



October 30, 2025

City of Ottawa
Development Review - East Branch
Planning, Development and Building Services Department
110 Laurier Ave West, 4th Floor East.
Ottawa, ON K1P 1J1

STORMWATER MANAGEMENT BRIEF: 4000 RIVERSIDE DR, OTTAWA, ON K1V 2E8

The intent of this letter is to address the Stormwater Management (SWM) strategy associated with the proposed site modification to reconfigure an existing drive-thru lane for the existing carwash and add a new drive-thru lane for a quick service restaurant for the subject site located at 4000 Riverside Drive in Ottawa, Ontario.

The existing site is approximately 0.527 ha in area and is located at the southwest quadrant of Riverside Drive and Hunt Club Road in Ottawa, ON. The site currently operates as an existing gas station with a carwash facility.

The current stormwater management onsite includes both quantity and quality controls, refer to the existing Site Services Plan prepared by Novatech Engineering Consultants Ltd and dated April 2002 located in the appendix. The quantity component is managed by a 165mm diameter orifice located at existing CBMH#3 which restricts the flow to an allowable release rate and creating storage via. surface ponding and storage within the piping and associated storm structures (CBs + MHs) prior to discharging offsite. The quality component is treated by an existing OWS (STC750) located downstream of the orifice. The treated flow will utilize existing 300mm storm outlet prior to discharging into 1350mm storm line within City Easement.

The proposed drive-thru modifications and addition will decrease overall site imperviousness by 1.0% and therefore confirming there is no increase in flow from the site as a result of the proposed modifications, refer to the comparison table below for the weighted surface runoff coefficient.

Surface Composition		Impervious	Pervious	Combined	Surface Composition		Impervious	Pervious	Combined
Proposed Condition	(m ²)	3837.00	1437.20	5274.20	Existing Condition	(m ²)	3900.80	1373.40	5274.20
	(ha)	0.384	0.144	0.527		(ha)	0.390	0.137	0.527
Runoff Coefficient		0.900	0.200	0.71	Runoff Coefficient		0.900	0.200	0.72

Table 1. Runoff Coefficients for Existing and Proposed Conditions.

Considering the existing stormwater report for the subject site is not available we have recomputed the required stormwater storage required based on the modified rational method. Based on an existing orifice size of 165mm diameter and a 100-year ponding elevation (as illustrated in the existing Site Services prepared by Novatech Engineering Consultants Ltd) a storage volume of 55.21 m³ is required and the site is able to achieve 71.38 m³ via surface ponding and underground storage within the storm network. Refer to the tables below for the storage calculation.

TOTAL STORAGE FOR UNDERGROUND PIPES				
Pipe ID	Diameter	Area	Length	Volume
	(mm)	(m ²)	(m)	(m ³)
1	300	0.07	7	0.49
2	300	0.07	36	2.54
3	300	0.07	6	0.42
4	300	0.07	19.5	5.51
5	100	0.01	2.5	0.02
6	100	0.01	2.5	0.02
7	100	0.01	2.5	0.02
8	100	0.01	2.5	0.02
9	300	0.07	23.5	1.66
10	300	0.07	20.5	1.45
11	150	0.02	4	0.07
12	300	0.07	7.5	0.53
13	300	0.07	11.5	0.81
14	300	0.07	27.5	1.94
15	300	0.07	6.5	0.46
16	300	0.07	2	0.14
17	300	0.07	25	1.77
18	300	0.07	21.5	1.52
19	300	0.07	8	0.57
20	300	0.07	9	0.64
Orifice	165	0.02	1	0.02
Sum				20.62

