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Iron Valley 2
Detailed Noise Control Study

Prepared for: Claridge Homes

IRON VALLEY 2
5331 Fernbank Road
OTTAWA, ONTARIO
Detailed Noise Control Study

Prepared By:

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Revised: November 5, 2021
Revised: November 14, 2025

Novatech File: 121011
Ref: R-2021-074

November 14, 2025

City of Ottawa
Planning and Infrastructure Approvals
110 Laurier Street West, 4th Floor
Ottawa, ON, K1P 1J1

Attention: Santhosh Kuruvilla

**Reference: Iron Valley 2
Detailed Noise Control Study
Our File No.: 121011**

Please find enclosed for your review the revised Detailed Noise Control Study to support a Site Plan application for the Iron Valley 2 (formerly Fernbank Zens) at 5331 Fernbank Road. The site is bounded by Cope Drive to the north, the existing SOHO development to the east, Fernbank Road to the south and Terry Fox Drive to the west.

This study evaluates the environmental impact of noise from traffic on the outdoor living areas and inside residential buildings and discusses the mitigation measures to attenuate noise to acceptable levels.

This report is submitted in support of the engineering detailed design for the Claridge Homes Site Plan application.

Trusting this report is adequate for your purposes. Should you have any questions, or require additional information pertaining to the enclosed report, please contact us.

Yours truly,

NOVATECH



Drew Blair, P. Eng.
Senior Project Coordinator, Land Development Engineering

Cc: Shawn Malhotra, Claridge Homes

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1.0 INTRODUCTION

This Detailed Noise Control Study was prepared as part of the engineering detailed design for the Iron Valley 2 (formerly Fernbank Zens) residential development at 5331 Fernbank Road. This report assesses the environmental impact of noise on the proposed development and outlines recommended mitigation measures, if required.

2.1 The Site

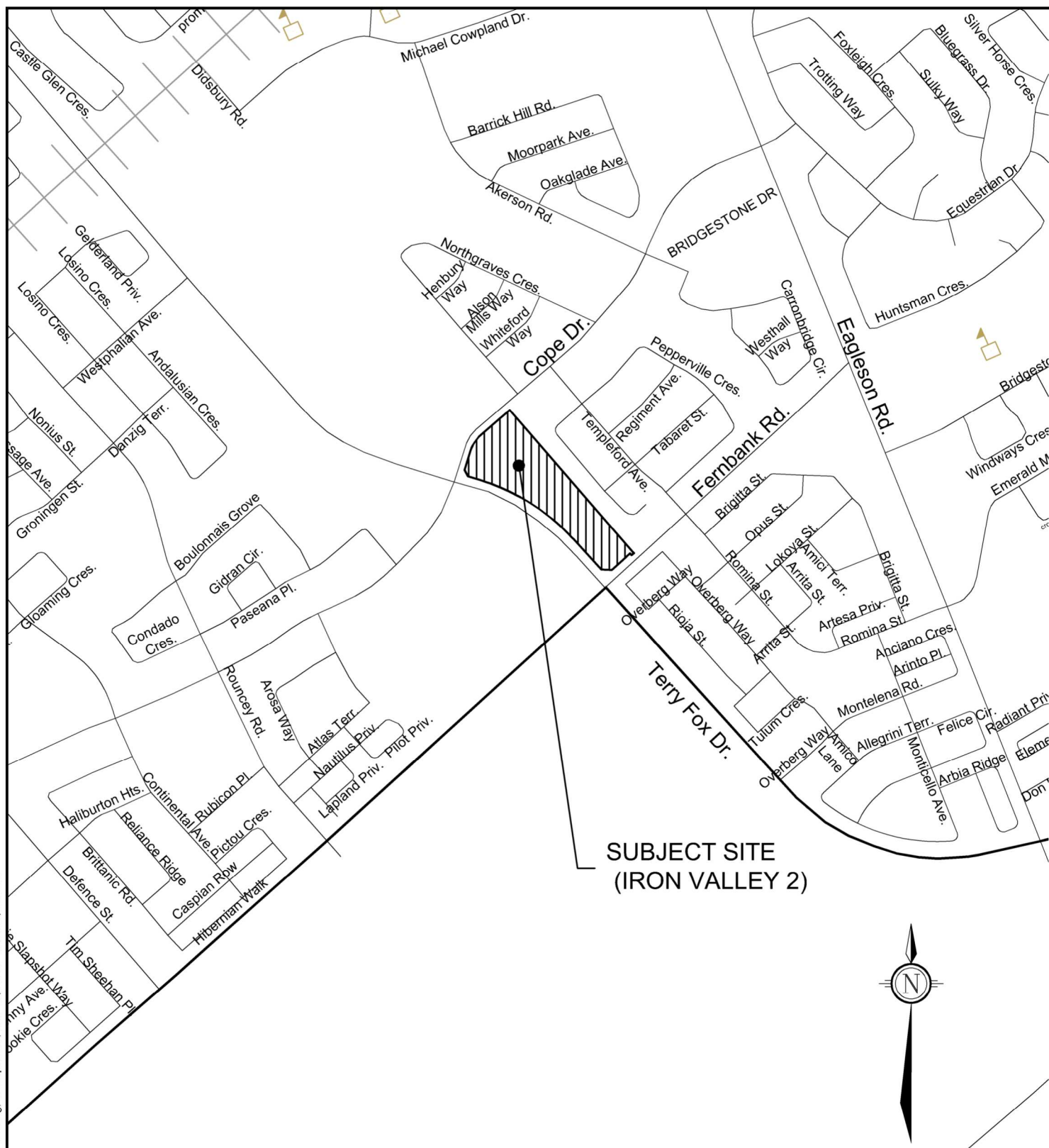
The proposed Iron Valley 2 site (approximately 3.68 ha) is owned by Claridge Homes and located within the City of Ottawa. The site is bounded by Cope Drive to the north, the existing SOHO development to the east, Fernbank Road to the south and Terry Fox Drive to the west as shown on **Figure 1A/1B – Key Plan**.

Figure 1A – Key Plan



The legal description of the property is designated as Part of Lot 30 Concession 10, Goulbourn, Part 1 Plan 4R17373, Except Part 4, Plan 4R20112; Ottawa. Subject to an Easement in Favour of Hydro Ottawa Limited Over Parts 5,6, 7, 8 and 9 Plan 4R20112 as in OC455206. Road Allowance Between Lots 30 and 31 Concession 10, Goulbourn Lying Between Parts 3 and 4 on 4R17373 and Part 2 on Plan 4R20112, as Closed by N599928; Ottawa. Part of Lot 31, Concession 10, Goulbourn, Part 1 on Plan 4R19334 City of Ottawa.

The site is proposed to be developed as a residential site plan which will consist of 64 townhouse units within 16 townhouse blocks and on-site parking with access from Cope Drive and Terry Fox Drive as shown on **Figure 2 – Site Plan**.



SUBJECT SITE
(IRON VALLEY 2)

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CITY OF OTTAWA
IRON VALLEY 2

KEY PLAN

SCALE

N.T.S.

DATE _____

NOV 2025

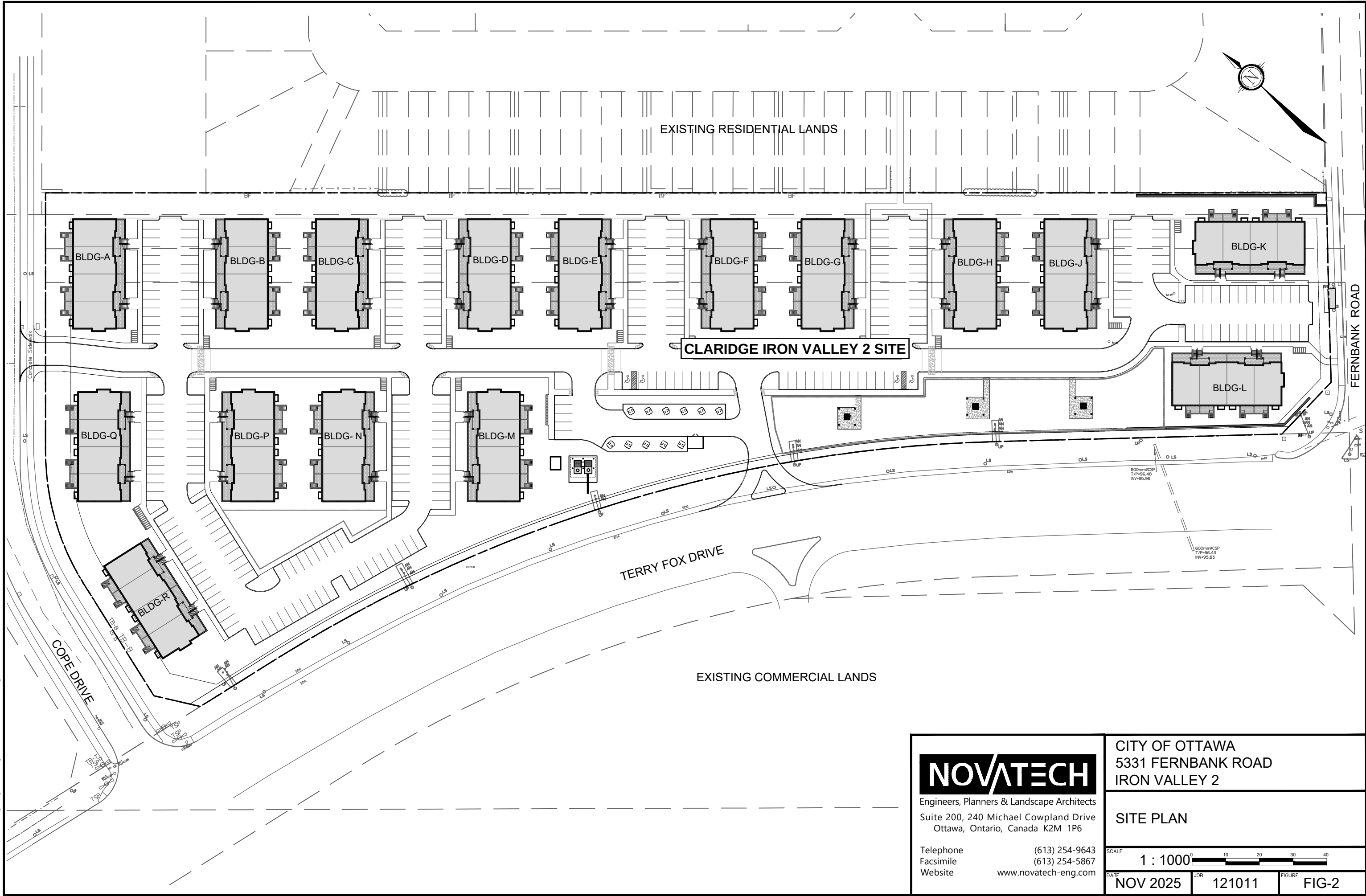
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121011

FIGURE

FIGURE 1B

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CITY OF OTTAWA
5331 FERNBANK ROAD
IRON VALLEY 2

SITE PLAN

SCALE 1 : 1000

DATE NOV 2025 JOB 121011 FIGURE FIG-2

2.0 NOISE SOURCES

The City of Ottawa Official Plan stipulates that a noise study shall be prepared when a new development is proposed within 100 metres of an arterial, major collector or collector roadway, or a rapid-transit corridor.

The potential surface road noise sources that were considered for the purposes of this study are Terry Fox Drive, Fernbank Road, and Cope Drive as all other roadways within the zone of influence were not arterial or collector roadways.

Terry Fox Drive is classified as an urban arterial roadway with a 44.5m protected ROW in the City of Ottawa Transportation Master Plan and Official Plan. Terry Fox Drive is currently a 2-lane undivided arterial road with a posted speed of 80km/hr fronting the site. As per Map 10 in the Transportation Master Plan (TMP), Road Network – 2031 Network Concept, there are future plans to widen Terry Fox Drive to 4 lanes. Therefore, for the purposes of this report, a 4-lane divided arterial road with an AADT level of 35,000 veh/day and a posted speed of 80km/hr will be utilized. This report separates Terry Fox into two separate noise sources: Terry Fox northbound lane and Terry Fox southbound lanes. The 35,000 veh/day is divided 50/50 between northbound and southbound lanes. The Terry Fox northbound lane is located approximately 10m closer to the site than the Terry Fox southbound lane. Refer to **Appendix A** for the excerpt from the TMP. A typical cross section for the Terry Fox Drive widening has been provided in **Appendix E**.

Fernbank Road is classified as an urban arterial roadway with a 30.0m protected ROW in the City of Ottawa Transportation Master Plan and Official Plan. Fernbank Road is currently a 2-lane undivided arterial road with a posted speed of 60km/hr fronting the site. Therefore, for the purposes of this report, a 2-lane undivided arterial road with an AADT level of 15,000 veh/day and a posted speed of 60km/hr will be utilized.

Cope Drive is classified as an urban collector roadway with a 24m protected ROW with an AADT level of 8,000 veh/day and a posted speed limit of 50km/hr.

There is no railway ROW within 250m that impacts the site.

There is no airport noise affecting this site.

There are no stationary noise sources that affect this site.

3.0 CITY OF OTTAWA NOISE CONTROL GUIDELINES

3.1 Sound Level Criteria

The City of Ottawa is concerned with noise from aircraft, roads, transitways, and railways, as expressed in Tables 2.2a: Sound Level Limit for Outdoor Living Areas – Road and Rail, Table 2.2b: Sound Level Limit for Indoor Living Areas Road and Rail, and Table 2.2c: Supplementary Sound Level Limits for Indoor Spaces – Road and Rail of the ENCG. The maximum suggested sound levels for outdoor and indoor living areas between 7am and

11pm are 55 dBA and 45 dBA, respectively. The maximum suggested sound level for indoor bedrooms is 40dBA between 11pm and 7am. For reference, Tables 2.2a, 2.2b and 2.2c of the ENCG are included in **Appendix A**.

Outdoor Living Area and Plane of Window receivers are defined as:

- **Outdoor Living Area (OLA):** The outdoor amenity area provided for quiet enjoyment of the outdoor environment during the daytime period (i.e., backyards, terraces and patios). OLA noise levels are considered 3.0m from the building façade (where applicable), 1.5m above grade.
- **Plane of Window (POW):** The indoor living space where the sound levels will affect the living room area during daytime hours and bedrooms during nighttime hours. Typically, POW noise levels are considered inside the building, 1.5m above the ground for the daytime and 4.5m above the ground for nighttime.

3.2 Alternative Methods for Noise Attenuation

When OLA sound levels are predicted to be approximately equal to or less than 55 dBA attenuation measures are not required. If the predicted noise levels are found to exceed 55 dBA, physical forms of mitigation are suggested and which may also include the provision of warning clauses to inform purchasers of the expected noise levels and specific mitigation measures.

These attenuation measures may include any or all of the following:

- Distance setback with soft ground;
- Insertion of noise insensitive land uses between the source and sensitive receptor;
- Orientation of building to provide sheltered zones;
- Construction of sound or acoustic barriers;
- Installation of air conditioning and ventilation; and
- Enhanced construction techniques and improved construction quality.

3.3 Noise Attenuation Requirements

When the noise attenuation measures listed above do not reduce noise levels below 55 dBA in the Outdoor Living Area, control measures (barriers) are required to reduce the Leq below or as close to 55 dBA as technically, economically and administratively feasible.

The noise barriers are to be compliant with the City standard for noise barriers and have the following characteristics:

- Minimum height of 2.2m; Maximum height of 2.5m, unless approved by the City;
- Situated 0.30m inside the private property line;
- A surface mass density not less than 20kg/sq.m; and
- No holes or gaps.

3.4 Ventilation Requirements

A forced air heating system with provision for a central air conditioning system is required if the plane of window daytime noise levels are between 55 dBA and 65 dBA and/or the nighttime noise levels are between 50 dBA and 60 dBA.

The installation of a central air conditioning system is required when the daytime noise level exceeds 65 dBA and/or the nighttime noise level exceeds 60 dBA.

3.5 Building Component Assessment

When plane of window noise levels exceeds 65 dBA (daytime) or 60 dBA (nighttime) the exterior cladding system of the building envelope must be acoustically assessed to ensure indoor sound criteria are achieved. This includes analysis of the exterior wall, door, and/or glazing system specifications as appropriate.

The NRC research *Acoustic Insulation Factor: A Rating for the Insulation of Buildings against Noise* (June 1980, JD Quirt) is used to assess the building components and the required acoustic insulation factor (AIF). This method is recognized by the City of Ottawa.

The required AIF is based on the Outside L_{eq} , Indoor L_{eq} required, and the number of exterior façade components.

Minimum Required AIF = Outside L_{eq} – Indoor L_{eq} + $10 \log_{10}$ (Number of Components) + 2dB

Where, N = Number of components (walls, windows and roof);

L = Sound Level expressed on a common decibel scale.

3.6 Warning Clauses

When predicted noise levels exceed the specified criteria, the City of Ottawa and the MOE recommend warning clauses be registered as a notice on title and incorporated into the lease/rental/sale agreements to warn potential purchaser/buyers/tenants of the possible elevated noise levels.

Typical warning clauses should be registered as shown below. Warning clauses are extracted from Part 4, Appendix A the City of Ottawa ENCG and excerpts have been provided in **Appendix A** of this report. As stated in the City of Ottawa ENCG, due to the variation of noise impacts for any given site, it may be necessary to amend the example warning clauses to recognize the site conditions in each development.

It is recommended that the following noise clauses be registered on title and incorporated into the agreement of purchase and sales as required. Results can be found in **Table 5** from Section 4.3 of this report:

Type A

“Purchasers/tenants are advised that sound levels due to increasing road traffic may occasionally interfere with some outdoor activities as the sound levels may exceed the sound level limits of the City and Ministry of the Environment.”

“To help address the need for sound attenuation this development has been designed so as to provide an outdoor amenity area and indoor environment that is within provincial guidelines. Measures for sound attenuation include:

- An acoustic barrier”

“To ensure that provincial sound level limits are not exceeded it is important to maintain sound attenuation features.”

“The acoustic barrier shall be maintained and kept in good repair by the property owner. Any maintenance, repair or replacement is the responsibility of the owner and shall be with the same material or to the same standards, having the same colour, appearance and function of the original.”

Additionally, if a tolerance of 5 dBA is being considered in some areas, it is recommended an additional noise clause be registered on title and incorporated into the agreement of purchase and sales:

Type B

“Purchasers/tenants are advised that despite the inclusion of noise control features in the development and within the building units, sound levels due to increasing road/rail/Light Rail/transitway traffic may, on occasion, interfere with some activities of the dwelling occupants as the sound levels exceed the sound level limits of the City and the Ministry of the Environment by up to 5 dBA.”

“To help address the need for sound attenuation this development has been designed so as to provide an outdoor amenity area and indoor environment that is within provincial guidelines. Measures for sound attenuation include:

- An acoustic barrier”

“To ensure that provincial sound level limits are not exceeded it is important to maintain sound attenuation features.”

“The acoustic barrier shall be maintained and kept in good repair by the property owner. Any maintenance, repair or replacement is the responsibility of the owner and shall be with the same material or to the same standards, having the same colour, appearance and function of the original.”

Type C

“Purchasers/tenants are advised that sound levels due to increasing road traffic may occasionally interfere with some outdoor activities as the sound levels may exceed the sound level limits of the City and Ministry of the Environment.”

“To help address the need for sound attenuation this development has been designed so as to provide an outdoor amenity area and indoor environment that is within provincial guidelines. Measures for sound attenuation may include:

- Multi-pane glass
- Double brick veneer”

“To ensure that provincial sound level limits are not exceeded it is important to maintain sound attenuation features.”

“This dwelling unit has also been designed with the provision for adding central air conditioning at the occupant’s discretion. Installation of central air conditioning will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the sound level limits of the City and the Ministry of the Environment”

Type D

“Purchasers/tenants are advised that sound levels due to increasing road traffic may occasionally interfere with some outdoor activities as the sound levels may exceed the sound level limits of the City and Ministry of the Environment.”

“To help address the need for sound attenuation this development has been designed so as to provide an outdoor amenity area and indoor environment that is within provincial guidelines. Measures for sound attenuation may include:

- Multi-pane glass
- Double brick veneer
- High sound transmission class walls”

“To ensure that provincial sound level limits are not exceeded it is important to maintain sound attenuation features.”

“This dwelling unit has also been supplied with a central air conditioning system and other measures which will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the sound level limits of the City and the Ministry of the Environment”

For units with multiple types of warning clauses, similar/identical wording can be combined as to not duplicate wording/information.

3.7 Summary of Noise Attenuation Requirements

Table 1 summarizes the required noise attenuation measures and warning clauses should sound criteria be exceeded. Excerpts from the MOE NPC-300 and City of Ottawa ENCG documents are included in **Appendix A** for reference.

Table 1: Noise Attenuation Measure Requirements

Assessment Location	L _{eq} (dBA)	Outdoor Control Measures	Indoor Control Measures		Warning Clause
			Ventilation Requirements	Building Components	
Outdoor Living Area (OLA)	Less than 55	None required	N/A	N/A	None required
	Between 55 and 60	Control measures (barriers) may not be required but should be considered	N/A	N/A	Required if resultant L _{eq} exceeds 55 dBA Type A* or Type B**
	More than 60	Barriers required	N/A	N/A	Required if resultant L _{eq} exceeds 55 dBA Type A* or Type B*
Plane of Living Room Window (POW)	Less than 55	N/A	None Required	None Required	None Required
	Between 55 and 65	N/A	Forced air heating with provision for central air conditioning	None Required	Required Type C
	More Than 65	N/A	Central Air Conditioning	Acoustical performance of the windows and walls should be specified	Required Type D
Plane of Bedroom Window (POW)	Less than 50	N/A	None Required	None Required	None Required
	Between 50 and 60	N/A	Forced air heating with provision for central air conditioning	None Required	Required Type C
	More than 60	N/A	Central Air Conditioning	Acoustical performance of the windows and walls should be specified	Required Type D

*Type A warning clause refers to units requiring a noise barrier that mitigates noise below 55dBA.

**Type B warning clause refers to units requiring a noise barrier, but is technically or economically not feasible to reduce levels below 55dBA and a tolerance of up to 5dBA can be granted by the City.

4.0 PREDICTION OF OUTDOOR NOISE LEVELS

4.1 Roadway Traffic

Noise levels from Terry Fox Drive, Fernbank Road, and Cope Drive were assessed using the ultimate road (as per the 2031 Network Concept Plan in the TMP) and traffic parameters below from "Appendix B of the City of Ottawa's Environmental Noise Control Guidelines, 2016". The posted speed for Terry Fox Drive, Fernbank Road and Cope Drive are consistent with the current conditions. The traffic and roadway parameters used for sound level predictions are shown in Table 2.

Table 2: Traffic and Roadway Parameters

Description	Terry Fox Drive	Fernbank Road	Cope Drive
Roadway Classification	4-Lane Urban Arterial Divided	2-Lane Urban Arterial Undivided	2-Lane Urban Collector
Annual Average Daily Traffic (AADT)	35,000 vehicles/day	15,000 vehicles/day	8,000 vehicles/day
Day/Night Split (%)	92/8	92/8	92/8
Medium Trucks (%)	7	7	7
Heavy Trucks (%)	5	5	5
Posted Speed	80 km/hr	60 km/hr	50 km/hr

For reference, excerpts from the ENCG confirming the Terry Fox Drive, Fernbank Road and Cope Drive AADT are included in **Appendix A**.

4.2 Noise Level Analysis

The noise levels were analyzed using Version 5.03 of the STAMSON computer program issued by the MOE. Proposed grades were required for the software and were obtained from elevations on the Grading Plans (121011-GR1-2), which have been included in **Appendix E** of this report.

For the purposes of this report, the townhouse blocks within the development were used as a barrier in the noise calculations have an assumed height of 9.1m. Refer to **Appendix D** for architectural elevations and drawings.

For the purposes of this report the Plane of Window calculations for the townhouse units have been taken at 1.5m and 4.5m above the finished floor elevation of the first-floor. The 1.5m height represents the first floor. The 4.5m height represents the second floor. Below ground level units were best case scenario in comparison to the other levels as they are partially below grade and were not analyzed as part of this report. It was also determined through several receiver points that the top floor was the worst-case scenario for each unit

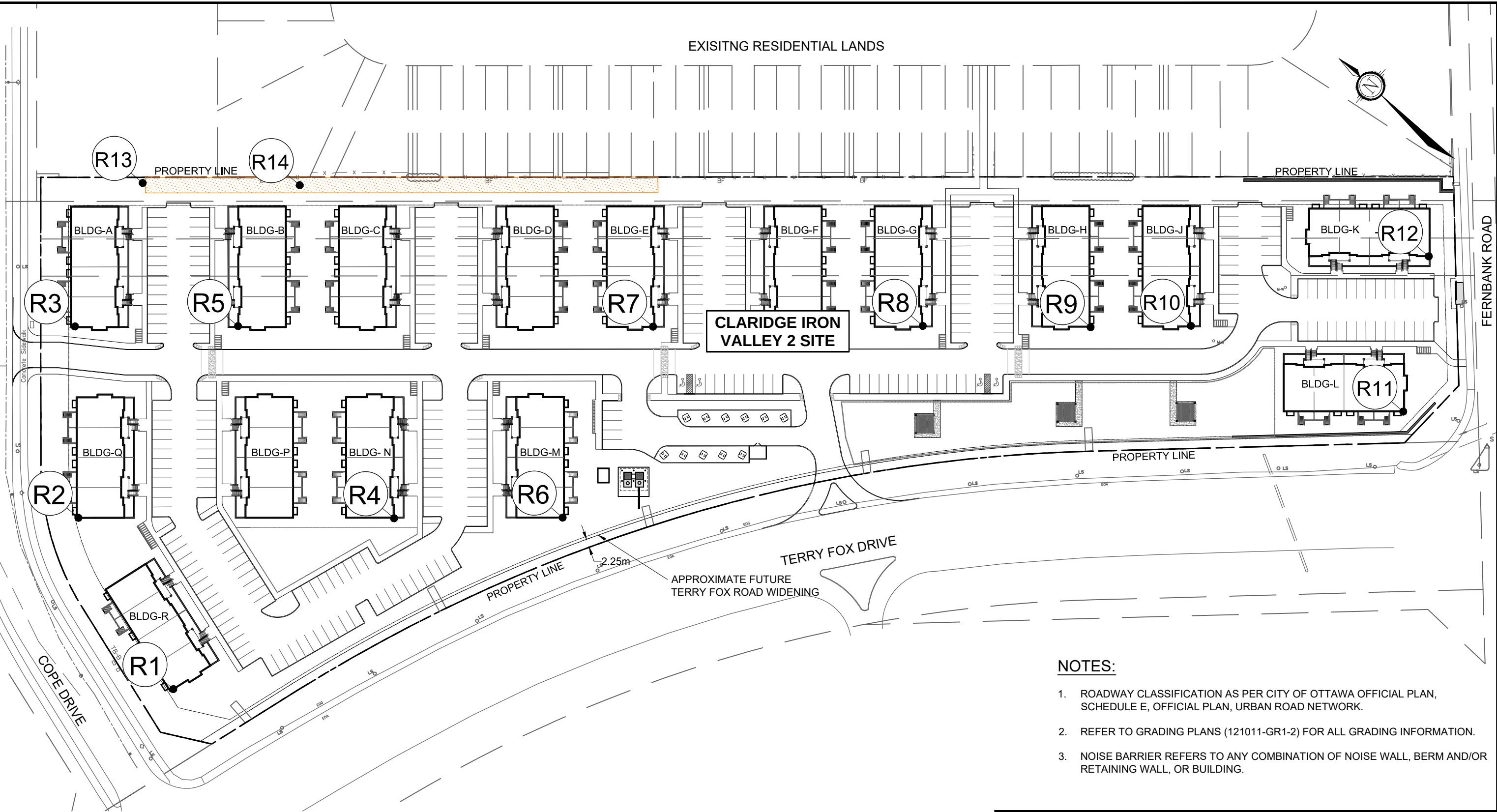
Receiver locations used in the noise simulations are shown on **Figure 3 – Receiver Location Plan**.

Table 3 confirms the units represented by each receiver's node.

Table 3: Nodes and the Units They Represent

Node	Unit	Node	Unit	Node	Unit
R1	R	R5	B, C	R9	H
R2	Q	R6	M	R10	J
R3	A	R7	D, E	R11	L
R4	P, N	R8	F, G	R12	K

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LEGEND

- PROPERTY LINE
- RECEIVER LOCATION
- AMENITY SPACE

- NOTES:
- ROADWAY CLASSIFICATION AS PER CITY OF OTTAWA OFFICIAL PLAN, SCHEDULE E, OFFICIAL PLAN, URBAN ROAD NETWORK.
 - REFER TO GRADING PLANS (121011-GR1-2) FOR ALL GRADING INFORMATION.
 - NOISE BARRIER REFERS TO ANY COMBINATION OF NOISE WALL, BERM AND/OR RETAINING WALL, OR BUILDING.

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CITY OF OTTAWA
5331 FERNBANK ROAD
IRON VALLEY 2

RECEIVER LOCATION PLAN

1 : 1000

NOV 2025 121011 FIGURE 3

4.3 Noise Level Results

Simulated noise levels confirm Node 5 is within the permitted noise levels, Nodes 2, 3, and 7 exceed the minimum permitted noise levels but remain within the maximum permitted noise levels, and Nodes 1, 4, 6, and 8-12 exceed the maximum permitted noise levels. No action is required for units represented by Node 5: B and C. Forced Air with provisions for air condition and warning clause “C” is required for units represented by Nodes 2, 3, and 7: A, D, E, and Q. Air conditioning, building component analysis, and warning clause “D” is required for all remaining units: F, G, H, J, K, L, N, P, and R.

Outdoor amenity space was identified as the open space area between the existing subdivision (SOHO) to the east and units A, B, and C. This area fulfills the communal outdoor amenity area requirement. R13 represents a node closest to Cope Drive while R14 represent the average (middle) of the amenity space.

The predicted outdoor noise levels at the selected receiver locations within the development are illustrated in **Table 4**.

Table 4: Simulation Results – Outdoor Living Areas

Receiver Location*	File	Un-attenuated Calculated Noise Level (dBA) 7:00-23:00	Outdoor Mitigation Method
R13	1r13	52.68	N/A
R14	1r14	47.68	N/A

*Locations correspond to receivers found on Figure 3 – Receiver Location Plan

Figures in **Appendix B** show angles used in the detailed modeling calculations. The noise levels for all receiver locations generated from STAMSON are listed in **Table 3** with detailed modeling results in **Appendix B**.

The predicted daytime and nighttime noise levels and required mitigation for the Plane of Window are shown in **Table 5**.

Table 5: Simulation Results – Plane of Window

Receiver Location	File	Unit	Un-attenuated Calculated Noise Level (dBA)		Mitigation Method
			7:00-23:00	23:00-7:00	
R1	1-R1	R	68.97	61.37	• Installation of Air Condition • Warning clause Type D • Building Façade Analysis
	2-R1		69.39	61.79	
R2	1-R2	Q	63.35	55.76	• Forced Air with provisions for AC • Warning clause Type C
	2-R2		63.93	56.34	
R3	1-R3	A	61.34	53.75	• Forced Air with provisions for AC • Warning clause Type C
	2-R3		61.65	54.06	

R4	1-R4	P, N	66.08	58.49	• Installation of Air Condition • Warning clause Type D • Building Façade Analysis
	2-R4		66.62	59.02	
R5	1-R5	B, C	51.71	44.11	• No Action Required
	2-R5		52.52	44.92	
R6	1-R6	M	69.92	62.33	• Installation of Air Condition • Warning clause Type D • Building Façade Analysis
	2-R6		70.27	62.68	
R7	1-R7	D, E	62.49	54.89	• Forced Air with provisions for AC • Warning clause Type C
	2-R7		63.22	55.62	
R8	1-R8	F, G	64.67	57.07	• Installation of Air Condition • Warning clause Type D • Building Façade Analysis
	2-R8		65.27	57.67	
R9	1-R9	H	65.11	57.52	• Installation of Air Condition • Warning clause Type D • Building Façade Analysis
	2-R9		65.74	58.14	
R10	1-R10	J	65.69	58.10	• Installation of Air Condition • Warning clause Type D • Building Façade Analysis
	2-R10		66.21	58.62	
R11	1-R11	L	71.26	63.67	• Installation of Air Condition • Warning clause Type D • Building Façade Analysis
	2-R11		71.60	64.00	
R12	1-R12	K	66.74	58.14	• Installation of Air Condition • Warning clause Type D • Building Façade Analysis
	2-R12		67.19	59.59	

Figures in **Appendix B** show angles used in the detailed modeling calculations. The noise levels for all receiver locations generated from STAMSON are listed in **Table 4 and 5** with detailed modeling results in **Appendix B**.

4.4 Implementation

The City of Ottawa ENCG requires that noise clauses be applied when noise levels are above minimum requirements outlined in **Table 1**; and, wall & window construction be reviewed when noise levels exceed the maximum requirements outlined in **Table 1**. The acoustical insulation factor (AIF) method recognized by the City of Ottawa is used to assess the wall and window requirements.

The Acoustic Insulation Factor (AIF) is used as a measure of the reduction of outdoor noise provided by the elements of the outer surface of a building. The difference between the indoor noise criterion and the outdoor noise level establishes the acoustical insulation requirement for the exterior shell. The exterior shell is comprised of primarily two components; windows and walls (patio doors are treated as windows). Canada Mortgage

and Housing (CMHC) Standards ¹ require that no component should transmit more than 1/N of the total sound power that would give the maximum acceptable noise level inside the room. Therefore, in a room with two exterior components, neither should transmit more than one-half of the total allowable sound power.

Mathematically, this Acoustical Insulation Factor can be expressed as:

$$\text{Required AIF} = L_{\text{eq}} (\text{Outside}) - L_{\text{eq}} (\text{Inside}) + 10 \log_{10} (N) + 2\text{dBA}$$

Where, N = Number of components;

L = Sound Level expressed on a common decibel scale.

Since noise levels and unit types vary over the site, acoustical insulation factors have been separated depending on exposure to different noise sources.

The largest acoustical insulation factors for the unit in closest proximity to Fernbank Road and Terry Fox Drive (R11) are calculated as follows:

- $\text{AIF}_{\text{Residential(day)}} = 72 \text{ dBA} - 45 \text{ dBA} + 10\log(2) \text{ dBA} + 2\text{dBA} = 32 \text{ dBA}$
- $\text{AIF}_{\text{Residential(night)}} = 64 \text{ dBA} - 40 \text{ dBA} + 10\log(2) \text{ dBA} + 2\text{dBA} = 29 \text{ dBA}$

Other AIF values calculated using the same method above are presented in **Table 6**:

Table 6: AIF Results

Receiver	AIF (dBA)	
	7:00-23:00	23:00-7:00
R1	29	27
R2	24	21
R3	22	19
R4	27	24
R5	13	10
R6	30	28
R7	23	21
R8	25	23
R9	26	23
R10	26	34
R11	32	29
R12	27	25

Refer to **Table 3** to confirm the units represented by the receivers.

Tables from the document entitled “Acoustic Insulation Factor: A Rating for the Insulation of Buildings Against Outdoor Noise”, produced by the Division of Building Research, National Research Council of Canada, June 1980 (J.D. Quirt) were used to assess the exterior facade against the required AIF. This reference material is included in **Appendix C**.

¹ Road and Rail Noise: Effects on Housing, CMHC, Ottawa. Publication NHA #185 1/78, 1978

In order to assess the façade against the required AIF respective Leq values, the number of components in a wall, the calculated required AIF, percentage of window to room areas and exterior wall to room areas are required. Exterior facade analysis data is presented in **Table 7**.

Table 7: Exterior Façade Analysis Data

Description				Percentage	
Floor	Unit	Room	No. of Components	Window to Floor Area	Percentage of Ext. Wall to Floor
1	1	Primary Bedroom	2	38	133
		Bedroom 2	2	16	172*
		Living Room	2	45	30
1	2/3	Primary Bedroom	2	37*	36*
		Bedroom 2	2	17	86
		Living Room	2	46	29
1	4	Primary Bedroom	2	42	124
		Bedroom 2	2	17	178
		Living Room	2	46	29
2	1	Primary Bedroom	2	37	132
		Bedroom 2	2	15	169
		Living Room	2	45	30
2	2/3	Primary Bedroom	2	36	38
		Bedroom 2	2	15	77
		Living Room	2	46	29
2	4	Primary Bedroom	2	43	123
		Bedroom 2	2	16	171
		Living Room	2	44	31

*Denotes an average

Components (2) include windows and exterior walls

Unit location Left side to right side 1, 2, 3, 4

Architect unit floor plans were reviewed to calculate the window and wall to floor ratios (as seen above). The architect plans are included in **Appendix D**.

Using the percentage of window area to room area, and the required acoustical insulation factor (AIF), **Table 5** in **Appendix C** was used to identify the various window assemblies that would satisfy the calculated AIF. The builder confirmed their minimum window STC rating is 31. All units requiring a window STC of 31 or below are grouped together. Units L and M were isolated because of their enhanced noise mitigation requirement.

Similarly, **Table 6.3** in **Appendix C** was used to select the typical wall assembly that would satisfy the required AIF. The worst case was used to complete the façade analysis for the whole unit. The only exception is Unit L. Unit L has an enhanced wall (EW3) compared to all other units (EW2).

The minimum required noise mitigation measures are listed in **Table 8**.

Table 8: Window and Wall Assemblies Required for Attenuation

Unit	Min. Required Window Rating		Min. Required Wall Rating		Recommended Wall Rating
	AIF	STC	AIF	STC	
A	22	24	22	29	EW2
B and C	13	15	13	22	EW2
D and E	23	25	23	32	EW2
F and G	25	27	25	34	EW2
H	26	28	26	35	EW2
J	26	28	26	35	EW2
K	27	29	27	36	EW2
L	32	34	32	41	EW3
M	30	32	30	39	EW2
N and P	27	29	27	36	EW2
Q	24	26	24	33	EW2
R	29	31	29	38	EW2

* Tables 11 and 12 in **Appendix C** were used to convert the AIF values to Sound Transmission Class or STC values.

Table 4 in **Appendix C** was considered to redistribute AIF requirements between the walls and windows for Units L and M. Unfortunately due to the window and wall to floor ratios of the units, redistribution it is not possible. All other unit's window and wall assembly STC requirements were low enough that redistribution is not needed. Redistribution is not considered in this report.

