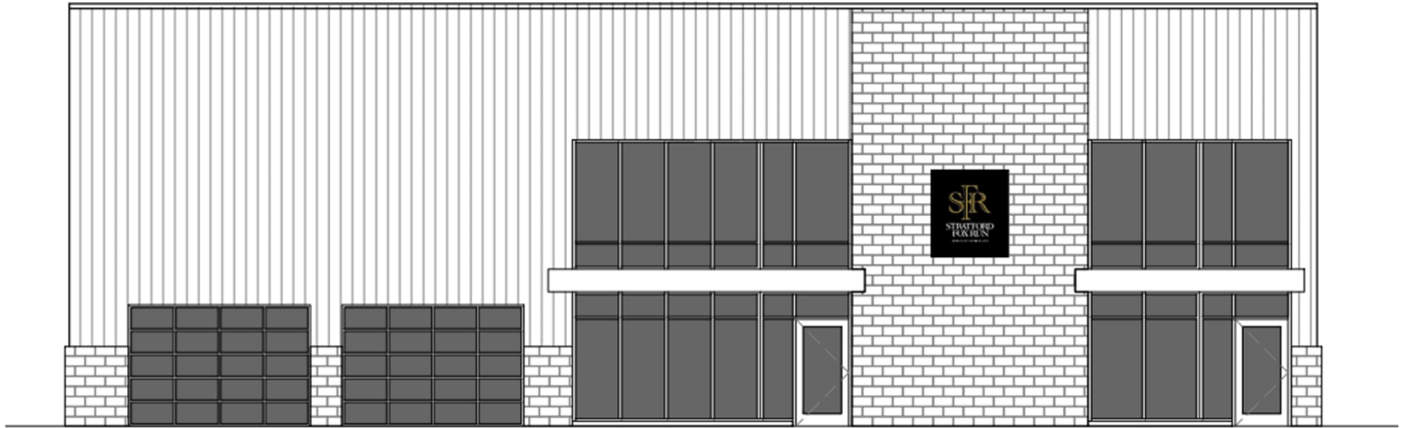


SERVICING & STORMWATER MANAGEMENT REPORT

DISTILLERY - 5923 OTTAWA STREET



Project No.: CCO-25-0415

City File No.:

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1.0 PROJECT DESCRIPTION

1.1 Purpose

Egis Canada (Egis) has been retained by 99117756 Canada Inc. to prepare this Servicing and Stormwater Management Report in support of the Site Plan Control process for the proposed development located at 5923 Ottawa Street within the City of Ottawa.

The main purpose of this report is to present a servicing design for the development in accordance with the recommendations and guidelines provided by the City of Ottawa (City), the Rideau Valley Conservation Authority (RVCA), and the Ministry of the Environment, Conservation and Parks (MECP). This report will address the water, sanitary, and storm sewer servicing for the development, ensuring that proposed services will adequately service the development.

This report should be read in conjunction with the following drawings:

- CCO-25-0415, C101 – Lot Grading and Drainage Plan,
- CCO-25-0415, C102 – Site Servicing Plan,
- CCO-25-0415, C103 – Erosion & Sediment Control Plan,
- CCO-25-0415, PRE – Pre-Development Drainage Area Plan (Appendix 'E'), and
- CCO-25-0415, POST – Post-Development Drainage Area Plan (Appendix 'F').

1.2 Site Description

Figure 1: Site Map



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The property is located at 5923 Ottawa Street within the City of Ottawa. It is described as Part of Unit 10, Index Plan D-26, geographic township of Goulbourn, City of Ottawa. The land in question covers approximately 2.27 ha and is located near the intersection of Ottawa Street and Eagleson Road. See Site Location Plan in Appendix 'A' for more details.

1.3 Proposed Development and Statistics

The proposed development consists of two phases. Phase 1 covers 1.17 ha and proposes a new 651 m² ground-floor area building with a distillery/warehouse, restaurant, and retail space. Phase 2 covers 1.10 ha and proposes a new 926 m² ground-floor area brewery building. Parking and drive aisles will be provided throughout each phase along with landscaping around the perimeter of the development area. The development will be accessed via the proposed site entrances from Ottawa Street.

1.4 Existing Conditions and Infrastructure

The existing site is currently undeveloped with no available municipal services. A municipal ditch fronts the subject site along Ottawa Street. The Smiths Falls Rail Corridor is located northwest of the subject site.

1.5 Approvals

The proposed development is subject to the City of Ottawa site plan control approval process. Site plan control requires the City to review, provide concurrence and approve the engineering design package. Permits to construct can be requested once the City has issued a site plan agreement.

An Environmental Compliance Approval (ECA) through the Ministry of Environment, Conservation and Parks (MECP) has been identified as a possible requirement within the Pre-Consultation notes provided by the City, based on the proposed industrial usage of the site. The requirement for an ECA will be confirmed prior to approval. Should an ECA be required, construction cannot begin until the ECA is approved.

2.0 BACKGROUND STUDIES, STANDARDS, AND REFERENCES

2.1 Background Reports / Reference Information

Background studies that have been completed for the proposed site include a topographical survey and a geotechnical report.

The topographic survey of the site was completed by Egis Canada Ltd and dated July 9, 2024.

The following reports have previously been completed and are available under separate cover:

- Geotechnical Investigation, Proposed Commercial Development, completed by Paterson Group, dated May 6, 2025.

- Ditch Hydrologic and Hydraulic Analysis, completed by JFSA, dated June 05, 2025
- Sewage System Layout Plan, Drawing PH4924-1 (rev.3), completed by Paterson Group, Dated June, 2025
- Village of Richmond Environmental Management Plan, dated June 17, 2010.

2.2 Applicable Guidelines and Standards

City of Ottawa:

- ◆ Ottawa Sewer Design Guidelines, City of Ottawa, SDG002, October 2012. (Ottawa Sewer Guidelines)
 - Technical Bulletin ISTB-2014-01 City of Ottawa, February 2014. (ISTB-2014-01)
 - Technical Bulletin PIETB-2016-01 City of Ottawa, September 2016. (PIETB-2016-01)
 - Technical Bulletin ISTB-2018-01 City of Ottawa, January 2018. (ISTB-2018-01)
 - Technical Bulletin ISTB-2018-04 City of Ottawa, March 2018. (ISTB-2018-04)
 - Technical Bulletin ISTB-2019-02 City of Ottawa, February 2019. (ISTB-2019-02)
 - Technical Bulletin IWSB-2024-04 City of Ottawa, September 2024. (ISTB-2024-04)
- ◆ Ottawa Design Guidelines – Water Distribution City of Ottawa, July 2010. (Ottawa Water Guidelines)
 - Technical Bulletin ISD-2010-2 City of Ottawa, December 15, 2010. (ISD-2010-2)
 - Technical Bulletin ISDTB-2014-02 City of Ottawa, May 2014. (ISDTB-2014-02)
 - Technical Bulletin ISTB-2018-02 City of Ottawa, March 2018. (ISTB-2018-02)
 - Technical Bulletin ISTB-2021-03 City of Ottawa, August 2021. (ISTB-2021-03)
 - Technical Bulletin IWSB-2024-05 City of Ottawa, November 2024. (IWSB-2024-05)

Ministry of Environment, Conservation and Parks:

- ◆ Stormwater Planning and Design Manual, Ministry of the Environment, March 2003. (MECP Stormwater Design Manual)
- ◆ Design Guidelines for Sewage Works, Ministry of the Environment, 2008. (MECP Sewer Design Guidelines)

Other:

- ◆ Water Supply for Public Fire Protection, Fire Underwriters Survey, 2020. (FUS Guidelines)

3.0 PRE-CONSULTATION SUMMARY

A pre-consultation meeting was conducted on March 21st, 2024, regarding the proposed site. Specific design parameters to be incorporated within this design include the following:

- Control post-development flows to the 2-year pre-development peak flow rate with $C=0.5$ or existing, whichever is lesser, for all storms up to and including the 100-year storm event.
- Quality control to be provided up to an enhanced level of treatment (80% TSS Removal).

The notes from the City of Ottawa can be found in Appendix 'B'.

4.0 WATER SERVICING

4.1 Existing Watermain

The subject site is currently undeveloped with no access to a municipal watermain. Neighbouring properties are serviced by private wells.

4.2 Proposed Water Servicing

A new private drilled well and pump system is proposed within each phase to provide the development with domestic water supply. The wells, which will be designed and specified by others, will be included on the Servicing Plan once the location has been confirmed. As the development will be phased, it is proposed to temporarily service the Phase 2 building via the Phase 1 well. After the Phase 2 well is drilled, the service from the Phase 1 well will be abandoned and both buildings will be independently serviced.

Fire protection is proposed to be provided by a remote fire protection system comprised of underground water storage tank(s), a dry hydrant, and a 150 mm diameter private watermain. The proposed Phase 1 building will be equipped with fully supervised sprinkler system supplied by underground water storage tank(s). The "Fully Supervised" sprinkler systems require a supervisory signal to indicate conditions that could impair the operation of the system, as well as a water flow alarm to indicate the sprinkler system has been activated. The alarms must be sent to approved receiving facilities identified by the Fire Underwriters Survey. A sprinkler system is not proposed within the Phase 2 Building.

Based on direction from Ottawa Fire Services, the Ontario Building Code method and NFPA13 method fire flow calculations must be provided to determine the required fire flow for the Phase 1 building. Per IWSB-2024-05, the fire flow requirement for the Phase 2 building will be based on the OBC method if the required fire flow is less than 9,000 L/min. Calculations based on the OBC method are included below. NFPA13 calculations will be provided when a mechanical engineer has joined the project team.

The 'K' factor (Water Supply Coefficient) for the OBC calculation was determined to be 17 for both buildings, based on a Medium-Hazard Industrial occupancy and non-combustible construction with fire separations and fire-resistance ratings provided in accordance with subsections 3.2.2., including loadbearing walls, columns, and arches. The Phase 1 and Phase 2 building volumes are 4,125 m³ and 7,200 m³, respectively. These inputs were confirmed through correspondence with the Architect.

The 'K' factor considers both the construction and general usage of the building to determine the additional volume of water that should be provided. In the case of the proposed restaurant/distillery and brewery buildings, the 'K' factor is based on the Medium-Hazard Industrial usage of the distillery and brewery, as the combustible contents found therein will necessitate a greater volume of water for firefighting than the restaurant or office uses.

The results of the OBC calculations yielded a required fire flow of 2,700 L/min, and a required on-site storage volume of 77,138 L for Phase 1. The results of the OBC calculations yielded a required fire flow of 3,600 L/min, and a required on-site storage volume of 122,400 L for Phase 2. The detailed calculations for the OBC can be found in Appendix 'C'.

As Ottawa Fire Services is Superior Tanker Shuttle Service accredited to provide 1,900 L/min for commercial lines, a reduction in the required storage volume of up to 57,000 L (1,900 L/min x 30 min) may apply. For this requirement to apply, the required fire flow must be less than or equal to 4,500 L/min. It should however be noted that the minimum tank size for on-site storage is 38,000 L.

The required on-site storage volume for Phase 2 has therefore been determined as (122,400 L – 57,000 L) = 65,400 Litres. The required on-site storage volume for Phase 1 will be confirmed with Ottawa Fire Services once the water demand for the Phase 1 sprinkler system is known, and NFPA13 calculations are provided. On-site storage for Phase 1 is proposed to be provided by underground concrete water storage tanks connected to both a dry hydrant and the building sprinkler system. On-site storage for Phase 2 is proposed to be provided by an underground concrete storage tank with a draw pipe and chute as per City of Ottawa Figure 5, Figure 10, and standard drawings W51 and W52.

As the site contains high groundwater, the underground water storage tanks will need to be reviewed for buoyancy once shop drawings are received. Measures to mitigate buoyancy, if needed, might include the use of ballast blocks, a concrete cap, or a deeper burial depth.

Although the building will be serviced via a drilled well and pump system as described above, water demands based on occupancy areas are provided below for information purposes only. The water demands have been calculated to adhere to the Ottawa Design Guidelines – Water Distribution manual and can be found in Appendix 'C'.

Table 1: Water Supply Design Criteria and Water Demands

Proposed Development	Phase 1	Phase 2
Site Area	1.17 ha	1.10 ha
Commercial	28,000 L/gross ha/day	
Commercial Peaking Factor (Max Day)	1.5 x avg. day	
Commercial Peaking Factor (Peak Hour)	1.8 x max. day	
Industrial	35,000 L/gross ha/day	

Industrial Peaking Factor (Max Day)	1.5 x avg. day	
Industrial Peaking Factor (Peak Hour)	1.8 x max. day	
Average Day Demand (L/s)	0.02	0.04
Maximum Daily Demand (L/s)	0.04	0.06
Peak Hourly Demand (L/s)	0.06	0.11
OBC Fire Flow Requirement (L/s)	45 (2,700 L/min)	60 (3,600 L/min)
NFPA13 Fire Flow Requirement (L/s)	To be confirmed	N/A
On-Site Water Storage Requirement (L)	To be confirmed	65,400

Detailed water demand and fire flow calculations can be found in Appendix 'C'.

5.0 SANITARY SERVICING

5.1 Existing Sanitary Sewers

The subject site is currently undeveloped with no access to a municipal sanitary sewer. Neighbouring properties are serviced by private septic systems.

5.2 Proposed Sanitary Servicing

A new septic bed located north of the proposed buildings will be installed for each phase and sized to accommodate the development.

Total Daily Design Sanitary Sewage Flow (TDDSSF) for Phases 1 and 2 was calculated by Paterson as 9,367 L/day and 600 L/day, respectively, when balanced over 7 days. It is understood that approval of on-site septic treatment will be governed by OBC, as the Daily Design Flow for each system will be less than 10,000 L/day. Refer to the septic design completed by Paterson Group, which will be submitted to the Ottawa Septic System Office (OSSO) for the required permits and approvals.

In summary, both the Phase 1 and Phase 2 systems have been designed using Class 4 raised leaching beds in combination with an Ejjen GSF treatment system.

Phase 1 will treat up to 9,367 L/day of Effluent. The Phase 1 system will include a 28,101 L pretreatment tank and an 18,500 L balancing tank complete with a time operated control panel. The sanitary service exiting the building will be 100 mm diameter and sleeved through a 150 mm diameter pipe overlain by rigid insulation boards.

Phase 2 will treat up to 600 L/day of Effluent. The Phase 2 system will include a 3,600 L pretreatment tank and a 450 L balancing tank complete with a time operated control panel. The sanitary service exiting the building will be 100 mm diameter and sleeved through a 150 mm diameter pipe overlain by rigid insulation boards.

For further design information pertaining to the on-site sewage system, please refer to the septic design completed by Paterson Group.

Although the building will be serviced via a septic system as described above, sanitary demands based on occupancy areas are provided below for information purposes only. The sanitary demands have been calculated to adhere to the Ottawa Sewer Design Guidelines and can be found in Appendix 'C'. To remain conservative, the restaurant area for Phase 1 has been increased to account for outdoor patio seating. The development area was considered instead of the property area to provide a more reasonable infiltration allowance estimate. Sanitary Demand Criteria are listed in Table 2, below.

Table 2: Sanitary Design Criteria

Design Parameter	Value
Phase 1 Development Area	0.48 ha
Phase 2 Development Area	0.45 ha
Commercial Area	280 L/person/day
Industrial – Light Area	35,000 L/gross ha/d
Restaurant Area	125 L/ (9.2 m ² /d)
Institutional/Commercial Peaking Factor	1.5
Extraneous Flow Allowance	0.33 L/s/ha

Table 3, below, summarizes the estimated wastewater flow from the proposed development. Refer to Appendix 'D' for detailed calculations.

Table 3: Summary of Estimated Sanitary Flow

Design Parameter	Total Flow (L/s)	
	Phase 1	Phase 2
Total Estimated Average Dry Weather Flow	0.10	0.04
Total Estimated Peak Dry Weather Flow	0.14	0.05
Total Estimated Peak Wet Weather Flow	0.27	0.17

As mentioned above, sanitary demand calculations based on the Ottawa Sewer Design Guidelines are provided for information only. The sanitary design and septic demand will be completed by Paterson Group based on Ontario Building Code requirements.

6.0 STORM SEWER SERVICING

6.1 Existing Storm Sewers

There are no existing storm sewers within the subject site or the adjacent municipal ROW. A municipal ditch fronts the subject site along Ottawa Street. A secondary ditch runs along the south of the Smiths Falls Rail Corridor at the rear of the site.

6.2 Proposed Storm Servicing

Runoff collected on the roof of the proposed Phase 1 and 2 buildings will be stored and controlled using flow restricting roof drains. Surface runoff from landscaped areas will be conveyed towards depressed surface storage areas located within the front yard of each phase. One minimum sized orifice for each phase will be used to direct controlled runoff from the surface storage areas to the municipal ditch along Ottawa Street during smaller storm events, while runoff exceeding the release rate of the orifices will be stored within the depressed surface storage areas. A weir is proposed for each surface storage area to permit greater flow during larger events.

Runoff will be directed towards oil and grit separator units before discharging to the municipal ditch along Ottawa Street.

See CCO-25-0415 - POST in Appendix 'F' of this report and drawing C102 for more details. The Stormwater Management design for the subject property will be outlined in Section 7.0.

7.0 PROPOSED STORMWATER MANAGEMENT

7.1 Design Criteria

Stormwater management for the proposed site will be maintained through positive drainage away from the proposed building and towards the proposed depressed surface storage areas. The proposed stormwater management areas will capture and restrict runoff to the greatest extent possible during smaller storm events with the use of minimum sized orifices. During larger storm events, a weir will activate to allow for additional outflow. The emergency overland flow route for the proposed site will be directed southeast towards the municipal ditch along Ottawa Street.

The quantitative and qualitative properties of the storm runoff for both the pre & post development flows are further detailed below. Stormwater Best Management Practices (SWM BMP's) will be implemented at the "Lot level", "Conveyance" and "End of Pipe" locations. These concepts will be explained further in Section 7.7.

In summary, the following design criteria have been employed in developing the stormwater management design for the site as directed by the RVCA and City:

Quality Control

- The site has been designed to achieve an 80% total suspended solids removal (enhanced level of treatment) using oil & grit separator units as part of a treatment train approach.

Quantity Control

- Post development 100-year flow is to be restricted to match the 2-year pre-development flow with a maximum Cvalue of 0.50.

7.2 Runoff Coefficient Calculations

Runoff values presented in the report have been derived from the Hydrologic & Hydraulic analysis completed by JFSA. Please refer to the "Stratford Foxrun Development – 5923 Ottawa Street, Richmond Ditch Hydrologic and Hydraulic Analysis" for additional information.

Egis provided JFSA with the site area and runoff coefficients to be incorporated into their larger drainage areas. The following coefficients were used to develop an average C for each area:

Roofs/ Concrete/ Asphalt	0.90
Gravel	0.60
Undeveloped and Grass	0.20

As per the City of Ottawa - Sewer Design Guidelines, the 2/5-year balanced 'C' value must be increased by 25% for a 100-year storm event to a maximum of 1.0.

7.3 Pre-Development Drainage

The existing site drainage limits are demonstrated on the Pre-and Post- Development Drainage Area Plan included in Appendix 'E'. The site is 2.27 ha overall, but for the purposes of this report, the pre-development drainage is focused on the area of development. A summary of the Pre-Development Runoff Coefficient Calculations can be found below.

Table 4: Pre-Development Runoff Coefficients Summary

Drainage Area	Area (ha)	Runoff Coefficient (2/5-Year)	Runoff Coefficient (100-Year)
A1	0.22	0.20	0.25
A2	0.26	0.20	0.25
Total (Phase 1)	0.48	-	-
A3	0.16	0.20	0.25
A4	0.29	0.20	0.25
Total (Phase 2)	0.45		

Area A1 and A3 represents the portion of the Phase 1 and Phase 2 development directed towards the rear yard in the existing condition, respectively. Areas A2 and A4 represent the portion of the Phase 1 and Phase 2 development areas directed towards the Ottawa Street municipal ditch in the existing condition, respectively.

Runoff directed towards the rear yard is conveyed along the railway ditch before discharging through a 1500 mm diameter culvert to Marlborough Creek, a tributary of the Jock River.

Runoff directed towards Ottawa Street is conveyed along the Ottawa Street and Eagleson Road municipal ditches before turning towards the ditch along the railway track and ultimately discharging through the same 1500 mm diameter culvert to Marlborough Creek.

7.4 Post-Development Drainage

The proposed site drainage limits are demonstrated on the Post-Development Drainage Area Plan. See CCO-25-0415 - POST in Appendix 'F' of this report for more details. A summary of the Post-Development Runoff Coefficients can be found below.

Table 5: Post-Development Runoff Coefficients Summary

Drainage Area	Area (ha)	Runoff Coefficient (2/5-Year)	Runoff Coefficient (100-Year)
B1	0.22	0.50	0.57
B2	0.26	0.90	1.00
Total (Phase 1)	0.48	-	-
B3	0.16	0.49	0.56
B4	0.29	0.90	1.00
Total (Phase 2)	0.45		

Areas B1 represents Phase 1 surface runoff, while area B2 represents the Phase 1 roof area. Area B3 represents Phase 2 surface runoff, and area B4 represents the Phase 2 roof area. See Appendix 'G' for calculations.

For each phase, controlled roof runoff and uncontrolled surface runoff will be directed towards a depressed surface storage area located within the front yard. Phase 1 and Phase 2 will each employ an 85 mm diameter orifice to control outflow from its respective storage area. Each storage area will also include a 0.30m earth weir to allow for greater outflow during larger storm events. The restriction of runoff will result in a ponding depth of 0.58m for Phase 1, and 0.65m for Phase 2. Stormwater management will be independent for each phase.

Runoff will be conveyed from the depressed surface storage areas to oil and grit separator units before discharging to the Ottawa Street municipal ditch.

7.5 Quantity Control

The 2- and 100-year post development runoff for the site must be restricted to match the 2-year pre-development flow rate.

JFSA was retained to complete a Hydrologic and Hydraulic analysis of the proposed stormwater management design to confirm there will be no negative impacts to the receiving ditch. A pre- and post-development hydrologic model was created with SWMHYMO, and hydraulic modeling was completed using HEC-RAS.

Table 6, below, summarizes the site release rates and required storage volumes for the post-development condition based on JFSA's analysis. For further information, refer to the memo prepared by JFSA and included in Appendix 'G'.

Table 6: Site Release Rates / Required Storage Volume / Ponding Depth

	Phase 1 (0.48 ha)			Phase 2 (0.45 ha)		
Storm	Peak Outflow (m ³ /s)	Required Storage (m ³)	Ponding Depth (m)	Peak Outflow (m ³ /s)	Required Storage (m ³)	Ponding Depth (m)
2YrCHI3Hr	0.008	41	0.31	0.009	40	0.40
5YrCHI3Hr	0.009	72	0.39	0.010	68	0.48
10YrCHI3Hr	0.010	93	0.44	0.011	87	0.53
25YrCHI3Hr	0.010	122	0.50	0.012	112	0.59
50YrCHI3Hr	0.011	143	0.54	0.014	127	0.62
100YrCHI3Hr	0.014	163	0.58	0.018	141	0.65
2YrSCS24Hr	0.008	46	0.33	0.009	44	0.41
5YrSCS24Hr	0.009	75	0.40	0.010	70	0.49
10YrSCS24Hr	0.010	95	0.44	0.011	87	0.53
25YrSCS24Hr	0.010	120	0.49	0.011	109	0.58
50YrSCS24Hr	0.011	139	0.53	0.013	124	0.62
100YrSCS24Hr	0.013	158	0.57	0.017	137	0.64

Table 7, below, summarizes the Pre- and Post- development peak flow within the Ottawa Street Municipal Ditch at the southeast corner of the property (Junction J1 from the modeling results).

Table 7: Pre- and Post-Development Peak Flow Summary

	Peak Flow (m ³ /s)		
Storm	Pre-Development	Post-Development	Difference
2YrCHI3Hr	0.015	0.024	0.009
5YrCHI3Hr	0.026	0.032	0.006
10YrCHI3Hr	0.035	0.037	0.002
25YrCHI3Hr	0.047	0.043	-0.004
50YrCHI3Hr	0.057	0.050	-0.007

100YrCHI3Hr	0.067	0.060	-0.007
2YrSCS24Hr	0.024	0.028	0.004
5YrSCS24Hr	0.038	0.037	-0.001
10YrSCS24Hr	0.049	0.042	-0.007
25YrSCS24Hr	0.062	0.049	-0.013
50YrSCS24Hr	0.073	0.055	-0.018
100YrSCS24Hr	0.084	0.063	-0.021

As seen in Table 7, above, there will be a minor increase in flow during smaller storm events. The increase in flow is the result of additional area being directed towards the Ottawa Street municipal ditch that was directed towards the rear yard in the existing condition. Outflow during smaller events is controlled by an orifice at the minimum allowable size, and so reducing flow by reducing orifice size would increase the risk of a blockage within the storm system and is not recommended.

During larger storm events, the modeling results indicate there will be a reduction in peak flow, and a reduction in the 100-year floodplain.

Based on JFSA's analysis, it has been determined that there will be no negative downstream impact to the roadway or existing buildings resulting from the minor increase in runoff during smaller events.

For more information on the Hydrologic and Hydraulic modeling completed by JFSA, please refer to the memo included in Appendix 'G'.

7.6 Quality Control

The development of this lot will employ Best Management Practices (BMP's) wherever possible. The intent of implementing stormwater BMP's is to ensure that water quality and quantity concerns are addressed at all stages of development. Lot level BMP's typically include temporary retention of the parking lot runoff, minimizing ground slopes and maximizing landscaped areas.

Within areas B1 and B3, surface runoff from the Phase 1 & 2 drive aisle, parking lots, and asphalt loading areas will be directed towards proposed grassed swales located along the phase line and property line. The grassed swales have been designed with minimal slope to reduce runoff velocity and promote filtration and settlement of suspended solids.

The proposed grassed swales will discharge to depressed surface storage areas located within Phase 1 and 2. The depressed surface storage areas will restrict runoff and provide further opportunity for suspended solids removal through filtration and settlement.

To ensure the quality control criteria is met, the depressed surface storage areas will discharge to oil and grit separator units located within their respective phases. The combination of grassed swales, surface storage, and the oil and grit separator units will provide a minimum 80% TSS removal for all runoff leaving the site.

7.7 Village of Richmond Environmental Management Plan

As the subject site is located within the Village of Richmond Environmental Management Plan study area, the site must conform to the findings of the EMP. Concurrence with the findings and recommendations are listed below:

7.7.1 Treatment Train

The proposed stormwater management system will convey runoff within gently sloped swales to a depressed surface storage area where runoff will be stored and released at a controlled rate. This will provide an opportunity for filtration through the vegetated medium, infiltration, and settlement of suspended solids. Before leaving the site, controlled runoff will be directed to an Oil & Grit separator where additional quality treatment will be provided. These lot level, conveyance, and end-of-pipe controls will ensure stormwater quality is properly addressed.

7.7.2 Thermal Mitigation

As mentioned above, stormwater conveyance will primarily be through gently sloped grass swales, and stormwater will be stored within a landscaped depressed surface storage area before discharging to the municipal ditch. After leaving the site, runoff will travel a minimum 745m within the municipal and ditches before discharging to Marlborough Creek. With on-site detention of stormwater within landscaped areas and the length of the flow path to the outlet, thermal impacts to the receiving watercourse are not anticipated.

7.7.3 Water Balance

Based on the findings of the Geotechnical Report prepared by Paterson, the site is heavily constrained by high groundwater and soils that are not suitable for infiltration. The borehole results identified that all soils warranted a UCSS classification containing either clay, silt, clayey, or silty. As per Technical Bulletin IWSB-2024-04, infiltration-type LID practices are not permitted in clay or silt soils, nor in soils that warrant a dual classification with silt or clay as per the USCS. While the site has been generally designed to promote infiltration with gently sloped grass conveyance swales and stormwater detention within landscaped surface storage areas, implementing an infiltration-type LID practice to ensure water balance will not be permitted, and so undertaking a water balance would not result in any changes to the design.

7.7.4 Volume Control (7 mm Storm Retention)

As mentioned above, an infiltration-type LID practice will not be permitted, and so the requirement to retain the first 7 mm of rainfall can not be achieved through infiltration. Abstraction will be limited to depression storage within the gently sloped swales and stormwater management areas, and through evapotranspiration of the stored surface and roof runoff. Evapotranspiration has been promoted to the greatest extent possible within the

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design by providing orifice controls with the minimum permissible size. This will detain stormwater on site for the longest duration possible, resulting in maximum surface stormwater volumes of 163 m³ for Phase 1 and 141 m³ for Phase 2.

7.7.5 Control 100-Year Post to 2-Year Pre

Stormwater modeling has been completed by JFSA. The results indicated that while there will be a minor increase in runoff during smaller storm events, the 100-year peak flow will be a reduction compared to existing conditions. Additionally, the proposed stormwater management design will reduce the extent of the 100-year floodplain.

7.7.6 Erosion Potential vs Additional Retention

As previously mentioned, the design relies on detention of stormwater runoff and not retention, as an infiltration-based design will not be permitted. Minimum orifice sizes are proposed which result in the maximum on-site storage volume. Modeling has also been completed by JFSA which indicates there will be a reduction in flow leaving the site during larger stormer events.

7.7.7 Implementation of LID

LID has been implemented with vegetated swales and depressed vegetated surface storage areas.

8.0 EROSION AND SEDIMENT CONTROL

8.1 Temporary Measures

Before construction begins, temporary silt fence, straw bale or rock flow check dams will be installed at all natural runoff outlets from the property. It is crucial that these controls be maintained throughout construction and inspection of sediment and erosion control will be facilitated by the Contractor or Contract Administration staff throughout the construction period.

Silt fences will be installed where shown on the final engineering plans, specifically along the downstream property limits. The Contractor, at their discretion or at the instruction of the City, Conservation Authority or the Contract Administrator shall increase the quantity of sediment and erosion controls on-site to ensure that the site is operating as intended and no additional sediment finds its way off site. The rock flow, straw bale & silt fence check dams and barriers shall be inspected weekly and after rainfall events. Care shall be taken to properly remove sediment from the fences and check dams as required. Care shall be taken at the removal stage to ensure that any silt that has accumulated is properly handled and disposed of. Removal of silt fences without prior removal of the sediments shall not be permitted.

Although not anticipated, work through winter months shall be closely monitored for erosion along sloped areas. Should erosion be noted, the Contractor shall be alerted and shall take all necessary steps to rectify the situation. Should the Contractor's efforts fail at remediating the eroded areas, the Contractor shall contact the City and/or Conservation Authority to review the site conditions and determine the appropriate course of action. As the ground begins to thaw, the Contractor shall place silt fencing at all required locations as soon as ground conditions warrant. Please see the Site Grading, Drainage Plan and Sediment & Erosion Control Plan for additional details regarding the temporary measures to be installed and their appropriate OPSD references.

8.2 Permanent Measures

Rip-rap will be placed at all locations that have the potential for concentrated flow. It is crucial that the Contractor ensure that the geotextile is keyed in properly to ensure runoff does not undermine the rip rapped area. Additional rip rap is to be placed at erosion prone locations as identified by the Contractor / Contract Administrator / City or Conservation Authority.

It is expected that the Contractor will promptly ensure that all disturbed areas receive topsoil and seed/sod and that grass be established as soon as possible. Any areas of excess fill shall be removed or levelled as soon as possible and must be located a sufficient distance from any watercourse to ensure that no sediment is washed out into the watercourse. As the vegetation growth within the site provides a key component to the control of sediment for the site, it must be properly maintained once established. Once the construction is complete, it will be up to the landowner to maintain the vegetation and ensure that the vegetation is not overgrown or impeded by foreign objects.

9.0 SUMMARY

- A new 651 m² distillery and restaurant/retail building is proposed within Phase 1 at 5923 Ottawa Street.
- A new 926 m² distillery building is proposed within Phase 2.
- Domestic water servicing will be provided by a new drilled well for each phase, designed by others.
- The Phase 2 building will be serviced by the Phase 1 well in the interim condition.
- Fire protection for Phase 1 will be provided by a remote hydrant systems and underground water storage tanks.
- Fire protection for Phase 2 will be provided by an underground water storage tank complete with a chute and draw pipe.
- Sanitary servicing will be provided by new on-site septic systems designed by Paterson.
- Storage for the 2- through 100-year storm events will be provided on the roof of the building and within proposed depressed surface storage areas. Runoff will discharge to the municipal ditch along Ottawa Street.
- Based on the hydrologic and hydraulic modeling completed by JFSA, there will be no negative downstream impact resulting from the stormwater management design.
- Quality control requirements will be achieved with oil and grit separator units as part of a treatment train approach.

10.0 CONCLUSIONS

This report has been provided to describe the servicing and stormwater management for the site located 5923 Ottawa Street.

This report is respectfully being submitted for review.

Regards,

Egis Canada Ltd.



Jessica Burden, P.Eng.
Project Engineer, Land Development
E: Jessica.burden@egis-group.com

A handwritten signature in cursive script that reads "Francis Valenti".

Francis Valenti, P.Eng.
Junior Project Engineer, Land Development
E: francis.valenti@egis-group.com

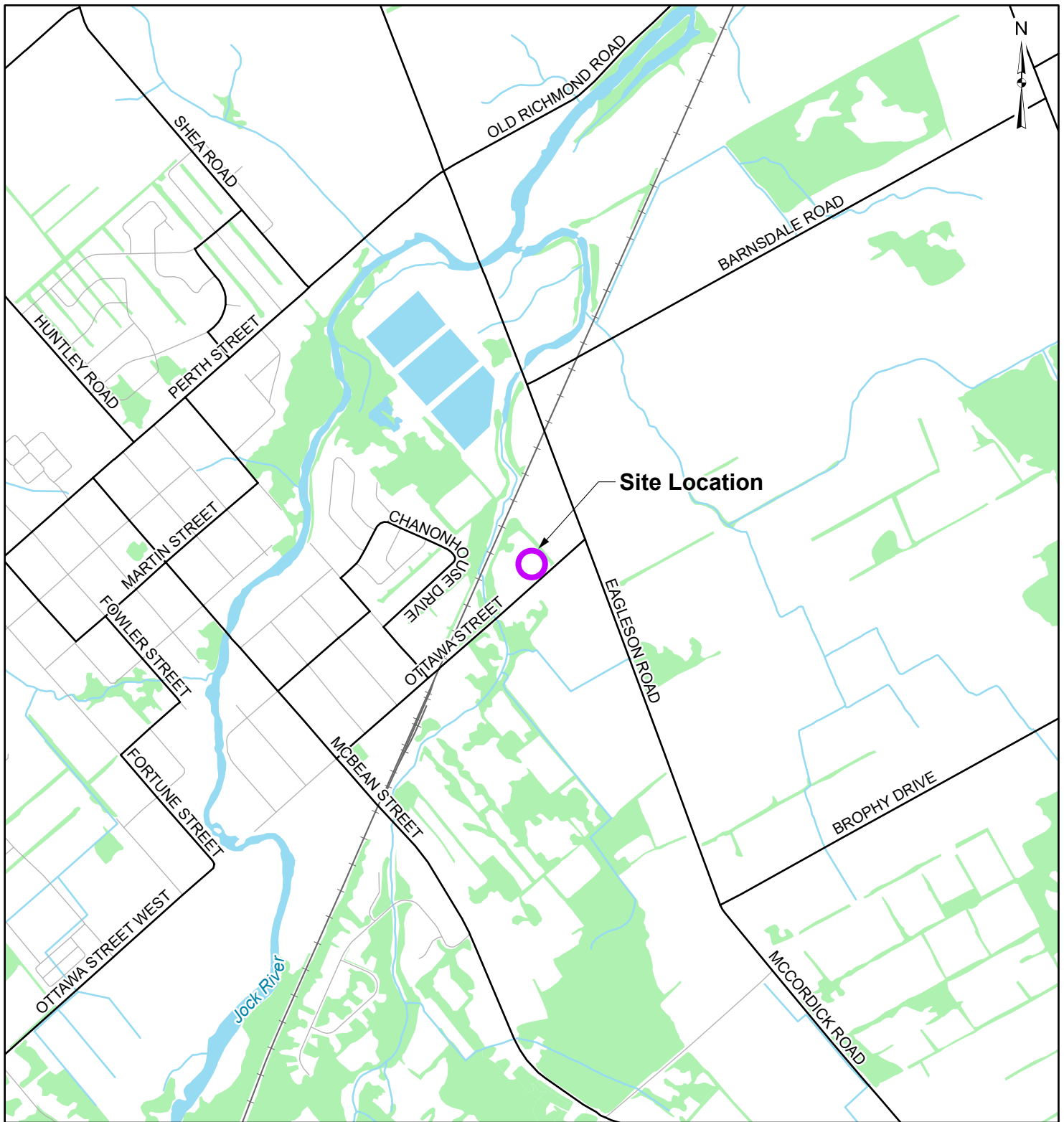
11.0 STATEMENT OF LIMITATIONS

This report was produced for the exclusive use of 99117756 Canada Inc. The purpose of the report is to assess the existing stormwater management system and provide recommendations and designs for the post-construction scenario that are in compliance with the guidelines and standards from the Ministry of the Environment, Conservation and Parks, City of Ottawa and local approval agencies. Egis Canada reviewed the site information and background documents listed in Section 2.0 of this report. While the previous data was reviewed by Egis Canada and site visits were performed, no field verification/measures of any information were conducted.

Any use of this review by a third party, or any reliance on decisions made based on it, without a reliance report is the responsibility of such third parties. Egis Canada accepts no responsibility for damages, if any, suffered by any third party as a result of decisions or actions made based on this review.

The findings, conclusions and/or recommendations of this report are only valid as of the date of this report. No assurance is made regarding any changes in conditions subsequent to this date. If additional information is discovered or becomes available at a future date, Egis Canada should be requested to re-evaluate the conclusions presented in this report, and provide amendments, if required.

APPENDIX A KEY PLAN



LEGEND

- Site Location
- Local Road
- Major Road
- Railroad
- Watercourse
- Waterbody
- Wooded Area

REFERENCE

GIS data provided by the Ontario Ministry of Natural Resources and Forestry, 2024.



CLIENT:		99117756 CANADA INC.	
PROJECT:		5923 OTTAWA STREET, RICHMOND	
TITLE:		SITE LOCATION PLAN	
egis 115 Walgreen Road, RR3, Carp, ON K0A1L0 Tel: 613-836-2184 Fax: 613-836-3742		PROJECT NO: CCO-25-0415	FIGURE:
		Date	Sep., 04, 2024
		GIS	CZ
		Checked By	AG
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APPENDIX B BACKGROUND DOCUMENTS

March 27, 2024

Bridgette Alchawa
Egis Canada Ltd.
Via email: bridgette.alchawa@egis-group.com

**Subject: Pre-Consultation: Meeting Feedback
Proposed Site Plan Control Application – 5923 Ottawa St**

Please find below information regarding next steps as well as consolidated comments from the above-noted pre-consultation meeting held on March 21, 2024.

Pre-Consultation Preliminary Assessment

1 ☐	2 ☐	3 ☐	4 ☒	5 ☐
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One (1) indicates that considerable major revisions are required while five (5) suggests that the proposal appears to meet the City's key land use policies and guidelines. This assessment is purely advisory and does not consider technical aspects of the proposal or in any way guarantee application approval.

Next Steps

1. A review of the proposal and materials submitted for the above-noted pre-consultation has been undertaken. Please proceed to complete a Phase 2 Pre-consultation Application Form and submit it together with the necessary studies and/or plans to planningcirculations@ottawa.ca.
2. In your subsequent pre-consultation submission, please ensure that all comments or issues detailed herein are addressed. A detailed cover letter stating how each issue has been addressed must be included with the submission materials. Please coordinate the numbering of your responses within the cover letter with the comment number(s) herein.
3. Please note, if your development proposal changes significantly in scope, design, or density before the Phase 3 pre-consultation, you may be required to complete or repeat the Phase 2 pre-consultation process.

Supporting Information and Material Requirements

1. The attached **Study and Plan Identification List** outlines the information and material that has been identified, during this phase of pre-consultation, as either required (R) or advised (A) as part of a future complete application submission.

- a. The required plans and studies must meet the City's Terms of Reference (ToR) and/or Guidelines, as available on Ottawa.ca. These ToR and Guidelines outline the specific requirements that must be met for each plan or study to be deemed adequate.

Consultation with Technical Agencies

1. You are encouraged to consult with technical agencies early in the development process and throughout the development of your project concept. A list of technical agencies and their contact information is enclosed.

Planning

Comments:

Questions:

1. What is the intent for the proposed bar/pub use. Restaurants are a prohibited use per 385r.

Response: It is understood that liquor can be sold if it is the product being produced. The current idea for the restaurant is to offer food that is easily prepared, (sandwiches, pizza, etc.) however, applicant suggested that they may be willing to consider different options based on zoning interpretation.

2. What is the idea for the severance component? May not have enough space to achieve the severance once the full build out of the lot is considered.
3. What is the timing of the severance? There are potential concerns regarding a pre-mature severance.

Response: The idea is for the severance to occur after the site plan application/approval and the establishment of the site.

Official Plan

1. The subject site is designated Village on Schedule B9 of the Official Plan.
2. The subject site is designated Village Industrial Area on Schedule A of the Village of Richmond Secondary Plan – Volume 2.
 - a. Uses permitted on lands designated Village Industrial Area include: light industrial uses, office, printing plant, service repair shop, small batch brewery, warehouse and heavy equipment and vehicle sales, rental and servicing, research, technology, nurseries, greenhouses, catering, places of assembly, broadcasting and training

- b. Maximum building height - four storeys
- c. Adequate buffering including landscaping and screening will be provided between uses in Industrial Areas to ensure that storage areas and parking areas are screened from adjacent properties

Zoning By-law

- 3. The subject site is zoned RG3 [385r] under the Zoning By-law. The purpose of the RG (Rural General Industrial) is to permit development of light industrial uses in Village designations; accommodate a range of light industrial uses and limited service commercial uses for the travelling public; and, regulate development in a manner that respects adjacent land uses and will have a minimal impact on the surrounding rural area. The RG3 subzone recognizes smaller parcels.
- 4. Permitted uses in the RG3 zone include [S.219 (1)]:
 - n. Light industrial uses
 - t. Warehouse
- 5. Conditional Permitted Uses - The following are permitted subject to the use being located on the same lot as a use listed above.
 - c. Bar
 - A bar must be ancillary to a permitted brewery, winery or distillery and, may not have a gross floor area exceeding the lesser of:
 - 300 square metres, or
 - 25% of the floor area of the brewery, winery or distillery to which it is ancillary.
- 6. The site is subject to Rural Exception 385r which lists restaurants as a prohibited use.**
- 7. The proposal must meet the following 385r Exception Provisions and the RG3 provisions provided in Section 219.
 - a. Minimum front yard – 15m
 - b. Maximum lot coverage – 35 percent
 - c. No maximum building height
- 8. Minimum parking space rates as required by S.101, Table 101.
 - a. Bars – 6 per 100sq.m of g.f.a
 - b. Light industrial use – 0.8 per 100sq.m of g.f.a
 - c. Retail Store – 3.4 per 100sq.m of g.f.a

9. A landscape buffer for the parking lot will be required in accordance Table 110.
10. Outdoor refuse collection and loading areas must be:
 - a. Located at least 9 metres from a lot line abutting a public street
 - b. Located at least 3 metres from any other lot line
 - c. Screened from view by an opaque screen with a minimum height of 2.0 metres
11. Bicycle parking must be provided in accordance with Section 111.
12. If loading spaces are provided, they must be in accordance with Section 113.

Discussion and Submission Requirements

13. Subject Exception Zone prohibits restaurants as a use.
14. Zoning by-law interpretation staff have confirmed that a bar/pub serving food and drink ancillary to the distillery and contained within the same structure would be aligned with the intent of the zoning.
15. If the bar/pub component were to be contained in a separate structure, it would be more closely aligned with a restaurant and would not be permitted under the current zoning.
16. A Site Plan will be required. The plan must be prepared as per the City's [Terms of Reference](#) and must address the following:
 - a. The site plan must clearly identify the required yard setbacks from all existing lot lines
 - b. The Site Plan must clearly identify all existing buildings
 - c. The required landscaped area must be included
 - d. Parking spaces must be clearly defined, as well as the access driveway, and any drive aisles throughout the site
17. A Landscape Plan will be required. The plan must be prepared in accordance with the [Landscape Plan Terms of Reference](#) and include all of the listed general elements as well as detail existing and proposed vegetation.
18. Plan of Survey showing the current site conditions prepared in accordance with the City's [Plan of Survey Terms of Reference](#).

Urban Design

Comments:

Submission Requirements:

19. Urban Design Brief is required.. Please see attached customized Terms of Reference to guide the preparation.
 - i. The Urban Design Brief should be structured by generally following the headings highlighted under Section 3 – Contents of these Terms of Reference.
 - ii. The proposal is not subject to the Urban Design Review Panel.
20. Additional drawings and studies are required as shown on the SPIL. Please follow the terms of references ([Planning application submission information and materials | City of Ottawa](#)) the prepare these drawings and studies.
 - i. Design Brief
 - ii. Site Plan
 - iii. Landscape Plan
 - iv. Elevations

Comments on Preliminary Design – Applicants are to provide a response to these comments in the Design Brief.

21. The following policies/guidelines apply:
 - a. Village Industrial within the Richmond Secondary Plan
 - b. Design Guidelines for Rural Villages
22. Please reference the direction within the Design Guidelines to help inform the design of the building as the design progresses. The architectural directions in the guidelines should guide the building design as closely as possible.
23. Please ensure that landscaping and tree planting is provided along Ottawa Street frontage.

24. Please ensure that the patio is a comfortable place for patrons and separated from road noise. Please provide screening and perimeter landscaping.

Feel free to contact Lisa Stern, Planner III, for follow-up questions.

Engineering

Comments:

25. Servicing

- a. A **Site Servicing Study** will be required with the Site Plan Control application. This report should be completed exceeding the minimum requirements laid out in the Site Servicing Study Terms of Reference. The report will serve to address how the design of the site complies with City design guidelines, Official Plan policies, among other evaluation criteria noted in the Terms of Reference. Stormwater management, which is a component of the Servicing Study, is required to mitigate the effects of urbanization on the hydrologic cycle including increased runoff and decreased infiltration, of rain and snowmelt. Without proper stormwater management, a site can negatively impact the environment by reducing baseflow, degrading water quality, and increasing flooding and erosion. This leads to reduced diversity of aquatic life, fewer opportunities for human uses of water resources, and loss of property and human life. The City looks to lessen these risks by reviewing development to ensure stormwater management practices are being implemented, infrastructure is resilient to future climate conditions, including extreme weather events, and using low impact development where feasible to manage smaller, infrequent events. The Official Plan, which receives authority through the Planning Act, identifies in Policy 6, section 2.2.3, that flooding is the costliest type of natural disaster in Canada.
- b. There is no public service capacity currently available to have the option of extending public services to the proposed development. Development therefore must be on the basis of private services. The Village has a limited municipal water network and limited sanitary network & pump station capacity. Any planned growth would need to include network, and possibly plant, upgrades to support proposed development, which is likely too onerous for the scope of this development.
- c. In terms of the Stormwater Management for the Site Plan Control application, the quantity criteria will be that the 100-yr post development peak flow rate must match the 2-year pre-development

peak flow rate. As part of complete Site Plan Control application, whether development or redevelopment, the report must identify and mitigate the impacts of additional runoff resulting from increased imperviousness through measures such as site-specific stormwater management postulated in policy 6, section 4.7.1 of the Official Plan.

- d. In terms of a Stormwater Management approach, runoff volume control should proceed in the following hierarchical order, with each step exhausted before proceeding to the next:
 - 1. Retention (infiltration, reuse, or evapotranspiration),
 - 2. Low Impact Development (LID) filtration, and
 - 3. Conventional Stormwater management. Conventional stormwater management, should proceed only once Maximum Extent Possible has been attained for Steps 1 and 2 for retention and filtration.
- e. The pre-development runoff coefficient or a maximum equivalent 'C' of 0.5, whichever is less as described in the Sewer Design Guidelines, Second Edition, document no. SDG002, October 2012, City of Ottawa, including technical bulletins ISDTB-2014-01, PIEDTB-2016-01, ISTB 2018-01, ISTB-2018-04, ISTB-2019-02, section 8.3.7.3.
- f. A calculated time of concentration cannot be less than 10 minutes as described in section 5.1.4 of the Sewer Design Guidelines.
- g. The water quality control should be an enhanced level treatment, 80% long term suspended sediment removal. The City will be looking for a treatment train approach for water quality treatment. Reporting of TSS removal shall be extensive and if peer reviewed and published papers are relied on for conclusions, the conclusions shall be patently clear and the report shall show overwhelming agreement.
- h. Runoff will need to be conveyed to a legal and sufficient outlet. If it is proposed to discharge storm water to the existing ditches in the ROW, the ditches will need to be shown to provide continuous flow to an outlet. This comment is sourced from the Official Plan which notes in policy 8, section 4.7.1, that proof of legal and sufficient outlet for proposed stormwater management and drainage systems will be required as a condition of future Site Plan Control.
 - i. The 1 in 100-year floodplain is present along the rear portion of the lot. Any site alteration within this area requires a permit from the Conservation Authority. The Official Plan, in section

10.1.1, notes that development and site alteration shall not be permitted in the 1 in 100 year flood plain.

- j. Low Impact Development (LID) is to be implemented as per the bulletin from the former MOECC (now MECP) titled Expectations RE: Stormwater Management released in February 2015. The infiltration target for the site is typically determined from an applicable higher-level study, which is confirmed through on-site infiltration/percolation testing. The reporting should identify the treatment train of processes proposed for the development. The Official Plan defines LID as a stormwater management strategy that seeks to mitigate the impacts of increased runoff and stormwater pollution by managing runoff as close to its source as possible. LID comprises a set of site design strategies that minimize runoff through distributed, small scale structural practices that mimic natural or predevelopment hydrology through the processes of infiltration, evapotranspiration, harvesting, filtration and detention of stormwater. These practices can effectively remove nutrients, pathogens and metals from runoff, and they reduce the volume and intensity of stormwater flows. The City has released a document titled 'Low Impact Development Technical Guidance Report – Implementation in Areas with Potential Hydrogeological Constraints' which aids sites which may have constraints such as low permeability or high groundwater.
- k. The anticipated water demands (average day, maximum daily, and maximum hour) must be presented and justified for any hydrogeological pumping test rate. The pumping rate should be the maximum daily demand rate. The Ottawa Design Guidelines – Water Distribution provide information for determining water demand rates for the proposed zoning or uses in Table 4.2 – Consumption Rates.

26. Fire Services

- a. The Site Servicing Study must include a section addressing the provision of a **water supply for fire suppression**, determination of the required fire flow, and confirmation of whether any on-site storage will be required. It is the responsibility of the owner to ensure that an adequate water supply for firefighting is provided. The FUS (Fire Underwriters Survey) methodology, as opposed to the OBC methodology shall be applied for all rural areas.
 - i. It is anticipated that mitigative measures, including on-site storage, will be required given the group F, division 1 for distilleries. This occupancy is considered a high hazard occupancy under the Ontario Building Code. There will be risks with regards to the flammable or explosive off-gasses or

vapours, that must be contemplated and appropriately mitigated by the reporting.

- ii. The project, due to the proposed occupancy, will not be eligible to forgo the requirement for on-site fire retention storage.
 - iii. As mentioned the Phase 1 meeting, the applicant could retain a fire safety consultant to aid in the preparation of the FUS calculations. The specialist fire-fighting consultant would review a number of factors and could propose an alternative approach satisfactory to Development Review and the City's Fire Protection Engineer, Allan Evans.
 - iv. Enhanced review will be invoked should the construction coefficient chosen be less than 1.
- b. Fire Routes now require designation with By-law through the Site Plan process by contacting fireroutes@ottawa.ca once preliminary Site Plan approval has been provided.

27. Grading

- a. A **Grading and Drainage Plan** will be required with the Site Plan Control application identifying the existing and proposed drainage patterns and their relationship with the surface runoff control. As part of a complete Site Plan Control application, the Grading and Drainage Plan should identify and implement site, grading, building, and servicing design measures to protect new development from flooding as per policy 6, section 4.7.1 of the Official Plan. The Grading and Drainage Plan forms part of the requirements for Site Plan Control applications noted in the Studies and Plan Identification List, provided with the feedback documents.
- b. The Plan should have a note that references the horizontal and vertical datums that were used and tied into to complete the project. The drawing should also make reference (on the face of the plan) to a site benchmark that can be used by anyone with a level to carry out checks on the particular project.

28. Erosion and Sediment Control

- a. An **Erosion and Sediment Control Plan** will be required with the Site Plan Control Application. Erosion and sediment control plans shall have regard to Canadian Standards Association (CSA) W202 Erosion and Sediment Control Inspection and Monitoring Standard (as amended).

29. Geotechnical

- a. A **Geotechnical Study** will be required with the Site Plan Control application. The report should provide sufficient soils and engineering information to confirm that the site(s) are suitable or can be made suitable for development based on the requirements of the Geotechnical Investigation and Reporting Guidelines for Development Applications in the City of Ottawa.
- b. It is highly likely that sensitive marine clays will be encountered on the site. If the presence of clays is confirmed, enhanced investigations must be undertaken with vane shear, Atterberg limits, shrinkage, size, grade raise restriction, consolidation, sensitivity, and liquefaction analysis-amongst others.
- c. As the site is potentially underlain by compressible marine clays, long term groundwater monitoring will be required to support the development. Groundwater elevations are anticipated to be high (shallow) given the location in Richmond. The capacity of the deposit to accept additional load depends on the groundwater level. The Stormwater Management and LID design will also be impacted by the groundwater level.

30. Hydrogeological and Terrain Analysis Requirements (private servicing)

- a. A **Hydrogeological and Terrain Analysis** will be required for the Site Plan Control application to establish that there is an adequate quantity and quality of groundwater to support the proposed development(s). The requirements for the Hydrogeological and Terrain Analysis Report are outlined in the City of Ottawa Hydrogeological and Terrain Analysis Guidelines, Section 5.0 for Site Plans. The study forms part of the requirements for Site Plan Control applications noted in the Studies and Plan Identification List, provided with the feedback documents.
- b. Note that the onsite well would provide groundwater which serves the public and thus may be considered a regulated small drinking water system under O.Reg. 319/08: Small Drinking Water Systems. The application would also need to contact and incorporate any requirements set by medical officers of health or Ottawa Public Health. Any requirements related to the regulated small drinking water system must be fulfilled prior to the use of the system. "drinking water system" means a system of works, excluding plumbing, that is established for the purpose of providing users of the system with drinking water and that includes, (a) any thing used for the collection, production, treatment, storage, supply or distribution of water and (b) a well or intake that serves as the source or entry point of raw water supply for the system;

- c. The supply well must be tested to confirm water quantity and quality suitability prior to site plan approval. Support must be provided for the pump test rate; which should be the maximum day rate. The rate should consider the actual use, or potential uses permitted through zoning if unknown.
- d. The parameters of water quality that will be tested will be the “subdivision suite” (known to local well testing laboratories), as well as trace metals and VOCs. Requirements are outlined in the Hydrogeological and Terrain Analysis Guidelines, City of Ottawa, March 2021. The report should also provide an assessment of adjacent land uses and concerns and determine if any other parameters need to be tested (e.g. petroleum hydrocarbons, etc.).
- e. The Hydrogeological and Terrain Analysis Report should outline potential on-site activities and risks to existing groundwater users and identify measures that should be implemented to protect the aquifer in the long-term.
- f. Bollards, or other means of preventing vehicle access, will need to be provided between areas with vehicle access and the existing or proposed well(s).
- g. Results from nearby wells indicate a potential for exceedances for hardness, colour, total dissolved solids (TDS), turbidity, chloride, iron, and sodium.
- h. A Septic System Impact Assessment must be completed as part of the Hydrogeological and Terrain Analysis Report, as per the City’s Hydrogeological and Terrain Analysis Report Guidelines and MECP Guideline D-5-4, please refer to the HGTA for the predictive assessment for commercial/industrial developments (not residential developments).
 - i. Note that compact gravel will be considered impermeable in the septic impact assessment unless accompanied by field testing to confirm infiltration rates.
 - ii. Since this application is a site plan (not lot creation or zoning) septic treatment (i.e. tertiary treatment with nitrate dilution) may be considered as part of the septic impact assessment calculations. A system certified though NSF or BNQ should be recommended.
- i. If the expected sewage daily design flow is 10,000 L/d or less, the septic permit from the Ottawa Septic System Office must be issued prior to Site Plan Approval being granted.

- j. If the sewage design flow from sewage systems exceeds 10,000 L/d, a Reasonable Use Assessment must accompany the application to the City. Sewage systems with design flows exceeding 10,000 L/d require the issuance of an Environmental Compliance Approval (ECA) from the MECP prior to Site Plan Approval being granted.
- k. Bollards, or other means of preventing vehicle access, will need to be provided between areas with vehicle access and the proposed septic system(s).
- l. Technical consultation with the hydrogeological report reviewer is encouraged, please contact the City hydrogeologist, Obai Mohammed and copy the project manager listed below to schedule a technical consultation.

31. Noise and Vibration

- a. A **Noise Control Study** is required with the Site Plan Control Application. Noise studies are required for new noise sensitive land uses in proximity to surface transportation (road and rail). The site is within the influence area of a Protected Transportation Corridor (identified on Schedule C2 of the Official Plan) for which the noise impacts must be contemplated. A Noise Feasibility Study is required for development proposals within 250 meters of a secondary main railway line or within 500 meters of a principal main railway line.
 - i. The Ministry of Ontario's NPC-300 Environmental Noise Guideline, for which the City's ENCG were based, defines a noise sensitive land use as a property of a person that accommodates a building used for a noise sensitive commercial purpose. The definition goes on to say that from a land use planning perspective, a noise sensitive land use may be comprised of spaces that are noise sensitive and spaces that are not noise sensitive. The outdoor living area (OLA) associated with a noise sensitive land use is considered a noise sensitive space.
 - ii. The City's Environmental Noise Control Guidelines identify that noise sensitive land uses includes other land uses that may contain outdoor and/or outdoor areas/spaces where an intruding noise may create an adverse effect, which appears to be the case for the proposal.
- b. The City will require a vibration study if there is proposed development within 75 metres of the railway right of way, based on Official Plan section 10.2.1.

- c. The owner of the rail corridor will be able to provide scoping for the future works in the rail corridor which will guide the classification as principal or secondary main rail line in terms of the preparation of the noise feasibility study.

32. Rail Safety

- a. A **Rail Proximity Study** will be required with the application to address rail safety, implement risk mitigation best practices, and to inform any development setbacks required based on proximity to the rail corridor. The Official Plan notes, in section 10.2.1, that land adjacent to all Protected Transportation Corridors and facilities shown on Schedule C2 must follow rail safety and risk mitigation best practices to determine appropriate development setbacks. The FCM-RAC Guidelines for New Development or its successor shall apply in this case.
 - i. One of the elements of the report will be to contemplate the use of safety barriers to reduce the risks associated with railway incidents by intercepting or deflecting derailed cars in order to reduce or eliminate potential loss of life and damage to property. The standard safety barrier is an earthen berm, which is intended to absorb the energy of derailed cars, slowing them down and limiting the distance they travel outside of the railway right-of-way. The berm works by intercepting the movement of a derailed car. As the car travels into the berm, it is pulled down by gravity, causing the car to begin to dig into the earth, and pulling it into the intervening earthen mass, slowing it down, and eventually bringing it to a stop.

33. An MECP Environmental Compliance Approval would be required for the proposed stormwater management facilities, LID works, or sewage works if the exemption requirements of O.Reg. 525/98 are not met. It appears based on the proposal that an ECA would be required given the industrial use. Please contact the Ministry of the Environment, Conservation and Parks, Ottawa District Office to arrange a pre-submission consultation.

- a. Please note that the process for ECAs is undergoing changes and may be different upon time of submission. Currently, once the development application has been submitted, a request can be made to the City to consider a Transfer of Review (ToR) ECA for SWM works (ponds, ditches, culverts, etc.) for private property, instead of a direct submission ECA. This is subject to approval by the City and MECP. Note that the ECA requirements are currently in transition towards the linear ECA process and more details may become available depending on application submission timeline. It is

recommended to check with the City when the development application is submitted to confirm the ECA process at that time.

34. Phase One Environmental Site Assessment

- a. A **Phase One Environmental Site Assessment (ESA)**, and possibly Phase Two ESA as deemed required by the Phase 1 ESA, is required for the proposed Site Plan Control application. This mandatory report serves to ensure that development only takes place on sites where the environmental conditions are suitable for the proposed use in accordance with provincial legislation and regulations. The City's Historic Land Use Inventory identifies that there is a potentially contaminating use of a Motor Vehicle Repair Shop, repair and service at 5949 Ottawa which should be contemplated by the environmental consultant.

35. Construction constraints

- a. More detailed constraints may be provided in the Phase 2 Pre-Application Consultation Meeting as the conceptual drawing has provided more detail.

36. Background studies

- a. Village of Richmond Master Servicing Study
- b. Village of Richmond Environmental Management Plan
- c. Village of Richmond Community Design Plan

37. Severance

- a. In terms of the requirements for a future proposed severance, there will be engineering conditions placed on the application. It is recommended that the applicant reach out to the Development Review All Wards group who now handles commenting on Committee of Adjustment applications.
 - i. It is anticipated that a condition will be for a Hydrogeological and Terrain Analysis report to demonstrate the adequacy of the groundwater and area/septic dilution to accommodate the development.
 - ii. It is anticipated that a condition for independent water, sanitary and storm servicing will be place. Each lot should have their own independent systems which do not cross the property line.

- iii. It is anticipated that Noise Studies, Phase 1 ESA, and Rail Safety reports would be required as conditions of the severance.

Feel free to contact Travis Smith, Infrastructure Project Manager, for follow-up questions.

Transportation

Comments:

38. A TIA is not required.

39. ROW Protection:

- a. Ensure that the development proposal complies with the Right-of-Way protection requirements of the Official Plan's Schedule C16.
- b. See [Schedule C16 of the Official Plan](#).
- c. Any requests for exceptions to ROW protection requirements must be discussed with Transportation Planning and concurrence provided by Transportation Planning management.
- d. ROW must be unincumbered and conveyed at no cost to the City. Note that conveyance of the ROW/corner triangle will be required prior to registration of the SP agreement. Additional information on the conveyance process can be provided upon request.

40. Clear throat requirement is 8m. Ensure this length is provided. The clear throat length is measured from the ends of the driveway curb return radii at the roadway and the point of first conflict on-site. Note the minimum throat length provided must be maintained with the future ROW protection (as applicable).

41. Signalization of Eagleson Road and Ottawa Street is identified on the Development Charges Bylaw. Warrants have not yet been met for this intersection.

42. As the proposed site is commercial/industrial, AODA legislation applies.

- a. Ensure all crosswalks located internally on the site provide a TWSI at the depressed curb, per requirements of the Integrated Accessibility Standards Regulation under the AODA.
- b. Clearly define accessible parking stalls and ensure they meet AODA standards (include an access aisle next to the parking stall and a pedestrian curb ramp at the end of the access aisle, as required).

- c. Please consider using the City's Accessibility Design Standards, which provide a summary of AODA requirements.
<https://ottawa.ca/en/city-hall/creating-equal-inclusive-and-diverse-city/accessibility-services/accessibility-design-standards-features#accessibility-design-standards>

43. On site plan:

- a. Ensure site access meets the City's Private Approach Bylaw.
- b. Show all details of the roads abutting the site; include such items as pavement markings, accesses and/or sidewalks.
- c. Turning movement diagrams required for all accesses showing the largest vehicle to access/egress the site.
- d. Turning movement diagrams required for internal movements (loading areas, garbage).
- e. Show all curb radii measurements; ensure that all curb radii are reduced as much as possible and fall within TAC guidelines (Figure 8.5.1).
- f. Show dimensions for site elements (i.e. lane/aisle widths, access width and throat length, parking stalls, sidewalks, pedestrian pathways, etc.).

Feel free to contact Josiane Gervais, Transportation Project Manager, for follow-up questions.

Environment

Comments:

- 44. Backs onto floodplain associated with Marlborough Creek. The village of Richmond EMP (2010) indicates that the floodplain on this property contains a "local woodlot". Since the site plan indicates that the woodlot in the floodplain will be retained, we have no significant natural heritage concerns with the proposal.
- 45. There is potential for species at risk on the site, particularly in the wooded portion of the site this can be addressed through a Tree Conservation Report since the most likely concerns are related to forest dwelling species like butternut trees, black ash, and bats (addressed through timing windows). Accordingly we recommend a Tree Conservation Report be prepared to address the potential presences of these species within 25 m of

the proposed site alteration. The TCR will also need to address the concerns of our Planning Foresters as well as the information above.

46. Bird-safe design - Please review and incorporate bird safe design elements. Some of the risk factors include glass and related design traps such as corner glass and fly-through conditions, ventilation grates and open pipes, landscaping, light pollution. More guidance and solutions are available in the guidelines which can be found here:
https://documents.ottawa.ca/sites/documents/files/birdsafedesign_guidelines_en.pdf

Feel free to contact Matthew Hayley, Environmental Planner, for follow-up questions.

Forestry

Comments:

47. A tree permit will not be required as part of this application, as there are no City Trees within the right-of-way fronting the site, and impacts to private trees in the rural area are not regulated by the tree by-law.
48. The following Tree Conservation Report (TCR) guidelines have been adapted from the Schedule E of the Tree Protection By-law – for more information on these requirements please contact julian.alvarez-barkham@ottawa.ca
- a. A Tree Conservation Report (TCR) must be supplied for review along with the suite of other plans/reports required by the City
 - i. An approved TCR is a requirement of Site Plan approval.
 - b. The TCR must contain 2 separate plans:
 - i. Plan/Map 1 - show existing conditions with tree cover information.
 - ii. Plan/Map 2 - show proposed development with tree cover information.
 - c. The TCR must list all trees on site, as well as off-site trees if the CRZ (critical root zone) extends into the developed area, by species, diameter, and health condition.
 - i. For ease of review, the Planning Forester suggests that all trees be numbered and referenced in an inventory table.
 - d. Please identify trees by ownership – private onsite, private on adjoining site, city owned, co-owned (trees on a property line)

- e. If trees are to be removed, the TCR must clearly show where they are, and document the reason they cannot be retained.
 - i. Compensation may be required for the removal of city owned trees.
 - f. The removal of trees on a property line will require the permission of both property owners.
 - g. All retained trees must be shown, and all retained trees within the area impacted by the development process must be protected as per City guidelines available on the Tree Protection Specification or by searching Ottawa.ca.
 - i. The location of tree protection fencing must be shown on the plan;
 - ii. Show the critical root zone of the retained trees.
 - h. The City encourages the retention of healthy trees; if possible, please seek opportunities for retention of trees that will contribute to the design/function of the site.
49. The following Landscape Plan (LP) guidelines have been adapted from Schedule E of the Tree Protection By-law – for more information on these requirements please contact julian.alvarez-barkham@ottawa.ca
- a. Please ensure any retained trees are shown on the LP.
 - b. Minimum Setbacks
 - i. Maintain 1.5m from sidewalk or MUP/cycle track or water service laterals.
 - ii. Maintain 2.5m from curb.
 - c. Coniferous species require a minimum 4.5m setback from curb, sidewalk, or MUP/cycle track/pathway.
 - d. Maintain 7.5m between large growing trees, and 4m between small growing trees. Park or open space planting should consider 10m spacing, except where otherwise approved in naturalization / afforestation areas.
 - e. Adhere to Ottawa Hydro's planting guidelines (species and setbacks) when planting around overhead primary conductors.
 - f. Tree specifications
 - i. Minimum stock size: 50mm tree caliper for deciduous, 200cm height for coniferous.
 - ii. Maximize the use of large deciduous species wherever possible to maximize future canopy coverage

- g. Tree planting on city property shall be in accordance with the City of Ottawa's Tree Planting Specification; and if possible, include watering and warranty as described in the specification.
- h. No root barriers, dead-man anchor systems, or planters are permitted.
- i. No tree stakes unless necessary (and only 1 on the prevailing winds side of the tree)
- j. Hard surface planting
 - i. If there are hard surface plantings, a planting detail must be provided.
 - ii. Curb style planter design is highly recommended.
 - iii. No grates are to be used and if guards are required, City of Ottawa standard (which can be provided) shall be used.
- k. Trees are to be planted at grade.
- l. Soil Volume - Please demonstrate as per the **Landscape Plan Terms of Reference** that the available soil volumes for new plantings will meet or exceed the following:

Tree Type/Size	Single Tree Soil Volume (m3)	Multiple Tree Soil Volume (m3/tree)
Ornamental	15	9
Columnar	15	9
Small	20	12
Medium	25	15
Large	30	18
Conifer	25	15

- i. It is strongly suggested that the proposed species list include a column listing the available soil volume.
- m. Sensitive Marine Clay - Please follow the City's 2017 Tree Planting in Sensitive Marine Clay guidelines.
- n. The City requests that consideration be given to planting native species wherever there is a high probability of survival to maturity.

- o. Efforts shall be made to provide as much future canopy cover as possible at a site level, through tree planting and tree retention. The Landscape Plan shall show/document that the proposed tree planting and retention will contribute to the City's overall canopy cover over time. **Please provide a projection of the future canopy cover for the site to 40 years.**

Feel free to contact Julian Alvarez-Barkham, Forester, for follow-up questions.

Parkland

Comments:

- 50. Parkland Dedication will be required in accordance with [By-law No. 2022-280](#).
- 51. The applicable parkland dedication rate for Industrial and Commercial uses is 2% of the gross land area. For Commercial and Industrial redevelopment, gross land area means the portion of the property that is impacted by the development, but not including any hazard lands or natural heritage features identified in the Official Plan, an approved Secondary Plan, or through an environmental impact study accepted by the City;
- 52. The applicant is advised that they must identify on the survey, site plan or supporting plan the portion of the property impacted by the development, for the purpose of calculating gross land area. The property appears to be impacted by floodplain. Floodplains may be excluded from the area subject to parkland dedication.
- 53. Parks & Facilities Planning is requesting payment of **Cash-in-lieu-of-Parkland** for this development. The value of the land, equivalent to the Parkland Dedication requirement, will be determined as of the day before planning approval is given for the development. A property valuation will be completed by the City prior to site plan approval at the owner's cost.
- 54. The conveyance of parkland or the payment of cash-in-lieu of parkland is required unless it can be demonstrated, that the required parkland conveyance or cash-in-lieu of parkland, or combination thereof, has been previously satisfied in accordance with the Planning Act.
- 55. The application notes a future severance of the lot. The owner is advised that if they provide CIL of parkland for the entirety of the subject property prior to severance, they should not be required to provide further parkland dedication at the time of lot creation.



Feel free to contact Anissa McAlpine, Parks Planner, for follow-up questions.

Conservation Authority

Comments:

- 56. No concerns with the proposal as no physical development is occurring within the floodplain or regulated area.

Feel free to contact Eric Lalande, Rideau Valley Conservation Authority, for follow-up questions.

Other

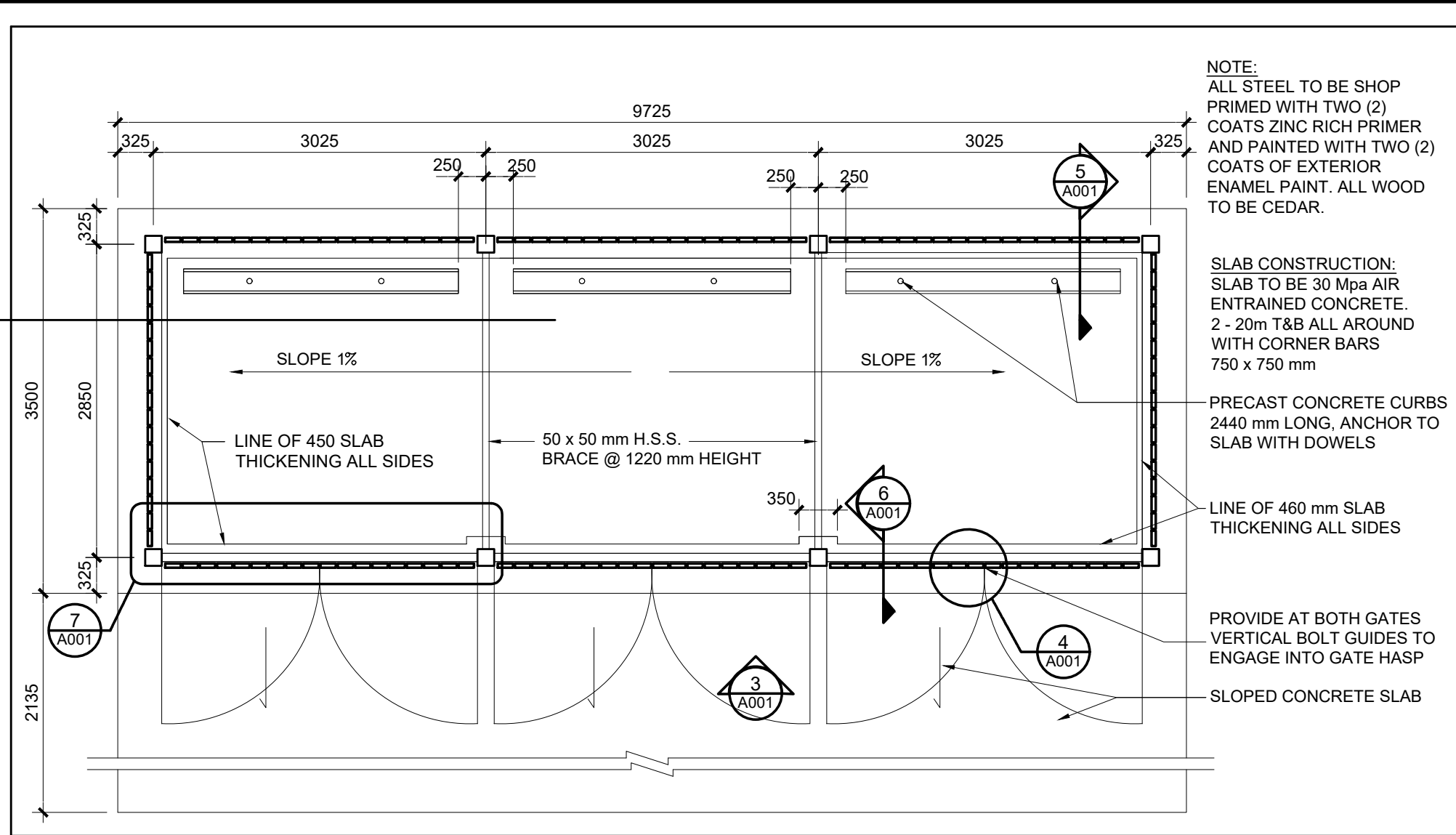
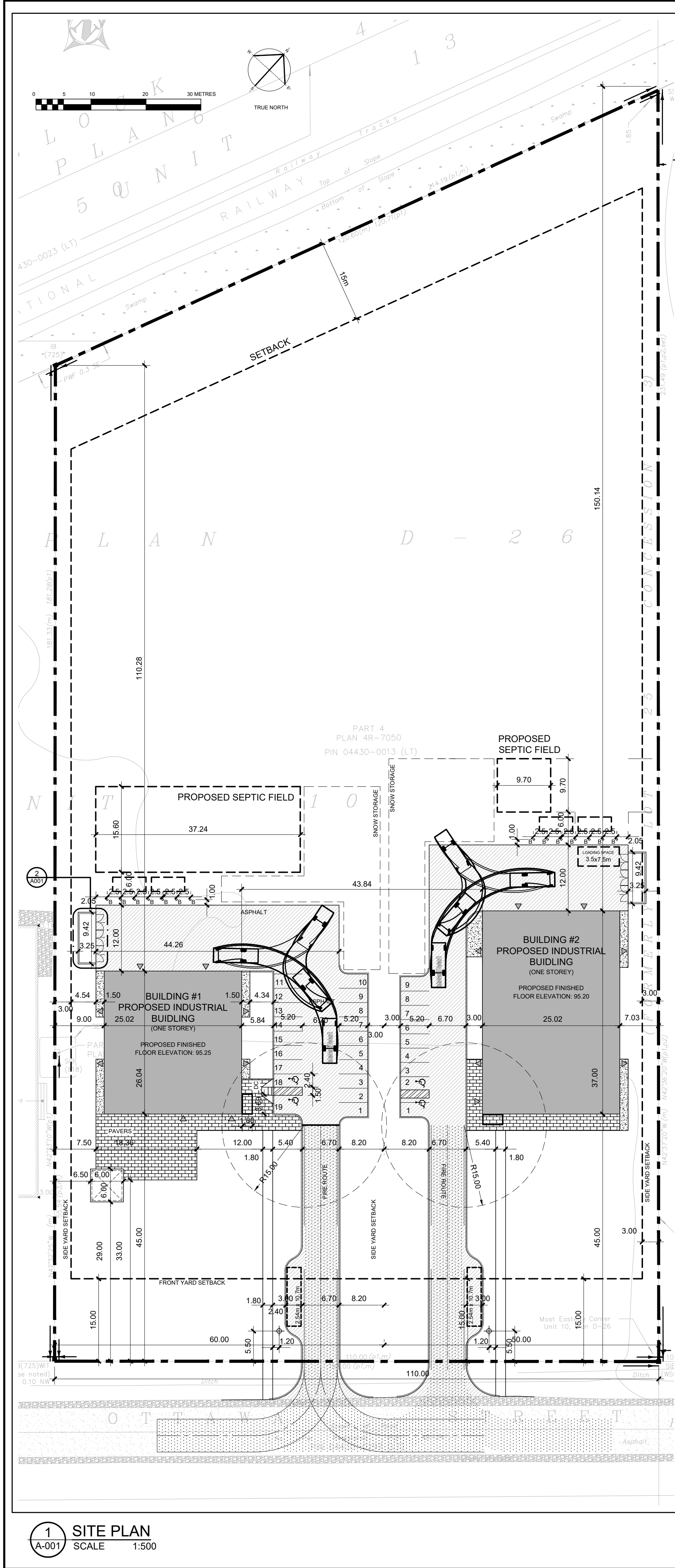
The High Performance Development Standard (HPDS) is a collection of voluntary and required standards that raise the performance of new building projects to achieve sustainable and resilient design. The HPDS was passed by Council on April 13, 2022.

- a. At this time, the HPDS is not in effect and Council has referred the 2023 HPDS Update Report back to staff with direction to bring forward an updated report to Committee with recommendations for revised phasing timelines, resource requirements and associated amendments to the Site Plan Control By-law by no later than Q1 2024.
- b. Please refer to the HPDS information attached and ottawa.ca/HPDS for more information.

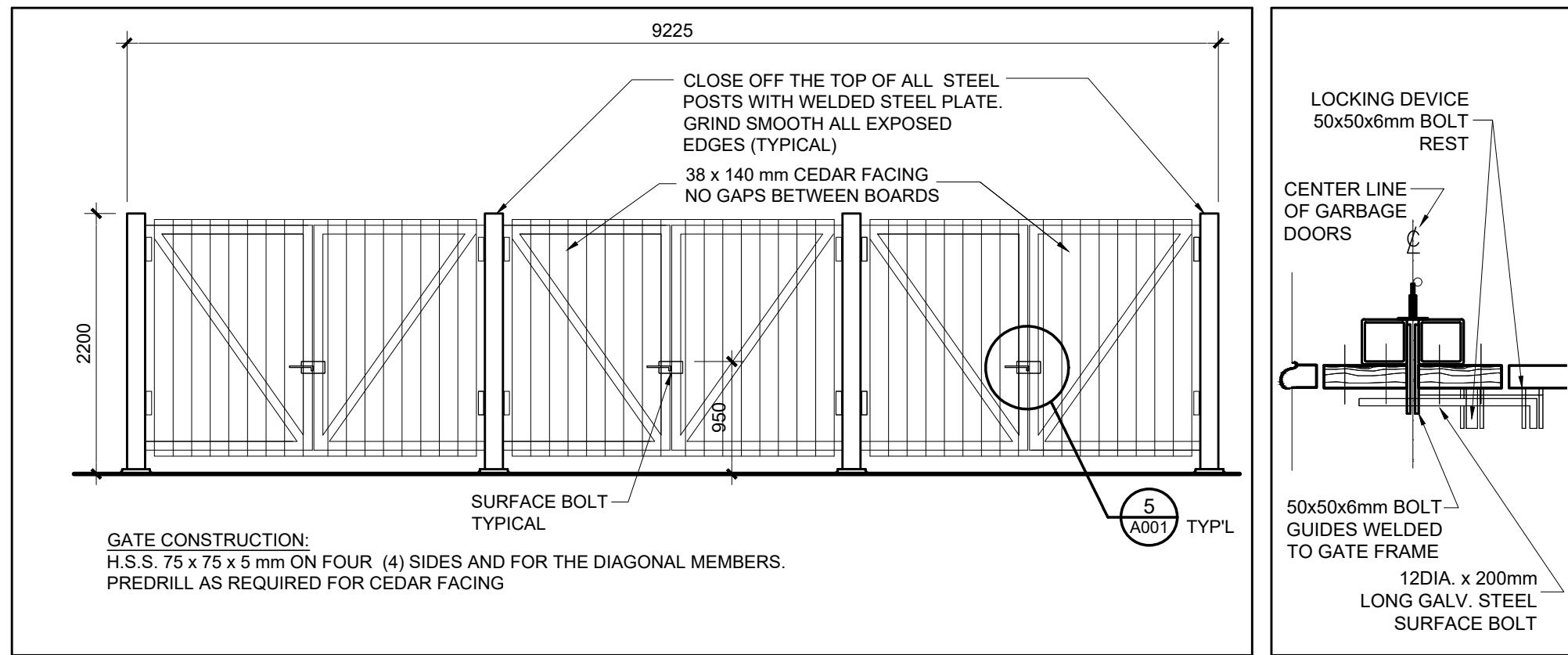
Should there be any questions, please do not hesitate to contact myself or the contact identified for the above areas / disciplines.

