January 2025

Prepared for:

#### CONSEIL DES ÉCOLES PUBLIQUES DE L'EST DE L'ONTARIO

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JLR No.: 33322-001



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#### 1.0 INTRODUCTION

J.L. Richards & Associates Limited (JLR) was retained by Conseil des Écoles publiques de l'Est de l'Ontario (CEPEO) to prepare a Noise Control Detailed Study for their proposed High School located at 2405 & 2419 Mer-Bleue Road, in the Orleans South area of the City of Ottawa. The purpose of this study is to assess the potential environmental noise impact on the site, due to vehicular traffic on Mer-Bleue Road.

This report is prepared to satisfy the Ministry of the Environment, Conservation and Parks (MECP) Environmental Noise Guidelines NPC-300 and the City of Ottawa Environmental Noise Control Guidelines (approved by City Council January 2016) and in particular Part 4 Section 3.2: Phase 2 Noise Control Detailed Study Requirements.

#### 2.0 PROJECT DESCRIPTION

The proposed high school development is situated on a ±6.4 ha parcel of land that is bounded by existing residential to the north and east, Mer-Bleue Road to the west and vacant land to the south, as shown on Figure 1 - Location Plan.

The proposed development will consist of 1 high school approximately 85,000 ft<sup>2</sup> (31 classrooms), a parking area, and outdoor recreation areas as shown on the Site Plan prepared by GRC Architects (January 10, 2025) provided in Appendix 'A'.

#### 3.0 TRANSPORTATION NOISE SOURCE

The transportation noise source is Mer-Bleue Road. Drawing N1 shows the location of the noise source and existing roadways in relation to the proposed development.

#### 3.1 Transportation Sound Level Criteria

For the purpose of determining the predicted noise levels, and based on the sound level criteria established by the City of Ottawa Environmental Noise Control Guidelines (ENCG), the following will be used as the maximum acceptable sound levels (Leq) for residential development and other land uses, such as nursing homes, schools and daycare centres:

Receiver Location	<u>Criteria</u>	<u>Time Period</u>
Outdoor Living Area:	55 dBA	Daytime (0700 - 2300 hrs.)
Indoor Living/Dining Rooms (inside):	45 dBA	Daytime (0700 - 2300 hrs.)
General Office, Reception Area (inside):	50 dBA	Daytime (0700 - 2300 hrs.)
Sleeping Quarters (inside):	40 dBA	Nighttime (2300 - 0700 hrs.)

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DRAWING #:

FIGURE 1

DRAWN:

JLR #:

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Outdoor Living Areas (OLA) are defined as that portion of the outdoor amenity area of a dwelling for the quiet enjoyment of the outdoor environment during the daytime period. Typically, the point of assessment in an OLA is 3.0 m from the building façade mid-point and 1.5 m above the ground within the designated OLA for each individual unit. OLAs commonly include backyards, balconies (with a minimum depth of 4 m as per NPC-300), common outdoor living areas, and passive recreational areas.

#### 3.2 Transportation Noise Attenuation Requirements

When the sound levels are equal to or less than the specified criteria, per the City of Ottawa ENCG and/or MOE NPC-300, no noise attenuation (control) measures are required.

The following tables outline noise attenuation measures to achieve required dBA Leq for surface transportation noise, per the City of Ottawa ENCG.

**Table 1: Outdoor Noise Control Measures for Surface Transportation Noise** 

	Secondary Mitigation Measures			
Primary Mitigation Measure (in order of preference)	Landscape Plantings and/or Non-acoustic Fence to Obscure Noise Source	Warning Clauses		
Distance setback with soft ground Insertion of Noise insensitive land uses between the source and receiver receptor	Recommended			
Orientation of buildings to provide sheltered zones in rear yards Shared outdoor amenity areas Earth berms (sound barriers) Acoustic barriers (acoustic barriers)	Required	<ul> <li>Warning Clauses necessary and to include:</li> <li>Reference to specific noise mitigation measures in the development.</li> <li>Whether noise is expected to increase in the future.</li> <li>That there is a need to maintain mitigation.</li> </ul>		

**Table 2: Indoor Noise Control Measures for Surface Transportation Noise** 

	Secondary Mitigation Measures			
Primary Mitigation Measure (in order of preference)	Landscape Plantings and/or Non-acoustic Fence to Obscure Noise Source	Warning Clauses		
Distance setback with soft ground Insertion of Noise insensitive land uses between the source and receiver receptor	Recommended	Not necessary		
Orientation of buildings to provide sheltered zones or modified interior spaces and amenity areas	Required	Warning Clauses necessary and to include:		

Enhanced construction techniques and construction quality	- Reference to specific noise mitigation measures in the
Earth berms (sound barriers)	development.
Indoor isolation – air conditioning and ventilation, enhanced dampening	- Whether noise is expected to increase in the future.
materials (indoor isolation)	- That there is a need to maintain mitigation.

The following tables outline the noise level limits per the MOE NPC-300 and City of Ottawa ENCG.

Table 3: Outdoor Living Area (OLA) Noise Limit for Surface Transportation

Time Period	Leq (16 hr) (dBA)
16 hr., 07:00 am - 23:00	55

**Table 4: Indoor Noise Limit for Surface Transportation** 

Type of Space	Time Period	Leq (dBA)	
Type of Space	Time Period	Road	Rail
Living/dining, den areas of residences, hospitals, nursing homes, schools, daycare centres, etc.	07:00-23:00	45	40
Living/dining, den areas of residences, hospitals, nursing homes, etc. (except schools or daycare centres)	23:00-07:00	45	40
Slooping quarters	07:00-23:00	45	40
Sleeping quarters	23:00-07:00	40	35

In addition to the implementation of noise attenuation features, if required, and depending on the severity of the noise problem, warning clauses may be recommended to advise the prospective purchasers/tenants of affected units of the potential environmental noise. These warning clauses should be included in the Site Plan Agreement and should be registered on Title. Warning clauses may be included for any development, irrespective of whether it is considered a noise sensitive land use.

Where site measures are required to mitigate noise levels, the City of Ottawa requires that notices be placed on Title informing potential buyers and/or tenants of the site conditions. Sample templates of the notices that could be registered on Title are included in Appendix 'B' as presented in the City of Ottawa ENCG.

Detailed wording for clauses should be provided as part of a detailed Noise Impact Study to be completed in support of the Site Plan Application. Clauses are to be worded to describe the mitigation measures and noise conditions applicable where MOE and City of Ottawa noise criteria are exceeded.

#### 3.3 Prediction of Noise Levels

#### 3.3.1 Road Traffic Data

The following traffic data was used to predict noise levels:

Table 5: Road Traffic Data to Predict Noise Levels

	Mer-Bleue Road	
Total Traffic Volume (AADT)	35,000	
Day/Night Split (%)	92/8	
Medium Trucks (%)	7	
Heavy Trucks (%)	5	
Posted Speed (km/hr.)	60	
Road Gradient (%)	1	
Road Classification	4-Lane Urban Arterial-Divided (4-UAD)	

Schedules 'C4' and 'C16' of the City of Ottawa Official Plan Adopted By-Law 2021-386 were utilized to determine the road classification and protected right-of-way. These findings were then compared to Table B1 (Part 4, Appendix 'B') of the City of Ottawa Environmental Noise Control Guidelines to determine an appropriate AADT value.

#### 3.3.2 Noise Level Calculations

The noise levels for the daytime and nighttime periods were calculated for a number of representative receivers described in 6 and shown on Drawing N1, using the MOE Road Traffic Noise Computer program STAMSON, Version 5.03.

Computer printouts are included in Appendix 'B'.

Table 6: Predicted Freefield Noise Levels and Distances from Noise Sources

		Noise Lev	rels (dBA)
Receiver No. and File Names	Receiver Description and Location	Daytime	Nighttime
R1 MB_R1	Plane of Window (front) fronting on Mer Bleue Road, at a distance of 15.7 m from the centerline of Mer Bleue Road Northbound and 29.7 m from the centerline of Mer Bleue Road Southbound.	70.23	n/a
R2 MB_R2	Plane of Window (front) fronting on Mer Bleue Road, at a distance of 35.4 m from the centerline of Mer Bleue Road Northbound and 49.8 m from the centerline of Mer Bleue Road Southbound.	65.10	n/a

#### 3.4 Summary of Findings (Transportation)

A summary of the minimum noise requirements and required Warning Clauses is shown on Table 7. The facility will require notices to be registered on Title as part of the Site Plan Agreement, advising the occupants of the environmental noise problems and/or of the noise attenuation measures being implemented.

**Table 7: Minimum Required Control Features/Warning Clauses (Transportation)** 

Receiver Location	Noise Attenuation Barrier	Central Air Conditioning	Forced Air Heating	Warning Clauses	Building Components Study
Plane of Window – Front Façade	n/a	Provisional	Yes	Type 'A'	Yes

#### 3.5 Summary of Findings (Preliminary Building Component)

JLR completed preliminary building component analysis of the cafeteria curtain wall to determine if sufficient acoustical mitigation is provided with the proposed window assembly to mitigate interior noise levels to MECP and City of Ottawa criteria. The Acoustical Insulation Factor (AIF) Method, as described in the Ministry of the Environment Ontario, Ontario Publication, Environmental Noise Assessment in Land Use Planning (ENALUP) 1987 (Page 10-29), was used; to assess the building construction required to mitigate exterior noise to meet interior noise criteria. A freefield noise level of 70 dBA was conservatively utilized to determine minimum wall and window construction.

CEPEO provided floor plan and building elevation drawings, for the Orleans South High School. Floor and elevation drawings are included in Appendix 'C'. Using the CEPEO drawings, JLR calculated the window and floor areas for the cafeteria. This data was then used to calculate the window to floor area ratios. Design tables provided in ENALUP were then utilized to identify minimum window construction requirements to mitigate the plane of window noise levels. Table 13 in Appendix 'D' presents the working calculations for the window requirements necessary to

acoustically insulate the cafeteria. The following table presents a summary of the analysis with the minimum standard window required.

**Table 8: Minimum Window and Wall Construction Types** 

Unit Type	Representative Window Type Glass Thickness (Spacing) Glass Thickness	Representative Exterior Wall Type	
Orleans South High School Cafeteria	6(6)6 Double Pane	n/a	

For this analysis, glass doors identified on the plans are treated as a window. The acoustic insulation factor methodology does not account for glass doors as a door type. It is noted that no additional doors are identified with a connection to the noise sensitive interior room.

It should be noted that other types of windows could be chosen to achieve the same minimum noise mitigation. These details will be established during the detailed building component study in consultation with CEPEO.

Tables A2 and A3 from Canada Mortgage and Housing's (CMHC) publication, Airport Noise, revised 1981 were used to convert AIF values to the more widely recognized Sound Transmission Class (STC) values. Appendix 'E' presents these CMHC tables.

AIF and equivalent STC values are presented in Table 9 for the town unit bedroom with the highest AIF requirement. It is recommended that at the time of building permit application that the AIF/STC be confirmed to suit the specific unit proposed for the Block.

Table 9: AIF Value Conversion to STC Value

	Windows			Walls			
Type of Unit	AIF Req.	Window/ Floor Area Ratio	AIF Conversion Formula	STC	Wall/Floor Area Ratio	AIF Conversion Formula	STC
Orleans South High School Cafeteria	30	33%	STC	31	n/a	n/a	n/a

# 4.0 OPINION OF PROBABLE COSTS (OPC) FOR MITIGATION MEASURES

Based on the results of the analysis identified in this report, additional noise mitigation measures are not required. The construction materials and cooling units chosen by the design team meet or exceed the minimum noise mitigation requirements.

# 5.0 STATIONARY NOISE SOURCES

The stationary noise sources for this study are the air handling units installed on the building rooftop. The Noise Impact Assessment Stationary Noise Source Drawing N2 (refer to Appendix 'A') shows the approximate location and distances of the proposed air handling units in relation to the existing adjacent developments.

#### 5.1 Stationary Source Sound Level Criteria

The stationary sound level criteria within a community are largely dependent on its location within the City. In the Ministry of the Environment (MOE) guideline NPC-300 and the City's ENCG there are four separate community class areas which are defined by their ambient sound level (see Table 10).

Table 10: Area Classes for Definition of Stationary Noise Ambient Sound Level (From the City's ENCG, Part 1 Table 3.0)

Class 1	Means an area with an acoustical environment typical of a major population centre, where the background sound level is dominated by the activities of people, usually road traffic, often referred to as "urban hum". Within the City Class 1 areas generally include all of the urban area as well as lands in proximity to Employment Lands and the 416/417 corridor.
Class 2	Means an area with an acoustical environment that has qualities representative of both Class 1 and Class 3 areas. These are the suburban areas of the City outside of the busy core where the urban hum is evident but within the urban boundary. Class 2 areas also include core areas of large and medium sized villages such as Manotick, Greely, Richmond, Carp and Metcalfe. Class 2 areas have the following characteristics:  i. sound levels characteristic of Class 1 during daytime (07:00 to 19:00 or to 23:00 hours); and ii. low evening and night background sound level defined by natural environment and infrequent human activity starting as early as 19:00 hours (19:00 or 23:00 to 07:00 hours).
Class 3	Means a rural area with an acoustical environment that is dominated by natural sounds having little or no road traffic, such as:  i. a small community or village; ii. agricultural area; iii. a rural recreational area such as a cottage or a resort area; or iv. a wilderness area.  Within the City, Class 3 areas are found in the rural area, Greenbelt and within small residential oriented villages such as Kinburn, Ashton, Sarsfield and Constance Bay.
Class 4	Means an area or specific site that would otherwise be defined as Class 1 or 2 and which: i. is an area intended for development with new noise sensitive land use(s) that are not yet built; ii. is in proximity to existing, lawfully established stationary source(s); and iii. has formal confirmation (designation) from the City of the Class 4 area classification through Council approval.  This classification may not be applied retroactively. Existing noise sensitive land use(s) cannot be classified as Class 4 areas until these land uses are replaced, redeveloped or rebuilt. Class 4 is only applied on a property-by-property basis and, if the noise source is removed (i.e., the Provincial ECA is removed or lapses), the classification will become consistent with that of the adjacent lands (either Class 1 or 2). Finally, lands adjacent to undeveloped industrially zoned properties or areas defined as employment lands in the Official Plan may not be classified Class 4.  Class 4 is considered to be an extraordinary circumstance that, while proposed by an applicant, can only be classified through a City or Ontario Municipal Board approval of a Planning Act application and accompanying noise study. A list and schedule for each Class 4 area that have been approved by the City is found in Appendix E.

For the purpose of determining the predicted noise levels, the sound level criteria established by the City's ENCG and the NPC-300, Tables 11 and 12 will be used as the maximum acceptable sound levels (Leq) for the existing residential development, which is noise sensitive land use. The high school is defined by Class 2.

Table 11: Guidelines for Stationary Noise – Steady and Varying Sound (From MOE NPC-300, Table C-6)

Time of Day	Class 1 Area		Class 2 Area		Class 3	Area	Class 4 Area	
-	Outdoor Point of Reception	Plane of Window						
07:00- 19:00	50	50	50	50	45	45	55	60
19:00- 23:00	50	50	45	50	40	40	55	60
23:00- 07:00	-	45	1	45	1	40	-	55

Table 12: Guidelines for Stationary Noise – Impulsive Sound (From City's ENCG, Part 1 Table 3.2b and MOE NPC-300, Tables C-7 and C-8)

Time of Day	No. of Impulses in Period of One- hour	Class 1 Area		Class 2 Area		Class 3 Area		Class 4 Area	
		Outdoor	Plane	Outdoor	Plane	Outdoor	Plane	Outdoor	Plane
		Point of	of Window						
		Reception		Reception		Reception		Reception	
	<u>&gt;</u> 9	50	50	50	50	45	45	55	60
	7 to 8	55	55	55	55	50	50	60	65
07:00-	5 to 6	60	60	60	60	55	55	65	70
23:00	4	65	65	65	65	60	60	70	75
23.00	3	70	70	70	70	65	65	75	80
	2	75	75	75	75	70	70	80	85
	1	80	80	80	80	75	75	85	90
	<u>&gt;</u> 9	-	45	-	45	-	40	-	55
	7 to 8	-	50	-	50	-	45	-	60
22:00	5 to 6	-	55	-	55	-	50	-	65
23:00- 07:00	4	-	60	-	60	-	55	-	70
	3	-	65	-	65	-	60	-	75
	2	-	70	-	70	-	65	-	80
	1	-	75	-	75	-	70	-	85

#### 5.2 Stationary Source Noise Requirements

When the sound levels are equal to or less than the specified criteria per Tables 11 and 12 no noise attenuation (control) measures are required.

