.14	0.32	1.19	20.24	200	15.0	0.35	0.62	19.05	94%		
Asturcon Street	44 A	45 A	5			17.0	107	4.00	1.76					0.36	2.16	0.60	2.36	20.24	200	82.2	0.35	0.62	17.87	88%		
External	Stub	45 A				412.1	412	4.00	6.76	1.40	1.40	0.85	6.39	6.39	1.79	9.40	31.01	250	15.0	0.25	0.61	21.61	70%	0.30	0.38	
Asturcon Street	45 A	46 A	5			17.0	536	3.96	8.70		1.40	0.85	0.37	8.92	2.50	12.05	31.01	250	82.0	0.25	0.61	18.96	61%	0.39	0.43	
External	Stub	46 A				1586.4	1586	3.66	23.82	0.73	5.15	5.88	3.57	28.97	28.97	8.11	35.50	45.09	300	15.0	0.20	0.62	9.59	21%	0.79	0.67
Cavesson Street	46 A	31 A	3			10.2	2133	3.56	31.17			4.42	0.29	38.18	10.69	46.28	127.18	300	82.0	1.59	1.74	80.90	64%	0.36	0.41	
Percheron Way	50 A	51 A	6			20.4	20	4.00	0.33					0.38	0.38	0.11	0.44	28.64	200	74.4	0.70	0.88	28.19	98%		
	51 A	52 A	2			6.8	27	4.00	0.45					0.21	0.59	0.17	0.61	61.68	200	10.7	3.25	1.90	61.07	99%		
	52 A	53 A	15			51.0	78	4.00	1.28					0.83	1.42	0.40	1.68	22.96	200	107.8	0.45	0.71	21.28	93%		
	53 A	31 A	6			20.4	99	4.00	1.62					0.37	1.79	0.50	2.12	42.61	200	48.6	1.55	1.31	40.49	95%		
Cavesson Street	31 A	30 A	6			20.4	2252	3.55	32.73			4.42	0.39	40.36	11.30	48.46	59.69	300	82.0	0.35	0.82	11.23	19%	0.81	0.68	

Where Q = average daily per capita flow (350 l/cap.d.) or (0.0041l/sec./cap)
 I = Unit of peak extraneous flow (0.28 l/sec/ha)
 M = Residential Peaking factor = Harmon Peaking Factor, $M = 1 + (14 / (4 + P^{0.5}))$, where P = population in thouse
 Q(p) = Peak population flow (l/s)
 Q(i) = peak extraneous flow (l/s)

Population Density
 Singles 3.4
 Towns/Semis 2.7
 Multi Residential

Commercial, Office Space and School - Average flow 35,000 l/day/ha (0.405 l/s/ha) with Peaking Factor = 1.5



IBI Group
333 Preston Street - Suite 400
Ottawa, Ontario
K1S 5N4

SANITARY SEWER DESIGN SHEET

PROJECT: WEST PARK IN FERNBANK - PHASE 1
DEVELOPER: MONARCH CORPORATION

JOB #: 25853-5.7
DATE PRINTED: 01-May-12
DESIGN: LE

LOCATION			INDIVIDUAL				CUM. RES. FLOW			ICI				INFILTRATION			TOTAL DESIGN FLOW (l/s)	PROPOSED SEWER						FLOW DEPTH		
STREET	FROM MH	TO MH	RESID. UNITS			POP.	POP.	PEAK FACT.	PEAK FLOW (l/s)	COMM. AREA (Ha)	INSTIT. AREA (Ha)	CUM. AREA (Ha)	PEAK FLOW (l/s)	INCR. AREA (Ha)	CUM. AREA (Ha)	FLOW (l/s)		CAP. l/s	PIPE (mm)	LGTH. (m)	SLOPE %	VEL. (full) m/s	AVAIL. CAP. (l/s)	AVAIL. CAP. (%)	Flow qa/Qa	Depth da/Df
			Sngls	Towns Semis	Multi Res																					
Equine Way	60 A	61 A	3			10.2	10	4.00	0.17																	
	61 A	62 A	15			51.0	61	4.00	1.00																	
	62 A	30 A	4			13.6	75	4.00	1.23																	
Cavesson Street	30 A	107 A	12			40.8	2368	3.53	34.24			7.28	4.42	0.62	42.22	11.82										
	107 A	106 A	9			30.6	2398	3.52	34.64			7.28	4.42	0.50	42.72	11.96										
Tapadero Avenue	106 B	105 A	8			27.2	2425	3.52	34.99			7.28	4.42	0.45	43.17	12.09										
Equine Way	60 A	105 A	10			34.0	34	4.00	0.56					0.55	0.55	0.15										
Tapadero Avenue	105 A	104 A	5			17.0	2476	3.51	35.66			7.28	4.42	0.34	44.06	12.34										
External	Stub	42 A				151.8	152	4.00	2.49					2.59	2.59	0.73										
Balikun Heights	42 A	70 A	6			20.4	172	4.00	2.82					0.37	2.96	0.83										
	70 A	71 A	2			6.8	179	4.00	2.94					0.18	3.14	0.88										
	71 A	72 A	3			10.2	189	4.00	3.10					0.18	3.32	0.93										
	72 A	73 A	3			10.2	199	4.00	3.27					0.27	3.59	1.01										
	73 A	74 A	5			17.0	216	4.00	3.55					0.35	3.94	1.10										
External	Stub	41 A				95.7	96	4.00	1.57					1.61	1.61	0.45										
Palfrey Way	41 A	80 A	7			23.8	120	4.00	1.96					0.39	2.00	0.56										
	80 A	81 A	13			44.2	164	4.00	2.68					0.76	2.76	0.77										
	81 B	82 A	1			3.4	167	4.00	2.74					0.09	2.85	0.80										
	82 A	74 A	15			51.0	218	4.00	3.58					0.91	3.76	1.05										
Balikun Heights	74 A	104 A	5			17.0	452	4.00	7.40					0.36	8.06	2.26										
Tapadero Avenue	104 A	103 A	10			34.0	2962	3.45	41.86			7.28	4.42	0.58	52.70	14.76										
Oxer Place	103 A	200 A	3			10.2	3881	3.35	53.22			7.28	4.42	0.20	61.24	17.15										
	200 A	201 A	4			13.6	3894	3.34	53.39			7.28	4.42	0.30	61.54	17.23										
	201 A	202 A	4			13.6	3908	3.34	53.55			7.28	4.42	0.28	61.82	17.31										
Street No. 26	Stub North	202 A	7	19		75.1	75	4.00	1.23					1.00	1.00	0.28										
Street No. 26	Stub South	202 A	31			105.4	105	4.00	1.73					1.80	1.80	0.50										
Block 205	202 A	203 A				0.0	4088	3.32	55.73			7.28	4.42		64.62	18.09										
	203 A	204 A				0.0	4088	3.32	55.73			7.28	4.42		64.62	18.09										