Yours Truly,
Stephan Kukkonen

c.c. Smith Travis - Infrastructure Project Manager
Josiane Gervais - Transportation Project Manager
Lisa Stern – Planner III (Urban Design)
Matthew Hayley – Environmental Planner
Julian Alvarez-Barkham – Planning Forester
Anissa McAlpine – Parks Planner
Eric Lalande – Rideau Valley Conservation Authority

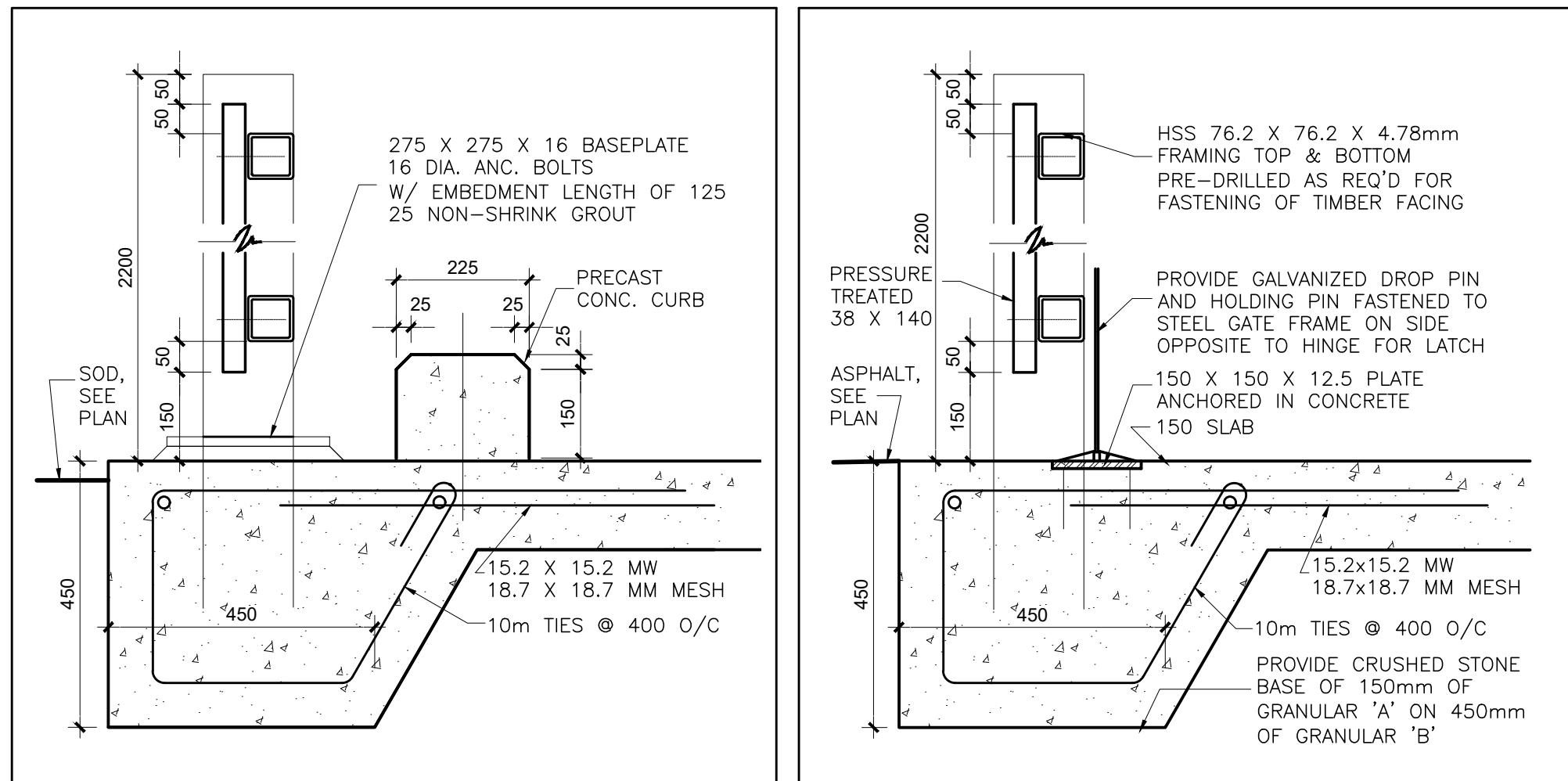


2 GARBAGE ENCLOSURE PLAN
SCALE 1:50



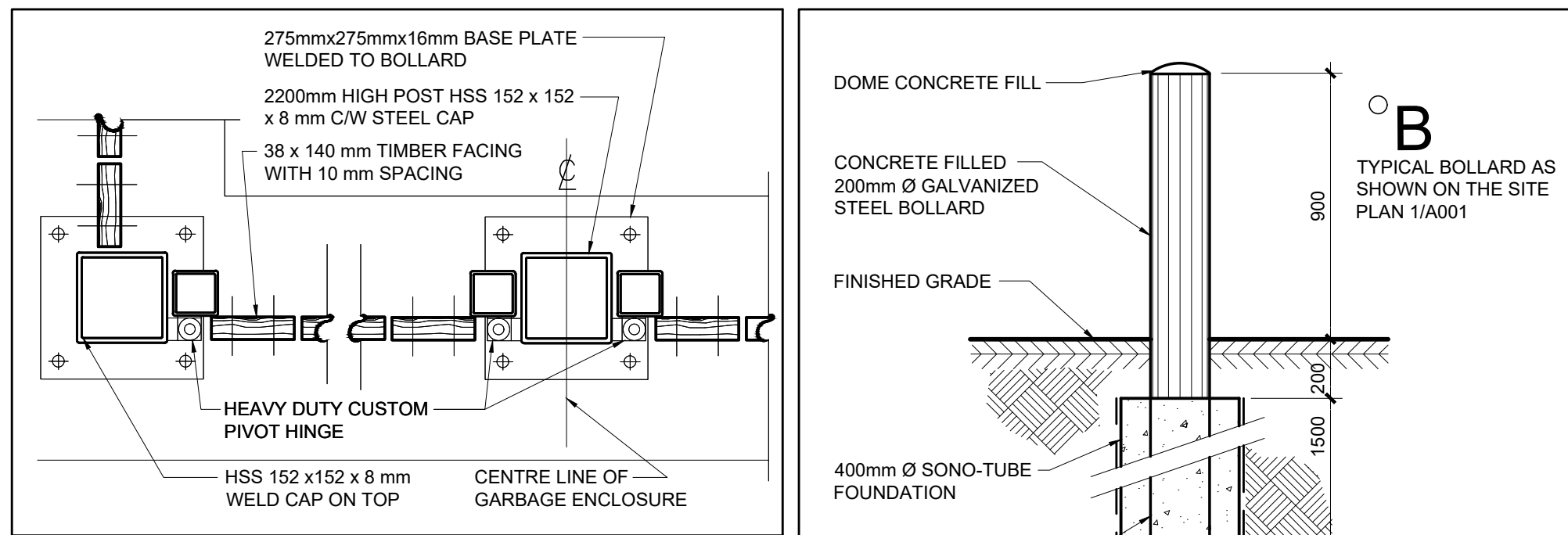
3 GARBAGE ENCLOSURE ELEVATION
SCALE 1:50

4 PLAN DETAIL
SCALE 1:10

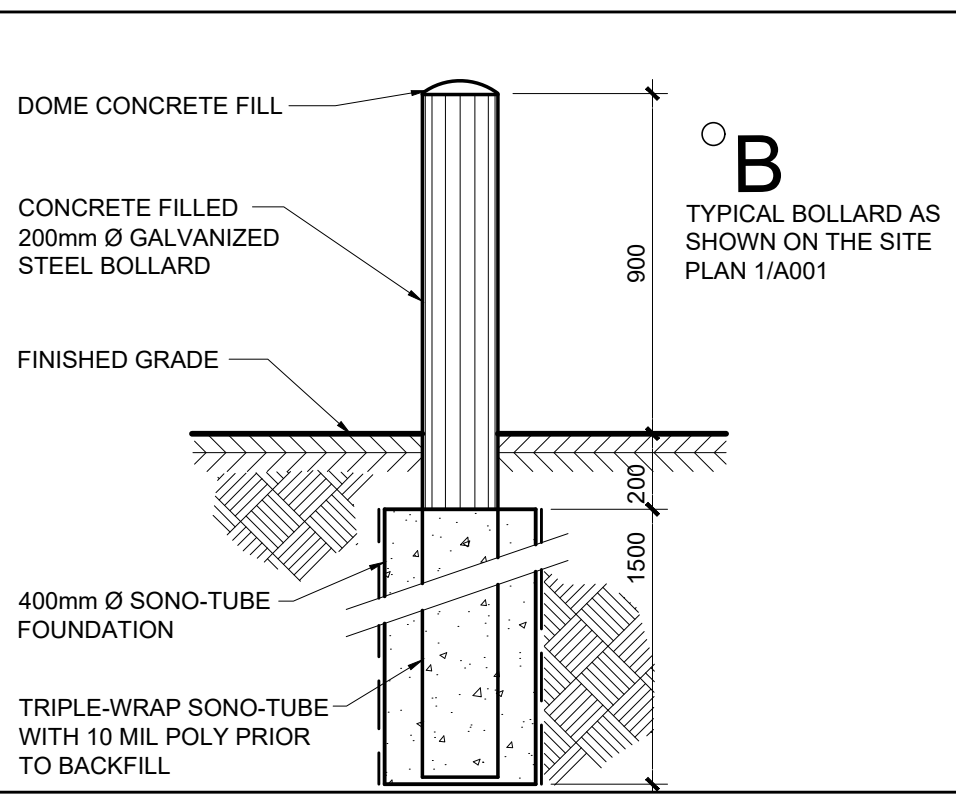


5 GARBAGE ENCLOSURE SECTION DETAIL
SCALE 1:10

6 GARBAGE ENCLOSURE SECTION DETAIL
SCALE 1:10



7 GARBAGE ENCLOSURE PLAN DETAIL
SCALE 1:10



8 BOLLARD DETAIL
SCALE 1:20

ZONING INFORMATION		
NOTE: ALL ZONING DEFINITIONS AND REQUIREMENTS AS PER CITY OF OTTAWA ZONING BY-LAW 2008-250		
ZONING MECHANISM	REQUIRED	PROVIDED
DEFINITION	RG3 (385) RURAL GENERAL INDUSTRIAL ZONE	BUILDING #1: WAREHOUSE, RETAIL STORE, BAR (25%) BUILDING #2: WAREHOUSE
MIN. LOT WIDTH	30.0 m	110.0 m
MIN. LOT AREA	2,000 m ²	22,680 m ² (± 5.6 Acres)
MIN. FRONT YARD SETBACK	15.0 m	45.0 m
MIN. REAR YARD SETBACK	15.0 m	110.0 m
MIN. INTERIOR SIDE YARD SETBACK	3.0 m	9.0 m
MAX. LOT COVERAGE	35%	2.85%
PARKING LANDSCAPE BUFFER	FOR A PARKING LOT CONTAINING 10-100 SPACES: ABUTTING A STREET = 3 m NOT ABUTTING A STREET = 1.5 m	ABUTTING A STREET 3 m NOT ABUTTING A STREET 3 m
STANDARD PARKING SPACE	2.6m WIDTH x 5.2m LENGTH	2.6m WIDTH x 5.2m LENGTH
PARALLEL PARKING SPACE	2.6m WIDTH x 6.7m LENGTH	2.6m WIDTH x 6.7m LENGTH
ACCESSIBLE PARKING SPACE	3.4x5.2m (A); 2.4x5.2m(B)	3.4x5.2m (A); 2.4x5.2m(B)
PARKING REQUIREMENTS	BUILDING#1: LIGHT INDUSTRIAL USE (N49): 0.8 PER 100 m ² OF GFA (3.405 REQUIRED) RETAIL STORE (N79): 3.4 PER 100m ² OF GFA (2.75 REQUIRED) BAR (N15): 6 PER 100m ² OF GFA (6.48 REQUIRED) TOTAL REQUIRED: 12.725 BUILDING#2: LIGHT INDUSTRIAL USE (N49): 0.8 PER 100 m ² OF GFA (8.336 REQUIRED)	BUILDING#1: 19 PARKING SPACES BUILDING#2: 9 PARKING SPACES
BARRIER FREE ACCESSIBLE	AS PER CITY OF OTTAWA ACCESSIBILITY DESIGN STANDARDS, PARAGRAPH 3.1.2, TABLE 3 1 TYPE 'A', 1 TYPE 'B'	BUILDING#1: 2 ACCESSIBLE PARKING SPACES (1xTYPE 'A' + 1xTYPE 'B') BUILDING#2: 2 ACCESSIBLE PARKING SPACES (1xTYPE 'A' + 1xTYPE 'B')
LOADING SPACES	GFA 350-999m ² - 0 required	0 PROVIDED
BICYCLE PARKING RATE	BUILDING#1: LIGHT INDUSTRIAL USE: 1 PER 1,000 m ² OF GFA (0.4365 REQUIRED) RETAIL STORE: 1 PER 250 m ² OF GFA (0.32 REQUIRED) BAR: 1 PER 1,500 m ² OF GFA (0.072) TOTAL REQUIRED: 0.8285 BUILDING#2: LIGHT INDUSTRIAL USE: 1 PER 1,000 m ² OF GFA (1.042 REQUIRED)	BUILDING#1: 6 BICYCLE SPACES BUILDING#2: 6 BICYCLE SPACES

PROJECT INFORMATION (BUILDING#1):

BUILDING CLASSIFICATION:
THE BUILDING IS CLASSIFIED AND DESIGNED TO CONFORM TO THE ONTARIO BUILDING CODE 2024 (CURRENT EDITION) PART 3

MAJOR OCCUPANCY:
GROUP F, DIVISION 2, SPRINKLERED, UP TO TWO STOREY (3.2.2.72)
MINOR OCCUPANCIES:
GROUP E, AND GROUP D

BUILDING STATISTICS:
BUILDING AREA (FOOTPRINT): 623 sq.m.
BUILDING GFA: 738 sq.m.
NUMBER OF STOREYS: 1 (+MEZZANINE)
BUILDING SPRINKLERED: YES
OF STREET ACCESS ROUTES: 1
CONSTRUCTION TYPE: NON-COMB.
FLOOR ASSEMBLY & F.R.R.: 1 HOUR

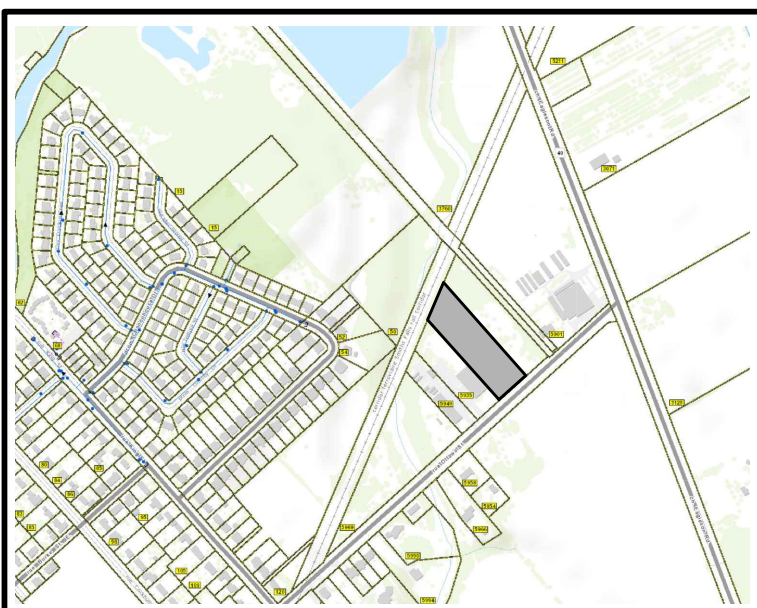
PROJECT INFORMATION (BUILDING#2):
BUILDING CLASSIFICATION:
THE BUILDING IS CLASSIFIED AND DESIGNED TO CONFORM TO THE ONTARIO BUILDING CODE 2024 (CURRENT EDITION) PART 3

MAJOR OCCUPANCY:
GROUP F, DIVISION 2, SPRINKLERED, UP TO TWO STOREY (3.2.2.72)
MINOR OCCUPANCIES:
GROUP D

BUILDING STATISTICS:
BUILDING AREA (FOOTPRINT): 925 sq.m.
BUILDING GFA: 1,042 sq.m.
NUMBER OF STOREYS: 1 (+MEZZANINE)
BUILDING SPRINKLERED: YES
OF STREET ACCESS ROUTES: 1
CONSTRUCTION TYPE: NON-COMB.
FLOOR ASSEMBLY & F.R.R.: 1 HOUR

TOPOGRAPHICAL PLAN INFORMATION:
SURVEY PROPERTY BOUNDARIES TAKEN FROM TOPOGRAPHICAL PLAN, PLAN OF SURVEY OF PART OF UNIT 10, INDEX PLAN D-26, GEOGRAPHIC TOWNSHIP OF GOULBOURN, CITY OF OTTAWA

PREPARED BY EGIS SURVEYING INC., JULY 9, 2024



KEY PLAN

2	ISSUED FOR SPA	15MAY25
1	ISSUED FOR SITE PLAN CONTROL	07OCT24
no.	revision	date

N45 ARCHITECTURE INC.
71 Bank Street, 7th floor - Ottawa, Ontario, K1P 5N2
tel. 613.224.0095 fax 613.224.9811

project
FOXRUN RICHMOND

5923 OTTAWA STREET
OTTAWA, ON

project north

seal
ONTARIO ASSOCIATION
OF
ARCHITECTS
VLADIMIR POPOVIC
LICENCE
5918

drawing title
SITE PLAN

scale AS NOTED	drawn by NF
date JUNE 2022	checked by VP
project number 24-826	drawing number A-001
CONTRACTOR TO VERIFY ALL DIMENSIONS AND NOTIFY THE ARCHITECT OF ANY DISCREPANCIES BEFORE WORK COMMENCES. DO NOT SCALE DRAWINGS.	
revision -	

APPENDIX C WATERMAIN CALCULATIONS

000-25-0415 - 5923 Ottawa Street - Water Demands - Phase 1

Project:	5923 Ottawa Street
Project No.:	000-25-0415
Designed By:	FV
Checked By:	AG
Date:	June 6, 2025
Development Area:	0.48 gross ha

Commercial	190 m2
Industrial - Light (Distillery)	432 m2

AVERAGE DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS
Residential	280	L/c/d
Industrial - Light	35,000	L/gross ha/d
Industrial - Heavy	55,000	L/gross ha/d
Shopping Centres	2,500	L/(1000m ² /d)
Hospital	900	L/(bed/day)
Schools	70	L/(Student/d)
Trailer Park with no Hook-Ups	340	L/(space/d)
Trailer Park with Hook-Ups	800	L/(space/d)
Campgrounds	225	L/(campsite/d)
Mobile Home Parks	1,000	L/(Space/d)
Motels	150	L/(bed-space/d)
Hotels	225	L/(bed-space/d)
Tourist Commercial	28,000	L/gross ha/d
Other Commercial	28,000	L/gross ha/d
AVERAGE DAILY DEMAND	Residential	0.00 L/s
	Commercial/ Industrial/ Institutional	0.02 L/s

MAXIMUM DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS
Residential	9.5 x avg. day	L/c/d
Industrial	1.5 x avg. day	L/gross ha/d
Commercial	1.5 x avg. day	L/gross ha/d
Institutional	1.5 x avg. day	L/gross ha/d
MAXIMUM DAILY DEMAND	Residential	0.00 L/s
	Commercial/ Industrial/ Institutional	0.04 L/s

MAXIMUM HOUR DEMAND

DEMAND TYPE	AMOUNT	UNITS
Residential	14.3 x avg. day	L/c/d
Industrial	1.8 x max. day	L/gross ha/d
Commercial	1.8 x max. day	L/gross ha/d
Institutional	1.8 x max. day	L/gross ha/d
MAXIMUM HOUR DEMAND	Residential	0.00 L/s
	Commercial/ Industrial/ Institutional	0.06 L/s

WATER DEMAND DESIGN FLOWS PER UNIT COUNT
CITY OF OTTAWA - WATER DISTRIBUTION GUIDELINES, JULY 2010

AVERAGE DAILY DEMAND	0.02	L/s
MAXIMUM DAILY DEMAND	0.04	L/s
MAXIMUM HOUR DEMAND	0.06	L/s

000-25-0415 - 5923 Ottawa Street - Water Demands - Phase 2

Project:	5923 Ottawa Street
Project No.:	000-25-0415
Designed By:	FV
Checked By:	AG
Date:	June 6, 2025
Development Area:	0.45 gross ha

Industrial - Light (Brewery)

926 m2

AVERAGE DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS
Residential	280	L/c/d
Industrial - Light	35,000	L/gross ha/d
Industrial - Heavy	55,000	L/gross ha/d
Shopping Centres	2,500	L/(1000m ² /d)
Hospital	900	L/(bed/day)
Schools	70	L/(Student/d)
Trailer Park with no Hook-Ups	340	L/(space/d)
Trailer Park with Hook-Ups	800	L/(space/d)
Campgrounds	225	L/(campsite/d)
Mobile Home Parks	1,000	L/(Space/d)
Motels	150	L/(bed-space/d)
Hotels	225	L/(bed-space/d)
Tourist Commercial	28,000	L/gross ha/d
Other Commercial	28,000	L/gross ha/d
AVERAGE DAILY DEMAND	Residential	0.00 L/s
	Commercial/ Industrial/ Institutional	0.04 L/s

MAXIMUM DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS
Residential	9.5 x avg. day	L/c/d
Industrial	1.5 x avg. day	L/gross ha/d
Commercial	1.5 x avg. day	L/gross ha/d
Institutional	1.5 x avg. day	L/gross ha/d
MAXIMUM DAILY DEMAND	Residential	0.00 L/s
	Commercial/ Industrial/ Institutional	0.06 L/s

MAXIMUM HOUR DEMAND

DEMAND TYPE	AMOUNT	UNITS
Residential	14.3 x avg. day	L/c/d
Industrial	1.8 x max. day	L/gross ha/d
Commercial	1.8 x max. day	L/gross ha/d
Institutional	1.8 x max. day	L/gross ha/d
MAXIMUM HOUR DEMAND	Residential	0.00 L/s
	Commercial/ Industrial/ Institutional	0.10 L/s

WATER DEMAND DESIGN FLOWS PER UNIT COUNT

CITY OF OTTAWA - WATER DISTRIBUTION GUIDELINES, JULY 2010

AVERAGE DAILY DEMAND	0.04	L/s
MAXIMUM DAILY DEMAND	0.06	L/s
MAXIMUM HOUR DEMAND	0.10	L/s

000-25-0415 - 5923 Ottawa Street - Phase 1 OBC Fire Calculations

Project:	5923 Ottawa Street
Project No.:	000-25-0415
Designed By:	FV
Checked By:	AG
Date:	June 6, 2025

Ontario 2006 Building Code Compendium (Div. B - Part 3)

Water Supply for Fire-Fighting - Distillery, Restaurant & Retail Building

Building is classified as Group : E and F2 up to 2 Storeys (from table 3.2.2.55)
 Building is of noncombustible construction with fire separations and fire-resistance ratings provided in accordance with subsections 3.2.2., including loadbearing walls, columns and arches

From Div. B A-3.2.5.7. of the Ontario Building Code - 3. Building On-Site Water Supply:

(a) $Q = K \times V \times S_{tot}$

where:

Q = minimum supply of water in litres

K = water supply coefficient from Table 1

V = total building volume in cubic metres

S_{tot} = total of spatial coefficient values from the property line exposures on all sides as obtained from the formula:

$S_{tot} = 1.0 + [S_{side1} + S_{side2} + S_{side3} + \dots \text{etc.}]$

K	17	(from Table 1 pg A-31)
V	4,125	(Total building volume in m ³ .)
S_{tot}	1.1	(From figure 1 pg A-32)
Q =	77,137.50 L	



			From Figure 1 (A-32)
Shorth	111	m	0.0
Seast	26	m	0.0
Ssouth	45	m	0.0
Swest	9	m	0.1

* approximate distances

From Table 2: Required Minimum Water Supply Flow Rate (L/s)

2,700 L/min if $Q < 108,000$ L
 713 gpm

000-25-0415 - 5923 Ottawa Street - Phase 2 OBC Fire Calculations

Project:	5923 Ottawa Street
Project No.:	000-25-0415
Designed By:	FV
Checked By:	AG
Date:	June 6, 2025

Ontario 2006 Building Code Compendium (Div. B - Part 3)

Water Supply for Fire-Fighting - Brewery

Building is classified as Group : E and F2 up to 2 Storeys (from table 3.2.2.55)
 Building is of noncombustible construction with fire separations and fire-resistance ratings provided in accordance with subsections 3.2.2., including loadbearing walls, columns and arches

From Div. B A-3.2.5.7. of the Ontario Building Code - 3. Building On-Site Water Supply:

$$(a) Q = K \times V \times S_{tot}$$

where:

Q = minimum supply of water in litres

K = water supply coefficient from Table 1

V = total building volume in cubic metres

S_{tot} = total of spatial coefficient values from the property line exposures on all sides as obtained from the formula:

$$S_{tot} = 1.0 + [S_{side1} + S_{side2} + S_{side3} + \dots \text{etc.}]$$

K	17	(from Table 1 pg A-31)
V	7,200	(Total building volume in m ³ .)
S _{tot}	1.0	(From figure 1 pg A-32)
Q =	122,400.00 L	

From Table 2: Required Minimum Water Supply Flow Rate (L/s)

3,600 L/min if Q > 108,000 L and < 135,000 L
 951 gpm

From Figure 1 (A-32)

Shorth	135	m	0.0
* Seast	17	m	0.0
Ssouth	57	m	0.0
Swest	18	m	0.0

* east exposure measured from centre of road allowance.

APPENDIX D SANITARY DESIGN

000-25-0415 - 5923 Ottawa Street - Sanitary Demands - Phase 1

Project:	5923 Ottawa Street
Project No.:	000-25-0415
Designed By:	FV
Checked By:	JB
Date:	May 5, 2025

Site Area	0.48	Gross ha
Commercial Area (Retail)	90	m ²
Industrial - Light (Distillery)	432	m ²
Restaurant	363	m ²

DESIGN PARAMETERS

Institutional/ Commercial Peaking Factor	1.5
Mannings coefficient (n)	0.013
Infiltration allowance	0.33 L/s/Ha

EXTRANEOUS FLOW ALLOWANCES

Infiltration / Inflow	Flow (L/s)
Dry	0.02
Wet	0.13
Total	0.16

AVERAGE DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS	POPULATION / AREA	Flow (L/s)
Residential	280	L/c/d		0.0
Industrial - Light**	35,000	L/gross ha/d	0.04	0.02
Industrial - Heavy**	55,000	L/gross ha/d		0
Commercial / Amenity	2,800	L/(1000m ² /d)	90	0.00
Restaurant	125	L/(9.2m ² /d)	363	0.06
Schools	70	L/(Student/d)		0
Trailer Parks no Hook-Ups	340	L/(space/d)		0
Trailer Park with Hook-Ups	800	L/(space/d)		0
Campgrounds	225	L/(campsite/d)		0
Mobile Home Parks	1,000	L/(Space/d)		0
Motels	150	L/(bed-space/d)		0
Hotels	225	L/(bed-space/d)		0
Office	75	L/7.0m ² /d		0
Tourist Commercial	28,000	L/gross ha/d		0
Other Commercial	28,000	L/gross ha/d		0

AVERAGE RESIDENTIAL FLOW	0.00	L/s
PEAK RESIDENTIAL FLOW	0.00	L/s
AVERAGE ICI FLOW	0.08	L/s
TOTAL PEAK ICI FLOW	0.12	L/s

TOTAL SANITARY DEMAND

TOTAL ESTIMATED AVERAGE DRY WEATHER FLOW	0.10	L/s
TOTAL ESTIMATED PEAK DRY WEATHER FLOW	0.14	L/s
TOTAL ESTIMATED PEAK WET WEATHER FLOW	0.27	L/s

000-25-0415 - 5923 Ottawa Street - Sanitary Demands - Phase 2

Project:	5923 Ottawa Street
Project No.:	000-25-0415
Designed By:	FV
Checked By:	JB
Date:	May 5, 2025

Site Area	0.45 Gross ha
Industrial - Light (Distillery)	926 m ²

DESIGN PARAMETERS

Institutional/ Commercial Peaking Factor	1.5
Mannings coefficient (n)	0.013
Infiltration allowance	0.33 L/s/Ha

EXTRANEOUS FLOW ALLOWANCES

Infiltration / Inflow	Flow (L/s)
Dry	0.02
Wet	0.13
Total	0.15

AVERAGE DAILY DEMAND

DEMAND TYPE	AMOUNT	UNITS	POPULATION / AREA	Flow (L/s)
Residential	280	L/c/d		0
Industrial - Light**	35,000	L/gross ha/d	0.04	0.02
Industrial - Heavy**	55,000	L/gross ha/d		0
Commercial / Amenity	2,800	L/(1000m ² /d)		0
Restaurant	125	L/(9.2m ² /d)		0
Schools	70	L/(Student/d)		0
Trailer Parks no Hook-Ups	340	L/(space/d)		0
Trailer Park with Hook-Ups	800	L/(space/d)		0
Campgrounds	225	L/(campsite/d)		0
Mobile Home Parks	1,000	L/(Space/d)		0
Motels	150	L/(bed-space/d)		0
Hotels	225	L/(bed-space/d)		0
Office	75	L/7.0m ² /d		0
Tourist Commercial	28,000	L/gross ha/d		0
Other Commercial	28,000	L/gross ha/d		0

AVERAGE RESIDENTIAL FLOW	0.00	L/s
PEAK RESIDENTIAL FLOW	0.00	L/s
AVERAGE IQ FLOW	0.02	L/s
TOTAL PEAK IQ FLOW	0.03	L/s

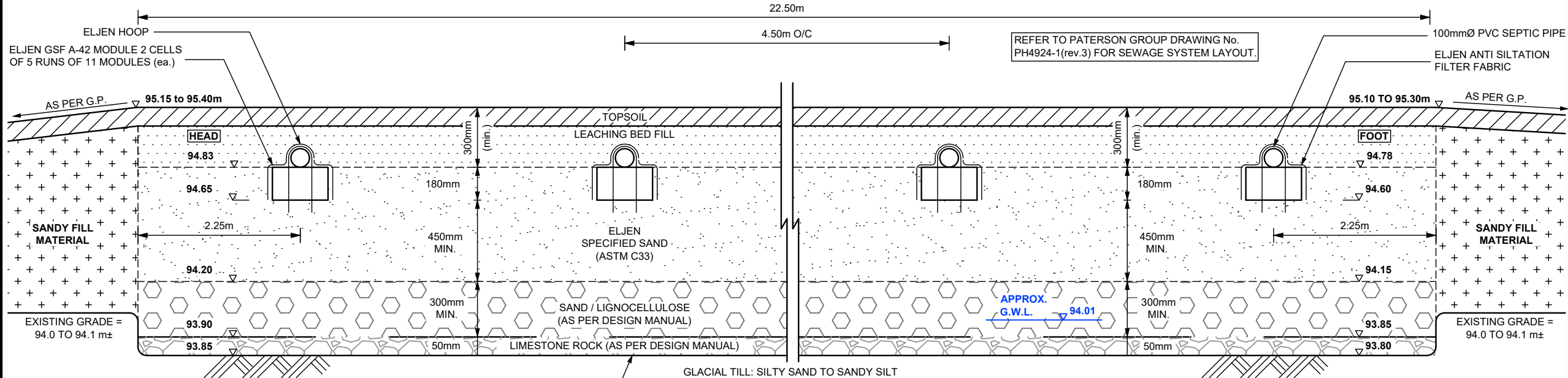
TOTAL SANITARY DEMAND

TOTAL ESTIMATED AVERAGE DRY WEATHER FLOW	0.04	L/s
TOTAL ESTIMATED PEAK DRY WEATHER FLOW	0.05	L/s
TOTAL ESTIMATED PEAK WET WEATHER FLOW	0.17	L/s

COVER MATERIAL TO CONSIST OF LEACHING BED FILL FOLLOWED BY APPROX. 100mm OF SANDY TOPSOIL. LEACHING BED TO BE VEGETATED AS SOON AS POSSIBLE.

SEWAGE SYSTEM DESIGN, SPECIFICATION, DETAILS AND NOTES HAVE BEEN COMPLETED IN ACCORDANCE WITH ELJEN DENITRIFICATION SUPPLEMENTAL DESIGN AND INSTALLATION MANUAL.

FINAL GRADING SHALL BE SUITABLY SHAPED TO DIRECT SURFACE WATER AWAY FROM THE PROPOSED SEWAGE SYSTEM.



NOTES:

1) ESTIMATE OF DAILY SEWAGE FLOW (Q)

THE PROPOSED SEWAGE SYSTEM HAS BEEN DESIGNED TO SUPPORT A COMMERCIAL TYPE USAGE CONSISTING OF OFFICE, STORE, WAREHOUSE AND RESTAURANT SPACE. THE DAILY DESIGN SEWAGE FLOW RATE IS CALCULATED IN ACCORDANCE WITH O.B.C. TABLE 8.2.1.3.B.

OFFICE SPACE:

- 70m² / 9.3 x 75 L/DAY = 565 L/DAY

STORE SPACE:

- 75 25m² x 5 L/DAY = 376.25 L/DAY

WAREHOUSE SPACE:

- 2 LOADING BAY x 150 L/DAY = 300 L/DAY

RESTAURANT/BAR:

- 65 SEATS x 125 L/DAY = 8,125 L/DAY

TOTAL DESIGN DAILY SANITARY SEWAGE FLOW = 9,367 L/DAY

2) SOIL CONDITIONS

SOILS INFORMATION GATHERED BY PATERSON GROUP INC. ON JUNE 17, 2024. REFER TO PATERSON GROUP REPORT PG7381-1 FOR FULL SOILS BREAKDOWN.

BH 4-24, ELEV. 94.11m

0-0.13	TOPSOIL AND ORGANICS
0.13-3.33	GLACIAL TILL: DENSE BROWN SILTY SAND, TO SANDY SILT WITH GRAVEL, COBBLES AND BOULDERS, SOME TO TRACE CLAY

- G.W.L. @ 0.10m DEPTH (94.01m)

3) PRETREATMENT TANK

- TANK SHALL BE CONNECTED TO BUILDING BY A 150mm Ø PVC PIPE SLEEVED THROUGH A 200mmØ PVC SDR 28 PIPE AND OVERLAIN WITH 50mm T x 600mm W RIGID INSULATION BOARDS (UNDER ROADWAY) AND SHALL BE INSTALLED AT 2.0% (min.) SLOPE TO THE PRETREATMENT TANK.
- MINIMUM WORKING CAPACITY OF PRETREATMENT TANK = (3 x Q) = 3 x 9,367 L/DAY = 28,101 L (min.)
- IT IS RECOMMENDED THAT A NEW 28,101L (min.) TWO-COMPARTMENT SEPTIC TANK BE INSTALLED.
- AN OBC APPROVED EFFLUENT FILTER (I.E. POLYLOK PL-525 EFFLUENT FILTER, OR EQUIVALENT) SHALL BE INSTALLED ON THE OUTLET PIPE IN THE PRETREATMENT TANK.
- THE ACCESS LIDS TO THE TANK OPENINGS SHALL BE EXTENDED TO THE GROUND SURFACE. INSTALL RISERS AND COVERS TO SUIT.
- ACCESS LIDS SHALL INCLUDE SAFETY DEVICES AS PER CSA B66-21.
- TANK SHALL BE CPA APPROVED (OR ENGINEERED) FOR 1.2m (min.) OF COVER MATERIAL.
- TANK SHALL BE REVIEWED FOR BALLASTING REQUIREMENTS.

4) BALANCING TANK

- INSTALL A 18,500L (min.) BALANCING TANK IN SERIES AND DOWNSTREAM FROM THE NEW SEPTIC TANK.
- A TIME OPERATED ALTERNATING DUPLEX PUMPING SYSTEM (I.E. MYERS ME3F, OR SIMILAR) AND A HIGH WATER ALARM SHALL BE INSTALLED IN THE BALANCING TANK.
- THE TIME OPERATIONAL PUMPING SYSTEM SHALL OPERATE EVERY HOUR (I.E. 391 L/DOSE + VOLUME TO CHARGE THE SYSTEM) AND SHALL ALTERNATE BETWEEN EACH CELL.
- A 3mmØ DRAIN HOLE SHALL BE INSTALLED IN THE UNDERSIDE OF THE FORCEMAIN IN THE BALANCING TANK NEAR THE WALL CONNECTION.
- RISERS WITH A COVER SHALL BE INSTALLED OVER THE BALANCING TANK TO PROVIDE ACCESS FROM THE GROUND SURFACE.
- DISCHARGE PIPING FOR PUMP SHALL BE CONFIGURED SUCH THAT THE PUMP IS EASILY SERVICED FROM THE GROUND SURFACE.

5) DISTRIBUTION BOX / FORCEMAIN

- A 38mmØ (NOMINAL) PVC SCH 40 FORCEMAIN (2) SHALL BE USED TO CARRY THE EFFLUENT FROM THE BALANCING TANK TO EACH 3m L x 100mm Ø PVC SEWER PIPE.
- 100mm SEWER PIPE SHALL DRAIN BY GRAVITY TO A 5 OUTLET DISTRIBUTION BOX.
- THE FORCE MAIN SHALL BE INSTALLED TO GRAVITY DRAIN TO THE BALANCING TANK
- THE FORCE MAIN SHALL BE OVERLAIN WITH 50mm T x 600mm C/W RIGID INSULATION.
- THE DISTRIBUTION BOX SHALL BE EQUIPPED WITH AN INLET Baffle AND OUTLET PIPES (5).
- EACH PIPING RUN SHALL BE FED BY A 5 OUTLET DISTRIBUTION BOX.
- THE DISTRIBUTION BOX SHALL BE CONNECTED TO THE DISTRIBUTION PIPING RUNS USING 100mmØ SOLID PVC SEWER PIPE @ 2% (min.) SLOPE.

6) LEACHING BED SIZING CRITERIA

- NO. OF MODULES REQUIRED = Q/95 = 9,367/95 = 98.6 MODULES
- USE 2 CELLS OF 5 RUNS OF 11 (110) ELJEN GSF A-42 MODULES EACH
- SAND AREA REQUIRED = QT/400 = 9,367(35)/400 = 819.7m²
- SAND AREA PROVIDED = 37.24m x 22.50m = 837.90m² (min.)

7) LEACHING BED CONSTRUCTION GUIDELINES

- REMOVE ALL EXISTING TOPSOIL, AND ANY FILL WITHIN LIMITS OF THE SAND AREA AND SUBEXCAVATE TO AT LEAST ELEVATION 93.80m TO 93.85m, WHICHEVER IS GREATER. RE-ESTABLISH THE SPECIFIED CONTACT LEVEL USING SELECT SAND FILL, WHERE REQUIRED.
- THE SUBGRADE SURFACE SHALL BE SCARIFIED, UNDER DRY CONDITIONS.
- PLACE A 50mm MIN. THICK LAYER OF LIMESTONE ROCK OVER THE SUITABLY PREPARED SUBGRADE.
- LIMESTONE ROCK SHALL NO SMALLER THAN 25mm IN DIAMETER UP TO 50mm IN DIAMETER. THE ROCK SHALL CONTAIN GREATER THAN 15% LIMESTONE AS PER ELJEN DENITRIFICATION SUPPLEMENTAL DESIGN AND INSTALLATION MANUAL.
- PLACE A 300mm THICK LAYER OF SAND / LIGNOCELLULOSE OVER THE LIMESTONE ROCK LAYER.
- SAND / LIGNOCELLULOSE SHALL CONSIST OF WOOD CHIPS OR SAW DUST FROM HARD WOOD TREES THAT HAVE NOT BEEN FURTHER PROCESSED BY CHEMICALS. THE 300mm SAND AND LIGNOCELLULOSE LAYER SHALL BE 50/50 EQUAL MIXTURE OF ASTM C33 SAND AND WOOD CHIPS FROM HARD WOOD TREES. THE MIXTURE MUST NOT EXCEED 60/40 IN FAVOR OF THE MORE WOOD TO SAND.
- PLACE A 450mm MIN. THICK LAYER OF ELJEN SPECIFIED SAND FILL OVER THE LEACHING BED FILL.
- THE ELJEN SPECIFIED SAND FILL SHALL CONSIST OF WASHED SAND MEETING THE REQUIREMENTS OF ASTM C33 "STANDARD SPECIFICATION FOR CONCRETE AGGREGATES" WITH LESS THAN 5% PASSING 0.075mm SIEVE. ELJEN SPECIFIED SAND FILL SHALL BE PRE-APPROVED BY THE CONSULTANT.
- THE MODULES SHALL BE INSTALLED IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS.
- THE MODULES SHALL BE INSTALLED AT A SLOPE OF 0.3%(min.) TO 0.5%(max.), END TO END AND WITH THE WHITE DEMARCATION LINE FACING UP.
- THE MODULAR BASE LEVEL (ELEV. 94.60m AT THE FOOT, TO 94.65m AT THE HEAD) SHALL BE ESTABLISHED WITH ELJEN SPECIFIED SAND FILL, HAVING A MINIMUM THICKNESS OF 450mm BELOW THE MODULES.
- THE ELJEN MODULES SHALL BE FED BY GRAVITY BY A 100mmØ PVC SEWER PIPE @ 2% (min.) SLOPE FROM THE DISTRIBUTION BOX
- THE DISTRIBUTION PIPE SHALL CONSIST OF A 100mmØ PERFORATED PVC PIPE CENTRED OVER THE MODULES. THE PIPE SHALL BE SECURED TO THE TOP OF THE MODULES USING AN ELJEN HOOP (MINIMUM 1 HOOP PER MODULE).
- THE INVERT LEVEL OF THE DISTRIBUTION PIPE SHALL BE SET ON THE MODULES AT ELEVATION 94.78m AT THE FOOT TO 94.83m AT THE HEAD. THE END OF THE PIPE RUNS SHALL BE CONNECTED TO A 100mmØ SOLID PVC FOOTER PIPE
- INSTALL ELJEN SYSTEM SAMPLING DEVICE AS PER MANUFACTURER'S RECOMMENDATIONS.
- THE ELJEN ANTI-SILTATION FILTER FABRIC SHALL BE SPREAD LENGTHWISE OVER THE PERFORATED SEPTIC PIPE AND DOWN THE SIDES OF THE MODULES. ENSURE ENDS OF MODULES ARE ALSO COVERED WITH FABRIC.
- THE MODULES SHALL BE BACKFILLED, WITH ELJEN SPECIFIED SAND FILL TO AT LEAST THE TOP OF THE ELJEN MODULES, FOLLOWED BY 200mm (min.) OF LEACHING BED FILL, FOLLOWED BY 100mm OF SANDY TOPSOIL, WITHIN THE LIMITS OF THE SAND AREA. THE BED AREA SHOULD BE VEGETATED AS SOON AS POSSIBLE.
- LEACHING BED SAND FILL SHALL BE UNIFORM SAND WITH GRADING LIMITS SIMILAR TO 100% PASSING 13.2mm SIEVE, LESS THAN 5% PASSING 0.075mm SIEVE, AND HAVING A PERCOLATION TIME OF 6 TO 8 min/cm. LEACHING BED FILL SHALL BE PRE-APPROVED BY THE CONSULTANT.

- THE SIDES OF THE BED SHOULD BE SLOPED AT 3H:1V OR SHALLOWER.
- VENT SYSTEM SHALL BE INSTALLED ON THE FOOTER PIPE. CONNECT A 100mmØ PVC VENT PIPE TO FOOTER PIPE, EXTENDING TO GROUND SURFACE. VENT PIPE TO BE INSTALLED IN 150mmØ LANDSCAPE VALVE COVER.

8) MINIMUM CLEARANCE DISTANCE FROM DISTRIBUTION PIPE

- 5.6m FROM ANY PROPERTY LINE
- 7.6m FROM ANY STRUCTURE: 5.0m FROM ANY BASEMENTLESS STRUCTURE
- 17.6m FROM ANY DRILLED WELL
- 5.0m FROM ANY TREE (UNLESS OTHERWISE APPROVED)

9) MINIMUM CLEARANCE DISTANCE FROM TANK(S)

- 1.5m FROM ANY STRUCTURE
- 15.0m FROM ANY DRILLED OR DUG WELL
- 3.0m FROM ANY PROPERTY LINE

10) GENERAL

- SNOW STORAGE SHALL NOT BE LOCATED OVER OR UPGRADIENT OF THE PROPOSED SEWAGE SYSTEM.**
- THE SEWAGE SYSTEM HAS NOT BEEN DESIGNED TO SUPPORT TRAFFIC LOADING.
- THE BACKFILLING OF THE SEWAGE SYSTEM SHOULD MINIMIZE THE RISK OF OVER COMPACTION WITH THE USE RUBBER TRACKED EQUIPMENT AND BY AVOIDING THE CREATION OF ANY CONSTRUCTION ROUTES OR PATHWAYS OVER THE SYSTEM.
- ANY NEW IRRIGATION / SPRINKLER SYSTEM SHOULD NOT BE USED IN PROXIMITY OF THE PROPOSED SEWAGE SYSTEM.
- ENSURE WALKWAYS AND/OR SHURBBERY ARE NOT PLACED WITHIN PROXIMITY OF THE TANKAGE.
- THE BACKWASH WATERS FROM ANY WATER TREATMENT UNIT, SUCH AS WATER SOFTENER, SHOULD NOT DISCHARGE INTO THE SEWAGE SYSTEM.
- THE SEWAGE SYSTEM HAS NOT BEEN DESIGNED FOR THE USE OF A GARBAGE DISPOSAL.
- SEWAGE SYSTEM INSTALLER SHALL BE QUALIFIED AND REGISTERED UNDER PART 8 OF THE ONTARIO BUILDING CODE AND SHALL BE AN AUTHORIZED ELJEN TREATMENT SYSTEM INSTALLER.
- ALL WORK SHALL BE CARRIED OUT IN ACCORDANCE WITH THE LATEST BY-LAWS, CODES AND REGULATIONS.
- CONTRACTOR SHALL REVIEW DRAWINGS IN DETAIL AND SHALL INFORM THE CONSULTANT OF ANY ERRORS AND/OR OMISSIONS ON DESIGN DRAWINGS IMMEDIATELY.
- CONTRACTOR SHALL BE RESPONSIBLE TO LOCATE AND PROTECT ALL EXISTING UNDERGROUND SERVICES.
- CONTRACTOR SHALL VISIT THE SITE AND REVIEW ALL DOCUMENTATION TO BECOME FAMILIAR WITH THE SITE AND SUBSURFACE SOIL CONDITIONS TO DETERMINE SUITABLE METHODS OF CONSTRUCTION.
- THE MANUFACTURER PROVIDES A LIMITED WARRANTY OF THE SYSTEM COMPONENTS. THE OWNER OF THE SYSTEM MUST SIGN A MAINTENANCE AGREEMENT WITH THE MANUFACTURER'S REPRESENTATIVE. THE HOMEOWNER IS RESPONSIBLE FOR THE ANNUAL FEES ASSOCIATED WITH THE MAINTENANCE.
- THE FIRM OF PATERSON GROUP INC. HAS PROVIDED DESIGN SERVICES ONLY FOR THE SUBJECT SEWAGE SYSTEM. THE DESIGN HAS BEEN CARRIED OUT IN ACCORDANCE WITH THE MANUFACTURER'S GUIDELINES AND OUR INTERPRETATION OF PART 8 OF THE ONTARIO BUILDING CODE.
- INSPECTIONS BY THE CONSULTANT DURING THE INSTALLATION OF THE SYSTEM IS A REQUIREMENT OF SOME REGULATING AUTHORITIES AND IS STRONGLY RECOMMENDED BY THIS FIRM.
- THE PROPERTY LINE / SEPARATION DISTANCES SHOULD BE CONFIRMED PRIOR TO CONSTRUCTION.
- CONSTRUCTION INSPECTIONS DURING THE INSTALLATION OF THE SEWAGE SYSTEM MAY BE REQUIRED BY THE REGULATING AUTHORITY AND ARE STRONGLY RECOMMENDED BY THIS FIRM. IF THIS FIRM IS TO COMPLETE ANY CONSTRUCTION INSPECTION(S), ADDITIONAL FEES MAY BE APPLIED. CONFIRMATION OF PAYMENT WILL BE REQUIRED PRIOR TO THE INSPECTION.**
- THE TEST HOLE INFORMATION PROVIDED, IS INTENDED TO BE USED FOR DESIGN PURPOSES ONLY, AND SHOULD NOT BE RELIED UPON FOR CONSTRUCTION PURPOSES. IF DISCREPANCIES ARE FOUND DURING THE CONSTRUCTION PROCESS, IT IS THE CLIENT'S RESPONSIBILITY TO CONTACT THIS FIRM TO MAKE ANY NECESSARY COMMENTS OR REVISIONS. ADDITIONAL REVISIONS ARE NOT CONSIDERED PART OF THE DESIGN WORKS AND WILL BE CONSIDERED AS AN ADDITIONAL COST.**



Professional Engineers
Ontario

Licensed Engineering Technologist

Name: H. G. VAN DE GLIND

Number: 100647862

Limitations: Inspecting, designing, and assessing residential and commercial sewage systems, grading designs and soil analysis, and overseeing installation and compliance.

Association of Professional Engineers of Ontario

04/06/25	Issued for Septic Permit	3
14/05/25	Issued with Revised Site Plan	2
03/10/24	Issued with Revised Site Plan	1
20/09/24	Issued for Preliminary Review	0
DD/MM/YY	DESCRIPTION	REV.

Consultant:



**PATERSON
GROUP**

9 AURIGA DRIVE
OTTAWA, ON
K2E 7S9
TEL: (613) 226-7381

Client:

STRATFORD FOXRUN

Project:

PROPOSED WAREHOUSE / RESTAURANT

**5923 OTTAWA STREET
OTTAWA (RICHMOND), ONTARIO**

Drawing:

SEWAGE SYSTEM DETAILS AND NOTES SEWAGE SYSTEM 'A'

Scale:	N.T.S.	Drawn by:	HV
Date:	06/2025	Checked by:	MK

Drawing No.:

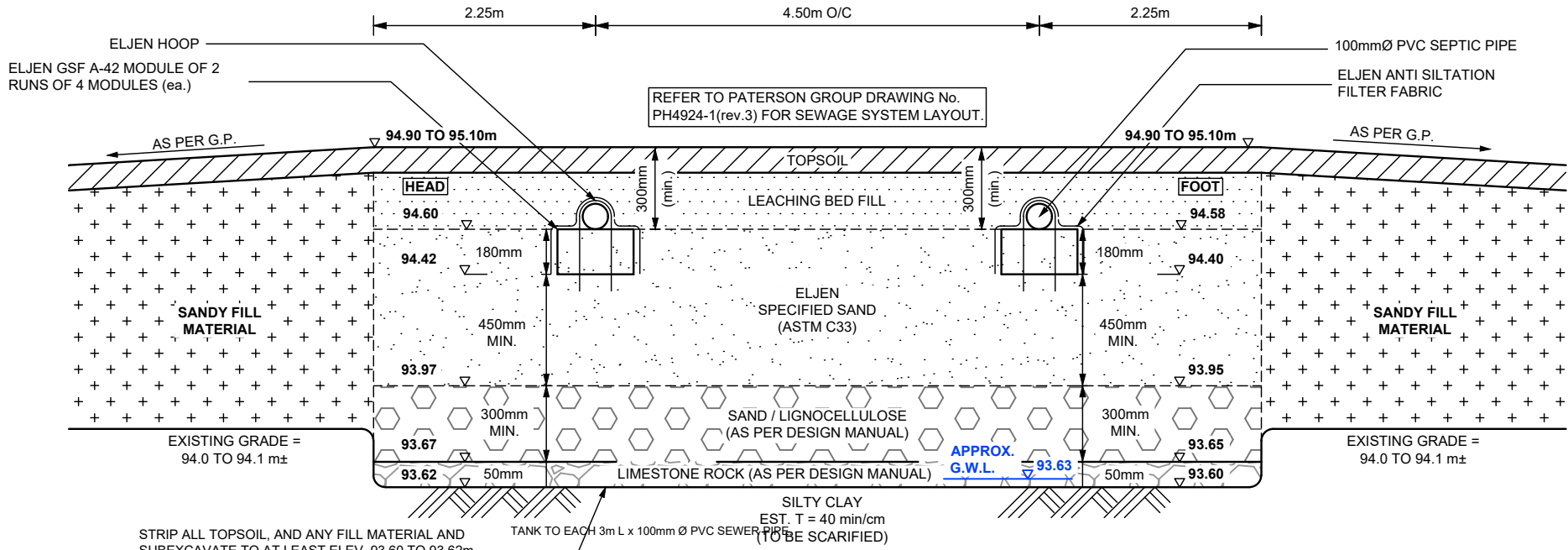
PH4924-2(rev.3)

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COVER MATERIAL TO CONSIST OF LEACHING BED FILL FOLLOWED BY APPROX. 100mm OF SANDY TOPSOIL. LEACHING BED TO BE VEGETATED AS SOON AS POSSIBLE.

SEWAGE SYSTEM DESIGN, SPECIFICATION, DETAILS AND NOTES HAVE BEEN COMPLETED IN ACCORDANCE WITH ELJEN DENITRIFICATION SUPPLEMENTAL DESIGN AND INSTALLATION MANUAL.

FINAL GRADING SHALL BE SUITABLY SHAPED TO DIRECT SURFACE WATER AWAY FROM THE PROPOSED SEWAGE SYSTEM.



NOTES:

1) ESTIMATE OF DAILY SEWAGE FLOW (Q)

THE PROPOSED SEWAGE SYSTEM HAS BEEN DESIGNED TO SUPPORT A COMMERCIAL TYPE USAGE CONSISTING OF OFFICE, AND WAREHOUSE SPACE. THE DAILY DESIGN SEWAGE FLOW RATE IS CALCULATED IN ACCORDANCE WITH O.B.C. TABLE 8.2.1.3.B.

OFFICE SPACE:

- 4 EMPLOYEES x 75 L/DAY = 300 L/DAY

WAREHOUSE SPACE:

- 2 LOADING BAY x 150 L/DAY = 300 L/DAY

TOTAL DESIGN DAILY SANITARY SEWAGE FLOW = 600 L/DAY

2) SOIL CONDITIONS

SOILS INFORMATION GATHERED BY PATERSON GROUP INC. ON JUNE 17, 2024. REFER TO PATERSON GROUP REPORT PG73781-1Rev.2 FOR FULL SOILS BREAKDOWN.

BH 1-25, ELEV. 94.07m

0-0.08 TOPSOIL AND ORGANICS
0.08-1.45 BROWN SILTY CLAY
1.45-6.60 GLACIAL TILL: BROWN SILTY SAND WITH GRAVEL, COBBLES BOULDERS AND CLAY (GREY @ 3.73 m DEPTH)

- G.W.L. @ 0.05m DEPTH (93.64m)

1) PRETREATMENT TANK

- TANK SHALL BE CONNECTED TO BUILDING BY A 150mm Ø PVC PIPE SLEEVED THROUGH A 200mmØ PVC SDR 28 PIPE AND OVERLAIN WITH 50mm T x 600mm W RIGID INSULATION BOARDS (UNDER ROADWAY) AND SHALL BE INSTALLED AT 2.0% (min.) SLOPE TO THE PRETREATMENT TANK.
- MINIMUM WORKING CAPACITY OF PRETREATMENT TANK = (3 x Q) OR 3,600 L (min.) = 3,600 L (min.)
- IT IS RECOMMENDED THAT A NEW 3,600L (min.) TWO-COMPARTMENT SEPTIC TANK BE INSTALLED.
- AN OBC APPROVED EFFLUENT FILTER (I.E. POLYLOK PL-525 EFFLUENT FILTER, OR EQUIVALENT) SHALL BE INSTALLED ON THE OUTLET PIPE IN THE PRETREATMENT TANK.
- THE ACCESS LIDS TO THE TANK OPENINGS SHALL BE EXTENDED TO THE GROUND SURFACE. INSTALL RISERS AND COVERS TO SUIT.
- ACCESS LIDS SHALL INCLUDE SAFETY DEVICES AS PER CSA B66-21.
- TANK SHALL BE CPA APPROVED (OR ENGINEERED) FOR 1.2m (min.) OF COVER MATERIAL.
- TANK SHALL BE REVIEWED FOR BALLASTING REQUIREMENTS.

4) BALANCING TANK

- INSTALL A 450L (min.) BALANCING TANK IN SERIES AND DOWNSTREAM FROM THE NEW SEPTIC TANK.
- A TIME OPERATED ALTERNATING DUPLEX PUMPING SYSTEM (I.E. MYERS ME3F, OR SIMILAR) AND A HIGH WATER ALARM SHALL BE INSTALLED IN THE BALANCING TANK.
- THE TIME OPERATIONAL PUMPING SYSTEM SHALL OPERATE EVERY HOUR (I.E. 25 L/DOSE + VOLUME TO CHARGE THE SYSTEM) AND SHALL ALTERNATE BETWEEN EACH CELL.
- A 3mmØ DRAIN HOLE SHALL BE INSTALLED IN THE UNDERSIDE OF THE FORCEMAIN IN THE BALANCING TANK NEAR THE WALL CONNECTION.
- RISERS WITH A COVER SHALL BE INSTALLED OVER THE BALANCING TANK TO PROVIDE ACCESS FROM THE GROUND SURFACE.
- DISCHARGE PIPING FOR PUMP SHALL BE CONFIGURED SUCH THAT THE PUMP IS EASILY SERVICED FROM THE GROUND SURFACE.

5) DISTRIBUTION BOX / FORCEMAIN

- A 38mmØ (NOMINAL) PVC SCH 40 FORCEMAIN (2) SHALL BE USED TO CARRY THE EFFLUENT FROM THE BALANCING

- 100mm SEWER PIPE SHALL DRAIN BY GRAVITY TO A 2 OUTLET DISTRIBUTION BOX.
- THE FORCE MAIN SHALL BE INSTALLED TO GRAVITY DRAIN TO THE BALANCING TANK
- THE FORCE MAIN SHALL BE OVERLAIN WITH 50mm T x 600mm C/W RIGID INSULATION.
- THE DISTRIBUTION BOX SHALL BE EQUIPPED WITH AN INLET BAFFLE AND OUTLET PIPES (2).
- EACH PIPING RUN SHALL BE FED BY A 2 OUTLET DISTRIBUTION BOX.
- THE DISTRIBUTION BOX SHALL BE CONNECTED TO THE DISTRIBUTION PIPING RUNS USING 100mmØ SOLID PVC SEWER PIPE @ 2% (min.) SLOPE.

6) LEACHING BED SIZING CRITERIA

- NO. OF MODULES REQUIRED = Q/95 = 600/95 = 6.3 MODULES
- USE 2 RUNS OF 4 (8) ELJEN GSF A-42 MODULES EACH
- SAND AREA REQUIRED = QT/400 = 600(40)/400 = 60m²
- SAND AREA PROVIDED = 9.60m x 9.68m = 92.9m² (min.)

7) LEACHING BED CONSTRUCTION GUIDELINES

- REMOVE ALL EXISTING TOPSOIL, AND ANY FILL WITHIN LIMITS OF THE SAND AREA AND SUBEXCAVATE TO AT LEAST ELEVATION 93.60m TO 93.62m, WHICHEVER IS GREATER. RE-ESTABLISH THE SPECIFIED CONTACT LEVEL USING SELECT SAND FILL, WHERE REQUIRED.
- THE SUBGRADE SURFACE SHALL BE SCARIFIED, UNDER DRY CONDITIONS.
- PLACE A 50mm MIN. THICK LAYER OF LIMESTONE ROCK OVER THE SUITABLY PREPARED SUBGRADE.
- LIMESTONE ROCK SHALL NO SMALLER THAN 25mm IN DIAMETER UP TO 50mm IN DIAMETER. THE ROCK SHALL CONTAIN GREATER THAN 15% LIMESTONE AS PER ELJEN DENITRIFICATION SUPPLEMENTAL DESIGN AND INSTALLATION MANUAL.
- PLACE A 300mm THICK LAYER OF SAND / LIGNOCELLULOSE OVER THE LIMESTONE ROCK LAYER.
- SAND / LIGNOCELLULOSE SHALL CONSIST OF WOOD CHIPS OR SAW DUST FROM HARD WOOD TREES THAT HAVE NOT BEEN FURTHER PROCESSED BY CHEMICALS. THE 300mm SAND AND LIGNOCELLULOSE LAYER SHALL BE 50/50 EQUAL MIXTURE OF ASTM C33 SAND AND WOOD CHIPS FROM HARD WOOD TREES. THE MIXTURE MUST NOT EXCEED 60/40 IN FAVOR OF THE MORE WOOD TO SAND.
- PLACE A 450mm MIN. THICK LAYER OF ELJEN SPECIFIED SAND FILL OVER THE LEACHING BED FILL.
- THE ELJEN SPECIFIED SAND FILL SHALL CONSIST OF WASHED SAND MEETING THE REQUIREMENTS OF ASTM C33 "STANDARD SPECIFICATION FOR CONCRETE AGGREGATES" WITH LESS THAN 5% PASSING 0.075mm SIEVE. ELJEN SPECIFIED SAND FILL SHALL BE PRE-APPROVED BY THE CONSULTANT.
- THE MODULES SHALL BE INSTALLED IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS.
- THE MODULES SHALL BE INSTALLED AT A SLOPE OF 0.3%(min.) TO 0.5%(max.), END TO END AND WITH THE WHITE DEMARCATION LINE FACING UP.
- THE MODULAR BASE LEVEL (ELEV. 94.40m AT THE FOOT, TO 94.42m AT THE HEAD) SHALL BE ESTABLISHED WITH ELJEN SPECIFIED SAND FILL, HAVING A MINIMUM THICKNESS OF 450mm BELOW THE MODULES.
- THE ELJEN MODULES SHALL BE FED BY GRAVITY BY A 100mmØ PVC SEWER PIPE @ 2% (min.) SLOPE FROM THE DISTRIBUTION BOX
- THE DISTRIBUTION PIPE SHALL CONSIST OF A 100mmØ PERFORATED PVC PIPE CENTRED OVER THE MODULES. THE PIPE SHALL BE SECURED TO THE TOP OF THE MODULES USING AN ELJEN HOOP (MINIMUM 1 HOOP PER MODULE).
- THE INVERT LEVEL OF THE DISTRIBUTION PIPE SHALL BE SET ON THE MODULES AT ELEVATION 94.58m AT THE FOOT TO 94.60m AT THE HEAD. THE END OF THE PIPE RUNS SHALL BE CONNECTED TO A 100mmØ SOLID PVC FOOTER PIPE
- INSTALL ELJEN SYSTEM SAMPLING DEVICE AS PER MANUFACTURER'S RECOMMENDATIONS.
- THE ELJEN ANTI-SILTATION FILTER FABRIC SHALL BE SPREAD LENGTHWISE OVER THE PERFORATED SEPTIC PIPE AND DOWN THE SIDES OF THE MODULES. ENSURE ENDS OF MODULES ARE ALSO COVERED WITH FABRIC.
- THE MODULES SHALL BE BACKFILLED, WITH ELJEN SPECIFIED SAND FILL TO AT LEAST THE TOP OF THE ELJEN MODULES, FOLLOWED BY 200mm (min.) OF LEACHING BED FILL, FOLLOWED BY 100mm OF SANDY TOPSOIL, WITHIN THE LIMITS OF THE SAND AREA. THE BED AREA SHOULD BE VEGETATED AS SOON AS POSSIBLE.
- LEACHING BED SAND FILL SHALL BE UNIFORM SAND WITH GRADING LIMITS SIMILAR TO 100% PASSING 13.2mm SIEVE, LESS THAN 5% PASSING 0.075mm SIEVE, AND HAVING A PERCOLATION TIME OF 6 TO 8 min/cm. LEACHING BED FILL SHALL BE PRE-APPROVED BY THE CONSULTANT.
- THE SIDES OF THE BED SHOULD BE SLOPED AT 3H:1V OR SHALLOWER.
- VENT SYSTEM SHALL BE INSTALLED ON THE FOOTER PIPE. CONNECT A 100mmØ PVC VENT PIPE TO FOOTER PIPE, EXTENDING TO GROUND SURFACE. VENT PIPE TO BE INSTALLED IN 150mmØ LANDSCAPE VALVE COVER.

8) MINIMUM CLEARANCE DISTANCE FROM DISTRIBUTION PIPE

- 5.6m FROM ANY PROPERTY LINE
- 7.6m FROM ANY STRUCTURE: 5.0m FROM ANY BASEMENTLESS STRUCTURE
- 17.6m FROM ANY DRILLED WELL
- 5.0m FROM ANY TREE (UNLESS OTHERWISE APPROVED)

9) MINIMUM CLEARANCE DISTANCE FROM TANK(S)

- 1.5m FROM ANY STRUCTURE
- 15.0m FROM ANY DRILLED OR DUG WELL
- 3.0m FROM ANY PROPERTY LINE

10) GENERAL

- SNOW STORAGE SHALL NOT BE LOCATED OVER OR UPGRADIENT OF THE PROPOSED SEWAGE SYSTEM.**
- THE SEWAGE SYSTEM HAS NOT BEEN DESIGNED TO SUPPORT TRAFFIC LOADING.
- THE BACKFILLING OF THE SEWAGE SYSTEM SHOULD MINIMIZE THE RISK OF OVER COMPACTION WITH THE USE RUBBER TRACKED EQUIPMENT AND BY AVOIDING THE CREATION OF ANY CONSTRUCTION ROUTES OR PATHWAYS OVER THE SYSTEM.
- ANY NEW IRRIGATION / SPRINKLER SYSTEM SHOULD NOT BE USED IN PROXIMITY OF THE PROPOSED SEWAGE SYSTEM.
- ENSURE WALKWAYS AND/OR SHURBBERY ARE NOT PLACED WITHIN PROXIMITY OF THE TANKAGE.
- THE BACKWASH WATERS FROM ANY WATER TREATMENT UNIT, SUCH AS WATER SOFTENER, SHOULD NOT DISCHARGE INTO THE SEWAGE SYSTEM.
- THE SEWAGE SYSTEM HAS NOT BEEN DESIGNED FOR THE USE OF A GARBAGE DISPOSAL.
- SEWAGE SYSTEM INSTALLER SHALL BE QUALIFIED AND REGISTERED UNDER PART 8 OF THE ONTARIO BUILDING CODE AND SHALL BE AN AUTHORIZED EJEN TREATMENT SYSTEM INSTALLER.
- ALL WORK SHALL BE CARRIED OUT IN ACCORDANCE WITH THE LATEST BY-LAWS, CODES AND REGULATIONS.
- CONTRACTOR SHALL REVIEW DRAWINGS IN DETAIL AND SHALL INFORM THE CONSULTANT OF ANY ERRORS AND/OR OMISSIONS ON DESIGN DRAWINGS IMMEDIATELY.
- CONTRACTOR SHALL BE RESPONSIBLE TO LOCATE AND PROTECT ALL EXISTING UNDERGROUND SERVICES.
- CONTRACTOR SHALL VISIT THE SITE AND REVIEW ALL DOCUMENTATION TO BECOME FAMILIAR WITH THE SITE AND SUBSURFACE SOIL CONDITIONS TO DETERMINE SUITABLE METHODS OF CONSTRUCTION.
- THE MANUFACTURER PROVIDES A LIMITED WARRANTY OF THE SYSTEM COMPONENTS. THE OWNER OF THE SYSTEM MUST SIGN A MAINTENANCE AGREEMENT WITH THE MANUFACTURER'S REPRESENTATIVE. THE HOMEOWNER IS RESPONSIBLE FOR THE ANNUAL FEES ASSOCIATED WITH THE MAINTENANCE.
- THE FIRM OF PATERSON GROUP INC. HAS PROVIDED DESIGN SERVICES ONLY FOR THE SUBJECT SEWAGE SYSTEM. THE DESIGN HAS BEEN CARRIED OUT IN ACCORDANCE WITH THE MANUFACTURER'S GUIDELINES AND OUR INTERPRETATION OF PART 8 OF THE ONTARIO BUILDING CODE.
- INSPECTIONS BY THE CONSULTANT DURING THE INSTALLATION OF THE SYSTEM IS A REQUIREMENT OF SOME REGULATING AUTHORITIES AND IS STRONGLY RECOMMENDED BY THIS FIRM.
- THE PROPERTY LINE / SEPARATION DISTANCES SHOULD BE CONFIRMED PRIOR TO CONSTRUCTION.
- CONSTRUCTION INSPECTIONS DURING THE INSTALLATION OF THE SEWAGE SYSTEM MAY BE REQUIRED BY THE REGULATING AUTHORITY AND ARE STRONGLY RECOMMENDED BY THIS FIRM. IF THIS FIRM IS TO COMPLETE ANY CONSTRUCTION INSPECTION(S), ADDITIONAL FEES MAY BE APPLIED. CONFIRMATION OF PAYMENT WILL BE REQUIRED PRIOR TO THE INSPECTION.**
- THE TEST HOLE INFORMATION PROVIDED, IS INTENDED TO BE USED FOR DESIGN PURPOSES ONLY, AND SHOULD NOT BE RELIED UPON FOR CONSTRUCTION PURPOSES. IF DISCREPANCIES ARE FOUND DURING THE CONSTRUCTION PROCESS, IT IS THE CLIENT'S RESPONSIBILITY TO CONTACT THIS FIRM TO MAKE ANY NECESSARY COMMENTS OR REVISIONS. ADDITIONAL REVISIONS ARE NOT CONSIDERED PART OF THE DESIGN WORKS AND WILL BE CONSIDERED AS AN ADDITIONAL COST.



Professional Engineers
Ontario

Licensed Engineering Technologist

Name: H. G. VAN DE GLIND

Number: 100647862

Limitations: Inspecting, designing, and assessing residential and commercial sewage systems, grading designs and soil analysis, and overseeing installation and compliance.

Association of Professional Engineers of Ontario

04/06/25	Issued for Septic Permit	3
14/05/25	Issued with Revised Site Plan	2
03/10/24	Issued with Revised Site Plan	1
20/09/24	Issued for Preliminary Review	0
DD/MM/YY	DESCRIPTION	REV.

Consultant:



PATERSON
GROUP

9 AURIGA DRIVE
OTTAWA, ON
K2E 7S9
TEL: (613) 226-7981

Client:

STRATFORD FOXRUN

Project:

**PROPOSED WAREHOUSE /
RESTAURANT**

**5923 OTTAWA STREET
OTTAWA (RICHMOND), ONTARIO**

Drawing:

**SEWAGE SYSTEM
DETAILS AND NOTES
SEWAGE SYSTEM 'B'**

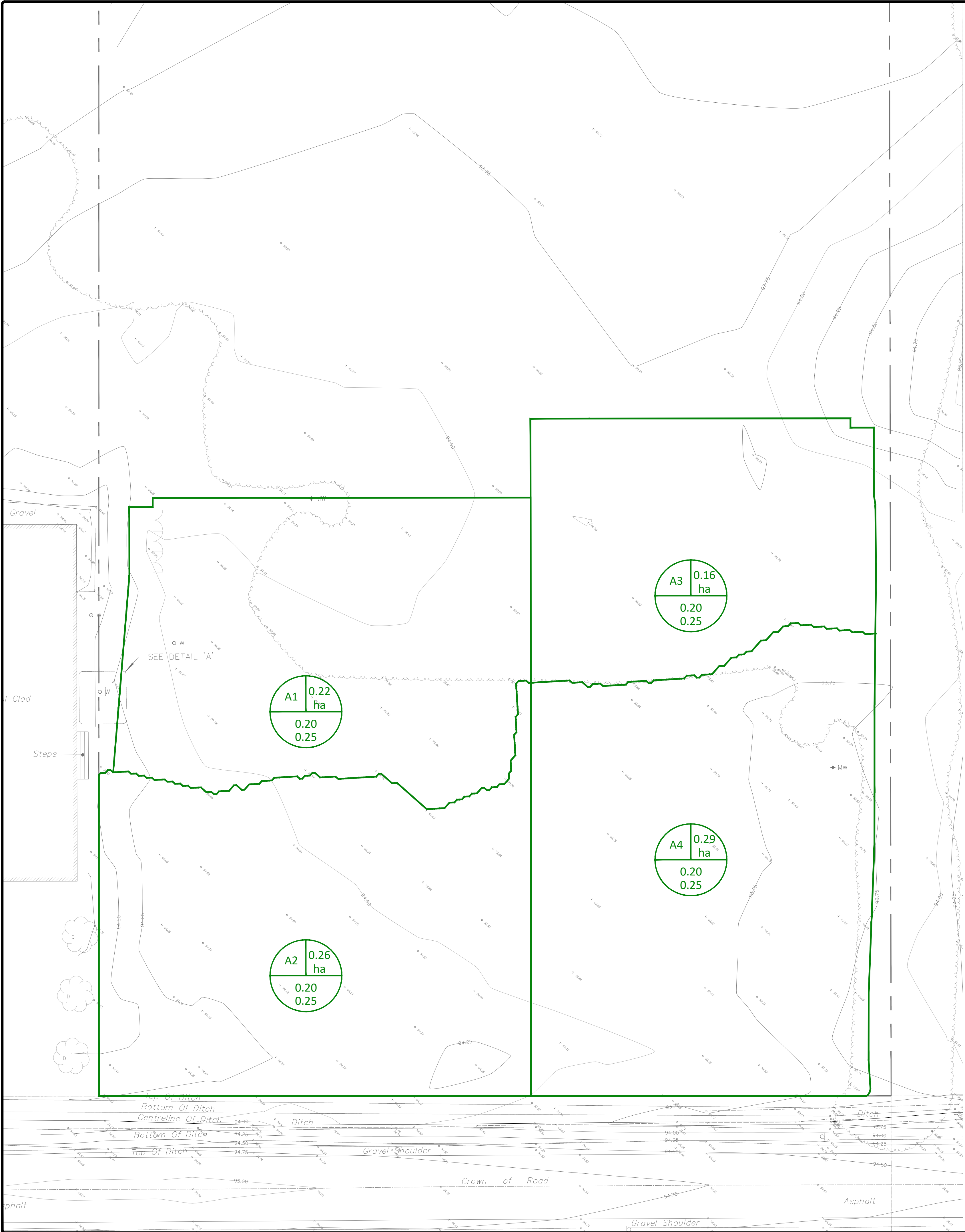
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Date:	06/2025	Checked by:	MK

Drawing No.:
PH4924-3(rev.3)

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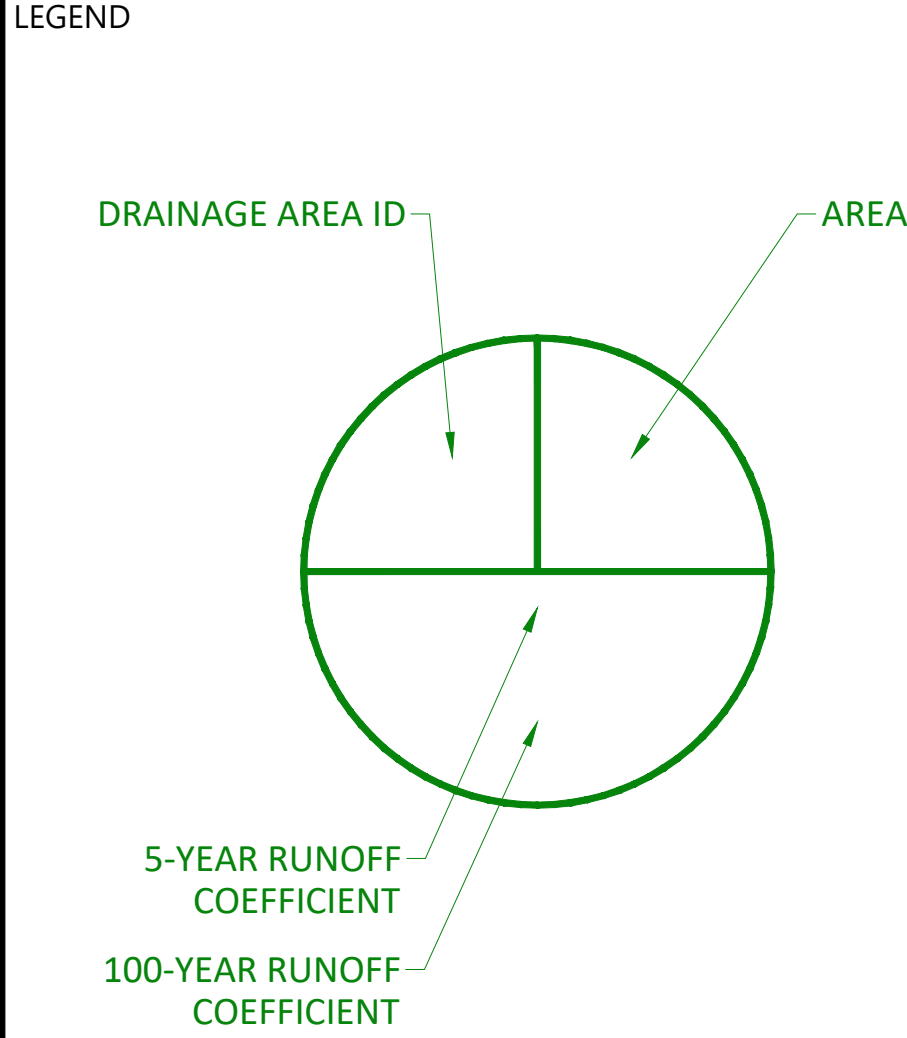
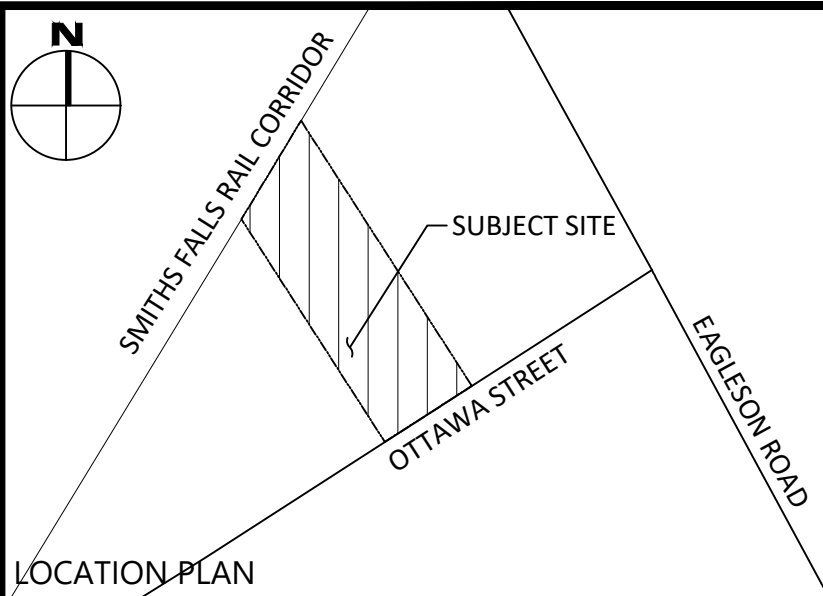
APPENDIX E PRE-DEVELOPMENT DRAINAGE PLAN

\\BAMAR-U\Infrastructure\2025\CCO-25-0415\99117756-Canada Inc. SPS Distillery & Warehouse, 9923 Ottawa Street\12 - Drawings\CCO-25-0415 - Presentation.dwg
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Plot: 12 - PRELIMINARY LAYOUT, MAP C:\STAND\040.dwg



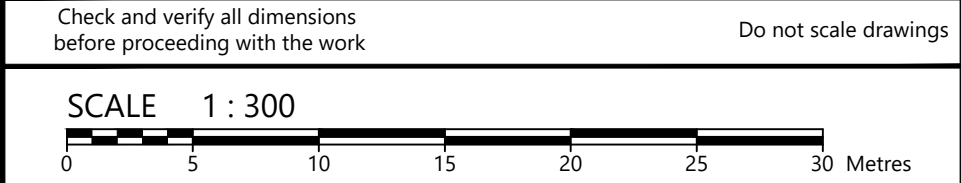
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7. EXCAVATE AND DISPOSE OF ALL EXCESS EXCAVATED MATERIAL, SUCH AS ASPHALT, CURBING AND DEBRIS, OFF SITE AS DIRECTED BY THE ENGINEER AND THE CITY.
8. TOPSOIL TO BE STRIPPED AND STOCKPILED FOR REHABILITATION. CLEAN FILL TO BE PLACED IN FILL AREAS AND COMPACTED TO 95% STANDARD PROCTOR DENSITY.
9. CONTRACTOR TO MINIMIZE THE ACTUAL LIMITS OF REMOVALS AND REINSTATEMENT WHEREVER POSSIBLE, AND SHALL MAKE THEIR OWN JUDGEMENT AND ACCOUNT FOR ALL MATERIAL AND LABOUR REQUIRED FOR ADEQUATELY REINSTATING THE AREA TO PRE-CONSTRUCTION CONDITIONS OR BETTER, AND BEAR THE COST OF THE SAME. NO ADDITIONAL PAYMENT WILL BE MADE FOR REINSTATEMENT WORK NOT SHOWN ON THE CONTRACT DRAWING AS A DIRECT RESULT FROM CONSTRUCTION.
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12. DO NOT ALTER GRADING OF THE SITE WITHOUT PRIOR APPROVAL OF THE ENGINEER/CITY.
13. ALL ROADWAY, PARKING LOT, AND GRADING WORKS TO BE UNDERTAKEN IN ACCORDANCE WITH CITY STANDARDS AND SPECIFICATIONS. THE CONTRACTOR IS TO PROVIDE POSITIVE DRAINAGE AWAY FROM THE BUILDING.
14. CONTACT THE CITY FOR INSPECTION OF ROUGH GRADING OF PARKING LOTS, ROADWAYS AND LANDSCAPED AREAS PRIOR TO PLACEMENT OF ASPHALT AND TOPSOIL. ALL DEFICIENCIES NOTED SHALL BE RECTIFIED TO THE CITY'S SATISFACTION PRIOR TO PLACEMENT OF ANY ASPHALT, TOPSOIL, SEED & MULCH AND/OR SOD.
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19. THIS PLAN MUST BE READ IN CONJUNCTION WITH THE GEOTECHNICAL INVESTIGATION COMPLETED BY PATERSON GROUP, DATED JULY 25, 2024.