The following Table 13 outlines noise attenuation measures which can be implemented to reduce the noise levels for stationary noise sources to the specified criteria, per the City of Ottawa ENCG.

**Table 13: Noise Control Measures for New Stationary Noise Sources** (From City's ENCG, Part 1 Table 3.3b)

Primary Mitigation Measure	Secondary Mitigation Measures		
(in order of preference)	Landscape plantings and/or non-acoustic fence to obscure noise source		
Earth berms (sound barriers)			
Development of non-noise producing and insensitive land uses between the source and sensitive receptor within facility.	Poguirod		
Development of additional related uses with enhanced construction and materials within facility between source and sensitive receptor.	Required		
Acoustic Barriers (acoustic barriers)			

#### 5.3 **Prediction of Freefield Noise Levels (Stationary)**

#### 5.3.1 Rooftop Unit Data

Table 14 summarizes the rooftop air handling unit data that was provided by the project mechanical engineer from the equipment supplier AAON (refer to Appendix 'F' for more detailed information) to predict noise levels.

**Table 14: Rooftop Unit Data** 

Unit	No. of Air Handling Units (Capacity)	Sound Levels for Rooftop Units at the Source, each @ 75% capacity	Approximate Height of Building	
DOAS 1-ASHP	1 (RN 50 Ton)	89.0 dBA	12.0m (Roof Level 5)	
DOAS GYM-ASHP	1 (RN 6 Ton)	74.0 dBA	4.0 m (Roof Level 1)	
Fluid Cooler - FEVR-26408 (Fans)	2	91.0 dBA	8.0 m (Roof Level 2)	
RTU1 GYM1-ASHP; RTU2 GYM2-ASHP;	2 (RN 11 Ton)	77.0 dBA	10.0 m (Roof Level 3)	
RTU4 CAFE Perimeter- ASHP	2 (RN 11 Ton)	77.0 dBA	8.0 m (Roof Level 2)	
RTU3 CAFE-ASHP	1 (RN 16 Ton)	84.0 dBA	8.0 m (Roof Level 2)	
Kitchen Exhaust Fan 1		66.0 dBA	8.0 m (Roof Level 2)	
Make-Up Exhaust Fan	1	78.0 dBA	8.0 m (Roof Level 2)	

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The typical practice for commercial developments is for the supply fan in a heating and cooling rooftop unit to be running continuously during normal operating hours. Whereas the compressor turns on and off at various times during the day, depending on cooling demands. The noise level difference between the fan continuously running and the compressor turning on is considered negligible. For the purposes of this Study, it is assumed that all of the heating and cooling units are running 24 hr/day at 75% capacity.

The existing residential dwellings fronting on Willow Aster Circle are 2-storey townhouses. The existing residential dwellings fronting on Mer Bleue Road are single storey dwellings. For the purposes of this Study, it is assumed that the point of reception for the plane of window is 2.5 m above the ground for the first level and the point of reception is 4.5 metres above the ground for the second-floor bedroom windows. As summarized in Table 14, the High School has various roof levels.

#### 5.3.2 Rooftop Unit Noise Level Calculations

Table 12 summarizes the sound pressure level data provided for the respective rooftop units. The following formula (from the 2005 ASHRAE Fundamentals Handbook, page 7.3 (12)) was used to combine decibel levels and determine a representative total decibel level on the rooftop of each commercial building.

The following formula (from the 2005 ASHRAE Fundamentals Handbook, page 7.8 (28)) was then used to determine a corresponding value at the exterior wall of the closest residential dwelling units.

Free Field Lp=Lw+10log(Q/(4 pi r^2))+10.5
Lp = Sound Pressure
Lw = Sound Power
Q = Directivity = 2 flat surface, 4 junction two large surfaces,
8 in a corner
r = distance from source in ft

Noise receivers R3, R4 and R5 represent the existing residential dwellings as shown on Drawing N2. Results have been summarized in Table 15, refer to Appendix 'G' for detailed calculations.

**Table 15: Estimated Stationary Noise Levels (Air Handling Units)** 

Representative Sound Pressure Level on Roof (total	Distance to Closest Noise- Sensitive Receptor			Estimated Freefield Sound Pressure Level at Rear Wall o Closest Noise-Sensitive Receptors		
for all units)	R3	R4	R5	R3	R4	R5
95.8 dBA	75.7m	98.8m	88.1m	48.5 dBA	46.1 dBA	46.9 dBA

#### 5.3.3 Rooftop Unit Summary of Findings

The results indicate that the City's stationary noise criterion will not be exceeded. As noted previously, these results assume that all the rooftop units will be operating simultaneously 24 hours a day at 75% capacity using the air handling units selected by the Mechanical consultant. Depending on commercial building occupancy, this could vary over time. Further to this, the criteria have not been adjusted to account for the background noise levels associated with vehicular traffic on Mer Bleue Road. Based on the transportation analysis of this report Mer Bleue is predicted to generate 70 dBA. Comparing the 70 dBA noise level to the predicted stationary noise level at receiver R3 (43.9 dBA) and using the nomograph method to add decibels, it can be expected that the noise levels will not be affected with the addition of the proposed stationary noise source. Regardless, a conservative analytic approach has been used to predict the noise levels from the proposed stationary noise source.

In addition, the results presented are conservative for the following reasons:

- Shielding of noise by the various school rooflines has not been accounted for in the calculations.
- Both air compressors and supply fans are assumed to operate 24 hours per day whereas normal operation allows compressors to turn on & off as required.

#### 6.0 CONCLUSION AND RECOMMENDATIONS

Predicted transportation noise levels are expected to exceed the City of Ottawa ENCG and MECP criteria at the plane of window of the cafeteria. Based on preliminary building component analysis, the standard building materials and cooling units being proposed no additional mitigation measures are required.

Predicted stationary noise levels generated from the high school are **not** expected to exceed the City of Ottawa ENCG and MECP criteria at the closest adjacent residential units.

#### 6.1 Indoor Noise Control Features

#### 6.1.1 Heating System

The High School shall be fitted with a forced air heating system or equivalent system.

#### 6.1.2 Cooling System

The High School shall be fitted with a central air conditioning system or equivalent system.

#### 6.2 Warning Clauses

#### 6.2.1 Warning Clause Type A

Clause A is to be registered on Title for the High School

"Purchasers/tenants are advised that despite the inclusion of noise control features within the building units, sound levels due to increasing road/transitway/rail/light rail traffic may, on occasion, interfere with some activities of the dwelling occupants as the sound levels exceed the sound level limits of the City and the Ministry of the Environment.

To help address the need for sound attenuation this dwelling unit includes:

- single/multi-pane glass windows;
- Central air conditioning.

To ensure that provincial sound level limits are not exceeded it is important to maintain these sound attenuation features.

This dwelling unit has been supplied with a central air conditioning system and other measures which will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the sound level limits of the City and the Ministry of the Environment."

#### 6.3 Site Plan Agreement and Notices on Title

It is recommended that the previous recommendations and Warning Clauses are to be included in the Site Plan Agreement and in the Sale and/or lease of the affected facility and be registered on Title.

#### 6.4 Building Permit Requirements

A report prepared and stamped by a Professional Engineer / Acoustical Consultant detailing building components (e.g., glazing/window, wall sections) to provide acoustical insulation to

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satisfy the City of Ottawa Environmental Noise Control Guidelines for indoor noise levels is required prior to the issuance of a Building Permit.

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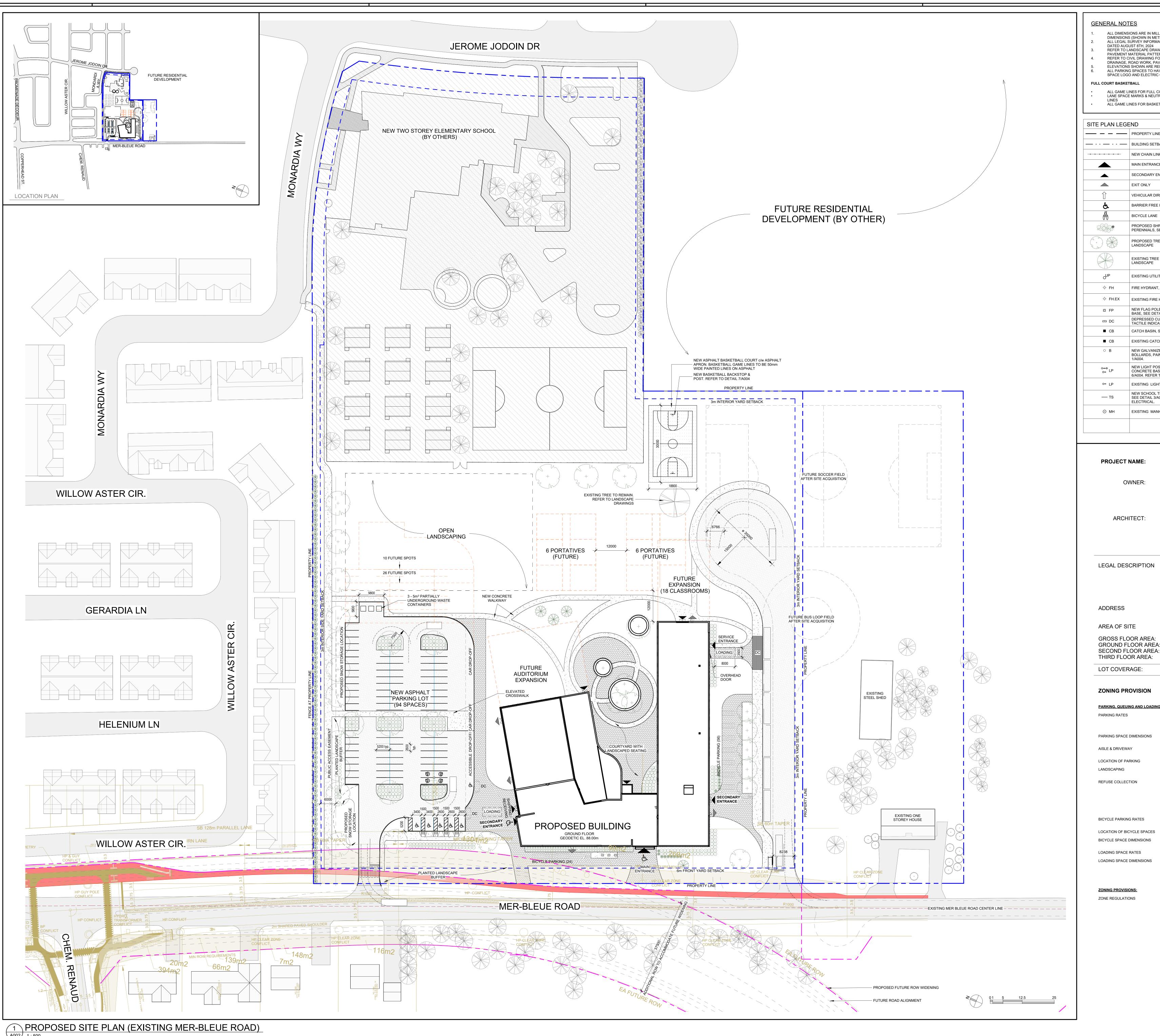
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Noise Control Detailed Study	
Proposed High School – ESP Orleans S	outh

# Appendix A

Drawings



**GENERAL NOTES** 

- ALL DIMENSIONS ARE IN MILLIMETERS EXCEPT GRADE, FLOOR ELEVATIONS AND PROPERTY LINE DIMENSIONS (SHOWN IN METERS).
  ALL LEGAL SURVEY INFORMATION OBTAINED FROM SURVEY PLANS PREPARED BY: CALLON DIETZ INC.,
- DATED AUGUST 8TH, 2024
  REFER TO LANDSCAPE DRAWINGS FOR SIDEWALK, CONCRETE CURBS, SOFT/HARD LANDSCAPING, AND
- PAVEMENT MATERIAL PATTERN LAYOUT.

  REFER TO CIVIL DRAWING FOR CATCH BASINS, MANHOLES, SITE SERVICES, SITE GRADING, SURFACE DRAINAGE, ROAD WORK, PAVEMENT, SIDEWALK AND CONCRETE CURBS. ELEVATIONS SHOWN ARE REFERRED TO GEODETIC DATUM. ALL PARKING SPACES TO HAVE 100mm WIDE PAINTED LINES ON ASPHALT, INCLUDING ACCESSIBLE PARKING SPACE LOGO AND ELECTRIC CAR CHARGING LOGO AS ILLUSTRATED.

  - ALL GAME LINES FOR FULL COURT BASKETBALL TO BE PAINTED WHITE, UNLESS NOTED OTHERWISE LANE SPACE MARKS & NEUTRAL ZONE MARKS TO BE PAINTED A CONTRASTING COLOR TO THE BOUNDING ALL GAME LINES FOR BASKETBALL TO BE 50mm WIDE, UNLESS NOTED OTHERWISE.

SITE PLAN LEGE	-ND	SITE PLAN LEGE	ND - HATCH PATTERN	
	PROPERTY LINE	51121231122	PROPOSED PRECAST	
	BUILDING SETBACK		CONCRETE PAVERS, REFER TO LANDSCAPE DRAWINGS	
-0-0-0-0-0-0-	NEW CHAIN LINK FENCE		PROPOSED PERMEABLE PAVERS, REFER TO LANDSCAPE DRAWINGS	
	MAIN ENTRANCE			
_	SECONDARY ENTRANCE		PROPOSED CONCRETE, REFER TO LANDSCAPE	
	EXIT ONLY		DRAWINGS	
	VEHICULAR DIRECTION		PROPOSED MULCH, REFER TO	
<u> </u>	BARRIER FREE PARKING STALL		LANDSCAPE DRAWINGS	
	BICYCLE LANE		PROPOSED HEAVY DUTY	
0000	PROPOSED SHRUBS & PERENNIALS, SEE LANDSCAPE		ASPHALT, REFER TO CIVIL DRAWINGS	
+	PROPOSED TREE, SEE LANDSCAPE		PROPOSED LIGHT DUTY ASPHALT, REFER TO CIVIL DRAWINGS	
	EXISTING TREE TO REMAIN, SEE LANDSCAPE		EXISTING ASPHALT	
O <sup>UP</sup>	EXISTING UTILITY POLE		EXISTING ASPRALT	
∲ FH	FIRE HYDRANT, SEE CIVIL			
∳ FH.EX	EXISTING FIRE HYDRANT			
□ FP	NEW FLAG POLE C/W CONCRETE BASE, SEE DETAIL 2/A004.			
₪ DC	DEPRESSED CURB WITH TACTILE INDICATOR			
■ СВ	CATCH BASIN, SEE CIVIL			

EXISTING CATCH BASIN

NEW GALVANIZED STEEL

NEW LIGHT POST C/W CONCRETE BASE. SEE DETAIL

EXISTING LIGHT POST

EXISTING MANHOLE

BOLLARDS, PAINTED. SEE DETAIL

6/A004. REFER TO ELECTRICAL.

