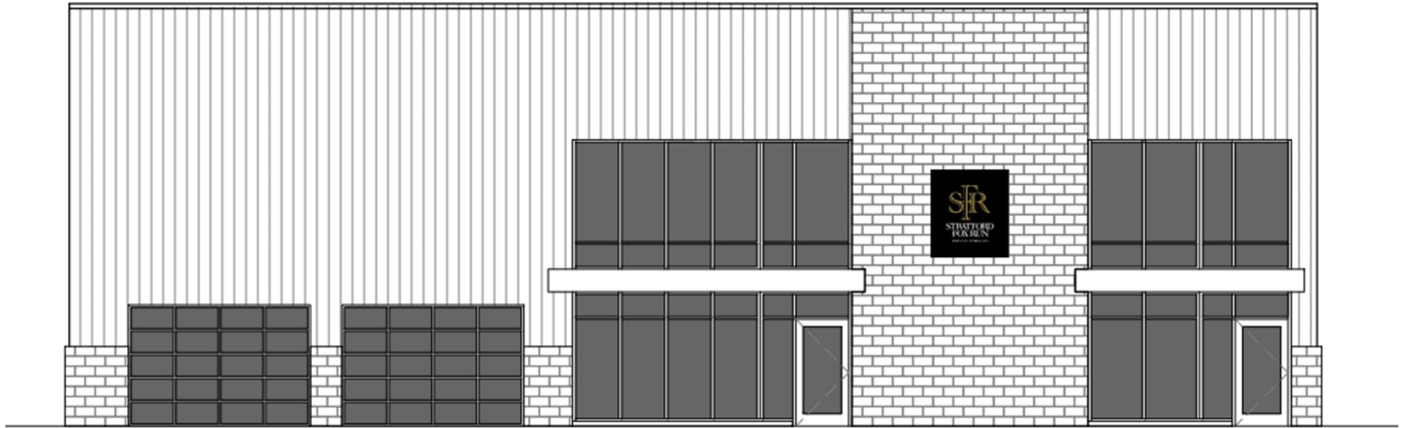


SERVICING & STORMWATER MANAGEMENT REPORT

DISTILLERY - 5923 OTTAWA STREET



Project No.: CCO-25-0415

City File No.:

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Table of Content

| | | |
|------------|--|-----------|
| 1.0 | PROJECT DESCRIPTION | 1 |
| 1.1 | Purpose | 1 |
| 1.2 | Site Description | 1 |
| 1.3 | Proposed Development and Statistics | 2 |
| 1.4 | Existing Conditions and Infrastructure | 2 |
| 1.5 | Approvals | 2 |
| 2.0 | BACKGROUND STUDIES, STANDARDS, AND REFERENCES | 2 |
| 2.1 | Background Reports / Reference Information | 2 |
| 2.2 | Applicable Guidelines and Standards | 3 |
| 3.0 | PRE-CONSULTATION SUMMARY | 4 |
| 4.0 | WATER SERVICING | 5 |
| 4.1 | Existing Watermain | 5 |
| 4.2 | Proposed Water Servicing | 5 |
| 5.0 | SANITARY SERVICING | 7 |
| 5.1 | Existing Sanitary Sewers | 7 |
| 5.2 | Proposed Sanitary Servicing | 7 |
| 6.0 | STORM SEWER SERVICING | 9 |
| 6.1 | Existing Storm Sewers | 9 |
| 6.2 | Proposed Storm Servicing | 9 |
| 7.0 | PROPOSED STORMWATER MANAGEMENT | 10 |
| 7.1 | Design Criteria | 10 |
| 7.2 | Runoff Coefficient Calculations | 10 |
| 7.3 | Pre-Development Drainage | 11 |
| 7.4 | Post-Development Drainage | 11 |
| 7.5 | Quantity Control | 12 |

| | | |
|-------|--|----|
| 7.6 | Quality Control..... | 14 |
| 7.7 | Village of Richmond Environmental Management Plan..... | 15 |
| 7.7.1 | Treatment Train..... | 15 |
| 7.7.2 | Thermal Mitigation..... | 15 |
| 7.7.3 | Water Balance..... | 16 |
| 7.7.4 | Volume Control (7 mm Storm Retention)..... | 16 |
| 7.7.5 | Control 100-Year Post to 2-Year Pre..... | 16 |
| 7.7.6 | Erosion Potential vs Additional Retention..... | 17 |
| 7.7.7 | Implementation of LID..... | 17 |
| 8.0 | EROSION AND SEDIMENT CONTROL..... | 18 |
| 8.1 | Temporary Measures..... | 18 |
| 8.2 | Permanent Measures..... | 18 |
| 9.0 | SUMMARY..... | 19 |
| 10.0 | CONCLUSIONS..... | 20 |
| 11.0 | STATEMENT OF LIMITATIONS..... | 21 |

Appendices

Appendix A: Site Location Plan

Appendix B: City of Ottawa Pre-Consultation Notes

Appendix C: Watermain Calculations

Appendix D: Sanitary Design

Appendix E: Pre-Development Drainage Plan

Appendix F: Post-Development Drainage Plan

Appendix G: Stormwater Management Calculations

Appendix H: City of Ottawa Design Checklist

1.0 PROJECT DESCRIPTION

1.1 Purpose

Egis Canada (Egis) has been retained by 99117756 Canada Inc. to prepare this Servicing and Stormwater Management Report in support of the Site Plan Control process for the proposed development located at 5923 Ottawa Street within the City of Ottawa.

The main purpose of this report is to present a servicing design for the development in accordance with the recommendations and guidelines provided by the City of Ottawa (City), the Rideau Valley Conservation Authority (RVCA), and the Ministry of the Environment, Conservation and Parks (MECP). This report will address the water, sanitary, and storm sewer servicing for the development, ensuring that proposed services will adequately service the development.

This report should be read in conjunction with the following drawings:

- CCO-25-0415, C101 – Lot Grading and Drainage Plan,
- CCO-25-0415, C102 – Site Servicing Plan,
- CCO-25-0415, C103 – Erosion & Sediment Control Plan,
- CCO-25-0415, PRE – Pre-Development Drainage Area Plan (Appendix 'E'), and
- CCO-25-0415, POST – Post-Development Drainage Area Plan (Appendix 'F').

1.2 Site Description

Figure 1: Site Map



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The property is located at 5923 Ottawa Street within the City of Ottawa. It is described as Part of Unit 10, Index Plan D-26, geographic township of Goulbourn, City of Ottawa. The land in question covers approximately 2.27 ha and is located near the intersection of Ottawa Street and Eagleson Road. See Site Location Plan in Appendix 'A' for more details.

1.3 Proposed Development and Statistics

The proposed development consists of two phases. Phase 1 covers 1.17 ha and proposes a new 651 m² ground-floor area building with a distillery/warehouse, restaurant, and retail space. Phase 2 covers 1.10 ha and proposes a new 926 m² ground-floor area brewery building. Parking and drive aisles will be provided throughout each phase along with landscaping around the perimeter of the development area. The development will be accessed via the proposed site entrances from Ottawa Street.

1.4 Existing Conditions and Infrastructure

The existing site is currently undeveloped with no available municipal services. A municipal ditch fronts the subject site along Ottawa Street. The Smiths Falls Rail Corridor is located northwest of the subject site.

1.5 Approvals

The proposed development is subject to the City of Ottawa site plan control approval process. Site plan control requires the City to review, provide concurrence and approve the engineering design package. Permits to construct can be requested once the City has issued a site plan agreement.

An Environmental Compliance Approval (ECA) through the Ministry of Environment, Conservation and Parks (MECP) will be required based on the proposed industrial usage of the site. An ECA application will be submitted following concurrence from the City on the grading, servicing, and stormwater management design.

2.0 BACKGROUND STUDIES, STANDARDS, AND REFERENCES

2.1 Background Reports / Reference Information

Background plans and studies that have been completed for the proposed site are listed below:

- Plan of Survey, drawing CCO-25-0415 Ottawa St, prepared by Egis Surveying Inc. and dated July 9, 2024.
- Site Plan, drawing A-001, prepared by N45 Architecture Inc. and dated July 29, 2025.
- Geotechnical Investigation, Proposed Commercial Development, prepared by Paterson Group, and dated July 9, 2025.
- Ditch Hydrologic and Hydraulic Analysis, prepared by JFSA, and dated September 10, 2025

- Sewage System Layout Plan, Drawing PH4924-1(rev.4), prepared by Paterson Group, and dated August 14, 2025
- 5923 Ottawa Street Occupancy Alternative Solution Roadmap memorandum, prepared by LRI, and dated August 21, 2025
- 5923 Ottawa Street Distillery water Storage Volume Estimate, prepared by LRI, and dated August 21, 2025
- Village of Richmond Environmental Management Plan, dated June 17, 2010.

2.2 Applicable Guidelines and Standards

City of Ottawa:

- ◆ Ottawa Sewer Design Guidelines, City of Ottawa, SDG002, October 2012. (Ottawa Sewer Guidelines)
 - Technical Bulletin ISTB-2014-01 City of Ottawa, February 2014. (ISTB-2014-01)
 - Technical Bulletin PIETB-2016-01 City of Ottawa, September 2016. (PIETB-2016-01)
 - Technical Bulletin ISTB-2018-01 City of Ottawa, January 2018. (ISTB-2018-01)
 - Technical Bulletin ISTB-2018-04 City of Ottawa, March 2018. (ISTB-2018-04)
 - Technical Bulletin ISTB-2019-02 City of Ottawa, February 2019. (ISTB-2019-02)
 - Technical Bulletin IWSB-2024-04 City of Ottawa, September 2024. (ISTB-2024-04)
- ◆ Ottawa Design Guidelines – Water Distribution City of Ottawa, July 2010. (Ottawa Water Guidelines)
 - Technical Bulletin ISD-2010-2 City of Ottawa, December 15, 2010. (ISD-2010-2)
 - Technical Bulletin ISDTB-2014-02 City of Ottawa, May 2014. (ISDTB-2014-02)
 - Technical Bulletin ISTB-2018-02 City of Ottawa, March 2018. (ISTB-2018-02)
 - Technical Bulletin ISTB-2021-03 City of Ottawa, August 2021. (ISTB-2021-03)
 - Technical Bulletin IWSB-2024-05 City of Ottawa, November 2024. (IWSB-2024-05)

Ministry of Environment, Conservation and Parks:

- ◆ Stormwater Planning and Design Manual, Ministry of the Environment, March 2003. (MECP Stormwater Design Manual)
- ◆ Design Guidelines for Sewage Works, Ministry of the Environment, 2008. (MECP Sewer Design Guidelines)

Other:

- ◆ Water Supply for Public Fire Protection, Fire Underwriters Survey, 2020. (FUS Guidelines)

3.0 PRE-CONSULTATION SUMMARY

A pre-consultation meeting was conducted on March 21st, 2024, regarding the proposed site. Specific design parameters to be incorporated within this design include the following:

- Control post-development flows to the 2-year pre-development peak flow rate with $C=0.5$ or existing, whichever is lesser, for all storms up to and including the 100-year storm event.
- Quality control to be provided up to an enhanced level of treatment (80% TSS Removal).

The notes from the City of Ottawa can be found in Appendix 'B'.

4.0 WATER SERVICING

4.1 Existing Watermain

The subject site is currently undeveloped with no access to a municipal watermain. Neighbouring properties are serviced by private wells.

4.2 Proposed Water Servicing

A new private drilled well and pump system is proposed within each phase to provide the development with domestic water supply. The wells, which will be designed and specified by others, will be included on the Servicing Plan once the location has been confirmed. As the development will be phased, it is proposed to temporarily service the Phase 2 building via the Phase 1 well. After the Phase 2 well is drilled, the service from the Phase 1 well will be abandoned and both buildings will be independently serviced. Please refer to the Hydrogeological Report and Terrain Analysis completed by Paterson Group for well capacity discussion.

Although the building will be serviced via a drilled well and pump system as described above, water demands based on occupancy areas are provided below for information purposes only. The water demands have been calculated to adhere to the Ottawa Design Guidelines – Water Distribution manual and can be found in Appendix 'C'.

Table 1: Water Supply Design Criteria and Water Demands

| Proposed Development | Phase 1 | Phase 2 |
|---------------------------------------|-----------------------|---------|
| Site Area | 1.17 ha | 1.10 ha |
| Commercial | 28,000 L/gross ha/day | |
| Commercial Peaking Factor (Max Day) | 1.5 x avg. day | |
| Commercial Peaking Factor (Peak Hour) | 1.8 x max. day | |
| Industrial | 35,000 L/gross ha/day | |
| Industrial Peaking Factor (Max Day) | 1.5 x avg. day | |
| Industrial Peaking Factor (Peak Hour) | 1.8 x max. day | |
| Average Day Demand (L/s) | 0.02 | 0.04 |
| Maximum Daily Demand (L/s) | 0.04 | 0.06 |
| Peak Hourly Demand (L/s) | 0.06 | 0.11 |

Fire protection is proposed to be provided by a remote fire protection system comprised of underground water storage tanks, dry hydrants, and a 150 mm diameter private watermain. The underground storage tanks will provide water to the building sprinkler systems as well as the dry hydrants. Both buildings will be equipped with fully supervised sprinkler systems, which require a supervisory signal to indicate conditions that could impair the operation of the system, as well as a water flow alarm to indicate the sprinkler system has been activated. The alarms must be sent to approved receiving facilities identified by the Fire Underwriters Survey.

The minimum required on-site storage volume was determined by LRI and provided in the 5923 Ottawa Street Distillery Water Storage Volume Estimate memo. The recommended on-site storage volume was determined by applying the Superior Tanker Shuttle reduction of 1,900 L/min to the NFPA13 mandated fire duration. The results are summarized in Table 2, below.

Table 2: On-Site Storage Volume Summary

| Proposed Development | Phase 1 | Phase 2 |
|---|-------------|-------------|
| OBC Flow Rate Requirement | 5,400 L/min | 5,400 L/min |
| OBC Volume Requirement | 177,100 L | 173,949 L |
| NFPA13 Volume Requirement | 288,442 L | 242,574 L |
| NFPA13 Evaluation w/Superior Tanker Shuttle Service Reduction | 118,117 L | 129,024 L |

As per Table 2, above, a minimum on-site water supply of 130,000 litres has been recommended by LRI. Please refer to the 5923 Ottawa Street Distillery Water Storage Volume Estimate prepared by LRI and included within Appendix 'C' for additional information.

On-site storage for both phases is proposed to be provided by shared underground concrete water storage tanks connected to two dry hydrants as well as the building sprinkler systems. The underground water storage tanks will be located adjacent to the Phase 2 layby area, and will include a draw pipe and chute as per City of Ottawa Figure 5, Figure 10, and standard drawings W51 and W52. A total of three 45,000 litre Boyd Bro's concrete water storage tanks are proposed for a total on-site storage volume of 135,000 litres. Each phase will include a layby area near the site entrance adjacent a private hydrant for firefighting access. A Siamese connection will be located within 45m of each layby area to allow Ottawa Fire Services to supplement sprinkler supply as required.

Please refer to the Site Servicing plan for more information on the servicing layout.

As the site contains high groundwater, a buoyancy review of the underground storage tanks was completed by Paterson Group. Paterson has indicated that ballasting blocks will be required to mitigation flotation of the tanks. Additional details will be provided once the servicing layout is approved and the tank locations are final.

5.0 SANITARY SERVICING

5.1 Existing Sanitary Sewers

The subject site is currently undeveloped with no access to a municipal sanitary sewer. Neighbouring properties are serviced by private septic systems.

5.2 Proposed Sanitary Servicing

A new septic bed located north of the proposed buildings will be installed for each phase and sized to accommodate the development.

Total Daily Design Sanitary Sewage Flow (TDDSSF) for Phases 1 and 2 was calculated by Paterson as 9,367 L/day and 600 L/day, respectively. It is understood that approval of on-site septic treatment will be governed by OBC, as the Daily Design Flow for each system will be less than 10,000 L/day. Refer to the septic design completed by Paterson Group, which has been submitted to the Ottawa Septic System Office (OSSO) and approved through Septic File #25-176 and #25-177. The permits can be found within Appendix 'D'.

In summary, both the Phase 1 and Phase 2 systems have been designed using Class 4 raised leaching beds in combination with an Ejjen GSF treatment system.

Phase 1 will treat up to 9,367 L/day of Effluent. The Phase 1 system will include a 28,101 L pretreatment tank and an 18,500 L balancing tank complete with a time operated control panel. The sanitary service exiting the building will be 100 mm diameter and sleeved through a 150 mm diameter pipe overlain by rigid insulation boards.

Phase 2 will treat up to 600 L/day of Effluent. The Phase 2 system will include a 3,600 L pretreatment tank and a 450 L balancing tank complete with a time operated control panel. The sanitary service exiting the building will be 100 mm diameter and sleeved through a 150 mm diameter pipe overlain by rigid insulation boards.

As the site contains high groundwater, a buoyancy review is required to mitigate flotation of the septic tanks. As per the Response to City Comments memorandum provided by Paterson Group and dated August 20th, 2025, this review was completed as part of the Sewage System Design process and no further action was deemed to be required.

For further design information pertaining to the on-site sewage system, please refer to the septic design completed by Paterson Group.

Although the building will be serviced via a septic system as described above, sanitary demands based on occupancy areas are provided below for information purposes only. The sanitary demands have been calculated to adhere to the Ottawa Sewer Design Guidelines and can be found in Appendix 'C'. Within the demand calculations, the restaurant area for Phase 1 has been increased to account for outdoor patio seating. The development area was considered instead of the full property area to provide a more reasonable infiltration

allowance estimate, as only a fraction of the property is being developed, and it is unlikely that downstream areas located a significant distance from the septic system will result in increased infiltration.

Sanitary Demand Criteria are listed in Table 3, below.

Table 3: Sanitary Design Criteria

| Design Parameter | Value |
|--|--------------------------------|
| Phase 1 Development Area | 0.48 ha |
| Phase 2 Development Area | 0.45 ha |
| Commercial Area | 280 L/person/day |
| Industrial – Light Area | 35,000 L/gross ha/d |
| Restaurant Area | 125 L/ (9.2 m ² /d) |
| Institutional/ Commercial Peaking Factor | 1.5 |
| Extraneous Flow Allowance | 0.33 L/s/ha |

Table 4, below, summarizes the estimated wastewater flow from the proposed development. Refer to Appendix 'D' for detailed calculations.

Table 4: Summary of Estimated Sanitary Flow

| Design Parameter | Total Flow (L/s) | |
|--|------------------|---------|
| | Phase 1 | Phase 2 |
| Total Estimated Average Dry Weather Flow | 0.10 | 0.04 |
| Total Estimated Peak Dry Weather Flow | 0.14 | 0.05 |
| Total Estimated Peak Wet Weather Flow | 0.27 | 0.17 |

As mentioned above, sanitary demand calculations based on the Ottawa Sewer Design Guidelines are provided for information only. The sanitary design and septic demand have been completed by Paterson Group based on Ontario Building Code requirements.

6.0 STORM SEWER SERVICING

6.1 Existing Storm Sewers

There are no existing storm sewers within the subject site or the adjacent municipal ROW. A municipal ditch fronts the subject site along Ottawa Street. A secondary ditch runs along the south of the Smiths Falls Rail Corridor at the rear of the site.

6.2 Proposed Storm Servicing

Runoff collected on the roof of the proposed Phase 1 and 2 buildings will be stored and controlled using flow restricting roof drains. Surface runoff from landscaped areas will be conveyed towards depressed surface storage areas located within the front yard of each phase. One minimum sized orifice for each phase will be used to direct controlled runoff from the surface storage areas to the municipal ditch along Ottawa Street during smaller storm events, while runoff exceeding the release rate of the orifices will be stored within the depressed surface storage areas. A weir is proposed for each surface storage area which will be located above the 100-year storage elevation. The weir will permit greater outflow in the event of a blockage within the system or a storm exceeding the 100-year event.

Runoff will be directed towards oil and grit separator units before discharging to the municipal ditch along Ottawa Street.

See CCO-25-0415 - POST in Appendix 'F' of this report and drawing C102 for more details. The Stormwater Management design for the subject property will be outlined in Section 7.0.

7.0 PROPOSED STORMWATER MANAGEMENT

7.1 Design Criteria

Stormwater management for the proposed site will be maintained through positive drainage away from the proposed building and towards the proposed depressed surface storage areas. The proposed stormwater management areas will capture and restrict runoff with the use of minimum sized orifices. The emergency overland flow route for the proposed site will be directed southeast towards the municipal ditch along Ottawa Street.

The quantitative and qualitative properties of the storm runoff for both the pre & post development flows are further detailed below. Stormwater Best Management Practices (SWM BMP's) will be implemented at the "Lot level", "Conveyance" and "End of Pipe" locations. These concepts will be explained further in Section 7.7.

In summary, the following design criteria have been employed in developing the stormwater management design for the site as directed by the RVCA and City:

Quality Control

- The site has been designed to achieve an 80% total suspended solids removal (enhanced level of treatment) using oil & grit separator units as part of a treatment train approach.

Quantity Control

- Post development 100-year flow is to be restricted to match the 2-year pre-development flow.

7.2 Runoff Coefficient Calculations

Runoff values presented in the report have been derived from the Hydrologic & Hydraulic analysis completed by JFSA. Please refer to the "Stratford Foxrun Development – 5923 Ottawa Street, Richmond Ditch Hydrologic and Hydraulic Analysis" for additional information.

Egis provided JFSA with the site area and runoff coefficients to be incorporated into their larger drainage areas. The following coefficients were used to develop an average C for each area:

| | |
|------------------------|------|
| Roofs/Concrete/Asphalt | 0.90 |
| Gravel | 0.60 |
| Undeveloped and Grass | 0.20 |

As per the City of Ottawa - Sewer Design Guidelines, the 2/5-year balanced 'C' value must be increased by 25% for a 100-year storm event to a maximum of 1.0.

7.3 Pre-Development Drainage

The existing site drainage limits are demonstrated on the Pre-and Post- Development Drainage Area Plans included in Appendix 'E'. The site is 2.27 ha overall, but for the purposes of this report, the pre-development drainage is focused on the area of development. A summary of the Pre-Development Runoff Coefficient Calculations can be found below.

Table 5: Pre-Development Runoff Coefficients Summary

| Drainage Area | Area (ha) | Runoff Coefficient (2/5-Year) | Runoff Coefficient (100-Year) |
|-----------------|-----------|-------------------------------|-------------------------------|
| A1 | 0.22 | 0.20 | 0.25 |
| A2 | 0.26 | 0.20 | 0.25 |
| Total (Phase 1) | 0.48 | - | - |
| A3 | 0.16 | 0.20 | 0.25 |
| A4 | 0.29 | 0.20 | 0.25 |
| Total (Phase 2) | 0.45 | | |

Area A1 and A3 represents the portion of the Phase 1 and Phase 2 development directed towards the rear yard in the existing condition, respectively. Areas A2 and A4 represent the portion of the Phase 1 and Phase 2 development areas directed towards the Ottawa Street municipal ditch in the existing condition, respectively.

Runoff directed towards the rear yard is conveyed along the railway ditch before discharging through a 1500 mm diameter culvert to Marlborough Creek, a tributary of the Jock River.

Runoff directed towards Ottawa Street is conveyed along the Ottawa Street and Eagleson Road municipal ditches before turning towards the ditch along the railway track and ultimately discharging through the same 1500 mm diameter culvert to Marlborough Creek. A Ditch Figure can be found within Appendix 'G'.

7.4 Post-Development Drainage

The proposed site drainage limits are demonstrated on the Post-Development Drainage Area Plan. See CCO-25-0415 - POST in Appendix 'F' of this report for more details. A summary of the Post-Development Runoff Coefficients can be found below.

Table 6: Post-Development Runoff Coefficients Summary

| Drainage Area | Area (ha) | Runoff Coefficient (2/5-Year) | Runoff Coefficient (100-Year) |
|-----------------|-----------|-------------------------------|-------------------------------|
| B1 | 0.42 | 0.51 | 0.58 |
| B2 | 0.07 | 0.90 | 1.00 |
| Total (Phase 1) | 0.48 | - | - |
| B3 | 0.35 | 0.49 | 0.56 |
| B4 | 0.09 | 0.90 | 1.00 |
| Total (Phase 2) | 0.45 | | |

Areas B1 represents Phase 1 surface runoff, while area B2 represents the Phase 1 roof area. Area B3 represents Phase 2 surface runoff, and area B4 represents the Phase 2 roof area. See Appendix 'G' for calculations.

For each phase, controlled roof runoff and uncontrolled surface runoff will be directed towards a depressed surface storage area located within the front yard. Phase 1 and Phase 2 will each employ a 75 mm diameter orifice to control outflow from its respective storage area. Each storage area will also include a 0.30m earth weir to allow for outflow in the event of a blockage within the system or a storm exceeding the 100-year event. The restriction of runoff will result in a ponding depth of 0.52m for Phase 1, and 0.66m for Phase 2 during the 100-year storm event. Stormwater management will be independent for each phase.

Runoff will be conveyed from the depressed surface storage areas to oil and grit separator units before discharging to the Ottawa Street municipal ditch.

7.5 Quantity Control

The 2- to 100-year post development runoff for the site must be restricted to match the 2-year pre-development flow rate.

JFSA was retained to complete a Hydrologic and Hydraulic analysis of the proposed stormwater management design to confirm there will be no negative impacts to the receiving ditch. A pre- and post-development hydrologic model was created with SWMHYMO, and hydraulic modeling was completed using HEC-RAS.

Table 7, below, summarizes the site release rates and required storage volumes for the post-development condition based on JFSA's analysis. For further information, refer to the memo prepared by JFSA and included in Appendix 'G'.

Table 7: Site Release Rates / Required Storage Volume / Ponding Elevation

| | Phase 1 (0.48 ha) | | | Phase 2 (0.45 ha) | | |
|--------------|----------------------------------|------------------------------------|-------------------|----------------------------------|------------------------------------|-------------------|
| Storm | Peak Outflow (m ³ /s) | Required Storage (m ³) | Storage Elev. (m) | Peak Outflow (m ³ /s) | Required Storage (m ³) | Storage Elev. (m) |
| 2YrCHI3Hr | 0.033 | 34 | 94.113 | 0.031 | 38 | 94.058 |
| 5YrCHI3Hr | 0.054 | 64 | 94.189 | 0.049 | 65 | 94.167 |
| 10YrCHI3Hr | 0.072 | 85 | 94.231 | 0.064 | 84 | 94.220 |
| 25YrCHI3Hr | 0.094 | 113 | 94.284 | 0.083 | 109 | 94.280 |
| 50YrCHI3Hr | 0.109 | 134 | 94.323 | 0.096 | 129 | 94.323 |
| 100YrCHI3Hr | 0.130 | 158 | 94.364 | 0.114 | 150 | 94.366 |
| 2YrSCS24Hr | 0.036 | 43 | 94.139 | 0.034 | 45 | 94.091 |
| 5YrSCS24Hr | 0.056 | 72 | 94.205 | 0.051 | 71 | 94.185 |
| 10YrSCS24Hr | 0.070 | 91 | 94.244 | 0.064 | 89 | 94.232 |
| 25YrSCS24Hr | 0.088 | 117 | 94.292 | 0.080 | 112 | 94.286 |
| 50YrSCS24Hr | 0.101 | 136 | 94.327 | 0.090 | 130 | 94.325 |
| 100YrSCS24Hr | 0.115 | 157 | 94.362 | 0.103 | 149 | 94.364 |

Table 8, below, summarizes the Pre- and Post- development peak flow within the Ottawa Street Municipal Ditch at the southeast corner of the property (Junction J1 from the modeling results).

Table 8: Pre- and Post-Development Peak Flow Summary

| | Peak Flow (m ³ /s) | | |
|------------|-------------------------------|------------------|------------|
| Storm | Pre-Development | Post-Development | Difference |
| 2YrCHI3Hr | 0.015 | 0.019 | 0.004 |
| 5YrCHI3Hr | 0.026 | 0.027 | 0.001 |
| 10YrCHI3Hr | 0.035 | 0.032 | -0.003 |
| 25YrCHI3Hr | 0.047 | 0.038 | -0.009 |
| 50YrCHI3Hr | 0.057 | 0.043 | -0.014 |

| | | | |
|--------------|-------|-------|--------|
| 100YrCHI3Hr | 0.067 | 0.048 | -0.019 |
| 2YrSCS24Hr | 0.024 | 0.024 | 0.000 |
| 5YrSCS24Hr | 0.038 | 0.032 | -0.006 |
| 10YrSCS24Hr | 0.049 | 0.037 | -0.012 |
| 25YrSCS24Hr | 0.062 | 0.044 | -0.018 |
| 50YrSCS24Hr | 0.073 | 0.049 | -0.024 |
| 100YrSCS24Hr | 0.084 | 0.055 | -0.029 |

As seen in Table 8, above, there will be a minor increase in flow during smaller storm events. The increase in flow is the result of additional area being directed towards the Ottawa Street municipal ditch that was directed towards the rear yard in the existing condition. Outflow during smaller events is controlled by an orifice at the minimum allowable size, and so reducing flow by reducing orifice size is not recommended. Furthermore, based on JFSA's analysis, it has been determined that there will be no negative downstream impact to the roadway or existing buildings resulting from the minor increase in runoff during smaller events.

During larger storm events, the modeling results indicate there will be a reduction in peak flow, and a reduction in the 100-year floodplain.

For more information on the Hydrologic and Hydraulic modeling completed by JFSA, please refer to the memo included in Appendix 'G'.

7.6 Quality Control

The development of this lot will employ Best Management Practices (BMP's) wherever possible. The intent of implementing stormwater BMP's is to ensure that water quality and quantity concerns are addressed at all stages of development. Lot level BMP's typically include temporary retention of the parking lot runoff, minimizing ground slopes and maximizing landscaped areas.

Within areas B1 and B3, surface runoff from the Phase 1 & 2 drive aisle, parking lots, and asphalt loading areas will be directed towards proposed grassed swales located along the phase line and property line. The grassed swales have been designed with minimal slope to reduce runoff velocity and promote filtration and settlement of suspended solids.

The proposed grassed swales will discharge to depressed surface storage areas located within Phase 1 and 2. The depressed surface storage areas will restrict runoff and provide further opportunity for suspended solids removal through filtration and settlement. Removal efficiency of the depressed surface storage area will be most comparable to a dry pond, given that runoff will be temporarily detained during storm events and then released at a controlled rate.

As per the Environmental Design Criteria section of the MECP Stormwater Management Planning and Design Manual, dry ponds can be credited with achieving a Basic 60% long-term suspended solid removal provided the storage volumes identified within Table 3.2 of the Manual are achieved.

For the Phase 1 site, with an imperviousness of 52%, a storage volume of 141 m³/ha or 67.7 m³ is required to achieve a basic long-term 60% TSS removal, based on Table 3.2 of the Manual. The Phase 1 surface storage area will provide up to 158 m³ of stormwater storage, more than doubling the requirement.

For the Phase 2 site, with an imperviousness of 53%, a storage volume of 144 m³/ha or 64.7 m³ is required to achieve a basic long-term 60% TSS removal, based on Table 3.2 of the Manual. The Phase 2 surface storage area will provide up to 150 m³ of stormwater storage, again more than doubling the requirement.

To ensure the quality control criteria are met, the depressed surface storage areas will discharge to Stormceptor EFO4 oil and grit separator units located at the outlet of each phase. The EFO4 unit is credited with achieving a TSS removal of 60% based on the ETV particle size distribution. Documentation supporting the 60% removal efficiency can be found within Appendix 'G'.

Given that runoff entering the EFO4 will already have undergone a 60% TSS removal within the depressed surface storage area, there will be a maximum remaining TSS of 40% of the baseline. As a result, runoff leaving the EFO4 units will have a remaining TSS of $[40\% - (60\% * 40\%)] = 16\%$, indicating a total TSS removal of 84%. It should be further noted that TSS reduction from the grassed swales has not been accounted for, and so the actual TSS removal efficiency of the site is expected to be increased.

7.7 Village of Richmond Environmental Management Plan

As the subject site is located within the Village of Richmond Environmental Management Plan study area, the site must conform to the findings of the EMP. Concurrence with the findings and recommendations are listed below:

7.7.1 Treatment Train

The proposed stormwater management system will convey runoff within gently sloped swales to a depressed surface storage area where runoff will be stored and released at a controlled rate. This will provide an opportunity for filtration through the vegetated medium, infiltration, and settlement of suspended solids. Before leaving the site, controlled runoff will be directed to an Oil & Grit separator where additional quality treatment will be provided. These lot level, conveyance, and end-of-pipe controls will ensure stormwater quality is properly addressed and 80% TSS reduction is achieved.

7.7.2 Thermal Mitigation

As mentioned above, stormwater conveyance will primarily be through gently sloped grass swales, and stormwater will be stored within a landscaped depressed surface storage area before discharging to the municipal ditch. After leaving the site, runoff will travel a minimum 745m within the municipal and railroad ditches

before discharging to Marlborough Creek. With on-site detention of stormwater within landscaped areas and the length of the flow path to the outlet, thermal impacts to the receiving watercourse are not anticipated.

7.7.3 Water Balance

Based on the findings of the Hydrogeological Report and Geotechnical Report prepared by Paterson, the site is heavily constrained by high groundwater and soils that are not suitable for infiltration. The borehole results identified that all soils warranted a description containing either clay, silt, clayey, or silty. As per Technical Bulletin IWSB-2024-04, infiltration-type LID practices are not permitted in clay or silt soils, nor in soils that warrant a dual classification with silt or clay as per the USCS.

While the borehole logs identified some areas of glacial till consisting of silty sand that may be suitable for infiltration, the glacial till is most often described as “silty sand to sandy silt”, with a USCS soil classification of ML (inorganic silts of high plasticity) determined from BH3-24 SS3. The glacial till which solely consists of silty sand is also located below the high groundwater elevation of 93.79m – 93.86m identified by the Groundwater Monitoring Program. As per the Hydrogeological Report and Terrain Analysis, the highest elevation of the glacial till layer not containing “sandy silt” or “clayey silt” in the description was at BH2-25, where the top of the glacial till layer was noted at an elevation of 93.71m. As the glacial till layer comprised of silty sand is located below the seasonally high groundwater level, it cannot be incorporated into an infiltration-type LID. Furthermore, there is insufficient grade change within the site to allow for an infiltration-type LID to achieve minimum separation from the high groundwater level specified above.

While the site has been generally designed to promote infiltration with gently sloped grass conveyance swales and stormwater detention within landscaped surface storage areas, implementing an infiltration-type LID practice to ensure water balance will not be permitted, and so undertaking a water balance would not result in any changes to the design.

7.7.4 Volume Control (7 mm Storm Retention)

As mentioned above, an infiltration-type LID practice will not be permitted, and so the requirement to retain the first 7 mm of rainfall cannot be achieved through infiltration. Abstraction will be limited to depression storage within the gently sloped swales and stormwater management areas, and through evapotranspiration of the stored surface and roof runoff. Evapotranspiration has been promoted to the greatest extent possible within the design by providing orifice controls with the minimum permissible size. This will detain stormwater on site for long durations, resulting in maximum surface stormwater volumes of 158 m³ for Phase 1 and 150 m³ for Phase 2.

7.7.5 Control 100-Year Post to 2-Year Pre

Stormwater modeling has been completed by JFSA. The results indicated that while there will be a minor increase in runoff during smaller storm events, the 100-year peak flow will be a reduction compared to existing conditions. Additionally, the proposed stormwater management design will reduce the extent of the 100-year floodplain.

7.7.6 Erosion Potential vs Additional Retention

As previously mentioned, the design relies on detention of stormwater runoff and not retention, as an infiltration-based design will not be permitted. Minimum orifice sizes are proposed which result in the maximum on-site storage volume. Modeling has also been completed by JFSA which indicates there will be a reduction in flow leaving the site during larger stormer events.

7.7.7 Implementation of LID

LID has been implemented with vegetated swales and depressed vegetated surface storage areas.

8.0 EROSION AND SEDIMENT CONTROL

8.1 Temporary Measures

Before construction begins, temporary silt fence, straw bale or rock flow check dams will be installed at all natural runoff outlets from the property. It is crucial that these controls be maintained throughout construction and inspection of sediment and erosion control will be facilitated by the Contractor or Contract Administration staff throughout the construction period.

Silt fences will be installed where shown on the final engineering plans, specifically along the downstream property limits. The Contractor, at their discretion or at the instruction of the City, Conservation Authority or the Contract Administrator shall increase the quantity of sediment and erosion controls on-site to ensure that the site is operating as intended and no additional sediment finds its way off site. The straw bale check dams, silt fence, and rip rap outlet treatments shall be inspected weekly and after rainfall events. Care shall be taken to properly remove sediment from the silt fences and check dams as required. Care shall be taken at the removal stage to ensure that any silt that has accumulated is properly handled and disposed of. Removal of silt fences without prior removal of the sediments shall not be permitted.

Although not anticipated, work through winter months shall be closely monitored for erosion along sloped areas. Should erosion be noted, the Contractor shall be alerted and shall take all necessary steps to rectify the situation. Should the Contractor's efforts fail at remediating the eroded areas, the Contractor shall contact the City and/or Conservation Authority to review the site conditions and determine the appropriate course of action. As the ground begins to thaw, the Contractor shall place silt fencing at all required locations as soon as ground conditions warrant. Please see the Erosion & Sediment Control Plan for additional details regarding the temporary measures to be installed and their appropriate OPSD references.

8.2 Permanent Measures

Rip-rap will be placed at all locations that have the potential for concentrated flow. It is crucial that the Contractor ensure that the geotextile is keyed in properly to ensure runoff does not undermine the rip rapped area. Additional rip rap is to be placed at erosion prone locations as identified by the Contractor / Contract Administrator / City or Conservation Authority.

It is expected that the Contractor will promptly ensure that all disturbed areas receive topsoil and seed/sod and that grass be established as soon as possible. Any areas of excess fill shall be removed or levelled as soon as possible and must be located a sufficient distance from any watercourse to ensure that no sediment is washed out into the watercourse. As the vegetation growth within the site provides a key component to the control of sediment for the site, it must be properly maintained once established. Once the construction is complete, it will be up to the landowner to maintain the vegetation and ensure that the vegetation is not overgrown or impeded by foreign objects.

9.0 SUMMARY

- A new 651 m² distillery and restaurant/retail building is proposed within Phase 1 at 5923 Ottawa Street.
- A new 926 m² distillery building is proposed within Phase 2.
- Domestic water servicing will be provided by a new drilled well for each phase, designed by others.
- The Phase 2 building will be serviced by the Phase 1 well in the interim condition.
- Fire protection for Phases 1 and 2 will be provided by a remote hydrant system, sprinkler systems, and underground water storage tanks.
- Sanitary servicing will be provided by new on-site septic systems designed by Paterson.
- Storage for the 2- through 100-year storm events will be provided on the roof of the building and within proposed depressed surface storage areas. Runoff will discharge to the municipal ditch along Ottawa Street.
- Based on the hydrologic and hydraulic modeling completed by JFSA, there will be no negative downstream impact resulting from the stormwater management design.
- Quality control requirements will be achieved with oil and grit separator units as part of a treatment train approach.

10.0 CONCLUSIONS

This report has been provided to describe the servicing and stormwater management for the site located 5923 Ottawa Street.

This report is respectfully being submitted for review.

Regards,

Egis Canada Ltd.



Jessica Burden, P.Eng.
Project Engineer, Land Development
E: Jessica.burden@egis-group.com

A handwritten signature in black ink that reads "Francis Valenti".

Francis Valenti, P.Eng.
Junior Project Engineer, Land Development
E: francis.valenti@egis-group.com

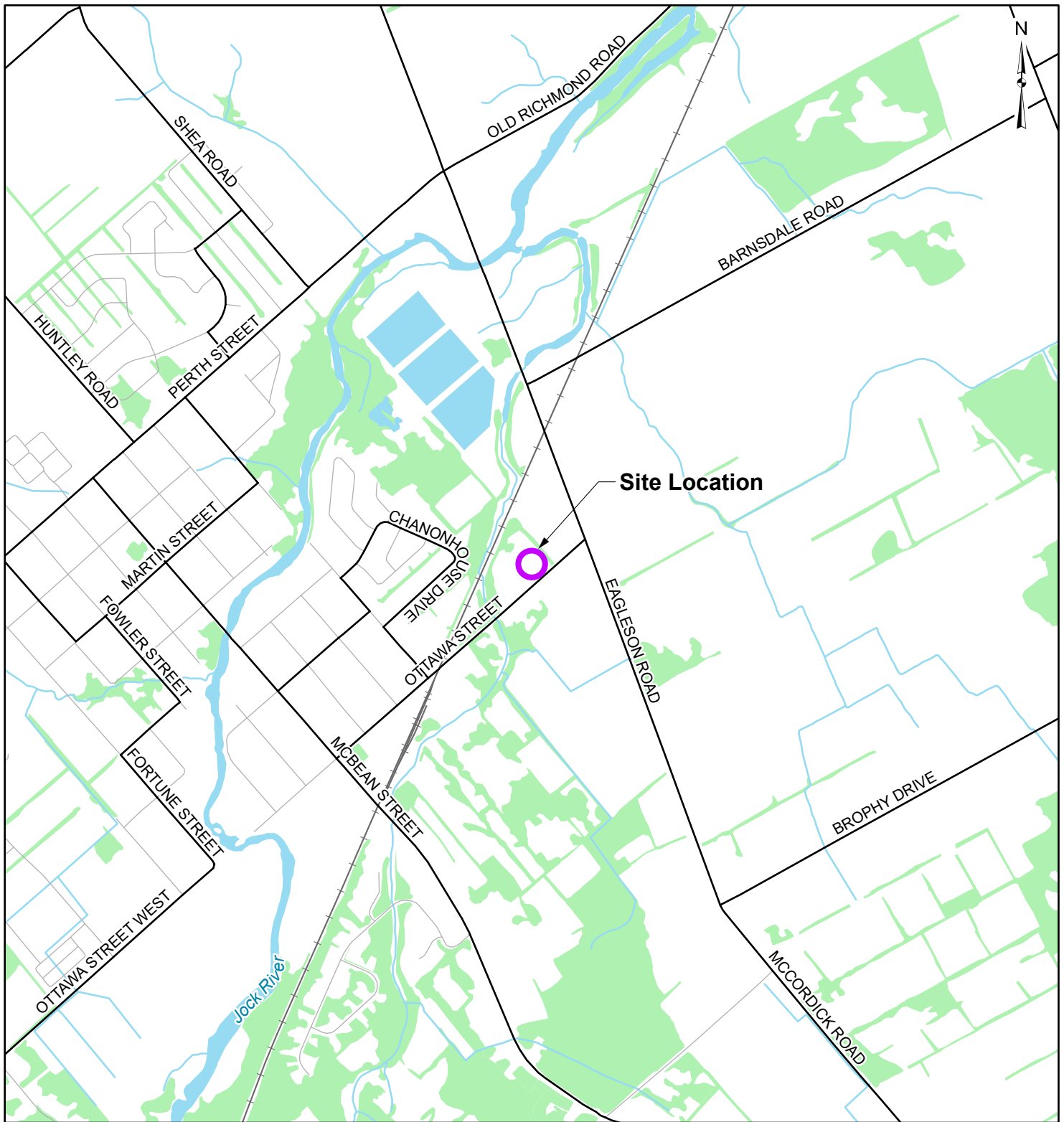
11.0 STATEMENT OF LIMITATIONS

This report was produced for the exclusive use of 99117756 Canada Inc. The purpose of the report is to assess the existing stormwater management system and provide recommendations and designs for the post-construction scenario that are in compliance with the guidelines and standards from the Ministry of the Environment, Conservation and Parks, City of Ottawa and local approval agencies. Egis Canada reviewed the site information and background documents listed in Section 2.0 of this report. While the previous data was reviewed by Egis Canada and site visits were performed, no field verification/measures of any information were conducted.








Any use of this review by a third party, or any reliance on decisions made based on it, without a reliance report is the responsibility of such third parties. Egis Canada accepts no responsibility for damages, if any, suffered by any third party as a result of decisions or actions made based on this review.

The findings, conclusions and/or recommendations of this report are only valid as of the date of this report. No assurance is made regarding any changes in conditions subsequent to this date. If additional information is discovered or becomes available at a future date, Egis Canada should be requested to re-evaluate the conclusions presented in this report, and provide amendments, if required.

APPENDIX A KEY PLAN



LEGEND

-  Site Location
-  Local Road
-  Major Road
-  Railroad
-  Watercourse
-  Waterbody
-  Wooded Area

REFERENCE

GIS data provided by the Ontario Ministry of Natural Resources and Forestry, 2024.



| | | | |
|---|--|------------------------------|----------------|
| CLIENT: | | 99117756 CANADA INC. | |
| PROJECT: | | 5923 OTTAWA STREET, RICHMOND | |
| TITLE: | | SITE LOCATION PLAN | |
|  115 Walgreen Road, RR3, Carp, ON K0A1L0 Tel: 613-836-2184 Fax: 613-836-3742 | | PROJECT NO: CCO-25-0415 | FIGURE: |
| | | Date | Sep., 04, 2024 |
| | | GIS | CZ |
| | | Checked By | AG |
| | | 1 | |

APPENDIX B BACKGROUND DOCUMENTS

March 27, 2024

Bridgette Alchawa
Egis Canada Ltd.
Via email: bridgette.alchawa@egis-group.com

**Subject: Pre-Consultation: Meeting Feedback
Proposed Site Plan Control Application – 5923 Ottawa St**

Please find below information regarding next steps as well as consolidated comments from the above-noted pre-consultation meeting held on March 21, 2024.

Pre-Consultation Preliminary Assessment

| | | | | |
|----------------------------|----------------------------|----------------------------|---------------------------------------|----------------------------|
| 1 <input type="checkbox"/> | 2 <input type="checkbox"/> | 3 <input type="checkbox"/> | 4 <input checked="" type="checkbox"/> | 5 <input type="checkbox"/> |
|----------------------------|----------------------------|----------------------------|---------------------------------------|----------------------------|

One (1) indicates that considerable major revisions are required while five (5) suggests that the proposal appears to meet the City's key land use policies and guidelines. This assessment is purely advisory and does not consider technical aspects of the proposal or in any way guarantee application approval.

Next Steps

1. A review of the proposal and materials submitted for the above-noted pre-consultation has been undertaken. Please proceed to complete a Phase 2 Pre-consultation Application Form and submit it together with the necessary studies and/or plans to planningcirculations@ottawa.ca.
2. In your subsequent pre-consultation submission, please ensure that all comments or issues detailed herein are addressed. A detailed cover letter stating how each issue has been addressed must be included with the submission materials. Please coordinate the numbering of your responses within the cover letter with the comment number(s) herein.
3. Please note, if your development proposal changes significantly in scope, design, or density before the Phase 3 pre-consultation, you may be required to complete or repeat the Phase 2 pre-consultation process.

Supporting Information and Material Requirements

1. The attached **Study and Plan Identification List** outlines the information and material that has been identified, during this phase of pre-consultation, as either required (R) or advised (A) as part of a future complete application submission.

- a. The required plans and studies must meet the City's Terms of Reference (ToR) and/or Guidelines, as available on Ottawa.ca. These ToR and Guidelines outline the specific requirements that must be met for each plan or study to be deemed adequate.

Consultation with Technical Agencies

1. You are encouraged to consult with technical agencies early in the development process and throughout the development of your project concept. A list of technical agencies and their contact information is enclosed.

Planning

Comments:

Questions:

1. What is the intent for the proposed bar/pub use. Restaurants are a prohibited use per 385r.

Response: It is understood that liquor can be sold if it is the product being produced. The current idea for the restaurant is to offer food that is easily prepared, (sandwiches, pizza, etc.) however, applicant suggested that they may be willing to consider different options based on zoning interpretation.

2. What is the idea for the severance component? May not have enough space to achieve the severance once the full build out of the lot is considered.
3. What is the timing of the severance? There are potential concerns regarding a pre-mature severance.

Response: The idea is for the severance to occur after the site plan application/approval and the establishment of the site.

Official Plan

1. The subject site is designated Village on Schedule B9 of the Official Plan.
2. The subject site is designated Village Industrial Area on Schedule A of the Village of Richmond Secondary Plan – Volume 2.
 - a. Uses permitted on lands designated Village Industrial Area include: light industrial uses, office, printing plant, service repair shop, small batch brewery, warehouse and heavy equipment and vehicle sales, rental and servicing, research, technology, nurseries, greenhouses, catering, places of assembly, broadcasting and training

- b. Maximum building height - four storeys
- c. Adequate buffering including landscaping and screening will be provided between uses in Industrial Areas to ensure that storage areas and parking areas are screened from adjacent properties

Zoning By-law

- 3. The subject site is zoned RG3 [385r] under the Zoning By-law. The purpose of the RG (Rural General Industrial) is to permit development of light industrial uses in Village designations; accommodate a range of light industrial uses and limited service commercial uses for the travelling public; and, regulate development in a manner that respects adjacent land uses and will have a minimal impact on the surrounding rural area. The RG3 subzone recognizes smaller parcels.
- 4. Permitted uses in the RG3 zone include [S.219 (1)]:
 - n. Light industrial uses
 - t. Warehouse
- 5. Conditional Permitted Uses - The following are permitted subject to the use being located on the same lot as a use listed above.
 - c. Bar
 - A bar must be ancillary to a permitted brewery, winery or distillery and, may not have a gross floor area exceeding the lesser of:
 - 300 square metres, or
 - 25% of the floor area of the brewery, winery or distillery to which it is ancillary.
- 6. The site is subject to Rural Exception 385r which lists restaurants as a prohibited use.**
- 7. The proposal must meet the following 385r Exception Provisions and the RG3 provisions provided in Section 219.
 - a. Minimum front yard – 15m
 - b. Maximum lot coverage – 35 percent
 - c. No maximum building height
- 8. Minimum parking space rates as required by S.101, Table 101.
 - a. Bars – 6 per 100sq.m of g.f.a
 - b. Light industrial use – 0.8 per 100sq.m of g.f.a
 - c. Retail Store – 3.4 per 100sq.m of g.f.a

9. A landscape buffer for the parking lot will be required in accordance Table 110.
10. Outdoor refuse collection and loading areas must be:
 - a. Located at least 9 metres from a lot line abutting a public street
 - b. Located at least 3 metres from any other lot line
 - c. Screened from view by an opaque screen with a minimum height of 2.0 metres
11. Bicycle parking must be provided in accordance with Section 111.
12. If loading spaces are provided, they must be in accordance with Section 113.

Discussion and Submission Requirements

13. Subject Exception Zone prohibits restaurants as a use.
14. Zoning by-law interpretation staff have confirmed that a bar/pub serving food and drink ancillary to the distillery and contained within the same structure would be aligned with the intent of the zoning.
15. If the bar/pub component were to be contained in a separate structure, it would be more closely aligned with a restaurant and would not be permitted under the current zoning.
16. A Site Plan will be required. The plan must be prepared as per the City's [Terms of Reference](#) and must address the following:
 - a. The site plan must clearly identify the required yard setbacks from all existing lot lines
 - b. The Site Plan must clearly identify all existing buildings
 - c. The required landscaped area must be included
 - d. Parking spaces must be clearly defined, as well as the access driveway, and any drive aisles throughout the site
17. A Landscape Plan will be required. The plan must be prepared in accordance with the [Landscape Plan Terms of Reference](#) and include all of the listed general elements as well as detail existing and proposed vegetation.
18. Plan of Survey showing the current site conditions prepared in accordance with the City's [Plan of Survey Terms of Reference](#).

Urban Design

Comments:

Submission Requirements:

19. Urban Design Brief is required.. Please see attached customized Terms of Reference to guide the preparation.
 - i. The Urban Design Brief should be structured by generally following the headings highlighted under Section 3 – Contents of these Terms of Reference.
 - ii. The proposal is not subject to the Urban Design Review Panel.
20. Additional drawings and studies are required as shown on the SPIL. Please follow the terms of references ([Planning application submission information and materials | City of Ottawa](#)) the prepare these drawings and studies.
 - i. Design Brief
 - ii. Site Plan
 - iii. Landscape Plan
 - iv. Elevations

Comments on Preliminary Design – Applicants are to provide a response to these comments in the Design Brief.

21. The following policies/guidelines apply:
 - a. Village Industrial within the Richmond Secondary Plan
 - b. Design Guidelines for Rural Villages
22. Please reference the direction within the Design Guidelines to help inform the design of the building as the design progresses. The architectural directions in the guidelines should guide the building design as closely as possible.
23. Please ensure that landscaping and tree planting is provided along Ottawa Street frontage.

24. Please ensure that the patio is a comfortable place for patrons and separated from road noise. Please provide screening and perimeter landscaping.

Feel free to contact Lisa Stern, Planner III, for follow-up questions.

Engineering

Comments:

25. Servicing

- a. A **Site Servicing Study** will be required with the Site Plan Control application. This report should be completed exceeding the minimum requirements laid out in the Site Servicing Study Terms of Reference. The report will serve to address how the design of the site complies with City design guidelines, Official Plan policies, among other evaluation criteria noted in the Terms of Reference. Stormwater management, which is a component of the Servicing Study, is required to mitigate the effects of urbanization on the hydrologic cycle including increased runoff and decreased infiltration, of rain and snowmelt. Without proper stormwater management, a site can negatively impact the environment by reducing baseflow, degrading water quality, and increasing flooding and erosion. This leads to reduced diversity of aquatic life, fewer opportunities for human uses of water resources, and loss of property and human life. The City looks to lessen these risks by reviewing development to ensure stormwater management practices are being implemented, infrastructure is resilient to future climate conditions, including extreme weather events, and using low impact development where feasible to manage smaller, infrequent events. The Official Plan, which receives authority through the Planning Act, identifies in Policy 6, section 2.2.3, that flooding is the costliest type of natural disaster in Canada.
- b. There is no public service capacity currently available to have the option of extending public services to the proposed development. Development therefore must be on the basis of private services. The Village has a limited municipal water network and limited sanitary network & pump station capacity. Any planned growth would need to include network, and possibly plant, upgrades to support proposed development, which is likely too onerous for the scope of this development.
- c. In terms of the Stormwater Management for the Site Plan Control application, the quantity criteria will be that the 100-yr post development peak flow rate must match the 2-year pre-development

peak flow rate. As part of complete Site Plan Control application, whether development or redevelopment, the report must identify and mitigate the impacts of additional runoff resulting from increased imperviousness through measures such as site-specific stormwater management postulated in policy 6, section 4.7.1 of the Official Plan.

- d. In terms of a Stormwater Management approach, runoff volume control should proceed in the following hierarchical order, with each step exhausted before proceeding to the next:
 - 1. Retention (infiltration, reuse, or evapotranspiration),
 - 2. Low Impact Development (LID) filtration, and
 - 3. Conventional Stormwater management. Conventional stormwater management, should proceed only once Maximum Extent Possible has been attained for Steps 1 and 2 for retention and filtration.
- e. The pre-development runoff coefficient or a maximum equivalent 'C' of 0.5, whichever is less as described in the Sewer Design Guidelines, Second Edition, document no. SDG002, October 2012, City of Ottawa, including technical bulletins ISDTB-2014-01, PIEDTB-2016-01, ISTB 2018-01, ISTB-2018-04, ISTB-2019-02, section 8.3.7.3.
- f. A calculated time of concentration cannot be less than 10 minutes as described in section 5.1.4 of the Sewer Design Guidelines.
- g. The water quality control should be an enhanced level treatment, 80% long term suspended sediment removal. The City will be looking for a treatment train approach for water quality treatment. Reporting of TSS removal shall be extensive and if peer reviewed and published papers are relied on for conclusions, the conclusions shall be patently clear and the report shall show overwhelming agreement.
- h. Runoff will need to be conveyed to a legal and sufficient outlet. If it is proposed to discharge storm water to the existing ditches in the ROW, the ditches will need to be shown to provide continuous flow to an outlet. This comment is sourced from the Official Plan which notes in policy 8, section 4.7.1, that proof of legal and sufficient outlet for proposed stormwater management and drainage systems will be required as a condition of future Site Plan Control.
 - i. The 1 in 100-year floodplain is present along the rear portion of the lot. Any site alteration within this area requires a permit from the Conservation Authority. The Official Plan, in section

10.1.1, notes that development and site alteration shall not be permitted in the 1 in 100 year flood plain.

- j. Low Impact Development (LID) is to be implemented as per the bulletin from the former MOECC (now MECP) titled Expectations RE: Stormwater Management released in February 2015. The infiltration target for the site is typically determined from an applicable higher-level study, which is confirmed through on-site infiltration/percolation testing. The reporting should identify the treatment train of processes proposed for the development. The Official Plan defines LID as a stormwater management strategy that seeks to mitigate the impacts of increased runoff and stormwater pollution by managing runoff as close to its source as possible. LID comprises a set of site design strategies that minimize runoff through distributed, small scale structural practices that mimic natural or predevelopment hydrology through the processes of infiltration, evapotranspiration, harvesting, filtration and detention of stormwater. These practices can effectively remove nutrients, pathogens and metals from runoff, and they reduce the volume and intensity of stormwater flows. The City has released a document titled 'Low Impact Development Technical Guidance Report – Implementation in Areas with Potential Hydrogeological Constraints' which aids sites which may have constraints such as low permeability or high groundwater.
- k. The anticipated water demands (average day, maximum daily, and maximum hour) must be presented and justified for any hydrogeological pumping test rate. The pumping rate should be the maximum daily demand rate. The Ottawa Design Guidelines – Water Distribution provide information for determining water demand rates for the proposed zoning or uses in Table 4.2 – Consumption Rates.

26. Fire Services

- a. The Site Servicing Study must include a section addressing the provision of a **water supply for fire suppression**, determination of the required fire flow, and confirmation of whether any on-site storage will be required. It is the responsibility of the owner to ensure that an adequate water supply for firefighting is provided. The FUS (Fire Underwriters Survey) methodology, as opposed to the OBC methodology shall be applied for all rural areas.
 - i. It is anticipated that mitigative measures, including on-site storage, will be required given the group F, division 1 for distilleries. This occupancy is considered a high hazard occupancy under the Ontario Building Code. There will be risks with regards to the flammable or explosive off-gasses or

vapours, that must be contemplated and appropriately mitigated by the reporting.

- ii. The project, due to the proposed occupancy, will not be eligible to forgo the requirement for on-site fire retention storage.
 - iii. As mentioned the Phase 1 meeting, the applicant could retain a fire safety consultant to aid in the preparation of the FUS calculations. The specialist fire-fighting consultant would review a number of factors and could propose an alternative approach satisfactory to Development Review and the City's Fire Protection Engineer, Allan Evans.
 - iv. Enhanced review will be invoked should the construction coefficient chosen be less than 1.
- b. Fire Routes now require designation with By-law through the Site Plan process by contacting fireroutes@ottawa.ca once preliminary Site Plan approval has been provided.

27. Grading

- a. A **Grading and Drainage Plan** will be required with the Site Plan Control application identifying the existing and proposed drainage patterns and their relationship with the surface runoff control. As part of a complete Site Plan Control application, the Grading and Drainage Plan should identify and implement site, grading, building, and servicing design measures to protect new development from flooding as per policy 6, section 4.7.1 of the Official Plan. The Grading and Drainage Plan forms part of the requirements for Site Plan Control applications noted in the Studies and Plan Identification List, provided with the feedback documents.
- b. The Plan should have a note that references the horizontal and vertical datums that were used and tied into to complete the project. The drawing should also make reference (on the face of the plan) to a site benchmark that can be used by anyone with a level to carry out checks on the particular project.

28. Erosion and Sediment Control

- a. An **Erosion and Sediment Control Plan** will be required with the Site Plan Control Application. Erosion and sediment control plans shall have regard to Canadian Standards Association (CSA) W202 Erosion and Sediment Control Inspection and Monitoring Standard (as amended).

29. Geotechnical

- a. A **Geotechnical Study** will be required with the Site Plan Control application. The report should provide sufficient soils and engineering information to confirm that the site(s) are suitable or can be made suitable for development based on the requirements of the Geotechnical Investigation and Reporting Guidelines for Development Applications in the City of Ottawa.
- b. It is highly likely that sensitive marine clays will be encountered on the site. If the presence of clays is confirmed, enhanced investigations must be undertaken with vane shear, Atterberg limits, shrinkage, size, grade raise restriction, consolidation, sensitivity, and liquefaction analysis-amongst others.
- c. As the site is potentially underlain by compressible marine clays, long term groundwater monitoring will be required to support the development. Groundwater elevations are anticipated to be high (shallow) given the location in Richmond. The capacity of the deposit to accept additional load depends on the groundwater level. The Stormwater Management and LID design will also be impacted by the groundwater level.

30. Hydrogeological and Terrain Analysis Requirements (private servicing)

- a. A **Hydrogeological and Terrain Analysis** will be required for the Site Plan Control application to establish that there is an adequate quantity and quality of groundwater to support the proposed development(s). The requirements for the Hydrogeological and Terrain Analysis Report are outlined in the City of Ottawa Hydrogeological and Terrain Analysis Guidelines, Section 5.0 for Site Plans. The study forms part of the requirements for Site Plan Control applications noted in the Studies and Plan Identification List, provided with the feedback documents.
- b. Note that the onsite well would provide groundwater which serves the public and thus may be considered a regulated small drinking water system under O.Reg. 319/08: Small Drinking Water Systems. The application would also need to contact and incorporate any requirements set by medical officers of health or Ottawa Public Health. Any requirements related to the regulated small drinking water system must be fulfilled prior to the use of the system. "drinking water system" means a system of works, excluding plumbing, that is established for the purpose of providing users of the system with drinking water and that includes, (a) any thing used for the collection, production, treatment, storage, supply or distribution of water and (b) a well or intake that serves as the source or entry point of raw water supply for the system;

- c. The supply well must be tested to confirm water quantity and quality suitability prior to site plan approval. Support must be provided for the pump test rate; which should be the maximum day rate. The rate should consider the actual use, or potential uses permitted through zoning if unknown.
- d. The parameters of water quality that will be tested will be the “subdivision suite” (known to local well testing laboratories), as well as trace metals and VOCs. Requirements are outlined in the Hydrogeological and Terrain Analysis Guidelines, City of Ottawa, March 2021. The report should also provide an assessment of adjacent land uses and concerns and determine if any other parameters need to be tested (e.g. petroleum hydrocarbons, etc.).
- e. The Hydrogeological and Terrain Analysis Report should outline potential on-site activities and risks to existing groundwater users and identify measures that should be implemented to protect the aquifer in the long-term.
- f. Bollards, or other means of preventing vehicle access, will need to be provided between areas with vehicle access and the existing or proposed well(s).
- g. Results from nearby wells indicate a potential for exceedances for hardness, colour, total dissolved solids (TDS), turbidity, chloride, iron, and sodium.
- h. A Septic System Impact Assessment must be completed as part of the Hydrogeological and Terrain Analysis Report, as per the City’s Hydrogeological and Terrain Analysis Report Guidelines and MECP Guideline D-5-4, please refer to the HGTA for the predictive assessment for commercial/industrial developments (not residential developments).
 - i. Note that compact gravel will be considered impermeable in the septic impact assessment unless accompanied by field testing to confirm infiltration rates.
 - ii. Since this application is a site plan (not lot creation or zoning) septic treatment (i.e. tertiary treatment with nitrate dilution) may be considered as part of the septic impact assessment calculations. A system certified though NSF or BNQ should be recommended.
- i. If the expected sewage daily design flow is 10,000 L/d or less, the septic permit from the Ottawa Septic System Office must be issued prior to Site Plan Approval being granted.

- j. If the sewage design flow from sewage systems exceeds 10,000 L/d, a Reasonable Use Assessment must accompany the application to the City. Sewage systems with design flows exceeding 10,000 L/d require the issuance of an Environmental Compliance Approval (ECA) from the MECP prior to Site Plan Approval being granted.
- k. Bollards, or other means of preventing vehicle access, will need to be provided between areas with vehicle access and the proposed septic system(s).
- l. Technical consultation with the hydrogeological report reviewer is encouraged, please contact the City hydrogeologist, Obai Mohammed and copy the project manager listed below to schedule a technical consultation.

31. Noise and Vibration

- a. A **Noise Control Study** is required with the Site Plan Control Application. Noise studies are required for new noise sensitive land uses in proximity to surface transportation (road and rail). The site is within the influence area of a Protected Transportation Corridor (identified on Schedule C2 of the Official Plan) for which the noise impacts must be contemplated. A Noise Feasibility Study is required for development proposals within 250 meters of a secondary main railway line or within 500 meters of a principal main railway line.
 - i. The Ministry of Ontario's NPC-300 Environmental Noise Guideline, for which the City's ENCG were based, defines a noise sensitive land use as a property of a person that accommodates a building used for a noise sensitive commercial purpose. The definition goes on to say that from a land use planning perspective, a noise sensitive land use may be comprised of spaces that are noise sensitive and spaces that are not noise sensitive. The outdoor living area (OLA) associated with a noise sensitive land use is considered a noise sensitive space.
 - ii. The City's Environmental Noise Control Guidelines identify that noise sensitive land uses includes other land uses that may contain outdoor and/or outdoor areas/spaces where an intruding noise may create an adverse effect, which appears to be the case for the proposal.
- b. The City will require a vibration study if there is proposed development within 75 metres of the railway right of way, based on Official Plan section 10.2.1.

- c. The owner of the rail corridor will be able to provide scoping for the future works in the rail corridor which will guide the classification as principal or secondary main rail line in terms of the preparation of the noise feasibility study.

32. Rail Safety

- a. A **Rail Proximity Study** will be required with the application to address rail safety, implement risk mitigation best practices, and to inform any development setbacks required based on proximity to the rail corridor. The Official Plan notes, in section 10.2.1, that land adjacent to all Protected Transportation Corridors and facilities shown on Schedule C2 must follow rail safety and risk mitigation best practices to determine appropriate development setbacks. The FCM-RAC Guidelines for New Development or its successor shall apply in this case.
 - i. One of the elements of the report will be to contemplate the use of safety barriers to reduce the risks associated with railway incidents by intercepting or deflecting derailed cars in order to reduce or eliminate potential loss of life and damage to property. The standard safety barrier is an earthen berm, which is intended to absorb the energy of derailed cars, slowing them down and limiting the distance they travel outside of the railway right-of-way. The berm works by intercepting the movement of a derailed car. As the car travels into the berm, it is pulled down by gravity, causing the car to begin to dig into the earth, and pulling it into the intervening earthen mass, slowing it down, and eventually bringing it to a stop.

33. An MECP Environmental Compliance Approval would be required for the proposed stormwater management facilities, LID works, or sewage works if the exemption requirements of O.Reg. 525/98 are not met. It appears based on the proposal that an ECA would be required given the industrial use. Please contact the Ministry of the Environment, Conservation and Parks, Ottawa District Office to arrange a pre-submission consultation.

- a. Please note that the process for ECAs is undergoing changes and may be different upon time of submission. Currently, once the development application has been submitted, a request can be made to the City to consider a Transfer of Review (ToR) ECA for SWM works (ponds, ditches, culverts, etc.) for private property, instead of a direct submission ECA. This is subject to approval by the City and MECP. Note that the ECA requirements are currently in transition towards the linear ECA process and more details may become available depending on application submission timeline. It is

recommended to check with the City when the development application is submitted to confirm the ECA process at that time.

34. Phase One Environmental Site Assessment

- a. A **Phase One Environmental Site Assessment (ESA)**, and possibly Phase Two ESA as deemed required by the Phase 1 ESA, is required for the proposed Site Plan Control application. This mandatory report serves to ensure that development only takes place on sites where the environmental conditions are suitable for the proposed use in accordance with provincial legislation and regulations. The City's Historic Land Use Inventory identifies that there is a potentially contaminating use of a Motor Vehicle Repair Shop, repair and service at 5949 Ottawa which should be contemplated by the environmental consultant.

35. Construction constraints

- a. More detailed constraints may be provided in the Phase 2 Pre-Application Consultation Meeting as the conceptual drawing has provided more detail.

36. Background studies

- a. Village of Richmond Master Servicing Study
- b. Village of Richmond Environmental Management Plan
- c. Village of Richmond Community Design Plan

37. Severance

- a. In terms of the requirements for a future proposed severance, there will be engineering conditions placed on the application. It is recommended that the applicant reach out to the Development Review All Wards group who now handles commenting on Committee of Adjustment applications.
 - i. It is anticipated that a condition will be for a Hydrogeological and Terrain Analysis report to demonstrate the adequacy of the groundwater and area/septic dilution to accommodate the development.
 - ii. It is anticipated that a condition for independent water, sanitary and storm servicing will be place. Each lot should have their own independent systems which do not cross the property line.

- iii. It is anticipated that Noise Studies, Phase 1 ESA, and Rail Safety reports would be required as conditions of the severance.

Feel free to contact Travis Smith, Infrastructure Project Manager, for follow-up questions.

Transportation

Comments:

38. A TIA is not required.

39. ROW Protection:

- a. Ensure that the development proposal complies with the Right-of-Way protection requirements of the Official Plan's Schedule C16.
- b. See [Schedule C16 of the Official Plan](#).
- c. Any requests for exceptions to ROW protection requirements must be discussed with Transportation Planning and concurrence provided by Transportation Planning management.
- d. ROW must be unincumbered and conveyed at no cost to the City. Note that conveyance of the ROW/corner triangle will be required prior to registration of the SP agreement. Additional information on the conveyance process can be provided upon request.

40. Clear throat requirement is 8m. Ensure this length is provided. The clear throat length is measured from the ends of the driveway curb return radii at the roadway and the point of first conflict on-site. Note the minimum throat length provided must be maintained with the future ROW protection (as applicable).

41. Signalization of Eagleson Road and Ottawa Street is identified on the Development Charges Bylaw. Warrants have not yet been met for this intersection.

42. As the proposed site is commercial/industrial, AODA legislation applies.

- a. Ensure all crosswalks located internally on the site provide a TWSI at the depressed curb, per requirements of the Integrated Accessibility Standards Regulation under the AODA.
- b. Clearly define accessible parking stalls and ensure they meet AODA standards (include an access aisle next to the parking stall and a pedestrian curb ramp at the end of the access aisle, as required).

- c. Please consider using the City's Accessibility Design Standards, which provide a summary of AODA requirements.
<https://ottawa.ca/en/city-hall/creating-equal-inclusive-and-diverse-city/accessibility-services/accessibility-design-standards-features#accessibility-design-standards>

43. On site plan:

- a. Ensure site access meets the City's Private Approach Bylaw.
- b. Show all details of the roads abutting the site; include such items as pavement markings, accesses and/or sidewalks.
- c. Turning movement diagrams required for all accesses showing the largest vehicle to access/egress the site.
- d. Turning movement diagrams required for internal movements (loading areas, garbage).
- e. Show all curb radii measurements; ensure that all curb radii are reduced as much as possible and fall within TAC guidelines (Figure 8.5.1).
- f. Show dimensions for site elements (i.e. lane/aisle widths, access width and throat length, parking stalls, sidewalks, pedestrian pathways, etc.).

Feel free to contact Josiane Gervais, Transportation Project Manager, for follow-up questions.

Environment

Comments:

- 44. Backs onto floodplain associated with Marlborough Creek. The village of Richmond EMP (2010) indicates that the floodplain on this property contains a "local woodlot". Since the site plan indicates that the woodlot in the floodplain will be retained, we have no significant natural heritage concerns with the proposal.
- 45. There is potential for species at risk on the site, particularly in the wooded portion of the site this can be addressed through a Tree Conservation Report since the most likely concerns are related to forest dwelling species like butternut trees, black ash, and bats (addressed through timing windows). Accordingly we recommend a Tree Conservation Report be prepared to address the potential presences of these species within 25 m of

the proposed site alteration. The TCR will also need to address the concerns of our Planning Foresters as well as the information above.

46. Bird-safe design - Please review and incorporate bird safe design elements. Some of the risk factors include glass and related design traps such as corner glass and fly-through conditions, ventilation grates and open pipes, landscaping, light pollution. More guidance and solutions are available in the guidelines which can be found here:
https://documents.ottawa.ca/sites/documents/files/birdsafedesign_guidelines_en.pdf

Feel free to contact Matthew Hayley, Environmental Planner, for follow-up questions.

Forestry

Comments:

47. A tree permit will not be required as part of this application, as there are no City Trees within the right-of-way fronting the site, and impacts to private trees in the rural area are not regulated by the tree by-law.
48. The following Tree Conservation Report (TCR) guidelines have been adapted from the Schedule E of the Tree Protection By-law – for more information on these requirements please contact julian.alvarez-barkham@ottawa.ca
- a. A Tree Conservation Report (TCR) must be supplied for review along with the suite of other plans/reports required by the City
 - i. An approved TCR is a requirement of Site Plan approval.
 - b. The TCR must contain 2 separate plans:
 - i. Plan/Map 1 - show existing conditions with tree cover information.
 - ii. Plan/Map 2 - show proposed development with tree cover information.
 - c. The TCR must list all trees on site, as well as off-site trees if the CRZ (critical root zone) extends into the developed area, by species, diameter, and health condition.
 - i. For ease of review, the Planning Forester suggests that all trees be numbered and referenced in an inventory table.
 - d. Please identify trees by ownership – private onsite, private on adjoining site, city owned, co-owned (trees on a property line)

- e. If trees are to be removed, the TCR must clearly show where they are, and document the reason they cannot be retained.
 - i. Compensation may be required for the removal of city owned trees.
 - f. The removal of trees on a property line will require the permission of both property owners.
 - g. All retained trees must be shown, and all retained trees within the area impacted by the development process must be protected as per City guidelines available on the Tree Protection Specification or by searching Ottawa.ca.
 - i. The location of tree protection fencing must be shown on the plan;
 - ii. Show the critical root zone of the retained trees.
 - h. The City encourages the retention of healthy trees; if possible, please seek opportunities for retention of trees that will contribute to the design/function of the site.
49. The following Landscape Plan (LP) guidelines have been adapted from Schedule E of the Tree Protection By-law – for more information on these requirements please contact julian.alvarez-barkham@ottawa.ca
- a. Please ensure any retained trees are shown on the LP.
 - b. Minimum Setbacks
 - i. Maintain 1.5m from sidewalk or MUP/cycle track or water service laterals.
 - ii. Maintain 2.5m from curb.
 - c. Coniferous species require a minimum 4.5m setback from curb, sidewalk, or MUP/cycle track/pathway.
 - d. Maintain 7.5m between large growing trees, and 4m between small growing trees. Park or open space planting should consider 10m spacing, except where otherwise approved in naturalization / afforestation areas.
 - e. Adhere to Ottawa Hydro's planting guidelines (species and setbacks) when planting around overhead primary conductors.
 - f. Tree specifications
 - i. Minimum stock size: 50mm tree caliper for deciduous, 200cm height for coniferous.
 - ii. Maximize the use of large deciduous species wherever possible to maximize future canopy coverage

- g. Tree planting on city property shall be in accordance with the City of Ottawa's Tree Planting Specification; and if possible, include watering and warranty as described in the specification.
- h. No root barriers, dead-man anchor systems, or planters are permitted.
- i. No tree stakes unless necessary (and only 1 on the prevailing winds side of the tree)
- j. Hard surface planting
 - i. If there are hard surface plantings, a planting detail must be provided.
 - ii. Curb style planter design is highly recommended.
 - iii. No grates are to be used and if guards are required, City of Ottawa standard (which can be provided) shall be used.
- k. Trees are to be planted at grade.
- l. Soil Volume - Please demonstrate as per the **Landscape Plan Terms of Reference** that the available soil volumes for new plantings will meet or exceed the following:

| Tree Type/Size | Single Tree Soil Volume (m3) | Multiple Tree Soil Volume (m3/tree) |
|----------------|------------------------------|-------------------------------------|
| Ornamental | 15 | 9 |
| Columnar | 15 | 9 |
| Small | 20 | 12 |
| Medium | 25 | 15 |
| Large | 30 | 18 |
| Conifer | 25 | 15 |

- i. It is strongly suggested that the proposed species list include a column listing the available soil volume.
- m. Sensitive Marine Clay - Please follow the City's 2017 Tree Planting in Sensitive Marine Clay guidelines.
- n. The City requests that consideration be given to planting native species wherever there is a high probability of survival to maturity.

- o. Efforts shall be made to provide as much future canopy cover as possible at a site level, through tree planting and tree retention. The Landscape Plan shall show/document that the proposed tree planting and retention will contribute to the City's overall canopy cover over time. **Please provide a projection of the future canopy cover for the site to 40 years.**

Feel free to contact Julian Alvarez-Barkham, Forester, for follow-up questions.

Parkland

Comments:

- 50. Parkland Dedication will be required in accordance with [By-law No. 2022-280](#).
- 51. The applicable parkland dedication rate for Industrial and Commercial uses is 2% of the gross land area. For Commercial and Industrial redevelopment, gross land area means the portion of the property that is impacted by the development, but not including any hazard lands or natural heritage features identified in the Official Plan, an approved Secondary Plan, or through an environmental impact study accepted by the City;
- 52. The applicant is advised that they must identify on the survey, site plan or supporting plan the portion of the property impacted by the development, for the purpose of calculating gross land area. The property appears to be impacted by floodplain. Floodplains may be excluded from the area subject to parkland dedication.
- 53. Parks & Facilities Planning is requesting payment of **Cash-in-lieu-of-Parkland** for this development. The value of the land, equivalent to the Parkland Dedication requirement, will be determined as of the day before planning approval is given for the development. A property valuation will be completed by the City prior to site plan approval at the owner's cost.
- 54. The conveyance of parkland or the payment of cash-in-lieu of parkland is required unless it can be demonstrated, that the required parkland conveyance or cash-in-lieu of parkland, or combination thereof, has been previously satisfied in accordance with the Planning Act.
- 55. The application notes a future severance of the lot. The owner is advised that if they provide CIL of parkland for the entirety of the subject property prior to severance, they should not be required to provide further parkland dedication at the time of lot creation.



Feel free to contact Anissa McAlpine, Parks Planner, for follow-up questions.

Conservation Authority

Comments:

- 56. No concerns with the proposal as no physical development is occurring within the floodplain or regulated area.

Feel free to contact Eric Lalande, Rideau Valley Conservation Authority, for follow-up questions.

Other

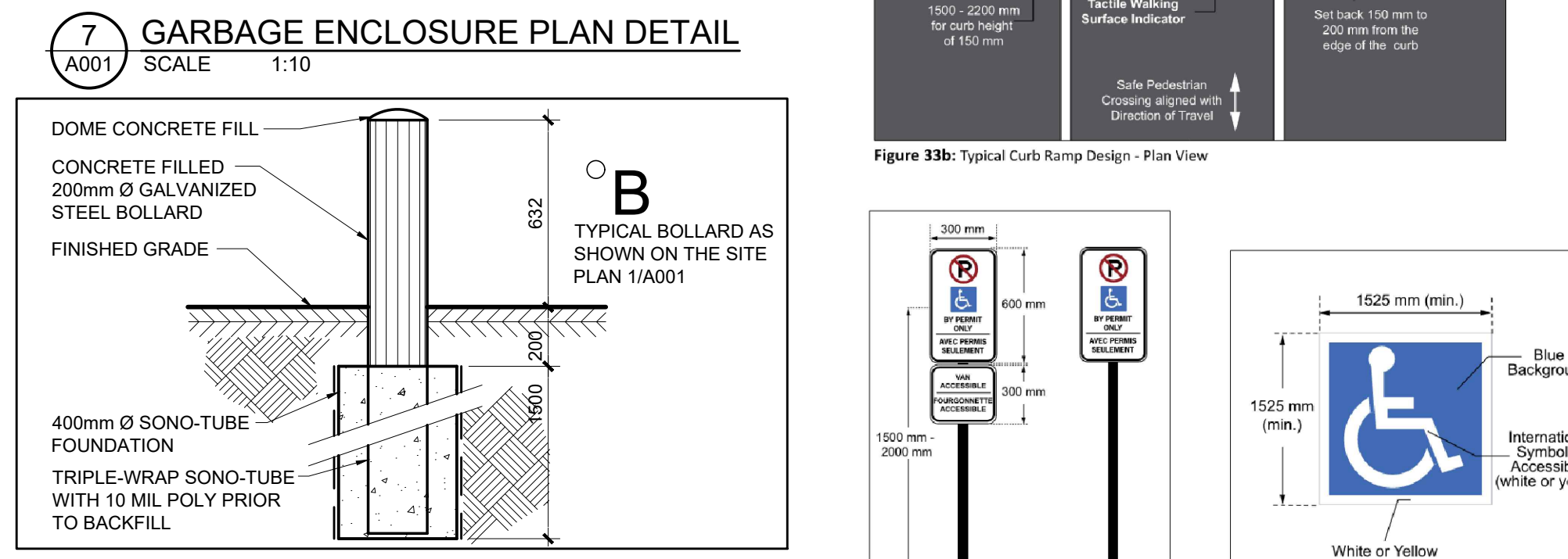
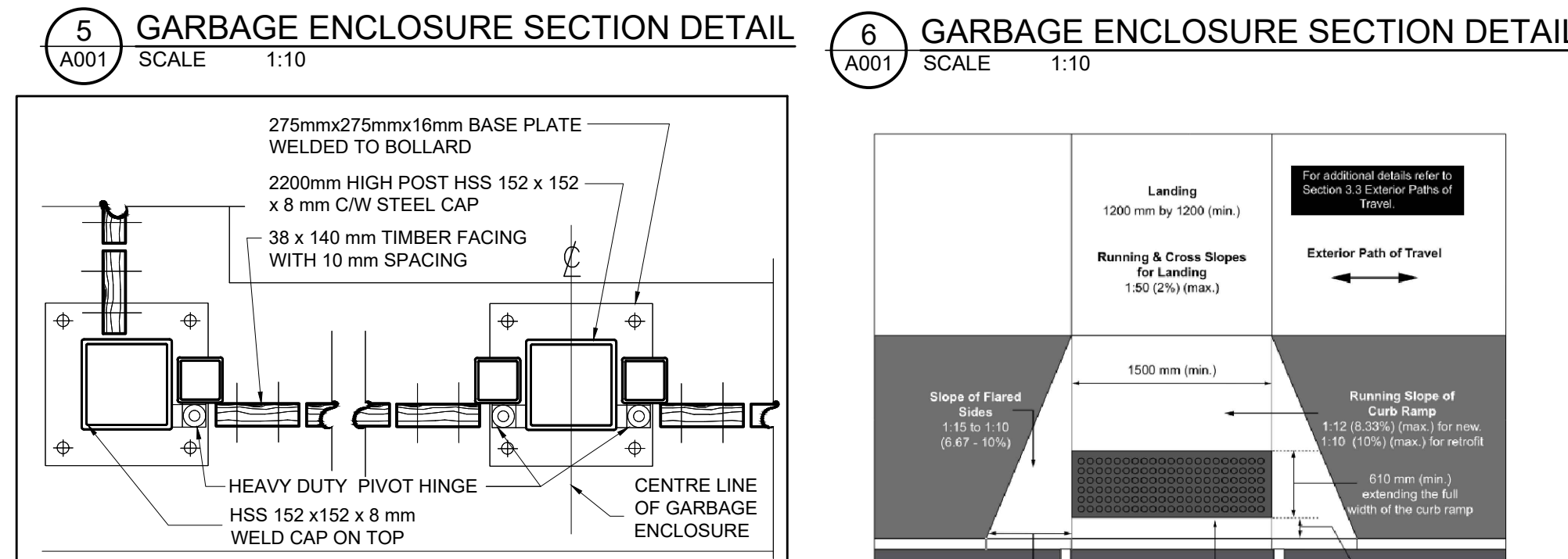
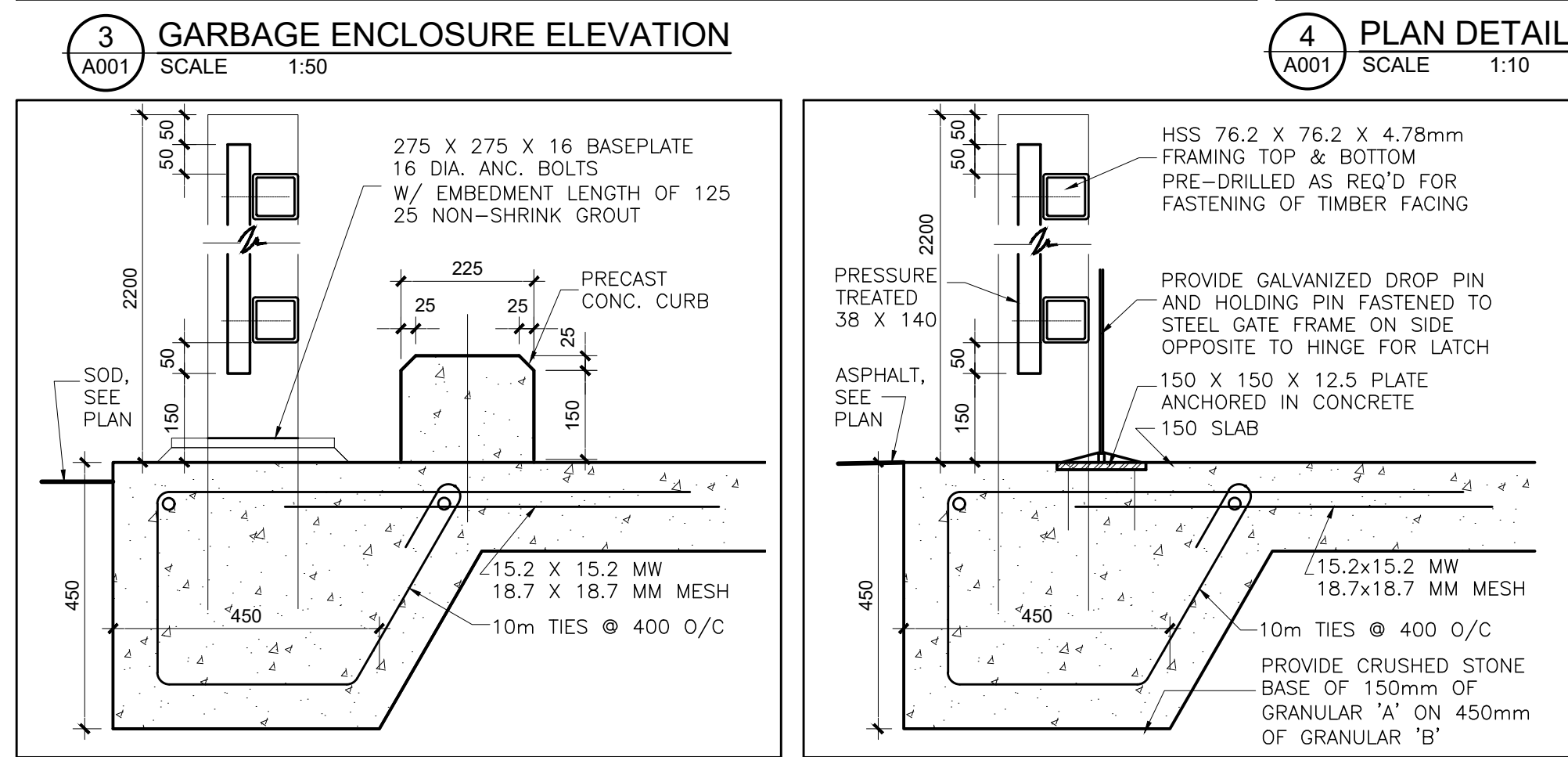
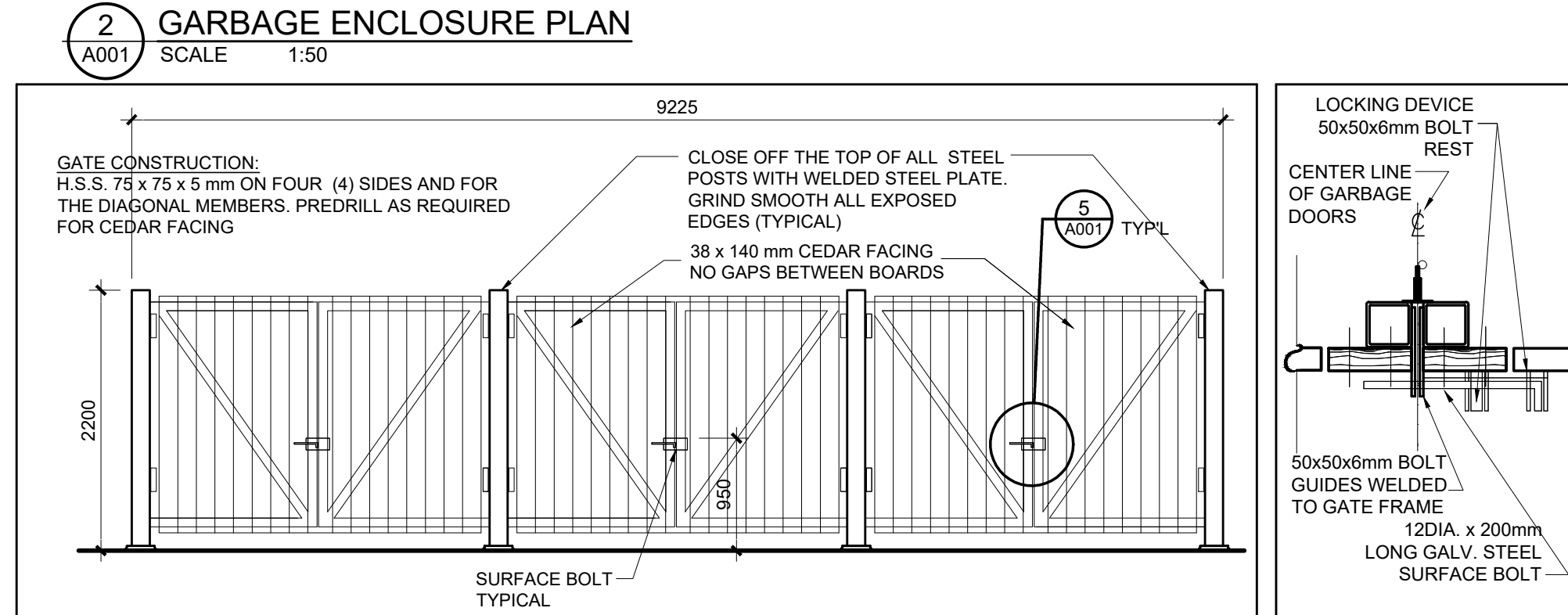
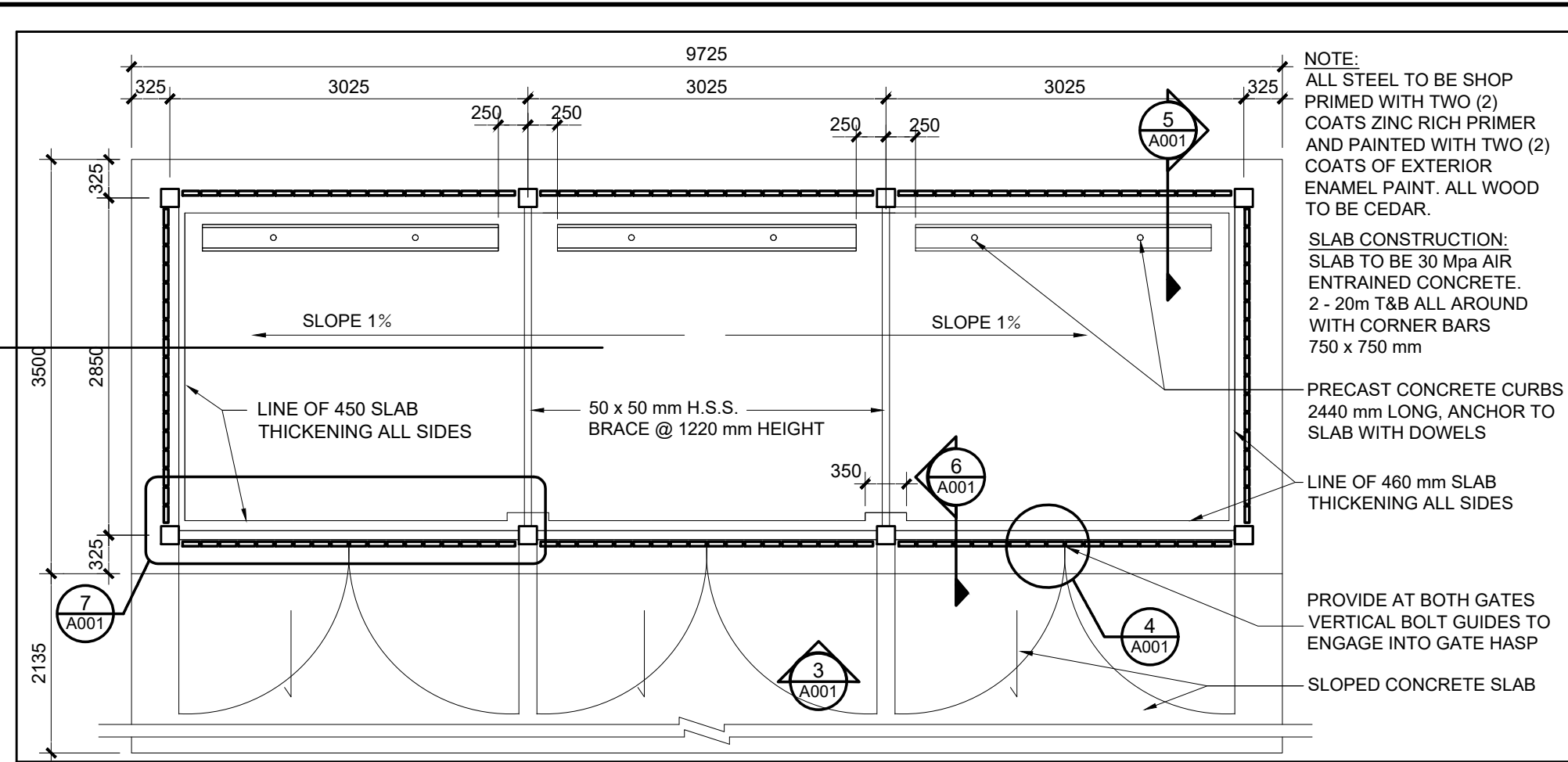
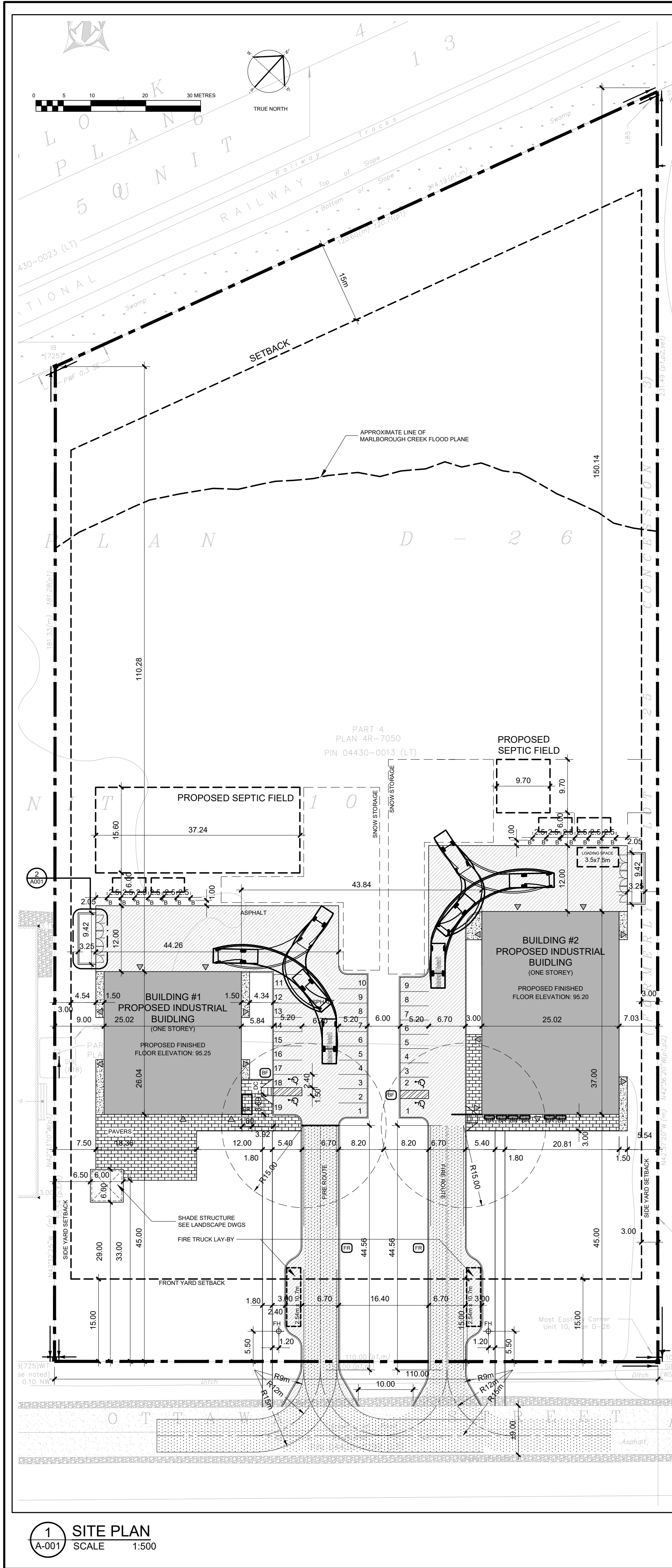
The High Performance Development Standard (HPDS) is a collection of voluntary and required standards that raise the performance of new building projects to achieve sustainable and resilient design. The HPDS was passed by Council on April 13, 2022.

- a. At this time, the HPDS is not in effect and Council has referred the 2023 HPDS Update Report back to staff with direction to bring forward an updated report to Committee with recommendations for revised phasing timelines, resource requirements and associated amendments to the Site Plan Control By-law by no later than Q1 2024.
- b. Please refer to the HPDS information attached and ottawa.ca/HPDS for more information.

Should there be any questions, please do not hesitate to contact myself or the contact identified for the above areas / disciplines.

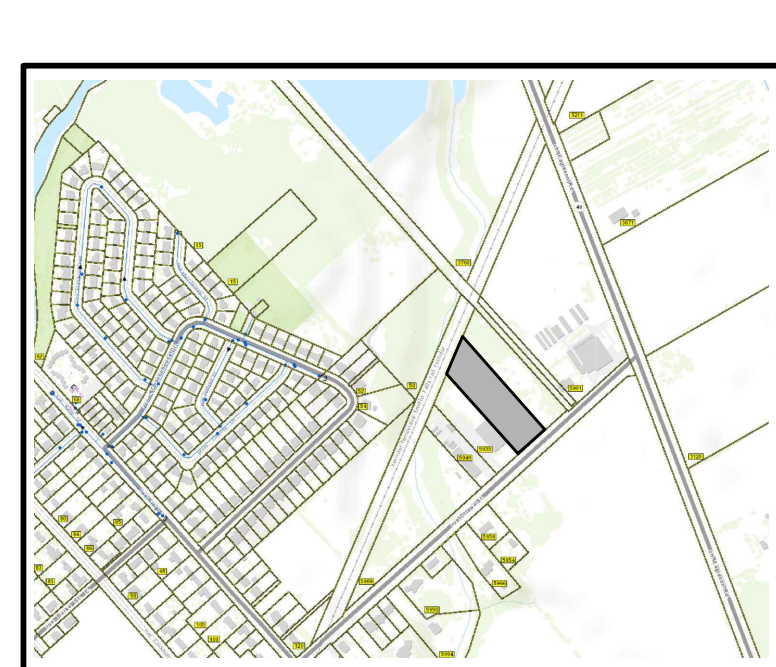
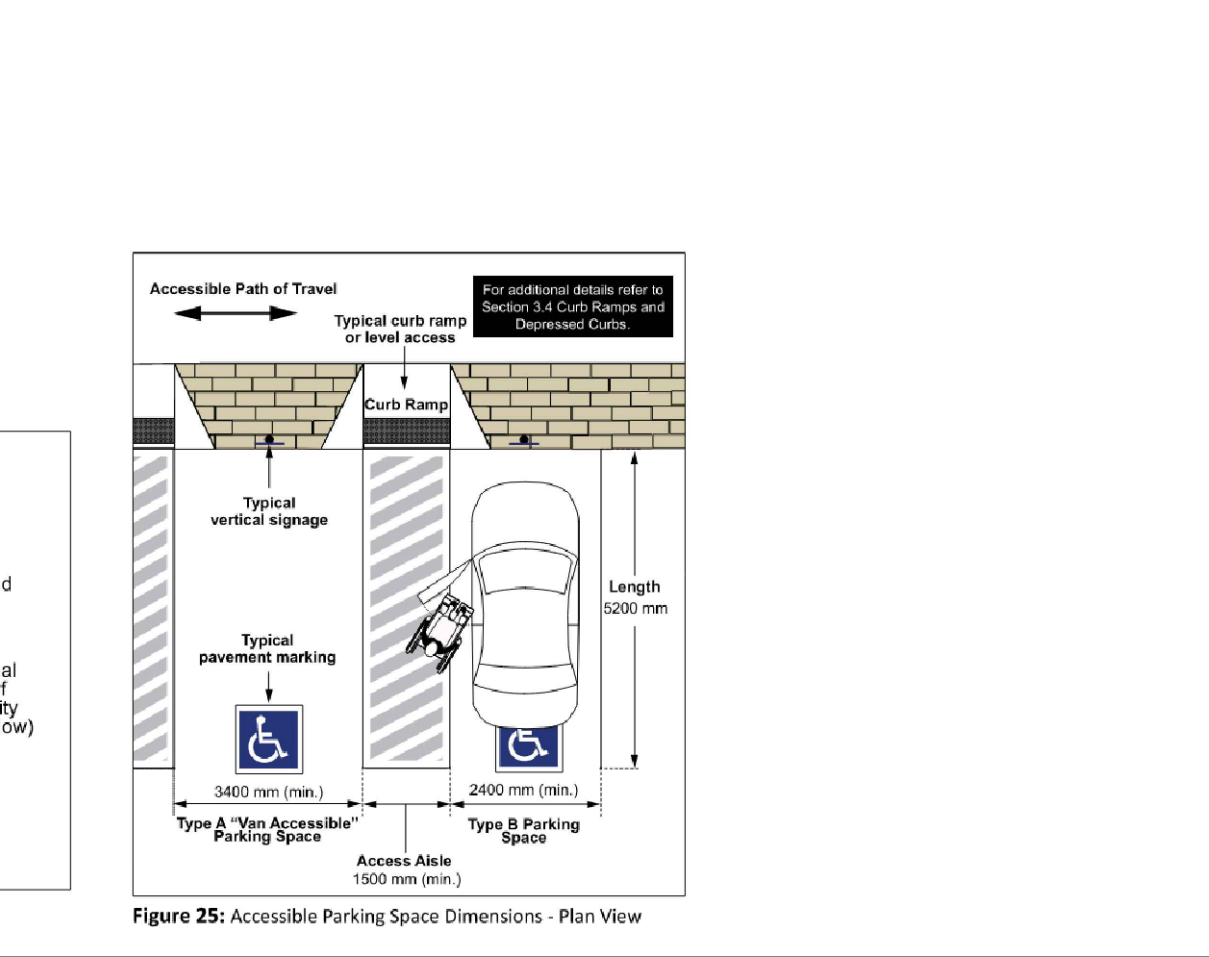
Yours Truly,
Stephan Kukkonen

c.c. Smith Travis - Infrastructure Project Manager
Josiane Gervais - Transportation Project Manager
Lisa Stern – Planner III (Urban Design)
Matthew Hayley – Environmental Planner
Julian Alvarez-Barkham – Planning Forester
Anissa McAlpine – Parks Planner
Eric Lalande – Rideau Valley Conservation Authority



| ZONING INFORMATION | | |
|--|--|--|
| NOTE: ALL ZONING DEFINITIONS AND REQUIREMENTS AS PER CITY OF OTTAWA ZONING BY-LAW 2008-250 | | |
| ZONING MECHANISM | REQUIRED | PROVIDED |
| DEFINITION | R3 (385) RURAL GENERAL INDUSTRIAL ZONE | BUILDING #1: WAREHOUSE, RETAIL STORE, BAR (25%) BUILDING #2: WAREHOUSE |
| MIN. LOT WIDTH | 30.0 m | 110.0 m |
| MIN. LOT AREA | 2,000 m ² | 22,680 m ² (± 5.6 Acres) |
| MIN. FRONT YARD SETBACK | 15.0 m | 45.0 m |
| MIN. REAR YARD SETBACK | 15.0 m | 110.0 m |
| MIN. INTERIOR SIDE YARD SETBACK | 3.0 m | 9.0 m |
| MAX. LOT COVERAGE | 35% | 2.85% |
| PARKING LANDSCAPE BUFFER | FOR A PARKING LOT CONTAINING 10-100 SPACES: ABUTTING A STREET = 3 m NOT ABUTTING A STREET = 1.5 m | ABUTTING A STREET 3 m NOT ABUTTING A STREET 3 m |
| STANDARD PARKING SPACE | 2.6m WIDTH x 5.2m LENGTH | 2.6m WIDTH x 5.2m LENGTH |
| PARALLEL PARKING SPACE | 2.6m WIDTH x 6.7m LENGTH | 2.6m WIDTH x 6.7m LENGTH |
| ACCESSIBLE PARKING SPACE | 3.4x5.2m (A); 2.4x5.2m(B) | 3.4x5.2m (A); 2.4x5.2m(B) |
| PARKING REQUIREMENTS | BUILDING#1: LIGHT INDUSTRIAL USE (N49): 0.8 PER 100 m ² OF GFA (3.45 REQUIRED) RETAIL STORE (N79): 3.4 PER 100m ² OF GFA (2.75 REQUIRED) BAR (N15): 6 PER 100m ² OF GFA (6.48 REQUIRED) TOTAL REQUIRED: 12.725 BUILDING#2: LIGHT INDUSTRIAL USE (N49): 0.8 PER 100 m ² OF GFA (3.45 REQUIRED) RETAIL STORE (N79): 3.4 PER 100m ² OF GFA (2.75 REQUIRED) BAR (N15): 6 PER 100m ² OF GFA (6.48 REQUIRED) TOTAL REQUIRED: 12.725 | BUILDING#1: 19 PARKING SPACES BUILDING#2: 9 PARKING SPACES |
| BARRIER FREE ACCESSIBLE | AS PER CITY OF OTTAWA ACCESSIBILITY DESIGN STANDARDS, PARAGRAPH 3.1.2, TABLE 3 1 TYPE 'A', 1 TYPE 'B' | BUILDING#1: 2 ACCESSIBLE PARKING SPACES (1xTYPE 'A' + 1xTYPE 'B') BUILDING#2: 2 ACCESSIBLE PARKING SPACES (1xTYPE 'A' + 1xTYPE 'B') |
| LOADING SPACES | GFA 350-999m ² - 0 required | 0 PROVIDED |
| BICYCLE PARKING RATE | BUILDING#1: LIGHT INDUSTRIAL USE: 1 PER 1,000 m ² OF GFA (0.4365 REQUIRED) RETAIL STORE: 1 PER 250 m ² OF GFA (0.32 REQUIRED) BAR: 1 PER 1,500 m ² OF GFA (0.072) TOTAL REQUIRED: 0.8285 BUILDING#2: LIGHT INDUSTRIAL USE: 1 PER 1,000 m ² OF GFA (1.042 REQUIRED) | 0 PROVIDED 6 BICYCLE SPACES 6 BICYCLE SPACES |

| SYMBOL LEGEND: | | |
|----------------------|---|--|
| ▲ ▼ | BLDG ENTRANCE/EXIT | |
| △ | FIRE DEPARTMENT CON | |
| ⊙ | NEW FIRE HYDRANT | |
| ○ | WATER METER | |
| — | NEW DEPRESSED CURB | |
| — | NEW CURB | |
| — | PROPERTY LINE | |
| — | NEW CHAIN LINK FENCE | |
| ○ | BOLLARD | |
| BR | BIKE RACKS | |
| SIGNAGE LEGEND: | | |
| BF | BF PARKING | |
| FR | FIRE ROUTE | |
| FR | FIRE ROUTE (AS PER OBC 3.2.5): | |
| | 6m WIDE | |
| | 12m CENTRE LINE RADIUS | |
| | 3m CLEAR OF ANY OBSTRUCTIONS AND/OR BUILDINGS | |
| | 15m TO FRONT ENTRANCE | |
| | 90m MAX TO TURN AROUND FACILITIES | |
| GROUND COVER LEGEND: | | |
| GRASS | CONCRETE | |
| ASPHALT | PAVERS | |



OWNER:
99117756 CANADA INC. c/o JACK GULAS
411 LEGGET DRIVE, SUITE 710, OTTAWA, ONTARIO, K2K 3C9

| | | |
|-----|------------------------------|---------|
| 3 | ISSUED FOR SPA | 29JUL25 |
| 2 | ISSUED FOR SPA | 15MAY25 |
| 1 | ISSUED FOR SITE PLAN CONTROL | 07OCT24 |
| no. | revision | date |

N45 ARCHITECTURE INC.
71 Bank Street, 7th floor - Ottawa, Ontario, K1P 5N2
tel. 613.224.0095 fax 613.224.9811

project
FOXRUN RICHMOND
5923 OTTAWA STREET
OTTAWA, ON
project north
seal
ONTARIO ASSOCIATION OF ARCHITECTS
VLADIMIR POPOVIC
LICENCE 5918

| drawing title | |
|---|-------------------------|
| SITE PLAN | |
| scale AS NOTED | drawn by NF |
| date JUNE 2022 | checked by VP |
| project number 24-826 | drawing number A-001 |
| CONTRACTOR TO VERIFY ALL DIMENSIONS AND NOTIFY THE ARCHITECT OF ANY DISCREPANCIES BEFORE WORK COMMENCES. DO NOT SCALE DRAWINGS. | |
| revision - | |

APPENDIX C WATERMAIN CALCULATIONS

000-25-0415 - 5923 Ottawa Street - Water Demands - Phase 1

| | |
|-------------------|--------------------|
| Project: | 5923 Ottawa Street |
| Project No.: | 000-25-0415 |
| Designed By: | FV |
| Checked By: | AG |
| Date: | September 10, 2025 |
| Development Area: | 0.48 gross ha |

| | |
|---------------------------------|--------|
| Commercial | 190 m2 |
| Industrial - Light (Distillery) | 432 m2 |

AVERAGE DAILY DEMAND

| DEMAND TYPE | AMOUNT | UNITS |
|-------------------------------|---------------------------------------|---------------------------|
| Residential | 280 | L/c/d |
| Industrial - Light | 35,000 | L/gross ha/d |
| Industrial - Heavy | 55,000 | L/gross ha/d |
| Shopping Centres | 2,500 | L/(1000m ² /d) |
| Hospital | 900 | L/(bed/day) |
| Schools | 70 | L/(Student/d) |
| Trailer Park with no Hook-Ups | 340 | L/(space/d) |
| Trailer Park with Hook-Ups | 800 | L/(space/d) |
| Campgrounds | 225 | L/(campsite/d) |
| Mobile Home Parks | 1,000 | L/(Space/d) |
| Motels | 150 | L/(bed-space/d) |
| Hotels | 225 | L/(bed-space/d) |
| Tourist Commercial | 28,000 | L/gross ha/d |
| Other Commercial | 28,000 | L/gross ha/d |
| AVERAGE DAILY DEMAND | Residential | 0.00 L/s |
| | Commercial/ Industrial/ Institutional | 0.02 L/s |

MAXIMUM DAILY DEMAND

| DEMAND TYPE | AMOUNT | UNITS |
|----------------------|---------------------------------------|--------------|
| Residential | 9.5 x avg. day | L/c/d |
| Industrial | 1.5 x avg. day | L/gross ha/d |
| Commercial | 1.5 x avg. day | L/gross ha/d |
| Institutional | 1.5 x avg. day | L/gross ha/d |
| MAXIMUM DAILY DEMAND | Residential | 0.00 L/s |
| | Commercial/ Industrial/ Institutional | 0.04 L/s |

MAXIMUM HOUR DEMAND

| DEMAND TYPE | AMOUNT | UNITS |
|---------------------|---------------------------------------|--------------|
| Residential | 14.3 x avg. day | L/c/d |
| Industrial | 1.8 x max. day | L/gross ha/d |
| Commercial | 1.8 x max. day | L/gross ha/d |
| Institutional | 1.8 x max. day | L/gross ha/d |
| MAXIMUM HOUR DEMAND | Residential | 0.00 L/s |
| | Commercial/ Industrial/ Institutional | 0.06 L/s |

WATER DEMAND DESIGN FLOWS PER UNIT COUNT
CITY OF OTTAWA - WATER DISTRIBUTION GUIDELINES, JULY 2010

| | | |
|----------------------|------|-----|
| AVERAGE DAILY DEMAND | 0.02 | L/s |
| MAXIMUM DAILY DEMAND | 0.04 | L/s |
| MAXIMUM HOUR DEMAND | 0.06 | L/s |

000-25-0415 - 5923 Ottawa Street - Water Demands - Phase 2

| | |
|-------------------|--------------------|
| Project: | 5923 Ottawa Street |
| Project No.: | 000-25-0415 |
| Designed By: | FV |
| Checked By: | AG |
| Date: | September 10, 2025 |
| Development Area: | 0.45 gross ha |

Industrial - Light (Brewery)

926 m2

AVERAGE DAILY DEMAND

| DEMAND TYPE | AMOUNT | UNITS |
|-------------------------------|---------------------------------------|---------------------------|
| Residential | 280 | L/c/d |
| Industrial - Light | 35,000 | L/gross ha/d |
| Industrial - Heavy | 55,000 | L/gross ha/d |
| Shopping Centres | 2,500 | L/(1000m ² /d) |
| Hospital | 900 | L/(bed/day) |
| Schools | 70 | L/(Student/d) |
| Trailer Park with no Hook-Ups | 340 | L/(space/d) |
| Trailer Park with Hook-Ups | 800 | L/(space/d) |
| Campgrounds | 225 | L/(campsite/d) |
| Mobile Home Parks | 1,000 | L/(Space/d) |
| Motels | 150 | L/(bed-space/d) |
| Hotels | 225 | L/(bed-space/d) |
| Tourist Commercial | 28,000 | L/gross ha/d |
| Other Commercial | 28,000 | L/gross ha/d |
| AVERAGE DAILY DEMAND | Residential | 0.00 L/s |
| | Commercial/ Industrial/ Institutional | 0.04 L/s |

MAXIMUM DAILY DEMAND

| DEMAND TYPE | AMOUNT | UNITS |
|----------------------|---------------------------------------|--------------|
| Residential | 9.5 x avg. day | L/c/d |
| Industrial | 1.5 x avg. day | L/gross ha/d |
| Commercial | 1.5 x avg. day | L/gross ha/d |
| Institutional | 1.5 x avg. day | L/gross ha/d |
| MAXIMUM DAILY DEMAND | Residential | 0.00 L/s |
| | Commercial/ Industrial/ Institutional | 0.06 L/s |

MAXIMUM HOUR DEMAND

| DEMAND TYPE | AMOUNT | UNITS |
|---------------------|---------------------------------------|--------------|
| Residential | 14.3 x avg. day | L/c/d |
| Industrial | 1.8 x max. day | L/gross ha/d |
| Commercial | 1.8 x max. day | L/gross ha/d |
| Institutional | 1.8 x max. day | L/gross ha/d |
| MAXIMUM HOUR DEMAND | Residential | 0.00 L/s |
| | Commercial/ Industrial/ Institutional | 0.10 L/s |

WATER DEMAND DESIGN FLOWS PER UNIT COUNT

CITY OF OTTAWA - WATER DISTRIBUTION GUIDELINES, JULY 2010

| | | |
|----------------------|------|-----|
| AVERAGE DAILY DEMAND | 0.04 | L/s |
| MAXIMUM DAILY DEMAND | 0.06 | L/s |
| MAXIMUM HOUR DEMAND | 0.10 | L/s |

4

3

2

1

D

D

C

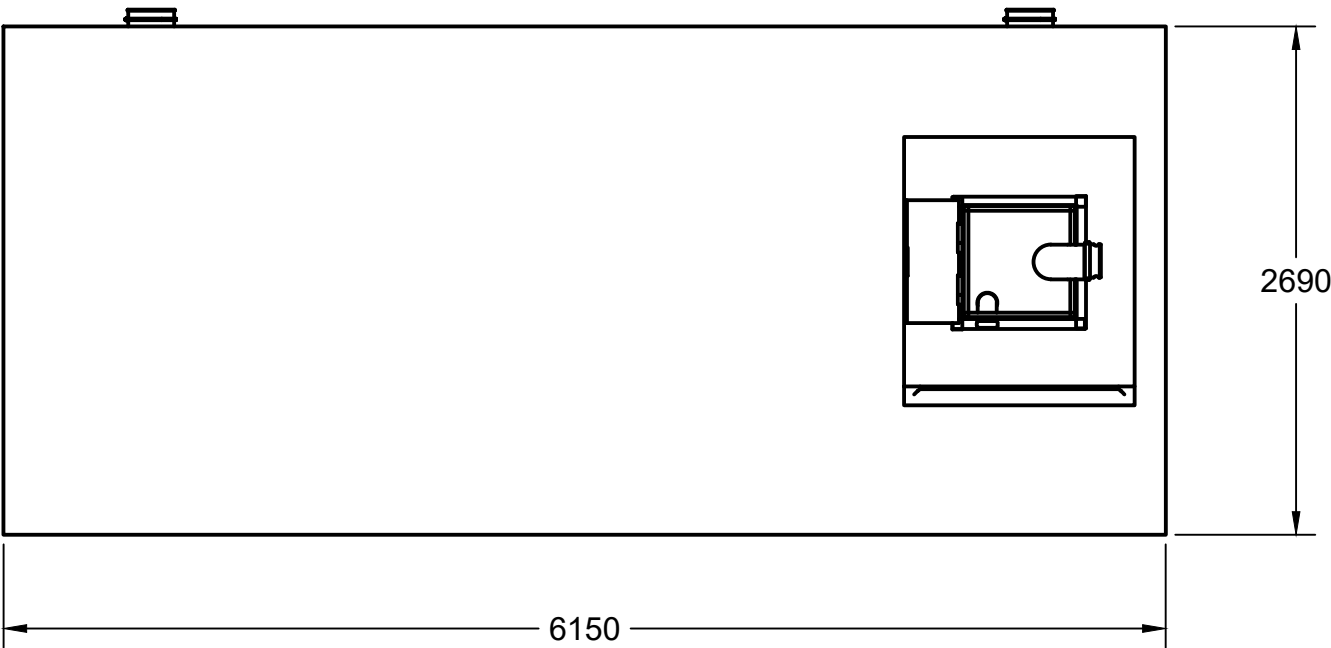
C

B

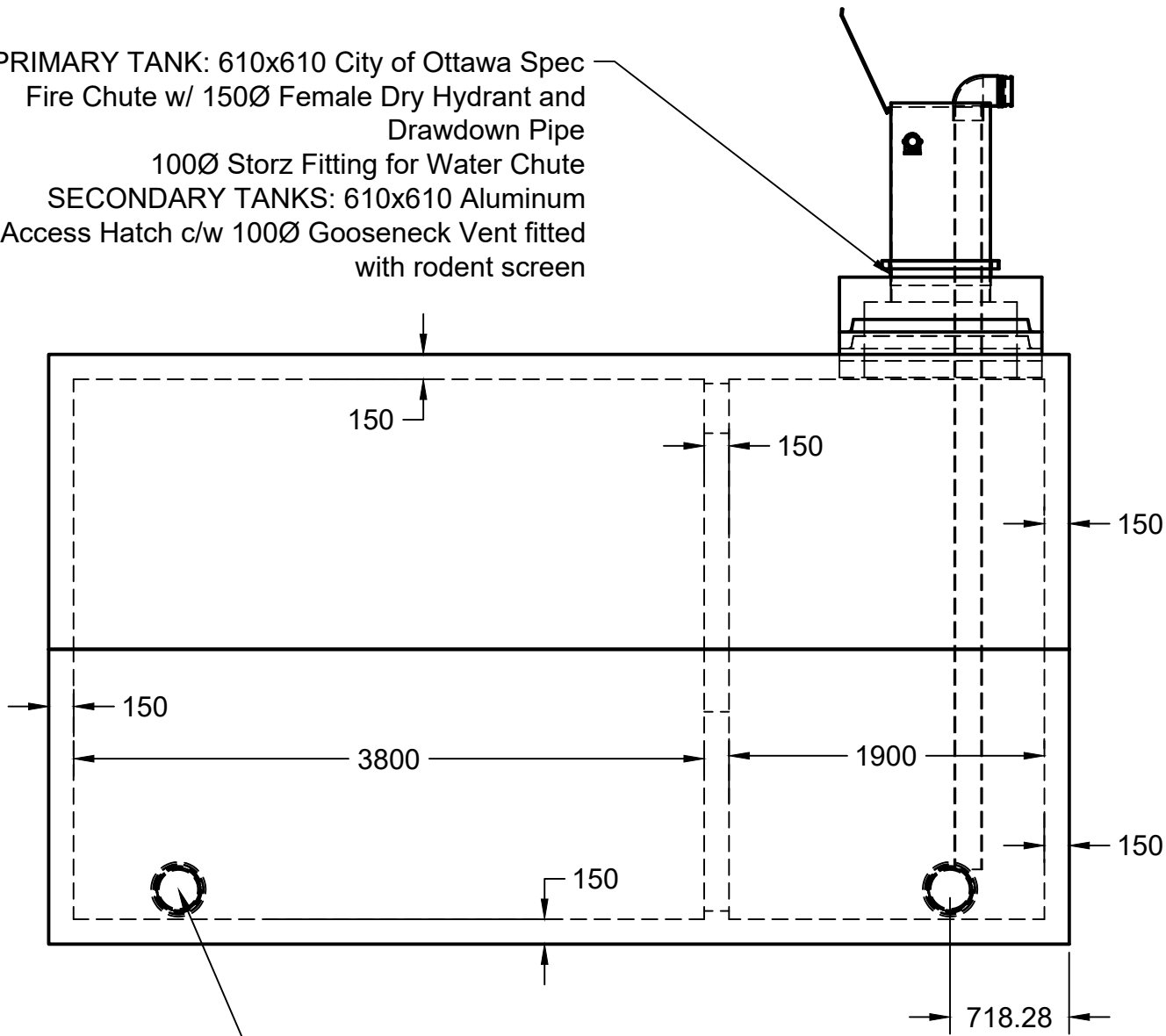
B

A

A



PRIMARY TANK: 610x610 City of Ottawa Spec Fire Chute w/ 150Ø Female Dry Hydrant and Drawdown Pipe
100Ø Storz Fitting for Water Chute
SECONDARY TANKS: 610x610 Aluminum Access Hatch c/w 100Ø Gooseneck Vent fitted with rodent screen



2- 200Ø Interconnection Bootseals For Multiple Tank Cluster Systems

TOTAL VOLUME: 45000L

CONCRETE: 35MPa WITH 5-8% AIR ENTRAINMENT
NON SULPHATE RESISTANT

REINFORCING: GRADE 400W CONFORMING TO CSA G30.18
15M @ 200mm ON CENTRE EACH WAY
ADDITIONAL 15M AROUND PERIMETER AT SEAM BETWEEN

SECTIONS 15M x900mm ON DIAGONAL AT EACH CORNER OF LID OPENING

WEIGHT: TOP SECTION 19000KGS
BOTTOM SECTION 19000KGS
TOTAL 38000KGS

MAXIMUM BURIAL DEPTH: 1200MM OF GROUND COVER IN AREA OF NON-VEHICULAR TRAFFIC

WATER TIGHTNESS: 2X ROWS CON-SEAL CS-102 MASTIC SEALANT BETWEEN SECTIONS. SEALANT APPLIED ONSITE BY BOYD BROS CONCRETE ACCORDING TO MANUFACTURER'S RECOMMENDED METHOD

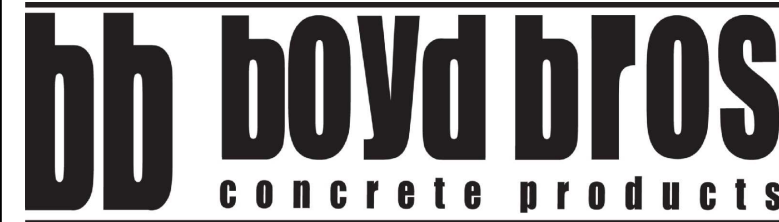
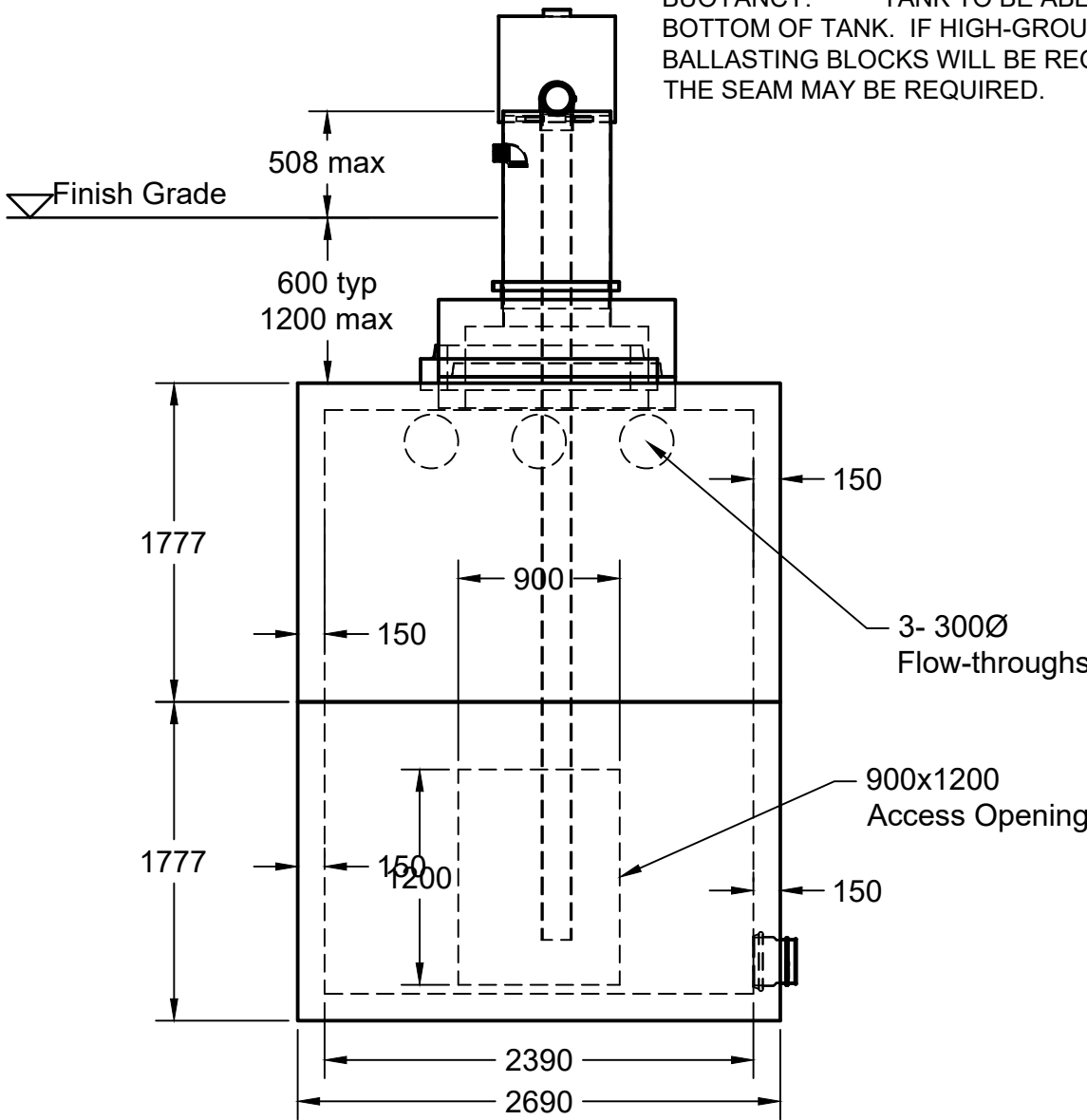
PIPE/WALL CONNECTIONS: 200mmØ Flexible Rubber Bootseal for PVC Supply Line

ACCESS OPENINGS:
PRIMARY TANK: 610X610 CITY OF OTTAWA SPEC FIRE CHUTE FOR FIRETRUCK CONNECTION
SECONDARY ACCESS (OPTIONAL) :1200x1300 CAST-IN RISER FLANGE WITH 610X610 DRIP PROOF ALUMINUM ACCESS HATCH
900X1200 OPENING IN DIVIDER WALL FOR ACCESS TO BOTH CHAMBERS FROM ONE ACCESS POINT

OPTIONAL STAINLESS STEEL BOLT-ON LADDER OPTIONAL

TANK DESIGN CONFORMS TO CSA STANDARD B66-15 WITH A NON-TRAFFIC LOAD ON TOP, AND WITH HEAVY TRUCK LOADING DIRECTLY ADJACENT TO TANK TO ACCOMMODATE FIRE TRUCK TO BE WITHIN 1M OF WATER DRAW-DOWN CHUTE, AS PER FIRE DEPT.

BUOYANCY: TANK TO BE ABLE TO WITHSTAND GROUNDWATER UP 2.0M FROM BOTTOM OF TANK. IF HIGH-GROUNDWATER LEVEL IS IN EXCESS OF THIS, ADDITIONAL BALLASTING BLOCKS WILL BE REQUIRED. ADDITIONAL WATERPROOFING MEASURES AT THE SEAM MAY BE REQUIRED.



5450 Cuddy St Osgoode, ON K0A 2W0
tel: (613) 826.2318 fax: (613) 826.3679
toll free: 888.846.6664
website: www.boydbrosconcrete.ca
email: info@boydbrosconcrete.ca

| | | |
|----------------------------------|-----------------|-----------|
| PROJECT | | |
| Boyd Bros Concrete | | |
| TITLE | | |
| 45000 Fire Tank | | |
| DRAWN Rob Sanna 6/19/23 APPROVED | | |
| SIZE | DWG NAME | REV |
| C | 45000 Fire Tank | 3 |
| SCALE 1:40 | WEIGHT 35000kgs | SHEET 1/1 |

4

3

2

1



August 21, 2025

Jack Gulas
Stratford Foxrun
6286 Prince of Wales Drive
North Gower, ON
K0A 2T0

EMAIL: jack@stratfordfoxrun.com
CC: josh.laginski@outlook.com

Dear Jack:

**RE: 5923 OTTAWA STREET DISTILLERY WATER STORAGE VOLUME ESTIMATE
LRI FILE 2025-04-0654**

PROJECT DESCRIPTION

The project at 5923 Ottawa Street, Ottawa, ON includes two buildings on one site to be used for a mix of industrial and assembly occupancies. Building 1 includes a distillery, mezzanine-level offices, a bar/tasting area, a retail store, and an outdoor patio. Building 2 includes a brewery, some storage space, a bottling line, and associated office space for staff of the site's operations.

The buildings are subject to the 2024 Ontario Building Code (OBC), and as such, are required to be supplied with water for firefighting purposes. The site and surrounding area are not connected to a municipal water supply for firefighting. As a result, water must be stored on site for this purpose. This letter is intended to summarize LRI's analysis of the buildings, the OBC, and OFS documentation regarding the applicable rules and regulations which help assess the required amount of water to be stored on site.

For clarity, the analysis below is based upon the design information available at this time, and is considered an order of magnitude estimate, subject to refinement when the sprinkler and fire pump systems for the buildings are designed. This detailed design is most commonly completed following building permit submission. The objective of the analysis is to explain the fire safety rationale applied to the buildings and to assist the design team and reviewers in aligning on an acceptable water volume to be stored on a general basis.





BUILDING DESCRIPTION

The subject site includes two buildings: Building 1, and Building 2. These buildings have the following characteristics based on the provided architectural drawings:

Building 1:

- One storey in building height, with mezzanine
- 8.5 m in height
- 647 m² in building area
- Sprinklered throughout
- Occupancies include:
 - Distillery
 - Offices
 - Bar/assembly
 - Retail

Building 2:

- One storey in building height, with mezzanine
- 8.5 m in height
- 926 m² in building area
- Sprinklered throughout
- Occupancies include:
 - Mashing/bottling
 - Brewery
 - Storage mezzanine
 - Offices

CODE REQUIREMENTS

In conformance with OBC 3.2.5.7 “every building shall be provided with an adequate water supply for firefighting”. As clarified by OBC Appendix A-3.2.5.7.(2) for sprinklered buildings, “water supply additional to that required by the sprinkler systems should be provided for firefighting using fire hoses in accordance with the hose stream demands and water supply durations for different hazard classifications as specified in NFPA 13, “Installation of Sprinkler Systems”.

Since the buildings are sprinklered, the water storage volume estimate, therefore, needs to provide sufficient water for the sprinklers to operate, plus necessary hose demands from fire crews.

In conformance with Technical Bulletin IWSTB-2024-05, rural fire flow calculation methods are to follow the Appendix J flow chart. Specifically, since both buildings are required to be sprinklered for insurance reasons, the highlighted green path will be followed:

Appendix J

RURAL FIRE FLOW CALCULATION PROCESS

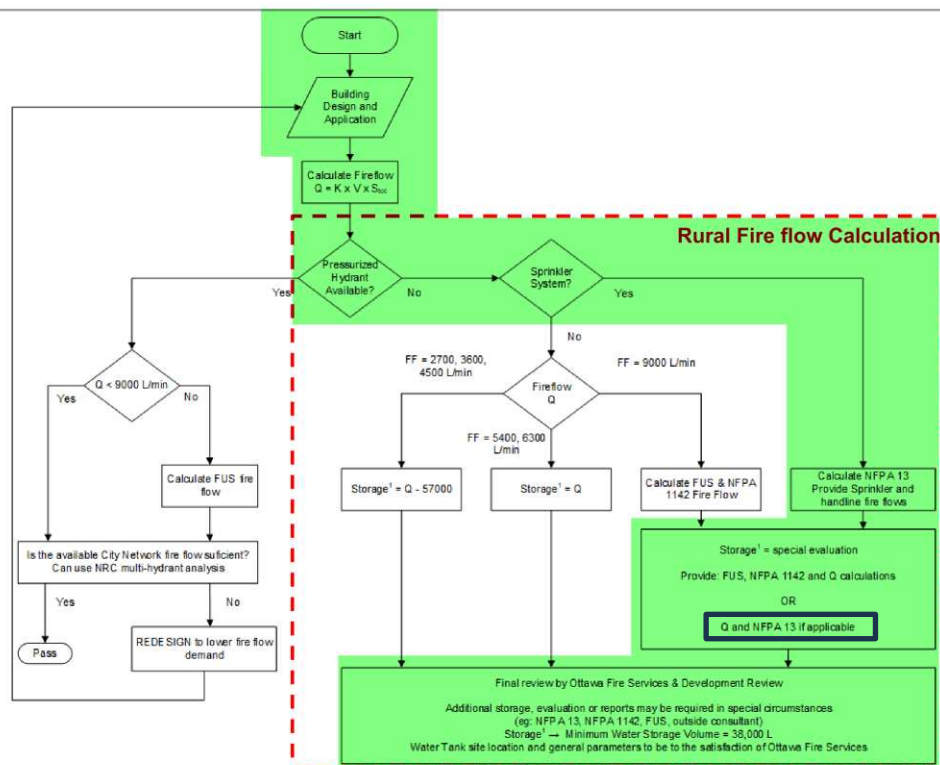


Figure J.1: Rural Fire Flow Calculation Process.

The following section outlines the methodology used for the storage volume estimates to permit OFS review.

METHODOLOGY

OBC-based Q volume analysis:

The following analysis uses the OBC-prescribed method to assess volumes based on the following inputs:

$Q = K \times V \times Stot$, where

Q = minimum supply of water in litres

K = water supply coefficient from the OBC

V = total building volume in cubic metres (m^3)

$Stot$ = total of spatial coefficient values from property line exposures on all sides.



Building 1:

| Variable | Value | Notes |
|----------|---|---|
| Q | 177,100 L, with 5,400 LPM minimum flow rate | |
| K | 23 | Conservatively assumes Group F, Division 1 occupancy despite pending alternative solution. Also assumes compliant 3.2.2. noncombustible construction. |
| V | 5,500 | Based on area and building height |
| Stot | 1.4 | 0.4 penalty assigned to southwest face with limiting distance of 9 m |

Building 2:

| Variable | Value | Notes |
|----------|---|---|
| Q | 173,949 L, with 5,400 LPM minimum flow rate | |
| K | 17 | Assumes Group F, Division 2 occupancy. Also assumes compliant 3.2.2. noncombustible construction. |
| V | 7,871 | Based on area and building height |
| Stot | 1.3 | 0.3 penalty assigned to southeast face with limiting distance of 7 m |

Based on the OBC volume Q analysis presented above, the calculated minimum supply of water required storage volumes of up to approximately 177,100 L for Building 1, or 173,949 L for Building 2. This translates to a minimum required flowrate of 5,400 LPM for both buildings at 30 minutes of supply duration.

As outlined in IWST-2024-05, for a proposed building equipped with a sprinkler system designed in accordance with NFPA 13, the OBC calculations noted above should be completed, and an additional NFPA 13 special evaluation may be carried out to determine the sprinkler water storage requirements.

NFPA 13-based volume analysis:

As the buildings will both be protected by automatic sprinkler systems, Appendix A demonstrates water volume calculations for the sprinkler systems anticipated to be designed for each building. It should be noted that these volumes are estimates, and final hydraulic designs will dictate the final volume requirements. At this time, the expected volume is to include sufficient water to supply the most demanding hydraulic area assuming one fire in one building at a time, includes for a 20% factor calculated based on water volumes discharged by the sprinklers, and considers NFPA 13-mandated hose demand calculations.



The calculations assume a sprinkler design on a “room area” method wherein different rooms must be individual enclosed fire compartments to permit the hydraulic area to be shrunk to the size of the room. This assumes that a fire separation will contain the fire during the time required for sprinkler operation.

The following tables summarize the assumed hazard classifications for the rooms. These assumptions are based off a combination of NFPA 13 compliance requirements, requirements described by the Distilled Spirits Council of the United States (DISCUS), and based on LRI’s expectation that the distillery/bar occupancy approach will require an alternative solution and correspondingly increases sprinkler density to improve suppression potential in support of that effort.

| Room | Area (ft ²) | Expected Occupancy Classification |
|------------------------|--|---|
| Building 1 | | |
| Grain Handling | 238 | Ordinary Hazard Group 2 |
| Brewing/bottling | 2,383 | Ordinary Hazard Group 2 (aligns with DISCUS recommendations) |
| Boiler Room | 277 | Ordinary Hazard Group 1 |
| Still house/still room | 965 | Extra Hazard Group 1 to support alternative solution approach |
| Office Mezzanine | 1,182 | Light Hazard |
| Kitchen | 190 | Ordinary Hazard Group 1* |
| Bar | 1,632 (hydraulic area assumed limited to 1500 ft ²) | Light Hazard* |
| Retail | 885 | Ordinary Hazard Group 2 |
| Building 2 | | |
| Mashing/brewing | 6,050 (hydraulic area assumed limited to 2000 ft ² per DISCUS) | Ordinary Hazard Group 2 |
| Bottling | 2,370 (hydraulic area assumed limited to 3000 ft ² or room area DISCUS) | Ordinary Hazard Group 2 |
| Office and admin area | 1,095 | Light Hazard |
| Storage mezzanine | 1,185 | Ordinary Hazard Group 2 |

* Note that depending on the hydraulic design, the kitchen and portions of the bar may end up being calculated together as a remote area. Their cumulative effect has been considered in Appendix A

As depicted in Appendix A, based on the NFPA 13 analysis presented above, expected storage volumes for both sprinkler and hose demand would result in required storage volumes of up to approximately 288,000 L for Building 1, or 243,000 L for Building 2. Both of these values are very high, and represent the provision of at least 100% of the NFPA 13-mandated volumes for both sprinkler operation and hose demands, for durations ranging between 30 minutes and 90 minutes (depending on NFPA 13 criteria). In order to provide a more reasonable estimate, in light of the IWSTRB documentation and OFS firefighting capacity, the following section evaluates the impact that water shuttling can have on the required storage volume.