FOR REVIEW ONLY
NOT FOR CONSTRUCTION

1	ISSUED FOR SITE PLAN CONTROL	JUN. 06, 2025
No.	Revisions	Date



115 Walgreen Road, R.R.3
Carp, ON K0A 1L0
Tel: 613-836-2184
Fax: 613-836-3742
www.egis-group.com

Stamp:

Client:
99117756 CANADA INC.
411 LEGGET DRIVE, SUITE 710
OTTAWA, ON K2K 3C9

Project:
DISTILLERY & WAREHOUSE
5923 OTTAWA STREET

Drawing Title:
PRE-DEVELOPMENT DRAINAGE AREA PLAN

Scale:	1:300	Project Number:	CCO-25-0415
Drawn By:	FV	Drawing Number:	
Checked By:	AG		
Designed By:	AG		

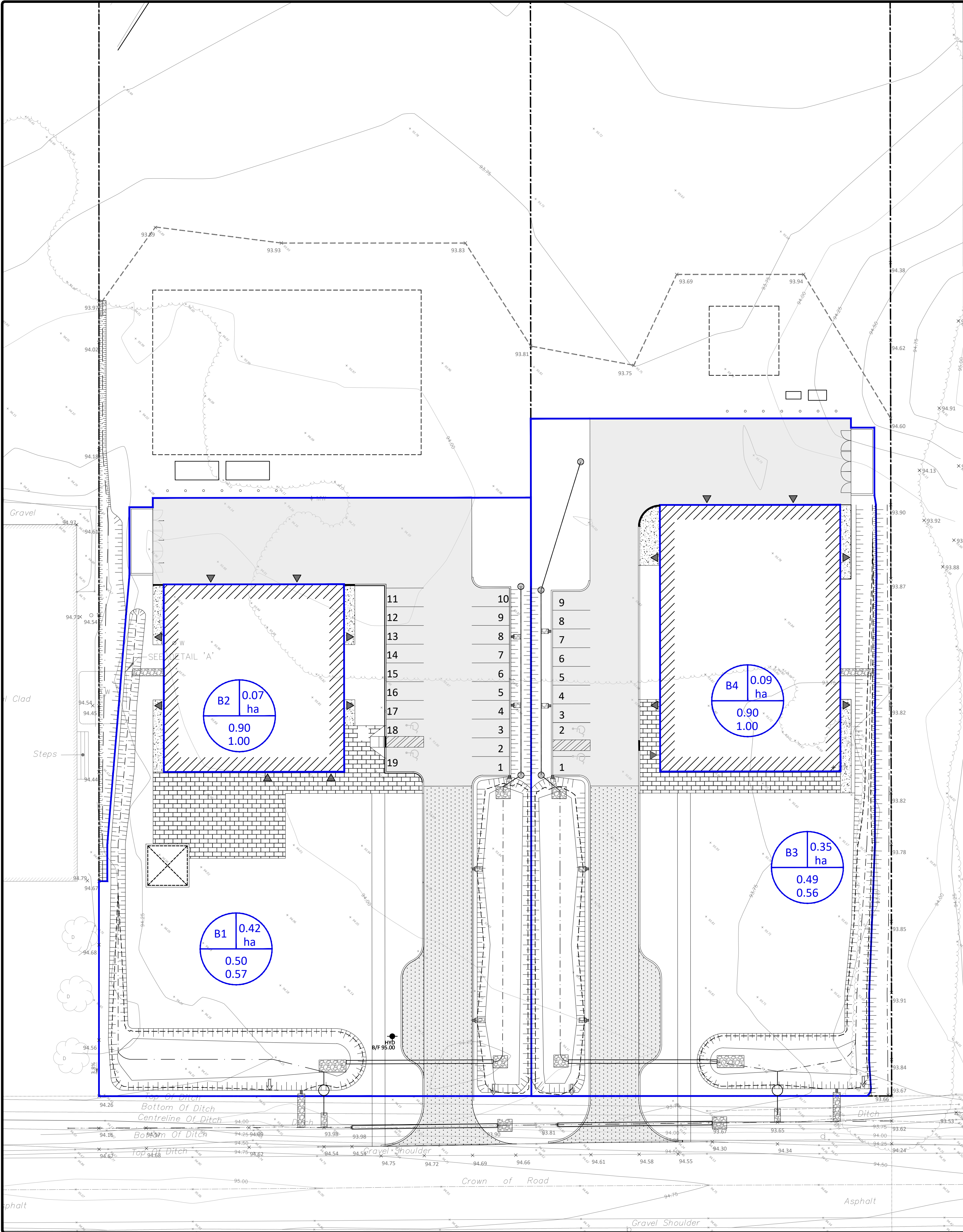
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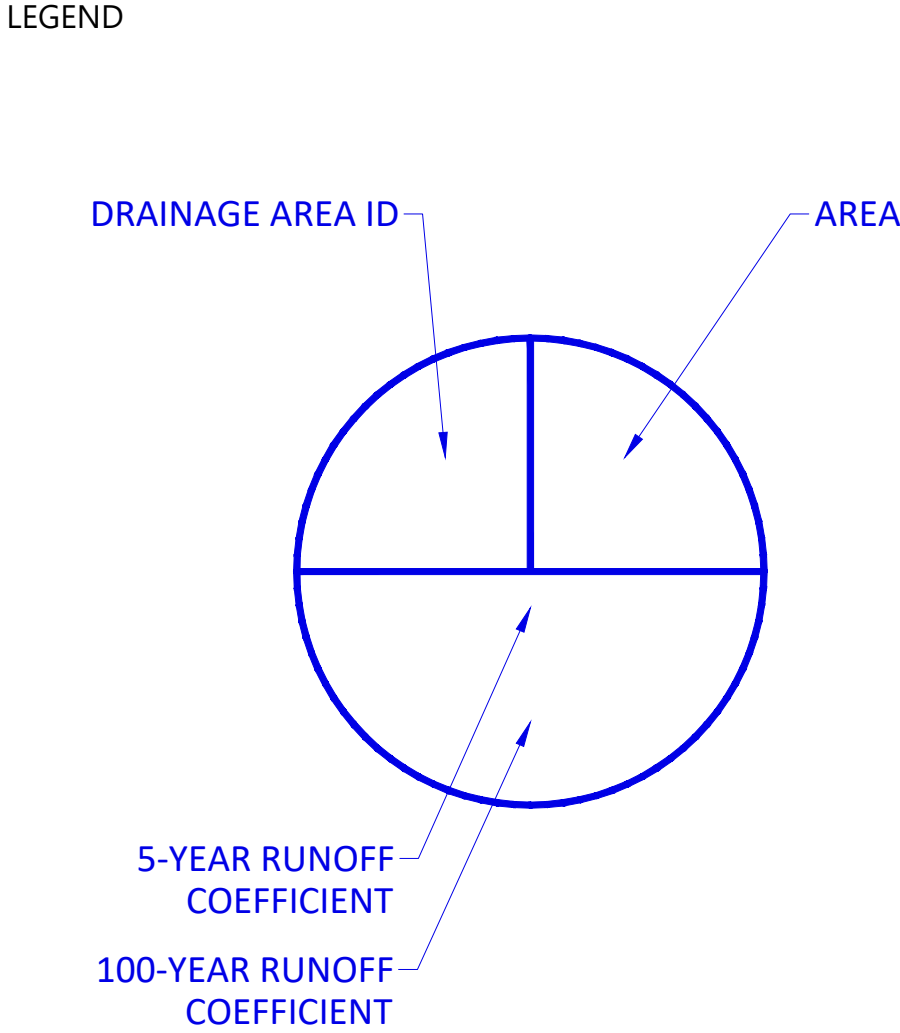
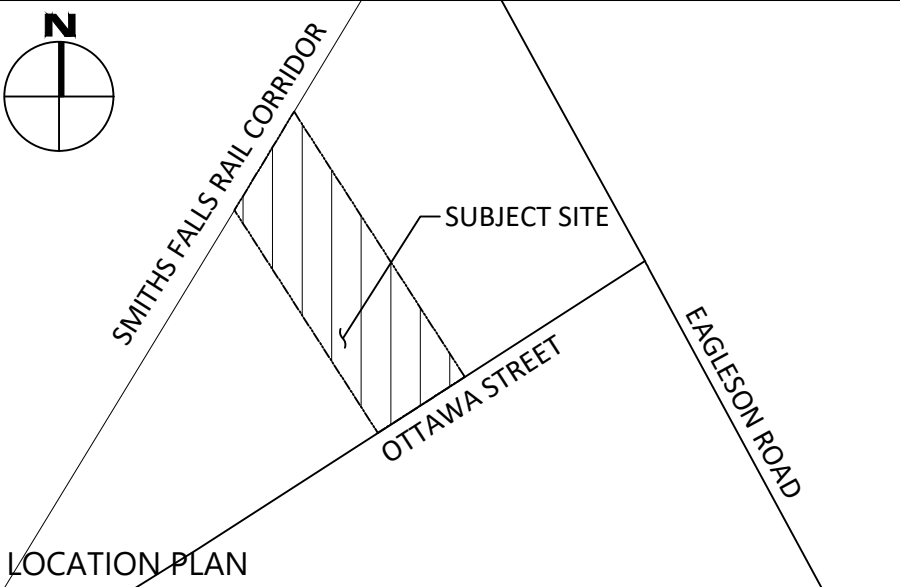
APPENDIX F POST-DEVELOPMENT DRAINAGE PLAN

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GENERAL NOTES

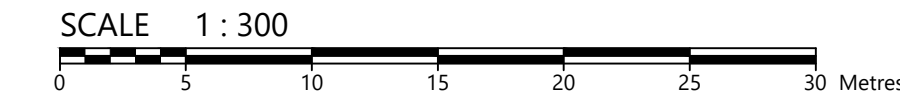
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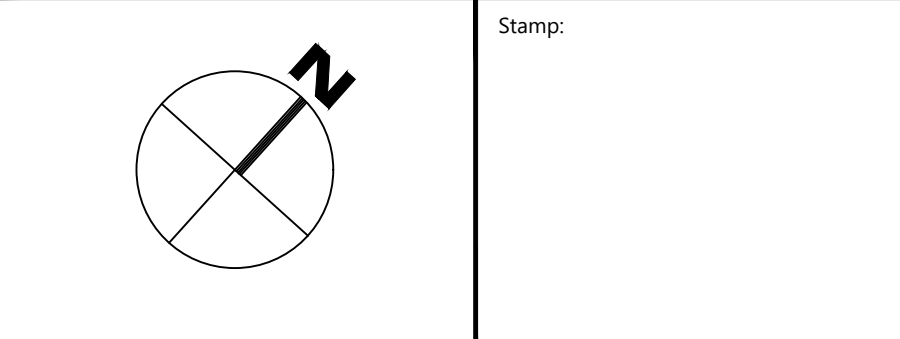
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1	ISSUED FOR SITE PLAN CONTROL	JUN. 06, 2025
No.	Revisions	Date

Check and verify all dimensions before proceeding with the work. Do not scale drawings.



egis 115 Walgreen Road, R.R.3
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Client: 99117756 CANADA INC.
411 LEGGET DRIVE, SUITE 710
OTTAWA, ON K2K 3C9

Project: DISTILLERY & WAREHOUSE
5923 OTTAWA STREET

Drawing Title: POST-DEVELOPMENT DRAINAGE AREA PLAN

Scale: 1:300	Project Number: CCO-25-0415
Drawn By: FV	Drawing Number: POST
Checked By: AG	
Designed By: AG	

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APPENDIX G STORMWATER MANAGEMENT CALCULATIONS

Tc (min)	Intensity (mm/ hr)		
	2-Year	5-Year	100-Year
20	52.0	70.3	120.0
10	76.8	104.2	178.6

C-Values	
Impervious	0.90
Gravel	0.60
Pervious	0.20

Pre-Development Runoff Coefficient

Drainage Area	Impervious Area (m ²)	Gravel (m ²)	Pervious Area (m ²)	Average C (2-Year)	Average C (100-Year)	
A1	0	0	2,219	0.20	0.25	Ph.1 Drainage to Rear Yard
A2	0	0	2,627	0.20	0.25	Ph.1 Drainage to Ottawa Street

Pre-Development Runoff Calculations

Drainage Area	Area (ha)	C 2/ 5-Year	C 100-Year	
A1	0.22	0.20	0.25	Ph.1 Drainage to Rear Yard
A2	0.26	0.20	0.25	Ph.1 Drainage to Ottawa Street
Total	0.48			

Post-Development Runoff Coefficient

Drainage Area	Impervious Area (m ²)	Gravel (m ²)	Pervious Area (m ²)	Average C (2-year)	Average C (100-year)	
B1	1,801	0	2,372	0.50	0.57	Ph.1 Surface Restricted
B2	651	0	0	0.90	1.00	Ph.2 Building - Restricted

Post-Development Runoff Calculations

Drainage Area	Area (ha)	C 2-Year	C 100-Year	
B1	0.42	0.50	0.57	Ph.1 Surface Restricted
B2	0.07	0.90	1.00	Ph.2 Building - Restricted
Total	0.48			

Tc (min)	Intensity (mm/ hr)		
	2-Year	5-Year	100-Year
20	52.0	70.3	120.0
10	76.8	104.2	178.6

C-Values	
Impervious	0.90
Gravel	0.60
Pervious	0.20

Pre-Development Runoff Coefficient

Drainage Area	Impervious Area (m ²)	Gravel (m ²)	Pervious Area (m ²)	Average C (2-Year)	Average C (100-Year)	
A3	0	0	1,604	0.20	0.25	Ph.2 Drainage to Rear Yard
A4	0	0	2,863	0.20	0.25	Ph.2 Drainage to Ottawa Street

Pre-Development Runoff Calculations

Drainage Area	Area (ha)	C 2/ 5-Year	C 100-Year	
A3	0.16	0.20	0.25	Ph.2 Drainage to Rear Yard
A4	0.29	0.20	0.25	Ph.2 Drainage to Ottawa Street
Total	0.45			

Post-Development Runoff Coefficient

Drainage Area	Impervious Area (m ²)	Gravel (m ²)	Pervious Area (m ²)	Average C (2-year)	Average C (100-year)	
B3	1,469	0	2,072	0.49	0.56	Ph.2 Surface Restricted
B4	926	0	0	0.90	1.00	Ph.2 Building - Restricted

Post-Development Runoff Calculations

Drainage Area	Area (ha)	C 2-Year	C 100-Year	
B3	0.35	0.49	0.56	Ph.2 Surface Restricted
B4	0.09	0.90	1.00	Ph.2 Building - Restricted
Total	0.45			



Adjustable Accutrol Weir

Tag: _____

Adjustable Flow Control for Roof Drains

ADJUSTABLE ACCUTROL (for Large Sump Roof Drains only)

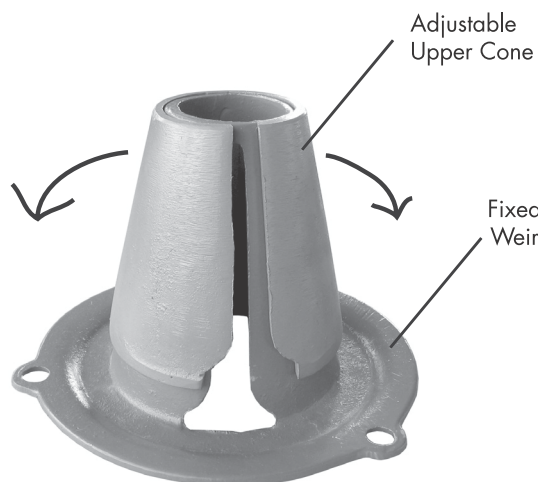
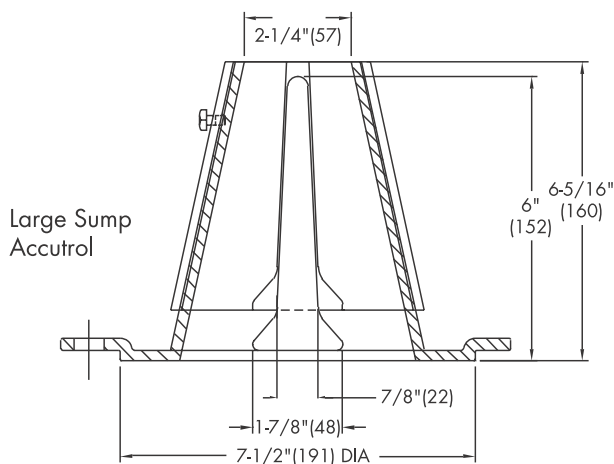
For more flexibility in controlling flow with heads deeper than 2", Watts Drainage offers the Adjustable Accutrol. The Adjustable Accutrol Weir is designed with a single parabolic opening that can be covered to restrict flow above 2" of head to less than 5 gpm per inch, up to 6" of head. To adjust the flow rate for depths over 2" of head, set the slot in the adjustable upper cone according to the flow rate required. Refer to Table 1 below.

Note: Flow rates are directly proportional to the amount of weir opening that is exposed.

EXAMPLE:

For example, if the adjustable upper cone is set to cover 1/2 of the weir opening, flow rates above 2" of head will be restricted to 2-1/2 gpm per inch of head.

Therefore, at 3" of head, the flow rate through the Accutrol Weir that has 1/2 the slot exposed will be:
[5 gpm (per inch of head) x 2 inches of head] + 2-1/2 gpm (for the third inch of head) = 12-1/2 gpm.



1/2 Weir Opening Exposed Shown Above

TABLE 1. Adjustable Accutrol Flow Rate Settings

Weir Opening Exposed	1"	2"	3"	4"	5"	6"
	Flow Rate (gallons per minute)					
Fully Exposed	5	10	15	20	25	30
3/4	5	10	13.75	17.5	21.25	25
1/2	5	10	12.5	15	17.5	20
1/4	5	10	11.25	12.5	13.75	15
Closed	5	5	5	5	5	5

Job Name _____

Contractor _____

Job Location _____

Contractor's P.O. No. _____

Engineer _____

Representative _____

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June 05, 2025

Project Number: P2710(e01)

Stratford Foxrun
6286 Prince of Wales Drive
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Attention: Joshua Laginski, P.Eng

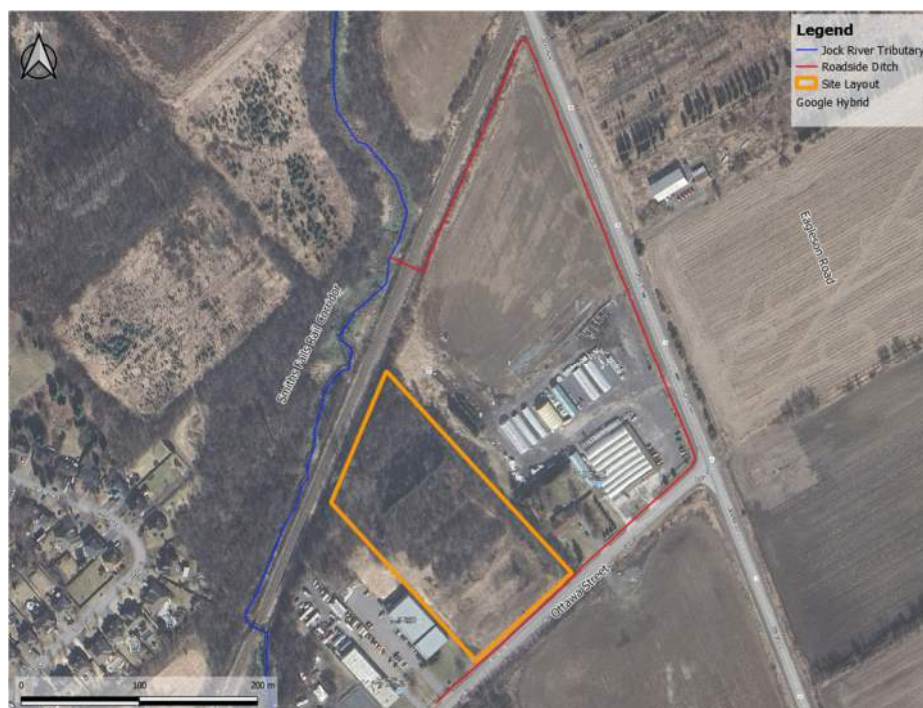
**Subject: Stratford Foxrun Development- 5923 Ottawa Street, Richmond
Ditch Hydrologic and Hydraulic Analysis**

OVERVIEW

Egis Group has commissioned JFSA Canada Inc. to develop detailed hydrologic and hydraulic models for the proposed Stratford Foxrun development. This development, located at 5923 Ottawa Street in Richmond, Ontario, will include local depressions within the site that will act as stormwater management controls to mitigate increases in peak flows resulting from the development. The site will outlet into an existing roadside ditch on Ottawa street before proceeding east to Eagleson Road and then turns north towards the rail corridor before finally discharging into Marlborough Creek, which is a tributary of the Jock River.

This memo presents a downstream hydrologic and hydraulic analysis of the aforementioned roadside ditch, specifically quantifying its capacity from 5923 Ottawa Street to the Marlborough Creek. **Figure 1** illustrates the development's location and extent, as well as the road site ditch relative to its outlet at Marlborough Creek.

Figure 1: Site Boundary and Existing Watercourse



HYDROLOGY

Existing Conditions

1.1.1 Drainage Areas

Existing drainage areas for the study were delineated using a comprehensive Digital Terrain Model (DTM). This DTM was developed from two primary sources: LiDAR data, obtained from the LIO (Land Information Ontario) Digital Terrain Model and flown in 2019-2020, and a detailed topographic survey of the existing ditch and associated crossings completed by Egis. This combined data was then imported into GIS software. Watershed delineation algorithms were subsequently applied to the DTM to automatically define the drainage areas. These automated delineations were manually reviewed against relevant previous studies and existing drainage delineations for accuracy and consistency. **Figure A1 in Attachment A** provides a visual overview of the existing drainage areas within the study area.

Land Use

Land use data has been taken from Land Information Ontario's (LIO) Land Use Data and then discretized based on the respective subcatchments. **Figure A2 in Attachment A** provides a visual overview of the respective land use data for each of the subcatchments within the study area.

Soil/Infiltration Data

Soil data within the study area has been taken from the Soil Survey Complex Data available on Land Information Ontario (LIO). **Figure A3 in Attachment A** provides a visual overview of the respective soil type data for each of the subcatchments within the study area. A full breakdown of the soil data for each drainage area has also been provided in **Table A1 in Attachment A**.

Curve Number (CN)

Based on the underlying Land Use Type and Soil Classification at each location within a subcatchment, a Curve Number (CN) was calculated, based on applicable values outlined in Tables A2 and A3 in the SWMHYMO Manual. Each Curve Number was then weighted based on the total area within a given subcatchment to determine the weighted CN for that subcatchment. The CN values calculated were then converted to CN*. Note that the traditional CN procedure assumes that Initial Abstraction (IA) = 0.2S. However, the traditional CN method is subject to errors because of this assumption, particularly for smaller rainfall events. Instead, it is recommended that a modified CN* and a user-defined IA value be used for SWMHYMO modelling. Modified CN* values have been shown to correlate well with measured flows and perform well in continuous SWMHYMO modelling (as discussed in the July 1989 INTERHYMO / OTTHYMO 89 Manual). The CN values derived were converted to CN* based on the formula provided in the November 2002 Runoff Curve Number Method: Examination of the Initial Abstract Ratio paper, and applied to the hydrologic model.

$$CN^* = \frac{100}{1.879 \left[\frac{100}{CN-1} \right]^{1.15} + 1}$$

Table A1 in Attachment provides a full summary of the CN/CN* calculations for each of the predevelopment subcatchments.

Time to Peak (t_p)

For natural areas within the study area, the time to peak values for each of the subcatchments has been calculated based on existing topography. Flow paths have been discretized based on the topographic data using GIS tools, and the longest major flow path within each subcatchment has been identified; refer to Figure B6 in Attachment B for the flow paths discretized for each subcatchment. The upstream and downstream topographic elevations and flow lengths were identified for each subcatchment and used in the calculations. For these natural subcatchments, the Federal Aviation Administration (FAA) method was determined to be the most appropriate method to calculate the Time to Peak. Full details of these calculations have been provided in **Table A2 in Attachment A**, along with other time-to-peak values using alternative t_p calculation methods.

Existing SWMHYMO modelling

An existing conditions SWMHYMO model of the drainage areas was developed based on the pre-development drainage areas provided. To represent the existing undeveloped lands, CALIB NASHYDs have been used, with Initial Abstraction (IA)=4.67 mm, and Number of Linear Reservoirs (N)=3. Full input and summary files of the existing conditions model have been provided in Attachment A

Channel Routing

To account for channel routing throughout the study area, LiDAR has been used to approximate the channel cross-section and associated flow parameters (length & slope). **Figure A4 in Attachment A** outlines the major flow paths within the study area, which have been used to account for channel routing and time to peak calculations within the subcatchments.

Proposed Conditions

Drainage Areas & Imperviousness

For the Stratford Foxrun development under proposed conditions, Egis provided JFSA with detailed design drawings that included drainage areas and associated imperviousness. The proposed development lot layout and the associated drainage areas have been provided in **Figure B1 of Attachment B**. To represent the proposed Stratford Foxrun development lands, DESIGN STANDHYDs have been used, with default parameters per the city of Ottawa Storm Sewer Design Guidelines.

Onsite SWM Controls

Egis's design for the proposed development included detailed grading of localized depressions within the site that will act as onsite stormwater management controls, along with corresponding stage-storage tables. These stage-storage tables were directly incorporated into the hydrologic model. This integration allowed for the determination of appropriate outlet configurations for these facilities, as well as an accurate assessment of the storage volumes provided by the proposed depressions. Full detailed Stage/Storage/Outflow curves have been provided in **Tables B1 and B2 in Attachment B**. Based on this analysis both sites will have a **85 mm** orifice at the bottom of the localized depression area and a small **30cm** overflow weir at an elevation of **94.40m** and **94.35m** for the west and east site respectively.

Results

Onsite Controls Summary

As mentioned, the modelling accurately reflects the site's detailed grading, particularly the localized depressions. **Table 2** provides a comprehensive overview of the maximum storage volumes achieved at each of these locations across various return periods, in addition to their associated peak outflows.

Table 1: Site Release Rates / Required Storage Volume / Ponding Depth

Storm	Site 1 (0.48 ha)			Site 2 (0.45 ha)		
	Peak Outflow (m ³ /s)	Required Storage (m ³)	Ponding Depth (m)	Peak Outflow (m ³ /s)	Required Storage (m ³)	Ponding Depth (m)
2YRCHI3Hr	0.008	41	0.31	0.009	40	0.40
5YRCHI3Hr	0.009	72	0.39	0.010	68	0.48
10YRCHI3Hr	0.010	93	0.44	0.011	87	0.53
25YRCHI3Hr	0.010	122	0.50	0.012	112	0.59
50YRCHI3Hr	0.011	143	0.54	0.014	127	0.62
100YRCHI3Hr	0.014	163	0.58	0.018	141	0.65
2YrSCS24Hr	0.008	46	0.33	0.009	44	0.41
5YrSCS24Hr	0.009	75	0.40	0.010	70	0.49
10YrSCS24Hr	0.010	95	0.44	0.011	87	0.53
25YrSCS24Hr	0.010	120	0.49	0.011	109	0.58
50YrSCS24Hr	0.011	139	0.53	0.013	124	0.62
100YrSCS24Hr	0.013	158	0.57	0.017	137	0.64

Peak Flows at Key Locations

The model was run for both existing and proposed conditions, and peak flows were extracted from the key nodes within the watercourse (refer to **Figure A4** for locations). **Table 2** outlines the peak flows for various return periods at each node, covering both the 3-hour Chicago and 24-hour SCS storms for 2- to 100-year events.

This analysis indicates minor increases in peak flows to the ditch for lower return periods under post-development conditions. However, for larger events (e.g., 100-year), peak flows are either less than or equal to existing conditions. Both sites will utilize an **85 mm** orifice at the outlet to maximize the storage capacity of these depression areas. While this orifice could be further reduced to ensure all post-development peak flows are less than pre-development levels, doing so carries the risk of increased likelihood of blockages due to its small size, increasing the potential for on-site flooding if not regularly inspected.

Table 2: Pre and Post Development Peak Flow Summary

	Node	J1		Node	J2		Node	J3		Node	J4	
Event	Pre	Post	Diff	Pre	Post	Diff	Pre	Post	Diff	Pre	Post	Diff
Area (ha)	0.85	1.23	0.38	4.62	5	0.38	4.93	5.31	0.38	5.52	5.9	0.38
2YRCHI3Hr	0.015	0.024	0.009	0.057	0.066	0.009	0.061	0.070	0.009	0.067	0.077	0.010
5YRCHI3Hr	0.026	0.032	0.006	0.102	0.107	0.005	0.109	0.114	0.005	0.121	0.127	0.006
10YRCHI3Hr	0.035	0.037	0.002	0.136	0.137	0.001	0.145	0.146	0.001	0.162	0.164	0.002
25YRCHI3Hr	0.047	0.043	-0.004	0.181	0.178	-0.003	0.194	0.190	-0.004	0.218	0.214	-0.004
50YRCHI3Hr	0.057	0.050	-0.007	0.219	0.212	-0.007	0.234	0.228	-0.006	0.263	0.257	-0.006
100YRCHI3Hr	0.067	0.060	-0.007	0.258	0.253	-0.005	0.277	0.271	-0.006	0.311	0.306	-0.005
2YrSCS24Hr	0.024	0.028	0.004	0.090	0.095	0.005	0.096	0.102	0.006	0.107	0.113	0.006
5YrSCS24Hr	0.038	0.037	-0.001	0.148	0.146	-0.002	0.158	0.157	-0.001	0.177	0.176	-0.001
10YrSCS24Hr	0.049	0.042	-0.007	0.189	0.182	-0.007	0.202	0.196	-0.006	0.227	0.221	-0.006
25YrSCS24Hr	0.062	0.049	-0.013	0.242	0.228	-0.014	0.259	0.247	-0.012	0.291	0.279	-0.012
50YrSCS24Hr	0.073	0.055	-0.018	0.284	0.267	-0.017	0.305	0.288	-0.017	0.343	0.326	-0.017
100YrSCS24Hr	0.084	0.063	-0.021	0.329	0.310	-0.019	0.354	0.335	-0.019	0.399	0.380	-0.019

Table 2: Pre and Post Development Peak Flow Summary

	Node	J5		Node	J6		Node	J7		Node	J8	
Event	Pre	Post	Diff	Pre	Post	Diff	Pre	Post	Diff	Pre	Post	Diff
Area (ha)	6.86	7.24	0.38	1.01	1.02	0.01	1.83	1.46	-0.37	13.1	13.1	0
2YRCHI3Hr	0.080	0.091	0.011	0.016	0.021	0.005	0.019	0.018	-0.001	0.141	0.151	0.010
5YRCHI3Hr	0.147	0.154	0.007	0.025	0.031	0.006	0.035	0.034	-0.001	0.264	0.270	0.006
10YRCHI3Hr	0.197	0.201	0.004	0.034	0.037	0.003	0.047	0.047	0.000	0.361	0.363	0.002
25YRCHI3Hr	0.267	0.266	-0.001	0.047	0.047	0.000	0.065	0.064	-0.001	0.493	0.489	-0.004
50YRCHI3Hr	0.323	0.320	-0.003	0.057	0.057	0.000	0.079	0.078	-0.001	0.602	0.594	-0.008
100YRCHI3Hr	0.384	0.381	-0.003	0.069	0.069	0.000	0.095	0.094	-0.001	0.721	0.712	-0.009
2YrSCS24Hr	0.128	0.135	0.007	0.023	0.023	0.000	0.032	0.031	-0.001	0.233	0.239	0.006
5YrSCS24Hr	0.215	0.216	0.001	0.039	0.039	0.000	0.054	0.053	-0.001	0.400	0.399	-0.001
10YrSCS24Hr	0.277	0.273	-0.004	0.051	0.051	0.000	0.070	0.069	-0.001	0.517	0.511	-0.006
25YrSCS24Hr	0.357	0.347	-0.010	0.066	0.066	0.000	0.092	0.090	-0.002	0.675	0.661	-0.014
50YrSCS24Hr	0.421	0.407	-0.014	0.079	0.079	0.000	0.110	0.107	-0.003	0.800	0.782	-0.018
100YrSCS24Hr	0.491	0.474	-0.017	0.093	0.093	0.000	0.129	0.126	-0.003	0.939	0.914	-0.025

HYDRAULICS

The detailed hydraulic analysis of the downstream study area was conducted using the US Army Corps of Engineers HEC-RAS software (version 6.6). The purpose of this hydraulic analysis is to assess the hydraulic impacts that the proposed Stratford Foxrun development may have on existing water levels for the applicable design storms.

Model Development & Parameters

The primary method for establishing cross-sections involved using detailed topographic measurements. These measurements were typically taken at approximately 50-meter intervals along the watercourse and supplemented with LiDAR in the floodplain. This close spacing is crucial for accurately capturing the unique hydraulic characteristics and flow conveyance capacity of the existing watercourse. In addition to the surveyed locations, supplementary cross-sections were added in areas that weren't explicitly surveyed. These were created by sampling the merged LiDAR and topographic Digital Terrain Model (DTM). This was done to ensure that critical cross-sections were included in the model to accurately capture the channel hydraulics. **Figure C1 in Attachment C** outlines the extent and location of model cross sections.

Existing hydraulic infrastructure, such as culverts, on the respective watercourses, was incorporated into the model based on the details obtained from the topographic surveys. Consistent with HEC-RAS technical guidelines, ineffective flow areas and expansion-contraction coefficients were appropriately applied at these locations. Typical Manning's values of 0.035 and 0.05 were applied to the roadside ditch channel bottom and over banks, respectively. A normal downstream boundary condition was applied for all events due to the significant difference in drainage area between Marlborough Creek and the roadside ditch. This approach was chosen because Marlborough Creek (a tributary of the Jock River) experiences flooding predominantly from spring snowmelt and rainfall, whereas the critical storm for a roadside ditch of this size typically occurs during summer events. Therefore, these two critical events can never coincide.

Results

The pre- and post-development models were run for the full range of design storms (2- to 100-Year Events) to accurately establish the existing and proposed floodplain extents within the study area. **Figures C2 and C3** illustrate the flood extents for both existing and proposed conditions during the 24-hour SCS type storms (the critical design storm). **Figure C4** provide a comparison between the 100-year floodplain under both existing and proposed conditions. From this figure, it is shown that the 100-year floodplain extents along the ditch are reduced under post-development conditions. This demonstrates that the proposed stormwater management solution is effective and that the proposed development will not worsen existing flood conditions along the ditch. **Attachment C** also includes pre- and post-development long- and cross-section plots, along with summary tables.

This analysis also revealed that flows in the roadside ditch overtop the banks during 5- to 10-year events (depending on the design storm). This is expected, as the typical level of service for driveway crossings is generally in this range. It's crucial to note that existing driveway crossings, not the channel itself, are constricting flows and causing them to overtop the bank. Upsizing several culverts along this stretch of roadside ditch would significantly reduce the floodplain in this area.

Along Eagleson Road, approximately halfway between the railway and the Ottawa Street intersection, flows will overtop the bank and spill west to the culvert under the railway. For a conservative design, the hydraulic modelling does not account for this spill, assuming all flows proceed to the next downstream cross-section. It's also important to emphasize that for all events (up to and including the 100-year event), water levels in the roadside ditch do not reach an elevation that would impede traffic on either Eagleson Road or Ottawa Street, as the flood extents do not touch the shoulder of the road. Furthermore, the maximum 100-year floodplain extents do not affect any nearby buildings, meaning the current and proposed flood extents pose no danger to existing structures.

CONCLUSION

In summary, JFSA Canada Inc.'s hydrologic and hydraulic modelling confirms that the proposed Stratford Foxrun development's stormwater management plan effectively mitigates downstream impacts. The on-site localized depressions, with 85 mm orifice outlets, will manage post-development runoff, ensuring peak flows for major storm events (up to 100-year) remain at or below pre-development levels.

The HEC-RAS analysis further demonstrates that the proposed SWM measures will lead to a reduction in the 100-year floodplain extent along the receiving roadside ditch. While existing culverts contribute to minor, more frequent overtopping, the development itself will not worsen these conditions or cause flooding that impedes traffic or endangers structures during major events. The findings indicate that the proposed SWM strategy for this site will not adversely impact downstream lands.

Yours truly,
JFSA Canada Inc.



Jonathon Burnett, B.Eng, P.Eng
Water Resource Engineer



cc: J.F. Sabourin, M.Eng, P.Eng
Director of Water Resources Projects

Figures

Figure 1: Site Boundary and Existing Watercourse

Tables

Table 1: Site Release Rates / Required Storage Volume / Ponding Depth

Table 2: Peak Flows at Key Locations

Attachments

Attachment A: Pre-Development Hydrology

Attachment B: Post Development Hydrology

Attachment C: Hydraulic Analysis

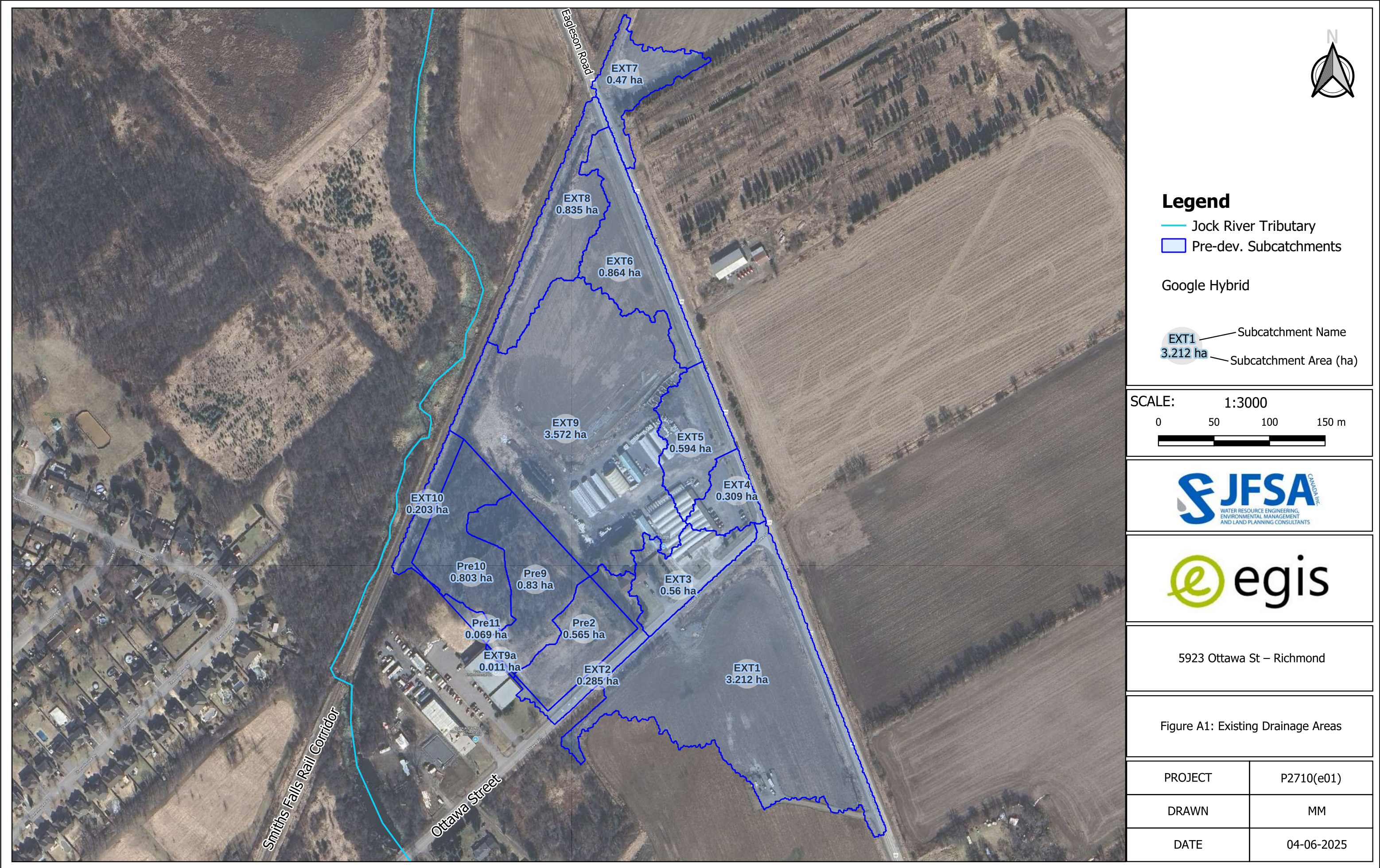


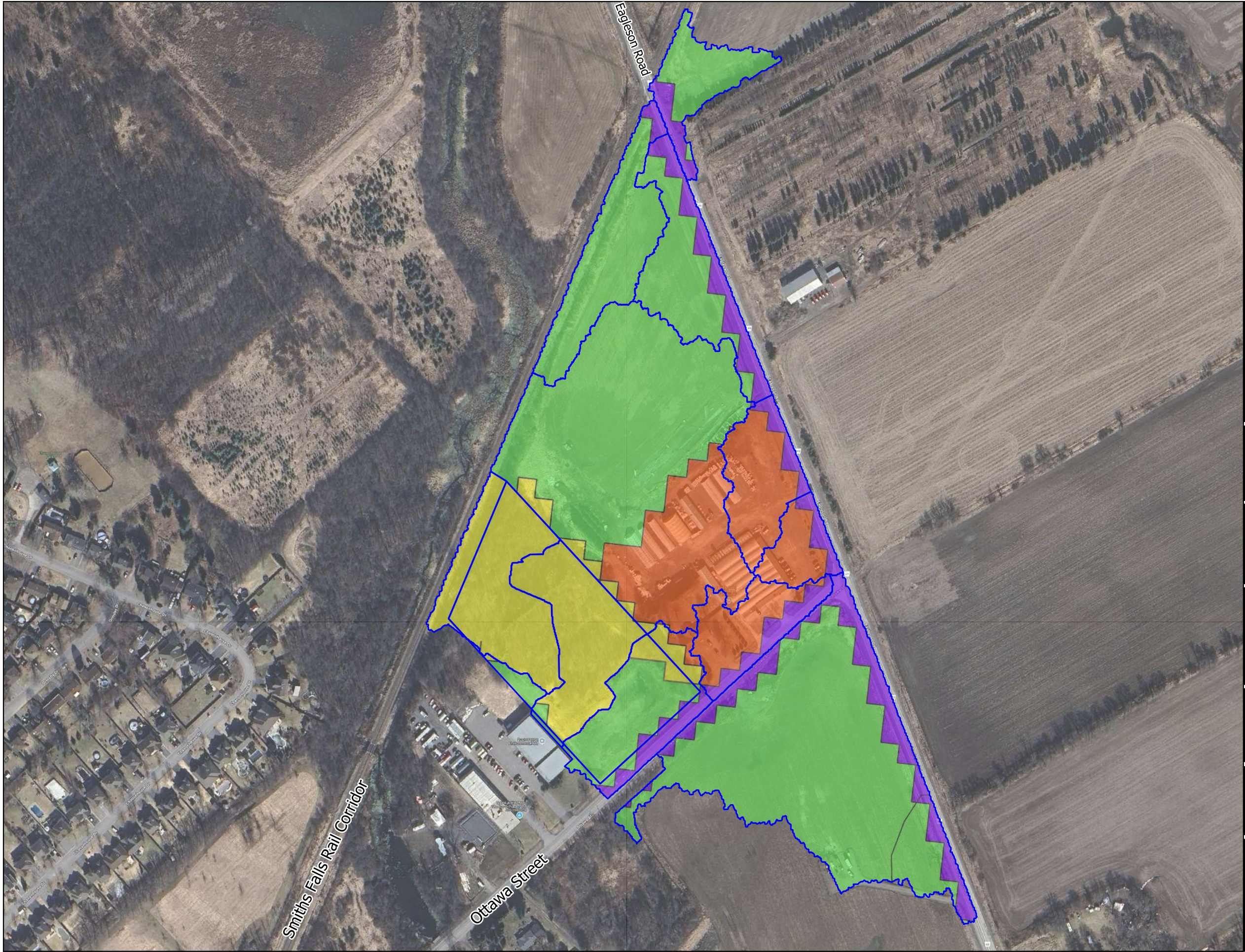
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Attachment A

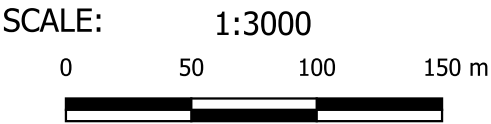
Pre-Development Hydrology





Legend

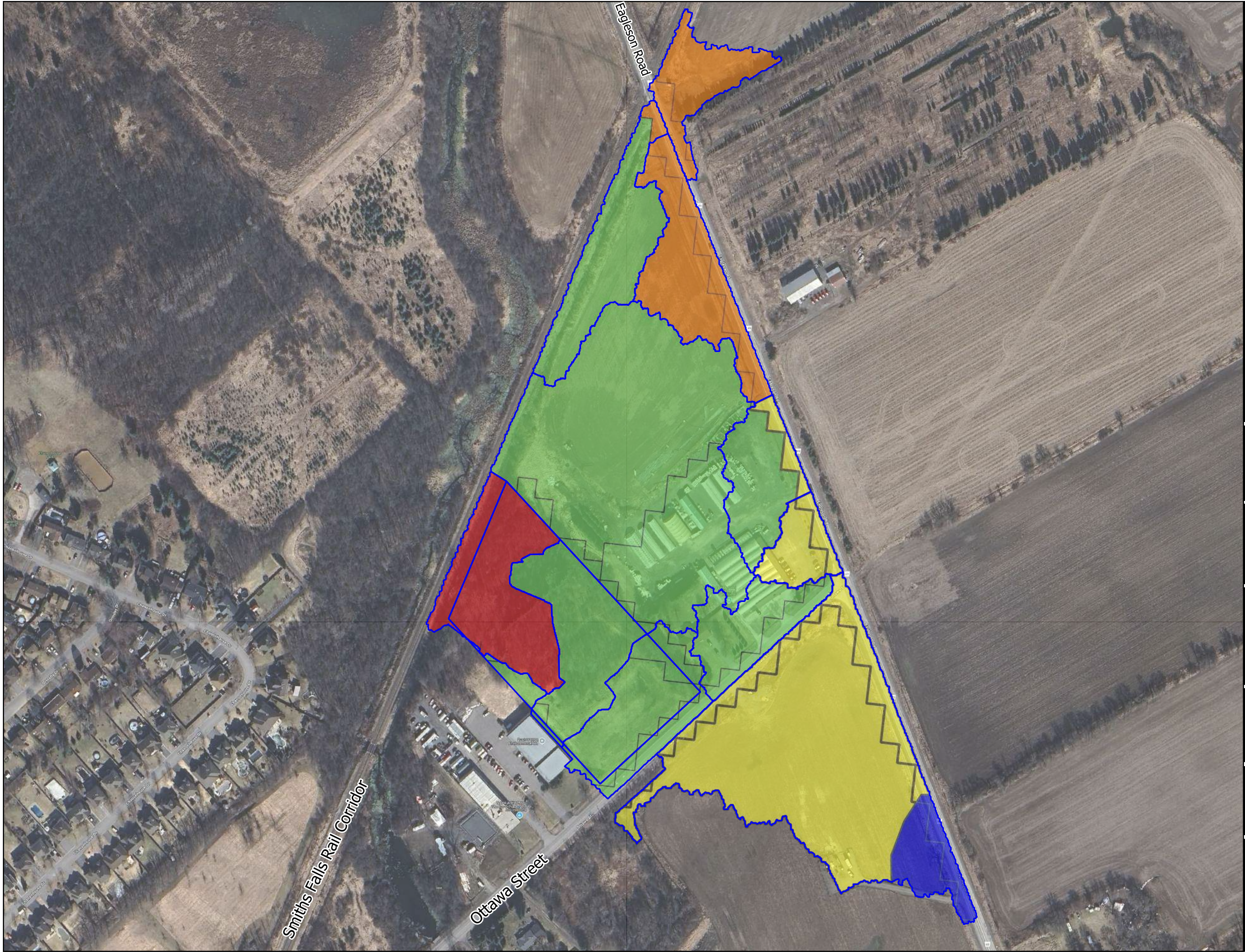
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-  CN
-  Built Up Area - Pervious
-  Transportation
-  Forest
-  Tilled
- Google Hybrid



5923 Ottawa St – Richmond

Figure A2: Land Use Data

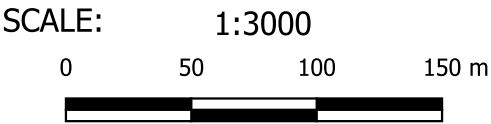
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DRAWN	MM
DATE	04-06-2025



Legend

-  Pre-dev. Subcatchments
- Soil Name (Soil Type)
-  ERODED CHANNEL (D)
-  NORTH GOWER (D)
-  DALHOUSIE (D)
-  BRANDON (D)
-  GRENVILLE (B)

Google Hybrid



5923 Ottawa St – Richmond

Figure A3: Soil Type

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DRAWN	MM
DATE	04-06-2025

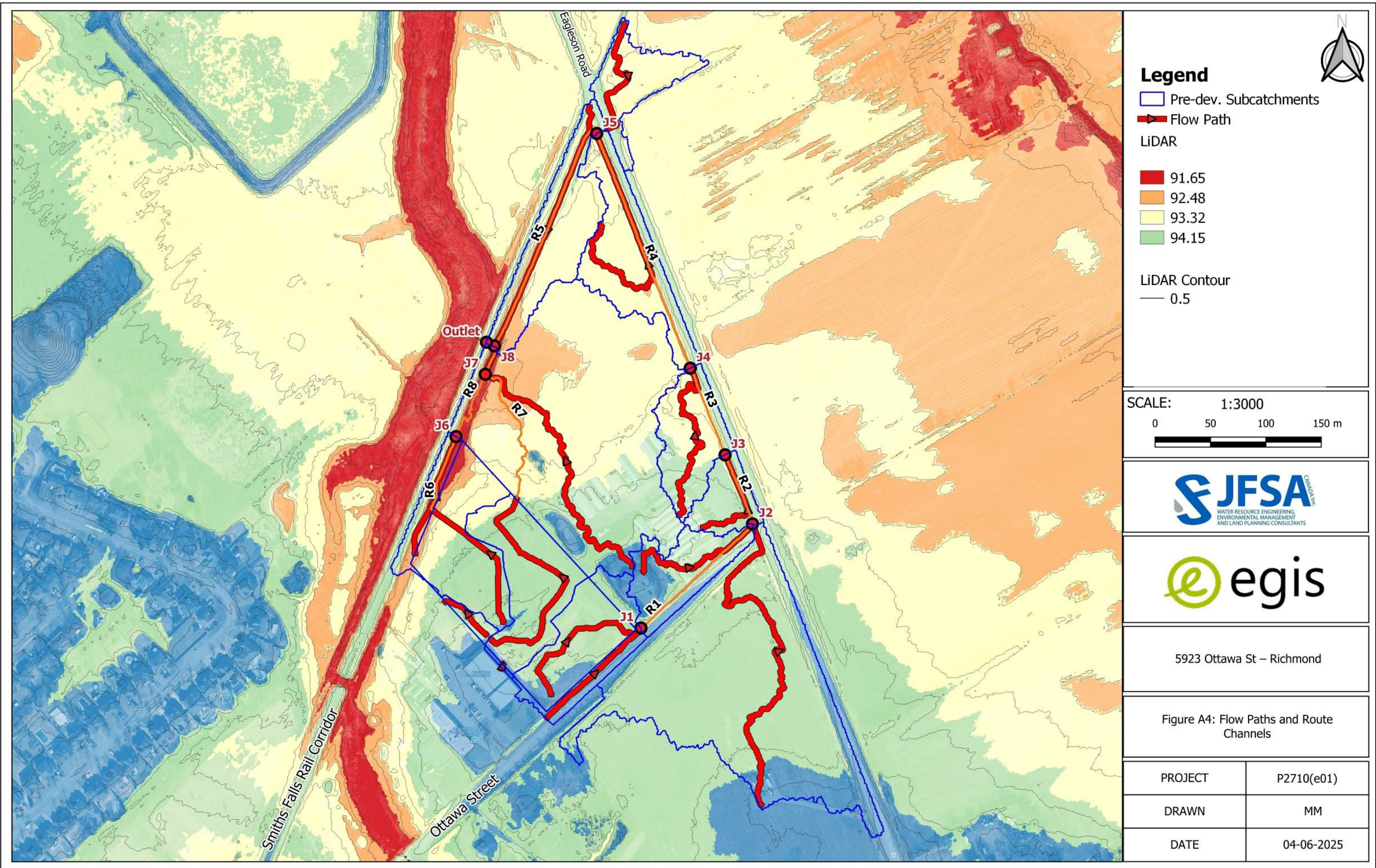


Table A1: Calculation of SCS Curve Number (CN) and Modified Curve Number (CN*)

EXT1 (3.212 ha)							
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
0.107	Transportation	GRENVILLE	Fair	B	98	3.3%	3.3
0.229	Tilled	GRENVILLE	Fair	B	69	7.1%	4.9
0.403	Transportation	BRANDON	Fair	D	98	12.5%	12.3
2.472	Tilled	BRANDON	Fair	D	84	77.0%	64.6
						CN	85
						CN*	80

EXT2 (0.285 ha)							
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
0.04	Built Up Area - Pervious	NORTH GOWER	Fair	D	80	14.0%	11.2
0.051	Tilled	NORTH GOWER	Fair	D	84	17.9%	15.0
0.067	Forest	NORTH GOWER	Fair	D	79	23.5%	18.6
0.127	Transportation	NORTH GOWER	Fair	D	98	44.6%	43.7
						CN	89
						CN*	85

EXT3 (0.56 ha)							
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
0	Forest	NORTH GOWER	Fair	D	79	0.0%	0.0
0.17	Transportation	NORTH GOWER	Fair	D	98	30.4%	29.8
0.39	Built Up Area - Pervious	NORTH GOWER	Fair	D	80	69.6%	55.7
						CN	85
						CN*	80

EXT4 (0.309 ha)							
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
0.074	Transportation	BRANDON	Fair	D	98	23.9%	23.5
0.235	Built Up Area - Pervious	BRANDON	Fair	D	80	76.1%	60.8
						CN	84
						CN*	79

EXT5 (0.594 ha)							
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
0.084	Transportation	BRANDON	Fair	D	98	14.1%	13.9
0.51	Built Up Area - Pervious	NORTH GOWER	Fair	D	80	85.9%	68.7
						CN	83
						CN*	76

Table A1: Calculation of SCS Curve Number (CN) and Modified Curve Number (CN*)

EXT6 (0.864 ha)							
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
0.271	Transportation	DALHOUSIE	Fair	D	98	31.4%	30.7
0.593	Tilled	DALHOUSIE	Fair	D	84	68.6%	57.7
						CN	88
						CN*	85

EXT7 (0.47 ha)							
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
0.097	Transportation	DALHOUSIE	Fair	D	98	20.6%	20.2
0.374	Tilled	DALHOUSIE	Fair	D	84	79.6%	66.8
						CN	87
						CN*	83

EXT8 (0.835 ha)							
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
0.036	Transportation	DALHOUSIE	Fair	D	98	4.3%	4.2
0.798	Tilled	NORTH GOWER	Fair	D	84	95.6%	80.3
						CN	85
						CN*	79

EXT9 (3.572 ha)							
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
0.001	Transportation	NORTH GOWER	Fair	D	98	0.0%	0.0
0.126	Forest	NORTH GOWER	Fair	D	79	3.5%	2.8
0.998	Built Up Area - Pervious	NORTH GOWER	Fair	D	80	27.9%	22.4
2.446	Tilled	NORTH GOWER	Fair	D	84	68.5%	57.5
						CN	83
						CN*	76

EXT9a (0.011 ha)							
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
0.011	Tilled	NORTH GOWER	Fair	D	84	100.0%	84.0
						CN	84
						CN*	78

EXT10 (0.203 ha)							
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
0.203	Forest	ERODED CHANNEL	Fair	D	79	100.0%	79.0
						CN	79
						CN*	71

Table A1: Calculation of SCS Curve Number (CN) and Modified Curve Number (CN*)

Pre10 (0.803 ha)							
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
0.803	Forest	ERODED CHANNEL	Fair	D	79	100.0%	79.0
						CN	79
						CN*	71

Pre11 (0.069 ha)							
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
0.004	Forest	NORTH GOWER	Fair	D	79	5.8%	4.6
0.065	Tilled	NORTH GOWER	Fair	D	84	94.2%	79.1
						CN	84
						CN*	78

Pre2 (0.565 ha)							
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
0.017	Transportation	NORTH GOWER	Fair	D	98	3.0%	2.9
0.066	Forest	NORTH GOWER	Fair	D	79	11.7%	9.2
0.483	Tilled	NORTH GOWER	Fair	D	84	85.5%	71.8
						CN	84
						CN*	78

Pre9 (0.83 ha)							
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
0	Built Up Area - Pervious	NORTH GOWER	Fair	D	80	0.0%	0.0
0.014	Tilled	NORTH GOWER	Fair	D	84	1.7%	1.4
0.815	Forest	NORTH GOWER	Fair	D	79	98.2%	77.6
						CN	79
						CN*	71

Table A2: Time to Peak Calculations

Parameter	Units	EXT1	EXT2	EXT3	EXT4	EXT5	EXT6	EXT7	EXT8	EXT9	EXT9a	EXT10	Pre10	Pre11	Pre2	Pre9
Area	ha	3.211	0.285	0.560	0.309	0.594	0.864	0.471	0.834	3.571	0.011	0.203	0.803	0.069	0.566	0.829
CN	-	80	85	80	79	76	85	83	79	76	78	71	71	78	78	71
Ptotal to calc C from CN, use 2 yr 24 hr Chicago storm	P(mm)	48.7	48.7	48.7	48.7	48.7	48.7	48.7	48.7	48.7	48.7	48.7	48.7	48.7	48.7	48.7
	la(mm)	5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00
	RV(mm)	17.7	21.4	18.0	16.9	15.4	21.2	19.7	17.1	15.6	16.7	12.9	12.9	16.4	16.7	12.9
C (From Chicago storm)	-	0.363	0.439	0.370	0.348	0.317	0.436	0.404	0.351	0.319	0.342	0.265	0.265	0.337	0.342	0.265
Length of Channel	m	404	121	161	116	215	279	140	263	344	5	121	135	54	145	236
	ft	1327	397	527	381	705	916	459	862	1128	15	398	443	176	475	776
Elevation of Head Water	m	94.63	94.17	94.91	93.95	94.08	92.97	93.24	93.52	94.94	94.74	91.69	94.14	94.09	94.34	94.11
	ft	310	309	311	308	309	305	306	307	311	311	301	309	309	310	309
Elevation of Outlet	m	92.98	93.57	93.00	92.69	92.44	91.96	92.11	90.43	90.46	94.55	91.11	91.71	93.58	93.80	93.20
	ft	305	307	305	304	303	302	302	297	297	310	299	301	307	308	306
Average Slope	%	0.41%	0.50%	1.18%	1.08%	0.76%	0.36%	0.81%	1.17%	1.30%	4.28%	0.49%	1.80%	0.96%	0.38%	0.38%
Flow Type (Uplands)	-	B	B	B	B	B	B	B	B	B	B	B	B	B	B	B
Kirpich																
Time of Concentration	mins	16	6	5	4	8	13	6	8	9	0	6	4	2	8	11
Time to Peak	min	11	4	4	3	5	9	4	5	6	0	4	3	2	5	7
Time to Peak	Hours	0.18	0.07	0.06	0.05	0.09	0.14	0.06	0.09	0.10	0.00	0.07	0.04	0.03	0.09	0.12
FAA (From Chicago storm)																
Time of Concentration	mins	65	30	29	26	41	51	29	37	43	3	38	26	18	41	58
Time to Peak	mins	43	20	19	17	27	34	19	25	29	2	25	17	12	27	38
Time to Peak	Hours	0.72	0.33	0.32	0.29	0.45	0.56	0.32	0.42	0.48	0.04	0.42	0.29	0.21	0.46	0.64
Barnsby Williams																
Time of Concentration	mins	25	9	9	7	14	20	9	15	17	0	9	7	4	11	17
Time to Peak	mins	17	6	6	5	9	13	6	10	11	0	6	5	3	7	11
Time to Peak	Hours	0.28	0.10	0.11	0.08	0.15	0.22	0.10	0.17	0.18	0.00	0.10	0.08	0.05	0.12	0.19
SCS																
Time of Concentration	mins	63	18	17	15	31	42	17	27	34	1	28	16	9	30	54
Time to Peak	mins	42	12	12	10	21	28	12	18	23	0	19	11	6	20	36
Time to Peak	Hours	0.70	0.20	0.19	0.16	0.34	0.47	0.19	0.30	0.38	0.01	0.31	0.18	0.10	0.34	0.61
Uplands																
Time of Concentration	mins	69	19	16	12	27	50	17	26	33	0	19	11	6	26	41
Time to Peak	mins	46	12	11	8	18	34	11	18	22	0	13	7	4	17	28
Time to Peak	Hours	0.76	0.21	0.18	0.13	0.30	0.56	0.19	0.29	0.36	0.00	0.21	0.12	0.07	0.28	0.46
Selected Method: FAA (From Chicago storm)																
Time to Peak	min	43	20	19	17	27	34	19	25	29	2	25	17	12	27	38
Time to Peak	Hours	0.72	0.33	0.32	0.29	0.45	0.56	0.32	0.42	0.48	0.04	0.42	0.29	0.21	0.46	0.64
Velocity	m/s	0.16	0.10	0.14	0.11	0.13	0.14	0.12	0.18	0.20	0.04	0.08	0.13	0.07	0.09	0.10


```

1  20      Metric units / ID numbers OFF
2  *#*****
   *****
3  *#  SWMHYMO  / INPUT DATA FILE
4  *#*****
   *****
5  *#  Project Name   : [5923 Ottawa St]
6  *#  Project Number: [P2710(e01)]
7  *#  Date           : [2025 FEB 05]
8  *#  Modeller       : [MM]
9  *#  Company        : JFSA Canada Inc.
10 *#  License #      : 2549237
11 *#*****
   *****
12 *# Model developed to simulate runoff from subcatchments under pre development conditions
13 *#*****
   *****
14 *%  25 mm Storm based on 2-Year, 3-Hour Chicago Storm
15 START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[002]
16                ["002YC3H.stm"] <--storm filename, one per line for NSTORM time
17 *%-----|-----
18 READ STORM      STORM_FILENAME=["STORM.001"]
19 *%-----|-----
20 *#*****
   *****
21 *#  EXT1
22 *#*****
   *****
23 CALIB NASHYD    NHYD=["EXT1"], DT[1] (min), AREA=[3.211] (ha),
24                DWF=[0] (cms), CN=[80],
25                IA=[4.67] (mm), N=[3], TP[0.72] (hrs),
26                RAINFALL[ , , -1]
27 *#*****
   *****
28 *#  EXT2
29 *#*****
   *****
30 CALIB NASHYD    NHYD=["EXT2"], DT[1] (min), AREA=[0.285] (ha),
31                DWF=[0] (cms), CN=[85],
32                IA=[4.67] (mm), N=[3], TP[0.33] (hrs),
33                RAINFALL[ , , -1]
34 *#*****
   *****
35 *#  EXT3
36 *#*****
   *****
37 CALIB NASHYD    NHYD=["EXT3"], DT[1] (min), AREA=[0.560] (ha),
38                DWF=[0] (cms), CN=[80],
39                IA=[4.67] (mm), N=[3], TP[0.32] (hrs),
40                RAINFALL[ , , -1]
41 *#*****
   *****
42 *#  EXT4
43 *#*****
   *****
44 CALIB NASHYD    NHYD=["EXT4"], DT[1] (min), AREA=[0.309] (ha),
45                DWF=[0] (cms), CN=[79],
46                IA=[4.67] (mm), N=[3], TP[0.29] (hrs),
47                RAINFALL[ , , -1]
48 *#*****
   *****
49 *#  EXT5
50 *#*****
   *****
51 CALIB NASHYD    NHYD=["EXT5"], DT[1] (min), AREA=[0.594] (ha),
52                DWF=[0] (cms), CN=[76],
53                IA=[4.67] (mm), N=[3], TP[0.45] (hrs),
54                RAINFALL[ , , -1]
55 *#*****

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*****
56 *# EXT6
57 *#*****
*****
58 CALIB NASHYD      NHYD=["EXT6"], DT[1] (min), AREA=[0.864] (ha),
59                   DWF=[0] (cms), CN=[85],
60                   IA=[4.67] (mm), N=[3], TP[0.56] (hrs),
61                   RAINFALL[ , , -1]
62 *#*****
*****
63 *# EXT7
64 *#*****
*****
65 CALIB NASHYD      NHYD=["EXT7"], DT[1] (min), AREA=[0.471] (ha),
66                   DWF=[0] (cms), CN=[83],
67                   IA=[4.67] (mm), N=[3], TP[0.32] (hrs),
68                   RAINFALL[ , , -1]
69 *#*****
*****
70 *# EXT8
71 *#*****
*****
72 CALIB NASHYD      NHYD=["EXT8"], DT[1] (min), AREA=[0.834] (ha),
73                   DWF=[0] (cms), CN=[79],
74                   IA=[4.67] (mm), N=[3], TP[0.42] (hrs),
75                   RAINFALL[ , , -1]
76 *#*****
*****
77 *# EXT9
78 *#*****
*****
79 CALIB NASHYD      NHYD=["EXT9"], DT[1] (min), AREA=[3.571] (ha),
80                   DWF=[0] (cms), CN=[76],
81                   IA=[4.67] (mm), N=[3], TP[0.48] (hrs),
82                   RAINFALL[ , , -1]
83 *#*****
*****
84 *# EXT9a
85 *#*****
*****
86 CALIB NASHYD      NHYD=["EXT9a"], DT[1] (min), AREA=[0.011] (ha),
87                   DWF=[0] (cms), CN=[78],
88                   IA=[4.67] (mm), N=[3], TP[0.04] (hrs),
89                   RAINFALL[ , , -1]
90 *#*****
*****
91 *# EXT10
92 *#*****
*****
93 CALIB NASHYD      NHYD=["EXT10"], DT[1] (min), AREA=[0.203] (ha),
94                   DWF=[0] (cms), CN=[71],
95                   IA=[4.67] (mm), N=[3], TP[0.42] (hrs),
96                   RAINFALL[ , , -1]
97 *#*****
*****
98 *# Pre2
99 *#*****
*****
100 CALIB NASHYD      NHYD=["Pre2"], DT[1] (min), AREA=[0.566] (ha),
101                   DWF=[0] (cms), CN=[78],
102                   IA=[4.67] (mm), N=[3], TP[0.46] (hrs),
103                   RAINFALL[ , , -1]
104 *#*****
*****
105 *# Pre9
106 *#*****
*****
107 CALIB NASHYD      NHYD=["Pre9"], DT[1] (min), AREA=[0.829] (ha),
108                   DWF=[0] (cms), CN=[71],

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109 IA=[4.67] (mm), N=[3], TP[0.64] (hrs),
110 RAINFALL[ , , -1]
111 *#*****
112 *# Pre10
113 *#*****
114 CALIB NASHYD NHYD=["Pre10"], DT[1] (min), AREA=[0.803] (ha),
115 DWF=[0] (cms), CN=[71],
116 IA=[4.67] (mm), N=[3], TP[0.29] (hrs),
117 RAINFALL[ , , -1]
118 *#*****
119 *# Pre11
120 *#*****
121 CALIB NASHYD NHYD=["Pre11"], DT[1] (min), AREA=[0.069] (ha),
122 DWF=[0] (cms), CN=[78],
123 IA=[4.67] (mm), N=[3], TP[0.21] (hrs),
124 RAINFALL[ , , -1]
125 *#*****
126 ADD HYD NHYDsum=["J1"], NHYDs to add=["EXT2"+"Pre2"]
127 *%-----|-----
128 * NOTE: Cross-section number 849.0434 is taken from HEC-RAS Model
129 * NOTE: SEGROUGH will be adjusted after completing the HEC-RAS model
130 ROUTE CHANNEL NHYDout=["R1"], NHYDin=["J1"], RDT=[1] (min),
131 CHLGTH=[143.151] (m), CHSLOPE=[0.394] (%), FPSLOPE=[0.394] (%),
132 SECNUM=[849.0434], NSEG=[3],
133 ( SEGROUGH, SEGDIST (m))=[0.08,18.95 -0.035,26.78 0.08,35.18] NSEG
times
134 ( DISTANCE (m), ELEVATION (m))=[0.48, 94.05]
135 [3.19, 93.99]
136 [6.85, 93.91]
137 [10.48, 93.87]
138 [17.45, 93.85]
139 [18.95, 93.84]
140 [20.36, 93.81]
141 [22.3, 93.76]
142 [22.53, 93.72]
143 [23.98, 93.35]
144 [24.35, 93.33]
145 [24.65, 93.37]
146 [25.04, 93.45]
147 [26.04, 93.74]
148 [26.44, 93.82]
149 [26.78, 93.87]
150 [29.14, 94.11]
151 [33.98, 94.26]
152 [35.18, 94.26]
153 *%-----|-----
154 ADD HYD NHYDsum=["J2"], NHYDs to add=["R1"+"EXT3"+"EXT1"]
155 *%-----|-----
156 * NOTE: Cross-section number 737.5813 is taken from HEC-RAS Model
157 * NOTE: SEGROUGH will be adjusted after completing the HEC-RAS model
158 ROUTE CHANNEL NHYDout=["R2"], NHYDin=["J2"], RDT=[1] (min),
159 CHLGTH=[73.338] (m), CHSLOPE=[0.425] (%), FPSLOPE=[0.425] (%),
160 SECNUM=[737.5813], NSEG=[3],
161 ( SEGROUGH, SEGDIST (m))=[0.08,8.4 -0.035,16.42 0.08,22.6] NSEG
times
162 ( DISTANCE (m), ELEVATION (m))=[0, 93.52]
163 [1.08, 93.5]
164 [4.37, 93.48]
165 [6.31, 93.45]
166 [8.4, 93.38]
167 [9.5, 93.31]
168 [10.49, 93.23]
169 [10.99, 93.18]
170 [12.4, 92.94]

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171                                     [13.11, 92.84]
172                                     [13.67, 92.92]
173                                     [16.42, 93.6]
174                                     [16.91, 93.65]
175                                     [17.97, 93.65]
176                                     [19, 93.83]
177                                     [19.51, 93.89]
178                                     [21.06, 93.94]
179                                     [22.6, 93.95]
180 *%-----|-----
181 ADD HYD          NHYDsum=["J3"], NHYDs to add=["R2"+"EXT4"]
182 *%-----|-----
183 * NOTE: Cross-section number 675.4097 is taken from HEC-RAS Model
184 * NOTE: SEGROUGH will be adjusted after completing the HEC-RAS model
185 ROUTE CHANNEL    NHYDout=["R3"], NHYDin=["J3"], RDT=[1] (min),
186                  CHLGTH=[92.08] (m), CHSLOPE=[0.274] (%), FPSLOPE=[0.274] (%),
187                  SECNUM=[675.4097], NSEG=[3],
188                  ( SEGROUGH, SEGDIST (m))=[0.08,31.64 -0.035,42.44 0.08,48.87] NSEG
189                  times
190                  ( DISTANCE (m), ELEVATION (m))=[30.59, 93.12]
191                  [31.64, 93.13]
192                  [34.35, 93.08]
193                  [35.18, 93.03]
194                  [37.78, 92.72]
195                  [38.25, 92.64]
196                  [38.7, 92.61]
197                  [39.74, 92.76]
198                  [42.44, 93.41]
199                  [42.89, 93.49]
200                  [43.97, 93.57]
201                  [44.92, 93.6]
202                  [46.07, 93.67]
203                  [48.87, 93.74]
204 *%-----|-----
205 ADD HYD          NHYDsum=["J4"], NHYDs to add=["R3"+"EXT5"]
206 *%-----|-----
207 * NOTE: Cross-section number 518.7506 is taken from HEC-RAS Model
208 * NOTE: SEGROUGH will be adjusted after completing the HEC-RAS model
209 ROUTE CHANNEL    NHYDout=["R4"], NHYDin=["J4"], RDT=[1] (min),
210                  CHLGTH=[251.495] (m), CHSLOPE=[0.19] (%), FPSLOPE=[0.19] (%),
211                  SECNUM=[518.7506], NSEG=[3],
212                  ( SEGROUGH, SEGDIST (m))=[0.08,51.48 -0.035,59.39 0.08,66.4] NSEG
213                  times
214                  ( DISTANCE (m), ELEVATION (m))=[0, 92.92]
215                  [4.26, 92.9]
216                  [48.31, 92.76]
217                  [51.48, 92.76]
218                  [53.64, 92.7]
219                  [55.33, 92.29]
220                  [55.44, 92.29]
221                  [56.43, 92.37]
222                  [56.97, 92.43]
223                  [59.39, 93.27]
224                  [59.74, 93.37]
225                  [60.8, 93.52]
226                  [63.31, 93.71]
227                  [66.4, 93.76]
228 *%-----|-----
229 ADD HYD          NHYDsum=["J5"], NHYDs to add=["R4"+"EXT6"+"EXT7"]
230 *%-----|-----
231 * NOTE: Cross-section number 275.0857 is taken from HEC-RAS Model
232 * NOTE: SEGROUGH will be adjusted after completing the HEC-RAS model
233 ROUTE CHANNEL    NHYDout=["R5"], NHYDin=["J5"], RDT=[1] (min),
234                  CHLGTH=[237.343] (m), CHSLOPE=[0.644] (%), FPSLOPE=[0.644] (%),
235                  SECNUM=[275.0857], NSEG=[3],
236                  ( SEGROUGH, SEGDIST (m))=[0.08,40.82 -0.035,53.64 0.08,57.93] NSEG
237                  times
238                  ( DISTANCE (m), ELEVATION (m))=[36.16, 92.63]
239                  [40.82, 92.97]

```



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237 [41.39, 92.9]
238 [44.69, 91.72]
239 [45.24, 91.58]
240 [46.33, 91.43]
241 [47.41, 91.64]
242 [47.87, 91.75]
243 [49.59, 92.2]
244 [50.99, 92.36]
245 [51.44, 92.48]
246 [53.18, 92.98]
247 [53.64, 93.15]
248 [55.92, 93.66]
249 [57.93, 93.68]
250 *%-----|-----
251 * NOTE: Cross-section number 124 is taken from HEC-RAS Model
252 * NOTE: SEGROUGH will be adjusted after completing the HEC-RAS model
253 ROUTE CHANNEL NHYDout=["R6"], NHYDin=["Pre10"], RDT=[1] (min),
254 CHLGTH=[77.414] (m), CHSLOPE=[0.776] (%), FPSLOPE=[0.776] (%),
255 SECNUM=[124], NSEG=[3],
256 ( SEGROUGH, SEGDIST (m))=[0.08,8.34 -0.035,31.31 0.08,84.97] NSEG
times
( DISTANCE (m), ELEVATION (m))=[1.78, 93.73]
[4.51, 93.54]
[5.06, 93.31]
[7.25, 92.98]
[7.79, 92.77]
[8.34, 92.49]
[9.43, 91.93]
[9.68, 91.81]
[10.53, 91.27]
[12.64, 90.92]
[14.44, 90.9]
[16.54, 91.06]
[17.64, 91.06]
[30.22, 92.3]
[31.31, 92.45]
[33.5, 92.41]
[55.37, 93.11]
[57.01, 93.2]
[84.97, 93.43]
276 *%-----|-----
277 * NOTE: Cross-section number 74 is taken from HEC-RAS Model
278 * NOTE: SEGROUGH will be adjusted after completing the HEC-RAS model
279 ROUTE CHANNEL NHYDout=["R7"], NHYDin=["Pre9"], RDT=[1] (min),
280 CHLGTH=[159.151] (m), CHSLOPE=[1.576] (%), FPSLOPE=[1.576] (%),
281 SECNUM=[74], NSEG=[3],
282 ( SEGROUGH, SEGDIST (m))=[0.08,4.67 -0.035,81.24 0.08,82.88] NSEG
times
( DISTANCE (m), ELEVATION (m))=[1.94, 93.64]
[4.67, 93.32]
[5.77, 93.15]
[7.41, 92.69]
[7.95, 92.37]
[9.36, 91.71]
[10.12, 91.22]
[10.49, 91.06]
[12.64, 90.89]
[16.16, 90.92]
[18.83, 91.66]
[19.59, 92.02]
[21.62, 92.39]
[24.87, 92.48]
[30.37, 92.55]
[34.37, 92.65]
[77.41, 92.82]
[80.6, 93.25]
[81.24, 93.48]
[82.88, 93.79]
303 *%-----|-----

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304 ADD HYD NHYDsum=["J6"], NHYDs to add=["R6"+"EXT10"]
305 *%-----|-----
306 * NOTE: Cross-section number 49 is taken from HEC-RAS Model
307 * NOTE: SEGROUGH will be adjusted after completing the HEC-RAS model
308 ROUTE CHANNEL NHYDout=["R8"], NHYDin=["J6"], RDT=[1] (min),
309 CHLGTH=[78.801] (m), CHSLOPE=[0.522] (%), FPSLOPE=[0.522] (%),
310 SECNUM=[49], NSEG=[3],
311 ( SEGROUGH, SEGDIST (m))=[0.08,8.71 -0.035,20.59 0.08,116.73] NSEG
times
( DISTANCE (m), ELEVATION (m))=[0, 93.36]
[1.93, 93.63]
[4.61, 93.26]
[6.23, 93.1]
[8.19, 92.26]
[8.71, 91.84]
[9.86, 91.47]
[10.53, 91.04]
[13.84, 91]
[14.5, 91.11]
[16.97, 91.27]
[20.59, 91.76]
[23.3, 91.64]
[30.34, 91.85]
[35.29, 91.92]
[116.73, 92.96]
328 *%-----|-----
329 ADD HYD NHYDsum=["J7"], NHYDs to add=["R8"+"R7"]
330 *%-----|-----
331 * NOTE: Cross-section number 7 is taken from HEC-RAS Model
332 * NOTE: SEGROUGH will be adjusted after completing the HEC-RAS model
333 ROUTE CHANNEL NHYDout=["R9"], NHYDin=["J7"], RDT=[1] (min),
334 CHLGTH=[29.445] (m), CHSLOPE=[0.887] (%), FPSLOPE=[0.887] (%),
335 SECNUM=[7], NSEG=[3],
336 ( SEGROUGH, SEGDIST (m))=[0.08,1.5 -0.035,22.44 0.08,100.08] NSEG
times
( DISTANCE (m), ELEVATION (m))=[0, 93.4]
[1.5, 93.63]
[3.13, 93.62]
[4.76, 93.28]
[5.3, 93.25]
[6.52, 93.08]
[6.96, 92.95]
[10.57, 90.95]
[13.59, 90.67]
[15.83, 90.72]
[16.42, 90.85]
[18.66, 91.76]
[20.82, 91.86]
[22.44, 91.92]
[27.84, 91.98]
[30.15, 91.96]
[100.08, 92.61]
354 *%-----|-----
355 ADD HYD NHYDsum=["J8"], NHYDs to add=["EXT9"+"R9"+"EXT8"+"R5"]
356 *%-----|-----
357 * Note: The pipe needs to be adjusted based on the Culvert-under-railway information
358 ROUTE PIPE PTYPE=[1]circ, NHYDout=["Outlet"], RNUMBER=[1.0],
359 PDIAM=[525] (mm), PLNGTH=[8.407] (m), PROUGH=[0.013],
PSLOPE=[0.0001] (m/m),
NHYDin=["J8"], RDT=[1] (min)
361 *%-----|-----
362 *#####
363 *# STORMS
364 *#####
365 *% 2-Year, 3-Hour Chicago Storm
366 START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[002]
367 ["002YC3H.stm"] <--storm filename, one per line for NSTORM time
368 *%-----|-----
369 *% 5-Year, 3-Hour Chicago Storm

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370 START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[005]
371 ["005YC3H.stm"] <--storm filename, one per line for NSTORM time
372 *%-----|
373 *% 10-Year, 3-Hour Chicago Storm
374 START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[010]
375 ["010YC3H.stm"] <--storm filename, one per line for NSTORM time
376 *%-----|
377 *% 25-Year, 3-Hour Chicago Storm
378 START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[025]
379 ["025YC3H.stm"] <--storm filename, one per line for NSTORM time
380 *%-----|
381 *% 50-Year, 3-Hour Chicago Storm
382 START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[050]
383 ["050YC3H.stm"] <--storm filename, one per line for NSTORM time
384 *%-----|
385 *% 100-Year, 3-Hour Chicago Storm
386 START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[099]
387 ["100YC3H.stm"] <--storm filename, one per line for NSTORM time
388 *%-----|
389 *% 2-Year, 24-Hour SCS Storm
390 START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[102]
391 ["SC24002x.stm"] <--storm filename, one per line for NSTORM time
392 *%-----|
393 *% 5-Year, 24-Hour SCS Storm
394 START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[105]
395 ["SC24005x.stm"] <--storm filename, one per line for NSTORM time
396 *%-----|
397 *% 10-Year, 24-Hour SCS Storm
398 START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[110]
399 ["SC24010x.stm"] <--storm filename, one per line for NSTORM time
400 *%-----|
401 *% 25-Year, 24-Hour SCS Storm
402 START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[125]
403 ["SC24025x.stm"] <--storm filename, one per line for NSTORM time
404 *%-----|
405 *% 50-Year, 24-Hour SCS Storm
406 START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[150]
407 ["SC24050x.stm"] <--storm filename, one per line for NSTORM time
408 *%-----|
409 *% 100-Year, 24-Hour SCS Storm
410 START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[199]
411 ["SC24100x.stm"] <--storm filename, one per line for NSTORM time
412 *%-----|
413 *% 100-Year, 24-Hour SCS Storm + 20%
414 *START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[998]
415 *%              ["SC24100x+.stm"] <--storm filename, one per line for NSTORM time
416 *%-----|
417 *% 100-Year, 3-Hour Chicago Storm + 20%
418 *START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[999]
419 *              ["100YRCHI3HR+.stm"] <--storm filename, one per line for NSTORM time
420 *%-----|
421 FINISH