NEW SCHOOL TITLE SIGNAGE SEE DETAIL 3/A004. REFER TO

> **REPEAT HIGHSCHOOL STUDY -ORLEANS**

CONSEIL DES ÉCOLES PUBLIQUES DE L'EST

DE L'ONTARIO (CEPEO) 2445 ST-LAURENT BLVD, OTTAWA, ON K1G 6C3 T: 613 742-8960

GRC ARCHITECTS 401-47 CLARENCE STREET, ARCHITECT OTTAWA, ON K1N 9K1

T: 613 241 8203 F: 613 241 4180

PART OF LOT 4

CONCESSION 11 (GEOGRAPHIC TOWNSHIP OF CUMBERLAND) PIN: 14563-1816(LT) & 14563-0513(LT) & 14563-0514(LT)

2405 & 2419, MER-BLEUE ROAD **ADDRESS** OTTAWA, ON K4A 3V1 GROUND FLOOR AREA: 1,949m² (20 981ft<sup>2</sup>)

1,637m<sup>2</sup> (17 622ft<sup>2</sup>) LOT COVERAGE:

**ZONING PROVISION PROVIDED** 88 Standard Spaces (3/Classroom x [31 Classrooms]) 2 'Type A' Accessible Spaces 'Type B' Accessible Spaces 93 Total Spaces

5.2m length 6.0m driveway 107.(1) (a)(ii): 6.0m driveway lane 107.(1) (c)(i): 6.7m aisle width >6.7m aisle width LOCATION OF PARKING 110.(1) (a),(b): min. 15% of parking lot

> min.3m from other lot line yes waste stored below gra with soft landscaping

> > 3.5m width

7.0m length

BICYCLE PARKING RATES Table 111A(d): 1 space per 100m<sup>2</sup> LOCATION OF BICYCLE SPACES 111.(3),(4),(6),(7),(9) BICYCLE SPACE DIMENSIONS 111.(9) 1.5m access aisle 1.5m acces aisle LOADING SPACE RATES Table 113A(a): 1 space LOADING SPACE DIMENSIONS Table 113B(a)(i): 6.0m driveway width >6.0m driveway width Table 113B(b)(i): 5.0m access width 7.5m access width

Table 113B(c): 3.5m min width

Table 113B(d)(ii): 7.0m min length

Table 113B(f):

**ZONING PROVISIONS:** ZONE REGULATIONS

INSTITUTIONAL ZONE I1A[2530]/R3Z , Schedule 1/1A - Area D(Rural) Table 170A (a): 15m min lot width (b): 400m² min lot area (c): 6m front yard setback >6m setback (Along Mer-Bleue Rd) (d): 7.5m rear yard setback >7.5m setback (e): 3m side yard setback >3m setback (f): 4.5m corner side yard >4.5m setback

(g): 20m max or 4 storeys building height 13m max height

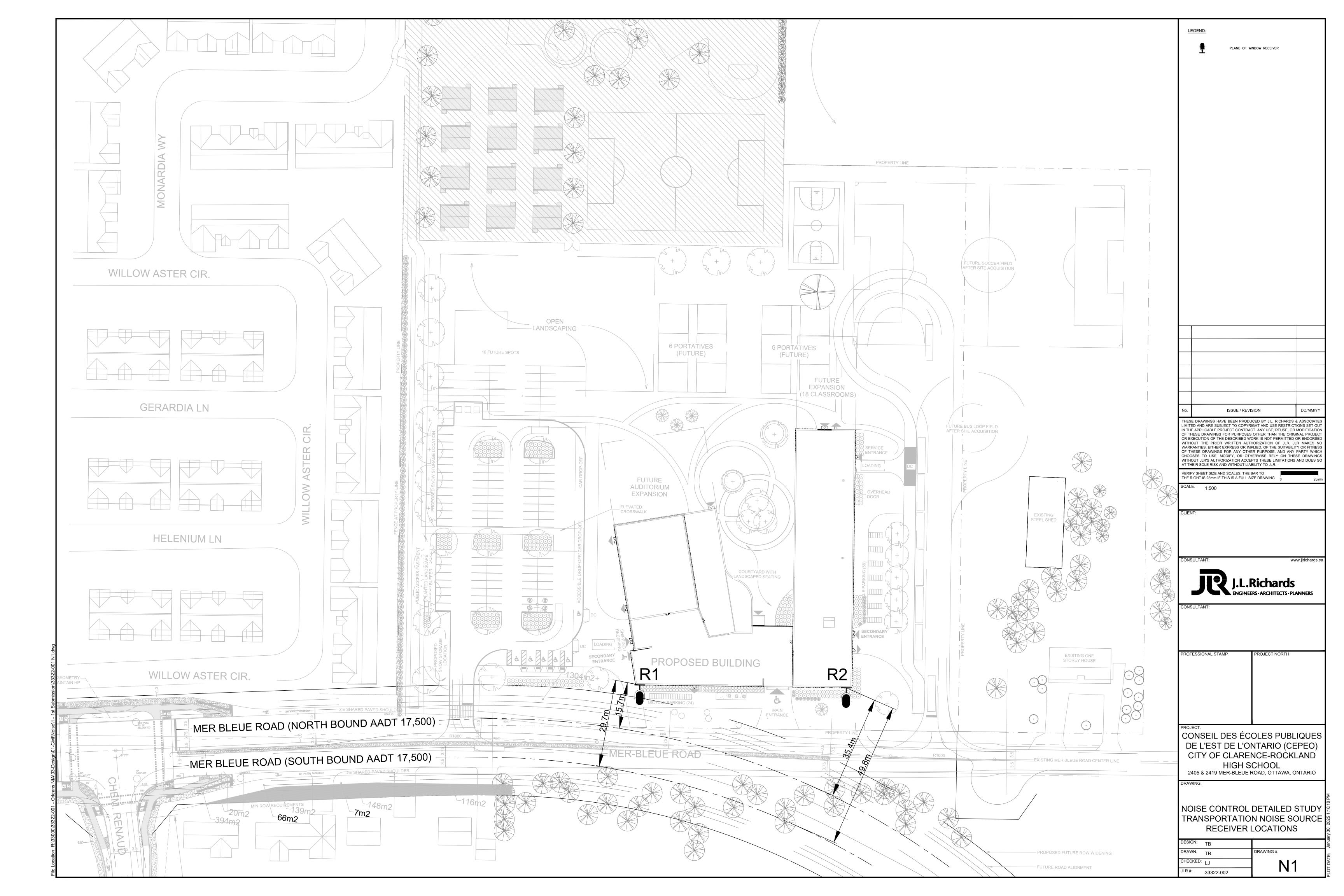
A PROVENCHER\_ROY COMPANY 47 Clarence Street, Suite 401 Ottawa, Ontario K1N 9K1 info@grcarchitects.com www.grcarchitects.com t:613-241-8203 f: 613-241-41-80

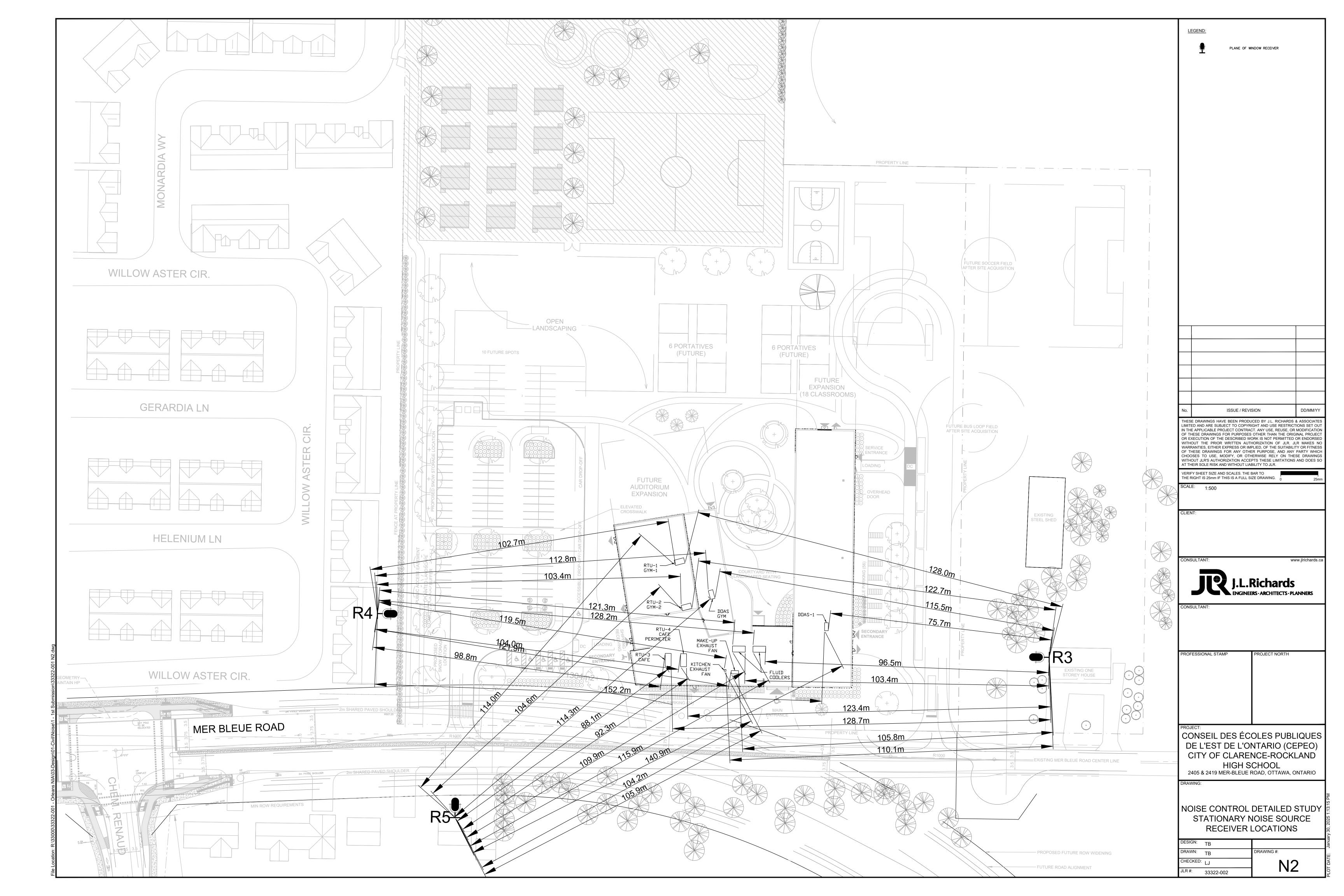
PROPOSED HIGH SCHOOL - ÉSP ORLEANS SUD

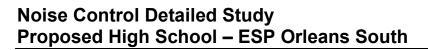
PROPOSED SITE PLAN

date	NOV 05, 2024	job. no.
scale	As indicated	3024
drawn	DH	drawing no.
approved	CJ/PD	A002
plot date	2025-01-10 5:10:40 PM	AUUZ
		•

. DO NOT SCALE FROM THIS DRAWING . CONTRACTOR TO VERIFY ALL DIMENSIONS AND NOTIFY THE ARCHITECT OF ANY DISCREPANCIES BEFORE WORK COMMENCES 3. THIS DRAWING TO BE READ IN CONJUNCTION WITH THE FOLLOWING DRAWINGS: STRUCTURAL, MECHANICAL, ELECTRICAL







# **Appendix B**

Transportation Noise Source Predictions

NORMAL REPORT STAMSON 5.0 Date: 17-01-2025 14:05:50

MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: MB R1.te Time Period: Day/Night 16/8 hours

Description: Orleans South HS Plane of Window R1

Road data, segment # 1: MerBleueN (day/night) \_\_\_\_\_

Car traffic volume : 14168/1232 veh/TimePeriod \* Medium truck volume : 1127/98 veh/TimePeriod Heavy truck volume : 805/70 veh/TimePeriod \*

Posted speed limit : 60 km/h Road gradient : 1 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500 Percentage of Annual Growth : 0.00 Number of Years of Growth : 0.00 Medium Truck % of Total Volume : 7.00 Heavy Truck % of Total Volume : 5.00 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: MerBleueN (day/night) -----

Angle1 Angle2 : -90.00 deg

90.00 deg Wood depth 0 (No woods.)

No of house rows 0 / 0

(Absorptive ground surface) Surface 1

Receiver source distance : 15.70 / 15.70 m Receiver height : 2.25 / 4.50

Topography 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

Road data, segment # 2: MerBleueS (day/night)

\_\_\_\_\_

Car traffic volume : 14168/1232 veh/TimePeriod Medium truck volume : 1127/98 veh/TimePeriod \* Heavy truck volume : 805/70 veh/TimePeriod \*

Posted speed limit : 60 km/h 1 % Road gradient :

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500 Percentage of Annual Growth 0.00 Number of Years of Growth : 0.00 Medium Truck % of Total Volume : 7.00 Heavy Truck % of Total Volume : 5.00 Day (16 hrs) % of Total Volume : 92.00

#### Data for Segment # 2: MerBleueS (day/night)

-----

Angle1 Angle2 : -90.00 deg 90.00 deg Wood depth : 0 (No woods No of house rows : 0 / 0 Surface : 1 (Absorptive (No woods.)

1 (Absorptive ground surface)

Receiver source distance : 29.70 / 29.70 m

Receiver height : 2.25 / 4.50 m
Topography : 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

Results segment # 1: MerBleueN (day)

\_\_\_\_\_\_

Source height = 1.50 m

ROAD (0.00 + 68.92 + 0.00) = 68.92 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq -----

-90 90 0.64 70.67 0.00 -0.32 -1.42 0.00 0.00 0.00 68.92 \_\_\_\_\_\_

Segment Leq: 68.92 dBA

Results segment # 2: MerBleueS (day)

\_\_\_\_\_\_

Source height = 1.50 m

ROAD (0.00 + 64.39 + 0.00) = 64.39 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

\_\_\_\_\_\_ -90 90 0.64 70.67 0.00 -4.86 -1.42 0.00 0.00 0.00 64.39

\_\_\_\_\_\_

Segment Leq: 64.39 dBA

Total Leq All Segments: 70.23 dBA

Results segment # 1: MerBleueN (night)

Source height = 1.50 m

ROAD (0.00 + 61.46 + 0.00) = 61.46 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

-90 90 0.57 63.07 0.00 -0.31 -1.30 0.00 0.00 0.00 61.46

Segment Leq: 61.46 dBA

Results segment # 2: MerBleueS (night)

Source height = 1.50 m

ROAD (0.00 + 57.11 + 0.00) = 57.11 dBA

-----

Segment Leq: 57.11 dBA

Total Leq All Segments: 62.82 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 70.23 (NIGHT): 62.82

STAMSON 5.0 NORMAL REPORT Date: 20-01-2025 09:38:09

MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: mb r2.te Time Period: Day/Night 16/8 hours

Description: Orleans South HS Plane of Window R2

Road data, segment # 1: MerBleueN (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod

Medium truck volume : 1127/98 veh/TimePeriod \* Heavy truck volume : 805/70 veh/TimePeriod \*

Posted speed limit : 60 km/h Road gradient : 1 %

Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500 Percentage of Annual Growth : 0.00 Number of Years of Growth : 0.00 Medium Truck % of Total Volume : 7.00 Heavy Truck % of Total Volume : 5.00 Day (16 hrs) % of Total Volume : 92.00

#### Data for Segment # 1: MerBleueN (day/night)

-----

Angle1 Angle2 : -90.00 deg 90.00 deg Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)

Receiver source distance : 35.40 / 15.70 m Receiver height : 2.25 / 4.50 m

: 1 (Flat/gentle slope; no barrier) Topography

Reference angle : 0.00

#### Road data, segment # 2: MerBleueS (day/night)

\_\_\_\_\_

Car traffic volume : 14168/1232 veh/TimePeriod \* Medium truck volume : 1127/98 veh/TimePeriod \* Heavy truck volume : 805/70 veh/TimePeriod \*

Posted speed limit : 60 km/h

Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500 Percentage of Annual Growth : 0.00 Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00 Day (16 hrs) % of Total Volume : 92.00

#### Data for Segment # 2: MerBleueS (day/night)

-----

Angle1 Angle2 : -90.00 deg 90.00 deg Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)

Receiver source distance : 49.80 / 29.70 m Receiver height : 2.25 / 4.50 m

: 1 (Flat/gentle slope; no barrier) Topography

Reference angle : 0.00

Results segment # 1: MerBleueN (day)

Source height = 1.50 m

Segment Leq: 63.14 dBA

Results segment # 2: MerBleueS (day)

Source height = 1.50 m

ROAD (0.00 + 60.71 + 0.00) = 60.71 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

-90 90 0.64 70.67 0.00 -8.53 -1.42 0.00 0.00 0.00 60.71

Segment Leq: 60.71 dBA

Total Leq All Segments: 65.10 dBA

Results segment # 1: MerBleueN (night)

Source height = 1.50 m

ROAD (0.00 + 61.46 + 0.00) = 61.46 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

-90 90 0.57 63.07 0.00 -0.31 -1.30 0.00 0.00 0.00 61.46

Segment Leq: 61.46 dBA

Results segment # 2: MerBleueS (night)

Source height = 1.50 m

ROAD (0.00 + 57.11 + 0.00) = 57.11 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