Influence of OFS Superior Tanker Shuttle level on the required storage volume:

IWSTB 2024-05 does not explicitly clarify if or how OFS Superior Tanker Shuttle service contributes to NFPA 13-derived water storage volume analysis. As a result, engineering judgement and alignment with the AHJ is necessary.

In conformance with IWSTB 2024-05, OFS is capable of delivering 1,900 LPM within 5 minutes of arrival. As such, some credit should be permissible to account for the fire department's ability to replenish stored water volumes during a fire. As a result, the proposed storage volumes consider a reduction of 1,900 LPM for the NFPA 13 mandated duration of the fire as a reasonable value. This effectively replenishes the hose demand required for higher hazard occupancies and exceeds that required for lower hazard occupancies. The resultant conclusions presented below and in Appendix A represent an amount of water stored that exceeds the minimum required by IWSTB 2024-05, is comparable to OBC-required amounts for unsprinklered buildings, and represents the ability of the system to automatically supply the sprinklers for the NFPA 13-derived duration of the fire without extra volumes. In other words, sufficient water is expected to be stored to supply the sprinklers automatically, allow initial fire crews to have access to water for hose lines, and provide time for shuttling water to start supplementing the available stored water.

| | Building 1 | Building 2 |
|--|-------------------|-------------------|
| OBC based Q Evaluation | 177,100 L | 173,949 L |
| NFPA 13 Evaluation | 288,442 L | 242,574 L |
| NFPA 13 Evaluation w/Superior Tanker Shuttle Service Reduction | 118,117 L | 129,024 L |

CONCLUSION

This letter summarizes LRI's review of the proposed building project at 5923 Ottawa Street, and the required firefighting water volumes to be stored on site.

As the buildings are sprinklered, and in conformance with IWSTB 2024-05, a special assessment aligning with NFPA 13 has been provided. This is summarized in Appendix A.

The resultant water volume to be stored is expected to be designed to accommodate the highest required volume of either building, is to be shared between both buildings, and assumes one fire in one building at a time. This assumption is reasonable, especially given the large separation distance between both buildings on the same property.

The resultant water volume also considers the impact of OFS water shuttling on the required amount.

Based on this analysis, stored water volumes of approximately 130,000 L are recommended at this time, with final volumes being determined based on detailed sprinkler and fire pump design criteria.



Sincerely,
LRI ENGINEERING

Matthew Hopley, M.Eng., P.Eng [AB]
Branch Manager - Alberta

Reviewed by,
LRI ENGINEERING



Jin Chen, M.Eng., P.Eng.
Associate

NFPA 13 Water Volume Estimate Analysis

LRI Engineering

Date

21-Aug-25

Site

5923 Ottawa Street

Prepared By

Matthew Hopley

Reviewed By

Jin Chen

| Building 1 | | | | | | | | | | | | |
|--|------------|-------------------|--------------|--------------------|----------------|-------------------|--------------------|--------------|--------------|---------------------------|--------------------|--------------------------|
| Safety Margin on Sprinkler only 20% | | | | | | | | | | | | |
| | Area (ft2) | Density (gpm/ft2) | Volume (gpm) | Duration (minutes) | Capacity (L) | Hose Demand (gpm) | Duration (minutes) | Capacity (L) | Combined (L) | Shuttling Allowance (lpm) | Duration (minutes) | Total Storage Volume (L) |
| Grain Handling (OH2) | 238 | 0.2 | 47.6 | 60 | 10,810 | 250 | 60 | 56,700 | 69,672 | -1,893 | 60 | -43,878 |
| Brewing and Bottling/Process (DISCUS) | 3000 | 0.2 | 600 | 60 | 136,260 | 250 | 60 | 56,700 | 220,212 | -1,893 | 60 | 106,662 |
| Boiler Room (OH1) | 277 | 0.15 | 41.55 | 60 | 9,436 | 250 | 60 | 56,700 | 68,023 | -1,893 | 60 | -45,527 |
| Distillery (DISCUS) | 965 | 0.2 | 193 | 90 | 65,745 | 500 | 90 | 170,100 | 248,995 | -1,893 | 90 | 78,670 |
| Distillery (as EH1 for AS) | 965 | 0.3 | 289.5 | 90 | 98,618 | 500 | 90 | 170,100 | 288,442 | -1,893 | 90 | 118,117 |
| Office Mezzanine (LH) | 1182 | 0.1 | 118.2 | 30 | 13,422 | 100 | 30 | 11,340 | 27,446 | -1,893 | 30 | -29,329 |
| Kitchen (OH1) | 190 | 0.15 | 28.5 | 60 | 6,472 | 250 | 60 | 56,700 | 64,467 | -1,893 | 60 | |
| Bar (LH) (limited to 1500 ft2) | 1632 | 0.1 | 150 | 30 | 17,033 | 100 | 30 | 11,340 | 31,779 | -1,893 | 30 | |
| Kitchen + Bar | | | | | 23,505 | 250 | 60 | 56,700 | 84,906 | -1,893 | 60 | -28,644 |
| Retail (OH2) | 885 | 0.15 | 132.75 | 60 | 30,148 | 250 | 60 | 56,700 | 92,877 | -1,893 | 60 | -20,673 |

| Building 2 | | | | | | | | | | | | |
|--|------------|-------------------|--------------|--------------------|----------------|-------------------|--------------------|--------------|--------------|---------------------------|--------------------|--------------------------|
| Safety Margin on Sprinkler only 20% | | | | | | | | | | | | |
| | Area (ft2) | Density (gpm/ft2) | Volume (gpm) | Duration (minutes) | Capacity (L) | Hose Demand (gpm) | Duration (minutes) | Capacity (L) | Combined (L) | Shuttling Allowance (lpm) | Duration (minutes) | Total Storage Volume (L) |
| Mashing (DISCUS), 2000 sqft max area | 6050 | 0.2 | 400 | 60 | 90,840 | 250 | 60 | 56,700 | 165,708 | -1,893 | 60 | 52,158 |
| Bottling, 3000 sqft max area | 2370 | 0.2 | 474 | 60 | 107,645 | 500 | 60 | 113,400 | 242,574 | -1,893 | 60 | 129,024 |
| Office and admin (light hazard) | 1095 | 0.1 | 109.5 | 30 | 12,434 | 100 | 30 | 11,340 | 26,260 | -1,893 | 30 | -30,515 |
| Storage mezzanine (OH2) | 1185 | 0.2 | 237 | 60 | 53,823 | 250 | 60 | 56,700 | 121,287 | -1,893 | 60 | 7,737 |



August 21, 2025

Jack Gulas
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North Gower, ON
K0A 2T0

EMAIL: jack@stratfordfoxrun.com
CC: josh.laginski@outlook.com

Dear Jack:

**RE: 5923 OTTAWA STREET OCCUPANCY ALTERNATIVE SOLUTION ROADMAP
LRI FILE 2025-08-0269**

INTRODUCTION

The project at 5923 Ottawa Street, Ottawa, ON includes two buildings on one site to be used for a mix of industrial and assembly occupancies. This letter is intended to help provide relevant information regarding the intended design and compliance process relative to the occupancy classification for the distillery building (Building 1). This letter's framework (or roadmap) summarizes important parts of the analysis that have been undertaken for the project, as well as future elements to be incorporated into the design of the building to align the design and use of the building to meet the level of safety required by the OBC. The overall approach will require an alternative solution to be submitted as part of the building permit process. This letter is not considered to be a formal alternative solution, but is instead, intended to allow project stakeholders to understand what future submissions will include to help inform processes such as development permit approval.

CONCEPT DISCUSSION

Building 1 at 5923 Ottawa Street, Ottawa, ON will include a distillery, some mezzanine offices, a bar/tasting area, a retail store, and an outdoor patio. The second building (Building 2) is an industrial building intended to comply with the acceptable solutions of the building code and is understood to be treated primarily as a Group F, Division 2 major occupancy (with other lower hazard subsidiary occupancies).

Buildings are required to be classified as a function of their major occupancies. OBC Article 3.1.2.1 specifies that a building is to be classified in conformance with this Article and includes Appendix A, Division B-3.1.2.1.(1) which gives examples of various occupancies, including distilleries as an example of a Group F, Division 1 high hazard industrial occupancy.





Similarly, OFC Sentence 4.9.1.1.(2) outlines that the “parts of a building in which distilled beverage alcohol is distilled, processed or stored in bulk shall be classified as high hazard industrial occupancies”.

The definition of distillery is generally understood to have not considered the potential for smaller operations. Conversely, “craft” or “micro” distilleries are not defined in any meaningful sense within the Building/Fire codes. Notwithstanding, absent a definition of “sufficient quantities” and “special fire hazard”, the strict application of the Code to all distilleries in all cases fails to acknowledge that where the quantities of alcohol are moderate and where fire safety features are sufficient, the level of risk of craft distilleries can be managed to an extent where the hazard is comparable to a medium-hazard industrial occupancy.

As a result, consideration pertaining to the OBC and the construction of distilleries must be reviewed in order to develop a compliant structure. The approach to protection in this design intends to incorporate features which limit the potential for fires and explosion with multiple layers of active and passive fire safety features. Explosion risks are mitigated by reducing the probability of an explosion occurring in the first place, rather than mitigating the consequence of the explosion through deflagration venting which offers little protection to those near the hazard. In addition to the use of mitigating design features, the use of a risk index serves to quantify what can be considered a “special fire hazard”, and at what point a fire hazard is no longer “special”. This risk indexing demonstrates that in combination with the safety features described in this report, that restricting the size and risks posed by the distillery itself further meets the requirements of the Code.

As this is a small craft distillery which processes and produces significantly smaller amounts of products, it is proposed that the hazard associated with the operation is considerably lower than the original intent of the Code, which did not consider the potential for smaller craft-style distilleries. The conclusion of this report is that where a sufficiently small, appropriately fire-protected distillery is installed in a building, the level of risk presented by the craft distillery is at least as low as a comparable medium-hazard industrial Group F, Division 2 occupancy. The future alternative solution will also provide details on requirements from the Building and Fire Codes which are considered essential for distillery operations of any size. The sections of this letter below provide an overview of how the subject distillery will be assessed in terms of occupancy classification, and outline the provided means to mitigate the design related risk to a level that aligns with the OBC requirements for medium-hazard industrial occupancies.

BUILDING DESCRIPTION

The subject site includes a distillery within Building 1, which consists of the following:

- One storey in building height, with mezzanine
- 8.5 m in height
- 647 m² in building area
- Sprinklered throughout
- Occupancies include:
 - Distillery
 - Offices
 - Bar/assembly
 - Retail



DISTILLERY PROCESS DESCRIPTION

The distillery portion of the building (still house) consists of distillation equipment located in one fire compartment within Building 1. The still house will be fire separated from the remainder of the building and includes the following equipment that includes alcohol above 20% ABV (which is the concentration at which the OFC defines the subject liquids as distilled beverage alcohol).

- Four totes containing 2,000 L each (8,000 L);
- One Doubler containing 500 L;
- One Pot Still containing 3,500 L;
- Two column Stills containing approximately 100 L each during use (200 L);

The total volume of higher proof ethanol above 20% ABV then totals approximately 12,200 L at varying concentrations above 20% ABV, ranging up to 95% ABV at the highest concentration.

CODE REQUIREMENTS

When assessing required fire safety features, it is important to assess the overall risk that a given process presents, which considers both the probability and magnitude of various hazards. In order to effectively analyze, identify, and mitigate the relevant hazards, a rigorous, practical, repeatable, and industry-accepted methodology needs to be applied. The objective of the assessment is to review a proposed process (the distillery), assess the hazards, and where necessary, add mitigating measures to reduce the level of risk such that it aligns with that accepted by the OBC.

Ultimately, the assessment in the future alternative solution will demonstrate that the occupancy will present a comparable level of risk as that posed by a medium-hazard industrial occupancy. The assessment considers more simplistic properties, such as fuel load concentrations, but also incorporates more advanced assessments to better highlight where necessary process changes or additional protection may be required.

METHODOLOGY

To mitigate the potential damage and harm that could arise from a fire or explosion occurring from within the distillery portion of the building, extra protection measures will be provided to both reduce the probability of explosions and limit the consequences of a fire or explosion should one occur. A measure must be provided to demonstrate that the proposed design mitigates the risks of fires and explosions to the level required by Code to permit the classification of the unit as a Group F, Division 2 major occupancy. For this project, it is proposed to use the DOW Fire and Explosion risk index (DOW F&EI) to provide a quantitative, relative measurement of the site's risk profile.

Fire risk indexes serve a role in fire protection by striking a balance between qualitative approaches which may or may not provide adequate detail or granularity, and fully quantitative methods which can be expensive, labour intensive, slow, and which tend to require specialist knowledge to adequately judge. "[The DOW F&EI guide] is intended to provide a direct and logical approach for determining the probable "risk exposure" of a process plant and to suggest approaches to fire protection and loss prevention design. An important application of the F&EI is to help decide when a more detailed quantitative risk analysis is warranted, as well as the appropriate depth of such a study"¹.

¹ Society of Fire Protection Engineers, SFPE Handbook of Fire Protection Engineering, 5th Edition, page 3162



The DOW F&EI method was developed by the Dow Chemical corporation where the first edition was released in 1964. Since its first release, the index has been used by DOW and other entities in the chemical industry. The current version, the 7th edition was released in 1994 and is still in use today. The DOW F&EI is “the leading hazard index recognized by the chemical industry” and “provides key information to help evaluate the overall risk from fire and explosion”². The method follows a regimented step-by-step process which is applied to each process unit of a plant. Expertise in selecting specific penalty values is needed, but the available guide to how each should be applied helps explain the rationale behind selecting certain values.

The full DOW F&EI follows a thirteen-step process to determine a variety of outputs which includes the index score, the area of exposure, a damage factor, and additional economic measurements used to analyse process plant layouts and designs. For the purpose of this analysis, the critical output of the analysis is to assess the F&EI score. This score is a function of the process material factor, general process hazard penalties, and special process hazard penalties.

The base score without loss control credit factors applied will be reviewed. Furthermore, an offset version of the score will be reviewed considering the methods proposed by Gupta³. The base DOW F&EI score will be considered appropriate where it does not exceed the threshold for “intermediate” hazards (a score of 127 or lower in the DOW F&EI). The offset score will be evaluated, and relevant mitigating features will be added to achieve an offset score in the “moderate” hazard range (a score of 96 or lower). Scores below this threshold can generally be managed through standard fire protection and building design measures, would not represent a special fire hazard, and would more closely align with the hazards typical of a medium-hazard industrial occupancy.

| DEGREE OF HAZARD FOR F&EI | |
|---------------------------|------------------|
| F&EI INDEX RANGE | DEGREE OF HAZARD |
| 1 - 60 | Light |
| 61 - 96 | Moderate |
| 97 - 127 | Intermediate |
| 128 - 158 | Heavy |
| 159 - up | Severe |

TYPICAL MITIGATING MEASURES

As outlined in the previous section, the use of the DOW F&EI analysis will firstly evaluate the proposed process and associated process units within the still house. Where a given process unit (or the collective group of units) produces an unacceptably high index score, the process can be adjusted to present a lower overall risk. Ways to address the raw hazard index score include process equipment changes like volume or operating pressure, ventilation within the process unit area, improving spill control or drainage, amongst other inherent features within the distillery area. The processes would be adjusted such that the raw score remains in the acceptable range (127 or lower) as indicated above, and then

² American Institute of Chemical Engineers, DOW’s Fire & Explosion Index Hazard Classification Guide, 7th Edition, 1994, Page 1.

³ J.P Gupta, G. Khemani, M. S. Mannan, “Calculation of Fire and Explosion Index (F&EI) value for the Dow Guide taking credit for the loss control measures”, Journal of Loss Prevention in the Process Industries, Issue 16, 2003, pages 235-241.



mitigating features are added to the building design to reduce that score to an “offset” value that is in the “moderate” range or below.

The following offset measures are used in the DOW F&EI and can be considered as the design develops and have been used in various distilleries, but for clarity, are not all necessarily required pending design development:

- Emergency power;
- Emergency cooling systems;
- Explosion control;
- Emergency shutdown systems;
- Computer control (as opposed to manual process units);
- Written/detailed operating instructions (including emergency procedures);
- Leak detection;
- Sprinkler systems;
- Hand extinguishers/monitors.

From an OBC and OFC perspective, the following features must be considered and, where deemed necessary, incorporated into a given design in order to assess a given craft distillery as a medium-hazard industrial occupancy and to meet the objective and functional statements:

| Rapid fire spread mitigation | Explosion risk mitigation |
|---|---|
| Limited maximum capacities of flammable liquids | Flammable vapour detection |
| Emergency containment and drainage | Closures and if they must be integrated with an LEL detection system |
| Enhanced sprinkler protection within the distillery | Integration of LEL detection system and fire alarm system |
| Fire separations between occupancies and from exits | Ventilation throughout distillery |
| Noncombustible construction, with combustible elements only where it is permissible | Still pressure relief and tank venting routed to the outside, with flame arrestors on vents |
| Combustible content limits below those historically associated with high-hazard industrial occupancies, and which align well with modern medium-hazard industrial occupancies | Appropriate pressure relief of still equipment |
| | Still pressure monitoring |
| | Process interlocks (both for still piping and ventilation) |
| | Classified electrical equipment within hazardous areas |
| | Indirect fired stills, no open flames to heat process equipment |
| | Computer temperature still control |



By completing this analysis, adjusting necessary design parameters within the context of the building permit submission package alongside the responsible Professionals, it will be shown that the process units and proposed occupancy classification can align with the requirements for a Group F, Division 2 medium-hazard industrial occupancy.

OTHER APPROVED DISTILLERIES

A range of distilleries have been analyzed and approved using the method outlined above, with LRI's involvement including:

- Ogham Craft Spirits Micro-Distillery, Ottawa, ON
- Burwood Distillery, Calgary, AB
- True Wild Distillery, Calgary, AB
- Spirit in Niagara Distillery, Niagara, ON

CONCLUSION

The proposed project to be located at 5923 Ottawa Street, Ottawa, includes two buildings located on one site. Building 1 includes a distillery area within the building to be used for the production of craft spirits. Since this necessarily involves the production and handling of distilled beverage alcohol, as indicated by the OBC Appendix and OFC, the acceptable solutions would ordinarily mandate this be classified as a Group F, Division 1 high hazard industrial occupancy. As explained in this letter, these requirements have historically been included as a result of prior production volume mandates and used for large-scale industrial processes. No consideration is given in either code for the size, volume, and protective features that might be included in a distillery which can thereby reduce the overall risk to a level below a "special fire hazard", the defining characteristic of this occupancy's definition.

As such, the distillery occupancy in Building 1 is proposed to be analyzed using a combination of fuel load assessment and semi-quantitative risk indexing to confirm the overall risk level that the craft distillery poses. Once analyzed, appropriate and necessary fire and explosion protection features will be added in order to mitigate the level of risk presented by the distillery to align with that permitted by Group F, Division 2, medium hazard industrial occupancies. As such, the OBC-related design features, and related engineering design, should consider the building as a Group F, Division 2 occupancy, while distillery-specific protective features will be incorporated as outlined above to protect the distillery and adjacent areas. This approach has been applied, accepted, and built in a number of jurisdictions using the same rationale and design approach, further demonstrating its acceptability in principal.

Sincerely,
LRI ENGINEERING

Matthew Hopley, M.Eng., P.Eng [AB]
Branch Manager - Alberta

Reviewed by,
LRI ENGINEERING

Jin Chen, M.Eng., P.Eng.
Associate

APPENDIX D SANITARY DESIGN

000-25-0415 - 5923 Ottawa Street - Sanitary Demands - Phase 1

| | |
|--------------|--------------------|
| Project: | 5923 Ottawa Street |
| Project No.: | 000-25-0415 |
| Designed By: | FV |
| Checked By: | JB |
| Date: | May 5, 2025 |

| | | |
|---------------------------------|------|----------------|
| Site Area | 0.48 | Gross ha |
| Commercial Area (Retail) | 90 | m ² |
| Industrial - Light (Distillery) | 432 | m ² |
| Restaurant | 363 | m ² |

DESIGN PARAMETERS

| | |
|--|-------------|
| Institutional/ Commercial Peaking Factor | 1.5 |
| Mannings coefficient (n) | 0.013 |
| Infiltration allowance | 0.33 L/s/Ha |

EXTRANEOUS FLOW ALLOWANCES

| Infiltration / Inflow | Flow (L/s) |
|-----------------------|------------|
| Dry | 0.02 |
| Wet | 0.13 |
| Total | 0.16 |

AVERAGE DAILY DEMAND

| DEMAND TYPE | AMOUNT | UNITS | POPULATION / AREA | Flow (L/s) |
|----------------------------|--------|---------------------------|-------------------|------------|
| Residential | 280 | L/c/d | | 0.0 |
| Industrial - Light** | 35,000 | L/gross ha/d | 0.04 | 0.02 |
| Industrial - Heavy** | 55,000 | L/gross ha/d | | 0 |
| Commercial / Amenity | 2,800 | L/(1000m ² /d) | 90 | 0.00 |
| Restaurant | 125 | L/(9.2m ² /d) | 363 | 0.06 |
| Schools | 70 | L/(Student/d) | | 0 |
| Trailer Parks no Hook-Ups | 340 | L/(space/d) | | 0 |
| Trailer Park with Hook-Ups | 800 | L/(space/d) | | 0 |
| Campgrounds | 225 | L/(campsite/d) | | 0 |
| Mobile Home Parks | 1,000 | L/(Space/d) | | 0 |
| Motels | 150 | L/(bed-space/d) | | 0 |
| Hotels | 225 | L/(bed-space/d) | | 0 |
| Office | 75 | L/7.0m ² /d | | 0 |
| Tourist Commercial | 28,000 | L/gross ha/d | | 0 |
| Other Commercial | 28,000 | L/gross ha/d | | 0 |

| | | |
|--------------------------|------|-----|
| AVERAGE RESIDENTIAL FLOW | 0.00 | L/s |
| PEAK RESIDENTIAL FLOW | 0.00 | L/s |
| AVERAGE ICI FLOW | 0.08 | L/s |
| TOTAL PEAK ICI FLOW | 0.12 | L/s |

TOTAL SANITARY DEMAND

| | | |
|--|------|-----|
| TOTAL ESTIMATED AVERAGE DRY WEATHER FLOW | 0.10 | L/s |
| TOTAL ESTIMATED PEAK DRY WEATHER FLOW | 0.14 | L/s |
| TOTAL ESTIMATED PEAK WET WEATHER FLOW | 0.27 | L/s |

000-25-0415 - 5923 Ottawa Street - Sanitary Demands - Phase 2

| | |
|--------------|--------------------|
| Project: | 5923 Ottawa Street |
| Project No.: | 000-25-0415 |
| Designed By: | FV |
| Checked By: | JB |
| Date: | May 5, 2025 |

| | |
|---------------------------------|--------------------|
| Site Area | 0.45 Gross ha |
| Industrial - Light (Distillery) | 926 m ² |

DESIGN PARAMETERS

| | |
|--|-------------|
| Institutional/ Commercial Peaking Factor | 1.5 |
| Mannings coefficient (n) | 0.013 |
| Infiltration allowance | 0.33 L/s/Ha |

EXTRANEOUS FLOW ALLOWANCES

| Infiltration / Inflow | Flow (L/s) |
|-----------------------|------------|
| Dry | 0.02 |
| Wet | 0.13 |
| Total | 0.15 |

AVERAGE DAILY DEMAND

| DEMAND TYPE | AMOUNT | UNITS | POPULATION / AREA | Flow (L/s) |
|----------------------------|--------|---------------------------|-------------------|------------|
| Residential | 280 | L/c/d | | 0 |
| Industrial - Light** | 35,000 | L/gross ha/d | 0.04 | 0.02 |
| Industrial - Heavy** | 55,000 | L/gross ha/d | | 0 |
| Commercial / Amenity | 2,800 | L/(1000m ² /d) | | 0 |
| Restaurant | 125 | L/(9.2m ² /d) | | 0 |
| Schools | 70 | L/(Student/d) | | 0 |
| Trailer Parks no Hook-Ups | 340 | L/(space/d) | | 0 |
| Trailer Park with Hook-Ups | 800 | L/(space/d) | | 0 |
| Campgrounds | 225 | L/(campsite/d) | | 0 |
| Mobile Home Parks | 1,000 | L/(Space/d) | | 0 |
| Motels | 150 | L/(bed-space/d) | | 0 |
| Hotels | 225 | L/(bed-space/d) | | 0 |
| Office | 75 | L/7.0m ² /d | | 0 |
| Tourist Commercial | 28,000 | L/gross ha/d | | 0 |
| Other Commercial | 28,000 | L/gross ha/d | | 0 |

| | | |
|--------------------------|------|-----|
| AVERAGE RESIDENTIAL FLOW | 0.00 | L/s |
| PEAK RESIDENTIAL FLOW | 0.00 | L/s |
| AVERAGE IQ FLOW | 0.02 | L/s |
| TOTAL PEAK IQ FLOW | 0.03 | L/s |

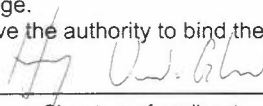
TOTAL SANITARY DEMAND

| | | |
|--|------|-----|
| TOTAL ESTIMATED AVERAGE DRY WEATHER FLOW | 0.04 | L/s |
| TOTAL ESTIMATED PEAK DRY WEATHER FLOW | 0.05 | L/s |
| TOTAL ESTIMATED PEAK WET WEATHER FLOW | 0.17 | L/s |

Application for a Permit to Construct or Demolish

This form is authorized under subsection 8(1.1) of the *Building Code Act, 1992*

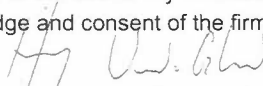
| For use by Principal Authority | | | |
|---|-------------|--|------------------------------|
| Application number: | | Permit number (if different): | |
| Date received: | | Roll number: | |
| Application submitted to: Ottawa Septic System Office | | <div style="border: 1px solid black; padding: 5px; display: inline-block;"> RVCA RECEIVED JUN 09 2025 REFER TO: _____ </div> <div style="margin-left: 20px; color: blue; font-weight: bold;"> SEPTIC FILE # 25-176 OTTAWA </div> | |
| (Name of municipality, upper-tier municipality, board of health or conservation authority) | | | |
| A. Project information | | | |
| Building number, street name | | Unit number | Lot/con. |
| 5923 Ottawa street | | | |
| Municipality | Postal code | Plan number/other description | |
| Ottawa (Richmond) | K0A 2Z0 | | |
| Project value est. \$ | | Area of work (m ²) | |
| | | | |
| B. Purpose of application | | | |
| <input checked="" type="checkbox"/> New construction <input type="checkbox"/> Addition to an existing building <input type="checkbox"/> Alteration/repair <input type="checkbox"/> Demolition <input type="checkbox"/> Conditional Permit | | | |
| Proposed use of building | | Current use of building | |
| Commercial | | | |
| Description of proposed work | | | |
| To construct a new class 4 sewage system, Eljen NSF 245 Denitrification treatment system: Eljen DN450 | | | |
| Sewage System 'A' | | | |
| C. Applicant | | | |
| Applicant is: <input type="checkbox"/> Owner or <input checked="" type="checkbox"/> Authorized agent of owner | | | |
| Last name | First name | Corporation or partnership | |
| Van de Glind | Hendrik | Paterson Group Inc. | |
| Street address | | Unit number | Lot/con. |
| 9 Auriga Drive | | | |
| Municipality | Postal code | Province | E-mail |
| Ottawa | K2E 7T9 | ON | hvandeglind@patersongroup.ca |
| Telephone number | Fax | | Cell number |
| 613-226-7381 | | | |
| D. Owner (if different from applicant) | | | |
| Last name | First name | Corporation or partnership | |
| Gulas | Jack | 99117756 Canada Inc. | |
| Street address | | Unit number | Lot/con. |
| 411 Leggett Drive, Suite 710 | | | |
| Municipality | Postal code | Province | E-mail |
| Ottawa | K2K 3C9 | ON | jack@stratfordfoxrun.com |
| Telephone number | Fax | | Cell number |
| 613-862-0087 | | | |

| E. Builder (optional) | | | | |
|---|-------------|--|----------|---------------|
| Last name | First name | Corporation or partnership (if applicable) | | |
| Street address | | Unit number | Lot/con. | |
| Municipality | Postal code | Province | E-mail | |
| Telephone number | Fax | Cell number | | |
| F. Tarion Warranty Corporation (Ontario New Home Warranty Program) | | | | |
| i. Is proposed construction for a new home as defined in the <i>Ontario New Home Warranties Plan Act</i> ? If no, go to section G. | | <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No | | |
| ii. Is registration required under the <i>Ontario New Home Warranties Plan Act</i> ? | | <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No | | |
| iii. If yes to (ii) provide registration number(s): _____ | | | | |
| G. Required Schedules | | | | |
| i) Attach Schedule 1 for each individual who reviews and takes responsibility for design activities. | | | | |
| ii) Attach Schedule 2 where application is to construct on-site, install or repair a sewage system. | | | | |
| H. Completeness and compliance with applicable law | | | | |
| i) This application meets all the requirements of clauses 1.3.1.3 (5) (a) to (d) of Division C of the <i>Building Code</i> (the application is made in the correct form and by the owner or authorized agent, all applicable fields have been completed on the application and required schedules, and all required schedules are submitted). | | <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No | | |
| Payment has been made of all fees that are required, under the applicable by-law, resolution or regulation made under clause 7(1)(c) of the <i>Building Code Act, 1992</i> , to be paid when the application is made. | | <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No | | |
| ii) This application is accompanied by the plans and specifications prescribed by the applicable by-law, resolution or regulation made under clause 7(1)(b) of the <i>Building Code Act, 1992</i> . | | <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No | | |
| iii) This application is accompanied by the information and documents prescribed by the applicable by-law, resolution or regulation made under clause 7(1)(b) of the <i>Building Code Act, 1992</i> which enable the chief building official to determine whether the proposed building, construction or demolition will contravene any applicable law. | | <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No | | |
| iv) The proposed building, construction or demolition will not contravene any applicable law. | | <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No | | |
| I. Declaration of applicant | | | | |
| Hendrik Van de Glind, L.E.T., C.E.T. - Paterson Group (print name) | | | | declare that: |
| 1. The information contained in this application, attached schedules, attached plans and specifications, and other attached documentation is true to the best of my knowledge. 2. If the owner is a corporation or partnership, I have the authority to bind the corporation or partnership. | | | | |
| June 6, 2025 | |  Signature of applicant | | |
| Date | | | | |

Personal information contained in this form and schedules is collected under the authority of subsection 8(1.1) of the *Building Code Act, 1992*, and will be used in the administration and enforcement of the *Building Code Act, 1992*. Questions about the collection of personal information may be addressed to: a) the Chief Building Official of the municipality or upper-tier municipality to which this application is being made, or, b) the inspector having the powers and duties of a chief building official in relation to sewage systems or plumbing for an upper-tier municipality, board of health or conservation authority to whom this application is made, or, c) Director, Building and Development Branch, Ministry of Municipal Affairs and Housing 777 Bay St., 2nd Floor. Toronto, M5G 2E5 (416) 585-6666.

Schedule 1: Designer Information

Use one form for each individual who reviews and takes responsibility for design activities with respect to the project.

| A. Project Information | | | |
|---|---|--|--|
| Building number, street name 5923 Ottawa Street | | Unit no. | Lot/con. |
| Municipality Ottawa (Richmond) | Postal code K0A 2Z0 | Plan number/ other description | |
| B. Individual who reviews and takes responsibility for design activities | | | |
| Name Hendrik Van de Glind, L.E.T., C.E.T. | | Firm Paterson Group Inc. | |
| Street address 9 Auriga Drive | | Unit no. | Lot/con. |
| Municipality Ottawa | Postal code K2E 7T9 | Province ON | E-mail hvandeglind@patersongroup.ca |
| Telephone number 613-226-7381 | Fax number | Cell number | |
| C. Design activities undertaken by individual identified in Section B. [Building Code Table 3.5.2.1. of Division C] | | | |
| <input type="checkbox"/> House <input type="checkbox"/> Small Buildings <input type="checkbox"/> Large Buildings <input type="checkbox"/> Complex Buildings | <input type="checkbox"/> HVAC – House <input type="checkbox"/> Building Services <input type="checkbox"/> Detection, Lighting and Power <input type="checkbox"/> Fire Protection | <input type="checkbox"/> Building Structural <input type="checkbox"/> Plumbing – House <input type="checkbox"/> Plumbing – All Buildings <input checked="" type="checkbox"/> On-site Sewage Systems | |
| Description of designer's work On-site Sewage System Design | | | |
| D. Declaration of Designer | | | |
| I, <u>Hendrik Van de Glind, L.E.T., C.E.T. - Paterson Group</u> declare that (choose one as appropriate): (print name) | | | |
| I review and take responsibility for the design work on behalf of a firm registered under subsection 3.2.4. of Division C, of the Building Code. I am qualified, and the firm is registered, in the appropriate classes/categories. | | | |
| Individual BCIN: <u>111499</u> | | | |
| Firm BCIN: <u>29346</u> | | | |
| I review and take responsibility for the design and am qualified in the appropriate category as an "other designer" under subsection 3.2.5. of Division C, of the Building Code. | | | |
| Individual BCIN: _____ | | | |
| Basis for exemption from registration: _____ | | | |
| The design work is exempt from the registration and qualification requirements of the Building Code. | | | |
| Basis for exemption from registration and qualification: _____ | | | |
| I certify that: | | | |
| 1. The information contained in this schedule is true to the best of my knowledge. | | | |
| 2. I have submitted this application with the knowledge and consent of the firm. | | | |
| June 6, 2025 Date | |  Signature of Designer | |

NOTE:

1. For the purposes of this form, "individual" means the "person" referred to in Clause 3.2.4.7(1) (c) of Division C, Article 3.2.5.1. of Division C, and all other persons who are exempt from qualification under Subsections 3.2.4. and 3.2.5. of Division C.
2. Schedule 1 is not required to be completed by a holder of a license, temporary license, or a certificate of practice, issued by the Ontario Association of Architects. Schedule 1 is also not required to be completed by a holder of a license to practise, a limited license to practise, or a certificate of authorization, issued by the Association of Professional Engineers of Ontario.



Schedule 2: Sewage System Installer Information

| | | | |
|---|----------------------------|--|----------|
| A. Project Information | | | |
| Building number, street name 5923 Ottawa Street | | Unit number | Lot/con. |
| Municipality Ottawa (Richmond) | Postal code K0A 2Z0 | Plan number/ other description | |
| B. Sewage system installer | | | |
| Is the installer of the sewage system engaged in the business of constructing on-site, installing, repairing, servicing, cleaning or emptying sewage systems, in accordance with Building Code Article 3.3.1.1, Division C? | | | |
| <input type="checkbox"/> Yes (Continue to Section C) | | <input type="checkbox"/> No (Continue to Section E) | |
| | | <input checked="" type="checkbox"/> Installer unknown at time of application (Continue to Section E) | |
| C. Registered installer information (where answer to B is "Yes") | | | |
| Name | | BCIN | |
| Street address | | Unit number | Lot/con. |
| Municipality | Postal code | Province | E-mail |
| Telephone number | Fax | Cell number | |
| D. Qualified supervisor information (where answer to section B is "Yes") | | | |
| Name of qualified supervisor(s) | | Building Code Identification Number (BCIN) | |
| | | 25-176 | |
| | | OTTAWA | |
| E. Declaration of Applicant: | | | |
| I <u>Hendrik Van de Glind, L.E.T., C.E.T. - Paterson Group</u> declare that: | | | |
| (print name) | | | |
| I am the applicant for the permit to construct the sewage system. If the installer is unknown at time of application, I shall submit a new Schedule 2 prior to construction when the installer is known; | | | |
| <u>OR</u> | | | |
| I am the holder of the permit to construct the sewage system, and am submitting a new Schedule 2, now that the installer is known. | | | |
| I certify that: | | | |
| 1. The information contained in this schedule is true to the best of my knowledge. | | | |
| 2. If the owner is a corporation or partnership, I have the authority to bind the corporation or partnership. | | | |
| June 6, 2025 | | <u>H. Van de Glind</u> | |
| Date | | Signature of applicant | |

SEPTIC FILE #
25-176
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JUN 09 2025
REFER TO:



Schedule 4: Proposed Services

Complete Sections 1 through 7

Do Not Complete

Permit number: _____

Revision number: _____

Date _____

1 Engineered

- ☒ Yes
☐ No

2 Water supply

- ☒ Proposed
☐ Existing

3 Use

- ☐ Apartment
☐ Dwelling
☒ Commercial
☒ Industrial

4 Type of work proposed

- ☒ New Installation
☐ Replacement
☐ Alteration

5 Type of Well

- ☐ Dug/Bored/Sandpoint well
☒ Drilled well
☐ Municipal
☐ Other

6 Residential Sewage Design Flow Info.

Bedrooms _____
House (floor area) _____ m²
People _____
Total Fixture Units _____ (Schedule 8)
Residential Flow _____ L/day

7 Sewage Design Flow Other Occupancies

Design Flow 9367 L/day

Detailed sewage flow calculations:

Refer to PGI Drawings No. PH4924-2(rev.3)

8 Type of System

- ☐ Class 2 – Leaching Pit
☐ Class 3 – Cesspool

Treatment Unit Eljen GSF A-42 (DN450)

☐ Class 4 – Trench (Schedule 9)

- ☐ Fully raised
☐ Partially raised
☐ In-ground

☐ Class 4 – Filter Media (Schedule 10)

- ☐ Fully raised
☐ Partially raised
☐ In-ground

☐ Class 4 – Shallow Buried Trench

- ☐ Fully raised
☐ Partially raised
☐ In-ground

☒ Class 4 – BMEC Area Bed (Schedule 11)

- ☒ Fully raised
☐ Partially raised
☐ In-ground

☐ Class 4 – "Type A" Dispersal (Schedule 13)

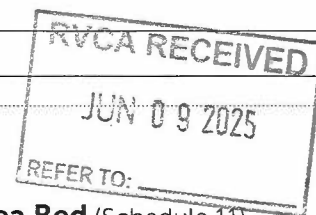
- ☐ Fully raised
☐ Partially raised
☐ In-ground

☐ Class 4 – "Type B" Dispersal (Schedule 14)

- ☐ Fully raised
☐ Partially raised
☐ In-ground

☐ Class 5 – Holding Tank (9000L min)

- ☐ Tank/Treatment Unit/Pump Chamber ONLY
☐ Effluent Filter/Risers ONLY
☐ Other _____



SEPTIC FILE #
25-176
OTTAWA



Schedule 5: Sewage System Details

SEPTIC FILE #
25-176
OTTAWA

Do Not Complete

Permit number:

Revision number:

Date

Complete below

Type of System Eljen GSF A-42 Modules (DN 450) (Schedule 4)

Septic/Holding Tank Size: 28,101 (Litres)

Make: _____

Septic Tank Effluent Filter Make: OBC Approved

Model: (Polylok PL-525 or equivalent)

Treatment Unit - Make & Model: Eljen GSF A-42 Modules (DN450)

Number of Units: 110

Refer to Typical Drawing #: PH4924-1&2(rev.3)

Pump ☒ Syphon ☐

Pump(s) required: Yes

Pump Rate: 391 + Charge L/15min Hour

Mantle Information

Native or imported = min. 15m in N/A direction(s)

Slope subgrade _____ % slope

_____ direction(s)

Note: Alarm required for all pumping systems

Installed ☐ Inside TBD By Installer @

☐ Outside time of Installation

Site to be Scarified (If clay) Yes ☒ No ☐

Clay Seal Required (If bedrock) Yes ☐ No ☐

☐ Trench

Distribution Pipe Length _____ m

Loading Area _____ m²

Type of Chamber _____

Length of Chamber _____ m

☐ Dispersal Bed

☒ BMEC ☐ Type A ☐ Type B

Stone N/A m²

Sand 837.9 m²

Pipe 134.2 m²

Linear Loading 11.2 L/m²

☐ Shallow Buried Trench

Pipe Length _____ m²

Pipe _____

☐ Filter Media Bed

Stone _____ m

Extended Base _____ m²

Pipe _____

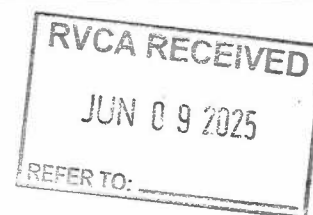
Weight of Filter Media _____ Kg

Loading Area _____ m²

☐ Tank/Treatment Unit/Pump Chamber Replacement **ONLY**

☐ Effluent Filter & Riser **ONLY**

Construction Notes:





Schedule 6: Soil and Water
Table Information (Minimum depth of test pit: 2 metres)

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JUN 09 2025

Do Not Complete

Permit number:

Revision number:

Date

Name of Applicant/Agent: Paterson Group Inc.

Date: June 17, 2024

Time:

Applicant/Agent Signature:

Inspector:

Date:

Time:

Inspector Signature:

| EG () | Soil Description |
|--------|------------------|
| m | |
| m | |
| m | |
| m | |
| m | |
| m | |
| m | |

Professional Engineers
Ontario

Licensed Engineering Technologist

Name: H. G. VAN DE GLIND
Number: 100647862
Limitations: Inspecting, designing, and assessing residential and commercial sewage systems, grading designs and soil analysis, and overseeing installation and compliance.

Association of Professional Engineers of Ontario

T-time 35 Min/cm

| EG () | Soil Description |
|--------|------------------|
| m | |
| m | |
| m | |
| m | |
| m | |
| m | |
| m | |

Test pits not available for inspection.
Engineer assumes all liability for soil and HGWT info/elev's.

T-time Min/cm

| EG () | Soil Description |
|--------|------------------|
| m | |
| m | |
| m | |
| m | |
| m | |
| m | |
| m | |

T-time Min/cm

| EG () | Soil Description |
|--------|------------------|
| m | |
| m | |
| m | |
| m | |
| m | |
| m | |
| m | |

T-time Min/cm

Legend

BR Bedrock
HGWT High ground water table
EG Existing grade

GWT Ground water table
M metres
T percolation rate



Schedule 7: Layout Section

Do Not Complete

Permit number:

Revision number:

Date

Scale: 1 Block = _____

- Dug Well
- Drilled Well

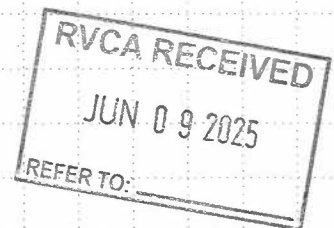
- ▲ Neighbouring Homes
- ◇ Benchmark

- Tile Drainage
- ___ Property Line

SEPTIC FILE #

25-176

OTTAWA



Elevations (metric only)

B.M. 94.86 m

B.M Description Top of spike in hydro pole across
from East Property Line of 5935 Ottawa Street

Exact Location _____

Min. of 5 elevations in proposed system area (in X pattern)

| | |
|----------------------|----------------------------|
| X ₁ _____ | X ₂ _____ |
| X ₃ _____ | X ₄ _____ |
| X ₅ _____ | X ₆ (toe) _____ |
| X ₇ _____ | X ₈ _____ |



SEPTIC FILE #

25-176

**Schedule 8: Fixture unit count****Do Not Complete**

Permit number:

Revision number:

Date

| Fixtures | # Existing | + | # Proposed | X | unit count | = | Fixture Count |
|---|------------|---|------------|---|------------|---|---------------|
| Bathroom | | | | | | | |
| Bathroom group (toilet, sink and tub or shower) installed in the same room | | + | | X | 6 | = | 0.00 |
| Bathtub with/without overhead shower | | + | | X | 1.5 | = | 0.00 |
| Shower stall | | + | | X | 1.5 | = | 0.00 |
| Wash basin (SINK) (1½ inch trap) | 6 | + | | X | 1.5 | = | 9.00 |
| Watercloset (TOILET) tank operated | 6 | + | | X | 4 | = | 24.00 |
| Bidet | | + | | X | 1 | = | 0.00 |
| Kitchen | | | | | | | |
| Dishwasher | 2 | + | | X | 1 | = | 2.00 |
| Sink with/without garbage grinder(s), domestic and other small type single, double or 2 single with a common trap | 5 | + | | X | 1.5 | = | 7.50 |
| Other | | | | | | | |
| Domestic washing machine | | + | | X | 1.5 | = | 0.00 |
| Combination sink and laundry tray single or double (Installed on 1½ trap) | | + | | X | 1.5 | = | 0.00 |
| Total* | | | | | | = | 42.50 |

***Insert the TOTAL in section 5 of Schedule 4 (O.Reg 151/13 Table 7.4.9.3)**

1. Sump pumps and floor drains are not to be connected to the sewage system. Connection of such fixtures to a sewage system may lead to a hydraulic failure of the said system. The above mentioned fixtures should be discharged separately to an approved Class 2 (leaching pit) sewage system.

2. Where laundry waste is not more than 20% of the total daily design sanitary sewage flow, it may discharge to a sewage system (Part 8, OBC, 8.1.3.1(2)).

Agent/Owner signature

June 6, 2025

Date

TIC FILE #

25-177

N42°37'20"W

OTTAWA

SEPTIC FILE #

25-175

OTTAWA

RECEIVED

9 2025

NOTE:

SEWAGE SYSTEM 'B' HAS BEEN DESIGNED BASED ON PATERSON GROUP REPORT PH4924-LET.01

TOTAL DESIGN DAILY SANITARY SEWAGE FLOW (T.D.D.S.S.F.) OR "Q" = 600 L/DAY WHEN BALANCED OVER 7 DAYS.

NATIVE SOILS = GLACIAL TILL TO SILTY CLAY = T = 40 min/cm

MINIMUM NITRATE REDUCTION LEVEL REQUIRED = 50% AS PER PATERSON GROUP REPORT No. PH4924-LET.01

ELJEN DN450 SHALL BE USED TO ACHIEVE THE MINIMUM REQUIRED NITRATE REDUCTION.

PRESENTLY PROPOSED ELEVATIONS ARE BASED OFF THE EXISTING TOPOGRAPHIC INFORMATION. THE PROPOSED LOT GRADING AND DRAINAGE ASSOCIATED WITH THE PROPOSED ADDITION MAY AFFECT THESE ELEVATIONS.

NOTE:

SEWAGE SYSTEM 'A' HAS BEEN DESIGNED BASED ON PATERSON GROUP REPORT PH4924-LET.01

TOTAL DESIGN DAILY SANITARY SEWAGE FLOW (T.D.D.S.S.F.) OR "Q" = 9,367 L/DAY WHEN BALANCED OVER 7 DAYS.

NATIVE SOILS = GLACIAL TILL TO SILTY CLAY = T = 35 min/cm

MINIMUM NITRATE REDUCTION LEVEL REQUIRED = 50% AS PER PATERSON GROUP REPORT No. PH4924-LET.01

ELJEN DN450 SHALL BE USED TO ACHIEVE THE MINIMUM REQUIRED NITRATE REDUCTION.

PRESENTLY PROPOSED ELEVATIONS ARE BASED OFF THE EXISTING TOPOGRAPHIC INFORMATION. THE PROPOSED LOT GRADING AND DRAINAGE ASSOCIATED WITH THE PROPOSED ADDITION MAY AFFECT THESE ELEVATIONS.

PART 4
R.P. 4R-7050Professional Engineers
Ontario

Licensed Engineering Technologist

Name: H. G. VAN DE GLIND
Number: 100647862Limitations: Inspecting, designing, and assessing
residential and commercial sewage systems, grading designs
and soil analysis, and overseeing installation and compliance.

Association of Professional Engineers of Ontario

LEGEND:

- 70.81 Existing Ground Surface Elev. (m)
- 72.70 Proposed Ground Surface Elev. (m)
- 72.70 Proposed Subgrade Elev. (m)
- (70.7) Groundwater Elev. (m) - Mar.6/22
- F.F.E. Finished Floor Elev. (m)
- Existing Structure
- Proposed Structure

All Units are in meters unless otherwise specified

BENCHMARK INFORMATION:

TBM: Top of Spike in Hydro Pole Across from
East Property Line of 5935 Ottawa Street
Approximate Geodetic Elevation = 94.86m

REFERENCE:

Topographic Information obtained from Plan of
Survey of Part of Unit 10 Index Plan D-26
Geographic Township of Goulbourn City of
Ottawa, dated July 9, 2024, by egis Surveying Inc.

Baseplan Obtained from Site Plan No. A-001,
dated May 2025, by N45 Architecture Inc.

- ELJEN SPECIFIED SAND AREA
- 630 mm THICK (TOP OF MODULE TO BASE)
 - 37.24m x 22.50m
 - FOLLOWED BY 300 mm THICK OF SAND/LIGNOCELLULOSE LAYER
 - FOLLOWED BY 50 mm THICK LAYER OF LIMESTONE

N42°32'25"W

- 2 CELLS OF 5 RUNS OF 11 ELJEN GSF A-42 MODULES
MODULAR BASE ELEV. @ HEAD = 94.65m
MODULAR BASE ELEV. @ FOOT = 94.60m

- ELJEN SAMPLING PAN
- INSTALL COLLECTION PLATES AS PER
MANUFACTURER SPECIFICATIONS

- 100mmØ PVC PIPE TO BE INSTALLED @ 2% (min.) SLOPE AND SHALL
BE SLEEVED THROUGH A 150mmØ PVC SDR28 PIPE AND OVERLAIN
BY 75mm T x 600mm W RIGID INSULATION BOARDS UNDER ASPHALT.
PATERSON TO REVIEW COVER UPON COMPLETION OF LOT GRADING
AND DRAINAGE.

- TYP.
2 OUTLET DISTRIBUTION BOX C/W INLET
BAFFLE AND POLYLOK FLOW EQUALIZERS
INLET INV. = 94.90m(min.)
OUTLET INV. = 94.80m (min.)

- ELJEN SAMPLING PAN
- INSTALL COLLECTION PLATES AS PER
MANUFACTURER SPECIFICATIONS
- 2 RUNS OF 4 ELJEN GSF A-42 MODULES
MODULAR BASE ELEV. @ HEAD = 94.42m
MODULAR BASE ELEV. @ FOOT = 94.40m

- TYP.
100mmØ VENT PIPE INSTALLED IN
150mmØ LANDSCAPE VALVE COVER

- TYP.
100mmØ SOLID PVC FOOTER PIPE
INV. = 94.58m

- NOTE:
SNOW STORAGE SHALL NOT BE LOCATED OVER OR
UPGRADIENT OF THE PROPOSED SEWAGE SYSTEM.

- NOTE:
SNOW STORAGE SHALL NOT BE LOCATED OVER OR
UPGRADIENT OF THE PROPOSED SEWAGE SYSTEM.

- TYP.
100mmØ VENT PIPE INSTALLED IN
150mmØ LANDSCAPE VALVE COVER

- 100mmØ PERFORATED PVC SEPTIC PIPE
INSTALLED @ APPROX. 0.5% ON ELJEN MODULES
HEAD INV. = 94.83m
FOOT INV. = 94.78m

- 3m L - 100mmØ PVC PIPE WITH
ELBOW @ 2% (min.) SLOPE

- 18,500L (min.) BALANCING TANK c/w TIME OPERATED EFFLUENT 1/2 H.P. DUPLEX
PUMPS AND AUDIBLE / VISUAL HIGH WATER ALARM.
- TANK SHALL BE CPA APPROVED (OR ENGINEERED) FOR 1.2m (min.) OF COVER.
 - TANK SHALL BE REVIEWED FOR BALLASTING REQUIREMENTS.
 - PUMPING SYSTEM SHALL BE TIME DOSED TO OPERATE EVERY HOUR AND
ALTERNATE BETWEEN CELLS.
 - POLY RISER AND COVER ASSEMBLY
 - INLET INV. = 94.40m±
 - TOP OF TANK (max.) = 94.75m±
 - FINISHED GRADE = 95.40m

PART 1
R.P. 4R-13387

- NEW 3,600L PRETREATMENT TANK c/w
- TANK SHALL BE CPA APPROVED (OR ENGINEERED) FOR 1.2m (min.) OF COVER.
 - TANK SHALL BE REVIEWED FOR BALLASTING REQUIREMENTS.
 - POLYLOK PL-525 EFFLUENT FILTER
 - POLY RISER & COVER ASSEMBLY (2)
 - INLET INV. = 94.27m±
 - OUTLET INV. = 94.22m±
 - TOP OF TANK = 94.55m±
 - FINISHED GRADE = 95.15m

- 3m L - 100mmØ PVC PIPE WITH
ELBOW @ 2% (min.) SLOPE

SS 'B'

BH 1-25
94.07
(93.63)

- 38mmØ PVC SCH 40 PIPE FORCEMAIN
- SHALL BE INSTALLED TO GRAVITY DRAIN TO THE TANK.
 - ENTIRE LENGTH OF FORCEMAIN SHALL BE BEDDED OF A
MINIMUM OF 150mm OF OPSS GRANULAR A, AND SHALL BE
COVERED WITH A MINIMUM OF 300mm OF OPSS GRANULAR A.
 - ALL GRANULAR A MATERIAL SHALL BE COMPACTED TO A
MINIMUM OF 98% SPMDD.

- 100mmØ PERFORATED PVC SEPTIC
PIPE INSTALLED @ APPROX. 0.5%
ON ELJEN MODULES
HEAD INV. = 94.60m
FOOT INV. = 94.58m

- ELJEN SPECIFIED SAND AREA
- 630 mm THICK (TOP OF MODULE TO BASE)
 - 9.60m x 9.68m
 - FOLLOWED BY 300 mm THICK OF SAND/LIGNOCELLULOSE LAYER
 - FOLLOWED BY 50 mm THICK LAYER OF LIMESTONE

SNOW STORAGE

SNOW STORAGE

- TYP.
2 x LARGE 4 OUTLET DISTRIBUTION BOX
C/W INLET BAFFLE AND POLYLOK FLOW
EQUALIZERS
INLET INV. = 95.10m(min.)
OUTLET INV. = 95.00m (min.)

- EXISTING
MONITORING
WELL TO BE
DECOMMISSIONED

PROPOSED INDUSTRIAL
BUILDING
(ONE STOREY)PROPOSED FINISHED
FLOOR ELEVATION: 95.25

PAVERS

CONCRETE

CONCRETE

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CONCRETE

BH 2-24
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(93.69)BH 2-24
93.69
(93.69)

- 450L (min.) BALANCING TANK c/w TIME OPERATED EFFLUENT 1/2 H.P. SIMPLEX PUMP
AND AUDIBLE / VISUAL HIGH WATER ALARM.
- TANK SHALL BE CPA APPROVED (OR ENGINEERED) FOR 1.2m (min.) OF COVER.
 - TANK SHALL BE REVIEWED FOR BALLASTING REQUIREMENTS.
 - POLY RISER AND COVER ASSEMBLY
 - INLET INV. = 94.17m
 - FINISHED GRADE = 95.15m

- 2 x 38mmØ PVC SCH 40 PIPE FORCEMAIN
- SHALL BE INSTALLED TO GRAVITY DRAIN TO THE TANK.
 - ENTIRE LENGTH OF FORCEMAIN SHALL BE BEDDED OF A MINIMUM OF 150mm OF
OPSS GRANULAR A, AND SHALL BE COVERED WITH A MINIMUM OF 300mm OF OPSS
GRANULAR A.
 - ALL GRANULAR A MATERIAL SHALL BE COMPACTED TO A MINIMUM OF 98% SPMDD.

- 100mmØ PERFORATED PVC SEPTIC
PIPE INSTALLED @ APPROX. 0.5%
ON ELJEN MODULES
HEAD INV. = 94.60m
FOOT INV. = 94.58m

- ELJEN SPECIFIED SAND AREA
- 630 mm THICK (TOP OF MODULE TO BASE)
 - 9.60m x 9.68m
 - FOLLOWED BY 300 mm THICK OF SAND/LIGNOCELLULOSE LAYER
 - FOLLOWED BY 50 mm THICK LAYER OF LIMESTONE

- NOTE:
INTERNAL GREASE TRAPS SHALL BE
PROVIDED ON KITCHEN FIXTURES.

- 2 x 38mmØ PVC SCH 40 PIPE FORCEMAIN
- SHALL BE INSTALLED TO GRAVITY DRAIN TO THE TANK.
 - ENTIRE LENGTH OF FORCEMAIN SHALL BE BEDDED OF A MINIMUM OF 150mm OF
OPSS GRANULAR A, AND SHALL BE COVERED WITH A MINIMUM OF 300mm OF OPSS
GRANULAR A.
 - ALL GRANULAR A MATERIAL SHALL BE COMPACTED TO A MINIMUM OF 98% SPMDD.

- 100mmØ PVC PIPE TO BE INSTALLED @ 2% (min.)
SLOPE AND SHALL BE SLEEVED THROUGH A 150mmØ
PVC SDR28 PIPE AND OVERLAIN BY 75mm T x 600mm W
RIGID INSULATION BOARDS UNDER ASPHALT.
OUTLET ELEV. @ PROPOSED BUILDING = 94.79m±

- NEW 28,101L PRETREATMENT TANK c/w
- TANK SHALL BE CPA APPROVED (OR ENGINEERED) FOR 1.2m (min.) OF COVER.
 - TANK SHALL BE REVIEWED FOR BALLASTING REQUIREMENTS
 - POLYLOK PL-525 EFFLUENT FILTER
 - POLY RISER & COVER ASSEMBLY (2)
 - INLET INV. = 94.50m±
 - OUTLET INV. = 94.45m±
 - TOP OF TANK = 94.80m±
 - FINISHED GRADE = 95.40m

- EXISTING DRILLED
WELL TO BE
DECOMMISSIONED

- EXISTING DRILLED
WELL
No. 5935
2 Storey
Block and Metal
Clad
Building

- EXISTING DRILLED
WELL
No. 5935
2 Storey
Block and Metal
Clad
Building

- EXISTING DRILLED
WELL
No. 5935
2 Storey
Block and Metal
Clad
Building

- EXISTING DRILLED
WELL
No. 5935
2 Storey
Block and Metal
Clad
Building

- EXISTING DRILLED
WELL
No. 5935
2 Storey
Block and Metal
Clad
Building

- EXISTING DRILLED
WELL
No. 5935
2 Storey
Block and Metal
Clad
Building

- EXISTING DRILLED
WELL
No. 5935
2 Storey
Block and Metal
Clad
Building

- EXISTING DRILLED
WELL
No. 5935
2 Storey
Block and Metal
Clad
Building

- EXISTING DRILLED
WELL
No. 5935
2 Storey
Block and Metal
Clad
Building

- EXISTING DRILLED
WELL
No. 5935
2 Storey
Block and Metal
Clad
Building

STRATFORD FOXRUN

PROPOSED WAREHOUSE / RESTAURANT
5923 OTTAWA STREET
OTTAWA (RICHMOND), ONTARIOSEWAGE SYSTEM LAYOUT PLAN
SEWAGE SYSTEM 'A' AND 'B'

Scale: 1:600
Date: 06/2025
Drawing no.: PH4924-1(rev.3)

Client: HV
Checked by: MK



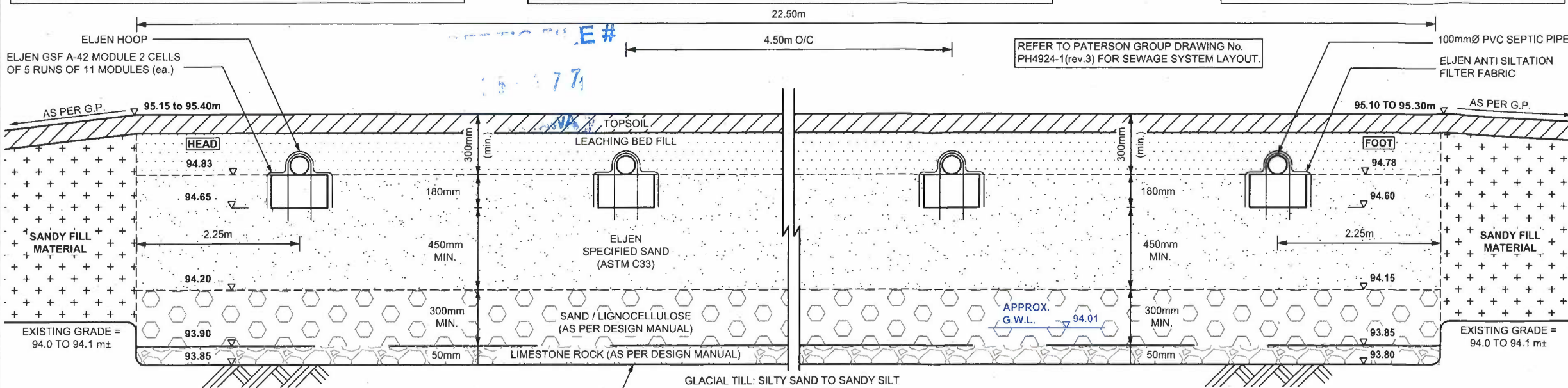
5 AURIGA DRIVE
OTTAWA, ON
K2E 7S8
TEL (613) 226-7351

| | | |
|----------|-------------------------------|------|
| 04/06/25 | Issued for Septic Permit | 3 |
| 14/05/25 | Issued with Revised Site Plan | 2 |
| 03/10/24 | Issued with Revised Site Plan | 1 |
| 20/09/24 | Issued for Preliminary Review | 0 |
| DD/MM/YY | Description | Rev. |

COVER MATERIAL TO CONSIST OF LEACHING BED FILL FOLLOWED BY APPROX. 100mm OF SANDY TOPSOIL. LEACHING BED TO BE VEGETATED AS SOON AS POSSIBLE.

SEWAGE SYSTEM DESIGN, SPECIFICATION, DETAILS AND NOTES HAVE BEEN COMPLETED IN ACCORDANCE WITH ELJEN DENITRIFICATION SUPPLEMENTAL DESIGN AND INSTALLATION MANUAL.

FINAL GRADING SHALL BE SUITABLY SHAPED TO DIRECT SURFACE WATER AWAY FROM THE PROPOSED SEWAGE SYSTEM.



NOTES:

1) ESTIMATE OF DAILY SEWAGE FLOW (Q)

THE PROPOSED SEWAGE SYSTEM HAS BEEN DESIGNED TO SUPPORT A COMMERCIAL TYPE USAGE CONSISTING OF OFFICE, STORE, WAREHOUSE AND RESTAURANT SPACE. THE DAILY DESIGN SEWAGE FLOW RATE IS CALCULATED IN ACCORDANCE WITH O.B.C. TABLE 8.2.1.3.B. **INTERNAL GREASE TRAP SHALL BE PROVIDED FOR KITCHEN FIXTURES.**

OFFICE SPACE:
• (70m² / 9.3) x 75 L/DAY = 565 L/DAY
STORE SPACE:
• 75.25m² x 5 L/DAY = 376.25 L/DAY
WAREHOUSE SPACE:
• 2 LOADING BAY x 150 L/DAY = 300 L/DAY
RESTAURANT/BAR:
65 SEATS x 125 L/DAY = 8,125 L/DAY

TOTAL DESIGN DAILY SANITARY SEWAGE FLOW = 9,367 L/DAY

2) SOIL CONDITIONS

SOILS INFORMATION GATHERED BY PATERSON GROUP INC. ON JUNE 17, 2024. REFER TO PATERSON GROUP REPORT PG7381-1 FOR FULL SOILS BREAKDOWN.

BH 4-24, ELEV. 94.11m

0-0.13 TOPSOIL AND ORGANICS
0.13-3.33 GLACIAL TILL: DENSE BROWN SILTY SAND, TO SANDY SILT WITH GRAVEL, COBBLES AND BOULDERS, SOME TO TRACE CLAY

- G.W.L. @ 0.10m DEPTH (94.01m)

3) PRETREATMENT TANK

- TANK SHALL BE CONNECTED TO BUILDING BY A 150mm Ø PVC PIPE SLEEVED THROUGH A 200mm Ø PVC SDR 28 PIPE AND OVERLAIN WITH 50mm T x 600mm W RIGID INSULATION BOARDS (UNDER ROADWAY) AND SHALL BE INSTALLED AT 2.0% (min.) SLOPE TO THE PRETREATMENT TANK.
- MINIMUM WORKING CAPACITY OF PRETREATMENT TANK = (3 x Q) = 3 x 9,367 L/DAY = 28,101 L (min.)
- IT IS RECOMMENDED THAT A NEW 28,101L (min.) TWO-COMPARTMENT SEPTIC TANK BE INSTALLED.
- AN OBC APPROVED EFFLUENT FILTER (I.E. POLYLOK PL-525 EFFLUENT FILTER, OR EQUIVALENT) SHALL BE INSTALLED ON THE OUTLET PIPE IN THE PRETREATMENT TANK.
- THE ACCESS LIDS TO THE TANK OPENINGS SHALL BE EXTENDED TO THE GROUND SURFACE. INSTALL RISERS AND COVERS TO SUIT.
- ACCESS LIDS SHALL INCLUDE SAFETY DEVICES AS PER CSA B66-21.
- TANK SHALL BE CPA APPROVED (OR ENGINEERED) FOR 1.2m (min.) OF COVER MATERIAL.
- TANK SHALL BE REVIEWED FOR BALLASTING REQUIREMENTS.

4) BALANCING TANK

- INSTALL A 18,500L (min.) BALANCING TANK IN SERIES AND DOWNSTREAM FROM THE NEW SEPTIC TANK.
- A TIME OPERATED ALTERNATING DUPLEX PUMPING SYSTEM (I.E. MYERS ME3F, OR SIMILAR) AND A HIGH WATER ALARM SHALL BE INSTALLED IN THE BALANCING TANK.
- THE TIME OPERATIONAL PUMPING SYSTEM SHALL OPERATE EVERY HOUR (I.E. 391 L/DUSE + VOLUME TO CHARGE THE SYSTEM) AND SHALL ALTERNATE BETWEEN EACH CELL.
- A 3mm Ø DRAIN HOLE SHALL BE INSTALLED IN THE UNDERSIDE OF THE FORCEMAIN IN THE BALANCING TANK NEAR THE WALL CONNECTION.
- RISERS WITH A COVER SHALL BE INSTALLED OVER THE BALANCING TANK TO PROVIDE ACCESS FROM THE GROUND SURFACE.
- DISCHARGE PIPING FOR PUMP SHALL BE CONFIGURED SUCH THAT THE PUMP IS EASILY SERVICED FROM THE GROUND SURFACE.

5) DISTRIBUTION BOX / FORCEMAIN

- A 38mm Ø (NOMINAL) PVC SCH 40 FORCEMAIN (2) SHALL BE USED TO CARRY THE EFFLUENT FROM THE BALANCING TANK TO EACH 3m L x 100mm Ø PVC SEWER PIPE.
- 100mm SEWER PIPE SHALL DRAIN BY GRAVITY TO A 5 OUTLET DISTRIBUTION BOX.
- THE FORCE MAIN SHALL BE INSTALLED TO GRAVITY DRAIN TO THE BALANCING TANK.
- THE FORCE MAIN SHALL BE OVERLAIN WITH 50mm T x 600mm CW RIGID INSULATION.
- THE DISTRIBUTION BOX SHALL BE EQUIPPED WITH AN INLET Baffle AND OUTLET PIPES (5).
- EACH PIPING RUN SHALL BE FED BY A 5 OUTLET DISTRIBUTION BOX.
- THE DISTRIBUTION BOX SHALL BE CONNECTED TO THE DISTRIBUTION PIPING RUNS USING 100mm Ø SOLID PVC SEWER PIPE @ 2% (min.) SLOPE.

6) LEACHING BED SIZING CRITERIA

- NO. OF MODULES REQUIRED = Q/95 = 9,367/95 = 98.6 MODULES
- USE 2 CELLS OF 5 RUNS OF 11 (110) ELJEN GSF A-42 MODULES EACH
- SAND AREA REQUIRED = Q/400 = 9,367/(35)/400 = 819.7m²
- SAND AREA PROVIDED = 37.24m x 22.50m = 837.90m² (min.)

7) LEACHING BED CONSTRUCTION GUIDELINES

- REMOVE ALL EXISTING TOPSOIL, AND ANY FILL WITHIN LIMITS OF THE SAND AREA AND SUBEXCAVATE TO AT LEAST ELEVATION 93.80m TO 93.85m, WHICHEVER IS GREATER. RE-ESTABLISH THE SPECIFIED CONTACT LEVEL USING SELECT SAND FILL, WHERE REQUIRED.
- THE SUBGRADE SURFACE SHALL BE SCARIFIED, **UNDER DRY CONDITIONS**.
- PLACE A 50mm MIN. THICK LAYER OF LIMESTONE ROCK OVER THE SUITABLY PREPARED SUBGRADE.
- LIMESTONE ROCK SHALL NO SMALLER THAN 25mm IN DIAMETER UP TO 50mm IN DIAMETER. THE ROCK SHALL CONTAIN GREATER THAN 15% LIMESTONE AS PER ELJEN DENITRIFICATION SUPPLEMENTAL DESIGN AND INSTALLATION MANUAL.
- PLACE A 300mm THICK LAYER OF SAND / LIGNOCELLULOSE OVER THE LIMESTONE ROCK LAYER.
- SAND / LIGNOCELLULOSE SHALL CONSIST OF WOOD CHIPS OR SAW DUST FROM HARD WOOD TREES THAT HAVE NOT BEEN FURTHER PROCESSED BY CHEMICALS. THE 300mm SAND AND LIGNOCELLULOSE LAYER SHALL BE 50/50 EQUAL MIXTURE OF ASTM C33 SAND AND WOOD CHIPS FROM HARD WOOD TREES. THE MIXTURE MUST NOT EXCEED 60/40 IN FAVOR OF THE MORE WOOD TO SAND.
- PLACE A 450mm MIN. THICK LAYER OF ELJEN SPECIFIED SAND FILL OVER THE LEACHING BED FILL.
- THE ELJEN SPECIFIED SAND FILL SHALL CONSIST OF WASHED SAND MEETING THE REQUIREMENTS OF ASTM C33 "STANDARD SPECIFICATION FOR CONCRETE AGGREGATES" WITH LESS THAN 5% PASSING 0.075mm SIEVE. ELJEN SPECIFIED SAND FILL SHALL BE PRE-APPROVED BY THE CONSULTANT.
- THE MODULES SHALL BE INSTALLED IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS.
- THE MODULES SHALL BE INSTALLED AT A SLOPE OF 0.3% (min.) TO 0.5% (max.), END TO END AND WITH THE WHITE DEMARCATION LINE FACING UP.
- THE MODULAR BASE LEVEL (ELEV. 94.60m AT THE FOOT, TO 94.65m AT THE HEAD) SHALL BE ESTABLISHED WITH ELJEN SPECIFIED SAND FILL, HAVING A MINIMUM THICKNESS OF 450mm BELOW THE MODULES.
- THE ELJEN MODULES SHALL BE FED BY GRAVITY BY A 100mm Ø PVC SEWER PIPE @ 2% (min.) SLOPE FROM THE DISTRIBUTION BOX
- THE DISTRIBUTION PIPE SHALL CONSIST OF A 100mm Ø PERFORATED PVC PIPE CENTRED OVER THE MODULES. THE PIPE SHALL BE SECURED TO THE TOP OF THE MODULES USING AN ELJEN HOOP (MINIMUM 1 HOOP PER MODULE).
- THE INVERT LEVEL OF THE DISTRIBUTION PIPE SHALL BE SET ON THE MODULES AT ELEVATION 94.78m AT THE FOOT TO 94.83m AT THE HEAD. THE END OF THE PIPE RUNS SHALL BE CONNECTED TO A 100mm Ø SOLID PVC FOOTER PIPE
- INSTALL ELJEN SYSTEM SAMPLING DEVICE AS PER MANUFACTURER'S RECOMMENDATIONS.
- THE ELJEN ANTI-SILTATION FILTER FABRIC SHALL BE SPREAD LENGTHWISE OVER THE PERFORATED SEPTIC PIPE AND DOWN THE SIDES OF THE MODULES. ENSURE ENDS OF MODULES ARE ALSO COVERED WITH FABRIC.
- THE MODULES SHALL BE BACKFILLED, WITH ELJEN SPECIFIED SAND FILL TO AT LEAST THE TOP OF THE ELJEN MODULES, FOLLOWED BY 200mm (min.) OF LEACHING BED FILL, FOLLOWED BY 100mm OF SANDY TOPSOIL, WITHIN THE LIMITS OF THE SAND AREA. THE BED AREA SHOULD BE VEGETATED AS SOON AS POSSIBLE.
- LEACHING BED SAND FILL SHALL BE UNIFORM SAND WITH GRADING LIMITS SIMILAR TO 100% PASSING 13.2mm SIEVE, LESS THAN 5% PASSING 0.075mm SIEVE, AND HAVING A PERCOLATION TIME OF 6 TO 8 min/cm. LEACHING BED FILL SHALL BE PRE-APPROVED BY THE CONSULTANT.

- THE SIDES OF THE BED SHOULD BE SLOPED AT 3H:1V OR SHALLOWER.
- VENT SYSTEM SHALL BE INSTALLED ON THE FOOTER PIPE. CONNECT A 100mm Ø PVC VENT PIPE TO FOOTER PIPE, EXTENDING TO GROUND SURFACE. VENT PIPE TO BE INSTALLED IN 150mm Ø LANDSCAPE VALVE COVER.

8) MINIMUM CLEARANCE DISTANCE FROM DISTRIBUTION PIPE

- 5.6m FROM ANY PROPERTY LINE
- 7.6m FROM ANY STRUCTURE: 5.0m FROM ANY BASEMENTLESS STRUCTURE
- 17.6m FROM ANY DRILLED WELL
- 5.0m FROM ANY TREE (UNLESS OTHERWISE APPROVED)

9) MINIMUM CLEARANCE DISTANCE FROM TANK(S)

- 1.5m FROM ANY STRUCTURE
- 15.0m FROM ANY DRILLED OR DUG WELL
- 3.0m FROM ANY PROPERTY LINE

10) GENERAL

- SNOW STORAGE SHALL NOT BE LOCATED OVER OR UPGRADIENT OF THE PROPOSED SEWAGE SYSTEM.**
- THE SEWAGE SYSTEM HAS NOT BEEN DESIGNED TO SUPPORT TRAFFIC LOADING.
- THE BACKFILLING OF THE SEWAGE SYSTEM SHOULD MINIMIZE THE RISK OF OVER COMPACTION WITH THE USE RUBBER TRACKED EQUIPMENT AND BY AVOIDING THE CREATION OF ANY CONSTRUCTION ROUTES OR PATHWAYS OVER THE SYSTEM.
- ANY NEW IRRIGATION / SPRINKLER SYSTEM SHOULD NOT BE USED IN PROXIMITY OF THE PROPOSED SEWAGE SYSTEM.
- ENSURE WALKWAYS AND/OR SHURBBERY ARE NOT PLACED WITHIN PROXIMITY OF THE TANKAGE.
- THE BACKWASH WATERS FROM ANY WATER TREATMENT UNIT, SUCH AS WATER SOFTENER, SHOULD NOT DISCHARGE INTO THE SEWAGE SYSTEM.
- THE SEWAGE SYSTEM HAS NOT BEEN DESIGNED FOR THE USE OF A GARBAGE DISPOSAL.
- SEWAGE SYSTEM INSTALLER SHALL BE QUALIFIED AND REGISTERED UNDER PART 8 OF THE ONTARIO BUILDING CODE AND SHALL BE AN AUTHORIZED ELJEN TREATMENT SYSTEM INSTALLER.
- ALL WORK SHALL BE CARRIED OUT IN ACCORDANCE WITH THE LATEST BY-LAWS, CODES AND REGULATIONS.
- CONTRACTOR SHALL REVIEW DRAWINGS IN DETAIL AND SHALL INFORM THE CONSULTANT OF ANY ERRORS AND/OR OMISSIONS ON DESIGN DRAWINGS IMMEDIATELY.
- CONTRACTOR SHALL BE RESPONSIBLE TO LOCATE AND PROTECT ALL EXISTING UNDERGROUND SERVICES.
- CONTRACTOR SHALL VISIT THE SITE AND REVIEW ALL DOCUMENTATION TO BECOME FAMILIAR WITH THE SITE AND SUBSURFACE SOIL CONDITIONS TO DETERMINE SUITABLE METHODS OF CONSTRUCTION.
- THE MANUFACTURER PROVIDES A LIMITED WARRANTY OF THE SYSTEM COMPONENTS. THE OWNER OF THE SYSTEM MUST SIGN A MAINTENANCE AGREEMENT WITH THE MANUFACTURER'S REPRESENTATIVE. THE HOMEOWNER IS RESPONSIBLE FOR THE ANNUAL FEES ASSOCIATED WITH THE MAINTENANCE.
- THE FIRM OF PATERSON GROUP INC. HAS PROVIDED DESIGN SERVICES ONLY FOR THE SUBJECT SEWAGE SYSTEM. THE DESIGN HAS BEEN CARRIED OUT IN ACCORDANCE WITH THE MANUFACTURER'S GUIDELINES AND OUR INTERPRETATION OF PART 8 OF THE ONTARIO BUILDING CODE.
- INSPECTIONS BY THE CONSULTANT DURING THE INSTALLATION OF THE SYSTEM IS A REQUIREMENT OF SOME REGULATING AUTHORITIES AND IS STRONGLY RECOMMENDED BY THIS FIRM.
- THE PROPERTY LINE / SEPARATION DISTANCES SHOULD BE CONFIRMED PRIOR TO CONSTRUCTION.
- CONSTRUCTION INSPECTIONS DURING THE INSTALLATION OF THE SEWAGE SYSTEM MAY BE REQUIRED BY THE REGULATING AUTHORITY AND ARE STRONGLY RECOMMENDED BY THIS FIRM. IF THIS FIRM IS TO COMPLETE ANY CONSTRUCTION INSPECTION(S), ADDITIONAL FEES MAY BE APPLIED. CONFIRMATION OF PAYMENT WILL BE REQUIRED PRIOR TO THE INSPECTION.
- THE TEST HOLE INFORMATION PROVIDED, IS INTENDED TO BE USED FOR DESIGN PURPOSES ONLY, AND SHOULD NOT BE RELIED UPON FOR CONSTRUCTION PURPOSES. IF DISCREPANCIES ARE FOUND DURING THE CONSTRUCTION PROCESS, IT IS THE CLIENT'S RESPONSIBILITY TO CONTACT THIS FIRM TO MAKE ANY NECESSARY COMMENTS OR REVISIONS. ADDITIONAL REVISIONS ARE NOT CONSIDERED PART OF THE DESIGN WORKS AND WILL BE CONSIDERED AS AN ADDITIONAL COST.

SEPTIC FILE #
25-176
OTTAWA



Professional Engineers
Ontario

Licensed Engineering Technologist

Name: H. G. VAN DE GLIND

Number: 100647862

Limitations: Inspecting, designing, and assessing residential and commercial sewage systems, grading designs and soil analysis, and overseeing installation and compliance.

Association of Professional Engineers of Ontario

| | | |
|----------|-------------------------------|------|
| 04/06/25 | Issued for Septic Permit | 3 |
| 14/05/25 | Issued with Revised Site Plan | 2 |
| 03/10/24 | Issued with Revised Site Plan | 1 |
| 20/09/24 | Issued for Preliminary Review | 0 |
| DD/MM/YY | DESCRIPTION | REV. |

Consultant:



PATERSON
GROUP

5 AURIGA DRIVE
OTTAWA, ON
K2E 7S9
TEL (613) 226-7361

Client:

STRATFORD FOXRUN

Project:

PROPOSED WAREHOUSE /
RESTAURANT

5923 OTTAWA STREET
OTTAWA (RICHMOND), ONTARIO

Drawing:

SEWAGE SYSTEM
DETAILS AND NOTES
SEWAGE SYSTEM 'A'

Scale:

N.T.S.

Drawn by:

HV

Date:

06/2025

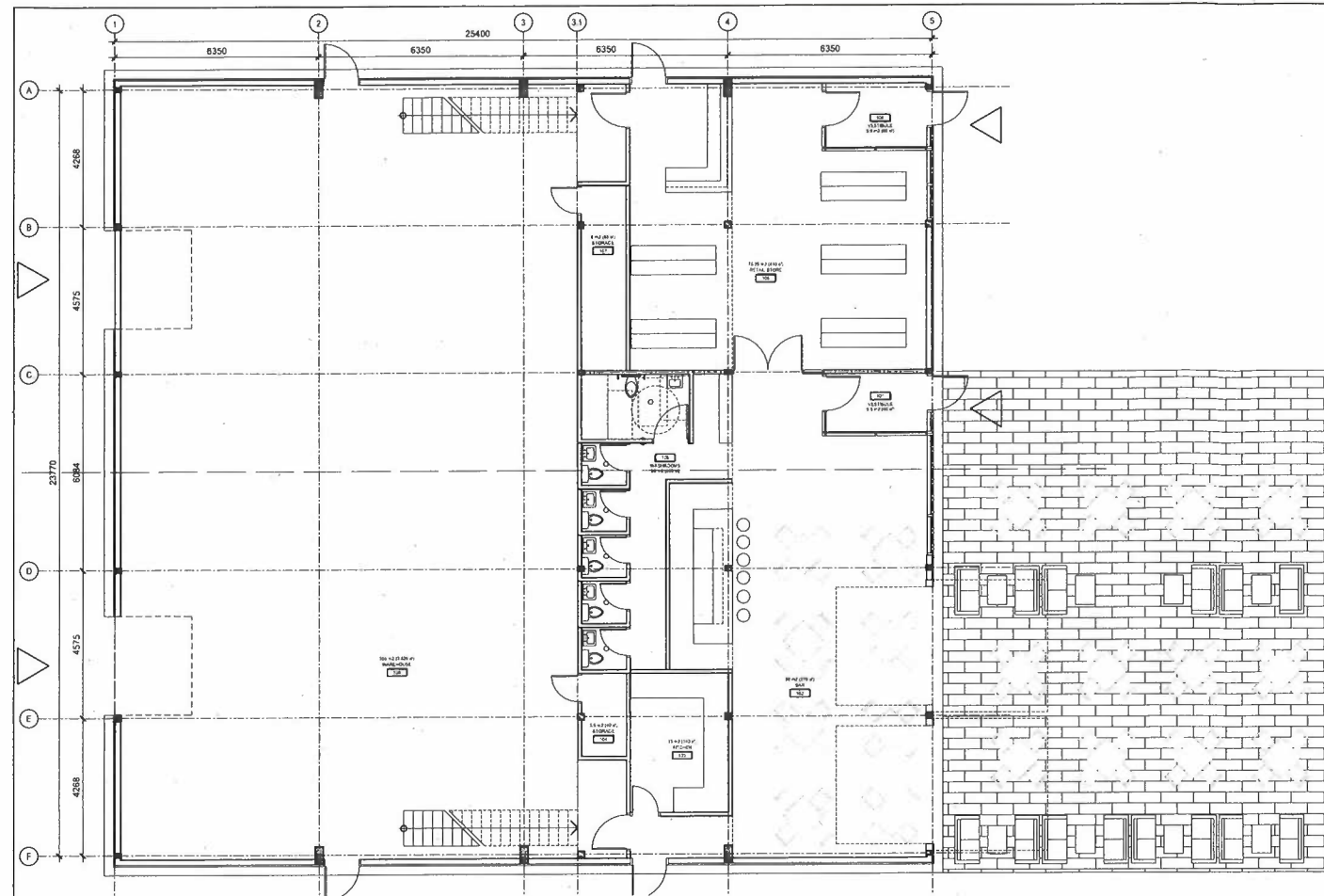
Checked by:

MK

Drawing No.:

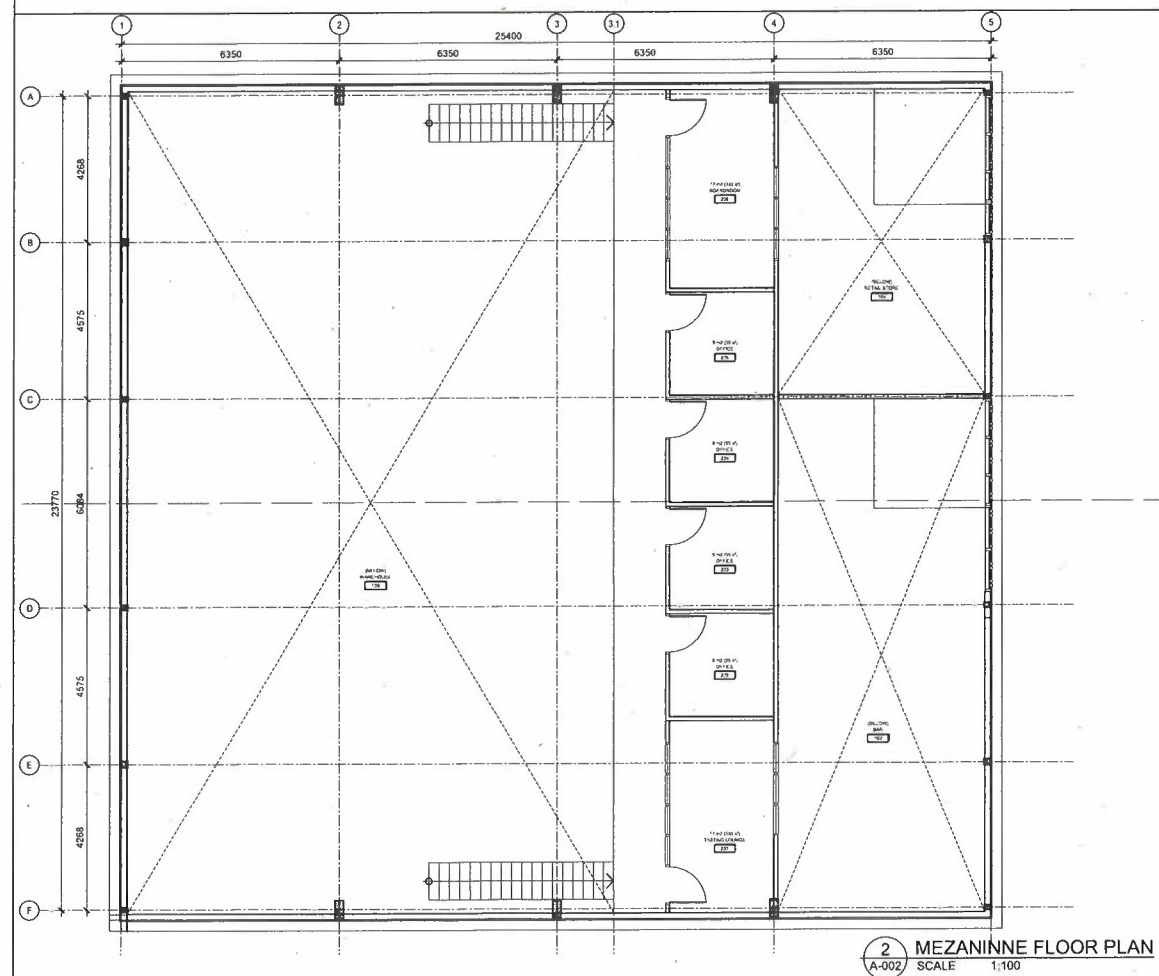
PH4924-2(rev.3)

p:\autocad drawings\hydrogeology\ph4924-2 - stratford foxrun -
jack gulas - 5923 ottawa street richmond\ph4924-2(rev.3).dwg

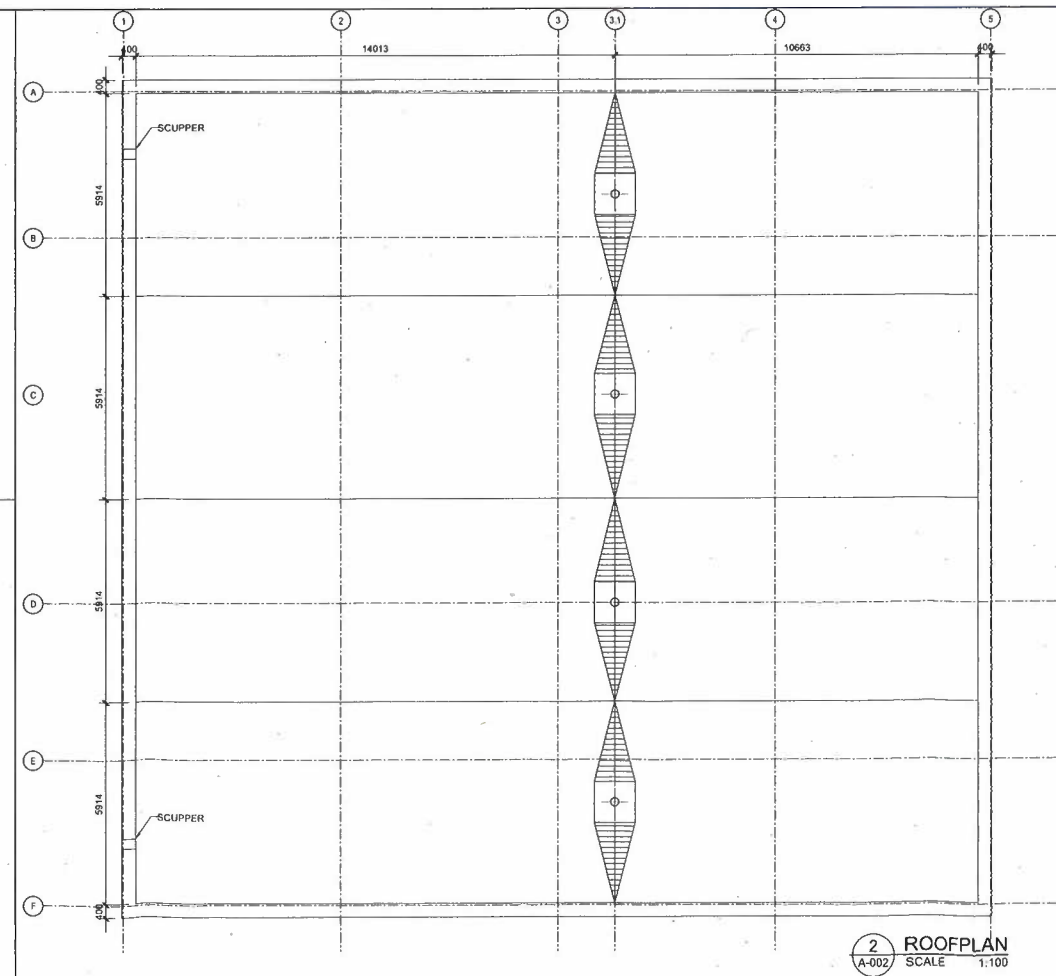


1 GROUND FLOOR PLAN
A-002 SCALE 1:100

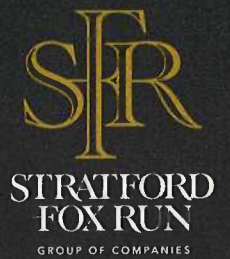
BUILDING 1
SEWAGE SYSTEM "A"
25-176



2 MEZANINNE FLOOR PLAN
A-002 SCALE 1:100



2 ROOFPLAN
A-002 SCALE 1:100



| | | |
|-----|------------------------------|---------|
| 3 | ISSUED FOR SPA | 08MAY25 |
| 2 | ISSUED FOR SITE PLAN CONTROL | 19NOV24 |
| 1 | ISSUED FOR SITE PLAN CONTROL | 07OCT24 |
| no. | revision | date |

N45 ARCHITECTURE INC.
71 Bank Street, 7th floor - Ottawa, Ontario, K1P 5N2
tel. 613.224.0095 fax 613.224.9811

project
FOXRUN RICHMOND

5923 OTTAWA STREET
OTTAWA, ON

project north



drawing title
FLOOR PLANS

| | |
|--------------------------|--------------------------------|
| scale AS NOTED | drawn by NF |
| date OCT 2022 | checked by VP |
| project number 24-826 | drawing number A-002 |

CONTRACTOR TO VERIFY ALL DIMENSIONS
AND NOTIFY THE ARCHITECT OF ANY
DISCREPANCIES BEFORE WORK COMMENCES.
DO NOT SCALE DRAWINGS.

revision
-



Permit
Part 8 – Sewage System
Ontario Building Code

| |
|---------------------|
| Do Not Complete |
| Permit No 25-176 |
| Revision No |
| Date |
| Related Application |

A copy of this permit must be posted on the property at all time during construction. OBC, Division C — Part 1, Section 1.3.2.1
This permit verifies that the on-site sewage system was reviewed and approved for construction under the Ontario Building Code Act (Building Code Act, 1992, S.O. 1992, c. 23) and Ontario Building Code (O. Reg. 163/24) as amended.

| | | | |
|--------------------------------|-------------------------------|----------|----------------------|
| Inspected & Recommended by: | Matt Panciuk | Owner: | 99117756 Canada Inc. |
| Inspection Date & Time: | | Weather: | |
| Address: | 5923 Ottawa Street - System A | Legal: | |
| In the former Township/City of | Goulbourn | | |

Design Flow for Commercial / Institutional / Industrial (as per Table 8.2.13.B)

| | | |
|----|-------|-------|
| Q: | 9,367 | L/day |
|----|-------|-------|

| | | | | | |
|-----------------|-----------------------|----------|------------------------------|---|--|
| septic tank | 28,101(min) | L | weigh bills for Eljen Sand | <input checked="" type="checkbox"/> yes | <input type="checkbox"/> no |
| effluent filter | Required | | grain size analysis required | <input checked="" type="checkbox"/> yes | <input type="checkbox"/> no |
| pump rate | 391 + Charge | L/15 MIN | site to be scarified | <input checked="" type="checkbox"/> yes | <input type="checkbox"/> no |
| treatment unit | Eljen GSF A42(DN 450) | | clay seal inspection | <input type="checkbox"/> yes | <input checked="" type="checkbox"/> no |
| number of units | 110 | | mantle required | <input type="checkbox"/> yes | <input checked="" type="checkbox"/> no |
| | | | sub-grade inspection | <input checked="" type="checkbox"/> yes | <input type="checkbox"/> no |

ELEVATION ☐ In Ground ☐ Partially Raised ☒ Fully Raised

TYPE OF SYSTEM

- ☐ Trench
☒ Pipe and Stone or ☐ Chambers

type of chamber _____

loading area _____ m²

total trench length _____ m

trench configuration _____

☒ Dispersal Bed

- ☒ BMEC ☐ Type A ☐ Type B

stone _____ m²

sand 837.9 m²

pipe 2 cells of 5 runs of 11 modules @ 4.5m o/c

weight of sand _____ kg

☐ Shallow Buried Trench

pipe length _____ m

orifice spacing _____ m

☐ Filter Media Bed

stone _____ m²

extended base _____ m²

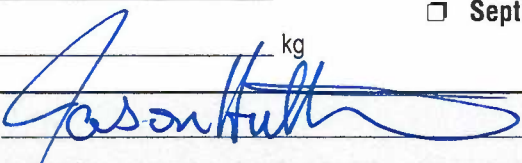
pipe _____

weight of filter media _____ kg

loading area _____ m²

☐ Class 5 Holding Tank

☐ Septic Tank Only

Manager, Septic System Approvals:  Permit Date: August 5, 2025

Comments: 1. Scarification inspection required prior to placement of sand fill.
2. One existing monitoring well and one existing drilled well to be decommissioned on site by a licensed well driller and documentation of the decommissioned wells provided to the RVCA.

- | | | |
|--|---|--|
| <input checked="" type="checkbox"/> maintenance/pumping required | <input checked="" type="checkbox"/> ESA permit # required | <input type="checkbox"/> engineer to verify |
| <input type="checkbox"/> Class 5 Holding Tank approval only valid for three years from date of issue | | <input checked="" type="checkbox"/> subgrade |
| | | <input type="checkbox"/> squirt height |

Manager, Septic System Approvals: _____ Revision Date: _____

Comments: _____

Application for a Permit to Construct or Demolish

This form is authorized under subsection 8(1.1) of the *Building Code Act, 1992*

| | | | |
|---|-------------|---|------------------------------|
| For use by Principal Authority | | | |
| Application number: | | Permit number (if different): | |
| Date received: | | Roll number: | |
| Application submitted to: Ottawa Septic System Office | | <div style="border: 2px solid blue; padding: 5px; display: inline-block;"> RVCA RECEIVED JUN 09 2025 REFER TO: </div> <div style="color: blue; font-weight: bold; margin-left: 20px;"> SEPTIC FILE # 25-177 OTTAWA </div> | |
| (Name of municipality, upper-tier municipality, board of health or conservation authority) | | | |
| A. Project information | | | |
| Building number, street name | | Unit number | Lot/con. |
| 5923 Ottawa street | | | |
| Municipality | Postal code | Plan number/other description | |
| Ottawa (Richmond) | K0A 2Z0 | | |
| Project value est. \$ | | Area of work (m ²) | |
| | | | |
| B. Purpose of application | | | |
| <input checked="" type="checkbox"/> New construction <input type="checkbox"/> Addition to an existing building <input type="checkbox"/> Alteration/repair <input type="checkbox"/> Demolition <input type="checkbox"/> Conditional Permit | | | |
| Proposed use of building | | Current use of building | |
| Commercial | | | |
| Description of proposed work | | | |
| To construct a new class 4 sewage system, Eljen NSF 245 Denitrification treatment system: Eljen DN450 | | | |
| Sewage System 'B' | | | |
| C. Applicant | | | |
| Applicant is: <input type="checkbox"/> Owner or <input checked="" type="checkbox"/> Authorized agent of owner | | | |
| Last name | First name | Corporation or partnership | |
| Van de Glind | Hendrik | Paterson Group Inc. | |
| Street address | | Unit number | Lot/con. |
| 9 Auriga Drive | | | |
| Municipality | Postal code | Province | E-mail |
| Ottawa | K2E 7T9 | ON | hvandeglind@patersongroup.ca |
| Telephone number | Fax | Cell number | |
| 613-226-7381 | | | |
| D. Owner (if different from applicant) | | | |
| Last name | First name | Corporation or partnership | |
| Gulas | Jack | 99117756 Canada Inc. | |
| Street address | | Unit number | Lot/con. |
| 411 Legget Drive, Suite 710 | | | |
| Municipality | Postal code | Province | E-mail |
| Ottawa | K2K 3C9 | ON | jack@stratfordfoxrun.com |
| Telephone number | Fax | Cell number | |
| 613.862.0087 | | | |

| E. Builder (optional) | | | |
|------------------------------|-------------|--|----------|
| Last name | First name | Corporation or partnership (if applicable) | |
| Street address | | Unit number | Lot/con. |
| Municipality | Postal code | Province | E-mail |
| Telephone number | Fax | Cell number | |

SEPTIC FILE #
 25-177
 P.A.W.A.

| F. Tarion Warranty Corporation (Ontario New Home Warranty Program) | | | |
|--|------------------------------|--|--|
| i. Is proposed construction for a new home as defined in the <i>Ontario New Home Warranties Plan Act</i> ? If no, go to section G. | <input type="checkbox"/> Yes | <input checked="" type="checkbox"/> No | |
| ii. Is registration required under the <i>Ontario New Home Warranties Plan Act</i> ? | <input type="checkbox"/> Yes | <input checked="" type="checkbox"/> No | |
| iii. If yes to (ii) provide registration number(s): _____ | | | |

| G. Required Schedules | |
|--|--|
| i) Attach Schedule 1 for each individual who reviews and takes responsibility for design activities. | |
| ii) Attach Schedule 2 where application is to construct on-site, install or repair a sewage system. | |

| H. Completeness and compliance with applicable law | | |
|---|---|-----------------------------|
| i) This application meets all the requirements of clauses 1.3.1.3 (5) (a) to (d) of Division C of the Building Code (the application is made in the correct form and by the owner or authorized agent, all applicable fields have been completed on the application and required schedules, and all required schedules are submitted). Payment has been made of all fees that are required, under the applicable by-law, resolution or regulation made under clause 7(1)(c) of the <i>Building Code Act, 1992</i> , to be paid when the application is made. | <input checked="" type="checkbox"/> Yes | <input type="checkbox"/> No |
| ii) This application is accompanied by the plans and specifications prescribed by the applicable by-law, resolution or regulation made under clause 7(1)(b) of the <i>Building Code Act, 1992</i> . | <input checked="" type="checkbox"/> Yes | <input type="checkbox"/> No |
| iii) This application is accompanied by the information and documents prescribed by the applicable by-law, resolution or regulation made under clause 7(1)(b) of the <i>Building Code Act, 1992</i> which enable the chief building official to determine whether the proposed building, construction or demolition will contravene any applicable law. | <input checked="" type="checkbox"/> Yes | <input type="checkbox"/> No |
| iv) The proposed building, construction or demolition will not contravene any applicable law. | <input checked="" type="checkbox"/> Yes | <input type="checkbox"/> No |

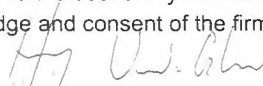
| I. Declaration of applicant | |
|---|--|
| <div style="display: flex; justify-content: space-between; align-items: flex-start;"> <div style="width: 60%;"> <p style="font-size: 1.2em; margin: 0;">Hendrik Van de Glind, L.E.T., C.E.T. - Paterson Group</p> <p style="font-size: 0.8em; margin: 5px 0;">(print name)</p> </div> <div style="width: 35%; text-align: right;"> <p style="margin: 0;">declare that:</p> </div> </div> <div style="margin-top: 10px;"> <p>1. The information contained in this application, attached schedules, attached plans and specifications, and other attached documentation is true to the best of my knowledge.</p> <p>2. If the owner is a corporation or partnership, I have the authority to bind the corporation or partnership.</p> </div> <div style="display: flex; justify-content: space-between; margin-top: 10px;"> <div style="width: 30%;"> <p style="font-size: 1.1em; margin: 0;">June 6, 2025</p> <p style="font-size: 0.8em; margin: 5px 0;">Date</p> </div> <div style="width: 60%; text-align: center;"> <p style="font-size: 0.8em; margin: 5px 0;">Signature of applicant</p> </div> </div> | |

RVCA RECEIVED
 JUN 09 2025
 REFER TO: _____

Personal information contained in this form and schedules is collected under the authority of subsection 8(1.1) of the *Building Code Act, 1992*, and will be used in the administration and enforcement of the *Building Code Act, 1992*. Questions about the collection of personal information may be addressed to: a) the Chief Building Official of the municipality or upper-tier municipality to which this application is being made, or, b) the inspector having the powers and duties of a chief building official in relation to sewage systems or plumbing for an upper-tier municipality, board of health or conservation authority to whom this application is made, or, c) Director, Building and Development Branch, Ministry of Municipal Affairs and Housing 777 Bay St., 2nd Floor. Toronto, M5G 2E5 (416) 585-6666.

Schedule 1: Designer Information

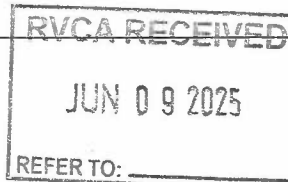
Use one form for each individual who reviews and takes responsibility for design activities with respect to the project.

| A. Project Information | | | |
|--|------------------------|---|--|
| Building number, street name 5923 Ottawa Street | | Unit no. | Lot/con. |
| Municipality Ottawa (Richmond) | Postal code K0A 2Z0 | Plan number/ other description | |
| B. Individual who reviews and takes responsibility for design activities | | | |
| Name Hendrik Van de Glind, L.E.T., C.E.T. | | Firm Paterson Group Inc. | |
| Street address 9 Auriga Drive | | Unit no. | Lot/con. |
| Municipality Ottawa | Postal code K2E 7T9 | Province ON | E-mail hvandeglind@patersongroup.ca |
| Telephone number 613-226-7381 | Fax number | Cell number | |
| C. Design activities undertaken by individual identified in Section B. [Building Code Table 3.5.2.1. of Division C] | | | |
| <div style="display: flex; justify-content: space-between;"> <div style="width: 30%;"> <input type="checkbox"/> House <input type="checkbox"/> Small Buildings <input type="checkbox"/> Large Buildings <input type="checkbox"/> Complex Buildings </div> <div style="width: 30%;"> <input type="checkbox"/> HVAC – House <input type="checkbox"/> Building Services <input type="checkbox"/> Detection, Lighting and Power <input type="checkbox"/> Fire Protection </div> <div style="width: 30%;"> <input type="checkbox"/> Building Structural <input type="checkbox"/> Plumbing – House <input type="checkbox"/> Plumbing – All Buildings <input checked="" type="checkbox"/> On-site Sewage Systems </div> </div> | | | |
| Description of designer's work On-site Sewage System Design | | | |
| D. Declaration of Designer | | | |
| I, <u>Hendrik Van de Glind, L.E.T., C.E.T. - Paterson Group</u> declare that (choose one as appropriate): (print name) | | | |
| I review and take responsibility for the design work on behalf of a firm registered under subsection 3.2.4. of Division C, of the Building Code. I am qualified, and the firm is registered, in the appropriate classes/categories. | | | |
| Individual BCIN: <u>111499</u> | | | |
| Firm BCIN: <u>29346</u> | | | |
| I review and take responsibility for the design and am qualified in the appropriate category as an "other designer" under subsection 3.2.5. of Division C, of the Building Code. | | | |
| Individual BCIN: _____ | | | |
| Basis for exemption from registration: _____ | | | |
| The design work is exempt from the registration and qualification requirements of the Building Code. | | | |
| Basis for exemption from registration and qualification: _____ | | | |
| I certify that: | | | |
| 1. The information contained in this schedule is true to the best of my knowledge. | | | |
| 2. I have submitted this application with the knowledge and consent of the firm. | | | |
| June 6, 2025 Date | |  Signature of Designer | |

SEPTIC FILE #

25 - 177

OTTAWA



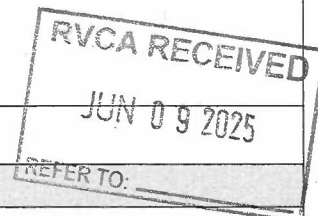
NOTE:

- For the purposes of this form, "individual" means the "person" referred to in Clause 3.2.4.7(1) (c) of Division C, Article 3.2.5.1. of Division C, and all other persons who are exempt from qualification under Subsections 3.2.4. and 3.2.5. of Division C.
- Schedule 1 is not required to be completed by a holder of a license, temporary license, or a certificate of practice, issued by the Ontario Association of Architects. Schedule 1 is also not required to be completed by a holder of a license to practise, a limited license to practise, or a certificate of authorization, issued by the Association of Professional Engineers of Ontario.



Schedule 2: Sewage System Installer Information

| | | | |
|---|---------------------|--|----------|
| A. Project Information | | | |
| Building number, street name 5923 Ottawa Street | | Unit number | Lot/con. |
| Municipality Ottawa (Richmond) | Postal code K0A 2Z0 | Plan number/ other description | |
| B. Sewage system installer | | | |
| Is the installer of the sewage system engaged in the business of constructing on-site, installing, repairing, servicing, cleaning or emptying sewage systems, in accordance with Building Code Article 3.3.1.1, Division C? | | | |
| <input type="checkbox"/> Yes (Continue to Section C) | | <input type="checkbox"/> No (Continue to Section E) | |
| | | <input checked="" type="checkbox"/> Installer unknown at time of application (Continue to Section E) | |
| C. Registered installer information (where answer to B is "Yes") | | | |
| Name | | BCIN | |
| Street address | | Unit number | Lot/con. |
| Municipality | Postal code | Province | E-mail |
| Telephone number | Fax | Cell number | |
| D. Qualified supervisor information (where answer to section B is "Yes") | | | |
| Name of qualified supervisor(s) | | Building Code Identification Number (BCIN) | |
| | | | |
| E. Declaration of Applicant: | | | |
| I <u>Hendrik Van de Glind, L.E.T., C.E.T. - Paterson Group</u> declare that: | | | |
| (print name) | | | |
| I am the applicant for the permit to construct the sewage system. If the installer is unknown at time of application, I shall submit a new Schedule 2 prior to construction when the installer is known; | | | |
| OR | | | |
| I am the holder of the permit to construct the sewage system, and am submitting a new Schedule 2, now that the installer is known. | | | |
| I certify that: | | | |
| 1. The information contained in this schedule is true to the best of my knowledge. | | | |
| 2. If the owner is a corporation or partnership, I have the authority to bind the corporation or partnership. | | | |
| June 6, 2025 | | Signature of applicant | |
| Date | | OTTAWA | |



SEPTIC FILE #
25-177
OTTAWA



Schedule 4: Proposed Services

Complete Sections 1 through 7

Do Not Complete

Permit number:

Revision number:

Date

1 Engineered

- ☒ Yes
☐ No

2 Water supply

- ☒ Proposed
☐ Existing

3 Use

- ☐ Apartment
☒ Dwelling
☒ Commercial
☐ Industrial

SEPTIC FILE #
25-177

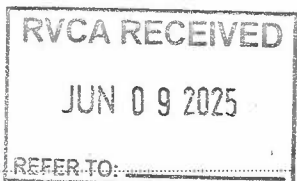
OTTAWA

4 Type of work proposed

- ☒ New Installation
☐ Replacement
☐ Alteration

5 Type of Well

- ☐ Dug/Bored/Sandpoint well
☒ Drilled well
☐ Municipal
☐ Other



6 Residential Sewage Design Flow Info.

Bedrooms _____
House (floor area) _____ m²
People _____
Total Fixture Units _____ (Schedule 8)
Residential Flow _____ L/day

7 Sewage Design Flow Other Occupancies

Design Flow 600 L/day

Detailed sewage flow calculations:

Refer to PGI Drawings No. PH4924-3(rev.3)

8 Type of System

- ☐ Class 2 – Leaching Pit
☐ Class 3 – Cesspool

Treatment Unit Eljen GSF A-42 (DN450)

☐ Class 4 – Trench (Schedule 9)

- ☐ Fully raised
☐ Partially raised
☐ In-ground

☐ Class 4 – Filter Media (Schedule 10)

- ☐ Fully raised
☐ Partially raised
☐ In-ground

☐ Class 4 – Shallow Buried Trench

- ☐ Fully raised
☐ Partially raised
☐ In-ground

☒ Class 4 – BMEC Area Bed (Schedule 11)

- ☒ Fully raised
☐ Partially raised
☐ In-ground

☐ Class 4 – "Type A" Dispersal (Schedule 13)

- ☐ Fully raised
☐ Partially raised
☐ In-ground

☐ Class 4 – "Type B" Dispersal (Schedule 14)

- ☐ Fully raised
☐ Partially raised
☐ In-ground

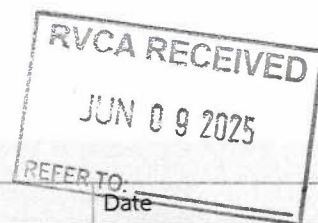
☐ Class 5 – Holding Tank (9000L min)

- ☐ Tank/Treatment Unit/Pump Chamber ONLY
☐ Effluent Filter/Risers ONLY
☐ Other _____



Schedule 5: Sewage System Details

OTTAWA



Do Not Complete

Permit number:

Revision number:

Complete below

Type of System Eljen GSF A-42 Modules (DN 450) (Schedule 4)

Septic/Holding Tank Size: 3,600 (Litres)

Make: _____

Septic Tank Effluent Filter Make: OBC Approved

Model: (Polylok PL-250 or equivalent)

Treatment Unit - Make & Model: Eljen GSF A-42 Modules (DN450)

Number of Units: 8

Refer to Typical Drawing #: PH4924-1&3(rev.3)

Pump ☒ Syphon ☐

Pump(s) required: Yes

Pump Rate: 25 + Charge L/15min Hour

Mantle Information

Native or imported = min. 15m in N/A direction(s)

Slope subgrade _____ % slope

_____ direction(s)

Note: Alarm required for all pumping systems

Installed ☐ Inside TBD By Installer @

☐ Outside time of Installation

Site to be Scarified (If clay) Yes ☒ No ☐

Clay Seal Required (If bedrock) Yes ☐ No ☐

☐ Trench

Distribution Pipe Length _____ m

Loading Area _____ m²

Type of Chamber _____

Length of Chamber _____ m

☐ Dispersal Bed

☒ BMEC ☐ Type A ☐ Type B

Stone N/A m²

Sand 92.9 m²

Pipe 9.76 m²

Linear Loading 6.5 L/m²

☐ Shallow Buried Trench

Pipe Length _____ m²

Pipe _____

☐ Filter Media Bed

Stone _____ m

Extended Base _____ m²

Pipe _____

Weight of Filter Media _____ Kg

Loading Area _____ m²

☐ Tank/Treatment Unit/Pump Chamber Replacement **ONLY**

☐ Effluent Filter & Riser **ONLY**

Construction Notes:



Schedule 6: Soil and Water

Table Information (Minimum depth of test pit: 2 metres)


Do Not Complete

| | | |
|----------------|------------------|------|
| Permit number: | Revision number: | Date |
|----------------|------------------|------|

Name of Applicant/Agent: Paterson Group Inc.
Date: April 17, 2025 Time: 11:00 AM
Applicant/Agent Signature: [Signature]

Inspector: _____
Date: _____ Time: _____
Inspector Signature: _____

| EG () | Soil Description |
|--------|------------------|
| — m — | — |
| — m — | — |
| — m — | — |
| — m — | — |
| — m — | — |
| — m — | — |
| — m — | — |

 Professional Engineers Ontario
Licensed Engineering Technologist
Name: H. G. VAN DE GLIND
Number: 100647862
Limitations: Inspecting, designing, and assessing residential and commercial sewage systems, grading designs and soil analysis, and overseeing installation and compliance.
Association of Professional Engineers of Ontario

T-time 40 Min/cm

| EG () | Soil Description |
|--------|------------------|
| — m — | — |
| — m — | — |
| — m — | — |
| — m — | — |
| — m — | — |
| — m — | — |
| — m — | — |

Test pits not available for inspection.
Engineer assumes all liability for soil and HGWT info/elev's.

T-time _____ Min/cm

| EG () | Soil Description |
|--------|------------------|
| — m — | — |
| — m — | — |
| — m — | — |
| — m — | — |
| — m — | — |
| — m — | — |
| — m — | — |

T-time _____ Min/cm

| EG () | Soil Description |
|--------|------------------|
| — m — | — |
| — m — | — |
| — m — | — |
| — m — | — |
| — m — | — |
| — m — | — |
| — m — | — |

T-time _____ Min/cm

Legend

BR Bedrock
HGWT High ground water table
EG Existing grade

GWT Ground water table
M metres
T percolation rate



Schedule 7: Layout Section

Do Not Complete

Permit number: _____

Revision number: _____

Date _____

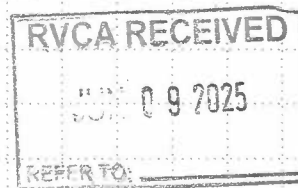
Scale: 1 Block = _____

- Dug Well
- Drilled Well

- ▲ Neighbouring Homes
- ◇ Benchmark

- Tile Drainage
- ___ Property Line

SEPTIC FILE #
25-177
OTTAWA



Elevations (metric only)

B.M. 94.86 m

B.M Description Top of spike in hydro pole across
from East Property Line of 5935 Ottawa Street

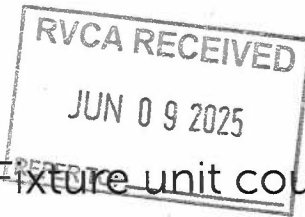
Exact Location _____

Min. of 5 elevations in proposed system area (in X pattern)

| | |
|----------------------|----------------------------|
| X ₁ _____ | X ₂ _____ |
| X ₃ _____ | X ₄ _____ |
| X ₅ _____ | X ₆ (toe) _____ |
| X ₇ _____ | X ₈ _____ |



Schedule 8: Fixture unit count



SEPTIC FILE #

25-177

OTTAWA

Do Not Complete

Permit number: Revision number: Date

| Fixtures | # Existing | + | # Proposed | X | unit count | = | Fixture Count |
|---|------------|---|------------|---|------------|---|---------------|
| Bathroom | | | | | | | |
| Bathroom group (toilet, sink and tub or shower) installed in the same room | | + | | X | 6 | = | 0.00 |
| Bathtub with/without overhead shower | | + | | X | 1.5 | = | 0.00 |
| Shower stall | | + | | X | 1.5 | = | 0.00 |
| Wash basin (SINK) (1½ inch trap) | 3 | + | | X | 1.5 | = | 4.50 |
| Watercloset (TOILET) tank operated | 3 | + | | X | 4 | = | 12.00 |
| Bidet | | + | | X | 1 | = | 0.00 |
| Kitchen | | | | | | | |
| Dishwasher | 1 | + | | X | 1 | = | 1.00 |
| Sink with/without garbage grinder(s), domestic and other small type single, double or 2 single with a common trap | 1 | + | | X | 1.5 | = | 1.50 |
| Other | | | | | | | |
| Domestic washing machine | | + | | X | 1.5 | = | 0.00 |
| Combination sink and laundry tray single or double (Installed on 1½ trap) | | + | | X | 1.5 | = | 0.00 |
| Total* | | | | | | = | 19.00 |

*Insert the TOTAL in section 5 of Schedule 4 (0.Reg 151/13 Table 7.4.9.3)

1. Sump pumps and floor drains are not to be connected to the sewage system. Connection of such fixtures to a sewage system may lead to a hydraulic failure of the said system. The above mentioned fixtures should be discharged separately to an approved Class 2 (leaching pit) sewage system.

2. Where laundry waste is not more than 20% of the total daily design sanitary sewage flow, it may discharge to a sewage system (Part 8, OBC, 8.1.3.1(2)).

Hy U. G. W.

June 6, 2025

Agent/Owner signature

Date

NOTE:

SEWAGE SYSTEM 'B' HAS BEEN DESIGNED BASED ON PATERSON GROUP REPORT PH4924-LET.01

TOTAL DESIGN DAILY SANITARY SEWAGE FLOW (T.D.D.S.S.F.) OR "Q" = 600 L/DAY WHEN BALANCED OVER 7 DAYS.

NATIVE SOILS = GLACIAL TILL TO SILTY CLAY = T = 40 min/cm

MINIMUM NITRATE REDUCTION LEVEL REQUIRED = 50% AS PER PATERSON GROUP REPORT No. PH4924-LET.01

ELJEN DN450 SHALL BE USED TO ACHIEVE THE MINIMUM REQUIRED NITRATE REDUCTION.

PRESENTLY PROPOSED ELEVATIONS ARE BASED OFF THE EXISTING TOPOGRAPHIC INFORMATION. THE PROPOSED LOT GRADING AND DRAINAGE ASSOCIATED WITH THE PROPOSED ADDITION MAY AFFECT THESE ELEVATIONS.

NOTE:

SEWAGE SYSTEM 'A' HAS BEEN DESIGNED BASED ON PATERSON GROUP REPORT PH4924-LET.01

TOTAL DESIGN DAILY SANITARY SEWAGE FLOW (T.D.D.S.S.F.) OR "Q" = 9,367 L/DAY WHEN BALANCED OVER 7 DAYS.

NATIVE SOILS = GLACIAL TILL TO SILTY CLAY = T = 35 min/cm

MINIMUM NITRATE REDUCTION LEVEL REQUIRED = 50% AS PER PATERSON GROUP REPORT No. PH4924-LET.01

ELJEN DN450 SHALL BE USED TO ACHIEVE THE MINIMUM REQUIRED NITRATE REDUCTION.

PRESENTLY PROPOSED ELEVATIONS ARE BASED OFF THE EXISTING TOPOGRAPHIC INFORMATION. THE PROPOSED LOT GRADING AND DRAINAGE ASSOCIATED WITH THE PROPOSED ADDITION MAY AFFECT THESE ELEVATIONS.

PART 4
R.P. 4R-7050PART 1
R.P. 4R-13387

100mm Ø PVC PIPE TO BE INSTALLED @ 2% (min.) SLOPE AND SHALL BE SLEEVED THROUGH A 150mm Ø PVC SDR28 PIPE AND OVERLAIN BY 75mm T x 600mm W RIGID INSULATION BOARDS UNDER ASPHALT. PATERSON TO REVIEW COVER UPON COMPLETION OF LOT GRADING AND DRAINAGE.

TYP.
2 OUTLET DISTRIBUTION BOX C/W INLET Baffle AND POLYLOK FLOW EQUALIZERS
INLET INV. 94.90m(min.)
OUTLET INV. = 94.80m (min.)

ELJEN SAMPLING PAN
• INSTALL COLLECTION PLATES AS PER MANUFACTURER SPECIFICATIONS

2 RUNS OF 4 ELJEN GSF A-42 MODULES
MODULAR BASE ELEV. @ HEAD = 94.42m
MODULAR BASE ELEV. @ FOOT = 94.40m

TYP.
100mm Ø VENT PIPE INSTALLED IN 150mm Ø LANDSCAPE VALVE COVER

TYP.
100mm Ø SOLID PVC FOOTER PIPE
INV. = 94.58m

NOTE:
SNOW STORAGE SHALL NOT BE LOCATED OVER OR UPGRADIENT OF THE PROPOSED SEWAGE SYSTEM.

NOTE:
SNOW STORAGE SHALL NOT BE LOCATED OVER OR UPGRADIENT OF THE PROPOSED SEWAGE SYSTEM.

TYP.
100mm Ø VENT PIPE INSTALLED IN 150mm Ø LANDSCAPE VALVE COVER

TYP.
100mm Ø SOLID PVC FOOTER PIPE
INV. = 94.78m

100mm Ø PERFORATED PVC SEPTIC PIPE
INSTALLED @ APPROX. 0.5% ON ELJEN MODULES
HEAD INV. = 94.83m
FOOT INV. = 94.78m

3m L - 100mm Ø PVC PIPE WITH ELBOW @ 2% (min.) SLOPE

2 CELLS OF 5 RUNS OF 11 ELJEN GSF A-42 MODULES
MODULAR BASE ELEV. @ HEAD = 94.65m
MODULAR BASE ELEV. @ FOOT = 94.60m

ELJEN SAMPLING PAN
• INSTALL COLLECTION PLATES AS PER MANUFACTURER SPECIFICATIONS

ELJEN SPECIFIED SAND AREA
• 630 mm THICK (TOP OF MODULE TO BASE)
• 37.24m x 22.50m
• FOLLOWED BY 300 mm THICK OF SAND/LIGNOCELLULOSE LAYER
• FOLLOWED BY 50 mm THICK LAYER OF LIMESTONE

18,500L (min.) BALANCING TANK c/w TIME OPERATED EFFLUENT 1/2 H.P. DUPLEX PUMPS AND AUDIBLE / VISUAL HIGH WATER ALARM.
• TANK SHALL BE CPA APPROVED (OR ENGINEERED) FOR 1.2m (min.) OF COVER.
• TANK SHALL BE REVIEWED FOR BALLASTING REQUIREMENTS.
• PUMPING SYSTEM SHALL BE TIME DOSED TO OPERATE EVERY HOUR AND ALTERNATE BETWEEN CELLS.
• POLY RISER AND COVER ASSEMBLY
• INLET INV. = 94.40m±
• TOP OF TANK (max.) = 94.75m±
• FINISHED GRADE = 95.40m

NEW 3,600L PRETREATMENT TANK c/w
• TANK SHALL BE CPA APPROVED (OR ENGINEERED) FOR 1.2m (min.) OF COVER.
• TANK SHALL BE REVIEWED FOR BALLASTING REQUIREMENTS.
• POLYLOK PL-525 EFFLUENT FILTER
• POLY RISER & COVER ASSEMBLY (2)
• INLET INV. = 94.27m±
• OUTLET INV. = 94.22m±
• TOP OF TANK = 94.55m±
• FINISHED GRADE = 95.15m

PROPOSED INDUSTRIAL BUILDING
(ONE STOREY)

38mm Ø PVC SCH 40 PIPE FORCEMAIN
• SHALL BE INSTALLED TO GRAVITY DRAIN TO THE TANK.
• ENTIRE LENGTH OF FORCEMAIN SHALL BE BEDDED OF A MINIMUM OF 150mm OF OPSS GRANULAR A, AND SHALL BE COVERED WITH A MINIMUM OF 300mm OF OPSS GRANULAR A.
• ALL GRANULAR A MATERIAL SHALL BE COMPACTED TO A MINIMUM OF 98% SPMDD.

100mm Ø PERFORATED PVC SEPTIC PIPE INSTALLED @ APPROX. 0.5% ON ELJEN MODULES
HEAD INV. = 94.60m
FOOT INV. = 94.58m

ELJEN SPECIFIED SAND AREA
• 630 mm THICK (TOP OF MODULE TO BASE)
• 9.60m x 9.68m
• FOLLOWED BY 300 mm THICK OF SAND/LIGNOCELLULOSE LAYER
• FOLLOWED BY 50 mm THICK LAYER OF LIMESTONE

TYP.
2 x LARGE 4 OUTLET DISTRIBUTION BOX C/W INLET Baffle AND POLYLOK FLOW EQUALIZERS
INLET INV. 95.10m(min.)
OUTLET INV. = 95.00m (min.)

EXISTING MONITORING WELL TO BE DECOMMISSIONED

PROPOSED INDUSTRIAL BUILDING
(ONE STOREY)

PROPOSED FINISHED FLOOR ELEVATION: 95.25

PAVERS

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CONCRETE

Professional Engineers
Ontario

Licensed Engineering Technologist

Name: H. G. VAN DE GLIND
Number: 100647862

Limitations: Inspecting, designing, and assessing residential and commercial sewage systems, grading designs and soil analysis, and overseeing installation and compliance.

Association of Professional Engineers of Ontario

| LEGEND: | BENCHMARK INFORMATION: |
|-----------------------------------|--|
| Bore Hole Location | TBM: Top of Spike in Hydro Pole Across from East Property Line of 5935 Ottawa Street Approximate Geodetic Elevation = 94.86m |
| Existing Ground Surface Elev. (m) | REFERENCE: |
| Proposed Ground Surface Elev. (m) | Topographic Information obtained from Plan of Survey of Part of Unit 10 Index Plan D-26 Geographic Township of Goulbourn City of Ottawa, dated July 9, 2024, by egis Surveying Inc. |
| Proposed Subgrade Elev. (m) | Baseplan Obtained from Site Plan No. A-001, dated May 2025, by N45 Architecture Inc. |
| Groundwater Elev. (m) - Mar.6/22 | |
| Finished Floor Elev. (m) | |
| Existing Structure | |
| Proposed Structure | |

All Units are in meters unless otherwise specified

Consultant

04/06/25 Issued for Septic Permit 3

14/05/25 Issued with Revised Site Plan 2

03/10/24 Issued with Revised Site Plan 1

20/09/24 Issued for Preliminary Review 0

DD/MM/YY Description Rev.

Rev.

Rev.

Rev.

Rev.

Rev.

Rev.

STRATFORD FOXRUN

PROPOSED WAREHOUSE / RESTAURANT
5923 OTTAWA STREET
OTTAWA (RICHMOND), ONTARIO

SEWAGE SYSTEM LAYOUT PLAN
SEWAGE SYSTEM 'A' AND 'B'

Scale: 1:600

Date: 06/2025

Drawn by: HV

Checked by: MK

Drawing no.:

PH4924-1(rev.3)

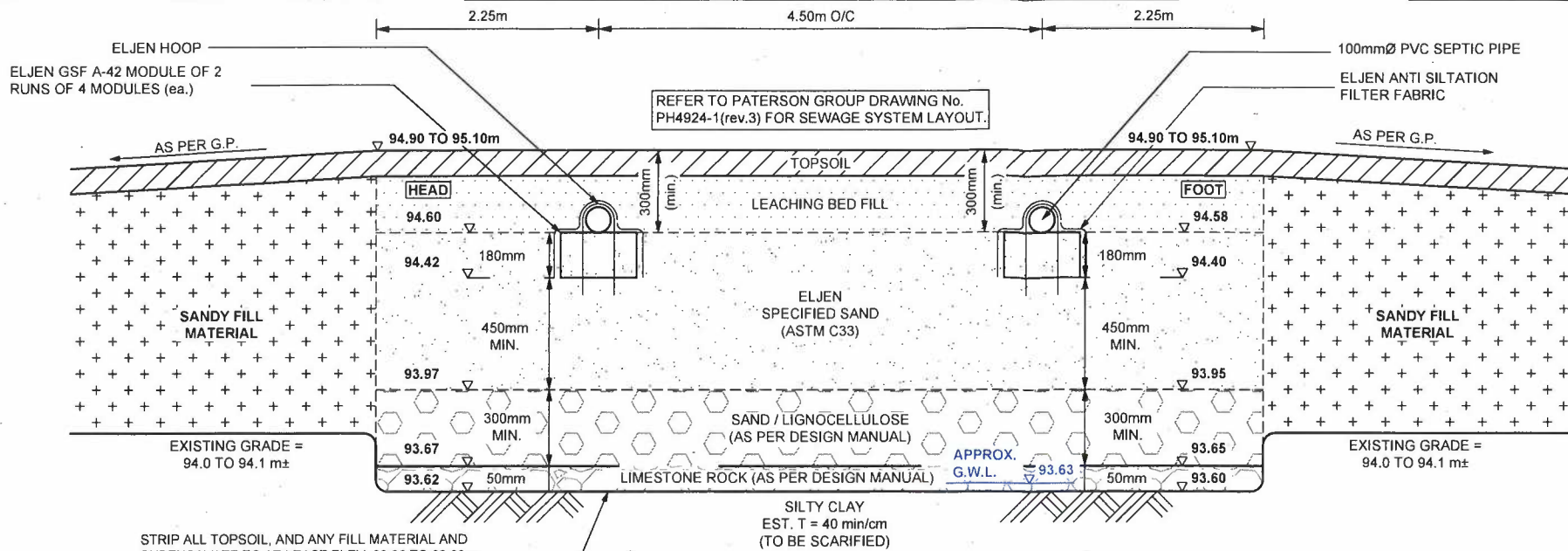


9 AURIGA DRIVE
OTTAWA, ON
K2E 7S5
TEL: (613) 228-7381

COVER MATERIAL TO CONSIST OF LEACHING BED FILL FOLLOWED BY APPROX. 100mm OF SANDY TOPSOIL. LEACHING BED TO BE VEGETATED AS SOON AS POSSIBLE.

SEWAGE SYSTEM DESIGN, SPECIFICATION, DETAILS AND NOTES HAVE BEEN COMPLETED IN ACCORDANCE WITH ELJEN DENITRIFICATION SUPPLEMENTAL DESIGN AND INSTALLATION MANUAL.

FINAL GRADING SHALL BE SUITABLY SHAPED TO DIRECT SURFACE WATER AWAY FROM THE PROPOSED SEWAGE SYSTEM.



NOTES:

1) ESTIMATE OF DAILY SEWAGE FLOW (Q)

THE PROPOSED SEWAGE SYSTEM HAS BEEN DESIGNED TO SUPPORT A COMMERCIAL TYPE USAGE CONSISTING OF OFFICE, AND WAREHOUSE SPACE. THE DAILY DESIGN SEWAGE FLOW RATE IS CALCULATED IN ACCORDANCE WITH O.B.C. TABLE 8.2.1.3.B.

OFFICE SPACE:

- 4 EMPLOYEES x 75 L/DAY = 300 L/DAY

WAREHOUSE SPACE:

- 2 LOADING BAY x 150 L/DAY = 300 L/DAY

TOTAL DESIGN DAILY SANITARY SEWAGE FLOW = 600 L/DAY

2) SOIL CONDITIONS

SOILS INFORMATION GATHERED BY PATERSON GROUP INC. ON APRIL 17, 2025. REFER TO PATERSON GROUP REPORT PG73781-1Rev.2 FOR FULL SOILS BREAKDOWN.

BH 1-25, ELEV. 94.07m

| | |
|-----------|--|
| 0-0.08 | TOPSOIL AND ORGANICS |
| 0.08-1.45 | BROWN SILTY CLAY |
| 1.45-6.60 | GLACIAL TILL: BROWN SILTY SAND WITH GRAVEL, COBBLES BOULDERS AND CLAY (GREY @ 3.73m DEPTH) |

- G.W.L. @ 0.05m DEPTH (93.54m)

1) PRETREATMENT TANK

- TANK SHALL BE CONNECTED TO BUILDING BY A 150mm Ø PVC PIPE SLEEVED THROUGH A 200mm Ø PVC SDR 28 PIPE AND OVERLAIN WITH 50mm T x 600mm W RIGID INSULATION BOARDS (UNDER ROADWAY) AND SHALL BE INSTALLED AT 2.0% (min.) SLOPE TO THE PRETREATMENT TANK.
- MINIMUM WORKING CAPACITY OF PRETREATMENT TANK = (3 x Q) OR 3,600 L (min.) = 3,600 L (min.)
- IT IS RECOMMENDED THAT A NEW 3,600L (min.) TWO-COMPARTMENT SEPTIC TANK BE INSTALLED.
- AN OBC APPROVED EFFLUENT FILTER (I.E. POLYLOK PL-525 EFFLUENT FILTER, OR EQUIVALENT) SHALL BE INSTALLED ON THE OUTLET PIPE IN THE PRETREATMENT TANK.
- THE ACCESS LIDS TO THE TANK OPENINGS SHALL BE EXTENDED TO THE GROUND SURFACE. INSTALL RISERS AND COVERS TO SUIT.
- ACCESS LIDS SHALL INCLUDE SAFETY DEVICES AS PER CSA B66-21.
- TANK SHALL BE CPA APPROVED (OR ENGINEERED) FOR 1.2m (min.) OF COVER MATERIAL.
- TANK SHALL BE REVIEWED FOR BALLASTING REQUIREMENTS.

4) BALANCING TANK

- INSTALL A 450L (min.) BALANCING TANK IN SERIES AND DOWNSTREAM FROM THE NEW SEPTIC TANK.
- A TIME OPERATED ALTERNATING DUPLEX PUMPING SYSTEM (I.E. MYERS ME3F, OR SIMILAR) AND A HIGH WATER ALARM SHALL BE INSTALLED IN THE BALANCING TANK.
- THE TIME OPERATIONAL PUMPING SYSTEM SHALL OPERATE EVERY HOUR (I.E. 25 L/DSE + VOLUME TO CHARGE THE SYSTEM) AND SHALL ALTERNATE BETWEEN EACH CELL.
- A 3mm Ø DRAIN HOLE SHALL BE INSTALLED IN THE UNDERSIDE OF THE FORCEMAIN IN THE BALANCING TANK NEAR THE WALL CONNECTION.
- RISERS WITH A COVER SHALL BE INSTALLED OVER THE BALANCING TANK TO PROVIDE ACCESS FROM THE GROUND SURFACE.
- DISCHARGE PIPING FOR PUMP SHALL BE CONFIGURED SUCH THAT THE PUMP IS EASILY SERVICED FROM THE GROUND SURFACE.

5) DISTRIBUTION BOX / FORCEMAIN

- A 38mm Ø (NOMINAL) PVC SCH 40 FORCEMAIN (2) SHALL BE USED TO CARRY THE EFFLUENT FROM THE BALANCING TANK TO EACH 3m L x 100mm Ø PVC SEWER PIPE.

- 100mm SEWER PIPE SHALL DRAIN BY GRAVITY TO A 2 OUTLET DISTRIBUTION BOX.
- THE FORCE MAIN SHALL BE INSTALLED TO GRAVITY DRAIN TO THE BALANCING TANK.
- THE FORCE MAIN SHALL BE OVERLAIN WITH 50mm T x 600mm C/W RIGID INSULATION.
- THE DISTRIBUTION BOX SHALL BE EQUIPPED WITH AN INLET BAFFLE AND OUTLET PIPES (2).
- EACH PIPING RUN SHALL BE FED BY A 2 OUTLET DISTRIBUTION BOX.
- THE DISTRIBUTION BOX SHALL BE CONNECTED TO THE DISTRIBUTION PIPING RUNS USING 100mm Ø SOLID PVC SEWER PIPE @ 2% (min.) SLOPE.

6) LEACHING BED SIZING CRITERIA

- NO. OF MODULES REQUIRED = $Q/95 = 600/95 = 6.3$ MODULES
- USE 2 RUNS OF 4 (8) ELJEN GSF A-42 MODULES EACH
- SAND AREA REQUIRED = $QT/400 = 600(40)/400 = 60m^2$
- SAND AREA PROVIDED = $9.60m \times 9.68m = 92.9m^2$ (min.)

7) LEACHING BED CONSTRUCTION GUIDELINES

- REMOVE ALL EXISTING TOPSOIL, AND ANY FILL WITHIN LIMITS OF THE SAND AREA AND SUBEXCAVATE TO AT LEAST ELEVATION 93.60m TO 93.62m, WHICHEVER IS GREATER. RE-ESTABLISH THE SPECIFIED CONTACT LEVEL USING SELECT SAND FILL, WHERE REQUIRED.
- THE SUBGRADE SURFACE SHALL BE SCARIFIED, UNDER DRY CONDITIONS.
- PLACE A 50mm MIN. THICK LAYER OF LIMESTONE ROCK OVER THE SUITABLY PREPARED SUBGRADE.
- LIMESTONE ROCK SHALL NO SMALLER THAN 25mm IN DIAMETER UP TO 50mm IN DIAMETER. THE ROCK SHALL CONTAIN GREATER THAN 15% LIMESTONE AS PER ELJEN DENITRIFICATION SUPPLEMENTAL DESIGN AND INSTALLATION MANUAL.
- PLACE A 300mm THICK LAYER OF SAND / LIGNOCELLULOSE OVER THE LIMESTONE ROCK LAYER.
- SAND / LIGNOCELLULOSE SHALL CONSIST OF WOOD CHIPS OR SAW DUST FROM HARD WOOD TREES THAT HAVE NOT BEEN FURTHER PROCESSED BY CHEMICALS. THE 300mm SAND AND LIGNOCELLULOSE LAYER SHALL BE 50/50 EQUAL MIXTURE OF ASTM C33 SAND AND WOOD CHIPS FROM HARD WOOD TREES. THE MIXTURE MUST NOT EXCEED 60/40 IN FAVOR OF THE MORE WOOD TO SAND.
- PLACE A 450mm MIN. THICK LAYER OF ELJEN SPECIFIED SAND FILL OVER THE LEACHING BED FILL.
- THE ELJEN SPECIFIED SAND FILL SHALL CONSIST OF WASHED SAND MEETING THE REQUIREMENTS OF ASTM C33 "STANDARD SPECIFICATION FOR CONCRETE AGGREGATES" WITH LESS THAN 5% PASSING 0.075mm SIEVE. ELJEN SPECIFIED SAND FILL SHALL BE PRE-APPROVED BY THE CONSULTANT.
- THE MODULES SHALL BE INSTALLED IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS.
- THE MODULES SHALL BE INSTALLED AT A SLOPE OF 0.3% (min.) TO 0.5% (max.), END TO END AND WITH THE WHITE DEMARCATION LINE FACING UP.
- THE MODULAR BASE LEVEL (ELEV. 94.40m AT THE FOOT, TO 94.42m AT THE HEAD) SHALL BE ESTABLISHED WITH ELJEN SPECIFIED SAND FILL, HAVING A MINIMUM THICKNESS OF 450mm BELOW THE MODULES.
- THE ELJEN MODULES SHALL BE FED BY GRAVITY BY A 100mm Ø PVC SEWER PIPE @ 2% (min.) SLOPE FROM THE DISTRIBUTION BOX.
- THE DISTRIBUTION PIPE SHALL CONSIST OF A 100mm Ø PERFORATED PVC PIPE CENTRED OVER THE MODULES. THE PIPE SHALL BE SECURED TO THE TOP OF THE MODULES USING AN ELJEN HOOP (MINIMUM 1 HOOP PER MODULE).
- THE INVERT LEVEL OF THE DISTRIBUTION PIPE SHALL BE SET ON THE MODULES AT ELEVATION 94.58m AT THE FOOT TO 94.60m AT THE HEAD. THE END OF THE PIPE RUNS SHALL BE CONNECTED TO A 100mm Ø SOLID PVC FOOTER PIPE.
- INSTALL ELJEN SYSTEM SAMPLING DEVICE AS PER MANUFACTURER'S RECOMMENDATIONS.
- THE ELJEN ANTI-SILTATION FILTER FABRIC SHALL BE SPREAD LENGTHWISE OVER THE PERFORATED SEPTIC PIPE AND DOWN THE SIDES OF THE MODULES. ENSURE ENDS OF MODULES ARE ALSO COVERED WITH FABRIC.
- THE MODULES SHALL BE BACKFILLED, WITH ELJEN SPECIFIED SAND FILL TO AT LEAST THE TOP OF THE ELJEN MODULES, FOLLOWED BY 200mm (min.) OF LEACHING BED FILL, FOLLOWED BY 100mm OF SANDY TOPSOIL, WITHIN THE LIMITS OF THE SAND AREA. THE BED AREA SHOULD BE VEGETATED AS SOON AS POSSIBLE.
- LEACHING BED SAND FILL SHALL BE UNIFORM SAND WITH GRADING LIMITS SIMILAR TO 100% PASSING 13.2mm SIEVE, LESS THAN 5% PASSING 0.075mm SIEVE, AND HAVING A PERCOLATION TIME OF 6 TO 8 min/cm. LEACHING BED FILL SHALL BE PRE-APPROVED BY THE CONSULTANT.
- THE SIDES OF THE BED SHOULD BE SLOPED AT 3H:1V OR SHALLOWER.
- VENT SYSTEM SHALL BE INSTALLED ON THE FOOTER PIPE. CONNECT A 100mm Ø PVC VENT PIPE TO FOOTER PIPE, EXTENDING TO GROUND SURFACE. VENT PIPE TO BE INSTALLED IN 150mm Ø LANDSCAPE VALVE COVER.