Where Q = average daily per capita flow (350 l/cap.d.) or (0.0041l/sec./cap)

I = Unit of peak extraneous flow (0.28 l/sec/ha)

M = Residential Peaking factor = Harmon Peaking Factor, $M = 1 + (14 / (4 + P^{0.5}))$, where P = population in thousand

Q(p) = Peak population flow (l/s)

Q(i) = peak extraneous flow (l/s)

Commercial, Office Space and School - Average flow 35,000 l/day/ha (0.405 l/s/ha) with Peaking Factor = 1.5

Population Density

Singles 3.4

Towns/Semis 2.7

Multi Residential



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SANITARY SEWER DESIGN SHEET

PROJECT: WEST PARK IN FERNBANK - PHASE 1
DEVELOPER: MONARCH CORPORATION

JOB #: 25853-5.7
DATE PRINTED: 01-May-12
DESIGN: LE

LOCATION			INDIVIDUAL				CUM. RES. FLOW			ICI				INFILTRATION			TOTAL DESIGN FLOW (l/s)	PROPOSED SEWER						FLOW DEPTH		
STREET	FROM MH	TO MH	RESID. UNITS			POP.	POP.	PEAK FACT.	PEAK FLOW (l/s)	COMM. AREA (Ha)	INSTIT. AREA (Ha)	CUM. AREA (Ha)	PEAK FLOW (l/s)	INCR. AREA (Ha)	CUM. AREA (Ha)	FLOW (l/s)		CAP. l/s	PIPE (mm)	LGTH. (m)	SLOPE %	VEL. (full) m/s	AVAIL. CAP. (l/s)	AVAIL. CAP. (%)	Flow qa/Qa	Depth da/Df
			Sngls	Towns Semis	Multi Res																					
Street No. 24	Stub North	204 A	15	29	46	235.1	235	4.00	3.86																	
Street No. 24	Stub South	204 A	82			278.8	279	4.00	4.57																	
Block 204	204 A	205 B				0.0	4602	3.28	61.86			7.28	4.42		73.24	20.51	86.79	129.29	375	89.7	0.50	1.13	42.50	33%	0.67	0.62
Westphalian Avenue	Stub North	209 A		42		113.4	113	4.00	1.86																	
	209 A	208 A	6	9		44.7	158	4.00	2.59																	
	208 A	207 A	4	4		24.4	183	4.00	2.99																	
Street No. 28	Stub North	207 A	12	35		135.3	135	4.00	2.22																	
Street No. 21	Stub South	207 A	97			329.8	330	4.00	5.41																	
Westphalian Avenue	207 A	206 A		9		24.3	672	3.90	10.76																	
Street No. 28	Stub North	206 A	20			68.0	68	4.00	1.12																	
Westphalian Avenue	206 A	205 A		9		24.3	764	3.87	12.13																	
Street No. 1	Stub South	205 B	27			91.8	92	4.00	1.51																	
Street No. 1	Stub North	205 B	10	15		74.5	75	4.00	1.22																	
Street No. 1	205 B	205 A				0.0	4769	3.26	63.81			7.28	4.42		75.54	21.15	89.39	129.29	375	2.5	0.50	1.13	39.90	31%	0.69	0.63
Street No. 1	Stub South	205 A	506	260	86	2620.2	2620	3.49	37.51		2.90	2.90	1.76	57.88	57.88	16.21	55.48	132.98	450	20.0	0.20	0.81	77.50	58%	0.42	0.47
Street No. 1	205 A	222 A				0.0	8153	3.04	101.69			10.18	6.18	0.30	145.66	40.78	148.66	221.82	600	120.0	0.12	0.76	73.16	33%	0.67	0.62
Street No. 1	222 A	221 A				0.0	8153	3.04	101.69			10.18	6.18	0.26	145.92	40.86	148.73	221.82	600	100.0	0.12	0.76	73.08	33%	0.67	0.62
Street No. 1	221 A	FT06				0.0	8153	3.04	101.69			10.18	6.18	0.19	146.11	40.91	148.79	221.82	600	94.0	0.12	0.76	73.03	33%	0.67	0.62