Table 2. Total Storage for underground storm pipes

TOTAL STORAGE FOR UNDERGROUND STRUCTURES					
Structure	Diameter	Area	Maximum.	Invert	Volume
	(mm)	(m ²)	Water level	(m)	(m ³)
EX.CB#01	600x600	0.36	101.38	100.06	0.48
CB#01	600x600	0.36	102.63	99.91	0.98
CB#02	600x600	0.36	102.44	99.43	1.08
CB#03	600x600	0.36	102.45	99.66	1.00
CBMH#01	1200	1.13	102.31	99.29	3.42
EX.CBMH#1	1200	1.13	102.14	99.89	2.54
EX.CBMH#2	1200	1.13	102.17	99.51	3.01
STM MH#1	1500	1.77	102.65	99.21	6.08
STM MH#2	1200	1.13	102.50	99.57	3.31
STM MH#3	1200	1.13	102.56	99.35	3.63
EX.STORMCEPTOR	1200	1.13	102.73	99.87	3.23
EX.STM MH2	1200	1.13	102.92	98.35	5.17
Sum					33.94

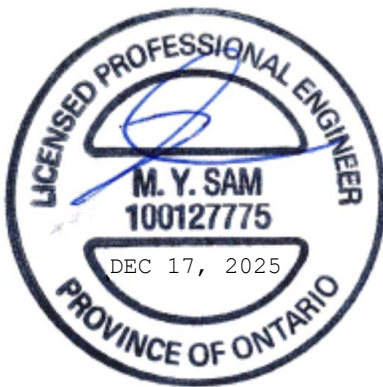
Table 3. Total Storage for underground structures (MH, CBMH, CB, OGS)

Storage Volume for 100-year Storm Event (m ³)	
Catch Basins and Manholes	33.94
Surface Ponding	16.82
Underground Conduits	20.62
Total Provided	71.38

Table 4. Total onsite storage for 100-year storm event

In conclusion, the proposed site modifications will not have an adverse impact to the existing drainage system and neighboring properties as the existing stormwater management system will be maintained for both quantity and quality purposes.

We trust that the contents of this letter meet your immediate needs. Should you have any questions or concerns regarding any aspect of this letter, or should you require any further assistance, please don't hesitate to contact our office.



James Sam, P.Eng
J and B Engineering Inc.



J+B ENGINEERING INC.
WWW.JANDB-INC.COM

APPENDIXES

APPENDIX A – STORMWATER MANAGEMENT CALCULATIONS
APPENDIX B – SITE SERVICES PREPARED BY NOVATECH ENGINEERING CONSULTANTS LTD
APPENDIX C – SITE SERVICES PREPARED



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APPENDIX A – STORMWATER MANAGEMENT CALCULATIONS

Site Location or Name City of Ottawa, ON - 4000 Riverside, Ottawa, ON			
Consultant JandB Engineering	Prepared By	David Liu	Date 15-Oct-25

VOLUMES REQUIRED WITH MODIFIED RATIONAL FORMULA

Surface Composition		Impervious	Pervious	Combined
Proposed	(m ²)	3837.00	1437.20	5274.20
Condition	(ha)	0.384	0.144	0.527
Runoff Coefficient		0.900	0.200	0.71

Surface Composition		Impervious	Pervious	Combined
Existing	(m ²)	3900.80	1373.40	5274.20
Condition	(ha)	0.390	0.137	0.527
Runoff Coefficient		0.900	0.200	0.72

St. Event	Existing	Proposed
2-Year	0.72	0.71
5-Year	0.72	0.71
10-Year	0.72	0.71
25-Year	0.79	0.78
50-Year	0.86	0.85
100-Year	0.90	0.89

Storm Event	Rainfall Intensity (mm/hr)				<Equation 1> Flow Rate (m³/sec)		
	a	b	c	I	Existing	Proposed	Excess Flow
2-Year	732.951	0.810	6.199	76.81	0.0811	0.0799	-0.0012
5-Year	998.071	0.814	6.053	104.19	0.1100	0.1084	-0.0016
10-Year	1174.184	0.816	6.014	122.14	0.1289	0.1270	-0.0019
25-Year	1402.884	0.819	6.018	144.69	0.1680	0.1655	-0.0025
50-Year	1569.580	0.820	6.014	161.47	0.2046	0.2015	-0.0031
100-Year	1735.688	0.820	6.014	178.56	0.2356	0.2321	-0.0035