8) MINIMUM CLEARANCE DISTANCE FROM DISTRIBUTION PIPE

- 5.6m FROM ANY PROPERTY LINE
- 7.6m FROM ANY STRUCTURE: 5.0m FROM ANY BASEMENTLESS STRUCTURE
- 17.6m FROM ANY DRILLED WELL
- 5.0m FROM ANY TREE (UNLESS OTHERWISE APPROVED)

9) MINIMUM CLEARANCE DISTANCE FROM TANK(S)

- 1.5m FROM ANY STRUCTURE
- 15.0m FROM ANY DRILLED OR DUG WELL
- 3.0m FROM ANY PROPERTY LINE

10) GENERAL

- SNOW STORAGE SHALL NOT BE LOCATED OVER OR UPGRADIENT OF THE PROPOSED SEWAGE SYSTEM.
- THE SEWAGE SYSTEM HAS NOT BEEN DESIGNED TO SUPPORT TRAFFIC LOADING.
- THE BACKFILLING OF THE SEWAGE SYSTEM SHOULD MINIMIZE THE RISK OF OVER COMPACTION WITH THE USE RUBBER TRACKED EQUIPMENT AND BY AVOIDING THE CREATION OF ANY CONSTRUCTION ROUTES OR PATHWAYS OVER THE SYSTEM.
- ANY NEW IRRIGATION / SPRINKLER SYSTEM SHOULD NOT BE USED IN PROXIMITY OF THE PROPOSED SEWAGE SYSTEM.
- ENSURE WALKWAYS AND/OR SHURBBERY ARE NOT PLACED WITHIN PROXIMITY OF THE TANKAGE.
- THE BACKWASH WATERS FROM ANY WATER TREATMENT UNIT, SUCH AS WATER SOFTENER, SHOULD NOT DISCHARGE INTO THE SEWAGE SYSTEM.
- THE SEWAGE SYSTEM HAS NOT BEEN DESIGNED FOR THE USE OF A GARBAGE DISPOSAL.
- SEWAGE SYSTEM INSTALLER SHALL BE QUALIFIED AND REGISTERED UNDER PART 8 OF THE ONTARIO BUILDING CODE AND SHALL BE AN AUTHORIZED ELJEN TREATMENT SYSTEM INSTALLER.
- ALL WORK SHALL BE CARRIED OUT IN ACCORDANCE WITH THE LATEST BY-LAWS, CODES AND REGULATIONS.
- CONTRACTOR SHALL REVIEW DRAWINGS IN DETAIL AND SHALL INFORM THE CONSULTANT OF ANY ERRORS AND/OR OMISSIONS ON DESIGN DRAWINGS IMMEDIATELY.
- CONTRACTOR SHALL BE RESPONSIBLE TO LOCATE AND PROTECT ALL EXISTING UNDERGROUND SERVICES.
- CONTRACTOR SHALL VISIT THE SITE AND REVIEW ALL DOCUMENTATION TO BECOME FAMILIAR WITH THE SITE AND SUBSURFACE SOIL CONDITIONS TO DETERMINE SUITABLE METHODS OF CONSTRUCTION.
- THE MANUFACTURER PROVIDES A LIMITED WARRANTY OF THE SYSTEM COMPONENTS. THE OWNER OF THE SYSTEM MUST SIGN A MAINTENANCE AGREEMENT WITH THE MANUFACTURER'S REPRESENTATIVE. THE HOMEOWNER IS RESPONSIBLE FOR THE ANNUAL FEES ASSOCIATED WITH THE MAINTENANCE.
- THE FIRM OF PATERSON GROUP INC. HAS PROVIDED DESIGN SERVICES ONLY FOR THE SUBJECT SEWAGE SYSTEM. THE DESIGN HAS BEEN CARRIED OUT IN ACCORDANCE WITH THE MANUFACTURER'S GUIDELINES AND OUR INTERPRETATION OF PART 8 OF THE ONTARIO BUILDING CODE.
- INSPECTIONS BY THE CONSULTANT DURING THE INSTALLATION OF THE SYSTEM IS A REQUIREMENT OF SOME REGULATING AUTHORITIES AND IS STRONGLY RECOMMENDED BY THIS FIRM.
- THE PROPERTY LINE / SEPARATION DISTANCES SHOULD BE CONFIRMED PRIOR TO CONSTRUCTION.
- CONSTRUCTION INSPECTIONS DURING THE INSTALLATION OF THE SEWAGE SYSTEM MAY BE REQUIRED BY THE REGULATING AUTHORITY AND ARE STRONGLY RECOMMENDED BY THIS FIRM. IF THIS FIRM IS TO COMPLETE ANY CONSTRUCTION INSPECTION(S), ADDITIONAL FEES MAY BE APPLIED. CONFIRMATION OF PAYMENT WILL BE REQUIRED PRIOR TO THE INSPECTION.
- THE TEST HOLE INFORMATION PROVIDED, IS INTENDED TO BE USED FOR DESIGN PURPOSES ONLY, AND SHOULD NOT BE RELIED UPON FOR CONSTRUCTION PURPOSES. IF DISCREPANCIES ARE FOUND DURING THE CONSTRUCTION PROCESS, IT IS THE CLIENT'S RESPONSIBILITY TO CONTACT THIS FIRM TO MAKE ANY NECESSARY COMMENTS OR REVISIONS. ADDITIONAL REVISIONS ARE NOT CONSIDERED PART OF THE DESIGN WORKS AND WILL BE CONSIDERED AS AN ADDITIONAL COST.



Professional Engineers
Ontario

Licensed Engineering Technologist

Name: H. G. VAN DE GLIND

Number: 100647862

Limitations: inspecting, designing, and assessing residential and commercial sewage systems, grading designs and soil analysis, and overseeing installation and compliance.

Association of Professional Engineers of Ontario

| 04/06/25 | Issued for Septic Permit | 3 |
|----------|-------------------------------|------|
| 14/05/25 | Issued with Revised Site Plan | 2 |
| 03/10/24 | Issued with Revised Site Plan | 1 |
| 20/09/24 | Issued for Preliminary Review | 0 |
| DD/MM/YY | DESCRIPTION | REV. |

Consultant:



PATERSON
GROUP

9 AURIGA DRIVE
OTTAWA, ON
K2E 7S9
TEL (613) 226-7581

Client:

STRATFORD FOXRUN

Project:

**PROPOSED WAREHOUSE /
RESTAURANT**

**5923 OTTAWA STREET
OTTAWA (RICHMOND), ONTARIO**

Drawing:

**SEWAGE SYSTEM
DETAILS AND NOTES
SEWAGE SYSTEM 'B'**

Scale:

N.T.S.

Drawn by:

HV

Date:

06/2025

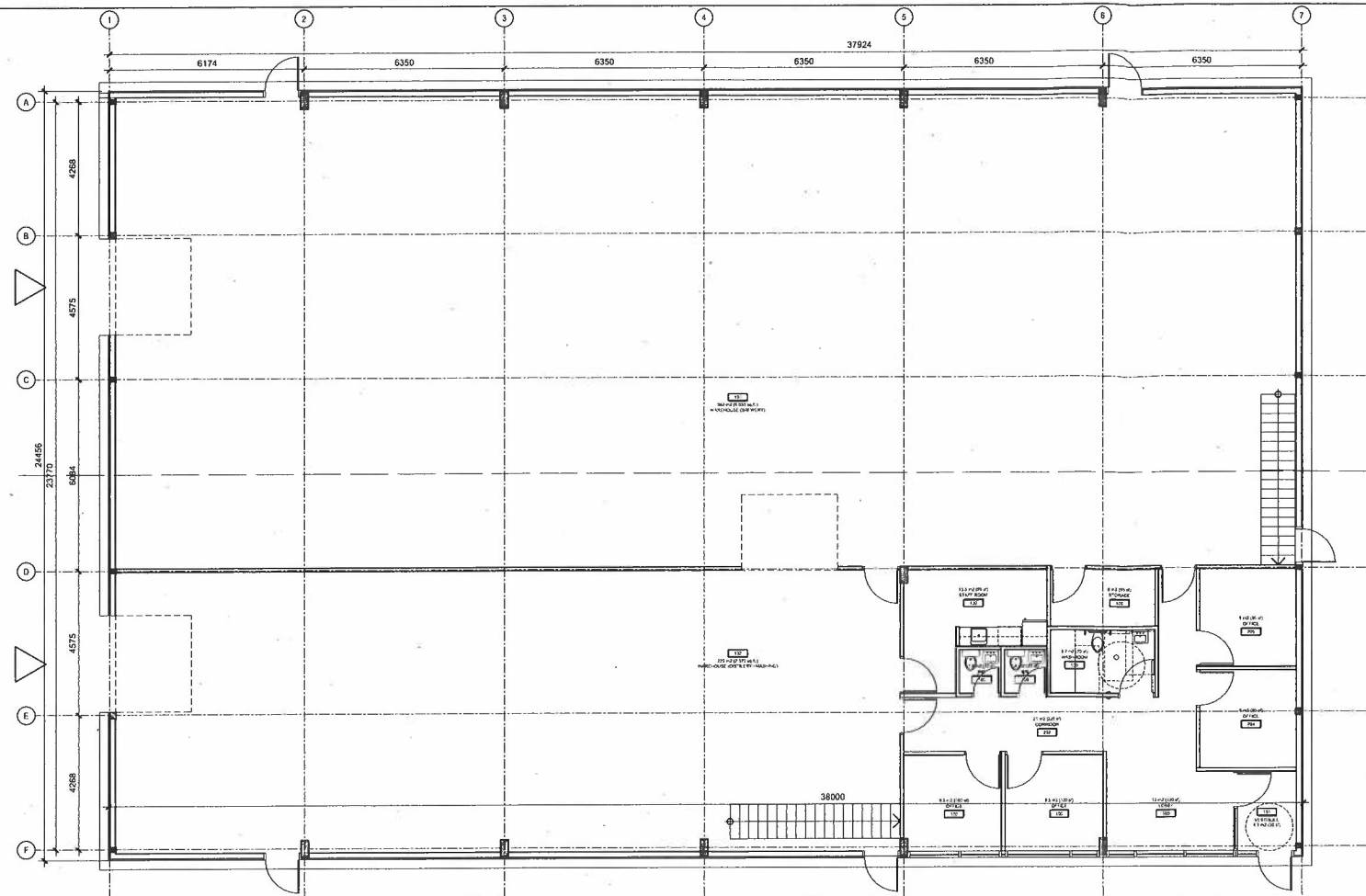
Checked by:

MK

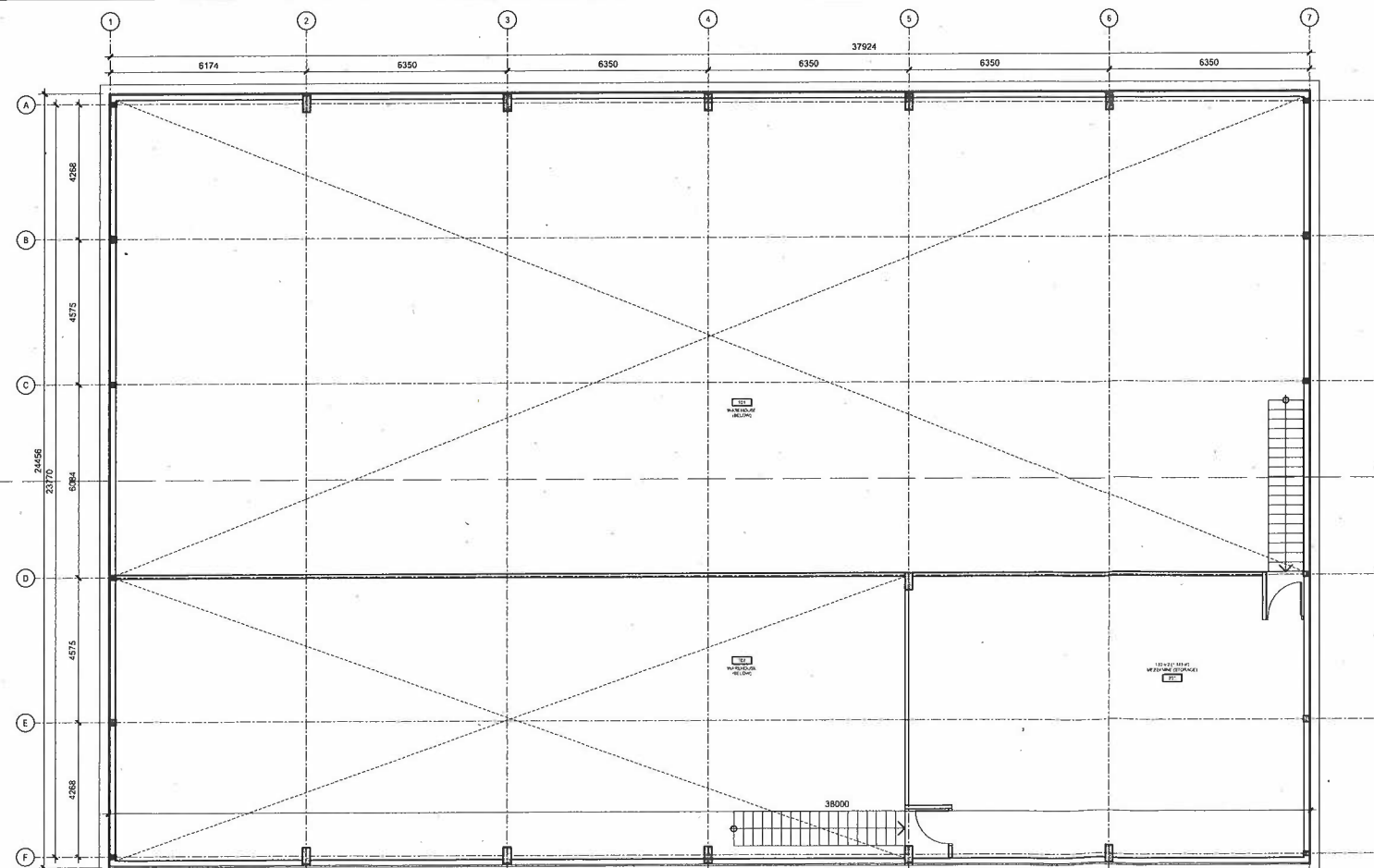
Drawing No.:

PH4924-3(rev.3)

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jack gulas - 5923 ottawa street richmond\ph4924-3(rev.3).dwg

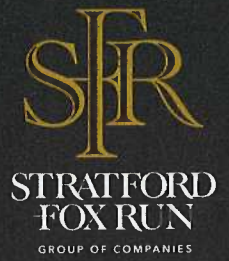


1 GROUND FLOOR PLAN
A-004 SCALE 1:100



2 MEZZANINE FLOOR PLAN
A-004 SCALE 1:100

BUILDING 2
SEWAGE SYSTEM "B"
25-177



| | | |
|-----|----------------|---------|
| 01 | ISSUED FOR SPA | 08MAY25 |
| no. | revision | date |

N45 ARCHITECTURE INC.
71 Bank Street, 7th floor - Ottawa, Ontario, K1P 5N2
tel. 613.224.0095 fax 613.224.9811

| | |
|----------------------------------|------------------|
| project | FOX RUN RICHMOND |
| 5923 OTTAWA STREET OTTAWA, ON | |
| project north | seal |
| | |

| | |
|---|------------------|
| drawing title | BREWERY BUILDING |
| scale | AS NOTED |
| date | MARCH 2025 |
| project number | 24-826 |
| drawn by | NF |
| checked by | VP |
| drawing number | A-004 |
| CONTRACTOR TO VERIFY ALL DIMENSIONS AND NOTIFY THE ARCHITECT OF ANY DISCREPANCIES BEFORE WORK COMMENCES. DO NOT SCALE DRAWINGS. | revision |
| | - |



Permit
Part 8 – Sewage System
Ontario Building Code

Do Not Complete
Permit No 25-177
Revision No _____
Date _____
Related Application _____

A copy of this permit must be posted on the property at all time during construction. OBC, Division C — Part 1, Section 1.3.2.1

This permit verifies that the on-site sewage system was reviewed and approved for construction under the Ontario Building Code Act (Building Code Act, 1992, S.O. 1992, c. 23) and Ontario Building Code (O. Reg. 163/24) as amended.

Inspected & Recommended by: Matt Panciuk Owner: 99117756 Canada Inc.
Inspection Date & Time: _____ Weather: _____
Address: 5923 Ottawa Street - System B Legal: _____
In the former Township/City of Goulbourn

Design Flow for Commercial / Institutional / Industrial (as per Table 8.2.1.3.B)

Q: 600 L/day

| | | | | |
|-----------------|------------------------------|------------------------------|---|--|
| septic tank | <u>3600(min)</u> L | weigh bills for Eljen Sand | <input checked="" type="checkbox"/> yes | <input type="checkbox"/> no |
| effluent filter | <u>YES</u> | grain size analysis required | <input checked="" type="checkbox"/> yes | <input type="checkbox"/> no |
| pump rate | <u>25 + Charge</u> L/15 MIN | site to be scarified | <input checked="" type="checkbox"/> yes | <input type="checkbox"/> no |
| treatment unit | <u>Eljen GSF A42(DN 450)</u> | clay seal inspection | <input type="checkbox"/> yes | <input checked="" type="checkbox"/> no |
| number of units | <u>8</u> | mantle required | <input type="checkbox"/> yes | <input checked="" type="checkbox"/> no |
| | | sub-grade inspection | <input checked="" type="checkbox"/> yes | <input type="checkbox"/> no |

ELEVATION ☐ In Ground ☐ Partially Raised ☒ Fully Raised

TYPE OF SYSTEM

☐ Trench

☒ Pipe and Stone or ☐ Chambers

type of chamber _____
loading area _____ m²
total trench length _____ m
trench configuration _____

☒ Dispersal Bed

☒ BMEC ☐ Type A ☐ Type B

stone _____ m²
sand 92.9 m²
pipe 2 runs of 4 modules @ 4.5m o/c
weight of sand _____ kg

☐ Shallow Buried Trench

pipe length _____ m
orifice spacing _____ m

☐ Filter Media Bed

stone _____ m²
extended base _____ m²
pipe _____
weight of filter media _____ kg
loading area _____ m²

☐ Class 5 Holding Tank

☐ Septic Tank Only

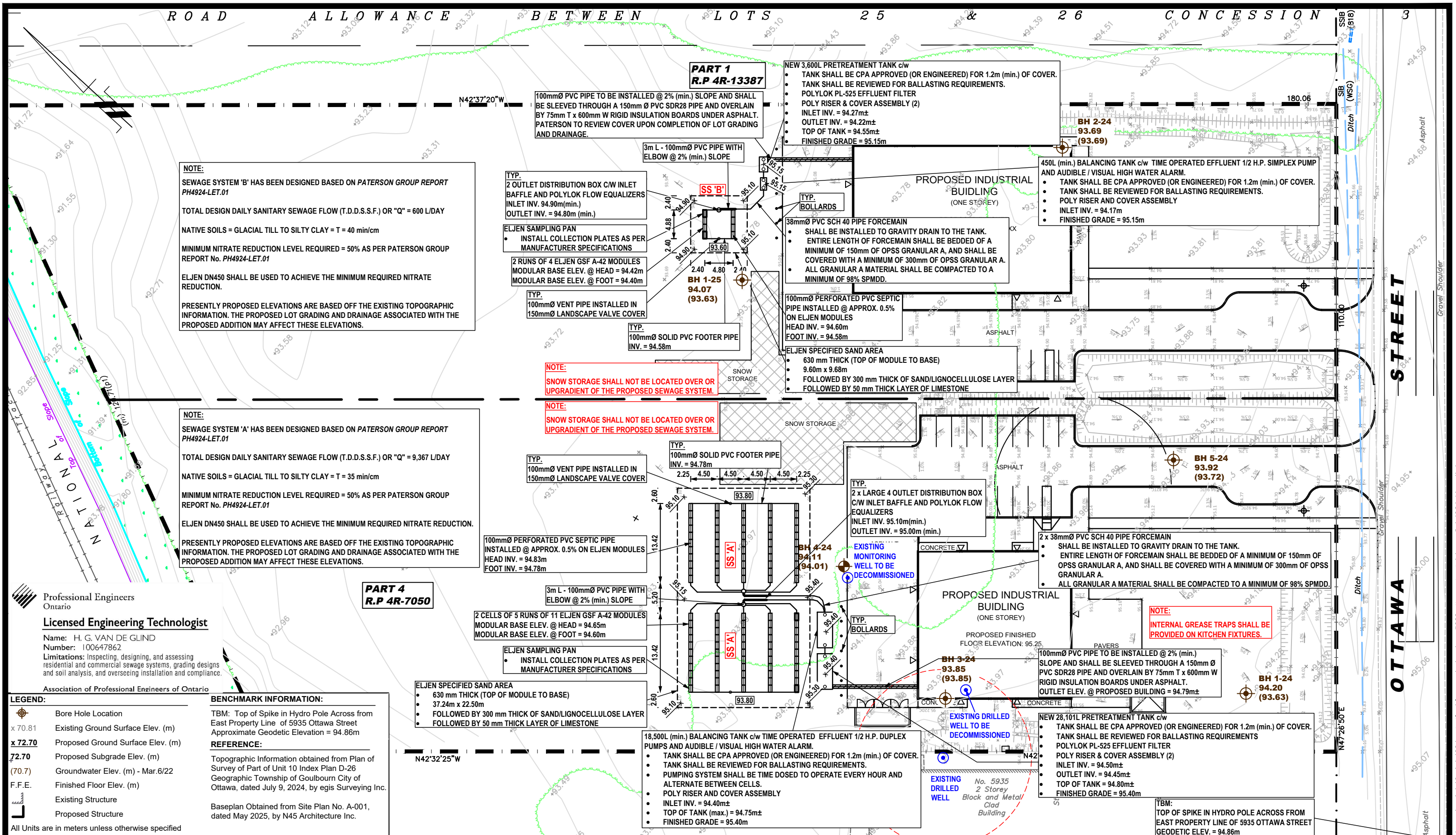
Manager, Septic System Approvals: [Signature] Permit Date: August 5, 2025

Comments: 1. Scarification inspection required prior to placement of sand fill.

☒ maintenance/pumping required ☒ ESA permit # required ☐ engineer to verify
☐ Class 5 Holding Tank approval only valid for three years from date of issue ☒ subgrade
☐ squirt height

Manager, Septic System Approvals: _____ Revision Date: _____

Comments: _____



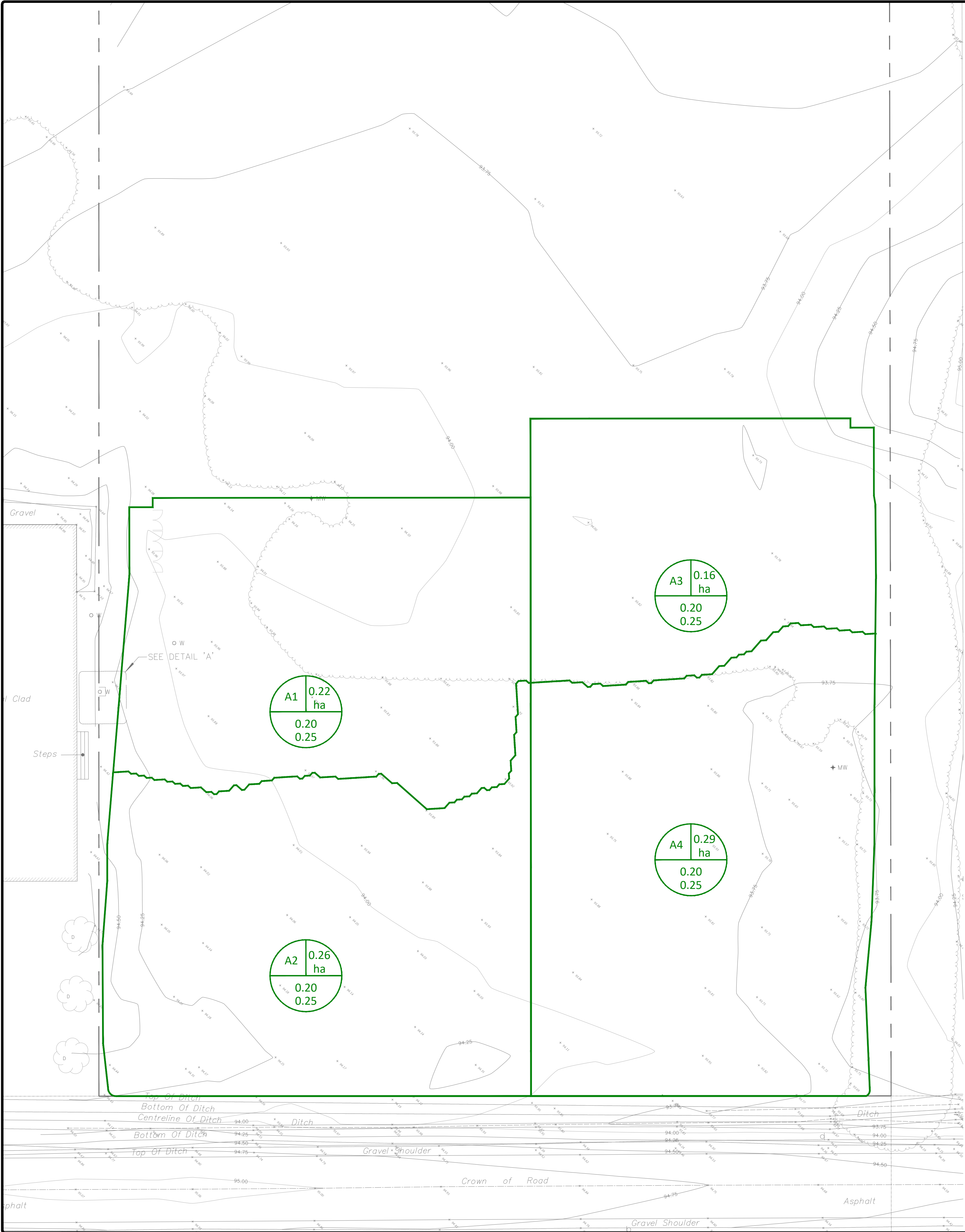
| | | | | | | | | | | | |
|--|----------|--|------|----------|---|----------|--|--------------|-----------------|-------------|----|
| <div>Consultant</div> <div><div>9 AURIGA DRIVE OTTAWA, ON K2E 7S9 TEL: (613) 226-7381</div></div> | 14/08/25 | Revised as per City of Ottawa Comments | 4 | Client: | STRATFORD FOXRUN | Drawing: | SEWAGE SYSTEM LAYOUT PLAN SEWAGE SYSTEM 'A' AND 'B' | Scale: | 1:600 | Drawn by: | HV |
| | 04/06/25 | Issued for Septic Permit | 3 | | | | | Date: | 08/2025 | Checked by: | MK |
| | 14/05/25 | Issued with Revised Site Plan | 2 | Project: | PROPOSED WAREHOUSE / RESTAURANT 5923 OTTAWA STREET OTTAWA (RICHMOND), ONTARIO | | | Drawing no.: | PH4924-1(rev.4) | | |
| | 03/10/24 | Issued with Revised Site Plan | 1 | | | | | | | | |
| | DD/MM/YY | Description | Rev. | | | | | | | | |



9 AURIGA DRIVE
OTTAWA, ON
K1E 7S9
TEL: (613) 226-7381

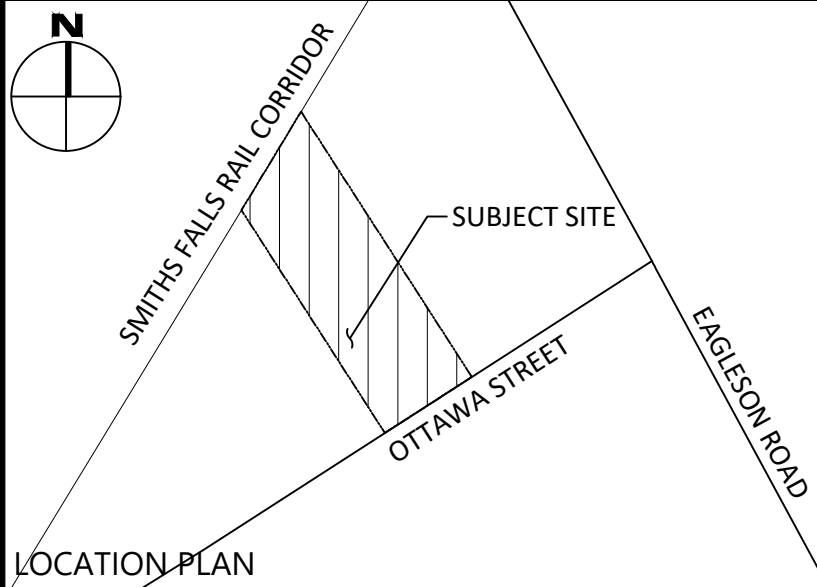
APPENDIX E PRE-DEVELOPMENT DRAINAGE PLAN

\\BAMAR_U\Infrastructure\2025\CCO-25-0415\99117756 Canada Inc. SPS Distillery & Warehouse_0303 Ottawa Street\12 Drawings\CCO-25-0415 - Presentation.dwg
User: JACQUES LEBLANC Date: 2025-06-11 10:00:00
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User: JACQUES LEBLANC Date: 2025-06-11 10:00:00

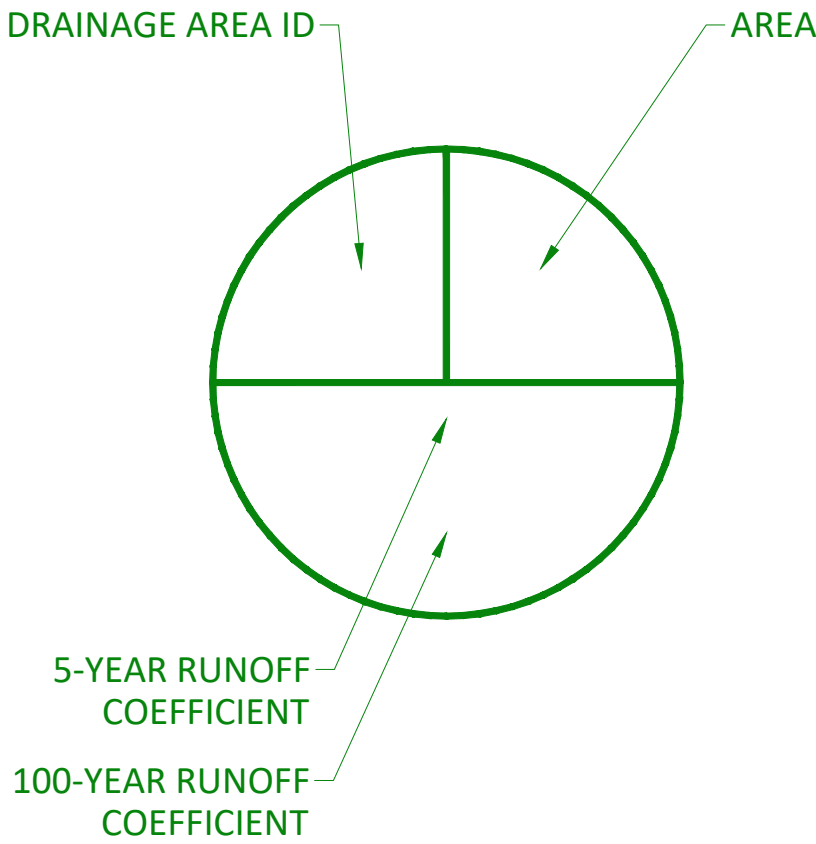


GENERAL NOTES

1. THE ORIGINAL TOPOGRAPHY, GROUND ELEVATION AND SURVEY DATA SHOWN ARE SUPPLIED FOR INFORMATION PURPOSES ONLY, AND IMPLY NO GUARANTEE OF ACCURACY. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO VERIFY ALL INFORMATION SHOWN.
2. THE CONTRACTOR IS TO OBTAIN AND PAY FOR ALL NECESSARY PERMITS AND APPROVALS FROM THE CITY BEFORE COMMENCING CONSTRUCTION.
3. THE CONTRACTOR IS RESPONSIBLE FOR ALL LAYOUT.
4. THE CONTRACTOR IS TO DETERMINE THE EXACT LOCATION, SIZE, MATERIAL AND ELEVATION OF ALL EXISTING UTILITIES PRIOR TO COMMENCING CONSTRUCTION. PROTECT AND ASSUME ALL RESPONSIBILITY FOR EXISTING UTILITIES WHETHER OR NOT SHOWN ON THESE DRAWINGS. IF THERE IS ANY DISCREPANCY THE CONTRACTOR IS TO NOTIFY THE ENGINEER PROMPTLY.
5. RESTORE ALL TRENCHES AND SURFACES OF PUBLIC ROAD ALLOWANCES TO CONDITION EQUAL OR BETTER THAN ORIGINAL CONDITION AND TO THE SATISFACTION OF THE CITY AUTHORITIES.
6. EXCAVATE AND DISPOSE OF ALL EXCESS EXCAVATED MATERIAL, SUCH AS ASPHALT, CURBING AND DEBRIS, OFF SITE AS DIRECTED BY THE ENGINEER AND THE CITY.
7. TOPSOIL TO BE STRIPPED AND STOCKPILED FOR REHABILITATION. CLEAN FILL TO BE PLACED IN FILL AREAS AND COMPACTED TO 95% STANDARD PROCTOR DENSITY.
8. CONTRACTOR TO MINIMIZE THE ACTUAL LIMITS OF REMOVALS AND DISTURBED AREA WHEREVER POSSIBLE, AND SHALL MAKE THEIR OWN JUDGEMENT AND ACCOUNT FOR ALL MATERIAL AND LABOUR REQUIRED FOR ADEQUATELY REINSTATING THE AREA TO PRE-CONSTRUCTION CONDITIONS OR BETTER, AND BEAR THE COST OF THE SAME. NO ADDITIONAL PAYMENT WILL BE MADE FOR REINSTATEMENT WORK NOT SHOWN ON THE CONTRACT DRAWING AS A DIRECT RESULT FROM CONSTRUCTION.
9. ALL DISTURBED AREAS TO BE RESTORED TO ORIGINAL CONDITION OR BETTER UNLESS OTHERWISE SPECIFIED.
10. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL TRAFFIC CONTROL AND SAFETY MEASURES DURING THE CONSTRUCTION PERIOD, INCLUDING THE SUPPLY, INSTALLATION, AND REMOVAL OF ALL NECESSARY SIGNAGE, DELINEATORS, MARKERS AND BARRIERS.
11. DO NOT ALTER GRADING OF THE SITE WITHOUT PRIOR APPROVAL OF THE ENGINEER/CITY.
12. ALL ROADWAY, PARKING LOT, AND GRADING WORKS TO BE UNDERTAKEN IN ACCORDANCE WITH CITY STANDARDS AND SPECIFICATIONS. THE CONTRACTOR IS TO PROVIDE POSITIVE DRAINAGE AWAY FROM THE BUILDING.
13. CONTACT THE CITY FOR INSPECTION OF ROUGH GRADING OF PARKING LOTS, ROADWAYS AND LANDSCAPED AREAS PRIOR TO PLACEMENT OF ASPHALT AND TOPSOIL. ALL DEFICIENCIES NOTED SHALL BE RECTIFIED TO THE CITY'S SATISFACTION PRIOR TO PLACEMENT OF ANY ASPHALT, TOPSOIL, SEED & MULCH AND/OR SOD.
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 - GAS SERVICE - ENBRIDGE,
 - TELEPHONE SERVICE - BELL CANADA,
 - TELEVISION SERVICE - ROGERS.
16. INSTALLATION TO BE IN ACCORDANCE WITH CURRENT CODES AND STANDARDS OF APPROVAL AGENCIES HYDRO ONE, BELL AND THE CITY.
17. CONTRACTOR TO ENSURE ALL APPLICABLE OPS SPECIFICATIONS ARE FOLLOWED DURING CONSTRUCTION.
18. ALL PROPOSED CURB TO BE CONCRETE BARRIER CURB UNLESS OTHERWISE SPECIFIED.



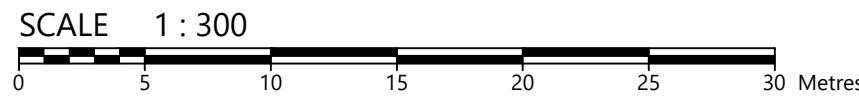
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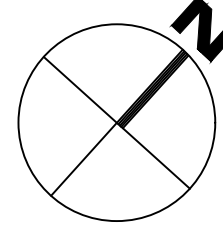
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| 2 | ISSUED FOR REVIEW | AUG. 12, 2025 |
| 1 | ISSUED FOR SITE PLAN CONTROL | JUN. 06, 2025 |
| No. | Revisions | Date |

Check and verify all dimensions before proceeding with the work. Do not scale drawings



115 Walgreen Road, R.R.3
Carp, ON K0A 1L0
Tel: 613-836-2184
Fax: 613-836-3742
www.egis-group.com



Stamp:

Client:

99117756 CANADA INC.
411 LEGGET DRIVE, SUITE 710
OTTAWA, ON K2K 3C9

Project:

DISTILLERY & WAREHOUSE
5923 OTTAWA STREET

Drawing Title:

PRE-DEVELOPMENT DRAINAGE AREA PLAN

Scale:

1:300

Drawn By:

FV

Checked By:

AG

Designed By:

AG

Project Number:

CCO-25-0415

Drawing Number:

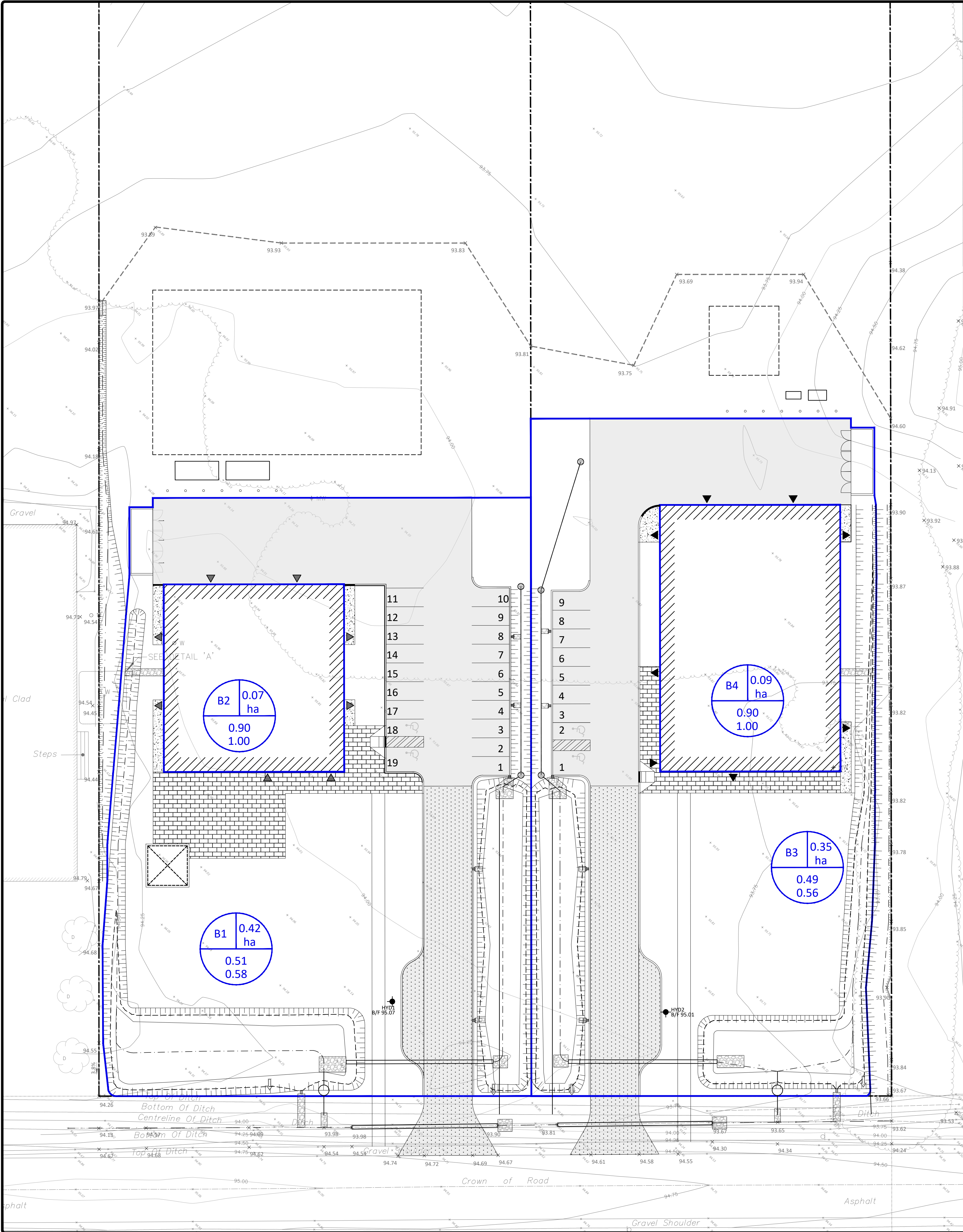
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D07-12-25-0078

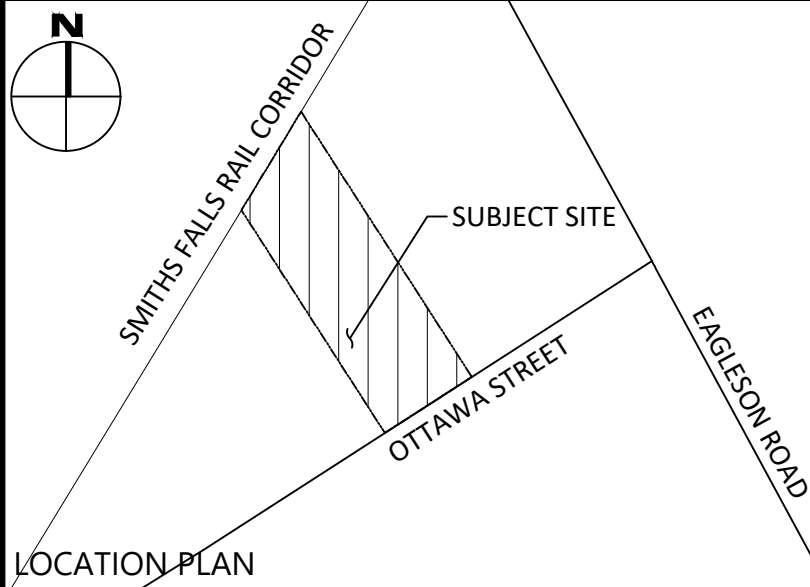
APPENDIX F POST-DEVELOPMENT DRAINAGE PLAN

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User: J. F. FORTIN (J. Fortin) Date: 11/20/2023 11:51:00 AM Plot Date: 11/20/2023 11:51:00 AM Plot By: J. F. FORTIN (J. Fortin) Plot Scale: 1:300
\\na\m\l\Infrastructure\2025\CCO-25-0415\99117756 Canada Inc. SPS Distillery & Warehouse_2023 Ottawa Street\12 - Drawings\CCO-25-0415 - Presentation.dwg

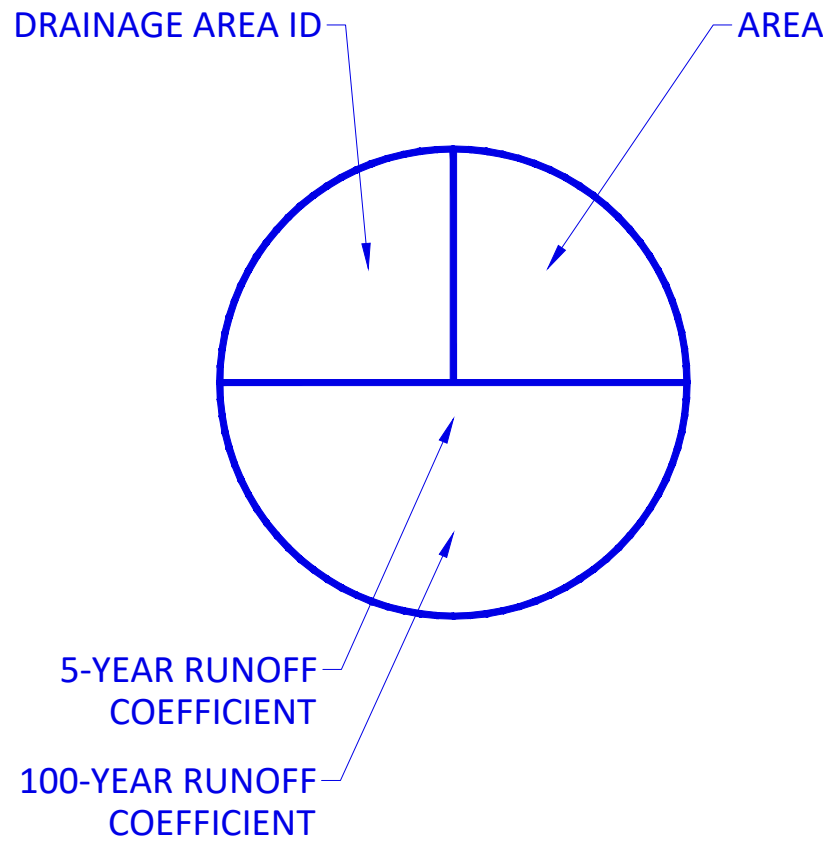


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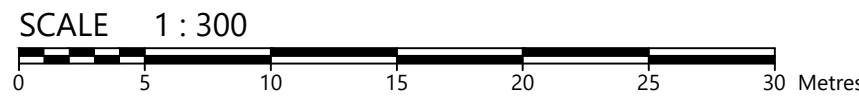
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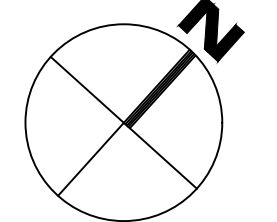
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| 2 | ISSUED FOR REVIEW | AUG. 11, 2025 |
| 1 | ISSUED FOR SITE PLAN CONTROL | JUN. 06, 2025 |
| No. | Revisions | Date |

Check and verify all dimensions before proceeding with the work. Do not scale drawings.



115 Walgreen Road, R.R.3
Carp, ON K0A 1L0
Tel: 613-836-2184
Fax: 613-836-3742
www.egis-group.com



Stamp:

Client:
99117756 CANADA INC.
411 LEGGET DRIVE, SUITE 710
OTTAWA, ON K2K 3C9

Project:
DISTILLERY & WAREHOUSE
5923 OTTAWA STREET

Drawing Title:
POST-DEVELOPMENT DRAINAGE AREA PLAN

| | | | |
|--------------|-------|-----------------|-------------|
| Scale: | 1:300 | Project Number: | CCO-25-0415 |
| Drawn By: | FV | Drawing Number: | POST |
| Checked By: | AG | | |
| Designed By: | AG | | |

#XXXXX

D07-12-25-0078

APPENDIX G STORMWATER MANAGEMENT CALCULATIONS

| Tc (min) | Intensity (mm/ hr) | | |
|-------------|-----------------------|--------|----------|
| | 2-Year | 5-Year | 100-Year |
| 20 | 52.0 | 70.3 | 120.0 |
| 10 | 76.8 | 104.2 | 178.6 |

| C-Values | |
|------------|------|
| Impervious | 0.90 |
| Gravel | 0.60 |
| Pervious | 0.20 |

Pre-Development Runoff Coefficient

| Drainage Area | Impervious Area (m ²) | Gravel (m ²) | Pervious Area (m ²) | Average C (2-Year) | Average C (100-Year) |
|---------------|-----------------------------------|--------------------------|---------------------------------|--------------------|----------------------|
| A1 | 0 | 0 | 2,219 | 0.20 | 0.25 |
| A2 | 0 | 0 | 2,583 | 0.20 | 0.25 |

Ph.1 Drainage to Rear Yard
Ph.1 Drainage to Ottawa Street

Pre-Development Runoff Calculations

| Drainage Area | Area (ha) | C 2/ 5-Year | C 100-Year |
|---------------|-----------|-------------|------------|
| A1 | 0.222 | 0.20 | 0.25 |
| A2 | 0.258 | 0.20 | 0.25 |
| Total | 0.480 | | |

Ph.1 Drainage to Rear Yard
Ph.1 Drainage to Ottawa Street

Post-Development Runoff Coefficient

| Drainage Area | Impervious Area (m ²) | Gravel (m ²) | Pervious Area (m ²) | Average C (2-year) | Average C (100-year) |
|---------------|-----------------------------------|--------------------------|---------------------------------|--------------------|----------------------|
| B1 | 1,844 | 0 | 2,307 | 0.51 | 0.58 |
| B2 | 651 | 0 | 0 | 0.90 | 1.00 |

Ph.1 Surface Restricted
Ph.2 Building - Restricted

Post-Development Runoff Calculations

| Drainage Area | Area (ha) | C 2-Year | C 100-Year |
|---------------|-----------|----------|------------|
| B1 | 0.415 | 0.51 | 0.58 |
| B2 | 0.065 | 0.90 | 1.00 |
| Total | 0.480 | | |

Ph.1 Surface Restricted
Ph.2 Building - Restricted

| Tc (min) | Intensity (mm/ hr) | | |
|-------------|-----------------------|--------|----------|
| | 2-Year | 5-Year | 100-Year |
| 20 | 52.0 | 70.3 | 120.0 |
| 10 | 76.8 | 104.2 | 178.6 |

| C-Values | |
|------------|------|
| Impervious | 0.90 |
| Gravel | 0.60 |
| Pervious | 0.20 |

Pre-Development Runoff Coefficient

| Drainage Area | Impervious Area (m ²) | Gravel (m ²) | Pervious Area (m ²) | Average C (2-Year) | Average C (100-Year) | |
|---------------|-----------------------------------|--------------------------|---------------------------------|--------------------|----------------------|--------------------------------|
| A3 | 0 | 0 | 1,604 | 0.20 | 0.25 | Ph.2 Drainage to Rear Yard |
| A4 | 0 | 0 | 2,858 | 0.20 | 0.25 | Ph.2 Drainage to Ottawa Street |

Pre-Development Runoff Calculations

| Drainage Area | Area (ha) | C 2/ 5-Year | C 100-Year | |
|---------------|-----------|-------------|------------|--------------------------------|
| A3 | 0.160 | 0.20 | 0.25 | Ph.2 Drainage to Rear Yard |
| A4 | 0.286 | 0.20 | 0.25 | Ph.2 Drainage to Ottawa Street |
| Total | 0.446 | | | |

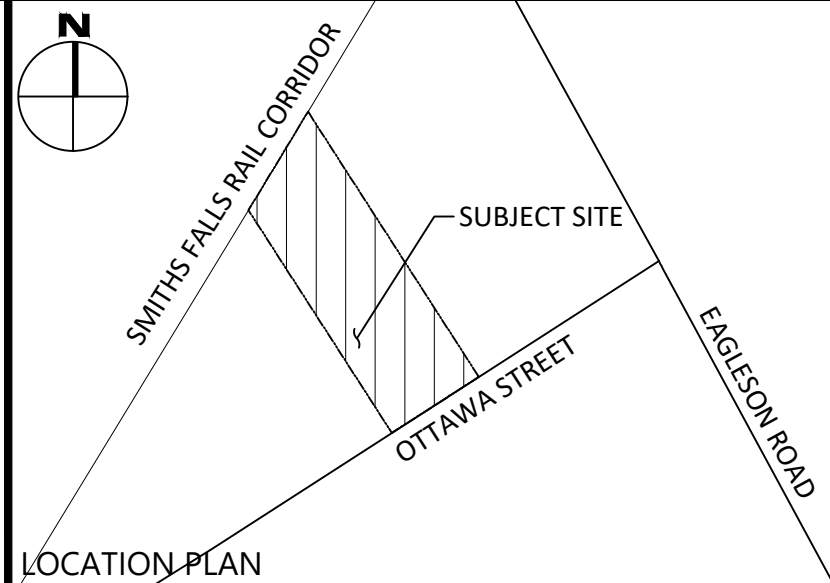
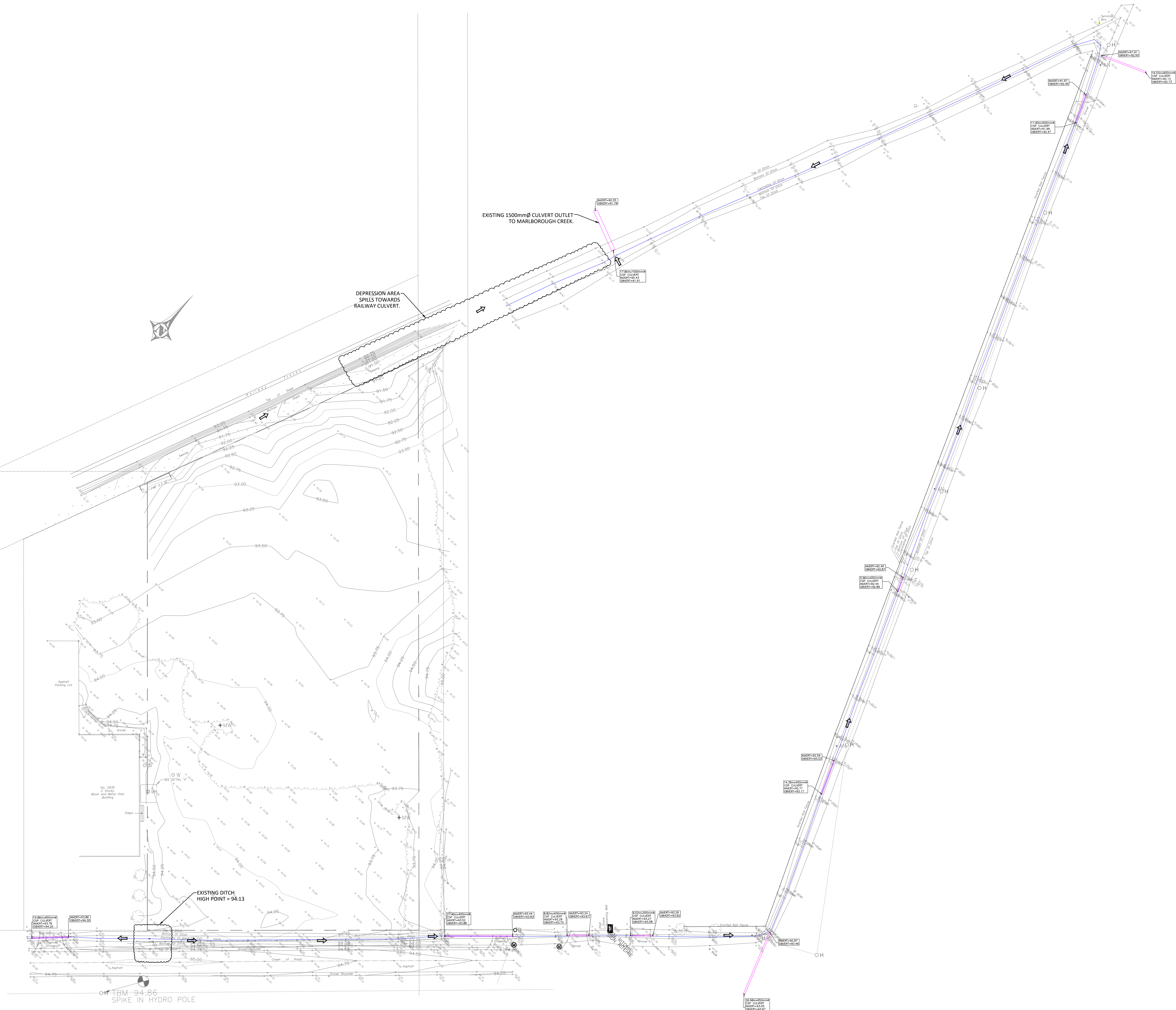
Post-Development Runoff Coefficient

| Drainage Area | Impervious Area (m ²) | Gravel (m ²) | Pervious Area (m ²) | Average C (2-year) | Average C (100-year) | |
|---------------|-----------------------------------|--------------------------|---------------------------------|--------------------|----------------------|----------------------------|
| B3 | 1,460 | 0 | 2,076 | 0.49 | 0.56 | Ph.2 Surface Restricted |
| B4 | 926 | 0 | 0 | 0.90 | 1.00 | Ph.2 Building - Restricted |

Post-Development Runoff Calculations

| Drainage Area | Area (ha) | C 2-Year | C 100-Year | |
|---------------|-----------|----------|------------|----------------------------|
| B3 | 0.354 | 0.49 | 0.56 | Ph.2 Surface Restricted |
| B4 | 0.093 | 0.90 | 1.00 | Ph.2 Building - Restricted |
| Total | 0.446 | | | |

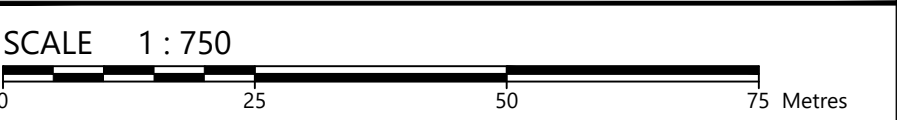
\\na\eng\1\Infrastructure\2025\CCO-25-0415\99117756 Canada Inc. SPS Distillery & Warehouse, 5923 Ottawa Street\12 Drawings\Drawings\Figures\CCO-25-0415 - Presentation - Ditch.dwg
User: C104 Date: 2025-08-07 10:25:13 Titled: C104.dwg Plot Date: 2025-08-07 10:25:13 Plot User: C104



- LEGEND
- DRAINAGE DIRECTION
 - DRAINAGE DITCH
 - EXISTING CULVERT

FOR REVIEW ONLY
NOT FOR CONSTRUCTION

| | | |
|---|-------------------|---------------|
| | | |
| | | |
| | | |
| | | |
| | | |
| | | |
| 1 | ISSUED FOR REVIEW | AUG. 07, 2025 |
| No. | Revisions | Date |
| Check and verify all dimensions before proceeding with the work. Do not scale drawings. | | |



115 Walgreen Road, R.R.3
Carp, ON K0A 1L0
Tel: 613-836-2184
Fax: 613-836-3742
www.egis-group.com

Stamp:

Client:
99117756 CANADA INC.
411 LEGGET DRIVE, SUITE 710
OTTAWA, ON K2K 3C9

Project:
DISTILLERY & WAREHOUSE
5923 OTTAWA STREET

Drawing Title:
EXISTING DITCH DRAINAGE FIGURE

| | | | |
|--------------|-------|-----------------|-------------|
| Scale: | 1:750 | Project Number: | CCO-25-0415 |
| Drawn By: | FV | Drawing Number: | C104 |
| Checked By: | CJM | | |
| Designed By: | FV | | |

D07-12-XX-XXXX

#XXXXX



Adjustable Accutrol Weir

Tag: _____

Adjustable Flow Control for Roof Drains

ADJUSTABLE ACCUTROL (for Large Sump Roof Drains only)

For more flexibility in controlling flow with heads deeper than 2", Watts Drainage offers the Adjustable Accutrol. The Adjustable Accutrol Weir is designed with a single parabolic opening that can be covered to restrict flow above 2" of head to less than 5 gpm per inch, up to 6" of head. To adjust the flow rate for depths over 2" of head, set the slot in the adjustable upper cone according to the flow rate required. Refer to Table 1 below.

Note: Flow rates are directly proportional to the amount of weir opening that is exposed.

EXAMPLE:

For example, if the adjustable upper cone is set to cover 1/2 of the weir opening, flow rates above 2" of head will be restricted to 2-1/2 gpm per inch of head.

Therefore, at 3" of head, the flow rate through the Accutrol Weir that has 1/2 the slot exposed will be:
[5 gpm (per inch of head) x 2 inches of head] + 2-1/2 gpm (for the third inch of head) = 12-1/2 gpm.

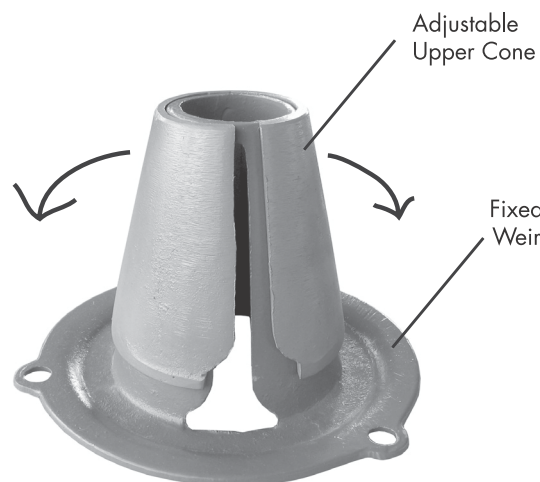
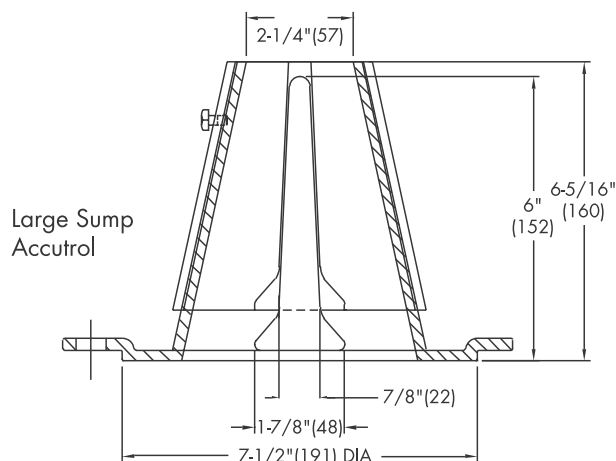


TABLE 1. Adjustable Accutrol Flow Rate Settings

| Weir Opening Exposed | 1" | 2" | 3" | 4" | 5" | 6" |
|----------------------|--------------------------------|----|-------|------|-------|----|
| | Flow Rate (gallons per minute) | | | | | |
| Fully Exposed | 5 | 10 | 15 | 20 | 25 | 30 |
| 3/4 | 5 | 10 | 13.75 | 17.5 | 21.25 | 25 |
| 1/2 | 5 | 10 | 12.5 | 15 | 17.5 | 20 |
| 1/4 | 5 | 10 | 11.25 | 12.5 | 13.75 | 15 |
| Closed | 5 | 5 | 5 | 5 | 5 | 5 |

Job Name _____

Contractor _____

Job Location _____

Contractor's P.O. No. _____

Engineer _____

Representative _____

Watts product specifications in U.S. customary units and metric are approximate and are provided for reference only. For precise measurements, please contact Watts Technical Service. Watts reserves the right to change or modify product design, construction, specifications, or materials without prior notice and without incurring any obligation to make such changes and modifications on Watts products previously or subsequently sold.

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A Watts Water Technologies Company

Stormceptor®EF Sizing Report

| | | | |
|---|----------------|---|--|
| Imbrium®Systems | | | |
| ESTIMATED NET ANNUAL SEDIMENT (TSS) LOAD REDUCTION | | | |
| 08/14/2025 | | | |
| Province: | Ontario | Project Name: | 5923 Ottawa St. (Distillery and Warehouse) |
| City: | Ottawa | Project Number: | COO-25-0415 |
| Nearest Rainfall Station: | OTTAWA CDA RCS | Designer Name: | Jessica Steffler |
| Climate Station Id: | 6105978 | Designer Company: | Forterra Pipe & Precast |
| Years of Rainfall Data: | 20 | Designer Email: | jessica.steffler@RinkerPipe.com |
| Site Name: | Phase 1 | Designer Phone: | 519-239-6958 |
| Drainage Area (ha): | 0.48 | EOR Name: | Francis VALENTI |
| Runoff Coefficient 'c': | 0.59 | EOR Company: | EGIS |
| Particle Size Distribution: | CA ETV | EOR Email: | Francis.VALENTI@egis-group.com |
| Target TSSRemoval (%): | 60.0 | EOR Phone: | 613-714-6895 |
| Required Water Quality Runoff Volume Capture (%): | 90.00 | Net Annual Sediment (TSS) Load Reduction Sizing Summary | |
| Estimated Water Quality Flow Rate (L/s): | 9.14 | Stormceptor Model | TSS Removal Provided (%) |
| Oil / Fuel Spill Risk Site? | Yes | EFO4 | 60 |
| Upstream Flow Control? | No | EFO5 | 63 |
| Peak Conveyance (maximum) Flow Rate (L/s): | 18.00 | EFO6 | 65 |
| Influent TSSConcentration (mg/L): | 200 | EFO8 | 68 |
| Estimated Average Annual Sediment Load (kg/yr): | 189 | EFO10 | 69 |
| Estimated Average Annual Sediment Volume (L/yr): | 154 | EFO12 | 70 |
| Recommended Stormceptor EFO Model: | | EFO4 | |
| Estimated Net Annual Sediment (TSS) Load Reduction (%): | | 60 | |
| Water Quality Runoff Volume Capture (%): | | > 90 | |



Stormceptor®EF Sizing Report

THIRD-PARTY TESTING AND VERIFICATION

► Stormceptor®EF and Stormceptor®EFO are the latest evolutions in the Stormceptor®oil-grit separator (OGS) technology series, and are designed to remove a wide variety of pollutants from stormwater and snowmelt runoff. These technologies have been third-party tested in accordance with the Canadian ETV Procedure for Laboratory Testing of Oil-Grit Separators and performance has been third-party verified in accordance with the ISO 14034 Environmental Technology Verification (ETV) protocol.

PERFORMANCE

► Stormceptor®EF and EFO remove stormwater pollutants through gravity separation and floatation, and feature a patent-pending design that generates positive removal of total suspended solids (TSS) throughout each storm event, including high-intensity storms. Captured pollutants include sediment, free oils, and sediment-bound pollutants such as nutrients, heavy metals, and petroleum hydrocarbons. Stormceptor is sized to remove a high level of TSS from the frequent rainfall events that contribute the vast majority of annual runoff volume and pollutant load. The technology incorporates an internal bypass to convey excessive stormwater flows from high-intensity storms through the device without resuspension and washout (scour) of previously captured pollutants. Proper routine maintenance ensures high pollutant removal performance and protection of downstream waterways.

PARTICLE SIZE DISTRIBUTION (PSD)

► The Canadian ETV PSD shown in the table below was used, or in part, for this sizing. This is the identical PSD that is referenced in the Canadian ETV Procedure for Laboratory Testing of Oil-Grit Separators for both sediment removal testing and scour testing. The Canadian ETV PSD contains a wide range of particle sizes in the sand and silt fractions, and is considered reasonably representative of the particle size fractions found in typical urban stormwater runoff.

| Particle Size (µm) | Percent Less Than | Particle Size Fraction (µm) | Percent |
|--------------------|-------------------|-----------------------------|---------|
| 1000 | 100 | 500-1000 | 5 |
| 500 | 95 | 250-500 | 5 |
| 250 | 90 | 150-250 | 15 |
| 150 | 75 | 100-150 | 15 |
| 100 | 60 | 75-100 | 10 |
| 75 | 50 | 50-75 | 5 |
| 50 | 45 | 20-50 | 10 |
| 20 | 35 | 8-20 | 15 |
| 8 | 20 | 5-8 | 10 |
| 5 | 10 | 2-5 | 5 |
| 2 | 5 | <2 | 5 |



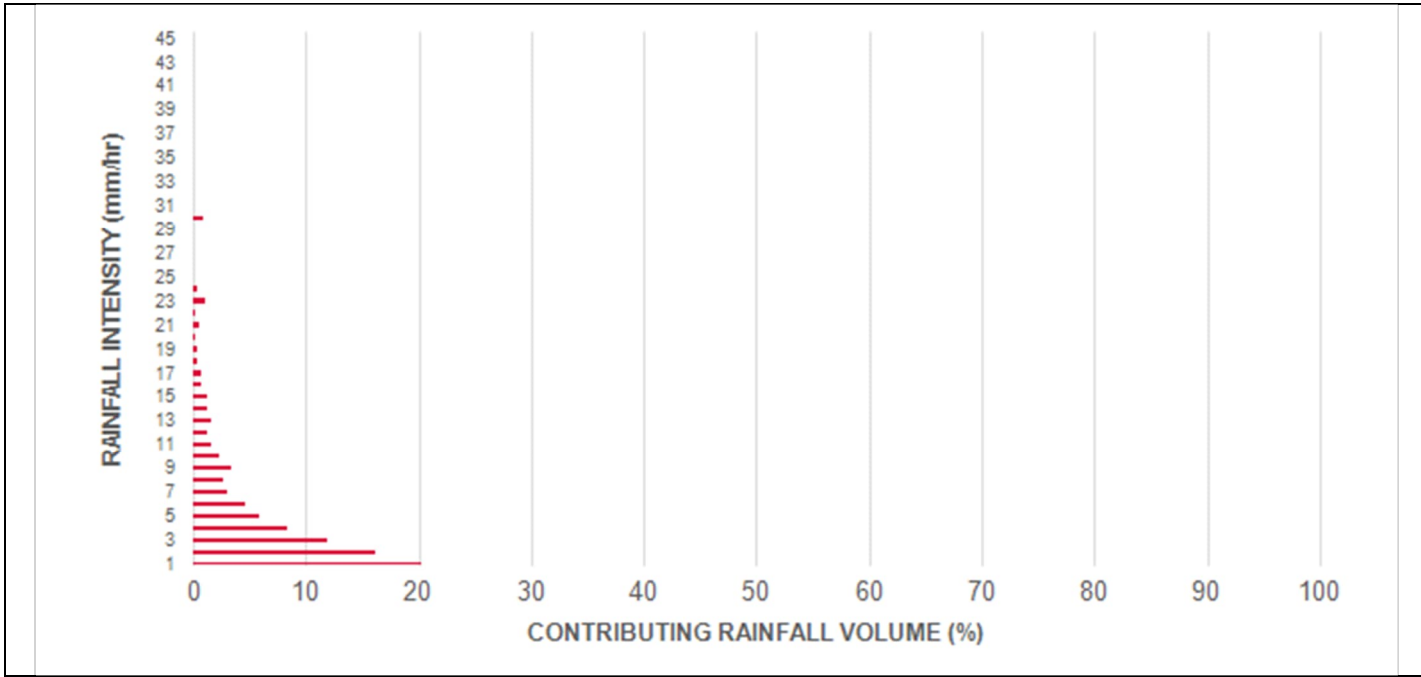
Stormceptor®EF Sizing Report

| Rainfall Intensity (mm / hr) | Percent Rainfall Volume (%) | Cumulative Rainfall Volume (%) | Flow Rate (L/s) | Flow Rate (L/min) | Surface Loading Rate (L/min/ m²) | Removal Efficiency (%) | Incremental Removal (%) | Cumulative Removal (%) |
|--|-----------------------------|--------------------------------|-----------------|-------------------|----------------------------------|------------------------|-------------------------|------------------------|
| 0.50 | 8.6 | 8.6 | 0.39 | 24.0 | 20.0 | 70 | 6.1 | 6.1 |
| 1.00 | 20.3 | 29.0 | 0.79 | 47.0 | 39.0 | 70 | 14.3 | 20.4 |
| 2.00 | 16.2 | 45.2 | 1.57 | 94.0 | 79.0 | 66 | 10.6 | 31.0 |
| 3.00 | 12.0 | 57.2 | 2.36 | 142.0 | 118.0 | 62 | 7.4 | 38.4 |
| 4.00 | 8.4 | 65.6 | 3.15 | 189.0 | 157.0 | 58 | 4.9 | 43.3 |
| 5.00 | 5.9 | 71.6 | 3.94 | 236.0 | 197.0 | 55 | 3.3 | 46.6 |
| 6.00 | 4.6 | 76.2 | 4.72 | 283.0 | 236.0 | 53 | 2.5 | 49.0 |
| 7.00 | 3.1 | 79.3 | 5.51 | 331.0 | 276.0 | 52 | 1.6 | 50.6 |
| 8.00 | 2.7 | 82.0 | 6.30 | 378.0 | 315.0 | 51 | 1.4 | 52.0 |
| 9.00 | 3.3 | 85.3 | 7.09 | 425.0 | 354.0 | 50 | 1.7 | 53.7 |
| 10.00 | 2.3 | 87.6 | 7.87 | 472.0 | 394.0 | 48 | 1.1 | 54.8 |
| 11.00 | 1.6 | 89.2 | 8.66 | 520.0 | 433.0 | 47 | 0.7 | 55.5 |
| 12.00 | 1.3 | 90.5 | 9.45 | 567.0 | 472.0 | 46 | 0.6 | 56.1 |
| 13.00 | 1.7 | 92.2 | 10.23 | 614.0 | 512.0 | 45 | 0.8 | 56.9 |
| 14.00 | 1.2 | 93.5 | 11.02 | 661.0 | 551.0 | 44 | 0.5 | 57.4 |
| 15.00 | 1.2 | 94.6 | 11.81 | 709.0 | 590.0 | 42 | 0.5 | 57.9 |
| 16.00 | 0.7 | 95.3 | 12.60 | 756.0 | 630.0 | 42 | 0.3 | 58.2 |
| 17.00 | 0.7 | 96.1 | 13.38 | 803.0 | 669.0 | 42 | 0.3 | 58.5 |
| 18.00 | 0.4 | 96.5 | 14.17 | 850.0 | 709.0 | 42 | 0.2 | 58.7 |
| 19.00 | 0.4 | 96.9 | 14.96 | 898.0 | 748.0 | 41 | 0.2 | 58.8 |
| 20.00 | 0.2 | 97.1 | 15.75 | 945.0 | 787.0 | 41 | 0.1 | 58.9 |
| 21.00 | 0.5 | 97.5 | 16.53 | 992.0 | 827.0 | 41 | 0.2 | 59.1 |
| 22.00 | 0.2 | 97.8 | 17.32 | 1039.0 | 866.0 | 41 | 0.1 | 59.2 |
| 23.00 | 1.0 | 98.8 | 18.11 | 1086.0 | 905.0 | 41 | 0.4 | 59.6 |
| 24.00 | 0.3 | 99.1 | 18.90 | 1134.0 | 945.0 | 40 | 0.1 | 59.7 |
| 25.00 | 0.0 | 99.1 | 19.68 | 1181.0 | 984.0 | 40 | 0.0 | 59.7 |
| 30.00 | 0.9 | 100.0 | 23.62 | 1417.0 | 1181.0 | 37 | 0.3 | 60.1 |
| 35.00 | 0.0 | 100.0 | 27.56 | 1653.0 | 1378.0 | 34 | 0.0 | 60.1 |
| 40.00 | 0.0 | 100.0 | 31.49 | 1890.0 | 1575.0 | 30 | 0.0 | 60.1 |
| 45.00 | 0.0 | 100.0 | 35.43 | 2126.0 | 1771.0 | 27 | 0.0 | 60.1 |
| Estimated Net Annual Sediment (TSS) Load Reduction = | | | | | | | | 60 % |

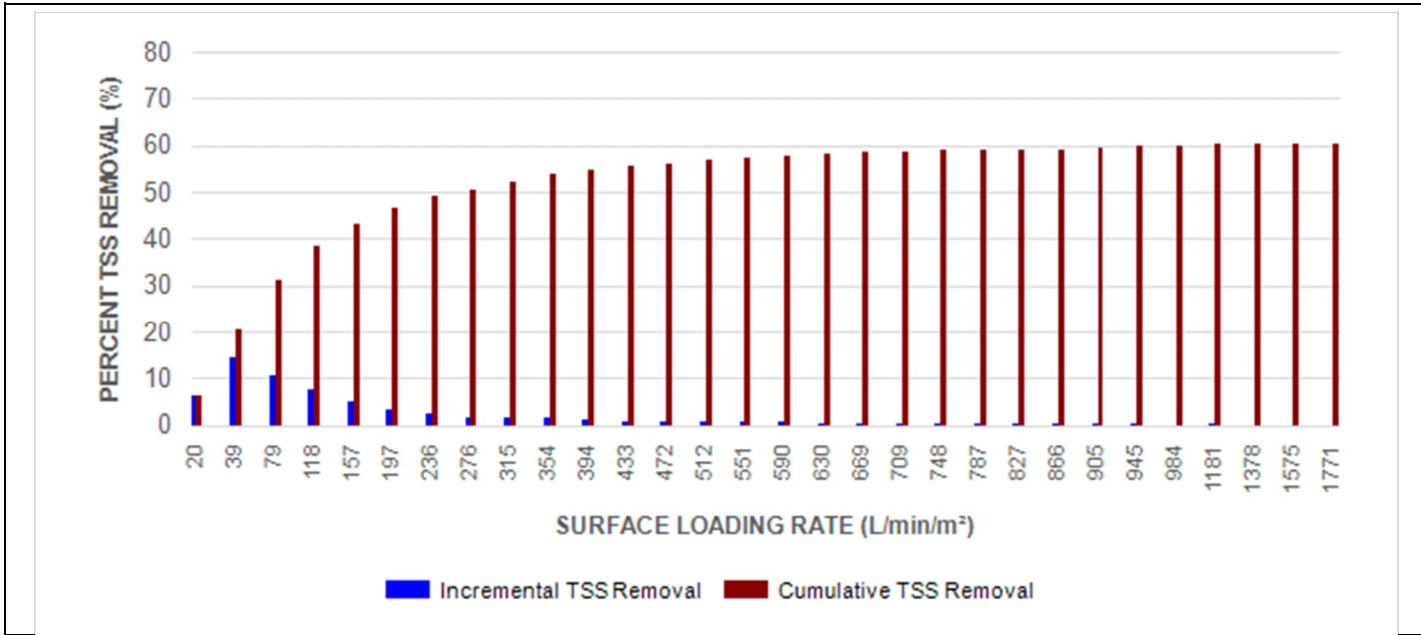
Climate Station ID: 6105978 Years of Rainfall Data: 20

Stormceptor®EF Sizing Report

RAINFALL DATA FROM OTTAWA CDA RCS RAINFALL STATION



INCREMENTAL AND CUMULATIVE TSS REMOVAL
FOR THE RECOMMENDED STORMCEPTOR® MODEL



Stormceptor®EF Sizing Report

Maximum Pipe Diameter / Peak Conveyance

| Stormceptor EF / EFO | Model Diameter | | Min Angle Inlet / Outlet Pipes | Max Inlet Pipe Diameter | | Max Outlet Pipe Diameter | | Peak Conveyance Flow Rate | |
|-------------------------|----------------|------|-----------------------------------|----------------------------|------|-----------------------------|------|------------------------------|-------|
| | (m) | (ft) | | (mm) | (in) | (mm) | (in) | (L/s) | (cfs) |
| EF4 / EFO4 | 1.2 | 4 | 90 | 609 | 24 | 609 | 24 | 425 | 15 |
| EF5 / EFO5 | 1.5 | 5 | 90 | 762 | 30 | 762 | 30 | 710 | 25 |
| EF6 / EFO6 | 1.8 | 6 | 90 | 914 | 36 | 914 | 36 | 990 | 35 |
| EF8 / EFO8 | 2.4 | 8 | 90 | 1219 | 48 | 1219 | 48 | 1700 | 60 |
| EF10 / EFO10 | 3.0 | 10 | 90 | 1828 | 72 | 1828 | 72 | 2830 | 100 |
| EF12 / EFO12 | 3.6 | 12 | 90 | 1828 | 72 | 1828 | 72 | 2830 | 100 |

SCOUR PREVENTION AND ONLINE CONFIGURATION

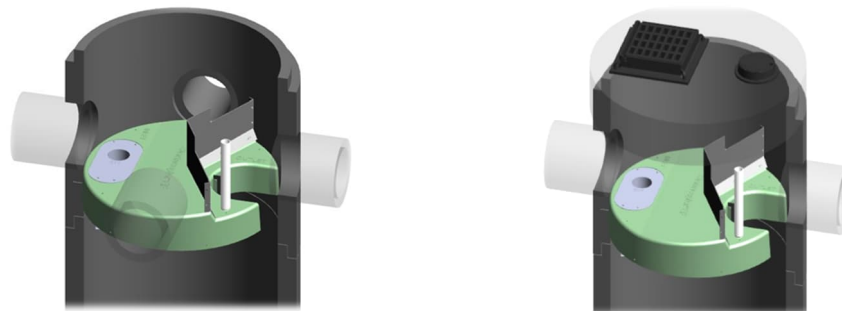
► Stormceptor®EF and EFO feature an internal bypass and superior scour prevention technology that have been demonstrated in third-party testing according to the scour testing provisions of the Canadian ETV Procedure for Laboratory Testing of Oil-Grit Separators, and the exceptional scour test performance has been third-party verified in accordance with the ISO 14034 ETV protocol. As a result, Stormceptor EF and EFO are approved for online installation, eliminating the need for costly additional bypass structures, piping, and installation expense.

DESIGN FLEXIBILITY

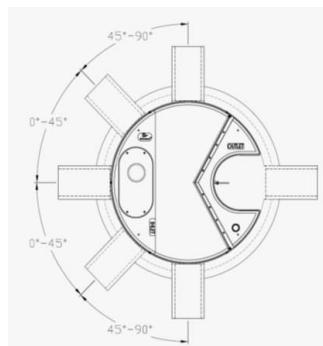
► Stormceptor®EF and EFO offers design flexibility in one simplified platform, accepting stormwater flow from a single inlet pipe or multiple inlet pipes, and/or surface runoff through an inlet grate. The device can also serve as a junction structure, accommodate a 90-degree inlet-to-outlet bend angle, and can be modified to ensure performance in submerged conditions.

OIL CAPTURE AND RETENTION

► While Stormceptor®EF will capture and retain oil from dry weather spills and low intensity runoff, Stormceptor®EFO has demonstrated superior oil capture and greater than 99% oil retention in third-party testing according to the light liquid re-entrainment testing provisions of the Canadian ETV Procedure for Laboratory Testing of Oil-Grit Separators. Stormceptor EFO is recommended for sites where oil capture and retention is a requirement.



Stormceptor®EF Sizing Report



INLET-TO-OUTLET DROP

Elevation differential between inlet and outlet pipe inverts is dictated by the angle at which the inlet pipe(s) enters the unit.

0° - 45° : The inlet pipe is 1-inch (25mm) higher than the outlet pipe.

45° - 90° : The inlet pipe is 2-inches (50mm) higher than the outlet pipe.

HEAD LOSS

The head loss through Stormceptor EF is similar to that of a 60-degree bend structure. The applicable K value for calculating minor losses through the unit is 1.1. For submerged conditions the applicable K value is 3.0.

Pollutant Capacity

| Stormceptor EF / EFO | Model Diameter | | Depth (Outlet Pipe Invert to Sump Floor) | | Oil Volume | | Recommended Sediment Maintenance Depth * | | Maximum Sediment Volume * | | Maximum Sediment Mass ** | |
|-------------------------|-------------------|------|--|------|------------|-------|--|------|------------------------------|-------|-----------------------------|--------|
| | (m) | (ft) | (m) | (ft) | (L) | (Gal) | (mm) | (in) | (L) | (ft³) | (kg) | (lb) |
| EF4 / EFO4 | 1.2 | 4 | 1.52 | 5.0 | 265 | 70 | 203 | 8 | 1190 | 42 | 1904 | 5250 |
| EF5 / EFO5 | 1.5 | 5 | 1.62 | 5.3 | 420 | 111 | 305 | 10 | 2124 | 75 | 2612 | 5758 |
| EF6 / EFO6 | 1.8 | 6 | 1.93 | 6.3 | 610 | 160 | 305 | 12 | 3470 | 123 | 5552 | 15375 |
| EF8 / EFO8 | 2.4 | 8 | 2.59 | 8.5 | 1070 | 280 | 610 | 24 | 8780 | 310 | 14048 | 38750 |
| EF10 / EFO10 | 3.0 | 10 | 3.25 | 10.7 | 1670 | 440 | 610 | 24 | 17790 | 628 | 28464 | 78500 |
| EF12 / EFO12 | 3.6 | 12 | 3.89 | 12.8 | 2475 | 655 | 610 | 24 | 31220 | 1103 | 49952 | 137875 |

* Increased sump depth may be added to increase sediment storage capacity

** Average density of wet packed sediment in sump = 1.6 kg/L (100 lb/ft³)

| Feature | Benefit | Feature Appeals To |
|---|---|---|
| Patent-pending enhanced flow treatment and scour prevention technology | Superior, verified third-party performance | Regulator, Specifying & Design Engineer |
| Third-party verified light liquid capture and retention for EFO version | Proven performance for fuel/oil hotspot locations | Regulator, Specifying & Design Engineer, Site Owner |
| Functions as bend, junction or inlet structure | Design flexibility | Specifying & Design Engineer |
| Minimal drop between inlet and outlet | Site installation ease | Contractor |
| Large diameter outlet riser for inspection and maintenance | Easy maintenance access from grade | Maintenance Contractor & Site Owner |

STANDARD STORMCEPTOR EF/ EFO DRAWINGS

For standard details, please visit <http://www.imbriumsystems.com/stormwater-treatment-solutions/stormceptor-ef>

STANDARD STORMCEPTOR EF/ EFO SPECIFICATION

For specifications, please visit <http://www.imbriumsystems.com/stormwater-treatment-solutions/stormceptor-ef>

Stormceptor®EF Sizing Report

Table of TSS Removal vs Surface Loading Rate Based on Third-Party Test Results
 Stormceptor®EFO

| SLR (L/min/m²) | TSS% REMOVAL | SLR (L/min/m²) | TSS% REMOVAL | SLR (L/min/m²) | TSS% REMOVAL | SLR (L/min/m²) | TSS% REMOVAL |
|-------------------|-----------------|-------------------|-----------------|-------------------|-----------------|-------------------|-----------------|
| 1 | 70 | 660 | 42 | 1320 | 35 | 1980 | 24 |
| 30 | 70 | 690 | 42 | 1350 | 35 | 2010 | 24 |
| 60 | 67 | 720 | 41 | 1380 | 34 | 2040 | 23 |
| 90 | 63 | 750 | 41 | 1410 | 34 | 2070 | 23 |
| 120 | 61 | 780 | 41 | 1440 | 33 | 2100 | 23 |
| 150 | 58 | 810 | 41 | 1470 | 32 | 2130 | 22 |
| 180 | 56 | 840 | 41 | 1500 | 32 | 2160 | 22 |
| 210 | 54 | 870 | 41 | 1530 | 31 | 2190 | 22 |
| 240 | 53 | 900 | 41 | 1560 | 31 | 2220 | 21 |
| 270 | 52 | 930 | 40 | 1590 | 30 | 2250 | 21 |
| 300 | 51 | 960 | 40 | 1620 | 29 | 2280 | 21 |
| 330 | 50 | 990 | 40 | 1650 | 29 | 2310 | 21 |
| 360 | 49 | 1020 | 40 | 1680 | 28 | 2340 | 20 |
| 390 | 48 | 1050 | 39 | 1710 | 28 | 2370 | 20 |
| 420 | 47 | 1080 | 39 | 1740 | 27 | 2400 | 20 |
| 450 | 47 | 1110 | 38 | 1770 | 27 | 2430 | 20 |
| 480 | 46 | 1140 | 38 | 1800 | 26 | 2460 | 19 |
| 510 | 45 | 1170 | 37 | 1830 | 26 | 2490 | 19 |
| 540 | 44 | 1200 | 37 | 1860 | 26 | 2520 | 19 |
| 570 | 43 | 1230 | 37 | 1890 | 25 | 2550 | 19 |
| 600 | 42 | 1260 | 36 | 1920 | 25 | 2580 | 18 |
| 630 | 42 | 1290 | 36 | 1950 | 24 | 2600 | 26 |

Stormceptor®EF Sizing Report

STANDARD PERFORMANCE SPECIFICATION FOR “OIL GRIT SEPARATOR” (OGS) STORMWATER QUALITY TREATMENT DEVICE

PART 1 – GENERAL

1.1 WORK INCLUDED

This section specifies requirements for selecting, sizing, and designing an underground Oil Grit Separator (OGS) device for stormwater quality treatment, with third-party testing results and a Statement of Verification in accordance with ISO 14034 Environmental Management – Environmental Technology Verification (ETV).

1.2 REFERENCE STANDARDS & PROCEDURES

ISO 14034:2016 Environmental management – Environmental technology verification (ETV)

Canadian Environmental Technology Verification (ETV) Program's **Procedure for Laboratory Testing of Oil-Grit Separators**

1.3 SUBMITTALS

1.3.1 All submittals, including sizing reports & shop drawings, shall be submitted upon request with each order to the contractor then forwarded to the Engineer of Record for review and acceptance. Shop drawings shall detail all OGS components, elevations, and sequence of construction.

1.3.2 Alternative devices shall have features identical to or greater than the specified device, including: treatment chamber diameter, treatment chamber wet volume, sediment storage volume, and oil storage volume.

1.3.3 Unless directed otherwise by the Engineer of Record, OGS stormwater quality treatment product substitutions or alternatives submitted within ten days prior to project bid shall not be accepted. All alternatives or substitutions submitted shall be signed and sealed by a local registered Professional Engineer, based on the exact same criteria detailed in Section 3, in entirety, subject to review and approval by the Engineer of Record.

PART 2 – PRODUCTS

2.1 OGS POLLUTANT STORAGE

The OGS device shall include a sump for sediment storage, and a protected volume for the capture and storage of petroleum hydrocarbons and buoyant gross pollutants. The minimum sediment & petroleum hydrocarbon storage capacity shall be as follows:

| | | |
|-------|-------------------------------------|---|
| 2.1.1 | 4 ft (1219 mm) Diameter OGS Units: | 1.19 m ³ sediment / 265 L oil |
| | 5 ft (1524 mm) Diameter OGS Units: | 1.95 m ³ sediment / 420 L oil |
| | 6 ft (1829 mm) Diameter OGS Units: | 3.48 m ³ sediment / 609 L oil |
| | 8 ft (2438 mm) Diameter OGS Units: | 8.78 m ³ sediment / 1,071 L oil |
| | 10 ft (3048 mm) Diameter OGS Units: | 17.78 m ³ sediment / 1,673 L oil |
| | 12 ft (3657 mm) Diameter OGS Units: | 31.23 m ³ sediment / 2,476 L oil |

PART 3 – PERFORMANCE & DESIGN

3.1 GENERAL

The OGS stormwater quality treatment device shall be verified in accordance with ISO 14034:2016 Environmental management – Environmental technology verification (ETV). The OGS stormwater quality treatment device shall

Stormceptor®EF Sizing Report

remove oil, sediment and gross pollutants from stormwater runoff during frequent wet weather events, and retain these pollutants during less frequent high flow wet weather events below the insert within the OGS for later removal during maintenance. The Manufacturer shall have at least ten (10) years of local experience, history and success in engineering design, manufacturing and production and supply of OGS stormwater quality treatment device systems, acceptable to the Engineer of Record.

3.2 SIZING METHODOLOGY

The OGS device shall be engineered, designed and sized to provide stormwater quality treatment based on treating a minimum of 90 percent of the average annual runoff volume and a minimum removal of an annual average 60% of the sediment (TSS) load based on the Particle Size Distribution (PSD) specified in the sizing report for the specified device. Sizing of the OGS shall be determined by use of a minimum ten (10) years of local historical rainfall data provided by Environment Canada. Sizing shall also be determined by use of the sediment removal performance data derived from the ISO 14034 ETV third-party verified laboratory testing data from testing conducted in accordance with the Canadian ETV protocol Procedure for Laboratory Testing of Oil-Grit Separators, as follows:

3.2.1 Sediment removal efficiency for a given surface loading rate and its associated flow rate shall be based on sediment removal efficiency demonstrated at the seven (7) tested surface loading rates specified in the protocol, ranging 40 L/min/m² to 1400 L/min/m², and as stated in the ISO 14034 ETV Verification Statement for the OGS device.

3.2.2 Sediment removal efficiency for surface loading rates between 40 L/min/m² and 1400 L/min/m² shall be based on linear interpolation of data between consecutive tested surface loading rates.

3.2.3 Sediment removal efficiency for surface loading rates less than the lowest tested surface loading rate of 40 L/min/m² shall be assumed to be identical to the sediment removal efficiency at 40 L/min/m². No extrapolation shall be allowed that results in a sediment removal efficiency that is greater than that demonstrated at 40 L/min/m².

3.2.4 Sediment removal efficiency for surface loading rates greater than the highest tested surface loading rate of 1400 L/min/m² shall assume zero sediment removal for the portion of flow that exceeds 1400 L/min/m², and shall be calculated using a simple proportioning formula, with 1400 L/min/m² in the numerator and the higher surface loading rate in the denominator, and multiplying the resulting fraction times the sediment removal efficiency at 1400 L/min/m².

The OGS device shall also have sufficient annual sediment storage capacity as specified and calculated in Section 2.1.

3.3 CANADIAN ETV or ISO 14034 ETV VERIFICATION OF SCOUR TESTING

The OGS device shall have Canadian ETV or ISO 14034 ETV Verification of third-party scour testing conducted in accordance with the Canadian ETV Program's **Procedure for Laboratory Testing of Oil-Grit Separators**.

3.3.1 To be acceptable for on-line installation, the OGS device must demonstrate an average scour test effluent concentration less than 10 mg/L at each surface loading rate tested, up to and including 2600 L/min/m².

3.4 LIGHT LIQUID RE-ENTRAINMENT SIMULATION TESTING

The OGS device shall have Canadian ETV or ISO 14034 ETV Verification of completed third-party Light Liquid Re-entrainment Simulation Testing in accordance with the Canadian ETV **Program's Procedure for Laboratory Testing of Oil-Grit Separators**, with results reported within the Canadian ETV or ISO 14034 ETV verification. This re-entrainment testing is conducted with the device pre-loaded with low density polyethylene (LDPE) plastic beads as a surrogate for light liquids such as oil and fuel. Testing is conducted on the same OGS unit tested for sediment removal to assess whether light liquids captured after a spill are effectively retained at high flow rates.

Stormceptor®EF Sizing Report

3.4.1 For an OGS device to be an acceptable stormwater treatment device on a site where vehicular traffic occurs and the potential for an oil or fuel spill exists, the OGS device must have reported verified performance results of greater than 99% cumulative retention of LDPE plastic beads for the five specified surface loading rates (ranging 200 L/min/m² to 2600 L/min/m²) in accordance with the Light Liquid Re-entrainment Simulation Testing within the Canadian ETV Program's **Procedure for Laboratory Testing of Oil-Grit Separators**. However, an OGS device shall not be allowed if the Light Liquid Re-entrainment Simulation Testing was performed with screening components within the OGS device that are effective at retaining the LDPE plastic beads, but would not be expected to retain light liquids such as oil and fuel.

Stormceptor®EF Sizing Report

| | | | |
|---|----------------|---|--|
| Imbrium®Systems | | | |
| ESTIMATED NET ANNUAL SEDIMENT (TSS) LOAD REDUCTION | | | |
| 08/14/2025 | | | |
| Province: | Ontario | Project Name: | 5923 Ottawa St. (Distillery and Warehouse) |
| City: | Ottawa | Project Number: | COO-25-0415 |
| Nearest Rainfall Station: | OTTAWA CDA RCS | Designer Name: | Jessica Steffler |
| Climate Station Id: | 6105978 | Designer Company: | Forterra Pipe & Precast |
| Years of Rainfall Data: | 20 | Designer Email: | jessica.steffler@RinkerPipe.com |
| Site Name: | Phase 2 | Designer Phone: | 519-239-6958 |
| Drainage Area (ha): | 0.45 | EOR Name: | Francis VALENTI |
| Runoff Coefficient 'c': | 0.60 | EOR Company: | EGIS |
| Particle Size Distribution: | CA ETV | EOR Email: | Francis.VALENTI@egis-group.com |
| Target TSSRemoval (%): | 60.0 | EOR Phone: | 613-714-6895 |
| Required Water Quality Runoff Volume Capture (%): | 90.00 | Net Annual Sediment (TSS) Load Reduction Sizing Summary | |
| Estimated Water Quality Flow Rate (L/s): | 8.71 | Stormceptor Model | TSS Removal Provided (%) |
| Oil / Fuel Spill Risk Site? | Yes | EFO4 | 60 |
| Upstream Flow Control? | No | EFO5 | 63 |
| Peak Conveyance (maximum) Flow Rate (L/s): | 18.00 | EFO6 | 66 |
| Influent TSSConcentration (mg/L): | 200 | EFO8 | 68 |
| Estimated Average Annual Sediment Load (kg/yr): | 184 | EFO10 | 69 |
| Estimated Average Annual Sediment Volume (L/yr): | 149 | EFO12 | 70 |
| Recommended Stormceptor EFO Model: | | EFO4 | |
| Estimated Net Annual Sediment (TSS) Load Reduction (%): | | 60 | |
| Water Quality Runoff Volume Capture (%): | | > 90 | |



Stormceptor®EF Sizing Report

THIRD-PARTY TESTING AND VERIFICATION

► Stormceptor®EF and Stormceptor®EFO are the latest evolutions in the Stormceptor®oil-grit separator (OGS) technology series, and are designed to remove a wide variety of pollutants from stormwater and snowmelt runoff. These technologies have been third-party tested in accordance with the Canadian ETV Procedure for Laboratory Testing of Oil-Grit Separators and performance has been third-party verified in accordance with the ISO 14034 Environmental Technology Verification (ETV) protocol.

PERFORMANCE

► Stormceptor®EF and EFO remove stormwater pollutants through gravity separation and floatation, and feature a patent-pending design that generates positive removal of total suspended solids (TSS) throughout each storm event, including high-intensity storms. Captured pollutants include sediment, free oils, and sediment-bound pollutants such as nutrients, heavy metals, and petroleum hydrocarbons. Stormceptor is sized to remove a high level of TSS from the frequent rainfall events that contribute the vast majority of annual runoff volume and pollutant load. The technology incorporates an internal bypass to convey excessive stormwater flows from high-intensity storms through the device without resuspension and washout (scour) of previously captured pollutants. Proper routine maintenance ensures high pollutant removal performance and protection of downstream waterways.

PARTICLE SIZE DISTRIBUTION (PSD)

► The Canadian ETV PSD shown in the table below was used, or in part, for this sizing. This is the identical PSD that is referenced in the Canadian ETV Procedure for Laboratory Testing of Oil-Grit Separators for both sediment removal testing and scour testing. The Canadian ETV PSD contains a wide range of particle sizes in the sand and silt fractions, and is considered reasonably representative of the particle size fractions found in typical urban stormwater runoff.

| Particle Size (µm) | Percent Less Than | Particle Size Fraction (µm) | Percent |
|--------------------|-------------------|-----------------------------|---------|
| 1000 | 100 | 500-1000 | 5 |
| 500 | 95 | 250-500 | 5 |
| 250 | 90 | 150-250 | 15 |
| 150 | 75 | 100-150 | 15 |
| 100 | 60 | 75-100 | 10 |
| 75 | 50 | 50-75 | 5 |
| 50 | 45 | 20-50 | 10 |
| 20 | 35 | 8-20 | 15 |
| 8 | 20 | 5-8 | 10 |
| 5 | 10 | 2-5 | 5 |
| 2 | 5 | <2 | 5 |



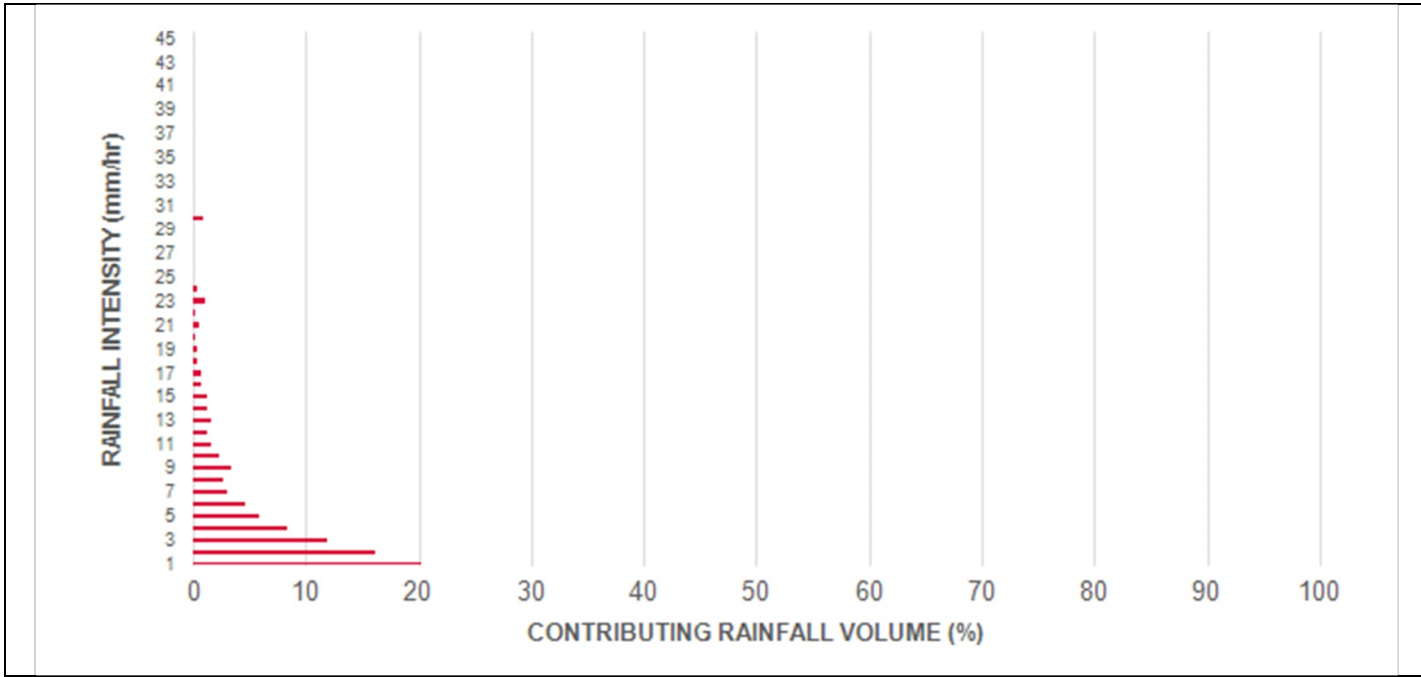
Stormceptor®EF Sizing Report

| Rainfall Intensity (mm / hr) | Percent Rainfall Volume (%) | Cumulative Rainfall Volume (%) | Flow Rate (L/s) | Flow Rate (L/min) | Surface Loading Rate (L/min/ m²) | Removal Efficiency (%) | Incremental Removal (%) | Cumulative Removal (%) |
|--|-----------------------------|--------------------------------|-----------------|-------------------|----------------------------------|------------------------|-------------------------|------------------------|
| 0.50 | 8.6 | 8.6 | 0.38 | 23.0 | 19.0 | 70 | 6.1 | 6.1 |
| 1.00 | 20.3 | 29.0 | 0.75 | 45.0 | 38.0 | 70 | 14.3 | 20.4 |
| 2.00 | 16.2 | 45.2 | 1.50 | 90.0 | 75.0 | 66 | 10.6 | 31.0 |
| 3.00 | 12.0 | 57.2 | 2.25 | 135.0 | 113.0 | 62 | 7.4 | 38.4 |
| 4.00 | 8.4 | 65.6 | 3.00 | 180.0 | 150.0 | 58 | 4.9 | 43.3 |
| 5.00 | 5.9 | 71.6 | 3.75 | 225.0 | 188.0 | 56 | 3.3 | 46.6 |
| 6.00 | 4.6 | 76.2 | 4.50 | 270.0 | 225.0 | 53 | 2.5 | 49.1 |
| 7.00 | 3.1 | 79.3 | 5.25 | 315.0 | 263.0 | 52 | 1.6 | 50.7 |
| 8.00 | 2.7 | 82.0 | 6.00 | 360.0 | 300.0 | 51 | 1.4 | 52.1 |
| 9.00 | 3.3 | 85.3 | 6.76 | 405.0 | 338.0 | 50 | 1.7 | 53.8 |
| 10.00 | 2.3 | 87.6 | 7.51 | 450.0 | 375.0 | 49 | 1.1 | 54.9 |
| 11.00 | 1.6 | 89.2 | 8.26 | 495.0 | 413.0 | 48 | 0.7 | 55.6 |
| 12.00 | 1.3 | 90.5 | 9.01 | 540.0 | 450.0 | 47 | 0.6 | 56.2 |
| 13.00 | 1.7 | 92.2 | 9.76 | 585.0 | 488.0 | 46 | 0.8 | 57.0 |
| 14.00 | 1.2 | 93.5 | 10.51 | 631.0 | 525.0 | 44 | 0.5 | 57.6 |
| 15.00 | 1.2 | 94.6 | 11.26 | 676.0 | 563.0 | 43 | 0.5 | 58.1 |
| 16.00 | 0.7 | 95.3 | 12.01 | 721.0 | 600.0 | 42 | 0.3 | 58.4 |
| 17.00 | 0.7 | 96.1 | 12.76 | 766.0 | 638.0 | 42 | 0.3 | 58.7 |
| 18.00 | 0.4 | 96.5 | 13.51 | 811.0 | 676.0 | 42 | 0.2 | 58.8 |
| 19.00 | 0.4 | 96.9 | 14.26 | 856.0 | 713.0 | 41 | 0.2 | 59.0 |
| 20.00 | 0.2 | 97.1 | 15.01 | 901.0 | 751.0 | 41 | 0.1 | 59.1 |
| 21.00 | 0.5 | 97.5 | 15.76 | 946.0 | 788.0 | 41 | 0.2 | 59.3 |
| 22.00 | 0.2 | 97.8 | 16.51 | 991.0 | 826.0 | 41 | 0.1 | 59.4 |
| 23.00 | 1.0 | 98.8 | 17.26 | 1036.0 | 863.0 | 41 | 0.4 | 59.8 |
| 24.00 | 0.3 | 99.1 | 18.01 | 1081.0 | 901.0 | 41 | 0.1 | 59.9 |
| 25.00 | 0.0 | 99.1 | 18.77 | 1126.0 | 938.0 | 40 | 0.0 | 59.9 |
| 30.00 | 0.9 | 100.0 | 22.52 | 1351.0 | 1126.0 | 38 | 0.4 | 60.3 |
| 35.00 | 0.0 | 100.0 | 26.27 | 1576.0 | 1314.0 | 35 | 0.0 | 60.3 |
| 40.00 | 0.0 | 100.0 | 30.02 | 1801.0 | 1501.0 | 32 | 0.0 | 60.3 |
| 45.00 | 0.0 | 100.0 | 33.78 | 2027.0 | 1689.0 | 28 | 0.0 | 60.3 |
| Estimated Net Annual Sediment (TSS) Load Reduction = | | | | | | | | 60 % |

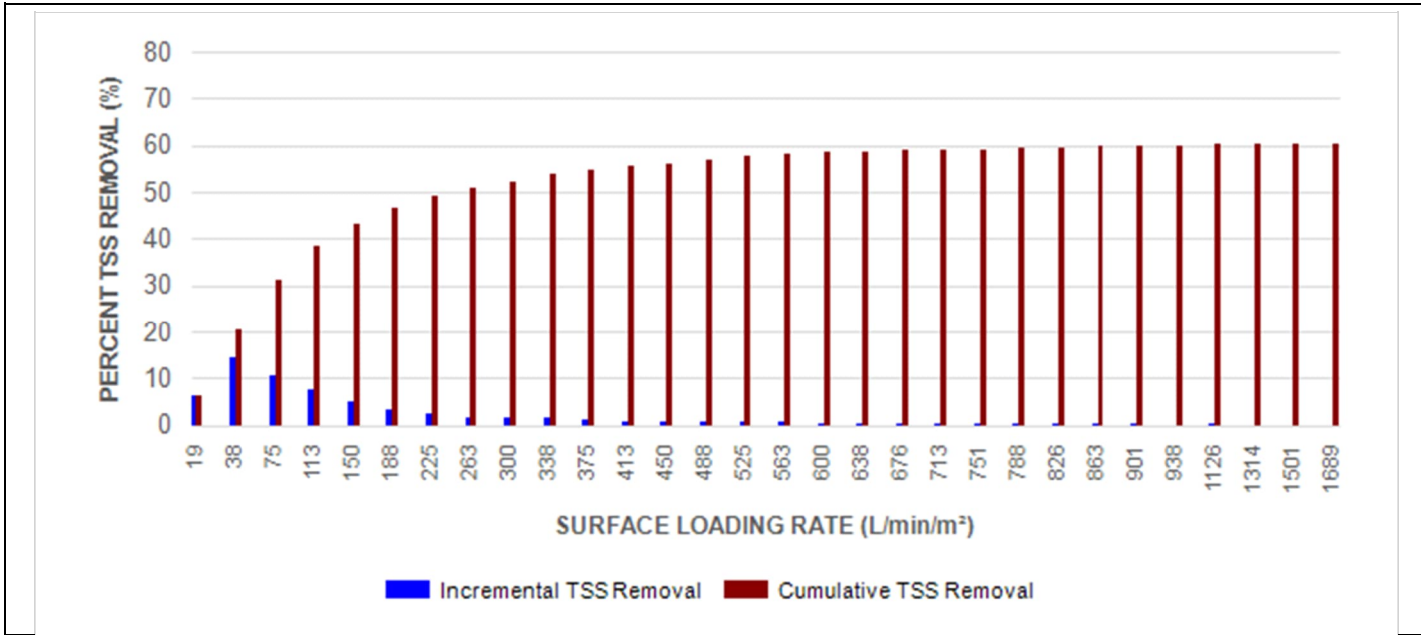
Climate Station ID: 6105978 Years of Rainfall Data: 20

Stormceptor®EF Sizing Report

RAINFALL DATA FROM OTTAWA CDA RCS RAINFALL STATION



INCREMENTAL AND CUMULATIVE TSS REMOVAL
FOR THE RECOMMENDED STORMCEPTOR® MODEL



Stormceptor®EF Sizing Report

Maximum Pipe Diameter / Peak Conveyance

| Stormceptor EF / EFO | Model Diameter | | Min Angle Inlet / Outlet Pipes | Max Inlet Pipe Diameter | | Max Outlet Pipe Diameter | | Peak Conveyance Flow Rate | |
|-------------------------|----------------|------|-----------------------------------|----------------------------|------|-----------------------------|------|------------------------------|-------|
| | (m) | (ft) | | (mm) | (in) | (mm) | (in) | (L/s) | (cfs) |
| EF4 / EFO4 | 1.2 | 4 | 90 | 609 | 24 | 609 | 24 | 425 | 15 |
| EF5 / EFO5 | 1.5 | 5 | 90 | 762 | 30 | 762 | 30 | 710 | 25 |
| EF6 / EFO6 | 1.8 | 6 | 90 | 914 | 36 | 914 | 36 | 990 | 35 |
| EF8 / EFO8 | 2.4 | 8 | 90 | 1219 | 48 | 1219 | 48 | 1700 | 60 |
| EF10 / EFO10 | 3.0 | 10 | 90 | 1828 | 72 | 1828 | 72 | 2830 | 100 |
| EF12 / EFO12 | 3.6 | 12 | 90 | 1828 | 72 | 1828 | 72 | 2830 | 100 |

SCOUR PREVENTION AND ONLINE CONFIGURATION

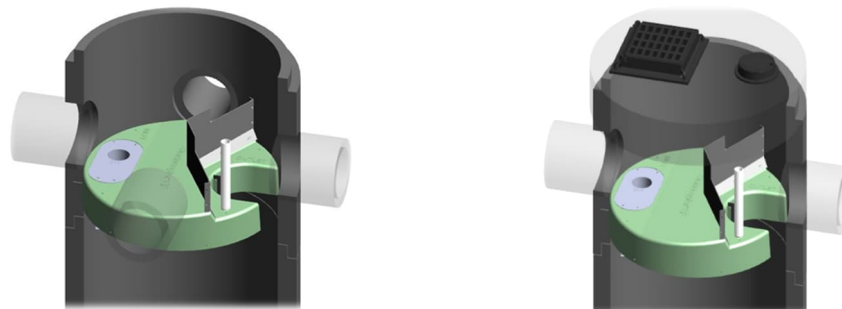
► Stormceptor®EF and EFO feature an internal bypass and superior scour prevention technology that have been demonstrated in third-party testing according to the scour testing provisions of the Canadian ETV Procedure for Laboratory Testing of Oil-Grit Separators, and the exceptional scour test performance has been third-party verified in accordance with the ISO 14034 ETV protocol. As a result, Stormceptor EF and EFO are approved for online installation, eliminating the need for costly additional bypass structures, piping, and installation expense.

DESIGN FLEXIBILITY

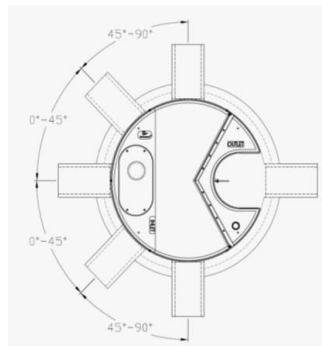
► Stormceptor®EF and EFO offers design flexibility in one simplified platform, accepting stormwater flow from a single inlet pipe or multiple inlet pipes, and/or surface runoff through an inlet grate. The device can also serve as a junction structure, accommodate a 90-degree inlet-to-outlet bend angle, and can be modified to ensure performance in submerged conditions.

OIL CAPTURE AND RETENTION

► While Stormceptor®EF will capture and retain oil from dry weather spills and low intensity runoff, Stormceptor®EFO has demonstrated superior oil capture and greater than 99% oil retention in third-party testing according to the light liquid re-entrainment testing provisions of the Canadian ETV Procedure for Laboratory Testing of Oil-Grit Separators. Stormceptor EFO is recommended for sites where oil capture and retention is a requirement.



Stormceptor®EF Sizing Report



INLET-TO-OUTLET DROP

Elevation differential between inlet and outlet pipe inverts is dictated by the angle at which the inlet pipe(s) enters the unit.

0° - 45° : The inlet pipe is 1-inch (25mm) higher than the outlet pipe.

45° - 90° : The inlet pipe is 2-inches (50mm) higher than the outlet pipe.

HEAD LOSS

The head loss through Stormceptor EF is similar to that of a 60-degree bend structure. The applicable K value for calculating minor losses through the unit is 1.1. For submerged conditions the applicable K value is 3.0.

Pollutant Capacity

| Stormceptor EF / EFO | Model Diameter | | Depth (Outlet Pipe Invert to Sump Floor) | | Oil Volume | | Recommended Sediment Maintenance Depth * | | Maximum Sediment Volume * | | Maximum Sediment Mass ** | |
|-------------------------|-------------------|------|--|------|------------|-------|--|------|------------------------------|-------|-----------------------------|--------|
| | (m) | (ft) | (m) | (ft) | (L) | (Gal) | (mm) | (in) | (L) | (ft³) | (kg) | (lb) |
| EF4 / EFO4 | 1.2 | 4 | 1.52 | 5.0 | 265 | 70 | 203 | 8 | 1190 | 42 | 1904 | 5250 |
| EF5 / EFO5 | 1.5 | 5 | 1.62 | 5.3 | 420 | 111 | 305 | 10 | 2124 | 75 | 2612 | 5758 |
| EF6 / EFO6 | 1.8 | 6 | 1.93 | 6.3 | 610 | 160 | 305 | 12 | 3470 | 123 | 5552 | 15375 |
| EF8 / EFO8 | 2.4 | 8 | 2.59 | 8.5 | 1070 | 280 | 610 | 24 | 8780 | 310 | 14048 | 38750 |
| EF10 / EFO10 | 3.0 | 10 | 3.25 | 10.7 | 1670 | 440 | 610 | 24 | 17790 | 628 | 28464 | 78500 |
| EF12 / EFO12 | 3.6 | 12 | 3.89 | 12.8 | 2475 | 655 | 610 | 24 | 31220 | 1103 | 49952 | 137875 |

* Increased sump depth may be added to increase sediment storage capacity

** Average density of wet packed sediment in sump = 1.6 kg/L (100 lb/ft³)

| Feature | Benefit | Feature Appeals To |
|---|---|---|
| Patent-pending enhanced flow treatment and scour prevention technology | Superior, verified third-party performance | Regulator, Specifying & Design Engineer |
| Third-party verified light liquid capture and retention for EFO version | Proven performance for fuel/oil hotspot locations | Regulator, Specifying & Design Engineer, Site Owner |
| Functions as bend, junction or inlet structure | Design flexibility | Specifying & Design Engineer |
| Minimal drop between inlet and outlet | Site installation ease | Contractor |
| Large diameter outlet riser for inspection and maintenance | Easy maintenance access from grade | Maintenance Contractor & Site Owner |

STANDARD STORMCEPTOR EF/ EFO DRAWINGS

For standard details, please visit <http://www.imbriumsystems.com/stormwater-treatment-solutions/stormceptor-ef>

STANDARD STORMCEPTOR EF/ EFO SPECIFICATION

For specifications, please visit <http://www.imbriumsystems.com/stormwater-treatment-solutions/stormceptor-ef>

Stormceptor®EF Sizing Report

Table of TSS Removal vs Surface Loading Rate Based on Third-Party Test Results
 Stormceptor®EFO

| SLR (L/min/m²) | TSS% REMOVAL | SLR (L/min/m²) | TSS% REMOVAL | SLR (L/min/m²) | TSS% REMOVAL | SLR (L/min/m²) | TSS% REMOVAL |
|-------------------|-----------------|-------------------|-----------------|-------------------|-----------------|-------------------|-----------------|
| 1 | 70 | 660 | 42 | 1320 | 35 | 1980 | 24 |
| 30 | 70 | 690 | 42 | 1350 | 35 | 2010 | 24 |
| 60 | 67 | 720 | 41 | 1380 | 34 | 2040 | 23 |
| 90 | 63 | 750 | 41 | 1410 | 34 | 2070 | 23 |
| 120 | 61 | 780 | 41 | 1440 | 33 | 2100 | 23 |
| 150 | 58 | 810 | 41 | 1470 | 32 | 2130 | 22 |
| 180 | 56 | 840 | 41 | 1500 | 32 | 2160 | 22 |
| 210 | 54 | 870 | 41 | 1530 | 31 | 2190 | 22 |
| 240 | 53 | 900 | 41 | 1560 | 31 | 2220 | 21 |
| 270 | 52 | 930 | 40 | 1590 | 30 | 2250 | 21 |
| 300 | 51 | 960 | 40 | 1620 | 29 | 2280 | 21 |
| 330 | 50 | 990 | 40 | 1650 | 29 | 2310 | 21 |
| 360 | 49 | 1020 | 40 | 1680 | 28 | 2340 | 20 |
| 390 | 48 | 1050 | 39 | 1710 | 28 | 2370 | 20 |
| 420 | 47 | 1080 | 39 | 1740 | 27 | 2400 | 20 |
| 450 | 47 | 1110 | 38 | 1770 | 27 | 2430 | 20 |
| 480 | 46 | 1140 | 38 | 1800 | 26 | 2460 | 19 |
| 510 | 45 | 1170 | 37 | 1830 | 26 | 2490 | 19 |
| 540 | 44 | 1200 | 37 | 1860 | 26 | 2520 | 19 |
| 570 | 43 | 1230 | 37 | 1890 | 25 | 2550 | 19 |
| 600 | 42 | 1260 | 36 | 1920 | 25 | 2580 | 18 |
| 630 | 42 | 1290 | 36 | 1950 | 24 | 2600 | 26 |

Stormceptor®EF Sizing Report

STANDARD PERFORMANCE SPECIFICATION FOR “OIL GRIT SEPARATOR” (OGS) STORMWATER QUALITY TREATMENT DEVICE

PART 1 – GENERAL

1.1 WORK INCLUDED

This section specifies requirements for selecting, sizing, and designing an underground Oil Grit Separator (OGS) device for stormwater quality treatment, with third-party testing results and a Statement of Verification in accordance with ISO 14034 Environmental Management – Environmental Technology Verification (ETV).

1.2 REFERENCE STANDARDS & PROCEDURES

ISO 14034:2016 Environmental management – Environmental technology verification (ETV)

Canadian Environmental Technology Verification (ETV) Program's **Procedure for Laboratory Testing of Oil-Grit Separators**

1.3 SUBMITTALS

1.3.1 All submittals, including sizing reports & shop drawings, shall be submitted upon request with each order to the contractor then forwarded to the Engineer of Record for review and acceptance. Shop drawings shall detail all OGS components, elevations, and sequence of construction.

1.3.2 Alternative devices shall have features identical to or greater than the specified device, including: treatment chamber diameter, treatment chamber wet volume, sediment storage volume, and oil storage volume.

1.3.3 Unless directed otherwise by the Engineer of Record, OGS stormwater quality treatment product substitutions or alternatives submitted within ten days prior to project bid shall not be accepted. All alternatives or substitutions submitted shall be signed and sealed by a local registered Professional Engineer, based on the exact same criteria detailed in Section 3, in entirety, subject to review and approval by the Engineer of Record.

PART 2 – PRODUCTS

2.1 OGS POLLUTANT STORAGE

The OGS device shall include a sump for sediment storage, and a protected volume for the capture and storage of petroleum hydrocarbons and buoyant gross pollutants. The minimum sediment & petroleum hydrocarbon storage capacity shall be as follows:

| | | |
|-------|-------------------------------------|---|
| 2.1.1 | 4 ft (1219 mm) Diameter OGS Units: | 1.19 m ³ sediment / 265 L oil |
| | 5 ft (1524 mm) Diameter OGS Units: | 1.95 m ³ sediment / 420 L oil |
| | 6 ft (1829 mm) Diameter OGS Units: | 3.48 m ³ sediment / 609 L oil |
| | 8 ft (2438 mm) Diameter OGS Units: | 8.78 m ³ sediment / 1,071 L oil |
| | 10 ft (3048 mm) Diameter OGS Units: | 17.78 m ³ sediment / 1,673 L oil |
| | 12 ft (3657 mm) Diameter OGS Units: | 31.23 m ³ sediment / 2,476 L oil |

PART 3 – PERFORMANCE & DESIGN

3.1 GENERAL

The OGS stormwater quality treatment device shall be verified in accordance with ISO 14034:2016 Environmental management – Environmental technology verification (ETV). The OGS stormwater quality treatment device shall

Stormceptor®EF Sizing Report

remove oil, sediment and gross pollutants from stormwater runoff during frequent wet weather events, and retain these pollutants during less frequent high flow wet weather events below the insert within the OGS for later removal during maintenance. The Manufacturer shall have at least ten (10) years of local experience, history and success in engineering design, manufacturing and production and supply of OGS stormwater quality treatment device systems, acceptable to the Engineer of Record.

3.2 SIZING METHODOLOGY

The OGS device shall be engineered, designed and sized to provide stormwater quality treatment based on treating a minimum of 90 percent of the average annual runoff volume and a minimum removal of an annual average 60% of the sediment (TSS) load based on the Particle Size Distribution (PSD) specified in the sizing report for the specified device. Sizing of the OGS shall be determined by use of a minimum ten (10) years of local historical rainfall data provided by Environment Canada. Sizing shall also be determined by use of the sediment removal performance data derived from the ISO 14034 ETV third-party verified laboratory testing data from testing conducted in accordance with the Canadian ETV protocol Procedure for Laboratory Testing of Oil-Grit Separators, as follows:

3.2.1 Sediment removal efficiency for a given surface loading rate and its associated flow rate shall be based on sediment removal efficiency demonstrated at the seven (7) tested surface loading rates specified in the protocol, ranging 40 L/min/m² to 1400 L/min/m², and as stated in the ISO 14034 ETV Verification Statement for the OGS device.

3.2.2 Sediment removal efficiency for surface loading rates between 40 L/min/m² and 1400 L/min/m² shall be based on linear interpolation of data between consecutive tested surface loading rates.

3.2.3 Sediment removal efficiency for surface loading rates less than the lowest tested surface loading rate of 40 L/min/m² shall be assumed to be identical to the sediment removal efficiency at 40 L/min/m². No extrapolation shall be allowed that results in a sediment removal efficiency that is greater than that demonstrated at 40 L/min/m².

3.2.4 Sediment removal efficiency for surface loading rates greater than the highest tested surface loading rate of 1400 L/min/m² shall assume zero sediment removal for the portion of flow that exceeds 1400 L/min/m², and shall be calculated using a simple proportioning formula, with 1400 L/min/m² in the numerator and the higher surface loading rate in the denominator, and multiplying the resulting fraction times the sediment removal efficiency at 1400 L/min/m².

The OGS device shall also have sufficient annual sediment storage capacity as specified and calculated in Section 2.1.

3.3 CANADIAN ETV or ISO 14034 ETV VERIFICATION OF SCOUR TESTING

The OGS device shall have Canadian ETV or ISO 14034 ETV Verification of third-party scour testing conducted in accordance with the Canadian ETV Program's **Procedure for Laboratory Testing of Oil-Grit Separators**.

3.3.1 To be acceptable for on-line installation, the OGS device must demonstrate an average scour test effluent concentration less than 10 mg/L at each surface loading rate tested, up to and including 2600 L/min/m².

3.4 LIGHT LIQUID RE-ENTRAINMENT SIMULATION TESTING

The OGS device shall have Canadian ETV or ISO 14034 ETV Verification of completed third-party Light Liquid Re-entrainment Simulation Testing in accordance with the Canadian ETV **Program's Procedure for Laboratory Testing of Oil-Grit Separators**, with results reported within the Canadian ETV or ISO 14034 ETV verification. This re-entrainment testing is conducted with the device pre-loaded with low density polyethylene (LDPE) plastic beads as a surrogate for light liquids such as oil and fuel. Testing is conducted on the same OGS unit tested for sediment removal to assess whether light liquids captured after a spill are effectively retained at high flow rates.

Stormceptor®EF Sizing Report

3.4.1 For an OGS device to be an acceptable stormwater treatment device on a site where vehicular traffic occurs and the potential for an oil or fuel spill exists, the OGS device must have reported verified performance results of greater than 99% cumulative retention of LDPE plastic beads for the five specified surface loading rates (ranging 200 L/min/m² to 2600 L/min/m²) in accordance with the Light Liquid Re-entrainment Simulation Testing within the Canadian ETV Program's **Procedure for Laboratory Testing of Oil-Grit Separators**. However, an OGS device shall not be allowed if the Light Liquid Re-entrainment Simulation Testing was performed with screening components within the OGS device that are effective at retaining the LDPE plastic beads, but would not be expected to retain light liquids such as oil and fuel.

September 11, 2025

Project Number: P2710(e01)

Stratford Foxrun
6286 Prince of Wales Drive
North Gower, ON
K0A 2T0

Attention: Joshua Laginski, P.Eng

**Subject: Stratford Foxrun Development- 5923 Ottawa Street, Richmond
Ditch Hydrologic and Hydraulic Analysis**

RATIONALE FOR UPDATE

The following memo has been revised to address comments received from the City of Ottawa on July 3, 2025, titled “*Feedback Form – Completeness Review #1 Site Plan Control 5923 Ottawa Street*”. Updates in this memo include refinements to the site grading and stormwater management design, as well as the incorporation of additional calculations and supporting text for justification of selected model parameters, as requested by the city review comments provided. These updates ensure consistency with the latest design information and compliance with applicable City of Ottawa guidelines.

OVERVIEW

Egis Group has commissioned JFSA Canada Inc. to develop detailed hydrologic and hydraulic models for the proposed Stratford Foxrun development. This development, located at 5923 Ottawa Street in Richmond, Ontario, will include local depressions within the site that will act as stormwater management controls to mitigate increases in peak flows resulting from the development. The site will outlet into an existing roadside ditch on Ottawa Street before proceeding east to Eagleson Road and then turning north towards the rail corridor before finally discharging into Marlborough Creek, which is a tributary of the Jock River.

This memo presents a downstream hydrologic and hydraulic analysis of the aforementioned roadside ditch, specifically quantifying its capacity from 5923 Ottawa Street to the Marlborough Creek. **Figure 1** illustrates the development's location and extent, as well as the road site ditch relative to its outlet at Marlborough Creek.

Figure 1: Site Boundary and Existing Watercourse



HYDROLOGY

Existing Conditions

Drainage Areas

Existing drainage areas for this study were delineated using a comprehensive Digital Terrain Model (DTM). This DTM was developed from two primary sources: LiDAR data, obtained from the LIO (Land Information Ontario) Digital Terrain Model and flown in 2019-2020, and a detailed topographic survey of the existing ditch and associated crossings completed by Egis in January 2025. This combined data was then imported into GIS software. Watershed delineation algorithms were subsequently applied to the DTM to automatically define the drainage areas. These automated delineations were manually reviewed against relevant previous studies and existing drainage delineations for accuracy and consistency. **Figure A1 in Attachment A** provides a visual overview of the existing drainage areas within the study area.

Land Use

Land use data has been taken from Land Information Ontario's (LIO) Land Use Data and then discretized based on the respective subcatchments. **Figure A2 in Attachment A** provides a visual overview of the respective land use data for each of the subcatchments within the study area.

Soil/Infiltration Data

Soil data within the study area has been taken from the Soil Survey Complex Data available on Land Information Ontario (LIO). **Figure A3 in Attachment A** provides a visual overview of the respective soil type data for each of the subcatchments within the study area. A full breakdown of the soil data for each drainage area has also been provided in **Table A1 in Attachment A**.

Curve Number (CN)

Based on the underlying Land Use Type and Soil Classification at each location within a subcatchment, a Curve Number (CN) was calculated, based on applicable values outlined in Tables A2 and A3 in the SWMHYMO Manual. Each Curve Number was then weighted based on the total area within a given subcatchment to determine the weighted CN for that subcatchment. The CN values calculated were then converted to CN*. Note that the traditional CN procedure assumes that Initial Abstraction (IA) = 0.2S. However, the traditional CN method is subject to errors because of this assumption, particularly for smaller rainfall events. Instead, it is recommended that a modified CN* and a user-defined IA value be used for SWMHYMO modelling. Modified CN* values have been shown to correlate well with measured flows and perform well in continuous SWMHYMO modelling (as discussed in the July 1989 INTERHYMO / OTTHYMO 89 Manual). The CN values derived were converted to CN* based on the formula provided in the November 2002 Runoff Curve Number Method: Examination of the Initial Abstract Ratio paper, and applied to the hydrologic model.

$$CN^* = \frac{100}{1.879 \left[\frac{100}{CN-1} \right]^{1.15} + 1}$$

Table A1 in Attachment provides a full summary of the CN/CN* calculations for each of the predevelopment subcatchments.

Time to Peak (tp)

For natural areas within the study area, the time to peak values for each of the subcatchments has been calculated based on existing topography. Flow paths have been discretized based on the topographic data using GIS tools, and the longest major flow path within each subcatchment has been identified; refer to Figure B6 in Attachment B for the flow paths discretized for each subcatchment. The upstream and downstream topographic elevations and flow lengths were identified for each subcatchment and used in the calculations. For these natural subcatchments, the Federal Aviation Administration (FAA) method was determined to be the most appropriate method to calculate the Time to Peak.

Other methods, such as the Uplands method, were also included in that analysis. The FAA method was selected for use in the final model because it produced longer time-to-peak (Tp) values for the same catchments, resulting in lower peak flows under pre-development conditions. These lower peak flows were then used to establish allowable release rates for the proposed stormwater management facilities.

This approach results in a more conservative design, as the SWM controls are sized to ensure post-development flows do not exceed these lower pre-development thresholds. While the Uplands method is preferred in the Sewer Design Guidelines (Appendix 5-D), the FAA method remains suitable for flat, rural catchments with longer overland flow paths, which characterizes the study area. Therefore, the FAA-based design applied in this analysis is more conservative and protective of downstream infrastructure.

Full details of these calculations have been provided in **Table A2 in Attachment A**, along with other time-to-peak values using alternative tp calculation methods.

Existing SWMHYMO modelling

An existing conditions SWMHYMO model of the drainage areas was developed based on the pre-development drainage areas provided. To represent the existing undeveloped lands, CALIB NASHYDs have been used, with Initial Abstraction (IA)=4.67 mm, and Number of Linear Reservoirs (N)=3. Full input and summary files of the existing conditions model have been provided in Attachment A

Channel Routing

To account for channel routing throughout the study area, LiDAR has been used to approximate the channel cross-section and associated flow parameters (length & slope). **Figure A4 in Attachment A** outlines the major flow paths within the study area, which have been used to account for channel routing and time to peak calculations within the subcatchments.

Design & Historical Storms

The stormwater management analysis incorporates both standard design storms and historical storm events in accordance with the City of Ottawa's guidelines. The selected design storms include the 3-hour Chicago distribution and the 24-hour SCS distribution, which are consistent with standard practice for stormwater management design in the region.

The 3-hour Chicago storm is widely used for urban infrastructure analysis because it provides a balanced representation of peak intensity and total rainfall volume. This duration is sufficient to generate meaningful runoff volumes for sizing stormwater management controls while capturing peak intensities that challenge conveyance systems. Although shorter-duration storms (e.g., 1-hour 100-year) exhibit higher peak intensities, their lower total rainfall volume often results in less conservative storage sizing. Conversely, the 24-hour SCS storm is included to assess broader floodplain impacts and downstream conveyance performance.

In addition to these design storms, the following historical events were simulated as per City requirements: July 1, 1979, August 4, 1988, and August 8, 1996. These events provide additional validation of system performance under real-world conditions and help ensure resiliency of the proposed stormwater management system.

Proposed Conditions

Drainage Areas & Imperviousness

For the Stratford Foxrun development under proposed conditions, Egis provided JFSA with detailed design drawings that included drainage areas and associated imperviousness. The proposed development lot layout and the associated drainage areas have been provided in **Figure B1 of Attachment B**. To represent the proposed Stratford Foxrun development lands, DESIGN STANDHYDs have been used, with default parameters per the city of Ottawa Storm Sewer Design Guidelines.

Onsite SWM Controls

Egis's design for the proposed development included detailed grading of localized depressions within the site that will act as onsite stormwater management controls, along with corresponding stage-storage tables. These stage-storage tables were directly incorporated into the hydrologic model. This integration allowed for the determination of appropriate outlet configurations for these facilities, as well as an accurate assessment of the storage volumes provided by the proposed depressions. Full detailed Stage/Storage/Outflow curves have been provided in **Tables B1 and B2 in Attachment B**. Based on this analysis, both sites will have a **75 mm** orifice at the bottom of the localized depression area and a **30cm** overflow weir at an elevation of **94.40m** and for extreme events.

Results

Onsite Controls Summary

Table 2 provides a comprehensive overview of the maximum storage volumes achieved at each of these locations across various return periods, in addition to their associated peak outflows and maximum water levels.

Table 1: Site Release Rates / Required Storage Volume / Ponding Depth/WSE

| Event | Site 1 (0.480 ha) | | | | Site 2 (0.447 ha) | | | |
|------------------|--|-------------------------------------|--------------------|--------------|--|-------------------------------------|--------------------|--------------|
| | Peak Outflow (m ³ /s) | Pond Volume (m ³) | Pond WSE (m) | Depth (m) | Peak Outflow (m ³ /s) | Pond Volume (m ³) | Pond WSE (m) | Depth (m) |
| 2YrCHI3Hr | 0.033 | 34 | 94.113 | 0.273 | 0.031 | 38 | 94.058 | 0.348 |
| 5YrCHI3Hr | 0.054 | 64 | 94.189 | 0.349 | 0.049 | 65 | 94.167 | 0.447 |
| 10YrCHI3Hr | 0.072 | 85 | 94.231 | 0.391 | 0.064 | 84 | 94.220 | 0.490 |
| 25YrCHI3Hr | 0.094 | 113 | 94.284 | 0.444 | 0.083 | 109 | 94.280 | 0.540 |
| 50YrCHI3Hr | 0.109 | 134 | 94.323 | 0.483 | 0.096 | 129 | 94.323 | 0.573 |
| 100YrCHI3Hr | 0.130 | 158 | 94.364 | 0.524 | 0.114 | 150 | 94.366 | 0.606 |
| 2YrSCS24Hr | 0.036 | 43 | 94.139 | 0.299 | 0.034 | 45 | 94.091 | 0.321 |
| 5YrSCS24Hr | 0.056 | 72 | 94.205 | 0.365 | 0.051 | 71 | 94.185 | 0.405 |
| 10YrSCS24Hr | 0.070 | 91 | 94.244 | 0.404 | 0.064 | 89 | 94.232 | 0.442 |
| 25YrSCS24Hr | 0.088 | 117 | 94.292 | 0.452 | 0.080 | 112 | 94.286 | 0.486 |
| 50YrSCS24Hr | 0.101 | 136 | 94.327 | 0.487 | 0.090 | 130 | 94.325 | 0.515 |
| 100YrSCS24Hr | 0.115 | 157 | 94.362 | 0.522 | 0.103 | 149 | 94.364 | 0.544 |
| July 1st, 1979 | 0.091 | 206 | 94.443 | 0.603 | 0.082 | 192 | 94.449 | 0.619 |
| August 4th, 1988 | 0.108 | 173 | 94.389 | 0.549 | 0.096 | 165 | 94.396 | 0.556 |
| August 8th, 1996 | 0.071 | 146 | 94.344 | 0.504 | 0.065 | 139 | 94.344 | 0.494 |
| 100YrCHI+20% | 0.165 | 203 | 94.438 | 0.598 | 0.144 | 188 | 94.439 | 0.579 |

Peak Flows at Key Locations

The model was run for both existing and proposed conditions, and peak flows were extracted from the key nodes within the watercourse (refer to **Figure A4** for locations). **Table 2** outlines the peak flows for various return periods at each node, covering both the 3-hour Chicago and 24-hour SCS storms for 2- to 100-year events, along with the stress test and historical events.

This analysis indicates minor increases in peak flows to the roadside ditch for lower return period events under post-development conditions (2YrCHI3Hr, 5YrCHI3Hr & 2YRSCS24Hr). However, for larger events (e.g., the 100-year storm), peak flows are equal to or less than those under existing conditions. For the lower return period events (2YrCHI3Hr, 5YrCHI3Hr & 2YRSCS24Hr) that exhibit slight increases in peak flows, the hydraulic modelling indicates that maximum velocities within the ditch remain below 1.5 m/s. This threshold aligns with the maximum permissible velocity for grassed roadside ditches without requiring bioengineering stabilization measures, as outlined in Section 2.3 of SD-9 Roadside Ditches (Conveyance Only) from the MTO Highway Drainage Design Standards. Therefore, it can be concluded that the modest increase in flow rates during smaller storm events will not result in adverse erosion within the grassed channel.

Additionally, both sites will utilize a **75 mm** orifice at the outlet to maximize the storage capacity of these depression areas; this is the smallest allowable outlet size per MECP SWM guidelines.