-90 90 0.57 63.07 0.00 -4.66 -1.30 0.00 0.00 0.00 57.11

Segment Leq: 57.11 dBA

Total Leq All Segments: 62.82 dBA

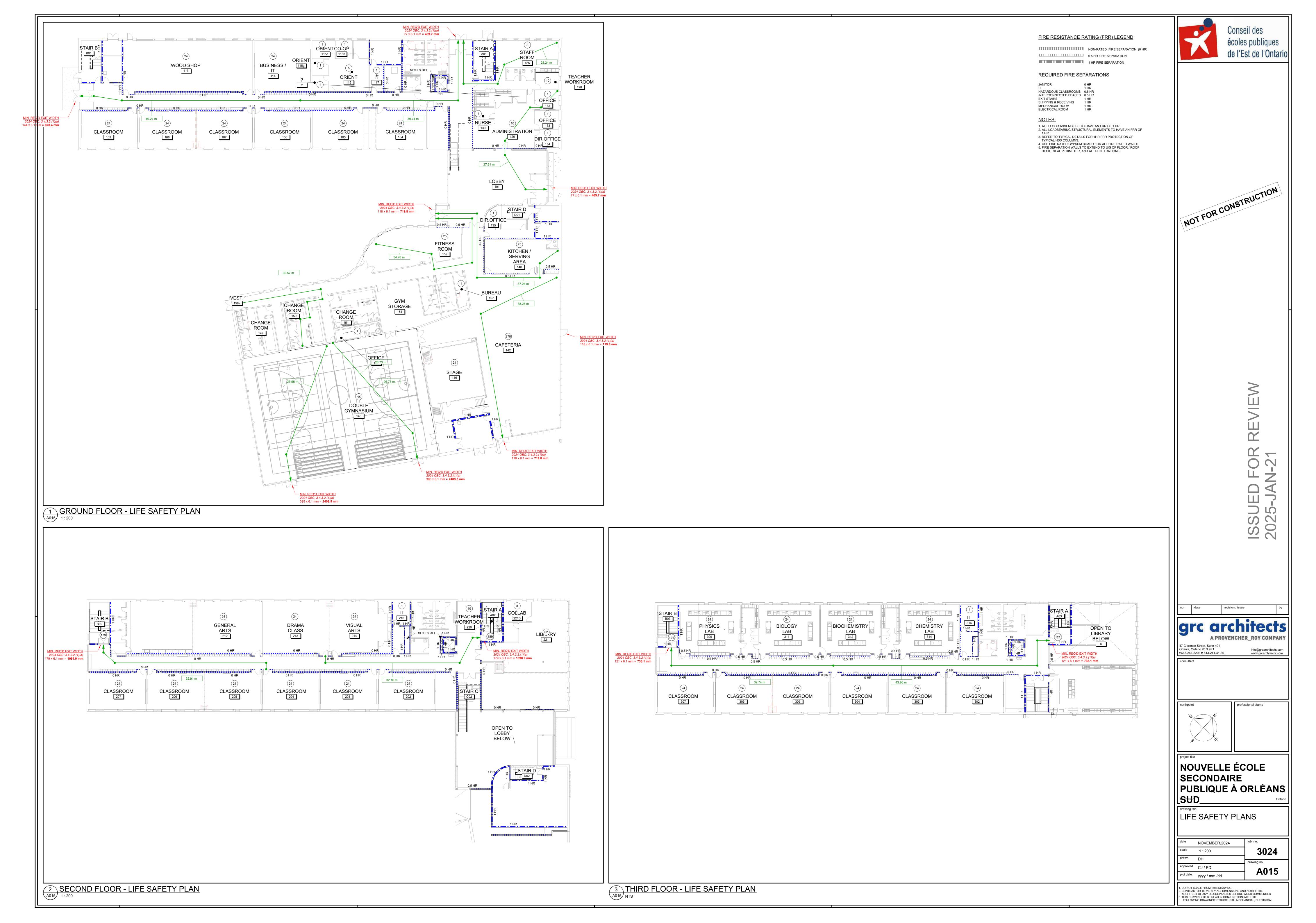
TOTAL Leq FROM ALL SOURCES (DAY): 65.10

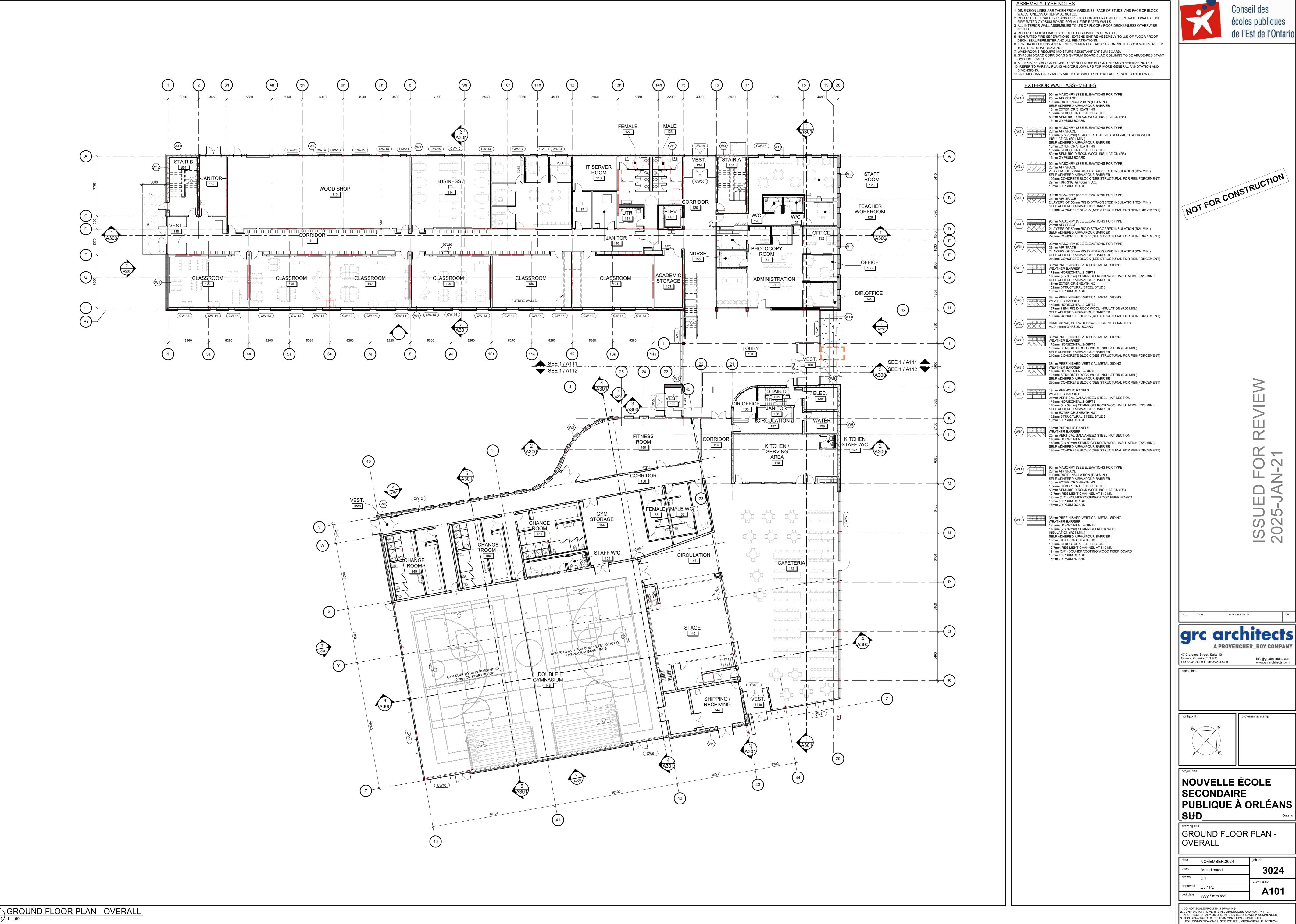
(NIGHT): 62.82

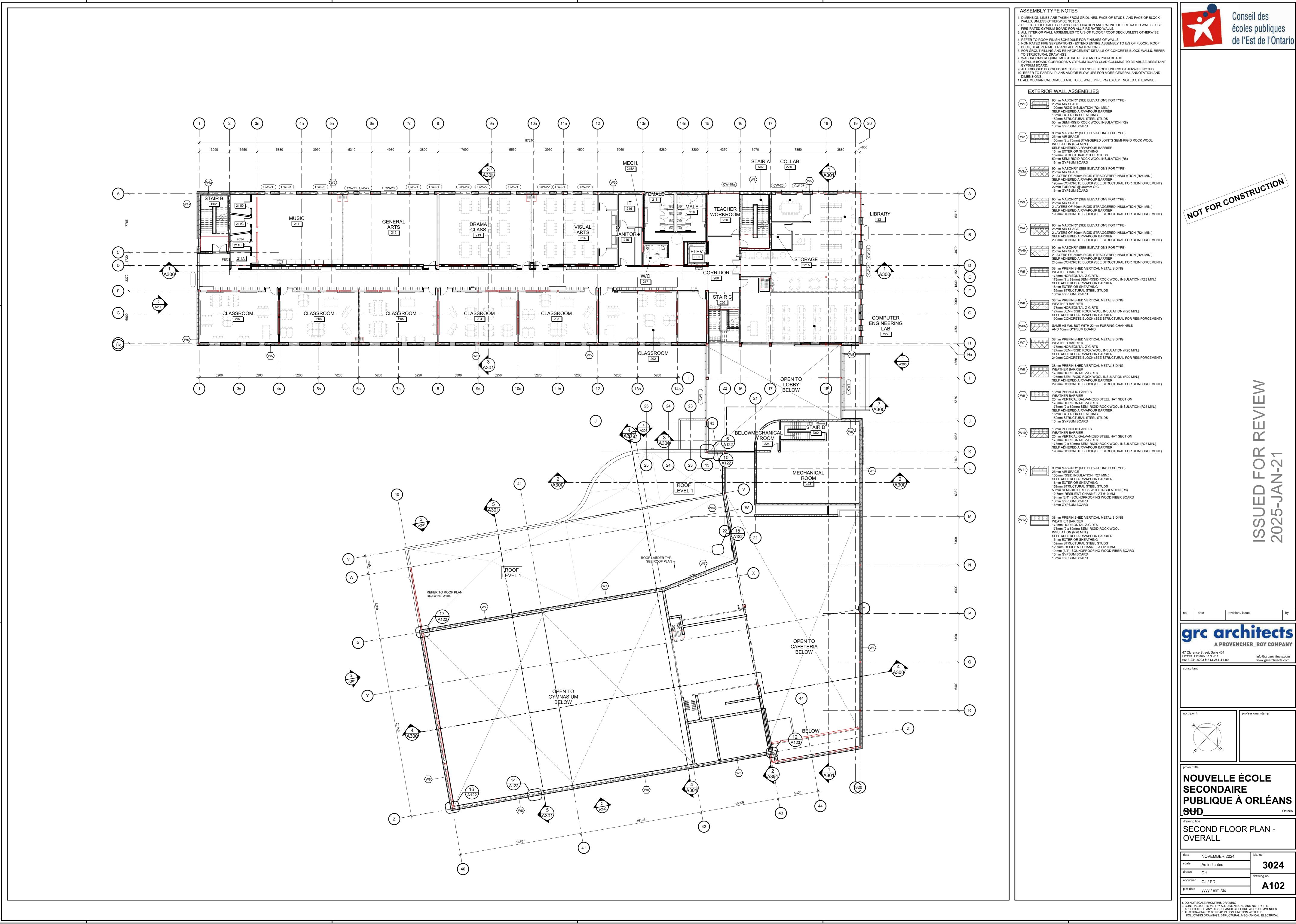


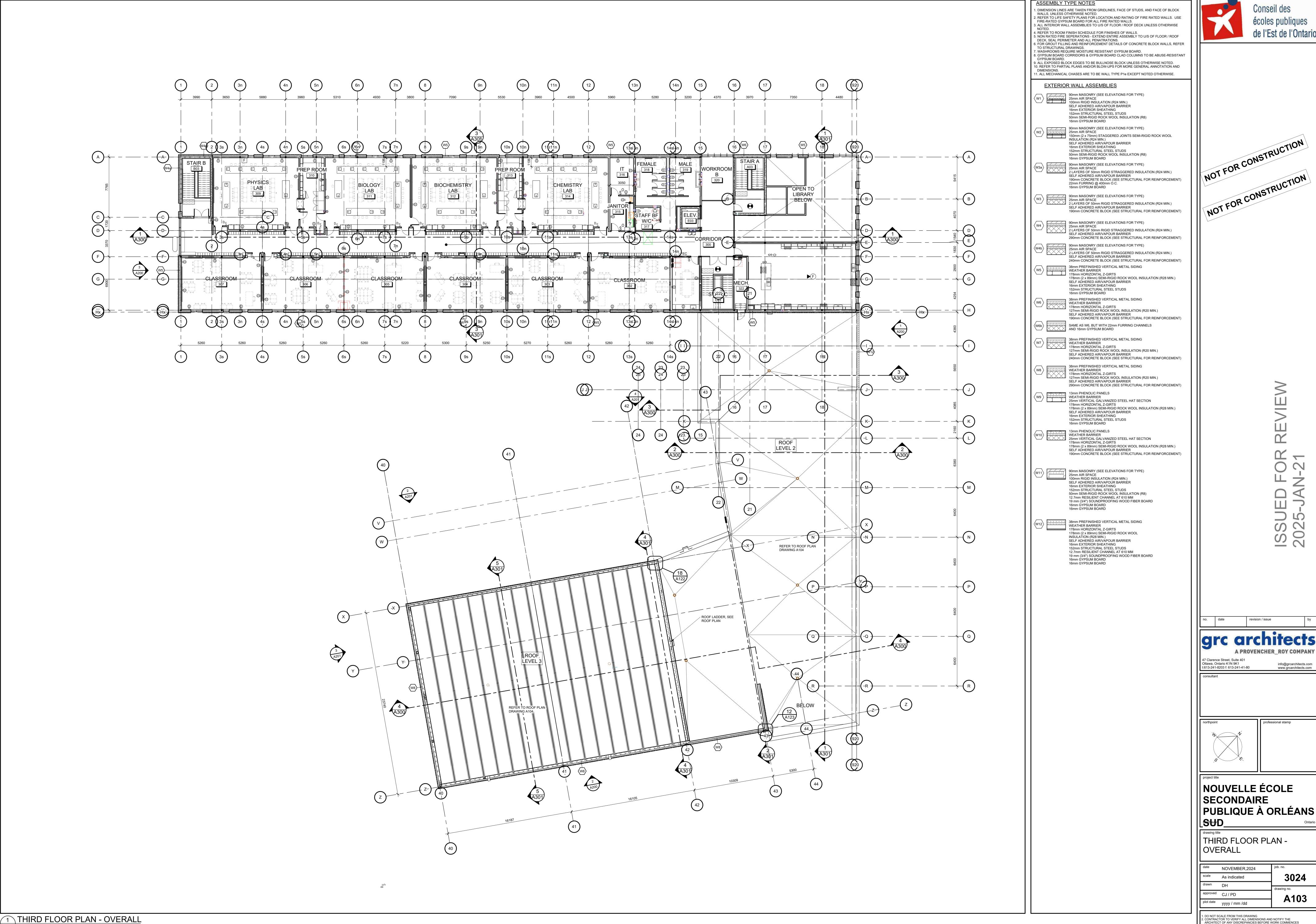
# **Appendix C**

Floor Plan & Building Elevation Drawings