Where Q = average daily per capita flow (350 l/cap.d.) or (0.0041l/sec./cap)

I = Unit of peak extraneous flow (0.28 l/sec/ha)

M = Residential Peaking factor = Harmon Peaking Factor, $M = 1 + (14 / (4 + P^{0.5}))$, where P = population in thousand

Q(p) = Peak population flow (l/s)

Q(i) = peak extraneous flow (l/s)

Commercial, Office Space and School - Average flow 35,000 l/day/ha (0.405 l/s/ha) with Peaking Factor = 1.5

Population Density

Singles 3.4

Towns/Semis 2.7

Multi Residential 2.3

Off-Site Sanitary Drainage Areas



Existing Townhouse Development
4.47 ha
137 units
5.6 L/s

Future Residential Block
1.7 ha
~433 units
8.9 L/s

Ex. 250 SAN
@ 0.35%
 $Q_{cap} = 36.7 \text{ L/s}$

$< 8.3 \text{ L/s}$

Subject Site

$< 2.5 \text{ L/s}$

Off-Site Sanitary Drainage Areas

5000 Robert Grant: Off-Site Townhome Development THEORETICAL SANITARY FLOWS

Residential Flows	Post-Development
Total Number of Townhomes	137
Average Number of Persons per Townhome	2.7
Design Population	370
Average Daily Flow per Resident	280 L/c/day
Peak Factor (Harmon Formula)	3.43
Peak Residential Flow	4.11 L/s
Commercial Flows	
Ground Floor Area	0 m ²
Average Commercial Daily Demand	2.8 L/m ² /day
Peaking Factor	1.5
Peak Commercial Flows	0.00 L/s
Extraneous Flow	
Site Area	4.47 ha
Infiltration Allowance	0.33 L/s/ha
Peak Extraneous Flow	1.48 L/s
Total Peak Sanitary Flow	5.6 L/s

5000 Robert Grant: Off-Site Future Residential Development THEORETICAL SANITARY FLOWS

Residential Flows	Post-Development
Total Number of Units	433
Average Number of Persons per Unit	1.8
Design Population	780
Average Daily Flow per Resident	280 L/c/day
Peak Factor (Harmon Formula)	3.29
Peak Residential Flow	8.33 L/s
Commercial Flows	
Ground Floor Area	150 m ²
Average Commercial Daily Demand	2.8 L/m ² /day
Peaking Factor	1.5
Peak Commercial Flows	0.01 L/s
Extraneous Flow	
Site Area	1.7 ha
Infiltration Allowance	0.33 L/s/ha
Peak Extraneous Flow	0.56 L/s
Total Peak Sanitary Flow	8.9 L/s

Post-Development Sanitary Flow Calculations

Location			Residential		Commercial / Institutional		Residential Cumulative		Peak Factor		Commercial / Institutional		Residential	Infiltration		Foundation		PEAK DESIGN FLOW (l/s)	Pipe Data					
Street / Area	From	To	Population	Area (ha)	Area (ha)	Accu. Area (ha)	Pop.	Area (ha)	Res Peak Factor	Comm Peak Factor	Peak Flow (l/s)	Accu. Peak Flow	Acc. Peak Flow (l/s)	Infiltr. Flow (l/s)	Accu Infil. Flow	Found. Flow (l/s)	Accu Found. Flow		Size (mm)	Slope (%)	Length (m)	Capacity (l/s)	Full Flow Vel. (m/s)	Q/Q _{full} (%)
Robert Grant Avenue	MHSA72812	MHSA72813	1198	6.17	0.02	0.02	1198	6.17	3.2	1.5	0.01	0.01	12.42	2.04	2.04	0.00	0.00	14.5	254	0.35	90.5	36.7	0.72	39.5%

Population includes both existing off-site townhome development area (4.47 ha) + future residential medium/high-density development parcel (1.7 ha) with average apartment units
 The number of units allotted to the 1.7 ha future parcel development has been approximated based on a pro-rated area comparison to the proposed subject site at 5000 Robert Grant Avenue

36.7 - 14.5 = 22.2 L/s available capacity in outlet sewer

City of Ottawa Sewer Design Guidelines

Studio / 1-Bedroom Apartment Unit	1.4	persons/unit
2-Bedroom Apartment Unit	2.1	persons/unit
3-Bedroom Apartment Unit	3.1	persons/unit
Average Medium / High-Density Apartment Unit	1.8	persons/unit
Townhomes	2.7	persons/unit
Average Domestic Flow	280	L/person/day
Institutional / Commercial Flow	28,000	L/ha/day
Extraneous Flows	0.33	L/s/ha
Foundation Drain Allowance	5.0	L/s/ha (use 5.0 L/s/ha for tributary areas < 10 ha; 3.0 L/s/ha for tributary areas >10 ha and < 100 ha; 2.0 L/s/ha for tributary areas >100 ha)
Residential Peaking Factor	Harmon Equation, Correction Factor = 0.8	
Institutional / Commercial Peaking Factor	1.5	