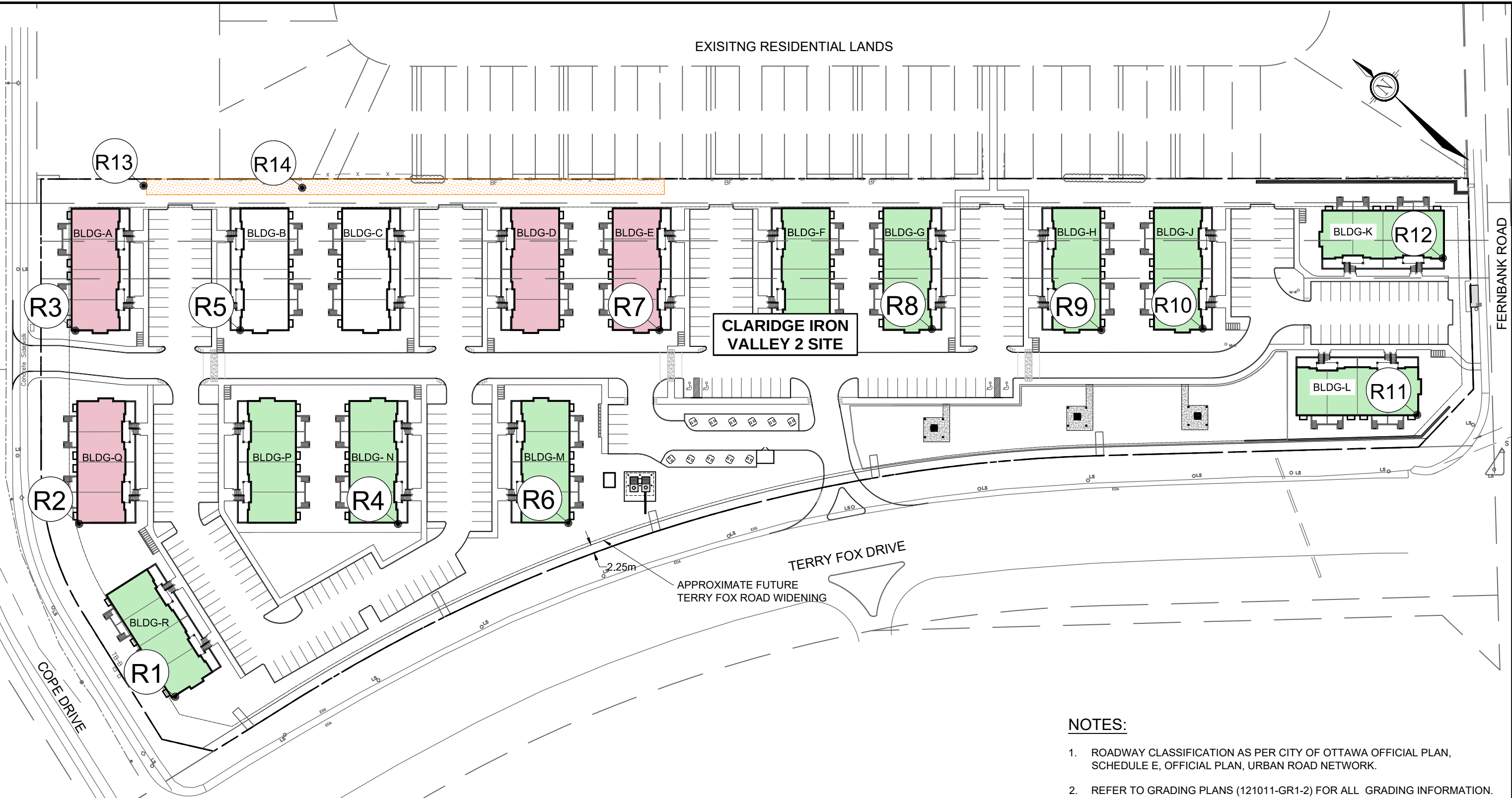
The attenuation measures required to satisfy the City of Ottawa noise criteria and the noise clauses that are to be included on title and in the Agreement of Purchase and Sale for the various dwelling units are summarized in **Table 9**.

Table 9 – Required Attenuation Measures and Associated Warning Clauses

Unit	Attenuation Measure	Notice on Title
B and C	• N/A	• N/A
A, D, E, and Q	• Forced air with provisions for AC	• Type C
F, G, H, J, K, L, M, N, P, R	• Installation of air conditioning • Building Façade Analysis	• Type D

Refer to **Figure 4 – Noise Attenuation Measures Plan** for building unit identification, node locations, and details of mitigation measures.

M:\2021\121011\CAD\Design\Figures\Noise\121011-Fig4-Noise Attenuation.dwg, FIG4, Nov 10, 2025 - 10:15am, mabdu



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CITY OF OTTAWA
5331 FERNBANK ROAD
IRON VALLEY 2

NOISE ATTENUATION
MEASURES PLAN

1 : 1000

NOV 2025 121011 FIGURE 4

SHT11X17.DWG - 279mmX432mm

5.0 CONCLUSIONS

An analysis of the roadway traffic along Terry Fox Drive, Fernbank Road, and Cope Drive indicates indoor noise attenuation measures is necessary for the Iron Valley 2 development. However, no outdoor noise attenuation is required.

The following is a summary of the attenuation measures and notice requirements to be placed on title. Refer to **Figure 2** for unit locations.

Units B and C

- No action required.

Units A, D, E, and Q

- Forced air ventilation with provisions for central air conditioning,
- Type D Warning Clause (refer to Section 3.6),
- Provide window assembly to meet a sound transmission class, STC of 31, and
- Provide EW2 wall assembly (minimum).

Units F, G, H, J, K, L, M, N, P, R

- Provide central air conditioning,
- Type D Warning Clause (refer to Section 3.6),
- Provide window assembly to meet a sound transmission class, STC of 31, and
- Provide EW2 wall assembly (minimum).

Units M

- Provide central air conditioning,
- Type D Warning Clause (refer to Section 3.6),
- Provide window assembly to meet a sound transmission class, STC of 32, and
- Provide EW2 wall assembly (minimum).

Units L

- Provide central air conditioning,
- Type D Warning Clause (refer to Section 3.6),
- Provide window assembly to meet a sound transmission class, STC of 34, and
- Provide EW3 wall assembly (minimum).

In closing, Novatech respectfully requests the City of Ottawa accept the findings of this Detailed Noise Control Study for the Iron Valley 2 residential development at 5331 Fernbank Road as part of the Site Plan application.

NOVATECH

Authorized by:



Mark Bowen, B. Eng.
Project Manager| Land Development

Reviewed by:



Drew Blair, P.Eng.
Senior Project Manager| Land Development



APPENDIX A

EXCERPTS FROM THE CITY OF OTTAWA ENVIRONMENTAL NOISE CONTROL GUIDELINES, THE MOE'S NPC-300, THE CITY OF OTTAWA'S TRANSPORTATION MASTER PLAN AND OFFICIAL PLAN

ENVIRONMENTAL NOISE CONTROL GUIDELINES: Introduction and Glossary

January 2016

Table 2.2a: Sound Level Limit for Outdoor Living Areas - Road and Rail
 (from NPC-300, 2013 Table C-1)

Time Period	Required Leq (16) (dBA)
16-hour, 07:00 – 23:00	55

Table 2.2b: Sound Level Limit for Indoor Living Areas Road and Rail
 (from NPC-300, 2013 Table C-2)

Type of Space	Time Period	Required Leq (dBA)	
		Road	Rail
Living/dining, den areas of residences, hospitals, nursing homes, schools, daycare centres, etc.	07:00 – 23:00	45	40
Living/dining, den areas of residences, hospitals, nursing homes, etc. (except schools or daycare centres)	23:00 – 07:00	45	40
Sleeping quarters	07:00 – 23:00	45	40
	23:00 – 07:00	40	35

The Province also provides for supplementary indoor sound level limits for land uses not generally considered noise sensitive (see Table 2.2c below). These good practice design objectives should be addressed in any noise study prepared for the City. These supplementary sound level limits are based on the windows and doors to an indoor space being closed.

Table 2.2c: Supplementary Sound Level Limits for Indoor Spaces - Road and Rail (adapted from NPC-300 Table C-9)

Type of Space	Time Period	Required Leq (dBA)	
		Road	Rail
General offices, reception areas, retail stores, etc.	16 hours between 07:00 – 23:00	50	45
Theatres, places of worship, libraries, individual or semi-private offices, conference rooms, reading rooms, etc.	16 hours between 07:00 – 23:00	45	40
Sleeping quarters of hotels/motels	8 hours between 23:00 – 07:00	45	40
Sleeping quarters of residences, hospitals, nursing/retirement homes, etc.	8 hours between 23:00 – 07:00	40	35

Appendix B: Table of Traffic and Road Parameters To Be Used For Sound Level Predictions

Table B1 Traffic And Road Parameters To Be Used For Sound Level Predictions

Row Width (m)	Implied Roadway Class	AADT Vehicles/Day	Posted Speed Km/Hr	Day/Night Split %	Medium Trucks %	Heavy Trucks % ¹
NA ²	Freeway, Queensway, Highway	18,333 per lane	100	92/8	7	5
37.5-44.5	6-Lane Urban Arterial-Divided (6-UAD)	50,000	50-80	92/8	7	5
34-37.5	4-Lane Urban Arterial-Divided (4-UAD)	35,000	50-80	92/8	7	5
23-34	4-Lane Urban Arterial-Undivided (4-UAU)	30,000	50-80	92/8	7	5
23-34	4-Lane Major Collector (4-UMCU)	24,000	40-60	92/8	7	5
30-35.5	2-Lane Rural Arterial (2-RAU)	15,000	50-80	92/8	7	5
20-30	2-Lane Urban Arterial (2-UAU)	15,000	50-80	92/8	7	5
20-30	2-Lane Major Collector (2-UMCU)	12,000	40-60	92/8	7	5
30-35.5	2-Lane Outer Rural Arterial (near the extremities of the City) (2-RAU)	10,000	50-80	92/8	7	5
20-30	2-Lane Urban Collector (2-UCU)	8,000	40-50	92/8	7	5

¹ The MOE Vehicle Classification definitions should be used to estimate automobiles, medium trucks and heavy trucks.

² The number of lanes is determined by the future mature state of the roadway.

Environmental Noise Guideline

Stationary and Transportation Sources –
Approval and Planning

Publication NPC-300

Table C-10
Supplementary Indoor Aircraft Noise Limits
(Applicable over 24-hour period)

Type of Space	Indoor NEF/NEP*
General offices, reception areas, retail stores, etc.	15
Individual or semi-private offices, conference rooms, etc.	10
Living/dining areas of residences, sleeping quarters of hotels/motels, theatres, libraries, schools, daycare centres, places of worship, etc.	5
Sleeping quarters of residences, hospitals, nursing/retirement homes, etc.	0

* The indoor NEF/NEP values listed in Table C-10 are not obtained from NEF/NEP contour maps. The values are representative of the indoor sound levels and are used as assessment criteria for the evaluation of acoustical insulation requirements.

C7 Noise Control Measures

The following sections provide MOE guidance for appropriate noise control measures. These sections constitute requirements that are applied to MOE approvals for stationary sources. This information is also provided as guidance which land use planning authorities may consider adopting.

The definition in Part A describes the various types and application of noise control measures. All the noise control measures described in the definition are appropriate to address the impact of noise of transportation sources (road, rail and aircraft) on planned sensitive land uses. Only some of the noise control measures described in the definition are appropriate to address the noise impact of stationary sources on planned sensitive land uses.

C7.1 Road Noise Control Measures

C7.1.1 Outdoor Living Areas

If the 16-Hour Equivalent Sound Level, $L_{eq}(16)$ in the OLA is greater than 55 dBA and less than or equal to 60 dBA, noise control measures may be applied to reduce the sound level to 55 dBA. If measures are not provided, prospective purchasers or tenants should be informed of potential noise problems by a warning clause Type A.

If the 16-Hour Equivalent Sound Level, $L_{eq}(16)$ in the OLA is greater than 60 dBA, noise control measures should be implemented to reduce the level to 55 dBA. Only in cases where the required noise control measures are not feasible for technical, economic or administrative reasons would an excess above the limit (55 dBA) be acceptable with a warning clause Type B. In the above situations, any excess above the limit will not be acceptable if it exceeds 5 dBA.

C7.1.2 Plane of a Window – Ventilation Requirements

C7.1.2.1 Daytime Period, 07:00 – 23:00 Hours

Noise control measures may not be required if the L_{eq} (16) daytime sound level in the plane of a bedroom or living/dining room window is less than or equal to 55 dBA. If the sound level in the plane of a bedroom or living/dining room window is greater than 55 dBA and less than or equal to 65 dBA, the dwelling should be designed with a provision for the installation of central air conditioning in the future, at the occupant's discretion. Warning clause Type C is also recommended.

If the daytime sound level in the plane of a bedroom or living/dining room window is greater than 65 dBA, installation of central air conditioning should be implemented with a warning clause Type D. In addition, building components including windows, walls and doors, where applicable, should be designed so that the indoor sound levels comply with the sound level limits in Table C-2. The location and installation of the outdoor air conditioning device should comply with sound level limits of Publication NPC-216, Reference [32], and guidelines contained in Environmental Noise Guidelines for Installation of Residential Air Conditioning Devices, Reference [6], or should comply with other criteria specified by the municipality.

C7.1.2.2 Nighttime Period, 23:00 – 07:00 Hours

Noise control measures may not be required if the L_{eq} (8) nighttime sound level in the plane of a bedroom or living/dining room window is less than or equal to 50 dBA. If the sound level in the plane of a bedroom or living/dining room window is greater than 50 dBA and less than or equal to 60 dBA, the dwelling should be designed with a provision for the installation of central air conditioning in the future, at the occupant's discretion. Warning clause Type C is also recommended.

If the nighttime sound level in the plane of a bedroom or living/dining room window is greater than 60 dBA, installation of central air conditioning should be implemented, with a warning clause Type D. In addition, building components including windows, walls and doors, where applicable, should be designed so that the indoor sound levels comply with the sound level limits in Table C-2. The location and installation of the outdoor air conditioning device should comply with sound level limits of Publication NPC-216, Reference [32], and guidelines contained in Environmental Noise Guidelines for Installation of Residential Air Conditioning Devices, Reference [6], or should comply with other criteria specified by the municipality.

C7.1.3 Indoor Living Areas – Building Components

If the nighttime sound level outside the bedroom or living/dining room windows exceeds 60 dBA or the daytime sound level outside the bedroom or living/dining area windows exceeds 65 dBA, building components including windows, walls and doors, where applicable, should be designed so that the indoor sound levels comply with the

sound level limits in Table C-2. The acoustical performance of the building components (windows, doors and walls) should be specified.

C7.2 Rail Noise Control Measures

C7.2.1 Outdoor Living Areas

Whistle noise is not included in the determination of the outdoor daytime sound level due to railway trains. All the provisions of Section C7.1.1 apply also to noise control requirements for rail noise.

C7.2.2 Plane of a Window – Ventilation Requirements

Whistle noise is not included in the determination of the sound level in the plane of a window. All the provisions of Section C7.1.2 apply also to noise control requirements for rail noise.

C7.2.3 Indoor Living Areas – Building Components

The sound level, L_{eq} , during the daytime (16-hour) and nighttime (8-hour) periods is determined using the prediction method STEAM, Reference [34], immediately outside the dwelling envelope. Whistle noise is included in the determination of the sound level.

If the nighttime sound level outside the bedroom or living/dining room windows exceeds 55 dBA or the daytime sound level outside the bedroom or living/dining area windows exceeds 60 dBA, building components including windows, walls and doors, where applicable, need to be designed so that the indoor sound levels comply with the sound level limits in Table C-2. The acoustical performance of the building components (windows, doors and walls) needs to be specified.

In addition, the exterior walls of the first row of dwellings next to railway tracks are to be built to a minimum of brick veneer or masonry equivalent construction, from the foundation to the rafters when the rail traffic L_{eq} (24-hour), estimated at a location of a nighttime receptor, is greater than 60 dBA, and when the first row of dwellings is within 100 metres of the tracks.

C7.3 Combination of Road and Rail Noise

The noise impact in the OLA and in the plane of a window, and the requirements for outdoor measures, ventilation measures and warning clauses, should be determined by combining road and rail traffic sound levels.

The assessment of the indoor sound levels and the resultant requirement for the acoustical descriptors of the building components should be done separately for road

In Class 4 areas, where windows for noise sensitive spaces are assumed to be closed, the use of central air conditioning may be acceptable if it forms an essential part of the overall building designs.

C7.9 Verification of Noise Control Measures

It is recommended that the implementation of noise control measures be verified by qualified individuals with experience in environmental acoustics.

C8 Warning Clauses

The use of warning clauses or easements in respect of noise are recommended when circumstances warrant. Noise warning clauses may be used to warn of potential annoyance due to an existing source of noise and/or to warn of excesses above the sound level limits. Direction on the use of warning clauses should be included in agreements that are registered on title to the lands in question. The warning clauses would be included in agreements of Offers of Purchase and Sale, lease/rental agreements and condominium declarations. Alternatively, the use of easements in respect of noise may be appropriate in some circumstances. Additional guidance on the use of noise warning clauses is provided in Section C7.1.1, Section C7.1.2.1, Section C7.1.2.2, Section C7.3 and Section C7.4.

C8.1 Transportation Sources

The following warning clauses may be used individually or in combination:

TYPE A: (see Section C7.1.1)

“Purchasers/tenants are advised that sound levels due to increasing road traffic (rail traffic) (air traffic) may occasionally interfere with some activities of the dwelling occupants as the sound levels exceed the sound level limits of the Municipality and the Ministry of the Environment.”

TYPE B: (see Section C7.1.1 and Section C7.4)

“Purchasers/tenants are advised that despite the inclusion of noise control features in the development and within the building units, sound levels due to increasing road traffic (rail traffic) (air traffic) may on occasions interfere with some activities of the dwelling occupants as the sound levels exceed the sound level limits of the Municipality and the Ministry of the Environment.”

TYPE C: (see Section C7.1.2.1, Section C7.1.2.2 and Section C7.4)

“This dwelling unit has been designed with the provision for adding central air conditioning at the occupant’s discretion. Installation of

central air conditioning by the occupant in low and medium density developments will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the sound level limits of the Municipality and the Ministry of the Environment.”

TYPE D: (see Section C7.1.2.1, Section C7.1.2.2 and Section C7.4)

“This dwelling unit has been supplied with a central air conditioning system which will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the sound level limits of the Municipality and the Ministry of the Environment.”

C8.2 Stationary Sources

It is not acceptable to use warning clauses in place of physical noise control measures to identify an excess over the MOE sound level limits. Warning clause (Type E) for stationary sources may identify a potential concern due to the proximity of the facility but it is not acceptable to justify exceeding the sound level limits.

TYPE E: (see Section C7.6)

“Purchasers/tenants are advised that due to the proximity of the adjacent industry (facility) (utility), noise from the industry (facility) (utility) may at times be audible.”

C8.3 Class 4 Area Notification

TYPE F: (see Section B9.2 and Section C4.4.2)

“Purchasers/tenants are advised that sound levels due to the adjacent industry (facility) (utility) are required to comply with sound level limits that are protective of indoor areas and are based on the assumption that windows and exterior doors are closed. This dwelling unit has been supplied with a ventilation/air conditioning system which will allow windows and exterior doors to remain closed.”

Appendix A: Warning Clauses

Under the Official Plan and this guideline warning clauses may be required to be incorporated into development through development agreements, registration on title and inclusion in Agreements of Purchase and Sale. This requirement may be included in any development, regardless of whether it is considered a noise sensitive land use.

A warning clause provides recognition for the City, Province landowner or tenants that noise may be a concern, that noise may be audible at times or even quite loud, and, depending on the type of development, provincial guidelines for noise may be exceeded. Warning clauses also recognize that environmental noise is a potential health hazard that does impact people and neighbourhoods. It is for this reason that, unless a non-noise sensitive land use is established, a warning clause should also include noise mitigation.

A warning clause is not considered a form of noise mitigation. It is not acceptable therefore to use warning clauses in place of physical noise control measures to identify an excess over the MOE or City noise limits. The reason for a warning clause on all development is twofold. Firstly, it is important to note that a land use that although the development may not be considered noise sensitive it may include employees or tenants that are personally sensitive to noise. A warning clause provides protection against complaints to the ministry of Environment should provincial guidelines be exceeded. Secondly, a warning clause on title could obviate the need for a new noise study in the future. In a redevelopment scenario the warning clause would provide recognition of the extent noise conditions.

Given the variation in potential intensity and impact of noise it will often be necessary to amend warning clauses to recognize the site specific conditions in each development. Final wording of any warning clause is to be approved by the City.

The following subsections provide example text to be adapted into warning clauses.

Surface Transportation Warning Clauses

Table A1 Surface Transportation Warning Clauses

Type	Example	Notes
Generic	<i>Purchasers/tenants are advised that sound levels due to increasing road/rail/Light Rail/transitway traffic may occasionally interfere with some outdoor activities as the sound levels may exceed the sound level limits of the City and the Ministry of the Environment.</i> <i>To help address the need for sound attenuation this development has been designed so as to provide an outdoor amenity area that is within provincial guidelines. Measures for sound attenuation include:</i> <i>• A setback of buildings from the noise source and</i> <i>• An acoustic barrier.</i> <i>To ensure that provincial sound level limits are not exceeded it is important to maintain sound attenuation features.</i> <i>The acoustic barrier shall be maintained and kept in good repair by the property owner. Any maintenance, repair or replacement is the responsibility of the owner and shall be with the same material or to the same standards, having the same colour, appearance and function of the original.</i> <i>Additionally this development includes trees and shrubs to screen the source of noise from occupants.</i>	The generic warning clause outlines that MOE sound levels may be exceeded but the indoor environment and outdoor amenity areas are within guidelines. Mitigation measures are described including urban design features. Mention is also made of landscaping to screen the development visually from the source of noise.
Extensive mitigation of indoor and	<i>“Purchasers/tenants are advised that despite the inclusion of noise control features in the development and within the building units,</i>	The warning clause makes reference to MOE sound levels

Table A1 Surface Transportation Warning Clauses

Type	Example	Notes
outdoor amenity area	<i>sound levels due to increasing road/rail/Light Rail/transitway traffic may, on occasion, interfere with some activities of the dwelling occupants as the sound levels exceed the sound level limits of the City and the Ministry of the Environment.</i> <i>To help address the need for sound attenuation this development includes:</i> • <i>multi-pane glass;</i> • <i>double brick veneer;</i> • <i>an earth berm; and</i> • <i>an acoustic barrier.</i> <i>To ensure that provincial sound level limits are not exceeded it is important to maintain these sound attenuation features.</i> <i>The acoustic barrier shall be maintained and kept in good repair by the property owner. Any maintenance, repair or replacement is the responsibility of the owner and shall be with the same material or to the same standards, having the same colour, appearance and function of the original.</i> <i>This dwelling unit has also been designed with the provision for adding central air conditioning at the occupant's discretion. Installation of central air conditioning will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the sound level limits of the City and the Ministry of the Environment.</i>	being exceeded from time to time and that there are sound attenuation features and landscaping within the development that should be maintained. An option for air conditioning is noted as well as landscaping to screen the source of noise.

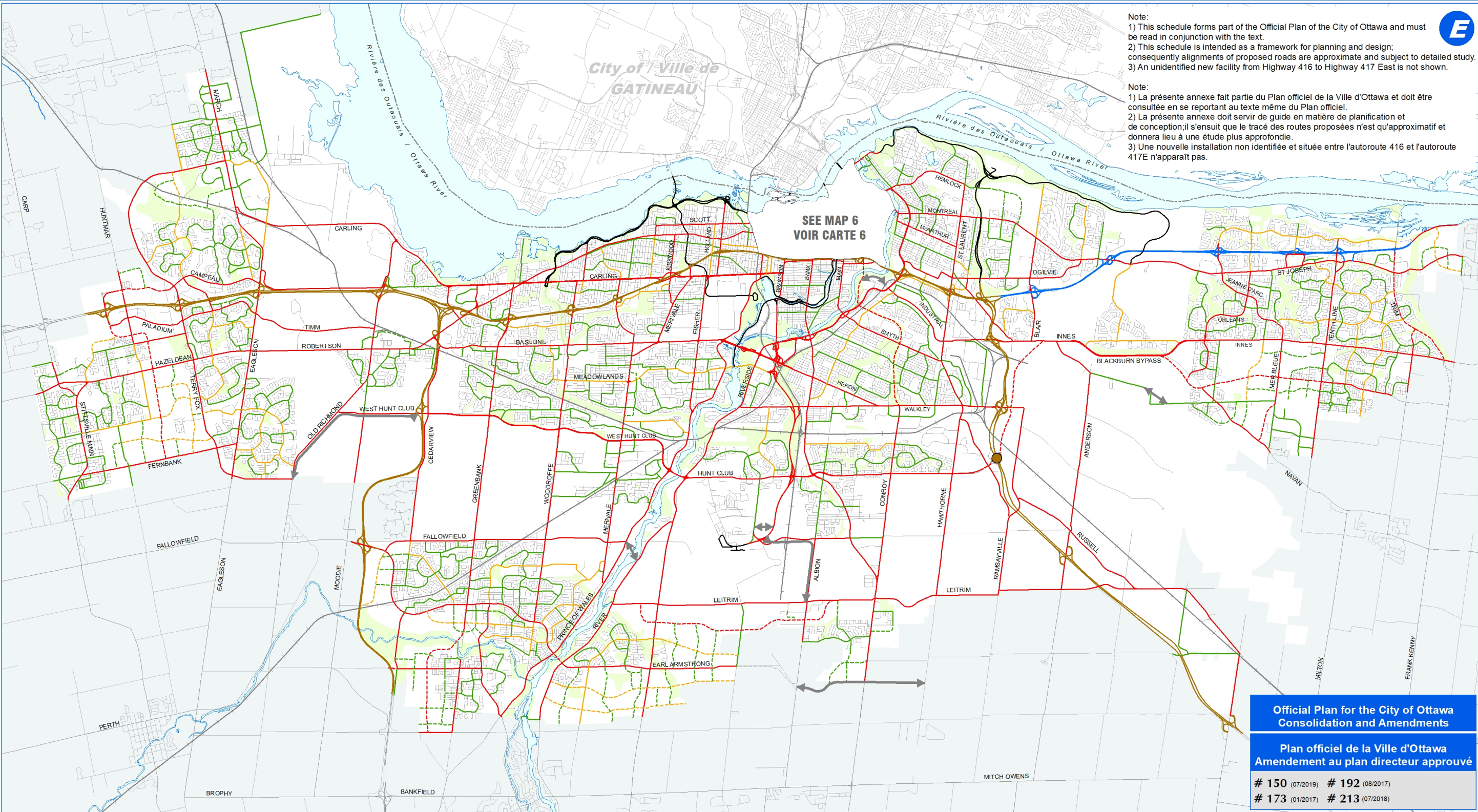
Table A1 Surface Transportation Warning Clauses

Type	Example	Notes
	<i>Additionally this development includes trees and shrubs to screen the source of noise from occupants.</i>	
No outdoor amenity area	<i>Purchasers/tenants are advised that sound levels due to increasing road/rail/Light Rail/transitway traffic will interfere with outdoor activities as the sound levels exceed the sound level limits of the City and the Ministry of the Environment.</i> <i>To help address the need for sound attenuation this development includes:</i> • multi-pane glass; • double brick veneer; • high sound transmission class walls. <i>To ensure that provincial sound level limits are not exceeded it is important to maintain these sound attenuation features.</i> <i>This dwelling unit has been supplied with a central air conditioning system and other measures which will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the sound level limits of the City and the Ministry of the Environment</i>	This warning clause notes that only an indoor environment is being provided for.

Stationary Source Warning Clauses

The Province notes that it is not acceptable to use warning clauses in place of physical noise control measures to identify an excess over the MOE sound level limits for stationary sources. The generic warning clause for stationary sources (called Type E in NPC-300) may identify a potential concern due to the proximity of the facility but it is not possible to justify exceeding the sound level limits.

The wording of the generic stationary noise warning clause may also be used as the basis for new development adjacent to areas licensed for mineral aggregate extraction.



Note:
1) This schedule forms part of the Official Plan of the City of Ottawa and must be read in conjunction with the text.
2) This schedule is intended as a framework for planning and design; consequently alignments of proposed roads are approximate and subject to detailed study.
3) An unidentified new facility from Highway 416 to Highway 417 East is not shown.

Note:
1) La présente annexe fait partie du Plan officiel de la Ville d'Ottawa et doit être consultée en se reportant au texte même du Plan officiel.
2) La présente annexe doit servir de guide en matière de planification et de conception; il s'ensuit que le tracé des routes proposées n'est qu'approximatif et donnera lieu à une étude plus approfondie.
3) Une nouvelle installation non identifiée et située entre l'autoroute 416 et l'autoroute 417E n'apparaît pas.



Official Plan for the City of Ottawa
Consolidation and Amendments

Plan officiel de la Ville d'Ottawa
Amendement au plan directeur approuvé

150 (07/2019) # 192 (08/2017)
173 (01/2017) # 213 (07/2018)

OFFICIAL PLAN - Schedule E
URBAN ROAD NETWORK

PLAN OFFICIEL - Annexe E
RÉSEAU ROUTIER - URBAIN

- | | | | |
|----------------------|-----------------------------|---|---|
| Provincial Highway | Chemin de propriété fédéral | Arterial - Existing | Artère - Établie |
| Federally Owned Road | Route provinciale | Arterial - Proposed (alignment defined) | Artère - Proposé (alignement déterminée) |
| City Freeway | Autoroute de ville | Arterial - Conceptual (alignment undefined) | Artère - Conceptuelle (alignement à déterminer) |
| | | Major Collector - Existing | Grande collectrice - Établie |
| | | Major Collector - Proposed | Grande collectrice - Proposé |
| | | Collector - Existing | Collectrice - Établie |
| | | Collector - Proposed | Collectrice - Proposé |
| | | New Interchange | Nouvel échangeur |

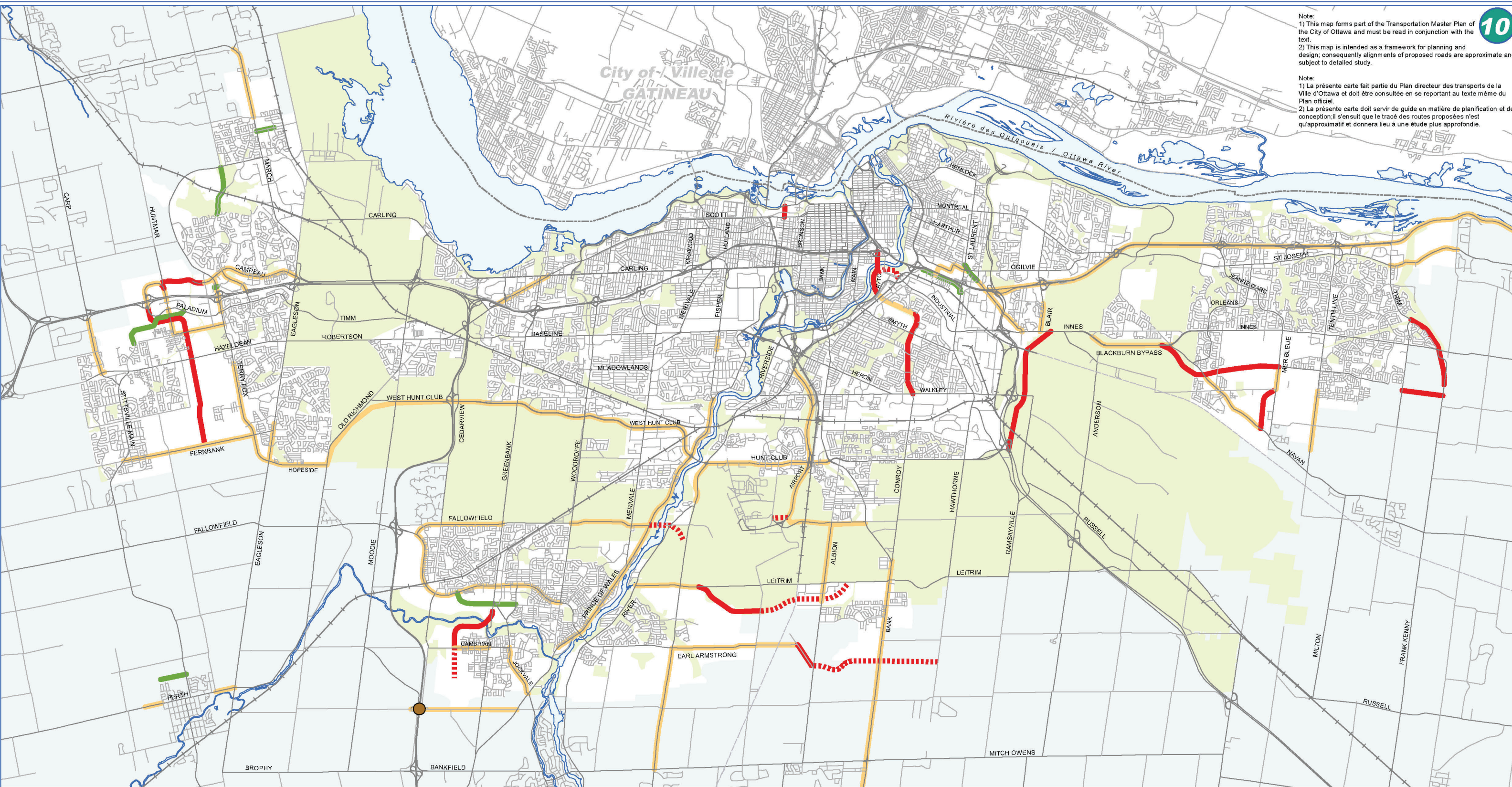
Ottawa

Planning, Infrastructure and Economic Development Department,
GIS and Data Management

Services de la planification, de l'infrastructure et du développement économique,
SIG et Gestion des données

Note:
1) This map forms part of the Transportation Master Plan of the City of Ottawa and must be read in conjunction with the text.
2) This map is intended as a framework for planning and design; consequently alignments of proposed roads are approximate and subject to detailed study.

Note:
1) La présente carte fait partie du Plan directeur des transports de la Ville d'Ottawa et doit être consultée en se reportant au texte même du Plan officiel.
2) La présente carte doit servir de guide en matière de planification et de conception; il s'ensuit que le tracé des routes proposées n'est qu'approximatif et donnera lieu à une étude plus approfondie.



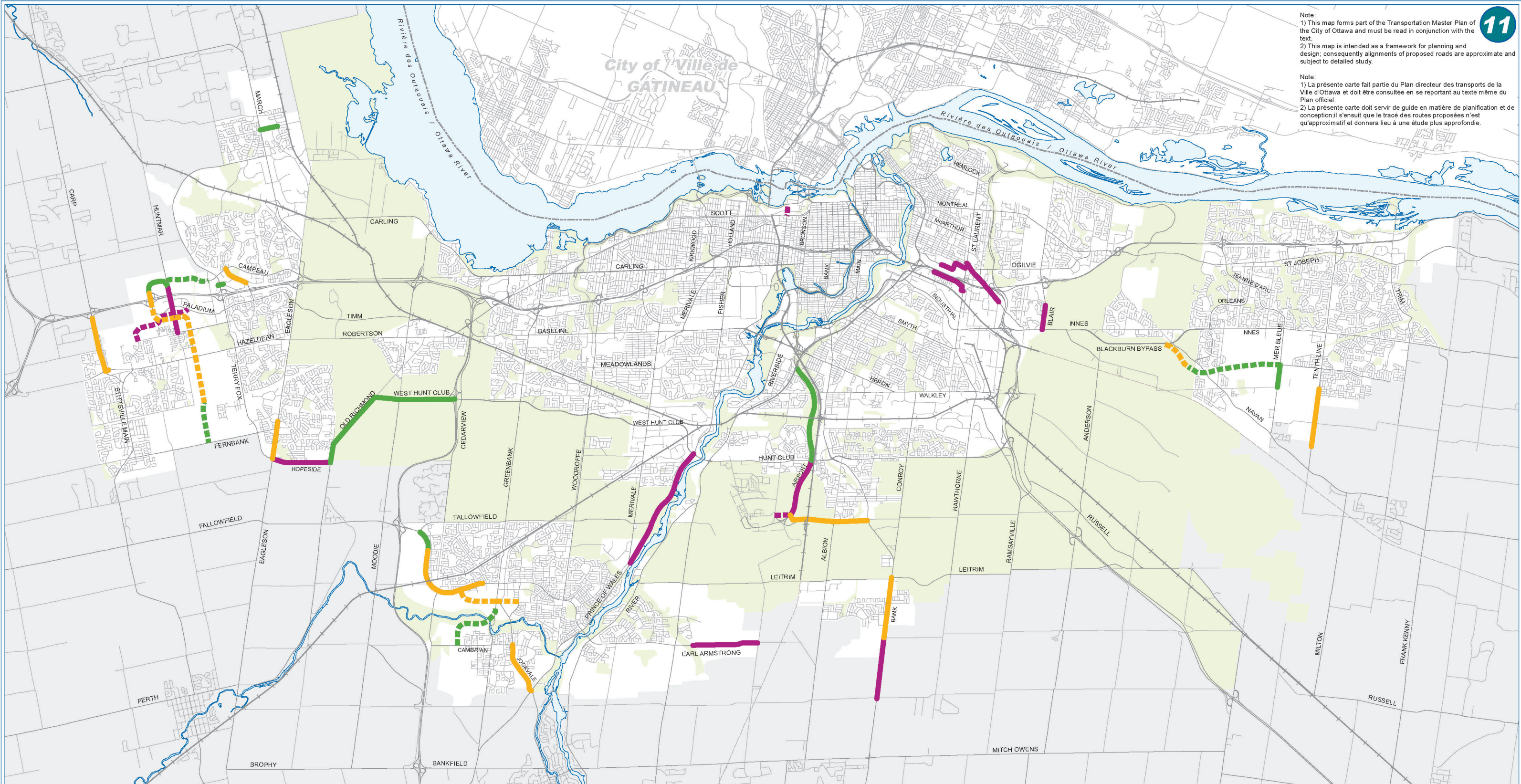
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Prepared by: Planning and Growth Management Department,
Mapping & Graphics Unit, 2015 Revision
Préparé par: Service de l'urbanisme et de la gestion de la
croissance, Unité de la cartographie et des graphiques, Révision 2015

- | | | |
|--------------------------|--|-------------------------------|
| New Arterials | | Nouvelles artères |
| Widened Arterial | | Artères élargies |
| Conceptual Arterial | | Conception d'artères |
| New or Widened Collector | | Artères élargies ou nouvelles |
| New Interchange | | Nouvel échangeur |

TRANSPORTATION MASTER PLAN - Map 10
ROAD NETWORK – 2031 NETWORK CONCEPT

PLAN DIRECTEUR DES TRANSPORTS - Carte 10
RÉSEAU ROUTIER - CONCEPT DU RÉSEAU 2031



11

Note:
1) This map forms part of the Transportation Master Plan of the City of Ottawa and must be read in conjunction with the text.
2) This map is intended as a framework for planning and design; consequently alignments of proposed roads are approximate and subject to detailed study.

Note:
1) La présente carte fait partie du Plan directeur des transports de la Ville d'Ottawa et doit être consultée en se reportant au texte même du Plan officiel.
2) La présente carte doit servir de guide en matière de planification et de conception; il s'ensuit que le tracé des routes proposées n'est qu'approximatif et donnera lieu à une étude plus approfondie.