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Page 0


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00362) # Extra
00363) CALIB NASHID 1.0 01:EXtr9a -----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00364) [CN: 79.0; W: 3.00; Tpm: .42]
00365) CALIB NASHID 1.0 01:EXtr9a .01 .001 No_date 1:00 13.07 .307 .000
00366) [CN: 79.0; W: 3.00; Tpm: .42]
00367) *****
00368) [CN: 79.0; W: 3.00; Tpm: .42]
00369) *****
00370) R0010/C00013-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00371) CALIB NASHID 1.0 01:EXtr10 -----
00372) [CN: 71.0; W: 3.00; Tpm: .42]
00373) *****
00374) # Fe#2
00375) R0010/C00014-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00376) CALIB NASHID 1.0 01:Fe#2 -----
00377) [CN: 71.0; W: 3.00; Tpm: .42]
00378) *****
00379) R0010/C00017-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00380) CALIB NASHID 1.0 01:Fe#1 -----
00381) [CN: 71.0; W: 3.00; Tpm: .42]
00382) *****
00383) R0010/C00015-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00384) CALIB NASHID 1.0 01:Fe#9 -----
00385) [CN: 71.0; W: 3.00; Tpm: .42]
00386) *****
00387) R0010/C00016-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00388) CALIB NASHID 1.0 01:Fe#10 -----
00389) [CN: 71.0; W: 3.00; Tpm: .42]
00390) *****
00391) R0010/C00017-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00392) # Fe#1
00393) CALIB NASHID 1.0 01:Fe#1 -----
00394) [CN: 71.0; W: 3.00; Tpm: .42]
00395) *****
00396) R0010/C00017-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00397) CALIB NASHID 1.0 01:Fe#1 -----
00398) [CN: 71.0; W: 3.00; Tpm: .42]
00399) *****
00400) ADD HYD 1.0 02:EXtr2 -----
00401) [CN: 71.0; W: 3.00; Tpm: .42]
00402) *****
00403) R0010/C00019-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00404) ROUTE CHANNEL -----
00405) [CN: 71.0; W: 3.00; Tpm: .42]
00406) *****
00407) R0010/C00017-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00408) CALIB NASHID 1.0 01:Fe#1 -----
00409) [CN: 71.0; W: 3.00; Tpm: .42]
00410) *****
00411) R0010/C00019-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00412) ROUTE CHANNEL -----
00413) [CN: 71.0; W: 3.00; Tpm: .42]
00414) *****
00415) [L/S= 143.7 / 394 / 035]
00416) (Vmax = 231/Max)
00417) R0010/C00019-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00418) CALIB NASHID 1.0 01:Fe#1 -----
00419) [CN: 71.0; W: 3.00; Tpm: .42]
00420) *****
00421) R0010/C00019-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00422) ROUTE CHANNEL -----
00423) [CN: 71.0; W: 3.00; Tpm: .42]
00424) *****
00425) [L/S= 92.7 / 274 / 035]
00426) (Vmax = 337/Max)
00427) R0010/C00024-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00428) ADD HYD 1.0 02:EXtr3 -----
00429) [CN: 71.0; W: 3.00; Tpm: .42]
00430) *****
00431) R0010/C00025-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00432) ROUTE CHANNEL -----
00433) [CN: 71.0; W: 3.00; Tpm: .42]
00434) *****
00435) [L/S= 251.7 / 190 / 035]
00436) (Vmax = 323/Max)
00437) R0010/C00018-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00438) ADD HYD 1.0 02:EXtr6 -----
00439) [CN: 71.0; W: 3.00; Tpm: .42]
00440) *****
00441) R0010/C00027-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00442) ROUTE CHANNEL -----
00443) [CN: 71.0; W: 3.00; Tpm: .42]
00444) *****
00445) [L/S= 217.7 / 644 / 035]
00446) (Vmax = 519/Max)
00447) R0010/C00018-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00448) ADD HYD 1.0 02:EXtr7 -----
00449) [CN: 71.0; W: 3.00; Tpm: .42]
00450) *****
00451) R0010/C00018-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00452) ROUTE CHANNEL -----
00453) [CN: 71.0; W: 3.00; Tpm: .42]
00454) *****
00455) [L/S= 251.7 / 190 / 035]
00456) (Vmax = 323/Max)
00457) R0010/C00018-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00458) ADD HYD 1.0 02:EXtr6 -----
00459) [CN: 71.0; W: 3.00; Tpm: .42]
00460) *****
00461) R0010/C00018-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00462) ROUTE CHANNEL -----
00463) [CN: 71.0; W: 3.00; Tpm: .42]
00464) *****
00465) [L/S= 251.7 / 190 / 035]
00466) (Vmax = 323/Max)
00467) R0010/C00018-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00468) ADD HYD 1.0 02:EXtr6 -----
00469) [CN: 71.0; W: 3.00; Tpm: .42]
00470) *****
00471) R0010/C00018-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00472) ROUTE CHANNEL -----
00473) [CN: 71.0; W: 3.00; Tpm: .42]
00474) *****
00475) [L/S= 251.7 / 190 / 035]
00476) (Vmax = 323/Max)
00477) R0010/C00018-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00478) ADD HYD 1.0 02:EXtr6 -----
00479) [CN: 71.0; W: 3.00; Tpm: .42]
00480) *****
00481) R0010/C00018-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00482) ROUTE CHANNEL -----
00483) [CN: 71.0; W: 3.00; Tpm: .42]
00484) *****
00485) [L/S= 251.7 / 190 / 035]
00486) (Vmax = 323/Max)
00487) R0010/C00018-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00488) ADD HYD 1.0 02:EXtr6 -----
00489) [CN: 71.0; W: 3.00; Tpm: .42]
00490) *****
00491) R0010/C00018-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00492) ROUTE CHANNEL -----
00493) [CN: 71.0; W: 3.00; Tpm: .42]
00494) *****
00495) [L/S= 251.7 / 190 / 035]
00496) (Vmax = 323/Max)
00497) R0010/C00018-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00498) ADD HYD 1.0 02:EXtr6 -----
00499) [CN: 71.0; W: 3.00; Tpm: .42]
00500) *****
00501) R0010/C00018-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00502) ROUTE CHANNEL -----
00503) [CN: 71.0; W: 3.00; Tpm: .42]
00504) *****
00505) [L/S= 251.7 / 190 / 035]
00506) (Vmax = 323/Max)
00507) R0010/C00018-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00508) ADD HYD 1.0 02:EXtr6 -----
00509) [CN: 71.0; W: 3.00; Tpm: .42]
00510) *****
00511) R0010/C00018-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00512) ROUTE CHANNEL -----
00513) [CN: 71.0; W: 3.00; Tpm: .42]
00514) *****
00515) [L/S= 251.7 / 190 / 035]
00516) (Vmax = 323/Max)
00517) R0010/C00018-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00518) ADD HYD 1.0 02:EXtr6 -----
00519) [CN: 71.0; W: 3.00; Tpm: .42]
00520) *****
00521) R0010/C00018-----Dtn=ID-INVD-----AREAaha-OPEAKs=Peakdate_hh:mm-----Rwm=R-C-----DWfms
00522)
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000001 Date = [2025 FEB 05]
000002 # Modifier = [NM]
000003 # Company = JPSA Canada Inc.
000004 # License # = 2549237
000005 # Model = CHICAGO STORM 25 Year, 3 Hours
000006 # [ID=10.00ID=8 3.00IPTOT= 58.23]
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010811 [RDT= 1.00] out<- 1.0 01:R5 6.86 .318 No_date 1:52 29.83 n/a .000
010812 [L/S/n= 227./, .644/.035]
010813 (Vmax=.658;Dmax=.288)
010814 R0050:C00028-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvm-R.C-----DWfcm
010815 ROUTE CHANNEL -> 1.0 01:Pre0 80 .049 No_date 1:20 22.07 n/a .000
010816 [RDT= 1.00] out<- 1.0 01:R6 80 .048 No_date 1:23 22.07 n/a .000
010817 [L/S/n= 71./, .775/.035]
010818 (Vmax=.492;Dmax=.036)
010819 R0050:C00029-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvm-R.C-----DWfcm
010820 ROUTE CHANNEL -> 1.0 01:Pre0 83 .029 No_date 1:48 22.07 n/a .000
010821 [RDT= 1.00] out<- 1.0 01:R7 83 .029 No_date 1:51 22.07 n/a .000
010822 [L/S/n= 159./, .171/.035]
010823 (Vmax=.797;Dmax=.009)
010824 R0050:C00030-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvm-R.C-----DWfcm
010825 ADD HYD + 1.0 02:R6 80 .048 No_date 1:23 22.08 n/a .000
010826 [RDT= 1.00] out<- 1.0 02:EXT10 .20 .010 No_date 1:30 22.06 n/a .000
010827 SUM= 1.0 02:R7 83 .029 No_date 1:51 22.09 n/a .000
010828 R0050:C00031-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvm-R.C-----DWfcm
010829 ROUTE CHANNEL -> 1.0 02:R6 1.01 .057 No_date 1:24 22.24 n/a .000
010830 [RDT= 1.00] out<- 1.0 01:R8 1.01 .056 No_date 1:27 22.24 n/a .000
010831 [L/S/n= 79./, .522/.035]
010832 (Vmax=.423;Dmax=.042)
010833 R0050:C00032-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvm-R.C-----DWfcm
010834 ADD HYD + 1.0 02:R8 1.01 .056 No_date 1:27 22.24 n/a .000
010835 SUM= 1.0 02:R7 83 .029 No_date 1:51 22.09 n/a .000
010836 R0050:C00033-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvm-R.C-----DWfcm
010837 ROUTE CHANNEL -> 1.0 02:R7 1.83 .079 No_date 1:32 22.17 n/a .000
010838 [RDT= 1.00] out<- 1.0 02:R7 1.83 .079 No_date 1:32 22.17 n/a .000
010839 [L/S/n= 29./, .887/.035]
010840 (Vmax=.543;Dmax=.054)
010841 R0050:C00034-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvm-R.C-----DWfcm
010842 ADD HYD + 1.0 02:EXT9 3.57 .183 No_date 1:35 25.77 n/a .000
010843 [RDT= 1.00] out<- 1.0 02:R9 1.83 .079 No_date 1:33 22.18 n/a .000
010844 [L/S/n= 1.0 02:EXT8 83 .052 No_date 1:30 28.13 n/a .000
010845 SUM= 1.0 02:R5 6.86 .318 No_date 1:52 29.83 n/a .000
010846 [RDT= 1.00] out<- 1.0 02:R6 80 .048 No_date 1:23 22.07 n/a .000
010847 SUM= 1.0 02:R9 1.83 .079 No_date 1:32 22.17 n/a .000
010848 R0050:C00035-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvm-R.C-----DWfcm
010849 ROUTE PIPE -> 1.0 02:R8 13.10 .602 No_date 1:44 27.56 n/a .000
010850 [RDT= 1.00] out<- 1.0 02:R8 13.10 .602 No_date 1:44 27.56 n/a .000
010851 [L/S/n= 8./, .010/.035]
010852 (Vmax=.481;Dmax=.043)
010853 [Dtn= .53;Dused=1.41]
010854 #####
010855 # STORM
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010857 *** END OF RUN 1 98
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01441# R0102/C00014-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01442# CALIB NASHYD 1.0 01:Pre11 .07 .003 No_date 12:07 16.60 343 .000
01443# [CN= 78.0; N= 3.00; Tpe = .46]
01444# # Pre9
01445# *****
01446# *****
01447# R0102/C00015-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01448# CALIB NASHYD 1.0 01:Pre9 .83 .012 No_date 12:37 12.99 268 .000
01449# [CN= 71.0; N= 3.00; Tpe = .44]
01450# *****
01451# # Pre10
01452# *****
01453# R0102/C00016-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01454# CALIB NASHYD 1.0 01:Pre10 .80 .020 No_date 12:12 12.99 268 .000
01455# [CN= 71.0; N= 3.00; Tpe = .44]
01456# *****
01457# # Pre11
01458# *****
01459# R0102/C00017-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01460# CALIB NASHYD 1.0 01:Pre11 .07 .003 No_date 12:07 16.60 343 .000
01461# [CN= 78.0; N= 3.00; Tpe = .21]
01462# *****
01463# R0102/C00018-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01464# ADD HYD + 1.0 02:EXT2 .28 .011 No_date 12:14 21.63 n/a .000
01465# + 1.0 02:EXT2 .57 .013 No_date 12:23 16.61 n/a .000
01466# SUM= 1.0 01:21 .85 .024 No_date 12:18 18.29 n/a .000
01467# R0102/C00019-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01468# ROUTE CHANNEL -> 1.0 02:21 .85 .024 No_date 12:18 18.29 n/a .000
01469# [RDTE=1.00] out<- 1.0 01:R1 .85 .022 No_date 12:25 18.29 n/a .000
01470# [L/S/n= 143./ / .394/.035]
01471# (Vmax=.278;Dmax=.103)
01472# R0102/C00020-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01473# ADD HYD + 1.0 02:R1 .85 .022 No_date 12:25 18.29 n/a .000
01474# + 1.0 02:EXT3 .56 .018 No_date 12:13 17.87 n/a .000
01475# + 1.0 02:EXT3 .31 .021 No_date 12:42 17.87 n/a .000
01476# SUM= 1.0 01:21 4.62 .090 No_date 12:30 17.95 n/a .000
01477# R0102/C00021-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01478# ROUTE CHANNEL -> 1.0 02:22 4.62 .090 No_date 12:30 17.95 n/a .000
01479# [RDTE=1.00] out<- 1.0 01:R2 4.62 .090 No_date 12:33 17.95 n/a .000
01480# [L/S/n= 73./ / .425/.035]
01481# (Vmax=.398;Dmax=.186)
01482# R0102/C00022-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01483# ADD HYD + 1.0 02:R2 4.62 .090 No_date 12:33 17.95 n/a .000
01484# + 1.0 02:EXT4 .31 .010 No_date 12:12 17.22 n/a .000
01485# SUM= 4.93 .096 No_date 12:30 17.90 n/a .000
01486# R0102/C00023-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01487# ROUTE CHANNEL -> 1.0 01:R3 4.93 .095 No_date 12:35 17.90 n/a .000
01488# [RDTE=1.00] out<- 1.0 01:R3 4.93 .095 No_date 12:35 17.90 n/a .000
01489# [L/S/n= 92./ / .274/.035]
01490# (Vmax=.324;Dmax=.186)
01491# R0102/C00024-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01492# ADD HYD + 1.0 02:EXT5 .59 .013 No_date 12:22 15.46 n/a .000
01493# + 1.0 02:EXT5 .52 .022 No_date 12:33 17.64 n/a .000
01494# SUM= 1.0 01:24 5.52 .107 No_date 12:33 17.64 n/a .000
01495# R0102/C00025-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01496# ROUTE CHANNEL -> 1.0 02:24 5.52 .107 No_date 12:33 17.64 n/a .000
01497# [RDTE=1.00] out<- 1.0 01:R4 5.52 .098 No_date 12:46 17.64 n/a .000
01498# [L/S/n= 251./ / .394/.035]
01499# (Vmax=.309;Dmax=.210)
01500# R0102/C00026-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01501# ADD HYD + 1.0 02:R4 5.52 .098 No_date 12:46 17.64 n/a .000
01502# + 1.0 02:EXT6 .20 .004 No_date 12:20 12.99 n/a .000
01503# + 1.0 02:EXT7 .47 .017 No_date 12:13 20.01 n/a .000
01504# SUM= 1.0 01:25 6.86 .128 No_date 12:40 18.31 n/a .000
01505# R0102/C00027-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01506# ROUTE CHANNEL -> 1.0 02:25 6.86 .128 No_date 12:40 18.31 n/a .000
01507# [RDTE=1.00] out<- 1.0 01:R5 6.86 .125 No_date 12:47 18.31 n/a .000
01508# [L/S/n= 237./ / .644/.035]
01509# (Vmax=.501;Dmax=.200)
01510# R0102/C00028-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01511# ROUTE CHANNEL -> 1.0 01:Pre10 .80 .020 No_date 12:12 12.99 n/a .000
01512# [RDTE=1.00] out<- 1.0 01:Pre10 .80 .019 No_date 12:15 12.99 n/a .000
01513# [L/S/n= 77./ / .776/.035]
01514# (Vmax=.492;Dmax=.041)
01515# R0102/C00029-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01516# ROUTE CHANNEL -> 1.0 01:Pre9 .83 .012 No_date 12:37 12.99 n/a .000
01517# [RDTE=1.00] out<- 1.0 01:Pre9 .83 .012 No_date 12:40 12.99 n/a .000
01518# [L/S/n= 159./ / .576/.035]
01519# (Vmax=.797;Dmax=.003)
01520# R0102/C00030-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01521# ADD HYD + 1.0 02:R6 .80 .019 No_date 12:15 13.03 n/a .000
01522# + 1.0 02:EXT10 .20 .004 No_date 12:20 12.99 n/a .000
01523# SUM= 1.0 01:26 1.01 .023 No_date 12:15 13.02 n/a .000
01524# R0102/C00031-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01525# ROUTE CHANNEL -> 1.0 02:26 1.01 .023 No_date 12:15 13.02 n/a .000
01526# [RDTE=1.00] out<- 1.0 01:R8 1.01 .023 No_date 12:19 13.02 n/a .000
01527# [L/S/n= 79./ / .321/.035]
01528# (Vmax=.423;Dmax=.017)
01529# R0102/C00032-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01530# ADD HYD + 1.0 02:R8 1.01 .023 No_date 12:19 13.02 n/a .000
01531# + 1.0 02:R7 .83 .011 No_date 12:40 13.00 n/a .000
01532# SUM= 1.0 01:27 1.83 .032 No_date 12:22 13.02 n/a .000
01533# R0102/C00033-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01534# ROUTE CHANNEL -> 1.0 02:27 1.83 .032 No_date 12:22 13.01 n/a .000
01535# [RDTE=1.00] out<- 1.0 01:R9 1.83 .032 No_date 12:23 13.01 n/a .000
01536# [L/S/n= 29./ / .887/.035]
01537# (Vmax=.543;Dmax=.004)
01538# R0102/C00034-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01539# ADD HYD + 1.0 02:EXT9 3.57 .074 No_date 12:25 15.46 n/a .000
01540# + 1.0 02:R9 1.83 .032 No_date 12:20 13.02 n/a .000
01541# + 1.0 02:EXT8 .83 .021 No_date 12:20 17.22 n/a .000
01542# SUM= 6.86 .129 No_date 12:47 18.31 n/a .000
01543# R0102/C00035-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01544# ROUTE PIPE -> 1.0 01:R10 13.10 .223 No_date 12:35 16.72 n/a .000
01545# [RDTE=1.00] out<- 1.0 01:Outlet 13.10 .229 No_date 12:42 16.72 n/a .000
01546# [L/S/n= 143./ / .394/.035]
01547# (Vmax=.345;Dmax=.012)
01548# [Dtn=.55;Dmax=.39]
01549# *****
01550# *****
01551# # STORMS
01552# *****
01553# ** END OF RUN : 104
01554# *****
01555# *****
01556# *****
01557# *****
01558# *****
01559# *****
01560# *****
01561# RUN COMMANDS
01562# *****
01563# START =.00 hrs on 0
01564# [METOUT= 2 (i=imperial, 2=metric output)]
01565# [INTFORM= 1]
01566# [RUN= 1]
01567# *****
01568# *****
01569# # SHWINFO / INPUT DATA FILE
01570# *****
01571# # Project Name : [5923 Ottawa St]
01572# # Project Number: [P2710(001)]
01573# # Date : [2025 FEB 05]
01574# # Modifier : [MW]
01575# # Company : JFSA Canada Inc.
01576# # License # : 2549237
01577# *****
01578# # Model developed to simulate runoff from subcatchments under pre development conditions
01579# *****
01580# R0105/C00002-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01581# READ STORM File=STORM.001
01582# Comment = 5 years RCS Type 2 Storm 24 Hours step 10 min, City of Ottawa
01583# [SDT=10.00;SDUR= 24.00;PTOT= 64.11]
01584# *****
01585# # EXT1
01586# *****
01587# *****
01588# R0105/C00003-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01589# CALIB NASHYD 1.0 01:EXT1 3.21 .095 No_date 12:41 28.73 448 .000
01590# [CN= 80.0; N= 3.00; Tpe = .21]
01591# *****
01592# # EXT2
01593# *****
01594# R0105/C00004-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01595# CALIB NASHYD 1.0 01:EXT2 .59 .021 No_date 12:22 25.29 395 .000
01596# [CN= 85.0; N= 3.00; Tpe = .33]
01597# *****
01598# # EXT3
01599# *****
01600# R0105/C00005-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01601# CALIB NASHYD 1.0 01:EXT3 .56 .030 No_date 12:13 28.73 448 .000
01602# [CN= 80.0; N= 3.00; Tpe = .21]
01603# *****
01604# # EXT4
01605# *****
01606# R0105/C00006-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01607# CALIB NASHYD 1.0 01:EXT4 .31 .017 No_date 12:11 27.82 434 .000
01608# [CN= 79.0; N= 3.00; Tpe = .29]
01609# *****
01610# # EXT5
01611# *****
01612# R0105/C00007-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01613# CALIB NASHYD 1.0 01:EXT5 .59 .021 No_date 12:22 25.29 395 .000
01614# [CN= 76.0; N= 3.00; Tpe = .45]
01615# *****
01616# # EXT6
01617# *****
01618# R0105/C00008-----DtnIn-ID:INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvwm-R.C-----DWfms
01619# CALIB NASHYD 1.0 01:EXT6 .86 .037 No_date 12:29 33.88 529 .000
01620# [CN= 85.0; N= 3.00; Tpe = .34]
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018001 DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018002 CALIB MASHD 1.0 01:EX17 3.21 .121 No_date 12:40 36.46 490 .000
018003 [CN= 80.0; N= 3.00; Tpe =.72]
018004 *****
018005 # EXT2
018006 *****
018007 R0110/C00004-----DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018008 CALIB MASHD 1.0 01:EX172 .28 .022 No_date 12:13 42.40 570 .000
018009 [CN= 85.0; N= 3.00; Tpe =.23]
018010 *****
018011 # EXT3
018012 *****
018013 R0110/C00005-----DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018014 CALIB MASHD 1.0 01:EX173 .24 .038 No_date 12:13 36.46 490 .000
018015 [CN= 80.0; N= 3.00; Tpe =.32]
018016 *****
018017 # EXT4
018018 *****
018019 R0110/C00006-----DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018020 CALIB MASHD 1.0 01:EX174 .31 .022 No_date 12:11 35.39 476 .000
018021 [CN= 80.0; N= 3.00; Tpe =.22]
018022 *****
018023 # EXT5
018024 *****
018025 R0110/C00007-----DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018026 CALIB MASHD 1.0 01:EX175 .59 .028 No_date 12:22 32.39 436 .000
018027 [CN= 76.0; N= 3.00; Tpe =.45]
018028 *****
018029 # EXT6
018030 *****
018031 R0110/C00008-----DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018032 CALIB MASHD 1.0 01:EX176 .86 .046 No_date 12:19 42.40 570 .000
018033 [CN= 76.0; N= 3.00; Tpe =.42]
018034 *****
018035 # EXT7
018036 *****
018037 R0110/C00009-----DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018038 CALIB MASHD 1.0 01:EX177 .47 .035 No_date 12:13 39.90 537 .000
018039 [CN= 83.0; N= 3.00; Tpe =.72]
018040 *****
018041 # EXT8
018042 *****
018043 R0110/C00010-----DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018044 CALIB MASHD 1.0 01:EX178 .83 .045 No_date 12:19 35.39 476 .000
018045 [CN= 78.0; N= 3.00; Tpe =.42]
018046 *****
018047 # EXT9
018048 *****
018049 R0110/C00011-----DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018050 CALIB MASHD 1.0 01:EX179 3.57 .158 No_date 12:24 32.39 436 .000
018051 [CN= 76.0; N= 3.00; Tpe =.48]
018052 *****
018053 # EXT10
018054 *****
018055 R0110/C00012-----DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018056 CALIB MASHD 1.0 01:EX179 .01 .002 No_date 12:10 34.35 462 .000
018057 [CN= 78.0; N= 3.00; Tpe =.04]
018058 *****
018059 # EXT11
018060 *****
018061 R0110/C00013-----DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018062 CALIB MASHD 1.0 01:EX179 .20 .008 No_date 12:20 27.99 377 .000
018063 [CN= 76.0; N= 3.00; Tpe =.42]
018064 *****
018065 # EXT12
018066 *****
018067 R0110/C00014-----DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018068 CALIB MASHD 1.0 01:EX179 .57 .028 No_date 12:22 34.36 462 .000
018069 [CN= 78.0; N= 3.00; Tpe =.46]
018070 *****
018071 # EXT13
018072 *****
018073 R0110/C00015-----DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018074 CALIB MASHD 1.0 01:EX179 .83 .026 No_date 12:16 28.00 377 .000
018075 [CN= 71.0; N= 3.00; Tpe =.44]
018076 *****
018077 # EXT14
018078 *****
018079 R0110/C00016-----DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018080 CALIB MASHD 1.0 01:EX180 .80 .043 No_date 12:11 28.00 377 .000
018081 [CN= 71.0; N= 3.00; Tpe =.29]
018082 *****
018083 # EXT15
018084 *****
018085 R0110/C00017-----DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018086 CALIB MASHD 1.0 01:EX181 .05 .006 No_date 12:07 34.35 462 .000
018087 [CN= 78.0; N= 3.00; Tpe =.21]
018088 *****
018089 R0110/C00018-----DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018090 ADD HYD 1.0 02:EX172 .28 .022 No_date 12:13 42.40 n/a .000
018091 [CN= 78.0; N= 3.00; Tpe =.46]
018092 *****
018093 R0110/C00019-----DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018094 ROUTE CHANNEL -> 1.0 02:EX181 .85 .049 No_date 12:17 37.05 n/a .000
018095 [L/S/fm= 423 / 394 / 035]
018096 *****
018097 R0110/C00020-----DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018098 ADD HYD 1.0 02:EX181 .85 .046 No_date 12:23 37.05 n/a .000
018099 [CN= 78.0; N= 3.00; Tpe =.46]
018100 *****
018101 R0110/C00021-----DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018102 ROUTE CHANNEL -> 1.0 02:EX182 .462 .189 No_date 12:19 36.57 n/a .000
018103 [L/S/fm= 73 / 425 / 035]
018104 *****
018105 R0110/C00022-----DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018106 ADD HYD 1.0 02:EX182 .462 .188 No_date 12:31 36.57 n/a .000
018107 [CN= 78.0; N= 3.00; Tpe =.46]
018108 *****
018109 R0110/C00023-----DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018110 ROUTE CHANNEL -> 1.0 02:EX183 .493 .202 No_date 12:28 36.49 n/a .000
018111 [L/S/fm= 82 / 274 / 035]
018112 *****
018113 R0110/C00024-----DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018114 ADD HYD 1.0 02:EX175 .59 .028 No_date 12:22 32.39 n/a .000
018115 [CN= 78.0; N= 3.00; Tpe =.46]
018116 *****
018117 R0110/C00025-----DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018118 ROUTE CHANNEL -> 1.0 02:EX176 .57 .028 No_date 12:19 28.00 n/a .000
018119 [L/S/fm= 251 / 190 / 035]
018120 *****
018121 R0110/C00026-----DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018122 ADD HYD 1.0 02:EX176 .57 .028 No_date 12:19 28.00 n/a .000
018123 [CN= 78.0; N= 3.00; Tpe =.46]
018124 *****
018125 R0110/C00027-----DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018126 ROUTE CHANNEL -> 1.0 02:EX177 .47 .035 No_date 12:13 39.90 n/a .000
018127 [L/S/fm= 277 / 216 / 035]
018128 *****
018129 R0110/C00028-----DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018130 ROUTE CHANNEL -> 1.0 02:EX178 .68 .277 No_date 12:36 37.12 n/a .000
018131 [L/S/fm= 237 / 644 / 035]
018132 *****
018133 R0110/C00029-----DRAIN-ID:INVDYD-----ARESHA-OPEAKMS-TPeakDate_hh:mm-----Rvum-R-C-----DWfms-
018134 ROUTE CHANNEL -> 1.0 02:EX179 .80 .043 No_date 12:11 28.00 n/a .000
018135 [L/S/fm= 79 / 322 / 035]
018136 *****
018137 R0110/C00030-----DRAIN-ID:INVD
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[illegible]

JFS Ainc.

Attachment B

Post-Development Hydrology

Table B1 - Site 1 - Stage/Storage/Outflow Curves

					Quality Control 1		Overflow			
					Vertical Orifice		Broad Crested Weir			
					Dia (m)	0.085	L (m)	0.300		
					Area (m ²)	0.006				
					Invert (m)	93.86	C _w	1.580		
					C _o	0.61	Invert (m)	94.40		
					Q @ D	0.003	n contr.	2	Total	
Elevation (m)	Storage 1 (m ³)	Storage 2 (m ³)	Total Volume (m ³)	Demarkation Points	Depth (m)	Outflow (m ³ /s)	Depth (m)	Outflow (m ³ /s)	Outflow (m ³ /s)	Storage (ha-m)
93.86		0.0	0.0	Pond Bottom	0.000	0.000	0.000	0.000	0.000	0.000
93.87		0.0	0.0		0.010	0.000	0.000	0.000	0.000	0.000
93.88		0.1	0.1		0.020	0.001	0.000	0.000	0.001	0.000
93.89		0.3	0.3		0.030	0.001	0.000	0.000	0.001	0.000
93.90		0.5	0.5		0.040	0.001	0.000	0.000	0.001	0.000
93.91		0.8	0.8		0.050	0.002	0.000	0.000	0.002	0.000
93.92		1.2	1.2		0.060	0.002	0.000	0.000	0.002	0.000
93.93		1.7	1.7		0.070	0.003	0.000	0.000	0.003	0.000
93.94		2.2	2.2		0.080	0.003	0.000	0.000	0.003	0.000
93.95		2.7	2.7		0.090	0.003	0.000	0.000	0.003	0.000
93.96		3.3	3.3		0.100	0.004	0.000	0.000	0.004	0.000
93.97		4.0	4.0		0.110	0.004	0.000	0.000	0.004	0.000
93.98		4.8	4.8		0.120	0.004	0.000	0.000	0.004	0.000
93.99		5.6	5.6		0.130	0.005	0.000	0.000	0.005	0.001
94.00		6.5	6.5		0.140	0.005	0.000	0.000	0.005	0.001
94.01		7.4	7.4		0.150	0.005	0.000	0.000	0.005	0.001
94.02		8.4	8.4		0.160	0.005	0.000	0.000	0.005	0.001
94.03	0.0	9.5	9.5		0.170	0.005	0.000	0.000	0.005	0.001
94.04	0.0	10.6	10.7		0.180	0.006	0.000	0.000	0.006	0.001
94.05	0.2	11.8	12.0		0.190	0.006	0.000	0.000	0.006	0.001
94.06	0.4	13.1	13.5		0.200	0.006	0.000	0.000	0.006	0.001
94.07	0.8	14.5	15.2		0.210	0.006	0.000	0.000	0.006	0.002
94.08	1.2	15.9	17.1		0.220	0.006	0.000	0.000	0.006	0.002
94.09	1.8	17.4	19.2		0.230	0.007	0.000	0.000	0.007	0.002
94.10	2.5	19.0	21.5		0.240	0.007	0.000	0.000	0.007	0.002
94.11	3.2	20.7	23.9		0.250	0.007	0.000	0.000	0.007	0.002
94.12	4.1	22.4	26.5		0.260	0.007	0.000	0.000	0.007	0.003
94.13	5.1	24.2	29.3		0.270	0.007	0.000	0.000	0.007	0.003
94.14	6.2	26.1	32.2		0.280	0.007	0.000	0.000	0.007	0.003
94.15	7.4	28.0	35.3		0.290	0.008	0.000	0.000	0.008	0.004
94.16	8.7	29.9	38.6		0.300	0.008	0.000	0.000	0.008	0.004
94.17	10.1	31.9	42.0		0.310	0.008	0.000	0.000	0.008	0.004
94.18	10.7	33.8	44.5		0.320	0.008	0.000	0.000	0.008	0.004
94.19	12.3	35.9	48.2		0.330	0.008	0.000	0.000	0.008	0.005
94.20	14.1	37.9	52.0		0.340	0.008	0.000	0.000	0.008	0.005
94.21	16.0	39.9	56.0		0.350	0.009	0.000	0.000	0.009	0.006
94.22	18.1	42.0	60.1		0.360	0.009	0.000	0.000	0.009	0.006
94.23	20.2	44.1	64.3		0.370	0.009	0.000	0.000	0.009	0.006
94.24	22.4	46.3	68.7		0.380	0.009	0.000	0.000	0.009	0.007
94.25	24.6	48.4	73.0		0.390	0.009	0.000	0.000	0.009	0.007
94.26	26.9	50.6	77.5		0.400	0.009	0.000	0.000	0.009	0.008
94.27	29.1	52.9	82.0		0.410	0.009	0.000	0.000	0.009	0.008
94.28	31.4	55.1	86.6		0.420	0.009	0.000	0.000	0.009	0.009
94.29	33.8	57.4	91.2		0.430	0.010	0.000	0.000	0.010	0.009
94.30	36.1	59.7	95.9		0.440	0.010	0.000	0.000	0.010	0.010
94.31	38.5	62.1	100.6		0.450	0.010	0.000	0.000	0.010	0.010
94.32	40.9	64.5	105.4		0.460	0.010	0.000	0.000	0.010	0.011
94.33	43.4	66.9	110.2		0.470	0.010	0.000	0.000	0.010	0.011
94.34	45.9	69.3	115.2		0.480	0.010	0.000	0.000	0.010	0.012
94.35	48.4	71.8	120.1		0.490	0.010	0.000	0.000	0.010	0.012
94.36	50.9	74.3	125.2		0.500	0.010	0.000	0.000	0.010	0.013
94.37	53.4	76.9	130.3		0.510	0.010	0.000	0.000	0.010	0.013
94.38	56.0	79.4	135.5		0.520	0.011	0.000	0.000	0.011	0.014
94.39	58.6	82.1	140.7		0.530	0.011	0.000	0.000	0.011	0.014
94.40	61.3	84.7	146.0	Overflow Weir	0.540	0.011	0.000	0.000	0.011	0.015
94.41	64.0	87.4	151.4		0.550	0.011	0.010	0.000	0.011	0.015
94.42	66.7	90.2	156.8		0.560	0.011	0.020	0.001	0.012	0.016
94.43	69.4	92.9	162.3		0.570	0.011	0.030	0.002	0.014	0.016
94.44	72.1	95.7	167.9	100-Yr WSE	0.580	0.011	0.040	0.004	0.015	0.017
94.45	74.9	98.6	173.5		0.590	0.011	0.050	0.005	0.016	0.017
94.46	77.7	101.5	179.2		0.600	0.011	0.060	0.007	0.018	0.018
94.47	80.6	104.4	185.0		0.610	0.012	0.070	0.008	0.020	0.019
94.48	83.5	107.4	190.9		0.620	0.012	0.080	0.010	0.022	0.019
94.49	86.4	110.4	196.8		0.630	0.012	0.090	0.012	0.024	0.020
94.50	89.3	113.5	202.8	Top of Pond	0.640	0.012	0.100	0.014	0.026	0.020

Table B2 - Site 2 - Stage/Storage/Outflow Curves

					Quality Control 1		Emergency Overflow			
					Vertical Orifice		Broad Crested Weir			
					Dia (m)	0.085	L (m)	0.300		
					Area (m ²)	0.006	C _w Invert (m) n contr.	1.580		
					Invert (m)	93.76		94.35		
					C _o	0.61				
					Q @ D	0.003				
Elevation (m)	Storage 3 (m³)	Storage 4 (m³)	Total Volume (m³)	Demarkation Points	Depth (m)	Outflow (m³/s)	Depth (m)	Outflow (m³/s)	Outflow (m³/s)	Storage (ha-m)
93.76		0.0	0.0	Pond Bottom	0.000	0.000	0.000	0.000	0.000	0.000
93.77		0.1	0.1		0.010	0.000	0.000	0.000	0.000	0.000
93.78		0.2	0.2		0.020	0.001	0.000	0.000	0.001	0.000
93.79		0.4	0.4		0.030	0.001	0.000	0.000	0.001	0.000
93.80		0.6	0.6		0.040	0.001	0.000	0.000	0.001	0.000
93.81		0.9	0.9		0.050	0.002	0.000	0.000	0.002	0.000
93.82		1.3	1.3		0.060	0.002	0.000	0.000	0.002	0.000
93.83		1.8	1.8		0.070	0.003	0.000	0.000	0.003	0.000
93.84		2.4	2.4		0.080	0.003	0.000	0.000	0.003	0.000
93.85		3.0	3.0		0.090	0.003	0.000	0.000	0.003	0.000
93.86		3.7	3.7		0.100	0.004	0.000	0.000	0.004	0.000
93.87		4.5	4.5		0.110	0.004	0.000	0.000	0.004	0.000
93.88		5.2	5.2		0.120	0.004	0.000	0.000	0.004	0.001
93.89		6.0	6.0		0.130	0.005	0.000	0.000	0.005	0.001
93.90		6.8	6.8		0.140	0.005	0.000	0.000	0.005	0.001
93.91		7.6	7.6		0.150	0.005	0.000	0.000	0.005	0.001
93.92		8.4	8.4		0.160	0.005	0.000	0.000	0.005	0.001
93.93		9.3	9.3		0.170	0.005	0.000	0.000	0.005	0.001
93.94		10.1	10.1		0.180	0.006	0.000	0.000	0.006	0.001
93.95		11.0	11.0		0.190	0.006	0.000	0.000	0.006	0.001
93.96		11.9	11.9		0.200	0.006	0.000	0.000	0.006	0.001
93.97		12.8	12.8		0.210	0.006	0.000	0.000	0.006	0.001
93.98		13.7	13.7		0.220	0.006	0.000	0.000	0.006	0.001
93.99		14.6	14.6		0.230	0.007	0.000	0.000	0.007	0.001
94.00		15.6	15.6		0.240	0.007	0.000	0.000	0.007	0.002
94.01		16.6	16.6		0.250	0.007	0.000	0.000	0.007	0.002
94.02		17.6	17.6		0.260	0.007	0.000	0.000	0.007	0.002
94.03		18.6	18.6		0.270	0.007	0.000	0.000	0.007	0.002
94.04	0.0	19.7	19.7		0.280	0.007	0.000	0.000	0.007	0.002
94.05	0.1	20.8	20.9		0.290	0.008	0.000	0.000	0.008	0.002
94.06	0.4	21.8	22.2		0.300	0.008	0.000	0.000	0.008	0.002
94.07	0.8	23.0	23.7		0.310	0.008	0.000	0.000	0.008	0.002
94.08	1.3	24.1	25.4		0.320	0.008	0.000	0.000	0.008	0.003
94.09	1.8	25.3	27.1		0.330	0.008	0.000	0.000	0.008	0.003
94.10	2.5	26.5	29.0		0.340	0.008	0.000	0.000	0.008	0.003
94.11	3.3	27.7	31.0		0.350	0.009	0.000	0.000	0.009	0.003
94.12	4.1	29.0	33.1		0.360	0.009	0.000	0.000	0.009	0.003
94.13	4.5	30.2	34.8		0.370	0.009	0.000	0.000	0.009	0.003
94.14	5.6	31.5	37.2		0.380	0.009	0.000	0.000	0.009	0.004
94.15	6.8	32.9	39.7		0.390	0.009	0.000	0.000	0.009	0.004
94.16	8.1	34.2	42.3	0.400	0.009	0.000	0.000	0.009	0.004	
94.17	8.6	35.6	44.2	0.410	0.009	0.000	0.000	0.009	0.004	
94.18	10.1	37.1	47.1	0.420	0.009	0.000	0.000	0.009	0.005	
94.19	11.7	38.5	50.2	0.430	0.010	0.000	0.000	0.010	0.005	
94.20	13.4	40.0	53.5	0.440	0.010	0.000	0.000	0.010	0.005	
94.21	15.3	41.6	56.9	0.450	0.010	0.000	0.000	0.010	0.006	
94.22	17.2	43.1	60.4	0.460	0.010	0.000	0.000	0.010	0.006	
94.23	19.3	44.7	64.0	0.470	0.010	0.000	0.000	0.010	0.006	
94.24	21.4	46.4	67.8	0.480	0.010	0.000	0.000	0.010	0.007	
94.25	23.5	48.1	71.6	0.490	0.010	0.000	0.000	0.010	0.007	
94.26	25.7	49.8	75.5	0.500	0.010	0.000	0.000	0.010	0.008	
94.27	27.9	51.5	79.4	0.510	0.010	0.000	0.000	0.010	0.008	
94.28	30.1	53.3	83.4	0.520	0.011	0.000	0.000	0.011	0.008	
94.29	32.4	55.1	87.5	0.530	0.011	0.000	0.000	0.011	0.009	
94.30	34.7	57.0	91.7	0.540	0.011	0.000	0.000	0.011	0.009	
94.31	37.0	58.9	95.9	0.550	0.011	0.000	0.000	0.011	0.010	
94.32	39.3	60.9	100.2	0.560	0.011	0.000	0.000	0.011	0.010	
94.33	41.7	62.9	104.6	0.570	0.011	0.000	0.000	0.011	0.010	
94.34	44.1	65.0	109.1	0.580	0.011	0.000	0.000	0.011	0.011	
94.35	46.5	67.1	113.6	Overflow Weir	0.590	0.011	0.000	0.000	0.011	0.011
94.36	49.0	69.2	118.2		0.600	0.011	0.010	0.000	0.012	0.012
94.37	51.5	71.4	122.9		0.610	0.012	0.020	0.001	0.013	0.012
94.38	54.0	73.7	127.7		0.620	0.012	0.030	0.002	0.014	0.013
94.39	56.5	76.0	132.5		0.630	0.012	0.040	0.004	0.015	0.013
94.40	59.1	78.4	137.5		0.640	0.012	0.050	0.005	0.017	0.014
94.41	61.7	80.8	142.5	100-Yr WSE	0.650	0.012	0.060	0.007	0.019	0.014
94.42	64.4	83.3	147.7		0.660	0.012	0.070	0.008	0.020	0.015
94.43	67.0	85.9	152.9		0.670	0.012	0.080	0.010	0.022	0.015
94.44	69.7	88.5	158.2		0.680	0.012	0.090	0.012	0.024	0.016
94.45	72.4	91.2	163.6	Top of Pond	0.690	0.012	0.100	0.014	0.026	0.016

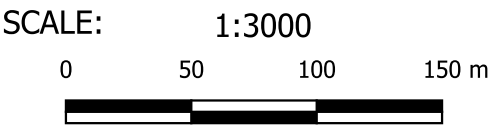


Legend

- Jock River Tributary
- Post-development Subcatchments
- EGIS AutoCAD layer
- Design for Post Subcatchments

Google Hybrid

EXT1 Subcatchment Name
3.212 ha Subcatchment Area (ha)



5923 Ottawa St – Richmond

Figure B1: Proposed Drainage Areas

PROJECT	P2710(e01)
DRAWN	MM
DATE	04-06-2025


```
1 20 Metric units / ID numbers OFF
2 *#*****
3 *# SWMHYMO / INPUT DATA FILE
4 *#*****
5 *# Project Name : [5923 Ottawa St]
6 *# Project Number: [P2710(e01)]
7 *# Date : [2025 April 28]
8 *# Modeller : [MM]
9 *# Company : JFSA Canada Inc.
10 *# License # : 2549237
11 *#*****
12 *# Model developed to simulate runoff from subcatchments under post development
conditions
13 *#*****
14 *% 25 mm Storm based on 2-Year, 3-Hour Chicago Storm
15 START TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[002]
16 ["002YC3H.stm"] <--storm filename, one per line for NSTORM time
17 *%-----|
18 READ STORM STORM_FILENAME=["STORM.001"]
19 *%-----|
20 *#*****
21 *%-----|
22 DEFAULT VALUES ICASEdef=[1], read values only
23 DEFVAL_FILENAME=["Ottawa.val"]
24 *%-----|
25 *#*****
26 *# EXT1
27 *#*****
28 CALIB NASHYD NHYD=["EXT1"], DT[1] (min), AREA=[3.211] (ha),
29 DWF=[0] (cms), CN=[80],
30 IA=[4.67] (mm), N=[3], TP[0.72] (hrs),
31 RAINFALL[ , , -1]
32 *#*****
33 *# EXT2
34 *#*****
35 CALIB NASHYD NHYD=["EXT2"], DT[1] (min), AREA=[0.285] (ha),
36 DWF=[0] (cms), CN=[85],
37 IA=[4.67] (mm), N=[3], TP[0.33] (hrs),
38 RAINFALL[ , , -1]
39 *#*****
40 *# EXT3
41 *#*****
42 CALIB NASHYD NHYD=["EXT3"], DT[1] (min), AREA=[0.560] (ha),
43 DWF=[0] (cms), CN=[80],
44 IA=[4.67] (mm), N=[3], TP[0.32] (hrs),
45 RAINFALL[ , , -1]
46 *#*****
47 *# EXT4
48 *#*****
49 CALIB NASHYD NHYD=["EXT4"], DT[1] (min), AREA=[0.309] (ha),
50 DWF=[0] (cms), CN=[79],
51 IA=[4.67] (mm), N=[3], TP[0.29] (hrs),
52 RAINFALL[ , , -1]
53 *#*****
54 *# EXT5
```

```

55  *#*****
56  CALIB NASHYD      NHYD=["EXT5"], DT[1] (min), AREA=[0.594] (ha),
57                    DWF=[0] (cms), CN=[76],
58                    IA=[4.67] (mm), N=[3], TP[0.45] (hrs),
59                    RAINFALL[ , , -1]
60  *#*****
61  *# EXT6
62  *#*****
63  CALIB NASHYD      NHYD=["EXT6"], DT[1] (min), AREA=[0.864] (ha),
64                    DWF=[0] (cms), CN=[85],
65                    IA=[4.67] (mm), N=[3], TP[0.56] (hrs),
66                    RAINFALL[ , , -1]
67  *#*****
68  *# EXT7
69  *#*****
70  CALIB NASHYD      NHYD=["EXT7"], DT[1] (min), AREA=[0.471] (ha),
71                    DWF=[0] (cms), CN=[83],
72                    IA=[4.67] (mm), N=[3], TP[0.32] (hrs),
73                    RAINFALL[ , , -1]
74  *#*****
75  *# EXT8
76  *#*****
77  CALIB NASHYD      NHYD=["EXT8"], DT[1] (min), AREA=[0.834] (ha),
78                    DWF=[0] (cms), CN=[79],
79                    IA=[4.67] (mm), N=[3], TP[0.42] (hrs),
80                    RAINFALL[ , , -1]
81  *#*****
82  *# EXT9
83  *#*****
84  CALIB NASHYD      NHYD=["EXT9"], DT[1] (min), AREA=[3.571] (ha),
85                    DWF=[0] (cms), CN=[76],
86                    IA=[4.67] (mm), N=[3], TP[0.48] (hrs),
87                    RAINFALL[ , , -1]
88  *#*****
89  *# EXT9a
90  *#*****
91  CALIB NASHYD      NHYD=["EXT9a"], DT[1] (min), AREA=[0.011] (ha),
92                    DWF=[0] (cms), CN=[78],
93                    IA=[4.67] (mm), N=[3], TP[0.04] (hrs),
94                    RAINFALL[ , , -1]
95  *#*****
96  *# EXT10
97  *#*****
98  CALIB NASHYD      NHYD=["EXT10"], DT[1] (min), AREA=[0.203] (ha),
99                    DWF=[0] (cms), CN=[71],
100                   IA=[4.67] (mm), N=[3], TP[0.42] (hrs),
101                   RAINFALL[ , , -1]
102  *#*****
103  *# Pre2_1
104  *#*****
105  CALIB NASHYD      NHYD=["Pre2_1"], DT[1] (min), AREA=[0.013] (ha),
106                    DWF=[0] (cms), CN=[72],
107                    IA=[4.67] (mm), N=[3], TP[0.03] (hrs),
108                    RAINFALL[ , , -1]

```

```

109  *#*****
110  *# Pre2_2
111  *#*****
112  CALIB NASHYD      NHYD=["Pre2_2"], DT[1] (min), AREA=[0.002] (ha),
113                   DWF=[0] (cms), CN=[78],
114                   IA=[4.67] (mm), N=[3], TP[0.02] (hrs),
115                   RAINFALL[ , , -1]
116  *#*****
117  *# Pre9_1
118  *#*****
119  CALIB NASHYD      NHYD=["Pre9_1"], DT[1] (min), AREA=[0.437] (ha),
120                   DWF=[0] (cms), CN=[71],
121                   IA=[4.67] (mm), N=[3], TP[0.38] (hrs),
122                   RAINFALL[ , , -1]
123  *#*****
124  *# Pre9_2
125  *#*****
126  CALIB NASHYD      NHYD=["Pre9_2"], DT[1] (min), AREA=[0.014] (ha),
127                   DWF=[0] (cms), CN=[59],
128                   IA=[4.67] (mm), N=[3], TP[0.03] (hrs),
129                   RAINFALL[ , , -1]
130  *#*****
131  *# Pre10_1
132  *#*****
133  CALIB NASHYD      NHYD=["Pre10_1"], DT[1] (min), AREA=[0.799] (ha),
134                   DWF=[0] (cms), CN=[71],
135                   IA=[4.67] (mm), N=[3], TP[0.29] (hrs),
136                   RAINFALL[ , , -1]
137  *#*****
138  *# Pre11_1
139  *#*****
140  CALIB NASHYD      NHYD=["Pre11_1"], DT[1] (min), AREA=[0.067] (ha),
141                   DWF=[0] (cms), CN=[78],
142                   IA=[4.67] (mm), N=[3], TP[0.21] (hrs),
143                   RAINFALL[ , , -1]
144  *#*****
145  *# Site 1
146  *#*****
147  DESIGN STANDHYD   NHYD=["S1-B1"], DT=[1] (min), AREA=[0.42] (ha),
148                   XIMP=[0.47], TIMP=[0.57], DWF=[0] (cms),
149                   LOSS=[1], SLOPE=[1.0] (%), RAINFALL=[ , , -1] (mm/hr)
150  *# Site 1 - Roof
151  *#*****
152  DESIGN STANDHYD   NHYD=["S1-Roof"], DT=[1] (min), AREA=[0.07] (ha),
153                   XIMP=[0.99], TIMP=[0.99], DWF=[0] (cms),
154                   LOSS=[1], SLOPE=[0.5] (%), RAINFALL=[ , , -1] (mm/hr)
155  *%-----|-----
156  * Rooftop Storage-Outflow Curve for B3 Facility - From EGIS Report
157  ROUTE RESERVOIR   NHYDout=["S1-Roof-Out"], NHYDin=["S1-Roof"], RDT=[1] (min),
158                   TABLE of ( OUTFLOW-STORAGE ) values
159                   (cms) - (ha-m)
160                   [ 0 , 0 ]
161                   [ 0.0008 , 0.0007 ]
162                   [ 0.001 , 0.001 ]
163                   [ 0.0015 , 0.0015 ]

```

```

164         [ 0.0018 , 0.0017 ]
165         [ 0.0023 , 0.0022 ]
166         [ 0.0025 , 0.0024 ]
167         [ 0.0028 , 0.0027 ]
168         [ 0.003 , 0.0029 ]
169         [ 0.0033 , 0.0032 ]
170         [ 0.0038 , 0.0037 ]
171         [ 0.004 , 0.0039 ]
172         [ 0.0045 , 0.0044 ]
173         [ 0.0048 , 0.0046 ]
174         [ 0.0051 , 0.0049 ]
175         [ 0.0056 , 0.0054 ]
176         [ 0.0063 , 0.0061 ]
177         [ 0.0066 , 0.0064 ]
178         [ 0.0076 , 0.0073 ]
179         [ -1 , -1 ]
180         NHYDovf=["S1-Roof-Over"],
181     *%-----|-----
182     ----|-----|
183     ADD HYD          NHYDsum=["SITE1-IN"], NHYDs to add=["S1-B1"+"S1-Roof-Out"+
184     "S1-Roof-Over"]
185     *%-----|-----
186     ----|-----|
187     * Pond for Site 1: Stage-Storage-Outflow
188     ROUTE RESERVOIR    NHYDout=["SITE1-Out"], NHYDin=["SITE1-IN"], RDT=[1] (min),
189     TABLE of ( OUTFLOW-STORAGE ) values
190     (cms) - (ha-m)
191     [ 0 , 0 ]
192     [ 0.00074 , 0.00001 ]
193     [ 0.00149 , 0.00005 ]
194     [ 0.00297 , 0.00022 ]
195     [ 0.00368 , 0.00033 ]
196     [ 0.00479 , 0.00065 ]
197     [ 0.00526 , 0.00084 ]
198     [ 0.00646 , 0.00171 ]
199     [ 0.00747 , 0.00322 ]
200     [ 0.00808 , 0.00445 ]
201     [ 0.00891 , 0.00687 ]
202     [ 0.00917 , 0.00775 ]
203     [ 0.00967 , 0.00959 ]
204     [ 0.00991 , 0.01054 ]
205     [ 0.01037 , 0.01252 ]
206     [ 0.01059 , 0.01355 ]
207     [ 0.01235 , 0.01568 ]
208     [ 0.01493 , 0.01679 ]
209     [ 0.0218 , 0.01909 ]
210     [ 0.02584 , 0.02028 ]
211     [ -1 , -1 ]
212     NHYDovf=["SITE1-Over"],
213     *%-----|-----
214     ----|-----|
215     *#*****
216     *****
217     *# Site 2
218     *#*****
219     *****
220     DESIGN STANDHYD    NHYD=["S2-B3"], DT=[1] (min), AREA=[0.35] (ha),
221     XIMP=[0.46], TIMP=[0.56], DWF=[0] (cms),
222     LOSS=[1], SLOPE=[1.0] (%), RAINFALL=[ , , -1] (mm/hr)
223     *#*****
224     *****
225     *# Site 2 - Roof
226     *#*****
227     *****
228     DESIGN STANDHYD    NHYD=["S2-Roof"], DT=[1] (min), AREA=[0.09] (ha),
229     XIMP=[0.99], TIMP=[0.99], DWF=[0] (cms),
230     LOSS=[1], SLOPE=[0.5] (%), RAINFALL=[ , , -1] (mm/hr)
231     *#*****
232     *****

```



```

*****
225 * Rooftop Storage-Outflow Curve for site 2 Facility - From EGIS Report
226 ROUTE RESERVOIR      NHYDout=["S2-Roof-Out"], NHYDin=["S2-Roof"], RDT=[1] (min),
227                      TABLE of ( OUTFLOW-STORAGE ) values
228                      (cms) - (ha-m)
229                      [ 0 , 0 ]
230                      [ 0.0007 , 0 ]
231                      [ 0.0015 , 0.0001 ]
232                      [ 0.003 , 0.0002 ]
233                      [ 0.0037 , 0.0004 ]
234                      [ 0.0048 , 0.0007 ]
235                      [ 0.0053 , 0.0008 ]
236                      [ 0.0065 , 0.0014 ]
237                      [ 0.0072 , 0.0018 ]
238                      [ 0.0081 , 0.0025 ]
239                      [ 0.0084 , 0.0029 ]
240                      [ 0.0092 , 0.0042 ]
241                      [ 0.0099 , 0.006 ]
242                      [ 0.0104 , 0.0075 ]
243                      [ 0.0106 , 0.0083 ]
244                      [ 0.0112 , 0.0109 ]
245                      [ 0.0143 , 0.0128 ]
246                      [ 0.0174 , 0.0138 ]
247                      [ 0.0253 , 0.0158 ]
248                      [ 0.0276 , 0.0164 ]
249                      [ -1 , -1 ]
250                      NHYDovf=["S2-Roof-Over"],
251 *%-----|-----
252 ADD HYD      NHYDsum=["SITE2-IN"], NHYDs to add=["S2-B3"+"S2-Roof-Out"+
253 "S2-Roof-Over"]
254 *%-----|-----
255 * Pond for Site 2: Stage-Storage-Outflow
256 ROUTE RESERVOIR      NHYDout=["SITE2-Out"], NHYDin=["SITE2-IN"], RDT=[1] (min),
257                      TABLE of ( OUTFLOW-STORAGE )
258                      (cms) - (ha-m)
259                      [ 0 , 0 ]
260                      [ 0.0007 , 0 ]
261                      [ 0.0015 , 0.0001 ]
262                      [ 0.003 , 0.0002 ]
263                      [ 0.0037 , 0.0004 ]
264                      [ 0.0048 , 0.0007 ]
265                      [ 0.0053 , 0.0008 ]
266                      [ 0.0065 , 0.0014 ]
267                      [ 0.0072 , 0.0018 ]
268                      [ 0.0081 , 0.0025 ]
269                      [ 0.0084 , 0.0029 ]
270                      [ 0.0092 , 0.0042 ]
271                      [ 0.0099 , 0.006 ]
272                      [ 0.0104 , 0.0075 ]
273                      [ 0.0106 , 0.0083 ]
274                      [ 0.0112 , 0.0109 ]
275                      [ 0.0141 , 0.0128 ]
276                      [ 0.017 , 0.0138 ]
277                      [ 0.0243 , 0.0158 ]
278                      [ 0.0263 , 0.0164 ]
279                      [ -1 , -1 ]
280                      NHYDovf=["SITE2-Over"],
281 *%-----|-----
282 ADD HYD      NHYDsum=["Site1"], NHYDs to add=["SITE1-Out"+"SITE1-Over"]
283 *%-----|-----
284 ADD HYD      NHYDsum=["Site2"], NHYDs to add=["SITE2-Out"+"SITE2-Over"]
285 *%-----|-----
286 ADD HYD      NHYDsum=["J1"], NHYDs to add=["EXT2"+"Pre2_1"+"Site1"+"Site2"]
287 *%-----|-----
288 * NOTE: Cross-section number 849.0434 is taken from HEC-RAS Model
289 * NOTE: SEGROUGH will be adjusted after completing the HEC-RAS model
290 ROUTE CHANNEL      NHYDout=["R1"], NHYDin=["J1"], RDT=[1] (min),
291                      CHLGTH=[143.151] (m), CHSLOPE=[0.394] (%), FPSLOPE=[0.394] (%),
292                      SECNUM=[849.0434], NSEG=[3],