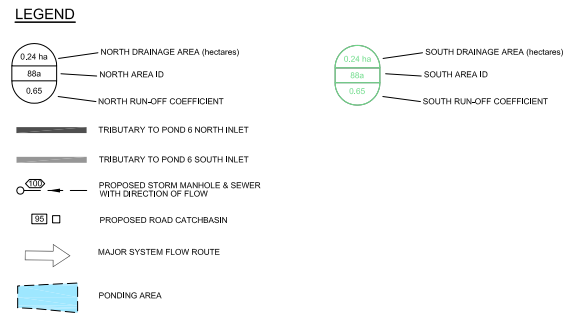
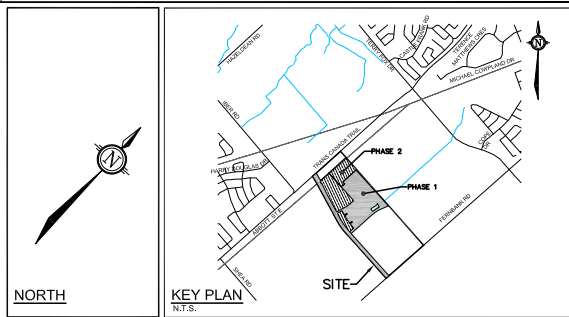
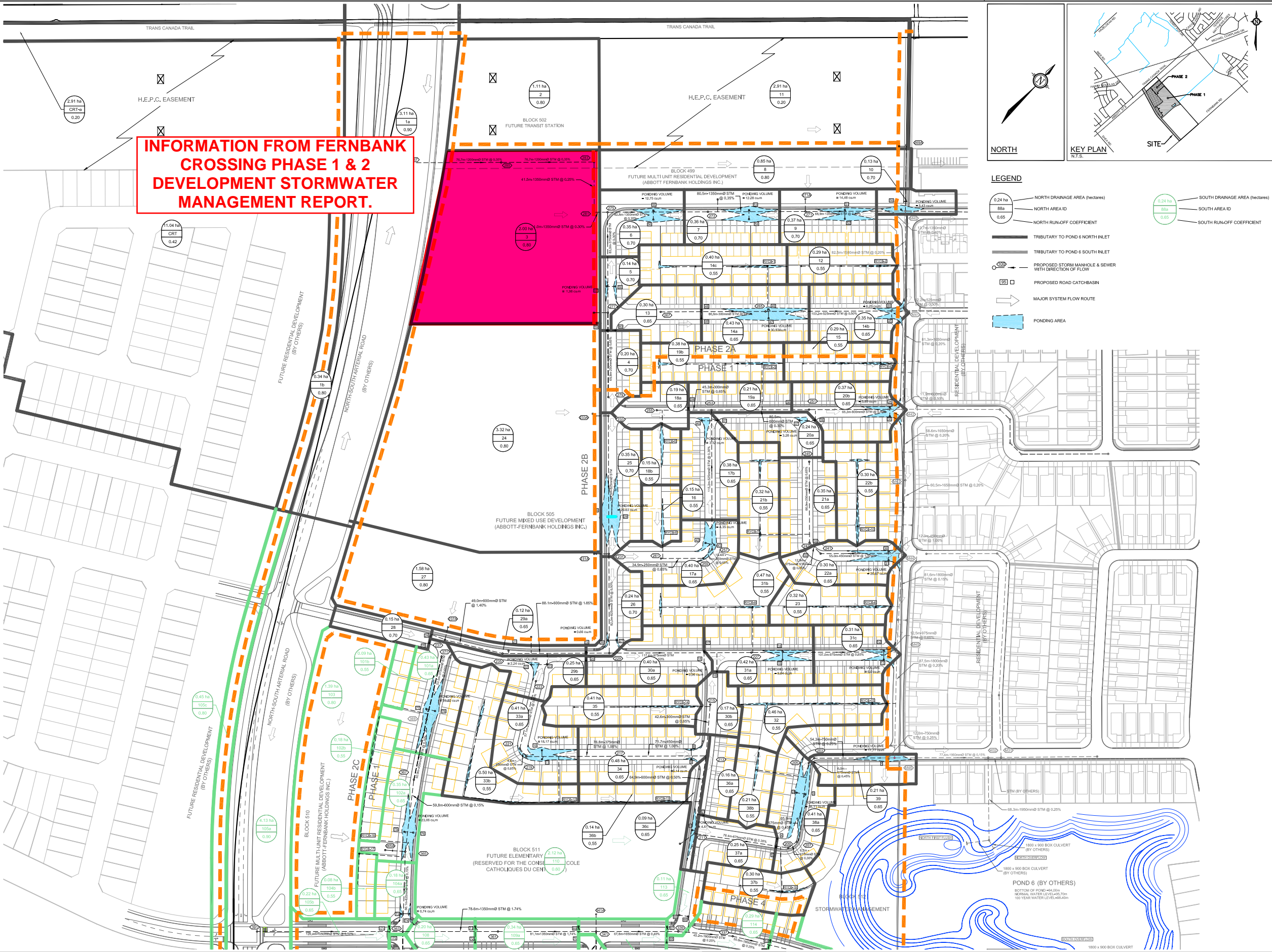
Notes: The number of units has been counted from geoOttawa imagery of the recently constructed townhouse development upstream of MHSA72812.
 Existing pipe information has been taken from the City of Ottawa geoOttawa website.
 A foundation drain allowance would only be accounted for along those existing streets that do not have a separated storm sewer as indicated on the geoOttawa website.