1 0.5 0 1 2 3 km

Prepared by: Planning and Growth Management Department,
Mapping & Graphics Unit, 2015 Revision
Préparé par: Service de l'urbanisme et de la gestion de la
croissance, Unité de la cartographie et des graphiques, Révision 2015

- | | | |
|--------------------------------|--|--------------------------------------|
| Phase 1 (2014 - 2019) Widening | | Phase 1 (2014 - 2019) Élargissement |
| Phase 1 (2014 - 2019) New Road | | Phase 1 (2014 - 2019) Nouvelle route |
| Phase 2 (2020 - 2025) Widening | | Phase 2 (2020 - 2025) Élargissement |
| Phase 2 (2020 - 2025) New Road | | Phase 2 (2020 - 2025) Nouvelle route |
| Phase 3 (2026 - 2031) Widening | | Phase 3 (2026 - 2031) Élargissement |
| Phase 3 (2026 - 2031) New Road | | Phase 3 (2026 - 2031) Nouvelle route |

TRANSPORTATION MASTER PLAN - Map 11

ROAD NETWORK – 2031 AFFORDABLE NETWORK

PLAN DIRECTEUR DES TRANSPORTS - Carte 11

RÉSEAU ROUTIER - RÉSEAU ABORDABLE 2031

Table A3 Road Projects

Project	General Description	Rationale	EA Status
Rideau River Crossing (Network Concept)	New four lane bridge and approaches between Prince of Wales Drive and Limebank Road	Provides for increased capacity across Rideau River screenline.	Not started
Riverside Drive (Network Concept)	Widen from four to six lanes between River Road and Hunt Club Road	Provides capacity for growth in Riverside South	Complete
Strandherd Drive (Affordable Network and Network Concept)	Affordable: Widen from two to four lanes between Fallowfield Road and Jockvale Road Concept: Widen from four to six lanes between Jockvale Road and Woodroffe Avenue	Addresses capacity deficiencies at the Rideau River South and Manotick screenlines, in conjunction with a Strandherd-Earl Armstrong Rideau River Bridge and Earl Armstrong Road widening	Complete
Stittsville Main Street Extension (Affordable Network and Network Concept)	New two-lane road between Palladium Drive and Maple Grove Road	Provides capacity for development in Stittsville	Not started
Stittsville North-South Arterial (Affordable Network and Network Concept)	New two-lane road between Palladium Drive and Fernbank Road	Provides capacity for development in Stittsville and provides a bypass for Stittsville Main Street congestion	Complete
Tenth Line Road (Affordable Network and Network Concept)	Widen from two to four lanes between Harvest Valley Drive and the urban boundary	Serves growth south of Innes Road	Complete
Terry Fox Drive (Network Concept)	Widen from two to four lanes between Winchester Drive and Eagleson Road	Provides access to adjacent developments	Complete
	Widen from four to six lanes between Campeau Drive and Palladium Drive	Accommodates Kanata West Development	Not started
Tremblay Road (Affordable Network and Network Concept)	Widen from two to four lanes between Pickering Place and St. Laurent Boulevard	Addresses the needs identified by the St. Laurent Station Transit-Oriented Development study and accommodates new employment land at St. Laurent Blvd at Tremblay Road	Not started
West Hunt Club Road (Network Concept)	Widen from four to six lanes between Highway 416 and Prince of Wales Drive	Serves on-going development/ redevelopment along corridor and makes full use of Rideau River Bridge	Not started

APPENDIX B

SOUND LEVEL CALCULATIONS

- Part 1 - Modelling Results
- Part 2 - Stamson Modelling Figures

PART 1 (APPENDIX B)

Stamson Modelling Results

Filename: 1r1.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: COPE (day/night)

Car traffic volume : 6477/563 veh/TimePeriod *
Medium truck volume : 515/45 veh/TimePeriod *
Heavy truck volume : 368/32 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 8000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: COPE (day/night)

Angle1 Angle2 : -50.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 21.80 / 21.80 m
Receiver height : 1.50 / 1.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

↑

Road data, segment # 2: TERRY FOX N (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00

Number of Years of Growth : 0.00
 Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: TERRY FOX N (day/night)

 Angle1 Angle2 : -75.00 deg 75.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 31.40 / 31.40 m
 Receiver height : 1.50 / 1.50 m
 Topography : 1 (Flat/gentle slope; no barrier)
 Reference angle : 0.00



Road data, segment # 3: TERRY FOX S (day/night)

 Car traffic volume : 14168/1232 veh/TimePeriod *
 Medium truck volume : 1127/98 veh/TimePeriod *
 Heavy truck volume : 805/70 veh/TimePeriod *
 Posted speed limit : 80 km/h
 Road gradient : 1 %
 Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
 Percentage of Annual Growth : 0.00
 Number of Years of Growth : 0.00
 Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: TERRY FOX S (day/night)

 Angle1 Angle2 : -75.00 deg 75.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 41.60 / 41.60 m
 Receiver height : 1.50 / 1.50 m
 Topography : 1 (Flat/gentle slope; no barrier)
 Reference angle : 0.00



Result summary (day)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.COPE	!	1.50	!	60.92	!	60.92
2.TERRY FOX N	!	1.50	!	66.11	!	66.11
3.TERRY FOX S	!	1.50	!	64.09	!	64.09
Total						68.97 dBA

↑

Result summary (night)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.COPE	!	1.50	!	53.33	!	53.33
2.TERRY FOX N	!	1.50	!	58.52	!	58.52
3.TERRY FOX S	!	1.50	!	56.49	!	56.49
Total						61.37 dBA

↑

TOTAL Leq FROM ALL SOURCES (DAY): 68.97
(NIGHT): 61.37

↑

↑

Filename: 2r1.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: COPE (day/night)

Car traffic volume : 6477/563 veh/TimePeriod *
Medium truck volume : 515/45 veh/TimePeriod *
Heavy truck volume : 368/32 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 8000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: COPE (day/night)

Angle1 Angle2 : -50.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 21.80 / 21.80 m
Receiver height : 4.50 / 4.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

↑

Road data, segment # 2: TERRY FOX N (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00

Number of Years of Growth : 0.00
 Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: TERRY FOX N (day/night)

 Angle1 Angle2 : -75.00 deg 75.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 31.40 / 31.40 m
 Receiver height : 4.50 / 4.50 m
 Topography : 1 (Flat/gentle slope; no barrier)
 Reference angle : 0.00

↑

Road data, segment # 3: TERRY FOX S (day/night)

 Car traffic volume : 14168/1232 veh/TimePeriod *
 Medium truck volume : 1127/98 veh/TimePeriod *
 Heavy truck volume : 805/70 veh/TimePeriod *
 Posted speed limit : 80 km/h
 Road gradient : 1 %
 Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
 Percentage of Annual Growth : 0.00
 Number of Years of Growth : 0.00
 Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: TERRY FOX S (day/night)

 Angle1 Angle2 : -75.00 deg 75.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 41.60 / 41.60 m
 Receiver height : 4.50 / 4.50 m
 Topography : 1 (Flat/gentle slope; no barrier)
 Reference angle : 0.00

↑

Result summary (day)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.COPE	!	1.50	!	61.18	!	61.18
2.TERRY FOX N	!	1.50	!	66.52	!	66.52
3.TERRY FOX S	!	1.50	!	64.60	!	64.60
Total						69.39 dBA

↑

Result summary (night)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.COPE	!	1.50	!	53.59	!	53.59
2.TERRY FOX N	!	1.50	!	58.92	!	58.92
3.TERRY FOX S	!	1.50	!	57.00	!	57.00
Total						61.79 dBA

↑

TOTAL Leq FROM ALL SOURCES (DAY): 69.39
(NIGHT): 61.79

↑

↑

Filename: 1r2.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: COPE (day/night)

Car traffic volume : 6477/563 veh/TimePeriod *
Medium truck volume : 515/45 veh/TimePeriod *
Heavy truck volume : 368/32 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 8000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: COPE (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 23.20 / 23.20 m
Receiver height : 1.50 / 1.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

↑

Road data, segment # 2: TERRY FOX N (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00

Number of Years of Growth	:	0.00
Medium Truck % of Total Volume	:	7.00
Heavy Truck % of Total Volume	:	5.00
Day (16 hrs) % of Total Volume	:	92.00

Data for Segment # 2: TERRY FOX N (day/night)

```

-----
Angle1   Angle2       : -65.00 deg   60.00 deg
Wood depth      :           0       (No woods.)
No of house rows :           0 / 0
Surface         :           1       (Absorptive ground surface)
Receiver source distance : 83.20 / 83.20 m
Receiver height  :    1.50 / 1.50 m
Topography      :           2       (Flat/gentle slope; with barrier)
Barrier angle1   : -25.00 deg   Angle2 : 15.00 deg
Barrier height   :    9.10 m
Barrier receiver distance : 20.50 / 20.50 m
Source elevation :   97.10 m
Receiver elevation :   99.30 m
Barrier elevation :   97.60 m
Reference angle  :    0.00

```

↑

Road data, segment # 3: TERRY FOX S (day/night)

```

-----
Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient      : 1 %
Road pavement      : 1 (Typical asphalt or concrete)

```

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT):	17500
Percentage of Annual Growth	: 0.00
Number of Years of Growth	: 0.00
Medium Truck % of Total Volume	: 7.00
Heavy Truck % of Total Volume	: 5.00
Day (16 hrs) % of Total Volume	: 92.00

Data for Segment # 3: TERRY FOX S (day/night)

```

-----
Angle1   Angle2       : -65.00 deg   60.00 deg
Wood depth      :           0       (No woods.)
No of house rows :           0 / 0
Surface         :           1       (Absorptive ground surface)
Receiver source distance : 93.40 / 93.40 m
Receiver height  :    1.50 / 1.50 m
Topography      :           2       (Flat/gentle slope; with barrier)

```

Barrier angle1 : -25.00 deg Angle2 : 15.00 deg
 Barrier height : 9.10 m
 Barrier receiver distance : 20.50 / 20.50 m
 Source elevation : 98.30 m
 Receiver elevation : 99.30 m
 Barrier elevation : 97.60 m
 Reference angle : 0.00

↑

Result summary (day)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.COPE	!	1.50	!	61.15	!	61.15
2.TERRY FOX N	!	1.50	!	56.73	!	56.73
3.TERRY FOX S	!	1.50	!	55.92	!	55.92
	!		!		!	
		Total				63.35 dBA

↑

Result summary (night)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.COPE	!	1.50	!	53.56	!	53.56
2.TERRY FOX N	!	1.50	!	49.13	!	49.13
3.TERRY FOX S	!	1.50	!	48.32	!	48.32
	!		!		!	
		Total				55.76 dBA

↑

TOTAL Leq FROM ALL SOURCES (DAY): 63.35
 (NIGHT): 55.76

↑

↑

Filename: 2r2.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: COPE (day/night)

Car traffic volume : 6477/563 veh/TimePeriod *
Medium truck volume : 515/45 veh/TimePeriod *
Heavy truck volume : 368/32 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 8000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: COPE (day/night)

Angle1 Angle2 : -90.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 23.20 / 23.20 m
Receiver height : 4.50 / 4.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

↑

Road data, segment # 2: TERRY FOX N (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00

Number of Years of Growth	:	0.00
Medium Truck % of Total Volume	:	7.00
Heavy Truck % of Total Volume	:	5.00
Day (16 hrs) % of Total Volume	:	92.00

Data for Segment # 2: TERRY FOX N (day/night)

```

-----
Angle1   Angle2       : -65.00 deg   60.00 deg
Wood depth      :           0       (No woods.)
No of house rows :           0 / 0
Surface         :           1       (Absorptive ground surface)
Receiver source distance : 83.20 / 83.20 m
Receiver height  :    4.50 / 4.50 m
Topography      :           2       (Flat/gentle slope; with barrier)
Barrier angle1   : -25.00 deg   Angle2 : 15.00 deg
Barrier height   :    9.10 m
Barrier receiver distance : 20.50 / 20.50 m
Source elevation :   97.10 m
Receiver elevation :   99.30 m
Barrier elevation :   97.60 m
Reference angle  :    0.00

```

↑

Road data, segment # 3: TERRY FOX S (day/night)

```

-----
Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient      : 1 %
Road pavement      : 1 (Typical asphalt or concrete)

```

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT):	17500
Percentage of Annual Growth	: 0.00
Number of Years of Growth	: 0.00
Medium Truck % of Total Volume	: 7.00
Heavy Truck % of Total Volume	: 5.00
Day (16 hrs) % of Total Volume	: 92.00

Data for Segment # 3: TERRY FOX S (day/night)

```

-----
Angle1   Angle2       : -65.00 deg   60.00 deg
Wood depth      :           0       (No woods.)
No of house rows :           0 / 0
Surface         :           1       (Absorptive ground surface)
Receiver source distance : 93.40 / 93.40 m
Receiver height  :    4.50 / 4.50 m
Topography      :           2       (Flat/gentle slope; with barrier)

```

Barrier angle1 : -25.00 deg Angle2 : 15.00 deg
 Barrier height : 9.10 m
 Barrier receiver distance : 20.50 / 20.50 m
 Source elevation : 98.30 m
 Receiver elevation : 99.30 m
 Barrier elevation : 97.60 m
 Reference angle : 0.00

↑

Result summary (day)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.COPE	!	1.50	!	61.47	!	61.47
2.TERRY FOX N	!	1.50	!	57.62	!	57.62
3.TERRY FOX S	!	1.50	!	56.90	!	56.90
Total						63.93 dBA

↑

Result summary (night)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.COPE	!	1.50	!	53.88	!	53.88
2.TERRY FOX N	!	1.50	!	50.03	!	50.03
3.TERRY FOX S	!	1.50	!	49.30	!	49.30
Total						56.34 dBA

↑

TOTAL Leq FROM ALL SOURCES (DAY): 63.93
 (NIGHT): 56.34

↑

↑

Filename: 1r3.te Time Period: Day/Night 16/8 hours
 Description:

Road data, segment # 1: COPE (day/night)

```
-----
Car traffic volume   : 6477/563   veh/TimePeriod  *
Medium truck volume : 515/45     veh/TimePeriod  *
Heavy truck volume  : 368/32     veh/TimePeriod  *
Posted speed limit  : 50 km/h
Road gradient       : 1 %
Road pavement       : 1 (Typical asphalt or concrete)
```

* Refers to calculated road volumes based on the following input:

```
24 hr Traffic Volume (AADT or SADT): 8000
Percentage of Annual Growth         : 0.00
Number of Years of Growth           : 0.00
Medium Truck % of Total Volume      : 7.00
Heavy Truck % of Total Volume       : 5.00
Day (16 hrs) % of Total Volume      : 92.00
```

Data for Segment # 1: COPE (day/night)

```
-----
Angle1  Angle2      : -90.00 deg   90.00 deg
Wood depth          : 0           (No woods.)
No of house rows    : 0 / 0
Surface             : 1           (Absorptive ground surface)
Receiver source distance : 22.60 / 22.60 m
Receiver height      : 1.50 / 1.50 m
Topography           : 1           (Flat/gentle slope; no barrier)
Reference angle      : 0.00
```

↑
 Result summary (day)

```
-----
! source ! Road ! Total
! height ! Leq  ! Leq
! (m)    ! (dBA) ! (dBA)
-----+-----+-----
1.COPE   ! 1.50 ! 61.34 ! 61.34
-----+-----+-----
Total                    61.34 dBA
```

↑
 Result summary (night)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
-----+-----+-----+-----						
1.COPE	!	1.50	!	53.75	!	53.75
-----+-----+-----+-----						
		Total				53.75 dBA

↑

TOTAL Leq FROM ALL SOURCES (DAY): 61.34
(NIGHT): 53.75

↑

↑

Filename: 2r3.te Time Period: Day/Night 16/8 hours
 Description:

Road data, segment # 1: COPE (day/night)

```
-----
Car traffic volume   : 6477/563   veh/TimePeriod  *
Medium truck volume : 515/45     veh/TimePeriod  *
Heavy truck volume  : 368/32     veh/TimePeriod  *
Posted speed limit  : 50 km/h
Road gradient       : 1 %
Road pavement       : 1 (Typical asphalt or concrete)
```

* Refers to calculated road volumes based on the following input:

```
24 hr Traffic Volume (AADT or SADT): 8000
Percentage of Annual Growth         : 0.00
Number of Years of Growth           : 0.00
Medium Truck % of Total Volume      : 7.00
Heavy Truck % of Total Volume       : 5.00
Day (16 hrs) % of Total Volume      : 92.00
```

Data for Segment # 1: COPE (day/night)

```
-----
Angle1  Angle2      : -90.00 deg   90.00 deg
Wood depth          : 0           (No woods.)
No of house rows    : 0 / 0
Surface             : 1           (Absorptive ground surface)
Receiver source distance : 22.60 / 22.60 m
Receiver height      : 4.50 / 4.50 m
Topography           : 1           (Flat/gentle slope; no barrier)
Reference angle      : 0.00
```

↑
 Result summary (day)

```
-----
! source ! Road ! Total
! height ! Leq ! Leq
! (m) ! (dBA) ! (dBA)
-----+-----+-----
1.COPE ! 1.50 ! 61.65 ! 61.65
-----+-----+-----
Total 61.65 dBA
```

↑
 Result summary (night)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
-----+-----+-----+-----						
1.COPE	!	1.50	!	54.06	!	54.06
-----+-----+-----+-----						
		Total				54.06 dBA

↑

TOTAL Leq FROM ALL SOURCES (DAY): 61.65
(NIGHT): 54.06

↑

↑

Filename: 1r4.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: COPE (day/night)

Car traffic volume : 6477/563 veh/TimePeriod *
Medium truck volume : 515/45 veh/TimePeriod *
Heavy truck volume : 368/32 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 8000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: COPE (day/night)

Angle1 Angle2 : -25.00 deg 30.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 97.10 / 97.10 m
Receiver height : 1.50 / 1.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -5.00 deg Angle2 : 20.00 deg
Barrier height : 9.10 m
Barrier receiver distance : 63.70 / 63.70 m
Source elevation : 97.08 m
Receiver elevation : 99.36 m
Barrier elevation : 97.70 m
Reference angle : 0.00

↑

Road data, segment # 2: TERRY FOX N (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %

Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: TERRY FOX N (day/night)

Angle1 Angle2 : -65.00 deg 70.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 42.00 / 42.00 m
Receiver height : 1.50 / 1.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

↑

Road data, segment # 3: TERRY FOX S (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: TERRY FOX S (day/night)

Angle1 Angle2 : -65.00 deg 70.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 52.10 / 52.10 m
Receiver height : 1.50 / 1.50 m
Topography : 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

↑

Result summary (day)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.COPE	!	1.50	!	44.48	!	44.48
2.TERRY FOX N	!	1.50	!	63.75	!	63.75
3.TERRY FOX S	!	1.50	!	62.20	!	62.20
Total						66.08 dBA

↑

Result summary (night)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.COPE	!	1.50	!	36.88	!	36.88
2.TERRY FOX N	!	1.50	!	56.16	!	56.16
3.TERRY FOX S	!	1.50	!	54.60	!	54.60
Total						58.49 dBA

↑

TOTAL Leq FROM ALL SOURCES (DAY): 66.08
(NIGHT): 58.49

↑

↑

Filename: 2r4.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: COPE (day/night)

Car traffic volume : 6477/563 veh/TimePeriod *
Medium truck volume : 515/45 veh/TimePeriod *
Heavy truck volume : 368/32 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 8000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: COPE (day/night)

Angle1 Angle2 : -25.00 deg 30.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 97.10 / 97.10 m
Receiver height : 4.50 / 4.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -5.00 deg Angle2 : 20.00 deg
Barrier height : 9.10 m
Barrier receiver distance : 63.70 / 63.70 m
Source elevation : 97.08 m
Receiver elevation : 99.36 m
Barrier elevation : 97.70 m
Reference angle : 0.00

↑

Road data, segment # 2: TERRY FOX N (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %

Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: TERRY FOX N (day/night)

Angle1 Angle2 : -65.00 deg 70.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 42.00 / 42.00 m
Receiver height : 4.50 / 4.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

↑

Road data, segment # 3: TERRY FOX S (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: TERRY FOX S (day/night)

Angle1 Angle2 : -65.00 deg 70.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 52.10 / 52.10 m
Receiver height : 4.50 / 4.50 m
Topography : 1 (Flat/gentle slope; no barrier)

Reference angle : 0.00

↑

Result summary (day)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.COPE	!	1.50	!	45.28	!	45.28
2.TERRY FOX N	!	1.50	!	64.25	!	64.25
3.TERRY FOX S	!	1.50	!	62.78	!	62.78
Total						66.62 dBA

↑

Result summary (night)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.COPE	!	1.50	!	37.69	!	37.69
2.TERRY FOX N	!	1.50	!	56.65	!	56.65
3.TERRY FOX S	!	1.50	!	55.18	!	55.18
Total						59.02 dBA

↑

TOTAL Leq FROM ALL SOURCES (DAY): 66.62
(NIGHT): 59.02

↑

↑

Filename: 1r5.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: COPE (day/night)

Car traffic volume : 6477/563 veh/TimePeriod *
Medium truck volume : 515/45 veh/TimePeriod *
Heavy truck volume : 368/32 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 8000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: COPE (day/night)

Angle1 Angle2 : -80.00 deg 70.00 deg
Wood depth : 0 (No woods.)
No of house rows : 1 / 1
House density : 90 %
Surface : 1 (Absorptive ground surface)
Receiver source distance : 67.10 / 67.10 m
Receiver height : 1.50 / 1.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

↑

Road data, segment # 2: TERRY FOX N (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500

Percentage of Annual Growth	:	0.00
Number of Years of Growth	:	0.00
Medium Truck % of Total Volume	:	7.00
Heavy Truck % of Total Volume	:	5.00
Day (16 hrs) % of Total Volume	:	92.00

Data for Segment # 2: TERRY FOX N (day/night)

```

-----
Angle1   Angle2      : -55.00 deg   60.00 deg
Wood depth      :      0      (No woods.)
No of house rows      :      1 / 1
House density    :      95 %
Surface         :      1      (Absorptive ground surface)
Receiver source distance : 106.40 / 106.40 m
Receiver height  :      1.50 / 1.50 m
Topography      :      1      (Flat/gentle slope; no barrier)
Reference angle  :      0.00

```

↑

Road data, segment # 3: TERRY FOX S (day/night)

```

-----
Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient      : 1 %
Road pavement      : 1 (Typical asphalt or concrete)

```

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT):	17500
Percentage of Annual Growth	: 0.00
Number of Years of Growth	: 0.00
Medium Truck % of Total Volume	: 7.00
Heavy Truck % of Total Volume	: 5.00
Day (16 hrs) % of Total Volume	: 92.00

Data for Segment # 3: TERRY FOX S (day/night)

```

-----
Angle1   Angle2      : -55.00 deg   60.00 deg
Wood depth      :      0      (No woods.)
No of house rows      :      1 / 1
House density    :      95 %
Surface         :      1      (Absorptive ground surface)
Receiver source distance : 116.30 / 116.30 m
Receiver height  :      1.50 / 1.50 m
Topography      :      1      (Flat/gentle slope; no barrier)
Reference angle  :      0.00

```

↑

Result summary (day)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.COPE	!	1.50	!	45.38	!	45.38
2.TERRY FOX N	!	1.50	!	47.79	!	47.79
3.TERRY FOX S	!	1.50	!	47.28	!	47.28
Total						51.71 dBA



Result summary (night)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.COPE	!	1.50	!	37.78	!	37.78
2.TERRY FOX N	!	1.50	!	40.19	!	40.19
3.TERRY FOX S	!	1.50	!	39.68	!	39.68
Total						44.11 dBA



TOTAL Leq FROM ALL SOURCES (DAY): 51.71
(NIGHT): 44.11



Filename: 2r5.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: COPE (day/night)

Car traffic volume : 6477/563 veh/TimePeriod *
Medium truck volume : 515/45 veh/TimePeriod *
Heavy truck volume : 368/32 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 8000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: COPE (day/night)

Angle1 Angle2 : -80.00 deg 70.00 deg
Wood depth : 0 (No woods.)
No of house rows : 1 / 1
House density : 90 %
Surface : 1 (Absorptive ground surface)
Receiver source distance : 67.10 / 67.10 m
Receiver height : 4.50 / 4.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

↑

Road data, segment # 2: TERRY FOX N (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500

Percentage of Annual Growth : 0.00
 Number of Years of Growth : 0.00
 Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: TERRY FOX N (day/night)

 Angle1 Angle2 : -55.00 deg 60.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 1 / 1
 House density : 95 %
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 106.40 / 106.40 m
 Receiver height : 4.50 / 4.50 m
 Topography : 1 (Flat/gentle slope; no barrier)
 Reference angle : 0.00

↑

Road data, segment # 3: TERRY FOX S (day/night)

 Car traffic volume : 14168/1232 veh/TimePeriod *
 Medium truck volume : 1127/98 veh/TimePeriod *
 Heavy truck volume : 805/70 veh/TimePeriod *
 Posted speed limit : 80 km/h
 Road gradient : 1 %
 Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
 Percentage of Annual Growth : 0.00
 Number of Years of Growth : 0.00
 Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: TERRY FOX S (day/night)

 Angle1 Angle2 : -55.00 deg 60.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 1 / 1
 House density : 95 %
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 116.30 / 116.30 m
 Receiver height : 4.50 / 4.50 m
 Topography : 1 (Flat/gentle slope; no barrier)
 Reference angle : 0.00

↑

Result summary (day)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.COPE	!	1.50	!	46.08	!	46.08
2.TERRY FOX N	!	1.50	!	48.62	!	48.62
3.TERRY FOX S	!	1.50	!	48.15	!	48.15
Total						52.52 dBA

↑

Result summary (night)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.COPE	!	1.50	!	38.48	!	38.48
2.TERRY FOX N	!	1.50	!	41.02	!	41.02
3.TERRY FOX S	!	1.50	!	40.55	!	40.55
Total						44.92 dBA

↑

TOTAL Leq FROM ALL SOURCES (DAY): 52.52
(NIGHT): 44.92

↑

↑

Filename: 1r6.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: TERRY FOX N (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: TERRY FOX N (day/night)

Angle1 Angle2 : -75.00 deg 75.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 24.30 / 24.30 m
Receiver height : 1.50 / 1.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

↑

Road data, segment # 2: TERRY FOX S (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00

Number of Years of Growth : 0.00
 Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: TERRY FOX S (day/night)

 Angle1 Angle2 : -75.00 deg 75.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 34.10 / 34.10 m
 Receiver height : 1.50 / 1.50 m
 Topography : 1 (Flat/gentle slope; no barrier)
 Reference angle : 0.00

↑
 Result summary (day)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
-----+						
1.TERRY FOX N	!	1.50	!	67.96	!	67.96
2.TERRY FOX S	!	1.50	!	65.52	!	65.52
-----+						
		Total				69.92 dBA

↑
 Result summary (night)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
-----+						
1.TERRY FOX N	!	1.50	!	60.37	!	60.37
2.TERRY FOX S	!	1.50	!	57.92	!	57.92
-----+						
		Total				62.33 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 69.92
 (NIGHT): 62.33

↑
 ↑

Filename: 2R6.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: TERRY FOX N (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: TERRY FOX N (day/night)

Angle1 Angle2 : -75.00 deg 75.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 24.30 / 24.30 m
Receiver height : 4.50 / 4.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

↑

Road data, segment # 2: TERRY FOX S (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00

Number of Years of Growth : 0.00
 Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: TERRY FOX S (day/night)

 Angle1 Angle2 : -75.00 deg 75.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 34.10 / 34.10 m
 Receiver height : 4.50 / 4.50 m
 Topography : 1 (Flat/gentle slope; no barrier)
 Reference angle : 0.00

↑
 Result summary (day)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.TERRY FOX N	!	1.50	!	68.26	!	68.26
2.TERRY FOX S	!	1.50	!	65.95	!	65.95
	+		+		+	
		Total				70.27 dBA

↑
 Result summary (night)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.TERRY FOX N	!	1.50	!	60.67	!	60.67
2.TERRY FOX S	!	1.50	!	58.36	!	58.36
	+		+		+	
		Total				62.68 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 70.27
 (NIGHT): 62.68

↑
 ↑

Filename: 1r7.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: TERRY FOX N (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: TERRY FOX N (day/night)

Angle1 Angle2 : -65.00 deg 65.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 65.20 / 65.20 m
Receiver height : 1.50 / 1.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : 45.00 deg Angle2 : 65.00 deg
Barrier height : 9.10 m
Barrier receiver distance : 11.80 / 11.80 m
Source elevation : 98.30 m
Receiver elevation : 99.49 m
Barrier elevation : 97.60 m
Reference angle : 0.00

↑

Road data, segment # 2: TERRY FOX S (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %

Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: TERRY FOX S (day/night)

Angle1 Angle2 : -65.00 deg 65.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 74.70 / 74.70 m
Receiver height : 1.50 / 1.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : 45.00 deg Angle2 : 65.00 deg
Barrier height : 9.10 m
Barrier receiver distance : 11.80 / 11.80 m
Source elevation : 98.30 m
Receiver elevation : 99.49 m
Barrier elevation : 97.60 m
Reference angle : 0.00

↑
Result summary (day)

! source ! Road ! Total
! height ! Leq ! Leq
! (m) ! (dBA) ! (dBA)

1.TERRY FOX N ! 1.50 ! 59.94 ! 59.94
2.TERRY FOX S ! 1.50 ! 58.96 ! 58.96

Total 62.49 dBA

↑
Result summary (night)

! source ! Road ! Total
! height ! Leq ! Leq
! (m) ! (dBA) ! (dBA)

1.TERRY FOX N ! 1.50 ! 52.34 ! 52.34

2.TERRY FOX S	!	1.50	!	51.37	!	51.37
-----+-----+-----+-----						
Total					54.89 dBA	

↑

TOTAL Leq FROM ALL SOURCES (DAY): 62.49
(NIGHT): 54.89

↑

↑

Filename: 2r7.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: TERRY FOX N (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: TERRY FOX N (day/night)

Angle1 Angle2 : -65.00 deg 65.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 65.20 / 65.20 m
Receiver height : 4.50 / 4.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : 45.00 deg Angle2 : 65.00 deg
Barrier height : 9.10 m
Barrier receiver distance : 11.80 / 11.80 m
Source elevation : 98.30 m
Receiver elevation : 99.49 m
Barrier elevation : 97.60 m
Reference angle : 0.00

↑

Road data, segment # 2: TERRY FOX S (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %

Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: TERRY FOX S (day/night)

Angle1 Angle2 : -65.00 deg 65.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 74.70 / 74.70 m
Receiver height : 4.50 / 4.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : 45.00 deg Angle2 : 65.00 deg
Barrier height : 9.10 m
Barrier receiver distance : 11.80 / 11.80 m
Source elevation : 98.30 m
Receiver elevation : 99.49 m
Barrier elevation : 97.60 m
Reference angle : 0.00

↑
Result summary (day)

! source ! Road ! Total
! height ! Leq ! Leq
! (m) ! (dBA) ! (dBA)

1.TERRY FOX N ! 1.50 ! 60.64 ! 60.64
2.TERRY FOX S ! 1.50 ! 59.73 ! 59.73

Total 63.22 dBA

↑
Result summary (night)

! source ! Road ! Total
! height ! Leq ! Leq
! (m) ! (dBA) ! (dBA)

1.TERRY FOX N ! 1.50 ! 53.04 ! 53.04

2.TERRY FOX S	!	1.50	!	52.13	!	52.13
-----+-----+-----+-----						
Total					55.62 dBA	

↑

TOTAL Leq FROM ALL SOURCES (DAY): 63.22
(NIGHT): 55.62

↑

↑

Filename: 1r8.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: TERRY FOX N (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: TERRY FOX N (day/night)

Angle1 Angle2 : -70.00 deg 65.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 51.40 / 51.40 m
Receiver height : 1.50 / 1.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

↑

Road data, segment # 2: TERRY FOX S (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00

Number of Years of Growth : 0.00
 Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: TERRY FOX S (day/night)

 Angle1 Angle2 : -70.00 deg 65.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 62.40 / 62.40 m
 Receiver height : 1.50 / 1.50 m
 Topography : 1 (Flat/gentle slope; no barrier)
 Reference angle : 0.00

↑
 Result summary (day)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
-----+						
1.TERRY FOX N	!	1.50	!	62.30	!	62.30
2.TERRY FOX S	!	1.50	!	60.90	!	60.90
-----+						
		Total				64.67 dBA

↑
 Result summary (night)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
-----+						
1.TERRY FOX N	!	1.50	!	54.70	!	54.70
2.TERRY FOX S	!	1.50	!	53.30	!	53.30
-----+						
		Total				57.07 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 64.67
 (NIGHT): 57.07

↑
 ↑

Filename: 2r8.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: TERRY FOX N (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: TERRY FOX N (day/night)

Angle1 Angle2 : -70.00 deg 65.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 51.40 / 51.40 m
Receiver height : 4.50 / 4.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

↑

Road data, segment # 2: TERRY FOX S (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00

Number of Years of Growth : 0.00
 Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: TERRY FOX S (day/night)

 Angle1 Angle2 : -70.00 deg 65.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 62.40 / 62.40 m
 Receiver height : 4.50 / 4.50 m
 Topography : 1 (Flat/gentle slope; no barrier)
 Reference angle : 0.00

↑
 Result summary (day)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
-----+						
1.TERRY FOX N	!	1.50	!	62.87	!	62.87
2.TERRY FOX S	!	1.50	!	61.55	!	61.55
-----+						
		Total				65.27 dBA

↑
 Result summary (night)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
-----+						
1.TERRY FOX N	!	1.50	!	55.27	!	55.27
2.TERRY FOX S	!	1.50	!	53.95	!	53.95
-----+						
		Total				57.67 dBA

↑
 TOTAL Leq FROM ALL SOURCES (DAY): 65.27
 (NIGHT): 57.67

↑
 ↑

Filename: 1r9.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: TERRY FOX N (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: TERRY FOX N (day/night)

Angle1 Angle2 : -75.00 deg 70.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 47.90 / 47.90 m
Receiver height : 1.50 / 1.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -75.00 deg Angle2 : -60.00 deg
Barrier height : 9.10 m
Barrier receiver distance : 14.80 / 14.80 m
Source elevation : 97.75 m
Receiver elevation : 99.81 m
Barrier elevation : 98.04 m
Reference angle : 0.00

↑

Road data, segment # 2: TERRY FOX S (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %

Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: TERRY FOX S (day/night)

Angle1 Angle2 : -75.00 deg 70.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 57.80 / 57.80 m
Receiver height : 1.50 / 1.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -75.00 deg Angle2 : -60.00 deg
Barrier height : 9.10 m
Barrier receiver distance : 14.80 / 14.80 m
Source elevation : 97.75 m
Receiver elevation : 99.81 m
Barrier elevation : 98.04 m
Reference angle : 0.00

↑

Road data, segment # 3: FERNBANK (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: FERNBANK (day/night)

Angle1 Angle2 : -60.00 deg 25.00 deg

Wood depth : 0 (No woods.)
 No of house rows : 1 / 1
 House density : 50 %
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 116.30 / 116.30 m
 Receiver height : 1.50 / 1.50 m
 Topography : 2 (Flat/gentle slope; with barrier)
 Barrier angle1 : -60.00 deg Angle2 : 25.00 deg
 Barrier height : 9.10 m
 Barrier receiver distance : 14.20 / 14.20 m
 Source elevation : 97.40 m
 Receiver elevation : 99.81 m
 Barrier elevation : 97.94 m
 Reference angle : 0.00

↑

Result summary (day)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.TERRY FOX N	!	1.50	!	62.71	!	62.71
2.TERRY FOX S	!	1.50	!	61.36	!	61.36
3.FERNBANK	!	1.50	!	38.38	!	38.38
	+		+		+	
		Total				65.11 dBA

↑

Result summary (night)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.TERRY FOX N	!	1.50	!	55.12	!	55.12
2.TERRY FOX S	!	1.50	!	53.77	!	53.77
3.FERNBANK	!	1.50	!	30.79	!	30.79
	+		+		+	
		Total				57.52 dBA

↑

TOTAL Leq FROM ALL SOURCES (DAY): 65.11
 (NIGHT): 57.52

↑

Filename: 2r9.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: TERRY FOX N (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: TERRY FOX N (day/night)

Angle1 Angle2 : -75.00 deg 70.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 47.90 / 47.90 m
Receiver height : 4.50 / 4.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -75.00 deg Angle2 : -60.00 deg
Barrier height : 9.10 m
Barrier receiver distance : 14.80 / 14.80 m
Source elevation : 97.75 m
Receiver elevation : 99.81 m
Barrier elevation : 98.04 m
Reference angle : 0.00



Road data, segment # 2: TERRY FOX S (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %

Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: TERRY FOX S (day/night)

Angle1 Angle2 : -75.00 deg 70.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 57.80 / 57.80 m
Receiver height : 4.50 / 4.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -75.00 deg Angle2 : -60.00 deg
Barrier height : 9.10 m
Barrier receiver distance : 14.80 / 14.80 m
Source elevation : 97.75 m
Receiver elevation : 99.81 m
Barrier elevation : 98.04 m
Reference angle : 0.00

↑

Road data, segment # 3: FERNBANK (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: FERNBANK (day/night)

Angle1 Angle2 : -60.00 deg 25.00 deg

Wood depth : 0 (No woods.)
 No of house rows : 1 / 1
 House density : 50 %
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 116.30 / 116.30 m
 Receiver height : 4.50 / 4.50 m
 Topography : 2 (Flat/gentle slope; with barrier)
 Barrier angle1 : -60.00 deg Angle2 : 25.00 deg
 Barrier height : 9.10 m
 Barrier receiver distance : 14.20 / 14.20 m
 Source elevation : 97.40 m
 Receiver elevation : 99.81 m
 Barrier elevation : 97.94 m
 Reference angle : 0.00

↑

Result summary (day)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.TERRY FOX N	!	1.50	!	63.28	!	63.28
2.TERRY FOX S	!	1.50	!	62.02	!	62.02
3.FERNBANK	!	1.50	!	44.03	!	44.03
	+		+		+	
		Total				65.74 dBA

↑

Result summary (night)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.TERRY FOX N	!	1.50	!	55.68	!	55.68
2.TERRY FOX S	!	1.50	!	54.42	!	54.42
3.FERNBANK	!	1.50	!	36.43	!	36.43
	+		+		+	
		Total				58.14 dBA

↑

TOTAL Leq FROM ALL SOURCES (DAY): 65.74
 (NIGHT): 58.14

↑

Filename: 1r10.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: TERRY FOX N (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: TERRY FOX N (day/night)

Angle1 Angle2 : -70.00 deg 75.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 46.40 / 46.40 m
Receiver height : 1.50 / 1.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -70.00 deg Angle2 : -45.00 deg
Barrier height : 9.10 m
Barrier receiver distance : 14.80 / 14.80 m
Source elevation : 97.70 m
Receiver elevation : 99.86 m
Barrier elevation : 98.04 m
Reference angle : 0.00

↑

Road data, segment # 2: TERRY FOX S (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %

Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: TERRY FOX S (day/night)

Angle1 Angle2 : -70.00 deg 75.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 56.40 / 56.40 m
Receiver height : 1.50 / 1.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -70.00 deg Angle2 : -45.00 deg
Barrier height : 9.10 m
Barrier receiver distance : 14.80 / 14.80 m
Source elevation : 97.70 m
Receiver elevation : 99.86 m
Barrier elevation : 98.04 m
Reference angle : 0.00

↑

Road data, segment # 3: FERNBANK (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: FERNBANK (day/night)

Angle1 Angle2 : -70.00 deg 15.00 deg

Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 2 (Reflective ground surface)
 Receiver source distance : 88.90 / 88.90 m
 Receiver height : 1.50 / 1.50 m
 Topography : 2 (Flat/gentle slope; with barrier)
 Barrier angle1 : -40.00 deg Angle2 : -15.00 deg
 Barrier height : 9.10 m
 Barrier receiver distance : 33.80 / 33.80 m
 Source elevation : 97.40 m
 Receiver elevation : 99.86 m
 Barrier elevation : 97.99 m
 Reference angle : 0.00

↑

Road data, segment # 4: FERBANK (day/night)

 Car traffic volume : 12144/1056 veh/TimePeriod *
 Medium truck volume : 966/84 veh/TimePeriod *
 Heavy truck volume : 690/60 veh/TimePeriod *
 Posted speed limit : 60 km/h
 Road gradient : 0 %
 Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
 Percentage of Annual Growth : 0.00
 Number of Years of Growth : 0.00
 Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 4: FERBANK (day/night)

 Angle1 Angle2 : 15.00 deg 30.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 2 (Reflective ground surface)
 Receiver source distance : 88.90 / 88.90 m
 Receiver height : 1.50 / 1.50 m
 Topography : 2 (Flat/gentle slope; with barrier)
 Barrier angle1 : 15.00 deg Angle2 : 30.00 deg
 Barrier height : 9.10 m
 Barrier receiver distance : 25.60 / 25.60 m
 Source elevation : 97.40 m
 Receiver elevation : 99.86 m
 Barrier elevation : 98.04 m
 Reference angle : 0.00



Result summary (day)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
-----+-----+-----+-----						
1.TERRY FOX N	!	1.50	!	62.60	!	62.60
2.TERRY FOX S	!	1.50	!	61.20	!	61.20
3.FERNBANK	!	1.50	!	57.53	!	57.53
4.FERBANK	!	1.50	!	33.62	!	33.62
-----+-----+-----+-----						
		Total				65.69 dBA



Result summary (night)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
-----+-----+-----+-----						
1.TERRY FOX N	!	1.50	!	55.01	!	55.01
2.TERRY FOX S	!	1.50	!	53.61	!	53.61
3.FERNBANK	!	1.50	!	49.93	!	49.93
4.FERBANK	!	1.50	!	26.02	!	26.02
-----+-----+-----+-----						
		Total				58.10 dBA



TOTAL Leq FROM ALL SOURCES (DAY): 65.69
(NIGHT): 58.10



Filename: 2R10.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: TERRY FOX N (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: TERRY FOX N (day/night)

Angle1 Angle2 : -70.00 deg 75.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 46.40 / 46.40 m
Receiver height : 4.50 / 4.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -70.00 deg Angle2 : -45.00 deg
Barrier height : 9.10 m
Barrier receiver distance : 14.80 / 14.80 m
Source elevation : 97.70 m
Receiver elevation : 99.86 m
Barrier elevation : 98.04 m
Reference angle : 0.00



Road data, segment # 2: TERRY FOX S (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %

Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: TERRY FOX S (day/night)

Angle1 Angle2 : -70.00 deg 75.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 56.40 / 56.40 m
Receiver height : 4.50 / 4.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -70.00 deg Angle2 : -45.00 deg
Barrier height : 9.10 m
Barrier receiver distance : 14.80 / 14.80 m
Source elevation : 97.70 m
Receiver elevation : 99.86 m
Barrier elevation : 98.04 m
Reference angle : 0.00