Table 2: Pre and Post Development Peak Flow Summary

| Event | Node | J1 | | Node | J2 | | Node | J3 | | Node | J4 | |
|------------------|-------|-------|--------|-------|-------|--------|-------|-------|--------|-------|-------|--------|
| | Pre | Post | Diff | Pre | Post | Diff | Pre | Post | Diff | Pre | Post | Diff |
| Area (ha) | 0.85 | 1.23 | 0.38 | 4.62 | 5 | 0.38 | 4.93 | 5.31 | 0.38 | 5.52 | 5.9 | 0.38 |
| 2YrCHI3Hr | 0.015 | 0.019 | 0.004 | 0.057 | 0.062 | 0.005 | 0.061 | 0.066 | 0.005 | 0.067 | 0.072 | 0.005 |
| 5YrCHI3Hr | 0.026 | 0.027 | 0.001 | 0.102 | 0.102 | 0.000 | 0.109 | 0.109 | 0.000 | 0.121 | 0.122 | 0.001 |
| 10YrCHI3Hr | 0.035 | 0.032 | -0.003 | 0.136 | 0.132 | -0.004 | 0.145 | 0.141 | -0.004 | 0.162 | 0.159 | -0.003 |
| 25YrCHI3Hr | 0.047 | 0.038 | -0.009 | 0.181 | 0.172 | -0.009 | 0.194 | 0.185 | -0.009 | 0.218 | 0.209 | -0.009 |
| 50YrCHI3Hr | 0.057 | 0.043 | -0.014 | 0.219 | 0.205 | -0.014 | 0.234 | 0.220 | -0.014 | 0.263 | 0.249 | -0.014 |
| 100YrCHI3Hr | 0.067 | 0.048 | -0.019 | 0.258 | 0.239 | -0.019 | 0.277 | 0.258 | -0.019 | 0.311 | 0.292 | -0.019 |
| 2YrSCS24Hr | 0.024 | 0.024 | 0.000 | 0.090 | 0.091 | 0.001 | 0.096 | 0.097 | 0.001 | 0.107 | 0.108 | 0.001 |
| 5YrSCS24Hr | 0.038 | 0.032 | -0.006 | 0.148 | 0.142 | -0.006 | 0.158 | 0.152 | -0.006 | 0.177 | 0.171 | -0.006 |
| 10YrSCS24Hr | 0.049 | 0.037 | -0.012 | 0.189 | 0.178 | -0.011 | 0.202 | 0.191 | -0.011 | 0.227 | 0.216 | -0.011 |
| 25YrSCS24Hr | 0.062 | 0.044 | -0.018 | 0.242 | 0.224 | -0.018 | 0.259 | 0.242 | -0.017 | 0.291 | 0.274 | -0.017 |
| 50YrSCS24Hr | 0.073 | 0.049 | -0.024 | 0.284 | 0.260 | -0.024 | 0.305 | 0.281 | -0.024 | 0.343 | 0.320 | -0.023 |
| 100YrSCS24Hr | 0.084 | 0.055 | -0.029 | 0.329 | 0.300 | -0.029 | 0.354 | 0.325 | -0.029 | 0.399 | 0.370 | -0.029 |
| July 1st, 1979 | 0.090 | 0.060 | -0.030 | 0.372 | 0.345 | -0.027 | 0.399 | 0.371 | -0.028 | 0.448 | 0.420 | -0.028 |
| August 4th, 1988 | 0.079 | 0.053 | -0.026 | 0.314 | 0.287 | -0.027 | 0.338 | 0.313 | -0.025 | 0.379 | 0.354 | -0.025 |
| August 8th, 1996 | 0.052 | 0.040 | -0.012 | 0.210 | 0.199 | -0.011 | 0.226 | 0.215 | -0.011 | 0.254 | 0.243 | -0.011 |
| 100YrCHI+20% | 0.090 | 0.061 | -0.029 | 0.346 | 0.321 | -0.025 | 0.372 | 0.345 | -0.027 | 0.419 | 0.392 | -0.027 |

Table 2: Pre and Post Development Peak Flow Summary

| Event | Node | J5 | | Node | J6 | | Node | J7 | | Node | J8 | |
|------------------|-------|-------|--------|-------|-------|-------|-------|-------|--------|-------|-------|--------|
| | Pre | Post | Diff | Pre | Post | Diff | Pre | Post | Diff | Pre | Post | Diff |
| Area (ha) | 6.86 | 7.23 | 0.37 | 1.01 | 1.02 | 0.01 | 1.83 | 1.46 | -0.37 | 13.1 | 13.09 | -0.01 |
| 2YrCHI3Hr | 0.080 | 0.086 | 0.006 | 0.016 | 0.021 | 0.005 | 0.019 | 0.018 | -0.001 | 0.141 | 0.146 | 0.005 |
| 5YrCHI3Hr | 0.147 | 0.149 | 0.002 | 0.025 | 0.028 | 0.003 | 0.035 | 0.034 | -0.001 | 0.264 | 0.265 | 0.001 |
| 10YrCHI3Hr | 0.197 | 0.196 | -0.001 | 0.034 | 0.034 | 0.000 | 0.047 | 0.047 | 0.000 | 0.361 | 0.357 | -0.004 |
| 25YrCHI3Hr | 0.267 | 0.260 | -0.007 | 0.047 | 0.047 | 0.000 | 0.065 | 0.064 | -0.001 | 0.493 | 0.483 | -0.010 |
| 50YrCHI3Hr | 0.323 | 0.312 | -0.011 | 0.057 | 0.057 | 0.000 | 0.079 | 0.078 | -0.001 | 0.602 | 0.586 | -0.016 |
| 100YrCHI3Hr | 0.384 | 0.368 | -0.016 | 0.069 | 0.069 | 0.000 | 0.095 | 0.094 | -0.001 | 0.721 | 0.700 | -0.021 |
| 2YrSCS24Hr | 0.128 | 0.130 | 0.002 | 0.023 | 0.023 | 0.000 | 0.032 | 0.031 | -0.001 | 0.233 | 0.234 | 0.001 |
| 5YrSCS24Hr | 0.215 | 0.211 | -0.004 | 0.039 | 0.039 | 0.000 | 0.054 | 0.053 | -0.001 | 0.400 | 0.393 | -0.007 |
| 10YrSCS24Hr | 0.277 | 0.268 | -0.009 | 0.051 | 0.051 | 0.000 | 0.070 | 0.069 | -0.001 | 0.517 | 0.505 | -0.012 |
| 25YrSCS24Hr | 0.357 | 0.342 | -0.015 | 0.066 | 0.066 | 0.000 | 0.092 | 0.090 | -0.002 | 0.675 | 0.656 | -0.019 |
| 50YrSCS24Hr | 0.421 | 0.400 | -0.021 | 0.079 | 0.079 | 0.000 | 0.110 | 0.107 | -0.003 | 0.800 | 0.776 | -0.024 |
| 100YrSCS24Hr | 0.491 | 0.465 | -0.026 | 0.093 | 0.093 | 0.000 | 0.129 | 0.126 | -0.003 | 0.939 | 0.906 | -0.033 |
| July 1st, 1979 | 0.557 | 0.530 | -0.027 | 0.094 | 0.094 | 0.000 | 0.137 | 0.130 | -0.007 | 1.057 | 1.018 | -0.039 |
| August 4th, 1988 | 0.462 | 0.440 | -0.022 | 0.085 | 0.085 | 0.000 | 0.121 | 0.115 | -0.006 | 0.883 | 0.857 | -0.026 |
| August 8th, 1996 | 0.308 | 0.300 | -0.008 | 0.058 | 0.058 | 0.000 | 0.082 | 0.079 | -0.003 | 0.586 | 0.576 | -0.010 |
| 100YrCHI+20% | 0.519 | 0.495 | -0.024 | 0.095 | 0.095 | 0.000 | 0.131 | 0.129 | -0.002 | 0.984 | 0.951 | -0.033 |

HYDRAULICS

The detailed hydraulic analysis of the downstream study area was conducted using the US Army Corps of Engineers HEC-RAS software (version 6.6). The purpose of this hydraulic analysis is to assess the hydraulic impacts that the proposed Stratford Foxrun development may have on existing water levels for the applicable design storms.

Model Development & Parameters

The primary method used to establish cross-sections involved detailed topographic surveying, typically conducted at approximately 50-meter intervals along the watercourse. These measurements were supplemented with LiDAR data in the floodplain to enhance spatial coverage and resolution. This close spacing is essential for accurately representing the hydraulic characteristics and flow conveyance capacity of the existing channel. The selected interval aligns with HEC-RAS best practices for open-channel flow modelling in rural systems, particularly where channel geometry and slope are relatively uniform. In general, cross-section spacing between 30 and 100 meters is considered appropriate for natural channels, unless abrupt changes in geometry, slope, or hydraulic controls are present.

To ensure the model captured localized hydraulic effects, additional cross-sections were inserted at key hydraulic structures (e.g., culverts and driveway crossings) and at locations where notable changes in channel geometry or slope occurred. This approach allowed for an accurate representation of hydraulic behaviour without introducing unnecessary complexity or instability into the model. In areas not explicitly surveyed, supplementary cross-sections were generated by sampling the merged LiDAR and topographic Digital Terrain Model (DTM). This ensured that all critical sections were included to accurately reflect channel hydraulics. The extent and location of all model cross-sections are illustrated in **Figure C1** of **Attachment C**.

Existing hydraulic infrastructure, such as culverts, on the respective watercourses, was incorporated into the model based on the details obtained from the topographic surveys. Consistent with HEC-RAS technical guidelines, ineffective flow areas and expansion-contraction coefficients were appropriately applied at these locations. Typical Manning's values of 0.035 and 0.05 were applied to the roadside ditch channel bottom and over banks, respectively.

A normal downstream boundary condition was applied for all events due to the substantial difference in drainage area between Marlborough Creek and the roadside ditch. The study area at the confluence with Marlborough Creek has a drainage area of **13.1 ha**, with a channel length of **1.034 km** and an average slope of **0.6%**, based on detailed modelling presented in this report. In contrast, Marlborough Creek at the same location has a drainage area of **437.4 ha**, a channel length of **5.120 km**, and an average slope of **0.26%**, as per the Ontario Watershed Information Tool. Using the velocity method outlined in Chapter 15 of the USDA's Hydrology National Engineering Handbook, the time to peak for the study area was calculated to be **1.2 hours**, while the time to peak for Marlborough Creek was estimated at **8.8 hours**. A full summary of these calculations is provided in **Table 3** below. Given the significant difference in time to peak between the two systems, it is evident that peak flows from the study area and Marlborough Creek cannot coincide. Therefore, the application of a normal downstream boundary condition is considered appropriate.

Table 3: Watercourse Time to Peak Calculations

| Parameter | Units | Study Area | Malbrough Creek |
|-----------------------|--------------|-------------|-----------------|
| Area | (ha) | 13.1 | 437.4 |
| Channel Length | (m) | 1034 | 5120 |
| Slope | (%) | 0.60% | 0.26% |
| Flow Type | - | Short grass | Short grass |
| Average Velocity | (m/s) | 0.165 | 0.108 |
| Time of Concentration | (secs) | 6,275 | 47,262 |
| Time of Concentration | (hrs) | 1.7 | 13.1 |
| Time to Peak | (hrs) | 1.2 | 8.8 |

Results

The pre- and post-development models were run for the full range of design storms (2- to 100-Year Events) to accurately establish the existing and proposed floodplain extents within the study area. **Figures C2 and C3** illustrate the flood extents for both existing and proposed conditions during the 24-hour SCS-type storms (the critical design storm). **Figure C4** provide a comparison between the 100-year floodplain under both existing and proposed conditions. From this figure, it is shown that the 100-year floodplain extents along the ditch are reduced under post-development conditions. This demonstrates that the proposed stormwater management solution is effective and that the proposed development will not worsen existing flood conditions along the ditch. **Attachment C** also includes pre- and post-development long- and cross-section plots, along with summary tables.

This analysis also revealed that flows in the roadside ditch overtop the banks during 5- to 10-year events (depending on the design storm). This is expected, as the typical level of service for driveway crossings is generally in this range. It's crucial to note that existing driveway crossings, not the channel itself, are constricting flows and causing them to overtop the bank. Upsizing several culverts along this stretch of roadside ditch would significantly reduce the floodplain in this area.

Along Eagleson Road, approximately halfway between the railway and the Ottawa Street intersection, flows will overtop the bank and spill west to the culvert under the railway. For a conservative design, the hydraulic modelling does not account for this spill, assuming all flows proceed to the next downstream cross-section. It's also important to emphasize that for all events (up to and including the 100-year event), water levels in the roadside ditch do not reach an elevation that would impede traffic on either Eagleson Road or Ottawa Street, as the flood extents do not touch the shoulder of the road. Furthermore, the maximum 100-year floodplain extents do not affect any nearby buildings, meaning the current and proposed flood extents pose no danger to existing structures.

CONCLUSION

In summary, JFSA Canada Inc.'s hydrologic and hydraulic modelling confirms that the proposed Stratford Foxrun development's stormwater management plan effectively mitigates downstream impacts. The on-site localized depressions, with **75 mm** orifice outlets, will manage post-development runoff, ensuring peak flows for major storm events (up to 100-year) remain at or below pre-development levels.

The HEC-RAS analysis further demonstrates that the proposed SWM measures will lead to a reduction in the 100-year floodplain extent along the receiving roadside ditch. While existing culverts contribute to minor, more frequent overtopping, the development itself will not worsen these conditions or cause flooding that impedes traffic or endangers structures during major events. The findings indicate that the proposed SWM strategy for this site is sufficient and will not adversely impact downstream lands.

Yours truly,
JFSA Canada Inc.



Jonathon Burnett, B.Eng, P.Eng
Water Resource Engineer



cc: J.F. Sabourin, M.Eng, P.Eng
Director of Water Resources Projects

Figures

Figure 1: Site Boundary and Existing Watercourse

Tables

Table 1: Site Release Rates / Required Storage Volume / Ponding Depth

Table 2: Peak Flows at Key Locations

Attachments

- Attachment A: Pre-Development Hydrology
- Attachment B: Post Development Hydrology
- Attachment C: Hydraulic Analysis



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Attachment A

Pre-Development Hydrology



Legend

- Jock River Tributary
- Pre-dev. Subcatchments

Google Hybrid

EXT1

Subcatchment Name

3.212 ha

Subcatchment Area (ha)

SCALE:

1:3000

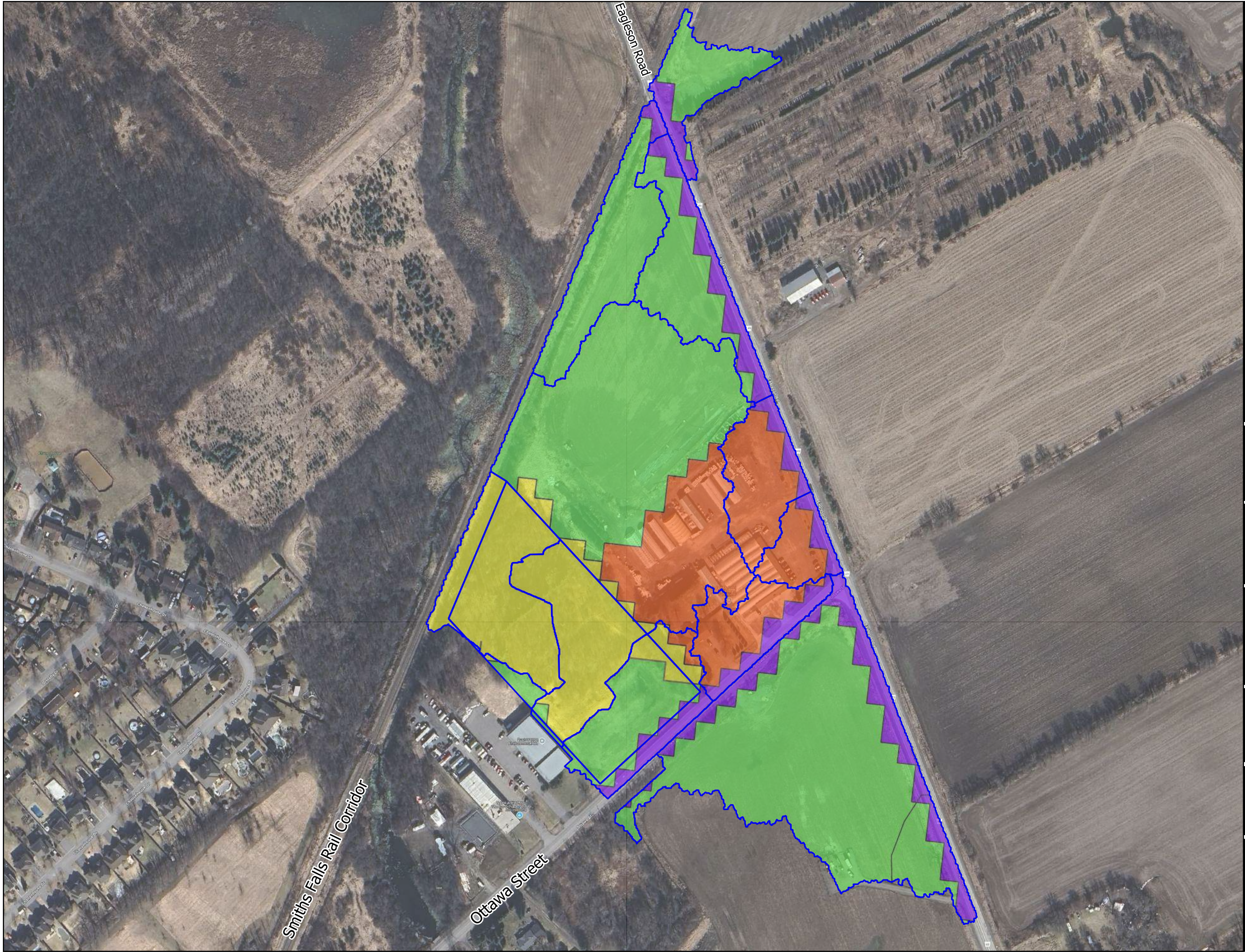
050100150 m



5923 Ottawa St – Richmond

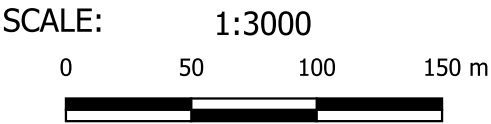
Figure A1: Existing Drainage Areas

| | |
|---------|------------|
| PROJECT | P2710(e01) |
| DRAWN | MM |
| DATE | 04-06-2025 |



Legend

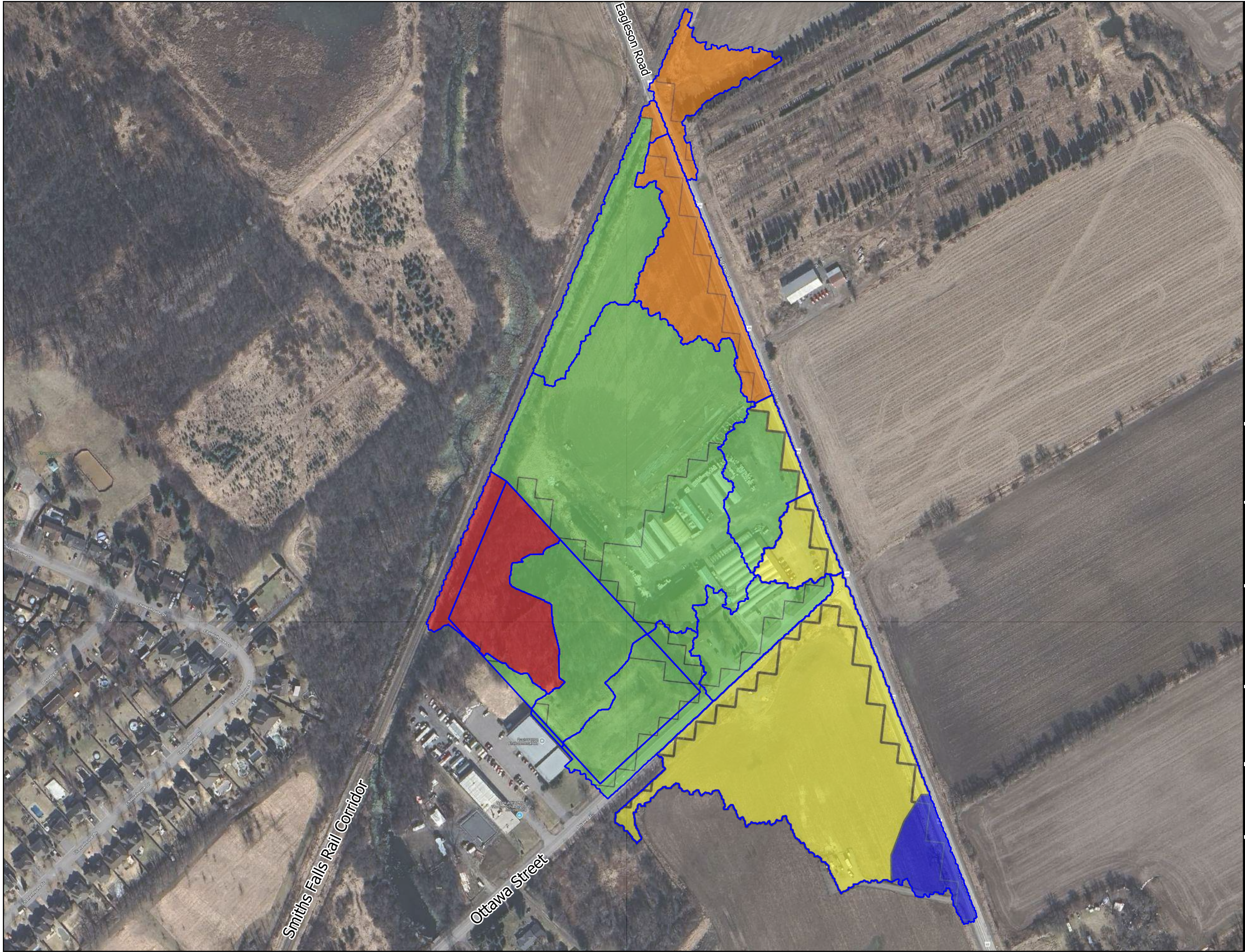
-  Pre-dev. Subcatchments
-  CN
-  Built Up Area - Pervious
-  Transportation
-  Forest
-  Tilled
- Google Hybrid









5923 Ottawa St – Richmond

Figure A2: Land Use Data

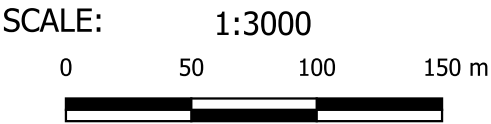
| | |
|---------|------------|
| PROJECT | P2710(e01) |
| DRAWN | MM |
| DATE | 04-06-2025 |



Legend

-  Pre-dev. Subcatchments
- Soil Name (Soil Type)
-  ERODED CHANNEL (D)
-  NORTH GOWER (D)
-  DALHOUSIE (D)
-  BRANDON (D)
-  GRENVILLE (B)

Google Hybrid



5923 Ottawa St – Richmond

Figure A3: Soil Type

| | |
|---------|------------|
| PROJECT | P2710(e01) |
| DRAWN | MM |
| DATE | 04-06-2025 |

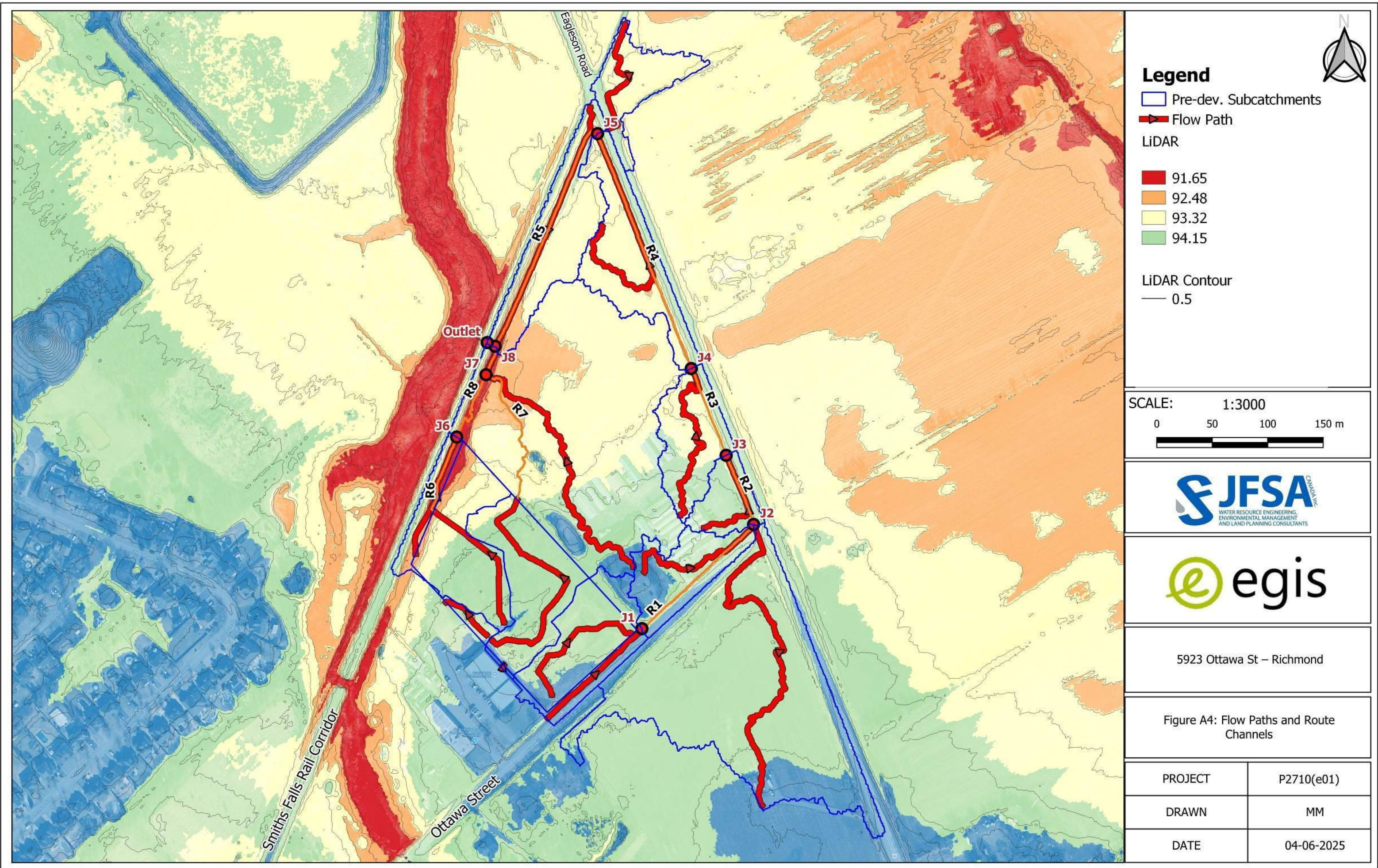


Table A1: Calculation of SCS Curve Number (CN) and Modified Curve Number (CN*)

| EXT1 (3.212 ha) | | | | | | | |
|------------------|----------------|-----------|----------------|------------|----|----------------|-------------|
| Area (ha) | Land Type | Soil Name | Soil Condition | Soil Group | CN | % of Catchment | Weighted CN |
| 0.107 | Transportation | GRENVILLE | Fair | B | 98 | 3.3% | 3.3 |
| 0.229 | Tilled | GRENVILLE | Fair | B | 69 | 7.1% | 4.9 |
| 0.403 | Transportation | BRANDON | Fair | D | 98 | 12.5% | 12.3 |
| 2.472 | Tilled | BRANDON | Fair | D | 84 | 77.0% | 64.6 |
| | | | | | | CN | 85 |
| | | | | | | CN* | 80 |

| EXT2 (0.285 ha) | | | | | | | |
|------------------|--------------------------|-------------|----------------|------------|----|----------------|-------------|
| Area (ha) | Land Type | Soil Name | Soil Condition | Soil Group | CN | % of Catchment | Weighted CN |
| 0.04 | Built Up Area - Pervious | NORTH GOWER | Fair | D | 80 | 14.0% | 11.2 |
| 0.051 | Tilled | NORTH GOWER | Fair | D | 84 | 17.9% | 15.0 |
| 0.067 | Forest | NORTH GOWER | Fair | D | 79 | 23.5% | 18.6 |
| 0.127 | Transportation | NORTH GOWER | Fair | D | 98 | 44.6% | 43.7 |
| | | | | | | CN | 89 |
| | | | | | | CN* | 85 |

| EXT3 (0.56 ha) | | | | | | | |
|-----------------|--------------------------|-------------|----------------|------------|----|----------------|-------------|
| Area (ha) | Land Type | Soil Name | Soil Condition | Soil Group | CN | % of Catchment | Weighted CN |
| 0 | Forest | NORTH GOWER | Fair | D | 79 | 0.0% | 0.0 |
| 0.17 | Transportation | NORTH GOWER | Fair | D | 98 | 30.4% | 29.8 |
| 0.39 | Built Up Area - Pervious | NORTH GOWER | Fair | D | 80 | 69.6% | 55.7 |
| | | | | | | CN | 85 |
| | | | | | | CN* | 80 |

| EXT4 (0.309 ha) | | | | | | | |
|------------------|--------------------------|-----------|----------------|------------|----|----------------|-------------|
| Area (ha) | Land Type | Soil Name | Soil Condition | Soil Group | CN | % of Catchment | Weighted CN |
| 0.074 | Transportation | BRANDON | Fair | D | 98 | 23.9% | 23.5 |
| 0.235 | Built Up Area - Pervious | BRANDON | Fair | D | 80 | 76.1% | 60.8 |
| | | | | | | CN | 84 |
| | | | | | | CN* | 79 |

| EXT5 (0.594 ha) | | | | | | | |
|------------------|--------------------------|-------------|----------------|------------|----|----------------|-------------|
| Area (ha) | Land Type | Soil Name | Soil Condition | Soil Group | CN | % of Catchment | Weighted CN |
| 0.084 | Transportation | BRANDON | Fair | D | 98 | 14.1% | 13.9 |
| 0.51 | Built Up Area - Pervious | NORTH GOWER | Fair | D | 80 | 85.9% | 68.7 |
| | | | | | | CN | 83 |
| | | | | | | CN* | 76 |

Table A1: Calculation of SCS Curve Number (CN) and Modified Curve Number (CN*)

| Pre10 (0.803 ha) | | | | | | | |
|-------------------|-----------|----------------|----------------|------------|----|----------------|-------------|
| Area (ha) | Land Type | Soil Name | Soil Condition | Soil Group | CN | % of Catchment | Weighted CN |
| 0.803 | Forest | ERODED CHANNEL | Fair | D | 79 | 100.0% | 79.0 |
| | | | | | | CN | 79 |
| | | | | | | CN* | 71 |

| Pre11 (0.069 ha) | | | | | | | |
|-------------------|-----------|-------------|----------------|------------|----|----------------|-------------|
| Area (ha) | Land Type | Soil Name | Soil Condition | Soil Group | CN | % of Catchment | Weighted CN |
| 0.004 | Forest | NORTH GOWER | Fair | D | 79 | 5.8% | 4.6 |
| 0.065 | Tilled | NORTH GOWER | Fair | D | 84 | 94.2% | 79.1 |
| | | | | | | CN | 84 |
| | | | | | | CN* | 78 |

| Pre2 (0.565 ha) | | | | | | | |
|------------------|----------------|-------------|----------------|------------|----|----------------|-------------|
| Area (ha) | Land Type | Soil Name | Soil Condition | Soil Group | CN | % of Catchment | Weighted CN |
| 0.017 | Transportation | NORTH GOWER | Fair | D | 98 | 3.0% | 2.9 |
| 0.066 | Forest | NORTH GOWER | Fair | D | 79 | 11.7% | 9.2 |
| 0.483 | Tilled | NORTH GOWER | Fair | D | 84 | 85.5% | 71.8 |
| | | | | | | CN | 84 |
| | | | | | | CN* | 78 |

| Pre9 (0.83 ha) | | | | | | | |
|-----------------|--------------------------|-------------|----------------|------------|----|----------------|-------------|
| Area (ha) | Land Type | Soil Name | Soil Condition | Soil Group | CN | % of Catchment | Weighted CN |
| 0 | Built Up Area - Pervious | NORTH GOWER | Fair | D | 80 | 0.0% | 0.0 |
| 0.014 | Tilled | NORTH GOWER | Fair | D | 84 | 1.7% | 1.4 |
| 0.815 | Forest | NORTH GOWER | Fair | D | 79 | 98.2% | 77.6 |
| | | | | | | CN | 79 |
| | | | | | | CN* | 71 |

Table A2: Time to Peak Calculations

| Parameter | Units | EXT1 | EXT2 | EXT3 | EXT4 | EXT5 | EXT6 | EXT7 | EXT8 | EXT9 | EXT9a | EXT10 | Pre10 | Pre11 | Pre2 | Pre9 |
|--|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Area | ha | 3.211 | 0.285 | 0.560 | 0.309 | 0.594 | 0.864 | 0.471 | 0.834 | 3.571 | 0.011 | 0.203 | 0.803 | 0.069 | 0.566 | 0.829 |
| CN | - | 80 | 85 | 80 | 79 | 76 | 85 | 83 | 79 | 76 | 78 | 71 | 71 | 78 | 78 | 71 |
| Ptotal to calc C from CN, use 2 yr 24 hr Chicago storm | P(mm) | 48.7 | 48.7 | 48.7 | 48.7 | 48.7 | 48.7 | 48.7 | 48.7 | 48.7 | 48.7 | 48.7 | 48.7 | 48.7 | 48.7 | 48.7 |
| | la(mm) | 5.00 | 5.00 | 5.00 | 5.00 | 5.00 | 5.00 | 5.00 | 5.00 | 5.00 | 5.00 | 5.00 | 5.00 | 5.00 | 5.00 | 5.00 |
| | RV(mm) | 17.7 | 21.4 | 18.0 | 16.9 | 15.4 | 21.2 | 19.7 | 17.1 | 15.6 | 16.7 | 12.9 | 12.9 | 16.4 | 16.7 | 12.9 |
| C (From Chicago storm) | - | 0.363 | 0.439 | 0.370 | 0.348 | 0.317 | 0.436 | 0.404 | 0.351 | 0.319 | 0.342 | 0.265 | 0.265 | 0.337 | 0.342 | 0.265 |
| Length of Channel | m | 404 | 121 | 161 | 116 | 215 | 279 | 140 | 263 | 344 | 5 | 121 | 135 | 54 | 145 | 236 |
| | ft | 1327 | 397 | 527 | 381 | 705 | 916 | 459 | 862 | 1128 | 15 | 398 | 443 | 176 | 475 | 776 |
| Elevation of Head Water | m | 94.63 | 94.17 | 94.91 | 93.95 | 94.08 | 92.97 | 93.24 | 93.52 | 94.94 | 94.74 | 91.69 | 94.14 | 94.09 | 94.34 | 94.11 |
| | ft | 310 | 309 | 311 | 308 | 309 | 305 | 306 | 307 | 311 | 311 | 301 | 309 | 309 | 310 | 309 |
| Elevation of Outlet | m | 92.98 | 93.57 | 93.00 | 92.69 | 92.44 | 91.96 | 92.11 | 90.43 | 90.46 | 94.55 | 91.11 | 91.71 | 93.58 | 93.80 | 93.20 |
| | ft | 305 | 307 | 305 | 304 | 303 | 302 | 302 | 297 | 297 | 310 | 299 | 301 | 307 | 308 | 306 |
| Average Slope | % | 0.41% | 0.50% | 1.18% | 1.08% | 0.76% | 0.36% | 0.81% | 1.17% | 1.30% | 4.28% | 0.49% | 1.80% | 0.96% | 0.38% | 0.38% |
| Flow Type (Uplands) | - | B | B | B | B | B | B | B | B | B | B | B | B | B | B | B |
| Kirpich | | | | | | | | | | | | | | | | |
| Time of Concentration | mins | 16 | 6 | 5 | 4 | 8 | 13 | 6 | 8 | 9 | 0 | 6 | 4 | 2 | 8 | 11 |
| Time to Peak | min | 11 | 4 | 4 | 3 | 5 | 9 | 4 | 5 | 6 | 0 | 4 | 3 | 2 | 5 | 7 |
| Time to Peak | Hours | 0.18 | 0.07 | 0.06 | 0.05 | 0.09 | 0.14 | 0.06 | 0.09 | 0.10 | 0.00 | 0.07 | 0.04 | 0.03 | 0.09 | 0.12 |
| FAA (From Chicago storm) | | | | | | | | | | | | | | | | |
| Time of Concentration | mins | 65 | 30 | 29 | 26 | 41 | 51 | 29 | 37 | 43 | 3 | 38 | 26 | 18 | 41 | 58 |
| Time to Peak | mins | 43 | 20 | 19 | 17 | 27 | 34 | 19 | 25 | 29 | 2 | 25 | 17 | 12 | 27 | 38 |
| Time to Peak | Hours | 0.72 | 0.33 | 0.32 | 0.29 | 0.45 | 0.56 | 0.32 | 0.42 | 0.48 | 0.04 | 0.42 | 0.29 | 0.21 | 0.46 | 0.64 |
| Barnsby Williams | | | | | | | | | | | | | | | | |
| Time of Concentration | mins | 25 | 9 | 9 | 7 | 14 | 20 | 9 | 15 | 17 | 0 | 9 | 7 | 4 | 11 | 17 |
| Time to Peak | mins | 17 | 6 | 6 | 5 | 9 | 13 | 6 | 10 | 11 | 0 | 6 | 5 | 3 | 7 | 11 |
| Time to Peak | Hours | 0.28 | 0.10 | 0.11 | 0.08 | 0.15 | 0.22 | 0.10 | 0.17 | 0.18 | 0.00 | 0.10 | 0.08 | 0.05 | 0.12 | 0.19 |
| SCS | | | | | | | | | | | | | | | | |
| Time of Concentration | mins | 63 | 18 | 17 | 15 | 31 | 42 | 17 | 27 | 34 | 1 | 28 | 16 | 9 | 30 | 54 |
| Time to Peak | mins | 42 | 12 | 12 | 10 | 21 | 28 | 12 | 18 | 23 | 0 | 19 | 11 | 6 | 20 | 36 |
| Time to Peak | Hours | 0.70 | 0.20 | 0.19 | 0.16 | 0.34 | 0.47 | 0.19 | 0.30 | 0.38 | 0.01 | 0.31 | 0.18 | 0.10 | 0.34 | 0.61 |
| Uplands | | | | | | | | | | | | | | | | |
| Time of Concentration | mins | 69 | 19 | 16 | 12 | 27 | 50 | 17 | 26 | 33 | 0 | 19 | 11 | 6 | 26 | 41 |
| Time to Peak | mins | 46 | 12 | 11 | 8 | 18 | 34 | 11 | 18 | 22 | 0 | 13 | 7 | 4 | 17 | 28 |
| Time to Peak | Hours | 0.76 | 0.21 | 0.18 | 0.13 | 0.30 | 0.56 | 0.19 | 0.29 | 0.36 | 0.00 | 0.21 | 0.12 | 0.07 | 0.28 | 0.46 |
| Selected Method: FAA (From Chicago storm) | | | | | | | | | | | | | | | | |
| Time to Peak | min | 43 | 20 | 19 | 17 | 27 | 34 | 19 | 25 | 29 | 2 | 25 | 17 | 12 | 27 | 38 |
| Time to Peak | Hours | 0.72 | 0.33 | 0.32 | 0.29 | 0.45 | 0.56 | 0.32 | 0.42 | 0.48 | 0.04 | 0.42 | 0.29 | 0.21 | 0.46 | 0.64 |
| Velocity | m/s | 0.16 | 0.10 | 0.14 | 0.11 | 0.13 | 0.14 | 0.12 | 0.18 | 0.20 | 0.04 | 0.08 | 0.13 | 0.07 | 0.09 | 0.10 |

```

1  20      Metric units / ID numbers OFF
2  *#*****
   *****
3  *#  SWMHYMO  / INPUT DATA FILE
4  *#*****
   *****
5  *#  Project Name   : [5923 Ottawa St]
6  *#  Project Number: [P2710(e01)]
7  *#  Date           : [2025 FEB 05]
8  *#  Modeller       : [MM]
9  *#  Company        : JFSA Canada Inc.
10 *#  License #      : 2549237
11 *#*****
   *****
12 *# Model developed to simulate runoff from subcatchments under pre development conditions
13 *#*****
   *****
14 *%  25 mm Storm based on 2-Year, 3-Hour Chicago Storm
15 START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[002]
16                [ "002YC3H.stm" ] <--storm filename, one per line for NSTORM time
17 *%-----|-----
18 READ STORM      STORM_FILENAME=[ "STORM.001" ]
19 *%-----|-----
20 *#*****
   *****
21 *#  EXT1
22 *#*****
   *****
23 CALIB NASHYD    NHYD=[ "EXT1" ], DT[1] (min), AREA=[3.211] (ha),
24                DWF=[0] (cms), CN=[80],
25                IA=[4.67] (mm), N=[3], TP[0.72] (hrs),
26                RAINFALL[ , , -1]
27 *#*****
   *****
28 *#  EXT2
29 *#*****
   *****
30 CALIB NASHYD    NHYD=[ "EXT2" ], DT[1] (min), AREA=[0.285] (ha),
31                DWF=[0] (cms), CN=[85],
32                IA=[4.67] (mm), N=[3], TP[0.33] (hrs),
33                RAINFALL[ , , -1]
34 *#*****
   *****
35 *#  EXT3
36 *#*****
   *****
37 CALIB NASHYD    NHYD=[ "EXT3" ], DT[1] (min), AREA=[0.560] (ha),
38                DWF=[0] (cms), CN=[80],
39                IA=[4.67] (mm), N=[3], TP[0.32] (hrs),
40                RAINFALL[ , , -1]
41 *#*****
   *****
42 *#  EXT4
43 *#*****
   *****
44 CALIB NASHYD    NHYD=[ "EXT4" ], DT[1] (min), AREA=[0.309] (ha),
45                DWF=[0] (cms), CN=[79],
46                IA=[4.67] (mm), N=[3], TP[0.29] (hrs),
47                RAINFALL[ , , -1]
48 *#*****
   *****
49 *#  EXT5
50 *#*****
   *****
51 CALIB NASHYD    NHYD=[ "EXT5" ], DT[1] (min), AREA=[0.594] (ha),
52                DWF=[0] (cms), CN=[76],
53                IA=[4.67] (mm), N=[3], TP[0.45] (hrs),
54                RAINFALL[ , , -1]
55 *#*****

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*****
56 *# EXT6
57 *#*****
*****
58 CALIB NASHYD      NHYD=["EXT6"], DT[1] (min), AREA=[0.864] (ha),
59                   DWF=[0] (cms), CN=[85],
60                   IA=[4.67] (mm), N=[3], TP[0.56] (hrs),
61                   RAINFALL[ , , -1]
62 *#*****
*****
63 *# EXT7
64 *#*****
*****
65 CALIB NASHYD      NHYD=["EXT7"], DT[1] (min), AREA=[0.471] (ha),
66                   DWF=[0] (cms), CN=[83],
67                   IA=[4.67] (mm), N=[3], TP[0.32] (hrs),
68                   RAINFALL[ , , -1]
69 *#*****
*****
70 *# EXT8
71 *#*****
*****
72 CALIB NASHYD      NHYD=["EXT8"], DT[1] (min), AREA=[0.834] (ha),
73                   DWF=[0] (cms), CN=[79],
74                   IA=[4.67] (mm), N=[3], TP[0.42] (hrs),
75                   RAINFALL[ , , -1]
76 *#*****
*****
77 *# EXT9
78 *#*****
*****
79 CALIB NASHYD      NHYD=["EXT9"], DT[1] (min), AREA=[3.571] (ha),
80                   DWF=[0] (cms), CN=[76],
81                   IA=[4.67] (mm), N=[3], TP[0.48] (hrs),
82                   RAINFALL[ , , -1]
83 *#*****
*****
84 *# EXT9a
85 *#*****
*****
86 CALIB NASHYD      NHYD=["EXT9a"], DT[1] (min), AREA=[0.011] (ha),
87                   DWF=[0] (cms), CN=[78],
88                   IA=[4.67] (mm), N=[3], TP[0.04] (hrs),
89                   RAINFALL[ , , -1]
90 *#*****
*****
91 *# EXT10
92 *#*****
*****
93 CALIB NASHYD      NHYD=["EXT10"], DT[1] (min), AREA=[0.203] (ha),
94                   DWF=[0] (cms), CN=[71],
95                   IA=[4.67] (mm), N=[3], TP[0.42] (hrs),
96                   RAINFALL[ , , -1]
97 *#*****
*****
98 *# Pre2
99 *#*****
*****
100 CALIB NASHYD      NHYD=["Pre2"], DT[1] (min), AREA=[0.566] (ha),
101                   DWF=[0] (cms), CN=[78],
102                   IA=[4.67] (mm), N=[3], TP[0.46] (hrs),
103                   RAINFALL[ , , -1]
104 *#*****
*****
105 *# Pre9
106 *#*****
*****
107 CALIB NASHYD      NHYD=["Pre9"], DT[1] (min), AREA=[0.829] (ha),
108                   DWF=[0] (cms), CN=[71],

```



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109             IA=[4.67] (mm), N=[3], TP[0.64] (hrs),
110             RAINFALL[ , , -1]
111 *#*****
112 *# Pre10
113 *#*****
114 CALIB NASHYD      NHYD=["Pre10"], DT[1] (min), AREA=[0.803] (ha),
115                   DWF=[0] (cms), CN=[71],
116                   IA=[4.67] (mm), N=[3], TP[0.29] (hrs),
117                   RAINFALL[ , , -1]
118 *#*****
119 *# Pre11
120 *#*****
121 CALIB NASHYD      NHYD=["Pre11"], DT[1] (min), AREA=[0.069] (ha),
122                   DWF=[0] (cms), CN=[78],
123                   IA=[4.67] (mm), N=[3], TP[0.21] (hrs),
124                   RAINFALL[ , , -1]
125 *#*****
126 ADD HYD           NHYDsum=["J1"], NHYDs to add=["EXT2"+"Pre2"]
127 *%-----|-----|
128 * NOTE: Cross-section number 849.0434 is taken from HEC-RAS Model
129 ROUTE CHANNEL     NHYDout=["R1"], NHYDin=["J1"], RDT=[1] (min),
130                   CHLGTH=[143.151] (m), CHSLOPE=[0.394] (%), FPSLOPE=[0.394] (%),
131                   SECNUM=[849.0434], NSEG=[3],
132                   ( SEGROUGH, SEGDIST (m))=[0.08,18.95 -0.035,26.78 0.08,35.18] NSEG
133                   times
134                   ( DISTANCE (m), ELEVATION (m))=[0.48, 94.05]
135                   [3.19, 93.99]
136                   [6.85, 93.91]
137                   [10.48, 93.87]
138                   [17.45, 93.85]
139                   [18.95, 93.84]
140                   [20.36, 93.81]
141                   [22.3, 93.76]
142                   [22.53, 93.72]
143                   [23.98, 93.35]
144                   [24.35, 93.33]
145                   [24.65, 93.37]
146                   [25.04, 93.45]
147                   [26.04, 93.74]
148                   [26.44, 93.82]
149                   [26.78, 93.87]
150                   [29.14, 94.11]
151                   [33.98, 94.26]
152                   [35.18, 94.26]
153 *%-----|-----|
154 ADD HYD           NHYDsum=["J2"], NHYDs to add=["R1"+"EXT3"+"EXT1"]
155 *%-----|-----|
156 * NOTE: Cross-section number 737.5813 is taken from HEC-RAS Model
157 ROUTE CHANNEL     NHYDout=["R2"], NHYDin=["J2"], RDT=[1] (min),
158                   CHLGTH=[73.338] (m), CHSLOPE=[0.425] (%), FPSLOPE=[0.425] (%),
159                   SECNUM=[737.5813], NSEG=[3],
160                   ( SEGROUGH, SEGDIST (m))=[0.08,8.4 -0.035,16.42 0.08,22.6] NSEG
161                   times
162                   ( DISTANCE (m), ELEVATION (m))=[0, 93.52]
163                   [1.08, 93.5]
164                   [4.37, 93.48]
165                   [6.31, 93.45]
166                   [8.4, 93.38]
167                   [9.5, 93.31]
168                   [10.49, 93.23]
169                   [10.99, 93.18]
170                   [12.4, 92.94]
171                   [13.11, 92.84]
172                   [13.67, 92.92]

```

```

171                                     [16.42, 93.6]
172                                     [16.91, 93.65]
173                                     [17.97, 93.65]
174                                     [19, 93.83]
175                                     [19.51, 93.89]
176                                     [21.06, 93.94]
177                                     [22.6, 93.95]
178 *%-----|-----
179 ADD HYD          NHYDsum=["J3"], NHYDs to add=["R2"+"EXT4"]
180 *%-----|-----
181 * NOTE: Cross-section number 675.4097 is taken from HEC-RAS Model
182 ROUTE CHANNEL    NHYDout=["R3"], NHYDin=["J3"], RDT=[1] (min),
183                  CHLGTH=[92.08] (m), CHSLOPE=[0.274] (%), FPSLOPE=[0.274] (%),
184                  SECNUM=[675.4097], NSEG=[3],
185                  ( SEGROUGH, SEGDIST (m))=[0.08,31.64 -0.035,42.44 0.08,48.87] NSEG
186                  times
187                  ( DISTANCE (m), ELEVATION (m))=[30.59, 93.12]
188                  [31.64, 93.13]
189                  [34.35, 93.08]
190                  [35.18, 93.03]
191                  [37.78, 92.72]
192                  [38.25, 92.64]
193                  [38.7, 92.61]
194                  [39.74, 92.76]
195                  [42.44, 93.41]
196                  [42.89, 93.49]
197                  [43.97, 93.57]
198                  [44.92, 93.6]
199                  [46.07, 93.67]
200                  [48.87, 93.74]
201 *%-----|-----
202 ADD HYD          NHYDsum=["J4"], NHYDs to add=["R3"+"EXT5"]
203 *%-----|-----
204 * NOTE: Cross-section number 518.7506 is taken from HEC-RAS Model
205 ROUTE CHANNEL    NHYDout=["R4"], NHYDin=["J4"], RDT=[1] (min),
206                  CHLGTH=[251.495] (m), CHSLOPE=[0.19] (%), FPSLOPE=[0.19] (%),
207                  SECNUM=[518.7506], NSEG=[3],
208                  ( SEGROUGH, SEGDIST (m))=[0.08,51.48 -0.035,59.39 0.08,66.4] NSEG
209                  times
210                  ( DISTANCE (m), ELEVATION (m))=[0, 92.92]
211                  [4.26, 92.9]
212                  [48.31, 92.76]
213                  [51.48, 92.76]
214                  [53.64, 92.7]
215                  [55.33, 92.29]
216                  [55.44, 92.29]
217                  [56.43, 92.37]
218                  [56.97, 92.43]
219                  [59.39, 93.27]
220                  [59.74, 93.37]
221                  [60.8, 93.52]
222                  [63.31, 93.71]
223                  [66.4, 93.76]
224 *%-----|-----
225 ADD HYD          NHYDsum=["J5"], NHYDs to add=["R4"+"EXT6"+"EXT7"]
226 *%-----|-----
227 * NOTE: Cross-section number 275.0857 is taken from HEC-RAS Model
228 ROUTE CHANNEL    NHYDout=["R5"], NHYDin=["J5"], RDT=[1] (min),
229                  CHLGTH=[237.343] (m), CHSLOPE=[0.644] (%), FPSLOPE=[0.644] (%),
230                  SECNUM=[275.0857], NSEG=[3],
231                  ( SEGROUGH, SEGDIST (m))=[0.08,40.82 -0.035,53.64 0.08,57.93] NSEG
232                  times
233                  ( DISTANCE (m), ELEVATION (m))=[36.16, 92.63]
234                  [40.82, 92.97]
235                  [41.39, 92.9]
236                  [44.69, 91.72]
237                  [45.24, 91.58]
238                  [46.33, 91.43]
239                  [47.41, 91.64]

```

```

237                                     [47.87, 91.75]
238                                     [49.59, 92.2]
239                                     [50.99, 92.36]
240                                     [51.44, 92.48]
241                                     [53.18, 92.98]
242                                     [53.64, 93.15]
243                                     [55.92, 93.66]
244                                     [57.93, 93.68]
245 *%-----|-----
246 * NOTE: Cross-section number 124 is taken from HEC-RAS Model
247 ROUTE CHANNEL      NHYDout=["R6"], NHYDin=["Pre10"], RDT=[1] (min),
248                   CHLGTH=[77.414] (m), CHSLOPE=[0.776] (%), FPSLOPE=[0.776] (%),
249                   SECNUM=[124], NSEG=[3],
250                   ( SEGROUGH, SEGDIST (m))=[0.08,8.34 -0.035,31.31 0.08,84.97] NSEG
251                   times
252                   ( DISTANCE (m), ELEVATION (m))=[1.78, 93.73]
253                                     [4.51, 93.54]
254                                     [5.06, 93.31]
255                                     [7.25, 92.98]
256                                     [7.79, 92.77]
257                                     [8.34, 92.49]
258                                     [9.43, 91.93]
259                                     [9.68, 91.81]
260                                     [10.53, 91.27]
261                                     [12.64, 90.92]
262                                     [14.44, 90.9]
263                                     [16.54, 91.06]
264                                     [17.64, 91.06]
265                                     [30.22, 92.3]
266                                     [31.31, 92.45]
267                                     [33.5, 92.41]
268                                     [55.37, 93.11]
269                                     [57.01, 93.2]
270                                     [84.97, 93.43]
271 *%-----|-----
272 * NOTE: Cross-section number 74 is taken from HEC-RAS Model
273 ROUTE CHANNEL      NHYDout=["R7"], NHYDin=["Pre9"], RDT=[1] (min),
274                   CHLGTH=[159.151] (m), CHSLOPE=[1.576] (%), FPSLOPE=[1.576] (%),
275                   SECNUM=[74], NSEG=[3],
276                   ( SEGROUGH, SEGDIST (m))=[0.08,4.67 -0.035,81.24 0.08,82.88] NSEG
277                   times
278                   ( DISTANCE (m), ELEVATION (m))=[1.94, 93.64]
279                                     [4.67, 93.32]
280                                     [5.77, 93.15]
281                                     [7.41, 92.69]
282                                     [7.95, 92.37]
283                                     [9.36, 91.71]
284                                     [10.12, 91.22]
285                                     [10.49, 91.06]
286                                     [12.64, 90.89]
287                                     [16.16, 90.92]
288                                     [18.83, 91.66]
289                                     [19.59, 92.02]
290                                     [21.62, 92.39]
291                                     [24.87, 92.48]
292                                     [30.37, 92.55]
293                                     [34.37, 92.65]
294                                     [77.41, 92.82]
295                                     [80.6, 93.25]
296                                     [81.24, 93.48]
297                                     [82.88, 93.79]
298 *%-----|-----
299 ADD HYD             NHYDsum=["J6"], NHYDs to add=["R6"+"EXT10"]
300 *%-----|-----
301 * NOTE: Cross-section number 49 is taken from HEC-RAS Model
302 ROUTE CHANNEL      NHYDout=["R8"], NHYDin=["J6"], RDT=[1] (min),
303                   CHLGTH=[78.801] (m), CHSLOPE=[0.522] (%), FPSLOPE=[0.522] (%),
304                   SECNUM=[49], NSEG=[3],
305                   ( SEGROUGH, SEGDIST (m))=[0.08,8.71 -0.035,20.59 0.08,116.73] NSEG

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304         times
305         ( DISTANCE (m), ELEVATION (m))=[0, 93.36]
306         [1.93, 93.63]
307         [4.61, 93.26]
308         [6.23, 93.1]
309         [8.19, 92.26]
310         [8.71, 91.84]
311         [9.86, 91.47]
312         [10.53, 91.04]
313         [13.84, 91]
314         [14.5, 91.11]
315         [16.97, 91.27]
316         [20.59, 91.76]
317         [23.3, 91.64]
318         [30.34, 91.85]
319         [35.29, 91.92]
320         [116.73, 92.96]
321 *%-----|-----
322 ADD HYD      NHYDsum=["J7"], NHYDs to add=["R8"+"R7"]
323 *%-----|-----
324 * NOTE: Cross-section number 7 is taken from HEC-RAS Model
325 ROUTE CHANNEL NHYDout=["R9"], NHYDin=["J7"], RDT=[1] (min),
326             CHLGTH=[29.445] (m), CHSLOPE=[0.887] (%), FPSLOPE=[0.887] (%),
327             SECNUM=[7], NSEG=[3],
328             ( SEGROUGH, SEGDIST (m))=[0.08,1.5 -0.035,22.44 0.08,100.08] NSEG
329             times
330             ( DISTANCE (m), ELEVATION (m))=[0, 93.4]
331             [1.5, 93.63]
332             [3.13, 93.62]
333             [4.76, 93.28]
334             [5.3, 93.25]
335             [6.52, 93.08]
336             [6.96, 92.95]
337             [10.57, 90.95]
338             [13.59, 90.67]
339             [15.83, 90.72]
340             [16.42, 90.85]
341             [18.66, 91.76]
342             [20.82, 91.86]
343             [22.44, 91.92]
344             [27.84, 91.98]
345             [30.15, 91.96]
346             [100.08, 92.61]
347 *%-----|-----
348 ADD HYD      NHYDsum=["J8"], NHYDs to add=["EXT9"+"R9"+"EXT8"+"R5"]
349 *%-----|-----
350 * Note: The pipe needs to be adjusted based on the Culvert-under-railway information
351 ROUTE PIPE    PTYPE=[1]circ, NHYDout=["Outlet"], RNUMBER=[1.0],
352             PDIAM=[525] (mm), PLNGTH=[8.407] (m), PROUGH=[0.013],
353             PSLOPE=[0.0001] (m/m),
354             NHYDin=["J8"], RDT=[1] (min)
355 *%-----|-----
356 *#####
357 *# STORMS
358 *#####
359 *% 2-Year, 3-Hour Chicago Storm
360 *START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[002]
361             ["002YC3H.stm"] <--storm filename, one per line for NSTORM time
362 *%-----|-----
363 *% 5-Year, 3-Hour Chicago Storm
364 *START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[005]
365             ["005YC3H.stm"] <--storm filename, one per line for NSTORM time
366 *%-----|-----
367 *% 10-Year, 3-Hour Chicago Storm
368 *START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[010]
369             ["010YC3H.stm"] <--storm filename, one per line for NSTORM time
370 *%-----|-----
371 *% 25-Year, 3-Hour Chicago Storm
372 *START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[025]

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370      ["025YC3H.stm"] <--storm filename, one per line for NSTORM time
371  *%-----|-----|
372  *% 50-Year, 3-Hour Chicago Storm
373  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[050]
374      ["050YC3H.stm"] <--storm filename, one per line for NSTORM time
375  *%-----|-----|
376  *% 100-Year, 3-Hour Chicago Storm
377  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[099]
378      ["100YC3H.stm"] <--storm filename, one per line for NSTORM time
379  *%-----|-----|
380  *% 2-Year, 24-Hour SCS Storm
381  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[102]
382      ["SC24002x.stm"] <--storm filename, one per line for NSTORM time
383  *%-----|-----|
384  *% 5-Year, 24-Hour SCS Storm
385  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[105]
386      ["SC24005x.stm"] <--storm filename, one per line for NSTORM time
387  *%-----|-----|
388  *% 10-Year, 24-Hour SCS Storm
389  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[110]
390      ["SC24010x.stm"] <--storm filename, one per line for NSTORM time
391  *%-----|-----|
392  *% 25-Year, 24-Hour SCS Storm
393  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[125]
394      ["SC24025x.stm"] <--storm filename, one per line for NSTORM time
395  *%-----|-----|
396  *% 50-Year, 24-Hour SCS Storm
397  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[150]
398      ["SC24050x.stm"] <--storm filename, one per line for NSTORM time
399  *%-----|-----|
400  *% 100-Year, 24-Hour SCS Storm
401  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[199]
402      ["SC24100x.stm"] <--storm filename, one per line for NSTORM time
403  *%-----|-----|
404  *% July 1st, 1979 Storm - Ottawa International Airport
405  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[1979]
406      ["19790701.stm"] <--storm filename, one per line for NSTORM time
407  *%-----|-----|
408  *% August 4th, 1988 Storm - Ottawa International Airport
409  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[1988]
410      ["19880804.stm"] <--storm filename, one per line for NSTORM time
411  *%-----|-----|
412  *% August 8th, 1996 Storm - Ottawa International Airport
413  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[1996]
414      ["19960808.stm"] <--storm filename, one per line for NSTORM time
415  *%-----|-----|
416  *% 100-Year, 3-Hour Chicago Storm + 20%
417  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[9999]
418      ["100YC3H+.STM"] <--storm filename, one per line for NSTORM time
419  *%-----|-----|
420  FINISH

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Page 0

Page 1

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Date: [2025 FEB 05]
07722 # Modeler [1926]
07723 # Computer JPSA Canada Inc.
07724 # License # 2549237
07725 #
07726 Model developed to simulate runoff from subcatchments under pre development conditions
07727
07728 *****
07729 HEAD STORM
07730 FileNm = STORM.001
07731 Comment = CHICAGO STORM 25 Year, 3 Hours
07732 [RT=10.00;HDD= 3.00;PTW= 58.23]
07733
07734 # EXT1
07735
07736 *****
07737 R0205/C00003-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07738 [CN= 80.0; W= 3.00; Tpm= .72]
07739
07740 # EXT2
07741
07742 *****
07743 R0205/C00004-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07744 [CN= 80.0; W= 3.00; Tpm= .33]
07745
07746 # EXT3
07747
07748 *****
07749 R0205/C00005-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07750 [CN= 80.0; W= 3.00; Tpm= .33]
07751
07752 # EXT4
07753
07754 *****
07755 R0205/C00006-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07756 [CN= 79.0; W= 3.00; Tpm= .31]
07757
07758 # EXT5
07759
07760 *****
07761 R0205/C00007-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07762 [CN= 76.0; W= 3.00; Tpm= .45]
07763
07764 # EXT6
07765
07766 *****
07767 R0205/C00008-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07768 [CN= 80.0; W= 3.00; Tpm= .56]
07769
07770 # EXT7
07771
07772 *****
07773 R0205/C00009-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07774 [CN= 83.0; W= 3.00; Tpm= .32]
07775
07776 # EXT8
07777
07778 *****
07779 R0205/C00010-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07780 [CN= 80.0; W= 3.00; Tpm= .42]
07781
07782 # EXT9
07783
07784 *****
07785 R0205/C00011-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07786 [CN= 76.0; W= 3.00; Tpm= .48]
07787
07788 # EXT9a
07789
07790 *****
07791 R0205/C00012-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07792 [CN= 78.0; W= 3.00; Tpm= .04]
07793
07794 # EXT10
07795
07796 *****
07797 R0205/C00013-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07798 [CN= 80.0; W= 3.00; Tpm= .42]
07799
07799 # EXT10
07800
07801 *****
07802 R0205/C00014-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07803 [CN= 80.0; W= 3.00; Tpm= .46]
07804
07805 # EXT10a
07806
07807 *****
07808 R0205/C00015-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07809 [CN= 71.0; W= 3.00; Tpm= .52]
07810
07811 # EXT10b
07812
07813 *****
07814 R0205/C00016-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07815 [CN= 71.0; W= 3.00; Tpm= .29]
07816
07817 # EXT10c
07818
07819 *****
07820 R0205/C00017-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07821 [CN= 78.0; W= 3.00; Tpm= .21]
07822
07823 # EXT10d
07824
07825 *****
07826 R0205/C00018-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07827 [CN= 80.0; W= 3.00; Tpm= .21]
07828
07829 # EXT10e
07830
07831 *****
07832 R0205/C00019-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07833 [CN= 80.0; W= 3.00; Tpm= .21]
07834
07835 # EXT10f
07836
07837 *****
07838 R0205/C00020-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07839 [CN= 80.0; W= 3.00; Tpm= .21]
07840
07841 # EXT10g
07842
07843 *****
07844 R0205/C00021-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07845 [CN= 80.0; W= 3.00; Tpm= .21]
07846
07847 # EXT10h
07848
07849 *****
07850 R0205/C00022-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07851 [CN= 80.0; W= 3.00; Tpm= .21]
07852
07853 # EXT10i
07854
07855 *****
07856 R0205/C00023-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07857 [CN= 80.0; W= 3.00; Tpm= .21]
07858
07859 # EXT10j
07860
07861 *****
07862 R0205/C00024-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07863 [CN= 80.0; W= 3.00; Tpm= .21]
07864
07865 # EXT10k
07866
07867 *****
07868 R0205/C00025-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07869 [CN= 80.0; W= 3.00; Tpm= .21]
07870
07871 # EXT10l
07872
07873 *****
07874 R0205/C00026-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07875 [CN= 80.0; W= 3.00; Tpm= .21]
07876
07877 # EXT10m
07878
07879 *****
07880 R0205/C00027-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07881 [CN= 80.0; W= 3.00; Tpm= .21]
07882
07883 # EXT10n
07884
07885 *****
07886 R0205/C00028-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07887 [CN= 80.0; W= 3.00; Tpm= .21]
07888
07889 # EXT10o
07890
07891 *****
07892 R0205/C00029-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07893 [CN= 80.0; W= 3.00; Tpm= .21]
07894
07895 # EXT10p
07896
07897 *****
07898 R0205/C00030-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07899 [CN= 80.0; W= 3.00; Tpm= .21]
07900
07901 # EXT10q
07902
07903 *****
07904 R0205/C00031-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07905 [CN= 80.0; W= 3.00; Tpm= .21]
07906
07907 # EXT10r
07908
07909 *****
07910 R0205/C00032-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07911 [CN= 80.0; W= 3.00; Tpm= .21]
07912
07913 # EXT10s
07914
07915 *****
07916 R0205/C00033-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07917 [CN= 80.0; W= 3.00; Tpm= .21]
07918
07919 # EXT10t
07920
07921 *****
07922 R0205/C00034-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07923 [CN= 80.0; W= 3.00; Tpm= .21]
07924
07925 # EXT10u
07926
07927 *****
07928 R0205/C00035-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07929 [CN= 80.0; W= 3.00; Tpm= .21]
07930
07931 # EXT10v
07932
07933 *****
07934 R0205/C00036-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07935 [CN= 80.0; W= 3.00; Tpm= .21]
07936
07937 # EXT10w
07938
07939 *****
07940 R0205/C00037-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07941 [CN= 80.0; W= 3.00; Tpm= .21]
07942
07943 # EXT10x
07944
07945 *****
07946 R0205/C00038-----Dtn-ID:INHYD-----AREHA-QFEAKMs-TpaakDate_hh:mm-----Rvwm-R.C-----DWfms
07947 [CN= 80.0; W=
```


JFSAinc. Page 3

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01441# R0102/C00014-----DtnIn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01442# CALIB NASHVD 1.0 01:Pre11 .07 .003 No_date 12:07 26.60 343 .000
01443# [CN= 78.0; Nm= 3.00; Tpe= .46]
01444# # Pre9
01445# *****
01446# *****
01447# R0102/C00015-----DtnIn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01448# CALIB NASHVD 1.0 01:Pre9 .83 .012 No_date 12:37 12.99 268 .000
01449# [CN= 71.0; Nm= 3.00; Tpe= .44]
01450# *****
01451# # Pre10
01452# *****
01453# R0102/C00016-----DtnIn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01454# CALIB NASHVD 1.0 01:Pre10 .80 .020 No_date 12:12 12.99 268 .000
01455# [CN= 71.0; Nm= 3.00; Tpe= .44]
01456# *****
01457# # Pre11
01458# *****
01459# R0102/C00017-----DtnIn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01460# CALIB NASHVD 1.0 01:Pre11 .07 .003 No_date 12:07 26.60 343 .000
01461# [CN= 78.0; Nm= 3.00; Tpe= .21]
01462# *****
01463# R0102/C00018-----DtnIn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01464# ADD HYD + 1.0 02:EXT2 .28 .011 No_date 12:14 21.63 n/a .000
01465# SUM= 1.0 02:EXT2 .57 .013 No_date 12:03 16.61 n/a .000
01466# ROUTE CHANNEL -> 1.0 01:J1 .85 .024 No_date 12:18 18.29 n/a .000
01467# R0102/C00019-----DtnIn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01468# ROUTE CHANNEL -> 1.0 02:J1 .85 .024 No_date 12:18 18.29 n/a .000
01469# [RDT= 1.00] out<- 1.0 01:R1 .85 .022 No_date 12:15 18.29 n/a .000
01470# [L/S/n= 143./ / .394/.035]
01471# (Vmax= .278;Dmax= .103)
01472# R0102/C00020-----DtnIn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01473# ADD HYD + 1.0 02:R1 .85 .022 No_date 12:15 18.29 n/a .000
01474# SUM= 1.0 02:EXT3 .56 .018 No_date 12:13 17.87 n/a .000
01475# ROUTE CHANNEL -> 1.0 01:EXT3 .31 .018 No_date 12:42 17.87 n/a .000
01476# SUM= 1.0 02:EXT2 4.62 .090 No_date 12:30 17.95 n/a .000
01477# R0102/C00021-----DtnIn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01478# ROUTE CHANNEL -> 1.0 02:J2 4.62 .090 No_date 12:30 17.95 n/a .000
01479# [RDT= 1.00] out<- 1.0 01:R2 4.62 .090 No_date 12:33 17.95 n/a .000
01480# [L/S/n= 73./ / .425/.035]
01481# (Vmax= .398;Dmax= .186)
01482# R0102/C00022-----DtnIn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01483# ADD HYD + 1.0 02:R2 4.62 .090 No_date 12:33 17.95 n/a .000
01484# SUM= 1.0 02:EXT4 .31 .010 No_date 12:12 17.22 n/a .000
01485# ROUTE CHANNEL -> 1.0 01:EXT4 4.93 .096 No_date 12:30 17.90 n/a .000
01486# R0102/C00023-----DtnIn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01487# ROUTE CHANNEL -> 1.0 01:R3 4.93 .095 No_date 12:35 17.90 n/a .000
01488# [RDT= 1.00] out<- 1.0 01:R3 4.93 .095 No_date 12:35 17.90 n/a .000
01489# [L/S/n= 92./ / .274/.035]
01490# (Vmax= .324;Dmax= .193)
01491# R0102/C00024-----DtnIn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01492# ADD HYD + 1.0 02:EXT5 .59 .013 No_date 12:22 15.46 n/a .000
01493# SUM= 1.0 01:EXT4 5.52 .107 No_date 12:33 17.64 n/a .000
01494# R0102/C00025-----DtnIn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01495# ROUTE CHANNEL -> 1.0 02:J4 5.52 .107 No_date 12:33 17.64 n/a .000
01496# [RDT= 1.00] out<- 1.0 01:R4 5.52 .098 No_date 12:46 17.64 n/a .000
01497# [L/S/n= 251./ / .394/.035]
01498# (Vmax= .309;Dmax= .210)
01499# R0102/C00026-----DtnIn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01500# ADD HYD + 1.0 02:R4 5.52 .098 No_date 12:46 17.64 n/a .000
01501# SUM= 1.0 01:EXT6 6.02 .114 No_date 12:40 18.31 n/a .000
01502# ROUTE CHANNEL -> 1.0 01:EXT6 4.47 .017 No_date 12:13 20.01 n/a .000
01503# SUM= 1.0 01:EXT5 6.86 .128 No_date 12:40 18.31 n/a .000
01504# R0102/C00027-----DtnIn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01505# ROUTE CHANNEL -> 1.0 02:J5 6.86 .128 No_date 12:40 18.31 n/a .000
01506# [RDT= 1.00] out<- 1.0 01:R5 6.86 .125 No_date 12:47 18.31 n/a .000
01507# [L/S/n= 237./ / .644/.035]
01508# (Vmax= .501;Dmax= .200)
01509# R0102/C00028-----DtnIn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01510# ROUTE CHANNEL -> 1.0 01:Pre10 .80 .020 No_date 12:12 12.99 n/a .000
01511# [RDT= 1.00] out<- 1.0 01:Pre10 .80 .020 No_date 12:12 12.99 n/a .000
01512# [L/S/n= 77./ / .776/.035]
01513# (Vmax= .492;Dmax= .041)
01514# R0102/C00029-----DtnIn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01515# ROUTE CHANNEL -> 1.0 01:Pre9 .83 .012 No_date 12:37 12.99 n/a .000
01516# [RDT= 1.00] out<- 1.0 01:Pre9 .83 .012 No_date 12:40 12.99 n/a .000
01517# [L/S/n= 159./ / .576/.035]
01518# (Vmax= .797;Dmax= .003)
01519# R0102/C00030-----DtnIn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01520# ADD HYD + 1.0 02:R6 .80 .019 No_date 12:15 13.03 n/a .000
01521# SUM= 1.0 02:EXT7 1.01 .023 No_date 12:15 13.02 n/a .000
01522# ROUTE CHANNEL -> 1.0 02:J6 1.01 .023 No_date 12:15 13.02 n/a .000
01523# [RDT= 1.00] out<- 1.0 01:R6 1.01 .023 No_date 12:19 13.02 n/a .000
01524# [L/S/n= 79./ / .797/.035]
01525# (Vmax= .423;Dmax= .017)
01526# R0102/C00031-----DtnIn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01527# ADD HYD + 1.0 02:R8 1.01 .023 No_date 12:19 13.02 n/a .000
01528# SUM= 1.0 02:EXT8 1.83 .022 No_date 12:40 13.00 n/a .000
01529# ROUTE CHANNEL -> 1.0 02:J7 1.83 .032 No_date 12:22 13.01 n/a .000
01530# [RDT= 1.00] out<- 1.0 01:R8 1.83 .032 No_date 12:23 13.01 n/a .000
01531# [L/S/n= 29./ / .887/.035]
01532# (Vmax= .543;Dmax= .004)
01533# R0102/C00032-----DtnIn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01534# ADD HYD + 1.0 02:EXT9 3.57 .074 No_date 12:25 15.46 n/a .000
01535# SUM= 1.0 02:R9 3.10 .028 No_date 12:15 13.02 n/a .000
01536# ROUTE CHANNEL -> 1.0 02:EXT9 1.83 .021 No_date 12:20 17.22 n/a .000
01537# [RDT= 1.00] out<- 1.0 01:R9 6.86 .129 No_date 12:47 18.31 n/a .000
01538# [L/S/n= 13.10 .223 No_date 12:35 16.72 n/a .000]
01539# R0102/C00033-----DtnIn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01540# ROUTE PIPE -> 1.0 01:R10 13.10 .229 No_date 12:42 16.72 n/a .000
01541# [RDT= 1.00] out<- 1.0 01:R10 13.10 .229 No_date 12:42 16.72 n/a .000
01542# [L/S/n= 77./ / .776/.035]
01543# (Vmax= .345;Dmax= .812)
01544# [Dtm= .55;Dmax= .99]
01545# *****
01546# *****
01547# *****
01548# *****
01549# *****
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01795# *****
01796# *****
01797# *****
01798# *****
01799# *****
01800# *****
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JFSAinc.

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02161+ 1.0 02:EXT10 .20 .011 No_date 12:20 36.34 n/a .000
02162+ 1.0 01:EXT5 1.01 .066 No_date 12:19 36.40 n/a .000
02163+ R0125:CO0031-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02164+ ROUTE CHANNEL -> 1.0 02:EXT6 1.01 .066 No_date 12:19 36.40 n/a .000
02165+ RDY=1.001 out<- 1.0 01:EXT8 1.01 .065 No_date 12:18 36.40 n/a .000
02166+ [L/S/n= 79./ .522/.035]
02167+ (Vmax=.441Dmax=.049)
02168+ R0125:CO0022-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02169+ ADD HYD + 1.0 02:EXT8 1.01 .065 No_date 12:18 36.40 n/a .000
02170+ + 1.0 02:EXT7 .83 .033 No_date 12:19 36.36 n/a .000
02171+ SUM= 1.0 01:EXT7 1.83 .092 No_date 12:21 36.38 n/a .000
02172+ R0125:CO0037-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02173+ ROUTE CHANNEL -> 1.0 02:EXT7 1.83 .092 No_date 12:21 36.38 n/a .000
02174+ RDY=1.001 out<- 1.0 01:RT 1.83 .092 No_date 12:22 36.38 n/a .000
02175+ [L/S/n= 29./ .887/.035]
02176+ (Vmax=.543Dmax=.062)
02177+ R0125:CO0004-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02178+ ADD HYD + 1.0 02:EXT9 3.57 .205 No_date 12:23 41.62 n/a .000
02179+ + 1.0 02:EXT8 1.83 .092 No_date 12:22 36.39 n/a .000
02180+ + 1.0 02:EXT7 .83 .033 No_date 12:19 36.36 n/a .000
02181+ + 1.0 02:EXT5 6.86 .352 No_date 12:19 47.13 n/a .000
02182+ SUM= 1.0 01:EXT8 13.10 .079 No_date 12:21 44.00 n/a .000
02183+ R0125:CO0035-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02184+ ROUTE PIPE -> 1.0 02:EXT8 13.10 .079 No_date 12:21 44.00 n/a .000
02185+ RDY=1.001 out<- 1.0 01:Outlet 13.10 .074 No_date 12:19 44.00 n/a .000
02186+ [L/S/n= 8./ .010/.013]
02187+ (Vmax=.451Dmax=1.210)
02188+ (Dtm=.53Dused=1.47)
02189+ #####
02190+ # STORMS
02191+ #####
02192+ ** END OF RUN 1 149
02193+
02194+
02195+
02196+
02197+
02198+
02199+
02200+ RUN:COMMAND#
02201+ R0150:CO0001-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02202+ START
02203+ [TZERO = .00 hrs on 0]
02204+ [METFORM= 2 (1=imperial, 2=metric output)]
02205+ [INSTORM= 1]
02206+ [NRUN = 0190]
02207+
02208+ # SWHYMO / INPUT DATA FILE
02209+
02210+ # Project Name : [5923 Ottawa St]
02211+ # Project Number: [92710(01)]
02212+ # Date : [2025 FEB 05]
02213+ # Modeler : [JPM]
02214+ # Company : [JFSA Canada Inc.]
02215+ # License #: [2549237]
02216+ *****
02217+ # Model developed to simulate runoff from subcatchments under pre development conditions
02218+ *****
02219+
02220+ R0150:CO0002-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02221+ READ STORM
02222+ File name = STORM.001
02223+ Comment = 10 years SCS Type 2 Storm 24 Hours step 10 min, City of Ottawa
02224+ [SDT=10.00;SDRM= 24.00;PTOT= 96.53]
02225+
02226+ # EXT1
02227+ R0150:CO0003-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02228+ CALIB NASHYD 1.0 01:EXT1 3.21 .182 No_date 12:40 54.31 .563 .000
02229+ [CN= 80.0; N= 3.00; Tpm=.72]
02230+
02231+ # EXT2
02232+ R0150:CO0004-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02233+ CALIB NASHYD 1.0 01:EXT2 .28 .033 No_date 12:13 61.73 .640 .000
02234+ [CN= 85.0; N= 3.00; Tpm=.46]
02235+
02236+ # EXT3
02237+ R0150:CO0005-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02238+ CALIB NASHYD 1.0 01:EXT3 .83 .068 No_date 12:19 52.94 .589 .000
02239+ [CN= 80.0; N= 3.00; Tpm=.72]
02240+
02241+ # EXT4
02242+ R0150:CO0006-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02243+ CALIB NASHYD 1.0 01:EXT4 .31 .033 No_date 12:11 52.94 .548 .000
02244+ [CN= 79.0; N= 3.00; Tpm=.42]
02245+
02246+ # EXT5
02247+ R0150:CO0007-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02248+ CALIB NASHYD 1.0 01:EXT5 .47 .052 No_date 12:12 58.64 .608 .000
02249+ [CN= 83.0; N= 3.00; Tpm=.46]
02250+
02251+ # EXT6
02252+ R0150:CO0008-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02253+ CALIB NASHYD 1.0 01:EXT6 .86 .068 No_date 12:28 61.73 .640 .000
02254+ [CN= 85.0; N= 3.00; Tpm=.56]
02255+
02256+ # EXT7
02257+ R0150:CO0009-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02258+ CALIB NASHYD 1.0 01:EXT7 .47 .052 No_date 12:12 58.64 .608 .000
02259+ [CN= 83.0; N= 3.00; Tpm=.46]
02260+
02261+ # EXT8
02262+ R0150:CO0010-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02263+ CALIB NASHYD 1.0 01:EXT8 .83 .068 No_date 12:19 52.94 .589 .000
02264+ [CN= 80.0; N= 3.00; Tpm=.72]
02265+
02266+ # EXT9
02267+ R0150:CO0011-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02268+ CALIB NASHYD 1.0 01:EXT9 3.57 .242 No_date 12:23 49.04 .508 .000
02269+ [CN= 79.0; N= 3.00; Tpm=.42]
02270+
02271+ # EXT10
02272+ R0150:CO0012-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02273+ CALIB NASHYD 1.0 01:EXT10 .20 .013 No_date 12:19 43.13 .447 .000
02274+ [CN= 71.0; N= 3.00; Tpm=.42]
02275+
02276+ # EXT11
02277+ R0150:CO0013-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02278+ CALIB NASHYD 1.0 01:EXT11 .07 .009 No_date 12:06 51.60 .535 .000
02279+ [CN= 78.0; N= 3.00; Tpm=.21]
02280+
02281+ # EXT12
02282+ R0150:CO0014-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02283+ CALIB NASHYD 1.0 01:EXT12 .46 .024 No_date 12:19 55.00 n/a .000
02284+ [CN= 79.0; N= 3.00; Tpm=.42]
02285+
02286+ # EXT13
02287+ R0150:CO0015-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02288+ CALIB NASHYD 1.0 01:EXT13 .83 .068 No_date 12:19 52.94 .589 .000
02289+ [CN= 80.0; N= 3.00; Tpm=.72]
02290+
02291+ # EXT14
02292+ R0150:CO0016-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02293+ CALIB NASHYD 1.0 01:EXT14 .31 .038 No_date 12:11 61.42 .576 .000
02294+ [CN= 79.0; N= 3.00; Tpm=.42]
02295+
02296+ # EXT15
02297+ R0150:CO0017-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02298+ CALIB NASHYD 1.0 01:EXT15 .83 .068 No_date 12:19 52.94 .589 .000
02299+ [CN= 80.0; N= 3.00; Tpm=.72]
02300+
02301+ # EXT16
02302+ R0150:CO0018-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02303+ CALIB NASHYD 1.0 01:EXT16 .83 .068 No_date 12:19 52.94 .589 .000
02304+ [CN= 80.0; N= 3.00; Tpm=.72]
02305+
02306+ # EXT17
02307+ R0150:CO0019-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02308+ CALIB NASHYD 1.0 01:EXT17 .83 .068 No_date 12:19 52.94 .589 .000
02309+ [CN= 80.0; N= 3.00; Tpm=.72]
02310+
02311+ # EXT18
02312+ R0150:CO0020-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02313+ CALIB NASHYD 1.0 01:EXT18 .83 .068 No_date 12:19 52.94 .589 .000
02314+ [CN= 80.0; N= 3.00; Tpm=.72]
02315+
02316+ # EXT19
02317+ R0150:CO0021-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02318+ CALIB NASHYD 1.0 01:EXT19 .83 .068 No_date 12:19 52.94 .589 .000
02319+ [CN= 80.0; N= 3.00; Tpm=.72]
02320+
02321+ # EXT20
02322+ R0150:CO0022-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02323+ CALIB NASHYD 1.0 01:EXT20 .83 .068 No_date 12:19 52.94 .589 .000
02324+ [CN= 80.0; N= 3.00; Tpm=.72]
02325+
02326+ # EXT21
02327+ R0150:CO0023-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02328+ CALIB NASHYD 1.0 01:EXT21 .83 .068 No_date 12:19 52.94 .589 .000
02329+ [CN= 80.0; N= 3.00; Tpm=.72]
02330+
02331+ # EXT22
02332+ R0150:CO0024-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02333+ CALIB NASHYD 1.0 01:EXT22 .83 .068 No_date 12:19 52.94 .589 .000
02334+ [CN= 80.0; N= 3.00; Tpm=.72]
02335+
02336+ # EXT23
02337+ R0150:CO0025-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02338+ CALIB NASHYD 1.0 01:EXT23 .83 .068 No_date 12:19 52.94 .589 .000
02339+ [CN= 80.0; N= 3.00; Tpm=.72]
02340+
02341+ # EXT24
02342+ R0150:CO0026-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02343+ CALIB NASHYD 1.0 01:EXT24 .83 .068 No_date 12:19 52.94 .589 .000
02344+ [CN= 80.0; N= 3.00; Tpm=.72]
02345+
02346+ # EXT25
02347+ R0150:CO0027-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02348+ CALIB NASHYD 1.0 01:EXT25 .83 .068 No_date 12:19 52.94 .589 .000
02349+ [CN= 80.0; N= 3.00; Tpm=.72]
02350+
02351+ # EXT26
02352+ R0150:CO0028-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02353+ CALIB NASHYD 1.0 01:EXT26 .83 .068 No_date 12:19 52.94 .589 .000
02354+ [CN= 80.0; N= 3.00; Tpm=.72]
02355+
02356+ # EXT27
02357+ R0150:CO0029-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02358+ CALIB NASHYD 1.0 01:EXT27 .83 .068 No_date 12:19 52.94 .589 .000
02359+ [CN= 80.0; N= 3.00; Tpm=.72]
02360+
02361+ # EXT28
02362+ R0150:CO0030-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02363+ CALIB NASHYD 1.0 01:EXT28 .83 .068 No_date 12:19 52.94 .589 .000
02364+ [CN= 80.0; N= 3.00; Tpm=.72]
02365+
02366+ # EXT29
02367+ R0150:CO0031-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02368+ CALIB NASHYD 1.0 01:EXT29 .83 .068 No_date 12:19 52.94 .589 .000
02369+ [CN= 80.0; N= 3.00; Tpm=.72]
02370+
02371+ # EXT30
02372+ R0150:CO0032-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02373+ CALIB NASHYD 1.0 01:EXT30 .83 .068 No_date 12:19 52.94 .589 .000
02374+ [CN= 80.0; N= 3.00; Tpm=.72]
02375+
02376+ # EXT31
02377+ R0150:CO0033-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02378+ CALIB NASHYD 1.0 01:EXT31 .83 .068 No_date 12:19 52.94 .589 .000
02379+ [CN= 80.0; N= 3.00; Tpm=.72]
02380+
02381+ # EXT32
02382+ R0150:CO0034-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02383+ CALIB NASHYD 1.0 01:EXT32 .83 .068 No_date 12:19 52.94 .589 .000
02384+ [CN= 80.0; N= 3.00; Tpm=.72]
02385+
02386+ # EXT33
02387+ R0150:CO0035-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02388+ CALIB NASHYD 1.0 01:EXT33 .83 .068 No_date 12:19 52.94 .589 .000
02389+ [CN= 80.0; N= 3.00; Tpm=.72]
02390+
02391+ # EXT34
02392+ R0150:CO0036-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02393+ CALIB NASHYD 1.0 01:EXT34 .83 .068 No_date 12:19 52.94 .589 .000
02394+ [CN= 80.0; N= 3.00; Tpm=.72]
02395+
02396+ # EXT35
02397+ R0150:CO0037-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02398+ CALIB NASHYD 1.0 01:EXT35 .83 .068 No_date 12:19 52.94 .589 .000
02399+ [CN= 80.0; N= 3.00; Tpm=.72]
02400+
02401+ # EXT36
02402+ R0150:CO0038-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02403+ CALIB NASHYD 1.0 01:EXT36 .83 .068 No_date 12:19 52.94 .589 .000
02404+ [CN= 80.0; N= 3.00; Tpm=.72]
02405+
02406+ # EXT37
02407+ R0150:CO0039-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02408+ CALIB NASHYD 1.0 01:EXT37 .83 .068 No_date 12:19 52.94 .589 .000
02409+ [CN= 80.0; N= 3.00; Tpm=.72]
02410+
02411+ # EXT38
02412+ R0150:CO0040-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02413+ CALIB NASHYD 1.0 01:EXT38 .83 .068 No_date 12:19 52.94 .589 .000
02414+ [CN= 80.0; N= 3.00; Tpm=.72]
02415+
02416+ # EXT39
02417+ R0150:CO0041-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02418+ CALIB NASHYD 1.0 01:EXT39 .83 .068 No_date 12:19 52.94 .589 .000
02419+ [CN= 80.0; N= 3.00; Tpm=.72]
02420+
02421+ # EXT40
02422+ R0150:CO0042-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02423+ CALIB NASHYD 1.0 01:EXT40 .83 .068 No_date 12:19 52.94 .589 .000
02424+ [CN= 80.0; N= 3.00; Tpm=.72]
02425+
02426+ # EXT41
02427+ R0150:CO0043-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02428+ CALIB NASHYD 1.0 01:EXT41 .83 .068 No_date 12:19 52.94 .589 .000
02429+ [CN= 80.0; N= 3.00; Tpm=.72]
02430+
02431+ # EXT42
02432+ R0150:CO0044-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02433+ CALIB NASHYD 1.0 01:EXT42 .83 .068 No_date 12:19 52.94 .589 .000
02434+ [CN= 80.0; N= 3.00; Tpm=.72]
02435+
02436+ # EXT43
02437+ R0150:CO0045-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02438+ CALIB NASHYD 1.0 01:EXT43 .83 .068 No_date 12:19 52.94 .589 .000
02439+ [CN= 80.0; N= 3.00; Tpm=.72]
02440+
02441+ # EXT44
02442+ R0150:CO0046-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02443+ CALIB NASHYD 1.0 01:EXT44 .83 .068 No_date 12:19 52.94 .589 .000
02444+ [CN= 80.0; N= 3.00; Tpm=.72]
02445+
02446+ # EXT45
02447+ R0150:CO0047-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02448+ CALIB NASHYD 1.0 01:EXT45 .83 .068 No_date 12:19 52.94 .589 .000
02449+ [CN= 80.0; N= 3.00; Tpm=.72]
02450+
02451+ # EXT46
02452+ R0150:CO0048-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02453+ CALIB NASHYD 1.0 01:EXT46 .83 .068 No_date 12:19 52.94 .589 .000
02454+ [CN= 80.0; N= 3.00; Tpm=.72]
02455+
02456+ # EXT47
02457+ R0150:CO0049-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02458+ CALIB NASHYD 1.0 01:EXT47 .83 .068 No_date 12:19 52.94 .589 .000
02459+ [CN= 80.0; N= 3.00; Tpm=.72]
02460+
02461+ # EXT48
02462+ R0150:CO0050-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02463+ CALIB NASHYD 1.0 01:EXT48 .83 .068 No_date 12:19 52.94 .589 .000
02464+ [CN= 80.0; N= 3.00; Tpm=.72]
02465+
02466+ # EXT49
02467+ R0150:CO0051-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02468+ CALIB NASHYD 1.0 01:EXT49 .83 .068 No_date 12:19 52.94 .589 .000
02469+ [CN= 80.0; N= 3.00; Tpm=.72]
02470+
02471+ # EXT50
02472+ R0150:CO0052-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02473+ CALIB NASHYD 1.0 01:EXT50 .83 .068 No_date 12:19 52.94 .589 .000
02474+ [CN= 80.0; N= 3.00; Tpm=.72]
02475+
02476+ # EXT51
02477+ R0150:CO0053-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02478+ CALIB NASHYD 1.0 01:EXT51 .83 .068 No_date 12:19 52.94 .589 .000
02479+ [CN= 80.0; N= 3.00; Tpm=.72]
02480+
02481+ # EXT52
02482+ R0150:CO0054-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02483+ CALIB NASHYD 1.0 01:EXT52 .83 .068 No_date 12:19 52.94 .589 .000
02484+ [CN= 80.0; N= 3.00; Tpm=.72]
02485+
02486+ # EXT53
02487+ R0150:CO0055-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02488+ CALIB NASHYD 1.0 01:EXT53 .83 .068 No_date 12:19 52.94 .589 .000
02489+ [CN= 80.0; N= 3.00; Tpm=.72]
02490+
02491+ # EXT54
02492+ R0150:CO0056-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02493+ CALIB NASHYD 1.0 01:EXT54 .83 .068 No_date 12:19 52.94 .589 .000
02494+ [CN= 80.0; N= 3.00; Tpm=.72]
02495+
02496+ # EXT55
02497+ R0150:CO0057-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02498+ CALIB NASHYD 1.0 01:EXT55 .83 .068 No_date 12:19 52.94 .589 .000
02499+ [CN= 80.0; N= 3.00; Tpm=.72]
02500+
02501+ # EXT56
02502+ R0150:CO0058-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02503+ CALIB NASHYD 1.0 01:EXT56 .83 .068 No_date 12:19 52.94 .589 .000
02504+ [CN= 80.0; N= 3.00; Tpm=.72]
02505+
02506+ # EXT57
02507+ R0150:CO0059-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02508+ CALIB NASHYD 1.0 01:EXT57 .83 .068 No_date 12:19 52.94 .589 .000
02509+ [CN= 80.0; N= 3.00; Tpm=.72]
02510+
02511+ # EXT58
02512+ R0150:CO0060-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02513+ CALIB NASHYD 1.0 01:EXT58 .83 .068 No_date 12:19 52.94 .589 .000
02514+ [CN= 80.0; N= 3.00; Tpm=.72]
02515+
02516+ # EXT59
02517+ R0150:CO0061-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02518+ CALIB NASHYD 1.0 01:EXT59 .83 .068 No_date 12:19 52.94 .589 .000
02519+ [CN= 80.0; N= 3.00; Tpm=.72]
02520+
02521+ # EXT60
02522+ R0150:CO0062-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02523+ CALIB NASHYD 1.0 01:EXT60 .83 .068 No_date 12:19 52.94 .589 .000
02524+ [CN= 80.0; N= 3.00; Tpm=.72]
02525+
02526+ # EXT61
02527+ R0150:CO0063-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02528+ CALIB NASHYD 1.0 01:EXT61 .83 .068 No_date 12:19 52.94 .589 .000
02529+ [CN= 80.0; N= 3.00; Tpm=.72]
02530+
02531+ # EXT62
02532+ R0150:CO0064-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02533+ CALIB NASHYD 1.0 01:EXT62 .83 .068 No_date 12:19 52.94 .589 .000
02534+ [CN= 80.0; N= 3.00; Tpm=.72]
02535+
02536+ # EXT63
02537+ R0150:CO0065-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02538+ CALIB NASHYD 1.0 01:EXT63 .83 .068 No_date 12:19 52.94 .589 .000
02539+ [CN= 80.0; N= 3.00; Tpm=.72]
02540+
02541+ # EXT64
02542+ R0150:CO0066-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02543+ CALIB NASHYD 1.0 01:EXT64 .83 .068 No_date 12:19 52.94 .589 .000
02544+ [CN= 80.0; N= 3.00; Tpm=.72]
02545+
02546+ # EXT65
02547+ R0150:CO0067-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02548+ CALIB NASHYD 1.0 01:EXT65 .83 .068 No_date 12:19 52.94 .589 .000
02549+ [CN= 80.0; N= 3.00; Tpm=.72]
02550+
02551+ # EXT66
02552+ R0150:CO0068-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02553+ CALIB NASHYD 1.0 01:EXT66 .83 .068 No_date 12:19 52.94 .589 .000
02554+ [CN= 80.0; N= 3.00; Tpm=.72]
02555+
02556+ # EXT67
02557+ R0150:CO0069-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02558+ CALIB NASHYD 1.0 01:EXT67 .83 .068 No_date 12:19 52.94 .589 .000
02559+ [CN= 80.0; N= 3.00; Tpm=.72]
02560+
02561+ # EXT68
02562+ R0150:CO0070-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02563+ CALIB NASHYD 1.0 01:EXT68 .83 .068 No_date 12:19 52.94 .589 .000
02564+ [CN= 80.0; N= 3.00; Tpm=.72]
02565+
02566+ # EXT69
02567+ R0150:CO0071-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02568+ CALIB NASHYD 1.0 01:EXT69 .83 .068 No_date 12:19 52.94 .589 .000
02569+ [CN= 80.0; N= 3.00; Tpm=.72]
02570+
02571+ # EXT70
02572+ R0150:CO0072-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02573+ CALIB NASHYD 1.0 01:EXT70 .83 .068 No_date 12:19 52.94 .589 .000
02574+ [CN= 80.0; N= 3.00; Tpm=.72]
02575+
02576+ # EXT71
02577+ R0150:CO0073-----Dtn-ID:INVD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
02578+ CALIB NASHYD 1.0 01:EXT71 .83 .068 No_date 12:19 52.94 .589 .000
02579+ [CN= 80.0; N= 3.00; Tpm=.72]
02580+
02581+ # EXT72
02
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025211 *****
025212 # Pre11-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025223 *****
025224 R1979:C0017-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025225 CALIB NASHYD 1.0 01:Pre11 .07 .010 No_date 12:06 59.96 .462 .000
025226 [CN= 78.0; N= 3.00; Tpe= .21]
025227 *****
025228 R1979:C0018-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025229 ADD HYD + 1.0 02:EXT2 .28 .037 No_date 12:13 70.91 n/a .000
025230 + 1.0 02:EXT1 3.21 .012 No_date 12:12 82.92 n/a .000
025231 SUM= 1.0 01:EXT .85 .084 No_date 12:17 63.63 n/a .000
025232 R1979:C0019-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025233 ROUTE CHANNEL -> 1.0 01:EXT1 .85 .084 No_date 12:17 63.63 n/a .000
025234 [RDT= 1.00] out<- 1.0 01:EXT1 .85 .081 No_date 12:22 63.63 n/a .000
025235 [L/S/n= 143./ .394/.035]
025236 (Vmax= .404;Dmax= .181)
025237 R1979:C0020-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025238 ADD HYD + 1.0 02:EXT1 .85 .081 No_date 12:22 63.63 n/a .000
025239 + 1.0 02:EXT3 .56 .066 No_date 12:13 62.92 n/a .000
025240 SUM= 1.0 01:EXT3 3.21 .012 No_date 12:12 82.92 n/a .000
025241 R1979:C0021-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025242 ROUTE CHANNEL -> 1.0 01:EXT2 4.62 .329 No_date 12:27 63.05 n/a .000
025243 + 1.0 01:EXT3 4.93 .352 No_date 12:27 62.95 n/a .000
025244 ROUTE CHANNEL -> 1.0 02:EXT2 4.62 .329 No_date 12:27 63.05 n/a .000
025245 [RDT= 1.00] out<- 1.0 01:EXT2 4.62 .329 No_date 12:29 63.05 n/a .000
025246 [L/S/n= 143./ .425/.035]
025247 (Vmax= .561;Dmax= .131)
025248 R1979:C0022-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025249 ADD HYD + 1.0 02:EXT2 4.62 .329 No_date 12:29 63.05 n/a .000
025250 + 1.0 02:EXT4 .31 .038 No_date 12:11 61.42 n/a .000
025251 SUM= 1.0 01:EXT3 4.93 .352 No_date 12:27 62.95 n/a .000
025252 R1979:C0023-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025253 ROUTE CHANNEL -> 1.0 01:EXT2 4.93 .354 No_date 12:27 62.95 n/a .000
025254 [RDT= 1.00] out<- 1.0 01:EXT3 4.93 .352 No_date 12:30 62.95 n/a .000
025255 [L/S/n= 92./ .274/.035]
025256 (Vmax= .459;Dmax= .121)
025257 R1979:C0024-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025258 ADD HYD + 1.0 02:EXT3 .59 .049 No_date 12:21 57.15 n/a .000
025259 + 1.0 02:EXT5 .52 .399 No_date 12:28 62.32 n/a .000
025260 SUM= 1.0 01:EXT4 4.93 .399 No_date 12:28 62.32 n/a .000
025261 R1979:C0025-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025262 ROUTE CHANNEL -> 1.0 01:EXT4 5.52 .399 No_date 12:28 62.32 n/a .000
025263 [RDT= 1.00] out<- 1.0 01:EXT4 5.52 .379 No_date 12:37 62.32 n/a .000
025264 [L/S/n= 251./ .190/.035]
025265 (Vmax= .456;Dmax= .172)
025266 R1979:C0026-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025267 ADD HYD + 1.0 02:EXT4 5.52 .379 No_date 12:37 62.32 n/a .000
025268 + 1.0 02:EXT6 .47 .060 No_date 12:12 67.60 n/a .000
025269 SUM= 1.0 01:EXT5 6.86 .491 No_date 12:33 63.77 n/a .000
025270 R1979:C0027-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025271 ROUTE CHANNEL -> 1.0 01:EXT5 6.86 .491 No_date 12:33 63.77 n/a .000
025272 [RDT= 1.00] out<- 1.0 01:EXT5 6.86 .485 No_date 12:38 63.77 n/a .000
025273 [L/S/n= 237./ .644/.035]
025274 (Vmax= .744;Dmax= .140)
025275 R1979:C0028-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025276 ROUTE CHANNEL -> 1.0 01:Pre10 .80 .080 No_date 12:11 50.61 n/a .000
025277 [RDT= 1.00] out<- 1.0 01:Pre10 .80 .078 No_date 12:14 50.61 n/a .000
025278 [L/S/n= 77./ .776/.035]
025279 (Vmax= .492;Dmax= .058)
025280 R1979:C0029-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025281 ROUTE CHANNEL -> 1.0 01:Pre9 .83 .047 No_date 12:35 50.61 n/a .000
025282 [RDT= 1.00] out<- 1.0 01:Pre7 .83 .047 No_date 12:38 50.61 n/a .000
025283 [L/S/n= 159./ .1576/.035]
025284 (Vmax= .797;Dmax= .014)
025285 R1979:C0030-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025286 ADD HYD + 1.0 02:EXT6 .80 .078 No_date 12:14 50.69 n/a .000
025287 + 1.0 02:EXT10 2.0 .016 No_date 12:19 50.61 n/a .000
025288 SUM= 1.0 01:EXT6 1.01 .093 No_date 12:14 50.67 n/a .000
025289 R1979:C0031-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025290 ROUTE CHANNEL -> 1.0 01:EXT6 1.01 .093 No_date 12:14 50.67 n/a .000
025291 [RDT= 1.00] out<- 1.0 01:EXT8 1.01 .091 No_date 12:18 50.67 n/a .000
025292 [L/S/n= 79./ .522/.035]
025293 (Vmax= .423;Dmax= .068)
025294 R1979:C0032-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025295 ADD HYD + 1.0 02:EXT8 1.83 .047 No_date 12:38 50.63 n/a .000
025296 + 1.0 02:EXT7 1.83 .129 No_date 12:22 50.65 n/a .000
025297 SUM= 1.0 01:EXT7 1.83 .129 No_date 12:21 50.65 n/a .000
025298 R1979:C0033-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025299 ROUTE CHANNEL -> 1.0 01:EXT7 1.83 .129 No_date 12:21 50.65 n/a .000
025300 [RDT= 1.00] out<- 1.0 01:EXT7 1.83 .129 No_date 12:22 50.65 n/a .000
025301 [L/S/n= 29./ .887/.035]
025302 (Vmax= .543;Dmax= .089)
025303 R1979:C0034-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025304 ADD HYD + 1.0 02:EXT9 3.57 .284 No_date 12:23 57.15 n/a .000
025305 + 1.0 02:EXT8 1.83 .129 No_date 12:22 50.66 n/a .000
025306 SUM= 1.0 02:EXT8 6.83 .079 No_date 12:19 61.43 n/a .000
025307 + 1.0 02:EXT9 6.86 .485 No_date 12:38 63.77 n/a .000
025308 SUM= 1.0 01:EXT8 13.10 .939 No_date 12:30 59.98 n/a .000
025309 R1979:C0035-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025310 ROUTE PIPE -> 1.0 01:Outlet 13.10 .939 No_date 12:30 59.98 n/a .000
025311 [RDT= 1.00] out<- 1.0 01:Outlet 13.10 .937 No_date 12:31 59.98 n/a .000
025312 [L/S/n= 101./ .101/.035]
025313 (Vmax= .489;Dmax= .1369)
025314 [Dln= .553;Dused= 1.67]
025315 *****
025316 ** STORMS *****
025317 *****
025318 ** END OF RUN : 1978 *****
025319 *****
025320 *****
025321 *****
025322 *****
025323 *****
025324 # SWHINDO / INPUT DATA FILE
025325 *****
025326 # Project Name : [5923 Ottawa St]
025327 # Project Number : [27131001]
025328 # Date : [2025 FEB 05]
025329 # Modeler : [JFS]
025330 # Company : JFSA Canada Inc.
025331 # License # : 2549237
025332 *****
025333 # Model developed to simulate runoff from subcatchments under pre development conditions
025334 *****
025335 R1979:C0002-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025336 READ STORM
025337 FileNm= STORM.001
025338 Comment = July 1st, 1979 Storm (3H) - Ottawa International Airport step 5 min
025339 [DRT= 5.00;DUSE= 3.00;PROT= 83.99]
025340 *****
025341 # EXT1 *****
025342 *****
025343 R1979:C0003-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025344 CALIB NASHYD 1.0 01:EXT1 3.21 .240 No_date 2:16 44.05 .524 .000
025345 [CN= 80.0; N= 3.00; Tpe= .33]
025346 *****
025347 # EXT2 *****
025348 *****
025349 R1979:C0004-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025350 CALIB NASHYD 1.0 01:EXT2 .28 .039 No_date 1:50 50.68 .403 .000
025351 [CN= 80.0; N= 3.00; Tpe= .33]
025352 *****
025353 # EXT3 *****
025354 *****
025355 R1979:C0005-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025356 CALIB NASHYD 1.0 01:EXT3 .56 .067 No_date 1:50 44.05 .524 .000
025357 [CN= 80.0; N= 3.00; Tpe= .33]
025358 *****
025359 # EXT4 *****
025360 *****
025361 R1979:C0006-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025362 CALIB NASHYD 1.0 01:EXT4 .31 .038 No_date 1:48 42.84 .510 .000
025363 [CN= 79.0; N= 3.00; Tpe= .29]
025364 *****
025365 # EXT5 *****
025366 *****
025367 R1979:C0007-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025368 CALIB NASHYD 1.0 01:EXT5 .59 .054 No_date 2:01 39.44 .470 .000
025369 [CN= 76.0; N= 3.00; Tpe= .45]
025370 *****
025371 R1979:C0008-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025372 CALIB NASHYD 1.0 01:EXT6 .86 .088 No_date 2:06 50.68 .603 .000
025373 [CN= 80.0; N= 3.00; Tpe= .33]
025374 *****
025375 # EXT6 *****
025376 *****
025377 R1979:C0009-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025378 CALIB NASHYD 1.0 01:EXT6 .83 .085 No_date 1:58 42.85 .510 .000
025379 [CN= 79.0; N= 3.00; Tpe= .29]
025380 *****
025381 # EXT7 *****
025382 *****
025383 R1979:C0010-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025384 CALIB NASHYD 1.0 01:EXT7 .56 .061 No_date 2:11 41.34 .513 .000
025385 [CN= 80.0; N= 3.00; Tpe= .32]
025386 *****
025387 # EXT8 *****
025388 *****
025389 R1979:C0011-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025390 CALIB NASHYD 1.0 01:EXT8 .83 .085 No_date 1:58 42.85 .510 .000
025391 [CN= 79.0; N= 3.00; Tpe= .29]
025392 *****
025393 # EXT9 *****
025394 *****
025395 R1979:C0012-----DtnIn-ID-INHYD-----AREAhA-QFEARcMs-TpeakDate_hh:mm-----RvM-R.C-----DWfCms
025396 CALIB NASHYD 1.0 01:EXT9 .56 .061 No_date 2:11 41.34 .513 .000
025397 [CN= 80.0; N= 3.00; Tpe= .32]
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JFSAinc

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03241) (Vmax=.543:Dmax=.056)-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03242) R1996:CO0010-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03243) ADD HYD + 1.0 02:EXT9 3.57 .177 No_date 3:36 32.07 n/a .000
03244) + 1.0 02:R9 1.83 .082 No_date 3:35 27.76 n/a .000
03245) + 1.0 02:EXT8 .83 .049 No_date 3:32 35.05 n/a .000
03246) + 1.0 02:R5 6.86 .302 No_date 3:50 36.76 n/a .000
03247) SUM= 13.10 .186 No_date 3:41 34.11 n/a .000
03248) R1996:CO0035-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03249) ROUTE PIPE -> 1.0 02:P8 13.10 .586 No_date 3:41 34.11 n/a .000
03250) + [RDT=1.00] out<- 13.10 .586 No_date 3:42 34.11 n/a .000
03251) [L/S/n= 8./ .010/.033]
03252) (Vmax=.493:Dmax=)-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03253) (Dln=.53:Dused=1.40)
03254) #####
03255) # STORMS
03256) #####
03257) *** END OF RUN : 1996
03258) #####
03259) #####
03260) #####
03261) #####
03262) #####
03263) #####
03264) #####
03265) RUN#:CONMAN#
03266) R9999:CO0001-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03267) START
03268) [TZERO = .00 hrs on 0]
03269) [MOUTP= 2 (1=imperial, 2=metric output)]
03270) [METFORM= 1]
03271) [NRUN = 9999]
03272) #####
03273) # SWHYHYD / INPUT DATA FILE
03274) #####
03275) # Project Name : [5923 Ottawa St]
03276) # Project Number: [P2710(e01)]
03277) # Date : [2025 FEB 05]
03278) # Modeller : [NM]
03279) # Company : JFSA Canada Inc.
03280) # License # : 254927
03281) #####
03282) # Model developed to simulate runoff from subcatchments under pre development conditions
03283) #####
03284) R9999:CO0002-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03285) HEAD STORM
03286) Filename = STORM.001
03287) Comment = CHICAGO STORM 100 Year, 3 Hours +20k Stress Test
03288) [SDT=10.0:SDUR= 3.00:PTOT= 86.00]
03289) #####
03290) # EXT1
03291) #####
03292) R9999:CO0003-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03293) CALIB NASHYD 1.0 01:EXT1 3.21 .224 No_date 1:51 45.67 .531 .000
03294) [Cm= 80.0: N= 3.00: Tpe=.72]
03295) #####
03296) # EXT2
03297) #####
03298) R9999:CO0004-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03299) CALIB NASHYD 1.0 01:EXT2 .28 .041 No_date 1:21 52.43 .610 .000
03300) [Cm= 83.0: N= 3.00: Tpe=.33]
03301) #####
03302) # EXT3
03303) #####
03304) R9999:CO0005-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03305) CALIB NASHYD 1.0 01:EXT3 .86 .070 No_date 1:21 45.67 .531 .000
03306) [Cm= 80.0: N= 3.00: Tpe=.32]
03307) #####
03308) # EXT4
03309) #####
03310) R9999:CO0006-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03311) CALIB NASHYD 1.0 01:EXT4 .31 .040 No_date 1:19 44.44 .517 .000
03312) [Cm= 79.0: N= 3.00: Tpe=.29]
03313) #####
03314) # EXT5
03315) #####
03316) R9999:CO0007-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03317) CALIB NASHYD 1.0 01:EXT5 .59 .052 No_date 1:31 40.94 .476 .000
03318) [Cm= 76.0: N= 3.00: Tpe=.45]
03319) #####
03320) # EXT6
03321) #####
03322) R9999:CO0008-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03323) CALIB NASHYD 1.0 01:EXT6 .86 .085 No_date 1:38 52.43 .610 .000
03324) [Cm= 85.0: N= 3.00: Tpe=.56]
03325) #####
03326) # EXT7
03327) #####
03328) R9999:CO0009-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03329) CALIB NASHYD 1.0 01:EXT7 .47 .064 No_date 1:21 49.60 .577 .000
03330) [Cm= 83.0: N= 3.00: Tpe=.29]
03331) #####
03332) # EXT8
03333) #####
03334) R9999:CO0010-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03335) CALIB NASHYD 1.0 01:EXT8 .83 .083 No_date 1:29 44.44 .517 .000
03336) [Cm= 79.0: N= 3.00: Tpe=.42]
03337) #####
03338) # EXT9
03339) #####
03340) R9999:CO0011-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03341) CALIB NASHYD 1.0 01:EXT9 3.57 .297 No_date 1:34 40.95 .476 .000
03342) [Cm= 76.0: N= 3.00: Tpe=.48]
03343) #####
03344) # EXT9a
03345) #####
03346) R9999:CO0012-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03347) CALIB NASHYD 1.0 01:EXT9a 4.01 .004 No_date 1:00 43.23 .503 .000
03348) [Cm= 78.0: N= 3.00: Tpe=.04]
03349) #####
03350) # EXT10
03351) #####
03352) R9999:CO0013-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03353) CALIB NASHYD 1.0 01:EXT10 .20 .016 No_date 1:29 35.74 .416 .000
03354) [Cm= 71.0: N= 3.00: Tpe=.42]
03355) #####
03356) # Pre2
03357) #####
03358) R9999:CO0014-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03359) CALIB NASHYD 1.0 01:Pre2 .57 .051 No_date 1:32 43.24 .503 .000
03360) [Cm= 78.0: N= 3.00: Tpe=.29]
03361) #####
03362) # Pre0
03363) #####
03364) R9999:CO0015-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03365) CALIB NASHYD 1.0 01:Pre0 .83 .048 No_date 1:47 35.74 .416 .000
03366) [Cm= 71.0: N= 3.00: Tpe=.44]
03367) #####
03368) # Pre10
03369) #####
03370) R9999:CO0016-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03371) CALIB NASHYD 1.0 01:Pre10 .80 .081 No_date 1:19 35.74 .416 .000
03372) [Cm= 71.0: N= 3.00: Tpe=.21]
03373) #####
03374) # Pre11
03375) #####
03376) R9999:CO0017-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03377) CALIB NASHYD 1.0 01:Pre11 .07 .011 No_date 1:13 43.23 .503 .000
03378) [Cm= 78.0: N= 3.00: Tpe=.21]
03379) #####
03380) R9999:CO0018-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03381) ADD HYD + 1.0 02:EXT2 .28 .041 No_date 1:21 52.43 .610 .000
03382) + 1.0 02:Pre2 .57 .051 No_date 1:32 43.24 n/a .000
03383) SUM= 1.0 01:P1 .85 .090 No_date 1:26 46.32 n/a .000
03384) R9999:CO0019-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03385) ROUTE CHANNEL -> 1.0 02:P1 .85 .090 No_date 1:26 46.32 n/a .000
03386) [RDT=1.00] out<- 1.0 01:P1 .85 .087 No_date 1:32 46.32 n/a .000
03387) [L/S/n= 143./ .394/.035]
03388) (Vmax=.410:Dmax=.185)
03389) #####
03390) R9999:CO0020-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03391) ADD HYD + 1.0 02:P1 .85 .087 No_date 1:32 46.32 n/a .000
03392) + 1.0 02:EXT3 .56 .070 No_date 1:21 45.67 n/a .000
03393) + 1.0 02:EXT8 3.21 .224 No_date 1:51 45.67 n/a .000
03394) SUM= 1.0 01:P2 4.62 .346 No_date 1:39 45.79 n/a .000
03395) R9999:CO0021-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03396) ROUTE CHANNEL -> 1.0 02:P2 4.62 .346 No_date 1:39 45.79 n/a .000
03397) [RDT=1.00] out<- 1.0 01:P2 4.62 .346 No_date 1:40 45.79 n/a .000
03398) [L/S/n= 71./ .423/.035]
03399) (Vmax=.568:Dmax=.320)
03400) #####
03401) R9999:CO0022-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03402) ADD HYD + 1.0 02:P2 4.62 .346 No_date 1:40 45.79 n/a .000
03403) + 1.0 02:EXT4 .31 .040 No_date 1:19 44.44 n/a .000
03404) SUM= 1.0 01:P3 4.93 .372 No_date 1:38 45.70 n/a .000
03405) R9999:CO0023-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03406) ROUTE CHANNEL -> 1.0 02:P3 4.93 .372 No_date 1:38 45.70 n/a .000
03407) [RDT=1.00] out<- 1.0 01:P3 4.93 .369 No_date 1:40 45.70 n/a .000
03408) [L/S/n= 92./ .274/.035]
03409) (Vmax=.463:Dmax=.320)
03410) #####
03411) R9999:CO0024-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03412) ADD HYD + 1.0 02:P3 4.93 .369 No_date 1:40 45.70 n/a .000
03413) + 1.0 02:EXT8 .59 .052 No_date 1:31 40.94 n/a .000
03414) SUM= 1.0 01:P4 5.52 .419 No_date 1:39 45.19 n/a .000
03415) R9999:CO0025-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03416) ROUTE CHANNEL -> 1.0 02:P4 5.52 .419 No_date 1:39 45.19 n/a .000
03417) [RDT=1.00] out<- 1.0 01:P4 5.52 .399 No_date 1:48 45.19 n/a .000
03418) [L/S/n= 251./ .190/.035]
03419) (Vmax=.463:Dmax=.380)
03420) #####
03421) R9999:CO0026-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03422) ADD HYD + 1.0 02:P4 5.52 .399 No_date 1:48 45.19 n/a .000
03423) + 1.0 02:EXT7 .47 .064 No_date 1:21 49.60 n/a .000
03424) SUM= 1.0 01:P5 6.86 .519 No_date 1:44 46.41 n/a .000
03425) [L/S/n= 237./ .544/.035]
03426) (Vmax=.757:Dmax=.348)
03427) R9999:CO0028-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03428) ROUTE CHANNEL -> 1.0 02:Pre10 .80 .080 No_date 1:19 35.74 n/a .000
03429) [RDT=1.00] out<- 1.0 01:Pre10 .80 .080 No_date 1:22 35.74 n/a .000
03430) [L/S/n= 71./ .776/.035]
03431) (Vmax=.492:Dmax=.059)
03432) R9999:CO0029-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03433) ROUTE CHANNEL -> 1.0 02:Pre9 .83 .048 No_date 1:47 35.74 n/a .000
03434) [RDT=1.00] out<- 1.0 01:Pre7 .83 .048 No_date 1:50 35.74 n/a .000
03435) [L/S/n= 159./ .576/.035]
03436) (Vmax=.797:Dmax=.014)
03437) R9999:CO0030-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03438) ADD HYD + 1.0 02:P6 .80 .080 No_date 1:22 36.02 n/a .000
03439) + 1.0 02:EXT10 .20 .016 No_date 1:29 35.74 n/a .000
03440) SUM= 1.0 01:P6 1.83 .048 No_date 1:29 35.96 n/a .000
03441) R9999:CO0031-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03442) ROUTE CHANNEL -> 1.0 02:P6 1.01 .095 No_date 1:22 35.96 n/a .000
03443) [RDT=1.00] out<- 1.0 01:P8 1.01 .093 No_date 1:26 35.96 n/a .000
03444) [L/S/n= 79./ .522/.035]
03445) (Vmax=.423:Dmax=.070)
03446) R9999:CO0032-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03447) ADD HYD + 1.0 02:P8 1.01 .093 No_date 1:26 35.96 n/a .000
03448) + 1.0 02:P7 .83 .048 No_date 1:50 35.77 n/a .000
03449) SUM= 1.0 01:P7 1.83 .131 No_date 1:31 35.88 n/a .000
03450) R9999:CO0033-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03451) ROUTE CHANNEL -> 1.0 02:P7 1.83 .131 No_date 1:31 35.88 n/a .000
03452) [RDT=1.00] out<- 1.0 01:P9 1.83 .131 No_date 1:32 35.88 n/a .000
03453) [L/S/n= 29./ .887/.035]
03454) (Vmax=.543:Dmax=.089)
03455) R9999:CO0034-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03456) ADD HYD + 1.0 02:EXT9 3.57 .297 No_date 1:34 40.95 n/a .000
03457) + 1.0 02:P9 1.83 .131 No_date 1:32 35.89 n/a .000
03458) + 1.0 02:EXT8 .83 .083 No_date 1:29 44.44 n/a .000
03459) SUM= 1.0 02:P5 6.86 .513 No_date 1:49 46.41 n/a .000
03460) 13.10 .186 No_date 3:41 34.11 n/a .000
03461) R9999:CO0035-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03462) ROUTE PIPE -> 1.0 02:P8 13.10 .586 No_date 3:41 34.11 n/a .000
03463) + [RDT=1.00] out<- 1.0 01:Outlet 13.10 .583 No_date 3:42 34.32 n/a .000
03464) [L/S/n= 8./ .010/.033]
03465) (Vmax=.493:Dmax=1.394)
03466) (Dln=.53:Dused=1.70)
03467) #####
03468) # STORMS
03469) #####
03470) R9999:CO0002-----Dtlm-ID-INHYD-----AREAh-QFEARcs-TpeakDate_hh:mm-----Rvnm-R.C.---DWfms
03471) FINISH
03472) #####
03473) #####
03474) WARNINGS / ERRORS / NOTES
03475) #####
03476) R0002:CO0035 ROUTE PIPE ->
03477) *** WARNING: New pipe size used for routing.
03478) *** WARNING: New pipe size used for routing.
03479) *** WARNING: New pipe size used for routing.
03480) *** WARNING: New pipe size used for routing.
03481) *** WARNING: New pipe size used for routing.
03482) *** WARNING: New pipe size used for routing.
03483) *** WARNING: New pipe size used for routing.
03484) *** WARNING: New pipe size used for routing.
03485) *** WARNING: New pipe size used for routing.
03486) *** WARNING: New pipe size used for routing.
03487) *** WARNING: New pipe size used for routing.
03488) *** WARNING: New pipe size used for routing.
03489) *** WARNING: New pipe size used for routing.
03490) *** WARNING: New pipe size used for routing.
03491) *** WARNING: New pipe size used for routing.
03492) *** WARNING: New pipe size used for routing.
03493) Simulation ended on 2025-09-10 at 20:42:50
03494) #####
```

Attachment B

Post-Development Hydrology



Legend

Post-development Subcatchments

Site Plan

EXT1
3.212 ha Subcatchment Name
Subcatchment Area (ha)

SCALE: 1:3000

0 50 100 150 m



5923 Ottawa St – Richmond

Figure B1: Proposed Drainage Areas

| | |
|---------|------------|
| PROJECT | P2710(e01) |
| DRAWN | MM |
| DATE | 04-06-2025 |

Table B1 - Site 1 - Stage/Storage/Outflow Curves

| | | | | | Quality Control 1 | | Overflow | | | |
|---------------|-----------------------------|-----------------------------|--------------------------------|--------------------|------------------------|-----------------------------|--------------------|-----------------------------|-----------------------------|----------------|
| | | | | | Vertical Orifice | | Broad Crested Weir | | | |
| | | | | | Dia (m) | 0.075 | L (m) | 0.300 | | |
| | | | | | Area (m ²) | 0.006 | C _w | 1.580 | | |
| | | | | | Invert (m) | 93.84 | | | | |
| | | | | | C _v | 0.61 | C _w | Invert (m) | 94.40 | Total |
| | | | | | Q @ D | 0.002 | n contr. | 2 | | |
| Elevation (m) | Storage 1 (m ³) | Storage 2 (m ³) | Total Volume (m ³) | Demarcation Points | Depth (m) | Outflow (m ³ /s) | Depth (m) | Outflow (m ³ /s) | Outflow (m ³ /s) | Storage (ha-m) |
| 93.84 | | 0.0 | 0.0 | Pond Bottom | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 93.85 | | 0.0 | 0.0 | | 0.010 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 93.86 | | 0.0 | 0.0 | | 0.020 | 0.001 | 0.000 | 0.000 | 0.001 | 0.000 |
| 93.87 | | 0.2 | 0.2 | | 0.030 | 0.001 | 0.000 | 0.000 | 0.001 | 0.000 |
| 93.88 | | 0.3 | 0.3 | | 0.040 | 0.001 | 0.000 | 0.000 | 0.001 | 0.000 |
| 93.89 | | 0.6 | 0.6 | | 0.050 | 0.002 | 0.000 | 0.000 | 0.002 | 0.000 |
| 93.90 | | 0.9 | 0.9 | | 0.060 | 0.002 | 0.000 | 0.000 | 0.002 | 0.000 |
| 93.91 | | 1.4 | 1.4 | | 0.070 | 0.002 | 0.000 | 0.000 | 0.002 | 0.000 |
| 93.92 | | 1.9 | 1.9 | | 0.080 | 0.002 | 0.000 | 0.000 | 0.002 | 0.000 |
| 93.93 | | 2.5 | 2.5 | | 0.090 | 0.003 | 0.000 | 0.000 | 0.003 | 0.000 |
| 93.94 | | 3.2 | 3.2 | | 0.100 | 0.003 | 0.000 | 0.000 | 0.003 | 0.000 |
| 93.95 | | 4.0 | 4.0 | | 0.110 | 0.003 | 0.000 | 0.000 | 0.003 | 0.000 |
| 93.96 | | 4.9 | 4.9 | | 0.120 | 0.003 | 0.000 | 0.000 | 0.003 | 0.000 |
| 93.97 | | 5.9 | 5.9 | | 0.130 | 0.004 | 0.000 | 0.000 | 0.004 | 0.001 |
| 93.98 | | 6.9 | 6.9 | | 0.140 | 0.004 | 0.000 | 0.000 | 0.004 | 0.001 |
| 93.99 | | 8.1 | 8.1 | | 0.150 | 0.004 | 0.000 | 0.000 | 0.004 | 0.001 |
| 94.00 | | 9.3 | 9.3 | | 0.160 | 0.004 | 0.000 | 0.000 | 0.004 | 0.001 |
| 94.01 | 0.00 | 10.6 | 10.6 | | 0.170 | 0.004 | 0.000 | 0.000 | 0.004 | 0.001 |
| 94.02 | 0.01 | 12.0 | 12.1 | | 0.180 | 0.005 | 0.000 | 0.000 | 0.005 | 0.001 |
| 94.03 | 0.05 | 13.6 | 13.6 | | 0.190 | 0.005 | 0.000 | 0.000 | 0.005 | 0.001 |
| 94.04 | 0.16 | 15.2 | 15.3 | | 0.200 | 0.005 | 0.000 | 0.000 | 0.005 | 0.002 |
| 94.05 | 0.39 | 16.9 | 17.2 | | 0.210 | 0.005 | 0.000 | 0.000 | 0.005 | 0.002 |
| 94.06 | 0.74 | 18.7 | 19.4 | | 0.220 | 0.005 | 0.000 | 0.000 | 0.005 | 0.002 |
| 94.07 | 1.20 | 20.5 | 21.7 | | 0.230 | 0.005 | 0.000 | 0.000 | 0.005 | 0.002 |
| 94.08 | 1.78 | 22.5 | 24.3 | | 0.240 | 0.005 | 0.000 | 0.000 | 0.005 | 0.002 |
| 94.09 | 2.46 | 24.6 | 27.1 | | 0.250 | 0.006 | 0.000 | 0.000 | 0.006 | 0.003 |
| 94.10 | 3.24 | 26.8 | 30.1 | | 0.260 | 0.006 | 0.000 | 0.000 | 0.006 | 0.003 |
| 94.11 | 4.12 | 29.1 | 33.2 | | 0.270 | 0.006 | 0.000 | 0.000 | 0.006 | 0.003 |
| 94.12 | 4.61 | 31.5 | 36.1 | | 0.280 | 0.006 | 0.000 | 0.000 | 0.006 | 0.004 |
| 94.13 | 5.63 | 34.0 | 39.7 | | 0.290 | 0.006 | 0.000 | 0.000 | 0.006 | 0.004 |
| 94.14 | 6.85 | 36.6 | 43.5 | | 0.300 | 0.006 | 0.000 | 0.000 | 0.006 | 0.004 |
| 94.15 | 8.19 | 39.3 | 47.5 | | 0.310 | 0.006 | 0.000 | 0.000 | 0.006 | 0.005 |
| 94.16 | 9.66 | 42.0 | 51.7 | | 0.320 | 0.006 | 0.000 | 0.000 | 0.006 | 0.005 |
| 94.17 | 11.17 | 44.8 | 56.0 | | 0.330 | 0.006 | 0.000 | 0.000 | 0.006 | 0.006 |
| 94.18 | 12.00 | 47.6 | 59.6 | | 0.340 | 0.007 | 0.000 | 0.000 | 0.007 | 0.006 |
| 94.19 | 13.82 | 50.5 | 64.3 | | 0.350 | 0.007 | 0.000 | 0.000 | 0.007 | 0.006 |
| 94.20 | 15.76 | 53.3 | 69.1 | | 0.360 | 0.007 | 0.000 | 0.000 | 0.007 | 0.007 |
| 94.21 | 17.78 | 56.3 | 74.0 | | 0.370 | 0.007 | 0.000 | 0.000 | 0.007 | 0.007 |
| 94.22 | 19.87 | 59.2 | 79.1 | | 0.380 | 0.007 | 0.000 | 0.000 | 0.007 | 0.008 |
| 94.23 | 22.01 | 62.2 | 84.2 | | 0.390 | 0.007 | 0.000 | 0.000 | 0.007 | 0.008 |
| 94.24 | 24.17 | 65.1 | 89.3 | | 0.400 | 0.007 | 0.000 | 0.000 | 0.007 | 0.009 |
| 94.25 | 26.36 | 68.2 | 94.5 | | 0.410 | 0.007 | 0.000 | 0.000 | 0.007 | 0.009 |
| 94.26 | 28.57 | 71.2 | 99.8 | | 0.420 | 0.007 | 0.000 | 0.000 | 0.007 | 0.010 |
| 94.27 | 30.81 | 74.3 | 105.1 | | 0.430 | 0.007 | 0.000 | 0.000 | 0.007 | 0.011 |
| 94.28 | 33.07 | 77.4 | 110.5 | | 0.440 | 0.008 | 0.000 | 0.000 | 0.008 | 0.011 |
| 94.29 | 35.35 | 80.5 | 115.9 | | 0.450 | 0.008 | 0.000 | 0.000 | 0.008 | 0.012 |
| 94.30 | 37.66 | 83.7 | 121.3 | | 0.460 | 0.008 | 0.000 | 0.000 | 0.008 | 0.012 |
| 94.31 | 39.99 | 86.9 | 126.9 | | 0.470 | 0.008 | 0.000 | 0.000 | 0.008 | 0.013 |
| 94.32 | 42.35 | 90.1 | 132.5 | | 0.480 | 0.008 | 0.000 | 0.000 | 0.008 | 0.013 |
| 94.33 | 44.74 | 93.4 | 138.1 | | 0.490 | 0.008 | 0.000 | 0.000 | 0.008 | 0.014 |
| 94.34 | 47.15 | 96.7 | 143.8 | | 0.500 | 0.008 | 0.000 | 0.000 | 0.008 | 0.014 |
| 94.35 | 49.58 | 100.0 | 149.6 | | 0.510 | 0.008 | 0.000 | 0.000 | 0.008 | 0.015 |
| 94.36 | 52.04 | 103.4 | 155.4 | | 0.520 | 0.008 | 0.000 | 0.000 | 0.008 | 0.016 |
| 94.37 | 54.52 | 106.8 | 161.3 | | 0.530 | 0.008 | 0.000 | 0.000 | 0.008 | 0.016 |
| 94.38 | 57.03 | 110.2 | 167.2 | | 0.540 | 0.008 | 0.000 | 0.000 | 0.008 | 0.017 |
| 94.39 | 59.56 | 113.7 | 173.3 | | 0.550 | 0.009 | 0.000 | 0.000 | 0.009 | 0.017 |
| 94.40 | 62.12 | 117.2 | 179.3 | Max 100-Yr WSE* | 0.560 | 0.009 | 0.000 | 0.000 | 0.009 | 0.018 |
| 94.41 | 64.70 | 120.8 | 185.5 | | 0.570 | 0.009 | 0.010 | 0.000 | 0.009 | 0.019 |
| 94.42 | 67.31 | 124.4 | 191.7 | | 0.580 | 0.009 | 0.020 | 0.001 | 0.010 | 0.019 |
| 94.43 | 69.95 | 128.0 | 197.9 | | 0.590 | 0.009 | 0.030 | 0.002 | 0.011 | 0.020 |
| 94.44 | 72.61 | 131.7 | 204.3 | | 0.600 | 0.009 | 0.040 | 0.004 | 0.013 | 0.020 |
| 94.45 | 75.29 | 135.4 | 210.7 | | 0.610 | 0.009 | 0.050 | 0.005 | 0.014 | 0.021 |
| 94.46 | 78.00 | 139.1 | 217.1 | | 0.620 | 0.009 | 0.060 | 0.007 | 0.016 | 0.022 |
| 94.47 | 80.74 | 142.9 | 223.7 | | 0.630 | 0.009 | 0.070 | 0.008 | 0.018 | 0.022 |
| 94.48 | 83.50 | 146.8 | 230.3 | | 0.640 | 0.009 | 0.080 | 0.010 | 0.019 | 0.023 |
| 94.49 | 86.29 | 150.7 | 237.0 | | 0.650 | 0.009 | 0.090 | 0.012 | 0.021 | 0.024 |
| 94.50 | 89.10 | 154.6 | 243.7 | | 0.660 | 0.009 | 0.100 | 0.014 | 0.023 | 0.024 |
| 94.51 | 91.94 | 158.6 | 250.5 | | 0.670 | 0.009 | 0.110 | 0.016 | 0.026 | 0.025 |
| 94.52 | 94.81 | 162.6 | 257.4 | | 0.680 | 0.010 | 0.120 | 0.018 | 0.028 | 0.026 |
| 94.53 | 97.70 | 166.7 | 264.4 | | 0.690 | 0.010 | 0.130 | 0.020 | 0.030 | 0.026 |
| 94.54 | 100.61 | 170.8 | 271.4 | | 0.700 | 0.010 | 0.140 | 0.023 | 0.032 | 0.027 |
| 94.55 | 103.56 | 175.0 | 278.5 | | 0.710 | 0.010 | 0.150 | 0.025 | 0.035 | 0.028 |
| 94.56 | 106.53 | 179.2 | 285.7 | | 0.720 | 0.010 | 0.160 | 0.027 | 0.037 | 0.029 |
| 94.57 | 109.52 | 183.5 | 293.0 | | 0.730 | 0.010 | 0.170 | 0.029 | 0.039 | 0.029 |
| 94.58 | 112.54 | 187.8 | 300.3 | | 0.740 | 0.010 | 0.180 | 0.032 | 0.042 | 0.030 |
| 94.59 | 115.59 | 192.2 | 307.7 | | 0.750 | 0.010 | 0.190 | 0.034 | 0.044 | 0.031 |
| 94.60 | 118.66 | 196.6 | 315.2 | | 0.760 | 0.010 | 0.200 | 0.037 | 0.047 | 0.032 |
| 94.61 | 119.86 | 201.1 | 320.9 | | 0.770 | 0.010 | 0.210 | 0.039 | 0.049 | 0.032 |
| 94.62 | 121.07 | 205.6 | 326.7 | | 0.780 | 0.010 | 0.220 | 0.042 | 0.052 | 0.033 |
| 94.63 | 124.27 | 210.2 | 334.5 | | 0.790 | 0.010 | 0.230 | 0.044 | 0.055 | 0.033 |
| 94.64 | 125.49 | 214.9 | 340.4 | | 0.800 | 0.010 | 0.240 | 0.047 | 0.057 | 0.034 |
| 94.65 | 125.52 | 219.6 | 345.1 | | 0.810 | 0.010 | 0.250 | 0.049 | 0.060 | 0.035 |
| 94.66 | 126.70 | 224.3 | 351.0 | | 0.820 | 0.011 | 0.260 | 0.052 | 0.063 | 0.035 |
| 94.67 | 127.87 | 229.2 | 357.0 | | 0.830 | 0.011 | 0.270 | 0.055 | 0.065 | 0.036 |
| 94.68 | 131.15 | 234.1 | 365.2 | | 0.840 | 0.011 | 0.280 | 0.057 | 0.068 | 0.037 |
| 94.69 | 132.31 | 239.0 | 371.3 | | 0.850 | 0.011 | 0.290 | 0.060 | 0.070 | 0.037 |
| 94.70 | 132.31 | 244.0 | 376.3 | Pond Spill | 0.860 | 0.011 | 0.300 | 0.062 | 0.073 | 0.038 |

*Maximum allowable 100-year water level in the pond - not the simulated 100 year water level