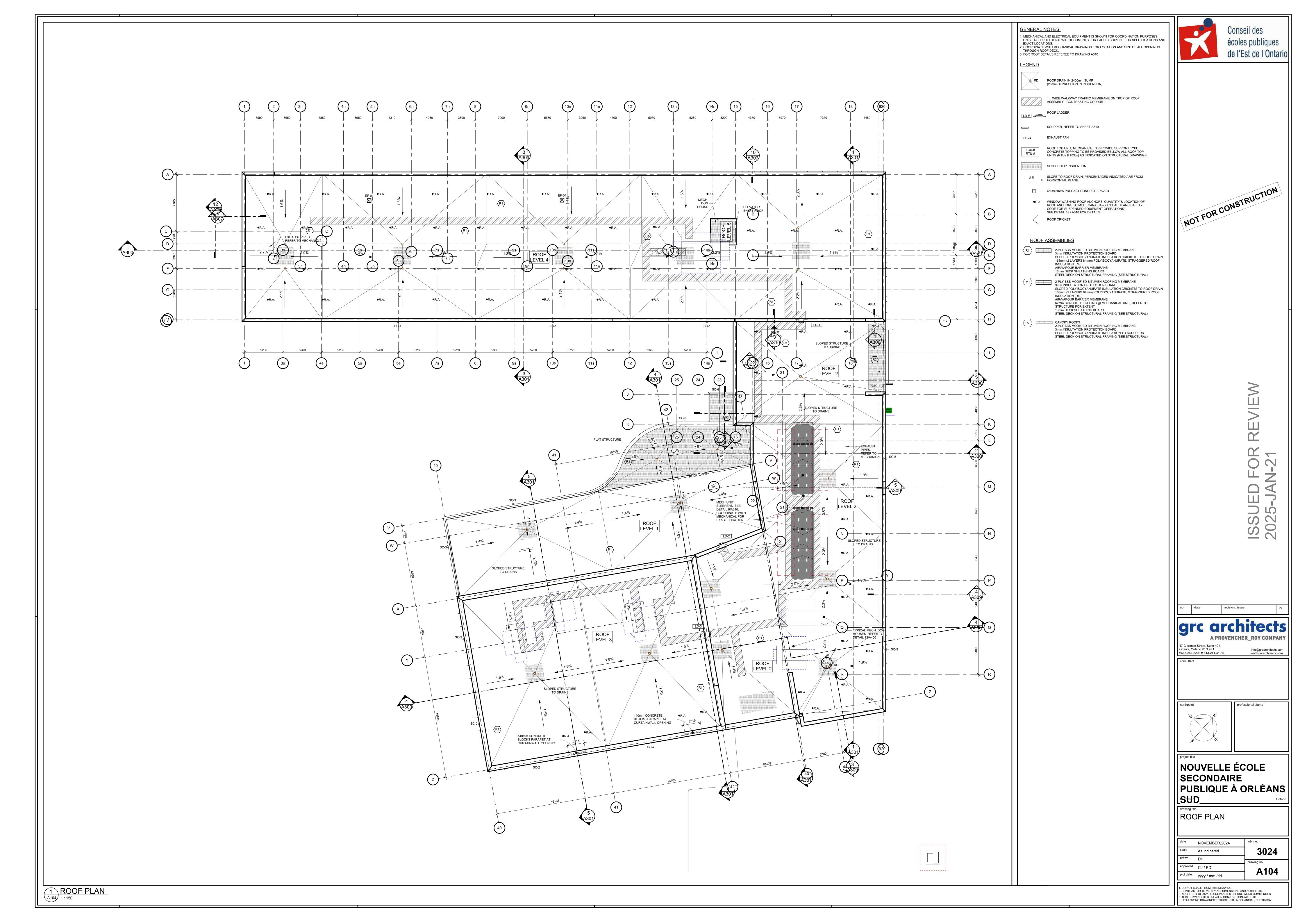


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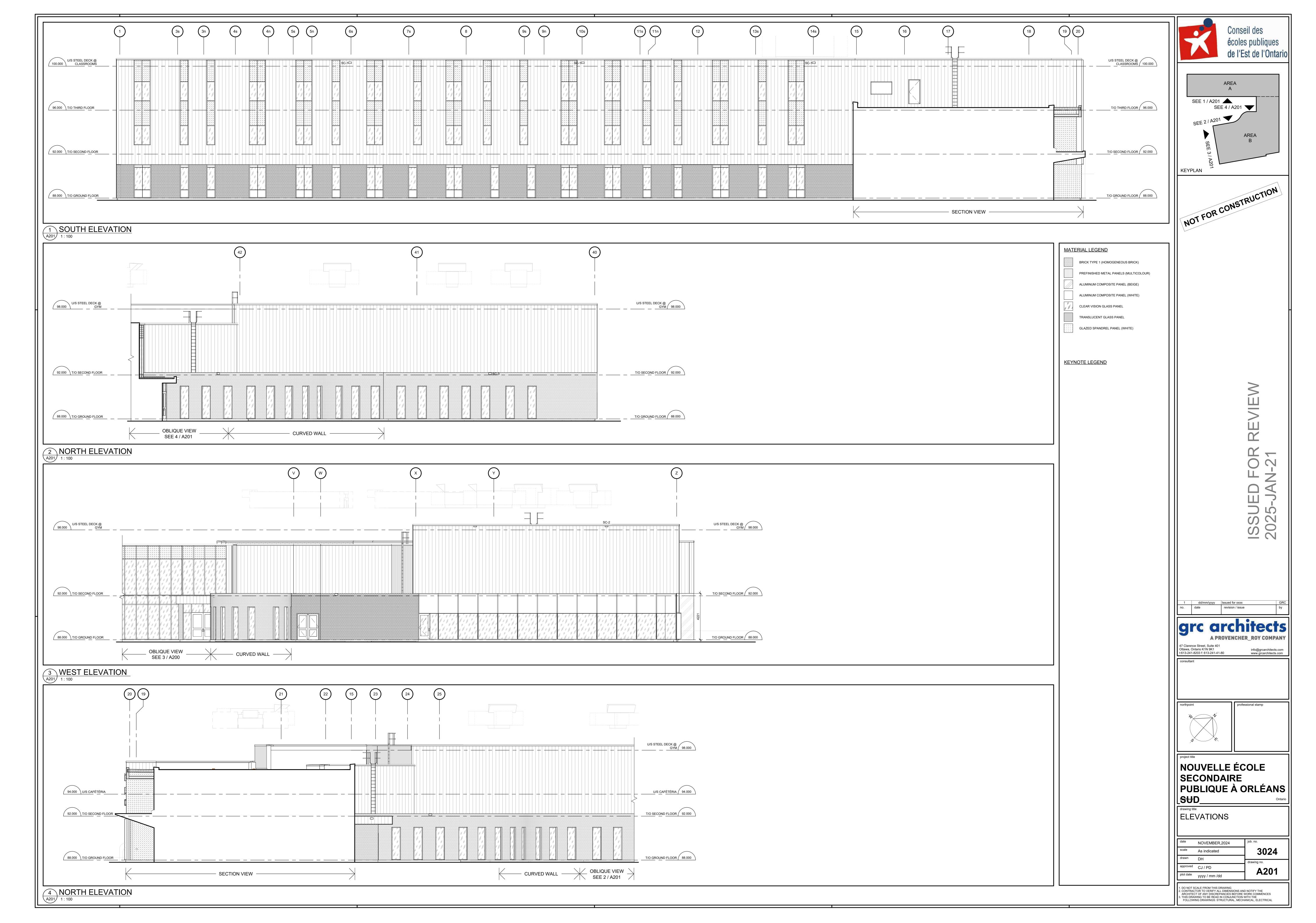
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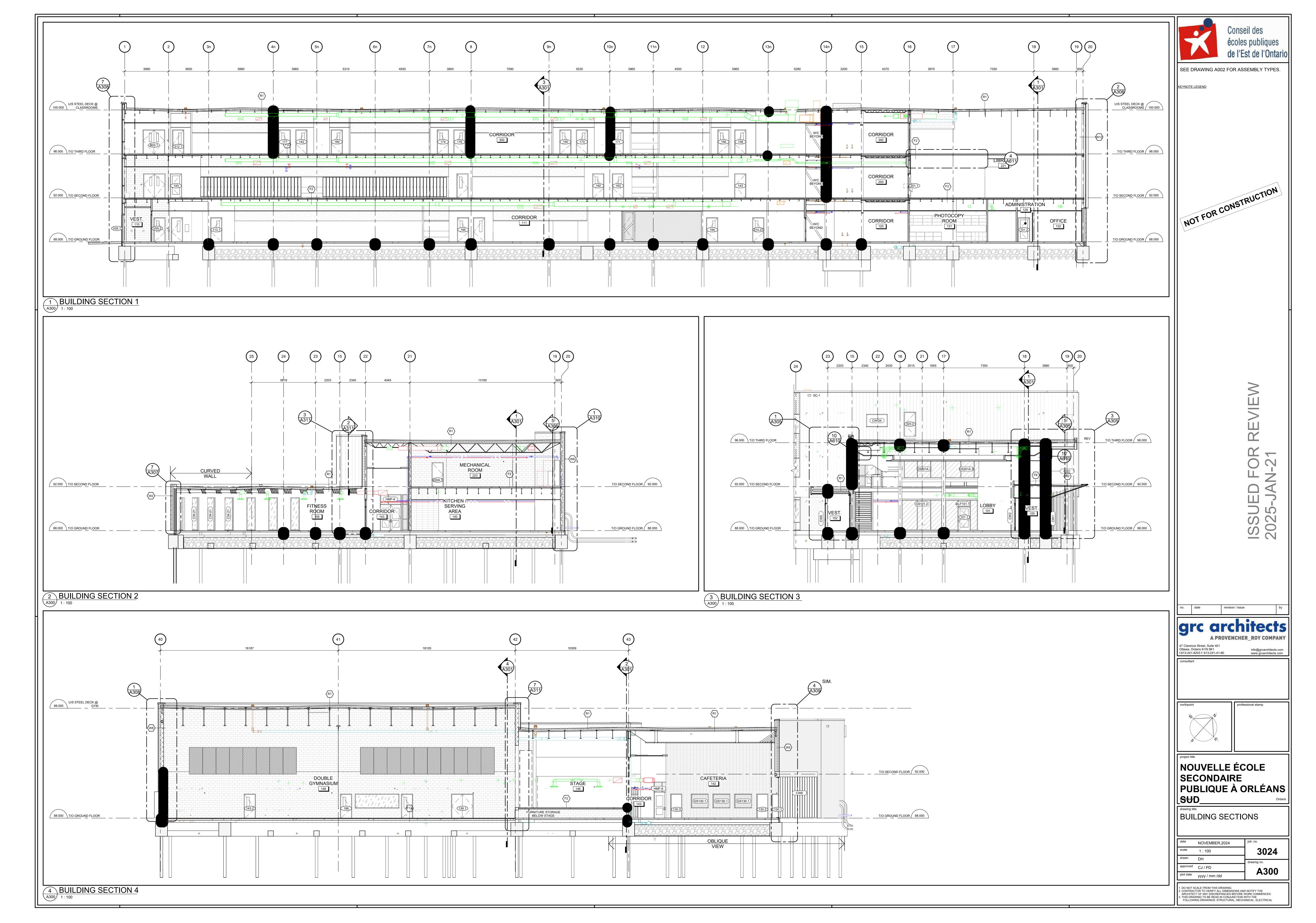
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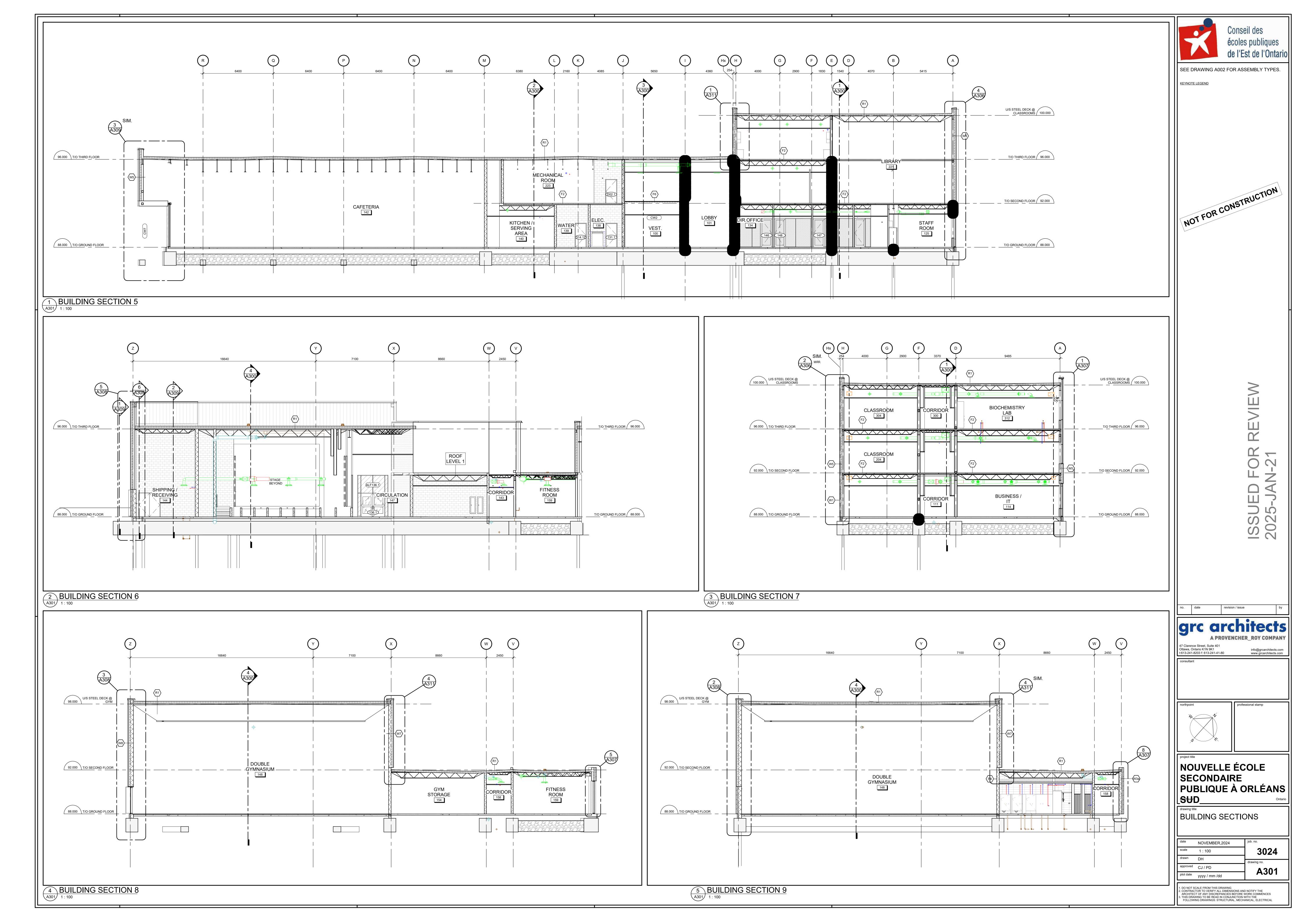
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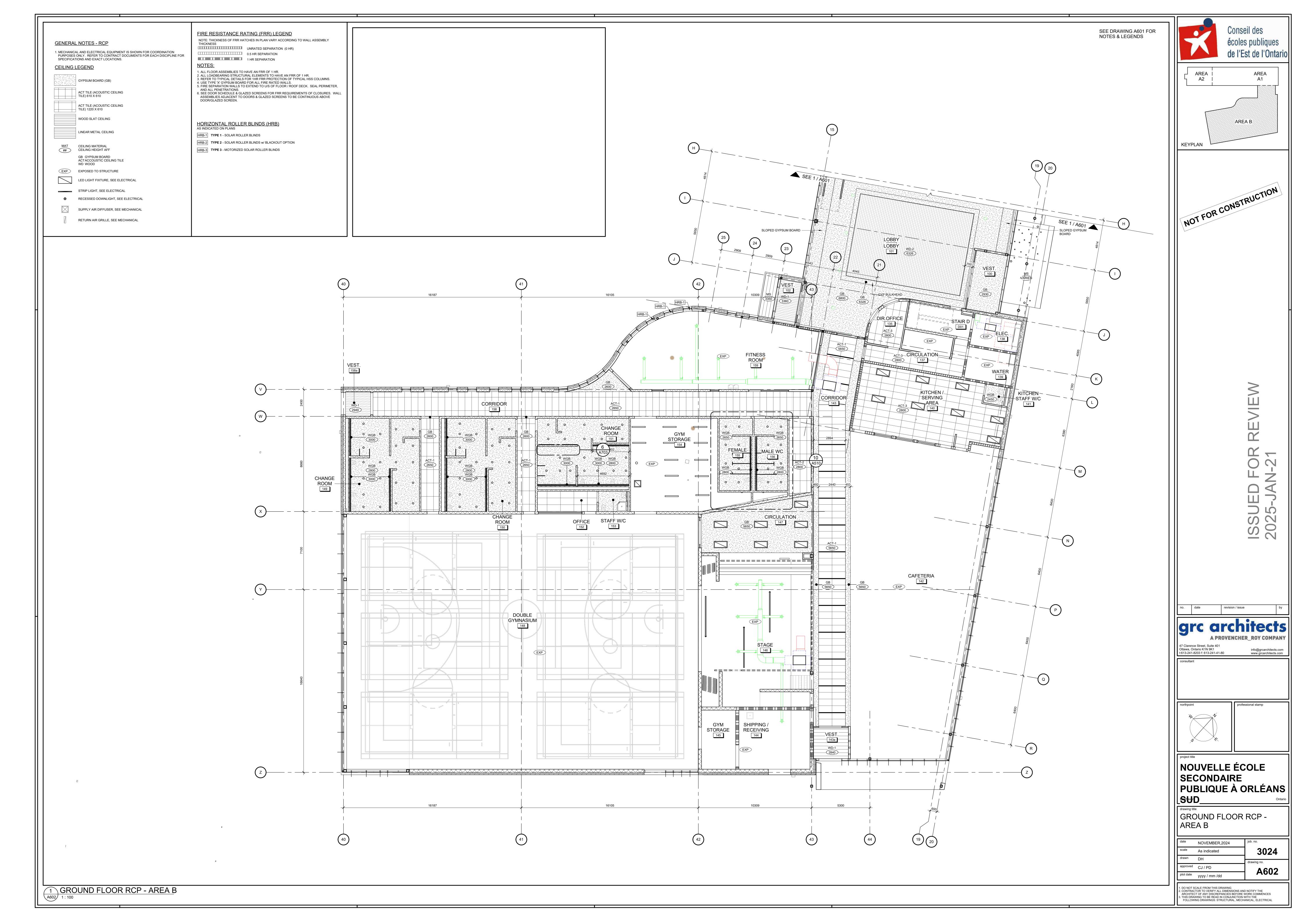