↑

Road data, segment # 3: FERNBANK (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: FERNBANK (day/night)

Angle1 Angle2 : -70.00 deg 15.00 deg

Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 2 (Reflective ground surface)
 Receiver source distance : 88.90 / 88.90 m
 Receiver height : 4.50 / 4.50 m
 Topography : 2 (Flat/gentle slope; with barrier)
 Barrier angle1 : -40.00 deg Angle2 : -15.00 deg
 Barrier height : 9.10 m
 Barrier receiver distance : 33.80 / 33.80 m
 Source elevation : 97.40 m
 Receiver elevation : 99.86 m
 Barrier elevation : 97.99 m
 Reference angle : 0.00

↑

Road data, segment # 4: FERBANK (day/night)

 Car traffic volume : 12144/1056 veh/TimePeriod *
 Medium truck volume : 966/84 veh/TimePeriod *
 Heavy truck volume : 690/60 veh/TimePeriod *
 Posted speed limit : 60 km/h
 Road gradient : 0 %
 Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
 Percentage of Annual Growth : 0.00
 Number of Years of Growth : 0.00
 Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 4: FERBANK (day/night)

 Angle1 Angle2 : 15.00 deg 30.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 2 (Reflective ground surface)
 Receiver source distance : 88.90 / 88.90 m
 Receiver height : 4.50 / 4.50 m
 Topography : 2 (Flat/gentle slope; with barrier)
 Barrier angle1 : 15.00 deg Angle2 : 30.00 deg
 Barrier height : 9.10 m
 Barrier receiver distance : 25.60 / 25.60 m
 Source elevation : 97.40 m
 Receiver elevation : 99.86 m
 Barrier elevation : 98.04 m
 Reference angle : 0.00



Result summary (day)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
-----+-----+-----+-----						
1.TERRY FOX N	!	1.50	!	63.16	!	63.16
2.TERRY FOX S	!	1.50	!	61.86	!	61.86
3.FERNBANK	!	1.50	!	57.56	!	57.56
4.FERBANK	!	1.50	!	37.02	!	37.02
-----+-----+-----+-----						
		Total				66.21 dBA



Result summary (night)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
-----+-----+-----+-----						
1.TERRY FOX N	!	1.50	!	55.57	!	55.57
2.TERRY FOX S	!	1.50	!	54.26	!	54.26
3.FERNBANK	!	1.50	!	49.96	!	49.96
4.FERBANK	!	1.50	!	29.43	!	29.43
-----+-----+-----+-----						
		Total				58.62 dBA



TOTAL Leq FROM ALL SOURCES (DAY): 66.21
(NIGHT): 58.62



Filename: 1r11.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: TERRY FOX N (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: TERRY FOX N (day/night)

Angle1 Angle2 : -80.00 deg 80.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 21.70 / 21.70 m
Receiver height : 1.50 / 1.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

↑

Road data, segment # 2: TERRY FOX S (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00

Number of Years of Growth : 0.00
 Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: TERRY FOX S (day/night)

 Angle1 Angle2 : -80.00 deg 80.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 31.70 / 31.70 m
 Receiver height : 1.50 / 1.50 m
 Topography : 1 (Flat/gentle slope; no barrier)
 Reference angle : 0.00

↑

Road data, segment # 3: FERNBANK (day/night)

 Car traffic volume : 12144/1056 veh/TimePeriod *
 Medium truck volume : 966/84 veh/TimePeriod *
 Heavy truck volume : 690/60 veh/TimePeriod *
 Posted speed limit : 60 km/h
 Road gradient : 0 %
 Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
 Percentage of Annual Growth : 0.00
 Number of Years of Growth : 0.00
 Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: FERNBANK (day/night)

 Angle1 Angle2 : -90.00 deg 40.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 33.40 / 33.40 m
 Receiver height : 1.50 / 1.50 m
 Topography : 2 (Flat/gentle slope; with barrier)
 Barrier angle1 : -90.00 deg Angle2 : -75.00 deg
 Barrier height : 9.10 m
 Barrier receiver distance : 1.00 / 1.00 m
 Source elevation : 97.50 m
 Receiver elevation : 99.63 m
 Barrier elevation : 97.99 m

Reference angle : 0.00

↑

Result summary (day)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.TERRY FOX N	!	1.50	!	68.91	!	68.91
2.TERRY FOX S	!	1.50	!	66.17	!	66.17
3.FERNBANK	!	1.50	!	61.64	!	61.64
Total						71.26 dBA

↑

Result summary (night)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.TERRY FOX N	!	1.50	!	61.31	!	61.31
2.TERRY FOX S	!	1.50	!	58.58	!	58.58
3.FERNBANK	!	1.50	!	54.04	!	54.04
Total						63.67 dBA

↑

TOTAL Leq FROM ALL SOURCES (DAY): 71.26
(NIGHT): 63.67

↑

↑

Filename: 2r11.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: TERRY FOX N (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: TERRY FOX N (day/night)

Angle1 Angle2 : -80.00 deg 80.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 21.70 / 21.70 m
Receiver height : 4.50 / 4.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

↑

Road data, segment # 2: TERRY FOX S (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00

Number of Years of Growth : 0.00
 Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: TERRY FOX S (day/night)

 Angle1 Angle2 : -80.00 deg 80.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 31.70 / 31.70 m
 Receiver height : 4.50 / 4.50 m
 Topography : 1 (Flat/gentle slope; no barrier)
 Reference angle : 0.00

↑

Road data, segment # 3: FERNBANK (day/night)

 Car traffic volume : 12144/1056 veh/TimePeriod *
 Medium truck volume : 966/84 veh/TimePeriod *
 Heavy truck volume : 690/60 veh/TimePeriod *
 Posted speed limit : 60 km/h
 Road gradient : 0 %
 Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
 Percentage of Annual Growth : 0.00
 Number of Years of Growth : 0.00
 Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: FERNBANK (day/night)

 Angle1 Angle2 : -90.00 deg 40.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 33.40 / 33.40 m
 Receiver height : 4.50 / 4.50 m
 Topography : 2 (Flat/gentle slope; with barrier)
 Barrier angle1 : -90.00 deg Angle2 : -75.00 deg
 Barrier height : 9.10 m
 Barrier receiver distance : 1.00 / 1.00 m
 Source elevation : 97.50 m
 Receiver elevation : 99.63 m
 Barrier elevation : 97.99 m

Reference angle : 0.00

↑

Result summary (day)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.TERRY FOX N	!	1.50	!	69.18	!	69.18
2.TERRY FOX S	!	1.50	!	66.59	!	66.59
3.FERNBANK	!	1.50	!	62.07	!	62.07
Total						71.60 dBA

↑

Result summary (night)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.TERRY FOX N	!	1.50	!	61.58	!	61.58
2.TERRY FOX S	!	1.50	!	59.00	!	59.00
3.FERNBANK	!	1.50	!	54.47	!	54.47
Total						64.00 dBA

↑

TOTAL Leq FROM ALL SOURCES (DAY): 71.60
(NIGHT): 64.00

↑

↑

Filename: 1r12.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: TERRY FOX N (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: TERRY FOX N (day/night)

Angle1 Angle2 : -70.00 deg 70.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 63.30 / 63.30 m
Receiver height : 1.50 / 1.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : 10.00 deg Angle2 : 55.00 deg
Barrier height : 9.10 m
Barrier receiver distance : 29.30 / 29.30 m
Source elevation : 97.60 m
Receiver elevation : 99.58 m
Barrier elevation : 98.04 m
Reference angle : 0.00

↑

Road data, segment # 2: TERRY FOX S (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %

Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: TERRY FOX S (day/night)

Angle1 Angle2 : -70.00 deg 70.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 74.30 / 74.30 m
Receiver height : 1.50 / 1.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : 10.00 deg Angle2 : 55.00 deg
Barrier height : 9.10 m
Barrier receiver distance : 29.30 / 29.30 m
Source elevation : 97.60 m
Receiver elevation : 99.58 m
Barrier elevation : 98.04 m
Reference angle : 0.00

↑

Road data, segment # 3: FERNBANK (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: FERNBANK (day/night)

Angle1 Angle2 : -90.00 deg 70.00 deg

Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 23.40 / 23.40 m
 Receiver height : 1.50 / 1.50 m
 Topography : 1 (Flat/gentle slope; no barrier)
 Reference angle : 0.00

↑

Result summary (day)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
-----+-----+-----+-----						
1.TERRY FOX N	!	1.50	!	59.18	!	59.18
2.TERRY FOX S	!	1.50	!	58.05	!	58.05
3.FERNBANK	!	1.50	!	65.13	!	65.13
-----+-----+-----+-----						
Total						66.74 dBA

↑

Result summary (night)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
-----+-----+-----+-----						
1.TERRY FOX N	!	1.50	!	51.58	!	51.58
2.TERRY FOX S	!	1.50	!	50.45	!	50.45
3.FERNBANK	!	1.50	!	57.53	!	57.53
-----+-----+-----+-----						
Total						59.14 dBA

↑

TOTAL Leq FROM ALL SOURCES (DAY): 66.74
 (NIGHT): 59.14

↑

↑

Filename: 2r12.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: TERRY FOX N (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: TERRY FOX N (day/night)

Angle1 Angle2 : -70.00 deg 70.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 63.30 / 63.30 m
Receiver height : 4.50 / 4.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : 10.00 deg Angle2 : 55.00 deg
Barrier height : 9.10 m
Barrier receiver distance : 29.30 / 29.30 m
Source elevation : 97.60 m
Receiver elevation : 99.58 m
Barrier elevation : 98.04 m
Reference angle : 0.00

↑

Road data, segment # 2: TERRY FOX S (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %

Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: TERRY FOX S (day/night)

Angle1 Angle2 : -70.00 deg 70.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 74.30 / 74.30 m
Receiver height : 4.50 / 4.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : 10.00 deg Angle2 : 55.00 deg
Barrier height : 9.10 m
Barrier receiver distance : 29.30 / 29.30 m
Source elevation : 97.60 m
Receiver elevation : 99.58 m
Barrier elevation : 98.04 m
Reference angle : 0.00

↑

Road data, segment # 3: FERNBANK (day/night)

Car traffic volume : 12144/1056 veh/TimePeriod *
Medium truck volume : 966/84 veh/TimePeriod *
Heavy truck volume : 690/60 veh/TimePeriod *
Posted speed limit : 60 km/h
Road gradient : 0 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 15000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: FERNBANK (day/night)

Angle1 Angle2 : -90.00 deg 70.00 deg

Wood depth : 0 (No woods.)
 No of house rows : 0 / 0
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 23.40 / 23.40 m
 Receiver height : 4.50 / 4.50 m
 Topography : 1 (Flat/gentle slope; no barrier)
 Reference angle : 0.00

↑

Result summary (day)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
-----+-----+-----+-----						
1.TERRY FOX N	!	1.50	!	59.90	!	59.90
2.TERRY FOX S	!	1.50	!	58.86	!	58.86
3.FERNBANK	!	1.50	!	65.43	!	65.43
-----+-----+-----+-----						
Total						67.19 dBA

↑

Result summary (night)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
-----+-----+-----+-----						
1.TERRY FOX N	!	1.50	!	52.31	!	52.31
2.TERRY FOX S	!	1.50	!	51.26	!	51.26
3.FERNBANK	!	1.50	!	57.83	!	57.83
-----+-----+-----+-----						
Total						59.59 dBA

↑

TOTAL Leq FROM ALL SOURCES (DAY): 67.19
 (NIGHT): 59.59

↑

↑

Filename: 1r13.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: COPE (day/night)

Car traffic volume : 6477/563 veh/TimePeriod *
Medium truck volume : 515/45 veh/TimePeriod *
Heavy truck volume : 368/32 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 8000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: COPE (day/night)

Angle1 Angle2 : -90.00 deg 20.00 deg
Wood depth : 0 (No woods.)
No of house rows : 0 / 0
Surface : 1 (Absorptive ground surface)
Receiver source distance : 40.40 / 40.40 m
Receiver height : 1.50 / 1.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -85.00 deg Angle2 : -20.00 deg
Barrier height : 9.10 m
Barrier receiver distance : 6.40 / 6.40 m
Source elevation : 97.20 m
Receiver elevation : 97.70 m
Barrier elevation : 97.35 m
Reference angle : 0.00

↑

Road data, segment # 2: COPE (day/night)

Car traffic volume : 6477/563 veh/TimePeriod *
Medium truck volume : 515/45 veh/TimePeriod *
Heavy truck volume : 368/32 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 1 %

Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 8000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: COPE (day/night)

Angle1 Angle2 : 20.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 1 / 1
House density : 95 %
Surface : 1 (Absorptive ground surface)
Receiver source distance : 40.40 / 40.40 m
Receiver height : 1.50 / 1.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

↑
Result summary (day)

! source ! Road ! Total
! height ! Leq ! Leq
! (m) ! (dBA) ! (dBA)
-----+-----+-----
1.COPE ! 1.50 ! 52.22 ! 52.22
2.COPE ! 1.50 ! 42.69 ! 42.69
-----+-----+-----
Total 52.68 dBA

↑
Result summary (night)

! source ! Road ! Total
! height ! Leq ! Leq
! (m) ! (dBA) ! (dBA)
-----+-----+-----
1.COPE ! 1.50 ! 44.63 ! 44.63
2.COPE ! 1.50 ! 35.10 ! 35.10
-----+-----+-----
Total 45.09 dBA

↑

TOTAL Leq FROM ALL SOURCES (DAY): 52.68
(NIGHT): 45.09



Filename: 1r14.te Time Period: Day/Night 16/8 hours
Description:

Road data, segment # 1: COPE (day/night)

Car traffic volume : 6477/563 veh/TimePeriod *
Medium truck volume : 515/45 veh/TimePeriod *
Heavy truck volume : 368/32 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 8000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 1: COPE (day/night)

Angle1 Angle2 : -90.00 deg 10.00 deg
Wood depth : 0 (No woods.)
No of house rows : 1 / 1
House density : 75 %
Surface : 1 (Absorptive ground surface)
Receiver source distance : 83.30 / 83.30 m
Receiver height : 1.50 / 1.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -90.00 deg Angle2 : -20.00 deg
Barrier height : 9.10 m
Barrier receiver distance : 4.50 / 4.50 m
Source elevation : 97.20 m
Receiver elevation : 97.45 m
Barrier elevation : 97.38 m
Reference angle : 0.00

↑

Road data, segment # 2: COPE (day/night)

Car traffic volume : 6477/563 veh/TimePeriod *
Medium truck volume : 515/45 veh/TimePeriod *
Heavy truck volume : 368/32 veh/TimePeriod *
Posted speed limit : 50 km/h

Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 8000
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 2: COPE (day/night)

Angle1 Angle2 : 10.00 deg 90.00 deg
Wood depth : 0 (No woods.)
No of house rows : 1 / 1
House density : 95 %
Surface : 1 (Absorptive ground surface)
Receiver source distance : 83.30 / 83.30 m
Receiver height : 1.50 / 1.50 m
Topography : 1 (Flat/gentle slope; no barrier)
Reference angle : 0.00

↑

Road data, segment # 3: TERRY FOX N (day/night)

Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 3: TERRY FOX N (day/night)

Angle1 Angle2 : -50.00 deg 30.00 deg
Wood depth : 0 (No woods.)
No of house rows : 1 / 1
House density : 75 %
Surface : 1 (Absorptive ground surface)

Receiver source distance : 134.90 / 134.90 m
 Receiver height : 1.50 / 1.50 m
 Topography : 2 (Flat/gentle slope; with barrier)
 Barrier angle1 : -50.00 deg Angle2 : 20.00 deg
 Barrier height : 9.10 m
 Barrier receiver distance : 11.30 / 11.30 m
 Source elevation : 98.45 m
 Receiver elevation : 97.45 m
 Barrier elevation : 97.40 m
 Reference angle : 0.00

↑

Road data, segment # 4: TERRY FOX N (day/night)

 Car traffic volume : 14168/1232 veh/TimePeriod *
 Medium truck volume : 1127/98 veh/TimePeriod *
 Heavy truck volume : 805/70 veh/TimePeriod *
 Posted speed limit : 80 km/h
 Road gradient : 1 %
 Road pavement : 1 (Typical asphalt or concrete)

* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 17500
 Percentage of Annual Growth : 0.00
 Number of Years of Growth : 0.00
 Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 4: TERRY FOX N (day/night)

 Angle1 Angle2 : 30.00 deg 60.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 1 / 1
 House density : 90 %
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 134.90 / 134.90 m
 Receiver height : 1.50 / 1.50 m
 Topography : 2 (Flat/gentle slope; with barrier)
 Barrier angle1 : 30.00 deg Angle2 : 60.00 deg
 Barrier height : 9.10 m
 Barrier receiver distance : 1.00 / 1.00 m
 Source elevation : 98.45 m
 Receiver elevation : 97.45 m
 Barrier elevation : 97.38 m
 Reference angle : 0.00

↑

Road data, segment # 5: TERRY FOX S (day/night)

```

-----
Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

```

* Refers to calculated road volumes based on the following input:

```

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00
Medium Truck % of Total Volume : 7.00
Heavy Truck % of Total Volume : 5.00
Day (16 hrs) % of Total Volume : 92.00

```

Data for Segment # 5: TERRY FOX S (day/night)

```

-----
Angle1 Angle2 : -50.00 deg 30.00 deg
Wood depth : 0 (No woods.)
No of house rows : 1 / 1
House density : 75 %
Surface : 1 (Absorptive ground surface)
Receiver source distance : 144.90 / 144.90 m
Receiver height : 1.50 / 1.50 m
Topography : 2 (Flat/gentle slope; with barrier)
Barrier angle1 : -50.00 deg Angle2 : 20.00 deg
Barrier height : 9.10 m
Barrier receiver distance : 11.30 / 11.30 m
Source elevation : 98.45 m
Receiver elevation : 97.45 m
Barrier elevation : 97.40 m
Reference angle : 0.00

```

↑

Road data, segment # 6: TERRY FOX S (day/night)

```

-----
Car traffic volume : 14168/1232 veh/TimePeriod *
Medium truck volume : 1127/98 veh/TimePeriod *
Heavy truck volume : 805/70 veh/TimePeriod *
Posted speed limit : 80 km/h
Road gradient : 1 %
Road pavement : 1 (Typical asphalt or concrete)

```

* Refers to calculated road volumes based on the following input:

```

24 hr Traffic Volume (AADT or SADT): 17500
Percentage of Annual Growth : 0.00
Number of Years of Growth : 0.00

```

Medium Truck % of Total Volume : 7.00
 Heavy Truck % of Total Volume : 5.00
 Day (16 hrs) % of Total Volume : 92.00

Data for Segment # 6: TERRY FOX S (day/night)

 Angle1 Angle2 : 30.00 deg 60.00 deg
 Wood depth : 0 (No woods.)
 No of house rows : 1 / 1
 House density : 90 %
 Surface : 1 (Absorptive ground surface)
 Receiver source distance : 144.90 / 144.90 m
 Receiver height : 1.50 / 1.50 m
 Topography : 2 (Flat/gentle slope; with barrier)
 Barrier angle1 : 30.00 deg Angle2 : 60.00 deg
 Barrier height : 9.10 m
 Barrier receiver distance : 1.00 / 1.00 m
 Source elevation : 98.45 m
 Receiver elevation : 97.45 m
 Barrier elevation : 97.38 m
 Reference angle : 0.00

↑
 Result summary (day)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.COPE	!	1.50	!	41.69	!	41.69
2.COPE	!	1.50	!	39.10	!	39.10
3.TERRY FOX N	!	1.50	!	42.00	!	42.00
4.TERRY FOX N	!	1.50	!	34.56	!	34.56
5.TERRY FOX S	!	1.50	!	41.57	!	41.57
6.TERRY FOX S	!	1.50	!	34.22	!	34.22
	+		+		+	
		Total				47.68 dBA

↑
 Result summary (night)

	!	source	!	Road	!	Total
	!	height	!	Leq	!	Leq
	!	(m)	!	(dBA)	!	(dBA)
1.COPE	!	1.50	!	34.10	!	34.10
2.COPE	!	1.50	!	31.51	!	31.51
3.TERRY FOX N	!	1.50	!	34.40	!	34.40

4.TERRY FOX N	!	1.50	!	26.97	!	26.97
5.TERRY FOX S	!	1.50	!	33.98	!	33.98
6.TERRY FOX S	!	1.50	!	26.62	!	26.62
-----+-----+-----+-----						
Total						40.09 dBA

↑

TOTAL Leq FROM ALL SOURCES (DAY): 47.68
(NIGHT): 40.09

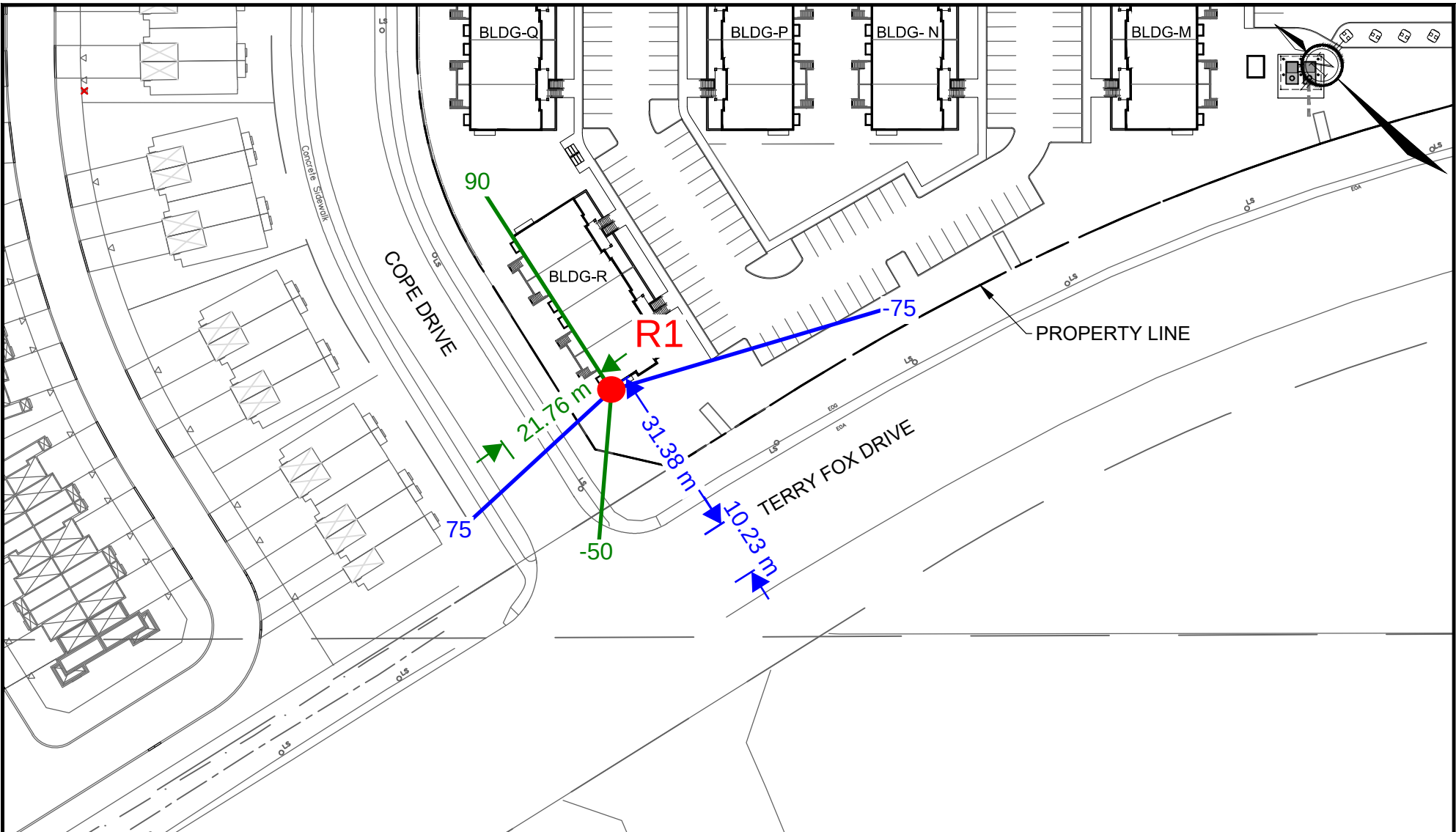
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↑

PART 2 (APPENDIX B)

Stamson Modelling Figures

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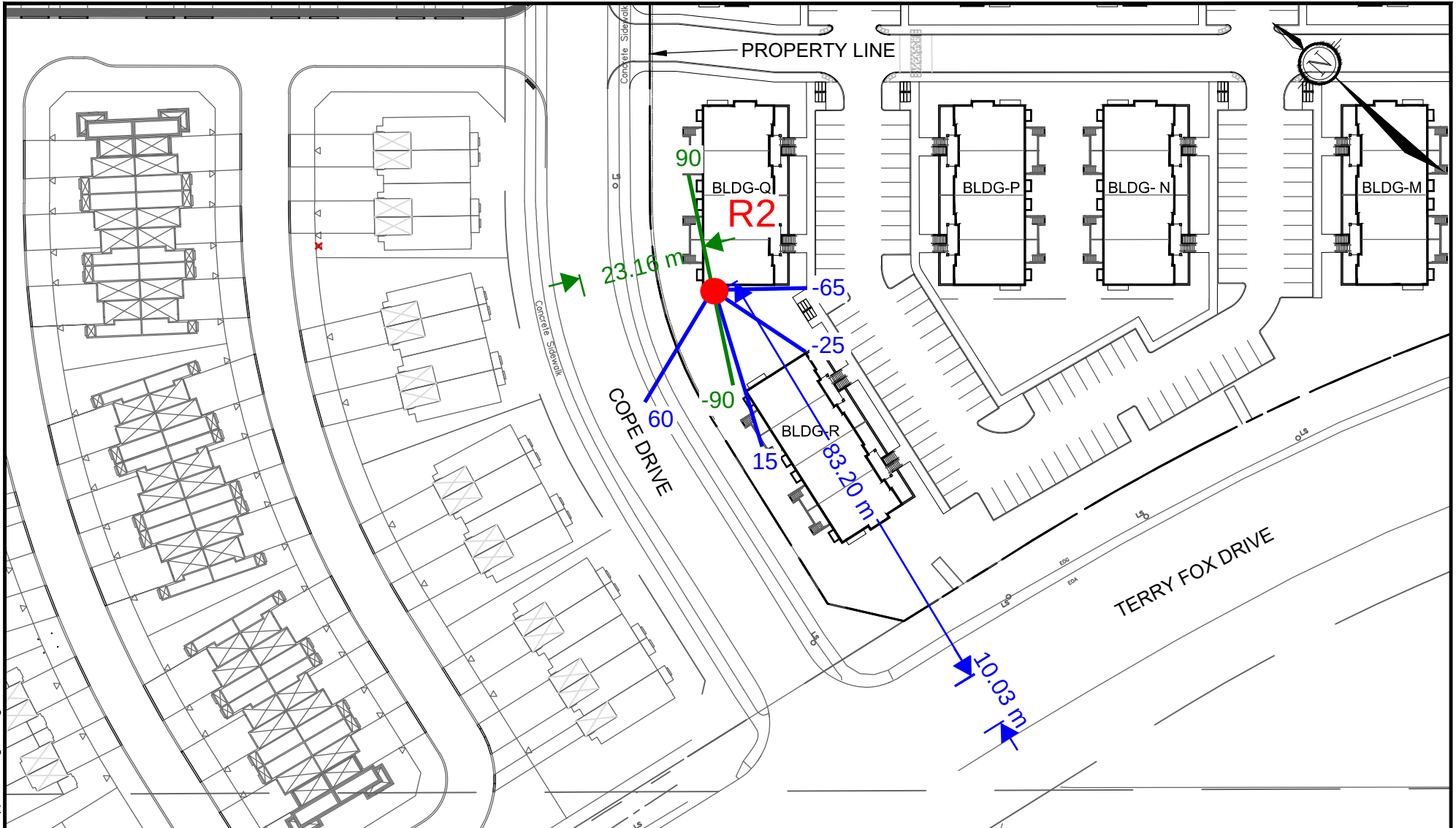
CITY OF OTTAWA
CLARIDGE FERNBANK

RECEIVER DISTANCE AND
ANGLES

SCALE 1 : 1000

DATE OCT 2025 JOB 121011 FIGURE FIG-R1

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ANGLES

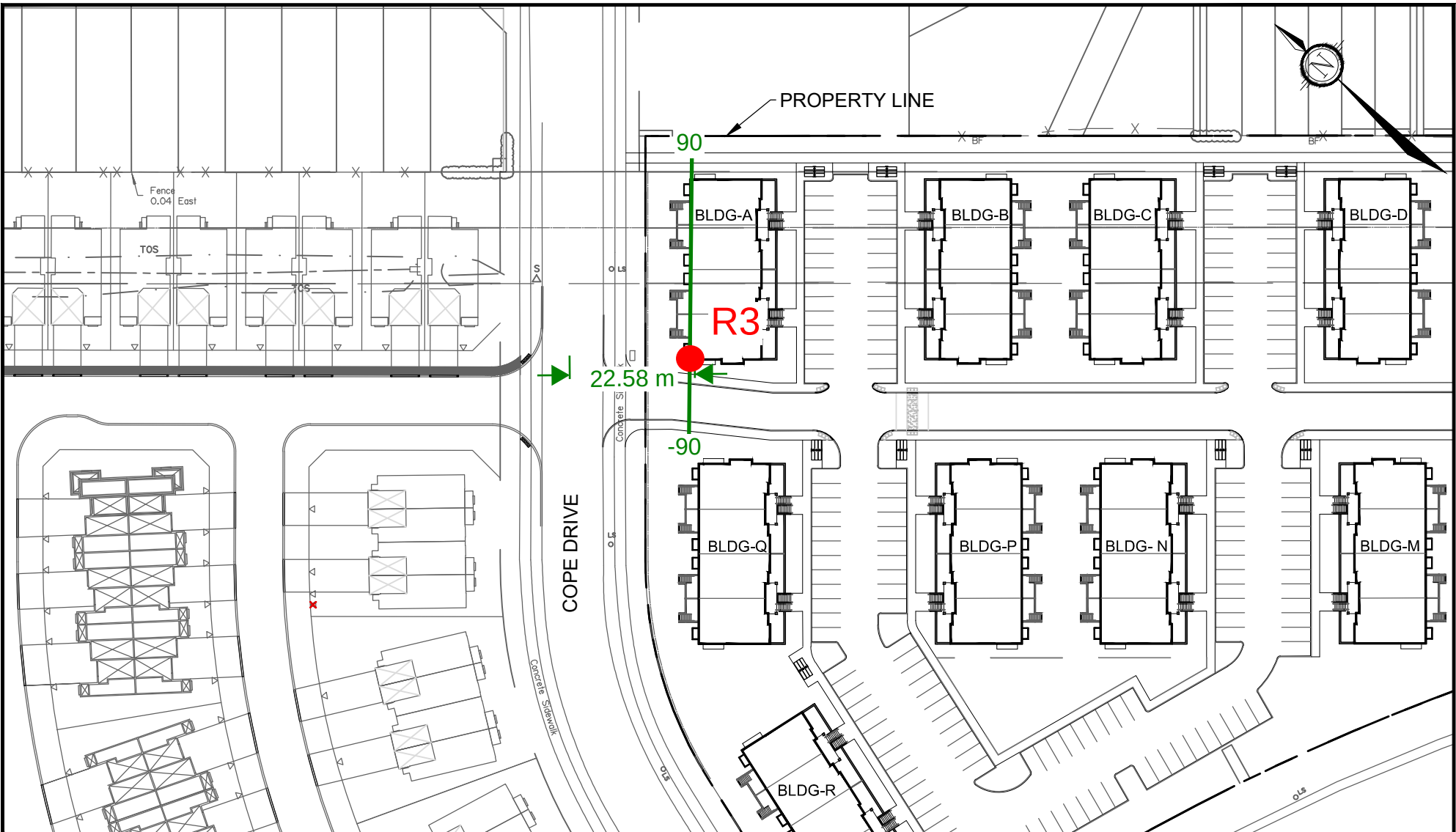
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DATE: OCT 2025

JOB: 121011

FIGURE: FIG-R2

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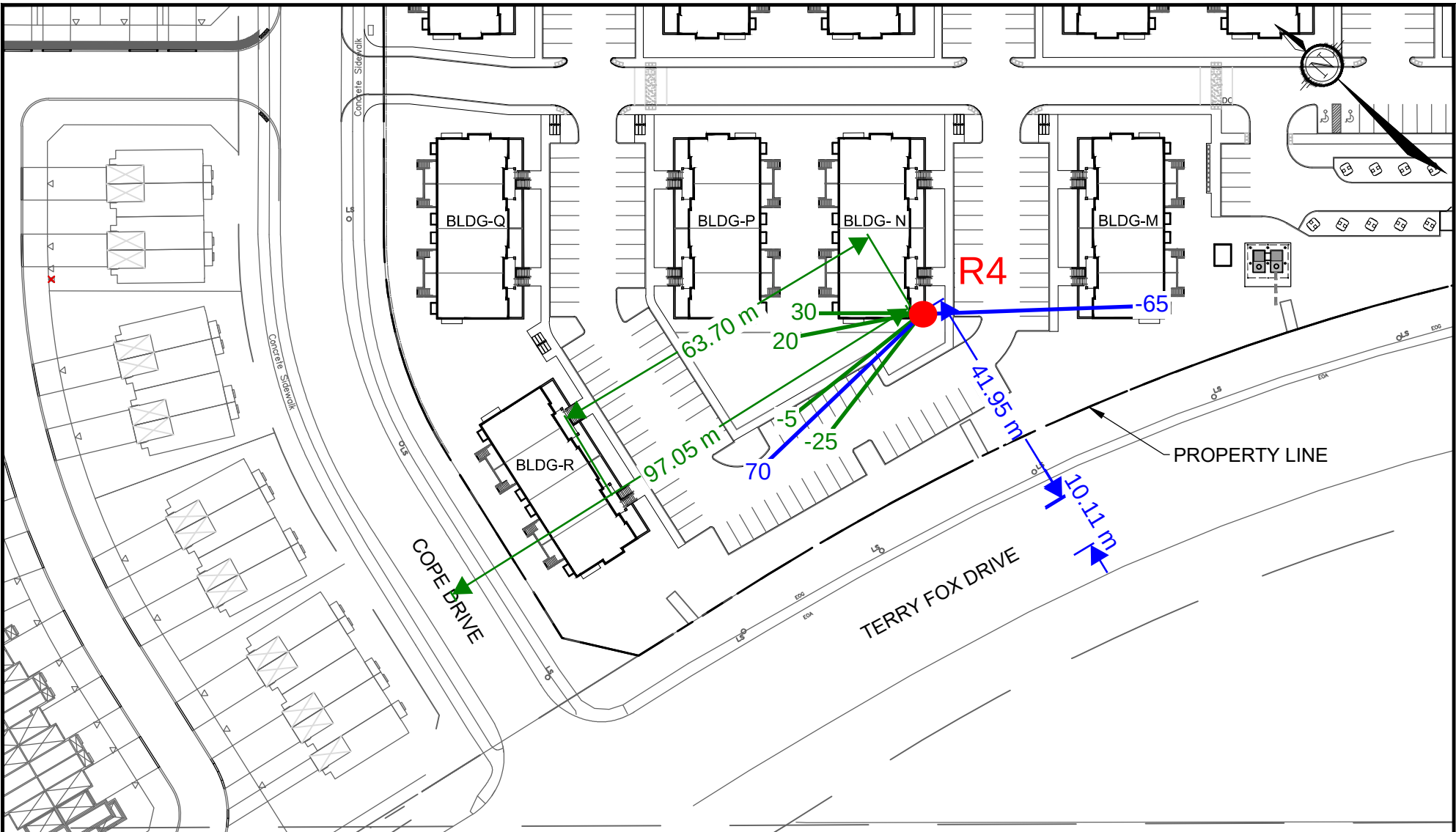
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RECEIVER DISTANCE AND ANGLES

SCALE 1 : 1000

DATE OCT 2025 JOB 121011 FIGURE FIG-R3

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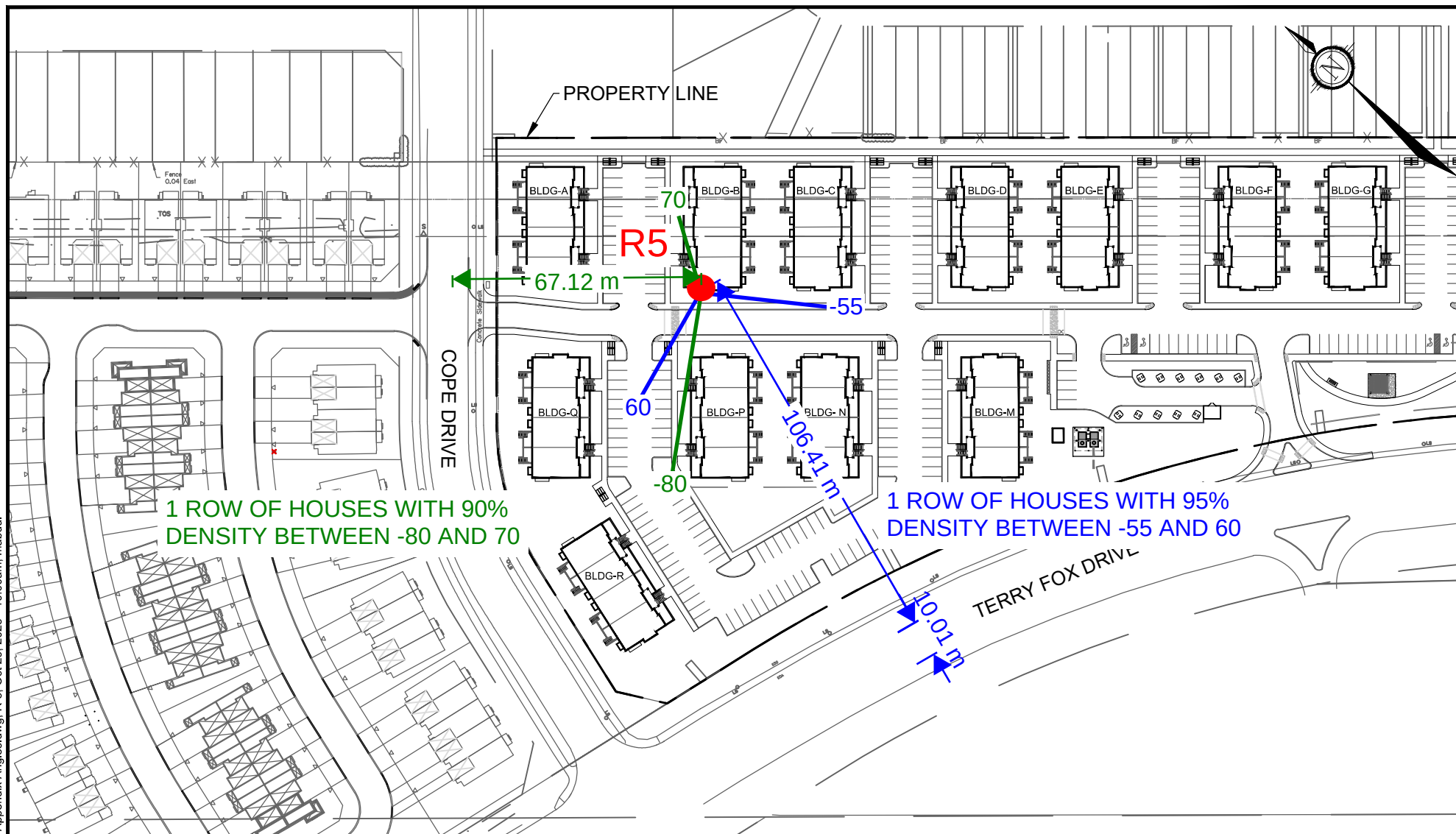
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SCALE 1 : 1000