```

```

292      ( SEGROUGH, SEGDIST (m))=[0.08,18.95 -0.035,26.78 0.08,35.18] NSEG
times
293      ( DISTANCE (m), ELEVATION (m))=[0.48, 94.05]
294      [3.19, 93.99]
295      [6.85, 93.91]
296      [10.48, 93.87]
297      [17.45, 93.85]
298      [18.95, 93.84]
299      [20.36, 93.81]
300      [22.3, 93.76]
301      [22.53, 93.72]
302      [23.98, 93.35]
303      [24.35, 93.33]
304      [24.65, 93.37]
305      [25.04, 93.45]
306      [26.04, 93.74]
307      [26.44, 93.82]
308      [26.78, 93.87]
309      [29.14, 94.11]
310      [33.98, 94.26]
311      [35.18, 94.26]
312  *%-----|-----
313  ADD HYD      NHYDsum=["J2"], NHYDs to add=["R1"+"EXT3"+"EXT1"]
314  *%-----|-----
315  * NOTE: Cross-section number 737.5813 is taken from HEC-RAS Model
316  * NOTE: SEGROUGH will be adjusted after completing the HEC-RAS model
317  ROUTE CHANNEL      NHYDout=["R2"], NHYDin=["J2"], RDT=[1] (min),
318      CHLGTH=[73.338] (m), CHSLOPE=[0.425] (%), FPSLOPE=[0.425] (%),
319      SECNUM=[737.5813], NSEG=[3],
320      ( SEGROUGH, SEGDIST (m))=[0.08,8.4 -0.035,16.42 0.08,22.6] NSEG
times
321      ( DISTANCE (m), ELEVATION (m))=[0, 93.52]
322      [1.08, 93.5]
323      [4.37, 93.48]
324      [6.31, 93.45]
325      [8.4, 93.38]
326      [9.5, 93.31]
327      [10.49, 93.23]
328      [10.99, 93.18]
329      [12.4, 92.94]
330      [13.11, 92.84]
331      [13.67, 92.92]
332      [16.42, 93.6]
333      [16.91, 93.65]
334      [17.97, 93.65]
335      [19, 93.83]
336      [19.51, 93.89]
337      [21.06, 93.94]
338      [22.6, 93.95]
339  *%-----|-----
340  ADD HYD      NHYDsum=["J3"], NHYDs to add=["R2"+"EXT4"]
341  *%-----|-----
342  * NOTE: Cross-section number 675.4097 is taken from HEC-RAS Model
343  * NOTE: SEGROUGH will be adjusted after completing the HEC-RAS model
344  ROUTE CHANNEL      NHYDout=["R3"], NHYDin=["J3"], RDT=[1] (min),
345      CHLGTH=[92.08] (m), CHSLOPE=[0.274] (%), FPSLOPE=[0.274] (%),
346      SECNUM=[675.4097], NSEG=[3],
347      ( SEGROUGH, SEGDIST (m))=[0.08,31.64 -0.035,42.44 0.08,48.87] NSEG
times
348      ( DISTANCE (m), ELEVATION (m))=[30.59, 93.12]
349      [31.64, 93.13]
350      [34.35, 93.08]
351      [35.18, 93.03]
352      [37.78, 92.72]
353      [38.25, 92.64]
354      [38.7, 92.61]
355      [39.74, 92.76]
356      [42.44, 93.41]
357      [42.89, 93.49]

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358                                     [43.97, 93.57]
359                                     [44.92, 93.6]
360                                     [46.07, 93.67]
361                                     [48.87, 93.74]
362 *%-----|-----
363 ADD HYD          NHYDsum=["J4"], NHYDs to add=["R3"+"EXT5"]
364 *%-----|-----
365 * NOTE: Cross-section number 518.7506 is taken from HEC-RAS Model
366 * NOTE: SEGROUGH will be adjusted after completing the HEC-RAS model
367 ROUTE CHANNEL    NHYDout=["R4"], NHYDin=["J4"], RDT=[1] (min),
368                  CHLGTH=[251.495] (m), CHSLOPE=[0.19] (%), FPSLOPE=[0.19] (%),
369                  SECNUM=[518.7506], NSEG=[3],
370                  ( SEGROUGH, SEGDIST (m))=[0.08,51.48 -0.035,59.39 0.08,66.4] NSEG
371                  times
372                  ( DISTANCE (m), ELEVATION (m))=[0, 92.92]
373                                     [4.26, 92.9]
374                                     [48.31, 92.76]
375                                     [51.48, 92.76]
376                                     [53.64, 92.7]
377                                     [55.33, 92.29]
378                                     [55.44, 92.29]
379                                     [56.43, 92.37]
380                                     [56.97, 92.43]
381                                     [59.39, 93.27]
382                                     [59.74, 93.37]
383                                     [60.8, 93.52]
384                                     [63.31, 93.71]
385                                     [66.4, 93.76]
386 *%-----|-----
387 ADD HYD          NHYDsum=["J5"], NHYDs to add=["R4"+"EXT6"+"EXT7"]
388 *%-----|-----
389 * NOTE: Cross-section number 275.0857 is taken from HEC-RAS Model
390 * NOTE: SEGROUGH will be adjusted after completing the HEC-RAS model
391 ROUTE CHANNEL    NHYDout=["R5"], NHYDin=["J5"], RDT=[1] (min),
392                  CHLGTH=[237.343] (m), CHSLOPE=[0.644] (%), FPSLOPE=[0.644] (%),
393                  SECNUM=[275.0857], NSEG=[3],
394                  ( SEGROUGH, SEGDIST (m))=[0.08,40.82 -0.035,53.64 0.08,57.93] NSEG
395                  times
396                  ( DISTANCE (m), ELEVATION (m))=[36.16, 92.63]
397                                     [40.82, 92.97]
398                                     [41.39, 92.9]
399                                     [44.69, 91.72]
400                                     [45.24, 91.58]
401                                     [46.33, 91.43]
402                                     [47.41, 91.64]
403                                     [47.87, 91.75]
404                                     [49.59, 92.2]
405                                     [50.99, 92.36]
406                                     [51.44, 92.48]
407                                     [53.18, 92.98]
408                                     [53.64, 93.15]
409                                     [55.92, 93.66]
410                                     [57.93, 93.68]
411 *%-----|-----
412 ADD HYD          NHYDsum=["Pre"], NHYDs to add=["Pre10_1"+"Pre9_2"+"Pre2_2"]
413 *%-----|-----
414 * NOTE: Cross-section number 124 is taken from HEC-RAS Model
415 * NOTE: SEGROUGH will be adjusted after completing the HEC-RAS model
416 ROUTE CHANNEL    NHYDout=["R6"], NHYDin=["Pre"], RDT=[1] (min),
417                  CHLGTH=[77.414] (m), CHSLOPE=[0.776] (%), FPSLOPE=[0.776] (%),
418                  SECNUM=[124], NSEG=[3],
419                  ( SEGROUGH, SEGDIST (m))=[0.08,8.34 -0.035,31.31 0.08,84.97] NSEG
420                  times
421                  ( DISTANCE (m), ELEVATION (m))=[1.78, 93.73]
422                                     [4.51, 93.54]
423                                     [5.06, 93.31]
424                                     [7.25, 92.98]
425                                     [7.79, 92.77]
426                                     [8.34, 92.49]

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424                                     [9.43, 91.93]
425                                     [9.68, 91.81]
426                                     [10.53, 91.27]
427                                     [12.64, 90.92]
428                                     [14.44, 90.9]
429                                     [16.54, 91.06]
430                                     [17.64, 91.06]
431                                     [30.22, 92.3]
432                                     [31.31, 92.45]
433                                     [33.5, 92.41]
434                                     [55.37, 93.11]
435                                     [57.01, 93.2]
436                                     [84.97, 93.43]
437 *%-----|-----
438 * NOTE: Cross-section number 74 is taken from HEC-RAS Model
439 * NOTE: SEGROUGH will be adjusted after completing the HEC-RAS model
440 ROUTE CHANNEL      NHYDout=["R7"], NHYDin=["Pre9_1"], RDT=[1] (min),
441                   CHLGTH=[159.151] (m), CHSLOPE=[1.576] (%), FPSLOPE=[1.576] (%),
442                   SECNUM=[74], NSEG=[3],
443                   ( SEGROUGH, SEGDIST (m))=[0.08,4.67 -0.035,81.24 0.08,82.88] NSEG
444                   times
445                   ( DISTANCE (m), ELEVATION (m))=[1.94, 93.64]
446                                     [4.67, 93.32]
447                                     [5.77, 93.15]
448                                     [7.41, 92.69]
449                                     [7.95, 92.37]
450                                     [9.36, 91.71]
451                                     [10.12, 91.22]
452                                     [10.49, 91.06]
453                                     [12.64, 90.89]
454                                     [16.16, 90.92]
455                                     [18.83, 91.66]
456                                     [19.59, 92.02]
457                                     [21.62, 92.39]
458                                     [24.87, 92.48]
459                                     [30.37, 92.55]
460                                     [34.37, 92.65]
461                                     [77.41, 92.82]
462                                     [80.6, 93.25]
463                                     [81.24, 93.48]
464                                     [82.88, 93.79]
465 *%-----|-----
466 ADD HYD            NHYDsum=["J6"], NHYDs to add=["R6"+"EXT10"]
467 *%-----|-----
468 * NOTE: Cross-section number 49 is taken from HEC-RAS Model
469 * NOTE: SEGROUGH will be adjusted after completing the HEC-RAS model
470 ROUTE CHANNEL      NHYDout=["R8"], NHYDin=["J6"], RDT=[1] (min),
471                   CHLGTH=[78.801] (m), CHSLOPE=[0.522] (%), FPSLOPE=[0.522] (%),
472                   SECNUM=[49], NSEG=[3],
473                   ( SEGROUGH, SEGDIST (m))=[0.08,8.71 -0.035,20.59 0.08,116.73] NSEG
474                   times
475                   ( DISTANCE (m), ELEVATION (m))=[0, 93.36]
476                                     [1.93, 93.63]
477                                     [4.61, 93.26]
478                                     [6.23, 93.1]
479                                     [8.19, 92.26]
480                                     [8.71, 91.84]
481                                     [9.86, 91.47]
482                                     [10.53, 91.04]
483                                     [13.84, 91]
484                                     [14.5, 91.11]
485                                     [16.97, 91.27]
486                                     [20.59, 91.76]
487                                     [23.3, 91.64]
488                                     [30.34, 91.85]
489                                     [35.29, 91.92]
490                                     [116.73, 92.96]
491 *%-----|-----
492 ADD HYD            NHYDsum=["J7"], NHYDs to add=["R8"+"R7"]

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491 *%-----|-----
492 * NOTE: Cross-section number 7 is taken from HEC-RAS Model
493 * NOTE: SEGROUGH will be adjusted after completing the HEC-RAS model
494 ROUTE CHANNEL      NHYDout=["R9"], NHYDin=["J7"], RDT=[1] (min),
495                   CHLGTH=[29.445] (m), CHSLOPE=[0.887] (%), FPSLOPE=[0.887] (%),
496                   SECNUM=[7], NSEG=[3],
497                   ( SEGROUGH, SEGDIST (m))=[0.08,1.5 -0.035,22.44 0.08,100.08] NSEG
498                   times
499                   ( DISTANCE (m), ELEVATION (m))=[0, 93.4]
500                                     [1.5, 93.63]
501                                     [3.13, 93.62]
502                                     [4.76, 93.28]
503                                     [5.3, 93.25]
504                                     [6.52, 93.08]
505                                     [6.96, 92.95]
506                                     [10.57, 90.95]
507                                     [13.59, 90.67]
508                                     [15.83, 90.72]
509                                     [16.42, 90.85]
510                                     [18.66, 91.76]
511                                     [20.82, 91.86]
512                                     [22.44, 91.92]
513                                     [27.84, 91.98]
514                                     [30.15, 91.96]
515                                     [100.08, 92.61]
516 *%-----|-----
517 ADD HYD            NHYDsum=["J8"], NHYDs to add=["EXT9"+"R9"+"EXT8"+"R5"]
518 *%-----|-----
519 * Note: The pipe needs to be adjusted based on the Culvert-under-railway information
520 ROUTE PIPE        PTYPE=[1]circ, NHYDout=["Outlet"], RNUMBER=[1.0],
521                   PDIAM=[525] (mm), PLNGTH=[8.407] (m), PROUGH=[0.013],
522                   PSLOPE=[0.0001] (m/m),
523                   NHYDin=["J8"], RDT=[1] (min)
524 *%-----|-----
525 #####
526 *# STORMS
527 #####
528 *% 2-Year, 3-Hour Chicago Storm
529 *START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[002]
530 *                  ["002YC3H.stm"] <--storm filename, one per line for NSTORM time
531 *%-----|-----
532 *% 5-Year, 3-Hour Chicago Storm
533 *START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[005]
534 *                  ["005YC3H.stm"] <--storm filename, one per line for NSTORM time
535 *%-----|-----
536 *% 10-Year, 3-Hour Chicago Storm
537 *START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[010]
538 *                  ["010YC3H.stm"] <--storm filename, one per line for NSTORM time
539 *%-----|-----
540 *% 25-Year, 3-Hour Chicago Storm
541 *START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[025]
542 *                  ["025YC3H.stm"] <--storm filename, one per line for NSTORM time
543 *%-----|-----
544 *% 50-Year, 3-Hour Chicago Storm
545 *START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[050]
546 *                  ["050YC3H.stm"] <--storm filename, one per line for NSTORM time
547 *%-----|-----
548 *% 100-Year, 3-Hour Chicago Storm
549 *START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[099]
550 *                  ["100YC3H.stm"] <--storm filename, one per line for NSTORM time
551 *%-----|-----
552 *% 2-Year, 24-Hour SCS Storm
553 *START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[102]
554 *                  ["SC24002x.stm"] <--storm filename, one per line for NSTORM time
555 *%-----|-----
556 *% 5-Year, 24-Hour SCS Storm
557 *START            TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[105]
558 *                  ["SC24005x.stm"] <--storm filename, one per line for NSTORM time
559 *%-----|-----

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558  *% 10-Year, 24-Hour SCS Storm
559  START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[110]
560                ["SC24010x.stm"] <--storm filename, one per line for NSTORM time
561  *%-----|-----
562  *% 25-Year, 24-Hour SCS Storm
563  START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[125]
564                ["SC24025x.stm"] <--storm filename, one per line for NSTORM time
565  *%-----|-----
566  *% 50-Year, 24-Hour SCS Storm
567  START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[150]
568                ["SC24050x.stm"] <--storm filename, one per line for NSTORM time
569  *%-----|-----
570  *% 100-Year, 24-Hour SCS Storm
571  START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[199]
572                ["SC24100x.stm"] <--storm filename, one per line for NSTORM time
573  *%-----|-----
574  *% 100-Year, 24-Hour SCS Storm + 20%
575  *START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[998]
576  *%              ["SC24100x+.stm"] <--storm filename, one per line for NSTORM time
577  *%-----|-----
578  *% 100-Year, 3-Hour Chicago Storm + 20%
579  *START          TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[999]
580  *              ["100YRCHI3HR+.stm"] <--storm filename, one per line for NSTORM time
581  *%-----|-----
582  FINISH

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00361# ADD HYD + 1.0 02:188 1.02 .015 No_date 4:41 5.83 n/a .000
00362# SUM= 3.57 .045 No_date 1:37 6.88 n/a .000
00363# 1.0 01:077 1.46 .018 No_date 1:31 5.84 n/a .000
00364# R0002.C00048 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00365# ROUTE CHANNEL -> 1.0 02:127 1.46 .018 No_date 1:31 5.84 n/a .000
00366# [RD7=1.00] out<= 1.0 01:189 1.46 .018 No_date 1:32 5.84 n/a .000
00367# [L/S/n= 29./, .887/.035]
00368# (Vmax=.543;Dmax=.012)
00369# R0002.C00050 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00370# ADD HYD + 1.0 02:189 1.46 .018 No_date 1:32 5.89 n/a .000
00371# SUM= 1.0 02:189 1.46 .018 No_date 1:32 5.89 n/a .000
00372# 1.0 01:287 8.9 .012 No_date 1:33 7.01 n/a .000
00373# + 1.0 02:185 7.24 .089 No_date 2:04 9.89 n/a .000
00374# SUM= 1.0 01:128 13.10 .151 No_date 1:52 8.49 n/a .000
00375# R0002.C00051 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00376# ROUTE PIPE -> 1.0 02:128 13.10 .151 No_date 1:52 8.49 n/a .000
00377# [RD7=1.00] out<= 1.0 01:128 13.10 .151 No_date 1:52 8.49 n/a .000
00378# [L/S/n= 8./, .010/.013]
00379# (Vmax=.310;Dmax=.691)
00380# [DtnIn=.53;Dmax=.94]
00381# #####
00382# # STORMS
00383# #####
00384# ** END OF RUN : 4
00385#
00386#
00387#
00388#
00389#
00390#
00391#
00392# RUN:COMMAND#
00393# R0005.C00001 -----
00394# START
00395# [TZERO = .00 hrs on 0]
00396# [METOUT= 2 (i=imperial, 2=metric output)]
00397# [NTHORN= 1]
00398# [NRUN = 0005]
00399#
00400# # SWEHYD / INPUT DATA FILE
00401# #
00402# # Project Name : [5923 201707 42.51]
00403# # Project Number: [P2701(e01)]
00404# # Date : [2025 April 28]
00405# # Modifier : [DW]
00406# # Company : JFSA Canada Inc.
00407# # License # : 2549227
00408# #
00409# # Model developed to simulate runoff from subcatchments under pre development conditions
00410# # THE FOLLOWING PARAMETERS ARE USED IN THE DESIGN STANDARD CCM
00411# R0005.C00002 -----
00412# HEAD STORM
00413# Filename = STORM.001
00414# Comment = CHICAGO STORM 5 Year, 3 Hours
00415# [EPIFALL= STORM 3.001707 42.51]
00416# #####
00417# R0005.C00003 -----
00418# DEFAULT VALUES
00419# Filename = C:\Temp\20250428-PostDev\Ottawa.val
00420# [CHSEV = 1 (read and print data)]
00421# FileTitle= File comment : [Parameters for City of Ottawa Projects]
00422#
00423# Horton's infiltration equation parameters:
00424# [Por=.72;mm/hr] [Por13.20 mm/hr] [DCAVE 4.14 /hr] [r=.00 mm]
00425# Parameters for PERVIOUS surfaces in STANDARD:
00426# [Iamp= 4.67 mm] [I2P=40.00 mm] [DWP=.250]
00427# Paramaters for IMPVIOUS out in STANDARD:
00428# [Iamp= 1.57 mm] [CILI=1.50] [DINI=.013]
00429# Parameters used in NASHD01:
00430# [I= 4.67 mm] [N= 3.00]
00431# Average monthly Pan Evaporation data in (mm)
00432# JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
00433# .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
00434# Average monthly Potential Evapotranspiration in (mm)
00435# JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
00436# .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
00437# #####
00438# # EXT1
00439# R0005.C00004 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00440# CALIB NASHD 1.0 01:EXT1 3.21 .066 No_date 1:55 14.13 .332 .000
00441# [CN= 76.0; N= 3.00; Tpe=.42]
00442# # EXT2
00443# R0005.C00005 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00444# CALIB NASHD 1.0 01:EXT2 .28 .012 No_date 1:23 17.32 .407 .000
00445# [CN= 85.0; N= 3.00; Tpe=.33]
00446# # EXT3
00447# R0005.C00006 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00448# CALIB NASHD 1.0 01:EXT3 .31 .011 No_date 1:21 13.59 .320 .000
00449# [CN= 76.0; N= 3.00; Tpe=.42]
00450# # EXT4
00451# R0005.C00007 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00452# CALIB NASHD 1.0 01:EXT4 .31 .011 No_date 1:21 13.59 .320 .000
00453# [CN= 76.0; N= 3.00; Tpe=.42]
00454# # EXT5
00455# R0005.C00008 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00456# CALIB NASHD 1.0 01:EXT5 .01 .001 No_date 1:00 10.48 .246 .000
00457# [CN= 76.0; N= 3.00; Tpe=.45]
00458# # EXT6
00459# R0005.C00009 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00460# CALIB NASHD 1.0 01:EXT6 .86 .026 No_date 1:42 17.32 .407 .000
00461# [CN= 76.0; N= 3.00; Tpe=.42]
00462# # EXT7
00463# R0005.C00010 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00464# CALIB NASHD 1.0 01:EXT7 .83 .024 No_date 1:31 13.59 .320 .000
00465# [CN= 76.0; N= 3.00; Tpe=.42]
00466# # EXT8
00467# R0005.C00011 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00468# CALIB NASHD 1.0 01:EXT8 .01 .001 No_date 1:00 10.48 .246 .000
00469# [CN= 76.0; N= 3.00; Tpe=.45]
00470# # EXT9
00471# R0005.C00012 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00472# CALIB NASHD 1.0 01:EXT9 3.57 .083 No_date 1:36 12.13 .285 .000
00473# [CN= 76.0; N= 3.00; Tpe=.48]
00474# # EXT10
00475# R0005.C00013 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00476# CALIB NASHD 1.0 01:EXT10 .20 .004 No_date 1:32 10.11 .238 .000
00477# [CN= 76.0; N= 3.00; Tpe=.42]
00478# # EXT11
00479# R0005.C00014 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00480# CALIB NASHD 1.0 01:EXT11 .80 .021 No_date 1:21 10.11 .238 .000
00481# [CN= 76.0; N= 3.00; Tpe=.42]
00482# # EXT12
00483# R0005.C00015 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00484# CALIB NASHD 1.0 01:EXT12 .00 .000 No_date 1:00 13.06 .307 .000
00485# [CN= 76.0; N= 3.00; Tpe=.02]
00486# # EXT13
00487# R0005.C00016 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00488# CALIB NASHD 1.0 01:EXT13 .07 .003 No_date 1:14 13.07 .308 .000
00489# [CN= 76.0; N= 3.00; Tpe=.21]
00490# # Site 1
00491# #####
00492# # STORMS
00493# #####
00494# ** END OF RUN : 9
00495#
00496#
00497#
00498#
00499#
00500#
00501#
00502# RUN:COMMAND#
00503# R0010.R0010.C00001 -----
00504# START
00505# [TZERO = .00 hrs on 0]
00506# [METOUT= 2 (i=imperial, 2=metric output)]
00507# [NTHORN= 1]
00508# [NRUN = 0010]
00509#
00510# # SWEHYD / INPUT DATA FILE
00511# #
00512# # Project Name : [5923 201707 42.51]
00513# # Project Number: [P2701(e01)]
00514# # Date : [2025 April 28]
00515# # Modifier : [DW]
00516# # Company : JFSA Canada Inc.
00517# # License # : 2549227
00518# #
00519# # Model developed to simulate runoff from subcatchments under pre development conditions
00520# # THE FOLLOWING PARAMETERS ARE USED IN THE DESIGN STANDARD CCM
00521# R0010.R0010.C00002 -----
00522# HEAD STORM
00523# Filename = STORM.001
00524# Comment = CHICAGO STORM 5 Year, 3 Hours
00525# [EPIFALL= STORM 3.001707 42.51]
00526# #####
00527# R0010.R0010.C00003 -----
00528# DEFAULT VALUES
00529# Filename = C:\Temp\20250428-PostDev\Ottawa.val
00530# [CHSEV = 1 (read and print data)]
00531# FileTitle= File comment : [Parameters for City of Ottawa Projects]
00532#
00533# Horton's infiltration equation parameters:
00534# [Por=.72;mm/hr] [Por13.20 mm/hr] [DCAVE 4.14 /hr] [r=.00 mm]
00535# Parameters for PERVIOUS surfaces in STANDARD:
00536# [Iamp= 4.67 mm] [I2P=40.00 mm] [DWP=.250]
00537# Paramaters for IMPVIOUS out in STANDARD:
00538# [Iamp= 1.57 mm] [CILI=1.50] [DINI=.013]
00539# Parameters used in NASHD01:
00540# [I= 4.67 mm] [N= 3.00]
00541# Average monthly Pan Evaporation data in (mm)
00542# JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
00543# .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
00544# Average monthly Potential Evapotranspiration in (mm)
00545# JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
00546# .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
00547# #####
00548# # EXT1
00549# R0010.R0010.C00004 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00550# CALIB NASHD 1.0 01:EXT1 3.21 .066 No_date 1:55 14.13 .332 .000
00551# [CN= 76.0; N= 3.00; Tpe=.42]
00552# # EXT2
00553# R0010.R0010.C00005 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00554# CALIB NASHD 1.0 01:EXT2 .28 .012 No_date 1:23 17.32 .407 .000
00555# [CN= 85.0; N= 3.00; Tpe=.33]
00556# # EXT3
00557# R0010.R0010.C00006 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00558# CALIB NASHD 1.0 01:EXT3 .31 .011 No_date 1:21 13.59 .320 .000
00559# [CN= 76.0; N= 3.00; Tpe=.42]
00560# # EXT4
00561# R0010.R0010.C00007 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00562# CALIB NASHD 1.0 01:EXT4 .31 .011 No_date 1:21 13.59 .320 .000
00563# [CN= 76.0; N= 3.00; Tpe=.42]
00564# # EXT5
00565# R0010.R0010.C00008 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00566# CALIB NASHD 1.0 01:EXT5 .01 .001 No_date 1:00 10.48 .246 .000
00567# [CN= 76.0; N= 3.00; Tpe=.45]
00568# # EXT6
00569# R0010.R0010.C00009 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00570# CALIB NASHD 1.0 01:EXT6 .86 .026 No_date 1:42 17.32 .407 .000
00571# [CN= 76.0; N= 3.00; Tpe=.42]
00572# # EXT7
00573# R0010.R0010.C00010 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00574# CALIB NASHD 1.0 01:EXT7 .83 .024 No_date 1:31 13.59 .320 .000
00575# [CN= 76.0; N= 3.00; Tpe=.42]
00576# # EXT8
00577# R0010.R0010.C00011 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00578# CALIB NASHD 1.0 01:EXT8 .01 .001 No_date 1:00 10.48 .246 .000
00579# [CN= 76.0; N= 3.00; Tpe=.45]
00580# # EXT9
00581# R0010.R0010.C00012 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00582# CALIB NASHD 1.0 01:EXT9 3.57 .083 No_date 1:36 12.13 .285 .000
00583# [CN= 76.0; N= 3.00; Tpe=.48]
00584# # EXT10
00585# R0010.R0010.C00013 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00586# CALIB NASHD 1.0 01:EXT10 .20 .004 No_date 1:32 10.11 .238 .000
00587# [CN= 76.0; N= 3.00; Tpe=.42]
00588# # EXT11
00589# R0010.R0010.C00014 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00590# CALIB NASHD 1.0 01:EXT11 .80 .021 No_date 1:21 10.11 .238 .000
00591# [CN= 76.0; N= 3.00; Tpe=.42]
00592# # EXT12
00593# R0010.R0010.C00015 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00594# CALIB NASHD 1.0 01:EXT12 .00 .000 No_date 1:00 13.06 .307 .000
00595# [CN= 76.0; N= 3.00; Tpe=.02]
00596# # EXT13
00597# R0010.R0010.C00016 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00598# CALIB NASHD 1.0 01:EXT13 .07 .003 No_date 1:14 13.07 .308 .000
00599# [CN= 76.0; N= 3.00; Tpe=.21]
00600# # Site 1
00601# #####
00602# # STORMS
00603# #####
00604# ** END OF RUN : 9
00605#
00606#
00607#
00608#
00609#
00610#
00611#
00612# RUN:COMMAND#
00613# R0015.R0015.C00001 -----
00614# START
00615# [TZERO = .00 hrs on 0]
00616# [METOUT= 2 (i=imperial, 2=metric output)]
00617# [NTHORN= 1]
00618# [NRUN = 0010]
00619#
00620# # SWEHYD / INPUT DATA FILE
00621# #
00622# # Project Name : [5923 201707 42.51]
00623# # Project Number: [P2701(e01)]
00624# # Date : [2025 April 28]
00625# # Modifier : [DW]
00626# # Company : JFSA Canada Inc.
00627# # License # : 2549227
00628# #
00629# # Model developed to simulate runoff from subcatchments under pre development conditions
00630# # THE FOLLOWING PARAMETERS ARE USED IN THE DESIGN STANDARD CCM
00631# R0015.R0015.C00002 -----
00632# HEAD STORM
00633# Filename = STORM.001
00634# Comment = CHICAGO STORM 5 Year, 3 Hours
00635# [EPIFALL= STORM 3.001707 42.51]
00636# #####
00637# R0015.R0015.C00003 -----
00638# DEFAULT VALUES
00639# Filename = C:\Temp\20250428-PostDev\Ottawa.val
00640# [CHSEV = 1 (read and print data)]
00641# FileTitle= File comment : [Parameters for City of Ottawa Projects]
00642#
00643# Horton's infiltration equation parameters:
00644# [Por=.72;mm/hr] [Por13.20 mm/hr] [DCAVE 4.14 /hr] [r=.00 mm]
00645# Parameters for PERVIOUS surfaces in STANDARD:
00646# [Iamp= 4.67 mm] [I2P=40.00 mm] [DWP=.250]
00647# Paramaters for IMPVIOUS out in STANDARD:
00648# [Iamp= 1.57 mm] [CILI=1.50] [DINI=.013]
00649# Parameters used in NASHD01:
00650# [I= 4.67 mm] [N= 3.00]
00651# Average monthly Pan Evaporation data in (mm)
00652# JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
00653# .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
00654# Average monthly Potential Evapotranspiration in (mm)
00655# JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
00656# .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
00657# #####
00658# # EXT1
00659# R0015.R0015.C00004 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00660# CALIB NASHD 1.0 01:EXT1 3.21 .066 No_date 1:55 14.13 .332 .000
00661# [CN= 76.0; N= 3.00; Tpe=.42]
00662# # EXT2
00663# R0015.R0015.C00005 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00664# CALIB NASHD 1.0 01:EXT2 .28 .012 No_date 1:23 17.32 .407 .000
00665# [CN= 85.0; N= 3.00; Tpe=.33]
00666# # EXT3
00667# R0015.R0015.C00006 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00668# CALIB NASHD 1.0 01:EXT3 .31 .011 No_date 1:21 13.59 .320 .000
00669# [CN= 76.0; N= 3.00; Tpe=.42]
00670# # EXT4
00671# R0015.R0015.C00007 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00672# CALIB NASHD 1.0 01:EXT4 .31 .011 No_date 1:21 13.59 .320 .000
00673# [CN= 76.0; N= 3.00; Tpe=.42]
00674# # EXT5
00675# R0015.R0015.C00008 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00676# CALIB NASHD 1.0 01:EXT5 .01 .001 No_date 1:00 10.48 .246 .000
00677# [CN= 76.0; N= 3.00; Tpe=.45]
00678# # EXT6
00679# R0015.R0015.C00009 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00680# CALIB NASHD 1.0 01:EXT6 .86 .026 No_date 1:42 17.32 .407 .000
00681# [CN= 76.0; N= 3.00; Tpe=.42]
00682# # EXT7
00683# R0015.R0015.C00010 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00684# CALIB NASHD 1.0 01:EXT7 .83 .024 No_date 1:31 13.59 .320 .000
00685# [CN= 76.0; N= 3.00; Tpe=.42]
00686# # EXT8
00687# R0015.R0015.C00011 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00688# CALIB NASHD 1.0 01:EXT8 .01 .001 No_date 1:00 10.48 .246 .000
00689# [CN= 76.0; N= 3.00; Tpe=.45]
00690# # EXT9
00691# R0015.R0015.C00012 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00692# CALIB NASHD 1.0 01:EXT9 3.57 .083 No_date 1:36 12.13 .285 .000
00693# [CN= 76.0; N= 3.00; Tpe=.48]
00694# # EXT10
00695# R0015.R0015.C00013 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00696# CALIB NASHD 1.0 01:EXT10 .20 .004 No_date 1:32 10.11 .238 .000
00697# [CN= 76.0; N= 3.00; Tpe=.42]
00698# # EXT11
00699# R0015.R0015.C00014 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00700# CALIB NASHD 1.0 01:EXT11 .80 .021 No_date 1:21 10.11 .238 .000
00701# [CN= 76.0; N= 3.00; Tpe=.42]
00702# # EXT12
00703# R0015.R0015.C00015 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00704# CALIB NASHD 1.0 01:EXT12 .00 .000 No_date 1:00 13.06 .307 .000
00705# [CN= 76.0; N= 3.00; Tpe=.02]
00706# # EXT13
00707# R0015.R0015.C00016 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00708# CALIB NASHD 1.0 01:EXT13 .07 .003 No_date 1:14 13.07 .308 .000
00709# [CN= 76.0; N= 3.00; Tpe=.21]
00710# # Site 1
00711# #####
00712# # STORMS
00713# #####
00714# ** END OF RUN : 9
00715#
00716#
00717#
00718#
00719#
00720#
00721#
00722# RUN:COMMAND#
00723# R0020.R0020.C00001 -----
00724# START
00725# [TZERO = .00 hrs on 0]
00726# [METOUT= 2 (i=imperial, 2=metric output)]
00727# [NTHORN= 1]
00728# [NRUN = 0010]
00729#
00730# # SWEHYD / INPUT DATA FILE
00731# #
00732# # Project Name : [5923 201707 42.51]
00733# # Project Number: [P2701(e01)]
00734# # Date : [2025 April 28]
00735# # Modifier : [DW]
00736# # Company : JFSA Canada Inc.
00737# # License # : 2549227
00738# #
00739# # Model developed to simulate runoff from subcatchments under pre development conditions
00740# # THE FOLLOWING PARAMETERS ARE USED IN THE DESIGN STANDARD CCM
00741# R0020.R0020.C00002 -----
00742# HEAD STORM
00743# Filename = STORM.001
00744# Comment = CHICAGO STORM 5 Year, 3 Hours
00745# [EPIFALL= STORM 3.001707 42.51]
00746# #####
00747# R0020.R0020.C00003 -----
00748# DEFAULT VALUES
00749# Filename = C:\Temp\20250428-PostDev\Ottawa.val
00750# [CHSEV = 1 (read and print data)]
00751# FileTitle= File comment : [Parameters for City of Ottawa Projects]
00752#
00753# Horton's infiltration equation parameters:
00754# [Por=.72;mm/hr] [Por13.20 mm/hr] [DCAVE 4.14 /hr] [r=.00 mm]
00755# Parameters for PERVIOUS surfaces in STANDARD:
00756# [Iamp= 4.67 mm] [I2P=40.00 mm] [DWP=.250]
00757# Paramaters for IMPVIOUS out in STANDARD:
00758# [Iamp= 1.57 mm] [CILI=1.50] [DINI=.013]
00759# Parameters used in NASHD01:
00760# [I= 4.67 mm] [N= 3.00]
00761# Average monthly Pan Evaporation data in (mm)
00762# JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
00763# .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
00764# Average monthly Potential Evapotranspiration in (mm)
00765# JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
00766# .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
00767# #####
00768# # EXT1
00769# R0020.R0020.C00004 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00770# CALIB NASHD 1.0 01:EXT1 3.21 .066 No_date 1:55 14.13 .332 .000
00771# [CN= 76.0; N= 3.00; Tpe=.42]
00772# # EXT2
00773# R0020.R0020.C00005 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00774# CALIB NASHD 1.0 01:EXT2 .28 .012 No_date 1:23 17.32 .407 .000
00775# [CN= 85.0; N= 3.00; Tpe=.33]
00776# # EXT3
00777# R0020.R0020.C00006 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00778# CALIB NASHD 1.0 01:EXT3 .31 .011 No_date 1:21 13.59 .320 .000
00779# [CN= 76.0; N= 3.00; Tpe=.42]
00780# # EXT4
00781# R0020.R0020.C00007 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00782# CALIB NASHD 1.0 01:EXT4 .31 .011 No_date 1:21 13.59 .320 .000
00783# [CN= 76.0; N= 3.00; Tpe=.42]
00784# # EXT5
00785# R0020.R0020.C00008 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00786# CALIB NASHD 1.0 01:EXT5 .01 .001 No_date 1:00 10.48 .246 .000
00787# [CN= 76.0; N= 3.00; Tpe=.45]
00788# # EXT6
00789# R0020.R0020.C00009 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00790# CALIB NASHD 1.0 01:EXT6 .86 .026 No_date 1:42 17.32 .407 .000
00791# [CN= 76.0; N= 3.00; Tpe=.42]
00792# # EXT7
00793# R0020.R0020.C00010 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00794# CALIB NASHD 1.0 01:EXT7 .83 .024 No_date 1:31 13.59 .320 .000
00795# [CN= 76.0; N= 3.00; Tpe=.42]
00796# # EXT8
00797# R0020.R0020.C00011 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00798# CALIB NASHD 1.0 01:EXT8 .01 .001 No_date 1:00 10.48 .246 .000
00799# [CN= 76.0; N= 3.00; Tpe=.45]
00800# # EXT9
00801# R0020.R0020.C00012 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00802# CALIB NASHD 1.0 01:EXT9 3.57 .083 No_date 1:36 12.13 .285 .000
00803# [CN= 76.0; N= 3.00; Tpe=.48]
00804# # EXT10
00805# R0020.R0020.C00013 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00806# CALIB NASHD 1.0 01:EXT10 .20 .004 No_date 1:32 10.11 .238 .000
00807# [CN= 76.0; N= 3.00; Tpe=.42]
00808# # EXT11
00809# R0020.R0020.C00014 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00810# CALIB NASHD 1.0 01:EXT11 .80 .021 No_date 1:21 10.11 .238 .000
00811# [CN= 76.0; N= 3.00; Tpe=.42]
00812# # EXT12
00813# R0020.R0020.C00015 -----DtnIn-ID:INHYD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvnm-R.C-----DWfcms
00814# CALIB NASHD 1.0 01:EXT12 .00 .000 No_date 1:00 13.06 .307 .000
00815# [CN= 76.0
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01081) *****
01082) # EXT1
01083)
01084) ROUTE2:C00004-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01085) CALIB NASHVD 1.0 01:EXT1 3.657 .118 No_date 1.12 24.30 .421 .000
01086) [CN= 80.0: N= 3.00: Tpe =.72]
01087) *****
01088) # EXT2
01089)
01090) ROUTE2:C00005-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01091) CALIB NASHVD 1.0 01:EXT2 .28 .022 No_date 1.12 29.15 .301 .000
01092) [CN= 80.0: N= 3.00: Tpe =.32]
01093) *****
01094) # EXT3
01095)
01096) ROUTE2:C00006-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01097) CALIB NASHVD 1.0 01:EXT3 .56 .036 No_date 1.12 24.50 .421 .000
01098) [CN= 80.0: N= 3.00: Tpe =.32]
01099) *****
01100) # EXT4
01101)
01102) ROUTE2:C00007-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01103) CALIB NASHVD 1.0 01:EXT4 .31 .020 No_date 1.12 23.69 .407 .000
01104) [CN= 79.0: N= 3.00: Tpe =.29]
01105) *****
01106) # EXT5
01107)
01108) ROUTE2:C00008-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01109) CALIB NASHVD 1.0 01:EXT5 .59 .026 No_date 1.13 21.44 .368 .000
01110) [CN= 76.0: N= 3.00: Tpe =.32]
01111) *****
01112) # EXT6
01113)
01114) ROUTE2:C00009-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01115) CALIB NASHVD 1.0 01:EXT6 .046 No_date 1.13 29.15 .301 .000
01116) [CN= 85.0: N= 3.00: Tpe =.56]
01117) *****
01118) # EXT7
01119)
01120) ROUTE2:C00010-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01121) CALIB NASHVD 1.0 01:EXT7 .47 .034 No_date 1.12 27.17 .467 .000
01122) [CN= 80.0: N= 3.00: Tpe =.42]
01123) *****
01124) # EXT8
01125)
01126) ROUTE2:C00011-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01127) CALIB NASHVD 1.0 01:EXT8 .83 .043 No_date 1.13 23.69 .407 .000
01128) [CN= 79.0: N= 3.00: Tpe =.42]
01129) *****
01130) # EXT9
01131)
01132) ROUTE2:C00012-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01133) CALIB NASHVD 1.0 01:EXT9 3.57 .151 No_date 1.13 21.44 .368 .000
01134) [CN= 76.0: N= 3.00: Tpe =.48]
01135) *****
01136) # EXT9a
01137)
01138) ROUTE2:C00013-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01139) CALIB NASHVD 1.0 01:EXT9a .01 .002 No_date 1.00 22.90 .393 .000
01140) [CN= 76.0: N= 3.00: Tpe =.48]
01141) *****
01142) # EXT10
01143)
01144) ROUTE2:C00014-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01145) CALIB NASHVD 1.0 01:EXT10 .20 .008 No_date 1.13 18.23 .313 .000
01146) [CN= 71.0: N= 3.00: Tpe =.42]
01147) *****
01148) # Pre2_1
01149)
01150) ROUTE2:C00015-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01151) * CALIB NASHVD 1.0 01:Pre2_1 .01 .002 No_date 1.00 18.23 .323 .000
01152) [CN= 76.0: N= 3.00: Tpe =.42]
01153) *****
01154) # Pre2_2
01155)
01156) ROUTE2:C00016-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01157) CALIB NASHVD 1.0 01:Pre2_2 .00 .000 No_date 1.00 22.87 .393 .000
01158) [CN= 78.0: N= 3.00: Tpe =.02]
01159) *****
01160) # Pre3_1
01161)
01162) ROUTE2:C00017-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01163) CALIB NASHVD 1.0 01:Pre3_1 .44 .018 No_date 1.12 18.23 .313 .000
01164) [CN= 71.0: N= 3.00: Tpe =.38]
01165) *****
01166) # Pre3_2
01167)
01168) ROUTE2:C00018-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01169) * CALIB NASHVD 1.0 01:Pre3_2 .01 .001 No_date 1.00 12.46 .214 .000
01170) [CN= 59.0: N= 3.00: Tpe =.03]
01171) *****
01172) # Pre3_3
01173)
01174) ROUTE2:C00019-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01175) CALIB NASHVD 1.0 01:Pre3_3 .20 .040 No_date 1.13 18.23 .313 .000
01176) [CN= 71.0: N= 3.00: Tpe =.29]
01177) *****
01178) # Pre3_4
01179)
01180) ROUTE2:C00020-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01181) CALIB NASHVD 1.0 01:Pre3_4 .07 .005 No_date 1.13 22.90 .393 .000
01182) [CN= 76.0: N= 3.00: Tpe =.03]
01183) *****
01184) # Site 1
01185)
01186) ROUTE2:C00021-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01187) DESION STANDYD 1.0 01:Site1-81 .42 .109 No_date 1.00 39.40 .677 .000
01188) [XMP= 47:TIMP= 57]
01189) [SLP= 50:DTU= 1.00]
01190) [LOGS= 1 : HORTONS]
01191) # Site 1 - Roof
01192)
01193) ROUTE2:C00022-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01194) DESION STANDYD 1.0 01:Site1-Roof .07 .028 No_date 1.00 56.28 .967 .000
01195) [XMP= 99:TIMP= 99]
01196) [SLP= 50:DTU= 1.00]
01197) [LOGS= 1 : HORTONS]
01198) ROUTE2:C00023-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01199) ROUTE RESERVOIR -> 1.0 01:Site1-Roof .07 .028 No_date 1.00 56.28 n/a .000
01200) out <= 1.0 01:Site1-Roof-Ov .09 .008 No_date 1.11 56.28 n/a .000
01201) overflow <= 1.0 01:Site1-Roof-Ov .00 .000 No_date 0.00 .00 n/a .000
01202) [MktDevVol= 2398E-02 m3, TotDevVol= .0000E+00 m3, N-Ov= 0, TotDurOv= 0 hrs]
01203) ROUTE2:C00024-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01204) ADD HYD + 1.0 01:Site1-81 .42 .109 No_date 1.00 39.40 n/a .000
01205) + 1.0 01:Site1-Roof-Ov .09 .008 No_date 1.11 56.28 n/a .000
01206) + 1.0 01:Site1-Roof-Ov .00 .000 No_date 0.00 .00 n/a .000
01207) SUM= 1.0 01:Site1-Roof-Ov .49 .111 No_date 1.00 41.81 n/a .000
01208) ROUTE2:C00025-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01209) ROUTE RESERVOIR -> 1.0 01:Site1-IN .49 .111 No_date 1.00 41.81 n/a .000
01210) out <= 1.0 01:Site1-IN .49 .111 No_date 1.00 41.81 n/a .000
01211) overflow <= 1.0 01:Site1-Over .00 .000 No_date 0.00 .00 n/a .000
01212) [MktDevVol= 1118E-01 m3, TotDevVol= .0000E+00 m3, N-Ov= 0, TotDurOv= 0 hrs]
01213) *****
01214) # Site 2
01215)
01216) ROUTE2:C00026-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01217) DESION STANDYD 1.0 01:Site2-83 .35 .090 No_date 1.00 39.04 .670 .000
01218) [XMP= 46:TIMP= 56]
01219) [SLP= 50:DTU= 1.00]
01220) [LOGS= 1 : HORTONS]
01221) # Site 2 - Roof
01222)
01223) ROUTE2:C00027-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01224) DESION STANDYD 1.0 01:Site2-Roof .09 .036 No_date 1.00 56.27 .966 .000
01225) [XMP= 99:TIMP= 99]
01226) [LOGS= 1 : HORTONS]
01227) *****
01228) # Site 2 - Roof
01229)
01230) ROUTE2:C00028-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01231) ROUTE RESERVOIR -> 1.0 01:Site2-Roof .09 .036 No_date 1.00 56.27 n/a .000
01232) out <= 1.0 01:Site2-Roof-Ov .09 .008 No_date 1.11 56.28 n/a .000
01233) overflow <= 1.0 01:Site2-Roof-Ov .00 .000 No_date 0.00 .00 n/a .000
01234) [MktDevVol= 2398E-02 m3, TotDevVol= .0000E+00 m3, N-Ov= 0, TotDurOv= 0 hrs]
01235) ROUTE2:C00029-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01236) ADD HYD + 1.0 01:Site2-83 .35 .090 No_date 1.00 39.04 n/a .000
01237) + 1.0 01:Site2-Roof-Ov .09 .008 No_date 1.11 56.28 n/a .000
01238) + 1.0 01:Site2-Roof-Ov .00 .000 No_date 0.00 .00 n/a .000
01239) SUM= 1.0 01:Site2-IN .49 .098 No_date 1.00 42.57 n/a .000
01240) ROUTE2:C00030-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01241) ROUTE RESERVOIR -> 1.0 01:Site2-IN .49 .098 No_date 1.00 42.57 n/a .000
01242) out <= 1.0 01:Site2-IN .49 .098 No_date 1.00 42.57 n/a .000
01243) overflow <= 1.0 01:Site2-Over .00 .000 No_date 0.00 .00 n/a .000
01244) [MktDevVol= 1118E-01 m3, TotDevVol= .0000E+00 m3, N-Ov= 0, TotDurOv= 0 hrs]
01245) ROUTE2:C00031-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01246) ADD HYD + 1.0 01:Site1-Over .49 .010 No_date 1.42 41.81 n/a .000
01247) + 1.0 01:Site1-Over .00 .000 No_date 0.00 .00 n/a .000
01248) SUM= 1.0 01:Site1 .49 .010 No_date 1.42 41.81 n/a .000
01249) ROUTE2:C00032-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01250) ADD HYD + 1.0 01:Site2-Over .00 .000 No_date 0.00 .00 n/a .000
01251) + 1.0 01:Site2-Over .49 .012 No_date 1.49 42.57 n/a .000
01252) SUM= 1.0 01:Site2-Over .49 .012 No_date 1.49 42.57 n/a .000
01253) ROUTE2:C00033-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01254) ADD HYD + 1.0 01:EXT2 .28 .022 No_date 1.12 29.15 n/a .000
01255) + 1.0 01:EXT2-Pre1 .01 .002 No_date 1.00 18.42 n/a .000
01256) + 1.0 01:Site1 .49 .010 No_date 1.42 41.81 n/a .000
01257) + 1.0 01:Site2 .44 .012 No_date 1.49 42.57 n/a .000
01258) SUM= 1.0 01:21 1.23 .043 No_date 1.12 38.90 n/a .000
01259) ROUTE2:C00034-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01260) ROUTE CHANNEL -> 1.0 01:21 1.23 .043 No_date 1.12 38.90 n/a .000
01261) [RD= 1.00] out<- 1.0 01:R1 1.23 .042 No_date 1.12 38.90 n/a .000
01262) [L/S/n= 142./, .394/.035]
01263) (Vmax= .331:Dmax= .134)
01264) ROUTE2:C00035-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01265) ADD HYD + 1.0 01:EXT3 .56 .036 No_date 1.12 24.50 n/a .000
01266) + 1.0 01:EXT3 .31 .020 No_date 1.13 21.44 n/a .000
01267) SUM= 1.0 01:EXT3 5.00 .177 No_date 1.14 28.04 n/a .000
01268) ROUTE2:C00036-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01269) ROUTE CHANNEL -> 1.0 01:22 5.00 .178 No_date 1.14 28.04 n/a .000
01270) [RD= 1.00] out<- 1.0 01:R2 5.00 .177 No_date 1.14 28.04 n/a .000
01271) [L/S/n= 92./, .274/.035]
01272) (Vmax= .391:Dmax= .253)
01273)
01274) ROUTE2:C00037-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01275) ADD HYD + 1.0 01:EXT4 .59 .026 No_date 1.13 21.44 n/a .000
01276) + 1.0 01:EXT4 .31 .020 No_date 1.12 23.69 n/a .000
01277) SUM= 1.0 01:EXT4 5.31 .189 No_date 1.41 27.79 n/a .000
01278) ROUTE2:C00038-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01279) ROUTE CHANNEL -> 1.0 01:23 5.31 .189 No_date 1.41 27.79 n/a .000
01280) [RD= 1.00] out<- 1.0 01:R3 5.31 .189 No_date 1.41 27.79 n/a .000
01281) [L/S/n= 92./, .274/.035]
01282) (Vmax= .391:Dmax= .253)
01283) ROUTE2:C00039-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01284) ADD HYD + 1.0 01:EXT5 5.31 .189 No_date 1.44 27.79 n/a .000
01285) + 1.0 01:EXT5 .59 .026 No_date 1.13 21.44 n/a .000
01286) SUM= 1.0 01:EXT5 5.90 .214 No_date 1.42 27.15 n/a .000
01287) ROUTE2:C00040-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01288) ROUTE CHANNEL -> 1.0 01:24 5.90 .214 No_date 1.42 27.15 n/a .000
01289) [RD= 1.00] out<- 1.0 01:R4 5.90 .203 No_date 1.53 27.15 n/a .000
01290) [L/S/n= 251./, .190/.035]
01291) (Vmax= .383:Dmax= .283)
01292) ROUTE2:C00041-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01293) ADD HYD + 1.0 01:EXT4 5.90 .203 No_date 1.53 27.15 n/a .000
01294) + 1.0 01:EXT6 .86 .046 No_date 1.40 29.15 n/a .000
01295) SUM= 1.0 01:EXT4 6.76 .249 No_date 1.53 27.15 n/a .000
01296) ROUTE2:C00042-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01297) ROUTE CHANNEL -> 1.0 01:25 7.24 .266 No_date 1.47 27.39 n/a .000
01298) [L/S/n= 251./, .190/.035]
01299) [RD= 1.00] out<- 1.0 01:R5 7.24 .262 No_date 1.53 27.39 n/a .000
01300) (Vmax= .622:Dmax= .266)
01301) ROUTE2:C00043-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01302) ADD HYD + 1.0 01:Pre2_1 .80 .040 No_date 1.20 18.23 n/a .000
01303) + 1.0 01:Pre2_2 .01 .001 No_date 1.00 12.46 n/a .000
01304) + 1.0 01:Pre2_2 .00 .000 No_date 1.00 22.87 n/a .000
01305) SUM= 1.0 01:Pre2 8.1 .040 No_date 1.20 18.15 n/a .000
01306) ROUTE2:C00044-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01307) ROUTE CHANNEL -> 1.0 01:Pre 8.1 .039 No_date 1.23 18.15 n/a .000
01308) [RD= 1.00] out<- 1.0 01:R6 8.1 .039 No_date 1.23 18.15 n/a .000
01309) [L/S/n= 271./, .176/.035]
01310) (Vmax= .492:Dmax= .029)
01311) ROUTE2:C00045-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01312) ROUTE CHANNEL -> 1.0 01:Pre2_1 .44 .018 No_date 1.12 18.23 n/a .000
01313) [RD= 1.00] out<- 1.0 01:R7 4.44 .018 No_date 1.13 18.23 n/a .000
01314) [L/S/n= 159./, .176/.035]
01315) (Vmax= .797:Dmax= .005)
01316) ROUTE2:C00046-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01317) ADD HYD + 1.0 01:EXT6 .81 .043 No_date 1.42 27.15 n/a .000
01318) + 1.0 01:EXT10 .20 .008 No_date 1.31 18.23 n/a .000
01319) SUM= 1.0 01:EXT6 1.02 .047 No_date 1.42 27.15 n/a .000
01320) ROUTE2:C00047-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01321) ROUTE CHANNEL -> 1.0 01:26 1.02 .047 No_date 1.27 18.41 n/a .000
01322) [L/S/n= 79./, .532/.035]
01323) (Vmax= .423:Dmax= .034)
01324) ROUTE2:C00048-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01325) ADD HYD + 1.0 01:EXT7 .44 .031 No_date 1.48 18.66 n/a .000
01326) + 1.0 01:EXT7 .44 .031 No_date 1.28 18.61 n/a .000
01327) SUM= 1.0 01:EXT7 1.02 .047 No_date 1.28 18.61 n/a .000
01328) ROUTE2:C00049-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01329) ROUTE CHANNEL -> 1.0 01:27 1.46 .064 No_date 1.28 18.61 n/a .000
01330) [RD= 1.00] out<- 1.0 01:R8 1.46 .064 No_date 1.29 18.61 n/a .000
01331) [L/S/n= 29./, .887/.035]
01332) (Vmax= .543:Dmax= .043)
01333) ROUTE2:C00050-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01334) ADD HYD + 1.0 01:EXT7 3.57 .151 No_date 1.35 21.44 n/a .000
01335) + 1.0 01:EXT8 .83 .043 No_date 1.30 23.69 n/a .000
01336) + 1.0 01:EXT8 .83 .043 No_date 1.30 23.69 n/a .000
01337) SUM= 1.0 01:EXT8 13.10 .128 No_date 1.44 24.57 n/a .000
01338) ROUTE2:C00051-----DtnIn-ID:INVD-----AREAh-QFEARcms-TpeakDate_hh:mm-----Rvm-R.C-----DWfms
01339) ROUTE CHANNEL -> 1.0 01:28 13.10 .489 No_date 1.44 24.57 n/a .000
01340) [RD= 1.00] out<- 1.0 01:Outlet 13.10 .489 No_date 1.44 24.57 n/a .000
01341) [L/S/n= 8./, .010/.035]
01342) (Vmax= .416:Dmax= 1.072)
01343) [RD= 1.00] out<- 1.0 01:Outlet 13.10 .489 No_date 1.44 24.57 n/a .000
01344) [L/S/n= 8./, .010/.035]
01345) [Div= .53:Dmax= 1.31]
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01710) *****
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01718) *****
01719) *****
01720) *****
01721) *****
01722) *****
01723) *****
01724) *****
01725) *****

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01443# R0505C00010-----DtnIn-ID:INVD-----AREHA-AFEARCS-TpaeDate_hh:mm-----Rwm-R-C-----Dwfms
01444# CALIB NASHD 1.0 01:EXT7 47 .041 No_date 1:27 32.24 4.98 .000
01445# [CNM 83.0; Nm 3.00; Tpm .32]
01446# *****
01447# # EXT8
01448# CALIB NASHD 1.0 01:EXT8 .83 .052 No_date 1:30 28.33 4.97 .000
01449# [CNM 79.0; Nm 3.00; Tpm .42]
01450# *****
01451# # EXT9
01452# CALIB NASHD 1.0 01:EXT9 3.57 .183 No_date 1:35 25.77 3.98 .000
01453# [CNM 81.0; Nm 3.00; Tpm .48]
01454# *****
01455# # EXT10
01456# CALIB NASHD 1.0 01:EXT10 .20 .010 No_date 1:30 22.06 3.40 .000
01457# [CNM 78.0; Nm 3.00; Tpm .04]
01458# *****
01459# # EXT11
01460# CALIB NASHD 1.0 01:EXT11 .07 .004 No_date 1:33 27.44 4.23 .000
01461# [CNM 78.0; Nm 3.00; Tpm .02]
01462# *****
01463# # EXT12
01464# CALIB NASHD 1.0 01:EXT12 .00 .000 No_date 1:00 27.40 4.23 .000
01465# [CNM 78.0; Nm 3.00; Tpm .02]
01466# *****
01467# # EXT13
01468# CALIB NASHD 1.0 01:EXT13 .01 .002 No_date 1:00 22.75 3.93 .000
01469# [CNM 72.0; Nm 3.00; Tpm .03]
01470# *****
01471# # EXT14
01472# CALIB NASHD 1.0 01:EXT14 .00 .000 No_date 1:00 27.40 4.23 .000
01473# [CNM 78.0; Nm 3.00; Tpm .02]
01474# *****
01475# # EXT15
01476# CALIB NASHD 1.0 01:EXT15 .01 .002 No_date 1:00 22.75 3.93 .000
01477# [CNM 72.0; Nm 3.00; Tpm .03]
01478# *****
01479# # EXT16
01480# CALIB NASHD 1.0 01:EXT16 .00 .000 No_date 1:00 27.40 4.23 .000
01481# [CNM 78.0; Nm 3.00; Tpm .02]
01482# *****
01483# # EXT17
01484# CALIB NASHD 1.0 01:EXT17 .01 .002 No_date 1:00 22.75 3.93 .000
01485# [CNM 72.0; Nm 3.00; Tpm .03]
01486# *****
01487# # EXT18
01488# CALIB NASHD 1.0 01:EXT18 .00 .000 No_date 1:00 27.40 4.23 .000
01489# [CNM 78.0; Nm 3.00; Tpm .02]
01490# *****
01491# # EXT19
01492# CALIB NASHD 1.0 01:EXT19 .01 .002 No_date 1:00 22.75 3.93 .000
01493# [CNM 72.0; Nm 3.00; Tpm .03]
01494# *****
01495# # EXT20
01496# CALIB NASHD 1.0 01:EXT20 .00 .000 No_date 1:00 27.40 4.23 .000
01497# [CNM 78.0; Nm 3.00; Tpm .02]
01498# *****
01499# # EXT21
01500# CALIB NASHD 1.0 01:EXT21 .01 .002 No_date 1:00 22.75 3.93 .000
01501# [CNM 72.0; Nm 3.00; Tpm .03]
01502# *****
01503# # EXT22
01504# CALIB NASHD 1.0 01:EXT22 .00 .000 No_date 1:00 27.40 4.23 .000
01505# [CNM 78.0; Nm 3.00; Tpm .02]
01506# *****
01507# # EXT23
01508# CALIB NASHD 1.0 01:EXT23 .01 .002 No_date 1:00 22.75 3.93 .000
01509# [CNM 72.0; Nm 3.00; Tpm .03]
01510# *****
01511# # EXT24
01512# CALIB NASHD 1.0 01:EXT24 .00 .000 No_date 1:00 27.40 4.23 .000
01513# [CNM 78.0; Nm 3.00; Tpm .02]
01514# *****
01515# # EXT25
01516# CALIB NASHD 1.0 01:EXT25 .01 .002 No_date 1:00 22.75 3.93 .000
01517# [CNM 72.0; Nm 3.00; Tpm .03]
01518# *****
01519# # EXT26
01520# CALIB NASHD 1.0 01:EXT26 .00 .000 No_date 1:00 27.40 4.23 .000
01521# [CNM 78.0; Nm 3.00; Tpm .02]
01522# *****
01523# # EXT27
01524# CALIB NASHD 1.0 01:EXT27 .01 .002 No_date 1:00 22.75 3.93 .000
01525# [CNM 72.0; Nm 3.00; Tpm .03]
01526# *****
01527# # EXT28
01528# CALIB NASHD 1.0 01:EXT28 .00 .000 No_date 1:00 27.40 4.23 .000
01529# [CNM 78.0; Nm 3.00; Tpm .02]
01530# *****
01531# # EXT29
01532# CALIB NASHD 1.0 01:EXT29 .01 .002 No_date 1:00 22.75 3.93 .000
01533# [CNM 72.0; Nm 3.00; Tpm .03]
01534# *****
01535# # EXT30
01536# CALIB NASHD 1.0 01:EXT30 .00 .000 No_date 1:00 27.40 4.23 .000
01537# [CNM 78.0; Nm 3.00; Tpm .02]
01538# *****
01539# # EXT31
01540# CALIB NASHD 1.0 01:EXT31 .01 .002 No_date 1:00 22.75 3.93 .000
01541# [CNM 72.0; Nm 3.00; Tpm .03]
01542# *****
01543# # EXT32
01544# CALIB NASHD 1.0 01:EXT32 .00 .000 No_date 1:00 27.40 4.23 .000
01545# [CNM 78.0; Nm 3.00; Tpm .02]
01546# *****
01547# # EXT33
01548# CALIB NASHD 1.0 01:EXT33 .01 .002 No_date 1:00 22.75 3.93 .000
01549# [CNM 72.0; Nm 3.00; Tpm .03]
01550# *****
01551# # EXT34
01552# CALIB NASHD 1.0 01:EXT34 .00 .000 No_date 1:00 27.40 4.23 .000
01553# [CNM 78.0; Nm 3.00; Tpm .02]
01554# *****
01555# # EXT35
01556# CALIB NASHD 1.0 01:EXT35 .01 .002 No_date 1:00 22.75 3.93 .000
01557# [CNM 72.0; Nm 3.00; Tpm .03]
01558# *****
01559# # EXT36
01560# CALIB NASHD 1.0 01:EXT36 .00 .000 No_date 1:00 27.40 4.23 .000
01561# [CNM 78.0; Nm 3.00; Tpm .02]
01562# *****
01563# # EXT37
01564# CALIB NASHD 1.0 01:EXT37 .01 .002 No_date 1:00 22.75 3.93 .000
01565# [CNM 72.0; Nm 3.00; Tpm .03]
01566# *****
01567# # EXT38
01568# CALIB NASHD 1.0 01:EXT38 .00 .000 No_date 1:00 27.40 4.23 .000
01569# [CNM 78.0; Nm 3.00; Tpm .02]
01570# *****
01571# # EXT39
01572# CALIB NASHD 1.0 01:EXT39 .01 .002 No_date 1:00 22.75 3.93 .000
01573# [CNM 72.0; Nm 3.00; Tpm .03]
01574# *****
01575# # EXT40
01576# CALIB NASHD 1.0 01:EXT40 .00 .000 No_date 1:00 27.40 4.23 .000
01577# [CNM 78.0; Nm 3.00; Tpm .02]
01578# *****
01579# # EXT41
01580# CALIB NASHD 1.0 01:EXT41 .01 .002 No_date 1:00 22.75 3.93 .000
01581# [CNM 72.0; Nm 3.00; Tpm .03]
01582# *****
01583# # EXT42
01584# CALIB NASHD 1.0 01:EXT42 .00 .000 No_date 1:00 27.40 4.23 .000
01585# [CNM 78.0; Nm 3.00; Tpm .02]
01586# *****
01587# # EXT43
01588# CALIB NASHD 1.0 01:EXT43 .01 .002 No_date 1:00 22.75 3.93 .000
01589# [CNM 72.0; Nm 3.00; Tpm .03]
01590# *****
01591# # EXT44
01592# CALIB NASHD 1.0 01:EXT44 .00 .000 No_date 1:00 27.40 4.23 .000
01593# [CNM 78.0; Nm 3.00; Tpm .02]
01594# *****
01595# # EXT45
01596# CALIB NASHD 1.0 01:EXT45 .01 .002 No_date 1:00 22.75 3.93 .000
01597# [CNM 72.0; Nm 3.00; Tpm .03]
01598# *****
01599# # EXT46
01600# CALIB NASHD 1.0 01:EXT46 .00 .000 No_date 1:00 27.40 4.23 .000
01601# [CNM 78.0; Nm 3.00; Tpm .02]
01602# *****
01603# # EXT47
01604# CALIB NASHD 1.0 01:EXT47 .01 .002 No_date 1:00 22.75 3.93
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01801# * CALIB NASHVD 1.0 01:Pre2 0.00 .001 No_date 1:00 32.36 .451 .000
01802# [CN= 76.0; N= 3.00; Tpe= .38]
01803# *****
01804# # Pre2_1
01805# *****
01806# R0099:CO0001-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01807# CALIB NASHVD 1.0 01:Pre2 0.00 .027 No_date 1:27 26.29 .367 .000
01808# [CN= 71.0; N= 3.00; Tpe= .38]
01809# *****
01810# # Pre2_2
01811# *****
01812# R0099:CO0001-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01813# * CALIB NASHVD 1.0 01:Pre2 0.01 .002 No_date 1:00 18.43 .257 .000
01814# [CN= 79.0; N= 3.00; Tpe= .03]
01815# *****
01816# # Pre1_1
01817# *****
01818# R0099:CO0019-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01819# CALIB NASHVD 1.0 01:Pre1_1 0.80 .058 No_date 1:20 26.29 .367 .000
01820# [CN= 71.0; N= 3.00; Tpe= .38]
01821# *****
01822# # Pre1_2
01823# *****
01824# R0099:CO0020-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01825# CALIB NASHVD 1.0 01:Pre1 0.07 .008 No_date 1:23 27.37 .452 .000
01826# [CN= 78.0; N= 3.00; Tpe= .21]
01827# *****
01828# # Site 1
01829# *****
01830# R0099:CO0021-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01831# DESIGN STANDYD 1.0 01:81-B1 .42 .146 No_date 1:00 51.46 .718 .000
01832# [XIMP= 47.71MP; .57]
01833# [SLP= 1.00DT; 1.00]
01834# *****
01835# # Site 1 - Roof
01836# *****
01837# R0099:CO0021-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01838# DESIGN STANDYD 1.0 01:81-Roof 0.07 .035 No_date 1:00 69.68 .972 .000
01839# [XIMP= 99.91MP; .99]
01840# [SLP= 50.0DT; 1.00]
01841# *****
01842# R0099:CO0021-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01843# ROUTE RESERVOIR -> 1.0 01:81-Roof 0.07 .035 No_date 1:00 69.68 n/a .000
01844# out <= 1.0 01:81-Roof-0u 0.07 .003 No_date 1:30 69.68 n/a .000
01845# overflow <= 1.0 01:81-Roof-0u 0.00 .000 No_date 0:00 .00 n/a .000
01846# [MettoUsed=.3296E-02 n3, TotovVol=.0000E+00 n3, N-Ovfr= 0, TotDurOvr= 0 hrs]
01847# R0099:CO0021-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01848# ADD HYD 1.0 01:81-Roof .42 .146 No_date 1:00 51.46 n/a .000
01849# + 1.0 01:81-Roof-0u 0.07 .003 No_date 1:30 69.68 n/a .000
01850# + 1.0 01:81-Roof-0u 0.00 .000 No_date 0:00 .00 n/a .000
01851# SUM= 1.0 01:SITE1-IN .49 .148 No_date 1:00 54.06 n/a .000
01852# R0099:CO0025-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01853# ROUTE RESERVOIR -> 1.0 01:SITE1-IN .49 .148 No_date 1:00 54.06 n/a .000
01854# out <= 1.0 01:SITE1-out .49 .014 No_date 1:41 54.06 n/a .000
01855# overflow <= 1.0 01:SITE1-out 0.00 .000 No_date 0:00 .00 n/a .000
01856# [MettoUsed=.1634E-01 n3, TotovVol=.0000E+00 n3, N-Ovfr= 0, TotDurOvr= 0 hrs]
01857# *****
01858# # Site 2
01859# *****
01860# R0099:CO0026-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01861# DESIGN STANDYD 1.0 01:82-B3 .35 .121 No_date 1:00 51.06 .712 .000
01862# [XIMP= 47.71MP; .56]
01863# [SLP= 1.00DT; 1.00]
01864# *****
01865# # Site 2 - Roof
01866# *****
01867# R0099:CO0027-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01868# DESIGN STANDYD 1.0 01:82-Roof .09 .044 No_date 1:00 69.68 .972 .000
01869# [XIMP= 99.91MP; .99]
01870# [SLP= 50.0DT; 1.00]
01871# *****
01872# R0099:CO0027-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01873# ROUTE RESERVOIR -> 1.0 01:82-Roof 0.09 .044 No_date 1:00 69.68 n/a .000
01874# out <= 1.0 01:82-Roof-0u 0.09 .009 No_date 1:12 69.70 n/a .000
01875# overflow <= 1.0 01:82-Roof-0u 0.00 .000 No_date 0:00 .00 n/a .000
01876# [MettoUsed=.3119E-02 n3, TotovVol=.0000E+00 n3, N-Ovfr= 0, TotDurOvr= 0 hrs]
01877# R0099:CO0029-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01878# ADD HYD 1.0 01:82-Roof .44 .129 No_date 1:00 54.87 n/a .000
01879# + 1.0 01:82-Roof-0u 0.09 .009 No_date 1:12 69.70 n/a .000
01880# + 1.0 01:82-Roof-0u 0.00 .000 No_date 0:00 .00 n/a .000
01881# SUM= 1.0 01:SITE2-IN .44 .129 No_date 1:00 54.87 n/a .000
01882# R0099:CO0030-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01883# ROUTE RESERVOIR -> 1.0 01:SITE2-IN .44 .129 No_date 1:00 54.87 n/a .000
01884# out <= 1.0 01:SITE2-out .44 .018 No_date 1:39 54.87 n/a .000
01885# overflow <= 1.0 01:SITE2-out 0.00 .000 No_date 0:00 .00 n/a .000
01886# [MettoUsed=.1413E-01 n3, TotovVol=.0000E+00 n3, N-Ovfr= 0, TotDurOvr= 0 hrs]
01887# R0099:CO0031-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01888# ADD HYD 1.0 01:SITE2-Over .49 .014 No_date 1:41 54.06 n/a .000
01889# + 1.0 01:SITE2-Over 0.00 .000 No_date 0:00 .00 n/a .000
01890# SUM= 1.0 01:SITE2-IN .49 .014 No_date 1:41 54.06 n/a .000
01891# R0099:CO0032-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01892# ADD HYD 1.0 01:SITE2-Over .44 .018 No_date 1:39 54.87 n/a .000
01893# + 1.0 01:SITE2-Over 0.00 .000 No_date 0:00 .00 n/a .000
01894# SUM= 1.0 01:SITE2-IN .44 .018 No_date 1:39 54.87 n/a .000
01895# R0099:CO0033-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01896# ADD HYD 1.0 01:SITE2 .28 .031 No_date 1:22 40.14 n/a .000
01897# + 1.0 01:SITE2_1 .01 .003 No_date 1:00 27.07 n/a .000
01898# + 1.0 01:SITE2_1 .01 .014 No_date 1:41 54.06 n/a .000
01899# + 1.0 01:SITE2 .44 .018 No_date 1:39 54.87 n/a .000
01900# SUM= 1.0 01:SITE2 1.23 .027 No_date 1:27 40.14 n/a .000
01901# R0099:CO0034-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01902# ROUTE CHANNEL -> 1.0 01:21 1.23 .060 No_date 1:27 50.84 n/a .000
01903# [RDY= 1.00 out<= 1.0 01:21 1.23 .059 No_date 1:32 50.84 n/a .000]
01904# [L/S= 143.7 / 394 / 035]