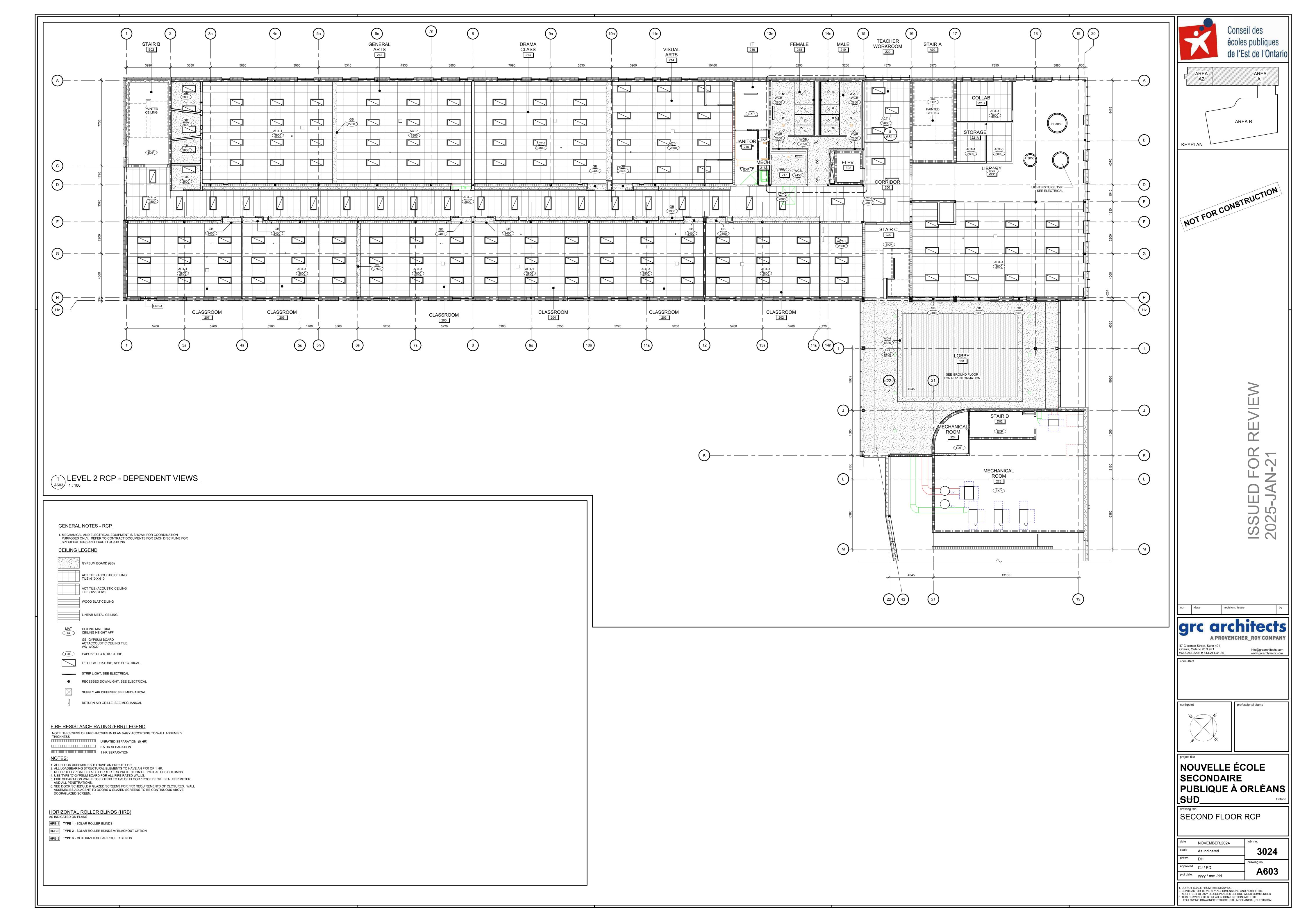


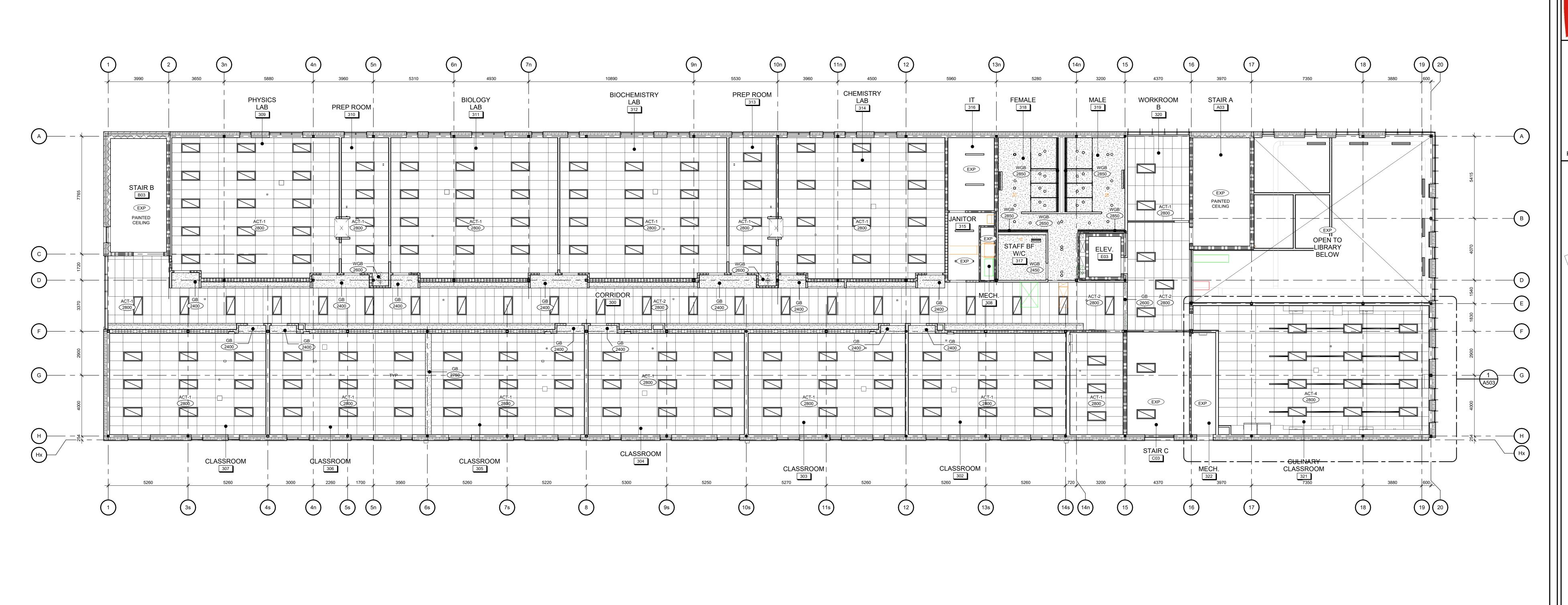




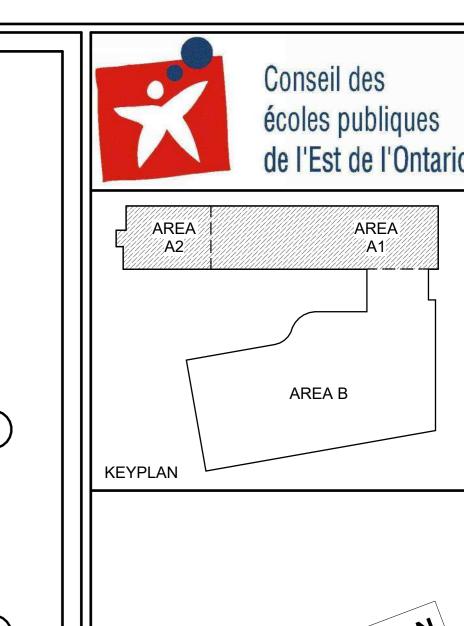
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LEVEL 3 RCP - DEPENDENT VIEWS **GENERAL NOTES - RCP** 1. MECHANICAL AND ELECTRICAL EQUIPMENT IS SHOWN FOR COORDINATION PURPOSES ONLY. REFER TO CONTRACT DOCUMENTS FOR EACH DISCIPLINE FOR SPECIFICATIONS AND EXACT LOCATIONS. **CEILING LEGEND** GYPSUM BOARD (GB) ACT TILE (ACOUSTIC CEILING TILE) 610 X 610 ACT TILE (ACOUSTIC CEILING TILE) 1220 X 610 WOOD SLAT CEILING LINEAR METAL CEILING CEILING MATERIAL ## CEILING HEIGHT AFF GB GYPSUM BOARD ACTACCOUSTIC CEILING TILE WD WOOD EXPOSED TO STRUCTURE LED LIGHT FIXTURE, SEE ELECTRICAL STRIP LIGHT, SEE ELECTRICAL ♠ RECESSED DOWNLIGHT, SEE ELECTRICAL SUPPLY AIR DIFFUSER, SEE MECHANICAL RETURN AIR GRILLE, SEE MECHANICAL FIRE RESISTANCE RATING (FRR) LEGEND NOTE: THICKNESS OF FRR HATCHES IN PLAN VARY ACCORDING TO WALL ASSEMBLY UNRATED SEPARATION (0 HR) 0.5 HR SEPARATION 1 HR SEPARATION 1. ALL FLOOR ASSEMBLIES TO HAVE AN FRR OF 1 HR. 2. ALL LOADBEARING STRUCTURAL ELEMENTS TO HAVE AN FRR OF 1 HR. 3. REFER TO TYPICAL DETAILS FOR 1HR FRR PROTECTION OF TYPICAL HSS COLUMNS. 4. USE TYPE 'X' GYPSUM BOARD FOR ALL FIRE RATED WALLS. 5. FIRE SEPARATION WALLS TO EXTEND TO U/S OF FLOOR / ROOF DECK. SEAL PERIMETER, AND ALL PENETRATIONS. 6. SEE DOOR SCHEDULE & GLAZED SCREENS FOR FRR REQUIREMENTS OF CLOSURES. WALL ASSEMBLIES ADJACENT TO DOORS & GLAZED SCREENS TO BE CONTINUOUS ABOVE DOOR/GLAZED SCREEN. HORIZONTAL ROLLER BLINDS (HRB) AS INDICATED ON PLANS HRB-1 TYPE 1 - SOLAR ROLLER BLINDS HRB-2 TYPE 2 - SOLAR ROLLER BLINDS w/ BLACKOUT OPTION HRB-3 TYPE 3 - MOTORIZED SOLAR ROLLER BLINDS



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project title

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Ontario

THIRD FLOOR RCP

date NOVEMBER,2024 jc
scale As indicated

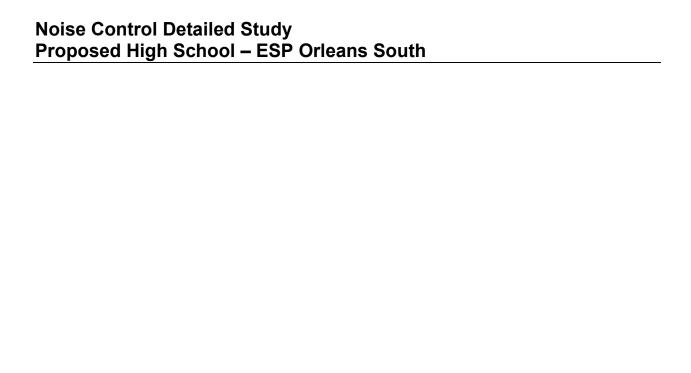
drawn DH

approved CJ / PD

plot date yyyy / mm /dd

approved yyyy / mm /dd

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 ARCHITECT OF ANY DISCREPANCIES BEFORE WORK COMMENCES
 THIS DRAWING TO BE READ IN CONJUNCTION WITH THE
 FOLLOWING DRAWINGS: STRUCTURAL, MECHANICAL, ELECTRICAL



# **Appendix D**

**Building Component Calculations** 

### **ROOM BY ROOM CALCULATIONS**

### Cafeteria

Floor Area (sq.m) 415.5

Window 1 (front) Window 2 (side) Patio Door (front)

Width	Height	Area
25.6	4.0	102.4
8.8	4.0	35.2
		0.0

137.6 Total Window Area 33.12% % of Floor Area

**Exterior Door** 

	Width	Height	Area	
Γ	0	0	0	
_			0	Total Door Area
			0.00%	% of Floor Area

Width Height Area Area minus windows/doors

Exterior Wall (front) 0.00 
Exterior Wall (side) 0.00 -

0.00 Total Exterior Wall Area
0.00% % of Floor Area

#### **TABLE 16: BUILDING COMPONENT TEMPLATE**

Architect:

Location: Orleans South HS
Building Type: High School

Block Number:

Front Façade Noise Level (dBA) 70

JLR No: 33322-001
Prepared by: Thomas Blais
Checked by: Lee Jablonski

ROOM	# OF COMPONENTS	ROOM FLOOR AREA (M <sup>2</sup> )	WINDOW AREA (M²)		DOOR AREA (M²)	D/RFA %	EXT. WALL AREA (M <sup>2</sup> )	EW/RFA %	REQUIRED AIF*	WIND	OW	EXT. I	DOOR	EXT. \	WALL	CEILING	G/ROOF
					-	-				Type	AIF**	Type	AIF***	Type	AIF****	Туре	AIF****
Cafeteria	2	415.5	137.6	33%	-	-	0.0	0%	30	6(6)6	30	-	-	-	-	-	-

<sup>\*</sup> Taken from Table 10.5: AIF required for Road and Rail Traffic Noise Cases

### **Exterior Door Details**

All prime doors should be fully weatherstripped. Except as noted specifically below, doors shall not have inset glazing:

D1 denotes 44 mm hollow-core wood door (up to 20% of area glazed).

D2 denotes 44 mm glass-fibre reinforced plastic door with foam or glass-fibre insulated core (up to 20% area glazed).

D3 denotes 35 mm in solid slab wood door.

D4 denotes 44 mm steel door with foam or glass-fibre insulated core.

D5 denotes 44 mm solid slab door.

sd denotes storm door of wood or aluminum with openable glazed sections.

#### **Exterior Wall Details**

The common structure of walls EW1 to EW5 is composed of 12.7 mm gypsum board, vapour barrier, and 38x89 mm studs with 50 mm (or thicker) mineral wool or glass fibre batts in the inter-stud cavities.

EW1 denotes the above plus sheathing, plus wood siding or metal siding and fibre backer board.

EW2 denotes the above plus rigid insulation (25-50mm), and wood siding or metal siding and fibre backer board.

EW2 also denotes exterior wall described in EW1 with the addition of rigid insulation (25-50mm) between the sheathing and the external finish.

EW3 denotes simulated mansard with structure as the above plus sheathing, 38 x 89 mm framing, sheathing and asphalt roofing material.

EW4 denotes the above plus sheathing and 20 mm stucco.

EW5 denotes the above plus sheathing, 25 mm air space, 100 mm brick veneer.

EW6 denotes exterior wall composed of 12.7 mm gypsum board, rigid insulation (25-50mm), 100 mm back-up block, 100 mm face brick.

EW6 also denotes an exterior wall conforming to rainscreen design principles and composed of same gypsum board and rigid insulation with 100 mm concrete block, 25 mm air space, and 100 mm brick veneer.

EW7 denotes exterior wall composed of 12.7 mm gypsum board, rigid insulation (25-50mm), 140 mm back-up block, 100 mm face brick.

EW8 denotes exterior wall composed of 12.7 mm gypsum board, rigid insulation (25-50mm), 200 mm concrete.

R denotes the mounting of the interior gypsum board on resilient clips

<sup>\*\*</sup> Taken from Table 10.6: Acoustic Insulation Factor for various types of windows (example: 2(100)2 denotes 2 mm glass (100 mm space) 2 mm glass).

<sup>\*\*\*</sup> Taken from Table 10.9: Acoustic Insulation Factor for various types of exterior doors

<sup>\*\*\*\*</sup> Taken from Table 10.7: Acoustic Insulation Factor for various types of exterior walls

<sup>\*\*\*\*\*</sup> Taken from Table 10.8: Acoustic Insulation Factor for various ceiling-roof combinations (only for aircraft noise)



## **Appendix E**

Canada Mortgage and Housing (CMHC) Table A2 and Table A3

Table A1: Standard source spectrum for calculating Acoustic Insulation Factor (AIF)

Frequency (Hz)	Source Sound Pressure Level	A-weighted Source Sound Pressure Level
100	66.1	47
125	69.1	53
160	71.4	58
200	71.9	61
250	71.6	63
315	71.6	65
400	71.8	67
500	71.2	68
630	70.9	69
800	70.8	70
1000	70.0	70
1250	69.4	70
1600	69.0	70
2000	68.8	70
2500	68.7	70
3150	67.8	69
4000	67.0	68
5000	65.5	66

Note: Values in the second and third columns of this table are \( \frac{1}{3}\)-octave band sound pressure levels expressed in dB.