Table B2 - Site 2 - Stage/Storage/Outflow Curves

| | | | | | Quality Control 1 | | Emergency Overflow | | | |
|---------------|-----------------------------|-----------------------------|--------------------------------|--------------------|------------------------|-----------------------------|--------------------|-----------------------------|-----------------------------|----------------|
| | | | | | Vertical Orifice | | Broad Crested Weir | | | |
| | | | | | Dia (m) | 0.075 | L (m) | 0.300 | | |
| | | | | | Area (m ²) | 0.006 | C _w | 1.580 | | |
| | | | | | Invert (m) | 93.71 | | | | |
| | | | | | C _e | 0.61 | Invert (m) | 94.40 | | |
| | | | | | Q @ D | 0.002 | n contr. | 2 | Total | |
| Elevation (m) | Storage 3 (m ³) | Storage 4 (m ³) | Total Volume (m ³) | Demarcation Points | Depth (m) | Outflow (m ³ /s) | Depth (m) | Outflow (m ³ /s) | Outflow (m ³ /s) | Storage (ha-m) |
| 93.71 | | 0.0 | 0.0 | Pond Bottom | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 93.72 | | 0.0 | 0.0 | | 0.010 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 93.73 | | 0.0 | 0.0 | | 0.020 | 0.001 | 0.000 | 0.000 | 0.001 | 0.000 |
| 93.74 | | 0.1 | 0.1 | | 0.030 | 0.001 | 0.000 | 0.000 | 0.001 | 0.000 |
| 93.75 | | 0.3 | 0.3 | | 0.040 | 0.001 | 0.000 | 0.000 | 0.001 | 0.000 |
| 93.76 | | 0.6 | 0.6 | | 0.050 | 0.002 | 0.000 | 0.000 | 0.002 | 0.000 |
| 93.77 | | 1.0 | 1.0 | | 0.060 | 0.002 | 0.000 | 0.000 | 0.002 | 0.000 |
| 93.78 | | 1.6 | 1.6 | | 0.070 | 0.002 | 0.000 | 0.000 | 0.002 | 0.000 |
| 93.79 | | 2.3 | 2.3 | | 0.080 | 0.002 | 0.000 | 0.000 | 0.002 | 0.000 |
| 93.80 | | 3.2 | 3.2 | | 0.090 | 0.003 | 0.000 | 0.000 | 0.003 | 0.000 |
| 93.81 | | 4.3 | 4.3 | | 0.100 | 0.003 | 0.000 | 0.000 | 0.003 | 0.000 |
| 93.82 | | 5.4 | 5.4 | | 0.110 | 0.003 | 0.000 | 0.000 | 0.003 | 0.001 |
| 93.83 | | 6.5 | 6.5 | | 0.120 | 0.003 | 0.000 | 0.000 | 0.003 | 0.001 |
| 93.84 | | 7.7 | 7.7 | | 0.130 | 0.004 | 0.000 | 0.000 | 0.004 | 0.001 |
| 93.85 | | 8.9 | 8.9 | | 0.140 | 0.004 | 0.000 | 0.000 | 0.004 | 0.001 |
| 93.86 | | 10.2 | 10.2 | | 0.150 | 0.004 | 0.000 | 0.000 | 0.004 | 0.001 |
| 93.87 | | 11.4 | 11.4 | | 0.160 | 0.004 | 0.000 | 0.000 | 0.004 | 0.001 |
| 93.88 | | 12.7 | 12.7 | | 0.170 | 0.004 | 0.000 | 0.000 | 0.004 | 0.001 |
| 93.89 | | 13.9 | 13.9 | | 0.180 | 0.005 | 0.000 | 0.000 | 0.005 | 0.001 |
| 93.90 | | 15.2 | 15.2 | | 0.190 | 0.005 | 0.000 | 0.000 | 0.005 | 0.002 |
| 93.91 | | 16.5 | 16.5 | | 0.200 | 0.005 | 0.000 | 0.000 | 0.005 | 0.002 |
| 93.92 | | 17.8 | 17.8 | | 0.210 | 0.005 | 0.000 | 0.000 | 0.005 | 0.002 |
| 93.93 | | 19.1 | 19.1 | | 0.220 | 0.005 | 0.000 | 0.000 | 0.005 | 0.002 |
| 93.94 | | 20.5 | 20.5 | | 0.230 | 0.005 | 0.000 | 0.000 | 0.005 | 0.002 |
| 93.95 | | 21.8 | 21.8 | | 0.240 | 0.005 | 0.000 | 0.000 | 0.005 | 0.002 |
| 93.96 | | 23.2 | 23.2 | | 0.250 | 0.006 | 0.000 | 0.000 | 0.006 | 0.002 |
| 93.97 | | 24.6 | 24.6 | | 0.260 | 0.006 | 0.000 | 0.000 | 0.006 | 0.002 |
| 93.98 | | 26.0 | 26.0 | | 0.270 | 0.006 | 0.000 | 0.000 | 0.006 | 0.003 |
| 93.99 | | 27.4 | 27.4 | | 0.280 | 0.006 | 0.000 | 0.000 | 0.006 | 0.003 |
| 94.00 | | 28.9 | 28.9 | | 0.290 | 0.006 | 0.000 | 0.000 | 0.006 | 0.003 |
| 94.01 | | 30.4 | 30.4 | | 0.300 | 0.006 | 0.000 | 0.000 | 0.006 | 0.003 |
| 94.02 | | 31.8 | 31.8 | | 0.310 | 0.006 | 0.000 | 0.000 | 0.006 | 0.003 |
| 94.03 | | 33.4 | 33.4 | | 0.320 | 0.006 | 0.000 | 0.000 | 0.006 | 0.003 |
| 94.04 | 0.0 | 34.9 | 34.9 | | 0.330 | 0.006 | 0.000 | 0.000 | 0.006 | 0.003 |
| 94.05 | 0.1 | 36.4 | 36.6 | | 0.340 | 0.007 | 0.000 | 0.000 | 0.007 | 0.004 |
| 94.06 | 0.4 | 38.0 | 38.4 | | 0.350 | 0.007 | 0.000 | 0.000 | 0.007 | 0.004 |
| 94.07 | 0.8 | 39.6 | 40.4 | | 0.360 | 0.007 | 0.000 | 0.000 | 0.007 | 0.004 |
| 94.08 | 1.3 | 41.2 | 42.5 | | 0.370 | 0.007 | 0.000 | 0.000 | 0.007 | 0.004 |
| 94.09 | 1.8 | 42.9 | 44.7 | | 0.380 | 0.007 | 0.000 | 0.000 | 0.007 | 0.004 |
| 94.10 | 2.5 | 44.5 | 47.0 | | 0.390 | 0.007 | 0.000 | 0.000 | 0.007 | 0.005 |
| 94.11 | 3.3 | 46.2 | 49.5 | | 0.400 | 0.007 | 0.000 | 0.000 | 0.007 | 0.005 |
| 94.12 | 4.1 | 48.0 | 52.1 | | 0.410 | 0.007 | 0.000 | 0.000 | 0.007 | 0.005 |
| 94.13 | 4.5 | 49.7 | 54.2 | | 0.420 | 0.007 | 0.000 | 0.000 | 0.007 | 0.005 |
| 94.14 | 5.6 | 51.5 | 57.1 | | 0.430 | 0.007 | 0.000 | 0.000 | 0.007 | 0.006 |
| 94.15 | 6.7 | 53.3 | 60.0 | | 0.440 | 0.008 | 0.000 | 0.000 | 0.008 | 0.006 |
| 94.16 | 8.0 | 55.1 | 63.1 | | 0.450 | 0.008 | 0.000 | 0.000 | 0.008 | 0.006 |
| 94.17 | 8.5 | 57.0 | 65.5 | | 0.460 | 0.008 | 0.000 | 0.000 | 0.008 | 0.007 |
| 94.18 | 10.0 | 58.9 | 68.9 | | 0.470 | 0.008 | 0.000 | 0.000 | 0.008 | 0.007 |
| 94.19 | 11.6 | 60.8 | 72.4 | | 0.480 | 0.008 | 0.000 | 0.000 | 0.008 | 0.007 |
| 94.20 | 13.3 | 62.7 | 76.0 | | 0.490 | 0.008 | 0.000 | 0.000 | 0.008 | 0.008 |
| 94.21 | 15.1 | 64.7 | 79.8 | | 0.500 | 0.008 | 0.000 | 0.000 | 0.008 | 0.008 |
| 94.22 | 17.0 | 66.7 | 83.8 | | 0.510 | 0.008 | 0.000 | 0.000 | 0.008 | 0.008 |
| 94.23 | 19.1 | 68.8 | 87.8 | | 0.520 | 0.008 | 0.000 | 0.000 | 0.008 | 0.009 |
| 94.24 | 21.1 | 70.9 | 92.0 | | 0.530 | 0.008 | 0.000 | 0.000 | 0.008 | 0.009 |
| 94.25 | 23.2 | 73.0 | 96.2 | | 0.540 | 0.008 | 0.000 | 0.000 | 0.008 | 0.010 |
| 94.26 | 25.4 | 75.1 | 100.5 | | 0.550 | 0.009 | 0.000 | 0.000 | 0.009 | 0.010 |
| 94.27 | 27.5 | 77.3 | 104.8 | | 0.560 | 0.009 | 0.000 | 0.000 | 0.009 | 0.010 |
| 94.28 | 29.7 | 79.5 | 109.2 | | 0.570 | 0.009 | 0.000 | 0.000 | 0.009 | 0.011 |
| 94.29 | 31.9 | 81.8 | 113.7 | | 0.580 | 0.009 | 0.000 | 0.000 | 0.009 | 0.011 |
| 94.30 | 34.1 | 84.1 | 118.2 | | 0.590 | 0.009 | 0.000 | 0.000 | 0.009 | 0.012 |
| 94.31 | 36.4 | 86.4 | 122.8 | | 0.600 | 0.009 | 0.000 | 0.000 | 0.009 | 0.012 |
| 94.32 | 38.7 | 88.7 | 127.4 | | 0.610 | 0.009 | 0.000 | 0.000 | 0.009 | 0.013 |
| 94.33 | 41.0 | 91.1 | 132.1 | | 0.620 | 0.009 | 0.000 | 0.000 | 0.009 | 0.013 |
| 94.34 | 43.3 | 93.6 | 136.9 | | 0.630 | 0.009 | 0.000 | 0.000 | 0.009 | 0.014 |
| 94.35 | 45.7 | 96.1 | 141.7 | | 0.640 | 0.009 | 0.000 | 0.000 | 0.009 | 0.014 |
| 94.36 | 48.1 | 98.6 | 146.7 | | 0.650 | 0.009 | 0.000 | 0.000 | 0.009 | 0.015 |
| 94.37 | 50.5 | 101.2 | 151.7 | | 0.660 | 0.009 | 0.000 | 0.000 | 0.009 | 0.015 |
| 94.38 | 52.9 | 103.8 | 156.7 | | 0.670 | 0.009 | 0.000 | 0.000 | 0.009 | 0.016 |
| 94.39 | 55.4 | 106.5 | 161.9 | | 0.680 | 0.010 | 0.000 | 0.000 | 0.010 | 0.016 |
| 94.40 | 57.9 | 109.2 | 167.1 | Max 100-Yr WSE* | 0.690 | 0.010 | 0.000 | 0.000 | 0.010 | 0.017 |
| 94.41 | 60.4 | 112.0 | 172.4 | | 0.700 | 0.010 | 0.010 | 0.000 | 0.010 | 0.017 |
| 94.42 | 62.9 | 114.8 | 177.7 | | 0.710 | 0.010 | 0.020 | 0.001 | 0.011 | 0.018 |
| 94.43 | 65.5 | 117.7 | 183.2 | | 0.720 | 0.010 | 0.030 | 0.002 | 0.012 | 0.018 |
| 94.44 | 68.1 | 119.9 | 188.0 | | 0.730 | 0.010 | 0.040 | 0.004 | 0.014 | 0.019 |
| 94.45 | 70.7 | 122.0 | 192.7 | | 0.740 | 0.010 | 0.050 | 0.005 | 0.015 | 0.019 |
| 94.46 | 73.4 | 123.8 | 197.2 | | 0.750 | 0.010 | 0.060 | 0.007 | 0.017 | 0.020 |
| 94.47 | 76.1 | 125.7 | 201.8 | | 0.760 | 0.010 | 0.070 | 0.008 | 0.019 | 0.020 |
| 94.48 | 78.8 | 127.2 | 206.0 | | 0.770 | 0.010 | 0.080 | 0.010 | 0.020 | 0.021 |
| 94.49 | 81.5 | 129.4 | 210.9 | | 0.780 | 0.010 | 0.090 | 0.012 | 0.022 | 0.021 |
| 94.50 | 84.3 | 131.0 | 215.2 | | 0.790 | 0.010 | 0.100 | 0.014 | 0.024 | 0.022 |
| 94.51 | 87.1 | 133.1 | 220.2 | | 0.800 | 0.010 | 0.110 | 0.016 | 0.026 | 0.022 |
| 94.52 | 89.9 | 134.7 | 224.6 | | 0.810 | 0.010 | 0.120 | 0.018 | 0.029 | 0.022 |
| 94.53 | 92.7 | 135.4 | 228.1 | | 0.820 | 0.011 | 0.130 | 0.020 | 0.031 | 0.023 |
| 94.53 | 92.7 | 135.4 | 228.1 | | 0.820 | 0.011 | 0.130 | 0.020 | 0.031 | 0.023 |
| 94.54 | 95.6 | 137.6 | 233.2 | | 0.830 | 0.011 | 0.140 | 0.023 | 0.033 | 0.023 |
| 94.55 | 98.5 | 137.6 | 236.1 | | 0.840 | 0.011 | 0.150 | 0.025 | 0.035 | 0.024 |
| 94.55 | 98.5 | 137.6 | 236.1 | | 0.840 | 0.011 | 0.150 | 0.025 | 0.035 | 0.024 |
| 94.56 | 101.4 | 138.4 | 239.9 | | 0.850 | 0.011 | 0.160 | 0.027 | 0.038 | 0.024 |
| 94.57 | 104.4 | 139.1 | 243.5 | | 0.860 | 0.011 | 0.170 | 0.029 | 0.040 | 0.024 |
| 94.57 | 104.4 | 139.1 | 243.5 | | 0.860 | 0.011 | 0.170 | 0.029 | 0.040 | 0.024 |
| 94.58 | 107.4 | 140.6 | 248.0 | | 0.870 | 0.011 | 0.180 | 0.032 | 0.043 | 0.025 |
| 94.59 | 110.4 | 141.4 | 251.8 | | 0.880 | 0.011 | 0.190 | 0.034 | 0.045 | 0.025 |
| 94.60 | 113.4 | 143.6 | 257.1 | | 0.890 | 0.011 | 0.200 | 0.037 | 0.048 | 0.026 |
| 94.61 | 114.6 | 144.4 | 259.1 | | 0.900 | 0.011 | 0.210 | 0.039 | 0.050 | 0.026 |
| 94.62 | 115.8 | 145.9 | 261.7 | | 0.910 | 0.011 | 0.220 | 0.042 | 0.053 | 0.026 |
| 94.63 | 119.0 | 148.1 | 267.1 | | 0.920 | 0.011 | 0.230 | 0.044 | 0.055 | 0.027 |
| 94.64 | 120.2 | 149.6 | 269.8 | | 0.930 | 0.011 | 0.240 | 0.047 | 0.058 | 0.027 |
| 94.65 | 120.2 | 150.4 | 270.6 | | 0.940 | 0.011 | 0.250 | 0.049 | 0.061 | 0.027 |
| 94.66 | 121.4 | 152.6 | 274.1 | | 0.950 | 0.011 | 0.260 | 0.052 | 0.063 | 0.027 |
| 94.67 | 122.6 | 153.4 | 276.0 | | 0.960 | 0.011 | 0.270 | 0.055 | 0.066 | 0.028 |
| 94.68 | 125.8 | 155.7 | 281.5 | | 0.970 | 0.012 | 0.280 | 0.057 | 0.069 | 0.028 |
| 94.69 | 127.0 | 156.5 | 283.5 | | 0.980 | 0.012 | 0.290 | 0.060 | 0.071 | 0.028 |
| 94.70 | 127.0 | 157.3 | 284.3 | Pond Spill | 0.990 | 0.012 | 0.300 | 0.062 | 0.074 | 0.028 |

```

1  20      Metric units / ID numbers OFF
2  *#*****
   *****
3  *#  SWMHYMO  / INPUT DATA FILE
4  *#*****
   *****
5  *#  Project Name   : [5923 Ottawa St]
6  *#  Project Number: [P2710(e01)]
7  *#  Date           : [2025 April 28]
8  *#  Modeller       : [MM]
9  *#  Company        : JFSA Canada Inc.
10 *#  License #      : 2549237
11 *#*****
   *****
12 *# Model developed to simulate runoff from subcatchments under post development
   conditions
13 *#*****
   *****
14 *%  25 mm Storm based on 2-Year, 3-Hour Chicago Storm
15 START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[002]
16                ["002YC3H.stm"] <--storm filename, one per line for NSTORM time
17 *%-----|-----
18 READ STORM      STORM_FILENAME=["STORM.001"]
19 *%-----|-----
20 *#*****
   *****
21 *%-----|-----
22 DEFAULT VALUES ICASEdef=[1],  read values only
23                DEFVAL_FILENAME=["Ottawa.val"]
24 *%-----|-----
25 *#*****
   *****
26 *#  EXT1
27 *#*****
   *****
28 CALIB NASHYD    NHYD=["EXT1"], DT[1] (min), AREA=[3.211] (ha),
29                DWF=[0] (cms), CN=[80],
30                IA=[4.67] (mm), N=[3], TP[0.72] (hrs),
31                RAINFALL[ , , -1]
32 *#*****
   *****
33 *#  EXT2
34 *#*****
   *****
35 CALIB NASHYD    NHYD=["EXT2"], DT[1] (min), AREA=[0.285] (ha),
36                DWF=[0] (cms), CN=[85],
37                IA=[4.67] (mm), N=[3], TP[0.33] (hrs),
38                RAINFALL[ , , -1]
39 *#*****
   *****
40 *#  EXT3
41 *#*****
   *****
42 CALIB NASHYD    NHYD=["EXT3"], DT[1] (min), AREA=[0.560] (ha),
43                DWF=[0] (cms), CN=[80],
44                IA=[4.67] (mm), N=[3], TP[0.32] (hrs),
45                RAINFALL[ , , -1]
46 *#*****
   *****
47 *#  EXT4
48 *#*****
   *****
49 CALIB NASHYD    NHYD=["EXT4"], DT[1] (min), AREA=[0.309] (ha),
50                DWF=[0] (cms), CN=[79],
51                IA=[4.67] (mm), N=[3], TP[0.29] (hrs),
52                RAINFALL[ , , -1]
53 *#*****
   *****
54 *#  EXT5

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55  *#*****
56  CALIB NASHYD      NHYD=["EXT5"], DT[1] (min), AREA=[0.594] (ha),
57                    DWF=[0] (cms), CN=[76],
58                    IA=[4.67] (mm), N=[3], TP[0.45] (hrs),
59                    RAINFALL[ , , -1]
60  *#*****
61  *# EXT6
62  *#*****
63  CALIB NASHYD      NHYD=["EXT6"], DT[1] (min), AREA=[0.864] (ha),
64                    DWF=[0] (cms), CN=[85],
65                    IA=[4.67] (mm), N=[3], TP[0.56] (hrs),
66                    RAINFALL[ , , -1]
67  *#*****
68  *# EXT7
69  *#*****
70  CALIB NASHYD      NHYD=["EXT7"], DT[1] (min), AREA=[0.471] (ha),
71                    DWF=[0] (cms), CN=[83],
72                    IA=[4.67] (mm), N=[3], TP[0.32] (hrs),
73                    RAINFALL[ , , -1]
74  *#*****
75  *# EXT8
76  *#*****
77  CALIB NASHYD      NHYD=["EXT8"], DT[1] (min), AREA=[0.834] (ha),
78                    DWF=[0] (cms), CN=[79],
79                    IA=[4.67] (mm), N=[3], TP[0.42] (hrs),
80                    RAINFALL[ , , -1]
81  *#*****
82  *# EXT9
83  *#*****
84  CALIB NASHYD      NHYD=["EXT9"], DT[1] (min), AREA=[3.571] (ha),
85                    DWF=[0] (cms), CN=[76],
86                    IA=[4.67] (mm), N=[3], TP[0.48] (hrs),
87                    RAINFALL[ , , -1]
88  *#*****
89  *# EXT9a
90  *#*****
91  CALIB NASHYD      NHYD=["EXT9a"], DT[1] (min), AREA=[0.011] (ha),
92                    DWF=[0] (cms), CN=[78],
93                    IA=[4.67] (mm), N=[3], TP[0.04] (hrs),
94                    RAINFALL[ , , -1]
95  *#*****
96  *# EXT10
97  *#*****
98  CALIB NASHYD      NHYD=["EXT10"], DT[1] (min), AREA=[0.203] (ha),
99                    DWF=[0] (cms), CN=[71],
100                   IA=[4.67] (mm), N=[3], TP[0.42] (hrs),
101                   RAINFALL[ , , -1]
102  *#*****
103  *# Pre2_1
104  *#*****
105  CALIB NASHYD      NHYD=["Pre2_1"], DT[1] (min), AREA=[0.013] (ha),
106                    DWF=[0] (cms), CN=[72],
107                    IA=[4.67] (mm), N=[3], TP[0.03] (hrs),
108                    RAINFALL[ , , -1]

```



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109  *#*****
110  *# Pre2_2
111  *#*****
112  CALIB NASHYD      NHYD=["Pre2_2"], DT[1] (min), AREA=[0.002] (ha),
113                   DWF=[0] (cms), CN=[78],
114                   IA=[4.67] (mm), N=[3], TP[0.02] (hrs),
115                   RAINFALL[ , , -1]
116  *#*****
117  *# Pre9_1
118  *#*****
119  CALIB NASHYD      NHYD=["Pre9_1"], DT[1] (min), AREA=[0.437] (ha),
120                   DWF=[0] (cms), CN=[71],
121                   IA=[4.67] (mm), N=[3], TP[0.38] (hrs),
122                   RAINFALL[ , , -1]
123  *#*****
124  *# Pre9_2
125  *#*****
126  CALIB NASHYD      NHYD=["Pre9_2"], DT[1] (min), AREA=[0.014] (ha),
127                   DWF=[0] (cms), CN=[59],
128                   IA=[4.67] (mm), N=[3], TP[0.03] (hrs),
129                   RAINFALL[ , , -1]
130  *#*****
131  *# Pre10_1
132  *#*****
133  CALIB NASHYD      NHYD=["Pre10_1"], DT[1] (min), AREA=[0.799] (ha),
134                   DWF=[0] (cms), CN=[71],
135                   IA=[4.67] (mm), N=[3], TP[0.29] (hrs),
136                   RAINFALL[ , , -1]
137  *#*****
138  *# Pre11_1
139  *#*****
140  CALIB NASHYD      NHYD=["Pre11_1"], DT[1] (min), AREA=[0.067] (ha),
141                   DWF=[0] (cms), CN=[78],
142                   IA=[4.67] (mm), N=[3], TP[0.21] (hrs),
143                   RAINFALL[ , , -1]
144  *#*****
145  *# Site 1
146  *#*****
147  DESIGN STANDHYD   NHYD=["S1-B1"], DT=[1] (min), AREA=[0.415] (ha),
148                   XIMP=[0.34], TIMP=[0.44], DWF=[0] (cms),
149                   LOSS=[1], SLOPE=[1.0] (%), RAINFALL=[ , , -1] (mm/hr)
150  *#*****
151  *# Site 1 - Roof
152  *#*****
153  DESIGN STANDHYD   NHYD=["S1-Roof"], DT=[1] (min), AREA=[0.065] (ha),
154                   XIMP=[0.99], TIMP=[0.99], DWF=[0] (cms),
155                   LOSS=[1], SLOPE=[0.5] (%), RAINFALL=[ , , -1] (mm/hr)
156  *%-----|-----
157  * Rooftop Storage-Outflow Curve for site 1 Facility - From EGIS Report
158  ROUTE RESERVOIR   NHYDout=["S1-Roof-Out"], NHYDin=["S1-Roof"], RDT=[1] (min),
159                   TABLE of ( OUTFLOW-STORAGE ) values
160                   (cms) - (ha-m)
161                   [ 0 , 0 ]
162                   [ 0.0008 , 0.0007 ]

```

```

163         [ 0.001 , 0.001 ]
164         [ 0.0015 , 0.0015 ]
165         [ 0.0018 , 0.0017 ]
166         [ 0.0023 , 0.0022 ]
167         [ 0.0025 , 0.0024 ]
168         [ 0.0028 , 0.0027 ]
169         [ 0.003 , 0.0029 ]
170         [ 0.0033 , 0.0032 ]
171         [ 0.0038 , 0.0037 ]
172         [ 0.004 , 0.0039 ]
173         [ 0.0045 , 0.0044 ]
174         [ 0.0048 , 0.0046 ]
175         [ 0.0051 , 0.0049 ]
176         [ 0.0056 , 0.0054 ]
177         [ 0.0063 , 0.0061 ]
178         [ 0.0066 , 0.0064 ]
179         [ 0.0076 , 0.0073 ]
180         [ -1 , -1 ]
181         NHYDovf=["S1-Roof-Over"],
182     *%-----|-----
183     ADD HYD          NHYDsum=["SITE1-IN"], NHYDs to add=["S1-B1"+"S1-Roof-Out"+
184     "S1-Roof-Over"]
185     *%-----|-----
186     * Pond for Site 1: Stage-Storage-Outflow
187     ROUTE RESERVOIR    NHYDout=["SITE1-Out"], NHYDin=["SITE1-IN"], RDT=[1] (min),
188                       TABLE of ( OUTFLOW-STORAGE ) values
189                           (cms) - (ha-m)
190                           [ 0.00000 , 0 ]
191                           [ 0.00154 , 0.00006 ]
192                           [ 0.00246 , 0.00019 ]
193                           [ 0.00321 , 0.0004 ]
194                           [ 0.00382 , 0.00069 ]
195                           [ 0.00435 , 0.00106 ]
196                           [ 0.00481 , 0.00153 ]
197                           [ 0.00524 , 0.00217 ]
198                           [ 0.00563 , 0.00301 ]
199                           [ 0.006 , 0.00397 ]
200                           [ 0.00634 , 0.00517 ]
201                           [ 0.00667 , 0.00643 ]
202                           [ 0.00699 , 0.00791 ]
203                           [ 0.00729 , 0.00945 ]
204                           [ 0.00757 , 0.01105 ]
205                           [ 0.00785 , 0.01269 ]
206                           [ 0.00812 , 0.01438 ]
207                           [ 0.00838 , 0.01613 ]
208                           [ 0.00863 , 0.01793 ]
209                           [ 0.01129 , 0.01979 ]
210                           [ 0.0158 , 0.02171 ]
211                           [ 0.02137 , 0.0237 ]
212                           [ 0.0277 , 0.02574 ]
213                           [ 0.03457 , 0.02785 ]
214                           [ 0.04186 , 0.03003 ]
215                           [ 0.04945 , 0.03209 ]
216                           [ 0.05724 , 0.03404 ]
217                           [ 0.06516 , 0.0357 ]
218                           [ 0.07313 , 0.03763 ]
219                           [ -1 , -1 ]
220         NHYDovf=["SITE1-Over"],
221     *%-----|-----
222     *# Site 2
223     *# Site 2
224     DESIGN STANDHYD    NHYD=["S2-B3"], DT=[1] (min), AREA=[0.354] (ha),
225     XIMP=[0.31], TIMP=[0.41], DWF=[0] (cms),

```

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226                LOSS=[1], SLOPE=[1.0] (%), RAINFALL=[ , , -1] (mm/hr)
227 *#*****
228 *# Site 2 - Roof
229 *#*****
230 DESIGN STANDHYD      NHYD=["S2-Roof"], DT=[1] (min), AREA=[0.093] (ha),
231                      XIMP=[0.99], TIMP=[0.99], DWF=[0] (cms),
232                      LOSS=[1], SLOPE=[0.5] (%), RAINFALL=[ , , -1] (mm/hr)
233 *#*****
234 * Rooftop Storage-Outflow Curve for site 2 Facility - From EGIS Report
235 ROUTE RESERVOIR      NHYDout=["S2-Roof-Out"], NHYDin=["S2-Roof"], RDT=[1] (min),
236                      TABLE of ( OUTFLOW-STORAGE ) values
237                      (cms) - (ha-m)
238                      [ 0 , 0 ]
239                      [ 0.0007 , 0 ]
240                      [ 0.0015 , 0.0001 ]
241                      [ 0.003 , 0.0002 ]
242                      [ 0.0037 , 0.0004 ]
243                      [ 0.0048 , 0.0007 ]
244                      [ 0.0053 , 0.0008 ]
245                      [ 0.0065 , 0.0014 ]
246                      [ 0.0072 , 0.0018 ]
247                      [ 0.0081 , 0.0025 ]
248                      [ 0.0084 , 0.0029 ]
249                      [ 0.0092 , 0.0042 ]
250                      [ 0.0099 , 0.006 ]
251                      [ 0.0104 , 0.0075 ]
252                      [ 0.0106 , 0.0083 ]
253                      [ 0.0112 , 0.0109 ]
254                      [ 0.0143 , 0.0128 ]
255                      [ 0.0174 , 0.0138 ]
256                      [ 0.0253 , 0.0158 ]
257                      [ 0.0276 , 0.0164 ]
258                      [ -1 , -1 ]
259                      NHYDovf=["S2-Roof-Over"],
260 *%-----|-----
261 ADD HYD          NHYDsum=["SITE2-IN"], NHYDs to add=["S2-B3"+"S2-Roof-Out"+
262 "S2-Roof-Over"]
263 *%-----|-----
264 * Pond for Site 2: Stage-Storage-Outflow
265 ROUTE RESERVOIR      NHYDout=["SITE2-Out"], NHYDin=["SITE2-IN"], RDT=[1] (min),
266                      TABLE of ( OUTFLOW-STORAGE
267                      (cms) - (ha-m)
268                      [ 0 , 0 ]
269                      [ 0.0022 , 0.0002 ]
270                      [ 0.003 , 0.0004 ]
271                      [ 0.0036 , 0.0008 ]
272                      [ 0.0042 , 0.0011 ]
273                      [ 0.0047 , 0.0015 ]
274                      [ 0.0051 , 0.0019 ]
275                      [ 0.0055 , 0.0023 ]
276                      [ 0.0059 , 0.0027 ]
277                      [ 0.0062 , 0.0032 ]
278                      [ 0.0066 , 0.0037 ]
279                      [ 0.0069 , 0.0042 ]
280                      [ 0.0072 , 0.0049 ]
281                      [ 0.0075 , 0.0057 ]
282                      [ 0.0078 , 0.0065 ]
283                      [ 0.008 , 0.0076 ]
284                      [ 0.0083 , 0.0088 ]
285                      [ 0.0085 , 0.01 ]
286                      [ 0.0088 , 0.0114 ]
287                      [ 0.009 , 0.0127 ]
288                      [ 0.0093 , 0.0142 ]
289                      [ 0.0095 , 0.0157 ]
290                      [ 0.0102 , 0.0172 ]
291                      [ 0.0136 , 0.0188 ]

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291 [ 0.0185 , 0.0202 ]
292 [ 0.0243 , 0.0215 ]
293 [ 0.0309 , 0.0228 ]
294 [ 0.0355 , 0.0236 ]
295 [ 0.0403 , 0.0244 ]
296 [ 0.0452 , 0.0252 ]
297 [ 0.0529 , 0.0262 ]
298 [ 0.0607 , 0.0271 ]
299 [ 0.0686 , 0.0282 ]
300 [ 0.074 , 0.0284 ]
301 [ 0.0766 , 0.0287 ]
302 [ 0.0793 , 0.0287 ]
303 [ 0.0819 , 0.0287 ]
304 [ 0.0819 , 0.0287 ]
305 [ 0.0846 , 0.0287 ]
306 [ 0.0872 , 0.0287 ]
307 [ 0.0898 , 0.0287 ]
308 [ 0.0924 , 0.0288 ]
309 [ 0.095 , 0.0288 ]
310 [ 0.0976 , 0.0288 ]
311 [ 0.1027 , 0.0288 ]
312 [ 0.1053 , 0.0288 ]
313 [ 0.1078 , 0.0288 ]
314 [ 0.1102 , 0.0288 ]
315 [ 0.1127 , 0.0288 ]
316 [ 0.1151 , 0.0289 ]
317 [ 0.1175 , 0.0289 ]
318 [ 0.1199 , 0.0289 ]
319 [ 0.1222 , 0.0289 ]
320 [ 0.129 , 0.0289 ]
321 [ 0.1355 , 0.0289 ]
322 [ 0.1417 , 0.0289 ]
323 [ 0.1474 , 0.0289 ]
324 [ 0.151 , 0.0289 ]
325 [ 0.156 , 0.0289 ]
326 [ -1 , -1 ]
327 NHYDovf=["SITE2-Over"],
328 *%-----|-----|
329 ADD HYD NHYDsum=["Site1"], NHYDs to add=["SITE1-Out"+"SITE1-Over"]
330 *%-----|-----|
331 ADD HYD NHYDsum=["Site2"], NHYDs to add=["SITE2-Out"+"SITE2-Over"]
332 *%-----|-----|
333 ADD HYD NHYDsum=["J1"], NHYDs to add=["EXT2"+"Pre2_1"+"Site1"+"Site2"]
334 *%-----|-----|
335 * NOTE: Cross-section number 849.0434 is taken from HEC-RAS Model
336 ROUTE CHANNEL NHYDout=["R1"], NHYDin=["J1"], RDT=[1] (min),
337 CHLGTH=[143.151] (m), CHSLOPE=[0.394] (%), FPSLOPE=[0.394] (%),
338 SECNUM=[849.0434], NSEG=[3],
339 ( SEGROUGH, SEGDIST (m))=[0.08,18.95 -0.035,26.78 0.08,35.18] NSEG
times
340 ( DISTANCE (m), ELEVATION (m))=[0.48, 94.05]
341 [3.19, 93.99]
342 [6.85, 93.91]
343 [10.48, 93.87]
344 [17.45, 93.85]
345 [18.95, 93.84]
346 [20.36, 93.81]
347 [22.3, 93.76]
348 [22.53, 93.72]
349 [23.98, 93.35]
350 [24.35, 93.33]
351 [24.65, 93.37]
352 [25.04, 93.45]
353 [26.04, 93.74]
354 [26.44, 93.82]
355 [26.78, 93.87]
356 [29.14, 94.11]
357 [33.98, 94.26]
358 [35.18, 94.26]

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359 *%-----|-----
360 ADD HYD      NHYDsum=["J2"], NHYDs to add=["R1"+"EXT3"+"EXT1"]
361 *%-----|-----
362 * NOTE: Cross-section number 737.5813 is taken from HEC-RAS Model
363 ROUTE CHANNEL NHYDout=["R2"], NHYDin=["J2"], RDT=[1] (min),
364              CHLGTH=[73.338] (m), CHSLOPE=[0.425] (%), FPSLOPE=[0.425] (%),
365              SECNUM=[737.5813], NSEG=[3],
366              ( SEGROUGH, SEGDIST (m))=[0.08,8.4 -0.035,16.42 0.08,22.6] NSEG
              times
              ( DISTANCE (m), ELEVATION (m))=[0, 93.52]
367              [1.08, 93.5]
368              [4.37, 93.48]
369              [6.31, 93.45]
370              [8.4, 93.38]
371              [9.5, 93.31]
372              [10.49, 93.23]
373              [10.99, 93.18]
374              [12.4, 92.94]
375              [13.11, 92.84]
376              [13.67, 92.92]
377              [16.42, 93.6]
378              [16.91, 93.65]
379              [17.97, 93.65]
380              [19, 93.83]
381              [19.51, 93.89]
382              [21.06, 93.94]
383              [22.6, 93.95]
384
385 *%-----|-----
386 ADD HYD      NHYDsum=["J3"], NHYDs to add=["R2"+"EXT4"]
387 *%-----|-----
388 * NOTE: Cross-section number 675.4097 is taken from HEC-RAS Model
389 ROUTE CHANNEL NHYDout=["R3"], NHYDin=["J3"], RDT=[1] (min),
390              CHLGTH=[92.08] (m), CHSLOPE=[0.274] (%), FPSLOPE=[0.274] (%),
391              SECNUM=[675.4097], NSEG=[3],
392              ( SEGROUGH, SEGDIST (m))=[0.08,31.64 -0.035,42.44 0.08,48.87] NSEG
              times
              ( DISTANCE (m), ELEVATION (m))=[30.59, 93.12]
393              [31.64, 93.13]
394              [34.35, 93.08]
395              [35.18, 93.03]
396              [37.78, 92.72]
397              [38.25, 92.64]
398              [38.7, 92.61]
399              [39.74, 92.76]
400              [42.44, 93.41]
401              [42.89, 93.49]
402              [43.97, 93.57]
403              [44.92, 93.6]
404              [46.07, 93.67]
405              [48.87, 93.74]
406
407 *%-----|-----
408 ADD HYD      NHYDsum=["J4"], NHYDs to add=["R3"+"EXT5"]
409 *%-----|-----
410 * NOTE: Cross-section number 518.7506 is taken from HEC-RAS Model
411 ROUTE CHANNEL NHYDout=["R4"], NHYDin=["J4"], RDT=[1] (min),
412              CHLGTH=[251.495] (m), CHSLOPE=[0.19] (%), FPSLOPE=[0.19] (%),
413              SECNUM=[518.7506], NSEG=[3],
414              ( SEGROUGH, SEGDIST (m))=[0.08,51.48 -0.035,59.39 0.08,66.4] NSEG
              times
              ( DISTANCE (m), ELEVATION (m))=[0, 92.92]
415              [4.26, 92.9]
416              [48.31, 92.76]
417              [51.48, 92.76]
418              [53.64, 92.7]
419              [55.33, 92.29]
420              [55.44, 92.29]
421              [56.43, 92.37]
422              [56.97, 92.43]
423              [59.39, 93.27]
424

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425                                     [59.74, 93.37]
426                                     [60.8, 93.52]
427                                     [63.31, 93.71]
428                                     [66.4, 93.76]
429 *%-----|-----
430 ADD HYD          NHYDsum=["J5"], NHYDs to add=["R4"+"EXT6"+"EXT7"]
431 *%-----|-----
432 * NOTE: Cross-section number 275.0857 is taken from HEC-RAS Model
433 ROUTE CHANNEL    NHYDout=["R5"], NHYDin=["J5"], RDT=[1] (min),
434                  CHLGTH=[237.343] (m), CHSLOPE=[0.644] (%), FPSLOPE=[0.644] (%),
435                  SECNUM=[275.0857], NSEG=[3],
436                  ( SEGROUGH, SEGDIST (m))=[0.08,40.82 -0.035,53.64 0.08,57.93] NSEG
                     times
437                  ( DISTANCE (m), ELEVATION (m))=[36.16, 92.63]
438                                     [40.82, 92.97]
439                                     [41.39, 92.9]
440                                     [44.69, 91.72]
441                                     [45.24, 91.58]
442                                     [46.33, 91.43]
443                                     [47.41, 91.64]
444                                     [47.87, 91.75]
445                                     [49.59, 92.2]
446                                     [50.99, 92.36]
447                                     [51.44, 92.48]
448                                     [53.18, 92.98]
449                                     [53.64, 93.15]
450                                     [55.92, 93.66]
451                                     [57.93, 93.68]
452 *%-----|-----
453 ADD HYD          NHYDsum=["Pre"], NHYDs to add=["Pre10_1"+"Pre9_2"+"Pre2_2"]
454 *%-----|-----
455 * NOTE: Cross-section number 124 is taken from HEC-RAS Model
456 ROUTE CHANNEL    NHYDout=["R6"], NHYDin=["Pre"], RDT=[1] (min),
457                  CHLGTH=[77.414] (m), CHSLOPE=[0.776] (%), FPSLOPE=[0.776] (%),
458                  SECNUM=[124], NSEG=[3],
459                  ( SEGROUGH, SEGDIST (m))=[0.08,8.34 -0.035,31.31 0.08,84.97] NSEG
                     times
460                  ( DISTANCE (m), ELEVATION (m))=[1.78, 93.73]
461                                     [4.51, 93.54]
462                                     [5.06, 93.31]
463                                     [7.25, 92.98]
464                                     [7.79, 92.77]
465                                     [8.34, 92.49]
466                                     [9.43, 91.93]
467                                     [9.68, 91.81]
468                                     [10.53, 91.27]
469                                     [12.64, 90.92]
470                                     [14.44, 90.9]
471                                     [16.54, 91.06]
472                                     [17.64, 91.06]
473                                     [30.22, 92.3]
474                                     [31.31, 92.45]
475                                     [33.5, 92.41]
476                                     [55.37, 93.11]
477                                     [57.01, 93.2]
478                                     [84.97, 93.43]
479 *%-----|-----
480 * NOTE: Cross-section number 74 is taken from HEC-RAS Model
481 ROUTE CHANNEL    NHYDout=["R7"], NHYDin=["Pre9_1"], RDT=[1] (min),
482                  CHLGTH=[159.151] (m), CHSLOPE=[1.576] (%), FPSLOPE=[1.576] (%),
483                  SECNUM=[74], NSEG=[3],
484                  ( SEGROUGH, SEGDIST (m))=[0.08,4.67 -0.035,81.24 0.08,82.88] NSEG
                     times
485                  ( DISTANCE (m), ELEVATION (m))=[1.94, 93.64]
486                                     [4.67, 93.32]
487                                     [5.77, 93.15]
488                                     [7.41, 92.69]
489                                     [7.95, 92.37]
490                                     [9.36, 91.71]

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491                                     [10.12, 91.22]
492                                     [10.49, 91.06]
493                                     [12.64, 90.89]
494                                     [16.16, 90.92]
495                                     [18.83, 91.66]
496                                     [19.59, 92.02]
497                                     [21.62, 92.39]
498                                     [24.87, 92.48]
499                                     [30.37, 92.55]
500                                     [34.37, 92.65]
501                                     [77.41, 92.82]
502                                     [80.6, 93.25]
503                                     [81.24, 93.48]
504                                     [82.88, 93.79]
505 *%-----|-----
506 ADD HYD          NHYDsum=["J6"], NHYDs to add=["R6"+"EXT10"]
507 *%-----|-----
508 * NOTE: Cross-section number 49 is taken from HEC-RAS Model
509 ROUTE CHANNEL    NHYDout=["R8"], NHYDin=["J6"], RDT=[1] (min),
510                  CHLGTH=[78.801] (m), CHSLOPE=[0.522] (%), FPSLOPE=[0.522] (%),
511                  SECNUM=[49], NSEG=[3],
512                  ( SEGROUGH, SEGDIST (m))=[0.08,8.71 -0.035,20.59 0.08,116.73] NSEG
513                  times
514                  ( DISTANCE (m), ELEVATION (m))=[0, 93.36]
515                  [1.93, 93.63]
516                  [4.61, 93.26]
517                  [6.23, 93.1]
518                  [8.19, 92.26]
519                  [8.71, 91.84]
520                  [9.86, 91.47]
521                  [10.53, 91.04]
522                  [13.84, 91]
523                  [14.5, 91.11]
524                  [16.97, 91.27]
525                  [20.59, 91.76]
526                  [23.3, 91.64]
527                  [30.34, 91.85]
528                  [35.29, 91.92]
529                  [116.73, 92.96]
530 *%-----|-----
531 ADD HYD          NHYDsum=["J7"], NHYDs to add=["R8"+"R7"]
532 *%-----|-----
533 * NOTE: Cross-section number 7 is taken from HEC-RAS Model
534 ROUTE CHANNEL    NHYDout=["R9"], NHYDin=["J7"], RDT=[1] (min),
535                  CHLGTH=[29.445] (m), CHSLOPE=[0.887] (%), FPSLOPE=[0.887] (%),
536                  SECNUM=[7], NSEG=[3],
537                  ( SEGROUGH, SEGDIST (m))=[0.08,1.5 -0.035,22.44 0.08,100.08] NSEG
538                  times
539                  ( DISTANCE (m), ELEVATION (m))=[0, 93.4]
540                  [1.5, 93.63]
541                  [3.13, 93.62]
542                  [4.76, 93.28]
543                  [5.3, 93.25]
544                  [6.52, 93.08]
545                  [6.96, 92.95]
546                  [10.57, 90.95]
547                  [13.59, 90.67]
548                  [15.83, 90.72]
549                  [16.42, 90.85]
550                  [18.66, 91.76]
551                  [20.82, 91.86]
552                  [22.44, 91.92]
553                  [27.84, 91.98]
554                  [30.15, 91.96]
555                  [100.08, 92.61]
556 *%-----|-----
557 ADD HYD          NHYDsum=["J8"], NHYDs to add=["EXT9"+"R9"+"EXT8"+"R5"]
558 *%-----|-----
559 * Note: The pipe needs to be adjusted based on the Culvert-under-railway information

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```

558 ROUTE PIPE PTYPE=[1]circ, NHYDout=["Outlet"], RNUMBER=[1.0],
559 PDIAM=[525] (mm), PLNGTH=[8.407] (m), PROUGH=[0.013],
PSLOPE=[0.0001] (m/m),
560 NHYDin=["J8"], RDT=[1] (min)
561 *%-----|-----|
562 *#####|
563 *# STORMS
564 *#####|
565 *% 2-Year, 3-Hour Chicago Storm
566 *START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[002]
567 * ["002YC3H.stm"] <--storm filename, one per line for NSTORM time
568 *%-----|-----|
569 *% 5-Year, 3-Hour Chicago Storm
570 *START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[005]
571 * ["005YC3H.stm"] <--storm filename, one per line for NSTORM time
572 *%-----|-----|
573 *% 10-Year, 3-Hour Chicago Storm
574 *START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[010]
575 * ["010YC3H.stm"] <--storm filename, one per line for NSTORM time
576 *%-----|-----|
577 *% 25-Year, 3-Hour Chicago Storm
578 *START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[025]
579 * ["025YC3H.stm"] <--storm filename, one per line for NSTORM time
580 *%-----|-----|
581 *% 50-Year, 3-Hour Chicago Storm
582 *START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[050]
583 * ["050YC3H.stm"] <--storm filename, one per line for NSTORM time
584 *%-----|-----|
585 *% 100-Year, 3-Hour Chicago Storm
586 *START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[099]
587 * ["100YC3H.stm"] <--storm filename, one per line for NSTORM time
588 *%-----|-----|
589 *% 2-Year, 24-Hour SCS Storm
590 *START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[102]
591 * ["SC24002x.stm"] <--storm filename, one per line for NSTORM time
592 *%-----|-----|
593 *% 5-Year, 24-Hour SCS Storm
594 *START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[105]
595 * ["SC24005x.stm"] <--storm filename, one per line for NSTORM time
596 *%-----|-----|
597 *% 10-Year, 24-Hour SCS Storm
598 *START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[110]
599 * ["SC24010x.stm"] <--storm filename, one per line for NSTORM time
600 *%-----|-----|
601 *% 25-Year, 24-Hour SCS Storm
602 *START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[125]
603 * ["SC24025x.stm"] <--storm filename, one per line for NSTORM time
604 *%-----|-----|
605 *% 50-Year, 24-Hour SCS Storm
606 *START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[150]
607 * ["SC24050x.stm"] <--storm filename, one per line for NSTORM time
608 *%-----|-----|
609 *% 100-Year, 24-Hour SCS Storm
610 *START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[199]
611 * ["SC24100x.stm"] <--storm filename, one per line for NSTORM time
612 *%-----|-----|
613 *% July 1st, 1979 Storm - Ottawa International Airport
614 *START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[1979]
615 * ["19790701.stm"] <--storm filename, one per line for NSTORM time
616 *%-----|-----|
617 *% August 4th, 1988 Storm - Ottawa International Airport
618 *START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[1988]
619 * ["19880804.stm"] <--storm filename, one per line for NSTORM time
620 *%-----|-----|
621 *% August 8th, 1996 Storm - Ottawa International Airport
622 *START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[1996]
623 * ["19960808.stm"] <--storm filename, one per line for NSTORM time
624 *%-----|-----|
625 *% 100-Year, 3-Hour Chicago Storm + 20%

```



```
626  START                                TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[9999]
627                                     [ "100YC3H+.STM" ] <--storm filename, one per line for NSTORM time
628  *%-----|-----|
629  FINISH
```

```
00001 ===== SSSSS W W M M M H H Y Y M M M O O O 222 000 11 5555 =====
00002
00003 SSSSS W W M M M H H Y Y M M M O O O 222 000 11 5555
00004 S W W M M M M H H Y Y M M M O O O 2 0 0 11 5
00005 SSSSS W W M M M H H Y Y M M M O O O 222 000 11 5555 Ver 5.500
00006 S W W M M M H H Y Y M M M O O O 222 0 0 11 555 FEB 2015
00007 SSSSS W W M M M H H Y Y M M M O O O 2 0 0 11 5
00008
00009 StormWater Management Hydrologic Model 222 000 11 555 =====
00010
00011 ***** SWMM990 Ver 5.500 *****
00012 ***** based on the principles of HMM and its successors *****
00013 ***** OTTHMM-SI and OTTHMM-99 *****
00014 ***** Distributed by: J.F. Sabourin and Associates Inc. *****
00015 ***** Ottawa, Ontario: (613) 836-3884 *****
00016 ***** Gatineau, Quebec: (819) 243-6858 *****
00017 ***** E-mail: jsabourin@jfas.com *****
00018 *****
00019 *****
00020 *****
00021 *****
00022 *****
00023 *****
00024 *****
00025 ***** SERIAL#:2549237 *****
00026 *****
00027 *****
00028 ***** PROGRAM ARRAY DIMENSIONS *****
00029 ***** Maximum value for ID numbers: 1 *****
00030 ***** Max. number of rainfall points: 105408 *****
00031 *****
00032 *****
00033 *****
00034 *****
00035 *****
00036 ***** SUMMARY OUTPUT *****
00037 *****
00038 ***** RUN DATE: 2025-09-11 TIME: 20:19:56 RUN COUNTER: 011833 *****
00039 *****
00040 ***** Input file: C:\Temp\20250910-PostDev\Ott_St-Post_v11.dat *****
00041 ***** Output file: C:\Temp\20250910-PostDev\Ott_St-Post_v11.out *****
00042 ***** Summary file: C:\Temp\20250910-PostDev\Ott_St-Post_v11.sum *****
00043 ***** User comments: *****
00044 ***** 1. *****
00045 ***** 2. *****
00046 ***** 3. *****
00047 *****
00048 *****
00049 *****
00050 *****
00051 ***** SWMM990 / INPUT DATA FILE *****
00052 *****
00053 ***** Project Name : [5923 Ottawa St] *****
00054 ***** Project Number: [P2710(eb1)] *****
00055 ***** Date : [2025 April 28] *****
00056 ***** Modeler : [JFM] *****
00057 ***** Company : JFSA Canada Inc. *****
00058 ***** License # : 2549237 *****
00059 *****
00060 ***** Model developed to simulate runoff from subcatchments under post development conditions *****
00061 *****
00062 ***** ** END OF RUN : 1 *****
00063 *****
00064 *****
00065 *****
00066 *****
00067 *****
00068 *****
00069 *****
00070 ***** RUN COMMAND *****
00071 ***** R0002:CO0001 *****
00072 ***** START *****
00073 ***** [TZERO = 0.0 hrs on 0] *****
00074 ***** [METOUT = 2 (1=Imperial, 2=metric output)] *****
00075 ***** [METFORM = 1] *****
00076 ***** [NRUN = 0002] *****
00077 *****
00078 ***** SWMM990 / INPUT DATA FILE *****
00079 *****
00080 ***** Project Name : [5923 Ottawa St] *****
00081 ***** Project Number: [P2710(eb1)] *****
00082 ***** Date : [2025 April 28] *****
00083 ***** Modeler : [JFM] *****
00084 ***** Company : JFSA Canada Inc. *****
00085 ***** License # : 2549237 *****
00086 *****
00087 ***** Model developed to simulate runoff from subcatchments under post development conditions *****
00088 *****
00089 ***** R0002:CO0002 *****
00090 ***** READ STORM *****
00091 ***** Filename = STORM.001 *****
00092 ***** Comment = CHICAGO STORM 2 Year, 3 Hours *****
00093 ***** [SDT=10.00;SDUR= 3.00;PTOT= 31.86] *****
00094 *****
00095 ***** R0002:CO0003 *****
00096 ***** DEFAULT VALUES *****
00097 ***** Filename = C:\Temp\20250910-PostDev\Ottawa.val *****
00098 ***** [CASEDEV = 1 (read and print data)] *****
00099 ***** FileTitle File comment: [Parameters for City of Ottawa Projects] *****
00100 ***** USE FOLLOWING PARAMETERS ARE USED IN THE DESIGN STANDARD COM *****
00101 ***** Horton's infiltration equation parameters: *****
00102 ***** [Fw 16.0 mm/hr] [Fw1 20 mm/hr] [Fw2 14 hr] [Fw 0.0 mm] *****
00103 ***** Parameters for IMPERVIOUS surfaces in STANDIHD: *****
00104 ***** [Ipxres 4.67 mm] [Ipxres4 0.0 mm] [Ipxres 2.50] *****
00105 ***** Parameters for IMPERVIOUS surfaces in STANDIHD: *****
00106 ***** [Ipxres 1.57 mm] [Ipxres 1.50] [Ipxres 0.13] *****
00107 ***** Parameters used in NASHVIT *****
00108 ***** [Iw 4.67 mm] [N 3.00] *****
00109 ***** Average monthly Pan Evaporation data in (mm) *****
00110 ***** JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC *****
00111 ***** .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 *****
00112 ***** Average monthly Potential Evapotranspiration in (mm) *****
00113 ***** JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC *****
00114 ***** .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 *****
00115 *****
00116 ***** EXT1 *****
00117 *****
00118 ***** R0002:CO0004 *****
00119 ***** CALIB NASHVD 1.0 01:EXT1 3.21 .037 No_date 1:58 8.15 .256 .000 *****
00120 ***** [CN= 60.0; N= 3.00; Tpe = .56] *****
00121 *****
00122 ***** EXT2 *****
00123 *****
00124 ***** R0002:CO0005 *****
00125 ***** CALIB NASHVD 1.0 01:EXT2 .59 .008 No_date 1:36 6.88 .216 .000 *****
00126 ***** [CN= 85.0; N= 3.00; Tpe = .33] *****
00127 *****
00128 ***** EXT3 *****
00129 *****
00130 ***** R0002:CO0006 *****
00131 ***** CALIB NASHVD 1.0 01:EXT3 .56 .011 No_date 1:24 8.15 .256 .000 *****
00132 ***** [CN= 60.0; N= 3.00; Tpe = .32] *****
00133 *****
00134 ***** EXT4 *****
00135 *****
00136 ***** R0002:CO0007 *****
00137 ***** CALIB NASHVD 1.0 01:EXT4 .31 .006 No_date 1:22 7.80 .245 .000 *****
00138 ***** [CN= 79.0; N= 3.00; Tpe = .29] *****
00139 *****
00140 ***** EXT5 *****
00141 *****
00142 ***** R0002:CO0008 *****
00143 ***** CALIB NASHVD 1.0 01:EXT5 .59 .008 No_date 1:36 6.88 .216 .000 *****
00144 ***** [CN= 76.0; N= 3.00; Tpe = .45] *****
00145 *****
00146 ***** EXT6 *****
00147 *****
00148 ***** R0002:CO0009 *****
00149 ***** CALIB NASHVD 1.0 01:EXT6 .86 .015 No_date 1:44 10.27 .322 .000 *****
00150 ***** [CN= 60.0; N= 3.00; Tpe = .56] *****
00151 *****
00152 ***** EXT7 *****
00153 *****
00154 ***** R0002:CO0010 *****
00155 ***** CALIB NASHVD 1.0 01:EXT7 .01 .001 No_date 1:00 7.47 .234 .000 *****
00156 ***** [CN= 83.0; N= 3.00; Tpe = .32] *****
00157 *****
00158 ***** EXT8 *****
00159 *****
00160 ***** R0002:CO0011 *****
00161 ***** CALIB NASHVD 1.0 01:EXT8 .83 .013 No_date 1:33 7.81 .245 .000 *****
00162 ***** [CN= 79.0; N= 3.00; Tpe = .29] *****
00163 *****
00164 ***** EXT9 *****
00165 *****
00166 ***** R0002:CO0012 *****
00167 ***** CALIB NASHVD 1.0 01:EXT9 3.57 .045 No_date 1:38 6.88 .216 .000 *****
00168 ***** [CN= 76.0; N= 3.00; Tpe = .48] *****
00169 *****
00170 ***** EXT10 *****
00171 *****
00172 ***** R0002:CO0013 *****
00173 ***** CALIB NASHVD 1.0 01:EXT10 .01 .001 No_date 1:00 7.47 .234 .000 *****
00174 ***** [CN= 76.0; N= 3.00; Tpe = .04] *****
00175 *****
00176 ***** EXT11 *****
00177 *****
00178 ***** R0002:CO0014 *****
00179 ***** CALIB NASHVD 1.0 01:EXT11 .20 .002 No_date 1:34 5.64 .177 .000 *****
00180 ***** [CN= 71.0; N= 3.00; Tpe = .42] *****
00181 *****
00182 *****
00183 *****
00184 ***** R0002:CO0015 *****
00185 ***** CALIB NASHVD 1.0 01:Pre2.1 .00 .000 No_date 1:00 7.46 .234 .000 *****
00186 ***** [CN= 72.0; N= 3.00; Tpe = .03] *****
00187 *****
00188 *****
00189 *****
00190 ***** R0002:CO0016 *****
00191 ***** CALIB NASHVD 1.0 01:Pre2.2 .00 .000 No_date 1:00 7.46 .234 .000 *****
00192 ***** [CN= 70.0; N= 3.00; Tpe = .03] *****
00193 *****
00194 *****
00195 *****
00196 ***** R0002:CO0017 *****
00197 ***** CALIB NASHVD 1.0 01:Pre2.1 .44 .003 No_date 1:30 5.64 .177 .000 *****
00198 ***** [CN= 71.0; N= 3.00; Tpe = .38] *****
00199 *****
00200 *****
00201 *****
00202 *****
00203 *****
00204 *****
00205 *****
00206 *****
00207 *****
00208 ***** R0002:CO0019 *****
00209 ***** CALIB NASHVD 1.0 01:Pre10.1 .80 .011 No_date 1:22 5.65 .177 .000 *****
00210 ***** [CN= 71.0; N= 3.00; Tpe = .39] *****
00211 *****
00212 *****
00213 *****
00214 ***** R0002:CO0020 *****
00215 ***** CALIB NASHVD 1.0 01:Pre10.1 .00 .002 No_date 1:13 7.47 .235 .000 *****
00216 ***** [CN= 78.0; N= 3.00; Tpe = .21] *****
00217 *****
00218 *****
00219 *****
00220 ***** R0002:CO0021 *****
00221 ***** DESIGN STANDARD 1.0 01:81-B1 .42 .032 No_date 1:00 13.81 .433 .000 *****
00222 ***** [XIMP= 24;TIMP= 44] *****
00223 ***** [SLP= 1.00;DT= 1.00] *****
00224 ***** [LOSS= 1 : HORTON] *****
00225 *****
00226 *****
00227 *****
00228 ***** R0002:CO0022 *****
00229 ***** DESIGN STANDARD 1.0 01:81-Roof .06 .014 No_date 1:00 30.00 .942 .000 *****
00230 ***** [XIMP= 99;TIMP= 99] *****
00231 ***** [SLP= .50;DT= 1.00] *****
00232 ***** [LOSS= 1 : HORTON] *****
00233 ***** R0002:CO0023 *****
00234 ***** ROUTE RESERVOIR -> 1.0 01:81-Roof .06 .014 No_date 1:00 30.00 n/a .000 *****
00235 ***** out <= 1.0 01:81-Roof-Ov .00 .001 No_date 1:31 30.00 n/a .000 *****
00236 ***** overflow <= 1.0 01:81-Roof-Ov .00 .000 No_date 0:00 .00 n/a .000 *****
00237 ***** [MaxStoCap= 13116.002 n3, ToEvVol= 0.000E+00 n3, N=0;Ev 0. ToEvRoOfEv 0. hrs] *****
00238 ***** R0002:CO0024 *****
00239 ***** ADD HYD 1.0 01:81-B1 .42 .032 No_date 1:00 13.81 n/a .000 *****
00240 ***** out <= 1.0 01:81-Roof-Ov .06 .001 No_date 1:31 30.00 n/a .000 *****
00241 ***** overflow <= 1.0 01:81-Roof-Ov .00 .000 No_date 0:00 .00 n/a .000 *****
00242 ***** SUM= 1.0 01:81-Roof .48 .033 No_date 1:00 16.00 n/a .000 *****
00243 ***** R0002:CO0025 *****
00244 ***** ROUTE RESERVOIR -> 1.0 01:81-T2-IN .48 .033 No_date 1:00 16.00 n/a .000 *****
00245 ***** out <= 1.0 01:81-T2-IN .00 .000 No_date 1:40 16.00 n/a .000 *****
00246 ***** overflow <= 1.0 01:81-T2-Over .00 .000 No_date 0:00 .00 n/a .000 *****
00247 ***** [MaxStoCap= 3418.002 n3, ToEvVol= 0.000E+00 n3, N=0;Ev 0. ToEvRoOfEv 0. hrs] *****
00248 *****
00249 *****
00250 *****
00251 ***** R0002:CO0026 *****
00252 ***** DESIGN STANDARD 1.0 01:82-B3 .35 .023 No_date 1:00 13.02 .409 .000 *****
00253 ***** [XIMP= 31;TIMP= 41] *****
00254 ***** [SLP= 1.00;DT= 1.00] *****
00255 ***** [LOSS= 1 : HORTON] *****
00256 *****
00257 *****
00258 *****
00259 ***** R0002:CO0027 *****
00260 ***** DESIGN STANDARD 1.0 01:82-Roof .09 .020 No_date 1:00 30.02 .942 .000 *****
00261 ***** [XIMP= 99;TIMP= 99] *****
00262 ***** [SLP= .50;DT= 1.00] *****
00263 ***** [LOSS= 1 : HORTON] *****
00264 *****
00265 ***** R0002:CO0028 *****
00266 ***** ROUTE RESERVOIR -> 1.0 01:82-Roof .09 .020 No_date 1:00 30.02 n/a .000 *****
00267 ***** out <= 1.0 01:82-Roof-Ov .00 .000 No_date 1:31 30.00 n/a .000 *****
00268 ***** overflow <= 1.0 01:82-Roof-Ov .00 .000 No_date 0:00 .00 n/a .000 *****
00269 ***** [MaxStoCap= 11178.002 n3, ToEvVol= 0.000E+00 n3, N=0;Ev 0. ToEvRoOfEv 0. hrs] *****
00270 ***** R0002:CO0029 *****
00271 ***** ADD HYD 1.0 01:82-B3 .35 .025 No_date 1:00 13.02 n/a .000 *****
00272 ***** out <= 1.0 01:82-Roof-Ov .09 .006 No_date 1:30 30.00 n/a .000 *****
00273 ***** overflow <= 1.0 01:82-Roof-Ov .00 .000 No_date 0:00 .00 n/a .000 *****
00274 ***** SUM= 1.0 01:82-Roof .45 .031 No_date 1:00 16.56 n/a .000 *****
00275 ***** R0002:CO0030 *****
00276 ***** ROUTE RESERVOIR -> 1.0 01:81-T2-IN .45 .031 No_date 1:00 16.56 n/a .000 *****
00277 ***** out <= 1.0 01:81-T2-IN .00 .000 No_date 1:40 16.56 n/a .000 *****
00278 ***** overflow <= 1.0 01:81-T2-Over .00 .000 No_date 0:00 .00 n/a .000 *****
00279 ***** [MaxStoCap= 3808.002 n3, ToEvVol= 0.000E+00 n3, N=0;Ev 0. ToEvRoOfEv 0. hrs] *****
00280 *****
00281 *****
00282 *****
00283 *****
00284 ***** R0002:CO0032 *****
00285 ***** ADD HYD 1.0 01:81-T2-IN .48 .007 No_date 1:40 16.00 n/a .000 *****
00286 ***** out <= 1.0 01:81-T2-Over .00 .000 No_date 0:00 .00 n/a .000 *****
00287 ***** SUM= 1.0 01:81-T2-IN .48 .006 No_date 1:40 16.00 n/a .000 *****
00288 ***** R0002:CO0033 *****
00289 ***** ADD HYD 1.0 01:EXT2 .28 .007 No_date 1:25 10.26 n/a .000 *****
00290 ***** out <= 1.0 01:EXT2 .00 .000 No_date 1:00 16.00 n/a .000 *****
00291 ***** overflow <= 1.0 01:EXT2 .00 .000 No_date 0:00 .00 n/a .000 *****
00292 ***** SUM= 1.0 01:EXT2 .28 .007 No_date 1:25 10.26 n/a .000 *****
00293 *****
00294 ***** R0002:CO0034 *****
00295 ***** ROUTE CHANNEL -> 1.0 01:21 1.23 .019 No_date 1:27 14.76 n/a .000 *****
00296 ***** [RDT= 1.00] out <= 1.0 01:R1 1.23 .019 No_date 1:36 14.76 n/a .000 *****
00297 ***** [L/S/N= 142.0 / 274 / 035] *****
00298 ***** (Vmax = 258.0;Tmax = 093) *****
00299 ***** R0002:CO0035 *****
00300 ***** ADD HYD 1.0 01:21 1.23 .019 No_date 1:36 14.76 n/a .000 *****
00301 ***** out <= 1.0 01:EXT3 .56 .011 No_date 1:24 8.15 n/a .000 *****
00302 ***** overflow <= 1.0 01:EXT3 .00 .000 No_date 0:00 .00 n/a .000 *****
00303 ***** SUM= 1.0 01:21 5.00 .062 No_date 1:46 9.77 n/a .000 *****
00304 ***** R0002:CO0036 *****
00305 ***** ROUTE CHANNEL -> 1.0 01:21 1.46 .062 No_date 1:46 9.77 n/a .000 *****
00306 ***** [RDT= 1.00] out <= 1.0 01:R2 5.00 .062 No_date 1:49 9.77 n/a .000 *****
00307 ***** [L/S/N= 73.0 / 425 / 035] *****
00308 ***** (Vmax = 359.0;Tmax = 160) *****
00309 ***** R0002:CO0037 *****
00310 ***** ADD HYD 1.0 01:21 1.49 .062 No_date 1:49 9.77 n/a .000 *****
00311 ***** out <= 1.0 01:EXT4 .31 .006 No_date 1:22 7.80 n/a .000 *****
00312 ***** overflow <= 1.0 01:EXT4 .00 .000 No_date 0:00 .00 n/a .000 *****
00313 ***** SUM= 1.0 01:21 5.31 .066 No_date 1:46 9.66 n/a .000 *****
00314 ***** R0002:CO0038 *****
00315 ***** ROUTE CHANNEL -> 1.0 01:23 5.31 .066 No_date 1:46 9.66 n/a .000 *****
00316 ***** [RDT= 1.00] out <= 1.0 01:R3 5.31 .065 No_date 1:53 9.66 n/a .000 *****
00317 ***** [L/S/N= 92.0 / 274 / 035] *****
00318 ***** (Vmax = 294.0;Tmax = 145) *****
00319 ***** R0002:CO0039 *****
00320 ***** ADD HYD 1.0 01:R3 5.31 .065 No_date 1:51 9.66 n/a .000 *****
00321 ***** out <= 1.0 01:EXT5 .59 .008 No_date 1:36 6.88 n/a .000 *****
00322 ***** SUM= 1.0 01:24 5.90 .072 No_date 1:49 9.38 n/a .000 *****
00323 ***** ROUTE CHANNEL -> 1.0 01:24 5.90 .072 No_date 1:49 9.38 n/a .000 *****
00324 ***** [RDT= 1.00] out <= 1.0 01:R4 5.90 .067 No_date 2:05 9.38 n/a .000 *****
00325 ***** [L/S/N= 251.0 / 190 / 035] *****
00326 ***** (Vmax = 273.0;Tmax = 178) *****
00327 ***** R0002:CO0041 *****
00328 ***** ADD HYD 1.0 01:R4 5.90 .067 No_date 2:05 9.38 n/a .000 *****
00329 ***** out <= 1.0 01:EXT6 .86 .015 No_date 1:44 10.27 n/a .000 *****
00330 ***** overflow <= 1.0 01:EXT6 .00 .000 No_date 0:00 .00 n/a .000 *****
00331 ***** SUM= 1.0 01:25 7.23 .086 No_date 1:58 9.48 n/a .000 *****
00332 ***** ROUTE CHANNEL -> 1.0 01:25 7.23 .086 No_date 1:58 9.48 n/a .000 *****
00333 ***** [RDT= 1.00] out <= 1.0 01:R5 7.23 .084 No_date 2:05 9.48 n/a .000 *****
00334 ***** [L/S/N= 237.0 / 644 / 035] *****
00335 ***** (Vmax = 444.0;Tmax = 172) *****
00336 ***** R0002:CO0043 *****
00337 ***** ADD HYD 1.0 01:Pre1.0 .80 .011 No_date 1:22 5.65 n/a .000 *****
00338 ***** out <= 1.0 01:Pre2.2 .01 .000 No_date 1:00 3.62 n/a .000 *****
00339 ***** overflow <= 1.0 01:Pre2.2 .00 .000 No_date 0:00 4.46 n/a .000 *****
00340 ***** SUM= 1.0 01:Pre 1.02 .021 No_date 1:22 5.62 n/a .000 *****
00341 ***** ROUTE CHANNEL -> 1.0 01:Pre 1.02 .021 No_date 1:22 5.62 n/a .000 *****
00342 ***** [RDT= 1.00] out <= 1.0 01:Pre 1.02 .021 No_date 1:22 5.62 n/a .000 *****
00343 ***** overflow <= 1.0 01:Pre 1.02 .021 No_date 1:22 5.62 n/a .000 *****
00344 ***** SUM= 1.0 01:Pre 1.02 .021 No_date 1:22 5.62 n/a .000 *****
00345 ***** [RDT= 1.00] out <= 1.0 01:R6 1.02 .013 No_date 1:30 5.64 n/a .000 *****
00346 ***** [L/S/N= 492.0;Tmax = 098] *****
00347 ***** R0002:CO0045 *****
00348 ***** ROUTE CHANNEL -> 1.0 01:Pre2.1 .44 .005 No_date 1:30 5.64 n/a .000 *****
00349 ***** [RDT= 1.00] out <= 1.0 01:R7 1.02 .013 No_date 1:34 5.64 n/a .000 *****
00350 ***** [L/S/N= 129.0 / 576 / 035] *****
00351 ***** (Vmax = 797.0;Tmax = 002) *****
00352 ***** R0002:CO0046 *****
00353 ***** ADD HYD 1.0 01:R6 1.02 .013 No_date 1:34 5.64 n/a .000 *****
00354 ***** out <= 1.0 01:EXT10 .81 .022 No_date 1:34 5.64 n/a .000 *****
00355 ***** overflow <= 1.0 01:EXT10 .00 .000 No_date 0:00 5.75 n/a .000 *****
00356 ***** SUM= 1.0 01:Pre 1.02 .021 No_date 1:30 5.75 n/a .000 *****
00357 ***** ROUTE CHANNEL -> 1.0 01:Pre 1.02 .021 No_date 1:30 5.75 n/a .000 *****
00358 ***** [RDT= 1.00] out <= 1.0 01:R8 1.02 .013 No_date 1:30 5.75 n/a .000 *****
00359 ***** [L/S/N= 79.0 / 522 / 035] *****
00360 ***** (Vmax = 423.0;Tmax = 016) *****
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Page 1

JFS Ainc.


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01081# Average monthly Potential Evapotranspiration in (mm)
01082# JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
01083# .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
01084# *****
01085# EXT1
01086# *****
01087# R0025:C00004-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01088# CALIB NASHYD 1.0 01:EXT1 3.21 .118 No_date 1:53 24.50 .421 .000
01089# [Cm 80.0: Nm 3.00: Tpe = .72]
01090# *****
01091# EXT2
01092# *****
01093# R0025:C00005-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01094# CALIB NASHYD 1.0 01:EXT2 .28 .022 No_date 1:22 29.15 .501 .000
01095# [Cm 80.0: Nm 3.00: Tpe = .33]
01096# *****
01097# EXT3
01098# *****
01099# R0025:C00006-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01100# CALIB NASHYD 1.0 01:EXT3 .56 .036 No_date 1:22 24.50 .421 .000
01101# [Cm 80.0: Nm 3.00: Tpe = .32]
01102# *****
01103# EXT4
01104# *****
01105# R0025:C00007-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01106# CALIB NASHYD 1.0 01:EXT4 .31 .020 No_date 1:20 23.69 .407 .000
01107# [Cm 79.0: Nm 3.00: Tpe = .29]
01108# *****
01109# EXT5
01110# *****
01111# R0025:C00008-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01112# CALIB NASHYD 1.0 01:EXT5 .59 .026 No_date 1:33 21.44 .368 .000
01113# [Cm 76.0: Nm 3.00: Tpe = .45]
01114# *****
01115# EXT6
01116# *****
01117# R0025:C00009-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01118# CALIB NASHYD 1.0 01:EXT6 .86 .046 No_date 1:40 29.15 .501 .000
01119# [Cm 85.0: Nm 3.00: Tpe = .56]
01120# *****
01121# EXT7
01122# *****
01123# R0025:C00010-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01124# CALIB NASHYD 1.0 01:EXT7 .47 .034 No_date 1:22 27.17 .467 .000
01125# [Cm 72.0: Nm 3.00: Tpe = .41]
01126# *****
01127# EXT8
01128# *****
01129# R0025:C00011-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01130# CALIB NASHYD 1.0 01:EXT8 .83 .043 No_date 1:30 23.69 .407 .000
01131# [Cm 79.0: Nm 3.00: Tpe = .42]
01132# *****
01133# EXT9
01134# *****
01135# R0025:C00012-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01136# CALIB NASHYD 1.0 01:EXT9 3.57 .151 No_date 1:35 21.44 .368 .000
01137# [Cm 79.0: Nm 3.00: Tpe = .48]
01138# *****
01139# EXT10
01140# *****
01141# R0025:C00013-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01142# CALIB NASHYD 1.0 01:EXT10 .01 .002 No_date 1:00 22.90 .393 .000
01143# [Cm 78.0: Nm 3.00: Tpe = .04]
01144# *****
01145# EXT11
01146# *****
01147# R0025:C00014-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01148# CALIB NASHYD 1.0 01:EXT11 .20 .008 No_date 1:31 18.23 .313 .000
01149# [Cm 71.0: Nm 3.00: Tpe = .42]
01150# *****
01151# Pres_1
01152# *****
01153# R0025:C00015-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01154# CALIB NASHYD 1.0 01:Pres_1 .01 .002 No_date 1:00 18.82 .323 .000
01155# [Cm 72.0: Nm 3.00: Tpe = .04]
01156# *****
01157# Pres_2
01158# *****
01159# R0025:C00016-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01160# CALIB NASHYD 1.0 01:Pres_2 .00 .000 No_date 1:00 22.97 .393 .000
01161# [Cm 78.0: Nm 3.00: Tpe = .02]
01162# *****
01163# Pres_3
01164# *****
01165# R0025:C00017-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01166# CALIB NASHYD 1.0 01:Pres_3 .44 .018 No_date 1:27 18.23 .313 .000
01167# [Cm 78.0: Nm 3.00: Tpe = .01]
01168# *****
01169# Pres_4
01170# *****
01171# R0025:C00018-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01172# CALIB NASHYD 1.0 01:Pres_4 .01 .001 No_date 1:00 12.46 .214 .000
01173# [Cm 59.0: Nm 3.00: Tpe = .03]
01174# *****
01175# Pres_5
01176# *****
01177# R0025:C00019-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01178# CALIB NASHYD 1.0 01:Pres_5 .80 .040 No_date 1:20 18.23 .313 .000
01179# [Cm 71.0: Nm 3.00: Tpe = .29]
01180# *****
01181# Pres_6
01182# *****
01183# R0025:C00020-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01184# CALIB NASHYD 1.0 01:Pres_6 .07 .005 No_date 1:13 22.90 .393 .000
01185# [Cm 78.0: Nm 3.00: Tpe = .01]
01186# *****
01187# Site 1
01188# *****
01189# R0025:C00021-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01190# DESIGN STANDHYD 1.0 01:Site-1 42 .092 No_date 1:00 34.53 .393 .000
01191# [Xfpe=34.7fpm=44]
01192# [SLP=1.00Dtn=1.00]
01193# [LOGS=1: HORTONS]
01194# *****
01195# Site 1 - Roof
01196# *****
01197# R0025:C00022-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01198# DESIGN STANDHYD 1.0 01:Site-Roof .06 .026 No_date 1:00 56.27 .966 .000
01199# [Xfpe=99.7fpm=99]
01200# [SLP=1.00Dtn=1.00]
01201# [LOGS=1: HORTONS]
01202# *****
01203# ROUTE RESERVOIR -> 1.0 01:Site-Roof .06 .026 No_date 1:00 56.27 n/a .000
01204# outflow <= 1.0 01:Site-Roof-Out .06 .003 No_date 1:30 56.27 n/a .000
01205# overflow <= 1.0 01:Site-Roof-Over .00 .000 No_date 0:00 .00 n/a .000
01206# [MetToUsed=2468E-02 m3, TotDurVol=0.000E+00 m3, N-Over= 0, TotDurOvr= 0 hrs]
01207# R0025:C00023-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01208# ADD HYD 1.0 01:Site-1 42 .092 No_date 1:00 34.53 n/a .000
01209# + 1.0 01:Site-Roof-Out .06 .003 No_date 1:30 56.27 n/a .000
01210# + 1.0 01:Site-Roof-Over .00 .000 No_date 0:00 .00 n/a .000
01211# SUM= 1.0 01:SITE1-IN 48 .094 No_date 1:00 37.47 n/a .000
01212# R0025:C00025-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01213# ROUTE RESERVOIR -> 1.0 01:SITE1-IN 48 .094 No_date 1:00 37.47 n/a .000
01214# outflow <= 1.0 01:SITE1-Out 48 .008 No_date 1:46 37.47 n/a .000
01215# overflow <= 1.0 01:SITE1-Over .00 .000 No_date 0:00 .00 n/a .000
01216# [MetToUsed=1128E-01 m3, TotDurVol=0.000E+00 m3, N-Over= 0, TotDurOvr= 0 hrs]
01217# *****
01218# Site 2
01219# *****
01220# R0025:C00026-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01221# DESIGN STANDHYD 1.0 01:Site-2 35 .076 No_date 1:00 33.45 .574 .000
01222# [Xfpe=31.7fpm=41]
01223# [SLP=1.00Dtn=1.00]
01224# [LOGS=1: HORTONS]
01225# *****
01226# Site 2 - Roof
01227# *****
01228# R0025:C00027-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01229# DESIGN STANDHYD 1.0 01:Site-Roof .09 .037 No_date 1:00 56.28 .967 .000
01230# [Xfpe=99.7fpm=99]
01231# [SLP=1.00Dtn=1.00]
01232# [LOGS=1: HORTONS]
01233# *****
01234# ROUTE RESERVOIR -> 1.0 01:Site-Roof .09 .037 No_date 1:00 56.28 n/a .000
01235# outflow <= 1.0 01:Site-Roof-Out .09 .008 No_date 1:11 56.29 n/a .000
01236# overflow <= 1.0 01:Site-Roof-Over .00 .000 No_date 0:00 .00 n/a .000
01237# [MetToUsed=2497E-02 m3, TotDurVol=0.000E+00 m3, N-Over= 0, TotDurOvr= 0 hrs]
01238# R0025:C00029-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01239# ADD HYD 1.0 01:SITE2-IN 45 .083 No_date 1:00 38.20 n/a .000
01240# + 1.0 01:SITE2-Out .00 .000 No_date 0:00 .00 n/a .000
01241# + 1.0 01:SITE2-Over .00 .000 No_date 0:00 .00 n/a .000
01242# SUM= 1.0 01:SITE2-IN 45 .083 No_date 1:00 38.20 n/a .000
01243# R0025:C00030-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01244# ROUTE RESERVOIR -> 1.0 01:SITE2-IN 45 .083 No_date 1:00 38.20 n/a .000
01245# outflow <= 1.0 01:SITE2-Out .00 .000 No_date 0:00 .00 n/a .000
01246# overflow <= 1.0 01:SITE2-Over .00 .000 No_date 0:00 .00 n/a .000
01247# [MetToUsed=1094E-01 m3, TotDurVol=0.000E+00 m3, N-Over= 0, TotDurOvr= 0 hrs]
01248# R0025:C00032-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01249# ADD HYD 1.0 01:SITE2-Out .00 .000 No_date 0:00 .00 n/a .000
01250# + 1.0 01:SITE2-Over .00 .000 No_date 0:00 .00 n/a .000
01251# + 1.0 01:SITE2-Over .00 .000 No_date 0:00 .00 n/a .000
01252# SUM= 1.0 01:SITE2-Over .00 .000 No_date 0:00 .00 n/a .000
01253# R0025:C00033-----DtnIn-ID:INHYD-----AREAhA-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01254# ADD HYD 1.0 01:SITE2-Out .00 .000 No_date 0:00 .00 n/a .000
01255# + 1.0 01:SITE2-Over .00 .000 No_date 0:00 .00 n/a .000
01256# + 1.0 01:SITE2-Over .00 .000 No_date 0:00 .00 n/a .000
01257# SUM= 1.0 01:SITE2-Out .00 .000 No_date 0:00 .00 n/a .000
01258# ADD HYD 1.0 01:SITE2-Out .00 .000 No_date 0:00 .00 n/a .000
01259# + 1.0 01:SITE2-Over .00 .000 No_date 0:00 .00 n/a .000
01260# + 1.0 01:SITE2-Over .00 .000 No_date 0:00 .00 n/a .000

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01441> CALIB NASHVD 1.0 01:EXT6 .86 .055 Mo_date 1:40 34.45 .532 .000
01442> [CN= 83.0: N= 3.00: Tpe= .42]
01443> *****
01444> # EXT7
01445> *****
01446> R0505/C00010-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01447> CALIB NASHVD 1.0 01:EXT8 .47 .041 Mo_date 1:21 32.24 .498 .000
01448> [CN= 83.0: N= 3.00: Tpe= .32]
01449> *****
01450> # EXT8
01451> *****
01452> R0505/C00011-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01453> CALIB NASHVD 1.0 01:EXT8 .83 .052 Mo_date 1:30 28.33 .437 .000
01454> [CN= 79.0: N= 3.00: Tpe= .42]
01455> *****
01456> # EXT9
01457> *****
01458> R0505/C00012-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01459> CALIB NASHVD 1.0 01:EXT9 3.57 .183 Mo_date 1:35 25.77 .398 .000
01460> [CN= 76.0: N= 3.00: Tpe= .42]
01461> *****
01462> # EXT9a
01463> *****
01464> R0505/C00013-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01465> CALIB NASHVD 1.0 01:EXT9a .01 .002 Mo_date 1:00 27.43 .423 .000
01466> [CN= 78.0: N= 3.00: Tpe= .04]
01467> *****
01468> # EXT10
01469> *****
01470> R0505/C00014-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01471> CALIB NASHVD 1.0 01:EXT10 .20 .010 Mo_date 1:30 22.06 .340 .000
01472> [CN= 72.0: N= 3.00: Tpe= .03]
01473> *****
01474> # Pre2_1
01475> *****
01476> R0505/C00015-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01477> CALIB NASHVD 1.0 01:Pre2_1 .01 .002 Mo_date 1:00 22.75 .351 .000
01478> [CN= 72.0: N= 3.00: Tpe= .03]
01479> *****
01480> # Pre2_2
01481> *****
01482> R0505/C00016-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01483> CALIB NASHVD 1.0 01:Pre2_2 .00 .000 Mo_date 1:00 27.40 .423 .000
01484> [CN= 78.0: N= 3.00: Tpe= .02]
01485> *****
01486> # Pre3_1
01487> *****
01488> R0505/C00017-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01489> CALIB NASHVD 1.0 01:Pre3_1 .44 .022 Mo_date 1:27 22.07 .340 .000
01490> [CN= 71.0: N= 3.00: Tpe= .03]
01491> *****
01492> # Pre3_2
01493> *****
01494> R0505/C00018-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01495> CALIB NASHVD 1.0 01:Pre3_2 .01 .002 Mo_date 1:00 25.27 .236 .000
01496> [CN= 59.0: N= 3.00: Tpe= .03]
01497> *****
01498> # Pre10_1
01499> *****
01500> R0505/C00019-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01501> CALIB NASHVD 1.0 01:Pre10_1 .80 .048 Mo_date 1:20 22.07 .340 .000
01502> [CN= 72.0: N= 3.00: Tpe= .03]
01503> *****
01504> # Pre1_1
01505> *****
01506> R0505/C00020-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01507> CALIB NASHVD 1.0 01:Pre1_1 .07 .006 Mo_date 1:13 27.44 .423 .000
01508> [CN= 78.0: N= 3.00: Tpe= .21]
01509> *****
01510> # Site 1
01511> *****
01512> R0505/C00021-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01513> DESIGN STANDHYD 1.0 01:Site-1 .42 .107 Mo_date 1:00 40.11 .619 .000
01514> [XMP= 34.7Tpe= .44]
01515> [SLP= 1.00DT= 1.00]
01516> [LOGSS= 1 : HORTONS]
01517> *****
01518> # Site 1 - Roof
01519> *****
01520> R0505/C00022-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01521> DESIGN STANDHYD 1.0 01:Site-Roof .06 .029 Mo_date 1:00 62.84 .970 .000
01522> [XMP= 99.7Tpe= .99]
01523> [SLP= .50DT= 1.00]
01524> [LOGSS= 1 : HORTONS]
01525> *****
01526> R0505/C00023-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01527> ROUTE RESERVOIR -> 1.0 01:Site-Roof .06 .029 Mo_date 1:00 62.84 n/a .000
01528> overflow <= 1.0 01:Site-Roof-Ov .00 .000 Mo_date 0:00 .00 n/a .000
01529> [MxTotDsed= 27576.02 n3, TotDvVol= .0000E+00 n3, N-Ovrf= 0, TotDvOvrf= 0 hrs]
01530> R0505/C00024-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01531> ADD HYD + 1.0 01:Site-Roof .42 .107 Mo_date 1:00 40.11 n/a .000
01532> + 1.0 01:Site-Roof-Ov .00 .000 Mo_date 1:00 62.84 n/a .000
01533> + 1.0 01:Site-Roof-Ov .00 .000 Mo_date 0:00 .00 n/a .000
01534> SUM= 1.0 01:SITE1-IN .48 .109 Mo_date 1:00 43.19 n/a .000
01535> R0505/C00025-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01536> ROUTE RESERVOIR -> 1.0 01:SITE1-IN .48 .109 Mo_date 1:00 43.19 n/a .000
01537> overflow <= 1.0 01:SITE1-Out .48 .109 Mo_date 1:00 43.19 n/a .000
01538> overflow <= 1.0 01:SITE1-Over .00 .000 Mo_date 0:00 .00 n/a .000
01539> [MxTotDsed= 13436.01 n3, TotDvVol= .0000E+00 n3, N-Ovrf= 0, TotDvOvrf= 0 hrs]
01540> *****
01541> # Site 2
01542> *****
01543> R0505/C00026-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01544> DESIGN STANDHYD 1.0 01:Site-2 .35 .088 Mo_date 1:00 38.93 .401 .000
01545> [XMP= 31.7Tpe= .41]
01546> [SLP= 1.00DT= 1.00]
01547> [LOGSS= 1 : HORTONS]
01548> *****
01549> # Site 2 - Roof
01550> *****
01551> R0505/C00027-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01552> DESIGN STANDHYD 1.0 01:Site-Roof .09 .041 Mo_date 1:00 62.84 .970 .000
01553> [XMP= 99.7Tpe= .99]
01554> [SLP= .50DT= 1.00]
01555> [LOGSS= 1 : HORTONS]
01556> *****
01557> R0505/C00028-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01558> ROUTE RESERVOIR -> 1.0 01:Site-Roof .09 .041 Mo_date 1:00 62.84 n/a .000
01559> overflow <= 1.0 01:Site-Roof-Ov .00 .000 Mo_date 1:11 62.85 n/a .000
01560> overflow <= 1.0 01:Site-Roof-Ov .00 .000 Mo_date 0:00 .00 n/a .000
01561> [MxTotDsed= 26836.02 n3, TotDvVol= .0000E+00 n3, N-Ovrf= 0, TotDvOvrf= 0 hrs]
01562> R0505/C00029-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01563> ADD HYD + 1.0 01:Site-Roof .35 .088 Mo_date 1:00 38.93 n/a .000
01564> + 1.0 01:Site-Roof-Ov .00 .000 Mo_date 1:11 62.85 n/a .000
01565> + 1.0 01:Site-Roof-Ov .00 .000 Mo_date 0:00 .00 n/a .000
01566> SUM= 1.0 01:SITE1-IN .45 .096 Mo_date 1:00 43.90 n/a .000
01567> R0505/C00030-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01568> ROUTE RESERVOIR -> 1.0 01:SITE1-IN .45 .096 Mo_date 1:00 43.90 n/a .000
01569> overflow <= 1.0 01:SITE1-Out .45 .096 Mo_date 2:05 43.90 n/a .000
01570> overflow <= 1.0 01:SITE1-Over .00 .000 Mo_date 0:00 .00 n/a .000
01571> [MxTotDsed= 12886.01 n3, TotDvVol= .0000E+00 n3, N-Ovrf= 0, TotDvOvrf= 0 hrs]
01572> R0505/C00031-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01573> ADD HYD + 1.0 01:SITE1-Out .48 .008 Mo_date 1:50 43.19 n/a .000
01574> + 1.0 01:SITE1-Over .00 .000 Mo_date 0:00 .00 n/a .000
01575> + 1.0 01:SITE1 .48 .008 Mo_date 1:50 43.19 n/a .000
01576> R0505/C00032-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01577> ADD HYD + 1.0 01:SITE1-Out .45 .009 Mo_date 2:05 43.90 n/a .000
01578> + 1.0 01:SITE1-Over .00 .000 Mo_date 0:00 .00 n/a .000
01579> SUM= 1.0 01:SITE2 .45 .009 Mo_date 2:05 43.90 n/a .000
01580> R0505/C00033-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01581> ADD HYD + 1.0 01:EXT7 .28 .026 Mo_date 1:22 34.45 n/a .000
01582> + 1.0 01:Pre2_1 .01 .002 Mo_date 1:00 22.75 n/a .000
01583> + 1.0 01:SITE1 .48 .008 Mo_date 1:50 43.19 n/a .000
01584> + 1.0 01:SITE2 .45 .009 Mo_date 2:05 43.90 n/a .000
01585> SUM= 1.0 01:21 .123 .043 Mo_date 1:22 41.20 n/a .000
01586> R0505/C00034-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01587> ROUTE CHANNEL -> 1.0 01:R1 1.23 .043 Mo_date 1:22 41.20 n/a .000
01588> [RD= 1.00] out<- 1.0 01:R1 1.23 .041 Mo_date 1:29 41.20 n/a .000
01589> [L/S= 143 / .394 / .035]
01590> *****
01591> R0505/C00035-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01592> ADD HYD + 1.0 01:21 1.23 .041 Mo_date 1:29 41.20 n/a .000
01593> + 1.0 01:EXT3 .56 .044 Mo_date 1:22 29.25 n/a .000
01594> + 1.0 01:EXT1 3.21 .142 Mo_date 1:53 29.25 n/a .000
01595> SUM= 1.0 01:22 5.00 .205 Mo_date 1:41 32.18 n/a .000
01596> R0505/C00036-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01597> ROUTE CHANNEL -> 1.0 01:23 5.31 .220 Mo_date 1:39 31.96 n/a .000
01598> [RD= 1.00] out<- 1.0 01:23 5.31 .219 Mo_date 1:43 31.96 n/a .000
01599> [L/S= 92 / .274 / .035]
01600> *****
01601> R0505/C00037-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01602> ADD HYD + 1.0 01:24 .31 .025 Mo_date 1:19 28.33 n/a .000
01603> + 1.0 01:EXT4 .31 .025 Mo_date 1:19 28.33 n/a .000
01604> SUM= 1.0 01:23 5.31 .220 Mo_date 1:39 31.96 n/a .000
01605> R0505/C00038-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01606> ROUTE CHANNEL -> 1.0 01:23 5.31 .220 Mo_date 1:39 31.96 n/a .000
01607> [RD= 1.00] out<- 1.0 01:23 5.31 .219 Mo_date 1:43 31.96 n/a .000
01608> [L/S= 92 / .274 / .035]
01609> *****
01610> R0505/C00039-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01611> ADD HYD + 1.0 01:23 5.31 .219 Mo_date 1:43 31.96 n/a .000
01612> + 1.0 01:24 .31 .025 Mo_date 1:19 28.33 n/a .000
01613> SUM= 1.0 01:24 5.90 .249 Mo_date 1:41 31.33 n/a .000
01614> R0505/C00040-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01615> ROUTE CHANNEL -> 1.0 01:24 5.90 .249 Mo_date 1:41 31.33 n/a .000
01616> [RD= 1.00] out<- 1.0 01:24 5.90 .236 Mo_date 1:52 31.33 n/a .000
01617> [L/S= 92 / .274 / .035]
01618> *****
01619> R0505/C00041-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01620> ADD HYD + 1.0 01:24 5.90 .236 Mo_date 1:52 31.33 n/a .000
01621> *****
01622> + 1.0 01:EXT6 .86 .055 Mo_date 1:40 34.45 n/a .000
01623> *****
01624> R0505/C00042-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01625> ROUTE CHANNEL -> 1.0 01:25 7.23 .312 Mo_date 1:46 31.76 n/a .000
01626> [RD= 1.00] out<- 1.0 01:R5 7.23 .308 Mo_date 1:53 31.76 n/a .000
01627> [L/S= 159 / .444 / .035]
01628> *****
01629> R0505/C00043-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01630> ADD HYD + 1.0 01:Pre10_1 .44 .022 Mo_date 1:27 22.07 n/a .000
01631> + 1.0 01:Pre2_1 .01 .002 Mo_date 1:00 22.75 n/a .000
01632> + 1.0 01:Pre3_1 .01 .002 Mo_date 1:00 22.75 n/a .000
01633> SUM= 1.0 01:Pre3_1 .01 .002 Mo_date 1:00 22.75 n/a .000
01634> R0505/C00044-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01635> ROUTE CHANNEL -> 1.0 01:Pre3_1 .01 .002 Mo_date 1:00 22.75 n/a .000
01636> [RD= 1.00] out<- 1.0 01:R6 1.02 .057 Mo_date 1:24 22.23 n/a .000
01637> [L/S= 159 / .444 / .035]
01638> *****
01639> R0505/C00045-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01640> ROUTE CHANNEL -> 1.0 01:R7 .44 .022 Mo_date 1:31 22.07 n/a .000
01641> [RD= 1.00] out<- 1.0 01:R7 .44 .022 Mo_date 1:31 22.07 n/a .000
01642> [L/S= 159 / .444 / .035]
01643> *****
01644> R0505/C00046-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01645> ADD HYD + 1.0 01:EXT10 .20 .010 Mo_date 1:30 22.06 n/a .000
01646> + 1.0 01:EXT10 .20 .010 Mo_date 1:30 22.06 n/a .000
01647> SUM= 1.0 01:EXT10 .20 .010 Mo_date 1:30 22.06 n/a .000
01648> R0505/C00047-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01649> ROUTE CHANNEL -> 1.0 01:26 1.02 .057 Mo_date 1:24 22.23 n/a .000
01650> [RD= 1.00] out<- 1.0 01:R8 1.02 .057 Mo_date 1:24 22.23 n/a .000
01651> [L/S= 79 / .522 / .035]
01652> *****
01653> R0505/C00048-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01654> ADD HYD + 1.0 01:R8 1.02 .057 Mo_date 1:27 22.23 n/a .000
01655> + 1.0 01:R8 .44 .030 Mo_date 1:50 22.47 n/a .000
01656> SUM= 1.0 01:27 1.46 .078 Mo_date 1:28 22.42 n/a .000
01657> R0505/C00049-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01658> ROUTE CHANNEL -> 1.0 01:27 1.46 .078 Mo_date 1:28 22.42 n/a .000
01659> [RD= 1.00] out<- 1.0 01:R9 1.46 .078 Mo_date 1:29 22.42 n/a .000
01660> [L/S= 23 / .877 / .035]
01661> *****
01662> R0505/C00050-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01663> ADD HYD + 1.0 01:EXT9 3.57 .183 Mo_date 1:35 25.77 n/a .000
01664> + 1.0 01:R9 1.46 .078 Mo_date 1:29 22.52 n/a .000
01665> + 1.0 01:R9 .44 .030 Mo_date 1:50 22.47 n/a .000
01666> SUM= 1.0 01:R9 7.23 .308 Mo_date 1:53 31.76 n/a .000
01667> *****
01668> R0505/C00051-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01669> ROUTE PIPE -> 1.0 01:R10 13.09 .584 Mo_date 1:42 28.88 n/a .000
01670> [RD= 1.00] out<- 1.0 01:Outlet 13.09 .585 Mo_date 1:42 28.88 n/a .000
01671> [L/S= 8 / .010 / .013]
01672> *****
01673> [Dine .53/Dosed= 1.40]
01674> #####
01675> *****
01676> *****
01677> *****
01678> *****
01679> *****
01680> *****
01681> *****
01682> *****
01683> *****
01684> *****
01685> RUN# / COMMAND#
01686> R099/C00001-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01687> START *****
01688> [ZERO = .00 hrs on 0]
01689> [NETOUT= 2 (1=imperial, 2=metric output)]
01690> [NETSUM= 1]
01691> [RUN= 0099]
01692> *****
01693> # SWHYNO / INPUT DATA FILE
01694> *****
01695> # STORM
01696> # Project Name : [S923 Ottawa St]
01697> # Project Number: [P2710(a01)]
01698> # Date : [2022 April 28]
01699> # Modeler : [JRM]
01700> # License # : [JFSa Canada Inc.]
01701> *****
01702> # Model developed from subcatchment to subcatchment development
01703> *****
01704> R099/C00002-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01705> HEAD STORM *****
01706> File name = STORM.001
01707> Comment = CH2CMM 100 Year 3 Hours
01708> [SDT=10.00SD= 3.00PTOT= 71.66]
01709> *****
01710> R099/C00003-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01711> DEFAULT VALUES *****
01712> File name = C:\Temp\20250910-PostDev\Ottawa_val
01713> ICASEDY = 1 (read and print data)
01714> FileTitle= File comment: (Parameters for City of Ottawa Projects)
01715> THE FOLLOWING PARAMETERS ARE USED IN THE DESIGN STANDHYD COM
01716> Horton's infiltration equation parameters:
01717> [Pw= 76.20 mm/hr] [IC= 4.14 /hr] [Fw= .00 mm]
01718> Parameters for Pervious surfaces in STANDHYD:
01719> [Iapex= 4.67 mm] [ISD= 40.00 mm] [Mw= .250]
01720> Parameters for IMPERVIOUS surfaces in STANDHYD:
01721> [Ialimp= 1.57 mm] [CL= 1.50] [Mw= .013]
01722> Parameters use HORTONS:
01723> [Ia= 4.67 mm] [W= 3.00]
01724> Average monthly Pan Evaporation data in (mm)
01725> JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
01726> .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
01727> Average monthly Precipitation in (mm)
01728> JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
01729> .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
01730> *****
01731> # EXT1
01732> *****
01733> R099/C00004-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01734> CALIB NASHVD 1.0 01:EXT1 3.21 .167 Mo_date 1:52 34.39 .480 .000
01735> [CN= 80.0: N= 3.00: Tpe= .21]
01736> *****
01737> # EXT2
01738> *****
01739> R099/C00005-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01740> CALIB NASHVD 1.0 01:EXT2 .40 .031 Mo_date 1:22 40.14 .560 .000
01741> [CN= 85.0: N= 3.00: Tpe= .33]
01742> *****
01743> # EXT3
01744> *****
01745> R099/C00006-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01746> CALIB NASHVD 1.0 01:EXT3 .56 .052 Mo_date 1:21 34.39 .480 .000
01747> [CN= 80.0: N= 3.00: Tpe= .21]
01748> *****
01749> # EXT4
01750> *****
01751> R099/C00007-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01752> CALIB NASHVD 1.0 01:EXT4 .31 .029 Mo_date 1:19 33.37 .466 .000
01753> [CN= 79.0: N= 3.00: Tpe= .29]
01754> *****
01755> # EXT5
01756> *****
01757> R099/C00008-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01758> CALIB NASHVD 1.0 01:EXT5 .59 .038 Mo_date 1:32 30.49 .425 .000
01759> [CN= 76.0: N= 3.00: Tpe= .45]
01760> *****
01761> # EXT6
01762> *****
01763> R099/C00009-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01764> CALIB NASHVD 1.0 01:EXT6 .86 .064 Mo_date 1:39 40.14 .560 .000
01765> [CN= 80.0: N= 3.00: Tpe= .21]
01766> *****
01767> # EXT7
01768> *****
01769> R099/C00010-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01770> CALIB NASHVD 1.0 01:EXT7 .40 .031 Mo_date 1:22 37.71 .526 .000
01771> [CN= 83.0: N= 3.00: Tpe= .32]
01772> *****
01773> # EXT8
01774> *****
01775> R099/C00011-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01776> CALIB NASHVD 1.0 01:EXT8 .83 .062 Mo_date 1:29 33.37 .466 .000
01777> [CN= 78.0: N= 3.00: Tpe= .42]
01778> *****
01779> # EXT9
01780> *****
01781> R099/C00012-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01782> CALIB NASHVD 1.0 01:EXT9 3.57 .218 Mo_date 1:34 30.49 .425 .000
01783> [CN= 76.0: N= 3.00: Tpe= .48]
01784> *****
01785> # EXT9a
01786> *****
01787> R099/C00013-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01788> CALIB NASHVD 1.0 01:EXT9a .01 .003 Mo_date 1:00 32.37 .452 .000
01789> [CN= 78.0: N= 3.00: Tpe= .04]
01790> *****
01791> # EXT10
01792> *****
01793> R099/C00014-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01794> CALIB NASHVD 1.0 01:EXT10 .20 .012 Mo_date 1:30 26.28 .367 .000
01795> [CN= 71.0: N= 3.00: Tpe= .02]
01796> *****
01797> # Pre_1
01798> *****
01799> R099/C00015-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeaDate_hh:mm-----RvM-R.C-----DWfMcs
01800> CALIB NASHVD 1.0 01:Pre_1 .01 .003 Mo_date 1:00 27.07 .378 .000
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[illegible]

Page 6

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028811 [L/S/m= 143./ .394/.035]
02882 (Vmax= .316;Dmax= .129)
02883 R0110:C00035 -----Dtn-ID-INHYD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02884 ADD HYD + 1.0 02:01 1.23 .036 No_date 12:21 43.37 n/a .000
02885 SUM= 1.0 02:01 1.23 .036 No_date 12:11 37.46 n/a .000
02886 + 1.0 02:EXT1 3.21 .121 No_date 12:40 36.46 n/a .000
02887 [L/S/m= 92./ .277/.035]
02888 R0110:C00036 -----Dtn-ID-INHYD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02889 ROUTE CHANNEL > 1.0 02:12 5.00 .178 No_date 12:29 38.15 n/a .000
02890 (RDT= 1.00) out<- 1.0 01:02 5.00 .177 No_date 12:31 38.15 n/a .000
02891 [L/S/m= 73./ .425/.035]
02892 (Vmax= .478;Dmax= .253)
02893 R0110:C00037 -----Dtn-ID-INHYD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02894 ADD HYD + 1.0 02:02 5.00 .177 No_date 12:31 38.15 n/a .000
02895 SUM= 1.0 02:EXT3 5.31 .190 No_date 12:13 37.99 n/a .000
02896 + 1.0 02:EXT4 5.31 .191 No_date 12:18 37.99 n/a .000
02897 R0110:C00038 -----Dtn-ID-INHYD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02898 ROUTE CHANNEL > 1.0 02:23 5.31 .191 No_date 12:28 37.99 n/a .000
02899 (RDT= 1.00) out<- 1.0 01:03 5.31 .190 No_date 12:31 37.99 n/a .000
02900 [L/S/m= 92./ .277/.035]
02901 (Vmax= .391;Dmax= .253)
02902 R0110:C00039 -----Dtn-ID-INHYD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02903 ADD HYD + 1.0 02:03 5.31 .190 No_date 12:31 37.99 n/a .000
02904 SUM= 1.0 02:EXT5 5.31 .190 No_date 12:22 32.39 n/a .000
02905 + 1.0 02:EXT6 5.90 .216 No_date 12:10 37.43 n/a .000
02906 R0110:C00040 -----Dtn-ID-INHYD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02907 ROUTE CHANNEL > 1.0 02:14 5.90 .216 No_date 12:30 37.43 n/a .000
02908 (RDT= 1.00) out<- 1.0 01:04 5.90 .204 No_date 12:40 37.43 n/a .000
02909 [L/S/m= 251./ .190/.035]
02910 (Vmax= .384;Dmax= .284)
02911 R0110:C00041 -----Dtn-ID-INHYD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02912 ADD HYD + 1.0 02:04 5.90 .204 No_date 12:40 37.43 n/a .000
02913 SUM= 1.0 02:EXT6 8.6 .046 No_date 12:29 42.40 n/a .000
02914 + 1.0 02:EXT7 7.23 .268 No_date 12:15 38.18 n/a .000
02915 R0110:C00042 -----Dtn-ID-INHYD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02916 ROUTE CHANNEL > 1.0 02:16 7.23 .268 No_date 12:15 38.18 n/a .000
02917 (RDT= 1.00) out<- 1.0 01:05 7.23 .264 No_date 12:41 38.18 n/a .000
02918 [L/S/m= 237./ .644/.035]
02919 (Vmax= .623;Dmax= .457)
02920 R0110:C00043 -----Dtn-ID-INHYD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02921 ADD HYD + 1.0 02:05 8.6 .043 No_date 12:11 38.00 n/a .000
02922 SUM= 1.0 02:Pre2_2 .01 .000 No_date 12:00 19.72 n/a .000
02923 + 1.0 02:Pre2_2 .01 .000 No_date 12:00 34.35 n/a .000
02924 R0110:C00044 -----Dtn-ID-INHYD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02925 ROUTE CHANNEL > 1.0 01:06 8.1 .043 No_date 12:11 37.87 n/a .000
02926 (RDT= 1.00) out<- 1.0 01:06 8.1 .043 No_date 12:14 37.87 n/a .000
02927 [L/S/m= 77./ .774/.035]
02928 (Vmax= .492;Dmax= .321)
02929 R0110:C00045 -----Dtn-ID-INHYD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02930 ADD HYD + 1.0 02:06 8.1 .043 No_date 12:14 37.87 n/a .000
02931 SUM= 1.0 02:EXT10 1.20 .008 No_date 12:20 27.99 n/a .000
02932 + 1.0 02:EXT10 1.02 .051 No_date 12:15 27.94 n/a .000
02933 R0110:C00046 -----Dtn-ID-INHYD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02934 ROUTE CHANNEL > 1.0 02:16 1.02 .051 No_date 12:15 27.94 n/a .000
02935 (RDT= 1.00) out<- 1.0 01:07 1.46 .069 No_date 12:10 28.00 n/a .000
02936 [L/S/m= 159./ .1574/.035]
02937 (Vmax= .791;Dmax= .535)
02938 R0110:C00047 -----Dtn-ID-INHYD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02939 ADD HYD + 1.0 02:07 1.20 .008 No_date 12:20 27.99 n/a .000
02940 SUM= 1.0 02:EXT10 1.02 .051 No_date 12:15 27.94 n/a .000
02941 R0110:C00048 -----Dtn-ID-INHYD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02942 ROUTE CHANNEL > 1.0 02:16 1.02 .051 No_date 12:15 27.94 n/a .000
02943 (RDT= 1.00) out<- 1.0 01:07 1.46 .069 No_date 12:10 28.00 n/a .000
02944 [L/S/m= 79./ .522/.035]
02945 (Vmax= .423;Dmax= .337)
02946 R0110:C00049 -----Dtn-ID-INHYD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02947 ADD HYD + 1.0 02:08 1.02 .050 No_date 12:18 27.97 n/a .000
02948 SUM= 1.0 02:EXT10 1.20 .008 No_date 12:20 27.99 n/a .000
02949 R0110:C00050 -----Dtn-ID-INHYD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02950 ROUTE CHANNEL > 1.0 02:16 1.02 .050 No_date 12:18 27.97 n/a .000
02951 (RDT= 1.00) out<- 1.0 01:08 1.46 .069 No_date 12:10 28.00 n/a .000
02952 [L/S/m= 29./ .887/.035]
02953 (Vmax= .543;Dmax= .447)
02954 R0110:C00051 -----Dtn-ID-INHYD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02955 ADD HYD + 1.0 02:09 1.46 .069 No_date 12:20 28.02 n/a .000
02956 SUM= 1.0 02:EXT5 5.31 .190 No_date 12:13 37.99 n/a .000
02957 + 1.0 02:EXT5 5.31 .190 No_date 12:18 37.99 n/a .000
02958 R0110:C00052 -----Dtn-ID-INHYD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02959 ROUTE CHANNEL > 1.0 02:18 13.09 .505 No_date 12:30 35.30 n/a .000
02960 (RDT= 1.00) out<- 1.0 01:08 13.09 .505 No_date 12:32 35.30 n/a .000
02961 [L/S/m= 9./ .010/.035]
02962 (Vmax= .419;Dmax= 1.085)
02963 R0110:C00053 -----Dtn-ID-INHYD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02964 ROUTE CHANNEL > 1.0 02:18 13.09 .505 No_date 12:30 35.30 n/a .000
02965 (RDT= 1.00) out<- 1.0 01:08 13.09 .505 No_date 12:32 35.30 n/a .000
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032411 [RDT= 1.00] out<- 1.0 01:R5 7.23 .338 No_date 12:13 48.09 n/a .000
03242 [L/S/N= 227./, 644./,035]
03243 (Vmax=.671;Dmax=.295)
03244 R0125:C00043-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03245 And HYD + 1.0 02:Pre1.1 .81 .056 No_date 12:11 36.35 n/a .000
03246 + 1.0 02:Pre2 .01 .002 No_date 12:00 26.12 n/a .000
03247 + 1.0 02:Pre3 .00 .000 No_date 12:00 43.92 n/a .000
03248 SUM= 1.0 01:Pre .81 .057 No_date 12:11 36.19 n/a .000
03249 R0125:C00044-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03250 ROUTE CHANNEL -> 1.0 01:Pre .81 .057 No_date 12:11 36.19 n/a .000
03251 [RDT= 1.00] out<- 1.0 01:R6 .81 .056 No_date 12:14 36.19 n/a .000
03252 [L/S/N= 159./,1157./,035]
03253 (Vmax=.492;Dmax=.041)
03254 R0125:C00045-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03255 ROUTE CHANNEL -> 1.0 01:Pre1.1 .44 .026 No_date 12:17 36.35 n/a .000
03256 [RDT= 1.00] out<- 1.0 01:R7 .44 .025 No_date 12:21 36.35 n/a .000
03257 [L/S/N= 159./,1157./,035]
03258 (Vmax=.797;Dmax=.008)
03259 R0125:C00046-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03260 And HYD + 1.0 02:EXT10 .20 .011 No_date 12:20 36.34 n/a .000
03261 + 1.0 02:EXT11 .02 .001 No_date 12:20 36.34 n/a .000
03262 SUM= 1.0 01:Pre .81 .056 No_date 12:15 36.27 n/a .000
03263 R0125:C00047-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03264 ROUTE CHANNEL -> 1.0 02:Pre .81 .056 No_date 12:15 36.27 n/a .000
03265 [RDT= 1.00] out<- 1.0 01:R8 .81 .056 No_date 12:18 36.27 n/a .000
03266 [L/S/N= 79./,522./,035]
03267 (Vmax=.423;Dmax=.049)
03268 R0125:C00048-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03269 ADD HYD + 1.0 02:EXT9 .357 .205 No_date 12:23 41.62 n/a .000
03270 + 1.0 02:EXT8 .1.02 .065 No_date 12:18 36.31 n/a .000
03271 + 1.0 02:EXT7 .44 .028 No_date 12:19 45.14 n/a .000
03272 SUM= 1.0 01:Pre .81 .057 No_date 12:19 36.34 n/a .000
03273 R0125:C00049-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03274 ROUTE CHANNEL -> 1.0 02:Pre .81 .057 No_date 12:19 36.34 n/a .000
03275 [RDT= 1.00] out<- 1.0 01:R9 .81 .057 No_date 12:19 36.34 n/a .000
03276 [L/S/N= 29./,887./,035]
03277 (Vmax=.543;Dmax=.061)
03278 R0125:C00050-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03279 ADD HYD + 1.0 02:EXT9 .3.57 .205 No_date 12:23 41.62 n/a .000
03280 + 1.0 02:EXT8 .1.02 .065 No_date 12:19 36.37 n/a .000
03281 + 1.0 02:EXT7 .7.23 .338 No_date 12:19 48.09 n/a .000
03282 SUM= 1.0 01:Pre .81 .056 No_date 12:19 36.34 n/a .000
03283 R0125:C00051-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03284 ROUTE PIPE -> 1.0 02:Pre .81 .056 No_date 12:29 44.84 n/a .000
03285 [RDT= 1.00] out<- 1.0 01:R10 .81 .056 No_date 12:31 44.84 n/a .000
03286 [L/S/N= 8./,010./,035]
03287 (Vmax=.437;Dmax=.049)
03288 (Dms=.53;Dused=1.44)
03289 #####
03290 # STORM
03291 #####
03292 ** END OF RUN : 149
03293
03294
03295
03296
03297
03298
03299
03300 R0125:COMMAND#
03301 R0125:C00001-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03302 START
03303 [TZERO = 0 hrs on 0]
03304 [METWOT= 2 (1=Imperial, 2=metric output)]
03305 [METWOM= 1]
03306 [NRUN = 0150]
03307
03308 # SWHYHYD / INPUT DATA FILE
03309
03310 # Project Name : [5923 Ottawa St]
03311 # Project Number: [92710(001)]
03312 # Date : [0225 April 28]
03313 # Modeler : [JFS]
03314 # Company : [OWA Canada Inc.]
03315 # License #: [254927]
03316 #####
03317 # Model developed to simulate the post development conditions
03318 #####
03319 R0125:C00002-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03320 READ STORM
03321
03322 # File name = STORM.001
03323 # [02 years SCS Type 2 Storm 24 Hours step 10 min, City of Ottawa]
03324 [SDT=10.00;SDRM= 24.00;PTOT= 96.53]
03325
03326 R0125:C00003-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03327 DEFAULT VALUES
03328 # File name = C:\Temp\20250910-PostDev\Ottawa.val
03329 # [CANEVD = 1 (read and print data)]
03330 # [FilterFile File comment: [Parameters for City of Ottawa Projects]]
03331 # [The following PARAMETERS ARE USED IN THE DESIGN STANDARHYD COM]
03332 # [Horizon's infiltration equation parameters:]
03333 # [F= 16.23 mm/hr; [F=13.20 mm/hr] [DOXY= 4.14 1/h; [F= .00 mm]]
03334 # [Parameters for FFWOVS surfaces in STANDHYD:]
03335 # [Iaxim= 4.67 mm] [LGR=40.00 m] [DHW= 2300]
03336 # [Parameters for FFWOVS surfaces in STANDHYD:]
03337 # [Iaxim= 1.57 mm] [CL=1.50] [DHW= .03]
03338 # [Parameters used in the model:]
03339 # [Ia= 4.67 mm] [N= 3.00]
03340 # [Average monthly Pan Evaporation data in (mm)]
03341 # [JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC]
03342 # [0.00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00]
03343 # [Average monthly Potential Transpiration (mm)]
03344 # [JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC]
03345 # [0.00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00]
03346 # [EXT1]
03347 #####
03348 R0125:C00004-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03349 CALIB NASHYD 1.0 01:EXT1 3.21 .182 No_date 12:40 54.31 .563 .000
03350 [Cm= 85.0; N= 3.00; Tpe= .33]
03351 # EXT1
03352 #####
03353 R0125:C00005-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03354 CALIB NASHYD 1.0 01:EXT2 .28 .033 No_date 12:13 61.73 .440 .000
03355 [Cm= 85.0; N= 3.00; Tpe= .33]
03356 # EXT2
03357 #####
03358 R0125:C00006-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03359 CALIB NASHYD 1.0 01:EXT3 .56 .057 No_date 12:13 54.31 .563 .000
03360 [Cm= 85.0; N= 3.00; Tpe= .33]
03361 # EXT3
03362 #####
03363 R0125:C00007-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03364 CALIB NASHYD 1.0 01:EXT4 .86 .068 No_date 12:28 61.73 .440 .000
03365 [Cm= 85.0; N= 3.00; Tpe= .33]
03366 # EXT4
03367 #####
03368 R0125:C00008-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03369 CALIB NASHYD 1.0 01:EXT5 .59 .042 No_date 12:21 49.04 .508 .000
03370 [Cm= 76.0; N= 3.00; Tpe= .45]
03371 # EXT5
03372 #####
03373 R0125:C00009-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03374 CALIB NASHYD 1.0 01:EXT6 .86 .068 No_date 12:28 61.73 .440 .000
03375 [Cm= 85.0; N= 3.00; Tpe= .33]
03376 # EXT6
03377 #####
03378 R0125:C00010-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03379 CALIB NASHYD 1.0 01:EXT7 .47 .052 No_date 12:12 58.44 .408 .000
03380 [Cm= 85.0; N= 3.00; Tpe= .33]
03381 # EXT7
03382 #####
03383 R0125:C00011-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03384 CALIB NASHYD 1.0 01:EXT8 .83 .068 No_date 12:19 52.94 .548 .000
03385 [Cm= 85.0; N= 3.00; Tpe= .33]
03386 # EXT8
03387 #####
03388 R0125:C00012-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03389 CALIB NASHYD 1.0 01:EXT9 .59 .042 No_date 12:21 49.04 .508 .000
03390 [Cm= 76.0; N= 3.00; Tpe= .45]
03391 # EXT9
03392 #####
03393 R0125:C00013-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03394 CALIB NASHYD 1.0 01:EXT10 .86 .068 No_date 12:28 61.73 .440 .000
03395 [Cm= 85.0; N= 3.00; Tpe= .33]
03396 # EXT10
03397 #####
03398 R0125:C00014-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03399 CALIB NASHYD 1.0 01:EXT11 .86 .068 No_date 12:28 61.73 .440 .000
03400 [Cm= 85.0; N= 3.00; Tpe= .33]
03401 # EXT11
03402 #####
03403 R0125:C00015-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03404 CALIB NASHYD 1.0 01:EXT12 .86 .068 No_date 12:28 61.73 .440 .000
03405 [Cm= 85.0; N= 3.00; Tpe= .33]
03406 # EXT12
03407 #####
03408 R0125:C00016-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03409 CALIB NASHYD 1.0 01:EXT13 .86 .068 No_date 12:28 61.73 .440 .000
03410 [Cm= 85.0; N= 3.00; Tpe= .33]
03411 # EXT13
03412 #####
03413 R0125:C00017-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03414 CALIB NASHYD 1.0 01:EXT14 .86 .068 No_date 12:28 61.73 .440 .000
03415 [Cm= 85.0; N= 3.00; Tpe= .33]
03416 # EXT14
03417 #####
03418 R0125:C00018-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03419 CALIB NASHYD 1.0 01:EXT15 .86 .068 No_date 12:28 61.73 .440 .000
03420 [Cm= 85.0; N= 3.00; Tpe= .33]
03421 # EXT15
03422 #####
03423 R0125:C00019-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03424 CALIB NASHYD 1.0 01:EXT16 .86 .068 No_date 12:28 61.73 .440 .000
03425 [Cm= 85.0; N= 3.00; Tpe= .33]
03426 # EXT16
03427 #####
03428 R0125:C00020-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03429 CALIB NASHYD 1.0 01:EXT17 .86 .068 No_date 12:28 61.73 .440 .000
03430 [Cm= 85.0; N= 3.00; Tpe= .33]
03431 # EXT17
03432 #####
03433 R0125:C00021-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03434 CALIB NASHYD 1.0 01:EXT18 .86 .068 No_date 12:28 61.73 .440 .000
03435 [Cm= 85.0; N= 3.00; Tpe= .33]
03436 # EXT18
03437 #####
03438 R0125:C00022-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03439 CALIB NASHYD 1.0 01:EXT19 .86 .068 No_date 12:28 61.73 .440 .000
03440 [Cm= 85.0; N= 3.00; Tpe= .33]
03441 # EXT19
03442 #####
03443 R0125:C00023-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03444 CALIB NASHYD 1.0 01:EXT20 .86 .068 No_date 12:28 61.73 .440 .000
03445 [Cm= 85.0; N= 3.00; Tpe= .33]
03446 # EXT20
03447 #####
03448 R0125:C00024-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03449 CALIB NASHYD 1.0 01:EXT21 .86 .068 No_date 12:28 61.73 .440 .000
03450 [Cm= 85.0; N= 3.00; Tpe= .33]
03451 # EXT21
03452 #####
03453 R0125:C00025-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03454 CALIB NASHYD 1.0 01:EXT22 .86 .068 No_date 12:28 61.73 .440 .000
03455 [Cm= 85.0; N= 3.00; Tpe= .33]
03456 # EXT22
03457 #####
03458 R0125:C00026-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03459 CALIB NASHYD 1.0 01:EXT23 .86 .068 No_date 12:28 61.73 .440 .000
03460 [Cm= 85.0; N= 3.00; Tpe= .33]
03461 # EXT23
03462 #####
03463 R0125:C00027-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03464 CALIB NASHYD 1.0 01:EXT24 .86 .068 No_date 12:28 61.73 .440 .000
03465 [Cm= 85.0; N= 3.00; Tpe= .33]
03466 # EXT24
03467 #####
03468 R0125:C00028-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03469 CALIB NASHYD 1.0 01:EXT25 .86 .068 No_date 12:28 61.73 .440 .000
03470 [Cm= 85.0; N= 3.00; Tpe= .33]
03471 # EXT25
03472 #####
03473 R0125:C00029-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03474 CALIB NASHYD 1.0 01:EXT26 .86 .068 No_date 12:28 61.73 .440 .000
03475 [Cm= 85.0; N= 3.00; Tpe= .33]
03476 # EXT26
03477 #####
03478 R0125:C00030-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03479 CALIB NASHYD 1.0 01:EXT27 .86 .068 No_date 12:28 61.73 .440 .000
03480 [Cm= 85.0; N= 3.00; Tpe= .33]
03481 # EXT27
03482 #####
03483 R0125:C00031-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03484 CALIB NASHYD 1.0 01:EXT28 .86 .068 No_date 12:28 61.73 .440 .000
03485 [Cm= 85.0; N= 3.00; Tpe= .33]
03486 # EXT28
03487 #####
03488 R0125:C00032-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03489 CALIB NASHYD 1.0 01:EXT29 .86 .068 No_date 12:28 61.73 .440 .000
03490 [Cm= 85.0; N= 3.00; Tpe= .33]
03491 # EXT29
03492 #####
03493 R0125:C00033-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03494 CALIB NASHYD 1.0 01:EXT30 .86 .068 No_date 12:28 61.73 .440 .000
03495 [Cm= 85.0; N= 3.00; Tpe= .33]
03496 # EXT30
03497 #####
03498 R0125:C00034-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03499 CALIB NASHYD 1.0 01:EXT31 .86 .068 No_date 12:28 61.73 .440 .000
03500 [Cm= 85.0; N= 3.00; Tpe= .33]
03501 # EXT31
03502 #####
03503 R0125:C00035-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03504 CALIB NASHYD 1.0 01:EXT32 .86 .068 No_date 12:28 61.73 .440 .000
03505 [Cm= 85.0; N= 3.00; Tpe= .33]
03506 # EXT32
03507 #####
03508 R0125:C00036-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03509 CALIB NASHYD 1.0 01:EXT33 .86 .068 No_date 12:28 61.73 .440 .000
03510 [Cm= 85.0; N= 3.00; Tpe= .33]
03511 # EXT33
03512 #####
03513 R0125:C00037-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03514 CALIB NASHYD 1.0 01:EXT34 .86 .068 No_date 12:28 61.73 .440 .000
03515 [Cm= 85.0; N= 3.00; Tpe= .33]
03516 # EXT34
03517 #####
03518 R0125:C00038-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03519 CALIB NASHYD 1.0 01:EXT35 .86 .068 No_date 12:28 61.73 .440 .000
03520 [Cm= 85.0; N= 3.00; Tpe= .33]
03521 # EXT35
03522 #####
03523 R0125:C00039-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03524 CALIB NASHYD 1.0 01:EXT36 .86 .068 No_date 12:28 61.73 .440 .000
03525 [Cm= 85.0; N= 3.00; Tpe= .33]
03526 # EXT36
03527 #####
03528 R0125:C00040-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03529 CALIB NASHYD 1.0 01:EXT37 .86 .068 No_date 12:28 61.73 .440 .000
03530 [Cm= 85.0; N= 3.00; Tpe= .33]
03531 # EXT37
03532 #####
03533 R0125:C00041-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03534 CALIB NASHYD 1.0 01:EXT38 .86 .068 No_date 12:28 61.73 .440 .000
03535 [Cm= 85.0; N= 3.00; Tpe= .33]
03536 # EXT38
03537 #####
03538 R0125:C00042-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03539 CALIB NASHYD 1.0 01:EXT39 .86 .068 No_date 12:28 61.73 .440 .000
03540 [Cm= 85.0; N= 3.00; Tpe= .33]
03541 # EXT39
03542 #####
03543 R0125:C00043-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03544 CALIB NASHYD 1.0 01:EXT40 .86 .068 No_date 12:28 61.73 .440 .000
03545 [Cm= 85.0; N= 3.00; Tpe= .33]
03546 # EXT40
03547 #####
03548 R0125:C00044-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03549 CALIB NASHYD 1.0 01:EXT41 .86 .068 No_date 12:28 61.73 .440 .000
03550 [Cm= 85.0; N= 3.00; Tpe= .33]
03551 # EXT41
03552 #####
03553 R0125:C00045-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03554 CALIB NASHYD 1.0 01:EXT42 .86 .068 No_date 12:28 61.73 .440 .000
03555 [Cm= 85.0; N= 3.00; Tpe= .33]
03556 # EXT42
03557 #####
03558 R0125:C00046-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03559 CALIB NASHYD 1.0 01:EXT43 .86 .068 No_date 12:28 61.73 .440 .000
03560 [Cm= 85.0; N= 3.00; Tpe= .33]
03561 # EXT43
03562 #####
03563 R0125:C00047-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03564 CALIB NASHYD 1.0 01:EXT44 .86 .068 No_date 12:28 61.73 .440 .000
03565 [Cm= 85.0; N= 3.00; Tpe= .33]
03566 # EXT44
03567 #####
03568 R0125:C00048-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03569 CALIB NASHYD 1.0 01:EXT45 .86 .068 No_date 12:28 61.73 .440 .000
03570 [Cm= 85.0; N= 3.00; Tpe= .33]
03571 # EXT45
03572 #####
03573 R0125:C00049-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03574 CALIB NASHYD 1.0 01:EXT46 .86 .068 No_date 12:28 61.73 .440 .000
03575 [Cm= 85.0; N= 3.00; Tpe= .33]
03576 # EXT46
03577 #####
03578 R0125:C00050-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03579 CALIB NASHYD 1.0 01:EXT47 .86 .068 No_date 12:28 61.73 .440 .000
03580 [Cm= 85.0; N= 3.00; Tpe= .33]
03581 # EXT47
03582 #####
03583 R0125:C00051-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03584 CALIB NASHYD 1.0 01:EXT48 .86 .068 No_date 12:28 61.73 .440 .000
03585 [Cm= 85.0; N= 3.00; Tpe= .33]
03586 # EXT48
03587 #####
03588 R0125:C00052-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03589 CALIB NASHYD 1.0 01:EXT49 .86 .068 No_date 12:28 61.73 .440 .000
03590 [Cm= 85.0; N= 3.00; Tpe= .33]
03591 # EXT49
03592 #####
03593 R0125:C00053-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03594 CALIB NASHYD 1.0 01:EXT50 .86 .068 No_date 12:28 61.73 .440 .000
03595 [Cm= 85.0; N= 3.00; Tpe= .33]
03596 # EXT50
03597 #####
03598 R0125:C00054-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03599 CALIB NASHYD 1.0 01:EXT51 .86 .068 No_date 12:28 61.73 .440 .000
03600 [Cm= 85.0; N= 3.00; Tpe= .33]
03601 # EXT51
03602 #####
03603 R0125:C00055-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03604 CALIB NASHYD 1.0 01:EXT52 .86 .068 No_date 12:28 61.73 .440 .000
03605 [Cm= 85.0; N= 3.00; Tpe= .33]
03606 # EXT52
03607 #####
03608 R0125:C00056-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03609 CALIB NASHYD 1.0 01:EXT53 .86 .068 No_date 12:28 61.73 .440 .000
03610 [Cm= 85.0; N= 3.00; Tpe= .33]
03611 # EXT53
03612 #####
03613 R0125:C00057-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03614 CALIB NASHYD 1.0 01:EXT54 .86 .068 No_date 12:28 61.73 .440 .000
03615 [Cm= 85.0; N= 3.00; Tpe= .33]
03616 # EXT54
03617 #####
03618 R0125:C00058-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03619 CALIB NASHYD 1.0 01:EXT55 .86 .068 No_date 12:28 61.73 .440 .000
03620 [Cm= 85.0; N= 3.00; Tpe= .33]
03621 # EXT55
03622 #####
03623 R0125:C00059-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03624 CALIB NASHYD 1.0 01:EXT56 .86 .068 No_date 12:28 61.73 .440 .000
03625 [Cm= 85.0; N= 3.00; Tpe= .33]
03626 # EXT56
03627 #####
03628 R0125:C00060-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03629 CALIB NASHYD 1.0 01:EXT57 .86 .068 No_date 12:28 61.73 .440 .000
03630 [Cm= 85.0; N= 3.00; Tpe= .33]
03631 # EXT57
03632 #####
03633 R0125:C00061-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03634 CALIB NASHYD 1.0 01:EXT58 .86 .068 No_date 12:28 61.73 .440 .000
03635 [Cm= 85.0; N= 3.00; Tpe= .33]
03636 # EXT58
03637 #####
03638 R0125:C00062-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03639 CALIB NASHYD 1.0 01:EXT59 .86 .068 No_date 12:28 61.73 .440 .000
03640 [Cm= 85.0; N= 3.00; Tpe= .33]
03641 # EXT59
03642 #####
03643 R0125:C00063-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03644 CALIB NASHYD 1.0 01:EXT60 .86 .068 No_date 12:28 61.73 .440 .000
03645 [Cm= 85.0; N= 3.00; Tpe= .33]
03646 # EXT60
03647 #####
03648 R0125:C00064-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03649 CALIB NASHYD 1.0 01:EXT61 .86 .068 No_date 12:28 61.73 .440 .000
03650 [Cm= 85.0; N= 3.00; Tpe= .33]
03651 # EXT61
03652 #####
03653 R0125:C00065-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03654 CALIB NASHYD 1.0 01:EXT62 .86 .068 No_date 12:28 61.73 .440 .000
03655 [Cm= 85.0; N= 3.00; Tpe= .33]
03656 # EXT62
03657 #####
03658 R0125:C00066-----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03659 CALIB NASHYD 1.0 01:EXT63 .86 .068 No_date 12:28 61
```