01905# *****
01906# R0099:CO0035-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01907# ADD HYD 1.0 01:21 1.23 .059 No_date 1:32 50.84 n/a .000
01908# + 1.0 01:21 1.23 .059 No_date 1:32 50.84 n/a .000
01909# SUM= 1.0 01:21 1.23 .059 No_date 1:32 50.84 n/a .000
01910# R0099:CO0036-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01911# ROUTE CHANNEL -> 1.0 01:21 1.23 .059 No_date 1:32 50.84 n/a .000
01912# [RDY= 1.00 out<= 1.0 01:21 1.23 .059 No_date 1:32 50.84 n/a .000]
01913# [L/S= 73.7 / 429 / 035]
01914# *****
01915# R0099:CO0037-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01916# ADD HYD 1.0 01:21 5.00 .253 No_date 1:43 38.43 n/a .000
01917# + 1.0 01:21 5.00 .253 No_date 1:43 38.43 n/a .000
01918# SUM= 1.0 01:21 5.00 .253 No_date 1:43 38.43 n/a .000
01919# R0099:CO0038-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01920# ROUTE CHANNEL -> 1.0 01:23 5.31 .271 No_date 1:39 38.14 n/a .000
01921# [RDY= 1.00 out<= 1.0 01:23 5.31 .270 No_date 1:43 38.14 n/a .000]
01922# [L/S= 92.7 / 274 / 043]
01923# *****
01924# R0099:CO0039-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01925# ADD HYD 1.0 01:23 5.31 .270 No_date 1:43 38.14 n/a .000
01926# + 1.0 01:23 5.31 .270 No_date 1:43 38.14 n/a .000
01927# SUM= 1.0 01:23 5.31 .270 No_date 1:43 38.14 n/a .000
01928# R0099:CO0040-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01929# ROUTE CHANNEL -> 1.0 01:24 5.90 .291 No_date 1:51 37.37 n/a .000
01930# [RDY= 1.00 out<= 1.0 01:24 5.90 .291 No_date 1:51 37.37 n/a .000]
01931# [L/S= 251.7 / 190 / 035]
01932# *****
01933# R0099:CO0041-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01934# ADD HYD 1.0 01:24 5.90 .291 No_date 1:51 37.37 n/a .000
01935# + 1.0 01:24 5.90 .291 No_date 1:51 37.37 n/a .000
01936# SUM= 1.0 01:24 5.90 .291 No_date 1:51 37.37 n/a .000
01937# R0099:CO0042-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01938# ROUTE CHANNEL -> 1.0 01:25 7.24 .381 No_date 1:46 37.72 n/a .000
01939# [RDY= 1.00 out<= 1.0 01:25 7.24 .377 No_date 1:50 37.72 n/a .000]
01940# [L/S= 237.7 / 644 / 035]
01941# *****
01942# R0099:CO0043-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01943# ADD HYD 1.0 01:25 7.24 .381 No_date 1:46 37.72 n/a .000
01944# + 1.0 01:25 7.24 .381 No_date 1:46 37.72 n/a .000
01945# SUM= 1.0 01:25 7.24 .381 No_date 1:46 37.72 n/a .000
01946# R0099:CO0044-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01947# ROUTE CHANNEL -> 1.0 01:26 8.81 .059 No_date 1:20 26.17 n/a .000
01948# [RDY= 1.00 out<= 1.0 01:26 8.81 .058 No_date 1:22 26.17 n/a .000]
01949# [L/S= 77.7 / 776 / 035]
01950# *****
01951# R0099:CO0045-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01952# ROUTE CHANNEL -> 1.0 01:27 9.16 .067 No_date 1:28 26.71 n/a .000
01953# [RDY= 1.00 out<= 1.0 01:27 9.16 .067 No_date 1:28 26.71 n/a .000]
01954# [L/S= 159.7 / 576 / 035]
01955# *****
01956# R0099:CO0046-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01957# ADD HYD 1.0 01:28 1.02 .069 No_date 1:23 26.48 n/a .000
01958# + 1.0 01:28 1.02 .069 No_date 1:23 26.48 n/a .000
01959# SUM= 1.0 01:28 1.02 .069 No_date 1:23 26.48 n/a .000
01960# R0099:CO0047-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01961# ROUTE CHANNEL -> 1.0 01:28 1.02 .069 No_date 1:23 26.48 n/a .000
01962# [RDY= 1.00 out<= 1.0 01:28 1.02 .069 No_date 1:23 26.48 n/a .000]
01963# [L/S= 79.7 / 522 / 035]
01964# *****
01965# R0099:CO0048-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01966# ADD HYD 1.0 01:28 1.02 .068 No_date 1:27 26.67 n/a .000
01967# + 1.0 01:28 1.02 .068 No_date 1:27 26.67 n/a .000
01968# SUM= 1.0 01:28 1.02 .068 No_date 1:27 26.67 n/a .000
01969# R0099:CO0049-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01970# ROUTE CHANNEL -> 1.0 01:27 1.46 .094 No_date 1:28 26.71 n/a .000
01971# [RDY= 1.00 out<= 1.0 01:27 1.46 .094 No_date 1:28 26.71 n/a .000]
01972# [L/S= 79.7 / 522 / 035]
01973# *****
01974# R0099:CO0050-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01975# ADD HYD 1.0 01:28 1.02 .068 No_date 1:27 26.67 n/a .000
01976# + 1.0 01:28 1.02 .068 No_date 1:27 26.67 n/a .000
01977# SUM= 1.0 01:28 1.02 .068 No_date 1:27 26.67 n/a .000
01978# R0099:CO0051-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01979# ROUTE CHANNEL -> 1.0 01:27 1.46 .094 No_date 1:28 26.71 n/a .000
01980# [RDY= 1.00 out<= 1.0 01:27 1.46 .094 No_date 1:28 26.71 n/a .000]
01981# [L/S= 79.7 / 522 / 035]
01982# *****
01983# R0099:CO0052-----Dtn-ID-INVD-----AREAh-QFEARcns-TpeakDate_hh:mm-----Rvmm-R.C-----DWfcm
01984# DESIGN STANDYD 1.0 01:81-Roof .07 .011 No_date 1:00 46.49 .359 .000
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[illegible]

[illegible]

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028811 (RDY= 1.00i out<- 1.0 01:R2 5.00 .182 No_date 12:131 39.34 n/a .000
02882 (L/S/= 71.7 / 423/.035)
02883 (Vmax= .481;Dmax= .247)
02884 R0125:C00037 -----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02885 ADD HYD + 1.0 02:EXT4 .31 .022 No_date 12:11 35.39 n/a .000
02886 (L/S/= 71.7 / 423/.035)
02887 SUM= 1.0 02:EXT4 .59 .028 No_date 12:12 39.21 n/a .000
02888 R0125:C00038 -----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02889 ROUTE CHANNEL -> 1.0 02:J3 5.31 .195 No_date 12:27 39.11 n/a .000
02890 (RDY= 1.00i out<- 1.0 01:R3 5.31 .195 No_date 12:31 39.11 n/a .000
02891 (L/S/= 92.7 / 274/.035)
02892 (Vmax= .384;Dmax= .287)
02893 R0125:C00039 -----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02894 ADD HYD + 1.0 02:R3 5.31 .195 No_date 12:31 39.11 n/a .000
02895 + 1.0 02:EXT7 .47 .025 No_date 12:13 39.90 n/a .000
02896 SUM= 1.0 02:J4 5.90 .221 No_date 12:29 38.43 n/a .000
02897 R0125:C00040 -----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02898 ROUTE CHANNEL -> 1.0 02:J4 5.90 .221 No_date 12:29 38.43 n/a .000
02899 (RDY= 1.00i out<- 1.0 01:R4 5.90 .209 No_date 12:40 38.43 n/a .000
02900 (L/S/= 251.7 / 139/.035)
02901 (Vmax= .386;Dmax= .287)
02902 R0125:C00041 -----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02903 ADD HYD + 1.0 02:R4 5.90 .209 No_date 12:40 38.43 n/a .000
02904 + 1.0 02:EXT6 .86 .046 No_date 12:29 42.40 n/a .000
02905 + 1.0 02:EXT7 .47 .025 No_date 12:13 39.90 n/a .000
02906 SUM= 1.0 02:J5 7.24 .273 No_date 12:35 39.00 n/a .000
02907 R0125:C00042 -----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02908 ROUTE CHANNEL -> 1.0 02:J5 7.24 .273 No_date 12:35 39.00 n/a .000
02909 (RDY= 1.00i out<- 1.0 01:R5 7.24 .269 No_date 12:41 39.00 n/a .000
02910 (L/S/= 237.7 / 644/.035)
02911 (Vmax= .492;Dmax= .269)
02912 R0125:C00043 -----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02913 ADD HYD + 1.0 02:Pre0_1 .80 .043 No_date 12:11 28.00 n/a .000
02914 + 1.0 02:EXT6 .01 .001 No_date 12:20 19.72 n/a .000
02915 SUM= 1.0 02:Pre0_2 .00 .000 No_date 12:00 34.35 n/a .000
02916 + 1.0 02:Pre .81 .043 No_date 12:11 27.87 n/a .000
02917 R0125:C00044 -----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02918 ROUTE CHANNEL -> 1.0 02:Pre .81 .043 No_date 12:11 27.87 n/a .000
02919 (RDY= 1.00i out<- 1.0 01:R6 .81 .043 No_date 12:14 27.87 n/a .000
02920 (L/S/= 71.7 / 777/.035)
02921 (Vmax= .492;Dmax= .032)
02922 R0125:C00045 -----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02923 ROUTE CHANNEL -> 1.0 02:Pre0_1 .44 .020 No_date 12:17 28.00 n/a .000
02924 (RDY= 1.00i out<- 1.0 01:R7 .44 .019 No_date 12:21 28.00 n/a .000
02925 (L/S/= 159.1 / 576/.035)
02926 (Vmax= .797;Dmax= .064)
02927 R0125:C00046 -----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02928 ADD HYD + 1.0 02:R6 .81 .043 No_date 12:14 27.92 n/a .000
02929 + 1.0 02:EXT10 .20 .008 No_date 12:20 27.99 n/a .000
02930 SUM= 1.0 02:R6 .81 .043 No_date 12:14 27.94 n/a .000
02931 R0125:C00047 -----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02932 ROUTE CHANNEL -> 1.0 02:R6 .81 .043 No_date 12:14 27.94 n/a .000
02933 (RDY= 1.00i out<- 1.0 01:R8 1.02 .050 No_date 12:18 27.94 n/a .000
02934 (L/S/= 79.7 / 522/.035)
02935 (Vmax= .423;Dmax= .037)
02936 R0125:C00048 -----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02937 ADD HYD + 1.0 02:R7 .44 .019 No_date 12:21 28.07 n/a .000
02938 + 1.0 02:EXT7 .44 .019 No_date 12:21 28.07 n/a .000
02939 SUM= 1.0 02:R7 1.46 .069 No_date 12:19 28.00 n/a .000
02940 R0125:C00049 -----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02941 ROUTE CHANNEL -> 1.0 02:J7 1.46 .069 No_date 12:19 28.00 n/a .000
02942 (RDY= 1.00i out<- 1.0 01:R9 1.46 .069 No_date 12:20 28.00 n/a .000
02943 (L/S/= 29.7 / 887/.035)
02944 (Vmax= .543;Dmax= .047)
02945 R0125:C00050 -----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02946 ADD HYD + 1.0 02:EXT9 3.57 .158 No_date 12:24 32.39 n/a .000
02947 + 1.0 02:EXT6 .86 .046 No_date 12:29 42.40 n/a .000
02948 + 1.0 02:EXT8 .83 .045 No_date 12:19 35.39 n/a .000
02949 SUM= 1.0 02:R5 13.02 .511 No_date 12:30 35.75 n/a .000
02950 R0125:C00051 -----Dtn-ID-INHYD-----AREAh-QFEARms-TpeakDate_hh:mm-----Rvmm-R.C-----DWfms
02951 ROUTE CHANNEL -> 1.0 02:R5 13.02 .511 No_date 12:30 35.75 n/a .000
02952 (RDY= 1.00i out<- 1.0 01:R10 13.10 .504 No_date 12:35 35.75 n/a .000
02953 (L/S/= 8.7 / 010/.013)
02954 (Vmax= .420;Dmax= 1.090)
02955 (Dln= .53;Dused= 1.33)
02956 *****
02957 *****
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03060 *****
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03601 *****
03602 * STORM
03603 *****
03604 ** END OF RUN : 198
03605
03606 .....
03607 .....
03608 .....
03609 .....
03610 .....
03611 .....
03612 RIN# COMMAND#
03613 R0199:C00001-----
03614 START
03615 [TZERO = .00 hrs on 0]
03616 [METOUT= 2 (1=imperial, 2=metric output)]
03617 [METOUT= 1]
03618 [NUN = 0199]
03619 .....
03620 * SWEV# / INPUT DATA FILE
03621 *****
03622 * Project Name : [5923 Ottawa St]
03623 * Project Number: [P2710(e01)]
03624 * Date : [2025 April 28]
03625 * Modeler : [JFM]
03626 * Company : [JFSA Canada Inc.]
03627 * License # : [2549237]
03628 .....
03629 * Model developed to simulate runoff from subcatchments under pre development conditions
03630 .....
03631 R0199:C00002-----
03632 READ STORM
03633 File name = STORM.001
03634 Catchment = 100 years SCM Type 2 Storm 24 hours step 10 min, City of Ottawa
03635 [EPA10.00] [EPA24.00] [EPA30.00] [EPA36.00] [EPA42.00] [EPA48.00] [EPA54.00] [EPA60.00] [EPA66.00] [EPA72.00] [EPA78.00] [EPA84.00] [EPA90.00] [EPA96.00] [EPA102.00] [EPA108.00] [EPA114.00] [EPA120.00] [EPA126.00] [EPA132.00] [EPA138.00] [EPA144.00] [EPA150.00] [EPA156.00] [EPA162.00] [EPA168.00] [EPA174.00] [EPA180.00] [EPA186.00] [EPA192.00] [EPA198.00] [EPA204.00] [EPA210.00] [EPA216.00] [EPA222.00] [EPA228.00] [EPA234.00] [EPA240.00] [EPA246.00] [EPA252.00] [EPA258.00] [EPA264.00] [EPA270.00] [EPA276.00] [EPA282.00] [EPA288.00] [EPA294.00] [EPA300.00] [EPA306.00] [EPA312.00] [EPA318.00] [EPA324.00] [EPA330.00] [EPA336.00] [EPA342.00] [EPA348.00] [EPA354.00] [EPA360.00] [EPA366.00] [EPA372.00] [EPA378.00] [EPA384.00] [EPA390.00] [EPA396.00] [EPA402.00] [EPA408.00] [EPA414.00] [EPA420.00] [EPA426.00] [EPA432.00] [EPA438.00] [EPA444.00] [EPA450.00] [EPA456.00] [EPA462.00] [EPA468.00] [EPA474.00] [EPA480.00] [EPA486.00] [EPA492.00] [EPA498.00] [EPA504.00] [EPA510.00] [EPA516.00] [EPA522.00] [EPA528.00] [EPA534.00] [EPA540.00] [EPA546.00] [EPA552.00] [EPA558.00] [EPA564.00] [EPA570.00] [EPA576.00] [EPA582.00] [EPA588.00] [EPA594.00] [EPA600.00] [EPA606.00] [EPA612.00] [EPA618.00] [EPA624.00] [EPA630.00] [EPA636.00] [EPA642.00] [EPA648.00] [EPA654.00] [EPA660.00] [EPA666.00] [EPA672.00] [EPA678.00] [EPA684.00] [EPA690.00] [EPA696.00] [EPA702.00] [EPA708.00] [EPA714.00] [EPA720.00] [EPA726.00] [EPA732.00] [EPA738.00] [EPA744.00] [EPA750.00] [EPA756.00] [EPA762.00] [EPA768.00] [EPA774.00] [EPA780.00] [EPA786.00] [EPA792.00] [EPA798.00] [EPA804.00] [EPA810.00] [EPA816.00] [EPA822.00] [EPA828.00] [EPA834.00] [EPA840.00] [EPA846.00] [EPA852.00] [EPA858.00] [EPA864.00] [EPA870.00] [EPA876.00] [EPA882.00] [EPA888.00] [EPA894.00] [EPA900.00] [EPA906.00] [EPA912.00] [EPA918.00] [EPA924.00] [EPA930.00] [EPA936.00] [EPA942.00] [EPA948.00] [EPA954.00] [EPA960.00] [EPA966.00] [EPA972.00] [EPA978.00] [EPA984.00] [EPA990.00] [EPA996.00] [EPA1002.00] [EPA1008.00] [EPA1014.00] 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```
03961: *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03962: R0125:C00015 ROUTE PIPE ->
03963: *** WARNING: New pipe size used for routing.
03964: R0050:C00015 CALIB NASHVD
03965: *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03966: R0050:C00016 CALIB NASHVD
03967: *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03968: R0050:C00018 CALIB NASHVD
03969: *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03970: R0099:C00051 ROUTE PIPE ->
03971: *** WARNING: New pipe size used for routing.
03972: R0099:C00015 CALIB NASHVD
03973: *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03974: R0099:C00016 CALIB NASHVD
03975: *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03976: R0099:C00018 CALIB NASHVD
03977: *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03978: R0099:C00051 ROUTE PIPE ->
03979: *** WARNING: New pipe size used for routing.
03980: R0102:C00015 CALIB NASHVD
03981: *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03982: R0102:C00016 CALIB NASHVD
03983: *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03984: R0102:C00018 CALIB NASHVD
03985: *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03986: R0102:C00051 ROUTE PIPE ->
03987: *** WARNING: New pipe size used for routing.
03988: R0105:C00015 CALIB NASHVD
03989: *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03990: R0105:C00016 CALIB NASHVD
03991: *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03992: R0105:C00018 CALIB NASHVD
03993: *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03994: R0105:C00051 ROUTE PIPE ->
03995: *** WARNING: New pipe size used for routing.
03996: R0110:C00015 CALIB NASHVD
03997: *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
03998: R0110:C00016 CALIB NASHVD
03999: *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
04000: R0110:C00018 CALIB NASHVD
04001: *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
04002: R0110:C00051 ROUTE PIPE ->
04003: *** WARNING: New pipe size used for routing.
04004: R0125:C00015 CALIB NASHVD
04005: *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
04006: R0125:C00016 CALIB NASHVD
04007: *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
04008: R0125:C00018 CALIB NASHVD
04009: *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
04010: R0125:C00051 ROUTE PIPE ->
04011: *** WARNING: New pipe size used for routing.
04012: R0150:C00015 CALIB NASHVD
04013: *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
04014: R0150:C00016 CALIB NASHVD
04015: *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
04016: R0150:C00018 CALIB NASHVD
04017: *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
04018: R0150:C00051 ROUTE PIPE ->
04019: *** WARNING: New pipe size used for routing.
04020: R0199:C00015 CALIB NASHVD
04021: *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
04022: R0199:C00016 CALIB NASHVD
04023: *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
04024: R0199:C00018 CALIB NASHVD
04025: *** WARNING: Time step is too large for value of TP. RV may be ok. Peak flow could be off.
04026: R0199:C00051 ROUTE PIPE ->
04027: *** WARNING: New pipe size used for routing.
04028: Simulation ended on 2025-06-02 at 18:47:34
04029: =====
04030:
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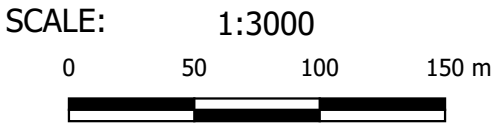
Attachment C

Hydraulic Analysis



Legend

- Site Boundary
- Jock River Tributary
- HEC-RAS Cross Sections
- Centerline



5923 Ottawa St – Richmond

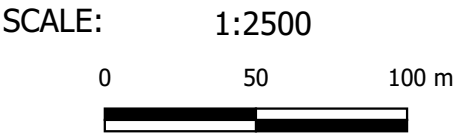
Figure C1: HEC-RAS Cross Sections

PROJECT	P2710(e01)
DRAWN	MM
DATE	5 June 2025



Legend

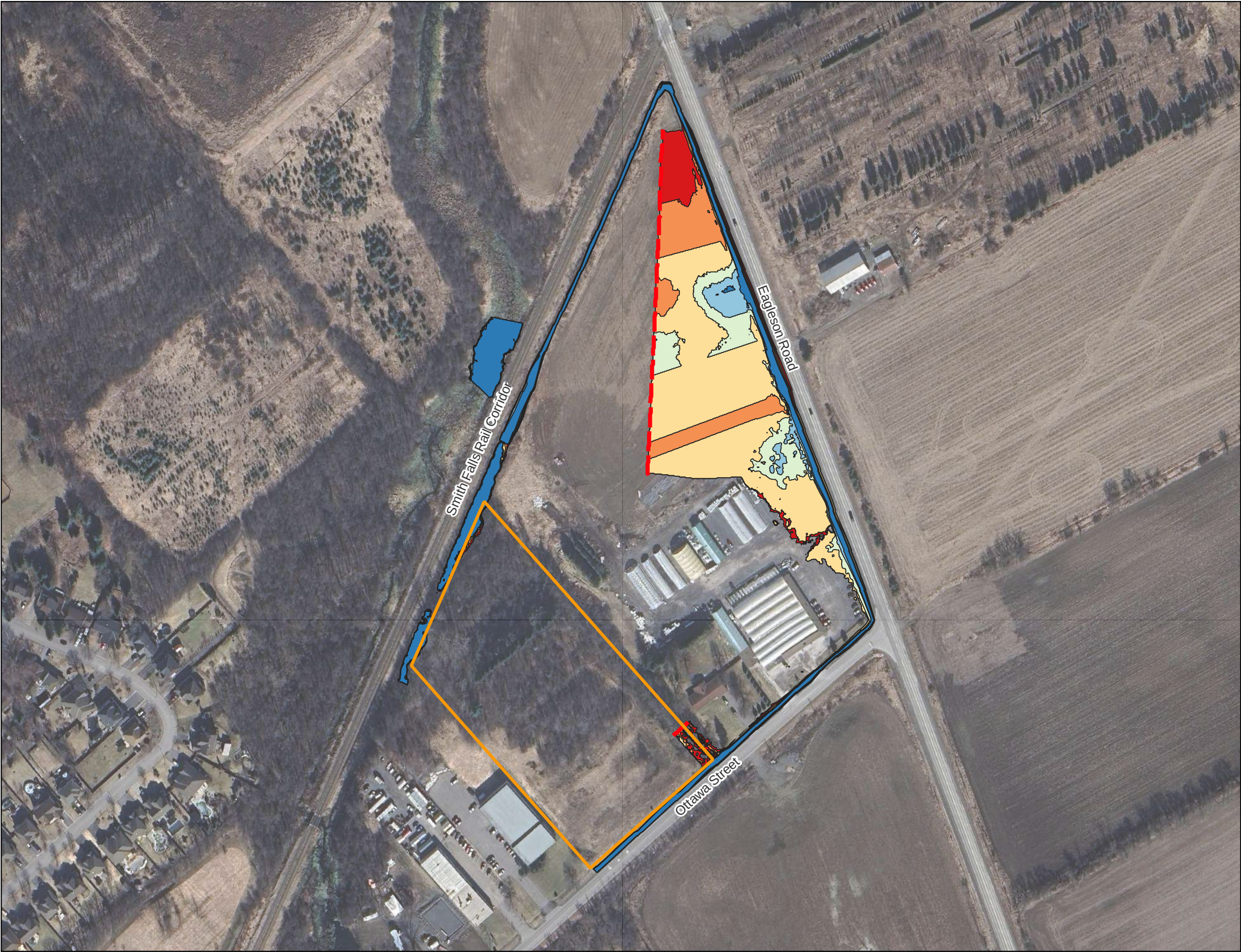
- Site Boundary
- Pre-Development Flood Extents
 - 2YrSCS24Hr
 - 5YrSCS24Hr
 - 10YrSCS24Hr
 - 25YrSCS24Hr
 - 50YrSCS24Hr
 - 100YrSCS24Hr
- Spill Line



5923 Ottawa St - Richmond

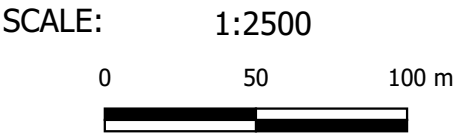
Figure C2: Pre-Development Flood Extents

PROJECT	P2719(e01)
DRAWN	BT
DATE	5 June 2025



Legend

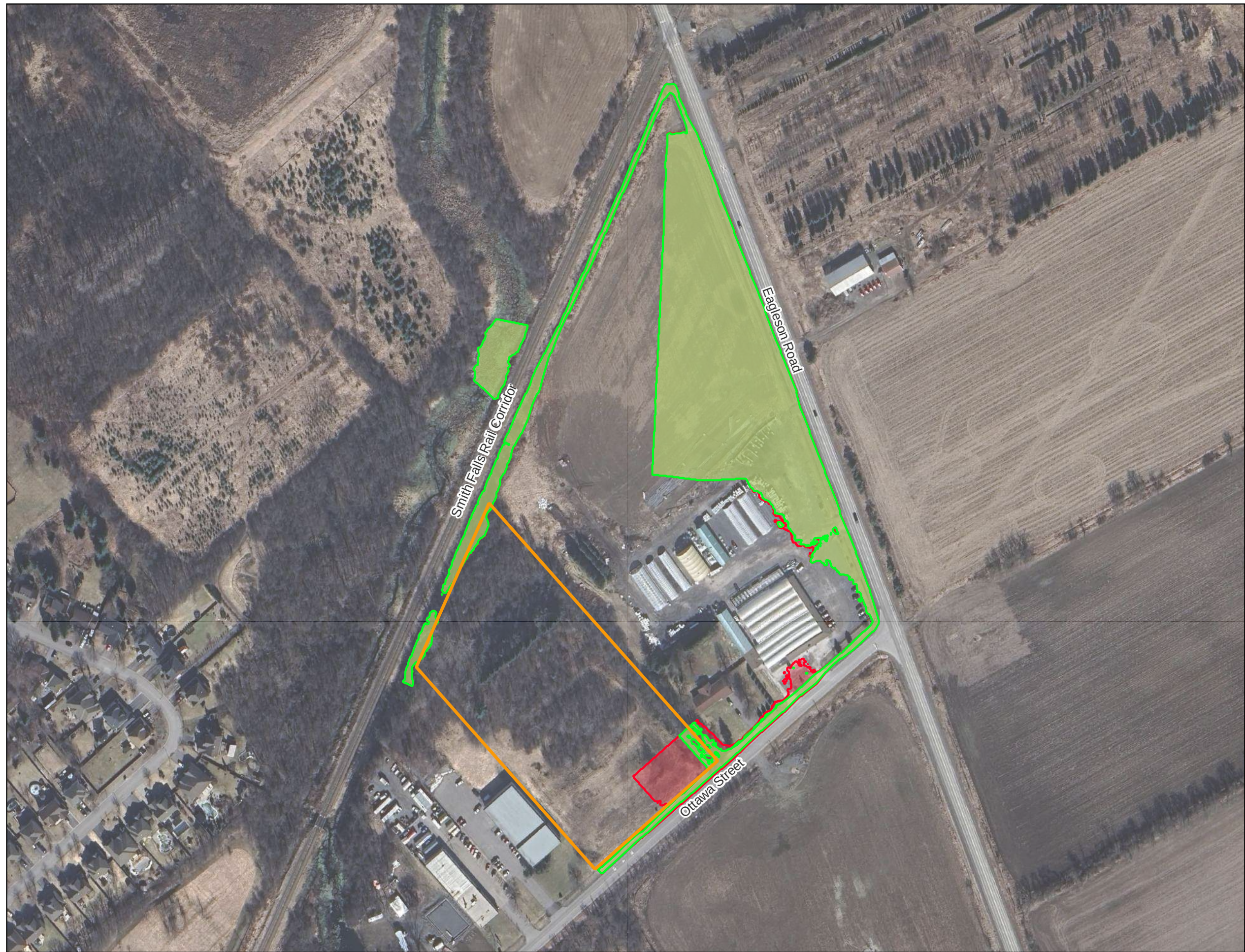
- Site Boundary
- Post-Development Flood Extents
 - 2YrSCS24Hr
 - 5YrSCS24Hr
 - 10YrSCS24Hr
 - 25YrSCS24Hr
 - 50YrSCS24Hr
 - 100YrSCS24Hr
- Spill Line



5923 Ottawa St - Richmond

Figure C3: Post-Development Flood Extents

PROJECT	P2719(e01)
DRAWN	BT
DATE	5 June 2025



Legend

-  Site Boundary
-  Pre-Development 100yr
-  Post-Development 100yr

SCALE: 1:2500

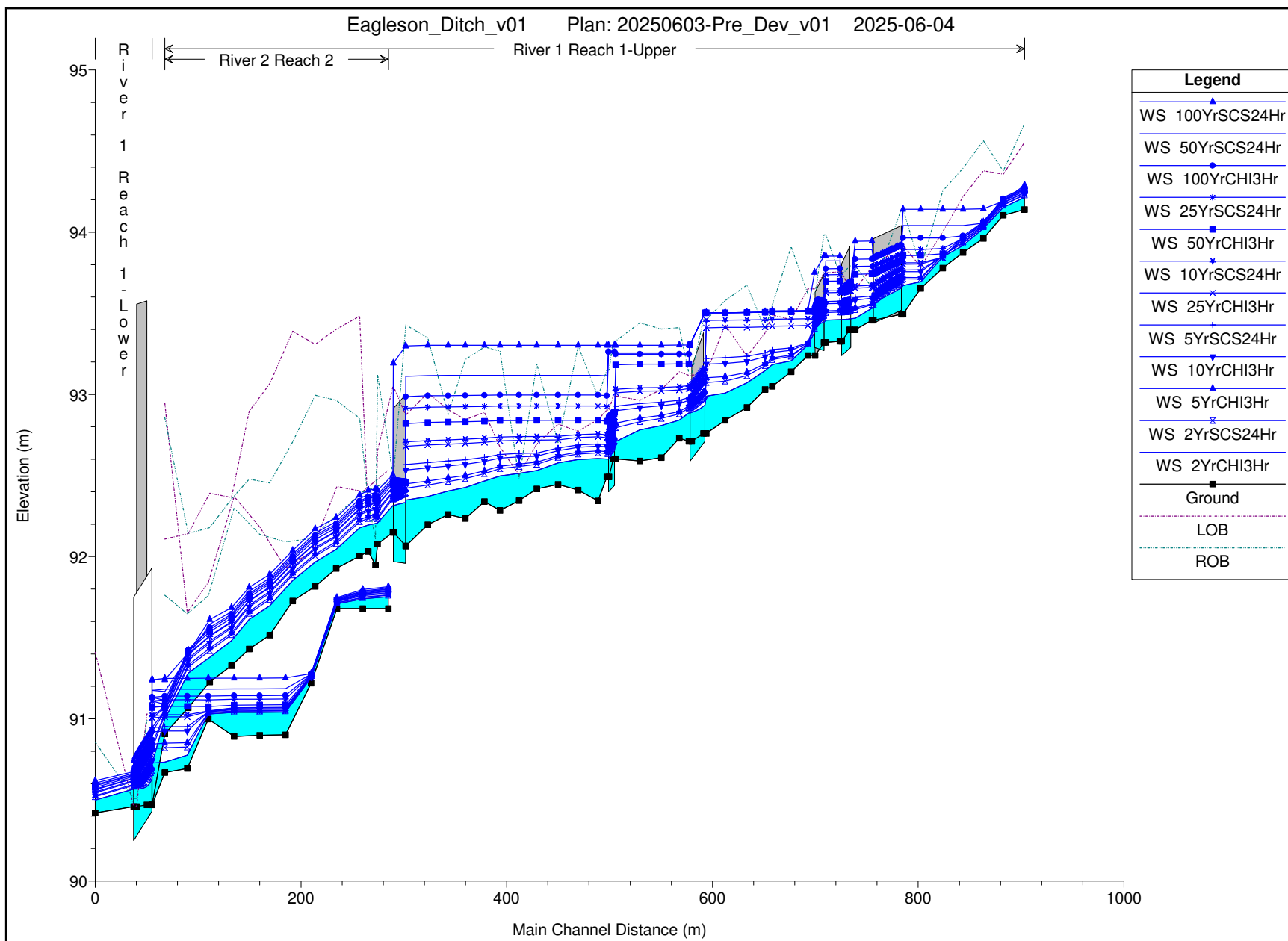
0 50 100 m

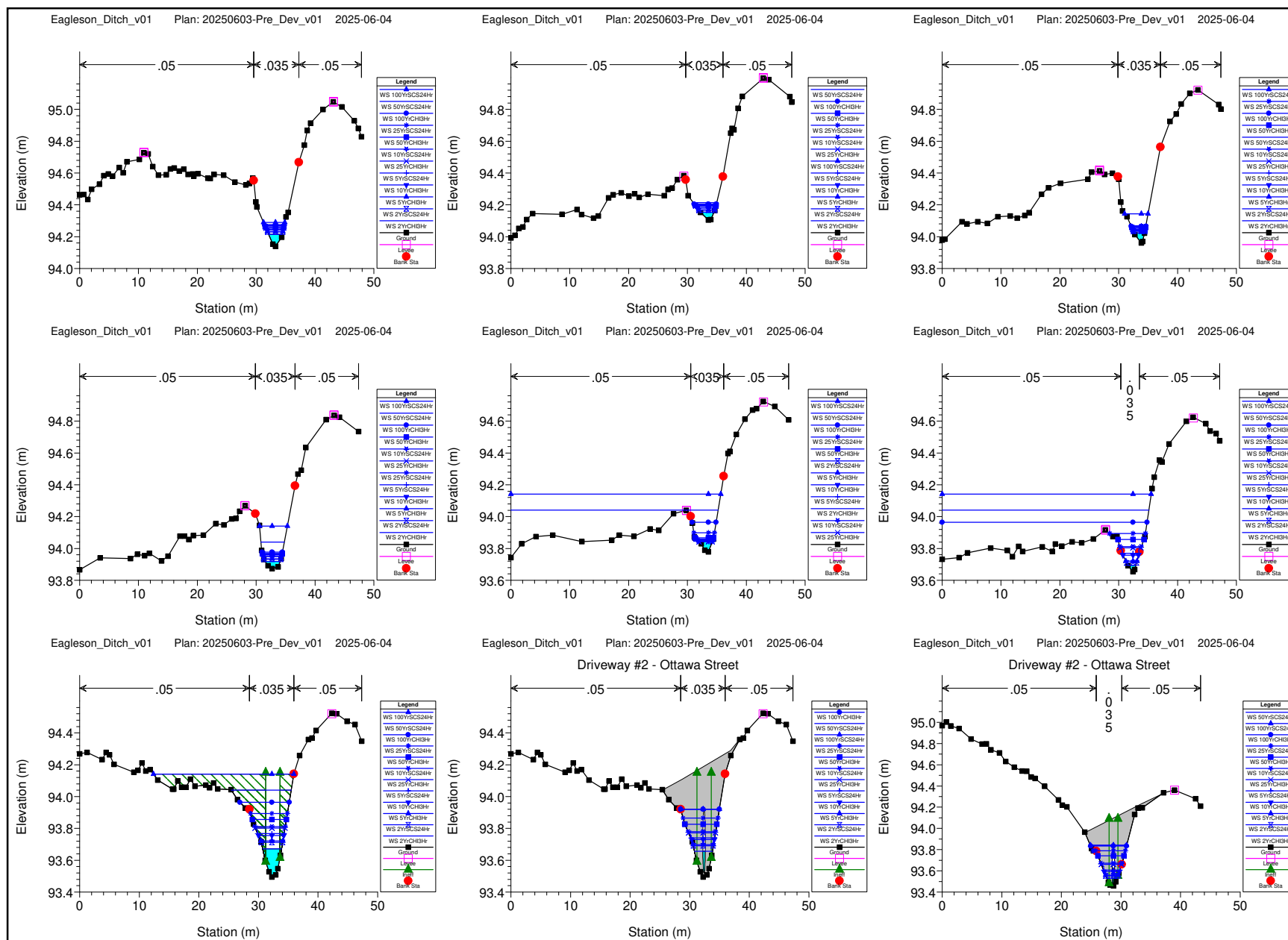


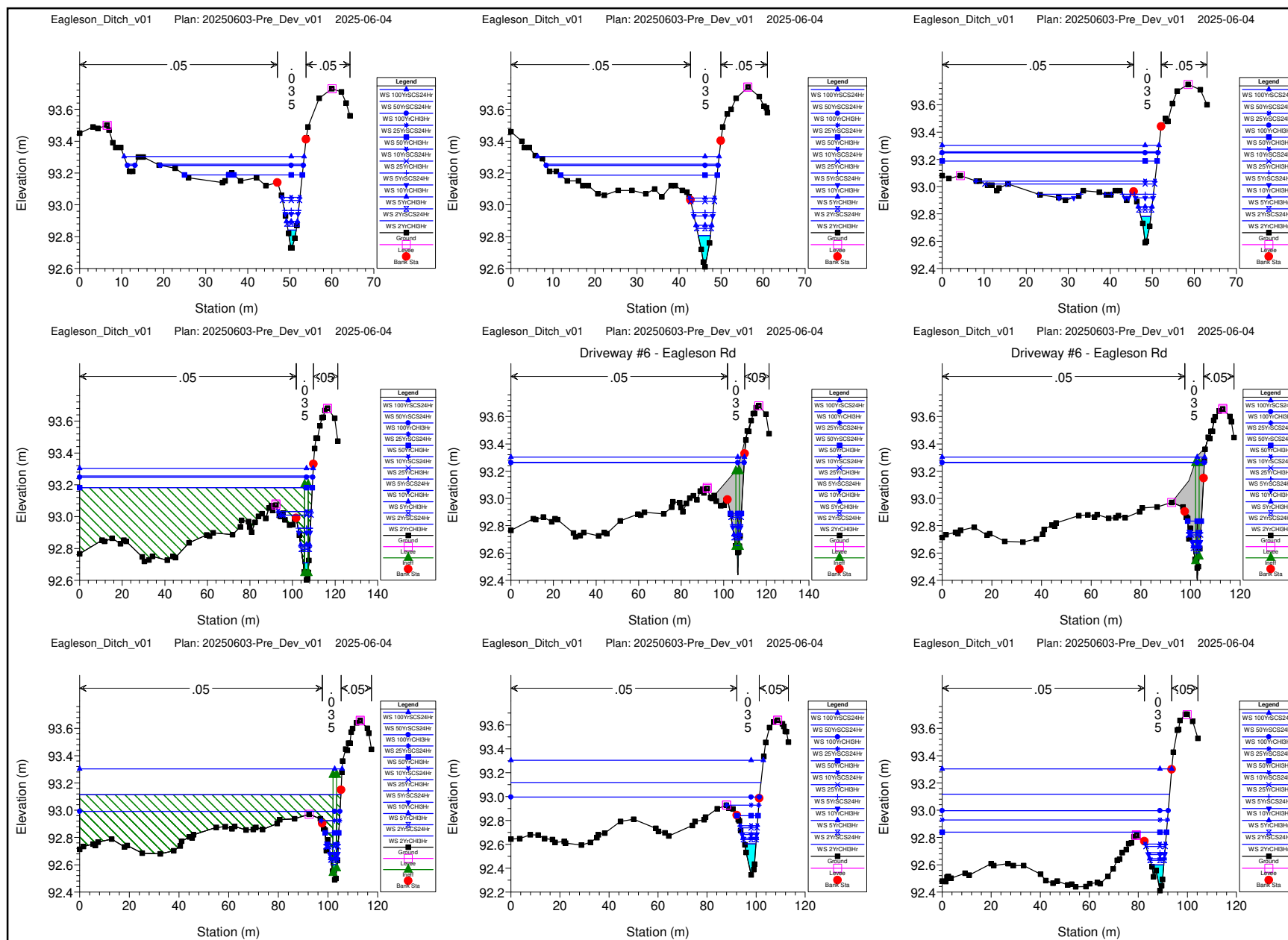
5923 Ottawa St - Richmond

Figure C4: 100-yr Floodplain Extents Comparison

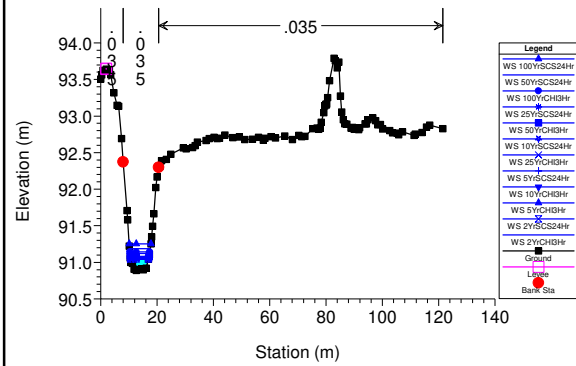
PROJECT	P2719(e01)
DRAWN	BT
DATE	5 June 2025



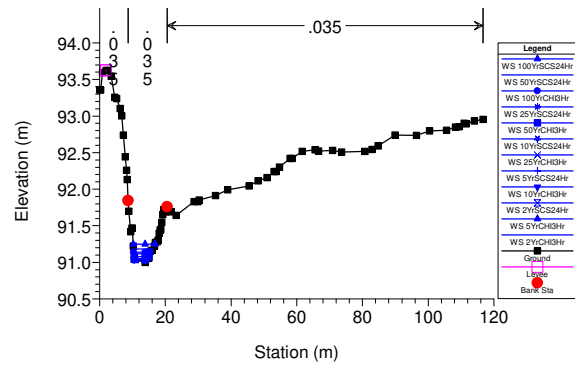




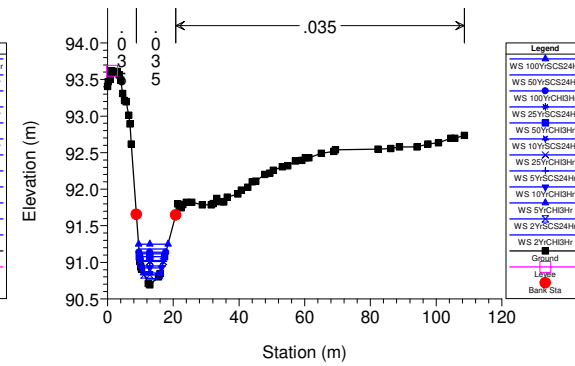
Eagleson_Ditch_v01 Plan: 20250603-Pre_Dev_v01 2025-06-04



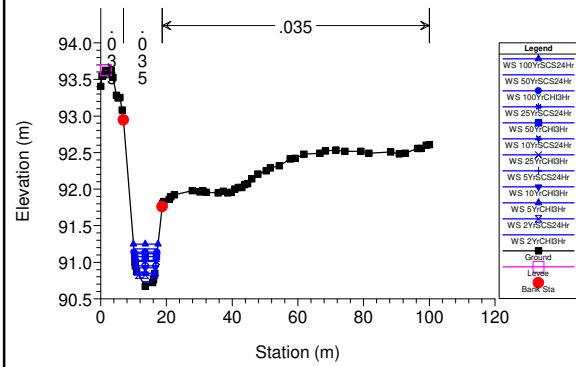
Eagleson_Ditch_v01 Plan: 20250603-Pre_Dev_v01 2025-06-04



Eagleson_Ditch_v01 Plan: 20250603-Pre_Dev_v01 2025-06-04



Eagleson_Ditch_v01 Plan: 20250603-Pre_Dev_v01 2025-06-04



River	Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
River 2	Reach 2	224	2YrCHI3Hr	0.02	91.68	91.75	91.71	91.75	0.000626	0.08	0.20	5.09	0.13
River 2	Reach 2	224	5YrCHI3Hr	0.03	91.68	91.76	91.72	91.76	0.000730	0.10	0.26	5.99	0.15
River 2	Reach 2	224	10YrCHI3Hr	0.03	91.68	91.77	91.72	91.77	0.000742	0.11	0.32	6.48	0.15
River 2	Reach 2	224	25YrCHI3Hr	0.05	91.68	91.78	91.73	91.79	0.000756	0.12	0.39	6.61	0.16
River 2	Reach 2	224	50YrCHI3Hr	0.06	91.68	91.79	91.73	91.79	0.000763	0.13	0.44	6.71	0.16
River 2	Reach 2	224	100YrCHI3Hr	0.07	91.68	91.80	91.74	91.80	0.000773	0.14	0.50	6.81	0.16
River 2	Reach 2	224	2YrSCS24Hr	0.02	91.68	91.76	91.72	91.76	0.000717	0.09	0.25	5.79	0.14
River 2	Reach 2	224	5YrSCS24Hr	0.04	91.68	91.78	91.73	91.78	0.000753	0.11	0.35	6.53	0.15
River 2	Reach 2	224	10YrSCS24Hr	0.05	91.68	91.79	91.73	91.79	0.000757	0.12	0.41	6.65	0.16
River 2	Reach 2	224	25YrSCS24Hr	0.07	91.68	91.80	91.74	91.80	0.000769	0.14	0.48	6.78	0.16
River 2	Reach 2	224	50YrSCS24Hr	0.08	91.68	91.81	91.74	91.81	0.000794	0.15	0.54	6.88	0.17
River 2	Reach 2	224	100YrSCS24Hr	0.09	91.68	91.81	91.75	91.82	0.000800	0.16	0.60	6.99	0.17
River 2	Reach 2	199	2YrCHI3Hr	0.02	91.68	91.74	91.71	91.74	0.000450	0.07	0.24	6.76	0.11
River 2	Reach 2	199	5YrCHI3Hr	0.03	91.68	91.75	91.71	91.75	0.000479	0.08	0.31	6.96	0.12
River 2	Reach 2	199	10YrCHI3Hr	0.03	91.68	91.76	91.71	91.76	0.000481	0.09	0.38	7.14	0.12
River 2	Reach 2	199	25YrCHI3Hr	0.05	91.68	91.77	91.72	91.77	0.000549	0.10	0.45	7.32	0.13
River 2	Reach 2	199	50YrCHI3Hr	0.06	91.68	91.78	91.72	91.78	0.000569	0.11	0.50	7.42	0.14
River 2	Reach 2	199	100YrCHI3Hr	0.07	91.68	91.78	91.73	91.78	0.000591	0.12	0.56	7.51	0.14
River 2	Reach 2	199	2YrSCS24Hr	0.02	91.68	91.75	91.71	91.75	0.000474	0.08	0.30	6.91	0.12
River 2	Reach 2	199	5YrSCS24Hr	0.04	91.68	91.76	91.72	91.76	0.000522	0.10	0.41	7.20	0.13
River 2	Reach 2	199	10YrSCS24Hr	0.05	91.68	91.77	91.72	91.77	0.000558	0.11	0.47	7.37	0.14
River 2	Reach 2	199	25YrSCS24Hr	0.07	91.68	91.78	91.72	91.78	0.000582	0.12	0.55	7.49	0.14
River 2	Reach 2	199	50YrSCS24Hr	0.08	91.68	91.79	91.73	91.79	0.000628	0.13	0.60	7.57	0.15
River 2	Reach 2	199	100YrSCS24Hr	0.09	91.68	91.80	91.73	91.80	0.000634	0.14	0.66	7.67	0.15
River 2	Reach 2	174	2YrCHI3Hr	0.02	91.68	91.71	91.70	91.71	0.009341	0.22	0.07	3.33	0.47
River 2	Reach 2	174	5YrCHI3Hr	0.03	91.68	91.71	91.70	91.72	0.010728	0.27	0.09	3.51	0.52
River 2	Reach 2	174	10YrCHI3Hr	0.03	91.68	91.72	91.71	91.73	0.009147	0.28	0.12	3.68	0.49
River 2	Reach 2	174	25YrCHI3Hr	0.05	91.68	91.73	91.72	91.73	0.010482	0.33	0.14	3.80	0.54
River 2	Reach 2	174	50YrCHI3Hr	0.06	91.68	91.73	91.72	91.74	0.010789	0.35	0.16	3.90	0.56
River 2	Reach 2	174	100YrCHI3Hr	0.07	91.68	91.74	91.72	91.75	0.011338	0.38	0.18	3.99	0.58
River 2	Reach 2	174	2YrSCS24Hr	0.02	91.68	91.71	91.70	91.72	0.009099	0.24	0.09	3.51	0.48
River 2	Reach 2	174	5YrSCS24Hr	0.04	91.68	91.73	91.71	91.73	0.009102	0.29	0.13	3.75	0.50
River 2	Reach 2	174	10YrSCS24Hr	0.05	91.68	91.73	91.72	91.74	0.010830	0.34	0.15	3.84	0.55
River 2	Reach 2	174	25YrSCS24Hr	0.07	91.68	91.74	91.72	91.74	0.010024	0.36	0.18	4.01	0.55
River 2	Reach 2	174	50YrSCS24Hr	0.08	91.68	91.74	91.73	91.75	0.010794	0.40	0.20	4.08	0.57
River 2	Reach 2	174	100YrSCS24Hr	0.09	91.68	91.75	91.73	91.76	0.010716	0.42	0.22	4.15	0.58
River 2	Reach 2	149	2YrCHI3Hr	0.02	91.22	91.25	91.25	91.26	0.049600	0.35	0.05	3.45	0.99
River 2	Reach 2	149	5YrCHI3Hr	0.03	91.22	91.26	91.26	91.27	0.037267	0.35	0.07	4.39	0.89
River 2	Reach 2	149	10YrCHI3Hr	0.03	91.22	91.26	91.26	91.27	0.052915	0.44	0.08	4.47	1.07
River 2	Reach 2	149	25YrCHI3Hr	0.05	91.22	91.27	91.27	91.28	0.039832	0.45	0.10	4.68	0.97
River 2	Reach 2	149	50YrCHI3Hr	0.06	91.22	91.27	91.27	91.28	0.037244	0.47	0.12	4.80	0.95
River 2	Reach 2	149	100YrCHI3Hr	0.07	91.22	91.27	91.27	91.29	0.034157	0.49	0.14	4.94	0.93
River 2	Reach 2	149	2YrSCS24Hr	0.02	91.22	91.26	91.26	91.26	0.052399	0.39	0.06	3.96	1.03
River 2	Reach 2	149	5YrSCS24Hr	0.04	91.22	91.26	91.26	91.27	0.052134	0.46	0.08	4.53	1.07
River 2	Reach 2	149	10YrSCS24Hr	0.05	91.22	91.27	91.27	91.28	0.037535	0.46	0.11	4.74	0.95
River 2	Reach 2	149	25YrSCS24Hr	0.07	91.22	91.27	91.27	91.29	0.044620	0.53	0.13	4.83	1.05
River 2	Reach 2	149	50YrSCS24Hr	0.08	91.22	91.28	91.28	91.29	0.037650	0.53	0.15	5.00	0.98
River 2	Reach 2	149	100YrSCS24Hr	0.09	91.22	91.28	91.28	91.30	0.038788	0.57	0.16	5.05	1.01
River 2	Reach 2	124	2YrCHI3Hr	0.02	90.90	91.04	90.93	91.04	0.000032	0.03	0.48	5.07	0.03
River 2	Reach 2	124	5YrCHI3Hr	0.03	90.90	91.05	90.93	91.05	0.000060	0.05	0.53	5.26	0.05
River 2	Reach 2	124	10YrCHI3Hr	0.03	90.90	91.06	90.94	91.06	0.000112	0.06	0.57	6.50	0.06
River 2	Reach 2	124	25YrCHI3Hr	0.05	90.90	91.07	90.95	91.07	0.000154	0.07	0.64	6.76	0.08
River 2	Reach 2	124	50YrCHI3Hr	0.06	90.90	91.09	90.95	91.09	0.000135	0.07	0.76	7.17	0.07
River 2	Reach 2	124	100YrCHI3Hr	0.07	90.90	91.14	90.95	91.14	0.000050	0.06	1.21	8.10	0.05
River 2	Reach 2	124	2YrSCS24Hr	0.02	90.90	91.05	90.93	91.05	0.000054	0.04	0.51	5.22	0.05
River 2	Reach 2	124	5YrSCS24Hr	0.04	90.90	91.06	90.94	91.06	0.000129	0.07	0.60	6.60	0.07
River 2	Reach 2	124	10YrSCS24Hr	0.05	90.90	91.07	90.95	91.07	0.000166	0.08	0.66	6.83	0.08
River 2	Reach 2	124	25YrSCS24Hr	0.07	90.90	91.12	90.95	91.12	0.000074	0.06	1.04	7.89	0.06
River 2	Reach 2	124	50YrSCS24Hr	0.08	90.90	91.19	90.96	91.19	0.000031	0.05	1.55	8.50	0.04
River 2	Reach 2	124	100YrSCS24Hr	0.09	90.90	91.25	90.96	91.25	0.000017	0.04	2.15	9.67	0.03
River 2	Reach 2	99	2YrCHI3Hr	0.02	90.90	91.04	90.92	91.04	0.000010	0.02	0.80	7.44	0.02
River 2	Reach 2	99	5YrCHI3Hr	0.03	90.90	91.05	90.92	91.05	0.000018	0.03	0.87	7.51	0.03
River 2	Reach 2	99	10YrCHI3Hr	0.03	90.90	91.06	90.93	91.06	0.000027	0.04	0.93	7.57	0.03
River 2	Reach 2	99	25YrCHI3Hr	0.05	90.90	91.07	90.93	91.07	0.000041	0.05	1.00	7.64	0.04
River 2	Reach 2	99	50YrCHI3Hr	0.06	90.90	91.09	90.94	91.09	0.000040	0.05	1.14	7.79	0.04
River 2	Reach 2	99	100YrCHI3Hr	0.07	90.90	91.14	90.94	91.14	0.000020	0.04	1.61	8.25	0.03
River 2	Reach 2	99	2YrSCS24Hr	0.02	90.90	91.05	90.92	91.05	0.000016	0.03	0.86	7.49	0.03
River 2	Reach 2	99	5YrSCS24Hr	0.04	90.90	91.06	90.93	91.06	0.000032	0.04	0.96	7.60	0.04
River 2	Reach 2	99	10YrSCS24Hr	0.05	90.90	91.07	90.94	91.07	0.000045	0.05	1.02	7.67	0.04
River 2	Reach 2	99	25YrSCS24Hr	0.07	90.90	91.12	90.94	91.12	0.000026	0.05	1.43	8.07	0.03
River 2	Reach 2	99	50YrSCS24Hr	0.08	90.90	91.19	90.94	91.19	0.000014	0.04	1.96	8.55	0.03
River 2	Reach 2	99	100YrSCS24Hr	0.09	90.90	91.25	90.95	91.25	0.000009	0.04	2.54	9.03	0.02
River 2	Reach 2	74	2YrCHI3Hr	0.02	90.89	91.04	90.91	91.04	0.000011	0.02	0.72	6.36	0.02
River 2	Reach 2	74	5YrCHI3Hr	0.03	90.89	91.05	90.92	91.05	0.000021	0.03	0.78	6.44	0.03
River 2	Reach 2	74	10YrCHI3Hr	0.03	90.89	91.06	90.92	91.06	0.000033	0.04	0.83	6.50	0.04
River 2	Reach 2	74	25YrCHI3Hr	0.05	90.89	91.07	90.93	91.07	0.000050	0.05	0.89	6.57	0.05
River 2	Reach 2	74	50YrCHI3Hr	0.06	90.89	91.08	90.93	91.08	0.000049	0.06	1.01	6.70	0.05
River 2	Reach 2	74	100YrCHI3Hr	0.07	90.89	91.14	90.93	91.14	0.000025	0.05	1.42	7.09	0.03
River 2	Reach 2	74	2YrSCS24Hr	0.02	90.89	91.05	90.92	91.05	0.000019	0.03	0.77	6.42	0.03
River 2	Reach 2	74	5YrSCS24Hr	0.04	90.89	91.06	90.92	91.06	0.000039	0.05	0.85	6.53	0.04
River 2	Reach 2	74	10YrSCS24Hr	0.05	90.89	91.07	90.93	91.07	0.000055	0.06	0.91	6.59	0.05
River 2	Reach 2	74	25YrSCS24Hr	0.07	90.89	91.12	90.93	91.12	0.000033	0.05	1.26	6.96	0.04
River 2	Reach 2	74	50YrSCS24Hr	0.08	90.89	91.18	90.93	91.18	0.000018	0.05	1.72	7.34	0.03
River 2	Reach 2	74	100YrSCS24Hr	0.09	90.89	91.25	90.94	91.25	0.000012	0.04	2.22	7.71	0.03

HEC-RAS Plan: 20250603-Pre_Dev_v01 (Continued)

River	Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
River 2	Reach 2	49	2YrCHI3Hr	0.02	91.00	91.03	91.03	91.04	0.048683	0.40	0.04	2.56	1.01
River 2	Reach 2	49	5YrCHI3Hr	0.03	91.00	91.04	91.04	91.05	0.045843	0.43	0.06	3.06	1.01
River 2	Reach 2	49	10YrCHI3Hr	0.03	91.00	91.04	91.04	91.05	0.036151	0.43	0.08	3.50	0.92
River 2	Reach 2	49	25YrCHI3Hr	0.05	91.00	91.05	91.05	91.06	0.042954	0.52	0.09	3.52	1.03
River 2	Reach 2	49	50YrCHI3Hr	0.06	91.00	91.08	91.05	91.08	0.005537	0.28	0.20	4.07	0.41
River 2	Reach 2	49	100YrCHI3Hr	0.07	91.00	91.14	91.05	91.14	0.000508	0.14	0.50	4.96	0.14
River 2	Reach 2	49	2YrSCS24Hr	0.02	91.00	91.04	91.04	91.04	0.038802	0.40	0.06	3.06	0.93
River 2	Reach 2	49	5YrSCS24Hr	0.04	91.00	91.04	91.04	91.06	0.043713	0.48	0.08	3.50	1.02
River 2	Reach 2	49	10YrSCS24Hr	0.05	91.00	91.05	91.05	91.06	0.037160	0.51	0.10	3.53	0.97
River 2	Reach 2	49	25YrSCS24Hr	0.07	91.00	91.12	91.05	91.12	0.001066	0.17	0.38	4.82	0.19
River 2	Reach 2	49	50YrSCS24Hr	0.08	91.00	91.18	91.06	91.18	0.000237	0.11	0.73	5.93	0.10
River 2	Reach 2	49	100YrSCS24Hr	0.09	91.00	91.25	91.06	91.25	0.000083	0.08	1.15	6.63	0.06
River 2	Reach 2	28	2YrCHI3Hr	0.02	90.69	90.78	90.74	90.78	0.001301	0.13	0.15	3.26	0.20
River 2	Reach 2	28	5YrCHI3Hr	0.03	90.69	90.85	90.75	90.85	0.000163	0.07	0.47	5.17	0.08
River 2	Reach 2	28	10YrCHI3Hr	0.05	90.69	90.93	90.75	90.93	0.000046	0.05	0.89	6.29	0.04
River 2	Reach 2	28	25YrCHI3Hr	0.06	90.69	91.01	90.76	91.01	0.000019	0.04	1.48	7.14	0.03
River 2	Reach 2	28	50YrCHI3Hr	0.08	90.69	91.08	90.77	91.08	0.000012	0.04	1.96	7.68	0.03
River 2	Reach 2	28	100YrCHI3Hr	0.09	90.69	91.14	90.78	91.14	0.000009	0.04	2.47	8.16	0.02
River 2	Reach 2	28	2YrSCS24Hr	0.03	90.69	90.83	90.74	90.83	0.000330	0.09	0.35	4.66	0.11
River 2	Reach 2	28	5YrSCS24Hr	0.05	90.69	90.95	90.76	90.95	0.000036	0.05	1.07	6.57	0.04
River 2	Reach 2	28	10YrSCS24Hr	0.07	90.69	91.03	90.76	91.03	0.000019	0.04	1.58	7.26	0.03
River 2	Reach 2	28	25YrSCS24Hr	0.09	90.69	91.12	90.78	91.12	0.000011	0.04	2.28	7.99	0.02
River 2	Reach 2	28	50YrSCS24Hr	0.11	90.69	91.18	90.78	91.18	0.000008	0.04	2.82	8.48	0.02
River 2	Reach 2	28	100YrSCS24Hr	0.13	90.69	91.25	90.79	91.25	0.000007	0.04	3.40	8.98	0.02
River 2	Reach 2	7	2YrCHI3Hr	0.02	90.67	90.73	90.71	90.74	0.003117	0.17	0.11	3.14	0.29
River 2	Reach 2	7	5YrCHI3Hr	0.03	90.67	90.85	90.72	90.85	0.000075	0.06	0.60	5.18	0.05
River 2	Reach 2	7	10YrCHI3Hr	0.05	90.67	90.92	90.73	90.92	0.000028	0.05	1.02	5.92	0.04
River 2	Reach 2	7	25YrCHI3Hr	0.06	90.67	91.01	90.73	91.01	0.000014	0.04	1.56	6.43	0.03
River 2	Reach 2	7	50YrCHI3Hr	0.08	90.67	91.08	90.74	91.08	0.000010	0.04	1.99	6.71	0.02
River 2	Reach 2	7	100YrCHI3Hr	0.09	90.67	91.14	90.74	91.14	0.000008	0.04	2.42	6.98	0.02
River 2	Reach 2	7	2YrSCS24Hr	0.03	90.67	90.82	90.72	90.82	0.000130	0.07	0.46	4.72	0.07
River 2	Reach 2	7	5YrSCS24Hr	0.05	90.67	90.95	90.73	90.95	0.000023	0.05	1.18	6.12	0.03
River 2	Reach 2	7	10YrSCS24Hr	0.07	90.67	91.03	90.73	91.03	0.000014	0.04	1.65	6.49	0.03
River 2	Reach 2	7	25YrSCS24Hr	0.09	90.67	91.12	90.74	91.12	0.000009	0.04	2.26	6.88	0.02
River 2	Reach 2	7	50YrSCS24Hr	0.11	90.67	91.18	90.75	91.18	0.000007	0.04	2.72	7.15	0.02
River 2	Reach 2	7	100YrSCS24Hr	0.13	90.67	91.25	90.75	91.25	0.000006	0.04	3.21	7.44	0.02
River 1	Reach 1-Upper	908	2YrCHI3Hr	0.02	94.14	94.22	94.18	94.22	0.001587	0.14	0.10	2.34	0.22
River 1	Reach 1-Upper	908	5YrCHI3Hr	0.03	94.14	94.23	94.19	94.23	0.001806	0.18	0.15	2.64	0.24
River 1	Reach 1-Upper	908	10YrCHI3Hr	0.03	94.14	94.24	94.20	94.24	0.002004	0.20	0.17	2.81	0.26
River 1	Reach 1-Upper	908	25YrCHI3Hr	0.05	94.14	94.25	94.20	94.26	0.002189	0.22	0.21	3.02	0.27
River 1	Reach 1-Upper	908	50YrCHI3Hr	0.06	94.14	94.26	94.21	94.27	0.002278	0.24	0.24	3.18	0.28
River 1	Reach 1-Upper	908	100YrCHI3Hr	0.07	94.14	94.27	94.21	94.27	0.002320	0.25	0.26	3.32	0.29
River 1	Reach 1-Upper	908	2YrSCS24Hr	0.02	94.14	94.23	94.19	94.23	0.001752	0.17	0.14	2.59	0.23
River 1	Reach 1-Upper	908	5YrSCS24Hr	0.04	94.14	94.25	94.20	94.25	0.002058	0.21	0.18	2.87	0.26
River 1	Reach 1-Upper	908	10YrSCS24Hr	0.05	94.14	94.26	94.20	94.26	0.002199	0.23	0.22	3.05	0.27
River 1	Reach 1-Upper	908	25YrSCS24Hr	0.06	94.14	94.27	94.21	94.27	0.002241	0.25	0.25	3.26	0.28
River 1	Reach 1-Upper	908	50YrSCS24Hr	0.07	94.14	94.28	94.22	94.28	0.002406	0.26	0.28	3.39	0.29
River 1	Reach 1-Upper	908	100YrSCS24Hr	0.08	94.14	94.29	94.22	94.29	0.002029	0.26	0.33	3.64	0.27
River 1	Reach 1-Upper	887	2YrCHI3Hr	0.02	94.10	94.15	94.14	94.16	0.007507	0.23	0.07	2.30	0.44
River 1	Reach 1-Upper	887	5YrCHI3Hr	0.03	94.10	94.17	94.15	94.17	0.005953	0.25	0.10	2.78	0.41
River 1	Reach 1-Upper	887	10YrCHI3Hr	0.03	94.10	94.18	94.15	94.18	0.005054	0.26	0.14	3.08	0.39
River 1	Reach 1-Upper	887	25YrCHI3Hr	0.05	94.10	94.19	94.16	94.20	0.004392	0.26	0.18	3.42	0.37
River 1	Reach 1-Upper	887	50YrCHI3Hr	0.06	94.10	94.20	94.17	94.20	0.004802	0.29	0.20	3.57	0.39
River 1	Reach 1-Upper	887	100YrCHI3Hr	0.07	94.10	94.21	94.17	94.21	0.004705	0.30	0.22	3.76	0.39
River 1	Reach 1-Upper	887	2YrSCS24Hr	0.02	94.10	94.17	94.15	94.17	0.006295	0.25	0.10	2.71	0.42
River 1	Reach 1-Upper	887	5YrSCS24Hr	0.04	94.10	94.18	94.15	94.19	0.004885	0.26	0.15	3.16	0.38
River 1	Reach 1-Upper	887	10YrSCS24Hr	0.05	94.10	94.19	94.16	94.20	0.004587	0.27	0.18	3.44	0.38
River 1	Reach 1-Upper	887	25YrSCS24Hr	0.06	94.10	94.20	94.17	94.20	0.005786	0.31	0.20	3.56	0.43
River 1	Reach 1-Upper	887	50YrSCS24Hr	0.07	94.10	94.21	94.17	94.22	0.003925	0.29	0.25	3.98	0.36
River 1	Reach 1-Upper	887	100YrSCS24Hr	0.08	94.10	94.19	94.18	94.20	0.014690	0.48	0.18	3.39	0.67
River 1	Reach 1-Upper	868	2YrCHI3Hr	0.02	93.96	94.02	94.01	94.03	0.006049	0.24	0.06	1.78	0.41
River 1	Reach 1-Upper	868	5YrCHI3Hr	0.03	93.96	94.04	94.01	94.04	0.007801	0.31	0.08	1.98	0.48
River 1	Reach 1-Upper	868	10YrCHI3Hr	0.03	93.96	94.04	94.02	94.05	0.010621	0.37	0.09	2.05	0.56
River 1	Reach 1-Upper	868	25YrCHI3Hr	0.05	93.96	94.05	94.03	94.06	0.013422	0.44	0.11	2.15	0.64
River 1	Reach 1-Upper	868	50YrCHI3Hr	0.06	93.96	94.06	94.04	94.07	0.010577	0.43	0.13	2.35	0.58
River 1	Reach 1-Upper	868	100YrCHI3Hr	0.07	93.96	94.06	94.04	94.07	0.010976	0.46	0.15	2.45	0.60
River 1	Reach 1-Upper	868	2YrSCS24Hr	0.02	93.96	94.03	94.01	94.04	0.007224	0.29	0.08	1.96	0.46
River 1	Reach 1-Upper	868	5YrSCS24Hr	0.04	93.96	94.04	94.02	94.05	0.011359	0.39	0.10	2.08	0.58
River 1	Reach 1-Upper	868	10YrSCS24Hr	0.05	93.96	94.05	94.03	94.06	0.012976	0.44	0.11	2.19	0.63
River 1	Reach 1-Upper	868	25YrSCS24Hr	0.06	93.96	94.07	94.04	94.08	0.007363	0.39	0.16	2.55	0.49
River 1	Reach 1-Upper	868	50YrSCS24Hr	0.07	93.96	94.06	94.05	94.07	0.019525	0.57	0.13	2.31	0.78
River 1	Reach 1-Upper	868	100YrSCS24Hr	0.08	93.96	94.14	94.05	94.15	0.001168	0.21	0.40	3.98	0.21
River 1	Reach 1-Upper	848	2YrCHI3Hr	0.02	93.87	93.92	93.90	93.92	0.004686	0.19	0.08	2.57	0.35
River 1	Reach 1-Upper	848	5YrCHI3Hr	0.03	93.87	93.93	93.91	93.94	0.003787	0.21	0.12	2.98	0.33
River 1	Reach 1-Upper	848	10YrCHI3Hr	0.03	93.87	93.95	93.92	93.95	0.002708	0.21	0.17	3.15	0.29
River 1	Reach 1-Upper	848	25YrCHI3Hr	0.05	93.87	93.97	93.92	93.97	0.002043	0.21	0.22	3.34	0.26
River 1	Reach 1-Upper	848	50YrCHI3Hr	0.06	93.87	93.97	93.93	93.97	0.002676	0.25	0.23	3.37	0.30
River 1	Reach 1-Upper	848	100YrCHI3Hr	0.07	93.87	93.98	93.93	93.98	0.002517	0.26	0.26	3.47	0.30
River 1	Reach 1-Upper	848	2YrSCS24Hr	0.02	93.87	93.93	93.91	93.93	0.004188	0.21	0.11	2.93	0.34
River 1	Reach 1-Upper	848	5YrSCS24Hr	0.04	93.87	93.95	93.92	93.96	0.002536	0.21	0.18	3.19	0.28
River 1	Reach 1-Upper	848	10YrSCS24Hr	0.05	93.87	93.97	93.92	93.97	0.002100	0.22	0.23	3.35	0.27
River 1	Reach 1-Upper	848	25YrSCS24Hr	0.06	93.87	93.96	93.93	93.97	0.004423	0.30	0.21	3.29	0.38
River 1	Reach 1-Upper	848	50YrSCS24Hr	0.07	93.87	94.04	93.93	94.04	0.000430	0.15	0.50	3.98	0.13

HEC-RAS Plan: 20250603-Pre_Dev_v01 (Continued)

River	Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
River 1	Reach 1-Upper	848	100YrSCS24Hr	0.08	93.87	94.14	93.94	94.14	0.000088	0.09	0.94	4.75	0.06
River 1	Reach 1-Upper	828	2YrCHI3Hr	0.02	93.78	93.85	93.82	93.85	0.002687	0.16	0.09	2.47	0.27
River 1	Reach 1-Upper	828	5YrCHI3Hr	0.03	93.78	93.86	93.83	93.86	0.004045	0.22	0.12	2.90	0.34
River 1	Reach 1-Upper	828	10YrCHI3Hr	0.03	93.78	93.85	93.83	93.86	0.010289	0.33	0.10	2.68	0.54
River 1	Reach 1-Upper	828	25YrCHI3Hr	0.05	93.78	93.84	93.84	93.86	0.040257	0.61	0.08	2.23	1.04
River 1	Reach 1-Upper	828	50YrCHI3Hr	0.06	93.78	93.87	93.85	93.87	0.011893	0.40	0.14	3.16	0.59
River 1	Reach 1-Upper	828	100YrCHI3Hr	0.07	93.78	93.96	93.85	93.97	0.000365	0.13	0.50	4.07	0.12
River 1	Reach 1-Upper	828	2YrSCS24Hr	0.02	93.78	93.86	93.82	93.86	0.003210	0.19	0.12	2.95	0.30
River 1	Reach 1-Upper	828	5YrSCS24Hr	0.04	93.78	93.85	93.84	93.86	0.014294	0.39	0.10	2.58	0.63
River 1	Reach 1-Upper	828	10YrSCS24Hr	0.05	93.78	93.84	93.84	93.86	0.036015	0.59	0.08	2.34	0.99
River 1	Reach 1-Upper	828	25YrSCS24Hr	0.06	93.78	93.90	93.85	93.90	0.002459	0.25	0.25	3.50	0.29
River 1	Reach 1-Upper	828	50YrSCS24Hr	0.07	93.78	94.04	93.86	94.04	0.000005	0.02	5.50	35.21	0.01
River 1	Reach 1-Upper	828	100YrSCS24Hr	0.08	93.78	94.14	93.86	94.14	0.000001	0.01	9.06	35.66	0.01
River 1	Reach 1-Upper	807	2YrCHI3Hr	0.02	93.65	93.70	93.70	93.71	0.039865	0.46	0.03	1.40	0.97
River 1	Reach 1-Upper	807	5YrCHI3Hr	0.03	93.65	93.72	93.71	93.73	0.011679	0.35	0.07	1.90	0.57
River 1	Reach 1-Upper	807	10YrCHI3Hr	0.03	93.65	93.76	93.71	93.76	0.002625	0.22	0.16	2.63	0.29
River 1	Reach 1-Upper	807	25YrCHI3Hr	0.05	93.65	93.80	93.72	93.80	0.000718	0.16	0.30	3.53	0.16
River 1	Reach 1-Upper	807	50YrCHI3Hr	0.06	93.65	93.86	93.73	93.86	0.000227	0.12	0.51	4.43	0.10
River 1	Reach 1-Upper	807	100YrCHI3Hr	0.07	93.65	93.96	93.73	93.96	0.000003	0.02	5.71	34.82	0.01
River 1	Reach 1-Upper	807	2YrSCS24Hr	0.02	93.65	93.71	93.70	93.72	0.021814	0.43	0.06	1.70	0.76
River 1	Reach 1-Upper	807	5YrSCS24Hr	0.04	93.65	93.77	93.71	93.77	0.001862	0.20	0.19	2.86	0.25
River 1	Reach 1-Upper	807	10YrSCS24Hr	0.05	93.65	93.81	93.72	93.81	0.000588	0.15	0.33	3.67	0.15
River 1	Reach 1-Upper	807	25YrSCS24Hr	0.06	93.65	93.89	93.73	93.89	0.000119	0.10	0.70	6.11	0.07
River 1	Reach 1-Upper	807	50YrSCS24Hr	0.07	93.65	94.04	93.74	94.04	0.000001	0.01	8.37	35.13	0.01
River 1	Reach 1-Upper	807	100YrSCS24Hr	0.08	93.65	94.14	93.74	94.14	0.000000	0.01	11.92	35.53	0.01
River 1	Reach 1-Upper	789	2YrCHI3Hr	0.02	93.49	93.67	93.53	93.67	0.000035	0.04	0.33	3.14	0.04
River 1	Reach 1-Upper	789	5YrCHI3Hr	0.03	93.49	93.72	93.54	93.72	0.000038	0.06	0.45	3.66	0.04
River 1	Reach 1-Upper	789	10YrCHI3Hr	0.03	93.49	93.76	93.55	93.76	0.000039	0.07	0.54	4.24	0.04
River 1	Reach 1-Upper	789	25YrCHI3Hr	0.05	93.49	93.80	93.56	93.80	0.000037	0.07	0.65	4.99	0.04
River 1	Reach 1-Upper	789	50YrCHI3Hr	0.06	93.49	93.86	93.57	93.86	0.000030	0.07	0.78	5.73	0.04
River 1	Reach 1-Upper	789	100YrCHI3Hr	0.07	93.49	93.96	93.57	93.96	0.000016	0.06	1.04	8.28	0.03
River 1	Reach 1-Upper	789	2YrSCS24Hr	0.02	93.49	93.71	93.54	93.71	0.000038	0.06	0.43	3.55	0.04
River 1	Reach 1-Upper	789	5YrSCS24Hr	0.04	93.49	93.77	93.55	93.77	0.000038	0.07	0.56	4.42	0.04
River 1	Reach 1-Upper	789	10YrSCS24Hr	0.05	93.49	93.81	93.56	93.81	0.000037	0.07	0.67	5.12	0.04
River 1	Reach 1-Upper	789	25YrSCS24Hr	0.06	93.49	93.89	93.57	93.89	0.000025	0.07	0.87	6.17	0.04
River 1	Reach 1-Upper	789	50YrSCS24Hr	0.07	93.49	94.04	93.57	94.04	0.000011	0.06	1.22	10.07	0.03
River 1	Reach 1-Upper	789	100YrSCS24Hr	0.08	93.49	94.14	93.58	94.14	0.000008	0.06	1.46	23.56	0.02
River 1	Reach 1-Upper	764		Culvert									
River 1	Reach 1-Upper	759	2YrCHI3Hr	0.02	93.46	93.53	93.50	93.53	0.002563	0.21	0.07	1.74	0.28
River 1	Reach 1-Upper	759	5YrCHI3Hr	0.03	93.46	93.56	93.51	93.56	0.002115	0.23	0.11	2.11	0.27
River 1	Reach 1-Upper	759	10YrCHI3Hr	0.03	93.46	93.59	93.52	93.60	0.001088	0.21	0.16	2.56	0.21
River 1	Reach 1-Upper	759	25YrCHI3Hr	0.05	93.46	93.66	93.53	93.66	0.000396	0.18	0.26	3.40	0.14
River 1	Reach 1-Upper	759	50YrCHI3Hr	0.06	93.46	93.74	93.54	93.74	0.000161	0.15	0.39	4.37	0.09
River 1	Reach 1-Upper	759	100YrCHI3Hr	0.07	93.46	93.83	93.54	93.84	0.000081	0.13	0.53	6.02	0.07
River 1	Reach 1-Upper	759	2YrSCS24Hr	0.02	93.46	93.55	93.51	93.56	0.002355	0.23	0.10	2.03	0.28
River 1	Reach 1-Upper	759	5YrSCS24Hr	0.04	93.46	93.61	93.52	93.61	0.000864	0.21	0.18	2.73	0.19
River 1	Reach 1-Upper	759	10YrSCS24Hr	0.05	93.46	93.67	93.53	93.67	0.000343	0.17	0.28	3.54	0.13
River 1	Reach 1-Upper	759	25YrSCS24Hr	0.06	93.46	93.79	93.54	93.79	0.000109	0.14	0.46	4.99	0.08
River 1	Reach 1-Upper	759	50YrSCS24Hr	0.07	93.46	93.89	93.54	93.89	0.000058	0.12	0.61	6.73	0.06
River 1	Reach 1-Upper	759	100YrSCS24Hr	0.08	93.46	93.95	93.55	93.95	0.000051	0.12	0.69	7.38	0.06
River 1	Reach 1-Upper	743	2YrCHI3Hr	0.02	93.40	93.47	93.45	93.47	0.006174	0.30	0.05	1.27	0.43
River 1	Reach 1-Upper	743	5YrCHI3Hr	0.03	93.40	93.53	93.46	93.54	0.001159	0.20	0.13	1.95	0.21
River 1	Reach 1-Upper	743	10YrCHI3Hr	0.03	93.40	93.58	93.47	93.58	0.000560	0.19	0.19	2.40	0.16
River 1	Reach 1-Upper	743	25YrCHI3Hr	0.05	93.40	93.66	93.48	93.66	0.000255	0.16	0.29	3.39	0.11
River 1	Reach 1-Upper	743	50YrCHI3Hr	0.06	93.40	93.74	93.49	93.74	0.000125	0.14	0.40	5.00	0.08
River 1	Reach 1-Upper	743	100YrCHI3Hr	0.07	93.40	93.83	93.50	93.83	0.000071	0.13	0.52	7.13	0.07
River 1	Reach 1-Upper	743	2YrSCS24Hr	0.02	93.40	93.52	93.46	93.52	0.001463	0.21	0.11	1.84	0.23
River 1	Reach 1-Upper	743	5YrSCS24Hr	0.04	93.40	93.60	93.47	93.60	0.000466	0.18	0.21	2.59	0.14
River 1	Reach 1-Upper	743	10YrSCS24Hr	0.05	93.40	93.67	93.48	93.67	0.000228	0.16	0.30	3.72	0.11
River 1	Reach 1-Upper	743	25YrSCS24Hr	0.06	93.40	93.79	93.49	93.79	0.000091	0.14	0.46	6.17	0.07
River 1	Reach 1-Upper	743	50YrSCS24Hr	0.07	93.40	93.89	93.50	93.89	0.000054	0.12	0.59	7.75	0.06
River 1	Reach 1-Upper	743	100YrSCS24Hr	0.08	93.40	93.94	93.51	93.95	0.000049	0.13	0.66	9.45	0.06
River 1	Reach 1-Upper	733		Culvert									
River 1	Reach 1-Upper	728	2YrCHI3Hr	0.02	93.33	93.46	93.38	93.46	0.000507	0.12	0.12	1.51	0.14
River 1	Reach 1-Upper	728	5YrCHI3Hr	0.03	93.33	93.52	93.40	93.52	0.000283	0.13	0.20	1.94	0.11
River 1	Reach 1-Upper	728	10YrCHI3Hr	0.03	93.33	93.56	93.41	93.56	0.000213	0.13	0.26	2.26	0.10
River 1	Reach 1-Upper	728	25YrCHI3Hr	0.05	93.33	93.63	93.42	93.63	0.000137	0.13	0.36	2.78	0.08
River 1	Reach 1-Upper	728	50YrCHI3Hr	0.06	93.33	93.70	93.43	93.70	0.000088	0.13	0.45	3.31	0.07
River 1	Reach 1-Upper	728	100YrCHI3Hr	0.07	93.33	93.78	93.43	93.78	0.000060	0.12	0.56	4.21	0.06
River 1	Reach 1-Upper	728	2YrSCS24Hr	0.02	93.33	93.51	93.39	93.51	0.000306	0.13	0.19	1.87	0.11
River 1	Reach 1-Upper	728	5YrSCS24Hr	0.04	93.33	93.58	93.41	93.58	0.000196	0.14	0.28	2.37	0.10
River 1	Reach 1-Upper	728	10YrSCS24Hr	0.05	93.33	93.64	93.42	93.64	0.000129	0.13	0.37	2.86	0.08
River 1	Reach 1-Upper	728	25YrSCS24Hr	0.06	93.33	93.74	93.43	93.74	0.000071	0.12	0.51	3.65	0.06
River 1	Reach 1-Upper	728	50YrSCS24Hr	0.07	93.33	93.82	93.44	93.82	0.000049	0.12	0.63	6.17	0.06
River 1	Reach 1-Upper	728	100YrSCS24Hr	0.08	93.33	93.85	93.45	93.85	0.000053	0.13	0.67	10.91	0.06
River 1	Reach 1-Upper	715	2YrCHI3Hr	0.02	93.32	93.46	93.36	93.46	0.000165	0.09	0.17	2.22	0.08
River 1	Reach 1-Upper	715	5YrCHI3Hr	0.03	93.32	93.52	93.37	93.52	0.000134	0.10	0.25	2.80	0.08
River 1	Reach 1-Upper	715	10YrCHI3Hr	0.03	93.32	93.56	93.38	93.56	0.000117	0.11	0.31	3.23	0.08
River 1	Reach 1-Upper	715	25YrCHI3Hr	0.05	93.32	93.63	93.39	93.63	0.000086	0.12	0.41	3.92	0.07
River 1	Reach 1-Upper	715	50YrCHI3Hr	0.06	93.32	93.70	93.39	93.70	0.000061	0.11	0.51	4.63	0.06
River 1	Reach 1-Upper	715	100YrCHI3Hr	0.07	93.32	93.77	93.40	93.78	0.000044	0.11	0.61	9.10	0.05

HEC-RAS Plan: 20250603-Pre_Dev_v01 (Continued)

River	Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
River 1	Reach 1-Upper	715	2YrSCS24Hr	0.02	93.32	93.51	93.36	93.51	0.000138	0.10	0.24	2.70	0.08
River 1	Reach 1-Upper	715	5YrSCS24Hr	0.04	93.32	93.57	93.38	93.57	0.000112	0.11	0.33	3.38	0.08
River 1	Reach 1-Upper	715	10YrSCS24Hr	0.05	93.32	93.64	93.39	93.64	0.000083	0.12	0.42	4.03	0.07
River 1	Reach 1-Upper	715	25YrSCS24Hr	0.06	93.32	93.74	93.40	93.74	0.000051	0.11	0.56	5.03	0.06
River 1	Reach 1-Upper	715	50YrSCS24Hr	0.07	93.32	93.82	93.40	93.82	0.000037	0.11	0.68	14.68	0.05
River 1	Reach 1-Upper	715	100YrSCS24Hr	0.08	93.32	93.85	93.41	93.85	0.000010	0.04	2.56	20.21	0.02
River 1	Reach 1-Upper	705	Culvert										
River 1	Reach 1-Upper	698	2YrCHI3Hr	0.02	93.24	93.31	93.29	93.31	0.009120	0.33	0.05	1.10	0.51
River 1	Reach 1-Upper	698	5YrCHI3Hr	0.03	93.24	93.31	93.30	93.32	0.019233	0.50	0.05	1.16	0.75
River 1	Reach 1-Upper	698	10YrCHI3Hr	0.03	93.24	93.31	93.31	93.33	0.027628	0.62	0.06	1.19	0.91
River 1	Reach 1-Upper	698	25YrCHI3Hr	0.05	93.24	93.42	93.32	93.43	0.000867	0.20	0.23	2.01	0.19
River 1	Reach 1-Upper	698	50YrCHI3Hr	0.06	93.24	93.51	93.33	93.51	0.000225	0.14	0.41	2.80	0.10
River 1	Reach 1-Upper	698	100YrCHI3Hr	0.07	93.24	93.51	93.34	93.51	0.000299	0.16	0.42	2.61	0.12
River 1	Reach 1-Upper	698	2YrSCS24Hr	0.02	93.24	93.31	93.30	93.32	0.015768	0.45	0.05	1.16	0.68
River 1	Reach 1-Upper	698	5YrSCS24Hr	0.04	93.24	93.32	93.31	93.34	0.027115	0.63	0.06	1.22	0.90
River 1	Reach 1-Upper	698	10YrSCS24Hr	0.05	93.24	93.47	93.32	93.47	0.000368	0.15	0.32	2.29	0.13
River 1	Reach 1-Upper	698	25YrSCS24Hr	0.06	93.24	93.51	93.33	93.51	0.000261	0.15	0.41	2.61	0.11
River 1	Reach 1-Upper	698	50YrSCS24Hr	0.07	93.24	93.51	93.34	93.52	0.000345	0.17	0.42	2.63	0.13
River 1	Reach 1-Upper	698	100YrSCS24Hr	0.08	93.24	93.52	93.35	93.52	0.000432	0.20	0.43	2.65	0.14
River 1	Reach 1-Upper	681	2YrCHI3Hr	0.02	93.14	93.21	93.18	93.21	0.004396	0.23	0.07	1.57	0.36
River 1	Reach 1-Upper	681	5YrCHI3Hr	0.03	93.14	93.24	93.19	93.24	0.001938	0.21	0.12	1.83	0.26
River 1	Reach 1-Upper	681	10YrCHI3Hr	0.03	93.14	93.27	93.20	93.27	0.001159	0.19	0.18	2.04	0.21
River 1	Reach 1-Upper	681	25YrCHI3Hr	0.05	93.14	93.42	93.21	93.42	0.000083	0.08	0.57	3.09	0.06
River 1	Reach 1-Upper	681	50YrCHI3Hr	0.06	93.14	93.51	93.22	93.51	0.000037	0.07	0.87	4.07	0.04
River 1	Reach 1-Upper	681	100YrCHI3Hr	0.07	93.14	93.51	93.22	93.51	0.000050	0.08	0.88	4.10	0.05
River 1	Reach 1-Upper	681	2YrSCS24Hr	0.02	93.14	93.23	93.19	93.24	0.002334	0.22	0.11	1.78	0.28
River 1	Reach 1-Upper	681	5YrSCS24Hr	0.04	93.14	93.29	93.20	93.29	0.000854	0.18	0.21	2.14	0.18
River 1	Reach 1-Upper	681	10YrSCS24Hr	0.05	93.14	93.46	93.21	93.46	0.000050	0.07	0.70	3.45	0.05
River 1	Reach 1-Upper	681	25YrSCS24Hr	0.06	93.14	93.51	93.22	93.51	0.000043	0.07	0.88	4.08	0.05
River 1	Reach 1-Upper	681	50YrSCS24Hr	0.07	93.14	93.51	93.23	93.51	0.000058	0.08	0.89	4.12	0.05
River 1	Reach 1-Upper	681	100YrSCS24Hr	0.08	93.14	93.52	93.23	93.52	0.000073	0.09	0.90	4.16	0.06
River 1	Reach 1-Upper	663	2YrCHI3Hr	0.02	93.05	93.18		93.18	0.000677	0.14	0.11	1.31	0.15
River 1	Reach 1-Upper	663	5YrCHI3Hr	0.03	93.05	93.22		93.23	0.000607	0.15	0.17	1.60	0.15
River 1	Reach 1-Upper	663	10YrCHI3Hr	0.03	93.05	93.26		93.26	0.000492	0.15	0.23	1.84	0.14
River 1	Reach 1-Upper	663	25YrCHI3Hr	0.05	93.05	93.42		93.42	0.000064	0.07	0.63	3.25	0.05
River 1	Reach 1-Upper	663	50YrCHI3Hr	0.06	93.05	93.51		93.51	0.000032	0.06	0.96	4.42	0.04
River 1	Reach 1-Upper	663	100YrCHI3Hr	0.07	93.05	93.51		93.51	0.000043	0.07	0.97	4.46	0.05
River 1	Reach 1-Upper	663	2YrSCS24Hr	0.02	93.05	93.21		93.22	0.000676	0.16	0.15	1.53	0.16
River 1	Reach 1-Upper	663	5YrSCS24Hr	0.04	93.05	93.28		93.28	0.000393	0.14	0.26	1.97	0.13
River 1	Reach 1-Upper	663	10YrSCS24Hr	0.05	93.05	93.46		93.46	0.000042	0.06	0.78	3.77	0.04
River 1	Reach 1-Upper	663	25YrSCS24Hr	0.06	93.05	93.51		93.51	0.000037	0.06	0.96	4.44	0.04
River 1	Reach 1-Upper	663	50YrSCS24Hr	0.07	93.05	93.51		93.51	0.000050	0.08	0.97	4.48	0.05
River 1	Reach 1-Upper	663	100YrSCS24Hr	0.08	93.05	93.51		93.52	0.000064	0.09	0.99	4.53	0.06
River 1	Reach 1-Upper	656	2YrCHI3Hr	0.06	93.03	93.15	93.12	93.16	0.008107	0.46	0.12	1.65	0.53
River 1	Reach 1-Upper	656	5YrCHI3Hr	0.10	93.03	93.19	93.14	93.20	0.006746	0.51	0.20	1.91	0.51
River 1	Reach 1-Upper	656	10YrCHI3Hr	0.14	93.03	93.23	93.16	93.24	0.004212	0.48	0.29	2.15	0.42
River 1	Reach 1-Upper	656	25YrCHI3Hr	0.18	93.03	93.42	93.18	93.42	0.000424	0.23	0.79	3.69	0.15
River 1	Reach 1-Upper	656	50YrCHI3Hr	0.22	93.03	93.51	93.20	93.51	0.000220	0.20	1.16	4.65	0.11
River 1	Reach 1-Upper	656	100YrCHI3Hr	0.26	93.03	93.51	93.21	93.51	0.000302	0.24	1.17	4.66	0.13
River 1	Reach 1-Upper	656	2YrSCS24Hr	0.09	93.03	93.18	93.14	93.19	0.007190	0.50	0.18	1.85	0.52
River 1	Reach 1-Upper	656	5YrSCS24Hr	0.15	93.03	93.26	93.17	93.27	0.003060	0.44	0.34	2.29	0.36
River 1	Reach 1-Upper	656	10YrSCS24Hr	0.19	93.03	93.46	93.18	93.46	0.000269	0.21	0.96	4.20	0.12
River 1	Reach 1-Upper	656	25YrSCS24Hr	0.24	93.03	93.51	93.20	93.51	0.000267	0.23	1.17	4.65	0.12
River 1	Reach 1-Upper	656	50YrSCS24Hr	0.28	93.03	93.51	93.22	93.51	0.000363	0.26	1.17	4.66	0.14
River 1	Reach 1-Upper	656	100YrSCS24Hr	0.33	93.03	93.51	93.23	93.51	0.000481	0.30	1.18	4.68	0.16
River 1	Reach 1-Upper	638	2YrCHI3Hr	0.06	92.92	93.07	93.00	93.08	0.002802	0.32	0.18	1.81	0.32
River 1	Reach 1-Upper	638	5YrCHI3Hr	0.10	92.92	93.14	93.04	93.14	0.001935	0.33	0.31	2.24	0.28
River 1	Reach 1-Upper	638	10YrCHI3Hr	0.14	92.92	93.20	93.05	93.21	0.001072	0.29	0.48	2.76	0.22
River 1	Reach 1-Upper	638	25YrCHI3Hr	0.18	92.92	93.41	93.07	93.42	0.000128	0.15	1.31	5.26	0.08
River 1	Reach 1-Upper	638	50YrCHI3Hr	0.22	92.92	93.50	93.09	93.51	0.000082	0.14	1.86	6.83	0.07
River 1	Reach 1-Upper	638	100YrCHI3Hr	0.26	92.92	93.50	93.10	93.51	0.000114	0.16	1.86	6.84	0.08
River 1	Reach 1-Upper	638	2YrSCS24Hr	0.09	92.92	93.12	93.03	93.12	0.002288	0.34	0.27	2.11	0.30
River 1	Reach 1-Upper	638	5YrSCS24Hr	0.15	92.92	93.24	93.06	93.24	0.000804	0.26	0.57	3.07	0.19
River 1	Reach 1-Upper	638	10YrSCS24Hr	0.19	92.92	93.46	93.08	93.46	0.000092	0.14	1.57	6.15	0.07
River 1	Reach 1-Upper	638	25YrSCS24Hr	0.24	92.92	93.50	93.10	93.51	0.000100	0.15	1.86	6.83	0.08
River 1	Reach 1-Upper	638	50YrSCS24Hr	0.28	92.92	93.50	93.11	93.51	0.000137	0.18	1.87	6.84	0.09
River 1	Reach 1-Upper	638	100YrSCS24Hr	0.33	92.92	93.51	93.13	93.51	0.000184	0.20	1.87	6.85	0.10
River 1	Reach 1-Upper	617	2YrCHI3Hr	0.06	92.84	93.01	92.95	93.01	0.003253	0.32	0.18	1.96	0.34
River 1	Reach 1-Upper	617	5YrCHI3Hr	0.10	92.84	93.11	92.98	93.11	0.000952	0.24	0.43	2.97	0.20
River 1	Reach 1-Upper	617	10YrCHI3Hr	0.14	92.84	93.19	93.00	93.19	0.000453	0.19	0.70	3.82	0.14
River 1	Reach 1-Upper	617	25YrCHI3Hr	0.18	92.84	93.41	93.01	93.41	0.000070	0.09	1.97	8.09	0.06
River 1	Reach 1-Upper	617	50YrCHI3Hr	0.22	92.84	93.50	93.03	93.50	0.000037	0.08	2.93	15.17	0.05
River 1	Reach 1-Upper	617	100YrCHI3Hr	0.26	92.84	93.50	93.04	93.50	0.000051	0.09	2.93	15.17	0.05
River 1	Reach 1-Upper	617	2YrSCS24Hr	0.09	92.84	93.08	92.97	93.09	0.001277	0.26	0.35	2.70	0.23
River 1	Reach 1-Upper	617	5YrSCS24Hr	0.15	92.84	93.23	93.00	93.23	0.000340	0.18	0.84	4.32	0.13
River 1	Reach 1-Upper	617	10YrSCS24Hr	0.19	92.84	93.46	93.02	93.46	0.000046	0.08	2.37	10.22	0.05
River 1	Reach 1-Upper	617	25YrSCS24Hr	0.24	92.84	93.50	93.04	93.50	0.000045	0.09	2.93	15.17	0.05
River 1	Reach 1-Upper	617	50YrSCS24Hr	0.28	92.84	93.50	93.05	93.50	0.000062	0.10	2.93	15.17	0.06
River 1	Reach 1-Upper	617	100YrSCS24Hr	0.33	92.84	93.50	93.06	93.50	0.000083	0.12	2.93	15.18	0.07
River 1	Reach 1-Upper	598	2YrCHI3Hr	0.06	92.76	92.99	92.86	92.99	0.000555	0.18	0.33	2.52	0.15
River 1	Reach 1-Upper	598	5YrCHI3Hr	0.11	92.76	93.10	92.89	93.10	0.000269	0.18	0.61	3.40	0.12
River 1	Reach 1-Upper	598	10YrCHI3Hr	0.15	92.76	93.19	92.91	93.19	0.000175	0.18	0.82	5.45	0.10

HEC-RAS Plan: 20250603-Pre_Dev_v01 (Continued)

River	Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
River 1	Reach 1-Upper	598	25YrCHI3Hr	0.19	92.76	93.41	92.93	93.41	0.000054	0.14	1.39	9.84	0.06
River 1	Reach 1-Upper	598	50YrCHI3Hr	0.23	92.76	93.50	92.94	93.50	0.000020	0.08	4.94	31.21	0.04
River 1	Reach 1-Upper	598	100YrCHI3Hr	0.28	92.76	93.50	92.96	93.50	0.000028	0.09	4.93	31.21	0.04
River 1	Reach 1-Upper	598	2YrSCS24Hr	0.10	92.76	93.07	92.88	93.07	0.000322	0.18	0.53	3.17	0.12
River 1	Reach 1-Upper	598	5YrSCS24Hr	0.16	92.76	93.22	92.91	93.22	0.000147	0.17	0.91	6.16	0.09
River 1	Reach 1-Upper	598	10YrSCS24Hr	0.20	92.76	93.46	92.93	93.46	0.000045	0.13	1.50	22.56	0.06
River 1	Reach 1-Upper	598	25YrSCS24Hr	0.26	92.76	93.50	92.95	93.50	0.000025	0.09	4.94	31.21	0.04
River 1	Reach 1-Upper	598	50YrSCS24Hr	0.30	92.76	93.50	92.96	93.50	0.000034	0.10	4.93	31.21	0.05
River 1	Reach 1-Upper	598	100YrSCS24Hr	0.35	92.76	93.50	92.98	93.50	0.000046	0.12	4.93	31.21	0.05
River 1	Reach 1-Upper	589		Culvert									
River 1	Reach 1-Upper	581	2YrCHI3Hr	0.06	92.71	92.89	92.81	92.89	0.002032	0.27	0.23	2.59	0.28
River 1	Reach 1-Upper	581	5YrCHI3Hr	0.11	92.71	92.93	92.84	92.93	0.001970	0.33	0.33	3.40	0.29
River 1	Reach 1-Upper	581	10YrCHI3Hr	0.15	92.71	92.96	92.86	92.97	0.001571	0.34	0.42	4.10	0.27
River 1	Reach 1-Upper	581	25YrCHI3Hr	0.19	92.71	93.04	92.88	93.04	0.000858	0.32	0.60	5.44	0.21
River 1	Reach 1-Upper	581	50YrCHI3Hr	0.23	92.71	93.19	92.89	93.19	0.000244	0.24	0.98	9.64	0.12
River 1	Reach 1-Upper	581	100YrCHI3Hr	0.28	92.71	93.25	92.90	93.25	0.000213	0.24	1.13	30.32	0.12
River 1	Reach 1-Upper	581	2YrSCS24Hr	0.10	92.71	92.92	92.83	92.92	0.002062	0.32	0.30	3.18	0.29
River 1	Reach 1-Upper	581	5YrSCS24Hr	0.16	92.71	92.98	92.86	92.99	0.001381	0.34	0.46	4.41	0.25
River 1	Reach 1-Upper	581	10YrSCS24Hr	0.20	92.71	93.05	92.88	93.06	0.000735	0.31	0.65	5.75	0.20
River 1	Reach 1-Upper	581	25YrSCS24Hr	0.26	92.71	93.25	92.90	93.25	0.000187	0.23	1.13	30.32	0.11
River 1	Reach 1-Upper	581	50YrSCS24Hr	0.30	92.71	93.26	92.91	93.26	0.000245	0.26	1.15	30.62	0.12
River 1	Reach 1-Upper	581	100YrSCS24Hr	0.35	92.71	93.30	92.92	93.30	0.000057	0.11	4.83	35.67	0.06
River 1	Reach 1-Upper	572	2YrCHI3Hr	0.06	92.73	92.84	92.82	92.85	0.009130	0.45	0.13	1.96	0.55
River 1	Reach 1-Upper	572	5YrCHI3Hr	0.11	92.73	92.90	92.84	92.90	0.004896	0.43	0.26	2.58	0.43
River 1	Reach 1-Upper	572	10YrCHI3Hr	0.15	92.73	92.94	92.86	92.95	0.002649	0.37	0.39	3.10	0.33
River 1	Reach 1-Upper	572	25YrCHI3Hr	0.19	92.73	93.03	92.88	93.03	0.001021	0.28	0.70	4.09	0.22
River 1	Reach 1-Upper	572	50YrCHI3Hr	0.23	92.73	93.19	92.89	93.19	0.000155	0.14	2.22	26.73	0.09
River 1	Reach 1-Upper	572	100YrCHI3Hr	0.28	92.73	93.25	92.90	93.25	0.000074	0.11	4.09	35.89	0.06
River 1	Reach 1-Upper	572	2YrSCS24Hr	0.10	92.73	92.88	92.84	92.89	0.005898	0.44	0.22	2.42	0.47
River 1	Reach 1-Upper	572	5YrSCS24Hr	0.16	92.73	92.96	92.86	92.97	0.002084	0.34	0.46	3.34	0.30
River 1	Reach 1-Upper	572	10YrSCS24Hr	0.20	92.73	93.05	92.88	93.05	0.000824	0.26	0.78	4.31	0.20
River 1	Reach 1-Upper	572	25YrSCS24Hr	0.26	92.73	93.25	92.90	93.25	0.000065	0.10	4.09	35.88	0.06
River 1	Reach 1-Upper	572	50YrSCS24Hr	0.30	92.73	93.26	92.91	93.26	0.000079	0.12	4.37	36.88	0.07
River 1	Reach 1-Upper	572	100YrSCS24Hr	0.35	92.73	93.30	92.92	93.30	0.000050	0.10	6.26	42.85	0.05
River 1	Reach 1-Upper	555	2YrCHI3Hr	0.06	92.61	92.81	92.71	92.81	0.000983	0.20	0.31	2.93	0.20
River 1	Reach 1-Upper	555	5YrCHI3Hr	0.11	92.61	92.87	92.74	92.87	0.000748	0.21	0.52	3.73	0.18
River 1	Reach 1-Upper	555	10YrCHI3Hr	0.15	92.61	92.93	92.75	92.93	0.000479	0.19	0.76	4.46	0.15
River 1	Reach 1-Upper	555	25YrCHI3Hr	0.19	92.61	93.02	92.77	93.02	0.000238	0.16	1.22	5.62	0.11
River 1	Reach 1-Upper	555	50YrCHI3Hr	0.23	92.61	93.19	92.78	93.19	0.000031	0.08	4.98	37.27	0.04
River 1	Reach 1-Upper	555	100YrCHI3Hr	0.28	92.61	93.25	92.80	93.25	0.000018	0.06	7.39	40.94	0.03
River 1	Reach 1-Upper	555	2YrSCS24Hr	0.10	92.61	92.85	92.73	92.85	0.000851	0.21	0.45	3.50	0.19
River 1	Reach 1-Upper	555	5YrSCS24Hr	0.16	92.61	92.95	92.76	92.95	0.000402	0.18	0.87	4.75	0.14
River 1	Reach 1-Upper	555	10YrSCS24Hr	0.20	92.61	93.04	92.77	93.04	0.000197	0.15	1.34	5.96	0.10
River 1	Reach 1-Upper	555	25YrSCS24Hr	0.26	92.61	93.25	92.79	93.25	0.000016	0.06	7.39	40.94	0.03
River 1	Reach 1-Upper	555	50YrSCS24Hr	0.30	92.61	93.26	92.81	93.26	0.000020	0.07	7.70	41.13	0.03
River 1	Reach 1-Upper	555	100YrSCS24Hr	0.35	92.61	93.30	92.82	93.30	0.000015	0.06	9.71	43.21	0.03
River 1	Reach 1-Upper	534	2YrCHI3Hr	0.06	92.59	92.78	92.69	92.78	0.001540	0.24	0.25	2.41	0.24
River 1	Reach 1-Upper	534	5YrCHI3Hr	0.11	92.59	92.85	92.72	92.86	0.001007	0.24	0.46	3.30	0.21
River 1	Reach 1-Upper	534	10YrCHI3Hr	0.15	92.59	92.92	92.74	92.92	0.000570	0.21	0.74	8.51	0.16
River 1	Reach 1-Upper	534	25YrCHI3Hr	0.19	92.59	93.02	92.76	93.02	0.000095	0.11	3.36	40.28	0.07
River 1	Reach 1-Upper	534	50YrCHI3Hr	0.23	92.59	93.19	92.78	93.19	0.000006	0.04	11.46	51.16	0.02
River 1	Reach 1-Upper	534	100YrCHI3Hr	0.28	92.59	93.25	92.79	93.25	0.000004	0.03	14.61	51.39	0.02
River 1	Reach 1-Upper	534	2YrSCS24Hr	0.10	92.59	92.83	92.71	92.83	0.001214	0.25	0.39	3.03	0.22
River 1	Reach 1-Upper	534	5YrSCS24Hr	0.16	92.59	92.94	92.75	92.95	0.000422	0.19	1.07	17.97	0.14
River 1	Reach 1-Upper	534	10YrSCS24Hr	0.20	92.59	93.04	92.76	93.04	0.000064	0.09	4.23	42.61	0.06
River 1	Reach 1-Upper	534	25YrSCS24Hr	0.26	92.59	93.25	92.78	93.25	0.000003	0.03	14.61	51.39	0.01
River 1	Reach 1-Upper	534	50YrSCS24Hr	0.30	92.59	93.26	92.80	93.26	0.000004	0.03	14.99	51.42	0.02
River 1	Reach 1-Upper	534	100YrSCS24Hr	0.35	92.59	93.30	92.81	93.30	0.000004	0.03	17.46	51.60	0.02
River 1	Reach 1-Upper	510	2YrCHI3Hr	0.06	92.60	92.71	92.67	92.72	0.005825	0.43	0.14	2.60	0.46
River 1	Reach 1-Upper	510	5YrCHI3Hr	0.11	92.60	92.82	92.70	92.83	0.001169	0.34	0.32	4.18	0.24
River 1	Reach 1-Upper	510	10YrCHI3Hr	0.15	92.60	92.90	92.72	92.90	0.000712	0.32	0.45	5.29	0.20
River 1	Reach 1-Upper	510	25YrCHI3Hr	0.19	92.60	93.01	92.73	93.01	0.000421	0.31	0.62	14.09	0.16
River 1	Reach 1-Upper	510	50YrCHI3Hr	0.23	92.60	93.18	92.75	93.19	0.000180	0.26	0.90	109.29	0.11
River 1	Reach 1-Upper	510	100YrCHI3Hr	0.28	92.60	93.25	92.77	93.25	0.000000	0.01	42.37	109.53	0.00
River 1	Reach 1-Upper	510	2YrSCS24Hr	0.10	92.60	92.79	92.69	92.80	0.001503	0.34	0.28	3.79	0.26
River 1	Reach 1-Upper	510	5YrSCS24Hr	0.16	92.60	92.93	92.72	92.93	0.000617	0.32	0.49	5.78	0.19
River 1	Reach 1-Upper	510	10YrSCS24Hr	0.20	92.60	93.03	92.74	93.04	0.000378	0.31	0.66	15.54	0.15
River 1	Reach 1-Upper	510	25YrSCS24Hr	0.26	92.60	93.25	92.76	93.25	0.000000	0.01	42.37	109.53	0.00
River 1	Reach 1-Upper	510	50YrSCS24Hr	0.30	92.60	93.26	92.78	93.26	0.000000	0.01	43.19	109.55	0.01
River 1	Reach 1-Upper	510	100YrSCS24Hr	0.35	92.60	93.30	92.79	93.30	0.000000	0.01	48.45	109.72	0.00
River 1	Reach 1-Upper	505		Culvert									
River 1	Reach 1-Upper	502	2YrCHI3Hr	0.07	92.49	92.60	92.57	92.61	0.007956	0.50	0.13	2.20	0.54
River 1	Reach 1-Upper	502	5YrCHI3Hr	0.12	92.49	92.65	92.60	92.67	0.006462	0.60	0.20	2.74	0.52
River 1	Reach 1-Upper	502	10YrCHI3Hr	0.16	92.49	92.68	92.62	92.70	0.006042	0.66	0.25	3.06	0.52
River 1	Reach 1-Upper	502	25YrCHI3Hr	0.22	92.49	92.73	92.64	92.76	0.004047	0.66	0.33	4.01	0.45
River 1	Reach 1-Upper	502	50YrCHI3Hr	0.26	92.49	92.83	92.66	92.85	0.001665	0.54	0.48	5.45	0.31
River 1	Reach 1-Upper	502	100YrCHI3Hr	0.31	92.49	92.99	92.68	93.00	0.000619	0.43	0.72	104.79	0.20
River 1	Reach 1-Upper	502	2YrSCS24Hr	0.11	92.49	92.64	92.59	92.65	0.006729	0.58	0.19	2.62	0.53
River 1	Reach 1-Upper	502	5YrSCS24Hr	0.18	92.49	92.69	92.63	92.71	0.005546	0.67	0.27	3.21	0.51
River 1	Reach 1-Upper	502	10YrSCS24Hr	0.23	92.49	92.75	92.65	92.77	0.003381	0.64	0.36	4.41	0.42
River 1	Reach 1-Upper	502	25YrSCS24Hr	0.29	92.49	92.92	92.67	92.94	0.000902	0.47	0.62	7.34	0.24
River 1	Reach 1-Upper	502	50YrSCS24Hr	0.34	92.49	93.11	92.69	93.12	0.000353	0.38	0.90	105.15	0.16

HEC-RAS Plan: 20250603-Pre_Dev_v01 (Continued)

River	Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
River 1	Reach 1-Upper	502	100YrSCS24Hr	0.40	92.49	93.30	92.71	93.30	0.000000	0.01	51.89	105.65	0.00
River 1	Reach 1-Upper	493	2YrCHI3Hr	0.07	92.34	92.60	92.42	92.60	0.000124	0.09	0.72	4.59	0.07
River 1	Reach 1-Upper	493	5YrCHI3Hr	0.12	92.34	92.65	92.45	92.65	0.000198	0.13	0.96	5.44	0.10
River 1	Reach 1-Upper	493	10YrCHI3Hr	0.16	92.34	92.68	92.46	92.68	0.000233	0.14	1.13	5.98	0.10
River 1	Reach 1-Upper	493	25YrCHI3Hr	0.22	92.34	92.74	92.48	92.74	0.000196	0.14	1.51	6.84	0.10
River 1	Reach 1-Upper	493	50YrCHI3Hr	0.26	92.34	92.84	92.49	92.84	0.000098	0.12	2.27	8.59	0.07
River 1	Reach 1-Upper	493	100YrCHI3Hr	0.31	92.34	93.00	92.50	93.00	0.000001	0.02	28.79	101.37	0.01
River 1	Reach 1-Upper	493	2YrSCS24Hr	0.11	92.34	92.64	92.44	92.64	0.000183	0.12	0.90	5.23	0.09
River 1	Reach 1-Upper	493	5YrSCS24Hr	0.18	92.34	92.70	92.46	92.70	0.000231	0.15	1.22	6.23	0.11
River 1	Reach 1-Upper	493	10YrSCS24Hr	0.23	92.34	92.76	92.48	92.76	0.000169	0.14	1.63	7.02	0.09
River 1	Reach 1-Upper	493	25YrSCS24Hr	0.29	92.34	92.93	92.50	92.93	0.000047	0.09	3.20	13.20	0.05
River 1	Reach 1-Upper	493	50YrSCS24Hr	0.34	92.34	93.12	92.51	93.12	0.000001	0.01	41.12	102.01	0.01
River 1	Reach 1-Upper	493	100YrSCS24Hr	0.40	92.34	93.30	92.52	93.30	0.000000	0.01	60.16	102.98	0.00
River 1	Reach 1-Upper	474	2YrCHI3Hr	0.07	92.41	92.60	92.50	92.60	0.000594	0.14	0.47	4.97	0.15
River 1	Reach 1-Upper	474	5YrCHI3Hr	0.12	92.41	92.64	92.53	92.65	0.000595	0.17	0.72	5.95	0.16
River 1	Reach 1-Upper	474	10YrCHI3Hr	0.16	92.41	92.67	92.54	92.68	0.000563	0.18	0.90	6.59	0.15
River 1	Reach 1-Upper	474	25YrCHI3Hr	0.22	92.41	92.73	92.56	92.74	0.000352	0.16	1.33	7.87	0.13
River 1	Reach 1-Upper	474	50YrCHI3Hr	0.26	92.41	92.84	92.57	92.84	0.000001	0.01	25.75	91.49	0.01
River 1	Reach 1-Upper	474	100YrCHI3Hr	0.31	92.41	93.00	92.58	93.00	0.000000	0.01	40.12	92.20	0.01
River 1	Reach 1-Upper	474	2YrSCS24Hr	0.11	92.41	92.63	92.52	92.63	0.000605	0.16	0.65	5.71	0.16
River 1	Reach 1-Upper	474	5YrSCS24Hr	0.18	92.41	92.69	92.55	92.69	0.000512	0.18	1.00	6.89	0.15
River 1	Reach 1-Upper	474	10YrSCS24Hr	0.23	92.41	92.75	92.56	92.75	0.000285	0.15	1.49	8.28	0.12