DATE OCT 2025 JOB 121011 FIGURE FIG-R4

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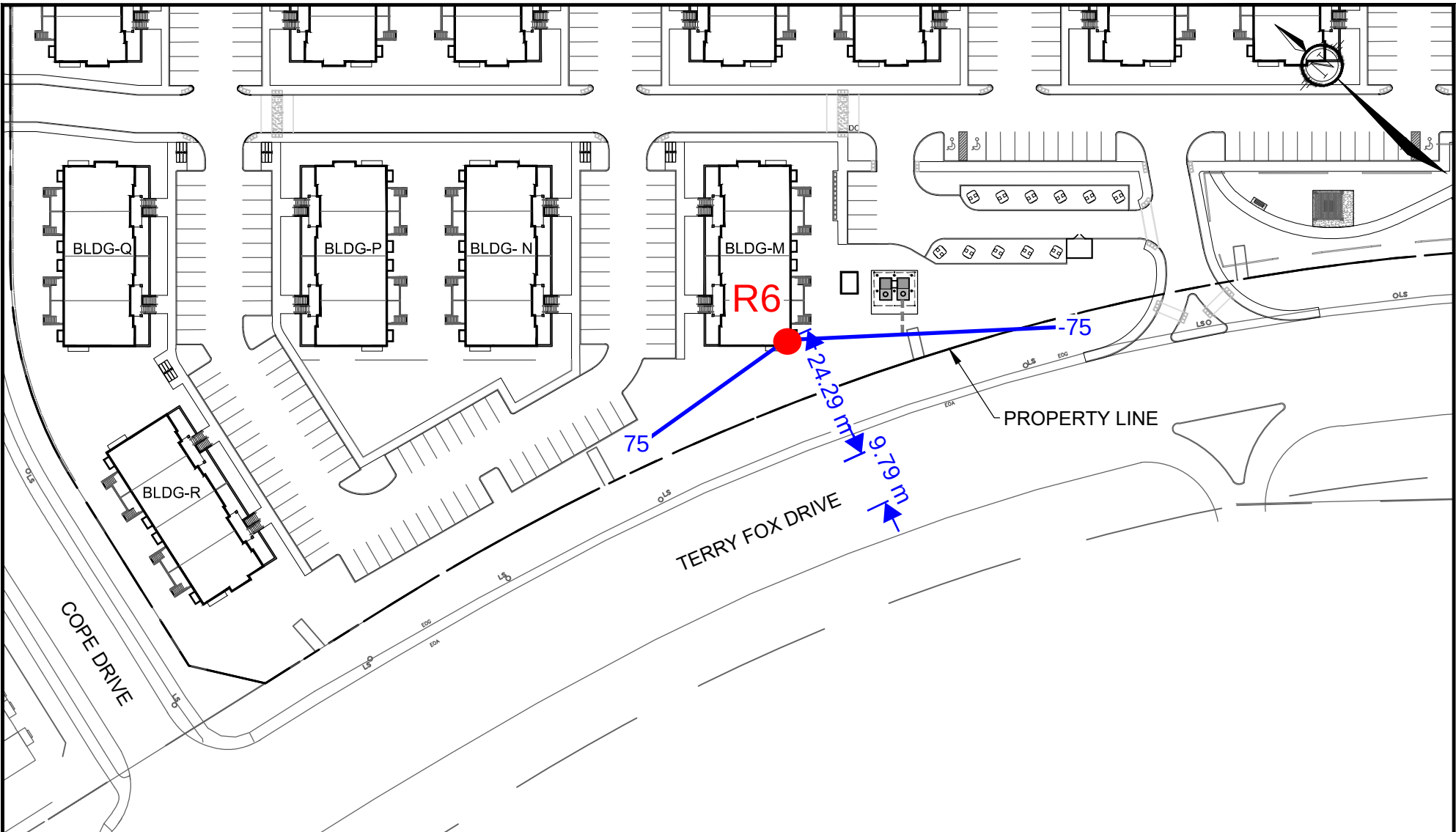
RECEIVER DISTANCE AND
ANGLES

SCALE
1 : 1500

DATE OCT 2025 JOB 121011 FIGURE FIG-R5

SHT8X11.DWG - 216mmx279mm

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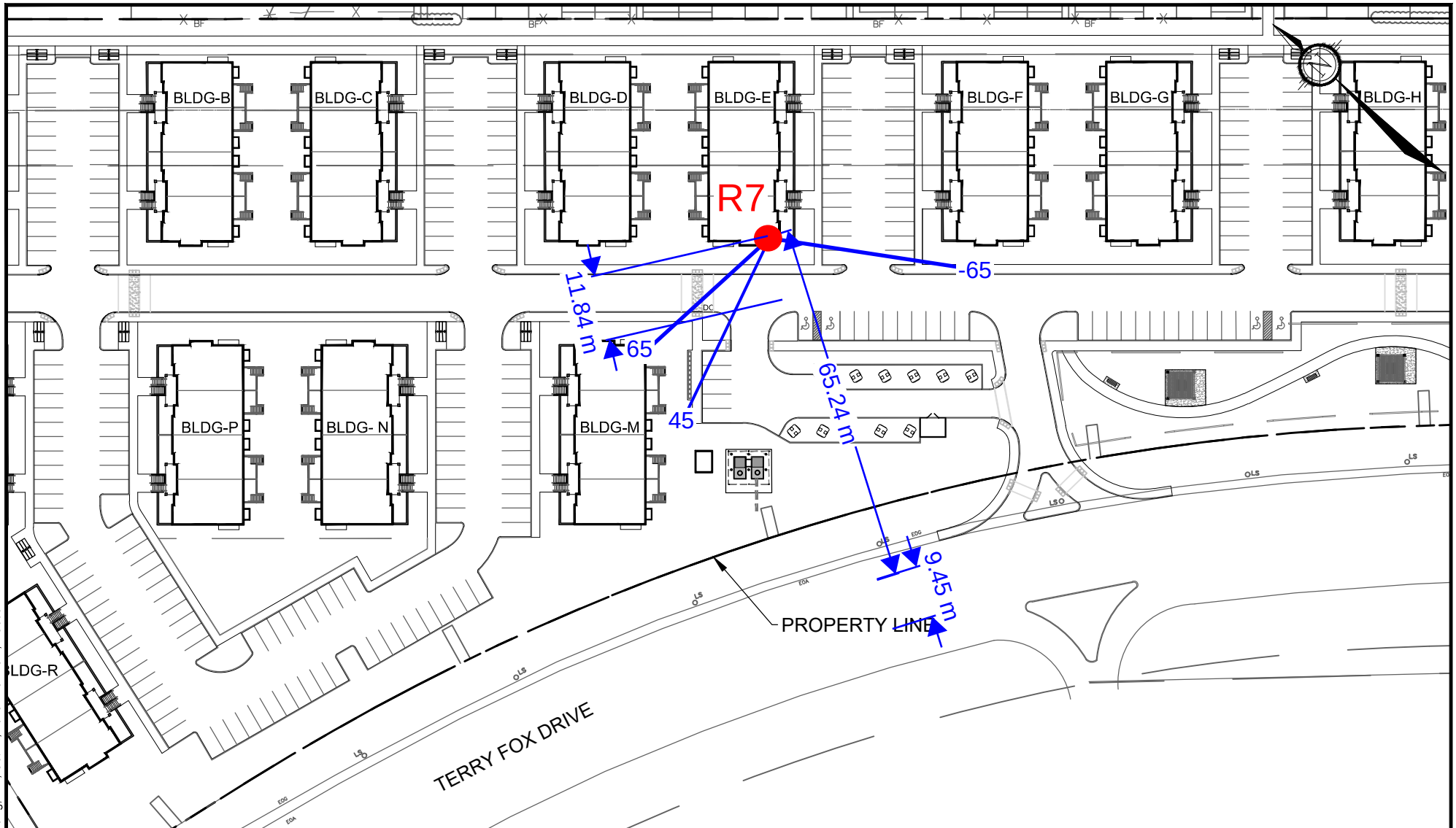
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RECEIVER DISTANCE AND
ANGLES

SCALE 1 : 1000

DATE OCT 2025 JOB 121011 FIGURE FIG-R6

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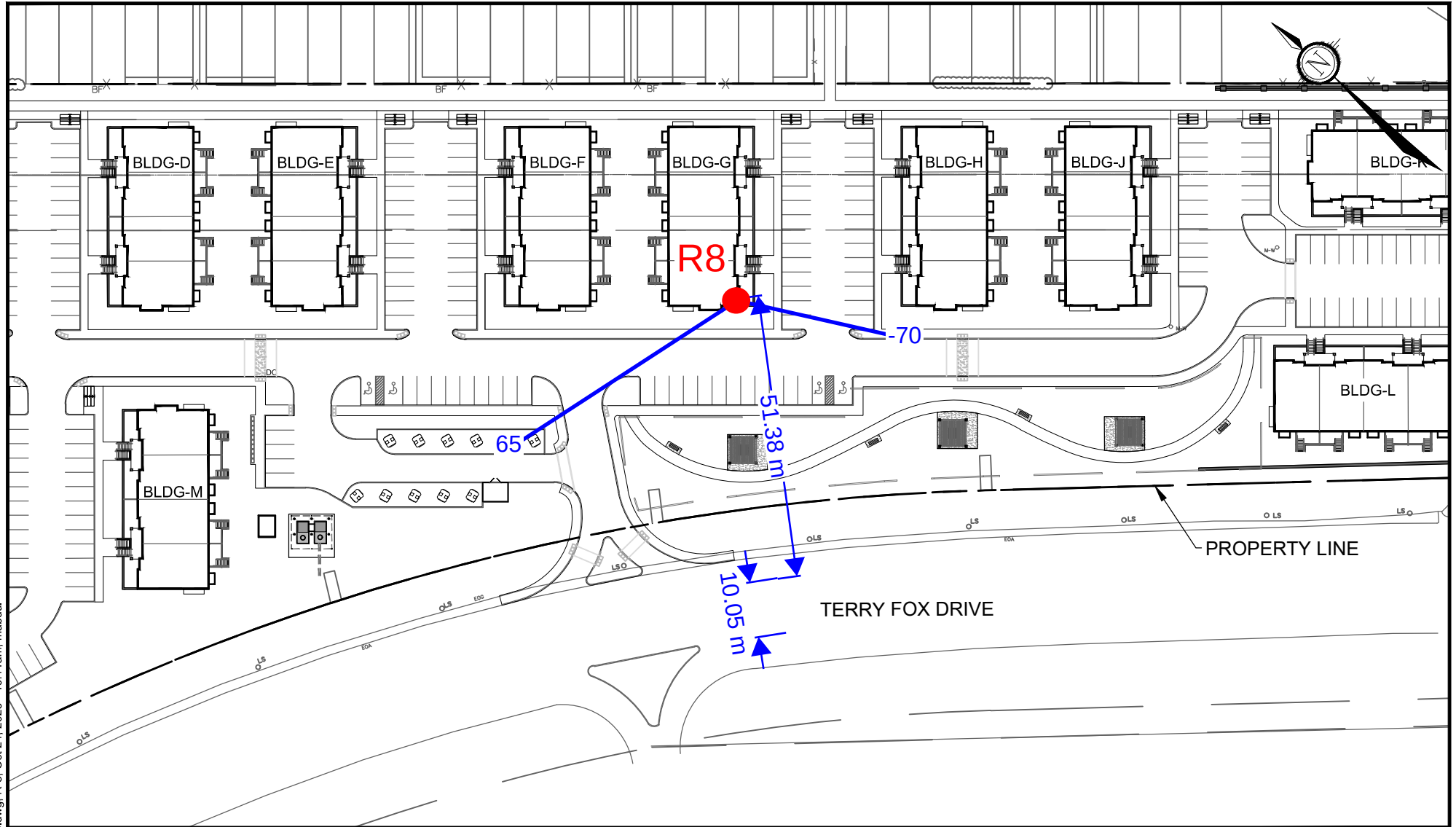
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RECEIVER DISTANCE AND
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SCALE 1 : 1000

DATE OCT 2025 JOB 121011 FIGURE FIG-R7



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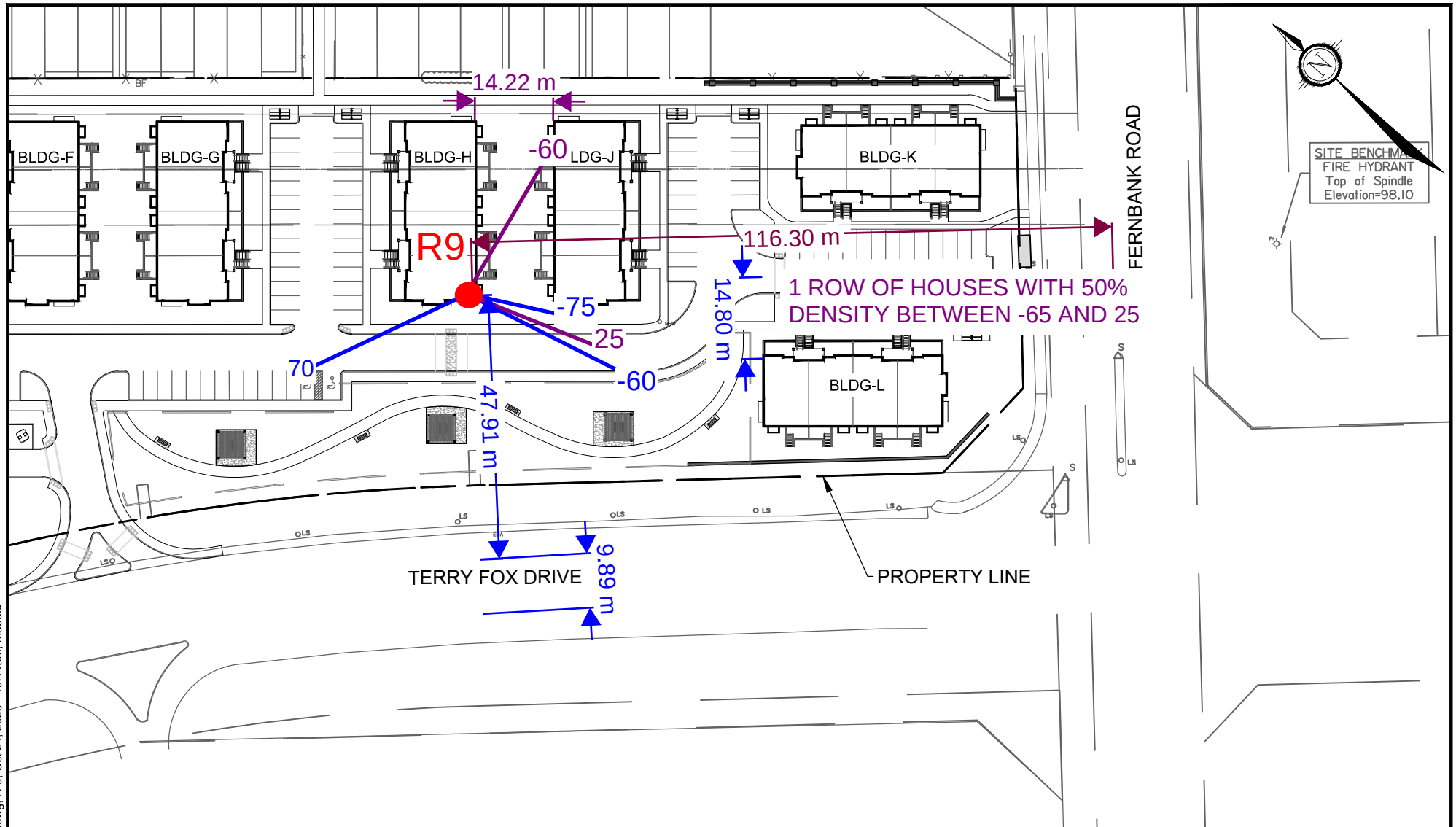
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SCALE 1 : 1000

DATE OCT 2025 JOB 121011 FIGURE FIG-R8



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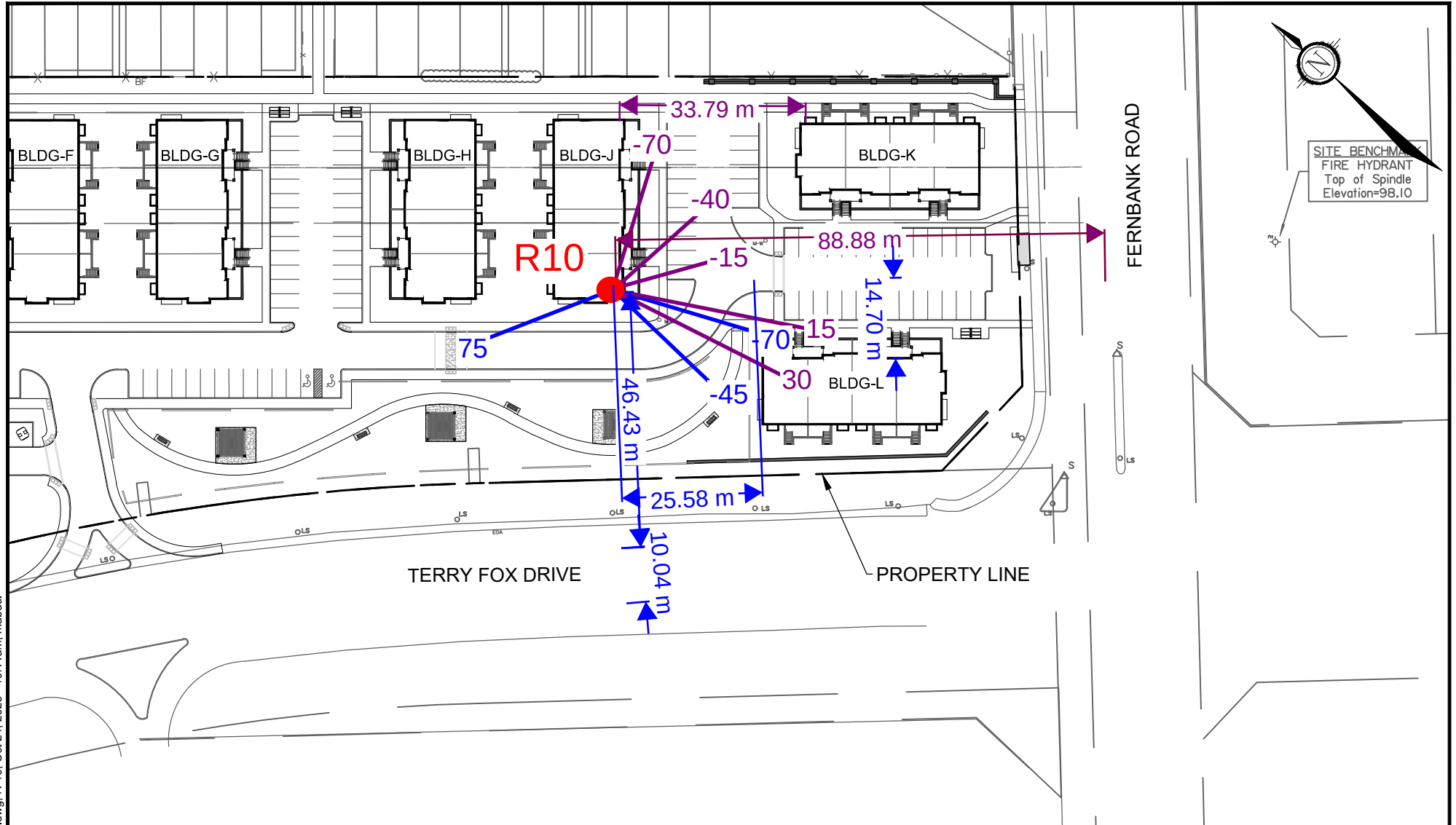
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SCALE 1 : 1000

DATE OCT 2025 JOB 121011 FIGURE FIG-R9



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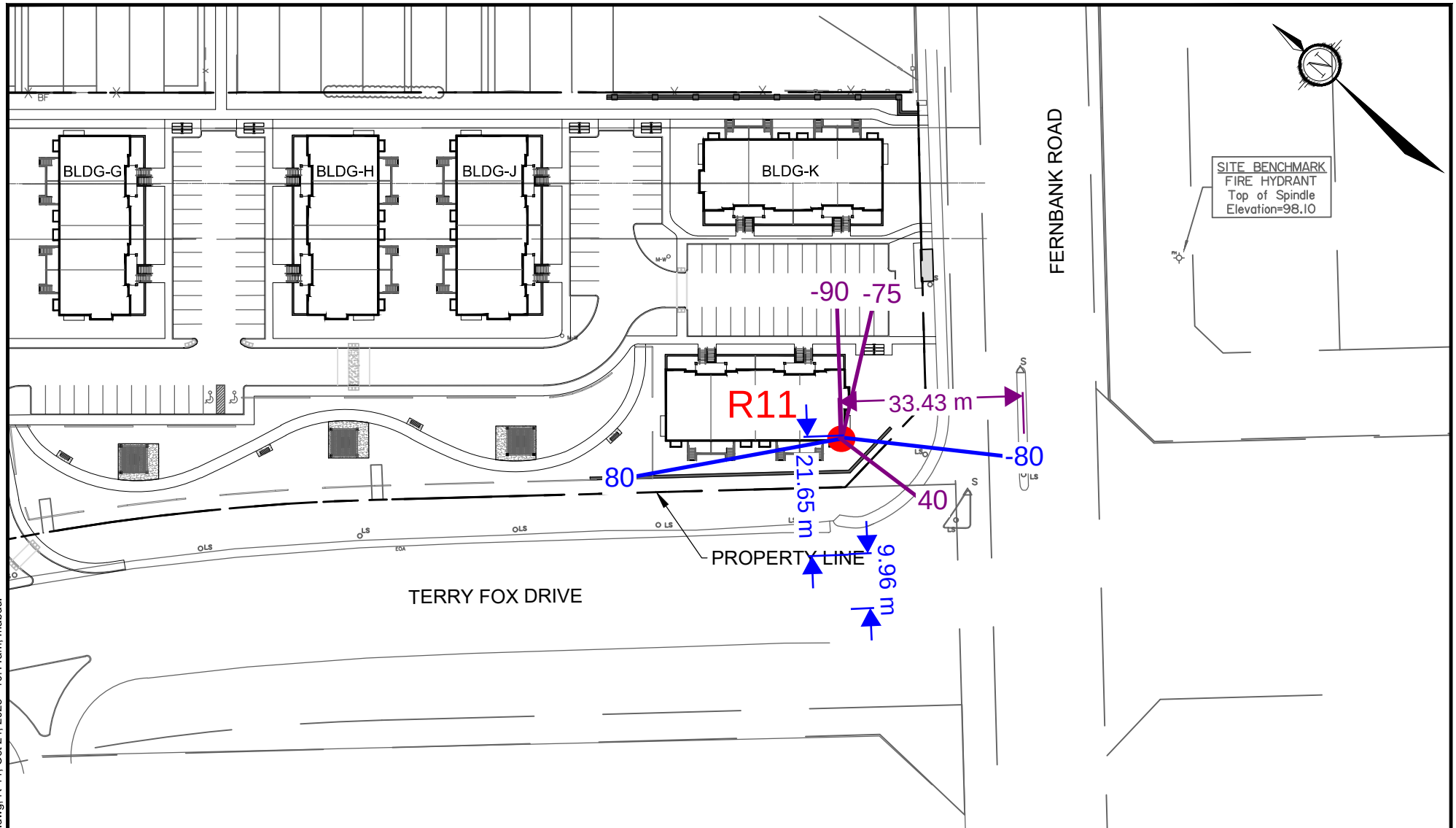
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SCALE 1 : 1000

DATE OCT 2025 JOB 121011 FIGURE FIG-R10



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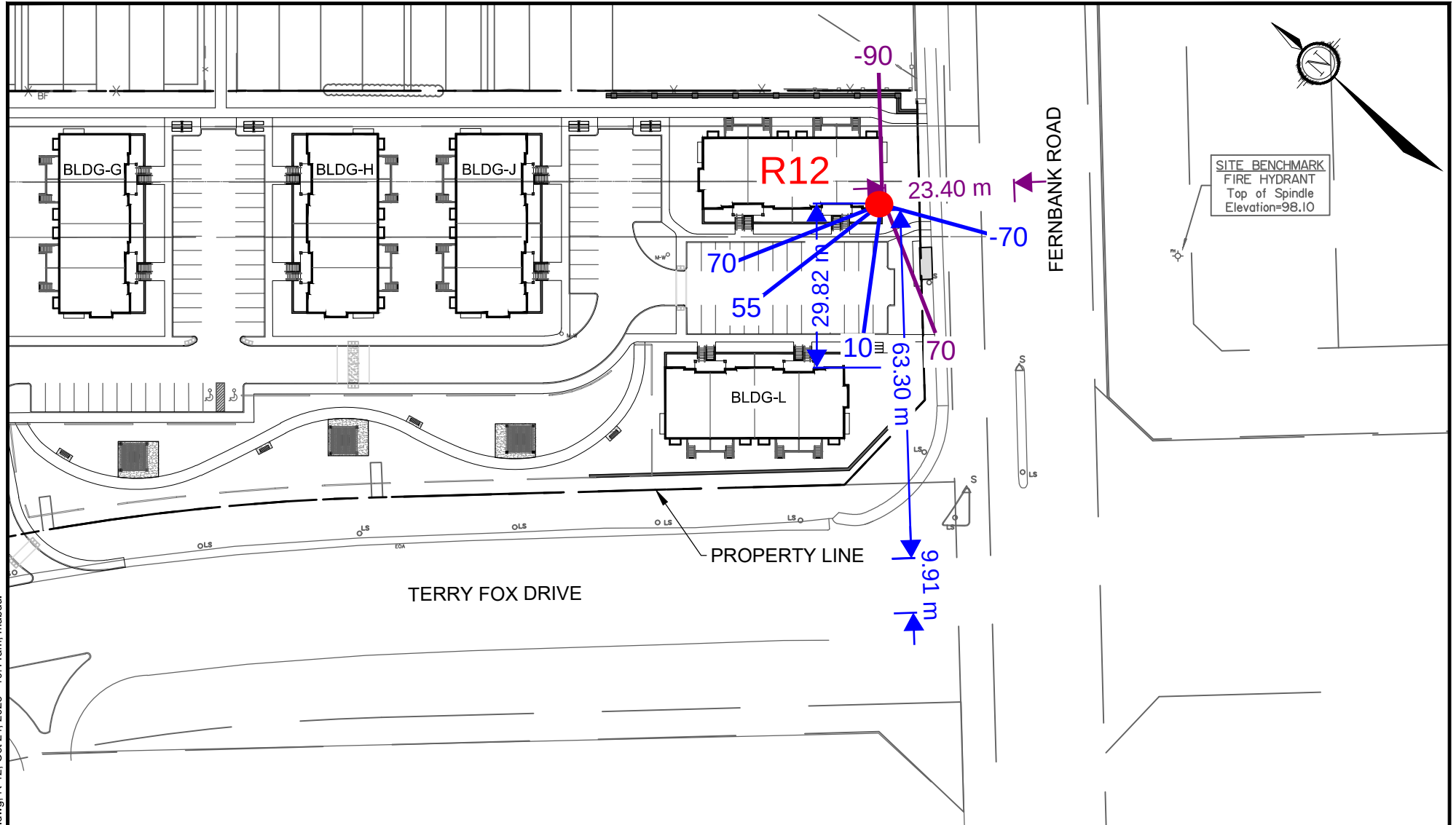
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ANGLES

SCALE 1 : 1000

DATE OCT 2025 JOB 121011 FIGURE FIG-R11



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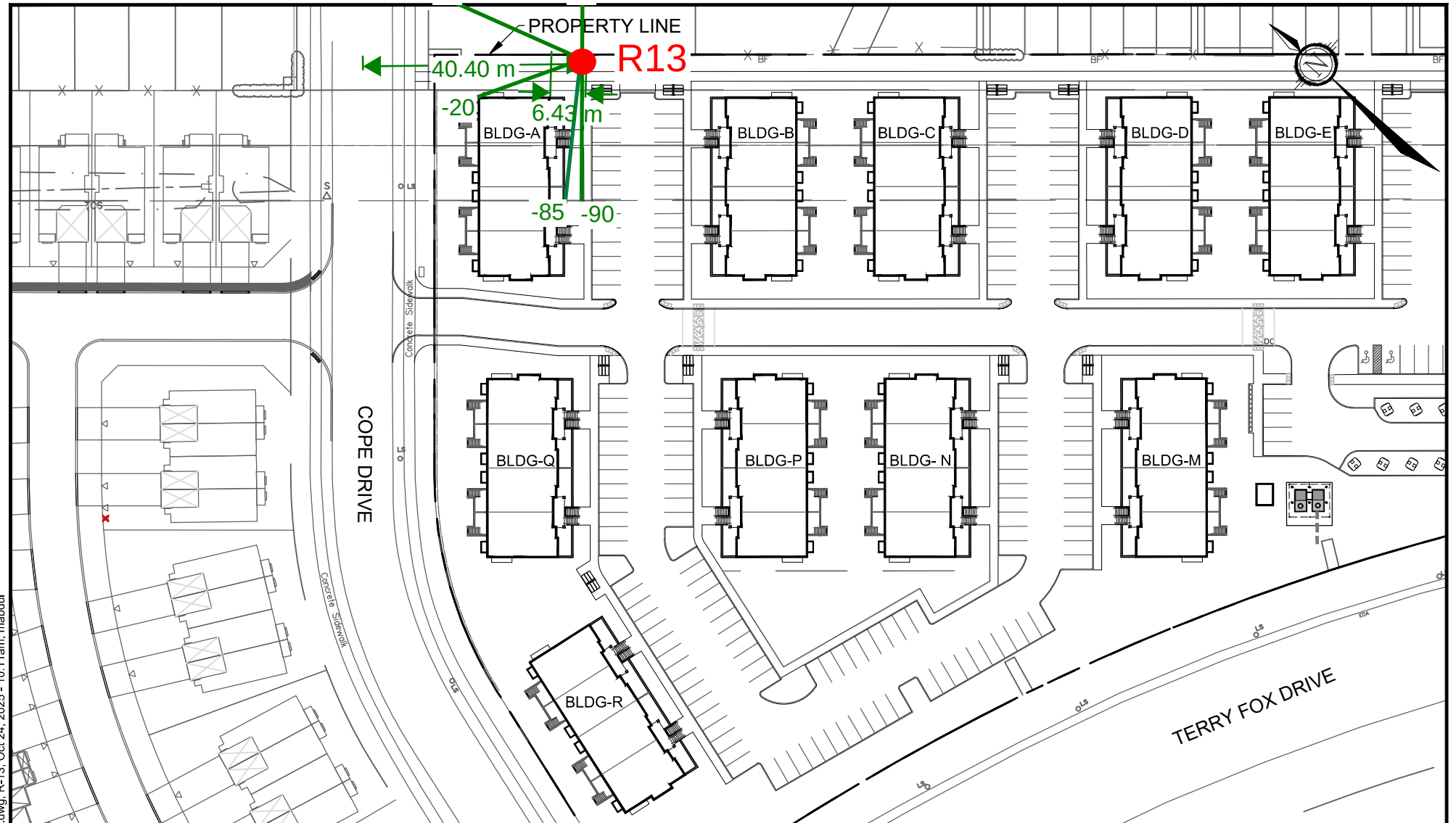
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**RECEIVER DISTANCE AND
ANGLES**

SCALE 1 : 1000

DATE OCT 2025 JOB 121011 FIGURE FIG-R12



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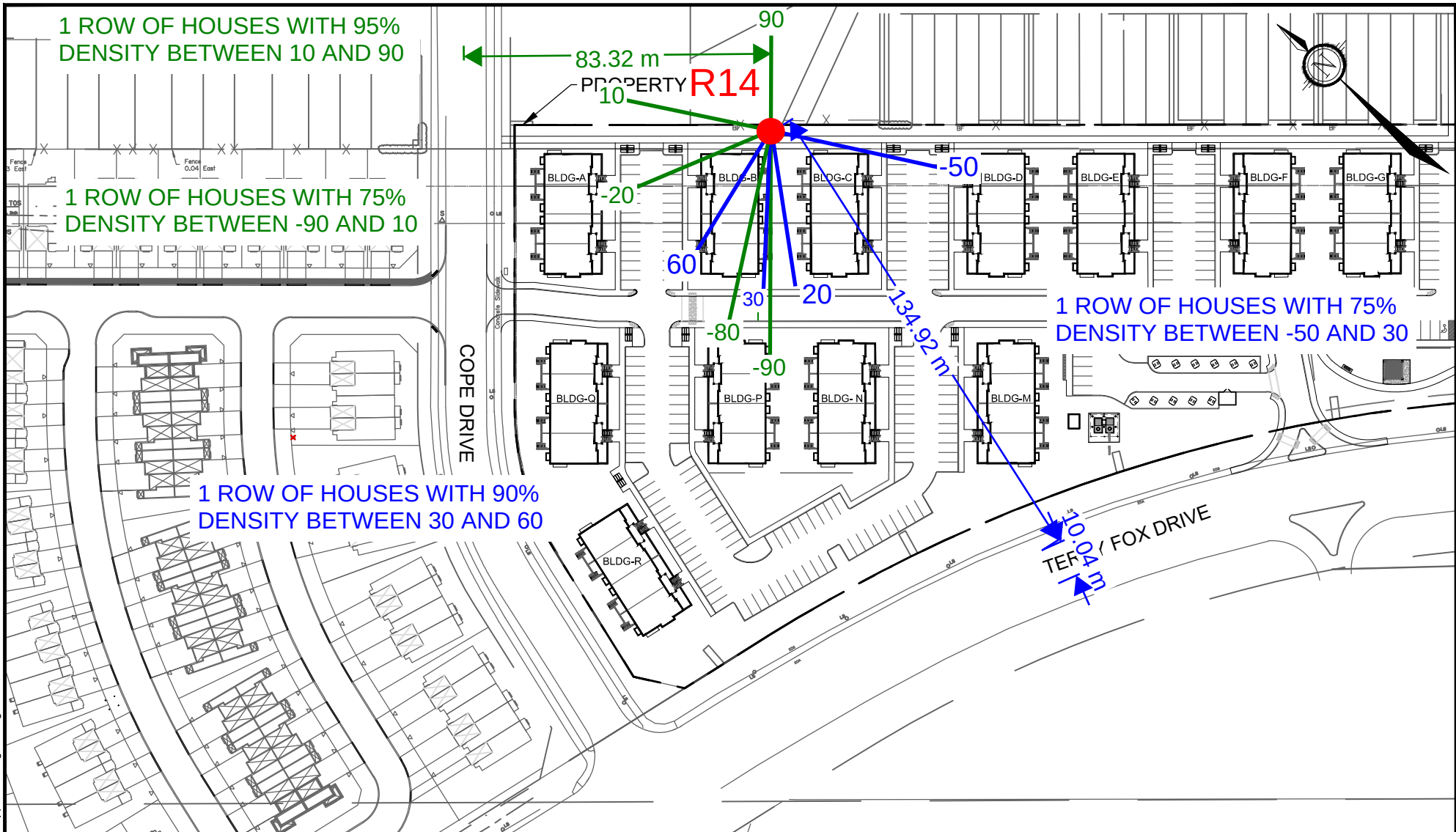
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CITY OF OTTAWA CLARIDGE FERNBANK RECEIVER DISTANCE AND ANGLES

SCALE 1 : 1000

DATE OCT 2025 JOB 121011 FIGURE FIG-R13

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RECEIVER DISTANCE AND
ANGLES

SCALE 1 : 1500 0 15 30 45 60

DATE OCT 2025

JOB 121011

FIGURE FIG-R14

APPENDIX C

Acoustic Insulation Factor Tables

R1 Primary Bedroom/Bedroom 2

TABLE 4: Chart for redistributing AIF requirements to compensate for components whose AIF's deviate from the average required value. Values in the body of the table indicate the percentage of transmitted sound power above (+ve) or below (-ve) the specified average sound power per component

Component AIF minus Average Required AIF	Total No. of Components					
	2	3	4	5	6	
10 or more	-45	-30	-22	-18	-15	Percentage change in total transmitted sound power
9	-44	-29	-22	-18	-15	
8	-42	-28	-21	-17	-14	
7	-40	-27	-20	-16	-13	
6	-37	-25	-19	-15	-12	
5	-34	-23	-17	-14	-10	
4	-30	-20	-15	-12	-11	
3	-25	-17	-12	-10	-8	
2	-18	-12	-9	-7	-6	
1	-10	-7	-5	-4	-3	
0	0	0	0	0	0	
-1	13	9	6	5	4	
-2	29	20	15	12	10	
-3	50	33	25	20	17	
-4	76	50	38	30	25	
-5	108	72	54	43	36	

Worksheet for Table 4 (using Example I)

Outdoor Noise Exposure Forecast _____

Number of components 2

Type of Room Bedroom

Averaged Required AIF 32
(from Table 3)

Component	AIF	AIF Minus Average Required AIF	Increase in Transmitted Sound
Wall	29	-3	50
Window	29	-3	50

Overall increase in total transmitted sound power = N/A
(sum of column above)

R1 Living Room

TABLE 4: Chart for redistributing AIF requirements to compensate for components whose AIF's deviate from the average required value. Values in the body of the table indicate the percentage of transmitted sound power above (+ve) or below (-ve) the specified average sound power per component

Component AIF minus Average Required AIF	Total No. of Components					
	2	3	4	5	6	
10 or more	-45	-30	-22	-18	-15	Percentage change in total transmitted sound power
9	-44	-29	-22	-18	-15	
8	-42	-28	-21	-17	-14	
7	-40	-27	-20	-16	-13	
6	-37	-25	-19	-15	-12	
5	-34	-23	-17	-14	-10	
4	-30	-20	-15	-12	-11	
3	-25	-17	-12	-10	-8	
2	-18	-12	-9	-7	-6	
1	-10	-7	-5	-4	-3	
0	0	0	0	0	0	
-1	13	9	6	5	4	
-2	29	20	15	12	10	
-3	50	33	25	20	17	
-4	76	50	38	30	25	
-5	108	72	54	43	36	

Worksheet for Table 4 (using Example I)

Outdoor Noise Exposure Forecast _____

Number of components 2

Type of Room Living Room

Averaged Required AIF 27
(from Table 3)

Component	AIF	AIF Minus Average Required AIF	Increase in Transmitted Sound
Wall	29	2	-18
Window	29	2	-18

Overall increase in total transmitted sound power = -36
(sum of column above)

R2 Primary Bedroom/Bedroom 2

TABLE 4: Chart for redistributing AIF requirements to compensate for components whose AIF's deviate from the average required value. Values in the body of the table indicate the percentage of transmitted sound power above (+ve) or below (-ve) the specified average sound power per component

Component AIF minus Average Required AIF	Total No. of Components					
	2	3	4	5	6	
10 or more	-45	-30	-22	-18	-15	Percentage change in total transmitted sound power
9	-44	-29	-22	-18	-15	
8	-42	-28	-21	-17	-14	
7	-40	-27	-20	-16	-13	
6	-37	-25	-19	-15	-12	
5	-34	-23	-17	-14	-10	
4	-30	-20	-15	-12	-11	
3	-25	-17	-12	-10	-8	
2	-18	-12	-9	-7	-6	
1	-10	-7	-5	-4	-3	
0	0	0	0	0	0	
-1	13	9	6	5	4	
-2	29	20	15	12	10	
-3	50	33	25	20	17	
-4	76	50	38	30	25	
-5	108	72	54	43	36	

Worksheet for Table 4 (using Example I)

Outdoor Noise Exposure Forecast _____

Number of components 2

Type of Room Bedroom

Averaged Required AIF 28
(from Table 3)

Component	AIF	AIF Minus Average Required AIF	Increase in Transmitted Sound
Wall	24	-4	76
Window	24	-4	76

Overall increase in total transmitted sound power = N/A
(sum of column above)

R2 Living Room

TABLE 4: Chart for redistributing AIF requirements to compensate for components whose AIF's deviate from the average required value. Values in the body of the table indicate the percentage of transmitted sound power above (+ve) or below (-ve) the specified average sound power per component

Component AIF minus Average Required AIF	Total No. of Components					
	2	3	4	5	6	
10 or more	-45	-30	-22	-18	-15	Percentage change in total transmitted sound power
9	-44	-29	-22	-18	-15	
8	-42	-28	-21	-17	-14	
7	-40	-27	-20	-16	-13	
6	-37	-25	-19	-15	-12	
5	-34	-23	-17	-14	-10	
4	-30	-20	-15	-12	-11	
3	-25	-17	-12	-10	-8	
2	-18	-12	-9	-7	-6	
1	-10	-7	-5	-4	-3	
0	0	0	0	0	0	
-1	13	9	6	5	4	
-2	29	20	15	12	10	
-3	50	33	25	20	17	
-4	76	50	38	30	25	
-5	108	72	54	43	36	