APPENDIX B

Storm Drainage Areas and Sewer Capacities

MANHOLE ID	OBVERT
203	S=98.33 NE=98.33
205	SE=98.38 NW=98.35
207	S=98.72 NW=98.68
209	SW=98.78 N=98.74
211	NW=99.01 NE=99.01
213	SW=99.33 NW=99.33 SE=99.33
215	SE=99.61
217	SW=100.05 NE=100.05
219	W=100.82 NE=100.82
221	NW=100.90 E=100.87
223	SE=101.27
227	SW=99.12 NE=99.12
229	SW=99.70 NE=99.70 NW=99.70
231	SE=100.11 SW=100.18 NW=100.11
233	SE=100.63 SW=100.68
235	SW=101.33 NE=101.33
237	NE=102.02
241	W=99.13 NE=99.13
243	NW=99.21 E=99.21
245	SE=99.65
251	SW=99.09 NE=99.09
253	SE=99.34 SW=99.34 NE=99.34
255	NE=99.63
257	S=99.68 NW=99.68
259	SW=99.78 N=99.75
261	NE=100.01
265	SW=99.45 NE=99.45
267	NE=100.01
269A	SE=99.19
271	SW=99.37 NW=99.37 NE=99.37
273	SW=99.65 NE=99.65
275	SW=99.94 SE=99.94 NE=99.94
277	SE=100.19 NW=100.19
279	NW=100.64
281	NW=100.03 NE=99.97
283	SW=100.13 SE=100.13
285	SW=100.40 NE=100.40
287	NE=100.67
301	SW=98.59 SE=98.59 NE=98.59
305	SW=98.76 SE=98.76 NE=98.76
337	SW=98.89 NE=98.89
339	SW=99.00 NE=99.00
341	SW=99.27 NW=99.27 SE=99.27 NE=99.27
361	SW=100.68 NE=100.68
363	NW=102.05 SW=102.05 SE=102.11 NE=102.05
365	NW=102.15 SW=102.15 SE=102.15
367	NW=102.34 SE=102.34
369	NW=102.34 SE=102.34
371	SE=102.69
391	NE=102.65

**INFORMATION FROM FERNBANK
CROSSING PHASE 1 & 2
DEVELOPMENT STORMWATER
MANAGEMENT REPORT.**



NOTE:
THE POSITION OF ALL POLE LINES, CONDUITS,
WATERMANS, SEWERS AND OTHER
UNDERGROUND AND OVERGROUND UTILITIES AND
STRUCTURES IS NOT NECESSARILY SHOWN ON
THE CONTRACT DRAWINGS, AND WHERE SHOWN,
THE ACCURACY OF THE POSITION OF SUCH
UTILITIES AND STRUCTURES IS NOT GUARANTEED,
BEFORE STARTING WORK, DETERMINE THE EXACT
LOCATION OF ALL SUCH UTILITIES AND
STRUCTURES AND ASSUME ALL LIABILITY FOR
DAMAGE TO THEM.



No.	REVISION	DATE	BY
3.	ISSUED FOR APPROVAL (PHASE 1&2)	AUG 17/12	KJM
2.	ISSUED FOR APPROVAL (PHASE 1&2)	JUN 21/12	KJM
1.	ISSUED FOR APPROVAL	MAR 9/12	KJM

SCALE	DESIGN	CHECKED	DRAWN	APPROVED
1:1250	KJM	MAB	RCH	KJM
0 10 20 30 40 50				MAB

FOR REVIEW ONLY

PROFESSIONAL ENGINEER
M.A. BISSETT
PROV. OF ONTARIO

PROFESSIONAL DESIGNER
M.A. BISSETT
PROV. OF ONTARIO

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Facsimile: (613) 254-9967
Email: novatech@novatech-eng.com

CITY OF OTTAWA
FERNBANK CROSSING

STORM DRAINAGE AREA PLAN
PHASE 1 & 2

PROJECT NO: 108180-10
REV: 108180-10
REV #3
DRAWING NO: 108180-STM1

Fernbank Crossing - Storm Sewer Design Sheet (Rational Method)