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036011 ADD HYD + 1.0 02:EXT9 3.57 .242 No_date 12:23 49.04 n/a .000
036022 + 1.0 02:EXT9 1.46 .107 No_date 12:19 43.15 n/a .000
036033 + 1.0 02:EXT8 .83 .068 No_date 12:19 52.94 n/a .000
036044 + 1.0 02:EXT8 .23 .396 No_date 12:38 55.95 n/a .000
036055 SUM= 1.0 01:EXT8 13.09 .776 No_date 12:28 52.45 n/a .000
036066 R0199:CO0001-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
036077 ROUTE RESERVOIR -> 1.0 01:EXT8 13.09 .776 No_date 12:28 52.45 n/a .000
036088 * (RDT=1.00) out<- 1.0 01:Outlet 13.09 .775 No_date 12:30 52.45 n/a .000
036099 [L/S/m= 87. /0107.035]
036100 (Vmax= 487.0Dmax= 1.275)
036111 Dln= 53.0Duse= 1.55)
036122 *****
036133 * STORMS
036144 *****
036155 ** END OF RUN = 198
036166 *****
036177 *****
036188 *****
036199 *****
036200 *****
036211 *****
036222 *****
036233 RUN:COMMAND#
036244 R0199:CO0001-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
036255 START
036266 (TZERO = .00 hrs on 0)
036277 (METOUT= 2 [Imperial, 2-metric output])
036288 (INSTORM= 1)
036299 (NRUN = 019)
036300 *****
036311 # SWHYMO / INPUT DATA FILE
036322 *****
036333 # Project Name : [5923 Ottawa St]
036344 # Project Number: [P2710(01)]
036355 # Date : [2025 April 28]
036366 # Modeller : [JFS]
036377 # Company : JFS Canada Inc.
036388 # License # : 2549237
036399 *****
036400 # Model developed to simulate runoff from subcatchments under post development conditions
036411 *****
036422 R0199:CO0001-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
036433 READ STORM
036444 Filename = STORM.001
036455 Comment = 100 Year SCS Type 2 Storm 24 Hours step 10 min, City of Ottawa
036466 (SDT=10.00:SDUR= 24.00:PDOT= 106.73)
036477 *****
036488 R0199:CO0003-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
036499 DEFAULT VALUES
036500 Filename = C:\Temp\20250910-PostDev\Ottawa.val
036511 ICAREV = 1 (read and print data)
036522 FileTitle File comment: [Parameters for City of Ottawa Projects]
036533 *****
036544 THE FOLLOWING PARAMETERS ARE USED IN THE DESIGN STANDARD COM
036555 R0199:CO0001-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
036566 [Fw= 76.20 mm/hr] [Fw1= 120 mm/hr] [DCAV= 4.14 /hr] [F= .00 mm]
036577 *****
036588 Parameters for Pervious surfaces in STANDARD:
036599 [Iapex= 4.67 mm] [Iap= 40.00 n/a] [DWT= .250]
036600 *****
036611 Parameters for IMPERVIOUS surfaces in STANDARD:
036622 [Iapex= 1.57 mm] [Iap= 1.50] [DWT= .013]
036633 *****
036644 Average monthly Pan Evaporation data in (mm)
036655 *****
036666 JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
036677 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
036688 *****
036699 Average monthly Potential Evapotranspiration in (mm)
036700 *****
036711 JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
036722 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
036733 *****
036744 JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
036755 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
036766 *****
036777 R0199:CO0004-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
036788 CALIB NASHYD 1.0 01:EXT4 3.21 .212 No_date 12:39 62.92 .589 .000
036799 [Cm= 80.0: N= 3.00: Tpe= .72]
036800 *****
036811 # EXT4
036822 *****
036833 R0199:CO0006-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
036844 CALIB NASHYD 1.0 01:EXT3 .56 .066 No_date 12:13 62.92 .589 .000
036855 [Cm= 78.0: N= 3.00: Tpe= .60]
036866 *****
036877 # EXT4
036888 *****
036899 R0199:CO0007-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
036900 CALIB NASHYD 1.0 01:EXT4 .31 .038 No_date 12:13 61.42 .474 .000
036911 [Cm= 79.0: N= 3.00: Tpe= .29]
036922 *****
036933 R0199:CO0008-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
036944 CALIB NASHYD 1.0 01:EXT5 .59 .049 No_date 12:21 57.15 .535 .000
036955 [Cm= 78.0: N= 3.00: Tpe= .60]
036966 *****
036977 # EXT6
036988 *****
036999 R0199:CO0009-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
037000 CALIB NASHYD 1.0 01:EXT4 .86 .078 No_date 12:28 70.92 .664 .000
037011 [Cm= 85.0: N= 3.00: Tpe= .56]
037022 *****
037033 # EXT7
037044 *****
037055 R0199:CO0010-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
037066 CALIB NASHYD 1.0 01:EXT7 .47 .060 No_date 12:12 67.60 .633 .000
037077 [Cm= 81.0: N= 3.00: Tpe= .32]
037088 *****
037099 R0199:CO0011-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
037100 CALIB NASHYD 1.0 01:EXT8 .83 .079 No_date 12:19 61.42 .576 .000
037111 [Cm= 78.0: N= 3.00: Tpe= .60]
037122 *****
037133 R0199:CO0012-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
037144 CALIB NASHYD 1.0 01:EXT8 .01 .003 No_date 12:00 59.96 .562 .000
037155 [Cm= 78.0: N= 3.00: Tpe= .60]
037166 *****
037177 # EXT9
037188 *****
037199 R0199:CO0013-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
037200 CALIB NASHYD 1.0 01:EXT8 3.57 .242 No_date 12:23 49.04 .576 .000
037211 [Cm= 76.0: N= 3.00: Tpe= .48]
037222 *****
037233 R0199:CO0014-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
037244 CALIB NASHYD 1.0 01:EXT9a .01 .003 No_date 12:00 59.96 .562 .000
037255 [Cm= 78.0: N= 3.00: Tpe= .60]
037266 *****
037277 # EXT10
037288 *****
037299 R0199:CO0015-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
037300 CALIB NASHYD 1.0 01:EXT10 .20 .016 No_date 12:19 50.61 .474 .000
037311 [Cm= 71.0: N= 3.00: Tpe= .42]
037322 *****
037333 # EXT11
037344 *****
037355 R0199:CO0016-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
037366 CALIB NASHYD 1.0 01:EXT11 .01 .003 No_date 12:00 51.86 .486 .000
037377 [Cm= 72.0: N= 3.00: Tpe= .03]
037388 *****
037399 R0199:CO0017-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
037400 CALIB NASHYD 1.0 01:EXT11 .80 .079 No_date 12:11 50.61 .474 .000
037411 [Cm= 71.0: N= 3.00: Tpe= .29]
037422 *****
037433 # EXT12
037444 *****
037455 R0199:CO0018-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
037466 CALIB NASHYD 1.0 01:EXT12 .00 .001 No_date 12:00 59.95 .562 .000
037477 [Cm= 78.0: N= 3.00: Tpe= .60]
037488 *****
037499 R0199:CO0019-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
037500 CALIB NASHYD 1.0 01:EXT12 .07 .010 No_date 12:06 59.96 .562 .000
037511 [Cm= 78.0: N= 3.00: Tpe= .21]
037522 *****
037533 # EXT13
037544 *****
037555 R0199:CO0020-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
037566 CALIB NASHYD 1.0 01:EXT13 .01 .002 No_date 12:00 37.39 .350 .000
037577 [Cm= 59.0: N= 3.00: Tpe= .04]
037588 *****
037599 R0199:CO0021-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
037600 CALIB NASHYD 1.0 01:EXT13 .80 .079 No_date 12:11 50.61 .474 .000
037611 [Cm= 71.0: N= 3.00: Tpe= .29]
037622 *****
037633 # EXT14
037644 *****
037655 R0199:CO0022-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
037666 CALIB NASHYD 1.0 01:EXT14 .01 .003 No_date 12:00 51.86 .486 .000
037677 [Cm= 72.0: N= 3.00: Tpe= .03]
037688 *****
037699 R0199:CO0023-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
037700 CALIB NASHYD 1.0 01:EXT14 .07 .010 No_date 12:06 59.96 .562 .000
037711 [Cm= 78.0: N= 3.00: Tpe= .21]
037722 *****
037733 # EXT15
037744 *****
037755 R0199:CO0024-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
037766 CALIB NASHYD 1.0 01:EXT15 .01 .002 No_date 12:00 37.39 .350 .000
037777 [Cm= 59.0: N= 3.00: Tpe= .04]
037788 *****
037799 R0199:CO0025-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
037800 CALIB NASHYD 1.0 01:EXT15 .80 .079 No_date 12:11 50.61 .474 .000
037811 [Cm= 71.0: N= 3.00: Tpe= .29]
037822 *****
037833 # EXT16
037844 *****
037855 R0199:CO0026-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
037866 CALIB NASHYD 1.0 01:EXT16 .01 .003 No_date 12:00 51.86 .486 .000
037877 [Cm= 72.0: N= 3.00: Tpe= .03]
037888 *****
037899 R0199:CO0027-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
037900 CALIB NASHYD 1.0 01:EXT16 .07 .010 No_date 12:06 59.96 .562 .000
037911 [Cm= 78.0: N= 3.00: Tpe= .21]
037922 *****
037933 # EXT17
037944 *****
037955 R0199:CO0028-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
037966 CALIB NASHYD 1.0 01:EXT17 .01 .002 No_date 12:00 37.39 .350 .000
037977 [Cm= 59.0: N= 3.00: Tpe= .04]
037988 *****
037999 R0199:CO0029-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
038000 CALIB NASHYD 1.0 01:EXT17 .80 .079 No_date 12:11 50.61 .474 .000
038011 [Cm= 71.0: N= 3.00: Tpe= .29]
038022 *****
038033 # EXT18
038044 *****
038055 R0199:CO0030-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
038066 CALIB NASHYD 1.0 01:EXT18 .01 .003 No_date 12:00 51.86 .486 .000
038077 [Cm= 72.0: N= 3.00: Tpe= .03]
038088 *****
038099 R0199:CO0031-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
038100 CALIB NASHYD 1.0 01:EXT18 .07 .010 No_date 12:06 59.96 .562 .000
038111 [Cm= 78.0: N= 3.00: Tpe= .21]
038122 *****
038133 # EXT19
038144 *****
038155 R0199:CO0032-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
038166 CALIB NASHYD 1.0 01:EXT19 .01 .002 No_date 12:00 37.39 .350 .000
038177 [Cm= 59.0: N= 3.00: Tpe= .04]
038188 *****
038199 R0199:CO0033-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
038200 CALIB NASHYD 1.0 01:EXT19 .80 .079 No_date 12:11 50.61 .474 .000
038211 [Cm= 71.0: N= 3.00: Tpe= .29]
038222 *****
038233 # EXT20
038244 *****
038255 R0199:CO0034-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
038266 CALIB NASHYD 1.0 01:EXT20 .01 .003 No_date 12:00 51.86 .486 .000
038277 [Cm= 72.0: N= 3.00: Tpe= .03]
038288 *****
038299 R0199:CO0035-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
038300 CALIB NASHYD 1.0 01:EXT20 .07 .010 No_date 12:06 59.96 .562 .000
038311 [Cm= 78.0: N= 3.00: Tpe= .21]
038322 *****
038333 # EXT21
038344 *****
038355 R0199:CO0036-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
038366 CALIB NASHYD 1.0 01:EXT21 .01 .002 No_date 12:00 37.39 .350 .000
038377 [Cm= 59.0: N= 3.00: Tpe= .04]
038388 *****
038399 R0199:CO0037-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
038400 CALIB NASHYD 1.0 01:EXT21 .80 .079 No_date 12:11 50.61 .474 .000
038411 [Cm= 71.0: N= 3.00: Tpe= .29]
038422 *****
038433 # EXT22
038444 *****
038455 R0199:CO0038-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
038466 CALIB NASHYD 1.0 01:EXT22 .01 .003 No_date 12:00 51.86 .486 .000
038477 [Cm= 72.0: N= 3.00: Tpe= .03]
038488 *****
038499 R0199:CO0039-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
038500 CALIB NASHYD 1.0 01:EXT22 .07 .010 No_date 12:06 59.96 .562 .000
038511 [Cm= 78.0: N= 3.00: Tpe= .21]
038522 *****
038533 # EXT23
038544 *****
038555 R0199:CO0040-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
038566 CALIB NASHYD 1.0 01:EXT23 .01 .002 No_date 12:00 37.39 .350 .000
038577 [Cm= 59.0: N= 3.00: Tpe= .04]
038588 *****
038599 R0199:CO0041-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
038600 CALIB NASHYD 1.0 01:EXT23 .80 .079 No_date 12:11 50.61 .474 .000
038611 [Cm= 71.0: N= 3.00: Tpe= .29]
038622 *****
038633 # EXT24
038644 *****
038655 R0199:CO0042-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
038666 CALIB NASHYD 1.0 01:EXT24 .01 .003 No_date 12:00 51.86 .486 .000
038677 [Cm= 72.0: N= 3.00: Tpe= .03]
038688 *****
038699 R0199:CO0043-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
038700 CALIB NASHYD 1.0 01:EXT24 .07 .010 No_date 12:06 59.96 .562 .000
038711 [Cm= 78.0: N= 3.00: Tpe= .21]
038722 *****
038733 # EXT25
038744 *****
038755 R0199:CO0044-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
038766 CALIB NASHYD 1.0 01:EXT25 .01 .002 No_date 12:00 37.39 .350 .000
038777 [Cm= 59.0: N= 3.00: Tpe= .04]
038788 *****
038799 R0199:CO0045-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
038800 CALIB NASHYD 1.0 01:EXT25 .80 .079 No_date 12:11 50.61 .474 .000
038811 [Cm= 71.0: N= 3.00: Tpe= .29]
038822 *****
038833 # EXT26
038844 *****
038855 R0199:CO0046-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
038866 CALIB NASHYD 1.0 01:EXT26 .01 .003 No_date 12:00 51.86 .486 .000
038877 [Cm= 72.0: N= 3.00: Tpe= .03]
038888 *****
038899 R0199:CO0047-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
038900 CALIB NASHYD 1.0 01:EXT26 .07 .010 No_date 12:06 59.96 .562 .000
038911 [Cm= 78.0: N= 3.00: Tpe= .21]
038922 *****
038933 # EXT27
038944 *****
038955 R0199:CO0048-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
038966 CALIB NASHYD 1.0 01:EXT27 .01 .002 No_date 12:00 37.39 .350 .000
038977 [Cm= 59.0: N= 3.00: Tpe= .04]
038988 *****
038999 R0199:CO0049-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
039000 CALIB NASHYD 1.0 01:EXT27 .80 .079 No_date 12:11 50.61 .474 .000
039011 [Cm= 71.0: N= 3.00: Tpe= .29]
039022 *****
039033 # EXT28
039044 *****
039055 R0199:CO0050-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
039066 CALIB NASHYD 1.0 01:EXT28 .01 .003 No_date 12:00 51.86 .486 .000
039077 [Cm= 72.0: N= 3.00: Tpe= .03]
039088 *****
039099 R0199:CO0051-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
039100 CALIB NASHYD 1.0 01:EXT28 .07 .010 No_date 12:06 59.96 .562 .000
039111 [Cm= 78.0: N= 3.00: Tpe= .21]
039122 *****
039133 # EXT29
039144 *****
039155 R0199:CO0052-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
039166 CALIB NASHYD 1.0 01:EXT29 .01 .002 No_date 12:00 37.39 .350 .000
039177 [Cm= 59.0: N= 3.00: Tpe= .04]
039188 *****
039199 R0199:CO0053-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
039200 CALIB NASHYD 1.0 01:EXT29 .80 .079 No_date 12:11 50.61 .474 .000
039211 [Cm= 71.0: N= 3.00: Tpe= .29]
039222 *****
039233 # EXT30
039244 *****
039255 R0199:CO0054-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
039266 CALIB NASHYD 1.0 01:EXT30 .01 .003 No_date 12:00 51.86 .486 .000
039277 [Cm= 72.0: N= 3.00: Tpe= .03]
039288 *****
039299 R0199:CO0055-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
039300 CALIB NASHYD 1.0 01:EXT30 .07 .010 No_date 12:06 59.96 .562 .000
039311 [Cm= 78.0: N= 3.00: Tpe= .21]
039322 *****
039333 # EXT31
039344 *****
039355 R0199:CO0056-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
039366 CALIB NASHYD 1.0 01:EXT31 .01 .002 No_date 12:00 37.39 .350 .000
039377 [Cm= 59.0: N= 3.00: Tpe= .04]
039388 *****
039399 R0199:CO0057-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
039400 CALIB NASHYD 1.0 01:EXT31 .80 .079 No_date 12:11 50.61 .474 .000
039411 [Cm= 71.0: N= 3.00: Tpe= .29]
039422 *****
039433 # EXT32
039444 *****
039455 R0199:CO0058-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
039466 CALIB NASHYD 1.0 01:EXT32 .01 .003 No_date 12:00 51.86 .486 .000
039477 [Cm= 72.0: N= 3.00: Tpe= .03]
039488 *****
039499 R0199:CO0059-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
039500 CALIB NASHYD 1.0 01:EXT32 .07 .010 No_date 12:06 59.96 .562 .000
039511 [Cm= 78.0: N= 3.00: Tpe= .21]
039522 *****
039533 # EXT33
039544 *****
039555 R0199:CO0060-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
039566 CALIB NASHYD 1.0 01:EXT33 .01 .002 No_date 12:00 37.39 .350 .000
039577 [Cm= 59.0: N= 3.00: Tpe= .04]
039588 *****
039599 R0199:CO0061-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
039600 CALIB NASHYD 1.0 01:EXT33 .80 .079 No_date 12:11 50.61 .474 .000
039611 [Cm= 71.0: N= 3.00: Tpe= .29]
039622 *****
039633 # EXT34
039644 *****
039655 R0199:CO0062-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
039666 CALIB NASHYD 1.0 01:EXT34 .01 .003 No_date 12:00 51.86 .486 .000
039677 [Cm= 72.0: N= 3.00: Tpe= .03]
039688 *****
039699 R0199:CO0063-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
039700 CALIB NASHYD 1.0 01:EXT34 .07 .010 No_date 12:06 59.96 .562 .000
039711 [Cm= 78.0: N= 3.00: Tpe= .21]
039722 *****
039733 # EXT35
039744 *****
039755 R0199:CO0064-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
039766 CALIB NASHYD 1.0 01:EXT35 .01 .002 No_date 12:00 37.39 .350 .000
039777 [Cm= 59.0: N= 3.00: Tpe= .04]
039788 *****
039799 R0199:CO0065-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
039800 CALIB NASHYD 1.0 01:EXT35 .80 .079 No_date 12:11 50.61 .474 .000
039811 [Cm= 71.0: N= 3.00: Tpe= .29]
039822 *****
039833 # EXT36
039844 *****
039855 R0199:CO0066-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
039866 CALIB NASHYD 1.0 01:EXT36 .01 .003 No_date 12:00 51.86 .486 .000
039877 [Cm= 72.0: N= 3.00: Tpe= .03]
039888 *****
039899 R0199:CO0067-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
039900 CALIB NASHYD 1.0 01:EXT36 .07 .010 No_date 12:06 59.96 .562 .000
039911 [Cm= 78.0: N= 3.00: Tpe= .21]
039922 *****
039933 # EXT37
039944 *****
039955 R0199:CO0068-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
039966 CALIB NASHYD 1.0 01:EXT37 .01 .002 No_date 12:00 37.39 .350 .000
039977 [Cm= 59.0: N= 3.00: Tpe= .04]
039988 *****
039999 R0199:CO0069-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
040000 CALIB NASHYD 1.0 01:EXT37 .80 .079 No_date 12:11 50.61 .474 .000
040011 [Cm= 71.0: N= 3.00: Tpe= .29]
040022 *****
040033 # EXT38
040044 *****
040055 R0199:CO0070-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
040066 CALIB NASHYD 1.0 01:EXT38 .01 .003 No_date 12:00 51.86 .486 .000
040077 [Cm= 72.0: N= 3.00: Tpe= .03]
040088 *****
040099 R0199:CO0071-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
040100 CALIB NASHYD 1.0 01:EXT38 .07 .010 No_date 12:06 59.96 .562 .000
040111 [Cm= 78.0: N= 3.00: Tpe= .21]
040122 *****
040133 # EXT39
040144 *****
040155 R0199:CO0072-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
040166 CALIB NASHYD 1.0 01:EXT39 .01 .002 No_date 12:00 37.39 .350 .000
040177 [Cm= 59.0: N= 3.00: Tpe= .04]
040188 *****
040199 R0199:CO0073-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
040200 CALIB NASHYD 1.0 01:EXT39 .80 .079 No_date 12:11 50.61 .474 .000
040211 [Cm= 71.0: N= 3.00: Tpe= .29]
040222 *****
040233 # EXT40
040244 *****
040255 R0199:CO0074-----Dtlm-ID:INVD-----AREAh-QFEARcm-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
040266 CALIB NASHYD 1.0 01:EXT40 .01 .003 No_date 12:00 51.86 .486 .000
0
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03961 # License # : 2549237
03962 #####
03963 # Model developed to simulate runoff from subcatchments under post development conditions
03964 #####
03965 R1979-C00002-----
03966 READ STORM
03967 Filename = STORM.001
03968 Comment = July 1st, 1979 Storm (3H) - Ottawa International Airport step 5 min
03969 [SDT= 5.00;SDRM= 3.00;PTOT= 83.99]
03970 #####
03971 R1979-C00003-----
03972 DEFAULT VALUES
03973 Filename = C:\Temp\20250910-PostDev\Ottawa.val
03974 ICASRDV = 1 (read and print data)
03975 FileTitle File comment: [Parameters for City of Ottawa Projects]
03976 THE FOLLOWING PARAMETERS ARE USED IN THE DESIGN STANDARD COM
03977 Horton's infiltration equation parameters:
03978 [Fw= 76.20 mm/hr] [Fw=13.20 mm/hr] [DCAV= 4.14 /hr] [Fw= .00 mm]
03979 Parameters for PERVIOUS surfaces in STANDHYD:
03980 [Iaper= 4.67 mm] [LGP=40.00 n] [MNP= .250]
03981 Parameters for IMPVIOUS surfaces in STANDHYD:
03982 [Iaper= 1.57 mm] [Cfil= 1.50] [DNI= .013]
03983 Parameters used in NASHDY:
03984 [Iaw= 4.67 mm] [N= 3.00]
03985 Average monthly Pan Evaporation data in (mm)
03986 JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
03987 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
03988 Average monthly Potential Evapotranspiration in (mm)
03989 JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
03990 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
03991 #####
03992 # EXT1
03993 #####
03994 R1979-C00004-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
03995 CALIB NASHDY 1.0 01:EXT1 3.21 .040 NoDate 2:16 44.05 .524 .000
03996 [Cw= 80.0; N= 3.00; Tpe= .72]
03997 #####
03998 # EXT2
03999 #####
04000 R1979-C00005-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04001 CALIB NASHDY 1.0 01:EXT2 .28 .039 NoDate 1:50 50.68 .603 .000
04002 [Cw= 80.0; N= 3.00; Tpe= .72]
04003 #####
04004 # EXT3
04005 #####
04006 R1979-C00006-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04007 CALIB NASHDY 1.0 01:EXT3 .56 .067 NoDate 1:50 44.05 .524 .000
04008 [Cw= 80.0; N= 3.00; Tpe= .32]
04009 #####
04010 # EXT4
04011 #####
04012 R1979-C00007-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04013 CALIB NASHDY 1.0 01:EXT4 .31 .038 NoDate 1:48 42.84 .510 .000
04014 [Cw= 79.0; N= 3.00; Tpe= .29]
04015 #####
04016 # EXT5
04017 #####
04018 R1979-C00008-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04019 CALIB NASHDY 1.0 01:EXT5 .59 .054 NoDate 2:01 39.44 .470 .000
04020 [Cw= 76.0; N= 3.00; Tpe= .40]
04021 #####
04022 # EXT6
04023 #####
04024 R1979-C00009-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04025 CALIB NASHDY 1.0 01:EXT6 .86 .088 NoDate 2:06 50.68 .603 .000
04026 [Cw= 85.0; N= 3.00; Tpe= .56]
04027 #####
04028 # EXT7
04029 #####
04030 R1979-C00010-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04031 CALIB NASHDY 1.0 01:EXT7 .47 .061 NoDate 1:49 47.90 .570 .000
04032 [Cw= 82.0; N= 3.00; Tpe= .40]
04033 #####
04034 # EXT8
04035 #####
04036 R1979-C00011-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04037 CALIB NASHDY 1.0 01:EXT8 .83 .085 NoDate 1:58 42.85 .510 .000
04038 [Cw= 79.0; N= 3.00; Tpe= .42]
04039 #####
04040 # EXT9
04041 #####
04042 R1979-C00012-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04043 CALIB NASHDY 1.0 01:EXT9 3.57 .311 NoDate 2:03 39.44 .470 .000
04044 [Cw= 76.0; N= 3.00; Tpe= .48]
04045 #####
04046 # EXT10
04047 #####
04048 R1979-C00013-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04049 CALIB NASHDY 1.0 01:EXT10 .01 .002 NoDate 1:30 41.67 .496 .000
04050 [Cw= 76.0; N= 3.00; Tpe= .04]
04051 #####
04052 # EXT10
04053 #####
04054 R1979-C00014-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04055 CALIB NASHDY 1.0 01:EXT10 .20 .017 NoDate 1:59 34.76 .409 .000
04056 [Cw= 71.0; N= 3.00; Tpe= .42]
04057 #####
04058 # Pre1_1
04059 #####
04060 R1979-C00015-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04061 CALIB NASHDY 1.0 01:Pre1_1 .01 .002 NoDate 1:30 35.32 .421 .000
04062 [Cw= 76.0; N= 3.00; Tpe= .04]
04063 #####
04064 # Pre1_2
04065 #####
04066 R1979-C00016-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04067 CALIB NASHDY 1.0 01:Pre1_2 .00 .000 NoDate 1:30 41.63 .496 .000
04068 [Cw= 78.0; N= 3.00; Tpe= .02]
04069 #####
04070 # Pre1_3
04071 #####
04072 R1979-C00017-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04073 CALIB NASHDY 1.0 01:Pre1_3 .44 .038 NoDate 1:55 34.37 .409 .000
04074 [Cw= 71.0; N= 3.00; Tpe= .38]
04075 #####
04076 # Pre1_4
04077 #####
04078 R1979-C00018-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04079 CALIB NASHDY 1.0 01:Pre1_4 .01 .002 NoDate 1:30 24.59 .293 .000
04080 [Cw= 59.0; N= 3.00; Tpe= .21]
04081 #####
04082 # Pre1_5
04083 #####
04084 R1979-C00019-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04085 CALIB NASHDY 1.0 01:Pre1_5 .00 .078 NoDate 1:48 34.37 .409 .000
04086 [Cw= 71.0; N= 3.00; Tpe= .29]
04087 #####
04088 # Pre1_6
04089 #####
04090 R1979-C00020-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04091 CALIB NASHDY 1.0 01:Pre1_6 .07 .009 NoDate 1:43 41.67 .496 .000
04092 [Cw= 76.0; N= 3.00; Tpe= .21]
04093 #####
04094 # Site 1
04095 #####
04096 R1979-C00021-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04097 DESIGN STANDHYD 1.0 01:Site1-81 .42 .088 NoDate 1:30 59.24 .705 .000
04098 [XMP= 34.71MP= 44]
04099 [SLP= 50.0DT= 1.00]
04100 [LOGS= 1 : HORTONS]
04101 #####
04102 # Site 1 - Roof
04103 #####
04104 R1979-C00022-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04105 DESIGN STANDHYD 1.0 01:Site1-81 .06 .019 NoDate 1:30 82.00 .976 .000
04106 [XMP= 99.71MP= 99]
04107 [SLP= 50.0DT= 1.00]
04108 [LOGS= 1 : HORTONS]
04109 #####
04110 R1979-C00023-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04111 ROUTE RESERVOIR -> 1.0 01:Site1-Roof .06 .004 NoDate 2:01 82.00 n/a .000
04112 out <= 1.0 01:Site1-Roof-Ov .06 .004 NoDate 2:01 82.00 n/a .000
04113 [MktToSsed= 3896E-02 m3, TotDurVol= 0.000E+00 m3, N-Ovrf= 0, TotDurOvrf= 0 hrs]
04114 R1979-C00024-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04115 ADD HYD + 1.0 01:Site1-Roof .42 .088 NoDate 1:30 59.24 n/a .000
04116 SUM= 1.0 01:Site1-IN 48 .004 NoDate 2:01 82.00 n/a .000
04117 1.0 01:SITE1-OUT 48 .013 NoDate 2:14 62.32 n/a .000
04118 1.0 01:SITE1-Over 48 .013 NoDate 2:14 62.32 n/a .000
04119 R1979-C00025-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04120 ROUTE RESERVOIR -> 1.0 01:SITE1-OUT 48 .013 NoDate 2:14 62.32 n/a .000
04121 out <= 1.0 01:SITE1-OUT 48 .013 NoDate 2:14 62.32 n/a .000
04122 overfill <= 1.0 01:SITE1-Over 48 .013 NoDate 2:14 62.32 n/a .000
04123 [MktToSsed= 2061E-01 m3, TotDurVol= 0.000E+00 m3, N-Ovrf= 0, TotDurOvrf= 0 hrs]
04124 #####
04125 # Site 2
04126 #####
04127 R1979-C00026-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04128 DESIGN STANDHYD 1.0 01:Site2-83 .35 .073 NoDate 1:30 58.02 .691 .000
04129 [XMP= 31.71MP= 41]
04130 [SLP= 50.0DT= 1.00]
04131 [LOGS= 1 : HORTONS]
04132 #####
04133 # Site 2 - Roof
04134 #####
04135 R1979-C00027-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04136 DESIGN STANDHYD 1.0 01:Site2-Roof .09 .027 NoDate 1:30 82.00 .976 .000
04137 [XMP= 50.0DT= 1.00]
04138 [SLP= 50.0DT= 1.00]
04139 [LOGS= 1 : HORTONS]
04140 #####
04141 R1979-C00028-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04142 ROUTE RESERVOIR -> 1.0 01:Site2-Roof .09 .027 NoDate 1:30 82.00 n/a .000
04143 out <= 1.0 01:Site2-Roof-Ov .09 .009 NoDate 1:43 82.00 n/a .000
04144 overfill <= 1.0 01:Site2-Over .09 .009 NoDate 1:43 82.00 n/a .000
04145 [MktToSsed= 3896E-02 m3, TotDurVol= 0.000E+00 m3, N-Ovrf= 0, TotDurOvrf= 0 hrs]
04146 R1979-C00029-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04147 ADD HYD + 1.0 01:Site2-Roof .48 .039 NoDate 1:50 50.68 n/a .000
04148 ADD HYD + 1.0 01:SITE1-Over .09 .009 NoDate 1:43 82.00 n/a .000
04149 SUM= 1.0 01:Site1 48 .013 NoDate 2:14 62.32 n/a .000
04150 1.0 01:SITE1-OUT 48 .013 NoDate 2:14 62.32 n/a .000
04151 R1979-C00030-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04152 ROUTE RESERVOIR -> 1.0 01:SITE1-OUT 48 .013 NoDate 2:14 62.32 n/a .000
04153 out <= 1.0 01:SITE1-OUT 48 .013 NoDate 2:14 62.32 n/a .000
04154 overfill <= 1.0 01:SITE1-Over 48 .013 NoDate 2:14 62.32 n/a .000
04155 [MktToSsed= 192E-01 m3, TotDurVol= 0.000E+00 m3, N-Ovrf= 0, TotDurOvrf= 0 hrs]
04156 R1979-C00031-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04157 ADD HYD + 1.0 01:SITE1-Over .48 .013 NoDate 2:14 62.32 n/a .000
04158 ADD HYD + 1.0 01:SITE1-Over .09 .009 NoDate 1:43 82.00 n/a .000
04159 SUM= 1.0 01:Site1 48 .013 NoDate 2:14 62.32 n/a .000
04160 1.0 01:SITE1-OUT 48 .013 NoDate 2:14 62.32 n/a .000
04161 R1979-C00032-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04162 ROUTE RESERVOIR -> 1.0 01:SITE1-OUT 48 .013 NoDate 2:14 62.32 n/a .000
04163 out <= 1.0 01:SITE1-OUT 48 .013 NoDate 2:14 62.32 n/a .000
04164 overfill <= 1.0 01:SITE1-Over 48 .013 NoDate 2:14 62.32 n/a .000
04165 [MktToSsed= 192E-01 m3, TotDurVol= 0.000E+00 m3, N-Ovrf= 0, TotDurOvrf= 0 hrs]
04166 R1979-C00033-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04167 ADD HYD + 1.0 01:SITE1-Over .48 .013 NoDate 2:14 62.32 n/a .000
04168 ADD HYD + 1.0 01:SITE1-Over .09 .009 NoDate 1:43 82.00 n/a .000
04169 SUM= 1.0 01:Site1 48 .013 NoDate 2:14 62.32 n/a .000
04170 1.0 01:SITE1-OUT 48 .013 NoDate 2:14 62.32 n/a .000
04171 R1979-C00034-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04172 ROUTE CHANNEL -> 1.0 01:J1 1.23 .060 NoDate 2:00 59.58 n/a .000
04173 [L/S/f= 143.7 / 394 / 035]
04174 [Vmax= 365;Dmax= 155]
04175 R1979-C00035-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04176 ADD HYD + 1.0 01:SITE1 1.23 .059 NoDate 2:04 59.58 n/a .000
04177 1.0 01:SITE1 1.23 .059 NoDate 2:04 59.58 n/a .000
04178 SUM= 1.0 01:SITE1 3.21 .240 NoDate 2:16 44.05 n/a .000
04179 1.0 01:SITE1 3.21 .240 NoDate 2:16 44.05 n/a .000
04180 R1979-C00036-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04181 ROUTE CHANNEL -> 1.0 01:J2 5.00 .345 NoDate 2:08 47.86 n/a .000
04182 [L/S/f= 82.7 / 474 / 035]
04183 [Vmax= 567;Dmax= 319]
04184 R1979-C00037-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04185 ADD HYD + 1.0 01:SITE1 5.31 .371 NoDate 2:10 47.57 n/a .000
04186 1.0 01:SITE1 5.31 .371 NoDate 2:10 47.57 n/a .000
04187 SUM= 1.0 01:SITE1 5.31 .371 NoDate 2:10 47.57 n/a .000
04188 1.0 01:SITE1 5.31 .371 NoDate 2:10 47.57 n/a .000
04189 R1979-C00038-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04190 ROUTE CHANNEL -> 1.0 01:J3 5.31 .369 NoDate 2:10 47.57 n/a .000
04191 [L/S/f= 82.7 / 474 / 035]
04192 [Vmax= 464;Dmax= 329]
04193 R1979-C00039-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04194 ADD HYD + 1.0 01:SITE1 5.31 .369 NoDate 2:10 47.57 n/a .000
04195 1.0 01:SITE1 5.31 .369 NoDate 2:10 47.57 n/a .000
04196 SUM= 1.0 01:SITE1 5.31 .369 NoDate 2:10 47.57 n/a .000
04197 1.0 01:SITE1 5.31 .369 NoDate 2:10 47.57 n/a .000
04198 R1979-C00040-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04199 ROUTE CHANNEL -> 1.0 01:J4 5.90 .404 NoDate 2:09 46.75 n/a .000
04200 [L/S/f= 251.7 / 190 / 035]
04201 [Vmax= 463;Dmax= 380]
04202 R1979-C00041-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04203 ADD HYD + 1.0 01:SITE1 5.90 .404 NoDate 2:15 46.75 n/a .000
04204 1.0 01:SITE1 5.90 .404 NoDate 2:15 46.75 n/a .000
04205 SUM= 1.0 01:SITE1 5.90 .404 NoDate 2:15 46.75 n/a .000
04206 1.0 01:SITE1 5.90 .404 NoDate 2:15 46.75 n/a .000
04207 R1979-C00042-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04208 ROUTE CHANNEL -> 1.0 01:J5 7.23 .530 NoDate 2:11 47.29 n/a .000
04209 [L/S/f= 237.7 / 644 / 035]
04210 [Vmax= 762;Dmax= 351]
04211 R1979-C00043-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04212 ADD HYD + 1.0 01:Pre1_1 .80 .078 NoDate 1:48 34.37 n/a .000
04213 1.0 01:Pre1_1 .80 .078 NoDate 1:48 34.37 n/a .000
04214 SUM= 1.0 01:Pre1_1 .80 .078 NoDate 1:48 34.37 n/a .000
04215 1.0 01:Pre1_1 .80 .078 NoDate 1:48 34.37 n/a .000
04216 R1979-C00044-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04217 ROUTE CHANNEL -> 1.0 01:Pre1_2 .00 .000 NoDate 1:30 41.63 n/a .000
04218 [L/S/f= 79.7 / 522 / 035]
04219 [Vmax= 443;Dmax= 241]
04220 R1979-C00045-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04221 ADD HYD + 1.0 01:Pre1_2 .44 .038 NoDate 1:55 34.37 n/a .000
04222 1.0 01:Pre1_2 .44 .038 NoDate 1:55 34.37 n/a .000
04223 SUM= 1.0 01:Pre1_2 .44 .038 NoDate 1:55 34.37 n/a .000
04224 1.0 01:Pre1_2 .44 .038 NoDate 1:55 34.37 n/a .000
04225 R1979-C00046-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04226 ADD HYD + 1.0 01:Pre1_3 .44 .038 NoDate 1:55 34.37 n/a .000
04227 1.0 01:Pre1_3 .44 .038 NoDate 1:55 34.37 n/a .000
04228 SUM= 1.0 01:Pre1_3 .44 .038 NoDate 1:55 34.37 n/a .000
04229 1.0 01:Pre1_3 .44 .038 NoDate 1:55 34.37 n/a .000
04230 R1979-C00047-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04231 ROUTE CHANNEL -> 1.0 01:Pre1_4 .01 .002 NoDate 1:30 41.67 .496 .000
04232 [L/S/f= 29.7 / 887 / 035]
04233 [Vmax= 543;Dmax= 284]
04234 R1979-C00048-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04235 ADD HYD + 1.0 01:Pre1_4 .44 .038 NoDate 1:55 34.37 n/a .000
04236 1.0 01:Pre1_4 .44 .038 NoDate 1:55 34.37 n/a .000
04237 SUM= 1.0 01:Pre1_4 .44 .038 NoDate 1:55 34.37 n/a .000
04238 1.0 01:Pre1_4 .44 .038 NoDate 1:55 34.37 n/a .000
04239 R1979-C00049-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04240 ROUTE CHANNEL -> 1.0 01:Pre1_5 .01 .002 NoDate 1:30 41.67 .496 .000
04241 [L/S/f= 29.7 / 887 / 035]
04242 [Vmax= 543;Dmax= 284]
04243 R1979-C00050-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04244 ADD HYD + 1.0 01:Pre1_5 .44 .038 NoDate 1:55 34.37 n/a .000
04245 1.0 01:Pre1_5 .44 .038 NoDate 1:55 34.37 n/a .000
04246 SUM= 1.0 01:Pre1_5 .44 .038 NoDate 1:55 34.37 n/a .000
04247 1.0 01:Pre1_5 .44 .038 NoDate 1:55 34.37 n/a .000
04248 R1979-C00051-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04249 ROUTE CHANNEL -> 1.0 01:Pre1_6 .07 .009 NoDate 1:43 41.67 .496 .000
04250 [L/S/f= 29.7 / 887 / 035]
04251 [Vmax= 543;Dmax= 284]
04252 R1979-C00052-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04253 ADD HYD + 1.0 01:Pre1_6 .44 .038 NoDate 1:55 34.37 n/a .000
04254 1.0 01:Pre1_6 .44 .038 NoDate 1:55 34.37 n/a .000
04255 SUM= 1.0 01:Pre1_6 .44 .038 NoDate 1:55 34.37 n/a .000
04256 1.0 01:Pre1_6 .44 .038 NoDate 1:55 34.37 n/a .000
04257 R1979-C00053-----DtnIn-ID:INVD-----AREAh-QFEARCs-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
04258 ROUTE CHANNEL -> 1.0 01:Pre1_7 .01 .002 NoDate 1:30 41.67 .496 .000
04259 [L/S/f= 29.7 / 887 / 035]
04260 [Vmax= 543;Dmax= 284]
04261 #####
04262 # STORMS
04263 #####
04264 # END OF RUN : 1987
04265 #####
04266 #####
04267 #####
04268 #####
04269 #####
04270 #####
04271 #####
04272 #####
04273 #####
04274 #####
04275 #####
04276 #####
04277 #####
04278 #####
04279 #####
04280 #####
04281 #####
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04306 #####
04307 #####
04308 #####
04309 #####
04310 #####
04311 #####
04312 #####
04313 #####
04314 #####
04315 #####
04316 #####
04317 #####
04318 #####
04319 #####
04320 #####
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04321# # EXT2
04322# *****
04323# R1988:C00005-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04324# CALIB NASHYD 1.0 01:EXT2 .28 .035 No_date 2:11 47.74 .592 .000
04325# [CN= 85.0: N= 3.00: Tpe=.33]
04326# *****
04327# # EXT3
04328# *****
04329# R1988:C00004-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04330# CALIB NASHYD 1.0 01:EXT3 .83 .06 .061 No_date 2:11 41.34 .513 .000
04331# [CN= 80.0: N= 3.00: Tpe=.32]
04332# *****
04333# # EXT4
04334# *****
04335# R1988:C00007-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04336# CALIB NASHYD 1.0 01:EXT4 .31 .035 No_date 2:10 40.18 .499 .000
04337# [CN= 79.0: N= 3.00: Tpe=.48]
04338# *****
04339# # EXT5
04340# *****
04341# R1988:C00008-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04342# CALIB NASHYD 1.0 01:EXT5 .59 .046 No_date 2:17 36.52 .458 .000
04343# [CN= 76.0: N= 3.00: Tpe=.45]
04344# *****
04345# # EXT6
04346# *****
04347# R1988:C00009-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04348# CALIB NASHYD 1.0 01:EXT6 .86 .074 No_date 2:21 47.74 .592 .000
04349# [CN= 85.0: N= 3.00: Tpe=.56]
04350# *****
04351# # EXT7
04352# *****
04353# R1988:C00010-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04354# CALIB NASHYD 1.0 01:EXT7 .47 .055 No_date 2:11 45.05 .559 .000
04355# [CN= 81.0: N= 3.00: Tpe=.48]
04356# *****
04357# # EXT8
04358# *****
04359# R1988:C00011-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04360# CALIB NASHYD 1.0 01:EXT8 .09 .074 No_date 2:10 39.04 .489 .000
04361# [CN= 79.0: N= 3.00: Tpe=.42]
04362# *****
04363# # EXT9
04364# *****
04365# R1988:C00012-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04366# CALIB NASHYD 1.0 01:EXT9 3.57 .266 No_date 2:18 36.92 .458 .000
04367# [CN= 76.0: N= 3.00: Tpe=.48]
04368# *****
04369# # EXT10
04370# *****
04371# R1988:C00013-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04372# CALIB NASHYD 1.0 01:EXT10 .01 .003 No_date 2:00 39.05 .485 .000
04373# [CN= 78.0: N= 3.00: Tpe=.04]
04374# *****
04375# # EXT10
04376# *****
04377# R1988:C00014-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04378# CALIB NASHYD 1.0 01:EXT10 .20 .014 No_date 2:16 32.08 .398 .000
04379# [CN= 71.0: N= 3.00: Tpe=.42]
04380# *****
04381# # Fre2_1
04382# *****
04383# R1988:C00015-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04384# CALIB NASHYD 1.0 01:Fre2_1 .01 .003 No_date 2:00 39.96 .409 .000
04385# [CN= 72.0: N= 3.00: Tpe=.01]
04386# *****
04387# # Fre2_2
04388# *****
04389# R1988:C00016-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04390# CALIB NASHYD 1.0 01:Fre2_2 .00 .001 No_date 2:00 39.04 .484 .000
04391# [CN= 78.0: N= 3.00: Tpe=.02]
04392# *****
04393# # Fre3_1
04394# *****
04395# R1988:C00017-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04396# CALIB NASHYD 1.0 01:Fre3_1 .44 .033 No_date 2:14 32.08 .398 .000
04397# [CN= 72.0: N= 3.00: Tpe=.48]
04398# *****
04399# # Fre3_2
04400# *****
04401# R1988:C00018-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04402# CALIB NASHYD 1.0 01:Fre3_2 .01 .003 No_date 2:00 32.83 .283 .000
04403# [CN= 59.0: N= 3.00: Tpe=.03]
04404# *****
04405# # Fre3_1
04406# *****
04407# R1988:C00019-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04408# CALIB NASHYD 1.0 01:Fre3_1 .80 .072 No_date 2:10 32.08 .398 .000
04409# [CN= 71.0: N= 3.00: Tpe=.29]
04410# *****
04411# # Fre3_1
04412# *****
04413# R1988:C00020-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04414# CALIB NASHYD 1.0 01:Fre3_1 .07 .009 No_date 2:06 39.06 .485 .000
04415# [CN= 78.0: N= 3.00: Tpe=.21]
04416# *****
04417# # Site 1
04418# *****
04419# R1988:C00021-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04420# DESIGN STANDYD 1.0 01:Site-1 42 .104 No_date 2:00 34.85 .481 .000
04421# [XMP=.34:TMP=.44]
04422# [SLP=.30:DT=.100]
04423# [LOGS= 1 : HORTONS]
04424# *****
04425# # Site 1 - Roof
04426# *****
04427# R1988:C00022-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04428# DESIGN STANDYD 1.0 01:Site-Roof .06 .028 No_date 2:00 78.59 .975 .000
04429# [XMP=.99:TMP=.99]
04430# [SLP=.100:DT=.100]
04431# [LOGS= 1 : HORTONS]
04432# *****
04433# R1988:C00023-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04434# ROUTE RESERVOIR -> 1.0 02:Site-Roof .06 .028 No_date 2:00 78.59 n/a .000
04435# outflow <= 1.0 02:Site-Roof-01 .06 .040 No_date 2:03 78.59 n/a .000
04436# overflow <= 1.0 02:Site-Roof-02 .00 .000 No_date 0:00 .00 n/a .000
04437# (MetToUsed=.3573E-02 n3, TotDurVol=.0000E+00 n3, N-Over= 0, TotDurOvr= 0 hrs)
04438# ADD HYD SUM= 1.0 02:Site-Roof .06 .040 No_date 2:00 54.85 n/a .000
04439# + 1.0 02:Site-Roof-01 .06 .040 No_date 2:03 78.59 n/a .000
04440# + 1.0 02:Site-Roof-02 .00 .000 No_date 0:00 .00 n/a .000
04441# 1.0 02:SITE1-IN .48 .108 No_date 2:00 58.06 n/a .000
04442# R1988:C00025-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04443# ROUTE RESERVOIR -> 1.0 02:SITE1-IN .48 .108 No_date 2:00 58.06 n/a .000
04444# outflow <= 1.0 02:SITE1-Over .48 .009 No_date 2:30 58.06 n/a .000
04445# overflow <= 1.0 02:SITE1-Over .00 .000 No_date 0:00 .00 n/a .000
04446# (MetToUsed=.1725E-01 n3, TotDurVol=.0000E+00 n3, N-Over= 0, TotDurOvr= 0 hrs)
04447# # Site 2
04448# *****
04449# R1988:C00026-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04450# DESIGN STANDYD 1.0 01:Site-2 35 .088 No_date 2:00 53.63 .665 .000
04451# [XMP=.41:TMP=.41]
04452# [SLP=.100:DT=.100]
04453# [LOGS= 1 : HORTONS]
04454# *****
04455# # Site 2 - Roof
04456# *****
04457# R1988:C00027-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04458# DESIGN STANDYD 1.0 01:Site-Roof .09 .040 No_date 2:00 78.59 .975 .000
04459# [XMP=.91:TMP=.99]
04460# [SLP=.50:DT=.100]
04461# [LOGS= 1 : HORTONS]
04462# *****
04463# *****
04464# R1988:C00028-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04465# ROUTE RESERVOIR -> 1.0 02:Site-Roof .09 .040 No_date 2:00 78.59 n/a .000
04466# outflow <= 1.0 02:Site-Roof-01 .09 .040 No_date 2:02 78.61 n/a .000
04467# overflow <= 1.0 02:Site-Roof-02 .00 .000 No_date 0:00 .00 n/a .000
04468# (MetToUsed=.3220E-02 n3, TotDurVol=.0000E+00 n3, N-Over= 0, TotDurOvr= 0 hrs)
04469# R1988:C00029-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04470# ADD HYD SUM= 1.0 02:Site-Roof .09 .040 No_date 2:00 58.83 n/a .000
04471# + 1.0 02:Site-Roof-01 .09 .040 No_date 2:02 78.61 n/a .000
04472# + 1.0 02:Site-Roof-02 .00 .000 No_date 0:00 .00 n/a .000
04473# 1.0 02:SITE2-IN .45 .096 No_date 2:00 58.83 n/a .000
04474# R1988:C00030-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04475# ROUTE RESERVOIR -> 1.0 02:SITE2-IN .45 .096 No_date 2:00 58.83 n/a .000
04476# outflow <= 1.0 02:SITE2-Over .45 .010 No_date 2:34 58.83 n/a .000
04477# overflow <= 1.0 02:SITE2-Over .00 .000 No_date 0:00 .00 n/a .000
04478# (MetToUsed=.1650E-01 n3, TotDurVol=.0000E+00 n3, N-Over= 0, TotDurOvr= 0 hrs)
04479# R1988:C00031-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04480# ADD HYD SUM= 1.0 02:SITE1-Over .48 .009 No_date 2:30 58.06 n/a .000
04481# + 1.0 02:SITE1-Over .00 .000 No_date 0:00 .00 n/a .000
04482# 1.0 02:SITE2-IN .45 .010 No_date 2:34 58.06 n/a .000
04483# R1988:C00032-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04484# ADD HYD SUM= 1.0 02:SITE2-Over .45 .010 No_date 2:34 58.83 n/a .000
04485# + 1.0 02:SITE2-Over .00 .000 No_date 0:00 .00 n/a .000
04486# 1.0 02:SITE2-IN .45 .010 No_date 2:34 58.83 n/a .000
04487# R1988:C00033-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04488# ADD HYD SUM= 1.0 02:EXT2 .28 .035 No_date 2:11 47.74 n/a .000
04489# + 1.0 02:Fre2_1 .01 .003 No_date 2:00 39.96 n/a .000
04490# + 1.0 02:SITE1-IN .48 .009 No_date 2:30 58.06 n/a .000
04491# + 1.0 02:SITE2-IN .45 .010 No_date 2:34 58.83 n/a .000
04492# 1.0 02:SITE2-Over .45 .010 No_date 2:34 58.83 n/a .000
04493# R1988:C00034-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04494# ROUTE CHANNEL -> 1.0 02:J1 1.23 .053 No_date 2:11 55.67 n/a .000
04495# (FV= 1.0: I= 0.1: S= 1.23 .051 No_date 2:15 55.67 n/a .000)
04496# [L/S/m= 143./ .394/.035]
04497# *****
04498# R1988:C00035-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04499# ADD HYD SUM= 1.0 02:R1 1.23 .051 No_date 2:15 55.67 n/a .000
04500# + 1.0 02:EXT3 .56 .061 No_date 2:11 41.34 n/a .000
04501# *****
04502# *****
04503# R1988:C00036-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04504# ROUTE CHANNEL -> 1.0 02:J2 5.00 .287 No_date 2:20 44.86 n/a .000
04505# (FV= 1.0: I= 0.1: S= 5.00 .286 No_date 2:22 44.86 n/a .000)
04506# [L/S/m= 73./ .425/.035]
04507# *****
04508# R1988:C00037-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04509# ADD HYD SUM= 1.0 02:R2 5.00 .286 No_date 2:22 44.86 n/a .000
04510# + 1.0 02:EXT4 .53 .035 No_date 2:10 40.18 n/a .000
04511# 1.0 01:J3 5.31 .313 No_date 2:20 44.58 n/a .000
04512# R1988:C00038-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04513# ROUTE CHANNEL -> 1.0 02:J3 5.31 .313 No_date 2:20 44.58 n/a .000
04514# (FV= 1.0: I= 0.1: S= 5.31 .309 No_date 2:22 44.58 n/a .000)
04515# [L/S/m= 82./ .274/.035]
04516# *****
04517# R1988:C00039-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04518# ADD HYD SUM= 1.0 02:R3 5.31 .309 No_date 2:22 44.58 n/a .000
04519# + 1.0 02:EXT5 .59 .046 No_date 2:17 36.92 n/a .000
04520# 1.0 01:J4 5.90 .354 No_date 2:21 43.81 n/a .000
04521# R1988:C00040-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04522# ROUTE CHANNEL -> 1.0 02:J4 5.90 .354 No_date 2:21 43.81 n/a .000
04523# (FV= 1.0: I= 0.1: S= 5.90 .332 No_date 2:29 43.81 n/a .000)
04524# [L/S/m= 251./ .196/.035]
04525# *****
04526# R1988:C00041-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04527# ADD HYD SUM= 1.0 02:R4 5.90 .332 No_date 2:29 43.81 n/a .000
04528# + 1.0 02:EXT6 .86 .074 No_date 2:21 47.74 n/a .000
04529# 1.0 02:EXT7 .47 .055 No_date 2:11 45.05 n/a .000
04530# 1.0 01:J5 7.23 .440 No_date 2:25 44.36 n/a .000
04531# R1988:C00042-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04532# ROUTE CHANNEL -> 1.0 02:J5 7.23 .440 No_date 2:25 44.36 n/a .000
04533# (FV= 1.0: I= 0.1: S= 7.23 .433 No_date 2:30 44.36 n/a .000)
04534# [L/S/m= 237./ .644/.035]
04535# *****
04536# R1988:C00043-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04537# ADD HYD SUM= 1.0 02:R5 7.23 .433 No_date 2:30 44.36 n/a .000
04538# + 1.0 02:Fre3_2 .01 .003 No_date 2:00 32.83 n/a .000
04539# + 1.0 02:Fre2_1 .00 .001 No_date 2:00 39.04 n/a .000
04540# 1.0 01:J6 7.23 .440 No_date 2:25 44.36 n/a .000
04541# R1988:C00044-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04542# ROUTE CHANNEL -> 1.0 02:J6 7.23 .440 No_date 2:25 44.36 n/a .000
04543# (FV= 1.0: I= 0.1: S= 7.23 .433 No_date 2:30 44.36 n/a .000)
04544# [L/S/m= 97./ .776/.035]
04545# *****
04546# R1988:C00045-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04547# ROUTE CHANNEL -> 1.0 02:J7 4.4 .033 No_date 2:17 32.08 n/a .000
04548# (FV= 1.0: I= 0.1: S= 4.4 .033 No_date 2:17 32.08 n/a .000)
04549# [L/S/m= 159./ .576/.035]
04550# *****
04551# R1988:C00046-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04552# ADD HYD SUM= 1.0 02:R6 4.4 .033 No_date 2:17 32.08 n/a .000
04553# + 1.0 02:EXT10 .20 .014 No_date 2:16 32.08 n/a .000
04554# 1.0 01:J7 4.4 .033 No_date 2:17 32.08 n/a .000
04555# R1988:C00047-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04556# ROUTE CHANNEL -> 1.0 02:J7 4.4 .033 No_date 2:17 32.08 n/a .000
04557# (FV= 1.0: I= 0.1: S= 4.4 .033 No_date 2:17 32.08 n/a .000)
04558# [L/S/m= 78./ .522/.035]
04559# *****
04560# R1988:C00048-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04561# ADD HYD SUM= 1.0 02:R7 4.4 .033 No_date 2:17 32.08 n/a .000
04562# + 1.0 02:EXT8 .14 .015 No_date 2:16 32.33 n/a .000
04563# 1.0 01:J8 4.4 .033 No_date 2:17 32.33 n/a .000
04564# R1988:C00049-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04565# ROUTE CHANNEL -> 1.0 02:J8 4.4 .033 No_date 2:17 32.33 n/a .000
04566# (FV= 1.0: I= 0.1: S= 4.4 .033 No_date 2:17 32.33 n/a .000)
04567# [L/S/m= 29./ .887/.035]
04568# *****
04569# R1988:C00050-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04570# ADD HYD SUM= 1.0 02:R8 4.4 .033 No_date 2:17 32.33 n/a .000
04571# + 1.0 02:R9 1.46 .115 No_date 2:17 32.43 n/a .000
04572# 1.0 01:J9 4.4 .033 No_date 2:17 32.43 n/a .000
04573# + 1.0 02:R5 7.23 .443 No_date 2:30 44.36 n/a .000
04574# 1.0 01:J8 4.4 .033 No_date 2:17 32.33 n/a .000
04575# R1988:C00051-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04576# ROUTE PIPE -> 1.0 02:R9 13.09 .857 No_date 2:22 40.74 n/a .000
04577# (FV= 1.0: I= 0.1: S= 13.09 .856 No_date 2:23 40.74 n/a .000)
04578# [L/S/m= 8./ .010/.013]
04579# *****
04580# *****
04581# *****
04582# *****
04583# *****
04584# *****
04585# *****
04586# *****
04587# *****
04588# *****
04589# *****
04590# *****
04591# *****
04592# *****
04593# R1988:C00001-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfms
04594# START *****
04595# (FV= 0.0: I= 0.0: S= 0.0 .000 No_date 0:00 0.00 n/a .000)
04596# (METOUT= 2 (Imperial, 2-metric output))
04597# (METIN= 1)
04598# (RUN= 1996)
04599# *****
04600# *****
04601# *****
04602# *****
04603# *****
04604# *****
04605# *****
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Page 13





JFSAinc.

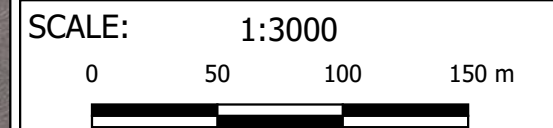
Attachment C

Hydraulic Analysis



Legend

-  Site Boundary
-  Jock River Tributary
-  Centerline
-  HEC-RAS XS



5923 Ottawa St – Richmond

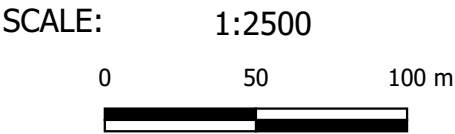
Figure C1: HEC-RAS Cross Sections

| | |
|---------|--------------|
| PROJECT | P2710(e01) |
| DRAWN | MM |
| DATE | 10 Sept 2025 |



Legend

- Site Boundary
- Pre-Development Flood Extents
 - 2YrSCS24Hr
 - 5YrSCS24Hr
 - 10YrSCS24Hr
 - 25YrSCS24Hr
 - 50YrSCS24Hr
 - 100YrSCS24Hr
- Spill Line



5923 Ottawa St - Richmond

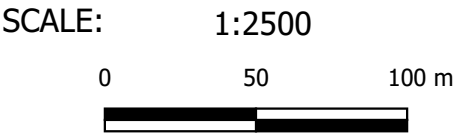
Figure C2: Pre-Development Flood Extents

| | |
|---------|-------------|
| PROJECT | P2719(e01) |
| DRAWN | BT |
| DATE | 5 June 2025 |



Legend

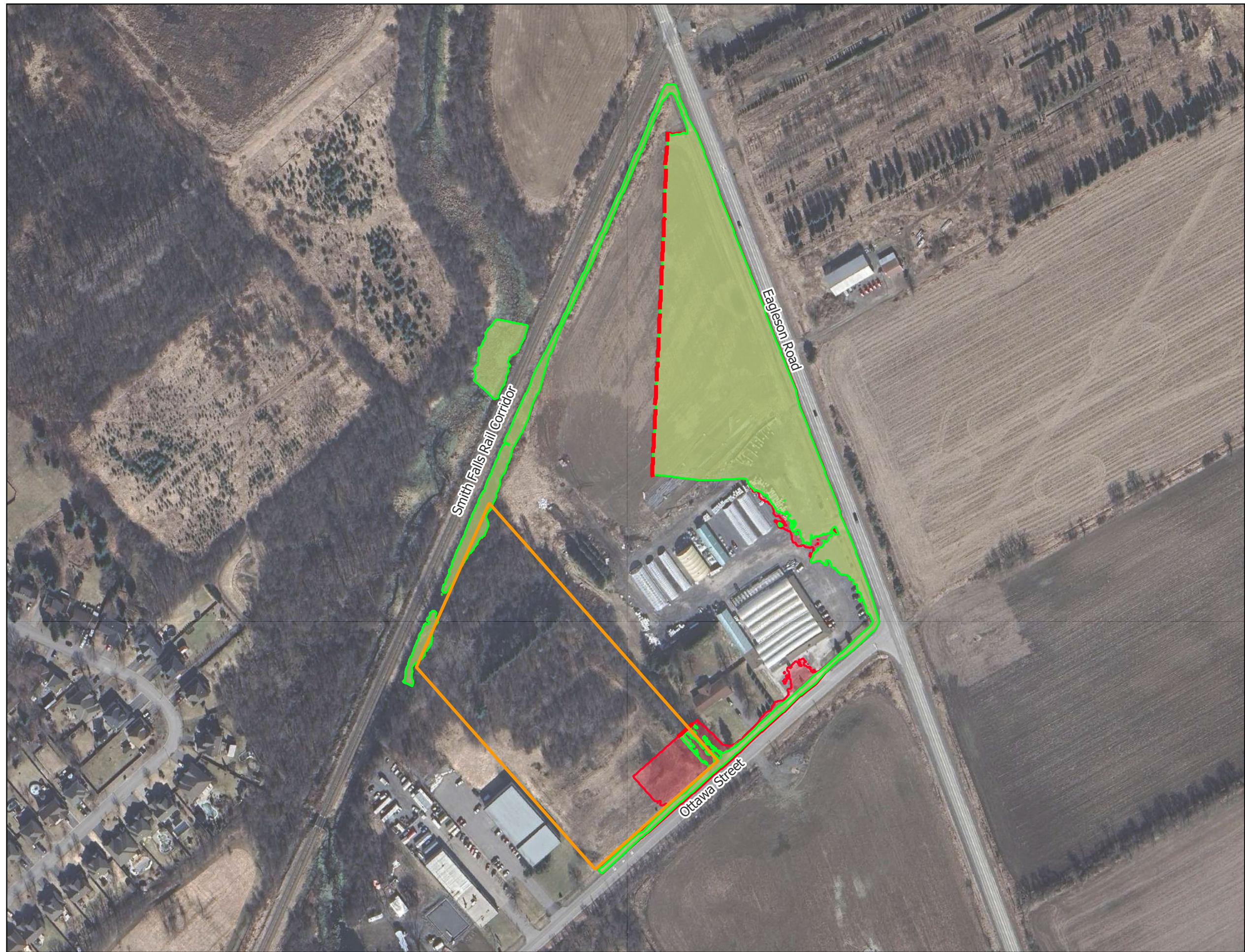
- Site Boundary
- Post-Development Flood Extents
 - 2YrSCS24Hr
 - 5YrSCS24Hr
 - 10YrSCS24Hr
 - 25YrSCS24Hr
 - 50YrSCS24Hr
 - 100YrSCS24Hr
- Spill Line







5923 Ottawa St - Richmond

Figure C3: Post-Development Flood Extents

| | |
|---------|--------------|
| PROJECT | P2719(e01) |
| DRAWN | BT |
| DATE | 10 Sept 2025 |




Legend

-  Site Boundary
-  Spill Line
-  Pre-Development 100yr
-  Post-Dev 100yr

SCALE: 1:2500

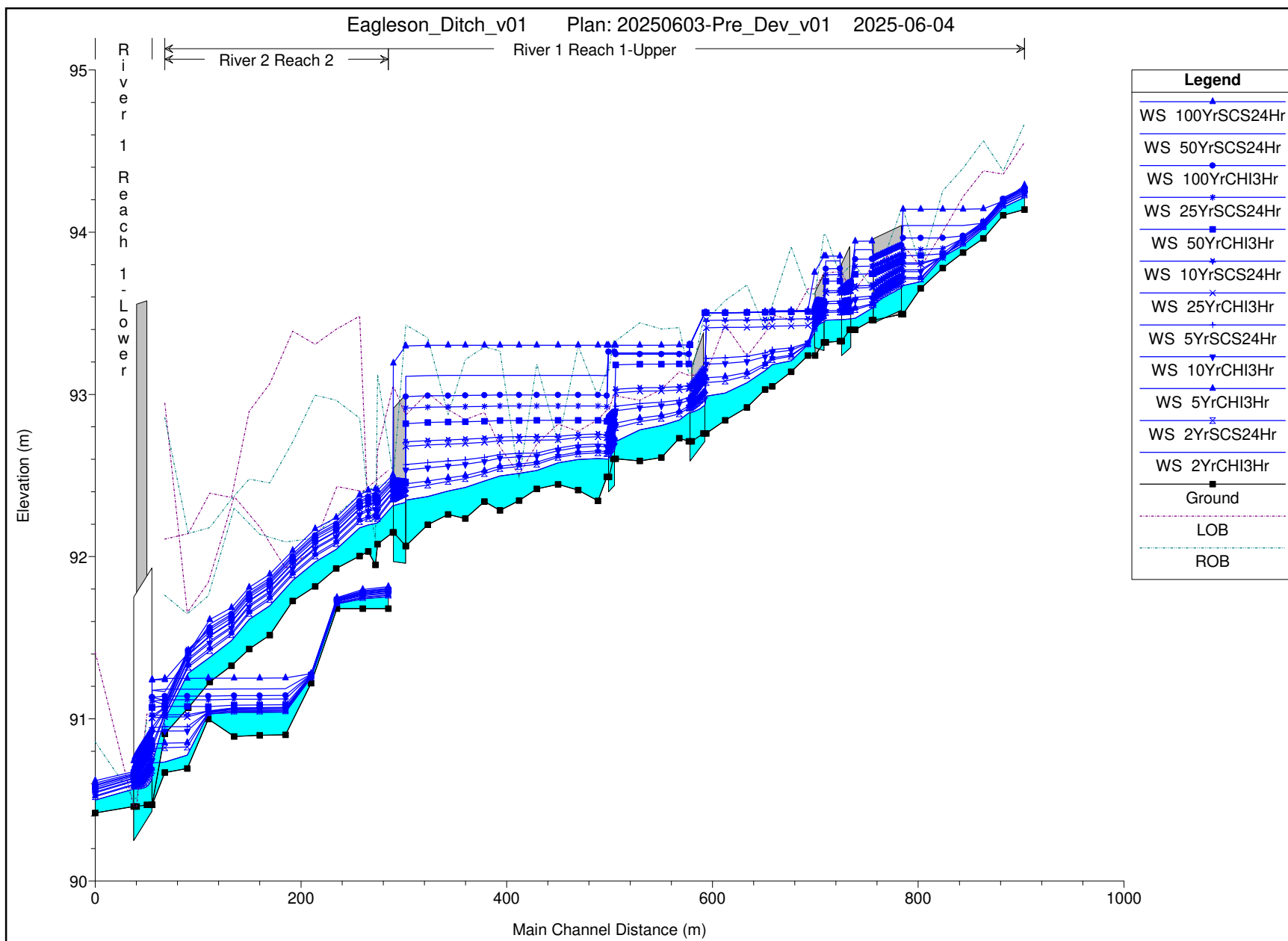
0 50 100 m

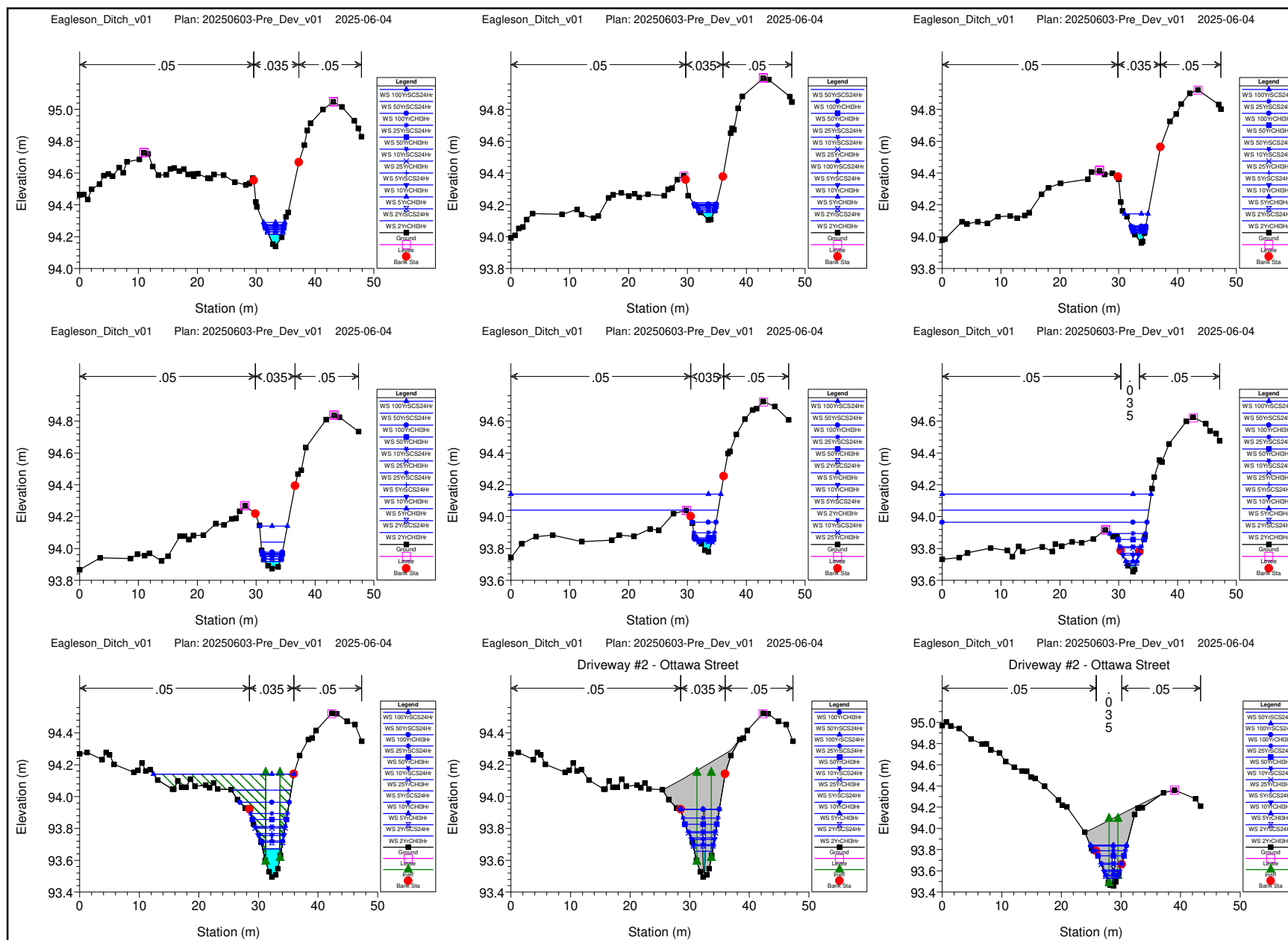


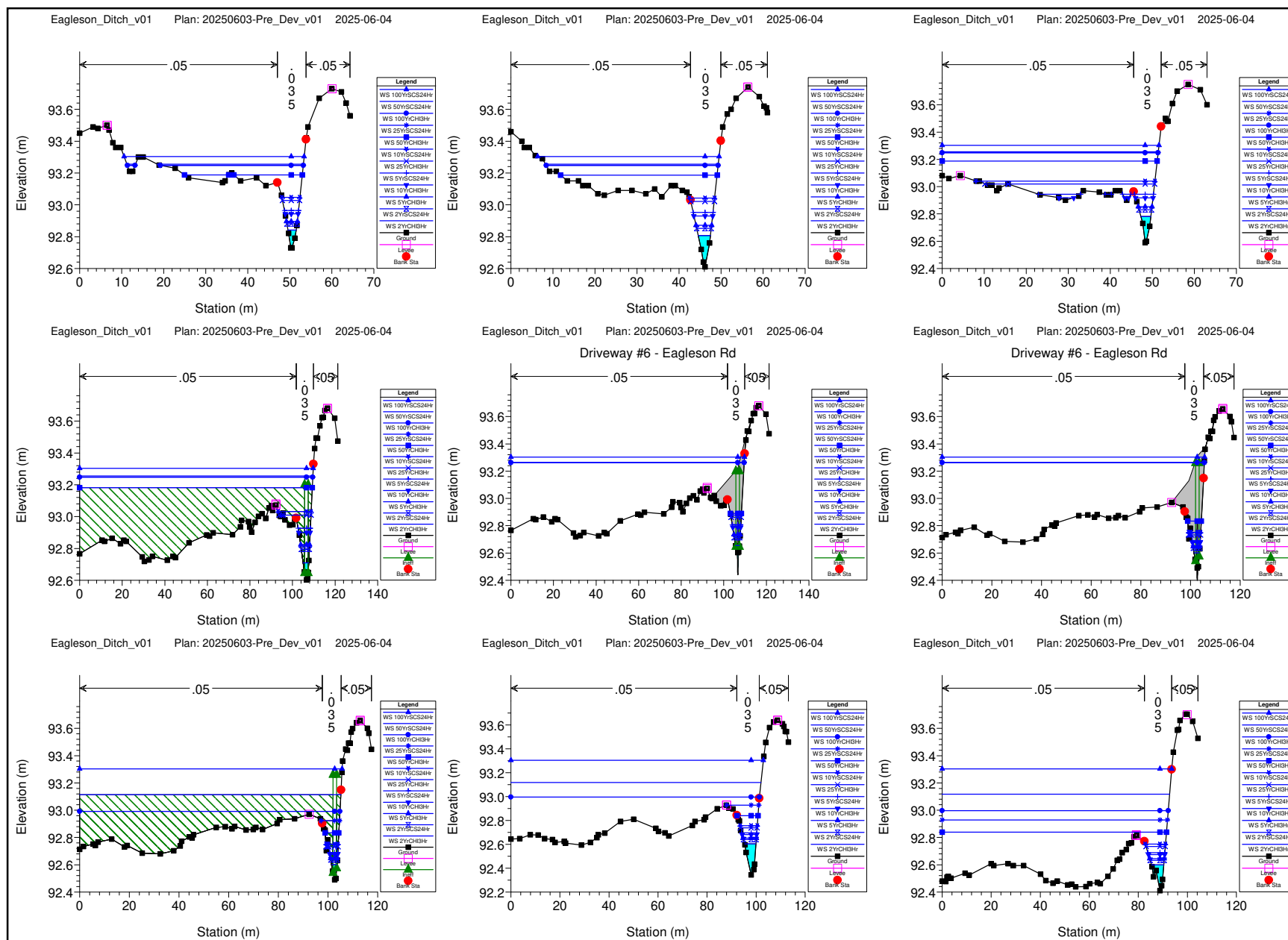
5923 Ottawa St - Richmond

Figure C4: 100-yr Floodplain Extents Comparison

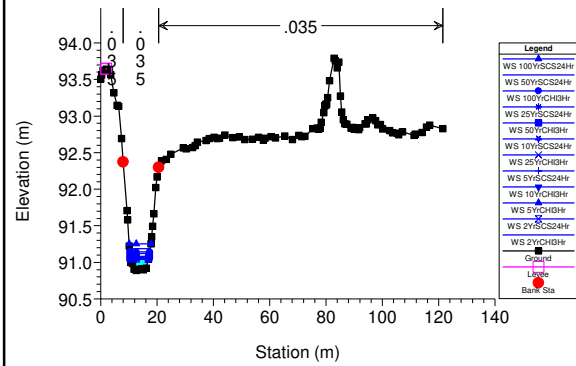
| | |
|---------|--------------|
| PROJECT | P2719(e01) |
| DRAWN | BT |
| DATE | 10 Sept 2025 |



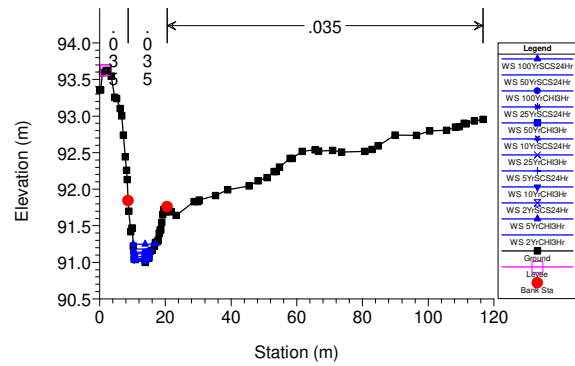




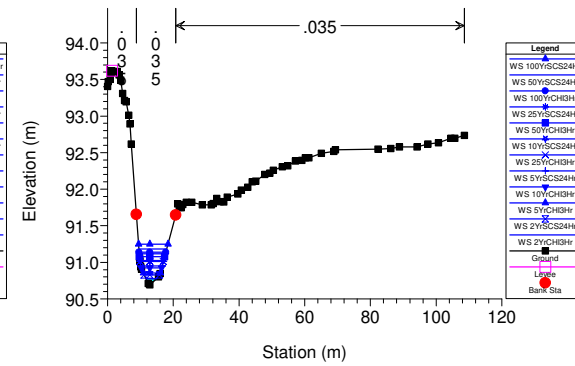
Eagleson_Ditch_v01 Plan: 20250603-Pre_Dev_v01 2025-06-04



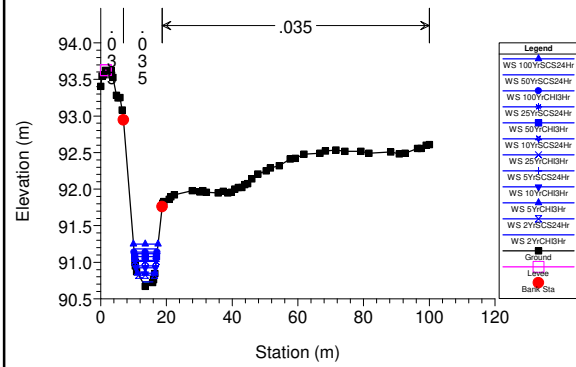
Eagleson_Ditch_v01 Plan: 20250603-Pre_Dev_v01 2025-06-04



Eagleson_Ditch_v01 Plan: 20250603-Pre_Dev_v01 2025-06-04



Eagleson_Ditch_v01 Plan: 20250603-Pre_Dev_v01 2025-06-04



| River | Reach | River Sta | Profile | Q Total (m3/s) | Min Ch El (m) | W.S. Elev (m) | Crit W.S. (m) | E.G. Elev (m) | E.G. Slope (m/m) | Vel Chnl (m/s) | Flow Area (m2) | Top Width (m) | Froude # Chl |
|---------|---------|-----------|--------------|-------------------|------------------|------------------|------------------|------------------|---------------------|-------------------|-------------------|------------------|--------------|
| River 2 | Reach 2 | 224 | 2YrCHI3Hr | 0.02 | 91.68 | 91.75 | 91.71 | 91.75 | 0.000626 | 0.08 | 0.20 | 5.09 | 0.13 |
| River 2 | Reach 2 | 224 | 5YrCHI3Hr | 0.03 | 91.68 | 91.76 | 91.72 | 91.76 | 0.000730 | 0.10 | 0.26 | 5.99 | 0.15 |
| River 2 | Reach 2 | 224 | 10YrCHI3Hr | 0.03 | 91.68 | 91.77 | 91.72 | 91.77 | 0.000742 | 0.11 | 0.32 | 6.48 | 0.15 |
| River 2 | Reach 2 | 224 | 25YrCHI3Hr | 0.05 | 91.68 | 91.78 | 91.73 | 91.79 | 0.000756 | 0.12 | 0.39 | 6.61 | 0.16 |
| River 2 | Reach 2 | 224 | 50YrCHI3Hr | 0.06 | 91.68 | 91.79 | 91.73 | 91.79 | 0.000763 | 0.13 | 0.44 | 6.71 | 0.16 |
| River 2 | Reach 2 | 224 | 100YrCHI3Hr | 0.07 | 91.68 | 91.80 | 91.74 | 91.80 | 0.000773 | 0.14 | 0.50 | 6.81 | 0.16 |
| River 2 | Reach 2 | 224 | 2YrSCS24Hr | 0.02 | 91.68 | 91.76 | 91.72 | 91.76 | 0.000717 | 0.09 | 0.25 | 5.79 | 0.14 |
| River 2 | Reach 2 | 224 | 5YrSCS24Hr | 0.04 | 91.68 | 91.78 | 91.73 | 91.78 | 0.000753 | 0.11 | 0.35 | 6.53 | 0.15 |
| River 2 | Reach 2 | 224 | 10YrSCS24Hr | 0.05 | 91.68 | 91.79 | 91.73 | 91.79 | 0.000757 | 0.12 | 0.41 | 6.65 | 0.16 |
| River 2 | Reach 2 | 224 | 25YrSCS24Hr | 0.07 | 91.68 | 91.80 | 91.74 | 91.80 | 0.000769 | 0.14 | 0.48 | 6.78 | 0.16 |
| River 2 | Reach 2 | 224 | 50YrSCS24Hr | 0.08 | 91.68 | 91.81 | 91.74 | 91.81 | 0.000794 | 0.15 | 0.54 | 6.88 | 0.17 |
| River 2 | Reach 2 | 224 | 100YrSCS24Hr | 0.09 | 91.68 | 91.81 | 91.75 | 91.82 | 0.000800 | 0.16 | 0.60 | 6.99 | 0.17 |
| River 2 | Reach 2 | 199 | 2YrCHI3Hr | 0.02 | 91.68 | 91.74 | 91.71 | 91.74 | 0.000450 | 0.07 | 0.24 | 6.76 | 0.11 |
| River 2 | Reach 2 | 199 | 5YrCHI3Hr | 0.03 | 91.68 | 91.75 | 91.71 | 91.75 | 0.000479 | 0.08 | 0.31 | 6.96 | 0.12 |
| River 2 | Reach 2 | 199 | 10YrCHI3Hr | 0.03 | 91.68 | 91.76 | 91.71 | 91.76 | 0.000481 | 0.09 | 0.38 | 7.14 | 0.12 |
| River 2 | Reach 2 | 199 | 25YrCHI3Hr | 0.05 | 91.68 | 91.77 | 91.72 | 91.77 | 0.000549 | 0.10 | 0.45 | 7.32 | 0.13 |
| River 2 | Reach 2 | 199 | 50YrCHI3Hr | 0.06 | 91.68 | 91.78 | 91.72 | 91.78 | 0.000569 | 0.11 | 0.50 | 7.42 | 0.14 |
| River 2 | Reach 2 | 199 | 100YrCHI3Hr | 0.07 | 91.68 | 91.78 | 91.73 | 91.78 | 0.000591 | 0.12 | 0.56 | 7.51 | 0.14 |
| River 2 | Reach 2 | 199 | 2YrSCS24Hr | 0.02 | 91.68 | 91.75 | 91.71 | 91.75 | 0.000474 | 0.08 | 0.30 | 6.91 | 0.12 |
| River 2 | Reach 2 | 199 | 5YrSCS24Hr | 0.04 | 91.68 | 91.76 | 91.72 | 91.76 | 0.000522 | 0.10 | 0.41 | 7.20 | 0.13 |
| River 2 | Reach 2 | 199 | 10YrSCS24Hr | 0.05 | 91.68 | 91.77 | 91.72 | 91.77 | 0.000558 | 0.11 | 0.47 | 7.37 | 0.14 |
| River 2 | Reach 2 | 199 | 25YrSCS24Hr | 0.07 | 91.68 | 91.78 | 91.72 | 91.78 | 0.000582 | 0.12 | 0.55 | 7.49 | 0.14 |
| River 2 | Reach 2 | 199 | 50YrSCS24Hr | 0.08 | 91.68 | 91.79 | 91.73 | 91.79 | 0.000628 | 0.13 | 0.60 | 7.57 | 0.15 |
| River 2 | Reach 2 | 199 | 100YrSCS24Hr | 0.09 | 91.68 | 91.80 | 91.73 | 91.80 | 0.000634 | 0.14 | 0.66 | 7.67 | 0.15 |
| River 2 | Reach 2 | 174 | 2YrCHI3Hr | 0.02 | 91.68 | 91.71 | 91.70 | 91.71 | 0.009341 | 0.22 | 0.07 | 3.33 | 0.47 |
| River 2 | Reach 2 | 174 | 5YrCHI3Hr | 0.03 | 91.68 | 91.71 | 91.70 | 91.72 | 0.010728 | 0.27 | 0.09 | 3.51 | 0.52 |
| River 2 | Reach 2 | 174 | 10YrCHI3Hr | 0.03 | 91.68 | 91.72 | 91.71 | 91.73 | 0.009147 | 0.28 | 0.12 | 3.68 | 0.49 |
| River 2 | Reach 2 | 174 | 25YrCHI3Hr | 0.05 | 91.68 | 91.73 | 91.72 | 91.73 | 0.010482 | 0.33 | 0.14 | 3.80 | 0.54 |
| River 2 | Reach 2 | 174 | 50YrCHI3Hr | 0.06 | 91.68 | 91.73 | 91.72 | 91.74 | 0.010789 | 0.35 | 0.16 | 3.90 | 0.56 |
| River 2 | Reach 2 | 174 | 100YrCHI3Hr | 0.07 | 91.68 | 91.74 | 91.72 | 91.75 | 0.011338 | 0.38 | 0.18 | 3.99 | 0.58 |
| River 2 | Reach 2 | 174 | 2YrSCS24Hr | 0.02 | 91.68 | 91.71 | 91.70 | 91.72 | 0.009099 | 0.24 | 0.09 | 3.51 | 0.48 |
| River 2 | Reach 2 | 174 | 5YrSCS24Hr | 0.04 | 91.68 | 91.73 | 91.71 | 91.73 | 0.009102 | 0.29 | 0.13 | 3.75 | 0.50 |
| River 2 | Reach 2 | 174 | 10YrSCS24Hr | 0.05 | 91.68 | 91.73 | 91.72 | 91.74 | 0.010830 | 0.34 | 0.15 | 3.84 | 0.55 |
| River 2 | Reach 2 | 174 | 25YrSCS24Hr | 0.07 | 91.68 | 91.74 | 91.72 | 91.74 | 0.010024 | 0.36 | 0.18 | 4.01 | 0.55 |
| River 2 | Reach 2 | 174 | 50YrSCS24Hr | 0.08 | 91.68 | 91.74 | 91.73 | 91.75 | 0.010794 | 0.40 | 0.20 | 4.08 | 0.57 |
| River 2 | Reach 2 | 174 | 100YrSCS24Hr | 0.09 | 91.68 | 91.75 | 91.73 | 91.76 | 0.010716 | 0.42 | 0.22 | 4.15 | 0.58 |
| River 2 | Reach 2 | 149 | 2YrCHI3Hr | 0.02 | 91.22 | 91.25 | 91.25 | 91.26 | 0.049600 | 0.35 | 0.05 | 3.45 | 0.99 |
| River 2 | Reach 2 | 149 | 5YrCHI3Hr | 0.03 | 91.22 | 91.26 | 91.26 | 91.27 | 0.037267 | 0.35 | 0.07 | 4.39 | 0.89 |
| River 2 | Reach 2 | 149 | 10YrCHI3Hr | 0.03 | 91.22 | 91.26 | 91.26 | 91.27 | 0.052915 | 0.44 | 0.08 | 4.47 | 1.07 |
| River 2 | Reach 2 | 149 | 25YrCHI3Hr | 0.05 | 91.22 | 91.27 | 91.27 | 91.28 | 0.039832 | 0.45 | 0.10 | 4.68 | 0.97 |
| River 2 | Reach 2 | 149 | 50YrCHI3Hr | 0.06 | 91.22 | 91.27 | 91.27 | 91.28 | 0.037244 | 0.47 | 0.12 | 4.80 | 0.95 |
| River 2 | Reach 2 | 149 | 100YrCHI3Hr | 0.07 | 91.22 | 91.27 | 91.27 | 91.29 | 0.034157 | 0.49 | 0.14 | 4.94 | 0.93 |
| River 2 | Reach 2 | 149 | 2YrSCS24Hr | 0.02 | 91.22 | 91.26 | 91.26 | 91.26 | 0.052399 | 0.39 | 0.06 | 3.96 | 1.03 |
| River 2 | Reach 2 | 149 | 5YrSCS24Hr | 0.04 | 91.22 | 91.26 | 91.26 | 91.27 | 0.052134 | 0.46 | 0.08 | 4.53 | 1.07 |
| River 2 | Reach 2 | 149 | 10YrSCS24Hr | 0.05 | 91.22 | 91.27 | 91.27 | 91.28 | 0.037535 | 0.46 | 0.11 | 4.74 | 0.95 |
| River 2 | Reach 2 | 149 | 25YrSCS24Hr | 0.07 | 91.22 | 91.27 | 91.27 | 91.29 | 0.044620 | 0.53 | 0.13 | 4.83 | 1.05 |
| River 2 | Reach 2 | 149 | 50YrSCS24Hr | 0.08 | 91.22 | 91.28 | 91.28 | 91.29 | 0.037650 | 0.53 | 0.15 | 5.00 | 0.98 |
| River 2 | Reach 2 | 149 | 100YrSCS24Hr | 0.09 | 91.22 | 91.28 | 91.28 | 91.30 | 0.038788 | 0.57 | 0.16 | 5.05 | 1.01 |
| River 2 | Reach 2 | 124 | 2YrCHI3Hr | 0.02 | 90.90 | 91.04 | 90.93 | 91.04 | 0.000032 | 0.03 | 0.48 | 5.07 | 0.03 |
| River 2 | Reach 2 | 124 | 5YrCHI3Hr | 0.03 | 90.90 | 91.05 | 90.93 | 91.05 | 0.000060 | 0.05 | 0.53 | 5.26 | 0.05 |
| River 2 | Reach 2 | 124 | 10YrCHI3Hr | 0.03 | 90.90 | 91.06 | 90.94 | 91.06 | 0.000112 | 0.06 | 0.57 | 6.50 | 0.06 |
| River 2 | Reach 2 | 124 | 25YrCHI3Hr | 0.05 | 90.90 | 91.07 | 90.95 | 91.07 | 0.000154 | 0.07 | 0.64 | 6.76 | 0.08 |
| River 2 | Reach 2 | 124 | 50YrCHI3Hr | 0.06 | 90.90 | 91.09 | 90.95 | 91.09 | 0.000135 | 0.07 | 0.76 | 7.17 | 0.07 |
| River 2 | Reach 2 | 124 | 100YrCHI3Hr | 0.07 | 90.90 | 91.14 | 90.95 | 91.14 | 0.000050 | 0.06 | 1.21 | 8.10 | 0.05 |
| River 2 | Reach 2 | 124 | 2YrSCS24Hr | 0.02 | 90.90 | 91.05 | 90.93 | 91.05 | 0.000054 | 0.04 | 0.51 | 5.22 | 0.05 |
| River 2 | Reach 2 | 124 | 5YrSCS24Hr | 0.04 | 90.90 | 91.06 | 90.94 | 91.06 | 0.000129 | 0.07 | 0.60 | 6.60 | 0.07 |
| River 2 | Reach 2 | 124 | 10YrSCS24Hr | 0.05 | 90.90 | 91.07 | 90.95 | 91.07 | 0.000166 | 0.08 | 0.66 | 6.83 | 0.08 |
| River 2 | Reach 2 | 124 | 25YrSCS24Hr | 0.07 | 90.90 | 91.12 | 90.95 | 91.12 | 0.000074 | 0.06 | 1.04 | 7.89 | 0.06 |
| River 2 | Reach 2 | 124 | 50YrSCS24Hr | 0.08 | 90.90 | 91.19 | 90.96 | 91.19 | 0.000031 | 0.05 | 1.55 | 8.50 | 0.04 |
| River 2 | Reach 2 | 124 | 100YrSCS24Hr | 0.09 | 90.90 | 91.25 | 90.96 | 91.25 | 0.000017 | 0.04 | 2.15 | 9.67 | 0.03 |
| River 2 | Reach 2 | 99 | 2YrCHI3Hr | 0.02 | 90.90 | 91.04 | 90.92 | 91.04 | 0.000010 | 0.02 | 0.80 | 7.44 | 0.02 |
| River 2 | Reach 2 | 99 | 5YrCHI3Hr | 0.03 | 90.90 | 91.05 | 90.92 | 91.05 | 0.000018 | 0.03 | 0.87 | 7.51 | 0.03 |
| River 2 | Reach 2 | 99 | 10YrCHI3Hr | 0.03 | 90.90 | 91.06 | 90.93 | 91.06 | 0.000027 | 0.04 | 0.93 | 7.57 | 0.03 |
| River 2 | Reach 2 | 99 | 25YrCHI3Hr | 0.05 | 90.90 | 91.07 | 90.93 | 91.07 | 0.000041 | 0.05 | 1.00 | 7.64 | 0.04 |
| River 2 | Reach 2 | 99 | 50YrCHI3Hr | 0.06 | 90.90 | 91.09 | 90.94 | 91.09 | 0.000040 | 0.05 | 1.14 | 7.79 | 0.04 |
| River 2 | Reach 2 | 99 | 100YrCHI3Hr | 0.07 | 90.90 | 91.14 | 90.94 | 91.14 | 0.000020 | 0.04 | 1.61 | 8.25 | 0.03 |
| River 2 | Reach 2 | 99 | 2YrSCS24Hr | 0.02 | 90.90 | 91.05 | 90.92 | 91.05 | 0.000016 | 0.03 | 0.86 | 7.49 | 0.03 |
| River 2 | Reach 2 | 99 | 5YrSCS24Hr | 0.04 | 90.90 | 91.06 | 90.93 | 91.06 | 0.000032 | 0.04 | 0.96 | 7.60 | 0.04 |
| River 2 | Reach 2 | 99 | 10YrSCS24Hr | 0.05 | 90.90 | 91.07 | 90.94 | 91.07 | 0.000045 | 0.05 | 1.02 | 7.67 | 0.04 |
| River 2 | Reach 2 | 99 | 25YrSCS24Hr | 0.07 | 90.90 | 91.12 | 90.94 | 91.12 | 0.000026 | 0.05 | 1.43 | 8.07 | 0.03 |
| River 2 | Reach 2 | 99 | 50YrSCS24Hr | 0.08 | 90.90 | 91.19 | 90.94 | 91.19 | 0.000014 | 0.04 | 1.96 | 8.55 | 0.03 |
| River 2 | Reach 2 | 99 | 100YrSCS24Hr | 0.09 | 90.90 | 91.25 | 90.95 | 91.25 | 0.000009 | 0.04 | 2.54 | 9.03 | 0.02 |
| River 2 | Reach 2 | 74 | 2YrCHI3Hr | 0.02 | 90.89 | 91.04 | 90.91 | 91.04 | 0.000011 | 0.02 | 0.72 | 6.36 | 0.02 |
| River 2 | Reach 2 | 74 | 5YrCHI3Hr | 0.03 | 90.89 | 91.05 | 90.92 | 91.05 | 0.000021 | 0.03 | 0.78 | 6.44 | 0.03 |
| River 2 | Reach 2 | 74 | 10YrCHI3Hr | 0.03 | 90.89 | 91.06 | 90.92 | 91.06 | 0.000033 | 0.04 | 0.83 | 6.50 | 0.04 |
| River 2 | Reach 2 | 74 | 25YrCHI3Hr | 0.05 | 90.89 | 91.07 | 90.93 | 91.07 | 0.000050 | 0.05 | 0.89 | 6.57 | 0.05 |
| River 2 | Reach 2 | 74 | 50YrCHI3Hr | 0.06 | 90.89 | 91.08 | 90.93 | 91.08 | 0.000049 | 0.06 | 1.01 | 6.70 | 0.05 |
| River 2 | Reach 2 | 74 | 100YrCHI3Hr | 0.07 | 90.89 | 91.14 | 90.93 | 91.14 | 0.000025 | 0.05 | 1.42 | 7.09 | 0.03 |
| River 2 | Reach 2 | 74 | 2YrSCS24Hr | 0.02 | 90.89 | 91.05 | 90.92 | 91.05 | 0.000019 | 0.03 | 0.77 | 6.42 | 0.03 |
| River 2 | Reach 2 | 74 | 5YrSCS24Hr | 0.04 | 90.89 | 91.06 | 90.92 | 91.06 | 0.000039 | 0.05 | 0.85 | 6.53 | 0.04 |
| River 2 | Reach 2 | 74 | 10YrSCS24Hr | 0.05 | 90.89 | 91.07 | 90.93 | 91.07 | 0.000055 | 0.06 | 0.91 | 6.59 | 0.05 |
| River 2 | Reach 2 | 74 | 25YrSCS24Hr | 0.07 | 90.89 | 91.12 | 90.93 | 91.12 | 0.000033 | 0.05 | 1.26 | 6.96 | 0.04 |
| River 2 | Reach 2 | 74 | 50YrSCS24Hr | 0.08 | 90.89 | 91.18 | 90.93 | 91.18 | 0.000018 | 0.05 | 1.72 | 7.34 | 0.03 |
| River 2 | Reach 2 | 74 | 100YrSCS24Hr | 0.09 | 90.89 | 91.25 | 90.94 | 91.25 | 0.000012 | 0.04 | 2.22 | 7.71 | 0.03 |

HEC-RAS Plan: 20250603-Pre_Dev_v01 (Continued)

| River | Reach | River Sta | Profile | Q Total (m3/s) | Min Ch El (m) | W.S. Elev (m) | Crit W.S. (m) | E.G. Elev (m) | E.G. Slope (m/m) | Vel Chnl (m/s) | Flow Area (m2) | Top Width (m) | Froude # Chl |
|---------|---------------|-----------|--------------|-------------------|------------------|------------------|------------------|------------------|---------------------|-------------------|-------------------|------------------|--------------|
| River 2 | Reach 2 | 49 | 2YrCHI3Hr | 0.02 | 91.00 | 91.03 | 91.03 | 91.04 | 0.048683 | 0.40 | 0.04 | 2.56 | 1.01 |
| River 2 | Reach 2 | 49 | 5YrCHI3Hr | 0.03 | 91.00 | 91.04 | 91.04 | 91.05 | 0.045843 | 0.43 | 0.06 | 3.06 | 1.01 |
| River 2 | Reach 2 | 49 | 10YrCHI3Hr | 0.03 | 91.00 | 91.04 | 91.04 | 91.05 | 0.036151 | 0.43 | 0.08 | 3.50 | 0.92 |
| River 2 | Reach 2 | 49 | 25YrCHI3Hr | 0.05 | 91.00 | 91.05 | 91.05 | 91.06 | 0.042954 | 0.52 | 0.09 | 3.52 | 1.03 |
| River 2 | Reach 2 | 49 | 50YrCHI3Hr | 0.06 | 91.00 | 91.08 | 91.05 | 91.08 | 0.005537 | 0.28 | 0.20 | 4.07 | 0.41 |
| River 2 | Reach 2 | 49 | 100YrCHI3Hr | 0.07 | 91.00 | 91.14 | 91.05 | 91.14 | 0.000508 | 0.14 | 0.50 | 4.96 | 0.14 |
| River 2 | Reach 2 | 49 | 2YrSCS24Hr | 0.02 | 91.00 | 91.04 | 91.04 | 91.04 | 0.038802 | 0.40 | 0.06 | 3.06 | 0.93 |
| River 2 | Reach 2 | 49 | 5YrSCS24Hr | 0.04 | 91.00 | 91.04 | 91.04 | 91.06 | 0.043713 | 0.48 | 0.08 | 3.50 | 1.02 |
| River 2 | Reach 2 | 49 | 10YrSCS24Hr | 0.05 | 91.00 | 91.05 | 91.05 | 91.06 | 0.037160 | 0.51 | 0.10 | 3.53 | 0.97 |
| River 2 | Reach 2 | 49 | 25YrSCS24Hr | 0.07 | 91.00 | 91.12 | 91.05 | 91.12 | 0.001066 | 0.17 | 0.38 | 4.82 | 0.19 |
| River 2 | Reach 2 | 49 | 50YrSCS24Hr | 0.08 | 91.00 | 91.18 | 91.06 | 91.18 | 0.000237 | 0.11 | 0.73 | 5.93 | 0.10 |
| River 2 | Reach 2 | 49 | 100YrSCS24Hr | 0.09 | 91.00 | 91.25 | 91.06 | 91.25 | 0.000083 | 0.08 | 1.15 | 6.63 | 0.06 |
| River 2 | Reach 2 | 28 | 2YrCHI3Hr | 0.02 | 90.69 | 90.78 | 90.74 | 90.78 | 0.001301 | 0.13 | 0.15 | 3.26 | 0.20 |
| River 2 | Reach 2 | 28 | 5YrCHI3Hr | 0.03 | 90.69 | 90.85 | 90.75 | 90.85 | 0.000163 | 0.07 | 0.47 | 5.17 | 0.08 |
| River 2 | Reach 2 | 28 | 10YrCHI3Hr | 0.05 | 90.69 | 90.93 | 90.75 | 90.93 | 0.000046 | 0.05 | 0.89 | 6.29 | 0.04 |
| River 2 | Reach 2 | 28 | 25YrCHI3Hr | 0.06 | 90.69 | 91.01 | 90.76 | 91.01 | 0.000019 | 0.04 | 1.48 | 7.14 | 0.03 |
| River 2 | Reach 2 | 28 | 50YrCHI3Hr | 0.08 | 90.69 | 91.08 | 90.77 | 91.08 | 0.000012 | 0.04 | 1.96 | 7.68 | 0.03 |
| River 2 | Reach 2 | 28 | 100YrCHI3Hr | 0.09 | 90.69 | 91.14 | 90.78 | 91.14 | 0.000009 | 0.04 | 2.47 | 8.16 | 0.02 |
| River 2 | Reach 2 | 28 | 2YrSCS24Hr | 0.03 | 90.69 | 90.83 | 90.74 | 90.83 | 0.000330 | 0.09 | 0.35 | 4.66 | 0.11 |
| River 2 | Reach 2 | 28 | 5YrSCS24Hr | 0.05 | 90.69 | 90.95 | 90.76 | 90.95 | 0.000036 | 0.05 | 1.07 | 6.57 | 0.04 |
| River 2 | Reach 2 | 28 | 10YrSCS24Hr | 0.07 | 90.69 | 91.03 | 90.76 | 91.03 | 0.000019 | 0.04 | 1.58 | 7.26 | 0.03 |
| River 2 | Reach 2 | 28 | 25YrSCS24Hr | 0.09 | 90.69 | 91.12 | 90.78 | 91.12 | 0.000011 | 0.04 | 2.28 | 7.99 | 0.02 |
| River 2 | Reach 2 | 28 | 50YrSCS24Hr | 0.11 | 90.69 | 91.18 | 90.78 | 91.18 | 0.000008 | 0.04 | 2.82 | 8.48 | 0.02 |
| River 2 | Reach 2 | 28 | 100YrSCS24Hr | 0.13 | 90.69 | 91.25 | 90.79 | 91.25 | 0.000007 | 0.04 | 3.40 | 8.98 | 0.02 |
| River 2 | Reach 2 | 7 | 2YrCHI3Hr | 0.02 | 90.67 | 90.73 | 90.71 | 90.74 | 0.003117 | 0.17 | 0.11 | 3.14 | 0.29 |
| River 2 | Reach 2 | 7 | 5YrCHI3Hr | 0.03 | 90.67 | 90.85 | 90.72 | 90.85 | 0.000075 | 0.06 | 0.60 | 5.18 | 0.05 |
| River 2 | Reach 2 | 7 | 10YrCHI3Hr | 0.05 | 90.67 | 90.92 | 90.73 | 90.92 | 0.000028 | 0.05 | 1.02 | 5.92 | 0.04 |
| River 2 | Reach 2 | 7 | 25YrCHI3Hr | 0.06 | 90.67 | 91.01 | 90.73 | 91.01 | 0.000014 | 0.04 | 1.56 | 6.43 | 0.03 |
| River 2 | Reach 2 | 7 | 50YrCHI3Hr | 0.08 | 90.67 | 91.08 | 90.74 | 91.08 | 0.000010 | 0.04 | 1.99 | 6.71 | 0.02 |
| River 2 | Reach 2 | 7 | 100YrCHI3Hr | 0.09 | 90.67 | 91.14 | 90.74 | 91.14 | 0.000008 | 0.04 | 2.42 | 6.98 | 0.02 |
| River 2 | Reach 2 | 7 | 2YrSCS24Hr | 0.03 | 90.67 | 90.82 | 90.72 | 90.82 | 0.000130 | 0.07 | 0.46 | 4.72 | 0.07 |
| River 2 | Reach 2 | 7 | 5YrSCS24Hr | 0.05 | 90.67 | 90.95 | 90.73 | 90.95 | 0.000023 | 0.05 | 1.18 | 6.12 | 0.03 |
| River 2 | Reach 2 | 7 | 10YrSCS24Hr | 0.07 | 90.67 | 91.03 | 90.73 | 91.03 | 0.000014 | 0.04 | 1.65 | 6.49 | 0.03 |
| River 2 | Reach 2 | 7 | 25YrSCS24Hr | 0.09 | 90.67 | 91.12 | 90.74 | 91.12 | 0.000009 | 0.04 | 2.26 | 6.88 | 0.02 |
| River 2 | Reach 2 | 7 | 50YrSCS24Hr | 0.11 | 90.67 | 91.18 | 90.75 | 91.18 | 0.000007 | 0.04 | 2.72 | 7.15 | 0.02 |
| River 2 | Reach 2 | 7 | 100YrSCS24Hr | 0.13 | 90.67 | 91.25 | 90.75 | 91.25 | 0.000006 | 0.04 | 3.21 | 7.44 | 0.02 |
| River 1 | Reach 1-Upper | 908 | 2YrCHI3Hr | 0.02 | 94.14 | 94.22 | 94.18 | 94.22 | 0.001587 | 0.14 | 0.10 | 2.34 | 0.22 |
| River 1 | Reach 1-Upper | 908 | 5YrCHI3Hr | 0.03 | 94.14 | 94.23 | 94.19 | 94.23 | 0.001806 | 0.18 | 0.15 | 2.64 | 0.24 |
| River 1 | Reach 1-Upper | 908 | 10YrCHI3Hr | 0.03 | 94.14 | 94.24 | 94.20 | 94.24 | 0.002004 | 0.20 | 0.17 | 2.81 | 0.26 |
| River 1 | Reach 1-Upper | 908 | 25YrCHI3Hr | 0.05 | 94.14 | 94.25 | 94.20 | 94.26 | 0.002189 | 0.22 | 0.21 | 3.02 | 0.27 |
| River 1 | Reach 1-Upper | 908 | 50YrCHI3Hr | 0.06 | 94.14 | 94.26 | 94.21 | 94.27 | 0.002278 | 0.24 | 0.24 | 3.18 | 0.28 |
| River 1 | Reach 1-Upper | 908 | 100YrCHI3Hr | 0.07 | 94.14 | 94.27 | 94.21 | 94.27 | 0.002320 | 0.25 | 0.26 | 3.32 | 0.29 |
| River 1 | Reach 1-Upper | 908 | 2YrSCS24Hr | 0.02 | 94.14 | 94.23 | 94.19 | 94.23 | 0.001752 | 0.17 | 0.14 | 2.59 | 0.23 |
| River 1 | Reach 1-Upper | 908 | 5YrSCS24Hr | 0.04 | 94.14 | 94.25 | 94.20 | 94.25 | 0.002058 | 0.21 | 0.18 | 2.87 | 0.26 |
| River 1 | Reach 1-Upper | 908 | 10YrSCS24Hr | 0.05 | 94.14 | 94.26 | 94.20 | 94.26 | 0.002199 | 0.23 | 0.22 | 3.05 | 0.27 |
| River 1 | Reach 1-Upper | 908 | 25YrSCS24Hr | 0.06 | 94.14 | 94.27 | 94.21 | 94.27 | 0.002241 | 0.25 | 0.25 | 3.26 | 0.28 |
| River 1 | Reach 1-Upper | 908 | 50YrSCS24Hr | 0.07 | 94.14 | 94.28 | 94.22 | 94.28 | 0.002406 | 0.26 | 0.28 | 3.39 | 0.29 |
| River 1 | Reach 1-Upper | 908 | 100YrSCS24Hr | 0.08 | 94.14 | 94.29 | 94.22 | 94.29 | 0.002029 | 0.26 | 0.33 | 3.64 | 0.27 |
| River 1 | Reach 1-Upper | 887 | 2YrCHI3Hr | 0.02 | 94.10 | 94.15 | 94.14 | 94.16 | 0.007507 | 0.23 | 0.07 | 2.30 | 0.44 |
| River 1 | Reach 1-Upper | 887 | 5YrCHI3Hr | 0.03 | 94.10 | 94.17 | 94.15 | 94.17 | 0.005953 | 0.25 | 0.10 | 2.78 | 0.41 |
| River 1 | Reach 1-Upper | 887 | 10YrCHI3Hr | 0.03 | 94.10 | 94.18 | 94.15 | 94.18 | 0.005054 | 0.26 | 0.14 | 3.08 | 0.39 |
| River 1 | Reach 1-Upper | 887 | 25YrCHI3Hr | 0.05 | 94.10 | 94.19 | 94.16 | 94.20 | 0.004392 | 0.26 | 0.18 | 3.42 | 0.37 |
| River 1 | Reach 1-Upper | 887 | 50YrCHI3Hr | 0.06 | 94.10 | 94.20 | 94.17 | 94.20 | 0.004802 | 0.29 | 0.20 | 3.57 | 0.39 |
| River 1 | Reach 1-Upper | 887 | 100YrCHI3Hr | 0.07 | 94.10 | 94.21 | 94.17 | 94.21 | 0.004705 | 0.30 | 0.22 | 3.76 | 0.39 |
| River 1 | Reach 1-Upper | 887 | 2YrSCS24Hr | 0.02 | 94.10 | 94.17 | 94.15 | 94.17 | 0.006295 | 0.25 | 0.10 | 2.71 | 0.42 |
| River 1 | Reach 1-Upper | 887 | 5YrSCS24Hr | 0.04 | 94.10 | 94.18 | 94.15 | 94.19 | 0.004885 | 0.26 | 0.15 | 3.16 | 0.38 |
| River 1 | Reach 1-Upper | 887 | 10YrSCS24Hr | 0.05 | 94.10 | 94.19 | 94.16 | 94.20 | 0.004587 | 0.27 | 0.18 | 3.44 | 0.38 |
| River 1 | Reach 1-Upper | 887 | 25YrSCS24Hr | 0.06 | 94.10 | 94.20 | 94.17 | 94.20 | 0.005786 | 0.31 | 0.20 | 3.56 | 0.43 |
| River 1 | Reach 1-Upper | 887 | 50YrSCS24Hr | 0.07 | 94.10 | 94.21 | 94.17 | 94.22 | 0.003925 | 0.29 | 0.25 | 3.98 | 0.36 |
| River 1 | Reach 1-Upper | 887 | 100YrSCS24Hr | 0.08 | 94.10 | 94.19 | 94.18 | 94.20 | 0.014690 | 0.48 | 0.18 | 3.39 | 0.67 |
| River 1 | Reach 1-Upper | 868 | 2YrCHI3Hr | 0.02 | 93.96 | 94.02 | 94.01 | 94.03 | 0.006049 | 0.24 | 0.06 | 1.78 | 0.41 |
| River 1 | Reach 1-Upper | 868 | 5YrCHI3Hr | 0.03 | 93.96 | 94.04 | 94.01 | 94.04 | 0.007801 | 0.31 | 0.08 | 1.98 | 0.48 |
| River 1 | Reach 1-Upper | 868 | 10YrCHI3Hr | 0.03 | 93.96 | 94.04 | 94.02 | 94.05 | 0.010621 | 0.37 | 0.09 | 2.05 | 0.56 |
| River 1 | Reach 1-Upper | 868 | 25YrCHI3Hr | 0.05 | 93.96 | 94.05 | 94.03 | 94.06 | 0.013422 | 0.44 | 0.11 | 2.15 | 0.64 |
| River 1 | Reach 1-Upper | 868 | 50YrCHI3Hr | 0.06 | 93.96 | 94.06 | 94.04 | 94.07 | 0.010577 | 0.43 | 0.13 | 2.35 | 0.58 |
| River 1 | Reach 1-Upper | 868 | 100YrCHI3Hr | 0.07 | 93.96 | 94.06 | 94.04 | 94.07 | 0.010976 | 0.46 | 0.15 | 2.45 | 0.60 |
| River 1 | Reach 1-Upper | 868 | 2YrSCS24Hr | 0.02 | 93.96 | 94.03 | 94.01 | 94.04 | 0.007224 | 0.29 | 0.08 | 1.96 | 0.46 |
| River 1 | Reach 1-Upper | 868 | 5YrSCS24Hr | 0.04 | 93.96 | 94.04 | 94.02 | 94.05 | 0.011359 | 0.39 | 0.10 | 2.08 | 0.58 |
| River 1 | Reach 1-Upper | 868 | 10YrSCS24Hr | 0.05 | 93.96 | 94.05 | 94.03 | 94.06 | 0.012976 | 0.44 | 0.11 | 2.19 | 0.63 |
| River 1 | Reach 1-Upper | 868 | 25YrSCS24Hr | 0.06 | 93.96 | 94.07 | 94.04 | 94.08 | 0.007363 | 0.39 | 0.16 | 2.55 | 0.49 |
| River 1 | Reach 1-Upper | 868 | 50YrSCS24Hr | 0.07 | 93.96 | 94.06 | 94.05 | 94.07 | 0.019525 | 0.57 | 0.13 | 2.31 | 0.78 |
| River 1 | Reach 1-Upper | 868 | 100YrSCS24Hr | 0.08 | 93.96 | 94.14 | 94.05 | 94.15 | 0.001168 | 0.21 | 0.40 | 3.98 | 0.21 |
| River 1 | Reach 1-Upper | 848 | 2YrCHI3Hr | 0.02 | 93.87 | 93.92 | 93.90 | 93.92 | 0.004686 | 0.19 | 0.08 | 2.57 | 0.35 |
| River 1 | Reach 1-Upper | 848 | 5YrCHI3Hr | 0.03 | 93.87 | 93.93 | 93.91 | 93.94 | 0.003787 | 0.21 | 0.12 | 2.98 | 0.33 |
| River 1 | Reach 1-Upper | 848 | 10YrCHI3Hr | 0.03 | 93.87 | 93.95 | 93.92 | 93.95 | 0.002708 | 0.21 | 0.17 | 3.15 | 0.29 |
| River 1 | Reach 1-Upper | 848 | 25YrCHI3Hr | 0.05 | 93.87 | 93.97 | 93.92 | 93.97 | 0.002043 | 0.21 | 0.22 | 3.34 | 0.26 |
| River 1 | Reach 1-Upper | 848 | 50YrCHI3Hr | 0.06 | 93.87 | 93.97 | 93.93 | 93.97 | 0.002676 | 0.25 | 0.23 | 3.37 | 0.30 |
| River 1 | Reach 1-Upper | 848 | 100YrCHI3Hr | 0.07 | 93.87 | 93.98 | 93.93 | 93.98 | 0.002517 | 0.26 | 0.26 | 3.47 | 0.30 |
| River 1 | Reach 1-Upper | 848 | 2YrSCS24Hr | 0.02 | 93.87 | 93.93 | 93.91 | 93.93 | 0.004188 | 0.21 | 0.11 | 2.93 | 0.34 |
| River 1 | Reach 1-Upper | 848 | 5YrSCS24Hr | 0.04 | 93.87 | 93.95 | 93.92 | 93.96 | 0.002536 | 0.21 | 0.18 | 3.19 | 0.28 |
| River 1 | Reach 1-Upper | 848 | 10YrSCS24Hr | 0.05 | 93.87 | 93.97 | 93.92 | 93.97 | 0.002100 | 0.22 | 0.23 | 3.35 | 0.27 |
| River 1 | Reach 1-Upper | 848 | 25YrSCS24Hr | 0.06 | 93.87 | 93.96 | 93.93 | 93.97 | 0.004423 | 0.30 | 0.21 | 3.29 | 0.38 |
| River 1 | Reach 1-Upper | 848 | 50YrSCS24Hr | 0.07 | 93.87 | 94.04 | 93.93 | 94.04 | 0.000430 | 0.15 | 0.50 | 3.98 | 0.13 |

HEC-RAS Plan: 20250603-Pre_Dev_v01 (Continued)

| River | Reach | River Sta | Profile | Q Total (m3/s) | Min Ch El (m) | W.S. Elev (m) | Crit W.S. (m) | E.G. Elev (m) | E.G. Slope (m/m) | Vel Chnl (m/s) | Flow Area (m2) | Top Width (m) | Froude # Chl |
|---------|---------------|-----------|--------------|-------------------|------------------|------------------|------------------|------------------|---------------------|-------------------|-------------------|------------------|--------------|
| River 1 | Reach 1-Upper | 848 | 100YrSCS24Hr | 0.08 | 93.87 | 94.14 | 93.94 | 94.14 | 0.000088 | 0.09 | 0.94 | 4.75 | 0.06 |
| River 1 | Reach 1-Upper | 828 | 2YrCHI3Hr | 0.02 | 93.78 | 93.85 | 93.82 | 93.85 | 0.002687 | 0.16 | 0.09 | 2.47 | 0.27 |
| River 1 | Reach 1-Upper | 828 | 5YrCHI3Hr | 0.03 | 93.78 | 93.86 | 93.83 | 93.86 | 0.004045 | 0.22 | 0.12 | 2.90 | 0.34 |
| River 1 | Reach 1-Upper | 828 | 10YrCHI3Hr | 0.03 | 93.78 | 93.85 | 93.83 | 93.86 | 0.010289 | 0.33 | 0.10 | 2.68 | 0.54 |
| River 1 | Reach 1-Upper | 828 | 25YrCHI3Hr | 0.05 | 93.78 | 93.84 | 93.84 | 93.86 | 0.040257 | 0.61 | 0.08 | 2.23 | 1.04 |
| River 1 | Reach 1-Upper | 828 | 50YrCHI3Hr | 0.06 | 93.78 | 93.87 | 93.85 | 93.87 | 0.011893 | 0.40 | 0.14 | 3.16 | 0.59 |
| River 1 | Reach 1-Upper | 828 | 100YrCHI3Hr | 0.07 | 93.78 | 93.96 | 93.85 | 93.97 | 0.000365 | 0.13 | 0.50 | 4.07 | 0.12 |
| River 1 | Reach 1-Upper | 828 | 2YrSCS24Hr | 0.02 | 93.78 | 93.86 | 93.82 | 93.86 | 0.003210 | 0.19 | 0.12 | 2.95 | 0.30 |
| River 1 | Reach 1-Upper | 828 | 5YrSCS24Hr | 0.04 | 93.78 | 93.85 | 93.84 | 93.86 | 0.014294 | 0.39 | 0.10 | 2.58 | 0.63 |
| River 1 | Reach 1-Upper | 828 | 10YrSCS24Hr | 0.05 | 93.78 | 93.84 | 93.84 | 93.86 | 0.036015 | 0.59 | 0.08 | 2.34 | 0.99 |
| River 1 | Reach 1-Upper | 828 | 25YrSCS24Hr | 0.06 | 93.78 | 93.90 | 93.85 | 93.90 | 0.002459 | 0.25 | 0.25 | 3.50 | 0.29 |
| River 1 | Reach 1-Upper | 828 | 50YrSCS24Hr | 0.07 | 93.78 | 94.04 | 93.86 | 94.04 | 0.000005 | 0.02 | 5.50 | 35.21 | 0.01 |
| River 1 | Reach 1-Upper | 828 | 100YrSCS24Hr | 0.08 | 93.78 | 94.14 | 93.86 | 94.14 | 0.000001 | 0.01 | 9.06 | 35.66 | 0.01 |
| River 1 | Reach 1-Upper | 807 | 2YrCHI3Hr | 0.02 | 93.65 | 93.70 | 93.70 | 93.71 | 0.039865 | 0.46 | 0.03 | 1.40 | 0.97 |
| River 1 | Reach 1-Upper | 807 | 5YrCHI3Hr | 0.03 | 93.65 | 93.72 | 93.71 | 93.73 | 0.011679 | 0.35 | 0.07 | 1.90 | 0.57 |
| River 1 | Reach 1-Upper | 807 | 10YrCHI3Hr | 0.03 | 93.65 | 93.76 | 93.71 | 93.76 | 0.002625 | 0.22 | 0.16 | 2.63 | 0.29 |
| River 1 | Reach 1-Upper | 807 | 25YrCHI3Hr | 0.05 | 93.65 | 93.80 | 93.72 | 93.80 | 0.000718 | 0.16 | 0.30 | 3.53 | 0.16 |
| River 1 | Reach 1-Upper | 807 | 50YrCHI3Hr | 0.06 | 93.65 | 93.86 | 93.73 | 93.86 | 0.000227 | 0.12 | 0.51 | 4.43 | 0.10 |
| River 1 | Reach 1-Upper | 807 | 100YrCHI3Hr | 0.07 | 93.65 | 93.96 | 93.73 | 93.96 | 0.000003 | 0.02 | 5.71 | 34.82 | 0.01 |
| River 1 | Reach 1-Upper | 807 | 2YrSCS24Hr | 0.02 | 93.65 | 93.71 | 93.70 | 93.72 | 0.021814 | 0.43 | 0.06 | 1.70 | 0.76 |
| River 1 | Reach 1-Upper | 807 | 5YrSCS24Hr | 0.04 | 93.65 | 93.77 | 93.71 | 93.77 | 0.001862 | 0.20 | 0.19 | 2.86 | 0.25 |
| River 1 | Reach 1-Upper | 807 | 10YrSCS24Hr | 0.05 | 93.65 | 93.81 | 93.72 | 93.81 | 0.000588 | 0.15 | 0.33 | 3.67 | 0.15 |
| River 1 | Reach 1-Upper | 807 | 25YrSCS24Hr | 0.06 | 93.65 | 93.89 | 93.73 | 93.89 | 0.000119 | 0.10 | 0.70 | 6.11 | 0.07 |
| River 1 | Reach 1-Upper | 807 | 50YrSCS24Hr | 0.07 | 93.65 | 94.04 | 93.74 | 94.04 | 0.000001 | 0.01 | 8.37 | 35.13 | 0.01 |
| River 1 | Reach 1-Upper | 807 | 100YrSCS24Hr | 0.08 | 93.65 | 94.14 | 93.74 | 94.14 | 0.000000 | 0.01 | 11.92 | 35.53 | 0.01 |
| River 1 | Reach 1-Upper | 789 | 2YrCHI3Hr | 0.02 | 93.49 | 93.67 | 93.53 | 93.67 | 0.000035 | 0.04 | 0.33 | 3.14 | 0.04 |
| River 1 | Reach 1-Upper | 789 | 5YrCHI3Hr | 0.03 | 93.49 | 93.72 | 93.54 | 93.72 | 0.000038 | 0.06 | 0.45 | 3.66 | 0.04 |
| River 1 | Reach 1-Upper | 789 | 10YrCHI3Hr | 0.03 | 93.49 | 93.76 | 93.55 | 93.76 | 0.000039 | 0.07 | 0.54 | 4.24 | 0.04 |
| River 1 | Reach 1-Upper | 789 | 25YrCHI3Hr | 0.05 | 93.49 | 93.80 | 93.56 | 93.80 | 0.000037 | 0.07 | 0.65 | 4.99 | 0.04 |
| River 1 | Reach 1-Upper | 789 | 50YrCHI3Hr | 0.06 | 93.49 | 93.86 | 93.57 | 93.86 | 0.000030 | 0.07 | 0.78 | 5.73 | 0.04 |
| River 1 | Reach 1-Upper | 789 | 100YrCHI3Hr | 0.07 | 93.49 | 93.96 | 93.57 | 93.96 | 0.000016 | 0.06 | 1.04 | 8.28 | 0.03 |
| River 1 | Reach 1-Upper | 789 | 2YrSCS24Hr | 0.02 | 93.49 | 93.71 | 93.54 | 93.71 | 0.000038 | 0.06 | 0.43 | 3.55 | 0.04 |
| River 1 | Reach 1-Upper | 789 | 5YrSCS24Hr | 0.04 | 93.49 | 93.77 | 93.55 | 93.77 | 0.000038 | 0.07 | 0.56 | 4.42 | 0.04 |
| River 1 | Reach 1-Upper | 789 | 10YrSCS24Hr | 0.05 | 93.49 | 93.81 | 93.56 | 93.81 | 0.000037 | 0.07 | 0.67 | 5.12 | 0.04 |
| River 1 | Reach 1-Upper | 789 | 25YrSCS24Hr | 0.06 | 93.49 | 93.89 | 93.57 | 93.89 | 0.000025 | 0.07 | 0.87 | 6.17 | 0.04 |
| River 1 | Reach 1-Upper | 789 | 50YrSCS24Hr | 0.07 | 93.49 | 94.04 | 93.57 | 94.04 | 0.000011 | 0.06 | 1.22 | 10.07 | 0.03 |
| River 1 | Reach 1-Upper | 789 | 100YrSCS24Hr | 0.08 | 93.49 | 94.14 | 93.58 | 94.14 | 0.000008 | 0.06 | 1.46 | 23.56 | 0.02 |
| River 1 | Reach 1-Upper | 764 | | Culvert | | | | | | | | | |
| River 1 | Reach 1-Upper | 759 | 2YrCHI3Hr | 0.02 | 93.46 | 93.53 | 93.50 | 93.53 | 0.002563 | 0.21 | 0.07 | 1.74 | 0.28 |
| River 1 | Reach 1-Upper | 759 | 5YrCHI3Hr | 0.03 | 93.46 | 93.56 | 93.51 | 93.56 | 0.002115 | 0.23 | 0.11 | 2.11 | 0.27 |
| River 1 | Reach 1-Upper | 759 | 10YrCHI3Hr | 0.03 | 93.46 | 93.59 | 93.52 | 93.60 | 0.001088 | 0.21 | 0.16 | 2.56 | 0.21 |
| River 1 | Reach 1-Upper | 759 | 25YrCHI3Hr | 0.05 | 93.46 | 93.66 | 93.53 | 93.66 | 0.000396 | 0.18 | 0.26 | 3.40 | 0.14 |
| River 1 | Reach 1-Upper | 759 | 50YrCHI3Hr | 0.06 | 93.46 | 93.74 | 93.54 | 93.74 | 0.000161 | 0.15 | 0.39 | 4.37 | 0.09 |
| River 1 | Reach 1-Upper | 759 | 100YrCHI3Hr | 0.07 | 93.46 | 93.83 | 93.54 | 93.84 | 0.000081 | 0.13 | 0.53 | 6.02 | 0.07 |
| River 1 | Reach 1-Upper | 759 | 2YrSCS24Hr | 0.02 | 93.46 | 93.55 | 93.51 | 93.56 | 0.002355 | 0.23 | 0.10 | 2.03 | 0.28 |
| River 1 | Reach 1-Upper | 759 | 5YrSCS24Hr | 0.04 | 93.46 | 93.61 | 93.52 | 93.61 | 0.000864 | 0.21 | 0.18 | 2.73 | 0.19 |
| River 1 | Reach 1-Upper | 759 | 10YrSCS24Hr | 0.05 | 93.46 | 93.67 | 93.53 | 93.67 | 0.000343 | 0.17 | 0.28 | 3.54 | 0.13 |
| River 1 | Reach 1-Upper | 759 | 25YrSCS24Hr | 0.06 | 93.46 | 93.79 | 93.54 | 93.79 | 0.000109 | 0.14 | 0.46 | 4.99 | 0.08 |
| River 1 | Reach 1-Upper | 759 | 50YrSCS24Hr | 0.07 | 93.46 | 93.89 | 93.54 | 93.89 | 0.000058 | 0.12 | 0.61 | 6.73 | 0.06 |
| River 1 | Reach 1-Upper | 759 | 100YrSCS24Hr | 0.08 | 93.46 | 93.95 | 93.55 | 93.95 | 0.000051 | 0.12 | 0.69 | 7.38 | 0.06 |
| River 1 | Reach 1-Upper | 743 | 2YrCHI3Hr | 0.02 | 93.40 | 93.47 | 93.45 | 93.47 | 0.006174 | 0.30 | 0.05 | 1.27 | 0.43 |
| River 1 | Reach 1-Upper | 743 | 5YrCHI3Hr | 0.03 | 93.40 | 93.53 | 93.46 | 93.54 | 0.001159 | 0.20 | 0.13 | 1.95 | 0.21 |
| River 1 | Reach 1-Upper | 743 | 10YrCHI3Hr | 0.03 | 93.40 | 93.58 | 93.47 | 93.58 | 0.000560 | 0.19 | 0.19 | 2.40 | 0.16 |
| River 1 | Reach 1-Upper | 743 | 25YrCHI3Hr | 0.05 | 93.40 | 93.66 | 93.48 | 93.66 | 0.000255 | 0.16 | 0.29 | 3.39 | 0.11 |
| River 1 | Reach 1-Upper | 743 | 50YrCHI3Hr | 0.06 | 93.40 | 93.74 | 93.49 | 93.74 | 0.000125 | 0.14 | 0.40 | 5.00 | 0.08 |
| River 1 | Reach 1-Upper | 743 | 100YrCHI3Hr | 0.07 | 93.40 | 93.83 | 93.50 | 93.83 | 0.000071 | 0.13 | 0.52 | 7.13 | 0.07 |
| River 1 | Reach 1-Upper | 743 | 2YrSCS24Hr | 0.02 | 93.40 | 93.52 | 93.46 | 93.52 | 0.001463 | 0.21 | 0.11 | 1.84 | 0.23 |
| River 1 | Reach 1-Upper | 743 | 5YrSCS24Hr | 0.04 | 93.40 | 93.60 | 93.47 | 93.60 | 0.000466 | 0.18 | 0.21 | 2.59 | 0.14 |
| River 1 | Reach 1-Upper | 743 | 10YrSCS24Hr | 0.05 | 93.40 | 93.67 | 93.48 | 93.67 | 0.000228 | 0.16 | 0.30 | 3.72 | 0.11 |
| River 1 | Reach 1-Upper | 743 | 25YrSCS24Hr | 0.06 | 93.40 | 93.79 | 93.49 | 93.79 | 0.000091 | 0.14 | 0.46 | 6.17 | 0.07 |
| River 1 | Reach 1-Upper | 743 | 50YrSCS24Hr | 0.07 | 93.40 | 93.89 | 93.50 | 93.89 | 0.000054 | 0.12 | 0.59 | 7.75 | 0.06 |
| River 1 | Reach 1-Upper | 743 | 100YrSCS24Hr | 0.08 | 93.40 | 93.94 | 93.51 | 93.95 | 0.000049 | 0.13 | 0.66 | 9.45 | 0.06 |
| River 1 | Reach 1-Upper | 733 | | Culvert | | | | | | | | | |
| River 1 | Reach 1-Upper | 728 | 2YrCHI3Hr | 0.02 | 93.33 | 93.46 | 93.38 | 93.46 | 0.000507 | 0.12 | 0.12 | 1.51 | 0.14 |
| River 1 | Reach 1-Upper | 728 | 5YrCHI3Hr | 0.03 | 93.33 | 93.52 | 93.40 | 93.52 | 0.000283 | 0.13 | 0.20 | 1.94 | 0.11 |
| River 1 | Reach 1-Upper | 728 | 10YrCHI3Hr | 0.03 | 93.33 | 93.56 | 93.41 | 93.56 | 0.000213 | 0.13 | 0.26 | 2.26 | 0.10 |
| River 1 | Reach 1-Upper | 728 | 25YrCHI3Hr | 0.05 | 93.33 | 93.63 | 93.42 | 93.63 | 0.000137 | 0.13 | 0.36 | 2.78 | 0.08 |
| River 1 | Reach 1-Upper | 728 | 50YrCHI3Hr | 0.06 | 93.33 | 93.70 | 93.43 | 93.70 | 0.000088 | 0.13 | 0.45 | 3.31 | 0.07 |
| River 1 | Reach 1-Upper | 728 | 100YrCHI3Hr | 0.07 | 93.33 | 93.78 | 93.43 | 93.78 | 0.000060 | 0.12 | 0.56 | 4.21 | 0.06 |
| River 1 | Reach 1-Upper | 728 | 2YrSCS24Hr | 0.02 | 93.33 | 93.51 | 93.39 | 93.51 | 0.000306 | 0.13 | 0.19 | 1.87 | 0.11 |
| River 1 | Reach 1-Upper | 728 | 5YrSCS24Hr | 0.04 | 93.33 | 93.58 | 93.41 | 93.58 | 0.000196 | 0.14 | 0.28 | 2.37 | 0.10 |
| River 1 | Reach 1-Upper | 728 | 10YrSCS24Hr | 0.05 | 93.33 | 93.64 | 93.42 | 93.64 | 0.000129 | 0.13 | 0.37 | 2.86 | 0.08 |
| River 1 | Reach 1-Upper | 728 | 25YrSCS24Hr | 0.06 | 93.33 | 93.74 | 93.43 | 93.74 | 0.000071 | 0.12 | 0.51 | 3.65 | 0.06 |
| River 1 | Reach 1-Upper | 728 | 50YrSCS24Hr | 0.07 | 93.33 | 93.82 | 93.44 | 93.82 | 0.000049 | 0.12 | 0.63 | 6.17 | 0.06 |
| River 1 | Reach 1-Upper | 728 | 100YrSCS24Hr | 0.08 | 93.33 | 93.85 | 93.45 | 93.85 | 0.000053 | 0.13 | 0.67 | 10.91 | 0.06 |
| River 1 | Reach 1-Upper | 715 | 2YrCHI3Hr | 0.02 | 93.32 | 93.46 | 93.36 | 93.46 | 0.000165 | 0.09 | 0.17 | 2.22 | 0.08 |
| River 1 | Reach 1-Upper | 715 | 5YrCHI3Hr | 0.03 | 93.32 | 93.52 | 93.37 | 93.52 | 0.000134 | 0.10 | 0.25 | 2.80 | 0.08 |
| River 1 | Reach 1-Upper | 715 | 10YrCHI3Hr | 0.03 | 93.32 | 93.56 | 93.38 | 93.56 | 0.000117 | 0.11 | 0.31 | 3.23 | 0.08 |
| River 1 | Reach 1-Upper | 715 | 25YrCHI3Hr | 0.05 | 93.32 | 93.63 | 93.39 | 93.63 | 0.000086 | 0.12 | 0.41 | 3.92 | 0.07 |
| River 1 | Reach 1-Upper | 715 | 50YrCHI3Hr | 0.06 | 93.32 | 93.70 | 93.39 | 93.70 | 0.000061 | 0.11 | 0.51 | 4.63 | 0.06 |
| River 1 | Reach 1-Upper | 715 | 100YrCHI3Hr | 0.07 | 93.32 | 93.77 | 93.40 | 93.78 | 0.000044 | 0.11 | 0.61 | 9.10 | 0.05 |

HEC-RAS Plan: 20250603-Pre_Dev_v01 (Continued)

| River | Reach | River Sta | Profile | Q Total (m3/s) | Min Ch El (m) | W.S. Elev (m) | Crit W.S. (m) | E.G. Elev (m) | E.G. Slope (m/m) | Vel Chnl (m/s) | Flow Area (m2) | Top Width (m) | Froude # Chl |
|---------|---------------|-----------|--------------|-------------------|------------------|------------------|------------------|------------------|---------------------|-------------------|-------------------|------------------|--------------|
| River 1 | Reach 1-Upper | 715 | 2YrSCS24Hr | 0.02 | 93.32 | 93.51 | 93.36 | 93.51 | 0.000138 | 0.10 | 0.24 | 2.70 | 0.08 |
| River 1 | Reach 1-Upper | 715 | 5YrSCS24Hr | 0.04 | 93.32 | 93.57 | 93.38 | 93.57 | 0.000112 | 0.11 | 0.33 | 3.38 | 0.08 |
| River 1 | Reach 1-Upper | 715 | 10YrSCS24Hr | 0.05 | 93.32 | 93.64 | 93.39 | 93.64 | 0.000083 | 0.12 | 0.42 | 4.03 | 0.07 |
| River 1 | Reach 1-Upper | 715 | 25YrSCS24Hr | 0.06 | 93.32 | 93.74 | 93.40 | 93.74 | 0.000051 | 0.11 | 0.56 | 5.03 | 0.06 |
| River 1 | Reach 1-Upper | 715 | 50YrSCS24Hr | 0.07 | 93.32 | 93.82 | 93.40 | 93.82 | 0.000037 | 0.11 | 0.68 | 14.68 | 0.05 |
| River 1 | Reach 1-Upper | 715 | 100YrSCS24Hr | 0.08 | 93.32 | 93.85 | 93.41 | 93.85 | 0.000010 | 0.04 | 2.56 | 20.21 | 0.02 |
| River 1 | Reach 1-Upper | 705 | Culvert | | | | | | | | | | |
| River 1 | Reach 1-Upper | 698 | 2YrCHI3Hr | 0.02 | 93.24 | 93.31 | 93.29 | 93.31 | 0.009120 | 0.33 | 0.05 | 1.10 | 0.51 |
| River 1 | Reach 1-Upper | 698 | 5YrCHI3Hr | 0.03 | 93.24 | 93.31 | 93.30 | 93.32 | 0.019233 | 0.50 | 0.05 | 1.16 | 0.75 |
| River 1 | Reach 1-Upper | 698 | 10YrCHI3Hr | 0.03 | 93.24 | 93.31 | 93.31 | 93.33 | 0.027628 | 0.62 | 0.06 | 1.19 | 0.91 |
| River 1 | Reach 1-Upper | 698 | 25YrCHI3Hr | 0.05 | 93.24 | 93.42 | 93.32 | 93.43 | 0.000867 | 0.20 | 0.23 | 2.01 | 0.19 |
| River 1 | Reach 1-Upper | 698 | 50YrCHI3Hr | 0.06 | 93.24 | 93.51 | 93.33 | 93.51 | 0.000225 | 0.14 | 0.41 | 2.80 | 0.10 |
| River 1 | Reach 1-Upper | 698 | 100YrCHI3Hr | 0.07 | 93.24 | 93.51 | 93.34 | 93.51 | 0.000299 | 0.16 | 0.42 | 2.61 | 0.12 |
| River 1 | Reach 1-Upper | 698 | 2YrSCS24Hr | 0.02 | 93.24 | 93.31 | 93.30 | 93.32 | 0.015768 | 0.45 | 0.05 | 1.16 | 0.68 |
| River 1 | Reach 1-Upper | 698 | 5YrSCS24Hr | 0.04 | 93.24 | 93.32 | 93.31 | 93.34 | 0.027115 | 0.63 | 0.06 | 1.22 | 0.90 |
| River 1 | Reach 1-Upper | 698 | 10YrSCS24Hr | 0.05 | 93.24 | 93.47 | 93.32 | 93.47 | 0.000368 | 0.15 | 0.32 | 2.29 | 0.13 |
| River 1 | Reach 1-Upper | 698 | 25YrSCS24Hr | 0.06 | 93.24 | 93.51 | 93.33 | 93.51 | 0.000261 | 0.15 | 0.41 | 2.61 | 0.11 |
| River 1 | Reach 1-Upper | 698 | 50YrSCS24Hr | 0.07 | 93.24 | 93.51 | 93.34 | 93.52 | 0.000345 | 0.17 | 0.42 | 2.63 | 0.13 |
| River 1 | Reach 1-Upper | 698 | 100YrSCS24Hr | 0.08 | 93.24 | 93.52 | 93.35 | 93.52 | 0.000432 | 0.20 | 0.43 | 2.65 | 0.14 |
| River 1 | Reach 1-Upper | 681 | 2YrCHI3Hr | 0.02 | 93.14 | 93.21 | 93.18 | 93.21 | 0.004396 | 0.23 | 0.07 | 1.57 | 0.36 |
| River 1 | Reach 1-Upper | 681 | 5YrCHI3Hr | 0.03 | 93.14 | 93.24 | 93.19 | 93.24 | 0.001938 | 0.21 | 0.12 | 1.83 | 0.26 |
| River 1 | Reach 1-Upper | 681 | 10YrCHI3Hr | 0.03 | 93.14 | 93.27 | 93.20 | 93.27 | 0.001159 | 0.19 | 0.18 | 2.04 | 0.21 |
| River 1 | Reach 1-Upper | 681 | 25YrCHI3Hr | 0.05 | 93.14 | 93.42 | 93.21 | 93.42 | 0.000083 | 0.08 | 0.57 | 3.09 | 0.06 |
| River 1 | Reach 1-Upper | 681 | 50YrCHI3Hr | 0.06 | 93.14 | 93.51 | 93.22 | 93.51 | 0.000037 | 0.07 | 0.87 | 4.07 | 0.04 |
| River 1 | Reach 1-Upper | 681 | 100YrCHI3Hr | 0.07 | 93.14 | 93.51 | 93.22 | 93.51 | 0.000050 | 0.08 | 0.88 | 4.10 | 0.05 |
| River 1 | Reach 1-Upper | 681 | 2YrSCS24Hr | 0.02 | 93.14 | 93.23 | 93.19 | 93.24 | 0.002334 | 0.22 | 0.11 | 1.78 | 0.28 |
| River 1 | Reach 1-Upper | 681 | 5YrSCS24Hr | 0.04 | 93.14 | 93.29 | 93.20 | 93.29 | 0.000854 | 0.18 | 0.21 | 2.14 | 0.18 |
| River 1 | Reach 1-Upper | 681 | 10YrSCS24Hr | 0.05 | 93.14 | 93.46 | 93.21 | 93.46 | 0.000050 | 0.07 | 0.70 | 3.45 | 0.05 |
| River 1 | Reach 1-Upper | 681 | 25YrSCS24Hr | 0.06 | 93.14 | 93.51 | 93.22 | 93.51 | 0.000043 | 0.07 | 0.88 | 4.08 | 0.05 |
| River 1 | Reach 1-Upper | 681 | 50YrSCS24Hr | 0.07 | 93.14 | 93.51 | 93.23 | 93.51 | 0.000058 | 0.08 | 0.89 | 4.12 | 0.05 |
| River 1 | Reach 1-Upper | 681 | 100YrSCS24Hr | 0.08 | 93.14 | 93.52 | 93.23 | 93.52 | 0.000073 | 0.09 | 0.90 | 4.16 | 0.06 |
| River 1 | Reach 1-Upper | 663 | 2YrCHI3Hr | 0.02 | 93.05 | 93.18 | | 93.18 | 0.000677 | 0.14 | 0.11 | 1.31 | 0.15 |
| River 1 | Reach 1-Upper | 663 | 5YrCHI3Hr | 0.03 | 93.05 | 93.22 | | 93.23 | 0.000607 | 0.15 | 0.17 | 1.60 | 0.15 |
| River 1 | Reach 1-Upper | 663 | 10YrCHI3Hr | 0.03 | 93.05 | 93.26 | | 93.26 | 0.000492 | 0.15 | 0.23 | 1.84 | 0.14 |
| River 1 | Reach 1-Upper | 663 | 25YrCHI3Hr | 0.05 | 93.05 | 93.42 | | 93.42 | 0.000064 | 0.07 | 0.63 | 3.25 | 0.05 |
| River 1 | Reach 1-Upper | 663 | 50YrCHI3Hr | 0.06 | 93.05 | 93.51 | | 93.51 | 0.000032 | 0.06 | 0.96 | 4.42 | 0.04 |
| River 1 | Reach 1-Upper | 663 | 100YrCHI3Hr | 0.07 | 93.05 | 93.51 | | 93.51 | 0.000043 | 0.07 | 0.97 | 4.46 | 0.05 |
| River 1 | Reach 1-Upper | 663 | 2YrSCS24Hr | 0.02 | 93.05 | 93.21 | | 93.22 | 0.000676 | 0.16 | 0.15 | 1.53 | 0.16 |
| River 1 | Reach 1-Upper | 663 | 5YrSCS24Hr | 0.04 | 93.05 | 93.28 | | 93.28 | 0.000393 | 0.14 | 0.26 | 1.97 | 0.13 |
| River 1 | Reach 1-Upper | 663 | 10YrSCS24Hr | 0.05 | 93.05 | 93.46 | | 93.46 | 0.000042 | 0.06 | 0.78 | 3.77 | 0.04 |
| River 1 | Reach 1-Upper | 663 | 25YrSCS24Hr | 0.06 | 93.05 | 93.51 | | 93.51 | 0.000037 | 0.06 | 0.96 | 4.44 | 0.04 |
| River 1 | Reach 1-Upper | 663 | 50YrSCS24Hr | 0.07 | 93.05 | 93.51 | | 93.51 | 0.000050 | 0.08 | 0.97 | 4.48 | 0.05 |
| River 1 | Reach 1-Upper | 663 | 100YrSCS24Hr | 0.08 | 93.05 | 93.51 | | 93.52 | 0.000064 | 0.09 | 0.99 | 4.53 | 0.06 |
| River 1 | Reach 1-Upper | 656 | 2YrCHI3Hr | 0.06 | 93.03 | 93.15 | 93.12 | 93.16 | 0.008107 | 0.46 | 0.12 | 1.65 | 0.53 |
| River 1 | Reach 1-Upper | 656 | 5YrCHI3Hr | 0.10 | 93.03 | 93.19 | 93.14 | 93.20 | 0.006746 | 0.51 | 0.20 | 1.91 | 0.51 |
| River 1 | Reach 1-Upper | 656 | 10YrCHI3Hr | 0.14 | 93.03 | 93.23 | 93.16 | 93.24 | 0.004212 | 0.48 | 0.29 | 2.15 | 0.42 |
| River 1 | Reach 1-Upper | 656 | 25YrCHI3Hr | 0.18 | 93.03 | 93.42 | 93.18 | 93.42 | 0.000424 | 0.23 | 0.79 | 3.69 | 0.15 |
| River 1 | Reach 1-Upper | 656 | 50YrCHI3Hr | 0.22 | 93.03 | 93.51 | 93.20 | 93.51 | 0.000220 | 0.20 | 1.16 | 4.65 | 0.11 |
| River 1 | Reach 1-Upper | 656 | 100YrCHI3Hr | 0.26 | 93.03 | 93.51 | 93.21 | 93.51 | 0.000302 | 0.24 | 1.17 | 4.66 | 0.13 |
| River 1 | Reach 1-Upper | 656 | 2YrSCS24Hr | 0.09 | 93.03 | 93.18 | 93.14 | 93.19 | 0.007190 | 0.50 | 0.18 | 1.85 | 0.52 |
| River 1 | Reach 1-Upper | 656 | 5YrSCS24Hr | 0.15 | 93.03 | 93.26 | 93.17 | 93.27 | 0.003060 | 0.44 | 0.34 | 2.29 | 0.36 |
| River 1 | Reach 1-Upper | 656 | 10YrSCS24Hr | 0.19 | 93.03 | 93.46 | 93.18 | 93.46 | 0.000269 | 0.21 | 0.96 | 4.20 | 0.12 |
| River 1 | Reach 1-Upper | 656 | 25YrSCS24Hr | 0.24 | 93.03 | 93.51 | 93.20 | 93.51 | 0.000267 | 0.23 | 1.17 | 4.65 | 0.12 |
| River 1 | Reach 1-Upper | 656 | 50YrSCS24Hr | 0.28 | 93.03 | 93.51 | 93.22 | 93.51 | 0.000363 | 0.26 | 1.17 | 4.66 | 0.14 |
| River 1 | Reach 1-Upper | 656 | 100YrSCS24Hr | 0.33 | 93.03 | 93.51 | 93.23 | 93.51 | 0.000481 | 0.30 | 1.18 | 4.68 | 0.16 |
| River 1 | Reach 1-Upper | 638 | 2YrCHI3Hr | 0.06 | 92.92 | 93.07 | 93.00 | 93.08 | 0.002802 | 0.32 | 0.18 | 1.81 | 0.32 |
| River 1 | Reach 1-Upper | 638 | 5YrCHI3Hr | 0.10 | 92.92 | 93.14 | 93.04 | 93.14 | 0.001935 | 0.33 | 0.31 | 2.24 | 0.28 |
| River 1 | Reach 1-Upper | 638 | 10YrCHI3Hr | 0.14 | 92.92 | 93.20 | 93.05 | 93.21 | 0.001072 | 0.29 | 0.48 | 2.76 | 0.22 |
| River 1 | Reach 1-Upper | 638 | 25YrCHI3Hr | 0.18 | 92.92 | 93.41 | 93.07 | 93.42 | 0.000128 | 0.15 | 1.31 | 5.26 | 0.08 |
| River 1 | Reach 1-Upper | 638 | 50YrCHI3Hr | 0.22 | 92.92 | 93.50 | 93.09 | 93.51 | 0.000082 | 0.14 | 1.86 | 6.83 | 0.07 |
| River 1 | Reach 1-Upper | 638 | 100YrCHI3Hr | 0.26 | 92.92 | 93.50 | 93.10 | 93.51 | 0.000114 | 0.16 | 1.86 | 6.84 | 0.08 |
| River 1 | Reach 1-Upper | 638 | 2YrSCS24Hr | 0.09 | 92.92 | 93.12 | 93.03 | 93.12 | 0.002288 | 0.34 | 0.27 | 2.11 | 0.30 |
| River 1 | Reach 1-Upper | 638 | 5YrSCS24Hr | 0.15 | 92.92 | 93.24 | 93.06 | 93.24 | 0.000804 | 0.26 | 0.57 | 3.07 | 0.19 |
| River 1 | Reach 1-Upper | 638 | 10YrSCS24Hr | 0.19 | 92.92 | 93.46 | 93.08 | 93.46 | 0.000092 | 0.14 | 1.57 | 6.15 | 0.07 |
| River 1 | Reach 1-Upper | 638 | 25YrSCS24Hr | 0.24 | 92.92 | 93.50 | 93.10 | 93.51 | 0.000100 | 0.15 | 1.86 | 6.83 | 0.08 |
| River 1 | Reach 1-Upper | 638 | 50YrSCS24Hr | 0.28 | 92.92 | 93.50 | 93.11 | 93.51 | 0.000137 | 0.18 | 1.87 | 6.84 | 0.09 |
| River 1 | Reach 1-Upper | 638 | 100YrSCS24Hr | 0.33 | 92.92 | 93.51 | 93.13 | 93.51 | 0.000184 | 0.20 | 1.87 | 6.85 | 0.10 |
| River 1 | Reach 1-Upper | 617 | 2YrCHI3Hr | 0.06 | 92.84 | 93.01 | 92.95 | 93.01 | 0.003253 | 0.32 | 0.18 | 1.96 | 0.34 |
| River 1 | Reach 1-Upper | 617 | 5YrCHI3Hr | 0.10 | 92.84 | 93.11 | 92.98 | 93.11 | 0.000952 | 0.24 | 0.43 | 2.97 | 0.20 |
| River 1 | Reach 1-Upper | 617 | 10YrCHI3Hr | 0.14 | 92.84 | 93.19 | 93.00 | 93.19 | 0.000453 | 0.19 | 0.70 | 3.82 | 0.14 |
| River 1 | Reach 1-Upper | 617 | 25YrCHI3Hr | 0.18 | 92.84 | 93.41 | 93.01 | 93.41 | 0.000070 | 0.09 | 1.97 | 8.09 | 0.06 |
| River 1 | Reach 1-Upper | 617 | 50YrCHI3Hr | 0.22 | 92.84 | 93.50 | 93.03 | 93.50 | 0.000037 | 0.08 | 2.93 | 15.17 | 0.05 |
| River 1 | Reach 1-Upper | 617 | 100YrCHI3Hr | 0.26 | 92.84 | 93.50 | 93.04 | 93.50 | 0.000051 | 0.09 | 2.93 | 15.17 | 0.05 |
| River 1 | Reach 1-Upper | 617 | 2YrSCS24Hr | 0.09 | 92.84 | 93.08 | 92.97 | 93.09 | 0.001277 | 0.26 | 0.35 | 2.70 | 0.23 |
| River 1 | Reach 1-Upper | 617 | 5YrSCS24Hr | 0.15 | 92.84 | 93.23 | 93.00 | 93.23 | 0.000340 | 0.18 | 0.84 | 4.32 | 0.13 |
| River 1 | Reach 1-Upper | 617 | 10YrSCS24Hr | 0.19 | 92.84 | 93.46 | 93.02 | 93.46 | 0.000046 | 0.08 | 2.37 | 10.22 | 0.05 |
| River 1 | Reach 1-Upper | 617 | 25YrSCS24Hr | 0.24 | 92.84 | 93.50 | 93.04 | 93.50 | 0.000045 | 0.09 | 2.93 | 15.17 | 0.05 |
| River 1 | Reach 1-Upper | 617 | 50YrSCS24Hr | 0.28 | 92.84 | 93.50 | 93.05 | 93.50 | 0.000062 | 0.10 | 2.93 | 15.17 | 0.06 |
| River 1 | Reach 1-Upper | 617 | 100YrSCS24Hr | 0.33 | 92.84 | 93.50 | 93.06 | 93.50 | 0.000083 | 0.12 | 2.93 | 15.18 | 0.07 |
| River 1 | Reach 1-Upper | 598 | 2YrCHI3Hr | 0.06 | 92.76 | 92.99 | 92.86 | 92.99 | 0.000555 | 0.18 | 0.33 | 2.52 | 0.15 |
| River 1 | Reach 1-Upper | 598 | 5YrCHI3Hr | 0.11 | 92.76 | 93.10 | 92.89 | 93.10 | 0.000269 | 0.18 | 0.61 | 3.40 | 0.12 |
| River 1 | Reach 1-Upper | 598 | 10YrCHI3Hr | 0.15 | 92.76 | 93.19 | 92.91 | 93.19 | 0.000175 | 0.18 | 0.82 | 5.45 | 0.10 |