Worksheet for Table 4 (using Example I)

Outdoor Noise Exposure Forecast _____

Number of components 2

Type of Room Living Room

Averaged Required AIF 23
(from Table 3)

Component	AIF	AIF Minus Average Required AIF	Increase in Transmitted Sound
Wall	24	1	-10
Window	24	1	-10

Overall increase in total transmitted sound power = -20
(sum of column above)

R3 Primary Bedroom/Bedroom 2

TABLE 4: Chart for redistributing AIF requirements to compensate for components whose AIF's deviate from the average required value. Values in the body of the table indicate the percentage of transmitted sound power above (+ve) or below (-ve) the specified average sound power per component

Component AIF minus Average Required AIF	Total No. of Components					
	2	3	4	5	6	
10 or more	-45	-30	-22	-18	-15	Percentage change in total transmitted sound power
9	-44	-29	-22	-18	-15	
8	-42	-28	-21	-17	-14	
7	-40	-27	-20	-16	-13	
6	-37	-25	-19	-15	-12	
5	-34	-23	-17	-14	-10	
4	-30	-20	-15	-12	-11	
3	-25	-17	-12	-10	-8	
2	-18	-12	-9	-7	-6	
1	-10	-7	-5	-4	-3	
0	0	0	0	0	0	
-1	13	9	6	5	4	
-2	29	20	15	12	10	
-3	50	33	25	20	17	
-4	76	50	38	30	25	
-5	108	72	54	43	36	

Worksheet for Table 4 (using Example I)

Outdoor Noise Exposure Forecast _____

Number of components 2

Type of Room Bedroom

Averaged Required AIF 25
(from Table 3)

Component	AIF	AIF Minus Average Required AIF	Increase in Transmitted Sound
Wall	22	-3	50
Window	22	-3	50

Overall increase in total transmitted sound power = N/A
(sum of column above)

R3 Living Room

TABLE 4: Chart for redistributing AIF requirements to compensate for components whose AIF's deviate from the average required value. Values in the body of the table indicate the percentage of transmitted sound power above (+ve) or below (-ve) the specified average sound power per component

Component AIF minus Average Required AIF	Total No. of Components					
	2	3	4	5	6	
10 or more	-45	-30	-22	-18	-15	Percentage change in total transmitted sound power
9	-44	-29	-22	-18	-15	
8	-42	-28	-21	-17	-14	
7	-40	-27	-20	-16	-13	
6	-37	-25	-19	-15	-12	
5	-34	-23	-17	-14	-10	
4	-30	-20	-15	-12	-11	
3	-25	-17	-12	-10	-8	
2	-18	-12	-9	-7	-6	
1	-10	-7	-5	-4	-3	
0	0	0	0	0	0	
-1	13	9	6	5	4	
-2	29	20	15	12	10	
-3	50	33	25	20	17	
-4	76	50	38	30	25	
-5	108	72	54	43	36	

Worksheet for Table 4 (using Example I)

Outdoor Noise Exposure Forecast _____

Number of components 2

Type of Room Living Room

Averaged Required AIF 23
(from Table 3)

Component	AIF	AIF Minus Average Required AIF	Increase in Transmitted Sound
Wall	22	-1	13
Window	22	-1	13

Overall increase in total transmitted sound power = -N/A
(sum of column above)

R4 Primary Bedroom/Bedroom 2

TABLE 4: Chart for redistributing AIF requirements to compensate for components whose AIF's deviate from the average required value. Values in the body of the table indicate the percentage of transmitted sound power above (+ve) or below (-ve) the specified average sound power per component

Component AIF minus Average Required AIF	Total No. of Components					
	2	3	4	5	6	
10 or more	-45	-30	-22	-18	-15	Percentage change in total transmitted sound power
9	-44	-29	-22	-18	-15	
8	-42	-28	-21	-17	-14	
7	-40	-27	-20	-16	-13	
6	-37	-25	-19	-15	-12	
5	-34	-23	-17	-14	-10	
4	-30	-20	-15	-12	-11	
3	-25	-17	-12	-10	-8	
2	-18	-12	-9	-7	-6	
1	-10	-7	-5	-4	-3	
0	0	0	0	0	0	
-1	13	9	6	5	4	
-2	29	20	15	12	10	
-3	50	33	25	20	17	
-4	76	50	38	30	25	
-5	108	72	54	43	36	

Worksheet for Table 4 (using Example I)

Outdoor Noise Exposure Forecast _____

Number of components 2

Type of Room Bedroom

Averaged Required AIF 30
(from Table 3)

Component	AIF	AIF Minus Average Required AIF	Increase in Transmitted Sound
Wall	27	-3	50
Window	27	-3	50

Overall increase in total transmitted sound power = N/A
(sum of column above)

R4 Living Room

TABLE 4: Chart for redistributing AIF requirements to compensate for components whose AIF's deviate from the average required value. Values in the body of the table indicate the percentage of transmitted sound power above (+ve) or below (-ve) the specified average sound power per component

Component AIF minus Average Required AIF	Total No. of Components					
	2	3	4	5	6	
10 or more	-45	-30	-22	-18	-15	Percentage change in total transmitted sound power
9	-44	-29	-22	-18	-15	
8	-42	-28	-21	-17	-14	
7	-40	-27	-20	-16	-13	
6	-37	-25	-19	-15	-12	
5	-34	-23	-17	-14	-10	
4	-30	-20	-15	-12	-11	
3	-25	-17	-12	-10	-8	
2	-18	-12	-9	-7	-6	
1	-10	-7	-5	-4	-3	
0	0	0	0	0	0	
-1	13	9	6	5	4	
-2	29	20	15	12	10	
-3	50	33	25	20	17	
-4	76	50	38	30	25	
-5	108	72	54	43	36	

Worksheet for Table 4 (using Example I)

Outdoor Noise Exposure Forecast _____

Number of components 2

Type of Room Living Room

Averaged Required AIF 25
(from Table 3)

Component	AIF	AIF Minus Average Required AIF	Increase in Transmitted Sound
Wall	27	2	-18
Window	27	2	-18

Overall increase in total transmitted sound power = -36
(sum of column above)

R5 Primary Bedroom/Bedroom 2

TABLE 4: Chart for redistributing AIF requirements to compensate for components whose AIF's deviate from the average required value. Values in the body of the table indicate the percentage of transmitted sound power above (+ve) or below (-ve) the specified average sound power per component

Component AIF minus Average Required AIF	Total No. of Components					
	2	3	4	5	6	
10 or more	-45	-30	-22	-18	-15	Percentage change in total transmitted sound power
9	-44	-29	-22	-18	-15	
8	-42	-28	-21	-17	-14	
7	-40	-27	-20	-16	-13	
6	-37	-25	-19	-15	-12	
5	-34	-23	-17	-14	-10	
4	-30	-20	-15	-12	-11	
3	-25	-17	-12	-10	-8	
2	-18	-12	-9	-7	-6	
1	-10	-7	-5	-4	-3	
0	0	0	0	0	0	
-1	13	9	6	5	4	
-2	29	20	15	12	10	
-3	50	33	25	20	17	
-4	76	50	38	30	25	
-5	108	72	54	43	36	

Worksheet for Table 4 (using Example I)

Outdoor Noise Exposure Forecast _____

Number of components 2

Type of Room Bedroom

Averaged Required AIF 28
(from Table 3)

Component	AIF	AIF Minus Average Required AIF	Increase in Transmitted Sound
Wall	13	-15	108
Window	13	-15	108

Overall increase in total transmitted sound power = N/A
(sum of column above)

R5 Living Room

TABLE 4: Chart for redistributing AIF requirements to compensate for components whose AIF's deviate from the average required value. Values in the body of the table indicate the percentage of transmitted sound power above (+ve) or below (-ve) the specified average sound power per component

Component AIF minus Average Required AIF	Total No. of Components					
	2	3	4	5	6	
10 or more	-45	-30	-22	-18	-15	Percentage change in total transmitted sound power
9	-44	-29	-22	-18	-15	
8	-42	-28	-21	-17	-14	
7	-40	-27	-20	-16	-13	
6	-37	-25	-19	-15	-12	
5	-34	-23	-17	-14	-10	
4	-30	-20	-15	-12	-11	
3	-25	-17	-12	-10	-8	
2	-18	-12	-9	-7	-6	
1	-10	-7	-5	-4	-3	
0	0	0	0	0	0	
-1	13	9	6	5	4	
-2	29	20	15	12	10	
-3	50	33	25	20	17	
-4	76	50	38	30	25	
-5	108	72	54	43	36	

Worksheet for Table 4 (using Example I)

Outdoor Noise Exposure Forecast _____

Number of components 2

Type of Room Living Room

Averaged Required AIF 23
(from Table 3)

Component	AIF	AIF Minus Average Required AIF	Increase in Transmitted Sound
Wall	13	-10	108
Window	13	-10	108

Overall increase in total transmitted sound power = N/A
(sum of column above)

R6 Primary Bedroom/Bedroom 2

TABLE 4: Chart for redistributing AIF requirements to compensate for components whose AIF's deviate from the average required value. Values in the body of the table indicate the percentage of transmitted sound power above (+ve) or below (-ve) the specified average sound power per component

Component AIF minus Average Required AIF	Total No. of Components					
	2	3	4	5	6	
10 or more	-45	-30	-22	-18	-15	Percentage change in total transmitted sound power
9	-44	-29	-22	-18	-15	
8	-42	-28	-21	-17	-14	
7	-40	-27	-20	-16	-13	
6	-37	-25	-19	-15	-12	
5	-34	-23	-17	-14	-10	
4	-30	-20	-15	-12	-11	
3	-25	-17	-12	-10	-8	
2	-18	-12	-9	-7	-6	
1	-10	-7	-5	-4	-3	
0	0	0	0	0	0	
-1	13	9	6	5	4	
-2	29	20	15	12	10	
-3	50	33	25	20	17	
-4	76	50	38	30	25	
-5	108	72	54	43	36	

Worksheet for Table 4 (using Example I)

Outdoor Noise Exposure Forecast _____

Number of components 2

Type of Room Bedroom

Averaged Required AIF 33
(from Table 3)

Component	AIF	AIF Minus Average Required AIF	Increase in Transmitted Sound
Wall	30	-3	50
Window	30	-3	50

Overall increase in total transmitted sound power = N/A
(sum of column above)

R6 Living Room

TABLE 4: Chart for redistributing AIF requirements to compensate for components whose AIF's deviate from the average required value. Values in the body of the table indicate the percentage of transmitted sound power above (+ve) or below (-ve) the specified average sound power per component

Component AIF minus Average Required AIF	Total No. of Components					
	2	3	4	5	6	
10 or more	-45	-30	-22	-18	-15	Percentage change in total transmitted sound power
9	-44	-29	-22	-18	-15	
8	-42	-28	-21	-17	-14	
7	-40	-27	-20	-16	-13	
6	-37	-25	-19	-15	-12	
5	-34	-23	-17	-14	-10	
4	-30	-20	-15	-12	-11	
3	-25	-17	-12	-10	-8	
2	-18	-12	-9	-7	-6	
1	-10	-7	-5	-4	-3	
0	0	0	0	0	0	
-1	13	9	6	5	4	
-2	29	20	15	12	10	
-3	50	33	25	20	17	
-4	76	50	38	30	25	
-5	108	72	54	43	36	

Worksheet for Table 4 (using Example I)

Outdoor Noise Exposure Forecast _____

Number of components 2

Type of Room Living Room

Averaged Required AIF 28
(from Table 3)

Component	AIF	AIF Minus Average Required AIF	Increase in Transmitted Sound
Wall	27	-1	13
Window	27	-1	13

Overall increase in total transmitted sound power = N/A
(sum of column above)

R7 Primary Bedroom/Bedroom 2

TABLE 4: Chart for redistributing AIF requirements to compensate for components whose AIF's deviate from the average required value. Values in the body of the table indicate the percentage of transmitted sound power above (+ve) or below (-ve) the specified average sound power per component

Component AIF minus Average Required AIF	Total No. of Components					
	2	3	4	5	6	
10 or more	-45	-30	-22	-18	-15	Percentage change in total transmitted sound power
9	-44	-29	-22	-18	-15	
8	-42	-28	-21	-17	-14	
7	-40	-27	-20	-16	-13	
6	-37	-25	-19	-15	-12	
5	-34	-23	-17	-14	-10	
4	-30	-20	-15	-12	-11	
3	-25	-17	-12	-10	-8	
2	-18	-12	-9	-7	-6	
1	-10	-7	-5	-4	-3	
0	0	0	0	0	0	
-1	13	9	6	5	4	
-2	29	20	15	12	10	
-3	50	33	25	20	17	
-4	76	50	38	30	25	
-5	108	72	54	43	36	

Worksheet for Table 4 (using Example I)

Outdoor Noise Exposure Forecast _____

Number of components 2

Type of Room Bedroom

Averaged Required AIF 28
(from Table 3)

Component	AIF	AIF Minus Average Required AIF	Increase in Transmitted Sound
Wall	23	-7	108
Window	23	-7	108

Overall increase in total transmitted sound power = N/A
(sum of column above)

R7 Living Room

TABLE 4: Chart for redistributing AIF requirements to compensate for components whose AIF's deviate from the average required value. Values in the body of the table indicate the percentage of transmitted sound power above (+ve) or below (-ve) the specified average sound power per component

Component AIF minus Average Required AIF	Total No. of Components					
	2	3	4	5	6	
10 or more	-45	-30	-22	-18	-15	Percentage change in total transmitted sound power
9	-44	-29	-22	-18	-15	
8	-42	-28	-21	-17	-14	
7	-40	-27	-20	-16	-13	
6	-37	-25	-19	-15	-12	
5	-34	-23	-17	-14	-10	
4	-30	-20	-15	-12	-11	
3	-25	-17	-12	-10	-8	
2	-18	-12	-9	-7	-6	
1	-10	-7	-5	-4	-3	
0	0	0	0	0	0	
-1	13	9	6	5	4	
-2	29	20	15	12	10	
-3	50	33	25	20	17	
-4	76	50	38	30	25	
-5	108	72	54	43	36	

Worksheet for Table 4 (using Example I)

Outdoor Noise Exposure Forecast _____

Number of components 2

Type of Room Living Room

Averaged Required AIF 23
(from Table 3)

Component	AIF	AIF Minus Average Required AIF	Increase in Transmitted Sound
Wall	23	0	0
Window	23	0	0

Overall increase in total transmitted sound power = N/A
(sum of column above)

R8 Primary Bedroom/Bedroom 2

TABLE 4: Chart for redistributing AIF requirements to compensate for components whose AIF's deviate from the average required value. Values in the body of the table indicate the percentage of transmitted sound power above (+ve) or below (-ve) the specified average sound power per component

Component AIF minus Average Required AIF	Total No. of Components					
	2	3	4	5	6	
10 or more	-45	-30	-22	-18	-15	Percentage change in total transmitted sound power
9	-44	-29	-22	-18	-15	
8	-42	-28	-21	-17	-14	
7	-40	-27	-20	-16	-13	
6	-37	-25	-19	-15	-12	
5	-34	-23	-17	-14	-10	
4	-30	-20	-15	-12	-11	
3	-25	-17	-12	-10	-8	
2	-18	-12	-9	-7	-6	
1	-10	-7	-5	-4	-3	
0	0	0	0	0	0	
-1	13	9	6	5	4	
-2	29	20	15	12	10	
-3	50	33	25	20	17	
-4	76	50	38	30	25	
-5	108	72	54	43	36	

Worksheet for Table 4 (using Example I)

Outdoor Noise Exposure Forecast _____

Number of components 2

Type of Room Bedroom

Averaged Required AIF 28
(from Table 3)

Component	AIF	AIF Minus Average Required AIF	Increase in Transmitted Sound
Wall	25	-3	50
Window	25	-3	50

Overall increase in total transmitted sound power = N/A
(sum of column above)

R8 Living Room

TABLE 4: Chart for redistributing AIF requirements to compensate for components whose AIF's deviate from the average required value. Values in the body of the table indicate the percentage of transmitted sound power above (+ve) or below (-ve) the specified average sound power per component

Component AIF minus Average Required AIF	Total No. of Components					
	2	3	4	5	6	
10 or more	-45	-30	-22	-18	-15	Percentage change in total transmitted sound power
9	-44	-29	-22	-18	-15	
8	-42	-28	-21	-17	-14	
7	-40	-27	-20	-16	-13	
6	-37	-25	-19	-15	-12	
5	-34	-23	-17	-14	-10	
4	-30	-20	-15	-12	-11	
3	-25	-17	-12	-10	-8	
2	-18	-12	-9	-7	-6	
1	-10	-7	-5	-4	-3	
0	0	0	0	0	0	
-1	13	9	6	5	4	
-2	29	20	15	12	10	
-3	50	33	25	20	17	
-4	76	50	38	30	25	
-5	108	72	54	43	36	

Worksheet for Table 4 (using Example I)

Outdoor Noise Exposure Forecast _____

Number of components 2

Type of Room Living Room

Averaged Required AIF 23
(from Table 3)

Component	AIF	AIF Minus Average Required AIF	Increase in Transmitted Sound
Wall	25	2	-18
Window	25	2	-18

Overall increase in total transmitted sound power = -36
(sum of column above)

R9 Primary Bedroom/Bedroom 2

TABLE 4: Chart for redistributing AIF requirements to compensate for components whose AIF's deviate from the average required value. Values in the body of the table indicate the percentage of transmitted sound power above (+ve) or below (-ve) the specified average sound power per component

Component AIF minus Average Required AIF	Total No. of Components					
	2	3	4	5	6	
10 or more	-45	-30	-22	-18	-15	Percentage change in total transmitted sound power
9	-44	-29	-22	-18	-15	
8	-42	-28	-21	-17	-14	
7	-40	-27	-20	-16	-13	
6	-37	-25	-19	-15	-12	
5	-34	-23	-17	-14	-10	
4	-30	-20	-15	-12	-11	
3	-25	-17	-12	-10	-8	
2	-18	-12	-9	-7	-6	
1	-10	-7	-5	-4	-3	
0	0	0	0	0	0	
-1	13	9	6	5	4	
-2	29	20	15	12	10	
-3	50	33	25	20	17	
-4	76	50	38	30	25	
-5	108	72	54	43	36	

Worksheet for Table 4 (using Example I)

Outdoor Noise Exposure Forecast _____

Number of components 2

Type of Room Bedroom

Averaged Required AIF 29
(from Table 3)

Component	AIF	AIF Minus Average Required AIF	Increase in Transmitted Sound
Wall	26	-3	50
Window	26	-3	50

Overall increase in total transmitted sound power = N/A
(sum of column above)

R9 Living Room

TABLE 4: Chart for redistributing AIF requirements to compensate for components whose AIF's deviate from the average required value. Values in the body of the table indicate the percentage of transmitted sound power above (+ve) or below (-ve) the specified average sound power per component

Component AIF minus Average Required AIF	Total No. of Components					
	2	3	4	5	6	
10 or more	-45	-30	-22	-18	-15	Percentage change in total transmitted sound power
9	-44	-29	-22	-18	-15	
8	-42	-28	-21	-17	-14	
7	-40	-27	-20	-16	-13	
6	-37	-25	-19	-15	-12	
5	-34	-23	-17	-14	-10	
4	-30	-20	-15	-12	-11	
3	-25	-17	-12	-10	-8	
2	-18	-12	-9	-7	-6	
1	-10	-7	-5	-4	-3	
0	0	0	0	0	0	
-1	13	9	6	5	4	
-2	29	20	15	12	10	
-3	50	33	25	20	17	
-4	76	50	38	30	25	
-5	108	72	54	43	36	

Worksheet for Table 4 (using Example I)

Outdoor Noise Exposure Forecast _____

Number of components 2

Type of Room Living Room

Averaged Required AIF 24
(from Table 3)

Component	AIF	AIF Minus Average Required AIF	Increase in Transmitted Sound
Wall	26	2	-18
Window	26	2	-18

Overall increase in total transmitted sound power = -36
(sum of column above)

R10 Primary Bedroom/Bedroom 2

TABLE 4: Chart for redistributing AIF requirements to compensate for components whose AIF's deviate from the average required value. Values in the body of the table indicate the percentage of transmitted sound power above (+ve) or below (-ve) the specified average sound power per component

Component AIF minus Average Required AIF	Total No. of Components					
	2	3	4	5	6	
10 or more	-45	-30	-22	-18	-15	Percentage change in total transmitted sound power
9	-44	-29	-22	-18	-15	
8	-42	-28	-21	-17	-14	
7	-40	-27	-20	-16	-13	
6	-37	-25	-19	-15	-12	
5	-34	-23	-17	-14	-10	
4	-30	-20	-15	-12	-11	
3	-25	-17	-12	-10	-8	
2	-18	-12	-9	-7	-6	
1	-10	-7	-5	-4	-3	
0	0	0	0	0	0	
-1	13	9	6	5	4	
-2	29	20	15	12	10	
-3	50	33	25	20	17	
-4	76	50	38	30	25	
-5	108	72	54	43	36	

Worksheet for Table 4 (using Example I)

Outdoor Noise Exposure Forecast _____

Number of components 2

Type of Room Bedroom

Averaged Required AIF 29
(from Table 3)

Component	AIF	AIF Minus Average Required AIF	Increase in Transmitted Sound
Wall	26	-3	50
Window	26	-3	50

Overall increase in total transmitted sound power = N/A
(sum of column above)

R10 Living Room

TABLE 4: Chart for redistributing AIF requirements to compensate for components whose AIF's deviate from the average required value. Values in the body of the table indicate the percentage of transmitted sound power above (+ve) or below (-ve) the specified average sound power per component

Component AIF minus Average Required AIF	Total No. of Components					
	2	3	4	5	6	
10 or more	-45	-30	-22	-18	-15	Percentage change in total transmitted sound power
9	-44	-29	-22	-18	-15	
8	-42	-28	-21	-17	-14	
7	-40	-27	-20	-16	-13	
6	-37	-25	-19	-15	-12	
5	-34	-23	-17	-14	-10	
4	-30	-20	-15	-12	-11	
3	-25	-17	-12	-10	-8	
2	-18	-12	-9	-7	-6	
1	-10	-7	-5	-4	-3	
0	0	0	0	0	0	
-1	13	9	6	5	4	
-2	29	20	15	12	10	
-3	50	33	25	20	17	
-4	76	50	38	30	25	
-5	108	72	54	43	36	

Worksheet for Table 4 (using Example I)

Outdoor Noise Exposure Forecast _____

Number of components 2

Type of Room Living Room

Averaged Required AIF 24
(from Table 3)

Component	AIF	AIF Minus Average Required AIF	Increase in Transmitted Sound
Wall	26	2	-18
Window	26	2	-18

Overall increase in total transmitted sound power = -36
(sum of column above)

R11 Primary Bedroom/Bedroom 2

TABLE 4: Chart for redistributing AIF requirements to compensate for components whose AIF's deviate from the average required value. Values in the body of the table indicate the percentage of transmitted sound power above (+ve) or below (-ve) the specified average sound power per component

Component AIF minus Average Required AIF	Total No. of Components					
	2	3	4	5	6	
10 or more	-45	-30	-22	-18	-15	Percentage change in total transmitted sound power
9	-44	-29	-22	-18	-15	
8	-42	-28	-21	-17	-14	
7	-40	-27	-20	-16	-13	
6	-37	-25	-19	-15	-12	
5	-34	-23	-17	-14	-10	
4	-30	-20	-15	-12	-11	
3	-25	-17	-12	-10	-8	
2	-18	-12	-9	-7	-6	
1	-10	-7	-5	-4	-3	
0	0	0	0	0	0	
-1	13	9	6	5	4	
-2	29	20	15	12	10	
-3	50	33	25	20	17	
-4	76	50	38	30	25	
-5	108	72	54	43	36	

Worksheet for Table 4 (using Example I)

Outdoor Noise Exposure Forecast _____

Number of components 2

Type of Room Bedroom

Averaged Required AIF 35
(from Table 3)

Component	AIF	AIF Minus Average Required AIF	Increase in Transmitted Sound
Wall	32	-3	50
Window	32	-3	50

Overall increase in total transmitted sound power = N/A
(sum of column above)

R11 Living Room

TABLE 4: Chart for redistributing AIF requirements to compensate for components whose AIF's deviate from the average required value. Values in the body of the table indicate the percentage of transmitted sound power above (+ve) or below (-ve) the specified average sound power per component

Component AIF minus Average Required AIF	Total No. of Components					
	2	3	4	5	6	
10 or more	-45	-30	-22	-18	-15	Percentage change in total transmitted sound power
9	-44	-29	-22	-18	-15	
8	-42	-28	-21	-17	-14	
7	-40	-27	-20	-16	-13	
6	-37	-25	-19	-15	-12	
5	-34	-23	-17	-14	-10	
4	-30	-20	-15	-12	-11	
3	-25	-17	-12	-10	-8	
2	-18	-12	-9	-7	-6	
1	-10	-7	-5	-4	-3	
0	0	0	0	0	0	
-1	13	9	6	5	4	
-2	29	20	15	12	10	
-3	50	33	25	20	17	
-4	76	50	38	30	25	
-5	108	72	54	43	36	

Worksheet for Table 4 (using Example I)

Outdoor Noise Exposure Forecast _____

Number of components 2

Type of Room Living Room

Averaged Required AIF 30
(from Table 3)

Component	AIF	AIF Minus Average Required AIF	Increase in Transmitted Sound
Wall	32	2	-18
Window	32	2	-18
.....			
.....			
.....			
.....			
.....			

Overall increase in total transmitted sound power = -36
(sum of column above)

R12 Primary Bedroom/Bedroom 2

TABLE 4: Chart for redistributing AIF requirements to compensate for components whose AIF's deviate from the average required value. Values in the body of the table indicate the percentage of transmitted sound power above (+ve) or below (-ve) the specified average sound power per component

Component AIF minus Average Required AIF	Total No. of Components					
	2	3	4	5	6	
10 or more	-45	-30	-22	-18	-15	Percentage change in total transmitted sound power
9	-44	-29	-22	-18	-15	
8	-42	-28	-21	-17	-14	
7	-40	-27	-20	-16	-13	
6	-37	-25	-19	-15	-12	
5	-34	-23	-17	-14	-10	
4	-30	-20	-15	-12	-11	
3	-25	-17	-12	-10	-8	
2	-18	-12	-9	-7	-6	
1	-10	-7	-5	-4	-3	
0	0	0	0	0	0	
-1	13	9	6	5	4	
-2	29	20	15	12	10	
-3	50	33	25	20	17	
-4	76	50	38	30	25	
-5	108	72	54	43	36	

Worksheet for Table 4 (using Example I)

Outdoor Noise Exposure Forecast _____

Number of components 2

Type of Room Bedroom

Averaged Required AIF 29
(from Table 3)

Component	AIF	AIF Minus Average Required AIF	Increase in Transmitted Sound
Wall	26	-3	50
Window	26	-3	50

Overall increase in total transmitted sound power = N/A
(sum of column above)

R12 Living Room

TABLE 4: Chart for redistributing AIF requirements to compensate for components whose AIF's deviate from the average required value. Values in the body of the table indicate the percentage of transmitted sound power above (+ve) or below (-ve) the specified average sound power per component

Component AIF minus Average Required AIF	Total No. of Components					
	2	3	4	5	6	
10 or more	-45	-30	-22	-18	-15	Percentage change in total transmitted sound power
9	-44	-29	-22	-18	-15	
8	-42	-28	-21	-17	-14	
7	-40	-27	-20	-16	-13	
6	-37	-25	-19	-15	-12	
5	-34	-23	-17	-14	-10	
4	-30	-20	-15	-12	-11	
3	-25	-17	-12	-10	-8	
2	-18	-12	-9	-7	-6	
1	-10	-7	-5	-4	-3	
0	0	0	0	0	0	
-1	13	9	6	5	4	
-2	29	20	15	12	10	
-3	50	33	25	20	17	
-4	76	50	38	30	25	
-5	108	72	54	43	36	

Worksheet for Table 4 (using Example I)

Outdoor Noise Exposure Forecast _____

Number of components 2

Type of Room Living Room

Averaged Required AIF 24
(from Table 3)

Component	AIF	AIF Minus Average Required AIF	Increase in Transmitted Sound
Wall	26	2	-18
Window	26	2	-18

Overall increase in total transmitted sound power = -36
(sum of column above)

Primary Bedroom
Floors 1 & 2
Unit 1, 2, 3, & 4

TABLE 5: Acoustic Insulation Factor for Various Types of Windows

Window area as a percentage of total floor area of room (1)														Single glazing	Double glazing of indicated glass thickness					Triple Glazing	
4	5	6	8	10	13	16	20	25	32	40	50	63	80		2mm and 2mm glass	3mm and 3mm glass	4mm and 4mm glass	3mm and 6mm glass	6mm and 6mm glass	3mm, 3mm and 3mm glass	3mm, 3mm and 6mm glass
Acoustic Insulation Factor (AIF) (2)														Thickness	Interpane spacing in mm (3)					Interpane spacings in mm (5)	
35	34	33	32	31	30	29	28	27	26	25	24	23	22	2mm	6						
36	35	34	33	32	31	30	29	28	27	26	25	24	23		13						
37	36	35	34	33	32	31	30	29	28	27	26	25	24	3mm	15	6					
38	37	36	35	34	33	32	31	30	29	28	27	26	25	3mm, 6mm	10	13	6				
39	38	37	36	35	34	33	32	31	30	29	28	27	26		22	16	13	6	6	6,6	
40	39	38	37	36	35	34	33	32	31	30	29	28	27	9mm (4)	28	20	16	13	13	6,10	6,6
41	40	39	38	37	36	35	34	33	32	31	30	29	28		35	25	20	16	16	6,15	6,10
42	41	40	39	38	37	36	35	34	33	32	31	30	29	12mm (4)	42	32	25	20	20	6,20	6,15
43	42	41	40	39	38	37	36	35	34	33	32	31	30		50	40	32	25	24	6,30	6,20
44	43	42	41	40	39	38	37	36	35	34	33	32	31		63	50	40	32	30	6,40	6,30
45	44	43	42	41	40	39	38	37	36	35	34	33	32		80	63	50	40	37	6,50	6,40
46	45	44	43	42	41	40	39	38	37	36	35	34	33		100	80	63	55	50	6,65	6,50
47	46	45	44	43	42	41	40	39	38	37	36	35	34		125	100	80	75	70	6,80	6,65
48	47	46	45	44	43	42	41	40	39	38	37	36	35		150	125	100	95	90	6,100	6,80
49	48	47	46	45	44	43	42	41	40	39	38	37	36			150	125	110	100		6,100
50	49	48	47	46	45	44	43	42	41	40	39	38	37				150	135	125		

All units except L and M

Unit M

Unit L

Source: National Research Council, Division of Building Research, June 1980.

Explanatory Notes:

- Where the calculated percentage window area is not presented as a column heading, the nearest percentage column in the table values should be used.
- AIF data listed in the table are for well-fitted weatherstripped units that can be opened. The AIF values apply only when the windows are closed. For windows fixed and sealed to the frame, add three (3) to the AIF given in the table.
- If the interpane spacing or glass thickness for a specific double-glazed window is not listed in the table, the nearest listed values should be used.
- The AIF ratings for 9mm and 12mm glass are for laminated glass only; for solid glass subtract two (2) from the AIF values listed in the table.
- If the interpane spacings for a specific triple-glazed window are not listed in the table, use the listed case whose combined spacings are nearest the actual combined spacing.
- The AIF data listed in the table are for typical windows, but details of glass mounting, window seals, etc. may result in slightly different performance for some manufacturers' products. If laboratory sound transmission loss data (conforming to ASTM test method E-90) are available, these should be used to calculate the AIF.

Bedroom 2
Floors 1 & 2
Unit 1, 2, 3, & 4

TABLE 5: Acoustic Insulation Factor for Various Types of Windows

Window area as a percentage of total floor area of room ⁽¹⁾													Single glazing	Double glazing of indicated glass thickness					Triple Glazing	
4	5	6	8	10	13	16	20	25	32	40	50	63	80	2mm and 2mm glass	3mm and 3mm glass	4mm and 4mm glass	3mm and 6mm glass	6mm and 6mm glass	3mm, 3mm and 3mm glass	3mm, 3mm and 6mm glass
Acoustic Insulation Factor (AIF) ⁽²⁾													Thickness	Interpane spacing in mm ⁽³⁾					Interpane spacings in mm ⁽⁵⁾	
35	34	33	32	31	30	29	28	27	26	25	24	23								
36	35	34	33	32	31	30	29	28	27	26	25	24	23	6	13					
37	36	35	34	33	32	31	30	29	28	27	26	25	24	15	6					
38	37	36	35	34	33	32	31	30	29	28	27	26	25	10	13	6				
39	38	37	36	35	34	33	32	31	30	29	28	27	26	22	16	13	6		6, 6	
40	39	38	37	36	35	34	33	32	31	30	29	28	27	28	20	16	13	13	6, 10	6, 6
41	40	39	38	37	36	35	34	33	32	31	30	29	28	35	25	20	16	16	6, 15	6, 10
42	41	40	39	38	37	36	35	34	33	32	31	30	29	42	32	25	20	20	6, 20	6, 15
43	42	41	40	39	38	37	36	35	34	33	32	31	30	50	40	32	25	24	6, 30	6, 20
44	43	42	41	40	39	38	37	36	35	34	33	32	31	63	50	40	32	30	6, 40	6, 30
45	44	43	42	41	40	39	38	37	36	35	34	33	32	80	63	50	40	37	6, 50	6, 40
46	45	44	43	42	41	40	39	38	37	36	35	34	33	100	80	63	55	50	6, 65	6, 50
47	46	45	44	43	42	41	40	39	38	37	36	35	34	125	100	80	75	70	6, 80	6, 65
48	47	46	45	44	43	42	41	40	39	38	37	36	35	150	125	100	95	90	6, 100	6, 80
49	48	47	46	45	44	43	42	41	40	39	38	37	36		150	125	110	100		6, 100
50	49	48	47	46	45	44	43	42	41	40	39	38	37			150	135	125		

Source: National Research Council, Division of Building Research, June 1980.

Explanatory Notes:

- Where the calculated percentage window area is not presented as a column heading, the nearest percentage column in the table values should be used.
- AIF data listed in the table are for well-fitted weatherstripped units that can be opened. The AIF values apply only when the windows are closed. For windows fixed and sealed to the frame, add three (3) to the AIF given in the table.
- If the interpane spacing or glass thickness for a specific double-glazed window is not listed in the table, the nearest listed values should be used.
- The AIF ratings for 9mm and 12mm glass are for laminated glass only; for solid glass subtract two (2) from the AIF values listed in the table.
- If the interpane spacings for a specific triple-glazed window are not listed in the table, use the listed case whose combined spacings are nearest the actual combined spacing.
- The AIF data listed in the table are for typical windows, but details of glass mounting, window seals, etc. may result in slightly different performance for some manufacturers' products. If laboratory sound transmission loss data (conforming to ASTM test method E-90) are available, these should be used to calculate the AIF.

Living Room
Floors 1 & 2
Unit 1, 2, 3, & 4

TABLE 5: Acoustic Insulation Factor for Various Types of Windows

Window area as a percentage of total floor area of room ⁽¹⁾														Single glazing	Double glazing of indicated glass thickness					Triple Glazing	
4	5	6	8	10	13	16	20	25	32	40	50	63	80		2mm and 2mm glass	3mm and 3mm glass	4mm and 4mm glass	3mm and 6mm glass	6mm and 6mm glass	3mm, 3mm and 3mm glass	3mm, 3mm and 6mm glass
Acoustic Insulation Factor (AIF) ⁽²⁾														Thickness	Interpane spacing in mm ⁽³⁾					Interpane spacings in mm ⁽⁵⁾	
35	34	33	32	31	30	29	28	27	26	25	24	23	22	2mm	6						
36	35	34	33	32	31	30	29	28	27	26	25	24	23		13						
37	36	35	34	33	32	31	30	29	28	27	26	25	24	3mm	15	6					
38	37	36	35	34	33	32	31	30	29	28	27	26	25	3mm, 6mm	10	13	6				
39	38	37	36	35	34	33	32	31	30	29	28	27	26		22	16	13	6	6	6,6	
40	39	38	37	36	35	34	33	32	31	30	29	28	27	9mm ⁽⁴⁾	28	20	16	13	13	6,10	6,6
41	40	39	38	37	36	35	34	33	32	31	30	29	28		35	25	20	16	16	6,15	6,10
42	41	40	39	38	37	36	35	34	33	32	31	30	29	12mm ⁽⁴⁾	42	32	25	20	20	6,20	6,15
43	42	41	40	39	38	37	36	35	34	33	32	31	30		50	40	32	25	24	6,30	6,20
44	43	42	41	40	39	38	37	36	35	34	33	32	31		63	50	40	32	30	6,40	
45	44	43	42	41	40	39	38	37	36	35	34	33	32		80	63	50	40	37	6,50	6,40
46	45	44	43	42	41	40	39	38	37	36	35	34	33		100	80	63	55	50	6,65	6,50
47	46	45	44	43	42	41	40	39	38	37	36	35	34		125	100	80	75	70	6,80	6,65
48	47	46	45	44	43	42	41	40	39	38	37	36	35		150	125	100	95	90	6,100	6,80
49	48	47	46	45	44	43	42	41	40	39	38	37	36			150	125	110	100		6,100
50	49	48	47	46	45	44	43	42	41	40	39	38	37				150	135	125		

Source: National Research Council, Division of Building Research, June 1980.

Explanatory Notes:

- Where the calculated percentage window area is not presented as a column heading, the nearest percentage column in the table values should be used.
- AIF data listed in the table are for well-fitted weatherstripped units that can be opened. The AIF values apply only when the windows are closed. For windows fixed and sealed to the frame, add three (3) to the AIF given in the table.
- If the interpane spacing or glass thickness for a specific double-glazed window is not listed in the table, the nearest listed values should be used.
- The AIF ratings for 9mm and 12mm glass are for laminated glass only; for solid glass subtract two (2) from the AIF values listed in the table.
- If the interpane spacings for a specific triple-glazed window are not listed in the table, use the listed case whose combined spacings are nearest the actual combined spacing.
- The AIF data listed in the table are for typical windows, but details of glass mounting, window seals, etc. may result in slightly different performance for some manufacturers' products. If laboratory sound transmission loss data (conforming to ASTM test method E-90) are available, these should be used to calculate the AIF.

Primary Bedroom
Floors 1 & 2
Unit 1 & 4

Table 6.3 - Acoustic Insulation Factor for Various Types of Exterior Wall

	Percentage of exterior wall area to total floor area of room											Type of Exterior Wall
	16	20	25	32	40	50	63	80	100	125	160	
Acoustic Insulation Factor	39	38	37	36	35	34	33	32	31	30	29	EW1
	41	40	39	38	37	36	35	34	33	32	31	EW2
	44	43	42	41	40	39	38	37	36	35	34	EW3
	47	46	45	44	43	42	41	40	39	38	37	EW4
	48	47	46	45	44	43	42	41	40	39	38	EW1R
	49	48	47	46	45	44	43	42	41	40	39	EW2R
	50	49	48	47	46	45	44	43	42	41	40	EW3R
	55	54	53	52	51	50	49	48	47	46	45	EW5
	56	55	54	53	52	51	50	49	48	47	46	EW4R
	58	57	56	55	54	53	52	51	50	49	48	EW6
	59	58	57	56	55	54	53	52	51	50	49	EW7 or EW5R
	63	62	61	60	59	58	57	56	55	54	53	EW8

Source : National Research Council, Division of Building Research, December 1980.