River 1	Reach 1-Upper	474	25YrSCS24Hr	0.29	92.41	92.93	92.57	92.93	0.000001	0.01	33.86	91.89	0.01
River 1	Reach 1-Upper	474	50YrSCS24Hr	0.34	92.41	93.12	92.58	93.12	0.000000	0.01	51.33	92.74	0.00
River 1	Reach 1-Upper	474	100YrSCS24Hr	0.40	92.41	93.30	92.59	93.30	0.000000	0.01	68.65	93.59	0.00
River 1	Reach 1-Upper	454	2YrCHI3Hr	0.07	92.44	92.58	92.50	92.58	0.001576	0.24	0.28	2.85	0.24
River 1	Reach 1-Upper	454	5YrCHI3Hr	0.12	92.44	92.62	92.53	92.63	0.001689	0.29	0.41	3.31	0.26
River 1	Reach 1-Upper	454	10YrCHI3Hr	0.16	92.44	92.65	92.55	92.66	0.001595	0.31	0.52	3.64	0.26
River 1	Reach 1-Upper	454	25YrCHI3Hr	0.22	92.44	92.72	92.56	92.72	0.000913	0.28	0.79	4.34	0.21
River 1	Reach 1-Upper	454	50YrCHI3Hr	0.26	92.44	92.84	92.57	92.84	0.000012	0.04	12.27	82.88	0.03
River 1	Reach 1-Upper	454	100YrCHI3Hr	0.31	92.44	93.00	92.59	93.00	0.000002	0.02	25.28	83.36	0.01
River 1	Reach 1-Upper	454	2YrSCS24Hr	0.11	92.44	92.61	92.52	92.62	0.001709	0.28	0.38	3.19	0.26
River 1	Reach 1-Upper	454	5YrSCS24Hr	0.18	92.44	92.67	92.55	92.67	0.001416	0.30	0.58	3.81	0.25
River 1	Reach 1-Upper	454	10YrSCS24Hr	0.23	92.44	92.74	92.56	92.74	0.000715	0.26	0.88	4.56	0.18
River 1	Reach 1-Upper	454	25YrSCS24Hr	0.29	92.44	92.93	92.58	92.93	0.000003	0.03	19.62	83.15	0.01
River 1	Reach 1-Upper	454	50YrSCS24Hr	0.34	92.44	93.12	92.60	93.12	0.000001	0.02	35.41	83.72	0.01
River 1	Reach 1-Upper	454	100YrSCS24Hr	0.40	92.44	93.30	92.61	93.30	0.000000	0.01	51.02	84.29	0.00
River 1	Reach 1-Upper	434	2YrCHI3Hr	0.07	92.42	92.53	92.49	92.54	0.003245	0.30	0.23	2.89	0.34
River 1	Reach 1-Upper	434	5YrCHI3Hr	0.12	92.42	92.58	92.51	92.59	0.002201	0.32	0.38	3.34	0.30
River 1	Reach 1-Upper	434	10YrCHI3Hr	0.16	92.42	92.62	92.52	92.62	0.001702	0.32	0.51	3.67	0.27
River 1	Reach 1-Upper	434	25YrCHI3Hr	0.22	92.42	92.72	92.54	92.72	0.000099	0.09	4.19	44.55	0.07
River 1	Reach 1-Upper	434	50YrCHI3Hr	0.26	92.42	92.84	92.55	92.84	0.000011	0.04	12.14	73.98	0.02
River 1	Reach 1-Upper	434	100YrCHI3Hr	0.31	92.42	93.00	92.56	93.00	0.000002	0.02	23.78	74.52	0.01
River 1	Reach 1-Upper	434	2YrSCS24Hr	0.11	92.42	92.57	92.50	92.57	0.002433	0.31	0.34	3.22	0.31
River 1	Reach 1-Upper	434	5YrSCS24Hr	0.18	92.42	92.64	92.53	92.64	0.001593	0.30	0.59	4.31	0.26
River 1	Reach 1-Upper	434	10YrSCS24Hr	0.23	92.42	92.74	92.54	92.74	0.000062	0.08	5.30	52.04	0.05
River 1	Reach 1-Upper	434	25YrSCS24Hr	0.29	92.42	92.93	92.55	92.93	0.000003	0.03	18.72	74.29	0.01
River 1	Reach 1-Upper	434	50YrSCS24Hr	0.34	92.42	93.12	92.57	93.12	0.000001	0.02	32.84	74.94	0.01
River 1	Reach 1-Upper	434	100YrSCS24Hr	0.40	92.42	93.30	92.58	93.30	0.000000	0.01	46.84	75.66	0.00
River 1	Reach 1-Upper	416	2YrCHI3Hr	0.07	92.34	92.51	92.42	92.51	0.000622	0.15	0.44	4.70	0.15
River 1	Reach 1-Upper	416	5YrCHI3Hr	0.12	92.34	92.57	92.45	92.57	0.000424	0.17	0.75	5.83	0.14
River 1	Reach 1-Upper	416	10YrCHI3Hr	0.16	92.34	92.62	92.46	92.62	0.000159	0.12	2.27	28.78	0.09
River 1	Reach 1-Upper	416	25YrCHI3Hr	0.22	92.34	92.72	92.48	92.72	0.000031	0.07	5.56	35.85	0.04
River 1	Reach 1-Upper	416	50YrCHI3Hr	0.26	92.34	92.84	92.48	92.84	0.000008	0.05	10.70	48.52	0.02
River 1	Reach 1-Upper	416	100YrCHI3Hr	0.31	92.34	93.00	92.49	93.00	0.000002	0.03	20.27	66.96	0.01
River 1	Reach 1-Upper	416	2YrSCS24Hr	0.11	92.34	92.56	92.44	92.56	0.000463	0.17	0.67	5.55	0.14
River 1	Reach 1-Upper	416	5YrSCS24Hr	0.18	92.34	92.64	92.47	92.64	0.000108	0.11	2.88	30.23	0.07
River 1	Reach 1-Upper	416	10YrSCS24Hr	0.23	92.34	92.74	92.48	92.74	0.000024	0.07	6.41	39.28	0.04
River 1	Reach 1-Upper	416	25YrSCS24Hr	0.29	92.34	92.93	92.49	92.93	0.000004	0.04	15.73	65.04	0.02
River 1	Reach 1-Upper	416	50YrSCS24Hr	0.34	92.34	93.12	92.50	93.12	0.000001	0.02	28.42	67.40	0.01
River 1	Reach 1-Upper	416	100YrSCS24Hr	0.40	92.34	93.30	92.51	93.30	0.000000	0.02	41.01	68.07	0.01
River 1	Reach 1-Upper	398	2YrCHI3Hr	0.07	92.28	92.50	92.40	92.50	0.000933	0.21	0.31	2.50	0.19
River 1	Reach 1-Upper	398	5YrCHI3Hr	0.12	92.28	92.56	92.42	92.56	0.000915	0.26	0.47	2.86	0.20
River 1	Reach 1-Upper	398	10YrCHI3Hr	0.16	92.28	92.61	92.44	92.61	0.000752	0.26	0.62	3.16	0.19
River 1	Reach 1-Upper	398	25YrCHI3Hr	0.22	92.28	92.71	92.46	92.72	0.000355	0.22	1.01	4.66	0.14
River 1	Reach 1-Upper	398	50YrCHI3Hr	0.26	92.28	92.84	92.47	92.84	0.000076	0.12	4.26	46.30	0.07
River 1	Reach 1-Upper	398	100YrCHI3Hr	0.31	92.28	93.00	92.49	93.00	0.000008	0.05	12.80	58.61	0.02
River 1	Reach 1-Upper	398	2YrSCS24Hr	0.11	92.28	92.54	92.42	92.55	0.000935	0.25	0.43	2.77	0.20
River 1	Reach 1-Upper	398	5YrSCS24Hr	0.18	92.28	92.63	92.44	92.63	0.000660	0.26	0.69	3.29	0.18
River 1	Reach 1-Upper	398	10YrSCS24Hr	0.23	92.28	92.74	92.46	92.74	0.000295	0.21	1.13	5.59	0.12
River 1	Reach 1-Upper	398	25YrSCS24Hr	0.29	92.28	92.93	92.48	92.93	0.000020	0.07	8.81	58.42	0.03
River 1	Reach 1-Upper	398	50YrSCS24Hr	0.34	92.28	93.12	92.50	93.12	0.000003	0.03	19.93	58.96	0.01
River 1	Reach 1-Upper	398	100YrSCS24Hr	0.40	92.28	93.30	92.51	93.30	0.000001	0.02	30.94	59.51	0.01
River 1	Reach 1-Upper	383	2YrCHI3Hr	0.07	92.34	92.47	92.42	92.47	0.004536	0.39	0.17	1.90	0.41
River 1	Reach 1-Upper	383	5YrCHI3Hr	0.12	92.34	92.53	92.45	92.54	0.002876	0.39	0.31	2.30	0.34
River 1	Reach 1-Upper	383	10YrCHI3Hr	0.16	92.34	92.59	92.47	92.59	0.001737	0.36	0.45	2.62	0.28
River 1	Reach 1-Upper	383	25YrCHI3Hr	0.22	92.34	92.70	92.49	92.71	0.000630	0.27	0.80	3.29	0.18
River 1	Reach 1-Upper	383	50YrCHI3Hr	0.26	92.34	92.83	92.50	92.84	0.000255	0.21	1.27	4.01	0.12
River 1	Reach 1-Upper	383	100YrCHI3Hr	0.31	92.34	92.99	92.52	93.00	0.000100	0.16	2.02	5.50	0.08
River 1	Reach 1-Upper	383	2YrSCS24Hr	0.11	92.34	92.51	92.44	92.52	0.003262	0.40	0.27	2.21	0.36
River 1	Reach 1-Upper	383	5YrSCS24Hr	0.18	92.34	92.61	92.47	92.62	0.001389	0.34	0.52	2.77	0.25
River 1	Reach 1-Upper	383	10YrSCS24Hr	0.23	92.34	92.73	92.49	92.73	0.000520	0.26	0.88	3.42	0.16
River 1	Reach 1-Upper	383	25YrSCS24Hr	0.29	92.34	92.93	92.51	92.93	0.000147	0.18	1.66	4.73	0.09

HEC-RAS Plan: 20250603-Pre_Dev_v01 (Continued)

River	Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
River 1	Reach 1-Upper	383	50YrSCS24Hr	0.34	92.34	93.12	92.53	93.12	0.000005	0.04	15.00	51.87	0.02
River 1	Reach 1-Upper	383	100YrSCS24Hr	0.40	92.34	93.30	92.54	93.30	0.000002	0.03	24.70	52.43	0.01
River 1	Reach 1-Upper	364	2YrCHI3Hr	0.07	92.23	92.43	92.33	92.43	0.001355	0.26	0.26	2.01	0.23
River 1	Reach 1-Upper	364	5YrCHI3Hr	0.12	92.23	92.50	92.36	92.50	0.001099	0.29	0.42	2.37	0.22
River 1	Reach 1-Upper	364	10YrCHI3Hr	0.16	92.23	92.57	92.38	92.57	0.000740	0.27	0.59	2.71	0.19
River 1	Reach 1-Upper	364	25YrCHI3Hr	0.22	92.23	92.70	92.40	92.70	0.000331	0.22	0.98	3.34	0.13
River 1	Reach 1-Upper	364	50YrCHI3Hr	0.26	92.23	92.83	92.42	92.83	0.000166	0.18	1.48	4.20	0.10
River 1	Reach 1-Upper	364	100YrCHI3Hr	0.31	92.23	92.99	92.43	92.99	0.000050	0.12	4.53	43.93	0.06
River 1	Reach 1-Upper	364	2YrSCS24Hr	0.11	92.23	92.48	92.35	92.48	0.001197	0.29	0.37	2.27	0.23
River 1	Reach 1-Upper	364	5YrSCS24Hr	0.18	92.23	92.60	92.39	92.60	0.000621	0.26	0.67	2.85	0.17
River 1	Reach 1-Upper	364	10YrSCS24Hr	0.23	92.23	92.72	92.41	92.73	0.000283	0.21	1.07	3.47	0.12
River 1	Reach 1-Upper	364	25YrSCS24Hr	0.29	92.23	92.92	92.43	92.93	0.000099	0.15	1.93	5.59	0.08
River 1	Reach 1-Upper	364	50YrSCS24Hr	0.34	92.23	93.12	92.44	93.12	0.000012	0.07	9.97	44.25	0.03
River 1	Reach 1-Upper	364	100YrSCS24Hr	0.40	92.23	93.30	92.46	93.30	0.000003	0.04	18.26	45.01	0.01
River 1	Reach 1-Upper	347	2YrCHI3Hr	0.07	92.26	92.40	92.33	92.41	0.001382	0.24	0.27	2.45	0.23
River 1	Reach 1-Upper	347	5YrCHI3Hr	0.12	92.26	92.49	92.35	92.49	0.000808	0.25	0.49	2.80	0.19
River 1	Reach 1-Upper	347	10YrCHI3Hr	0.16	92.26	92.56	92.36	92.56	0.000488	0.23	0.71	3.12	0.15
River 1	Reach 1-Upper	347	25YrCHI3Hr	0.22	92.26	92.69	92.38	92.70	0.000213	0.19	1.16	3.69	0.11
River 1	Reach 1-Upper	347	50YrCHI3Hr	0.26	92.26	92.83	92.40	92.83	0.000107	0.15	1.71	4.28	0.08
River 1	Reach 1-Upper	347	100YrCHI3Hr	0.31	92.26	92.99	92.41	92.99	0.000050	0.13	2.54	7.35	0.06
River 1	Reach 1-Upper	347	2YrSCS24Hr	0.11	92.26	92.46	92.34	92.47	0.000932	0.25	0.43	2.71	0.20
River 1	Reach 1-Upper	347	5YrSCS24Hr	0.18	92.26	92.59	92.37	92.59	0.000403	0.22	0.80	3.25	0.14
River 1	Reach 1-Upper	347	10YrSCS24Hr	0.23	92.26	92.72	92.39	92.72	0.000183	0.18	1.26	3.81	0.10
River 1	Reach 1-Upper	347	25YrSCS24Hr	0.29	92.26	92.92	92.41	92.92	0.000071	0.14	2.13	5.02	0.07
River 1	Reach 1-Upper	347	50YrSCS24Hr	0.34	92.26	93.12	92.42	93.12	0.000020	0.09	6.30	37.59	0.04
River 1	Reach 1-Upper	347	100YrSCS24Hr	0.40	92.26	93.30	92.43	93.30	0.000005	0.06	13.35	38.07	0.02
River 1	Reach 1-Upper	328	2YrCHI3Hr	0.07	92.20	92.37	92.28	92.38	0.001873	0.30	0.22	1.82	0.27
River 1	Reach 1-Upper	328	5YrCHI3Hr	0.12	92.20	92.47	92.32	92.47	0.001020	0.29	0.42	2.24	0.21
River 1	Reach 1-Upper	328	10YrCHI3Hr	0.16	92.20	92.55	92.34	92.55	0.000618	0.26	0.61	2.58	0.17
River 1	Reach 1-Upper	328	25YrCHI3Hr	0.22	92.20	92.69	92.36	92.69	0.000277	0.21	1.02	3.16	0.12
River 1	Reach 1-Upper	328	50YrCHI3Hr	0.26	92.20	92.83	92.38	92.83	0.000152	0.17	1.51	4.11	0.09
River 1	Reach 1-Upper	328	100YrCHI3Hr	0.31	92.20	92.99	92.40	92.99	0.000074	0.14	2.26	5.12	0.07
River 1	Reach 1-Upper	328	2YrSCS24Hr	0.11	92.20	92.44	92.31	92.45	0.001182	0.29	0.36	2.14	0.23
River 1	Reach 1-Upper	328	5YrSCS24Hr	0.18	92.20	92.58	92.34	92.58	0.000513	0.25	0.70	2.71	0.16
River 1	Reach 1-Upper	328	10YrSCS24Hr	0.23	92.20	92.72	92.36	92.72	0.000240	0.21	1.11	3.28	0.11
River 1	Reach 1-Upper	328	25YrSCS24Hr	0.29	92.20	92.92	92.39	92.92	0.000098	0.15	1.92	4.61	0.07
River 1	Reach 1-Upper	328	50YrSCS24Hr	0.34	92.20	93.12	92.40	93.12	0.000035	0.11	4.57	29.52	0.05
River 1	Reach 1-Upper	328	100YrSCS24Hr	0.40	92.20	93.30	92.42	93.30	0.000009	0.06	10.13	29.96	0.02
River 1	Reach 1-Upper	306	2YrCHI3Hr	0.07	92.07	92.35	92.18	92.35	0.000722	0.25	0.27	1.49	0.18
River 1	Reach 1-Upper	306	5YrCHI3Hr	0.12	92.07	92.45	92.23	92.45	0.000689	0.30	0.40	1.84	0.18
River 1	Reach 1-Upper	306	10YrCHI3Hr	0.16	92.07	92.53	92.25	92.54	0.000559	0.31	0.52	2.13	0.17
River 1	Reach 1-Upper	306	25YrCHI3Hr	0.22	92.07	92.68	92.28	92.68	0.000321	0.29	0.74	2.69	0.13
River 1	Reach 1-Upper	306	50YrCHI3Hr	0.26	92.07	92.82	92.30	92.82	0.000203	0.28	0.95	3.29	0.11
River 1	Reach 1-Upper	306	100YrCHI3Hr	0.31	92.07	92.99	92.32	92.99	0.000131	0.26	1.20	4.54	0.09
River 1	Reach 1-Upper	306	2YrSCS24Hr	0.11	92.07	92.42	92.21	92.43	0.000712	0.29	0.37	1.75	0.18
River 1	Reach 1-Upper	306	5YrSCS24Hr	0.18	92.07	92.57	92.26	92.57	0.000497	0.31	0.58	2.25	0.16
River 1	Reach 1-Upper	306	10YrSCS24Hr	0.23	92.07	92.71	92.28	92.71	0.000290	0.29	0.79	2.81	0.13
River 1	Reach 1-Upper	306	25YrSCS24Hr	0.29	92.07	92.91	92.31	92.92	0.000156	0.27	1.10	3.90	0.10
River 1	Reach 1-Upper	306	50YrSCS24Hr	0.34	92.07	93.11	92.33	93.11	0.000098	0.25	1.39	20.53	0.08
River 1	Reach 1-Upper	306	100YrSCS24Hr	0.40	92.07	93.30	92.36	93.30	0.000072	0.24	1.67	20.98	0.07
River 1	Reach 1-Upper	300		Culvert									
River 1	Reach 1-Upper	294	2YrCHI3Hr	0.07	92.15	92.32	92.23	92.32	0.001567	0.31	0.22	2.08	0.26
River 1	Reach 1-Upper	294	5YrCHI3Hr	0.12	92.15	92.37	92.26	92.38	0.001840	0.41	0.29	2.34	0.30
River 1	Reach 1-Upper	294	10YrCHI3Hr	0.16	92.15	92.39	92.28	92.41	0.002165	0.49	0.33	2.48	0.33
River 1	Reach 1-Upper	294	25YrCHI3Hr	0.22	92.15	92.42	92.30	92.44	0.002528	0.57	0.38	2.64	0.36
River 1	Reach 1-Upper	294	50YrCHI3Hr	0.26	92.15	92.45	92.32	92.47	0.002769	0.63	0.41	2.76	0.38
River 1	Reach 1-Upper	294	100YrCHI3Hr	0.31	92.15	92.47	92.33	92.49	0.002956	0.69	0.45	2.87	0.40
River 1	Reach 1-Upper	294	2YrSCS24Hr	0.11	92.15	92.36	92.25	92.36	0.001762	0.39	0.28	2.28	0.29
River 1	Reach 1-Upper	294	5YrSCS24Hr	0.18	92.15	92.40	92.28	92.41	0.002296	0.51	0.35	2.52	0.34
River 1	Reach 1-Upper	294	10YrSCS24Hr	0.23	92.15	92.43	92.30	92.45	0.002610	0.59	0.39	2.66	0.37
River 1	Reach 1-Upper	294	25YrSCS24Hr	0.29	92.15	92.46	92.33	92.48	0.002895	0.67	0.43	2.82	0.40
River 1	Reach 1-Upper	294	50YrSCS24Hr	0.34	92.15	92.48	92.35	92.51	0.003128	0.73	0.47	2.94	0.42
River 1	Reach 1-Upper	294	100YrSCS24Hr	0.40	92.15	92.50	92.36	92.54	0.003396	0.80	0.50	3.05	0.44
River 1	Reach 1-Upper	279	2YrCHI3Hr	0.08	92.08	92.21	92.21	92.24	0.029991	0.80	0.10	1.51	0.99
River 1	Reach 1-Upper	279	5YrCHI3Hr	0.15	92.08	92.25	92.24	92.29	0.026320	0.91	0.16	1.84	0.98
River 1	Reach 1-Upper	279	10YrCHI3Hr	0.20	92.08	92.28		92.32	0.017826	0.87	0.23	2.04	0.83
River 1	Reach 1-Upper	279	25YrCHI3Hr	0.27	92.08	92.32		92.36	0.013314	0.86	0.31	2.27	0.74
River 1	Reach 1-Upper	279	50YrCHI3Hr	0.32	92.08	92.34		92.38	0.011695	0.87	0.37	2.42	0.71
River 1	Reach 1-Upper	279	100YrCHI3Hr	0.38	92.08	92.37		92.41	0.010643	0.88	0.43	2.57	0.69
River 1	Reach 1-Upper	279	2YrSCS24Hr	0.13	92.08	92.23	92.23	92.28	0.029039	0.90	0.14	1.75	1.01
River 1	Reach 1-Upper	279	5YrSCS24Hr	0.22	92.08	92.29		92.33	0.015917	0.86	0.25	2.10	0.80
River 1	Reach 1-Upper	279	10YrSCS24Hr	0.28	92.08	92.32		92.36	0.012955	0.86	0.32	2.30	0.74
River 1	Reach 1-Upper	279	25YrSCS24Hr	0.36	92.08	92.36		92.40	0.011055	0.88	0.41	2.51	0.70
River 1	Reach 1-Upper	279	50YrSCS24Hr	0.42	92.08	92.38		92.42	0.010063	0.89	0.47	2.66	0.67
River 1	Reach 1-Upper	279	100YrSCS24Hr	0.49	92.08	92.41		92.45	0.009502	0.91	0.54	2.81	0.66
River 1	Reach 1-Upper	277	2YrCHI3Hr	0.08	91.95	92.20		92.21	0.000695	0.21	0.39	2.70	0.17
River 1	Reach 1-Upper	277	5YrCHI3Hr	0.15	91.95	92.26		92.26	0.000856	0.28	0.54	3.02	0.20
River 1	Reach 1-Upper	277	10YrCHI3Hr	0.20	91.95	92.29		92.30	0.000927	0.32	0.64	3.19	0.21
River 1	Reach 1-Upper	277	25YrCHI3Hr	0.27	91.95	92.33		92.33	0.001006	0.37	0.76	3.41	0.23
River 1	Reach 1-Upper	277	50YrCHI3Hr	0.32	91.95	92.35		92.36	0.001068	0.41	0.85	3.55	0.24
River 1	Reach 1-Upper	277	100YrCHI3Hr	0.38	91.95	92.38		92.39	0.001131	0.44	0.95	3.69	0.25
River 1	Reach 1-Upper	277	2YrSCS24Hr	0.13	91.95	92.25		92.25	0.000826	0.26	0.50	2.94	0.20

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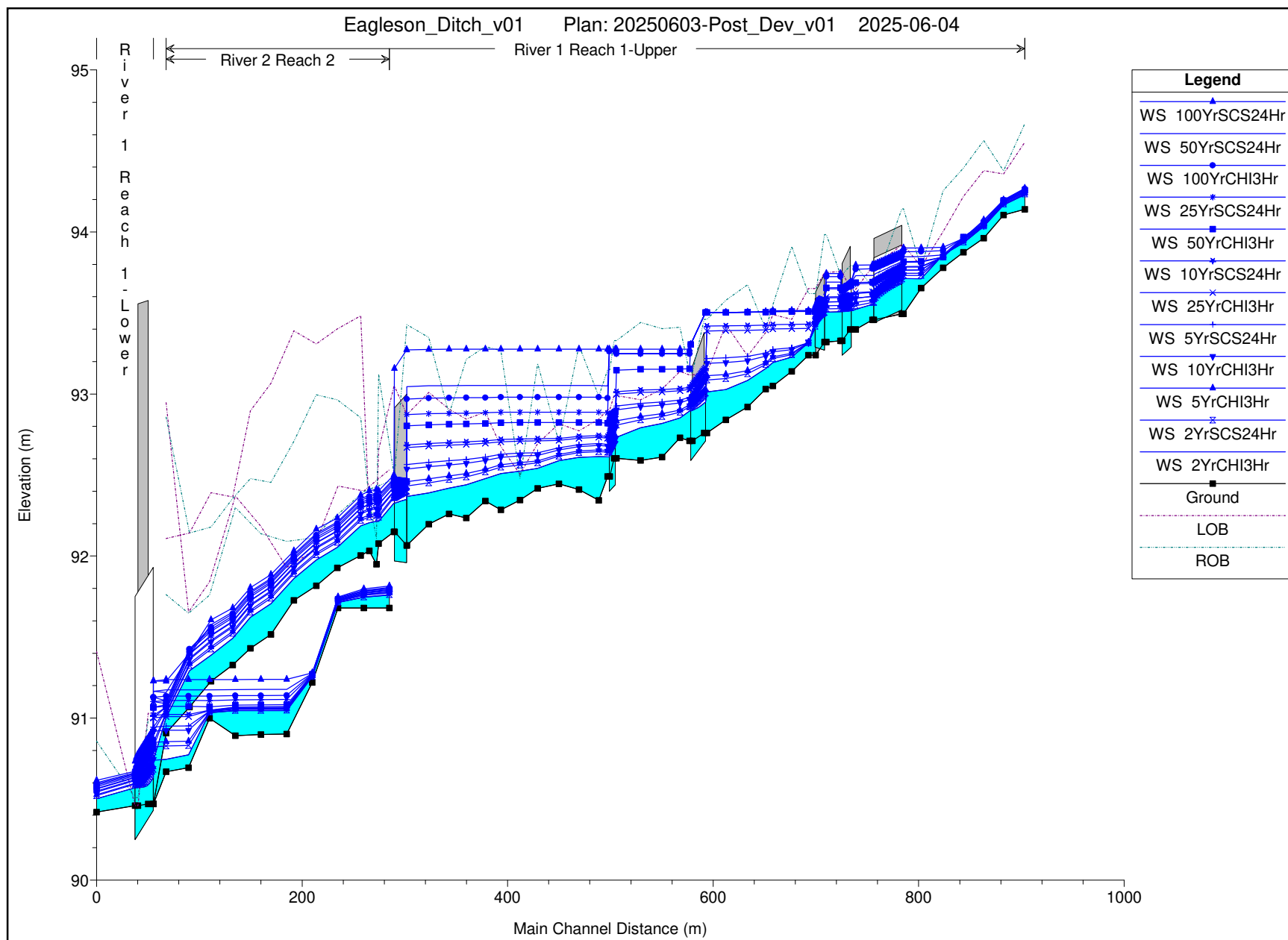
River	Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
River 1	Reach 1-Upper	277	5YrSCS24Hr	0.22	91.95	92.30		92.31	0.000941	0.33	0.68	3.25	0.22
River 1	Reach 1-Upper	277	10YrSCS24Hr	0.28	91.95	92.33		92.34	0.001018	0.38	0.78	3.43	0.23
River 1	Reach 1-Upper	277	25YrSCS24Hr	0.36	91.95	92.37		92.38	0.001104	0.43	0.91	3.63	0.25
River 1	Reach 1-Upper	277	50YrSCS24Hr	0.42	91.95	92.39		92.40	0.001159	0.46	1.00	3.77	0.26
River 1	Reach 1-Upper	277	100YrSCS24Hr	0.49	91.95	92.42		92.43	0.001229	0.50	1.09	3.91	0.27
River 1	Reach 1-Upper	270	2YrCHI3Hr	0.08	92.03	92.20		92.20	0.001692	0.27	0.29	2.60	0.26
River 1	Reach 1-Upper	270	5YrCHI3Hr	0.15	92.03	92.25		92.25	0.001753	0.33	0.45	3.07	0.27
River 1	Reach 1-Upper	270	10YrCHI3Hr	0.20	92.03	92.28		92.29	0.001743	0.36	0.55	3.36	0.28
River 1	Reach 1-Upper	270	25YrCHI3Hr	0.27	92.03	92.32		92.33	0.001732	0.40	0.68	3.72	0.29
River 1	Reach 1-Upper	270	50YrCHI3Hr	0.32	92.03	92.34		92.35	0.001721	0.42	0.78	4.13	0.29
River 1	Reach 1-Upper	270	100YrCHI3Hr	0.38	92.03	92.37		92.38	0.001663	0.45	0.90	5.00	0.29
River 1	Reach 1-Upper	270	2YrSCS24Hr	0.13	92.03	92.24		92.24	0.001760	0.32	0.40	2.95	0.27
River 1	Reach 1-Upper	270	5YrSCS24Hr	0.22	92.03	92.29		92.30	0.001717	0.37	0.58	3.47	0.28
River 1	Reach 1-Upper	270	10YrSCS24Hr	0.28	92.03	92.32		92.33	0.001734	0.40	0.70	3.76	0.29
River 1	Reach 1-Upper	270	25YrSCS24Hr	0.36	92.03	92.36		92.37	0.001687	0.44	0.84	4.62	0.29
River 1	Reach 1-Upper	270	50YrSCS24Hr	0.42	92.03	92.38		92.39	0.001617	0.46	0.97	5.51	0.29
River 1	Reach 1-Upper	270	100YrSCS24Hr	0.49	92.03	92.41		92.42	0.001578	0.48	1.11	5.76	0.29
River 1	Reach 1-Upper	261	2YrCHI3Hr	0.08	92.00	92.18	92.10	92.18	0.002216	0.32	0.25	2.09	0.30
River 1	Reach 1-Upper	261	5YrCHI3Hr	0.15	92.00	92.23	92.13	92.24	0.002543	0.41	0.36	2.34	0.33
River 1	Reach 1-Upper	261	10YrCHI3Hr	0.20	92.00	92.26	92.15	92.27	0.002719	0.46	0.43	2.48	0.35
River 1	Reach 1-Upper	261	25YrCHI3Hr	0.27	92.00	92.29	92.18	92.31	0.002882	0.51	0.52	2.66	0.37
River 1	Reach 1-Upper	261	50YrCHI3Hr	0.32	92.00	92.32	92.19	92.33	0.003012	0.55	0.59	2.78	0.38
River 1	Reach 1-Upper	261	100YrCHI3Hr	0.38	92.00	92.34	92.21	92.36	0.003124	0.58	0.66	2.90	0.39
River 1	Reach 1-Upper	261	2YrSCS24Hr	0.13	92.00	92.22	92.12	92.22	0.002466	0.39	0.33	2.27	0.32
River 1	Reach 1-Upper	261	5YrSCS24Hr	0.22	92.00	92.27	92.16	92.28	0.002719	0.47	0.46	2.53	0.35
River 1	Reach 1-Upper	261	10YrSCS24Hr	0.28	92.00	92.30	92.18	92.31	0.002908	0.52	0.54	2.68	0.37
River 1	Reach 1-Upper	261	25YrSCS24Hr	0.36	92.00	92.33	92.20	92.35	0.003077	0.57	0.63	2.84	0.38
River 1	Reach 1-Upper	261	50YrSCS24Hr	0.42	92.00	92.36	92.22	92.38	0.003155	0.60	0.70	2.97	0.39
River 1	Reach 1-Upper	261	100YrSCS24Hr	0.49	92.00	92.38	92.24	92.40	0.003314	0.63	0.77	3.10	0.41
River 1	Reach 1-Upper	239	2YrCHI3Hr	0.08	91.93	92.05	92.03	92.07	0.018146	0.68	0.12	1.54	0.79
River 1	Reach 1-Upper	239	5YrCHI3Hr	0.15	91.93	92.09	92.07	92.12	0.014163	0.75	0.20	1.88	0.73
River 1	Reach 1-Upper	239	10YrCHI3Hr	0.20	91.93	92.12	92.09	92.15	0.012598	0.78	0.25	2.06	0.71
River 1	Reach 1-Upper	239	25YrCHI3Hr	0.27	91.93	92.15	92.12	92.19	0.011181	0.82	0.33	2.23	0.69
River 1	Reach 1-Upper	239	50YrCHI3Hr	0.32	91.93	92.18	92.13	92.21	0.010479	0.85	0.38	2.36	0.68
River 1	Reach 1-Upper	239	100YrCHI3Hr	0.38	91.93	92.20	92.15	92.24	0.009912	0.88	0.44	2.49	0.67
River 1	Reach 1-Upper	239	2YrSCS24Hr	0.13	91.93	92.08	92.06	92.11	0.014943	0.73	0.18	1.79	0.75
River 1	Reach 1-Upper	239	5YrSCS24Hr	0.22	91.93	92.13	92.10	92.16	0.012137	0.79	0.27	2.10	0.70
River 1	Reach 1-Upper	239	10YrSCS24Hr	0.28	91.93	92.16	92.12	92.19	0.011036	0.83	0.34	2.26	0.68
River 1	Reach 1-Upper	239	25YrSCS24Hr	0.36	91.93	92.19	92.14	92.23	0.010147	0.86	0.41	2.43	0.67
River 1	Reach 1-Upper	239	50YrSCS24Hr	0.42	91.93	92.22	92.16	92.26	0.009585	0.89	0.47	2.56	0.66
River 1	Reach 1-Upper	239	100YrSCS24Hr	0.49	91.93	92.24	92.18	92.28	0.009080	0.91	0.54	2.69	0.65
River 1	Reach 1-Upper	218	2YrCHI3Hr	0.08	91.82	91.97	91.89	91.97	0.002000	0.29	0.27	2.48	0.28
River 1	Reach 1-Upper	218	5YrCHI3Hr	0.15	91.82	92.02	91.92	92.02	0.002151	0.37	0.40	2.72	0.30
River 1	Reach 1-Upper	218	10YrCHI3Hr	0.20	91.82	92.05	91.94	92.05	0.002198	0.40	0.49	2.86	0.31
River 1	Reach 1-Upper	218	25YrCHI3Hr	0.27	91.82	92.08	91.96	92.09	0.002327	0.45	0.59	3.03	0.33
River 1	Reach 1-Upper	218	50YrCHI3Hr	0.32	91.82	92.11	91.98	92.12	0.002390	0.49	0.67	3.15	0.34
River 1	Reach 1-Upper	218	100YrCHI3Hr	0.38	91.82	92.13	91.99	92.14	0.002438	0.52	0.75	3.27	0.34
River 1	Reach 1-Upper	218	2YrSCS24Hr	0.13	91.82	92.00	91.92	92.01	0.002117	0.35	0.37	2.66	0.30
River 1	Reach 1-Upper	218	5YrSCS24Hr	0.22	91.82	92.06	91.95	92.06	0.002238	0.42	0.51	2.91	0.32
River 1	Reach 1-Upper	218	10YrSCS24Hr	0.28	91.82	92.09	91.96	92.10	0.002340	0.46	0.60	3.05	0.33
River 1	Reach 1-Upper	218	25YrSCS24Hr	0.36	91.82	92.12	91.98	92.13	0.002418	0.50	0.71	3.22	0.34
River 1	Reach 1-Upper	218	50YrSCS24Hr	0.42	91.82	92.14	92.00	92.16	0.002473	0.53	0.79	3.36	0.35
River 1	Reach 1-Upper	218	100YrSCS24Hr	0.49	91.82	92.17	92.02	92.19	0.002504	0.56	0.88	3.53	0.35
River 1	Reach 1-Upper	197	2YrCHI3Hr	0.08	91.73	91.85	91.84	91.87	0.016181	0.66	0.12	1.55	0.75
River 1	Reach 1-Upper	197	5YrCHI3Hr	0.15	91.73	91.90	91.87	91.93	0.013293	0.73	0.20	1.87	0.72
River 1	Reach 1-Upper	197	10YrCHI3Hr	0.20	91.73	91.93	91.89	91.96	0.012335	0.78	0.25	2.02	0.71
River 1	Reach 1-Upper	197	25YrCHI3Hr	0.27	91.73	91.96	91.92	91.99	0.011527	0.84	0.32	2.18	0.70
River 1	Reach 1-Upper	197	50YrCHI3Hr	0.32	91.73	91.98	91.94	92.02	0.010809	0.87	0.37	2.29	0.69
River 1	Reach 1-Upper	197	100YrCHI3Hr	0.38	91.73	92.00	91.96	92.04	0.010540	0.91	0.42	2.39	0.68
River 1	Reach 1-Upper	197	2YrSCS24Hr	0.13	91.73	91.89	91.87	91.91	0.013973	0.71	0.18	1.81	0.72
River 1	Reach 1-Upper	197	5YrSCS24Hr	0.22	91.73	91.93	91.90	91.97	0.012083	0.80	0.27	2.06	0.70
River 1	Reach 1-Upper	197	10YrSCS24Hr	0.28	91.73	91.96	91.92	92.00	0.011418	0.84	0.33	2.20	0.70
River 1	Reach 1-Upper	197	25YrSCS24Hr	0.36	91.73	91.99	91.95	92.03	0.010650	0.89	0.40	2.34	0.69
River 1	Reach 1-Upper	197	50YrSCS24Hr	0.42	91.73	92.02	91.97	92.06	0.010407	0.93	0.45	2.44	0.69
River 1	Reach 1-Upper	197	100YrSCS24Hr	0.49	91.73	92.04	91.99	92.08	0.010221	0.96	0.51	2.55	0.69
River 1	Reach 1-Upper	174	2YrCHI3Hr	0.08	91.52	91.70	91.63	91.71	0.004212	0.41	0.19	1.80	0.40
River 1	Reach 1-Upper	174	5YrCHI3Hr	0.15	91.52	91.75	91.67	91.76	0.004464	0.50	0.30	2.17	0.43
River 1	Reach 1-Upper	174	10YrCHI3Hr	0.20	91.52	91.78	91.69	91.79	0.004633	0.55	0.36	2.31	0.45
River 1	Reach 1-Upper	174	25YrCHI3Hr	0.27	91.52	91.81	91.72	91.83	0.004788	0.61	0.44	2.47	0.46
River 1	Reach 1-Upper	174	50YrCHI3Hr	0.32	91.52	91.83	91.74	91.85	0.004947	0.65	0.50	2.58	0.48
River 1	Reach 1-Upper	174	100YrCHI3Hr	0.38	91.52	91.85	91.76	91.88	0.005078	0.69	0.56	2.69	0.49
River 1	Reach 1-Upper	174	2YrSCS24Hr	0.13	91.52	91.74	91.66	91.75	0.004366	0.47	0.27	2.08	0.42
River 1	Reach 1-Upper	174	5YrSCS24Hr	0.22	91.52	91.78	91.70	91.80	0.004685	0.57	0.38	2.35	0.45
River 1	Reach 1-Upper	174	10YrSCS24Hr	0.28	91.52	91.81	91.73	91.83	0.004821	0.62	0.45	2.49	0.46
River 1	Reach 1-Upper	174	25YrSCS24Hr	0.36	91.52	91.84	91.75	91.87	0.005024	0.67	0.53	2.65	0.48
River 1	Reach 1-Upper	174	50YrSCS24Hr	0.42	91.52	91.87	91.77	91.89	0.005141	0.71	0.59	2.76	0.49
River 1	Reach 1-Upper	174	100YrSCS24Hr	0.49	91.52	91.89	91.79	91.92	0.005179	0.75	0.66	2.87	0.50
River 1	Reach 1-Upper	154	2YrCHI3Hr	0.08	91.43	91.61	91.56	91.62	0.004328	0.39	0.21	2.16	0.40
River 1	Reach 1-Upper	154	5YrCHI3Hr	0.15	91.43	91.66	91.59	91.67	0.004181	0.46	0.32	2.60	0.41
River 1	Reach 1-Upper	154	10YrCHI3Hr	0.20	91.43	91.69	91.61	91.70	0.004190	0.49	0.40	2.83	0.42
River 1	Reach 1-Upper	154	25YrCHI3Hr	0.27	91.43	91.72	91.64	91.74	0.004087	0.53	0.50	3.11	0.42
River 1	Reach 1-Upper	154	50YrCHI3Hr	0.32	91.43	91.75	91.65	91.76	0.003985	0.56	0.58	3.28	0.43
River 1	Reach 1-Upper	154	100YrCHI3Hr	0.38	91.43	91.77	91.67	91.79	0.003882	0.58	0.66	3.44	0.43

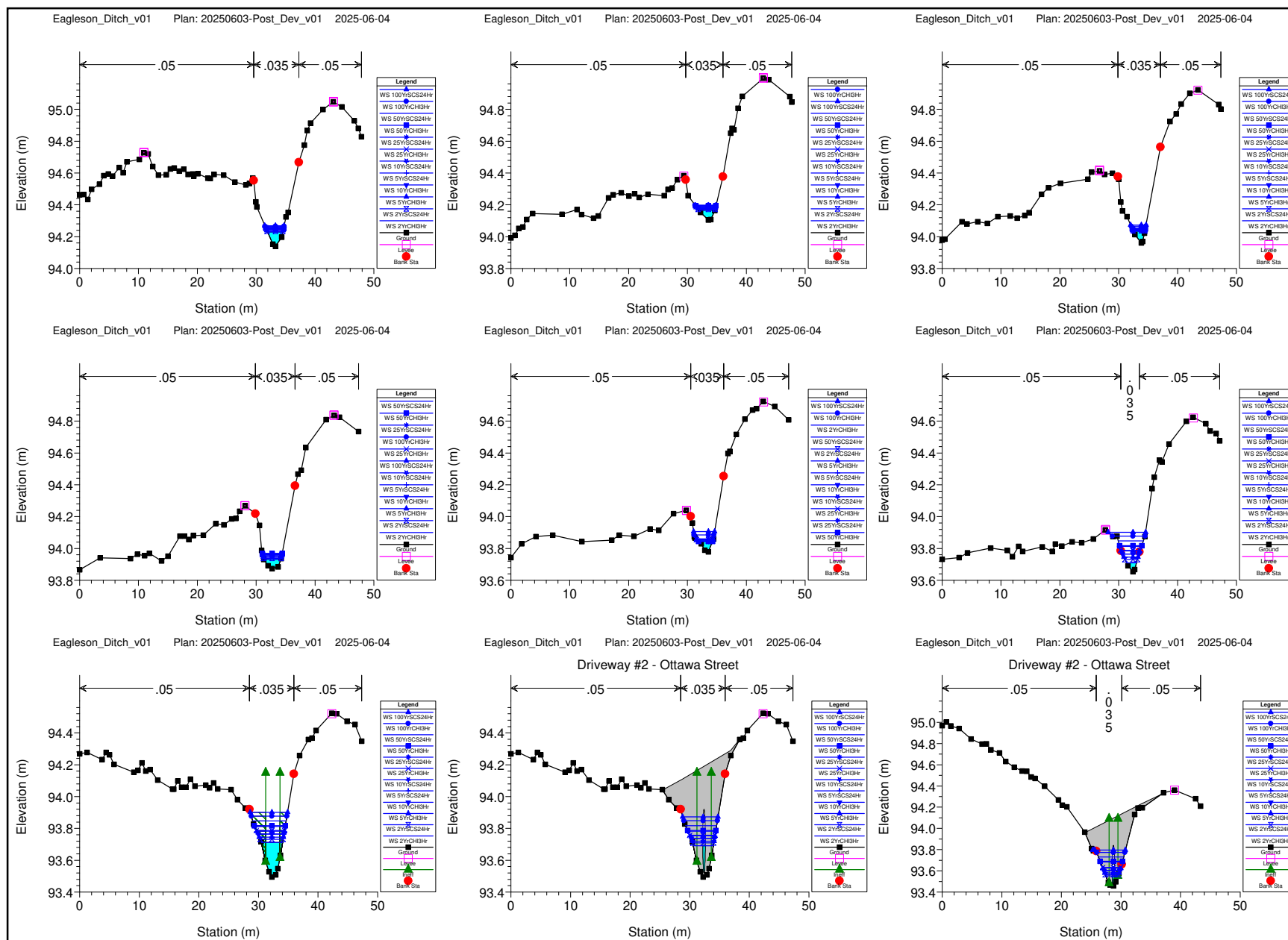
HEC-RAS Plan: 20250603-Pre_Dev_v01 (Continued)

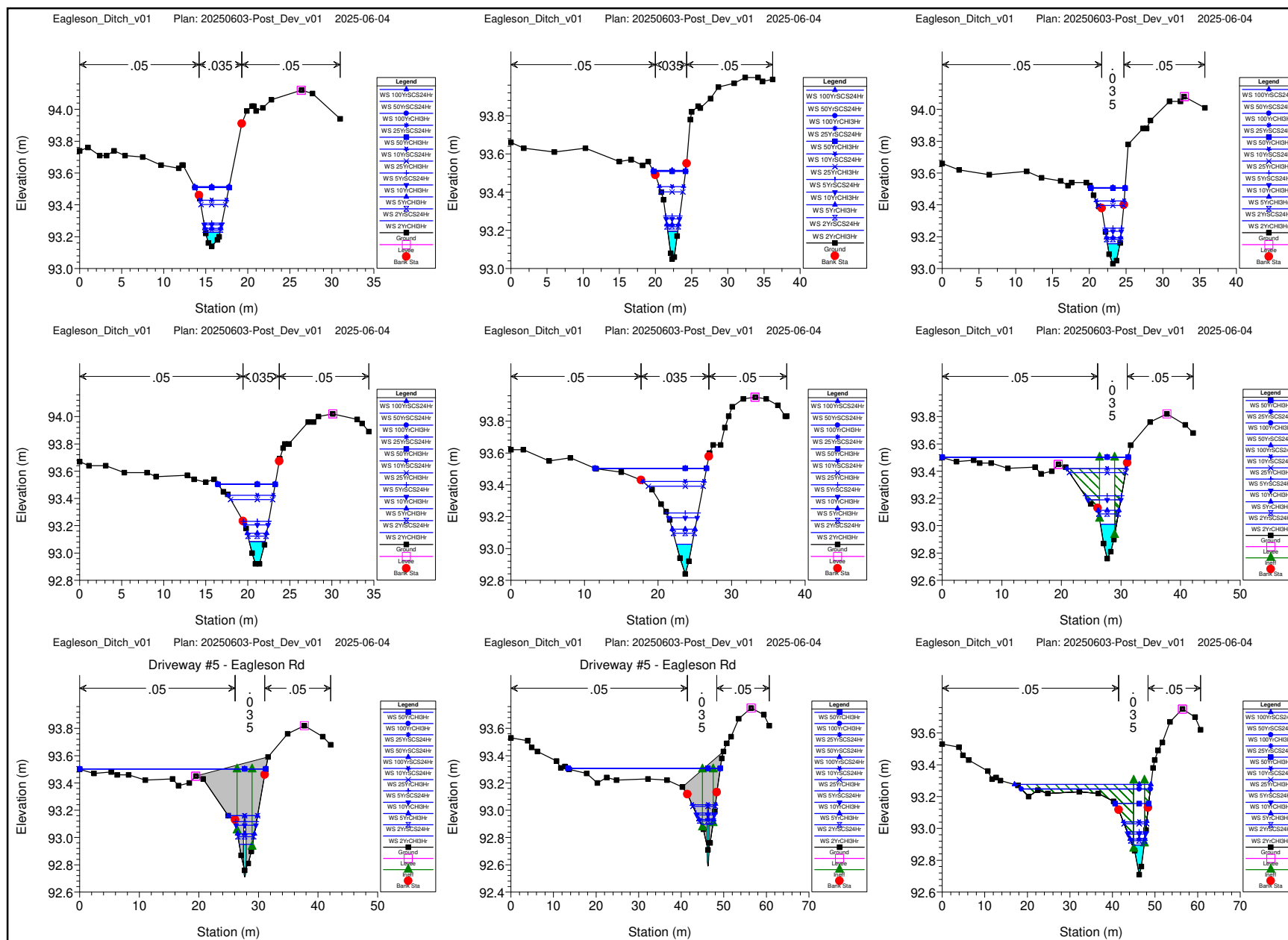
River	Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
River 1	Reach 1-Upper	154	2YrSCS24Hr	0.13	91.43	91.65	91.58	91.66	0.004251	0.44	0.29	2.49	0.41
River 1	Reach 1-Upper	154	5YrSCS24Hr	0.22	91.43	91.70	91.62	91.71	0.004167	0.51	0.43	2.91	0.42
River 1	Reach 1-Upper	154	10YrSCS24Hr	0.28	91.43	91.73	91.64	91.74	0.004071	0.54	0.51	3.14	0.43
River 1	Reach 1-Upper	154	25YrSCS24Hr	0.36	91.43	91.76	91.66	91.78	0.003925	0.57	0.62	3.37	0.43
River 1	Reach 1-Upper	154	50YrSCS24Hr	0.42	91.43	91.79	91.68	91.80	0.003830	0.60	0.71	3.53	0.43
River 1	Reach 1-Upper	154	100YrSCS24Hr	0.49	91.43	91.81	91.70	91.83	0.003747	0.62	0.79	3.69	0.43
River 1	Reach 1-Upper	137	2YrCHI3Hr	0.08	91.33	91.48	91.46	91.50	0.012189	0.63	0.13	1.39	0.66
River 1	Reach 1-Upper	137	5YrCHI3Hr	0.15	91.33	91.53	91.50	91.56	0.011338	0.73	0.20	1.65	0.67
River 1	Reach 1-Upper	137	10YrCHI3Hr	0.20	91.33	91.56	91.52	91.59	0.011017	0.79	0.25	1.80	0.67
River 1	Reach 1-Upper	137	25YrCHI3Hr	0.27	91.33	91.60	91.55	91.63	0.010550	0.84	0.32	1.99	0.67
River 1	Reach 1-Upper	137	50YrCHI3Hr	0.32	91.33	91.62	91.57	91.66	0.010206	0.88	0.37	2.12	0.67
River 1	Reach 1-Upper	137	100YrCHI3Hr	0.38	91.33	91.65	91.59	91.69	0.009820	0.90	0.42	2.25	0.66
River 1	Reach 1-Upper	137	2YrSCS24Hr	0.13	91.33	91.52	91.49	91.54	0.011464	0.71	0.18	1.58	0.67
River 1	Reach 1-Upper	137	5YrSCS24Hr	0.22	91.33	91.57	91.53	91.60	0.010898	0.80	0.27	1.85	0.67
River 1	Reach 1-Upper	137	10YrSCS24Hr	0.28	91.33	91.60	91.55	91.64	0.010487	0.85	0.33	2.01	0.67
River 1	Reach 1-Upper	137	25YrSCS24Hr	0.36	91.33	91.63	91.58	91.68	0.009938	0.89	0.40	2.20	0.67
River 1	Reach 1-Upper	137	50YrSCS24Hr	0.42	91.33	91.66	91.60	91.70	0.009574	0.92	0.46	2.33	0.66
River 1	Reach 1-Upper	137	100YrSCS24Hr	0.49	91.33	91.69	91.62	91.73	0.009283	0.95	0.52	2.46	0.66
River 1	Reach 1-Upper	116	2YrCHI3Hr	0.08	91.23	91.38	91.32	91.39	0.003082	0.36	0.22	2.06	0.35
River 1	Reach 1-Upper	116	5YrCHI3Hr	0.15	91.23	91.43	91.35	91.44	0.002930	0.42	0.35	2.36	0.35
River 1	Reach 1-Upper	116	10YrCHI3Hr	0.20	91.23	91.47	91.37	91.48	0.002864	0.46	0.43	2.55	0.36
River 1	Reach 1-Upper	116	25YrCHI3Hr	0.27	91.23	91.51	91.39	91.52	0.002818	0.50	0.54	2.77	0.36
River 1	Reach 1-Upper	116	50YrCHI3Hr	0.32	91.23	91.54	91.41	91.55	0.002807	0.52	0.62	2.92	0.36
River 1	Reach 1-Upper	116	100YrCHI3Hr	0.38	91.23	91.56	91.42	91.58	0.002814	0.55	0.70	3.06	0.37
River 1	Reach 1-Upper	116	2YrSCS24Hr	0.13	91.23	91.42	91.34	91.43	0.002964	0.41	0.31	2.29	0.35
River 1	Reach 1-Upper	116	5YrSCS24Hr	0.22	91.23	91.48	91.37	91.49	0.002843	0.47	0.46	2.61	0.36
River 1	Reach 1-Upper	116	10YrSCS24Hr	0.28	91.23	91.51	91.39	91.53	0.002817	0.50	0.55	2.79	0.36
River 1	Reach 1-Upper	116	25YrSCS24Hr	0.36	91.23	91.55	91.42	91.57	0.002792	0.54	0.66	3.00	0.37
River 1	Reach 1-Upper	116	50YrSCS24Hr	0.42	91.23	91.58	91.43	91.60	0.002600	0.55	0.76	3.16	0.36
River 1	Reach 1-Upper	116	100YrSCS24Hr	0.49	91.23	91.61	91.45	91.63	0.002607	0.58	0.85	3.28	0.36
River 1	Reach 1-Upper	95	2YrCHI3Hr	0.08	91.07	91.28	91.23	91.29	0.006001	0.51	0.16	1.35	0.48
River 1	Reach 1-Upper	95	5YrCHI3Hr	0.15	91.07	91.33	91.27	91.35	0.006981	0.63	0.23	1.60	0.53
River 1	Reach 1-Upper	95	10YrCHI3Hr	0.20	91.07	91.36	91.30	91.39	0.007514	0.71	0.28	1.73	0.56
River 1	Reach 1-Upper	95	25YrCHI3Hr	0.27	91.07	91.39	91.33	91.43	0.008051	0.78	0.34	1.89	0.59
River 1	Reach 1-Upper	95	50YrCHI3Hr	0.32	91.07	91.42	91.35	91.45	0.008531	0.84	0.38	1.99	0.61
River 1	Reach 1-Upper	95	100YrCHI3Hr	0.38	91.07	91.42	91.37	91.47	0.011364	0.98	0.39	2.01	0.71
River 1	Reach 1-Upper	95	2YrSCS24Hr	0.13	91.07	91.32	91.26	91.34	0.006833	0.61	0.21	1.53	0.52
River 1	Reach 1-Upper	95	5YrSCS24Hr	0.22	91.07	91.37	91.30	91.40	0.007484	0.72	0.30	1.78	0.56
River 1	Reach 1-Upper	95	10YrSCS24Hr	0.28	91.07	91.40	91.33	91.43	0.008260	0.80	0.35	1.90	0.60
River 1	Reach 1-Upper	95	25YrSCS24Hr	0.36	91.07	91.43	91.36	91.47	0.008800	0.87	0.41	2.08	0.63
River 1	Reach 1-Upper	95	50YrSCS24Hr	0.42	91.07	91.39	91.38	91.47	0.022828	1.30	0.32	1.85	0.99
River 1	Reach 1-Upper	95	100YrSCS24Hr	0.49	91.07	91.41	91.41	91.50	0.022422	1.34	0.37	1.95	0.99
River 1	Reach 1-Upper	72	2YrCHI3Hr	0.08	90.91	91.00	91.00	91.03	0.030836	0.74	0.11	1.93	0.99
River 1	Reach 1-Upper	72	5YrCHI3Hr	0.15	90.91	91.03	91.03	91.07	0.028202	0.84	0.18	2.40	0.99
River 1	Reach 1-Upper	72	10YrCHI3Hr	0.20	90.91	91.05	91.05	91.09	0.027394	0.90	0.22	2.63	0.99
River 1	Reach 1-Upper	72	25YrCHI3Hr	0.27	90.91	91.07	91.07	91.12	0.026901	0.98	0.27	2.82	1.01
River 1	Reach 1-Upper	72	50YrCHI3Hr	0.32	90.91	91.08	91.08	91.14	0.025605	1.02	0.32	2.96	1.00
River 1	Reach 1-Upper	72	100YrCHI3Hr	0.38	90.91	91.11	91.10	91.16	0.016324	0.92	0.42	3.23	0.82
River 1	Reach 1-Upper	72	2YrSCS24Hr	0.13	90.91	91.02	91.02	91.06	0.027869	0.80	0.16	2.30	0.97
River 1	Reach 1-Upper	72	5YrSCS24Hr	0.22	90.91	91.05	91.05	91.10	0.028793	0.94	0.23	2.67	1.02
River 1	Reach 1-Upper	72	10YrSCS24Hr	0.28	90.91	91.07	91.07	91.12	0.025957	0.98	0.28	2.86	0.99
River 1	Reach 1-Upper	72	25YrSCS24Hr	0.36	90.91	91.09	91.09	91.15	0.025859	1.06	0.34	3.02	1.01
River 1	Reach 1-Upper	72	50YrSCS24Hr	0.42	90.91	91.17	91.11	91.19	0.006772	0.70	0.60	3.69	0.55
River 1	Reach 1-Upper	72	100YrSCS24Hr	0.49	90.91	91.24	91.12	91.26	0.002972	0.55	0.89	4.14	0.38
River 1	Reach 1-Lower	56	2YrCHI3Hr	0.14	90.47	90.73	90.57	90.73	0.000365	0.19	0.73	10.09	0.13
River 1	Reach 1-Lower	56	5YrCHI3Hr	0.26	90.47	90.84	90.60	90.85	0.000293	0.23	1.14	14.27	0.13
River 1	Reach 1-Lower	56	10YrCHI3Hr	0.36	90.47	90.92	90.62	90.92	0.000277	0.26	1.40	17.00	0.13
River 1	Reach 1-Lower	56	25YrCHI3Hr	0.49	90.47	91.01	90.64	91.01	0.000267	0.29	1.71	19.79	0.13
River 1	Reach 1-Lower	56	50YrCHI3Hr	0.60	90.47	91.07	90.66	91.08	0.000264	0.31	1.93	20.02	0.13
River 1	Reach 1-Lower	56	100YrCHI3Hr	0.72	90.47	91.13	90.68	91.14	0.000264	0.34	2.15	20.02	0.14
River 1	Reach 1-Lower	56	2YrSCS24Hr	0.23	90.47	90.82	90.59	90.82	0.000307	0.22	1.05	13.08	0.13
River 1	Reach 1-Lower	56	5YrSCS24Hr	0.40	90.47	90.95	90.63	90.95	0.000273	0.27	1.50	18.26	0.13
River 1	Reach 1-Lower	56	10YrSCS24Hr	0.52	90.47	91.02	90.65	91.02	0.000269	0.29	1.75	19.92	0.13
River 1	Reach 1-Lower	56	25YrSCS24Hr	0.68	90.47	91.11	90.67	91.12	0.000263	0.33	2.07	20.02	0.14
River 1	Reach 1-Lower	56	50YrSCS24Hr	0.80	90.47	91.17	90.70	91.18	0.000261	0.35	2.30	20.02	0.14
River 1	Reach 1-Lower	56	100YrSCS24Hr	0.94	90.47	91.24	90.71	91.25	0.000262	0.37	2.53	20.02	0.14
River 1	Reach 1-Lower	50		Culvert									
River 1	Reach 1-Lower	38	2YrCHI3Hr	0.14	90.46	90.57	90.53	90.58	0.004969	0.42	0.33	30.00	0.43
River 1	Reach 1-Lower	38	5YrCHI3Hr	0.26	90.46	90.60	90.55	90.62	0.006999	0.60	0.44	34.38	0.54
River 1	Reach 1-Lower	38	10YrCHI3Hr	0.36	90.46	90.61	90.57	90.64	0.008612	0.72	0.50	35.69	0.61
River 1	Reach 1-Lower	38	25YrCHI3Hr	0.49	90.46	90.63	90.60	90.67	0.010692	0.87	0.56	36.54	0.70
River 1	Reach 1-Lower	38	50YrCHI3Hr	0.60	90.46	90.64	90.62	90.69	0.012409	0.99	0.61	36.97	0.76
River 1	Reach 1-Lower	38	100YrCHI3Hr	0.72	90.46	90.66	90.64	90.72	0.014104	1.11	0.65	37.73	0.82
River 1	Reach 1-Lower	38	2YrSCS24Hr	0.23	90.46	90.59	90.55	90.61	0.006395	0.56	0.42	33.55	0.51
River 1	Reach 1-Lower	38	5YrSCS24Hr	0.40	90.46	90.62	90.58	90.65	0.009230	0.77	0.52	36.26	0.64
River 1	Reach 1-Lower	38	10YrSCS24Hr	0.52	90.46	90.64	90.60	90.68	0.011069	0.90	0.57	36.60	0.71
River 1	Reach 1-Lower	38	25YrSCS24Hr	0.68	90.46	90.65	90.63	90.71	0.013373	1.06	0.64	37.45	0.79
River 1	Reach 1-Lower	38	50YrSCS24Hr	0.80	90.46	90.66	90.64	90.74	0.015442	1.19	0.68	38.06	0.86
River 1	Reach 1-Lower	38	100YrSCS24Hr	0.94	90.46	90.67	90.66	90.76	0.018005	1.32	0.71	38.54	0.94
River 1	Reach 1-Lower	0	2YrCHI3Hr	0.14	90.42	90.50	90.46	90.50	0.001001	0.13	1.06	18.74	0.18
River 1	Reach 1-Lower	0	5YrCHI3Hr	0.26	90.42	90.53	90.47	90.53	0.001000	0.17	1.59	20.04	0.19
River 1	Reach 1-Lower	0	10YrCHI3Hr	0.36	90.42	90.54	90.48	90.55	0.001000	0.19	1.92	20.29	0.19

HEC-RAS Plan: 20250603-Pre_Dev_v01 (Continued)

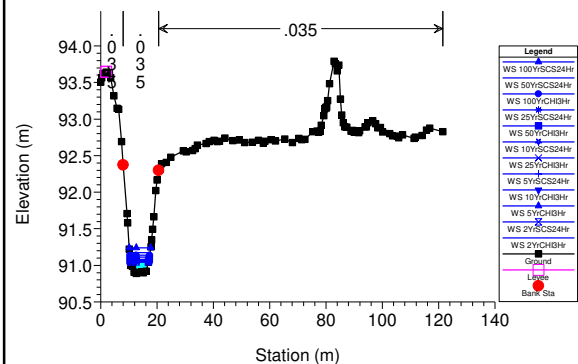
River	Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
River 1	Reach 1-Lower	0	25YrCHI3Hr	0.49	90.42	90.56	90.49	90.57	0.001001	0.21	2.33	20.58	0.20
River 1	Reach 1-Lower	0	50YrCHI3Hr	0.60	90.42	90.58	90.49	90.58	0.001000	0.23	2.64	20.80	0.20
River 1	Reach 1-Lower	0	100YrCHI3Hr	0.72	90.42	90.59	90.50	90.60	0.001000	0.24	2.98	21.46	0.21
River 1	Reach 1-Lower	0	2YrSCS24Hr	0.23	90.42	90.52	90.46	90.52	0.001000	0.16	1.47	19.96	0.19
River 1	Reach 1-Lower	0	5YrSCS24Hr	0.40	90.42	90.55	90.48	90.55	0.001001	0.20	2.05	20.38	0.20
River 1	Reach 1-Lower	0	10YrSCS24Hr	0.52	90.42	90.57	90.48	90.57	0.001001	0.22	2.40	20.63	0.20
River 1	Reach 1-Lower	0	25YrSCS24Hr	0.68	90.42	90.59	90.49	90.59	0.001000	0.24	2.85	21.31	0.21
River 1	Reach 1-Lower	0	50YrSCS24Hr	0.80	90.42	90.60	90.50	90.61	0.001001	0.25	3.18	21.58	0.21
River 1	Reach 1-Lower	0	100YrSCS24Hr	0.94	90.42	90.62	90.51	90.62	0.001000	0.27	3.51	21.78	0.21



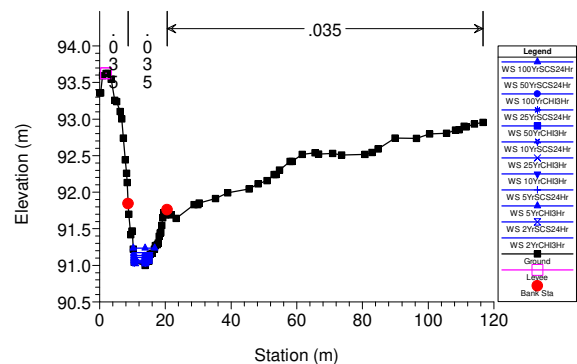




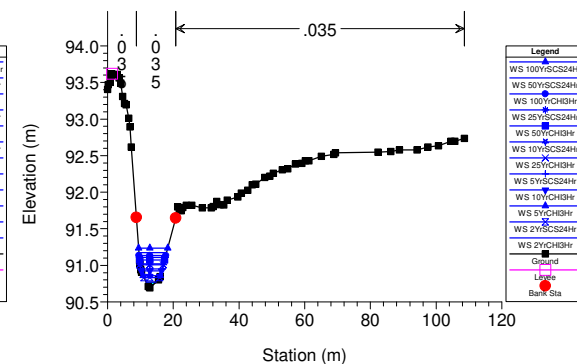
Eagleson_Ditch_v01 Plan: 20250603-Post_Dev_v01 2025-06-04



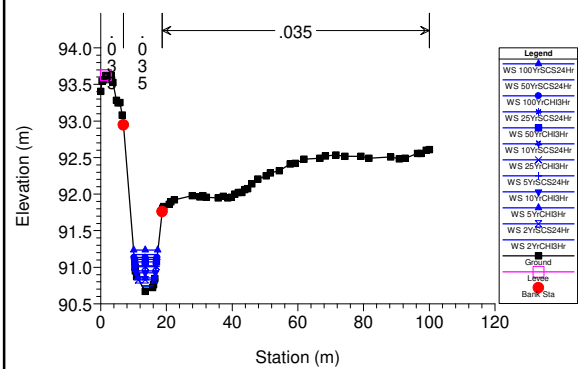
Eagleson_Ditch_v01 Plan: 20250603-Post_Dev_v01 2025-06-04



Eagleson_Ditch_v01 Plan: 20250603-Post_Dev_v01 2025-06-04



Eagleson_Ditch_v01 Plan: 20250603-Post_Dev_v01 2025-06-04



River	Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
River 2	Reach 2	224	2YrCHI3Hr	0.02	91.68	91.76	91.71	91.76	0.000697	0.09	0.23	5.59	0.14
River 2	Reach 2	224	5YrCHI3Hr	0.03	91.68	91.77	91.72	91.77	0.000738	0.10	0.31	6.45	0.15
River 2	Reach 2	224	10YrCHI3Hr	0.04	91.68	91.78	91.72	91.78	0.000754	0.11	0.34	6.51	0.15
River 2	Reach 2	224	25YrCHI3Hr	0.05	91.68	91.78	91.73	91.79	0.000756	0.12	0.39	6.61	0.16
River 2	Reach 2	224	50YrCHI3Hr	0.06	91.68	91.79	91.73	91.79	0.000763	0.13	0.44	6.71	0.16
River 2	Reach 2	224	100YrCHI3Hr	0.07	91.68	91.80	91.74	91.80	0.000773	0.14	0.50	6.81	0.16
River 2	Reach 2	224	2YrSCS24Hr	0.02	91.68	91.76	91.72	91.76	0.000717	0.09	0.25	5.79	0.14
River 2	Reach 2	224	5YrSCS24Hr	0.04	91.68	91.78	91.73	91.78	0.000753	0.11	0.35	6.53	0.15
River 2	Reach 2	224	10YrSCS24Hr	0.05	91.68	91.79	91.73	91.79	0.000757	0.12	0.41	6.65	0.16
River 2	Reach 2	224	25YrSCS24Hr	0.07	91.68	91.80	91.74	91.80	0.000769	0.14	0.48	6.78	0.16
River 2	Reach 2	224	50YrSCS24Hr	0.08	91.68	91.81	91.74	91.81	0.000794	0.15	0.54	6.88	0.17
River 2	Reach 2	224	100YrSCS24Hr	0.09	91.68	91.81	91.75	91.82	0.000800	0.16	0.60	6.99	0.17
River 2	Reach 2	199	2YrCHI3Hr	0.02	91.68	91.75	91.71	91.75	0.000471	0.07	0.28	6.87	0.12
River 2	Reach 2	199	5YrCHI3Hr	0.03	91.68	91.76	91.71	91.76	0.000460	0.08	0.37	7.09	0.12
River 2	Reach 2	199	10YrCHI3Hr	0.04	91.68	91.76	91.72	91.76	0.000521	0.09	0.39	7.17	0.13
River 2	Reach 2	199	25YrCHI3Hr	0.05	91.68	91.77	91.72	91.77	0.000549	0.10	0.45	7.32	0.13
River 2	Reach 2	199	50YrCHI3Hr	0.06	91.68	91.78	91.72	91.78	0.000569	0.11	0.50	7.42	0.14
River 2	Reach 2	199	100YrCHI3Hr	0.07	91.68	91.78	91.73	91.78	0.000591	0.12	0.56	7.51	0.14
River 2	Reach 2	199	2YrSCS24Hr	0.02	91.68	91.75	91.71	91.75	0.000474	0.08	0.30	6.91	0.12
River 2	Reach 2	199	5YrSCS24Hr	0.04	91.68	91.76	91.72	91.76	0.000522	0.10	0.41	7.20	0.13
River 2	Reach 2	199	10YrSCS24Hr	0.05	91.68	91.77	91.72	91.77	0.000558	0.11	0.47	7.37	0.14
River 2	Reach 2	199	25YrSCS24Hr	0.07	91.68	91.78	91.72	91.78	0.000582	0.12	0.55	7.49	0.14
River 2	Reach 2	199	50YrSCS24Hr	0.08	91.68	91.79	91.73	91.79	0.000628	0.13	0.60	7.57	0.15
River 2	Reach 2	199	100YrSCS24Hr	0.09	91.68	91.80	91.73	91.80	0.000634	0.14	0.66	7.67	0.15
River 2	Reach 2	174	2YrCHI3Hr	0.02	91.68	91.71	91.70	91.72	0.008871	0.23	0.09	3.47	0.47
River 2	Reach 2	174	5YrCHI3Hr	0.03	91.68	91.72	91.71	91.72	0.009858	0.28	0.11	3.63	0.51
River 2	Reach 2	174	10YrCHI3Hr	0.04	91.68	91.72	91.71	91.73	0.009862	0.30	0.12	3.70	0.51
River 2	Reach 2	174	25YrCHI3Hr	0.05	91.68	91.73	91.72	91.73	0.010482	0.33	0.14	3.80	0.54
River 2	Reach 2	174	50YrCHI3Hr	0.06	91.68	91.73	91.72	91.74	0.010789	0.35	0.16	3.90	0.56
River 2	Reach 2	174	100YrCHI3Hr	0.07	91.68	91.74	91.72	91.75	0.011338	0.38	0.18	3.99	0.58
River 2	Reach 2	174	2YrSCS24Hr	0.02	91.68	91.71	91.70	91.72	0.009099	0.24	0.09	3.51	0.48
River 2	Reach 2	174	5YrSCS24Hr	0.04	91.68	91.73	91.71	91.73	0.009102	0.29	0.13	3.75	0.50
River 2	Reach 2	174	10YrSCS24Hr	0.05	91.68	91.73	91.72	91.74	0.010830	0.34	0.15	3.84	0.55
River 2	Reach 2	174	25YrSCS24Hr	0.07	91.68	91.74	91.72	91.74	0.010024	0.36	0.18	4.01	0.55
River 2	Reach 2	174	50YrSCS24Hr	0.08	91.68	91.74	91.73	91.75	0.010794	0.40	0.20	4.08	0.57
River 2	Reach 2	174	100YrSCS24Hr	0.09	91.68	91.75	91.73	91.76	0.010716	0.42	0.22	4.15	0.58
River 2	Reach 2	149	2YrCHI3Hr	0.02	91.22	91.26	91.26	91.26	0.055689	0.39	0.05	3.77	1.06
River 2	Reach 2	149	5YrCHI3Hr	0.03	91.22	91.26	91.26	91.27	0.043989	0.40	0.08	4.47	0.97
River 2	Reach 2	149	10YrCHI3Hr	0.04	91.22	91.26	91.26	91.27	0.044110	0.43	0.09	4.54	0.99
River 2	Reach 2	149	25YrCHI3Hr	0.05	91.22	91.27	91.27	91.28	0.039832	0.45	0.10	4.68	0.97
River 2	Reach 2	149	50YrCHI3Hr	0.06	91.22	91.27	91.27	91.28	0.037244	0.47	0.12	4.80	0.95
River 2	Reach 2	149	100YrCHI3Hr	0.07	91.22	91.27	91.27	91.29	0.034157	0.49	0.14	4.94	0.93
River 2	Reach 2	149	2YrSCS24Hr	0.02	91.22	91.26	91.26	91.26	0.052399	0.39	0.06	3.96	1.03
River 2	Reach 2	149	5YrSCS24Hr	0.04	91.22	91.26	91.26	91.27	0.052134	0.46	0.08	4.53	1.07
River 2	Reach 2	149	10YrSCS24Hr	0.05	91.22	91.27	91.27	91.28	0.037535	0.46	0.11	4.74	0.95
River 2	Reach 2	149	25YrSCS24Hr	0.07	91.22	91.27	91.27	91.29	0.044620	0.53	0.13	4.83	1.05
River 2	Reach 2	149	50YrSCS24Hr	0.08	91.22	91.28	91.28	91.29	0.037650	0.53	0.15	5.00	0.98
River 2	Reach 2	149	100YrSCS24Hr	0.09	91.22	91.28	91.28	91.30	0.038788	0.57	0.16	5.05	1.01
River 2	Reach 2	124	2YrCHI3Hr	0.02	90.90	91.05	90.93	91.05	0.000047	0.04	0.51	5.19	0.04
River 2	Reach 2	124	5YrCHI3Hr	0.03	90.90	91.06	90.94	91.06	0.000089	0.06	0.55	5.84	0.06
River 2	Reach 2	124	10YrCHI3Hr	0.04	90.90	91.06	90.94	91.06	0.000122	0.06	0.59	6.56	0.07
River 2	Reach 2	124	25YrCHI3Hr	0.05	90.90	91.07	90.95	91.07	0.000154	0.07	0.64	6.76	0.08
River 2	Reach 2	124	50YrCHI3Hr	0.06	90.90	91.08	90.95	91.08	0.000148	0.08	0.74	7.10	0.08
River 2	Reach 2	124	100YrCHI3Hr	0.07	90.90	91.14	90.95	91.14	0.000055	0.06	1.18	8.05	0.05
River 2	Reach 2	124	2YrSCS24Hr	0.02	90.90	91.05	90.93	91.05	0.000054	0.04	0.51	5.22	0.05
River 2	Reach 2	124	5YrSCS24Hr	0.04	90.90	91.06	90.94	91.06	0.000129	0.07	0.60	6.60	0.07
River 2	Reach 2	124	10YrSCS24Hr	0.05	90.90	91.07	90.95	91.07	0.000166	0.08	0.66	6.83	0.08
River 2	Reach 2	124	25YrSCS24Hr	0.07	90.90	91.11	90.95	91.12	0.000090	0.07	0.98	7.81	0.06
River 2	Reach 2	124	50YrSCS24Hr	0.08	90.90	91.18	90.96	91.18	0.000036	0.05	1.48	8.41	0.04
River 2	Reach 2	124	100YrSCS24Hr	0.09	90.90	91.24	90.96	91.24	0.000020	0.05	2.03	9.41	0.03
River 2	Reach 2	99	2YrCHI3Hr	0.02	90.90	91.05	90.93	91.05	0.000014	0.02	0.84	7.48	0.02
River 2	Reach 2	99	5YrCHI3Hr	0.03	90.90	91.05	90.93	91.05	0.000024	0.03	0.91	7.55	0.03
River 2	Reach 2	99	10YrCHI3Hr	0.04	90.90	91.06	90.93	91.06	0.000030	0.04	0.94	7.58	0.04
River 2	Reach 2	99	25YrCHI3Hr	0.05	90.90	91.07	90.93	91.07	0.000041	0.05	1.00	7.64	0.04
River 2	Reach 2	99	50YrCHI3Hr	0.06	90.90	91.08	90.94	91.08	0.000043	0.05	1.11	7.76	0.04
River 2	Reach 2	99	100YrCHI3Hr	0.07	90.90	91.14	90.94	91.14	0.000021	0.04	1.57	8.21	0.03
River 2	Reach 2	99	2YrSCS24Hr	0.02	90.90	91.05	90.92	91.05	0.000016	0.03	0.86	7.49	0.03
River 2	Reach 2	99	5YrSCS24Hr	0.04	90.90	91.06	90.93	91.06	0.000032	0.04	0.96	7.60	0.04
River 2	Reach 2	99	10YrSCS24Hr	0.05	90.90	91.07	90.94	91.07	0.000045	0.05	1.02	7.67	0.04
River 2	Reach 2	99	25YrSCS24Hr	0.07	90.90	91.11	90.94	91.11	0.000030	0.05	1.37	8.01	0.04
River 2	Reach 2	99	50YrSCS24Hr	0.08	90.90	91.18	90.94	91.18	0.000016	0.04	1.88	8.49	0.03
River 2	Reach 2	99	100YrSCS24Hr	0.09	90.90	91.24	90.95	91.24	0.000010	0.04	2.43	8.94	0.02
River 2	Reach 2	74	2YrCHI3Hr	0.02	90.89	91.05	90.92	91.05	0.000016	0.03	0.76	6.41	0.03
River 2	Reach 2	74	5YrCHI3Hr	0.03	90.89	91.05	90.92	91.05	0.000029	0.04	0.81	6.48	0.03
River 2	Reach 2	74	10YrCHI3Hr	0.04	90.89	91.06	90.92	91.06	0.000037	0.04	0.84	6.52	0.04
River 2	Reach 2	74	25YrCHI3Hr	0.05	90.89	91.07	90.93	91.07	0.000050	0.05	0.89	6.57	0.05
River 2	Reach 2	74	50YrCHI3Hr	0.06	90.89	91.08	90.93	91.08	0.000053	0.06	0.98	6.68	0.05
River 2	Reach 2	74	100YrCHI3Hr	0.07	90.89	91.14	90.93	91.14	0.000027	0.05	1.39	7.06	0.04
River 2	Reach 2	74	2YrSCS24Hr	0.02	90.89	91.05	90.92	91.05	0.000019	0.03	0.77	6.42	0.03
River 2	Reach 2	74	5YrSCS24Hr	0.04	90.89	91.06	90.92	91.06	0.000039	0.05	0.85	6.53	0.04
River 2	Reach 2	74	10YrSCS24Hr	0.05	90.89	91.07	90.93	91.07	0.000055	0.06	0.91	6.59	0.05
River 2	Reach 2	74	25YrSCS24Hr	0.07	90.89	91.11	90.93	91.11	0.000038	0.05	1.21	6.91	0.04
River 2	Reach 2	74	50YrSCS24Hr	0.08	90.89	91.18	90.93	91.18	0.000020	0.05	1.65	7.28	0.03
River 2	Reach 2	74	100YrSCS24Hr	0.09	90.89	91.24	90.94	91.24	0.000013	0.04	2.12	7.64	0.03

HEC-RAS Plan: 20250603-Post_Dev_v01 (Continued)

River	Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
River 2	Reach 2	49	2YrCHI3Hr	0.02	91.00	91.03	91.03	91.04	0.054210	0.44	0.05	2.78	1.08
River 2	Reach 2	49	5YrCHI3Hr	0.03	91.00	91.04	91.04	91.05	0.044076	0.45	0.07	3.35	1.00
River 2	Reach 2	49	10YrCHI3Hr	0.04	91.00	91.04	91.04	91.05	0.038624	0.46	0.08	3.50	0.96
River 2	Reach 2	49	25YrCHI3Hr	0.05	91.00	91.05	91.05	91.06	0.042954	0.52	0.09	3.52	1.03
River 2	Reach 2	49	50YrCHI3Hr	0.06	91.00	91.07	91.05	91.08	0.007772	0.32	0.18	3.99	0.48
River 2	Reach 2	49	100YrCHI3Hr	0.07	91.00	91.14	91.05	91.14	0.000594	0.15	0.48	4.93	0.15
River 2	Reach 2	49	2YrSCS24Hr	0.02	91.00	91.04	91.04	91.04	0.038802	0.40	0.06	3.06	0.93
River 2	Reach 2	49	5YrSCS24Hr	0.04	91.00	91.04	91.04	91.06	0.043713	0.48	0.08	3.50	1.02
River 2	Reach 2	49	10YrSCS24Hr	0.05	91.00	91.05	91.05	91.06	0.037160	0.51	0.10	3.53	0.97
River 2	Reach 2	49	25YrSCS24Hr	0.07	91.00	91.11	91.05	91.11	0.001479	0.19	0.34	4.59	0.23
River 2	Reach 2	49	50YrSCS24Hr	0.08	91.00	91.17	91.06	91.17	0.000297	0.12	0.68	5.81	0.11
River 2	Reach 2	49	100YrSCS24Hr	0.09	91.00	91.24	91.06	91.24	0.000105	0.09	1.07	6.54	0.07
River 2	Reach 2	28	2YrCHI3Hr	0.02	90.69	90.77	90.73	90.77	0.001515	0.14	0.13	3.11	0.21
River 2	Reach 2	28	5YrCHI3Hr	0.03	90.69	90.86	90.75	90.86	0.000133	0.07	0.50	5.25	0.07
River 2	Reach 2	28	10YrCHI3Hr	0.05	90.69	90.93	90.75	90.93	0.000046	0.05	0.90	6.29	0.04
River 2	Reach 2	28	25YrCHI3Hr	0.06	90.69	91.01	90.76	91.01	0.000020	0.04	1.46	7.11	0.03
River 2	Reach 2	28	50YrCHI3Hr	0.08	90.69	91.07	90.77	91.07	0.000013	0.04	1.93	7.65	0.03
River 2	Reach 2	28	100YrCHI3Hr	0.09	90.69	91.14	90.78	91.14	0.000009	0.04	2.43	8.13	0.02
River 2	Reach 2	28	2YrSCS24Hr	0.03	90.69	90.83	90.74	90.83	0.000261	0.08	0.37	4.76	0.10
River 2	Reach 2	28	5YrSCS24Hr	0.05	90.69	90.95	90.76	90.95	0.000035	0.05	1.06	6.56	0.04
River 2	Reach 2	28	10YrSCS24Hr	0.07	90.69	91.02	90.76	91.02	0.000019	0.04	1.55	7.24	0.03
River 2	Reach 2	28	25YrSCS24Hr	0.09	90.69	91.11	90.77	91.11	0.000011	0.04	2.21	7.92	0.02
River 2	Reach 2	28	50YrSCS24Hr	0.11	90.69	91.17	90.78	91.17	0.000008	0.04	2.74	8.41	0.02
River 2	Reach 2	28	100YrSCS24Hr	0.13	90.69	91.24	90.79	91.24	0.000007	0.04	3.29	8.89	0.02
River 2	Reach 2	7	2YrCHI3Hr	0.02	90.67	90.75	90.71	90.75	0.001146	0.12	0.15	3.37	0.18
River 2	Reach 2	7	5YrCHI3Hr	0.03	90.67	90.86	90.72	90.86	0.000063	0.05	0.62	5.26	0.05
River 2	Reach 2	7	10YrCHI3Hr	0.05	90.67	90.92	90.73	90.92	0.000028	0.05	1.02	5.92	0.04
River 2	Reach 2	7	25YrCHI3Hr	0.06	90.67	91.01	90.73	91.01	0.000014	0.04	1.54	6.42	0.03
River 2	Reach 2	7	50YrCHI3Hr	0.08	90.67	91.07	90.74	91.07	0.000010	0.04	1.96	6.69	0.02
River 2	Reach 2	7	100YrCHI3Hr	0.09	90.67	91.14	90.74	91.14	0.000008	0.04	2.39	6.96	0.02
River 2	Reach 2	7	2YrSCS24Hr	0.03	90.67	90.83	90.72	90.83	0.000105	0.06	0.49	4.81	0.06
River 2	Reach 2	7	5YrSCS24Hr	0.05	90.67	90.95	90.73	90.95	0.000023	0.05	1.17	6.11	0.03
River 2	Reach 2	7	10YrSCS24Hr	0.07	90.67	91.02	90.73	91.02	0.000014	0.04	1.63	6.48	0.03
River 2	Reach 2	7	25YrSCS24Hr	0.09	90.67	91.11	90.74	91.11	0.000010	0.04	2.20	6.84	0.02
River 2	Reach 2	7	50YrSCS24Hr	0.11	90.67	91.17	90.75	91.17	0.000008	0.04	2.66	7.12	0.02
River 2	Reach 2	7	100YrSCS24Hr	0.13	90.67	91.24	90.76	91.24	0.000007	0.04	3.11	7.38	0.02
River 1	Reach 1-Upper	908	2YrCHI3Hr	0.02	94.14	94.23	94.19	94.23	0.001752	0.17	0.14	2.59	0.23
River 1	Reach 1-Upper	908	5YrCHI3Hr	0.03	94.14	94.24	94.19	94.24	0.001946	0.19	0.17	2.76	0.25
River 1	Reach 1-Upper	908	10YrCHI3Hr	0.04	94.14	94.24	94.20	94.25	0.002043	0.20	0.18	2.85	0.26
River 1	Reach 1-Upper	908	25YrCHI3Hr	0.04	94.14	94.25	94.20	94.25	0.002127	0.22	0.20	2.96	0.27
River 1	Reach 1-Upper	908	50YrCHI3Hr	0.05	94.14	94.26	94.20	94.26	0.002210	0.23	0.22	3.07	0.28
River 1	Reach 1-Upper	908	100YrCHI3Hr	0.06	94.14	94.27	94.21	94.27	0.002252	0.24	0.25	3.23	0.28
River 1	Reach 1-Upper	908	2YrSCS24Hr	0.03	94.14	94.23	94.19	94.24	0.001856	0.18	0.15	2.68	0.24
River 1	Reach 1-Upper	908	5YrSCS24Hr	0.04	94.14	94.24	94.20	94.25	0.002043	0.20	0.18	2.85	0.26
River 1	Reach 1-Upper	908	10YrSCS24Hr	0.04	94.14	94.25	94.20	94.25	0.002124	0.22	0.19	2.94	0.27
River 1	Reach 1-Upper	908	25YrSCS24Hr	0.05	94.14	94.26	94.20	94.26	0.002199	0.23	0.22	3.05	0.27
River 1	Reach 1-Upper	908	50YrSCS24Hr	0.06	94.14	94.26	94.21	94.26	0.002260	0.24	0.23	3.15	0.28
River 1	Reach 1-Upper	908	100YrSCS24Hr	0.06	94.14	94.27	94.21	94.27	0.002214	0.25	0.26	3.28	0.28
River 1	Reach 1-Upper	887	2YrCHI3Hr	0.02	94.10	94.17	94.15	94.17	0.006295	0.25	0.10	2.71	0.42
River 1	Reach 1-Upper	887	5YrCHI3Hr	0.03	94.10	94.18	94.15	94.18	0.005292	0.25	0.13	2.98	0.39
River 1	Reach 1-Upper	887	10YrCHI3Hr	0.04	94.10	94.18	94.15	94.19	0.004912	0.26	0.14	3.14	0.38
River 1	Reach 1-Upper	887	25YrCHI3Hr	0.04	94.10	94.19	94.16	94.19	0.004656	0.26	0.16	3.30	0.38
River 1	Reach 1-Upper	887	50YrCHI3Hr	0.05	94.10	94.19	94.16	94.20	0.004554	0.27	0.18	3.46	0.38
River 1	Reach 1-Upper	887	100YrCHI3Hr	0.06	94.10	94.20	94.17	94.20	0.005462	0.31	0.20	3.56	0.42
River 1	Reach 1-Upper	887	2YrSCS24Hr	0.03	94.10	94.17	94.15	94.17	0.005714	0.25	0.11	2.85	0.40
River 1	Reach 1-Upper	887	5YrSCS24Hr	0.04	94.10	94.18	94.15	94.19	0.004912	0.26	0.14	3.14	0.38
River 1	Reach 1-Upper	887	10YrSCS24Hr	0.04	94.10	94.19	94.16	94.19	0.004513	0.26	0.16	3.29	0.37
River 1	Reach 1-Upper	887	25YrSCS24Hr	0.05	94.10	94.19	94.16	94.20	0.004587	0.27	0.18	3.44	0.38
River 1	Reach 1-Upper	887	50YrSCS24Hr	0.06	94.10	94.20	94.16	94.20	0.004954	0.29	0.19	3.52	0.39
River 1	Reach 1-Upper	887	100YrSCS24Hr	0.06	94.10	94.20	94.17	94.20	0.006457	0.33	0.19	3.52	0.45
River 1	Reach 1-Upper	868	2YrCHI3Hr	0.02	93.96	94.03	94.01	94.04	0.007224	0.29	0.08	1.96	0.46
River 1	Reach 1-Upper	868	5YrCHI3Hr	0.03	93.96	94.04	94.02	94.04	0.009697	0.35	0.09	2.03	0.53
River 1	Reach 1-Upper	868	10YrCHI3Hr	0.04	93.96	94.04	94.02	94.05	0.011232	0.39	0.10	2.07	0.58
River 1	Reach 1-Upper	868	25YrCHI3Hr	0.04	93.96	94.04	94.03	94.05	0.012506	0.42	0.10	2.12	0.61
River 1	Reach 1-Upper	868	50YrCHI3Hr	0.05	93.96	94.05	94.03	94.06	0.013181	0.45	0.11	2.20	0.64
River 1	Reach 1-Upper	868	100YrCHI3Hr	0.06	93.96	94.06	94.04	94.07	0.008320	0.40	0.15	2.47	0.52
River 1	Reach 1-Upper	868	2YrSCS24Hr	0.03	93.96	94.04	94.02	94.04	0.008571	0.33	0.09	1.99	0.50
River 1	Reach 1-Upper	868	5YrSCS24Hr	0.04	93.96	94.04	94.02	94.05	0.011232	0.39	0.10	2.07	0.58
River 1	Reach 1-Upper	868	10YrSCS24Hr	0.04	93.96	94.04	94.03	94.05	0.012446	0.42	0.10	2.11	0.61
River 1	Reach 1-Upper	868	25YrSCS24Hr	0.05	93.96	94.05	94.03	94.06	0.012976	0.44	0.11	2.19	0.63
River 1	Reach 1-Upper	868	50YrSCS24Hr	0.06	93.96	94.06	94.04	94.06	0.011152	0.43	0.13	2.31	0.59
River 1	Reach 1-Upper	868	100YrSCS24Hr	0.06	93.96	94.07	94.04	94.08	0.006475	0.37	0.17	2.61	0.46
River 1	Reach 1-Upper	848	2YrCHI3Hr	0.02	93.87	93.93	93.91	93.93	0.004188	0.21	0.11	2.93	0.34
River 1	Reach 1-Upper	848	5YrCHI3Hr	0.03	93.87	93.94	93.91	93.95	0.002995	0.21	0.15	3.10	0.30
River 1	Reach 1-Upper	848	10YrCHI3Hr	0.04	93.87	93.95	93.92	93.95	0.002574	0.21	0.18	3.18	0.29
River 1	Reach 1-Upper	848	25YrCHI3Hr	0.04	93.87	93.96	93.92	93.96	0.002211	0.21	0.20	3.28	0.27
River 1	Reach 1-Upper	848	50YrCHI3Hr	0.05	93.87	93.97	93.92	93.97	0.002070	0.22	0.23	3.37	0.26
River 1	Reach 1-Upper	848	100YrCHI3Hr	0.06	93.87	93.96	93.93	93.97	0.003639	0.28	0.22	3.32	0.35
River 1	Reach 1-Upper	848	2YrSCS24Hr	0.03	93.87	93.94	93.91	93.94	0.003360	0.21	0.13	3.03	0.31
River 1	Reach 1-Upper	848	5YrSCS24Hr	0.04	93.87	93.95	93.92	93.95	0.002574	0.21	0.18	3.18	0.29
River 1	Reach 1-Upper	848	10YrSCS24Hr	0.04	93.87	93.96	93.92	93.96	0.002254	0.21	0.20	3.26	0.27
River 1	Reach 1-Upper	848	25YrSCS24Hr	0.05	93.87	93.97	93.92	93.97	0.002100	0.22	0.23	3.35	0.27
River 1	Reach 1-Upper	848	50YrSCS24Hr	0.06	93.87	93.97	93.92	93.97	0.002494	0.24	0.23	3.37	0.29

HEC-RAS Plan: 20250603-Post_Dev_v01 (Continued)

River	Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
River 1	Reach 1-Upper	848	100YrSCS24Hr	0.06	93.87	93.96	93.93	93.96	0.005013	0.31	0.20	3.26	0.41
River 1	Reach 1-Upper	828	2YrCHI3Hr	0.02	93.78	93.86	93.82	93.86	0.003210	0.19	0.12	2.95	0.30
River 1	Reach 1-Upper	828	5YrCHI3Hr	0.03	93.78	93.86	93.83	93.86	0.007085	0.28	0.11	2.81	0.45
River 1	Reach 1-Upper	828	10YrCHI3Hr	0.04	93.78	93.85	93.84	93.86	0.012962	0.37	0.10	2.61	0.60
River 1	Reach 1-Upper	828	25YrCHI3Hr	0.04	93.78	93.84	93.84	93.86	0.027482	0.51	0.08	2.34	0.87
River 1	Reach 1-Upper	828	50YrCHI3Hr	0.05	93.78	93.84	93.84	93.86	0.037796	0.60	0.08	2.33	1.02
River 1	Reach 1-Upper	828	100YrCHI3Hr	0.06	93.78	93.88	93.85	93.89	0.004443	0.29	0.20	3.38	0.38
River 1	Reach 1-Upper	828	2YrSCS24Hr	0.03	93.78	93.86	93.83	93.86	0.005209	0.24	0.12	2.83	0.39
River 1	Reach 1-Upper	828	5YrSCS24Hr	0.04	93.78	93.85	93.84	93.86	0.012962	0.37	0.10	2.61	0.60
River 1	Reach 1-Upper	828	10YrSCS24Hr	0.04	93.78	93.85	93.84	93.86	0.023615	0.48	0.09	2.40	0.81
River 1	Reach 1-Upper	828	25YrSCS24Hr	0.05	93.78	93.84	93.84	93.86	0.036015	0.59	0.08	2.34	0.99
River 1	Reach 1-Upper	828	50YrSCS24Hr	0.06	93.78	93.86	93.85	93.87	0.017759	0.46	0.12	2.91	0.71
River 1	Reach 1-Upper	828	100YrSCS24Hr	0.06	93.78	93.91	93.85	93.91	0.001940	0.23	0.28	3.55	0.26
River 1	Reach 1-Upper	807	2YrCHI3Hr	0.02	93.65	93.71	93.70	93.72	0.021814	0.43	0.06	1.70	0.76
River 1	Reach 1-Upper	807	5YrCHI3Hr	0.03	93.65	93.75	93.71	93.75	0.003849	0.25	0.13	2.40	0.35
River 1	Reach 1-Upper	807	10YrCHI3Hr	0.04	93.65	93.77	93.71	93.77	0.002057	0.21	0.18	2.79	0.26
River 1	Reach 1-Upper	807	25YrCHI3Hr	0.04	93.65	93.79	93.72	93.79	0.001125	0.17	0.25	3.25	0.20
River 1	Reach 1-Upper	807	50YrCHI3Hr	0.05	93.65	93.82	93.72	93.82	0.000498	0.14	0.35	3.78	0.14
River 1	Reach 1-Upper	807	100YrCHI3Hr	0.06	93.65	93.88	93.73	93.88	0.000155	0.11	0.61	5.55	0.08
River 1	Reach 1-Upper	807	2YrSCS24Hr	0.03	93.65	93.73	93.71	93.74	0.006535	0.29	0.10	2.12	0.44
River 1	Reach 1-Upper	807	5YrSCS24Hr	0.04	93.65	93.77	93.71	93.77	0.002057	0.21	0.18	2.79	0.26
River 1	Reach 1-Upper	807	10YrSCS24Hr	0.04	93.65	93.78	93.72	93.79	0.001247	0.18	0.23	3.18	0.21
River 1	Reach 1-Upper	807	25YrSCS24Hr	0.05	93.65	93.81	93.72	93.81	0.000553	0.15	0.34	3.70	0.15
River 1	Reach 1-Upper	807	50YrSCS24Hr	0.06	93.65	93.85	93.73	93.85	0.000265	0.12	0.47	4.27	0.11
River 1	Reach 1-Upper	807	100YrSCS24Hr	0.06	93.65	93.90	93.73	93.90	0.000106	0.10	0.75	6.37	0.07
River 1	Reach 1-Upper	789	2YrCHI3Hr	0.02	93.49	93.71	93.54	93.71	0.000038	0.06	0.43	3.55	0.04
River 1	Reach 1-Upper	789	5YrCHI3Hr	0.03	93.49	93.74	93.55	93.74	0.000038	0.06	0.51	4.05	0.04
River 1	Reach 1-Upper	789	10YrCHI3Hr	0.04	93.49	93.76	93.55	93.76	0.000038	0.07	0.56	4.37	0.04
River 1	Reach 1-Upper	789	25YrCHI3Hr	0.04	93.49	93.79	93.55	93.79	0.000038	0.07	0.61	4.73	0.04
River 1	Reach 1-Upper	789	50YrCHI3Hr	0.05	93.49	93.82	93.56	93.82	0.000035	0.07	0.68	5.23	0.04
River 1	Reach 1-Upper	789	100YrCHI3Hr	0.06	93.49	93.88	93.57	93.88	0.000027	0.07	0.83	5.99	0.04
River 1	Reach 1-Upper	789	2YrSCS24Hr	0.03	93.49	93.73	93.54	93.73	0.000037	0.06	0.48	3.83	0.04
River 1	Reach 1-Upper	789	5YrSCS24Hr	0.04	93.49	93.76	93.55	93.76	0.000038	0.07	0.56	4.37	0.04
River 1	Reach 1-Upper	789	10YrSCS24Hr	0.04	93.49	93.78	93.55	93.78	0.000038	0.07	0.60	4.67	0.04
River 1	Reach 1-Upper	789	25YrSCS24Hr	0.05	93.49	93.81	93.56	93.81	0.000036	0.07	0.67	5.15	0.04
River 1	Reach 1-Upper	789	50YrSCS24Hr	0.06	93.49	93.85	93.56	93.85	0.000031	0.07	0.75	5.62	0.04
River 1	Reach 1-Upper	789	100YrSCS24Hr	0.06	93.49	93.90	93.57	93.90	0.000024	0.07	0.88	6.26	0.04
River 1	Reach 1-Upper	764		Culvert									
River 1	Reach 1-Upper	759	2YrCHI3Hr	0.02	93.46	93.55	93.51	93.56	0.002355	0.23	0.10	2.03	0.28
River 1	Reach 1-Upper	759	5YrCHI3Hr	0.03	93.46	93.58	93.51	93.58	0.001375	0.22	0.14	2.40	0.23
River 1	Reach 1-Upper	759	10YrCHI3Hr	0.04	93.46	93.60	93.52	93.60	0.000932	0.21	0.18	2.67	0.19
River 1	Reach 1-Upper	759	25YrCHI3Hr	0.04	93.46	93.63	93.52	93.63	0.000592	0.19	0.22	3.05	0.16
River 1	Reach 1-Upper	759	50YrCHI3Hr	0.05	93.46	93.69	93.53	93.69	0.000264	0.16	0.31	3.75	0.11
River 1	Reach 1-Upper	759	100YrCHI3Hr	0.06	93.46	93.77	93.54	93.77	0.000125	0.14	0.43	4.71	0.08
River 1	Reach 1-Upper	759	2YrSCS24Hr	0.03	93.46	93.57	93.51	93.57	0.001859	0.23	0.12	2.20	0.26
River 1	Reach 1-Upper	759	5YrSCS24Hr	0.04	93.46	93.60	93.52	93.60	0.000932	0.21	0.18	2.67	0.19
River 1	Reach 1-Upper	759	10YrSCS24Hr	0.04	93.46	93.63	93.52	93.63	0.000639	0.20	0.21	2.98	0.17
River 1	Reach 1-Upper	759	25YrSCS24Hr	0.05	93.46	93.68	93.53	93.68	0.000285	0.16	0.30	3.67	0.12
River 1	Reach 1-Upper	759	50YrSCS24Hr	0.06	93.46	93.73	93.53	93.73	0.000174	0.15	0.37	4.24	0.09
River 1	Reach 1-Upper	759	100YrSCS24Hr	0.06	93.46	93.80	93.54	93.80	0.000105	0.13	0.47	5.36	0.08
River 1	Reach 1-Upper	743	2YrCHI3Hr	0.02	93.40	93.52	93.46	93.52	0.001463	0.21	0.11	1.84	0.23
River 1	Reach 1-Upper	743	5YrCHI3Hr	0.03	93.40	93.57	93.47	93.57	0.000686	0.19	0.17	2.25	0.17
River 1	Reach 1-Upper	743	10YrCHI3Hr	0.04	93.40	93.59	93.47	93.59	0.000494	0.18	0.20	2.53	0.15
River 1	Reach 1-Upper	743	25YrCHI3Hr	0.04	93.40	93.62	93.48	93.63	0.000350	0.17	0.25	2.92	0.13
River 1	Reach 1-Upper	743	50YrCHI3Hr	0.05	93.40	93.69	93.48	93.69	0.000183	0.15	0.33	4.20	0.10
River 1	Reach 1-Upper	743	100YrCHI3Hr	0.06	93.40	93.77	93.49	93.77	0.000101	0.14	0.44	5.44	0.08
River 1	Reach 1-Upper	743	2YrSCS24Hr	0.03	93.40	93.54	93.46	93.55	0.000951	0.20	0.14	2.05	0.19
River 1	Reach 1-Upper	743	5YrSCS24Hr	0.04	93.40	93.59	93.47	93.59	0.000494	0.18	0.20	2.53	0.15
River 1	Reach 1-Upper	743	10YrSCS24Hr	0.04	93.40	93.62	93.48	93.62	0.000370	0.18	0.24	2.85	0.13
River 1	Reach 1-Upper	743	25YrSCS24Hr	0.05	93.40	93.68	93.48	93.68	0.000195	0.15	0.32	4.01	0.10
River 1	Reach 1-Upper	743	50YrSCS24Hr	0.06	93.40	93.73	93.49	93.73	0.000132	0.14	0.38	4.86	0.08
River 1	Reach 1-Upper	743	100YrSCS24Hr	0.06	93.40	93.79	93.49	93.80	0.000089	0.14	0.47	6.32	0.07
River 1	Reach 1-Upper	733		Culvert									
River 1	Reach 1-Upper	728	2YrCHI3Hr	0.02	93.33	93.51	93.39	93.51	0.000306	0.13	0.19	1.87	0.11
River 1	Reach 1-Upper	728	5YrCHI3Hr	0.03	93.33	93.55	93.40	93.55	0.000233	0.13	0.24	2.16	0.10
River 1	Reach 1-Upper	728	10YrCHI3Hr	0.04	93.33	93.57	93.41	93.57	0.000202	0.14	0.27	2.34	0.10
River 1	Reach 1-Upper	728	25YrCHI3Hr	0.04	93.33	93.60	93.41	93.60	0.000169	0.14	0.32	2.57	0.09
River 1	Reach 1-Upper	728	50YrCHI3Hr	0.05	93.33	93.66	93.42	93.66	0.000110	0.13	0.39	2.99	0.08
River 1	Reach 1-Upper	728	100YrCHI3Hr	0.06	93.33	93.72	93.43	93.73	0.000076	0.12	0.49	3.52	0.07
River 1	Reach 1-Upper	728	2YrSCS24Hr	0.03	93.33	93.53	93.40	93.53	0.000264	0.13	0.21	2.01	0.11
River 1	Reach 1-Upper	728	5YrSCS24Hr	0.04	93.33	93.57	93.41	93.57	0.000202	0.14	0.27	2.34	0.10
River 1	Reach 1-Upper	728	10YrSCS24Hr	0.04	93.33	93.60	93.41	93.60	0.000174	0.14	0.31	2.53	0.09
River 1	Reach 1-Upper	728	25YrSCS24Hr	0.05	93.33	93.65	93.42	93.65	0.000113	0.13	0.39	2.94	0.08
River 1	Reach 1-Upper	728	50YrSCS24Hr	0.06	93.33	93.69	93.42	93.69	0.000090	0.12	0.44	3.25	0.07
River 1	Reach 1-Upper	728	100YrSCS24Hr	0.06	93.33	93.74	93.43	93.74	0.000070	0.12	0.52	3.70	0.06
River 1	Reach 1-Upper	715	2YrCHI3Hr	0.02	93.32	93.51	93.36	93.51	0.000138	0.10	0.24	2.70	0.08
River 1	Reach 1-Upper	715	5YrCHI3Hr	0.03	93.32	93.54	93.37	93.54	0.000123	0.11	0.29	3.09	0.08
River 1	Reach 1-Upper	715	10YrCHI3Hr	0.04	93.32	93.57	93.38	93.57	0.000114	0.11	0.32	3.33	0.08
River 1	Reach 1-Upper	715	25YrCHI3Hr	0.04	93.32	93.60	93.38	93.60	0.000102	0.12	0.37	3.63	0.07
River 1	Reach 1-Upper	715	50YrCHI3Hr	0.05	93.32	93.65	93.39	93.66	0.000072	0.11	0.44	4.19	0.06
River 1	Reach 1-Upper	715	100YrCHI3Hr	0.06	93.32	93.72	93.39	93.72	0.000054	0.11	0.54	4.88	0.06

HEC-RAS Plan: 20250603-Post_Dev_v01 (Continued)

River	Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
River 1	Reach 1-Upper	715	2YrSCS24Hr	0.03	93.32	93.52	93.37	93.53	0.000130	0.11	0.26	2.89	0.08
River 1	Reach 1-Upper	715	5YrSCS24Hr	0.04	93.32	93.57	93.38	93.57	0.000114	0.11	0.32	3.33	0.08
River 1	Reach 1-Upper	715	10YrSCS24Hr	0.04	93.32	93.59	93.38	93.59	0.000104	0.12	0.36	3.58	0.07
River 1	Reach 1-Upper	715	25YrSCS24Hr	0.05	93.32	93.65	93.39	93.65	0.000074	0.11	0.44	4.13	0.06
River 1	Reach 1-Upper	715	50YrSCS24Hr	0.06	93.32	93.69	93.39	93.69	0.000061	0.11	0.49	4.54	0.06
River 1	Reach 1-Upper	715	100YrSCS24Hr	0.06	93.32	93.74	93.40	93.74	0.000051	0.11	0.57	5.33	0.06
River 1	Reach 1-Upper	705	Culvert										
River 1	Reach 1-Upper	698	2YrCHI3Hr	0.02	93.24	93.32	93.30	93.33	0.011619	0.41	0.06	1.21	0.59
River 1	Reach 1-Upper	698	5YrCHI3Hr	0.03	93.24	93.32	93.31	93.33	0.017273	0.51	0.06	1.23	0.72
River 1	Reach 1-Upper	698	10YrCHI3Hr	0.04	93.24	93.32	93.31	93.34	0.025269	0.61	0.06	1.22	0.87
River 1	Reach 1-Upper	698	25YrCHI3Hr	0.04	93.24	93.41	93.32	93.41	0.001221	0.22	0.20	1.87	0.22
River 1	Reach 1-Upper	698	50YrCHI3Hr	0.05	93.24	93.51	93.33	93.51	0.000175	0.12	0.41	2.59	0.09
River 1	Reach 1-Upper	698	100YrCHI3Hr	0.06	93.24	93.51	93.33	93.51	0.000242	0.15	0.41	2.61	0.11
River 1	Reach 1-Upper	698	2YrSCS24Hr	0.03	93.24	93.32	93.30	93.33	0.015763	0.48	0.06	1.21	0.69
River 1	Reach 1-Upper	698	5YrSCS24Hr	0.04	93.24	93.32	93.31	93.34	0.028385	0.64	0.06	1.20	0.92
River 1	Reach 1-Upper	698	10YrSCS24Hr	0.04	93.24	93.43	93.32	93.43	0.000585	0.17	0.25	2.05	0.15
River 1	Reach 1-Upper	698	25YrSCS24Hr	0.05	93.24	93.51	93.32	93.51	0.000166	0.12	0.41	2.60	0.09
River 1	Reach 1-Upper	698	50YrSCS24Hr	0.06	93.24	93.51	93.33	93.51	0.000202	0.13	0.41	2.61	0.10
River 1	Reach 1-Upper	698	100YrSCS24Hr	0.06	93.24	93.52	93.33	93.52	0.000253	0.15	0.42	2.63	0.11
River 1	Reach 1-Upper	681	2YrCHI3Hr	0.02	93.14	93.23	93.19	93.23	0.003325	0.24	0.10	1.73	0.32
River 1	Reach 1-Upper	681	5YrCHI3Hr	0.03	93.14	93.25	93.20	93.25	0.002014	0.23	0.14	1.89	0.26
River 1	Reach 1-Upper	681	10YrCHI3Hr	0.04	93.14	93.27	93.20	93.28	0.001201	0.20	0.19	2.05	0.21
River 1	Reach 1-Upper	681	25YrCHI3Hr	0.04	93.14	93.40	93.21	93.40	0.000094	0.08	0.51	2.95	0.07
River 1	Reach 1-Upper	681	50YrCHI3Hr	0.05	93.14	93.51	93.21	93.51	0.000029	0.06	0.87	4.06	0.04
River 1	Reach 1-Upper	681	100YrCHI3Hr	0.06	93.14	93.51	93.22	93.51	0.000040	0.07	0.88	4.09	0.04
River 1	Reach 1-Upper	681	2YrSCS24Hr	0.03	93.14	93.24	93.20	93.24	0.002280	0.23	0.12	1.83	0.28
River 1	Reach 1-Upper	681	5YrSCS24Hr	0.04	93.14	93.28	93.20	93.29	0.000864	0.18	0.21	2.13	0.18
River 1	Reach 1-Upper	681	10YrSCS24Hr	0.04	93.14	93.43	93.21	93.43	0.000059	0.07	0.59	3.14	0.05
River 1	Reach 1-Upper	681	25YrSCS24Hr	0.05	93.14	93.51	93.21	93.51	0.000027	0.06	0.87	4.07	0.04
River 1	Reach 1-Upper	681	50YrSCS24Hr	0.06	93.14	93.51	93.22	93.51	0.000033	0.06	0.88	4.10	0.04
River 1	Reach 1-Upper	681	100YrSCS24Hr	0.06	93.14	93.51	93.22	93.51	0.000042	0.07	0.89	4.14	0.05
River 1	Reach 1-Upper	663	2YrCHI3Hr	0.02	93.05	93.19		93.20	0.001200	0.19	0.12	1.39	0.21
River 1	Reach 1-Upper	663	5YrCHI3Hr	0.03	93.05	93.23		93.23	0.000807	0.18	0.18	1.64	0.18
River 1	Reach 1-Upper	663	10YrCHI3Hr	0.04	93.05	93.26		93.26	0.000532	0.16	0.23	1.85	0.15
River 1	Reach 1-Upper	663	25YrCHI3Hr	0.04	93.05	93.40		93.40	0.000069	0.08	0.56	3.00	0.06
River 1	Reach 1-Upper	663	50YrCHI3Hr	0.05	93.05	93.51		93.51	0.000025	0.05	0.96	4.41	0.03
River 1	Reach 1-Upper	663	100YrCHI3Hr	0.06	93.05	93.51		93.51	0.000035	0.06	0.97	4.45	0.04
River 1	Reach 1-Upper	663	2YrSCS24Hr	0.03	93.05	93.22		93.22	0.000807	0.17	0.16	1.56	0.17
River 1	Reach 1-Upper	663	5YrSCS24Hr	0.04	93.05	93.27		93.28	0.000390	0.14	0.26	1.95	0.13
River 1	Reach 1-Upper	663	10YrSCS24Hr	0.04	93.05	93.43		93.43	0.000047	0.06	0.65	3.34	0.05
River 1	Reach 1-Upper	663	25YrSCS24Hr	0.05	93.05	93.51		93.51	0.000024	0.05	0.96	4.43	0.03
River 1	Reach 1-Upper	663	50YrSCS24Hr	0.06	93.05	93.51		93.51	0.000029	0.06	0.97	4.47	0.04
River 1	Reach 1-Upper	663	100YrSCS24Hr	0.06	93.05	93.51		93.51	0.000037	0.06	0.98	4.51	0.04
River 1	Reach 1-Upper	656	2YrCHI3Hr	0.07	93.03	93.16	93.12	93.17	0.007808	0.47	0.14	1.72	0.53