Time of Concentration		
(minutes)	10.00	
Orifice	Contraction Coeff.	0.80
	Orifice Diameter	0.1650
	Gravity Constant	9.81
	Pond Elev.	102.04
	Invert Elev.	98.35
	Pressure Head	3.61
	Qallow	0.0990
	Qorif	0.1439

Storm Event	Tc	Id 100 Years	Qpost	Qpredev	Excess Flow	Volume(m³)
5 Yr Pre 100 Yr Post	5	242.7039	0.3155	0.1439	0.1716	51.474
	6	226.0101	0.2938	0.1439	0.1499	53.956
	7	211.6678	0.2751	0.1439	0.1312	55.119
	8	199.2006	0.2589	0.1439	0.1150	55.214
	9	188.2542	0.2447	0.1439	0.1008	54.432
	10	178.5590	0.2321	0.1439	0.0882	52.918
	12	162.1330	0.2108	0.1439	0.0668	48.128
	14	148.7229	0.1933	0.1439	0.0494	41.507
	16	137.5493	0.1788	0.1439	0.0349	33.493
	18	128.0828	0.1665	0.1439	0.0226	24.389
	20	119.9504	0.1559	0.1439	0.0120	14.414
	25	103.8471	0.1350	0.1439	-0.0089	-13.382
	30	91.8682	0.1194	0.1439	-0.0245	-44.087
	35	82.5786	0.1073	0.1439	-0.0366	-76.794
	40	75.1453	0.0977	0.1439	-0.0462	-110.955
	45	69.0504	0.0898	0.1439	-0.0542	-146.216
	50	63.9541	0.0831	0.1439	-0.0608	-182.336
	55	59.6238	0.0775	0.1439	-0.0664	-219.146
	Max Volume Required cum					55.21

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EX.CBMH#1	1200	1.13	102.14	99.89	2.54
EX.CBMH#2	1200	1.13	102.17	99.51	3.01
STM MH#1	1500	1.77	102.65	99.21	6.08
STM MH#2	1200	1.13	102.50	99.57	3.31
STM MH#3	1200	1.13	102.56	99.35	3.63
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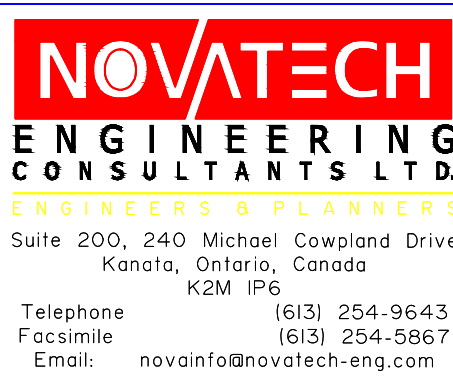
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APPENDIX B – SITE SERVICES PREPARED BY NOVATECH ENGINEERING CONSULTANTS LTD



7.	ISSUED FOR CONSTRUCTION	SEPT. 11/03	MER
No.	REVISION	DATE	BY

7.	REVISED PER TENDER ADDENDUM #1	MAY 12/03	MER
6.	ISSUED FOR PHASE 1 TENDER	MAY 2/03	MER
5.	REVISED PER CITY COMMENTS/ISSUED FOR MOE	FEB 28/03	MER
4.	ISSUED FOR APPROVAL	DEC 02/02	MER
3.	REVISED PER CITY COMMENTS	OCT 29/02	MER
2.	REVISED PER SWM REPORT	JUNE 7/02	JGR
1.	ISSUED FOR SITE PLAN APPLICATION	MAY 1/02	JGR
No.	REVISION	DATE	BY