Explanatory Notes :

- 1) Where the calculated percentage wall area is not presented as a column heading, the nearest percentage column in the table should be used.
- 2) The common structure of walls EW1 to EW5 is composed of 12.7 mm gypsum board, vapour barrier, and 38 x 89 mm studs with 50 mm (or thicker) mineral wool or glass fibre batts in inter-stud cavities.
- 3) EW1 denotes exterior wall as in Note 2), plus sheathing, plus wood siding or metal siding and fibre backer board.
EW2 denotes exterior wall as in Note 2), plus rigid insulation (25-30 mm), and wood siding or metal siding and fibre backer board.
EW3 denotes simulated mansard with structure as in Note 2), plus sheathing, 28 x 89 mm framing, sheathing, and asphalt roofing material.
EW4 denotes exterior wall as in Note 2), plus sheathing and 20 mm stucco.
EW5 denotes exterior wall as in Note 2), plus sheathing, 25 mm air space, 100 mm brick veneer.
EW6 denotes exterior wall composed of 12.7 mm gypsum board, rigid insulation (25-50 mm), 100 mm back-up block, 100 mm face brick.
EW7 denotes exterior wall composed of 12.7 mm gypsum board, rigid insulation (25-50 mm), 140 mm back-up block, 100 mm face brick.
EW8 denotes exterior wall composed of 12.7 mm gypsum board, rigid insulation (25-50 mm), 200 mm concrete.
- 4) R signifies the mounting of the interior gypsum board on resilient clips.
- 5) An exterior wall conforming to rainscreen design principles and composed of 12.7 mm gypsum board, 100 mm concrete block, rigid insulation (25-50 mm), 25 mm air space, and 100 mm brick veneer has the same AIF as EW6.
- 6) An exterior wall described in EW1 with the addition of rigid insulation (25-50 mm) between the sheathing and the external finish has the same AIF as EW2.

Primary Bedroom
Floors 1 & 2
Unit 2 & 3

Table 6.3 - Acoustic Insulation Factor for Various Types of Exterior Wall

Percentage of exterior wall area to total floor area of room												Type of Exterior Wall
16	20	25	32	40	50	63	80	100	125	160		
				32								
Acoustic	39	38	37	36	35	34	33	32	31	30	29	EW1
Insulation	41	40	39	38	37	36	35	34	33	32	31	EW2
Factor	44	43	42	41	40	39	38	37	36	35	34	EW3
	47	46	45	44	43	42	41	40	39	38	37	EW4
	48	47	46	45	44	43	42	41	40	39	38	EW1R
	49	48	47	46	45	44	43	42	41	40	39	EW2R
	50	49	48	47	46	45	44	43	42	41	40	EW3R
	55	54	53	52	51	50	49	48	47	46	45	EW5
	56	55	54	53	52	51	50	49	48	47	46	EW4R
	58	57	56	55	54	53	52	51	50	49	48	EW6
	59	58	57	56	55	54	53	52	51	50	49	EW7 or EW5R
	63	62	61	60	59	58	57	56	55	54	53	EW8

Source : National Research Council, Division of Building Research, December 1980.

Explanatory Notes :

- 1) Where the calculated percentage wall area is not presented as a column heading, the nearest percentage column in the table should be used.
- 2) The common structure of walls EW1 to EW5 is composed of 12.7 mm gypsum board, vapour barrier, and 38 x 89 mm studs with 50 mm (or thicker) mineral wool or glass fibre batts in inter-stud cavities.
- 3) EW1 denotes exterior wall as in Note 2), plus sheathing, plus wood siding or metal siding and fibre backer board.
EW2 denotes exterior wall as in Note 2), plus rigid insulation (25-30 mm), and wood siding or metal siding and fibre backer board.
EW3 denotes simulated mansard with structure as in Note 2), plus sheathing, 28 x 89 mm framing, sheathing, and asphalt roofing material.
EW4 denotes exterior wall as in Note 2), plus sheathing and 20 mm stucco.
EW5 denotes exterior wall as in Note 2), plus sheathing, 25 mm air space, 100 mm brick veneer.
EW6 denotes exterior wall composed of 12.7 mm gypsum board, rigid insulation (25-50 mm), 100 mm back-up block, 100 mm face brick.
EW7 denotes exterior wall composed of 12.7 mm gypsum board, rigid insulation (25-50 mm), 140 mm back-up block, 100 mm face brick.
EW8 denotes exterior wall composed of 12.7 mm gypsum board, rigid insulation (25-50 mm), 200 mm concrete.
- 4) R signifies the mounting of the interior gypsum board on resilient clips.
- 5) An exterior wall conforming to rainscreen design principles and composed of 12.7 mm gypsum board, 100 mm concrete block, rigid insulation (25-50 mm), 25 mm air space, and 100 mm brick veneer has the same AIF as EW6.
- 6) An exterior wall described in EW1 with the addition of rigid insulation (25-50 mm) between the sheathing and the external finish has the same AIF as EW2.

Bedroom 2
Floors 1 & 2
Unit 1 & 4

Table 6.3 - Acoustic Insulation Factor for Various Types of Exterior Wall

	Percentage of exterior wall area to total floor area of room											Type of Exterior Wall
	16	20	25	32	40	50	63	80	100	125	160	
Acoustic Insulation Factor	39	38	37	36	35	34	33	32	31	30	29	EW1
	41	40	39	38	37	36	35	34	33	32	31	EW2
	44	43	42	41	40	39	38	37	36	35	34	EW3
	47	46	45	44	43	42	41	40	39	38	37	EW4
	48	47	46	45	44	43	42	41	40	39	38	EW1R
	49	48	47	46	45	44	43	42	41	40	39	EW2R
	50	49	48	47	46	45	44	43	42	41	40	EW3R
	55	54	53	52	51	50	49	48	47	46	45	EW5
	56	55	54	53	52	51	50	49	48	47	46	EW4R
	58	57	56	55	54	53	52	51	50	49	48	EW6
	59	58	57	56	55	54	53	52	51	50	49	EW7 or EW5R
	63	62	61	60	59	58	57	56	55	54	53	EW8

For all units except "L"
Unit "L" only

Source : National Research Council, Division of Building Research, December 1980.

Explanatory Notes :

- 1) Where the calculated percentage wall area is not presented as a column heading, the nearest percentage column in the table should be used.
- 2) The common structure of walls EW1 to EW5 is composed of 12.7 mm gypsum board, vapour barrier, and 38 x 89 mm studs with 50 mm (or thicker) mineral wool or glass fibre batts in inter-stud cavities.
- 3) EW1 denotes exterior wall as in Note 2), plus sheathing, plus wood siding or metal siding and fibre backer board.
EW2 denotes exterior wall as in Note 2), plus rigid insulation (25-30 mm), and wood siding or metal siding and fibre backer board.
EW3 denotes simulated mansard with structure as in Note 2), plus sheathing, 28 x 89 mm framing, sheathing, and asphalt roofing material.
EW4 denotes exterior wall as in Note 2), plus sheathing and 20 mm stucco.
EW5 denotes exterior wall as in Note 2), plus sheathing, 25 mm air space, 100 mm brick veneer.
EW6 denotes exterior wall composed of 12.7 mm gypsum board, rigid insulation (25-50 mm), 100 mm back-up block, 100 mm face brick.
EW7 denotes exterior wall composed of 12.7 mm gypsum board, rigid insulation (25-50 mm), 140 mm back-up block, 100 mm face brick.
EW8 denotes exterior wall composed of 12.7 mm gypsum board, rigid insulation (25-50 mm), 200 mm concrete.
- 4) R signifies the mounting of the interior gypsum board on resilient clips.
- 5) An exterior wall conforming to rainscreen design principles and composed of 12.7 mm gypsum board, 100 mm concrete block, rigid insulation (25-50 mm), 25 mm air space, and 100 mm brick veneer has the same AIF as EW6.
- 6) An exterior wall described in EW1 with the addition of rigid insulation (25-50 mm) between the sheathing and the external finish has the same AIF as EW2.

Bedroom 2
Floors 1 & 2
Unit 2 & 3

Table 6.3 - Acoustic Insulation Factor for Various Types of Exterior Wall

	Percentage of exterior wall area to total floor area of room											Type of Exterior Wall
	16	20	25	32	40	50	63	80	100	125	160	
Acoustic Insulation Factor	39	38	37	36	35	34	33	32	31	30	29	EW1
	41	40	39	38	37	36	35	34	33	32	31	EW2
	44	43	42	41	40	39	38	37	36	35	34	EW3
	47	46	45	44	43	42	41	40	39	38	37	EW4
	48	47	46	45	44	43	42	41	40	39	38	EW1R
	49	48	47	46	45	44	43	42	41	40	39	EW2R
	50	49	48	47	46	45	44	43	42	41	40	EW3R
	55	54	53	52	51	50	49	48	47	46	45	EW5
	56	55	54	53	52	51	50	49	48	47	46	EW4R
	58	57	56	55	54	53	52	51	50	49	48	EW6
	59	58	57	56	55	54	53	52	51	50	49	EW7 or EW5R
	63	62	61	60	59	58	57	56	55	54	53	EW8

Source : National Research Council, Division of Building Research, December 1980.

Explanatory Notes :

- 1) Where the calculated percentage wall area is not presented as a column heading, the nearest percentage column in the table should be used.
- 2) The common structure of walls EW1 to EW5 is composed of 12.7 mm gypsum board, vapour barrier, and 38 x 89 mm studs with 50 mm (or thicker) mineral wool or glass fibre batts in inter-stud cavities.
- 3) EW1 denotes exterior wall as in Note 2), plus sheathing, plus wood siding or metal siding and fibre backer board.
EW2 denotes exterior wall as in Note 2), plus rigid insulation (25-30 mm), and wood siding or metal siding and fibre backer board.
EW3 denotes simulated mansard with structure as in Note 2), plus sheathing, 28 x 89 mm framing, sheathing, and asphalt roofing material.
EW4 denotes exterior wall as in Note 2), plus sheathing and 20 mm stucco.
EW5 denotes exterior wall as in Note 2), plus sheathing, 25 mm air space, 100 mm brick veneer.
EW6 denotes exterior wall composed of 12.7 mm gypsum board, rigid insulation (25-50 mm), 100 mm back-up block, 100 mm face brick.
EW7 denotes exterior wall composed of 12.7 mm gypsum board, rigid insulation (25-50 mm), 140 mm back-up block, 100 mm face brick.
EW8 denotes exterior wall composed of 12.7 mm gypsum board, rigid insulation (25-50 mm), 200 mm concrete.
- 4) R signifies the mounting of the interior gypsum board on resilient clips.
- 5) An exterior wall conforming to rainscreen design principles and composed of 12.7 mm gypsum board, 100 mm concrete block, rigid insulation (25-50 mm), 25 mm air space, and 100 mm brick veneer has the same AIF as EW6.
- 6) An exterior wall described in EW1 with the addition of rigid insulation (25-50 mm) between the sheathing and the external finish has the same AIF as EW2.

Living Room
Floors 1 & 2
Unit 1, 2, 3, & 4

Table 6.3 - Acoustic Insulation Factor for Various Types of Exterior Wall

Percentage of exterior wall area to total floor area of room												Type of Exterior Wall
16	20	25	32	40	50	63	80	100	125	160		
			32									
Acoustic	39	38	37	36	35	34	33	32	31	30	29	EW1
Insulation	41	40	39	38	37	36	35	34	33	32	31	EW2
Factor	44	43	42	41	40	39	38	37	36	35	34	EW3
	47	46	45	44	43	42	41	40	39	38	37	EW4
	48	47	46	45	44	43	42	41	40	39	38	EW1R
	49	48	47	46	45	44	43	42	41	40	39	EW2R
	50	49	48	47	46	45	44	43	42	41	40	EW3R
	55	54	53	52	51	50	49	48	47	46	45	EW5
	56	55	54	53	52	51	50	49	48	47	46	EW4R
	58	57	56	55	54	53	52	51	50	49	48	EW6
	59	58	57	56	55	54	53	52	51	50	49	EW7 or EW5R
	63	62	61	60	59	58	57	56	55	54	53	EW8

Source : National Research Council, Division of Building Research, December 1980.

Explanatory Notes :

- 1) Where the calculated percentage wall area is not presented as a column heading, the nearest percentage column in the table should be used.
- 2) The common structure of walls EW1 to EW5 is composed of 12.7 mm gypsum board, vapour barrier, and 38 x 89 mm studs with 50 mm (or thicker) mineral wool or glass fibre batts in inter-stud cavities.
- 3) EW1 denotes exterior wall as in Note 2), plus sheathing, plus wood siding or metal siding and fibre backer board.
EW2 denotes exterior wall as in Note 2), plus rigid insulation (25-30 mm), and wood siding or metal siding and fibre backer board.
EW3 denotes simulated mansard with structure as in Note 2), plus sheathing, 28 x 89 mm framing, sheathing, and asphalt roofing material.
EW4 denotes exterior wall as in Note 2), plus sheathing and 20 mm stucco.
EW5 denotes exterior wall as in Note 2), plus sheathing, 25 mm air space, 100 mm brick veneer.
EW6 denotes exterior wall composed of 12.7 mm gypsum board, rigid insulation (25-50 mm), 100 mm back-up block, 100 mm face brick.
EW7 denotes exterior wall composed of 12.7 mm gypsum board, rigid insulation (25-50 mm), 140 mm back-up block, 100 mm face brick.
EW8 denotes exterior wall composed of 12.7 mm gypsum board, rigid insulation (25-50 mm), 200 mm concrete.
- 4) R signifies the mounting of the interior gypsum board on resilient clips.
- 5) An exterior wall conforming to rainscreen design principles and composed of 12.7 mm gypsum board, 100 mm concrete block, rigid insulation (25-50 mm), 25 mm air space, and 100 mm brick veneer has the same AIF as EW6.
- 6) An exterior wall described in EW1 with the addition of rigid insulation (25-50 mm) between the sheathing and the external finish has the same AIF as EW2.

R1
Primary Bedroom
Floors 1 & 2
Unit 1, 2, 3, & 4

TABLE 11: Approximate conversion from STC to AIF for windows and doors:

Window (or door) area expressed as percentage of room floor area	Acoustic Insulation Factor (AIF)
80	STC-5
63	STC-4
50	STC-3
40	STC-2
32	STC-1
25	STC
20	STC+1
16	STC+2
12.5	STC+3
10	STC+4
8	STC+5
6.3	STC+6
5	STC+7
4	STC+8

Note: For area percentages not listed in the table use the nearest listed value.

Examples: For a window whose area = 20% of the room floor area and STC = 32 the AIF is 32 + 1 = 33.

AIF = STC-2

For a window whose area = 60% of the room floor area and STC = 29 the AIF is 29 - 4 = 25.

AIF

Daytime/Nighttime

STC

Daytime/Nighttime

R1 = 29/27	R1 = 31/29
R2 = 24/21	R2 = 26/23
R3 = 22/19	R3 = 24/21
R4 = 27/24	R4 = 29/26
R5 = 13/10	R5 = 15/12
R6 = 30/28	R6 = 32/30
R7 = 23/21	R7 = 25/23
R8 = 25/23	R8 = 27/25
R9 = 26/23	R9 = 28/25
R10 = 26/24	R10 = 28/26
R11 = 32/29	R11 = 34/31
R12 = 27/25	R12 = 29/27

R1
Bedroom 2
Floors 1 & 2
Unit 1, 2, 3, & 4

TABLE 11: Approximate conversion from STC to AIF for windows and doors:

Window (or door) area expressed as percentage of room floor area	Acoustic Insulation Factor (AIF)
80	STC-5
63	STC-4
50	STC-3
40	STC-2
32	STC-1
25	STC
20	STC+1
16	STC+2
12.5	STC+3
10	STC+4
8	STC+5
6.3	STC+6
5	STC+7
4	STC+8

Note: For area percentages not listed in the table use the nearest listed value.

Examples: For a window whose area = 20% of the room floor area and STC = 32 the AIF is $32 + 1 = 33$.

AIF = STC+2

For a window whose area = 60% of the room floor area and STC = 29 the AIF is $29 - 4 = 25$.

Daytime/Nighttime Daytime/Nighttime

R1 = 29/27	R1 = 27/25
R2 = 24/21	R2 = 22/19
R3 = 22/19	R3 = 20/17
R4 = 27/24	R4 = 25/22
R5 = 13/10	R5 = 11/8
R6 = 30/28	R6 = 28/26
R7 = 23/21	R7 = 21/19
R8 = 25/23	R8 = 23/21
R9 = 26/23	R9 = 24/21
R10 = 26/24	R10 = 24/22
R11 = 32/29	R11 = 30/27
R12 = 27/25	R12 = 25/23

R1
Living Room
Floors 1 & 2
Unit 1, 2, 3, & 4

TABLE 11: Approximate conversion from STC to AIF for windows and doors:

Window (or door) area expressed as percentage of room floor area	Acoustic Insulation Factor (AIF)
80	STC-5
63	STC-4
50	STC-3
40	STC-2
32	STC-1
25	STC
20	STC+1
16	STC+2
12.5	STC+3
10	STC+4
8	STC+5
6.3	STC+6
5	STC+7
4	STC+8

Note: For area percentages not listed in the table use the nearest listed value.

Examples: For a window whose area = 20% of the room floor area and STC = 32 the AIF is $32 + 1 = 33$.

AIF = STC-1

For a window whose area = 60% of the room floor area and STC = 29 the AIF is $29 - 4 = 25$.

Daytime/Nighttime Daytime/Nighttime

R1 = 29/27	R1 = 30/28
R2 = 24/21	R2 = 25/22
R3 = 22/19	R3 = 23/20
R4 = 27/24	R4 = 28/25
R5 = 13/10	R5 = 14/11
R6 = 30/28	R6 = 31/29
R7 = 23/21	R7 = 24/22
R8 = 25/23	R8 = 26/24
R9 = 26/23	R9 = 27/24
R10 = 26/24	R10 = 27/25
R11 = 32/29	R11 = 33/30
R12 = 27/25	R12 = 28/26

Primary Bedroom
Floors 1 & 2
Unit 1 & 4

TABLE 12: Approximate conversion from STC to AIF for exterior walls:

Exterior wall area expressed as percentage of room floor area	Acoustic Insulation Factor (AIF)
200	STC-10
160	STC-9
125	STC-8
100	STC-7
80	STC-6
63	STC-5
50	STC-4
40	STC-3
32	STC-2
25	STC-1
20	STC
16	STC+1
12.5	STC+2
10	STC+3
8	

Note: For area percentages not listed in the table use the nearest listed value.

Example: For a wall whose area = 120% of room floor area and STC = 48 the AIF is $48 - 8 = 40$.

$$\text{AIF} = \text{STC} - 8$$

AIF
Daytime/Nighttime

STC
Daytime/Nighttime

R1 = 29/27

R1 = 37/35

R2 = 24/21

R2 = 32/29

R3 = 22/19

R3 = 30/27

R4 = 27/24

R4 = 35/32

R5 = 13/10

R5 = 21/18

R6 = 30/28

R6 = 38/36

R7 = 23/21

R7 = 31/29

R8 = 25/23

R8 = 33/31

R9 = 26/23

R9 = 34/31

R10 = 26/24

R10 = 34/32

R11 = 32/29

R11 = 40/37

R12 = 27/25

R12 = 35/33

Primary Bedroom
Floors 1 & 2
Unit 2 & 3

TABLE 12: Approximate conversion from STC to AIF for exterior walls:

Exterior wall area expressed as percentage of room floor area	Acoustic Insulation Factor (AIF)
200	STC-10
160	STC-9
125	STC-8
100	STC-7
80	STC-6
63	STC-5
50	STC-4
40	STC-3
32	STC-2
25	STC-1
20	STC
16	STC+1
12.5	STC+2
10	STC+3
8	

Note: For area percentages not listed in the table use the nearest listed value.

Example: For a wall whose area = 120% of room floor area and STC = 48 the AIF is $48 - 8 = 40$.

$$\text{AIF} = \text{STC} - 3$$

AIF Daytime/Nighttime	STC Daytime/Nighttime
R1 = 29/27	R1 = 32/30
R2 = 24/21	R2 = 27/24
R3 = 22/19	R3 = 25/22
R4 = 27/24	R4 = 30/27
R5 = 13/10	R5 = 16/13
R6 = 30/28	R6 = 33/31
R7 = 23/21	R7 = 26/24
R8 = 25/23	R8 = 28/26
R9 = 26/23	R9 = 29/26
R10 = 26/24	R10 = 29/27
R11 = 32/29	R11 = 35/32
R12 = 27/25	R12 = 30/28

Bedroom 2
Floors 1 & 2
Unit 1 & 4

TABLE 12: Approximate conversion from STC to AIF for exterior walls:

Exterior wall area expressed as percentage of room floor area	Acoustic Insulation Factor (AIF)
200	STC-10
160	STC-9
125	STC-8
100	STC-7
80	STC-6
63	STC-5
50	STC-4
40	STC-3
32	STC-2
25	STC-1
20	STC
16	STC+1
12.5	STC+2
10	STC+3
8	

Note: For area percentages not listed in the table use the nearest listed value.

Example: For a wall whose area = 120% of room floor area and STC = 48 the AIF is $48 - 8 = 40$.

$$\text{AIF} = \text{STC} - 9$$

AIF Daytime/Nighttime	STC Daytime/Nighttime
R1 = 29/27	R1 = 38/36
R2 = 24/21	R2 = 33/30
R3 = 22/19	R3 = 29/27
R4 = 27/24	R4 = 36/33
R5 = 13/10	R5 = 22/19
R6 = 30/28	R6 = 39/30
R7 = 23/21	R7 = 32/30
R8 = 25/23	R8 = 34/32
R9 = 26/23	R9 = 35/32
R10 = 26/24	R10 = 35/33
R11 = 32/29	R11 = 41/38
R12 = 27/25	R12 = 36/34

Bedroom 2
Floors 1 & 2
Unit 2 & 3

TABLE 12: Approximate conversion from STC to AIF for exterior walls:

Exterior wall area expressed as percentage of room floor area	Acoustic Insulation Factor (AIF)
200	STC-10
160	STC-9
125	STC-8
100	STC-7
80	STC-6
63	STC-5
50	STC-4
40	STC-3
32	STC-2
25	STC-1
20	STC
16	STC+1
12.5	STC+2
10	STC+3
8	

Note: For area percentages not listed in the table use the nearest listed value.

Example: For a wall whose area = 120% of room floor area and STC = 48 the AIF is $48 - 8 = 40$.

AIF = STC-6

AIF	STC
Daytime/Nighttime	Daytime/Nighttime

R1 = 29/27	R1 = 35/33
R2 = 24/21	R2 = 30/27
R3 = 22/19	R3 = 28/25
R4 = 27/24	R4 = 33/30
R5 = 13/10	R5 = 19/16
R6 = 30/28	R6 = 36/34
R7 = 23/21	R7 = 29/27
R8 = 25/23	R8 = 31/29
R9 = 26/23	R9 = 32/29
R10 = 26/24	R10 = 32/29
R11 = 32/29	R11 = 38/35
R12 = 27/25	R12 = 33/31

Living Room
Floors 1 & 2
Unit 1, 2, 3, & 4

TABLE 12: Approximate conversion from STC to AIF for exterior walls:

Exterior wall area expressed as percentage of room floor area	Acoustic Insulation Factor (AIF)
200	STC-10
160	STC-9
125	STC-8
100	STC-7
80	STC-6
63	STC-5
50	STC-4
40	STC-3
32	STC-2
25	STC-1
20	STC
16	STC+1
12.5	STC+2
10	STC+3
8	

Note: For area percentages not listed in the table use the nearest listed value.

Example: For a wall whose area = 120% of room floor area and STC = 48 the AIF is $48 - 8 = 40$.

$$\text{AIF} = \text{STC} - 2$$

AIF	STC
Daytime/Nighttime	Daytime/Nighttime

R1 = 29/27	R1 = 31/27
R2 = 24/21	R2 = 26/23
R3 = 22/19	R3 = 24/21
R4 = 27/24	R4 = 29/26
R5 = 13/10	R5 = 15/12
R6 = 30/28	R6 = 32/30
R7 = 23/21	R7 = 25/23
R8 = 25/23	R8 = 27/25
R9 = 26/23	R9 = 28/25
R10 = 26/24	R10 = 28/26
R11 = 32/29	R11 = 34/31
R12 = 27/25	R12 = 29/27

APPENDIX D

Architectural Drawings & Correspondence

From: Steve Zorgel
Sent: Tuesday, May 25, 2021 1:53 PM
To: Steve Zorgel
Subject: FW: Hydro Pole Anchors - 5331 Fernbank

From: Colleen McKeracher <cmckeracher@rlaarchitecture.ca>
Sent: Thursday, May 6, 2021 6:14 PM
To: Drew Blair <D.Blair@novatech-eng.com>
Subject: RE: Hydro Pole Anchors - 5331 Fernbank

Hi Drew,

At Bridlewood we required a few windows with an STC not less than 31, and being around the same neighbourhood and facing the same road as this project I would expect a similar requirement and hope we wouldn't need higher than that. We don't typically specify an STC performance for our woodframe buildings, but the base products would be around the 27 STC range, although the shop drawings we receive for these often don't carry that information. Our walls themselves are around a max of 37 STC (for the Hardie board and siding, the brick will perform better) our problem being finding a tested assembly that fits our wall types exactly.

Colleen McKeracher *M.Arch, OAA*
Architect
RLA/ Architecture
Tel: 613.724.9932 x 316

From: Drew Blair <D.Blair@novatech-eng.com>
Sent: May 6, 2021 11:45 AM
To: Colleen McKeracher <cmckeracher@rlaarchitecture.ca>
Subject: RE: Hydro Pole Anchors - 5331 Fernbank

Thanks Colleen,

Early question but do you have typical STC window values? Do you have a range that you use? Is there a maximum you'd like to stay below? We have our noise study to perform but I'm curious about what architect's would normally prescribe.

Thanks,

Drew

Drew Blair, P.Eng., Project Manager | Land Development Engineering

NOVATECH Engineers, Planners & Landscape Architects

240 Michael Cowpland Drive, Suite 200, Ottawa, ON, K2M 1P6 | Tel: 613.254.9643 x 236 | Fax: 613.254.5867

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ZEN - SPRATT ROAD

4624 Spratt Road, Ottawa, Ontario

RLA PROJECT #: 2033



Revision Spc

Date 1

ARCHITECTURAL

RLA ARCHITECTURE
56 BEECH ST
OTTAWA, ON K1S 3J6
613-724-9932

ARCHITECTURAL	
Sheet Number	Sheet Name

ELECTRICAL

COMPANY NAME
ADDRESS
CITY POSTAL CODE
PHONE NUMBER

ELECTRICAL	
Sheet Number	Sheet Name
E001	SHEET TITLE

MECHANICAL

COMPANY NAME
ADDRESS
CITY POSTAL CODE
PHONE NUMBER

MECHANICAL	
Sheet Number	Sheet Name
M.01	SHEET TITLE

STRUCTURAL

COMPANY NAME
ADDRESS
CITY POSTAL CODE
PHONE NUMBER

STRUCTURAL	
Sheet Number	Sheet Name
S001	SHEET TITLE

CIVIL

COMPANY NAME
ADDRESS
CITY POSTAL CODE
PHONE NUMBER

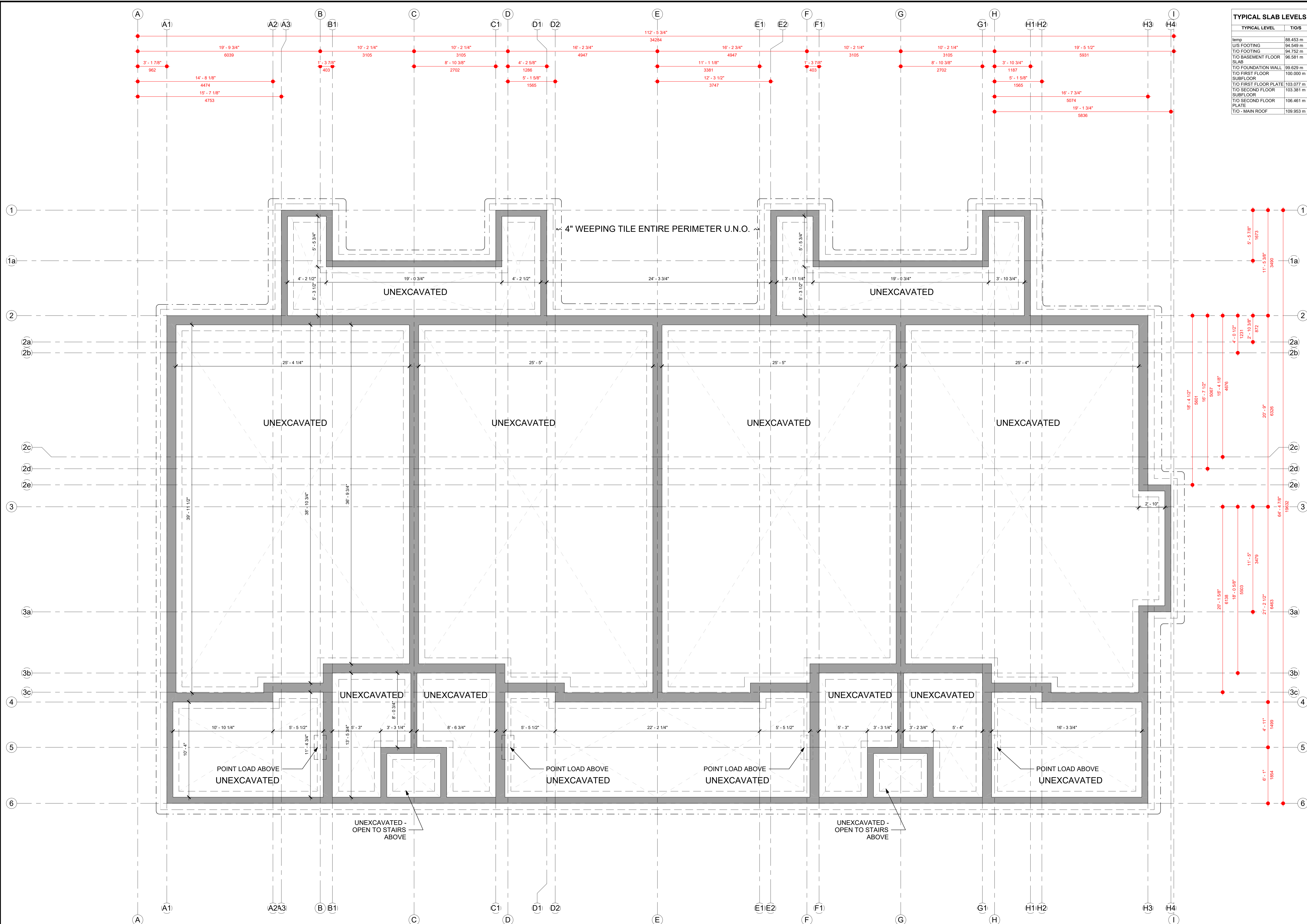
CIVIL	
Sheet Number	Sheet Name
EC-1	EROSION CONTROL PLAN
EX-1	EXISTING CONDITIONS PLAN
GP-1	GRADING PLAN
SSP-1	SITE SERVICING PLAN
SWM-1	STORMWATER MANAGEMENT PLAN

LANDSCAPE

COMPANY NAME
ADDRESS
CITY POSTAL CODE
PHONE NUMBER

LANDSCAPE	
Sheet Number	Sheet Name
L001	SHEET TITLE





TYPICAL SLAB LEVELS	
TYPICAL LEVEL	T/O/S
temp	88.453 m
U/S FOOTING	94.549 m
T/O FOOTING	94.732 m
T/O BASEMENT FLOOR SLAB	96.581 m
T/O FOUNDATION WALL	99.629 m
T/O FIRST FLOOR SUBFLOOR	100.000 m
T/O FIRST FLOOR PLATE	103.077 m
T/O SECOND FLOOR SUBFLOOR	103.381 m
T/O SECOND FLOOR PLATE	106.461 m
T/O - MAIN ROOF	109.953 m

IT IS THE RESPONSIBILITY OF THE APPROPRIATE CONTRACTOR TO CHECK AND VERIFY ALL DIMENSIONS ON SITE AND TO REPORT ALL ERRORS AND/OR OMISSIONS TO THE ARCHITECT.

ALL CONTRACTORS MUST COMPLY WITH ALL PERTINENT CODES AND BY-LAWS.

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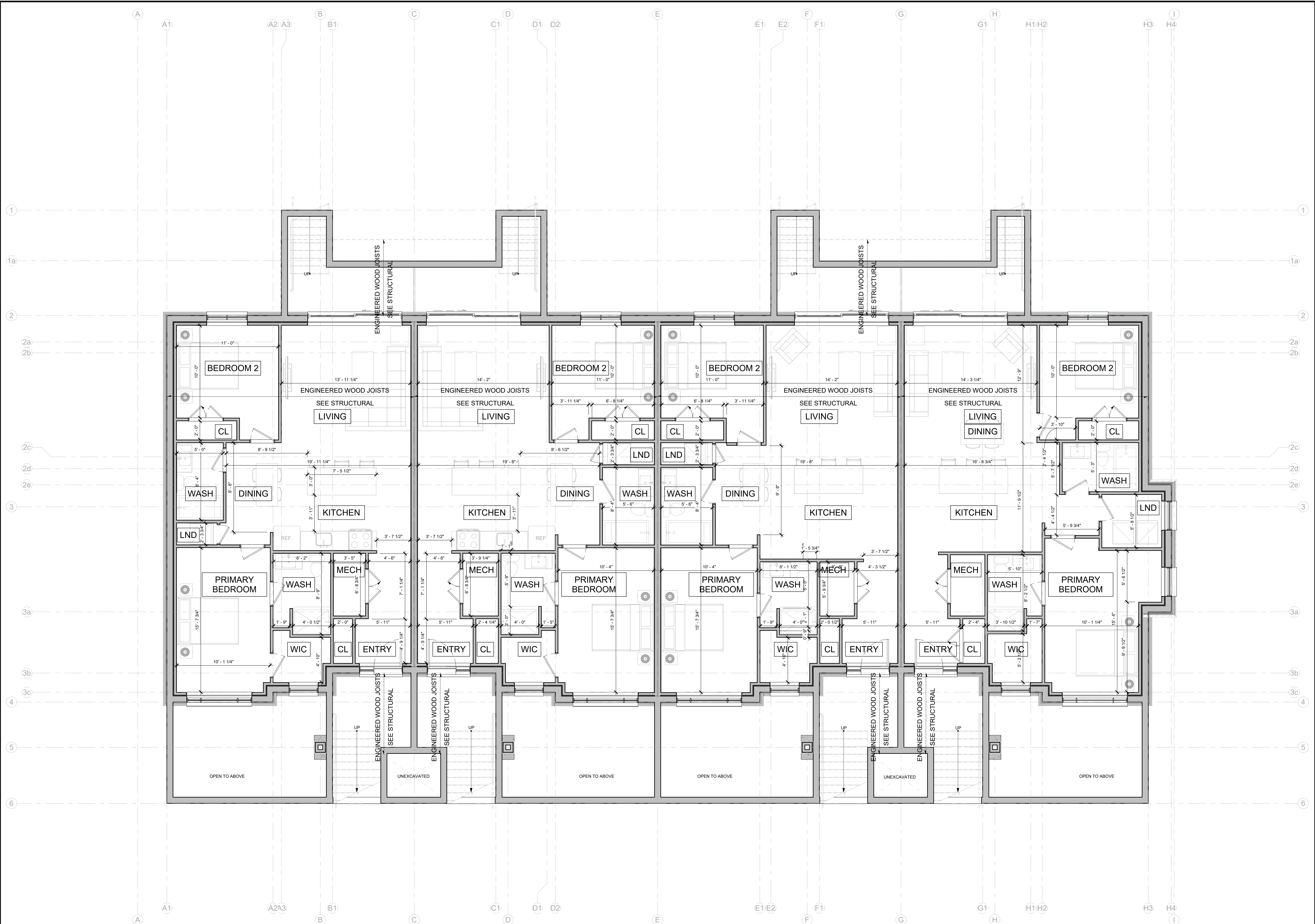
GENERAL NOTES FOR SLAB EDGE DRAWINGS.

- ALL COLUMNS & SHEAR WALLS ARE ALIGNED w/ GRID LINES EITHER AT THEIR FACE OR AT THEIR CENTRE LINES UNLESS DIMENSIONED OTHERWISE.
- VERIFY THE SIZE OF ALL STRUCTURAL ELEMENTS INCLUDING COLUMNS, BEAMS, AND WALLS WITH STRUCTURAL DRAWINGS. REPORT TO THE ARCHITECT AND THE STRUCTURAL ENGINEER ANY INCONSISTENCIES. THE CONTRACTOR SHALL NOT PROCEED WITH THE WORK AFFECTED UNTIL THE CONTRACTOR HAS RECEIVED CORRECTED OR ADDITIONAL INFORMATION FROM THE ARCHITECT AND THE STRUCTURAL ENGINEER.
- ELEVATION MARKS INDICATE ELEVATION IN METRES OR CHANGE IN ELEVATION FROM LEVEL IN MILLIMETRES.

NOT FOR CONSTRUCTION

No. DESCRIPTION YYYY-MM-DD	
REVISIONS:	
ARCHITECT SEAL:	NORTH ARROW: TRUE NORTH
CLIENT: 	
ARCHITECT: rla/architecture 56 Beech Street, Ottawa, Ontario K1S 3J6 t.613.724.9932 f.613.724.1209 www.rodericklahey.ca	
PROJECT TITLE: ZEN - SPRATT ROAD 4624 Spratt Road, Ottawa, Ontario	
SHEET TITLE: FOUNDATION PLAN	
DRAWN: Author	CHECKED: Checker
SCALE: As indicated	SHEET No: A101
PROJECT No: 2033	

1 FOUNDATION PLAN
A101 1:50



1 BASEMENT FLOOR PLAN
A151 1:50

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- 3 HOUR REQ'D FIRE RESISTANCE RATING
- 2 HOUR REQ'D FIRE RESISTANCE RATING
- 1.5 HOUR REQ'D FIRE RESISTANCE RATING
- 1 HOUR REQ'D FIRE RESISTANCE RATING
- 0 HOUR REQ'D FIRE RESISTANCE RATING

NOT FOR CONSTRUCTION

No.	DESCRIPTION	YYYY-MM-DD
REVISIONS:		

ARCHITECT SEAL:

NORTH ARROW:

TRUE NORTH

CLIENT:

CLARIDGE
HOMES

ARCHITECT:

rla/architecture
56 Beech Street, Ottawa, Ontario K1S 3J6
t.613.724.9932 f.613.724.1209 www.rodericklahey.ca

PROJECT TITLE:

ZEN - SPRATT ROAD

4624 Spratt Road, Ottawa, Ontario

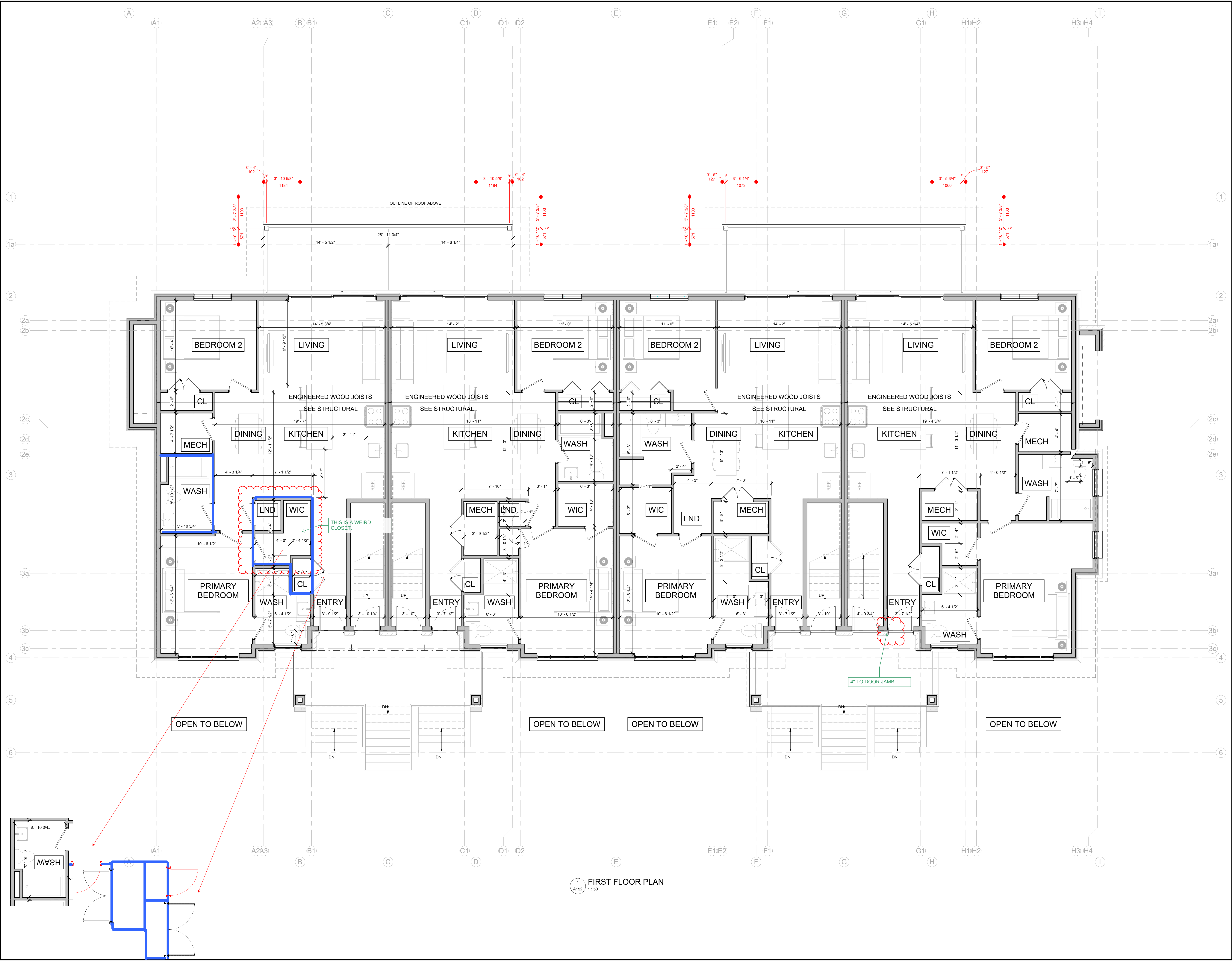
SHEET TITLE:

BASEMENT FLOOR PLAN

DRAWN: Author	CHECKED: Checker
SCALE: As indicated	SHEET No:
PROJECT No: 2033	A151

PLOT DATE: 2025-09-10 4:39:02 PM

PAPER SIZE: ISO Full Bleed B1 (707.00 x 1000.00mm)



IT IS THE RESPONSIBILITY OF THE APPROPRIATE CONTRACTOR TO CHECK AND VERIFY ALL DIMENSIONS ON SITE AND TO REPORT ALL ERRORS AND/OR OMISSIONS TO THE ARCHITECT.