Table A2: Approximate conversion from STC to AIF for windows and doors

Window (or door)	Acoustic
Area Expressed	Insulation
as Percentage of	Factor
Room Floor Area	(AIF)
80.0	STC-5
63.0	STC-4
50.0	STC-3
40.0	STC-2
32.0	STC-1
25.0	STC
20.0	STC+1
16.0	STC+2
12.5	STC+3
10.0	STC+4
8.0	STC+5
6.3	STC+6
5.0	STC+7
4.0	STC+8

Note: For area percentages not listed in the table, use the nearest listed value.

Examples: For a window whose area = 20% of the room floor area and STC = 32, the AIF is 32 + 1 = 33.

For a window whose area = 60% of the room floor area

and STC = 29, the AIF is 29 - 4 = 25.

Table A3: Approximate conversion from STC to AIF for exterior walls and ceiling-roof systems.

Exterior Wall	Acoustic
Area Expressed	Insulation
as Percentage of Room Floor Area	Factor
	(AIF)
200.0	STC-10
160.0	STC-9
125.0	STC-8
100.0	STC-7
80.0	STC-6
63.0	STC-5
50.0	STC-4
40.0	STC-3
32.0	STC-2
25.0	STC-1
20.0	STC
16.0	STC+1
12.5	STC+2
10.0	STC+3
8.0	STC+4

Note: For area percentages not listed in the table, use the nearest listed value.

Example: For a wall whose area = 120% of room floor area and STC = 48, the AIF is 48 - 8 = 40.

Note: For ceiling-roof systems, AIF = STC - 7.

Figure A1: Worksheet for Calculating AIF from Transmission Loss Data

F	A-weighted Source Sound Pressure	Sound Transmission Loss	A-weighted Indoor Sound Pressure	Energy Equivalent of Indoor
Frequency (Hz)	Level (dB)	(dB)	Level (dB)	SPL
	(A)	(B)	(C = A-B)	$(D = 10^{c/10})$
100	47	24	23	200
125	53	26	27	501
160	58	19	39	7 943
200	61	21	40	10 000
250	63	20	43	19 953
315	65	20	45	31 623
400	67	25	42	15 849
500	68	30	38	6310
630	69	33	36	3 981
800	70	37	33	1 995
1000	70	39	31	1 259
1250	70	41	29	794
1600	70	43	27	501
2000	70	44	26	398
2500	70	45	25	316
3150	89	43	26	398
4000	68	37	31	1 259
5000	88	35	31	1 259
	S	um of values in	column D:	104 539=E

Calculated indoor A-weighted sound level: 10 log<sub>10</sub> (E) = 50.2 = F

AIF (component area = 80% of floor area): (77 - F) = 26.8 = G

Component Area	Acoustic
as a Percentage of	Insulation
Room Floor Area	Factor (AIF)
6.3	(G + 11) = 38
8.0	(G + 10) = 37
10.0	(G+ 9) = 36
12.5	(G+ 8) = 35
16.0	(G + 7) = 34
20.0	(G + 6) = 33
25.0	(G+ 5) = 32
32.0	(G + 4) = 31
40.0	(G+ 3) = 30
50.0	(G + 2) = 29
63.0	(G + 1) = 28
80.0	(G ) = 27
100.0	(G - 1) = 26
125.0	(G - 2) = 25
160.0	(G - 3) = 24



# **Appendix F**

Stationary Noise Source Data

### **AAON Standard Condenser Fan Radiated Sound Levels**

**Updated 10/26/2018** 

**Sound Pressure Level in a** Dist (ft) **Hemispherical Free Field** 

15

					Sound Power Level								S	ound	l Pres	sure l	_evel		$\Box$			
		Fans	Dia	RPM	63	125	250	500	1000	2000	4000	8000	LwA	63	125	250	500	1000	2000	4000	8000	dBA
	Inlet				79	74	72	70	66	62	59	59	72	58	53	51	48	44	41	38	38	50
RQ 2 & 3 Ton	Outlet	1	30	850	81	77	71	71	67	62	59	58	73	60	56	49	50	46	41	38	37	51
	Total				83	79	74	73	69	65	62	61	75	62	58	53	52	48	44	41	40	54
	Inlet				85	79	77	<i>75</i>	71	68	<i>65</i>	64	77	63	58	56	54	50	46	44	43	56
RQ 4-6 Ton & RN 6 & 7 Ton	Outlet	1	30	1085	86	83	76	76	72	68	<i>65</i>	<i>63</i>	78	65	62	55	55	51	46	44	42	57
	Total				89	84	80	79	75	71	68	67	80	67	63	58	57	53	49	47	46	59
	Inlet				92	86	85	82	78	75	72	71	84	71	65	63	61	57	54	51	50	63
RN 8 & 10 Ton	Outlet	1	30	1085	94	90	83	83	79	75	72	71	85	72	69	62	62	58	54	51	49	64
	Total				96	91	87	86	82	78	75	74	88	75	70	66	65	60	57	54	53	66
	Inlet				88	82	80	78	74	71	68	67	80	66	61	59	57	53	49	47	46	59
RN 09 & 11 Ton	Outlet	2	30	1085	89	86	79	79	75	71	68	66	81	68	65	58	58	54	49	47	45	60
	Total				92	87	83	82	78	74	71	70	83	70	66	61	60	56	52	50	49	62
	Inlet				95	89	88	85	81	78	75	74	87	74	68	66	64	60	57	54	53	66
RN 13-20 Ton	Outlet	2	30	1085	97	93	86	86	82	78	75	74	88	75	72	65	65	61	57	54	52	67
	Total				99	94	90	89	85	81	78	77	91	78	73	69	68	63	60	57	56	69
	Inlet				97	91	89	87	83	80	77	76	89	75	70	68	66	62	58	55	55	68
RN 25 & 30 Ton	Outlet	3	30	1085	98	95	88	88	84	80	77	75	90	77	73	67	67	63	58	55	54	69
	Total				101	96	92	91	86	83	80	79	92	79	75	70	69	65	61	58	57	71
	Inlet				98	92	91	88	84	81	78	77	90	77	71	69	67	63	60	57	56	69
RN 26,31 & 40 Ton	Outlet	4	30	1085	100	96	89	89	85	81	78	77	91	78	75	68	68	64	60	57	55	70
	Total				102	98	93	92	88	84	81	80	94	81	76	72	71	66	63	60	59	72
	Inlet				100	94	92	90	86	83	80	79	92	78	73	71	69	65	61	58	58	71
RN 50,60 & 70 Ton	Outlet	6	30	1085	101	98	91	91	87	83	80	78	93	80	76	70	70	66	61	58	57	72
	Total				104	99	95	94	89	86	83	82	95	82	78	73	72	68	64	61	60	74
RN E 55,65 & 75 Ton	Inlet				92	86	87	87	86	85	85	78	92	71	65	66	66	65	64	64	57	71
LN & LZ 45-60 Ton	Outlet	4	30	1170	92	86	87	87	86	85	85	78	92	71	65	66	66	65	64	64	57	71
RZ 45-75	Total				95	89	90	90	89	88	88	81	95	74	68	69	69	68	67	67	60	74
RN E 90-140 Ton	Inlet				95	89	90	90	89	88	88	81	95	74	68	69	69	68	67	67	60	74
LN & LZ 75-140 Ton	Outlet	8	30	1170	95	89	90	90	89	88	88	81	95	74	68	69	69	68	67	67	60	74
RZ 90-140	Total				98	92	93	93	92	91	91	84	98	77	71	72	72	71	70	70	63	77
	Inlet				97	91	92	92	91	90	90	83	97	76	70	71	71	70	69	69	62	76
RZ 145-180	Outlet	12	30	1170	97	91	92	92	91	90	90	83	97	76	70	71	71	70	69	69	62	76
	Total				100	94	95	95	94	93	93	86	100	79	73	74	74	73	72	72	65	79
	Inlet				98	92	93	93	92	91	91	84	98	77	71	72	72	71	70	70	63	77
RZ 200-240	Outlet	16	30	1170	98	92	93	93	92	91	91	84	98	77	71	72	72	71	70	70	63	77
	Total				101	95	96	96	95	94	94	87	101	80	74	75	75	74	73	73	66	80

Tested in Accordance with AMCA 300 - Updated 6-15-15

										Sour	nd Pov	wer Le	evel			Ī
ı	Speed %		lulat	Fans	Dia	RPM	<b>63</b>	<b>125</b> 74	<b>250</b> 72	<b>500</b> 70	<b>1000</b>	<b>2000</b> 62	<b>4000</b> 59	<b>8000</b> 59	<b>LwA</b> 72	
	100%	RQ 2 & 3 Ton	Inlet Outlet	1	30	850	81	77	71	71	67	62	59	58	73	
			Total Inlet				83 73	79 68	74 66	73 63	69 59	65 56	62 53	61 52	75 65	
	75%	RQ 2 & 3 Ton	Outlet Total	1	30	638	75 77	71 73	64 68	65 67	60 63	56 59	53 56	52 55	66 69	
	50%	RQ 2 & 3 Ton	Inlet Outlet	1	30	425	64 66	59 62	57 56	54 56	51 52	47 47	44 44	44 43	57 57	
			Total Inlet				68 49	64	59 42	58 39	54 36	50 32	47 29	46 29	60 42	
	25%	RQ 2 & 3 Ton	Outlet	1	30	213	51	47	40	41	37 39	32	29	28	42	
			Total					49	44			35	32	31	45	!
	100%	RQ 4-6 RN 6 & 7 Ton	Inlet Outlet	1	30	1085	85 86	79 83	77 76	75 76	71 72	68 68	65 65	64 63	77 78	
5	m	·····	<mark>Tetal √</mark> Inlet	m	~~~	~~	89 78	73	80 71	79 69	75 65	61	58 58	67 58	71	2
٤	75%	<del>RQ 4-6</del> RN 6 <del>&amp; 7</del> Ton	Outlet Total	1	30	814	80 82	77 78	70 73	70 72	66 68	61 64	58 61	57 61	72 74	3
٩	50%	RQ 4-6 RN 6 & 7 Ton	Inlet Outlet	1	30	543	70 71	64 68	62 61	60 61	56 57	53	50 50	49 48	63	9
	0070		Total Inlet	·		0.0	74 54	69 49	65 47	64	59 41	56 37	53 35	52 34	65 47	
	25%	RQ 4-6 RN 6 & 7 Ton	Outlet	1	30	271	56	53	46	46	42	38	35	33	48	
			Total				59	54	50	48	44	41	38	37	50	<u> </u>  -
	100%	RN 8 & 10 Ton	Inlet Outlet	1	30	1085	92 94	86 90	85 83	82 83	78 79	75 75	72 72	71 71	84 85	
			Total Inlet				96 86	91 80	87 78	86 76	82 72	78 68	75 66	74 65	88 78	
	75%	RN 8 & 10 Ton	Outlet Total	1	30	814	87 90	84 85	77 81	77 80	73 75	69 72	66 69	64 68	79 81	
	50%	RN 8 & 10 Ton	Inlet Outlet	1	30	543	77 79	71 75	69 68	67 68	63 64	60 60	57 57	56 56	69 70	
	00,0		Total Inlet				81	76 56	72 54	71 52	67 48	63 45	60 42	59 41	73 54	
	25%	RN 8 & 10 Ton	Outlet Total	1	30	271	64	60	53 57	53 56	49 52	45 48	42 45	41	55 58	
																I
	100%	RN 9 & 11 Ton	Inlet Outlet	2	30	1085	88	82 86	80 79	78 79	74 75	71 71	68 68	67 66	80 81	
ع	750/		Total	~~~	<u>~~~</u>	~~	81	76	74	72	68	64	61	61	74	3
ع	75%	<del>RN 9 &amp;</del> 11 Ton	Outlet Total	2	30	814	83 85	80 81	73 76	73 75	69 71	64 67	61 64	60 64	75 77	3
	50%	RN 9 & 11 Ton	Inlet Outlet	2	30	407	66 68	61 64	59 58	57 58	53 54	49 49	46 46	46 45	59 60	
			Total Inlet				70 57	66 52	61 50	60 48	56 44	52 40	49 38	48 37	62 50	
	25%	RN 9 & 11 Ton	Outlet Total	2	30	271	59 62	56 57	49 53	49 51	45 47	41 44	38 41	36 40	51 53	
Ī			Inlet				95	89	88	85	81	78	75	74	87	1
	100%	RN 13-20 Ton	Outlet Total	2	30	1085	97 99	93 94	86 90	86 89	82 85	78 81	75 78	74 77	88 91	
ع	75%	16 TON	Inlet Outlet	2	30	814	89 90	83 87	81 80	79 80	75 76	71 72	69 69	68 67	81 82	3
کے		<del></del>	Total	<del>·····</del>	<del></del>		93	88 ンテム	84 72	83	78 <b>18</b>	75 <b>1831</b>	72	71 <del>U</del> 53-1	84 1 <del>7</del> 21	3
	50%	RN 13-20 Ton	Outlet Total	2	30	543	82	78 79	71 75	71 74	67 70	63 66	60 63	59 62	73 76	
	25%	RN 13-20 Ton	Inlet Outlet	2	30	271	65 67	59 63	57 56	55 56	51 52	48 48	45 45	44 44	57 58	
	2070	1111 10 20 1011	Total	_		_, .	69	64	60	59	55	51	48	47	61	
	100%	RN 25 & 30 Ton	Inlet Outlet	3	30	1085	97 98	91 95	89 88	87 88	83 84	80 80	77 77	76 75	89 90	
	100 /6	HIV 23 & 30 TOII	Total	3	30	1003	101	96	92	91	86	83	80	79	92	
	75%	RN 25 & 30 Ton	Inlet Outlet	3	30	814	90 92	85 88	83 82	81 82	77 78	73 73	70 70	70 69	83 83	
			Total Inlet			- 10	94 81	90 76	85 74	72	80 68	76 64	73 62	72 61	86 74	
	50%	RN 25 & 30 Ton	Outlet Total	3	30	543	83	80 81	73 77	73 75	69 71	65 67	62 65	60 64	75 77	
	25%	RN 25 & 30 Ton	Inlet Outlet	3	30	271	66 68	61 65	59 58	57 58	53 54	49 49	47 47	46 45	59 60	
ļ			Total				70	66	62	60	56	52	50	49	62	  -
	100%	RN 26, 31 & 40 Ton	Inlet Outlet	4	30	1085	98 100	92 96	91 89	88 89	84 85	81 81	78 78	77 77	90 91	
			Total Inlet				102 92	98 86	93 84	92 82	88 78	84 75	81 72	80 71	94 84	
	75%	RN 26, 31 & 40 Ton	Outlet Total	4	30	814	93 96	90 91	83 87	83 86	79 81	75 78	72 75	70 74	85 87	
	50%	RN 26, 31 & 40 Ton	Inlet Outlet	2	30	1085	95	89 93	88 86	85 86	81 82	78 78	75 75	74 74	87 88	
		,	Total Inlet				99	95 74	90 72	89 70	85 66	81 63	<del>78</del>	77 59	91 72	
	25%	RN 26, 31 & 40 Ton	Outlet Total	2	30	543	82	78 79	71 75	71 74	67 70	63 66	60 63	59 62	73 76	
ı			Inlet				100		92	90	86	83	80	79	92	
	100%	RN 50, 60 & 70 Ton	Outlet Total	6	30	1085	101	98	92 91 -95	90 91 94	87	83	80	78	93	
کے	750	PN 50 00 0 70 7	Inlet		~~~	~~~	93 95	88	86	84	89 80	76 76	83 73	73 70	95 86	کر
ع	75%	RN 50, <del>60 &amp; 70 Ton</del>	Outlet Total	6	30	814	95 97	91 93	85 88	85 87	81 83	76 79	73 76	72 75	87 89	3
٦	50%	RN 50, 60 & 70 Ton	inlet Outlet	3	30	1085	97 98	95	88	88	84	80	77	75	90	
			Total Inlet				101 81	96 76	92 74	91 72	86 68	83 64	80 62	79 61	92 74	
	25%	RN 50, 60 & 70 Ton	Outlet Total	3	30	543	83	80	73 77	73 75	69 71	65 68	62 65	60 64	75 77	
	100%	RN 55,65 & 75 Ton	Total	4	30	1170	89	84	84	84	84	83	83	79	90	I
	75%	RN 55,65 & 75 Ton	Total	4	30	877.5	83	78	78	78	78	77	77	73	84 75	
	50% 25%	RN 55,65 & 75 Ton RN 55,65 & 75 Ton	Total Total	4	30	585 292.5	74 59	69 54	69 54	69 54	69 54	68 53	68 53	64 49	60	
	100%	RN 90,105,120,130,140		8	30	1170	92	87	87	87	87	86	86	82	93	l
	75% 50%	RN 90,105,120,130,140 RN 90,105,120,130,140	Total	8	30	877.5 1170	89	81 84	81 84	81 84	81 84	80 83	80 83	76 79	87 90	
	25%	BN 90 105 120 130 140	Total	4	30	585	74	69	69	69	69	68	68	64	75	1