LOCATION			AREA											FLOW					Total Peak Flow (Q) (L/s)	PROPOSED SEWER									
Location	From node	To node	Mixed Use	Park N' Ride Paramedic Post Medium Block	Arterial Road ROW	Schools	Parks	Hydro Corridor	Singles Front Yards	Singles Rear Yard	Towns Front Yard	Towns Rear Yard	Total Area (ha)	Weighted Runoff Coefficient	Indivi 2.78 AR	Accum 2.78 AR	Time of Concentration	Rain Intensity (mm/hr)		Peak Flow (L/s)	Pipe Type	Size (mm)	Grade (%)	Length (m)	Capacity (l/s)	Full Flow Velocity (m/s)	Time of Flow (min.)	Q/Qfull (%)	
			0.80	0.80	0.90	0.60	0.40	0.20	0.65	0.55	0.70	0.60						5yr		10yr									
POND 6 North Inlet																													
CRT	CRT	287						2.91					13.95	0.38	14.54	14.54	15.00	83.6		1215.2									
													0.00	0.00	0.00	14.54	15.00	83.6		1215.2									
1	287	285		0.34	3.11								3.45	0.89	8.54	8.54	10.00		122.1	1042.8	2257.9	CONC	1200	0.35	76.7	2406.2	2.06	0.62	93.8%
													0.00		0.00	14.54	15.62	81.6		1186.8									
													0.00		0.00	8.54	15.62		95.6	815.8	2002.6	CONC	1200	0.35	76.7	2406.2	2.06	0.62	83.2%
2	283	281		1.11									1.11	0.80	2.47	17.01	16.24	79.8		1356.7									
													0.00		0.00	8.54	16.24	93.4		797.2									
3	281	275	2.00										2.00	0.80	4.45	21.46	16.61	78.7		1688.9	2475.5	CONC	1350	0.30	11.0	3049.8	2.06	0.09	81.2%
													0.00		0.00	8.54	16.61	92.1		786.6									
4	279	277									0.20		0.20	0.70	0.39	0.39	10.00	104.2		40.6									
													0.00		0.00	0.00	10.00			0.0									
5	277	275									0.14		0.14	0.70	0.27	0.66	11.18	98.4		65.1									
													0.00		0.00	0.00	11.18			0.0									
6	275	273									0.35		0.35	0.70	0.68	22.80	16.70	78.4		1788.8									
													0.00		0.00	8.54	16.70		91.8	784.1	2572.9	CONC	1350	0.35	82.8	3294.2	2.23	0.62	78.1%
7	273	271									0.36		0.36	0.70	0.70	23.50	17.32	76.8		1803.9									
													0.00		0.00	8.54	17.32		89.9	767.1	2571.0	CONC	1350	0.35	80.5	3294.2	2.23	0.60	78.0%
8	271A	271		0.85									0.85	0.80	1.89	1.89	10.00	104.2		197.0									
													0.00		0.00	0.00	10.00			0.0									
9,10	271	M40									0.50		0.50	0.70	0.97	26.37	17.92	75.2		1982.2									
													0.00		0.00	8.54	17.92		88.0	751.3	2733.6	CONC	1350	0.40	82.6	3521.6	2.38	0.58	77.6%
11	269A	M40						2.91					2.91	0.20	1.62	1.62	15.00	83.6		135.2									
													0.00		0.00	0.00	15.00			0.0									
13	267	265							0.30				0.30	0.65	0.54	0.54	10.00	104.2		56.5									
													0.00		0.00	0.00	10.00			0.0									
14	265	M41							0.78	0.40			1.18	0.62	2.02	2.56	15.00	83.6		214.2									
													0.00		0.00	0.00	15.00			0.0									
16	261	259									0.15		0.15	0.55	0.23	0.23	15.00	83.6		19.2									
													0.00		0.00	0.00	15.00			0.0									
													0.00		0.00	0.23	15.59	81.7		18.7									
													0.00		0.00	0.00	15.59			0.0									
17	257	253							0.79				0.79	0.65	1.43	1.66	15.76	81.2		134.5									
													0.00		0.00	0.00	15.76			0.0									
18	255	253							0.19	0.15			0.34	0.61	0.57	0.57	15.00	83.6		47.9									
													0.00		0.00	0.00	15.00			0.0									
19	253	251							0.21	0.38			0.59	0.59	0.96	3.19	17.51	76.2		243.2									
													0.00		0.00	0.00	17.51			0.0									
20	251	M42							0.61				0.61	0.65	1.10	4.29	18.63	73.4		315.1									
													0.00		0.00	0.00	18.63			0.0									

INFORMATION FROM FERNBANK
 CROSSING PHASE 1 & 2
 DEVELOPMENT STORMWATER
 MANAGEMENT REPORT.



Fernbank Crossing - Storm Sewer Design Sheet (Rational Method)