HEC-RAS Plan: 20250603-Pre_Dev_v01 (Continued)

| River | Reach | River Sta | Profile | Q Total (m3/s) | Min Ch El (m) | W.S. Elev (m) | Crit W.S. (m) | E.G. Elev (m) | E.G. Slope (m/m) | Vel Chnl (m/s) | Flow Area (m2) | Top Width (m) | Froude # Chl |
|---------|---------------|-----------|--------------|-------------------|------------------|------------------|------------------|------------------|---------------------|-------------------|-------------------|------------------|--------------|
| River 1 | Reach 1-Upper | 598 | 25YrCHI3Hr | 0.19 | 92.76 | 93.41 | 92.93 | 93.41 | 0.000054 | 0.14 | 1.39 | 9.84 | 0.06 |
| River 1 | Reach 1-Upper | 598 | 50YrCHI3Hr | 0.23 | 92.76 | 93.50 | 92.94 | 93.50 | 0.000020 | 0.08 | 4.94 | 31.21 | 0.04 |
| River 1 | Reach 1-Upper | 598 | 100YrCHI3Hr | 0.28 | 92.76 | 93.50 | 92.96 | 93.50 | 0.000028 | 0.09 | 4.93 | 31.21 | 0.04 |
| River 1 | Reach 1-Upper | 598 | 2YrSCS24Hr | 0.10 | 92.76 | 93.07 | 92.88 | 93.07 | 0.000322 | 0.18 | 0.53 | 3.17 | 0.12 |
| River 1 | Reach 1-Upper | 598 | 5YrSCS24Hr | 0.16 | 92.76 | 93.22 | 92.91 | 93.22 | 0.000147 | 0.17 | 0.91 | 6.16 | 0.09 |
| River 1 | Reach 1-Upper | 598 | 10YrSCS24Hr | 0.20 | 92.76 | 93.46 | 92.93 | 93.46 | 0.000045 | 0.13 | 1.50 | 22.56 | 0.06 |
| River 1 | Reach 1-Upper | 598 | 25YrSCS24Hr | 0.26 | 92.76 | 93.50 | 92.95 | 93.50 | 0.000025 | 0.09 | 4.94 | 31.21 | 0.04 |
| River 1 | Reach 1-Upper | 598 | 50YrSCS24Hr | 0.30 | 92.76 | 93.50 | 92.96 | 93.50 | 0.000034 | 0.10 | 4.93 | 31.21 | 0.05 |
| River 1 | Reach 1-Upper | 598 | 100YrSCS24Hr | 0.35 | 92.76 | 93.50 | 92.98 | 93.50 | 0.000046 | 0.12 | 4.93 | 31.21 | 0.05 |
| River 1 | Reach 1-Upper | 589 | | Culvert | | | | | | | | | |
| River 1 | Reach 1-Upper | 581 | 2YrCHI3Hr | 0.06 | 92.71 | 92.89 | 92.81 | 92.89 | 0.002032 | 0.27 | 0.23 | 2.59 | 0.28 |
| River 1 | Reach 1-Upper | 581 | 5YrCHI3Hr | 0.11 | 92.71 | 92.93 | 92.84 | 92.93 | 0.001970 | 0.33 | 0.33 | 3.40 | 0.29 |
| River 1 | Reach 1-Upper | 581 | 10YrCHI3Hr | 0.15 | 92.71 | 92.96 | 92.86 | 92.97 | 0.001571 | 0.34 | 0.42 | 4.10 | 0.27 |
| River 1 | Reach 1-Upper | 581 | 25YrCHI3Hr | 0.19 | 92.71 | 93.04 | 92.88 | 93.04 | 0.000858 | 0.32 | 0.60 | 5.44 | 0.21 |
| River 1 | Reach 1-Upper | 581 | 50YrCHI3Hr | 0.23 | 92.71 | 93.19 | 92.89 | 93.19 | 0.000244 | 0.24 | 0.98 | 9.64 | 0.12 |
| River 1 | Reach 1-Upper | 581 | 100YrCHI3Hr | 0.28 | 92.71 | 93.25 | 92.90 | 93.25 | 0.000213 | 0.24 | 1.13 | 30.32 | 0.12 |
| River 1 | Reach 1-Upper | 581 | 2YrSCS24Hr | 0.10 | 92.71 | 92.92 | 92.83 | 92.92 | 0.002062 | 0.32 | 0.30 | 3.18 | 0.29 |
| River 1 | Reach 1-Upper | 581 | 5YrSCS24Hr | 0.16 | 92.71 | 92.98 | 92.86 | 92.99 | 0.001381 | 0.34 | 0.46 | 4.41 | 0.25 |
| River 1 | Reach 1-Upper | 581 | 10YrSCS24Hr | 0.20 | 92.71 | 93.05 | 92.88 | 93.06 | 0.000735 | 0.31 | 0.65 | 5.75 | 0.20 |
| River 1 | Reach 1-Upper | 581 | 25YrSCS24Hr | 0.26 | 92.71 | 93.25 | 92.90 | 93.25 | 0.000187 | 0.23 | 1.13 | 30.32 | 0.11 |
| River 1 | Reach 1-Upper | 581 | 50YrSCS24Hr | 0.30 | 92.71 | 93.26 | 92.91 | 93.26 | 0.000245 | 0.26 | 1.15 | 30.62 | 0.12 |
| River 1 | Reach 1-Upper | 581 | 100YrSCS24Hr | 0.35 | 92.71 | 93.30 | 92.92 | 93.30 | 0.000057 | 0.11 | 4.83 | 35.67 | 0.06 |
| River 1 | Reach 1-Upper | 572 | 2YrCHI3Hr | 0.06 | 92.73 | 92.84 | 92.82 | 92.85 | 0.009130 | 0.45 | 0.13 | 1.96 | 0.55 |
| River 1 | Reach 1-Upper | 572 | 5YrCHI3Hr | 0.11 | 92.73 | 92.90 | 92.84 | 92.90 | 0.004896 | 0.43 | 0.26 | 2.58 | 0.43 |
| River 1 | Reach 1-Upper | 572 | 10YrCHI3Hr | 0.15 | 92.73 | 92.94 | 92.86 | 92.95 | 0.002649 | 0.37 | 0.39 | 3.10 | 0.33 |
| River 1 | Reach 1-Upper | 572 | 25YrCHI3Hr | 0.19 | 92.73 | 93.03 | 92.88 | 93.03 | 0.001021 | 0.28 | 0.70 | 4.09 | 0.22 |
| River 1 | Reach 1-Upper | 572 | 50YrCHI3Hr | 0.23 | 92.73 | 93.19 | 92.89 | 93.19 | 0.000155 | 0.14 | 2.22 | 26.73 | 0.09 |
| River 1 | Reach 1-Upper | 572 | 100YrCHI3Hr | 0.28 | 92.73 | 93.25 | 92.90 | 93.25 | 0.000074 | 0.11 | 4.09 | 35.89 | 0.06 |
| River 1 | Reach 1-Upper | 572 | 2YrSCS24Hr | 0.10 | 92.73 | 92.88 | 92.84 | 92.89 | 0.005898 | 0.44 | 0.22 | 2.42 | 0.47 |
| River 1 | Reach 1-Upper | 572 | 5YrSCS24Hr | 0.16 | 92.73 | 92.96 | 92.86 | 92.97 | 0.002084 | 0.34 | 0.46 | 3.34 | 0.30 |
| River 1 | Reach 1-Upper | 572 | 10YrSCS24Hr | 0.20 | 92.73 | 93.05 | 92.88 | 93.05 | 0.000824 | 0.26 | 0.78 | 4.31 | 0.20 |
| River 1 | Reach 1-Upper | 572 | 25YrSCS24Hr | 0.26 | 92.73 | 93.25 | 92.90 | 93.25 | 0.000065 | 0.10 | 4.09 | 35.88 | 0.06 |
| River 1 | Reach 1-Upper | 572 | 50YrSCS24Hr | 0.30 | 92.73 | 93.26 | 92.91 | 93.26 | 0.000079 | 0.12 | 4.37 | 36.88 | 0.07 |
| River 1 | Reach 1-Upper | 572 | 100YrSCS24Hr | 0.35 | 92.73 | 93.30 | 92.92 | 93.30 | 0.000050 | 0.10 | 6.26 | 42.85 | 0.05 |
| River 1 | Reach 1-Upper | 555 | 2YrCHI3Hr | 0.06 | 92.61 | 92.81 | 92.71 | 92.81 | 0.000983 | 0.20 | 0.31 | 2.93 | 0.20 |
| River 1 | Reach 1-Upper | 555 | 5YrCHI3Hr | 0.11 | 92.61 | 92.87 | 92.74 | 92.87 | 0.000748 | 0.21 | 0.52 | 3.73 | 0.18 |
| River 1 | Reach 1-Upper | 555 | 10YrCHI3Hr | 0.15 | 92.61 | 92.93 | 92.75 | 92.93 | 0.000479 | 0.19 | 0.76 | 4.46 | 0.15 |
| River 1 | Reach 1-Upper | 555 | 25YrCHI3Hr | 0.19 | 92.61 | 93.02 | 92.77 | 93.02 | 0.000238 | 0.16 | 1.22 | 5.62 | 0.11 |
| River 1 | Reach 1-Upper | 555 | 50YrCHI3Hr | 0.23 | 92.61 | 93.19 | 92.78 | 93.19 | 0.000031 | 0.08 | 4.98 | 37.27 | 0.04 |
| River 1 | Reach 1-Upper | 555 | 100YrCHI3Hr | 0.28 | 92.61 | 93.25 | 92.80 | 93.25 | 0.000018 | 0.06 | 7.39 | 40.94 | 0.03 |
| River 1 | Reach 1-Upper | 555 | 2YrSCS24Hr | 0.10 | 92.61 | 92.85 | 92.73 | 92.85 | 0.000851 | 0.21 | 0.45 | 3.50 | 0.19 |
| River 1 | Reach 1-Upper | 555 | 5YrSCS24Hr | 0.16 | 92.61 | 92.95 | 92.76 | 92.95 | 0.000402 | 0.18 | 0.87 | 4.75 | 0.14 |
| River 1 | Reach 1-Upper | 555 | 10YrSCS24Hr | 0.20 | 92.61 | 93.04 | 92.77 | 93.04 | 0.000197 | 0.15 | 1.34 | 5.96 | 0.10 |
| River 1 | Reach 1-Upper | 555 | 25YrSCS24Hr | 0.26 | 92.61 | 93.25 | 92.79 | 93.25 | 0.000016 | 0.06 | 7.39 | 40.94 | 0.03 |
| River 1 | Reach 1-Upper | 555 | 50YrSCS24Hr | 0.30 | 92.61 | 93.26 | 92.81 | 93.26 | 0.000020 | 0.07 | 7.70 | 41.13 | 0.03 |
| River 1 | Reach 1-Upper | 555 | 100YrSCS24Hr | 0.35 | 92.61 | 93.30 | 92.82 | 93.30 | 0.000015 | 0.06 | 9.71 | 43.21 | 0.03 |
| River 1 | Reach 1-Upper | 534 | 2YrCHI3Hr | 0.06 | 92.59 | 92.78 | 92.69 | 92.78 | 0.001540 | 0.24 | 0.25 | 2.41 | 0.24 |
| River 1 | Reach 1-Upper | 534 | 5YrCHI3Hr | 0.11 | 92.59 | 92.85 | 92.72 | 92.86 | 0.001007 | 0.24 | 0.46 | 3.30 | 0.21 |
| River 1 | Reach 1-Upper | 534 | 10YrCHI3Hr | 0.15 | 92.59 | 92.92 | 92.74 | 92.92 | 0.000570 | 0.21 | 0.74 | 8.51 | 0.16 |
| River 1 | Reach 1-Upper | 534 | 25YrCHI3Hr | 0.19 | 92.59 | 93.02 | 92.76 | 93.02 | 0.000095 | 0.11 | 3.36 | 40.28 | 0.07 |
| River 1 | Reach 1-Upper | 534 | 50YrCHI3Hr | 0.23 | 92.59 | 93.19 | 92.78 | 93.19 | 0.000006 | 0.04 | 11.46 | 51.16 | 0.02 |
| River 1 | Reach 1-Upper | 534 | 100YrCHI3Hr | 0.28 | 92.59 | 93.25 | 92.79 | 93.25 | 0.000004 | 0.03 | 14.61 | 51.39 | 0.02 |
| River 1 | Reach 1-Upper | 534 | 2YrSCS24Hr | 0.10 | 92.59 | 92.83 | 92.71 | 92.83 | 0.001214 | 0.25 | 0.39 | 3.03 | 0.22 |
| River 1 | Reach 1-Upper | 534 | 5YrSCS24Hr | 0.16 | 92.59 | 92.94 | 92.75 | 92.95 | 0.000422 | 0.19 | 1.07 | 17.97 | 0.14 |
| River 1 | Reach 1-Upper | 534 | 10YrSCS24Hr | 0.20 | 92.59 | 93.04 | 92.76 | 93.04 | 0.000064 | 0.09 | 4.23 | 42.61 | 0.06 |
| River 1 | Reach 1-Upper | 534 | 25YrSCS24Hr | 0.26 | 92.59 | 93.25 | 92.78 | 93.25 | 0.000003 | 0.03 | 14.61 | 51.39 | 0.01 |
| River 1 | Reach 1-Upper | 534 | 50YrSCS24Hr | 0.30 | 92.59 | 93.26 | 92.80 | 93.26 | 0.000004 | 0.03 | 14.99 | 51.42 | 0.02 |
| River 1 | Reach 1-Upper | 534 | 100YrSCS24Hr | 0.35 | 92.59 | 93.30 | 92.81 | 93.30 | 0.000004 | 0.03 | 17.46 | 51.60 | 0.02 |
| River 1 | Reach 1-Upper | 510 | 2YrCHI3Hr | 0.06 | 92.60 | 92.71 | 92.67 | 92.72 | 0.005825 | 0.43 | 0.14 | 2.60 | 0.46 |
| River 1 | Reach 1-Upper | 510 | 5YrCHI3Hr | 0.11 | 92.60 | 92.82 | 92.70 | 92.83 | 0.001169 | 0.34 | 0.32 | 4.18 | 0.24 |
| River 1 | Reach 1-Upper | 510 | 10YrCHI3Hr | 0.15 | 92.60 | 92.90 | 92.72 | 92.90 | 0.000712 | 0.32 | 0.45 | 5.29 | 0.20 |
| River 1 | Reach 1-Upper | 510 | 25YrCHI3Hr | 0.19 | 92.60 | 93.01 | 92.73 | 93.01 | 0.000421 | 0.31 | 0.62 | 14.09 | 0.16 |
| River 1 | Reach 1-Upper | 510 | 50YrCHI3Hr | 0.23 | 92.60 | 93.18 | 92.75 | 93.19 | 0.000180 | 0.26 | 0.90 | 109.29 | 0.11 |
| River 1 | Reach 1-Upper | 510 | 100YrCHI3Hr | 0.28 | 92.60 | 93.25 | 92.77 | 93.25 | 0.000000 | 0.01 | 42.37 | 109.53 | 0.00 |
| River 1 | Reach 1-Upper | 510 | 2YrSCS24Hr | 0.10 | 92.60 | 92.79 | 92.69 | 92.80 | 0.001503 | 0.34 | 0.28 | 3.79 | 0.26 |
| River 1 | Reach 1-Upper | 510 | 5YrSCS24Hr | 0.16 | 92.60 | 92.93 | 92.72 | 92.93 | 0.000617 | 0.32 | 0.49 | 5.78 | 0.19 |
| River 1 | Reach 1-Upper | 510 | 10YrSCS24Hr | 0.20 | 92.60 | 93.03 | 92.74 | 93.04 | 0.000378 | 0.31 | 0.66 | 15.54 | 0.15 |
| River 1 | Reach 1-Upper | 510 | 25YrSCS24Hr | 0.26 | 92.60 | 93.25 | 92.76 | 93.25 | 0.000000 | 0.01 | 42.37 | 109.53 | 0.00 |
| River 1 | Reach 1-Upper | 510 | 50YrSCS24Hr | 0.30 | 92.60 | 93.26 | 92.78 | 93.26 | 0.000000 | 0.01 | 43.19 | 109.55 | 0.01 |
| River 1 | Reach 1-Upper | 510 | 100YrSCS24Hr | 0.35 | 92.60 | 93.30 | 92.79 | 93.30 | 0.000000 | 0.01 | 48.45 | 109.72 | 0.00 |
| River 1 | Reach 1-Upper | 505 | | Culvert | | | | | | | | | |
| River 1 | Reach 1-Upper | 502 | 2YrCHI3Hr | 0.07 | 92.49 | 92.60 | 92.57 | 92.61 | 0.007956 | 0.50 | 0.13 | 2.20 | 0.54 |
| River 1 | Reach 1-Upper | 502 | 5YrCHI3Hr | 0.12 | 92.49 | 92.65 | 92.60 | 92.67 | 0.006462 | 0.60 | 0.20 | 2.74 | 0.52 |
| River 1 | Reach 1-Upper | 502 | 10YrCHI3Hr | 0.16 | 92.49 | 92.68 | 92.62 | 92.70 | 0.006042 | 0.66 | 0.25 | 3.06 | 0.52 |
| River 1 | Reach 1-Upper | 502 | 25YrCHI3Hr | 0.22 | 92.49 | 92.73 | 92.64 | 92.76 | 0.004047 | 0.66 | 0.33 | 4.01 | 0.45 |
| River 1 | Reach 1-Upper | 502 | 50YrCHI3Hr | 0.26 | 92.49 | 92.83 | 92.66 | 92.85 | 0.001665 | 0.54 | 0.48 | 5.45 | 0.31 |
| River 1 | Reach 1-Upper | 502 | 100YrCHI3Hr | 0.31 | 92.49 | 92.99 | 92.68 | 93.00 | 0.000619 | 0.43 | 0.72 | 104.79 | 0.20 |
| River 1 | Reach 1-Upper | 502 | 2YrSCS24Hr | 0.11 | 92.49 | 92.64 | 92.59 | 92.65 | 0.006729 | 0.58 | 0.19 | 2.62 | 0.53 |
| River 1 | Reach 1-Upper | 502 | 5YrSCS24Hr | 0.18 | 92.49 | 92.69 | 92.63 | 92.71 | 0.005546 | 0.67 | 0.27 | 3.21 | 0.51 |
| River 1 | Reach 1-Upper | 502 | 10YrSCS24Hr | 0.23 | 92.49 | 92.75 | 92.65 | 92.77 | 0.003381 | 0.64 | 0.36 | 4.41 | 0.42 |
| River 1 | Reach 1-Upper | 502 | 25YrSCS24Hr | 0.29 | 92.49 | 92.92 | 92.67 | 92.94 | 0.000902 | 0.47 | 0.62 | 7.34 | 0.24 |
| River 1 | Reach 1-Upper | 502 | 50YrSCS24Hr | 0.34 | 92.49 | 93.11 | 92.69 | 93.12 | 0.000353 | 0.38 | 0.90 | 105.15 | 0.16 |

HEC-RAS Plan: 20250603-Pre_Dev_v01 (Continued)

| River | Reach | River Sta | Profile | Q Total (m3/s) | Min Ch El (m) | W.S. Elev (m) | Crit W.S. (m) | E.G. Elev (m) | E.G. Slope (m/m) | Vel Chnl (m/s) | Flow Area (m2) | Top Width (m) | Froude # Chl |
|---------|---------------|-----------|--------------|-------------------|------------------|------------------|------------------|------------------|---------------------|-------------------|-------------------|------------------|--------------|
| River 1 | Reach 1-Upper | 502 | 100YrSCS24Hr | 0.40 | 92.49 | 93.30 | 92.71 | 93.30 | 0.000000 | 0.01 | 51.89 | 105.65 | 0.00 |
| River 1 | Reach 1-Upper | 493 | 2YrCHI3Hr | 0.07 | 92.34 | 92.60 | 92.42 | 92.60 | 0.000124 | 0.09 | 0.72 | 4.59 | 0.07 |
| River 1 | Reach 1-Upper | 493 | 5YrCHI3Hr | 0.12 | 92.34 | 92.65 | 92.45 | 92.65 | 0.000198 | 0.13 | 0.96 | 5.44 | 0.10 |
| River 1 | Reach 1-Upper | 493 | 10YrCHI3Hr | 0.16 | 92.34 | 92.68 | 92.46 | 92.68 | 0.000233 | 0.14 | 1.13 | 5.98 | 0.10 |
| River 1 | Reach 1-Upper | 493 | 25YrCHI3Hr | 0.22 | 92.34 | 92.74 | 92.48 | 92.74 | 0.000196 | 0.14 | 1.51 | 6.84 | 0.10 |
| River 1 | Reach 1-Upper | 493 | 50YrCHI3Hr | 0.26 | 92.34 | 92.84 | 92.49 | 92.84 | 0.000098 | 0.12 | 2.27 | 8.59 | 0.07 |
| River 1 | Reach 1-Upper | 493 | 100YrCHI3Hr | 0.31 | 92.34 | 93.00 | 92.50 | 93.00 | 0.000001 | 0.02 | 28.79 | 101.37 | 0.01 |
| River 1 | Reach 1-Upper | 493 | 2YrSCS24Hr | 0.11 | 92.34 | 92.64 | 92.44 | 92.64 | 0.000183 | 0.12 | 0.90 | 5.23 | 0.09 |
| River 1 | Reach 1-Upper | 493 | 5YrSCS24Hr | 0.18 | 92.34 | 92.70 | 92.46 | 92.70 | 0.000231 | 0.15 | 1.22 | 6.23 | 0.11 |
| River 1 | Reach 1-Upper | 493 | 10YrSCS24Hr | 0.23 | 92.34 | 92.76 | 92.48 | 92.76 | 0.000169 | 0.14 | 1.63 | 7.02 | 0.09 |
| River 1 | Reach 1-Upper | 493 | 25YrSCS24Hr | 0.29 | 92.34 | 92.93 | 92.50 | 92.93 | 0.000047 | 0.09 | 3.20 | 13.20 | 0.05 |
| River 1 | Reach 1-Upper | 493 | 50YrSCS24Hr | 0.34 | 92.34 | 93.12 | 92.51 | 93.12 | 0.000001 | 0.01 | 41.12 | 102.01 | 0.01 |
| River 1 | Reach 1-Upper | 493 | 100YrSCS24Hr | 0.40 | 92.34 | 93.30 | 92.52 | 93.30 | 0.000000 | 0.01 | 60.16 | 102.98 | 0.00 |
| River 1 | Reach 1-Upper | 474 | 2YrCHI3Hr | 0.07 | 92.41 | 92.60 | 92.50 | 92.60 | 0.000594 | 0.14 | 0.47 | 4.97 | 0.15 |
| River 1 | Reach 1-Upper | 474 | 5YrCHI3Hr | 0.12 | 92.41 | 92.64 | 92.53 | 92.65 | 0.000595 | 0.17 | 0.72 | 5.95 | 0.16 |
| River 1 | Reach 1-Upper | 474 | 10YrCHI3Hr | 0.16 | 92.41 | 92.67 | 92.54 | 92.68 | 0.000563 | 0.18 | 0.90 | 6.59 | 0.15 |
| River 1 | Reach 1-Upper | 474 | 25YrCHI3Hr | 0.22 | 92.41 | 92.73 | 92.56 | 92.74 | 0.000352 | 0.16 | 1.33 | 7.87 | 0.13 |
| River 1 | Reach 1-Upper | 474 | 50YrCHI3Hr | 0.26 | 92.41 | 92.84 | 92.57 | 92.84 | 0.000001 | 0.01 | 25.75 | 91.49 | 0.01 |
| River 1 | Reach 1-Upper | 474 | 100YrCHI3Hr | 0.31 | 92.41 | 93.00 | 92.58 | 93.00 | 0.000000 | 0.01 | 40.12 | 92.20 | 0.01 |
| River 1 | Reach 1-Upper | 474 | 2YrSCS24Hr | 0.11 | 92.41 | 92.63 | 92.52 | 92.63 | 0.000605 | 0.16 | 0.65 | 5.71 | 0.16 |
| River 1 | Reach 1-Upper | 474 | 5YrSCS24Hr | 0.18 | 92.41 | 92.69 | 92.55 | 92.69 | 0.000512 | 0.18 | 1.00 | 6.89 | 0.15 |
| River 1 | Reach 1-Upper | 474 | 10YrSCS24Hr | 0.23 | 92.41 | 92.75 | 92.56 | 92.75 | 0.000285 | 0.15 | 1.49 | 8.28 | 0.12 |
| River 1 | Reach 1-Upper | 474 | 25YrSCS24Hr | 0.29 | 92.41 | 92.93 | 92.57 | 92.93 | 0.000001 | 0.01 | 33.86 | 91.89 | 0.01 |
| River 1 | Reach 1-Upper | 474 | 50YrSCS24Hr | 0.34 | 92.41 | 93.12 | 92.58 | 93.12 | 0.000000 | 0.01 | 51.33 | 92.74 | 0.00 |
| River 1 | Reach 1-Upper | 474 | 100YrSCS24Hr | 0.40 | 92.41 | 93.30 | 92.59 | 93.30 | 0.000000 | 0.01 | 68.65 | 93.59 | 0.00 |
| River 1 | Reach 1-Upper | 454 | 2YrCHI3Hr | 0.07 | 92.44 | 92.58 | 92.50 | 92.58 | 0.001576 | 0.24 | 0.28 | 2.85 | 0.24 |
| River 1 | Reach 1-Upper | 454 | 5YrCHI3Hr | 0.12 | 92.44 | 92.62 | 92.53 | 92.63 | 0.001689 | 0.29 | 0.41 | 3.31 | 0.26 |
| River 1 | Reach 1-Upper | 454 | 10YrCHI3Hr | 0.16 | 92.44 | 92.65 | 92.55 | 92.66 | 0.001595 | 0.31 | 0.52 | 3.64 | 0.26 |
| River 1 | Reach 1-Upper | 454 | 25YrCHI3Hr | 0.22 | 92.44 | 92.72 | 92.56 | 92.72 | 0.000913 | 0.28 | 0.79 | 4.34 | 0.21 |
| River 1 | Reach 1-Upper | 454 | 50YrCHI3Hr | 0.26 | 92.44 | 92.84 | 92.57 | 92.84 | 0.000012 | 0.04 | 12.27 | 82.88 | 0.03 |
| River 1 | Reach 1-Upper | 454 | 100YrCHI3Hr | 0.31 | 92.44 | 93.00 | 92.59 | 93.00 | 0.000002 | 0.02 | 25.28 | 83.36 | 0.01 |
| River 1 | Reach 1-Upper | 454 | 2YrSCS24Hr | 0.11 | 92.44 | 92.61 | 92.52 | 92.62 | 0.001709 | 0.28 | 0.38 | 3.19 | 0.26 |
| River 1 | Reach 1-Upper | 454 | 5YrSCS24Hr | 0.18 | 92.44 | 92.67 | 92.55 | 92.67 | 0.001416 | 0.30 | 0.58 | 3.81 | 0.25 |
| River 1 | Reach 1-Upper | 454 | 10YrSCS24Hr | 0.23 | 92.44 | 92.74 | 92.56 | 92.74 | 0.000715 | 0.26 | 0.88 | 4.56 | 0.18 |
| River 1 | Reach 1-Upper | 454 | 25YrSCS24Hr | 0.29 | 92.44 | 92.93 | 92.58 | 92.93 | 0.000003 | 0.03 | 19.62 | 83.15 | 0.01 |
| River 1 | Reach 1-Upper | 454 | 50YrSCS24Hr | 0.34 | 92.44 | 93.12 | 92.60 | 93.12 | 0.000001 | 0.02 | 35.41 | 83.72 | 0.01 |
| River 1 | Reach 1-Upper | 454 | 100YrSCS24Hr | 0.40 | 92.44 | 93.30 | 92.61 | 93.30 | 0.000000 | 0.01 | 51.02 | 84.29 | 0.00 |
| River 1 | Reach 1-Upper | 434 | 2YrCHI3Hr | 0.07 | 92.42 | 92.53 | 92.49 | 92.54 | 0.003245 | 0.30 | 0.23 | 2.89 | 0.34 |
| River 1 | Reach 1-Upper | 434 | 5YrCHI3Hr | 0.12 | 92.42 | 92.58 | 92.51 | 92.59 | 0.002201 | 0.32 | 0.38 | 3.34 | 0.30 |
| River 1 | Reach 1-Upper | 434 | 10YrCHI3Hr | 0.16 | 92.42 | 92.62 | 92.52 | 92.62 | 0.001702 | 0.32 | 0.51 | 3.67 | 0.27 |
| River 1 | Reach 1-Upper | 434 | 25YrCHI3Hr | 0.22 | 92.42 | 92.72 | 92.54 | 92.72 | 0.000099 | 0.09 | 4.19 | 44.55 | 0.07 |
| River 1 | Reach 1-Upper | 434 | 50YrCHI3Hr | 0.26 | 92.42 | 92.84 | 92.55 | 92.84 | 0.000011 | 0.04 | 12.14 | 73.98 | 0.02 |
| River 1 | Reach 1-Upper | 434 | 100YrCHI3Hr | 0.31 | 92.42 | 93.00 | 92.56 | 93.00 | 0.000002 | 0.02 | 23.78 | 74.52 | 0.01 |
| River 1 | Reach 1-Upper | 434 | 2YrSCS24Hr | 0.11 | 92.42 | 92.57 | 92.50 | 92.57 | 0.002433 | 0.31 | 0.34 | 3.22 | 0.31 |
| River 1 | Reach 1-Upper | 434 | 5YrSCS24Hr | 0.18 | 92.42 | 92.64 | 92.53 | 92.64 | 0.001593 | 0.30 | 0.59 | 4.31 | 0.26 |
| River 1 | Reach 1-Upper | 434 | 10YrSCS24Hr | 0.23 | 92.42 | 92.74 | 92.54 | 92.74 | 0.000062 | 0.08 | 5.30 | 52.04 | 0.05 |
| River 1 | Reach 1-Upper | 434 | 25YrSCS24Hr | 0.29 | 92.42 | 92.93 | 92.55 | 92.93 | 0.000003 | 0.03 | 18.72 | 74.29 | 0.01 |
| River 1 | Reach 1-Upper | 434 | 50YrSCS24Hr | 0.34 | 92.42 | 93.12 | 92.57 | 93.12 | 0.000001 | 0.02 | 32.84 | 74.94 | 0.01 |
| River 1 | Reach 1-Upper | 434 | 100YrSCS24Hr | 0.40 | 92.42 | 93.30 | 92.58 | 93.30 | 0.000000 | 0.01 | 46.84 | 75.66 | 0.00 |
| River 1 | Reach 1-Upper | 416 | 2YrCHI3Hr | 0.07 | 92.34 | 92.51 | 92.42 | 92.51 | 0.000622 | 0.15 | 0.44 | 4.70 | 0.15 |
| River 1 | Reach 1-Upper | 416 | 5YrCHI3Hr | 0.12 | 92.34 | 92.57 | 92.45 | 92.57 | 0.000424 | 0.17 | 0.75 | 5.83 | 0.14 |
| River 1 | Reach 1-Upper | 416 | 10YrCHI3Hr | 0.16 | 92.34 | 92.62 | 92.46 | 92.62 | 0.000159 | 0.12 | 2.27 | 28.78 | 0.09 |
| River 1 | Reach 1-Upper | 416 | 25YrCHI3Hr | 0.22 | 92.34 | 92.72 | 92.48 | 92.72 | 0.000031 | 0.07 | 5.56 | 35.85 | 0.04 |
| River 1 | Reach 1-Upper | 416 | 50YrCHI3Hr | 0.26 | 92.34 | 92.84 | 92.48 | 92.84 | 0.000008 | 0.05 | 10.70 | 48.52 | 0.02 |
| River 1 | Reach 1-Upper | 416 | 100YrCHI3Hr | 0.31 | 92.34 | 93.00 | 92.49 | 93.00 | 0.000002 | 0.03 | 20.27 | 66.96 | 0.01 |
| River 1 | Reach 1-Upper | 416 | 2YrSCS24Hr | 0.11 | 92.34 | 92.56 | 92.44 | 92.56 | 0.000463 | 0.17 | 0.67 | 5.55 | 0.14 |
| River 1 | Reach 1-Upper | 416 | 5YrSCS24Hr | 0.18 | 92.34 | 92.64 | 92.47 | 92.64 | 0.000108 | 0.11 | 2.88 | 30.23 | 0.07 |
| River 1 | Reach 1-Upper | 416 | 10YrSCS24Hr | 0.23 | 92.34 | 92.74 | 92.48 | 92.74 | 0.000024 | 0.07 | 6.41 | 39.28 | 0.04 |
| River 1 | Reach 1-Upper | 416 | 25YrSCS24Hr | 0.29 | 92.34 | 92.93 | 92.49 | 92.93 | 0.000004 | 0.04 | 15.73 | 65.04 | 0.02 |
| River 1 | Reach 1-Upper | 416 | 50YrSCS24Hr | 0.34 | 92.34 | 93.12 | 92.50 | 93.12 | 0.000001 | 0.02 | 28.42 | 67.40 | 0.01 |
| River 1 | Reach 1-Upper | 416 | 100YrSCS24Hr | 0.40 | 92.34 | 93.30 | 92.51 | 93.30 | 0.000000 | 0.02 | 41.01 | 68.07 | 0.01 |
| River 1 | Reach 1-Upper | 398 | 2YrCHI3Hr | 0.07 | 92.28 | 92.50 | 92.40 | 92.50 | 0.000933 | 0.21 | 0.31 | 2.50 | 0.19 |
| River 1 | Reach 1-Upper | 398 | 5YrCHI3Hr | 0.12 | 92.28 | 92.56 | 92.42 | 92.56 | 0.000915 | 0.26 | 0.47 | 2.86 | 0.20 |
| River 1 | Reach 1-Upper | 398 | 10YrCHI3Hr | 0.16 | 92.28 | 92.61 | 92.44 | 92.61 | 0.000752 | 0.26 | 0.62 | 3.16 | 0.19 |
| River 1 | Reach 1-Upper | 398 | 25YrCHI3Hr | 0.22 | 92.28 | 92.71 | 92.46 | 92.72 | 0.000355 | 0.22 | 1.01 | 4.66 | 0.14 |
| River 1 | Reach 1-Upper | 398 | 50YrCHI3Hr | 0.26 | 92.28 | 92.84 | 92.47 | 92.84 | 0.000076 | 0.12 | 4.26 | 46.30 | 0.07 |
| River 1 | Reach 1-Upper | 398 | 100YrCHI3Hr | 0.31 | 92.28 | 93.00 | 92.49 | 93.00 | 0.000008 | 0.05 | 12.80 | 58.61 | 0.02 |
| River 1 | Reach 1-Upper | 398 | 2YrSCS24Hr | 0.11 | 92.28 | 92.54 | 92.42 | 92.55 | 0.000935 | 0.25 | 0.43 | 2.77 | 0.20 |
| River 1 | Reach 1-Upper | 398 | 5YrSCS24Hr | 0.18 | 92.28 | 92.63 | 92.44 | 92.63 | 0.000660 | 0.26 | 0.69 | 3.29 | 0.18 |
| River 1 | Reach 1-Upper | 398 | 10YrSCS24Hr | 0.23 | 92.28 | 92.74 | 92.46 | 92.74 | 0.000295 | 0.21 | 1.13 | 5.59 | 0.12 |
| River 1 | Reach 1-Upper | 398 | 25YrSCS24Hr | 0.29 | 92.28 | 92.93 | 92.48 | 92.93 | 0.000020 | 0.07 | 8.81 | 58.42 | 0.03 |
| River 1 | Reach 1-Upper | 398 | 50YrSCS24Hr | 0.34 | 92.28 | 93.12 | 92.50 | 93.12 | 0.000003 | 0.03 | 19.93 | 58.96 | 0.01 |
| River 1 | Reach 1-Upper | 398 | 100YrSCS24Hr | 0.40 | 92.28 | 93.30 | 92.51 | 93.30 | 0.000001 | 0.02 | 30.94 | 59.51 | 0.01 |
| River 1 | Reach 1-Upper | 383 | 2YrCHI3Hr | 0.07 | 92.34 | 92.47 | 92.42 | 92.47 | 0.004536 | 0.39 | 0.17 | 1.90 | 0.41 |
| River 1 | Reach 1-Upper | 383 | 5YrCHI3Hr | 0.12 | 92.34 | 92.53 | 92.45 | 92.54 | 0.002876 | 0.39 | 0.31 | 2.30 | 0.34 |
| River 1 | Reach 1-Upper | 383 | 10YrCHI3Hr | 0.16 | 92.34 | 92.59 | 92.47 | 92.59 | 0.001737 | 0.36 | 0.45 | 2.62 | 0.28 |
| River 1 | Reach 1-Upper | 383 | 25YrCHI3Hr | 0.22 | 92.34 | 92.70 | 92.49 | 92.71 | 0.000630 | 0.27 | 0.80 | 3.29 | 0.18 |
| River 1 | Reach 1-Upper | 383 | 50YrCHI3Hr | 0.26 | 92.34 | 92.83 | 92.50 | 92.84 | 0.000255 | 0.21 | 1.27 | 4.01 | 0.12 |
| River 1 | Reach 1-Upper | 383 | 100YrCHI3Hr | 0.31 | 92.34 | 92.99 | 92.52 | 93.00 | 0.000100 | 0.16 | 2.02 | 5.50 | 0.08 |
| River 1 | Reach 1-Upper | 383 | 2YrSCS24Hr | 0.11 | 92.34 | 92.51 | 92.44 | 92.52 | 0.003262 | 0.40 | 0.27 | 2.21 | 0.36 |
| River 1 | Reach 1-Upper | 383 | 5YrSCS24Hr | 0.18 | 92.34 | 92.61 | 92.47 | 92.62 | 0.001389 | 0.34 | 0.52 | 2.77 | 0.25 |
| River 1 | Reach 1-Upper | 383 | 10YrSCS24Hr | 0.23 | 92.34 | 92.73 | 92.49 | 92.73 | 0.000520 | 0.26 | 0.88 | 3.42 | 0.16 |
| River 1 | Reach 1-Upper | 383 | 25YrSCS24Hr | 0.29 | 92.34 | 92.93 | 92.51 | 92.93 | 0.000147 | 0.18 | 1.66 | 4.73 | 0.09 |

HEC-RAS Plan: 20250603-Pre_Dev_v01 (Continued)

| River | Reach | River Sta | Profile | Q Total (m3/s) | Min Ch El (m) | W.S. Elev (m) | Crit W.S. (m) | E.G. Elev (m) | E.G. Slope (m/m) | Vel Chnl (m/s) | Flow Area (m2) | Top Width (m) | Froude # Chl |
|---------|---------------|-----------|--------------|-------------------|------------------|------------------|------------------|------------------|---------------------|-------------------|-------------------|------------------|--------------|
| River 1 | Reach 1-Upper | 383 | 50YrSCS24Hr | 0.34 | 92.34 | 93.12 | 92.53 | 93.12 | 0.000005 | 0.04 | 15.00 | 51.87 | 0.02 |
| River 1 | Reach 1-Upper | 383 | 100YrSCS24Hr | 0.40 | 92.34 | 93.30 | 92.54 | 93.30 | 0.000002 | 0.03 | 24.70 | 52.43 | 0.01 |
| River 1 | Reach 1-Upper | 364 | 2YrCHI3Hr | 0.07 | 92.23 | 92.43 | 92.33 | 92.43 | 0.001355 | 0.26 | 0.26 | 2.01 | 0.23 |
| River 1 | Reach 1-Upper | 364 | 5YrCHI3Hr | 0.12 | 92.23 | 92.50 | 92.36 | 92.50 | 0.001099 | 0.29 | 0.42 | 2.37 | 0.22 |
| River 1 | Reach 1-Upper | 364 | 10YrCHI3Hr | 0.16 | 92.23 | 92.57 | 92.38 | 92.57 | 0.000740 | 0.27 | 0.59 | 2.71 | 0.19 |
| River 1 | Reach 1-Upper | 364 | 25YrCHI3Hr | 0.22 | 92.23 | 92.70 | 92.40 | 92.70 | 0.000331 | 0.22 | 0.98 | 3.34 | 0.13 |
| River 1 | Reach 1-Upper | 364 | 50YrCHI3Hr | 0.26 | 92.23 | 92.83 | 92.42 | 92.83 | 0.000166 | 0.18 | 1.48 | 4.20 | 0.10 |
| River 1 | Reach 1-Upper | 364 | 100YrCHI3Hr | 0.31 | 92.23 | 92.99 | 92.43 | 92.99 | 0.000050 | 0.12 | 4.53 | 43.93 | 0.06 |
| River 1 | Reach 1-Upper | 364 | 2YrSCS24Hr | 0.11 | 92.23 | 92.48 | 92.35 | 92.48 | 0.001197 | 0.29 | 0.37 | 2.27 | 0.23 |
| River 1 | Reach 1-Upper | 364 | 5YrSCS24Hr | 0.18 | 92.23 | 92.60 | 92.39 | 92.60 | 0.000621 | 0.26 | 0.67 | 2.85 | 0.17 |
| River 1 | Reach 1-Upper | 364 | 10YrSCS24Hr | 0.23 | 92.23 | 92.72 | 92.41 | 92.73 | 0.000283 | 0.21 | 1.07 | 3.47 | 0.12 |
| River 1 | Reach 1-Upper | 364 | 25YrSCS24Hr | 0.29 | 92.23 | 92.92 | 92.43 | 92.93 | 0.000099 | 0.15 | 1.93 | 5.59 | 0.08 |
| River 1 | Reach 1-Upper | 364 | 50YrSCS24Hr | 0.34 | 92.23 | 93.12 | 92.44 | 93.12 | 0.000012 | 0.07 | 9.97 | 44.25 | 0.03 |
| River 1 | Reach 1-Upper | 364 | 100YrSCS24Hr | 0.40 | 92.23 | 93.30 | 92.46 | 93.30 | 0.000003 | 0.04 | 18.26 | 45.01 | 0.01 |
| River 1 | Reach 1-Upper | 347 | 2YrCHI3Hr | 0.07 | 92.26 | 92.40 | 92.33 | 92.41 | 0.001382 | 0.24 | 0.27 | 2.45 | 0.23 |
| River 1 | Reach 1-Upper | 347 | 5YrCHI3Hr | 0.12 | 92.26 | 92.49 | 92.35 | 92.49 | 0.000808 | 0.25 | 0.49 | 2.80 | 0.19 |
| River 1 | Reach 1-Upper | 347 | 10YrCHI3Hr | 0.16 | 92.26 | 92.56 | 92.36 | 92.56 | 0.000488 | 0.23 | 0.71 | 3.12 | 0.15 |
| River 1 | Reach 1-Upper | 347 | 25YrCHI3Hr | 0.22 | 92.26 | 92.69 | 92.38 | 92.70 | 0.000213 | 0.19 | 1.16 | 3.69 | 0.11 |
| River 1 | Reach 1-Upper | 347 | 50YrCHI3Hr | 0.26 | 92.26 | 92.83 | 92.40 | 92.83 | 0.000107 | 0.15 | 1.71 | 4.28 | 0.08 |
| River 1 | Reach 1-Upper | 347 | 100YrCHI3Hr | 0.31 | 92.26 | 92.99 | 92.41 | 92.99 | 0.000050 | 0.13 | 2.54 | 7.35 | 0.06 |
| River 1 | Reach 1-Upper | 347 | 2YrSCS24Hr | 0.11 | 92.26 | 92.46 | 92.34 | 92.47 | 0.000932 | 0.25 | 0.43 | 2.71 | 0.20 |
| River 1 | Reach 1-Upper | 347 | 5YrSCS24Hr | 0.18 | 92.26 | 92.59 | 92.37 | 92.59 | 0.000403 | 0.22 | 0.80 | 3.25 | 0.14 |
| River 1 | Reach 1-Upper | 347 | 10YrSCS24Hr | 0.23 | 92.26 | 92.72 | 92.39 | 92.72 | 0.000183 | 0.18 | 1.26 | 3.81 | 0.10 |
| River 1 | Reach 1-Upper | 347 | 25YrSCS24Hr | 0.29 | 92.26 | 92.92 | 92.41 | 92.92 | 0.000071 | 0.14 | 2.13 | 5.02 | 0.07 |
| River 1 | Reach 1-Upper | 347 | 50YrSCS24Hr | 0.34 | 92.26 | 93.12 | 92.42 | 93.12 | 0.000020 | 0.09 | 6.30 | 37.59 | 0.04 |
| River 1 | Reach 1-Upper | 347 | 100YrSCS24Hr | 0.40 | 92.26 | 93.30 | 92.43 | 93.30 | 0.000005 | 0.06 | 13.35 | 38.07 | 0.02 |
| River 1 | Reach 1-Upper | 328 | 2YrCHI3Hr | 0.07 | 92.20 | 92.37 | 92.28 | 92.38 | 0.001873 | 0.30 | 0.22 | 1.82 | 0.27 |
| River 1 | Reach 1-Upper | 328 | 5YrCHI3Hr | 0.12 | 92.20 | 92.47 | 92.32 | 92.47 | 0.001020 | 0.29 | 0.42 | 2.24 | 0.21 |
| River 1 | Reach 1-Upper | 328 | 10YrCHI3Hr | 0.16 | 92.20 | 92.55 | 92.34 | 92.55 | 0.000618 | 0.26 | 0.61 | 2.58 | 0.17 |
| River 1 | Reach 1-Upper | 328 | 25YrCHI3Hr | 0.22 | 92.20 | 92.69 | 92.36 | 92.69 | 0.000277 | 0.21 | 1.02 | 3.16 | 0.12 |
| River 1 | Reach 1-Upper | 328 | 50YrCHI3Hr | 0.26 | 92.20 | 92.83 | 92.38 | 92.83 | 0.000152 | 0.17 | 1.51 | 4.11 | 0.09 |
| River 1 | Reach 1-Upper | 328 | 100YrCHI3Hr | 0.31 | 92.20 | 92.99 | 92.40 | 92.99 | 0.000074 | 0.14 | 2.26 | 5.12 | 0.07 |
| River 1 | Reach 1-Upper | 328 | 2YrSCS24Hr | 0.11 | 92.20 | 92.44 | 92.31 | 92.45 | 0.001182 | 0.29 | 0.36 | 2.14 | 0.23 |
| River 1 | Reach 1-Upper | 328 | 5YrSCS24Hr | 0.18 | 92.20 | 92.58 | 92.34 | 92.58 | 0.000513 | 0.25 | 0.70 | 2.71 | 0.16 |
| River 1 | Reach 1-Upper | 328 | 10YrSCS24Hr | 0.23 | 92.20 | 92.72 | 92.36 | 92.72 | 0.000240 | 0.21 | 1.11 | 3.28 | 0.11 |
| River 1 | Reach 1-Upper | 328 | 25YrSCS24Hr | 0.29 | 92.20 | 92.92 | 92.39 | 92.92 | 0.000098 | 0.15 | 1.92 | 4.61 | 0.07 |
| River 1 | Reach 1-Upper | 328 | 50YrSCS24Hr | 0.34 | 92.20 | 93.12 | 92.40 | 93.12 | 0.000035 | 0.11 | 4.57 | 29.52 | 0.05 |
| River 1 | Reach 1-Upper | 328 | 100YrSCS24Hr | 0.40 | 92.20 | 93.30 | 92.42 | 93.30 | 0.000009 | 0.06 | 10.13 | 29.96 | 0.02 |
| River 1 | Reach 1-Upper | 306 | 2YrCHI3Hr | 0.07 | 92.07 | 92.35 | 92.18 | 92.35 | 0.000722 | 0.25 | 0.27 | 1.49 | 0.18 |
| River 1 | Reach 1-Upper | 306 | 5YrCHI3Hr | 0.12 | 92.07 | 92.45 | 92.23 | 92.45 | 0.000689 | 0.30 | 0.40 | 1.84 | 0.18 |
| River 1 | Reach 1-Upper | 306 | 10YrCHI3Hr | 0.16 | 92.07 | 92.53 | 92.25 | 92.54 | 0.000559 | 0.31 | 0.52 | 2.13 | 0.17 |
| River 1 | Reach 1-Upper | 306 | 25YrCHI3Hr | 0.22 | 92.07 | 92.68 | 92.28 | 92.68 | 0.000321 | 0.29 | 0.74 | 2.69 | 0.13 |
| River 1 | Reach 1-Upper | 306 | 50YrCHI3Hr | 0.26 | 92.07 | 92.82 | 92.30 | 92.82 | 0.000203 | 0.28 | 0.95 | 3.29 | 0.11 |
| River 1 | Reach 1-Upper | 306 | 100YrCHI3Hr | 0.31 | 92.07 | 92.99 | 92.32 | 92.99 | 0.000131 | 0.26 | 1.20 | 4.54 | 0.09 |
| River 1 | Reach 1-Upper | 306 | 2YrSCS24Hr | 0.11 | 92.07 | 92.42 | 92.21 | 92.43 | 0.000712 | 0.29 | 0.37 | 1.75 | 0.18 |
| River 1 | Reach 1-Upper | 306 | 5YrSCS24Hr | 0.18 | 92.07 | 92.57 | 92.26 | 92.57 | 0.000497 | 0.31 | 0.58 | 2.25 | 0.16 |
| River 1 | Reach 1-Upper | 306 | 10YrSCS24Hr | 0.23 | 92.07 | 92.71 | 92.28 | 92.71 | 0.000290 | 0.29 | 0.79 | 2.81 | 0.13 |
| River 1 | Reach 1-Upper | 306 | 25YrSCS24Hr | 0.29 | 92.07 | 92.91 | 92.31 | 92.92 | 0.000156 | 0.27 | 1.10 | 3.90 | 0.10 |
| River 1 | Reach 1-Upper | 306 | 50YrSCS24Hr | 0.34 | 92.07 | 93.11 | 92.33 | 93.11 | 0.000098 | 0.25 | 1.39 | 20.53 | 0.08 |
| River 1 | Reach 1-Upper | 306 | 100YrSCS24Hr | 0.40 | 92.07 | 93.30 | 92.36 | 93.30 | 0.000072 | 0.24 | 1.67 | 20.98 | 0.07 |
| River 1 | Reach 1-Upper | 300 | | Culvert | | | | | | | | | |
| River 1 | Reach 1-Upper | 294 | 2YrCHI3Hr | 0.07 | 92.15 | 92.32 | 92.23 | 92.32 | 0.001567 | 0.31 | 0.22 | 2.08 | 0.26 |
| River 1 | Reach 1-Upper | 294 | 5YrCHI3Hr | 0.12 | 92.15 | 92.37 | 92.26 | 92.38 | 0.001840 | 0.41 | 0.29 | 2.34 | 0.30 |
| River 1 | Reach 1-Upper | 294 | 10YrCHI3Hr | 0.16 | 92.15 | 92.39 | 92.28 | 92.41 | 0.002165 | 0.49 | 0.33 | 2.48 | 0.33 |
| River 1 | Reach 1-Upper | 294 | 25YrCHI3Hr | 0.22 | 92.15 | 92.42 | 92.30 | 92.44 | 0.002528 | 0.57 | 0.38 | 2.64 | 0.36 |
| River 1 | Reach 1-Upper | 294 | 50YrCHI3Hr | 0.26 | 92.15 | 92.45 | 92.32 | 92.47 | 0.002769 | 0.63 | 0.41 | 2.76 | 0.38 |
| River 1 | Reach 1-Upper | 294 | 100YrCHI3Hr | 0.31 | 92.15 | 92.47 | 92.33 | 92.49 | 0.002956 | 0.69 | 0.45 | 2.87 | 0.40 |
| River 1 | Reach 1-Upper | 294 | 2YrSCS24Hr | 0.11 | 92.15 | 92.36 | 92.25 | 92.36 | 0.001762 | 0.39 | 0.28 | 2.28 | 0.29 |
| River 1 | Reach 1-Upper | 294 | 5YrSCS24Hr | 0.18 | 92.15 | 92.40 | 92.28 | 92.41 | 0.002296 | 0.51 | 0.35 | 2.52 | 0.34 |
| River 1 | Reach 1-Upper | 294 | 10YrSCS24Hr | 0.23 | 92.15 | 92.43 | 92.30 | 92.45 | 0.002610 | 0.59 | 0.39 | 2.66 | 0.37 |
| River 1 | Reach 1-Upper | 294 | 25YrSCS24Hr | 0.29 | 92.15 | 92.46 | 92.33 | 92.48 | 0.002895 | 0.67 | 0.43 | 2.82 | 0.40 |
| River 1 | Reach 1-Upper | 294 | 50YrSCS24Hr | 0.34 | 92.15 | 92.48 | 92.35 | 92.51 | 0.003128 | 0.73 | 0.47 | 2.94 | 0.42 |
| River 1 | Reach 1-Upper | 294 | 100YrSCS24Hr | 0.40 | 92.15 | 92.50 | 92.36 | 92.54 | 0.003396 | 0.80 | 0.50 | 3.05 | 0.44 |
| River 1 | Reach 1-Upper | 279 | 2YrCHI3Hr | 0.08 | 92.08 | 92.21 | 92.21 | 92.24 | 0.029991 | 0.80 | 0.10 | 1.51 | 0.99 |
| River 1 | Reach 1-Upper | 279 | 5YrCHI3Hr | 0.15 | 92.08 | 92.25 | 92.24 | 92.29 | 0.026320 | 0.91 | 0.16 | 1.84 | 0.98 |
| River 1 | Reach 1-Upper | 279 | 10YrCHI3Hr | 0.20 | 92.08 | 92.28 | | 92.32 | 0.017826 | 0.87 | 0.23 | 2.04 | 0.83 |
| River 1 | Reach 1-Upper | 279 | 25YrCHI3Hr | 0.27 | 92.08 | 92.32 | | 92.36 | 0.013314 | 0.86 | 0.31 | 2.27 | 0.74 |
| River 1 | Reach 1-Upper | 279 | 50YrCHI3Hr | 0.32 | 92.08 | 92.34 | | 92.38 | 0.011695 | 0.87 | 0.37 | 2.42 | 0.71 |
| River 1 | Reach 1-Upper | 279 | 100YrCHI3Hr | 0.38 | 92.08 | 92.37 | | 92.41 | 0.010643 | 0.88 | 0.43 | 2.57 | 0.69 |
| River 1 | Reach 1-Upper | 279 | 2YrSCS24Hr | 0.13 | 92.08 | 92.23 | 92.23 | 92.28 | 0.029039 | 0.90 | 0.14 | 1.75 | 1.01 |
| River 1 | Reach 1-Upper | 279 | 5YrSCS24Hr | 0.22 | 92.08 | 92.29 | | 92.33 | 0.015917 | 0.86 | 0.25 | 2.10 | 0.80 |
| River 1 | Reach 1-Upper | 279 | 10YrSCS24Hr | 0.28 | 92.08 | 92.32 | | 92.36 | 0.012955 | 0.86 | 0.32 | 2.30 | 0.74 |
| River 1 | Reach 1-Upper | 279 | 25YrSCS24Hr | 0.36 | 92.08 | 92.36 | | 92.40 | 0.011055 | 0.88 | 0.41 | 2.51 | 0.70 |
| River 1 | Reach 1-Upper | 279 | 50YrSCS24Hr | 0.42 | 92.08 | 92.38 | | 92.42 | 0.010063 | 0.89 | 0.47 | 2.66 | 0.67 |
| River 1 | Reach 1-Upper | 279 | 100YrSCS24Hr | 0.49 | 92.08 | 92.41 | | 92.45 | 0.009502 | 0.91 | 0.54 | 2.81 | 0.66 |
| River 1 | Reach 1-Upper | 277 | 2YrCHI3Hr | 0.08 | 91.95 | 92.20 | | 92.21 | 0.000695 | 0.21 | 0.39 | 2.70 | 0.17 |
| River 1 | Reach 1-Upper | 277 | 5YrCHI3Hr | 0.15 | 91.95 | 92.26 | | 92.26 | 0.000856 | 0.28 | 0.54 | 3.02 | 0.20 |
| River 1 | Reach 1-Upper | 277 | 10YrCHI3Hr | 0.20 | 91.95 | 92.29 | | 92.30 | 0.000927 | 0.32 | 0.64 | 3.19 | 0.21 |
| River 1 | Reach 1-Upper | 277 | 25YrCHI3Hr | 0.27 | 91.95 | 92.33 | | 92.33 | 0.001006 | 0.37 | 0.76 | 3.41 | 0.23 |
| River 1 | Reach 1-Upper | 277 | 50YrCHI3Hr | 0.32 | 91.95 | 92.35 | | 92.36 | 0.001068 | 0.41 | 0.85 | 3.55 | 0.24 |
| River 1 | Reach 1-Upper | 277 | 100YrCHI3Hr | 0.38 | 91.95 | 92.38 | | 92.39 | 0.001131 | 0.44 | 0.95 | 3.69 | 0.25 |
| River 1 | Reach 1-Upper | 277 | 2YrSCS24Hr | 0.13 | 91.95 | 92.25 | | 92.25 | 0.000826 | 0.26 | 0.50 | 2.94 | 0.20 |

HEC-RAS Plan: 20250603-Pre_Dev_v01 (Continued)

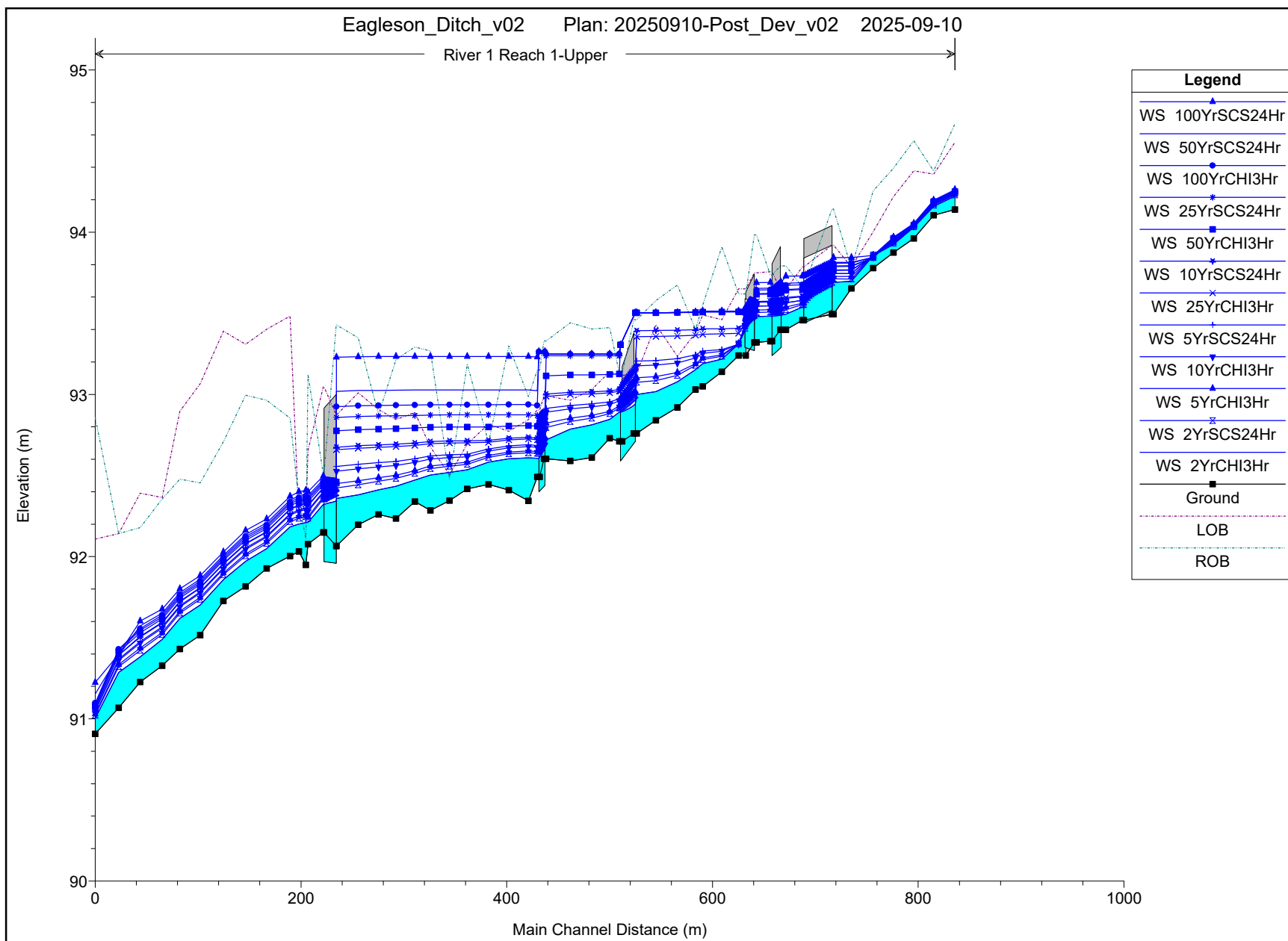
| River | Reach | River Sta | Profile | Q Total (m3/s) | Min Ch El (m) | W.S. Elev (m) | Crit W.S. (m) | E.G. Elev (m) | E.G. Slope (m/m) | Vel Chnl (m/s) | Flow Area (m2) | Top Width (m) | Froude # Chl |
|---------|---------------|-----------|--------------|-------------------|------------------|------------------|------------------|------------------|---------------------|-------------------|-------------------|------------------|--------------|
| River 1 | Reach 1-Upper | 277 | 5YrSCS24Hr | 0.22 | 91.95 | 92.30 | | 92.31 | 0.000941 | 0.33 | 0.68 | 3.25 | 0.22 |
| River 1 | Reach 1-Upper | 277 | 10YrSCS24Hr | 0.28 | 91.95 | 92.33 | | 92.34 | 0.001018 | 0.38 | 0.78 | 3.43 | 0.23 |
| River 1 | Reach 1-Upper | 277 | 25YrSCS24Hr | 0.36 | 91.95 | 92.37 | | 92.38 | 0.001104 | 0.43 | 0.91 | 3.63 | 0.25 |
| River 1 | Reach 1-Upper | 277 | 50YrSCS24Hr | 0.42 | 91.95 | 92.39 | | 92.40 | 0.001159 | 0.46 | 1.00 | 3.77 | 0.26 |
| River 1 | Reach 1-Upper | 277 | 100YrSCS24Hr | 0.49 | 91.95 | 92.42 | | 92.43 | 0.001229 | 0.50 | 1.09 | 3.91 | 0.27 |
| River 1 | Reach 1-Upper | 270 | 2YrCHI3Hr | 0.08 | 92.03 | 92.20 | | 92.20 | 0.001692 | 0.27 | 0.29 | 2.60 | 0.26 |
| River 1 | Reach 1-Upper | 270 | 5YrCHI3Hr | 0.15 | 92.03 | 92.25 | | 92.25 | 0.001753 | 0.33 | 0.45 | 3.07 | 0.27 |
| River 1 | Reach 1-Upper | 270 | 10YrCHI3Hr | 0.20 | 92.03 | 92.28 | | 92.29 | 0.001743 | 0.36 | 0.55 | 3.36 | 0.28 |
| River 1 | Reach 1-Upper | 270 | 25YrCHI3Hr | 0.27 | 92.03 | 92.32 | | 92.33 | 0.001732 | 0.40 | 0.68 | 3.72 | 0.29 |
| River 1 | Reach 1-Upper | 270 | 50YrCHI3Hr | 0.32 | 92.03 | 92.34 | | 92.35 | 0.001721 | 0.42 | 0.78 | 4.13 | 0.29 |
| River 1 | Reach 1-Upper | 270 | 100YrCHI3Hr | 0.38 | 92.03 | 92.37 | | 92.38 | 0.001663 | 0.45 | 0.90 | 5.00 | 0.29 |
| River 1 | Reach 1-Upper | 270 | 2YrSCS24Hr | 0.13 | 92.03 | 92.24 | | 92.24 | 0.001760 | 0.32 | 0.40 | 2.95 | 0.27 |
| River 1 | Reach 1-Upper | 270 | 5YrSCS24Hr | 0.22 | 92.03 | 92.29 | | 92.30 | 0.001717 | 0.37 | 0.58 | 3.47 | 0.28 |
| River 1 | Reach 1-Upper | 270 | 10YrSCS24Hr | 0.28 | 92.03 | 92.32 | | 92.33 | 0.001734 | 0.40 | 0.70 | 3.76 | 0.29 |
| River 1 | Reach 1-Upper | 270 | 25YrSCS24Hr | 0.36 | 92.03 | 92.36 | | 92.37 | 0.001687 | 0.44 | 0.84 | 4.62 | 0.29 |
| River 1 | Reach 1-Upper | 270 | 50YrSCS24Hr | 0.42 | 92.03 | 92.38 | | 92.39 | 0.001617 | 0.46 | 0.97 | 5.51 | 0.29 |
| River 1 | Reach 1-Upper | 270 | 100YrSCS24Hr | 0.49 | 92.03 | 92.41 | | 92.42 | 0.001578 | 0.48 | 1.11 | 5.76 | 0.29 |
| River 1 | Reach 1-Upper | 261 | 2YrCHI3Hr | 0.08 | 92.00 | 92.18 | 92.10 | 92.18 | 0.002216 | 0.32 | 0.25 | 2.09 | 0.30 |
| River 1 | Reach 1-Upper | 261 | 5YrCHI3Hr | 0.15 | 92.00 | 92.23 | 92.13 | 92.24 | 0.002543 | 0.41 | 0.36 | 2.34 | 0.33 |
| River 1 | Reach 1-Upper | 261 | 10YrCHI3Hr | 0.20 | 92.00 | 92.26 | 92.15 | 92.27 | 0.002719 | 0.46 | 0.43 | 2.48 | 0.35 |
| River 1 | Reach 1-Upper | 261 | 25YrCHI3Hr | 0.27 | 92.00 | 92.29 | 92.18 | 92.31 | 0.002882 | 0.51 | 0.52 | 2.66 | 0.37 |
| River 1 | Reach 1-Upper | 261 | 50YrCHI3Hr | 0.32 | 92.00 | 92.32 | 92.19 | 92.33 | 0.003012 | 0.55 | 0.59 | 2.78 | 0.38 |
| River 1 | Reach 1-Upper | 261 | 100YrCHI3Hr | 0.38 | 92.00 | 92.34 | 92.21 | 92.36 | 0.003124 | 0.58 | 0.66 | 2.90 | 0.39 |
| River 1 | Reach 1-Upper | 261 | 2YrSCS24Hr | 0.13 | 92.00 | 92.22 | 92.12 | 92.22 | 0.002466 | 0.39 | 0.33 | 2.27 | 0.32 |
| River 1 | Reach 1-Upper | 261 | 5YrSCS24Hr | 0.22 | 92.00 | 92.27 | 92.16 | 92.28 | 0.002719 | 0.47 | 0.46 | 2.53 | 0.35 |
| River 1 | Reach 1-Upper | 261 | 10YrSCS24Hr | 0.28 | 92.00 | 92.30 | 92.18 | 92.31 | 0.002908 | 0.52 | 0.54 | 2.68 | 0.37 |
| River 1 | Reach 1-Upper | 261 | 25YrSCS24Hr | 0.36 | 92.00 | 92.33 | 92.20 | 92.35 | 0.003077 | 0.57 | 0.63 | 2.84 | 0.38 |
| River 1 | Reach 1-Upper | 261 | 50YrSCS24Hr | 0.42 | 92.00 | 92.36 | 92.22 | 92.38 | 0.003155 | 0.60 | 0.70 | 2.97 | 0.39 |
| River 1 | Reach 1-Upper | 261 | 100YrSCS24Hr | 0.49 | 92.00 | 92.38 | 92.24 | 92.40 | 0.003314 | 0.63 | 0.77 | 3.10 | 0.41 |
| River 1 | Reach 1-Upper | 239 | 2YrCHI3Hr | 0.08 | 91.93 | 92.05 | 92.03 | 92.07 | 0.018146 | 0.68 | 0.12 | 1.54 | 0.79 |
| River 1 | Reach 1-Upper | 239 | 5YrCHI3Hr | 0.15 | 91.93 | 92.09 | 92.07 | 92.12 | 0.014163 | 0.75 | 0.20 | 1.88 | 0.73 |
| River 1 | Reach 1-Upper | 239 | 10YrCHI3Hr | 0.20 | 91.93 | 92.12 | 92.09 | 92.15 | 0.012598 | 0.78 | 0.25 | 2.06 | 0.71 |
| River 1 | Reach 1-Upper | 239 | 25YrCHI3Hr | 0.27 | 91.93 | 92.15 | 92.12 | 92.19 | 0.011181 | 0.82 | 0.33 | 2.23 | 0.69 |
| River 1 | Reach 1-Upper | 239 | 50YrCHI3Hr | 0.32 | 91.93 | 92.18 | 92.13 | 92.21 | 0.010479 | 0.85 | 0.38 | 2.36 | 0.68 |
| River 1 | Reach 1-Upper | 239 | 100YrCHI3Hr | 0.38 | 91.93 | 92.20 | 92.15 | 92.24 | 0.009912 | 0.88 | 0.44 | 2.49 | 0.67 |
| River 1 | Reach 1-Upper | 239 | 2YrSCS24Hr | 0.13 | 91.93 | 92.08 | 92.06 | 92.11 | 0.014943 | 0.73 | 0.18 | 1.79 | 0.75 |
| River 1 | Reach 1-Upper | 239 | 5YrSCS24Hr | 0.22 | 91.93 | 92.13 | 92.10 | 92.16 | 0.012137 | 0.79 | 0.27 | 2.10 | 0.70 |
| River 1 | Reach 1-Upper | 239 | 10YrSCS24Hr | 0.28 | 91.93 | 92.16 | 92.12 | 92.19 | 0.011036 | 0.83 | 0.34 | 2.26 | 0.68 |
| River 1 | Reach 1-Upper | 239 | 25YrSCS24Hr | 0.36 | 91.93 | 92.19 | 92.14 | 92.23 | 0.010147 | 0.86 | 0.41 | 2.43 | 0.67 |
| River 1 | Reach 1-Upper | 239 | 50YrSCS24Hr | 0.42 | 91.93 | 92.22 | 92.16 | 92.26 | 0.009585 | 0.89 | 0.47 | 2.56 | 0.66 |
| River 1 | Reach 1-Upper | 239 | 100YrSCS24Hr | 0.49 | 91.93 | 92.24 | 92.18 | 92.28 | 0.009080 | 0.91 | 0.54 | 2.69 | 0.65 |
| River 1 | Reach 1-Upper | 218 | 2YrCHI3Hr | 0.08 | 91.82 | 91.97 | 91.89 | 91.97 | 0.002000 | 0.29 | 0.27 | 2.48 | 0.28 |
| River 1 | Reach 1-Upper | 218 | 5YrCHI3Hr | 0.15 | 91.82 | 92.02 | 91.92 | 92.02 | 0.002151 | 0.37 | 0.40 | 2.72 | 0.30 |
| River 1 | Reach 1-Upper | 218 | 10YrCHI3Hr | 0.20 | 91.82 | 92.05 | 91.94 | 92.05 | 0.002198 | 0.40 | 0.49 | 2.86 | 0.31 |
| River 1 | Reach 1-Upper | 218 | 25YrCHI3Hr | 0.27 | 91.82 | 92.08 | 91.96 | 92.09 | 0.002327 | 0.45 | 0.59 | 3.03 | 0.33 |
| River 1 | Reach 1-Upper | 218 | 50YrCHI3Hr | 0.32 | 91.82 | 92.11 | 91.98 | 92.12 | 0.002390 | 0.49 | 0.67 | 3.15 | 0.34 |
| River 1 | Reach 1-Upper | 218 | 100YrCHI3Hr | 0.38 | 91.82 | 92.13 | 91.99 | 92.14 | 0.002438 | 0.52 | 0.75 | 3.27 | 0.34 |
| River 1 | Reach 1-Upper | 218 | 2YrSCS24Hr | 0.13 | 91.82 | 92.00 | 91.92 | 92.01 | 0.002117 | 0.35 | 0.37 | 2.66 | 0.30 |
| River 1 | Reach 1-Upper | 218 | 5YrSCS24Hr | 0.22 | 91.82 | 92.06 | 91.95 | 92.06 | 0.002238 | 0.42 | 0.51 | 2.91 | 0.32 |
| River 1 | Reach 1-Upper | 218 | 10YrSCS24Hr | 0.28 | 91.82 | 92.09 | 91.96 | 92.10 | 0.002340 | 0.46 | 0.60 | 3.05 | 0.33 |
| River 1 | Reach 1-Upper | 218 | 25YrSCS24Hr | 0.36 | 91.82 | 92.12 | 91.98 | 92.13 | 0.002418 | 0.50 | 0.71 | 3.22 | 0.34 |
| River 1 | Reach 1-Upper | 218 | 50YrSCS24Hr | 0.42 | 91.82 | 92.14 | 92.00 | 92.16 | 0.002473 | 0.53 | 0.79 | 3.36 | 0.35 |
| River 1 | Reach 1-Upper | 218 | 100YrSCS24Hr | 0.49 | 91.82 | 92.17 | 92.02 | 92.19 | 0.002504 | 0.56 | 0.88 | 3.53 | 0.35 |
| River 1 | Reach 1-Upper | 197 | 2YrCHI3Hr | 0.08 | 91.73 | 91.85 | 91.84 | 91.87 | 0.016181 | 0.66 | 0.12 | 1.55 | 0.75 |
| River 1 | Reach 1-Upper | 197 | 5YrCHI3Hr | 0.15 | 91.73 | 91.90 | 91.87 | 91.93 | 0.013293 | 0.73 | 0.20 | 1.87 | 0.72 |
| River 1 | Reach 1-Upper | 197 | 10YrCHI3Hr | 0.20 | 91.73 | 91.93 | 91.89 | 91.96 | 0.012335 | 0.78 | 0.25 | 2.02 | 0.71 |
| River 1 | Reach 1-Upper | 197 | 25YrCHI3Hr | 0.27 | 91.73 | 91.96 | 91.92 | 91.99 | 0.011527 | 0.84 | 0.32 | 2.18 | 0.70 |
| River 1 | Reach 1-Upper | 197 | 50YrCHI3Hr | 0.32 | 91.73 | 91.98 | 91.94 | 92.02 | 0.010809 | 0.87 | 0.37 | 2.29 | 0.69 |
| River 1 | Reach 1-Upper | 197 | 100YrCHI3Hr | 0.38 | 91.73 | 92.00 | 91.96 | 92.04 | 0.010540 | 0.91 | 0.42 | 2.39 | 0.68 |
| River 1 | Reach 1-Upper | 197 | 2YrSCS24Hr | 0.13 | 91.73 | 91.89 | 91.87 | 91.91 | 0.013973 | 0.71 | 0.18 | 1.81 | 0.72 |
| River 1 | Reach 1-Upper | 197 | 5YrSCS24Hr | 0.22 | 91.73 | 91.93 | 91.90 | 91.97 | 0.012083 | 0.80 | 0.27 | 2.06 | 0.70 |
| River 1 | Reach 1-Upper | 197 | 10YrSCS24Hr | 0.28 | 91.73 | 91.96 | 91.92 | 92.00 | 0.011418 | 0.84 | 0.33 | 2.20 | 0.70 |
| River 1 | Reach 1-Upper | 197 | 25YrSCS24Hr | 0.36 | 91.73 | 91.99 | 91.95 | 92.03 | 0.010650 | 0.89 | 0.40 | 2.34 | 0.69 |
| River 1 | Reach 1-Upper | 197 | 50YrSCS24Hr | 0.42 | 91.73 | 92.02 | 91.97 | 92.06 | 0.010407 | 0.93 | 0.45 | 2.44 | 0.69 |
| River 1 | Reach 1-Upper | 197 | 100YrSCS24Hr | 0.49 | 91.73 | 92.04 | 91.99 | 92.08 | 0.010221 | 0.96 | 0.51 | 2.55 | 0.69 |
| River 1 | Reach 1-Upper | 174 | 2YrCHI3Hr | 0.08 | 91.52 | 91.70 | 91.63 | 91.71 | 0.004212 | 0.41 | 0.19 | 1.80 | 0.40 |
| River 1 | Reach 1-Upper | 174 | 5YrCHI3Hr | 0.15 | 91.52 | 91.75 | 91.67 | 91.76 | 0.004464 | 0.50 | 0.30 | 2.17 | 0.43 |
| River 1 | Reach 1-Upper | 174 | 10YrCHI3Hr | 0.20 | 91.52 | 91.78 | 91.69 | 91.79 | 0.004633 | 0.55 | 0.36 | 2.31 | 0.45 |
| River 1 | Reach 1-Upper | 174 | 25YrCHI3Hr | 0.27 | 91.52 | 91.81 | 91.72 | 91.83 | 0.004788 | 0.61 | 0.44 | 2.47 | 0.46 |
| River 1 | Reach 1-Upper | 174 | 50YrCHI3Hr | 0.32 | 91.52 | 91.83 | 91.74 | 91.85 | 0.004947 | 0.65 | 0.50 | 2.58 | 0.48 |
| River 1 | Reach 1-Upper | 174 | 100YrCHI3Hr | 0.38 | 91.52 | 91.85 | 91.76 | 91.88 | 0.005078 | 0.69 | 0.56 | 2.69 | 0.49 |
| River 1 | Reach 1-Upper | 174 | 2YrSCS24Hr | 0.13 | 91.52 | 91.74 | 91.66 | 91.75 | 0.004366 | 0.47 | 0.27 | 2.08 | 0.42 |
| River 1 | Reach 1-Upper | 174 | 5YrSCS24Hr | 0.22 | 91.52 | 91.78 | 91.70 | 91.80 | 0.004685 | 0.57 | 0.38 | 2.35 | 0.45 |
| River 1 | Reach 1-Upper | 174 | 10YrSCS24Hr | 0.28 | 91.52 | 91.81 | 91.73 | 91.83 | 0.004821 | 0.62 | 0.45 | 2.49 | 0.46 |
| River 1 | Reach 1-Upper | 174 | 25YrSCS24Hr | 0.36 | 91.52 | 91.84 | 91.75 | 91.87 | 0.005024 | 0.67 | 0.53 | 2.65 | 0.48 |
| River 1 | Reach 1-Upper | 174 | 50YrSCS24Hr | 0.42 | 91.52 | 91.87 | 91.77 | 91.89 | 0.005141 | 0.71 | 0.59 | 2.76 | 0.49 |
| River 1 | Reach 1-Upper | 174 | 100YrSCS24Hr | 0.49 | 91.52 | 91.89 | 91.79 | 91.92 | 0.005179 | 0.75 | 0.66 | 2.87 | 0.50 |
| River 1 | Reach 1-Upper | 154 | 2YrCHI3Hr | 0.08 | 91.43 | 91.61 | 91.56 | 91.62 | 0.004328 | 0.39 | 0.21 | 2.16 | 0.40 |
| River 1 | Reach 1-Upper | 154 | 5YrCHI3Hr | 0.15 | 91.43 | 91.66 | 91.59 | 91.67 | 0.004181 | 0.46 | 0.32 | 2.60 | 0.41 |
| River 1 | Reach 1-Upper | 154 | 10YrCHI3Hr | 0.20 | 91.43 | 91.69 | 91.61 | 91.70 | 0.004190 | 0.49 | 0.40 | 2.83 | 0.42 |
| River 1 | Reach 1-Upper | 154 | 25YrCHI3Hr | 0.27 | 91.43 | 91.72 | 91.64 | 91.74 | 0.004087 | 0.53 | 0.50 | 3.11 | 0.42 |
| River 1 | Reach 1-Upper | 154 | 50YrCHI3Hr | 0.32 | 91.43 | 91.75 | 91.65 | 91.76 | 0.003985 | 0.56 | 0.58 | 3.28 | 0.43 |
| River 1 | Reach 1-Upper | 154 | 100YrCHI3Hr | 0.38 | 91.43 | 91.77 | 91.67 | 91.79 | 0.003882 | 0.58 | 0.66 | 3.44 | 0.43 |

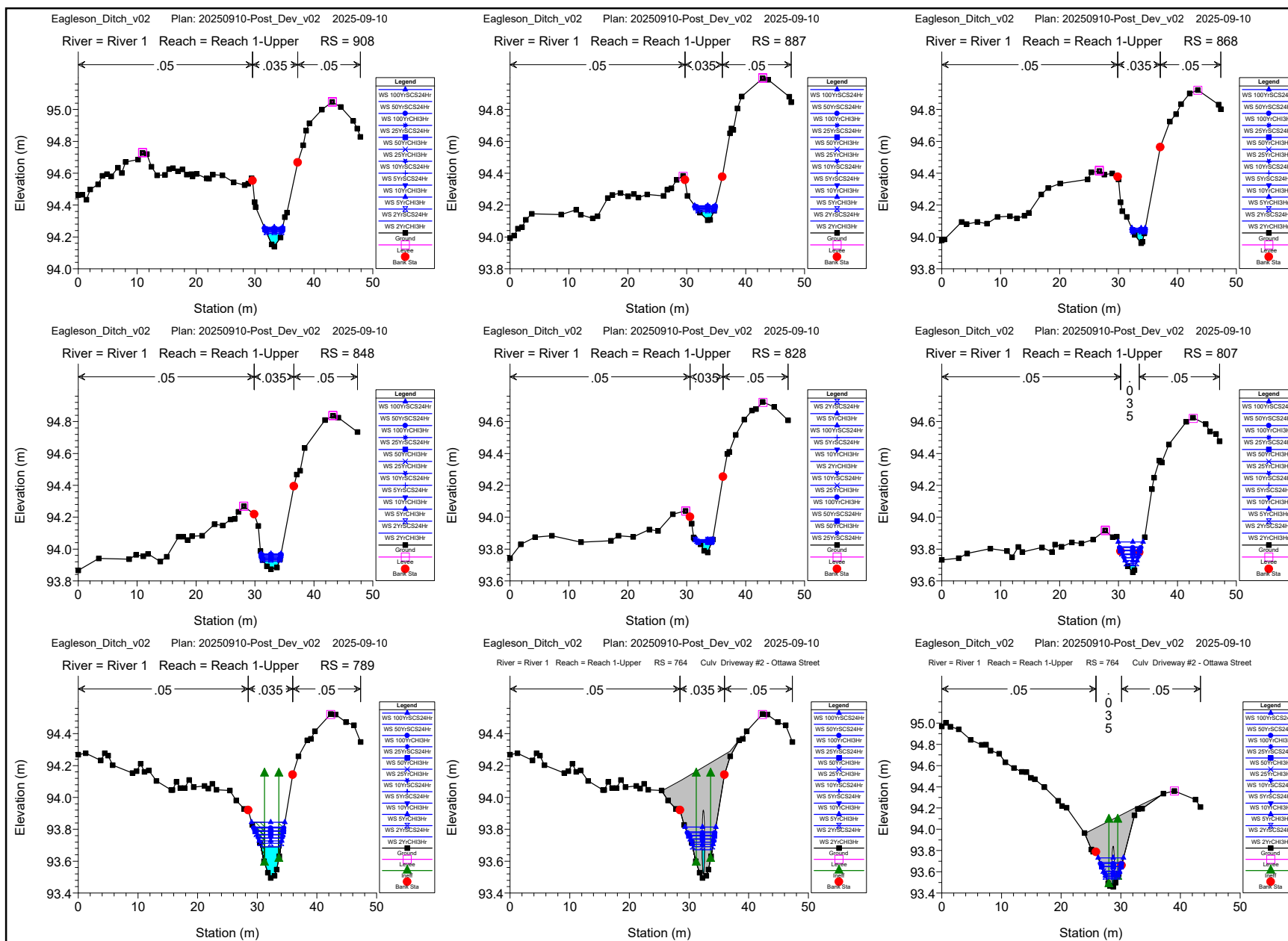
HEC-RAS Plan: 20250603-Pre_Dev_v01 (Continued)

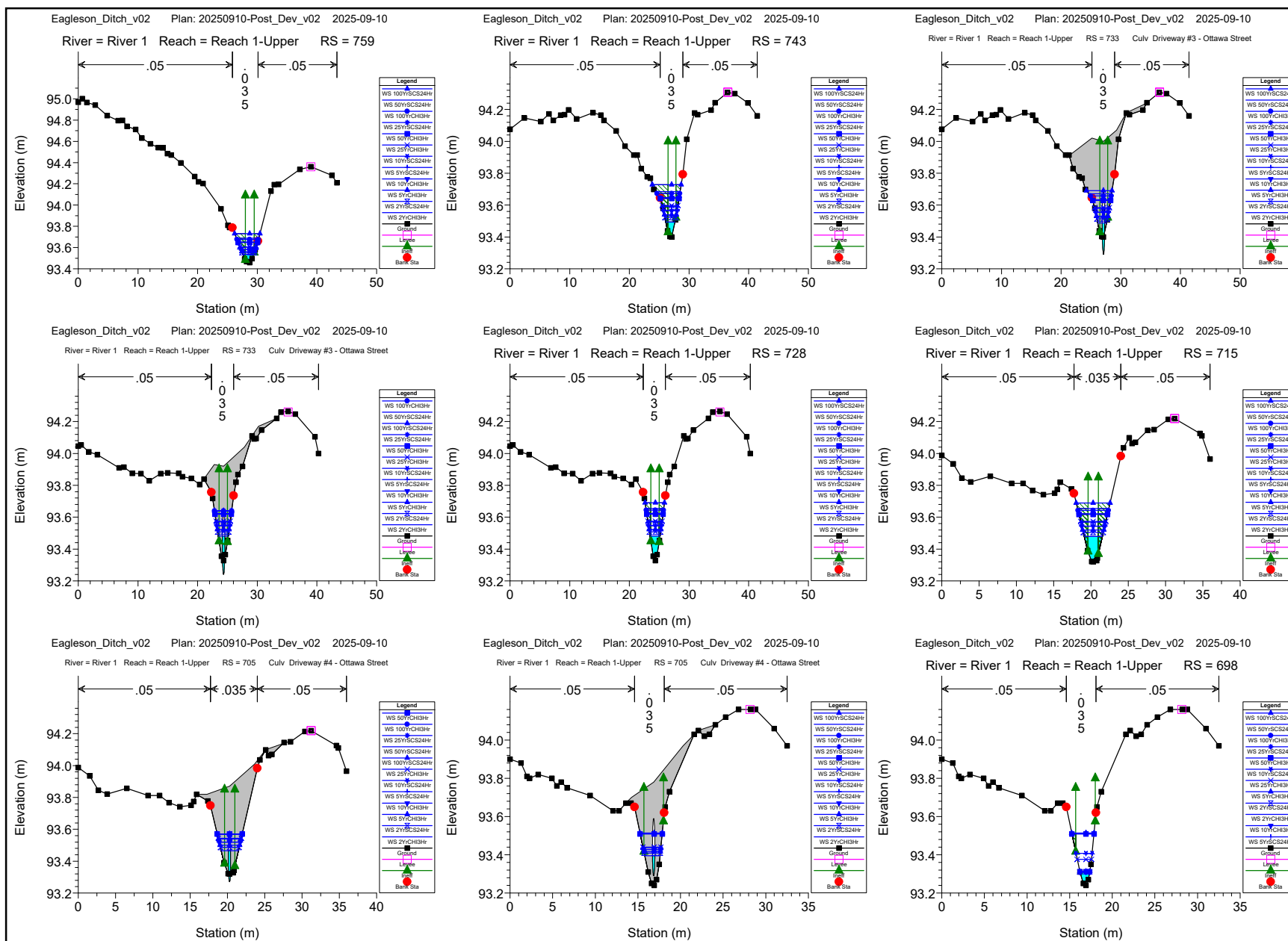
| River | Reach | River Sta | Profile | Q Total (m3/s) | Min Ch El (m) | W.S. Elev (m) | Crit W.S. (m) | E.G. Elev (m) | E.G. Slope (m/m) | Vel Chnl (m/s) | Flow Area (m2) | Top Width (m) | Froude # Chl |
|---------|---------------|-----------|--------------|-------------------|------------------|------------------|------------------|------------------|---------------------|-------------------|-------------------|------------------|--------------|
| River 1 | Reach 1-Upper | 154 | 2YrSCS24Hr | 0.13 | 91.43 | 91.65 | 91.58 | 91.66 | 0.004251 | 0.44 | 0.29 | 2.49 | 0.41 |
| River 1 | Reach 1-Upper | 154 | 5YrSCS24Hr | 0.22 | 91.43 | 91.70 | 91.62 | 91.71 | 0.004167 | 0.51 | 0.43 | 2.91 | 0.42 |
| River 1 | Reach 1-Upper | 154 | 10YrSCS24Hr | 0.28 | 91.43 | 91.73 | 91.64 | 91.74 | 0.004071 | 0.54 | 0.51 | 3.14 | 0.43 |
| River 1 | Reach 1-Upper | 154 | 25YrSCS24Hr | 0.36 | 91.43 | 91.76 | 91.66 | 91.78 | 0.003925 | 0.57 | 0.62 | 3.37 | 0.43 |
| River 1 | Reach 1-Upper | 154 | 50YrSCS24Hr | 0.42 | 91.43 | 91.79 | 91.68 | 91.80 | 0.003830 | 0.60 | 0.71 | 3.53 | 0.43 |
| River 1 | Reach 1-Upper | 154 | 100YrSCS24Hr | 0.49 | 91.43 | 91.81 | 91.70 | 91.83 | 0.003747 | 0.62 | 0.79 | 3.69 | 0.43 |
| River 1 | Reach 1-Upper | 137 | 2YrCHI3Hr | 0.08 | 91.33 | 91.48 | 91.46 | 91.50 | 0.012189 | 0.63 | 0.13 | 1.39 | 0.66 |
| River 1 | Reach 1-Upper | 137 | 5YrCHI3Hr | 0.15 | 91.33 | 91.53 | 91.50 | 91.56 | 0.011338 | 0.73 | 0.20 | 1.65 | 0.67 |
| River 1 | Reach 1-Upper | 137 | 10YrCHI3Hr | 0.20 | 91.33 | 91.56 | 91.52 | 91.59 | 0.011017 | 0.79 | 0.25 | 1.80 | 0.67 |
| River 1 | Reach 1-Upper | 137 | 25YrCHI3Hr | 0.27 | 91.33 | 91.60 | 91.55 | 91.63 | 0.010550 | 0.84 | 0.32 | 1.99 | 0.67 |
| River 1 | Reach 1-Upper | 137 | 50YrCHI3Hr | 0.32 | 91.33 | 91.62 | 91.57 | 91.66 | 0.010206 | 0.88 | 0.37 | 2.12 | 0.67 |
| River 1 | Reach 1-Upper | 137 | 100YrCHI3Hr | 0.38 | 91.33 | 91.65 | 91.59 | 91.69 | 0.009820 | 0.90 | 0.42 | 2.25 | 0.66 |
| River 1 | Reach 1-Upper | 137 | 2YrSCS24Hr | 0.13 | 91.33 | 91.52 | 91.49 | 91.54 | 0.011464 | 0.71 | 0.18 | 1.58 | 0.67 |
| River 1 | Reach 1-Upper | 137 | 5YrSCS24Hr | 0.22 | 91.33 | 91.57 | 91.53 | 91.60 | 0.010898 | 0.80 | 0.27 | 1.85 | 0.67 |
| River 1 | Reach 1-Upper | 137 | 10YrSCS24Hr | 0.28 | 91.33 | 91.60 | 91.55 | 91.64 | 0.010487 | 0.85 | 0.33 | 2.01 | 0.67 |
| River 1 | Reach 1-Upper | 137 | 25YrSCS24Hr | 0.36 | 91.33 | 91.63 | 91.58 | 91.68 | 0.009938 | 0.89 | 0.40 | 2.20 | 0.67 |
| River 1 | Reach 1-Upper | 137 | 50YrSCS24Hr | 0.42 | 91.33 | 91.66 | 91.60 | 91.70 | 0.009574 | 0.92 | 0.46 | 2.33 | 0.66 |
| River 1 | Reach 1-Upper | 137 | 100YrSCS24Hr | 0.49 | 91.33 | 91.69 | 91.62 | 91.73 | 0.009283 | 0.95 | 0.52 | 2.46 | 0.66 |
| River 1 | Reach 1-Upper | 116 | 2YrCHI3Hr | 0.08 | 91.23 | 91.38 | 91.32 | 91.39 | 0.003082 | 0.36 | 0.22 | 2.06 | 0.35 |
| River 1 | Reach 1-Upper | 116 | 5YrCHI3Hr | 0.15 | 91.23 | 91.43 | 91.35 | 91.44 | 0.002930 | 0.42 | 0.35 | 2.36 | 0.35 |
| River 1 | Reach 1-Upper | 116 | 10YrCHI3Hr | 0.20 | 91.23 | 91.47 | 91.37 | 91.48 | 0.002864 | 0.46 | 0.43 | 2.55 | 0.36 |
| River 1 | Reach 1-Upper | 116 | 25YrCHI3Hr | 0.27 | 91.23 | 91.51 | 91.39 | 91.52 | 0.002818 | 0.50 | 0.54 | 2.77 | 0.36 |
| River 1 | Reach 1-Upper | 116 | 50YrCHI3Hr | 0.32 | 91.23 | 91.54 | 91.41 | 91.55 | 0.002807 | 0.52 | 0.62 | 2.92 | 0.36 |
| River 1 | Reach 1-Upper | 116 | 100YrCHI3Hr | 0.38 | 91.23 | 91.56 | 91.42 | 91.58 | 0.002814 | 0.55 | 0.70 | 3.06 | 0.37 |
| River 1 | Reach 1-Upper | 116 | 2YrSCS24Hr | 0.13 | 91.23 | 91.42 | 91.34 | 91.43 | 0.002964 | 0.41 | 0.31 | 2.29 | 0.35 |
| River 1 | Reach 1-Upper | 116 | 5YrSCS24Hr | 0.22 | 91.23 | 91.48 | 91.37 | 91.49 | 0.002843 | 0.47 | 0.46 | 2.61 | 0.36 |
| River 1 | Reach 1-Upper | 116 | 10YrSCS24Hr | 0.28 | 91.23 | 91.51 | 91.39 | 91.53 | 0.002817 | 0.50 | 0.55 | 2.79 | 0.36 |
| River 1 | Reach 1-Upper | 116 | 25YrSCS24Hr | 0.36 | 91.23 | 91.55 | 91.42 | 91.57 | 0.002792 | 0.54 | 0.66 | 3.00 | 0.37 |
| River 1 | Reach 1-Upper | 116 | 50YrSCS24Hr | 0.42 | 91.23 | 91.58 | 91.43 | 91.60 | 0.002600 | 0.55 | 0.76 | 3.16 | 0.36 |
| River 1 | Reach 1-Upper | 116 | 100YrSCS24Hr | 0.49 | 91.23 | 91.61 | 91.45 | 91.63 | 0.002607 | 0.58 | 0.85 | 3.28 | 0.36 |
| River 1 | Reach 1-Upper | 95 | 2YrCHI3Hr | 0.08 | 91.07 | 91.28 | 91.23 | 91.29 | 0.006001 | 0.51 | 0.16 | 1.35 | 0.48 |
| River 1 | Reach 1-Upper | 95 | 5YrCHI3Hr | 0.15 | 91.07 | 91.33 | 91.27 | 91.35 | 0.006981 | 0.63 | 0.23 | 1.60 | 0.53 |
| River 1 | Reach 1-Upper | 95 | 10YrCHI3Hr | 0.20 | 91.07 | 91.36 | 91.30 | 91.39 | 0.007514 | 0.71 | 0.28 | 1.73 | 0.56 |
| River 1 | Reach 1-Upper | 95 | 25YrCHI3Hr | 0.27 | 91.07 | 91.39 | 91.33 | 91.43 | 0.008051 | 0.78 | 0.34 | 1.89 | 0.59 |
| River 1 | Reach 1-Upper | 95 | 50YrCHI3Hr | 0.32 | 91.07 | 91.42 | 91.35 | 91.45 | 0.008531 | 0.84 | 0.38 | 1.99 | 0.61 |
| River 1 | Reach 1-Upper | 95 | 100YrCHI3Hr | 0.38 | 91.07 | 91.42 | 91.37 | 91.47 | 0.011364 | 0.98 | 0.39 | 2.01 | 0.71 |
| River 1 | Reach 1-Upper | 95 | 2YrSCS24Hr | 0.13 | 91.07 | 91.32 | 91.26 | 91.34 | 0.006833 | 0.61 | 0.21 | 1.53 | 0.52 |
| River 1 | Reach 1-Upper | 95 | 5YrSCS24Hr | 0.22 | 91.07 | 91.37 | 91.30 | 91.40 | 0.007484 | 0.72 | 0.30 | 1.78 | 0.56 |
| River 1 | Reach 1-Upper | 95 | 10YrSCS24Hr | 0.28 | 91.07 | 91.40 | 91.33 | 91.43 | 0.008260 | 0.80 | 0.35 | 1.90 | 0.60 |
| River 1 | Reach 1-Upper | 95 | 25YrSCS24Hr | 0.36 | 91.07 | 91.43 | 91.36 | 91.47 | 0.008800 | 0.87 | 0.41 | 2.08 | 0.63 |
| River 1 | Reach 1-Upper | 95 | 50YrSCS24Hr | 0.42 | 91.07 | 91.39 | 91.38 | 91.47 | 0.022828 | 1.30 | 0.32 | 1.85 | 0.99 |
| River 1 | Reach 1-Upper | 95 | 100YrSCS24Hr | 0.49 | 91.07 | 91.41 | 91.41 | 91.50 | 0.022422 | 1.34 | 0.37 | 1.95 | 0.99 |
| River 1 | Reach 1-Upper | 72 | 2YrCHI3Hr | 0.08 | 90.91 | 91.00 | 91.00 | 91.03 | 0.030836 | 0.74 | 0.11 | 1.93 | 0.99 |
| River 1 | Reach 1-Upper | 72 | 5YrCHI3Hr | 0.15 | 90.91 | 91.03 | 91.03 | 91.07 | 0.028202 | 0.84 | 0.18 | 2.40 | 0.99 |
| River 1 | Reach 1-Upper | 72 | 10YrCHI3Hr | 0.20 | 90.91 | 91.05 | 91.05 | 91.09 | 0.027394 | 0.90 | 0.22 | 2.63 | 0.99 |
| River 1 | Reach 1-Upper | 72 | 25YrCHI3Hr | 0.27 | 90.91 | 91.07 | 91.07 | 91.12 | 0.026901 | 0.98 | 0.27 | 2.82 | 1.01 |
| River 1 | Reach 1-Upper | 72 | 50YrCHI3Hr | 0.32 | 90.91 | 91.08 | 91.08 | 91.14 | 0.025605 | 1.02 | 0.32 | 2.96 | 1.00 |
| River 1 | Reach 1-Upper | 72 | 100YrCHI3Hr | 0.38 | 90.91 | 91.11 | 91.10 | 91.16 | 0.016324 | 0.92 | 0.42 | 3.23 | 0.82 |
| River 1 | Reach 1-Upper | 72 | 2YrSCS24Hr | 0.13 | 90.91 | 91.02 | 91.02 | 91.06 | 0.027869 | 0.80 | 0.16 | 2.30 | 0.97 |
| River 1 | Reach 1-Upper | 72 | 5YrSCS24Hr | 0.22 | 90.91 | 91.05 | 91.05 | 91.10 | 0.028793 | 0.94 | 0.23 | 2.67 | 1.02 |
| River 1 | Reach 1-Upper | 72 | 10YrSCS24Hr | 0.28 | 90.91 | 91.07 | 91.07 | 91.12 | 0.025957 | 0.98 | 0.28 | 2.86 | 0.99 |
| River 1 | Reach 1-Upper | 72 | 25YrSCS24Hr | 0.36 | 90.91 | 91.09 | 91.09 | 91.15 | 0.025859 | 1.06 | 0.34 | 3.02 | 1.01 |
| River 1 | Reach 1-Upper | 72 | 50YrSCS24Hr | 0.42 | 90.91 | 91.17 | 91.11 | 91.19 | 0.006772 | 0.70 | 0.60 | 3.69 | 0.55 |
| River 1 | Reach 1-Upper | 72 | 100YrSCS24Hr | 0.49 | 90.91 | 91.24 | 91.12 | 91.26 | 0.002972 | 0.55 | 0.89 | 4.14 | 0.38 |
| River 1 | Reach 1-Lower | 56 | 2YrCHI3Hr | 0.14 | 90.47 | 90.73 | 90.57 | 90.73 | 0.000365 | 0.19 | 0.73 | 10.09 | 0.13 |
| River 1 | Reach 1-Lower | 56 | 5YrCHI3Hr | 0.26 | 90.47 | 90.84 | 90.60 | 90.85 | 0.000293 | 0.23 | 1.14 | 14.27 | 0.13 |
| River 1 | Reach 1-Lower | 56 | 10YrCHI3Hr | 0.36 | 90.47 | 90.92 | 90.62 | 90.92 | 0.000277 | 0.26 | 1.40 | 17.00 | 0.13 |
| River 1 | Reach 1-Lower | 56 | 25YrCHI3Hr | 0.49 | 90.47 | 91.01 | 90.64 | 91.01 | 0.000267 | 0.29 | 1.71 | 19.79 | 0.13 |
| River 1 | Reach 1-Lower | 56 | 50YrCHI3Hr | 0.60 | 90.47 | 91.07 | 90.66 | 91.08 | 0.000264 | 0.31 | 1.93 | 20.02 | 0.13 |
| River 1 | Reach 1-Lower | 56 | 100YrCHI3Hr | 0.72 | 90.47 | 91.13 | 90.68 | 91.14 | 0.000264 | 0.34 | 2.15 | 20.02 | 0.14 |
| River 1 | Reach 1-Lower | 56 | 2YrSCS24Hr | 0.23 | 90.47 | 90.82 | 90.59 | 90.82 | 0.000307 | 0.22 | 1.05 | 13.08 | 0.13 |
| River 1 | Reach 1-Lower | 56 | 5YrSCS24Hr | 0.40 | 90.47 | 90.95 | 90.63 | 90.95 | 0.000273 | 0.27 | 1.50 | 18.26 | 0.13 |
| River 1 | Reach 1-Lower | 56 | 10YrSCS24Hr | 0.52 | 90.47 | 91.02 | 90.65 | 91.02 | 0.000269 | 0.29 | 1.75 | 19.92 | 0.13 |
| River 1 | Reach 1-Lower | 56 | 25YrSCS24Hr | 0.68 | 90.47 | 91.11 | 90.67 | 91.12 | 0.000263 | 0.33 | 2.07 | 20.02 | 0.14 |
| River 1 | Reach 1-Lower | 56 | 50YrSCS24Hr | 0.80 | 90.47 | 91.17 | 90.70 | 91.18 | 0.000261 | 0.35 | 2.30 | 20.02 | 0.14 |
| River 1 | Reach 1-Lower | 56 | 100YrSCS24Hr | 0.94 | 90.47 | 91.24 | 90.71 | 91.25 | 0.000262 | 0.37 | 2.53 | 20.02 | 0.14 |
| River 1 | Reach 1-Lower | 50 | | Culvert | | | | | | | | | |
| River 1 | Reach 1-Lower | 38 | 2YrCHI3Hr | 0.14 | 90.46 | 90.57 | 90.53 | 90.58 | 0.004969 | 0.42 | 0.33 | 30.00 | 0.43 |
| River 1 | Reach 1-Lower | 38 | 5YrCHI3Hr | 0.26 | 90.46 | 90.60 | 90.55 | 90.62 | 0.006999 | 0.60 | 0.44 | 34.38 | 0.54 |
| River 1 | Reach 1-Lower | 38 | 10YrCHI3Hr | 0.36 | 90.46 | 90.61 | 90.57 | 90.64 | 0.008612 | 0.72 | 0.50 | 35.69 | 0.61 |
| River 1 | Reach 1-Lower | 38 | 25YrCHI3Hr | 0.49 | 90.46 | 90.63 | 90.60 | 90.67 | 0.010692 | 0.87 | 0.56 | 36.54 | 0.70 |
| River 1 | Reach 1-Lower | 38 | 50YrCHI3Hr | 0.60 | 90.46 | 90.64 | 90.62 | 90.69 | 0.012409 | 0.99 | 0.61 | 36.97 | 0.76 |
| River 1 | Reach 1-Lower | 38 | 100YrCHI3Hr | 0.72 | 90.46 | 90.66 | 90.64 | 90.72 | 0.014104 | 1.11 | 0.65 | 37.73 | 0.82 |
| River 1 | Reach 1-Lower | 38 | 2YrSCS24Hr | 0.23 | 90.46 | 90.59 | 90.55 | 90.61 | 0.006395 | 0.56 | 0.42 | 33.55 | 0.51 |
| River 1 | Reach 1-Lower | 38 | 5YrSCS24Hr | 0.40 | 90.46 | 90.62 | 90.58 | 90.65 | 0.009230 | 0.77 | 0.52 | 36.26 | 0.64 |
| River 1 | Reach 1-Lower | 38 | 10YrSCS24Hr | 0.52 | 90.46 | 90.64 | 90.60 | 90.68 | 0.011069 | 0.90 | 0.57 | 36.60 | 0.71 |
| River 1 | Reach 1-Lower | 38 | 25YrSCS24Hr | 0.68 | 90.46 | 90.65 | 90.63 | 90.71 | 0.013373 | 1.06 | 0.64 | 37.45 | 0.79 |
| River 1 | Reach 1-Lower | 38 | 50YrSCS24Hr | 0.80 | 90.46 | 90.66 | 90.64 | 90.74 | 0.015442 | 1.19 | 0.68 | 38.06 | 0.86 |
| River 1 | Reach 1-Lower | 38 | 100YrSCS24Hr | 0.94 | 90.46 | 90.67 | 90.66 | 90.76 | 0.018005 | 1.32 | 0.71 | 38.54 | 0.94 |
| River 1 | Reach 1-Lower | 0 | 2YrCHI3Hr | 0.14 | 90.42 | 90.50 | 90.46 | 90.50 | 0.001001 | 0.13 | 1.06 | 18.74 | 0.18 |
| River 1 | Reach 1-Lower | 0 | 5YrCHI3Hr | 0.26 | 90.42 | 90.53 | 90.47 | 90.53 | 0.001000 | 0.17 | 1.59 | 20.04 | 0.19 |
| River 1 | Reach 1-Lower | 0 | 10YrCHI3Hr | 0.36 | 90.42 | 90.54 | 90.48 | 90.55 | 0.001000 | 0.19 | 1.92 | 20.29 | 0.19 |

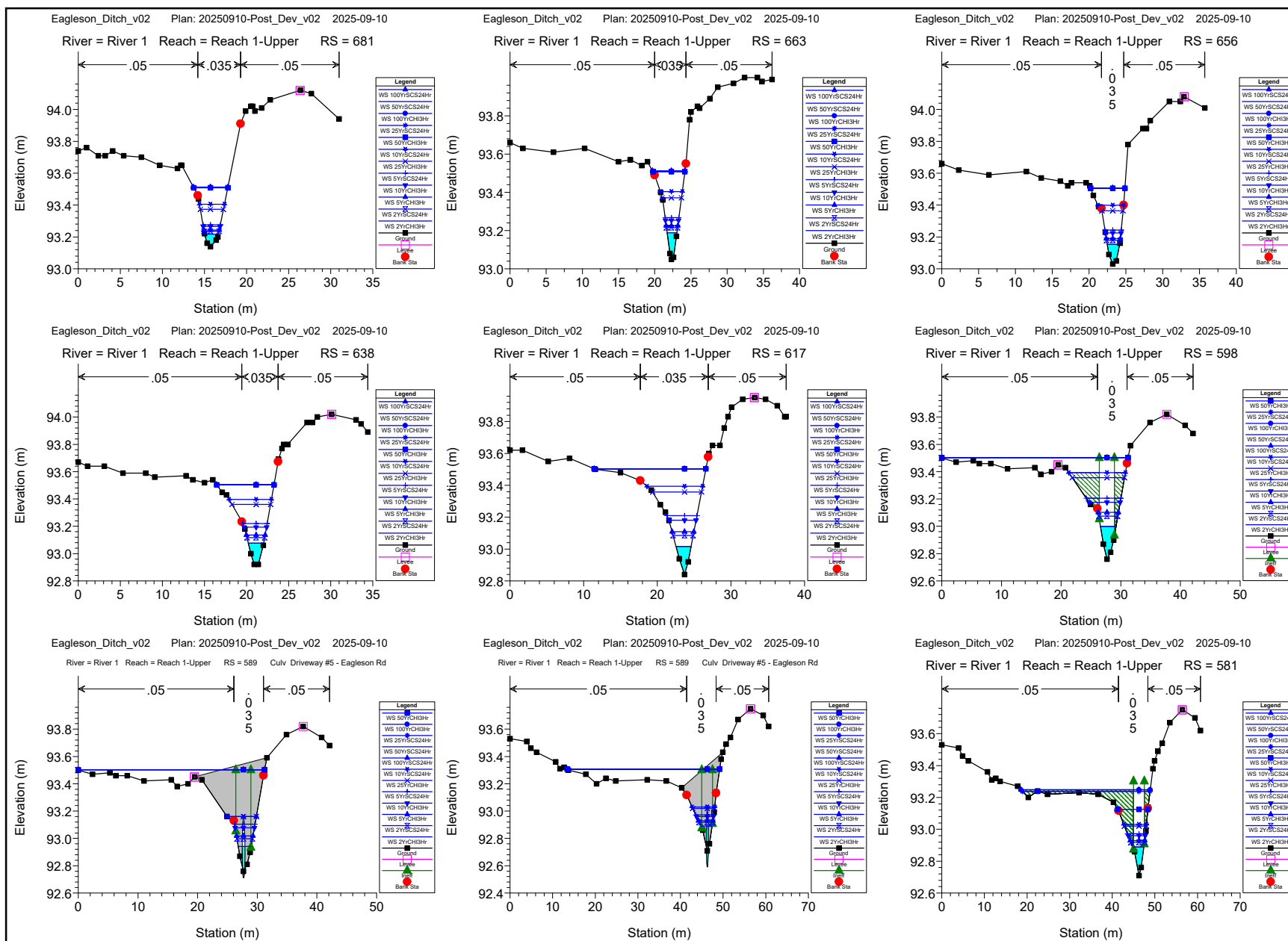
HEC-RAS Plan: 20250603-Pre_Dev_v01 (Continued)

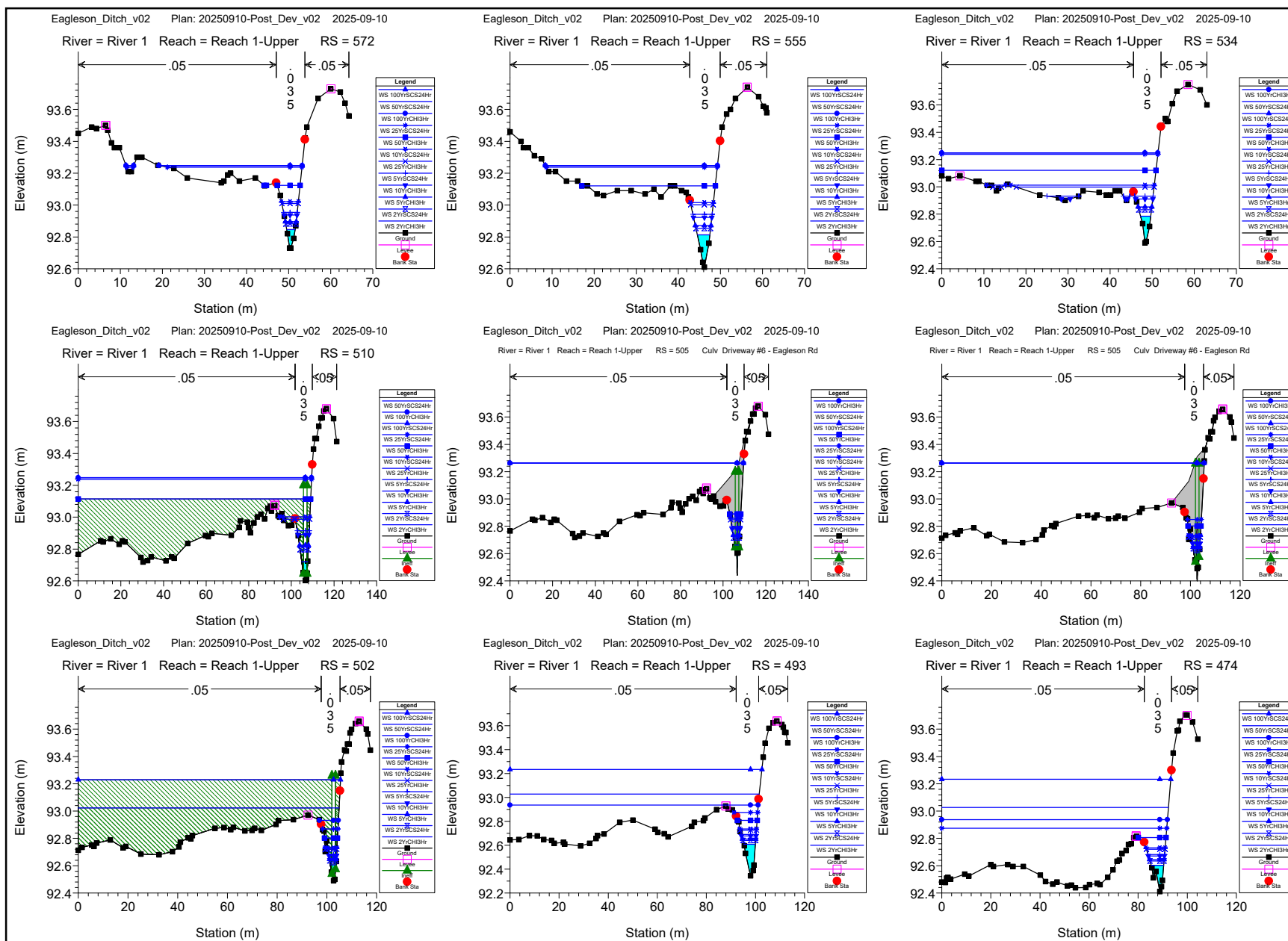
| River | Reach | River Sta | Profile | Q Total (m3/s) | Min Ch El (m) | W.S. Elev (m) | Crit W.S. (m) | E.G. Elev (m) | E.G. Slope (m/m) | Vel Chnl (m/s) | Flow Area (m2) | Top Width (m) | Froude # Chl |
|---------|---------------|-----------|--------------|-------------------|------------------|------------------|------------------|------------------|---------------------|-------------------|-------------------|------------------|--------------|
| River 1 | Reach 1-Lower | 0 | 25YrCHI3Hr | 0.49 | 90.42 | 90.56 | 90.49 | 90.57 | 0.001001 | 0.21 | 2.33 | 20.58 | 0.20 |
| River 1 | Reach 1-Lower | 0 | 50YrCHI3Hr | 0.60 | 90.42 | 90.58 | 90.49 | 90.58 | 0.001000 | 0.23 | 2.64 | 20.80 | 0.20 |
| River 1 | Reach 1-Lower | 0 | 100YrCHI3Hr | 0.72 | 90.42 | 90.59 | 90.50 | 90.60 | 0.001000 | 0.24 | 2.98 | 21.46 | 0.21 |
| River 1 | Reach 1-Lower | 0 | 2YrSCS24Hr | 0.23 | 90.42 | 90.52 | 90.46 | 90.52 | 0.001000 | 0.16 | 1.47 | 19.96 | 0.19 |
| River 1 | Reach 1-Lower | 0 | 5YrSCS24Hr | 0.40 | 90.42 | 90.55 | 90.48 | 90.55 | 0.001001 | 0.20 | 2.05 | 20.38 | 0.20 |
| River 1 | Reach 1-Lower | 0 | 10YrSCS24Hr | 0.52 | 90.42 | 90.57 | 90.48 | 90.57 | 0.001001 | 0.22 | 2.40 | 20.63 | 0.20 |
| River 1 | Reach 1-Lower | 0 | 25YrSCS24Hr | 0.68 | 90.42 | 90.59 | 90.49 | 90.59 | 0.001000 | 0.24 | 2.85 | 21.31 | 0.21 |
| River 1 | Reach 1-Lower | 0 | 50YrSCS24Hr | 0.80 | 90.42 | 90.60 | 90.50 | 90.61 | 0.001001 | 0.25 | 3.18 | 21.58 | 0.21 |
| River 1 | Reach 1-Lower | 0 | 100YrSCS24Hr | 0.94 | 90.42 | 90.62 | 90.51 | 90.62 | 0.001000 | 0.27 | 3.51 | 21.78 | 0.21 |

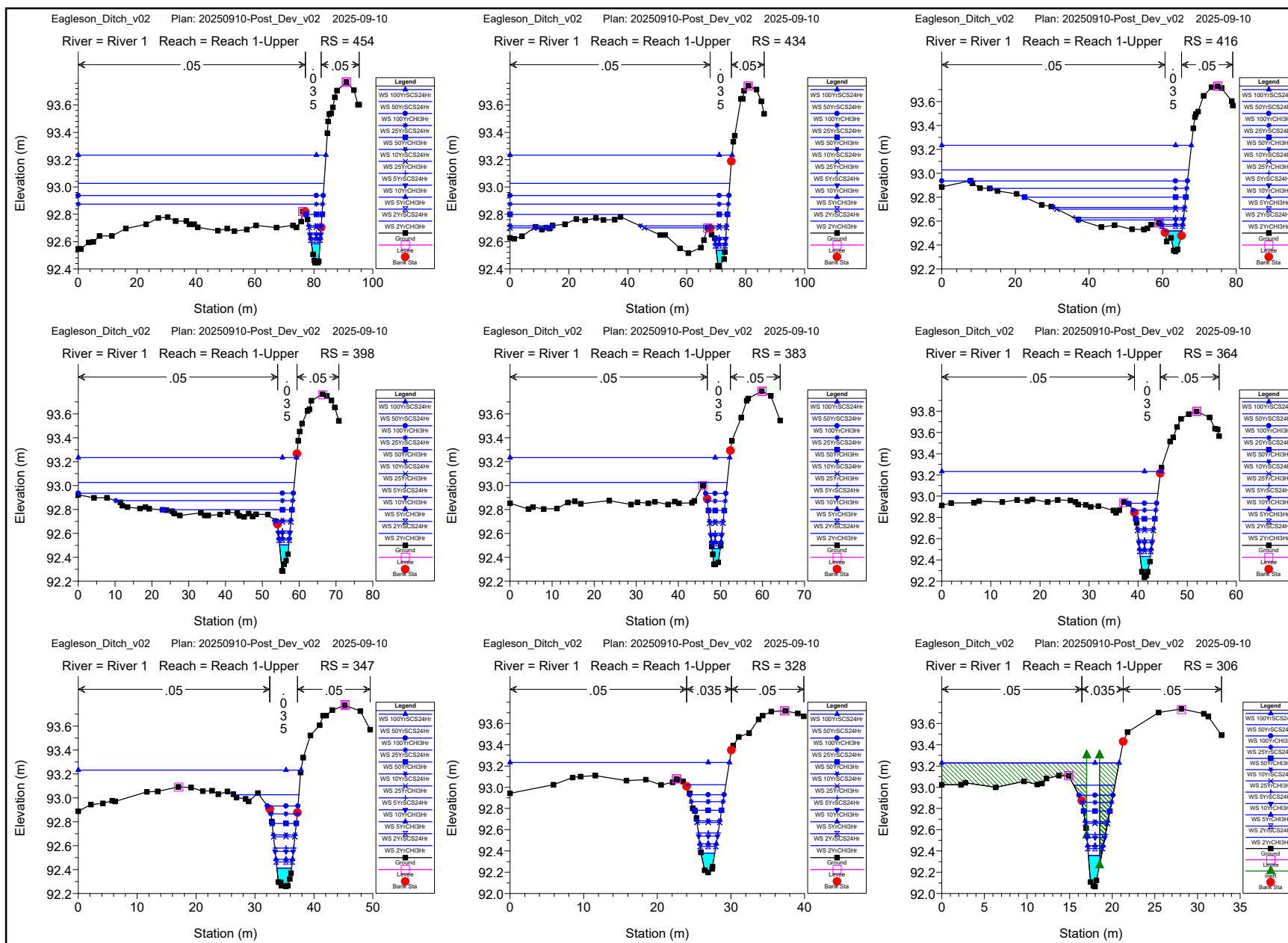


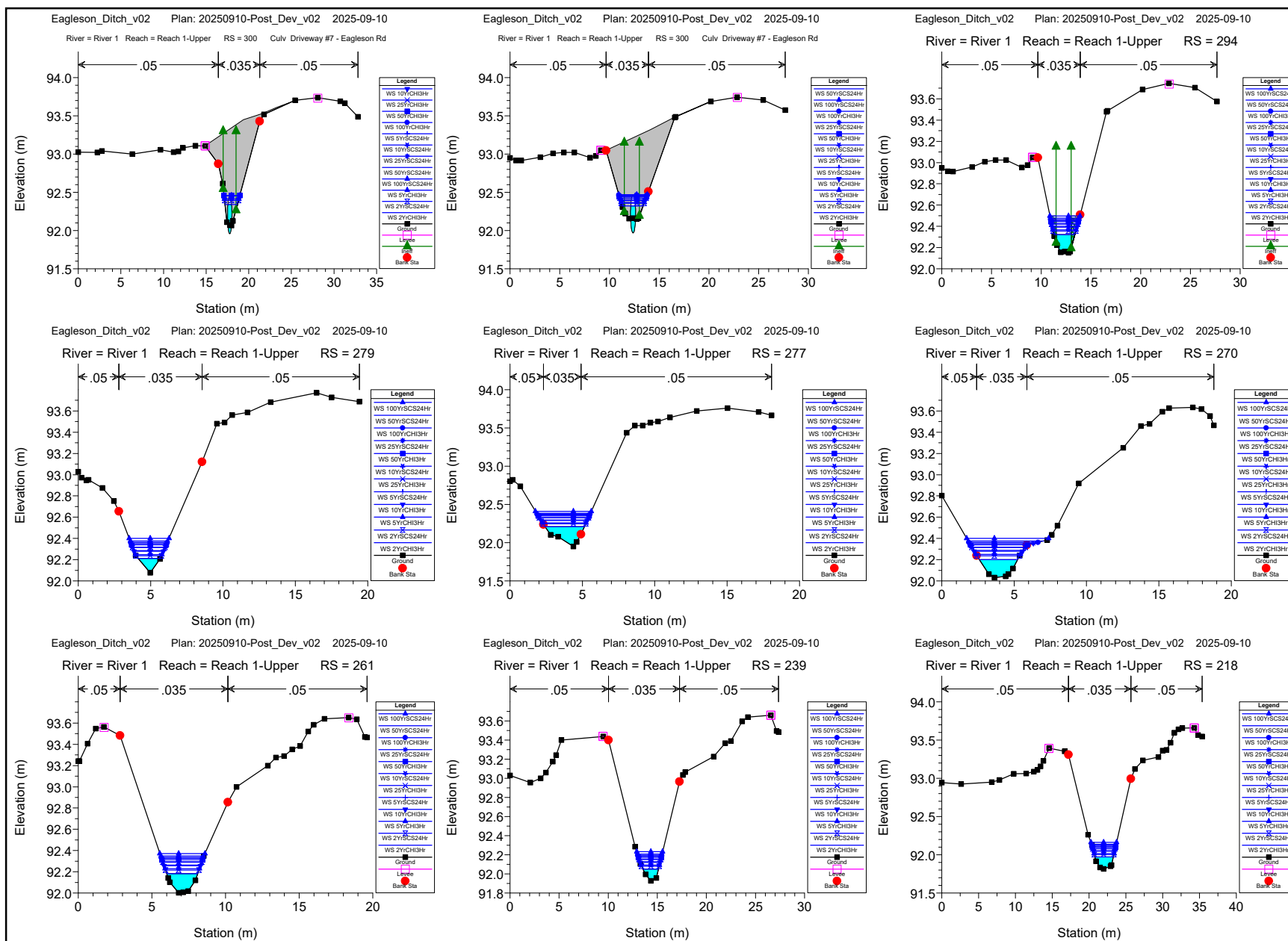


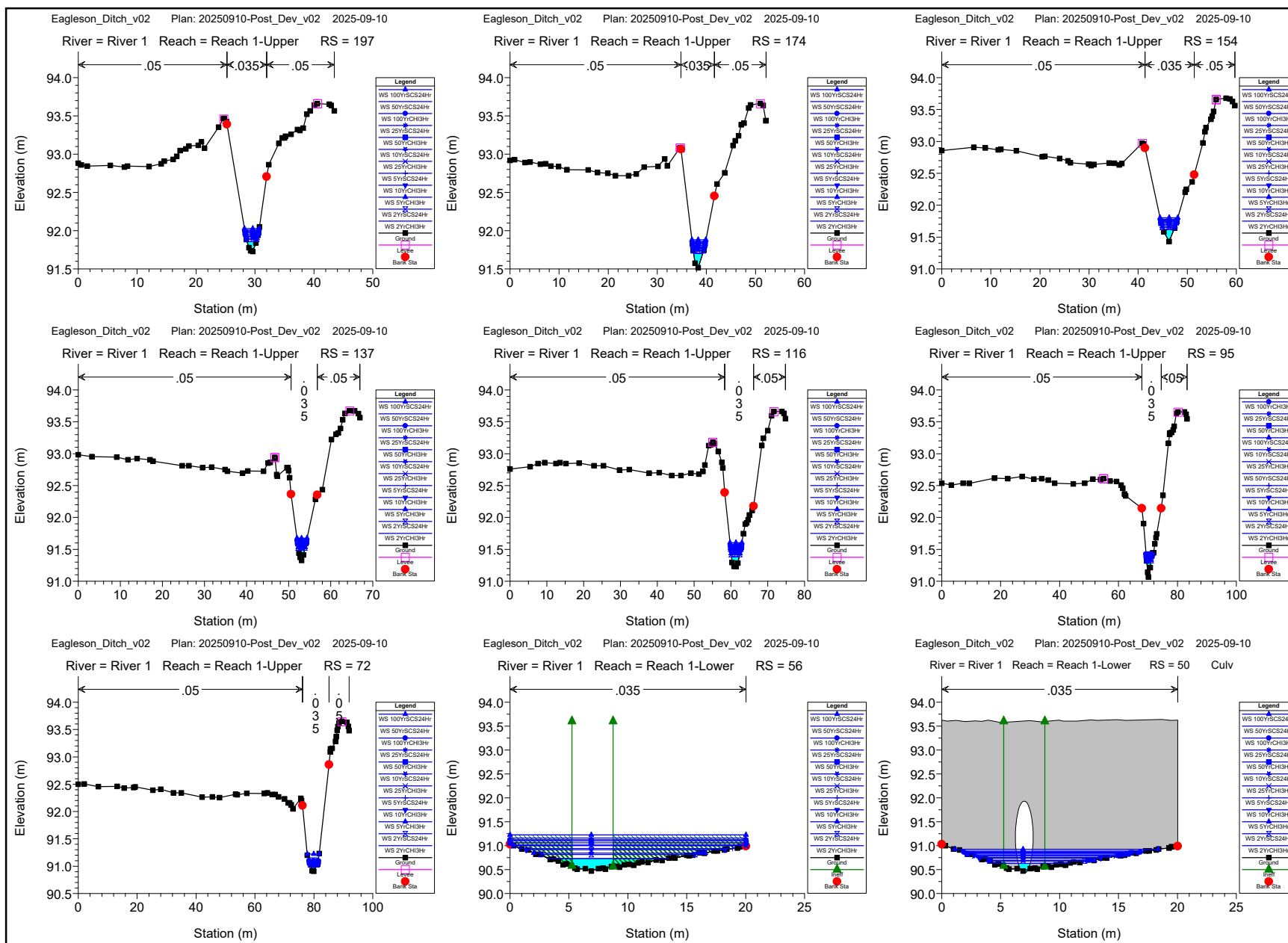


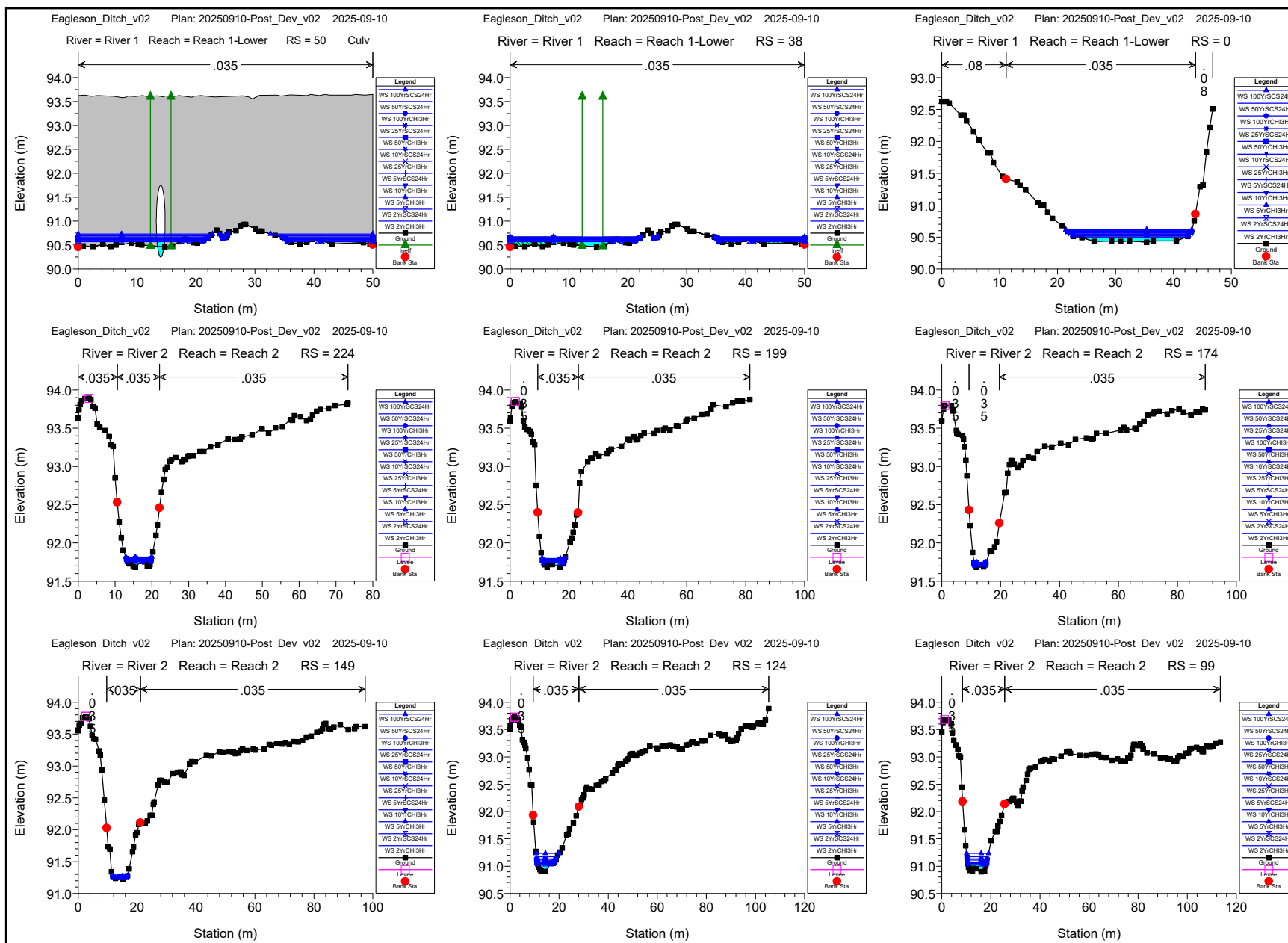




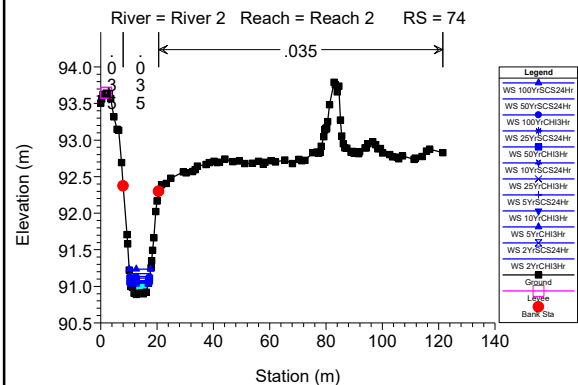




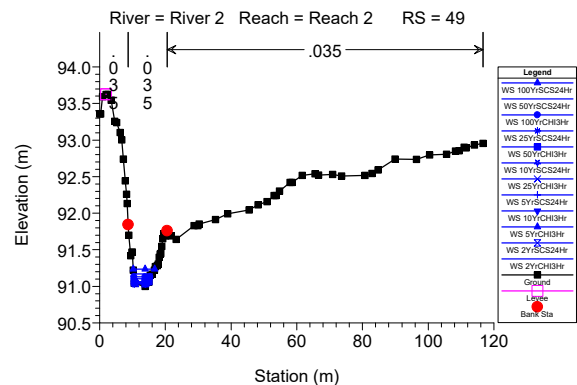




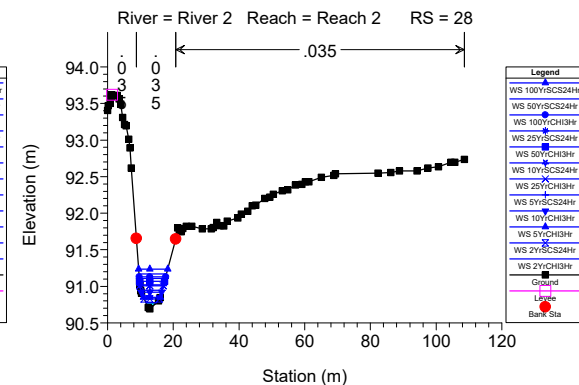
Eagleson_Ditch_v02 Plan: 20250910-Post_Dev_v02 2025-09-10



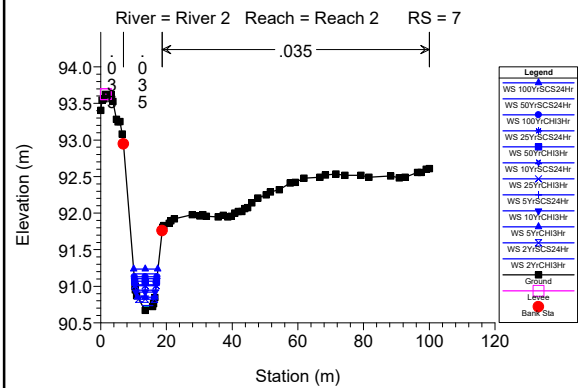
Eagleson_Ditch_v02 Plan: 20250910-Post_Dev_v02 2025-09-10