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No.	DESCRIPTION	YYYY-MM-DD
REVISIONS:		

ARCHITECT SEAL:

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ARCHITECT:

rla/architecture
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PROJECT TITLE:

ZEN - SPRATT ROAD

4624 Spratt Road, Ottawa, Ontario

SHEET TITLE:

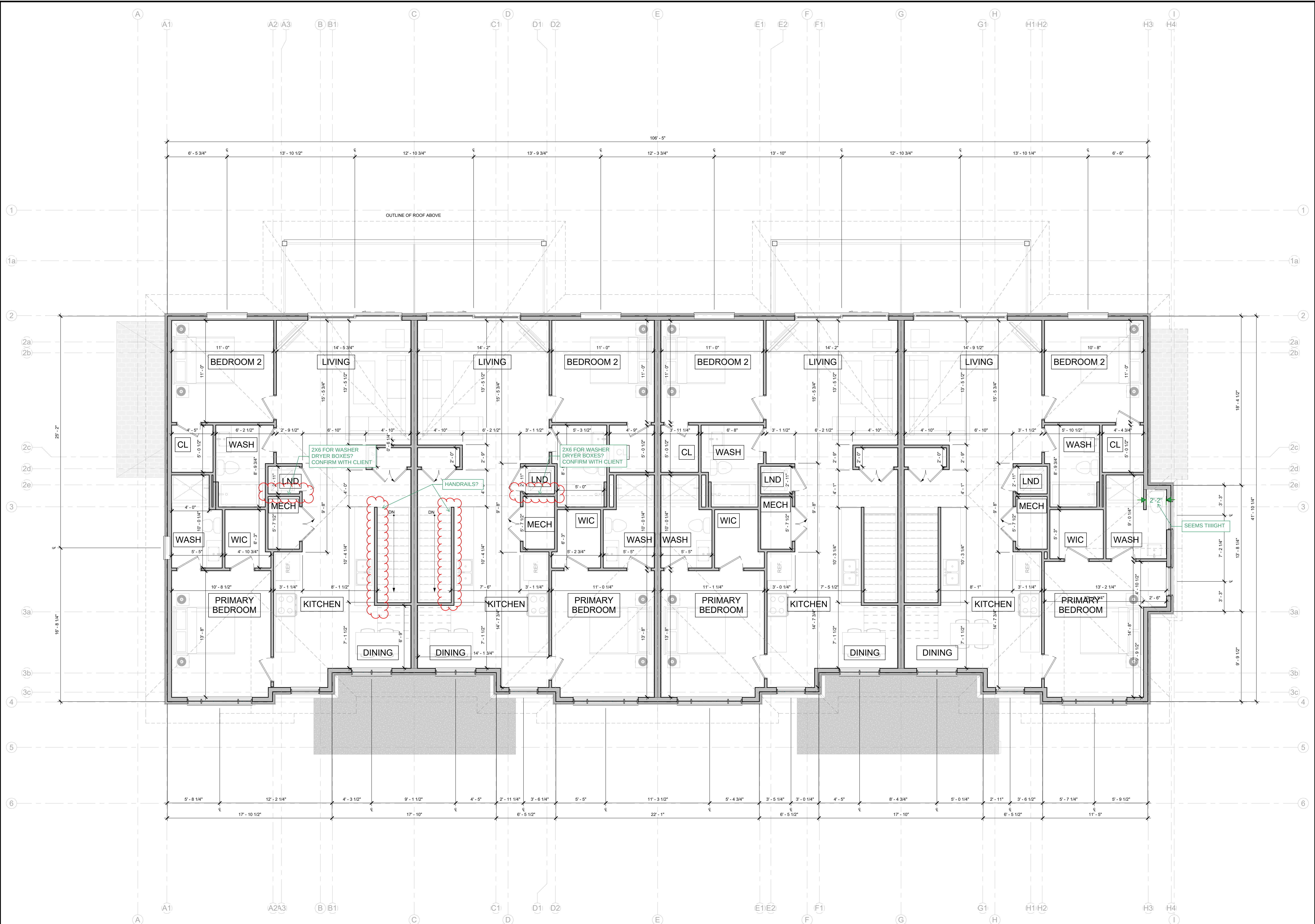
FIRST FLOOR PLAN

DRAWN: Author	CHECKED: Checker
SCALE: 1 : 50	SHEET No:
PROJECT No: 2033	A152

PLOT DATE: 2025-09-10 4:39:03 PM

PAPER SIZE: ISO Full Bleed B1 (702.00 x 1000.00mm)

DDP-12-17-0171



1 SECOND FLOOR PLAN
A153 1:50

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No.	DESCRIPTION	YYYY-MM-DD

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PROJECT TITLE:

ZEN - SPRATT ROAD

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SHEET TITLE:

SECOND FLOOR PLAN

DRAWN: Author	CHECKED: Checker
SCALE: 1 : 50	SHEET No:
PROJECT No: 2033	A153

NOT FOR CONSTRUCTION

No.	DESCRIPTION	YYYY-MM-DD
REVISIONS:		

ARCHITECT SEAL:	NORTH ARROW:
	 TRUE NORTH

ARCHITECT:

rla / architecture

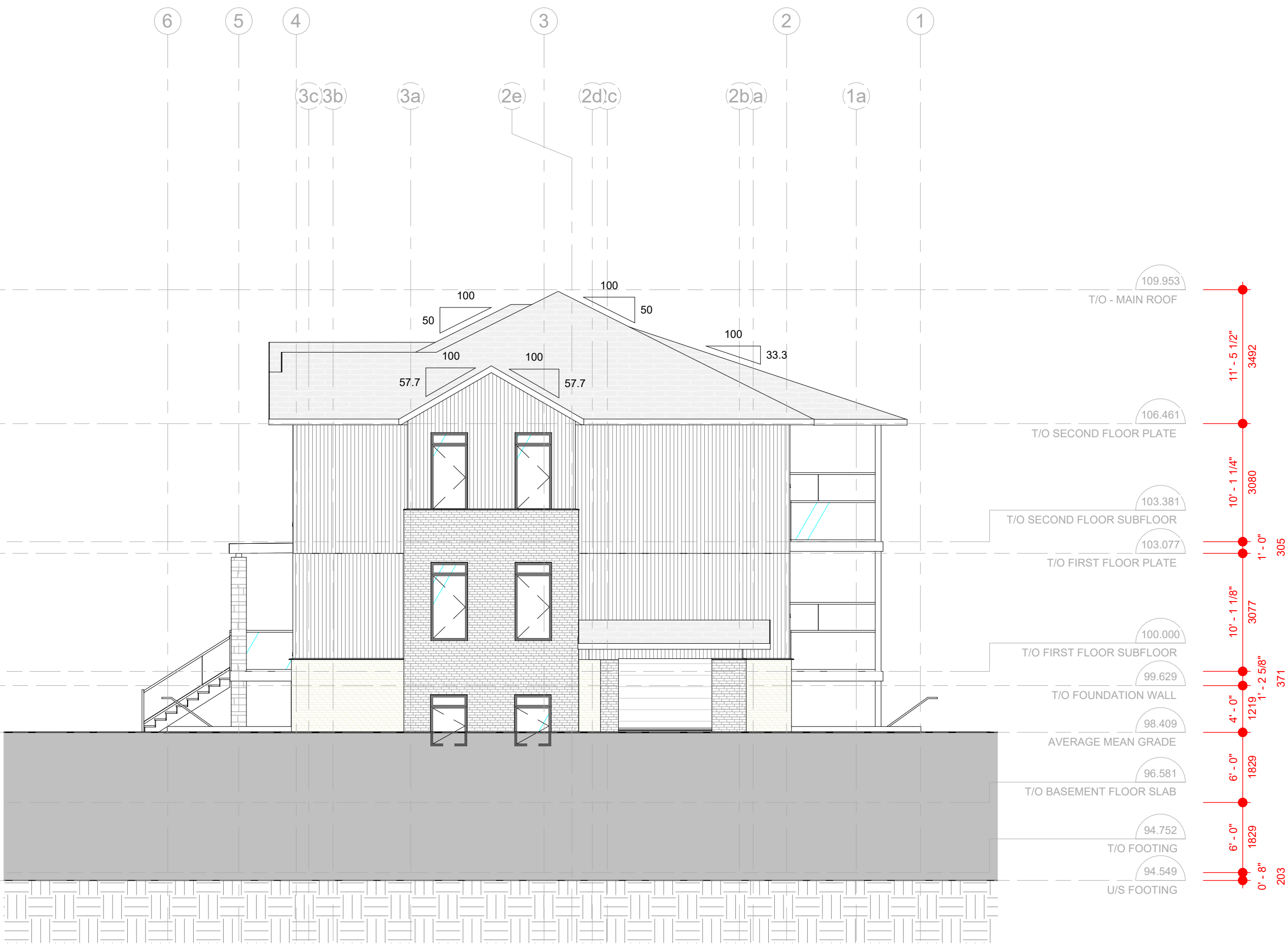
56 Beech Street, Ottawa, Ontario K1S 3J6
t.613.724.9932 f.613.724.1209 www.rodericklahey.ca

ROOF PLAN

DRAWN: Author	CHECKED: Checker
SCALE: 1 : 50	SHEET No: A154
PROJECT No: 2033	



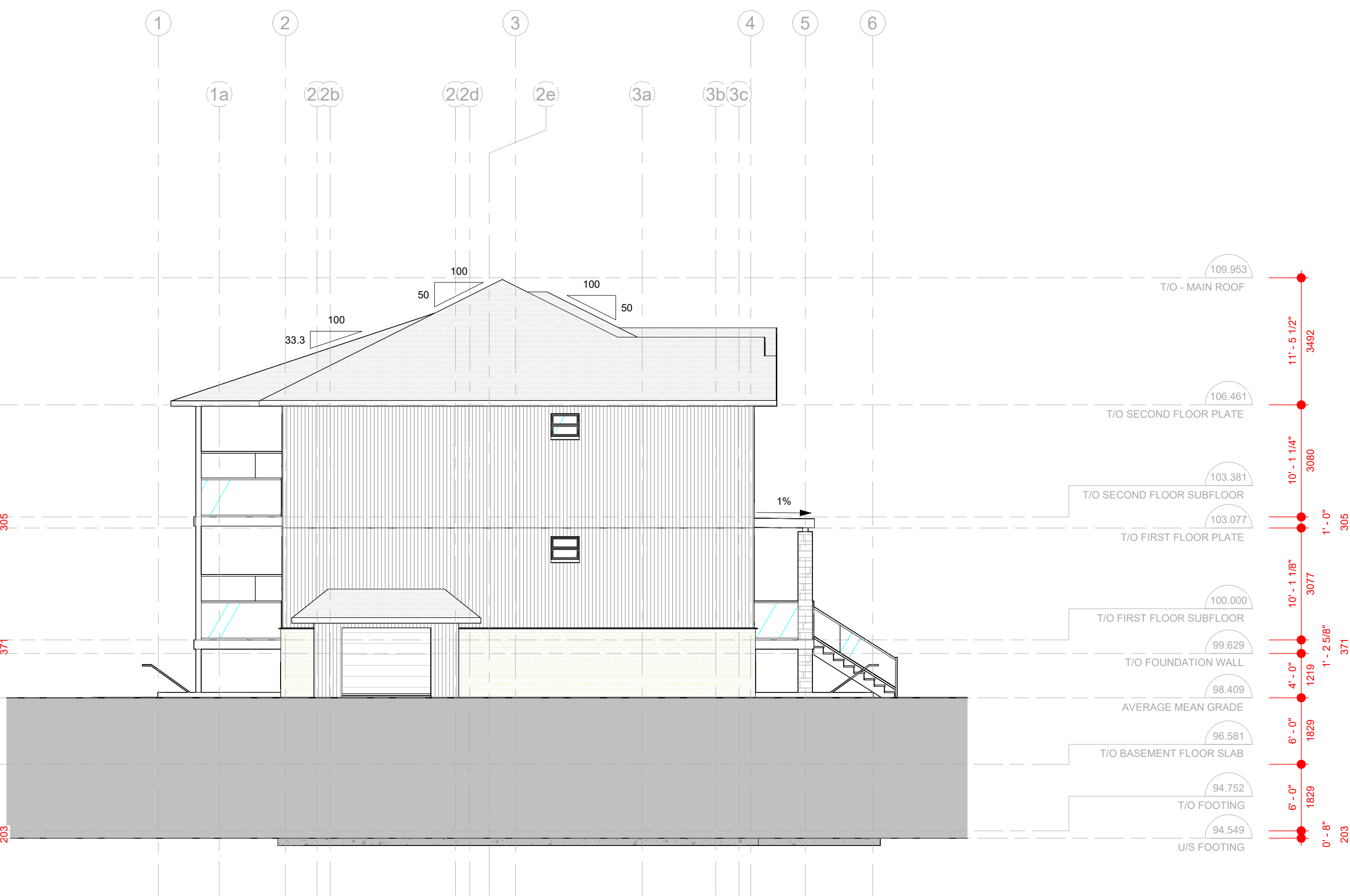
1 NORTH ELEVATION
A201 1:100



2 EAST ELEVATION
A201 1:100



3 SOUTH ELEVATION
A201 1:100



4 WEST ELEVATION
A201 1:100

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OPERABLE GLAZING

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No.	DESCRIPTION	YYYY-MM-DD
REVISIONS:		

ARCHITECT SEAL:

NORTH ARROW:

TRUE NORTH

CLIENT:

CLARIDGE
HOMES

ARCHITECT:

r/a architecture
56 Beech Street, Ottawa, Ontario K1S 3J6
t.613.724.9932 f.613.724.1209 www.roderricklahey.ca

PROJECT TITLE:

ZEN - SPRATT ROAD

4624 Spratt Road, Ottawa, Ontario

SHEET TITLE:

ELEVATIONS

DRAWN:
Author

CHECKED:
Checker

SCALE:
As indicated

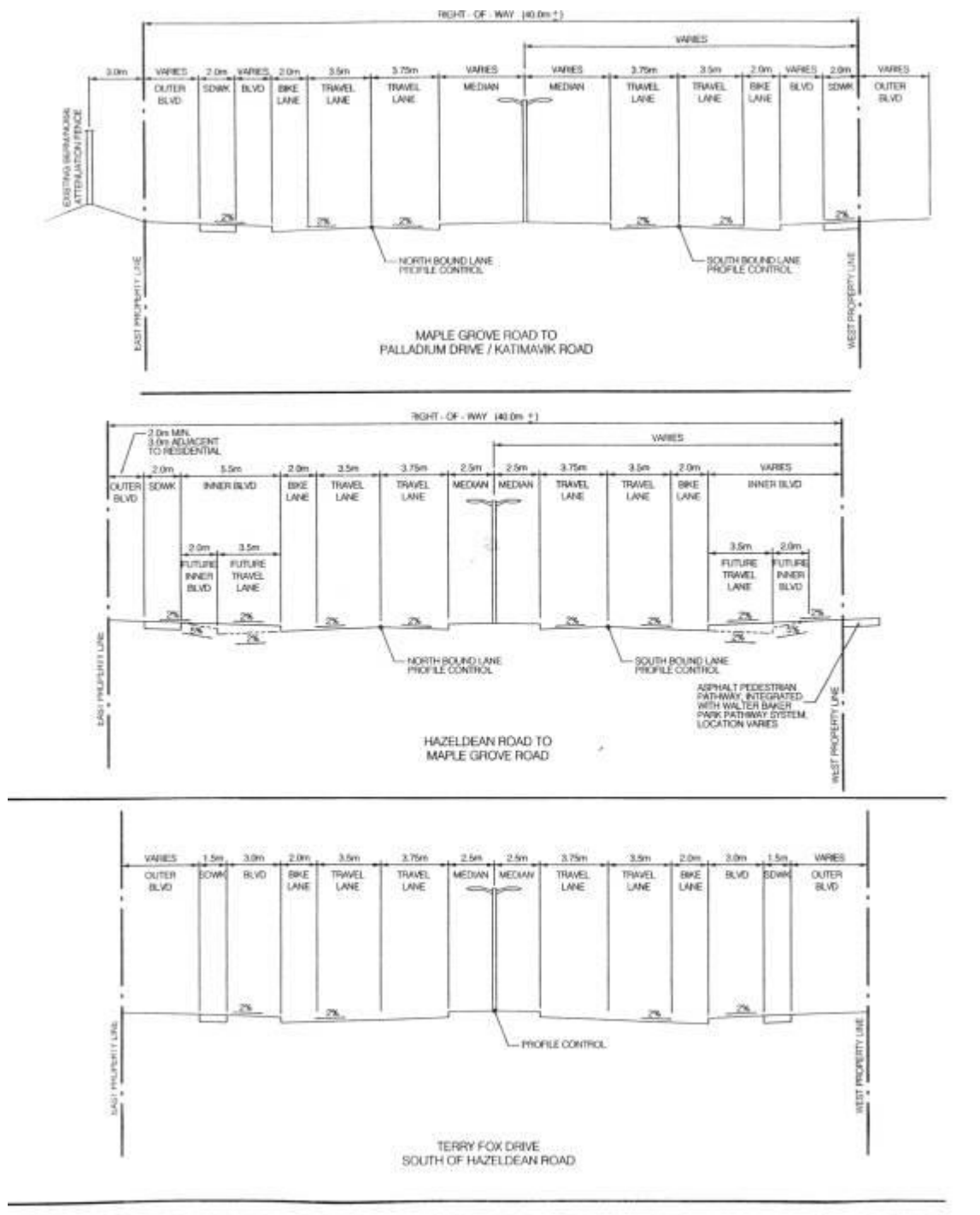
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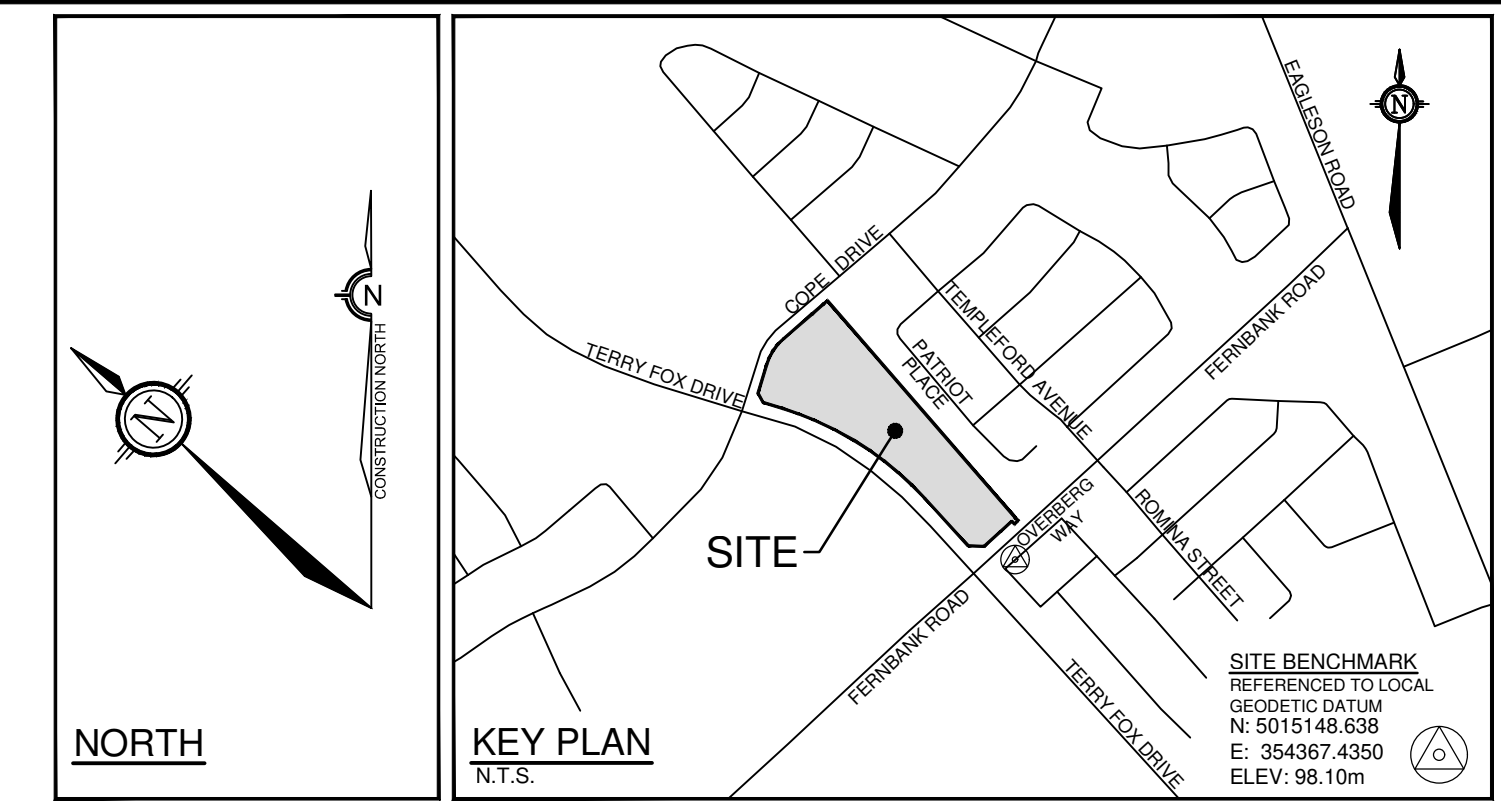
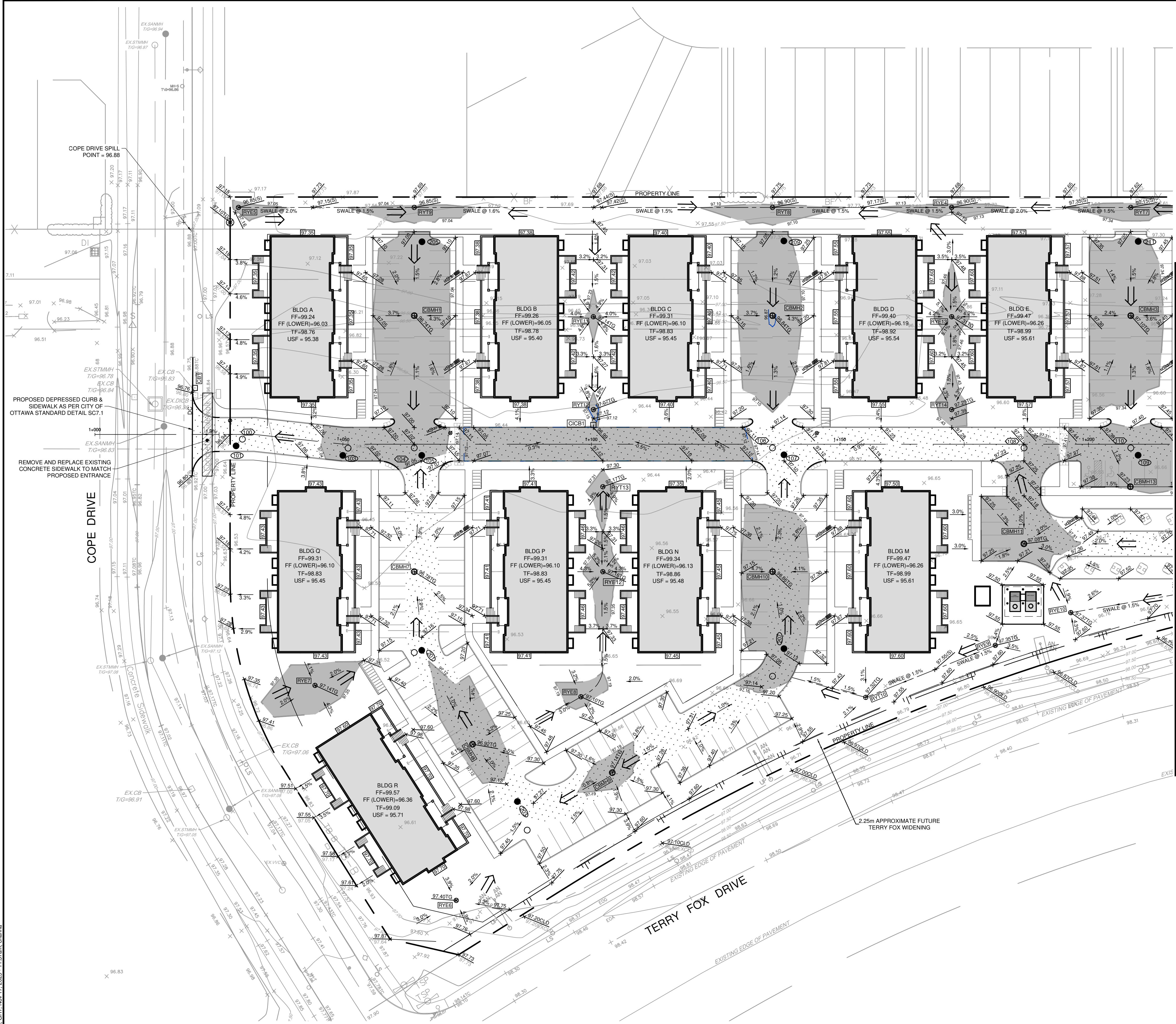
PROJECT No:
2033

A201

APPENDIX E

Terry Fox Drive Ultimate Condition Typical Cross Section
Grading Plan GR1
Grading Plan GR2





LEGEND

SITE BOUNDARY
PROPOSED ELEVATION
EXISTING ELEVATION
PROPOSED TOP OF WALL ELEVATION
PROPOSED BOTTOM OF WALL ELEVATION
PROPOSED TOP OF CURB ELEVATION
PROPOSED SWALE ELEVATION
PROPOSED TOP OF GRATE ELEVATION
PROPOSED CENTERLINE OF DITCH ELEVATION

PROPOSED RETAINING WALL
FF= FINISHED FLOOR ELEVATION
TF= TOP OF FOUNDATION ELEVATION
USF= UNDERSIDE OF FOOTING ELEVATION
MUSF= MINIMUM UNDERSIDE OF FOOTING ELEVATION
PROPOSED TERRACE ELEVATION
MAXIMUM 3:1 SIDESLOPE

PROPOSED CENTRELINE SWALE
PROPOSED GRADE AND DIRECTION
MAJOR OVERLAND FLOW ROUTE

PROPOSED HYDRANT LOCATION
TF=127.55
VVB= PROPOSED VALVE & VALVE BOX
CS= PROPOSED CURB STOP LOCATION
DMA= PROPOSED WATER CHAMBER (AS PER CITY OF OTTAWA DETAIL W3)
VVC= PROPOSED VALVE & VALVE CHAMBER (AS PER CITY OF OTTAWA DETAIL W3)
100= PROPOSED SANITARY MANHOLE
100= PROPOSED STORM MANHOLE
CB1= PROPOSED ROAD CATCHBASIN
CBMH1= PROPOSED CATCHBASIN MANHOLE
RYE1= PROPOSED REAR YARD ELBOW
RYT1= PROPOSED REAR YARD TEE
V= PROPOSED WATER METER LOCATION
R= PROPOSED REMOTE WATER METER LOCATION
PROPOSED TWSI AS PER CITY OF OTTAWA DETAIL 7.2
100YR PONDING LIMITS AND ELEVATION
1.5yr PONDING AREA AND ELEVATION

EXISTING CONTOUR LINE AND ELEVATION
EX HYD= EXISTING FIRE HYDRANT
EX SANMH= EXISTING SANITARY MANHOLE
EX STMMH= EXISTING STORMMANHOLE
VVB= EXISTING WATER VALVE
HP= EXISTING HYDRO POLE
EX CB= EXISTING CATCH BASIN

PAVEMENT STRUCTURE DETAILS
*REFER TO GEOTECHNICAL REPORT FOR SUBSURFACE CONDITIONS AND CONSTRUCTION RECOMMENDATIONS.

ACCESS LANES AND HEAVY DUTY TRUCK PARKING

- 40mm SUPERPAVE 12.5
- 50mm SUPERPAVE 19.0
- 150mm GRANULAR 'A'
- 400mm GRANULAR 'B' TYPE II
- SUBGRADE TO BE FILL, IN SITU SOIL, OR O.P.S.S. GRANULAR 'B' TYPE 1 OR 2 MATERIAL PLACED OVER IN SITU SOIL OR FILL

LIGHT DUTY PARKING

- 50mm HL3 OR SUPERPAVE 12.5
- 150mm GRANULAR 'A'
- 300mm GRANULAR 'B' TYPE II
- SUBGRADE TO BE FILL, IN SITU SOIL, OR O.P.S.S. GRANULAR 'B' TYPE 1 OR 2 MATERIAL PLACED OVER IN SITU SOIL OR FILL

NOTE:
THE POSITION OF ALL POLE LINES, CONDUITS, WATERMANS, SEWERS AND OTHER UNDERGROUND AND OVERGROUND UTILITIES AND STRUCTURES IS NOT NECESSARILY SHOWN ON THE CONTRACT DRAWINGS, AND WHERE SHOWN, THE ACCURACY OF THE POSITION OF SUCH UTILITIES AND STRUCTURES IS NOT GUARANTEED, BEFORE STARTING WORK, DETERMINE THE EXACT LOCATION OF ALL SUCH UTILITIES AND STRUCTURES AND ASSUME ALL LIABILITY FOR DAMAGE TO THEM.

No.	REVISION	DATE	BY
7.	REVISED SITE PLAN SUBMISSION	NOV 14/25	DOB
6.	RE-ISSUED FOR TENDER	JAN 18/24	DOB
5.	ISSUED FOR ADDENDUM #2	JUNE 8/22	DOB
4.	ISSUED FOR TENDER	MAY 20/22	DOB
3.	REVISED PER CITY COMMENTS	FEB 17/22	DOB
2.	REVISED PER CITY COMMENTS	NOV 5/21	DOB
1.	ISSUED FOR CITY OF OTTAWA REVIEW	JUN 2/21	DOB

SCALE
1:400
0 4 8 12 16

DESIGN
DOB

CHECKED
MSP

DRAWN
ATE

CHECKED
DOB

APPROVED
MSP

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PROFESSIONAL ENGINEER
D. D. BLAIR
100122737
NOV 14 2025
PROVINCE OF ONTARIO

NOVATECH
Engineers, Planners & Landscape Architects
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Telephone (613) 254-9643
Facsimile (613) 254-5867
Website www.novatech-eng.com

CITY OF OTTAWA
5331 FERNBANK ROAD
IRON VALLEY 2

DRAWING NAME
GRADING PLAN

PROJECT No.
121011-00

REV
REV # 6
REV # 7

DRAWING No.
121011-GR1

M:\2021\121011\CAD\Design\121011-GR.dwg, GR2, Nov 17, 2025 - 1:37am, channa

NOTE:
THE POSITION OF ALL POLE LINES, CONDUITS, WATERMANS, SEWERS AND OTHER UNDERGROUND AND OVERGROUND UTILITIES AND STRUCTURES IS NOT NECESSARILY SHOWN ON THE CONTRACT DRAWINGS, AND WHERE SHOWN, THE ACCURACY OF THE POSITION OF SUCH UTILITIES AND STRUCTURES IS NOT GUARANTEED, BEFORE STARTING WORK, DETERMINE THE EXACT LOCATION OF ALL SUCH UTILITIES AND STRUCTURES AND ASSUME ALL LIABILITY FOR DAMAGE TO THEM.

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2.	REVISED PER CITY COMMENTS	NOV 5/21	DOB
1.	ISSUED FOR CITY OF OTTAWA REVIEW	JUN 2/21	DOB

SCALE	DESIGN
1:400	DOB
1:400	MSP
1:400	ATE
1:400	DOB
1:400	MSP

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CITY OF OTTAWA
5331 FERNBANK ROAD
IRON VALLEY 2

DRAWING NAME

GRADING PLAN

PROJECT No.

121011-00

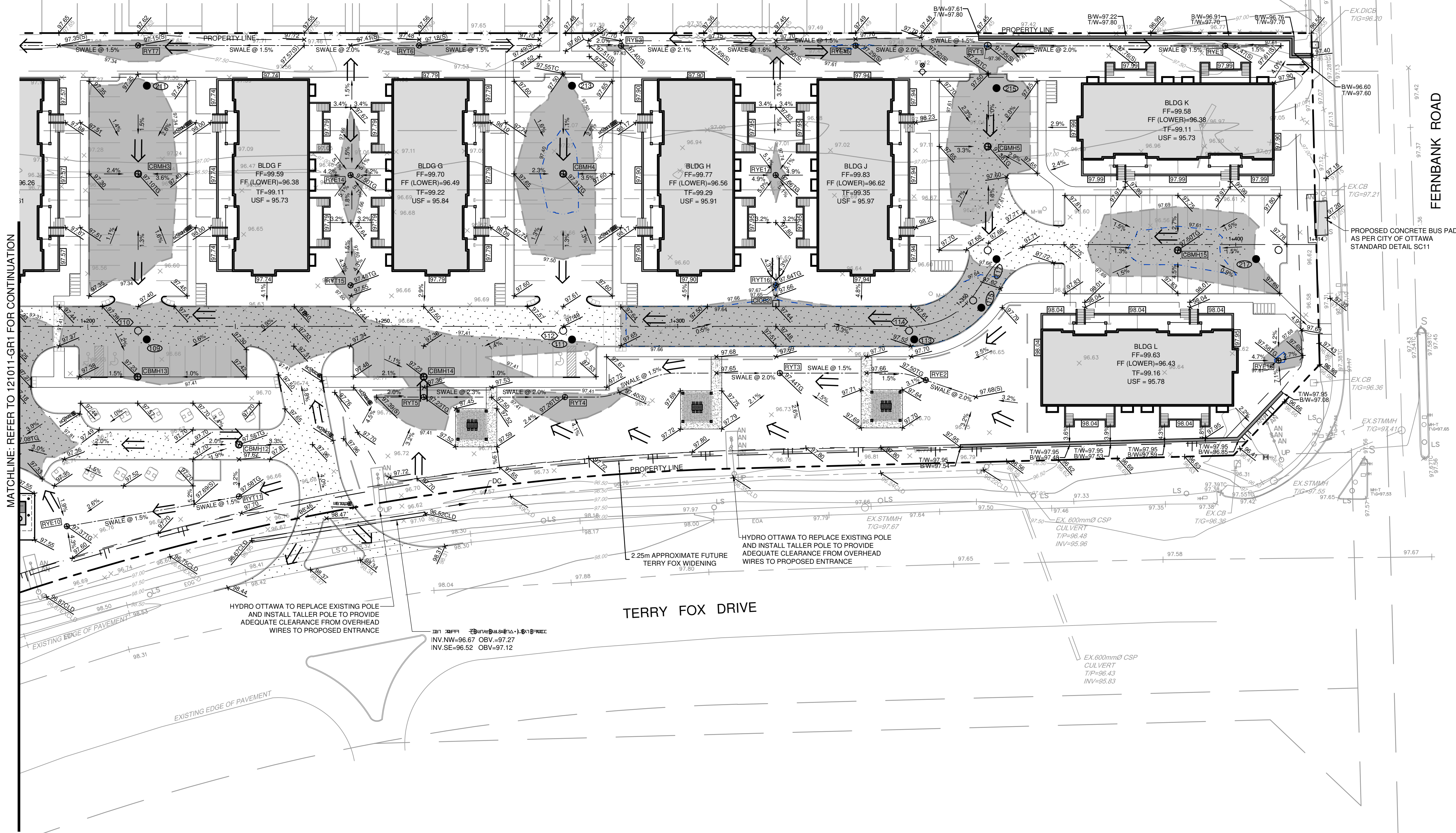
REV

REV # 7

DRAWING No.

121011-GR2

#18539



FERNBANK ROAD

NORTH

LEGEND

- SITE BOUNDARY
- PROPOSED ELEVATION
- EXISTING ELEVATION
- PROPOSED TOP OF WALL ELEVATION
- PROPOSED BOTTOM OF WALL ELEVATION
- PROPOSED TOP OF CURB ELEVATION
- PROPOSED SWALE ELEVATION
- PROPOSED TOP OF GRATE ELEVATION
- PROPOSED CENTERLINE OF DITCH ELEVATION
- PROPOSED RETAINING WALL
- FINISHED FLOOR ELEVATION
- TOP OF FOUNDATION ELEVATION
- UNDERSIDE OF FOOTING ELEVATION
- MINIMUM UNDERSIDE OF FOOTING ELEVATION
- PROPOSED TERRACE ELEVATION
- MAXIMUM 3:1 SIDESLOPE
- PROPOSED CENTRELIN SWALE
- PROPOSED GRADE AND DIRECTION
- MAJOR OVERLAND FLOW ROUTE
- PROPOSED HYDRANT LOCATION
- PROPOSED TOP OF BOTTOM FLANGE
- PROPOSED VALVE & VALVE BOX
- PROPOSED CURB STOP LOCATION
- PROPOSED WATER CHAMBER (AS PER CITY OF OTTAWA DETAIL W3)
- PROPOSED VALVE & VALVE CHAMBER (AS PER CITY OF OTTAWA DETAIL W3)
- PROPOSED SANITARY MANHOLE
- PROPOSED STORM MANHOLE
- PROPOSED ROAD CATCHBASIN
- PROPOSED CATCHBASIN MANHOLE
- PROPOSED REAR YARD ELBOW
- PROPOSED REAR YARD TEE
- PROPOSED WATER METER LOCATION
- PROPOSED REMOTE WATER METER LOCATION
- PROPOSED TWSI AS PER CITY OF OTTAWA DETAIL 7.2
- 100YR PONDING LIMITS AND ELEVATION
- 1.5yr PONDING AREA AND ELEVATION

EXISTING CONTOUR LINE AND ELEVATION

- EXISTING FIRE HYDRANT
- EXISTING SANITARY MANHOLE
- EXISTING STORMMANHOLE
- EXISTING WATER VALVE
- EXISTING HYDRO POLE
- EXISTING CATCH BASIN

PAVEMENT STRUCTURE DETAILS

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- 50mm HL3 OR SUPERPAVE 12.5
- 150mm GRANULAR 'A'
- 300mm GRANULAR 'B' TYPE II
- SUBGRADE TO BE FILL, IN SITU SOIL, OR O.P.S.S. GRANULAR 'B' TYPE 1 OR 2 MATERIAL PLACED OVER IN SITU SOIL OR FILL