LOCATION			AREA											FLOW					Total Peak Flow (Q) (L/s)	PROPOSED SEWER									
Location	From node	To node	Mixed Use	Park N' Ride Paramedic Post Medium Block	Arterial Road ROW	Schools	Parks	Hydro Corridor	Singles Front Yards	Singles Rear Yard	Towns Front Yard	Towns Rear Yard	Total Area (ha)	Weighted Runoff Coefficient	Indivi 2.78 AR	Accum 2.78 AR	Time of Concentration	Rain Intensity (mm/hr)		Peak Flow (L/s)	Pipe Type	Pipe Size (mm)	Grade (%)	Length (m)	Capacity (l/s)	Full Flow Velocity (m/s)	Time of Flow (min.)	Q/Qfull (%)	
																		5yr											10yr
			0.80	0.80	0.90	0.60	0.40	0.20	0.65	0.55	0.70	0.60																	
21	245	243								0.32			0.32	0.55	0.49	0.49	15.00	83.6		40.9	40.9	PVC	250	0.65	66.9	50.0	0.99	1.13	81.7%
	243	241							0.35				0.00	0.65	0.00	0.00	15.00			0.0		PVC	375	0.65	12.9	147.5	1.29	0.17	60.9%
22	241	M44							0.30	0.30			0.60	0.60	1.00	2.12	16.30	79.6		168.9	168.9	CONC	450	1.00	67.3	297.4	1.81	0.62	56.8%
													0.00		0.00	0.00	16.30			0.0									
24	233A	233	3.32										3.32	0.80	7.38	7.38	10.00	104.2		769.3	769.3	CONC	825	0.45	8.5	1004.6	1.82	0.08	76.6%
													0.00		0.00	0.00	10.00			0.0									
25	233	231									0.35		0.35	0.70	0.68	8.06	10.08	103.8		837.0	837.0	CONC	825	0.45	114.0	1004.6	1.82	1.04	83.3%
													0.00		0.00	0.00	10.08			0.0									
26	231	229									0.24		0.24	0.70	0.47	8.53	11.12	98.6		841.4	841.4	CONC	825	0.50	82.0	1058.9	1.92	0.71	79.5%
													0.00		0.00	0.00	11.12			0.0									
27	237A	237	1.58										1.58	0.80	3.51	3.51	10.00	104.2		366.1	366.1	CONC	600	0.50	9.0	452.9	1.55	0.10	80.8%
													0.00		0.00	0.00	10.00			0.0									
28	237	235									0.15		0.15	0.70	0.29	3.81	10.10	103.7		394.6	394.6	CONC	600	1.40	49.0	757.9	2.60	0.31	52.1%
													0.00		0.00	0.00	10.10			0.0									
29	235	229							0.37				0.37	0.65	0.67	4.47	10.41	102.1		456.7	456.7	CONC	600	1.85	88.1	871.3	2.99	0.49	52.4%
													0.00		0.00	0.00	10.41			0.0									
30	229	227							0.57				0.57	0.65	1.03	14.04	11.83	95.4		1339.2	1339.2	CONC	975	0.50	117.4	1653.2	2.15	0.91	81.0%
													0.00		0.00	0.00	11.83			0.0									
31	227	M45							0.73	0.47			1.20	0.61	2.04	16.07	15.00	83.6		1343.1	1343.1	CONC	975	0.65	120.0	1884.9	2.45	0.82	71.3%
													0.00		0.00	0.00	15.00			0.0									
	223	221											0.00		0.00	0.00	10.00			0.0	0.0	PVC	250	0.65	57.1	50.0	0.99	0.96	0.0%
	221	219											0.00		0.00	0.00	10.00			0.0	0.0	PVC	250	0.65	8.6	50.0	0.99	0.15	0.0%
													0.00		0.00	0.00	10.96			0.0									
33	219	217							0.41	0.50			0.91	0.60	1.51	1.51	15.00	83.6		125.8	125.8	PVC	375	1.00	76.8	182.9	1.60	0.80	68.8%
													0.00		0.00	0.00	15.00			0.0									
34	217	213							0.48				0.48	0.65	0.87	2.37	15.80	81.1		192.3	192.3	CONC	450	1.00	71.7	297.4	1.81	0.66	64.7%
													0.00		0.00	0.00	15.80			0.0									
35	215	213								0.41			0.41	0.55	0.63	0.63	15.00	83.6		52.4	52.4	PVC	300	0.65	42.6	81.3	1.11	0.64	64.4%
													0.00		0.00	0.00	15.00			0.0									
36	213	211							0.25	0.14			0.39	0.61	0.67	3.67	16.46	79.1		290.0	290.0	CONC	600	0.50	64.9	452.9	1.55	0.70	64.0%
													0.00		0.00	0.00	16.46			0.0									
37	211	209							0.25	0.30			0.55	0.60	0.91	4.58	17.15	77.2		353.2	353.2	CONC	675	0.30	78.4	480.3	1.30	1.00	73.5%
													0.00		0.00	0.00	17.15			0.0									
	209	207											0.00		0.00	4.58	18.16	74.6		341.2	341.2	CONC	675	0.30	8.7	480.3	1.30	0.11	71.0%
													0.00		0.00	0.00	18.16			0.0									
38	207	205							0.41	0.21			0.62	0.62	1.06	5.64	18.27	74.3		418.8	418.8	CONC	675	0.45	65.8	588.3	1.59	0.69	71.2%
													0.00		0.00	0.00	18.27			0.0									
	205	203											0.00		0.00	5.64	18.96	72.6		409.4	409.4	CONC	675	0.45	6.0	588.3	1.59	0.06	69.6%
													0.00		0.00	0.00	18.96			0.0									
	203	M46							0.21				0.21	0.65	0.38	6.02	19.02	72.5		436.1	436.1	CONC	750	0.25	66.3	580.7	1.27	0.87	75.1%
													0.00		0.00	0.00	19.02			0.0									

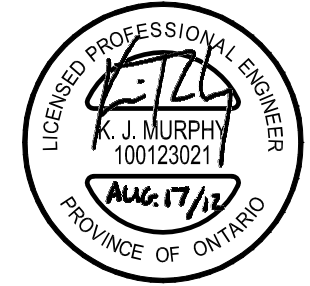
Fernbank Crossing - Storm Sewer Design Sheet (Rational Method)