Eagleson_Ditch_v02 Plan: 20250910-Post_Dev_v02 2025-09-10



Eagleson_Ditch_v02 Plan: 20250910-Post_Dev_v02 2025-09-10



HEC-RAS Plan: 20250910-Post_Dev_v02 River: River 1 Reach: Reach 1-Upper

| Reach | River Sta | Profile | Q Total (m3/s) | Min Ch El (m) | W.S. Elev (m) | Crit W.S. (m) | E.G. Elev (m) | E.G. Slope (m/m) | Vel Chnl (m/s) | Flow Area (m2) | Top Width (m) | Froude # Chl |
|---------------|-----------|--------------|-------------------|------------------|------------------|------------------|------------------|---------------------|-------------------|-------------------|------------------|--------------|
| Reach 1-Upper | 908 | 2YrCHI3Hr | 0.02 | 94.14 | 94.22 | 94.18 | 94.22 | 0.001632 | 0.16 | 0.12 | 2.47 | 0.22 |
| Reach 1-Upper | 908 | 5YrCHI3Hr | 0.03 | 94.14 | 94.23 | 94.19 | 94.23 | 0.001834 | 0.18 | 0.15 | 2.66 | 0.24 |
| Reach 1-Upper | 908 | 10YrCHI3Hr | 0.03 | 94.14 | 94.24 | 94.19 | 94.24 | 0.001946 | 0.19 | 0.17 | 2.76 | 0.25 |
| Reach 1-Upper | 908 | 25YrCHI3Hr | 0.04 | 94.14 | 94.25 | 94.20 | 94.25 | 0.002058 | 0.21 | 0.18 | 2.87 | 0.26 |
| Reach 1-Upper | 908 | 50YrCHI3Hr | 0.04 | 94.14 | 94.25 | 94.20 | 94.25 | 0.002138 | 0.22 | 0.20 | 2.95 | 0.27 |
| Reach 1-Upper | 908 | 100YrCHI3Hr | 0.05 | 94.14 | 94.26 | 94.20 | 94.26 | 0.002189 | 0.23 | 0.21 | 3.04 | 0.27 |
| Reach 1-Upper | 908 | 2YrSCS24Hr | 0.02 | 94.14 | 94.23 | 94.19 | 94.23 | 0.001752 | 0.17 | 0.14 | 2.59 | 0.23 |
| Reach 1-Upper | 908 | 5YrSCS24Hr | 0.03 | 94.14 | 94.24 | 94.19 | 94.24 | 0.001946 | 0.19 | 0.17 | 2.76 | 0.25 |
| Reach 1-Upper | 908 | 10YrSCS24Hr | 0.04 | 94.14 | 94.24 | 94.20 | 94.25 | 0.002043 | 0.20 | 0.18 | 2.85 | 0.26 |
| Reach 1-Upper | 908 | 25YrSCS24Hr | 0.04 | 94.14 | 94.25 | 94.20 | 94.25 | 0.002153 | 0.22 | 0.20 | 2.97 | 0.27 |
| Reach 1-Upper | 908 | 50YrSCS24Hr | 0.05 | 94.14 | 94.26 | 94.20 | 94.26 | 0.002199 | 0.23 | 0.22 | 3.05 | 0.27 |
| Reach 1-Upper | 908 | 100YrSCS24Hr | 0.06 | 94.14 | 94.26 | 94.21 | 94.26 | 0.002259 | 0.24 | 0.23 | 3.15 | 0.28 |
| Reach 1-Upper | 887 | 2YrCHI3Hr | 0.02 | 94.10 | 94.16 | 94.14 | 94.16 | 0.007210 | 0.24 | 0.08 | 2.48 | 0.44 |
| Reach 1-Upper | 887 | 5YrCHI3Hr | 0.03 | 94.10 | 94.17 | 94.15 | 94.17 | 0.005770 | 0.25 | 0.11 | 2.82 | 0.40 |
| Reach 1-Upper | 887 | 10YrCHI3Hr | 0.03 | 94.10 | 94.18 | 94.15 | 94.18 | 0.005292 | 0.25 | 0.13 | 2.98 | 0.39 |
| Reach 1-Upper | 887 | 25YrCHI3Hr | 0.04 | 94.10 | 94.18 | 94.15 | 94.19 | 0.004885 | 0.26 | 0.15 | 3.16 | 0.38 |
| Reach 1-Upper | 887 | 50YrCHI3Hr | 0.04 | 94.10 | 94.19 | 94.16 | 94.19 | 0.004480 | 0.26 | 0.17 | 3.32 | 0.37 |
| Reach 1-Upper | 887 | 100YrCHI3Hr | 0.05 | 94.10 | 94.19 | 94.16 | 94.20 | 0.004579 | 0.27 | 0.18 | 3.42 | 0.38 |
| Reach 1-Upper | 887 | 2YrSCS24Hr | 0.02 | 94.10 | 94.17 | 94.15 | 94.17 | 0.006295 | 0.25 | 0.10 | 2.71 | 0.42 |
| Reach 1-Upper | 887 | 5YrSCS24Hr | 0.03 | 94.10 | 94.18 | 94.15 | 94.18 | 0.005292 | 0.25 | 0.13 | 2.98 | 0.39 |
| Reach 1-Upper | 887 | 10YrSCS24Hr | 0.04 | 94.10 | 94.18 | 94.15 | 94.19 | 0.004912 | 0.26 | 0.14 | 3.14 | 0.38 |
| Reach 1-Upper | 887 | 25YrSCS24Hr | 0.04 | 94.10 | 94.19 | 94.16 | 94.19 | 0.004434 | 0.26 | 0.17 | 3.35 | 0.37 |
| Reach 1-Upper | 887 | 50YrSCS24Hr | 0.05 | 94.10 | 94.19 | 94.16 | 94.20 | 0.004587 | 0.27 | 0.18 | 3.44 | 0.38 |
| Reach 1-Upper | 887 | 100YrSCS24Hr | 0.06 | 94.10 | 94.20 | 94.16 | 94.20 | 0.004863 | 0.29 | 0.19 | 3.53 | 0.39 |
| Reach 1-Upper | 868 | 2YrCHI3Hr | 0.02 | 93.96 | 94.03 | 94.01 | 94.03 | 0.006094 | 0.26 | 0.07 | 1.89 | 0.41 |
| Reach 1-Upper | 868 | 5YrCHI3Hr | 0.03 | 93.96 | 94.04 | 94.02 | 94.04 | 0.008117 | 0.32 | 0.09 | 1.99 | 0.49 |
| Reach 1-Upper | 868 | 10YrCHI3Hr | 0.03 | 93.96 | 94.04 | 94.02 | 94.04 | 0.009697 | 0.35 | 0.09 | 2.03 | 0.53 |
| Reach 1-Upper | 868 | 25YrCHI3Hr | 0.04 | 93.96 | 94.04 | 94.02 | 94.05 | 0.011359 | 0.39 | 0.10 | 2.08 | 0.58 |
| Reach 1-Upper | 868 | 50YrCHI3Hr | 0.04 | 93.96 | 94.04 | 94.03 | 94.05 | 0.012637 | 0.42 | 0.10 | 2.12 | 0.62 |
| Reach 1-Upper | 868 | 100YrCHI3Hr | 0.05 | 93.96 | 94.05 | 94.03 | 94.06 | 0.013009 | 0.44 | 0.11 | 2.18 | 0.63 |
| Reach 1-Upper | 868 | 2YrSCS24Hr | 0.02 | 93.96 | 94.03 | 94.01 | 94.04 | 0.007224 | 0.29 | 0.08 | 1.96 | 0.46 |
| Reach 1-Upper | 868 | 5YrSCS24Hr | 0.03 | 93.96 | 94.04 | 94.02 | 94.04 | 0.009697 | 0.35 | 0.09 | 2.03 | 0.53 |
| Reach 1-Upper | 868 | 10YrSCS24Hr | 0.04 | 93.96 | 94.04 | 94.02 | 94.05 | 0.011232 | 0.39 | 0.10 | 2.07 | 0.58 |
| Reach 1-Upper | 868 | 25YrSCS24Hr | 0.04 | 93.96 | 94.04 | 94.03 | 94.05 | 0.013016 | 0.43 | 0.10 | 2.13 | 0.63 |
| Reach 1-Upper | 868 | 50YrSCS24Hr | 0.05 | 93.96 | 94.05 | 94.03 | 94.06 | 0.012976 | 0.44 | 0.11 | 2.19 | 0.63 |
| Reach 1-Upper | 868 | 100YrSCS24Hr | 0.06 | 93.96 | 94.05 | 94.04 | 94.06 | 0.011619 | 0.44 | 0.12 | 2.30 | 0.60 |
| Reach 1-Upper | 848 | 2YrCHI3Hr | 0.02 | 93.87 | 93.92 | 93.90 | 93.93 | 0.004549 | 0.20 | 0.09 | 2.73 | 0.35 |
| Reach 1-Upper | 848 | 5YrCHI3Hr | 0.03 | 93.87 | 93.94 | 93.91 | 93.94 | 0.003629 | 0.21 | 0.13 | 3.01 | 0.32 |
| Reach 1-Upper | 848 | 10YrCHI3Hr | 0.03 | 93.87 | 93.94 | 93.91 | 93.95 | 0.002995 | 0.21 | 0.15 | 3.10 | 0.30 |
| Reach 1-Upper | 848 | 25YrCHI3Hr | 0.04 | 93.87 | 93.95 | 93.92 | 93.96 | 0.002536 | 0.21 | 0.18 | 3.19 | 0.28 |
| Reach 1-Upper | 848 | 50YrCHI3Hr | 0.04 | 93.87 | 93.96 | 93.92 | 93.96 | 0.002177 | 0.21 | 0.21 | 3.28 | 0.27 |
| Reach 1-Upper | 848 | 100YrCHI3Hr | 0.05 | 93.87 | 93.97 | 93.92 | 93.97 | 0.002108 | 0.22 | 0.22 | 3.34 | 0.27 |
| Reach 1-Upper | 848 | 2YrSCS24Hr | 0.02 | 93.87 | 93.93 | 93.91 | 93.93 | 0.004188 | 0.21 | 0.11 | 2.93 | 0.34 |
| Reach 1-Upper | 848 | 5YrSCS24Hr | 0.03 | 93.87 | 93.94 | 93.91 | 93.95 | 0.002995 | 0.21 | 0.15 | 3.10 | 0.30 |
| Reach 1-Upper | 848 | 10YrSCS24Hr | 0.04 | 93.87 | 93.95 | 93.92 | 93.95 | 0.002574 | 0.21 | 0.18 | 3.18 | 0.29 |
| Reach 1-Upper | 848 | 25YrSCS24Hr | 0.04 | 93.87 | 93.96 | 93.92 | 93.96 | 0.002104 | 0.21 | 0.21 | 3.30 | 0.26 |
| Reach 1-Upper | 848 | 50YrSCS24Hr | 0.05 | 93.87 | 93.97 | 93.92 | 93.97 | 0.002100 | 0.22 | 0.23 | 3.35 | 0.27 |
| Reach 1-Upper | 848 | 100YrSCS24Hr | 0.06 | 93.87 | 93.97 | 93.92 | 93.97 | 0.002380 | 0.23 | 0.23 | 3.38 | 0.28 |
| Reach 1-Upper | 828 | 2YrCHI3Hr | 0.02 | 93.78 | 93.86 | 93.82 | 93.86 | 0.002644 | 0.17 | 0.11 | 2.77 | 0.27 |
| Reach 1-Upper | 828 | 5YrCHI3Hr | 0.03 | 93.78 | 93.86 | 93.83 | 93.86 | 0.004666 | 0.23 | 0.12 | 2.86 | 0.37 |
| Reach 1-Upper | 828 | 10YrCHI3Hr | 0.03 | 93.78 | 93.86 | 93.83 | 93.86 | 0.007085 | 0.28 | 0.11 | 2.81 | 0.45 |
| Reach 1-Upper | 828 | 25YrCHI3Hr | 0.04 | 93.78 | 93.85 | 93.84 | 93.86 | 0.014294 | 0.39 | 0.10 | 2.58 | 0.63 |
| Reach 1-Upper | 828 | 50YrCHI3Hr | 0.04 | 93.78 | 93.84 | 93.84 | 93.86 | 0.029914 | 0.53 | 0.08 | 2.30 | 0.90 |
| Reach 1-Upper | 828 | 100YrCHI3Hr | 0.05 | 93.78 | 93.84 | 93.84 | 93.86 | 0.034267 | 0.57 | 0.08 | 2.34 | 0.97 |
| Reach 1-Upper | 828 | 2YrSCS24Hr | 0.02 | 93.78 | 93.86 | 93.82 | 93.86 | 0.003210 | 0.19 | 0.12 | 2.95 | 0.30 |
| Reach 1-Upper | 828 | 5YrSCS24Hr | 0.03 | 93.78 | 93.86 | 93.83 | 93.86 | 0.007085 | 0.28 | 0.11 | 2.81 | 0.45 |
| Reach 1-Upper | 828 | 10YrSCS24Hr | 0.04 | 93.78 | 93.85 | 93.84 | 93.86 | 0.012962 | 0.37 | 0.10 | 2.61 | 0.60 |
| Reach 1-Upper | 828 | 25YrSCS24Hr | 0.04 | 93.78 | 93.84 | 93.84 | 93.86 | 0.035615 | 0.57 | 0.08 | 2.22 | 0.98 |
| Reach 1-Upper | 828 | 50YrSCS24Hr | 0.05 | 93.78 | 93.84 | 93.84 | 93.86 | 0.036015 | 0.59 | 0.08 | 2.34 | 0.99 |
| Reach 1-Upper | 828 | 100YrSCS24Hr | 0.06 | 93.78 | 93.86 | 93.85 | 93.87 | 0.020193 | 0.48 | 0.11 | 2.83 | 0.76 |
| Reach 1-Upper | 807 | 2YrCHI3Hr | 0.02 | 93.65 | 93.70 | 93.70 | 93.71 | 0.044163 | 0.52 | 0.04 | 1.46 | 1.04 |
| Reach 1-Upper | 807 | 5YrCHI3Hr | 0.03 | 93.65 | 93.73 | 93.71 | 93.73 | 0.007733 | 0.31 | 0.09 | 2.04 | 0.47 |
| Reach 1-Upper | 807 | 10YrCHI3Hr | 0.03 | 93.65 | 93.75 | 93.71 | 93.75 | 0.003849 | 0.25 | 0.13 | 2.40 | 0.35 |
| Reach 1-Upper | 807 | 25YrCHI3Hr | 0.04 | 93.65 | 93.77 | 93.71 | 93.77 | 0.001862 | 0.20 | 0.19 | 2.86 | 0.25 |
| Reach 1-Upper | 807 | 50YrCHI3Hr | 0.04 | 93.65 | 93.79 | 93.72 | 93.79 | 0.001072 | 0.17 | 0.25 | 3.27 | 0.20 |
| Reach 1-Upper | 807 | 100YrCHI3Hr | 0.05 | 93.65 | 93.81 | 93.72 | 93.81 | 0.000618 | 0.15 | 0.32 | 3.62 | 0.15 |
| Reach 1-Upper | 807 | 2YrSCS24Hr | 0.02 | 93.65 | 93.71 | 93.70 | 93.72 | 0.021814 | 0.43 | 0.06 | 1.70 | 0.76 |
| Reach 1-Upper | 807 | 5YrSCS24Hr | 0.03 | 93.65 | 93.75 | 93.71 | 93.75 | 0.003849 | 0.25 | 0.13 | 2.40 | 0.35 |
| Reach 1-Upper | 807 | 10YrSCS24Hr | 0.04 | 93.65 | 93.77 | 93.71 | 93.77 | 0.002057 | 0.21 | 0.18 | 2.79 | 0.26 |
| Reach 1-Upper | 807 | 25YrSCS24Hr | 0.04 | 93.65 | 93.79 | 93.72 | 93.79 | 0.000946 | 0.17 | 0.26 | 3.34 | 0.18 |
| Reach 1-Upper | 807 | 50YrSCS24Hr | 0.05 | 93.65 | 93.81 | 93.72 | 93.82 | 0.000538 | 0.15 | 0.34 | 3.71 | 0.14 |
| Reach 1-Upper | 807 | 100YrSCS24Hr | 0.06 | 93.65 | 93.84 | 93.73 | 93.85 | 0.000286 | 0.13 | 0.46 | 4.22 | 0.11 |
| Reach 1-Upper | 789 | 2YrCHI3Hr | 0.02 | 93.49 | 93.69 | 93.53 | 93.69 | 0.000037 | 0.05 | 0.38 | 3.33 | 0.04 |
| Reach 1-Upper | 789 | 5YrCHI3Hr | 0.03 | 93.49 | 93.73 | 93.54 | 93.73 | 0.000036 | 0.06 | 0.47 | 3.77 | 0.04 |
| Reach 1-Upper | 789 | 10YrCHI3Hr | 0.03 | 93.49 | 93.74 | 93.55 | 93.74 | 0.000038 | 0.06 | 0.51 | 4.05 | 0.04 |
| Reach 1-Upper | 789 | 25YrCHI3Hr | 0.04 | 93.49 | 93.77 | 93.55 | 93.77 | 0.000038 | 0.07 | 0.56 | 4.42 | 0.04 |
| Reach 1-Upper | 789 | 50YrCHI3Hr | 0.04 | 93.49 | 93.79 | 93.55 | 93.79 | 0.000038 | 0.07 | 0.61 | 4.75 | 0.04 |

HEC-RAS Plan: 20250910-Post_Dev_v02 River: River 1 Reach: Reach 1-Upper (Continued)

| Reach | River Sta | Profile | Q Total (m3/s) | Min Ch El (m) | W.S. Elev (m) | Crit W.S. (m) | E.G. Elev (m) | E.G. Slope (m/m) | Vel Chnl (m/s) | Flow Area (m2) | Top Width (m) | Froude # Chl |
|---------------|-----------|--------------|-------------------|------------------|------------------|------------------|------------------|---------------------|-------------------|-------------------|------------------|--------------|
| Reach 1-Upper | 789 | 100YrCHI3Hr | 0.05 | 93.49 | 93.81 | 93.56 | 93.81 | 0.000036 | 0.07 | 0.66 | 5.08 | 0.04 |
| Reach 1-Upper | 789 | 2YrSCS24Hr | 0.02 | 93.49 | 93.71 | 93.54 | 93.71 | 0.000038 | 0.06 | 0.43 | 3.55 | 0.04 |
| Reach 1-Upper | 789 | 5YrSCS24Hr | 0.03 | 93.49 | 93.74 | 93.55 | 93.74 | 0.000038 | 0.06 | 0.51 | 4.05 | 0.04 |
| Reach 1-Upper | 789 | 10YrSCS24Hr | 0.04 | 93.49 | 93.76 | 93.55 | 93.76 | 0.000038 | 0.07 | 0.56 | 4.37 | 0.04 |
| Reach 1-Upper | 789 | 25YrSCS24Hr | 0.04 | 93.49 | 93.79 | 93.56 | 93.79 | 0.000037 | 0.07 | 0.62 | 4.81 | 0.04 |
| Reach 1-Upper | 789 | 50YrSCS24Hr | 0.05 | 93.49 | 93.81 | 93.56 | 93.81 | 0.000035 | 0.07 | 0.67 | 5.17 | 0.04 |
| Reach 1-Upper | 789 | 100YrSCS24Hr | 0.06 | 93.49 | 93.84 | 93.56 | 93.84 | 0.000032 | 0.07 | 0.75 | 5.59 | 0.04 |
| Reach 1-Upper | 764 | Culvert | | | | | | | | | | |
| Reach 1-Upper | 759 | 2YrCHI3Hr | 0.02 | 93.46 | 93.54 | 93.50 | 93.54 | 0.002883 | 0.23 | 0.08 | 1.83 | 0.30 |
| Reach 1-Upper | 759 | 5YrCHI3Hr | 0.03 | 93.46 | 93.56 | 93.51 | 93.56 | 0.001988 | 0.23 | 0.12 | 2.15 | 0.26 |
| Reach 1-Upper | 759 | 10YrCHI3Hr | 0.03 | 93.46 | 93.58 | 93.51 | 93.58 | 0.001375 | 0.22 | 0.14 | 2.40 | 0.23 |
| Reach 1-Upper | 759 | 25YrCHI3Hr | 0.04 | 93.46 | 93.61 | 93.52 | 93.61 | 0.000864 | 0.21 | 0.18 | 2.73 | 0.19 |
| Reach 1-Upper | 759 | 50YrCHI3Hr | 0.04 | 93.46 | 93.65 | 93.52 | 93.65 | 0.000433 | 0.18 | 0.24 | 3.23 | 0.14 |
| Reach 1-Upper | 759 | 100YrCHI3Hr | 0.05 | 93.46 | 93.68 | 93.53 | 93.68 | 0.000309 | 0.17 | 0.29 | 3.59 | 0.12 |
| Reach 1-Upper | 759 | 2YrSCS24Hr | 0.02 | 93.46 | 93.55 | 93.51 | 93.56 | 0.002355 | 0.23 | 0.10 | 2.03 | 0.28 |
| Reach 1-Upper | 759 | 5YrSCS24Hr | 0.03 | 93.46 | 93.58 | 93.51 | 93.58 | 0.001375 | 0.22 | 0.14 | 2.40 | 0.23 |
| Reach 1-Upper | 759 | 10YrSCS24Hr | 0.04 | 93.46 | 93.60 | 93.52 | 93.60 | 0.000932 | 0.21 | 0.18 | 2.67 | 0.19 |
| Reach 1-Upper | 759 | 25YrSCS24Hr | 0.04 | 93.46 | 93.65 | 93.52 | 93.65 | 0.000408 | 0.17 | 0.25 | 3.29 | 0.14 |
| Reach 1-Upper | 759 | 50YrSCS24Hr | 0.05 | 93.46 | 93.69 | 93.53 | 93.69 | 0.000262 | 0.16 | 0.31 | 3.73 | 0.11 |
| Reach 1-Upper | 759 | 100YrSCS24Hr | 0.06 | 93.46 | 93.73 | 93.53 | 93.73 | 0.000176 | 0.15 | 0.37 | 4.23 | 0.10 |
| Reach 1-Upper | 743 | 2YrCHI3Hr | 0.02 | 93.40 | 93.49 | 93.45 | 93.50 | 0.002754 | 0.25 | 0.08 | 1.55 | 0.30 |
| Reach 1-Upper | 743 | 5YrCHI3Hr | 0.03 | 93.40 | 93.54 | 93.46 | 93.54 | 0.001046 | 0.20 | 0.13 | 2.00 | 0.20 |
| Reach 1-Upper | 743 | 10YrCHI3Hr | 0.03 | 93.40 | 93.57 | 93.47 | 93.57 | 0.000686 | 0.19 | 0.17 | 2.25 | 0.17 |
| Reach 1-Upper | 743 | 25YrCHI3Hr | 0.04 | 93.40 | 93.60 | 93.47 | 93.60 | 0.000466 | 0.18 | 0.21 | 2.59 | 0.14 |
| Reach 1-Upper | 743 | 50YrCHI3Hr | 0.04 | 93.40 | 93.64 | 93.48 | 93.64 | 0.000265 | 0.16 | 0.27 | 3.11 | 0.11 |
| Reach 1-Upper | 743 | 100YrCHI3Hr | 0.05 | 93.40 | 93.67 | 93.48 | 93.67 | 0.000207 | 0.16 | 0.31 | 3.83 | 0.10 |
| Reach 1-Upper | 743 | 2YrSCS24Hr | 0.02 | 93.40 | 93.52 | 93.46 | 93.52 | 0.001463 | 0.21 | 0.11 | 1.84 | 0.23 |
| Reach 1-Upper | 743 | 5YrSCS24Hr | 0.03 | 93.40 | 93.57 | 93.47 | 93.57 | 0.000686 | 0.19 | 0.17 | 2.25 | 0.17 |
| Reach 1-Upper | 743 | 10YrSCS24Hr | 0.04 | 93.40 | 93.59 | 93.47 | 93.59 | 0.000495 | 0.18 | 0.20 | 2.53 | 0.15 |
| Reach 1-Upper | 743 | 25YrSCS24Hr | 0.04 | 93.40 | 93.65 | 93.48 | 93.65 | 0.000254 | 0.16 | 0.27 | 3.18 | 0.11 |
| Reach 1-Upper | 743 | 50YrSCS24Hr | 0.05 | 93.40 | 93.68 | 93.48 | 93.69 | 0.000181 | 0.15 | 0.32 | 4.15 | 0.10 |
| Reach 1-Upper | 743 | 100YrSCS24Hr | 0.06 | 93.40 | 93.73 | 93.49 | 93.73 | 0.000134 | 0.14 | 0.38 | 4.85 | 0.09 |
| Reach 1-Upper | 733 | Culvert | | | | | | | | | | |
| Reach 1-Upper | 728 | 2YrCHI3Hr | 0.02 | 93.33 | 93.48 | 93.39 | 93.48 | 0.000387 | 0.13 | 0.15 | 1.68 | 0.12 |
| Reach 1-Upper | 728 | 5YrCHI3Hr | 0.03 | 93.33 | 93.52 | 93.40 | 93.52 | 0.000273 | 0.13 | 0.21 | 1.98 | 0.11 |
| Reach 1-Upper | 728 | 10YrCHI3Hr | 0.03 | 93.33 | 93.55 | 93.40 | 93.55 | 0.000233 | 0.13 | 0.24 | 2.16 | 0.10 |
| Reach 1-Upper | 728 | 25YrCHI3Hr | 0.04 | 93.33 | 93.58 | 93.41 | 93.58 | 0.000196 | 0.14 | 0.28 | 2.37 | 0.10 |
| Reach 1-Upper | 728 | 50YrCHI3Hr | 0.04 | 93.33 | 93.62 | 93.41 | 93.62 | 0.000131 | 0.13 | 0.34 | 2.70 | 0.08 |
| Reach 1-Upper | 728 | 100YrCHI3Hr | 0.05 | 93.33 | 93.64 | 93.42 | 93.64 | 0.000117 | 0.13 | 0.38 | 2.90 | 0.08 |
| Reach 1-Upper | 728 | 2YrSCS24Hr | 0.02 | 93.33 | 93.51 | 93.39 | 93.51 | 0.000306 | 0.13 | 0.19 | 1.87 | 0.11 |
| Reach 1-Upper | 728 | 5YrSCS24Hr | 0.03 | 93.33 | 93.55 | 93.40 | 93.55 | 0.000233 | 0.13 | 0.24 | 2.16 | 0.10 |
| Reach 1-Upper | 728 | 10YrSCS24Hr | 0.04 | 93.33 | 93.57 | 93.41 | 93.57 | 0.000202 | 0.14 | 0.27 | 2.34 | 0.10 |
| Reach 1-Upper | 728 | 25YrSCS24Hr | 0.04 | 93.33 | 93.62 | 93.41 | 93.62 | 0.000128 | 0.13 | 0.35 | 2.74 | 0.08 |
| Reach 1-Upper | 728 | 50YrSCS24Hr | 0.05 | 93.33 | 93.66 | 93.42 | 93.66 | 0.000106 | 0.12 | 0.39 | 2.98 | 0.08 |
| Reach 1-Upper | 728 | 100YrSCS24Hr | 0.06 | 93.33 | 93.69 | 93.42 | 93.69 | 0.000091 | 0.12 | 0.44 | 3.24 | 0.07 |
| Reach 1-Upper | 715 | 2YrCHI3Hr | 0.02 | 93.32 | 93.48 | 93.36 | 93.48 | 0.000151 | 0.10 | 0.20 | 2.44 | 0.08 |
| Reach 1-Upper | 715 | 5YrCHI3Hr | 0.03 | 93.32 | 93.52 | 93.37 | 93.52 | 0.000132 | 0.11 | 0.26 | 2.85 | 0.08 |
| Reach 1-Upper | 715 | 10YrCHI3Hr | 0.03 | 93.32 | 93.54 | 93.37 | 93.54 | 0.000123 | 0.11 | 0.29 | 3.09 | 0.08 |
| Reach 1-Upper | 715 | 25YrCHI3Hr | 0.04 | 93.32 | 93.57 | 93.38 | 93.57 | 0.000112 | 0.11 | 0.33 | 3.38 | 0.08 |
| Reach 1-Upper | 715 | 50YrCHI3Hr | 0.04 | 93.32 | 93.62 | 93.38 | 93.62 | 0.000081 | 0.11 | 0.39 | 3.82 | 0.07 |
| Reach 1-Upper | 715 | 100YrCHI3Hr | 0.05 | 93.32 | 93.64 | 93.39 | 93.64 | 0.000075 | 0.11 | 0.43 | 4.07 | 0.06 |
| Reach 1-Upper | 715 | 2YrSCS24Hr | 0.02 | 93.32 | 93.51 | 93.36 | 93.51 | 0.000138 | 0.10 | 0.24 | 2.70 | 0.08 |
| Reach 1-Upper | 715 | 5YrSCS24Hr | 0.03 | 93.32 | 93.54 | 93.37 | 93.54 | 0.000123 | 0.11 | 0.29 | 3.09 | 0.08 |
| Reach 1-Upper | 715 | 10YrSCS24Hr | 0.04 | 93.32 | 93.57 | 93.38 | 93.57 | 0.000114 | 0.11 | 0.32 | 3.33 | 0.08 |
| Reach 1-Upper | 715 | 25YrSCS24Hr | 0.04 | 93.32 | 93.62 | 93.39 | 93.62 | 0.000080 | 0.11 | 0.40 | 3.86 | 0.07 |
| Reach 1-Upper | 715 | 50YrSCS24Hr | 0.05 | 93.32 | 93.65 | 93.39 | 93.65 | 0.000070 | 0.11 | 0.44 | 4.19 | 0.06 |
| Reach 1-Upper | 715 | 100YrSCS24Hr | 0.06 | 93.32 | 93.69 | 93.39 | 93.69 | 0.000062 | 0.11 | 0.49 | 4.53 | 0.06 |
| Reach 1-Upper | 705 | Culvert | | | | | | | | | | |
| Reach 1-Upper | 698 | 2YrCHI3Hr | 0.02 | 93.24 | 93.31 | 93.29 | 93.32 | 0.010647 | 0.37 | 0.05 | 1.15 | 0.56 |
| Reach 1-Upper | 698 | 5YrCHI3Hr | 0.03 | 93.24 | 93.31 | 93.30 | 93.33 | 0.018452 | 0.50 | 0.05 | 1.17 | 0.74 |
| Reach 1-Upper | 698 | 10YrCHI3Hr | 0.03 | 93.24 | 93.31 | 93.31 | 93.33 | 0.030771 | 0.62 | 0.05 | 1.15 | 0.95 |
| Reach 1-Upper | 698 | 25YrCHI3Hr | 0.04 | 93.24 | 93.38 | 93.31 | 93.38 | 0.002195 | 0.26 | 0.15 | 1.67 | 0.28 |
| Reach 1-Upper | 698 | 50YrCHI3Hr | 0.04 | 93.24 | 93.51 | 93.32 | 93.51 | 0.000131 | 0.11 | 0.41 | 2.59 | 0.08 |
| Reach 1-Upper | 698 | 100YrCHI3Hr | 0.05 | 93.24 | 93.51 | 93.32 | 93.51 | 0.000158 | 0.12 | 0.41 | 2.60 | 0.09 |
| Reach 1-Upper | 698 | 2YrSCS24Hr | 0.02 | 93.24 | 93.31 | 93.30 | 93.32 | 0.016098 | 0.46 | 0.05 | 1.16 | 0.69 |
| Reach 1-Upper | 698 | 5YrSCS24Hr | 0.03 | 93.24 | 93.31 | 93.31 | 93.33 | 0.033358 | 0.64 | 0.05 | 1.14 | 0.98 |
| Reach 1-Upper | 698 | 10YrSCS24Hr | 0.04 | 93.24 | 93.41 | 93.31 | 93.41 | 0.000855 | 0.18 | 0.20 | 1.88 | 0.18 |
| Reach 1-Upper | 698 | 25YrSCS24Hr | 0.04 | 93.24 | 93.51 | 93.32 | 93.51 | 0.000135 | 0.11 | 0.41 | 2.59 | 0.08 |
| Reach 1-Upper | 698 | 50YrSCS24Hr | 0.05 | 93.24 | 93.51 | 93.32 | 93.51 | 0.000162 | 0.12 | 0.41 | 2.61 | 0.09 |
| Reach 1-Upper | 698 | 100YrSCS24Hr | 0.06 | 93.24 | 93.51 | 93.33 | 93.52 | 0.000196 | 0.13 | 0.42 | 2.63 | 0.10 |
| Reach 1-Upper | 681 | 2YrCHI3Hr | 0.02 | 93.14 | 93.22 | 93.19 | 93.22 | 0.003726 | 0.23 | 0.08 | 1.65 | 0.34 |
| Reach 1-Upper | 681 | 5YrCHI3Hr | 0.03 | 93.14 | 93.24 | 93.20 | 93.25 | 0.001985 | 0.21 | 0.13 | 1.84 | 0.26 |
| Reach 1-Upper | 681 | 10YrCHI3Hr | 0.03 | 93.14 | 93.27 | 93.20 | 93.27 | 0.001166 | 0.19 | 0.17 | 2.00 | 0.21 |
| Reach 1-Upper | 681 | 25YrCHI3Hr | 0.04 | 93.14 | 93.37 | 93.20 | 93.37 | 0.000122 | 0.09 | 0.42 | 2.74 | 0.07 |

HEC-RAS Plan: 20250910-Post_Dev_v02 River: River 1 Reach: Reach 1-Upper (Continued)

| Reach | River Sta | Profile | Q Total (m3/s) | Min Ch El (m) | W.S. Elev (m) | Crit W.S. (m) | E.G. Elev (m) | E.G. Slope (m/m) | Vel Chnl (m/s) | Flow Area (m2) | Top Width (m) | Froude # Chl |
|---------------|-----------|--------------|-------------------|------------------|------------------|------------------|------------------|---------------------|-------------------|-------------------|------------------|--------------|
| Reach 1-Upper | 681 | 50YrCHI3Hr | 0.04 | 93.14 | 93.51 | 93.21 | 93.51 | 0.000021 | 0.05 | 0.87 | 4.05 | 0.03 |
| Reach 1-Upper | 681 | 100YrCHI3Hr | 0.05 | 93.14 | 93.51 | 93.21 | 93.51 | 0.000026 | 0.06 | 0.88 | 4.08 | 0.04 |
| Reach 1-Upper | 681 | 2YrSCS24Hr | 0.02 | 93.14 | 93.24 | 93.19 | 93.24 | 0.002292 | 0.21 | 0.11 | 1.78 | 0.27 |
| Reach 1-Upper | 681 | 5YrSCS24Hr | 0.03 | 93.14 | 93.28 | 93.20 | 93.28 | 0.000837 | 0.17 | 0.19 | 2.07 | 0.18 |
| Reach 1-Upper | 681 | 10YrSCS24Hr | 0.04 | 93.14 | 93.41 | 93.20 | 93.41 | 0.000067 | 0.07 | 0.52 | 2.97 | 0.05 |
| Reach 1-Upper | 681 | 25YrSCS24Hr | 0.04 | 93.14 | 93.51 | 93.21 | 93.51 | 0.000022 | 0.05 | 0.87 | 4.07 | 0.03 |
| Reach 1-Upper | 681 | 50YrSCS24Hr | 0.05 | 93.14 | 93.51 | 93.21 | 93.51 | 0.000027 | 0.06 | 0.88 | 4.09 | 0.04 |
| Reach 1-Upper | 681 | 100YrSCS24Hr | 0.06 | 93.14 | 93.51 | 93.22 | 93.51 | 0.000033 | 0.06 | 0.89 | 4.13 | 0.04 |
| Reach 1-Upper | 663 | 2YrCHI3Hr | 0.02 | 93.05 | 93.19 | | 93.19 | 0.000887 | 0.16 | 0.12 | 1.35 | 0.18 |
| Reach 1-Upper | 663 | 5YrCHI3Hr | 0.03 | 93.05 | 93.22 | | 93.23 | 0.000652 | 0.16 | 0.17 | 1.60 | 0.16 |
| Reach 1-Upper | 663 | 10YrCHI3Hr | 0.03 | 93.05 | 93.25 | | 93.25 | 0.000460 | 0.15 | 0.22 | 1.80 | 0.13 |
| Reach 1-Upper | 663 | 25YrCHI3Hr | 0.04 | 93.05 | 93.37 | | 93.37 | 0.000079 | 0.08 | 0.48 | 2.67 | 0.06 |
| Reach 1-Upper | 663 | 50YrCHI3Hr | 0.04 | 93.05 | 93.51 | | 93.51 | 0.000018 | 0.05 | 0.96 | 4.41 | 0.03 |
| Reach 1-Upper | 663 | 100YrCHI3Hr | 0.05 | 93.05 | 93.51 | | 93.51 | 0.000022 | 0.05 | 0.96 | 4.44 | 0.03 |
| Reach 1-Upper | 663 | 2YrSCS24Hr | 0.02 | 93.05 | 93.22 | | 93.22 | 0.000662 | 0.16 | 0.15 | 1.54 | 0.16 |
| Reach 1-Upper | 663 | 5YrSCS24Hr | 0.03 | 93.05 | 93.27 | | 93.27 | 0.000342 | 0.13 | 0.24 | 1.90 | 0.12 |
| Reach 1-Upper | 663 | 10YrSCS24Hr | 0.04 | 93.05 | 93.40 | | 93.40 | 0.000049 | 0.06 | 0.57 | 3.04 | 0.05 |
| Reach 1-Upper | 663 | 25YrSCS24Hr | 0.04 | 93.05 | 93.51 | | 93.51 | 0.000019 | 0.05 | 0.96 | 4.42 | 0.03 |
| Reach 1-Upper | 663 | 50YrSCS24Hr | 0.05 | 93.05 | 93.51 | | 93.51 | 0.000023 | 0.05 | 0.97 | 4.46 | 0.03 |
| Reach 1-Upper | 663 | 100YrSCS24Hr | 0.06 | 93.05 | 93.51 | | 93.51 | 0.000028 | 0.06 | 0.98 | 4.50 | 0.04 |
| Reach 1-Upper | 656 | 2YrCHI3Hr | 0.06 | 93.03 | 93.15 | 93.12 | 93.16 | 0.007897 | 0.46 | 0.13 | 1.69 | 0.53 |
| Reach 1-Upper | 656 | 5YrCHI3Hr | 0.10 | 93.03 | 93.19 | 93.14 | 93.20 | 0.006746 | 0.51 | 0.20 | 1.91 | 0.51 |
| Reach 1-Upper | 656 | 10YrCHI3Hr | 0.13 | 93.03 | 93.23 | 93.16 | 93.24 | 0.004563 | 0.48 | 0.27 | 2.12 | 0.43 |
| Reach 1-Upper | 656 | 25YrCHI3Hr | 0.17 | 93.03 | 93.36 | 93.18 | 93.37 | 0.000762 | 0.28 | 0.62 | 2.87 | 0.19 |
| Reach 1-Upper | 656 | 50YrCHI3Hr | 0.20 | 93.03 | 93.51 | 93.19 | 93.51 | 0.000191 | 0.19 | 1.16 | 4.64 | 0.10 |
| Reach 1-Upper | 656 | 100YrCHI3Hr | 0.24 | 93.03 | 93.51 | 93.20 | 93.51 | 0.000260 | 0.22 | 1.17 | 4.65 | 0.12 |
| Reach 1-Upper | 656 | 2YrSCS24Hr | 0.09 | 93.03 | 93.18 | 93.14 | 93.19 | 0.007161 | 0.50 | 0.18 | 1.86 | 0.52 |
| Reach 1-Upper | 656 | 5YrSCS24Hr | 0.14 | 93.03 | 93.24 | 93.17 | 93.25 | 0.003570 | 0.45 | 0.31 | 2.22 | 0.39 |
| Reach 1-Upper | 656 | 10YrSCS24Hr | 0.18 | 93.03 | 93.40 | 93.18 | 93.40 | 0.000513 | 0.24 | 0.73 | 3.49 | 0.16 |
| Reach 1-Upper | 656 | 25YrSCS24Hr | 0.22 | 93.03 | 93.51 | 93.20 | 93.51 | 0.000228 | 0.21 | 1.16 | 4.65 | 0.11 |
| Reach 1-Upper | 656 | 50YrSCS24Hr | 0.26 | 93.03 | 93.51 | 93.21 | 93.51 | 0.000307 | 0.24 | 1.17 | 4.66 | 0.13 |
| Reach 1-Upper | 656 | 100YrSCS24Hr | 0.30 | 93.03 | 93.51 | 93.22 | 93.51 | 0.000401 | 0.28 | 1.17 | 4.67 | 0.15 |
| Reach 1-Upper | 638 | 2YrCHI3Hr | 0.06 | 92.92 | 93.08 | 93.01 | 93.08 | 0.002811 | 0.33 | 0.19 | 1.85 | 0.33 |
| Reach 1-Upper | 638 | 5YrCHI3Hr | 0.10 | 92.92 | 93.14 | 93.04 | 93.14 | 0.001935 | 0.33 | 0.31 | 2.24 | 0.28 |
| Reach 1-Upper | 638 | 10YrCHI3Hr | 0.13 | 92.92 | 93.19 | 93.05 | 93.20 | 0.001151 | 0.29 | 0.45 | 2.68 | 0.23 |
| Reach 1-Upper | 638 | 25YrCHI3Hr | 0.17 | 92.92 | 93.36 | 93.07 | 93.36 | 0.000204 | 0.17 | 1.05 | 4.59 | 0.10 |
| Reach 1-Upper | 638 | 50YrCHI3Hr | 0.20 | 92.92 | 93.50 | 93.08 | 93.50 | 0.000071 | 0.13 | 1.86 | 6.83 | 0.06 |
| Reach 1-Upper | 638 | 100YrCHI3Hr | 0.24 | 92.92 | 93.50 | 93.10 | 93.51 | 0.000098 | 0.15 | 1.86 | 6.83 | 0.08 |
| Reach 1-Upper | 638 | 2YrSCS24Hr | 0.09 | 92.92 | 93.12 | 93.03 | 93.12 | 0.002263 | 0.34 | 0.27 | 2.12 | 0.30 |
| Reach 1-Upper | 638 | 5YrSCS24Hr | 0.14 | 92.92 | 93.22 | 93.06 | 93.22 | 0.000920 | 0.27 | 0.52 | 2.92 | 0.20 |
| Reach 1-Upper | 638 | 10YrSCS24Hr | 0.18 | 92.92 | 93.40 | 93.07 | 93.40 | 0.000146 | 0.16 | 1.22 | 5.04 | 0.09 |
| Reach 1-Upper | 638 | 25YrSCS24Hr | 0.22 | 92.92 | 93.50 | 93.09 | 93.51 | 0.000085 | 0.14 | 1.86 | 6.83 | 0.07 |
| Reach 1-Upper | 638 | 50YrSCS24Hr | 0.26 | 92.92 | 93.50 | 93.10 | 93.51 | 0.000115 | 0.16 | 1.86 | 6.84 | 0.08 |
| Reach 1-Upper | 638 | 100YrSCS24Hr | 0.30 | 92.92 | 93.50 | 93.12 | 93.51 | 0.000152 | 0.18 | 1.87 | 6.84 | 0.09 |
| Reach 1-Upper | 617 | 2YrCHI3Hr | 0.06 | 92.84 | 93.02 | 92.95 | 93.02 | 0.002976 | 0.32 | 0.19 | 2.05 | 0.33 |
| Reach 1-Upper | 617 | 5YrCHI3Hr | 0.10 | 92.84 | 93.11 | 92.98 | 93.11 | 0.000952 | 0.24 | 0.43 | 2.97 | 0.20 |
| Reach 1-Upper | 617 | 10YrCHI3Hr | 0.13 | 92.84 | 93.18 | 92.99 | 93.18 | 0.000487 | 0.20 | 0.66 | 3.68 | 0.15 |
| Reach 1-Upper | 617 | 25YrCHI3Hr | 0.17 | 92.84 | 93.36 | 93.01 | 93.36 | 0.000104 | 0.11 | 1.56 | 6.63 | 0.07 |
| Reach 1-Upper | 617 | 50YrCHI3Hr | 0.20 | 92.84 | 93.50 | 93.02 | 93.50 | 0.000032 | 0.07 | 2.93 | 15.16 | 0.04 |
| Reach 1-Upper | 617 | 100YrCHI3Hr | 0.24 | 92.84 | 93.50 | 93.04 | 93.50 | 0.000044 | 0.09 | 2.93 | 15.17 | 0.05 |
| Reach 1-Upper | 617 | 2YrSCS24Hr | 0.09 | 92.84 | 93.08 | 92.97 | 93.09 | 0.001249 | 0.26 | 0.35 | 2.72 | 0.23 |
| Reach 1-Upper | 617 | 5YrSCS24Hr | 0.14 | 92.84 | 93.21 | 93.00 | 93.21 | 0.000388 | 0.18 | 0.77 | 4.08 | 0.13 |
| Reach 1-Upper | 617 | 10YrSCS24Hr | 0.18 | 92.84 | 93.39 | 93.01 | 93.39 | 0.000078 | 0.10 | 1.82 | 7.56 | 0.06 |
| Reach 1-Upper | 617 | 25YrSCS24Hr | 0.22 | 92.84 | 93.50 | 93.03 | 93.50 | 0.000038 | 0.08 | 2.93 | 15.17 | 0.05 |
| Reach 1-Upper | 617 | 50YrSCS24Hr | 0.26 | 92.84 | 93.50 | 93.04 | 93.50 | 0.000052 | 0.09 | 2.93 | 15.17 | 0.05 |
| Reach 1-Upper | 617 | 100YrSCS24Hr | 0.30 | 92.84 | 93.50 | 93.06 | 93.50 | 0.000069 | 0.11 | 2.93 | 15.18 | 0.06 |
| Reach 1-Upper | 598 | 2YrCHI3Hr | 0.06 | 92.76 | 93.00 | 92.86 | 93.00 | 0.000514 | 0.18 | 0.36 | 2.60 | 0.15 |
| Reach 1-Upper | 598 | 5YrCHI3Hr | 0.11 | 92.76 | 93.10 | 92.89 | 93.10 | 0.000269 | 0.18 | 0.61 | 3.40 | 0.12 |
| Reach 1-Upper | 598 | 10YrCHI3Hr | 0.14 | 92.76 | 93.18 | 92.91 | 93.18 | 0.000184 | 0.18 | 0.80 | 5.26 | 0.10 |
| Reach 1-Upper | 598 | 25YrCHI3Hr | 0.19 | 92.76 | 93.36 | 92.92 | 93.36 | 0.000070 | 0.15 | 1.25 | 8.76 | 0.07 |
| Reach 1-Upper | 598 | 50YrCHI3Hr | 0.22 | 92.76 | 93.50 | 92.94 | 93.50 | 0.000018 | 0.07 | 4.94 | 31.21 | 0.03 |
| Reach 1-Upper | 598 | 100YrCHI3Hr | 0.26 | 92.76 | 93.50 | 92.95 | 93.50 | 0.000024 | 0.09 | 4.94 | 31.21 | 0.04 |
| Reach 1-Upper | 598 | 2YrSCS24Hr | 0.10 | 92.76 | 93.07 | 92.88 | 93.08 | 0.000317 | 0.18 | 0.54 | 3.19 | 0.12 |
| Reach 1-Upper | 598 | 5YrSCS24Hr | 0.15 | 92.76 | 93.20 | 92.91 | 93.21 | 0.000160 | 0.17 | 0.87 | 5.82 | 0.10 |
| Reach 1-Upper | 598 | 10YrSCS24Hr | 0.19 | 92.76 | 93.39 | 92.93 | 93.39 | 0.000059 | 0.14 | 1.34 | 9.49 | 0.06 |
| Reach 1-Upper | 598 | 25YrSCS24Hr | 0.24 | 92.76 | 93.50 | 92.94 | 93.50 | 0.000021 | 0.08 | 4.94 | 31.21 | 0.04 |
| Reach 1-Upper | 598 | 50YrSCS24Hr | 0.28 | 92.76 | 93.50 | 92.96 | 93.50 | 0.000029 | 0.09 | 4.93 | 31.21 | 0.04 |
| Reach 1-Upper | 598 | 100YrSCS24Hr | 0.33 | 92.76 | 93.50 | 92.97 | 93.50 | 0.000039 | 0.11 | 4.93 | 31.21 | 0.05 |
| Reach 1-Upper | 589 | | Culvert | | | | | | | | | |
| Reach 1-Upper | 581 | 2YrCHI3Hr | 0.06 | 92.71 | 92.89 | 92.81 | 92.89 | 0.002034 | 0.27 | 0.24 | 2.66 | 0.28 |
| Reach 1-Upper | 581 | 5YrCHI3Hr | 0.11 | 92.71 | 92.93 | 92.84 | 92.93 | 0.001970 | 0.33 | 0.33 | 3.40 | 0.29 |
| Reach 1-Upper | 581 | 10YrCHI3Hr | 0.14 | 92.71 | 92.96 | 92.86 | 92.97 | 0.001627 | 0.34 | 0.41 | 4.01 | 0.27 |
| Reach 1-Upper | 581 | 25YrCHI3Hr | 0.19 | 92.71 | 93.02 | 92.88 | 93.03 | 0.000990 | 0.33 | 0.56 | 5.14 | 0.22 |
| Reach 1-Upper | 581 | 50YrCHI3Hr | 0.22 | 92.71 | 93.13 | 92.89 | 93.13 | 0.000386 | 0.27 | 0.83 | 7.07 | 0.15 |
| Reach 1-Upper | 581 | 100YrCHI3Hr | 0.26 | 92.71 | 93.25 | 92.90 | 93.25 | 0.000184 | 0.23 | 1.13 | 30.32 | 0.11 |
| Reach 1-Upper | 581 | 2YrSCS24Hr | 0.10 | 92.71 | 92.92 | 92.84 | 92.92 | 0.002055 | 0.32 | 0.31 | 3.20 | 0.29 |

HEC-RAS Plan: 20250910-Post_Dev_v02 River: River 1 Reach: Reach 1-Upper (Continued)

| Reach | River Sta | Profile | Q Total (m3/s) | Min Ch El (m) | W.S. Elev (m) | Crit W.S. (m) | E.G. Elev (m) | E.G. Slope (m/m) | Vel Chnl (m/s) | Flow Area (m2) | Top Width (m) | Froude # Chl |
|---------------|-----------|--------------|-------------------|------------------|------------------|------------------|------------------|---------------------|-------------------|-------------------|------------------|--------------|
| Reach 1-Upper | 581 | 5YrSCS24Hr | 0.15 | 92.71 | 92.97 | 92.86 | 92.98 | 0.001468 | 0.34 | 0.44 | 4.26 | 0.26 |
| Reach 1-Upper | 581 | 10YrSCS24Hr | 0.19 | 92.71 | 93.03 | 92.88 | 93.04 | 0.000901 | 0.32 | 0.59 | 5.33 | 0.21 |
| Reach 1-Upper | 581 | 25YrSCS24Hr | 0.24 | 92.71 | 93.24 | 92.89 | 93.24 | 0.000175 | 0.22 | 1.11 | 29.51 | 0.10 |
| Reach 1-Upper | 581 | 50YrSCS24Hr | 0.28 | 92.71 | 93.25 | 92.90 | 93.25 | 0.000220 | 0.25 | 1.13 | 30.33 | 0.12 |
| Reach 1-Upper | 581 | 100YrSCS24Hr | 0.33 | 92.71 | 93.25 | 92.91 | 93.25 | 0.000294 | 0.29 | 1.13 | 30.33 | 0.14 |
| Reach 1-Upper | 572 | 2YrCHI3Hr | 0.06 | 92.73 | 92.85 | 92.82 | 92.86 | 0.008674 | 0.45 | 0.14 | 2.02 | 0.54 |
| Reach 1-Upper | 572 | 5YrCHI3Hr | 0.11 | 92.73 | 92.90 | 92.84 | 92.90 | 0.004896 | 0.43 | 0.26 | 2.58 | 0.43 |
| Reach 1-Upper | 572 | 10YrCHI3Hr | 0.14 | 92.73 | 92.94 | 92.86 | 92.94 | 0.002847 | 0.38 | 0.38 | 3.03 | 0.34 |
| Reach 1-Upper | 572 | 25YrCHI3Hr | 0.19 | 92.73 | 93.01 | 92.87 | 93.01 | 0.001251 | 0.30 | 0.62 | 3.87 | 0.24 |
| Reach 1-Upper | 572 | 50YrCHI3Hr | 0.22 | 92.73 | 93.12 | 92.88 | 93.12 | 0.000367 | 0.19 | 1.14 | 5.93 | 0.13 |
| Reach 1-Upper | 572 | 100YrCHI3Hr | 0.26 | 92.73 | 93.25 | 92.90 | 93.25 | 0.000064 | 0.10 | 4.09 | 35.88 | 0.06 |
| Reach 1-Upper | 572 | 2YrSCS24Hr | 0.10 | 92.73 | 92.88 | 92.84 | 92.89 | 0.005817 | 0.44 | 0.22 | 2.44 | 0.46 |
| Reach 1-Upper | 572 | 5YrSCS24Hr | 0.15 | 92.73 | 92.95 | 92.86 | 92.96 | 0.002326 | 0.36 | 0.43 | 3.23 | 0.31 |
| Reach 1-Upper | 572 | 10YrSCS24Hr | 0.19 | 92.73 | 93.02 | 92.88 | 93.03 | 0.001095 | 0.28 | 0.67 | 4.01 | 0.22 |
| Reach 1-Upper | 572 | 25YrSCS24Hr | 0.24 | 92.73 | 93.24 | 92.89 | 93.24 | 0.000067 | 0.10 | 3.72 | 33.49 | 0.06 |
| Reach 1-Upper | 572 | 50YrSCS24Hr | 0.28 | 92.73 | 93.25 | 92.90 | 93.25 | 0.000076 | 0.11 | 4.10 | 35.90 | 0.06 |
| Reach 1-Upper | 572 | 100YrSCS24Hr | 0.33 | 92.73 | 93.25 | 92.92 | 93.25 | 0.000102 | 0.13 | 4.10 | 35.94 | 0.07 |
| Reach 1-Upper | 555 | 2YrCHI3Hr | 0.06 | 92.61 | 92.81 | 92.71 | 92.81 | 0.000982 | 0.20 | 0.32 | 2.99 | 0.20 |
| Reach 1-Upper | 555 | 5YrCHI3Hr | 0.11 | 92.61 | 92.87 | 92.74 | 92.87 | 0.000748 | 0.21 | 0.52 | 3.73 | 0.18 |
| Reach 1-Upper | 555 | 10YrCHI3Hr | 0.14 | 92.61 | 92.92 | 92.75 | 92.92 | 0.000505 | 0.19 | 0.73 | 4.38 | 0.15 |
| Reach 1-Upper | 555 | 25YrCHI3Hr | 0.19 | 92.61 | 93.00 | 92.77 | 93.00 | 0.000277 | 0.17 | 1.12 | 5.37 | 0.12 |
| Reach 1-Upper | 555 | 50YrCHI3Hr | 0.22 | 92.61 | 93.12 | 92.78 | 93.12 | 0.000080 | 0.11 | 2.69 | 31.73 | 0.07 |
| Reach 1-Upper | 555 | 100YrCHI3Hr | 0.26 | 92.61 | 93.25 | 92.79 | 93.25 | 0.000015 | 0.06 | 7.39 | 40.94 | 0.03 |
| Reach 1-Upper | 555 | 2YrSCS24Hr | 0.10 | 92.61 | 92.85 | 92.73 | 92.86 | 0.000843 | 0.21 | 0.46 | 3.51 | 0.19 |
| Reach 1-Upper | 555 | 5YrSCS24Hr | 0.15 | 92.61 | 92.94 | 92.76 | 92.94 | 0.000435 | 0.19 | 0.82 | 4.62 | 0.14 |
| Reach 1-Upper | 555 | 10YrSCS24Hr | 0.19 | 92.61 | 93.02 | 92.77 | 93.02 | 0.000251 | 0.16 | 1.19 | 5.53 | 0.11 |
| Reach 1-Upper | 555 | 25YrSCS24Hr | 0.24 | 92.61 | 93.24 | 92.79 | 93.24 | 0.000016 | 0.06 | 6.96 | 40.67 | 0.03 |
| Reach 1-Upper | 555 | 50YrSCS24Hr | 0.28 | 92.61 | 93.25 | 92.80 | 93.25 | 0.000018 | 0.07 | 7.39 | 40.94 | 0.03 |
| Reach 1-Upper | 555 | 100YrSCS24Hr | 0.33 | 92.61 | 93.25 | 92.81 | 93.25 | 0.000025 | 0.08 | 7.39 | 40.94 | 0.04 |
| Reach 1-Upper | 534 | 2YrCHI3Hr | 0.06 | 92.59 | 92.79 | 92.69 | 92.79 | 0.001542 | 0.25 | 0.26 | 2.47 | 0.24 |
| Reach 1-Upper | 534 | 5YrCHI3Hr | 0.11 | 92.59 | 92.85 | 92.72 | 92.86 | 0.001007 | 0.24 | 0.46 | 3.30 | 0.21 |
| Reach 1-Upper | 534 | 10YrCHI3Hr | 0.14 | 92.59 | 92.91 | 92.74 | 92.91 | 0.000612 | 0.21 | 0.68 | 6.64 | 0.17 |
| Reach 1-Upper | 534 | 25YrCHI3Hr | 0.19 | 92.59 | 93.00 | 92.76 | 93.00 | 0.000148 | 0.12 | 2.58 | 34.75 | 0.09 |
| Reach 1-Upper | 534 | 50YrCHI3Hr | 0.22 | 92.59 | 93.12 | 92.77 | 93.12 | 0.000015 | 0.05 | 8.09 | 50.92 | 0.03 |
| Reach 1-Upper | 534 | 100YrCHI3Hr | 0.26 | 92.59 | 93.25 | 92.78 | 93.25 | 0.000003 | 0.03 | 14.61 | 51.39 | 0.01 |
| Reach 1-Upper | 534 | 2YrSCS24Hr | 0.10 | 92.59 | 92.83 | 92.71 | 92.84 | 0.001197 | 0.25 | 0.39 | 3.05 | 0.22 |
| Reach 1-Upper | 534 | 5YrSCS24Hr | 0.15 | 92.59 | 92.93 | 92.74 | 92.93 | 0.000491 | 0.20 | 0.89 | 13.42 | 0.15 |
| Reach 1-Upper | 534 | 10YrSCS24Hr | 0.19 | 92.59 | 93.01 | 92.76 | 93.01 | 0.000110 | 0.11 | 3.08 | 38.60 | 0.07 |
| Reach 1-Upper | 534 | 25YrSCS24Hr | 0.24 | 92.59 | 93.24 | 92.78 | 93.24 | 0.000003 | 0.03 | 14.06 | 51.35 | 0.01 |
| Reach 1-Upper | 534 | 50YrSCS24Hr | 0.28 | 92.59 | 93.25 | 92.79 | 93.25 | 0.000004 | 0.03 | 14.61 | 51.39 | 0.02 |
| Reach 1-Upper | 534 | 100YrSCS24Hr | 0.33 | 92.59 | 93.25 | 92.80 | 93.25 | 0.000005 | 0.04 | 14.61 | 51.39 | 0.02 |
| Reach 1-Upper | 510 | 2YrCHI3Hr | 0.06 | 92.60 | 92.72 | 92.68 | 92.73 | 0.004446 | 0.41 | 0.16 | 2.77 | 0.41 |
| Reach 1-Upper | 510 | 5YrCHI3Hr | 0.11 | 92.60 | 92.82 | 92.70 | 92.83 | 0.001169 | 0.34 | 0.32 | 4.18 | 0.24 |
| Reach 1-Upper | 510 | 10YrCHI3Hr | 0.14 | 92.60 | 92.89 | 92.71 | 92.90 | 0.000746 | 0.33 | 0.43 | 5.14 | 0.20 |
| Reach 1-Upper | 510 | 25YrCHI3Hr | 0.19 | 92.60 | 92.99 | 92.73 | 92.99 | 0.000465 | 0.32 | 0.59 | 11.84 | 0.17 |
| Reach 1-Upper | 510 | 50YrCHI3Hr | 0.22 | 92.60 | 93.11 | 92.75 | 93.12 | 0.000243 | 0.28 | 0.79 | 109.05 | 0.13 |
| Reach 1-Upper | 510 | 100YrCHI3Hr | 0.26 | 92.60 | 93.25 | 92.76 | 93.25 | 0.000000 | 0.01 | 42.37 | 109.53 | 0.00 |
| Reach 1-Upper | 510 | 2YrSCS24Hr | 0.10 | 92.60 | 92.80 | 92.69 | 92.80 | 0.001471 | 0.34 | 0.28 | 3.82 | 0.26 |
| Reach 1-Upper | 510 | 5YrSCS24Hr | 0.15 | 92.60 | 92.91 | 92.72 | 92.92 | 0.000658 | 0.32 | 0.47 | 5.55 | 0.19 |
| Reach 1-Upper | 510 | 10YrSCS24Hr | 0.19 | 92.60 | 93.00 | 92.73 | 93.01 | 0.000435 | 0.31 | 0.61 | 13.01 | 0.16 |
| Reach 1-Upper | 510 | 25YrSCS24Hr | 0.24 | 92.60 | 93.24 | 92.75 | 93.24 | 0.000000 | 0.01 | 41.20 | 109.49 | 0.00 |
| Reach 1-Upper | 510 | 50YrSCS24Hr | 0.28 | 92.60 | 93.25 | 92.77 | 93.25 | 0.000000 | 0.01 | 42.37 | 109.53 | 0.00 |
| Reach 1-Upper | 510 | 100YrSCS24Hr | 0.33 | 92.60 | 93.25 | 92.78 | 93.25 | 0.000000 | 0.01 | 42.37 | 109.53 | 0.01 |
| Reach 1-Upper | 505 | | Culvert | | | | | | | | | |
| Reach 1-Upper | 502 | 2YrCHI3Hr | 0.07 | 92.49 | 92.61 | 92.57 | 92.62 | 0.007737 | 0.51 | 0.14 | 2.26 | 0.54 |
| Reach 1-Upper | 502 | 5YrCHI3Hr | 0.12 | 92.49 | 92.65 | 92.60 | 92.67 | 0.006529 | 0.60 | 0.20 | 2.74 | 0.53 |
| Reach 1-Upper | 502 | 10YrCHI3Hr | 0.16 | 92.49 | 92.67 | 92.62 | 92.70 | 0.006103 | 0.66 | 0.24 | 3.03 | 0.52 |
| Reach 1-Upper | 502 | 25YrCHI3Hr | 0.21 | 92.49 | 92.72 | 92.64 | 92.74 | 0.004564 | 0.67 | 0.31 | 3.72 | 0.47 |
| Reach 1-Upper | 502 | 50YrCHI3Hr | 0.25 | 92.49 | 92.80 | 92.65 | 92.82 | 0.002112 | 0.57 | 0.43 | 5.24 | 0.34 |
| Reach 1-Upper | 502 | 100YrCHI3Hr | 0.29 | 92.49 | 92.93 | 92.67 | 92.94 | 0.000855 | 0.47 | 0.63 | 7.55 | 0.23 |
| Reach 1-Upper | 502 | 2YrSCS24Hr | 0.11 | 92.49 | 92.64 | 92.59 | 92.65 | 0.006707 | 0.58 | 0.19 | 2.62 | 0.53 |
| Reach 1-Upper | 502 | 5YrSCS24Hr | 0.17 | 92.49 | 92.68 | 92.62 | 92.71 | 0.005738 | 0.66 | 0.26 | 3.15 | 0.51 |
| Reach 1-Upper | 502 | 10YrSCS24Hr | 0.22 | 92.49 | 92.73 | 92.64 | 92.75 | 0.004158 | 0.66 | 0.33 | 3.95 | 0.45 |
| Reach 1-Upper | 502 | 25YrSCS24Hr | 0.27 | 92.49 | 92.87 | 92.66 | 92.88 | 0.001286 | 0.51 | 0.53 | 6.24 | 0.27 |
| Reach 1-Upper | 502 | 50YrSCS24Hr | 0.32 | 92.49 | 93.02 | 92.68 | 93.03 | 0.000528 | 0.42 | 0.76 | 104.88 | 0.19 |
| Reach 1-Upper | 502 | 100YrSCS24Hr | 0.37 | 92.49 | 93.23 | 92.70 | 93.24 | 0.000228 | 0.34 | 1.08 | 105.45 | 0.13 |
| Reach 1-Upper | 493 | 2YrCHI3Hr | 0.07 | 92.34 | 92.61 | 92.42 | 92.61 | 0.000133 | 0.10 | 0.75 | 4.68 | 0.08 |
| Reach 1-Upper | 493 | 5YrCHI3Hr | 0.12 | 92.34 | 92.65 | 92.45 | 92.65 | 0.000201 | 0.13 | 0.96 | 5.45 | 0.10 |
| Reach 1-Upper | 493 | 10YrCHI3Hr | 0.16 | 92.34 | 92.68 | 92.46 | 92.68 | 0.000231 | 0.14 | 1.12 | 5.93 | 0.10 |
| Reach 1-Upper | 493 | 25YrCHI3Hr | 0.21 | 92.34 | 92.73 | 92.47 | 92.73 | 0.000214 | 0.15 | 1.42 | 6.71 | 0.10 |
| Reach 1-Upper | 493 | 50YrCHI3Hr | 0.25 | 92.34 | 92.81 | 92.49 | 92.81 | 0.000122 | 0.12 | 2.01 | 8.05 | 0.08 |
| Reach 1-Upper | 493 | 100YrCHI3Hr | 0.29 | 92.34 | 92.94 | 92.50 | 92.94 | 0.000003 | 0.02 | 22.75 | 101.14 | 0.01 |
| Reach 1-Upper | 493 | 2YrSCS24Hr | 0.11 | 92.34 | 92.64 | 92.44 | 92.64 | 0.000184 | 0.12 | 0.90 | 5.25 | 0.09 |
| Reach 1-Upper | 493 | 5YrSCS24Hr | 0.17 | 92.34 | 92.69 | 92.46 | 92.69 | 0.000232 | 0.14 | 1.18 | 6.13 | 0.11 |
| Reach 1-Upper | 493 | 10YrSCS24Hr | 0.22 | 92.34 | 92.74 | 92.48 | 92.74 | 0.000200 | 0.15 | 1.49 | 6.81 | 0.10 |
| Reach 1-Upper | 493 | 25YrSCS24Hr | 0.27 | 92.34 | 92.87 | 92.49 | 92.87 | 0.000073 | 0.11 | 2.58 | 9.70 | 0.06 |

HEC-RAS Plan: 20250910-Post_Dev_v02 River: River 1 Reach: Reach 1-Upper (Continued)

| Reach | River Sta | Profile | Q Total (m3/s) | Min Ch El (m) | W.S. Elev (m) | Crit W.S. (m) | E.G. Elev (m) | E.G. Slope (m/m) | Vel Chnl (m/s) | Flow Area (m2) | Top Width (m) | Froude # Chl |
|---------------|-----------|--------------|-------------------|------------------|------------------|------------------|------------------|---------------------|-------------------|-------------------|------------------|--------------|
| Reach 1-Upper | 493 | 50YrSCS24Hr | 0.32 | 92.34 | 93.03 | 92.50 | 93.03 | 0.000001 | 0.02 | 31.90 | 101.53 | 0.01 |
| Reach 1-Upper | 493 | 100YrSCS24Hr | 0.37 | 92.34 | 93.23 | 92.52 | 93.23 | 0.000000 | 0.01 | 52.95 | 102.61 | 0.00 |
| Reach 1-Upper | 474 | 2YrCHI3Hr | 0.07 | 92.41 | 92.60 | 92.50 | 92.60 | 0.000597 | 0.15 | 0.49 | 5.07 | 0.15 |
| Reach 1-Upper | 474 | 5YrCHI3Hr | 0.12 | 92.41 | 92.64 | 92.53 | 92.65 | 0.000602 | 0.17 | 0.72 | 5.95 | 0.16 |
| Reach 1-Upper | 474 | 10YrCHI3Hr | 0.16 | 92.41 | 92.67 | 92.54 | 92.67 | 0.000570 | 0.18 | 0.88 | 6.52 | 0.16 |
| Reach 1-Upper | 474 | 25YrCHI3Hr | 0.21 | 92.41 | 92.72 | 92.55 | 92.72 | 0.000404 | 0.17 | 1.23 | 7.58 | 0.13 |
| Reach 1-Upper | 474 | 50YrCHI3Hr | 0.25 | 92.41 | 92.81 | 92.56 | 92.81 | 0.000152 | 0.13 | 1.98 | 11.32 | 0.09 |
| Reach 1-Upper | 474 | 100YrCHI3Hr | 0.29 | 92.41 | 92.94 | 92.57 | 92.94 | 0.000001 | 0.01 | 34.63 | 91.93 | 0.01 |
| Reach 1-Upper | 474 | 2YrSCS24Hr | 0.11 | 92.41 | 92.63 | 92.52 | 92.64 | 0.000604 | 0.16 | 0.66 | 5.73 | 0.16 |
| Reach 1-Upper | 474 | 5YrSCS24Hr | 0.17 | 92.41 | 92.68 | 92.54 | 92.68 | 0.000532 | 0.18 | 0.96 | 6.77 | 0.15 |
| Reach 1-Upper | 474 | 10YrSCS24Hr | 0.22 | 92.41 | 92.73 | 92.56 | 92.73 | 0.000363 | 0.16 | 1.31 | 7.81 | 0.13 |
| Reach 1-Upper | 474 | 25YrSCS24Hr | 0.27 | 92.41 | 92.87 | 92.57 | 92.87 | 0.000001 | 0.01 | 28.89 | 91.64 | 0.01 |
| Reach 1-Upper | 474 | 50YrSCS24Hr | 0.32 | 92.41 | 93.03 | 92.58 | 93.03 | 0.000000 | 0.01 | 42.95 | 92.33 | 0.00 |
| Reach 1-Upper | 474 | 100YrSCS24Hr | 0.37 | 92.41 | 93.23 | 92.59 | 93.23 | 0.000000 | 0.01 | 62.09 | 93.27 | 0.00 |
| Reach 1-Upper | 454 | 2YrCHI3Hr | 0.07 | 92.44 | 92.58 | 92.51 | 92.59 | 0.001604 | 0.25 | 0.29 | 2.89 | 0.25 |
| Reach 1-Upper | 454 | 5YrCHI3Hr | 0.12 | 92.44 | 92.62 | 92.53 | 92.63 | 0.001687 | 0.29 | 0.42 | 3.32 | 0.26 |
| Reach 1-Upper | 454 | 10YrCHI3Hr | 0.16 | 92.44 | 92.65 | 92.54 | 92.66 | 0.001616 | 0.31 | 0.51 | 3.60 | 0.26 |
| Reach 1-Upper | 454 | 25YrCHI3Hr | 0.21 | 92.44 | 92.70 | 92.56 | 92.71 | 0.001084 | 0.29 | 0.72 | 4.18 | 0.22 |
| Reach 1-Upper | 454 | 50YrCHI3Hr | 0.25 | 92.44 | 92.80 | 92.57 | 92.80 | 0.000421 | 0.22 | 1.17 | 5.42 | 0.14 |
| Reach 1-Upper | 454 | 100YrCHI3Hr | 0.29 | 92.44 | 92.94 | 92.58 | 92.94 | 0.000003 | 0.02 | 20.32 | 83.17 | 0.01 |
| Reach 1-Upper | 454 | 2YrSCS24Hr | 0.11 | 92.44 | 92.61 | 92.52 | 92.62 | 0.001708 | 0.28 | 0.38 | 3.20 | 0.26 |
| Reach 1-Upper | 454 | 5YrSCS24Hr | 0.17 | 92.44 | 92.66 | 92.55 | 92.67 | 0.001485 | 0.31 | 0.56 | 3.74 | 0.25 |
| Reach 1-Upper | 454 | 10YrSCS24Hr | 0.22 | 92.44 | 92.72 | 92.56 | 92.72 | 0.000949 | 0.28 | 0.77 | 4.30 | 0.21 |
| Reach 1-Upper | 454 | 25YrSCS24Hr | 0.27 | 92.44 | 92.87 | 92.58 | 92.87 | 0.000007 | 0.03 | 15.12 | 82.99 | 0.02 |
| Reach 1-Upper | 454 | 50YrSCS24Hr | 0.32 | 92.44 | 93.03 | 92.59 | 93.03 | 0.000001 | 0.02 | 27.84 | 83.45 | 0.01 |
| Reach 1-Upper | 454 | 100YrSCS24Hr | 0.37 | 92.44 | 93.23 | 92.60 | 93.23 | 0.000000 | 0.01 | 45.11 | 84.07 | 0.01 |
| Reach 1-Upper | 434 | 2YrCHI3Hr | 0.07 | 92.42 | 92.54 | 92.49 | 92.54 | 0.003131 | 0.30 | 0.24 | 2.93 | 0.33 |
| Reach 1-Upper | 434 | 5YrCHI3Hr | 0.12 | 92.42 | 92.58 | 92.51 | 92.59 | 0.002184 | 0.32 | 0.39 | 3.35 | 0.30 |
| Reach 1-Upper | 434 | 10YrCHI3Hr | 0.16 | 92.42 | 92.61 | 92.52 | 92.62 | 0.001764 | 0.32 | 0.50 | 3.63 | 0.27 |
| Reach 1-Upper | 434 | 25YrCHI3Hr | 0.21 | 92.42 | 92.70 | 92.53 | 92.70 | 0.000136 | 0.10 | 3.47 | 39.92 | 0.08 |
| Reach 1-Upper | 434 | 50YrCHI3Hr | 0.25 | 92.42 | 92.80 | 92.55 | 92.80 | 0.000022 | 0.05 | 9.17 | 73.84 | 0.03 |
| Reach 1-Upper | 434 | 100YrCHI3Hr | 0.29 | 92.42 | 92.94 | 92.56 | 92.94 | 0.000003 | 0.03 | 19.34 | 74.32 | 0.01 |
| Reach 1-Upper | 434 | 2YrSCS24Hr | 0.11 | 92.42 | 92.57 | 92.50 | 92.57 | 0.002416 | 0.31 | 0.34 | 3.23 | 0.31 |
| Reach 1-Upper | 434 | 5YrSCS24Hr | 0.17 | 92.42 | 92.63 | 92.52 | 92.64 | 0.001606 | 0.31 | 0.56 | 4.00 | 0.26 |
| Reach 1-Upper | 434 | 10YrSCS24Hr | 0.22 | 92.42 | 92.71 | 92.54 | 92.71 | 0.000108 | 0.09 | 4.02 | 43.59 | 0.07 |
| Reach 1-Upper | 434 | 25YrSCS24Hr | 0.27 | 92.42 | 92.87 | 92.55 | 92.87 | 0.000006 | 0.03 | 14.69 | 74.10 | 0.02 |
| Reach 1-Upper | 434 | 50YrSCS24Hr | 0.32 | 92.42 | 93.03 | 92.56 | 93.03 | 0.000001 | 0.02 | 26.07 | 74.63 | 0.01 |
| Reach 1-Upper | 434 | 100YrSCS24Hr | 0.37 | 92.42 | 93.23 | 92.57 | 93.23 | 0.000000 | 0.01 | 41.53 | 75.37 | 0.01 |
| Reach 1-Upper | 416 | 2YrCHI3Hr | 0.07 | 92.34 | 92.52 | 92.42 | 92.52 | 0.000594 | 0.15 | 0.47 | 4.81 | 0.15 |
| Reach 1-Upper | 416 | 5YrCHI3Hr | 0.12 | 92.34 | 92.57 | 92.45 | 92.57 | 0.000421 | 0.17 | 0.75 | 5.85 | 0.14 |
| Reach 1-Upper | 416 | 10YrCHI3Hr | 0.16 | 92.34 | 92.61 | 92.46 | 92.61 | 0.000173 | 0.13 | 2.14 | 28.43 | 0.09 |
| Reach 1-Upper | 416 | 25YrCHI3Hr | 0.21 | 92.34 | 92.70 | 92.47 | 92.70 | 0.000038 | 0.08 | 4.95 | 34.66 | 0.05 |
| Reach 1-Upper | 416 | 50YrCHI3Hr | 0.25 | 92.34 | 92.80 | 92.48 | 92.80 | 0.000012 | 0.05 | 8.86 | 43.80 | 0.03 |
| Reach 1-Upper | 416 | 100YrCHI3Hr | 0.29 | 92.34 | 92.94 | 92.49 | 92.94 | 0.000004 | 0.04 | 16.28 | 66.50 | 0.02 |
| Reach 1-Upper | 416 | 2YrSCS24Hr | 0.11 | 92.34 | 92.56 | 92.44 | 92.56 | 0.000460 | 0.17 | 0.67 | 5.57 | 0.14 |
| Reach 1-Upper | 416 | 5YrSCS24Hr | 0.17 | 92.34 | 92.63 | 92.46 | 92.63 | 0.000124 | 0.11 | 2.65 | 29.68 | 0.08 |
| Reach 1-Upper | 416 | 10YrSCS24Hr | 0.22 | 92.34 | 92.71 | 92.47 | 92.71 | 0.000032 | 0.07 | 5.42 | 35.57 | 0.04 |
| Reach 1-Upper | 416 | 25YrSCS24Hr | 0.27 | 92.34 | 92.87 | 92.49 | 92.87 | 0.000006 | 0.04 | 12.48 | 53.40 | 0.02 |
| Reach 1-Upper | 416 | 50YrSCS24Hr | 0.32 | 92.34 | 93.03 | 92.49 | 93.03 | 0.000002 | 0.03 | 22.33 | 67.07 | 0.01 |
| Reach 1-Upper | 416 | 100YrSCS24Hr | 0.37 | 92.34 | 93.23 | 92.50 | 93.23 | 0.000001 | 0.02 | 36.24 | 67.81 | 0.01 |
| Reach 1-Upper | 398 | 2YrCHI3Hr | 0.07 | 92.28 | 92.50 | 92.40 | 92.51 | 0.000938 | 0.22 | 0.33 | 2.54 | 0.20 |
| Reach 1-Upper | 398 | 5YrCHI3Hr | 0.12 | 92.28 | 92.56 | 92.42 | 92.56 | 0.000913 | 0.26 | 0.48 | 2.86 | 0.20 |
| Reach 1-Upper | 398 | 10YrCHI3Hr | 0.16 | 92.28 | 92.60 | 92.44 | 92.61 | 0.000768 | 0.26 | 0.61 | 3.13 | 0.19 |
| Reach 1-Upper | 398 | 25YrCHI3Hr | 0.21 | 92.28 | 92.70 | 92.46 | 92.70 | 0.000401 | 0.23 | 0.93 | 4.03 | 0.14 |
| Reach 1-Upper | 398 | 50YrCHI3Hr | 0.25 | 92.28 | 92.80 | 92.47 | 92.80 | 0.000150 | 0.16 | 2.51 | 35.14 | 0.09 |
| Reach 1-Upper | 398 | 100YrCHI3Hr | 0.29 | 92.28 | 92.94 | 92.48 | 92.94 | 0.000018 | 0.07 | 9.30 | 58.44 | 0.03 |
| Reach 1-Upper | 398 | 2YrSCS24Hr | 0.11 | 92.28 | 92.54 | 92.42 | 92.55 | 0.000934 | 0.25 | 0.43 | 2.78 | 0.20 |
| Reach 1-Upper | 398 | 5YrSCS24Hr | 0.17 | 92.28 | 92.62 | 92.44 | 92.62 | 0.000689 | 0.26 | 0.67 | 3.24 | 0.18 |
| Reach 1-Upper | 398 | 10YrSCS24Hr | 0.22 | 92.28 | 92.71 | 92.46 | 92.71 | 0.000365 | 0.22 | 0.99 | 4.50 | 0.14 |
| Reach 1-Upper | 398 | 25YrSCS24Hr | 0.27 | 92.28 | 92.87 | 92.48 | 92.87 | 0.000042 | 0.10 | 5.90 | 48.09 | 0.05 |
| Reach 1-Upper | 398 | 50YrSCS24Hr | 0.32 | 92.28 | 93.03 | 92.49 | 93.03 | 0.000006 | 0.04 | 14.60 | 58.70 | 0.02 |
| Reach 1-Upper | 398 | 100YrSCS24Hr | 0.37 | 92.28 | 93.23 | 92.50 | 93.23 | 0.000001 | 0.02 | 26.77 | 59.29 | 0.01 |
| Reach 1-Upper | 383 | 2YrCHI3Hr | 0.07 | 92.34 | 92.47 | 92.42 | 92.48 | 0.004360 | 0.39 | 0.19 | 1.94 | 0.40 |
| Reach 1-Upper | 383 | 5YrCHI3Hr | 0.12 | 92.34 | 92.53 | 92.45 | 92.54 | 0.002848 | 0.39 | 0.31 | 2.30 | 0.34 |
| Reach 1-Upper | 383 | 10YrCHI3Hr | 0.16 | 92.34 | 92.58 | 92.46 | 92.59 | 0.001812 | 0.36 | 0.43 | 2.59 | 0.28 |
| Reach 1-Upper | 383 | 25YrCHI3Hr | 0.21 | 92.34 | 92.69 | 92.48 | 92.69 | 0.000720 | 0.28 | 0.74 | 3.18 | 0.19 |
| Reach 1-Upper | 383 | 50YrCHI3Hr | 0.25 | 92.34 | 92.79 | 92.50 | 92.80 | 0.000334 | 0.22 | 1.11 | 3.78 | 0.13 |
| Reach 1-Upper | 383 | 100YrCHI3Hr | 0.29 | 92.34 | 92.93 | 92.51 | 92.94 | 0.000138 | 0.17 | 1.71 | 4.83 | 0.09 |
| Reach 1-Upper | 383 | 2YrSCS24Hr | 0.11 | 92.34 | 92.51 | 92.44 | 92.52 | 0.003235 | 0.40 | 0.27 | 2.21 | 0.36 |
| Reach 1-Upper | 383 | 5YrSCS24Hr | 0.17 | 92.34 | 92.60 | 92.47 | 92.61 | 0.001493 | 0.35 | 0.49 | 2.71 | 0.26 |
| Reach 1-Upper | 383 | 10YrSCS24Hr | 0.22 | 92.34 | 92.70 | 92.49 | 92.70 | 0.000650 | 0.28 | 0.78 | 3.26 | 0.18 |
| Reach 1-Upper | 383 | 25YrSCS24Hr | 0.27 | 92.34 | 92.87 | 92.51 | 92.87 | 0.000205 | 0.19 | 1.42 | 4.21 | 0.11 |
| Reach 1-Upper | 383 | 50YrSCS24Hr | 0.32 | 92.34 | 93.03 | 92.52 | 93.03 | 0.000014 | 0.06 | 10.30 | 51.61 | 0.03 |
| Reach 1-Upper | 383 | 100YrSCS24Hr | 0.37 | 92.34 | 93.23 | 92.53 | 93.23 | 0.000002 | 0.03 | 21.02 | 52.21 | 0.01 |
| Reach 1-Upper | 364 | 2YrCHI3Hr | 0.07 | 92.23 | 92.43 | 92.33 | 92.44 | 0.001347 | 0.27 | 0.27 | 2.04 | 0.23 |
| Reach 1-Upper | 364 | 5YrCHI3Hr | 0.12 | 92.23 | 92.50 | 92.36 | 92.51 | 0.001091 | 0.29 | 0.42 | 2.38 | 0.22 |

HEC-RAS Plan: 20250910-Post_Dev_v02 River: River 1 Reach: Reach 1-Upper (Continued)

| Reach | River Sta | Profile | Q Total (m3/s) | Min Ch El (m) | W.S. Elev (m) | Crit W.S. (m) | E.G. Elev (m) | E.G. Slope (m/m) | Vel Chnl (m/s) | Flow Area (m2) | Top Width (m) | Froude # Chl |
|---------------|-----------|--------------|-------------------|------------------|------------------|------------------|------------------|---------------------|-------------------|-------------------|------------------|--------------|
| Reach 1-Upper | 364 | 10YrCHI3Hr | 0.16 | 92.23 | 92.56 | 92.38 | 92.57 | 0.000763 | 0.28 | 0.57 | 2.68 | 0.19 |
| Reach 1-Upper | 364 | 25YrCHI3Hr | 0.21 | 92.23 | 92.68 | 92.40 | 92.68 | 0.000366 | 0.23 | 0.92 | 3.24 | 0.14 |
| Reach 1-Upper | 364 | 50YrCHI3Hr | 0.25 | 92.23 | 92.79 | 92.41 | 92.79 | 0.000203 | 0.19 | 1.31 | 3.88 | 0.11 |
| Reach 1-Upper | 364 | 100YrCHI3Hr | 0.29 | 92.23 | 92.93 | 92.43 | 92.93 | 0.000094 | 0.15 | 1.98 | 5.87 | 0.07 |
| Reach 1-Upper | 364 | 2YrSCS24Hr | 0.11 | 92.23 | 92.48 | 92.35 | 92.49 | 0.001191 | 0.29 | 0.37 | 2.28 | 0.23 |
| Reach 1-Upper | 364 | 5YrSCS24Hr | 0.17 | 92.23 | 92.59 | 92.38 | 92.59 | 0.000655 | 0.27 | 0.64 | 2.80 | 0.18 |
| Reach 1-Upper | 364 | 10YrSCS24Hr | 0.22 | 92.23 | 92.69 | 92.40 | 92.70 | 0.000339 | 0.22 | 0.97 | 3.32 | 0.13 |
| Reach 1-Upper | 364 | 25YrSCS24Hr | 0.27 | 92.23 | 92.87 | 92.42 | 92.87 | 0.000135 | 0.17 | 1.64 | 4.67 | 0.09 |
| Reach 1-Upper | 364 | 50YrSCS24Hr | 0.32 | 92.23 | 93.03 | 92.44 | 93.03 | 0.000033 | 0.10 | 5.95 | 44.01 | 0.05 |
| Reach 1-Upper | 364 | 100YrSCS24Hr | 0.37 | 92.23 | 93.23 | 92.45 | 93.23 | 0.000005 | 0.04 | 15.12 | 44.59 | 0.02 |
| Reach 1-Upper | 347 | 2YrCHI3Hr | 0.07 | 92.26 | 92.41 | 92.33 | 92.41 | 0.001311 | 0.25 | 0.29 | 2.48 | 0.23 |
| Reach 1-Upper | 347 | 5YrCHI3Hr | 0.12 | 92.26 | 92.49 | 92.35 | 92.49 | 0.000799 | 0.25 | 0.49 | 2.81 | 0.19 |
| Reach 1-Upper | 347 | 10YrCHI3Hr | 0.16 | 92.26 | 92.55 | 92.36 | 92.56 | 0.000505 | 0.23 | 0.69 | 3.09 | 0.16 |
| Reach 1-Upper | 347 | 25YrCHI3Hr | 0.21 | 92.26 | 92.67 | 92.38 | 92.68 | 0.000235 | 0.19 | 1.09 | 3.61 | 0.11 |
| Reach 1-Upper | 347 | 50YrCHI3Hr | 0.25 | 92.26 | 92.79 | 92.39 | 92.79 | 0.000131 | 0.16 | 1.52 | 4.09 | 0.09 |
| Reach 1-Upper | 347 | 100YrCHI3Hr | 0.29 | 92.26 | 92.93 | 92.41 | 92.93 | 0.000067 | 0.13 | 2.17 | 5.17 | 0.06 |
| Reach 1-Upper | 347 | 2YrSCS24Hr | 0.11 | 92.26 | 92.46 | 92.34 | 92.47 | 0.000924 | 0.25 | 0.43 | 2.71 | 0.20 |
| Reach 1-Upper | 347 | 5YrSCS24Hr | 0.17 | 92.26 | 92.58 | 92.37 | 92.58 | 0.000426 | 0.22 | 0.77 | 3.20 | 0.14 |
| Reach 1-Upper | 347 | 10YrSCS24Hr | 0.22 | 92.26 | 92.69 | 92.38 | 92.69 | 0.000218 | 0.19 | 1.15 | 3.67 | 0.11 |
| Reach 1-Upper | 347 | 25YrSCS24Hr | 0.27 | 92.26 | 92.87 | 92.40 | 92.87 | 0.000091 | 0.15 | 1.87 | 4.46 | 0.07 |
| Reach 1-Upper | 347 | 50YrSCS24Hr | 0.32 | 92.26 | 93.03 | 92.41 | 93.03 | 0.000042 | 0.12 | 2.84 | 10.46 | 0.05 |
| Reach 1-Upper | 347 | 100YrSCS24Hr | 0.37 | 92.26 | 93.23 | 92.43 | 93.23 | 0.000008 | 0.06 | 10.68 | 37.82 | 0.02 |
| Reach 1-Upper | 328 | 2YrCHI3Hr | 0.07 | 92.20 | 92.38 | 92.29 | 92.38 | 0.001752 | 0.30 | 0.24 | 1.87 | 0.27 |
| Reach 1-Upper | 328 | 5YrCHI3Hr | 0.12 | 92.20 | 92.47 | 92.32 | 92.47 | 0.001008 | 0.29 | 0.42 | 2.25 | 0.21 |
| Reach 1-Upper | 328 | 10YrCHI3Hr | 0.16 | 92.20 | 92.54 | 92.33 | 92.54 | 0.000638 | 0.26 | 0.60 | 2.55 | 0.17 |
| Reach 1-Upper | 328 | 25YrCHI3Hr | 0.21 | 92.20 | 92.67 | 92.36 | 92.67 | 0.000304 | 0.22 | 0.95 | 3.08 | 0.13 |
| Reach 1-Upper | 328 | 50YrCHI3Hr | 0.25 | 92.20 | 92.78 | 92.37 | 92.78 | 0.000178 | 0.19 | 1.34 | 3.69 | 0.10 |
| Reach 1-Upper | 328 | 100YrCHI3Hr | 0.29 | 92.20 | 92.93 | 92.39 | 92.93 | 0.000093 | 0.15 | 1.96 | 4.66 | 0.07 |
| Reach 1-Upper | 328 | 2YrSCS24Hr | 0.11 | 92.20 | 92.44 | 92.31 | 92.45 | 0.001172 | 0.29 | 0.37 | 2.14 | 0.23 |
| Reach 1-Upper | 328 | 5YrSCS24Hr | 0.17 | 92.20 | 92.57 | 92.34 | 92.57 | 0.000541 | 0.26 | 0.67 | 2.67 | 0.16 |
| Reach 1-Upper | 328 | 10YrSCS24Hr | 0.22 | 92.20 | 92.68 | 92.36 | 92.69 | 0.000283 | 0.22 | 1.00 | 3.14 | 0.12 |
| Reach 1-Upper | 328 | 25YrSCS24Hr | 0.27 | 92.20 | 92.86 | 92.38 | 92.87 | 0.000127 | 0.16 | 1.67 | 4.31 | 0.08 |
| Reach 1-Upper | 328 | 50YrSCS24Hr | 0.32 | 92.20 | 93.02 | 92.40 | 93.02 | 0.000064 | 0.13 | 2.44 | 5.46 | 0.06 |
| Reach 1-Upper | 328 | 100YrSCS24Hr | 0.37 | 92.20 | 93.23 | 92.41 | 93.23 | 0.000014 | 0.07 | 8.02 | 29.79 | 0.03 |
| Reach 1-Upper | 306 | 2YrCHI3Hr | 0.07 | 92.07 | 92.36 | 92.19 | 92.36 | 0.000723 | 0.26 | 0.28 | 1.53 | 0.18 |
| Reach 1-Upper | 306 | 5YrCHI3Hr | 0.12 | 92.07 | 92.45 | 92.22 | 92.45 | 0.000687 | 0.30 | 0.40 | 1.84 | 0.18 |
| Reach 1-Upper | 306 | 10YrCHI3Hr | 0.16 | 92.07 | 92.53 | 92.25 | 92.53 | 0.000564 | 0.31 | 0.51 | 2.11 | 0.17 |
| Reach 1-Upper | 306 | 25YrCHI3Hr | 0.21 | 92.07 | 92.66 | 92.27 | 92.66 | 0.000340 | 0.29 | 0.71 | 2.60 | 0.14 |
| Reach 1-Upper | 306 | 50YrCHI3Hr | 0.25 | 92.07 | 92.78 | 92.29 | 92.78 | 0.000232 | 0.28 | 0.89 | 3.10 | 0.12 |
| Reach 1-Upper | 306 | 100YrCHI3Hr | 0.29 | 92.07 | 92.92 | 92.31 | 92.93 | 0.000151 | 0.26 | 1.11 | 3.98 | 0.10 |
| Reach 1-Upper | 306 | 2YrSCS24Hr | 0.11 | 92.07 | 92.42 | 92.22 | 92.43 | 0.000711 | 0.29 | 0.37 | 1.75 | 0.18 |
| Reach 1-Upper | 306 | 5YrSCS24Hr | 0.17 | 92.07 | 92.56 | 92.26 | 92.56 | 0.000514 | 0.31 | 0.56 | 2.21 | 0.16 |
| Reach 1-Upper | 306 | 10YrSCS24Hr | 0.22 | 92.07 | 92.67 | 92.28 | 92.68 | 0.000325 | 0.29 | 0.74 | 2.67 | 0.13 |
| Reach 1-Upper | 306 | 25YrSCS24Hr | 0.27 | 92.07 | 92.86 | 92.31 | 92.86 | 0.000182 | 0.27 | 1.01 | 3.45 | 0.11 |
| Reach 1-Upper | 306 | 50YrSCS24Hr | 0.32 | 92.07 | 93.02 | 92.32 | 93.02 | 0.000121 | 0.25 | 1.25 | 4.84 | 0.09 |
| Reach 1-Upper | 306 | 100YrSCS24Hr | 0.37 | 92.07 | 93.23 | 92.34 | 93.23 | 0.000077 | 0.24 | 1.57 | 20.82 | 0.07 |
| Reach 1-Upper | 300 | | Culvert | | | | | | | | | |
| Reach 1-Upper | 294 | 2YrCHI3Hr | 0.07 | 92.15 | 92.32 | 92.23 | 92.33 | 0.001574 | 0.32 | 0.23 | 2.11 | 0.26 |
| Reach 1-Upper | 294 | 5YrCHI3Hr | 0.12 | 92.15 | 92.37 | 92.26 | 92.38 | 0.001843 | 0.41 | 0.30 | 2.35 | 0.30 |
| Reach 1-Upper | 294 | 10YrCHI3Hr | 0.16 | 92.15 | 92.39 | 92.27 | 92.40 | 0.002090 | 0.48 | 0.33 | 2.47 | 0.32 |
| Reach 1-Upper | 294 | 25YrCHI3Hr | 0.21 | 92.15 | 92.42 | 92.30 | 92.44 | 0.002418 | 0.56 | 0.38 | 2.62 | 0.35 |
| Reach 1-Upper | 294 | 50YrCHI3Hr | 0.25 | 92.15 | 92.44 | 92.31 | 92.46 | 0.002632 | 0.61 | 0.41 | 2.73 | 0.37 |
| Reach 1-Upper | 294 | 100YrCHI3Hr | 0.29 | 92.15 | 92.46 | 92.33 | 92.49 | 0.002788 | 0.66 | 0.44 | 2.84 | 0.39 |
| Reach 1-Upper | 294 | 2YrSCS24Hr | 0.11 | 92.15 | 92.36 | 92.25 | 92.36 | 0.001772 | 0.39 | 0.28 | 2.29 | 0.29 |
| Reach 1-Upper | 294 | 5YrSCS24Hr | 0.17 | 92.15 | 92.40 | 92.28 | 92.41 | 0.002190 | 0.50 | 0.34 | 2.51 | 0.33 |
| Reach 1-Upper | 294 | 10YrSCS24Hr | 0.22 | 92.15 | 92.42 | 92.30 | 92.44 | 0.002481 | 0.57 | 0.38 | 2.64 | 0.36 |
| Reach 1-Upper | 294 | 25YrSCS24Hr | 0.27 | 92.15 | 92.45 | 92.32 | 92.48 | 0.002750 | 0.64 | 0.43 | 2.79 | 0.39 |
| Reach 1-Upper | 294 | 50YrSCS24Hr | 0.32 | 92.15 | 92.48 | 92.34 | 92.50 | 0.002924 | 0.70 | 0.46 | 2.90 | 0.40 |
| Reach 1-Upper | 294 | 100YrSCS24Hr | 0.37 | 92.15 | 92.50 | 92.35 | 92.53 | 0.003160 | 0.76 | 0.49 | 3.01 | 0.42 |
| Reach 1-Upper | 279 | 2YrCHI3Hr | 0.09 | 92.08 | 92.21 | 92.21 | 92.25 | 0.030968 | 0.83 | 0.10 | 1.54 | 1.01 |
| Reach 1-Upper | 279 | 5YrCHI3Hr | 0.15 | 92.08 | 92.25 | 92.24 | 92.29 | 0.025757 | 0.90 | 0.16 | 1.85 | 0.97 |
| Reach 1-Upper | 279 | 10YrCHI3Hr | 0.20 | 92.08 | 92.28 | | 92.32 | 0.017921 | 0.87 | 0.23 | 2.03 | 0.83 |
| Reach 1-Upper | 279 | 25YrCHI3Hr | 0.26 | 92.08 | 92.31 | | 92.35 | 0.013590 | 0.86 | 0.30 | 2.25 | 0.75 |
| Reach 1-Upper | 279 | 50YrCHI3Hr | 0.31 | 92.08 | 92.34 | | 92.38 | 0.011935 | 0.87 | 0.36 | 2.40 | 0.71 |
| Reach 1-Upper | 279 | 100YrCHI3Hr | 0.37 | 92.08 | 92.36 | | 92.40 | 0.010878 | 0.88 | 0.42 | 2.54 | 0.69 |
| Reach 1-Upper | 279 | 2YrSCS24Hr | 0.13 | 92.08 | 92.24 | 92.24 | 92.28 | 0.028026 | 0.89 | 0.15 | 1.77 | 1.00 |
| Reach 1-Upper | 279 | 5YrSCS24Hr | 0.21 | 92.08 | 92.29 | | 92.33 | 0.016973 | 0.87 | 0.24 | 2.08 | 0.82 |
| Reach 1-Upper | 279 | 10YrSCS24Hr | 0.27 | 92.08 | 92.32 | | 92.36 | 0.013275 | 0.86 | 0.31 | 2.27 | 0.74 |
| Reach 1-Upper | 279 | 25YrSCS24Hr | 0.34 | 92.08 | 92.35 | | 92.39 | 0.011320 | 0.87 | 0.39 | 2.47 | 0.70 |
| Reach 1-Upper | 279 | 50YrSCS24Hr | 0.40 | 92.08 | 92.38 | | 92.42 | 0.010426 | 0.89 | 0.45 | 2.61 | 0.68 |
| Reach 1-Upper | 279 | 100YrSCS24Hr | 0.47 | 92.08 | 92.40 | | 92.44 | 0.009682 | 0.90 | 0.52 | 2.76 | 0.67 |
| Reach 1-Upper | 277 | 2YrCHI3Hr | 0.09 | 91.95 | 92.21 | | 92.21 | 0.000715 | 0.22 | 0.40 | 2.73 | 0.18 |
| Reach 1-Upper | 277 | 5YrCHI3Hr | 0.15 | 91.95 | 92.26 | | 92.26 | 0.000859 | 0.28 | 0.55 | 3.02 | 0.20 |
| Reach 1-Upper | 277 | 10YrCHI3Hr | 0.20 | 91.95 | 92.29 | | 92.29 | 0.000926 | 0.32 | 0.64 | 3.19 | 0.21 |
| Reach 1-Upper | 277 | 25YrCHI3Hr | 0.26 | 91.95 | 92.32 | | 92.33 | 0.000998 | 0.37 | 0.75 | 3.39 | 0.23 |
| Reach 1-Upper | 277 | 50YrCHI3Hr | 0.31 | 91.95 | 92.35 | | 92.36 | 0.001055 | 0.40 | 0.84 | 3.52 | 0.24 |

HEC-RAS Plan: 20250910-Post_Dev_v02 River: River 1 Reach: Reach 1-Upper (Continued)

| Reach | River Sta | Profile | Q Total (m3/s) | Min Ch El (m) | W.S. Elev (m) | Crit W.S. (m) | E.G. Elev (m) | E.G. Slope (m/m) | Vel Chnl (m/s) | Flow Area (m2) | Top Width (m) | Froude # Chl |
|---------------|-----------|--------------|-------------------|------------------|------------------|------------------|------------------|---------------------|-------------------|-------------------|------------------|--------------|
| Reach 1-Upper | 277 | 100YrCHI3Hr | 0.37 | 91.95 | 92.37 | | 92.38 | 0.001115 | 0.43 | 0.92 | 3.65 | 0.25 |
| Reach 1-Upper | 277 | 2YrSCS24Hr | 0.13 | 91.95 | 92.25 | | 92.25 | 0.000829 | 0.26 | 0.51 | 2.95 | 0.20 |
| Reach 1-Upper | 277 | 5YrSCS24Hr | 0.21 | 91.95 | 92.30 | | 92.30 | 0.000956 | 0.33 | 0.66 | 3.23 | 0.22 |
| Reach 1-Upper | 277 | 10YrSCS24Hr | 0.27 | 91.95 | 92.33 | | 92.34 | 0.001007 | 0.37 | 0.77 | 3.41 | 0.23 |
| Reach 1-Upper | 277 | 25YrSCS24Hr | 0.34 | 91.95 | 92.36 | | 92.37 | 0.001088 | 0.42 | 0.88 | 3.60 | 0.24 |
| Reach 1-Upper | 277 | 50YrSCS24Hr | 0.40 | 91.95 | 92.39 | | 92.40 | 0.001147 | 0.45 | 0.97 | 3.73 | 0.25 |
| Reach 1-Upper | 277 | 100YrSCS24Hr | 0.47 | 91.95 | 92.41 | | 92.42 | 0.001203 | 0.48 | 1.06 | 3.86 | 0.26 |
| Reach 1-Upper | 270 | 2YrCHI3Hr | 0.09 | 92.03 | 92.20 | | 92.20 | 0.001702 | 0.28 | 0.31 | 2.65 | 0.26 |
| Reach 1-Upper | 270 | 5YrCHI3Hr | 0.15 | 92.03 | 92.25 | | 92.26 | 0.001752 | 0.33 | 0.45 | 3.08 | 0.28 |
| Reach 1-Upper | 270 | 10YrCHI3Hr | 0.20 | 92.03 | 92.28 | | 92.29 | 0.001743 | 0.36 | 0.54 | 3.36 | 0.28 |
| Reach 1-Upper | 270 | 25YrCHI3Hr | 0.26 | 92.03 | 92.31 | | 92.32 | 0.001731 | 0.40 | 0.67 | 3.69 | 0.29 |
| Reach 1-Upper | 270 | 50YrCHI3Hr | 0.31 | 92.03 | 92.34 | | 92.35 | 0.001733 | 0.42 | 0.76 | 3.96 | 0.29 |
| Reach 1-Upper | 270 | 100YrCHI3Hr | 0.37 | 92.03 | 92.36 | | 92.37 | 0.001677 | 0.44 | 0.86 | 4.77 | 0.29 |
| Reach 1-Upper | 270 | 2YrSCS24Hr | 0.13 | 92.03 | 92.24 | | 92.24 | 0.001762 | 0.32 | 0.41 | 2.96 | 0.27 |
| Reach 1-Upper | 270 | 5YrSCS24Hr | 0.21 | 92.03 | 92.29 | | 92.29 | 0.001769 | 0.37 | 0.57 | 3.43 | 0.28 |
| Reach 1-Upper | 270 | 10YrSCS24Hr | 0.27 | 92.03 | 92.32 | | 92.33 | 0.001732 | 0.40 | 0.68 | 3.72 | 0.29 |
| Reach 1-Upper | 270 | 25YrSCS24Hr | 0.34 | 92.03 | 92.35 | | 92.36 | 0.001702 | 0.43 | 0.81 | 4.41 | 0.29 |
| Reach 1-Upper | 270 | 50YrSCS24Hr | 0.40 | 92.03 | 92.38 | | 92.39 | 0.001650 | 0.45 | 0.93 | 5.21 | 0.29 |
| Reach 1-Upper | 270 | 100YrSCS24Hr | 0.47 | 92.03 | 92.40 | | 92.41 | 0.001589 | 0.48 | 1.06 | 5.67 | 0.29 |
| Reach 1-Upper | 261 | 2YrCHI3Hr | 0.09 | 92.00 | 92.18 | 92.10 | 92.19 | 0.002251 | 0.33 | 0.26 | 2.11 | 0.30 |
| Reach 1-Upper | 261 | 5YrCHI3Hr | 0.15 | 92.00 | 92.23 | 92.13 | 92.24 | 0.002551 | 0.41 | 0.36 | 2.34 | 0.33 |
| Reach 1-Upper | 261 | 10YrCHI3Hr | 0.20 | 92.00 | 92.26 | 92.15 | 92.27 | 0.002717 | 0.45 | 0.43 | 2.48 | 0.35 |
| Reach 1-Upper | 261 | 25YrCHI3Hr | 0.26 | 92.00 | 92.29 | 92.17 | 92.30 | 0.002863 | 0.50 | 0.52 | 2.64 | 0.36 |
| Reach 1-Upper | 261 | 50YrCHI3Hr | 0.31 | 92.00 | 92.31 | 92.19 | 92.33 | 0.002989 | 0.54 | 0.58 | 2.75 | 0.38 |
| Reach 1-Upper | 261 | 100YrCHI3Hr | 0.37 | 92.00 | 92.34 | 92.21 | 92.35 | 0.003096 | 0.57 | 0.64 | 2.86 | 0.39 |
| Reach 1-Upper | 261 | 2YrSCS24Hr | 0.13 | 92.00 | 92.22 | 92.12 | 92.22 | 0.002475 | 0.39 | 0.33 | 2.28 | 0.32 |
| Reach 1-Upper | 261 | 5YrSCS24Hr | 0.21 | 92.00 | 92.26 | 92.16 | 92.28 | 0.002821 | 0.47 | 0.45 | 2.51 | 0.36 |
| Reach 1-Upper | 261 | 10YrSCS24Hr | 0.27 | 92.00 | 92.29 | 92.18 | 92.31 | 0.002885 | 0.51 | 0.53 | 2.66 | 0.37 |
| Reach 1-Upper | 261 | 25YrSCS24Hr | 0.34 | 92.00 | 92.33 | 92.20 | 92.34 | 0.003049 | 0.56 | 0.61 | 2.81 | 0.38 |
| Reach 1-Upper | 261 | 50YrSCS24Hr | 0.40 | 92.00 | 92.36 | 92.22 | 92.37 | 0.003150 | 0.59 | 0.68 | 2.92 | 0.39 |
| Reach 1-Upper | 261 | 100YrSCS24Hr | 0.47 | 92.00 | 92.37 | 92.23 | 92.39 | 0.003253 | 0.62 | 0.75 | 3.06 | 0.40 |
| Reach 1-Upper | 239 | 2YrCHI3Hr | 0.09 | 91.93 | 92.05 | 92.04 | 92.07 | 0.017641 | 0.69 | 0.12 | 1.58 | 0.78 |
| Reach 1-Upper | 239 | 5YrCHI3Hr | 0.15 | 91.93 | 92.09 | 92.07 | 92.12 | 0.014089 | 0.75 | 0.20 | 1.89 | 0.73 |
| Reach 1-Upper | 239 | 10YrCHI3Hr | 0.20 | 91.93 | 92.12 | 92.09 | 92.15 | 0.012625 | 0.78 | 0.25 | 2.05 | 0.71 |
| Reach 1-Upper | 239 | 25YrCHI3Hr | 0.26 | 91.93 | 92.15 | 92.11 | 92.18 | 0.011287 | 0.82 | 0.32 | 2.22 | 0.69 |
| Reach 1-Upper | 239 | 50YrCHI3Hr | 0.31 | 91.93 | 92.17 | 92.13 | 92.21 | 0.010600 | 0.84 | 0.37 | 2.34 | 0.68 |
| Reach 1-Upper | 239 | 100YrCHI3Hr | 0.37 | 91.93 | 92.20 | 92.15 | 92.23 | 0.010052 | 0.87 | 0.42 | 2.45 | 0.67 |
| Reach 1-Upper | 239 | 2YrSCS24Hr | 0.13 | 91.93 | 92.08 | 92.06 | 92.11 | 0.014856 | 0.73 | 0.18 | 1.80 | 0.74 |
| Reach 1-Upper | 239 | 5YrSCS24Hr | 0.21 | 91.93 | 92.13 | 92.10 | 92.16 | 0.012234 | 0.79 | 0.27 | 2.09 | 0.70 |
| Reach 1-Upper | 239 | 10YrSCS24Hr | 0.27 | 91.93 | 92.15 | 92.12 | 92.19 | 0.011165 | 0.82 | 0.33 | 2.24 | 0.69 |
| Reach 1-Upper | 239 | 25YrSCS24Hr | 0.34 | 91.93 | 92.19 | 92.14 | 92.22 | 0.010287 | 0.86 | 0.40 | 2.40 | 0.67 |
| Reach 1-Upper | 239 | 50YrSCS24Hr | 0.40 | 91.93 | 92.21 | 92.16 | 92.25 | 0.009763 | 0.88 | 0.45 | 2.52 | 0.66 |
| Reach 1-Upper | 239 | 100YrSCS24Hr | 0.47 | 91.93 | 92.23 | 92.17 | 92.27 | 0.009233 | 0.90 | 0.52 | 2.64 | 0.65 |
| Reach 1-Upper | 218 | 2YrCHI3Hr | 0.09 | 91.82 | 91.97 | 91.90 | 91.98 | 0.002011 | 0.30 | 0.29 | 2.50 | 0.28 |
| Reach 1-Upper | 218 | 5YrCHI3Hr | 0.15 | 91.82 | 92.02 | 91.92 | 92.02 | 0.002154 | 0.37 | 0.41 | 2.72 | 0.30 |
| Reach 1-Upper | 218 | 10YrCHI3Hr | 0.20 | 91.82 | 92.05 | 91.94 | 92.05 | 0.002195 | 0.40 | 0.49 | 2.86 | 0.31 |
| Reach 1-Upper | 218 | 25YrCHI3Hr | 0.26 | 91.82 | 92.08 | 91.96 | 92.09 | 0.002317 | 0.45 | 0.58 | 3.01 | 0.33 |
| Reach 1-Upper | 218 | 50YrCHI3Hr | 0.31 | 91.82 | 92.10 | 91.97 | 92.11 | 0.002380 | 0.48 | 0.65 | 3.13 | 0.34 |
| Reach 1-Upper | 218 | 100YrCHI3Hr | 0.37 | 91.82 | 92.12 | 91.99 | 92.14 | 0.002427 | 0.51 | 0.72 | 3.24 | 0.34 |
| Reach 1-Upper | 218 | 2YrSCS24Hr | 0.13 | 91.82 | 92.00 | 91.92 | 92.01 | 0.002121 | 0.35 | 0.37 | 2.66 | 0.30 |
| Reach 1-Upper | 218 | 5YrSCS24Hr | 0.21 | 91.82 | 92.05 | 91.94 | 92.06 | 0.002229 | 0.42 | 0.51 | 2.90 | 0.32 |
| Reach 1-Upper | 218 | 10YrSCS24Hr | 0.27 | 91.82 | 92.08 | 91.96 | 92.09 | 0.002328 | 0.45 | 0.59 | 3.03 | 0.33 |
| Reach 1-Upper | 218 | 25YrSCS24Hr | 0.34 | 91.82 | 92.11 | 91.98 | 92.13 | 0.002406 | 0.50 | 0.69 | 3.19 | 0.34 |
| Reach 1-Upper | 218 | 50YrSCS24Hr | 0.40 | 91.82 | 92.14 | 92.00 | 92.15 | 0.002454 | 0.52 | 0.77 | 3.31 | 0.35 |
| Reach 1-Upper | 218 | 100YrSCS24Hr | 0.47 | 91.82 | 92.16 | 92.01 | 92.18 | 0.002479 | 0.55 | 0.85 | 3.47 | 0.35 |
| Reach 1-Upper | 197 | 2YrCHI3Hr | 0.09 | 91.73 | 91.86 | 91.84 | 91.88 | 0.015766 | 0.67 | 0.13 | 1.59 | 0.75 |
| Reach 1-Upper | 197 | 5YrCHI3Hr | 0.15 | 91.73 | 91.90 | 91.87 | 91.93 | 0.013264 | 0.74 | 0.20 | 1.88 | 0.72 |
| Reach 1-Upper | 197 | 10YrCHI3Hr | 0.20 | 91.73 | 91.92 | 91.89 | 91.96 | 0.012348 | 0.78 | 0.25 | 2.01 | 0.71 |
| Reach 1-Upper | 197 | 25YrCHI3Hr | 0.26 | 91.73 | 91.95 | 91.92 | 91.99 | 0.011605 | 0.83 | 0.31 | 2.16 | 0.70 |
| Reach 1-Upper | 197 | 50YrCHI3Hr | 0.31 | 91.73 | 91.98 | 91.94 | 92.01 | 0.010864 | 0.86 | 0.36 | 2.27 | 0.69 |
| Reach 1-Upper | 197 | 100YrCHI3Hr | 0.37 | 91.73 | 92.00 | 91.95 | 92.04 | 0.010606 | 0.90 | 0.41 | 2.36 | 0.69 |
| Reach 1-Upper | 197 | 2YrSCS24Hr | 0.13 | 91.73 | 91.89 | 91.87 | 91.91 | 0.013909 | 0.72 | 0.18 | 1.81 | 0.72 |
| Reach 1-Upper | 197 | 5YrSCS24Hr | 0.21 | 91.73 | 91.93 | 91.90 | 91.96 | 0.012137 | 0.79 | 0.27 | 2.05 | 0.70 |
| Reach 1-Upper | 197 | 10YrSCS24Hr | 0.27 | 91.73 | 91.96 | 91.92 | 91.99 | 0.011514 | 0.84 | 0.32 | 2.18 | 0.70 |
| Reach 1-Upper | 197 | 25YrSCS24Hr | 0.34 | 91.73 | 91.99 | 91.95 | 92.03 | 0.010714 | 0.88 | 0.39 | 2.32 | 0.69 |
| Reach 1-Upper | 197 | 50YrSCS24Hr | 0.40 | 91.73 | 92.01 | 91.96 | 92.05 | 0.010482 | 0.92 | 0.44 | 2.41 | 0.69 |
| Reach 1-Upper | 197 | 100YrSCS24Hr | 0.47 | 91.73 | 92.03 | 91.98 | 92.08 | 0.010295 | 0.95 | 0.49 | 2.51 | 0.69 |
| Reach 1-Upper | 174 | 2YrCHI3Hr | 0.09 | 91.52 | 91.70 | 91.64 | 91.71 | 0.004240 | 0.42 | 0.20 | 1.84 | 0.40 |
| Reach 1-Upper | 174 | 5YrCHI3Hr | 0.15 | 91.52 | 91.75 | 91.67 | 91.76 | 0.004464 | 0.50 | 0.30 | 2.18 | 0.43 |
| Reach 1-Upper | 174 | 10YrCHI3Hr | 0.20 | 91.52 | 91.78 | 91.70 | 91.79 | 0.004630 | 0.55 | 0.36 | 2.30 | 0.45 |
| Reach 1-Upper | 174 | 25YrCHI3Hr | 0.26 | 91.52 | 91.81 | 91.72 | 91.82 | 0.004764 | 0.60 | 0.43 | 2.46 | 0.46 |
| Reach 1-Upper | 174 | 50YrCHI3Hr | 0.31 | 91.52 | 91.83 | 91.74 | 91.85 | 0.004920 | 0.64 | 0.48 | 2.56 | 0.47 |
| Reach 1-Upper | 174 | 100YrCHI3Hr | 0.37 | 91.52 | 91.85 | 91.76 | 91.87 | 0.005045 | 0.68 | 0.54 | 2.67 | 0.48 |
| Reach 1-Upper | 174 | 2YrSCS24Hr | 0.13 | 91.52 | 91.74 | 91.67 | 91.75 | 0.004376 | 0.48 | 0.27 | 2.09 | 0.42 |
| Reach 1-Upper | 174 | 5YrSCS24Hr | 0.21 | 91.52 | 91.78 | 91.70 | 91.80 | 0.004673 | 0.56 | 0.37 | 2.34 | 0.45 |
| Reach 1-Upper | 174 | 10YrSCS24Hr | 0.27 | 91.52 | 91.81 | 91.72 | 91.83 | 0.004791 | 0.61 | 0.44 | 2.47 | 0.46 |
| Reach 1-Upper | 174 | 25YrSCS24Hr | 0.34 | 91.52 | 91.84 | 91.75 | 91.86 | 0.004993 | 0.67 | 0.51 | 2.62 | 0.48 |

HEC-RAS Plan: 20250910-Post_Dev_v02 River: River 1 Reach: Reach 1-Upper (Continued)

| Reach | River Sta | Profile | Q Total (m3/s) | Min Ch El (m) | W.S. Elev (m) | Crit W.S. (m) | E.G. Elev (m) | E.G. Slope (m/m) | Vel Chnl (m/s) | Flow Area (m2) | Top Width (m) | Froude # Chl |
|---------------|-----------|--------------|-------------------|------------------|------------------|------------------|------------------|---------------------|-------------------|-------------------|------------------|--------------|
| Reach 1-Upper | 174 | 50YrSCS24Hr | 0.40 | 91.52 | 91.86 | 91.77 | 91.89 | 0.005106 | 0.70 | 0.57 | 2.72 | 0.49 |
| Reach 1-Upper | 174 | 100YrSCS24Hr | 0.47 | 91.52 | 91.88 | 91.78 | 91.91 | 0.005150 | 0.73 | 0.63 | 2.83 | 0.50 |
| Reach 1-Upper | 154 | 2YrCHI3Hr | 0.09 | 91.43 | 91.62 | 91.56 | 91.63 | 0.004316 | 0.40 | 0.22 | 2.21 | 0.40 |
| Reach 1-Upper | 154 | 5YrCHI3Hr | 0.15 | 91.43 | 91.66 | 91.59 | 91.67 | 0.004196 | 0.46 | 0.33 | 2.61 | 0.41 |
| Reach 1-Upper | 154 | 10YrCHI3Hr | 0.20 | 91.43 | 91.69 | 91.61 | 91.70 | 0.004192 | 0.49 | 0.40 | 2.83 | 0.42 |
| Reach 1-Upper | 154 | 25YrCHI3Hr | 0.26 | 91.43 | 91.72 | 91.63 | 91.74 | 0.004098 | 0.53 | 0.49 | 3.08 | 0.42 |
| Reach 1-Upper | 154 | 50YrCHI3Hr | 0.31 | 91.43 | 91.74 | 91.65 | 91.76 | 0.004007 | 0.55 | 0.56 | 3.25 | 0.43 |
| Reach 1-Upper | 154 | 100YrCHI3Hr | 0.37 | 91.43 | 91.77 | 91.67 | 91.78 | 0.003907 | 0.58 | 0.64 | 3.40 | 0.43 |
| Reach 1-Upper | 154 | 2YrSCS24Hr | 0.13 | 91.43 | 91.65 | 91.58 | 91.66 | 0.004250 | 0.44 | 0.29 | 2.50 | 0.41 |
| Reach 1-Upper | 154 | 5YrSCS24Hr | 0.21 | 91.43 | 91.70 | 91.62 | 91.71 | 0.004172 | 0.50 | 0.42 | 2.89 | 0.42 |
| Reach 1-Upper | 154 | 10YrSCS24Hr | 0.27 | 91.43 | 91.72 | 91.64 | 91.74 | 0.004085 | 0.53 | 0.50 | 3.11 | 0.42 |
| Reach 1-Upper | 154 | 25YrSCS24Hr | 0.34 | 91.43 | 91.76 | 91.66 | 91.77 | 0.003951 | 0.57 | 0.60 | 3.33 | 0.43 |
| Reach 1-Upper | 154 | 50YrSCS24Hr | 0.40 | 91.43 | 91.78 | 91.67 | 91.80 | 0.003859 | 0.59 | 0.68 | 3.48 | 0.43 |
| Reach 1-Upper | 154 | 100YrSCS24Hr | 0.47 | 91.43 | 91.80 | 91.69 | 91.82 | 0.003775 | 0.61 | 0.76 | 3.63 | 0.43 |
| Reach 1-Upper | 137 | 2YrCHI3Hr | 0.09 | 91.33 | 91.49 | 91.46 | 91.51 | 0.011391 | 0.63 | 0.14 | 1.43 | 0.65 |
| Reach 1-Upper | 137 | 5YrCHI3Hr | 0.15 | 91.33 | 91.53 | 91.50 | 91.56 | 0.011329 | 0.73 | 0.20 | 1.66 | 0.67 |
| Reach 1-Upper | 137 | 10YrCHI3Hr | 0.20 | 91.33 | 91.56 | 91.52 | 91.59 | 0.011021 | 0.78 | 0.25 | 1.80 | 0.67 |
| Reach 1-Upper | 137 | 25YrCHI3Hr | 0.26 | 91.33 | 91.59 | 91.55 | 91.63 | 0.010598 | 0.84 | 0.31 | 1.97 | 0.67 |
| Reach 1-Upper | 137 | 50YrCHI3Hr | 0.31 | 91.33 | 91.62 | 91.57 | 91.65 | 0.010270 | 0.87 | 0.36 | 2.09 | 0.67 |
| Reach 1-Upper | 137 | 100YrCHI3Hr | 0.37 | 91.33 | 91.64 | 91.58 | 91.68 | 0.009883 | 0.90 | 0.41 | 2.22 | 0.67 |
| Reach 1-Upper | 137 | 2YrSCS24Hr | 0.13 | 91.33 | 91.52 | 91.49 | 91.55 | 0.011458 | 0.71 | 0.18 | 1.59 | 0.67 |
| Reach 1-Upper | 137 | 5YrSCS24Hr | 0.21 | 91.33 | 91.57 | 91.53 | 91.60 | 0.010925 | 0.80 | 0.26 | 1.84 | 0.67 |
| Reach 1-Upper | 137 | 10YrSCS24Hr | 0.27 | 91.33 | 91.60 | 91.55 | 91.63 | 0.010544 | 0.84 | 0.32 | 1.99 | 0.67 |
| Reach 1-Upper | 137 | 25YrSCS24Hr | 0.34 | 91.33 | 91.63 | 91.58 | 91.67 | 0.010099 | 0.89 | 0.39 | 2.16 | 0.67 |
| Reach 1-Upper | 137 | 50YrSCS24Hr | 0.40 | 91.33 | 91.65 | 91.60 | 91.69 | 0.009709 | 0.91 | 0.44 | 2.29 | 0.66 |
| Reach 1-Upper | 137 | 100YrSCS24Hr | 0.47 | 91.33 | 91.68 | 91.61 | 91.72 | 0.009370 | 0.93 | 0.50 | 2.42 | 0.66 |
| Reach 1-Upper | 116 | 2YrCHI3Hr | 0.09 | 91.23 | 91.38 | 91.32 | 91.39 | 0.003211 | 0.37 | 0.23 | 2.08 | 0.35 |
| Reach 1-Upper | 116 | 5YrCHI3Hr | 0.15 | 91.23 | 91.44 | 91.35 | 91.44 | 0.002924 | 0.42 | 0.35 | 2.37 | 0.35 |
| Reach 1-Upper | 116 | 10YrCHI3Hr | 0.20 | 91.23 | 91.47 | 91.37 | 91.48 | 0.002866 | 0.46 | 0.43 | 2.54 | 0.36 |
| Reach 1-Upper | 116 | 25YrCHI3Hr | 0.26 | 91.23 | 91.50 | 91.39 | 91.52 | 0.002818 | 0.49 | 0.53 | 2.75 | 0.36 |
| Reach 1-Upper | 116 | 50YrCHI3Hr | 0.31 | 91.23 | 91.53 | 91.41 | 91.54 | 0.002810 | 0.52 | 0.60 | 2.89 | 0.36 |
| Reach 1-Upper | 116 | 100YrCHI3Hr | 0.37 | 91.23 | 91.56 | 91.42 | 91.57 | 0.002804 | 0.54 | 0.68 | 3.03 | 0.37 |
| Reach 1-Upper | 116 | 2YrSCS24Hr | 0.13 | 91.23 | 91.42 | 91.34 | 91.43 | 0.002958 | 0.41 | 0.32 | 2.29 | 0.35 |
| Reach 1-Upper | 116 | 5YrSCS24Hr | 0.21 | 91.23 | 91.48 | 91.37 | 91.49 | 0.002849 | 0.47 | 0.45 | 2.59 | 0.36 |
| Reach 1-Upper | 116 | 10YrSCS24Hr | 0.27 | 91.23 | 91.51 | 91.39 | 91.52 | 0.002820 | 0.50 | 0.54 | 2.77 | 0.36 |
| Reach 1-Upper | 116 | 25YrSCS24Hr | 0.34 | 91.23 | 91.54 | 91.41 | 91.56 | 0.002805 | 0.53 | 0.64 | 2.96 | 0.37 |
| Reach 1-Upper | 116 | 50YrSCS24Hr | 0.40 | 91.23 | 91.57 | 91.43 | 91.59 | 0.002678 | 0.55 | 0.73 | 3.11 | 0.36 |
| Reach 1-Upper | 116 | 100YrSCS24Hr | 0.47 | 91.23 | 91.60 | 91.45 | 91.62 | 0.002583 | 0.57 | 0.82 | 3.24 | 0.36 |
| Reach 1-Upper | 95 | 2YrCHI3Hr | 0.09 | 91.07 | 91.29 | 91.23 | 91.30 | 0.006154 | 0.52 | 0.16 | 1.38 | 0.48 |
| Reach 1-Upper | 95 | 5YrCHI3Hr | 0.15 | 91.07 | 91.33 | 91.27 | 91.35 | 0.006882 | 0.63 | 0.24 | 1.61 | 0.53 |
| Reach 1-Upper | 95 | 10YrCHI3Hr | 0.20 | 91.07 | 91.36 | 91.30 | 91.39 | 0.007544 | 0.71 | 0.28 | 1.73 | 0.56 |
| Reach 1-Upper | 95 | 25YrCHI3Hr | 0.26 | 91.07 | 91.39 | 91.33 | 91.42 | 0.007915 | 0.77 | 0.34 | 1.88 | 0.58 |
| Reach 1-Upper | 95 | 50YrCHI3Hr | 0.31 | 91.07 | 91.41 | 91.35 | 91.45 | 0.008499 | 0.83 | 0.37 | 1.97 | 0.61 |
| Reach 1-Upper | 95 | 100YrCHI3Hr | 0.37 | 91.07 | 91.43 | 91.37 | 91.47 | 0.009495 | 0.90 | 0.41 | 2.07 | 0.65 |
| Reach 1-Upper | 95 | 2YrSCS24Hr | 0.13 | 91.07 | 91.32 | 91.26 | 91.34 | 0.006702 | 0.60 | 0.21 | 1.55 | 0.52 |
| Reach 1-Upper | 95 | 5YrSCS24Hr | 0.21 | 91.07 | 91.37 | 91.30 | 91.39 | 0.007595 | 0.72 | 0.29 | 1.76 | 0.57 |
| Reach 1-Upper | 95 | 10YrSCS24Hr | 0.27 | 91.07 | 91.39 | 91.33 | 91.43 | 0.008212 | 0.79 | 0.34 | 1.88 | 0.60 |
| Reach 1-Upper | 95 | 25YrSCS24Hr | 0.34 | 91.07 | 91.42 | 91.36 | 91.46 | 0.008586 | 0.86 | 0.40 | 2.03 | 0.62 |
| Reach 1-Upper | 95 | 50YrSCS24Hr | 0.40 | 91.07 | 91.39 | 91.38 | 91.46 | 0.019163 | 1.20 | 0.33 | 1.87 | 0.91 |
| Reach 1-Upper | 95 | 100YrSCS24Hr | 0.47 | 91.07 | 91.40 | 91.40 | 91.49 | 0.023191 | 1.34 | 0.35 | 1.90 | 1.00 |
| Reach 1-Upper | 72 | 2YrCHI3Hr | 0.09 | 90.91 | 91.00 | 91.00 | 91.03 | 0.030446 | 0.75 | 0.12 | 1.98 | 0.99 |
| Reach 1-Upper | 72 | 5YrCHI3Hr | 0.15 | 90.91 | 91.03 | 91.03 | 91.07 | 0.029306 | 0.85 | 0.18 | 2.40 | 1.01 |
| Reach 1-Upper | 72 | 10YrCHI3Hr | 0.20 | 90.91 | 91.05 | 91.05 | 91.09 | 0.027108 | 0.89 | 0.22 | 2.63 | 0.99 |
| Reach 1-Upper | 72 | 25YrCHI3Hr | 0.26 | 90.91 | 91.06 | 91.06 | 91.11 | 0.027545 | 0.98 | 0.27 | 2.80 | 1.02 |
| Reach 1-Upper | 72 | 50YrCHI3Hr | 0.31 | 90.91 | 91.08 | 91.08 | 91.13 | 0.025861 | 1.01 | 0.31 | 2.94 | 1.00 |
| Reach 1-Upper | 72 | 100YrCHI3Hr | 0.37 | 90.91 | 91.10 | 91.09 | 91.15 | 0.022250 | 1.01 | 0.36 | 3.09 | 0.95 |
| Reach 1-Upper | 72 | 2YrSCS24Hr | 0.13 | 90.91 | 91.02 | 91.02 | 91.06 | 0.029339 | 0.82 | 0.16 | 2.29 | 1.00 |
| Reach 1-Upper | 72 | 5YrSCS24Hr | 0.21 | 90.91 | 91.05 | 91.05 | 91.09 | 0.027610 | 0.92 | 0.23 | 2.67 | 1.00 |
| Reach 1-Upper | 72 | 10YrSCS24Hr | 0.27 | 90.91 | 91.07 | 91.07 | 91.12 | 0.025875 | 0.97 | 0.28 | 2.84 | 0.99 |
| Reach 1-Upper | 72 | 25YrSCS24Hr | 0.34 | 90.91 | 91.09 | 91.09 | 91.14 | 0.025973 | 1.05 | 0.33 | 2.99 | 1.01 |
| Reach 1-Upper | 72 | 50YrSCS24Hr | 0.40 | 90.91 | 91.15 | 91.10 | 91.18 | 0.008061 | 0.73 | 0.55 | 3.56 | 0.59 |
| Reach 1-Upper | 72 | 100YrSCS24Hr | 0.47 | 90.91 | 91.22 | 91.11 | 91.24 | 0.003417 | 0.57 | 0.82 | 4.07 | 0.40 |

APPENDIX H CITY OF OTTAWA DESIGN CHECKLIST

4. Development Servicing Study Checklist

The following section describes the checklist of the required content of servicing studies. It is expected that the proponent will address each one of the following items for the study to be deemed complete and ready for review by City of Ottawa Infrastructure Approvals staff.

The level of required detail in the Servicing Study will increase depending on the type of application. For example, for Official Plan amendments and re-zoning applications, the main issues will be to determine the capacity requirements for the proposed change in land use and confirm this against the existing capacity constraint, and to define the solutions, phasing of works and the financing of works to address the capacity constraint. For subdivisions and site plans, the above will be required with additional detailed information supporting the servicing within the development boundary.

4.1 General Content

| Criteria | Location (if applicable) |
|---|---|
| <input type="checkbox"/> Executive Summary (for larger reports only). | N/A |
| <input type="checkbox"/> Date and revision number of the report. | On Cover |
| <input type="checkbox"/> Location map and plan showing municipal address, boundary, and layout of proposed development. | Appendix A |
| <input type="checkbox"/> Plan showing the site and location of all existing services. | Site Servicing Plan (C102) |
| <input type="checkbox"/> Development statistics, land use, density, adherence to zoning and official plan, and reference to applicable subwatershed and watershed plans that provide context to which individual developments must adhere. | 1.1 Purpose 1.2 Site Description 6.0 Proposed Stormwater Management |
| <input type="checkbox"/> Summary of pre-consultation meetings with City and other approval agencies. | Appendix B |
| <input type="checkbox"/> Reference and confirm conformance to higher level studies and reports (Master Servicing Studies, Environmental Assessments, Community Design Plans), or in the case where it is not in conformance, the proponent must provide justification and develop a defensible design criteria. | 1.1 Purpose 1.2 Site Description 6.0 Proposed Stormwater Management |
| <input type="checkbox"/> Statement of objectives and servicing criteria. | 3.0 Pre-Consultation Summary |

| | |
|---|--|
| <input type="checkbox"/> Identification of existing and proposed infrastructure available in the immediate area. | N/ A |
| <input type="checkbox"/> Identification of Environmentally Significant Areas, watercourses and Municipal Drains potentially impacted by the proposed development (Reference can be made to the Natural Heritage Studies, if available). | Ste Grading Plan (C101) |
| <input type="checkbox"/> Concept level master grading plan to confirm existing and proposed grades in the development. This is required to confirm the feasibility of proposed stormwater management and drainage, soil removal and fill constraints, and potential impacts to neighbouring properties. This is also required to confirm that the proposed grading will not impede existing major system flow paths. | Ste Grading Plan (C101) |
| <input type="checkbox"/> Identification of potential impacts of proposed piped services on private services (such as wells and septic fields on adjacent lands) and mitigation required to address potential impacts. | N/ A |
| <input type="checkbox"/> Proposed phasing of the development, if applicable. | N/ A |
| <input type="checkbox"/> Reference to geotechnical studies and recommendations concerning servicing. | Section 2.0 Background Studies, Standards and References |
| <input type="checkbox"/> All preliminary and formal site plan submissions should have the following information: <ul style="list-style-type: none"> ○ Metric scale ○ North arrow (including construction North) ○ Key plan ○ Name and contact information of applicant and property owner ○ Property limits including bearings and dimensions ○ Existing and proposed structures and parking areas ○ Easements, road widening and rights-of-way ○ Adjacent street names | Ste Grading Plan (C101) |

4.2 Development Servicing Report: Water

| Criteria | Location (if applicable) |
|---|--|
| <input type="checkbox"/> Confirm consistency with Master Servicing Study, if available | N/ A |
| <input type="checkbox"/> Availability of public infrastructure to service proposed development | N/ A |
| <input type="checkbox"/> Identification of system constraints | N/ A |
| <input type="checkbox"/> Identify boundary conditions | Appendix C |
| <input type="checkbox"/> Confirmation of adequate domestic supply and pressure | N/ A |
| <input type="checkbox"/> Confirmation of adequate fire flow protection and confirmation that fire flow is calculated as per the Fire Underwriter's Survey. Output should show available fire flow at locations throughout the development. | Appendix C |
| <input type="checkbox"/> Provide a check of high pressures. If pressure is found to be high, an assessment is required to confirm the application of pressure reducing valves. | N/ A |
| <input type="checkbox"/> Definition of phasing constraints. Hydraulic modeling is required to confirm servicing for all defined phases of the project including the ultimate design | N/ A |
| <input type="checkbox"/> Address reliability requirements such as appropriate location of shut-off valves | N/ A |
| <input type="checkbox"/> Check on the necessity of a pressure zone boundary modification. | N/ A |
| <input type="checkbox"/> Reference to water supply analysis to show that major infrastructure is capable of delivering sufficient water for the proposed land use. This includes data that shows that the expected demands under average day, peak hour and fire flow conditions provide water within the required pressure range | Appendix C, Section 4.2 Proposed Water Servicing |

| | |
|---|----------------------------|
| <input type="checkbox"/> Description of the proposed water distribution network, including locations of proposed connections to the existing system, provisions for necessary looping, and appurtenances (valves, pressure reducing valves, valve chambers, and fire hydrants) including special metering provisions. | Site Servicing Plan (C101) |
| <input type="checkbox"/> Description of off-site required feeder mains, booster pumping stations, and other water infrastructure that will be ultimately required to service proposed development, including financing, interim facilities, and timing of implementation. | N/A |
| <input type="checkbox"/> Confirmation that water demands are calculated based on the City of Ottawa Design Guidelines. | Appendix C |
| <input type="checkbox"/> Provision of a model schematic showing the boundary conditions locations, streets, parcels, and building locations for reference. | N/A |

4.3 Development Servicing Report: Wastewater

| Criteria | Location (if applicable) |
|--|---|
| <input type="checkbox"/> Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitored flow data from relatively new infrastructure cannot be used to justify capacity requirements for proposed infrastructure). | N/A |
| <input type="checkbox"/> Confirm consistency with Master Servicing Study and/or justifications for deviations. | N/A |
| <input type="checkbox"/> Consideration of local conditions that may contribute to extraneous flows that are higher than the recommended flows in the guidelines. This includes groundwater and soil conditions, and age and condition of sewers. | N/A |
| <input type="checkbox"/> Description of existing sanitary sewer available for discharge of wastewater from proposed development. | Section 5.2 Proposed Sanitary Servicing |

| | |
|---|---|
| <input type="checkbox"/> Verify available capacity in downstream sanitary sewer and/or identification of upgrades necessary to service the proposed development. (Reference can be made to previously completed Master Servicing Study if applicable) | Section 5.2 Proposed Sanitary Servicing |
| <input type="checkbox"/> Calculations related to dry-weather and wet-weather flow rates from the development in standard MOE sanitary sewer design table (Appendix 'C') format. | N/ A |
| <input type="checkbox"/> Description of proposed sewer network including sewers, pumping stations, and forcemains. | Section 5.2 Proposed Sanitary Servicing |
| <input type="checkbox"/> Discussion of previously identified environmental constraints and impact on servicing (environmental constraints are related to limitations imposed on the development in order to preserve the physical condition of watercourses, vegetation, soil cover, as well as protecting against water quantity and quality). | N/ A |
| <input type="checkbox"/> Pumping stations: impacts of proposed development on existing pumping stations or requirements for new pumping station to service development. | N/ A |
| <input type="checkbox"/> Forcemain capacity in terms of operational redundancy, surge pressure and maximum flow velocity. | N/ A |
| <input type="checkbox"/> Identification and implementation of the emergency overflow from sanitary pumping stations in relation to the hydraulic grade line to protect against basement flooding. | N/ A |
| <input type="checkbox"/> Special considerations such as contamination, corrosive environment etc. | N/ A |

4.4 Development Servicing Report: Stormwater Checklist

| Criteria | Location (if applicable) |
|---|--|
| <input type="checkbox"/> Description of drainage outlets and downstream constraints including legality of outlets (i.e. municipal drain, right-of-way, watercourse, or private property) | Section 6.0 Storm Sewer Servicing & Section 7.0 Proposed Stormwater Management |
| <input type="checkbox"/> Analysis of available capacity in existing public infrastructure. | N/A |
| <input type="checkbox"/> A drawing showing the subject lands, its surroundings, the receiving watercourse, existing drainage patterns, and proposed drainage pattern. | Pre & Post-Development Plans |
| <input type="checkbox"/> Water quantity control objective (e.g. controlling post-development peak flows to pre-development level for storm events ranging from the 2 or 5-year event (dependent on the receiving sewer design) to 100-year return period); if other objectives are being applied, a rationale must be included with reference to hydrologic analyses of the potentially affected subwatersheds, taking into account long-term cumulative effects. | Section 6.0 Storm Sewer Servicing & Section 7.0 Proposed Stormwater Management |
| <input type="checkbox"/> Water Quality control objective (basic, normal or enhanced level of protection based on the sensitivities of the receiving watercourse) and storage requirements. | Section 6.0 Storm Sewer Servicing & Section 7.0 Proposed Stormwater Management |
| <input type="checkbox"/> Description of the stormwater management concept with facility locations and descriptions with references and supporting information. | Section 6.0 Storm Sewer Servicing & Section 7.0 Proposed Stormwater Management |
| <input type="checkbox"/> Set-back from private sewage disposal systems. | N/A |
| <input type="checkbox"/> Watercourse and hazard lands setbacks. | N/A |
| <input type="checkbox"/> Record of pre-consultation with the Ontario Ministry of Environment and the Conservation Authority that has jurisdiction on the affected watershed. | N/A |
| <input type="checkbox"/> Confirm consistency with sub-watershed and Master Servicing Study, if applicable study exists. | N/A |
| <input type="checkbox"/> Storage requirements (complete with calculations) and conveyance capacity for minor events (1:5-year return period) and major events (1:100-year return period). | Appendix G |

| | |
|---|--|
| <input type="checkbox"/> Identification of watercourses within the proposed development and how watercourses will be protected, or, if necessary, altered by the proposed development with applicable approvals. | Site Grading Plan (C101) |
| <input type="checkbox"/> Calculate pre-and post development peak flow rates including a description of existing site conditions and proposed impervious areas and drainage catchments in comparison to existing conditions. | Appendix G, Section 7.0 Proposed Stormwater Management |
| <input type="checkbox"/> Any proposed diversion of drainage catchment areas from one outlet to another. | Section 6.0 Storm Sewer Servicing & Section 7.0 Proposed Stormwater Management |
| <input type="checkbox"/> Proposed minor and major systems including locations and sizes of stormwater trunk sewers, and stormwater management facilities. | Section 6.0 Storm Sewer Servicing & Section 7.0 Proposed Stormwater Management |
| <input type="checkbox"/> If quantity control is not proposed, demonstration that downstream system has adequate capacity for the post-development flows up to and including the 100-year return period storm event. | N/A |
| <input type="checkbox"/> Identification of potential impacts to receiving watercourses | N/A |
| <input type="checkbox"/> Identification of municipal drains and related approval requirements. | N/A |
| <input type="checkbox"/> Descriptions of how the conveyance and storage capacity will be achieved for the development. | Section 6.0 Storm Sewer Servicing & Section 7.0 Proposed Stormwater Management |
| <input type="checkbox"/> 100-year flood levels and major flow routing to protect proposed development from flooding for establishing minimum building elevations (MBE) and overall grading. | Site Grading Plan (C101) |
| <input type="checkbox"/> Inclusion of hydraulic analysis including hydraulic grade line elevations. | N/A |

| | |
|--|--|
| <input type="checkbox"/> Description of approach to erosion and sediment control during construction for the protection of receiving watercourse or drainage corridors. | Section 8.0 Sediment & Erosion Control |
| <input type="checkbox"/> Identification of floodplains – proponent to obtain relevant floodplain information from the appropriate Conservation Authority. The proponent may be required to delineate floodplain elevations to the satisfaction of the Conservation Authority if such information is not available or if information does not match current conditions. | N/ A |
| <input type="checkbox"/> Identification of fill constraints related to floodplain and geotechnical investigation. | N/ A |

4.5 Approval and Permit Requirements: Checklist

The Servicing Study shall provide a list of applicable permits and regulatory approvals necessary for the proposed development as well as the relevant issues affecting each approval. The approval and permitting shall include but not be limited to the following:

| Criteria | Location (if applicable) |
|---|--------------------------|
| <input type="checkbox"/> Conservation Authority as the designated approval agency for modification of floodplain, potential impact on fish habitat, proposed works in or adjacent to a watercourse, cut/fill permits and Approval under Lakes and Rivers Improvement Act. The Conservation Authority is not the approval authority for the Lakes and Rivers Improvement Act. Where there are Conservation Authority regulations in place, approval under the Lakes and Rivers Improvement Act is not required, except in cases of dams as defined in the Act. | N/ A |
| <input type="checkbox"/> Application for Certificate of Approval (CofA) under the Ontario Water Resources Act. | N/ A |
| <input type="checkbox"/> Changes to Municipal Drains. | N/ A |
| <input type="checkbox"/> Other permits (National Capital Commission, Parks Canada, Public Works and Government Services Canada, Ministry of Transportation etc.) | N/ A |

4.6 Conclusion Checklist

| Criteria | Location (if applicable) |
|--|---|
| <input type="checkbox"/> Clearly stated conclusions and recommendations | Section 9.0 Summary Section 10.0 Recommendations |
| <input type="checkbox"/> Comments received from review agencies including the City of Ottawa and information on how the comments were addressed. Final sign-off from the responsible reviewing agency. | All are stamped |
| <input type="checkbox"/> All draft and final reports shall be signed and stamped by a professional Engineer registered in Ontario | All are stamped |