River 1	Reach 1-Upper	656	5YrCHI3Hr	0.11	93.03	93.19	93.15	93.21	0.006501	0.51	0.21	1.94	0.50
River 1	Reach 1-Upper	656	10YrCHI3Hr	0.14	93.03	93.23	93.16	93.24	0.004115	0.47	0.29	2.16	0.41
River 1	Reach 1-Upper	656	25YrCHI3Hr	0.18	93.03	93.40	93.18	93.40	0.000544	0.25	0.72	3.45	0.16
River 1	Reach 1-Upper	656	50YrCHI3Hr	0.21	93.03	93.51	93.19	93.51	0.000206	0.20	1.16	4.65	0.11
River 1	Reach 1-Upper	656	100YrCHI3Hr	0.25	93.03	93.51	93.21	93.51	0.000291	0.24	1.17	4.65	0.13
River 1	Reach 1-Upper	656	2YrSCS24Hr	0.09	93.03	93.18	93.14	93.20	0.007027	0.51	0.19	1.88	0.51
River 1	Reach 1-Upper	656	5YrSCS24Hr	0.15	93.03	93.25	93.16	93.26	0.003125	0.44	0.33	2.27	0.36
River 1	Reach 1-Upper	656	10YrSCS24Hr	0.18	93.03	93.42	93.18	93.43	0.000386	0.23	0.82	3.78	0.14
River 1	Reach 1-Upper	656	25YrSCS24Hr	0.23	93.03	93.51	93.20	93.51	0.000238	0.21	1.16	4.65	0.12
River 1	Reach 1-Upper	656	50YrSCS24Hr	0.27	93.03	93.51	93.21	93.51	0.000323	0.25	1.17	4.66	0.13
River 1	Reach 1-Upper	656	100YrSCS24Hr	0.31	93.03	93.51	93.23	93.51	0.000430	0.29	1.17	4.67	0.15
River 1	Reach 1-Upper	638	2YrCHI3Hr	0.07	92.92	93.08	93.01	93.09	0.002729	0.33	0.20	1.89	0.32
River 1	Reach 1-Upper	638	5YrCHI3Hr	0.11	92.92	93.14	93.04	93.15	0.001802	0.33	0.33	2.30	0.28
River 1	Reach 1-Upper	638	10YrCHI3Hr	0.14	92.92	93.21	93.05	93.21	0.001049	0.28	0.48	2.79	0.22
River 1	Reach 1-Upper	638	25YrCHI3Hr	0.18	92.92	93.39	93.07	93.39	0.000154	0.16	1.20	4.99	0.09
River 1	Reach 1-Upper	638	50YrCHI3Hr	0.21	92.92	93.50	93.09	93.50	0.000077	0.13	1.86	6.83	0.07
River 1	Reach 1-Upper	638	100YrCHI3Hr	0.25	92.92	93.50	93.10	93.51	0.000109	0.16	1.86	6.84	0.08
River 1	Reach 1-Upper	638	2YrSCS24Hr	0.09	92.92	93.12	93.03	93.13	0.002117	0.33	0.28	2.17	0.29
River 1	Reach 1-Upper	638	5YrSCS24Hr	0.15	92.92	93.23	93.06	93.24	0.000815	0.26	0.56	3.04	0.19
River 1	Reach 1-Upper	638	10YrSCS24Hr	0.18	92.92	93.42	93.07	93.42	0.000119	0.15	1.36	5.36	0.08
River 1	Reach 1-Upper	638	25YrSCS24Hr	0.23	92.92	93.50	93.09	93.51	0.000089	0.14	1.86	6.83	0.07
River 1	Reach 1-Upper	638	50YrSCS24Hr	0.27	92.92	93.50	93.11	93.51	0.000122	0.16	1.86	6.84	0.08
River 1	Reach 1-Upper	638	100YrSCS24Hr	0.31	92.92	93.51	93.12	93.51	0.000163	0.19	1.87	6.84	0.10
River 1	Reach 1-Upper	617	2YrCHI3Hr	0.07	92.84	93.03	92.95	93.03	0.002518	0.31	0.22	2.15	0.31
River 1	Reach 1-Upper	617	5YrCHI3Hr	0.11	92.84	93.12	92.98	93.12	0.000858	0.23	0.46	3.08	0.19
River 1	Reach 1-Upper	617	10YrCHI3Hr	0.14	92.84	93.19	93.00	93.20	0.000444	0.19	0.71	3.86	0.14
River 1	Reach 1-Upper	617	25YrCHI3Hr	0.18	92.84	93.39	93.01	93.39	0.000082	0.10	1.79	7.45	0.06
River 1	Reach 1-Upper	617	50YrCHI3Hr	0.21	92.84	93.50	93.03	93.50	0.000035	0.08	2.93	15.17	0.04
River 1	Reach 1-Upper	617	100YrCHI3Hr	0.25	92.84	93.50	93.04	93.50	0.000049	0.09	2.93	15.17	0.05
River 1	Reach 1-Upper	617	2YrSCS24Hr	0.09	92.84	93.09	92.97	93.10	0.001101	0.25	0.38	2.82	0.21
River 1	Reach 1-Upper	617	5YrSCS24Hr	0.15	92.84	93.22	93.00	93.22	0.000343	0.18	0.83	4.28	0.13
River 1	Reach 1-Upper	617	10YrSCS24Hr	0.18	92.84	93.42	93.01	93.42	0.000065	0.09	2.03	8.33	0.06
River 1	Reach 1-Upper	617	25YrSCS24Hr	0.23	92.84	93.50	93.03	93.50	0.000040	0.08	2.93	15.17	0.05
River 1	Reach 1-Upper	617	50YrSCS24Hr	0.27	92.84	93.50	93.04	93.50	0.000055	0.10	2.93	15.17	0.06
River 1	Reach 1-Upper	617	100YrSCS24Hr	0.31	92.84	93.50	93.06	93.50	0.000074	0.11	2.93	15.18	0.06
River 1	Reach 1-Upper	598	2YrCHI3Hr	0.07	92.76	93.01	92.87	93.01	0.000473	0.18	0.38	2.69	0.14
River 1	Reach 1-Upper	598	5YrCHI3Hr	0.11	92.76	93.11	92.89	93.12	0.000252	0.18	0.64	3.49	0.11
River 1	Reach 1-Upper	598	10YrCHI3Hr	0.15	92.76	93.19	92.91	93.19	0.000173	0.18	0.83	5.51	0.10

HEC-RAS Plan: 20250603-Post_Dev_v01 (Continued)

River	Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
River 1	Reach 1-Upper	598	25YrCHI3Hr	0.19	92.76	93.39	92.93	93.39	0.000060	0.14	1.33	9.41	0.06
River 1	Reach 1-Upper	598	50YrCHI3Hr	0.23	92.76	93.50	92.94	93.50	0.000019	0.08	4.94	31.21	0.03
River 1	Reach 1-Upper	598	100YrCHI3Hr	0.27	92.76	93.50	92.95	93.50	0.000027	0.09	4.93	31.21	0.04
River 1	Reach 1-Upper	598	2YrSCS24Hr	0.10	92.76	93.09	92.89	93.09	0.000296	0.18	0.57	3.28	0.12
River 1	Reach 1-Upper	598	5YrSCS24Hr	0.16	92.76	93.22	92.91	93.22	0.000149	0.17	0.90	6.10	0.09
River 1	Reach 1-Upper	598	10YrSCS24Hr	0.20	92.76	93.42	92.93	93.42	0.000053	0.14	1.41	10.00	0.06
River 1	Reach 1-Upper	598	25YrSCS24Hr	0.25	92.76	93.50	92.95	93.50	0.000022	0.08	4.94	31.21	0.04
River 1	Reach 1-Upper	598	50YrSCS24Hr	0.29	92.76	93.50	92.96	93.50	0.000030	0.10	4.93	31.21	0.04
River 1	Reach 1-Upper	598	100YrSCS24Hr	0.33	92.76	93.50	92.97	93.50	0.000041	0.11	4.93	31.21	0.05
River 1	Reach 1-Upper	589		Culvert									
River 1	Reach 1-Upper	581	2YrCHI3Hr	0.07	92.71	92.89	92.82	92.90	0.002047	0.28	0.25	2.75	0.28
River 1	Reach 1-Upper	581	5YrCHI3Hr	0.11	92.71	92.93	92.84	92.94	0.001929	0.33	0.34	3.49	0.29
River 1	Reach 1-Upper	581	10YrCHI3Hr	0.15	92.71	92.97	92.86	92.97	0.001556	0.34	0.43	4.12	0.27
River 1	Reach 1-Upper	581	25YrCHI3Hr	0.19	92.71	93.03	92.88	93.03	0.000917	0.33	0.58	5.30	0.22
River 1	Reach 1-Upper	581	50YrCHI3Hr	0.23	92.71	93.16	92.89	93.16	0.000310	0.25	0.90	7.86	0.13
River 1	Reach 1-Upper	581	100YrCHI3Hr	0.27	92.71	93.25	92.90	93.25	0.000204	0.24	1.13	30.32	0.11
River 1	Reach 1-Upper	581	2YrSCS24Hr	0.10	92.71	92.92	92.84	92.93	0.002022	0.32	0.32	3.28	0.29
River 1	Reach 1-Upper	581	5YrSCS24Hr	0.16	92.71	92.98	92.87	92.98	0.001396	0.34	0.46	4.38	0.26
River 1	Reach 1-Upper	581	10YrSCS24Hr	0.20	92.71	93.04	92.88	93.05	0.000827	0.32	0.61	5.51	0.21
River 1	Reach 1-Upper	581	25YrSCS24Hr	0.25	92.71	93.25	92.89	93.25	0.000170	0.22	1.13	30.32	0.10
River 1	Reach 1-Upper	581	50YrSCS24Hr	0.29	92.71	93.25	92.91	93.25	0.000231	0.25	1.13	30.33	0.12
River 1	Reach 1-Upper	581	100YrSCS24Hr	0.33	92.71	93.28	92.92	93.28	0.000256	0.28	1.20	32.04	0.13
River 1	Reach 1-Upper	572	2YrCHI3Hr	0.07	92.73	92.85	92.82	92.86	0.008247	0.45	0.15	2.09	0.53
River 1	Reach 1-Upper	572	5YrCHI3Hr	0.11	92.73	92.90	92.84	92.91	0.004531	0.42	0.27	2.64	0.42
River 1	Reach 1-Upper	572	10YrCHI3Hr	0.15	92.73	92.95	92.86	92.95	0.002601	0.37	0.40	3.12	0.33
River 1	Reach 1-Upper	572	25YrCHI3Hr	0.19	92.73	93.02	92.87	93.02	0.001121	0.29	0.66	3.99	0.22
River 1	Reach 1-Upper	572	50YrCHI3Hr	0.23	92.73	93.15	92.89	93.16	0.000259	0.17	1.45	15.47	0.11
River 1	Reach 1-Upper	572	100YrCHI3Hr	0.27	92.73	93.25	92.90	93.25	0.000071	0.11	4.09	35.89	0.06
River 1	Reach 1-Upper	572	2YrSCS24Hr	0.10	92.73	92.89	92.84	92.90	0.005425	0.43	0.24	2.49	0.45
River 1	Reach 1-Upper	572	5YrSCS24Hr	0.16	92.73	92.96	92.86	92.97	0.002123	0.35	0.45	3.32	0.30
River 1	Reach 1-Upper	572	10YrSCS24Hr	0.20	92.73	93.03	92.88	93.04	0.000971	0.27	0.72	4.14	0.21
River 1	Reach 1-Upper	572	25YrSCS24Hr	0.25	92.73	93.25	92.89	93.25	0.000059	0.10	4.09	35.88	0.06
River 1	Reach 1-Upper	572	50YrSCS24Hr	0.29	92.73	93.25	92.91	93.25	0.000080	0.12	4.10	35.91	0.07
River 1	Reach 1-Upper	572	100YrSCS24Hr	0.33	92.73	93.28	92.92	93.28	0.000068	0.11	5.15	39.12	0.06
River 1	Reach 1-Upper	555	2YrCHI3Hr	0.07	92.61	92.82	92.72	92.82	0.001001	0.21	0.34	3.06	0.20
River 1	Reach 1-Upper	555	5YrCHI3Hr	0.11	92.61	92.88	92.74	92.88	0.000708	0.21	0.55	3.83	0.17
River 1	Reach 1-Upper	555	10YrCHI3Hr	0.15	92.61	92.93	92.76	92.93	0.000472	0.19	0.77	4.49	0.15
River 1	Reach 1-Upper	555	25YrCHI3Hr	0.19	92.61	93.01	92.77	93.01	0.000255	0.16	1.17	5.51	0.11
River 1	Reach 1-Upper	555	50YrCHI3Hr	0.23	92.61	93.15	92.78	93.15	0.000051	0.10	3.73	35.66	0.05
River 1	Reach 1-Upper	555	100YrCHI3Hr	0.27	92.61	93.25	92.80	93.25	0.000017	0.06	7.39	40.94	0.03
River 1	Reach 1-Upper	555	2YrSCS24Hr	0.10	92.61	92.86	92.73	92.86	0.000804	0.21	0.48	3.60	0.18
River 1	Reach 1-Upper	555	5YrSCS24Hr	0.16	92.61	92.95	92.76	92.95	0.000407	0.18	0.86	4.73	0.14
River 1	Reach 1-Upper	555	10YrSCS24Hr	0.20	92.61	93.03	92.77	93.03	0.000229	0.16	1.25	5.68	0.11
River 1	Reach 1-Upper	555	25YrSCS24Hr	0.25	92.61	93.25	92.79	93.25	0.000014	0.06	7.39	40.94	0.03
River 1	Reach 1-Upper	555	50YrSCS24Hr	0.29	92.61	93.25	92.80	93.25	0.000019	0.07	7.39	40.94	0.03
River 1	Reach 1-Upper	555	100YrSCS24Hr	0.33	92.61	93.28	92.81	93.28	0.000018	0.07	8.55	41.65	0.03
River 1	Reach 1-Upper	534	2YrCHI3Hr	0.07	92.59	92.79	92.70	92.79	0.001558	0.25	0.28	2.54	0.25
River 1	Reach 1-Upper	534	5YrCHI3Hr	0.11	92.59	92.86	92.72	92.86	0.000934	0.24	0.48	3.41	0.20
River 1	Reach 1-Upper	534	10YrCHI3Hr	0.15	92.59	92.92	92.74	92.92	0.000559	0.20	0.76	9.05	0.16
River 1	Reach 1-Upper	534	25YrCHI3Hr	0.19	92.59	93.01	92.76	93.01	0.000116	0.11	2.99	37.02	0.08
River 1	Reach 1-Upper	534	50YrCHI3Hr	0.23	92.59	93.15	92.77	93.15	0.000009	0.04	9.72	51.04	0.02
River 1	Reach 1-Upper	534	100YrCHI3Hr	0.27	92.59	93.25	92.79	93.25	0.000004	0.03	14.61	51.39	0.02
River 1	Reach 1-Upper	534	2YrSCS24Hr	0.10	92.59	92.84	92.72	92.84	0.001116	0.24	0.42	3.15	0.22
River 1	Reach 1-Upper	534	5YrSCS24Hr	0.16	92.59	92.94	92.75	92.94	0.000434	0.19	1.04	17.37	0.14
River 1	Reach 1-Upper	534	10YrSCS24Hr	0.20	92.59	93.02	92.76	93.02	0.000089	0.10	3.56	40.73	0.07
River 1	Reach 1-Upper	534	25YrSCS24Hr	0.25	92.59	93.25	92.78	93.25	0.000003	0.03	14.61	51.39	0.01
River 1	Reach 1-Upper	534	50YrSCS24Hr	0.29	92.59	93.25	92.79	93.25	0.000004	0.03	14.61	51.39	0.02
River 1	Reach 1-Upper	534	100YrSCS24Hr	0.33	92.59	93.28	92.81	93.28	0.000004	0.03	16.05	51.49	0.02
River 1	Reach 1-Upper	510	2YrCHI3Hr	0.07	92.60	92.73	92.68	92.74	0.003415	0.39	0.18	2.95	0.37
River 1	Reach 1-Upper	510	5YrCHI3Hr	0.11	92.60	92.83	92.70	92.84	0.001076	0.33	0.34	4.33	0.23
River 1	Reach 1-Upper	510	10YrCHI3Hr	0.15	92.60	92.90	92.72	92.91	0.000704	0.32	0.45	5.33	0.20
River 1	Reach 1-Upper	510	25YrCHI3Hr	0.19	92.60	93.00	92.73	93.00	0.000440	0.31	0.61	12.66	0.16
River 1	Reach 1-Upper	510	50YrCHI3Hr	0.23	92.60	93.15	92.75	93.15	0.000211	0.27	0.84	109.17	0.12
River 1	Reach 1-Upper	510	100YrCHI3Hr	0.27	92.60	93.25	92.76	93.25	0.000000	0.01	42.37	109.53	0.00
River 1	Reach 1-Upper	510	2YrSCS24Hr	0.10	92.60	92.81	92.69	92.81	0.001328	0.34	0.30	3.97	0.25
River 1	Reach 1-Upper	510	5YrSCS24Hr	0.16	92.60	92.93	92.72	92.93	0.000623	0.32	0.49	5.74	0.19
River 1	Reach 1-Upper	510	10YrSCS24Hr	0.20	92.60	93.01	92.74	93.02	0.000410	0.31	0.63	14.62	0.16
River 1	Reach 1-Upper	510	25YrSCS24Hr	0.25	92.60	93.25	92.75	93.25	0.000000	0.01	42.37	109.53	0.00
River 1	Reach 1-Upper	510	50YrSCS24Hr	0.29	92.60	93.25	92.77	93.25	0.000000	0.01	42.37	109.53	0.00
River 1	Reach 1-Upper	510	100YrSCS24Hr	0.33	92.60	93.28	92.78	93.28	0.000000	0.01	45.44	109.63	0.01
River 1	Reach 1-Upper	505		Culvert									
River 1	Reach 1-Upper	502	2YrCHI3Hr	0.08	92.49	92.61	92.58	92.63	0.007402	0.52	0.15	2.32	0.53
River 1	Reach 1-Upper	502	5YrCHI3Hr	0.13	92.49	92.65	92.60	92.67	0.006455	0.61	0.21	2.78	0.52
River 1	Reach 1-Upper	502	10YrCHI3Hr	0.16	92.49	92.68	92.62	92.70	0.006009	0.66	0.25	3.08	0.52
River 1	Reach 1-Upper	502	25YrCHI3Hr	0.21	92.49	92.73	92.64	92.75	0.004266	0.67	0.32	3.89	0.46
River 1	Reach 1-Upper	502	50YrCHI3Hr	0.26	92.49	92.82	92.66	92.84	0.001871	0.56	0.46	5.35	0.32
River 1	Reach 1-Upper	502	100YrCHI3Hr	0.31	92.49	92.97	92.67	92.98	0.000675	0.44	0.69	104.74	0.21
River 1	Reach 1-Upper	502	2YrSCS24Hr	0.11	92.49	92.64	92.60	92.66	0.006605	0.59	0.19	2.67	0.52
River 1	Reach 1-Upper	502	5YrSCS24Hr	0.18	92.49	92.69	92.62	92.71	0.005579	0.67	0.26	3.20	0.51
River 1	Reach 1-Upper	502	10YrSCS24Hr	0.22	92.49	92.74	92.64	92.76	0.003886	0.66	0.34	4.12	0.44
River 1	Reach 1-Upper	502	25YrSCS24Hr	0.28	92.49	92.88	92.66	92.90	0.001173	0.50	0.56	6.47	0.26
River 1	Reach 1-Upper	502	50YrSCS24Hr	0.33	92.49	93.05	92.68	93.06	0.000467	0.41	0.80	104.96	0.18

HEC-RAS Plan: 20250603-Post_Dev_v01 (Continued)

River	Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
River 1	Reach 1-Upper	502	100YrSCS24Hr	0.38	92.49	93.28	92.70	93.28	0.000000	0.01	48.99	105.56	0.01
River 1	Reach 1-Upper	493	2YrCHI3Hr	0.08	92.34	92.61	92.43	92.61	0.000140	0.10	0.77	4.77	0.08
River 1	Reach 1-Upper	493	5YrCHI3Hr	0.13	92.34	92.66	92.45	92.66	0.000206	0.13	0.98	5.52	0.10
River 1	Reach 1-Upper	493	10YrCHI3Hr	0.16	92.34	92.68	92.46	92.68	0.000234	0.14	1.14	6.01	0.11
River 1	Reach 1-Upper	493	25YrCHI3Hr	0.21	92.34	92.73	92.48	92.73	0.000204	0.15	1.47	6.78	0.10
River 1	Reach 1-Upper	493	50YrCHI3Hr	0.26	92.34	92.82	92.49	92.83	0.000109	0.12	2.14	8.33	0.08
River 1	Reach 1-Upper	493	100YrCHI3Hr	0.31	92.34	92.98	92.50	92.98	0.000002	0.02	27.11	101.30	0.01
River 1	Reach 1-Upper	493	2YrSCS24Hr	0.11	92.34	92.64	92.44	92.65	0.000190	0.12	0.93	5.32	0.09
River 1	Reach 1-Upper	493	5YrSCS24Hr	0.18	92.34	92.69	92.46	92.70	0.000232	0.15	1.21	6.21	0.11
River 1	Reach 1-Upper	493	10YrSCS24Hr	0.22	92.34	92.74	92.48	92.74	0.000189	0.14	1.54	6.89	0.10
River 1	Reach 1-Upper	493	25YrSCS24Hr	0.28	92.34	92.89	92.50	92.89	0.000065	0.10	2.72	10.17	0.06
River 1	Reach 1-Upper	493	50YrSCS24Hr	0.33	92.34	93.05	92.51	93.05	0.000001	0.02	34.55	101.67	0.01
River 1	Reach 1-Upper	493	100YrSCS24Hr	0.38	92.34	93.28	92.52	93.28	0.000000	0.01	57.34	102.84	0.00
River 1	Reach 1-Upper	474	2YrCHI3Hr	0.08	92.41	92.61	92.50	92.61	0.000593	0.15	0.52	5.18	0.15
River 1	Reach 1-Upper	474	5YrCHI3Hr	0.13	92.41	92.65	92.53	92.65	0.000598	0.17	0.74	6.03	0.16
River 1	Reach 1-Upper	474	10YrCHI3Hr	0.16	92.41	92.68	92.54	92.68	0.000560	0.18	0.91	6.62	0.15
River 1	Reach 1-Upper	474	25YrCHI3Hr	0.21	92.41	92.73	92.56	92.73	0.000375	0.17	1.29	7.74	0.13
River 1	Reach 1-Upper	474	50YrCHI3Hr	0.26	92.41	92.82	92.57	92.82	0.000002	0.01	24.36	91.42	0.01
River 1	Reach 1-Upper	474	100YrCHI3Hr	0.31	92.41	92.98	92.57	92.98	0.000000	0.01	38.60	92.12	0.01
River 1	Reach 1-Upper	474	2YrSCS24Hr	0.11	92.41	92.64	92.52	92.64	0.000601	0.17	0.68	5.81	0.16
River 1	Reach 1-Upper	474	5YrSCS24Hr	0.18	92.41	92.69	92.55	92.69	0.000516	0.18	0.99	6.87	0.15
River 1	Reach 1-Upper	474	10YrSCS24Hr	0.22	92.41	92.74	92.56	92.74	0.000335	0.16	1.37	7.98	0.12
River 1	Reach 1-Upper	474	25YrSCS24Hr	0.28	92.41	92.89	92.57	92.89	0.000001	0.01	30.17	91.71	0.01
River 1	Reach 1-Upper	474	50YrSCS24Hr	0.33	92.41	93.05	92.58	93.05	0.000000	0.01	45.36	92.45	0.00
River 1	Reach 1-Upper	474	100YrSCS24Hr	0.38	92.41	93.28	92.59	93.28	0.000000	0.01	66.08	93.46	0.00
River 1	Reach 1-Upper	454	2YrCHI3Hr	0.08	92.44	92.59	92.51	92.59	0.001595	0.25	0.31	2.95	0.25
River 1	Reach 1-Upper	454	5YrCHI3Hr	0.13	92.44	92.63	92.53	92.63	0.001681	0.30	0.43	3.36	0.26
River 1	Reach 1-Upper	454	10YrCHI3Hr	0.16	92.44	92.66	92.55	92.66	0.001585	0.31	0.53	3.66	0.26
River 1	Reach 1-Upper	454	25YrCHI3Hr	0.21	92.44	92.71	92.56	92.72	0.000986	0.28	0.76	4.27	0.21
River 1	Reach 1-Upper	454	50YrCHI3Hr	0.26	92.44	92.82	92.57	92.82	0.000017	0.04	11.00	82.83	0.03
River 1	Reach 1-Upper	454	100YrCHI3Hr	0.31	92.44	92.98	92.59	92.98	0.000002	0.02	23.90	83.31	0.01
River 1	Reach 1-Upper	454	2YrSCS24Hr	0.11	92.44	92.62	92.53	92.62	0.001702	0.29	0.39	3.25	0.26
River 1	Reach 1-Upper	454	5YrSCS24Hr	0.18	92.44	92.67	92.55	92.67	0.001428	0.31	0.58	3.79	0.25
River 1	Reach 1-Upper	454	10YrSCS24Hr	0.22	92.44	92.73	92.56	92.73	0.000862	0.27	0.81	4.39	0.20
River 1	Reach 1-Upper	454	25YrSCS24Hr	0.28	92.44	92.89	92.58	92.89	0.000006	0.03	16.27	83.03	0.02
River 1	Reach 1-Upper	454	50YrSCS24Hr	0.33	92.44	93.05	92.59	93.05	0.000001	0.02	30.02	83.53	0.01
River 1	Reach 1-Upper	454	100YrSCS24Hr	0.38	92.44	93.28	92.61	93.28	0.000000	0.01	48.71	84.20	0.00
River 1	Reach 1-Upper	434	2YrCHI3Hr	0.08	92.42	92.54	92.49	92.55	0.003018	0.30	0.25	2.97	0.33
River 1	Reach 1-Upper	434	5YrCHI3Hr	0.13	92.42	92.59	92.51	92.59	0.002121	0.32	0.40	3.39	0.29
River 1	Reach 1-Upper	434	10YrCHI3Hr	0.16	92.42	92.62	92.52	92.63	0.001672	0.31	0.52	3.69	0.27
River 1	Reach 1-Upper	434	25YrCHI3Hr	0.21	92.42	92.71	92.54	92.71	0.000117	0.10	3.85	43.01	0.07
River 1	Reach 1-Upper	434	50YrCHI3Hr	0.26	92.42	92.82	92.55	92.82	0.000014	0.04	11.01	73.93	0.03
River 1	Reach 1-Upper	434	100YrCHI3Hr	0.31	92.42	92.98	92.56	92.98	0.000002	0.02	22.55	74.47	0.01
River 1	Reach 1-Upper	434	2YrSCS24Hr	0.11	92.42	92.57	92.50	92.58	0.002333	0.31	0.36	3.27	0.30
River 1	Reach 1-Upper	434	5YrSCS24Hr	0.18	92.42	92.64	92.53	92.64	0.001598	0.30	0.58	4.26	0.26
River 1	Reach 1-Upper	434	10YrSCS24Hr	0.22	92.42	92.72	92.54	92.72	0.000089	0.09	4.45	47.65	0.06
River 1	Reach 1-Upper	434	25YrSCS24Hr	0.28	92.42	92.89	92.55	92.89	0.000005	0.03	15.73	74.15	0.02
River 1	Reach 1-Upper	434	50YrSCS24Hr	0.33	92.42	93.05	92.57	93.05	0.000001	0.02	28.02	74.72	0.01
River 1	Reach 1-Upper	434	100YrSCS24Hr	0.38	92.42	93.28	92.58	93.28	0.000000	0.01	44.76	75.55	0.00
River 1	Reach 1-Upper	416	2YrCHI3Hr	0.08	92.34	92.52	92.42	92.53	0.000570	0.16	0.50	4.92	0.15
River 1	Reach 1-Upper	416	5YrCHI3Hr	0.13	92.34	92.58	92.45	92.58	0.000411	0.17	0.78	5.95	0.14
River 1	Reach 1-Upper	416	10YrCHI3Hr	0.16	92.34	92.62	92.46	92.62	0.000153	0.12	2.34	28.94	0.09
River 1	Reach 1-Upper	416	25YrCHI3Hr	0.21	92.34	92.71	92.47	92.71	0.000034	0.07	5.28	35.31	0.04
River 1	Reach 1-Upper	416	50YrCHI3Hr	0.26	92.34	92.82	92.48	92.82	0.000009	0.05	9.98	45.71	0.02
River 1	Reach 1-Upper	416	100YrCHI3Hr	0.31	92.34	92.98	92.49	92.98	0.000003	0.03	19.16	66.90	0.01
River 1	Reach 1-Upper	416	2YrSCS24Hr	0.11	92.34	92.56	92.44	92.56	0.000446	0.17	0.70	5.67	0.14
River 1	Reach 1-Upper	416	5YrSCS24Hr	0.18	92.34	92.64	92.47	92.64	0.000111	0.11	2.84	30.13	0.07
River 1	Reach 1-Upper	416	10YrSCS24Hr	0.22	92.34	92.72	92.48	92.72	0.000029	0.07	5.77	36.29	0.04
River 1	Reach 1-Upper	416	25YrSCS24Hr	0.28	92.34	92.89	92.49	92.89	0.000006	0.04	13.26	57.17	0.02
River 1	Reach 1-Upper	416	50YrSCS24Hr	0.33	92.34	93.05	92.50	93.05	0.000002	0.03	24.08	67.16	0.01
River 1	Reach 1-Upper	416	100YrSCS24Hr	0.38	92.34	93.28	92.50	93.28	0.000000	0.02	39.14	67.97	0.01
River 1	Reach 1-Upper	398	2YrCHI3Hr	0.08	92.28	92.51	92.40	92.51	0.000941	0.23	0.34	2.57	0.20
River 1	Reach 1-Upper	398	5YrCHI3Hr	0.13	92.28	92.56	92.43	92.57	0.000911	0.26	0.49	2.89	0.20
River 1	Reach 1-Upper	398	10YrCHI3Hr	0.16	92.28	92.61	92.44	92.61	0.000744	0.26	0.63	3.17	0.19
River 1	Reach 1-Upper	398	25YrCHI3Hr	0.21	92.28	92.71	92.46	92.71	0.000375	0.22	0.97	4.34	0.14
River 1	Reach 1-Upper	398	50YrCHI3Hr	0.26	92.28	92.82	92.47	92.82	0.000101	0.14	3.54	45.04	0.08
River 1	Reach 1-Upper	398	100YrCHI3Hr	0.31	92.28	92.98	92.49	92.98	0.000010	0.05	11.83	58.56	0.02
River 1	Reach 1-Upper	398	2YrSCS24Hr	0.11	92.28	92.55	92.42	92.55	0.000929	0.25	0.45	2.81	0.20
River 1	Reach 1-Upper	398	5YrSCS24Hr	0.18	92.28	92.63	92.44	92.63	0.000665	0.26	0.69	3.28	0.18
River 1	Reach 1-Upper	398	10YrSCS24Hr	0.22	92.28	92.72	92.46	92.72	0.000340	0.22	1.03	4.90	0.13
River 1	Reach 1-Upper	398	25YrSCS24Hr	0.28	92.28	92.89	92.48	92.89	0.000034	0.09	6.58	49.48	0.04
River 1	Reach 1-Upper	398	50YrSCS24Hr	0.33	92.28	93.05	92.49	93.05	0.000005	0.04	16.13	58.78	0.02
River 1	Reach 1-Upper	398	100YrSCS24Hr	0.38	92.28	93.28	92.51	93.28	0.000001	0.02	29.31	59.42	0.01
River 1	Reach 1-Upper	383	2YrCHI3Hr	0.08	92.34	92.48	92.42	92.49	0.004195	0.39	0.20	1.99	0.40
River 1	Reach 1-Upper	383	5YrCHI3Hr	0.13	92.34	92.54	92.45	92.54	0.002725	0.39	0.32	2.34	0.34
River 1	Reach 1-Upper	383	10YrCHI3Hr	0.16	92.34	92.59	92.46	92.60	0.001702	0.36	0.46	2.64	0.28
River 1	Reach 1-Upper	383	25YrCHI3Hr	0.21	92.34	92.70	92.49	92.70	0.000669	0.28	0.77	3.24	0.18
River 1	Reach 1-Upper	383	50YrCHI3Hr	0.26	92.34	92.82	92.50	92.82	0.000280	0.21	1.21	3.92	0.12
River 1	Reach 1-Upper	383	100YrCHI3Hr	0.31	92.34	92.98	92.52	92.98	0.000109	0.16	1.93	5.32	0.08
River 1	Reach 1-Upper	383	2YrSCS24Hr	0.11	92.34	92.52	92.44	92.53	0.003103	0.40	0.28	2.24	0.36
River 1	Reach 1-Upper	383	5YrSCS24Hr	0.18	92.34	92.61	92.47	92.62	0.001407	0.34	0.51	2.76	0.25
River 1	Reach 1-Upper	383	10YrSCS24Hr	0.22	92.34	92.71	92.49	92.71	0.000603	0.27	0.82	3.32	0.17
River 1	Reach 1-Upper	383	25YrSCS24Hr	0.28	92.34	92.88	92.51	92.89	0.000190	0.19	1.48	4.29	0.10

HEC-RAS Plan: 20250603-Post_Dev_v01 (Continued)

River	Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
River 1	Reach 1-Upper	383	50YrSCS24Hr	0.33	92.34	93.05	92.52	93.05	0.000010	0.05	11.65	51.68	0.03
River 1	Reach 1-Upper	383	100YrSCS24Hr	0.38	92.34	93.28	92.54	93.28	0.000002	0.03	23.26	52.34	0.01
River 1	Reach 1-Upper	364	2YrCHI3Hr	0.08	92.23	92.44	92.34	92.44	0.001335	0.27	0.28	2.08	0.23
River 1	Reach 1-Upper	364	5YrCHI3Hr	0.13	92.23	92.51	92.36	92.51	0.001059	0.29	0.44	2.41	0.22
River 1	Reach 1-Upper	364	10YrCHI3Hr	0.16	92.23	92.57	92.38	92.58	0.000730	0.27	0.60	2.72	0.19
River 1	Reach 1-Upper	364	25YrCHI3Hr	0.21	92.23	92.69	92.40	92.69	0.000346	0.23	0.95	3.30	0.13
River 1	Reach 1-Upper	364	50YrCHI3Hr	0.26	92.23	92.82	92.42	92.82	0.000178	0.18	1.41	4.08	0.10
River 1	Reach 1-Upper	364	100YrCHI3Hr	0.31	92.23	92.98	92.43	92.98	0.000062	0.13	3.78	43.88	0.06
River 1	Reach 1-Upper	364	2YrSCS24Hr	0.11	92.23	92.49	92.36	92.49	0.001160	0.29	0.39	2.31	0.23
River 1	Reach 1-Upper	364	5YrSCS24Hr	0.18	92.23	92.60	92.39	92.60	0.000628	0.26	0.66	2.84	0.17
River 1	Reach 1-Upper	364	10YrSCS24Hr	0.22	92.23	92.70	92.40	92.71	0.000320	0.22	1.00	3.37	0.13
River 1	Reach 1-Upper	364	25YrSCS24Hr	0.28	92.23	92.88	92.42	92.88	0.000125	0.16	1.71	4.91	0.08
River 1	Reach 1-Upper	364	50YrSCS24Hr	0.33	92.23	93.05	92.44	93.05	0.000024	0.09	7.11	44.08	0.04
River 1	Reach 1-Upper	364	100YrSCS24Hr	0.38	92.23	93.28	92.46	93.28	0.000003	0.04	17.03	44.82	0.02
River 1	Reach 1-Upper	347	2YrCHI3Hr	0.08	92.26	92.42	92.33	92.42	0.001247	0.25	0.31	2.52	0.22
River 1	Reach 1-Upper	347	5YrCHI3Hr	0.13	92.26	92.49	92.35	92.50	0.000764	0.25	0.51	2.84	0.19
River 1	Reach 1-Upper	347	10YrCHI3Hr	0.16	92.26	92.56	92.37	92.57	0.000481	0.23	0.72	3.13	0.15
River 1	Reach 1-Upper	347	25YrCHI3Hr	0.21	92.26	92.68	92.38	92.69	0.000223	0.19	1.13	3.65	0.11
River 1	Reach 1-Upper	347	50YrCHI3Hr	0.26	92.26	92.81	92.40	92.81	0.000114	0.16	1.64	4.21	0.08
River 1	Reach 1-Upper	347	100YrCHI3Hr	0.31	92.26	92.98	92.41	92.98	0.000054	0.13	2.42	6.23	0.06
River 1	Reach 1-Upper	347	2YrSCS24Hr	0.11	92.26	92.47	92.35	92.48	0.000881	0.25	0.45	2.74	0.20
River 1	Reach 1-Upper	347	5YrSCS24Hr	0.18	92.26	92.59	92.37	92.59	0.000407	0.22	0.80	3.24	0.14
River 1	Reach 1-Upper	347	10YrSCS24Hr	0.22	92.26	92.70	92.38	92.70	0.000206	0.19	1.19	3.72	0.11
River 1	Reach 1-Upper	347	25YrSCS24Hr	0.28	92.26	92.88	92.40	92.88	0.000085	0.14	1.93	4.52	0.07
River 1	Reach 1-Upper	347	50YrSCS24Hr	0.33	92.26	93.05	92.41	93.05	0.000037	0.12	3.16	14.13	0.05
River 1	Reach 1-Upper	347	100YrSCS24Hr	0.38	92.26	93.28	92.43	93.28	0.000006	0.06	12.31	37.97	0.02
River 1	Reach 1-Upper	328	2YrCHI3Hr	0.08	92.20	92.39	92.29	92.39	0.001651	0.30	0.26	1.92	0.26
River 1	Reach 1-Upper	328	5YrCHI3Hr	0.13	92.20	92.48	92.32	92.48	0.000966	0.29	0.44	2.28	0.21
River 1	Reach 1-Upper	328	10YrCHI3Hr	0.16	92.20	92.55	92.34	92.55	0.000609	0.26	0.62	2.59	0.17
River 1	Reach 1-Upper	328	25YrCHI3Hr	0.21	92.20	92.68	92.36	92.68	0.000289	0.22	0.99	3.12	0.12
River 1	Reach 1-Upper	328	50YrCHI3Hr	0.26	92.20	92.81	92.38	92.81	0.000165	0.18	1.44	4.02	0.09
River 1	Reach 1-Upper	328	100YrCHI3Hr	0.31	92.20	92.97	92.39	92.98	0.000079	0.14	2.18	4.99	0.07
River 1	Reach 1-Upper	328	2YrSCS24Hr	0.11	92.20	92.45	92.31	92.46	0.001116	0.29	0.39	2.18	0.22
River 1	Reach 1-Upper	328	5YrSCS24Hr	0.18	92.20	92.58	92.34	92.58	0.000518	0.25	0.69	2.70	0.16
River 1	Reach 1-Upper	328	10YrSCS24Hr	0.22	92.20	92.70	92.36	92.70	0.000268	0.21	1.04	3.19	0.12
River 1	Reach 1-Upper	328	25YrSCS24Hr	0.28	92.20	92.88	92.38	92.88	0.000119	0.16	1.73	4.39	0.08
River 1	Reach 1-Upper	328	50YrSCS24Hr	0.33	92.20	93.05	92.40	93.05	0.000056	0.13	2.59	5.81	0.06
River 1	Reach 1-Upper	328	100YrSCS24Hr	0.38	92.20	93.28	92.42	93.28	0.000010	0.07	9.31	29.89	0.03
River 1	Reach 1-Upper	306	2YrCHI3Hr	0.08	92.07	92.37	92.19	92.37	0.000732	0.26	0.29	1.56	0.18
River 1	Reach 1-Upper	306	5YrCHI3Hr	0.13	92.07	92.46	92.23	92.46	0.000682	0.31	0.42	1.87	0.18
River 1	Reach 1-Upper	306	10YrCHI3Hr	0.16	92.07	92.54	92.25	92.54	0.000557	0.31	0.53	2.14	0.17
River 1	Reach 1-Upper	306	25YrCHI3Hr	0.21	92.07	92.67	92.28	92.67	0.000330	0.29	0.73	2.65	0.13
River 1	Reach 1-Upper	306	50YrCHI3Hr	0.26	92.07	92.80	92.30	92.81	0.000212	0.28	0.93	3.22	0.11
River 1	Reach 1-Upper	306	100YrCHI3Hr	0.31	92.07	92.97	92.32	92.97	0.000136	0.26	1.18	4.39	0.09
River 1	Reach 1-Upper	306	2YrSCS24Hr	0.11	92.07	92.43	92.22	92.44	0.000706	0.30	0.38	1.78	0.18
River 1	Reach 1-Upper	306	5YrSCS24Hr	0.18	92.07	92.57	92.26	92.57	0.000500	0.31	0.57	2.24	0.16
River 1	Reach 1-Upper	306	10YrSCS24Hr	0.22	92.07	92.69	92.28	92.69	0.000315	0.29	0.75	2.72	0.13
River 1	Reach 1-Upper	306	25YrSCS24Hr	0.28	92.07	92.87	92.31	92.88	0.000176	0.27	1.03	3.52	0.10
River 1	Reach 1-Upper	306	50YrSCS24Hr	0.33	92.07	93.05	92.33	93.05	0.000113	0.25	1.29	5.08	0.09
River 1	Reach 1-Upper	306	100YrSCS24Hr	0.38	92.07	93.27	92.35	93.27	0.000071	0.23	1.63	20.92	0.07
River 1	Reach 1-Upper	300		Culvert									
River 1	Reach 1-Upper	294	2YrCHI3Hr	0.08	92.15	92.33	92.24	92.33	0.001623	0.33	0.23	2.13	0.27
River 1	Reach 1-Upper	294	5YrCHI3Hr	0.13	92.15	92.37	92.26	92.38	0.001907	0.42	0.30	2.36	0.30
River 1	Reach 1-Upper	294	10YrCHI3Hr	0.16	92.15	92.39	92.28	92.41	0.002165	0.49	0.34	2.49	0.33
River 1	Reach 1-Upper	294	25YrCHI3Hr	0.21	92.15	92.42	92.30	92.44	0.002461	0.56	0.38	2.64	0.36
River 1	Reach 1-Upper	294	50YrCHI3Hr	0.26	92.15	92.45	92.32	92.47	0.002689	0.62	0.41	2.75	0.38
River 1	Reach 1-Upper	294	100YrCHI3Hr	0.31	92.15	92.47	92.33	92.49	0.002898	0.68	0.45	2.87	0.40
River 1	Reach 1-Upper	294	2YrSCS24Hr	0.11	92.15	92.36	92.25	92.37	0.001813	0.40	0.28	2.31	0.29
River 1	Reach 1-Upper	294	5YrSCS24Hr	0.18	92.15	92.40	92.28	92.41	0.002263	0.51	0.35	2.52	0.34
River 1	Reach 1-Upper	294	10YrSCS24Hr	0.22	92.15	92.43	92.30	92.44	0.002532	0.58	0.38	2.65	0.36
River 1	Reach 1-Upper	294	25YrSCS24Hr	0.28	92.15	92.46	92.32	92.48	0.002786	0.65	0.43	2.80	0.39
River 1	Reach 1-Upper	294	50YrSCS24Hr	0.33	92.15	92.48	92.34	92.50	0.002974	0.71	0.46	2.92	0.41
River 1	Reach 1-Upper	294	100YrSCS24Hr	0.38	92.15	92.50	92.36	92.53	0.003240	0.77	0.49	3.02	0.43
River 1	Reach 1-Upper	279	2YrCHI3Hr	0.09	92.08	92.21	92.21	92.25	0.030677	0.84	0.11	1.56	1.01
River 1	Reach 1-Upper	279	5YrCHI3Hr	0.15	92.08	92.25	92.25	92.29	0.024457	0.90	0.17	1.87	0.95
River 1	Reach 1-Upper	279	10YrCHI3Hr	0.20	92.08	92.28		92.32	0.017438	0.87	0.23	2.05	0.83
River 1	Reach 1-Upper	279	25YrCHI3Hr	0.27	92.08	92.32		92.36	0.013351	0.86	0.31	2.26	0.74
River 1	Reach 1-Upper	279	50YrCHI3Hr	0.32	92.08	92.34		92.38	0.011757	0.87	0.37	2.42	0.71
River 1	Reach 1-Upper	279	100YrCHI3Hr	0.38	92.08	92.37		92.41	0.010680	0.88	0.43	2.57	0.69
River 1	Reach 1-Upper	279	2YrSCS24Hr	0.14	92.08	92.24	92.24	92.28	0.027916	0.90	0.15	1.79	1.00
River 1	Reach 1-Upper	279	5YrSCS24Hr	0.22	92.08	92.29		92.33	0.015850	0.86	0.25	2.11	0.79
River 1	Reach 1-Upper	279	10YrSCS24Hr	0.27	92.08	92.32		92.36	0.013094	0.86	0.32	2.29	0.74
River 1	Reach 1-Upper	279	25YrSCS24Hr	0.35	92.08	92.35		92.39	0.011229	0.87	0.40	2.49	0.70
River 1	Reach 1-Upper	279	50YrSCS24Hr	0.41	92.08	92.38		92.42	0.010330	0.89	0.46	2.63	0.68
River 1	Reach 1-Upper	279	100YrSCS24Hr	0.47	92.08	92.40		92.44	0.009621	0.90	0.52	2.77	0.66
River 1	Reach 1-Upper	277	2YrCHI3Hr	0.09	91.95	92.21		92.22	0.000731	0.22	0.41	2.76	0.18
River 1	Reach 1-Upper	277	5YrCHI3Hr	0.15	91.95	92.26		92.27	0.000866	0.29	0.56	3.04	0.20
River 1	Reach 1-Upper	277	10YrCHI3Hr	0.20	91.95	92.29		92.30	0.000933	0.33	0.65	3.21	0.22
River 1	Reach 1-Upper	277	25YrCHI3Hr	0.27	91.95	92.33		92.33	0.001005	0.37	0.76	3.40	0.23
River 1	Reach 1-Upper	277	50YrCHI3Hr	0.32	91.95	92.35		92.36	0.001064	0.41	0.85	3.54	0.24
River 1	Reach 1-Upper	277	100YrCHI3Hr	0.38	91.95	92.38		92.39	0.001128	0.44	0.94	3.68	0.25
River 1	Reach 1-Upper	277	2YrSCS24Hr	0.14	91.95	92.25		92.25	0.000837	0.27	0.52	2.97	0.20

HEC-RAS Plan: 20250603-Post_Dev_v01 (Continued)

River	Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
River 1	Reach 1-Upper	277	5YrSCS24Hr	0.22	91.95	92.30		92.31	0.000942	0.34	0.68	3.26	0.22
River 1	Reach 1-Upper	277	10YrSCS24Hr	0.27	91.95	92.33		92.34	0.001013	0.38	0.77	3.42	0.23
River 1	Reach 1-Upper	277	25YrSCS24Hr	0.35	91.95	92.36		92.37	0.001094	0.42	0.89	3.61	0.24
River 1	Reach 1-Upper	277	50YrSCS24Hr	0.41	91.95	92.39		92.40	0.001153	0.46	0.98	3.74	0.25
River 1	Reach 1-Upper	277	100YrSCS24Hr	0.47	91.95	92.41		92.42	0.001212	0.49	1.07	3.88	0.26
River 1	Reach 1-Upper	270	2YrCHI3Hr	0.09	92.03	92.21		92.21	0.001711	0.28	0.32	2.69	0.26
River 1	Reach 1-Upper	270	5YrCHI3Hr	0.15	92.03	92.25		92.26	0.001749	0.34	0.46	3.12	0.28
River 1	Reach 1-Upper	270	10YrCHI3Hr	0.20	92.03	92.28		92.29	0.001743	0.37	0.55	3.39	0.28
River 1	Reach 1-Upper	270	25YrCHI3Hr	0.27	92.03	92.32		92.33	0.001732	0.40	0.68	3.71	0.29
River 1	Reach 1-Upper	270	50YrCHI3Hr	0.32	92.03	92.34		92.35	0.001724	0.42	0.77	4.08	0.29
River 1	Reach 1-Upper	270	100YrCHI3Hr	0.38	92.03	92.37		92.38	0.001666	0.45	0.89	4.95	0.29
River 1	Reach 1-Upper	270	2YrSCS24Hr	0.14	92.03	92.24		92.25	0.001760	0.32	0.42	2.99	0.27
River 1	Reach 1-Upper	270	5YrSCS24Hr	0.22	92.03	92.29		92.30	0.001718	0.37	0.59	3.47	0.28
River 1	Reach 1-Upper	270	10YrSCS24Hr	0.27	92.03	92.32		92.33	0.001733	0.40	0.69	3.75	0.29
River 1	Reach 1-Upper	270	25YrSCS24Hr	0.35	92.03	92.35		92.36	0.001697	0.43	0.82	4.48	0.29
River 1	Reach 1-Upper	270	50YrSCS24Hr	0.41	92.03	92.38		92.39	0.001643	0.46	0.94	5.31	0.29
River 1	Reach 1-Upper	270	100YrSCS24Hr	0.47	92.03	92.40		92.41	0.001586	0.48	1.08	5.71	0.29
River 1	Reach 1-Upper	261	2YrCHI3Hr	0.09	92.00	92.19	92.11	92.19	0.002280	0.34	0.27	2.14	0.30
River 1	Reach 1-Upper	261	5YrCHI3Hr	0.15	92.00	92.23	92.14	92.24	0.002570	0.41	0.37	2.36	0.33
River 1	Reach 1-Upper	261	10YrCHI3Hr	0.20	92.00	92.26	92.15	92.27	0.002733	0.46	0.44	2.49	0.35
River 1	Reach 1-Upper	261	25YrCHI3Hr	0.27	92.00	92.29	92.18	92.31	0.002879	0.51	0.52	2.65	0.37
River 1	Reach 1-Upper	261	50YrCHI3Hr	0.32	92.00	92.32	92.19	92.33	0.003006	0.54	0.59	2.77	0.38
River 1	Reach 1-Upper	261	100YrCHI3Hr	0.38	92.00	92.34	92.21	92.36	0.003119	0.58	0.66	2.89	0.39
River 1	Reach 1-Upper	261	2YrSCS24Hr	0.14	92.00	92.22	92.13	92.23	0.002496	0.39	0.34	2.30	0.33
River 1	Reach 1-Upper	261	5YrSCS24Hr	0.22	92.00	92.27	92.16	92.28	0.002723	0.47	0.46	2.54	0.35
River 1	Reach 1-Upper	261	10YrSCS24Hr	0.27	92.00	92.30	92.18	92.31	0.002897	0.51	0.53	2.67	0.37
River 1	Reach 1-Upper	261	25YrSCS24Hr	0.35	92.00	92.33	92.20	92.34	0.003059	0.56	0.62	2.82	0.38
River 1	Reach 1-Upper	261	50YrSCS24Hr	0.41	92.00	92.35	92.22	92.37	0.003161	0.59	0.69	2.94	0.39
River 1	Reach 1-Upper	261	100YrSCS24Hr	0.47	92.00	92.37	92.24	92.39	0.003275	0.63	0.76	3.07	0.40
River 1	Reach 1-Upper	239	2YrCHI3Hr	0.09	91.93	92.05	92.04	92.08	0.017237	0.70	0.13	1.61	0.78
River 1	Reach 1-Upper	239	5YrCHI3Hr	0.15	91.93	92.10	92.07	92.12	0.013911	0.75	0.21	1.91	0.73
River 1	Reach 1-Upper	239	10YrCHI3Hr	0.20	91.93	92.12	92.09	92.15	0.012488	0.78	0.26	2.07	0.71
River 1	Reach 1-Upper	239	25YrCHI3Hr	0.27	91.93	92.15	92.12	92.19	0.011193	0.82	0.32	2.23	0.69
River 1	Reach 1-Upper	239	50YrCHI3Hr	0.32	91.93	92.18	92.13	92.21	0.010512	0.85	0.38	2.35	0.68
River 1	Reach 1-Upper	239	100YrCHI3Hr	0.38	91.93	92.20	92.15	92.24	0.009943	0.87	0.44	2.48	0.67
River 1	Reach 1-Upper	239	2YrSCS24Hr	0.14	91.93	92.08	92.06	92.11	0.014638	0.74	0.18	1.83	0.74
River 1	Reach 1-Upper	239	5YrSCS24Hr	0.22	91.93	92.13	92.10	92.16	0.012117	0.79	0.27	2.11	0.70
River 1	Reach 1-Upper	239	10YrSCS24Hr	0.27	91.93	92.16	92.12	92.19	0.011093	0.82	0.33	2.25	0.69
River 1	Reach 1-Upper	239	25YrSCS24Hr	0.35	91.93	92.19	92.14	92.23	0.010240	0.86	0.40	2.41	0.67
River 1	Reach 1-Upper	239	50YrSCS24Hr	0.41	91.93	92.21	92.16	92.25	0.009700	0.88	0.46	2.53	0.66
River 1	Reach 1-Upper	239	100YrSCS24Hr	0.47	91.93	92.23	92.18	92.28	0.009178	0.90	0.52	2.66	0.65
River 1	Reach 1-Upper	218	2YrCHI3Hr	0.09	91.82	91.98	91.90	91.98	0.002022	0.31	0.30	2.52	0.28
River 1	Reach 1-Upper	218	5YrCHI3Hr	0.15	91.82	92.02	91.93	92.03	0.002161	0.37	0.41	2.74	0.31
River 1	Reach 1-Upper	218	10YrCHI3Hr	0.20	91.82	92.05	91.94	92.06	0.002207	0.41	0.49	2.87	0.31
River 1	Reach 1-Upper	218	25YrCHI3Hr	0.27	91.82	92.08	91.96	92.09	0.002325	0.45	0.59	3.03	0.33
River 1	Reach 1-Upper	218	50YrCHI3Hr	0.32	91.82	92.10	91.97	92.12	0.002387	0.48	0.66	3.14	0.34
River 1	Reach 1-Upper	218	100YrCHI3Hr	0.38	91.82	92.13	91.99	92.14	0.002436	0.51	0.74	3.27	0.34
River 1	Reach 1-Upper	218	2YrSCS24Hr	0.14	91.82	92.01	91.92	92.01	0.002130	0.35	0.38	2.68	0.30
River 1	Reach 1-Upper	218	5YrSCS24Hr	0.22	91.82	92.06	91.95	92.06	0.002240	0.42	0.52	2.91	0.32
River 1	Reach 1-Upper	218	10YrSCS24Hr	0.27	91.82	92.08	91.96	92.09	0.002335	0.46	0.60	3.04	0.33
River 1	Reach 1-Upper	218	25YrSCS24Hr	0.35	91.82	92.12	91.98	92.13	0.002410	0.50	0.70	3.20	0.34
River 1	Reach 1-Upper	218	50YrSCS24Hr	0.41	91.82	92.14	92.00	92.15	0.002460	0.53	0.78	3.33	0.35
River 1	Reach 1-Upper	218	100YrSCS24Hr	0.47	91.82	92.17	92.01	92.18	0.002488	0.55	0.86	3.49	0.35
River 1	Reach 1-Upper	197	2YrCHI3Hr	0.09	91.73	91.86	91.84	91.88	0.015440	0.67	0.14	1.62	0.74
River 1	Reach 1-Upper	197	5YrCHI3Hr	0.15	91.73	91.90	91.88	91.93	0.013158	0.74	0.21	1.89	0.71
River 1	Reach 1-Upper	197	10YrCHI3Hr	0.20	91.73	91.93	91.90	91.96	0.012270	0.78	0.26	2.03	0.70
River 1	Reach 1-Upper	197	25YrCHI3Hr	0.27	91.73	91.96	91.92	91.99	0.011534	0.84	0.32	2.17	0.70
River 1	Reach 1-Upper	197	50YrCHI3Hr	0.32	91.73	91.98	91.94	92.02	0.010821	0.87	0.37	2.28	0.69
River 1	Reach 1-Upper	197	100YrCHI3Hr	0.38	91.73	92.00	91.96	92.04	0.010553	0.90	0.42	2.38	0.68
River 1	Reach 1-Upper	197	2YrSCS24Hr	0.14	91.73	91.89	91.87	91.92	0.013722	0.72	0.19	1.83	0.72
River 1	Reach 1-Upper	197	5YrSCS24Hr	0.22	91.73	91.93	91.90	91.97	0.012069	0.80	0.27	2.07	0.70
River 1	Reach 1-Upper	197	10YrSCS24Hr	0.27	91.73	91.96	91.92	92.00	0.011461	0.84	0.32	2.19	0.70
River 1	Reach 1-Upper	197	25YrSCS24Hr	0.35	91.73	91.99	91.95	92.03	0.010693	0.88	0.39	2.33	0.69
River 1	Reach 1-Upper	197	50YrSCS24Hr	0.41	91.73	92.01	91.96	92.05	0.010457	0.92	0.44	2.42	0.69
River 1	Reach 1-Upper	197	100YrSCS24Hr	0.47	91.73	92.03	91.98	92.08	0.010270	0.96	0.50	2.52	0.69
River 1	Reach 1-Upper	174	2YrCHI3Hr	0.09	91.52	91.71	91.64	91.72	0.004267	0.43	0.21	1.87	0.41
River 1	Reach 1-Upper	174	5YrCHI3Hr	0.15	91.52	91.75	91.68	91.77	0.004475	0.50	0.31	2.19	0.43
River 1	Reach 1-Upper	174	10YrCHI3Hr	0.20	91.52	91.78	91.70	91.79	0.004646	0.55	0.36	2.32	0.45
River 1	Reach 1-Upper	174	25YrCHI3Hr	0.27	91.52	91.81	91.72	91.83	0.004785	0.61	0.44	2.47	0.46
River 1	Reach 1-Upper	174	50YrCHI3Hr	0.32	91.52	91.83	91.74	91.85	0.004939	0.65	0.49	2.58	0.47
River 1	Reach 1-Upper	174	100YrCHI3Hr	0.38	91.52	91.85	91.76	91.88	0.005072	0.69	0.55	2.69	0.49
River 1	Reach 1-Upper	174	2YrSCS24Hr	0.14	91.52	91.74	91.67	91.75	0.004398	0.48	0.28	2.12	0.42
River 1	Reach 1-Upper	174	5YrSCS24Hr	0.22	91.52	91.79	91.70	91.80	0.004687	0.57	0.38	2.35	0.45
River 1	Reach 1-Upper	174	10YrSCS24Hr	0.27	91.52	91.81	91.72	91.83	0.004808	0.61	0.44	2.48	0.46
River 1	Reach 1-Upper	174	25YrSCS24Hr	0.35	91.52	91.84	91.75	91.86	0.005003	0.67	0.52	2.63	0.48
River 1	Reach 1-Upper	174	50YrSCS24Hr	0.41	91.52	91.86	91.77	91.89	0.005118	0.71	0.58	2.73	0.49
River 1	Reach 1-Upper	174	100YrSCS24Hr	0.47	91.52	91.89	91.78	91.91	0.005160	0.74	0.64	2.85	0.50
River 1	Reach 1-Upper	154	2YrCHI3Hr	0.09	91.43	91.62	91.56	91.63	0.004368	0.40	0.23	2.24	0.41
River 1	Reach 1-Upper	154	5YrCHI3Hr	0.15	91.43	91.67	91.60	91.68	0.004241	0.46	0.33	2.63	0.42
River 1	Reach 1-Upper	154	10YrCHI3Hr	0.20	91.43	91.69	91.61	91.70	0.004186	0.50	0.40	2.85	0.42
River 1	Reach 1-Upper	154	25YrCHI3Hr	0.27	91.43	91.72	91.64	91.74	0.004089	0.53	0.50	3.10	0.42
River 1	Reach 1-Upper	154	50YrCHI3Hr	0.32	91.43	91.75	91.65	91.76	0.003991	0.56	0.57	3.27	0.43
River 1	Reach 1-Upper	154	100YrCHI3Hr	0.38	91.43	91.77	91.67	91.79	0.003887	0.58	0.65	3.43	0.43

HEC-RAS Plan: 20250603-Post_Dev_v01 (Continued)

River	Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
River 1	Reach 1-Upper	154	2YrSCS24Hr	0.14	91.43	91.65	91.59	91.66	0.004250	0.45	0.30	2.53	0.41
River 1	Reach 1-Upper	154	5YrSCS24Hr	0.22	91.43	91.70	91.62	91.71	0.004166	0.51	0.43	2.91	0.42
River 1	Reach 1-Upper	154	10YrSCS24Hr	0.27	91.43	91.73	91.64	91.74	0.004078	0.54	0.51	3.13	0.43
River 1	Reach 1-Upper	154	25YrSCS24Hr	0.35	91.43	91.76	91.66	91.77	0.003941	0.57	0.61	3.34	0.43
River 1	Reach 1-Upper	154	50YrSCS24Hr	0.41	91.43	91.78	91.67	91.80	0.003849	0.59	0.69	3.49	0.43
River 1	Reach 1-Upper	154	100YrSCS24Hr	0.47	91.43	91.80	91.69	91.82	0.003765	0.61	0.77	3.65	0.43
River 1	Reach 1-Upper	137	2YrCHI3Hr	0.09	91.33	91.49	91.46	91.51	0.011873	0.65	0.14	1.44	0.66
River 1	Reach 1-Upper	137	5YrCHI3Hr	0.15	91.33	91.54	91.50	91.56	0.011294	0.74	0.21	1.67	0.67
River 1	Reach 1-Upper	137	10YrCHI3Hr	0.20	91.33	91.56	91.52	91.59	0.010987	0.79	0.25	1.81	0.67
River 1	Reach 1-Upper	137	25YrCHI3Hr	0.27	91.33	91.59	91.55	91.63	0.010557	0.84	0.32	1.98	0.67
River 1	Reach 1-Upper	137	50YrCHI3Hr	0.32	91.33	91.62	91.57	91.66	0.010224	0.87	0.37	2.11	0.67
River 1	Reach 1-Upper	137	100YrCHI3Hr	0.38	91.33	91.64	91.59	91.69	0.009831	0.90	0.42	2.25	0.66
River 1	Reach 1-Upper	137	2YrSCS24Hr	0.14	91.33	91.52	91.49	91.55	0.011421	0.72	0.19	1.61	0.67
River 1	Reach 1-Upper	137	5YrSCS24Hr	0.22	91.33	91.57	91.53	91.60	0.010887	0.80	0.27	1.85	0.67
River 1	Reach 1-Upper	137	10YrSCS24Hr	0.27	91.33	91.60	91.55	91.63	0.010513	0.85	0.32	2.00	0.67
River 1	Reach 1-Upper	137	25YrSCS24Hr	0.35	91.33	91.63	91.58	91.67	0.010071	0.89	0.39	2.17	0.67
River 1	Reach 1-Upper	137	50YrSCS24Hr	0.41	91.33	91.65	91.60	91.70	0.009667	0.91	0.45	2.30	0.66
River 1	Reach 1-Upper	137	100YrSCS24Hr	0.47	91.33	91.68	91.62	91.72	0.009323	0.94	0.51	2.43	0.66
River 1	Reach 1-Upper	116	2YrCHI3Hr	0.09	91.23	91.39	91.32	91.40	0.003087	0.37	0.24	2.11	0.35
River 1	Reach 1-Upper	116	5YrCHI3Hr	0.15	91.23	91.44	91.35	91.45	0.002919	0.43	0.36	2.39	0.35
River 1	Reach 1-Upper	116	10YrCHI3Hr	0.20	91.23	91.47	91.37	91.48	0.002861	0.46	0.44	2.56	0.36
River 1	Reach 1-Upper	116	25YrCHI3Hr	0.27	91.23	91.51	91.39	91.52	0.002819	0.50	0.54	2.76	0.36
River 1	Reach 1-Upper	116	50YrCHI3Hr	0.32	91.23	91.53	91.41	91.55	0.002809	0.52	0.61	2.91	0.36
River 1	Reach 1-Upper	116	100YrCHI3Hr	0.38	91.23	91.56	91.43	91.58	0.002814	0.55	0.69	3.05	0.37
River 1	Reach 1-Upper	116	2YrSCS24Hr	0.14	91.23	91.43	91.34	91.43	0.002948	0.41	0.33	2.32	0.35
River 1	Reach 1-Upper	116	5YrSCS24Hr	0.22	91.23	91.48	91.37	91.49	0.002848	0.47	0.46	2.61	0.36
River 1	Reach 1-Upper	116	10YrSCS24Hr	0.27	91.23	91.51	91.39	91.52	0.002816	0.50	0.55	2.78	0.36
River 1	Reach 1-Upper	116	25YrSCS24Hr	0.35	91.23	91.55	91.41	91.56	0.002808	0.54	0.65	2.98	0.37
River 1	Reach 1-Upper	116	50YrSCS24Hr	0.41	91.23	91.58	91.43	91.59	0.002653	0.55	0.74	3.12	0.36
River 1	Reach 1-Upper	116	100YrSCS24Hr	0.47	91.23	91.61	91.45	91.62	0.002570	0.57	0.83	3.26	0.36
River 1	Reach 1-Upper	95	2YrCHI3Hr	0.09	91.07	91.29	91.24	91.31	0.006025	0.53	0.17	1.41	0.48
River 1	Reach 1-Upper	95	5YrCHI3Hr	0.15	91.07	91.34	91.27	91.36	0.007024	0.64	0.24	1.62	0.54
River 1	Reach 1-Upper	95	10YrCHI3Hr	0.20	91.07	91.36	91.30	91.39	0.007632	0.71	0.28	1.74	0.57
River 1	Reach 1-Upper	95	25YrCHI3Hr	0.27	91.07	91.39	91.33	91.42	0.008133	0.79	0.34	1.88	0.59
River 1	Reach 1-Upper	95	50YrCHI3Hr	0.32	91.07	91.41	91.35	91.45	0.008601	0.84	0.38	1.98	0.62
River 1	Reach 1-Upper	95	100YrCHI3Hr	0.38	91.07	91.43	91.37	91.47	0.010479	0.95	0.40	2.04	0.68
River 1	Reach 1-Upper	95	2YrSCS24Hr	0.14	91.07	91.32	91.26	91.34	0.006791	0.61	0.22	1.56	0.52
River 1	Reach 1-Upper	95	5YrSCS24Hr	0.22	91.07	91.37	91.30	91.40	0.007803	0.73	0.29	1.77	0.57
River 1	Reach 1-Upper	95	10YrSCS24Hr	0.27	91.07	91.40	91.33	91.43	0.008086	0.79	0.35	1.90	0.59
River 1	Reach 1-Upper	95	25YrSCS24Hr	0.35	91.07	91.42	91.36	91.46	0.008817	0.87	0.40	2.03	0.63
River 1	Reach 1-Upper	95	50YrSCS24Hr	0.41	91.07	91.39	91.38	91.47	0.020127	1.23	0.33	1.86	0.93
River 1	Reach 1-Upper	95	100YrSCS24Hr	0.47	91.07	91.40	91.40	91.49	0.023204	1.35	0.35	1.91	1.01
River 1	Reach 1-Upper	72	2YrCHI3Hr	0.09	90.91	91.00	91.00	91.03	0.032221	0.77	0.12	2.00	1.02
River 1	Reach 1-Upper	72	5YrCHI3Hr	0.15	90.91	91.03	91.03	91.07	0.028410	0.85	0.18	2.44	0.99
River 1	Reach 1-Upper	72	10YrCHI3Hr	0.20	90.91	91.05	91.05	91.09	0.026746	0.90	0.22	2.65	0.98
River 1	Reach 1-Upper	72	25YrCHI3Hr	0.27	90.91	91.07	91.07	91.12	0.026304	0.97	0.27	2.83	1.00
River 1	Reach 1-Upper	72	50YrCHI3Hr	0.32	90.91	91.08	91.08	91.13	0.025112	1.01	0.32	2.96	0.99
River 1	Reach 1-Upper	72	100YrCHI3Hr	0.38	90.91	91.11	91.10	91.15	0.019074	0.97	0.39	3.17	0.88
River 1	Reach 1-Upper	72	2YrSCS24Hr	0.14	90.91	91.03	91.03	91.06	0.028884	0.82	0.16	2.32	0.99
River 1	Reach 1-Upper	72	5YrSCS24Hr	0.22	90.91	91.05	91.05	91.10	0.026334	0.91	0.24	2.69	0.98
River 1	Reach 1-Upper	72	10YrSCS24Hr	0.27	90.91	91.07	91.07	91.12	0.026938	0.99	0.28	2.83	1.01
River 1	Reach 1-Upper	72	25YrSCS24Hr	0.35	90.91	91.09	91.09	91.14	0.024807	1.03	0.34	3.02	0.99
River 1	Reach 1-Upper	72	50YrSCS24Hr	0.41	90.91	91.16	91.10	91.18	0.007645	0.72	0.57	3.60	0.58
River 1	Reach 1-Upper	72	100YrSCS24Hr	0.47	90.91	91.23	91.12	91.24	0.003374	0.57	0.83	4.09	0.40
River 1	Reach 1-Lower	56	2YrCHI3Hr	0.15	90.47	90.74	90.58	90.74	0.000351	0.20	0.77	10.31	0.13
River 1	Reach 1-Lower	56	5YrCHI3Hr	0.27	90.47	90.85	90.60	90.85	0.000292	0.23	1.16	14.65	0.13
River 1	Reach 1-Lower	56	10YrCHI3Hr	0.36	90.47	90.92	90.62	90.92	0.000280	0.26	1.40	17.01	0.13
River 1	Reach 1-Lower	56	25YrCHI3Hr	0.49	90.47	91.00	90.64	91.01	0.000270	0.29	1.70	19.75	0.13
River 1	Reach 1-Lower	56	50YrCHI3Hr	0.59	90.47	91.07	90.66	91.07	0.000264	0.31	1.92	20.02	0.13
River 1	Reach 1-Lower	56	100YrCHI3Hr	0.71	90.47	91.13	90.68	91.13	0.000265	0.33	2.14	20.02	0.14
River 1	Reach 1-Lower	56	2YrSCS24Hr	0.24	90.47	90.82	90.60	90.82	0.000304	0.22	1.06	13.59	0.13
River 1	Reach 1-Lower	56	5YrSCS24Hr	0.40	90.47	90.94	90.63	90.95	0.000274	0.27	1.49	18.21	0.13
River 1	Reach 1-Lower	56	10YrSCS24Hr	0.51	90.47	91.02	90.64	91.02	0.000269	0.29	1.74	19.88	0.13
River 1	Reach 1-Lower	56	25YrSCS24Hr	0.66	90.47	91.10	90.67	91.11	0.000265	0.32	2.04	20.02	0.14
River 1	Reach 1-Lower	56	50YrSCS24Hr	0.78	90.47	91.17	90.69	91.17	0.000261	0.34	2.27	20.02	0.14
River 1	Reach 1-Lower	56	100YrSCS24Hr	0.91	90.47	91.23	90.71	91.24	0.000263	0.37	2.49	20.02	0.14
River 1	Reach 1-Lower	50		Culvert									
River 1	Reach 1-Lower	38	2YrCHI3Hr	0.15	90.46	90.57	90.53	90.58	0.005136	0.44	0.35	30.55	0.44
River 1	Reach 1-Lower	38	5YrCHI3Hr	0.27	90.46	90.60	90.55	90.62	0.007100	0.61	0.44	34.54	0.54
River 1	Reach 1-Lower	38	10YrCHI3Hr	0.36	90.46	90.61	90.57	90.64	0.008644	0.73	0.50	35.72	0.61
River 1	Reach 1-Lower	38	25YrCHI3Hr	0.49	90.46	90.63	90.60	90.67	0.010630	0.87	0.56	36.53	0.69
River 1	Reach 1-Lower	38	50YrCHI3Hr	0.59	90.46	90.64	90.61	90.69	0.012282	0.98	0.60	36.92	0.75
River 1	Reach 1-Lower	38	100YrCHI3Hr	0.71	90.46	90.66	90.63	90.72	0.013950	1.10	0.65	37.68	0.81
River 1	Reach 1-Lower	38	2YrSCS24Hr	0.24	90.46	90.59	90.55	90.61	0.006473	0.56	0.42	33.74	0.52
River 1	Reach 1-Lower	38	5YrSCS24Hr	0.40	90.46	90.62	90.58	90.65	0.009216	0.77	0.52	36.25	0.64
River 1	Reach 1-Lower	38	10YrSCS24Hr	0.51	90.46	90.63	90.60	90.68	0.010974	0.89	0.57	36.59	0.71
River 1	Reach 1-Lower	38	25YrSCS24Hr	0.66	90.46	90.65	90.63	90.71	0.013194	1.05	0.63	37.35	0.79
River 1	Reach 1-Lower	38	50YrSCS24Hr	0.78	90.46	90.66	90.64	90.73	0.015131	1.17	0.67	38.00	0.85
River 1	Reach 1-Lower	38	100YrSCS24Hr	0.91	90.46	90.67	90.66	90.76	0.017508	1.30	0.70	38.44	0.92
River 1	Reach 1-Lower	0	2YrCHI3Hr	0.15	90.42	90.50	90.46	90.50	0.001001	0.14	1.11	19.02	0.18
River 1	Reach 1-Lower	0	5YrCHI3Hr	0.27	90.42	90.53	90.47	90.53	0.001000	0.17	1.61	20.06	0.19
River 1	Reach 1-Lower	0	10YrCHI3Hr	0.36	90.42	90.54	90.48	90.55	0.001000	0.19	1.93	20.29	0.19

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River	Reach	River Sta	Profile	Q Total (m3/s)	Min Ch El (m)	W.S. Elev (m)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
River 1	Reach 1-Lower	0	25YrCHI3Hr	0.49	90.42	90.56	90.49	90.56	0.001001	0.21	2.32	20.57	0.20
River 1	Reach 1-Lower	0	50YrCHI3Hr	0.59	90.42	90.58	90.49	90.58	0.001000	0.23	2.62	20.78	0.20
River 1	Reach 1-Lower	0	100YrCHI3Hr	0.71	90.42	90.59	90.50	90.60	0.001000	0.24	2.95	21.44	0.21
River 1	Reach 1-Lower	0	2YrSCS24Hr	0.24	90.42	90.52	90.46	90.52	0.001000	0.16	1.49	19.97	0.19
River 1	Reach 1-Lower	0	5YrSCS24Hr	0.40	90.42	90.55	90.48	90.55	0.001000	0.20	2.04	20.38	0.20
River 1	Reach 1-Lower	0	10YrSCS24Hr	0.51	90.42	90.57	90.49	90.57	0.001001	0.21	2.38	20.62	0.20
River 1	Reach 1-Lower	0	25YrSCS24Hr	0.66	90.42	90.59	90.49	90.59	0.001001	0.24	2.81	21.20	0.21
River 1	Reach 1-Lower	0	50YrSCS24Hr	0.78	90.42	90.60	90.50	90.60	0.001001	0.25	3.13	21.55	0.21
River 1	Reach 1-Lower	0	100YrSCS24Hr	0.91	90.42	90.62	90.51	90.62	0.001000	0.26	3.45	21.74	0.21

APPENDIX H CITY OF OTTAWA DESIGN CHECKLIST

4. Development Servicing Study Checklist

The following section describes the checklist of the required content of servicing studies. It is expected that the proponent will address each one of the following items for the study to be deemed complete and ready for review by City of Ottawa Infrastructure Approvals staff.

The level of required detail in the Servicing Study will increase depending on the type of application. For example, for Official Plan amendments and re-zoning applications, the main issues will be to determine the capacity requirements for the proposed change in land use and confirm this against the existing capacity constraint, and to define the solutions, phasing of works and the financing of works to address the capacity constraint. For subdivisions and site plans, the above will be required with additional detailed information supporting the servicing within the development boundary.

4.1 General Content

Criteria	Location (if applicable)
☐ Executive Summary (for larger reports only).	N/A
☐ Date and revision number of the report.	On Cover
☐ Location map and plan showing municipal address, boundary, and layout of proposed development.	Appendix A
☐ Plan showing the site and location of all existing services.	Site Servicing Plan (C102)
☐ Development statistics, land use, density, adherence to zoning and official plan, and reference to applicable subwatershed and watershed plans that provide context to which individual developments must adhere.	1.1 Purpose 1.2 Site Description 6.0 Proposed Stormwater Management
☐ Summary of pre-consultation meetings with City and other approval agencies.	Appendix B
☐ Reference and confirm conformance to higher level studies and reports (Master Servicing Studies, Environmental Assessments, Community Design Plans), or in the case where it is not in conformance, the proponent must provide justification and develop a defensible design criteria.	1.1 Purpose 1.2 Site Description 6.0 Proposed Stormwater Management
☐ Statement of objectives and servicing criteria.	3.0 Pre-Consultation Summary

☐ Identification of existing and proposed infrastructure available in the immediate area.	N/ A
☐ Identification of Environmentally Significant Areas, watercourses and Municipal Drains potentially impacted by the proposed development (Reference can be made to the Natural Heritage Studies, if available).	Ste Grading Plan (C101)
☐ Concept level master grading plan to confirm existing and proposed grades in the development. This is required to confirm the feasibility of proposed stormwater management and drainage, soil removal and fill constraints, and potential impacts to neighbouring properties. This is also required to confirm that the proposed grading will not impede existing major system flow paths.	Ste Grading Plan (C101)
☐ Identification of potential impacts of proposed piped services on private services (such as wells and septic fields on adjacent lands) and mitigation required to address potential impacts.	N/ A
☐ Proposed phasing of the development, if applicable.	N/ A
☐ Reference to geotechnical studies and recommendations concerning servicing.	Section 2.0 Background Studies, Standards and References
☐ All preliminary and formal site plan submissions should have the following information: ○ Metric scale ○ North arrow (including construction North) ○ Key plan ○ Name and contact information of applicant and property owner ○ Property limits including bearings and dimensions ○ Existing and proposed structures and parking areas ○ Easements, road widening and rights-of-way ○ Adjacent street names	Ste Grading Plan (C101)

4.2 Development Servicing Report: Water

Criteria	Location (if applicable)
☐ Confirm consistency with Master Servicing Study, if available	N/ A
☐ Availability of public infrastructure to service proposed development	N/ A
☐ Identification of system constraints	N/ A
☐ Identify boundary conditions	Appendix C
☐ Confirmation of adequate domestic supply and pressure	N/ A
☐ Confirmation of adequate fire flow protection and confirmation that fire flow is calculated as per the Fire Underwriter's Survey. Output should show available fire flow at locations throughout the development.	Appendix C
☐ Provide a check of high pressures. If pressure is found to be high, an assessment is required to confirm the application of pressure reducing valves.	N/ A
☐ Definition of phasing constraints. Hydraulic modeling is required to confirm servicing for all defined phases of the project including the ultimate design	N/ A
☐ Address reliability requirements such as appropriate location of shut-off valves	N/ A
☐ Check on the necessity of a pressure zone boundary modification.	N/ A
☐ Reference to water supply analysis to show that major infrastructure is capable of delivering sufficient water for the proposed land use. This includes data that shows that the expected demands under average day, peak hour and fire flow conditions provide water within the required pressure range	Appendix C, Section 4.2 Proposed Water Servicing

☐ Description of the proposed water distribution network, including locations of proposed connections to the existing system, provisions for necessary looping, and appurtenances (valves, pressure reducing valves, valve chambers, and fire hydrants) including special metering provisions.	Site Servicing Plan (C101)
☐ Description of off-site required feeder mains, booster pumping stations, and other water infrastructure that will be ultimately required to service proposed development, including financing, interim facilities, and timing of implementation.	N/A
☐ Confirmation that water demands are calculated based on the City of Ottawa Design Guidelines.	Appendix C
☐ Provision of a model schematic showing the boundary conditions locations, streets, parcels, and building locations for reference.	N/A

4.3 Development Servicing Report: Wastewater

Criteria	Location (if applicable)
☐ Summary of proposed design criteria (Note: Wet-weather flow criteria should not deviate from the City of Ottawa Sewer Design Guidelines. Monitored flow data from relatively new infrastructure cannot be used to justify capacity requirements for proposed infrastructure).	N/A
☐ Confirm consistency with Master Servicing Study and/or justifications for deviations.	N/A
☐ Consideration of local conditions that may contribute to extraneous flows that are higher than the recommended flows in the guidelines. This includes groundwater and soil conditions, and age and condition of sewers.	N/A
☐ Description of existing sanitary sewer available for discharge of wastewater from proposed development.	Section 5.2 Proposed Sanitary Servicing

☐ Verify available capacity in downstream sanitary sewer and/or identification of upgrades necessary to service the proposed development. (Reference can be made to previously completed Master Servicing Study if applicable)	Section 5.2 Proposed Sanitary Servicing
☐ Calculations related to dry-weather and wet-weather flow rates from the development in standard MOE sanitary sewer design table (Appendix 'C') format.	N/ A
☐ Description of proposed sewer network including sewers, pumping stations, and forcemains.	Section 5.2 Proposed Sanitary Servicing
☐ Discussion of previously identified environmental constraints and impact on servicing (environmental constraints are related to limitations imposed on the development in order to preserve the physical condition of watercourses, vegetation, soil cover, as well as protecting against water quantity and quality).	N/ A
☐ Pumping stations: impacts of proposed development on existing pumping stations or requirements for new pumping station to service development.	N/ A
☐ Forcemain capacity in terms of operational redundancy, surge pressure and maximum flow velocity.	N/ A
☐ Identification and implementation of the emergency overflow from sanitary pumping stations in relation to the hydraulic grade line to protect against basement flooding.	N/ A
☐ Special considerations such as contamination, corrosive environment etc.	N/ A

4.4 Development Servicing Report: Stormwater Checklist

Criteria	Location (if applicable)
☐ Description of drainage outlets and downstream constraints including legality of outlets (i.e. municipal drain, right-of-way, watercourse, or private property)	Section 6.0 Storm Sewer Servicing & Section 7.0 Proposed Stormwater Management
☐ Analysis of available capacity in existing public infrastructure.	N/A
☐ A drawing showing the subject lands, its surroundings, the receiving watercourse, existing drainage patterns, and proposed drainage pattern.	Pre & Post-Development Plans
☐ Water quantity control objective (e.g. controlling post-development peak flows to pre-development level for storm events ranging from the 2 or 5-year event (dependent on the receiving sewer design) to 100-year return period); if other objectives are being applied, a rationale must be included with reference to hydrologic analyses of the potentially affected subwatersheds, taking into account long-term cumulative effects.	Section 6.0 Storm Sewer Servicing & Section 7.0 Proposed Stormwater Management
☐ Water Quality control objective (basic, normal or enhanced level of protection based on the sensitivities of the receiving watercourse) and storage requirements.	Section 6.0 Storm Sewer Servicing & Section 7.0 Proposed Stormwater Management
☐ Description of the stormwater management concept with facility locations and descriptions with references and supporting information.	Section 6.0 Storm Sewer Servicing & Section 7.0 Proposed Stormwater Management
☐ Set-back from private sewage disposal systems.	N/A
☐ Watercourse and hazard lands setbacks.	N/A
☐ Record of pre-consultation with the Ontario Ministry of Environment and the Conservation Authority that has jurisdiction on the affected watershed.	N/A
☐ Confirm consistency with sub-watershed and Master Servicing Study, if applicable study exists.	N/A
☐ Storage requirements (complete with calculations) and conveyance capacity for minor events (1:5-year return period) and major events (1:100-year return period).	Appendix G

☐ Identification of watercourses within the proposed development and how watercourses will be protected, or, if necessary, altered by the proposed development with applicable approvals.	Site Grading Plan (C101)
☐ Calculate pre-and post development peak flow rates including a description of existing site conditions and proposed impervious areas and drainage catchments in comparison to existing conditions.	Appendix G, Section 7.0 Proposed Stormwater Management
☐ Any proposed diversion of drainage catchment areas from one outlet to another.	Section 6.0 Storm Sewer Servicing & Section 7.0 Proposed Stormwater Management
☐ Proposed minor and major systems including locations and sizes of stormwater trunk sewers, and stormwater management facilities.	Section 6.0 Storm Sewer Servicing & Section 7.0 Proposed Stormwater Management
☐ If quantity control is not proposed, demonstration that downstream system has adequate capacity for the post-development flows up to and including the 100-year return period storm event.	N/A
☐ Identification of potential impacts to receiving watercourses	N/A
☐ Identification of municipal drains and related approval requirements.	N/A
☐ Descriptions of how the conveyance and storage capacity will be achieved for the development.	Section 6.0 Storm Sewer Servicing & Section 7.0 Proposed Stormwater Management
☐ 100-year flood levels and major flow routing to protect proposed development from flooding for establishing minimum building elevations (MBE) and overall grading.	Site Grading Plan (C101)
☐ Inclusion of hydraulic analysis including hydraulic grade line elevations.	N/A

☐ Description of approach to erosion and sediment control during construction for the protection of receiving watercourse or drainage corridors.	Section 8.0 Sediment & Erosion Control
☐ Identification of floodplains – proponent to obtain relevant floodplain information from the appropriate Conservation Authority. The proponent may be required to delineate floodplain elevations to the satisfaction of the Conservation Authority if such information is not available or if information does not match current conditions.	N/A
☐ Identification of fill constraints related to floodplain and geotechnical investigation.	N/A

4.5 Approval and Permit Requirements: Checklist

The Servicing Study shall provide a list of applicable permits and regulatory approvals necessary for the proposed development as well as the relevant issues affecting each approval. The approval and permitting shall include but not be limited to the following:

Criteria	Location (if applicable)
☐ Conservation Authority as the designated approval agency for modification of floodplain, potential impact on fish habitat, proposed works in or adjacent to a watercourse, cut/fill permits and Approval under Lakes and Rivers Improvement Act. The Conservation Authority is not the approval authority for the Lakes and Rivers Improvement Act. Where there are Conservation Authority regulations in place, approval under the Lakes and Rivers Improvement Act is not required, except in cases of dams as defined in the Act.	N/A
☐ Application for Certificate of Approval (CofA) under the Ontario Water Resources Act.	N/A
☐ Changes to Municipal Drains.	N/A
☐ Other permits (National Capital Commission, Parks Canada, Public Works and Government Services Canada, Ministry of Transportation etc.)	N/A

4.6 Conclusion Checklist

Criteria	Location (if applicable)
☐ Clearly stated conclusions and recommendations	Section 9.0 Summary Section 10.0 Recommendations
☐ Comments received from review agencies including the City of Ottawa and information on how the comments were addressed. Final sign-off from the responsible reviewing agency.	All are stamped
☐ All draft and final reports shall be signed and stamped by a professional Engineer registered in Ontario	All are stamped