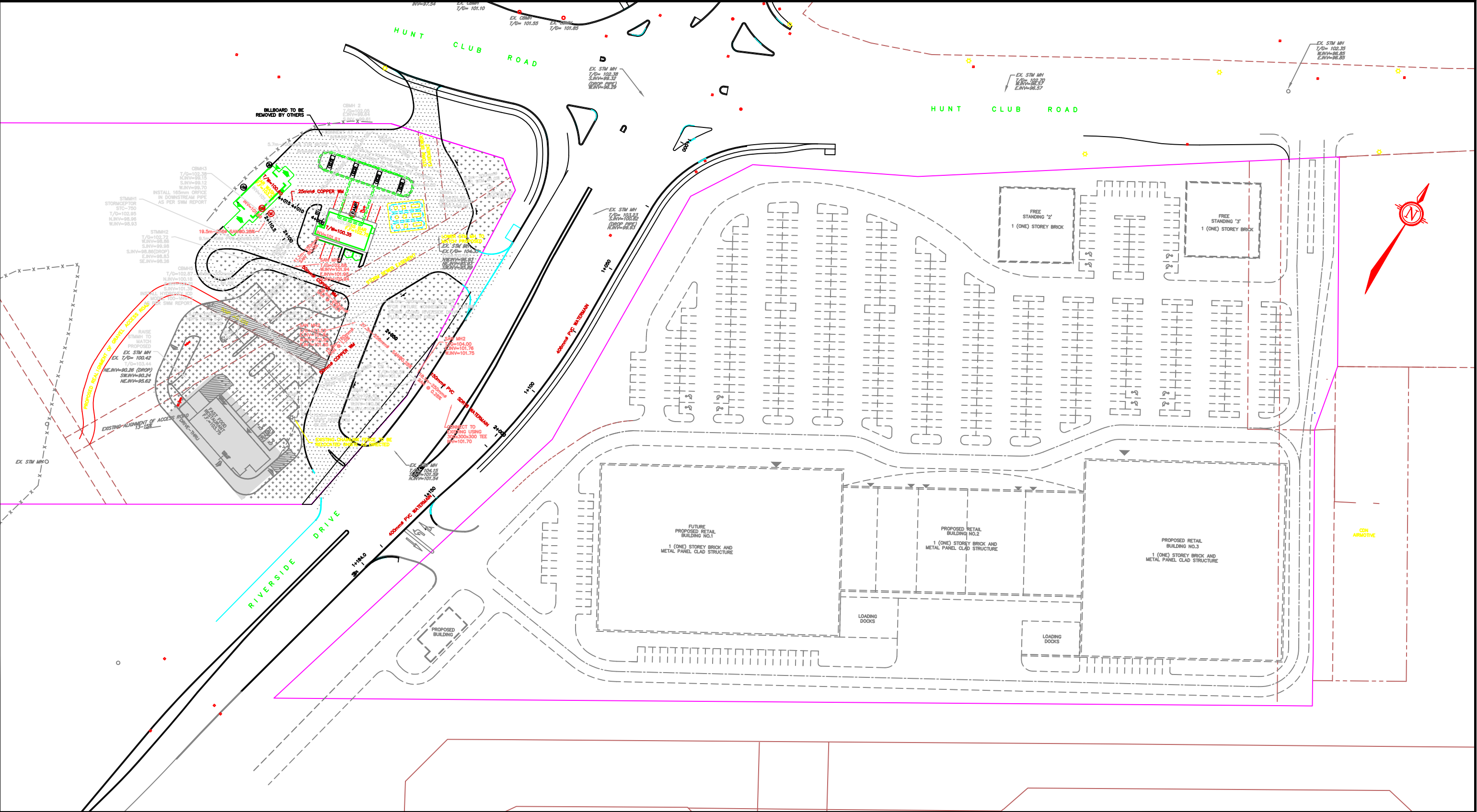
DESIGN	MER	SCALE
CHECKED	JGR	1:500
DRAWN	SAM	
CHECKED	MER	
APPROVED	JGR	

PROJECT No.	101048
DATE	APRIL 2002
DRAWING No.	101048-GP

WATERMAIN TABLE				RESTRAINING RINGS (AS PER W 25.5 AND W25.6)	THRUST BLOCK (AS PER W 25.3 AND W25.4)
STATION	SURFACE ELEVATION	TOP OF WATERMAIN ELEVATION	DESCRIPTION		
2+000.0	104.01	101.61	400x400x150 TEE	AS PER 101048-P1	AS PER 101048-P1
2+016.0	104.17	101.77	22.5" VERTICAL BEND	ALL JOINTS WITHIN 6m	—
2+017.0	104.17	101.40	22.5" VERTICAL BEND	ALL JOINTS WITHIN 6m	—
2+018.2	104.17	101.40	SAN CROSSING (INV.=101.70)	—	—
2+019.5	104.17	101.40	VPI	—	—
2+022.0	104.17	101.40	22.5" VERTICAL BEND	ALL JOINTS WITHIN 6m	—
2+023.0	104.17	101.13	22.5" VERTICAL BEND	ALL JOINTS WITHIN 6m	—
2+024.4	104.17	101.13	STM CROSSING (INV.=101.47)	—	—
2+024.4	104.17	101.13	22.5" VERTICAL BEND	ALL JOINTS WITHIN 6m	—
2+025.4	104.17	101.62	22.5" VERTICAL BEND	ALL JOINTS WITHIN 6m	—
2+029.1	104.02	101.62	V&VB	ALL JOINTS WITHIN 9m	—
2+046.0	102.75	100.35	LOW POINT=-11.25" VERTICAL BEND	ALL JOINTS WITHIN 6m	—
2+055.7	103.75	101.35	HYDRANT TEE	ALL JOINTS WITHIN 3m	A=350 (HYDRANT AS PER W-19)
2+057.0	103.60	101.20	50mmø SERVICE	—	—
2+058.0	103.50	101.10	150mm TO 50mm REDUCER	ALL JOINTS WITHIN 6m	—
2+063.0	103.48	101.08	V&VB	—	—
2+092.5	102.75	100.35	WM BEND	—	—
2+110.5	103.00	100.60	1.0m FROM BUILDING FACE	—	—
3+000.00	103.60	101.20	SERVICE FROM 150mm MAIN	—	—
3+006.00	103.70	101.30	V&VB	—	—