RN 90,105,120,130,140 Total 4 30 585 74 69 69 69 69 68 68 64 75

DOAS-GYM

RTU1, RTU2, RTU4

RTU3

DOAS-1







Type: AKFD 800-6 K.6LA A1 UL

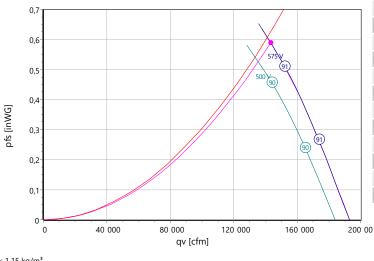
Installation type 1 direction of airflow A

Part no.: E61-80205

Quantity: 12



### **Curve:**



### **Operating Point:**

$q_V$	143249	cfm
$p_{fs}$	0,589	inWG
p <sub>fd</sub>	0,29	inWG
$\eta_{\text{e,fs}}$	35,5	%
$\eta_{\text{e,tot}}$	53,1	%
$P_{e}$	27,9	kW
l .	39,3	Α
n	1035	r/min
$L_WA_{A,IN}$	91	dB(A)
U	575	V
V	36,82	ft/s
SFP	412	Ws/m³

### **ErP-Data:**

	(EU) Nr. 327/2011 (Lot11)									
i	$q_V$	8554,39746	cfm							
i	$p_fs$	0,651	inWG							
	$\eta_{fs}$	39,1	%							
	$P_{e}$	1,67	kW							
	n	893	r/min							
	N	44	N							
1	v	26,385	ft/s							
)										

### Set point:

$q_V$	143390	cfm
p <sub>fs</sub>	0,59	inWG

ρ: 1,15 kg/m³

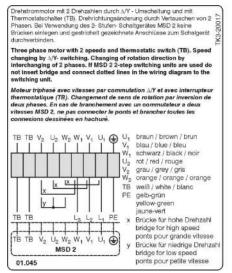
### **Nominal Data:**

U [V]	f [Hz]	C [μF]	P <sub>e</sub> [kW]	I <sub>N</sub> [A]	n <sub>N</sub> [r/min]	t <sub>R</sub> [°C]	k <sub>10</sub> [m <sup>2</sup> s/h]	I <sub>A</sub> / I <sub>N</sub>	IP	m [kg]
575 D	60		29,28	38,88	1030	-25 +50	-	3,6	IP 54	202.6
575 Y	60	-	18,6	22,08	810			5,0	IP 34	303,6

### **Sound Data:**

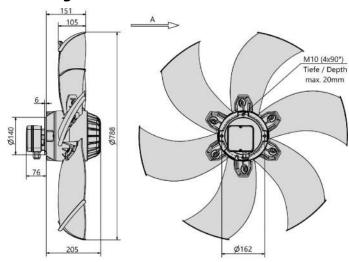
Frequency	Σ		125Hz	250Hz	500Hz	1kHz	2kHz	4kHz	8kHz	Distances	1 m	4 m	
LwA(A,in) [dB(A)]	91	-	72	78	84	87	85	79	75	LpA(A,in) [dB(A)]	84	74	

### **Wiring Diagram:**



ErP-Data @ 50Hz-Type

### **Drawing:**











Type: **AKFD 800-6 K.6LA A1 UL** 

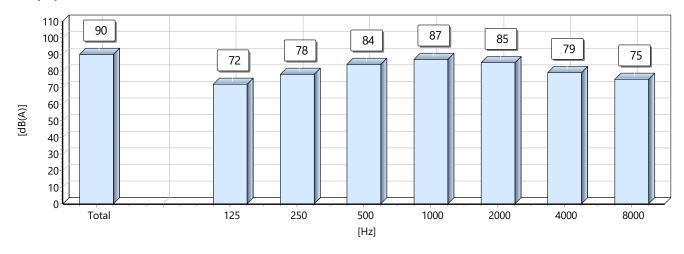
Installation type 1 direction of airflow A

Part no.: E61-80205

Quantity: 12

# ErP ready

### LwA(in)





### Loren Cook Company certifies that the model shown herein is licensed to bear the AMCA Seal. The ratings shown are based on tests and procedures performed in accordance with AMCA Publication 211 and AMCA Publication 311 and comply with the requirements of the AMCA Certified Ratings Program.

CFM vs SP

### **VCR-HP**

Performance (Belt Drive)

Model	CFM	SP	Fan RPM	Power* HP	FEG	FEI	Motor HP	_	TSPD (fpm)	SE	TEMP (ºF)	ELEV (Ft)	*Drive Loss Included
195 VCR-HP	1602	.680	837	.35	n/a	-	.5	414	4272	57%	70	700	15%

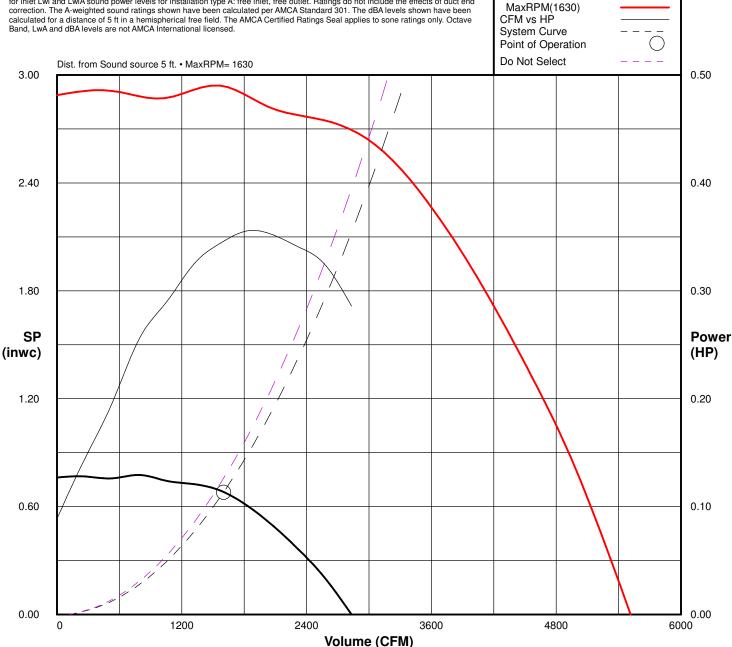
Sound Data 8 Octave Bands 10 -12 Watts

1	2	3	4	5	6	7	8	LwA	dBA	SONES
64	67	67	61	60	59	54	47	66	54	7.

Performance certified is for installation type A: free inlet, free outlet. Power rating (BHP/kW) does not include transmission losses. Performance ratings do not include the effects of appurtenances (accessories). The sound ratings shown are loudness values in hemispherical sones at 5 ft. in a hemispherical free field calculated per AMCA Standard 301. Values shown are for Installation type A: free inlet hemispherical sone levels. The AMCA International licensed air and/or sound performance data has been modified for installation, appurtenances or accessories, etc. not included in the certified data. The modified performance is not AMCA licensed but is provided to aid in selection and applications of the product.

The sound power level ratings shown are in decibels, referred to 10(-12) watts calculated per AMCA Standard 301. Values shown are

for inlet Lwi and LwiA sound power levels for installation type A: free inlet, free outlet. Ratings do not include the effects of duct end correction. The A-weighted sound ratings shown have been calculated per AMCA Standard 301. The dBA levels shown have been calculated for a distance of 5 ft in a hemispherical free field. The AMCA Certified Ratings Seal applies to sone ratings only. Octave





Date: January 31, 2025 Page 1 of 2

Project No: Submitted by: Project Name: Ecole Secondaire Rockland

Location: Engineer: Architect:

Reference: 2025-01-31 11:41:47 AM

**Equipment Tag** 

Contractor:

SAA8-DFOD

### **Model Information**

Model: G10-9 Part Number:

CFM: 1521 Shaft Diameter: 0.75 Unit Weight: 0
SP: 1.2 Wheel Diameter: 11.125 Ship Weight: 0

RPM: 1001 Tip Speed: 2915 FPM

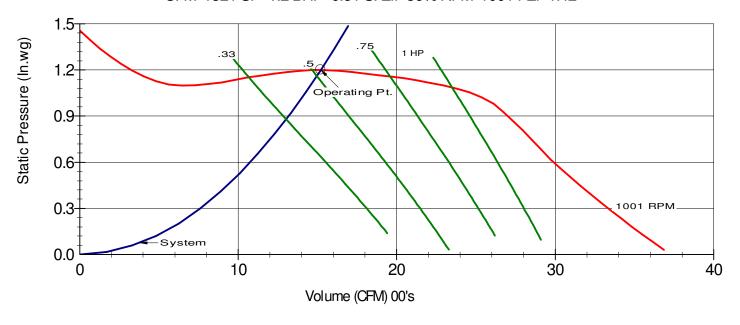
BHP: 0.51 Static Efficiency: 56 Elevation: 0
FEI: n/a Outlet Velocity: 1572 FPM Temperature: 70

Sound Data (Hz) 63 125 250 500 1000 2000 4000 8000 LwA: 78 Sound Power Level @ Frequency, re: 10^-12 Watts 78 74 SONES: 15.5 83 81 72 70 66 64 (dB)

Ducted inlet or ducted outlet dBA @5 ft. 67 Ducted inlet and ducted outlet dBA @5 ft. 47

### Performance Curve

### DELHI Model G10-9 CFM=1521 SP=1.2 BHP=0.51 S. Eff=56% RPM=1001 FEI=1.42

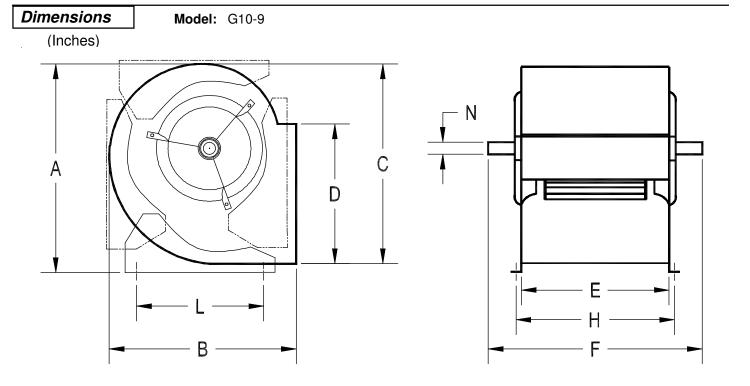




Drive Information						
Motor Pulley	Turns Open	Blower P	•	Bushin	g	Belt
8400 x 1/2" \ 8500035	3	MBL67 \ 85	00003	H x 3/4 \ 85	00062	4L380 \ 8200008
Motor Data				Motor		
Motor HP and Type	Volts/F	hase	Frame	RPM	Position	Canarm Part Number
3/4 ODP	[115] 115/	1 Phase	48	1750	1	1MD113-48-RS

Date: January 31, 2025

### Options



<u>A</u> <u>B</u> <u>C</u> <u>D</u> <u>E</u> <u>F</u> <u>H</u> <u>L</u> 19.0 16.75 17.375 11.375 12.25 17.25 13.25 13.375

### Standard Features

### G Series FC DWDI Blowers

- "Strong wheel design permits operation at speeds well beyond any normal requirements.
- Forward curved wheel provides quiet, low rpm operation.
- " Matte finish zinc coated wheel and cut-off baffle in a galvanized housing.
- Permanently lubricated bearings, mounted in resilient rings for quiet operation.
- Twin blowers are joined with steel angle pieces and have a common shaft.



# **Appendix G**

**Stationary Noise Calculations** 

### APPENDIX 'G'

Combining Sound Levels Power or Pressure Lsum=10log(10^(L1/10)+10^(L2/10)+....)
ASHRAE 2005 Fundamentals 7.3 eq. 12

Air Handling Unit*	Unit Size	Noise Level At Unit
DOAS 1-ASHP	50 Ton	89.0
DOAS GYM-ASHP	6 Ton	74.0
Fluid Cooler - FEVR-26408 (Fans)	n/a	91.0
Fluid Cooler - FEVR-26408 (Fans)	n/a	91.0
RTU1 GYM1-ASHP	11 Ton	77.0
RTU2 GYM2-ASHP	11 Ton	77.0
RTU3 CAFE-ASHP	16 Ton	84.0
RTU4 CAFE Perimeter-ASHP	11 Ton	77.0
Kitchen Exhaust Fan	n/a	66.0
Make-Up Exhaust Fan	n/a	78.0
Total dBA		95.8

Convert From Sound Power to Sound Pressure
ASHRAE 2005 Fundamentals 7.8 (28)
Free Field Lp=Lw+10log(Q/4 pi r^2)+10.5
Lp = Sound Pressure
Lw = Sound Power
Q = Directivity = 2 flat surface, 4 junction two large
surfaces, 8 in a corner
r = distance from source in ft

r = distance from source in ft

R3 - Noise Sensitive Receptor	Unit	Sound Power	Sound Pressure @ Receiver	Estimated Attenuation	Estimated dBA @ R3
		dBA @ 75% Unit Capacity	Distance (m) (Approx.)	dBA	
Stationary Noise Sources	DOAS 1-ASHP	89.0	75.7		43.6
	DOAS GYM-ASHP	74.0	115.5		24.9
	Fluid Cooler - FEVR-26408 (Fans)	91.0	96.5		43.5
	Fluid Cooler - FEVR-26408 (Fans)	91.0	103.4		42.9
	RTU1 GYM1-ASHP	77.0	128.0		27.1
	RTU2 GYM2-ASHP	77.0	122.7		27.4
	RTU3 CAFE-ASHP	84.0	128.7		34.0
	RTU4 CAFE Perimeter-ASHP	77.0	123.4		27.4
	Kitchen Exhaust Fan	66.0	110.1		17.4
	Make-Up Exhaust Fan	78.0	105.8		29.7
	Total R3 dBA				48.5

R4 - Noise Sensitive Receptor		Sound Power	Sound Pressure @ Receiver	Estimated Attenuation	Estimated dBA @ R4
		dBA @ 75% Unit Capacity	Distance (m) (Approx.)	dBA	
Stationary Noise Sources	DOAS 1-ASHP	89.0	152.2		37.6
	DOAS GYM-ASHP	74.0	112.8		25.2
	Fluid Cooler - FEVR-26408 (Fans)	91.0	121.3		41.5
	Fluid Cooler - FEVR-26408 (Fans)	91.0	128.2		41.0
	RTU1 GYM1-ASHP	77.0	102.7		29.0
	RTU2 GYM2-ASHP	77.0	103.4		28.9
	RTU3 CAFE-ASHP	84.0	98.8		36.3
	RTU4 CAFE Perimeter-ASHP	77.0	104.0		28.9
	Kitchen Exhaust Fan	66.0	119.5		16.7
	Make-Up Exhaust Fan	78.0	121.9		28.5
	Total R4 dBA				46.1

R5 - Noise Sensitive Receptor		Sound Power	Sound Pressure @ Receiver	Estimated Attenuation	Estimated dBA @ R5
		dBA @ 75% Unit Capacity	Distance (m) (Approx.)	dBA	
Stationary Noise Sources	DOAS 1-ASHP	89.0	140.9		38.2
	DOAS GYM-ASHP	74.0	114.3		25.0
	Fluid Cooler - FEVR-26408 (Fans)	91.0	115.9		41.9
	Fluid Cooler - FEVR-26408 (Fans)	91.0	109.9		42.4
	RTU1 GYM1-ASHP	77.0	114.0		28.1
	RTU2 GYM2-ASHP	77.0	104.6		28.8
	RTU3 CAFE-ASHP	84.0	88.1		37.3
	RTU4 CAFE Perimeter-ASHP	77.0	92.3		29.9
	Kitchen Exhaust Fan	66.0	104.2		17.8
	Make-Up Exhaust Fan	78.0	105.9		29.7
	Total R5 dBA				46.9



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