LOCATION			AREA											FLOW					Total Peak Flow (Q) (L/s)	PROPOSED SEWER									
Location	From node	To node	Mixed Use	Park N' Ride Paramedic Post Medium Block	Arterial Road ROW	Schools	Parks	Hydro Corridor	Singles Front Yards	Singles Rear Yard	Towns Front Yard	Towns Rear Yard	Total Area (ha)	Weighted Runoff Coefficient	Indivi 2.78 AR	Accum 2.78 AR	Time of Concentration	Rain Intensity (mm/hr)		Peak Flow (L/s)	Pipe Type	Size (mm)	Grade (%)	Length (m)	Capacity (l/s)	Full Flow Velocity (m/s)	Time of Flow (min.)	Q/Qfull (%)	
			0.80	0.80	0.90	0.60	0.40	0.20	0.65	0.55	0.70	0.60						5yr		10yr									
South Outlet																													
107	FUT	363		5.15					3.90	1.36			10.41	0.71	20.58	20.58	20.48	69.2		1424.5	CONC	1350	0.20	58.8	2490.2	1.69	0.58	57.2%	
105	391	363		0.64	4.13				0.22				4.13	0.65	0.40	0.40	15.00	83.6		33.2	CONC	1050	0.50	120.4	2014.4	2.25	0.89	72.9%	
101	371	369							0.42	0.09			0.51	0.63	0.90	0.90	15.00	83.6		74.9	PVC	375	0.65	53.5	147.5	1.29	0.69	50.8%	
	369	367											0.00	0.00	0.00	0.90	15.69	81.4		73.0	CONC	450	0.20	50.9	133.0	0.81	1.05	54.9%	
102	367	365							0.35	0.18			0.53	0.62	0.91	1.80	16.74	78.3		141.3	CONC	600	0.15	59.8	248.1	0.85	1.17	57.0%	
103	365A	365		1.39									1.39	0.80	3.09	3.09	10.00	104.2		322.1	CONC	600	0.30	8.7	350.8	1.20	0.12	91.8%	
104	365	363							0.18	0.08			0.26	0.62	0.45	5.34	17.91	75.2		401.8	CONC	825	0.15	66.1	580.0	1.05	1.05	69.3%	
108	363	361							0.20				0.20	0.65	0.36	6.10	20.48	69.2		422.4	CONC	1350	1.74	78.6	7344.9	4.97	0.26	18.7%	
109	361	341							0.34	0.36			0.70	0.60	1.16	7.27	20.74	68.7	81.0	952.2	CONC	1350	1.74	81.1	7344.9	4.97	0.27	19.7%	
111	FUT	341							3.23	1.67			4.90	0.62	8.39	8.39	19.28	71.9		603.1	CONC	825	1.88	86.2	2053.3	3.72	0.39	29.4%	
110	341A	341				2.12							2.12	0.60	3.54	3.54	10.00	104.2		368.4	CONC	675	0.25	12.5	438.5	1.19	0.18	84.0%	
112	341	339							0.18				0.18	0.65	0.33	19.52	21.01	68.1		1329.2	CONC	1650	0.40	67.8	6013.7	2.72	0.41	37.7%	
113	339	337							0.11				0.11	0.65	0.20	19.72	21.43	67.3	79.7	936.8	CONC	1800	0.25	45.2	5995.9	2.28	0.33	37.6%	
114	337	335							0.29				0.29	0.65	0.52	20.24	21.76	66.6	78.7	925.3	CONC	1800	0.25	50.8	5995.9	2.28	0.37	37.8%	
115	335A	335				2.83							2.83	0.60	4.72	4.72	10.00	104.2		491.8	CONC	750	0.25	17.9	580.7	1.27	0.23	84.7%	
116	335	301							0.21				0.21	0.65	0.38	25.34	22.13	65.9		1669.9	CONC	1800	0.30	57.7	6568.2	2.50	0.38	39.2%	
117	FUT	301				1.20			5.13	1.57			7.90	0.59	11.67	11.67	23.33	63.7		743.4	CONC	975	0.61	54.7	1826.0	2.37	0.38	40.7%	
118	301	M97									0.30		0.30	0.70	0.58	37.60	23.76	63.0		2366.8	CONC	1950	0.30	78.3	8131.0	2.64	0.49	39.8%	
119	M97	M98								0.94	0.40		1.34	0.59	2.22	39.81	24.25	62.1	73.6	2473.0	CONC	2100	0.20	78.3	8089.5	2.26	0.58	41.1%	
119	M98	M99											0.00	0.00	0.00	11.76	24.25	61.2	72.7	854.2	CONC	2400	0.15	29.6	10002.3	2.14	0.23	32.8%	

Q = 2.78 AIR WHERE : Q = PEAK FLOW IN LITRES PER SECOND (L/s) A = AREA IN HECTARES (ha) I = RAINFALL INTENSITY IN MILLIMETERS PER HOUR (mm/hr) R = WEIGHTED RUNOFF COEFFICIENT

Q = (1/n) A R(2/3)So(1/2) WHERE : Q = CAPACITY (L/s) n = MANNING COEFFICIENT OF ROUGHNESS (0.013) A = FLOW AREA (m2)

Project: Fernbank Crossing (108180-10) Designed: KJM Checked: MAB Date: August 17 2012



APPENDIX C

Proposed Servicing Sketch

PROPOSED SERVICING SKETCH