3+024.00	103.65	101.25	VERTICAL BEND	—	—
3+025.50	103.65	100.53	VERTICAL BEND	—	—
3+027.00	103.65	100.53	STM CROSSING (INV.=100.78)	—	—
3+028.50	103.65	100.53	VERT BEND	—	—
3+030.00	103.65	101.25	VERTICAL BEND C/W TEMP CAP	—	—
3+050.00	103.65	101.25	FUTURE	—	—
3+056.02	103.75	101.35	FUTURE WM CAPPED 1m FROM BLDG.	—	—
4+000.00	102.75	100.35	WM CAPPED 1m FROM BLDG.	—	—
4+011.00	102.33	99.93	V&VB	—	—
4+015.00	103.00	100.60	WM CAPPED 1m FROM BLDG.	—	—

200mm	PROPOSED WATERMAIN AND DIAMETER
—	PROPOSED VALVE LOCATION
V&VB	VALVE & VALVE BOX
HD	PROPOSED HYDRANT C/W VALVE & LEAD
T/F=98.45	PROPOSED TOP OF BOTTOM FLOOD
BEND	PROPOSED BEND AND THRUSTBLOCK
11:1	11.25', 22.5', 45' or TEE (SEE PLAN AND PROFILES)
100'	PROPOSED STORM MH & SEWER
CB 2	PROPOSED ROAD CATCHBASIN
CBMH 2	PROPOSED CATCHBASIN MANHOLE
☀	PROPOSED STREETLIGHT

200mm <i>WM</i>	EXISTING WATERMAIN
	SILT FENCE
	PROPOSED DEPRESSED CURB
DC	
	WATER METER
	REMOTE METER
	CAUTION SIGN WARNING OF PONDING DURING STORM EVENTS
	PREPARE SUBGRADE TO FINISHED GRADE LESS 0.50m
	PREPARE LANDSCAPE AREAS TO FINISHED GRADE LESS 0.10m
	PREPARE PAD AT 103.10m
	LEAVE FLAT AT 103.00m



NOVATECH

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K2M 1P6

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Facsimile (613) 254-5867
Email: novainfo@novatech-eng.com

RUNWAY CENTRE

CONCEPTUAL DEVELOPMENT PLAN

MAY 20021:1250101048-FIG1



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APPENDIX C – SITE SERVICES PREPARED

